

Attachment I

Hydrology Report

Pura Vineyards Project Ground Water Hydrology Report



FEBRUARY 2022

HYDROGEOLOGICAL REPORT

PURA VINEYARDS

KELSEYVILLE, LAKE COUNTY, CALIFORNIA

Prepared for:

Pura Industries
100 Shoreline Hwy, Bldg B. Ste. 100
Mill Valley, CA 93941

Prepared By:

Kimley»Horn

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Kimley-Horn Project No. 197456001

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1.0 INTRODUCTION

The following *Hydrogeologic Report* was prepared to document the subsurface hydrogeologic conditions and groundwater availability within the vicinity of the Pura Vineyards (“Vineyard” or “project area”) (**Figure 1**). The project area is located southeast of Kelseyville, CA and is comprised of 5 contiguous parcels totaling 314.8 acres. The Lake County property appraiser identifies the project area parcels as APNs 007-018-02, 007-018-04, 007-018-11, 007-029-04, and 007-029-05. Pura Vineyards intends to replace approximately 14.85 acres of vineyards on the Site with 14.85 acres of cannabis cultivation. The remaining vineyards on the Site are intended to remain in production and independent of the proposed cannabis production.

Lake County Board of Supervisors Ordinance 3106 specifies that due to the on-going drought conditions throughout the County, land use approval is contingent upon demonstrating that sufficient groundwater quantities are available for the intended land use. The proposed commercial cannabis production facility (cannabis facility) will occupy parcels numbers 007-029-04 and 007-029-05. The remaining parcels (007-018-02, 007-018-04, and 007-018-11) will be used to meet Lake County’s requirement that 20 acres of land be set aside for every acre (1-acre) of cannabis cultivation. Together, the commercial cannabis production facility and the additional parcels comprise the project area. The cannabis facility has a projected total outdoor canopy area of 646,820 square feet (sqft) or approximately 14.84 acres.

1.1 WATER USE DEMAND ESTIMATES

Water use demand for the cannabis facility varies and is governed by the life stage of the current crop. Early in the growing season, when the plants are young, a maximum daily water use demand for cultivation is approximately 25,000 gallons per day (GPD). During the summer months, when the local temperatures increase and plants mature, the maximum daily water use demand for cultivation at the cannabis facility is estimated to be up to 375,000 GPD. During a single growing season, the cannabis facility is expected to use 25,652,000 gallons of groundwater each year, which equates to approximately 78.72 acre feet/year (AF/year). Additional water use at the cannabis facility for non-cultivation operations is estimated to be approximately 720,720 gallons per year (gpy) or roughly 2.21 AF/yr. The total water use demand for all facility operations equates to 26,372,720 gpy or 80.93 AF/yr.

1.2 EXISTING ON-SITE WATER WELLS

Kimley-Horn was provided a well completion report for an existing water well located on the project site. The well is located on APN 007-029-05 and is identified as WE-1664. WE-1664 (on-site production well) was constructed in April 1999 and completed to a depth of 635 feet with an 8.32-inch casing. A review of Water Well Completion Reports (WWCR) by California Department of Water Resources (CDWR) identified an additional well (western well) on the western portion of the project area. It is Kimley-Horn’s understanding the western well will not be utilized to meet the demands of the proposed cannabis facility. The western well is located on APN 007-018-02 and is identified by permit number WE-4585. This 6-inch diameter domestic supply well was completed on June 5, 2015 and has a total depth of 593 feet. The approximate well locations are depicted on **Figure 2**. PDFs of the well completion report is included in **Appendix A**. Lithology and construction information for the on-site wells are provided in **Exhibit 1**.

In 2020, Russ and Cramer Enterprises conducted a specificity capacity test to evaluate the yield of well WE-1664. The corresponding drawdown data is presented in **Appendix B**.

Additional water wells in the vicinity of the project area are discussed in **Section 2.9**.

2.0 HYDROGEOLOGIC SETTINGS

The following is a discussion of the localized hydrogeologic setting in the vicinity of the Vineyard.

2.1 AQUIFER IDENTIFICATION

According to the March 2006 *Lake County Groundwater Management Plan (LCGMP)*, completed for Lake County Watershed Protection District (LCWPD) the Pura Vineyards site is underlain by the Clear Lake Volcanics and to a lesser degree the Big Valley Groundwater Basin (**Figure 3**). The two existing wells on the Site were completed into the Clear Lake Volcanics. The Clear Lake Volcanics and Big Valley Groundwater Basin are further discussed below.

2.2 SURFACE AND SUBSURFACE GEOLOGY

The landscape of Lake County is dominated by Mt. Konocti, a dormant volcano, which is apart of the Clear Lake Volcanic Field. The Pura Vineyards Site is located within the Clear Lake Volcanic Field on the western flank of Mt. Konocti. The geology in the immediate area of the Site consists of a complex of faulted igneous rocks from late-Pliocene to early Holocene volcanic activity (**Figure 4**). The US Geological Survey (USGS) has mapped faults across the Site, which are depicted on **Figure 4**. The northwest to southeast trending fault located on the western boundary of the Site is known as the Big Valley Fault. Further discussion of the geologic units and tectonic features underlying the Pura Vineyards Site is provided in the following sections.

2.2.1 *Dacite of Benson Ridge (Pleistocene) (Hearn) (dbr) 220.09 acres*

Volcanic flows resulting in dacite containing biotite. Cooling of the dacite occurred gradually resulting in the formation of distinct crystals. Contains inclusions up to 4 feet in diameter. These flows originated from the South Peak and possibly additional vents on Benson Ridge and east of Shaul Valley. The maximum thickness of this unit is 980 feet.

2.2.2 *Rhyolite of Cole Creek (Pleistocene) (Hearn)(rcc) 49.85 acres*

Volcanic flows of rhyolite containing biotite. This rhyolite is concentrated in fine-grain volcanic rocks and ash and has a maximum exposed thickness of 260 feet.

2.2.3 *Colluvium (Holocene) (Hearn) (co) 30.69 acres*

Slope deposits of silt, sand, and coarser pieces of older rocks. This unit is only mapped in areas where extensive or overlies a critical contact of bedrock units.

2.2.4 *Flows and Domes (Hearn) (dof) 6.34 acres*

Characterized by low viscosity volcanic flows and high viscosity volcanic domes.

2.2.5 *Alluvium (Holocene) (Hearn)(al) 5.08*

Flood-plain, channel, and lake deposits of clay, silt, sand, and gravel. Locally may include youngest part of the basin deposits of Clear Lake.

2.2.6 *Kelsey Tuff Member (named by Rymer1 1981, formerly aquifer ash of Hearn and others, 1976) (Hearn) (kk) 0.95 acres*

The upper section of the Kelsey Tuff Member consists of approximately 4 feet of ash, small volcanic rocks, and vesicular andesite. The lower section consists of 1.5 feet of clay and silt. In the Shaul Valley, the lower part contains subangular to subrounded fragmented dacite up to 1 foot in diameter. It is speculated the source vent for the volcanic rock was a cinder cone in the vicinity of Mount Konocti. The Kelsey Tuff Member occurs roughly 100 to 130 feet beneath the eroded top of the Kelseyville Formation. It is classified as a major aquifer as deep as 230 feet below a majority of the southern Big Valley (Soil Mechanics and Foundation Engineers, Inc. 1967). The total outcrop thickness of the Kelsey Tuff Member is between 1 and 6 feet.

2.2.7 Kelseyville Formation, undivided (named by Ryner, 1981; includes pyroclastic and lake deposits of Shaul Valley area of Hearn and others, 1976) (Pleistocene) (Hearn)(k) 0.66 acres

Fluvial deposits originating from lakes and rivers and consist of all grain sized from ash to cobbles. Fractured rock is predominantly from Franciscan assemblage rocks and serpentinite with minor amounts of dacite. This formation was initially deposited in an ancestral Clear Lake basin and is likely from 0.35 and 0.45 Ma. The thickness of the Kelseyville Formation is approximately 1275 feet.

2.2.8 Andesite west of Shaul Valley (Pleistocene) (Hearn) (aws) 0.60 acres

Bomb and block tephra, small flows, and dikes of sparsely porphyritic andesite. Vented from the dikes that cut the rhyolite of Cole Creek (rcc) and rhyodacite of Mount Olive. Vesicular blocks of this andesite, up to 1 foot in diameter are 5-10 percent of the mudflow deposit of mixed biotite rhyolite and andesite that overlies the rhyolite of Cole Creek (rcc). Maximum thickness about 5 meters.

2.2.9 Terrace deposits, undivided (Pleistocene) (Unit 2) (Hearn)(t₂) 0.54 acres

Comprised predominantly of pebble to boulder sized material with minor amounts of sand. Four terraces from the Pleistocene, between 11,700 to 2.5 MA were mapped in riverine systems in the vicinity of the project area. In Cole Creek, the gravel is a mixture of volcanic rock and erosion tolerant gravels from the Kelseyville Formation. The Terrace deposits have a maximum thickness of 16 feet.

2.2.10 Big Valley Fault

According to the USGS, the Big Valley Fault crosses the southern and western portions of the project area (**Figure 4**). This fault originated in the late Quaternary period and is reportedly well constrained and has a reported slip rate of 0.2 to 1.0 millimeter per year (mm/year). Within the last 200 years displacement along the fault has reportedly occurred in the vicinity of the Pura Vineyards Site.

2.3 SURFACE SOILS

According to the United States Department of Agriculture (USDA) Natural Resources Conservation Service (NRCS), there are six (6) different types of soil across the Vineyard Site (**Appendix C**). A concise description of the soil types is provided below.

1 – Benridge-Konocti association (112): The Benridge-Konocti association consists of well drained, high runoff class soil derived primarily from volcanic ash. These soils have 15 to 30 percent slopes with an average depth to water greater than 80 inches and are not considered prime farmland.

2 – Benridge-Konocti association (113): The Benridge-Konocti association soils are well drained and commonly found within high runoff areas. Volcanic ash is the parent material for the soil, which is not classified as prime farmland.

3 – *Bottlerock-Glenview-Arrowhead complex*: The Bottlerock-Glenview-Arrowhead complex has 30 to 50 percent slopes and is not classified as prime farmland. The soils are reportedly well drained and in the very high runoff class. Soils in this series are derived from weathered obsidian.

4 – *Kidd-Forward complex*: The Kidd-Forward complex is not classified as prime farmland. Soils in this series contain 5 to 30 percent slopes and are derived from weathered rhyolite. These soils are reportedly are well drained and runoff is low.

5 – *Konocti-Benridge complex*: The Konocti-Benridge complex consists of soils derived from weathered andesite. These soils have slopes from 50 to 75 percent, are considered well drained, and have a runoff classification of high. The soils in the Konocti-Benridge complex are determined to not be prime farmland.

6 – *San Joaquin variant fine sandy loam*: The San Joaquin variant is a fine sandy loam complex that is well drained and determined to have a medium runoff class. These soils are not considered prime farmland and have slopes from 0 to 5 percent. Additionally, these soils originated from volcanic rock alluvium.

2.4 SUBSURFACE HYDROGEOLOGY

The Pura Vineyard is predominantly located within the Clear Lake Volcanics which is where the existing on-site production well is located (**Figure 2**). The Big Valley Groundwater Basin comprises the southwestern corner of the site and constitutes approximately 7% of the total project area. According to the *Lake County Groundwater Management Plan*, the amount of groundwater available within the Clear Lake Volcanics is highly variable and depends on the size, openness, frequency, and interconnection of fractures and joints encountered in the formation.

The Pura Vineyards Site lies between two mapped fault systems, the Big Valley Fault to the west and the Konocti Bay Fault System to the east. The Big Valley Fault crosses the western and southern portions of the Vineyards (approximately 524 feet west of well WE-1664) while the Konocti Bay Fault System is located approximately 0.7 miles east and consists of multiple faults. A third fault mapped by the USGS traverses the central portion of the Site approximately 0.4 miles north of well WE-1664. Little to no detailed information is available regarding this third fault.

The regional faulting affects the localized hydrogeology. The fractured bedrock results in secondary porosity within the water-bearing units. Additionally, the faults can create hydrogeologic boundary conditions that dictate localized groundwater flow regimes.

2.5 CLIMATE DATA

The nearest weather station with historical climatological data is located in Clearlake, according to the Western Regional Climate Center (WRCC). Annual average precipitation at the Clearlake station is approximately 27.48 inches per year based on data collected from October 1954 to June 2016. Approximately 720.9 AF/year of precipitation is anticipated to fall on the project area during a normal year. Drought conditions have dominated the project area and surrounding areas over recent years. Kimley-Horn assumes 60 percent of normal rainfall during drought conditions. This equates to 432.5 AF/year of rainfall on the project area during drought conditions.

Appendix A of Title 23 of the California Code of Regulations (23 CCR), Chapter 2.7 provides tables for the calculation of annual potential evapotranspiration for different areas of California. The Lower Lake area of Lake County where the Vineyards is proposed, is estimated to have a mean annual potential evapotranspiration of approximately 45.4 inches per year.

2.6 PRODUCTION ZONE

The fractured rock within the Clear Lake Volcanics, between the Big Valley Fault and the Konocti Bay Fault Zone, comprises the primary aquifer beneath the Pura Vineyards Site. Boring logs for well MW-031 associated with the Benson Ridge Facility (**Section 3.1**) document the localized lithology in the project area as fractured dacite to a depth of at least 455 feet (1,402 feet NAVD 88). Based on the fractured nature of the geologic units above and comprising the aquifer, the aquifer is presumed to be unconfined. The thickness of the Clear Lake Volcanics varies and is underlain by the Franciscan Formation. Near Mount Konocti, approximately 2.1 miles east of the project area, the Clear Lake Volcanics are over 4,000 feet thick, according to the 2006 LCGWMP. Additionally, a well drilled near the intersection of Red Hills Road and Highway 29, approximately 3.6 miles southeast of the project site, the formation is 1,600 feet thick. A water well construction log for Test Hole #1 located approximately 2.1 miles southeast of the on-site production well indicated the Clear Lake Volcanics appear to be greater than 700 feet thick. Test Hole #1 is roughly located at a similar elevation as the on-site production well.

According to the Lake County Groundwater Management Plan (2006), “...groundwater in the Clear Lake Volcanics occurs primarily in fractures, joints, and within weathered zones that formed in between volcanic eruptions. Additionally, the amount of groundwater available to a well in the formation is highly dependent on the size, openness, frequency, and interconnection of fractures and joints encountered in the well. Therefore, the hydrogeologic properties of the Clear Lake Volcanics vary from one location to the next.

2.7 WATER BEARING ZONE THICKNESS

According to information from well construction logs from deep wells constructed on and around the Site (**Appendix A**), the Clear Lake Volcanics formation at the Pura Vineyards site is greater than 635 feet thick. At the Site, the static water level is approximately 500 feet below land surface. According to 6 well construction logs summarized in **Table 2**, average thickness of the aquifer is 101 feet thick. Therefore, a conservative estimate of the aquifer thickness is approximately 100 feet at the Pura Vineyards Site.

2.8 CONFINING LAYERS

The Clear Lake Volcanics comprise the underlying geologic unit and aquifer. The aquifer is presumed to be unconfined due to the fractured nature of the volcanics and faulting in the local area. The Franciscan Formation forms the fractured bedrock in the majority of Lake County (LCGWMP 2006).

2.9 ON-SITE AND NEARBY WELLS

Kimley-Horn reviewed the Well Completion Report Map Application available through the California Department of Water Resources (DWR). Registered wells are not individually georeferenced in the map application. Instead, they are referenced by section, township, and range. Well density for the Sections at and surrounding the Site are outlined in the table below:

**Table 1
NEARBY WELLS**

Section, Township, and Range	Number of Registered Wells	Number of Production Wells	Number of Domestic Wells
S25 T13N R09W	33	1	11
S24 T13N R09W	14	1	11
S23 T13N R09W	20	3	16
S19 T13N R08W	6	NA	1
S26 T13N R09W	26	1	25
S30 T13N R08W	9	1	2

Wells listed in this database include domestic, production, agricultural, and dry wells. This includes wells located on the Pura Vineyard property, such as WE-4585 and WE 1664. WE-4585 is located on the western side of the project area and has a total depth of 593 feet. The reported static water level in the well is 405 feet. Testing performed in August 2015 estimated the yield of the well to be 25 gallons per minute. This well will not be used for cannabis cultivation. Well WE-1664 was installed in 2020 on the southern portion of the project area. The well was constructed to a depth of 598 feet and has a reported static water level of approximately 500 feet. The specific capacity estimated for the well is 721.9 feet³/day/foot.

Well WE-3486, located approximately 1,230 feet north of the project area, has a total depth of 500 feet and a static water level of 380 feet based on the well completion report (**Appendix A**). Locations of the four (4) identified wells were determined based on location diagrams included in the completion reports (**Appendix A**). Wells with a completion depth of 300 feet or greater bls and whose approximate location could be determined are depicted on **Figure 5**. Also depicted on **Figure 5** are shallow monitoring wells located on the Benson Ridge Facility.

Kimley-Horn also reviewed available water well information from the DWR sustainable groundwater management act (SGMA) Data Viewer and the California Water Boards Ground Ambient Monitoring and Assessment Program (GAMA) online databases. Twelve (12) water wells associated with the Benson Ridge Facility (**Section 3.2**), which is less than 0.25 miles to the east of the project area. These wells range in depth from 11 feet to 435 feet. Well completion logs able to be obtained for these wells are included in **Appendix A**.

Two (2) water wells were identified on the SGMA Data Viewer online portal in the immediate vicinity of the project area. Well completion report WCR1979-004728 is georeferenced on the northern corner of the project area. However, the well completion report (**Appendix A**) states this was a dry well with a total depth of 263 feet bls. Additionally, the location of the well depicted in the diagram provided in the completion report cannot be definitively determined but the approximate location appears to be contradictory of the georeferenced location. The second water well is georeferenced on the southern adjacent property and is associated with well completion report WRC1979-004726. This well is an observation well and was completed to a depth of 159 feet bls. Depth to water information was not provided in the well completion report.

2.10 LOCAL STREAMS OR SPRINGS

Data from the United States Fish and Wildlife Service (USFWS) and the National Wetland Inventory (NWI) confirmed the presence wetlands, ponds, and riverine systems are located in the vicinity of the project site (**Figure 6**). A freshwater emergent wetland is located approximately 1,900 feet east of the project site. A freshwater pond is located approximately 1,050 feet southwest of the Pura Vineyard Site. A freshwater forested / shrub wetland associated with McIntire Creek, is located approximately 1,060 feet south of the

Vineyard. A riverine system is located to the south, southwest, and west of the vineyards and is associated with the Cole Creek. Wetlands, lakes, ponds, riverine systems, and other mapped features in the NWI database are not located on the project site.

3.0 SURROUNDING DEVELOPMENT

The project area is situated within an area consisting of rural residential and agricultural development. A singular regulated facility, identified as the Benson Ridge Facility, is located on the eastern adjacent property.

3.1 SURROUNDING LAND USE

Properties north of the Pura Vineyards Site consist of orchards, vineyards, and rural land use. The Benson Ridge Facility is located on the eastern adjacent property and is followed by undeveloped vegetated land. Rural land use and a small greenhouse cultivation operation are located to the south of the proposed facility and are followed by State Highway 29 South. Rural land use is predominant to the west of the Pura Vineyards Site and is followed by State Highway 29 South.

3.2 BENSON RIDGE FACILITY

The Benson Ridge Facility, located at 7620 Highway 29, Kelseysville, CA, 95451, is listed in the California Department of Toxic Substance Control (DTSC) database. According to DTSC, this facility received liquid, sludge, and solid waste from the geothermal industry in the Geysers area. A Waste Consolidation Area, located at the facility, is used to contain roughly 103,000 cubic yards of waste, subsoils, and solidification agents. Since December 1992, the facility has been in post-closure Detection and Corrective Action Monitoring. Currently, semi-annual groundwater monitoring is conducted in March and September at the facility. Shallow and deep groundwater bearing zones are monitored and are associated with the corrective action and detection programs respectively.

On August 21, 2021, a *Semi-Annual Groundwater Monitoring Report* was completed for the Benson Ridge Facility. Groundwater samples collected during the March 2021 sampling event from the perched groundwater zone (corrective action program) exceeded the background concentration limits (CL) for sulfate, total dissolved solids, boron, and sodium. As the perched zone monitoring network is also used as recovery wells, static conditions did not exist and groundwater flow cannot be inferred. However, data collected prior to the sampling event suggests the perched groundwater flows to the south. This is consistent with topographic gradient.

Analytical data for groundwater samples collected from the deep monitoring wells was compared to the CL for their respective wells. The report stated “*Over thirty years of groundwater monitoring at the Benson Ridge facility have shown no impacts to the deep zone groundwater. It would be appropriate that the deep zone monitoring program could be reduced or discontinued and the wells designated for beneficial use*”. Groundwater flow in deep water bearing zone is calculated to be to the south.

Groundwater contamination plume?

Well construction and boring logs for selected wells associated with the Benson Ridge Facility monitoring network are included in **Appendix A** and discussed in **Section 2.4** and **Section 6** and included in **Exhibit 2**.

4.0 CUMULATIVE IMPACT AREA

Water for the proposed cannabis cultivation will be sources from on-site water wells. The Cumulative Impact Area (CIA) for this investigation is defined as the area influenced by the projected groundwater use and existing groundwater demand within the vicinity of the Pura Vineyard project. Local topography, hydrology, hydrogeology, and existing groundwater usage are important components when determining the CIA.

The CIA for the Vineyard project was delineated based on the localized topography, and geology/hydrogeology. The northern boundary of the CIA was determined by topography and the location of a tributary to Cole Creek. The Konocti Bay Fault Zone mapped by USGS constitutes the eastern boundary of the CIA. The southern and western extents of the CIA are defined by the location of Cole Creek. The extent of the CIA is depicted on **Figure 7**. The delineated CIA encompasses an area of approximately 2,375 acres. Including the five Pura Vineyard parcels there are 92 parcels within the CIA. Portions of the Clear Lake Volcanics and the Big Valley Groundwater Basin are included within the CIA. As the Clear Lake Volcanics is the dominant component of the CIA, Clear Lake Volcanic aquifer characteristics were utilized for the analyses summarized in **Section 6.1**.

5.0 EXISTING AND PROJECTED GROUNDWATER USE

Kimley-Horn evaluated the current and projected water demand within the CIA. Water use demands for the proposed Vineyard were calculated by Kimley-Horn based on information provided by Pura Industries.

5.1 EXISTING PROJECT AREA WATER DEMAND

The project area was previously used as a vineyard for the cultivation of grapes. Approximately 15 acres of vineyard are being removed and replaced by the proposed cannabis facility.

5.2 CALCULATED WATER DEMAND

As stated in **Section 1.1**, the total water use demand for facility operations equates to approximately 26,372,720 gallons per year or 80.93-acre feet per year. This includes water demands for both cannabis cultivation and non-cultivation operations.

5.3 EXISTING OFF-SITE WATER DEMAND

The CIA encompasses all or portions of 87 off-site properties. These properties are utilized for a mixture of uses including single-family dwellings, vineyards, and orchards. It can be presumed that each of the 87 off-site properties is serviced by their own respective water well. The amount of groundwater extraction for off-site properties cannot be verifiably quantified. However, estimates can be extrapolated based on size of dwellings, property use, and application of usage rates for the identified development types (**Table 2**).

Land use for each parcel within the CIA was determined by aerial imagery. For estimation purposes, residential structures are surmised to be 3-bedroom houses. For parcels not completely within the CIA boundary, the total estimated water usage was included regardless of the land use distribution throughout the parcel. Agriculture on parcels within the CIA was observed to primarily consist of grape cultivation and orchard production. The agricultural production was not observed to cover the entirety of the parcels. However, the entire acreage of applicable parcels was used to calculate the existing water demand for the agricultural production.

5.4 PROJECTED OFF-SITE WATER DEMAND

Future water demand for undeveloped parcels was presumed to be equivalent to a 3-bedroom residence.

Table 2
Summary of Existing / Projected Groundwater Use

Description	Existing (acre-feet/year)	Future Development (acre-feet/year)	Total (acre-feet/year)
On-Site Groundwater Use			
Cannabis Production	0	78.72	78.72
Non-Production operations	0	2.21	2.21
Grape Cultivation ¹	30.7	-7.5 ⁵	23.2
Off-Site Groundwater Use			
Single Family Dwellings – Domestic Use ²	36	21	57
Single Family Dwellings – Nonessential Use ³	12	7	19
Grape Cultivation ¹	147.7	0	147.7
Orchard Dry Farming ⁴	1.9	0	1.9
Total Groundwater Use			
Totals	228.3	101.43	329.73

Notes:

¹: Usage rate of 0.5 AF/year per acre of grape cultivation (295.4 acres)

²: Usage rate of 0.25 AF/year per bedroom

³: Usage rate of 0.25 AF/year per dwelling

⁴: Usage rate of 0.01 AF/year per acre utilizing dry farming techniques (189.9 acres)

⁵: This accounts for the removal of 15-acres of current vineyard which will be replaced by proposed Pura Vineyards Site.

6.0 GROUNDWATER AVAILABILITY ANALYSIS

Kimley-Horn estimated the groundwater availability for the CIA based on the prevailing hydrogeologic conditions and the projected water use demands.

6.1 AQUIFER STORAGE CAPACITY

The LCWPD estimated the specific yield of the Clear Lake Volcanics to range from 0 to 15 percent. A conservative estimate of 7 percent was used in this analysis. The CIA encompasses a total area of 2,375 acres. Wells within the CIA which are presumed to target the lower water-bearing zone (>200 feet deep), based on well depth, were reviewed. The six (6) correspond wells are summarized on **Exhibit 2**. Approximate top of casing elevations were calculated with Google Earth Pro and topographic maps. Average static depth to water and aquifer depth is 385 feet and 486 feet respectively. Given the above parameters, the calculated storage capacity of the aquifer within the CIA is 16,792 AF. As stated in **Section 1.1**, the calculated water use demand of the Vineyard is 80.93 AF/year. The calculated water use of the Vineyard is less than one-half of a percent of the stored groundwater within the CIA. The total existing and projected water demand within the CIA, approximately 329.73 AF/year, is less than two (2) percent of the estimated groundwater in storage.

6.2 VINEYARD'S WATER BUDGET

To estimate the water balance of the project area, Kimley-Horn compared groundwater recharge to the calculated water use demand for the Vineyard. Precipitation is presumed to constitute the primary source of inflow into the underlying aquifer. The primary outflow of the aquifer is assumed to be evapotranspiration. Secondary sources of inflow and outflow to the groundwater are considered to be relatively equal. Based on the above assumptions, the below formula was used to calculate groundwater recharge beneath the project area.

