Appendix E
Geotechnical Investigation

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GEOTECHNICAL INVESTIGATION

PROPOSED COMMERCIAL DEVELOPMENT
21611 SOUTH PERRY STREET
CARSON, CALIFORNIA
APN: 7327-010-014

GEOCON
WEST, INC.
GEOTECHNICAL
ENVIRONMENTAL
MATERIALS

PREPARED FOR
FARING CAPITAL, LLC
WEST HOLLYWOOD, CALIFORNIA

PROJECT NO. W1301-06-01

APRIL 23, 2021

GEOCON
WEST, INC.
GEOTECHNICAL ■ ENVIRONMENTAL ■ MATERIALS

Project No. W1301-06-01
April 23, 2021

Faring Capital, LLC
659 North Robertson Boulevard,
West Hollywood, California 90069

Attention: Mr. Darren Embry

Subject: GEOTECHNICAL INVESTIGATION
PROPOSED COMMERCIAL DEVELOPMENT
21611 SOUTH PERRY STREET
CARSON, CALIFORNIA
APN: 7327-010-014

Dear Mr. Embry:

In accordance with your authorization of our proposal dated December 11, 2020, we have prepared this geotechnical investigation report for the proposed commercial development located at 21611 South Perry Street in the City of Carson, California. The accompanying report presents the findings of our study, and our conclusions and recommendations pertaining to the geotechnical aspects of proposed design and construction. Based on the results of our investigation, it is our opinion that the site can be developed as proposed, provided the recommendations of this report are followed and implemented during design and construction.

If you have any questions regarding this report, or if we may be of further service, please contact the undersigned.

Very truly yours,

GEOCON WEST, INC.

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GEOTECHNICAL INVESTIGATION

1. PURPOSE AND SCOPE

This report presents the results of a geotechnical investigation for the proposed commercial development located at 21611 South Perry Street in the City of Carson, California (see Vicinity Map, Figure 1). The purpose of the investigation was to evaluate subsurface soil and geologic conditions underlying the site and, based on conditions encountered, to provide conclusions and recommendations pertaining to the geotechnical aspects of design and construction.

The scope of this investigation included a review of prior environmental reports for the site provided by the client, a site reconnaissance, field exploration, laboratory testing, engineering analysis, and the preparation of this report. The site was explored on February 9, 2021 by drilling five 8-inch diameter borings using a truck-mounted hollow-stem auger drilling machine and advancing five cone penetrometer tests (CPTs). The borings were excavated to depths between approximately 20½ and 51 feet beneath the existing ground surface. The CPTs were advanced to depths of approximately 60 feet below existing ground surface. The approximate locations of the exploratory borings and CPTs are depicted on the Site Plan (see Figure 2). A detailed discussion of the field investigation, including the boring and CPT logs, is presented in Appendix A.

Laboratory tests were performed on selected soil samples obtained during the investigation to determine pertinent physical and chemical soil properties. Appendix B presents a summary of the laboratory test results.

The recommendations presented herein are based on analysis of the data obtained during the investigation and our experience with similar soil and geologic conditions. References reviewed to prepare this report are provided in the *List of References* section.

If project details vary significantly from those described herein, Geocon should be contacted to determine the necessity for review and possible revision of this report.

2. SITE AND PROJECT DESCRIPTION

The subject site is an approximately 2.6-acre irregularly shaped parcel located at 21611 South Perry Street in the City of Carson, California. The site is currently vacant. The site is bounded by South Perry Street on the east, by the Dominguez Channel to the west, by one- to two-story single-family homes to the north, and by East Carson Street to the south. The site is relatively level, with no pronounced highs or lows. Surface water drainage at the site appears to be by sheet flow along the existing ground contours to the city streets.

Based on the information provided by the Client, it is our understanding that the proposed development will consist of three 2-story self-storage structures. Based on preliminary plans it is anticipated that the development will be approximately 25 feet in height and will be constructed at or near present grade (see Figure 2).

Based on the preliminary nature of the design at this time, wall and column loads were not available. It is anticipated that column loads for the proposed structures will be up to 300 kips, and wall loads will be up to 3 kips per linear foot.

Once the design phase and foundation loading configuration proceeds to a more finalized plan, the recommendations within this report should be reviewed and revised, if necessary. Any changes in the design, location or elevation of any structure, as outlined in this report, should be reviewed by this office. Geocon should be contacted to determine the necessity for review and possible revision of this report.

3. BACKGROUND

Prior environmental reports were prepared for the site and provided for our review, and include the following:

Phase 1 Environmental Site Assessment, 21611 S. Perry Street, Carson, CA. 90745-1613, Prepared by Weis Environmental, dated January 25, 2021.

2020 First Semi-Annual Groundwater Monitoring Report, January Through June 2020, Dominguez Channel Release, Carson, California, Prepared by AECOM, dated July 14, 2020.

Based on the prior reports, petroleum hydrocarbon impacted soil and groundwater were previously identified at the site that originated from on-site underground storage tanks (USTs) and migration of contaminants from off-site sources. AECOM (formerly URS) developed a workplan that developed cleanup goals and excavation limits to remove impacted soils that was approved by the LARWQCB. In 2014, approximately 4,800 cubic yards of impacted soils were excavated from four areas and removed from the site. The excavations were approximately 5 to 8 feet deep and were backfilled with clean import soils (Weis Environmental, 2021). The approximate locations and depths of these areas are indicated on the Site Plan (see Figure 2). The backfill was reportedly placed, compacted, and tested as a certified backfill material; however, a copy of the compaction report was not included as an exhibit. Therefore, for the purposes of this report, the backfill is considered to be uncertified fill.

Also, as part of the prior site remediation, groundwater monitoring wells were installed at the site and the immediately surrounding area. The monitoring wells present at the site are limited to the eastern, western, and southern property boundaries. Groundwater monitoring is ongoing in these wells in compliance with a semi-annual groundwater monitoring program required by the LARWQCB.

Based on documents included in the referenced environmental reports, the known soil and groundwater impacts are within acceptable levels for commercial use and further assessment or remediation is not required. However, a soil management plan (SMP) is anticipated required for further development of the site. Development of a soil management plan is beyond the scope of the Geotechnical Investigation.

4. GEOLOGIC SETTING

The site is located in the southern portion of the Los Angeles Basin, a coastal plain bounded by the Santa Monica Mountains on the north, the Elysian Hills and Repetto Hills on the northeast, the Puente Hills and the Whittier Fault on the east, the Palos Verdes Peninsula and Pacific Ocean on the west and south, and the Santa Ana Mountains and San Joaquin Hills on the southeast. The basin is underlain by a deep structural depression which has been filled by both marine and continental sedimentary deposits underlain by a basement complex of igneous and metamorphic composition. Regionally, the site is located within the northern portion of the Peninsular Ranges geomorphic province. This geomorphic province is characterized by northwest-trending physiographic and geologic features such as the nearby Newport-Inglewood Fault Zone located approximately 2.7 miles to the east-northeast.

5. SOIL AND GEOLOGIC CONDITIONS

Based on our field investigation and published geologic maps of the area, the site is underlain by artificial fill and Holocene age alluvium consisting sand, silt, and clay (California Geological Survey, 2010). Detailed stratigraphic profiles of the materials encountered at the site are provided on the boring logs in Appendix A.

5.1 Artificial Fill

Artificial fill was encountered in our explorations to depths ranging from 3 to 9 feet below existing ground surface. The deep fill, observed in boring B3, is associated with an area of a former UST removal. The artificial generally consists of light brown to brown or grayish brown sand and silty sand. The artificial fill is characterized as fine-grained with some medium-grained, moist, and loose to dense. The fill is likely the result of past grading, UST removal and environmental remediation, and past construction activities at the site. Deeper fill may exist between excavations and in other portions of the site that were not directly explored.

5.2 Alluvium

Holocene age alluvium was encountered beneath the fill to the maximum depth explored (51 feet below the ground surface). The alluvium generally consists of light brown to brown, olive brown, or gray to dark gray interbedded clay, sandy clay, silt, sandy silt, silty sand and clayey sand. The alluvial soils are characterized as primarily fine-grained, moist to wet, and loose to dense or soft to stiff.

6. GROUNDWATER

A review of the Seismic Hazard Zone Report for the Torrance Quadrangle (California Division of Mines and Geology [CDMG], 1998) indicates the historically highest groundwater level in the area is approximately 9 feet beneath the ground surface. Groundwater information presented in this document is generated from data collected in the early 1900's to the late 1990s. Based on current groundwater basin management practices, it is unlikely that groundwater levels will ever exceed the historic high levels.

Groundwater was encountered in borings B1 and B3 at depths of 12.5 feet and 17.6 feet beneath the existing ground surface, respectively. Additionally, readings from groundwater monitoring wells established on the site were taken on February 23, 2021. The locations of the accessible monitoring wells are indicated on the site plan (see Figure 2) and a summary of groundwater levels at the time of the investigation is provided in the table below.

Monitoring Well Readings

Well ID	MW-3	MW-4	MW-5	MW-7A	MW-8A	MW-9B
Depth to GW (Below Ground Surface)	12.0'	13.17'	12.25'	12.33'	12.67'	14.67'

Based on the depth to groundwater and the on-grade nature of the development, groundwater is not expected to have a detrimental effect on the project. Groundwater may be encountered during construction in deep drilled excavations, such as for ground improvement or elevator pistons. It is not uncommon for groundwater levels to vary seasonally or for groundwater seepage conditions to develop where none previously existed, especially in impermeable fine-grained soils which are heavily irrigated or after seasonal rainfall. In addition, recent requirements for stormwater infiltration could result in shallower seepage conditions in the immediate site vicinity. Proper surface drainage of irrigation and precipitation will be critical for future performance of the project. Recommendations for drainage are provided in the S*urface Drainage* section of this report (see Section 8.20).

7. GEOLOGIC HAZARDS

7.1 Surface Fault Rupture

The numerous faults in Southern California include Holocene-active, pre-Holocene, and inactive faults. The criteria for these major groups are based on criteria developed by the California Geological Survey (CGS, formerly known as CDMG) for the Alquist-Priolo Earthquake Fault Zone Program (CGS, 2018). By definition, a Holocene-active fault is one that has had surface displacement within Holocene time (about the last 11,700 years). A pre-Holocene fault has demonstrated surface displacement during Quaternary time (approximately the last 1.6 million years) but has had no known Holocene movement. Faults that have not moved in the last 1.6 million years are considered inactive.

The site is not within a state-designated Alquist-Priolo Earthquake Fault Zone for surface fault rupture hazards (CGS, 2021a; CGS, 2021b; CDMG 1986). No Holocene-active or pre-Holocene active faults with the potential for surface fault rupture are known to pass directly beneath the site. Therefore, the potential for surface rupture due to faulting occurring beneath the site during the design life of the proposed development is considered low. However, the site is located in the seismically active Southern California region, and could be subjected to moderate to strong ground shaking in the event of an earthquake on one of the many active Southern California faults. The faults in the vicinity of the site are shown in Figure 3, Regional Fault Map.

The closest surface trace of an active fault to the site is the Newport-Inglewood Fault Zone located approximately 2.7 miles to the east-northeast (USGS, 2006; CDMG, 1986). Other nearby active faults are the Palos Verdes Fault, the Cabrillo Fault, and the Whittier Fault located approximately 4.2 miles south-southwest, 8.2 miles south, and 16 miles northeast of the site, respectively. The active San Andreas Fault Zone is located approximately 48 miles northeast of the site.

Several buried thrust faults, commonly referred to as blind thrusts, underlie the Los Angeles Basin at depth. These faults are not exposed at the ground surface and are typically identified at depths greater than 3.0 kilometers. The October 1, 1987, M_w 5.9 Whittier Narrows earthquake and the January 17, 1994, M_w 6.7 Northridge earthquake were a result of movement on the Puente Hills Blind Thrust and the Northridge Thrust, respectively. These thrust faults and others in the Los Angeles area are not exposed at the surface and do not present a potential surface fault rupture hazard at the site; however, these deep thrust faults are considered active features capable of generating future earthquakes that could result in moderate to significant ground shaking at the site.

7.2 Seismicity

As with all of Southern California, the site has experienced historic earthquakes from various regional faults. The seismicity of the region surrounding the site was formulated based on research of an electronic database of earthquake data. The epicenters of recorded earthquakes with magnitudes equal to or greater than 5.0 in the site vicinity are depicted on Figure 4, Regional Seismicity Map. A partial list of moderate to major magnitude earthquakes that have occurred in the Southern California area within the last 100 years is included in the following table.

LIST OF HISTORIC EARTHQUAKES

Earthquake (Oldest to Youngest)	Date of Earthquake	Magnitude	Distance to Epicenter (Miles)	Direction to Epicenter
Near Redlands	July 23, 1923	6.3	59	E
Long Beach	March 10, 1933	6.4	22	SE
Tehachapi	July 21, 1952	7.5	91	NW
San Fernando	February 9, 1971	6.6	41	NNW
Whittier Narrows	October 1, 1987	5.9	19	NE
Sierra Madre	June 28, 1991	5.8	33	NE
Landers	June 28, 1992	7.3	107	ENE
Big Bear	June 28, 1992	6.4	85	ENE
Northridge	January 17, 1994	6.7	31	NW
Hector Mine	October 16, 1999	7.1	125	ENE
Ridgecrest	July 5, 2019	7.1	138	NNE

The site could be subjected to strong ground shaking in the event of an earthquake. However, this hazard is common in Southern California and the effects of ground shaking can be mitigated if the proposed structures are designed and constructed in conformance with current building codes and engineering practices.

7.3 Seismic Design Criteria

The following table summarizes the site-specific design criteria obtained from the 2019 California Building Code (CBC; Based on the 2018 International Building Code [IBC] and NEHRP-2015), Chapter 16 Structural Design, Section 1613, Earthquake Loads. The data was calculated using the online application *Seismic Design Maps*, provided by OSHPD. The short spectral response uses a period of 0.2 second. We evaluated the Site Class based on the discussion in Section 1613.2.2 of the 2019 CBC and Section 11.4.3 of NEHRP-2015. The values presented on the following page are for the risk-targeted maximum considered earthquake (MCE_R).

2019 CBC SEISMIC DESIGN PARAMETERS

Parameter	Value	2019 CBC Reference
Site Class	D	Section 1613.2.2
MCE_R Ground Motion Spectral Response Acceleration – Class B (short), S_S	1.711g	Figure 1613.2.1(1)
MCE_R Ground Motion Spectral Response Acceleration – Class B (1 sec), S_1	0.618g	Figure 1613.2.1(2)
Site Coefficient, F_A	1	Table 1613.2.3(1)
Site Coefficient, F_V	1.7*	Table 1613.2.3(2)
Site Class Modified MCE_R Spectral Response Acceleration (short), S_{MS}	1.711g	Section 1613.2.3 (Eqn 16-36)
Site Class Modified MCE_R Spectral Response Acceleration – (1 sec), S_{M1}	1.05g*	Section 1613.2.3 (Eqn 16-37)
5% Damped Design Spectral Response Acceleration (short), S_{DS}	1.141g	Section 1613.2.4 (Eqn 16-38)
5% Damped Design Spectral Response Acceleration (1 sec), S_{D1}	0.7g*	Section 1613.2.4 (Eqn 16-39)
Note: *Per Section 11.4.8 of ASCE/SEI 7-16, a ground motion hazard analysis shall be performed for projects for Site Class "E" sites with Ss greater than or equal to 1.0g and for Site Class "D" and "E" sites with S1 greater than 0.2g. Section 11.4.8 also provides exceptions which indicates that the ground motion hazard analysis may be waived provided the exceptions are followed. Using the code based values presented in the table above, in lieu of a performing a ground motion hazard analysis, requires the exceptions outlined in ASCE 7-16 Section 11.4.8 be followed.		

The table below presents the mapped maximum considered geometric mean (MCE_G) seismic design parameters for projects located in Seismic Design Categories of D through F in accordance with NEHRP-2015.

ASCE 7-16 PEAK GROUND ACCELERATION

Parameter	Value	ASCE 7-16 Reference
Mapped MCE_G Peak Ground Acceleration, PGA	0.748g	Figure 22-7
Site Coefficient, F_{PGA}	1.1	Table 11.8-1
Site Class Modified MCE_G Peak Ground Acceleration, PGA_M	0.823g	Section 11.8.3 (Eqn 11.8-1)

The Maximum Considered Earthquake Ground Motion (MCE) is the level of ground motion that has a 2 percent chance of exceedance in 50 years, with a statistical return period of 2,475 years. According to the 2019 California Building Code and ASCE 7-16, the MCE is to be utilized for the evaluation of liquefaction, lateral spreading, seismic settlements, and it is our understanding that the intent of the Building code is to maintain "Life Safety" during a MCE event. The Design Earthquake Ground Motion (DE) is the level of ground motion that has a 10 percent chance of exceedance in 50 years, with a statistical return period of 475 years.

