

PRELIMINARY WATER QUALITY MANAGEMENT PLAN (WQMP)

FOR: **IDI ECKHOFF** ECKHOFF STREET ORANGE, CA 92868

PREPARED FOR: **IDI ECKHOFF ORANGE LLC** 840 APOLLO STREET, SUITE 343 EL SEGUNDO, CA 90245 PHONE: (213) 330-8066

> MARCH 26, 2021 AUGUST 10, 2021 OCTOBER 15, 2021 APRIL 4, 2022 NOVEMBER 3, 2022

> > JOB NO. 3910

PREPARED BY: **THIENES ENGINEERING** 14349 FIRESTONE BLVD. LA MIRADA, CALIFORNIA 90638 PHONE: (714) 521-4811 FAX: (714) 521-4173 CONTACT: LUIS PRADO (luisp@thieneseng.com)



PRELIMINARY WATER QUALITY MANAGEMENT PLAN (WQMP)

For: IDI Eckhoff Eckhoff Street Orange, CA 92868

Prepared for: IDI Eckhoff Orange LLC 840 Apollo Street, Suite 343 El Segundo, CA 90245 (213) 330-8066

Prepared by: Thienes Engineering, Inc. Engineer: Reinhard Stenzel Registration No. 56155 14349 Firestone Blvd. La Mirada, CA 90638 (714) 521-4811 Contact: Luis Prado (luisp@thieneseng.com) Job No. 3910

> 1st Submittal: March 26, 2021 2nd Submittal: August 10, 2021 3rd Submittal: October 15, 2021 4th Submittal: April 4, 2022 5th Submittal: November 3, 2022



Public Works Director

Date

City Engineer

Date

OWNER'S CERTIFICATION

WATER QUALITY MANAGEMENT PLAN

FOR

IDI Eckhoff

This Water Quality Management Plan (WQMP) for the **IDI Eckhoff** has been prepared for **IDI Eckhoff Orange LLC**. This WQMP is intended to comply with the requirements of the City of Orange's **Parcel Map #XX** requiring preparation of a Water Quality Management Plan.

The undersigned, while it owns the subject property, is responsible for the implementation of the provisions of this plan and will ensure that this plan is amended as appropriate to reflect up-to-date conditions on the site consistent with the City of Orange Local Implementation Plan (LIP), and the intent of NPDES Permit and Waste Discharge Requirements for the City of Orange, County of Orange, Orange County Flood Control District and the incorporated Cities of Orange County within the Santa Ana Region.

This WQMP will be reviewed with the facility operator, facility supervisors, employees, tenants, maintenance and service contractors, or any other party having responsibility for implementing portions of this WQMP. Maintenance requirements within Section V and Appendix D will be adhered to with particular emphasis on maintaining the BMPs described within Sections IV and V. The Owner's Annual Self Certification Statement along with a BMP maintenance implementation table will be submitted by June 30th every year following project completion. At least one copy of the approved WQMP shall be available on the subject property in perpetuity.

Once the undersigned transfers its interest in the property, its successors-in-interest shall bear the aforementioned responsibility to implement and amend the WQMP. The City of Orange will be notified of the change of ownership and the new owner will submit a new certification.

Signature:		Date:
Name:	Charles McPhee	
Title:	Sr. VP and Regional Director	
Company:	IDI Eckhoff Orange LLC	
Address:	840 Apollo Street, Suite 343, El Seg	gundo, CA 90245
Telephone Number:	(213) 330-8066	

Notice of Transfer of Responsibility

Water Quality Management Plan (WQMP)

WQMP Number – As assigned by the City of Orange:_____

Submission of this Notice of Transfer of Responsibility constitutes notice to the City that responsibility for the Water Quality Management Plan (WQMP) for the subject property identified below, and implementation of that plan, is being transferred from the Previous Owner (and his/her agent) of the site (or portion thereof) to the New Owner, as further described below.

I. <u>Previous Owner/ Responsible Party Information</u>

Company/Individual:	IDI Eckhoff Orange LLC	Contact Person:	Charles McPhee
Street Address:	840 Apollo Street	Title:	Sr. VP and
	Suite 343		Regional Director
City, State and Zip:	El Segundo, CA 90245	Phone:	(213) 330-8066

II. Information about Site Relevant to WQMP

Name of Project:	IDI Eckhoff
Title of WQMP applicable to site:	Water Quality Management Program for Eckhoff Street
	Proposed Buildings
Street Address of the site:	XX Eckhoff Street, Orange, CA 92868
Date of Transfer of Responsibility:	

III. <u>New Owner/ Responsible Party Information</u>

Company/Individual:	Contact Person:	
Street Address:	Title:	
City, State and Zip:	Phone:	

Table of Contents

I.	Discretionary Permit Number(s), Water Quality Condition Number(s) and Conditions					
II.	Project Description	3				
III.	Site Description	7				
IV.	Best Management Practices	9				
V.	 IV.1 Site Design BMPs IV.2 Source Control BMPs IV.3 Low Impact Development BMP Selection IV.4 Water Quality Credits IV.5 Alternative Compliance Plan IV.6 Vector Control IV.7 Drainage Management Areas IV.8 Calculations 	10 11 15 21 21 21 21 22				
v.	Implementation, Maintenance and Inspection Responsibility for BMPs (O&M Plan)	23				
VI.	Location Map, Site Plan, and BMP Details	32				
VII.	II. Educational Materials					
Арр	endices					
	Conditions of Approval, Resolution Number dated Educational Material					

- C. BMP Details
- D. BMP Maintenance Information
- E. Infiltration Feasibility (for reference only)
- F. Hydrology Information (for reference only)

List of Tables

Table 1	Site Design BMPs	10
Table 2	Routine Non-Structural BMPs	11
Table 3	Routine Structural BMPs	13
Table 4	Hydrologic Source Control BMPs	15
Table 5	Infiltration BMPs	16
Table 6	Evapotranspiration, Rainwater Harvesting	17
Table 7	Biotreatment BMPs	18
Table 8	Frequency Inspection Matrix	21

I. Discretionary Permit Number(s), Water Quality Condition Number(s) and Conditions of Approval

Tract No. XXX

Lot No. XX

GPS Coordinates (Google Maps): 33.800435, -117.872793

Water Quality Conditions (WQMP conditions listed below)

A complete copy of the signed Conditions of Approval, Resolution Number _____ dated ______ are included as Appendix A

All water quality conditions related to the project will be added in the Final WQMP after approval by City and governing body.

Conditions of Approval:

Insert text providing the discretionary permit numbers and the conditions of approval related to water quality (stated verbatim).

Conditions of approval pending.

Prior to the issuance of any grading permits the applicant shall submit a Project WQMP for review and approval to the Public Works Department that:

- Prioritizes the use of Low Impact Development principles as follows: preserves natural features; minimizes runoff and reduces impervious surfaces; and utilizes infiltration of runoff as the method of pollutant treatment. Infiltration BMPs to be considered include the use of permeable materials such as concrete and concrete pavers, infiltration trenches, infiltration planters, and other infiltration BMPs as applicable.
- Incorporates the applicable Routine Source and Structural Control BMPs as defined in the Drainage Area Management Plan (DAMP)
- Maintains the hydrologic characteristics of the site by matching time of concentration, runoff, velocity, volume and hydrograph for a 2-year storm event.
- Minimizes the potential increase in downstream erosion and avoids downstream impacts to physical structures, aquatic and riparian habitat.
- Generally describes the long-term operation and maintenance requirements for structural and Treatment Control BMPs
- Identifies the entity or employees that will be responsible for long-term operation, maintenance, repair and or replacement of the structural and Treatment Control BMPs and the training that qualifies them to operate and maintain the BMPs

- Describes the mechanism for funding the long-term operation and maintenance of all structural and Treatment Control BMPs.
- A copy of the forms to be used in conducting maintenance and inspection activities
- Recordkeeping requirements (forms to be kept for 5 years)
- A copy of the form to be submitted annually by the project owner to the Public Works Department that certifies that the project's structural and treatment BMPs are being inspected and maintained in accordance with the project's WQMP.

Prior to the issuance of certificates for use of occupancy, the applicant shall demonstrate the following to the Public Works Department:

- That all structural and treatment control best management practices (BMPs) described in the Project WQMP have been constructed and installed in conformance with the approved plans and specifications,
- That applicant is prepared to implement all non-structural BMPs described in the Project WQMP,
- That an adequate number of copies of the project's approved final Project WQMP are available for the future occupiers.

Prior to the issuance of certificates for use of occupancy or final signoff by the Public Works Department, the applicant shall demonstrate to the satisfaction of Public Works, that the preparer of the WQMP has reviewed the BMP maintenance requirements in Section V of the WQMP with the responsible person and that a copy of the WQMP has been provided to that person. A certification letter from the WQMP preparer may be used to satisfy this condition.

The project applicant shall maintain all structural, treatment and low impact development BMPs at the frequency specified in the approved water quality management plan (WQMP). Upon transfer of ownership or management responsibilities for the project site, the applicant shall notify the City of Orange Public Works Department of the new person(s) or entity responsible for maintenance of the BMPs.

II. Project Description

Planning Area: LI Light Industrial

Project Size (ac): 12.7 acres onsite and 1.20 acres of offsite run-on

Percent Change in Impermeable Surfaces: 9% decrease

SIC Code: 4225 – General Warehousing

Project Description

*P*roposed improvements consist of two warehouse type buildings. Building 1 is the westerly building and Building 2 is the easterly building. Each building has a truck yard area and vehicle parking around the site. There is landscaping adjacent to Eckhoff Street and smaller areas throughout the project site.

Three (3) flow-based proprietary biofiltration BMPs (Modular Wetlands Systems), with catch basin filter inserts for pretreatment, are used to address water quality requirements. Two of the three systems are located on the north and south sides of Building 1 and the third system is located on the south side of Building 2.

There is no outdoor storage on the project and no food preparation, cooking or eating area. There are no activities that are routinely conducted outdoors (ie. vehicle maintenance and associated activities).

Project Purpose and Activities

The project currently consists of two empty shell buildings with no tenant in mind during the preparation of this WQMP. However, the anticipated use would be for warehousing of finished goods and/or used for light industrial activities. If the future tenant's business operations do not align themselves with this WQMP then an addendum to the WQMP will be required and specific tenant improvements may be necessary.

Potential Storm Water Pollutants

Potential Storm Water Pollutants						
Pollutant	Circle One: E=Expected to be of concern N=Not Expected to be of concern		Additional Information and Comments			
Suspended-Solid/ Sediment	E	N	Potentially expected due to landscaping			
Nutrients	E	N	Potentially expected due to landscaping			
Heavy Metals	Е	N	Expected due to vehicles			
Pathogens (Bacteria/Virus)	Е	N	Potentially expected due to uncovered parking areas			
Pesticides	E	N	Potentially expected due to landscaping			
Oil and Grease	Е	N	Expected due to vehicles			
Toxic Organic Compounds	E		Expected due to solvents			
Trash and Debris	E	X	Expected			

2 year, 24-hr Storm Event								
Flowrate (cfs) Volume (cu-ft) Time of Concentration (min)								
Pre-Development	20.6	74,257	9.0					
Post-Development 18.4 74,305 9.5								
Difference (%)	-10.68%	+0.06%	+5.55%					

Hydrologic Conditions of Concern

The 2-year, 24-hr storm event in proposed conditions does not change significantly compared to existing conditions since the site was already developed. In the proposed conditions, the storm volume will increase by 0.068% which is within the allowable 5% change. The time of concentration will increase by 5.55% which is generally allowable seeing as a longer time of concentration typically results in lower hydromodification impact. The peak flowrate has been reduced by 10.68% which also has a lower hydromodification impact.

The project is also exempt from HCOCs. See Attachment F for map of susceptibility analysis of the Santa Ana River.

Post Development Drainage Characteristics

Drainage from the project will surface flow into catch basins utilizing filter inserts for pretreatment. Filter inserts have 100% removal of trash and debris, meeting full capture requirements. Additionally, the filter is equipped with a floating hydrocarbon boom used to control and absorb oil and hydrocarbons. After pretreatment, the proposed onsite storm drain will direct runoff towards sump pumps. The sump pumps will then convey runoff into the MWS systems (primary BMPs) for treatment. The MWS' treatment capacities will exceed the stormwater quality design flowrate (SQDF); therefore, the MWS systems will utilize internal bypass weirs to discharge flows greater than the SQDF to the MWS' discharge chamber to outlet. Treated flows will be conveyed back to the main storm drain lines.

Proposed drainage conditions will alter the existing condition drainage patterns as well as drainage divides shown in the City's Master Plan of Drainage. The tributary runoff to Eckhoff Street will be reduced, thus providing relief to the street and downstream facilities. An onsite storm drain system is proposed to direct the majority of the project site easterly to a proposed storm drain in Poplar Street. This storm drain will continue southerly and connect to the existing 54" storm drain system. The site's runoff will ultimately discharge into Santa Ana River, Reach 2.

Santa Ana River, Reach 2 is a stabilized earthen channel not susceptible to Hydrologic Conditions of Concern (HCOC). See Attachment F for map of susceptibility analysis of the Santa Ana River.

The proposed project will not affect offsite drainage characteristics as the downstream MS4 is fully developed and managed.

Commercial Projects

N/A

Residential Projects

N/A

Site Ownership and any Easements

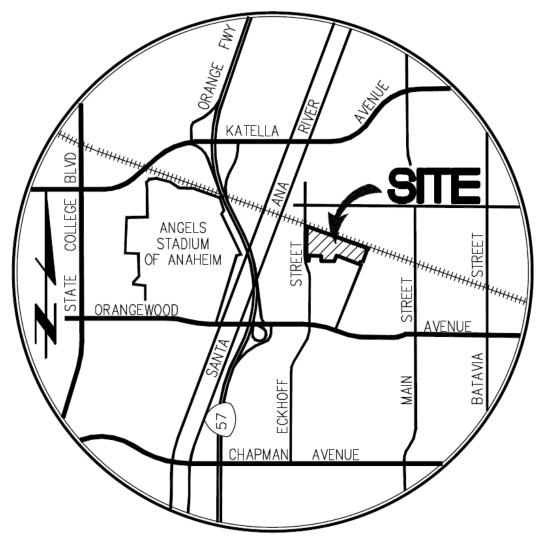
Owner Information:

IDI Eckhoff Orange LLC 840 Apollo Street, Suite 343 El Segundo, CA 90245 (213) 330-8066 Contact: Charles McPhee, Sr. VP and Regional Director

No easements by others.

III. Site Description

Reference Location Map:



Site Address: XX Eckhoff Street, Orange, CA 92868

Zoning: M-1

Predominant Soil type: A

Pre-project percent pervious: 1% Post-project percent pervious: 10%

Pre-project percent impervious: 99%

Post-project percent impervious: 90%

Site Characteristics

The project site is an existing commercial/industrial development consisting of several large buildings and various smaller structures, sheds and storage areas. Existing drainage patterns differ from the City's Master Plan of Drainage.

The site is generally flat and lies on type A soils. Per the site-specific Geotechnical Investigation attached in Appendix E, measured infiltration rates resulted in 21.60 in/hr, 2.50 in/hr, and 1.80 in/hr. Additionally, groundwater was not encountered at any of the borings. Based on the lack of any water within the borings, and the moisture contents of the recovered soil samples, the static groundwater table is considered to have existed at a depth in excess of 50 feet below existing site grades, at the time of the subsurface investigation.

Although infiltration BMPs are feasible from a geotechnical standpoint, per email correspondence with the City of Orange, the Orange County Water District (OCWD) does not recommend introducing (infiltrating) stormwater into the larger groundwater table near the site. OCWD has made this finding based on concerns from historical uses on the sites that are in the vicinity and up-gradient of the proposed project. Refer to the email correspondence in Appendix E.

Watershed Characteristics

Watershed: Lower Santa Ana Watershed

Downstream Receiving Waters:

Santa Ana River, Reach 2 via the County of Orange's Bitterbush Channel

Water Quality Impairments (if applicable):

Santa Ana River, Reach 2: None

Identify hydromodification susceptibility:

An onsite storm drain system is proposed to direct the majority of the project site easterly to a proposed storm drain in Poplar Street. This storm drain will continue southerly and connect to the existing 54" storm drain system. The site's runoff will ultimately discharge into Santa Ana River, Reach 2.

Santa Ana River, Reach 2 is a stabilized earthen channel not susceptible to Hydrologic Conditions of Concern (HCOC). See Attachment F for map of susceptibility analysis of the Santa Ana River.

The proposed project will not affect offsite drainage characteristics as the downstream MS4 is fully developed and managed.

Identify watershed management priorities:

N/A

IV. Best Management Practices

The project does not utilize HSCs or infiltration BMPs. Instead, the project proposes to treat the SQDF via flow-based proprietary biofiltration BMPs (MWS) that are suitable for the proposed light industrial warehouses.

LID BMPs must be selected based on a hierarchy of controls and sized to capture the maximum feasible portion of the DCV using the higher priority type control (e.g., retention), before attempting to address the remaining volume with the next lower priority control (biotreatment). Per email correspondence with the City of Orange (see Appendix E), the Orange County Water District (OCWD) does not recommend introducing (infiltrating) stormwater into the larger groundwater table near the site. OCWD has made this finding based on concerns from historical uses on the sites that are in the vicinity and up-gradient of the proposed project. Based on this, it is infeasible to retain any of the DCV and instead biotreatment BMPs are utilized.

IV.1 Site Design and Drainage Characteristics

Table 1

Site Design BMPs

Technique	Included?		Tf no state instification		
Technique	Yes No		If no, state justification.		
Minimize Directly Connected Impervious Areas (DCIAs) (C-Factor Reduction)		x	The project is designed for the storage of finished goods (indoors), truck trailer parking, and by design maximizes impervious areas.		
Create Reduced or "Zero Discharge" Areas (Runoff Volume Reduction) ¹		x			
Minimize Impervious Area/Maximize Permeability (C-Factor Reduction) ²	x				
Conserve Natural Areas (C-Factor Reduction)		x	Not applicable, there are no natural areas to conserve.		

1 Detention and retention areas incorporated into landscape design provide areas for retaining and detaining stormwater flows, resulting in lower runoff rates and reductions in volume due to limited infiltration and evaporation. Such Site Design BMPs may reduce the size of Treatment Control BMPs.

- 2 The "C Factor" is a representation of the ability of a surface to produce runoff. Surfaces that produce higher volumes of runoff are represented by higher C Factors. By incorporating more pervious, lower C Factor surfaces into a development, lower volumes of runoff will be produced. Lower volumes and rates of runoff translate directly to lowering treatment requirements.
 - Minimize Directly Connected Impervious Areas: The project will minimize directly connected impervious areas by capturing and conveying stormwater from impervious areas to the MWS systems prior to discharging offsite and entering the public storm drain Poplar Street.
 - Minimize Impervious Area/Maximize Permeability: Although the project by use/design is for maximum warehouse storage (indoors) and truck trailer parking, the layout of the site was adjusted to ensure that perimeter landscape was achieved, and that all drainage could reach the BMPs onsite.

IV.2 Source Control BMPs

IV.2.1 Routine Non-Structural BMPs

Table 2

Routine Non-Structural BMPs

		Che	ck One	The strength ship
BMP No.	Name	Included	Not Applicable	If not applicable, state brief reason.
N1	Education for Property Owners, Tenants and Occupants	x		
N2	Activity Restriction	x		
N3	Common Area Landscape Management	x		
N4	BMP Maintenance	x		
N5	Title 22 CCR Compliance		x	Not applicable, no hazardous waste anticipated onsite.
N6	Local Water Quality Permit Compliance		x	This BMP is not applicable. The City of Orange does not issue water quality permits.
N7	Spill Contingency Plan	x		
N8	Underground Storage Tank Compliance		x	Not applicable, no UST proposed.
N9	Hazardous Materials Disclosure Compliance		x	Not applicable on the site
N10	Uniform Fire Code Implementation	X		
N11	Common Area Litter Control	x		
N12	Employee Training	X		
N13	Housekeeping of Loading Docks	X		
N14	Common Area Catch Basin Inspection	x		
N15	Street Sweeping Private Streets and Parking Lots	X		

- N1 Education for Property Owners, Tenants and Occupants: Property owner will familiarize him/herself with the educational materials in Appendix B and the contents of the WQMP. Practical information materials will be provided on general housekeeping practices that contribute to the protection of stormwater quality.
- **N2** Activity Restrictions: No outdoor work areas, processing, storage or wash areas. No maintenance of any vehicles. All activities must remain in compliance with the OMC at all times.

- N3 Common Area Landscape Management: Maintenance personnel responsible for the activities that may impact water quality shall undergo certified BMP training and educational programs. Irrigation must be consistent with the City of Orange Landscape & Water Efficiency Ordinance. Fertilizer and pesticide usage will be consistent with EPA, DAMP, and manufacturer's Management Guidelines for Use of Fertilizers and Pesticides. IPM (integrated pest management) strategies will be implemented when applicable.
- **N4** BMP Maintenance: BMPs will be routinely inspected and maintained in order to preserve the functionality of each BMP. BMP maintenance, implementation schedules, and responsible parties are included in Section V.
- **N10** Uniform Fire Code Implementation: Owner will comply with Article 80 of the Uniform Fire Code enforced by the fire protection agency. The facility operators will be educated annually regarding requirements for handling, storage and proper disposal of hazardous substances.
- **N11** Common Area Litter Control: Owner will contract with their landscape maintenance firm to provide this service during regularly schedule maintenance. They are required to implement weekly trash management and litter control procedures in the parking lot aimed at reducing pollution of drainage water.
- **N12** Employee Training: The owner will ensure that employees are familiar with activities that impact water quality and BMPs to be used in conducting those activities. Owner will review all educational materials at least once a year and obtain new or updated educational materials to use these materials to train employees. Employees shall participate in ongoing maintenance. The WQMP requires annual employee training and new hires within 2 months.
- **N13** Housekeeping of Loading Docks: Loading docks must be swept regularly for trash, debris, and sediment. Docks will not be hosed down. Absorbent will be used for cleanup of small spills. Used absorbent will be properly disposed of.
- N14 Common Area Catch Basin Inspection: Clear of trash, debris, and any accumulated sediment. Inspections will be conducted annually by October 1st (at minimum) and following any rain events.
- **N15** Street Sweeping Private Streets and Parking Lots: All landscape maintenance contractors will be required to sweep up all landscape cuttings, mowings and fertilizer materials off paved areas and dispose of properly. Parking areas and drive ways will be swept weekly by sweeping contractor, or more often as needed.

IV.2.2 Routine Structural BMPs

Table 3

Routine Structural BMPs

	Che	ck One	Tf not applicable, state brief
Name	Included	Not Applicable	If not applicable, state brief reason
Provide storm drain system stenciling and signage- "No Dumping – Drains to Ocean"	x		
Design and construct outdoor material storage areas to reduce pollution introduction		x	Not applicable, no outdoor storage is proposed.
Design and construct trash and waste storage areas to reduce pollution introduction	x		
Use efficient irrigation systems & landscape design	x		
Protect slopes and channels and provide energy dissipation		x	Not applicable, no slopes or channels proposed.
Incorporate requirements applicable to individual project features			
a. Dock areas	X		
b. Maintenance bays		x	Not applicable, no maintenance bays proposed.
c. Vehicle or community wash areas		x	Not applicable, vehicles wash areas are not proposed.
d. Outdoor processing areas		x	Not applicable, outdoor processing areas are not proposed.
e. Equipment wash areas		x	Not applicable, equipment wash areas are not proposed.
f. Fueling areas		x	Not applicable, fueling areas are not proposed.
g. Hillside landscaping		x	Not applicable, there are no hillsides onsite.
h. Wash water control for food preparation areas		x	Not applicable, there are no food preparation areas onsite.

- Storm drain system stenciling will contain a brief statement that prohibits the dump of improper materials into the municipal storm drain system.
- Trash enclosures will be paved with an impervious surface, designed not to allow run-on, walled to prevent off-site transport of trash, and roofed to prevent direct precipitation.
- Irrigation is proposed to meet the intent of efficient design by employing rain shutoff devices, landscape area's specific water requirements, shutoff valves, landscape plan consistent with Planning and Community Services standards for landscape and water use efficiency, timing application, plant similarity grouping, and mulch.

• Loading docks are designed aboveground and the anticipated materials loaded/unloaded are expected to be finished goods which do not have the potential to contribute to stormwater pollution.

IV.3 Low Impact Development BMP Selection

IV.3.1 Hydrologic Source Controls

Table 4

Hydrologic Source Control BMPs

Name	Check If Used
Localized on-lot infiltration	
Impervious area dispersion (e.g. roof top disconnection)	
Street trees (canopy interception)	
Residential rain barrels (not actively managed)	
Green roofs/Brown roofs	
Blue roofs	
Other:	

N/A

IV.3.2 Infiltration BMPs

Table 5

Infiltration BMPs

Name	Check If Used
Bioretention without underdrains	
Rain gardens	
Porous landscaping	
Infiltration planters	
Retention swales	
Infiltration trench	
Infiltration basin	
Drywells	
Subsurface infiltration galleries	
French drains	
Permeable asphalt	
Permeable concrete	
Permeable concrete pavers	
Other:	
Other:	

N/A

Per email correspondence with the City of Orange (see Appendix E), the Orange County Water District (OCWD) does not recommend introducing (infiltrating) stormwater into the larger groundwater table near the site. OCWD has made this finding based on concerns from historical uses on the sites that are in the vicinity and up-gradient of the proposed project. Based on this, it is infeasible to retain any of the DCV and instead biotreatment BMPs are utilized.

IV.3.3 Evapotranspiration, Rainwater Harvesting BMPs Table 6

Evapotranspiration, Rainwater Harvesting BMP

Name	Check If Used
All HSCs; See Section IV.3.1	
Surface-based infiltration BMPs	
Biotreatment BMPs	
Above-ground cisterns and basins	
Underground detention	
Other:	
Other:	
Other:	

Rainwater Harvesting BMPs are infeasible based on the calculations below.

Worksheet J: Summary of Harvested Water Demand and Feasibility

1	What demands for harvested water exist in the tributa all that apply):	ary area (cl	heck	
2	Toilet and urinal flushing			
3 Landscape irrigation		Х		
4	Other:			
5	What is the design capture storm depth? (Figure III.1)	d	0.85	inches
6	What is the project size?	А	12.70	ac
7	7 What is the acreage of impervious area? IA		11.43	ac
	For projects with multiple types of demand (toilet f and/or other demand)	flushing, irr	igation de	mand,
8	What is the minimum use required for partial capture? (Table X.6)	n/a gpd		gpd
9	What is the project estimated wet season total daily use (Section X.2)?	n/	n/a gpd	
10	Is partial capture potentially feasible? (Line 9 > Line	n/	'a	

Worksheet J: Summary of Harvested Water Demand and Feasibility

	8?)						
	For projects with on	ly toilet flus	shing dema	ind	I		
11	What is the minimum (Table X.7)	m TUTIA fo	or partial ca	pture?		n/a	
12	What is the project	estimated ⁻	stimated TUTIA?			n/a	
13	Is partial capture potentially feasible? (Line 12 > Line 11?)					n/a	
	For projects with on	ly irrigatior	n demand				
14	What is the minimul on conservation lan	•			1	0.86	ac
15	What is the propose (multiply conservation active turf by 2)					1.27	ac
16	Is partial capture po Line 14?)	tentially fe	asible? (Lin	ie 15 >		No	
EIA	TA = LA x KL / (IE x T LA = landscape an K _L = Area-weighted IE = irrigation effici Imp area = 497.89	ea irrigateo d landscap ency (assu	with harve coefficier ume 0.90)	ested water	, sq-ft = 5	5,321 (1.27	acres)
EIA	LA = landscape are K_L = Area-weighted IE = irrigation effici Imp area = 497,89 = (55,321 x 0.35) / = 0.0432	ea irrigated d landscap ency (assu 1 (11.43 ad (0.9 x 497	d with harve le coefficier ume 0.90) cres) (891)	ested water at = 0.35			acres)
EIA	LA = landscape are K_L = Area-weighted IE = irrigation effici Imp area = 497,89 = (55,321 x 0.35) / = 0.0432 Table X.8: Minimum In	ea irrigated d landscap ency (assu 1 (11.43 ad (0.9 x 497 rrigated Area	d with harve be coefficier ume 0.90) cres) (891) for Potential	ested water at = 0.35 I Partial Capt	ure Feasibi	llity	
	LA = landscape are K_L = Area-weighted IE = irrigation effici Imp area = 497,89 = (55,321 x 0.35) / = 0.0432	ea irrigated d landscap ency (assu 1 (11.43 ad (0.9 x 497 rrigated Area	d with harve le coefficier ume 0.90) cres) (891)	ested water at = 0.35 I Partial Capt	ure Feasibi		
	LA = landscape are K_L = Area-weighted IE = irrigation effici Imp area = 497,89 = (55,321 x 0.35) / = 0.0432 Table X.8: Minimum In General Landscape Type Closest ET Station	ea irrigated d landscap ency (assu 1 (11.43 ad (0.9 x 497 rrigated Area Conserva	d with harve be coefficier ume 0.90) cres) (891) a for Potential ation Design: Santa Ana	ested water at = 0.35 I Partial Capt K _L = 0.35 Laguna	ure Feasibi Active	ility Turf Areas: I Santa Ana	К _L = 0.7 Laguna
	LA = landscape are K_L = Area-weighted IE = irrigation effici Imp area = 497,89 = (55,321 x 0.35) / = 0.0432 Table X.8: Minimum In General Landscape Type Closest ET Station Design Capture Storm	ea irrigated d landscap ency (assu 1 (11.43 ad (0.9 x 497 rrigated Area Conserva	d with harve be coefficier ume 0.90) cres) (891) a for Potential ation Design: Santa Ana Required Irr	ested water at = 0.35 I Partial Capt K _L = 0.35 Laguna igated Area p	ure Feasibi Active Irvine Der Tributa	llity Turf Areas: I Santa Ana ry Imperviou	K _L = 0.7 Laguna
	LA = landscape are K_L = Area-weighted IE = irrigation effici Imp area = 497,89 = (55,321 x 0.35) / = 0.0432 Table X.8: Minimum In General Landscape Type Closest ET Station	ea irrigated d landscap ency (assu 1 (11.43 ad (0.9 x 497 rrigated Area Conserva	d with harve be coefficier ume 0.90) cres) (891) a for Potential ation Design: Santa Ana Required Irr	ested water at = 0.35 I Partial Capt K _L = 0.35 Laguna	ure Feasibi Active Irvine Der Tributa	llity Turf Areas: I Santa Ana ry Imperviou	K _L = 0.7 Laguna
	LA = landscape are K_L = Area-weighted IE = irrigation effici Imp area = 497,89 = (55,321 x 0.35) / = 0.0432 Table X.8: Minimum In General Landscape Type Closest ET Station Design Capture Storm Depth, inches	ea irrigated d landscap ency (assu 1 (11.43 ad (0.9 x 497 rrigated Area Conserva Irvine Minimum	d with harve be coefficien ume 0.90) cres) ,891) a for Potential ation Design: Santa Ana Required Irr Pote	ested water t = 0.35 I Partial Capt $K_L = 0.35$ Laguna igated Area p ential Partial	ure Feasibi Active Irvine Der Tributa Capture, ac	llity Turf Areas: I Santa Ana ry Imperviou ;/ac	K _L = 0.7 Laguna s Acre for
	LA = landscape are K_L = Area-weighted IE = irrigation effici Imp area = 497,89 = (55,321 x 0.35) / = 0.0432 Table X.8: Minimum In General Landscape Type Closest ET Station Design Capture Storm Depth, inches 0.60	ea irrigated d landscap ency (assu 1 (11.43 ad (0.9 x 497 rrigated Area Conserva Irvine Minimum 0.66	d with harve be coefficien ume 0.90) cres) (891) a for Potential ation Design: Santa Ana Required Irr Pote 0.68	ested water t = 0.35 I Partial Capt $K_L = 0.35$ Laguna igated Area p ential Partial 0.72	ure Feasibi Active Irvine Der Tributa Capture, ac 0.33	Ility Turf Areas: I Santa Ana ry Imperviou Jac 0.34	K _L = 0.7 <i>Laguna</i> s Acre for 0.36
	LA = landscape are K_L = Area-weighter IE = irrigation effici Imp area = 497,89 = (55,321 x 0.35) / = 0.0432 Table X.8: Minimum In General Landscape Type Closest ET Station Design Capture Storm Depth, inches 0.60 0.65	ea irrigated d landscap ency (assu 1 (11.43 ad (0.9 x 497 rrigated Area Conserva Irvine Minimum 0.66 0.72	d with harve le coefficier ume 0.90) cres) ,891) a for Potential ation Design: Santa Ana Required Irr Pote 0.68 0.73	ested water t = 0.35 I Partial Capt $K_L = 0.35$ Laguna igated Area p ential Partial 0.72 0.78	ure Feasibi Active Irvine Capture, ac 0.33 0.36	llity Turf Areas: 1 Santa Ana ry Imperviou Jac 0.34 0.37	K _L = 0.7 <i>Laguna</i> s Acre for 0.36 0.39
	LA = landscape are K_L = Area-weighted IE = irrigation effici Imp area = 497,89 = (55,321 x 0.35) / = 0.0432 Table X.8: Minimum In General Landscape Type Closest ET Station Design Capture Storm Depth, inches 0.60 0.65 0.70	ea irrigated d landscap ency (assu 1 (11.43 ad (0.9 x 497 rrigated Area Conserva Irvine Minimum 0.66 0.72 0.77	a with harve be coefficien ume 0.90) cres) (891) a for Potential ation Design: Santa Ana Required Irr Pote 0.68 0.73 0.79	ested water t = 0.35 I Partial Capt $K_L = 0.35$ Laguna igated Area p ential Partial 0.72 0.78 0.84	ure Feasibi Active Irvine Der Tributar Capture, ac 0.33 0.36 0.39	Ility Turf Areas: I Santa Ana ry Imperviou Jac 0.34 0.37 0.39	K _L = 0.7 <i>Laguna</i> s Acre for 0.36 0.39 0.42
	LA = landscape are K_L = Area-weighter IE = irrigation effici Imp area = 497,89 = (55,321 x 0.35) / = 0.0432 Table X.8: Minimum In General Landscape Type Closest ET Station Design Capture Storm Depth, inches 0.60 0.65 0.70 0.75	ea irrigated d landscap ency (assu 1 (11.43 ad (0.9 x 497 rrigated Area Conserva Irvine Minimum 0.66 0.72 0.77 0.83 0.88 0.93	d with harve le coefficier ume 0.90) cres) ,891) a for Potential ation Design: Santa Ana Required Irr Pote 0.68 0.73 0.79 0.84	ested water at = 0.35 I Partial Capt K _L = 0.35 Laguna igated Area p ential Partial 0.72 0.78 0.84 0.90 0.96 1.02	ure Feasibi Active Irvine Der Tributar Capture, ac 0.33 0.36 0.39 0.41 0.44 0.47	llity Turf Areas: Santa Ana ry Imperviou /ac 0.34 0.37 0.39 0.42 0.45 0.48	K _L = 0.7 <i>Laguna</i> s Acre for 0.36 0.39 0.42 0.45 0.48 0.51
	LA = landscape are K_L = Area-weighted IE = irrigation effici Imp area = 497,89 = (55,321 x 0.35) / = 0.0432 Table X.8: Minimum In General Landscape Type Closest ET Station Design Capture Storm Depth, inches 0.60 0.65 0.70 0.75 0.80 0.85 0.90	ea irrigated d landscap ency (assu 1 (11.43 ad (0.9 x 497 rrigated Area Conserva Irvine Minimum 0.66 0.72 0.77 0.83 0.88 0.93 0.99	a with harve be coefficient and 0.90) cres) (891) a for Potential ation Design: Santa Ana Required Irr Pote 0.68 0.73 0.79 0.84 0.90 0.95 1.01	ested water at = 0.35 I Partial Capt K _L = 0.35 Laguna igated Area p ential Partial 0.72 0.78 0.84 0.90 0.96 1.02 1.08	ure Feasibi Active Irvine Der Tributar Capture, ac 0.33 0.36 0.39 0.41 0.44 0.47 0.49	llity Turf Areas: 1 Santa Ana ry Imperviou /ac 0.34 0.37 0.39 0.42 0.45 0.48 0.51	K _L = 0.7 <i>Laguna</i> s Acre for 0.36 0.39 0.42 0.45 0.45 0.48 0.51 0.54
	LA = landscape are K_L = Area-weighted IE = irrigation effici Imp area = 497,89 = (55,321 x 0.35) / = 0.0432 Table X.8: Minimum In General Landscape Type Closest ET Station Design Capture Storm Depth, inches 0.60 0.65 0.70 0.75 0.80 0.85	ea irrigated d landscap ency (assu 1 (11.43 ad (0.9 x 497 rrigated Area Conserva Irvine Minimum 0.66 0.72 0.77 0.83 0.88 0.93	d with harve le coefficier ume 0.90) cres) ,891) a for Potential ation Design: Santa Ana Required Irr Pote 0.68 0.73 0.79 0.84 0.90 0.95	ested water at = 0.35 I Partial Capt K _L = 0.35 Laguna igated Area p ential Partial 0.72 0.78 0.84 0.90 0.96 1.02	ure Feasibi Active Irvine per Tributar Capture, ac 0.33 0.36 0.39 0.41 0.44 0.47	llity Turf Areas: Santa Ana ry Imperviou /ac 0.34 0.37 0.39 0.42 0.45 0.48	K _L = 0.7 <i>Laguna</i> s Acre for 0.36 0.39 0.42 0.45 0.48 0.51

IV.3.4 Biotreatment BMPs

Table 7
Biotreatment BMPs

Bioretention with underdrains	
Storm water planter boxes with underdrains	
Rain gardens with underdrains	
Constructed wetlands	
Vegetated swales	
Vegetated filter strips	
Proprietary vegetated biotreatment systems	
Wet extended detention basin	
Dry extended detention basins	
Other:	
Other:	

							M		Iodular Wetlands System	
MWS #		Tc (mins)	i (in/hr)	imp	с	SQDF (cfs)	Treatment Per Unit	QTY	Model	Total Treatment
							(cfs)			(cfs)
А	5.18	5.0	0.263	0.89	0.819	1.114	0.577	2	MWS-L-8-20-V @ 3.40' HGL	1.154
В	3.32	5.0	0.263	0.95	0.865	0.754	0.462	2	MWS-L-8-16-V @ 3.40' HGL	0.924
С	4.70	5.0	0.263	0.90	0.829	1.022	0.577	2	MWS-L-8-20-V @ 3.40' HGL	1.154

Drainage from the project will surface flow into catch basins utilizing filter inserts for pretreatment. Filter inserts have 100% removal of trash and debris, meeting full capture requirements. Additionally, the filter is equipped with a floating hydrocarbon boom used to control and absorb oil and hydrocarbons. After pretreatment, the proposed onsite storm drain will direct runoff towards sump pumps. The sump pumps will then convey runoff into the MWS systems (primary BMPs) for treatment. The MWS' treatment capacities will exceed the stormwater quality design flowrate (SQDF); therefore, the MWS systems will utilize internal bypass weirs to discharge flows greater than the SQDF to the MWS' discharge chamber to outlet. Treated flows will be conveyed back to the main storm drain line.

Per the MWS performance summary attached in Appendix C, MWS systems have medium/high effectiveness against sediment, nutrients, trash, metals, bacteria, oil and grease and organics.

IV.3.5 Hydromodification Control BMPs

N/A

IV.3.6 Regional/Sub-Regional LID BMPs

N/A

IV.3.7 Treatment Control BMPs

N/A

IV. 4 Water Quality Credits

N/A

IV.5 Alternative Compliance Plan

N/A

IV.6 Vector Control

Based on the current design (flow-based biotreatment BMPs), it is not anticipated to have ponded/nuisance water that would result in a need for vector control. All surface detention mitigating the 100-year storm event will drain offsite via the storm drain system shortly after the peak of the storm.

IV.7 Drainage Management Area (DMA)

DMA Number	BMPs	Area Treated
A & Offsite Run-on	Two (2) MWS-L-8-20-V units (at 3.4' HGL) with filter inserts at all tributary catch basins.	4.83 + 0.35 (offsite)
B & Offsite Run-on	Two (2) MWS-L-8-16-V units (at 3.4' HGL) with filter inserts at all tributary catch basins.	3.10 + 0.22 (offsite)
C & Offsite Run-on	Two (2) MWS-L-8-20-V units (at 3.4' HGL) with filter inserts at all tributary catch basins.	4.45 + 0.25 (offsite)
Total Area		12.38 + 0.82 (offsite)

Describe each DMA used in project, the BMPs in each DMA and the area treated.

Total Project Area = 12.38 acres onsite and 0.82 acres of offsite run-on

DMA A will consist of the northerly two-thirds of Building 1, the northerly truck yard, vehicle parking areas along the northerly PL, and offsite run-on from the existing railroad right-of-way. Runoff will sheet flow into several catch basins with filter inserts (for pretreatment) in the truck yard area and then be conveyed easterly (via a storm drain) towards a diversion structure. Once here, a pipe set at a lower elevation will direct the SQDF to Pump "A". Low flows/SQDF are then pumped into MWS "A". This MWS will biofilter the SQDF to comply with water quality requirements. MWS "A" has a treatment capacity of 1.154 cfs which exceeds the SQDF; therefore, it will utilize an internal bypass weir to discharge flows greater than the SQDF to the MWS' discharge chamber to outlet. Treated flows will be conveyed back to the main storm drain line.

DMA B will consist of the southerly one-third of Building 1, vehicle parking areas south of Building 1, the westerly half of the drive aisle between Building 1 and 2, and offsite run-on from the existing site south of the site. Runoff will sheet flow to several catch

basins with filter inserts (for pretreatment) throughout DMA B and then conveyed easterly (via a storm drain) towards a diversion structure. Once here, a pipe set at a lower elevation will direct the SQDF to Pump "B". Low flows/SQDF are then pumped into MWS "B". This MWS will biofilter the SQDF to comply with water quality requirements. MWS "B" has a treatment capacity of 0.924 cfs which exceeds the SQDF; therefore, it will utilize an internal bypass weir to discharge flows greater than the SQDF to the MWS' discharge chamber to outlet. Treated flows will be conveyed back to the main storm drain line.

DMA C will consist of Building 2, it's truck yard, the drive aisle north of Building 2, vehicle parking areas surrounding Building 2, and offsite run-on from the existing railroad right-of-way. Runoff will sheet flow to several catch basins with filter inserts (for pretreatment) in the truck yard area and in the easterly vehicle parking area. Runoff will then be conveyed westerly (via a storm drain) towards a diversion structure. Once here, a pipe set at a lower elevation will direct the SQDF to Pump "C". Low flows/SQDF are then pumped into MWS "C". This MWS will biofilter the SQDF to comply with water quality requirements. MWS "C" has a treatment capacity of 1.154 cfs which exceeds the SQDF; therefore, it will utilize an internal bypass weir to discharge flows greater than the SQDF to the MWS' discharge chamber to outlet. Treated flows will be conveyed back to the main storm drain line.

Approximately 0.32 acres of self-treating landscape located at the southwest corner of the site will sheet flow offsite without being routed through the onsite BMPs.

IV.8 Calculations

See following pages.

Table 2.7: Infiltration BMP Feasibility Worksheet DMAs A, B and C

	Infeasibility Criteria	Yes	No
1	Would Infiltration BMPs pose significant risk for groundwater related concerns? Refer to Appendix VII (Worksheet I) for guidance on groundwater-related infiltration feasibility criteria.	х	
District (groundw historica	basis: Per email correspondence with the City of Orange, t OCWD) does not recommend introducing (infiltrating) storn vater table near the site. OCWD has made this finding base I uses on the sites that are in the vicinity and up-gradient of the email correspondence in Appendix E.	nwater into the	larger from
	ize findings of studies provide reference to studies, calcula /ide narrative discussion of study/data source applicability.	tions, maps, da	ta sources,
2	 Would Infiltration BMPs pose significant risk of increasing risk of geotechnical hazards that cannot be mitigated to an acceptable level? (Yes if the answer to any of the following questions is yes, as established by a geotechnical expert): The BMP can only be located less than 50 feet away from slopes steeper than 15 percent The BMP can only be located less than eight feet from building foundations or an alternative setback. A study prepared by a geotechnical professional or an available watershed study substantiates that stormwater infiltration would potentially result in significantly increased risks of geotechnical hazards that cannot be mitigated to an acceptable level. 		Х
Provide Summar	basis: ize findings of studies provide reference to studies, calcula	tions, maps, da	ta sources,
etc. Prov	vide narrative discussion of study/data source applicability. Would infiltration of the DCV from drainage area violate downstream water rights ?		х
Provide	basis:		
	ize findings of studies provide reference to studies, calcula vide narrative discussion of study/data source applicability.		ta sources,

Table 2.7: Infiltration BMP Feasibility Worksheet (continued)

	Partial Infeasibility Criteria	Yes	No
4	Is proposed infiltration facility located on HSG D soils or the site geotechnical investigation identifies presence of soil characteristics which support categorization as D soils?		х
Provid	e basis:		
	arize findings of studies provide reference to studies, calculatio ovide narrative discussion of study/data source applicability.	ons, maps, da	ta sources,
5	Is measured infiltration rate below proposed facility less than 0.3 inches per hour? This calculation shall be based on the methods described in Appendix VII.		х
Provid	e basis:		
	arize findings of studies provide reference to studies, calculatio ovide narrative discussion of study/data source applicability.	ons, maps, da	ta sources,
6	Would reduction of over predeveloped conditions cause impairments to downstream beneficial uses, such as change of seasonality of ephemeral washes or increased discharge of contaminated groundwater to surface waters?		х
that is	e citation to applicable study and summarize findings relative to permissible:		
	arize findings of studies provide reference to studies, calculatio ovide narrative discussion of study/data source applicability.	ons, maps, da	ta sources,
7	Would an increase in infiltration over predeveloped conditions cause impairments to downstream beneficial uses, such as change of seasonality of ephemeral washes or increased discharge of contaminated groundwater to surface waters?		х
	e citation to applicable study and summarize findings relative to permissible:	the amount	of infiltration
	arize findings of studies provide reference to studies, calculatio ovide narrative discussion of study/data source applicability.	ons, maps, da	ta sources,

Infiltra	ation Screening Results (check box corresponding to resul	t):
	Is there substantial evidence that infiltration from the project would result in a significant increase in I&I to the sanitary sewer that cannot be sufficiently mitigated? (See Appendix XVII)	- 10
8	Provide narrative discussion and supporting evidence:	n/a
	Summarize findings of studies provide reference to studies, calculations, maps, data sources, etc. Provide narrative discussion of study/data source applicability.	
	If any answer from row 1-3 is yes: infiltration of any volume is not feasible within the DMA or equivalent.	
9	Provide basis: Per email correspondence with the City of Orange, the Orange County Water District (OCWD) does not recommend introducing (infiltrating) stormwater into the larger groundwater table near the site. OCWD has made this finding based on concerns from historical uses on the sites that are in the vicinity and up-gradient of the proposed project. Refer to the email correspondence in Appendix E. Summarize findings of infeasibility screening	Yes
10	If any answer from row 4-7 is yes, infiltration is permissible but is not presumed to be feasible for the entire DCV. Criteria for designing biotreatment BMPs to achieve the maximum feasible infiltration and ET shall apply. Provide basis:	n/a
	Summarize findings of infeasibility screening	
11	If all answers to rows 1 through 11 are no, infiltration of the full DCV is potentially feasible, BMPs must be designed to infiltrate the full DCV to the maximum extent practicable.	Infiltration is Infeasible

Table 2.7: Infiltration BMP Feasibility Worksheet (continued)

Worksheet D: Capture Efficiency Method for Flow-Based BMPs DMA A - MWS "A"

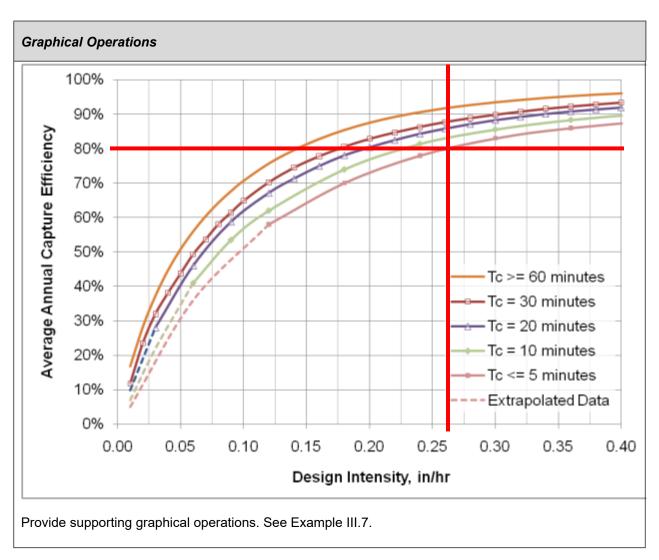
Г

sing Figure III.4, determine the design intensity at which the stimated time of concentration (T_c) achieves 80% capture ficiency, I_1 Inter the effect depth of provided HSCs upstream, d_{HSC} inches) (Worksheet A) Inter capture efficiency corresponding to d_{HSC} , Y_2 Vorksheet A) sing Figure III.4, determine the design intensity at which the me of concentration (T_c) achieves the upstream capture ficiency(Y_2), I_2	I ₁ = d _{HSC} = Y ₂ =	0.2625 	in/hr inches
nches) (Worksheet A) nter capture efficiency corresponding to d_{HSC} , Y_2 Vorksheet A) sing Figure III.4, determine the design intensity at which the ne of concentration (T _c) achieves the upstream capture			inches
Vorksheet A) sing Figure III.4, determine the design intensity at which the ne of concentration (T _c) achieves the upstream capture	Y ₂ =		
ne of concentration (T _c) achieves the upstream capture			%
	I ₂ =		in/hr
etermine the design intensity that must be provided by BMP, $_{esign} = I_1 - I_2$	I _{design} =	0.2625	in/hr
2: Calculate the design flowrate			
nter Project area tributary to BMP (s), A (acres)	A=	5.18	acres
nter Project Imperviousness, <i>imp</i> (unitless)	imp=	0.89	(
alculate runoff coefficient, C= (0.75 x imp) + 0.15	C=	0.820	(
alculate design flowrate, $Q_{design} = (C \times i_{design} \times A)$	Q _{design} =	1.114	cfs
orting Calculations			
ribe system: "A": I: MWS-L-8-20-V @ 3.4' HGL 2 ment Rate: 0.577 cfs each Treatment Rate: 1.154 cfs > SQDF			
de time of concentration assumptions:			
	tter Project area tributary to BMP (s), <i>A</i> (acres) tter Project Imperviousness, <i>imp</i> (unitless) alculate runoff coefficient, $C = (0.75 \times imp) + 0.15$ alculate design flowrate, $Q_{design} = (C \times i_{design} \times A)$ orting Calculations tbe system: "A": : MWS-L-8-20-V @ 3.4' HGL 2 nent Rate: 0.577 cfs each Treatment Rate: 1.154 cfs > SQDF	ter Project area tributary to BMP (s), A (acres)A=iter Project Imperviousness, imp (unitless)imp=alculate runoff coefficient, $C = (0.75 \times imp) + 0.15$ C=alculate design flowrate, $Q_{design} = (C \times i_{design} \times A)$ $Q_{design} =$ orting Calculationsibe system: "A": : MWS-L-8-20-V @ 3.4' HGL 2 nent Rate: 0.577 cfs each Treatment Rate: 1.154 cfs > SQDF	ther Project area tributary to BMP (s), A (acres)A=5.18iter Project Imperviousness, imp (unitless)imp=0.89alculate runoff coefficient, $C = (0.75 \times imp) + 0.15$ C=0.820alculate design flowrate, $Q_{design} = (C \times i_{design} \times A)$ $Q_{design} =$ 1.114orting Calculationsibe system: "A": : : MWS-L-8-20-V @ 3.4' HGL 2 nent Rate: 0.577 cfs each Treatment Rate: 1.154 cfs > SQDF

Worksheet D: Capture Efficiency Method for Flow-Based BMPs DMA A - MWS "A"

📽 WinTR-55 Main	Window			_		×
ile <u>O</u> ptions <u>P</u> roj	jectData <u>G</u> lobalData <u>F</u>	<u>R</u> un <u>H</u> elp				
	тс 🔺 🌾 🜌	۳ 🔨 🗹	1 📐 🥐]		
Wi	nTR-55 Sma	II Watersio	utput Definit	ion ology	,	
Project Identification						_
User: TEI		itate: California			•	-
Project: Eckhoff :	Street (3910) C	County: Orange			•	-
Subtitle: WQMP			Exec	cution Date: 1	1/3/2022	
Sub-areas are expr	Storr Rain	ensionless Unit Hydrogra m Data Source: User- fall Distribution Identifier	provided cus		tα	•
Sub-area Name	Sub-area Description	Sub-area Flows to Reach/Outlet	Area (ac)	Weighted CN	Tc (hr)	
MW5 'A'		Outlet 💌	5.18	96	0.100	
MW5 'B'		Outlet 💌	3.32	98	0.100	
MW5 'C'		Outlet 💌	4.70	96	0.109	_
		Project Area	: 13.20 (ac)		<u>,</u>	
e: 0:\3900-3999\391	0\WQMP\2022-11-XX PW	QMP 5th Submittal\Atta	ichments\ 1	1/3/2022	10:11 PM	1 //

Worksheets from Orange County Technical Guidance Document (5-19-2011) See TGD for instructions and/or examples related to these worksheets www.ocwatersheds.com/WQMP.aspx



Worksheet D: Capture Efficiency Method for Flow-Based BMPs DMA A - MWS "A"

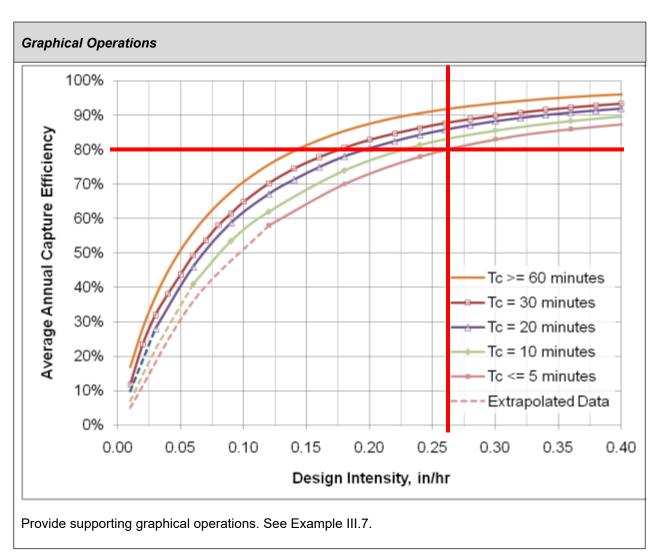
Worksheets from Orange County Technical Guidance Document (5-19-2011) See TGD for instructions and/or examples related to these worksheets www.ocwatersheds.com/WQMP.aspx

Worksheet D: Capture Efficiency Method for Flow-Based BMPs DMA B - MWS "B"

1	Enter the time of concentration, T_c (min) (See Appendix IV.2)	T _c =	5	min
2	Using Figure III.4, determine the design intensity at which the estimated time of concentration (T_c) achieves 80% capture efficiency, I_1	I ₁ =	0.2625	in/hr
3	Enter the effect depth of provided HSCs upstream, d_{HSC} (inches) (Worksheet A)	d _{HSC} =		inches
4	Enter capture efficiency corresponding to d_{HSC} , Y_2 (Worksheet A)	Y ₂ =		%
5	Using Figure III.4, determine the design intensity at which the time of concentration (T_c) achieves the upstream capture efficiency(Y_2), I_2	I ₂ =		in/hr
6	Determine the design intensity that must be provided by BMP, $I_{design} = I_1 - I_2$	I _{design} =	0.2625	in/hr
St	ep 2: Calculate the design flowrate			
1	Enter Project area tributary to BMP (s), A (acres)	A=	3.32	acres
2	Enter Project Imperviousness, <i>imp</i> (unitless)	imp=	0.95	(
3	Calculate runoff coefficient, C= (0.75 x imp) + 0.15	C=	0.865	(
4	Calculate design flowrate, $Q_{design} = (C \times i_{design} \times A)$	Q _{design} =	0.754	(cfs
Sι	pporting Calculations			
M\ Q1 Tro To	escribe system: WS "B": odel: MWS-L-8-16-V @ 3.4' HGL TY: 2 eatment Rate: 0.462 cfs each tal Treatment Rate: 0.924 cfs > SQDF			
μ	ovide time of concentration assumptions:			

Worksheet D: Capture Efficiency Method for Flow-Based BMPs DMA B - MWS "B"

Vir Wir	ectData <u>G</u> lobalData <u>F</u> C 🏊 🖌 🛒 遳				1		
Vir Wir					1		
	nTR-55 Sma	II W	atersh	ed Hyd	drology	,	
Project Identification D				<u> </u>			_
Jser: TEI		itate:	California			-]
Project: Eckhoff S	treet (3910) C	County:	Orange			-	·]
Subtitle: WQMP				Exec	ution Date: 1	1/3/2022	
Sub-areas are expre	Storr Rain	n Data 9	s Unit Hydrogra Source: <mark>User-</mark> ibution Identifier	provided cus		ta	•
Sub-area Entry and Su Sub-area Name	Sub-area Description		irea Flows to ich/Outlet	Area (ac)	Weighted CN	Tc (hr)	
MW5 'A'		Outlet	+	5.18	96	0.100	
MWS 'B'		Outlet	•	3.32	98	0.100	
MW5 'C'		Outlet	<u> </u>	4.70	96	0.109	-



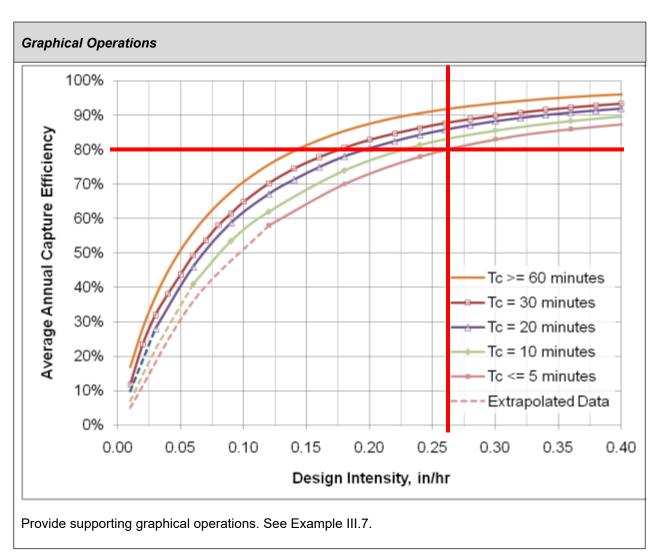
Worksheet D: Capture Efficiency Method for Flow-Based BMPs DMA B - MWS "B"

Worksheet D: Capture Efficiency Method for Flow-Based BMPs DMA C - MWS "C"

1	Enter the time of concentration, $T_{\rm c}$ (min) (See Appendix IV.2)	T _c =	5	min
2	Using Figure III.4, determine the design intensity at which the estimated time of concentration (T_c) achieves 80% capture efficiency, I_1	I ₁ =	0.2625	in/hr
3	Enter the effect depth of provided HSCs upstream, d_{HSC} (inches) (Worksheet A)	d _{HSC} =		inches
4	Enter capture efficiency corresponding to d_{HSC} , Y_2 (Worksheet A)	Y ₂ =		%
5	Using Figure III.4, determine the design intensity at which the time of concentration (T_c) achieves the upstream capture efficiency(Y_2), I_2	l ₂ =		in/hr
6	Determine the design intensity that must be provided by BMP, $I_{design} = I_1 - I_2$	I _{design} =	0.2625	in/hr
St	ep 2: Calculate the design flowrate			
1	Enter Project area tributary to BMP (s), A (acres)	A=	4.70	acres
2	Enter Project Imperviousness, <i>imp</i> (unitless)	imp=	0.90	(
3	Calculate runoff coefficient, C= (0.75 x imp) + 0.15	C=	0.829	(
4	Calculate design flowrate, $Q_{design} = (C \times i_{design} \times A)$	Q _{design} =	1.022	(cfs
Su	pporting Calculations			
MV Mc QT Tre	escribe system: VS "C": odel: MWS-L-8-20-V @ 3.4' HGL 'Y: 2 eatment Rate: 0.577 cfs each tal Treatment Rate: 1.154 cfs > SQDF			
	ovide time of concentration assumptions:			

Worksheet D: Capture Efficiency Method for Flow-Based BMPs DMA C - MWS "C"

-	Window				_		×
e <u>O</u> ptions <u>P</u> ro	jectData <u>G</u> lobalData	<u>R</u> un <u>H</u>	lelp				
	тс 🔺 🌾 😼			K ?]		
W	inTR-55 Smo	dl W	/atersh	ed Hyd	drology	,	
Project Identification							_
User: TEI		State:	California			•	- I
Project: Eckhoff	Street (3910)	County:	Orange			•	- I I
Subtitle: WQMP				Exec	ution Date: 1	1/3/2022	
Sub-areas are exp	Stor Rair	m Data 9	ss Unit Hydrogra Source: <mark>User-</mark> ibution Identifier	provided cus		ta	•
Sub-area Entry and	Summary Sub-area Description		area Flows to ach/Outlet	Area (ac)	Weighted CN	Tc (hr)	
Sub-area Name		I NOL					
Sub-area Name		Outlet	•	5.18	96	0.100	
				5.18 3.32	96 98	0.100	
MW5 'A'		Outlet	-				



Worksheet D: Capture Efficiency Method for Flow-Based BMPs DMA C - MWS "C"

Worksheet B: Simple Design Capture Volume Sizing Method (DMA A – Offsite Runon)

St	ep 1: Determine the design capture storm depth used for cal	culating volu	me	
1	Enter design capture storm depth from Figure III.1, <i>d</i> (inches)	d=	0.85	inches
2	Enter the effect of provided HSCs, <i>d</i> _{HSC} (inches) (Worksheet A)	d _{HSC} =	0	inches
3	Calculate the remainder of the design capture storm depth, $d_{remainder}$ (inches) (Line 1 – Line 2)	d _{remainder} =	0.85	inches
St	ep 2: Calculate the DCV			
1	Enter Project area tributary to BMP (s), A (acres)	A=	0.35	acres
2	Enter Project Imperviousness, <i>imp</i> (unitless)	imp=	0.10	
3	Calculate runoff coefficient, $C = (0.75 \times imp) + 0.15$	C=	0.2250	
4	Calculate runoff volume, V_{design} = (C x $d_{remainder}$ x A x 43560 x	V _{design} =	243	cu-ft
4	(1/12))	- design		
	ep 3: Design BMPs to ensure full retention of the DCV	- design		
St		Georgi		
St	ep 3: Design BMPs to ensure full retention of the DCV	K _{observed} =	N/A*	In/hr
St St	ep 3: Design BMPs to ensure full retention of the DCV ep 3a: Determine design infiltration rate Enter measured infiltration rate, K _{observed} ¹ (in/hr)			1
St St	ep 3: Design BMPs to ensure full retention of the DCV ep 3a: Determine design infiltration rate Enter measured infiltration rate, $K_{observed}$ ¹ (in/hr) (Appendix VII) Enter combined safety factor from Worksheet H, S _{total}	K _{observed} =	N/A*	1
St St 1 2 3	ep 3: Design BMPs to ensure full retention of the DCV ep 3a: Determine design infiltration rate Enter measured infiltration rate, $K_{observed}$ ¹ (in/hr) (Appendix VII) Enter combined safety factor from Worksheet H, S_{total} (unitless)	K _{observed} = S _{total} =	N/A* N/A*	In/hr
St St 1 2 3	ep 3: Design BMPs to ensure full retention of the DCV ep 3a: Determine design infiltration rate Enter measured infiltration rate, $K_{observed}^{1}$ (in/hr) (Appendix VII) Enter combined safety factor from Worksheet H, S_{total} (unitless) Calculate design infiltration rate, $K_{design} = K_{observed} / S_{total}$	K _{observed} = S _{total} =	N/A* N/A*	In/hr
St St 1 2 3 St	ep 3: Design BMPs to ensure full retention of the DCV ep 3a: Determine design infiltration rate Enter measured infiltration rate, $K_{observed}^{-1}$ (in/hr) (Appendix VII) Enter combined safety factor from Worksheet H, S_{total} (unitless) Calculate design infiltration rate, $K_{design} = K_{observed} / S_{total}$ ep 3b: Determine minimum BMP footprint	K _{observed} = S _{total} = K _{design} =	N/A* N/A* N/A*	In/hr In/hr

Worksheet B: Simple Design Capture Volume Sizing Method (DMA A)

St	ep 1: Determine the design capture storm depth used for cal	culating volu	me	
1	Enter design capture storm depth from Figure III.1, <i>d</i> (inches)	d=	0.85	inches
2	Enter the effect of provided HSCs, <i>d</i> _{HSC} (inches) (Worksheet A)	d _{HSC} =	0	inches
3	Calculate the remainder of the design capture storm depth, $d_{remainder}$ (inches) (Line 1 – Line 2)	d _{remainder} =	0.85	inches
St	ep 2: Calculate the DCV			
1	Enter Project area tributary to BMP (s), A (acres)	A=	4.83	acres
2	Enter Project Imperviousness, imp (unitless)	imp=	0.95	
3	Calculate runoff coefficient, C= (0.75 x imp) + 0.15	C=	0.8625	
4	Calculate runoff volume, V_{design} = (C x $d_{remainder}$ x A x 43560 x (1/12))	V _{design} =	12,854	cu-ft
St	ep 3: Design BMPs to ensure full retention of the DCV			
	ep 3: Design BMPs to ensure full retention of the DCV ep 3a: Determine design infiltration rate			
	· · · ·	K _{observed} =	N/A*	In/hr
St	ep 3a: Determine design infiltration rate Enter measured infiltration rate, <i>K</i> _{observed} ¹ (in/hr)	K _{observed} = S _{total} =	N/A* N/A*	In/hr
St 1	ep 3a: Determine design infiltration rate Enter measured infiltration rate, $K_{observed}$ ¹ (in/hr) (Appendix VII) Enter combined safety factor from Worksheet H, S _{total}			In/hr In/hr
St 1 2 3	ep 3a: Determine design infiltration rate Enter measured infiltration rate, $K_{observed}^{1}$ (in/hr) (Appendix VII) Enter combined safety factor from Worksheet H, S_{total} (unitless)	S _{total} =	N/A*	
St 1 2 3	ep 3a: Determine design infiltration rate Enter measured infiltration rate, $K_{observed}^{1}$ (in/hr) (Appendix VII) Enter combined safety factor from Worksheet H, S_{total} (unitless) Calculate design infiltration rate, $K_{design} = K_{observed} / S_{total}$	S _{total} =	N/A*	
St 1 2 3 St	ep 3a: Determine design infiltration rate Enter measured infiltration rate, $K_{observed}^{-1}$ (in/hr) (Appendix VII) Enter combined safety factor from Worksheet H, S_{total} (unitless) Calculate design infiltration rate, $K_{design} = K_{observed} / S_{total}$ ep 3b: Determine minimum BMP footprint	S _{total} = K _{design} =	N/A* N/A*	In/hr