According to the National Oceanic and Atmospheric Administration (NOAA) and the National Integrated Drought Information System (NIDIS), Lake County, CA is currently in severe drought and January 2022 was the 9th driest January on record over the past 128 years. During drought conditions, 60 percent of the average precipitation can be assumed.

$$\text{Recharge} = P - (ET_A + R + E_{CI} + S)$$

Precipitation (P)

As stated in **Section 2.5**, the Clearlake weather station recorded an average rainfall of 27.5 inches per year. Total annual precipitation over the project area is equivalent to 721.4 AF/year during a year with average precipitation and 432.9 AF/year during a year effected by drought.

Actual Evapotranspiration (ET_A)

Appendix A of Title 23 of the California Code of Regulations (23 CCR), Chapter 2.7, as stated in **Section 2.5**, determined Lower Lake area of Lake County is estimated to have a mean annual potential evapotranspiration of approximately 45.4 inches per year. This equates to an estimated 1,191 AF/year of potential evapotranspiration.

Kimley-Horn calculated actual evapotranspiration (ET_A) for the project area using a site specific model as described in *A Guide to Estimating Irrigation Water Needs of Landscape Plantings in California* (UC Cooperative Extension, 2000). Acreage of varying vegetation types were calculated using GIS. A landscape

coefficient was calculated for each vegetation type including the proposed cannabis production area. Based on the variability of the species coefficient depending on cannabis subtype, highly conservative estimates were used for the species and density coefficient. Each landscape coefficient was multiplied by the potential evapotranspiration to get landscape evapotranspiration (ET_L). ET_L was multiplied by acreages for the identified vegetation types to calculate ET_A for the project area. Actual evapotranspiration for the project area was calculated to be 135.65 AF/year.

For ease of calculation, conservative assumptions and coefficients were utilized. Assumptions made within the calculation include constant year-round evapotranspiration rates were assumed for the cannabis and grape production

Runoff (R)

Type curves for various surfaces were calculated by the Sonoma County Water Agency in the Flood Management Design Manual, March 2020 (FMDM, 2020) (**Appendix XX**). Based on soil data reviewed and summarized in **Section 2.3 (Appendix XX)**, the majority of the slopes across the project area are greater than 20 percent. For conservative estimates, the entire project area was assumed to be greater than 20 percent slopes. Based on the project area estimates, the run-off coefficient of 0.47 was determined by the FMDM. The annual precipitation volume was multiplied by the run-off coefficient to estimate the annual outflow run-off volume. The run-off volume for a year with average rainfall equates to 339.1 AF/year while 203.4 AF/year is estimated during years of drought.

Canopy Interception Losses (E_{ci})

Canopy interception loss, as defined by Helvey and Patric 1965, is *rainfall retained on standing vegetation and evaporated without dripping off or running down the stems*. Studies conducted by Helve and Patric excluded grassland and other land surfaces without tree canopy cover. The interception loss coefficient is multiplied by the average rainfall and drought conditions for areas over the Vineyard with canopy cover. Canopy interception loss within the project area equates to 12.75 AF/year during years with average rainfall and 8.46 AF/year during years with drought conditions.

Spring Flow (S)

Springs are not located within the project area. As such, spring flow discharge is not incorporated in the groundwater recharge analysis.

Water Budget Results

Table 3
Pura Vineyard's Water Budget

Description	Inflow/Outflow	Volume (acre-feet/year) Average Precipitation	Volume (acre-feet/year) Drought Conditions
Precipitation	Inflow	+721.4	+432.9
Actual Evapotranspiration	Outflow	-146.05	-146.05
Run-off	Outflow	-339.1	-203.4
Canopy Interception	Outflow	-12.75	-8.46
Springs	Outflow	0	0
Total		+223.5	+74.99

6.3 CIA'S WATER BUDGET

Groundwater recharge potential for the entirety of the CIA was calculated (minus the project area as this was calculated in Table 4). Conservative assumptions applied in the project area water budget calculations were similarly applied in the for figures within **Table 5**.

Table 4
CIA's Water Budget

Description	Inflow/Outflow	Volume (acre-feet/year) Average Precipitation	Volume (acre-feet/year) Drought Conditions
Precipitation	Inflow	+4,721.3	+2,832.8
Evapotranspiration	Outflow	-966.5	-966.5
Run-off	Outflow	-2,030.2	-1,217.1
Canopy Interception	Outflow	-129.49	-85.94
Springs	Outflow	0	0
Total		+1595.11	+563.26

7.0 WATER QUALITY

Groundwater quality in the Clear Lake Volcanics is unavailable according to the Lake County Groundwater Management Plan. However, the California Department of Health Services (DHS) provided information during the preparation of the *LCGWMP* which indicated iron, aluminum, and manganese were detected above surface water quality levels (SWQLs) in the Clear Lake Volcanics. The location of the groundwater samples with elevated concentrations was not provided.

Semi-annual groundwater monitoring is conducted at the Benson Ridge Facility on the eastern adjacent property. Groundwater monitoring is conducted on the perched and deep water bearing zones beneath the facility. The deep monitoring wells and the on-site production well roughly target the same water bearing zone. In 30 years of monitoring, the deep water bearing zone has never show signs of groundwater contamination. The perched water bearing zone is continuously pumped and discharged into lined basins at the facility.

8.0 WELL EVALUATION AND DRAWDOWN ANALYSIS

The on-site production well, WE-1664 was installed in April of 1999 to a depth of 598 feet below land surface. In May 2020, a specific capacity test was performed during which the well was pumped continuously at a rate of 225 gallons per minute (gpm) for 4.5 hours. During the test, the well experienced a maximum of 60 feet of drawdown. The corresponding specific capacity of the well was estimated to be 3.75 gpm per foot of drawdown. This data was used to estimate a transmissivity value for the aquifer of approximately 795 feet²/day.

The average water use demand for the project is approximately 72,250 gallons per day. This equates to approximately 50 gpm. Kimley-Horn used the Theis drawdown equation to estimate the drawdown and radius of influence for the pumping well based on the average daily demand (**Appendix D**). Drawdown in the well is estimated to be approximately 11 feet, which correlates with the estimated specific capacity. At a radial distance of 200 feet from the well, drawdown in the aquifer is estimated to be less than 1-foot.

9.0 CONCLUSIONS AND RECOMMENDATIONS

Kimley-Horn has prepared the following conclusions and recommendations for the proposed cannabis production facility, identified as Pura Vineyards, located approximately 2.5 miles southeast of Kelseyville, CA:

- Based on published hydrogeologic data for Clear Lake Volcanics, the deep aquifer will be able to meet the water use demands for the proposed cannabis production facility. We anticipate that the existing on-site production well installed south of the production facility is sufficient to meet the proposed water use demands.
- The current water use within the CIA is 228.3 AF/year. The future water use demand within the CIA which includes cannabis cultivation is 101.43 AF/year.
- The estimated groundwater availability of the CIA is 16,792 AF. The future water use demand accounts for 2% of the total groundwater availability in the CIA.
- Under drought conditions, the proposed groundwater demand for Pura Vineyards is approximately 12% of the total recharge available to the CIA (638.25).
- The proposed cannabis cultivation will result in a net increase in the water use demand for the CIA. The available groundwater within the CIA is capable of sustaining the proposed increase. Furthermore, it is not anticipated that the increased demands will adversely impact other legal users of the groundwater resource or sensitive environmental receptors.
- Pura Industries may want to install a second well in the future to provide redundancy for the irrigation system.

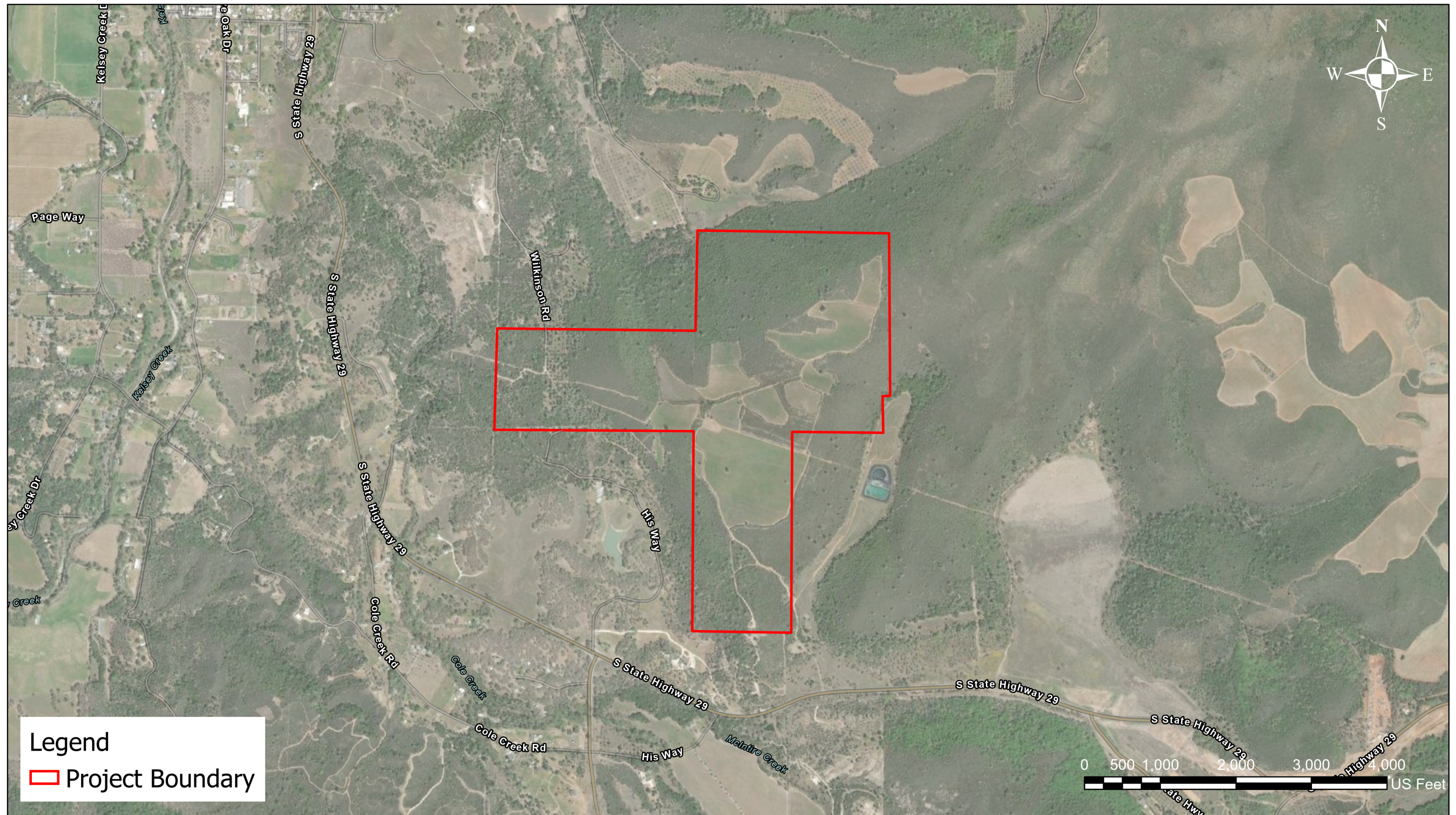
REFERENCES


Hearn B.C.Jr, J.M. Donnelly-Nolan, F.E. Goff, 1995 “*Geologic Map and Structure Sections of Clear Lake Volcanics, Northern California*” <https://pubs.usgs.gov/imap/2362/>

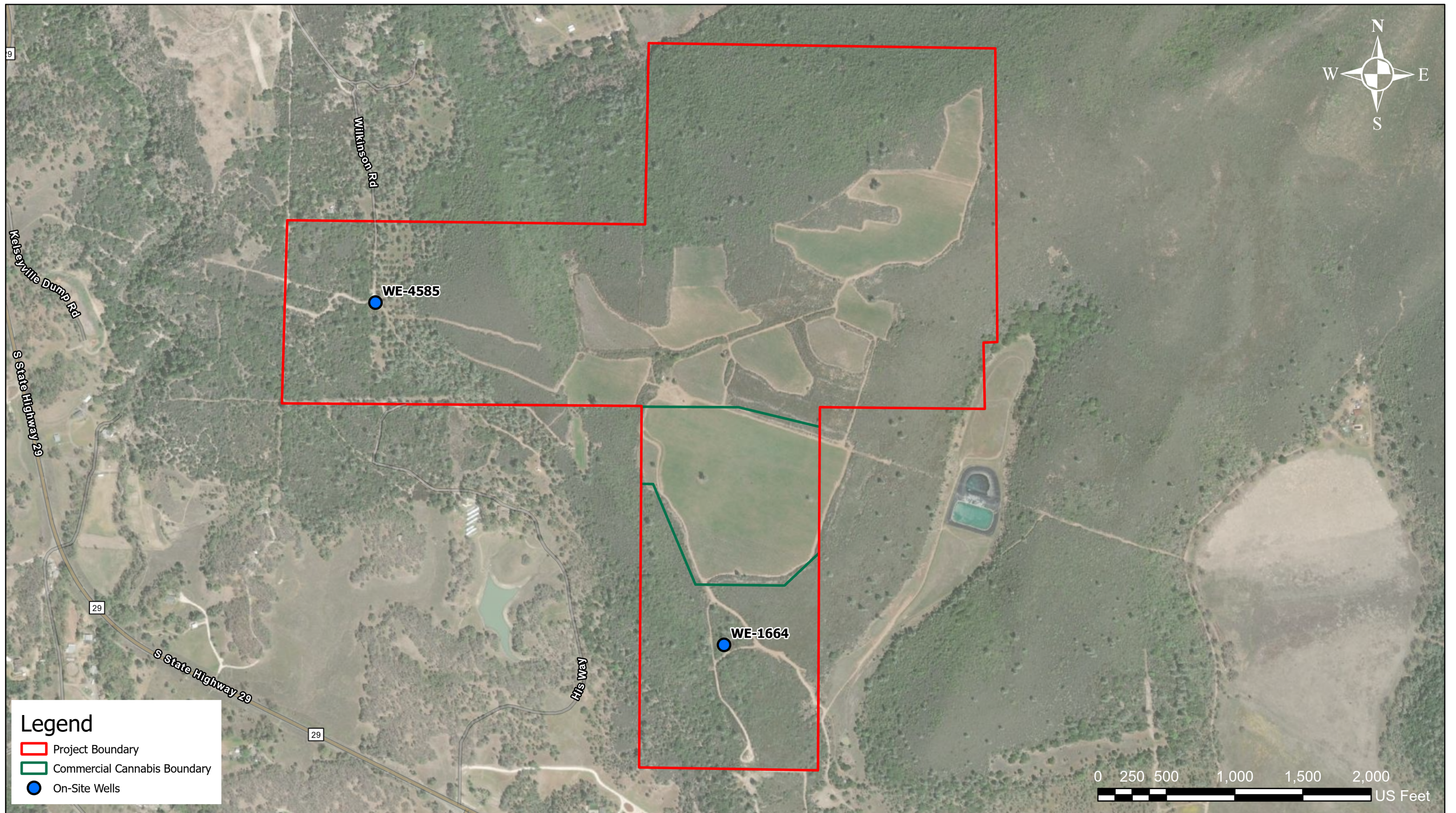
Domenico, P.A., F.W. Schwartz, 1990. *Physical and Chemical Hydrogeology*, John Wiley & Sons, New York, 824 p.

Helvey, J.D., J.H. Patric 1965. *Canopy and litter interception of rainfall by hardwoods of eastern United States*, Water Resources Research, Vol. 1, No. 2

FIGURES




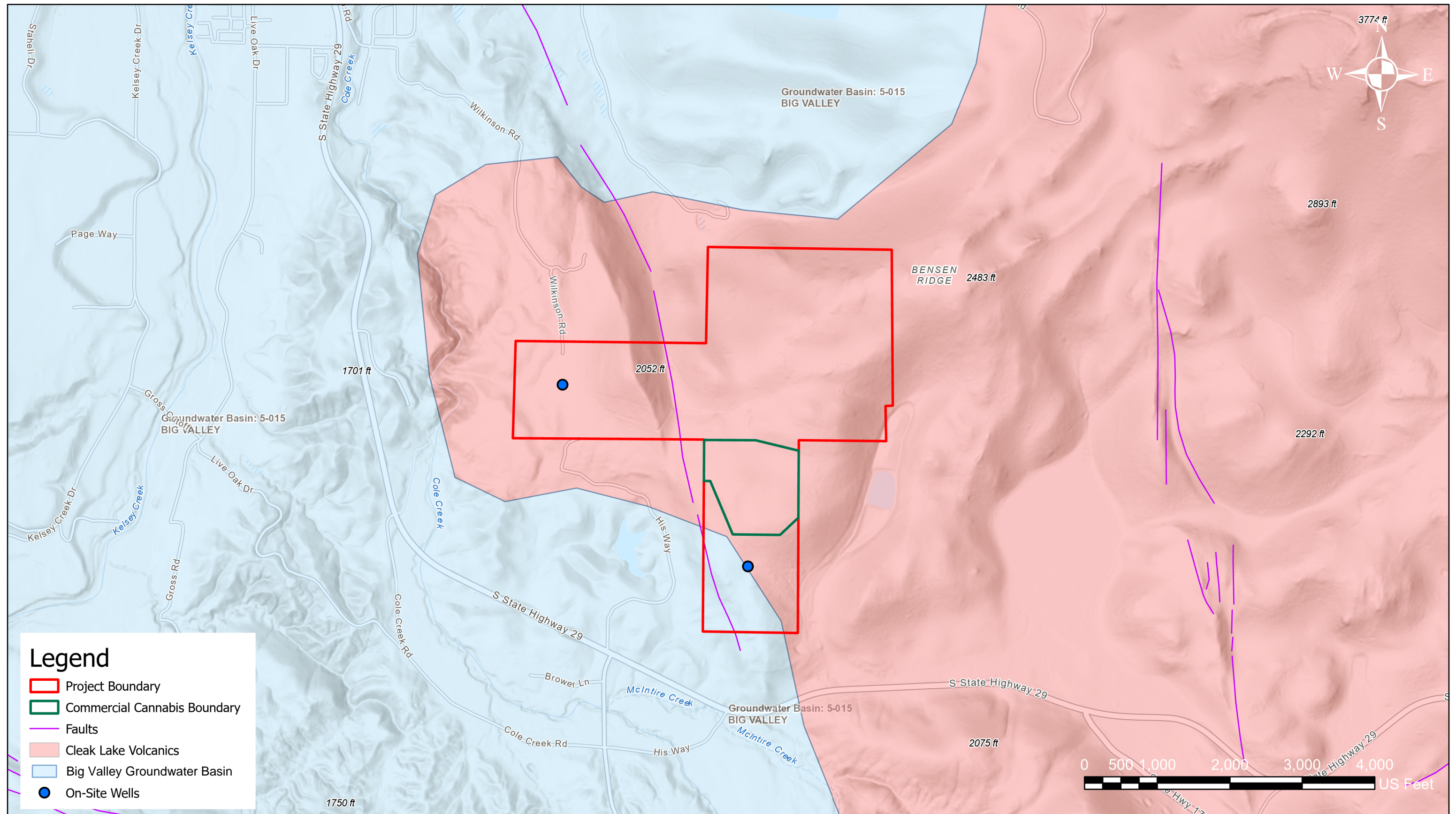
	Property Location Map Pura Vineyards Kelseyville, Lake County, CA		197456001
			Figure No. 1

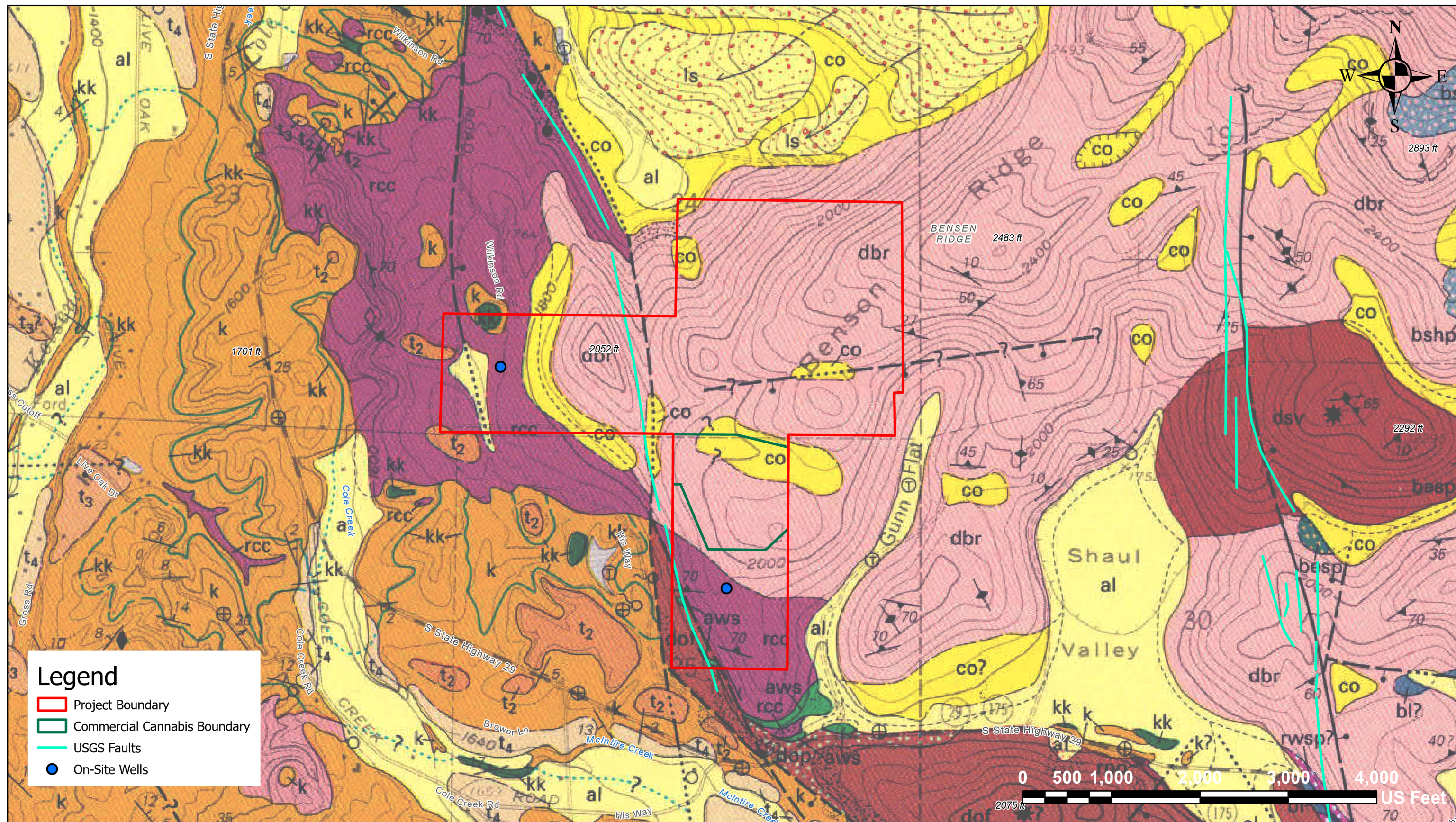


Legend

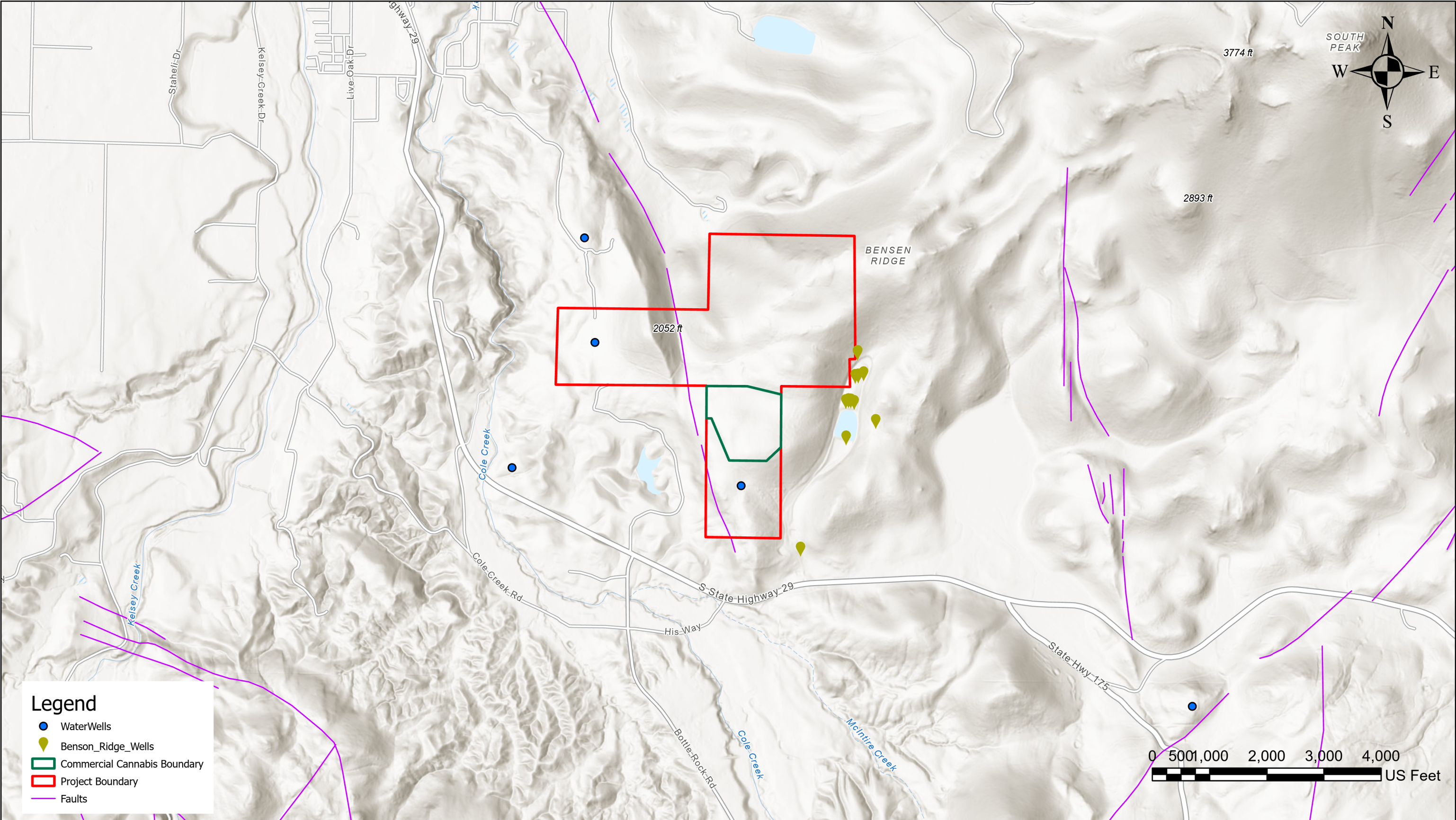
- ▭ Project Boundary
- ▭ Commercial Cannabis Boundary
- On-Site Wells