Deaggregation of the MCE peak ground acceleration was performed using the USGS online Unified Hazard Tool, 2014 Conterminous U.S. Dynamic edition (v4.2.0). The result of the deaggregation analysis indicates that the predominant earthquake contributing to the MCE peak ground acceleration is characterized as a 6.87 magnitude event occurring at a hypocentral distance of 8.35 kilometers from the site.

Deaggregation was also performed for the Design Earthquake (DE) peak ground acceleration, and the result of the analysis indicates that the predominant earthquake contributing to the DE peak ground acceleration is characterized as a 6.68 magnitude occurring at a hypocentral distance of 13.48 kilometers from the site.

Conformance to the criteria in the above tables for seismic design does not constitute any kind of guarantee or assurance that significant structural damage or ground failure will not occur if a large earthquake occurs. The primary goal of seismic design is to protect life, not to avoid all damage, since such design may be economically prohibitive.

7.4 Liquefaction Potential

Liquefaction is a phenomenon in which loose, saturated, relatively cohesionless soil deposits lose shear strength during strong ground motions. Primary factors controlling liquefaction include intensity and duration of ground motion, gradation characteristics of the subsurface soils, in-situ stress conditions, and the depth to groundwater. Liquefaction is typified by a loss of shear strength in the liquefied layers due to rapid increases in pore water pressure generated by earthquake accelerations.

The current standard of practice, as outlined in the "Recommended Procedures for Implementation of DMG Special Publication 117, Guidelines for Analyzing and Mitigating Liquefaction in California" and "Special Publication 117A, Guidelines for Evaluating and Mitigating Seismic Hazards in California" requires liquefaction analysis to a depth of 50 feet below the lowest portion of the proposed structure. Liquefaction typically occurs in areas where the soils below the water table are composed of poorly consolidated, fine to medium-grained, primarily sandy soil. In addition to the requisite soil conditions, the ground acceleration and duration of the earthquake must also be of a sufficient level to induce liquefaction.

A review of the State of California Seismic Hazard Zone Map for the Torrance Quadrangle (CDMG, 1999) indicates that the site is located in an area designated as having a potential for liquefaction. Also, the City of Carson (2002) indicates the site is located within an area that has a potential for liquefaction.

The Standard Penetration Test (SPT) blow counts obtained from boring B3 were compared with the blow counts estimated from the CPT soundings. SPTs were performed in boring B3 at intervals of approximately 5 feet. In order to supplement the SPT blow count data, select California Modified Sampler blow count data were converted to equivalent SPT blow counts based on a correlation factor of 0.55 (Rogers, 2006). The field collected blow counts were corrected for hammer efficiency to N60 blow count values. The boring N60 values were compared with the N60 values generated by the program CpetIT (Version 3.2.1.7). The comparison of CPT-3 and boring B3 are shown as Figure 5. It is our opinion that the boring and CPT N60 values show a very reasonable correlation and that analysis of the liquefaction potential may be based on the CPT data.

Liquefaction analyses of the CPT soundings were performed using the program CLiq (Version 3.0.3.2). This program utilizes the 2001 NCEER method of analysis. This semi-empirical method is based on correlations with the data collected from the CPT soundings.

The liquefaction analysis was performed for a Design Earthquake level by using a historic groundwater level of 9 feet below the ground surface, a magnitude 6.68 earthquake, and a peak horizontal acceleration of 0.549g (⅔PGAM). The results of the enclosed liquefaction analyses included herein for CPTs 1 through 5 indicate that the alluvial soils below the design groundwater level could be susceptible to the liquefaction induced settlements summarized in the table below during Design Earthquake ground motion. A summary of the anticipated liquefaction induced settlements is provided as Figure 6; calculations and output from CLiq are provided as Appendix C.

Liquefaction Induced Settlements (Design Earthquake)

CPT Number	CPT-1	CPT-2	CPT-3	CPT-4	CPT-5
Liquefaction Settlement (in)	0.43	0.11	0.20	0.00	0.28

It is our understanding that the intent of the Building Code is to maintain "Life Safety" during Maximum Considered Earthquake level events. Therefore, additional analysis was performed to evaluate the potential for liquefaction during a MCE event. The structural engineer should evaluate the proposed structure for the anticipated MCE liquefaction induced settlements and verify that anticipated deformations would not cause the foundation system to lose the ability to support the gravity loads and/or cause collapse of the structure.

The liquefaction analysis performed for the Maximum Considered Earthquake level by using a historic groundwater level of 9 feet below the ground surface, a magnitude 6.87 earthquake, and a peak horizontal acceleration of 0.823g (PGAM). The results of the enclosed liquefaction analyses included herein for CPTs 1 through 5 indicate that the alluvial soils below the design groundwater level could be susceptible to the liquefaction induced settlements summarized in the table below during Maximum Considered Earthquake ground motion. A summary of the anticipated liquefaction induced settlements is provided as Figure 7.

Liquefaction Induced Settlements (Maximum Considered Earthquake)

CPT Number	CPT-1	CPT-2	CPT-3	CPT-4	CPT-4
Liquefaction Settlement (in)	0.80	0.19	0.33	0.00	0.41

7.5 Seismically Induced Settlement

Dynamic compaction of dry and loose sands may occur during a major earthquake. Typically, settlements occur in thick beds of such soils. The seismically induced settlement calculations were performed in accordance with the American Society of Civil Engineers, Technical Engineering and Design Guides as adapted from the US Army Corps of Engineers, No. 9.

The calculations provided herein in Figures 8 and 9 indicate that the soil above the historic high groundwater level of 9 feet would not be susceptible to significant settlement as a result of the Design Earthquake peak ground acceleration ($\frac{2}{3}PGA_M$).

7.6 Lateral Spreading

Due to the presence of the Dominguez Channel located to the west of the site, the potential for lateral spread was evaluated. Lateral spread occurs as a result of liquefaction induced lateral ground movement and typically occurs due to the presence of a slope comprised of and/or underlain by liquefiable soils.

Analysis of the potential for lateral spread was performed using the program CLiq (Version 1.7). The program utilizes the method proposed by Zhang et. al. (2004) to evaluate the potential for lateral spread and the resulting lateral displacements.

This method of analysis recommends evaluating the potential for lateral displacements to a distance of 50H from the slope, where H is the height of the slope. Beyond a horizontal distance of 50H lateral displacements due to the presence of a slope are not anticipated to occur. This method of analysis considers soils to a depth of twice the total slope height as potentially subject to lateral spread, up to a distance of 50H away from the toe of the slope.

The drainage channel is trapezoidal in shape and consists of two slopes approximately 12 feet in height inclined at a gradient of approximately 2:1 (estimated via satellite images). The proposed improvements have a minimum setback of 90 feet from the toe of the drainage channel. Therefore, lateral displacements using a horizontal setback of 90 feet was utilized.

Based on the results of the analyses it is anticipated that up to 10 inches of lateral displacements towards the drainage channel could occur during a Design Earthquake ground motion. The lateral displacements are anticipated to occur between depths of 10 and 15 feet below the ground surface. Calculations and output from CLiq are provided as Appendix C.

The grading and foundation design recommendations presented in this report are intended to minimize the effects of lateral spread on the proposed improvements.

7.7 Slope Stability

The topography at the site is relatively level and the topography in the immediate site vicinity slopes gently to the west-southwest. The County of Los Angeles Safety Element (Leighton, 1990) indicates the site is not located within an area identified as a "hillside area" or having a potential for slope instability. Additionally, the site is not within an area identified as having a potential for seismic slope instability (CDMG, 1999). There are no known landslides near the site, nor is the site in the path of any known or potential landslides. Therefore, the potential for slope stability hazards to adversely affect the proposed development is considered low.

7.8 Earthquake-Induced Flooding

Earthquake-induced flooding is inundation caused by failure of dams or other water-retaining structures due to earthquakes. Based on a review of the County of Los Angeles Safety Element (Leighton, 1990), the site is not located within a potential inundation area for an earthquake-induced dam failure. Therefore, the probability of earthquake-induced flooding is considered very low.

7.9 Tsunamis, Seiches, and Flooding

The site is not located within a coastal area. Therefore, tsunamis are not considered a significant hazard at the site.

Seiches are large waves generated in enclosed bodies of water in response to ground shaking. No major water-retaining structures are located immediately up gradient from the project site. Therefore, flooding resulting from a seismic-induced seiche is considered unlikely.

The site is within an area of minimal flooding (Zone X) as defined by the Federal Emergency Management Agency (FEMA, 2021; LACDPW, 2021).

7.10 Oil Fields & Methane Potential

Based on a review of the California Geologic Energy Management Division (CalGEM) Well Finder Website, the site is not located within an oil field and oil or gas wells are not documented in the immediate site vicinity (CalGEM, 2021). However, due to the voluntary nature of record reporting by the oil well drilling companies, wells may be improperly located or not shown on the location map and undocumented wells could be encountered during construction. Any wells encountered during construction will need to be properly abandoned in accordance with the current requirements of the CalGEM.

Since the site is not located within an oil field, the potential for methane or other volatile gases associated with oil and gas fields to be present at the site is considered low. However, as discussed in the Background section of this report (see Section 3), due to the site history there is a potential for low levels of volatile gases to be present, particularly during site grading. Should it be determined that a methane study or further environmental studies are required for the proposed development, it is recommended that a qualified methane or environmental consultant be retained to perform the study and provide mitigation measures as necessary.

7.11 Subsidence

Subsidence occurs when a large portion of land is displaced vertically, usually due to the withdrawal of groundwater, oil, or natural gas. Soils that are particularly subject to subsidence include those with high silt or clay content. The site is not located within an area of known ground subsidence. No large-scale extraction of groundwater, gas, oil, or geothermal energy is occurring or planned at the site or in the general site vicinity. There appears to be little or no potential for ground subsidence due to withdrawal of fluids or gases at the site.

8. CONCLUSIONS AND RECOMMENDATIONS

8.1 General

8.1.1 It is our opinion that neither soil nor geologic conditions were encountered during the investigation that would preclude construction of the proposed development provided the recommendations presented herein are followed and implemented during design and construction.

8.1.2 Up to 5 feet of existing artificial fill was encountered during the site investigation with localized areas of deeper fill of to 9 feet in depth. The existing fill encountered is believed to be the result of past grading and construction activities at the site. Deeper fill may exist in other areas of the site that were not directly explored. It is our opinion that the existing fill, in its present condition, is not suitable for direct support of proposed foundations or slabs. The existing fill and site soils are suitable for re-use as engineered fill provided the recommendations in the Grading section of this report are followed (see Section 8.4).

8.1.3 The enclosed liquefaction and seismically-induced settlement analyses indicate that the site soils could be susceptible to approximately ½ inch of total settlement as a result of the Design Earthquake peak ground acceleration ($\frac{2}{3}PGA_M$). Differential settlement at the foundation level is anticipated to be less than ¼ inch over a distance of 20 feet.

8.1.4 The results of the field data and laboratory testing indicate that the upper alluvial soils are relatively soft and compressible in their current condition (see Figure B5 thru B17) and could yield excessive static and differential settlements upon application of foundation loads.

8.1.5 The foundation design recommendations presented herein are intended to minimize the effects of settlement from liquefaction and consolidation on the proposed improvements. Based on our discussions with you, we understand that the preferred foundation system is a reinforced concrete mat foundation deriving support in newly placed engineered fill. Recommendations for a reinforced mat foundation system is provided in Sections 8.7 of this report.

8.1.6 For support of a mat foundation, it is recommended that the upper 6 feet of existing earth materials within the proposed building footprint areas be excavated and properly compacted for foundation and slab support. Deeper excavations should be conducted as necessary to remove deeper artificial fill or soft alluvial soil at the direction of the Geotechnical Engineer (a representative of Geocon). Proposed building foundations should be underlain by a minimum of 4 feet of newly placed engineered fill. The excavation should extend laterally a minimum distance of 3 feet beyond the building footprint area, including building appurtenances, or a distance equal to the depth of fill below the foundation, whichever is greater. The contractor should be aware that up to 9 feet of artificial fill was encountered in Boring B3. The limits of existing fill and/or soft alluvial soils removal will be verified by the Geocon representative during site grading activities. All excavations must be observed and approved in writing by the Geotechnical Engineer (a representative of Geocon).

8.1.7 It is anticipated that the recommended grading can be achieved with sloping measures. However, if excavations in close proximity to an adjacent property line and/or structure are required, special excavation measures in order to maintain lateral support of existing adjacent improvements will be required. Excavation recommendations are provided in the *Temporary Excavations* section of this report (Section 8.18).

8.1.8 Based on the relatively shallow groundwater table, the upper alluvial soils have the potential to be very moist and the grading contractor should be aware that the soils may be above optimum moisture content. If the soils are more than 3 percent above the optimum moisture content at the time of construction the soils will likely require some spreading and drying activities in order to achieve proper compaction. Bottom stabilization may also be necessary. Recommendations for bottom stabilization and earthwork are provided in the *Grading* section of this report (see Section 8.4).

8.1.9 Foundations for small outlying structures, such as block walls up to 6 feet in height, planter walls or trash enclosures, which will not be tied to the proposed structure, may be supported on conventional foundations deriving support on a minimum of 12 inches of newly placed engineered fill which extends laterally at least 12 inches beyond the foundation area. Where excavation and compaction cannot be performed or is undesirable, foundations may derive support directly in the competent undisturbed alluvial soils and should be deepened as necessary to maintain a minimum 12 inch embedment into the recommended bearing materials. If the soils exposed in the excavation bottom are soft or loose, compaction of the soils will be required prior to placing steel or concrete. Compaction of the foundation excavation bottom is typically accomplished with a compaction wheel or mechanical whacker and must be observed and approved in writing by a Geocon representative.

8.1.10 Where new paving is to be placed, it is recommended that all existing fill and soft alluvial soils be excavated and properly compacted for paving support. The client should be aware that excavation and compaction of all existing fill and soft alluvial soils in the area of new paving is not required; however, paving constructed over existing uncertified fill or unsuitable alluvial soil may experience increased settlement and/or cracking, and may therefore have a shorter design life and increased maintenance costs. As a minimum, the upper 12 inches of subgrade soil should be scarified and properly compacted for paving support. Paving recommendations are provided in *Preliminary Pavement Recommendations* section of this report (see Section 8.13).

8.1.11 Based on the shallow groundwater and impermeable nature of the fine grained soils which underly the site, infiltration of stormwater at this site is not considered feasible. Infiltration of stormwater at this site would be considered detrimental to the project. It is recommended that stormwater be retained, filtered, and discharged in accordance with the requirements of the local governing agency.

8.1.12 It should be noted that implementation of the recommendations presented herein is not intended to completely prevent damage to the structure during the occurrence of strong ground shaking as a result of nearby earthquakes. It is intended that the structure be designed in such a way that the amount of damage incurred as a result of strong ground shaking be minimized.

8.1.13 It is recommended that flexible utility connections be utilized for all rigid utilities to minimize or prevent damage to utilities from minor differential movements.

8.1.14 Once the design and foundation loading configuration for the proposed structure proceeds to a more finalized plan, the recommendations within this report should be reviewed and revised, if necessary. Based on the final foundation loading configurations, the potential for settlement should be reevaluated by this office.

8.1.15 Any changes in the design, location or elevation of improvements, as outlined in this report, should be reviewed by this office. Geocon should be contacted to determine the necessity for review and possible revision of this report.

8.2 Soil and Excavation Characteristics

8.2.1 The in-situ soils can be excavated with moderate effort using conventional excavation equipment. Some caving should be anticipated in unshored excavations, especially where granular soils are encountered.

8.2.2 It is the responsibility of the contractor to ensure that all excavations and trenches are properly shored and maintained in accordance with applicable OSHA rules and regulations to maintain safety and maintain the stability of existing adjacent improvements.

8.2.3 All onsite excavations must be conducted in such a manner that potential surcharges from existing structures, construction equipment, and vehicle loads are resisted. The surcharge area may be defined by a 1:1 projection down and away from the bottom of an existing foundation or vehicle load. Penetrations below this 1:1 projection will require special excavation measures such as sloping or shoring. Excavation recommendations are provided in the *Temporary Excavations* section of this report (see Section 8.18).

8.2.4 The upper 5 feet of existing site soils encountered during the investigation are considered to have a "medium" expansive potential (EI = 63) and are classified as "expansive" in accordance with the 2019 California Building Code (CBC) Section 1803.5.3. The recommendations presented herein assume that the building foundations and slabs will derive support in these materials.

