RECON

Noise Technical Report for the Nakano Project Chula Vista, California

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RECON Number 3396-1 September 20, 2023

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TABLE OF CONTENTS

Acro	nyms a	and Abbreviations	iii		
1.0	Intro	duction and Background	1		
	1.1	Project Description	1		
	1.2	Noise Characteristics	5		
	1.3	Vibration Fundamentals	6		
2.0	Regu	ulatory Setting	7		
	2.1	Federal	7		
	2.2	State	7		
	2.3	Local	8		
3.0	Exist	ing Conditions	15		
4.0	Thresholds of Significance				
	4.1	City of Chula Vista Significance Determination Thresholds			
	4.2	City of San Diego Significance Determination Thresholds			
5.0	Impa	act Discussion			
	5.1	Short-Term Construction Noise			
	5.2	Conventional Construction Activity Vibration	25		
	5.3	Long-Term Operational Noise	26		
	5.4	Land Use Noise Compatibility (Non-CEQA Analysis)			
6.0	Mitig	gation Measures and Project Design Features	40		
	6.1	Mitigation Measures	40		
	6.2	Project Design Features	42		
7.0	Refe	rences Cited	43		

FIGURES

Project Location	2
Project Location on Aerial Photograph	3
Site Plan	4
Noise Assessment Locations	16
Existing Vehicle Traffic Noise Contours	. 24
Operational Noise Contours	. 29
Future Vehicle Traffic Noise Contours	. 32
Noise Barriers	. 35
	Project Location Project Location on Aerial Photograph Site Plan Noise Assessment Locations Existing Vehicle Traffic Noise Contours Operational Noise Contours Future Vehicle Traffic Noise Contours Noise Barriers

TABLE OF CONTENTS (cont.)

TABLES

1:	City of Chula Vista Exterior Property-Line Noise Limits	9
2:	City of Chula Vista Exterior Land Use/Noise Compatibility Guidelines	10
3:	San Diego Exterior Noise Limits	11
4:	City of San Diego Land Use – Noise Compatibility Guidelines	13
5:	Measured Baseline Outdoor Ambient Noise Levels	15
6:	Typical Construction Equipment Maximum Noise Levels	20
7:	Estimated Distances between Construction Activities and the Nearest Existing City of	
	San Diego and City of Chula Vista Noise-Sensitive Receptors	21
8:	Predicted Construction Noise Levels per Activity Phase at Sensitive Receptors	22
9:	Predicted Construction Noise Levels at Sensitive Habitat	23
10:	Roadway Segment ADT Volumes	27
11:	Traffic Noise Level with and without Project and Ambient Noise Increases	27
12:	Predicted Project Stationary Source Operations Noise	30
13:	Future Vehicle Traffic Noise Levels	32
14:	Unmitigated and Mitigated Noise Levels at Exterior Use Areas	36
15:	Predicted Net Sound Transmission Class of Sample Occupied Room Façade	39

ATTACHMENTS

- 1: Baseline Noise Measurement Field Data
- 2: Construction Noise Modeling Input and Output
- 3: SoundPLAN Data Existing Vehicle Traffic Noise and Construction Noise at Sensitive Habitat
- 4: FHWA-RD-77-108 Off-Site Traffic Noise Calculations
- 5: SoundPLAN Data Operational Noise
- 6: SoundPLAN Data Future Vehicle Traffic Noise

Acronyms and Abbreviations

ACC	air-cooled condenser
ADT	average daily traffic
ALUCP	Airport Land Use Compatibility Plan
Caltrans	California Department of Transportation
CEQA	California Environmental Quality Act
CNEL	Community Noise Equivalent Level
CVMC	Chula Vista Municipal Code
dB	decibel
dB(A)	A-weighted decibel
FHWA	Federal Highway Administration
FTA	Federal Transit Administration
I-805	Interstate 805
ips	inches per second
LAFCO	Local Agency Formation Commission
L _{dn}	day–night average noise level
L _{eq}	equivalent noise level
L _{max}	maximum sound level
L _{min}	minimum sound level
MSCP	Multiple Species Conservation Plan
NSR	noise-sensitive receptor
PPV	peak particle velocity
project	Nakano Project
RCNM	Roadway Construction Noise Model
SANDAG	San Diego Association of Governments
SDCRAA	San Diego County Regional Airport Authority
SDMC	San Diego Municipal Code
SLM	sound level meter
ST	short-term
STC	sound transmission class

1.0 Introduction and Background

This technical noise report evaluates the potential noise impacts during construction and operation of the proposed Nakano project (project). This assessment is based on Appendix G of the California Environmental Quality Act (CEQA) Guidelines (14 CCR 15000 et seq.) and the City of San Diego CEQA Significance Determination Thresholds (City of San Diego 2022).

1.1 Project Description

The project consists of development of 215 residential dwellings units consisting of 61 detached condominiums, 84 duplexes and 70 townhome dwelling units on 23.8 acres with approximately 5 acres of hardscaped/paved roadway area. However, to represent a conservative analysis of potential unit mix, the environmental analysis assumes a maximum of 221 residential units. The project site is located on the 450 block of Dennery Road, in the city of Chula Vista, California. Figure 1 shows the project location and Figure 2 shows an aerial photograph of the project site and vicinity. Figure 3 shows the site plan.

The project is evaluated under Scenario 1: No Annexation Scenario where the project would remain within the City of Chula Vista in addition to two Annexation scenarios.

Scenario 1, the No Annexation Scenario, assumes the project would stay in Chula Vista and not be annexed into San Diego. Local Agency Formation Commission (LAFCO) approval of out of agency service agreements for services and utilities from San Diego would be required. Under this scenario, Chula Vista would issue grading and development permits for the project site; however, the City of San Diego would require a site development permit and grading permit for the off-site improvements associated with primary site access and secondary emergency access.

Two potential Annexation scenarios are described below. The key difference between the two Annexation scenarios would be the agency responsibility for issuance of grading and development permits for the project site.

In Annexation Scenario 2a, grading and development of the project site would not proceed until the LAFCO reorganization process is complete. In this scenario, the City of San Diego would issue grading and development permits for the project site and all off-site improvement areas after approval of the LAFCO reorganization.

In Annexation Scenario 2b, grading and site development would proceed prior to LAFCO reorganization. In this scenario, the City of Chula Vista would issue grading and development permits for the project site and City of San Diego would issue a grading permit for the off-site portions. Grading permits, recordation of a final map, and Chula Vista issuance of all final certificates of occupancy would be completed prior to approval of the LAFCO reorganization. Annexation of the project site to San Diego would not occur until after site development in Chula Vista is complete.



🔆 Project Location

FIGURE 1 Regional Location



0 Feet 300



Map Source: Civil Sense, Inc.



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PCC SIDEN

— 4' PARKWAY (PRIVATE STREET 'H ONLY) =

- 4" PCC SIDE

LEGEND

TM BOUNDARY ____ 1 BUILDING NUMBER (110.9) PROPOSED PAD ELEVATION 10' X 10' VISIBILITY TRIANGLE

+++21A

PROPOSED CURB / CURB AND GUTTER PROPOSED SIDEWALK NO OBSTRUCTION INCLUDING FENCES/SHRUBS OR SOLID WALLS IN THE VISIBILITY AREA SHALL EXCEED 24 INCHES IN HEIGHT. PROPOSED PEDESTRIAN PATH OF TRAVEL PROPOSED STREET PER CITY STANDARD DRAWINGS

A = ACCESSIBLE SPACES V = VAN ACCESSIBLE SPACES



FIGURE 3 Site Plan While the physical improvements proposed would be the same under all project scenarios, the discretionary actions would differ. The No Annexation Scenario would include a City of Chula Vista General Plan Amendment, Tentative Map, Specific Plan, out of service agreements for services and utilities, and certification of the Environmental Impact Report. More specifically, the General Plan Amendment would change the land use designation to Specific Plan – Residential Medium and the Specific Plan would implement the R-3 zone in Chula Vista.

The Annexation scenarios would include the annexation of the site from the City of Chula Vista and Otay Water District to the City of San Diego, an annexation agreement, City of San Diego and City of Chula Vista Sphere of Influence revision, City of San Diego and City of Chula Vista General Plan Amendment, Otay Mesa Community Plan Amendment, prezone in San Diego, San Diego Resolution of Initiation and Chula Vista Resolution Support, a Tentative Map, and certification of the Environmental Impact Report. Under the Annexation scenarios, the site would be designated by the City of San Diego as Residential – Low Medium and zoned as RM-1-1 (Residential-Multiple Unit). The Local Agency Formation Commission would provide oversight of the annexation process.

For purposes of the environmental analysis, the responsibility for permitting and implementing required mitigation measures detailed in this report would be the City of Chula Vista for the No Annexation Scenario and the Annexation Scenario 2b. Therefore, the analysis for these two scenarios is combined. The analysis for Annexation Scenario 2a is addressed separately as the City of San Diego would have responsibility for implementing applicable mitigation for project under this scenario.

1.2 Noise Characteristics

Sound is mechanical energy transmitted by pressure waves in a compressible medium, such as air. Noise is defined as sound that is loud, unpleasant, unexpected, or undesired. The sound pressure level has become the most common descriptor used to characterize the loudness of an ambient sound level. The unit of measurement of sound pressure is a decibel (dB). Under controlled conditions in an acoustics laboratory, the trained, healthy human ear is able to discern changes in sound levels of 1 A-weighted dB [dB(A)] when exposed to steady, single-frequency signals in the mid-frequency range.

Outside such controlled conditions, the trained ear can detect changes of 2 dB(A) in normal environmental noise. It is widely accepted that the average healthy ear, however, can barely perceive noise level changes of 3 dB. A change of 5 dB(A) is readily perceptible, and a change of 10 dB(A) is perceived as twice or half as loud (California Department of Transportation [Caltrans] 2013). A doubling of sound energy results in a 3 dB(A) increase in sound, which means that a doubling of sound energy (e.g., doubling the number of daily trips along a given road) would result in a barely perceptible change in sound level.

Sound may be described in terms of level or amplitude (measured in dB), frequency or pitch (measured in hertz or cycles per second), and duration (measured in seconds or minutes). Because the human ear is not equally sensitive to sound at all frequencies, a special frequency-dependent rating scale is used to relate noise to human sensitivity. The dB(A) scale performs this compensation by discriminating against low and very high frequencies in a manner approximating the sensitivity of the human ear.

Several descriptors of noise (also known as, noise metrics) exist to help predict average community reactions to the adverse effects of environmental noise, including traffic-generated noise. These descriptors include the equivalent noise level over a given period (L_{eq}), the day–night average noise level (L_{dn}), and the community noise equivalent level (CNEL). Each of these descriptors uses units of dB(A).

 L_{eq} is a dB quantity that represents the constant or energy-averaged value equivalent to the amount of variable sound energy received by a receptor during a time interval. For example, a 1-hour L_{eq} measurement of 60 dB(A) would represent the average amount of energy contained in all the noise that occurred in that hour. L_{eq} is an effective noise descriptor because of its ability to assess the total time-varying effects of noise on sensitive receptors, which can then be compared to an established L_{eq} standard or threshold of the same duration. Another descriptor is maximum sound level (L_{max}), which is the greatest sound level measured during a designated time interval or event. The minimum sound level (L_{min}) is often called the *floor* of a measurement period.

Unlike the L_{eq} , L_{max} , and L_{min} metrics, L_{dn} and CNEL descriptors always represent 24-hour periods and differ from a 24-hour L_{eq} value because they apply a time-weighted factor designed to emphasize noise events that occur during the non-daytime hours (when speech and sleep disturbance is of more concern). *Time weighted* refers to the fact that L_{dn} and CNEL penalize noise that occurs during certain sensitive periods. In the case of CNEL, noise occurring during the daytime (7:00 a.m. to 7:00 p.m.) receives no penalty. Noise during the evening (7:00 p.m. to 10:00 p.m.) is penalized by adding 5 dB(A) to the actual levels, and nighttime (10:00 p.m. to 7:00 a.m.) noise is penalized by adding 10 dB(A) to the actual levels. L_{dn} differs from CNEL in that the daytime period is longer (defined instead as 7:00 a.m. to 10:00 p.m.), thus eliminating the dB(A) adjustment for the evening period. L_{dn} and CNEL are the predominant criteria used to measure roadway noise affecting residential receptors. These two metrics generally differ from one another by no more than 0.5–1 dB(A), and are often considered or actually defined as being essentially equivalent by many jurisdictions.

1.3 Vibration Fundamentals

Vibration is oscillatory movement of mass (typically a solid) over time. It is described in terms of frequency and amplitude and, unlike sound, can be expressed as displacement, velocity, or acceleration. For environmental studies, vibration is often studied as a velocity that, akin to the discussion of sound pressure levels, can also be expressed in dB as a way to cast a large range of quantities into a more convenient scale and with respect to a reference quantity. Vibration impacts to buildings are generally discussed in terms of inches per second (ips) peak particle velocity (PPV), which will be used herein to discuss vibration levels for ease of reading and comparison with relevant standards. Vibration can also be annoying and thereby impact occupants of structures, and vibration of sufficient amplitude can disrupt sensitive equipment and processes (Caltrans 2020a), such as those involving the use of electron microscopes and lithography equipment. Common sources of vibration within communities include construction activities and railroads. Groundborne vibration generated by construction projects is usually highest during pile driving, rock blasting, soil compacting, jack hammering, and demolition-related activities where sudden releases of subterranean energy or powerful impacts of tools on hard materials occur. Depending on their distances to a sensitive receptor, operation of large bulldozers, graders, loaded dump trucks, or other heavy construction

equipment and vehicles on a construction site also have the potential to cause high vibration amplitudes.

2.0 Regulatory Setting

2.1 Federal

2.1.1 Federal Transit Administration

In its Transit Noise and Vibration Impact Assessment guidance manual, the Federal Transit Administration (FTA) recommends a daytime construction noise level threshold of 80 dB(A) L_{eq} over an 8-hour period (FTA 2018) when detailed construction noise assessments are performed to evaluate potential impacts to community residences surrounding a project. Although this FTA guidance is not a regulation, it can serve as a quantified standard in the absence of such noise limits at the state and local jurisdictional levels.

2.2 State

2.2.1 California Code of Regulations, Title 24

Title 24 of the California Code of Regulations sets standards that new development in California must meet. According to Title 24, interior noise levels are not to exceed 45 CNEL in any habitable room (International Construction Code 2019).

2.2.2 California Department of Health Services Guidelines

The California Department of Health Services has developed guidelines of community noise acceptability for use by local agencies (State of California 2017). Selected relevant levels are listed here:

- Below 60 CNEL: normally acceptable for low-density residential use
- 50 to 70 CNEL: conditionally acceptable for low-density residential use
- Below 65 CNEL: normally acceptable for high-density residential use and transient lodging
- 60 to 70 CNEL: conditionally acceptable for high-density residential, transient lodging, churches, educational, and medical facilities

The normally acceptable exterior noise level for high-density residential use is up to 65 CNEL. Additionally, this exterior noise level limit is consistent with the City of Chula Vista General Plan Noise Element, which considers multi- family units noise-sensitive land uses.

2.2.3 California Department of Transportation

In its Transportation and Construction Vibration Guidance Manual (Caltrans 2020a), Caltrans recommends 0.5 ips PPV as a threshold for the avoidance of structural damage to typical newer residential buildings exposed to continuous or frequent intermittent sources of groundborne vibration. For transient vibration events, such as blasting, the damage risk threshold would be 1.0 ips PPV (Caltrans 2020a) at the same type of newer residential structures. For older structures, these guidance thresholds would be more stringent: 0.3 ips PPV for continuous/intermittent vibration sources, and 0.5 ips PPV for transient vibration events. With respect to human annoyance, Caltrans guidance indicates that building occupants exposed to continuous groundborne vibration at a level of 0.1 ips PPV would find it either "strongly perceptible" or "begins to annoy" and thus for purposes of this assessment would be considered a likely significant impact. Although these Caltrans guidance thresholds are not regulations, they can serve as quantified standards in the absence of such limits at the local jurisdictional level.

2.3 Local

The following are summarized or reproduced portions of relevant City of Chula Vista and City of San Diego regulations and General Plan policies.

2.3.1 City of Chula Vista

2.3.1.1 City of Chula Vista Municipal Code 19.68 (Noise Ordinance)

The City of Chula Vista Noise Ordinance (Chula Vista Municipal Code [CVMC] Section 19.68) (City of Chula Vista 2020) contains regulations restricting land use related noise-generating activities and operations, so as to avoid noise nuisance in the community. Section 19.68.030 of the CVMC establishes the maximum allowable exterior noise limits, based upon the classification of the receiving land use. These standards typically apply to stationary sources such as noise from mechanical equipment (including mechanical ventilation and air condition noise, pool pump noise, etc.) or event noise, as opposed to traffic noise. For instance, a school, commercial enterprise, or industrial operation must not generate noise that exceeds a certain specified noise level at any property boundary where an adjacent residential use exists. The property-line noise standards are presented in Table 1.

Table 1 City of Chula Vista Exterior Property-Line Noise Limits							
Noise Level (dB(A) L _{eo})							
	10 p.m. to 7 a.m. (Weekdays) 7 a.m. to 10 p.m. (Weekdays)						
Receiving Land Use Category 10 p.m. to 8 a.m. (Weekends) 8 a.m. to 10 p.m. (
All residential (except multiple dwelling)	45	55					
Multiple-dwelling residential	50	60					
Commercial	60	65					
Light industry – I-R and I-L zone	70	70					
Heavy industry – I zone 80 80							
Note: dB(A) = A-weighted decibels							

Title 17 of the CVMC (Environmental Quality), Chapter 24, addresses managing noisy and disorderly conduct. Section 17.24.040.C.8 specifically addresses restrictions against generation of construction noise in overnight periods. The use of any tools, power machinery, or equipment, or the conduct of construction and building work in residential zones so as to cause noises disturbing to the peace, comfort, and quiet enjoyment of property of any person residing or working in the vicinity, shall be prohibited between the hours of 10:00 p.m. and 7:00 a.m., Monday through Friday, and between the hours of 10:00 p.m. Saturday and Sunday, except when the work is necessary for emergency repairs required for the health and safety of any member of the community (City of Chula Vista 2020).

Although the City does not set specific numerical limits for noise associated with temporary construction activities, it can be perceived as a nuisance; thus, the City restricts the times of day when construction may occur (7:00 a.m.–10:00 p.m., Monday–Friday, and 8:00 a.m.–10:00 p.m., Saturday and Sunday).

2.3.1.2 City of Chula Vista General Plan Noise Element

The City of Chula Vista General Plan Noise Element establishes noise criteria for various land uses (City of Chula Vista 2005). The maximum allowable exterior noise level at outdoor usable areas for new residential development is an annual CNEL of 65 dB. The City's exterior land use-noise compatibility guidelines for various land uses are depicted in Table 2. For residential development, the City typically applies the noise criteria at the backyards of single-family homes and at private patios, exterior balconies, and exterior common use areas of multi-family developments. The minimum amount of required exterior use space shall meet this criteria, with any additional are being provided being exempt from this requirement.

Table 2 City of Chula Victa Exterior Land Use (Noice Compatibility Cuidelines							
Land Use	50	55	60	65	70	75	
Residential							
Schools, Libraries, Daycare Facilities, Convalescent Homes,							
Outdoor Use Areas, and other Similar Uses Considered							
Noise Sensitive							
Neighborhood Parks, Playgrounds							
Community Parks, Athletic Fields							
Offices and Professional							
Places of Worship (excluding outdoor use areas)							
Golf Courses							
Retail and Wholesale Commercial, Restaurants, Movie							
Theaters							
Industrial, Manufacturing							
Note: Shaded box indicates allowable decibel level							
Source: City of Chula Vista 2005							

Policy E21.1 of the Chula Vista General Plan requires the application of the exterior land use-noise compatibility guidelines listed in Table 2 to "new development, where applicable, and in light of project-specific considerations." In addition, Objective E22 (Protect the community from the effects of transportation noise) of the City's General Plan Noise Element, Policy E22.5 requires projects to construct appropriate mitigation measures to attenuate existing and projected traffic noise levels, in accordance with applicable standards, including the exterior land use/noise compatibility guidelines listed in Table 2.

For off-site project-related traffic, Chula Vista considers a noise impact to be significant if implementation of the project results in noise levels that exceed the exterior noise limits established in the City's General Plan, including 65 CNEL for residences, schools, and recreational uses; 70 CNEL for offices, community parks and athletic fields; and 75 CNEL for commercial uses. For transportation-related noise, a significant impact would occur if the project results in a 3 dB(A) or greater increase in traffic noise on a roadway segment and the resultant noise level would exceed the General Plan exterior noise limits.

2.3.1.3 City of Chula Vista Multiple Species Conservation Program Subarea Plan

The municipalities of southwestern San Diego County collaborated in producing the Multiple Species Conservation Program (MSCP) Subregional Plan (City of San Diego 1998). The MSCP Subregional Plan is implemented through individual Subarea Plans adopted by each jurisdiction in order to receive take authorization for impacts to covered species and habitats. The MSCP is implemented in Chula Vista through the City of Chula Vista's MSCP Subarea Plan (City of Chula Vista 2003). The MSCP Subarea Plan regulates impacts to sensitive biological resources, including noise impacts. In accordance with Section 7.5.2 of the Chula Vista Subarea Plan, Adjacency Management Issues, uses in or adjacent to the Preserve should be designed to minimize noise impacts. Berms or walls should be constructed adjacent to commercial areas and any other use that may introduce noises that could impact or interfere with wildlife utilization of the Preserve. Excessively noisy areas or activities adjacent to breeding areas, including temporary grading activities, must incorporate noise reduction measures or be curtailed during the breeding season of sensitive bird species, consistent with Table 3-5 of the MSCP Subregional Plan, included as Appendix A to the MSCP Subarea Plan. In general, the construction noise threshold for sensitive biological resources is an hourly average noise level of 60 dB(A) and no clearing, grubbing, and/or grading is permitted within the MSCP Preserve during the breeding season of the sensitive species present. Within the City of Chula Vista Subarea Plan, the project area is designated as "Development Area Outside Covered Projects" (i.e., not designated a preserve or conservation area) and is not located immediately adjacent to any 75 percent or 100 percent Conservation Areas. The closest Chula Vista Subarea Plan conservation area (75 percent) is located approximately 197 feet north of the project area within the Otay River.

2.3.2 City of San Diego

2.3.2.1 City of San Diego Municipal Code 9.5 (Noise Ordinance)

Applicable noise standards for the project are codified in the following City of San Diego Municipal Code (SDMC) regulations (City of San Diego 2010):

SDMC Section 59.5.0401: Sound Level Limits

It shall be unlawful for any person to cause noise by any means to the extent that the one-hour average sound level exceeds the applicable limit given in Table 3, at any location in the City of San Diego on or beyond the boundaries of the property on which the noise is produced. The noise subject to these limits is that part of the total noise at the specified location that is due solely to the action of said person.