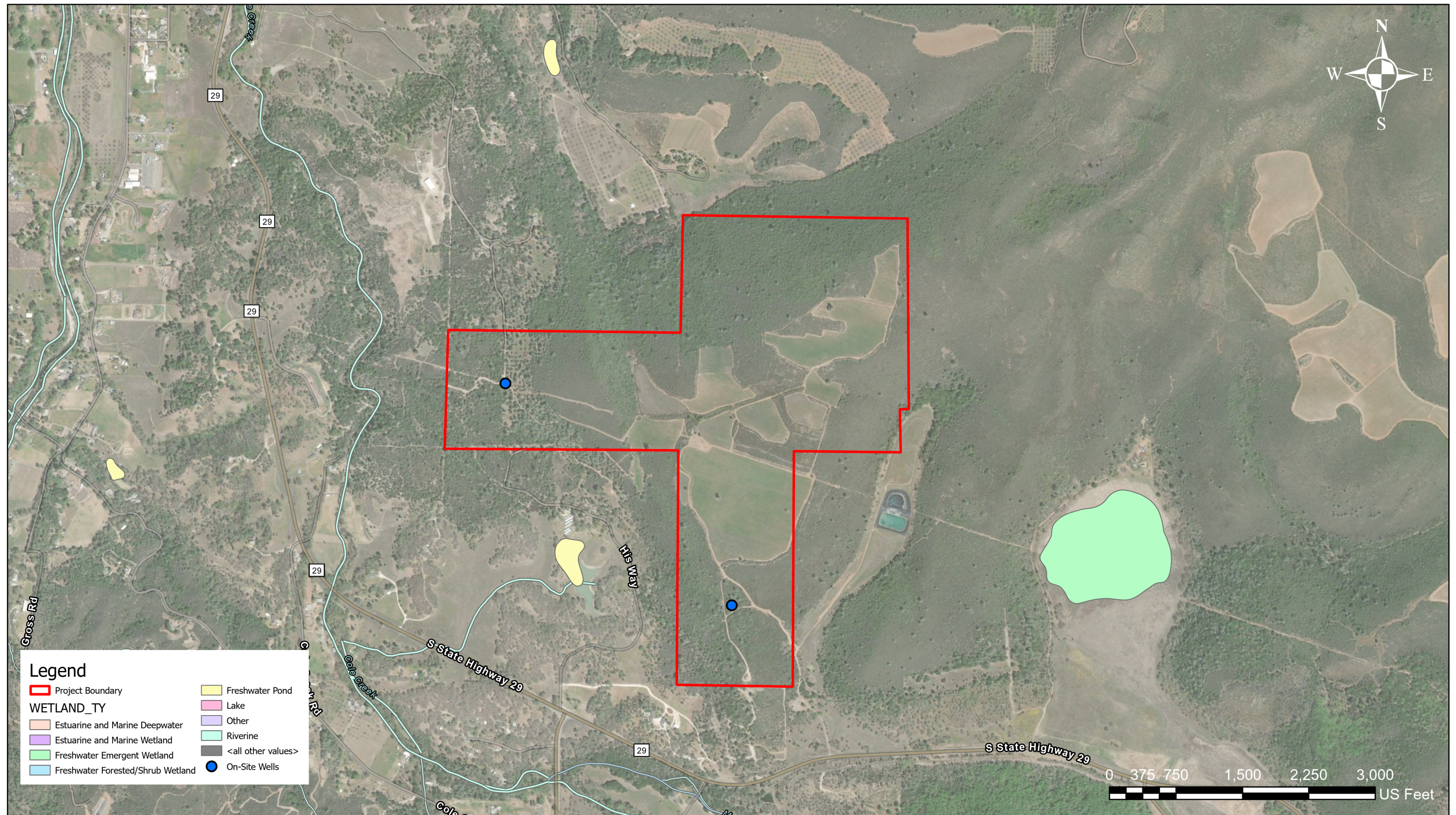
	Location of Existing On-Site Water Wells Pura Vineyards Kelseyville, Lake County, CA		197456001
			Figure No. 2

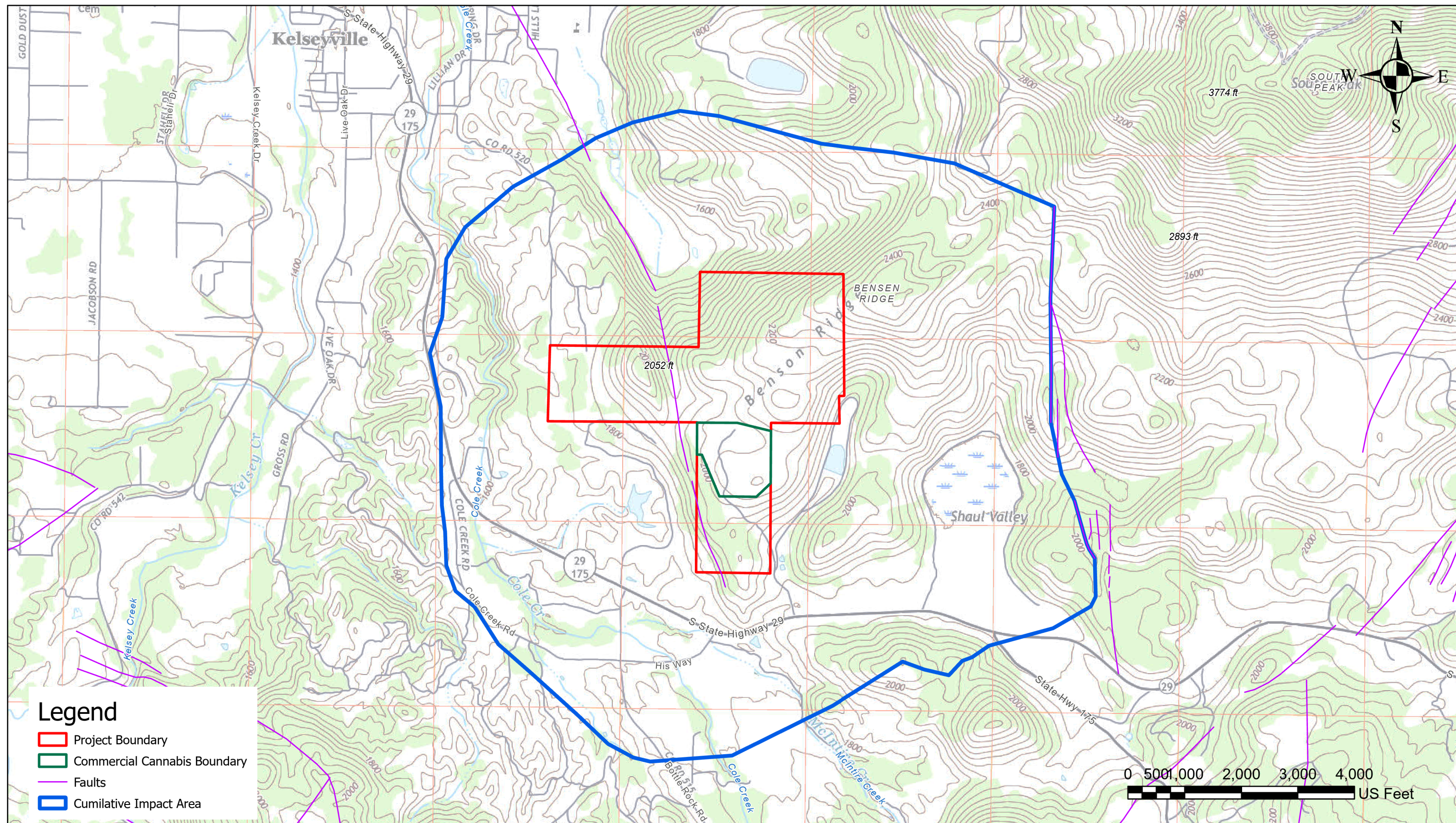




	Geologic Map Pura Vineyards Kelseyville, Lake County, CA	197456001
		Figure No. 4







	<p>Cumulative Impact Area Pura Vineyards Kelseyville, Lake County, CA</p>	<p>197456001</p>
		<p>Figure No. 7</p>

EXHIBIT 1

Exhibit 1
On-Site Wells

Well ID	Construction Date	Construction Type	Casing Diameter (in)	Approximate Elevation (ft)	Top of Screen (ft bls)	Bottom of Screen (ft bls)	Depth (ft bls)
WE-1664	April 1999	Irrigation	8.32	1957	555	635	635
WE-4585	August 2015	Domestic	6	1784	433	593	593

WE-1664

Lithology	Top (ft bls)	Base (ft bls)
White volcanic rock	0	460
Red volcanic rock	460	500
Pink volcanic rock	500	635

WE-4585

Lithology	Top (ft bls)	Base (ft bls)
Sandy silt	0	3
Tan volcanic rock	3	37
Pink/tan volcanic rock	37	53
Tan volcanic rock with fractures from 480 ft to bottom	53	600

Notes:
Elevation: estimated using Google Earth Pro
bls: below land surface

EXHIBIT 2

Exhibit 2
Water Wells in the Vicinity of Pura Vineyards

Well Permit No. / Well ID	Approximate Elevation (ft)	Top of Screen (ft bls)	Bottom of Screen (ft bls)	Depth (ft bls)	Static Depth to Water (ft bls)	Estimated Groundwater Elevation (ft)	Aquifer Thickness (ft)
WE-4585	1783	433	593	593	405	1378	188
WE-3486	1650	400	500	500	380	1270	120
WE-1664	1958	555	635	635	500	1458	135
MW-32	1874.25	365	385	385	326	1548.25	59
MW-31	1857.61	415	435	435	385	1472.61	50
MW-13	1780.47	352	362	370	312.5	1467.97	57.5
Averages				486.33	384.75	1432.47	101.58

Notes:

Elevations for wells MW-13, MW-31, and MW-32 have been surveyed

Aquifer thickness is equal to well depth minus static depth to water and is therefore limited by the depth of the wells.

APPENDIX A

QUADRUPPLICATE
For Local Requirements

STATE OF CALIFORNIA
WELL COMPLETION REPORT

Refer to Instruction Pamphlet

Page 1 of 1
Owner's Well No. WP2570

No. **713396**

Date Work Began 3-22-99, Ended 4-30-99

Local Permit Agency Health Dept.

Permit No. WE-1164 Permit Date 3-21-99

DD-1-024-05
DWR USE ONLY - DO NOT FILL IN

STATE WELL NO./STATION NO.	
LATITUDE	LONGITUDE
APN/TRS/OTHER	

GEOLOGIC LOG

ORIENTATION (✓)		DRILLING METHOD	FLUID	DESCRIPTION
VERTICAL		HORIZONTAL	ANGLE	(SPECIFY)
DEPTH FROM SURFACE		Describe material, grain size, color, etc.		
FL	to	FL		
0	460			White Volcanic Rock
460	500			Red Vol Rock
500	635			Red Vol Rock
TOTAL DEPTH OF BORING <u>635</u> (Feet)				
TOTAL DEPTH OF COMPLETED WELL <u>635</u> (Feet)				

WELL OWNER

Name Gary Snider
Mailing Address 130 Pepper Ave
City La Grange State CA ZIP 95429

Address 7630 Hwy 29
City Kelseyville
County Lake
APN Book 07 Page 029 Parcel 05
Township 13 Range 9 Section 25
Latitude 39 NORTH Longitude 122 WEST

LOCATION SKETCH



ACTIVITY (✓)

☒ NEW WELL
☐ MODIFICATION/REPAIR
 ☐ Deepen
 ☐ Other (Specify) _____

☐ DESTROY (Describe Procedures and Materials Under "GEOLOGIC LOG")

PLANNED USES (✓)

WATER SUPPLY
 ☐ Domestic ☐ Public
 ☒ Irrigation ☐ Industrial

☒ MONITORING
☐ TEST WELL
☐ CATHODIC PROTECTION
☐ HEAT EXCHANGE
☐ DIRECT PUSH
☐ INJECTION
☐ VAPOR EXTRACTION
☐ SPARGING
☐ REMEDIATION
☐ OTHER (SPECIFY) _____

WATER LEVEL & YIELD OF COMPLETED WELL

DEPTH TO FIRST WATER 530 (FL) BELOW SURFACE
DEPTH OF STATIC WATER LEVEL 500 (FL) & DATE MEASURED 4-25-99
ESTIMATED YIELD 300+ (GPM) & TEST TYPE air lift
TEST LENGTH 4 (Hrs.) TOTAL DRAWDOWN _____ (FL)
* May not be representative of a well's long-term yield.

DEPTH FROM SURFACE			BORE-HOLE DIA. (Inches)	CASING (S)							DEPTH FROM SURFACE			ANNULAR MATERIAL			
				TYPE (✓)				MATERIAL / GRADE	INTERNAL DIAMETER (Inches)	GAUGE OR WALL THICKNESS				SLOT SIZE IF ANY (Inches)	TYPE		
FL	to	FL	BLANK	SCREEN	CON-DUCTOR	FILL PIPE									FL	to	FL
0	500	12 1/4	X				5H.156	8.32	156		0	20		X			Per. Gr. #1
500	555	8 3/4	X								20	500					
555	635		X							Factory Part.							

ATTACHMENTS (✓)

- ☐ Geologic Log
- ☐ Well Construction Diagram
- ☐ Geophysical Log(s)
- ☐ Soil/Water Chemical Analyses
- ☐ Other _____

ATTACH ADDITIONAL INFORMATION, IF IT EXISTS.

CERTIFICATION STATEMENT

I, the undersigned, certify that this report is complete and accurate to the best of my knowledge and belief.

NAME Larry Newman Drilling
(PERSON, FIRM, OR CORPORATION) (TYPED OR PRINTED)

ADDRESS 13011 Hwy 29 La Grange CA 95429
CITY STATE ZIP

Signed Larry Newman DATE SIGNED 4-16-99 C-57 LICENSE NUMBER 445211
WELL DRILLER/AUTHORIZED REPRESENTATIVE

DWR USE ONLY										DO NOT FILL IN									
13N109W-24																			
STATE										WELL NO./STATION NO.									
LATITUDE										LONGITUDE									
APN/TRS/OTHER																			

GEOLOGIC LOG

[illegible]

WELL LOCATION

Address 6700 Wilkinson Road
City Kelseyville CA
County Lake
APN Book 007 Page 018 Parcel 020
Township 13 N Range 9 W Section 24 ✓
Latitude 38° 57' 287 N 122° 49' 059 W
DEG. MIN. SEC. DEG. MIN. SEC.

LOCATION SKETCH

<div style="text-align: center;"> <p>———— NORTH ————</p> <p style="text-align: center;">———— SOUTH ————</p> </div> <p style="margin-top: 20px;"><i>Illustrate or Describe Distance of Well from Roads, Buildings, Fences, Rivers, etc. and attach a map. Use additional paper if necessary. PLEASE BE ACCURATE & COMPLETE.</i></p>	<div style="text-align: center;"> <p>———— WEST ————</p> <p style="text-align: right;">EAST ————</p> </div> <div style="margin-top: 20px;"> <p><input checked="" type="checkbox"/> NEW WELL</p> <p>MODIFICATION/REPAIR</p> <p style="margin-left: 20px;"><input type="checkbox"/> Deepen</p> <p style="margin-left: 20px;"><input type="checkbox"/> Other (Specify) _____</p> <hr/> <p><input type="checkbox"/> DESTROY (Describe Procedures and Materials Under "GEOLOGIC LOG")</p> <p>PLANNED USES (<input checked="" type="checkbox"/>)</p> <p>WATER SUPPLY</p> <p style="margin-left: 20px;"><input checked="" type="checkbox"/> Domestic <input type="checkbox"/> Public</p> <p style="margin-left: 20px;"><input type="checkbox"/> Irrigation <input type="checkbox"/> Industrial</p> <p>MONITORING <input type="checkbox"/></p> <p>TEST WELL <input type="checkbox"/></p> <p>CATHODIC PROTECTION <input type="checkbox"/></p> <p>HEAT EXCHANGE <input type="checkbox"/></p> <p>DIRECT PUSH <input type="checkbox"/></p> <p>INJECTION <input type="checkbox"/></p> <p>VAPOR EXTRACTION <input type="checkbox"/></p> <p>SPARGING <input type="checkbox"/></p> <p>REMEDIATION <input type="checkbox"/></p> <p>OTHER (SPECIFY) _____</p> </div>
--	--

WATER LEVEL & YIELD OF COMPLETED WELL

DEPTH TO FIRST WATER N/A (Ft.) BELOW SURFACE 1
DEPTH OF STATIC
WATER LEVEL 405 (Ft.) & DATE MEASURED 8/11/2015
ESTIMATED YIELD * 25 (GPM) & TEST TYPE Air Developed
TEST LENGTH 4 (Hrs.) TOTAL DRAWDOWN BTM (Ft.)
May not be representative of a well's long-term yield.

DEPTH FROM SURFACE			BORE - HOLE DIA. (Inches)	CASING (S)				
				TYPE (✓)	MATERIAL / GRADE	INTERNAL DIAMETER (Inches)	GAUGE OR WALL THICKNESS	SLOT SIZE IF ANY (Inches)
Ft.	to	Ft.	BLANK	SCREEN				
0		20	13 1/2					
20		600	10					
+2		433		✓		PVC	6	SDR21
433		593			✓	PVC	6	SDR21
								.032

DEPTH FROM SURFACE			ANNULAR MATERIAL			
			TYPE			
Ft.	to	Ft.	CE- MENT (✓)	BEN- TONITE (✓)	FILL (✓)	FILTER PACK (TYPE/SIZE)
0		21		✓		
21		593			✓	3/8 Pea Gravel

ATTACHMENTS (☒)

- ATTACH ADDITIONAL INFORMATION, IF IT EXISTS.

CERTIFICATION STATEMENT

I, the undersigned, certify that this report is complete and accurate to the best of my knowledge and belief.

NAME Weeks Drilling & Pump

(PERSON, FIRM, OR CORPORATION) (TYPED OR PRINTED)

P.O. Box 176

ADDRESS

Signed

Sebastopol

CIT

09/17/15

CA

ST

177681

95473

ZIP

681

Permit Date 6/7/2011

FLUID N/A

NAME _____
ADDRESS _____
CITY _____ STATE _____ ZIP _____

DEG.	MIN.	SEC.
------	------	------

DEG.	MIN.	SEC.
------	------	------

ACTIVITY (✓)

☒ NEW WELL

MODIFICATIONS

MODIFICATION/REPAIR
 — Deepen
 — Other (Specify)

— DESTROY (Describe Procedures and Materials Under "GEOLOGIC LOG")

PLANNED USES (✓)

WATER SUPPLY
☒ Domestic ☐ Public
☐ Irrigation ☐ Industrial

MONITORING_____

TEST WELL

CATHODIC PROTECTION

HEAT EXCHANGE____

DIRECT PUSH ____

INJECTION _____

VAPOR EXTRACTION —

SPARGING _____

REMEDICATION_____

OTHER (SPECIFY) _____

DEPTH TO FIRST WATER N/A (Ft.) BELOW SURFACE

DEPTH OF STATIC, .

DEPTH OF STATIC
WATER LEVEL N/A (Ft.) & DATE MEASURED _____

ESTIMATED YIELD * N/A (GPM) & TEST TYPE N/A

TEST LENGTH N/A (Hrs.) TOTAL DRAWDOWN N/A (Fl.)

May not be representative of a well's long-term yield.

[illegible]

ATTACH ADDITIONAL INFORMATION, IF IT EXISTS.

I, the undersigned, certify that this report is complete and accurate to the best of my knowledge and belief.

NAME Weeks Drilling & Pump

(PERSON, FIRM, OR CORPORATION) (TYPED OR PRINTED)

P.O. Box 176
ADDRESS

Signed

Sebastopol
CITY

$$\frac{CA}{S^*}$$

95473

STATE

177681

WELL DRILLER/AUTHORIZED REPRESENTATIVE

08/04/11
DATE SIGNED

C-57 LICENSE NUMBER

STATE OF CALIFORNIA
WELL COMPLETION REPORT

Refer to Instruction Pamphlet

Page of

Owner's Well No.

No. **1075325**

Date Work Began **8-9-04**, Ended **9-21-04**

Local Permit Agency **Health Dept.**

Permit No. **WE-3486** Permit Date **8-3-04**

DO NOT USE ONLY DO NOT FILL IN

(3N) 09W - 24

STATE WELL NO./STATION NO.

LATITUDE LONGITUDE

APN/TRS/OTHER

GEOLOGIC LOG

ORIENTATION () ☒ VERTICAL ☐ HORIZONTAL ☐ ANGLE ☐ (SPECIFY)

DRILLING METHOD **Air Rotary** FLUID

DESCRIPTION

Describe material, grain size, color, etc.

DEPTH FROM SURFACE

Ft. to Ft.

0 80

80 295

295 440

440 525

Blue Sand (med Hard)

Brown Sand (Harder)

Lost circulation

HARD Green + white Volcanic

+ clear Quartz

WELL LOCATION
Address **6680 WILKINSON Road**

City **Kelseyville Ca 95451**

County **Lake**

APN Book **007** Page **018** Parcel **10**

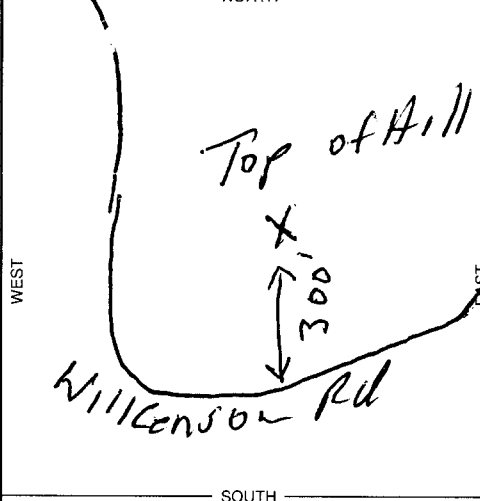
Township **13N** Range **9W** Section **24**

Lat Long

DEG. MIN. SEC. N Long DEG. MIN. SEC. W

LOCATION SKETCH

NORTH



ACTIVITY ()

☒ NEW WELL
☐ MODIFICATION/REPAIR
 ☐ Deepen
 ☐ Other (Specify)

☐ DESTROY (Describe Procedures and Materials Under "GEOLOGIC LOG")

USES ()
WATER SUPPLY
☒ Domestic ☐ Public
☐ Irrigation ☐ Industrial

☐ MONITORING
☐ TEST WELL
☐ CATHODIC PROTECTION
☐ HEAT EXCHANGE
☐ DIRECT PUSH
☐ INJECTION
☐ VAPOR EXTRACTION
☐ SPARGING
☐ REMEDIATION
☐ OTHER (SPECIFY)

Illustrate or Describe Distance of Well from Roads, Buildings, Fences, Rivers, etc. and attach a map. Use additional paper if necessary. **PLEASE BE ACCURATE & COMPLETE.**

WATER LEVEL & YIELD OF COMPLETED WELL

DEPTH TO FIRST WATER **440** (Ft.) BELOW SURFACE

DEPTH OF STATIC WATER LEVEL **380** (Ft.) & DATE MEASURED **9-20-04**

ESTIMATED YIELD **40** (GPM) & TEST TYPE **Air Lift**

TEST LENGTH **2** (Hrs.) TOTAL DRAWDOWN (Ft.)

* May not be representative of a well's long-term yield.

TOTAL DEPTH OF BORING **525** (Feet)

TOTAL DEPTH OF COMPLETED WELL **500** (Feet)

DEPTH FROM SURFACE			BORE-HOLE DIA. (Inches)	CASING (S)							DEPTH FROM SURFACE			ANNULAR MATERIAL			
				TYPE (≤)				MATERIAL / GRADE	INTERNAL DIAMETER (Inches)	GAUGE OR WALL THICKNESS				SLOT SIZE IF ANY (Inches)	TYPE		
Ft.	to	Ft.	BLANK	SCREEN	CON- DUCTOR	FILL PIPE										CE- MENT (≤)	BEN- TONITE (≤)
0	20		X				PVC	4 1/2	160								
20	400		X				PVC	4 1/2	160							5/16 pea	
400	500			X			PVC	4 1/2	200	.030						5/16 pea	

ATTACHMENTS ()

- ☐ Geologic Log
- ☐ Well Construction Diagram
- ☐ Geophysical Log(s)
- ☐ Soil/Water Chemical Analyses
- ☐ Other

ATTACH ADDITIONAL INFORMATION, IF IT EXISTS.

CERTIFICATION STATEMENT

I, the undersigned, certify that this report is complete and accurate to the best of my knowledge and belief.

NAME **Larry Herman Drilling**
(PERSON, FIRM, OR CORPORATION) (TYPED OR PRINTED)

ADDRESS **13011 Hwy 29 Lower Lake Ca 95454**
CITY STATE ZIP

Signed **Janet Herman** DATE SIGNED **9-22-04** C-57 LICENSE NUMBER **465071**
C-57 LICENSED WATER WELL CONTRACTOR

ORIGINAL
File with DWR

RECEIVED

STATE OF CALIFORNIA
WELL COMPLETION REPORT

Refer to Instruction Pamphlet

Page ____ of ____
Owner's Well No. _____

MAR 29 1999

No. 705638

Date Work Began 12-22-98 Ended 12-29-98

Local Permit Agency Lake County Environmental Health
Permit No. WE 1642 Permit Date 12-22-98

DWR USE ONLY - DO NOT FILL IN

13N/09W-26M

STATE WELL NO./STATION NO.