8.3 Minimum Resistivity, pH, and Water-Soluble Sulfate

8.3.1 Potential of Hydrogen (pH) and resistivity testing, as well as chloride content testing, were performed on representative samples of on-site material to generally evaluate the corrosion potential to surface utilities. The tests were performed in accordance with California Test Method Nos. 643 and 422 and indicate that the soils are considered "moderately corrosive" to "severely corrosive" with respect to corrosion of buried ferrous metals on site. The results are presented in Appendix B (Figure B23) and should be considered for design of underground structures. Due to the corrosive potential of the soils, it is suggested that ABS pipes be considered in lieu of cast-iron for subdrains and retaining wall drains beneath the structure.

8.3.2 Laboratory tests were performed on representative samples of the site materials to measure the percentage of water-soluble sulfate content. Results from the laboratory water-soluble sulfate tests are presented in Appendix B (Figure B23) and indicate that the on-site materials possess a sulfate exposure class of "S0" to concrete structures as defined by 2019 CBC Section 1904 and ACI 318-14 Table 19.3.1.1.

8.3.3 Geocon West, Inc. does not practice in the field of corrosion engineering and mitigation. If corrosion sensitive improvements are planned, it is recommended that a corrosion engineer be retained to evaluate corrosion test results and incorporate the necessary precautions to avoid premature corrosion of buried metal pipes and concrete structures in direct contact with the soils.

8.4 Grading

8.4.1 Grading is anticipated to include preparation of building pads and paving subgrade, excavation of site soils for proposed foundations and utility trenches, as well as placement of backfill for utility trenches.

8.4.2 A preconstruction conference should be held at the site prior to the beginning of grading operations with the owner, contractor, civil engineer and soil engineer in attendance. Special soil handling requirements can be discussed at that time.

8.4.3 Earthwork should be observed, and compacted fill tested by representatives of Geocon West, Inc. The existing fill and alluvial soils encountered during exploration are suitable for reuse as engineered fill, provided any encountered oversize material (greater than 6 inches) and any encountered deleterious debris is removed.

8.4.4 Grading should commence with the removal of all existing vegetation and existing improvements from the area to be graded. Deleterious debris such as wood and root structures should be exported from the site and should not be mixed with the fill soils. Asphalt and concrete should not be mixed with the fill soils unless approved by the Geotechnical Engineer. All existing underground improvements planned for removal should be completely excavated and the resulting depressions properly backfilled in accordance with the procedures described herein. Once a clean excavation bottom has been established it must be observed and approved in writing by the Geotechnical Engineer (a representative of Geocon West, Inc.).

8.4.5 For support of a mat foundation, it is recommended that the upper 6 feet of existing earth materials within the proposed building footprint areas be excavated and properly compacted for foundation and slab support. Deeper excavations should be conducted as necessary to remove deeper artificial fill or soft alluvial soil at the direction of the Geotechnical Engineer (a representative of Geocon). Proposed building foundations should be underlain by a minimum of 4 feet of newly placed engineered fill. The excavation should extend laterally a minimum distance of 3 feet beyond the building footprint area, including building appurtenances, or a distance equal to the depth of fill below the foundation, whichever is greater. The contractor should be aware that up to 9 feet of artificial fill was encountered in Boring B3. The limits of existing fill and/or soft alluvial soils removal will be verified by the Geocon representative during site grading activities.

8.4.6 All excavations must be observed and approved in writing by the Geotechnical Engineer (a representative of Geocon). If determined to be excessively soft, stabilization of the bottom of the excavation may be required in order to provide a firm working surface upon which engineered fill can be placed and heavy equipment can operate.

8.4.7 Prior to placing fill or constructing proposed improvements, a stable excavation bottom must be established. In areas where the subgrade is saturated or soft, proper compaction will likely not be possible or achieved in a timely manner without introducing stabilization measures. If subgrade stabilization is required at the excavation bottom, rubber tire equipment should not be allowed in the excavation bottom until it is stabilized or extensive soil disturbance could result. It is suggested that excavation and grading be performed during the summer season to promote moisture control of the soils. In addition, the use of track equipment should be used to minimize disturbance to the soils at the excavation bottom.

8.4.8 Bottom stabilization, if necessary, may be achieved placing a thin lift of 3- to 6-inch-diameter crushed angular rock into the soft excavation bottom. The use of crushed concrete will also be acceptable. The crushed rock should be spread thinly across the excavation bottom and pressed into the soils by track rolling or wheel rolling with heavy equipment. It is very important that voids between the rock fragments are not created so the rock must be thoroughly pressed or blended into the soils. All subgrade soils must be properly compacted and proof-rolled in the presence of the Geotechnical Engineer (a representative of Geocon West, Inc.).

8.4.9 An alternative method of subgrade stabilization may be accomplished by placing a one-foot-thick layer of washed, angular 3/4-inch gravel atop a stabilization fabric (Mirafi 500X or equivalent) subsequent to subgrade approval. Stabilization fabric should also be placed over the top of the gravel. This procedure should be conducted in sections until the entire excavation bottom has been blanketed by fabric and gravel. Heavy equipment may operate on the gravel once it has been placed. The gravel should be compacted to a dense state using a vibratory drum roller. It is recommended that the contractor meet with the Geotechnical Engineer to discuss this procedure in more detail.

8.4.10 The upper soils encountered during site exploration were moist to wet and the grading contractor should be aware that the existing soils are currently above optimum moisture content. Conditions could change seasonally. If the soils are more than 3 percent above the optimum moisture content at the time of construction the soils will likely require spreading, processing, and drying activities in order to achieve proper compaction.

8.4.11 All fill and backfill soils should be placed in horizontal loose layers approximately 6 to 8 inches thick, moisture conditioned to near 2 percent above optimum moisture content, and properly compacted to a minimum of 90 percent of the maximum dry density per ASTM D 1557 (latest edition).

8.4.12 It is anticipated that stable excavations for the recommended grading can be achieved with sloping measures. However, if excavations in close proximity to an adjacent property line and/or structure are required, special excavation measures may be necessary in order to maintain lateral support of offsite improvements. Excavation recommendations are provided in the *Temporary Excavations* section of this report (see Section 8.18).

8.4.13 Although not anticipated for this project, all imported fill shall be observed, tested, and approved by Geocon West, Inc. prior to bringing soil to the site. Rocks larger than 6 inches in diameter shall not be used in the fill. If necessary, import soils used as structural fill should have an expansion index less than 50 and corrosivity properties that are equally or less detrimental to that of the existing onsite soils (see Figure B23).

8.4.14. Where new paving is to be placed, it is recommended that all existing fill and soft alluvium be excavated and properly compacted for paving support. As a minimum, the upper 12 inches of soil should be scarified, moisture conditioned to near two percent over optimum moisture content, and compacted to at least 92 percent relative compaction, as determined by ASTM Test Method D 1557 (latest edition). Paving recommendations are provided in *Preliminary Pavement Recommendations* section of this report (see Section 8.13).

8.4.15 Foundations for small outlying structures, such as block walls up to 6 feet in height, planter walls or trash enclosures, which will not be tied to the proposed structure, may be supported on conventional foundations deriving support on a minimum of 12 inches of newly placed engineered fill which extends laterally at least 12 inches beyond the foundation area. Where excavation and compaction cannot be performed or is undesirable, foundations may derive support directly in the competent undisturbed alluvial soils and should be deepened as necessary to maintain a minimum 12 inch embedment into the recommended bearing materials. If the soils exposed in the excavation bottom are soft or loose, compaction of the soils will be required prior to placing steel or concrete. Compaction of the foundation excavation bottom is typically accomplished with a compaction wheel or mechanical whacker and must be observed and approved by a Geocon representative.

8.4.16 It is recommended that flexible utility connections be utilized for all rigid utilities to minimize or prevent damage to utilities from minor differential movements. Utility trenches should be properly backfilled in accordance with the requirements of the Green Book (latest edition). The pipe should be bedded with clean sands (Sand Equivalent greater than 30) to a depth of at least 1 foot over the pipe, and the bedding material must be inspected and approved in writing by the Geotechnical Engineer (a representative of Geocon). The use of gravel is not acceptable unless used in conjunction with filter fabric to prevent the gravel from having direct contact with soil. The remainder of the trench backfill may be derived from onsite soil or approved import soil, compacted as necessary, until the required compaction is obtained. The use of minimum 2-sack slurry as backfill is also acceptable. Prior to placing any bedding materials or pipes, the trench excavation bottom must be observed and approved in writing by the Geotechnical Engineer (a representative of Geocon).

8.4.17 All trench and foundation excavation bottoms must be observed and approved in writing by the Geotechnical Engineer (a representative of Geocon), prior to placing bedding sands, fill, steel, gravel, or concrete.

8.5 Shrinkage

8.5.1 Shrinkage results when a volume of material removed at one density is compacted to a higher density. A shrinkage factor between 10 and 15 percent should be anticipated when excavating and compacting the upper 5 feet of existing earth materials on the site to an average relative compaction of 92 percent.

8.5.2 If import soils will be utilized in the building pad, the soils must be placed uniformly and at equal thickness at the direction of the Geotechnical Engineer (a representative of Geocon West, Inc.). Soils can be borrowed from non-building pad areas and later replaced with imported soils.

8.6 Mat Foundation Design

8.6.1 Subsequent to the recommended grading, a reinforced concrete mat foundation may be utilized for support of the proposed structures. The reinforced concrete mat foundation should derive support in the newly placed engineered fill and be underlain by at least 4 feet of newly placed engineered fill.

8.6.2 Foundation excavations should be observed and approved in writing by the Geotechnical Engineer (a representative of Geocon West, Inc.), prior to the placement of reinforcing steel and concrete to verify that the excavations and exposed soil conditions are consistent with those anticipated. If unanticipated soil conditions are encountered, foundation modifications may be required.

8.6.3 It is anticipated that the mat foundation constructed for the on-grade structure will impart an average pressure between 2,000 psf to 3,500 psf. The recommended maximum allowable bearing value is 3,500 psf. The allowable bearing pressure may be increased by up to one-third for transient loads due to wind or seismic forces.

8.6.4 A vertical modulus of subgrade reaction of 100 pci may be used in the design of mat foundations deriving support in competent alluvial soils. This value is a unit value for use with a 1-foot square footing. The modulus should be reduced in accordance with the following equation when used with larger foundations:

$$K_R = K\left[\frac{B+1}{2B}\right]^2$$

where: K_R = reduced subgrade modulus
K = unit subgrade modulus
B = foundation width (in feet)

8.6.5 The thickness of and reinforcement for the mat foundation should be designed by the project structural engineer.

8.6.6 For seismic design purposes, a coefficient of friction of 0.35 may be utilized between the concrete mat and newly placed engineered fill without a moisture barrier, and 0.15 for slabs underlain by a moisture barrier.

8.6.7 The enclosed liquefaction settlement analyses indicate that the site soils could be susceptible to less than ½ inch of total seismic settlement as a result of the Design Earthquake peak ground acceleration ($⅔PGA_M$). Differential settlement at the foundation level is anticipated to be less than ¼ inches over a distance of 20 feet. The foundation design recommendations presented herein are intended to minimize the effects of settlement on proposed improvements.

8.6.8 The maximum expected total settlement for a structure support on a mat foundation system designed with the maximum allowable bearing value of 3,500 psf and deriving support in the recommended bearing materials is estimated to be approximately 2 inches and occur below the heaviest loaded structural element. A majority of the settlement of the foundation system is expected to occur on initial application of loading; however, additional settlements are expected within the first twelve months. Differential settlement is not expected to exceed 1 inch over a distance of 20 feet.

8.6.9 Based on these considerations is it recommended that the proposed structure, designed with a maximum allowable bearing value of 3,500 psf, be designed for a combined static and seismically induced differential settlement of 1 ½ inch over a distance of 20 feet.

8.6.10 This office should be provided a copy of the final construction plans so that the excavation recommendations presented herein could be properly reviewed and revised if necessary.

8.6.11 Once the design and foundation loading configurations for the proposed structures proceeds to a more finalized plan, the estimated settlements presented in this report should be reviewed and revised, if necessary. If the final foundation loading configurations are greater than the assumed loading conditions, the potential for settlement should be reevaluated by this office.

8.7 Miscellaneous Foundations

8.7.1 Foundations for small outlying structures, such as block walls up to 6 feet in height, planter walls or trash enclosures, which will not be tied to the proposed structure, may be supported on conventional foundations deriving support on a minimum of 12 inches of newly placed engineered fill which extends laterally at least 12 inches beyond the foundation area. Where excavation and compaction cannot be performed or is undesirable, foundations may derive support directly in the competent undisturbed alluvial soils, and should be deepened as necessary to maintain a minimum 12 inch embedment into the recommended bearing materials.

8.7.2 If the soils exposed in the excavation bottom are soft, compaction of the soft soils will be required prior to placing steel or concrete. Compaction of the foundation excavation bottom is typically accomplished with a compaction wheel or mechanical whacker and must be observed and approved by a Geocon representative. Miscellaneous foundations may be designed for a bearing value of 1,500 psf, and should be a minimum of 12 inches in width, 24 ,inches in depth below the lowest adjacent grade and 12 inches into the recommended bearing material. The allowable bearing pressure may be increased by up to one-third for transient loads due to wind or seismic forces.

8.7.3 Foundation excavations should be observed and approved in writing by the Geotechnical Engineer (a representative of Geocon West, Inc.), prior to the placement of reinforcing steel and concrete to verify that the excavations and exposed soil conditions are consistent with those anticipated.

8.8 Lateral Design

8.8.1 Resistance to lateral loading may be provided by friction acting at the base of foundations, slabs and by passive earth pressure. An allowable coefficient of friction of 0.35 may be used with the dead load forces in the undisturbed alluvial soils and newly placed engineered fill.

8.8.2 Passive earth pressure for the sides of foundations and slabs poured against newly placed engineered fill or undisturbed alluvial soils may be computed as an equivalent fluid having a density of 230 pounds per cubic foot (pcf) with a maximum earth pressure of 2,300 psf. When combining passive and friction for lateral resistance, the passive component should be reduced by one-third. A one-third increase in the passive value may be used for wind or seismic loads.

8.9 Concrete Slabs-on-Grade

8.9.1 Exterior concrete slabs-on-grade subject to vehicle loading should be designed in accordance with the recommendations in the *Preliminary Pavement Recommendations* section of this report (Section 8.10).

8.9.2 Slabs-on-grade at the ground surface that may receive moisture-sensitive floor coverings or may be used to store moisture-sensitive materials should be underlain by a vapor retarder placed directly beneath the slab. The vapor retarder and acceptable permeance should be specified by the project architect or developer based on the type of floor covering that will be installed. The vapor retarder design should be consistent with the guidelines presented in Section 9.3 of the American Concrete Institute's (ACI) Guide for Concrete Slabs that Receive Moisture-Sensitive Flooring Materials (ACI 302.2R-06) and should be installed in general conformance with ASTM E 1643 (latest edition) and the manufacturer's recommendations. A minimum thickness of 15 mils extruded polyolefin plastic is recommended; vapor retarders which contain recycled content or woven materials are not recommended. The vapor retarder should have a permeance of less than 0.01 perms demonstrated by testing before and after mandatory conditioning. The vapor retarder should be installed in direct contact with the concrete slab with proper perimeter seal. If the Los Angeles Green Building Code requirements apply to this project, the vapor retarder should be underlain by 4 inches of clean aggregate. It is important that the vapor retarder be puncture resistant since it will be in direct contact with angular gravel. As an alternative to the clean aggregate suggested in the Los Angeles Green Building Code, it is our opinion that the concrete slab-on-grade may be underlain by a vapor retarder over 4 inches of clean sand (sand equivalent greater than 30), since the sand will serve a capillary break and will minimize the potential for punctures and damage to the vapor barrier.

8.9.3 For seismic design purposes, a coefficient of friction of 0.35 may be utilized between concrete slabs and subgrade soils without a moisture barrier, and 0.15 for slabs underlain by a moisture barrier.

8.9.4 Exterior slabs, not subject to traffic loads, should be at least 4 inches thick and reinforced with No. 3 steel reinforcing bars placed 18 inches on center in both horizontal directions, positioned near the slab midpoint. Prior to construction of slabs, the upper 12 inches of subgrade should be moistened to optimum moisture content and properly compacted to at least 92 percent relative compaction, as determined by ASTM Test Method D 1557 (latest edition). Crack control joints should be spaced at intervals not greater than 10 feet and should be constructed using saw-cuts or other methods as soon as practical following concrete placement. Crack control joints should extend a minimum depth of one-fourth the slab thickness. The project structural engineer should design construction joints as necessary.