Worksheet B: Simple Design Capture Volume Sizing Method (DMA B – Offsite Runon)

St	tep 1: Determine the design capture storm depth used for calc	culating volu	ıme			
1	Enter design capture storm depth from Figure III.1, <i>d</i> (inches)	d=	0.85	inches		
2	Enter the effect of provided HSCs, <i>d</i> _{HSC} (inches) (Worksheet A)	d _{HSC} =	0	inches		
3	Calculate the remainder of the design capture storm depth, $d_{remainder}$ (inches) (Line 1 – Line 2)	d _{remainder} =	0.85	inches		
Step 2: Calculate the DCV						
1	Enter Project area tributary to BMP (s), A (acres)	A=	0.22	acres		
2	Enter Project Imperviousness, <i>imp</i> (unitless)	imp=	1.00			
3	Calculate runoff coefficient, C= (0.75 x imp) + 0.15	C=	0.9000			
	O_{a} level at a mum off we have $a = 1/2 + a$ and $a = 1/2 + a$					
4	Calculate runoff volume, V_{design} = (C x $d_{remainder}$ x A x 43560 x (1/12))	V _{design} =	611	cu-ft		
		V _{design} =	611	cu-ft		
St	(1/12))	V _{design} =	611	cu-ft		
St	(1/12)) tep 3: Design BMPs to ensure full retention of the DCV	V _{design} = K _{observed} =	611 N/A*	cu-ft		
St St	(1/12)) tep 3: Design BMPs to ensure full retention of the DCV tep 3a: Determine design infiltration rate Enter measured infiltration rate, $K_{observed}^{1}$ (in/hr)					
St St 1	(1/12)) tep 3: Design BMPs to ensure full retention of the DCV tep 3a: Determine design infiltration rate Enter measured infiltration rate, $K_{observed}$ ¹ (in/hr) (Appendix VII) Enter combined safety factor from Worksheet H, S _{total}	K _{observed} =	N/A*			
St St 1 2 3	(1/12)) tep 3: Design BMPs to ensure full retention of the DCV tep 3a: Determine design infiltration rate Enter measured infiltration rate, $K_{observed}$ ¹ (in/hr) (Appendix VII) Enter combined safety factor from Worksheet H, S_{total} (unitless)	K _{observed} = S _{total} =	N/A*	In/hr		
St St 1 2 3	(1/12)) tep 3: Design BMPs to ensure full retention of the DCV tep 3a: Determine design infiltration rate Enter measured infiltration rate, $K_{observed}^{1}$ (in/hr) (Appendix VII) Enter combined safety factor from Worksheet H, S_{total} (unitless) Calculate design infiltration rate, $K_{design} = K_{observed} / S_{total}$	K _{observed} = S _{total} =	N/A*	In/hr		
St St 1 2 3 St	(1/12)) tep 3: Design BMPs to ensure full retention of the DCV tep 3a: Determine design infiltration rate Enter measured infiltration rate, $K_{observed}$ ¹ (in/hr) (Appendix VII) Enter combined safety factor from Worksheet H, S_{total} (unitless) Calculate design infiltration rate, $K_{design} = K_{observed} / S_{total}$ tep 3b: Determine minimum BMP footprint	K _{observed} = S _{total} = K _{design} =	N/A* N/A* N/A*	In/hr In/hr		

Worksheet B: Simple Design Capture Volume Sizing Method (DMA B)

St	ep 1: Determine the design capture storm depth used for cal	culating volu	me				
1	Enter design capture storm depth from Figure III.1, <i>d</i> (inches)	d=	0.85	inches			
2	Enter the effect of provided HSCs, <i>d</i> _{HSC} (inches) (Worksheet A)	d _{HSC} =	0	inches			
3	Calculate the remainder of the design capture storm depth, $d_{remainder}$ (inches) (Line 1 – Line 2)	d _{remainder} =	0.85	inches			
St	Step 2: Calculate the DCV						
1	Enter Project area tributary to BMP (s), A (acres)	A=	3.10	acres			
2	Enter Project Imperviousness, <i>imp</i> (unitless)	imp=	0.95				
3	Calculate runoff coefficient, <i>C</i> = (0.75 x imp) + 0.15	C=	0.8625				
	Calculate runoff volume, V _{design} = (C x d _{remainder} x A x 43560 x						
4	(1/12))	V _{design} =	8,250	cu-ft			
		V _{design} =	8,250	cu-ft			
St	(1/12))	V _{design} =	8,250	cu-ft			
St	(1/12)) ep 3: Design BMPs to ensure full retention of the DCV	V _{design} = K _{observed} =	8,250	In/hr			
St St	(1/12)) The p 3: Design BMPs to ensure full retention of the DCV the p 3a: Determine design infiltration rate Enter measured infiltration rate, $K_{observed}^{1}$ (in/hr)						
St St 1	(1/12)) ep 3: Design BMPs to ensure full retention of the DCV ep 3a: Determine design infiltration rate Enter measured infiltration rate, $K_{observed}$ ¹ (in/hr) (Appendix VII) Enter combined safety factor from Worksheet H, S _{total}	K _{observed} =	N/A*				
S 1 1 2 3	(1/12)) ep 3: Design BMPs to ensure full retention of the DCV ep 3a: Determine design infiltration rate Enter measured infiltration rate, $K_{observed}^{1}$ (in/hr) (Appendix VII) Enter combined safety factor from Worksheet H, S_{total} (unitless)	K _{observed} = S _{total} =	N/A* N/A*	In/hr			
S 1 1 2 3	(1/12)) ep 3: Design BMPs to ensure full retention of the DCV ep 3a: Determine design infiltration rate Enter measured infiltration rate, $K_{observed}^{1}$ (in/hr) (Appendix VII) Enter combined safety factor from Worksheet H, S _{total} (unitless) Calculate design infiltration rate, $K_{design} = K_{observed} / S_{total}$	K _{observed} = S _{total} =	N/A* N/A*	In/hr			
S 1 3 S 1 3	(1/12)) ep 3: Design BMPs to ensure full retention of the DCV ep 3a: Determine design infiltration rate Enter measured infiltration rate, $K_{observed}$ ¹ (in/hr) (Appendix VII) Enter combined safety factor from Worksheet H, S_{total} (unitless) Calculate design infiltration rate, $K_{design} = K_{observed} / S_{total}$ ep 3b: Determine minimum BMP footprint	K _{observed} = S _{total} = K _{design} =	N/A* N/A* N/A*	In/hr In/hr			

Worksheet B: Simple Design Capture Volume Sizing Method (DMA C – Offsite Runon)

St	ep 1: Determine the design capture storm depth used for cal	culating volu	me	
1	Enter design capture storm depth from Figure III.1, <i>d</i> (inches)	d=	0.85	inches
2	Enter the effect of provided HSCs, <i>d</i> _{HSC} (inches) (Worksheet A)	d _{HSC} =	0	inches
3	Calculate the remainder of the design capture storm depth, $d_{remainder}$ (inches) (Line 1 – Line 2)	d _{remainder} =	0.85	inches
Si	ep 2: Calculate the DCV			
1	Enter Project area tributary to BMP (s), A (acres)	A=	0.25	acres
2	Enter Project Imperviousness, <i>imp</i> (unitless)	imp=	0.10	
3	Calculate runoff coefficient, <i>C</i> = (0.75 x imp) + 0.15	C=	0.2250	
	Calculate runoff volume, V _{design} = (C x d _{remainder} x A x 43560 x			
4	(1/12))	V _{design} =	174	cu-ft
		V _{design} =	174	cu-ft
St	(1/12))	V _{design} =	174	cu-ft
St	(1/12)) ep 3: Design BMPs to ensure full retention of the DCV	V _{design} = K _{observed} =	174 N/A*	cu-ft
St St	(1/12)) The p 3: Design BMPs to ensure full retention of the DCV The p 3a: Determine design infiltration rate Enter measured infiltration rate, $K_{observed}^{1}$ (in/hr)			
St St	(1/12)) ep 3: Design BMPs to ensure full retention of the DCV ep 3a: Determine design infiltration rate Enter measured infiltration rate, $K_{observed}$ ¹ (in/hr) (Appendix VII) Enter combined safety factor from Worksheet H, S _{total}	K _{observed} =	N/A*	<u> </u>
S 1 1 2 3	(1/12)) ep 3: Design BMPs to ensure full retention of the DCV ep 3a: Determine design infiltration rate Enter measured infiltration rate, $K_{observed}$ ¹ (in/hr) (Appendix VII) Enter combined safety factor from Worksheet H, S_{total} (unitless)	K _{observed} = S _{total} =	N/A* N/A*	In/hr
S 1 1 2 3	(1/12)) ep 3: Design BMPs to ensure full retention of the DCV ep 3a: Determine design infiltration rate Enter measured infiltration rate, $K_{observed}^{1}$ (in/hr) (Appendix VII) Enter combined safety factor from Worksheet H, S _{total} (unitless) Calculate design infiltration rate, $K_{design} = K_{observed} / S_{total}$	K _{observed} = S _{total} =	N/A* N/A*	In/hr
S 1 3 S 1 3 S 1	(1/12)) ep 3: Design BMPs to ensure full retention of the DCV ep 3a: Determine design infiltration rate Enter measured infiltration rate, $K_{observed}$ ¹ (in/hr) (Appendix VII) Enter combined safety factor from Worksheet H, S_{total} (unitless) Calculate design infiltration rate, $K_{design} = K_{observed} / S_{total}$ ep 3b: Determine minimum BMP footprint	K _{observed} = S _{total} = K _{design} =	N/A* N/A* N/A*	In/hr In/hr

Worksheet B: Simple Design Capture Volume Sizing Method (DMA C)

St	tep 1: Determine the design capture storm depth used for calc	culating volu	ime				
1	Enter design capture storm depth from Figure III.1, <i>d</i> (inches)	d=	0.85	inches			
2	Enter the effect of provided HSCs, <i>d</i> _{HSC} (inches) (Worksheet A)	d _{HSC} =	0	inches			
3	Calculate the remainder of the design capture storm depth, $d_{remainder}$ (inches) (Line 1 – Line 2)	d _{remainder} =	0.85	inches			
St	Step 2: Calculate the DCV						
1	Enter Project area tributary to BMP (s), A (acres)	A=	4.45	acres			
2	Enter Project Imperviousness, <i>imp</i> (unitless)	imp=	0.95				
3	Calculate runoff coefficient, C= (0.75 x imp) + 0.15	C=	0.8625				
4	Calculate runoff volume, V_{design} = (C x $d_{remainder}$ x A x 43560 x (1/12))	V _{design} =	11,843	cu-ft			
		V _{design} =	11,843	cu-ft			
St	(1/12))	V _{design} =	11,843	cu-ft			
St	(1/12)) tep 3: Design BMPs to ensure full retention of the DCV	V _{design} = K _{observed} =	11,843 N/A*	cu-ft			
St St	(1/12)) tep 3: Design BMPs to ensure full retention of the DCV tep 3a: Determine design infiltration rate Enter measured infiltration rate, $K_{observed}^{1}$ (in/hr)			1			
St St 1	(1/12)) tep 3: Design BMPs to ensure full retention of the DCV tep 3a: Determine design infiltration rate Enter measured infiltration rate, $K_{observed}$ ¹ (in/hr) (Appendix VII) Enter combined safety factor from Worksheet H, S _{total}	K _{observed} =	N/A*	1			
St St 1 2 3	(1/12)) tep 3: Design BMPs to ensure full retention of the DCV tep 3a: Determine design infiltration rate Enter measured infiltration rate, $K_{observed}^{1}$ (in/hr) (Appendix VII) Enter combined safety factor from Worksheet H, S_{total} (unitless)	K _{observed} = S _{total} =	N/A* N/A*	In/hr			
St St 1 2 3	(1/12)) tep 3: Design BMPs to ensure full retention of the DCV tep 3a: Determine design infiltration rate Enter measured infiltration rate, $K_{observed}^{1}$ (in/hr) (Appendix VII) Enter combined safety factor from Worksheet H, S _{total} (unitless) Calculate design infiltration rate, $K_{design} = K_{observed} / S_{total}$	K _{observed} = S _{total} =	N/A* N/A*	In/hr			
St St 1 2 3 St	(1/12)) tep 3: Design BMPs to ensure full retention of the DCV tep 3a: Determine design infiltration rate Enter measured infiltration rate, $K_{observed}$ ¹ (in/hr) (Appendix VII) Enter combined safety factor from Worksheet H, S_{total} (unitless) Calculate design infiltration rate, $K_{design} = K_{observed} / S_{total}$ tep 3b: Determine minimum BMP footprint	K _{observed} = S _{total} = K _{design} =	N/A* N/A* N/A*	In/hr In/hr			

V. Implementation, Maintenance and Inspection Responsibility for BMPs (O&M Plan)

Responsible Party Information (Local Contact Information)

Name:	Charles McPhee	Title:	Sr. VP and Regional Director
Company:	IDI Eckhoff Orange LLC	-	
Phone Number:	(213) 330-8066		

	Table 8 -	Frequency	Inspection Matrix	
--	-----------	-----------	--------------------------	--

BMP	Responsible Party	*Maintenance Activity	*Inspection/Maintenance Frequency
Source Control BMF	s (Structural and Non	-structural)	1
N1 Education for Property Owners, Tenants and Occupants	Name: Charles McPhee Title: Sr. VP and Regional Director Company: IDI Eckhoff Orange LLC	To educate employees on stormwater pollution prevention.	Annually and within 2 weeks of being hired.
	Phone Number: (213) 330-8066		
N2 Activity Restriction	Name: Charles McPhee Title: Sr. VP and Regional Director Company: IDI Eckhoff Orange LLC	There shall be no discharges of fertilizers, pesticides, wastes, or washing of pavement to streets or storm drains. All debris shall be collected and relocated to an	Daily
	Phone Number: (213) 330-8066	approved landfill. No vehicle maintenance and no vehicle wash areas.	

N3 Common Area Landscape management	Name: Charles McPhee Title: Sr. VP and Regional Director Company: IDI Eckhoff Orange LLC Phone Number: (213) 330-8066	Irrigation system shall be inspected monthly by landscape contractor to check for over-watering, leaks, or excessive runoff to paved areas and landscaping shall be maintained weekly and maintenance contractor shall properly dispose of all landscape wastes.	Landscaping should be inspected/maintained in a weekly basis. Irrigation system shall be inspected monthly.
N4 BMP Maintenance	Name: Charles McPhee Title: Sr. VP and Regional Director Company: IDI Eckhoff Orange LLC Phone Number: (213) 330-8066	See specific BMP maintenance at the end of this table.	See specific BMP maintenance at the end of this table.
N11 Common Area Litter Control	Name: Charles McPhee Title: Sr. VP and Regional Director Company: IDI Eckhoff Orange LLC Phone Number: (213) 330-8066	Clear of trash and debris.	Daily

N12 Employee Training	Name: Charles McPhee Title: Sr. VP and Regional Director Company: IDI Eckhoff Orange LLC Phone Number: (213) 330-8066	To educate employees on stormwater pollution prevention.	Annually and within two weeks of being hired.
N13 Housekeeping of Loading Docks	Name: Charles McPhee Title: Sr. VP and Regional Director Company: IDI Eckhoff Orange LLC Phone Number: (213) 330-8066	Loading docks must be swept regularly for trash, debris, and sediment. Docks will not be hosed down. Absorbent will be used for cleanup of small spills. Used absorbent will be properly disposed of.	Daily
N14 Common Area Catch Basin Inspection	Name: Charles McPhee Title: Sr. VP and Regional Director Company: IDI Eckhoff Orange LLC Phone Number: (213) 330-8066	Clear of trash, debris, and any accumulated sediment.	Inspect monthly and vacuum as necessary.
N15 Street Sweeping Private Streets and Parking Lots	Name: Charles McPhee Title: Sr. VP and Regional Director Company: IDI Eckhoff Orange LLC Phone Number: (213) 330-8066	The paved parking areas shall be mechanical broom swept on a regular basis to remove debris.	Weekly or more often as needed to remove visible trash and debris.
Low Impact Develop	ment and Treatment E	3MPs	

BIO-7: Modular Wetlands System	Name: Charles McPhee Title: Sr. VP and Regional Director Company: IDI Eckhoff Orange LLC Phone Number: (213) 330-8066	Per manufactures specifications all units shall remove trash from the screening device twice a year. Sediment will be removed from the separation chamber once a year. The cartridge filter media and the drain down filter media will be replaced once a year. The vegetation will be trimmed twice a year. The units shall be inspected and maintained by a qualified technician with proper disposal of all waste.	Per manufactures specifications and units shall be inspected twice a year and maintained at least once a year (replacement of media filter), prior to October 1.
PRE-2: Filter Inserts	Name: Charles McPhee Title: Sr. VP and Regional Director Company: IDI Eckhoff Orange LLC Phone Number: (213) 330-8066	Filter inserts will need to be inspected. Debris will be removed that may cause the drain to clog. Hydrocarbon booms needs to be replaced per manufacturer's specifications.	Per manufacturer's specifications; after September 1 and prior to October 1.

Name: Charles	Verify automatic and	One (1) per year per
McPhee	manual operation of	manufacturer's
Title: Sr. VP and Regional Director	pump. Inspect floats for proper elevation and movement	recommendations. Inspection of mechanical seals to be done once
Company: IDI Eckhoff Orange LLC Phone Number: (213) 330-8066	and movement. Correct any obstructions. Check incoming power and amperage for proper voltage. Hose down lift station to clean pump and floats. Inspect floats for proper elevation and movement. Correct any obstructions. Check incoming power and amperage for proper voltage. Hose down lift station to clean	seals to be done once every two (2) years.
	McPhee Title: Sr. VP and Regional Director Company: IDI Eckhoff Orange LLC Phone Number:	McPhee Title: Sr. VP and Regional Director Company: IDI Eckhoff Orange LLC Phone Number: (213) 330-8066 McPhee Title: Sr. VP and Regional Director Company: IDI Eckhoff Orange LLC Phone Number: (213) 330-8066 McPhee Manual operation of pump. Inspect floats for proper elevation and movement. Correct any obstructions. Check incoming power and amperage for proper voltage. Hose down lift station to clean pump and floats. Inspect floats for proper elevation and movement. Correct any obstructions. Check incoming power and amperage for proper voltage. Hose down

*Attach in appendix additional inspection, maintenance and operations information if required.

Regulatory Permits

City of Orange: Grading Permit State: Water Discharge Identification (WDID #8 XXCXXXXX) State: Construction General Permit (CGP) State: Industrial General Permit (IGP); Non-Exposure Certification

Funding

Funding for installation and on-going maintenance for all BMPs will be the responsibility of the owner.

OWNER SELF CERTIFICATION STATEMENT

As the owner representative of the **IDI Eckhoff** for which a Water Quality Management Plan (WQMP) was approved by the City, I hereby certify under penalty of law that all Best Management Practices contained within the approved Project WQMP have been maintained and inspected in accordance with the schedule and frequency outlined in the approved WQMP Maintenance Table.

The maintenance activities and inspections conducted are shown in the attached table and have been performed by qualified and knowledgeable individuals. Structural Treatment BMPs have been inspected and certified by a licensed professional engineer.

To the best of my knowledge, the information submitted is true and accurate and complete. I am aware that there are significant penalties for submitting false information, including the possibility of fines and citations for violating water quality regulations.

Signed:	
0	

Name: Charles McPhee

Title: Sr. VP and Regional Director

Company:	IDI Eckhoff	Orange LLC)
----------	-------------	------------	---

Address: 840 Apollo Street, Suite 343, El Segundo, CA 90245

Telephone Number: (213) 330-8066

Date:						

BMP	Activity	Completion Dates or Frequency	Initial
Source Control BMF	s (Structural and Nonstructural)	1	
N1 Education for Property Owners, Tenants and Occupants	To educate employees on stormwater pollution		
N2 Activity Restriction	There shall be no discharges of fertilizers, pesticides, wastes, or washing of pavement to streets or storm drains. All debris shall be collected and relocated to an approved landfill. No vehicle maintenance and no vehicle wash areas.		
N3 Common Area Landscape management	Clear area of trash, debris, weeds and any accumulated sediment.		
N4 BMP Maintenance	See BMP maintenance at the end of this table.		
N11 Common Area Litter Control	Clear of trash and debris. Dispose of all materials properly offsite.		
N12 Employee Training	To educate employees on stormwater pollution.		
N13 Housekeeping of Loading Docks	Loading docks must be swept regularly for trash, debris, and sediment. Docks will not be hosed down. Absorbent will be used for cleanup of small spills. Used absorbent will be properly disposed of.		
N14 Common Area Catch Basin Inspection	Clear of trash, debris, and any accumulated sediment.		
N15 Street Sweeping Private Streets and Parking Lots	The paved parking areas shall be mechanical broom swept every two weeks, or more often as needed, to remove pollutants from the site.		

BMP Implementation Tracking Table

Low Impact Develop	oment and Treatment BMPs	
BIO-7: Modular Wetlands System	Per manufactures specifications all units shall remove trash from the screening device twice a year. Sediment will be removed from the separation chamber once a year. The cartridge filter media and the drain down filter media will be replaced once a year. The vegetation will be trimmed twice a year. The units shall be inspected and maintained by a qualified technician with proper disposal of all waste.	
PRE-2: Filter Inserts	Filter inserts will need to be inspected. Debris will be removed that may cause the drain to clog. Hydrocarbon booms needs to be replaced per manufacturer's specifications.	
Sump Pump	Verify automatic and manual operation of pump. Inspect floats for proper elevation and movement. Correct any obstructions. Check incoming power and amperage for proper voltage. Hose down lift station to clean pump and floats. Inspect floats for proper elevation and movement. Correct any obstructions. Check incoming power and amperage for proper voltage. Hose down lift station to clean pump and floats.	

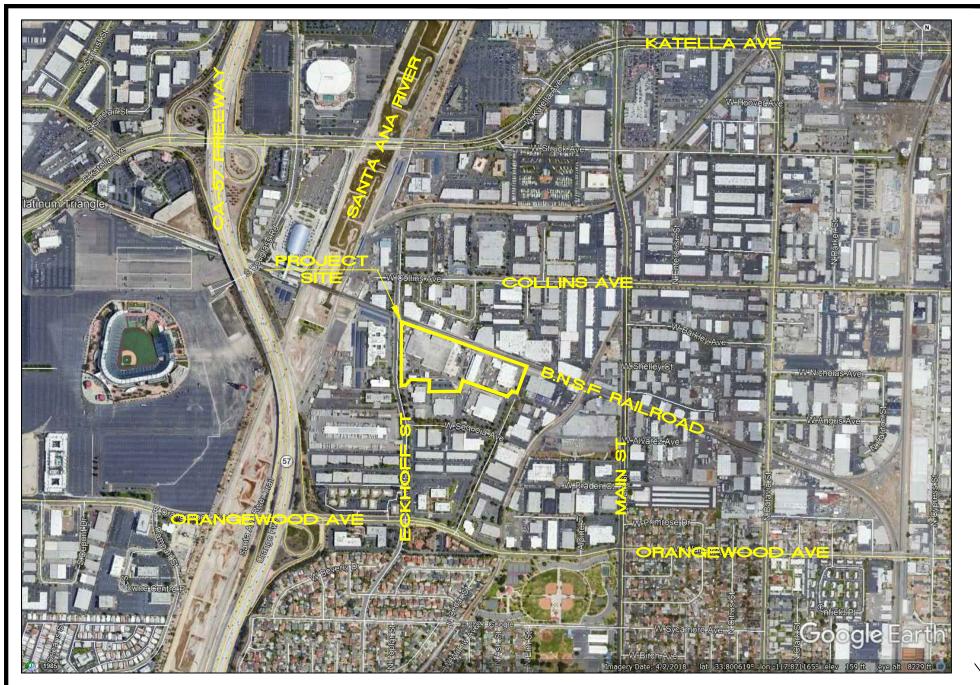
- * This sheet is to be submitted annually with the Owner Self Certification Statement.
- ** Structural Treatment BMPs should be certified by a Licensed Professional Engineer.

VI. Location Map, Site Plan, and BMP Details

Include a location map that identifies project location and proximity to nearby water bodies. In an 11X17 sheet Identify land use, cover, feasibility constraints, structures, buildings, number of units, landscape areas, storm drain inlets, storm drain facilities, drainage flow direction, structural and treatment BMP locations, dumpsters, trash enclosures, wash areas, etc.

Delineate drainage management areas showing limits (acreage) of each drainage area for all structural, treatment and Low Impact Development BMPs used and provide BMP details on plan or in Appendix C.

- Location Map Show downstream receiving waters
- Location Map Show nearby/structures and uses
- Site plan including drainage pathways, on-site and of imperviousness/ perviousness, BMP locations, etc.
- BMP Detail Plans Show unique features of all BMPs to be used on-site.



• Thienes Engineering, Inc. civil engineering • land surveying 14349 firestone boulevard la mirada, california 90638 ph.(714)521-4811 fax(714)521-4173

VICINITY MAP FOR ECKHOFF STREET



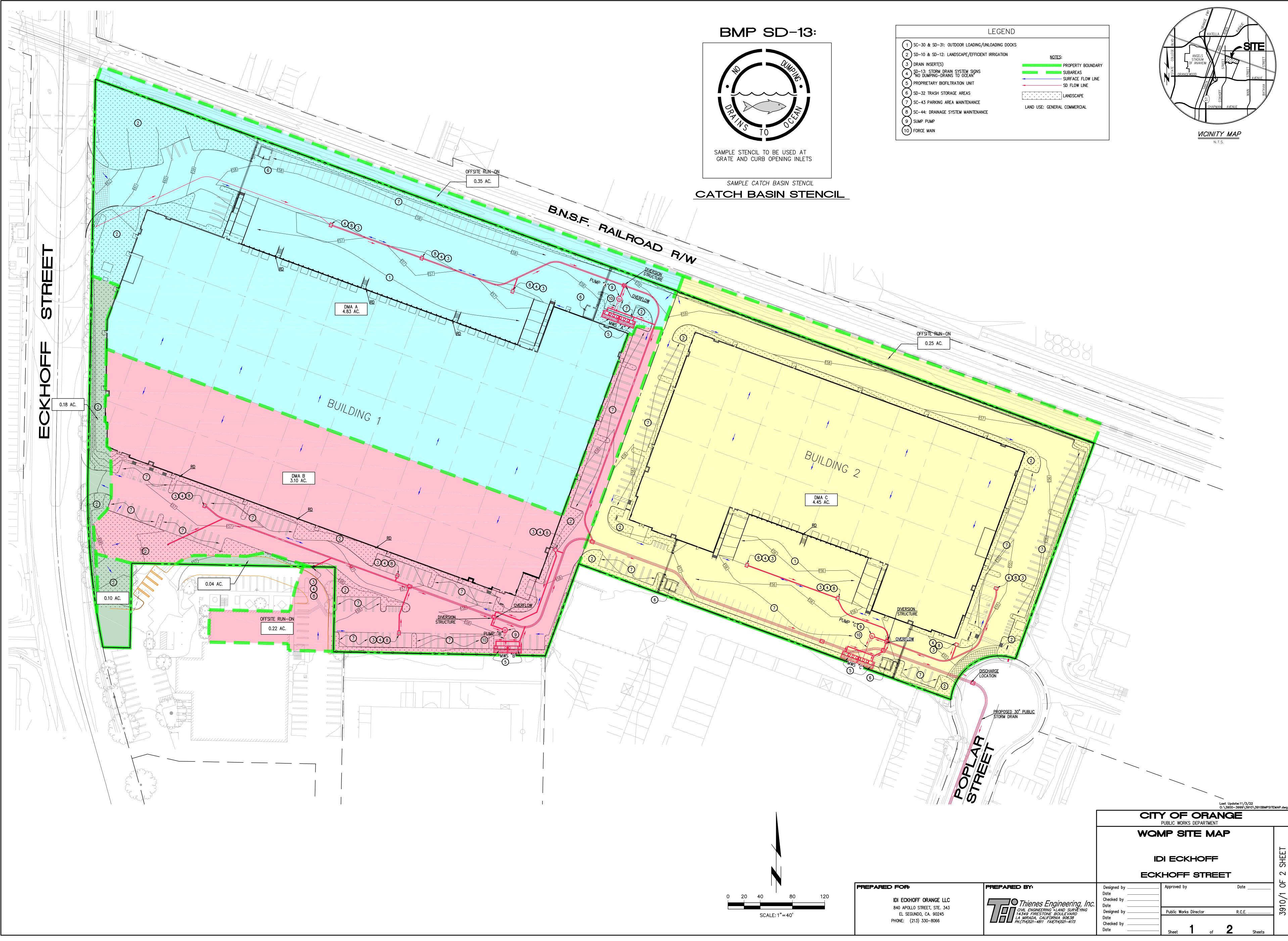
"RECEIVING WATERS MAP"

FLOW

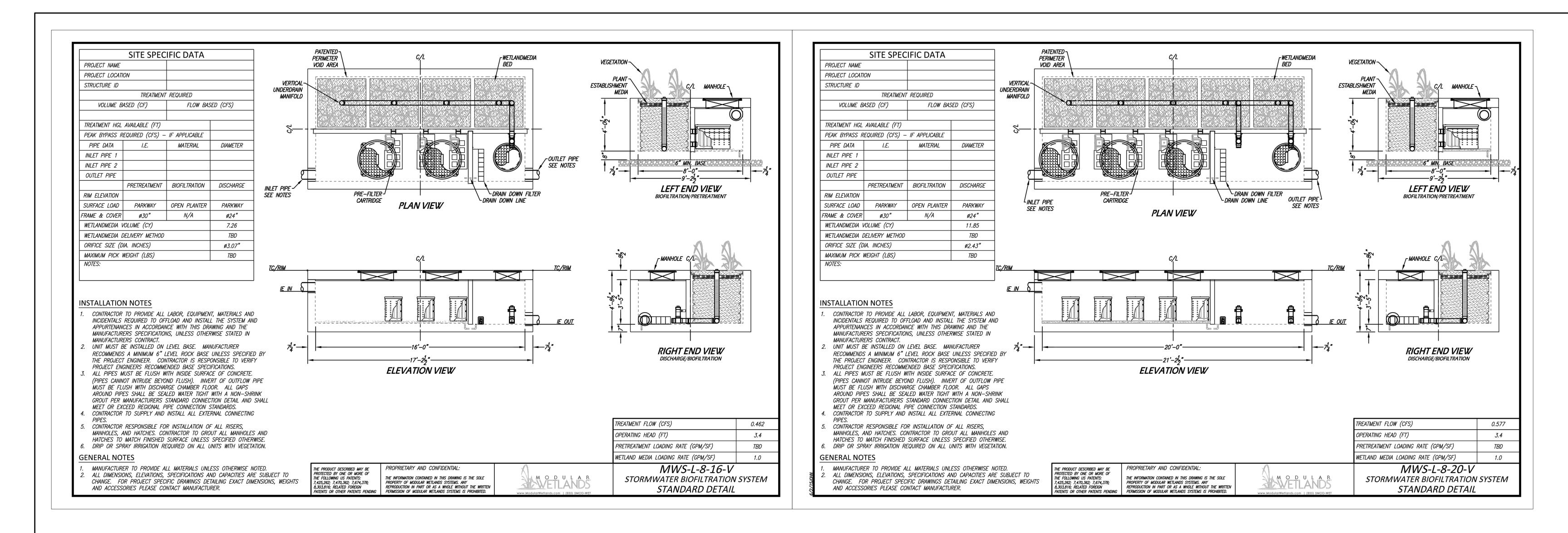
FOR

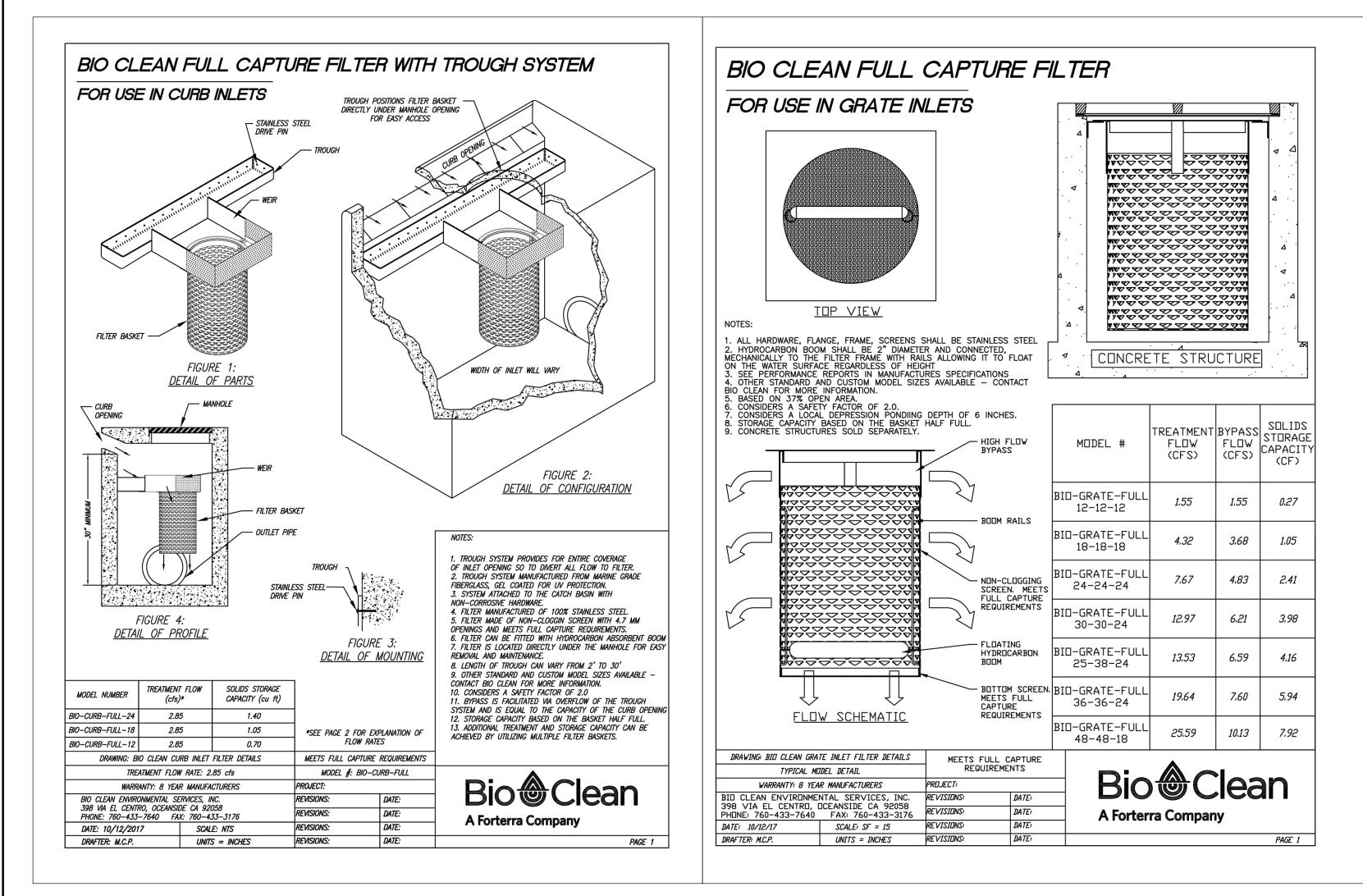
ECKHOFF STREET





COFORA		TEMAP.dwg
AP SITE MA		2 SHEET
Approved by	Date	3910/1 OF
Public Works Director	R.C.E	39
Sheet of	2 Sheets	





		c):\3900-3999\3910\3910BMPSITE	EMAP.dwg
	CIT	Y OF ORAN PUBLIC WORKS DEPARTMENT	NGE	
	WQI	MP SITE MA	\P	
		DI ECKHOFF KHOFF STREE	∃T	2 SHEET
n, Inc.	Designed by Date Checked by Date	Approved by	Date	3910/2 OF
YING	Date Date Checked by Date	Public Works Director Sheet 2 of	R.C.E	162

Last Update:11/3/22

PREPARED FOR:

IDI ECKHOFF ORANGE LLC 840 APOLLO STREET, STE. 343 EL SEGUNDO, CA. 90245 PHONE: (213) 330-8066 PREPARED BY:



VII. Educational Materials

Refer to the City's website or the Orange County Stormwater Program (H2OC.org) for a library of materials available. Attach only the educational materials specifically applicable to the project.

E	ducatio	n Materials	
Residential Material (http://www.ocwatersheds.com)	Check If Applicable	Business Material (http://www.ocwatersheds.com)	Check If Applicable
The Ocean Begins at Your Front Door		Tips for the Automotive Industry	
Tips for Car Wash Fund-raisers		Tips for Using Concrete and Mortar	
Tips for the Home Mechanic		Tips for the Food Service Industry	
Homeowners Guide for Sustainable Water Use		Proper Maintenance Practices for Your Business	
Household Tips			Check If
Proper Disposal of Household Hazardous Waste		Other Material	Attached
Recycle at Your Local Used Oil Collection Center (North County)		IC3. Building Maintenance	
Recycle at Your Local Used Oil Collection Center (Central County)		IC7. Landscape Maintenance	\boxtimes
Recycle at Your Local Used Oil Collection Center (South County)		IC15. Parking and Storage Area Maintenance	
Tips for Maintaining a Septic Tank System			
Responsible Pest Control			
Sewer Spill Response			
Tips for the Home Improvement Projects			
Tips for Horse Care			
Tips for Landscaping and Gardening			
Tips for Pet Care			
Tips for Pool Maintenance			
Tips for Residential Pool, Landscape and Hardscape Drains			
Tips for Projects Using Paint			

Appendix A: Conditions of Approval Resolution _____ dated _____ Appendix B: Educational Material

The Ocean Begins at Your Front Door

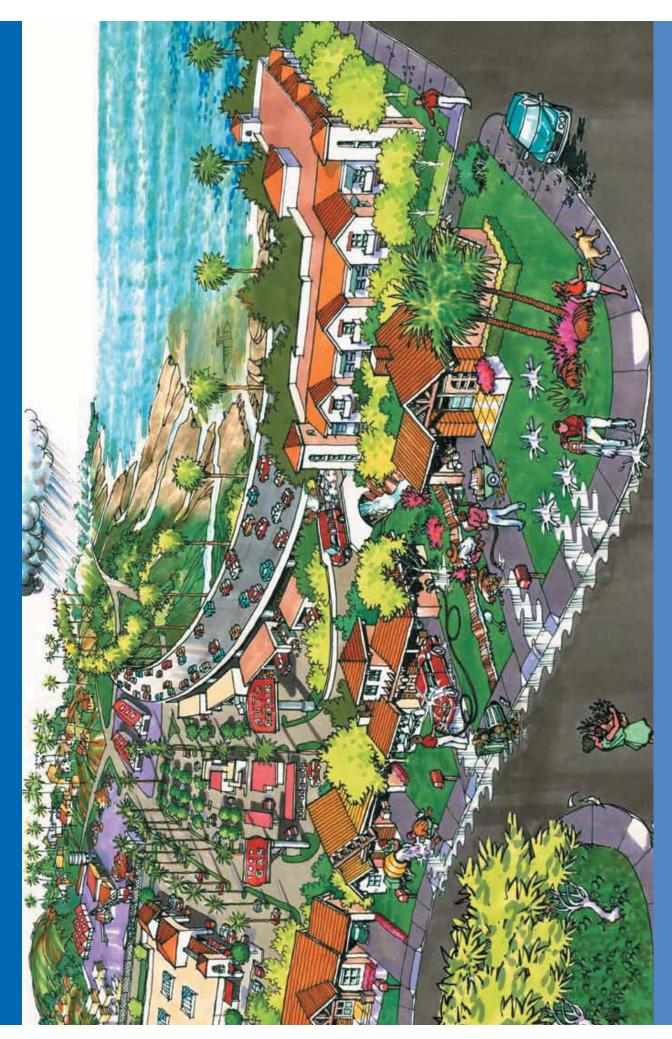


Household Activities	Pool Maintenance	Trash
Do not rinse spills with water. Use dry cleanup	Pool and spa water must be dechlorinated and free	■ Place trash and litter that cannot be recycled in
methods such as applying cat litter or another	of excess acid, alkali or color to be allowed in the	securely covered trash cans.
absorbent material, sweep and dispose of in	street, gutter or storm drain.	Whenever possible, buy recycled products.
the trash. Take items such as used or excess	■ When it is not raining, drain dechlorinated pool and	Remember: Reduce, Reuse, Recycle.
batteries, oven cleaners, automotive fluids,	spa water directly into the	č ,
painting products and cathode ray tubes, like	sanitary sewer.	Pet Care
TVs and computer monitors, to a Household	Some cities may have ordinances that do not allow	Always pick up after your pet. Flush waste down
Hazardous Waste Collection Center (HHWCC).	pool water to be disposed of in the storm drain.	the toilet or dispose of it in the trash. Pet waste,
■ For a HHWCC near you call (714) 834-6752 or	Check with your city.	if left outdoors, can wash into the street, gutter
visit www.oclandfills.com.		or storm drain.
Do not hose down your driveway, sidewalk or	Landscape and Gardening	■ If possible, bathe your pets indoors. If you must
patio to the street, gutter or storm drain. Sweep	Do not over-water. Water your lawn and garden by	bathe your pet outside, wash it on your lawn or
up debris and dispose of it in the trash.	hand to control the amount of water you use or set	another absorbent/permeable surface to keep
	irrigation systems to reflect seasonal water needs.	the washwater from entering the street, gutter or
Automotive	If water flows off your yard onto your driveway or	storm drain.
Take your vehicle to a commercial car	sidewalk, your system is over-watering. Periodically	Follow directions for use of pet care products
wash whenever possible. If you wash your	inspect and fix leaks and misdirected sprinklers.	and dispose of any unused products at a
vehicle at home, choose soaps, cleaners, or	Do not rake or blow leaves, clippings or pruning	HHWCC.
detergents labeled non-toxic, phosphate- free	waste into the street, gutter or storm drain. Instead,	
or biodegradable. Vegetable and citrus-based	dispose of waste by composting, hauling it to a	
products are typically safest for the environment.	permitted landfill, or as green waste through your	Common Pollutants
Do not allow washwater from vehicle washing	city's recycling program.	Home Maintenance
to drain into the street, gutter or storm drain.	Follow directions on pesticides and fertilizer,	 Detergents, cleaners and solvents
Excess washwater should be disposed of in the	(measure, do not estimate amounts) and do not use	 Oil and latex paint
sanitary sewer (through a sink or toilet) or onto	if rain is predicted within 48 hours.	 Swimming pool chemicals
an absorbent surface like your lawn.	■ Take unwanted pesticides to a HHWCC to be	 Outdoor trash and litter
Monitor your vehicles for leaks and place a pan	recycled. For locations and hours of HHWCC, call	
under leaks. Keep your vehicles well maintained	(714) 834-6752 or visit www.oclandfills.com.	Lawn and Garden
to stop and prevent leaks.		• Pet and animal waste
Never pour oil or antifreeze in the street, gutter		• Pesticides
or storm drain. Recycle these substances at a		• Clippings, leaves and soil
service station, a waste oil collection center or		• Fertuizer
used oil recycling center. For the nearest Used		Automobilo
Oil Collection Center call 1-800-CLEANUP or		• Oil and orease
visit www.1800cleanup.org.		• Radiator fluids and antifreeze
		 Cleaning chemicals
		 Brake pad dust

Follow these simple steps to help reduce water

pollution:

The Ocean Begins at Your Front Door



Never allow pollutants to enter the street, gutter or storm drain!

Did You Know?

neighborhoods, construction sites and parking of water pollution in urban areas comes from specific sources such as factories and sewage Most people believe that the largest source treatment plants. In fact, the largest source of water pollution comes from city streets, pollution: stormwater and urban runoff There are two types of non-point source lots. This type of pollution is sometimes called "non-point source" pollution. pollution.

other urban pollutants into storm drains sources carries trash, lawn clippings and the year when excessive water use from Stormwater runoff results from rainfall Urban runoff can happen any time of When rainstorms cause large volumes of water to rinse the urban landscape, irrigation, vehicle washing and other picking up pollutants along the way.

Where Does It Go?

fertilizers and cleaners - can be blown or washed Anything we use outside homes, vehicles and businesses - like motor oil, paint, pesticides, into storm drains.

A little water from a garden hose or rain can also (from sinks or toilets), water in storm drains is sewer systems; unlike water in sanitary sewers Storm drains are separate from our sanitary send materials into storm drains.

not treated before entering our waterways.

Sources of Non-Point Source Pollution

- Automotive leaks and spills.
- Improper disposal of used oil and other engine fluids.
- Metals found in vehicle exhaust, weathered paint, rust, metal plating and tires.
 - Pesticides and fertilizers from lawns, gardens and farms.
- Improper disposal of cleaners, paint and paint removers.
- Soil erosion and dust debris from landscape and construction activities.
- Litter, lawn clippings, animal waste, and other organic matter.
- Oil stains on parking lots and paved surfaces.



The Effect on the Ocean

can harm marine life Pollutants from the storm drain system pollution can have in Orange County. Non-point source a serious impact on water quality

as well as coastal and wetland habitats. They can also degrade recreation areas such as beaches, harbors and bays.

educate and encourage the public to protect water quality, monitor runoff in the storm drain system, Stormwater quality management programs have investigate illegal dumping and maintain storm been developed throughout Orange County to drains.

and disposal of materials will help stop pollution before it reaches the storm drain and the ocean. and reduce urban runoff pollution. Proper use businesses is needed to improve water quality Support from Orange County residents and



For More Information

California Environmental Protection Agency www.calepa.ca.gov

- Air Resources Board www.arb.ca.gov
- **Department of Pesticide Regulation** www.cdpr.ca.gov
- **Department of Toxic Substances Control** www.dtsc.ca.gov
- Integrated Waste Management Board www.ciwmb.ca.gov
- Office of Environmental Health Hazard Assessment www.oehha.ca.gov
- State Water Resources Control Board www.waterboards.ca.gov

Earth 911 - Community-Specific Environmental Information 1-800-cleanup or visit www.1800cleanup. org

Health Care Agency's Ocean and Bay Water Closure and Posting Hotline

(714) 433-6400 or visit www.ocbeachinfo.com

Integrated Waste Management Dept. of Orange

County (714) 834-6752 or visit www.oclandfills.com for information on household hazardous waste collection centers, recycling centers and solid waste collection

O.C. Agriculture Commissioner

(714) 447-7100 or visit www.ocagcomm.com

Stormwater Best Management Practice Handbook Visit www.cabmphandbooks.com

UC Master Gardener Hotline

(714) 708-1646 or visit www.uccemg.com

The Orange County Stormwater Program has created and moderates an electronic mailing list to facilitate communications, take questions and exchange ideas among its users about issues and topics related to stormwater and urban runoff and the implementation of program elements. To join the list, please send an email to ocstormwaterinfo-join@list.ocwatersheds.com

Orange County Stormwater Program

5-2535
5-6860
0-7666
2-3655
4-5323
9-6740
8-3584
3-4441
8-6853
1-5956
6-5431
4-6315
5-9792
0-3310
7-0378
7-2650
2-4337
9-0500
1-3480
1-3538
0-3056
4-3215
2-6480
3-8245
5-1800
1-6143
4-4413
7-3380
7 x317
2 x204
3-3150
8-1500
1 x446
1-7138
7-7455
2

On-line Water Pollution Problem Reporting Form

www.ocwatersheds.com





Iean beaches and healthy many common activities such as toilets), water in storm drains is sanitary sewers (from sinks and not treated before entering our creeks, rivers, bays and pollution if you're not careful. pest control can lead to water planned and applied properly to Orange County. However, Pesticide treatments must be not enter the street, gutter or storm drain. Unlike water in ocean are important to ensure that pesticides do water ways. You would never dump pesticides into the ocean, so don't let it enter the storm drains. Pesticides can cause significant damage to our environment if used improperly. If you are thinking of using a pesticide to control a pest, there are some important things to consider.

For more information, please call University of California Cooperative Extension Master Gardeners at (714) 708-1646 or visit these Web sites: www.uccemg.org www.ipm.ucdavis.edu For instructions on collecting a specimen sample visit the Orange County Agriculture Commissioner's website at: http://www.ocagcomm.com/ser_lab.asp

To report a spill, call the Orange County 24-Hour Water Pollution Problem Reporting Hotline at 1-877-89-SPILL (1-877-897-7455).

For emergencies, dial 911.

Information From: Cheryl Wilen, Area IPM Advisor; Darren Haver, Watershed Management Advisor; Mary Louise Flint, IPM Education and Publication Director; Pamela M. Geisel, Environmental Horticulture Advisor; Carolyn L. Unruh, University of California Cooperative Extension staff writer. Photos courtesy of the UC Statewide IPM Program and Darren Haver.

Funding for this brochure has been provided in full or in part through an agreement with the State Water Resources Control Board (SWRCB) pursuant to the Costa-Machado Water Act of 2000 (Prop. 13).



Help Prevent Ocean Pollution:

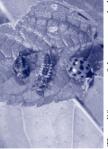
Responsible Pest Control



Tips for Pest Control

Key Steps to Follow:

Steb 1: Correctly identify the pest (insect, weed, rodent, or disease) and verify that it is actually causing the problem.



because beneficial

insects are often

This is important

Three life stages of the common lady peetle, a beneficial insect.

pesticides needlessly. mistaken for pests **Certified Nursery** and sprayed with Consult with a

Professional at a local nursery or garden center County Agricultural Commissioner's Office. or send a sample of the pest to the Orange

though you see damage, the pest may have left. Determine if the pest is still present - even

Steb 2: Determine present and causing now many pests are damage. Small pest populations more safely using nonmay be controlled

pesticide techniques. These include removing stream of water, blocking entry into the home food sources, washing off leaves with a strong using caulking and replacing problem plants with ones less susceptible to pests



control methods for long-term prevention usually combines several least toxic pest Integrated Pest Management (IPM) and management of pest problems without harming you, your family, or the environment

Steb 3: If a pesticide must be used, choose the feast toxic chemical.

Obtain information on the least toxic pesticides pest from the UC Statewide Integrated Pest that are effective at controlling the target Management (IPM) Program's Web site at www.ipm.ucdavis.edu.

Professional at a local nursery or garden center Seek out the assistance of a Certified Nursery when selecting a pesticide. Purchase the smallest amount of pesticide available.

Apply the pesticide to the pest during its most vulnerable life stage. This information can be found on the pesticide label

Step 4: Wear appropriate protective clothing.

Follow pesticide labels regarding specific types Protective clothing should always be washed of protective equipment you should wear separately from other clothing.

weather, irrigation, and the presence of children conditions when applying pesticides such as Step 5: Continuously monitor external and animals

after applying pesticides unless the directions say Never apply pesticides when rain is predicted within the next 48 hours. Also, do not water it is necessary.

conditions may cause the spray or dust to drift Apply pesticides when the air is still; breezy away from your targeted area.

In case of an emergency call 911 and/or the (714) 634-5988 or (800) 544-4404 (CA only) regional poison control number at

For general questions you may also visit www.calpoison.org.

sweep up or use an absorbent agent to remove any excess pesticides. Avoid the use of water. Steb 6: In the event of accidental spills,

absorbent material, such as cat litter, newspapers Be prepared. Have a broom, dust pan, or dry or paper towels, ready to assist in cleaning up spills. Contain and clean up the spill right away. Place contaminated materials in a doubled plastic bag. be properly disposed of according to your local All materials used to clean up the spill should Houseĥold Hazardous Waste Disposal site.

Step 7: Properly store and dispose of unused pesticides.

Use (RTU) products Purchase Ready-Tolarge concentrated to avoid storing quantities of pesticides.



Store unused chemicals in a locked cabinet.

of at a Household Hazardous Waste Collection Unused pesticide chemicals may be disposed Center.

rinsed prior to disposing of them in the trash. Empty pesticide containers should be triple

Household Hazardous Waste www.oclandfills.com **Collection Center** (714) 834-6752



Regulatory Requirements Sewage Spill

Allowing sewage to discharge to a gutter or storm drain may subject you to penalties and/or out-of-pocket costs to reimburse cities or public agencies for clean-up efforts.

Here are the pertinent codes, fines, and agency contact information that apply.

Orange County Stormwater Program 24 Hour Water Pollution Reporting Hotline 1-877-89-SPILL (1-877-897-7455)

Country and city water quality ordinances prohibit discharges containingpollutants.

Orange County Health Care Agency Environmental Health (714) 433-6419

California Health and Safety Code, Sections 5410-5416

No person shall discharge raw or treated sewage or other waste in a manner that results in contamination, pollution or a nuisance.

Any person who causes or permits a sewage discharge to any

 must immediately notify the local health agency of the discharge. state waters:

- shall reimburse the local health agency for services that protect the public's health and safety (water-contact receiving waters).
- who fails to provide the required notice to the local health agency is guilty of a misdemeanor and shall be punished by a fine (between \$500–\$1,000) and/or imprisonment for less than one year.

Regional Water Quality Control Board Santa Ana Region San Diego Region (951) 782-4130 (858) 467-2952

Requires the prevention, mitigation, response to and reporting of sewagespills.

California Office of Emergency Services (800) 852-7550 California Water Code, Article 4, Chapter 4, Sections 13268-13271 California Code of Regulations, Title 23, Division 3, Chapter 9.2, Article 2, Sections 2250-2260

Any person who causes or permits sewage in excess of 1,000 gallons to be discharged to state waters shall immediately notify the Office of Emergency Services.

Any person who fails to provide the notice required by this section is **guilty of a misdemeanor** and shall be punished by a fine (less than \$20,000) and/or imprisonmentfor not more than one year.

Sewage Spill **Reference Guide**

as a Private Property Owner Your Responsibilities

Residences Businesses Homeowner/Condominium Associations Federal and State Complexes Military Facilities



Sanitation District Orange County



V

20sution REVENTIO mental Health This brochure was designed courtesy of the Orange County Sanitation District (OCSD). For additional information, call (714) 962-2411, or visit their website at www.ocsd.con

Sewage Spill? What is a

a manhole, cleanout or broken pipe. Sewage spills can cause health hazards, damage to homes and businesses, spills occur when the wastewater being transported via underground pipes overflows through and threaten the environment, local waterways and Sewage beaches.

Common Causes of Sewage Spills

sewer pipes. Grease gets into the sewer from food establishments, household drains, as well as from poorly Grease builds up inside and eventually blocks maintained commercial grease traps and interceptors.

Structure problems caused by tree roots in the lines, broken/cracked pipes, missing or broken cleanout caps or undersized sewers can cause blockages.

is caused when groundwater or rainwater enters the sewer system through pipe defects and illegal connections. Infiltration and inflow (I/I) impacts pipe capacity and

Sewage Spill Caused by a Blockage or Break in Your Sewer Lines! You Are Responsible for a

Time is of the essence in dealing with sewage spills. You are required to immediately:

on private property and out of gutters, storm drains and Control and minimize the spill. Keep spills contained public waterways by shutting off or not using the water.

5 Use sandbags, dirt and/or plastic sheeting prevent sewage from entering the storm drain system.

wash your hands. It is recommended that a plumbing professional be called for clearing blockages and making Clear the sewer blockage. Always wear gloves and necessary repairs.

Health Care Agency. In addition, if it exceeds 1,000 gallons notify the Office of Emergency Services. Refer to department or public sewer district of sewage spills. If the spill enters the storm drains also notify the Always notify your city sewer/public works the numbers listed in this brochure.



You Could Be Liable

to discharge to a gutter or storm drain may subject you to Allowing sewage from your home, business or property penalties and/or out-of-pocket costs to reimburse cities or public agencies for clean-up and enforcement efforts. See Regulatory Codes & Fines section for pertinent codes and fines that apply.

What to Look For

from a manhole or a slow water leak that may take time to Sewage spills can be a very noticeable gushing of water be noticed. Don't dismiss unaccounted-for wet areas.

Drain backups inside the building. Lookfor:

Wet ground and water leaking around manhole lids onto your street.

Unusual odorous wet areas: sidewalks, external Leaking water from cleanouts or outside drains.

walls or ground/landscape around a building.

Caution

Untreated sewage has high levels of disease-causing viruses and bacteria. Call your local health care agency listed on the back for more information. Keep people and pets away from the affected area

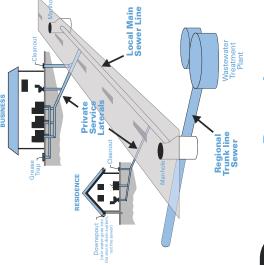
If You See a Sewage Spill Occurring, Notify Your City Sewer/Public Works Department or Public Sewer District 1

IMMEDIATELY!

DTP113 Rev 4/06

How a Sewer System Works

A property owner's sewer pipes are called service laterals and are connected to larger local main and regional trunk lines. Service laterals run from the connection at the home to the connection with the public sewer fincluding the area under the streat. These laterals are the responsibility of the property owner and must be maintained by the property owner. Many city agencies have adopted ordinances requiring maintenance of servicel laterals. Checkwith your city sewer/local public works departmentfor more information. Operation and maintenance of **local and** regional sever lines are the responsibility of the city sever/public works departments and public sever districts.



Preventing Grease Blockages

The drain is not a dump! Recycle or dispose of grease properly and never pour grease down the drain.

Homeowners should mix fats, oils and grease with absorbent waste materials usuch as paper, coffee grounds, or kitty litter and place it in the trash. Wipe food scraps from plates and pans and dump them in the trash.

> Perform periodic cleaning to eliminate grease, debris and roots in your servicelaterals.

2

Never put grease down garbage

~

disposals, drains or toilets.

Prevent Sewage Spills

<u>How You Can</u>

Restaurants and commercial food service establishments should always use "Kitchen Best Management Practices." These include:

 Collecting all cooking grease and liquid oil from pots, pans and fryers in covered grease containers for recycling.

Repair any structural problems in your sewer system and eliminate any rainwater infiltration/inflow leaks into your service laterals.

m

- Scraping or dry-wiping excess food and grease from dishes, pots, pans and fryers into the trash.
- Installing drain screens on all kitchen drains.
- Having spill kits readily available for cleaning up spills.

Sewage spills can cause damage to the environme Help prevent them!

 Properly maintaining grease traps or interceptors by having them serviced regularly. Check your local city codes.

Orange County Agency Responsibilites

- **City Sewer/Public Works Departments–** Responsible for protecting city property and streets, the local storm drain system, sewage collection system and other publicareas.
 - Public Sewer/Sanitation District— Responsible for collecting, treating and disposing of wastewater.
- County of Orange Health Care Agency— Responsible for protecting public health by closing ocean/bay waters and may close food-service businesses if a spill poses a threatto public health.
- Regional Water Quality Control Boards— Responsible for protecting State waters.
- Orange County Stormwater Program— Responsible for preventing harmful pollutants from being discharged or washed by stormwater runoff into the municipal storm drain system, creeks, bays and the ocean.

You Could Be Liable for Not Protecting the Environment

Local and state agencies have legal jurisdiction and enforcement authority to ensure that sewage spills are remedied. They may respond and assist with containment, relieving pipe blockages, and/or clean-up of the sewage spill, especially if the spill is flowing into storm drains or onto public property. A property owner may be charged for costs incurred by these agencies responding to spills from private properties.



Report Sewage Spills!

	ts	8	860	56	; 8	760	295	8 8	5 ×	120	300	765	20	37	200	18	310	88	500	: 2		245	8	553 26.2	380	57	222	411 500	553	170		33/	8	0.5	: 12	8	នេះ	2 8	:=	2:	2 9	32	18	19
	ment		765-6860	3 2	645-8400	229-67	248-35	593-4600	7/1-6276		ριφ	10-7et	-26	362-43	639-0500 905-9792	461-3480	690-33	ŝ	831-2500 644-3011	532-6480	567-636	993-82	Ξ.	366-15! 442.626	647-33	2	6	962-241 998-150	~~~~	1	ts	393-4433/	645-8400	837-0660	741-5375	453-5300	431-2223 002 2552	831-2500	962-241	459-6420	499-4550 234-5400	93-9	858-027	433-6419 852-7550
	epart	(646)	(714)	(714)	(646)	(714)	4	(114)	(114)		- 4	(949)	(949)	(646)	(562)	(949)	(714)	(562)	(049)	(114)	(114)	(714)	(949)	(949)		52	(714)	(714)	(114)	(714)	strict		66	(049)		÷.	(562)		-		(646)	62)	(949)	(714)
	s De	ł	÷	÷		-	÷	ł	ł	-			-	÷	-		-	÷	÷				÷	ł			ł				er Di	-		-		-	rict	Inster		-	thority			gencies _{gency}
	Work	-	-	-		-	÷	÷	-				-	-	:		-	-	-					÷			ł				Wate	t			·	-	er Disti	wesum ct	strict.	rict	vater Au	ict.	strict .	Agen Agency
	blic /	ł	÷	÷			÷	ł	ł	-			-	-	-		-	÷	-				rita	ł			ł				Sewer/	Distric		Dietvio	v District .	strict .	or Sew	r District (we	tion D	er Dist	strict . Vastew	y Distr	tary Di strict .	Other A
	r/Pu	-	-	-			-	-	-		3		-	-	-		-	-	÷,				Margai				ł			-	lic Se	nitary		<u>District</u>	Sanitary	ater Di	DSSm0	INUATE UN	Sanita	a Wat	ater Di: ountv V	Sanitar	n Sani ater Di:	Health Health
P	Sewe	Viejo		Park	esa	-	int	ountain Valley		Juntineton Pond		Beach	Hills	Niguel	.aguna Woods a Hahra	rest	е в	nitos .	Vission Viejo Vewnort Beach		ំដី	a	Rancho Santa Mar	San Clemente San Luan Caniet	na vapri	ach	ł		nster .	nda	Publi	Costa Mesa Sanitary District		El Toro Water District	Grove	Irvine Ranch Water District	Los Alamitos/Rossmoor Sewer District	Midway City Saintary District (wesum Moulton Niguel Water District	Drange County Sanitation District.	Santa Margarita Water District	Coast Water District Orange County Wastewater	Sunset Beach Sanitary District	Irabuco Canyon Sanitary District Yorba Linda Water District	Other Orange County Health Care
	City S	Aliso Vie	Anaheim. Pron		Costa Mesa	Cypress	Dana Point	ountair	Fullerton Garden Grove	tinter t	rvine	8	-aguna I	aguna l	aguna W a Hahra	ake Forest	.a Palma	os Alamitos	Vission Viejo Vewnort Base	Orange.	range (Placentia	ancho	San Cler		Seal Beach.	Stanton	lustın Villa Park	Westminster	Yorba Linda	-	osta M	1	Toro V	Garden (/ine Rá	s Alan	oulton	ange (anta M	sourn uo South Or:	Inset E	abuco rba Lir	Orange (



Preventing water pollution at your commercial/industrial site

Clean beaches and healthy creeks, rivers, bays and ocean are important to Orange County. However, many landscape and building maintenance activities can lead to water pollution if you're not careful. Paint, chemicals, plant clippings and other materials can be blown or washed into storm drains that flow to the ocean. Unlike water in sanitary sewers (from sinks and toilets), water in storm drains is not treated before entering our waterways.

You would never pour soap or fertilizers into the ocean, so why would you let them enter the storm drains? Follow these easy tips to help prevent water pollution.

Some types of industrial facilities are required to obtain coverage under the State General Industrial Permit. For more information visit: www.swrcb.ca.gov/stormwater/industrial.html For more information, please call the Orange County Stormwater Program at 1-877-89-SPILL (1-877-897-7455) or visit www.ocwatersheds.com

To report a spill, call the **Orange County 24-Hour Water Pollution Problem Reporting Hotline** at **1-877-89-SPILL** (1-877-897-7455).

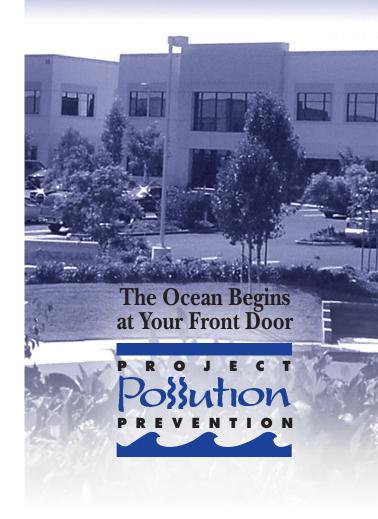
For emergencies, dial 911.



Printed on Recycled Paper

Help Prevent Ocean Pollution:

Proper Maintenance Practices for Your Business



Proper Maintenance Practices for your Business

Landscape Maintenance

- Compost grass clippings, leaves, sticks and other vegetation, or dispose of it at a permitted landfill or in green waste containers. Do not dispose of these materials in the street, gutter or storm drain.
- Irrigate slowly and inspect the system for leaks, overspraying and runoff. Adjust automatic timers to avoid overwatering.
- Follow label directions for the use and disposal of fertilizers and pesticides.
- Do not apply pesticides or fertilizers if rain is expected within 48 hours or if wind speeds are above 5 mph.
- Do not spray pesticides within 100 feet of waterways.
- Fertilizers should be worked into the soil rather than dumped onto the surface.
- If fertilizer is spilled on the pavement or sidewalk, sweep it up immediately and place it back in the container.

Building Maintenance

- Never allow washwater, sweepings or sediment to enter the storm drain.
- Sweep up dry spills and use cat litter, towels or similar materials to absorb wet spills. Dispose of it in the trash.
- If you wash your building, sidewalk or parking lot, you **must** contain the water. Use a shop vac to collect the water and contact your city or sanitation agency for proper disposal information. Do not let water enter the street, gutter or storm drain.
- Use drop cloths underneath outdoor painting, scraping, and sandblasting work, and properly dispose of materials in the trash.
- Use a ground cloth or oversized tub for mixing paint and cleaning tools.
- Use a damp mop or broom to clean floors.
- Cover dumpsters to keep insects, animals, rainwater and sand from entering. Keep the area around the dumpster clear of trash and debris. Do not overfill the dumpster.