LATITUDE LONGITUDE

APN/TRS/OTHER

GEOLOGIC LOG

ORIENTATION () ☒ VERTICAL ☐ HORIZONTAL ☐ ANGLE (SPECIFY)

DRILLING METHOD Rotary FLUID Air

DEPTH FROM SURFACE	DESCRIPTION
Fl. to Fl.	Describe material, grain size, color, etc.
0 to 3	Bra. Soil
3 to 10	Vol. Sand & Gravel
10 to 25	Bra. Clay
25 to 60	Gray Clay
60 to 150	Gray Vol. Rock
150 to 190	Black, Pink & Gray Pol. Rock
190 to 270	Gray Vol. Rock
270 to 310	Green Vol. Rock

TOTAL DEPTH OF BORING 310 (Feet)

TOTAL DEPTH OF COMPLETED WELL 300 (Feet)

WELL LOCATION

Address 7230 S. Hwy 29

City Kelseyville CA

County Lake

APN Book 009 Page 027 Parcel 21

Township 13N Range 09W Section 26

Latitude _____ Longitude _____

LOCATION SKETCH

Illustrate or Describe Distance of Well from Roads, Buildings, Fences, Rivers, etc. and attach a map. Use additional paper if necessary. PLEASE BE ACCURATE & COMPLETE.

ACTIVITY ()

☒ NEW WELL

MODIFICATION/REPAIR

☐ Deepen

☐ Other (Specify)

DESTROY (Describe Procedures and Materials Under "GEOLOGIC LOG")

PLANNED USES ()

WATER SUPPLY

☒ Domestic ☐ Public

☐ Irrigation ☐ Industrial

MONITORING

TEST WELL

CATHODIC PROTECTION

HEAT EXCHANGE

DIRECT PUSH

INJECTION

VAPOR EXTRACTION

SPARGING

REMEDIATION

OTHER (SPECIFY)

WATER LEVEL & YIELD OF COMPLETED WELL

DEPTH TO FIRST WATER 302 (Ft.) BELOW SURFACE

DEPTH OF STATIC WATER LEVEL 273 (Ft.) & DATE MEASURED 12-29-98

ESTIMATED YIELD 26 (GPM) & TEST TYPE Air Lift

TEST LENGTH 1 (Hrs.) TOTAL DRAWDOWN _____ (Ft.)

* May not be representative of a well's long-term yield.

DEPTH FROM SURFACE	BORE-HOLE DIA. (Inches)	CASING (S)						DEPTH FROM SURFACE	ANNULAR MATERIAL					
		TYPE ()				MATERIAL / GRADE	INTERNAL DIAMETER (Inches)		GAUGE OR WALL THICKNESS	SLOT SIZE IF ANY (Inches)	TYPE			
Fl. to Fl.		BLANK	SCREEN	CON- DUCTOR	FILL PIPE									Fl. to Fl.
0 to 60	9	X				PVC F480	4 1/2	SDR26		0 to 20	X			
60 to 288	7	X				PVC F480	4 1/2	SDR26		20 to 300				Pa Gravel
288 to 300	7	X				PVC F480	4 1/2	SDR26	2X 1/8					

APR 20 1999

ATTACHMENTS ()

- ☐ Geologic Log
- ☐ Well Construction Diagram
- ☐ Geophysical Log(s)
- ☐ Soil/Water Chemical Analyses
- ☐ Other

ATTACH ADDITIONAL INFORMATION, IF IT EXISTS.

CERTIFICATION STATEMENT

I, the undersigned, certify that this report is complete and accurate to the best of my knowledge and belief.

NAME Dan Mc Mullen Well Drilling

(PERSON, FIRM, OR CORPORATION) (TYPED OR PRINTED)

1407 Old Long Valley Rd. Clearlake Oaks CA 95423

ADDRESS CITY STATE ZIP

Signed Dan 1 Mullen 12-29-98 533152

WELL DRILLER/AUTHORIZED REPRESENTATIVE DATE SIGNED C-57 LICENSE NUMBER

ORIGINAL

File with DWR

STATE OF CALIFORNIA

THE RESOURCES AGENCY

DEPARTMENT OF WATER RESOURCES

WATER WELL DRILLERS REPORT

13N/09W-25M

Do not fill in

No. 171570

Notice Tent No. _____

Local Permit No. or Date _____

State Well No. _____

Other Well No. _____

(12) WELL LOG: Total depth 70 ft. Depth of completed well 70 ft.
from ft. to ft. Formation (Describe by color, character, size or material)

(2) LOCATION OF WELL (See instructions):

County LAKE Owner's Well Number MU-12BWell address if different from above BENSON RIDGE FACILITYTownship 13N Range 8W Section 36

Distance from cities, roads, railroads, fences, etc. _____

See accompanying borehole logs

(3) TYPE OF WORK:

New Well ☒ Deepening ☐Reconstruction ☐Reconditioning ☐Horizontal Well ☐Destruction ☐ (Describe destruction materials and procedures in Item 12)

(4) PROPOSED USE:

Domestic ☐Irrigation ☐Industrial ☐Test Well ☒Stock ☐Municipal ☐Other ☐

WELL LOCATION SKETCH

(5) EQUIPMENT:

Rotary ☐ Reverse ☐Cable ☐ Air ☐Other ☒ Bucket ☐

(6) GRAVEL PACK:

Yes ☒ No ☐ Size 3/4" SANDDiameter of bore 12 INCHPacked from 5' to 60' ft.

(7) CASING INSTALLED:

Steel ☐ Plastic ☒ Concrete ☐

(8) PERFORATIONS:

Type of perforation or size of screen

From ft.	To ft.	Dia. in.	Gage or Wall	From ft.	To ft.	Slot size
+2.5	64	2	64x40	54	64	620 INCH

(9) WELL SEAL:

Was surface sanitary seal provided? Yes ☒ No ☐ If yes, to depth _____ ft.Were strata sealed against pollution? Yes ☒ No ☐ Interval 0-5' ft.Method of sealing Bentonite pellets & cement

(10) WATER LEVELS:

Depth of first water, if known _____ ft.

Standing level after well completion 33 ft.

(11) WELL TESTS:

Was well test made? Yes ☐ No ☒ If yes, by whom? _____Type of test Pump ☐ Bailer ☐ Air lift ☐

Depth to water at start of test _____ ft. At end of test _____ ft.

Discharge _____ gal/min after _____ hours Water temperature _____

Chemical analysis made? Yes ☒ No ☐ If yes, by whom? IT CorpWas electric log made? Yes ☐ No ☒ If yes, attach copy to this reportWork started JANUARY 7 19 85 Completed JANUARY 10 19 85

WELL DRILLER'S STATEMENT:

This well was drilled under my jurisdiction and this report is true to the best of my knowledge and belief

SIGNED M. M. M. M. (Well Driller)NAME IT Corporation

(Person, firm, or corporation) (Typed or printed)

Address 17500 Red Hill AvenueCity Irvine Zip 92714License No. EG 940 Date of this report November 14, 1985

DWR 188 (REV. 7-76)

IF ADDITIONAL SPACE IS NEEDED, USE NEXT CONSECUTIVELY NUMBERED FORM

DEPTH IN FEET	LABORATORY TEST DATA								BORING NO. MW-12B			
	TESTS REPORTED ELSEWHERE	ATTERBERG LIMITS		STRENGTH TEST DATA				PENETRATION RESISTANCE (BLOWS/FT.) SAMPLE	USCS	PROFILE	DESCRIPTION	
		LIQUID LIMIT (%)	PLASTICITY INDEX (%)	TYPE OF TEST	NORMAL OR CONFINING PRESSURE (PSF)	DEVIATOR STRESS (PSF)	SHEAR STRENGTH (PSF)					
												MOISTURE CONTENT (%)
0												
5												
10												
15												
20												
25												
30												
35												
40												
45												
50												
55												
60												
65												
70												

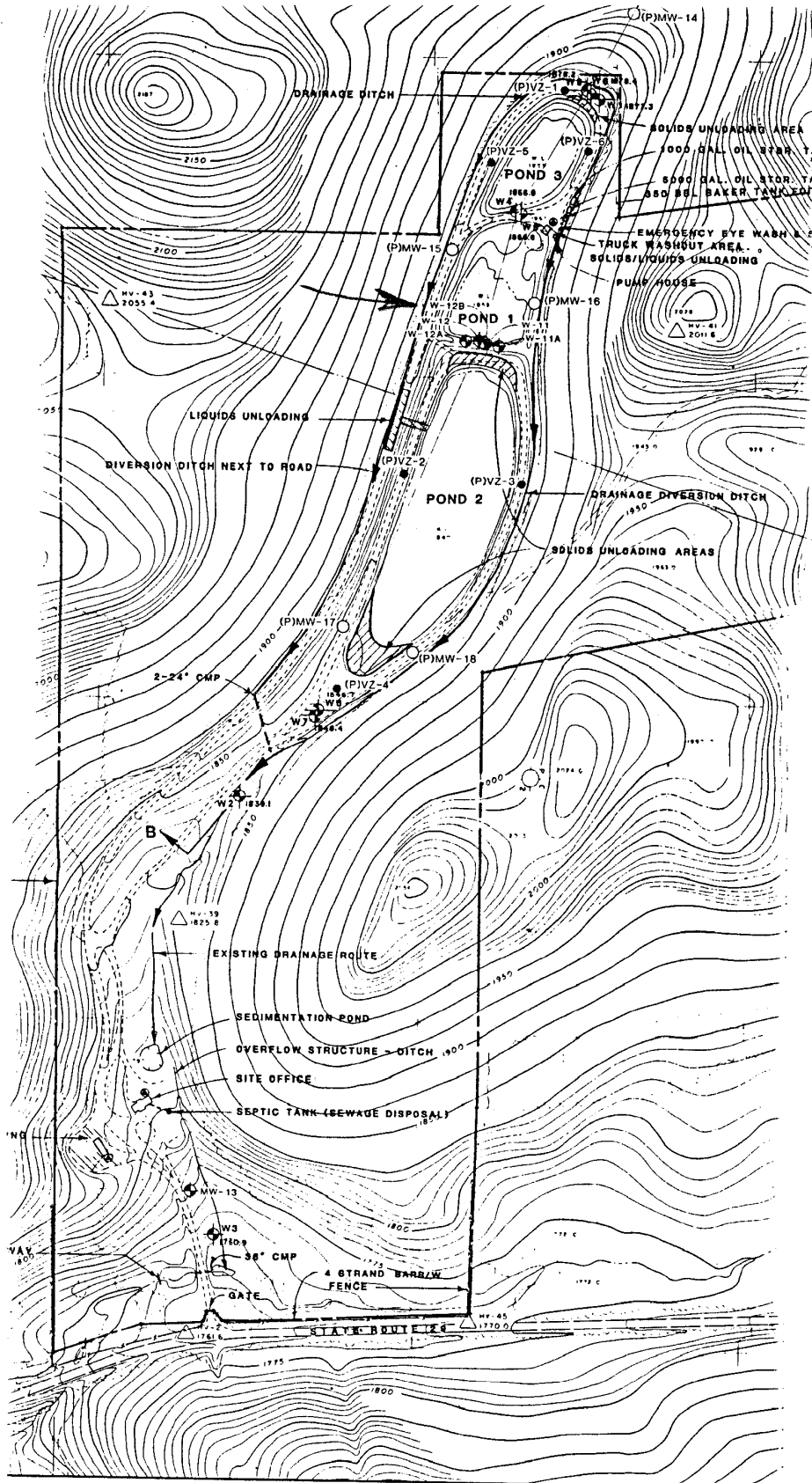
FIELD ENGINEER	DATE BEGAN	COORDINATES	DATE FINISHED	CHECKED BY	GROUND SURFACE EL.
V. Shupe	01/07/85	N Not yet surveyed	01/10/85	M. Egli	Not yet surveyed
M. Egli		E Not yet surveyed		M. Ralderman	

USCS	PROFILE	DESCRIPTION
8-1	cl/ch	FILL. Hard, REDDISH-BROWN sandy clay with gravels, moist, contains approximately 75 percent clay and silt, 20 percent fine to medium grained sand, and 5 percent gravels; gravels consist of gray-blue tuffaceous ash clasts up to a maximum size of 1 1/4 inches, contains wood and other vegetation.
8-2		Approximately 70 percent clay and silt, 20 percent sand, and 10 percent gravel; gravels consist of friable gray-green tuffaceous ash clasts up to a maximum size of 1 1/4 inches.
8-3		Approximately 60 percent clay and silt, 20 percent sand, and 20 percent gravel, ash clasts up to 1 3/4 inches, roots.
8-4	sm/ml	Loose to hard, orange-brown SANDY to CLAYEY SILT, moist, contains approximately 80 percent clay and silt, 15 percent very fine sand, and 2 percent fine gravels, roots.
8-5	cl	Hard, reddish-brown SANDY CLAY with gravel, moist.
8-6		Hard, orange-brown SILTY CLAY, decrease in moisture, contains approximately 80 percent clay and silt, 20 percent sand, and trace amounts of gravel.
8-7		Hard, orange-brown SILTY CLAY, decrease in moisture, contains approximately 80 percent clay and silt, 20 percent sand, and trace amounts of gravel.
8-8	cl/ch	Approximately 70 percent clay and silt, 20 percent sand, and 10 percent gravel.
8-9	sc/cl	Very hard to very dense, reddish-brown SANDY CLAYEY SILT, and CLAYEY SILTY SAND, moist, contains approximately 45 percent clay and silt, 45 percent sand, and 10 percent gravel; sand increasing in content and grain size, gravels consist of gray to light gray, white, and orange ash clasts.
8-10		Wet.
8-11	sc/cl	Indurated, gray TUFFACEOUS ASH, slightly moist, friable, iron stained (weathered surface?).
8-12	S-12	Very hard to very dense, reddish orange-brown SANDY CLAYEY SILT to CLAYEY SILTY SAND, very hard to very dense, moist to wet, contains approximately 45 percent clay and silt, 45 percent fine sand, and 10 percent fine gravels.
8-13		Well consolidated, fractured.
		Moist to wet.

TOTAL DEPTH 70.0 FEET

PROJECT NO. B4H040
 CLIENT IT - BENSON RIDGE

IT CORPORATION



BENSON RIDGE
WELL LOCATIONS

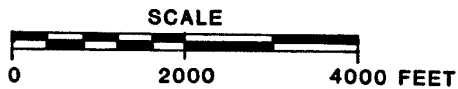
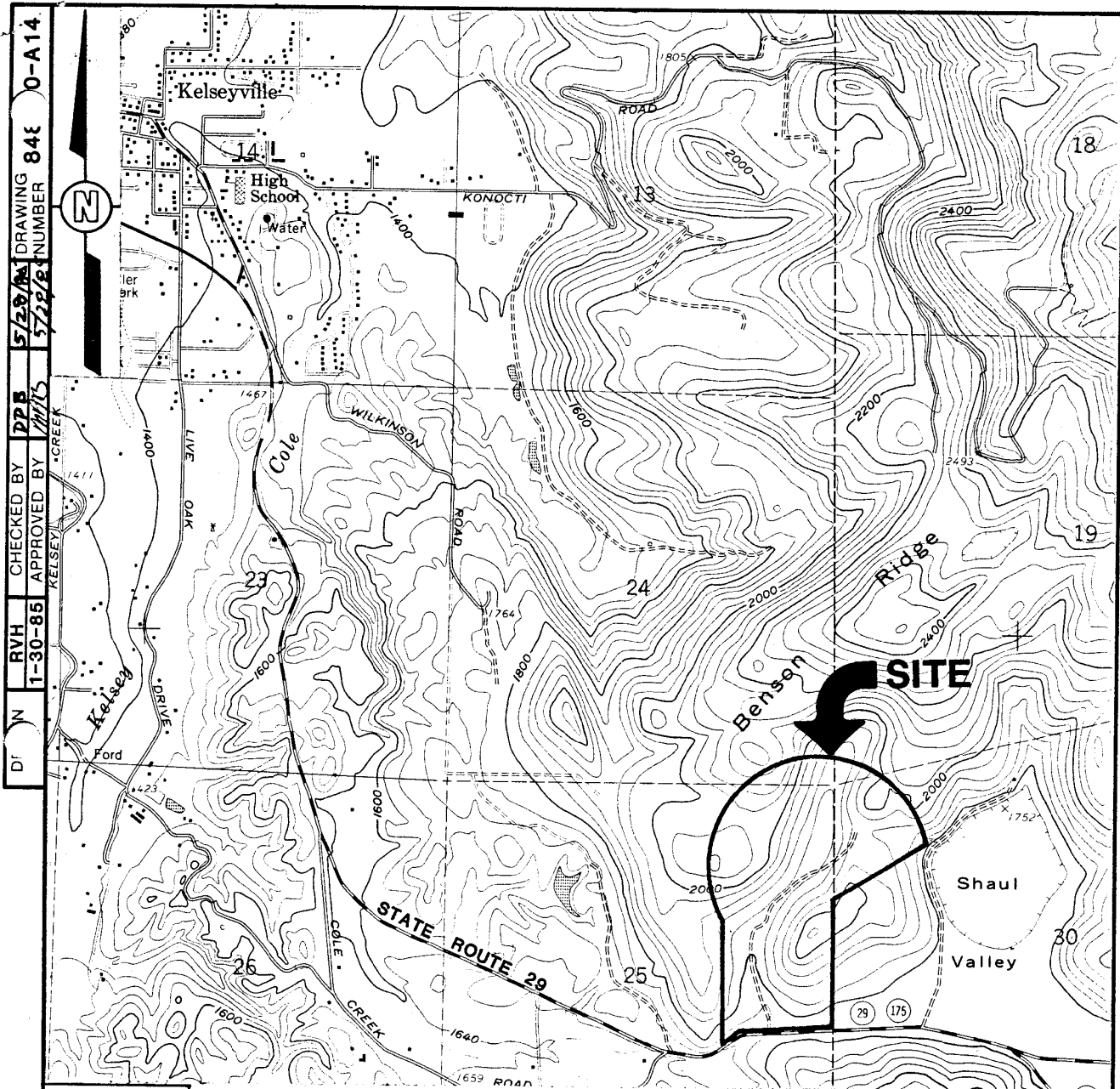


FIGURE 1

SITE LOCATION MAP

BENSON RIDGE FACILITY

PREPARED FOR

IT CORPORATION BENSON RIDGE FACILITY

REFERENCE:

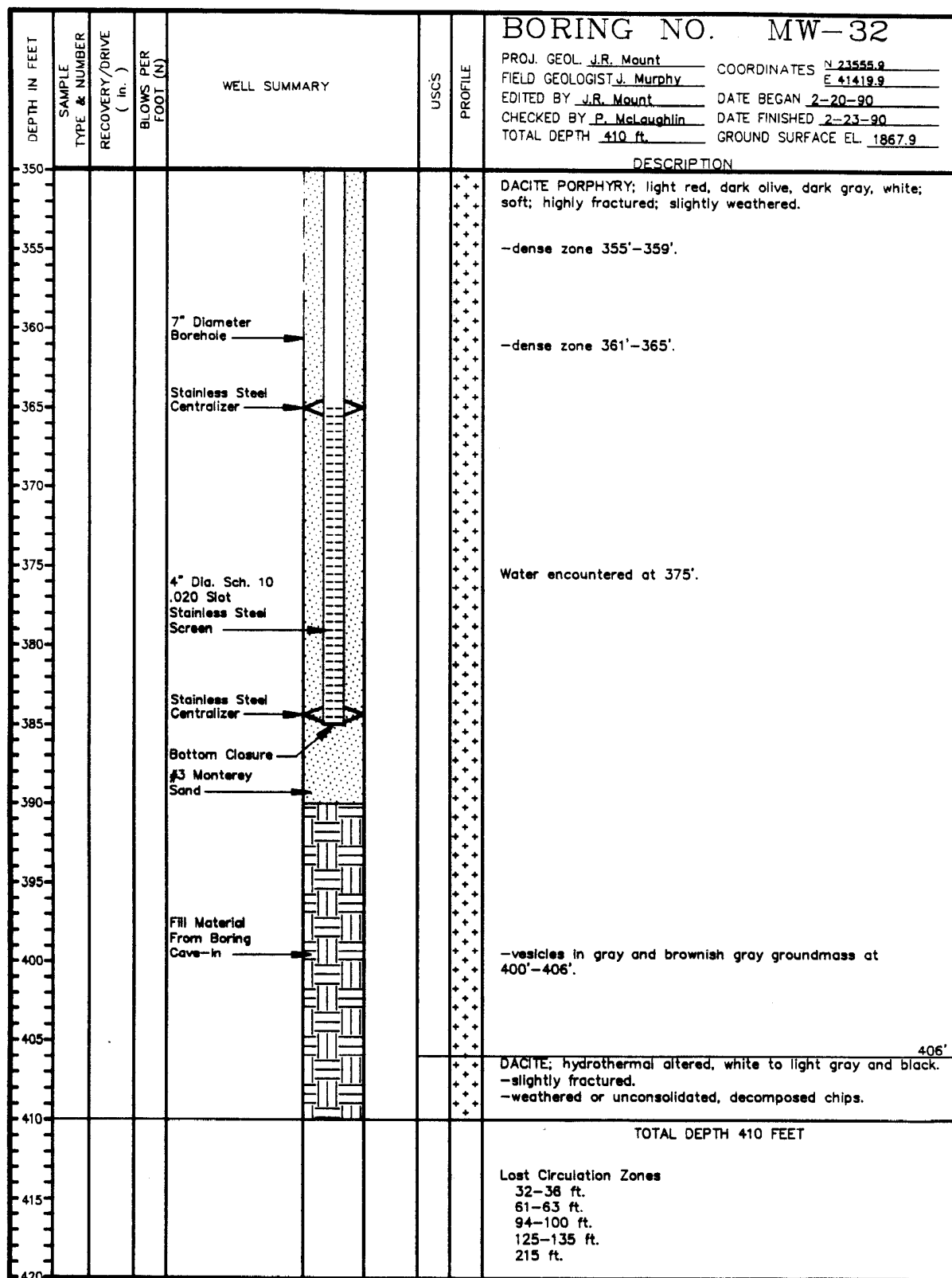
7.5 MINUTE U.S.G.S. TOPOGRAPHIC MAP
OF KELSEYVILLE CALIFORNIA QUADRANGLE
DATED: 1959, PHOTOREVISED 1975
SCALE 1:24,000

© 1984 IT CORPORATION
ALL COPYRIGHTS RESERVED



... Creating a Safer Tomorrow

"Do Not Scale This Drawing"



DRILLING CO.: Water Development Corporation
 DRILL METHOD: Air Rotary with Foam & Water

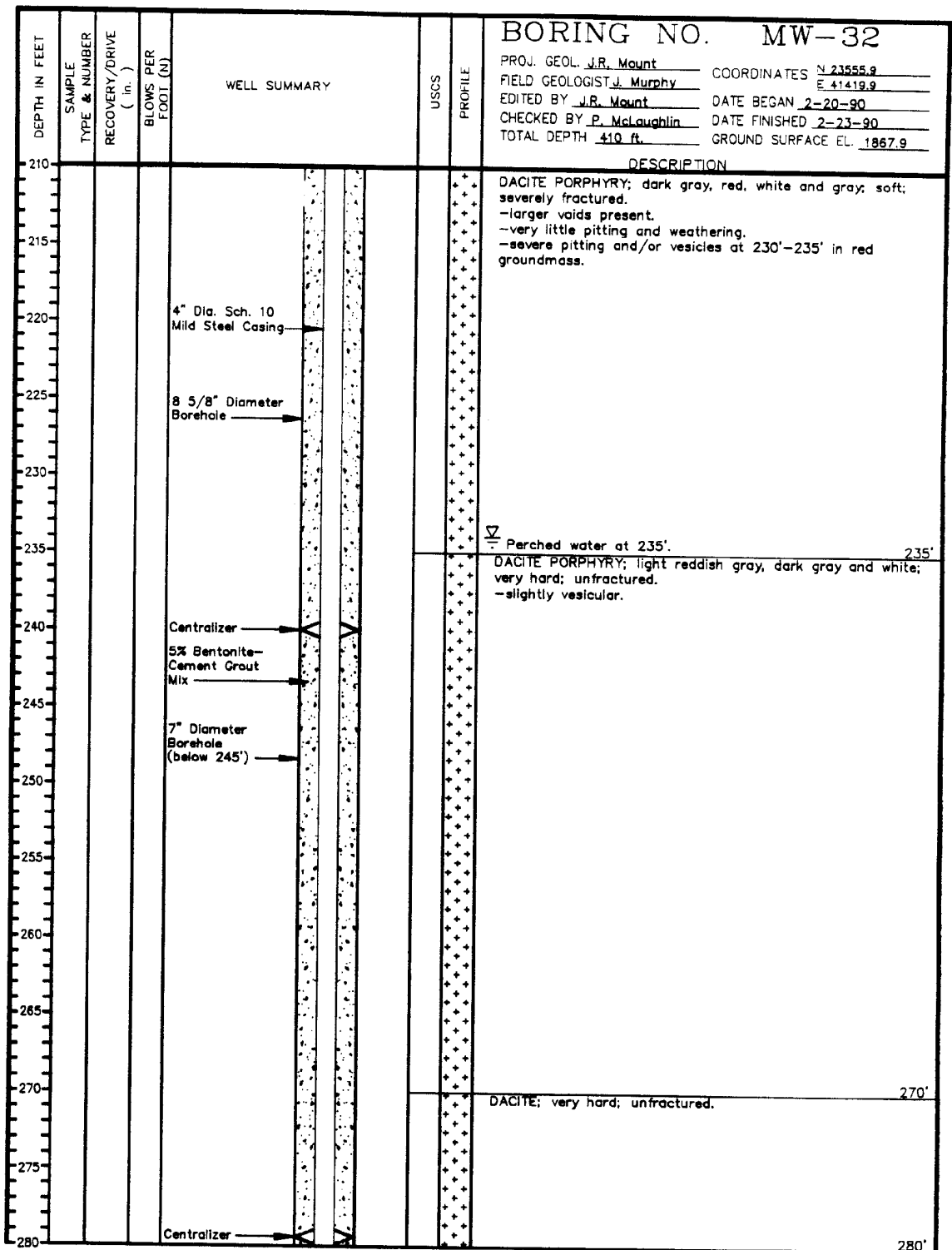
PAGE 6 OF 6

PROJECT NO.: ADBEO2
 CLIENT: Benson Ridge
 LOCATION: Martinez, California

SEE LEGEND FOR LOGS AND TEST PITS
 FOR EXPLANATION OF SYMBOLS AND TERMS

BR-MW32(BR3)





DRILLING CO.: Water Development Corporation
 DRILL METHOD: Air Rotary with Foam & Water

PAGE 4 OF 6

PROJECT NO.: AD8EO2
 CLIENT: Benson Ridge
 LOCATION: Martinez, California

SEE LEGEND FOR LOGS AND TEST PITS
 FOR EXPLANATION OF SYMBOLS AND TERMS

BR-MW32(BR3)