8.9.5 Due to the expansive potential of the anticipated subgrade soils, the moisture content of the slab subgrade should be maintained and sprinkled as necessary to maintain a moist condition as would be expected in any concrete placement. Furthermore, consideration should be given to doweling slabs into adjacent curbs and foundations to minimize movements and offsets which could lead to a potential tripping hazard.

8.9.6 The recommendations of this report are intended to reduce the potential for cracking of slabs due to settlement. However, even with the incorporation of the recommendations presented herein, foundations, stucco walls, and slabs-on-grade may exhibit some cracking due to minor soil movement and/or concrete shrinkage. The occurrence of concrete shrinkage cracks is independent of the supporting soil characteristics. Their occurrence may be reduced and/or controlled by limiting the slump of the concrete, proper concrete placement and curing, and by the placement of crack control joints at periodic intervals, in particular, where re-entrant slab corners occur.

8.10 Preliminary Paving Design

8.10.1 Where new paving is to be placed, it is recommended that all existing fill and soft alluvium materials be excavated and properly compacted for paving support. The client should be aware that excavation and compaction of all existing artificial fill and soft alluvium in the area of new paving is not required; however, paving constructed over existing uncertified fill or unsuitable alluvium material may experience increased settlement and/or cracking, and may therefore have a shorter design life and increased maintenance costs. As a minimum, the upper 12 inches of paving subgrade should be scarified, moisture conditioned to at least 2 percent above optimum moisture content, and properly compacted to at least 92 percent relative compaction, as determined by ASTM Test Method D 1557 (latest edition).

8.10.2 The following pavement sections are based on an assumed R-Value of 20. Once site grading activities are complete an R-Value should be obtained by laboratory testing to confirm the properties of the soils serving as paving subgrade, prior to placing pavement.

8.10.3 The Traffic Indices listed below are estimates. Geocon does not practice in the field of traffic engineering. The actual Traffic Index for each area should be determined by the project civil engineer. If pavement sections for Traffic Indices other than those listed below are required, Geocon should be contacted to provide additional recommendations. Pavement thicknesses were determined following procedures outlined in the *California Highway Design Manual* (Caltrans). It is anticipated that the majority of traffic will consist of automobile and large truck traffic.

PRELIMINARY PAVEMENT DESIGN SECTIONS

Location	Estimated Traffic Index (TI)	Asphalt Concrete (inches)	Class 2 Aggregate Base (inches)
Automobile Parking and Driveways	4.0	3.0	4.0
Trash Truck & Fire Lanes	7.0	4.0	12.0

8.10.4 Asphalt concrete should conform to Section 203-6 of the "*Standard Specifications for Public Works Construction"* (Green Book). Class 2 aggregate base materials should conform to Section 26-1.02A of the "*Standard Specifications of the State of California, Department of Transportation"* (Caltrans). The use of Crushed Miscellaneous Base (CMB) in lieu of Class 2 aggregate base is acceptable. Crushed Miscellaneous Base should conform to Section 200-2.4 of the "*Standard Specifications for Public Works Construction"* (Green Book).

8.10.5 Unless specifically designed and evaluated by the project structural engineer, where exterior concrete paving will be utilized for support of vehicles, it is recommended that the concrete be a minimum of 6 inches of concrete reinforced with No. 3 steel reinforcing bars placed 18 inches on center in both horizontal directions. Concrete paving supporting vehicular traffic should be underlain by a minimum of 4 inches of aggregate base and a properly compacted subgrade. As a minimum, the upper 12 inches of paving subgrade should be scarified, moisture conditioned to 2 percent above optimum moisture content, and properly compacted to at least 92 percent relative compaction, as determined by ASTM Test Method D 1557 (latest edition). The base material should be compacted to 95 percent relative compaction as determined by ASTM Test Method D 1557 (latest edition).

8.10.6 The performance of pavements is highly dependent upon providing positive surface drainage away from the edge of pavements. Ponding of water on or adjacent to the pavement will likely result in saturation of the subgrade materials and subsequent cracking, subsidence and pavement distress. If planters are planned adjacent to paving, it is recommended that the perimeter curb be extended at least 12 inches below the bottom of the aggregate base to minimize the introduction of water beneath the paving.

8.11 Retaining Wall Design

8.11.1 The recommendations presented below are generally applicable to the design of rigid concrete or masonry retaining walls having a maximum height of 5 feet. In the event that walls significantly higher than 5 feet are planned, Geocon should be contacted for additional recommendations.

8.11.2 Retaining wall foundations should be designed in accordance with the recommendations provided in the *Foundation Design* section of this report (see Sections 8.6 through 8.9).

8.11.3 Retaining walls with a level backfill surface that are not restrained at the top should be designed utilizing a triangular distribution of pressure (active pressure). Restrained walls are those that are not allowed to rotate more than 0.001H (where H equals the height of the retaining portion of the wall in feet) at the top of the wall. Where walls are restrained from movement at the top, walls may be designed utilizing a triangular distribution of pressure (at-rest pressure). The table on the following page presents recommended pressures to be used in retaining wall design.

RETAINING WALL WITH LEVEL BACKFILL SURFACE

HEIGHT OF RETAINING WALL (Feet)	ACTIVE PRESSURE EQUIVALENT FLUID PRESSURE (Pounds Per Cubic Foot)	AT-REST PRESSURE EQUIVALENT FLUID PRESSURE (Pounds Per Cubic Foot)
Up to 5	30	74

8.11.4 The wall pressures provided above assume that the proposed retaining walls will support a wedge of engineered fill derived from onsite soils. If import soil will be used to backfill proposed retaining walls, revised earth pressures may be required to account for the geotechnical properties of the import soil used as engineered fill. This should be evaluated once the use of import soil is established. All imported fill shall be observed, tested, and approved by Geocon West, Inc. prior to bringing soil to the site.

8.11.5 The wall pressures provided above assume that the retaining wall will be properly drained preventing the buildup of hydrostatic pressure. If retaining wall drainage is not implemented, the equivalent fluid pressure to be used in design of undrained walls is 100 pcf. The value includes hydrostatic pressures plus buoyant lateral earth pressures.

8.11.6 Additional active pressure should be added for a surcharge condition due to sloping ground, vehicular traffic or adjacent structures and should be designed for each condition as the project progresses. Surcharges may be evaluated using Section 8.19 of this report. Once the design becomes more finalized, an addendum letter can be prepared revising recommendations and addressing specific surcharge conditions throughout the project, if necessary.

8.12 Retaining Wall Drainage

8.12.1 Where not designed for hydrostatic pressure, retaining walls should be provided with a drainage system. At the base of the drain system, a subdrain covered with a minimum of 12 inches of gravel should be installed, and a compacted fill blanket or other seal placed at the surface (see Figure 10). The clean bottom and subdrain pipe, behind a retaining wall, should be observed by the Geotechnical Engineer (a representative of Geocon), prior to placement of gravel or compacting backfill.

8.12.2 As an alternative, a plastic drainage composite such as Miradrain or equivalent may be installed in continuous, 4-foot-wide columns along the entire back face of the wall, at 8 feet on center. The top of these drainage composite columns should terminate approximately 18 inches below the ground surface, where either hardscape or a minimum of 18 inches of relatively cohesive material should be placed as a cap (see Figure 11). These vertical columns of drainage material would then be connected at the bottom of the wall to a collection panel or a 1-cubic-foot rock pocket drained by a 4-inch subdrain pipe.

8.12.3 Subdrainage pipes at the base of the retaining wall drainage system should outlet to an acceptable location via controlled drainage structures.

8.12.4 Moisture affecting below grade walls is one of the most common post-construction complaints. Poorly applied or omitted waterproofing can lead to efflorescence or standing water. Particular care should be taken in the design and installation of waterproofing to avoid moisture problems, or actual water seepage into the structure through any normal shrinkage cracks which may develop in the concrete walls, floor slab, foundations and/or construction joints. The design and inspection of the waterproofing is not the responsibility of the geotechnical engineer. A waterproofing consultant should be retained in order to recommend a product or method, which would provide protection to subterranean walls, floor slabs and foundations.

8.13 Elevator Pit Design

8.13.1 The elevator pit slab and retaining wall should be designed by the project structural engineer. Elevator pit walls may be designed in accordance with the recommendations in the *Retaining Wall Design* section of this report (see Section 8.14).

8.13.2 Additional active pressure should be added for a surcharge condition due to sloping ground, vehicular traffic or adjacent foundations and should be designed for each condition as the project progresses.

8.13.3 If retaining wall drainage is to be provided, the drainage system should be designed in accordance with the *Retaining Wall Drainage* section of this report (see Section 8.15).

8.13.4 It is suggested that the exterior walls and slab be waterproofed to prevent excessive moisture inside of the elevator pit. Waterproofing design and installation is not the responsibility of the geotechnical engineer.

8.14 Elevator Piston

8.14.1 If a plunger-type elevator piston is installed for this project, a deep drilled excavation will be required. It is important to verify that the drilled excavation is not situated immediately adjacent to a foundation, or the drilled excavation could compromise the existing foundation support, especially if the drilling is performed subsequent to the foundation construction.

8.14.2 Due to the preliminary nature of the project at this time, it is unknown if a plunger-type elevator piston will be included for this project. If in the future it is determined that a plunger-type elevator piston will be constructed, the location of the proposed elevator should be reviewed by the Geotechnical Engineer to evaluate the setback from foundations. Additional recommendations will be provided as necessary.

8.14.3 Some caving is anticipated in the granular soils below a depth of 20 feet. The contractor should be prepared to use casing and should have it readily available at the commencement of drilling activities. Continuous observation of the drilling and installation of the elevator piston by the Geotechnical Engineer (a representative of Geocon West, Inc.) is required.

8.14.4 The annular space between the piston casing and drilled excavation wall should be filled with a minimum of 1½-sack slurry pumped from the bottom up. As an alternative, pea gravel may be utilized. The use of soil to backfill the annular space is not acceptable.

8.15 Temporary Excavations

8.15.1 Excavations on the order of 6 feet in height are generally anticipated during grading activities, and isolated excavations up to 9 feet in height may also be required. The excavations are expected to expose artificial fill and alluvial soils, which may be subject to some caving where granular soils are exposed. Temporary vertical excavations up to 5 feet in height may be attempted where not surcharged by adjacent traffic or structures.

8.15.2 Vertical excavations greater than 5 feet or where surcharged by existing structures will require sloping or shoring measures in order to provide a stable excavation. Where sufficient space is available, temporary unsurcharged embankments could be sloped back at a uniform 1:1 slope gradient or flatter up to a maximum of 9 feet in height. A uniform slope does not have a vertical portion. Where space is limited, shoring measures will be required. *Shoring* recommendations can be provided under separate cover if necessary.

8.15.3 If excavations in close proximity to an adjacent property line and/or structure are required, special excavation measures such as slot-cutting or shoring may be necessary in order to maintain lateral support of offsite improvements. Recommendations for slot-cutting and shoring can be provided under separate cover.

8.15.4 Where sloped embankments are utilized, the top of the slope should be barricaded to prevent vehicles and storage loads at the top of the slope within a horizontal distance equal to the height of the slope. If the temporary construction embankments are to be maintained during the rainy season, berms are suggested along the tops of the slopes where necessary to prevent runoff water from entering the excavation and eroding the slope faces. Geocon personnel should inspect the soils exposed in the cut slopes during excavation so that modifications of the slopes can be made if variations in the soil conditions occur. All excavations should be stabilized within 30 days of initial excavation.

8.16 Surcharge from Adjacent Structures and Improvements

8.16.1 Additional pressure should be added for a surcharge condition due to sloping ground, vehicular traffic or adjacent structures and should be designed for each condition as the project progresses.

8.16.2 It is recommended that line-load surcharges from adjacent wall footings, use horizontal pressures generated from NAV-FAC DM 7.2. The governing equations are:

$$For\ {}^{x}/_{H} \leq 0.4$$

$$\sigma_H(z) = \frac{0.20 \times \left(\frac{z}{H}\right)}{\left[0.16 + \left(\frac{z}{H}\right)^2\right]^2} \times \frac{Q_L}{H}$$

and

$$For\ {}^{x}/_{H} > 0.4$$

$$\sigma_H(z) = \frac{1.28 \times \left(\frac{x}{H}\right)^2 \times \left(\frac{z}{H}\right)}{\left[\left(\frac{x}{H}\right)^2 + \left(\frac{z}{H}\right)^2\right]^2} \times \frac{Q_L}{H}$$

where x is the distance from the face of the excavation or wall to the vertical line-load, H is the distance from the bottom of the footing to the bottom of excavation or wall, z is the depth at which the horizontal pressure is desired, Q_L is the vertical line-load and $\sigma_H(z)$ is the horizontal pressure at depth z.

8.16.3 It is recommended that vertical point-loads, from construction equipment outriggers or adjacent building columns use horizontal pressures generated from NAV-FAC DM 7.2. The governing equations are:

$$For\ {}^{x}/_{H} \leq 0.4$$

$$\sigma_H(z) = \frac{0.28 \times \left(\frac{z}{H}\right)^2}{\left[0.16 + \left(\frac{z}{H}\right)^2\right]^3} \times \frac{Q_P}{H^2}$$

and

$$For\ {}^{x}/_{H} > 0.4$$

$$\sigma_H(z) = \frac{1.77 \times \left(\frac{x}{H}\right)^2 \times \left(\frac{z}{H}\right)^2}{\left[\left(\frac{x}{H}\right)^2 + \left(\frac{z}{H}\right)^2\right]^3} \times \frac{Q_P}{H^2}$$

then

$$\sigma'_H(z) = \sigma_H(z) cos^2(1.1\theta)$$

where x is the distance from the face of the excavation/wall to the vertical point-load, H is distance from the outrigger/bottom of column footing to the bottom of excavation, z is the depth at which the horizontal pressure is desired, Qp is the vertical point-load, $\sigma_H(z)$ is the horizontal pressure at depth z, θ is the angle between a line perpendicular to the excavation/wall and a line from the point-load to location on the excavation/wall where the surcharge is being evaluated, and $\sigma_H(z)$ is the horizontal pressure at depth z.

8.17 Surface Drainage

8.17.1 Proper surface drainage is critical to the future performance of the project. Uncontrolled infiltration of irrigation excess and storm runoff into the soils can adversely affect the performance of the planned improvements. Saturation of a soil can cause it to lose internal shear strength and increase its compressibility, resulting in a change in the original designed engineering properties. Proper drainage should be maintained at all times.

8.17.2 All site drainage should be collected and controlled in non-erosive drainage devices. Drainage should not be allowed to pond anywhere on the site, and especially not against any foundation or retaining wall. The site should be graded and maintained such that surface drainage is directed away from structures in accordance with 2019 CBC 1804.4 or other applicable standards. In addition, drainage should not be allowed to flow uncontrolled over any descending slope. Discharge from downspouts, roof drains and scuppers are not recommended onto unprotected soils within 5 feet of the building perimeter. Planters which are located adjacent to foundations should be sealed to prevent moisture intrusion into the soils providing foundation support. Landscape irrigation is not recommended within 5 feet of the building perimeter footings except when enclosed in protected planters.

8.17.3 Positive site drainage should be provided away from structures, pavement, and the tops of slopes to swales or other controlled drainage structures. The building pad and pavement areas should be fine graded such that water is not allowed to pond.

8.17.4 Landscaping planters immediately adjacent to paved areas are not recommended due to the potential for surface or irrigation water to infiltrate the pavement's subgrade and base course. Either a subdrain, which collects excess irrigation water and transmits it to drainage structures, or impervious above-grade planter boxes should be used. In addition, where landscaping is planned adjacent to the pavement, it is recommended that consideration be given to providing a cutoff wall along the edge of the pavement that extends at least 12 inches below the base material.

8.18 Plan Review

8.18.1 Grading, foundation, and shoring plans should be reviewed by the Geotechnical Engineer (a representative of Geocon West, Inc.), prior to finalization to verify that the plans have been prepared in substantial conformance with the recommendations of this report and to provide additional analyses or recommendations.

LIMITATIONS AND UNIFORMITY OF CONDITIONS

1. The recommendations of this report pertain only to the site investigated and are based upon the assumption that the soil conditions do not deviate from those disclosed in the investigation. If any variations or undesirable conditions are encountered during construction, or if the proposed construction will differ from that anticipated herein, Geocon West, Inc. should be notified so that supplemental recommendations can be given. The evaluation or identification of the potential presence of hazardous or corrosive materials was not part of the scope of services provided by Geocon West, Inc.

2. This report is issued with the understanding that it is the responsibility of the owner, or of his representative, to ensure that the information and recommendations contained herein are brought to the attention of the architect and engineer for the project and incorporated into the plans, and the necessary steps are taken to see that the contractor and subcontractors carry out such recommendations in the field.