- Call your trash hauler to replace leaking dumpsters.
- Do not dump any toxic substance or liquid waste on the pavement, the

ground, or near a storm drain. Even materials that seem harmless such as latex paint or biodegradable cleaners can damage the environment.

Never Dispose of Anything in the Storm Drain.

- Recycle paints, solvents and other materials. For more information about recycling and collection centers, visit www.oclandfills.com.
- Store materials indoors or under cover and away from storm drains.
- Use a construction and demolition recycling company to recycle lumber, paper, cardboard, metals, masonry, carpet, plastic, pipes, drywall, rocks, dirt, and green waste. For a listing of construction and demolition recycling locations in your area, visit www.ciwmb.ca.gov/recycle.
- Properly label materials. Familiarize employees with Material Safety Data Sheets.



IC3. BUILDING MAINTENANCE

Best Management Practices (BMPs)

A BMP is a technique, measure or structural control that is used for a given set of conditions to improve the quality of the stormwater runoff in a cost effective manner¹. The minimum required BMPs for this activity are outlined in the box to the right. Implementation of pollution prevention/good housekeeping measures may reduce or eliminate the need to implement other more costly or complicated procedures. Proper employee training is key to the success of BMP implementation.

The BMPs outlined in this fact sheet target the following pollutants:

Targeted Constituents				
Sediment	Х			
Nutrients	Х			
Floatable Materials				
Metals	Х			
Bacteria	Х			
Oil & Grease				
Organics & Toxicants				
Pesticides				
Oxygen Demanding				

MINIMUM BEST MANAGEMENT PRACTICES

Pollution Prevention/Good Housekeeping

- Properly collect and dispose of water when pressure washing buildings, rooftops, and other large objects.
- Properly prepare work area before conducting building maintenance.
- Properly clean and dispose of equipment and wastes used and generated during building maintenance.
- Store toxic material under cover when not in use and during precipitation events.

Stencil storm drains

Training

- Train employees on these BMPs, storm water discharge prohibitions, and wastewater discharge requirements.
- Provide on-going employee training in pollution prevention.

Provided below are specific procedures associated with each of the minimum BMPs along with procedures for additional BMPs that should be considered if this activity takes place at a facility located near a sensitive waterbody. In order to meet the requirements for medium and high priority facilities, the owners/operators must select, install and maintain appropriate BMPs on site. Since the selection of the appropriate BMPs is a site-specific process, the types and numbers of additional BMPs will vary for each facility.

1. Properly collect and dispose of water when pressure washing buildings, rooftops, and other large objects.

- If pressure washing where the surrounding area is paved, use a water collection device that enables collection of wash water and associated solids. Use a sump pump, wet vacuum or similarly effective device to collect the runoff and loose materials. Dispose of the collected runoff and solids properly. Refer to fact sheet *IC24 Wastewater Disposal* for guidance on appropriate methods for disposal of wash water to the sanitary sewer.
- If pressure washing on a landscaped area (with or without soap), runoff must be dispersed as sheet flow as much as possible, rather than as a concentrated stream. The wash runoff must remain on the landscaping and not drain to pavement.

2. Properly prepare work area before conducting building maintenance.

- Use ground or drop cloths underneath outdoor painting, scraping, and sandblasting work, and properly dispose of collected material daily.
- Use a ground cloth or oversized tub for activities such as paint mixing and tool cleaning.

¹ EPA " Preliminary Data Summary of Urban Stormwater Best Management Practices"

- 3. Properly clean and dispose of equipment and wastes used and generated during building maintenance.
 - Clean paint brushes and tools covered with water-based paints in sinks connected to sanitary
 sewers or in portable containers that can be dumped into a sanitary sewer drain. Brushes and
 tools covered with non-water-based paints, finishes, or other materials must be cleaned in a
 manner that enables collection of used solvents (e.g., paint thinner, turpentine, etc.) for
 recycling or proper disposal.
 - Properly dispose of wash water, sweepings, and sediments.
 - Properly store equipment, chemicals, and wastes.
 - Do not dump any toxic substance or liquid waste on the pavement, the ground, or toward a storm drain.

OPTIONAL:

- Recycle residual paints, solvents, lumber, and other materials to the maximum extent practicable
- 4. Employ soil erosion and stabilization techniques when exposing large areas of soil.
 - Confine excavated materials to pervious surfaces away from storm drain inlets, sidewalks, pavement, and ditches. Material must be covered if rain is expected.
 - Use chemical stabilization or geosynthetics to stabilize bare ground surfaces.
- 5. Store toxic material under cover when not in use and during precipitation events.
- 6. Properly dispose of fluids from air conditioning, cooling tower, and condensate drains.
- 7. Regularly inspect air emission control equipment under AQMD permit.
- 8. Switch to non-toxic chemicals for maintenance when possible.
 - If cleaning agents are used, select biodegradable products whenever feasible
 - Consider using a waterless and non-toxic chemical cleaning method for graffiti removal (e.g. gels or spray compounds).
- 9. Use chemicals that can be recycled.
 - Buy recycled products to the maximum extent practicable

Training

- 1. Train employees on these BMPs, storm water discharge prohibitions, and wastewater discharge requirements.
- 2. Train employees on proper spill containment and cleanup.
 - Establish training that provides employees with the proper tools and knowledge to immediately begin cleaning up a spill.
 - Ensure that employees are familiar with the site's spill control plan and/or proper spill cleanup procedures.
 - Fact sheet IC17 discusses Spill Prevention and Control in detail.
- 3. Establish a regular training schedule, train all new employees, and conduct annual refresher training.
- 4. Use a training log or similar method to document training.

Stencil storm drains

Storm drain system signs act as highly visible source controls that are typically stenciled directly adjacent to storm drain inlets. Stencils should read "No Dumping Drains to Ocean".

References

California Storm Water Best Management Practice Handbook. Industrial and Commercial. 2003. www.cabmphandbooks.com

California Storm Water Best Management Practice Handbooks. Industrial/Commercial Best Management Practice Handbook. Prepared by Camp Dresser& McKee, Larry Walker Associates, Uribe and Associates, Resources Planning Associates for Stormwater Quality Task Force. March 1993.

King County Stormwater Pollution Control Manual. Best Management Practices for Businesses. King County Surface Water Management. July 1995. On-line: <u>http://dnr.metrokc.gov/wlr/dss/spcm.htm</u>

Stormwater Management Manual for Western Washington. Volume IV Source Control BMPs. Prepared by Washington State Department of Ecology Water Quality Program. Publication No. 99-14. August 2001.

For additional information contact:

County of Orange/ OC Watersheds Main: (714) 955-0600 24 hr Water Pollution Hotline: 1-877-89-SPILL or visit our website at www.ocwatersheds.com

IC7. LANDSCAPE MAINTENANCE

Best Management Practices (BMPs)

A BMP is a technique, measure or structural control that is used for a given set of conditions to improve the quality of the stormwater runoff in a cost effective manner¹. The minimum required BMPs for this activity are outlined in the box to the right. Implementation of pollution prevention/good housekeeping measures may reduce or eliminate the need to implement other more costly or complicated procedures. Proper employee training is key to the success of BMP implementation.

The BMPs outlined in this fact sheet target the following pollutants:

Targeted Constituents				
Sediment	Х			
Nutrients	Х			
Floatable Materials	Х			
Metals				
Bacteria	Х			
Oil & Grease				
Organics & Toxicants				
Pesticides	Х			
Oxygen Demanding	Х			

MINIMUM BEST MANAGEMENT PRACTICES Pollution Prevention/Good Housekeeping

- Properly store and dispose of gardening wastes.
- Use mulch or other erosion control measures on exposed soils.
- Properly manage irrigation and runoff.
- Properly store and dispose of chemicals.
- Properly manage pesticide and herbicide use.
- Properly manage fertilizer use.

Stencil storm drains

Training

- Train employees on these BMPs, storm water discharge prohibitions, and wastewater discharge requirements.
- Provide on-going employee training in pollution prevention.

Provided below are specific procedures associated with each of the minimum BMPs along with procedures for additional BMPs that should be considered if this activity takes place at a facility located near a sensitive waterbody. In order to meet the requirements for medium and high priority facilities, the owners/operators must select, install and maintain appropriate BMPs on site. Since the selection of the appropriate BMPs is a site-specific process, the types and numbers of additional BMPs will vary for each facility.

1. Take steps to reduce landscape maintenance requirements.

- Where feasible, retain and/or plant native vegetation with features that are determined to be beneficial. Native vegetation usually requires less maintenance than planting new vegetation.
- When planting or replanting consider using low water use flowers, trees, shrubs, and groundcovers.
- Consider alternative landscaping techniques such as naturescaping and xeriscaping.

2. Properly store and dispose of gardening wastes.

- Dispose of grass clippings, leaves, sticks, or other collected vegetation as garbage at a permitted landfill or by composting.
- Do not dispose of gardening wastes in streets, waterways, or storm drainage systems.
- Place temporarily stockpiled material away from watercourses and storm drain inlets, and berm and/or cover.
- 3. Use mulch or other erosion control measures on exposed soils.

¹ EPA " Preliminary Data Summary of Urban Stormwater Best Management Practices"

4. Properly manage irrigation and runoff.

- Irrigate slowly or pulse irrigate so the infiltration rate of the soil is not exceeded.
- Inspect irrigation system regularly for leaks and to ensure that excessive runoff is not occurring.
- If re-claimed water is used for irrigation, ensure that there is no runoff from the landscaped area(s).
- If bailing of muddy water is required (e.g. when repairing a water line leak), do not put it in the storm drain; pour over landscaped areas.
- Use automatic timers to minimize runoff.
- Use popup sprinkler heads in areas with a lot of activity or where pipes may be broken. Consider the use of mechanisms that reduce water flow to broken sprinkler heads.

5. Properly store and dispose of chemicals.

- Implement storage requirements for pesticide products with guidance from the local fire department and/or County Agricultural Commissioner.
- Provide secondary containment for chemical storage.
- Dispose of empty containers according to the instructions on the container label.
- Triple rinse containers and use rinse water as product.

6. Properly manage pesticide and herbicide use.

- Follow all federal, state, and local laws and regulations governing the use, storage, and disposal of pesticides and herbicides and training of applicators and pest control advisors.
- Follow manufacturers' recommendations and label directions.
- Use pesticides only if there is an actual pest problem (not on a regular preventative schedule). When applicable use less toxic pesticides that will do the job. Avoid use of copper-based pesticides if possible. Use the minimum amount of chemicals needed for the job.
- Do not apply pesticides if rain is expected or if wind speeds are above 5 mph.
- Do not mix or prepare pesticides for application near storm drains. Prepare the minimum amount of pesticide needed for the job and use the lowest rate that will effectively control the targeted pest.
- Whenever possible, use mechanical methods of vegetation removal rather than applying herbicides. Use hand weeding where practical.
- Do not apply any chemicals directly to surface waters, unless the application is approved and permitted by the state. Do not spray pesticides within 100 feet of open waters.
- Employ techniques to minimize off-target application (e.g. spray drift) of pesticides, including consideration of alternative application techniques.
- When conducting mechanical or manual weed control, avoid loosening the soil, which could lead to erosion.
- Purchase only the amount of pesticide that you can reasonably use in a given time period.
- Careful soil mixing and layering techniques using a topsoil mix or composted organic material can be used as an effective measure to reduce herbicide use and watering.

7. Properly manage fertilizer use.

- Follow all federal, state, and local laws and regulations governing the use, storage, and disposal of fertilizers.
- Follow manufacturers' recommendations and label directions.
- Employ techniques to minimize off-target application (e.g. spray drift) of fertilizer, including consideration of alternative application techniques. Calibrate fertilizer distributors to avoid excessive application.
- Periodically test soils for determining proper fertilizer use.
- Fertilizers should be worked into the soil rather than dumped or broadcast onto the surface.
- Sweep pavement and sidewalk if fertilizer is spilled on these surfaces before applying irrigation water.
- Use slow release fertilizers whenever possible to minimize leaching

8. Incorporate the following integrated pest management techniques where appropriate:

- Mulching can be used to prevent weeds where turf is absent.
- Remove insects by hand and place in soapy water or vegetable oil. Alternatively, remove insects with water or vacuum them off the plants.
- Use species-specific traps (e.g. pheromone-based traps or colored sticky cards).
- Sprinkle the ground surface with abrasive diatomaceous earth to prevent infestations by soft-bodied insects and slugs. Slugs also can be trapped in small cups filled with beer that are set in the ground so the slugs can get in easily.
- In cases where microscopic parasites, such as bacteria and fungi, are causing damage to plants, the affected plant material can be removed and disposed of (pruning equipment should be disinfected with bleach to prevent spreading the disease organism).
- Small mammals and birds can be excluded using fences, netting, and tree trunk guards.
- Promote beneficial organisms, such as bats, birds, green lacewings, ladybugs, praying mantis, ground beetles, parasitic nematodes, trichogramma wasps, seedhead weevils, and spiders that prey on detrimental pest species.

Training

- 1. Train employees on these BMPs, storm water discharge prohibitions, and wastewater discharge requirements.
- 2. Educate and train employees on the use of pesticides and pesticide application techniques. Only employees properly trained to use pesticides can apply them.
- 3. Train and encourage employees to use integrated pest management techniques.
- 4. Train employees on proper spill containment and cleanup.
 - Establish training that provides employees with the proper tools and knowledge to immediately begin cleaning up a spill.
 - Ensure that employees are familiar with the site's spill control plan and/or proper spill cleanup procedures.
 - Fact sheet IC17 discusses Spill Prevention and Control in detail.
- 5. Establish a regular training schedule, train all new employees, and conduct annual refresher training.
- 6. Use a training log or similar method to document training.

Stencil storm drains

Storm drain system signs act as highly visible source controls that are typically stenciled directly adjacent to storm drain inlets. Stencils should read "No Dumping Drains to Ocean".

References

California Storm Water Best Management Practice Handbook. Industrial and Commercial. 2003. www.cabmphandbooks.com

California Storm Water Best Management Practice Handbooks. Industrial/Commercial Best Management Practice Handbook. Prepared by Camp Dresser& McKee, Larry Walker Associates, Uribe and Associates, Resources Planning Associates for Stormwater Quality Task Force. March 1993.

King County Stormwater Pollution Control Manual. Best Management Practices for Businesses. King County Surface Water Management. July 1995. On-line: <u>http://dnr.metrokc.gov/wlr/dss/spcm.htm</u>

Stormwater Management Manual for Western Washington. Volume IV Source Control BMPs. Prepared by Washington State Department of Ecology Water Quality Program. Publication No. 99-14. August 2001.

Water Quality Handbook for Nurseries. Oklahoma Cooperative Extension Service. Division of Agricultural Sciences and Natural Resources. Oklahoma State University. E-951. September 1999.

For additional information contact:

County of Orange/ OC Watersheds Main: (714) 955-0600 24 hr Water Pollution Hotline: 1-877-89-SPILL or visit our website at <u>www.ocwatersheds.com</u>

IC15. PARKING AND STORAGE AREA MAINTENANCE

Best Management Practices (BMPs)

A BMP is a technique, measure or structural control that is used for a given set of conditions to improve the quality of the stormwater runoff in a cost effective manner¹. The minimum required BMPs for this activity are outlined in the box to the right. Implementation of pollution prevention/good housekeeping measures may reduce or eliminate the need to implement other more costly or complicated procedures. Proper employee training is key to the success of BMP implementation.

The BMPs outlined in this fact sheet target the following pollutants:

Targeted Constituents				
Sediment	Х			
Nutrients	Х			
Floatable Materials	Х			
Metals	Х			
Bacteria	Х			
Oil & Grease	Х			
Organics & Toxicants	Х			
Pesticides	Х			
Oxygen Demanding	Х			

MINIMUM BEST MANAGEMENT PRACTICES Pollution Prevention/Good Housekeeping

- Conduct regular cleaning.
- Properly collect and dispose of wash water.
- Keep the parking and storage areas clean and orderly.
- Use absorbent materials and properly dispose of them when cleaning heavy oily deposits.
- When conducting surface repair work cover materials and clean paintbrushes and tools appropriately.

Stencil storm drains

Training

- Train employees on these BMPs, storm water discharge prohibitions, and wastewater discharge requirements.
- Provide on-going employee training in pollution prevention.

Provided below are specific procedures associated with each of the minimum BMPs along with procedures for additional BMPs that should be considered if this activity takes place at a facility located near a sensitive waterbody. In order to meet the requirements for medium and high priority facilities, the owners/operators must select, install and maintain appropriate BMPs on site. Since the selection of the appropriate BMPs is a site-specific process, the types and numbers of additional BMPs will vary for each facility.

1. Conduct regular cleaning.

- Sweeping or vacuuming the parking facility is encouraged over other methods.
- Sweep all parking lots at least once before the onset of the wet season.
- Establish frequency of sweeping based on usage and field observations of waste accumulation.

2. Properly collect and dispose of wash water.

- Block the storm drain or contain runoff.
- Wash water should be collected and pumped to the sanitary sewer or discharged to a pervious surface, do not allow wash water to enter storm drains. Refer to fact sheet *IC24 Wastewater Disposal* for guidance on appropriate methods for disposal of wash water to the sanitary sewer.
- Dispose of parking lot sweeping debris and dirt at a landfill.
- 3. Consider use of source treatment BMPs to treat runoff.
 - Allow sheet runoff to flow into biofilters (vegetated strip and swale) and/or infiltration devices.
 - Utilize sand filters or oleophilic collectors for oily waste in low quantities.

¹ EPA " Preliminary Data Summary of Urban Stormwater Best Management Practices"

- 4. Keep the parking and storage areas clean and orderly.
 - Clean out and cover litter receptacles frequently to prevent spillage.
 - Remove debris in a timely fashion.
 - OPTIONAL:
 - Post "No Littering" signs.
- 5. When cleaning heavy oily deposits:
 - If possible, clean oily spots with absorbent materials.
 - Do not allow discharges to the storm drain.
 - Appropriately dispose of spilled materials and absorbents.
- 6. When conducting surface repair work:
 - Pre-heat, transfer or load hot bituminous material away from storm drain inlets.
 - Conduct surface repair work during dry weather to prevent contamination from contacting stormwater runoff.
 - Cover and seal nearby storm drain inlets (with waterproof material or mesh) and manholes before applying seal coat, slurry seal, etc. Leave covers in place until job is complete and clean any debris for proper disposal.
 - To avoid runoff, use only as much water as necessary for dust control.
 - Use drip pans or absorbent material to catch drips from paving equipment that is not in use. Dispose of collected material and absorbents properly.
- 7. Conduct inspections on a regular basis.
 - Designate personnel to conduct inspections of the parking facilities and stormwater conveyance systems associated with them.
 - Inspect cleaning equipment/sweepers for leaks on a regular basis.
- 8. Keep accurate maintenance logs to evaluate materials removed/stored and improvements made.
- 9. Arrange rooftop drains to prevent drainage directly onto paved surfaces.

Training

- 1. Train employees on these BMPs, storm water discharge prohibitions, and wastewater discharge requirements.
- 2. Train employees on proper spill containment and cleanup.
 - Establish training that provides employees with the proper tools and knowledge to immediately begin cleaning up a spill.
 - Ensure that employees are familiar with the site's spill control plan and/or proper spill cleanup procedures.
 - Fact sheet IC17 discusses Spill Prevention and Control in detail.
- 3. Provide regular training to field employees and/or contractors regarding cleaning of paved areas and proper operation of equipment.
- 4. Establish a regular training schedule, train all new employees, and conduct annual refresher training.
- 5. Use a training log or similar method to document training.

Stencil storm drains

Storm drain system signs act as highly visible source controls that are typically stenciled directly adjacent to storm drain inlets. Stencils should read "No Dumping Drains to Ocean".

References

California Storm Water Best Management Practice Handbook. Industrial and Commercial. 2003. www.cabmphandbooks.com

California Storm Water Best Management Practice Handbooks. Industrial/Commercial Best Management Practice Handbook. Prepared by Camp Dresser& McKee, Larry Walker Associates, Uribe and Associates, Resources Planning Associates for Stormwater Quality Task Force. March 1993.

King County Stormwater Pollution Control Manual. Best Management Practices for Businesses. King County Surface Water Management. July 1995. On-line: <u>http://dnr.metrokc.gov/wlr/dss/spcm.htm</u>

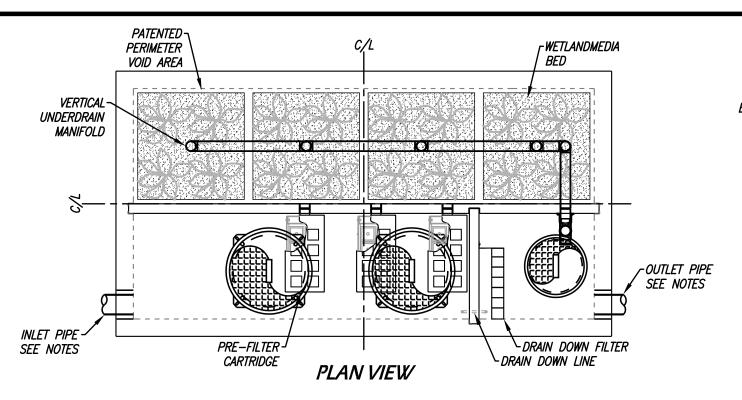
Model Urban Runoff Program: A How-To Guide for Developing Urban Runoff Programs for Small Municipalities. Prepared by City of Monterey, City of Santa Cruz, California Coastal Commission, Monterey Bay National Marine Sanctuary, Association of Monterey Bay Area Governments, Woodward-Clyde, Central Coast Regional Water Quality Control Board. July 1998 (Revised February 2002 by the California Coastal Commission).

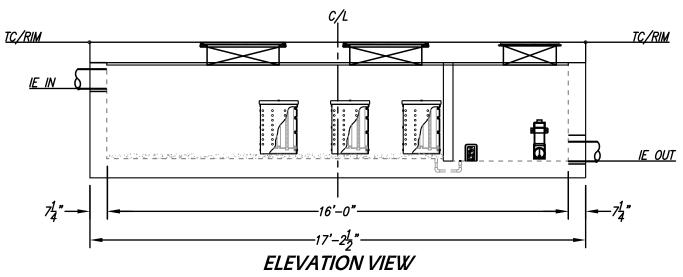
Stormwater Management Manual for Western Washington. Volume IV Source Control BMPs. Prepared by Washington State Department of Ecology Water Quality Program. Publication No. 99-14. August 2001.

For additional information contact:

County of Orange/ OC Watersheds Main: (714) 955-0600 24 hr Water Pollution Hotline: 1-877-89-SPILL or visit our website at www.ocwatersheds.com Appendix C: BMP Details

PROJECT NAME			
PROJECT LOCATI	ON		
STRUCTURE ID			
SINCEIONE ID	TREATMENT	REQUIRED	
VOLUME B		FLOW BASE	
TREATMENT HGL	AVAILABLE (FT)		
PEAK BYPASS R	EQUIRED (CFS) –	IF APPLICABLE	
PIPE DATA	<i>I.E.</i>	MATERIAL	DIAMETER
INLET PIPE 1			
INLET PIPE 2			
OUTLET PIPE			
	PRETREATMENT	BIOFILTRATION	DISCHARGE
RIM ELEVATION			
SURFACE LOAD	PARKWAY	OPEN PLANTER	PARKWAY
FRAME & COVER	ø30"	N/A	ø24"
WETLANDMEDIA V	7.26		
WETLANDMEDIA L	TBD		
ORIFICE SIZE (D		ø3.07"	
MAXIMUM PICK	WEIGHT (LBS)		TBD







- 1. CONTRACTOR TO PROVIDE ALL LABOR, EQUIPMENT, MATERIALS AND INCIDENTALS REQUIRED TO OFFLOAD AND INSTALL THE SYSTEM AND APPURTENANCES IN ACCORDANCE WITH THIS DRAWING AND THE MANUFACTURERS SPECIFICATIONS, UNLESS OTHERWISE STATED IN MANUFACTURERS CONTRACT.
- 2. UNIT MUST BE INSTALLED ON LEVEL BASE. MANUFACTURER RECOMMENDS A MINIMUM 6" LEVEL ROCK BASE UNLESS SPECIFIED BY THE PROJECT ENGINEER. CONTRACTOR IS RESPONSIBLE TO VERIFY PROJECT ENGINEERS RECOMMENDED BASE SPECIFICATIONS.
- 3. ALL PIPES MUST BE FLUSH WITH INSIDE SURFACE OF CONCRETE. (PIPES CANNOT INTRUDE BEYOND FLUSH). INVERT OF OUTFLOW PIPE MUST BE FLUSH WITH DISCHARGE CHAMBER FLOOR. ALL GAPS AROUND PIPES SHALL BE SEALED WATER TIGHT WITH A NON-SHRINK GROUT PER MANUFACTURERS STANDARD CONNECTION DETAIL AND SHALL MEET OR EXCEED REGIONAL PIPE CONNECTION STANDARDS.
- 4. CONTRACTOR TO SUPPLY AND INSTALL ALL EXTERNAL CONNECTING PIPES.
- 5. CONTRACTOR RESPONSIBLE FOR INSTALLATION OF ALL RISERS, MANHOLES, AND HATCHES. CONTRACTOR TO GROUT ALL MANHOLES AND HATCHES TO MATCH FINISHED SURFACE UNLESS SPECIFIED OTHERWISE.
- 6. DRIP OR SPRAY IRRIGATION REQUIRED ON ALL UNITS WITH VEGETATION.

GENERAL NOTES

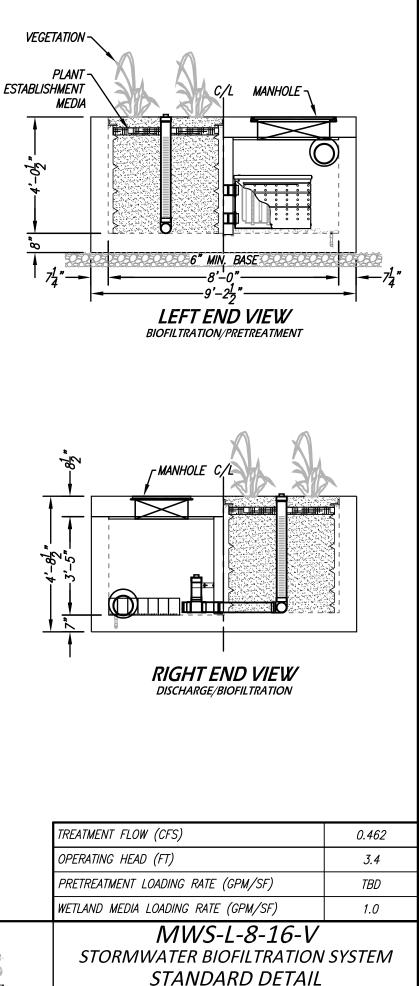
- 1. MANUFACTURER TO PROVIDE ALL MATERIALS UNLESS OTHERWISE NOTED.
- 2. ALL DIMENSIONS, ELEVATIONS, SPECIFICATIONS AND CAPACITIES ARE SUBJECT TO CHANGE. FOR PROJECT SPECIFIC DRAWINGS DETAILING EXACT DIMENSIONS, WEIGHTS AND ACCESSORIES PLEASE CONTACT MANUFACTURER.

THE PRODUCT DESCRIBED MAY BE PROTECTED BY ONE OR MORE OF THE FOLLOWING US PATENTS: 7,425,262; 7,470,362; 7,674,378; 8,303,816; RELATED FOREIGN PATENTS OR OTHER PATENTS PENDING

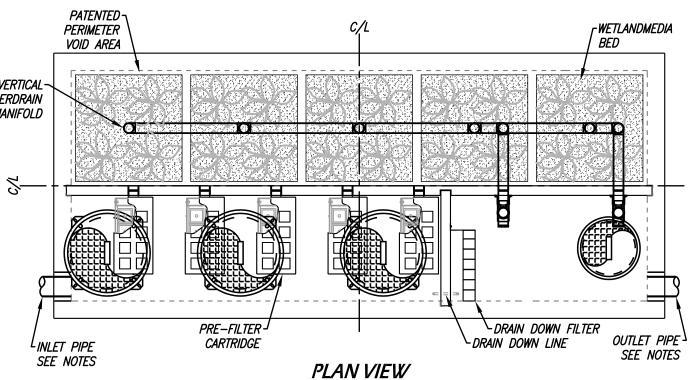
PROPRIETARY AND CONFIDENTIAL:

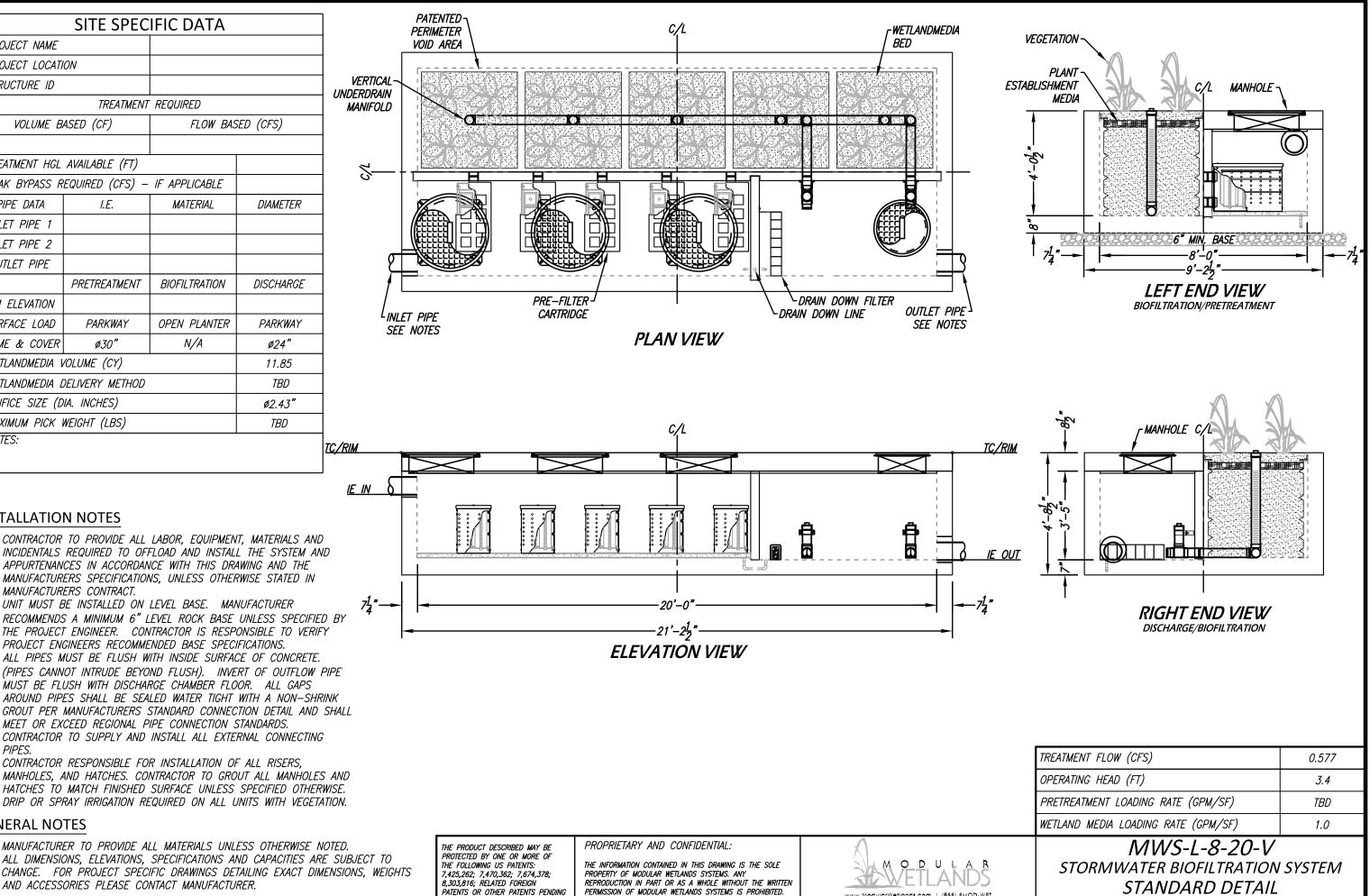
THE INFORMATION CONTAINED IN THIS DRAWING IS THE SOLE PROPERTY OF MODULAR WETLANDS SYSTEMS. ANY REPRODUCTION IN PART OR AS A WHOLE WITHOUT THE WRITTEN PERMISSION OF MODULAR WETLANDS SYSTEMS IS PROHIBITED.





	SITE SPEC	IFIC DATA			
PROJECT NAME					
PROJECT LOCAT	'ON				
STRUCTURE ID					
	TREATMENT	REQUIRED			
VOLUME B	ASED (CF)	FLOW BAS	ED (CFS)		
TREATMENT HGL	AVAILABLE (FT)				
PEAK BYPASS R	PEQUIRED (CFS) –	IF APPLICABLE			
PIPE DATA	<i>I.E.</i>	MATERIAL	DIAMETER		
INLET PIPE 1					
INLET PIPE 2					
OUTLET PIPE					
	PRETREATMENT	BIOFILTRATION	DISCHARGE		
RIM ELEVATION					
SURFACE LOAD	PARKWAY	OPEN PLANTER	PARKWAY		
FRAME & COVER	ø30"	N/A	ø24"		
WETLANDMEDIA		11.85			
	TBD				
WETLANDMEDIA L	ORIFICE SIZE (DIA. INCHES)				
	NA. INCHES)		ø2.43"		





PROJECT ENGINEERS RECOMMENDED BASE SPECIFICATIONS. 3. ALL PIPES MUST BE FLUSH WITH INSIDE SURFACE OF CONCRETE. (PIPES CANNOT INTRUDE BEYOND FLUSH). INVERT OF OUTFLOW PIPE MUST BE FLUSH WITH DISCHARGE CHAMBER FLOOR. ALL GAPS AROUND PIPES SHALL BE SEALED WATER TIGHT WITH A NON-SHRINK GROUT PER MANUFACTURERS STANDARD CONNECTION DETAIL AND SHALL MEET OR EXCEED REGIONAL PIPE CONNECTION STANDARDS.

THE PROJECT ENGINEER. CONTRACTOR IS RESPONSIBLE TO VERIFY

1. CONTRACTOR TO PROVIDE ALL LABOR, EQUIPMENT, MATERIALS AND

2. UNIT MUST BE INSTALLED ON LEVEL BASE. MANUFACTURER

APPURTENANCES IN ACCORDANCE WITH THIS DRAWING AND THE MANUFACTURERS SPECIFICATIONS, UNLESS OTHERWISE STATED IN

- CONTRACTOR TO SUPPLY AND INSTALL ALL EXTERNAL CONNECTING 4. PIPES.
- 5. CONTRACTOR RESPONSIBLE FOR INSTALLATION OF ALL RISERS, MANHOLES, AND HATCHES. CONTRACTOR TO GROUT ALL MANHOLES AND HATCHES TO MATCH FINISHED SURFACE UNLESS SPECIFIED OTHERWISE.
- 6. DRIP OR SPRAY IRRIGATION REQUIRED ON ALL UNITS WITH VEGETATION.

GENERAL NOTES

INSTALLATION NOTES

MANUFACTURERS CONTRACT.

- MANUFACTURER TO PROVIDE ALL MATERIALS UNLESS OTHERWISE NOTED. 1
- ALL DIMENSIONS, ELEVATIONS, SPECIFICATIONS AND CAPACITIES ARE SUBJECT TO 2. CHANGE. FOR PROJECT SPECIFIC DRAWINGS DETAILING EXACT DIMENSIONS, WEIGHTS AND ACCESSORIES PLEASE CONTACT MANUFACTURER.





Section [____] Modular Subsurface Flow Wetland System

PART 1 – GENERAL

01.01.00 Purpose

The purpose of this specification is to establish generally acceptable criteria for Modular Subsurface Flow Wetland Systems used for biofiltration of stormwater runoff including dry weather flows and other contaminated water sources. It is intended to serve as a guide to producers, distributors, architects, engineers, contractors, plumbers, installers, inspectors, agencies and users; to promote understanding regarding materials, manufacture and installation; and to provide for identification of devices complying with this specification.

01.02.00 Description

Modular Subsurface Flow Wetland Systems (MSFWS) are used for filtration of stormwater runoff including dry weather flows. The MSFWS is a pre-engineered biofiltration system composed of a pretreatment chamber containing filtration cartridges, a horizontal flow biofiltration chamber with a peripheral void area and a centralized and vertically extending underdrain, the biofiltration chamber containing a sorptive media mix which does not contain any organic material and a layer of plant establishment media, and a discharge chamber containing an orifice control structure . Treated water flows horizontally in series through the pretreatment chamber cartridges, biofiltration chamber and orifice control structure.

01.03.00 Manufacturer

The manufacturer of the MSFWS shall be one that is regularly engaged in the engineering design and production of systems developed for the treatment of stormwater runoff for at least (10) years, and which have a history of successful production, acceptable to the engineer of work. In accordance with the drawings, the MSFWS(s) shall be a filter device Manufactured by Bio Clean or assigned distributors or licensees. Bio Clean can be reached at:

Corporate Headquarters: Bio Clean 398 Via El Centro Oceanside, CA 92058 Phone: (855) 566-3938 Fax: (760) 433-3176 www.biocleanenvironmental.com



01.04.00 Submittals

01.04.01 Shop drawings are to be submitted with each order to the contractor and consulting engineer.

01.04.02 Shop drawings are to detail the MSFWS and all components required and the sequence for installation, including:

- System configuration with primary dimensions
- Interior components
- Any accessory equipment called out on shop drawings
- 01.04.03 Inspection and maintenance documentation submitted upon request.

01.05.00 Work Included

01.05.01	Specification requirements for installation of MSFWS.
01.05.02	Manufacturer to supply components of the MSFWS(s):
	Ducture stars and all such an assure such that (such as a such la

- Pretreatment chamber components (pre-assembled)
- Concrete Structure(s)
- Biofiltration chamber components (pre-assembled)
- Flow control discharge structure (pre-assembled)

01.06.00 Reference Standards

Standard Test Method for Unit Weight and Voids in Aggregate
C 88 Standard Test Method for Soundness of Aggregates by Use of Sodium
Sulfate or Magnesium Sulfate
C 131 Standard Test Method for Resistance to Degradation of Small-Size
Coarse Aggregates by Abrasion and Impact in the Los Angeles Machine
C 136 Standard Test Method for Sieve Analysis of Fine and Coarse Aggregates
C 330 Standard Specification for Lightweight Aggregate for Structural Concrete
Test Method for Laboratory Compaction Characteristics of Soil Using Standard
Effort (12,400 ftlbf/ft3 (600 kN-m/m3)
10 Standard Test Method for Compressive Properties Of Rigid Cellular Plastics
ASTM D1777 - 96(2007) Standard Test Method for Thickness of Textile
Materials
Standard Test Method for Determining the (In-plane) Flow Rate per Unit Width
and Hydraulic Transmissivity of a Geosynthetic Using a Constant Head
Standard Method of Test for Moisture-Density Relations of Soils Using a 2.5-kg
(5.5-lb) Rammer and a 305-mm (12-in) Drop
Standard Method of Test for Soundness of Aggregate by Use of Sodium Sulfate
or Magnesium Sulfate
Standard Method of Test for Sampling and Testing for Chloride Ion in Concrete
and Concrete Raw Materials.
Standard Method of Test for Determining Minimum Laboratory Soil Resistivity
Standard Method of Test for Determining ph of Soil for Use in Corrosion Testing
Standard Method of Test for Determining Water Soluble Chloride Ion Content in
Soil
T 290 Standard Method of Test for Determining Water Soluble Sulfate Ion
Content in Soil



PART 2 – COMPONENTS

The Modular Subsurface Flow Wetland Systems (MSFWS) and all of its components shall be self-contained within a concrete structure constructed of concrete with a minimum 28 day compressive strength of 5,000 psi, with reinforcing per ASTM A 615, Grade 60, and supports and H20 loading as indicated by AASHTO. Each Chamber shall have appropriate access hatches for easy maintenance and sized to allow removal of all internal components without disassembly. All water transfer system components shall conform with the following;

- Filter netting shall be 100% Polyester with a number 16 sieve size, and strength tested per ASTM D 3787.
- Drainage cells shall be manufactured of lightweight injectionmolded plastic and have a minimum compressive strength test of 6,000 psi and a void area along the surface making contact with the filter media of 75% or greater. The cells shall be at least 2" in thickness and allow water to freely flow in all four directions.

02.01.00 Pretreatment Chamber Components

- 02.01.01 <u>Filter Cartridges</u> shall operate at a loading rate not to exceed 3 gallons per minute per square foot surface area.
- 02.01.02 <u>Drain Down System</u> shall include a pervious floor that allows water to drain into the underdrain pipe that is connected to the discharge chamber.

02.02.00 Biofiltration Chamber Components

02.02.01	Media shall consist of ceramic material produced by expanding and vitrifying select material in a rotary kiln. Media must be produced to meet the requirements of ASTM C330, ASTM C331, and AASHTO M195. Aggregates must have a minimum 24-hour water absorption of 10.5% mass. Media shall not contain any organic material. Flow through media shall be horizontal from the outer perimeter of the chamber toward the centralized and vertically extending underdrain. The retention time in the media shall be at least 3 minutes. Downward flow filters are not acceptable alternatives. The thickness of the media shall be at least 19" from influent end to effluent end. The loading rate on the media shall not exceed 1.1 gallons per minute per square foot surface area. Media must be contained within structure that spaces the surface of the media at least 2" from all vertically extending walls of the concrete structure.
02.02.02	Planting shall be native, drought tolerant species recommend by manufacturer and/or landscape architect.
02.02.03	<u>Plant Support Media</u> shall be made of a 3" thick moisture retention cell that is inert and contains no chemicals or fertilizers, is not made of organic material and has an internal void percentage of 80%.

02.03.00 Discharge Chamber

The discharge device shall house a flow control orifice plate that restricts flows greater than designed treatment flow rate. All piping components shall be made of a high-density polyethylene. The discharge chamber shall also contain a drain down filter if specified on the drawing.



PART 3 – PERFORMANCE

03.01.00 General

- 03.01.01 Function - The MSFWS has no moving internal components and functions based on gravity flow, unless otherwise specified. The MSFWS is composed of a pretreatment chamber, a biofiltration chamber and a discharge chamber. The pretreatment device houses cartridge media filters, which consist of filter media housed in a perforated enclosure. The untreated runoff flows into the system via subsurface piping and or surface inlet. Water entering the system is forced through the filter cartridge enclosures by gravity flow. Then the flow contacts the filter media. The flow through the media is horizontal toward the center of each individual media filter. In the center of the media shall be a round slotted PVC pipe of no greater than 1.5" in diameter. The slotted PVC pipe shall extend downward into the water transfer cavity of the cartridge. The slotted PVC pipe shall be threaded on the bottom to connect to the water transfer cavity. After pollutants have been removed by the filter media the water discharges the pretreatment chamber and flows into the water transfer system and is conveyed to the biofiltration chamber. Once runoff has been filtered by the biofiltration chamber it is collected by the vertical underdrain and conveyed to a discharge chamber equipped with a flow control orifice plate. Finally the treated flow exits the system.
- 03.01.02 <u>Pollutants</u> The MSFWS will remove and retain debris, sediments, TSS, dissolved and particulate metals and nutrients including nitrogen and phosphorus species, bacteria, BOD, oxygen demanding substances, organic compounds and hydrocarbons entering the filter during frequent storm events and continuous dry weather flows.
- 03.01.03 <u>Treatment Flow Rate and Bypass</u> The MSFWS operates in-line. The MSFWS will treat 100% of the required water quality treatment flow based on a minimum filtration capacities listed in section 03.02.00. The size of the system must match those provided on the drawing to ensure proper performance and hydraulic residence time.

Minimum Treatment Capabilities

• System must be capable of treating flows to the specified treatment flow rate on the drawings. The flow rate shall be controlled by an orifice plate.

PART 4 - EXECUTION

04.01.00 General

The installation of the MSFWS shall conform to all applicable national, state, state highway, municipal and local specifications.

04.02.00 Installation

The Contractor shall furnish all labor, equipment, materials and incidentals required to install the (MSFWS) device(s) and appurtenances in accordance with the drawings and these specifications.



A Forterra Company

04.02.01	<u>Grading and Excavation</u> site shall be properly surveyed by a registered professional surveyor, and clearly marked with excavation limits and elevations After site is marked it is the responsibility of the contractor to contact local utility companies and/or DigAlert to check for underground utilities. All grading permits shall be approved by governing agencies before commencement of grading and excavation. Soil conditions shall be tested in accordance with the governing agencies requirements. All earth removed shall be transported, disposed, stored, and handled per governing agencies standards. It is the responsibility of the contractor to install and maintain proper erosion control
	measures during grading and excavation operations.
04.02.02	<u>Compaction</u> – All soil shall be compacted per registered professional soils engineer's recommendations prior to installation of MSFWS components.
04.02.03	<u>Backfill</u> shall be placed according to a registered professional soils engineer's recommendations, and with a minimum of 6" of gravel under all concrete structures.
04.02.04	<u>Concrete Structures</u> – After backfill has been inspected by the governing agency and approved the concrete structures shall be lifted and placed in proper position per plans.
04.02.05	Subsurface Flow Wetland Media shall be carefully loaded into area so not to damage the Wetland Liner or Water Transfer Systems. The entire wetland area shall be filled to a level 9 inches below finished surface.
04.02.06	<u>Planting</u> layer shall be installed per manufacturer's drawings and consist of a minimum 3" grow enhancement media that ensures greater than 95% plant survival rate, and 6" of wetland media. Planting shall consist of native plants recommended by manufacturer and/or landscape architect. Planting shall be drip irrigated for at least the first 3 months to insure long term plant growth. No chemical herbicides, pesticides, or fertilizers shall be used in the planting or care and maintenance of the planted area.

04.03.00 Shipping, Storage and Handling

- 04.03.01 <u>Shipping</u> MSFWS shall be shipped to the contractor's address or job site, and is the responsibility of the contractor to offload the unit(s) and place in the exact site of installation.
- 04.03.02 <u>Storage and Handling</u>– The contractor shall exercise care in the storage and handling of the MSFWS and all components prior to and during installation. Any repair or replacement costs associated with events occurring after delivery is accepted and unloading has commenced shall be born by the contractor. The MSFWS(s) and all components shall always be stored indoors and transported inside the original shipping container until the unit(s) are ready to be installed. The MSFWS shall always be handled with care and lifted according to OSHA and NIOSA lifting recommendations and/or contractor's workplace safety professional recommendations.

04.04.00 Maintenance and Inspection

04.04.01 <u>Inspection</u> – After installation, the contractor shall demonstrate that the MSFWS has been properly installed at the correct location(s), elevations, and with appropriate components. All components associated with the MSFWS and its installation shall be subject to inspection by the engineer at the place of installation. In addition, the contractor shall demonstrate that the MSFWS has been installed per the manufacturer's specifications and recommendations. All



A Forterra Company

components shall be inspected by a qualified person once a year and results of inspection shall be kept in an inspection log.

04.04.02 <u>Maintenance</u> – The manufacturer recommends cleaning and debris removal maintenance of once a year and replacement of the Cartridge Filters as needed. The maintenance shall be performed by someone qualified. A Maintenance Manual is available upon request from the manufacturer. The manual has detailed information regarding the maintenance of the MSFWS. A Maintenance/Inspection record shall be kept by the maintenance operator. The record shall include any maintenance activities preformed, amount and description of debris collected, and the condition of the filter.
 04.04.03 <u>Material Disposal</u> - All debris, trash, organics, and sediments captured by the MSFWS shall be transported and disposed of at an approved facility for disposal in accordance with local and state requirements. Please refer to state and local regulations for the proper disposal of toxic and non-toxic material.

PART 5 – QUALITY ASSURNACE

05.01.00 Warranty

The Manufacturer shall guarantee the MSFWS against all manufacturing defects in materials and workmanship for a period of (5) years from the date of delivery to the ______. The manufacturer shall be notified of repair or replacement issues in writing within the warranty period. The MSFWS is limited to recommended application for which it was designed.

05.02.00 Performance Certification

The MSFWS manufacturer shall submit to the Engineer of Record a "Manufacturer's Performance Certificate" certifying the MSFWS is capable of achieving the specified removal efficiency for suspended solids, phosphorous and dissolved metals.

PERFORMANCE SUMMARY MWS-LINEAR 2.0

Application: Stand Alone Stormwater Treatment Best Management Practice **Type of Treatment:** High Flow Rate Media Filtration and Biofiltration (dual-stage)

DESCRIPTION

Modular Wetland System Linear 2.0 (MWS-L 2.0) is an advanced dual-stage high flow rate media and biofiltration system for the treatment of urban stormwater runoff. Superior pollutant removal efficiencies are achieved by treating runoff through a pre-treatment chamber containing a screening device for trash and larger debris, a separation chamber for larger TSS and a series of media filter cartridges for removal of fine TSS and other particulate pollutants. Pre-treated runoff is transferred to the biofiltration chamber which contains an engineered ion exchange media designed to support an abundant plant and microbe community that captures, absorbs, transforms and uptakes pollutants through an array of physical, chemical, and biological mechanisms.

MWS-L 2.0 is a self-contained treatment train that is supplied to the job site completely assembled and ready for use. Once installed, stormwater runoff drains directly from impervious surfaces through an built-in curb inlet, drop in, or via pipe from upstream inlets or downspouts. Treated runoff is discharged from the system through an orifice control riser to assure the proper amount of flow is treated. The treated water leaving the system is connected to the storm drain system, infiltration basins, or to be re-used on site for irrigation or other uses.



HEAVY METALS: Copper / Zinc

Description	Туре	Avg. Influent (mg/L)	Avg. Effluent (mg/L)	Removal Efficiency	Notes
Waves Environmen- tal - 1/4 Scale Lab Testing - 2007	Lab	.76 / .95	.06 / .19	92% / 80%	Majority Dissolved Fraction
City of Oceanside Boat Wash / Waves Environmental - 2008	Field	.04 / .24	< .02 / < .05	>50% / >79%	Effluent Concentra- tions Below Detectable Limits
Recycling Facility, Kileen, TX / CERL - 2011-2012	Field	.058 / .425	.032 / .061	44% / 86%	Test Unit 2
TAPE Field Test- ing / Portland, OR 2011/2012	Field	.017/ .120	.009 / .038	50% / 69%	Total Metals

TOTAL SUSPENDED SOLIDS:

Description	Туре	Avg. Influent (mg/L)	Avg. Effluent (mg/L)	Removal Efficiency	Notes
Waves Environmen- tal - 1/4 Scale Lab Testing - 2007	Lab	270	3	99%	Sil-co-sil 106 - 20 micron mean par- ticle size
City of Oceanside Boat Wash / Waves Environmental - 2008	Field	45.67	8.24	82%	Mean Particle Size by Count < 8 Microns
Recycling Facility, Kileen, TX / CERL - 2011-2012	Field	676	39	94%	Test Unit 2
TAPE Field Test- ing / Portland, OR 2011/2012	Field	75.0	15.7	85%	Means par- ticle size of 8 microns



Modular Wetland System, Inc. 2972 San Luis Rey Rd Oceanside, CA 92058

Nature & Technology Working Together In Perfect Harmony™

www.modularwetlands.com P 760-433-7640 F 760-433-3179

PERFORMANCE SUMMARY **MWS-LINEAR 2.0**

Removal

Efficiency

64%

67%

Avg.

Effluent

(MPN)

535 /

637

8667 /

1058

Notes

TOTAL P

ORTHO P

Removal

Efficiency

67% /

60%

73% /

83%

Notes

Fecal /

E. Coli

Fecal /

E. Coli

PHOSPHORUS:

Avg.

Effluent

(mg/L)

.074

.031

Avg.

Influent

(mg/L)

.227

.093

BACTERIA:

Avg. Influent

(MPN)

1600 /

1600

31666 /

6280

Type

Field

Field

Type

Lab

Field

Description

TAPE Field Testing / Portland, OR

2011/2012 TAPE Field Testing / Portland, OR

2011/2012

Description

Waves Environmen-

tal - 1/4 Scale Lab

Testing - 2007 City of Oceanside

Boat Wash / Waves

Environmental - 2008

NITROGEN:

Description	Туре	Avg. Influent (mg/L)	Avg. Effluent (mg/L)	Removal Efficiency	Notes
City of Oceanside Boat Wash / Waves Environmental - 2008	Field	.85	.21	75%	NITRATE
TAPE Field Test- ing / Portland, OR 2011/2012	Field	1.40	0.77	45%	TKN

HYDROCARBONS:

Description	Туре	Avg. Influent (mg/L)	Avg. Effluent (mg/L)	Removal Efficiency	Notes
Waves Environmen- tal - 1/4 Scale Lab Testing - 2007	Lab	10	1.625	84%	Oils & Grease
City of Oceanside Boat Wash / Waves Environmental - 2008	Field	.83	0	100%	TPH Motor Oil
TAPE Field Test- ing / Portland, OR 2011/2012	Field	24.157	1.133	95%	Motor Oil

TURBIDITY:

Description	Туре	Avg. Influent (NTU)	Avg. Effluent (NTU)	Removal Efficiency	Notes
Waves Environmen- tal - 1/4 Scale Lab Testing - 2007	Lab	21	1.575	93%	Field Measure- ment
City of Oceanside Boat Wash / Waves Environmental - 2008	Field	21	6	71%	Field Measure- ment

COD:

Description	Туре	Avg. Influent (mg/L)	Avg. Effluent (mg/L)	Removal Efficiency	Notes
Recycling Facility, Kileen, TX / CERL - 2011-2012	Field	516 / 1450	90 / 356	83% / 75%	Both Test Units

Nature & Technology Working Together In Perfect Harmony™

www.modularwetlands.com P 760-433-7640 F 760-433-3179

LEAD:

Description	Туре	Avg. Influent (mg/L)	Avg. Effluent (mg/L)	Removal Efficiency	Notes
Waves Environmen- tal - 1/4 Scale Lab Testing - 2007	Lab	.54	.10	82%	Total
Recycling Facility, Kileen, TX / CERL - 2011-2012	Field	.01 / .043	.004 / .014	60% / 68%	Both Test Units
TAPE Field Test- ing / Portland, OR 2011/2012	Field	.011	.003	70%	Total

All removal efficiencies and concentrations rounded up for easy viewing. Please call us for more information, including full copies of the reports reference above.

MODULA



Modular Wetlands and Pesticides

Independent field data using the Modular Wetlands System was obtained showing the removal of Tetrachlorphenol and Pentachlorophenol (herbicides/pesticides). The following test results outline the analyte removal results in mg/Kg.

Analyte	Sample A Inlet mg/Kg	Sample B Outlet mg/Kg	Sample C Inlet mg/Kg	Sample D Outlet mg/Kg
Oil	6980	<560	5260	<530
Tetrachlorophenol 5	3.4	<2.5	4.6	<2.5
Tetrachlorophenol 6	9	4.9	9.7	5.4
Pentachlorophenol	47	16	52	22

*Data sample matrix consisted of untreated influent water and was conducted independently by SPECTRA Laboratories

Sean M. Hasan

Western Regional Director



398 Via El Centro, Oceanside, CA 92058 (760) 433-7640 • Fax (760) 433-3176 www.BioCleanEnvironmental.com

2221 Ross Way • Tacoma, WA 98421 • (253) 272-4850 • Fax (253) 572-9838 • www.spectra-lab.com

05/12/2015

Tacoma Public Utilities PO Box 11007 Tacoma, WA 98411 Attn: Mike Rhubright

P.O.#: 15-04-20-024 Project: SW Substation Pole Yard Client ID: Pole Yard Separator 2nd Ch. Sample Matrix: Water Date Sampled: 04/20/2015 Date Received: 04/20/2015 Spectra Project: 2015040532 Spectra Number:1

Analyte	Result	Units	Method	Analyte	Dogula	T T., *4	N.C. (1)
Diesel	<25000	μg/L	NWTPH-D		Result	Units	Method
Oil	1200000	μg/L	NWTPH-D	3,3-Dichlorobenzidine	<2000	μg/L	SW846 8270D
1,2,4-Trichlorobenzene				3-Nitroaniline	<250	μg/L	SW846 8270D
	<250	μg/L	SW846 8270D	4,6-Dinitro-2-Methylphenol	<1000	μg/L	SW846 8270D
1,2-Dichlorobenzene	<250	μg/L	SW846 8270D	4-Bromophenyl-phenylether	<250	μg/L	SW846 8270D
1,3-Dichlorobenzene	<250	μg/L	SW846 8270D	4-Chloro-3-Methylphenol	<250	μg/L	SW846 8270D
1,4-Dichlorobenzene	<250	μg/L	SW846 8270D	4-Chloroaniline	<250	μg/L	SW846 8270D
2,3,4,5-Tetrachlorophenol	<250	μg/L	SW846 8270D	4-Chlorophenyl-phenylether	<250		
2,3,4,6-Tetrachlorophenol	<250	μg/L	SW846 8270D	4-Methylphenol	<250	μg/L	SW846 8270D
2,4,5-Trichlorophenol	<250	μg/L	SW846 8270D	4-Nitroaniline		μg/L	SW846 8270D
2,4,6-Trichlorophenol	<250	μg/L	SW846 8270D		<250	μg/L	SW846 8270D
2,4-Dichlorophenol	<250	μg/L	SW846 8270D	4-Nitrophenol	<250	μg/L	SW846 8270D
2,4-Dimethylphenol	<250			Acenaphthene	<100	μg/L	SW846 8270D
		µg/L	SW846 8270D	Acenaphthylene	<100	μg/L	SW846 8270D
2,4-Dinitrophenol	<1000	μg/L	SW846 8270D	Aniline	<1000	μg/L	SW846 8270D
2,4-Dinitrotoluene	<250	μg/L	SW846 8270D	Anthracene	<100	μg/L	SW846 8270D
2,6-Dinitrotoluene	<250	μg/L	SW846 8270D	Azobenzene	<250	μg/L	SW846 8270D
2-Chloronaphthalene	<250	μg/L	SW846 8270D	Benzidine	<2000	-	
2-Chlorophenol	<250	μg/L	SW846 8270D	Benzo(a)Anthracene		μg/L	SW846 8270D
2-Methylnaphthalene	<100	μg/L	SW846 8270D	_	<100	μg/L	SW846 8270D
2-Methylphenol	<250			Benzo(a)Pyrene	<100	μg/L	SW846 8270D
2-Nitroaniline		µg/L	SW846 8270D	Benzo(b)Fluoranthene	<100	μg/L	SW846 8270D
	<250	μg/L	SW846 8270D	Benzo(ghi)Perylene	<100	μg/L	SW846 8270D
2-Nitrophenol	<250	µg/L	SW846 8270D	Benzo(k)Fluoranthene	<100	< μg/L	SW846 8270D
						ro-~	~ 0 10 02 / 0D

Surrogate	Recovery	Method	Surrogate	Recovery	Method
p-Terphenyl	0	NWTPH-D	Phenol-d6	0*	
Nitrobenzene-d6	0*	SW846 8270D		04	SW846 8270D
n Tamband did			2-Fluorophenol	0*	SW846 8270D
p-Terphenyl-d14	0*	SW846 8270D	2,4,6-Tribromophenol	0*	SW846 8270D
2-Fluorobiphenyl	0*	SW846 8270D	.,	v	3 W 040 82/UD
SPECTRA LABORATO	RIES				

2221 Ross Way • Tacoma, WA 98421 • (253) 272-4850 • Fax (253) 572-9838 • www.spectra-lab.com

05/12/2015

Tacoma Public Utilities PO Box 11007 Tacoma, WA 98411 Attn: Mike Rhubright

P.O.#: 15-04-20-024 Project: SW Substation Pole Yard Client ID: Pole Yard Separator 2nd Ch. Sample Matrix: Water Date Sampled: 04/20/2015 Date Received: 04/20/2015 Spectra Project: 2015040532 Spectra Number:1

Analyte	Result	Units	Method
Benzoic Acid	<1000	 μg/L	SW846 8270D
Benzyl Alcohol	<250	μg/L	SW846 8270D
Biphenyl	<250	μg/L	SW846 8270D
Bis(2-Chloroethyl)Ether	<250	μg/L	SW846 8270D
Butylbenzyl phthalate	<250	μg/L	SW846 8270D
Carbazole	<250	μg/L	SW846 8270D
Chrysene	<100	μg/L	SW846 8270D
Di-n-Butylphthalate	<250	μg/L	SW846 8270D
Di-n-Octyl Phthalate	<250	μg/L	SW846 8270D
Dibenzo(a,h)Anthracene	<100	μg/L	SW846 8270D
Dibenzofuran	<250	μg/L	SW846 8270D
Dibenzothiophene	<250	μg/L	SW846 8270D
Diethylphthalate	<250	μg/L	SW846 8270D
Dimethyl Phthalate	<250	μg/L	SW846 8270D
Fluoranthene	<100	μg/L	SW846 8270D
Fluorene	<100	μg/L	SW846 8270D
Hexachlorobenzene	<250	μg/L	SW846 8270D
Hexachlorobutadiene	<250	μg/L	SW846 8270D
Hexachlorocyclopentadiene	<250	μg/L	SW846 8270D
Hexachloroethane	<250	μg/L	SW846 8270D
Indeno(1,2,3-cd)Pyrene	<100	μg/L	SW846 8270D

Analyte	Result	<u>Units</u>	Method
Isophorone	<250	μg/L	SW846 8270D
N-Nitroso-Di-n-Propylamine	<250	μg/L	SW846 8270D
N-Nitrosodiphenylamine	<250	μg/L	SW846 8270D
N-nitrosodimethylamine	<250	μg/L	SW846 8270D
Naphthalene	<100	μg/L	SW846 8270D
Nitrobenzene	<250	μg/L	SW846 8270D
Pentachlorophenol	25700	μg/L	SW846 8270D
Phenanthrene	<100	μg/L	SW846 8270D
Phenol	<250	μg/L	SW846 8270D
Pyrene	<100	μg/L	SW846 8270D
Pyridine	<1000	μg/L	SW846 8270D
bis(2-Chloroethoxy)Methane	<250	μg/L	SW846 8270D
bis(2-Ethylhexyl)Phthalate	<250	μg/L	SW846 8270D
bis(2-chloroisopropyl)Ether	<250	μg/L	SW846 8270D

Surrogate	Recovery	Method	Surrogate	Recovery	Method
p-Terphenyl	0	NWTPH-D	Phenol-d6	0*	
Nitrobenzene-d6	0*	SW846 8270D	2-Fluorophenol	0*	SW846 8270D
p-Terphenyl-d14	0*	SW846 8270D	2.4,6-Tribromophenol	-	SW846 8270D
2-Fluorobiphenyl	0*	SW846 8270D		0*	SW846 8270D
SPECTRA LABORATO	RIES				

2221 Ross Way • Tacoma, WA 98421 • (253) 272-4850 • Fax (253) 572-9838 • www.spectra-lab.com

05/12/2015

Tacoma Public Utilities PO Box 11007 Tacoma, WA 98411 Attn: Mike Rhubright

P.O.#: 15-04-20-024 Project: SW Substation Pole Yard Client ID: Pole Yard Separator 1st Ch. Sample Matrix: Sludge Date Sampled: 04/20/2015 Date Received: 04/20/2015 Spectra Project: 2015040532 Spectra Number:2

Analyte	Result	Units	Method	Analyte	Result	Units	Method
Diesel	<9000	mg/Kg	NWTPH-D	4,6-Dinitro-2-Methylphenol	<21	mg/Kg	·
Oil	138000	mg/Kg	NWTPH-D	4-Bromophenyl-phenylether	<5.25	mg/Kg	
1,2,4-Trichlorobenzene	<5.25	mg/Kg	SW846 8270D	4-Chloro-3-Methylphenol	<5.25	mg/Kg	SW846 8270D
1,2-Dichlorobenzene	<5.25	mg/Kg	SW846 8270D	4-Chloroaniline	<5.25	mg/Kg	
1,3-Dichlorobenzene	<5.25	mg/Kg	SW846 8270D	4-Chlorophenyl-phenylether	<5.25		SW846 8270D
1,4-Dichlorobenzene	<5.25	mg/Kg	SW846 8270D	4-Methylphenol	19.2	mg/Kg	SW846 8270D
2,4,5-Trichlorophenol	6.03	mg/Kg	SW846 8270D	4-Nitroaniline	<5.25	mg/Kg	SW846 8270D
2,4,6-Trichlorophenol	13.2	mg/Kg	SW846 8270D	4-Nitrophenol		mg/Kg	SW846 8270D
2,4-Dichlorophenol	<5.25	mg/Kg	SW846 8270D	Acenaphthene	<5.25	mg/Kg	SW846 8270D
2,4-Dimethylphenol	<5.25	mg/Kg	SW846 8270D	Acenaphthylene	<2.20	mg/Kg	SW846 8270D
2,4-Dinitrophenol	<21	mg/Kg	SW846 8270D	Aniline	<2.20	mg/Kg	SW846 8270D
2,4-Dinitrotoluene	<5.25	mg/Kg	SW846 8270D	Anthracene	<21	mg/Kg	SW846 8270D
2,6-Dinitrotoluene	<5.25	mg/Kg	SW846 8270D	Azobenzene	8.62	mg/Kg	SW846 8270D
2-Chloronaphthalene	<5.25	mg/Kg	SW846 8270D	Benzidine	<5.25	mg/Kg	SW846 8270D
2-Chlorophenol	<5.25	mg/Kg	SW846 8270D		<42	mg/Kg	SW846 8270D
2-Methylnaphthalene	<2.20	mg/Kg	SW846 8270D	Benzo(a)Anthracene	<2.20	mg/Kg	SW846 8270D
2-Methylphenol	<5.25			Benzo(a)Pyrene	<2.20	mg/Kg	SW846 8270D
2-Nitroaniline	<5.25	mg/Kg	SW846 8270D	Benzo(b)Fluoranthene	<2.20	mg/Kg	SW846 8270D
2-Nitrophenol		mg/Kg	SW846 8270D	Benzo(ghi)Perylene	<2.20	mg/Kg	SW846 8270D
	<5.25	mg/Kg	SW846 8270D	Benzo(k)Fluoranthene	<2.20	mg/Kg	SW846 8270D
3,3-Dichlorobenzidine	<42		SW846 8270D	Benzoic Acid	<21	mg/K.g	SW846 8270D
3-Nitroaniline	<5.25	mg/Kg	SW846 8270D	Benzyl Alcohol	<5.25	mg/Kg	SW846 8270D

Results reported on a dry weight basis. Sample is 7.6% Solids.