				BORING NO. MW-32			
DEPTH IN FEET	SAMPLE TYPE & NUMBER	RECOVERY/DRIVE (in.)	BLOWS PER FOOT (N)	WELL SUMMARY	USCS PROFILE	DESCRIPTION	
140						PROJ. GEOL. <u>J.R. Mount</u> COORDINATES <u>N 23555.9</u> FIELD GEOLOGIST <u>J. Murphy</u> <u>E 41419.9</u> EDITED BY <u>J.R. Mount</u> DATE BEGAN <u>2-20-90</u> CHECKED BY <u>P. McLaughlin</u> DATE FINISHED <u>2-23-90</u> TOTAL DEPTH <u>410 ft.</u> GROUND SURFACE EL. <u>1867.9</u>	
145						DACITE; red; soft; very fractured; vesicular. -color changing to dark yellowish red (groundmass) after depth of 155', rock becomes hard, less fractured.	
150				8 5/8" Diameter Borehole			
155				4" Dia. Sch. 10 Mild Steel Casing			
160				Centralizer			
165							
170							
175				5% Bentonite-Cement Grout Mix		DACITE; red; hard; moderately to slightly fractured; vesicular. -fewer vesicles and less fracturing below 180'. -weathering or pitting less severe with depth. -increased number of phenocrysts; white plagioclase and quartz.	
180							
185							
190							
195							
200				Centralizer			
205						DACITE PORPHYRY; dark gray, red, white; very hard; moderately fractured. -voids present.	
210							

DRILLING CO.: Water Development Corporation
 DRILL METHOD: Air Rotary with Foam & Water

PAGE 3 OF 6

PROJECT NO.: AD8E02
 CLIENT: Benson Ridge
 LOCATION: Martinez, California

SEE LEGEND FOR LOGS AND TEST PITS
 FOR EXPLANATION OF SYMBOLS AND TERMS

BR-MW32(BR3)



DEPTH IN FEET		SAMPLE TYPE & NUMBER	RECOVERY/DRIVE (in.)	BLOWS PER FOOT (N)	WELL SUMMARY	USCS	PROFILE	BORING NO. MW-32	
								PROJ. GEOL. J.R. Mount	COORDINATES N 23555.9 E 41419.9
								EDITED BY J.R. Mount	DATE BEGAN 2-20-90
								CHECKED BY P. McLaughlin	DATE FINISHED 2-23-90
								TOTAL DEPTH 410 ft.	GROUND SURFACE EL. 1867.9
DESCRIPTION									
70								DACITE; hard; fractured; severely weathered. -zones of extensive weathering with voids and fracturing.	
75								75'	
80					Centralizer			80'	
85					4" Dia. Sch. 10 Mild Steel Casing			DACITE PORPHYRY; dark gray and brownish red/light red; hard; fractured; moderately to severely weathered. -void detected--circulation loss. -closely spaced fractures.	
90									
95								-large void at 94' to 100'.	
100					5% Bentonite- Cement Grout Mix				
105					8 5/8" diameter Borehole			DACITE PORPHYRY; brownish red/red, dark gray, white, gray; soft; highly fractured; weathered. -closely spaced fractures. -large size chips indicates fracturing is extensive. -weathering along fracture surfaces. -larger percentage of red groundmass.	
110									
115								117'	
120					Centralizer			DACITE; predominantly dark gray with brown red/red and white; hard; moderately fractured. -less fracturing than above. -slight weathering.	
125								126'	
130								DACITE; red, pale reddish gray, white; soft; fracture; severely weathered. -extensive pale gray groundmass with vesicles.	
135									
140									

DRILLING CO.: Water Development Corporation
DRILL METHOD: Air Rotary with Foam & Water

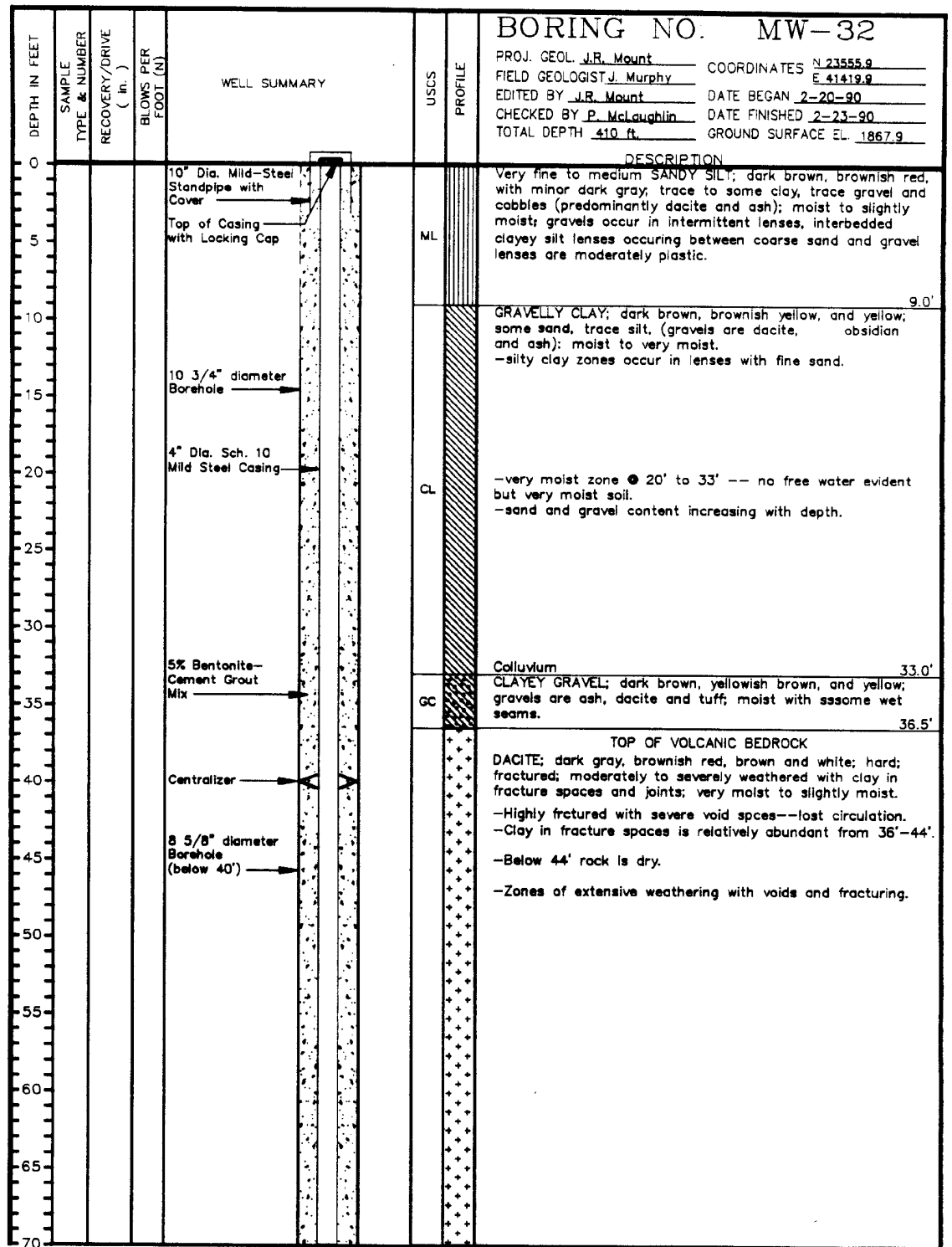
PAGE 2 OF 6

PROJECT NO.: ADBEO2
CLIENT: Benson Ridge
LOCATION: Martinez, California

SEE LEGEND FOR LOGS AND TEST PITS
FOR EXPLANATION OF SYMBOLS AND TERMS

BR-MW32(BR3)





DRILLING CO.: Water Development Corporation
 DRILL METHOD: Air Rotary with Foam & Water

PAGE 1 OF 6

PROJECT NO.: ADBEO2
 CLIENT: Benson Ridge
 LOCATION: Martinez, California

SEE LEGEND FOR LOGS AND TEST PITS
 FOR EXPLANATION OF SYMBOLS AND TERMS

BR-MW32(BR3)



15N109W-25M

ORIGINAL
File with DWR

STATE OF CALIFORNIA
THE RESOURCES AGENCY
DEPARTMENT OF WATER RESOURCES
WATER WELL DRILLERS REPORT

Do not fill in

No. 324448

License of Intent No. 91025
Local Permit No. or Date WE088

State Well No. _____
Other Well No. MW-32

(12) WELL LOG: Total depth 410 ft. Completed depth 385 ft.
from ft. to ft. Formation (Describe by color, character, size or material)

See attached boring log

(2) LOCATION OF WELL (See instructions):

County Lake Owner's Well Number MW-32
Well address if different from above 7620 Hwy 29, Kelseyville
Township 13N Range 9W Section 24 25
Distance from cities, roads, railroads, fences, etc. 2.5 mi southeast
of Kelseyville, approx 1900 ft north of state
Hwy 29, approx 25 ft east of WMU3
Marked MW-32

(3) TYPE OF WORK:

New Well ☒ Deepening ☐
Reconstruction ☐
Reconditioning ☐
Horizontal Well ☐
Destruction ☐ (Describe
destruction materials and pro-
cedures in Item 12)

(4) PROPOSED USE:

Domestic ☐
Irrigation ☐
Industrial ☐
Test Well ☐
Municipal ☐
Other ☒ Monitoring
(Describe)

WELL LOCATION SKETCH

(5) EQUIPMENT:

Rotary ☒ Reverse ☐
Cable ☐ Air ☒
Other ☐ Bucket ☐

(6) GRAVEL PACK:

Yes ☒ No ☐ Size #3 Sand
Diameter of bore Telescope 9" - 7 1/2"
Packed from 290 to 350 ft

(7) CASING INSTALLED:

Steel ☒ Plastic ☐ Concrete ☐

(8) PERFORATIONS:

Type of perforation or size of screen

From ft.	To ft.	Dia. in.	Cage or Wall	From ft.	To ft.	Slot size
<u>0</u>	<u>365</u>	<u>4</u>	<u>Sch 10</u>	<u>365</u>	<u>385</u>	<u>.020</u>

(9) WELL SEAL:

Was surface sanitary seal provided? Yes ☒ No ☐ If yes, to depth 340 ft.
Were strata sealed against pollution? Yes ☐ No ☒ Interval _____ ft.
Method of sealing Tremmy, Neat Cement & Sand/cement mix

(10) WATER LEVELS:

Depth of first water, if known 375 (Encountered) ft.
Standing level after well completion 326 ft.

(11) WELL TESTS:

Was well test made? Yes ☐ No ☒ If yes, by whom? _____
Type of test Pump ☐ Bailer ☐ Air lift ☐
_____ h to water at start of test _____ ft. At end of test _____ ft.
_____ gal/min after _____ hours Water temperature _____
Chemical analysis made? Yes ☐ No ☒ If yes, by whom? _____
Was electric log made Yes ☐ No ☒ If yes, attach copy to this report

Work started 2/20 19 90 Completed 3/1 19 90

WELL DRILLER'S STATEMENT:

106
This well was drilled under my jurisdiction and this report is true to the
best of my knowledge and belief.

Signed Jeffrey C. Barrow RME
(Well Driller)
NAME Water Development Corp.
(Person, firm, or corporation) (Typed or printed)
Address 1202 Kentucky Ave.
City Woodland, CA ZIP 95695
License No. 283326 Date of this report _____

13N/09W-25N

ORIGINAL
File with DWRSTATE OF CALIFORNIA
THE RESOURCES AGENCY
DEPARTMENT OF WATER RESOURCES
WATER WELL DRILLERS REPORT

Do not fill in

No. 324449

Well Intent No. 91025
Local Permit No. or Date WE08ZState Well No. _____
County Well No. MW-31112 WELL LOG Well depth 455 ft. (see place depth 435 ft.
from Boring Log when Description of Log is not available)

See attached boring log

2. LOCATION OF WELL (See instructions)

County Lake Owner - Well Number MW-31
Well address (if different from above) 7620 Hwy 29, Kelseyville
Township 13N Range 9W Section 24-25
Distance from cities, roads, railroads, etc. 2.5 mi southeast
of Kelseyville, approx 1400 ft north of State
Hwy 29, between MMU 1 and MMU 2, Marked MW-31

3. TYPE OF WORK

New Well ☒ Deepening

Reconstruction

Re-establishing

Horizontal Well

Destruction Describe
destruction, materials and pro-
cedure in Item 11

4. PROPOSED USE

Domestic

Irrigation

Industrial

Test Well

Municipal

Other

Monitoring ☒

WELL LOCATION SKETCH

5. EQUIPMENT

Liner ☒

Casing

Other

Reverse

Air

Pulver

GRAVEL BACK

10 5/8" #3 Sand

407 438

407 438

7. CASING/STABILIZER

Steel

PVC

PVC

Casing or Wall

8. PENETRATIONS

Type of penetration and depth

From

To

To

From

To

To

To

0

415

5

Sch 80

415

435

020

10. WELL SEAL

Well is sealed against pollution Yes ☒ No ☐ Depth of seal 340Well is sealed against pollution Yes ☒ No ☐ Depth of seal 340Method of seal Tremmy, Neat Cement & Bent. (5%)

11. WATER LEVELS

Water level at time of test

420.0 (Encountered)

Standing level after well is completed

385.0

12. WELL TESTS

Was well tested

Yes ☒

Flow rate (gpm)

Was well tested

Yes ☒

Flow rate (gpm)

Was well tested

Yes ☒

Flow rate (gpm)

Was well tested

Yes ☒

Flow rate (gpm)

Was well tested

Yes ☒

Flow rate (gpm)

Was well tested

Yes ☒

Flow rate (gpm)

Was well tested

Yes ☒

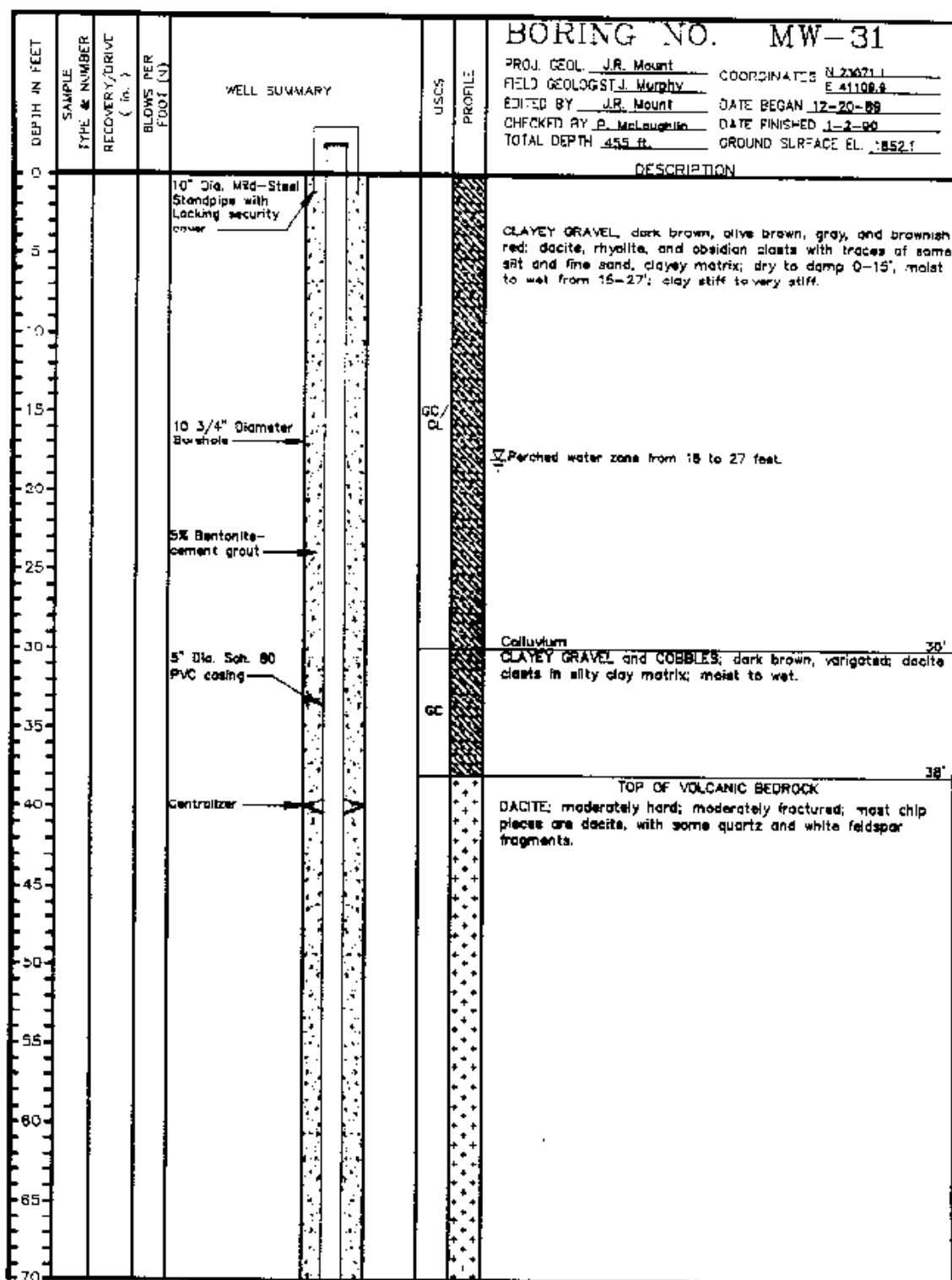
Flow rate (gpm)

Work started 12/20 89 Completed 1/3 90

WELL DRILLER'S STATEMENT

This well is drilled under my supervision and the responsibility for the
depth, location, construction and log is mine.Signed [Signature] Well DrillerNAME [Signature] State of CaliforniaAddress [Signature] City [Signature] State [Signature]Phone [Signature] Date [Signature]License No. [Signature] Exp. Date [Signature]

If additional space is needed, use next consecutively numbered form



DRILLING CO.: Water Development Corporation
 DRILL METHOD: Air Rotary with Foam and Water

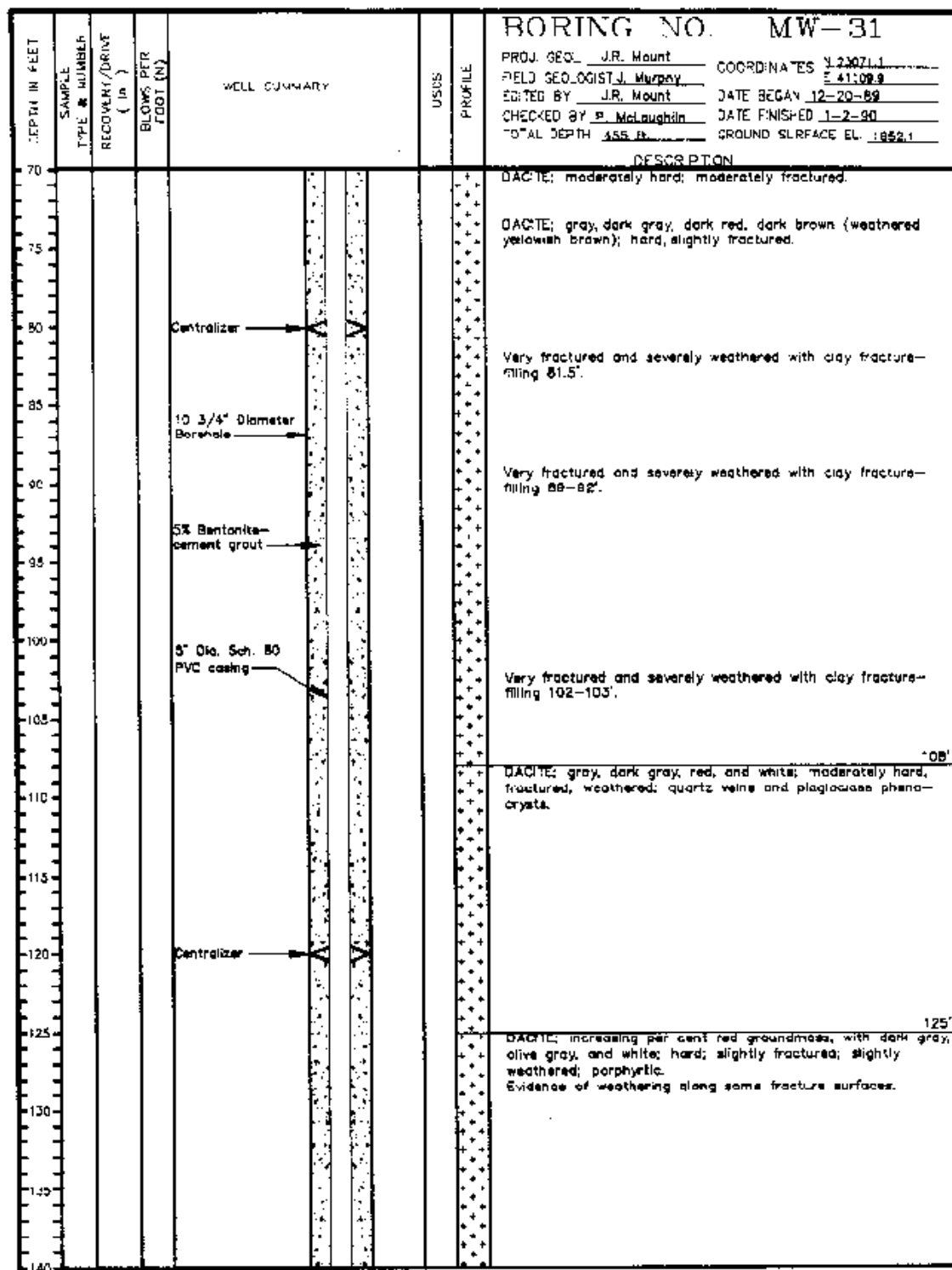
PAGE 1 OF 7

PROJECT NO.: ADBE02
 CLIENT: Benson Ridge
 LOCATION: Martinez, California

SEE LEGEND FOR LOGS AND TEST PITS
 FOR EXPLANATION OF SYMBOLS AND TERMS

BR-MW31(+BR3)





DRILLING CO.: Water Development Corporation
 DRILL METHOD: Air Rotary with Foam and Water

PAGE 2 OF 7

PROJECT NO.: ADBE02
 CLIENT: Benson Ridge
 LOCATION: Martinez, California

SEE LEGEND FOR LOGS AND TEST PITS
 FOR EXPLANATION OF SYMBOLS AND TERMS

BR-MW31(4BR3)



DEPTH IN FEET	SAMPLE TYPE & NUMBER	RECOVERY/DRIVE (in.)	BLOWS PER FOOT (B)	WELL SUMMARY	LOGS	PROFILE	BORING NO. MW-31	
							PROJ. GEOL. J.R. Mount	COORDINATES N 2307.1 E 41.00.0
							FIELD GEOLOGIST J. Murphy <td>DATE BEGAN 12-20-88</td>	DATE BEGAN 12-20-88
							EDITED BY J.R. Mount <td>DATE FINISHED 1-2-89</td>	DATE FINISHED 1-2-89
							CHECKED BY P. McLaughlin <td>GROUND SURFACE E. 1852.1</td>	GROUND SURFACE E. 1852.1
							TOTAL DEPTH 455 ft.	
							DESCRIPTION	
40							DACITE; increasing per cent red groundmass, with dark gray, olive gray, and white; hard; slightly fractured; slightly weathered; porphyritic. Evidence of weathering along some fracture surfaces.	
145								
150								
155								
160								
165								
170								
175								
180							177'	
185							DACITE; brownish red and dark gray; very hard; unfractured and unweathered.	
190							185'	
195							DACITE; with zones of dark gray, brownish red/red, and white; hard; moderately fractured; weathered. Highly fractured at 185-188'.	
200								
205							Highly fractured at 203-205'.	
210								

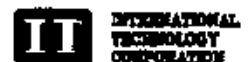
DRILLING CO.: Water Development Corporation
 DRILL METHOD: Air Rotary with Foam and Water

PAGE 3 OF 7

PROJECT NO.: ADBE02
 CLIENT: Benson Ridge
 LOCATION: Martinez, California

SEE LEGEND FOR LOGS AND TEST PITS
 FOR EXPLANATION OF SYMBOLS AND TERMS

BR-MW31(483)



DEPTH IN FEET		SAMPLE TYPE & NUMBER		RECOVERY/DRIVE (in.)		BLOWS PER FOOT (B)		WELL SUMMARY		USCS		PROFILE		BORING NO. MW-31	
		PROJ. GEOL. J.R. Mount		COORDINATES N 23071.1		E 41109.9		FIELD GEOLOGIST J. Murphy		EDITED BY J.R. Mount		DATE BEGAN 12-20-89		CHECKED BY P. McLaughlin	
		TOTAL DEPTH 455 ft		GROUND SURFACE EL. 1852.1											
														DESCRIPTION	
210														DACITE; dark gray, brownish red/red, and white; hard; moderately fractured; weathered.	
215														215'	
220														DACITE; color change to dark olive (groundmass), brownish red, and white; soft to moderately hard; moderately to severely fractured; weathered; minor phenocrysts.	
225															
230															
235														235'	
240														DACITE; dark olive, dark gray, reddish brown, yellow; very hard; slightly fractured; slightly weathered.	
245														Some fragments of turf or breccia.	
250															
255														245'	
260														DACITE; color changing to predominantly dark gray, with reddish brown, yellow, and white; moderately hard; moderately to severely fractured; slightly weathered.	
265														Excessive cuttings fall—in 260'-270', during drilling pause for pipe connections.	
270															
275														272'	
280														DACITE; color changing to light reddish gray and light brownish red with some dark gray and white; moderately hard to soft; severely fractured, vesicular.	
														Weathering surfaces more prominent.	