3. The findings of this report are valid as of the date of this report. However, changes in the conditions of a property can occur with the passage of time, whether they are due to natural processes or the works of man on this or adjacent properties. In addition, changes in applicable or appropriate standards may occur, whether they result from legislation or the broadening of knowledge. Accordingly, the findings of this report may be invalidated wholly or partially by changes outside our control. Therefore, this report is subject to review and should not be relied upon after a period of three years.

4. The firm that performed the geotechnical investigation for the project should be retained to provide testing and observation services during construction to provide continuity of geotechnical interpretation and to check that the recommendations presented for geotechnical aspects of site development are incorporated during site grading, construction of improvements, and excavation of foundations. If another geotechnical firm is selected to perform the testing and observation services during construction operations, that firm should prepare a letter indicating their intent to assume the responsibilities of project geotechnical engineer of record. A copy of the letter should be provided to the regulatory agency for their records. In addition, that firm should provide revised recommendations concerning the geotechnical aspects of the proposed development, or a written acknowledgement of their concurrence with the recommendations presented in our report. They should also perform additional analyses deemed necessary to assume the role of Geotechnical Engineer of Record.

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U.S. Geological Survey and California Geological Survey, 2006, *Quaternary Fault and Fold Database for the United States,* accessed March 4, 2021 from USGS web site: http//earthquake.usgs.gov/hazards/qfaults/.

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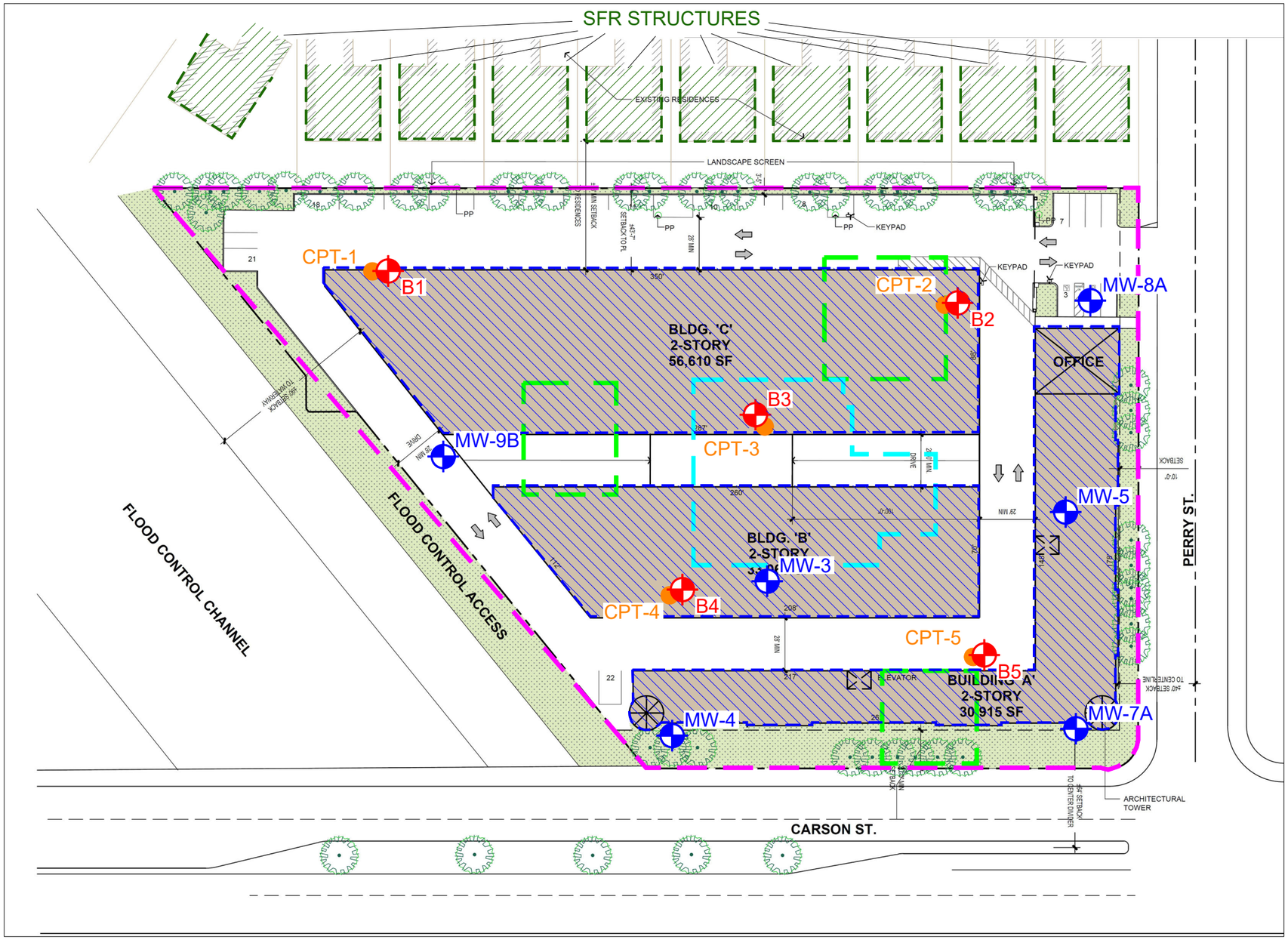
Ziony, J. I., and Jones, L. M., 1989, *Map Showing Late Quaternary Faults and 1978–1984 Seismicity of the Los Angeles Region, California*, U.S. Geological Survey Miscellaneous Field Studies Map MF-1964.



LEGEND

- B5 — Approximate Location of Boring
- CPT-5 — Approximate Location of CPT
- MW-9B — Approximate Location of Monitoring Well
- Property Limits
- Existing Off-Site Structures
- Proposed New Medical Office Building
- Extent of URS Removal and Recompaction (5 FT BGS)
- Extent of URS Removal and Recompaction (8 FT BGS)

North

0 60' 120'

GEOCON WEST, INC.
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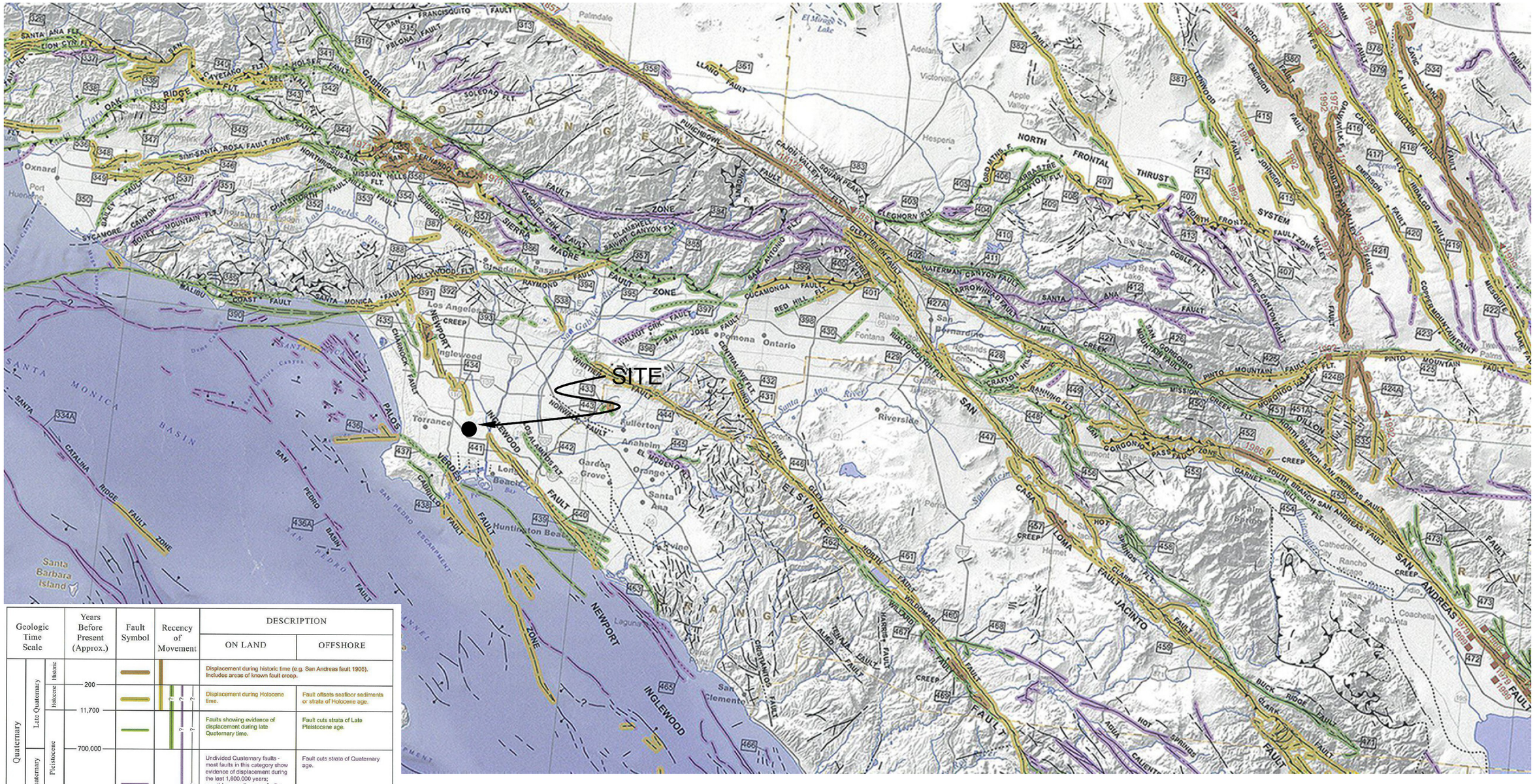
DRAFTED BY: JMH | CHECKED BY: JTA

SITE PLAN

21611 S PERRY STREET
CARSON, CALIFORNIA

APRIL 2021 | PROJECT NO. W1301-06-01 | FIG. 2

Reference: Jennings, C.W. and Bryant, W. A., 2010, Fault Activity Map of California, California Geological Survey Geologic Data Map No. 6.



Geologic Time Scale			Years Before Present (Approx.)	Fault Symbol	Recency of Movement	DESCRIPTION: ON LAND	DESCRIPTION: OFFSHORE
Quaternary	Late Quaternary	Historic				Displacement during historic time (e.g. San Andreas fault 1906). Includes areas of known fault creep.	
		Holocene	200			Displacement during Holocene time.	Fault offsets seafloor sediments or strata of Holocene age.
			11,700			Faults showing evidence of displacement during late Quaternary time.	Fault cuts strata of Late Pleistocene age.
	Early Quaternary	Pleistocene	700,000			Undivided Quaternary faults - most faults in this category show evidence of displacement during the last 1,600,000 years; possible exceptions are faults which displace rocks of undifferentiated Plio-Pleistocene age.	Fault cuts strata of Quaternary age.
Pre-Quaternary			1,600,000*			Faults without recognized Quaternary displacement or showing evidence of no displacement during Quaternary time. Not necessarily inactive.	Fault cuts strata of Pliocene or older age.
			4.5 billion (Age of Earth)				

* Quaternary now recognized as extending to 2.6 Ma (Walker and Geissman, 2009). Quaternary faults in this map were established using the previous 1.8 Ma criterion.

N

0 12 24 Miles

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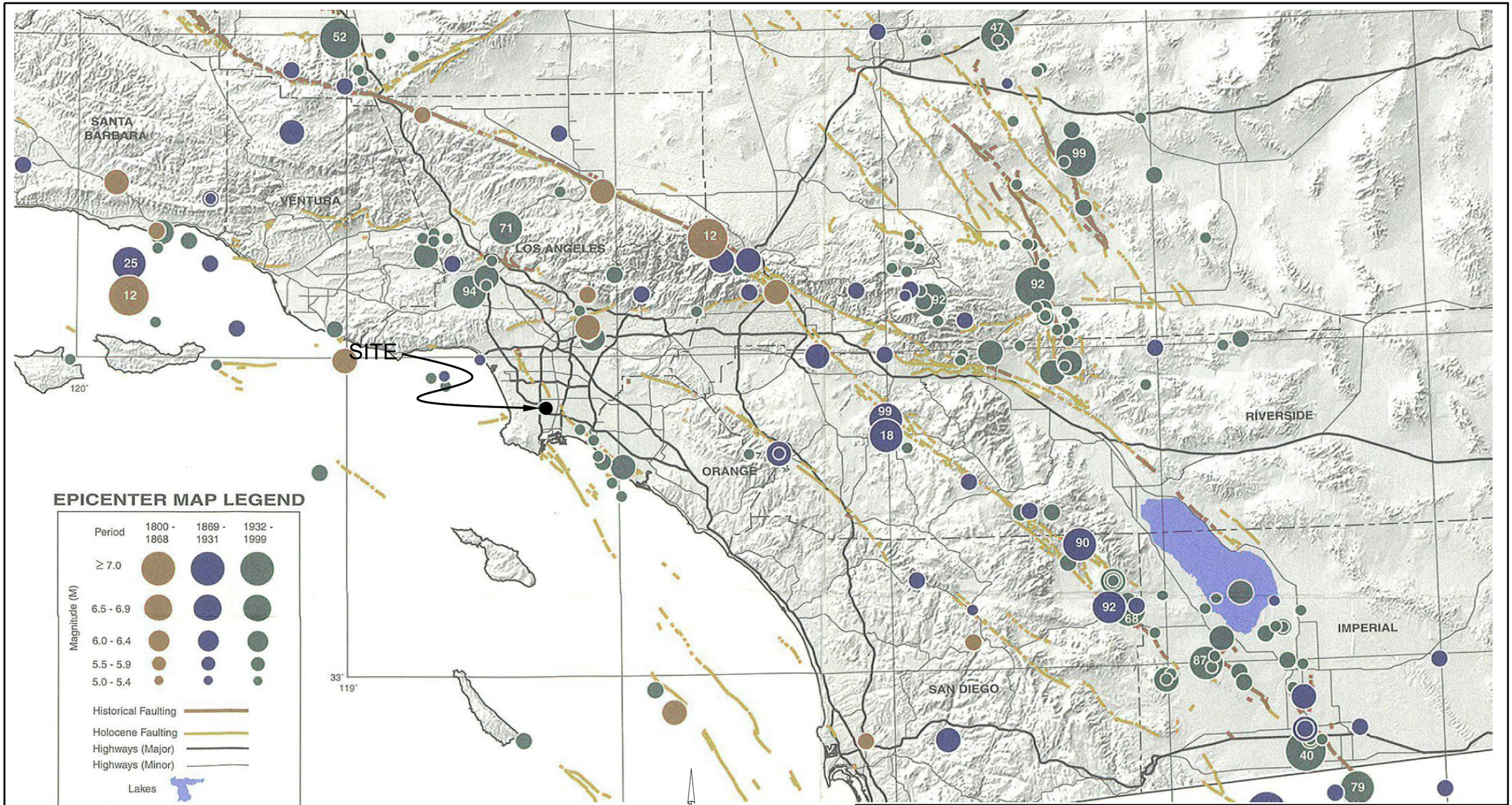
REGIONAL FAULT MAP

21611 SOUTH PERRY STREET
CARSON, CALIFORNIA

APRIL 2021 | PROJECT NO. W1301-06-01 | FIG. 3



EPICENTER MAP LEGEND

Period	1800 - 1868	1869 - 1931	1932 - 1999
Magnitude (M) ≥ 7.0			
6.5 - 6.9			
6.0 - 6.4			
5.5 - 5.9			
5.0 - 5.4			

Historical Faulting
Holocene Faulting
Highways (Major)
Highways (Minor)
Lakes
65 Last two digits of M ≥ 6.5 earthquake year

Reference: Toppozada, T., Branum, D., Petersen, M., Hallstrom, C., Cramer, C., and Reichle, M., 2000, Epicenters and Areas Damaged by M≥5 California Earthquakes, 1800 - 1999, California Geological Survey, Map Sheet 49.