Surrogate	Recovery	Method	Surrogate	Recovery	Method
2-Fluorophenol	39	SW846 8270D	2,4,6-Tribromophenol	68	SW846 8270D
Nitrobenzene-d6	63	SW846 8270D	p-Terphenyl-d14	74	SW846 8270D
Phenol-d6	57	SW846 8270D	p-Terphenyl	0	NWTPH-D
2-Fluorobiphenyl SPECTRA LABORAT	67 ORIES	SW846 8270D			

2221 Ross Way • Tacoma, WA 98421 • (253) 272-4850 • Fax (253) 572-9838 • www.spectra-lab.com

05/12/2015

Tacoma Public Utilities PO Box 11007 Tacoma, WA 98411 Attn: Mike Rhubright

15-04-20-024
SW Substation Pole Yard
Pole Yard Separator 1st Ch.
Sludge
04/20/2015
04/20/2015
2015040532
:2

Analyte	Result	Units	Method
Biphenyl	<5.25	mg/Kg	
Bis(2-Chloroethyl)Ether	<5.25	mg/Kg	
Butylbenzylphthalate	<5.25	mg/Kg	
Carbazole	<5.25	mg/Kg	
Chrysene	2.61	mg/Kg	
Di-n-Butylphthalate	<5.25	mg/Kg	•
Di-n-Octyl Phthalate	<5.25	mg/Kg	
Dibenz(a,h)Anthracene	<2.20	mg/Kg	
Dibenzofuran	<5.25	mg/Kg	
Dibenzothiophene	<5.25	mg/Kg	
Diethylphthalate	<5.25	mg/Kg	
Dimethyl Phthalate	<5.25	mg/Kg	
Fluoranthene	<2.20	mg/Kg	
Fluorene	<2.20	mg/Kg	
Hexachlorobenzene	<5.25	mg/Kg	SW846 8270D
Hexachlorobutadiene	<5.25	mg/Kg	SW846 8270D
Hexachlorocyclopentadiene	<5.25	mg/Kg	SW846 8270D
Hexachloroethane	<5.25	mg/Kg	SW846 8270D
Indeno(1,2,3-cd)Pyrene	<2.20	mg/Kg	SW846 8270D
Isophorone	<5.25	mg/Kg	SW846 8270D
N-Nitroso-Di-n-Propylamine	<5.25	mg/Kg	SW846 8270D

Analyte	Result	Units	Method
N-Nitrosodiphenylamine	<5.25	mg/Kg	SW846 8270D
N-nitrosodimethylamine	<5.25	mg/Kg	SW846 8270D
Naphthalene	19.0	mg/Kg	SW846 8270D
Nitrobenzene	<5.25	mg/Kg	SW846 8270D
Pentachlorophenol	487	mg/Kg	SW846 8270D
Phenanthrene	6.10	mg/Kg	SW846 8270D
Phenol	<5.25	mg/Kg	SW846 8270D
Pyrene	3.27	mg/Kg	SW846 8270D
Pyridine	<21	mg/Kg	SW846 8270D
Tetrachlorophenol	45.9	mg/Kg	SW846 8270D
bis(2-Chloroethoxy)Methane	<5.25	mg/Kg	SW846 8270D
bis(2-Ethylhexyl)Phthalate	<5.25	mg/Kg	
bis(2-chloroisopropyl)Ether			SW846 8270D
ons(2-omoronsopropyr)Ether	<5.25	mg/Kg	SW846 8270D

Results reported on a dry weight basis. Sample is 7.6% Solids.

Surrogate	Recovery	Method	Surrogate	Recovery	Method
2-Fluorophenol	39	SW846 8270D	2,4,6-Tribromophenol		
Nitrobenzene-d6	63	SW846 8270D	-	68	SW846 8270D
Dhomal de		3W040 82/UD	p-Terphenyl-d14	74	SW846 8270D
Phenol-d6	57	SW846 8270D	p-Terphenyl	0	
2-Fluorobiphenyl	67	SW846 8270D	F conputerior	0	NWTPH-D
SPECTRA LABORATO	ORIES				

2221 Ross Way • Tacoma, WA 98421 • (253) 272-4850 • Fax (253) 572-9838 • www.spectra-lab.com

May 12, 2015

Tacoma Public Utilities PO Box 11007 Tacoma, WA 98411 Method:NWTPH-DxSample Matrix:SoilSpectra Project:2015040532Applies to Spectra #:2Units:mg/Kg

HYDROCARBON ANALYSIS QUALITY CONTROL RESULTS

			MS/MS	D			
Spiked Sample:	050156-2			Date Extra	acted:	5/8/2015	
				Date Anal	yzed:	5/8/2015	
					Dup.		
	a 1	Spike	Spike		Spike		
Commonweil	Sample	Amount	Amount	Percent	Amount	Percent	%
Compound	<u>Result</u>	Added	Found	<u>Recovery</u>	<u>Found</u>	Recovery	<u>RPD</u>
Diesel	<10.0	125	85	68	86	69	1.2
		BLA	NK SPIKE	E (LCS)			
Date Extracted:	4/22/2015			Date Analy	/zed:	4/24/2015	
		Spike	Spike	•		· •	
-	Sample	Amount	Amount	Percent			
<u>Compound</u>	<u>Result</u>	Added	Found	Recovery			
Diesel	<10.0	125	102.3	81.84			
		ME	THOD BL	ANK			
Date Extracted:	4/22/2015			Date Analy	zed:	4/24/2015	
WTPH-D	<10.0						
Heavy Oils	<50.0						
Surrogate Percent Reco	overies:						
	p-terphenyl		82%				

SPECTRA LABORATORIES

Steven G. Hibbs, Laboratory Manager

2221 Ross Way • Tacoma, WA 98421 • (253) 272-4850 • Fax (253) 572-9838 • www.spectra-lab.com

May 12, 2015

Tacoma Public Utilities PO Box 11007 Tacoma, WA 98411

Method: NWTPH-Dx Sample Matrix: Water Spectra Project: 2015040532 Applies to Spectra #: 1

		DROCAR LITY CO					
			S/MSD				
Spiked Sample: Units:	Method Blank ug/L			Date Extrac Date Analyz		4/7/2015 4/8/2015	
Compound	Sample <u>Result</u>	Spike Amount <u>Added</u>	Spike Amount <u>Found</u>	Percent <u>Recovery</u>	Spike Amount <u>Found</u>	t Percent <u>Recovery</u>	% <u>RPD</u>
Diesel	0	2500	2165	87	2625	105	19
		METHO	D BLAN	K			
Date Extracted: Units:	4/22/2015 ug/L			Date Analyz	ed:	5/5/2015	
WTPH-D	<100						
Heavy Oils	<500						
Surrogate Recoveries:	p-terphenyl	98%					

SPECTRA LABORATORIES

Steven G. Hibbs, Laboratory Manager

2221 Ross Way • Tacoma, WA 98421 • (253) 272-4850 • Fax (253) 572-9838 • www.spectra-lab.com

May 12, 2015

Tacoma Public Utilities PO Box 11007 Tacoma, WA 98411

Spectra Project #	2015040532
Sample Spiked:	Method Blank
Date Extracted:	4/23/2015
Date Analyzed:	4/24/2015
Units:	ug/L
Applies to Spectra #s:	#1

GCMS Semi-Volatile Organic Analysis Method 625/8270 Blank Spike (LCS) Results

Compound	Sample	Spike	MS	MS	Rec.
	Conc.	Added	Conc.	%Rec	Limits
Phenol	<2.50	75	36.7	49	32-84
2-Chlorophenol	<2.50	75	35.3	47	35-84
1,4-Dichlorobenzene	<2.50	50	17.9	36	15-90
N-Nitroso-Di-N-Propylamine	<2.50	50	32.7	65	31-104
1,2,4-Trichlorobenzene	<2.50	50	24.2	48	24-82
4-Chloro-3-Methylphenol	<2.50	75	46.8	62	34-107
Acenaphthene	<1.00	50	27.3	55	34-98
2,4-Dinitrotoluene	<2.50	50	22.8		32-105
4-Nitrophenol	<2.50	75	53.7	72	26-156
Pentachlorophenol	<2.50	75	27.5		34-101
Pyrene	<1.00	50	28.6		30-130

Surrogates	% Rec	Limits
2-Fluorophenol	47	33-77
Phenol-d5	64	34-122
Nitrobenzene-d5	83	32-122
2-Fluorobipheny!	38	35-98
2,4,6-Tribromophenol	71	30-127
p-Terphenyl-d14	72	66-130

Steven G. Hibbs Laboratory Manager

2221 Ross Way • Tacoma, WA 98421 • (253) 272-4850 • Fax (253) 572-9838 • www.spectra-lab.com

SPECTRA Laboratories

< = less than

May 12, 2015

SEMIVOLATILE ORGANIC ANALYSIS METHOD BLANK RESULTS

SEMIVOLATILE ORGANIC ANALY		ug/L	Compound	MET	HOD 625/827
Pyridine		< 10	2,4-Dinitrophenol		ug/L
N-Nitrosodimethylamine		< 2.5	4-Nitrophenol		< 10
Aniline		< 10	Dibenzofuran		< 2.5
Phenol		< 2.5	2,4-Dinitrotoluene		< 2.5
bis(2-Chloroethyl)Ether		< 2.5	2,6-Dinitrotoluene		< 2.5
2-Chlorophenol		< 2.5	Diethylphthalate		< 2.5
1,3-Dichlorobenzene		< 2.5	4-Chlorophenyl-phenylether		< 2.5
1,4-Dichlorobenzene		< 2.5	Fluorene		< 2.5
Benzyl Alcohol		< 2.5	4-Nitroaniline		< 1.0
1,2-Dichlorobenzene		< 2.5	4,6-Dinitro-2-Methylphenol		< 2.5
2-Methylphenol		< 2.5			< 10
bis(2-Chlorolsipropyl)Ether		< 2.5	Ni-Nitrosodiphenylamine		< 2.5
4-Methylphenol		< 2.5	4-Bromophenyl-phenylether Hexachlorobenzene		< 2.5
N-Nitroso-di-n-Propylamine		< 2.5	Pentachlorophenol		< 2.5
Hexachloroethane		< 2.5	Phenanthrene		< 2.5
Nitrobenzene		< 2.5	Anthracene		< 1.0
Isophorone		< 2.5			< 1.0
2-Nitrophenol		< 2.5	Di-n-butylphthalate		< 2.5
2,4-Dimethylphenol		< 2.5	Fluoranthene		< 1.0
Senzoic Acid		< 10	Benzidine		< 20
bis(2-Chloroethoxy)methane		< 2.5	Pyrene Both discussion in the second		< 1.0
2,4-Dichlorophenot		< 2.5	Butylbenzylphthalate		< 2.5
.2,4-Trichlorobenzene		< 2.5 <	3,3-Dichlorobenzidine		< 20
laphthalene		< 1.0	Benzo(a)anthracene		< 1.0
-Chloroaniline		< 10	bis(2-ethylhexyl)phthalate		< 2.5
fexachlorobutadiene		< 2.5	Chrysene		< 1.0
-Chloro-3-Methylphenol		< 2.5	Di-n-octyl phthalate		< 2.5
-Methylnaphthalene		< 1.0	Benzo(b)Fluoranthene		< 1.0
exachiorocyclopentadiene		< 2.5	Benzo(k)Fluoranthene		< 1.0
4,6-Trichlorophenol		< 2.5	Benzo(a)pyrene		≤ 1.0
4,5-Trichlorophenol		< 2.5	Indeno(1,2,3-c,d)pyrene		< 1.0
Chloronaphthalene			Dibenzo(a,h)anthracene		≪ 1.0
Nitroaniline		< 2.5	Benzo(g,h,i)perylene		< 1.0
imethyl Phthalate		< 2.5	Carbazole		< 2.5
cenaphthylene		< 2.5	Biphenyl		< 2.5
Nitroaniline		< 1.0	n-decane		< 2.5
cenaphthene		< 2.5	n-octadecane		< 2.5
		< 1.0	1-Methylnaphthalene		< 1.0
			2,3,4,5-tetrachlorophenol		< 2.5
			2,3,4,6-tetrachlorophenol		< 2.5
		SURROGATE RE(COVERIES		
trobenzene-d5	76	%Rec. (Limits)			%Rec. (Limits
Fluorobiphenyl	-	% (32-122)	2-Fluorophenol	48	% (20-100)
accounterly	65	% (35-98)	Phenol-d5	58	% (34-122)
Ferphenyl-d14	80	% (30-130)	2,4,6-Tribromophenol	41	% (30-127)

Steven G. Hibbs

Laboratory Manager

2221 Ross Way • Tacoma, WA 98421 • (253) 272-4850 • Fax (253) 572-9838 • www.spectra-lab.com

SPECTRA Laboratories

May 12, 2015

Tacoma Public Utilities PO Box 11007 Tacoma, WA 98411

Spectra Project #	2015040532
Sample Spiked:	Method Blank
Date Extracted:	4/22/2015
Date Analyzed:	4/22/2015
Units:	mg/Kg
Applies to Spectra #'s:	#2

GCMS Semi-Volatile Organic Analysis, Method 8270D (Scan Mode) Blank Spike (LCS) Results in Soil/ Solids

Compound				
	Blank	Spike	LCS	LCS
	Conc.	Added	Conc.	%Rec
Phenol	<0.08	2.50	1.31	52
2-Chlorophenol	<0.08	2.50	1.22	49
1,4-Dichlorobenzene	<0.08	1.67	0.76	46
N-Nitroso-Di-N-Propylamine	<0.08	1.67	1.05	63
1,2,4-Trichlorobenzene	<0.08	1.67	0.86	51
4-Chloro-3-Methylphenol	<0.08	2.50	1.62	65
Acenaphthene	< 0.03	1.67	0.88	53
2,4-Dinitrotoluene	<0.08	1.67	0.83	50
4-Nitrophenol	<0.08	2.50	2.20	88
Pentachlorophenol	<0.08	2.50	0.87	35
Pyrene	<0.03	1.67	1.21	73
Surrogates				
2-Fluorophenol				%Rec
Phenol-d5				46
Nitrobenzene-d5				64
2-Fluorobiphenyl				78
2,4,6-Tribromophenol				67
p-Terphenyl-d14				65
				91

Steven G. Hibbs Laboratory Manager

2221 Ross Way • Tacoma, WA 98421 • (253) 272-4850 • Fax (253) 572-9838 • www.spectra-lab.com

< = less than

May 12, 2015

SEMIVOLATILE ORGANIC ANALYSIS METHOD BLANK RESULTS

Compound	mg/Kg	Compound	METH	OD 8270
Pyridine	< 0.33	Acenaphthene		mg/Kg
N-Nitrosodimethylamine	< 0.08	2,4-Dinitrophenol		< 0.03
Aniline	< 0.33	4-Nitrophenol		< 0.33
Phenol	< 0.08			< 0.08
bis(2-Chloroethyl)Ether	< 0.08	Dibenzofuran		< 0.08
2-Chlorophenol	< 0.08	2.4-Dinitrotoluene		< 0.08
1,3-Dichlorobenzene	< 0.08	2,6-Dinitrotoluene		< 0.08
1,4-Dichlorobenzene	< 0.08	Diethylphthalate		< 0.08
Benzyl Alcohol		4-Chlorophenyl-phenylether		< 0.08
1,2-Dichlorobenzene	< 0.08	Fluorene		< 0.03
2-Methylphenol	< 0.08	4-Nitroaniline		< 0.08
pis(2-Chloroisipropyl)Ether	< 0.08	4,6-Dinitro-2-Methylphenol		< 0.33
I-Methylphenol	< 0.08	NI-Nitrosodiphenylamine		< 0.08
V-Nitroso-di-n-Propylamine	< 0.08	4-Bromophenyl-phenylether		< 0.08
fexachloroethane	< 0.08	Hexachlorobenzene		< 0.08
litrobenzene	< 0.08	Pentachlorophenol		< 0.08
sophorone	< 0.08	Phenanthrene		
-Nitrophenol	< 0.08	Anthracene		< 0.03
	< 0.08	Di-n-butylphthalate		< 0.03
.4-Dimethylphenol	< 0.08	Fluoranthene		< 0.08
enzoic Acid	< 0.33	Benzidine		< 0.03
s(2-Chloroethoxy)methane	< 0.08	Pyrene		< 0.67
4-Dichlorophenol	< 0.08	Butylbenzylphthalate		< 0.03
2,4-Trichlorobenzene	< 0.08	3,3-Dichlorobenzidine		< 0.08
aphthalene	< 0.03	Benzo(a)anthracene		< 0.67
Chloroaniline	< 0.08			< 0.03
exachlorobutadiene	< 0.08	bis(2-ethylhexyl)phthalate		< 0.08
Chloro-3-Methylphenol	< 0.08	Chrysene		< 0.03
Methylnaphthalene	< 0.03	Di-n-octyl phthalate		< 0.08
exachlorocyclopentadiene	< 0.08	Benzo(b)Fluoranthene		< 0.03
4,6-Trichlorophenol	< 0.08	Benzo(k)Fluoranthene		< 0.03
4,5-Trichlorophenol		Benzo(a)pyrene		< 0.03
Chloronaphthalene	< 0.08	Indeno(1,2,3-c,d)pyrene		0.03
Nitroaniline	< 0.08	Dibenzo(a,h)anthracene		< 0.03
methyl Phthalate	< 0.08	Benzo(g,h,i)perylene		0.03
enaphthylene	< 0.08	Carbazole		0.08
litroaniline	< 0.03	Biphenyl		0.08
	< 0.08	1-Methylnaphthalene		0.08
		Dibenzothiophene		
		Tetrachlorophenol		0.08
	SURROGATE R	• • • •	<	0.08
obenzene-d5	77 %			
	•• 70	2-Fluorophenol	44	%
luorobiphenyt	66 %			
	50 <i>7</i> 8	Phenol-d5	57	%
erphenyl-d14	9 4 W			
· ·	84 %	2,4,6-Tribromophenol	52	%

Steven G. Hibbs

Laboratory Manager

2221 Ross Way • Tacoma, WA 98421 • (253) 272-4850 • Fax (253) 572-9838 • www.spectra-lab.com

SPECTRA Laboratories

May 12, 2015

Tacoma Public Utilities PO Box 11007 Tacoma, WA 98411

 Spectra Project #
 2015040532

 Sample Spiked:
 2015040143-4

 Date Extracted:
 4/8/2015

 Date Analyzed:
 4/8/2015

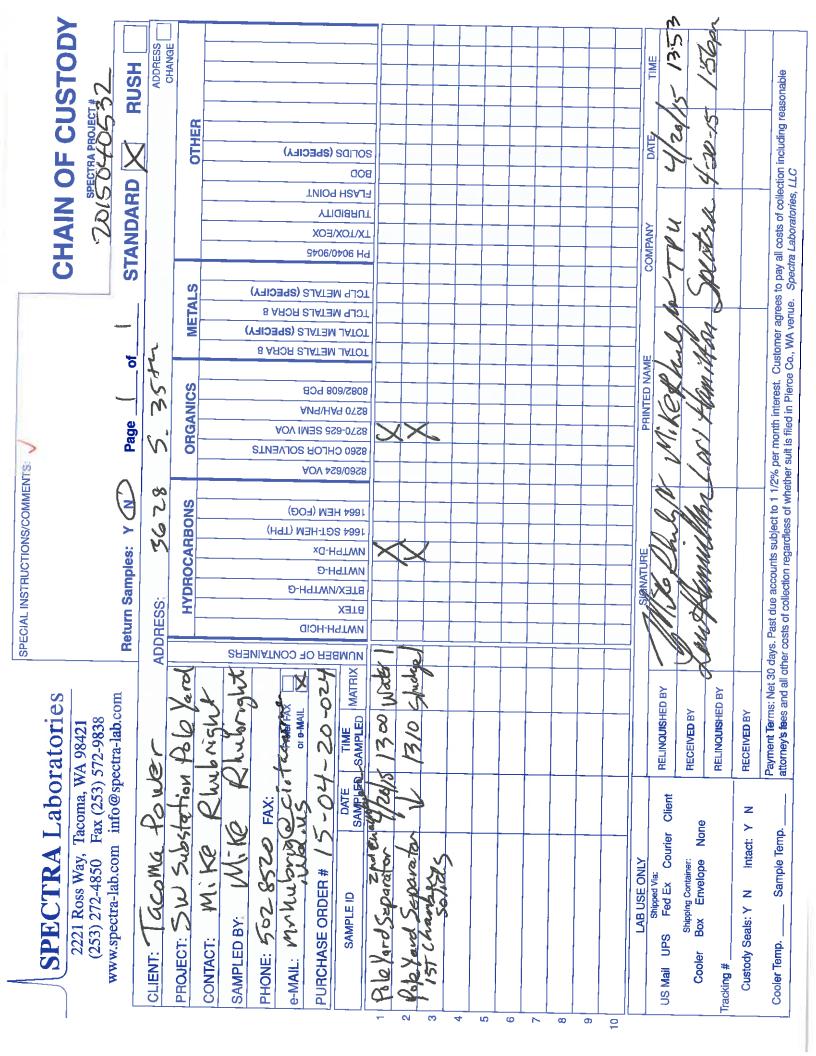
 Units:
 mg/kg wet wt.

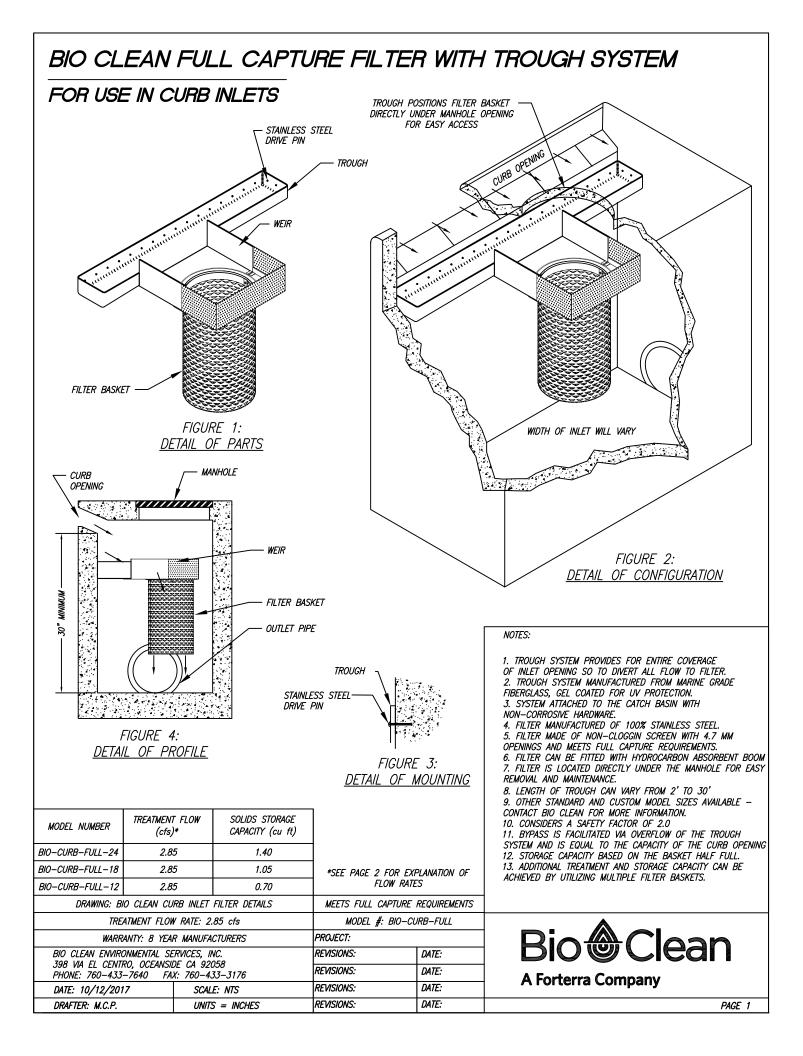
 Applies to Spectra #'s:
 #2

GCMS Semi-Volatile Organic Analysis, Method 8270D (Scan Mode) Matrix Spike/ Matrix Spike Duplicate Results in Soil

Compound	Sample	Spike	MS	MS	MSD	MSD	
	Conc.	Added	Conc.	%Rec	Conc	%Rec	RPD
Phenol	<0.08	2.50	1.47	59	1.51	60	2
2-Chlorophenol	<0.08	2.50	1.38	55	1.45	58	5
1,4-Dichlorobenzene	<0.08	1.67	0.81	49	0.86	51	6
N-Nitroso-Di-N-Propylamine	<0.08	1.67	1.09	65	1.12	67	3
1,2,4-Trichlorobenzene	<0.08	1.67	0.95	57	1.00	60	5
4-Chloro-3-Methylphenol	<0.08	2.50	1.97	79	1.96	78	0 1
Acenaphthene	< 0.03	1.67	1.02	61	1.05	63	3
2,4-Dinitrotoluene	<0.08	1.67	0.97	58	0.92	55	4
4-Nitrophenol	<0.08	2.50	2.55	102	2.60	104	2
Pentachloropheno!	<0.08	2.50	1.56	62	1.43	57	_
Pyrene	<0.03	1.67	1.23	74	1.43	57 76	9 3

Steven G. Hibbs Laboratory Manager







Section [____] Stormwater Catch Basin Filtration Device

PART 1 – GENERAL

01.01.00 Purpose

The purpose of this specification is to establish generally acceptable criteria for devices used for filtration of stormwater runoff captured by catch basins with curb openings. It is intended to serve as a guide to producers, distributors, architects, engineers, contractors, plumbers, installers, inspectors, agencies and users; to promote understanding regarding materials, manufacture and installation; and to provide for identification of devices complying with this specification.

01.02.00 Description

Stormwater Catch Basin Filtration Devices (SCBFD) are used to filter stormwater runoff captured by catch basins. The SCBFD is a filter system composed of a filter basket, media filtration boom and a trough system. SCBFDs are used to remove various pollutants from stormwater by means of screening, separation and media filtration.

01.03.00 Manufacturer

The manufacturer of the SCBFD shall be one that is regularly engaged in the engineering, design and production of systems developed for the treatment of stormwater runoff for at least (10) years, and which have a history of successful production, acceptable to the engineer of work. In accordance with the drawings, the SCBFD(s) shall be a filter device manufactured/distributed by Bio Clean Environmental Services, Inc. or assigned distributors or licensees. Bio Clean Environmental Services, Inc. can be reached at:

Corporate Headquarters: 398 Via El Centro Oceanside, CA 92058 Phone: (855) 566-3938 Fax: (760) 433-3176 www.BioCleanEnvironmental.com

01.04.00 Submittals

01.04.01	Shop drawings are to be submitted with each order to the contractor and engineer of work.
01.04.02	Shop drawings are to detail the SCBFD, its components and the sequence for installation, including:
	 SCBFD configuration with primary dimensions
	 Various SCBFD components
	 Any accessory equipment
01.04.03	Inspection and maintenance documentation submitted upon request.
01.05.00 Work Inc	luded

01.05.01	Specification requirements for installation of SCBFD.
01.05.02	Manufacturer to supply SCBFD(s):

- Filter Basket
- Trough System (weir and trough)
- Media Filtration Boom



01.05.03 Media Filtration Boom shall be provided with each Filter Basket housed in nylon netting and securely fastened entrance to the Filtration basket. Each media boom shall contain polymer beads to permanently absorb hydrocarbons.

01.06.00 Reference Standards

ASTM A 240	Standard Specification for Chromium and Chromium-Nickel Stainless Steel Plate, Sheet, and Strip for Pressure Vessels and for General Applications		
ASTM F 716	Testing Sorbent Performance of Absorbents		
ASTM F 726	Sorbent Performance of Absorbents		
ASTM D3787 - 07	Standard Test Method for Bursting Strength of Textiles-Constant-Rate-of-Traverse (CRT) Ball Burst Test		
ASTM D2690-98	Standard Test Method for Isophthalic Acid in Alkyd and Polyester Resins		
ASTM C 582-02	Standard Specification for Contact-Molded Reinforced Thermosetting Plastic (RTP) Laminates for Corrosion-Resistant Equipment		
ASTM D 638	Standard Test Method for Tensile Properties of Plastics		
ASTM D 790	Standard Test Methods for Flexural Properties of Unreinforced and Reinforced Plastics and Electrical Insulating Materials		
ASTM D 648	Standard Test Method for Deflection Temperature of Plastics Under Flexural Load in the Edgewise Position		
ASTM D 2583	Standard Test Method for Indentation Hardness of Rigid Plastics by Means of a Barcol Impressor		
ASTM D 4097	Standard Specification for Contact-Molded Glass-Fiber-Reinforced Thermoset Resin Corrosion-Resistant Tanks		
ASTM D3409	Standard Test Method for Adhesion of Asphalt-Roof Cement to Damp, Wet, or Underwater Surfaces		
IFI 114	Break Mandrel Blind Rivets		

PART 2 – COMPONENTS

02.01.00 Trough System Components

02.01.01	 <u>Trough</u> shall be manufactured from 100% marine grade polyester resin and fiberglass strands and stainless steel. The entire fiberglass structure must be coated with a polyester gel coating with ultra violet inhibitors incorporated into the coating for maximum ultra violet protection.
	 Fiberglass must have a minimum thickness of 3/16".
02.01.02	Weir portion of the Trough System shall be manufactured from 100%
	stainless steel.
	• The Weir shall fully surround the Filter Basket on all sides. On the end of the weir the sides shall be made of screen with perforated round openings less than 5 mm in size.
	 Water flows in access of the capacity of the Filter Basket shall pass through the additional weir screen for added treatment and retention of trash and debris during higher bypass flows. The Weir shall be hinged in the middle along the centerline of the Filter Basket and hinge upward to allow for access into the catch basin.
00.04.00	
02.01.03	Mounting Hardware shall be 100% non-corrosive metals.



- Nuts and bolts
- Rivets
- Support brackets
- Concrete anchors
- 02.01.04 Concrete Filler and Sealant shall be made of Acrylic Emulsion and have a minimum service temperature range of -30°F to 150°F.

02.02.00 Filter Basket Components

02.02.01 02.02.02	 <u>Filter Basket Housing</u> shall be manufactured of 100% stainless steel. <u>Side Screens</u> shall be manufactured of 100% stainless steel louver expanded metal with openings equal to or less than 4.7 mm in size. Screens shall be oriented with openings opposite to the flow of water into the filter and be non-clogging based on perpetual deflective shielding.
02.02.03	Bottom Screens shall be manufactured of 100% stainless steel perforated round openings less than 5 mm in size.
02.02.03	<u>Handle</u> shall be manufactured entirely of 100% stainless steel and be mounted to the Filter Basket Housing using mounting hardware per section 02.01.03
02.02.04	<u>Media Filtration Boom</u> shall be made up of granulated oil absorbing polymers that have been tested in accordance with section 11.2 of ASTM F 716.07 and held within a netting.
	 Oil absorbing polymers must be proven to absorb 180% of its weight within a 300 second contact time, and at this absorption percentage the physical increase in the size of the granules is not more that 50%.
	 Netting shall be 100% polyester with a number 16 sieve size, and strength tested per ASTM D 3787.

PART 3 – PERFORMANCE

03.01.00 <u>General</u>

03.01.01 Function - The SCBFD has no moving internal components and functions based on gravity flow, unless otherwise specified. The SCBFD is composed of a Trough System, Media Filtration Boom and a Filter Basket. Runoff enters the SCBFD from a curb opening and flows into the Trough System which is mounted under the face of the curb opening. It then flows horizontally inside the System's Trough to the Weir which holds the Filter Basket. This Trough System positions the Filter Basket directly under the catch basin access point (manhole cover, grate or hatch). The Filter Basket can be removed through the access point without disassembly. The Filter Basket can also be cleaned without entering the access point by using a vacuum truck. Within the Filter Basket is a Media Filtration Boom. Water flows through the Weir and into the Filter Basket. Stormwater enters the inside of the Filter Basket and flows downward toward the bottom portion of the Basket. The non-clogging screen has openings that are facing upward. As water flows downward the screening continuously removes debris from the screen's surface. Flowing water also makes contact with the Media Filtration Boom which absorbs free floating oils. Stormwater flow up to the peak treatment flow rate is processed through the



filtration screens. During the heaviest flows the Filter Basket fills with water and spills over the top to bypass directly into the bottom of the catch basin, while previously captured debris and solids are contained by the weir screens which prevents re-suspension.

03.01.02	<u>Pollutants</u> - The SCBFD will remove and retain debris, sediments, metals, nutrients, oxygen demanding substances, bacteria and hydrocarbons entering
	the filter during frequent storm events and specified flow rates. For pollutant
	removal performance see section 03.02.00.
03.01.03	<u>Treatment Flow Rate</u> - The SCBFD operates using gravity flow. The SCBFD
	treatment flow rate varies by size and is provided on the drawings for each
	model. Flow rates must be supported by independent lab results.
03.01.04	Bypass Flow Rate – The SCBFD is designed to fit within the catch basin in a
	way not to affect the hydraulics. The area over the top of the Trough System
	is always greater than the curb opening area and/or the area of the outflow
	pipe. Therefore, the SCBFD does not create a critical point of restriction.
03.01.05	Pollutant Load – The SCBFD must be designed to have minimum storage
	capacity as documented on the drawing for each particular size and model.
03.01.06	Performance Protocol and Results – All lab testing on filtration media must be
	performed by an independent third party consultant and testing lab.

03.02.00 Test Performance

At a minimum, the SCBFD shall be tested, according to section 03.01.03 & 03.01.06, and meet these performance specifications:

	REMOVAL
POLLUTANT	EFFICIENCY
Trash and Debris - (down to 5 mm)	100%

03.02.02 <u>Maintenance Performance</u> – The Filter Basket must be able to be maintained and cleaned from finish surface using a vacuum hose inserted through the manhole or hatch opening and not the curb face. All cleaning shall be done without entering the catch basin. The Filter Basket shall be removable from finish surface and reinstalled from finish surface without entrance into the catch basin.

PART 4 - EXECUTION

04.01.00 General

The installation and use of the SCBFD shall conform to all applicable national, state, municipal and local specifications.

04.02.00 Installation

The contractor shall furnish all labor, equipment, materials and incidentals required to install the (SCBFD) device(s) and appurtenances in accordance with the drawings, installation manual, and these specifications, and be inspected and approved by the local governing agency. Installation contractor should possess a Confined Space Entry Certification Permit, pursuant to OSHA standards. Any damage to catch basin and surrounding infrastructure caused by the installation of the SCBFD is the responsibility of the installation contractor.



04.02.01 Trough System will be installed in accordance with manufactures' recommendations. The Trough component will be installed the complete width of the curb opening, or underneath any wings as to provide 100% coverage of incoming stormwater. The Weir component of the Trough System must be located directly under the manhole opening or other access point (not including the curb opening) regardless of its position relative of the curb opening. The Trough System must be properly mounted and assembled inside the catch basin with drive pins and pop rivets per manufacture's recommendations. Once the Trough System is secured to the walls of the catch basin all seams must be filled with sealant per section 02.01.03. 04.02.02 Filter Basket will be inserted through the manhole opening or access point of the catch basin directly without entry into the basin. The Filter Basket shall be fully visible from finish surface while looking into the access point for ease of inspection and maintenance. The curb opening itself is not a point of access as maintenance personnel cannot enter.

04.03.00 Shipping, Storage and Handling

- 04.03.01 <u>Shipping</u> SCBFD shall be shipped to the contractor's address and is the responsibility of the contractor to transport the unit(s) to the exact site of installation.
- 04.03.02 <u>Storage and Handling</u>– The contractor shall exercise care in the storage and handling of the SCBFD(s) and its components prior to and during installation. Any repair or replacement costs associated with events occurring after delivery is accepted, and unloading has commenced shall be born by the contractor. The SCBFD(s) and its components shall always be stored indoors and transported inside the original shipping container(s) until the SCBFD(s) are ready to be installed. The SCBFD shall always be handled with care and lifted according to OSHA and NIOSA lifting recommendations and/or contractor's workplace safety professional recommendations.

04.04.00 Maintenance and Inspection

- 04.04.01 <u>Inspection</u> After installation, the contractor shall demonstrate that the SCBFD has been properly installed at the correct location(s), elevations, and with appropriate supports and fasteners. All components associated with the SCBFD and its installation shall be subject to inspection by the engineer of work, governing agency, and the manufacture at the place of installation. In addition, the contractor shall demonstrate that the SCBFD has been installed per the manufacturer's specifications and recommendations. SCBFD(s) shall be physically inspected regularly in accordance to owner's Stormwater Pollution Prevention Plans (SWPPP) and manufacture's recommendations. An inspection record shall be kept by the inspection operator. The record shall include the condition of the SCBFD and its appurtenances. The most current copy of the inspection record shall always be copied and placed in the owner's SWPPP.
- 04.04.02 <u>Maintenance</u> SCBFD(s) must be completely maintained from outside the catch basin. The SCBFD(s) shall be inspected, maintained and cleaned 1 to 4 times a year and/or in accordance to owner's Stormwater Pollution Prevention Plans (SWPPP). The maintenance shall be preformed by someone qualified. A Maintenance Manual is available upon request from the manufacturer. The manual has detailed information regarding the maintenance of the SCBFD. A Maintenance Record shall be kept by the



maintenance operator. The Maintenance Record shall include any maintenance activities preformed, amount and description of debris collected, and the condition of the filter. The most current copy of the Maintenance Record shall always be copied and placed in the owner's SWPPP.

04.04.03 <u>Material Disposal</u> - All debris, trash, organics, and sediments captured and removed from the SCBFD shall be transported and disposed of at an approved facility for disposal in accordance with local and state regulations. Please refer to state and local regulations for the proper disposal of toxic and non-toxic material.

PART 5 – QUALITY ASSURANCE

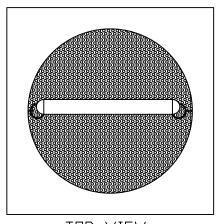
05.01.00 Warranty

The manufacturer shall guarantee the SCBFD against all manufacturing defects in materials and workmanship for a period of (8) years from the date of delivery to the contractor. The manufacturer shall be notified of repair or replacement issues in writing within the warranty period. The SCBFD is limited to recommended application for which it was designed.

[End of This Section]

BIO CLEAN FULL CAPTURE FILTER

FOR USE IN GRATE INLETS



<u>top view</u>

NOTES:

- ALL HARDWARE, FLANGE, FRAME, SCREENS SHALL BE STAINLESS STEEL
 HYDROCARBON BOOM SHALL BE 2" DIAMETER AND CONNECTED, MECHANICALLY TO THE FILTER FRAME WITH RAILS ALLOWING IT TO FLOAT ON THE WATER SURFACE REGARDLESS OF HEIGHT
 SEE PERFORMANCE REPORTS IN MANUFACTURES SPECIFICATIONS
 OTHER STANDARD AND CUSTOM MODEL SIZES AVAILABLE CONTACT BIO CLEAN FOR MORE INFORMATION.
 BASED ON 37% OPEN AREA.
 CONSIDERS A LOCAL DEPRESSION PONDING DEPTH OF 6 INCHES.
 STORAGE CAPACITY BASED ON THE BASKET HALF FULL.
 CONCRETE STRUCTURES SOLD SEPARATELY.