Table 3								
San Diego Exterior Noise Limits								
One-Hour Average Sound Level								
Land Use	Time of Day	(Decibels)						
	7 a.m. to 7 p.m.	50						
1. Single Family Residential	7 p.m. to 10 p.m.	45						
	10 p.m. to 7 a.m.	40						
2 Multi Family Desidential	7 a.m. to 7 p.m.	55						
2. Multi-Family Residential	7 p.m. to 10 p.m.	50						
(Op to a maximum density of 1/2000)	10 p.m. to 7 a.m.	45						
	7 a.m. to 7 p.m.	60						
3. All other Residential	7 p.m. to 10 p.m.	55						
	10 p.m. to 7 a.m.	50						
	7 a.m. to 7 p.m.	65						
4. Commercial	7 p.m. to 10 p.m.	60						
	10 p.m. to 7 a.m.	60						
5. Industrial or Agriculture	75							
Source: City of San Diego 2010								

The sound level limit at a location on a boundary between two zoning districts is the arithmetic mean of the respective limits for the two districts. Permissible construction noise level limits shall be governed by SDMC Sections 59.5.0404 of this article.

Fixed–location public utility distribution or transmission facilities located on or adjacent to a property line shall be subject to the noise level limits of Part A of this section, measured at or beyond six feet from the boundary of the easement upon which the equipment is located.

SDMC Section 59.5.0404: Construction Noise

It shall be unlawful for any person, between the hours of 7:00 p.m. of any day and 7:00 a.m. of the following day, or on legal holidays as specified in Section 21.04 of the SDMC, with exception of Columbus Day and Washington's Birthday, or on Sundays, to erect, construct, demolish, excavate for, alter or repair any building or structure in such a manner as to create disturbing, excessive or offensive noise unless a permit has been applied for and granted beforehand by the Noise Abatement and Control Administrator. In granting such permit, the Administrator shall consider whether the construction noise in the vicinity of the proposed work site would be less objectionable at night than during the daytime because of different population densities or different neighboring activities; whether obstruction and interference with traffic particularly on streets of major importance, would be less objectionable at night than during the daytime; whether the type of work to be performed emits noises at such a low level as to not cause significant disturbances in the vicinity of the work site; the character and nature of the neighborhood of the proposed work site; whether great economic hardship would occur if the work were spread over a longer time; whether proposed night work is in the general public interest; and he shall prescribe such conditions, working times, types of construction equipment to be used, and permissible noise levels as he deems to be required in the public interest.

Except as provided in subsection C, hereof, it shall be unlawful for any person, including the City of San Diego, to conduct any construction activity so as to cause, at or beyond the property lines of any property zoned residential, an average sound level no greater than 75 dB during the 12-hour period from 7:00 a.m. to 7:00 p.m.

The provisions of subsection B. of this section shall not apply to construction equipment used in construction with emergency work, provided the Administrator is notified within 48 hours after commencement of work.

2.3.2.2 City of San Diego General Plan Noise Element

The City of San Diego General Plan Noise Element (2015) establishes noise compatibility guidelines for uses affected by traffic noise, as detailed in Table 4.

Table 4								
	C	ity of San Diego	Land Use – Noise Comp	patibilit	y Guideliı	nes	(0) (5)	
Land Lise Category			Exterior Noise Exposure (CNEL)				7 -	
Parks and R	Li	and Use Category			60	65	/0 /	'5
Parks Activ	ecreational e and Passive Recrea	ation						
Outdoor Si	pectator Sports, Golf	Courses: Water Recre	eational Facilities: Indoor					
Recreation	Facilities							
Agricultural								
Crop Raisir	ig and Farming; Com	imunity Gardens, Aqu	Jaculture, Dairies;					
Horticultur	e Nurseries and Gree	nhouses; Animal Rais	sing, Maintaining and					
Keeping; C	ommercial Stables							
Residential								
Single Dwe	lling Units; Mobile H	omes			45			
Multiple D	welling Units				45	45		
*For uses a	ffected by aircraft noi	se, refer to Policies NI	E-D.2. & NE-D.3.					
	Jursing Escilitios: Inte	ormodiato Caro Eacilit	ios: Kindorgartan through					
Grade 12 F	ducational Facilities.	Libraries: Museums: (Thild Care Facilities		45			
Other Educ	rational Facilities inclu	Iding Vocational/Tra	de Schools and Colleges					
and Univer	sities				45	45		
Cemeteries								
Retail Sales								
Building Su	pplies/Equipment; Fo	ood, Beverage, and G	iroceries; Pets and Pet					
Supplies; S	undries, Pharmaceuti	ical, and Convenience	e Sales; Wearing Apparel			50	50	
and Access	ories							
Commercial	Services		in an Eire an sint to stitution an					
Building Se	rvices; Business Supp	Dort; Eating and Drink	(ing; Financial Institutions;					
nublic and	religious assembly):	Radio and Television	Studios: Golf Course			50	50	
Support	religious assertibly), i							
Visitor Acco	ommodations				45	45	45	
Offices								
Business ar	nd Professional; Gove	ernment; Medical, Dei	ntal, and Health			50	EO	
Practitione	r; Regional and Corp	orate Headquarters				50	50	
Vehicle and	Vehicular Equipment	Sales and Services Us	se					
Commercia	l or Personal Vehicle	Repair and Mainten	ance; Commercial or					
Personal V	ehicle Sales and Rent	als; Vehicle Equipme	nt and Supplies Sales and					
Wholesale [nicle Parking Distribution Storage I	lse Category						
Equipment	and Materials Storage	ne Vards: Moving and	Storage Facilities					
Warehouse	: Wholesale Distribut	tion	i Storage raemies,					
Industrial	,							-
Heavy Mar	ufacturing; Light Ma	nufacturing; Marine I	ndustry; Trucking and					
Transporta	tion Terminals; Minin	g and Extractive Indu	istries					
Research a	nd Development	1	1				50	
	.	Indoor Uses	Standard construction met	hods sho	uld attenua	ate exterior r	noise to an a	acceptable
Compatible Indoor noise level.								
		Outdoor Uses	Building structure must atte	ie iana us	terior poice	to the index	or noise leve	lindicated
	Conditionally	Indoor Uses	by the number for occupie	d areas				indicated
45, 50	Compatible		Feasible noise mitigation	techniau	es should	be analyzed	l and incorr	porated to
		Outdoor Uses	make the outdoor activities	accepta	ble.	. ,		
	In compatible	Indoor Uses	New construction should not be undertaken.					
	ncompauble	Outdoor Uses	Severe noise interference n	nakes ou	tdoor activi	ties unaccep	table.	
SOURCE: Cit	y of San Diego 2015.							

Applicable Noise Element policies with respect to the project include are as follows:

- NE-A.1. Separate excessive noise-generating uses from residential and other noise-sensitive land uses with a sufficient spatial buffer of less sensitive uses.
- NE-A.2. Assure the appropriateness of proposed developments relative to existing and future noise levels by consulting the guidelines for noise-compatible land use (shown on Table 4) to minimize the effects on noise-sensitive land uses.
- NE-A.3. Limit future residential and other noise-sensitive land uses in areas exposed to high levels of noise.
- NE-A.4. Require an acoustical study consistent with Acoustical Study Guidelines (Table NE-4) for proposed developments in areas where the existing or future noise level exceeds or would exceed the "compatible" noise level thresholds as indicated on the Land Use Noise Compatibility Guidelines (see Table 4), so that noise mitigation measures can be included in the project design to meet the noise guidelines.
- NE-A.5. Prepare noise studies to address existing and future noise levels from noise sources that are specific to a community when updating community plans.

2.3.2.3 City of San Diego Multiple Species Conservation Program Subarea Plan

The MSCP is implemented in the City of San Diego through the City of San Diego's MSCP Subarea Plan (City of San Diego 1997). The City of San Diego's MSCP Subarea Plan identifies lands designated as Multi-Habitat Planning Area (MHPA), which is a "hard-line" preserve developed by the City of San Diego in cooperation with the wildlife agencies, developers, property owners, and various environmental groups. Within the MHPA, biological core resource areas and corridors targeted for conservation are identified and discussed, in which development restrictions may occur (City of San Diego 1997). Development adjacent to MHPA is subject to the City's Land Use Adjacency Guidelines which include minimizing noise impacts to the MHPA as well as control of noise during the breeding season of sensitive species. No MHPA is located on-site and the nearest City of San Diego MHPA is approximately 180 feet west of the project site, across Interstate 805 (I-805). The project is located outside the City of San Diego Subarea Plan, with the exception that the project's primary and secondary access roads are located within the City of San Diego and the San Diego's Subarea Plan. These off-site access road areas are subject to San Diego's Subarea Plan which requires that noise impacts to certain sensitive species are avoided. Under the Annexation Scenario 2a, the project parcel would be annexed and developed into the City of San Diego and subject to the City of San Diego's Subarea Plan (City of San Diego 1997) as well as the associated City of San Diego Biology Guidelines (City of San Diego 2018).

2.3.3 Brown Field Airport Land Use Compatibility Plan

The Airport Land Use Compatibility Plan (ALUCP) for Brown Field identifies land uses compatible with annual noise levels due to operations at Brown Field. These land use compatibility noise levels are to

be used in determining whether a proposed land use is consistent with ALUCP policies and guidelines. The Brown Field Municipal ALUCP residential exterior and interior noise exposure standards are 65 CNEL and 45 CNEL, respectively (San Diego County Regional Airport Authority [SDCRAA] 2010).

3.0 Existing Conditions

Noise measurements were conducted near the project site on June 4, 2020, to quantify and characterize the existing outdoor ambient sound levels. Table 5 provides the location, date, and time period at which these baseline noise level measurements were performed by an attending Dudek field investigator using a Rion-branded Model NL-52 sound level meter (SLM) equipped with a 0.5-inch, pre-polarized condenser microphone with pre- amplifier. The SLM meets the current American National Standards Institute standard for a Type 1 (Precision Grade) sound level meter. The accuracy of the SLM was verified using a field calibrator before and after the measurements, and the measurements were conducted with the microphone positioned approximately 5 feet above the ground.

Four (4) short-term (ST) noise level measurement locations (ST1–ST4) that represent existing noise-sensitive receivers were selected on and near the project site. These locations are depicted as receivers ST1, ST2, ST3, and ST4 on Figure 4, Noise Assessment Locations. The measured L_{eq} and L_{max} noise levels are provided in Table 5. The primary noise sources at the sites identified in Table 5 consisted of traffic along adjacent roadways, the sounds of leaves rustling, audible distant aircrafts, and birdsong. As shown in Table 5, noise levels ranged from approximately 62 dB(A) L_{eq} at ST1 to 65.6 dB(A) L_{eq} at ST4. Beyond the summarized information presented in Table 5, detailed noise measurement data is included in Attachment 1, Baseline Noise Measurement Field Data (Dudek 2022).

Table 5							
Site	Location/Address	Date (yyyy-mm-dd), Time	L _{eq} dB(A)	L _{max} dB(A)			
ST1	Southeast of project site boundary; north of Dennery Road	2020-06-04, 10:50 AM to 11:00 AM	62.0	75.1			
ST2	South of southern project site boundary; northeast corner of Kaiser Permanente parking structure	2020-06-04, 11:45 AM to 11:55 AM	62.1	66.3			
ST3	East of project site; near 122 Golden Sky Way, San Diego, CA 92154	2020-06-04, 10:30 AM to 10:40 AM	62.8	64.5			
ST4	Southwest corner of project site boundary	2020-06-04, 11:20 AM to 11:30 AM	65.6	74.6			
Source: Attachment 1. Notes: L_{eq} = equivalent continuous sound level (time-averaged sound level); L_{max} = maximum sound level during the measurement interval: dB(A) = A-weighted decibels: ST = short-term noise measurement locations							

Generally, the measured samples of daytime L_{eq} agree with expectations: ST4 is above 65 dB(A) due largely to its proximity to Interstate 805, a major roadway; ST2 is farther up the bluff, south of the southern boundary of the project; and ST1 and ST3 are closer to the residential neighborhoods east of the project and much more distant from these sources of roadway traffic noise.



 \bigcirc

Project Boundary Measurement Location

FIGURE 4 Noise Measurement Locations

Feet

300

0

4.0 Thresholds of Significance

The following significance criteria are based on Appendix G of the CEQA Guidelines (14 CCR 15000 et seq.) and intended to frame the assessment of potentially significant noise and vibration impacts associated with a studied project's effects to the neighboring off-site community:

- a. Generation of a substantial temporary or permanent increase in ambient noise levels in the vicinity of the project in excess of standards established in the local general plan or noise ordinance, or applicable standards of other agencies;
- b. Generation of excessive groundborne vibration or groundborne noise levels; and,
- c. Expose people residing or working in the project area to excessive noise levels (for a project located within the vicinity of a private airstrip or an airport land use plan, or where such a plan has not been adopted, within 2 miles of a public airport or public use airport).

The City of San Diego has adopted its own CEQA Significance Thresholds (and corresponding impact assessment metrics) that are presented in Section 4.2 below.

4.1 City of Chula Vista Significance Determination Thresholds

The analysis for the No Annexation Scenario and Annexation Scenario 2b uses the following City of Chula Vista standards to evaluate potential noise and vibration impacts at on-site and off-site land uses under City of Chula Vista jurisdiction.

- <u>Construction noise</u> The City regulates construction noise by restricting the allowable hours of construction. Section 9.40.110 of the CVMC exempts construction noise from the stationary noise standards, provided that construction occurs between 7:00 a.m. and 10:00 p.m., Monday through Friday, and 8:00 a.m. to 10:00 p.m., Saturday and Sunday. Through adherence to the limitation of allowable construction times provided in the CVMC, the construction-related noise levels would not exceed any municipal standards. However, since the City of Chula Vista lacks a quantified construction noise level threshold, consistent with the "or applicable standards of other agencies" clause in the first bulleted CEQA Guidelines Appendix G criterion above for noise, for purposes of information disclosure this assessment adopts the FTA guidance-based standard of 80 dB(A) over an 8-hour L_{eq} at the exterior of a residential land use. This FTA standard would be applied to the nearest existing medium (zoned "R2") and high-density (zoned "R3P13") City of Chula Vista residential receptors that are approximately 700 feet northwest of the project site.
- <u>Off-site project-attributed transportation noise</u> For purposes for this analysis, a direct roadway noise impact would be considered significant if increases in roadway traffic noise levels attributed to the project are greater than 3 dB(A) at an existing noise-sensitive land use.

- <u>Off-site project-attributed stationary noise</u> For purposes for this analysis, a noise impact would be considered significant if noise from typical operation of heating, ventilation, and air conditioning and other electro-mechanical systems associated with the project exceeded 55 dB(A) hourly L_{eq} at the property line from 7:00 a.m. to 9:59 p.m., and 45 dB(A) hourly L_{eq} from 10:00 p.m. to 6:59 a.m.
- <u>Construction vibration</u> Guidance from Caltrans indicates that a vibration velocity level of 0.1 ips PPV received at a structure would be considered potentially annoying to occupants within (Caltrans 2020a). As for the receiving structure itself, aforementioned Caltrans guidance from Section 2 recommends that a vibration level of 0.3 ips PPV would represent the threshold for building damage risk to older residences, and 0.5 ips PPV to newer residential structures.

For purposes of disclosure, since current CEQA noise criteria listed above do not consider the impacts of the environment on a project, this analysis also evaluates compatibility of on-site noise levels with the City of Chula Vista exterior and interior noise standards of 65 CNEL and 45 CNEL, respectively, as well as the Brown Field Municipal ALUCP residential noise exposure standard of 65 CNEL (SDCRAA 2010).

4.2 City of San Diego Significance Determination Thresholds

This analysis for the Annexation Scenario 2a uses the following City of San Diego CEQA Significance Determination Thresholds (City of San Diego 2022) to evaluate potential noise impacts at off-site land uses under City of San Diego jurisdiction. For the purposes of this assessment for the project, the aforementioned Caltrans guidance is used to determine potential vibration impacts.

Based on the City of San Diego's CEQA Significance Determination Thresholds (City of San Diego 2022), noise impacts may be significant if the project would:

- <u>Construction noise</u> Result in construction noise exposure levels that exceeds 75 dB(A) L_{eq} (12-hour) at the property line of a residentially-zoned property from 7:00 a.m. to 7:00 p.m. (as identified in Section 59.0404 of the City of San Diego's Municipal Code) or if non-emergency construction occurs during the 12-hour period from 7:00 p.m. to 7:00 a.m. Additionally, where temporary construction noise would substantially interfere with normal business communication, or affect sensitive receptors, such as day care facilities, a significant noise impact may be identified.
- <u>Project-attributed stationary noise</u> Result in the exposure of people to noise levels that exceed the City of San Diego's adopted Noise Ordinance, SDMC Section 5.9.5.0401.
- <u>Project-attributed transportation noise</u> Result in the exposure of people to transportation noise levels that exceed the sound level limits as presented in City of San Diego Land Use – Noise Compatibility Guidelines (refer to Table 4 above) and generates more than a 3 dB increase (City of San Diego 2022).

 <u>Construction vibration</u> – Result in the generation of excessive groundborne vibration or groundborne noise levels. Guidance from Caltrans indicates that a vibration velocity level of 0.1 ips PPV received at a structure would be considered potentially annoying to occupants within (Caltrans 2020a). As for the receiving structure itself, aforementioned Caltrans guidance from Section 2 recommends that a vibration level of 0.3 ips PPV would represent the threshold for building damage risk to older residences, and 0.5 ips PPV to newer residential structures.

For purposes of disclosure, since current CEQA noise criteria listed above do not consider the impacts of the environment on a project, this analysis also evaluates compatibility of on-site noise levels with the City of San Diego exterior and interior noise standards of 65 CNEL and 45 CNEL, respectively, as well as the Brown Field Municipal ALUCP residential noise exposure standard of 65 CNEL (SDCRAA 2010).

5.0 Impact Discussion

5.1 Short-Term Construction Noise

5.1.1 Potential Effects to Neighboring Communities

Construction noise and vibration are temporary phenomena. Construction noise and vibration levels vary from hour to hour and day to day, depending on the equipment in use, the operations performed, and the distance between the source and receptor.

Equipment that would be in use during construction would include, in part, graders, backhoes, concrete saws, excavators, dump trucks, loaders, cranes, manlifts, cement mixers, pavers, rollers, welders, and air compressors. The typical maximum noise levels for various pieces of construction equipment at a distance of 50 feet are presented in Table 6. Usually, construction equipment operates in alternating cycles of full power and low power, producing average noise levels over time that are less than the listed maximum noise level. The average sound level of construction activity also depends on the amount of time that the equipment operates and the intensity of construction activities during that time.

Table 6						
Typical Construction Equipment Maximum Noise Levels						
	Typical Equipment					
Equipment Type	(L _{max} , dB(A) at 50 Feet)					
Air compressor	78					
Backhoe	78					
Concrete pump truck	81					
Grader	85					
Crane	81					
Dump Truck	76					
Roller	80					
Manlift	75					
Generator	72					
Front End Loader	79					
Paver	77					
Concrete Saw	90					
Welder	74					
Source: U.S. Department of Transportation 2006						
Note: L_{max} = maximum sound level; dB(A) = A-weighted decibels.						

Aggregate noise emission from project construction activities, broken down by sequential phase, was predicted at two distances to the nearest existing noise-sensitive receptor (NSR): 1) from the nearest position of the construction site boundary and 2) from the geographic center of the construction site, which serves as the time-averaged location or geographic acoustical centroid of active construction equipment for the phase under study. The intent of the former distance is to help evaluate anticipated construction noise from a limited quantity of equipment or vehicle activity expected to be at the boundary for some period of time, which would be most appropriate for phases such as site preparation, grading, and paving. The latter distance is used in a manner similar to the general assessment technique as described in FTA guidance for construction noise assessment (FTA 2018), when the location of individual equipment for a given construction phase is uncertain over some extent of (or the entirety of) the construction site area. Because of this uncertainty, all the equipment for a construction phase is assumed to operate-on average-from the acoustical centroid. Table 7 summarizes these two distances for each apparent closest NSR within the City of San Diego and the City of Chula Vista. For the former, the existing NSR would be one of the existing multi-family residential structures to the east of the project site on Golden Sky Way in the "River Edge Terrace" community; and for the latter, there are multi-family homes south of Rancho Drive immediately west of the I-805 southbound lanes.

At the project site boundary, and as detailed in Attachment 2 (Dudek 2022), this analysis assumes that up to only one piece of equipment of each listed type per phase will be involved in the construction activity for a limited portion of a typical 8-hour construction work shift. In other words, at such proximity, the operating equipment cannot "stack" or crowd the vicinity and still operate. For the acoustical centroid case, which is a geographic average position for all equipment during the indicated phase, this analysis assumes that the equipment may be operating up to all of eight (8) hours per day (i.e., comparable to a typical on-site work shift).

Table 7								
Estimated Distances between Construction Activities and the Nearest Existing City of San Diego								
and City of Chula Vista Noise-Sensitive Receptors (NSR)								
	Distance	Distance	Distance	Distance				
	from	from	from	from				
	Construction	Acoustical	Construction	Acoustical				
	Site	Centroid	Site	Centroid of				
	Boundary	of Site	Boundary	Site				
Construction Phase	(feet)	(feet)	(feet)	(feet)				
(and Equipment Types Involved)	to City of San	Diego NSR	to City of Chu	ula Vista NSR				
Site Preparation (Dozer, Loader)	180	743	700	1,230				
Grading (Excavator, Grader, Dozer, Scraper, Backhoe)*	60	743	700	1,230				
Building Construction (Crane, Forklift, Loader, Welder,	210	743	700	1230				
Generator)	210	7 15	100	1,230				
Architectural Finishes (Air Compressor)	210	743	700	1,230				
Paving (Roller, Backhoe, Dump Truck, Paver)	60	743	700	1,230				
*Off-site improvement areas are accounted for in the	grading phase	of constructi	on					

A Microsoft Excel-based noise prediction model emulating and using reference data from the Federal Highway Administration Roadway Construction Noise Model (RCNM) (Federal Highway Administration [FHWA] 2008) was used to estimate construction noise levels at the nearest occupied noise-sensitive land use. (Although the RCNM was funded and promulgated by the Federal Highway Administration, it is often used for non-roadway projects, because the same types of construction equipment used for roadway projects are often used for other types of construction.) Input variables for the predictive modeling consist of the equipment type and number of each (e.g., two graders, a loader, a tractor), the duty cycle for each piece of equipment (e.g., percentage of time within a specific time period, such as an hour, when the equipment is expected to operate at full power or capacity and thus make noise at a level comparable to what is presented in Table 6, Typical Construction Equipment Maximum Noise Levels), and the distance from the noise-sensitive receptor. The predictive model also considers how many hours that equipment may be on site and operating (or idling) within an established work shift. For the City of San Diego receivers, the shielding provided by the topography of the project site, the slope to the east of the project site, and the elevation of the residential receivers was taken into account. For the more distant City of Chula Vista residential receivers, no topographical or structural shielding was assumed in the modeling. The RCNM has default duty-cycle values for the various pieces of equipment, which were derived from an extensive study of typical construction activity patterns. Those default duty-cycle values were used for this noise analysis, which is detailed in Attachment 2, Construction Noise Modeling Input and Output. Modeling results generated predicted construction noise levels as detailed in Table 8.