0 20 40 Miles

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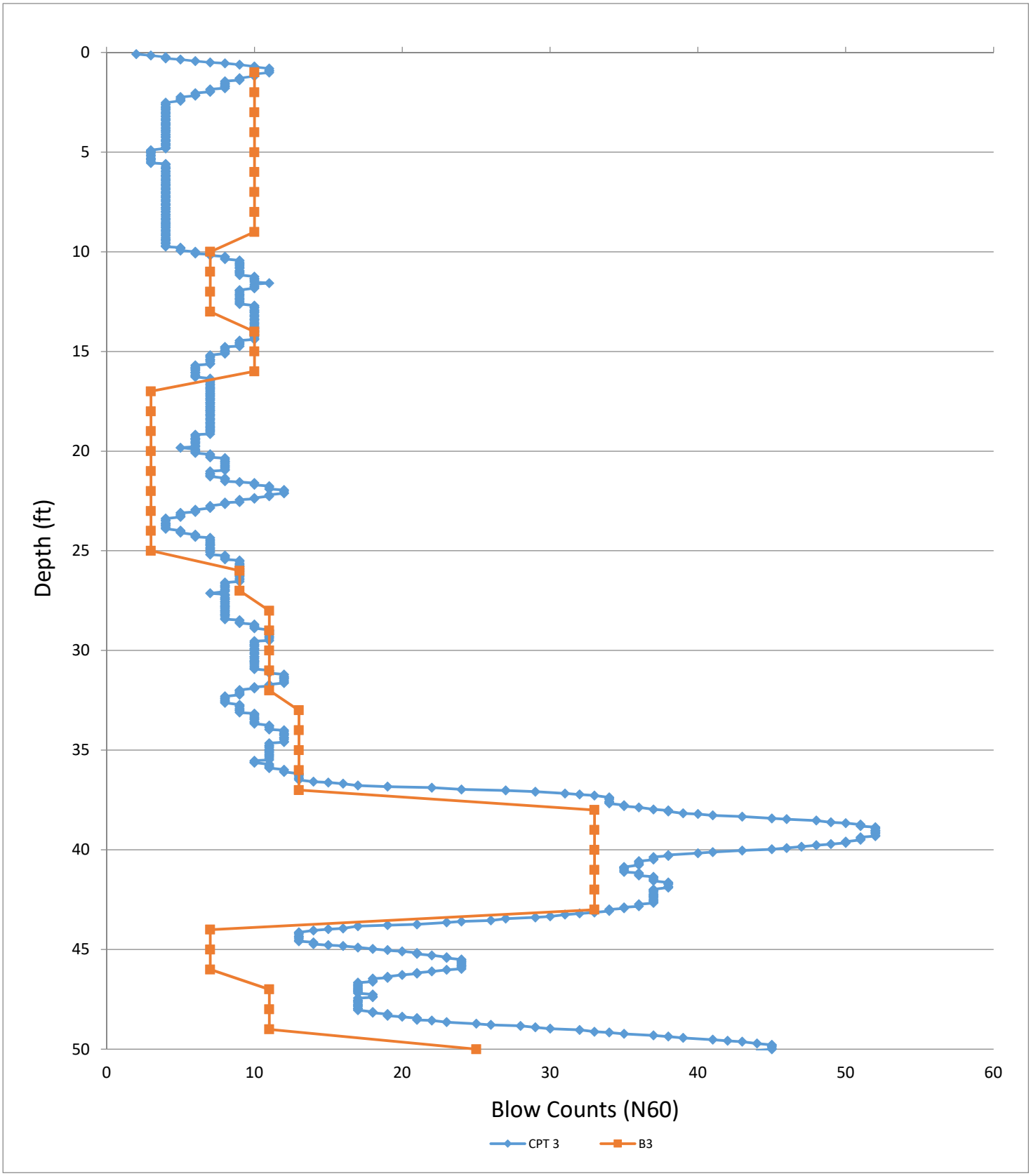
REGIONAL SEISMICITY MAP

21611 SOUTH PERRY STREET
CARSON, CALIFORNIA

APRIL 2021 | PROJECT NO. W1301-06-01 | FIG.4



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JMH		

CORRELATION OF BORING & CPT N60

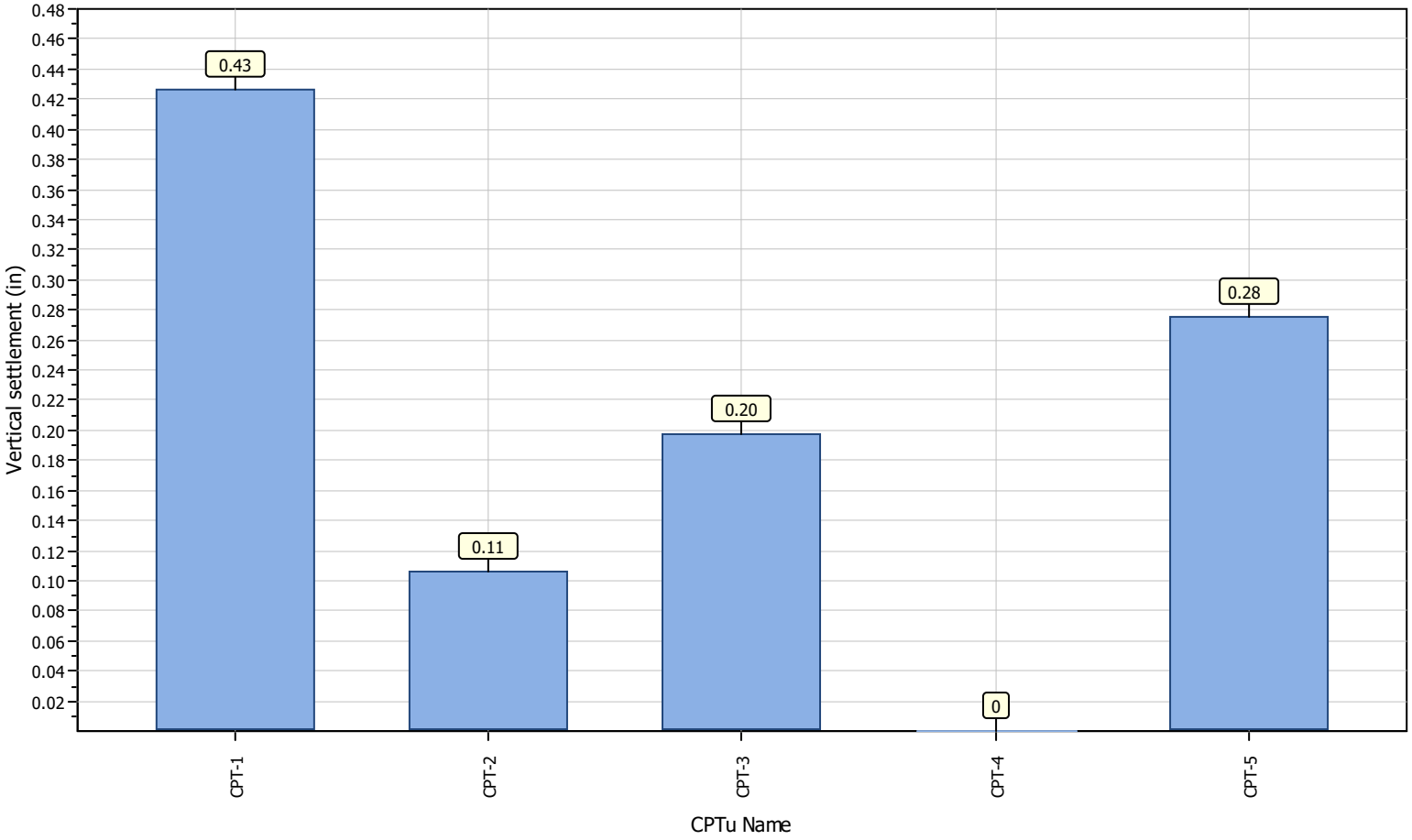
21611 SOUTH PERRY STREET
CARSON, CA

APRIL 2021	PROJECT NO. W1301-06-01	FIG.5

Project title : W1301-06-01

Location : Perry Street

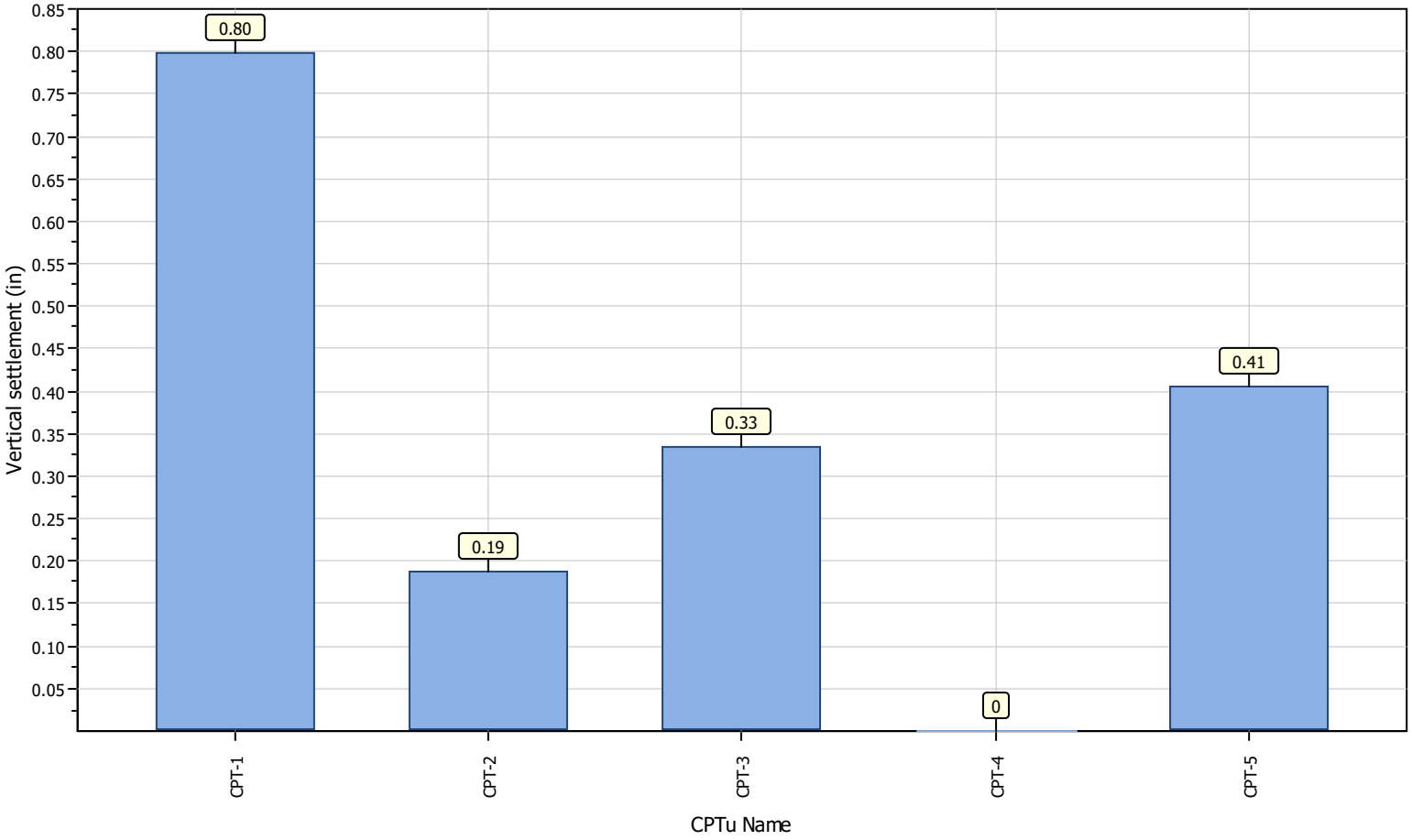
Overall vertical settlements report



Project title : W1301-06-01

Location : Perry Street

Overall vertical settlements report



GEOCON

Client : Perry Street
File No. : W1301-06-01
Boring : 3

TECHNICAL ENGINEERING AND DESIGN GUIDES AS ADAPTED FROM THE US ARMY CORPS OF ENGINEERS, NO. 9
EVALUATION OF EARTHQUAKE-INDUCED SETTLEMENTS IN DRY SANDY SOILS
DESIGN EARTHQUAKE

DE EARTHQUAKE INFORMATION:

Earthquake Magnitude:	6.68
Peak Horiz. Acceleration (g):	0.549

Fig 4.1 Fig 4.2 Fig 4.4

Depth of Base of Strata (ft)	Thickness of Layer (ft)	Depth of Mid-point of Layer (ft)	Soil Unit Weight (pcf)	Overburden Pressure at Mid-point (tsf)	Mean Effective Pressure at Mid-point (tsf)	Average Cyclic Shear Stress [Tav]	Field SPT [N]	Correction Factor [Cer]	Relative Density [Dr] (%)	Correction Factor [Cn]	Corrected [N1]60	rd Factor	Maximum Shear Mod. [Gmax] (tsf)	[yeff]*[Geff] [Gmax]	yeff Shear Strain	[yeff]*100%	Volumetric Strain M7.5 [E15] (%)	Number of Strain Cycles [Nc]	Corrected Vol. Strains [Ec]	Estimated Settlement [S] (inches)
1.0	1.0	0.5	120.0	0.03	0.02	0.011	10	1.25	76.6	1.7	19.1	1.0	169.475	6.25E-05	1.00E-04	0.010	1.06E-02	8.4928	8.17E-03	0.00
2.0	1.0	1.5	120.0	0.09	0.06	0.032	10	1.25	74.4	1.7	19.1	1.0	293.540	1.06E-04	2.30E-04	0.023	2.43E-02	8.4928	1.88E-02	0.00
3.0	1.0	2.5	120.0	0.15	0.10	0.053	10	1.25	72.5	1.7	19.1	1.0	378.958	1.34E-04	1.70E-04	0.017	1.79E-02	8.4928	1.39E-02	0.00
4.0	1.0	3.5	120.0	0.21	0.14	0.075	10	1.25	70.7	1.7	19.1	1.0	448.389	1.56E-04	1.70E-04	0.017	1.79E-02	8.4928	1.39E-02	0.00
5.0	1.0	4.5	120.0	0.27	0.18	0.096	10	1.25	69.0	1.7	19.1	1.0	508.425	1.74E-04	1.70E-04	0.017	1.79E-02	8.4928	1.39E-02	0.00
6.0	1.0	5.5	120.0	0.33	0.22	0.117	10	1.25	67.4	1.7	19.1	1.0	562.085	1.88E-04	1.50E-04	0.015	1.58E-02	8.4928	1.23E-02	0.00
7.0	1.0	6.5	120.0	0.39	0.26	0.139	10	1.25	65.9	1.6	18.4	1.0	603.301	2.03E-04	4.50E-04	0.045	4.97E-02	8.4928	3.85E-02	0.01
8.0	1.0	7.5	120.0	0.45	0.30	0.160	10	1.25	64.5	1.5	17.1	1.0	632.776	2.20E-04	4.50E-04	0.045	5.42E-02	8.4928	4.19E-02	0.01
9.0	1.0	8.5	120.0	0.51	0.34	0.181	10	1.25	63.3	1.4	16.1	1.0	659.735	2.34E-04	4.50E-04	0.045	5.84E-02	8.4928	4.52E-02	0.01
10.0	1.0	9.5	120.0	0.57	0.38	0.202	7	1.25	52.2	1.4	10.7	1.0	607.907	2.79E-04	4.50E-04	0.045	9.58E-02	8.4928	7.41E-02	0.00
11.0	1.0	10.5	120.0	0.63	0.42	0.222	7	1.25	52.2	1.3	10.1	1.0	628.529	2.93E-04	4.50E-04	0.045	1.02E-01	8.4928	7.87E-02	0.00
12.0	1.0	11.5	120.0	0.69	0.46	0.243	7	1.25	52.2	1.2	9.8	0.9	650.354	3.05E-04	1.00E-03	0.100	2.35E-01	8.4928	1.82E-01	0.00
13.0	1.0	12.5	120.0	0.75	0.50	0.263	7	1.25	52.2	1.2	9.6	0.9	673.332	3.14E-04	7.10E-04	0.071	1.71E-01	8.4928	1.33E-01	0.00
14.0	1.0	13.5	120.0	0.81	0.54	0.284	10	1.25	59.6	1.2	14.4	0.9	802.030	2.80E-04	3.70E-04	0.037	5.47E-02	8.4928	4.23E-02	0.00
15.0	1.0	14.5	120.0	0.87	0.58	0.304	10	1.25	59.6	1.2	14.2	0.9	825.875	2.87E-04	3.70E-04	0.037	5.59E-02	8.4928	4.33E-02	0.00
16.0	1.0	15.5	120.0	0.93	0.62	0.324	10	1.25	59.6	1.1	13.9	0.9	848.608	2.93E-04	3.70E-04	0.037	5.72E-02	8.4928	4.43E-02	0.00
17.0	1.0	16.5	120.0	0.99	0.66	0.344	3	1.25	31.4	1.1	4.5	0.9	603.195	4.31E-04	1.20E-03	0.120	7.10E-01	8.4928	5.49E-01	0.00
18.0	1.0	17.5	120.0	1.05	0.70	0.364	3	1.25	31.4	1.1	4.5	0.9	617.634	4.39E-04	1.20E-03	0.120	7.24E-01	8.4928	5.61E-01	0.00
19.0	1.0	18.5	120.0	1.11	0.74	0.383	3	1.25	31.4	1.1	4.4	0.9	631.508	4.47E-04	1.20E-03	0.120	7.39E-01	8.4928	5.72E-01	0.00
20.0	1.0	19.5	120.0	1.17	0.78	0.402	3	1.25	31.4	1.1	4.3	0.9	644.865	4.53E-04	1.20E-03	0.120	7.54E-01	8.4928	5.83E-01	0.00
21.0	1.0	20.5	120.0	1.23	0.82	0.421	3	1.25	31.4	1.1	4.3	0.9	657.749	4.60E-04	1.20E-03	0.120	7.68E-01	8.4928	5.94E-01	0.00
22.0	1.0	21.5	120.0	1.29	0.86	0.440	3	1.25	31.4	1.0	4.2	0.9	670.198	4.65E-04	1.20E-03	0.120	7.82E-01	8.4928	6.05E-01	0.00
23.0	1.0	22.5	120.0	1.35	0.90	0.458	3	1.25	31.4	1.0	4.1	0.9	682.246	4.70E-04	1.20E-03	0.120	7.96E-01	8.4928	6.16E-01	0.00
24.0	1.0	23.5	120.0	1.41	0.94	0.477	3	1.25	31.4	1.0	4.1	0.9	693.922	4.75E-04	1.20E-03	0.120	8.10E-01	8.4928	6.27E-01	0.00
25.0	1.0	24.5	120.0	1.47	0.98	0.495	3	1.25	31.4	1.0	4.0	0.9	705.252	4.80E-04	1.20E-03	0.120	8.23E-01	8.4928	6.37E-01	0.00
26.0	1.0	25.5	120.0	1.53	1.03	0.513	9	1.25	52.3	1.0	12.7	0.9	1055.741	3.28E-04	5.20E-04	0.052	8.97E-02	8.4928	6.95E-02	0.00
27.0	1.0	26.5	120.0	1.59	1.07	0.530	9	1.25	52.3	1.0	12.5	0.9	1071.522	3.31E-04	5.20E-04	0.052	9.12E-02	8.4928	7.06E-02	0.00
28.0	1.0	27.5	120.0	1.65	1.11	0.547	11	1.25	55.9	1.0	15.8	0.9	1179.921	3.07E-04	5.20E-04	0.052	6.89E-02	8.4928	5.33E-02	0.00
29.0	1.0	28.5	120.0	1.71	1.15	0.564	11	1.25	55.9	0.9	15.6	0.9	1196.177	3.09E-04	5.20E-04	0.052	6.99E-02	8.4928	5.41E-02	0.00
30.0	1.0	29.5	120.0	1.77	1.19	0.581	11	1.25	55.9	0.9	15.4	0.9	1212.035	3.11E-04	5.20E-04	0.052	7.10E-02	8.4928	5.49E-02	0.00
31.0	1.0	30.5	120.0	1.83	1.23	0.597	11	1.25	55.9	0.9	15.3	0.9	1227.516	3.12E-04	5.20E-04	0.052	7.20E-02	8.4928	5.57E-02	0.00
32.0	1.0	31.5	120.0	1.89	1.27	0.613	11	1.25	55.9	0.9	15.1	0.9	1242.641	3.14E-04	5.20E-04	0.052	7.30E-02	8.4928	5.65E-02	0.00
33.0	1.0	32.5	120.0	1.95	1.31	0.629	13	1.25	58.8	0.9	17.6	0.9	1329.436	2.98E-04	3.00E-04	0.030	3.49E-02	8.4928	2.70E-02	0.00
34.0	1.0	33.5	120.0	2.01	1.35	0.645	13	1.25	58.8	0.9	17.4	0.8	1344.735	2.99E-04	3.00E-04	0.030	3.54E-02	8.4928	2.74E-02	0.00
35.0	1.0	34.5	120.0	2.07	1.39	0.660	13	1.25	58.8	0.9	17.2	0.8	1359.713	3.00E-04	5.20E-04	0.052	6.22E-02	8.4928	4.81E-02	0.00
36.0	1.0	35.5	120.0	2.13	1.43	0.675	13	1.25	58.8	0.9	17.0	0.8	1374.387	3.01E-04	5.20E-04	0.052	6.30E-02	8.4928	4.88E-02	0.00
37.0	1.0	36.5	120.0	2.19	1.47	0.690	13	1.25	58.8	0.9	16.9	0.8	1388.771	3.02E-04	5.20E-04	0.052	6.38E-02	8.4928	4.94E-02	0.00
38.0	1.0	37.5	120.0	2.25	1.51	0.704	33	1.25	90.8	0.9	42.4	0.8	1913.714	2.22E-04	3.00E-04	0.030	1.22E-02	8.4928	9.43E-03	0.00
39.0	1.0	38.5	120.0	2.31	1.55	0.718	33	1.25	90.8	0.8	42.0	0.8	1932.598	2.22E-04	3.00E-04	0.030	1.23E-02	8.4928	9.54E-03	0.00
40.0	1.0	39.5	120.0	2.37	1.59	0.732	33	1.25	90.8	0.8	41.6	0.8	1951.139	2.23E-04	3.00E-04	0.030	1.25E-02	8.4928	9.65E-03	0.00
41.0	1.0	40.5	120.0	2.43	1.63	0.745	33	1.25	90.8	0.8	41.2	0.8	1969.350	2.23E-04	3.00E-04	0.030	1.26E-02	8.4928	9.77E-03	0.00
42.0	1.0	41.5	120.0	2.49	1.67	0.758	33	1.25	90.8	0.8	40.8	0.8	1987.246	2.23E-04	3.00E-04	0.030	1.28E-02	8.4928	9.88E-03	0.00
43.0	1.0	42.5	120.0	2.55	1.71	0.771	33	1.25	90.8	0.8	40.4	0.8	2004.839	2.23E-04	3.00E-04	0.030	1.29E-02	8.4928	9.99E-03	0.00
44.0	1.0	43.5	120.0	2.61	1.75	0.783	7	1.25	40.6	0.8	15.5	0.8	1473.568	3.07E-04	5.20E-04	0.052	7.06E-02	8.4928	5.47E-02	0.00
45.0	1.0	44.5	120.0	2.67	1.79	0.795	7	1.25	40.6	0.8	15.4	0.8	1487.981	3.07E-04	5.20E-04	0.052	7.11E-02	8.4928	5.50E-02	0.00
46.0	1.0	45.5	120.0	2.73	1.83	0.807	7	1.25	40.6	0.8	15.3	0.8	1502.208	3.06E-04	5.20E-04	0.052	7.15E-02	8.4928	5.53E-02	0.00
47.0	1.0	46.5	120.0	2.79	1.87	0.819	11	1.25	50.1	0.8	13.0	0.8	1436.934	3.23E-04	5.20E-04	0.052	8.72E-02	8.4928	6.75E-02	0.00
48.0	1.0	47.5	120.0	2.85	1.91	0.830	11	1.25	50.1	0.8	12.9	0.8	1448.200	3.23E-04	5.20E-04	0.052	8.81E-02	8.4928	6.82E-02	0.00
49.0	1.0	48.5	120.0	2.91	1.95	0.841	11	1.25	50.1	0.8	12.8	0.8	1459.300	3.23E-04	5.20E-04	0.052	8.90E-02	8.4928	6.89E-02	0.00
50.0	1.0	49.5	120.0	2.97	1.99	0.851	25	1.25	74.5	0.8	34.0	0.8	2042.085	2.32E-04	3.00E-04	0.030	1.59E-02	8.4928	1.23E-02	0.00

TOTAL SETTLEMENT = **0.05**

Figure 9

GEOCON

Client : Perry Street
File No. : W1301-06-01
Boring : 3

TECHNICAL ENGINEERING AND DESIGN GUIDES AS ADAPTED FROM THE US ARMY CORPS OF ENGINEERS, NO. 9
EVALUATION OF EARTHQUAKE-INDUCED SETTLEMENTS IN DRY SANDY SOILS
MAXIMUM CONSIDERED EARTHQUAKE

MCE EARTHQUAKE INFORMATION:

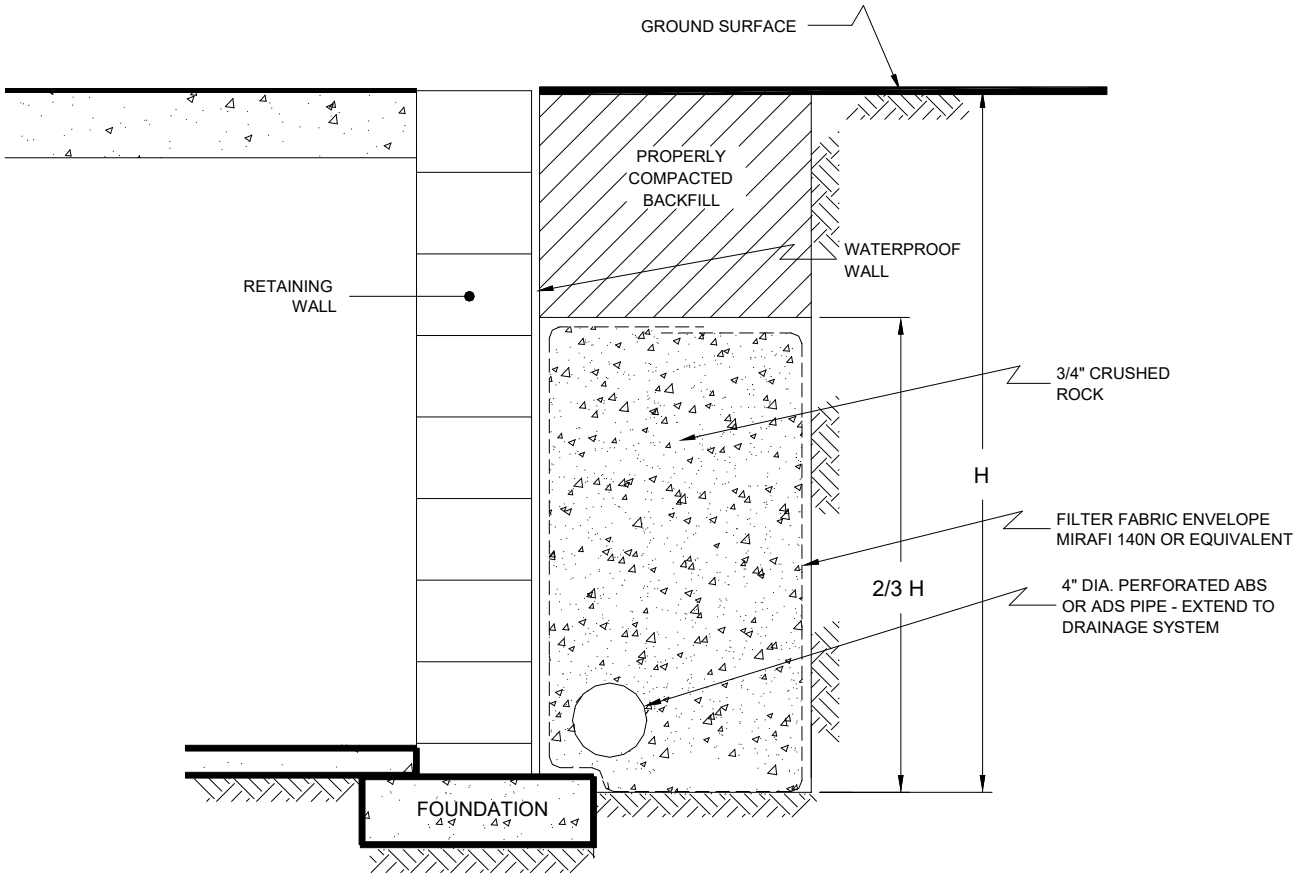
Earthquake Magnitude:	6.87
Peak Horiz. Acceleration (g):	0.823