 \sim

 \sim

 \leftrightarrow

 \simeq $\overline{}$ $\overline{\nabla}$

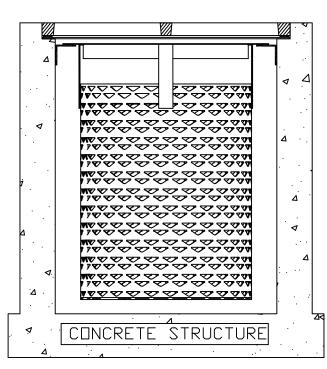
 $\overline{ }$

 $\overline{}$ \sim

~~~

<u> ^~~~~~~~~~</u>

FLOW SCHEMATIC



| 6 INCHES.<br>- HIGH FLOW<br>BYPASS                              | MODEL #                    | TREATMENT<br>FLDW<br>(CFS) | BYPASS<br>FLOW<br>(CFS) | SOLIDS<br>STORAGE<br>CAPACITY<br>(CF) |
|-----------------------------------------------------------------|----------------------------|----------------------------|-------------------------|---------------------------------------|
| - BOOM RAILS                                                    | BID-GRATE-FULL<br>12-12-12 | 1.55                       | 1,55                    | 0.27                                  |
| - DUUM KAILS                                                    | BID-GRATE-FULL<br>18-18-18 | 4.32                       | 3.68                    | 1.05                                  |
| - NDN-CLDGGING<br>SCREEN. MEETS<br>FULL CAPTURE<br>REQUIREMENTS | BID-GRATE-FULL<br>24-24-24 | 7.67                       | 4.83                    | 2.41                                  |
|                                                                 | BID-GRATE-FULL<br>30-30-24 | 12.97                      | 6.21                    | 3.98                                  |
| - FLDATING<br>HYDROCARBON<br>BOOM                               | BID-GRATE-FULL<br>25-38-24 | 13.53                      | 6.59                    | 4.16                                  |
| - BOTTOM SCREEN.<br>MEETS FULL<br>CAPTURE<br>REQUIREMENTS       | BID-GRATE-FULL<br>36-36-24 | 19.64                      | 7.60                    | 5.94                                  |
| NEWOIKEMENTS                                                    | BID-GRATE-FULL<br>48-48-18 | 25.59                      | 10.13                   | 7.92                                  |

| DRAWING: BIO CLEAN GRA                                                         | MEETS FULL CAPTURE<br>REQUIREMENTS |            |       |  |
|--------------------------------------------------------------------------------|------------------------------------|------------|-------|--|
| TYPICAL MODEL DETAIL                                                           |                                    |            |       |  |
| WARRANTY: 8 YEAR MANUFACTURERS                                                 |                                    | PROJECTI   |       |  |
| BID CLEAN ENVIRONMENTAL SERVICES, INC.                                         |                                    | REVISIONS; | DATE: |  |
| 398 ∨IA EL CENTR□, □CEANSIDE CA 92058<br>PH□NE: 760-433-7640 FAX: 760-433-3176 |                                    | REVISIONS; | DATE: |  |
| DATE: 10/12/17                                                                 | SCALE: SF = 15                     | REVISIONS; | DATE: |  |
| DRAFTER: M.C.P.                                                                | UNITS = INCHES                     | REVISIONS; | DATE  |  |

| Bio | C | ea |   |
|-----|---|----|---|
| Bio | C | ea | r |

A Forterra Company

PAGE 1



# Section [\_\_\_\_] Stormwater Catch Basin Filtration Device

# PART 1 – GENERAL

### 01.01.00 Purpose

The purpose of this specification is to establish generally acceptable criteria for devices used for filtration of stormwater runoff captured by catch basins with grates. It is intended to serve as a guide to producers, distributors, architects, engineers, contractors, plumbers, installers, inspectors, agencies and users; to promote understanding regarding materials, manufacture and installation; and to provide for identification of devices complying with this specification.

### 01.02.00 Description

Stormwater Catch Basin Filtration Devices (SCBFD) are used to filter stormwater runoff captured by catch basins. The SCBFD is a filter system composed of a SCBFD with a media filtration storm boom. SCBFDs are used to remove various pollutants from stormwater by means of screening, separation and media filtration.

### 01.03.00 Manufacturer

The manufacturer of the SCBFD shall be one that is regularly engaged in the engineering, design and production of systems developed for the treatment of stormwater runoff for at least (10) years, and which have a history of successful production, acceptable to the engineer of work. In accordance with the drawings, the SCBFD(s) shall be a filter device manufactured/distributed by Bio Clean Environmental Services, Inc., or assigned distributors or licensees. Bio Clean Environmental Services, Inc. can be reached at:

Corporate Headquarters: 398 Via El Centro Oceanside, CA 92058 Phone: (760) 433-7640 Fax: (760) 433-3176 www.biocleanenvironmental.net

### 01.04.00 Submittals

| 01.04.01                 | Submittal drawings will be provided with each order to the contractor and engineer of work.                                                                                                                |
|--------------------------|------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|
| 01.04.02                 | Submittal drawings are to detail the SCBFD, its components and the sequence for installation, including: <ul> <li>SCBFD configuration with primary dimensions</li> <li>Various SCBFD components</li> </ul> |
| 01.04.03                 | <ul> <li>Any accessory equipment<br/>Inspection and maintenance documentation submitted upon request.</li> </ul>                                                                                           |
| 01.05.00 <u>Work Inc</u> |                                                                                                                                                                                                            |

| 01.05.01 | Specification requirements for installation of SCBFD. |
|----------|-------------------------------------------------------|
| 01.05.02 | Manufacturer to supply SCBFD(s):                      |

- Filter Basket
- Media Filtration Storm Boom



01.05.03 Media Filtration Boom shall be provided with each Filter Basket housed in nylon netting and securely fastened entrance to the Filtration basket. Each media boom shall contain polymer beads to permanently absorb hydrocarbons.

### 01.06.00 Reference Standards

| ASTM A 240      | Standard Specification for Chromium and Chromium-Nickel Stainless Steel Plate,<br>Sheet, and Strip for Pressure Vessels and for General Applications |
|-----------------|------------------------------------------------------------------------------------------------------------------------------------------------------|
| ASTM F 716      | Testing Sorbent Performance of Absorbents                                                                                                            |
| ASTM F 726      | Sorbent Performance of Absorbents                                                                                                                    |
| ASTM D3787 - 07 | Standard Test Method for Bursting Strength of Textiles-Constant-Rate-of-Traverse (CRT) Ball Burst Test                                               |
| ASTM D2690-98   | Standard Test Method for Isophthalic Acid in Alkyd and Polyester Resins                                                                              |
| ASTM C 582-02   | Standard Specification for Contact-Molded Reinforced Thermosetting Plastic<br>(RTP) Laminates for Corrosion-Resistant Equipment                      |
| ASTM D 638      | Standard Test Method for Tensile Properties of Plastics                                                                                              |
| ASTM D 790      | Standard Test Methods for Flexural Properties of Unreinforced and Reinforced<br>Plastics and Electrical Insulating Materials                         |
| ASTM D 648      | Standard Test Method for Deflection Temperature of Plastics Under Flexural Load<br>in the Edgewise Position                                          |
| ASTM D 2583     | Standard Test Method for Indentation Hardness of Rigid Plastics by Means of a<br>Barcol Impressor                                                    |
| ASTM D 4097     | Standard Specification for Contact-Molded Glass-Fiber-Reinforced Thermoset<br>Resin Corrosion-Resistant Tanks                                        |
| ASTM D3409      | Standard Test Method for Adhesion of Asphalt-Roof Cement to Damp, Wet, or<br>Underwater Surfaces                                                     |
| IFI 114         | Break Mandrel Blind Rivets                                                                                                                           |

# PART 2 – COMPONENTS

### 02.01.00 Filter Basket Components

All SCBFD components must be made of stainless steel, per these specifications. SCBFD's containing any fabrics or plastics will not be accepted.

| 02.01.01<br>02.02.02 | <ul> <li><u>Filter Housing</u> shall be manufactured of 100% stainless steel.</li> <li><u>Side Screens</u> shall be manufactured of 100% stainless steel louver expanded metal with openings equal to or less than 4.7 mm in size.</li> <li>Screens shall be oriented with openings opposite to the flow of water into the filter and be non-clogging based on perpetual</li> </ul>                                       |
|----------------------|---------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|
|                      | deflective shielding.                                                                                                                                                                                                                                                                                                                                                                                                     |
| 02.02.03             | Bottom Screens shall be manufactured of 100% stainless steel perforated round openings less than 5 mm in size.                                                                                                                                                                                                                                                                                                            |
| 02.02.04             | <ul> <li>Media Filtration Boom shall be made up of granulated oil absorbing polymers that have been tested in accordance with section 11.2 of ASTM F 716.07 and held within a netting.</li> <li>Oil absorbing polymers must be proven to absorb 180% of its weight within a 300 second contact time, and at this absorption percentage the physical increase in the size of the granules is not more that 50%.</li> </ul> |



- Netting shall be 100% polyester with a number 16 sieve size, and strength tested per ASTM D 3787.
- Filter netting shall be 100% polyester with a number 16 sieve size, and strength tested per ASTM D 3787.

### PART 3 – PERFORMANCE

### 03.01.00 General

| 03.01.01                         | <u>Function</u> - The SCBFD has no moving internal components and functions<br>based on gravity flow, unless otherwise specified. Runoff enters the SCBFD<br>from a catch basin with a grate opening and flows downward into the SCBFD.<br>This SCBFD shall be positioned directly under the catch basin grate. After<br>removal of the grate the SCBFD must be able to be removed through the<br>catch basin opening without any further disassembly Stormwater enters the<br>inside of the Filter Basket and flows downward toward the bottom portion of<br>the Basket. The non-clogging screen has openings that are facing upward. As<br>water flows downward the screening continuously removes debris from the<br>screen's surface. Flowing water also makes contact with the Media Filtration<br>Boom which absorbs free floating oils. Stormwater flow up to the peak<br>treatment flow rate is processed through the filtration screens. During the<br>heaviest flows the Basket fills with water and spills out the internal bypass and<br>into the bottom of the catch basin. |
|----------------------------------|------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|
| 03.01.02                         | <u>Pollutants</u> - The SCBFD will remove and retain debris, sediments, metals, nutrients, oxygen demanding substances and hydrocarbons entering the catch basin during frequent storm events and specified flow rates. For pollutant removal performance see section 03.02.00.                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          |
| 03.01.03                         | <u>Treatment Flow Rate</u> - The SCBFD operates using gravity flow. The SCBFD treatment flow rate varies by size and is provided on the drawings for each model. Flow rates must be supported by independent lab results.                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                |
| 03.01.04                         | Bypass Flow Rate – The SCBFD is designed to fit within the catch basin in a way not to affect the existing hydraulics and treat or bypass all flows. The bypass must be sized with a surface area greater then the outlet pipe size, thus the SCBFD shall not be a critical point of flow restriction. Bypass flow rate must be based on the SCBFD's inlet throat or bypass orifice capacity, which ever is less.                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        |
| 03.01.05<br>03.01.06<br>03.01.07 | Pollutant Load – The SCBFD must be designed to have minimum storage capacity as documented on the drawing for each particular size and model.<br><u>Performance Protocol and Results</u> – All lab testing on filtration media must be performed by an independent third party consultant and testing lab.                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               |

### 03.02.00 Test Performance

At a minimum, the SCBFD shall be tested, according to section 03.01.06, and meet these performance specifications:

### 03.02.01 Filter Pollutant Removal Table

|                                   | REMOVAL    |
|-----------------------------------|------------|
| POLLUTANT                         | EFFICIENCY |
| Trash and Debris - (down to 5 mm) | 100%       |



# PART 4 - EXECUTION

### 04.01.00 General

The installation and use of the SCBFD shall conform to all applicable national, state, municipal and local specifications.

### 04.02.00 Installation

The contractor shall furnish all labor, equipment, materials and incidentals required to install the (SCBFD) device(s) and appurtenances in accordance with the drawings, installation manual, and these specifications, and be inspected and approved by the local governing agency. Installation contractor should possess a Confined Space Entry Certification Permit, pursuant to OSHA standards. Any damage to catch basin and surrounding infrastructure caused by the installation of the SCBFD is the responsibility of the installation contractor.

04.02.01 <u>Filter Basket</u> and all components or accessories shall be inserted through the catch basin and properly secured per manufactures installation manual and these specifications.

### 04.03.00 Shipping, Storage and Handling

- 04.03.01 <u>Shipping</u> SCBFD shall be shipped to the contractor's address and is the responsibility of the contractor to transport the unit(s) to the exact site of installation.
- 04.03.02 <u>Storage and Handling</u>- The contractor shall exercise care in the storage and handling of the SCBFD(s) and its components prior to and during installation. Any repair or replacement costs associated with events occurring after delivery is accepted, and unloading has commenced shall be born by the contractor. The SCBFD(s) and its components shall always be stored indoors and transported inside the original shipping container(s) until the SCBFD(s) are ready to be installed. The SCBFD shall always be handled with care and lifted according to OSHA and NIOSA lifting recommendations and/or contractor's workplace safety professional recommendations.

### 04.04.00 Maintenance and Inspection

- 04.04.01 Inspection – After installation, the contractor shall demonstrate that the SCBFD has been properly installed at the correct location(s), elevations, and with appropriate supports and fasteners. All components associated with the SCBFD and its installation shall be subject to inspection by the engineer of work, governing agency, and the manufacture at the place of installation. In addition, the contractor shall demonstrate that the SCBFD has been installed per the manufacturer's specifications and recommendations. SCBFD(s) shall be physically inspected regularly in accordance to owner's Stormwater Pollution Prevention Plans (SWPPP) and manufacture's recommendations. An inspection record shall be kept by the inspection operator. The record shall include the condition of the SCBFD and its appurtenances. The most current copy of the inspection record shall always be copied and placed in the owner's SWPPP. 04.04.02 Maintenance – The manufacturer recommends cleaning and debris removal
  - 04.04.02 <u>Maintenance</u> The manufacturer recommends cleaning and debris removal and replacement of the Media Filtration Boom as needed. The maintenance shall be preformed by someone qualified. A Maintenance Manual is available upon request from the manufacturer. The manual has detailed information



regarding the maintenance of the SCBFD(s). A detailed Maintenance Record shall be kept by the maintenance operator. The Maintenance Record shall include any maintenance activities preformed, amount and description of debris collected, and the condition of the filter. The most current copy of the Maintenance Record shall always be copied and placed in the owner's Stormwater Pollution Prevention Plan (SWPPP) per governing agency. <u>Material Disposal</u> - All debris, trash, organics, and sediments captured and

04.04.03

<u>Material Disposal</u> - All debris, trash, organics, and sediments captured and removed from the SCBFD shall be transported and disposed of at an approved facility for disposal in accordance with local and state regulations. Please refer to state and local regulations for the proper disposal of toxic and non-toxic material.

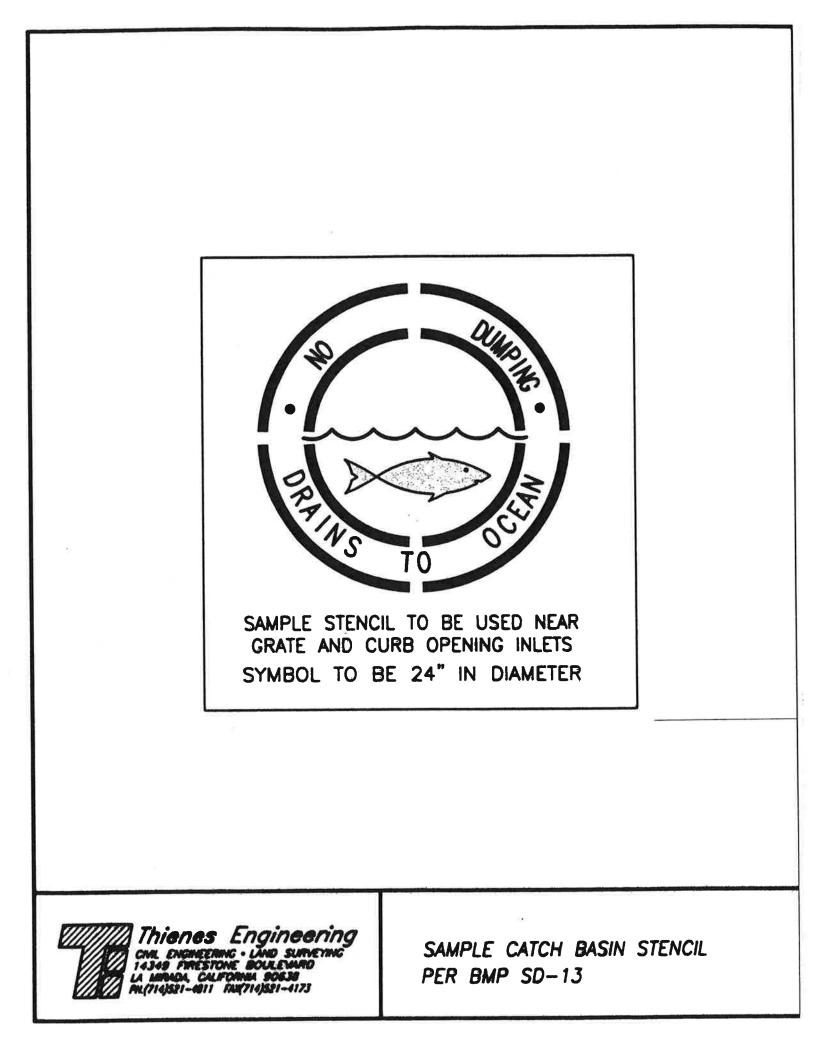
## PART 5 – QUALITY ASSURANCE

### 05.01.00 Warranty

The manufacturer shall guarantee the SCBFD against all manufacturing defects in materials and workmanship for a period of (5) years from the date of delivery to the contractor. The manufacturer shall be notified of repair or replacement issues in writing within the warranty period. The SCBFD is limited to recommended application for which it was designed.

# [End of This Section]

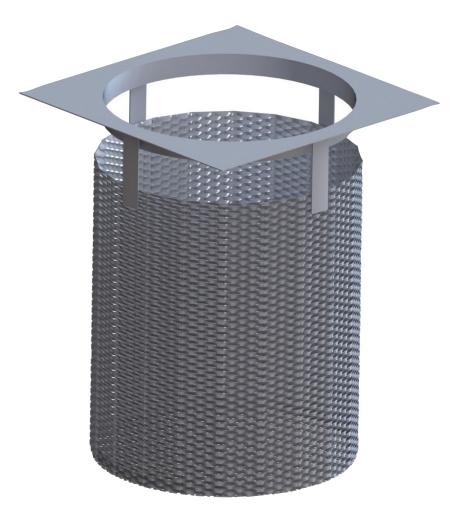
Appendix D: BMP Maintenance Information



# Grate Inlet Filter



# **OPERATION & MAINTENANCE**



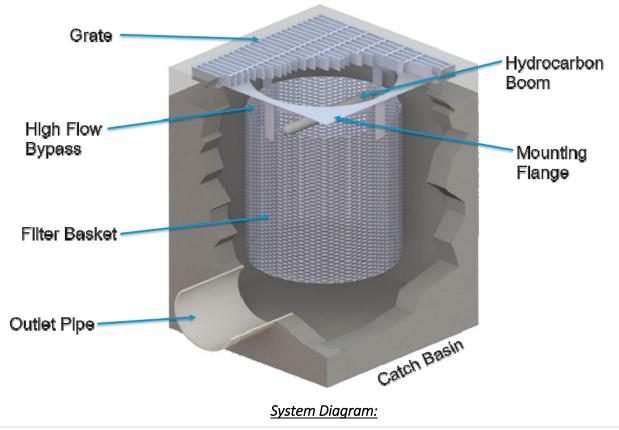
Bio Clean Environmental Services, Inc. 398 Via El Centro Oceanside, CA 92058 www.BioCleanEnvironmental.com p: 760.433.7640 f: 760.433.3176



# **OPERATION & MAINTENANCE**

The Bio Clean Grate Inlet Filter is a stormwater device designed to remove high levels of trash, debris, sediments and hydrocarbons. The filter is available in several configurations including trash full capture, multi-level screening, Kraken membrane filter and media filter variations. This manual covers maintenance procedures of the trash full capture and multi-level screening configurations. A supplemental manual is available for the Kraken and media filter variations. This filter is made of 100% stainless steel and is available and various sizes and depths allowing it to fit in any grated catch basin inlet. The filters heavy duty construction allows for cleaning with any vacuum truck. The filter can also easily be cleaned by hand.

As with all stormwater BMPs, inspection and maintenance on the Grate Inlet Filter is necessary. Stormwater regulations require BMPs be inspected and maintained to ensure they are operating as designed to allow for effective pollutant removal and provide protection to receiving water bodies. It is recommended that inspections be performed multiple times during the first year to assess sitespecific loading conditions. This is recommended because pollutant loading can vary greatly from site to site. Variables such as nearby soil erosion or construction sites, winter sanding of roads, amount of daily traffic and land use can increase pollutant loading on the system. The first year of inspections can be used to set inspection and maintenance intervals for subsequent years. Without appropriate maintenance a BMP can exceed its storage capacity which can negatively affect its continued performance in removing and retaining captured pollutants.





### Inspection Equipment

Following is a list of equipment to allow for simple and effective inspection of the Grate Inlet Filter:

- Bio Clean Environmental Inspection Form (contained within this manual).
- Manhole hook or appropriate tools to remove access hatches and covers.
- Appropriate traffic control signage and procedures.
- Protective clothing and eye protection.
- Note: entering a confined space requires appropriate safety and certification. It is generally not required for routine inspections or maintenance of the system.



### **Inspection Steps**

The core to any successful stormwater BMP maintenance program is routine inspections. The inspection steps required on the Grate Inlet Filter are quick and easy. As mentioned above the first year should be seen as the maintenance interval establishment phase. During the first year more frequent inspections should occur in order to gather loading data and maintenance requirements for that specific site. This information can be used to establish a base for long-term inspection and maintenance interval requirements.

The Grate Inlet Filter can be inspected though visual observation. All necessary pre-inspection steps must be carried out before inspection occurs, such as safety measures to protect the inspector and nearby pedestrians from any dangers associated with an open grated inlet. Once the grate has been safely removed the inspection process can proceed:

- Prepare the inspection form by writing in the necessary information including project name, location, date & time, unit number and other info (see inspection form).
- Observe the filter with the grate removed.
- Look for any out of the ordinary obstructions on the grate or in the filter and its bypass. Write down any observations on the inspection form.
- Through observation and/or digital photographs estimate the amount of trash, foliage and sediment accumulated inside the filter basket. Record this information on the inspection form.
- Observe the condition and color of the hydrocarbon boom. Record this information on the inspection form.
- Finalize inspection report for analysis by the maintenance manager to determine if maintenance is required.



### Maintenance Indicators

Based upon observations made during inspection, maintenance of the system may be required based on the following indicators:

- Missing or damaged internal components.
- Obstructions in the filter basket and its bypass.
- Excessive accumulation of trash, foliage and sediment in the filter basket. Maintenance is required when the basket is greater than half-full.
- The following chart shows the 50% and 100% storage capacity of each filter height:

| Model             | Filter Basket<br>Diameter (in) | Filter Basket<br>Height (in) | 50% Storage<br>Capacity (cu ft) | 100% Storage<br>Capacity (cu ft) |
|-------------------|--------------------------------|------------------------------|---------------------------------|----------------------------------|
| BC-GRATE-12-12-12 | 10.00                          | 12.00                        | 0.27                            | 0.55                             |
| BC-GRATE-18-18-18 | 16.00                          | 18.00                        | 1.05                            | 2.09                             |
| BC-GRATE-24-24-24 | 21.00                          | 24.00                        | 2.41                            | 4.81                             |
| BC-GRATE-30-30-24 | 27.00                          | 24.00                        | 3.98                            | 7.95                             |
| BC-GRATE-36-36-24 | 33.00                          | 24.00                        | 5.94                            | 11.88                            |
| BC-GRATE-48-48-18 | 44.00                          | 18.00                        | 7.92                            | 15.84                            |

### Maintenance Equipment

It is recommended that a vacuum truck be utilized to minimize the time required to maintain the Curb Inlet Filter, though it can easily cleaned by hand:

- Bio Clean Environmental Maintenance Form (contained in O&M Manual).
- Manhole hook or appropriate tools to remove the grate.
- Appropriate safety signage and procedures.
- Protective clothing and eye protection.
- Note: entering a confined space requires appropriate safety and certification. It is generally not required for routine maintenance of the system. Small or large vacuum truck (with pressure washer attachment preferred).

### Maintenance Procedures

It is recommended that maintenance occurs at least two days after the most recent rain event to allow debris and sediments to dry out. Maintaining the system while flows are still entering it will increase the time and complexity required for maintenance. Cleaning of the Grate Inlet Filter can be performed utilizing a vacuum truck. Once all safety measures have been set up cleaning of the Grate Inlet Filter can proceed as followed:

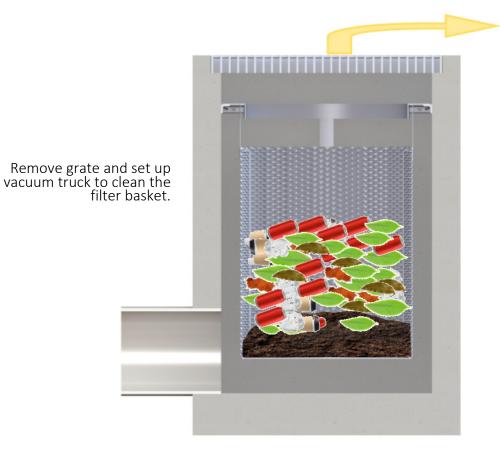


- Remove grate (traffic control and safety measures to be completed prior).
- Using an extension on a vacuum truck position the hose over the opened catch basin. Insert the vacuum hose down into the filter basket and suck out trash, foliage and sediment. A pressure wash is recommended and will assist in spraying of any debris stuck on the side or bottom of the filter basket. Power wash off the filter basket sides and bottom.
- Next remove the hydrocarbon boom that is attached to the inside of the filter basket. The hydrocarbon boom is fastened to rails on two opposite sides of the basket (vertical rails). Assess the color and condition of the boom using the following information in the next bullet point. If replacement is required install and fasten on a new hydrocarbon boom. Booms can be ordered directly from the manufacturer.
  - Excellent Good Minimal Replacement Condition Condition
- Follow is a replacement indication color chart for the hydrocarbon booms:

- The last step is to replace the grate and remove all traffic control.
- All removed debris and pollutants shall be disposed of following local and state requirements.
- Disposal requirements for recovered pollutants may vary depending on local guidelines. In most areas the sediment, once dewatered, can be disposed of in a sanitary landfill. It is not anticipated that the sediment would be classified as hazardous waste.
- In the case of damaged components, replacement parts can be ordered from the manufacturer. Hydrocarbon booms can also be ordered directly from the manufacturer as previously noted.



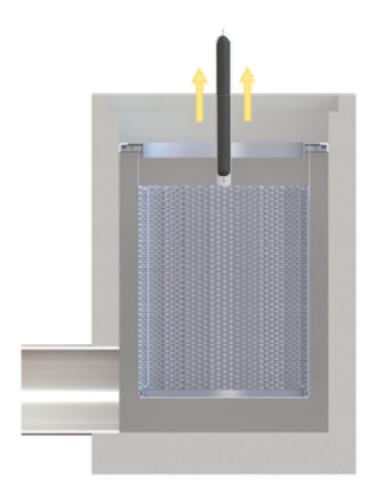
Maintenance Sequence





Insert the vacuum hose down into the filter basket and suck out debris. Use a pressure washer to assist in vacuum removal. Pressure wash off screens.





Remove the hydrocarbon boom that is attached to the inside of the filter basket. The hydrocarbon boom is fastened to rails on two opposite sides of the basket (vertical rails). Assess the color and condition of the boom using the following information in the next bullet point. If replacement is required install and fasten on a new hydrocarbon boom.

Close up and replace the grate and remove all traffic control. All removed debris and pollutants shall be disposed of following local and state requirements.



For Maintenance Services or Information Please Contact Us At: 760-433-7640 Or Email: info@biocleanenvironmental.com

# Bio Clean

# Inspection and Maintenance Report Catch Basin Only

| Project Name For Office Use Only                                                    |                              |                  |                                      |                       |                         |                          |                    |                       |                                                |  |
|-------------------------------------------------------------------------------------|------------------------------|------------------|--------------------------------------|-----------------------|-------------------------|--------------------------|--------------------|-----------------------|------------------------------------------------|--|
| Project A                                                                           | ddress                       |                  |                                      |                       |                         |                          |                    |                       |                                                |  |
| Owner /                                                                             | Management Company           |                  |                                      |                       | (city)                  | (Zip Code)               |                    | (Reviewed B           | ¥Y)                                            |  |
|                                                                                     |                              |                  |                                      | Phone (               |                         |                          |                    | (Date)<br>Office pers | onnel to complete section to the left.         |  |
| Inspector Name Date// Time AM / PM                                                  |                              |                  |                                      |                       |                         |                          |                    |                       |                                                |  |
| Type of Inspection Routine I collow Up Complaint torm Storm Event in Last 72-hours? |                              |                  |                                      |                       |                         |                          |                    |                       |                                                |  |
|                                                                                     | Condition                    |                  |                                      | Additiona             | Notes                   |                          |                    | -                     |                                                |  |
| Weather                                                                             |                              |                  |                                      |                       |                         |                          |                    |                       |                                                |  |
| Site<br>Map #                                                                       | GPS Coordinates of<br>Insert | Catch Basin Size | Evidence of<br>Illicit<br>Discharge? | Trash<br>Accumulation | Foliage<br>Accumulation | Sediment<br>Accumulation | Signs of S<br>Dama |                       | Functioning Properly or<br>Maintenance Needed? |  |
| 1                                                                                   | Lat:                         |                  |                                      |                       |                         |                          |                    |                       |                                                |  |
| 2                                                                                   | Long:<br>Lat:                |                  |                                      |                       |                         |                          |                    |                       |                                                |  |
| 3                                                                                   | Long:<br>Lat:                |                  |                                      |                       |                         |                          |                    |                       |                                                |  |
| 4                                                                                   | Long:<br>Lat:                |                  |                                      |                       |                         |                          |                    |                       |                                                |  |
|                                                                                     | Long:                        |                  |                                      |                       |                         |                          |                    |                       |                                                |  |
| 5                                                                                   | Lat:<br>Long:                |                  |                                      |                       |                         |                          |                    |                       |                                                |  |
| 6                                                                                   | Lat:                         |                  |                                      |                       |                         |                          |                    |                       |                                                |  |
| 7                                                                                   | Long:<br>Lat:                |                  |                                      |                       |                         |                          |                    |                       |                                                |  |
|                                                                                     | Long:                        |                  |                                      |                       |                         |                          |                    |                       |                                                |  |
| 8                                                                                   | Lat:                         |                  |                                      |                       |                         |                          |                    |                       |                                                |  |
| 10                                                                                  | Long:<br>Lat:                |                  |                                      |                       |                         |                          |                    |                       |                                                |  |
|                                                                                     | Long:                        |                  |                                      |                       |                         |                          |                    |                       |                                                |  |
| 11                                                                                  | Lat:<br>Long:                |                  |                                      |                       |                         |                          |                    |                       |                                                |  |
| 12                                                                                  | Lat:                         |                  |                                      |                       |                         |                          |                    |                       |                                                |  |
|                                                                                     | Long:                        |                  |                                      |                       |                         |                          |                    |                       |                                                |  |
| Commen                                                                              | ts:                          |                  |                                      |                       |                         |                          |                    |                       |                                                |  |
|                                                                                     |                              |                  |                                      |                       |                         |                          |                    |                       |                                                |  |

# Curb Inlet Filter



# **OPERATION & MAINTENANCE**



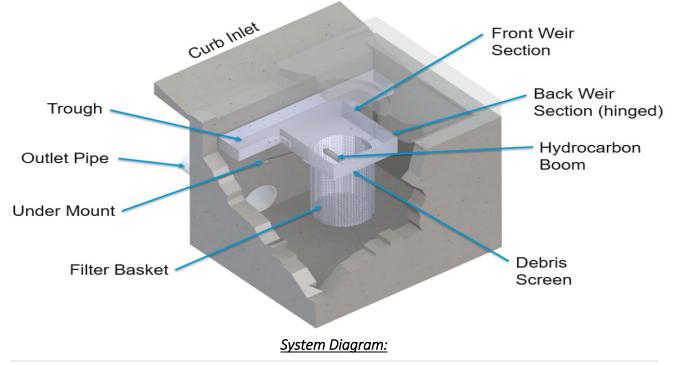
Bio Clean Environmental Services, Inc. 398 Via El Centro Oceanside, CA 92058 www.BioCleanEnvironmental.com p: 760.433.7640 f: 760.433.3176



# **OPERATION & MAINTENANCE**

The Bio Clean Curb Inlet Filter is a stormwater device designed to remove high levels of trash, debris, sediments and hydrocarbons. The filter is available in several configurations including trash full capture, multi-level screening, Kraken membrane filter and media filter variations. This manual covers maintenance procedures of the trash full capture and multi-level screening configurations. A supplemental manual is available for the Kraken and media filter variations. The innovative trough & weir system is mounted along the curb face and directs incoming stormwater toward the filter basket which is positioned "directly" under the manhole access opening regardless of its location in the catch basin. This innovative design allows the filter to be cleaned from finish surface without access into the catch basin, therefore drastically reducing maintenance time and eliminating confined space entry. The filter has a lifting handle allowing for the filter to be removed easily through the manhole. The weir also folds up to allow for unimpeded access into the basin for routine maintenance or pipe jetting.

As with all stormwater BMPs, inspection and maintenance on the Curb Inlet Filter is necessary. Stormwater regulations require BMPs be inspected and maintained to ensure they are operating as designed to allow for effective pollutant removal and provide protection to receiving water bodies. It is recommended that inspections be performed multiple times during the first year to assess sitespecific loading conditions. This is recommended because pollutant loading can vary greatly from site to site. Variables such as nearby soil erosion or construction sites, winter sanding of roads, amount of daily traffic and land use can increase pollutant loading on the system. The first year of inspections can be used to set inspection and maintenance intervals for subsequent years. Without appropriate maintenance a BMP can exceed its storage capacity which can negatively affect its continued performance in removing and retaining captured pollutants.





### Inspection Equipment

Following is a list of equipment to allow for simple and effective inspection of the Curb Inlet Filter:

- Bio Clean Environmental Inspection Form (contained within this manual).
- Manhole hook or appropriate tools to remove access hatches and covers.
- Appropriate traffic control signage and procedures.
- Protective clothing and eye protection.
- Note: entering a confined space requires appropriate safety and certification. It is generally not required for routine inspections or maintenance of the system.



### Inspection Steps

The core to any successful stormwater BMP maintenance program is routine inspections. The inspection steps required on the Curb Inlet Fitler are quick and easy. As mentioned above the first year should be seen as the maintenance interval establishment phase. During the first year more frequent inspections should occur in order to gather loading data and maintenance requirements for that specific site. This information can be used to establish a base for long-term inspection and maintenance interval requirements.

The Curb Inlet Filter can be inspected though visual observation without entry into the catch basin. All necessary pre-inspection steps must be carried out before inspection occurs, such as safety measures to protect the inspector and nearby pedestrians from any dangers associated with an open access hatch or manhole. Once the manhole has been safely opened the inspection process can proceed:

- Prepare the inspection form by writing in the necessary information including project name, location, date & time, unit number and other info (see inspection form).
- Observe the inside of the catch basin through the manhole. If minimal light is available and vision into the unit is impaired utilize a flashlight to see inside the catch basin.
- Look for any out of the ordinary obstructions in the catch basin, trough, weir, filter basket, basin floor our outlet pipe. Write down any observations on the inspection form.
- Through observation and/or digital photographs estimate the amount of trash, foliage and sediment accumulated inside the filter basket. Record this information on the inspection form.
- Observe the condition and color of the hydrocarbon boom. Record this information on the inspection form.



• Finalize inspection report for analysis by the maintenance manager to determine if maintenance is required.

### Maintenance Indicators

Based upon observations made during inspection, maintenance of the system may be required based on the following indicators:

- Missing or damaged internal components.
- Obstructions in the trough, weir, filter basket or catch basin.
- Excessive accumulation of trash, foliage and sediment in the filter basket and/or trough and weir sections. Maintenance is required when the basket is greater than half-full.
- The following chart shows the 50% and 100% storage capacity of each filter height:

| Model      | Filter Basket<br>Diameter (in) | Filter Basket<br>Height (in) | 50% Storage<br>Capacity (cu ft) | 100% Storage<br>Capacity (cu ft) |  |
|------------|--------------------------------|------------------------------|---------------------------------|----------------------------------|--|
| BC-CURB-30 | 18                             | 30                           | 2.21                            | 4.42                             |  |
| BC-CURB-24 | 18                             | 24                           | 1.77                            | 3.53                             |  |
| BC-CURB-18 | 18                             | 18                           | 1.33                            | 2.65                             |  |
| BC-CURB-12 | 18                             | 12                           | 0.88                            | 1.77                             |  |

### Maintenance Equipment

It is recommended that a vacuum truck be utilized to minimize the time required to maintain the Curb Inlet Filter though it can easily cleaned by hand:

- Bio Clean Environmental Maintenance Form (contained in O&M Manual).
- Manhole hook or appropriate tools to access hatches and covers.
- Appropriate safety signage and procedures.
- Protective clothing and eye protection.
- Note: entering a confined space requires appropriate safety and certification. It is generally not required for routine maintenance of the system. Small or large vacuum truck (with pressure washer attachment preferred).

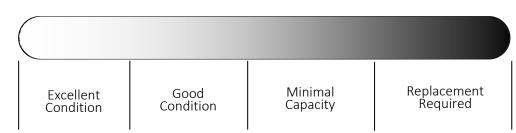
### Maintenance Procedures

It is recommended that maintenance occurs at least two days after the most recent rain event to allow debris and sediments to dry out. Maintaining the system while flows are still entering it will increase the time and complexity required for maintenance. Cleaning of the Curb Inlet Filter can be performed from finish surface without entry into catch basin utilizing a vacuum truck. Some unique



and custom configurations may create conditions which would require entry for some or all of the maintenance procedures. Once all safety measures have been set up cleaning of the Curb Inlet Filter can proceed as followed:

- Remove all manhole cover or access hatches (traffic control and safety measures to be completed prior).
- Using an extension on a vacuum truck position the hose over the opened manhole or hatch opening. Insert the vacuum hose down into the filter basket and suck out trash, foliage and sediment. A pressure wash is recommended and will assist in spraying of any debris stuck on the side or bottom of the filter basket. If the filter basket is full, trash, sediment, and debris will accumulate inside the trough and weir sections of the system. Once the filter basket is clean power wash the weir and trough pushing these debris into the filter basket (leave the hose in the filter basket during this process so entering debris will be sucked out). Power wash off the trough, weir, debris screen, and filter basket sides and bottom.
- Next remove the hydrocarbon boom that is attached to the inside of the filter basket. The hydrocarbon boom is fastened to rails on two opposite sides of the basket (vertical rails). Assess the color and condition of the boom using the following information in the next bullet point. If replacement is required install and fasten on a new hydrocarbon boom. Booms can be ordered directly from the manufacturer.

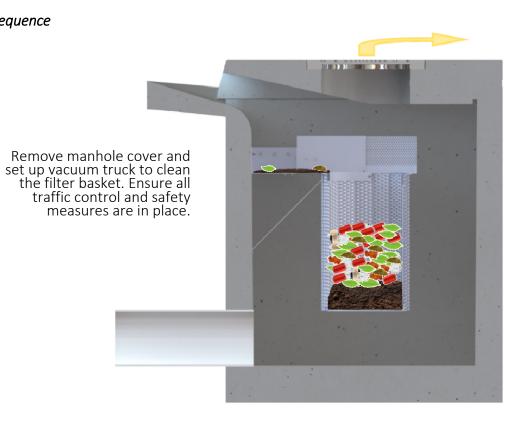


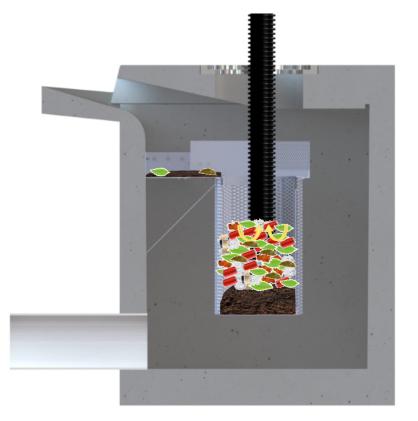
• Follow is a replacement indication color chart for the hydrocarbon booms:

- The last step is to close up and replace the manhole or hatch and remove all traffic control.
- All removed debris and pollutants shall be disposed of following local and state requirements.
- Disposal requirements for recovered pollutants may vary depending on local guidelines. In most areas the sediment, once dewatered, can be disposed of in a sanitary landfill. It is not anticipated that the sediment would be classified as hazardous waste.
- In the case of damaged components, replacement parts can be ordered from the manufacturer. Hydrocarbon booms can also be ordered directly from the manufacturer as previously noted.



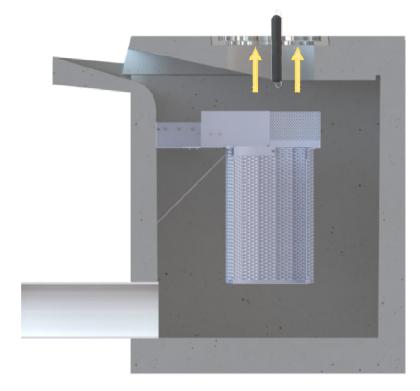
### Maintenance Sequence





Insert the vacuum hose down into the filter basket and suck out debris. Use a pressure washer to assist in vacuum removal. Pressure wash off the weir and trough and vacuum out any remaining debris.





Remove the hydrocarbon boom that is attached to the inside of the filter basket. The hydrocarbon boom is fastened to rails on two opposite sides of the basket (vertical rails). Assess the color and condition of the boom using the following information in the next bullet point. If replacement is required install and fasten on a new hydrocarbon boom.

Close up and replace the manhole or hatch and remove all traffic control. All removed debris and pollutants shall be disposed of following local and state requirements.

# For Maintenance Services or Information Please Contact Us At: 760-433-7640 Or Email: info@biocleanenvironmental.com

# Bio Clean

# Inspection and Maintenance Report Catch Basin Only

| Project Name For Office Use Only                                                    |                              |                  |                                      |                       |                         |                          |                    |                       |                                                |  |
|-------------------------------------------------------------------------------------|------------------------------|------------------|--------------------------------------|-----------------------|-------------------------|--------------------------|--------------------|-----------------------|------------------------------------------------|--|
| Project A                                                                           | ddress                       |                  |                                      |                       |                         |                          |                    |                       |                                                |  |
| Owner /                                                                             | Management Company           |                  |                                      |                       | (city)                  | (Zip Code)               |                    | (Reviewed B           | ¥Y)                                            |  |
|                                                                                     |                              |                  |                                      | Phone (               |                         |                          |                    | (Date)<br>Office pers | onnel to complete section to the left.         |  |
| Inspector Name Date// Time AM / PM                                                  |                              |                  |                                      |                       |                         |                          |                    |                       |                                                |  |
| Type of Inspection Routine I collow Up Complaint torm Storm Event in Last 72-hours? |                              |                  |                                      |                       |                         |                          |                    |                       |                                                |  |
|                                                                                     | Condition                    |                  |                                      | Additiona             | Notes                   |                          |                    | -                     |                                                |  |
| Weather                                                                             |                              |                  |                                      |                       |                         |                          |                    |                       |                                                |  |
| Site<br>Map #                                                                       | GPS Coordinates of<br>Insert | Catch Basin Size | Evidence of<br>Illicit<br>Discharge? | Trash<br>Accumulation | Foliage<br>Accumulation | Sediment<br>Accumulation | Signs of S<br>Dama |                       | Functioning Properly or<br>Maintenance Needed? |  |
| 1                                                                                   | Lat:                         |                  |                                      |                       |                         |                          |                    |                       |                                                |  |
| 2                                                                                   | Long:<br>Lat:                |                  |                                      |                       |                         |                          |                    |                       |                                                |  |
| 3                                                                                   | Long:<br>Lat:                |                  |                                      |                       |                         |                          |                    |                       |                                                |  |
| 4                                                                                   | Long:<br>Lat:                |                  |                                      |                       |                         |                          |                    |                       |                                                |  |
|                                                                                     | Long:                        |                  |                                      |                       |                         |                          |                    |                       |                                                |  |
| 5                                                                                   | Lat:<br>Long:                |                  |                                      |                       |                         |                          |                    |                       |                                                |  |
| 6                                                                                   | Lat:                         |                  |                                      |                       |                         |                          |                    |                       |                                                |  |
| 7                                                                                   | Long:<br>Lat:                |                  |                                      |                       |                         |                          |                    |                       |                                                |  |
|                                                                                     | Long:                        |                  |                                      |                       |                         |                          |                    |                       |                                                |  |
| 8                                                                                   | Lat:                         |                  |                                      |                       |                         |                          |                    |                       |                                                |  |
| 10                                                                                  | Long:<br>Lat:                |                  |                                      |                       |                         |                          |                    |                       |                                                |  |
|                                                                                     | Long:                        |                  |                                      |                       |                         |                          |                    |                       |                                                |  |
| 11                                                                                  | Lat:<br>Long:                |                  |                                      |                       |                         |                          |                    |                       |                                                |  |
| 12                                                                                  | Lat:                         |                  |                                      |                       |                         |                          |                    |                       |                                                |  |
|                                                                                     | Long:                        |                  |                                      |                       |                         |                          |                    |                       |                                                |  |
| Commen                                                                              | ts:                          |                  |                                      |                       |                         |                          |                    |                       |                                                |  |
|                                                                                     |                              |                  |                                      |                       |                         |                          |                    |                       |                                                |  |



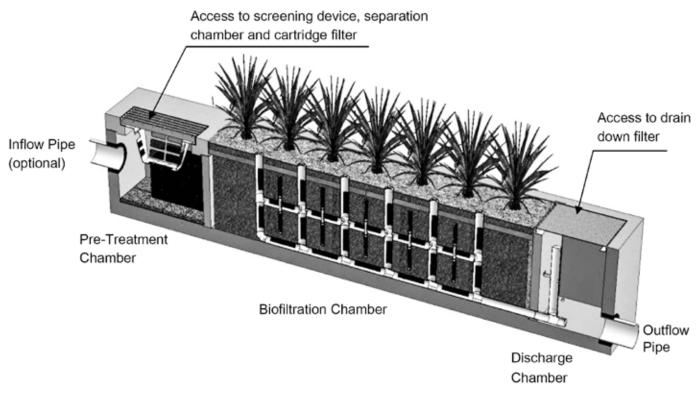
# Modular Wetlands<sup>®</sup> Linear Operation & Maintenance Manual





## **Maintenance Summary**

- Remove Trash from Screening Device average maintenance interval is 6 to 12 months.
  - (5 minute average service time ).
- Remove Sediment from Separation Chamber average maintenance interval is 12 to 24 months.
  - (10 minute average service time).
- Replace Cartridge Filter Media average maintenance interval 12 to 24 months.
  - (10-15 minute per cartridge average service time ).
- Replace Drain Down Filter Media average maintenance interval is 12 to 24 months.
  - (5 minute average service time).
- Trim Vegetation average maintenance interval is 6 to 12 months.
  - (Service time varies).



System Diagram

## **Maintenance Procedures**

### Screening Device

- 1. Remove grate or manhole cover to gain access to the screening device in the Pre- Treatment Chamber. Vault type units do not have screening device. Maintenance can be performed without entry.
- 2. Remove all pollutants collected by the screening device. Removal can be done manually or with the use of a vacuum truck.
- 3. Screening device can easily be removed from the Pre-Treatment Chamber to gain access to separation chamber and media filters below. Replace grate or manhole cover when completed.

### Separation Chamber

- 1. Perform maintenance procedures of screening device listed above before maintaining the separation chamber.
- 2. With a pressure washer, spray down pollutants accumulated on walls and cartridge filters.
- 3. Vacuum out Separation Chamber and remove all accumulated pollutants. Replace screening device, grate or manhole cover when completed.

### **Cartridge Filters**

- 1. Perform maintenance procedures on screening device and separation chamber before maintaining cartridge filters.
- 2. Enter separation chamber.
- 3. Unscrew the two bolts holding the lid on each cartridge filter and remove lid.
- 4. Remove each of 4 to 8 media cages holding the media in place.
- 5. Spray down the cartridge filter to remove any accumulated pollutants.
- 6. Vacuum out old media and accumulated pollutants.
- 7. Reinstall media cages and fill with new media from manufacturer or outside supplier. Manufacturer will provide specification of media and sources to purchase.
- 8. Replace the lid and tighten down bolts. Replace screening device, grate or manhole cover when completed.

### Drain Down Filter

- 1. Remove hatch or manhole cover over discharge chamber and enter chamber. Entry into chambers may require confined space training based on state and local regulations.
- 2. Unlock and lift drain down filter housing and remove old media block. Replace with new media block. Lower drain down filter housing and lock into place.
- 3. Exit chamber and replace hatch or manhole cover.

### **Maintenance Notes**

- 1. Following maintenance and/or inspection, it is recommended the maintenance operator prepare a maintenance/ inspection record. The record should include any maintenance activities performed, amount and description of debris collected, and condition of the system and its various filter mechanisms.
- 2. The owner should keep maintenance/inspection record(s) for a minimum of five years from the date of maintenance. These records should be made available to the governing municipality for inspection upon request at any time.
- 3. Transport all debris, trash, organics and sediments to approved facility for disposal in accordance with local and state requirements.
- 4. Entry into chambers may require confined space training based on state and local regulations.
- 5. No fertilizer shall be used in the Biofiltration Chamber.
- 6. Irrigation should be provided as recommended by manufacturer and/or landscape architect. Amount of irrigation required is dependent on plant species. Some plants may require irrigation.

### **Maintenance Procedure Illustration**

### Screening Device

The screening device is located directly under the manhole or grate over the Pre-Treatment Chamber. It's mounted directly underneath for easy access and cleaning. Device can be cleaned by hand or with a vacuum truck.



### Separation Chamber

The separation chamber is located directly beneath the screening device. It can be quickly cleaned using a vacuum truck or by hand. A pressure washer is useful to assist in the cleaning process.



### **Cartridge Filters**

The cartridge filters are located in the Pre-Treatment chamber connected to the wall adjacent to the biofiltration chamber. The cartridges have removable tops to access the individual media filters. Once the cartridge is open media can be easily removed and replaced by hand or a vacuum truck.





### Drain Down Filter

The drain down filter is located in the Discharge Chamber. The drain filter unlocks from the wall mount and hinges up. Remove filter block and replace with new block.

### **Trim Vegetation**

Vegetation should be maintained in the same manner as surrounding vegetation and trimmed as needed. No fertilizer shall be used on the plants. Irrigation per the recommendation of the manufacturer and or landscape

architect. Different types of vegetation requires different amounts of irrigation.





### Inspection Report Modular Wetlands Linear

| Project Name                                                     |                  |                |                 |                |               |               |             |           |                | For Office Use Only | 4                 |
|------------------------------------------------------------------|------------------|----------------|-----------------|----------------|---------------|---------------|-------------|-----------|----------------|---------------------|-------------------|
| Project Address                                                  |                  |                |                 |                |               | (city)        | (Zip Code)  |           |                | (Reviewed By)       |                   |
| Owner / Management Company                                       | (zip oode)       |                |                 | (Date)         |               |               |             |           |                |                     |                   |
| Contact Phone ( ) –                                              |                  |                |                 |                |               |               |             |           |                |                     | nplete section to |
| Inspector Name / / Time                                          |                  |                |                 |                |               |               |             |           |                |                     | AM / PM           |
| Type of Inspection   Routin                                      | Storm Eve        | ent in Last 72 | 2-houi          | rs? 🗌 No 🗌 Y   | es            |               |             |           |                |                     |                   |
| Weather Condition                                                |                  |                |                 | A              | dditional Not | es            |             |           |                |                     |                   |
|                                                                  |                  |                | l               | nspectio       | n Checkl      | ist           |             |           |                |                     |                   |
| Modular Wetland System T                                         | ype (Curb,       | Grate or L     | JG Vault):      | -              |               | Size          | (22', 14' ( | or etc.): |                |                     |                   |
| Structural Integrity:                                            |                  |                |                 |                |               |               | Yes         | s No      |                | Commen              | its               |
| Damage to pre-treatment access<br>pressure?                      | cover (manh      | nole cover/gr  | ate) or cannot  | be opened u    | using normal  | lifting       |             |           |                |                     |                   |
| Damage to discharge chamber a<br>pressure?                       | ccess cover      | (manhole co    | ver/grate) or c | annot be ope   | ened using n  | ormal lifting |             |           |                |                     |                   |
| Does the MWS unit show signs o                                   | of structural of | deterioration  | (cracks in the  | wall, damag    | e to frame)?  |               |             |           |                |                     |                   |
| Is the inlet/outlet pipe or drain do                             | wn pipe dam      | aged or othe   | erwise not fund | ctioning prop  | erly?         |               |             |           |                |                     |                   |
| Working Condition:                                               |                  |                |                 |                |               |               |             |           |                |                     |                   |
| Is there evidence of illicit dischar<br>unit?                    | ge or excess     | ive oil, greas | e, or other au  | tomobile fluid | ds entering a | nd clogging   | the         |           |                |                     |                   |
| Is there standing water in inappro                               | opriate areas    | after a dry p  | eriod?          |                |               |               |             |           |                |                     |                   |
| Is the filter insert (if applicable) a                           | t capacity and   | d/or is there  | an accumulati   | on of debris/  | trash on the  | shelf syster  | n?          |           |                |                     |                   |
| Does the depth of sediment/trash specify which one in the commen |                  |                |                 |                |               |               | /es         |           |                |                     | Depth:            |
| Does the cartridge filter media ne                               | ed replacem      | ent in pre-tre | eatment cham    | ber and/or di  | scharge cha   | mber?         |             |           | C              | Chamber:            |                   |
| Any signs of improper functioning                                | g in the disch   | arge chambe    | er? Note issu   | es in comme    | nts section.  |               |             |           |                |                     |                   |
| Other Inspection Items:                                          |                  |                |                 |                |               |               |             |           |                |                     |                   |
| Is there an accumulation of sedir                                | nent/trash/de    | bris in the w  | etland media    | (if applicable | )?            |               |             |           |                |                     |                   |
| Is it evident that the plants are al                             | ive and healt    | hy (if applica | ble)? Please i  | note Plant In  | formation bel | ow.           |             |           |                |                     |                   |
| Is there a septic or foul odor com                               | ing from insid   | de the syster  | n?              |                |               |               |             |           |                |                     |                   |
| Waste:                                                           | Yes              | No             |                 | Rec            | ommende       | d Mainte      | nance       |           |                | Plant Inform        | nation            |
| Sediment / Silt / Clay                                           |                  |                |                 | No Cleaning    | Needed        |               |             |           | C              | Damage to Plants    |                   |
| Trash / Bags / Bottles                                           |                  |                |                 | Schedule Ma    | aintenance as | s Planned     |             |           | F              | Plant Replacement   |                   |
| Green Waste / Leaves / Foliage                                   |                  |                |                 |                |               |               |             |           | Plant Trimming |                     |                   |

Additional Notes:



#### Cleaning and Maintenance Report Modular Wetlands Linear

| Project N     | lame                         |                                        |                       |                         |                          |                              | For Of                                                           | fice Use Only                                                        |
|---------------|------------------------------|----------------------------------------|-----------------------|-------------------------|--------------------------|------------------------------|------------------------------------------------------------------|----------------------------------------------------------------------|
| Project A     | ddress                       |                                        |                       |                         | (city)                   | (Zip Code)                   | (Review                                                          | ed Bv)                                                               |
| Owner /       | Management Company           |                                        |                       |                         |                          |                              | (Date)                                                           |                                                                      |
| Contact       |                              |                                        |                       | Phone (                 | )                        | _                            | Office                                                           | bersonnel to complete section to the left.                           |
| Inspecto      | Name                         |                                        |                       | Date                    | /                        | /                            | Time                                                             | AM / PM                                                              |
| Type of I     | nspection 🗌 Routir           | ne 🗌 Follow Up                         | Complaint             | Storm                   |                          | Storm Event in               | Last 72-hours?                                                   | No 🗌 Yes                                                             |
| Weather       | Condition                    |                                        |                       | Additiona               | al Notes                 |                              |                                                                  |                                                                      |
| Site<br>Map # | GPS Coordinates<br>of Insert | Manufacturer /<br>Description / Sizing | Trash<br>Accumulation | Foliage<br>Accumulation | Sediment<br>Accumulation | Total Debris<br>Accumulation | Condition of Media<br>25/50/75/100<br>(will be changed<br>@ 75%) | Operational Per<br>Manufactures'<br>Specifications<br>(If not, why?) |
|               | Lat:<br>Long:                | MWS<br>Catch Basins                    |                       |                         |                          |                              |                                                                  |                                                                      |
|               |                              | MWS<br>Sedimentation<br>Basin          |                       |                         |                          |                              |                                                                  |                                                                      |
|               |                              | Media Filter<br>Condition              |                       |                         |                          |                              |                                                                  |                                                                      |
|               |                              | - Plant Condition                      |                       |                         |                          |                              |                                                                  |                                                                      |
|               |                              | Drain Down Media<br>Condition          |                       |                         |                          |                              |                                                                  |                                                                      |
|               |                              | Discharge Chamber<br>Condition         |                       |                         |                          |                              |                                                                  |                                                                      |
|               |                              | Drain Down Pipe<br>Condition           |                       |                         |                          |                              |                                                                  |                                                                      |
|               |                              | Inlet and Outlet<br>Pipe Condition     |                       |                         |                          |                              |                                                                  |                                                                      |
| Commer        | ts:                          |                                        |                       |                         |                          |                              |                                                                  |                                                                      |
|               |                              |                                        |                       |                         |                          |                              |                                                                  |                                                                      |
|               |                              |                                        |                       |                         |                          |                              |                                                                  |                                                                      |





© 2022 CONTECH ENGINEERED SOLUTIONS LLC, A QUIKRETE COMPANY

800-338-1122

WWW.CONTECHES.COM

ALL RIGHTS RESERVED. PRINTED IN THE USA.

CONTECH ENGINEERED SOLUTIONS LLC PROVIDES SITE SOLUTIONS FOR THE CIVIL ENGINEERING INDUSTRY. CONTECH'S PORTFOLIO INCLUDES BRIDGES, DRAINAGE, SANITARY SEWER, STORMWATER AND EARTH STABILIZATION PRODUCTS. FOR INFORMATION ON OTHER CONTECH DIVISION OFFERINGS, VISIT CONTECHES.COM OR CALL 800-338-1122. NOTHING IN THIS CATALOG SHOULD BE CONSTRUED AS A WARRANTY. APPLICATIONS SUGGESTED HEREIN ARE DESCRIBED ONLY TO HELP READERS MAKE THEIR OWN EVALUATIONS AND DECISIONS, AND ARE NEITHER GUARANTEES NOR WARRANTIES OF SUITABILITY FOR ANY APPLICATION. CONTECH MAKES NO WARRANTY WHATSOEVER, EXPRESS OR IMPLIED, RELATED TO THE APPLICATIONS, MATERIALS, COATINGS, OR PRODUCTS DISCUSSED HEREIN. ALL IMPLIED WARRANTIES OF FITNESS FOR ANY PARTICULAR PURPOSE ARE DISCLAIMED BY CONTECH. SEE CONTECH'S CONDITIONS OF SALE (AVAILABLE AT WWW.CONTECHES.COM/COS) FOR MORE INFORMATION.

#### SUPPORT

DRAWINGS AND SPECIFICATIONS ARE AVAILABLE AT WWW.CONTECHES.COM

# PSI Pacific Southwest Industries

ENGINEERED - PUMPS/FLUID HANDLING & DISPOSAL SYSTEMS - PACKAGED LIFT STATIONS

#### LIFT STATION REQUIRED MAINTENANCE

The lift station should be inspected twice a year for proper operation, and should be checked for overabundance of solid matter such as grease and soap buildup.

Proper operation and inspection would include the following:

- 1) Automatic operation of the system by float activation. One pump starting at lead on levels, second pump starting at high level conditions; manual operation by use of the selector switches.
- 2) Inspect floats for proper elevation and for proper movement. Correct any obstructions.
- 3) Check incoming power for proper voltage. Check voltage at motor connections.
- 4) Check amperage of each motor.
- 5) Hose down lift station to clean the walls of the wet well, pumps and floats.

#### MECHANICAL SEAL INSPECTION OF PUMPS

Inspection of the mechanical seals should be done every two years.

The inspection will include the following:

Pull pump out of wet well. Remove oil seal plug and inspect the oil for clarity. Clear oil indicates no water intrusion and chamber is to be topped off with 30 weight turbine oil. If oil is cloudy the mechanical seal and oil needs to be replaced.

PSI recommends that preventive maintenance and service be performed by a qualified technician.

Any question regarding your lift station should be directed to Scott Richardson at 800-358-9095.

Appendix E: Infiltration Feasibility

(For Reference Purposes Only)

From: Tawnie Schraan <tschraan@cityoforange.org> Sent: Tuesday, March 22, 2022 8:29 AM To: Nicole Morse <NMorse@tbplanning.com> Subject: RE: 759 Eckhoff

#### Hi Nicole,

During the final step of our review, we are required to submit the WQMP to OCWD. During their review, there was a concern about using infiltration. Although there is no direct evidence of contamination of the soils at either the deep or shallow ground water level at the proposed site; Orange County Water District does not recommend introducing (infiltrating) storm water into the larger ground water table near the site, without any further comprehensive analysis. OCWD has made this finding based on concerns from historical uses on sites that are in the vicinity and up-gradient of the proposed project.

In light of this concern raised by the OCWD, we are not recommending the use of infiltration at the site and new BMPs must be presented capable of treating the DCV. Please feel free to contact me or the Program Manager – Mike Carney, with any further questions.

Thank you,

Tawnie Schraan, P.E. Associate Civil Engineer City of Public Works – Development Services

300 E. Chapman Ave | Orange, CA 92866 Direct: (714) 744-5528 | <u>www.cityoforange.org</u> October 4, 2021

IDI Logistics 840 Apollo Street Suite 343 El Segundo, CA 90245



- Attention: Mr. Brandon Dickens Vice President of Capital Deployment
- Project No.: **20G199-3**
- Subject: **Results of Updated Infiltration Testing** Two Proposed Industrial Buildings 759 North Eckhoff Street Orange, California
- Reference: <u>Geotechnical Investigation, Two Proposed Industrial Buildings, 759 North Echoff</u> <u>Street, Orange. California</u>, prepared by Southern California Geotechnical, Inc. (SCG), prepared for IDI Logistics, LLC, SCG Project No. 20G199-1, dated October 30, 2020.

Mr. Dickens:

In accordance with your request, we have conducted infiltration testing at the subject site. We are pleased to present this report summarizing the results of the infiltration testing and our design recommendations.

#### Scope of Services

The scope of services performed for this project was in general accordance with our Proposal No. 20P342R and Change Order No. 20G199-CO, dated September 15, 2020 and June 17, 2021, respectively. The scope of services included site reconnaissance, subsurface exploration, field testing, and engineering analysis to determine the infiltration rates of the onsite soils. The infiltration testing was performed in general accordance with the guidelines published by Orange County: <u>Technical Guidance Document for the Preparation of Conceptual/Preliminary and/or Project Water Quality Management Plans (WQMPs), Appendix VII</u>. These guidelines are dated December 20, 2013.

#### Site and Project Description

The subject site is located on the east side of Eckhoff Street,  $500\pm$  feet north of the intersection with Sequoia Avenue in Orange, California. The site is also referenced by the street address of 759 North Eckhoff Street. The site is bounded to the west by Eckhoff Street, to the north by the BNSF railroad and to the south and east by existing commercial/industrial developments. The general location of the site is illustrated on the Site Location Map, included as Plate 1 of this report.

The subject site is an irregularly-shaped area, 12.57± acres in size. The site is presently developed with several commercial/industrial facilities, including Oilwell Varco. These buildings are of tilt-up concrete and/or steel frame construction, and are assumed to be supported on conventional shallow foundations with concrete slab-on-grade floors. The buildings are surrounded by Portland cement concrete pavements within the fenced areas. Heavy machinery, scaffolds, and stored products surround the buildings. A steel tower, approximately 150 feet in height, apparently used for testing drilling equipment, is located in the north-central area of the site. Several gates and chain-link fences are located on the property. The buildings are surrounded by Portland cement concrete pavements within the fenced areas. The remaining areas of the site are paved with asphaltic concrete pavements for automobile and truck parking. Several landscaped planters are present along Eckhoff Avenue.

Preliminary topographic information was obtained from an ALTA survey provided by the client. Based on this survey, the site is relatively level, sloping slightly downward to the west/Southwest. There appears to be less than 3 to  $4\pm$  feet of elevation differential across the site.

#### Proposed Development

Based on the site plan (Scheme 1) provided to our office, the proposed development will consist of two (2) new industrial buildings,  $187,710\pm$  and  $102,270\pm$  ft<sup>2</sup> in size. Loading docks will be constructed along a portion of one building wall for each new building. We expect that the buildings will be surrounded by asphaltic concrete pavements in the parking and drive areas, Portland cement concrete pavements in the truck court areas, with isolated areas of concrete flatwork and landscape planters.

We understand that the proposed development will include on-site stormwater infiltration. The infiltration system will consist of a below-grade chamber systems located in the northern, southern, and southeastern regions of the site. Based on conversations with the project civil engineer, the bottom of the infiltration systems will range from 10 to  $12\pm$  feet below the existing site grades.

#### Concurrent Study

SCG concurrently conducted a geotechnical investigation at the subject site, also referenced above. As part of this study seven (7) borings were advanced to depths of 15 to  $50\pm$  feet below existing site grades. Portland cement concrete (PCC) was encountered at the ground surface of Boring Nos. B-1 and B-3 through B-6. The pavement sections consist of 8 to  $10^{1/2}\pm$  inches of reinforced PCC. Boring Nos. B-2 and B-7 encountered asphaltic concrete (AC) pavements at the ground surface. These pavement sections consist of  $3^{1/2}$  to  $4\pm$  inches of AC underlain by  $6\pm$  inches of aggregate base. With the exception of Boring No. B-3, all the borings encountered fill soils immediately beneath the pavement surface. These fill soils extend to depths of  $2^{1/2}$  to  $5^{1/2}\pm$  feet. The fill soils generally consist of loose to dense silty fine sands and silty fine to coarse gravel. Additional soils classified as possible fill were also encountered, extending to depths of up to  $6^{1/2}\pm$  feet. The possible fill soils generally consist of loose to medium dense silty fine sands and fine to coarse sands with occasional gravel content, extending to depths of  $1^{1/2}\pm$  feet. Native alluvium was encountered beneath the fill/possible fill soils and



beneath the pavement surface at Boring No. B-3. Within the upper  $25\pm$  feet the alluvium generally consists of loose to medium dense sands, silty sands and sandy silt as well as soft to medium stiff silty clays and clayey silts. At greater depths, the alluvium consists of dense to very dense silty fine to coarse sands with occasional fine to coarse gravel and cobbles, extending to depths of at least  $50\pm$  feet. Boring No. B-7 was terminated within the dense native alluvium at a depth of  $36\pm$  feet after encountering refusal within dense gravel and cobbles.

#### <u>Groundwater</u>

Groundwater was not encountered at any of the borings. Based on the lack of any water within the borings, and the moisture contents of the recovered soil samples, the static groundwater table is considered to have existed at a depth in excess of  $50\pm$  feet below existing site grades, at the time of the subsurface investigation.

As part of our research, we reviewed available groundwater data in order to determine the historic high groundwater level for the site. The primary reference used to determine the historic groundwater depths in area of the subject site is CGS Seismic Hazard Zone Report (SHZR) 011 for the Orange 7.5 Minute Quadrangle, which indicates that the historic high groundwater level for the site was  $20\pm$  feet below the ground surface in the western area of the site, and slightly over  $30\pm$  feet in the eastern area.

Recent water level data was obtained from the California Department of Water Resources, Water Data Library Station Map, website, <u>https://wdl.water.ca.gov/waterdatalibrary/Home.aspx</u>. The nearest monitoring well on record is located 0.91 miles south-southwest of the site. Water level readings within this monitoring well indicate a groundwater level of 60± feet below the ground surface in June 2008.

#### Subsurface Exploration

#### Scope of Exploration

The subsurface exploration conducted for the infiltration testing consisted of eight (8) infiltration test borings, advanced to depths of 10 to  $12\pm$  feet below the existing site grades. The infiltration borings were advanced using a truck-mounted drilling rig, equipped with 8-inch diameter hollow stem augers and were logged during drilling by a member of our staff. The approximate locations of the infiltration test borings (identified as I-1 through I-8) are indicated on the Infiltration Test Location Plan, enclosed as Plate 2 of this report.

Upon the completion of the infiltration borings, the bottom of each test boring was covered with  $2\pm$  inches of clean 3/4-inch gravel. A sufficient length of 3-inch-diameter perforated PVC casing was then placed into each test hole so that the PVC casing extended from the bottom of the test hole to the ground surface. Clean 3/4-inch gravel was then installed in the annulus surrounding the PVC casing.



#### Geotechnical Conditions

#### Pavement

AC or PCC pavements were encountered at all eight (8) boring locations. The encountered pavements consisted of 2 to  $6\pm$  inches AC with 3 to  $6\pm$  inches AB. Infiltration Test Nos. I-1, I-2, I-7 and I-8 encountered  $8\frac{1}{2}$  to  $10\pm$  inches of PCC with no discernable aggregate base at the ground surface.

#### Artificial Fill

Artificial fill and possible fill soils were encountered beneath the pavements at all eight (8) boring locations, extending to depths of 3 to  $5\frac{1}{2}\pm$  feet below existing site grades. The artificial fill soils consisted of medium dense silty fine sands, fine sandy silts, and fine sands. Dense fine sands were also encountered within the fill strata. Trace quantities of medium to coarse sand and clay nodules were also encountered within the artificial fill.

#### <u>Alluvium</u>

Native alluvial soils were encountered beneath the artificial fill soils at all eight (8) boring locations, extending to at least the maximum explored depth of 12± feet below existing site grades. The alluvium generally consisted of very loose to medium dense fine sands, loose silty fine sands and silts, medium dense fine to medium sands, and stiff silty clays and clayey silts. Variable trace quantities of medium to coarse sand, silt, and clay were encountered within the alluvial strata. The Boring Logs, which illustrate the conditions encountered at the boring locations, are included with this report.

#### Infiltration Testing

As previously mentioned, the infiltration testing was performed in general accordance with the Orange County guidelines: <u>Technical Guidance Document for the Preparation of Conceptual/Preliminary and/or Project Water Quality Management Plans (WOMPs), Appendix VII.</u>

#### Pre-soaking

In accordance with the county infiltration standards, all eight (8) of the infiltration test borings were pre-soaked prior to the infiltration testing. The pre-soaking process consisted of filling the test borings by inverting a full 5-gallon bottle of clear water supported over each hole so that the water level reaches a level of at least 5 times the hole's radius above the gravel at the bottom of each hole. The pre-soaking was completed after all of the water had percolated through each test hole or after 15 hours since initiating the pre-soak. Based on the results of the pre-soaking process, different infiltration procedures were used during the infiltration testing at the infiltration boring locations.



#### Infiltration Testing

Following the pre-soaking process of the infiltration test borings, SCG performed the infiltration testing. Each test hole was filled with water to a depth of at least 5 times the hole's radius above the gravel at the bottom of each test hole, and less than or equal to the water level used during the pre-soaking process. In accordance with the Orange County guidelines, since "sandy soils" were encountered at the bottom of Infiltration Boring Nos. I-1, I-4, I-6, and I-7 (when two-consecutive measurements show that 6 inches of water seep away in less than 25 minutes), these tests were run for an additional hour with measurements taken at 10-minute and 1-minute intervals. Since "non-sandy soils" were encountered at the bottom of Infiltration Boring Nos. I-2, I-3, I-5, and I-8, readings were taken at 30-minute intervals for a total of 6 hours at the test locations. After each reading, the borings were refilled to the correct water level above the gravel at the bottom of each test hole. The water level readings are presented on the spreadsheets enclosed with this report. The infiltration rates for each of the timed intervals are also tabulated on the spreadsheets.

The infiltration rates from the test are tabulated in inches per hour. In accordance with the typically accepted practice, it is recommended that the most conservative reading from the latter part of the infiltration tests be used as the design infiltration rate. The rates are summarized below:

| Infiltration<br>Test No. | Surface<br>Elevation<br>(feet) | <u>Depth to</u><br><u>Bottom of</u><br><u>Test</u><br><u>(feet)</u> | <u>Bottom of</u><br><u>Infiltration</u><br><u>system</u><br>(msl feet) | Soil Description                                                          | <u>Infiltration</u><br><u>Rate</u><br>(inches/hour) |
|--------------------------|--------------------------------|---------------------------------------------------------------------|------------------------------------------------------------------------|---------------------------------------------------------------------------|-----------------------------------------------------|
| I-1                      | 158.3                          | 10                                                                  | 158.0                                                                  | Light Gray Brown fine to<br>medium Sand, trace coarse<br>Sand, trace Silt | 21.1                                                |
| I-2                      | 158.2                          | 10                                                                  | 158.0                                                                  | Gray Brown fine Sandy Silt,<br>trace medium Sand                          | 1.0                                                 |
| I-3                      | 157.7                          | 12                                                                  | 158.0                                                                  | Light Gray Brown fine Sandy<br>Silt, trace medium Sand                    | 0.5                                                 |
| I-4                      | 158.1                          | 12                                                                  | 158.0                                                                  | Light Brown fine to medium<br>Sand, trace coarse Sand, little<br>Silt     | 4.4                                                 |
| I-5                      | 158.3                          | 12                                                                  | 158.0                                                                  | Brown Silty Clay, little fine<br>Sand                                     | 0.3                                                 |
| I-6                      | 156.4                          | 12                                                                  | 158.0                                                                  | Gray Brown Gravelly Silt, some fine to coarse Sand                        | 4.3                                                 |
| I-7                      | 158.3                          | 10                                                                  | 158.0                                                                  | Brown fine to coarse Sand,<br>trace Silt                                  | 22.1                                                |
| I-8                      | 158.5                          | 12                                                                  | 158.0                                                                  | Gray Brown Clayey Silt,<br>little fine Sand                               | 0.8                                                 |

Note: Infiltration Test Nos. I-1, I-2, and I-7 are located approximately 30 feet away from the B.N.S.F. Railroad tracks.



#### Laboratory Testing

#### Moisture Content

The moisture contents for the recovered soil samples within the borings were determined in accordance with ASTM D-2216 and are expressed as a percentage of the dry weight. These test results are presented on the Boring Logs.

#### Grain Size Analysis

The grain size distribution of selected soils collected from the bottom of each infiltration test boring have been determined using a range of wire mesh screens. These tests were performed in general accordance with ASTM D-422 and/or ASTM D-1140. The weight of the portion of the sample retained on each screen is recorded and the percentage finer or coarser of the total weight is calculated. The results of these tests are presented on Plates C-1 through C-8 of this report.