Table 8								
Predicted Construction Noise Levels per Activity Phase at Sensitive Receptors								
	12-Hour L _{eq} at	12-Hour L _{eq} at	8-Hour L _{eq} at	8-Hour L _{eq} at				
	Nearest NSR to	Nearest NSR to	Nearest NSR to	Nearest NSR to				
	Construction	Acoustical	Construction	Acoustical				
	Site Boundary	Centroid of Site	Site Boundary	Centroid of Site				
Construction Phase	dB(A)	dB(A)	dB(A)	dB(A)				
(and Equipment Types Involved)	at nearest City o	f San Diego NSR	at nearest City of	f Chula Vista NSR				
First Floor Receptors								
Site Preparation (Dozer, Loader)	52.9	54.5	51.6	51.3				
Grading (Excavator, Grader, Dozer, Scraper,	70.2	56.8	57.5	53.6				
Backhoe)								
Building Construction (Crane, Forklift,	55.7	55.2	53.3	52.0				
Loader, Welder, Generator)								
Architectural Finishes (Air Compressor)	47.0	43.5	44.6	40.3				
Paving (Roller, Backhoe, Dump Truck,	62.4	50.4	49.7	47.2				
Paver)								
Second Floor Receptors								
Site Preparation (Dozer, Loader)	63.2	54.5	51.6	51.3				
Grading (Excavator, Grader, Dozer, Scraper,	74.0	56.8	57.5	53.6				
Backhoe)								
Building Construction (Crane, Forklift,	63.3	55.2	53.3	52.0				
Loader, Welder, Generator)								
Architectural Finishes (Air Compressor)	54.6	43.5	44.6	40.3				
Paving (Roller, Backhoe, Dump Truck,	66.2	50.4	49.7	47.2				
Paver)								
Notes: L_{co} = equivalent noise level: dB(A) = A-weighted decibels: NSR = noise-sensitive recentor								

As presented in Table 8, the estimated construction noise levels at the nearest City of Chula Vista NSR are predicted to be far less than 80 dB(A) L_{eq} over an 8-hour period—even when phase activities may take place near the northwest project boundaries. At the nearest City of San Diego NSR, predicted 12-hour L_{eq} values shown in Table 8 for each project construction phase are less than 75 dB(A). Hence, under these conditions, predicted operation of construction equipment and processes do not exceed both the FTA-based guidance construction noise threshold of 80 dB(A) 8-hour L_{eq} and the City of San Diego code-based threshold for construction noise level of 75 dB(A) 12-hour L_{eq} .

Compared to measurements of the daytime outdoor ambient sound level at representative sample locations as shown in Table 5, predicted construction noise levels ranging in the middle to upper sixties (for City of San Diego second floor receptors) of dB(A) as appearing in Table 8 are considerably higher and would be clearly perceptible to an average listener having healthy human hearing. However, at nearby off-site residences exposed to such construction-related noise, the increased noise levels would typically be relatively short term and temporary—lasting only as long as construction occurs during allowable hours. Construction activities associated with the project would be limited to those hours specified in the applicable city municipal code, which are detailed in Section 2.3, Local. More specifically, the No Annexation Scenario construction would be limited to 7:00 a.m.– 10:00 p.m., Monday–Friday, and 8:00 a.m.–10:00 p.m., Saturday and Sunday). Under the Annexation Scenario 2a, construction activities would be limited to 7:00 a.m. to 7:00 p.m., and construction noise would not exceed 75 dB during that 12-hour period. Temporary construction noise would not interfere with normal business communication, or affect sensitive receptors. Thus, project would

comply with both the SDMC and the City of Chula Vista Municipal Code, and construction noise impacts would be **less than significant** under both the No Annexation and Annexation scenarios.

5.1.2 Potential Effects to Nearby Sensitive Biological Resources

Indirect noise impacts to sensitive biological resources result primarily from adverse edge effects on-site or off-site, and may be short term (temporary), related to construction, or long term, associated with development in proximity to biological resources within natural open space. Noise impacts would be significant if construction or operational noise levels would exceed 60 dB(A) L_{eq} , or the existing ambient noise level if already above 60 dB(A) L_{eq} during the breeding season.

Within the City of Chula Vista Subarea Plan, the project parcel is designated as "Development Area Outside Covered Projects" (i.e., not designated a preserve or conservation area) and is not located immediately adjacent to any 75 percent or 100 percent Conservation Areas. The closest conservation area (75 percent) is located approximately 197 feet north of the project area within the Otay River. While the project parcel and land to the north of the parcel is within the City of Chula Vista Subarea Plan, the land to the west, south and east of the parcel are located within the City of San Diego Subarea Plan. The nearest City of San Diego Subarea Plan MHPA area is located approximately 180 feet west of the project parcel, across I-805.

Noise in the vicinity of the project site is dominated by vehicle traffic on I-805. To determine the existing ambient noise level at the adjacent habitat, existing noise levels due to traffic on I-805 and Dennery Road were modeled using the SoundPLAN program. Based on Caltrans traffic counts, the existing volume on I-805 is 150,000 average daily traffic (ADT) (Caltrans 2020b). The existing traffic volumes on Dennery Road are 13,869 ADT south of Regatta Lane and 8,333 ADT north of Regatta Lane (LOS Engineers, Inc. 2022). Existing vehicle traffic noise contours are shown in Figure 5.

Existing ambient noise levels and maximum construction noise levels, which would occur during the grading phase) were calculated at three specific receivers located at the Chula Vista conservation areas and the San Diego MHPA (see Figure 5). The results are shown in Table 9. SoundPLAN data is provided in Attachment 3.

Table 9 Predicted Construction Noise Levels at Sensitive Habitat							
		Existing Ambient Noise Level Maximu					
		Average Daytime	Peak Hour	Construction			
		Hourly Noise Level	Noise Level	Noise Level			
Receiver	Location	[dB(A) L _{eq}]	[dB(A) L _{eq}]	[dB(A) L _{eq}]			
1	Chula Vista Conservation Area – West	71	72	57			
2	Chula Vista Conservation Area – East	60	62	58			
3	San Diego MHPA - 180 feet to the West	77	79	57			



City of San Diego MSCP Subarea Plan

City of San Diego MHPA

RE(

City of Chula Vista MSCP Subarea Plan

75% Conservation Area - Habitat Preserve

55 CNEL - 60 CNEL - 65 CNEL

- 70 CNEL - 75 CNEL

FIGURE 5

Existing Vehicle Traffic Noise Contours

JON M:\JOBS\3396-1\common_gis\Reports\Nostec\Fig5.mxd 05/16/2023 bma As shown, existing ambient noise levels currently exceed 60 dB(A) Lea. During daytime hours when construction activity noise would occur, pre-existing outdoor ambient sound in the MSCP preserve areas north of the project site are already dominated by I-805 traffic noise that is greater than 60 dB(A) as shown in Table 9. Therefore, construction noise levels would not have the potential to result in a construction noise impact to sensitive species inhabiting proximate preserve areas as the pre-existing outdoor noise environment is already in excess of 60 dB(A) Leq. On this basis, potential construction noise impacts to sensitive wildlife species inside the MSCP preserve would be considered less than significant. However, as further detailed in the Biological Resources Technical Report (RECON 2023), Least Bell's vireo are located on and adjacent to the project site outside the MSCP preserve. Indirect impacts to least Bell's vireo may occur if construction activities are conducted during this species' breeding season of March 15 to September 15. Occupied suitable habitat (southern willow scrub, mule fat scrub) for this species occurs both on-site and adjacent to the project impact area and construction is likely to cause noise levels within these habitat areas to exceed 60 dB(A) Lea, which would be considered a significant indirect impact requiring mitigation under both cities' Subarea Plans. Implementation of mitigation measures SD-BIO-5 and CV-BIO-5, as detailed in the Biological Resources Technical Report would be required.

5.2 Conventional Construction Activity Vibration

Construction activities may expose persons to excessive groundborne vibration or groundborne noise, causing a potentially significant impact. Caltrans has collected groundborne vibration information related to construction activities (Caltrans 2020a). Information from Caltrans indicates that continuous vibrations with a velocity amplitude of approximately 0.1 ips PPV can be characterized as being "strongly perceptible" or "begins to annoy" building occupants. For context, heavier pieces of construction equipment, such as a bulldozer that may be expected on the project site, have peak particle velocities of approximately 0.089 ips or less at a reference distance of 25 feet (FTA 2018).

Groundborne vibration attenuates rapidly, even over short distances. The attenuation of groundborne vibration as it propagates from source to receptor through intervening soils and rock strata can be estimated with expressions found in FTA and Caltrans guidance. By way of example, for a bulldozer operating on site and as close as the eastern project boundary (i.e., approximately 60 feet from the nearest receiving occupied structure on Golden Sky Way, when the project emergency access roadway would be graded) the estimated vibration velocity level would be 0.024 ips per the equation as follows (FTA 2018):

$$PPV_{rcvr} = PPV_{ref} * (25/D)^{1.5} = 0.024 = 0.089 * (25/60)^{1.5};$$

where PPV_{revr} is the predicted vibration velocity at the receiver position, PPV_{ref} is the reference value at 25 feet from the vibration source (the bulldozer), and D is the actual horizontal distance to the receiver. Therefore, at this predicted PPV that is less than the 0.1 ips PPV guidance-based threshold adopted herein, the impact of vibration-induced annoyance to occupants of nearby existing homes would be **less than significant** under both the No Annexation and Annexation scenarios.

Construction vibration, at sufficiently high levels, can also present a building damage risk. However, the predicted 0.024 ips PPV at the nearest residential receiver 60 feet away from on-site operation

of the bulldozer during grading would not surpass the guidance limit of 0.3 to 0.5 ips PPV for preventing damage to residential structures (Caltrans 2020a). Because the predicted vibration level at 60 feet (in the City of San Diego) is less than both the annoyance and building damage risk thresholds, vibration from project conventional construction activities is considered less than significant. The nearest City of Chula Vista existing residential receptor is even more distant from the project, and would therefore also be expected to experience a less than significant impact.

Once operational, the project would not be expected to feature major on-site producers of groundborne vibration. Anticipated mechanical systems like pumps are designed and manufactured to feature rotating components (e.g., impellers) that are well-balanced with isolated vibration within or external to the equipment casings. On this basis, potential vibration impacts due to project operation would be **less than significant**.

5.3 Long-Term Operational Noise

5.3.1 Off-Site Roadway Traffic Noise

The project would increase traffic volumes on local roadways. However, the project would not substantially alter the vehicle classifications mix on local or regional roadways nor would the project alter the speed on an existing roadway or create a new roadway. Thus, the primary factor affecting off-site noise levels would be increased traffic volumes. While changes in noise levels would occur along any roadway where project-related traffic occurs, for noise assessment purposes, noise level increases are assumed to be greatest nearest the project site, as this location would represent the greatest concentration of project-related traffic. A substantial noise increase is defined as an increase of 3 dB(A) above existing conditions.

The roadways included in the traffic impact analysis are Dennery Road and Palm Avenue. Traffic noise levels were calculated based on the total average daily traffic volumes on each roadway segment. For modeling purposes, "hard" ground conditions were used for the analysis of future conditions since a majority of the project area is paved and the hard site provides the most conservative impact assessment. Modeled off-site noise levels do not account for shielding provided by intervening barriers and structures.

Existing (year 2020), near term (year 2025), and future (year 2062) traffic volumes on Dennery Road and Palm Avenue with and without the project were obtained from the Local Mobility Analysis prepared for the project (LOS Engineers, Inc. 2022). Table 10 summarizes the roadway segment volumes.

Table 10 Roadway Segment ADT Volumes								
	Average Daily Traffic							
		Year		Year		Year		
		2020 +	Year	2025 +	Year	2062 +	Speed	
Roadway Segment	Year 2020	Project	2025	Project	2062	Project	(mph)	
Dennery Road								
Palm Avenue to Regatta Lane	13,869	15,733	13,994	15,858	19,500	21,364	35	
Regatta Lane to Landing Driveway	8,333	10,235	8,473	10,375	12,500	14,402	35	
Landing Driveway to Red Coral	8,224	10,126	8,354	10,256	12,500	14,402	35	
Palm Avenue								
I-805 Southbound Ramps to I-805 Northbound Ramps	36,383	37,315	38,031	38,963	46,000	46,932	45	
I-805 Northbound Ramps to Dennery Road	49,173	50,733	51,613	53,173	59,500	31,060	45	
mph = miles per hour SOURCE: LOS Engineering, Inc. 2023.								

Using these parameters, noise levels were calculated at 50 feet from the centerline using the FHWA RD-77-108 model. Table 11 presents a conservative assessment of traffic noise levels based on the existing (year 2020), near term (year 2025), and future (year 2062) noise levels without and with the project. Table 11 also summarizes the direct and cumulative traffic noise level increases due to the project. Noise level calculations are contained in Attachment 4. It is noted that this traffic volume data is considered conservative, as the Local Mobility Analysis (LOS Engineering, Inc. 2023) utilized a 221-unit project scenario that has higher volumes than the proposed 215-unit project.

Table 11 Traffic Noise Level with and without Project and Ambient Noise Increases (CNEL)										
	Year 2020			Year 2025			Year 2062			Cumulative
	No			No			No			Over
Roadway Segment	Project	Project	Increase	Project	Project	Increase	Project	Project	Increase	Existing
Dennery Road										
Palm Avenue to Regatta Lane	69.6	70.2	0.6	69.6	70.2	0.6	71.1	71.5	0.4	1.9
Regatta Lane to Landing Driveway	67.4	68.3	0.9	67.5	68.3	0.8	69.2	69.8	0.6	2.4
Landing Driveway to Red Coral	67.3	68.2	0.9	67.4	68.3	0.9	69.2	69.8	0.6	2.5
Palm Avenue										
I-805 Southbound Ramps to I-805 Northbound Ramps	75.9	76.0	0.1	76.1	76.2	0.1	76.9	77.0	0.1	1.1
I-805 Northbound Ramps to Dennery Road	77.2	77.3	0.1	77.4	77.5	0.1	78.0	78.1	0.1	0.9
Note: Increase calculations may vary due to independent rounding.										

As shown, the project would result in direct noise level increases ranging from 0.4 to 0.9 dB(A) on Dennery Road, and a direct noise level increase of 0.1 dB(A) on Palm Avenue. Cumulatively, when

comparing future year 2062 traffic noise levels to existing noise levels, the increase would range from 0.9 to 2.5 dB(A). The project would not result in a direct or cumulative noise increase of more than 3 dB. Therefore, the project would result in less than significant direct and cumulative impacts related to traffic noise for both the No Annexation and Annexation scenarios.

5.3.2 Stationary Operations Noise

The proposed residential project will add a variety of noise-producing mechanical equipment discussed below. Most of these noise-producing equipment or sound sources would be considered stationary, or limited in mobility to a defined area. Predicted noise levels associated with the post-construction operation of the project on-site stationary equipment have been calculated using the SoundPLAN model.

The project includes 61 detached condominiums that function similar to single-family home structures, 84 duplexes, and 70 townhome dwelling unit structures. Each of these 215 structures would be expected to feature mechanical ventilation and an outdoor-exposed air-cooled condenser (ACC) that provides cooling (expressed herein as refrigeration tonnage). For purposes of this analysis, each single-family structure was assigned an ACC rated for 1.5 to 3 tons of cooling, which can be represented by a Carrier 16NA18 model having a sound pressure level of 68 dB(A) at a distance of one meter (Carrier 2012). Each duplex and multi-family structure would have two such Carrier units (or comparable from a different manufacturer) or a larger unit delivering twice the refrigeration capacity but emitting a 3 dB(A) (i.e., double the sound energy) higher noise level. The locations of these anticipated ACC units, assumed to be point-type sources at a height of one meter above local grade, are shown in Figure 6.

The project would also include pocket parks throughout the site. These pocket parks would include mostly passive uses such as benches, shade structures, trails, and decorative landscaping that would not be a significant source of noise. However, pocket parks may also include play structures or tot-lots that would generate noise from children at play. Noise levels due to children at play are not anticipated to exceed Chula Vista or San Diego noise level limits; however, as a conservative analysis, these noise sources were also included in the SoundPLAN modeling. A sound power level of 55 dB(A) was modeled at each pocket park location (Navcon Engineering, Inc. 2018).

Noise levels were modeled at receivers located at the multi-family residential uses to the east and at the project property lines. The results are summarized in Table 12. SoundPLAN data is provided in Attachment 5.



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Table 12 Predicted Project Stationary Source Operations Noise						
Modeled Receiver		Predicted hourly L_{eq}				
Position	Receiver Position Description	[dB(A)]				
R01	Near southwestern corner of River Edge Terrace building north of Golden Sky Way	36.1				
R02	Near River Edge Terrace building east of Golden Sky Way	34.7				
R03	Near River Edge Terrace building east of Golden Sky Way	35.5				
R04	Near River Edge Terrace building west of Ocean Mist Place	39.6				
R05	Near River Edge Terrace building west of Ocean Mist Place	39.7				
R06	Near River Edge Terrace building west of Ocean Mist Place	37.6				
R07	Near River Edge Terrace building south of Ocean Mist Place	29.9				
REPL	Approximate midpoint of eastern project property line	43.5				
RSPL	Approximate midpoint of southern project property line	38.9				
RWPL	Approximate midpoint of western project property line	45.4				
RNPL	Approximate midpoint of northern project property line	43.8				

The most restrictive City of Chula Vista noise level limit for multi-family uses is 50 dB(A) L_{eq} , and the most restrictive City of San Diego noise level limit for multi-family uses is 45 dB(A) L_{eq} . Predicted aggregate pocket park and ACC operation noise levels, even assuming all units are operating on a hot summer night, at receiver positions along the River Edge Terrace property line (R01 through R07) would be less than 45 dB(A) and thus be considered compliant with both the City of Chula Vista and the City of San Diego noise ordinance limits, resulting in a **less than significant** impact related to stationary operational noise for both the No Annexation and Annexation scenarios.

Furthermore, the predicted stationary-source operation noise level of 29.9 to 39.7 dB(A) at Receivers R01 through R07 are substantially lower than the predicted transportation noise level of 60 CNEL as shown in Figure 5; hence, noise from the project's residential air-conditioning units is not expected to cause more than an imperceptible dB increase to the outdoor ambient sound level at off-site receivers, which would be considered a **less than significant** impact for both the No Annexation and Annexation scenarios.

As previously discussed, noise impacts would be significant if construction or operational noise levels would exceed 60 dB(A) L_{eq} , or the existing ambient noise level if already above 60 dB(A) L_{eq} during the breeding season. As discussed in Section 5.1.2, least Bell's vireo have been observed on and adjacent to the project site. As shown in Table 12, operational noise levels at the property boundaries would range from 38.9 to 45.4 dB(A) L_{eq} at the property lines. These noise levels would be less at greater distances from the property line. Additionally, as shown in Figure 6, operational noise levels within the avoided on-site areas that would be placed in a covenant of easement as detailed in the Biological Resources Technical Report, are not projected to exceed 60 dB(A) L_{eq} . Therefore, operational noise levels would not exceed 60 dB(A) L_{eq} within the on-site drainage or adjacent habitat areas that may support least Bell's vireo. Impacts would be considered **less than significant**.

5.4 Land Use Noise Compatibility (Non-CEQA Analysis)

CEQA requires analysis of a project's effects on the environment and is not intended to evaluate the impacts of the environment on a project. Therefore, the analysis of potential adverse effects of

existing noise levels on the project is not a required analysis under CEQA. However, for the purposes of disclosure and land use consistency analysis, a noise compatibility analysis is provided of on-site noise levels with the City of Chula Vista and City of San Diego exterior and interior noise standards of 65 CNEL and 45 CNEL, respectively, as well as the Brown Field Municipal ALUCP residential noise exposure standard of 65 CNEL (SDCRAA 2010).

5.4.1 Aviation Noise Exposure

There are no private airstrips within the vicinity of the project site. The closest airport to the project site is the Brown Field Municipal Airport approximately 2.3 miles southeast of the site. Although the project site is located within "Review 2 Area" Airport Influence Area per Exhibit III-6 of the Brown Field Municipal ALUCP (SDCRAA 2010), the project site is located outside of the 55 CNEL future aviation noise contour and thus well below the 65 CNEL compatibility standard. Hence, future residences would not be exposed to significant aircraft noise levels under both the No Annexation and Annexation scenarios.

5.4.2 Traffic Noise Exposure

The SoundPLAN program was used to calculate on-site vehicle traffic noise levels. The SoundPLAN program uses the FHWA Traffic Noise Model algorithms and reference levels to calculate noise levels at selected receiver locations. The model uses various input parameters, such as projected hourly average traffic rates; vehicle mix, distribution, and speed; roadway lengths and gradients; distances between sources, barriers, and receivers; and shielding provided by intervening terrain, barriers, and structures. Receivers, roadways, and barriers were input into the model using three-dimensional coordinates. The locations of future buildings were obtained from project plans and drawings. Project site grading and area topography were taken into account.

The main source of traffic noise at the project site is from vehicle traffic on I-805 and Dennery Road. Future year 2062 with project traffic volumes for Dennery Road (see Table 10) were obtained from the Local Mobility Analysis prepared for the project (LOS Engineers 2022). Future year 2050 traffic volumes for I-805 were obtained from San Diego Association of Governments (SANDAG) Series 14 traffic projections (SANDAG 2022). I-805 has a future year 2050 traffic volume of 157,250 (73,700 ADT on the northbound segments and 81,500 ADT on the southbound segments). A vehicle classification mix of 93.0 percent automobiles, 3.7 percent medium trucks, and 3.3 percent heavy trucks was obtained from Caltrans truck counts (Caltrans 2020c).

Vehicle traffic noise level contours across the project site were calculated using SoundPLAN. These contours take into account shielding provided by proposed buildings, topography, and proposed grading. These noise contours are shown in Figure 7. As shown, first-floor noise levels would exceed 70 CNEL across the western portion project site closest to I-805. Noise levels would be less than 65 CNEL across the eastern half of the project site.

To determine exterior noise levels at the exterior use areas and the first-, second-, and third-floor building façades, noise levels were modeled at 75 specific receiver locations, as shown in Figure 7. Exterior noise levels were modeled at first- through third-floor elevations. The results are summarized in Table 13. SoundPLAN data are provided in Attachment 6.