DRILLING CO.: Water Development Corporation
 DRILL METHOD: Air Rotary with Foam and Water

PAGE 4 OF 7

PROJECT NO.: ADBE02
 CLIENT: Benson Ridge
 LOCATION: Martinez, California

SEE LEGEND FOR LOGS AND TEST PITS
 FOR EXPLANATION OF SYMBOLS AND TERMS

BR-MW31(-BR3)



DEPTH IN FEET	SAMPLE TYPE & NUMBER	RECOVERY/DRIVE (in.)	BLOWS PER FOOT (N)	WELL SUMMARY	USCS	PROFILE	BORING NO. MW-31
							PROJ. GEOL. <u>J.R. Mount</u> FIELD GEOLOGIST <u>J. Murphy</u> EDITED BY <u>J.R. Mount</u> CHECKED BY <u>P. McLaughlin</u> TOTAL DEPTH <u>455 ft.</u> COORD. DATES <u>N 230211</u> <u>E 411088</u> DATE BEGAN <u>12-20-89</u> DATE FINISHED <u>1-2-90</u> GROUND SURFACE EL. <u>1852'</u>
							DESCRIPTION
280							DACITE; color changing to light reddish gray and light brownish red with some dark gray and white; moderately hard to soft; severely fractured, vesicular.
285							Weathering surfaces more prominent.
290							
295							
300							
305							DACITE; severely fractured; moderately weathered.
310							
315							
320							
325							
330							
335							
340							Crumbly, decomposed dacite chips.
345							
350							

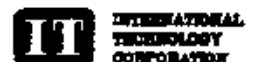
DRILLING CO.: Water Development Corporation
 DRILL METHOD: Air Rotary with Foam and Water

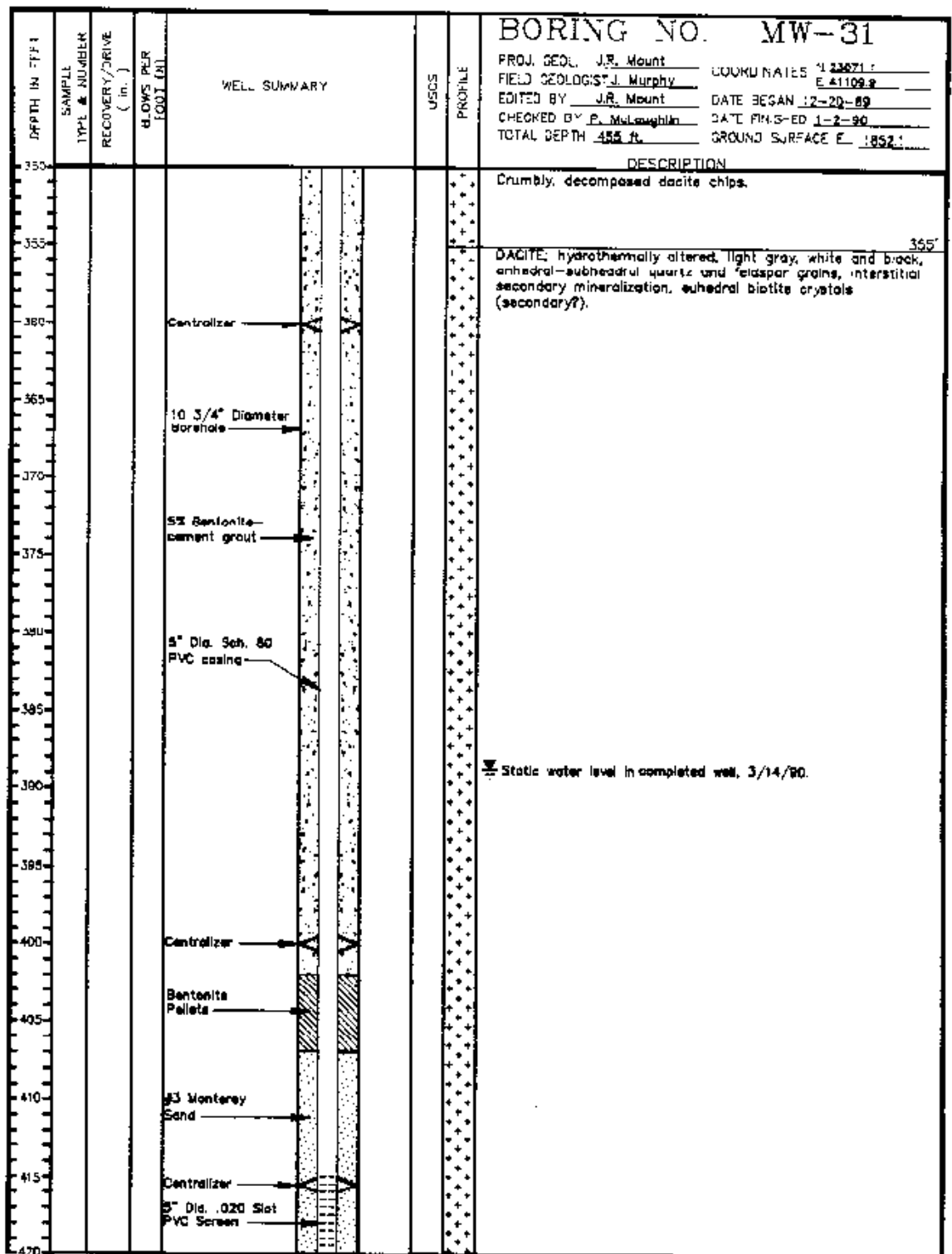
PAGE 5 OF 7

PROJECT NO.: ADBE02
 CLIENT: Benson Ridge
 LOCATION: Martinez, California

SEE LEGEND FOR LOGS AND TEST PITS
 FOR EXPLANATION OF SYMBOLS AND TERMS

BR-MW31(4BR3)





DRILLING CO.: Water Development Corporation
 DRILL METHOD: Air Rotary with Foam and Water

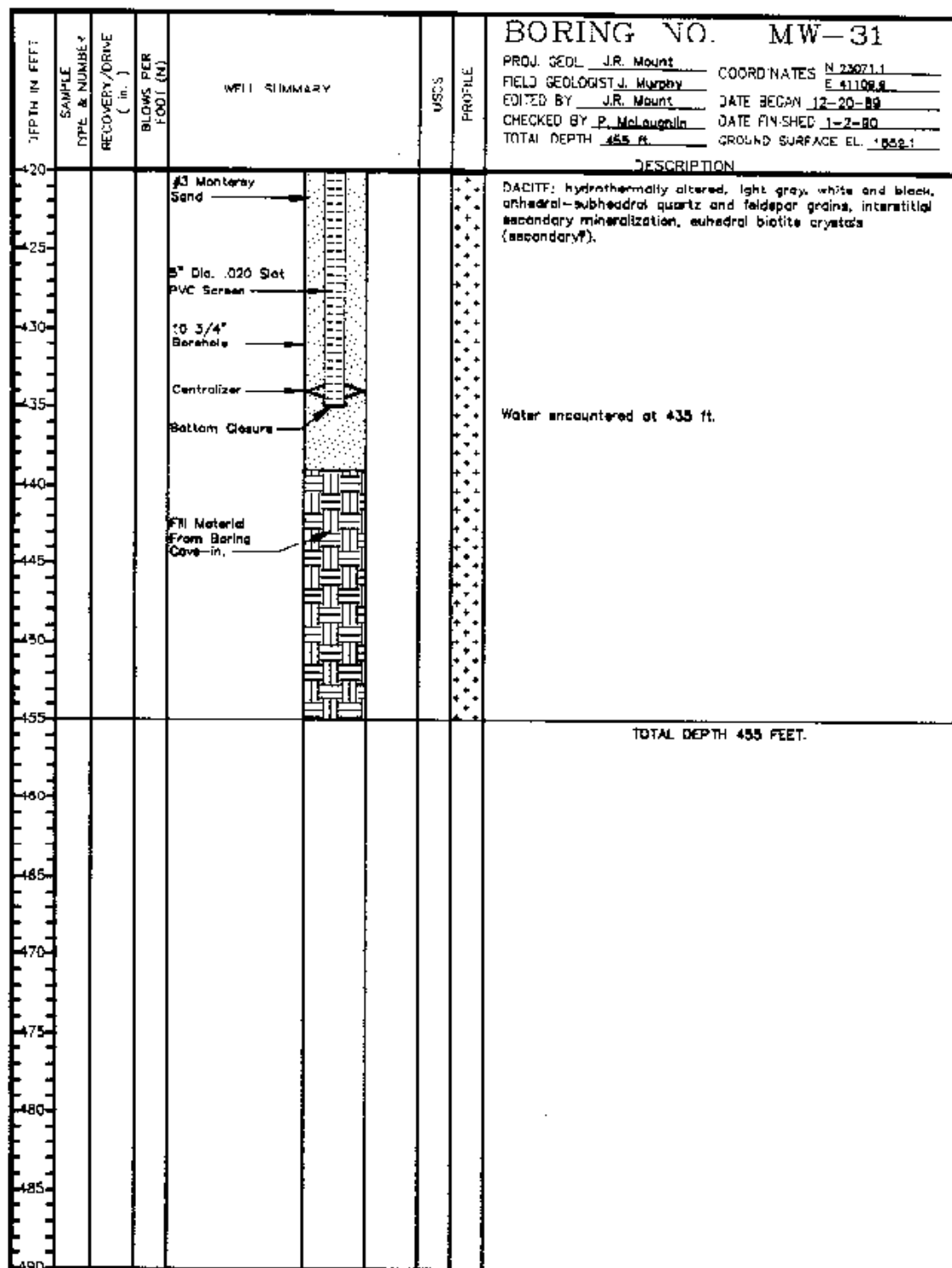
PAGE 6 OF 7

PROJECT NO.: AUB002
 CLIENT: Benson Ridge
 LOCATION: Martinez, California

SEE LEGEND FOR LOGS AND TEST PITS
 FOR EXPLANATION OF SYMBOLS AND TERMS

BR-MW31(-BR3)





DRILLING CO.: Water Development Corporation
 DRILL METHOD: Air Rotary with Foam and Water

PAGE 7 OF 7

PROJECT NO.: ADBE02
 CLIENT: Benson Ridge
 LOCATION: Martinez, California

SEE LEGEND FOR LOGS AND TEST PITS
 FOR EXPLANATION OF SYMBOLS AND TERMS

DR - MW31(-BR3)



ORIGINAL

File with DWR

 Notice of Intent No. _____
 Local Permit No. or Date _____

 STATE OF CALIFORNIA
 THE RESOURCES AGENCY
 DEPARTMENT OF WATER RESOURCES
 WATER WELL DRILLERS REPORT

13N/09W-25M

Do not fill in

No. 172378

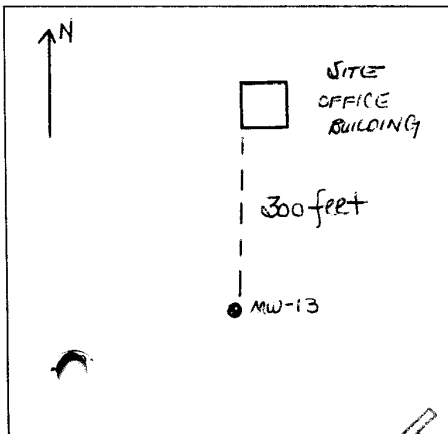
 State Well No. _____
 Other Well No. _____

 (12) WELL LOG: Total depth 370 ft. Depth of completed well 362 ft.
 from ft. to ft. Formation (Describe by color, character, size or material)

(2) LOCATION OF WELL (See instructions):

 County Lake Owner's Well Number MW-13
 Well address if different from above Benson Ridge Facility
 Township 13N Range 8W Section 30
 Distance from cities, roads, railroads, fences, etc. _____

See accompanying boring logs



WELL LOCATION SKETCH

(3) TYPE OF WORK:

 New Well ☒ Deepening ☐
 Reconstruction ☐
 Reconditioning ☐
 Horizontal Well ☐

 Destruction ☐ (Describe destruction materials and procedures in Item 12)

(4) PROPOSED USE:

 Domestic ☐
 Irrigation ☐
 Industrial ☐
 Test Well ☒
 Stock ☐
 Municipal ☐
 Other ☐

(5) EQUIPMENT:

 Rotary ☒ Reverse ☐
 Cable ☐ Air ☐
 Other ☐ Bucket ☐

(6) GRAVEL PACK:

 Yes ☒ No ☐ Size #2 sand
 Diameter of bore 8.5 inch
 Packed from 347 to 362 ft.

(7) CASING INSTALLED:

 Steel ☐ Plastic ☒ Concrete ☐

(8) PERFORATIONS:

Type of perforation or size of screen

From ft.	To ft.	Dia. in.	Gauge or Wall	From ft.	To ft.	Slot size
0	362	4	SM 40	352	362	.020 INCH

(9) WELL SEAL:

 Was surface sanitary seal provided? Yes ☒ No ☐ If yes, to depth _____ ft.
 Were strata sealed against pollution? Yes ☒ No ☐ Interval 0-347 ft.
 Method of sealing Bentonite pellets & grout

(10) WATER LEVELS:

 Depth of first water, if known 348 ft.
 Standing level after well completion 362.5 ft.

(11) WELL TESTS:

 Was well test made? Yes ☐ No ☒ If yes, by whom? _____
 Type of test Pump ☐ Bailer ☐ Air lift ☐
 Depth to water at start of test _____ ft. At end of test _____ ft.
 Discharge _____ gal/min after _____ hours Water temperature _____
 Chem. analysis made? Yes ☒ No ☐ If yes, by whom? IT CORP
 Was electric log made? Yes ☐ No ☒ If yes, attach copy to this report

 HAM Drilling Inc. 1407
 1538 WILLOW PASS RD.
 PITTSBURG, CA. 94565
 P.O. Box 1271

LICENSE # 426664 JAN 05 1987

 Work started September 26, 1984 Completed October 6, 1984

WELL DRILLER'S STATEMENT:

This well was drilled under my jurisdiction and this report is true to the best of my knowledge and belief.

SIGNED

(Well Driller)

NAME IT Corporation

(Person, firm, or corporation) (Typed or printed)

Address 17500 Red Hill Avenue

City Irvine

Zip 92714

License No. EG 940

Date of this report November 15, 1984

BORING NO. MW-13

COORDINATES N 300 Feet south of office building.
E _____

FIELD ENGINEER D. Collins DATE BEGAN 9/26/76
 EDITED BY D. Collins DATE FINISHED 10/06/84
 CHECKED BY M. Balderman GROUND SURFACE EL. APPROX. 1,768 feet
 TOTAL DEPTH 370 Feet

DESCRIPTION

Silty gravels with cobbles of dacite as described below.

TOP OF ROCK

Oxidized DACITE - aphanitic groundmass with 1 mm plagioclase and quartz phenocrysts. Reddish colored, froathy cinder (50%) and dark gray dacite fragments (50%) in cuttings. Small vesicles present.

Dark grey DACITE - No brick red fragments of cinder. No or few vesicles.

Balls of greenish clay with greenish chalcedony fragments coming up with cucking

Oxidized DACITE - with abundant red cinder.

Dark gray DACITE - no red cinders.

29 1/2" - heavy drill chatter rapid drilling.
Oxidized DACITE with approximately 50 percent
brick red cinders.

Dark grey DACITE - no red cinders, harder drilling.

40 1/4' - loss of drilling fluid. Medium greenish gray microcrystalline
 dacite with 1/2 mm black microphenocrysts altered
 to chlorite.

Medium gray aphanitic-no chlorite.

Rock with reddish stained, 1 mm to 5 mm long fractures. Also some greenish alteration coloring has returned. Iron oxide staining on fracture surfaces, with slight weathering.

Medium dark gray DACITE, sphanitic to micro-crystalline texture.



TH IN FEET

TESTS REPORTED ELSEWHERE

LIQUID LIMIT (%)	LI
10	10
20	20
30	30
40	40
50	50
60	60
70	70
80	80
90	90
100	100

PLASTICITY INDEX (%)

TYPE OF TEST	STR
1	1
2	2
3	3
4	4
5	5
6	6
7	7
8	8
9	9
10	10
11	11
12	12
13	13
14	14
15	15
16	16
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79	79
80	80
81	81
82	82
83	83
84	84
85	85
86	86
87	87
88	88
89	89
90	90
91	91
92	92
93	93
94	94
95	95
96	96
97	97
98	98
99	99
100	100

NORMAL OR
CONFINING
PRESSURE (PSF)

VIATOR STRESS
(PSE)

[illegible]

(PSF)	A
-------	---

DRY DENSITY
(%)

(PCF)

DRILL PENETRATION RATE

SAMPLE NUMBER

PROFILE

ROTARY AIR
— DRILLING —

— ROTARY SUD
— DRILLING

G-2	

G-3

		76	

SHOD DRILLING —

G-5	

ONLY AIR DRILLING

----- ROTAM -----

6-6	
-----	--

PROJECT NO. 5440461

LABORATORY TEST DATA

BORING NO. MW-13

COORDINATES N 40° 40' 00" S E 100° 00' 00" W

FIELD ENGINEER D. Collins DATE BEGAN 9/26/84
 EDITED BY D. Collins DATE FINISHED 10/06/84
 CHECKED BY M. Balderman GROUND SURFACE EL. APPROX. 1,768 Feet
 TOTAL DEPTH 370 Feet

DESCRIPTION

DEPTH IN FEET

ATTERBERG LIMITS		STRENGTH TEST DATA				MOISTURE CONTENT (%)	DRY DENSITY (PCF)
LIQUID LIMIT (%)	PLASTICITY INDEX (%)	TYPE OF TEST	NORMAL OR CONFINING PRESSURE (PSF)	DEVIATOR STRESS (PSF)	SHEAR STRENGTH (PSF)		

DRILL PENETRATION RATE

SAMPLE NUMBER

PROFILE

70
75
80
85
90
95
100
105
110
115
120
125
130
135

ROTARY AIR DRILLING

G-8

G-9

G-10

G-11

G-12

G-13

G-14

Contains some reddish discontinuous streaks, occasional greenish alteration on fractures.

Oxidized DACITE - with red cinders in cutting; faster drilling.

Dark grey DACITE.

101' loss of air circulation. No cuttings returning.

Oxidized DACITE with approximately 25 percent brick red cinder fragments. Increases to 45 percent. Damp.

111' - 80 percent red cinders. Overall color is murre-red.

Dark grey DACITE.

LABORATORY TEST DATA										DRILL PENETRATION RATE		SAMPLE NUMBER	PROFILE	BORING NO. MW-13		
ATTERBERG LIMITS		STRENGTH TEST DATA				MOISTURE CONTENT (%)	DRY DENSITY (PCF)									
TESTS REPORTED ELSEWHERE	LIQUID LIMIT (%)	PLASTICITY INDEX (%)	TYPE OF TEST	NORMAL OR CONFINING PRESSURE (PSF)	DEVIATOR STRESS (PSF)			SHEAR STRENGTH (PSF)								
DEPTH IN FEET	140															
	145															
	150															
	155															
	160															
	165															
	170															
	175															
	180															
	185															
190																
195																
200																
205																

COORDINATES		DATE		FIELD ENGINEER		DATE BEGAN		EDITED BY		DATE FINISHED		CHECKED BY		GROUND SURFACE EL.		TOTAL DEPTH	
N	101 E. E. south of office building.			D. Collins	9/26/84	D. Collins	10/16/84	M. Halderman	Approximately 1.745	170 Feet							

DESCRIPTION	
Dark grey DACITE - as before, microcrystalline to aphanitic texture. Greenish colored quartz is distinguishable. Also has 1 mm plagioclase crystals.	161.0'
Oxidized DACITE - Purplish gray colored rock with 5 percent brick red colored cinder.	167.0'
Dark grey DACITE.	172.0'
Oxidized DACITE - Contains abundant red cinders. Much faster drilling.	

LABORATORY TEST DATA										BORING NO. MW-13	
DEPTH IN FEET	TESTS REPORTED ELSEWHERE	ATTERBERG LIMITS		STRENGTH TEST DATA				DRILL PENETRATION RATE	SAMPLE NUMBER	PROFILE	DESCRIPTION
		LIQUID LIMIT (%)	PLASTICITY INDEX (%)	TYPE OF TEST	NORMAL OR CONFINING PRESSURE (PSF)	DEVIATOR STRESS (PSF)	SHEAR STRENGTH (PSF)				
210											Oxidized DACITE - as before.
215											
220											
225											
230											Greenish grey DACITE - dark to light grey greenish grey aphanitic. Partially altered to give grayish-white rock fragments with greenish chlorite patches and hydrothermally attacked plagioclase crystals. Slower drilling than above rock; medium coarse cuttings up to 1/4" or 1/2".
235											
240											G-21 FOAM DRILLING
245											
250											G-22 G-22 sample: Medium to light greenish colored, aphanitic to microcrystalline with some microporphyritic textures present. Basic color is greenish with pinkish white patches.
255											
260											
265											
270											G-21
275											

PROJECT NO. RLW 40

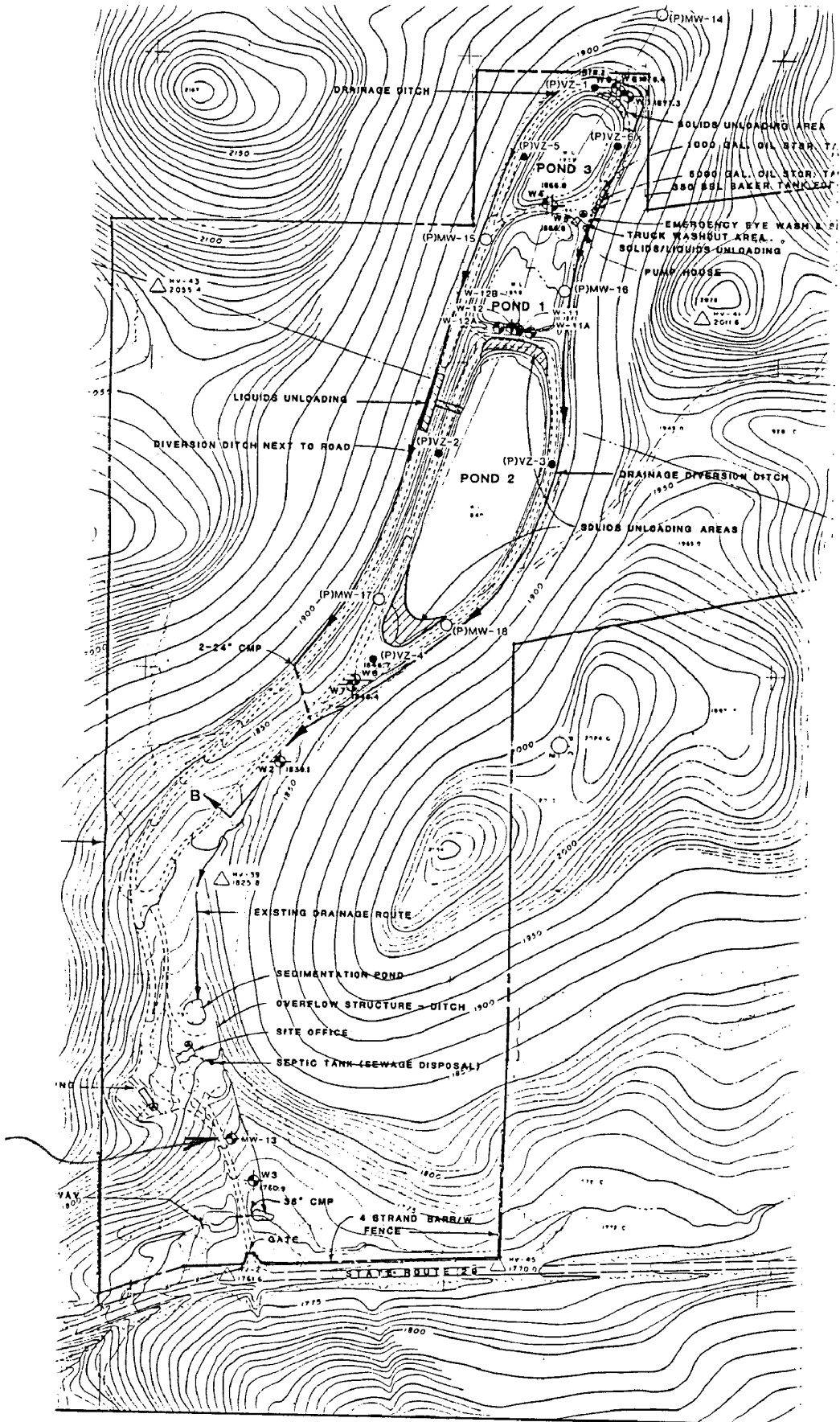
IT CORPORATION
IT CORPORATION

COORDINATES N 300 feet south of office building.
E _____

FIELD ENGINEER D. Collins DATE BEGAN 9/26/84
 EDITED BY D. Collins DATE FINISHED 10/06/84
 CHECKED BY M. Balderman GROUND SURFACE EL. Approx. 1,764 Feet
 TOTAL DEPTH 370 Feet

HYDROTHERMALLY ALTERED DACITE - as before.