#### **Design Recommendations**

Eight (8) infiltration tests were performed at the subject site. As noted above, the infiltration rates at these locations range from 0.3 to 22.1 inches per hour. **Based on the results of the infiltration testing, we recommend the following design infiltration rates for the proposed below-grade chamber systems:** 

| Infiltration Test<br>No. | Infiltration<br>System | Measured Infiltration Rate<br>(Inches per Hour)* | Design Infiltration Rate<br>(Inches per Hour)** |
|--------------------------|------------------------|--------------------------------------------------|-------------------------------------------------|
| I-1, I-2, I-7            | "A″                    | 21.6                                             | 9.8                                             |
| I-3, I-4                 | "В″                    | 2.5                                              | 0.8                                             |
| I-5, I-6, I-8            | "С"                    | 1.8                                              | 0.5                                             |

\* Measured infiltration rate based on average rate between each group of tests. Infiltration Test No. I-2 was not included in the average, since it is not located within the proposed system.

**\*\***Design infiltration rate based on Worksheet H: Factor of Safety and Design Infiltration Rate and Worksheet in the Orange County Technical Guidance Document Appendix VII.

We recommend that a representative from the geotechnical engineer be on-site during the construction of the proposed infiltration system to identify the soil classification at the base of the chamber system. It should be confirmed that the soils at the base of the proposed infiltration system corresponds with those presented in this report to ensure that the performance of the system will be consistent with the rates reported herein.



The design of the proposed storm water infiltration system should be performed by the project civil engineer, in accordance with the City of Orange and/or County of Orange guidelines. However, it is recommended that the system be constructed so as to facilitate removal of silt and clay, or other deleterious materials from any water that may enter the system. The presence of such materials would decrease the effective infiltration rates. **It is recommended that the project civil engineer apply an appropriate factor of safety. The infiltration rate recommended above is based on the assumption that only clean water will be introduced to the subsurface profile. Any fines, debris, or organic materials could significantly impact the infiltration rates.** It should be noted that the recommended infiltration rate of the storm water infiltration system could vary considerably.

#### **Infiltration Rate Considerations**

The infiltration rates presented herein was determined in accordance with the City of Orange and/or County of Orange guidelines and are considered valid only for the time and place of the actual test. Varying subsurface conditions will exist in other areas of the site, which could alter the recommended infiltration rates presented above. The infiltration rates will decline over time between maintenance cycles as silt or clay particles accumulate on the BMP surface. The infiltration rate is highly dependent upon a number of factors, including density, silt and clay content, grainsize distribution throughout the range of particle sizes, and particle shape. Small changes in these factors can cause large changes in the infiltration rates.

Infiltration rates are based on unsaturated flow. As water is introduced into soils by infiltration, the soils become saturated and the wetting front advances from the unsaturated zone to the saturated zone. Once the soils become saturated, infiltration rates become zero, and water can only move through soils by hydraulic conductivity at a rate determined by pressure head and soil permeability. Changes in soil moisture content will affect the infiltration rate. Infiltration rates should be expected to decrease until the soils become saturated. Soil permeability values will then govern groundwater movement. Permeability values may be on the order of 10 to 20 times less than infiltration rates. The system designer should incorporate adequate factors of safety and allow for overflow design into appropriate traditional storm drain systems, which would transport storm water off-site.

#### **Construction Considerations**

The infiltration rates presented in this report are specific to the tested locations and tested depths. Infiltration rates can be significantly reduced if the soils are exposed to excessive disturbance or compaction during construction. Compaction of the soils at the bottom of the infiltration system can significantly reduce the infiltration ability of the basins. Therefore, the subgrade soils within proposed infiltration system areas should not be over-excavated, undercut or compacted in any significant manner. **It is recommended that a note to this effect be added to the project plans and/or specifications.** 

We recommend that a representative from the geotechnical engineer be on-site during the construction of the proposed infiltration systems to identify the soil classification at the base of each system. It should be confirmed that the soils at the base of the proposed infiltration systems correspond with those presented in this report to ensure that the performance of the systems will be consistent with the rates reported herein.



We recommend that scrapers and other rubber-tired heavy equipment not be operated on the basin bottom, or at levels lower than 2 feet above the bottom of the system, particularly within basins. As such, the bottom 24 inches of the infiltration systems should be excavated with non-rubber-tired equipment, such as excavators.

#### **Basin Maintenance**

The proposed project may include infiltration basins. Water flowing into these basins will carry some level of sediment. Wind-blown sediments and erosion of the basin side walls will also contribute to sediment deposition at the bottom of the basin. This layer has the potential to significantly reduce the infiltration rate of the basin subgrade soils. Therefore, a formal basin maintenance program should be established to ensure that these silt and clay deposits are removed from the basin on a regular basis. Appropriate vegetation on the basin sidewalls and bottom may reduce erosion and sediment deposition.

Basin maintenance should also include measures to prevent animal burrows, and to repair any burrows or damage caused by such. Animal burrows in the basin sidewalls can significantly increase the risk of erosion and piping failures.

#### Location of Infiltration Systems

The use of on-site storm water infiltration systems carries a risk of creating adverse geotechnical conditions. Increasing the moisture content of the soil can cause the soil to lose internal shear strength and increase its compressibility, resulting in a change in the designed engineering properties. Overlying structures and pavements in the infiltration area could potentially be damaged due to saturation of the subgrade soils. **The proposed infiltration systems for this site should be located at least 25 feet away from any structures, including retaining walls and railroad tracks.** Even with this provision of locating the infiltration system at least 25 feet from the building(s), it is possible that infiltrating water into the subsurface soils could have an adverse effect on the proposed or existing structures. It should also be noted that utility trenches which happen to collect storm water can also serve as conduits to transmit storm water toward the structure, depending on the slope of the utility trench. Therefore, consideration should also be given to the proposed locations of underground utilities which may pass near the proposed infiltration system.

The infiltration system designer should also give special consideration to the effect that the proposed infiltration systems may have on nearby subterranean structures, open excavations, or descending slopes. In particular, infiltration systems should not be located near the crest of descending slopes, particularly where the slopes are comprised of granular soils. Such systems will require specialized design and analysis to evaluate the potential for slope instability, piping failures and other phenomena that typically apply to earthen dam design. This type of analysis is beyond the scope of this infiltration test report, but these factors should be considered by the infiltration system designer when locating the infiltration systems.



#### **General Comments**

This report has been prepared as an instrument of service for use by the client in order to aid in the evaluation of this property and to assist the architects and engineers in the design and preparation of the project plans and specifications. This report may be provided to the contractor(s) and other design consultants to disclose information relative to the project. However, this report is not intended to be utilized as a specification in and of itself, without appropriate interpretation by the project architect, structural engineer, and/or civil engineer. The design of the infiltration system is the responsibility of the civil engineer. The role of the geotechnical engineer is limited to determination of infiltration rate only. By using the design infiltration rates contained herein, the civil engineer agrees to indemnify, defend, and hold harmless the geotechnical engineer for all aspects of the design and performance of the infiltration system. The reproduction and distribution of this report must be authorized by the client and Southern California Geotechnical, Inc. Furthermore, any reliance on this report by an unauthorized third party is at such party's sole risk, and we accept no responsibility for damage or loss which may occur. The analysis of this site was based on a subsurface profile interpolated from limited discrete soil samples. While the materials encountered in the project area are considered to be representative of the total area, some variations should be expected between trench locations and testing depths. If the conditions encountered during construction vary significantly from those detailed herein, we should be contacted immediately to determine if the conditions alter the recommendations contained herein.

This report has been based on assumed or provided characteristics of the proposed development. It is recommended that the owner, client, architect, structural engineer, and civil engineer carefully review these assumptions to ensure that they are consistent with the characteristics of the proposed development. If discrepancies exist, they should be brought to our attention to verify that they do not affect the conclusions and recommendations contained herein. We also recommend that the project plans and specifications be submitted to our office for review to verify that our recommendations have been correctly interpreted. The analysis, conclusions, and recommendations contained within this report have been promulgated in accordance with generally accepted professional geotechnical engineering practice. No other warranty is implied or expressed.



#### <u>Closure</u>

We sincerely appreciate the opportunity to be of service on this project. We look forward to providing additional consulting services during the course of the project. If we may be of further assistance in any manner, please contact our office.

No. 236

xp. 09/30/2

Respectfully Submitted,

#### SOUTHERN CALIFORNIA GEOTECHNICAL, INC.

. ha

Daryl Kas, CEG 2467 Senior Geologist

Mitul

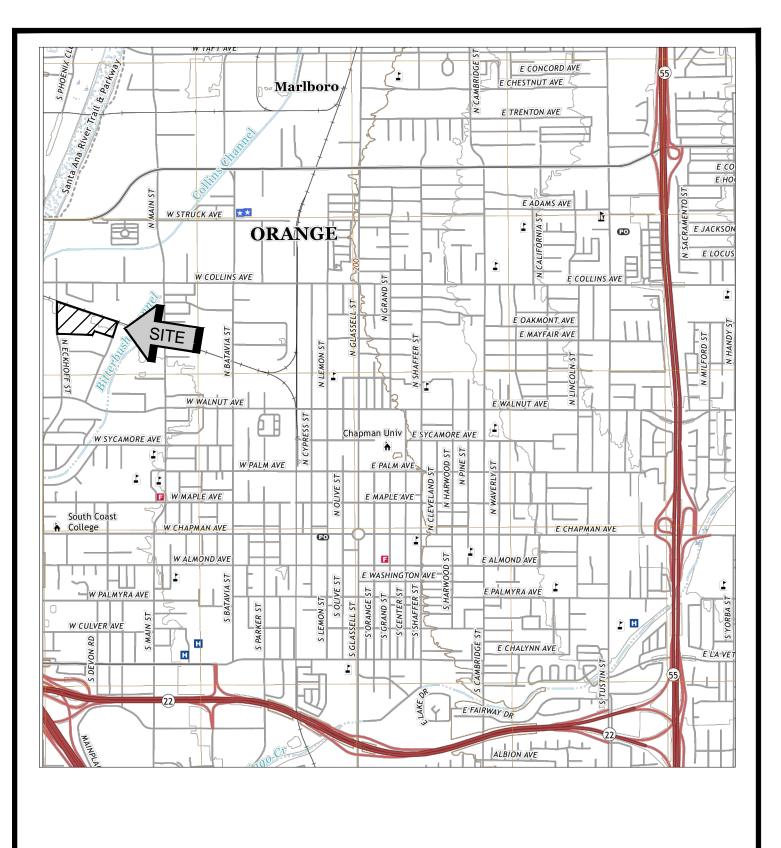
Gregory K. Mitchell, GE 2364 Principal Engineer

Distribution: (1) Addressee

Enclosures: Plate 1 - Site Location Map Plate 2 - Infiltration Test Location Plan Boring Log Legend and Logs (10 pages) Infiltration Test Results Spreadsheets (10 pages) Grain Size Distribution Graphs (8 pages)

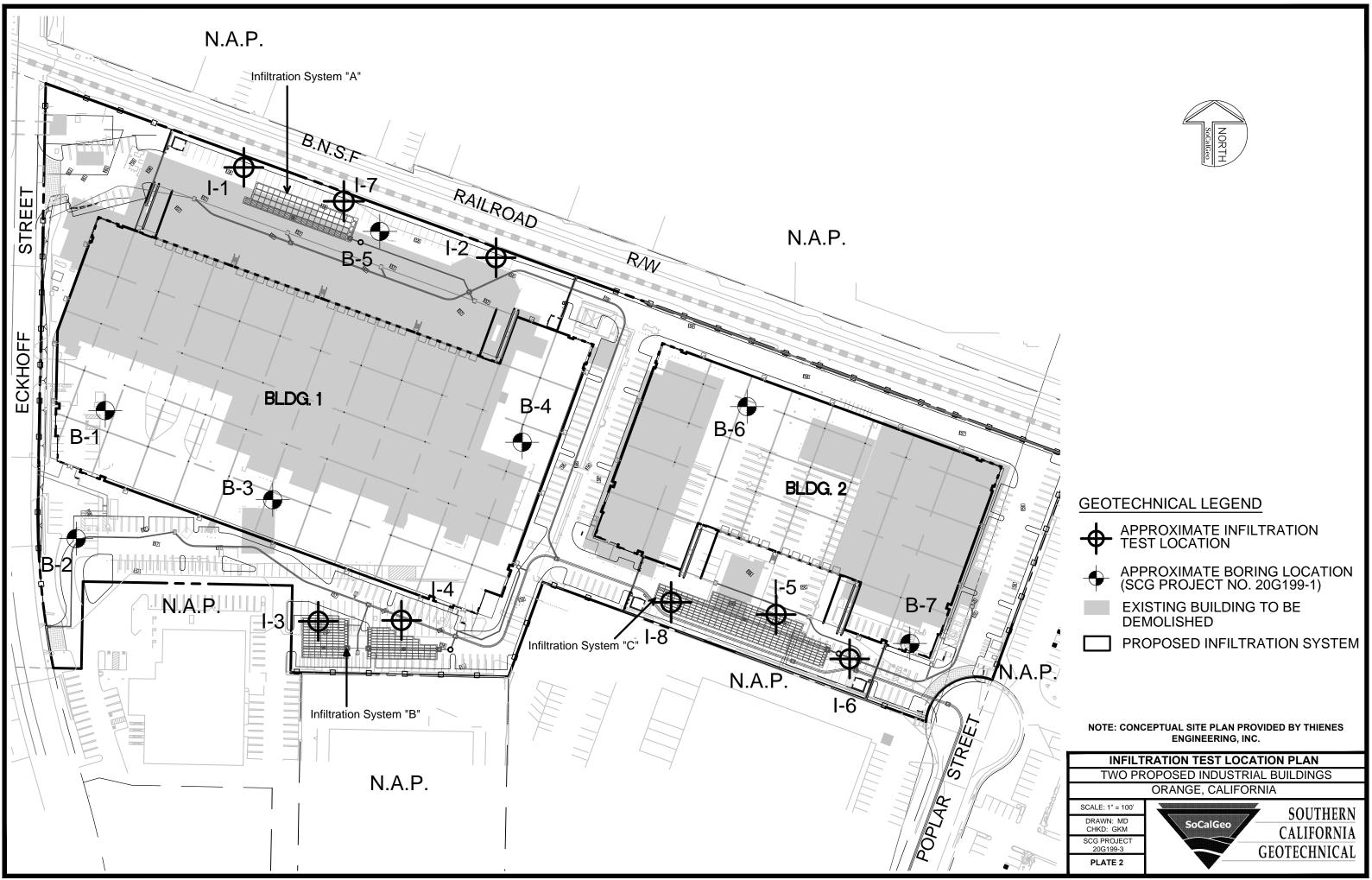








SOURCE: USGS TOPOGRAPHIC MAP OF THE ORANGE QUADRANGLE, ORANGE COUNTY, CALIFORNIA, 2018





## BORING LOG LEGEND

| SAMPLE TYPE | GRAPHICAL<br>SYMBOL | SAMPLE DESCRIPTION                                                                                                                                      |
|-------------|---------------------|---------------------------------------------------------------------------------------------------------------------------------------------------------|
| AUGER       |                     | SAMPLE COLLECTED FROM AUGER CUTTINGS, NO FIELD<br>MEASUREMENT OF SOIL STRENGTH. (DISTURBED)                                                             |
| CORE        |                     | ROCK CORE SAMPLE: TYPICALLY TAKEN WITH A<br>DIAMOND-TIPPED CORE BARREL. TYPICALLY USED<br>ONLY IN HIGHLY CONSOLIDATED BEDROCK.                          |
| GRAB        | M                   | SOIL SAMPLE TAKEN WITH NO SPECIALIZED<br>EQUIPMENT, SUCH AS FROM A STOCKPILE OR THE<br>GROUND SURFACE. (DISTURBED)                                      |
| CS          |                     | CALIFORNIA SAMPLER: 2-1/2 INCH I.D. SPLIT BARREL<br>SAMPLER, LINED WITH 1-INCH HIGH BRASS RINGS.<br>DRIVEN WITH SPT HAMMER. (RELATIVELY<br>UNDISTURBED) |
| NSR         | $\bigcirc$          | NO RECOVERY: THE SAMPLING ATTEMPT DID NOT<br>RESULT IN RECOVERY OF ANY SIGNIFICANT SOIL OR<br>ROCK MATERIAL.                                            |
| SPT         |                     | STANDARD PENETRATION TEST: SAMPLER IS A 1.4<br>INCH INSIDE DIAMETER SPLIT BARREL, DRIVEN 18<br>INCHES WITH THE SPT HAMMER. (DISTURBED)                  |
| SH          |                     | SHELBY TUBE: TAKEN WITH A THIN WALL SAMPLE<br>TUBE, PUSHED INTO THE SOIL AND THEN EXTRACTED.<br>(UNDISTURBED)                                           |
| VANE        |                     | VANE SHEAR TEST: SOIL STRENGTH OBTAINED USING<br>A 4 BLADED SHEAR DEVICE. TYPICALLY USED IN SOFT<br>CLAYS-NO SAMPLE RECOVERED.                          |

#### **COLUMN DESCRIPTIONS**

| <u>DEPTH</u> :       | Distance in feet below the ground surface.                                                                                                                                                                                                                        |
|----------------------|-------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|
| <u>SAMPLE</u> :      | Sample Type as depicted above.                                                                                                                                                                                                                                    |
| BLOW COUNT:          | Number of blows required to advance the sampler 12 inches using a 140 lb hammer with a 30-inch drop. 50/3" indicates penetration refusal (>50 blows) at 3 inches. WH indicates that the weight of the hammer was sufficient to push the sampler 6 inches or more. |
| POCKET PEN.:         | Approximate shear strength of a cohesive soil sample as measured by pocket penetrometer.                                                                                                                                                                          |
| <b>GRAPHIC LOG</b> : | Graphic Soil Symbol as depicted on the following page.                                                                                                                                                                                                            |
| DRY DENSITY:         | Dry density of an undisturbed or relatively undisturbed sample in lbs/ft <sup>3</sup> .                                                                                                                                                                           |
| MOISTURE CONTENT:    | Moisture content of a soil sample, expressed as a percentage of the dry weight.                                                                                                                                                                                   |
| LIQUID LIMIT:        | The moisture content above which a soil behaves as a liquid.                                                                                                                                                                                                      |
| PLASTIC LIMIT:       | The moisture content above which a soil behaves as a plastic.                                                                                                                                                                                                     |
| PASSING #200 SIEVE:  | The percentage of the sample finer than the #200 standard sieve.                                                                                                                                                                                                  |
| UNCONFINED SHEAR:    | The shear strength of a cohesive soil sample, as measured in the unconfined state.                                                                                                                                                                                |

### SOIL CLASSIFICATION CHART

| м                                                                | AJOR DIVISI                            | ONS                              |       | BOLS   | TYPICAL                                                                                                                     |
|------------------------------------------------------------------|----------------------------------------|----------------------------------|-------|--------|-----------------------------------------------------------------------------------------------------------------------------|
|                                                                  |                                        |                                  | GRAPH | LETTER | DESCRIPTIONS                                                                                                                |
|                                                                  | GRAVEL<br>AND                          | CLEAN<br>GRAVELS                 |       | GW     | WELL-GRADED GRAVELS, GRAVEL -<br>SAND MIXTURES, LITTLE OR NO<br>FINES                                                       |
|                                                                  | GRAVELLY<br>SOILS                      | (LITTLE OR NO FINES)             |       | GP     | POORLY-GRADED GRAVELS,<br>GRAVEL - SAND MIXTURES, LITTLE<br>OR NO FINES                                                     |
| COARSE<br>GRAINED<br>SOILS                                       | MORE THAN 50%<br>OF COARSE             | GRAVELS WITH<br>FINES            |       | GM     | SILTY GRAVELS, GRAVEL - SAND -<br>SILT MIXTURES                                                                             |
|                                                                  | FRACTION<br>RETAINED ON NO.<br>4 SIEVE | (APPRECIABLE<br>AMOUNT OF FINES) |       | GC     | CLAYEY GRAVELS, GRAVEL - SAND -<br>CLAY MIXTURES                                                                            |
| MORE THAN 50%<br>OF MATERIAL IS                                  | SAND<br>AND                            | CLEAN SANDS                      |       | SW     | WELL-GRADED SANDS, GRAVELLY<br>SANDS, LITTLE OR NO FINES                                                                    |
| LARGER THAN<br>NO. 200 SIEVE<br>SIZE                             | SANDY<br>SOILS                         | (LITTLE OR NO FINES)             |       | SP     | POORLY-GRADED SANDS,<br>GRAVELLY SAND, LITTLE OR NO<br>FINES                                                                |
|                                                                  | MORE THAN 50%<br>OF COARSE<br>FRACTION | SANDS WITH<br>FINES              |       | SM     | SILTY SANDS, SAND - SILT<br>MIXTURES                                                                                        |
|                                                                  | PASSING ON NO.<br>4 SIEVE              | (APPRECIABLE<br>AMOUNT OF FINES) |       | SC     | CLAYEY SANDS, SAND - CLAY<br>MIXTURES                                                                                       |
|                                                                  |                                        |                                  |       | ML     | INORGANIC SILTS AND VERY FINE<br>SANDS, ROCK FLOUR, SILTY OR<br>CLAYEY FINE SANDS OR CLAYEY<br>SILTS WITH SLIGHT PLASTICITY |
| FINE<br>GRAINED<br>SOILS                                         | SILTS<br>AND<br>CLAYS                  | LIQUID LIMIT<br>LESS THAN 50     |       | CL     | INORGANIC CLAYS OF LOW TO<br>MEDIUM PLASTICITY, GRAVELLY<br>CLAYS, SANDY CLAYS, SILTY CLAYS,<br>LEAN CLAYS                  |
| 00120                                                            |                                        |                                  |       | OL     | ORGANIC SILTS AND ORGANIC<br>SILTY CLAYS OF LOW PLASTICITY                                                                  |
| MORE THAN 50%<br>OF MATERIAL IS<br>SMALLER THAN<br>NO. 200 SIEVE |                                        |                                  |       | МН     | INORGANIC SILTS, MICACEOUS OR<br>DIATOMACEOUS FINE SAND OR<br>SILTY SOILS                                                   |
| SIZE                                                             | SILTS<br>AND<br>CLAYS                  | LIQUID LIMIT<br>GREATER THAN 50  |       | СН     | INORGANIC CLAYS OF HIGH<br>PLASTICITY                                                                                       |
|                                                                  |                                        |                                  |       | ОН     | ORGANIC CLAYS OF MEDIUM TO<br>HIGH PLASTICITY, ORGANIC SILTS                                                                |
| HI                                                               | GHLY ORGANIC S                         | SOILS                            |       | PT     | PEAT, HUMUS, SWAMP SOILS WITH<br>HIGH ORGANIC CONTENTS                                                                      |

NOTE: DUAL SYMBOLS ARE USED TO INDICATE BORDERLINE SOIL CLASSIFICATIONS



| PF                                | ROJE   | CT: 1        | G199-3<br>wo Pro<br>Orange | posed                                 | DRILLING DATE: 10/3/20<br>I Industrial Buildings DRILLING METHOD: Hollow Stem Auger<br>fornia LOGGED BY: Ryan Bremer |                      | CA                      | AVE D           | DEP1<br>EPTH     | :                         |                        | mpletion |
|-----------------------------------|--------|--------------|----------------------------|---------------------------------------|----------------------------------------------------------------------------------------------------------------------|----------------------|-------------------------|-----------------|------------------|---------------------------|------------------------|----------|
|                                   |        |              | ULTS                       |                                       |                                                                                                                      | LAE                  |                         |                 | RY R             |                           |                        |          |
| DEPTH (FEFT)                      | SAMPLE | BLOW COUNT   | POCKET PEN.<br>(TSF)       | GRAPHIC LOG                           | DESCRIPTION<br>SURFACE ELEVATION: 158.3 feet MSL                                                                     | DRY DENSITY<br>(PCF) | MOISTURE<br>CONTENT (%) | LIQUID<br>LIMIT | PLASTIC<br>LIMIT | PASSING<br>#200 SIEVE (%) | ORGANIC<br>CONTENT (%) | COMMENTS |
|                                   |        | 10           |                            |                                       | PAVEMENT:10± inches PCC with no discernible Aggregate                                                                |                      |                         |                 |                  |                           |                        |          |
|                                   |        | 10           |                            |                                       | FILL: Brown Silty fine Sand, trace medium to coarse Sand, trace Clay nodules, loose to medium dense-damp to moist    | -                    | 8                       |                 |                  |                           |                        | -        |
| 5                                 | 5      | 9            |                            |                                       | -                                                                                                                    | -                    | 9                       |                 |                  |                           |                        | -        |
|                                   |        | 3            |                            |                                       | ALLUVIUM: Gray Brown fine Sand, trace to little Silt, trace medium to coarse Sand, very loose-moist                  | -                    | 10                      |                 |                  |                           |                        | -        |
| -1(                               |        | 7 13         |                            | · · · · · · · · · · · · · · · · · · · | Light Gray Brown fine to medium Sand, trace coarse Sand, trace Silt, medium dense-damp                               | -                    | 5                       |                 |                  | 5                         |                        | -        |
|                                   |        |              |                            |                                       | Boring Terminated at 10'                                                                                             |                      |                         |                 |                  |                           |                        |          |
|                                   |        |              |                            |                                       |                                                                                                                      |                      |                         |                 |                  |                           |                        |          |
|                                   |        |              |                            |                                       |                                                                                                                      |                      |                         |                 |                  |                           |                        |          |
| DT 8/10/21                        |        |              |                            |                                       |                                                                                                                      |                      |                         |                 |                  |                           |                        |          |
| 20G199-3.GPJ SOCALGEO.GDT 8/10/21 |        |              |                            |                                       |                                                                                                                      |                      |                         |                 |                  |                           |                        |          |
|                                   |        |              |                            |                                       |                                                                                                                      |                      |                         |                 |                  |                           |                        |          |
| ≓<br>TE                           | EST    | Г <b>В</b> ( | DRIN                       | IG L                                  | _OG                                                                                                                  |                      |                         |                 |                  |                           | P                      | LATE B-1 |



|                                   |           |            | G199-3<br>wo Pro     |                    | DRILLING DATE: 10/3/20<br>I Industrial Buildings DRILLING METHOD: Hollow Stem Auger                                        |                      |                         |                 | DEPT<br>EPTH     |                           | -                      |          |
|-----------------------------------|-----------|------------|----------------------|--------------------|----------------------------------------------------------------------------------------------------------------------------|----------------------|-------------------------|-----------------|------------------|---------------------------|------------------------|----------|
| LO                                | CATI      | ON: (      | Orange               | , Calif            |                                                                                                                            |                      | RE                      | EADIN           | G TAł            | KEN:                      |                        | mpletion |
| FIE                               |           | KESI       | JLTS                 |                    |                                                                                                                            |                      | SOR/                    | AT OF           | ry Ri            | -SUI                      |                        |          |
| DEPTH (FEET)                      | SAMPLE    | BLOW COUNT | POCKET PEN.<br>(TSF) | <b>GRAPHIC LOG</b> | DESCRIPTION<br>SURFACE ELEVATION: 158.2 feet MSL                                                                           | DRY DENSITY<br>(PCF) | MOISTURE<br>CONTENT (%) | LIQUID<br>LIMIT | PLASTIC<br>LIMIT | PASSING<br>#200 SIEVE (%) | ORGANIC<br>CONTENT (%) | COMMENTS |
|                                   |           |            |                      | 0                  | PAVEMENT: 10± inches PCC with no discernible Aggregate                                                                     |                      | 20                      |                 |                  | L #                       | 00                     | 0        |
|                                   |           | 12         |                      |                    | Base<br><u>FILL:</u> Gray Brown intermixed layers of Silty fine Sand, fine<br>Sand, and fine Sandy Silt, medium dense-damp |                      | 7                       |                 |                  |                           |                        |          |
|                                   |           | 7          |                      |                    | ALLUVIUM: Gray Brown fine Sand, trace medium Sand, loose-dry                                                               |                      | 2                       |                 |                  |                           |                        |          |
| 5                                 |           | 4          |                      |                    | Gray Brown fine Sandy Silt, trace medium Sand, trace Iron<br>Oxide staining, loose-very moist to wet                       |                      | 24                      |                 |                  |                           |                        | -        |
|                                   |           | 7 5        |                      |                    | - · · ·                                                                                                                    |                      | 17                      |                 |                  | 58                        |                        |          |
| -10                               | $\square$ |            |                      |                    |                                                                                                                            |                      |                         |                 |                  |                           |                        |          |
| 20G199-3.GPJ SOCALGEO.GDT 8/10/21 |           |            |                      |                    | Boring Terminated at 10'                                                                                                   |                      |                         |                 |                  |                           |                        |          |
| TBL 20G199-3.GPJ                  |           |            |                      |                    |                                                                                                                            |                      |                         |                 |                  |                           |                        |          |
|                                   |           |            |                      |                    | 06                                                                                                                         |                      |                         |                 |                  |                           |                        |          |



| PROJECT: Two P<br>LOCATION: Orang                   | ge, Califor |                                                                                                                                                                                                                              |           | C/<br>RE                | EPTH<br>G TAł | :<br>KEN:                 | At Co                  | mpletion |
|-----------------------------------------------------|-------------|------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|-----------|-------------------------|---------------|---------------------------|------------------------|----------|
| DEPTH (FEET)<br>SAMPLE<br>BLOW COUNT<br>POCKET PEN. |             | DESCRIPTION                                                                                                                                                                                                                  |           | MOISTURE<br>CONTENT (%) |               | PASSING<br>#200 SIEVE (%) | ORGANIC<br>CONTENT (%) | COMMENTS |
|                                                     | GR          | SURFACE ELEVATION: 157.7 feet MSL<br><u>PAVEMENT:</u> 2± inches Asphaltic Concrete with 3± inches<br>Aggregate Base<br><u>FILL:</u> Yellow Brown fine Sand, trace Clay nodules, medium<br>dense to dense-moist to very moist | DR<br>(PC | 90<br>90<br>12          |               | PA:<br>#20                | OR<br>CO               | 8        |
| 5                                                   |             | POSSIBLE FILL: Dark Brown Silty fine Sand, little Iron Oxide<br>staining, medium dense to dense-moist<br><u>ALLUVIUM:</u> Light Gray Brown fine Sand, medium dense-dry to<br>damp                                            |           | 9                       |               |                           |                        |          |
| 6                                                   |             | Light Gray Brown fine Sandy Silt, trace medium Sand, trace<br>Iron Oxide staining, trace Calcareous nodules, loose-dry to<br>wet                                                                                             |           | 3                       |               |                           |                        |          |
|                                                     |             |                                                                                                                                                                                                                              |           | 25<br>20                |               | 52                        |                        |          |
|                                                     | 1.1.1.1.    | Boring Terminated at 12'                                                                                                                                                                                                     |           |                         |               |                           |                        |          |
|                                                     |             |                                                                                                                                                                                                                              |           |                         |               |                           |                        |          |
|                                                     |             |                                                                                                                                                                                                                              |           |                         |               |                           |                        |          |
|                                                     |             |                                                                                                                                                                                                                              |           |                         |               |                           |                        |          |
|                                                     |             |                                                                                                                                                                                                                              |           |                         |               |                           |                        |          |
|                                                     |             |                                                                                                                                                                                                                              |           |                         |               |                           |                        |          |



| PRO          | JEC    | Τ: Τ\      |                      |             | DRILLING DATE: 10/3/20<br>Industrial Buildings DRILLING METHOD: Hollow Stem Auger<br>cornia LOGGED BY: Jamie Hayward                                                                                                                                 |                      | C                       | ATER<br>AVE D<br>EADIN | EPTH             | :                         |                        | ompletion |
|--------------|--------|------------|----------------------|-------------|------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|----------------------|-------------------------|------------------------|------------------|---------------------------|------------------------|-----------|
| FIEL         |        |            |                      |             |                                                                                                                                                                                                                                                      | LA                   |                         | ATOF                   |                  |                           |                        |           |
| DEPTH (FEET) | SAMPLE | BLOW COUNT | POCKET PEN.<br>(TSF) | GRAPHIC LOG | DESCRIPTION<br>SURFACE ELEVATION: 158.1 feet MSL                                                                                                                                                                                                     | DRY DENSITY<br>(PCF) | MOISTURE<br>CONTENT (%) | LIQUID                 | PLASTIC<br>LIMIT | PASSING<br>#200 SIEVE (%) | ORGANIC<br>CONTENT (%) | COMMENTS  |
| -            | X      | 22         |                      |             | PAVEMENT: 2± inches Asphaltic Concrete, 3± inches<br>Aggregate Base<br>FILL: Yellow Brown fine Sand, trace Clay nodules, medium<br>dense-damp to moist<br>POSSIBLE FILL: Dark Brown Silty fine Sand, trace Iron Oxide<br>staining, medium dense-damp | -                    | 9<br>7                  |                        |                  |                           |                        |           |
| 5 -          | X      | 14         |                      |             | ALLUVIUM: Light Gray Brown fine Sand, medium dense-damp                                                                                                                                                                                              | -                    | 5                       |                        |                  |                           |                        |           |
| -            |        | 8          |                      |             | Light Brown fine to medium Sand, little Silt, medium dense-very moist                                                                                                                                                                                | -                    | 11                      |                        |                  |                           |                        |           |
| 10-          | X      | 12         |                      |             | -                                                                                                                                                                                                                                                    | -                    | 15                      |                        |                  | 12                        |                        |           |
|              |        |            |                      |             | Boring Terminated at 12'                                                                                                                                                                                                                             |                      |                         |                        |                  |                           |                        |           |
|              |        |            |                      |             |                                                                                                                                                                                                                                                      |                      |                         |                        |                  |                           |                        |           |
|              |        |            |                      |             |                                                                                                                                                                                                                                                      |                      |                         |                        |                  |                           |                        |           |
|              |        |            |                      |             |                                                                                                                                                                                                                                                      |                      |                         |                        |                  |                           |                        |           |
|              |        |            |                      |             |                                                                                                                                                                                                                                                      |                      |                         |                        |                  |                           |                        |           |
|              |        |            |                      |             |                                                                                                                                                                                                                                                      |                      |                         |                        |                  |                           |                        |           |
| ΓES          | ST     | BC         | )<br>RIN             | IG L        | .OG                                                                                                                                                                                                                                                  |                      |                         |                        |                  |                           | P                      | LATE B-   |



| PRO          | IEC          | Т: Т\      | 6199-3<br>vo Pro<br>Drange | posed       | DRILLING DATE: 10/3/20<br>Industrial Buildings DRILLING METHOD: Hollow Stem Auger<br>Cornia LOGGED BY: Jamie Hayward |                      | C                       | AVE D           | DEPT<br>DEPTH    | :                         |                        | ompletion |
|--------------|--------------|------------|----------------------------|-------------|----------------------------------------------------------------------------------------------------------------------|----------------------|-------------------------|-----------------|------------------|---------------------------|------------------------|-----------|
| IEL          | D R          | ESL        | JLTS                       |             |                                                                                                                      | LAE                  | BOR/                    | ATOF            | RY R             | ESU                       | LTS                    |           |
| DEPTH (FEET) | SAMPLE       | BLOW COUNT | POCKET PEN.<br>(TSF)       | GRAPHIC LOG | DESCRIPTION<br>SURFACE ELEVATION: 158.3 feet MSL                                                                     | DRY DENSITY<br>(PCF) | MOISTURE<br>CONTENT (%) | LIQUID<br>LIMIT | PLASTIC<br>LIMIT | PASSING<br>#200 SIEVE (%) | ORGANIC<br>CONTENT (%) | COMMENTS  |
| _            |              |            |                            | -           | PAVEMENT: 6± inches Asphaltic Concrete, 6± inches                                                                    |                      |                         |                 |                  | - 14                      |                        |           |
|              | X            | 20         | 3.0                        |             | Aggregate Base<br><u>FILL:</u> Dark Brown Silty fine Sand, trace fine Gravel, medium<br>dense-moist                  | -                    | 10                      |                 |                  |                           |                        |           |
| 5            | X            | 22         |                            |             | POSSIBLE FILL: Light Gray Brown fine Sand, medium dense-damp to moist                                                | -                    | 9                       |                 |                  |                           |                        |           |
|              | X            | 7          | 1.5                        |             | <u>ALLUVIUM:</u> Brown fine Sandy Silt, little Iron Oxide staining,<br>loose-wet                                     | -                    | 23                      |                 |                  |                           |                        |           |
| -            | $\mathbf{X}$ | 5          |                            |             | Brown Silt, trace to little Clay, little Iron Oxide staining, loose-very moist                                       | -                    | 23                      |                 |                  |                           |                        |           |
| 10           |              | 9          | 2.0                        |             | Brown Silty Clay, little Iron Oxide staining, little fine Sand,<br>stiff-very moist                                  | -                    | 24                      |                 |                  | 83                        |                        |           |
|              |              |            |                            |             | Boring Terminated at 12'                                                                                             |                      |                         |                 |                  |                           |                        |           |
|              |              |            |                            |             |                                                                                                                      |                      |                         |                 |                  |                           |                        |           |
|              |              |            |                            |             |                                                                                                                      |                      |                         |                 |                  |                           |                        |           |
|              |              |            |                            |             |                                                                                                                      |                      |                         |                 |                  |                           |                        |           |
|              |              |            |                            |             |                                                                                                                      |                      |                         |                 |                  |                           |                        |           |
|              |              |            |                            |             |                                                                                                                      |                      |                         |                 |                  |                           |                        |           |
|              |              |            |                            |             |                                                                                                                      |                      |                         |                 |                  |                           |                        |           |
|              |              |            |                            |             |                                                                                                                      |                      |                         |                 |                  |                           |                        |           |
|              |              |            |                            |             | _OG                                                                                                                  |                      |                         |                 |                  |                           |                        | LATE B    |



| JOB NO<br>PROJEC<br>LOCATI | CT: 1 | Two P       | roposed | DRILLING DATE: 10/3/20<br>I Industrial Buildings DRILLING METHOD: Hollow Stem Auger<br>fornia LOGGED BY: Jamie Hayward                                                                   |                      | C/                      | AVE D |      | :                         |                        | mpletion |
|----------------------------|-------|-------------|---------|------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|----------------------|-------------------------|-------|------|---------------------------|------------------------|----------|
| FIELD I                    |       |             |         |                                                                                                                                                                                          | LAF                  |                         |       | RY R |                           |                        |          |
| DEPTH (FEET)               | DUNT  | POCKET PEN. |         | DESCRIPTION<br>SURFACE ELEVATION: 156.4 feet MSL                                                                                                                                         | DRY DENSITY<br>(PCF) | MOISTURE<br>CONTENT (%) | LIMIT | 0    | PASSING<br>#200 SIEVE (%) | ORGANIC<br>CONTENT (%) | COMMENTS |
|                            | 7 28  |             |         | <u>PAVEMENT:</u> 4± inches Asphaltic Concrete, 6± inches<br>Aggregate Base<br><u>FILL:</u> Gray Brown fine Sand, trace Silt, trace fine Gravel, trace<br>AC fragments, medium dense-damp | -                    | 6                       |       |      |                           |                        |          |
| 5                          | 7 9   |             |         | <u>ALLUVIUM:</u> Gray Brown fine Sandy Silt, trace fine root fibers,<br>trace Iron Oxide staining, trace Calcareous veining,<br>loose-damp to very moist                                 | -                    | 11                      |       |      |                           |                        |          |
|                            | 7 14  |             |         | -<br>-                                                                                                                                                                                   | -                    | 8                       |       |      |                           |                        |          |
| 10                         | 7 12  |             |         | - ·                                                                                                                                                                                      | -                    | 15                      |       |      |                           |                        |          |
|                            | 7 19  |             |         |                                                                                                                                                                                          | -                    | 10                      |       |      | 39                        |                        |          |
|                            |       |             |         | Boring Terminated at 12'                                                                                                                                                                 |                      |                         |       |      |                           |                        |          |
| rest                       | B     | )<br>DRI    | NG I    | LOG                                                                                                                                                                                      |                      |                         |       |      |                           | P                      | LATE B   |



| JOB NO.: 20G199-3       DRILLING DATE: 6/29/21       WATER DEPTH:         PROJECT: Two Proposed Industrial Buildings       DRILLING METHOD: Hollow Stem Auger       CAVE DEPTH:         LOCATION: Orange, California       LOGGED BY: Ryan Bremer       READING TAKEN: At Completion |               |            |                      |             |                                                                                                | mpletion |                         |                 |                  |                           |                        |          |
|--------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|---------------|------------|----------------------|-------------|------------------------------------------------------------------------------------------------|----------|-------------------------|-----------------|------------------|---------------------------|------------------------|----------|
|                                                                                                                                                                                                                                                                                      | FIELD RESULTS |            |                      |             |                                                                                                |          | BOR/                    |                 |                  |                           |                        |          |
| DEPTH (FEET)                                                                                                                                                                                                                                                                         | SAMPLE        | BLOW COUNT | POCKET PEN.<br>(TSF) | GRAPHIC LOG | DESCRIPTION                                                                                    |          |                         | LIQUID<br>LIMIT | PLASTIC<br>LIMIT | PASSING<br>#200 SIEVE (%) | ORGANIC<br>CONTENT (%) | COMMENTS |
| -                                                                                                                                                                                                                                                                                    |               |            |                      |             | PAVEMENT:81/2± inches PCC with no discernible Aggregate                                        |          | MOISTURE<br>CONTENT (%) |                 |                  |                           |                        |          |
|                                                                                                                                                                                                                                                                                      |               | 20         |                      |             | Base<br><u>FILL:</u> Brown Silty fine Sand, trace medium to coarse Sand,<br>medium dense-moist |          | 10                      |                 |                  |                           |                        |          |
| 5                                                                                                                                                                                                                                                                                    |               | 14         |                      |             | POSSIBLE FILL: Gray Brown Silty fine to medium Sand,<br>medium dense-damp                      |          | 4                       |                 |                  |                           |                        |          |
|                                                                                                                                                                                                                                                                                      |               | 6          |                      |             | ALLUVIUM: Brown fine to coarse Sand, trace Silt, loose-damp                                    |          | 5                       |                 |                  |                           |                        |          |
| -10                                                                                                                                                                                                                                                                                  |               | 11         |                      |             | · · · · · · · · · · · · · · · · · · ·                                                          |          | 3                       |                 |                  | 3                         |                        |          |
|                                                                                                                                                                                                                                                                                      |               |            |                      |             | Boring Terminated at 10'                                                                       |          |                         |                 |                  |                           |                        |          |
|                                                                                                                                                                                                                                                                                      |               |            |                      |             |                                                                                                |          |                         |                 |                  |                           |                        |          |
|                                                                                                                                                                                                                                                                                      |               |            |                      |             |                                                                                                |          |                         |                 |                  |                           |                        |          |
|                                                                                                                                                                                                                                                                                      |               |            |                      |             |                                                                                                |          |                         |                 |                  |                           |                        |          |
| 1/21                                                                                                                                                                                                                                                                                 |               |            |                      |             |                                                                                                |          |                         |                 |                  |                           |                        |          |
| TBL 20G199-3.GPJ SOCALGEO.GDT 8/10/21                                                                                                                                                                                                                                                |               |            |                      |             |                                                                                                |          |                         |                 |                  |                           |                        |          |
| -3.GPJ SOCAL                                                                                                                                                                                                                                                                         |               |            |                      |             |                                                                                                |          |                         |                 |                  |                           |                        |          |
| -                                                                                                                                                                                                                                                                                    |               |            |                      |             | 06                                                                                             |          |                         |                 |                  |                           |                        |          |



| P                                 | JOB NO.: 20G199-3     DRILLING DATE: 6/29/21       PROJECT: Two Proposed Industrial Buildings     DRILLING METHOD: Hollow Stem Auger       LOCATION: Orange, California     LOGGED BY: Ryan Bremer |                    |            |                      |                    |                                                                                        |                      | WATER DEPTH:<br>CAVE DEPTH:<br>READING TAKEN: At Completion |                 |                  |                           |                        | mpletion |
|-----------------------------------|----------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|--------------------|------------|----------------------|--------------------|----------------------------------------------------------------------------------------|----------------------|-------------------------------------------------------------|-----------------|------------------|---------------------------|------------------------|----------|
| FI                                | EL                                                                                                                                                                                                 | DF                 | RESU       | JLTS                 |                    |                                                                                        | LABORATORY RESULTS   |                                                             |                 |                  |                           |                        |          |
|                                   | UEPIH (FEEI)                                                                                                                                                                                       | SAMPLE             | BLOW COUNT | POCKET PEN.<br>(TSF) | <b>GRAPHIC LOG</b> | DESCRIPTION<br>SURFACE ELEVATION: 158.5 feet MSL                                       | DRY DENSITY<br>(PCF) | MOISTURE<br>CONTENT (%)                                     | LIQUID<br>LIMIT | PLASTIC<br>LIMIT | PASSING<br>#200 SIEVE (%) | ORGANIC<br>CONTENT (%) | COMMENTS |
|                                   |                                                                                                                                                                                                    |                    |            |                      |                    | PAVEMENT:9± inches PCC with no discernible Aggregate Base                              | _                    |                                                             |                 |                  |                           |                        |          |
|                                   |                                                                                                                                                                                                    | X                  | 20         |                      |                    | FILL: Brown Silty fine Sand, trace to little medium to coarse Sand, medium dense-moist |                      | 8                                                           |                 |                  |                           |                        |          |
|                                   | 5 -                                                                                                                                                                                                | $\square$          | 16         |                      |                    |                                                                                        | -                    | 9                                                           |                 |                  |                           |                        |          |
|                                   |                                                                                                                                                                                                    |                    |            |                      |                    | ALLUVIUM: Gray Brown Silty fine Sand to fine Sandy Silt,                               | -                    |                                                             |                 |                  |                           |                        |          |
|                                   |                                                                                                                                                                                                    | X                  | 4          |                      |                    | trace medium Sand, very loose to loose-very moist                                      |                      | 23                                                          |                 |                  |                           |                        |          |
|                                   |                                                                                                                                                                                                    |                    |            |                      |                    | -                                                                                      | -                    |                                                             |                 |                  |                           |                        |          |
|                                   | -                                                                                                                                                                                                  | $\bigtriangledown$ | 7          |                      |                    | -                                                                                      |                      | 18                                                          |                 |                  |                           |                        | -        |
| 1                                 | 0-                                                                                                                                                                                                 | Д                  |            |                      |                    | Gray Brown Clayey Silt, little fine Sand, little Iron oxide                            | _                    |                                                             |                 |                  |                           |                        | -        |
|                                   | -                                                                                                                                                                                                  | $\bigtriangledown$ | 6          | 1.5                  |                    | staining, micaceous, medium stiff-very moist                                           |                      | 24                                                          |                 |                  | 85                        |                        |          |
|                                   |                                                                                                                                                                                                    | Д                  |            |                      |                    |                                                                                        |                      |                                                             |                 |                  |                           |                        |          |
|                                   |                                                                                                                                                                                                    |                    |            |                      |                    | Boring Terminated at 12'                                                               |                      |                                                             |                 |                  |                           |                        |          |
|                                   |                                                                                                                                                                                                    |                    |            |                      |                    |                                                                                        |                      |                                                             |                 |                  |                           |                        |          |
|                                   |                                                                                                                                                                                                    |                    |            |                      |                    |                                                                                        |                      |                                                             |                 |                  |                           |                        |          |
|                                   |                                                                                                                                                                                                    |                    |            |                      |                    |                                                                                        |                      |                                                             |                 |                  |                           |                        |          |
|                                   |                                                                                                                                                                                                    |                    |            |                      |                    |                                                                                        |                      |                                                             |                 |                  |                           |                        |          |
|                                   |                                                                                                                                                                                                    |                    |            |                      |                    |                                                                                        |                      |                                                             |                 |                  |                           |                        |          |
|                                   |                                                                                                                                                                                                    |                    |            |                      |                    |                                                                                        |                      |                                                             |                 |                  |                           |                        |          |
|                                   |                                                                                                                                                                                                    |                    |            |                      |                    |                                                                                        |                      |                                                             |                 |                  |                           |                        |          |
|                                   |                                                                                                                                                                                                    |                    |            |                      |                    |                                                                                        |                      |                                                             |                 |                  |                           |                        |          |
|                                   |                                                                                                                                                                                                    |                    |            |                      |                    |                                                                                        |                      |                                                             |                 |                  |                           |                        |          |
| /10/21                            |                                                                                                                                                                                                    |                    |            |                      |                    |                                                                                        |                      |                                                             |                 |                  |                           |                        |          |
| GDT 8                             |                                                                                                                                                                                                    |                    |            |                      |                    |                                                                                        |                      |                                                             |                 |                  |                           |                        |          |
| 20G199-3.GPJ SOCALGEO.GDT 8/10/21 |                                                                                                                                                                                                    |                    |            |                      |                    |                                                                                        |                      |                                                             |                 |                  |                           |                        |          |
| SOCA                              |                                                                                                                                                                                                    |                    |            |                      |                    |                                                                                        |                      |                                                             |                 |                  |                           |                        |          |
| 3.GPJ                             |                                                                                                                                                                                                    |                    |            |                      |                    |                                                                                        |                      |                                                             |                 |                  |                           |                        |          |
| 0G199-                            |                                                                                                                                                                                                    |                    |            |                      |                    |                                                                                        |                      |                                                             |                 |                  |                           |                        |          |
| TBL 20                            |                                                                                                                                                                                                    |                    |            |                      |                    |                                                                                        |                      |                                                             |                 |                  |                           |                        |          |
| т                                 |                                                                                                                                                                                                    | хт                 |            | DIN                  |                    | OG                                                                                     |                      |                                                             |                 |                  |                           | D                      | IATE B-8 |

| Project Name     | Two Proposed Industrial Buildings |
|------------------|-----------------------------------|
| Project Location | Orange, CA                        |
| Project Number   | 20G199-3                          |
| Engineer         | Luis Arriaga                      |

Test Hole Radius Test Depth

Infiltration Test Hole

| 4<br>10.2 | (in) |
|-----------|------|
| 10.2      | (ft) |
|           |      |
| I-1       |      |

| Interval<br>Number |         | Time    | Time<br>Interval<br>(min) | Water<br>Depth (ft) | Change in<br>Water<br>Level (ft) | Average<br>Head<br>Height (ft) | Infiltration<br>Rate Q<br>(in/hr) |  |
|--------------------|---------|---------|---------------------------|---------------------|----------------------------------|--------------------------------|-----------------------------------|--|
| PS1                | Initial | 8:00 AM | 1.0                       | 8.70                | 0.42                             | 1.29                           | 34.60                             |  |
|                    | Final   | 8:01 AM |                           | 9.12                |                                  |                                |                                   |  |
| PS2                | Initial | 8:02 AM | 1.0                       | 8.70                | 0.40                             | 1.30                           | 32.73                             |  |
|                    | Final   | 8:03 AM |                           | 9.10                |                                  |                                |                                   |  |
| 1                  | Initial | 8:04 AM | 1.0                       | 8.70                | 0.38                             | 1.31                           | 30.88                             |  |
|                    | Final   | 8:05 AM |                           | 9.08                |                                  |                                |                                   |  |
| 2                  | Initial | 8:07 AM | 1.0                       | 8.70                | 0.38                             | 1.31                           | 30.88                             |  |
| _                  | Final   | 8:08 AM | 1.0                       | 9.08                | 0.50                             |                                |                                   |  |
| 3                  | Initial | 8:09 AM | 1.0                       | 8.70                | 0.37                             | 1.32                           | 29.97                             |  |
| Ŭ                  | Final   | 8:10 AM |                           | 9.07                |                                  |                                | 20.07                             |  |
| 4                  | Initial | 8:12 AM | 1.0                       | 8.70                | 0.36                             | 1.32                           | 29.06                             |  |
| 7                  | Final   | 8:13 AM |                           | 9.06                |                                  |                                |                                   |  |
| 5                  | Initial | 8:15 AM | 1.0                       | 8.70                | 0.35                             | 1.33                           | 28.16                             |  |
| 5                  | Final   | 8:16 AM |                           | 9.05                |                                  |                                |                                   |  |
| 6                  | Initial | 8:17 AM | 1.0                       | 8.70                | 0.33                             | 1.34                           | 26.37                             |  |
| 0                  | Final   | 8:18 AM | 1.0                       | 9.03                | 0.55                             |                                |                                   |  |
| 7                  | Initial | 8:20 AM | 1.0                       | 8.70                | 0.33                             | 1.34                           | 26.37                             |  |
| ľ                  | Final   | 8:21 AM | 1.0                       | 9.03                | 0.55                             | 1.54                           | 20.57                             |  |
| 8                  | Initial | 8:22 AM | 1.0                       | 8.70                | 0.33                             | 1.34                           | 26.37                             |  |
| 0                  | Final   | 8:23 AM | 1.0                       | 9.03                | 0.55                             | 1.34                           | 26.37                             |  |
| 9                  | Initial | 8:24 AM | 1.0                       | 8.70                | 0.34                             | 1.33                           | 27.26                             |  |
| 3                  | Final   | 8:25 AM | 1.0                       | 9.04                | 0.54                             | 1.55                           | 21.20                             |  |
| 10                 | Initial | 8:27 AM | 1.0                       | 8.70                | 0.22                             | 1.34                           | 25.40                             |  |
| 10                 | Final   | 8:28 AM | 1.0                       | 9.02                | 0.32                             |                                | 25.49                             |  |

Per County Standards, Infiltration Rate calculated as follows:

$$\boxed{Q = \frac{\Delta H(60r)}{\Delta t(r + 2H_{avg})}}$$

Where: Q = Infiltration Rate (in inches per hour)

 $\Delta H$  = Change in Height (Water Level) over the time interval

r = Test Hole (Borehole) Radius

 $\Delta t = Time Interval$ 

| Project Name     | Two Proposed Industrial Buildings |
|------------------|-----------------------------------|
| Project Location | Orange, CA                        |
| Project Number   | 20G199-3                          |
| Engineer         | Luis Arriaga                      |

Test Hole Radius Test Depth

Infiltration Test Hole

| 4<br>10.2 | (in) |
|-----------|------|
| 10.2      | (ft) |
|           |      |
| I-1       |      |

| Interval<br>Number |         | Time    | Time<br>Interval<br>(min) | Water<br>Depth (ft) | Change in<br>Water<br>Level (ft) | Average<br>Head<br>Height (ft) | Infiltration<br>Rate Q<br>(in/hr) |
|--------------------|---------|---------|---------------------------|---------------------|----------------------------------|--------------------------------|-----------------------------------|
| 11                 | Initial | 8:29 AM | 1.0                       | 8.70                | 0.31                             | 1.35                           | 24.61                             |
|                    | Final   | 8:30 AM |                           | 9.01                |                                  |                                |                                   |
| 12                 | Initial | 8:32 AM | 1.0                       | 8.70                | 0.31                             | 1.35                           | 24.61                             |
|                    | Final   | 8:33 AM |                           | 9.01                | 0.01                             |                                | 2                                 |
| 13                 | Initial | 8:34 AM | 1.0                       | 8.70                | 0.30                             | 1.35                           | 23.74                             |
| 10                 | Final   | 8:35 AM | 1.0                       | 9.00                | 0.00                             | 1.00                           | 20.74                             |
| 14                 | Initial | 8:37 AM | 1.0                       | 8.70                | 0.30                             | 1.35                           | 23.74                             |
| 14                 | Final   | 8:38 AM | 1.0                       | 9.00                | 0.50                             |                                | 20.14                             |
| 15                 | Initial | 8:39 AM | 1.0                       | 8.70                | 0.31                             | 1.35                           | 24.61                             |
| 10                 | Final   | 8:40 AM |                           | 9.01                |                                  |                                | 2                                 |
| 16                 | Initial | 8:42 AM | 1.0                       | 8.70                | 0.29                             | 1.36                           | 22.87                             |
| 10                 | Final   | 8:43 AM |                           | 8.99                |                                  |                                |                                   |
| 17                 | Initial | 8:45 AM | 1.0                       | 8.70                | 0.29                             | 1.36                           | 22.87                             |
|                    | Final   | 8:46 AM |                           | 8.99                | 0.20                             |                                |                                   |
| 18                 | Initial | 8:47 AM | 1.0                       | 8.70                | 0.28                             | 1.36                           | 22.01                             |
|                    | Final   | 8:48 AM |                           | 8.98                |                                  |                                |                                   |
| 19                 | Initial | 8:50 AM | 1.0                       | 8.70                | 0.27                             | 1.37                           | 21.15                             |
|                    | Final   | 8:51 AM |                           | 8.97                |                                  |                                | 21.10                             |
| 20                 | Initial | 8:53 AM | 1.0                       | 8.70                | 0.27                             | 1.37                           | 21.15                             |
|                    | Final   | 8:54 AM |                           | 8.97                |                                  |                                |                                   |
| 21                 | Initial | 8:55 AM | 1.0                       | 8.70                | 0.27                             | 1.37                           | 21.15                             |
|                    | Final   | 8:56 AM |                           | 8.97                |                                  |                                |                                   |
| 22                 | Initial | 8:58 AM | 1.0                       | 8.70                | 0.27                             | 1.37                           | 21.15                             |
|                    | Final   | 8:59 AM |                           | 8.97                | <u></u>                          |                                | 2                                 |

Per County Standards, Infiltration Rate calculated as follows:

$$Q = \frac{\Delta H(60r)}{\Delta t(r+2H_{avg})}$$

Where: Q = Infiltration Rate (in inches per hour)

 $\Delta H$  = Change in Height (Water Level) over the time interval

r = Test Hole (Borehole) Radius

 $\Delta t = Time Interval$ 

| Project Name     | Two Proposed Industrial Buildings |
|------------------|-----------------------------------|