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Table 13							
Future Vehicle Traffic Noise Levels							
Exterior Noise Level (CNEL)							
Receiver	Location	First Floor	Second Floor	Third Floor			
1	Duplex Backyard	47	51	54			
2	2 Mini Park		54	58			
3	Duplex Backyard	55	56	58			
4	Duplex Backyard	59	58	60			
5	Duplex Backyard	59	61	64			
6	Duplex Backyard	63	67	70			
7	Building Façade	67	69	72			
8	Building Façade	63	64	66			
9	Building Façade	64	67	69			
10	Building Façade	68	71	73			
11	Duplex Backyard	66	68	69			
12	Duplex Backyard	58	59	62			
13	Duplex Backyard	56	57	60			
14	Duplex Backvard	54	56	59			
15	Building Facade	70	73	74			
16	Building Facade	69	71	72			
17	Building Facade	67	68	69			
18	Building Facade	65	65	66			
19	Building Facade	63	64	65			
20	Building Facade	64	65	66			
21	Building Facade	65	66	67			
22	Building Facade	67	68	69			
23	Building Facade	72	74	75			
24	Building Facade	67	68	69			
25	Building Facade	64	64	65			
26	Building Facade	61	62	63			
27	Building Facade	73	74	75			
28	Building Facade	70	71	72			
29	Building Facade	67	69	70			
30	Building Facade	65	66	67			
31	Building Facade	63	64	65			
32	Building Facade	61	62	63			
33	Building Facade	62	62	64			
34	Building Facade	63	64	66			
35	Building Façade	64	65	67			
36	Building Facade	68	69	71			
37	Building Facade	72	73	74			
38	Condo Backvard	66	67	69			
30	Condo Backvard	62	63	65			
40	Condo Backyard	61	62	64			
<u>41</u>	Building Facade	70	70	71			
42	Building Facade	70	70	70			
42	Building Facada	70	70	70			
44	Building Façade	69	69	69			
45	Building Facada	67	67	67			
46	Building Facada	63	64	64			
<u>40</u>	Building Facada	60	61	62			
	Building Eacado	60	61	63			
40	Building Escado	62	62	64			
43	bullulliy Façaue	0.5	0.5	04			

Table 13								
Exterior Noise Level (CNEL)								
Receiver	Location	First Floor	Second Floor	Third Floor				
50	Building Façade	66	66	67				
51	Building Façade	70	71	71				
52	Condo Backyard	69	69	69				
53	Condo Backyard	66	67	66				
54	Condo Backyard	64	65	65				
55	Condo Backyard	63	64	64				
56	Building Façade	61	63	63				
57	Building Façade	63	64	64				
58	Building Façade	65	65	66				
59	Building Façade	67	67	68				
60	Mini Park	71	71	71				
61	Condo Backyard	69	69	69				
62	Condo Backyard	69	68	68				
63	Condo Backyard	68	68	68				
64	Condo Backyard	68	67	67				
65	Condo Backyard	67	67	67				
66	Mini Park	63	62	63				
67	Condo Backyard	67	67	66				
68	Condo Backyard	66	66	66				
69	Condo Backyard	66	66	66				
70	Condo Backyard	66	65	65				
71	Condo Backyard	65	65	65				
72	Condo Backyard	65	64	64				
73	Eastern Property Line	48	49	52				
74	Eastern Property Line	48	50	53				
75	75 Eastern Property Line 44 46 51							
Bold = Exceeds 65 CNEL at exterior use area								

5.4.2.1 Exterior Noise

No Annexation Scenario and Annexation Scenario 2b

Under the No Annexation Scenario and Annexation Scenario 2b, the project would be developed within the City of Chula Vista; therefore, the City of Chula Vista standards apply. The City of Chula Vista's exterior noise level standard for residential uses is 65 CNEL. This noise level is applicable at the exterior use areas. The interior noise level standard is 45 CNEL.

As shown in Table 13, exterior noise levels are projected to range from 44 to 75 CNEL. The exterior use areas include the mini parks (Receivers 2, 60, and 66) and the backyards of the duplexes (Receivers 1, 3 through 6, and 11 through 14) and detached condominiums (Receivers 38 through 40, 52 through 55, 61 through 65, and 67 through 72). As shown in Table 13, exterior noise levels are projected to exceed the residential standard of 65 CNEL at the mini park closest to I-805 (Receiver 60) and at the backyards closest to I-805 (Receivers 11, 38, 52, 53, 61 through 65, and 67 through 70). To reduce exterior noise levels at these locations, as a project design feature, six-foot barriers were modeled as shown in Figure 8. The resulting noise levels at the exterior use areas are summarized in Table 14.



6-foot Park Barrier Site

Plan RECON M:\/OBS\3396-1\common_gis\Reports\Nostec\Fig8.mxd 05/16/2023 bma FIGURE 8 Noise Barriers

Table 14						
Unmitigated and Mitigated Noise Levels at Exterior Use Areas						
		Exterior Noise Level (CNEL)				
Receiver		Without Barrier	With Barrier			
1	Duplex Backyard	47	47			
2	Mini Park	51	51			
3	Duplex Backyard	55	55			
4	Duplex Backyard	59	59			
5	Duplex Backyard	59	59			
6	Duplex Backyard	63	63			
11	Duplex Backyard	66	64			
12	Duplex Backyard	58	58			
13	Duplex Backyard	56	56			
14	Duplex Backyard	54	54			
38	Condo Backyard	66	65			
39	Condo Backyard	62	63			
40	Condo Backyard	61	61			
52	Condo Backyard	69	65			
53	Condo Backyard	66	63			
54	Condo Backyard	64	63			
55	Condo Backyard	63	62			
60	Mini Park	71	67			
61	Condo Backyard	69	63			
62	Condo Backyard	69	62			
63	Condo Backyard	68	62			
64	Condo Backyard	68	61			
65	Condo Backyard	67	61			
66	Mini Park	63	62			
67	Condo Backyard	67	59			
68	Condo Backyard	66	63			
69	Condo Backyard	66	62			
70	Condo Backyard	66	60			
71	Condo Backyard	65	58			
72	Condo Backyard	65	57			
Bold = Exceeds 65 CNEL at exterior use area						

As shown in Table 14, without incorporation of the six-foot barriers shown in Figure 8, exterior noise levels at the proposed backyards would exceed 65 CNEL at Receivers 11, 38, 52, 53, 61 through 65, and 67 through 70. With the incorporation of noise barriers, noise levels at the mini park would be reduced, but not to 65 CNEL or less. However, as discussed in Section 2.3.1.2, the minimum amount of required exterior use space shall meet the 65 CNEL criteria, with any additional area being exempt from this requirement. As the mini park is in excess of minimum required exterior use space, it is not subject to the 65 CNEL exterior noise level. Construction of the six-foot backyard barriers identified in Figure 8 would be required to reduce exterior noise levels at the backyards to 65 CNEL or less. The following project design feature would be required as a condition of approval.

PDF-CV- NOS-1On-Site Noise Barriers. Exterior noise levels at the backyards (Receivers 11, 38, 52, 53, 61 through 65, and 67 through 70) as identified on Figure 8 shall be reduced to the City of Chula Vista's threshold of 65 CNEL for residential uses. Noise reduction for exterior traffic noise impacts can be accomplished through

on-site noise barriers. Six-foot sound walls as identified on Figure 8 shall be constructed. The sound attenuation walls must be solid and free of cracks or holes. They can be constructed of masonry, wood, plastic, plexi-glass, fiberglass, steel, or a combination of those materials, as long as there are no cracks or gaps, through or below the wall. Any seams or cracks must be filled or caulked. If wood is used, it can be tongue and groove and must be at least one-inch total thickness or have a density of at least 3.5 pounds per square foot.

With the incorporation of project design feature PDF-CV-NOS-1, exterior noise levels at all backyards would be reduced to the City of Chula Vista's compatibility standard 65 CNEL or below.

Annexation Scenario 2a

Under Annexation Scenario 2a, the project would be annexed to the City of San Diego. Multi-family residential uses are "compatible" with exterior noise levels up to 60 CNEL, and "conditionally compatible" with exterior noise levels up to 70 CNEL. In "conditionally compatible" areas, feasible noise mitigation techniques should be analyzed and incorporated to make the outdoor activities acceptable, and building structures must attenuate exterior noise levels to an indoor noise level of 45 CNEL. Additionally, as stated in Section B of the City's Noise Element, although not generally considered compatible, the City conditionally allows multi-family and mixed-use residential uses up to 75 CNEL in areas affected by motor vehicle traffic noise with existing residential uses. Any future residential use exposed to noise levels up to 75 CNEL must include attenuation measures to ensure an interior noise level of 45 CNEL and be located in an area where a community plan allows multi-family and mixed-use residential uses. The project would also include pocket parks. Parks are "compatible" in areas up to 70 CNEL and "conditionally compatible" in areas up to 75 CNEL. Refer to Section 5.3.2.2. for Interior Noise Analysis.

As shown in Figure 7 and Table 13, exterior noise levels are projected to exceed 70 CNEL only at the receivers located closest to I-805 (Receivers 23, 27, 37, and 60). However, Receivers 23, 27, and 37 do not represent exterior use areas, and were modeled for the purposes of the interior noise analysis below. Noise levels at Receiver 60 (Mini Park) would exceed the parks compatibility level of 70 CNEL and noise levels at the residential exterior use areas would be exposed to the "conditionally compatible" range of 60 to 70 CNEL at (Receivers 11, 38, 52, 53, 61 through 65, and 67 through 70). The following project design feature would be required as a condition of approval.

PDF-SD-NOS-1 On-Site Noise Barriers. Exterior noise levels at the backyards and at the mini park (Receivers 11, 38, 52, 53, 60, 61 through 65, and 67 through 70) as identified on Figure 8 shall be reduced to the City of San Diego noise compatibility standards for residential and park uses (60 CNEL and 70 CNEL, respectively). Noise reduction for exterior traffic noise impacts can be accomplished through on-site noise barriers. Six-foot sound walls as identified on Figure 6 shall be constructed. The sound attenuation walls must be solid and free of cracks or holes. They can be constructed of masonry, wood, plastic, plexi-glass, fiberglass, steel, or a combination of those materials, as long as there are no cracks or gaps, through or below the wall. Any seams or cracks must be filled or caulked. If wood is used, it can be tongue and groove and must be at least one-inch total thickness or have a density of at least 3.5 pounds per square foot.

As shown in Table 14, construction of the six-foot park barrier would reduce noise levels to 67 CNEL at the mini park (Receiver 60) which would result in noise compatible with the City's exterior noise level standard for parks. For the receivers located in areas exposed to the "conditionally compatible" range of 60 to 70 CNEL, construction of the six-foot backyard barriers shown in Figure 8 (PDF-SD-NOS-1) would reduce exterior noise levels to 65 CNEL or less. While the noise levels at residential receivers would be above the exterior noise exposure compatibility level of 60 CNEL identified in the City of San Diego General Plan Noise Element (City of San Diego 2015), interior residential noise levels would be controlled to the 45 CNEL interior noise limit as discussed below.

5.4.2.2 Interior Noise

No Annexation and Annexation Scenarios

Typically, with the windows open, building shells provide approximately 15 dB(A) (i.e., an average of 12–18 dB(A) [OPR 2017]) of exterior-to-interior noise reduction; while with windows closed residential construction generally provides a minimum of 25 dB(A) attenuation (FHWA 2011). Arithmetically adding this minimum 25 dB(A) closed-window exterior-to-interior sound insulation performance to the acoustical goal of 45 CNEL interior background sound level means up to 70 CNEL exterior noise level (i.e., 25+45=70) would not be anticipated to cause an exceedance to the inhabited indoor space. But Table 13 shows that the 1st floor through 3rd floor façade locations at the western portion of the project site are anticipated to be exposed to an exterior noise level greater than 70 CNEL, resulting in interior noise levels that would exceed the compatibility standard of 45 CNEL.

For these future occupied residences, where predicted exterior noise exposure would exceed 70 CNEL as shown in Table 13, an exterior-to-interior noise analysis was performed to assess compliance with the interior background sound level threshold of 45 CNEL. This analysis involves estimating the composite sound transmission class (STC) of sample project exterior wall assemblies, including fenestration, that are typical of modern energy-efficient residential building construction.

This exterior-to-interior noise assessment presumes the above exterior wall assembly features represent a minimum for purposes of sound insulation performance and are compatible with the Design Guidelines outlined in the Specific Plan. Results of this analysis for the three listed façade receptor positions (and their associated inhabited interior spaces, such as a bedroom or living room) appears in Table 15.

Table 15 Predicted Net Sound Transmission Class of Sample Occupied Room Facade						
Modeled	Modeled Predicted Net Sound Warshission class of Sample Occupied Noom Aquat					
Receiver			Closed	Window Open		
Position	Occupied Room Façade	No Window	Window	(1-foot tall)		
6 Proposed SW Duplex – 2 nd or 3 rd Floor "Bedroom 4" (facing I-805) ¹ n/a 38 13						
37	n/a	n/a				
37Proposed NW Single-Family – 2 nd Floor "Bedroom 4" (facing I-805)3n/a3914						
STC = sound	l transmission class; I-805 = Interstate 805; n	/a = not applica	able			
¹ per Nakano Design Guidelines, room has 10.5-foot-long wall; analysis assumes 9 feet tall; window is 4' x 4'						
² per Nakano Design Guidelines, room has 16-foot-long wall; analysis assumes 9 feet tall; no window						
³ per Nakano Design Guidelines, room has 13-foot-long wall; analysis assumes 9 feet tall; window is 4' x 4'						
n/a = not ap	plicable					

Table 15 illustrates that partially open windows greatly compromise the sound insulation performance of the studied wall assemblies, consistent with aforementioned guidance. However, when such windows are closed, all studied sample facades are anticipated to exhibit a predicted STC rating of at least 38, and thus would provide sufficient exterior-to-interior sound insulation from outdoor traffic noise to yield interior background sound levels that are less than 45 CNEL and thus compliant with the City and state standards. Recall that none of the predicted exterior traffic noise levels at the studied receptor locations exceeded 75 CNEL; thus, the STC rating value (for closed windows and doors) subtracted from these exterior noise values must result in interior noise levels of less than 45 CNEL (e.g., 75 - 38 = 37 CNEL, which is less than 45).

To ensure that the interior noise level standard for residential uses of 45 CNEL can be met, a site-specific interior noise analysis would be required prior to issuance of a building permit to ensure that window, door, and wall components would achieve a necessary sound transmission class rating required to reduce interior noise levels to 45 CNEL or less. As a condition of approval, the following project design feature would be required:

PDF-NOS-2 Interior Noise An exterior-to-interior noise analysis shall be conducted by the project applicant for the proposed dwelling units expected to be exposed to noise levels in excess of 60 CNEL (e.g., units facing Interstate 805) prior to issuance of building permits. Installation of mechanical ventilation systems or air conditioning systems and sound-rated windows shall be required if the predicted interior background noise due to traffic noise intrusion through the building envelope assemblies exceeds the 45 CNEL interior standard. The acoustical analysis shall substantiate that the resulting interior background noise levels, with appropriate implementation of interior comfort systems and sound insulation, would be less than this noise standard.

Implementation of project design feature PDF-NOS-2 would ensure that the interior background noise level for inhabited rooms would meet the state and both City of San Diego and City of Chula Vista interior noise standard of 45 CNEL.

6.0 Mitigation Measures and Project Design Features

6.1 Mitigation Measures

Noise impacts associated with short-term construction noise to neighboring communities, vibration, off-site traffic noise, and stationary noise would be less than significant. No mitigation would be required. However, short-term construction noise would result in indirect impacts to least Bell's vireo. With implementation of mitigation measures CV-BIO-5 in the No Annexation Scenario and Annexation Scenario 2b and SD-BIO-5 in the Annexation Scenario 2a, construction noise impacts to sensitive wildlife species would be reduced to less than significant.

CV-BIO-5 Least Bell's Vireo Avoidance. For any work proposed between March 15 and September 15, a pre-construction survey for the least Bell's vireo shall be performed in order to reaffirm the presence and extent of occupied habitat. The pre-construction survey area for the species shall encompass all potentially suitable habitat within the project work zone, as well as a 300-foot survey buffer. The pre-construction survey shall be performed to the satisfaction of the Development Services Director (or their designee) by a qualified biologist familiar with the City of Chula Vista MSCP Subarea Plan. The results of the pre-construction survey must be submitted in a report to the Development Services Director (or their designee) for review and approval prior to the issuance of any land development permits and prior to initiating any construction activities. If least Bell's vireo is detected, a minimum 300-foot buffer delineated by orange biological fencing shall be established around the detected species to ensure that no work shall occur within occupied habitat from March 15 through September 15. On-site noise reduction techniques shall be implemented to ensure that construction noise levels not exceed 60 dB(A) Leq at the location of any occupied sensitive habitat areas. The Development Services Director (or their designee) shall have the discretion to modify the buffer width depending on site-specific conditions. If the results of the pre-construction survey determine that the survey area is unoccupied, the work may commence at the discretion of the Development Services Director (or their designee) following the review and approval of the pre-construction report.

SD-BIO-5 Direct Impact Avoidance and Noise Restrictions for Least Bell's Vireo

Prior to the preconstruction meeting, the City Manager (or appointed designee) shall verify that the following project requirements regarding the least Bell's vireo are shown on the construction plans:

No clearing, grubbing, grading, or other construction activities shall occur between March 15 and September 15, the breeding season of the least Bell's vireo, until the following requirements have been met to the satisfaction of the City Manager:

- A. A Qualified Biologist (possessing a valid Endangered Species Act Section 10(a)(1)(a) Recovery Permit) shall survey those wetland areas that would be subject to construction noise levels exceeding 60 decibels [dB(A)] hourly average for the presence of the least Bell's vireo. Surveys for this species shall be conducted pursuant to the protocol survey guidelines established by the USFWS within the breeding season prior to the commencement of construction. If the least Bell's vireo is present, then the following conditions must be met:
 - I. Between March 15 and September 15, no clearing, grubbing, or grading of occupied least Bell's vireo habitat shall be permitted. Areas restricted from such activities shall be staked or fenced under the supervision of a Qualified Biologist; and
 - II. Between March 15 and September 15, no construction activities shall occur within any portion of the site where construction activities would result in noise levels exceeding 60 dB(A) hourly average at the edge of occupied least Bell's vireo or habitat. An analysis showing that noise generated by construction activities would not exceed 60 dB(A) hourly average at the edge of occupied habitat must be completed a qualified acoustician (possessing current noise engineer license or registration with monitoring noise level experience with listed animal species) and approved by the City Manager at least two weeks prior to the commencement of construction activities. Prior to the commencement of any of construction activities during the breeding season, areas restricted from such activities shall be staked or fenced under the supervision of a qualified biologist; or
 - III. At least two weeks prior to the commencement of construction activities, under the direction of a qualified acoustician, noise attenuation measures (e.g., berms, walls) shall be implemented to ensure that noise levels resulting from construction activities will not exceed 60 dB(A) hourly average at the edge of habitat occupied by the least Bell's vireo. Concurrent with the commencement of construction activities and the construction of necessary noise attenuation facilities, noise monitoring* shall be conducted at the edge of the occupied habitat area to ensure that noise levels do not exceed 60 dB(A) hourly average. If the noise attenuation techniques implemented are determined to be inadequate by the qualified acoustician or biologist, then the associated construction activities shall cease until such time that adequate noise attenuation is achieved or until the end of the breeding season (September 16).

*Construction noise monitoring shall continue to be monitored at least twice weekly on varying days, or more frequently depending on the construction activity, to verify that noise levels at the edge of occupied habitat are maintained below 60 dB(A) hourly average or to the ambient noise level if it already exceeds 60 dB(A) hourly average. If not, other measures shall be implemented in consultation with the biologist and the City Manager, as necessary, to reduce noise levels to below 60 dB(A) hourly average or to the ambient noise level if it already exceeds 60 dB(A) hourly average or to the ambient noise level if it already exceeds 60 dB(A) hourly average or to the ambient noise level if it already exceeds 60 dB(A) hourly average or to the ambient noise level if it already exceeds 60 dB(A) hourly average. Such measures may include, but are not limited to, limitations on the placement of construction equipment and the simultaneous use of equipment.

- B. If least Bell's vireo are not detected during the protocol survey, the Qualified Biologist shall submit substantial evidence to the City Manager and applicable resource agencies which demonstrates whether or not mitigation measures such as noise walls are necessary between March 15 and September 15 as follows:
 - I. If this evidence indicates the potential is high for least Bell's vireo to be present based on historical records or site conditions, then condition A.III shall be adhered to as specified above.
 - II. If this evidence concludes that no impacts to this species are anticipated, no mitigation measures would be necessary.

6.2 Project Design Features

Due to the project site's location adjacent to I-805, future residents would be exposed to exterior and interior noise levels that exceed the City of Chula Vista and City of San Diego land use compatibility levels. With implementation of project design features PDF-CV-NOS-1, PDF-SD-NOS-1 and PDF-NOS-2, on-site exterior and interior traffic noise levels would be reduced to within the compatibility standards. The following project design features would be required as a condition of approval for each scenario as specified.

The following project design feature applies to the No Annexation Scenario and Annexation Scenario 2b:

PDF-CV-NOS-1 On-Site Noise Barriers. Exterior noise levels at the backyards (Receivers 11, 38, 52, 53, 61 through 65, and 67 through 70) as identified on Figure 8 shall be reduced to the City of Chula Vista's threshold of 65 CNEL for residential uses. Noise reduction for exterior traffic noise impacts can be accomplished through on-site noise barriers. Six-foot sound walls as identified on Figure 8 shall be constructed. The sound attenuation walls must be solid and free of cracks or holes. They can be constructed of masonry, wood, plastic, plexi-glass, fiberglass, steel, or a combination of those materials, as long as there are no cracks or gaps, through or below the wall. Any seams or cracks must be filled or caulked. If wood is used, it can be tongue and groove and must be at least one-inch total thickness or have a density of at least 3.5 pounds per square foot.

The following project design feature applies to Annexation Scenario 2a:

PDF-SD-NOS-1 On-Site Noise Barriers. Exterior noise levels at the backyards (Receivers 11, 38, 52, 53, 61 through 65, and 67 through 70) as identified on Figure 8 shall be reduced to the City of San Diego noise compatibility standards for residential and park uses (60 CNEL and 70 CNEL, respectively). Noise reduction for exterior traffic noise impacts can be accomplished through on-site noise barriers. Six-foot sound walls as identified on Figure 8 shall be constructed. The sound attenuation walls must be solid and free of cracks or holes. They can be constructed of masonry, wood, plastic, plexi-glass, fiberglass, steel, or a combination of those materials, as long as there are no cracks or gaps, through or below the wall. Any seams or cracks must be filled

or caulked. If wood is used, it can be tongue and groove and must be at least one-inch total thickness or have a density of at least 3.5 pounds per square foot.