TOTAL DEPTH 370 FEET



BENSON RIDGE
WELL LOCATIONS

D'WN
RVH
1-30-85
CHECKED BY
APPROVED BY
DRAWING
5/28/84
NUMBER
84-10-A14

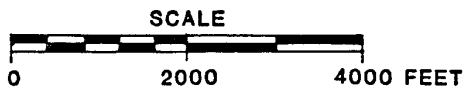
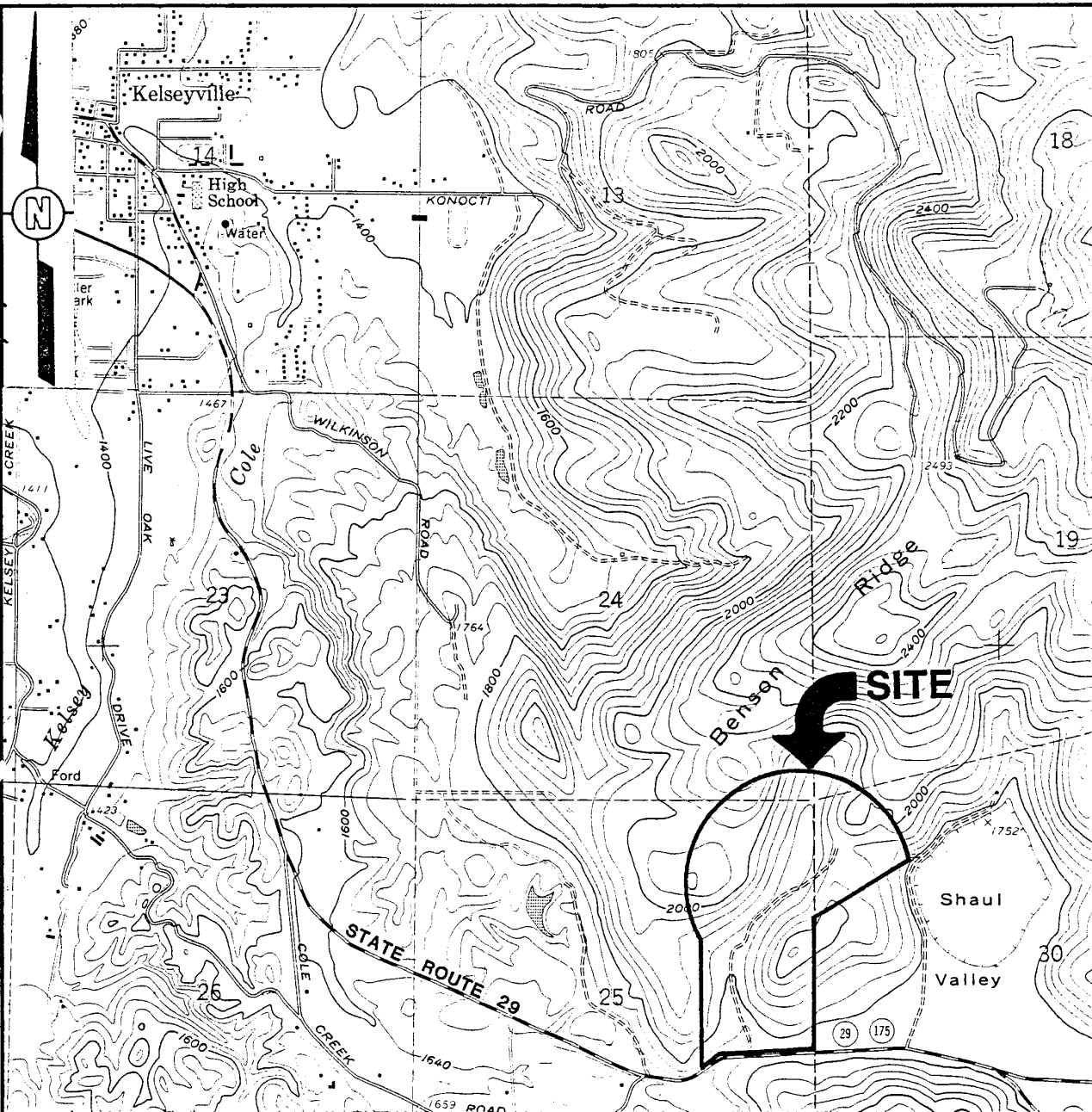


FIGURE 1

SITE LOCATION MAP

BENSON RIDGE FACILITY

PREPARED FOR

IT CORPORATION BENSON RIDGE FACILITY

REFERENCE:

7.5 MINUTE U.S.G.S. TOPOGRAPHIC MAP
OF KELSEYVILLE CALIFORNIA QUADRANGLE
DATED: 1959, PHOTOREVISED 1975
SCALE 1:24,000

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... Creating a Safer Tomorrow

"Do Not Scale This Drawing"

ORIGINAL

File with DWR

STATE OF CALIFORNIA

THE RESOURCES AGENCY

DEPARTMENT OF WATER RESOURCES

WATER WELL DRILLERS REPORT

Do not fill in

No. 087440

CONFIDENTIAL LOG

State Well No. Water Code Sec. 13752

Other Well No. _____

Notice of Intent No. _____

Permit No. or Date _____

(1) OV

Address _____

City _____

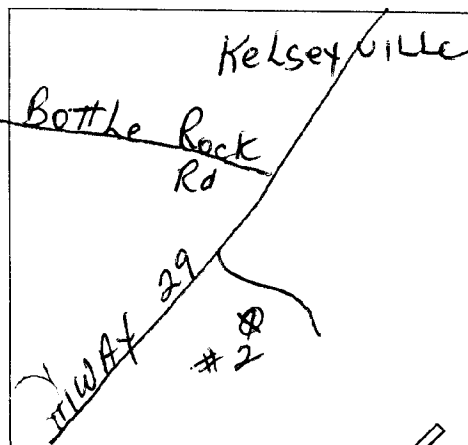
(2) LOCATION OF WELL (See instructions):

County Lake Owner's Well Number _____

Well address if different from above _____

Township _____ Range _____ Section _____

Distance from cities, roads, railroads, fences, etc. _____

7620 Hiway 29Kelseyville

(3) TYPE OF WORK:

New Well ☒ Deepening ☐Reconstruction ☐Reconditioning ☐Horizontal Well ☐Destruction ☐ (Describe destruction materials and procedures in Item 12)

(4) PROPOSED USE:

Domestic ☐Irrigation ☐Industrial ☐Test Well ☐Stock ☐Municipal ☐Other ☒ observation(12) WELL LOG: Total depth 159 ft. Depth of completed well 159 ft.
from ft. to ft. Formation (Describe by color, character, size or material)

OBSERVATION HOLE # 2

0 - 18 Sand & rocks
 18 - 23 Clayee sand & rocks
 23 - 38 Brown sandy clay & clayee
 - brown sand w/rocks
 38 - 46 Highly fractured rock
 46 - 63 Volcanic conglomerate rock
 63 - 80 Very hard multicolored conglomerate rock
 80 - 159 Hard multicolored conglomerate rock

WELL LOCATION SKETCH

(5) EQUIPMENT:

Rotary ☐Reverse ☐Cable ☐Air ☒Other ☐Bucket ☐

(6) GRAVEL PACK:

Yes ☒ No ☐Size 1/8"Diameter of bore 9 7/8"Packed from 10' to 159'

(7) CASING INSTALLED:

Steel ☐Plastic ☒Concrete ☐

(8) PERFORATIONS:

sawn

Type of perforation or size of screen

From ft.	To ft.	Dia. in.	Gage or Wall	From ft.	To ft.	Slot size
0	162	4 1/2"	200 PSI	119	159	
				22	119	1/8x4"

(9) WELL SEAL:

Was surface sanitary seal provided? Yes ☒ No ☐ If yes, to depth 10' ft.Were strata sealed against pollution? Yes ☐ No ☒ Interval _____ ft.Method of sealing cement on gravel pack

(10) WATER LEVELS:

Depth of first water, if known _____ ft.

Standing level after well completion _____ ft.

(11) WELL TESTS:

Was well test made? Yes ☐ No ☒ If yes, by whom? _____Type of test Pump ☐ Bailer ☐ Air lift ☐

Depth to water at start of test _____ ft. At end of test _____ ft.

Discharge _____ gal/min after _____ hours Water temperature _____

Cal analysis made? Yes ☐ No ☒ If yes, by whom? _____Electric log made? Yes ☐ No ☒ If yes, attach copy to this reportWork started July 13, 19 79 Completed July 16, 19 79

WELL DRILLER'S STATEMENT:

This well was drilled under my jurisdiction and this report is true to the best of my knowledge and belief.

SIGNED Gerald Thompson By: Mary E. Thompson
(Well Driller)NAME WEEKS DRILLING AND PUMP COMPANY

(Person, firm, or corporation) (Typed or printed)

Address Sebastopol RoadCity Sebastopol, California 95472License No. C57-177681 Date of this report July 23, 1979

DWR 188 (REV. 7-76)

IF ADDITIONAL SPACE IS NEEDED, USE NEXT CONSECUTIVELY NUMBERED FORM

Permit Date 6/5/2015

IF ADDITIONAL SPACE IS NEEDED, USE NEXT CONSECUTIVELY NUMBERED FORM

ORIGINAL
File with DWR

STATE OF CALIFORNIA
THE RESOURCES AGENCY
DEPARTMENT OF WATER RESOURCES
WATER WELL DRILLERS REPORT

No. 087444

State Well No. _____
Other Well No. _____

Permit No. or Date _____

(1) OV

Address _____

City _____

(2) LOCATION OF WELL (See instructions):

County Lake Owner's Well Number _____

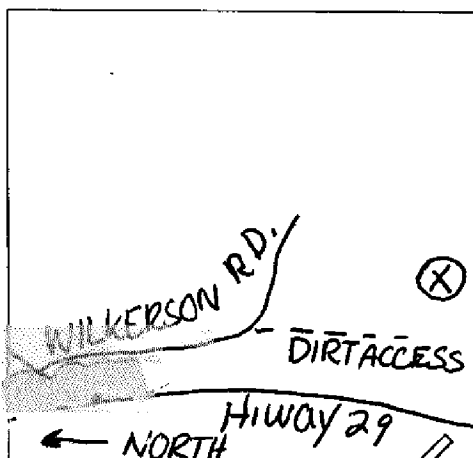
Well address if different from above _____

Township _____ Range _____ Section _____

Distance from cities, roads, railroads, fences, etc. _____

Wilkinson Road

Kelseyville



WELL LOCATION SKETCH

(3) TYPE OF WORK:

New Well ☒ Deepening ☐

Reconstruction ☐

Reconditioning ☐

Horizontal Well ☐

Destruction ☐ (Describe destruction materials and procedures in Item 12)

(4) PROPOSED USE:

Domestic ☒

Irrigation ☐

Industrial ☐

Test Well ☐

Stock ☐

Municipal ☐

Other ☐

(12) WELL LOG: Total depth 263 ft. Depth of completed well 263 ft.
from ft. to ft. Formation (Describe by color, character, size or material)

UNCASED DRY HOLE # 1

0 - 1 Red volcanic's
1 - 6 Red volcanic clay
6 - 10 Volcanic conglomerate
10 - 12 Hard red volcanic rock
12 - 29 Multicolored conglomerate rock
29 - 33 Moist brown sand & rocks
33 - 38 Multicolored volcanic conglomerate
38 - 194 Tan tuffa
194 - 263 Hard multicolored volcanic rock w/ occasional fracture

(5) EQUIPMENT:

Rotary ☐

Reverse ☐

Cable ☐

Air ☒

Other ☐

Bucket ☐

(6) GRAVEL PACK:

Yes ☐ No ☒

Size _____

Diameter of bore 9 7/8 - 10 1/2"

Packed from _____

(7) CASING INSTALLED:

Steel ☐

Plastic ☐

Concrete ☒

(8) PERFORATIONS:

Type of perforation or size of screen _____

From ft.	To ft.	Dia. in.	Cage or Wall	From ft.	To ft.	Slot size

(9) WELL SEAL:

Was surface sanitary seal provided? Yes ☐ No ☐ If yes, to depth _____ ft.

Were strata sealed against pollution? Yes ☐ No ☐ Interval _____ ft.

Method of sealing _____

(10) WATER LEVELS:

Depth of first water, if known _____ ft.

Standing level after well completion _____ ft.

(11) WELL TESTS:

Was well test made? Yes ☐ No ☐ If yes, by whom? _____

Type of test Pump ☐ Bailer ☐ Air lift ☐

Depth to water at start of test _____ ft. At end of test _____ ft.

Discharge in _____ min after _____ hours Water temperature _____

Was well sealed? Yes ☐ No ☐ If yes, by whom? _____

Was discharge log made? Yes ☐ No ☐ If yes, attach copy to this report

Work started July 9, 1979 Completed July 11, 1979

WELL DRILLER'S STATEMENT:

This well was drilled under my jurisdiction and this report is true to the best of my knowledge and belief.

SIGNED Gerald Thompson By: Mary E. Thompson

(Well Driller)

NAME WEEKS DRILLING AND PUMP COMPANY

(Person, firm, or corporation) (Typed or printed)

Address Sebastopol Road

City Sebastopol, California Zip 95472

License No. 057-177681 Date of this report July 25, 1979

APPENDIX B

WELL YIELD TEST LOG

Static Water Level¹ (ft): Static - 500', Depth of well - 598'

¹ Measured from the established ground surface. ² Water level minus static level.

APPENDIX C



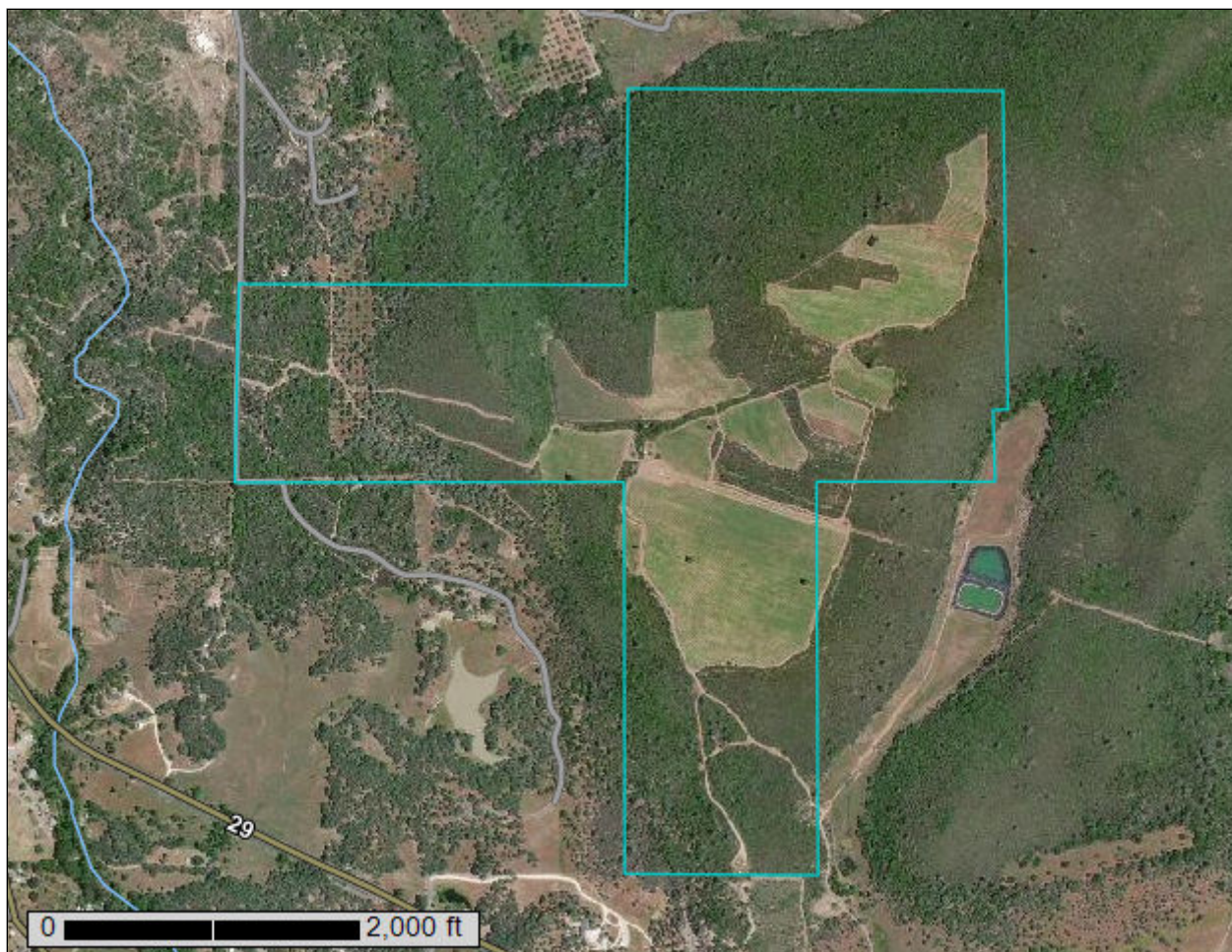
United States
Department of
Agriculture

NRCS

Natural
Resources
Conservation
Service

A product of the National
Cooperative Soil Survey,
a joint effort of the United
States Department of
Agriculture and other
Federal agencies, State
agencies including the
Agricultural Experiment
Stations, and local
participants

Custom Soil Resource Report for Lake County, California



January 6, 2022

Preface

Soil surveys contain information that affects land use planning in survey areas. They highlight soil limitations that affect various land uses and provide information about the properties of the soils in the survey areas. Soil surveys are designed for many different users, including farmers, ranchers, foresters, agronomists, urban planners, community officials, engineers, developers, builders, and home buyers. Also, conservationists, teachers, students, and specialists in recreation, waste disposal, and pollution control can use the surveys to help them understand, protect, or enhance the environment.

Various land use regulations of Federal, State, and local governments may impose special restrictions on land use or land treatment. Soil surveys identify soil properties that are used in making various land use or land treatment decisions. The information is intended to help the land users identify and reduce the effects of soil limitations on various land uses. The landowner or user is responsible for identifying and complying with existing laws and regulations.

Although soil survey information can be used for general farm, local, and wider area planning, onsite investigation is needed to supplement this information in some cases. Examples include soil quality assessments (<http://www.nrcs.usda.gov/wps/portal/nrcs/main/soils/health/>) and certain conservation and engineering applications. For more detailed information, contact your local USDA Service Center (<https://offices.sc.egov.usda.gov/locator/app?agency=nrcs>) or your NRCS State Soil Scientist (http://www.nrcs.usda.gov/wps/portal/nrcs/detail/soils/contactus/?cid=nrcs142p2_053951).

Great differences in soil properties can occur within short distances. Some soils are seasonally wet or subject to flooding. Some are too unstable to be used as a foundation for buildings or roads. Clayey or wet soils are poorly suited to use as septic tank absorption fields. A high water table makes a soil poorly suited to basements or underground installations.

The National Cooperative Soil Survey is a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local agencies. The Natural Resources Conservation Service (NRCS) has leadership for the Federal part of the National Cooperative Soil Survey.

Information about soils is updated periodically. Updated information is available through the NRCS Web Soil Survey, the site for official soil survey information.

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How Soil Surveys Are Made

Soil surveys are made to provide information about the soils and miscellaneous areas in a specific area. They include a description of the soils and miscellaneous areas and their location on the landscape and tables that show soil properties and limitations affecting various uses. Soil scientists observed the steepness, length, and shape of the slopes; the general pattern of drainage; the kinds of crops and native plants; and the kinds of bedrock. They observed and described many soil profiles. A soil profile is the sequence of natural layers, or horizons, in a soil. The profile extends from the surface down into the unconsolidated material in which the soil formed or from the surface down to bedrock. The unconsolidated material is devoid of roots and other living organisms and has not been changed by other biological activity.

Currently, soils are mapped according to the boundaries of major land resource areas (MLRAs). MLRAs are geographically associated land resource units that share common characteristics related to physiography, geology, climate, water resources, soils, biological resources, and land uses (USDA, 2006). Soil survey areas typically consist of parts of one or more MLRA.

The soils and miscellaneous areas in a survey area occur in an orderly pattern that is related to the geology, landforms, relief, climate, and natural vegetation of the area. Each kind of soil and miscellaneous area is associated with a particular kind of landform or with a segment of the landform. By observing the soils and miscellaneous areas in the survey area and relating their position to specific segments of the landform, a soil scientist develops a concept, or model, of how they were formed. Thus, during mapping, this model enables the soil scientist to predict with a considerable degree of accuracy the kind of soil or miscellaneous area at a specific location on the landscape.

Commonly, individual soils on the landscape merge into one another as their characteristics gradually change. To construct an accurate soil map, however, soil scientists must determine the boundaries between the soils. They can observe only a limited number of soil profiles. Nevertheless, these observations, supplemented by an understanding of the soil-vegetation-landscape relationship, are sufficient to verify predictions of the kinds of soil in an area and to determine the boundaries.

Soil scientists recorded the characteristics of the soil profiles that they studied. They noted soil color, texture, size and shape of soil aggregates, kind and amount of rock fragments, distribution of plant roots, reaction, and other features that enable them to identify soils. After describing the soils in the survey area and determining their properties, the soil scientists assigned the soils to taxonomic classes (units). Taxonomic classes are concepts. Each taxonomic class has a set of soil characteristics with precisely defined limits. The classes are used as a basis for comparison to classify soils systematically. Soil taxonomy, the system of taxonomic classification used in the United States, is based mainly on the kind and character of soil properties and the arrangement of horizons within the profile. After the soil

scientists classified and named the soils in the survey area, they compared the individual soils with similar soils in the same taxonomic class in other areas so that they could confirm data and assemble additional data based on experience and research.

The objective of soil mapping is not to delineate pure map unit components; the objective is to separate the landscape into landforms or landform segments that have similar use and management requirements. Each map unit is defined by a unique combination of soil components and/or miscellaneous areas in predictable proportions. Some components may be highly contrasting to the other components of the map unit. The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The delineation of such landforms and landform segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, onsite investigation is needed to define and locate the soils and miscellaneous areas.

Soil scientists make many field observations in the process of producing a soil map. The frequency of observation is dependent upon several factors, including scale of mapping, intensity of mapping, design of map units, complexity of the landscape, and experience of the soil scientist. Observations are made to test and refine the soil-landscape model and predictions and to verify the classification of the soils at specific locations. Once the soil-landscape model is refined, a significantly smaller number of measurements of individual soil properties are made and recorded. These measurements may include field measurements, such as those for color, depth to bedrock, and texture, and laboratory measurements, such as those for content of sand, silt, clay, salt, and other components. Properties of each soil typically vary from one point to another across the landscape.

Observations for map unit components are aggregated to develop ranges of characteristics for the components. The aggregated values are presented. Direct measurements do not exist for every property presented for every map unit component. Values for some properties are estimated from combinations of other properties.

While a soil survey is in progress, samples of some of the soils in the area generally are collected for laboratory analyses and for engineering tests. Soil scientists interpret the data from these analyses and tests as well as the field-observed characteristics and the soil properties to determine the expected behavior of the soils under different uses. Interpretations for all of the soils are field tested through observation of the soils in different uses and under different levels of management. Some interpretations are modified to fit local conditions, and some new interpretations are developed to meet local needs. Data are assembled from other sources, such as research information, production records, and field experience of specialists. For example, data on crop yields under defined levels of management are assembled from farm records and from field or plot experiments on the same kinds of soil.

Predictions about soil behavior are based not only on soil properties but also on such variables as climate and biological activity. Soil conditions are predictable over long periods of time, but they are not predictable from year to year. For example, soil scientists can predict with a fairly high degree of accuracy that a given soil will have a high water table within certain depths in most years, but they cannot predict that a high water table will always be at a specific level in the soil on a specific date.

After soil scientists located and identified the significant natural bodies of soil in the survey area, they drew the boundaries of these bodies on aerial photographs and

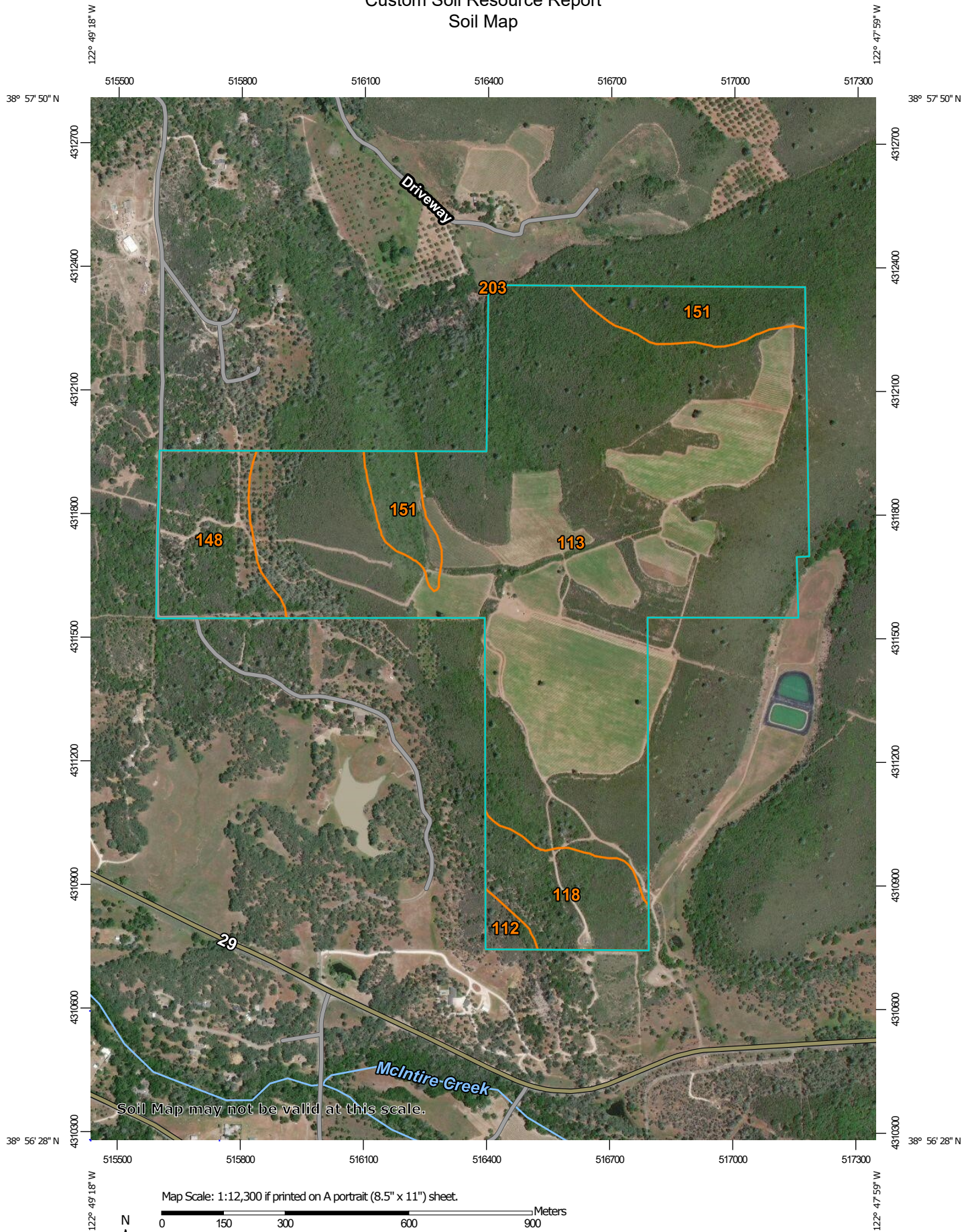
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identified each as a specific map unit. Aerial photographs show trees, buildings, fields, roads, and rivers, all of which help in locating boundaries accurately.

Soil Map

The soil map section includes the soil map for the defined area of interest, a list of soil map units on the map and extent of each map unit, and cartographic symbols displayed on the map. Also presented are various metadata about data used to produce the map, and a description of each soil map unit.

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MAP LEGEND

Area of Interest (AOI)

 Area of Interest (AOI)

Soils

 Soil Map Unit Polygons

 Soil Map Unit Lines

 Soil Map Unit Points

Special Point Features

 Blowout

 Borrow Pit


 Clay Spot


 Closed Depression

 Gravel Pit

 Gravelly Spot


 Landfill

 Lava Flow

 Marsh or swamp

 Mine or Quarry

 Miscellaneous Water

 Perennial Water

 Rock Outcrop


 Saline Spot

 Sandy Spot

 Severely Eroded Spot

 Sinkhole

 Slide or Slip

 Sodic Spot


 Spoil Area

 Stony Spot

 Very Stony Spot

 Wet Spot

 Other

 Special Line Features

Water Features

 Streams and Canals

Transportation

 Rails

 Interstate Highways

 US Routes

 Major Roads

 Local Roads

Background

 Aerial Photography

MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:24,000.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service
Web Soil Survey URL:
Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: Lake County, California
Survey Area Data: Version 18, Sep 6, 2021

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Sep 18, 2016—Nov 4, 2017

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Map Unit Legend

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
112	Benridge-Konocti association, 15 to 30 percent slopes	2.8	0.9%
113	Benridge-Konocti association, 30 to 50 percent slopes	241.6	76.7%
118	Bottlerock-Glenview-Arrowhead complex, 30 to 50 percent slopes	21.1	6.7%
148	Kidd-Forward complex, 5 to 30 percent slopes	24.9	7.9%
151	Konocti-Benridge complex, 50 to 75 percent slopes	24.4	7.7%
203	San Joaquin variant fine sandy loam, 0 to 5 percent slopes	0.1	0.0%
Totals for Area of Interest		314.8	100.0%

Map Unit Descriptions

The map units delineated on the detailed soil maps in a soil survey represent the soils or miscellaneous areas in the survey area. The map unit descriptions, along with the maps, can be used to determine the composition and properties of a unit.