| Project Location | Orange, CA                        |
| Project Number   | 20G199-3                          |
| Engineer         | Luis Arriaga                      |
|                  |                                   |

Test Hole Radius Test Depth

Infiltration Test Hole

4 (in) 10.2 (ft)

| Interval<br>Number |         | Time    | Time<br>Interval<br>(min) | Water<br>Depth (ft) | Change in<br>Water<br>Level (ft) | Average<br>Head<br>Height (ft) | Infiltration<br>Rate Q<br>(in/hr) |  |
|--------------------|---------|---------|---------------------------|---------------------|----------------------------------|--------------------------------|-----------------------------------|--|
| 23                 | Initial | 9:01 AM | 1.0                       | 8.70                | 0.27                             | 1.37                           | 21.15                             |  |
| 20                 | Final   | 9:02 AM | 1.0                       | 8.97                | 0.27                             | 1.07                           | 21.10                             |  |
| 24                 | Initial | 9:03 AM | 1.0                       | 8.70                | 0.27                             | 1.37                           | 21.15                             |  |
| 24                 | Final   | 9:04 AM | 1.0                       | 8.97                | 0.27                             | 1.57                           | 21.15                             |  |
| 25                 | Initial | 9:05 AM | 1.0                       | 8.70                | 0.27                             | 1.37                           | 21.15                             |  |
| 25                 | Final   | 9:06 AM | 1.0                       | 8.97                | 0.27                             |                                | 21.15                             |  |
| 26                 | Initial | 9:08 AM | 1.0                       | 8.70                | 0.27                             | 1.37                           | 21.15                             |  |
| 20                 | Final   | 9:09 AM | 1.0                       | 8.97                | 0.27                             |                                | 21.15                             |  |
| 27                 | Initial | 9:10 AM | 1.0                       | 8.70                | 0.27                             | 1.37                           | 21.15                             |  |
| 21                 | Final   | 9:11 AM | 1.0                       | 8.97                | 0.27                             | 1.57                           | 21.15                             |  |
| 28                 | Initial | 9:13 AM | 1.0                       | 8.70                | 0.28                             | 1.36                           | 22.01                             |  |
| 20                 | Final   | 9:14 AM | 1.0                       | 8.98                | 0.20                             | 1.50                           | 22.01                             |  |
| 29                 | Initial | 9:15 AM | 1.0                       | 8.70                | 0.27                             | 1.37                           | 21.15                             |  |
| 23                 | Final   | 9:16 AM | 1.0                       | 8.97                | 0.27                             | 1.57                           | 21.10                             |  |
| 30                 | Initial | 9:18 AM | 1.0                       | 8.70                | 0.27                             | 4.07                           | 04.45                             |  |
| - 30               | Final   | 9:19 AM | 1.0                       | 8.97                | 0.27                             | 1.37                           | 21.15                             |  |

Per County Standards, Infiltration Rate calculated as follows:

$$Q = \frac{\Delta H(60r)}{\Delta t(r+2H_{avg})}$$

Where: Q = Infiltration Rate (in inches per hour)

 $\Delta H$  = Change in Height (Water Level) over the time interval

r = Test Hole (Borehole) Radius

 $\Delta t = Time Interval$ 

| Project Name     | Two Proposed Industrial Buildings |
|------------------|-----------------------------------|
| Project Location | Orange, CA                        |
| Project Number   | 20G199-3                          |
| Engineer         | Luis Arriaga                      |

Test Hole Radius Test Depth

Infiltration Test Hole

| 4<br>10.1 | (in) |
|-----------|------|
| 10.1      | (ft) |
|           |      |
| I-2       |      |

Change in Water Level (ft) Infiltration Rate Q (in/hr) Average Head Height (ft) Water Depth (ft) Interval Number Time Interval (min) Time 7.49 Initial 9:25 AM PS1 30.0 0.71 2.26 1.17 Final 9:55 AM 8.20 9:55 AM 7.49 Initial PS2 30.0 0.71 1.17 2.26 10:25 AM 8.20 Final Initial 10:26 AM 7.49 30.0 1 0.71 2.26 1.17 10:56 AM 8.20 Final Initial 10:57 AM 7.49 2 30.0 2.25 0.73 1.21 Final 11:27 AM 8.22 Initial 11:28 AM 7.49 3 30.0 0.74 2.24 1.23 11:58 AM 8.23 Final Initial 12:00 PM 7.49 4 30.0 0.72 2.25 1.19 12:30 PM 8.21 Final 12:31 PM 7.49 Initial 5 30.0 0.71 2.26 1.17 1:01 PM 8.20 Final Initial 1:02 PM 7.49 6 30.0 0.70 2.26 1.15 Final 1:32 PM 8.19 Initial 1:33 PM 7.49 7 30.0 0.66 2.28 1.08 Final 2:03 PM 8.15 Initial 2:04 PM 7.49 8 30.0 0.66 1.08 2.28 Final 2:34 PM 8.15 Initial 2:37 PM 7.49 9 30.0 0.65 2.29 1.06 Final 3:07 PM 8.14 Initial 3:08 PM 7.49 10 30.0 0.64 2.29 1.04 3:38 PM 8.13 Final 3:40 PM Initial 7.49 2.29 11 30.0 0.64 1.04 Final 4:10 PM 8.13 4:11 PM 7.49 Initial 12 30.0 2.29 0.64 1.04 4:41 PM 8.13 Final

Per County Standards, Infiltration Rate calculated as follows:

$$Q = \frac{\Delta H(60r)}{\Delta t(r+2H_{avg})}$$

Where: Q = Infiltration Rate (in inches per hour)

- $\Delta H$  = Change in Height (Water Level) over the time interval
  - r = Test Hole (Borehole) Radius

∆t = Time Interval

H<sub>avg</sub> = Average Head Height over the time interval

| Project Name     | Two Proposed Industrial Buildings |
|------------------|-----------------------------------|
| Project Location | Orange, CA                        |
| Project Number   | 20G199-3                          |
| Engineer         | Luis Arriaga                      |

Test Hole Radius Test Depth

Infiltration Test Hole

4 (in) 12.2 (ft) I-3

Change in Water Level (ft) Infiltration Rate Q (in/hr) Average Head Height (ft) Water Depth (ft) Interval Number Time Interval (min) Time 10.20 Initial 9:30 AM PS1 30.0 0.21 1.90 0.41 Final 10:00 AM 10.41 10:01 AM 10.20 Initial PS2 30.0 0.45 0.23 1.89 10:31 AM 10.43 Final Initial 10:33 AM 10.20 30.0 1 0.24 1.88 0.47 11:03 AM 10.44 Final Initial 11:04 AM 10.20 2 30.0 0.49 0.25 1.88 Final 11:34 AM 10.45 Initial 11:34 AM 10.20 3 30.0 0.26 1.87 0.51 12:04 PM 10.46 Final Initial 12:04 PM 10.20 4 30.0 0.25 1.88 0.49 12:34 PM 10.45 Final 12:35 PM 10.20 Initial 5 30.0 0.25 1.88 0.49 1:05 PM 10.45 Final Initial 1:06 PM 10.20 6 30.0 0.26 1.87 0.51 Final 1:36 PM 10.46 Initial 1:37 PM 10.20 7 30.0 0.25 1.88 0.49 10.45 Final 2:07 PM Initial 2:07 PM 10.20 8 30.0 0.49 0.25 1.88 Final 2:37 PM 10.45 Initial 2:38 PM 10.20 9 30.0 0.25 1.88 0.49 Final 3:08 PM 10.45 Initial 3:12 PM 10.20 10 30.0 0.25 1.88 0.49 3:42 PM 10.45 Final 3:43 PM Initial 10.20 11 30.0 0.26 1.87 0.50 Final 4:13 PM 10.46 4:13 PM 10.20 Initial 12 30.0 0.49 0.25 1.88 4:43 PM 10.45 Final

Per County Standards, Infiltration Rate calculated as follows:

$$Q = \frac{\Delta H(60r)}{\Delta t(r+2H_{avg})}$$

Where: Q = Infiltration Rate (in inches per hour)

- $\Delta H$  = Change in Height (Water Level) over the time interval
  - r = Test Hole (Borehole) Radius

∆t = Time Interval

H<sub>avg</sub> = Average Head Height over the time interval

| Project Name     | Two Proposed Industrial Buildings |
|------------------|-----------------------------------|
| Project Location | Orange, CA                        |
| Project Number   | 20G199-3                          |
| Engineer         | Luis Arriaga                      |
|                  |                                   |

Test Hole Radius Test Depth

Infiltration Test Hole

4 (in) 12.0 (ft) I-4

| Interval<br>Number |         | Time    | Time<br>Interval<br>(min) | Water<br>Depth (ft) | Change in<br>Water<br>Level (ft) | Average<br>Head<br>Height (ft) | Infiltration<br>Rate Q<br>(in/hr) |
|--------------------|---------|---------|---------------------------|---------------------|----------------------------------|--------------------------------|-----------------------------------|
| PS1                | Initial | 7:30 AM | 5.0                       | 9.90                | 0.40                             | 1.85                           | 4.76                              |
|                    | Final   | 7:35 AM |                           | 10.30               |                                  |                                |                                   |
| PS2                | Initial | 7:40 AM | 5.0                       | 9.90                | 0.42                             | 1.84                           | 5.02                              |
| 1.02               | Final   | 7:45 AM | 5.0                       | 10.32               |                                  |                                |                                   |
| 1                  | Initial | 7:47 AM | 10.0                      | 9.90                | 0.70                             | 1.70                           | 4.50                              |
| 1                  | Final   | 7:57 AM | 10.0                      | 10.60               |                                  |                                |                                   |
| 2                  | Initial | 7:58 AM | 10.0                      | 9.90                | 0.69                             | 1.71                           | 4.42                              |
| 2                  | Final   | 8:08 AM | 10.0                      | 10.59               |                                  |                                |                                   |
| 3                  | Initial | 8:09 AM | 10.0                      | 9.90                | 0.70                             | 1.70                           | 4.50                              |
| 5                  | Final   | 8:19 AM | 10.0                      | 10.60               |                                  |                                |                                   |
| 4                  | Initial | 8:20 AM | 10.0                      | 9.90                | 0.70                             | 1.70                           | 4.50                              |
| 4                  | Final   | 8:30 AM | 10.0                      | 10.60               |                                  |                                |                                   |
| 5                  | Initial | 8:31 AM | 10.0                      | 9.90                | 0.68                             | 1.71                           | 4.35                              |
| 5                  | Final   | 8:41 AM |                           | 10.58               |                                  |                                |                                   |
| 6                  | Initial | 8:42 AM | 10.0                      | 9.90                | 0.69                             | 1.71                           | 4.42                              |
|                    | Final   | 8:52 AM |                           | 10.59               |                                  |                                |                                   |

Per County Standards, Infiltration Rate calculated as follows:

$$Q = \frac{\Delta H(60r)}{\Delta t(r+2H_{avg})}$$

Where: Q = Infiltration Rate (in inches per hour)

 $\Delta H$  = Change in Height (Water Level) over the time interval

r = Test Hole (Borehole) Radius

 $\Delta t = Time Interval$ 

| Project Name     | Two Proposed Industrial Buildings |
|------------------|-----------------------------------|
| Project Location | Orange, CA                        |
| Project Number   | 20G199-3                          |
| Engineer         | Luis Arriaga                      |

Test Hole Radius Test Depth

Infiltration Test Hole

4 (in) 12.1 (ft) I-5

Change in Water Level (ft) Infiltration Rate Q (in/hr) Average Head Height (ft) Water Depth (ft) Interval Number Time Interval (min) Time Initial 8:55 AM 10.00 PS1 30.0 0.13 2.04 0.24 Final 9:25 AM 10.13 9:26 AM 10.00 Initial PS2 30.0 0.14 2.03 0.25 9:56 AM 10.14 Final Initial 9:57 AM 10.00 30.0 2.03 0.15 0.27 1 10:27 AM 10.15 Final Initial 10:29 AM 10.00 2 30.0 0.27 0.15 2.03 Final 10:59 AM 10.15 Initial 11:00 AM 10.00 3 30.0 0.15 2.03 0.27 11:30 AM 10.15 Final Initial 11:31 AM 10.00 4 30.0 0.16 2.02 0.29 12:01 PM 10.16 Final 12:02 PM 10.00 Initial 5 30.0 0.15 2.03 0.27 12:32 PM 10.15 Final Initial 12:35 PM 10.00 6 30.0 0.15 2.03 0.27 Final 1:05 PM 10.15 Initial 1:06 PM 10.00 7 30.0 0.15 2.03 0.27 Final 1:36 PM 10.15 Initial 1:37 PM 10.00 8 30.0 2.02 0.29 0.16 Final 2:07 PM 10.16 Initial 2:08 PM 10.00 9 30.0 0.16 2.02 0.29 Final 2:38 PM 10.16 Initial 2:40 PM 10.00 10 30.0 0.16 2.02 0.29 3:10 PM 10.16 Final 3:10 PM 10.00 Initial 2.02 11 30.0 0.16 0.29 Final 3:40 PM 10.16 3:41 PM 10.00 Initial 12 30.0 2.02 0.16 0.29 4:11 PM 10.16 Final

Per County Standards, Infiltration Rate calculated as follows:

$$Q = \frac{\Delta H(60r)}{\Delta t(r+2H_{avg})}$$

Where: Q = Infiltration Rate (in inches per hour)

- $\Delta H$  = Change in Height (Water Level) over the time interval
  - r = Test Hole (Borehole) Radius

∆t = Time Interval

| Project Name     | Two Proposed Industrial Buildings |
|------------------|-----------------------------------|
| Project Location | Orange, CA                        |
| Project Number   | 20G199-3                          |
| Engineer         | Luis Arriaga                      |
|                  |                                   |

Test Hole Radius Test Depth

Infiltration Test Hole

4 (in) 12.2 (ft) I-6

| Interval<br>Number |         | Time     | Time<br>Interval<br>(min) | Water<br>Depth (ft) | Change in<br>Water<br>Level (ft) | Average<br>Head<br>Height (ft) | Infiltration<br>Rate Q<br>(in/hr) |
|--------------------|---------|----------|---------------------------|---------------------|----------------------------------|--------------------------------|-----------------------------------|
| PS1                | Initial | 9:01 AM  | 1.0                       | 8.70                | 0.27                             | 3.37                           | 9.17                              |
|                    | Final   | 9:02 AM  |                           | 8.97                | 0.21                             |                                |                                   |
| PS2                | Initial | 9:03 AM  | 1.0                       | 8.70                | 0.27                             | 3.37                           | 9.17                              |
| 1 02               | Final   | 9:04 AM  | 1.0                       | 8.97                |                                  |                                |                                   |
| 1                  | Initial | 10:02 AM | 10.0                      | 10.10               | 0.55                             | 1.83                           | 3.31                              |
| I                  | Final   | 10:12 AM |                           | 10.65               |                                  |                                |                                   |
| 2                  | Initial | 10:13 AM | 10.0                      | 10.10               | 0.59                             | 1.81                           | 3.59                              |
| 2                  | Final   | 10:23 AM | 10.0                      | 10.69               |                                  |                                |                                   |
| 3                  | Initial | 10:24 AM | 10.0                      | 10.10               | 0.60                             | 1.80                           | 3.66                              |
| 5                  | Final   | 10:34 AM | 10.0                      | 10.70               |                                  |                                |                                   |
| 4                  | Initial | 10:35 AM | 10.0                      | 10.10               | 0.65                             | 1.78                           | 4.02                              |
| 7                  | Final   | 10:45 AM | 10.0                      | 10.75               |                                  |                                |                                   |
| 5                  | Initial | 10:46 AM | 10.0                      | 10.10               | 0.68                             | 1.76                           | 4.24                              |
| 5                  | Final   | 10:56 AM |                           | 10.78               |                                  |                                |                                   |
| 6                  | Initial | 10:58 AM | 10.0                      | 10.10               | 0.69                             | 1.76                           | 4.31                              |
|                    | Final   | 11:08 AM |                           | 10.79               |                                  |                                |                                   |

Per County Standards, Infiltration Rate calculated as follows:

$$Q = \frac{\Delta H(60r)}{\Delta t(r+2H_{avg})}$$

Where: Q = Infiltration Rate (in inches per hour)

 $\Delta H$  = Change in Height (Water Level) over the time interval

r = Test Hole (Borehole) Radius

 $\Delta t = Time Interval$ 

| Project Name     | Two Proposed Industrial Buildings |
|------------------|-----------------------------------|
| Project Location | Orange, CA                        |
| Project Number   | 20G199-3                          |
| Engineer         | Ryan Bremer                       |
|                  |                                   |

Test Hole Radius Test Depth

Infiltration Test Hole

4 (in) 10.0 (ft) I-7

Change in Water Level (ft) Average Head Height (ft) Infiltration Rate Q (in/hr) Water Depth (ft) Interval Number Time Interval (min) Time 7:00 AM 6.00 Initial PS1 9.0 4.00 2.00 24.62 Final 7:09 AM 10.00 Initial 7:10 AM 6.00 PS2 9.0 4.00 2.00 24.62 10.00 Final 7:19 AM Initial 7:20 AM 6.00 1 10.0 4.00 2.00 22.15 7:30 AM 10.00 Final 7:31 AM 6.00 Initial 2 10.0 2.00 22.15 4.00 7:41 AM 10.00 Final Initial 7:42 AM 6.00 3 10.0 2.00 22.15 4.00 7:52 AM Final 10.00 Initial 7:53 AM 6.00 4 10.0 4.00 2.00 22.15 Final 8:03 AM 10.00 Initial 8:04 AM 6.00 5 10.0 4.00 2.00 22.15 10.00 Final 8:14 AM 6.00 Initial 8:15 AM 6 10.0 4.00 2.00 22.15 8:25 AM 10.00 Final

Per County Standards, Infiltration Rate calculated as follows:

$$Q = \frac{\Delta H(60r)}{\Delta t(r+2H_{avg})}$$

Where: Q = Infiltration Rate (in inches per hour)

 $\Delta H$  = Change in Height (Water Level) over the time interval

r = Test Hole (Borehole) Radius

 $\Delta t = Time Interval$ 

H<sub>avg</sub> = Average Head Height over the time interval

## INFILTRATION CALCULATIONS

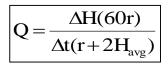
| Project Name     | Two Proposed Industrial Buildings |
|------------------|-----------------------------------|
| Project Location | Orange, CA                        |
| Project Number   | 20G199-3                          |
| Engineer         | Ryan Bremer                       |
|                  |                                   |

Test Hole Radius Test Depth

Infiltration Test Hole

| Interval<br>Number |         | Time     | Time<br>Interval<br>(min) | Water<br>Depth (ft) | Change in<br>Water<br>Level (ft) | Average<br>Head<br>Height (ft) | Infiltration<br>Rate Q<br>(in/hr) |
|--------------------|---------|----------|---------------------------|---------------------|----------------------------------|--------------------------------|-----------------------------------|
| PS1                | Initial | 8:59 AM  | 25.0                      | 9.19                | 0.43                             | 2.10                           | 0.91                              |
| 1.51               | Final   | 9:24 AM  | 25.0                      | 9.62                | 0.45                             | 2.10                           | 0.91                              |
| PS2                | Initial | 9:25 AM  | 25.0                      | 9.39                | 0.39                             | 1.92                           | 0.90                              |
| 1.52               | Final   | 9:50 AM  | 25.0                      | 9.78                | 0.55                             | 1.52                           | 0.30                              |
| 1                  | Initial | 9:50 AM  | 30.0                      | 9.19                | 0.49                             | 2.07                           | 0.88                              |
| 1                  | Final   | 10:20 AM | 30.0                      | 9.68                | 0.49                             | 2.07                           | 0.00                              |
| 2                  | Initial | 10:20 AM | 30.0                      | 9.45                | 0.42                             | 1.84                           | 0.84                              |
| 2                  | Final   | 10:50 AM | 30.0                      | 9.87                | 0.42                             | 1.04                           | 0.04                              |
| 3                  | Initial | 10:50 AM | 30.0                      | 9.56                | 0.39                             | 1.75                           | 0.82                              |
| 5                  | Final   | 11:20 AM | 30.0                      | 9.95                | 0.59                             | 1.75                           | 0.02                              |
| 4                  | Initial | 11:20 AM | 30.0                      | 9.57                | 0.39                             | 1.74                           | 0.82                              |
| 4                  | Final   | 11:50 AM | 50.0                      | 9.96                | 0.55                             | 1.74                           | 0.02                              |
| 5                  | Initial | 11:50 AM | 30.0                      | 9.56                | 0.39                             | 1.75                           | 0.82                              |
| 5                  | Final   | 12:20 PM | 30.0                      | 9.95                | 0.39                             | 1.75                           | 0.02                              |
| 6                  | Initial | 12:20 PM | 30.0                      | 9.55                | 0.39                             | 1.76                           | 0.81                              |
| 0                  | Final   | 12:50 PM | 30.0                      | 9.94                | 0.39                             | 1.70                           | 0.81                              |

Per County Standards, Infiltration Rate calculated as follows:



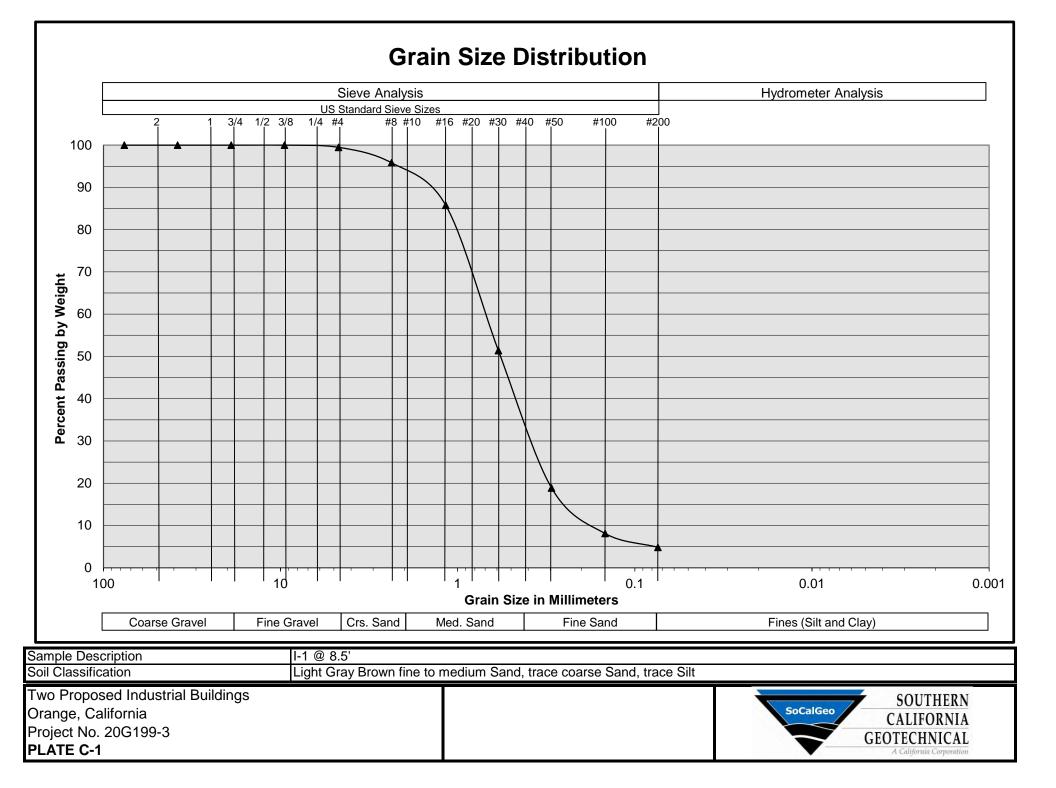
Where: Q = Infiltration Rate (in inches per hour)

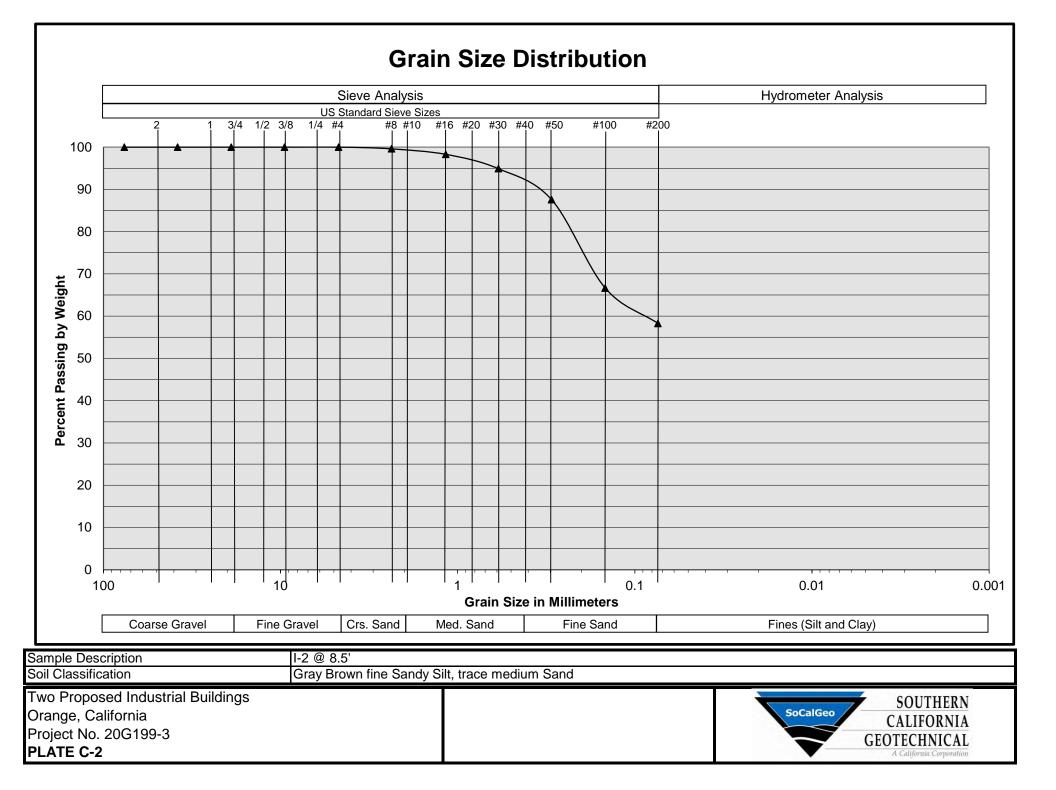
 $\Delta H$  = Change in Height (Water Level) over the time interval

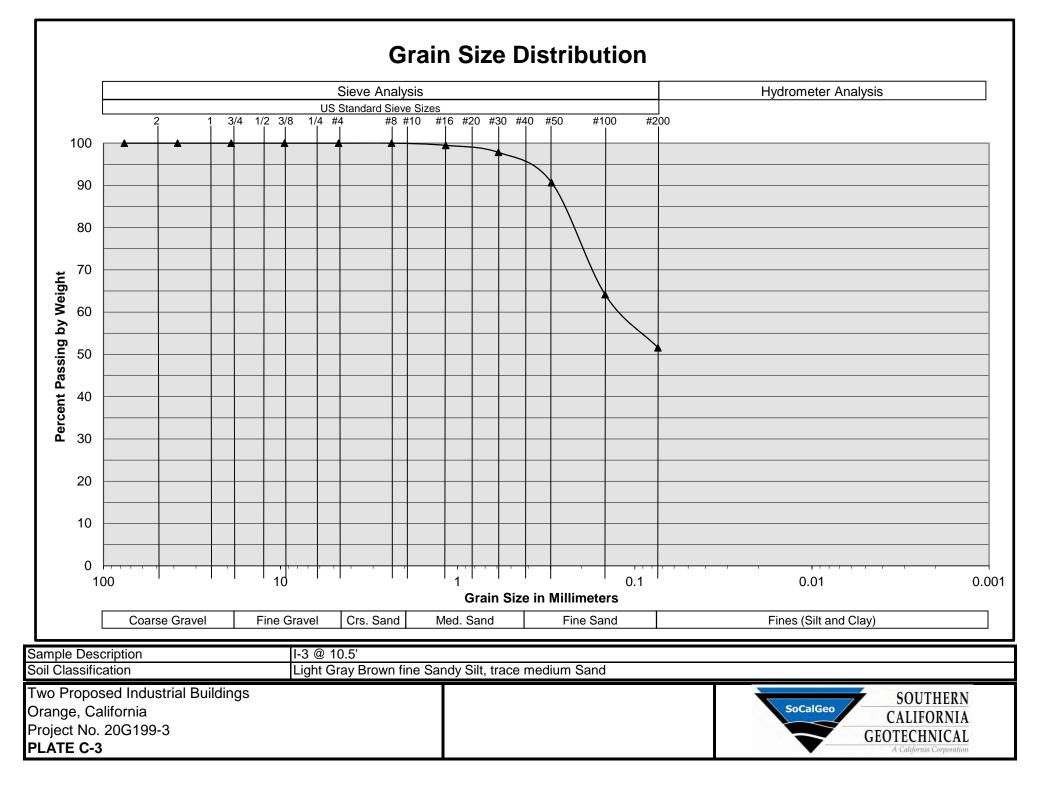
r = Test Hole (Borehole) Radius

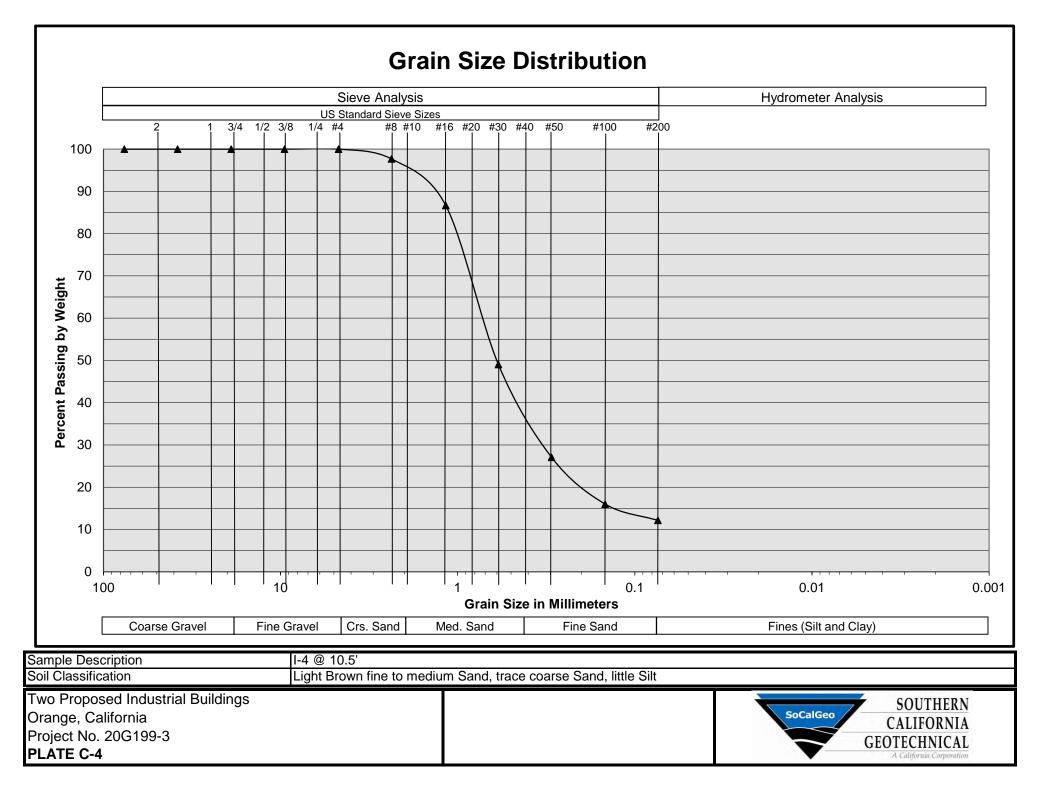
 $\Delta t = Time Interval$ 

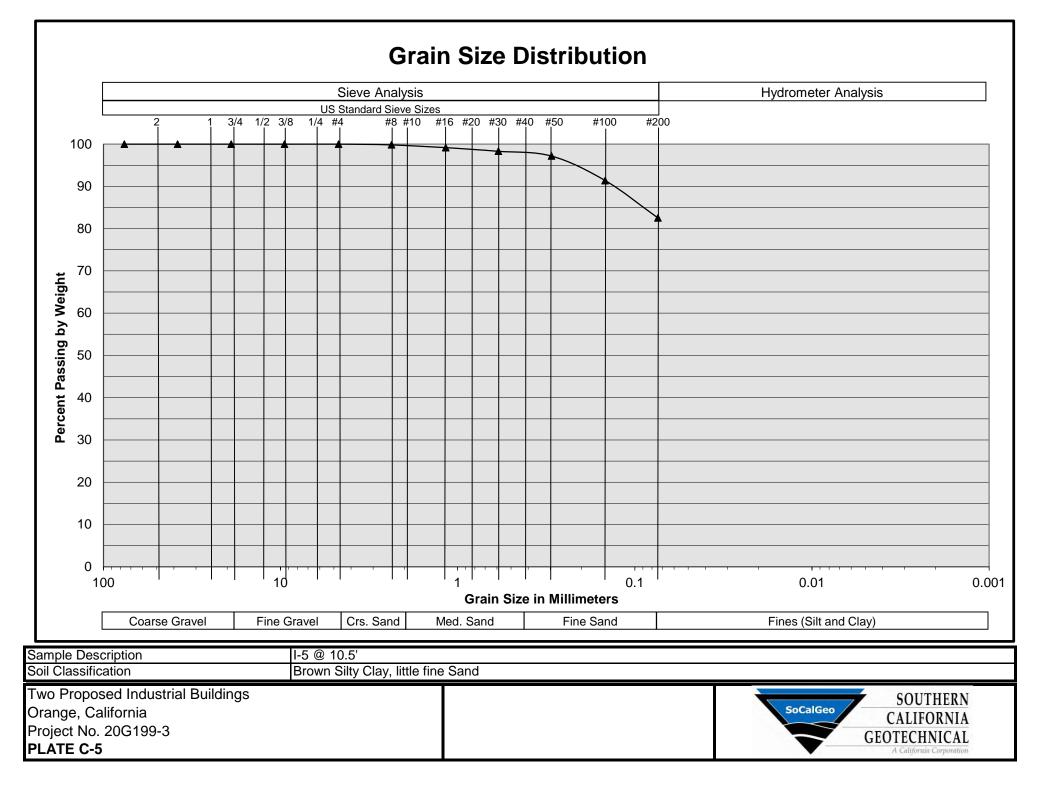
 $\mathrm{H}_{\mathrm{avg}}$  = Average Head Height over the time interval



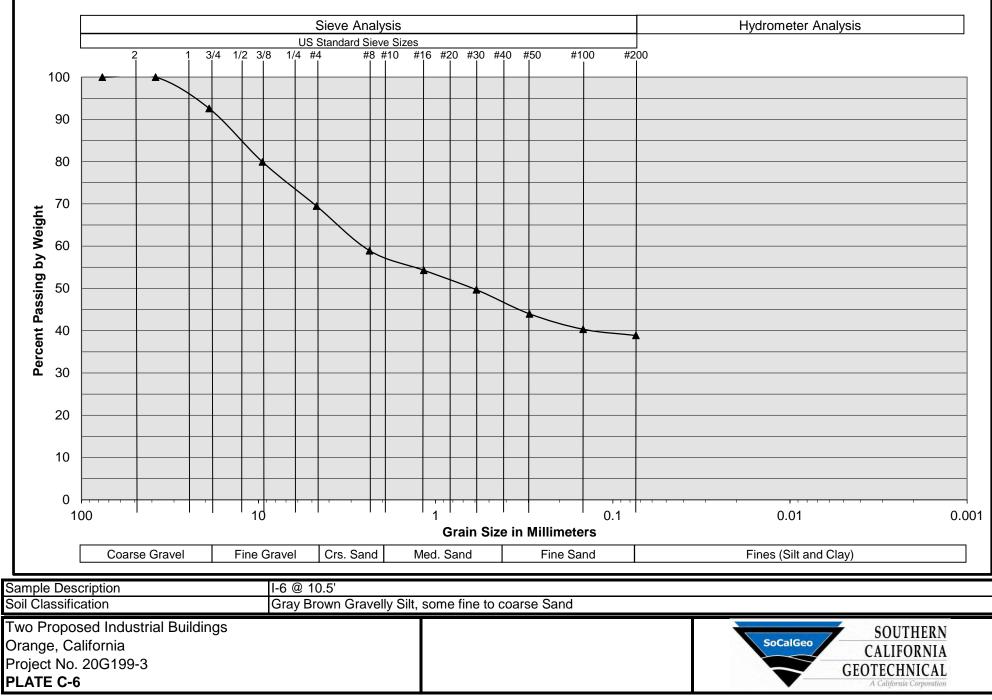




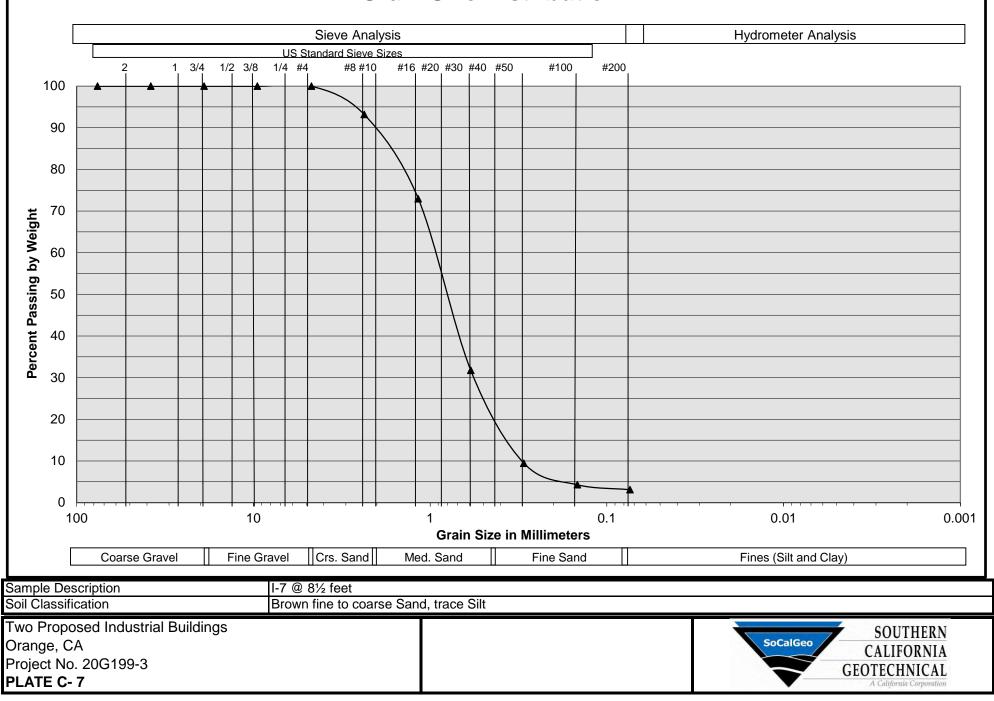


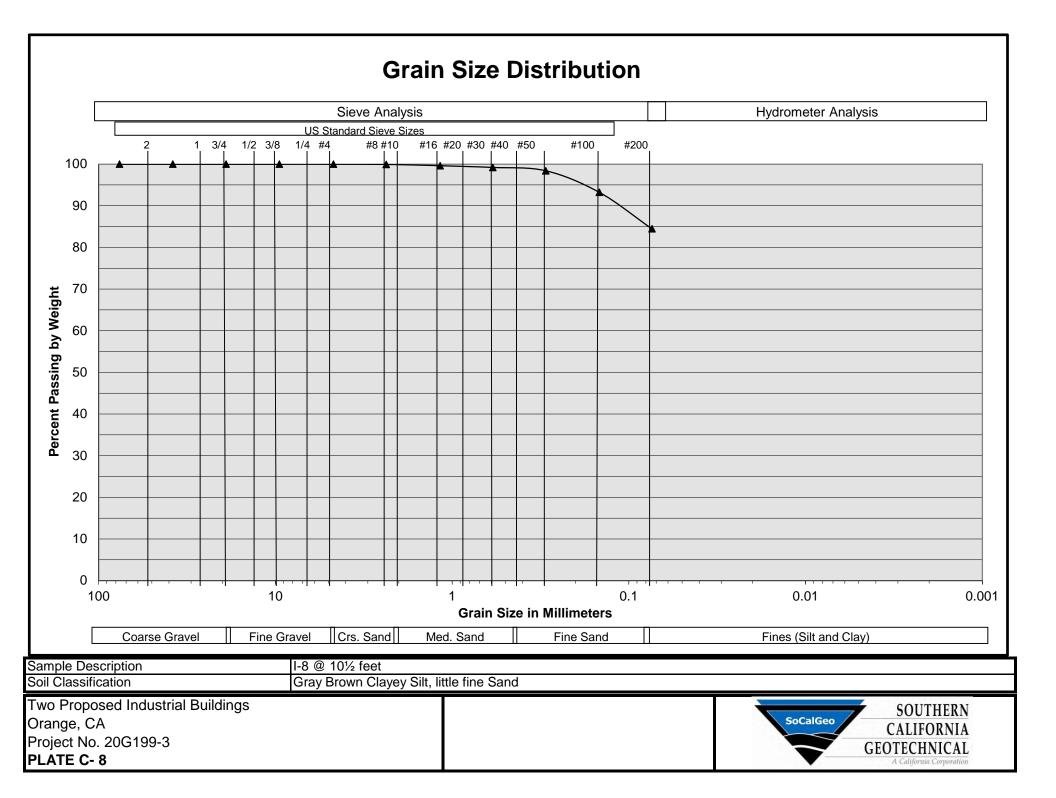


## **Grain Size Distribution**

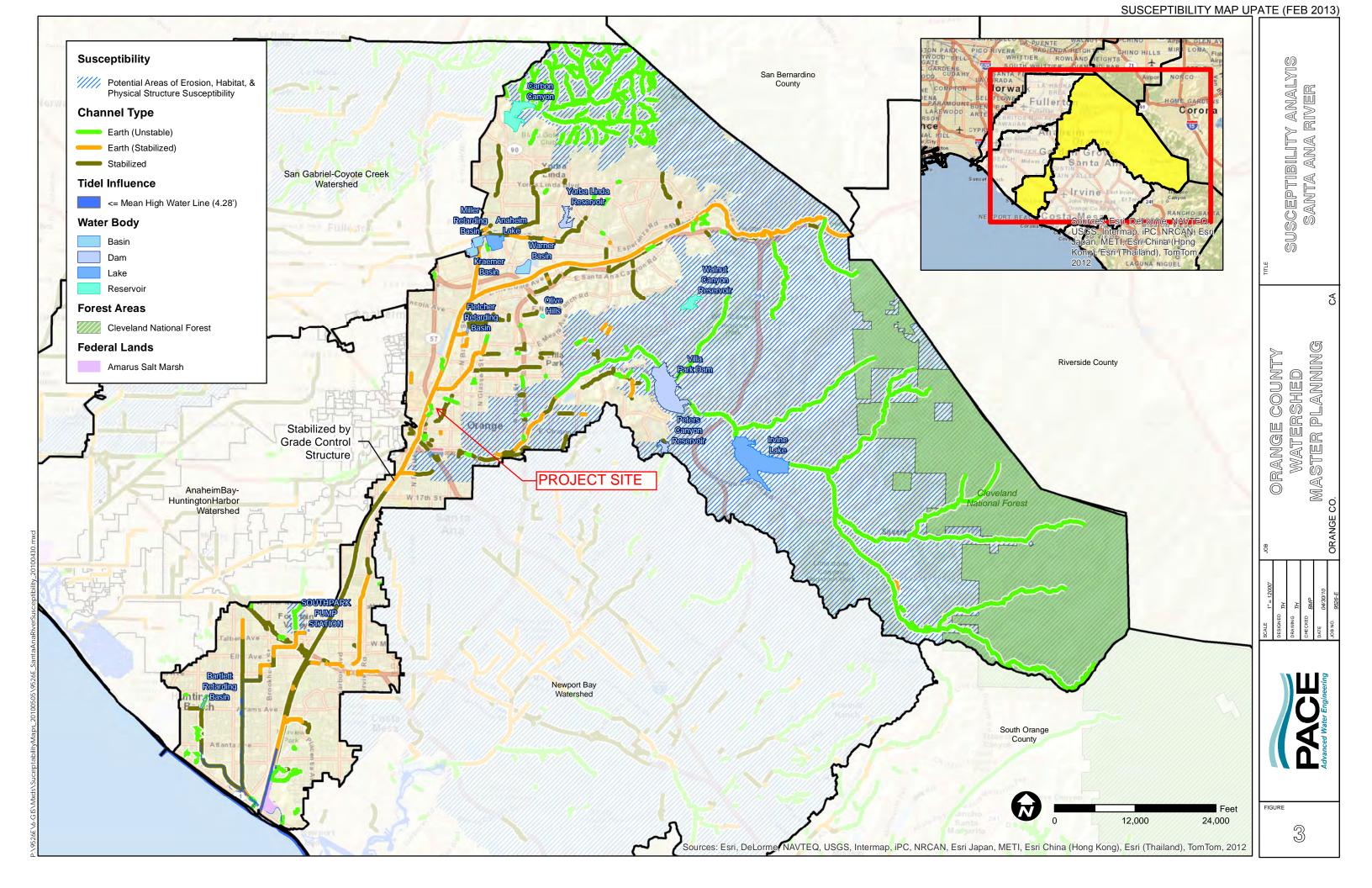


## **Grain Size Distribution**





Appendix F: Hydrology Information



| ***************************************                                                                                                                                            |
|------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|
| NON-HOMOGENEOUS WATERSHED AREA-AVERAGED LOSS RATE (Fm)                                                                                                                             |
| AND LOW LOSS FRACTION ESTIMATIONS                                                                                                                                                  |
|                                                                                                                                                                                    |
| (C) Copyright 1989-2016 Advanced Engineering Software (aes)                                                                                                                        |
| Ver. 23.0 Release Date: 07/01/2016 License ID 1435                                                                                                                                 |
|                                                                                                                                                                                    |
| Analysis prepared by:                                                                                                                                                              |
|                                                                                                                                                                                    |
| THIENES ENGINEERING, INC.                                                                                                                                                          |
| 14349 FIRESTONE BLVD                                                                                                                                                               |
| LA MIRADA, CA 90638                                                                                                                                                                |
| 714-521-4811                                                                                                                                                                       |
|                                                                                                                                                                                    |
| ***************************************                                                                                                                                            |
|                                                                                                                                                                                    |
|                                                                                                                                                                                    |
| Problem Descriptions:                                                                                                                                                              |
| TELIOB 3910                                                                                                                                                                        |
| 2-YEAR LOSS RATES                                                                                                                                                                  |
| EXISTING CONDITION                                                                                                                                                                 |
|                                                                                                                                                                                    |
| *** NON-HOMOGENEOUS WATERSHED AREA-AVERAGED LOSS RATE (Fm)                                                                                                                         |
| AND LOW LOSS FRACTION ESTIMATIONS FOR AMC I:                                                                                                                                       |
| AND HOW HOSD FRACTION ESTIMATIONS FOR ANC I.                                                                                                                                       |
| TOTAL 24-HOUR DURATION RAINFALL DEPTH = 2.05 (inches)                                                                                                                              |
| IOTAL 24-ROOK DORATION RAINFALL DEPTH - 2.05 (Inches)                                                                                                                              |
| SOIL-COVER AREA PERCENT OF SCS CURVE LOSS RATE                                                                                                                                     |
|                                                                                                                                                                                    |
| TYPE         (Acres)         PERVIOUS AREA         NUMBER         Fp(in./hr.)         YIELD           1         12.70         10.00         32.(AMC II)         0.400         0.80 |
| 1 12.70 10.00 32.(AMC 11) 0.400 0.80                                                                                                                                               |
| TOTAL AREA (Acres) = 12.70                                                                                                                                                         |
| -                                                                                                                                                                                  |
| AREA-AVERAGED LOSS RATE, Fm (in./hr.) = 0.040                                                                                                                                      |
| _                                                                                                                                                                                  |
| AREA-AVERAGED LOW LOSS FRACTION, $Y = 0.199$                                                                                                                                       |
|                                                                                                                                                                                    |

SMALL AREA UNIT HYDROGRAPH MODEL (C) Copyright 1989-2016 Advanced Engineering Software (aes) Ver. 23.0 Release Date: 07/01/2016 License ID 1435 Analysis prepared by: THIENES ENGINEERING, INC. 14349 FIRESTONE BLVD LA MIRADA, CA 90638 714-521-4811 \_\_\_\_\_ Problem Descriptions: TEI JOB 3910 2-YEAR HYDROGRAPH EXISTING CONDITION TO CONCRETE CHANNEL \_\_\_\_\_ RATIONAL METHOD CALIBRATION COEFFICIENT = 0.90 TOTAL CATCHMENT AREA(ACRES) = 5.00 SOIL-LOSS RATE, Fm,(INCH/HR) = 0.040 LOW LOSS FRACTION = 0.199 TIME OF CONCENTRATION(MIN.) = 9.00 SMALL AREA PEAK Q COMPUTED USING PEAK FLOW RATE FORMULA ORANGE COUNTY "VALLEY" RAINFALL VALUES ARE USED RETURN FREQUENCY(YEARS) = 2 5-MINUTE POINT RAINFALL VALUE(INCHES) = 0.19 30-MINUTE POINT RAINFALL VALUE(INCHES) = 0.40 1-HOUR POINT RAINFALL VALUE(INCHES) = 0.53 POINT RAINFALL VALUE(INCHES) = 0.89 3-HOUR POINT RAINFALL VALUE(INCHES) = 1.22 6-HOUR 24-HOUR POINT RAINFALL VALUE(INCHES) = 2.05 \_\_\_\_\_ TOTAL CATCHMENT RUNOFF VOLUME(ACRE-FEET) = 0.64 TOTAL CATCHMENT RUNOFF VOLUME(ACRE-FEET) = 0.64 TOTAL CATCHMENT SOIL-LOSS VOLUME(ACRE-FEET) = 0.22 \*\*\*\*\*\* TIME VOLUME Q 0. 2.5 5.0 7.5 10.0 (HOURS) (AF) (CFS) .\_\_\_\_\_ 0.0000 0.0007 0.0022 0.0036 0.0051 0.0065 0.0080 0.0095 0.00 Q 0.10 . . . . 0.25 0.12 Q . . 0.40 0.12 Q . 0.12 0.12 0.12 0.12 0.12 0.12 0.55 0.70 0 . . Q . . . . 0.85 Q . . . . 1.00 Q . . . 1.15 Q 0.0095 0.0110 0.0125 0.0140 0.0155 0.0171 0.0186 0.0202 1.30 0.12 0 . . . . 1.45 0.12 0 . . 1.60 õ 0.12 . . 1.75 0.12 Q . . . 1.90 0.12 Q . . 2.05 0.13 0 0.13 2.20 0 . . 0.0217 0.0233 0.0249 2.35 0.13 0 . . . 2.50 0.13 õ . 2.65 0.13 Q 0.0265 0.0281 2.80 0.13 Q 2.95 0.13 0 . . 0.0297 3.10 0.13 0 . . 3.25 0.13 Q . . . 3.40 0.0330 0.13 Q . . 3.55 3.70 0.0346 0.13 Q 0.13 0 0.0380 0.0397 3.85 0.14 0 . . . . 4.00 0.14 0 . . . . 0.0414 4.15 0.14 Q . . . 4.30 0.0431 0.14 Q . . . 0.0448 4 45 0.14 0 0.0466 4.60 0.14 0 . . 0.14 4.75 0 . . . . 0.14 Q 0.14 Q 0.15 Q 0.15 Q 0.15 Q 0.0501 0.0519 0.0537 4.90 . . . 5.05 . 5.20 . 0.0555 5.35

1

| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | 5.50<br>5.65<br>5.95<br>6.10<br>6.25<br>6.40<br>6.55<br>6.70<br>6.85<br>7.00<br>7.15<br>7.30<br>7.45<br>7.60                        | 0.0574<br>0.0592<br>0.0611<br>0.0630<br>0.0649<br>0.0668<br>0.0707<br>0.0727<br>0.0727<br>0.0747<br>0.0767<br>0.0767<br>0.0788<br>0.0808<br>0.0829<br>0.0850 | $\begin{array}{cccccccccccccccccccccccccccccccccccc$                                                                                     |     | ·<br>·<br>·<br>·<br>·                                                                       |     |
|------------------------------------------------------|-------------------------------------------------------------------------------------------------------------------------------------|--------------------------------------------------------------------------------------------------------------------------------------------------------------|------------------------------------------------------------------------------------------------------------------------------------------|-----|---------------------------------------------------------------------------------------------|-----|
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | 7.90<br>8.05<br>8.20<br>8.50<br>8.65<br>8.80<br>8.95<br>9.10<br>9.25<br>9.40<br>9.55<br>9.70<br>9.85                                | 0.0893<br>0.0915<br>0.0937<br>0.0959<br>0.0982<br>0.1005<br>0.1028<br>0.1051<br>0.1075<br>0.1099<br>0.1123<br>0.1148<br>0.1173<br>0.1199                     | 0.17 Q<br>0.18 Q<br>0.18 Q<br>0.18 Q<br>0.19 Q<br>0.19 Q<br>0.19 Q<br>0.19 Q<br>0.19 Q<br>0.20 Q<br>0.20 Q<br>0.20 Q<br>0.20 Q<br>0.21 Q |     | -<br>-<br>-<br>-<br>-<br>-<br>-<br>-<br>-<br>-<br>-<br>-<br>-<br>-<br>-<br>-<br>-<br>-<br>- |     |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | 10.15<br>10.30<br>10.45<br>10.60<br>10.75<br>10.90<br>11.05<br>11.20<br>11.35<br>11.50<br>11.65<br>11.80<br>11.95<br>12.10<br>12.25 | 0.1251<br>0.1278<br>0.1305<br>0.1332<br>0.1360<br>0.1389<br>0.1418<br>0.1447<br>0.1447<br>0.1447<br>0.1508<br>0.1550<br>0.1550<br>0.1638<br>0.1676           | $\begin{array}{cccccccccccccccccccccccccccccccccccc$                                                                                     |     |                                                                                             |     |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | 12.55 12.70 12.85 13.00 13.15 13.30 13.45 13.60 13.75 13.90 14.05 14.20 14.35 14.50                                                 | 0.1762<br>0.1806<br>0.1852<br>0.1947<br>0.1996<br>0.2047<br>0.2099<br>0.2153<br>0.2209<br>0.2267<br>0.2328<br>0.2394<br>0.2462                               | $\begin{array}{cccccccccccccccccccccccccccccccccccc$                                                                                     |     | ·<br>·<br>·<br>·<br>·<br>·<br>·<br>·                                                        |     |
|                                                      | 14.80<br>14.95<br>15.10<br>15.25<br>15.40<br>15.55<br>15.70<br>15.85<br>16.00<br><b>16.15</b><br>16.30<br>16.45<br>16.60            | 0.2609<br>0.2689<br>0.2775<br>0.2870<br>0.2974<br>0.3085<br>0.3206<br>0.3370<br>0.3608<br>0.4188<br>0.4188<br>0.4836<br>0.4936                               | $\begin{array}{cccccccccccccccccccccccccccccccccccc$                                                                                     | Q . | ·<br>·<br>·<br>·<br>·<br>·                                                                  | Q . |

| 18.10 | 0.5520 | 0.34 | .Q |   |   |          |          |  |
|-------|--------|------|----|---|---|----------|----------|--|
| 18.25 | 0.5557 | 0.26 | .Q |   |   |          |          |  |
| 18.40 | 0.5589 | 0.25 | .Q |   |   |          |          |  |
| 18.55 | 0.5620 | 0.24 | Q  |   |   |          |          |  |
| 18.70 | 0.5650 | 0.23 | Q  |   |   |          |          |  |
| 18.85 | 0.5678 | 0.23 | õ  |   |   | -        | -        |  |
| 19.00 | 0.5706 | 0.22 | õ  |   |   | -        | -        |  |
| 19.15 | 0.5733 | 0.21 | õ  |   |   | -        | -        |  |
| 19.30 | 0.5758 | 0.21 | õ  |   |   |          |          |  |
| 19.45 | 0.5784 | 0.20 | õ  |   |   | -        | -        |  |
| 19.60 | 0.5808 | 0.19 | õ  |   |   | <u>.</u> | <u>.</u> |  |
| 19.75 | 0.5832 | 0.19 | Q  | - | - | -        | -        |  |
| 19.90 | 0.5855 | 0.18 | õ  | • | • |          | •        |  |
| 20.05 | 0.5877 | 0.18 | õ  | • | • | •        | •        |  |
| 20.20 | 0.5900 | 0.18 | õ  | • | • | •        | •        |  |
| 20.35 | 0.5921 | 0.17 | õ  | • | • | •        | •        |  |
| 20.50 | 0.5942 | 0.17 | õ  | • | • | •        | •        |  |
| 20.50 | 0.5963 | 0.16 | õ  | • | • | •        | •        |  |
| 20.80 | 0.5983 | 0.10 | õ  | • | • | •        | •        |  |
| 20.80 | 0.6003 | 0.10 |    |   | • |          | •        |  |
| 20.95 | 0.6022 | 0.16 | Q  | • | • | •        | •        |  |
| 21.10 | 0.6041 | 0.16 | Q  | • | • | •        | •        |  |
| 21.25 |        |      | Q  | • | • | •        | •        |  |
|       | 0.6060 | 0.15 | Q  | • | • | •        | •        |  |
| 21.55 | 0.6078 | 0.15 | Q  | • | • | •        | •        |  |
| 21.70 | 0.6096 | 0.14 | Q  |   | • | •        | •        |  |
| 21.85 | 0.6114 | 0.14 | Q  | • | • | •        | •        |  |
| 22.00 | 0.6132 | 0.14 | Q  | • |   | •        |          |  |
| 22.15 | 0.6149 | 0.14 | Q  | • |   | •        |          |  |
| 22.30 | 0.6166 | 0.14 | Q  |   |   | •        |          |  |
| 22.45 | 0.6182 | 0.13 | Q  | • | • |          | •        |  |
| 22.60 | 0.6199 | 0.13 | Q  | • | • | •        | •        |  |
| 22.75 | 0.6215 | 0.13 | Q  | • | • | •        |          |  |
| 22.90 | 0.6231 | 0.13 | Q  |   |   |          |          |  |
| 23.05 | 0.6247 | 0.13 | Q  |   | • | •        |          |  |
| 23.20 | 0.6262 | 0.12 | Q  |   |   |          |          |  |
| 23.35 | 0.6278 | 0.12 | Q  |   |   |          |          |  |
| 23.50 | 0.6293 | 0.12 | Q  |   |   |          |          |  |
| 23.65 | 0.6308 | 0.12 | Q  |   |   |          |          |  |
| 23.80 | 0.6322 | 0.12 | Q  |   |   |          |          |  |
| 23.95 | 0.6337 | 0.12 | Q  |   |   |          |          |  |
| 24.10 | 0.6351 | 0.12 | Q  |   |   | •        |          |  |
| 24.25 | 0.6359 | 0.00 | Q  |   |   |          |          |  |
|       |        |      |    |   |   |          |          |  |
|       |        |      |    |   |   |          |          |  |
|       |        |      |    |   |   |          |          |  |

TIME DURATION(minutes) OF PERCENTILES OF ESTIMATED PEAK FLOW RATE: (Note: 100% of Peak Flow Rate estimate assumed to have an instantaneous time duration)

| Percentile of Estimated | Duration  |
|-------------------------|-----------|
| Peak Flow Rate          | (minutes) |
|                         |           |
| 0%                      | 1440.0    |
| 10%                     | 90.0      |
| 20%                     | 27.0      |
| 30%                     | 18.0      |
| 40%                     | 9.0       |
| 50%                     | 9.0       |
| 60%                     | 9.0       |
| 70%                     | 9.0       |
| 80%                     | 9.0       |
| 90%                     | 9.0       |
|                         |           |

SMALL AREA UNIT HYDROGRAPH MODEL (C) Copyright 1989-2016 Advanced Engineering Software (aes) Ver. 23.0 Release Date: 07/01/2016 License ID 1435 Analysis prepared by: THIENES ENGINEERING, INC. 14349 FIRESTONE BLVD LA MIRADA, CA 90638 714-521-4811 \_\_\_\_\_ Problem Descriptions: TEI JOB 3910 2-YEAR HYDROGRAPH EXISTING CONDITION TO ECKHOFF STREET RATIONAL METHOD CALIBRATION COEFFICIENT = 0.90 TOTAL CATCHMENT AREA(ACRES) = 6.00 SOIL-LOSS RATE, Fm,(INCH/HR) = 0.040 LOW LOSS FRACTION = 0.199 TIME OF CONCENTRATION(MIN.) = 7.10 SMALL AREA PEAK Q COMPUTED USING PEAK FLOW RATE FORMULA ORANGE COUNTY "VALLEY" RAINFALL VALUES ARE USED RETURN FREQUENCY(YEARS) = 2 5-MINUTE POINT RAINFALL VALUE(INCHES) = 0.19 30-MINUTE POINT RAINFALL VALUE(INCHES) = 0.40 1-HOUR POINT RAINFALL VALUE(INCHES) = 0.53 POINT RAINFALL VALUE(INCHES) = 0.89 3-HOUR POINT RAINFALL VALUE(INCHES) = 1.22 6-HOUR 24-HOUR POINT RAINFALL VALUE(INCHES) = 2.05 \_\_\_\_\_ TOTAL CATCHMENT RUNOFF VOLUME(ACRE-FEET) = 0.76 TOTAL CATCHMENT RUNOFF VOLUME(ACRE-FEET) = 0.76 TOTAL CATCHMENT SOIL-LOSS VOLUME(ACRE-FEET) = 0.26 \*\*\*\*\*\* TIME VOLUME Q 0. 2.5 5.0 7.5 10.0 (HOURS) (AF) (CFS) .\_\_\_\_\_ 0.0000 0.0007 0.0020 0.0034 0.0048 0.0061 0.0075 0.0089 0.0102 0.00 Q 0.03 . . . . 0.14 0.14 Q  $\begin{array}{c} 0.14 \\ 0.14 \\ 0.14 \\ 0.14 \\ 0.14 \\ 0.14 \\ 0.14 \\ 0.14 \\ 0.14 \\ 0.14 \end{array}$ . . 0.26 Q . 0.38 0.50 0 . . Q . . . . 0.62 Q . . . . 0.74 Q . . . 0.85 Q 0.0103 0.0117 0.0131 0.97 0.14 0 . . . . 1.09 0.14 0 . . 0.14 õ 1.21 . . 0.0146 1.33 0.15 Q . . . 1.45 0.15 Q . . 0.0174 0.0189 1.56 0.15 0 1.68 0.15 0 . . 0.0203 0.0218 0.0232 1.80 0.15 0 . . . 1.92 0.15 õ . 2.04 0.15 Q 0.0247 0.0262 2.16 0.15 Q 2.27 0.15 0 . . 0.0277 0.0291 2.39 0.15 0 . . 2.51 0.15 Q . . . 2.63 0.0307 0.15 Q . . 2.75 0.0322 0.15 Q 0.0337 2.87 0.16 0 0.0352 0.0367 2.98 0.16 0 . . . . 3.10 0.16 0 . . . . 0.0383 3.22 0.16 Q . . . 3.34 0.0398 0.16 Q . . . 0.0414 3.46 0.16 0 0.0430 3.58 0.16 0 . . 3.69 0.16 0 . . . . 0.0462 0.0478 0.0494 0.16 Q 0.16 Q 0.16 Q 0.17 Q 3.81 . . . 3.93 . 4.05 0.17 Q 0.17 O 4.17 0.0510

| 4.29  | 0.0526 | 0.17 | Q   |   |   |   |     |
|-------|--------|------|-----|---|---|---|-----|
| 4.40  | 0.0543 | 0.17 |     |   |   |   |     |
|       |        |      | Q   | • | • | • | •   |
| 4.52  | 0.0559 | 0.17 | Q   | • | • | • | •   |
| 4.64  | 0.0576 | 0.17 | Q   | • | • | • | •   |
| 4.76  | 0.0592 | 0.17 | Q   |   |   |   |     |
| 4.88  | 0.0609 | 0.17 | Q   |   |   |   |     |
| 5.00  | 0.0626 | 0.17 | õ   |   |   |   |     |
|       |        |      |     | • | • | • | •   |
| 5.11  | 0.0643 | 0.17 | Q   | • | • | • | •   |
| 5.23  | 0.0660 | 0.18 | Q   | • | • | • | •   |
| 5.35  | 0.0678 | 0.18 | Q   |   |   |   |     |
| 5.47  | 0.0695 | 0.18 | Q   |   |   |   |     |
| 5.59  | 0.0713 | 0.18 | õ   |   |   |   |     |
| 5.71  |        |      |     | • | • | • | •   |
|       | 0.0730 | 0.18 | Q   | • | • | • | •   |
| 5.82  | 0.0748 | 0.18 | Q   | • | • | • | •   |
| 5.94  | 0.0766 | 0.18 | Q   |   |   |   |     |
| 6.06  | 0.0784 | 0.18 | Q   |   |   |   |     |
| 6.18  | 0.0802 | 0.19 | õ   |   |   |   |     |
|       |        |      |     | • | • | • | •   |
| 6.30  | 0.0820 | 0.19 | Q   | • | • | • | •   |
| 6.41  | 0.0839 | 0.19 | Q   | • | • | • | •   |
| 6.53  | 0.0858 | 0.19 | Q   |   |   |   |     |
| 6.65  | 0.0876 | 0.19 | Q   |   |   |   |     |
| 6.77  | 0.0895 | 0.19 | õ   |   |   |   |     |
| 6.89  | 0.0914 |      |     | • | • | • | •   |
|       |        | 0.20 | Q   | • | • | • | •   |
| 7.01  | 0.0933 | 0.20 | Q   | • | • | • | •   |
| 7.12  | 0.0953 | 0.20 | Q   |   |   |   |     |
| 7.24  | 0.0972 | 0.20 | Q   |   |   |   |     |
| 7.36  | 0.0992 | 0.20 | õ   |   |   |   |     |
| 7.48  |        |      |     | • | • | • | •   |
|       | 0.1012 | 0.20 | Q   | • | • | • | •   |
| 7.60  | 0.1032 | 0.21 | Q   | • | • | • | ·   |
| 7.72  | 0.1052 | 0.21 | Q   |   |   |   |     |
| 7.84  | 0.1072 | 0.21 | Q   |   |   |   |     |
| 7.95  | 0.1093 | 0.21 | õ   |   |   |   |     |
|       |        |      |     | • | • | • | •   |
| 8.07  | 0.1114 | 0.21 | Q   | • | • | • | •   |
| 8.19  | 0.1134 | 0.21 | Q   | • | • | • | ·   |
| 8.31  | 0.1156 | 0.22 | Q   |   |   |   |     |
| 8.43  | 0.1177 | 0.22 | Q   |   |   |   |     |
| 8.55  | 0.1198 | 0.22 | õ   |   |   |   |     |
|       |        |      |     | • | • | • | •   |
| 8.66  | 0.1220 | 0.22 | Q   | • | • | • | ·   |
| 8.78  | 0.1242 | 0.23 | Q   | • | • | • | ·   |
| 8.90  | 0.1264 | 0.23 | Q   |   |   |   |     |
| 9.02  | 0.1287 | 0.23 | Q   |   |   |   |     |
| 9.14  | 0.1309 | 0.23 | õ   |   |   |   |     |
|       |        |      |     | • | • | • | •   |
| 9.26  | 0.1332 | 0.24 | Q   | • | • | • | ·   |
| 9.37  | 0.1355 | 0.24 | Q   | • | • | • | •   |
| 9.49  | 0.1379 | 0.24 | Q   |   |   |   |     |
| 9.61  | 0.1402 | 0.24 | Q   |   |   |   |     |
| 9.73  | 0.1426 | 0.25 | õ   |   |   |   |     |
|       |        |      |     | • | • | • | •   |
| 9.85  | 0.1451 | 0.25 | Q   | • | • | • | •   |
| 9.97  | 0.1475 | 0.25 | .Q  | • | • | • | ·   |
| 10.08 | 0.1500 | 0.25 | .Q  |   |   |   |     |
| 10.20 | 0.1525 | 0.26 | .Q  |   |   |   |     |
| 10.32 | 0.1550 | 0.26 | .Q  |   |   |   |     |
| 10.44 | 0.1576 | 0.27 | . Q |   |   |   |     |
| 10.56 | 0.1602 |      |     | • | • | • | •   |
|       |        | 0.27 | .Q  | • | • | • | •   |
| 10.68 | 0.1629 | 0.27 | .Q  | • | • | • | ·   |
| 10.79 | 0.1655 | 0.28 | .Q  |   |   |   |     |
| 10.91 | 0.1683 | 0.28 | .Q  |   |   |   |     |
| 11.03 | 0.1710 | 0.28 | . Q |   |   |   |     |
| 11.15 | 0.1738 | 0.20 | .Q  | · |   |   | -   |
|       |        |      |     | • | • | • | •   |
| 11.27 | 0.1767 | 0.29 | .Q  | • | • | • | ·   |
| 11.38 | 0.1795 | 0.30 | .Q  | • | • | • |     |
| 11.50 | 0.1825 | 0.30 | .Q  |   |   |   |     |
| 11.62 | 0.1854 | 0.31 | . Q |   |   |   |     |
| 11.74 | 0.1885 | 0.31 | .Q  |   |   |   | -   |
|       |        |      |     | • | • | • | •   |
| 11.86 | 0.1916 | 0.32 | .Q  | • | • | • | ·   |
| 11.98 | 0.1947 | 0.32 | .Q  | • | • | • | •   |
| 12.10 | 0.1981 | 0.38 | .Q  |   |   |   |     |
| 12.21 | 0.2020 | 0.41 | . Q |   |   |   |     |
| 12.33 | 0.2060 | 0.41 |     |   |   |   | · · |
|       |        |      | .Q  | • | • | • | •   |
| 12.45 | 0.2100 | 0.42 | .Q  | • | • | • | ·   |
| 12.57 | 0.2142 | 0.43 | .Q  |   |   |   |     |
| 12.69 | 0.2184 | 0.44 | .Q  |   |   |   |     |
| 12.80 | 0.2227 | 0.45 | . Q |   |   |   |     |
| 12.92 | 0.2271 | 0.45 |     |   |   |   | -   |
|       |        |      | .Q  | • | • | • | ·   |
| 13.04 | 0.2316 | 0.46 | .Q  | • | • | • | ·   |
| 13.16 | 0.2362 | 0.47 | .Q  | • | • | • |     |
| 13.28 | 0.2409 | 0.49 | .Q  |   |   |   |     |
| 13.40 | 0.2457 | 0.49 | .Q  |   |   |   |     |
| 13.52 | 0.2506 | 0.51 | . Q | _ |   |   |     |
| 13.63 | 0.2556 | 0.52 |     |   |   |   | -   |
|       |        |      | . Q | • | • | • | •   |
| 13.75 | 0.2608 | 0.54 | . Q | • | • | • | ·   |
| 13.87 | 0.2661 | 0.55 | . Q | • | • | • |     |
| 13.99 | 0.2715 | 0.57 | . Q |   |   |   |     |
| 14.11 | 0.2772 | 0.59 | . Q |   |   |   |     |
|       |        |      | ~   |   |   |   |     |

| 14.23<br>14.34<br>14.46<br>14.58<br>14.70<br>14.82<br>14.93<br>15.05<br>15.17<br>15.29<br>15.41<br>15.53<br>15.65<br>15.76<br>15.88<br>16.00<br><b>16.12</b><br>16.24                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         | 0.2832<br>0.2959<br>0.3026<br>0.3096<br>0.3169<br>0.3246<br>0.3227<br>0.3414<br>0.3508<br>0.3607<br>0.3709<br>0.3822<br>0.3958<br>0.4140<br>0.4403<br>0.5036<br>0.5603                     | 0.63<br>0.64<br>0.68<br>0.70<br>0.74<br>0.76<br>0.81<br>0.84<br>0.99<br>1.05<br>1.03<br>1.29<br>1.49<br>2.24<br>3.13<br>9.81<br>1.79                         | . Q<br>. Q<br>. Q<br>. Q<br>. Q<br>. Q<br>. Q<br>. Q<br>. Q<br>. Q |                                      | · · · · · · · · · · · · · · · · · · · | · · · · · · · · · · · · · · · · · · · |
|-----------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|--------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|--------------------------------------------------------------------------------------------------------------------------------------------------------------|--------------------------------------------------------------------|--------------------------------------|---------------------------------------|---------------------------------------|
| $16.35 \\ 16.47 \\ 16.59 \\ 16.71 \\ 16.83 \\ 16.95 \\ 17.07 \\ 17.18 \\ 17.30 \\ 17.42 \\ 17.54 \\ 17.54 \\ 17.66 \\ 17.77 \\ 17.89 \\ 18.01 \\ 18.13 \\ 18.25 \\ 18.25 \\ 18.13 \\ 18.25 \\ 10.11 \\ 18.13 \\ 18.25 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.11 \\ 10.1$ | 0.5747<br>0.5854<br>0.5949<br>0.6031<br>0.6104<br>0.6234<br>0.6291<br>0.6345<br>0.6442<br>0.6442<br>0.6488<br>0.6532<br>0.6575<br>0.6615<br>0.6683                                         | $\begin{array}{c} 1.14\\ 1.05\\ 0.88\\ 0.79\\ 0.72\\ 0.66\\ 0.62\\ 0.53\\ 0.50\\ 0.46\\ 0.44\\ 0.42\\ 0.41\\ 0.33\\ 0.31\\ \end{array}$                      | · Q<br>· Q<br>· Q<br>· Q<br>· Q<br>· Q<br>· Q<br>· Q<br>· Q<br>· Q | ·<br>·<br>·<br>·<br>·<br>·<br>·<br>· | ·<br>·<br>·<br>·<br>·<br>·<br>·       |                                       |
| 18.37<br>18.48<br>18.60<br>18.72<br>18.84<br>18.96<br>19.08<br>19.19<br>19.31<br>19.43<br>19.55<br>19.67<br>19.79<br>19.91<br>20.02<br>20.14<br>20.26                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         | 0.6713<br>0.6742<br>0.6771<br>0.6798<br>0.6825<br>0.6851<br>0.6877<br>0.6901<br>0.6926<br>0.6949<br>0.6972<br>0.6995<br>0.7017<br>0.7039<br>0.7060<br>0.7081<br>0.7102                     | $\begin{array}{c} 0.30\\ 0.29\\ 0.28\\ 0.27\\ 0.26\\ 0.26\\ 0.26\\ 0.25\\ 0.24\\ 0.23\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.21\\ 0.21\\ \end{array}$ |                                                                    | ·<br>·<br>·<br>·<br>·<br>·           | ·<br>·<br>·<br>·<br>·<br>·            |                                       |
| 20.38<br>20.50<br>20.61<br>20.73<br>20.85<br>20.97<br>21.09<br>21.21<br>21.33<br>21.44<br>21.56<br>21.68<br>21.80<br>21.92<br>22.03<br>22.15                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  | 0.7122<br>0.7142<br>0.7141<br>0.7180<br>0.7199<br>0.7218<br>0.7236<br>0.7254<br>0.7272<br>0.7290<br>0.7307<br>0.7324<br>0.7341<br>0.7357<br>0.7374<br>0.7374<br>0.7374                     | 0.21<br>0.20<br>0.20<br>0.19<br>0.19<br>0.19<br>0.19<br>0.19<br>0.19<br>0.18<br>0.18<br>0.18<br>0.18<br>0.17<br>0.17<br>0.17<br>0.17<br>0.16                 | ~~~~~~~~~~~~~~~~~~~                                                | ·<br>·<br>·<br>·<br>·<br>·           | ·<br>·<br>·<br>·<br>·<br>·            |                                       |
| 22.27<br>22.39<br>22.51<br>22.63<br>22.74<br>22.86<br>22.98<br>23.10<br>23.22<br>23.34<br>23.45<br>23.57<br>23.69<br>23.81<br>23.93<br>24.05                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  | 0.7406<br>0.7406<br>0.7422<br>0.7437<br>0.7453<br>0.7468<br>0.7483<br>0.7498<br>0.7513<br>0.7528<br>0.7513<br>0.7528<br>0.7542<br>0.7556<br>0.7571<br>0.7585<br>0.7599<br>0.7612<br>0.7626 | 0.16<br>0.16<br>0.16<br>0.16<br>0.16<br>0.15<br>0.15<br>0.15<br>0.15<br>0.15<br>0.15<br>0.15<br>0.15                                                         | x Q Q Q Q Q Q Q Q Q Q Q Q Q Q Q Q Q Q Q                            | ·<br>·<br>·<br>·<br>·<br>·           | ·<br>·<br>·<br>·<br>·<br>·            |                                       |

| 24.17 | 0.7633 | 0.00 Q |  |  |  |
|-------|--------|--------|--|--|--|
|       |        |        |  |  |  |

TIME DURATION(minutes) OF PERCENTILES OF ESTIMATED PEAK FLOW RATE: (Note: 100% of Peak Flow Rate estimate assumed to have an instantaneous time duration)

| Percentile of Estimated<br>Peak Flow Rate | Duration<br>(minutes) |
|-------------------------------------------|-----------------------|
|                                           |                       |
| 0%                                        | 1441.3                |
| 10%                                       | 78.1                  |
| 20%                                       | 21.3                  |
| 30%                                       | 14.2                  |
| 40%                                       | 7.1                   |
| 50%                                       | 7.1                   |
| 60%                                       | 7.1                   |
| 70%                                       | 7.1                   |
| 80%                                       | 7.1                   |
| 90%                                       | 7.1                   |

SMALL AREA UNIT HYDROGRAPH MODEL (C) Copyright 1989-2016 Advanced Engineering Software (aes) Ver. 23.0 Release Date: 07/01/2016 License ID 1435 Analysis prepared by: THIENES ENGINEERING, INC. 14349 FIRESTONE BLVD LA MIRADA, CA 90638 714-521-4811 \_\_\_\_\_ Problem Descriptions: TEI JOB 3910 2-YEAR HYDROGRAPH EXISTING CONDITION TO POPLAR STREET RATIONAL METHOD CALIBRATION COEFFICIENT = 0.90 TOTAL CATCHMENT AREA(ACRES) = 2.40 SOIL-LOSS RATE, Fm,(INCH/HR) = 0.040 LOW LOSS FRACTION = 0.199 TIME OF CONCENTRATION(MIN.) = 7.90 SMALL AREA PEAK Q COMPUTED USING PEAK FLOW RATE FORMULA ORANGE COUNTY "VALLEY" RAINFALL VALUES ARE USED RETURN FREQUENCY(YEARS) = 2 5-MINUTE POINT RAINFALL VALUE(INCHES) = 0.19 30-MINUTE POINT RAINFALL VALUE(INCHES) = 0.40 1-HOUR POINT RAINFALL VALUE(INCHES) = 0.53 POINT RAINFALL VALUE(INCHES) = 0.89 3-HOUR POINT RAINFALL VALUE(INCHES) = 1.22 6-HOUR 24-HOUR POINT RAINFALL VALUE(INCHES) = 2.05 \_\_\_\_\_ TOTAL CATCHMENT RUNOFF VOLUME(ACRE-FEET) = 0.31 TOTAL CATCHMENT RUNOFF VOLUME(ACRE-FEET) = 0.31 TOTAL CATCHMENT SOIL-LOSS VOLUME(ACRE-FEET) = 0.10 \*\*\*\*\*\* TIME VOLUME Q 0. 2.5 5.0 7.5 10.0 (HOURS) (AF) (CFS) .\_\_\_\_\_ 0.0002 0.0008 0.0014 0.0020 0.0026 0.0032 0.0038 0.0044 0.0051 0.06 Q 0.07 . . . . 0.20 0.06 Q . . 0.06 Q 0.33 . 0.06 0.06 0.06 0.06 0.06 0.46 0.59 0 . . Q . . . . 0.73 Q . . . . 0.86 Q . . . 0.99 Q 0.0051 0.0057 . 1.12 0.06 0 . . . 1.25 0.06 0 . . 1.38 0.0063 0.06 õ . . 0.0070 1.52 0.06 Q . . . 1.65 0.0076 0.06 Q . . 1.78 1.91 0.0082 0.0089 0.06 0 0.06 0 . . 0.0095 0.0102 0.0109 2.04 0.06 0 . . . 2.17 0.06 õ . 2.31 0.06 Q 2.44 0.0115 0.06 Q 0.0122 2.57 0.06 0 . . . 2.70 0.0129 0.06 0 . . 2.83 0.0135 0.06 Q . . . 2.96 0.0142 0.06 Q . . 3.10 0.0149 0.06 Q 0.0156 3.23 0.06 0 0.0163 3.36 0.06 0 . . . . 3.49 0.0170 0.06 0 . . . . 0.0177 0.06 3.62 Q . . . 3.75 0.0184 0.07 Q . . . 0.0191 0.07 3 89 0 0.0198 0.07 4.02 0 . . 4.15 0.0205 0.07 0 . . . 0.0212 0.0220 0.0227 4.28 0.07 Q 0.07 Q 0.07 Q 0.07 Q . . . 4.41 . 4.54 0.07 Q 0.07 Q . 0.0234 4.68

| 4.81                                                                                                                                                                                                                                                                                                                                           |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                |                                                     |                                                                                             |                                                                                             |                                                                                             |                                       |
|------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|-----------------------------------------------------|---------------------------------------------------------------------------------------------|---------------------------------------------------------------------------------------------|---------------------------------------------------------------------------------------------|---------------------------------------|
|                                                                                                                                                                                                                                                                                                                                                | 0.0242                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       | 0.07                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           | Q                                                   | •                                                                                           | •                                                                                           | •                                                                                           |                                       |
| 4.94                                                                                                                                                                                                                                                                                                                                           | 0.0249                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       | 0.07                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           | Q                                                   |                                                                                             |                                                                                             |                                                                                             |                                       |
| 5.07                                                                                                                                                                                                                                                                                                                                           | 0.0257                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       | 0.07                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           | Q                                                   |                                                                                             |                                                                                             |                                                                                             |                                       |
| 5.20                                                                                                                                                                                                                                                                                                                                           | 0.0265                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       | 0.07                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           | Q                                                   |                                                                                             |                                                                                             |                                                                                             |                                       |
| 5.34                                                                                                                                                                                                                                                                                                                                           | 0.0272                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       | 0.07                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           | Q                                                   |                                                                                             |                                                                                             |                                                                                             |                                       |
| 5.47                                                                                                                                                                                                                                                                                                                                           | 0.0280                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       | 0.07                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           | Q                                                   |                                                                                             |                                                                                             |                                                                                             |                                       |
| 5.60                                                                                                                                                                                                                                                                                                                                           | 0.0288                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       | 0.07                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           |                                                     | •                                                                                           | •                                                                                           | •                                                                                           | •                                     |
|                                                                                                                                                                                                                                                                                                                                                |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                | Q                                                   | •                                                                                           | •                                                                                           | •                                                                                           | •                                     |
| 5.73                                                                                                                                                                                                                                                                                                                                           | 0.0296                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       | 0.07                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           | Q                                                   | •                                                                                           | •                                                                                           | •                                                                                           | •                                     |
| 5.86                                                                                                                                                                                                                                                                                                                                           | 0.0304                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       | 0.07                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           | Q                                                   | •                                                                                           | •                                                                                           | •                                                                                           | •                                     |
| 5.99                                                                                                                                                                                                                                                                                                                                           | 0.0312                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       | 0.07                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           | Q                                                   | •                                                                                           | •                                                                                           | •                                                                                           | •                                     |
| 6.12                                                                                                                                                                                                                                                                                                                                           | 0.0320                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       | 0.07                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           | Q                                                   | •                                                                                           | •                                                                                           | •                                                                                           | •                                     |
| 6.26                                                                                                                                                                                                                                                                                                                                           | 0.0328                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       | 0.07                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           | Q                                                   |                                                                                             |                                                                                             |                                                                                             |                                       |
| 6.39                                                                                                                                                                                                                                                                                                                                           | 0.0336                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       | 0.08                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           | Q                                                   |                                                                                             |                                                                                             |                                                                                             |                                       |
| 6.52                                                                                                                                                                                                                                                                                                                                           | 0.0344                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       | 0.08                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           | Q                                                   |                                                                                             |                                                                                             |                                                                                             |                                       |
| 6.65                                                                                                                                                                                                                                                                                                                                           | 0.0353                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       | 0.08                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           | Q                                                   |                                                                                             |                                                                                             |                                                                                             |                                       |
| 6.78                                                                                                                                                                                                                                                                                                                                           | 0.0361                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       | 0.08                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           | Q                                                   |                                                                                             |                                                                                             |                                                                                             |                                       |
| 6.91                                                                                                                                                                                                                                                                                                                                           | 0.0369                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       | 0.08                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           | Q                                                   |                                                                                             |                                                                                             |                                                                                             | -                                     |
| 7.05                                                                                                                                                                                                                                                                                                                                           | 0.0378                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       | 0.08                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           | Q                                                   | -                                                                                           | -                                                                                           |                                                                                             | •                                     |
| 7.18                                                                                                                                                                                                                                                                                                                                           | 0.0387                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       | 0.08                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           |                                                     | •                                                                                           | •                                                                                           | •                                                                                           | •                                     |
|                                                                                                                                                                                                                                                                                                                                                |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                | Q                                                   | •                                                                                           | •                                                                                           | •                                                                                           | •                                     |
| 7.31                                                                                                                                                                                                                                                                                                                                           | 0.0395                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       | 0.08                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           | Q                                                   | •                                                                                           | •                                                                                           | •                                                                                           | •                                     |
| 7.44                                                                                                                                                                                                                                                                                                                                           | 0.0404                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       | 0.08                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           | Q                                                   | •                                                                                           | •                                                                                           | •                                                                                           | ·                                     |
| 7.57                                                                                                                                                                                                                                                                                                                                           | 0.0413                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       | 0.08                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           | Q                                                   | •                                                                                           | •                                                                                           | •                                                                                           | •                                     |
| 7.70                                                                                                                                                                                                                                                                                                                                           | 0.0422                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       | 0.08                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           | Q                                                   | •                                                                                           | •                                                                                           | •                                                                                           | •                                     |
| 7.84                                                                                                                                                                                                                                                                                                                                           | 0.0431                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       | 0.08                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           | Q                                                   |                                                                                             |                                                                                             |                                                                                             |                                       |
| 7.97                                                                                                                                                                                                                                                                                                                                           | 0.0440                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       | 0.08                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           | Q                                                   |                                                                                             |                                                                                             |                                                                                             |                                       |
| 8.10                                                                                                                                                                                                                                                                                                                                           | 0.0449                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       | 0.09                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           | Q                                                   |                                                                                             |                                                                                             |                                                                                             |                                       |
| 8.23                                                                                                                                                                                                                                                                                                                                           | 0.0459                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       | 0.09                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           | Q                                                   |                                                                                             |                                                                                             |                                                                                             |                                       |
| 8.36                                                                                                                                                                                                                                                                                                                                           | 0.0468                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       | 0.09                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           | õ                                                   |                                                                                             | <u>.</u>                                                                                    | _                                                                                           |                                       |
| 8.49                                                                                                                                                                                                                                                                                                                                           | 0.0478                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       | 0.09                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           | Q                                                   | -                                                                                           | -                                                                                           |                                                                                             | •                                     |
| 8.63                                                                                                                                                                                                                                                                                                                                           | 0.0487                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       | 0.09                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           | Q                                                   | •                                                                                           | •                                                                                           | •                                                                                           | •                                     |
| 8.76                                                                                                                                                                                                                                                                                                                                           | 0.0497                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       | 0.09                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           |                                                     | •                                                                                           | •                                                                                           | •                                                                                           | •                                     |
| 8.89                                                                                                                                                                                                                                                                                                                                           | 0.0507                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       | 0.09                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           | Q                                                   | •                                                                                           | •                                                                                           | •                                                                                           | •                                     |
| 9.02                                                                                                                                                                                                                                                                                                                                           | 0.0517                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       | 0.09                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           | Q                                                   |                                                                                             |                                                                                             | •                                                                                           | •                                     |
|                                                                                                                                                                                                                                                                                                                                                |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              | 0.09                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           | Q                                                   | •                                                                                           | •                                                                                           | •                                                                                           | •                                     |
| 9.15                                                                                                                                                                                                                                                                                                                                           | 0.0527                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                | Q                                                   |                                                                                             |                                                                                             | •                                                                                           | •                                     |
| 9.28                                                                                                                                                                                                                                                                                                                                           | 0.0537                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       | 0.09                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           | Q                                                   | •                                                                                           | •                                                                                           | •                                                                                           | •                                     |
| 9.42                                                                                                                                                                                                                                                                                                                                           | 0.0547                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       | 0.10                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           | Q                                                   | •                                                                                           | •                                                                                           | •                                                                                           | •                                     |
| 9.55                                                                                                                                                                                                                                                                                                                                           | 0.0558                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       | 0.10                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           | Q                                                   | •                                                                                           | •                                                                                           | •                                                                                           | ·                                     |
| 9.68                                                                                                                                                                                                                                                                                                                                           | 0.0569                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       | 0.10                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           | Q                                                   | •                                                                                           | •                                                                                           | •                                                                                           | ·                                     |
| 9.81                                                                                                                                                                                                                                                                                                                                           | 0.0579                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       | 0.10                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           | Q                                                   | •                                                                                           | •                                                                                           | •                                                                                           | ·                                     |
| 9.94                                                                                                                                                                                                                                                                                                                                           | 0.0590                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       | 0.10                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           | Q                                                   | •                                                                                           | •                                                                                           | •                                                                                           | •                                     |
| 10.07                                                                                                                                                                                                                                                                                                                                          | 0.0601                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       | 0.10                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           | Q                                                   | •                                                                                           | •                                                                                           | •                                                                                           | ·                                     |
| 10.21                                                                                                                                                                                                                                                                                                                                          | 0.0612                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       | 0.10                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           | Q                                                   | •                                                                                           | •                                                                                           | •                                                                                           | •                                     |
| 10.34                                                                                                                                                                                                                                                                                                                                          | 0.0624                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       | 0.10                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           | Q                                                   | •                                                                                           | •                                                                                           |                                                                                             |                                       |
| 10.47                                                                                                                                                                                                                                                                                                                                          | 0.0635                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       | 0.11                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           | Q                                                   |                                                                                             |                                                                                             |                                                                                             |                                       |