The following project design feature applies to all scenarios:

PDF-NOS-2 Interior Noise. An exterior-to-interior noise analysis shall be conducted by the project applicant for the proposed dwelling units facing the adjoining major highway (e.g., I-805) prior to issuance of building permits. Installation of mechanical ventilation systems or air conditioning systems and sound-rated windows shall be required if the predicted interior background noise due to traffic noise intrusion through the building envelope assemblies exceeds the 45 CNEL interior standard. The acoustical analysis shall substantiate that the resulting interior background noise levels, with appropriate implementation of interior comfort systems and sound insulation, would be less than this noise standard.

In addition, for all proposed dwelling units in project areas where exterior noise levels (largely attributed to I-805 acoustical contribution) are expected to exceed 60 CNEL, mechanical ventilation and/or air conditioning systems shall be installed so as to allow closed windows and thus ensure attainment of the 45 CNEL interior background sound level due to exterior-to-interior noise intrusion.

7.0 References Cited

California, State of

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Carrier

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2023 Local Mobility Analysis Report. June 30.

Navcon Engineering, Inc.

2018 SoundPLAN Essential version 4.1.

RECON Environmental, Inc. (RECON)

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San Diego, City of

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- 2010 City of San Diego Municipal Code, Article 9.5: Noise Abatement and Control.
- 2015 City of San Diego General Plan Noise Element.

- 2018 San Diego Municipal Code Land Development Code, Biology Guidelines. Amended February 1, 2018.
- 2021 A Resolution of the Council of the City of San Diego Adopting a New Citywide Park Development Impact Fee. https://docs.sandiego.gov/council_reso_ordinance/rao2021/R-313688.pdf
- 2022 City of San Diego CEQA Significance Determination Thresholds. September.

San Diego Association of Governments (SANDAG)

2022 Series 14: Regional Growth Forecast. https://tfic.sandag.org/

San Diego County Regional Airport Authority (SDCRAA)

- 2010 Brown Field Municipal Airport Land Use Compatibility Plan. Amended December 20.
- U.S. Department of Transportation
 - 2006 FHWA Roadway Construction Noise Model: User's Guide. Final Report. FHWA-HEP-06-015. DOT-VNTSC-FHWA-06-02. Cambridge, Massachusetts: DOT, Research and Innovative Technology Administration. August 2006.

ATTACHMENTS

ATTACHMENT 1

Baseline Noise Measurement Field Data

Field Noise Measurement Data

Record: 1279				
Project Name	Nakano			
Observer(s)	Connor Burke			
Date	2020-06-04			

and the second

Meteorological Conditions				
Temp (F)	68			
Humidity % (R.H.)	77			
Wind	Light			
Wind Speed (MPH)	6			
Wind Direction	East			
Sky	Overcast			

Instrument and Calibrator Information				
Instrument Name List	(ENC) Rion NL-52			
Instrument Name	(ENC) Rion NL-52			
Instrument Name Lookup Key	(ENC) Rion NL-52			
Manufacturer	Rion			
Model	NL-52			
Serial Number	553896			
Calibrator Name	(ENC) LD CAL150			
Calibrator Name	(ENC) LD CAL150			
Calibrator Name Lookup Key	(ENC) LD CAL150			
Calibrator Manufacturer	Larson Davis			
Calibrator Model	LD CAL150			
Calibrator Serial #	5152			
Pre-Test (dBA SPL)	94			
Post-Test (dBA SPL)	94			
Windscreen	Yes			
Weighting?	A-WTD			
Slow/Fast?	Slow			
ANSI?	Yes			

Aonitoring			
Monitoring			
Record #	1		
Site ID	ST3		
Site Location Lat/Long	32.589889, -117.031977		
Begin (Time)	10:30:00		
End (Time)	10:40:00		
Leq	62.8		
Lmax	64.5		
Lmin	60		
Other Lx?	L90, L50, L10		
L90	61.7		
L50	62.8		
L10	63.9		
Other Lx (Specify Metric)	L		
Primary Noise Source	Traffic		
Other Noise Sources (Background)	Birds, Distant Aircraft, Distant Traffic		
Other Noise Sources Additional Description	805 traffic dominant		
Is the same instrument and calibrator being used	Yes		
as previously noted?			
Are the meteorological conditions the same as	Yes		
previously noted?			



Description / Photos

Site Photos

Photo



Comments / Description

Facing west

Monitoring	
Record #	2
Site ID	ST1
Site Location Lat/Long	32.587685, -117.031401
Begin (Time)	10:50:00
End (Time)	11:00:00
Leq	62
Lmax	75.1
Lmin	54.9
Other Lx?	L90, L50, L10
L90	56.6
L50	58.8
L10	65.10
Other Lx (Specify Metric)	L
Primary Noise Source	Traffic
Other Noise Sources (Background)	Birds, Distant Aircraft, Distant Traffic
Other Noise Sources Additional Description	805 traffic dominant
Is the same instrument and calibrator being used	Yes
as previously noted?	
Are the meteorological conditions the same as	Yes
previously noted?	

EMERMS FIELD DATA REPORT

Site Photos

Photo



Monitoring	
Record #	3
Site ID	ST4
Site Location Lat/Long	32.588248, -117.035646
Begin (Time)	11:20:00
End (Time)	11:30:00
Leq	65.6
Lmax	74.6
Lmin	61.2
Other Lx?	L90, L50, L10
L90	62.6
L50	64.8
L10	67.1
Other Lx (Specify Metric)	L
Primary Noise Source	Traffic
Other Noise Sources (Background)	
Other Noise Sources Additional Description	805 traffic dominant
Is the same instrument and calibrator being used	Yes
as previously noted?	
Are the meteorological conditions the same as	Yes
previously noted?	



Site Photos

Photo



Monitoring	
Record #	4
Site ID	ST2
Site Location Lat/Long	32.586611, -117.033279
Begin (Time)	11:45:00
End (Time)	11:55:00
Leq	62.1
Lmax	66.3
Lmin	55
Other Lx?	L90, L50, L10
L90	58.7
L50	61.8
L10	64.4
Other Lx (Specify Metric)	L
Primary Noise Source	Traffic
Other Noise Sources (Background)	Birds, Distant Traffic
Other Noise Sources Additional Description	805 traffic dominant
Is the same instrument and calibrator being used	Yes
as previously noted?	
Are the meteorological conditions the same as	Yes
previously noted?	



Site Photos

Photo



Comments / Description

Facing north

ATTACHMENT 2

Construction Noise Modeling Input and Output



To User: bordered cells are inputs, unbordered cells have formulae

Reference Lmax @ 50 ft. from FHWA RCNM Allowable Allowable Total Equipment Qty AUF % (from FHWA RCNM) Source to NSR Temporary Barrier Source Receiver Elevation (ft) Elevation (ft) Barrier Height (ft $\label{eq:client} \textbf{Client Equipment Description, Data Source and/or}$ Predicted 8-Additional Noise Distance-**Construction Activity** Equipment Operation Time Operation Time Distance (ft.) Insertion Loss (dB) Reduction Adjusted Lmax hour Leq (hours) (minutes) Site Preparation Dozer 1 40 700 0.0 53.8 480 50 Front End Loader 1 40 700 0.0 50.8 480 47 Total for Site Preparation Phase: 51.6 Grading Excavator 40 700 52.8 480 49 0.0 1 81 0.0 0.0 0.0 40 700 480 Grader 1 56.8 53 40 40 480 480 480 50 52 Dozer 1 700 53.8 82 5 Scraper Backhoe 700 55.8 1 40 700 0.0 46 1 49.8 78 Total for Grading Phase: 57.5 Crane Gradall 0.0 0.0 Building Construction 16 40 50 700 420 1 52.8 44 480 480 700 1 54.8 51 0.0 0.0 Generator 700 43.8 41 1 72 8 Front End Loader Welder / Torch 40 420 1 700 50.8 46 40 0.0 1 700 480 41 44.8 73 8 53.3 Total for Building Construction Phase: Paving Paver 50 700 0.0 48.8 480 46 1 0.0 480 480 40 Dump Truck Roller 700 44 1 47.8 1 20 700 51.8 45 8 Total for Paving Phase: 49.7 0.0 Architectural Coating Compressor (air) 1 40 700 49.8 360 45 44.6 Total for Architectural Coating Phase:

)	Source to Barr. ("A") Horiz. (ft)	Rcvr. to Barr. ("B") Horiz. (ft)	Source to Rcvr. ("C") Horiz. (ft)	"A" (ft)	"B" (ft)	"C" (ft)	Path Length Diff. "P" (ft)	Abarr (dB)	ILbarr (dB)
0	350	350	700	350.0	350.0	700.0	0.00	0.1	0.0
0	350	350	700	350.0	350.0	700.0	0.00	0.1	0.0
0	350	350	700	350.0	350.0	700.0	0.00	0.1	0.0
0	350	350	700	350.0	350.0	700.0	0.00	0.1	0.0
0	350	350	700	350.0	350.0	700.0	0.00	0.1	0.0
0	350	350	700	350.0	350.0	700.0	0.00	0.1	0.0
0	350	350	700	350.0	350.0	700.0	0.00	0.1	0.0
0	350	350	700	350.0	350.0	700.0	0.00	0.1	0.0
0	350	350	700	350.0	350.0	700.0	0.00	0.1	0.0
0	350	350	700	350.0	350.0	700.0	0.00	0.1	0.0
0	350	350	700	350.0	350.0	700.0	0.00	0.1	0.0
0	350	350	700	350.0	350.0	700.0	0.00	0.1	0.0
0	350	350	700	350.0	350.0	700.0	0.00	0.1	0.0
0	350	350	700	350.0	350.0	700.0	0.00	0.1	0.0
0	350	350	700	350.0	350.0	700.0	0.00	0.1	0.0
0	350	350	700	350.0	350.0	700.0	0.00	0.1	0.0



To User: bordered cells are inputs, unbordered cells have formulae

allowable hours over which Leq is to be averaged: 8 per FTA Guidance =

Construction Activity	Equipment	Total Equipment Qty	AUF % (from / FHWA RCNM)	Reference Lmax @ 50 ft. from FHWA RCNM	Client Equipment Description, Data Source and/or Notes	Source to NSR Distance (ft.)	Temporary Barrier Insertion Loss (dB)	Additional Noise Reduction	Distance- Adjusted Lmax	Allowable Operation Time (hours)	Allowable Operation Time (minutes)	Predicted 8- hour Leq	Sou Elevat	urce F tion (ft) Ele	Receiver evation (ft)	Barrier Height (ft)	Source to Barr. ("A") Horiz. (ft)	Rcvr. to Barr. ("B") Horiz. (ft)	Source to Rcvr. ("C") Horiz. (ft)	"A" (ft)	"B" (ft)	"C" (ft)	Path Length Diff. "P" (ft)	Abarr (dB)	ILbarr (dB)
Site Preparation	Dozer	1	40	82		700	0.	ס	53.8	8	480	5	0	5	13	0	350	350	700	350.0	350.2	700.	0.00	0.1	0.0
	Front End Loader	1	40	79		700	0.	ס 🗌 🗌 רבי די	50.8	8	480	4	7	5	13	0	350	350	700	350.0	350.2	700.	0.00	0.1	0.0
			_						Total for Site Pre	eparation Phase:	<u>.</u>	51.	6												
Grading	Excavator	1	40	81		700	0.	D	52.8	8	8 480	4	9	5	13	0	350	350	700	350.0	350.2	700.	0.00	0.1	0.0
	Grader	1	40	85		700	0.	D	56.8	8	480	5	3	5	13	0	350	350	700	350.0	350.2	700.	0.00	0.1	0.0
	Dozer	1	40	82		700	0.	D	53.8	8	480	5	0	5	13	0	350	350	700	350.0	350.2	700.	0.00	0.1	0.0
	Scraper	1	40	84		700	0.	0	55.8	8	480	5	2	5	13	0	350	350	700	350.0	350.2	700.0	0.00	0.1	0.0
	Backhoe	1	40	78		700	0.	D	49.8	8	480	4	6	5	13	0	350	350	700	350.0	350.2	700.	0.00	0.1	0.0
			_			_			Total for	Grading Phase:	<u>.</u>	57.	5												
Building Construction	Crane	1	16	81		700	0.	D	52.8	7	420	4	4	5	13	0	350	350	700	350.0	350.2	700.	0.00	0.1	0.0
	Gradall	1	40	83		700	0.	D	54.8	8	480	5	1	5	13	0	350	350	700	350.0	350.2	700.	0.00	0.1	0.0
	Generator	1	50	72		700	0.	D	43.8	8	480	4	1	5	13	0	350	350	700	350.0	350.2	700.	0.00	0.1	0.0
	Front End Loader	1	40	79		700	0.	D	50.8	7	420	4	6	5	13	0	350	350	700	350.0	350.2	700.	0.00	0.1	0.0
	Welder / Torch	1	40	73		700	0.	D	44.8	8	480	4	1	5	13	0	350	350	700	350.0	350.2	700.	0.00	0.1	0.0
								To	tal for Building Con	struction Phase:	:	53.	3												
Paving	Paver	1	50	77		700	0.	D	48.8	8	480	4	6	5	13	0	350	350	700	350.0	350.2	700.0	0.00	0.1	0.0
• • •	Dump Truck	1	40	76		700	0.	D	47.8	8	480	4	4	5	13	0	350	350	700	350.0	350.2	700.0	0.00	0.1	0.0
	Roller	1	20	80		700	0.	D	51.8	8	480	4	5	5	13	0	350	350	700	350.0	350.2	700.0	0.00	0.1	0.0
			_			-			Total fo	or Paving Phase:	⊿ :	49.	7		I										
Architectural Coating	Compressor (air)	1	40	78		700	0.	0	49.8	6	360	4	5	5	13	0	350	350	700	350.0	350.2	700.	0.00	0.1	0.0
	• · · ·	•				_		To	tal for Architectural	Coating Phase:	 :	44.	6												

noise level limit for construction phase at occupied building, per FTA Guidance = allowable hours over which Leq is to be averaged: 8 per FTA Guidance =

Construction Activity	Equipment	Total Equipment Qty	AUF % (from FHWA RCNM)	Reference Lmax @ 50 ft. from FHWA RCNM	Client Equipment Description, Data Source and/or Notes	Source to NSR Distance (ft.)	Temporary Barrier Insertion Loss (dB)	Additional Noise Reduction	Distance- Adjusted Lmax	Allowable Operation Time (hours)	Allowable Operation Time (minutes)	Predicted 8- hour Leq	Source Elevation	e Receiver (ft) Elevation (f	Barrier) Height (ft)	Source to Barr. ("A") Horiz. (ft)	Rcvr. to Barr. ("B") Horiz. (ft)	Source to Rcvr. ("C") Horiz. (ft)	"A" (ft)	"B" (ft)	"C" (ft) F	ath Length Diff. "P" (ft) A	barr (dB)	ILbarr (dB)
Site Preparation	Dozer	3	40	82		1230	0.0)	48.3	8	480	4	9	5	5 0	615	615	1230	615.0	615.0	1230.0	0.00	0.1	0.0
	Front End Loader	4	40	79		1230	0.0)	45.3	8	480	4	7	5	5 0	615	615	1230	615.0	615.0	1230.0	0.00	0.1	0.0
			-			_			Total for Site Prep	paration Phase:		51.	3											
Grading	Excavator	2	40	81		1230	0.0)	47.3	8	480	4	6	5	5 0	615	615	1230	615.0	615.0	1230.0	0.00	0.1	0.0
	Grader	1	40	85		1230	0.0)	51.3	8	480	4	7	5	5 0	615	615	1230	615.0	615.0	1230.0	0.00	0.1	0.0
	Dozer	1	40	82		1230	0.0)	48.3	8	480	4	4	5	5 0	615	615	1230	615.0	615.0	1230.0	0.00	0.1	0.0
	Scraper	2	40	84		1230	0.0)	50.3	8	480	4	9	5	5 0	615	615	1230	615.0	615.0	1230.0	0.00	0.1	0.0
	Backhoe	2	40	78		1230	0.0)	44.3	8	480	4	3	5	5 0	615	615	1230	615.0	615.0	1230.0	0.00	0.1	0.0
			-			_			Total for	Grading Phase:		53.	6											
Building Construction	Crane	1	16	81		1230	0.0)	47.3	8	480	3	9	5	5 0	615	615	1230	615.0	615.0	1230.0	0.00	0.1	0.0
	Gradall	3	40	83		1230	0.0)	49.3	8	480	5	0	5	5 0	615	615	1230	615.0	615.0	1230.0	0.00	0.1	0.0
	Generator	1	50	72		1230	0.0)	38.3	8	480	3	5	5	5 0	615	615	1230	615.0	615.0	1230.0	0.00	0.1	0.0
	Front End Loader	3	40	79		1230	0.0)	45.3	8	480	4	6	5	5 0	615	615	1230	615.0	615.0	1230.0	0.00	0.1	0.0
	Welder / Torch	1	40	73		1230	0.0)	39.3	8	480	3	5	5	5 0	615	615	1230	615.0	615.0	1230.0	0.00	0.1	0.0
								Tot	al for Building Cons	truction Phase:		52.	0											
Paving	Paver	2	50	77		1230	0.0		43.3	8	480	4	3	5	5 0	615	615	1230	615.0	615.0	1230.0	0.00	0.1	0.0
	Dump Truck	2	40	76		1230	0.0		42.3	8	480	4	1	5	5 0	615	615	1230	615.0	615.0	1230.0	0.00	0.1	0.0
	Roller	2	20	80		1230	0.0)	46.3	8	480	4	2	5	5 0	615	615	1230	615.0	615.0	1230.0	0.00	0.1	0.0
			_			_			Total for	Paving Phase:		47.	2					-						
Architectural Coating	Compressor (air)	1	40	78		1230	0.0) Tot	44.3	8 Coating Phase:	480	4 40 .	0 3	5	5 0	615	615] 1230	615.0	615.0	1230.0	0.00	0.1	0.0



Construction Activity	Equipment	Total Equipment Qt	AUF % (from y FHWA RCNM)	Reference Lmax @ 50 ft. from FHWA RCNM	Client Equipment Description, Data Source and/or Notes	Source to NSR Distance (ft.)	Temporary Barrier Insertion Loss (dB)	Additional Noise Reduction	Distance- Adjusted Lmax	Allowable Operation Time (hours)	Allowable Operation Time (minutes)	Predicted 8- hour Leq	Source Elevation (Receiver (ft) Elevation (ft	Barrier t) Height (ft)	Source to Barr. ("A") Horiz. (ft)	Rcvr. to Barr. ("B") Horiz. (ft)	Source to Rcvr. ("C") Horiz. (ft)	"A" (ft)	"B" (ft)	"C" (ft) Pi	ath Length A liff. "P" (ft)	barr (dB) I	lLbarr (dB)
Site Preparation	Dozer	3	40) 82		1230	0.0		48.3	8	480	49		5 1	3	0 61	5 615	1230	615.0	615.1	1230.0	0.00	0.1	0.0
	Front End Loader	4	40) 79		1230	0.0		45.3	8	480	47		5 1	3	0 61	5 615	1230	615.0	615.1	1230.0	0.00	0.1	0.0
			_			_			Total for Site Pre	paration Phase:		51.3												
Grading	Excavator	2	40) 81		1230	0.0		47.3	8	480	46		5 1	3	0 61	5 615	1230	615.0	615.1	1230.0	0.00	0.1	0.0
	Grader	1	40) 85		1230	0.0		51.3	8	480	47		5 1	3	0 61	5 615	1230	615.0	615.1	1230.0	0.00	0.1	0.0
	Dozer	1	40) 82		1230	0.0		48.3	8	480	44		5 1	3	0 61	5 615	1230	615.0	615.1	1230.0	0.00	0.1	0.0
	Scraper	2	40) 84		1230	0.0		50.3	8	480	49		5 1	3	0 61	5 615	1230	615.0	615.1	1230.0	0.00	0.1	0.0
	Backhoe	2	40) 78		1230	0.0		44.3	8	480	43		5 1	3	0 61	5 615	1230	615.0	615.1	1230.0	0.00	0.1	0.0
			_	,		_			Total for	Grading Phase:		53.6						,						
Building Construction	Crane	1	16	6 81		1230	0.0		47.3	8	480	39		5 1	3	0 61	5 615	1230	615.0	615.1	1230.0	0.00	0.1	0.0
	Gradall	3	40) 83		1230	0.0		49.3	8	480	50		5 1	3	0 61	5 615	1230	615.0	615.1	1230.0	0.00	0.1	0.0
	Generator	1	50) 72		1230	0.0		38.3	8	480	35		5 1	3	0 61	5 615	1230	615.0	615.1	1230.0	0.00	0.1	0.0
	Front End Loader	3	40) 79		1230	0.0		45.3	8	480	46		5 1	3	0 61	5 615	1230	615.0	615.1	1230.0	0.00	0.1	0.0
	Welder / Torch	1	40) 73		1230	0.0		39.3	8	480	35		5 1	3	0 61	5 615	1230	615.0	615.1	1230.0	0.00	0.1	0.0
			_			_		Tot	tal for Building Con	struction Phase:		52.0			_									
Paving	Paver	2	50) 77		1230	0.0		43.3	8	480	43		5 1	3	0 61	5 615	1230	615.0	615.1	1230.0	0.00	0.1	0.0
	Dump Truck	2	40) 76		1230	0.0		42.3		480	41		5 1	3	0 61	5 615	1230	615.0	615.1	1230.0	0.00	0.1	0.0
	Roller	2	20) 80		1230	0.0		46.3	8	480	42		5 1	3	0 61	5 615	1230	615.0	615.1	1230.0	0.00	0.1	0.0
			_			_			Total fo	or Paving Phase:		47.2												
Architectural Coating	Compressor (air)	1	40) 78		1230	0.0		44.3	8	480	40		5 1	3	0 61	5 615	1230	615.0	615.1	1230.0	0.00	0.1	0.0
								Tot	tal for Architectura	Coating Phase:		40.3												



noise level limit for construction phase at occupied building, per City of San Diego (59.5.0404(b)) = allowable hours over which Leq is to be averaged: 12 per City of San Diego (59.5.0404(b)) =