A map unit delineation on a soil map represents an area dominated by one or more major kinds of soil or miscellaneous areas. A map unit is identified and named according to the taxonomic classification of the dominant soils. Within a taxonomic class there are precisely defined limits for the properties of the soils. On the landscape, however, the soils are natural phenomena, and they have the characteristic variability of all natural phenomena. Thus, the range of some observed properties may extend beyond the limits defined for a taxonomic class. Areas of soils of a single taxonomic class rarely, if ever, can be mapped without including areas of other taxonomic classes. Consequently, every map unit is made up of the soils or miscellaneous areas for which it is named and some minor components that belong to taxonomic classes other than those of the major soils.

Most minor soils have properties similar to those of the dominant soil or soils in the map unit, and thus they do not affect use and management. These are called noncontrasting, or similar, components. They may or may not be mentioned in a particular map unit description. Other minor components, however, have properties and behavioral characteristics divergent enough to affect use or to require different management. These are called contrasting, or dissimilar, components. They generally are in small areas and could not be mapped separately because of the scale used. Some small areas of strongly contrasting soils or miscellaneous areas are identified by a special symbol on the maps. If included in the database for a given area, the contrasting minor components are identified in the map unit descriptions along with some characteristics of each. A few areas of minor components may not have been observed, and consequently they are not

mentioned in the descriptions, especially where the pattern was so complex that it was impractical to make enough observations to identify all the soils and miscellaneous areas on the landscape.

The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The objective of mapping is not to delineate pure taxonomic classes but rather to separate the landscape into landforms or landform segments that have similar use and management requirements. The delineation of such segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, however, onsite investigation is needed to define and locate the soils and miscellaneous areas.

An identifying symbol precedes the map unit name in the map unit descriptions. Each description includes general facts about the unit and gives important soil properties and qualities.

Soils that have profiles that are almost alike make up a *soil series*. Except for differences in texture of the surface layer, all the soils of a series have major horizons that are similar in composition, thickness, and arrangement.

Soils of one series can differ in texture of the surface layer, slope, stoniness, salinity, degree of erosion, and other characteristics that affect their use. On the basis of such differences, a soil series is divided into *soil phases*. Most of the areas shown on the detailed soil maps are phases of soil series. The name of a soil phase commonly indicates a feature that affects use or management. For example, Alpha silt loam, 0 to 2 percent slopes, is a phase of the Alpha series.

Some map units are made up of two or more major soils or miscellaneous areas. These map units are complexes, associations, or undifferentiated groups.

A *complex* consists of two or more soils or miscellaneous areas in such an intricate pattern or in such small areas that they cannot be shown separately on the maps. The pattern and proportion of the soils or miscellaneous areas are somewhat similar in all areas. Alpha-Beta complex, 0 to 6 percent slopes, is an example.

An *association* is made up of two or more geographically associated soils or miscellaneous areas that are shown as one unit on the maps. Because of present or anticipated uses of the map units in the survey area, it was not considered practical or necessary to map the soils or miscellaneous areas separately. The pattern and relative proportion of the soils or miscellaneous areas are somewhat similar. Alpha-Beta association, 0 to 2 percent slopes, is an example.

An *undifferentiated group* is made up of two or more soils or miscellaneous areas that could be mapped individually but are mapped as one unit because similar interpretations can be made for use and management. The pattern and proportion of the soils or miscellaneous areas in a mapped area are not uniform. An area can be made up of only one of the major soils or miscellaneous areas, or it can be made up of all of them. Alpha and Beta soils, 0 to 2 percent slopes, is an example.

Some surveys include *miscellaneous areas*. Such areas have little or no soil material and support little or no vegetation. Rock outcrop is an example.

Lake County, California

112—Benridge-Konocti association, 15 to 30 percent slopes

Map Unit Setting

National map unit symbol: hf52
Elevation: 1,000 to 4,500 feet
Mean annual precipitation: 30 to 35 inches
Mean annual air temperature: 57 degrees F
Frost-free period: 140 to 200 days
Farmland classification: Not prime farmland

Map Unit Composition

Benridge and similar soils: 40 percent
Konocti and similar soils: 20 percent
Konocti and similar soils: 20 percent
Minor components: 20 percent
Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Benridge

Setting

Landform: Hills, mountains
Landform position (two-dimensional): Backslope
Landform position (three-dimensional): Upper third of mountainflank, side slope
Down-slope shape: Concave, linear
Across-slope shape: Convex, linear
Parent material: Volcanic ash

Typical profile

H1 - 0 to 6 inches: loam
H2 - 6 to 21 inches: gravelly clay loam
H3 - 21 to 63 inches: gravelly clay
H4 - 63 to 68 inches: gravelly clay

Properties and qualities

Slope: 15 to 30 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Well drained
Runoff class: High
Capacity of the most limiting layer to transmit water (Ksat): Moderately high (0.20 to 0.57 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Available water supply, 0 to 60 inches: Moderate (about 8.6 inches)

Interpretive groups

Land capability classification (irrigated): None specified
Land capability classification (nonirrigated): 4e
Hydrologic Soil Group: C
Ecological site: R015XY014CA - Loamy Mountains 20-40"ppt
Hydric soil rating: No

Description of Konocti

Setting

Landform: Hills, mountains, ravines, ridges

Landform position (two-dimensional): Shoulder, backslope, summit

Landform position (three-dimensional): Upper third of mountainflank, side slope, nose slope

Down-slope shape: Concave, linear

Across-slope shape: Convex, linear

Parent material: Residuum weathered from andesite

Typical profile

H1 - 0 to 8 inches: cobbly loam

H2 - 8 to 16 inches: stony loam

H3 - 16 to 32 inches: very stony sandy clay loam

H4 - 32 to 39 inches: very stony sandy loam

H5 - 39 to 49 inches: bedrock

Properties and qualities

Slope: 15 to 30 percent

Depth to restrictive feature: 39 to 43 inches to lithic bedrock

Drainage class: Well drained

Runoff class: High

Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately low (0.00 to 0.06 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None

Frequency of ponding: None

Available water supply, 0 to 60 inches: Low (about 4.1 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 4e

Hydrologic Soil Group: C

Ecological site: R015XY009CA - Hills 20-40"ppt

Hydric soil rating: No

Description of Konocti

Setting

Landform: Hills, mountains, ridges, ravines

Landform position (two-dimensional): Shoulder, backslope, summit

Landform position (three-dimensional): Upper third of mountainflank, side slope, nose slope

Down-slope shape: Concave, linear

Across-slope shape: Convex, linear

Parent material: Residuum weathered from andesite

Typical profile

H1 - 0 to 4 inches: stony loam

H2 - 4 to 11 inches: stony loam

H3 - 11 to 28 inches: very stony sandy clay loam

H4 - 28 to 38 inches: bedrock

Properties and qualities

Slope: 15 to 30 percent

Surface area covered with cobbles, stones or boulders: 0.1 percent

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Depth to restrictive feature: 28 to 32 inches to lithic bedrock
Drainage class: Well drained
Runoff class: High
Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately low (0.00 to 0.06 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Available water supply, 0 to 60 inches: Low (about 3.1 inches)

Interpretive groups

Land capability classification (irrigated): None specified
Land capability classification (nonirrigated): 4e
Hydrologic Soil Group: C
Ecological site: R015XY009CA - Hills 20-40"ppt
Hydric soil rating: No

Minor Components

Konocti, variant

Percent of map unit: 4 percent
Hydric soil rating: No

Steeper slopes

Percent of map unit: 4 percent
Hydric soil rating: No

Rock outcrop

Percent of map unit: 4 percent
Hydric soil rating: No

Gentler slopes

Percent of map unit: 4 percent
Hydric soil rating: No

Unnamed

Percent of map unit: 4 percent
Hydric soil rating: No

113—Benridge-Konocti association, 30 to 50 percent slopes

Map Unit Setting

National map unit symbol: hf53
Elevation: 1,000 to 4,500 feet
Mean annual precipitation: 30 to 35 inches
Mean annual air temperature: 57 degrees F
Frost-free period: 140 to 200 days
Farmland classification: Not prime farmland

Map Unit Composition

Benridge and similar soils: 40 percent

Konocti and similar soils: 30 percent

Konocti and similar soils: 15 percent

Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Benridge

Setting

Landform: Hills, mountains

Landform position (two-dimensional): Backslope

Landform position (three-dimensional): Upper third of mountainflank, side slope

Down-slope shape: Concave, linear

Across-slope shape: Convex, linear

Parent material: Volcanic ash

Typical profile

H1 - 0 to 6 inches: loam

H2 - 6 to 21 inches: gravelly clay loam

H3 - 21 to 63 inches: gravelly clay

H4 - 63 to 68 inches: gravelly clay

Properties and qualities

Slope: 30 to 50 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Well drained

Runoff class: High

Capacity of the most limiting layer to transmit water (Ksat): Moderately high (0.20 to 0.57 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None

Frequency of ponding: None

Available water supply, 0 to 60 inches: Moderate (about 8.6 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 6e

Hydrologic Soil Group: C

Ecological site: R015XY014CA - Loamy Mountains 20-40"ppt

Hydric soil rating: No

Description of Konocti

Setting

Landform: Hills, hills, mountains, ridges

Landform position (two-dimensional): Backslope, shoulder, summit

Landform position (three-dimensional): Upper third of mountainflank, side slope, nose slope

Down-slope shape: Concave, linear

Across-slope shape: Convex, linear

Parent material: Residuum weathered from andesite

Typical profile

H1 - 0 to 8 inches: cobbly loam

H2 - 8 to 16 inches: stony loam

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H3 - 16 to 32 inches: very stony sandy clay loam
H4 - 32 to 39 inches: very stony sandy loam
H5 - 39 to 49 inches: bedrock

Properties and qualities

Slope: 30 to 50 percent
Depth to restrictive feature: 39 to 43 inches to lithic bedrock
Drainage class: Well drained
Runoff class: High
Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately low (0.00 to 0.06 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Available water supply, 0 to 60 inches: Low (about 4.1 inches)

Interpretive groups

Land capability classification (irrigated): None specified
Land capability classification (nonirrigated): 6e
Hydrologic Soil Group: C
Ecological site: R015XY014CA - Loamy Mountains 20-40"ppt
Hydric soil rating: No

Description of Konocti

Setting

Landform: Hills, hills, mountains, ridges
Landform position (two-dimensional): Backslope, shoulder, summit
Landform position (three-dimensional): Upper third of mountainflank, side slope, nose slope
Down-slope shape: Concave, linear
Across-slope shape: Convex, linear
Parent material: Residuum weathered from andesite

Typical profile

H1 - 0 to 4 inches: stony loam
H2 - 4 to 9 inches: stony loam
H3 - 9 to 28 inches: very stony sandy clay loam
H4 - 28 to 38 inches: bedrock

Properties and qualities

Slope: 30 to 50 percent
Surface area covered with cobbles, stones or boulders: 0.1 percent
Depth to restrictive feature: 28 to 32 inches to lithic bedrock
Drainage class: Well drained
Runoff class: High
Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately low (0.00 to 0.06 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Available water supply, 0 to 60 inches: Low (about 3.0 inches)

Interpretive groups

Land capability classification (irrigated): None specified
Land capability classification (nonirrigated): 6e
Hydrologic Soil Group: C

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Ecological site: R015XY014CA - Loamy Mountains 20-40"ppt
Hydric soil rating: No

Minor Components

Steeper slopes

Percent of map unit: 3 percent
Hydric soil rating: No

Rock outcrop

Percent of map unit: 3 percent
Hydric soil rating: No

Konocti, variant

Percent of map unit: 3 percent
Hydric soil rating: No

Unnamed

Percent of map unit: 2 percent
Hydric soil rating: No

Unnamed

Percent of map unit: 2 percent
Hydric soil rating: No

Unnamed

Percent of map unit: 2 percent
Hydric soil rating: No

118—Bottlerock-Glenview-Arrowhead complex, 30 to 50 percent slopes

Map Unit Setting

National map unit symbol: hf58
Elevation: 1,500 to 3,000 feet
Mean annual precipitation: 40 inches
Mean annual air temperature: 55 degrees F
Frost-free period: 150 to 200 days
Farmland classification: Not prime farmland

Map Unit Composition

Bottlerock and similar soils: 40 percent
Glenview and similar soils: 20 percent
Arrowhead and similar soils: 15 percent
Minor components: 25 percent
Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Bottlerock

Setting

Landform: Hills

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Landform position (two-dimensional): Backslope
Landform position (three-dimensional): Side slope
Down-slope shape: Concave
Across-slope shape: Convex
Parent material: Residuum weathered from obsidian

Typical profile

H1 - 0 to 5 inches: very gravelly loam
H2 - 5 to 19 inches: very gravelly loam
H3 - 19 to 39 inches: very gravelly sandy clay loam
H4 - 39 to 63 inches: very gravelly clay

Properties and qualities

Slope: 30 to 50 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Well drained
Runoff class: Very high
Capacity of the most limiting layer to transmit water (Ksat): Moderately low to moderately high (0.06 to 0.20 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Available water supply, 0 to 60 inches: Low (about 4.8 inches)

Interpretive groups

Land capability classification (irrigated): None specified
Land capability classification (nonirrigated): 6e
Hydrologic Soil Group: C
Ecological site: F005XZ010CA - Very Deep Gravelly Mesic Hills 40-60"ppt
Hydric soil rating: No

Description of Glenview

Setting

Landform: Hills
Landform position (two-dimensional): Backslope
Landform position (three-dimensional): Side slope
Down-slope shape: Concave
Across-slope shape: Concave
Parent material: Residuum weathered from obsidian

Typical profile

H1 - 0 to 1 inches: very gravelly loam
H2 - 1 to 6 inches: gravelly loam
H3 - 6 to 15 inches: clay loam
H4 - 15 to 65 inches: gravelly clay
H5 - 65 to 75 inches: bedrock

Properties and qualities

Slope: 30 to 50 percent
Depth to restrictive feature: 65 to 69 inches to lithic bedrock
Drainage class: Well drained
Runoff class: High
Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately low (0.00 to 0.06 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None

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Frequency of ponding: None

Available water supply, 0 to 60 inches: Moderate (about 8.4 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 6e

Hydrologic Soil Group: C

Ecological site: F005XZ010CA - Very Deep Gravelly Mesic Hills 40-60"ppt

Hydric soil rating: No

Description of Arrowhead

Setting

Landform: Hills

Landform position (two-dimensional): Backslope

Landform position (three-dimensional): Side slope

Down-slope shape: Convex

Across-slope shape: Convex

Parent material: Residuum weathered from obsidian

Typical profile

H1 - 0 to 1 inches: very gravelly sandy loam

H2 - 1 to 8 inches: gravelly sandy loam

H3 - 8 to 14 inches: gravelly sandy clay loam

H4 - 14 to 31 inches: very stony clay

H5 - 31 to 41 inches: bedrock

Properties and qualities

Slope: 30 to 50 percent

Depth to restrictive feature: 31 to 35 inches to lithic bedrock

Drainage class: Well drained

Runoff class: High

Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately low (0.00 to 0.06 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None

Frequency of ponding: None

Available water supply, 0 to 60 inches: Very low (about 2.6 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 6e

Hydrologic Soil Group: C

Ecological site: F005XZ006CA - Mesic Hills <40"ppt

Hydric soil rating: No

Minor Components

Steeper slopes

Percent of map unit: 10 percent

Hydric soil rating: No

Unnamed, cobbly

Percent of map unit: 10 percent

Hydric soil rating: No

Unname, severely eroded

Percent of map unit: 5 percent

Hydric soil rating: No

148—Kidd-Forward complex, 5 to 30 percent slopes

Map Unit Setting

National map unit symbol: hf67
Elevation: 400 to 4,500 feet
Mean annual precipitation: 30 to 60 inches
Mean annual air temperature: 48 to 55 degrees F
Frost-free period: 145 to 260 days
Farmland classification: Not prime farmland

Map Unit Composition

Kidd and similar soils: 60 percent
Forward and similar soils: 20 percent
Minor components: 20 percent
Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Kidd

Setting

Landform: Hillslopes, mountains
Landform position (two-dimensional): Backslope
Landform position (three-dimensional): Center third of mountainflank, side slope
Down-slope shape: Convex
Across-slope shape: Convex
Parent material: Residuum weathered from rhyolite

Typical profile

H1 - 0 to 9 inches: gravelly loam
H2 - 9 to 16 inches: gravelly sandy loam
H3 - 16 to 26 inches: bedrock

Properties and qualities

Slope: 5 to 30 percent
Depth to restrictive feature: 16 to 20 inches to lithic bedrock
Drainage class: Well drained
Runoff class: Low
Capacity of the most limiting layer to transmit water (Ksat): Low to high (0.01 to 5.95 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Available water supply, 0 to 60 inches: Very low (about 1.9 inches)

Interpretive groups

Land capability classification (irrigated): None specified
Land capability classification (nonirrigated): 6e

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Hydrologic Soil Group: D

Ecological site: F015XY015CA - Loamy Mountains >40"ppt

Hydric soil rating: No

Description of Forward

Setting

Landform: Mountains, hillslopes

Landform position (two-dimensional): Backslope

Landform position (three-dimensional): Center third of mountainflank, side slope

Down-slope shape: Concave

Across-slope shape: Concave

Parent material: Residuum weathered from rhyolite

Typical profile

H1 - 0 to 9 inches: loam

H2 - 9 to 25 inches: gravelly sandy loam

H3 - 25 to 60 inches: bedrock

Properties and qualities

Slope: 5 to 30 percent

Depth to restrictive feature: 25 to 29 inches to paralithic bedrock

Drainage class: Somewhat excessively drained

Runoff class: Low

Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately low (0.00 to 0.06 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None

Frequency of ponding: None

Available water supply, 0 to 60 inches: Low (about 3.1 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 6e

Hydrologic Soil Group: B

Ecological site: F015XY010CA - Hills >40"ppt

Hydric soil rating: No

Minor Components

Aiken

Percent of map unit: 10 percent

Hydric soil rating: No

Rock outcrop

Percent of map unit: 5 percent

Hydric soil rating: No

Unnamed, steeper slopes

Percent of map unit: 5 percent

Hydric soil rating: No

151—Konocti-Benridge complex, 50 to 75 percent slopes

Map Unit Setting

National map unit symbol: hf6b

Elevation: 1,000 to 4,500 feet

Mean annual precipitation: 30 to 35 inches

Mean annual air temperature: 57 degrees F

Frost-free period: 140 to 200 days

Farmland classification: Not prime farmland

Map Unit Composition

Konocti and similar soils: 40 percent

Konocti and similar soils: 30 percent

Benridge and similar soils: 15 percent

Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Konocti

Setting

Landform: Hillslopes, mountains

Landform position (two-dimensional): Backslope

Landform position (three-dimensional): Mountainflank, side slope

Down-slope shape: Concave

Across-slope shape: Convex

Parent material: Residuum weathered from andesite

Typical profile

H1 - 0 to 4 inches: stony loam

H2 - 4 to 9 inches: stony loam

H3 - 9 to 28 inches: very stony sandy clay loam

H4 - 28 to 38 inches: bedrock

Properties and qualities

Slope: 50 to 75 percent

Depth to restrictive feature: 28 to 32 inches to lithic bedrock

Drainage class: Well drained

Runoff class: High

Capacity of the most limiting layer to transmit water (Ksat): Low to moderately high
(0.01 to 0.57 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None

Frequency of ponding: None

Available water supply, 0 to 60 inches: Low (about 3.0 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 7e

Hydrologic Soil Group: C

Custom Soil Resource Report

Ecological site: R015XY014CA - Loamy Mountains 20-40"ppt
Hydric soil rating: No

Description of Konocti

Setting

Landform: Hillslopes, mountains
Landform position (two-dimensional): Backslope
Landform position (three-dimensional): Mountainflank, side slope
Down-slope shape: Concave
Across-slope shape: Convex
Parent material: Residuum weathered from andesite

Typical profile

H1 - 0 to 8 inches: cobbly loam
H2 - 8 to 16 inches: stony loam
H3 - 16 to 32 inches: very stony sandy clay loam
H4 - 32 to 39 inches: very stony sandy loam
H5 - 39 to 49 inches: bedrock

Properties and qualities

Slope: 50 to 75 percent
Surface area covered with cobbles, stones or boulders: 0.1 percent
Depth to restrictive feature: 39 to 43 inches to lithic bedrock
Drainage class: Well drained
Runoff class: High
Capacity of the most limiting layer to transmit water (Ksat): Low to moderately high
(0.01 to 0.57 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Available water supply, 0 to 60 inches: Low (about 4.1 inches)

Interpretive groups

Land capability classification (irrigated): None specified
Land capability classification (nonirrigated): 7e
Hydrologic Soil Group: C
Ecological site: R015XY014CA - Loamy Mountains 20-40"ppt
Hydric soil rating: No

Description of Benridge

Setting

Landform: Hillslopes, mountains
Landform position (two-dimensional): Backslope
Landform position (three-dimensional): Mountainflank, side slope
Down-slope shape: Concave
Across-slope shape: Concave
Parent material: Residuum weathered from andesite

Typical profile

H1 - 0 to 6 inches: loam
H2 - 6 to 21 inches: gravelly clay loam
H3 - 21 to 63 inches: gravelly clay
H4 - 63 to 68 inches: gravelly clay

Properties and qualities

Slope: 50 to 75 percent

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Depth to restrictive feature: More than 80 inches
Drainage class: Well drained
Runoff class: High
Capacity of the most limiting layer to transmit water (Ksat): Moderately high (0.20 to 0.57 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Available water supply, 0 to 60 inches: Moderate (about 8.6 inches)

Interpretive groups

Land capability classification (irrigated): None specified
Land capability classification (nonirrigated): 7e
Hydrologic Soil Group: C
Ecological site: R015XY014CA - Loamy Mountains 20-40"ppt
Hydric soil rating: No

Minor Components

Unnamed

Percent of map unit: 5 percent
Hydric soil rating: No

Konocti, variant

Percent of map unit: 5 percent
Hydric soil rating: No

Sodabay

Percent of map unit: 5 percent
Hydric soil rating: No

203—San Joaquin variant fine sandy loam, 0 to 5 percent slopes

Map Unit Setting

National map unit symbol: hf80
Elevation: 1,300 to 1,500 feet
Mean annual precipitation: 25 to 35 inches
Mean annual air temperature: 57 degrees F
Frost-free period: 155 to 205 days
Farmland classification: Not prime farmland

Map Unit Composition

San joaquin, variant, and similar soils: 85 percent
Minor components: 15 percent
Estimates are based on observations, descriptions, and transects of the mapunit.

Description of San Joaquin, Variant

Setting

Landform: Terraces
Landform position (two-dimensional): Backslope
Landform position (three-dimensional): Tread
Down-slope shape: Linear
Across-slope shape: Linear
Parent material: Alluvium derived from volcanic rock

Typical profile

H1 - 0 to 21 inches: fine sandy loam
H2 - 21 to 25 inches: clay
H3 - 25 to 30 inches: indurated
H4 - 30 to 65 inches: stratified loamy sand to fine sandy loam

Properties and qualities

Slope: 0 to 5 percent
Depth to restrictive feature: More than 80 inches; 25 to 30 inches to duripan
Drainage class: Well drained
Runoff class: Medium
Capacity of the most limiting layer to transmit water (Ksat): Very low (0.00 to 0.00 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Available water supply, 0 to 60 inches: Very low (about 2.9 inches)

Interpretive groups

Land capability classification (irrigated): 4e
Land capability classification (nonirrigated): 4e
Hydrologic Soil Group: B
Hydric soil rating: No

Minor Components

Wolfcreek

Percent of map unit: 5 percent
Hydric soil rating: No

Unnamed

Percent of map unit: 5 percent
Hydric soil rating: No

Unnamed

Percent of map unit: 5 percent
Landform: Depressions
Hydric soil rating: Yes

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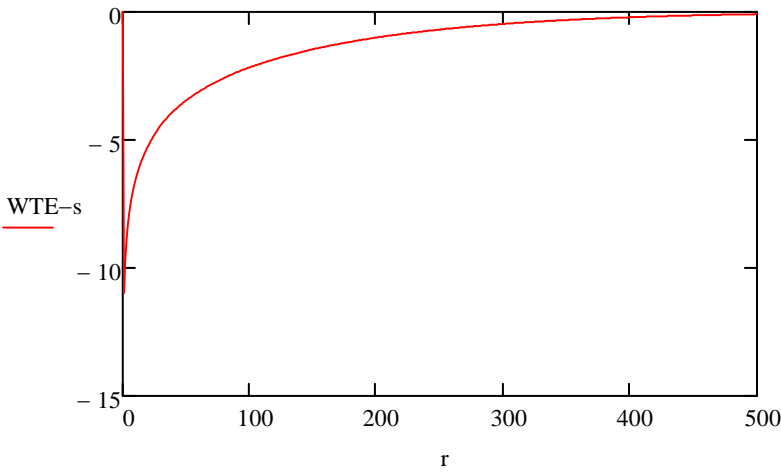
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APPENDIX D

THEIS DRAWDOWN ANALYSIS

$$K := 7.95 \cdot \frac{\text{ft}}{\text{day}}$$
$$B := 100 \cdot \text{ft}$$
$$Q := 9625 \cdot \frac{\text{ft}^3}{\text{day}}$$
$$u_d := \frac{S \cdot \left(r_d\right)^2}{4 \cdot K \cdot B \cdot t}$$
$$s_d := \frac{Q}{4 \cdot \pi \cdot K \cdot B} \left(\int_{u_d}^{\infty} \frac{e^{-u}}{u} du \right)$$

$$d := 1..500$$
$$r_d := d \cdot \text{ft}$$
$$t := 1 \cdot \text{day}$$
$$S := .02$$
$$\text{WTE} := 0 \cdot \text{ft}$$



s =

	0
197	1.024
198	1.016
199	1.009
200	1.001
201	0.994
202	0.987
203	0.979
204	0.972
205	0.965
206	0.957
207	0.95
208	0.943
209	0.936
210	0.929
211	0.922
212	0.915
213	0.909
214	0.902
215	...

ft