| 10.60                                                                                                                                                                                                                                                                                                                                          | 0.0647                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       | 0.11                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           | Q                                                   |                                                                                             |                                                                                             |                                                                                             |                                       |
| 10.73                                                                                                                                                                                                                                                                                                                                          | 0.0659                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       | 0.11                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           | Q                                                   |                                                                                             |                                                                                             |                                                                                             |                                       |
| 10 05                                                                                                                                                                                                                                                                                                                                          |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                |                                                     | •                                                                                           | •                                                                                           | •                                                                                           |                                       |
| 10.87                                                                                                                                                                                                                                                                                                                                          | 0.0671                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       | 0.11                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           | õ                                                   |                                                                                             |                                                                                             |                                                                                             |                                       |
| 10.87<br>11.00                                                                                                                                                                                                                                                                                                                                 | 0.0671<br>0.0683                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             | 0.11<br>0.11                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   |                                                     | ·<br>·                                                                                      |                                                                                             |                                                                                             | ·                                     |
|                                                                                                                                                                                                                                                                                                                                                |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                | Q                                                   | ·<br>·<br>·                                                                                 |                                                                                             |                                                                                             |                                       |
| 11.00                                                                                                                                                                                                                                                                                                                                          | 0.0683                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       | 0.11                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           | Q<br>Q                                              |                                                                                             |                                                                                             |                                                                                             |                                       |
| 11.00<br>11.13<br>11.26                                                                                                                                                                                                                                                                                                                        | 0.0683<br>0.0695                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             | 0.11<br>0.12                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   | Q<br>Q<br>Q<br>Q                                    |                                                                                             |                                                                                             |                                                                                             |                                       |
| 11.00<br>11.13<br>11.26<br>11.39                                                                                                                                                                                                                                                                                                               | 0.0683<br>0.0695<br>0.0708                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   | 0.11<br>0.12<br>0.12<br>0.12                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   |                                                     | ·<br>·<br>·                                                                                 |                                                                                             |                                                                                             |                                       |
| 11.00<br>11.13<br>11.26<br>11.39<br>11.52                                                                                                                                                                                                                                                                                                      | 0.0683<br>0.0695<br>0.0708<br>0.0721<br>0.0734                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               | 0.11<br>0.12<br>0.12<br>0.12<br>0.12                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           |                                                     | ·<br>·<br>·<br>·                                                                            |                                                                                             |                                                                                             |                                       |
| 11.00<br>11.13<br>11.26<br>11.39<br>11.52<br>11.65                                                                                                                                                                                                                                                                                             | 0.0683<br>0.0695<br>0.0708<br>0.0721<br>0.0734<br>0.0747                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     | 0.11<br>0.12<br>0.12<br>0.12<br>0.12<br>0.12<br>0.12                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           | Q<br>Q<br>Q<br>Q<br>Q<br>Q<br>Q<br>Q<br>Q           | ·<br>·<br>·<br>·                                                                            |                                                                                             | ·<br>·<br>·<br>·                                                                            |                                       |
| 11.00<br>11.13<br>11.26<br>11.39<br>11.52<br>11.65<br>11.79                                                                                                                                                                                                                                                                                    | 0.0683<br>0.0695<br>0.0708<br>0.0721<br>0.0734<br>0.0747<br>0.0760                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           | 0.11<br>0.12<br>0.12<br>0.12<br>0.12<br>0.12<br>0.12<br>0.13                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   | Q<br>Q<br>Q<br>Q<br>Q<br>Q<br>Q<br>Q<br>Q<br>Q<br>Q | ·<br>·<br>·<br>·                                                                            | ·<br>·<br>·<br>·                                                                            | ·<br>·<br>·<br>·                                                                            |                                       |
| 11.00<br>11.13<br>11.26<br>11.39<br>11.52<br>11.65<br>11.79<br>11.92                                                                                                                                                                                                                                                                           | 0.0683<br>0.0695<br>0.0708<br>0.0721<br>0.0734<br>0.0747<br>0.0760<br>0.0774                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 | 0.11<br>0.12<br>0.12<br>0.12<br>0.12<br>0.12<br>0.12<br>0.13<br>0.13                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           |                                                     | -<br>-<br>-<br>-<br>-<br>-<br>-<br>-<br>-                                                   | ·<br>·<br>·<br>·<br>·                                                                       | ·<br>·<br>·<br>·<br>·                                                                       |                                       |
| 11.00<br>11.13<br>11.26<br>11.39<br>11.52<br>11.65<br>11.79<br>11.92<br>12.05                                                                                                                                                                                                                                                                  | 0.0683<br>0.0695<br>0.0708<br>0.0721<br>0.0734<br>0.0747<br>0.0760<br>0.0774<br>0.0788                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       | 0.11<br>0.12<br>0.12<br>0.12<br>0.12<br>0.12<br>0.12<br>0.13<br>0.13                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           |                                                     | -<br>-<br>-<br>-<br>-<br>-<br>-<br>-<br>-<br>-<br>-                                         | ·<br>·<br>·<br>·<br>·                                                                       | ·<br>·<br>·<br>·<br>·                                                                       |                                       |
| 11.00<br>11.13<br>11.26<br>11.39<br>11.52<br>11.65<br>11.79<br>11.92<br>12.05<br>12.18                                                                                                                                                                                                                                                         | 0.0683<br>0.0695<br>0.0708<br>0.0721<br>0.0734<br>0.0747<br>0.0760<br>0.0774<br>0.0778<br>0.0788                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             | 0.11<br>0.12<br>0.12<br>0.12<br>0.12<br>0.12<br>0.12<br>0.13<br>0.13<br>0.13<br>0.16                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           |                                                     |                                                                                             | ·<br>·<br>·<br>·<br>·<br>·                                                                  | ·<br>·<br>·<br>·<br>·                                                                       |                                       |
| 11.00<br>11.13<br>11.26<br>11.39<br>11.52<br>11.65<br>11.79<br>11.92<br>12.05<br>12.18<br>12.31                                                                                                                                                                                                                                                | 0.0683<br>0.0695<br>0.0708<br>0.0721<br>0.0734<br>0.0747<br>0.0760<br>0.0760<br>0.0774<br>0.0788<br>0.0804<br>0.0822                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         | 0.11<br>0.12<br>0.12<br>0.12<br>0.12<br>0.12<br>0.13<br>0.13<br>0.13<br>0.13<br>0.16<br>0.16                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   |                                                     | ·<br>·<br>·<br>·<br>·                                                                       | ·<br>·<br>·<br>·<br>·<br>·                                                                  | ·<br>·<br>·<br>·<br>·<br>·                                                                  | • • • • • • • • •                     |
| 11.00<br>11.13<br>11.26<br>11.39<br>11.52<br>11.65<br>11.79<br>11.92<br>12.05<br>12.18<br>12.18<br>12.45                                                                                                                                                                                                                                       | 0.0683<br>0.0695<br>0.0708<br>0.0721<br>0.0734<br>0.0747<br>0.0760<br>0.0774<br>0.0788<br>0.0804<br>0.0804<br>0.0822<br>0.0840                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               | 0.11<br>0.12<br>0.12<br>0.12<br>0.12<br>0.13<br>0.13<br>0.13<br>0.13<br>0.16<br>0.16<br>0.17                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   | 0 0 0 0 0 0 0 0 0 0 0 0 0                           | ·<br>·<br>·<br>·<br>·                                                                       | ·<br>·<br>·<br>·<br>·<br>·<br>·<br>·                                                        | ·<br>·<br>·<br>·<br>·<br>·                                                                  | • • • • • • • • • • •                 |
| 11.00<br>11.13<br>11.26<br>11.39<br>11.52<br>11.65<br>11.79<br>11.92<br>12.05<br>12.18<br>12.31<br>12.45<br>12.58                                                                                                                                                                                                                              | 0.0683<br>0.0695<br>0.0708<br>0.0721<br>0.0734<br>0.0747<br>0.0747<br>0.0760<br>0.0774<br>0.0788<br>0.0804<br>0.0822<br>0.0840<br>0.0858                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     | 0.11<br>0.12<br>0.12<br>0.12<br>0.12<br>0.13<br>0.13<br>0.13<br>0.13<br>0.16<br>0.16<br>0.17<br>0.17                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           | ~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~             | ·<br>·<br>·<br>·<br>·<br>·                                                                  | ·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·                                              | ·<br>·<br>·<br>·<br>·<br>·                                                                  | · · · · · · · · · · · · · · · · · · · |
| 11.00<br>11.13<br>11.26<br>11.39<br>11.52<br>11.65<br>11.79<br>11.92<br>12.05<br>12.18<br>12.31<br>12.45<br>12.58<br>12.71                                                                                                                                                                                                                     | 0.0683<br>0.0695<br>0.0708<br>0.0721<br>0.0734<br>0.0747<br>0.0760<br>0.0774<br>0.0778<br>0.0788<br>0.0804<br>0.0822<br>0.0840<br>0.0858<br>0.0877                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           | 0.11<br>0.12<br>0.12<br>0.12<br>0.12<br>0.12<br>0.13<br>0.13<br>0.13<br>0.16<br>0.16<br>0.17<br>0.17<br>0.18                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   | ~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~             | ·<br>·<br>·<br>·<br>·<br>·                                                                  | ·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>· | ·<br>·<br>·<br>·<br>·<br>·<br>·<br>·                                                        | · · · · · · · · · · · · · · · · · · · |
| 11.00<br>11.13<br>11.26<br>11.39<br>11.52<br>11.65<br>11.79<br>11.92<br>12.05<br>12.18<br>12.31<br>12.45<br>12.58<br>12.71<br>12.84                                                                                                                                                                                                            | 0.0683<br>0.0695<br>0.0708<br>0.0721<br>0.0734<br>0.0747<br>0.0760<br>0.0774<br>0.0760<br>0.0804<br>0.0804<br>0.0822<br>0.0840<br>0.0858<br>0.0877<br>0.0896                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 | 0.11<br>0.12<br>0.12<br>0.12<br>0.12<br>0.12<br>0.13<br>0.13<br>0.13<br>0.13<br>0.16<br>0.16<br>0.16<br>0.17<br>0.17<br>0.18<br>0.18                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           | ~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~             | ·<br>·<br>·<br>·<br>·<br>·                                                                  | ·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>· | ·<br>·<br>·<br>·<br>·<br>·<br>·                                                             | · · · · · · · · · · · · · · · · · · · |
| 11.00<br>11.13<br>11.26<br>11.39<br>11.52<br>11.65<br>11.79<br>12.05<br>12.18<br>12.45<br>12.45<br>12.45<br>12.58<br>12.71<br>12.84<br>12.97                                                                                                                                                                                                   | 0.0683<br>0.0695<br>0.0708<br>0.0721<br>0.0734<br>0.0747<br>0.0760<br>0.0774<br>0.0788<br>0.0804<br>0.0822<br>0.0840<br>0.0840<br>0.0858<br>0.0877<br>0.0896<br>0.0916                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       | 0.11<br>0.12<br>0.12<br>0.12<br>0.12<br>0.12<br>0.13<br>0.13<br>0.13<br>0.13<br>0.16<br>0.16<br>0.16<br>0.17<br>0.17<br>0.18<br>0.18<br>0.18                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   | ~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~             | ·<br>·<br>·<br>·<br>·<br>·<br>·                                                             | ·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>· | ·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>· | · · · · · · · · · · · · · · · · · · · |
| 11.00<br>11.13<br>11.26<br>11.39<br>11.52<br>11.65<br>11.79<br>11.92<br>12.05<br>12.18<br>12.31<br>12.45<br>12.58<br>12.71<br>12.84<br>12.97<br>13.10                                                                                                                                                                                          | 0.0683<br>0.0695<br>0.0708<br>0.0721<br>0.0734<br>0.0747<br>0.0760<br>0.0774<br>0.0788<br>0.0804<br>0.0804<br>0.0822<br>0.0804<br>0.0822<br>0.0840<br>0.0858<br>0.0877<br>0.0896<br>0.0936                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   | 0.11<br>0.12<br>0.12<br>0.12<br>0.12<br>0.13<br>0.13<br>0.13<br>0.13<br>0.16<br>0.16<br>0.16<br>0.17<br>0.17<br>0.17<br>0.18<br>0.18<br>0.18<br>0.19                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           | ~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~             | ·<br>·<br>·<br>·<br>·<br>·<br>·                                                             | ·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>· | ·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·                                              | · · · · · · · · · · · · · · · · · · · |
| 11.00<br>11.13<br>11.26<br>11.39<br>11.52<br>11.65<br>11.79<br>11.92<br>12.05<br>12.18<br>12.31<br>12.45<br>12.58<br>12.71<br>12.84<br>12.97<br>13.10<br>13.23                                                                                                                                                                                 | 0.0683<br>0.0695<br>0.0708<br>0.0721<br>0.0734<br>0.0747<br>0.0760<br>0.0774<br>0.0788<br>0.0804<br>0.0822<br>0.0840<br>0.0822<br>0.0840<br>0.0858<br>0.0877<br>0.0858<br>0.0877<br>0.0896<br>0.0916<br>0.0957                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               | 0.11<br>0.12<br>0.12<br>0.12<br>0.12<br>0.13<br>0.13<br>0.13<br>0.16<br>0.16<br>0.16<br>0.16<br>0.17<br>0.17<br>0.17<br>0.18<br>0.18<br>0.18<br>0.19<br>0.19                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   | ~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~             | ·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>· |                                                                                             | ·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>· | · · · · · · · · · · · · · · · · · · · |
| 11.00<br>11.13<br>11.26<br>11.39<br>11.52<br>11.65<br>11.79<br>12.05<br>12.18<br>12.45<br>12.58<br>12.71<br>12.84<br>12.97<br>13.10<br>13.23<br>13.37                                                                                                                                                                                          | 0.0683<br>0.0695<br>0.0708<br>0.0721<br>0.0734<br>0.0747<br>0.0760<br>0.0774<br>0.0788<br>0.0804<br>0.0822<br>0.0840<br>0.0858<br>0.0858<br>0.0857<br>0.0896<br>0.0916<br>0.0936<br>0.0957<br>0.0978                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         | 0.11<br>0.12<br>0.12<br>0.12<br>0.12<br>0.13<br>0.13<br>0.13<br>0.16<br>0.16<br>0.16<br>0.17<br>0.17<br>0.18<br>0.18<br>0.18<br>0.18<br>0.19<br>0.19<br>0.20                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   | ~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~             | ·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>· | ·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>· | ·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>· | · · · · · · · · · · · · · · · · · · · |
| 11.00<br>11.13<br>11.26<br>11.39<br>11.52<br>11.65<br>11.79<br>12.05<br>12.18<br>12.45<br>12.45<br>12.58<br>12.71<br>12.84<br>12.97<br>13.10<br>13.23<br>13.50                                                                                                                                                                                 | 0.0683<br>0.0695<br>0.0708<br>0.0721<br>0.0734<br>0.0747<br>0.0760<br>0.0774<br>0.0788<br>0.0804<br>0.0804<br>0.0822<br>0.0840<br>0.0858<br>0.0877<br>0.0858<br>0.0877<br>0.0896<br>0.0916<br>0.0957<br>0.0957<br>0.0978<br>0.1000                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           | 0.11<br>0.12<br>0.12<br>0.12<br>0.12<br>0.13<br>0.13<br>0.13<br>0.13<br>0.16<br>0.16<br>0.17<br>0.17<br>0.17<br>0.17<br>0.18<br>0.18<br>0.18<br>0.19<br>0.20<br>0.20                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           | ~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~             | ·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>· |                                                                                             | ·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>· | · · · · · · · · · · · · · · · · · · · |
| $\begin{array}{c} 11.00\\ 11.13\\ 11.26\\ 11.39\\ 11.52\\ 11.65\\ 11.79\\ 11.92\\ 12.05\\ 12.18\\ 12.31\\ 12.45\\ 12.58\\ 12.71\\ 12.84\\ 12.97\\ 13.10\\ 13.23\\ 13.37\\ 13.50\\ 13.63\\ \end{array}$                                                                                                                                         | 0.0683<br>0.0695<br>0.0708<br>0.0721<br>0.0747<br>0.0747<br>0.0760<br>0.0774<br>0.0788<br>0.0804<br>0.0804<br>0.0822<br>0.0840<br>0.0858<br>0.0877<br>0.0896<br>0.0916<br>0.0916<br>0.0957<br>0.0978<br>0.1000<br>0.1022                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     | 0.11<br>0.12<br>0.12<br>0.12<br>0.12<br>0.13<br>0.13<br>0.13<br>0.13<br>0.16<br>0.16<br>0.17<br>0.17<br>0.17<br>0.17<br>0.18<br>0.19<br>0.19<br>0.20<br>0.21                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   | ~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~             | ·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>· |                                                                                             | ·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>· | · · · · · · · · · · · · · · · · · · · |
| 11.00<br>11.13<br>11.26<br>11.39<br>11.52<br>11.65<br>11.79<br>11.92<br>12.05<br>12.18<br>12.31<br>12.45<br>12.58<br>12.71<br>12.84<br>12.97<br>13.10<br>13.23<br>13.37<br>13.50<br>13.76                                                                                                                                                      | 0.0683<br>0.0695<br>0.0708<br>0.0721<br>0.0734<br>0.0747<br>0.0760<br>0.0774<br>0.0760<br>0.0804<br>0.0822<br>0.0840<br>0.0858<br>0.0877<br>0.0858<br>0.0877<br>0.0858<br>0.0916<br>0.0916<br>0.0957<br>0.0936<br>0.0957<br>0.0978<br>0.1000<br>0.1022<br>0.1045                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             | $\begin{array}{c} 0.11\\ 0.12\\ 0.12\\ 0.12\\ 0.12\\ 0.13\\ 0.13\\ 0.13\\ 0.13\\ 0.16\\ 0.16\\ 0.17\\ 0.17\\ 0.18\\ 0.18\\ 0.18\\ 0.18\\ 0.19\\ 0.20\\ 0.20\\ 0.20\\ 0.21\\ 0.22\\ \end{array}$                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                | ~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~             | ·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>· |                                                                                             | ·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>· | · · · · · · · · · · · · · · · · · · · |
| 11.00<br>11.13<br>11.26<br>11.39<br>11.52<br>11.65<br>11.79<br>11.92<br>12.05<br>12.18<br>12.45<br>12.58<br>12.71<br>12.84<br>12.97<br>13.10<br>13.23<br>13.37<br>13.50<br>13.63<br>13.76<br>13.89                                                                                                                                             | 0.0683<br>0.0695<br>0.0708<br>0.0721<br>0.0734<br>0.0747<br>0.0760<br>0.0774<br>0.0788<br>0.0804<br>0.0822<br>0.0840<br>0.0858<br>0.0858<br>0.0857<br>0.0896<br>0.0916<br>0.0936<br>0.0957<br>0.0936<br>0.0978<br>0.1000<br>0.1022<br>0.1045<br>0.1069                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       | 0.11<br>0.12<br>0.12<br>0.12<br>0.12<br>0.13<br>0.13<br>0.13<br>0.13<br>0.16<br>0.17<br>0.17<br>0.17<br>0.17<br>0.18<br>0.18<br>0.18<br>0.19<br>0.20<br>0.20<br>0.22<br>0.22                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   | ~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~             | ·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>· |                                                                                             | ·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>· | · · · · · · · · · · · · · · · · · · · |
| 11.00<br>11.13<br>11.26<br>11.39<br>11.52<br>11.65<br>11.79<br>12.05<br>12.18<br>12.45<br>12.58<br>12.71<br>12.45<br>12.58<br>12.71<br>12.84<br>12.97<br>13.10<br>13.23<br>13.50<br>13.63<br>13.76<br>13.89<br>14.02                                                                                                                           | 0.0683<br>0.0695<br>0.0708<br>0.0721<br>0.0734<br>0.0747<br>0.0760<br>0.0760<br>0.0774<br>0.0804<br>0.0804<br>0.0822<br>0.0840<br>0.0858<br>0.0877<br>0.0896<br>0.0916<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.05 | 0.11<br>0.12<br>0.12<br>0.12<br>0.12<br>0.13<br>0.13<br>0.13<br>0.13<br>0.16<br>0.16<br>0.17<br>0.17<br>0.17<br>0.17<br>0.18<br>0.18<br>0.18<br>0.19<br>0.20<br>0.20<br>0.21<br>0.22<br>0.22                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   | ~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~             | ·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>· |                                                                                             | ·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>· | · · · · · · · · · · · · · · · · · · · |
| $\begin{array}{c} 11.00\\ 11.13\\ 11.26\\ 11.39\\ 11.52\\ 11.65\\ 11.79\\ 11.92\\ 12.05\\ 12.18\\ 12.31\\ 12.45\\ 12.58\\ 12.71\\ 12.84\\ 12.97\\ 13.10\\ 13.23\\ 13.37\\ 13.50\\ 13.63\\ 13.76\\ 13.89\\ 14.02\\ 14.16\\ \end{array}$                                                                                                         | 0.0683<br>0.0695<br>0.0708<br>0.0721<br>0.0734<br>0.0760<br>0.0774<br>0.0760<br>0.0822<br>0.0840<br>0.0822<br>0.0840<br>0.0858<br>0.0877<br>0.0858<br>0.0877<br>0.0916<br>0.0916<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.1000<br>0.1022<br>0.1045<br>0.1093<br>0.1119                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   | 0.11<br>0.12<br>0.12<br>0.12<br>0.12<br>0.13<br>0.13<br>0.13<br>0.13<br>0.16<br>0.17<br>0.17<br>0.17<br>0.17<br>0.18<br>0.18<br>0.18<br>0.19<br>0.20<br>0.20<br>0.22<br>0.22                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   | ~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~             |                                                                                             |                                                                                             | ·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>· | · · · · · · · · · · · · · · · · · · · |
| $\begin{array}{c} 11.00\\ 11.13\\ 11.26\\ 11.39\\ 11.52\\ 11.65\\ 11.79\\ 11.92\\ 12.05\\ 12.18\\ 12.31\\ 12.45\\ 12.58\\ 12.71\\ 12.84\\ 12.97\\ 13.10\\ 13.23\\ 13.37\\ 13.50\\ 13.63\\ 13.76\\ 13.89\\ 14.02\\ 14.16\\ 14.29 \end{array}$                                                                                                   | 0.0683<br>0.0695<br>0.0708<br>0.0721<br>0.0734<br>0.0747<br>0.0760<br>0.0760<br>0.0774<br>0.0804<br>0.0804<br>0.0822<br>0.0840<br>0.0858<br>0.0877<br>0.0896<br>0.0916<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.05 | 0.11<br>0.12<br>0.12<br>0.12<br>0.12<br>0.13<br>0.13<br>0.13<br>0.13<br>0.16<br>0.16<br>0.17<br>0.17<br>0.17<br>0.17<br>0.18<br>0.18<br>0.18<br>0.19<br>0.20<br>0.20<br>0.21<br>0.22<br>0.22                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   | ~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~             | ·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>· |                                                                                             | ·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>· |                                       |
| $\begin{array}{c} 11.00\\ 11.13\\ 11.26\\ 11.39\\ 11.52\\ 11.65\\ 11.79\\ 11.92\\ 12.05\\ 12.18\\ 12.31\\ 12.45\\ 12.58\\ 12.71\\ 12.84\\ 12.97\\ 13.10\\ 13.23\\ 13.37\\ 13.50\\ 13.63\\ 13.76\\ 13.89\\ 14.02\\ 14.16\\ \end{array}$                                                                                                         | 0.0683<br>0.0695<br>0.0708<br>0.0721<br>0.0734<br>0.0760<br>0.0774<br>0.0760<br>0.0822<br>0.0840<br>0.0822<br>0.0840<br>0.0858<br>0.0877<br>0.0858<br>0.0877<br>0.0916<br>0.0916<br>0.0957<br>0.0957<br>0.0957<br>0.0957<br>0.1000<br>0.1022<br>0.1045<br>0.1093<br>0.1119                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   | $\begin{array}{c} 0.11\\ 0.12\\ 0.12\\ 0.12\\ 0.12\\ 0.13\\ 0.13\\ 0.13\\ 0.13\\ 0.16\\ 0.16\\ 0.17\\ 0.18\\ 0.18\\ 0.18\\ 0.18\\ 0.19\\ 0.20\\ 0.20\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.24\\ \end{array}$                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  | ~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~             | ·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>· |                                                                                             | ·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>· |                                       |
| $\begin{array}{c} 11.00\\ 11.13\\ 11.26\\ 11.39\\ 11.52\\ 11.65\\ 11.79\\ 11.92\\ 12.05\\ 12.18\\ 12.31\\ 12.45\\ 12.58\\ 12.71\\ 12.84\\ 12.97\\ 13.10\\ 13.23\\ 13.37\\ 13.50\\ 13.63\\ 13.76\\ 13.89\\ 14.02\\ 14.16\\ 14.29 \end{array}$                                                                                                   | 0.0683<br>0.0695<br>0.0708<br>0.0721<br>0.0747<br>0.0760<br>0.0774<br>0.0760<br>0.0774<br>0.0788<br>0.0804<br>0.0822<br>0.0840<br>0.0858<br>0.0858<br>0.0877<br>0.0936<br>0.0936<br>0.0936<br>0.0978<br>0.0978<br>0.10022<br>0.1045<br>0.1069<br>0.1193<br>0.1146                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            | $\begin{array}{c} 0.11\\ 0.12\\ 0.12\\ 0.12\\ 0.12\\ 0.13\\ 0.13\\ 0.13\\ 0.13\\ 0.16\\ 0.17\\ 0.18\\ 0.18\\ 0.18\\ 0.18\\ 0.19\\ 0.20\\ 0.20\\ 0.20\\ 0.20\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\ 0.22\\$ | 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0               |                                                                                             |                                                                                             | ·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>· |                                       |
| $\begin{array}{c} 11.00\\ 11.13\\ 11.26\\ 11.39\\ 11.52\\ 11.65\\ 11.79\\ 12.05\\ 12.18\\ 12.45\\ 12.45\\ 12.45\\ 12.58\\ 12.71\\ 12.84\\ 12.97\\ 13.10\\ 13.23\\ 13.37\\ 13.50\\ 13.63\\ 13.76\\ 13.89\\ 14.02\\ 14.16\\ 14.29\\ 14.42\\ \end{array}$                                                                                         | 0.0683<br>0.0695<br>0.0708<br>0.0721<br>0.0734<br>0.0747<br>0.0760<br>0.0774<br>0.0788<br>0.0804<br>0.0822<br>0.0840<br>0.0858<br>0.0858<br>0.0877<br>0.0936<br>0.0936<br>0.0937<br>0.0937<br>0.0937<br>0.0937<br>0.1000<br>0.1022<br>0.1045<br>0.1093<br>0.1119<br>0.1146<br>0.1174                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         | 0.11<br>0.12<br>0.12<br>0.12<br>0.13<br>0.13<br>0.13<br>0.13<br>0.16<br>0.17<br>0.17<br>0.17<br>0.18<br>0.18<br>0.18<br>0.19<br>0.20<br>0.20<br>0.21<br>0.22<br>0.22<br>0.23<br>0.24<br>0.26                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   |                                                     |                                                                                             |                                                                                             | ·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>· |                                       |
| $\begin{array}{c} 11.00\\ 11.13\\ 11.26\\ 11.39\\ 11.52\\ 11.65\\ 11.79\\ 11.92\\ 12.05\\ 12.18\\ 12.31\\ 12.45\\ 12.58\\ 12.58\\ 12.71\\ 12.84\\ 12.97\\ 13.10\\ 13.23\\ 13.37\\ 13.50\\ 13.63\\ 13.76\\ 13.89\\ 14.02\\ 14.16\\ 14.29\\ 14.55\\ \end{array}$                                                                                 | 0.0683<br>0.0695<br>0.0708<br>0.0721<br>0.0734<br>0.0747<br>0.0760<br>0.0774<br>0.0788<br>0.0804<br>0.0822<br>0.0840<br>0.0858<br>0.0877<br>0.0858<br>0.0916<br>0.0936<br>0.0927<br>0.0936<br>0.0978<br>0.1000<br>0.1045<br>0.1069<br>0.1174<br>0.1203<br>0.1234                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             | 0.11<br>0.12<br>0.12<br>0.12<br>0.12<br>0.13<br>0.13<br>0.13<br>0.16<br>0.17<br>0.17<br>0.18<br>0.18<br>0.19<br>0.20<br>0.20<br>0.21<br>0.22<br>0.22<br>0.22<br>0.23<br>0.24<br>0.26<br>0.28                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   |                                                     | ·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>· |                                                                                             | ·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>· |                                       |
| $\begin{array}{c} 11.00\\ 11.13\\ 11.26\\ 11.39\\ 11.52\\ 11.65\\ 11.79\\ 11.92\\ 12.05\\ 12.18\\ 12.31\\ 12.45\\ 12.58\\ 12.71\\ 12.84\\ 12.97\\ 13.10\\ 13.23\\ 13.37\\ 13.50\\ 13.63\\ 13.76\\ 13.89\\ 14.02\\ 14.16\\ 14.29\\ 14.42\\ 14.55\\ 14.68\\ \end{array}$                                                                         | 0.0683<br>0.0695<br>0.0708<br>0.0721<br>0.0734<br>0.0747<br>0.0760<br>0.0774<br>0.0788<br>0.0804<br>0.0822<br>0.0840<br>0.0858<br>0.0858<br>0.0877<br>0.0896<br>0.0916<br>0.0936<br>0.0978<br>0.1000<br>0.1022<br>0.1045<br>0.1069<br>0.1045<br>0.1069<br>0.1146<br>0.1174<br>0.1203                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         | 0.11<br>0.12<br>0.12<br>0.12<br>0.13<br>0.13<br>0.13<br>0.13<br>0.16<br>0.17<br>0.17<br>0.17<br>0.18<br>0.18<br>0.18<br>0.19<br>0.20<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22                                                                                                                                                                                                                                                                                                                                                                   |                                                     | ·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>· |                                                                                             | ·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>· |                                       |
| $\begin{array}{c} 11.00\\ 11.13\\ 11.26\\ 11.39\\ 11.52\\ 11.65\\ 11.79\\ 11.92\\ 12.05\\ 12.18\\ 12.31\\ 12.45\\ 12.58\\ 12.71\\ 12.84\\ 12.97\\ 13.10\\ 13.23\\ 13.37\\ 13.50\\ 13.63\\ 13.76\\ 13.89\\ 14.02\\ 14.16\\ 14.29\\ 14.42\\ 14.55\\ 14.68\\ 14.82\\ \end{array}$                                                                 | 0.0683<br>0.0695<br>0.0708<br>0.0721<br>0.0747<br>0.0760<br>0.0774<br>0.0760<br>0.0774<br>0.0882<br>0.0804<br>0.0858<br>0.0877<br>0.0936<br>0.0936<br>0.0936<br>0.0978<br>0.0978<br>0.0978<br>0.0978<br>0.0978<br>0.0978<br>0.0978<br>0.0978<br>0.0978<br>0.0978<br>0.0978<br>0.0978<br>0.0978<br>0.0978<br>0.0978<br>0.0978<br>0.0978<br>0.0978<br>0.0978<br>0.0978<br>0.0978<br>0.1009<br>0.1119<br>0.1146<br>0.1174<br>0.12234<br>0.1267                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  | 0.11<br>0.12<br>0.12<br>0.12<br>0.12<br>0.13<br>0.13<br>0.13<br>0.13<br>0.16<br>0.17<br>0.17<br>0.17<br>0.18<br>0.18<br>0.18<br>0.18<br>0.19<br>0.20<br>0.20<br>0.20<br>0.22<br>0.22<br>0.23<br>0.24<br>0.26<br>0.26<br>0.29<br>0.31                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           |                                                     | ·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>· |                                                                                             | ·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>· |                                       |
| $\begin{array}{c} 11.00\\ 11.13\\ 11.26\\ 11.39\\ 11.52\\ 11.65\\ 11.79\\ 11.92\\ 12.05\\ 12.18\\ 12.31\\ 12.45\\ 12.58\\ 12.71\\ 12.84\\ 12.97\\ 13.10\\ 13.23\\ 13.37\\ 13.50\\ 13.63\\ 13.76\\ 13.89\\ 14.02\\ 14.16\\ 14.29\\ 14.16\\ 14.29\\ 14.68\\ 14.82\\ 14.55\\ 14.68\\ 14.82\\ 14.95\\ 15.08\\ \end{array}$                         | 0.0683<br>0.0695<br>0.0708<br>0.0721<br>0.0734<br>0.0747<br>0.0760<br>0.0774<br>0.0760<br>0.0822<br>0.0840<br>0.0822<br>0.0840<br>0.0858<br>0.0877<br>0.0896<br>0.0916<br>0.0936<br>0.0957<br>0.0978<br>0.1000<br>0.1022<br>0.1045<br>0.1069<br>0.1093<br>0.1119<br>0.1146<br>0.1174<br>0.1203<br>0.1234<br>0.1267<br>0.1301<br>0.1337                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       | 0.11<br>0.12<br>0.12<br>0.12<br>0.13<br>0.13<br>0.13<br>0.13<br>0.16<br>0.17<br>0.17<br>0.18<br>0.18<br>0.18<br>0.19<br>0.20<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.23<br>0.24<br>0.26<br>0.28<br>0.29<br>0.31<br>0.35                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           |                                                     | ·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>· |                                                                                             | ·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>· |                                       |
| $\begin{array}{c} 11.00\\ 11.13\\ 11.26\\ 11.39\\ 11.52\\ 11.65\\ 11.79\\ 11.92\\ 12.05\\ 12.18\\ 12.31\\ 12.45\\ 12.58\\ 12.71\\ 12.84\\ 12.97\\ 13.10\\ 13.23\\ 13.37\\ 13.50\\ 13.63\\ 13.76\\ 13.89\\ 14.02\\ 14.6\\ 14.29\\ 14.42\\ 14.55\\ 14.68\\ 14.82\\ 14.95\\ 15.08\\ 15.21\\ \end{array}$                                          | 0.0683<br>0.0695<br>0.0708<br>0.0721<br>0.0734<br>0.0747<br>0.0760<br>0.0774<br>0.0788<br>0.0804<br>0.0822<br>0.0840<br>0.0858<br>0.0877<br>0.0896<br>0.0916<br>0.0936<br>0.0997<br>0.0978<br>0.1009<br>0.1022<br>0.1045<br>0.1069<br>0.1174<br>0.1203<br>0.1234<br>0.1267<br>0.1337<br>0.1376                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               | 0.11<br>0.12<br>0.12<br>0.12<br>0.13<br>0.13<br>0.13<br>0.13<br>0.16<br>0.17<br>0.17<br>0.18<br>0.18<br>0.18<br>0.18<br>0.19<br>0.20<br>0.20<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.22<br>0.23<br>0.24<br>0.26<br>0.26<br>0.26<br>0.26<br>0.26<br>0.26<br>0.26<br>0.23<br>0.23<br>0.31<br>0.35<br>0.37                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           |                                                     | ·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>· |                                                                                             | ·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>· |                                       |
| $\begin{array}{c} 11.00\\ 11.13\\ 11.26\\ 11.39\\ 11.52\\ 11.65\\ 11.79\\ 11.92\\ 12.05\\ 12.18\\ 12.45\\ 12.45\\ 12.58\\ 12.71\\ 12.45\\ 12.58\\ 12.71\\ 12.84\\ 12.97\\ 13.10\\ 13.23\\ 13.37\\ 13.50\\ 13.63\\ 13.76\\ 13.89\\ 14.02\\ 14.16\\ 14.29\\ 14.42\\ 14.55\\ 14.68\\ 14.82\\ 14.95\\ 15.08\\ 15.21\\ 15.34\\ \end{array}$         | 0.0683<br>0.0695<br>0.0708<br>0.0721<br>0.0734<br>0.0747<br>0.0760<br>0.0774<br>0.0788<br>0.0804<br>0.0822<br>0.0840<br>0.0858<br>0.0877<br>0.0896<br>0.0916<br>0.0936<br>0.0936<br>0.0936<br>0.0937<br>0.0936<br>0.0978<br>0.1000<br>0.1022<br>0.1045<br>0.1069<br>0.1093<br>0.1119<br>0.1146<br>0.1174<br>0.1234<br>0.1234<br>0.1234<br>0.1237<br>0.1301<br>0.1337<br>0.1376<br>0.1419                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     | 0.11<br>0.12<br>0.12<br>0.12<br>0.13<br>0.13<br>0.13<br>0.13<br>0.16<br>0.17<br>0.17<br>0.17<br>0.18<br>0.18<br>0.18<br>0.18<br>0.19<br>0.20<br>0.20<br>0.22<br>0.22<br>0.23<br>0.24<br>0.26<br>0.28<br>0.26<br>0.28<br>0.28<br>0.22<br>0.23<br>0.24<br>0.26<br>0.28<br>0.28<br>0.26<br>0.28<br>0.28<br>0.26<br>0.28<br>0.26<br>0.28<br>0.28<br>0.26<br>0.28<br>0.28<br>0.26<br>0.28<br>0.28<br>0.26<br>0.28<br>0.26<br>0.28<br>0.29<br>0.31<br>0.32<br>0.37<br>0.42                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           |                                                     |                                                                                             |                                                                                             | ·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>·<br>· |                                       |
| $\begin{array}{c} 11.00\\ 11.13\\ 11.26\\ 11.39\\ 11.52\\ 11.65\\ 11.79\\ 11.92\\ 12.05\\ 12.18\\ 12.31\\ 12.45\\ 12.58\\ 12.58\\ 12.71\\ 12.84\\ 12.97\\ 13.10\\ 13.23\\ 13.37\\ 13.50\\ 13.63\\ 13.76\\ 13.89\\ 14.02\\ 14.16\\ 14.29\\ 14.68\\ 14.82\\ 14.55\\ 14.68\\ 14.82\\ 14.95\\ 15.08\\ 15.08\\ 15.21\\ 15.34\\ 15.47\\ \end{array}$ | 0.0683<br>0.0695<br>0.0708<br>0.0721<br>0.0734<br>0.0747<br>0.0760<br>0.0774<br>0.0822<br>0.0840<br>0.0822<br>0.0840<br>0.0858<br>0.0877<br>0.0896<br>0.0916<br>0.0936<br>0.0978<br>0.1000<br>0.1022<br>0.1045<br>0.1069<br>0.1045<br>0.1203<br>0.1234<br>0.1267<br>0.1337<br>0.1376<br>0.1465                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               | 0.11<br>0.12<br>0.12<br>0.12<br>0.13<br>0.13<br>0.13<br>0.16<br>0.17<br>0.18<br>0.18<br>0.18<br>0.18<br>0.19<br>0.20<br>0.20<br>0.221<br>0.22<br>0.22<br>0.223<br>0.24<br>0.26<br>0.28<br>0.29<br>0.32<br>0.35<br>0.37<br>0.41                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 |                                                     |                                                                                             |                                                                                             |                                                                                             |                                       |
| $\begin{array}{c} 11.00\\ 11.13\\ 11.26\\ 11.39\\ 11.52\\ 11.65\\ 11.79\\ 11.92\\ 12.05\\ 12.18\\ 12.45\\ 12.45\\ 12.58\\ 12.71\\ 12.45\\ 12.58\\ 12.71\\ 12.84\\ 12.97\\ 13.10\\ 13.23\\ 13.37\\ 13.50\\ 13.63\\ 13.76\\ 13.89\\ 14.02\\ 14.16\\ 14.29\\ 14.42\\ 14.55\\ 14.68\\ 14.82\\ 14.95\\ 15.08\\ 15.21\\ 15.34\\ \end{array}$         | 0.0683<br>0.0695<br>0.0708<br>0.0721<br>0.0734<br>0.0747<br>0.0760<br>0.0774<br>0.0788<br>0.0804<br>0.0822<br>0.0840<br>0.0858<br>0.0877<br>0.0896<br>0.0916<br>0.0936<br>0.0936<br>0.0936<br>0.0937<br>0.0936<br>0.0978<br>0.1000<br>0.1022<br>0.1045<br>0.1069<br>0.1093<br>0.1119<br>0.1146<br>0.1174<br>0.1234<br>0.1234<br>0.1234<br>0.1237<br>0.1301<br>0.1337<br>0.1376<br>0.1419                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     | 0.11<br>0.12<br>0.12<br>0.12<br>0.13<br>0.13<br>0.13<br>0.13<br>0.16<br>0.17<br>0.17<br>0.17<br>0.18<br>0.18<br>0.18<br>0.18<br>0.19<br>0.20<br>0.20<br>0.22<br>0.22<br>0.23<br>0.24<br>0.26<br>0.28<br>0.26<br>0.28<br>0.28<br>0.22<br>0.23<br>0.24<br>0.26<br>0.28<br>0.28<br>0.26<br>0.28<br>0.28<br>0.26<br>0.28<br>0.26<br>0.28<br>0.28<br>0.26<br>0.28<br>0.28<br>0.26<br>0.28<br>0.28<br>0.26<br>0.28<br>0.26<br>0.28<br>0.29<br>0.31<br>0.32<br>0.37<br>0.42                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           |                                                     |                                                                                             |                                                                                             |                                                                                             |                                       |

| 16.00                                          | 0.1644<br>0.1753                                                                               | 0.84<br>1.17 | . Q<br>. Q | •                                  | •                                                               | • | •    |
|------------------------------------------------|------------------------------------------------------------------------------------------------|--------------|------------|------------------------------------|-----------------------------------------------------------------|---|------|
| 16.13                                          | 0.2018                                                                                         | 3.68         | · v        | . Q                                |                                                                 | • |      |
| 16.26                                          | 0.2254                                                                                         | 0.67         | . Q        | . 2                                | -                                                               | - | -    |
| 16.40                                          | 0.2313                                                                                         | 0.42         | . Q        | -                                  | -                                                               | • | -    |
|                                                |                                                                                                |              |            | •                                  | •                                                               | • | •    |
| 16.53                                          | 0.2358                                                                                         | 0.39         | .Q         | •                                  | •                                                               | • |      |
| 16.66                                          | 0.2397                                                                                         | 0.33         | .Q         |                                    | •                                                               | • | •    |
| 16.79                                          | 0.2432                                                                                         | 0.30         | .Q         |                                    |                                                                 |   |      |
| 16.92                                          | 0.2463                                                                                         | 0.27         | . Q        |                                    |                                                                 |   |      |
| 17.05                                          | 0.2491                                                                                         | 0.25         | Q          |                                    |                                                                 |   |      |
|                                                |                                                                                                | 0.23         |            | •                                  | •                                                               | • | •    |
| 17.18                                          | 0.2517                                                                                         |              | Q          | •                                  | •                                                               | • | •    |
| 17.32                                          | 0.2540                                                                                         | 0.21         | Q          | •                                  | •                                                               | • | •    |
| 17.45                                          | 0.2563                                                                                         | 0.20         | Q          |                                    |                                                                 |   |      |
| 17.58                                          | 0.2584                                                                                         | 0.19         | Q          |                                    |                                                                 |   |      |
| 17.71                                          | 0.2604                                                                                         | 0.18         | õ          |                                    |                                                                 |   | _    |
| 17.84                                          | 0.2623                                                                                         | 0.17         | Q          |                                    |                                                                 |   |      |
|                                                |                                                                                                |              |            | •                                  | •                                                               | • | •    |
| 17.98                                          | 0.2642                                                                                         | 0.17         | Q          | •                                  | •                                                               | • | •    |
| 18.11                                          | 0.2659                                                                                         | 0.15         | Q          | •                                  | •                                                               | • | •    |
| 18.24                                          | 0.2674                                                                                         | 0.13         | Q          |                                    |                                                                 |   |      |
| 18.37                                          | 0.2687                                                                                         | 0.12         | Q          |                                    |                                                                 |   |      |
| 18.50                                          | 0.2700                                                                                         | 0.12         |            |                                    |                                                                 |   |      |
|                                                |                                                                                                |              | Q          | •                                  | •                                                               | • | •    |
| 18.63                                          | 0.2713                                                                                         | 0.11         | Q          | •                                  | •                                                               | • | •    |
| 18.77                                          | 0.2725                                                                                         | 0.11         | Q          |                                    |                                                                 |   |      |
| 18.90                                          | 0.2737                                                                                         | 0.11         | Q          |                                    |                                                                 |   |      |
| 19.03                                          | 0.2748                                                                                         | 0.10         | Q          |                                    |                                                                 |   |      |
|                                                |                                                                                                |              |            | •                                  | •                                                               | • | •    |
| 19.16                                          | 0.2759                                                                                         | 0.10         | Q          | •                                  | •                                                               | • | •    |
| 19.29                                          | 0.2770                                                                                         | 0.10         | Q          |                                    | •                                                               | • | •    |
| 19.42                                          | 0.2781                                                                                         | 0.10         | Q          |                                    |                                                                 |   |      |
| 19.56                                          | 0.2791                                                                                         | 0.09         | õ          |                                    | -                                                               | - |      |
| 19.69                                          | 0.2801                                                                                         | 0.09         |            | -                                  | -                                                               | • | -    |
|                                                |                                                                                                |              | Q          | •                                  | •                                                               | • | •    |
| 19.82                                          | 0.2811                                                                                         | 0.09         | Q          | •                                  | •                                                               |   | •    |
| 19.95                                          | 0.2821                                                                                         | 0.09         | Q          |                                    |                                                                 |   |      |
| 20.08                                          | 0.2830                                                                                         | 0.09         | Q          |                                    |                                                                 |   |      |
| 20.21                                          | 0.2839                                                                                         | 0.08         | õ          |                                    |                                                                 |   |      |
|                                                |                                                                                                |              |            | •                                  | •                                                               | • | •    |
| 20.34                                          | 0.2848                                                                                         | 0.08         | Q          | •                                  | •                                                               | • | •    |
| 20.48                                          | 0.2857                                                                                         | 0.08         | Q          | •                                  | •                                                               | • | •    |
| 20.61                                          | 0.2866                                                                                         | 0.08         | Q          |                                    |                                                                 |   |      |
| 20.74                                          | 0.2875                                                                                         | 0.08         | Q          |                                    |                                                                 |   | _    |
| 20.87                                          | 0.2883                                                                                         | 0.08         |            | •                                  | •                                                               | • | •    |
|                                                |                                                                                                |              | Q          | •                                  | •                                                               | • | •    |
| 21.00                                          | 0.2891                                                                                         | 0.08         | Q          | •                                  | •                                                               | • | •    |
| 21.14                                          | 0.2899                                                                                         | 0.07         | Q          |                                    |                                                                 |   |      |
| 21.27                                          | 0.2907                                                                                         | 0.07         | Q          |                                    |                                                                 |   |      |
| 21.40                                          | 0.2915                                                                                         | 0.07         |            |                                    | -                                                               | - | -    |
|                                                |                                                                                                |              | Q          | •                                  | •                                                               | • | •    |
| 21.53                                          | 0.2923                                                                                         | 0.07         | Q          | •                                  | •                                                               | • | •    |
| 21.66                                          | 0.2931                                                                                         | 0.07         | Q          |                                    |                                                                 |   |      |
| 21.79                                          | 0.2938                                                                                         | 0.07         | Q          |                                    |                                                                 |   |      |
| 21.92                                          | 0.2946                                                                                         | 0.07         | õ          |                                    |                                                                 |   |      |
| 22.06                                          | 0.2953                                                                                         | 0.07         | Q          | •                                  | •                                                               | • | •    |
|                                                |                                                                                                |              |            | •                                  | •                                                               | • | •    |
| 22.19                                          | 0.2960                                                                                         | 0.07         | Q          | •                                  | •                                                               | • | •    |
| 22.32                                          | 0.2967                                                                                         | 0.06         | Q          |                                    |                                                                 |   |      |
| 22.45                                          | 0.2974                                                                                         | 0.06         | Q          |                                    |                                                                 |   |      |
| 22.58                                          | 0.2981                                                                                         | 0.06         | õ          |                                    |                                                                 |   |      |
|                                                | 0.2988                                                                                         |              |            | •                                  | •                                                               | • | •    |
| 22.72                                          |                                                                                                | 0.06         | Q          | •                                  | •                                                               | • | •    |
| 22.85                                          | 0.2995                                                                                         | 0.06         | Q          | •                                  | •                                                               | • | •    |
| 22.98                                          | 0.3001                                                                                         | 0.06         | Q          |                                    |                                                                 |   |      |
| 23.11                                          | 0.3008                                                                                         | 0.06         | õ          |                                    | -                                                               |   |      |
| 23.24                                          | 0.3014                                                                                         | 0.06         | Q          |                                    | -                                                               | - | -    |
|                                                |                                                                                                |              |            | •                                  | •                                                               | • | •    |
| 23.37                                          | 0.3021                                                                                         | 0.06         | Q          | •                                  | •                                                               | • | •    |
| 23.51                                          | 0.3027                                                                                         | 0.06         | Q          |                                    | •                                                               | • | •    |
| 23.64                                          | 0.3033                                                                                         | 0.06         | Q          |                                    |                                                                 | • |      |
| 23.77                                          | 0.3040                                                                                         | 0.06         |            |                                    | -                                                               |   |      |
| 23.90                                          | 0.3046                                                                                         | 0.06         |            | -                                  | -                                                               | • | -    |
|                                                |                                                                                                |              |            | •                                  | •                                                               | • | •    |
| 24.03                                          | 0.3052                                                                                         | 0.06         |            | •                                  | •                                                               | • |      |
| 24.16                                          | 0.3055                                                                                         | 0.00         |            |                                    |                                                                 |   |      |
|                                                | 0.3055<br><br>JRATION(minu                                                                     |              |            |                                    |                                                                 |   |      |
|                                                | MATTON ( III TUR                                                                               |              | ate estim  |                                    |                                                                 |   | n15. |
| TIME DU<br>(Note:<br>an inst                   | 100% of Peak<br>antaneous t                                                                    |              |            | Dura                               | tion                                                            |   |      |
| TIME DU<br>(Note:<br>an inst<br>Percent<br>Pea | antaneous t<br>tile of Estin<br>ak Flow Rate                                                   | mated        |            | (min<br>====                       | utes)<br>=====                                                  |   |      |
| TIME DU<br>(Note:<br>an inst<br>Percent<br>Pea | antaneous t<br>le of Estin<br>k Flow Rate                                                      | mated        |            | (min<br>====                       | utes)                                                           |   |      |
| TIME DU<br>(Note:<br>an inst<br>Percent<br>Pea | antaneous t<br>tile of Estin<br>ak Flow Rate                                                   | mated        |            | (min<br>====<br>144                | utes)<br>=====<br>5.7                                           |   |      |
| TIME DU<br>(Note:<br>an inst<br>Percent<br>Pea | antaneous t<br>tile of Estin<br>k Flow Rate<br>0%<br>10%                                       | mated        |            | (min<br>====<br>144<br>8           | utes)<br>=====<br>5.7<br>6.9                                    |   |      |
| TIME DU<br>(Note:<br>an inst<br>Percent<br>Pea | antaneous t<br>tile of Estin<br>k Flow Rate<br>0%<br>10%<br>20%                                | mated        |            | (min<br>====<br>144<br>8<br>2      | utes)<br>=====<br>5.7<br>6.9<br>3.7                             |   |      |
| TIME DU<br>(Note:<br>an inst<br>Percent<br>Pea | cantaneous t<br>cile of Estin<br>ak Flow Rate<br>0%<br>10%<br>20%<br>30%                       | mated        |            | (min<br>====<br>144<br>8<br>2<br>1 | utes)<br>=====<br>5.7<br>6.9<br>3.7<br>5.8                      |   |      |
| TIME DU<br>(Note:<br>an inst<br>Percent<br>Pea | cantaneous t:<br>tile of Estin<br>lk Flow Rate<br>0%<br>10%<br>20%<br>30%<br>40%               | mated        |            | (min<br>====<br>144<br>8<br>2<br>1 | utes)<br>=====<br>5.7<br>6.9<br>3.7<br>5.8<br>7.9               |   |      |
| TIME DU<br>(Note:<br>an inst<br>Percent<br>Pea | cantaneous t.<br>cile of Estin<br>ak Flow Rate<br>0%<br>10%<br>20%<br>30%<br>40%<br>50%        | mated        |            | (min<br>====<br>144<br>8<br>2<br>1 | utes)<br>=====<br>5.7<br>6.9<br>3.7<br>5.8<br>7.9<br>7.9        |   |      |
| TIME DU<br>(Note:<br>an inst<br>Percent<br>Pea | cantaneous t:<br>tile of Estin<br>lk Flow Rate<br>0%<br>10%<br>20%<br>30%<br>40%               | mated        |            | (min<br>====<br>144<br>8<br>2<br>1 | utes)<br>=====<br>5.7<br>6.9<br>3.7<br>5.8<br>7.9<br>7.9<br>7.9 |   |      |
| TIME DU<br>(Note:<br>an inst<br>Percent<br>Pea | cantaneous t.<br>cile of Estin<br>ak Flow Rate<br>0%<br>10%<br>20%<br>30%<br>40%<br>50%        | mated        |            | (min<br>====<br>144<br>8<br>2<br>1 | utes)<br>=====<br>5.7<br>6.9<br>3.7<br>5.8<br>7.9<br>7.9        |   |      |
| TIME DU<br>(Note:<br>an inst<br>Percent<br>Pea | cantaneous t.<br>cile of Estin<br>ak Flow Rate<br>0%<br>10%<br>20%<br>30%<br>40%<br>50%<br>60% | mated        |            | (min<br>====<br>144<br>8<br>2<br>1 | utes)<br>=====<br>5.7<br>6.9<br>3.7<br>5.8<br>7.9<br>7.9<br>7.9 |   |      |

| ***************************************                                                                                                                                            |
|------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|
| NON-HOMOGENEOUS WATERSHED AREA-AVERAGED LOSS RATE (Fm)                                                                                                                             |
| AND LOW LOSS FRACTION ESTIMATIONS                                                                                                                                                  |
|                                                                                                                                                                                    |
| (C) Copyright 1989-2016 Advanced Engineering Software (aes)                                                                                                                        |
| Ver. 23.0 Release Date: 07/01/2016 License ID 1435                                                                                                                                 |
|                                                                                                                                                                                    |
| Analysis prepared by:                                                                                                                                                              |
|                                                                                                                                                                                    |
| THIENES ENGINEERING, INC.                                                                                                                                                          |
| 14349 FIRESTONE BLVD                                                                                                                                                               |
| LA MIRADA, CA 90638                                                                                                                                                                |
| 714-521-4811                                                                                                                                                                       |
|                                                                                                                                                                                    |
| ***************************************                                                                                                                                            |
|                                                                                                                                                                                    |
|                                                                                                                                                                                    |
| Problem Descriptions:                                                                                                                                                              |
| TEL JOB 3910                                                                                                                                                                       |
| 2-YEAR LOSS RATES                                                                                                                                                                  |
| PROPOSED CONDITION                                                                                                                                                                 |
|                                                                                                                                                                                    |
| *** NON-HOMOGENEOUS WATERSHED AREA-AVERAGED LOSS RATE (Fm)                                                                                                                         |
| AND LOW LOSS FRACTION ESTIMATIONS FOR AMC I:                                                                                                                                       |
| AND LOW LOSS FRACTION ESTIMATIONS FOR AME I.                                                                                                                                       |
| TOTAL 24-HOUR DURATION RAINFALL DEPTH = 2.05 (inches)                                                                                                                              |
| TOTAL 24-NOUR DURATION RAINFALL DEPTR = 2.05 (Inches)                                                                                                                              |
| SOIL-COVER AREA PERCENT OF SCS CURVE LOSS RATE                                                                                                                                     |
| SULL-CUVER AREA PERCENT OF SUS CURVE LOSS RATE                                                                                                                                     |
| TYPE         (Acres)         PERVIOUS AREA         NUMBER         Fp(in./hr.)         YIELD           1         12.70         10.00         32.(AMC II)         0.400         0.80 |
| 1 12.70 10.00 32.(AMC 11) 0.400 0.80                                                                                                                                               |
| TOTAL AREA (Acres) = $12.70$                                                                                                                                                       |
| IUIAL AREA (ACTES) = 12.70                                                                                                                                                         |
| AREA-AVERAGED LOSS RATE, Fm (in./hr.) = 0.040                                                                                                                                      |
| AREA-AVERAGED LOSS RAIE, Fill (III./III.) = 0.040                                                                                                                                  |
| ADEA AVERACED LOW LOSS ERACTION $\overline{V} = 0.100$                                                                                                                             |
| AREA-AVERAGED LOW LOSS FRACTION, $Y = 0.199$                                                                                                                                       |
|                                                                                                                                                                                    |

SMALL AREA UNIT HYDROGRAPH MODEL (C) Copyright 1989-2016 Advanced Engineering Software (aes) Ver. 23.0 Release Date: 07/01/2016 License ID 1435 Analysis prepared by: THIENES ENGINEERING, INC. 14349 FIRESTONE BLVD LA MIRADA, CA 90638 714-521-4811 \_\_\_\_\_ Problem Descriptions: TEI JOB 3910 2-YEAR HYDROGRAPH PROPOSED CONDITION \_\_\_\_\_ RATIONAL METHOD CALIBRATION COEFFICIENT = 0.90 TOTAL CATCHMENT AREA(ACRES) = 13.40 SOIL-LOSS RATE, Fm,(INCH/HR) = 0.040 LOW LOSS FRACTION = 0.199 TIME OF CONCENTRATION(MIN.) = 9.50 SMALL AREA PEAK Q COMPUTED USING PEAK FLOW RATE FORMULA ORANGE COUNTY "VALLEY" RAINFALL VALUES ARE USED RETURN FREQUENCY(YEARS) = 2 5-MINUTE POINT RAINFALL VALUE(INCHES) = 0.19 30-MINUTE POINT RAINFALL VALUE(INCHES) = 0.40 1-HOUR POINT RAINFALL VALUE(INCHES) = 0.53 POINT RAINFALL VALUE(INCHES) = 0.89 3-HOUR POINT RAINFALL VALUE(INCHES) = 1.22 6-HOUR 24-HOUR POINT RAINFALL VALUE(INCHES) = 2.05 \_\_\_\_\_ TOTAL CATCHMENT RUNOFF VOLUME(ACRE-FEET) = 1.71 TOTAL CATCHMENT SOIL-LOSS VOLUME(ACRE-FEET) = 0.58 TIME VOLUME Q 0. 5.0 10.0 15.0 20.0 (HOURS) (AF) (CFS) -----\_\_\_\_\_ 0.0000 0.0020 0.0061 0.0102 0.0143 0.0184 0.0226 0.0268 0.0268 0.00 Q 0.01 . . . . 0.17 0.31 Q . . 0.31 0.32 Q . 0.31 0.31 0.32 0.32 0.32 0.48 0.64 0 . . . Q . . . . 0.80 Q . . . . 0.96 Q . . . . 1.12 0.32 Q 0.0310 0.0352 1.27 0.32 0 . . . . 1.43 0.33 0 . . . 1.59 0.0395 0.33 õ . . . 0.0438 1.75 0.33 Q . . . 1.91 0.0482 0.33 Q . . 2.07 0.0525 0.0569 0.33 Q 2.22 0.34 0 . . 0.0614 0.0658 0.0703 2.38 0.34 0 . . . . 2.54 0.34 õ . . 2.70 0.34 Q . 2.86 0.0748 0.35 Q 0.0794 3.02 0.35 0 . . . . 3.17 0.0840 0.35 0 . . . 3.33 0.0886 0.35 Q . . . . 3.49 0.0933 0.36 Q . . 3.65 0.0980 0.36 Q . 0.1027 3.81 0.36 Q 3.97 0.1075 0.37 0 . . . . 4.12 0.1123 0.37 õ . . . . 4.28 0.1172 0.37 Q . . . . 4.44 0.1221 0.38 Q . . . 4.60 0 1270 0.38 0 0.1320 4.76 0.38 0 . . . . 4.92 0.1370 0.39 0 . . . . 0.1421 0.1472 5.07 0.39 Q 0.39 Q 0.39 Q 0.40 Q 0.40 Q . . . . 5.23 . 5.39 0.1524 . 5.55 0.1576

| 5.71<br>5.87<br>6.03 | 0.1629<br>0.1682<br>0.1735 | 0.40<br>0.41<br>0.41 | Q<br>Q<br>Q | •  |   |        |
|----------------------|----------------------------|----------------------|-------------|----|---|--------|
| 6.18<br>6.34         | 0.1789<br>0.1844           | 0.42<br>0.42         | Q<br>Q      |    | · | •      |
| 6.50<br>6.66         | 0.1899<br>0.1955           | 0.42<br>0.43         | Q<br>Q      |    |   |        |
| 6.82<br>6.97         | 0.2012                     | 0.43                 | Q           |    | • |        |
| 7.13                 | 0.2126                     | 0.44                 | Q<br>Q      |    | • |        |
| 7.29                 | 0.2185                     | 0.45<br>0.45         | Q<br>Q      | •  | • |        |
| 7.61<br>7.77         | 0.2303<br>0.2363           | 0.46<br>0.46         | Q<br>Q      | •  | • | •      |
| 7.93<br>8.08         | 0.2424<br>0.2486           | 0.47<br>0.47         | Q<br>Q      |    | • | •<br>• |
| 8.24<br>8.40         | 0.2549<br>0.2612           | 0.48<br>0.49         | Q<br>Q      |    |   | •      |
| 8.56<br>8.72         | 0.2676<br>0.2741           | 0.49<br>0.50         | Q<br>Q      | •  |   |        |
| 8.88<br>9.03         | 0.2807                     | 0.51                 | .Q<br>.Q    |    | • |        |
| 9.19                 | 0.2941                     | 0.52                 | .Q          |    | • |        |
| 9.35<br>9.51         | 0.3010<br>0.3080           | 0.53                 | .Q<br>.Q    | •  | • |        |
| 9.67<br>9.82         | 0.3150<br>0.3222           | 0.54<br>0.55         | .Q<br>.Q    | •  | • | •      |
| 9.98<br>10.14        | 0.3295<br>0.3369           | 0.56<br>0.57         | .Q<br>.Q    |    | • | •<br>• |
| 10.30<br>10.46       | 0.3445<br>0.3521           | 0.58<br>0.59         | .Q<br>.Q    |    |   | •      |
| 10.62<br>10.77       | 0.3599<br>0.3679           | 0.60<br>0.61         | .Q<br>.Q    | •  | • |        |
| 10.93                | 0.3760                     | 0.62                 | .Q          |    | • |        |
| 11.25                | 0.3926                     | 0.65                 | .Q<br>.Q    | •  | • |        |
| 11.41<br>11.57       | 0.4012                     | 0.67<br>0.67         | .Q<br>.Q    |    | • |        |
| 11.73<br>11.88       | 0.4189<br>0.4281           | 0.69<br>0.71         | .Q<br>.Q    | •  | • | •      |
| 12.04<br>12.20       | 0.4375<br>0.4480           | 0.73<br>0.88         | .Q<br>.Q    |    | • | •<br>• |
| 12.36<br>12.52       | 0.4598<br>0.4720           | 0.93<br>0.94         | .Q<br>.Q    |    |   | •      |
| 12.68                | 0.4846                     | 0.97                 | .Q<br>.Q    | •  | • |        |
| 12.99                | 0.5106                     | 1.02                 | . Q         |    | • |        |
| 13.15<br>13.31       | 0.5241<br>0.5380           | 1.04                 | . Q<br>. Q  | •  | • |        |
| 13.47<br>13.62       | 0.5524<br>0.5672           | 1.11<br>1.16         | . Q<br>. Q  |    | • |        |
| 13.78<br>13.94       | 0.5826<br>0.5985           | 1.19<br>1.25         | . Q<br>. Q  |    | • | ·      |
| 14.10<br>14.26       | 0.6151<br>0.6327           | 1.28<br>1.41         | . Q<br>. Q  | •  | • |        |
| 14.42<br>14.57       | 0.6515<br>0.6712           | 1.45<br>1.56         | . Q<br>. Q  | •  |   |        |
| 14.73<br>14.89       | 0.6920                     | 1.62                 | . Q<br>. Q  |    | • |        |
| 15.05                | 0.7377                     | 1.85                 | . Q         |    | • |        |
| 15.21<br>15.37       | 0.7635<br>0.7921           | 2.10                 | . Q<br>. Q  | •  | • |        |
| 15.52<br>15.68       | 0.8222                     | 2.34<br>2.70         | . Q<br>. Q  |    | • |        |
| 15.84<br>16.00       | 0.8999<br>0.9651           | 4.14<br>5.82         | . Q         | .Q | • |        |
| 16.16<br>16.32       | 1.1237<br>1.2653           | 18.41<br>3.23        | . Q         | •  | • | . Q    |
| 16.48<br>16.63       | 1.3018<br>1.3300           | 2.36<br>1.95         | . Q<br>. Q  |    |   |        |
| 16.79<br>16.95       | 1.3538<br>1.3747           | 1.68<br>1.50         | . Q<br>. Q  | •  | • |        |
| 17.11                | 1.3934<br>1.4103           | 1.37                 | . Q         |    | • |        |
| 17.42                | 1.4257                     | 1.13                 | . Q<br>. Q  | •  | • |        |
| 17.58<br>17.74       | 1.4401<br>1.4537           | 1.06                 | . Q<br>. Q  |    |   |        |
| 17.90<br>18.06       | 1.4665<br>1.4787           | 0.96<br>0.91         | .Q<br>.Q    | •  |   | •      |
| 18.22<br>18.38       | 1.4894<br>1.4985           | 0.72<br>0.68         | . Q<br>. Q  | •  |   |        |
| 18.53<br>18.69       | 1.5073<br>1.5157           | 0.66<br>0.63         | .Q<br>.Q    | •  | • | •      |
| 18.85                | 1.5238                     | 0.61                 | .Q          | •  |   |        |

•

2

| 19.01       1.5316       0.59       Q       .       .       .       .         19.17       1.5392       0.57       Q       .       .       .       .         19.33       1.5465       0.55       Q       .       .       .       . |  |
|-----------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|--|
|                                                                                                                                                                                                                                   |  |
| 19.33 1.5465 0.55 .Q                                                                                                                                                                                                              |  |
|                                                                                                                                                                                                                                   |  |
| 19.48 1.5535 0.53 .Q                                                                                                                                                                                                              |  |
| 19.64 1.5604 0.52 .Q                                                                                                                                                                                                              |  |
| 19.80 1.5671 0.50 .Q                                                                                                                                                                                                              |  |
| 19.96 1.5736 0.49 Q                                                                                                                                                                                                               |  |
| $20.12$ 1.5799 $0.48$ $\tilde{Q}$                                                                                                                                                                                                 |  |
| 20.27 1.5861 0.47 Q                                                                                                                                                                                                               |  |
| 20.43 1.5921 0.46 Q                                                                                                                                                                                                               |  |
| 20.59 1.5980 0.45 Q                                                                                                                                                                                                               |  |
| · · · · · · · · · · · · · · · · · · ·                                                                                                                                                                                             |  |
|                                                                                                                                                                                                                                   |  |
| 20.91 1.6094 0.43 Q                                                                                                                                                                                                               |  |
| 21.07 1.6149 0.42 Q                                                                                                                                                                                                               |  |
| 21.23 1.6203 0.41 Q                                                                                                                                                                                                               |  |
| 21.38 1.6257 0.40 Q                                                                                                                                                                                                               |  |
| 21.54 1.6309 0.39 Q                                                                                                                                                                                                               |  |
| 21.70 1.6360 0.39 Q                                                                                                                                                                                                               |  |
| 21.86 1.6410 0.38 Q                                                                                                                                                                                                               |  |
| 22.02 1.6460 0.37 Q                                                                                                                                                                                                               |  |
| 22.17 1.6508 0.37 Q                                                                                                                                                                                                               |  |
| 22.33 1.6556 0.36 $\tilde{Q}$                                                                                                                                                                                                     |  |
| 22.49 1.6603 0.36 $\tilde{Q}$                                                                                                                                                                                                     |  |
| 22.65 1.6649 0.35 Q                                                                                                                                                                                                               |  |
| 22.81 1.6695 0.35 Q                                                                                                                                                                                                               |  |
| 22.97 1.6740 0.34 Q                                                                                                                                                                                                               |  |
|                                                                                                                                                                                                                                   |  |
|                                                                                                                                                                                                                                   |  |
|                                                                                                                                                                                                                                   |  |
| 23.44 1.6871 0.33 Q                                                                                                                                                                                                               |  |
| 23.60 1.6913 0.32 Q                                                                                                                                                                                                               |  |
| 23.76 1.6955 0.32 Q                                                                                                                                                                                                               |  |
| 23.92 1.6997 0.31 Q                                                                                                                                                                                                               |  |
| 24.08 1.7037 0.31 Q                                                                                                                                                                                                               |  |
| <b>24.23 1.7058</b> 0.00 Q                                                                                                                                                                                                        |  |
|                                                                                                                                                                                                                                   |  |

TIME DURATION(minutes) OF PERCENTILES OF ESTIMATED PEAK FLOW RATE: (Note: 100% of Peak Flow Rate estimate assumed to have an instantaneous time duration)

| Percentile of E<br>Peak Flow F | <br>Duration<br>(minutes) |
|--------------------------------|---------------------------|
|                                | <br>=========             |
| 0%                             | 1444.0                    |
| 10%                            | 104.5                     |
| 20%                            | 28.5                      |
| 30%                            | 19.0                      |
| 40%                            | 9.5                       |
| 50%                            | 9.5                       |
| 60%                            | 9.5                       |
| 70%                            | 9.5                       |
| 80%                            | 9.5                       |
| 90%                            | 9.5                       |