Construction Activity	Equipment	Total Equipment Qty	AUF % (from FHWA RCNM)	Reference Lmax @ 50 ft. from FHWA RCNM	Client Equipment Description, Data Source and/or Notes	Source to NSR Distance (ft.)	Temporary Barrier Insertion Loss (dB)	Additional Noise Reduction	Distance- Adjusted Lmax Op	Allowable peration Time ((hours)	Allowable Dperation Time (minutes)	Predicted 12- hour Leq	Source Elevation (ft)	Receiver Elevation (ft)	Barrier Height (ft)	Source to Barr. ("A") Horiz. (ft)	Rcvr. to Barr. ("B") Horiz. (ft)	Source to Rcvr. ("C") Horiz. (ft)	"A" (ft)	"B" (ft)	"C" (ft) Pa Di	th Length ff. "P" (ft) A	ıbarr (dB) II	Lbarr (dB)
Site Preparation	Dozer	1	40	82		180	10.2		56.9	8	480	51	110	155	150	128	52	180	134.1	52.2	185.5	0.80	12.1	10.2
	Front End Loader	1	40	79		180	10.2		53.9	8	480	48	110	155	150	128	52	180	134.1	52.2	185.5	0.80	12.1	10.2
			-			_			Total for Site Prepar	ration Phase:		52.9												
Grading	Excavator	1	40	81		60	12.0		67.3	8	480	62	145	155	150	8	52	60	9.4	52.2	60.8	0.85	12.3	12.0
	Grader	1	40	85		60	12.0		71.3	8	480	66	145	155	150	8	52	60	9.4	52.2	60.8	0.85	12.3	12.0
	Dozer	1	40	82		60	12.0		68.3	8	480	63	145	155	150	8	52	60	9.4	52.2	60.8	0.85	12.3	12.0
	Scraper	1	40	84		60	12.0		70.3	8	480	65	145	155	150	8	52	60	9.4	52.2	60.8	0.85	12.3	12.0
	Backhoe	1	40	78		60	12.0		64.3	8	480	59	145	155	150	8	52	60	9.4	52.2	60.8	0.85	12.3	12.0
			_						Total for Gra	ading Phase:		70.2												
Building Construction	Crane	1	16	81		210	7.6		57.0	7	420	47	110	155	150	158	52	210	163.0	52.2	214.8	0.46	9.6	7.6
	Gradall	1	40	83		210	7.6		59.0	8	480	53	110	155	150	158	52	210	163.0	52.2	214.8	0.46	9.6	7.6
	Generator	1	50	72		210	7.6		48.0	8	480	43	110	155	150	158	52	210	163.0	52.2	214.8	0.46	9.6	7.6
	Front End Loader	1	40	79		210	7.6		55.0	7	420	49	110	155	150	158	52	210	163.0	52.2	214.8	0.46	9.6	7.6
	Welder / Torch	1	40	73		210	7.6		49.0	8	480	43	110	155	150	158	52	210	163.0	52.2	214.8	0.46	9.6	7.6
								Tot	al for Building Constru	uction Phase:		55.7												
Paving	Paver	1	50	77		60	12.0		63.3	8	480	59	145	155	150	8	52	60	9.4	52.2	60.8	0.85	12.3	12.0
	Dump Truck	1	40	76		60	12.0		62.3	8	480	57	145	155	150	8	52	60	9.4	52.2	60.8	0.85	12.3	12.0
	Roller	1	20	80		60	12.0		66.3	8	480	58	145	155	150	8	52	60	9.4	52.2	60.8	0.85	12.3	12.0
			•			-			Total for Pa	aving Phase:		62.4												
Architectural Coating	Compressor (air)	1	40	78		210	7.6		54.0	6	360	47	110	155	150	158	52	210	163.0	52.2	214.8	0.46	9.6	7.6
		•	-			_		Tot	al for Architectural Co	ating Phase:		47.0						•						

To User: bordered cells are inputs, unbordered cells have formulae



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noise level limit for construction phase at occupied building, per City of San Diego (59.5.0404(b)) allowable hours over which Leq is to be averaged: 12 per City of San Diego (59.5.0404(b)) =

Reference Lmax @ 50 ft. from FHWA RCNM AUF % (from FHWA RCNM) Allowable Allowable Total Source to NSR Source Receiver Barrier Elevation (ft) Elevation (ft) Height (ft $\label{eq:client} \textbf{Client Equipment Description, Data Source and/or}$ Predicted 12-Temporary Barrier Additional Noise Distance-**Construction Activity** Equipment Operation Time Operation Time Equipment Qty Distance (ft.) Insertion Loss (dB) Reduction Adjusted Lmax hour Leq (hours) (minutes) Site Preparation Dozer 40 180 0.0 67.1 480 61 110 164 Front End Loader 1 40 180 0.0 480 58 110 164 64.1 Total for Site Preparation Phase: 63.2 Grading Excavator 40 60 480 65 145 164 8.3 71.1 1 81 40 480 145 164 Grader 1 60 8.3 75.1 69 40 40 480 480 66 68 Dozer 1 8.3 145 164 60 72.1 82 Scraper Backhoe 8.3 145 164 1 60 74.1 40 480 62 145 164 60 8.3 68.1 1 78 Total for Grading Phase: 74.0 Building Construction 16 40 50 210 0.0 0.0 420 110 Crane 1 64.6 54 164 Gradall 210 480 61 110 164 1 66.6 210 0.0 480 51 110 164 Generator 1 55.6 72 2 Front End Loader Welder / Torch 110 110 40 0.0 420 164 1 210 62.6 56 40 0.0 164 210 480 51 1 56.6 73 8 Total for Building Construction Phase: 63.3 Paving Paver 50 60 67.1 480 62 60 145 164 8.3 1 40 480 Dump Truck Roller 8.3 164 145 1 60 66.1 1 20 60 8.3 70.1 480 61 145 164 8 Total for Paving Phase: 66.2 0.0 Architectural Coating Compressor (air) 1 40 210 61.6 360 55 110 164 54.6 Total for Architectural Coating Phase:

)	Source to Barr. ("A") Horiz. (ft)	Rcvr. to Barr. ("B") Horiz. (ft)	Source to Rcvr. ("C") Horiz. (ft)	"A" (ft)	"B" (ft)	"C" (ft)	Path Length Diff. "P" (ft)	Abarr (dB)	ILbarr (dB)
50	128	52	180	134.1	53.9	187.9	0.03	1.6	0.0
50	128	52	180	134.1	53.9	187.9	0.03	1.6	0.0
50	8	52	60	9.4	53.9	62.9	0.35	8.5	8.3
50	8	52	60	9.4	53.9	62.9	0.35	8.5	8.3
50	8	52	60	9.4	53.9	62.9	0.35	8.5	8.3
50	8	52	60	9.4	53.9	62.9	0.35	8.5	8.3
50	8	52	60	9.4	53.9	62.9	0.35	8.5	8.3
50	158	52	210	163.0	53.9	216.8	0.00	0.1	0.0
50	158	52	210	163.0	53.9	216.8	0.00	0.1	0.0
50	158	52	210	163.0	53.9	216.8	0.00	0.1	0.0
50	158	52	210	163.0	53.9	216.8	0.00	0.1	0.0
50	158	52	210	163.0	53.9	216.8	0.00	0.1	0.0
50	8	52	60	9.4	53.9	62.9	0.35	8.5	8.3
50	8	52	60	9.4	53.9	62.9	0.35	8.5	8.3
50	8	52	60	9.4	53.9	62.9	0.35	8.5	8.3
50	158	52	210	163.0	53.9	216.8	0.00	0.1	0.0



noise level limit for construction phase at occupied building, per City of San Diego (59.5.0404(b)) = allowable hours over which Leq is to be averaged: 12 per City of San Diego (59.5.0404(b)) =

Construction Activity	Equipment	Total Equipment Qty	AUF % (from FHWA RCNM)	Reference Lmax @ 50 ft. from FHWA RCNM	Client Equipment Description, Data Source and/or Notes	Source to NSR Distance (ft.)	Temporary Barrier Insertion Loss (dB)	Additional Noise Reduction	Distance- Adjusted Lmax	Allowable Operation Time (hours)	Allowable Operation Time (minutes)	Predicted 12- hour Leq	Source Elevation (ft)	Receiver Elevation (ft)	Barrier Height (ft)	Source to Rc Barr. ("A") (" Horiz. (ft)	cvr. to Barr. "B") Horiz. (ft)	Source to Rcvr. ("C") Horiz. (ft)	"A" (ft)	"B" (ft)	"C" (ft) P	ath Length Diff. "P" (ft)	Abarr (dB)	lLbarr (dB)
Site Preparation	Dozer	3	40	82		743	3 0.	0	53.3	8	480	52	110	155	150	691	52	743	692.2	52.2	744.4	0.00	0.1	0.0
	Front End Loader	4	40) 79		743	3 0.	כ	50.3	8	480	51	110	155	150	691	52	743	692.2	52.2	744.4	0.00	0.1	0.0
			_			_			Total for Site Pre	paration Phase:		54.5												
Grading	Excavator	2	40) 81		743	8 0.	0	52.3	8	480	50	145	155	150	691	52	743	691.0	52.2	743.1	0.00	0.1	0.0
	Grader	1	40) 85		743	B 0.	D	56.3	8	480	51	145	155	150	691	52	743	691.0	52.2	743.1	0.00	0.1	0.0
	Dozer	1	40) 82		743	3 0.	D	53.3	8	480	48	145	155	150	691	52	743	691.0	52.2	743.1	0.00	0.1	0.0
	Scraper	2	40) 84		743	8 0.	D	55.3	8	480	53	145	155	150	691	52	743	691.0	52.2	743.1	0.00	0.1	0.0
	Backhoe	2	40) 78		743	8 0.	D	49.3	8	480	47	145	155	150	691	52	743	691.0	52.2	743.1	0.00	0.1	0.0
									Total for	Grading Phase:		56.8												
Building Construction	Crane	1	16	6 81		743	8 0.	D	52.3	8	480	43	110	155	150	691	52	743	692.2	52.2	744.4	0.00	0.1	0.0
	Gradall	3	40) 83		743	3 0.	D	54.3	8	480	53	110	155	150	691	52	743	692.2	52.2	744.4	0.00	0.1	0.0
	Generator	1	50) 72		743	3 0.1	D	43.3	8	480	38	110	155	150	691	52	743	692.2	52.2	744.4	0.00	0.1	0.0
	Front End Loader	3	40) 79		743	3 0.	D	50.3	8	480	49	110	155	150	691	52	743	692.2	52.2	744.4	0.00	0.1	0.0
	Welder / Torch	1	40) 73		743	8 0.0	ס[44.3	8	480	39	110	155	150	691	52	743	692.2	52.2	744.4	0.00	0.1	0.0
			-			_		To	tal for Building Con	struction Phase:		55.2												
Paving	Paver	2	50) 77		743	3 0.	D	48.3	8	480	47	145	155	150	691	52	743	691.0	52.2	743.1	0.00	0.1	0.0
· · · ·	Dump Truck	2	40) 76		743	3 0.1	D	47.3	8	480	45	145	155	150	691	52	743	691.0	52.2	743.1	0.00	0.1	0.0
	Roller	2	20	80		743	3 0.1	D	51.3	8	480	46	145	155	150	691	52	743	691.0	52.2	743.1	0.00	0.1	0.0
		•	-			_			Total fo	r Paving Phase:		50.4	· · · · ·	•	•									
Architectural Coating	Compressor (air)	1	40	78		743	3 0.1	0	49.3	8	480	44	110	155	150	691	52	743	692.2	52.2	744.4	0.00	0.1	0.0
		·	-			-		To	tal for Architectural	Coating Phase:		43.5	·											



noise level limit for construction phase at occupied building, per City of San Diego (59.5.0404(b)) = allowable hours over which Leq is to be averaged: 12 per City of San Diego (59.5.0404(b)) =

Construction Activity	Equipment	Total Equipment Qty	AUF % (from FHWA RCNM)	ference Lmax	Client Equipment Description, Data Source and/or Notes	Source to NSR Distance (ft.)	Temporary Barrier Insertion Loss (dB)	Additional Noise Reduction	Distance- Adjusted Lmax	Allowable Operation Time (hours)	Allowable Operation Time (minutes)	Predicted 12- hour Leq	Source Elevation (f	Receiver t) Elevation (f	Barrier) Height (ft)	Source to Barr. ("A") Horiz. (ft)	Rcvr. to Barr ("B") Horiz. (ft)	. Source to Rcvr. ("C") Horiz. (ft)	"A" (ft)	"B" (ft)	"C" (ft) F	ath Length Diff. "P" (ft)	Abarr (dB)	Lbarr (dB)
Site Preparation	Dozer	3	40	82		743	0.	0	53.3	8	480	52	11	0 16	4 1	50 69	91 51	2 743	692.2	53.9	745.0	0.00	0.1	0.0
	Front End Loader	4	40	79		743	0.	0	50.3	8	480	51	11	0 16	4 1	50 69	91 55	2 743	692.2	53.9	745.0	0.00	0.1	0.0
			_	-		_			Total for Site Prep	paration Phase:	-	54.5			_			_						
Grading	Excavator	2	40	81		743	0.	0	52.3	8	480	50	14	5 16	4 1	50 69	91 53	2 743	691.0	53.9	743.2	0.00	0.1	0.0
	Grader	1	40	85		743	0.	0	56.3	8	480	51	14	5 16	4 1	50 69	91 52	2 743	691.0	53.9	743.2	0.00	0.1	0.0
	Dozer	1	40	82		743	0.	0	53.3	8	480	48	14	5 16	4 1	50 69	91 52	2 743	691.0	53.9	743.2	0.00	0.1	0.0
	Scraper	2	40	84		743	0.	0	55.3	8	480	53	14	5 16	4 1	50 69	91 52	2 743	691.0	53.9	743.2	0.00	0.1	0.0
	Backhoe	2	40	78		743	0.	0	49.3	8	480	47	14	5 16	4 1	50 69	91 55	2 743	691.0	53.9	743.2	0.00	0.1	0.0
			-	-		_			Total for C	Grading Phase:	-	56.8						-						
Building Construction	Crane	1	16	81		743	0.	0	52.3	8	480	43	11	0 16	4 1:	50 69	91 5	2 743	692.2	53.9	745.0	0.00	0.1	0.0
	Gradall	3	40	83		743	0.	0	54.3	8	480	53	11	0 16	4 1:	50 69	91 5	2 743	692.2	53.9	745.0	0.00	0.1	0.0
	Generator	1	50	72		743	0.	0	43.3	8	480	38	11	0 16	4 1:	50 69	91 5	2 743	692.2	53.9	745.0	0.00	0.1	0.0
	Front End Loader	3	40	79		743	0.	0	50.3	8	480	49	11	0 16	4 1:	50 69	91 5	2 743	692.2	53.9	745.0	0.00	0.1	0.0
	Welder / Torch	1	40	73		743	0.	0	44.3	8	480	39	11	0 16	4 1	50 69	91 5	2 743	692.2	53.9	745.0	0.00	0.1	0.0
	-	ł	-	•		-		To	tal for Building Const	truction Phase:	•	55.2						-						
Paving	Paver	2	50	77		743	0.	0	48.3	8	480	47	14	5 16	4 1:	50 69	5	2 743	691.0	53.9	743.2	0.00	0.1	0.0
	Dump Truck	2	40	76		743	0.0	0	47.3	8	480	45	14	5 16	4 1:	50 69	91 5	2 743	691.0	53.9	743.2	0.00	0.1	0.0
	Roller	2	20	80		743	0.	0	51.3	8	480	46	14	5 16	4 1:	50 69	01 5	2 743	691.0	53.9	743.2	0.00	0.1	0.0
	L		-	L		-			Total for	Paving Phase:	1	50.4												
Architectural Coating	Compressor (air)	1	40	78		743	0.	0	49.3	8	480	44	11	0 16	4 1:	50 69	5	2 743	692.2	53.9	745.0	0.00	0.1	0.0
-		1	-	L		-		To	tal for Architectural (Coating Phase:	4	43.5	I					-						

Equipment Description	Impact Device?	Acoustical Use Factor (%)	Lesser of or available Lmax	Spec. 721 Lmax	Measured L _{max} @50ft (dBA, slow)
All Other Equipment > 5 HP	No	50	85	85	N/A
Auger Drill Rig	No	20	84	85	84
Backhoe	No	40	78	80	78
Bar Bender	No	20	80	80	N/A
Blasting	Yes	N/A	94	94	N/A
Boring Jack Power Unit	No	50	80	80	83
Chain Saw	No	20	84	85	84
Clam Shovel (dropping)	Yes	20	87	93	87
Compactor (ground)	No	20	80	80	83
Compressor (air)	No	40	78	80	78
Concrete Batch Plant	No	15	83	83	N/A
Concrete Mixer Truck	No	40	79	85	79
Concrete Pump Truck	No	20	81	82	81
Concrete Saw	No	20	90	90	90
Crane	No	16	81	85	81
Dozer	No	40	82	85	82
Drill Rig Truck	No	20	79	84	79
Drum Mixer	No	50	80	80	80
Dump Truck	No	40	76	84	76
Excavator	No	40	81	85	81
Flat Bed Truck	No	40	74	84	74
Front End Loader	No	40	79	80	79
Generator	No	50	72	72	81
Generator (<25KVA, VMS signs)	No	50	70	70	73
Gradall	No	40	83	85	83
Grader	No	40	85	85	N/A
Grapple (on backhoe)	No	40	85	85	87
Horizontal Boring Hydr. Jack	No	25	80	80	82
Hydra Break Ram	Yes	10	90	90	N/A
Impact Pile Driver	Yes	20	95	95	101
Jackhammer	Yes	20	85	85	89
Man Lift	No	20	75	85	75
Mounted Impact Hammer (hoe ram)	Yes	20	90	90	90
Pavement Scarafier	No	20	85	85	90
Paver	No	50	77	85	77
Pickup Truck	No	40	55	55	75
Pneumatic Tools	No	50	85	85	85
Pumps	No	50	77	77	81
Refrigerator Unit	No	100	73	82	73
Rivit Buster/chipping gun	Yes	20	79	85	79
Rock Drill	No	20	81	85	81
Roller	No	20	80	85	80
Sand Blasting (Single Nozzle)	No	20	85	85	96
Scraper	No	40	84	85	84
Shears (on backhoe)	No	40	85	85	96
Slurry Plant	No	100	78	78	78
Slurry Trenching Machine	No	50	80	82	80
Soil Mix Drill Rig	No	50	80	80	N/A
Tractor	No	40	84	84	N/A
Vacuum Excavator (Vac-truck)	No	40	85	85	85
Vacuum Street Sweeper	No	10	80	80	82
Ventilation Fan	No	100	79	85	79
Vibrating Hopper	No	50	85	85	87
Vibratory Concrete Mixer	No	20	80	80	80
Vibratory Pile Driver	No	20	95	95	101
Warning Horn	No	5	83	85	83
Welder / Torch	No	40	73	73	74

ATTACHMENT 3

SoundPLAN Data – Existing Vehicle Traffic Noise and Construction Noise at Sensitive Habitat

3396.1 Nakano SoundPLAN Data - Existing Vehicle Traffic and Construction at Sensitive Habitat

Station		Traffic values	Vohiclo namo	dav	ovoning	night	Spood	Control	Constr.	Affect.	Pood surface	Gradient Min / Max
km	ADT Vob/24b	venicies type	venicle name	Udy Voh/h	Vob/b	Vob/b	speeu km/b	uevice	speeu km/b	0/	Road sufface	1VIII1 / 1VIdX 0/
1_805 N	orthbound	Traffic direction	· In entry direc	tion	VEH/H	Ven/m	KIII/II		KIII/II	70		70
0+000	75003	Total	-	/1813	2500	1083		none			Average (of DGAC and PCC)	-2.08
0+000	75003	Automobilos	_	4015	2300	1005	105	none		_	Average (of DGAC and PCC)	-2.00
0+000	75003	Medium trucks		178	2323	40	89	none		_	Average (of DGAC and PCC)	-2.08
0+000	75003	Hoppy trucks	_	170	83	36	80	nono	_	_	Average (of DGAC and PCC)	-2.08
0+000	75003	Buses		-		50	105	none		_	Average (of DGAC and PCC)	-2.08
0+000	75003	Motorcycles	_	_			105	none	-	_	Average (of DGAC and PCC)	-2.08
0+000	75003	Auxiliary vehicle	_	_			-	none	-	_	Average (of DGAC and PCC)	-2.08
0+912	-	-						none			weruge (of beste und rec)	2.00
1-805 Sc	outhbound	Traffic direction	· In entry direc	tion								
0+000	75003	Total	-	4813	2500	1083	-	none	-	-	Average (of DGAC and PCC)	-0.484848485
0+000	75003	Automobiles	-	4476	2325	1007	105	none	-	-	Average (of DGAC and PCC)	-0.484848485
0+000	75003	Medium trucks	-	178	93	40	89	none	-	-	Average (of DGAC and PCC)	-0.484848485
0+000	75003	Heavy trucks	-	159	83	36	89	none	-	-	Average (of DGAC and PCC)	-0.484848485
0+000	75003	Buses	-	-			105	none	-	-	Average (of DGAC and PCC)	-0.484848485
0+000	75003	Motorcycles	-	-			105	none	-	-	Average (of DGAC and PCC)	-0.484848485
0+000	75003	Auxiliary vehicle	-	-			-	none	-	-	Average (of DGAC and PCC)	-0.484848485
0+906	-	-	-	-							-	
Denner	y Road Ti	affic direction: I	n entry directior									
0+000	13866	Total	-	890	462	200	-	none	-	-	Average (of DGAC and PCC)	102
0+000	13866	Automobiles	-	828	430	196	56	none	-	-	Average (of DGAC and PCC)	102
0+000	13866	Medium trucks	-	33	17	2	56	none	-	-	Average (of DGAC and PCC)	102
0+000	13866	Heavy trucks	-	29	15	2	56	none	-	-	Average (of DGAC and PCC)	102
0+000	13866	Buses	-	-			56	none	-	-	Average (of DGAC and PCC)	102
0+000	13866	Motorcycles	-	-			56	none	-	-	Average (of DGAC and PCC)	102
0+000	13866	Auxiliary vehicle	-	-			-	none	-	-	Average (of DGAC and PCC)	102
0+442	8334	Total	-	535	278	120	-	none	-	-	Average (of DGAC and PCC)	-1
0+442	8334	Automobiles	-	498	259	117	56	none	-	-	Average (of DGAC and PCC)	-1
0+442	8334	Medium trucks	-	20	10	1	56	none	-	-	Average (of DGAC and PCC)	-1
0+442	8334	Heavy trucks	-	18	9	1	56	none	-	-	Average (of DGAC and PCC)	-1
0+442	8334	Buses	-	-			56	none	-	-	Average (of DGAC and PCC)	-1
0+442	8334	Motorcycles	-	-			56	none	-	-	Average (of DGAC and PCC)	-1
0+442	8334	Auxiliary vehicle	-	-			-	none	-	-	Average (of DGAC and PCC)	-1
0+764	-	-	-	-								

			339	96.1 Nakano	C		
	SoundPLAN [Data - Exis	sting Vehicle	Traffic and	Constructio	on at Sensiti	ve Habitat
			Noise Level			Corrections	
Source name	Reference	Day	Evening	Night	Cwall	CI	CT
		dB(A)	dB(A)	dB(A)	dB(A)	dB(A)	dB(A)
Construction	Lw/unit	117.3	-	-	-	-	-

3396.1 Nakano SoundPLAN Data - Existing Vehicle Traffic and Construction at Sensitive Habitat

	Coord	dinates		E	Existing Traffic	c Noise Lev	vel	Construction Noise Level
No.	Х	Y	Height	Day	Evening	Night	CNEL	
	(me	eters)	(meters)		dB((A)		dB(A)
1	496664.13	3605899.48	26.71	70.5	67.6	64	72.4	57.4
2	496945.74	3605949.98	32.76	60.2	57.4	53.7	62.1	57.5
3	496554.05	3605847.58	45.47	76.9	74.1	70.4	78.8	56.7

3396.1 Nakano SoundPLAN Data - Existing Vehicle Traffic and Construction at Sensitive Habitat Noise Level

							INOIS	e Levei	
Sourc	e name					Day	Evening	Night	CNEL
							d	B(A)	
1	1.FI	70.7	67.6	64.0	72.4				
Const	ruction					57.4	-	-	54.4
Denn	ery Road					29.5	26.6	21.1	30.4
I-805	Northbo	und				68.7	65.9	62.3	70.6
I-805	Southbo	und				65.7	62.8	59.2	67.6
2	1.Fl	62.1	57.4	53.7	62.8				
Const	ruction					57.5	-	-	54.5
Denn	ery Road					38.9	36.0	30.8	40.0
I-805	Northbo	und				57.5	54.7	51.0	59.4
I-805	Southbo	und				56.8	53.9	50.3	58.7
3	1.Fl	77.0	74.1	70.4	78.8				
Const	ruction					56.7	-	-	53.7
Denn	ery Road					38.4	35.6	30.2	39.5
I-805	Northbo	und				71.5	68.6	65.0	73.4
I-805	Southbo	und				75.5	72.6	69.0	77.4

ATTACHMENT 4

FHWA RD-77-108 Off-Site Traffic Noise Calculations
FHWA RD-77-108 Traffic Noise Prediction Model

Project Name : Nakano Project Number : 3396.1 Modeled Condition : 2020

Surface Refelction: CNEL Assessment Metric: Hard Peak ratio to ADT: 10.0 Traffic Desc. (Peak or ADT) : ADT

Data Input Sheet

				Speed	Distance						
Segmen	t Roadway	Segment	Traffic Vol.	(Mph)	to CL	% Autos	%MT	% HT	Day %	Eve %	Night % K-Factor
WITHOU	JT PROJECT										
1	Dennery Road	Palm Avenue to Regatta Lane	13,869	35	50	93.00	3.70	3.30	77.00	10.00	13.00
2		Regatta Lane to Landing Driveway	8,333	35	50	93.00	3.70	3.30	77.00	10.00	13.00
3		Landing Driveway to Red Coral	8,224	35	50	93.00	3.70	3.30	77.00	10.00	13.00
4	Palm Avenue	I-805 SB Ramps to NB Ramps	36,383	45	50	93.00	3.70	3.30	77.00	10.00	13.00
5		I-805 NB Ramps to Dennery Road	49,173	45	50	93.00	3.70	3.30	77.00	10.00	13.00
WITH PI	ROJECT										
1	Dennery Road	Palm Avenue to Regatta Lane	15,733	35	50	93.00	3.70	3.30	77.00	10.00	13.00
2		Regatta Lane to Landing Driveway	10,235	35	50	93.00	3.70	3.30	77.00	10.00	13.00
3		Landing Driveway to Red Coral	10,126	35	50	93.00	3.70	3.30	77.00	10.00	13.00
4	Palm Avenue	I-805 SB Ramps to NB Ramps	37,315	45	50	93.00	3.70	3.30	77.00	10.00	13.00
5		I-805 NB Ramps to Dennery Road	50,733	45	50	93.00	3.70	3.30	77.00	10.00	13.00

FHWA RD-77-108 Traffic Noise Prediction Model

Predicted Noise Levels

Project Name : Nakano Project Number : 3396.1 Modeled Condition : 2020 Assessment Metric: Hard

			N	oise Levels	, dBA Hai	ď		Distance to Traffic Noise Level Contours, Fe				
Segmer	nt Roadway	Segment	Auto	MT	ΗT	Tota	75 dB	70 dB	65 dB	60 dB	55 dB	50 dB
WITHO	JT PROJECT											
1	Dennery Road	Palm Avenue to Regatta Lane	65.7	61.4	66.1	69.6	14	46	144	456	1,442	4,560
2		Regatta Lane to Landing Driveway	63.5	59.2	63.9	67.4	9	27	87	275	869	2,748
3		Landing Driveway to Red Coral	63.4	59.1	63.8	67.3	8	27	85	269	849	2,685
4	Palm Avenue	I-805 SB Ramps to NB Ramps	73.0	67.3	71.3	75.9	62	195	615	1,945	6,151	19,452
5		I-805 NB Ramps to Dennery Road	74.3	68.6	72.6	77.2	83	262	830	2,624	8,298	26,240
WITH P	ROJECT											
1	Dennery Road	Palm Avenue to Regatta Lane	66.2	61.9	66.6	70.2	17	52	166	524	1,656	5,236
2		Regatta Lane to Landing Driveway	64.4	60.1	64.8	68.3	11	34	107	338	1,069	3,380
3		Landing Driveway to Red Coral	64.3	60.0	64.7	68.2	10	33	104	330	1,045	3,303
4	Palm Avenue	I-805 SB Ramps to NB Ramps	73.1	67.4	71.4	76.0	63	199	629	1,991	6,295	19,905
5		I-805 NB Ramps to Dennery Road	74.5	68.7	72.7	77.3	85	269	849	2,685	8,491	26,852

FHWA RD-77-108 Traffic Noise Prediction Model

Data Input Sheet

Project Name : Nakano Project Number : 3396.1 Modeled Condition : 2024

Surface Refelction: CNEL Assessment Metric: Hard Peak ratio to ADT: 10.0 Traffic Desc. (Peak or ADT) : ADT

				Speed	Distance						
Segmer	nt Roadway	Segment	Traffic Vol.	(Mph)	to CL	% Autos	%MT	% HT	Day %	Eve %	Night % K-Factor
WITHO	JT PROJECT										
1	Dennery Road	Palm Avenue to Regatta Lane	13,994	35	50	93.00	3.70	3.30	77.00	10.00	13.00
2		Regatta Lane to Landing Driveway	8,473	35	50	93.00	3.70	3.30	77.00	10.00	13.00
3		Landing Driveway to Red Coral	8,354	35	50	93.00	3.70	3.30	77.00	10.00	13.00
4	Palm Avenue	I-805 SB Ramps to NB Ramps	38,031	45	50	93.00	3.70	3.30	77.00	10.00	13.00
5		I-805 NB Ramps to Dennery Road	51,613	45	50	93.00	3.70	3.30	77.00	10.00	13.00
WITH P	ROJECT										
1	Dennery Road	Palm Avenue to Regatta Lane	15,858	35	50	93.00	3.70	3.30	77.00	10.00	13.00
2		Regatta Lane to Landing Driveway	10,375	35	50	93.00	3.70	3.30	77.00	10.00	13.00
3		Landing Driveway to Red Coral	10,256	35	50	93.00	3.70	3.30	77.00	10.00	13.00
4	Palm Avenue	I-805 SB Ramps to NB Ramps	38,963	45	50	93.00	3.70	3.30	77.00	10.00	13.00
5		I-805 NB Ramps to Dennery Road	53,173	45	50	93.00	3.70	3.30	77.00	10.00	13.00

FHWA RD-77-108 Traffic Noise Prediction Model

Predicted Noise Levels

Project Name :	Nakano
Project Number :	3396.1
Modeled Condition :	2024
Assessment Metric:	Hard

			No	Noise Levels, dBA Hard							Distance to Traffic Noise Level Contours, Fee					
Segmer	nt Roadway	Segment	Auto	MT	HT	Tota	75 dB	70 dB	65 dB	60 dB	55 dB	50 dB				
WITHO	JT PROJECT															
1	Dennery Road	Palm Avenue to Regatta Lane	65.7	61.4	66.1	69.6	14	46	144	456	1,442	4,560				
2		Regatta Lane to Landing Driveway	63.6	59.2	63.9	67.5	9	28	89	281	889	2,812				
3		Landing Driveway to Red Coral	63.5	59.2	63.9	67.4	9	27	87	275	869	2,748				
4	Palm Avenue	I-805 SB Ramps to NB Ramps	73.2	67.5	71.5	76.1	64	204	644	2,037	6,441	20,369				
5		I-805 NB Ramps to Dennery Road	74.5	68.8	72.8	77.4	87	275	869	2,748	8,689	27,477				
WITH P	ROJECT															
1	Dennery Road	Palm Avenue to Regatta Lane	66.3	62.0	66.7	70.2	17	52	166	524	1,656	5,236				
2		Regatta Lane to Landing Driveway	64.4	60.1	64.8	68.3	11	34	107	338	1,069	3,380				
3		Landing Driveway to Red Coral	64.4	60.1	64.8	68.3	11	34	107	338	1,069	3,380				
4	Palm Avenue	I-805 SB Ramps to NB Ramps	73.3	67.6	71.6	76.2	66	208	659	2,084	6,591	20,843				
5		I-805 NB Ramps to Dennery Road	74.7	68.9	72.9	77.5	89	281	889	2,812	8,891	28,117				

FHWA RD-77-108 Traffic Noise Prediction Model

Project Name : Nakano Project Number : 3396.1 Modeled Condition : 2062

Surface Refelction: CNEL Assessment Metric: Hard Peak ratio to ADT: 10.0 Traffic Desc. (Peak or ADT) : ADT

Data Input Sheet

				Speed	Distance						
Segmen	t Roadway	Segment	Traffic Vol.	(Mph)	to CL	% Autos	%MT	% HT	Day %	Eve %	Night % K-Factor
WITHOU	JT PROJECT										
1	Dennery Road	Palm Avenue to Regatta Lane	19,500	35	50	93.00	3.70	3.30	77.00	10.00	13.00
2		Regatta Lane to Landing Driveway	12,500	35	50	93.00	3.70	3.30	77.00	10.00	13.00
3		Landing Driveway to Red Coral	12,500	35	50	93.00	3.70	3.30	77.00	10.00	13.00
4	Palm Avenue	I-805 SB Ramps to NB Ramps	46,000	45	50	93.00	3.70	3.30	77.00	10.00	13.00
5		I-805 NB Ramps to Dennery Road	59,500	45	50	93.00	3.70	3.30	77.00	10.00	13.00
WITH PI	ROJECT										
1	Dennery Road	Palm Avenue to Regatta Lane	21,364	35	50	93.00	3.70	3.30	77.00	10.00	13.00
2		Regatta Lane to Landing Driveway	14,402	35	50	93.00	3.70	3.30	77.00	10.00	13.00
3		Landing Driveway to Red Coral	14,402	35	50	93.00	3.70	3.30	77.00	10.00	13.00
4	Palm Avenue	I-805 SB Ramps to NB Ramps	46,932	45	50	93.00	3.70	3.30	77.00	10.00	13.00
5		I-805 NB Ramps to Dennery Road	61,060	45	50	93.00	3.70	3.30	77.00	10.00	13.00

FHWA RD-77-108 Traffic Noise Prediction Model

Predicted Noise Levels

Project Name : Nakano Project Number : 3396.1 Modeled Condition : 2062 Assessment Metric: Hard

			Noise Levels, dBA Hard					Distance to Traffic Noise Level Contours, Feet					
Segmer	it Roadway	Segment	Auto	MT	HT	Tota	75 dB	70 dB	65 dB	60 dB	55 dB	50 dB	
WITHO	JT PROJECT												
1	Dennery Road	Palm Avenue to Regatta Lane	67.2	62.9	67.6	71.1	20	64	204	644	2,037	6,441	
2		Regatta Lane to Landing Driveway	65.2	60.9	65.6	69.2	13	42	132	416	1,315	4,159	
3		Landing Driveway to Red Coral	65.2	60.9	65.6	69.2	13	42	132	416	1,315	4,159	
4	Palm Avenue	I-805 SB Ramps to NB Ramps	74.0	68.3	72.3	76.9	77	245	774	2,449	7,744	24,489	
5		I-805 NB Ramps to Dennery Road	75.2	69.4	73.4	78.0	100	315	998	3,155	9,976	31,548	
WITH P	ROJECT												
1	Dennery Road	Palm Avenue to Regatta Lane	67.6	63.3	68.0	71.5	22	71	223	706	2,233	7,063	
2		Regatta Lane to Landing Driveway	65.9	61.5	66.2	69.8	15	48	151	477	1,510	4,775	
3		Landing Driveway to Red Coral	65.9	61.5	66.2	69.8	15	48	151	477	1,510	4,775	
4	Palm Avenue	I-805 SB Ramps to NB Ramps	74.1	68.4	72.4	77.0	79	251	792	2,506	7,924	25,059	
5		I-805 NB Ramps to Dennery Road	75.3	69.5	73.5	78.1	102	323	1,021	3,228	10,209	32,283	

ATTACHMENT 5

SoundPLAN Data – Operational Noise

		Level		Corrections	5
Source name	Reference	Leq1	Cwall	CI	CT
		dB(A)	dB(A)	dB(A)	dB(A)
HVAC1	Lw/unit	76	-	-	-
HVAC2	Lw/unit	76	-	-	-
HVAC3	Lw/unit	76	-	-	-
HVAC4	Lw/unit	/6	-	-	-
HVAC5	Lw/unit	/6	-	-	-
HVAC6	Lw/unit	/6	-	-	-
HVAC7	Lw/unit	/6	-	-	-
HVAC8	Lw/unit	/6	-	-	-
HVAC9	Lw/unit	76	-	-	-
HVACIU	Lw/unit	70	-	-	-
HVACII	Lw/unit	70	-	-	-
HVACI2	Lw/unit	70	-	-	-
HVAC13	Lw/unit	76	-	-	-
	Lw/unit	70	-	-	-
	Lw/unit	70	-	-	-
	Lw/unit	70	-	-	-
	Lw/unit	70	-	-	-
	Lw/unit	70	-	-	-
	Lw/unit	70	-	-	-
HVAC20	Lw/unit	76	-	-	-
	Lw/unit	70	-	-	-
HVAC22	Lw/unit	70	-	-	-
HVAC23	Lw/unit	76	-	-	-
HVAC24	Lw/unit	70	-	-	-
HVAC25	Lw/unit	70	-	-	-
HVAC26	Lw/unit	70	-	-	-
HVAC27	Lw/unit	70	-	-	-
HVAC28	Lw/unit	70	-	-	-
HVAC29	Lw/unit	70	-	-	-
HVAC30	Lw/unit	76	-	-	-
	Lw/unit	70	-	-	-
	Lw/unit	70	-	-	-
HVAC33	Lw/unit	70	-	-	-
	Lw/unit	70	-	-	-
HVAC36	Lw/unit	76	-	-	-
	Lw/unit	76	-	-	-
	Lw/unit	76	-	-	-
	Lw/unit	76	-	-	-
	Lw/unit	76	-	-	-
	Lw/unit	76	_	_	_
HVAC42	Lw/unit	76	_	_	_
HVAC43	Lw/unit	76	_	_	_
HVAC44	Lw/unit	76	-	-	-
HVAC45	Lw/unit	76	_	_	_
HVAC46	Lw/unit	76	-	-	-
HVAC47	Lw/unit	76	-	-	-
HVAC48	Lw/unit	76	-	-	-
HVAC49	Lw/unit	76	-	-	-
HVAC50	Lw/unit	76	-	-	-
HVAC51	Lw/unit	76	-	-	-
HVAC52	Lw/unit	76	-	-	-
HVAC53	Lw/unit	76	-	-	-
HVAC54	Lw/unit	76	-	-	-
HVAC55	Lw/unit	76	-	-	-
HVAC56	Lw/unit	76	-	-	-
HVAC57	Lw/unit	76	-	-	-
HVAC58	Lw/unit	76	-	-	-
HVAC59	Lw/unit	76	-	-	-
HVAC60	Lw/unit	76	-	-	-
HVAC61	Lw/unit	76	-	-	-
HVAC62	Lw/unit	76	-	-	-
HVAC63	Lw/unit	76	-	-	-
HVAC64	Lw/unit	76	-	-	-
HVAC65	Lw/unit	76	-	-	-
HVAC66	Lw/unit	76	-	-	-
HVAC67	Lw/unit	76	-	-	-
HVAC68	Lw/unit	76	-	-	-
HVAC69	Lw/unit	76	-	-	-
HVAC70	Lw/unit	76	-	-	-
HVAC71	Lw/unit	76	-	-	-
HVAC72	Lw/unit	76	-	-	-

HVAC73	Lw/unit	76	-	-	-
	lw/unit	76			
ITVAC74	Lw/unit	70			
HVAC75	Lw/unit	76	-	-	-
HVAC76	Lw/unit	76	-	-	-
	luu/upit	76			
HVAC//	Lw/unit	70	-	-	-
HVAC78	Lw/unit	76	-	-	-
HVAC79	Lw/unit	76	-	-	-
	Lw/ drift	70			
HVAC80	Lw/unit	/6	-	-	-
HVAC81	l w/unit	76	-	-	-
111/10/02		70			
HVAC82	Lw/unit	76	-	-	-
HVAC83	Lw/unit	76	-	-	-
	Lw/upit	76			
TTVAC04	Lw/unit	70	-	-	-
HVAC85	Lw/unit	76	-	-	-
HVAC86	lw/unit	76	-	-	-
111/1000	211/ 01/10	70			
HVAC8/	Lw/unit	76	-	-	-
HVAC88	Lw/unit	76	-	-	-
	luu/upit	76			
HVAC09	Lw/unit	70	-	-	-
HVAC90	Lw/unit	76	-	-	-
Ηνας91	Lw/unit	76	-	-	-
	Lw/ drift	70			
HVAC92	Lw/unit	/6	-	-	-
HVAC93	Lw/unit	76	-	-	-
	1	70			
HVAC94	Lw/unit	76	-	-	-
HVAC95	Lw/unit	76	-	-	-
HVAC96	Lw/unit	76	-	-	-
IIVAC50	Lwy unit	70			
HVAC97	Lw/unit	76	-	-	-
HVAC98	lw/unit	76	-	-	-
111/1.000	211/ 01/10	70			
HVAC99	Lw/unit	76	-	-	-
HVAC100	Lw/unit	76	-	-	-
	luu/upit	76			
HVACIUI	Lw/unit	70	-	-	-
HVAC102	Lw/unit	76	-	-	-
HVAC103	Lw/unit	76	-	-	-
	Lw/ drift	70			
HVAC104	Lw/unit	/6	-	-	-
HVAC105	Lw/unit	76	-	-	-
	luu/upit	76			
HVAC100	Lw/unit	70	-	-	-
HVAC107	Lw/unit	76	-	-	-
	Lw/unit	76	-	-	-
	Lw/ drift	70			
HVAC109	Lw/unit	76	-	-	-
HVAC110	Lw/unit	76	-	-	-
	luu/upit	76			
HVACIII	Lw/unit	76	-	-	-
HVAC112	Lw/unit	76	-	-	-
	Lw/unit	76	_	_	_
IIVACIIS	Lwy unit	70			
HVAC114	Lw/unit	76	-	-	-
HVAC115	l w/unit	76	-	-	-
111/10/11/		70			
HVACIIO	Lw/unit	76	-	-	-
HVAC117	Lw/unit	76	-	-	-
	Lw/unit	76	_	_	_
INACIIO	Lwy unit	70			
HVAC119	Lw/unit	76	-	-	-
HVAC120	Lw/unit	76	-	-	-
LIV (A C121	1	70			
HVACIZI	Lw/unit	70	-	-	-
HVAC122	Lw/unit	76	-	-	-
HV/AC123	Lw/unit	76	_	_	_
TIV/ (CIES	Lw, and				
HVAC124	Lw/unit	/6	-	-	-
HVAC125	Lw/unit	76	-	-	-
	1.44/100-14	76			
ITVACIZO	Lw/unit	01	-	-	-
HVAC127	Lw/unit	76	-	-	-
HVAC128	lw/unit	76	-	-	-
	Livy annu				
HVAC129	Lw/unit	/6	-	-	-
HVAC130		70		-	-
111/10/101	Lw/unit	/6	-		
TVACIST	Lw/unit	76	-		
	Lw/unit Lw/unit	76 76	-	-	-
HVAC132	Lw/unit Lw/unit Lw/unit	76 76 76	-	-	-
HVAC132 HVAC133	Lw/unit Lw/unit Lw/unit Lw/unit	76 76 76 76	-	- -	-
HVAC132 HVAC133	Lw/unit Lw/unit Lw/unit Lw/unit	76 76 76 76	- - -	- - -	- -
HVAC132 HVAC133 HVAC134	Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit	76 76 76 76 76	- - -	- - -	- - -
HVAC132 HVAC133 HVAC134 HVAC135	Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit	76 76 76 76 76 76		- - -	- - -
HVAC132 HVAC133 HVAC134 HVAC135 HVAC136	Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit	76 76 76 76 76 76 76			- - -
HVAC132 HVAC133 HVAC134 HVAC135 HVAC136	Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit	76 76 76 76 76 76		- - - -	- - - -
HVAC132 HVAC133 HVAC134 HVAC135 HVAC136 HVAC137	Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit	76 76 76 76 76 76 76 76			- - - -
HVAC132 HVAC133 HVAC134 HVAC135 HVAC136 HVAC137 HVAC138	Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit	76 76 76 76 76 76 76 76 76			-
HVAC132 HVAC133 HVAC134 HVAC135 HVAC136 HVAC137 HVAC138 HVAC132	Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit	76 76 76 76 76 76 76 76 76 76			-
HVAC132 HVAC133 HVAC134 HVAC135 HVAC136 HVAC137 HVAC138 HVAC139	Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit	76 76 76 76 76 76 76 76 76			
HVAC132 HVAC133 HVAC134 HVAC135 HVAC136 HVAC137 HVAC138 HVAC139 HVAC140	Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit	76 76 76 76 76 76 76 76 76 76 76			
HVAC132 HVAC133 HVAC134 HVAC135 HVAC136 HVAC137 HVAC137 HVAC138 HVAC139 HVAC140 HVAC141	Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit	76 76 76 76 76 76 76 76 76 76 76 76	-		
HVAC132 HVAC133 HVAC134 HVAC135 HVAC136 HVAC136 HVAC137 HVAC138 HVAC139 HVAC140 HVAC141	Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit	76 76 76 76 76 76 76 76 76 76 76	-		
HVAC132 HVAC133 HVAC134 HVAC135 HVAC136 HVAC137 HVAC138 HVAC139 HVAC140 HVAC141 HVAC142	Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit	76 76 76 76 76 76 76 76 76 76 76 76			
HVAC132 HVAC133 HVAC134 HVAC135 HVAC136 HVAC137 HVAC137 HVAC138 HVAC139 HVAC140 HVAC141 HVAC141 HVAC142 HVAC143	Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit	76 76 76 76 76 76 76 76 76 76 76 76 76 7	-		
HVAC132 HVAC133 HVAC134 HVAC135 HVAC136 HVAC136 HVAC137 HVAC138 HVAC139 HVAC140 HVAC141 HVAC142 HVAC143	Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit	76 76 76 76 76 76 76 76 76 76 76 76	-	-	
HVAC132 HVAC133 HVAC134 HVAC135 HVAC136 HVAC137 HVAC138 HVAC139 HVAC140 HVAC141 HVAC142 HVAC143 HVAC143 HVAC144	Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit	76 76 76 76 76 76 76 76 76 76 76 76 76 7			
HVAC132 HVAC133 HVAC134 HVAC135 HVAC136 HVAC137 HVAC137 HVAC138 HVAC139 HVAC140 HVAC141 HVAC142 HVAC143 HVAC144 HVAC144 HVAC145	Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit	76 76 76 76 76 76 76 76 76 76 76 76 76 7			-
HVAC132 HVAC133 HVAC134 HVAC135 HVAC136 HVAC136 HVAC137 HVAC138 HVAC139 HVAC140 HVAC141 HVAC142 HVAC143 HVAC144 HVAC145 HVAC146	Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit	76 76 76 76 76 76 76 76 76 76 76 76 76 7			-
HVAC132 HVAC133 HVAC134 HVAC135 HVAC136 HVAC137 HVAC137 HVAC138 HVAC140 HVAC140 HVAC141 HVAC142 HVAC143 HVAC144 HVAC145 HVAC146	Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit Lw/unit	76 76 76 76 76 76 76 76 76 76 76 76 76 7			

HVAC148	Lw/unit	76	-	-	-
HVAC149	Lw/unit	76	-	-	-
HVAC150	Lw/unit	76	-	-	-
HVAC151	Lw/unit	76	-	-	-
HVAC152	l w/unit	76	-	_	-
HVAC153	Lw/unit	76	-	_	_
HVAC154	Lw/unit	76	_	_	_
	Lw/unit	70			
HVACISS	Lw/unit	70	-	-	-
HVAC156	Lw/unit	/6	-	-	-
HVAC157	Lw/unit	76	-	-	-
HVAC158	Lw/unit	76	-	-	-
HVAC159	Lw/unit	76	-	-	-
HVAC160	Lw/unit	76	-	-	-
HVAC161	Lw/unit	76	-	-	-
HVAC162	l w/unit	76	-	-	_
HVAC163	lw/unit	76	_	_	_
	Lw/unit	76			
	Lw/unit	70			
HVAC165	Lw/unit	/6	-	-	-
HVAC166	Lw/unit	/6	-	-	-
HVAC167	Lw/unit	76	-	-	-
HVAC168	Lw/unit	76	-	-	-
HVAC169	Lw/unit	76	-	-	-
HVAC170	Lw/unit	76	-	-	-
HVAC171	l w/unit	76	-	-	_
HVAC172	Lw/unit	76	_	_	_
	Lw/unit	70			
HVACI/3	Lw/unit	/0	-	-	-
HVAC1/4	Lw/unit	/6	-	-	-
HVAC175	Lw/unit	76	-	-	-
HVAC176	Lw/unit	76	-	-	-
HVAC177	Lw/unit	76	-	-	-
HVAC178	Lw/unit	76	-	-	-
HVAC179	Lw/unit	76	-	-	-
HVAC180	l w/unit	76	-	_	-
	Lw/unit	76			
	Lw/unit	70			
HVAC162	Lw/unit	76	-	-	-
HVAC183	Lw/unit	/6	-	-	-
HVAC184	Lw/unit	76	-	-	-
HVAC185	Lw/unit	76	-	-	-
HVAC186	Lw/unit	76	-	-	-
HVAC187	Lw/unit	76	-	-	-
HVAC188	Lw/unit	76	-	-	-
HVAC189	l w/unit	76	-	_	-
HVAC190	Lw/unit	76	_	_	_
	Lw/unit	76			
HVAC191	Lw/unit	76	-	-	-
HVAC192	Lw/unit	76	-	-	-
HVAC193	Lw/unit	76	-	-	-
HVAC194	Lw/unit	76	-	-	-
HVAC195	Lw/unit	76	-	-	-
HVAC196	Lw/unit	76	-	-	-
HVAC197	Lw/unit	76	-	-	-
HVAC198	l w/unit	76	-	_	-
	Lw/unit	76			
	Lw/unit	70			
HVAC200	Lw/unit	76	-	-	-
HVAC201	Lw/unit	/6	-	-	-
HVAC202	Lw/unit	76	-	-	-
HVAC203	Lw/unit	76	-	-	-
HVAC204	Lw/unit	76	-	-	-
HVAC205	Lw/unit	76	-	-	-
HVAC206	Lw/unit	76	-	-	-
HVAC207	l w/unit	76	-	_	-
	Lw/unit	76			
11VAC200	Lw/unit	70			
LIVAC209	Ew/unit	70	-	-	-
HVAC210	Lw/unit	/0	-	-	-
HVAC211	Lw/unit	/6	-	-	-
HVAC212	Lw/unit	76	-	-	-
HVAC213	Lw/unit	76	-	-	-
HVAC214	Lw/unit	76	-	-	-
HVAC215	Lw/unit	76	-	-	-
Park1	Lw/unit	55	-	-	-
Park2	Lw/unit	55	-	-	-
Park3	l w/unit	55	-	_	_
Park4	Lw/unit	55	_	_	_
Park5	Lw/unit	55			-
I AINJ	LW/ UTIL	رر	-	-	-

	Coord	linates		
No.	Х	Y	Height	Noise Level
	(me	ters)	m	dB(A) Leq
1	497015.59	3605890.54	47.83	36.1
2	497010.86	3605836.20	48.44	34.7
3	497009.68	3605805.48	48.95	35.5
4	497000.23	3605760.59	48.69	39.6
5	496999.05	3605715.11	49.50	39.7
6	496996.69	3605667.26	49.66	37.6
7	497038.03	3605635.37	51.19	29.9
8	496967.68	3605735.78	38.26	43.5
9	496812.41	3605560.69	54.77	38.9
10	496652.46	3605715.51	34.75	45.4
11	496822.43	3605865.82	31.98	43.8

ATTACHMENT 6

SoundPLAN Data – Future Vehicle Traffic Noise

3396.1 Nakano SoundPLAN Data - Vehicle Traffic

	Traffic values						Control	Constr.	Affect.		Gradient
Station	ADT Vehicles type	Vehicle	nar day	evening	night	Speed	device	Speed	veh.	Road surface	Min / Max
km	Veh/24h		Veh/h	Veh/h	Veh/h	km/h		km/h	%		%
I-805 N	lorthbound Traffic direct	tion: In en	try direction								
0+000	73704 Total	-	4729	2457	1065	5 -	none	-	-	Average (of DGAC and PCC)	-1.875
0+000	73704 Automobiles	-	4398	2285	990) 105	none	-	-	Average (of DGAC and PCC)	-1.875
0+000	73704 Medium trucl	ks -	175	91	39	89	none	-	-	Average (of DGAC and PCC)	-1.875
0+000	73704 Heavy trucks	-	156	81	35	5 89	none	-	-	Average (of DGAC and PCC)	-1.875
0+000	73704 Buses	-	-	-	-	105	none	-	-	Average (of DGAC and PCC)	-1.875
0+000	73704 Motorcycles	-	-	-	-	105	none	-	-	Average (of DGAC and PCC)	-1.875
0+000	73704 Auxiliary vehi	cle -	-	-	-	-	none	-	-	Average (of DGAC and PCC)	-1.875
0+912		-	-	-	-						
I-805 S	outhbound Traffic direct	tion: In en	try direction								
0+000	81504 Total	-	5230	2717	1177	7 _	none	-	-	Average (of DGAC and PCC)	-0.516129032
0+000	81504 Automobiles	-	4864	2527	1095	5 105	none	-	-	Average (of DGAC and PCC)	-0.516129032
0+000	81504 Medium trucl	ks -	194	101	44	4 89	none	-	-	Average (of DGAC and PCC)	-0.516129032
0+000	81504 Heavy trucks	-	173	90	39	89	none	-	-	Average (of DGAC and PCC)	-0.516129032
0+000	81504 Buses	-	-	-	-	105	none	-	-	Average (of DGAC and PCC)	-0.516129032
0+000	81504 Motorcycles	-	-	-	-	105	none	-	-	Average (of DGAC and PCC)	-0.516129032
0+000	81504 Auxiliary vehi	cle -	-	-	-	-	none	-	-	Average (of DGAC and PCC)	-0.516129032
0+906		-	-	-	-						
Denner	y Road Traffic direction:	In entry c	lirection								
0+000	21432 Total	-	1371	712	316	ō -	none	-	-	Average (of DGAC and PCC)	1.375
0+000	21432 Automobiles	-	1275	662	309	9 56	none	-	-	Average (of DGAC and PCC)	1.375
0+000	21432 Medium trucl	ks -	51	26	j ∠	4 56	none	-	-	Average (of DGAC and PCC)	1.375
0+000	21432 Heavy trucks	-	45	23	3	3 56	none	-	-	Average (of DGAC and PCC)	1.375
0+000	21432 Buses	-	-	-	-	56	none	-	-	Average (of DGAC and PCC)	1.375
0+000	21432 Motorcycles	-	-	-	-	56	none	-	-	Average (of DGAC and PCC)	1.375
0+000	21432 Auxiliary vehi	cle -	-	-	-	-	none	-	-	Average (of DGAC and PCC)	1.375
0+442	14400 Total	-	924	480	208	3 -	none	-	-	Average (of DGAC and PCC)	-8.25
0+442	14400 Automobiles	-	859	446	203	3 56	none	-	-	Average (of DGAC and PCC)	-8.25
0+442	14400 Medium trucl	ks -	34	18	i á	2 56	none	-	-	Average (of DGAC and PCC)	-8.25
0+442	14400 Heavy trucks	-	30	16	i ź	2 56	none	-	-	Average (of DGAC and PCC)	-8.25
0+442	14400 Buses	-	-	-	-	56	none	-	-	Average (of DGAC and PCC)	-8.25
0+442	14400 Motorcycles	-	-	-	-	56	none	-	-	Average (of DGAC and PCC)	-8.25
0+442	14400 Auxiliary vehi	cle -	-	-	-	-	none	-	-	Average (of DGAC and PCC)	-8.25
0+764		-	-	-	-						

3396.1 Nakano SoundPLAN Data - Vehicle Traffic

	Coordinates				Noise Level without Barrier					Noise Level with Barrier				Difference			
No.	Х	Y	Floor	Height	Day	Evening	Night	Lden	Day	Evening	Night	Lden		Day	Evening	Night	Lden
1	496915.02	3605622.56	3.Fl	43.55	52.6	49.8	45.6	54.2	52.6	49.8	45.6	54.2		0	0	0	0
2	496862.79	3605613.92	3.FI	43.57	55.6	52.8	49.0	57.5	55.6	52.7	49.0	57.4		0	0	0	0
3	496771.28	3605615.38	3.FI	42.65	56.3	53.5	49.8	58.2	56.2	53.4	49.7	58.1		-0.1	-0.1	-0.1	-0.1
4	496733.70	3605615.35	3.FI	42.34	57.8	55.0	51.3	59.7	58.1	55.2	51.6	60.0		0.3	0.3	0.3	0.3
5	496697.63	3605614.83	3.FI	42.35	61.7	58.9	55.3	63.6	61.9	59.1	55.4	63.8		0.2	0.2	0.2	0.2
6	496662.79	3605614.34	3.FI	42.35	67.7	64.9	61.3	69.6	67.4	64.6	61.0	69.3		-0.3	-0.3	-0.3	-0.3
7	496656.15	3605634.57	3.FI	42.20	70.1	67.3	63.6	72.0	70.2	67.3	63.7	72.1		0	0	0	0
8	496703.49	3605645.08	3.FI	41.56	64.4	61.6	57.9	66.3	64.4	61.6	57.9	66.3		0	0	0	0
9	496676.19	3605644.68	3.FI	41.24	66.8	64.0	60.4	68.7	66.8	64.0	60.3	68.7		0	0	0	0
10	496667 19	3605653 53	3 FI	41.24	713	68.5	64.9	73.2	71.4	68.5	64.9	73.3		0	0	0	0
11	496675 35	3605663.82	3 FI	41 33	67.4	64.5	60.9	69.3	67.4	64.5	60.9	69.3		0	0	0	0
12	496694.86	3605664.40	3 FI	41 58	59.8	57.0	53.3	61.7	59.9	57.0	53.4	61.8		01	01	01	01
12	406711.00	2605664.40	2 51	41.50	E0 0	57.0	55.5 E1.0	60.2	55.5 EQ /	57.0	55.4 E1.0	60.2		0.1	0.1	0.1	0.1
13	490711.02	3003004.20	3.FI 3.FI	41.74	50.5	53.5	51.5	00.2 F0.0	50.4	55.5	51.5	00.5 F0.0		0	0	0	0
14	496750.06	3003004.03	3.FI 3.FI	41.00	20.9	54.0	50.4	20.0	20.9	54.1	50.4	20.0		01	0	01	0
15	490007.25	3005073.90	5.FI	41.47	72.5	09.5	65.9	74.2	72.4	69.6	65.9	74.5		0.1	0.1	0.1	0.1
16	496676.12	3605682.84	3.FI	41.63	70.3	67.4	63.8	12.2	70.3	67.4	63.8	72.2		0	0	0	0
17	496693.97	3605682.81	3.FI	41.69	66.9	64.1	60.4	68.8	66.9	64.1	60.4	68.8		0	0	0	0
18	496712.16	3605682.93	3.FI	41.83	64.3	61.5	57.9	66.2	64.3	61.5	57.8	66.2		0	0	0	0
19	496730.02	3605682.85	3.FI	41.85	62.7	59.9	56.3	64.6	62.7	59.9	56.2	64.6		0	0	0	0
20	496724.66	3605695.08	3.FI	41.84	63.6	60.8	57.1	65.5	63.6	60.8	57.1	65.5		0	0	0	0
21	496704.70	3605695.12	3.FI	41.76	64.9	62.1	58.4	66.8	64.9	62.1	58.5	66.8		0	0	0	0
22	496686.11	3605694.80	3.FI	41.72	67.3	64.4	60.8	69.2	67.3	64.4	60.8	69.2		0	0	0	0
23	496670.36	3605702.54	3.FI	41.57	73.2	70.4	66.7	75.1	73.2	70.4	66.7	75.1		0	0	0	0
24	496682.74	3605714.04	3.FI	41.40	67.3	64.5	60.9	69.2	67.3	64.5	60.9	69.2		0	0	0	0
25	496702.02	3605714.16	3.FI	41.41	63.1	60.3	56.7	65.0	63.1	60.3	56.7	65.0		0	0	0	0
26	496721.99	3605714.16	3.FI	41.63	61.0	58.1	54.5	62.9	61.0	58.1	54.5	62.9		0	0	0	0
27	496670.27	3605723.09	3.FI	41.36	73.4	70.5	66.9	75.3	73.4	70.5	66.9	75.3		0	0	0	0
28	496681.18	3605733.06	3.FI	41.08	70.5	67.6	64.0	72.4	70.5	67.6	64.0	72.4		0	0	0	0
29	496696 61	3605733.11	3 FI	41.02	68.3	65.4	61.8	70.2	68.3	65.4	61.8	70.2		0	0	0	0
30	496712 56	3605733.43	3 FI	41.28	65.5	62.6	59.0	67.4	65.5	62.6	59.0	67.4		0	0	0	0
21	490712.30	2605733.43	2 51	41.20	62.4	60.6	55.0	65.2	62.4	60.6	55.0	65.2		0	0	0	0
32	490729.79	3605733.19	3 61	41.44	611	58.2	54.6	63.0	611	58.2	54.6	63.0		0	0	0	0
22	496749.00	2605735.15	2 51	41.34	61.7	50.2	54.0	62.6	61.7	50.2	54.0	62.6		0	0	0	0
22	496749.29	3005745.54	5.FI	41.44	61.7	50.9	55.2	05.0	61.7	50.9	55.2	05.0		0	0	0	0
34	496729.34	3605744.75	3.FI	41.40	63.6	60.8	57.2	65.5	63.6	60.8	57.2	65.5		0	0	0	0
35	496/13.15	3605744.75	3.FI	41.19	65.0	62.2	58.5	66.9	65.0	62.2	58.5	66.9		0	0	0	0
36	496693.99	3605/44.0/	3.FI	40.93	68.6	65.7	62.1	/0.5	68.6	65.7	62.1	70.5		0	0	0	0
37	496682.87	3605755.00	3.FI	40.85	72.3	69.4	65.8	74.2	72.2	69.4	65.8	74.2		0	0	0	0
38	496698.67	3605763.73	3.FI	40.78	66.8	63.9	60.3	68.7	66.7	63.8	60.2	68.6		-0.1	-0.1	-0.1	-0.1
39	496712.99	3605763.84	3.FI	40.95	63.2	60.3	56.7	65.1	63.1	60.3	56.6	65.0		-0.1	-0.1	-0.1	-0.1
40	496725.69	3605763.93	3.FI	41.03	61.6	58.8	55.2	63.5	61.6	58.8	55.1	63.5		0	0	0	0
41	496696.27	3605782.90	3.FI	40.63	69.4	66.5	62.9	71.3	69.4	66.5	62.9	71.3		0	0	0	0
42	496714.87	3605783.27	3.Fl	40.70	68.3	65.4	61.8	70.2	68.3	65.4	61.8	70.2		0	0	0	0
43	496731.98	3605783.27	3.FI	40.80	67.7	64.9	61.2	69.6	67.7	64.9	61.2	69.6		0	0	0	0
44	496748.72	3605784.02	3.Fl	41.00	66.9	64.1	60.5	68.8	66.9	64.1	60.4	68.8		0	0	0	0
45	496765.84	3605783.27	3.FI	41.02	65.2	62.4	58.7	67.1	65.2	62.4	58.8	67.1		0	0	0	0
46	496782.58	3605784.02	3.FI	41.21	62.2	59.4	55.7	64.1	62.2	59.4	55.7	64.1		0	0	0	0
47	496797.46	3605783.27	3.FI	41.21	60.5	57.7	54.0	62.4	60.5	57.7	54.0	62.4		0	0	0	0
48	496795.60	3605795.18	3.FI	41.22	60.8	57.9	54.3	62.7	60.8	57.9	54.3	62.7		0	0	0	0
49	496776.95	3605796.13	3.FI	41.03	62.4	59.6	55.9	64.3	62.4	59.6	55.9	64.3		0	0	0	0
50	496760.09	3605796.83	3.FI	40.89	64.7	61.9	58.2	66.6	64.7	61.9	58.2	66.6		0	0	0	0
51	496754 09	3605805 95	3 FI	40 58	687	65.9	62.2	70.6	68.7	65.9	62.2	70.6		0	0	0	0
52	49676113	3605813 91	3 FI	40.63	66.9	641	60.4	68.8	66.9	641	60.5	68.8		0	0	0	0
53	496774 53	3605813 91	3 FI	40.70	64.5	61.7	58.1	66.4	64.7	61.8	58.2	66.6		01	01	0.1	01
54	496788 38	3605814.15	3 FI	40.75	63.0	60.1	56.5	64.9	62.8	59.9	56.3	647		-0.2	-0.2	-0.2	-0.2
55	496801.43	3605814.15	3 FI	41.03	61.7	58.9	55.3	63.6	61.8	58.9	55.3	63.7		0.2	0	0.2	0.2
55	406905 02	2605014.15	2 51	40.79	61.7	50.5	55.5	62.2	61.0	E0 0	53.5 E 4 7	62.1		0.2	0.2	0.2	0.2
50	490003.93	3003020.23	3.FI 3.FI	40.70	01.4	50.0	55.0	03.5	01.2	50.5	J4.7	64.2		-0.5	-0.5	-0.5	-0.5
57	496791.38	3605828.23	3.FI	40.46	62.5	59.6	56.0	64.4	62.3	59.4	55.8	64.2		-0.2	-0.2	-0.2	-0.2
50	496776.64	3003027.77	5.FI	40.55	05.0	60.7	57.1	05.5	05.7	60.9	57.2	05.0		0.1	0.1	0.1	0.1
59	496759.06	3605828.12	3.FI	40.43	65.6	62.8	59.1	67.5	65.8	63.0	59.3	67.7		0.2	0.2	0.2	0.2
60	496/44.51	3605838.16	3.FI	40.09	68.9	66.1	62.4	/0.8	68.9	66.1	62.4	/0.8		0	0	0	0
61	496758.13	3605845.43	3.FI	40.08	66.9	64.0	60.4	68.8	66.7	63.8	60.2	68.6		-0.2	-0.2	-0.2	-0.2
62	496772.45	3605845.55	3.FI	40.08	66.1	63.3	59.6	68.0	66.2	63.3	59.7	68.1		0.1	0.1	0.1	0.1
63	496785.61	3605845.55	3.FI	40.08	65.9	63.0	59.4	67.8	65.8	63.0	59.3	67.7		-0.1	-0.1	-0.1	-0.1
64	496799.47	3605845.78	3.FI	40.08	65.4	62.6	58.9	67.3	65.4	62.6	59.0	67.3		0	0	0	0
65	496812.86	3605845.90	3.Fl	40.08	64.9	62.1	58.4	66.8	64.9	62.1	58.4	66.8		0	0	0	0
66	496826.02	3605841.28	3.FI	40.4	60.6	57.7	54.1	62.5	60.7	57.9	54.2	62.6		0.1	0.1	0.1	0.1
67	496838.76	3605847.4	3.FI	40.67	64.3	61.5	57.8	66.2	64.3	61.5	57.8	66.2		0	0	0	0
68	496853.3	3605849.94	3.Fl	41.28	63.9	61.1	57.5	65.9	64.0	61.2	57.5	65.9		0.1	0.1	0.1	0.1
69	496871.08	3605852.94	3.Fl	41.34	63.7	60.9	57.2	65.6	63.7	60.9	57.3	65.6		0	0	0	0
70	496894.41	3605856.87	3.Fl	41.34	62.9	60.1	56.4	64.8	63.1	60.2	56.6	65.0		0.2	0.2	0.2	0.2
71	496910.57	3605859.52	3.FI	41.34	62.6	59.8	56.1	64.5	62.7	59.9	56.3	64.6		0.1	0.1	0.1	0.1
72	496934.93	3605863.56	3.FI	41.34	62.1	59.2	55.6	64.0	62.1	59.3	55.7	64.1		0.1	0.1	0.1	0.1
73	496960.41	3605791.26	3.Fl	40.93	50.5	47.6	43.6	52.2	50.4	47.6	43.6	52.2		0	0	0	0
74	496947.84	3605734.28	3.FI	41.33	51.3	48.5	44.4	53.0	51.3	48.5	44.4	53.0		0	0	0	0
75	496951.15	3605692.28	3.FI	41.85	49.4	46.6	42.1	50.9	49.4	46.6	42.1	50.9		0	0	0	0