Fig 4.1 Fig 4.2 Fig 4.4

Depth of Base of Strata (ft)	Thickness of Layer (ft)	Depth of Mid-point of Layer (ft)	Soil Unit Weight (pcf)	Overburden Pressure at Mid-point (tsf)	Mean Effective Pressure at Mid-point (tsf)	Average Cyclic Shear Stress [Tav]	Field SPT [N]	Correction Factor [Cer]	Relative Density [Dr] (%)	Correction Factor [Cn]	Corrected [N1]60	rd Factor	Maximum Shear Mod. [Gmax] (tsf)	[yeff]*[Geff] [Gmax]	yeff Shear Strain	[yeff]*100%	Volumetric Strain M7.5 [E15] (%)	Number of Strain Cycles [Nc]	Corrected Vol. Strains [Ec]	Estimated Settlement [S] (inches)
1.0	1.0	0.5	120.0	0.03	0.02	0.016	10	1.25	76.6	1.7	19.1	1.0	169.475	9.38E-05	1.90E-04	0.019	2.00E-02	9.8538	1.66E-02	0.00
2.0	1.0	1.5	120.0	0.09	0.06	0.048	10	1.25	74.4	1.7	19.1	1.0	293.540	1.59E-04	2.30E-04	0.023	2.43E-02	9.8538	2.01E-02	0.00
3.0	1.0	2.5	120.0	0.15	0.10	0.080	10	1.25	72.5	1.7	19.1	1.0	378.958	2.02E-04	8.10E-04	0.081	8.55E-02	9.8538	7.07E-02	0.02
4.0	1.0	3.5	120.0	0.21	0.14	0.112	10	1.25	70.7	1.7	19.1	1.0	448.389	2.34E-04	8.10E-04	0.081	8.55E-02	9.8538	7.07E-02	0.02
5.0	1.0	4.5	120.0	0.27	0.18	0.144	10	1.25	69.0	1.7	19.1	1.0	508.425	2.60E-04	8.10E-04	0.081	8.55E-02	9.8538	7.07E-02	0.02
6.0	1.0	5.5	120.0	0.33	0.22	0.176	10	1.25	67.4	1.7	19.1	1.0	562.085	2.82E-04	4.50E-04	0.045	4.75E-02	9.8538	3.93E-02	0.01
7.0	1.0	6.5	120.0	0.39	0.26	0.208	10	1.25	65.9	1.6	18.4	1.0	603.301	3.05E-04	1.00E-03	0.100	1.10E-01	9.8538	9.14E-02	0.02
8.0	1.0	7.5	120.0	0.45	0.30	0.239	10	1.25	64.5	1.5	17.1	1.0	632.776	3.29E-04	1.00E-03	0.100	1.20E-01	9.8538	9.96E-02	0.02
9.0	1.0	8.5	120.0	0.51	0.34	0.271	10	1.25	63.3	1.4	16.1	1.0	659.735	3.51E-04	1.00E-03	0.100	1.30E-01	9.8538	1.07E-01	0.03
10.0	1.0	9.5	120.0	0.57	0.38	0.302	7	1.25	52.2	1.4	10.7	1.0	607.907	4.18E-04	2.70E-03	0.270	5.75E-01	9.8538	4.76E-01	0.00
11.0	1.0	10.5	120.0	0.63	0.42	0.333	7	1.25	52.2	1.3	10.1	1.0	628.529	4.39E-04	2.70E-03	0.270	6.10E-01	9.8538	5.05E-01	0.00
12.0	1.0	11.5	120.0	0.69	0.46	0.364	7	1.25	52.2	1.2	9.8	0.9	650.354	4.57E-04	2.70E-03	0.270	6.36E-01	9.8538	5.26E-01	0.00
13.0	1.0	12.5	120.0	0.75	0.50	0.395	7	1.25	52.2	1.2	9.6	0.9	673.332	4.71E-04	1.20E-03	0.120	2.90E-01	9.8538	2.40E-01	0.00
14.0	1.0	13.5	120.0	0.81	0.54	0.426	10	1.25	59.6	1.2	14.4	0.9	802.030	4.19E-04	1.20E-03	0.120	1.77E-01	9.8538	1.47E-01	0.00
15.0	1.0	14.5	120.0	0.87	0.58	0.456	10	1.25	59.6	1.2	14.2	0.9	825.875	4.30E-04	1.20E-03	0.120	1.81E-01	9.8538	1.50E-01	0.00
16.0	1.0	15.5	120.0	0.93	0.62	0.486	10	1.25	59.6	1.1	13.9	0.9	848.608	4.39E-04	1.20E-03	0.120	1.86E-01	9.8538	1.54E-01	0.00
17.0	1.0	16.5	120.0	0.99	0.66	0.516	3	1.25	31.4	1.1	4.5	0.9	603.195	6.47E-04	4.10E-03	0.410	2.42E+00	9.8538	2.01E+00	0.00
18.0	1.0	17.5	120.0	1.05	0.70	0.545	3	1.25	31.4	1.1	4.5	0.9	617.634	6.59E-04	4.10E-03	0.410	2.47E+00	9.8538	2.05E+00	0.00
19.0	1.0	18.5	120.0	1.11	0.74	0.574	3	1.25	31.4	1.1	4.4	0.9	631.508	6.70E-04	4.10E-03	0.410	2.53E+00	9.8538	2.09E+00	0.00
20.0	1.0	19.5	120.0	1.17	0.78	0.603	3	1.25	31.4	1.1	4.3	0.9	644.865	6.80E-04	4.10E-03	0.410	2.57E+00	9.8538	2.13E+00	0.00
21.0	1.0	20.5	120.0	1.23	0.82	0.631	3	1.25	31.4	1.1	4.3	0.9	657.749	6.89E-04	4.10E-03	0.410	2.62E+00	9.8538	2.17E+00	0.00
22.0	1.0	21.5	120.0	1.29	0.86	0.660	3	1.25	31.4	1.0	4.2	0.9	670.198	6.98E-04	4.10E-03	0.410	2.67E+00	9.8538	2.21E+00	0.00
23.0	1.0	22.5	120.0	1.35	0.90	0.687	3	1.25	31.4	1.0	4.1	0.9	682.246	7.05E-04	1.00E-02	1.000	6.63E+00	9.8538	5.49E+00	0.00
24.0	1.0	23.5	120.0	1.41	0.94	0.715	3	1.25	31.4	1.0	4.1	0.9	693.922	7.13E-04	1.00E-02	1.000	6.75E+00	9.8538	5.59E+00	0.00
25.0	1.0	24.5	120.0	1.47	0.98	0.742	3	1.25	31.4	1.0	4.0	0.9	705.252	7.19E-04	1.00E-02	1.000	6.86E+00	9.8538	5.68E+00	0.00
26.0	1.0	25.5	120.0	1.53	1.03	0.769	9	1.25	52.3	1.0	12.7	0.9	1055.741	4.92E-04	8.10E-04	0.081	1.40E-01	9.8538	1.16E-01	0.00
27.0	1.0	26.5	120.0	1.59	1.07	0.795	9	1.25	52.3	1.0	12.5	0.9	1071.522	4.96E-04	8.10E-04	0.081	1.42E-01	9.8538	1.18E-01	0.00
28.0	1.0	27.5	120.0	1.65	1.11	0.821	11	1.25	55.9	1.0	15.8	0.9	1179.921	4.60E-04	8.10E-04	0.081	1.07E-01	9.8538	8.88E-02	0.00
29.0	1.0	28.5	120.0	1.71	1.15	0.846	11	1.25	55.9	0.9	15.6	0.9	1196.177	4.63E-04	8.10E-04	0.081	1.09E-01	9.8538	9.02E-02	0.00
30.0	1.0	29.5	120.0	1.77	1.19	0.871	11	1.25	55.9	0.9	15.4	0.9	1212.035	4.66E-04	8.10E-04	0.081	1.11E-01	9.8538	9.15E-02	0.00
31.0	1.0	30.5	120.0	1.83	1.23	0.896	11	1.25	55.9	0.9	15.3	0.9	1227.516	4.68E-04	8.10E-04	0.081	1.12E-01	9.8538	9.28E-02	0.00
32.0	1.0	31.5	120.0	1.89	1.27	0.920	11	1.25	55.9	0.9	15.1	0.9	1242.641	4.71E-04	8.10E-04	0.081	1.14E-01	9.8538	9.41E-02	0.00
33.0	1.0	32.5	120.0	1.95	1.31	0.943	13	1.25	58.8	0.9	17.6	0.9	1329.436	4.47E-04	8.10E-04	0.081	9.43E-02	9.8538	7.81E-02	0.00
34.0	1.0	33.5	120.0	2.01	1.35	0.967	13	1.25	58.8	0.9	17.4	0.8	1344.735	4.49E-04	8.10E-04	0.081	9.56E-02	9.8538	7.91E-02	0.00
35.0	1.0	34.5	120.0	2.07	1.39	0.990	13	1.25	58.8	0.9	17.2	0.8	1359.713	4.50E-04	8.10E-04	0.081	9.68E-02	9.8538	8.02E-02	0.00
36.0	1.0	35.5	120.0	2.13	1.43	1.012	13	1.25	58.8	0.9	17.0	0.8	1374.387	4.52E-04	8.10E-04	0.081	9.81E-02	9.8538	8.12E-02	0.00
37.0	1.0	36.5	120.0	2.19	1.47	1.034	13	1.25	58.8	0.9	16.9	0.8	1388.771	4.53E-04	8.10E-04	0.081	9.93E-02	9.8538	8.22E-02	0.00
38.0	1.0	37.5	120.0	2.25	1.51	1.055	33	1.25	90.8	0.9	42.4	0.8	1913.714	3.33E-04	5.20E-04	0.052	2.11E-02	9.8538	1.75E-02	0.00
39.0	1.0	38.5	120.0	2.31	1.55	1.076	33	1.25	90.8	0.8	42.0	0.8	1932.598	3.33E-04	5.20E-04	0.052	2.14E-02	9.8538	1.77E-02	0.00
40.0	1.0	39.5	120.0	2.37	1.59	1.097	33	1.25	90.8	0.8	41.6	0.8	1951.139	3.34E-04	5.20E-04	0.052	2.16E-02	9.8538	1.79E-02	0.00
41.0	1.0	40.5	120.0	2.43	1.63	1.117	33	1.25	90.8	0.8	41.2	0.8	1969.350	3.34E-04	5.20E-04	0.052	2.19E-02	9.8538	1.81E-02	0.00
42.0	1.0	41.5	120.0	2.49	1.67	1.136	33	1.25	90.8	0.8	40.8	0.8	1987.246	3.35E-04	5.20E-04	0.052	2.21E-02	9.8538	1.83E-02	0.00
43.0	1.0	42.5	120.0	2.55	1.71	1.155	33	1.25	90.8	0.8	40.4	0.8	2004.839	3.35E-04	5.20E-04	0.052	2.24E-02	9.8538	1.85E-02	0.00
44.0	1.0	43.5	120.0	2.61	1.75	1.174	7	1.25	40.6	0.8	15.5	0.8	1473.568	4.60E-04	8.10E-04	0.081	1.10E-01	9.8538	9.11E-02	0.00
45.0	1.0	44.5	120.0	2.67	1.79	1.192	7	1.25	40.6	0.8	15.4	0.8	1487.981	4.60E-04	8.10E-04	0.081	1.11E-01	9.8538	9.16E-02	0.00
46.0	1.0	45.5	120.0	2.73	1.83	1.210	7	1.25	40.6	0.8	15.3	0.8	1502.208	4.59E-04	8.10E-04	0.081	1.11E-01	9.8538	9.22E-02	0.00
47.0	1.0	46.5	120.0	2.79	1.87	1.227	11	1.25	50.1	0.8	13.0	0.8	1436.934	4.84E-04	8.10E-04	0.081	1.36E-01	9.8538	1.12E-01	0.00
48.0	1.0	47.5	120.0	2.85	1.91	1.244	11	1.25	50.1	0.8	12.9	0.8	1448.200	4.84E-04	8.10E-04	0.081	1.37E-01	9.8538	1.14E-01	0.00
49.0	1.0	48.5	120.0	2.91	1.95	1.260	11	1.25	50.1	0.8	12.8	0.8	1459.300	4.84E-04	8.10E-04	0.081	1.39E-01	9.8538	1.15E-01	0.00
50.0	1.0	49.5	120.0	2.97	1.99	1.276	25	1.25	74.5	0.8	34.0	0.8	2042.085	3.48E-04	5.20E-04	0.052	2.75E-02	9.8538	2.28E-02	0.00

TOTAL SETTLEMENT = **0.14**

Figure 10



NO SCALE

GEOCON WEST, INC.

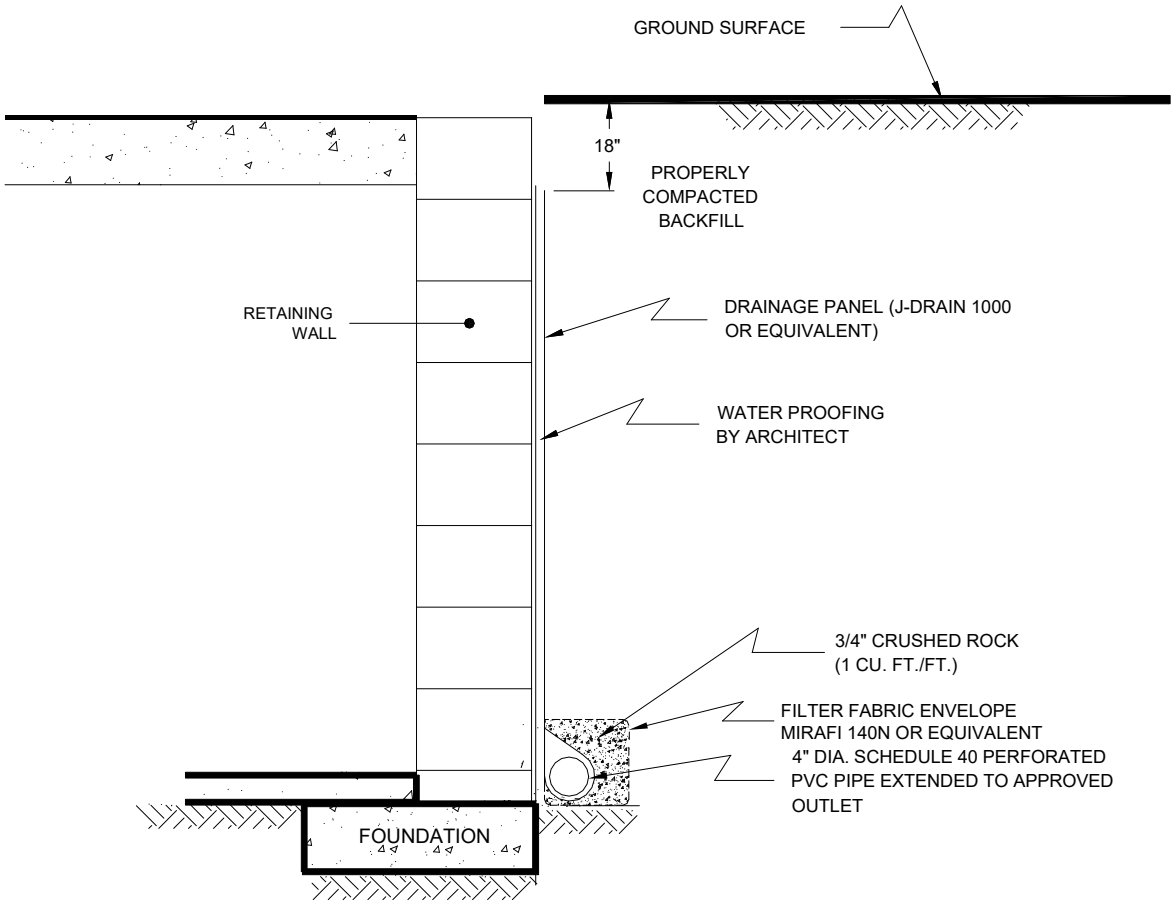
ENVIRONMENTAL GEOTECHNICAL MATERIALS
3303 N. SAN FERNANDO BLVD. - SUITE 100 - BURBANK, CA 91504
PHONE (818) 841-8388 - FAX (818) 841-1704

DRAFTED BY: JMH	CHECKED BY: JTA

RETAINING WALL DRAIN DETAIL

21611 SOUTH PERRY STREET
CARSON, CALIFORNIA

APRIL 2021	NO. W1301-06-01	FIG. 10



NO SCALE

GEOCON WEST, INC.

ENVIRONMENTAL GEOTECHNICAL MATERIALS
3303 N. SAN FERNANDO BLVD. - SUITE 100 - BURBANK, CA 91504
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DRAFTED BY: JMH	CHECKED BY: JTA

RETAINING WALL DRAIN DETAIL

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CARSON, CALIFORNIA

APRIL 2021	NO. W1301-06-01	FIG. 11

APPENDIX A

APPENDIX A

FIELD INVESTIGATION

The site was explored on February 9, 2021 by drilling five 8-inch diameter borings using a truck-mounted hollow-stem auger drilling machine and advancing five cone penetrometer tests (CPTs). The borings were excavated to depths between approximately 20½ and 51 feet beneath the existing ground surface. The CPTs were advanced to depths of approximately 60 feet below existing ground surface. Representative and relatively undisturbed samples were obtained by driving a 4 inch, O. D., California Modified Sampler into the "undisturbed" soil mass with blows from a 140 pound hammer falling 30 inches. Bulk samples were also obtained. Standard Penetration Tests were performed in boring B3.

The soil conditions encountered in the borings were visually examined, classified and logged in general accordance with the Unified Soil Classification System (USCS). Logs of the borings are presented on Figures A1 through A5. The CPT data is presented as Figures A6 through A10. The logs depict the soil and geologic conditions encountered and the depth at which samples were obtained. The logs also include our interpretation of the conditions between sampling intervals. Therefore, the logs contain both observed and interpreted data. We determined the lines designating the interface between soil materials on the logs using visual observations, penetration rates, excavation characteristics and other factors. The transition between materials may be abrupt or gradual. Where applicable, the boring logs were revised based on subsequent laboratory testing. The approximate locations of the borings and CPTs are depicted on the Site Plan (see Figure 2)

PROJECT NO. W1301-06-01

BORING 1

ELEV. (MSL.) -- DATE COMPLETED **2/9/2021**

EQUIPMENT **HOLLOW STEM AUGER** BY: **JMH**

DEPTH IN FEET	SAMPLE NO.	LITHOLOGY	GROUNDWATER	SOIL CLASS (USCS)	MATERIAL DESCRIPTION	PENETRATION RESISTANCE (BLOWS/FT*)	DRY DENSITY (P.C.F.)	MOISTURE CONTENT (%)
0	BULK 0-5'				**ARTIFICIAL FILL** Silty Sand, poorly graded, dense, moist, light brown, fine-grained, some medium-grained, some gravel.			
2								
4								
6	B1@5'			CH	**ALLUVIUM** Clay, firm, moist, dark gray, high plasticity.	19	105.0	24.0
8	B1@7.5'				- some sand	13	106.1	19.7
10	B1@10'				- olive brown mottles	21	103.7	22.0
12			▼					
14					Clayey Sand, poorly graded, loose, saturated, brown, fine-grained.			
16	B1@15'			SC		10	111.6	19.8
18					Silty Sand, poorly graded, medium dense, saturated, brown, fine-grained.			
20	B1@20'			SM		22	114.5	19.2

Total depth of boring: 20.5 feet
Fill to 4.5 feet.
Groundwater encountered at 12.5 feet.
Backfilled with grout.

*Penetration resistance for 140-pound hammer falling 30 inches by auto-hammer.
NOTE: The stratification lines presented herein represent the approximate boundary between earth types; the transitions may be gradual.

W1301-06-01 BORING LOGS.GPJ

Figure A1,
Log of Boring 1, Page 1 of 1

SAMPLE SYMBOLS

- ☐ ... SAMPLING UNSUCCESSFUL
- ◧ ... STANDARD PENETRATION TEST
- ■ ... DRIVE SAMPLE (UNDISTURBED)
- ⊠ ... DISTURBED OR BAG SAMPLE
- ◪ ... CHUNK SAMPLE
- ▼ ... WATER TABLE OR SEEPAGE

NOTE: THE LOG OF SUBSURFACE CONDITIONS SHOWN HEREON APPLIES ONLY AT THE SPECIFIC BORING OR TRENCH LOCATION AND AT THE DATE INDICATED. IT IS NOT WARRANTED TO BE REPRESENTATIVE OF SUBSURFACE CONDITIONS AT OTHER LOCATIONS AND TIMES.

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PROJECT NO. W1301-06-01

BORING 2

ELEV. (MSL.) -- DATE COMPLETED **2/9/2021**

EQUIPMENT **HOLLOW STEM AUGER** BY: **JMH**

DEPTH IN FEET	SAMPLE NO.	LITHOLOGY	GROUNDWATER	SOIL CLASS (USCS)	MATERIAL DESCRIPTION	PENETRATION RESISTANCE (BLOWS/FT*)	DRY DENSITY (P.C.F.)	MOISTURE CONTENT (%)
0	BULK 0-5'				**ARTIFICIAL FILL** Silty Sand, poorly graded, loose, moist, brown, fine-grained.			
2								
4	B2@3'			ML	**ALLUVIUM** Sandy Silt, firm, moist, dark gray.	14	73.4	29.6
6	B2@6'				Clay, soft, wet, gray, high plasticity.	10	29.3	32.0
8								
10	B2@9'			CH	- firm, dark gray	15	73.9	49.8
12	B2@12'					15	87.2	35.9
14								
16	B2@15'				- soft	8	75.1	45.2
18								
20	B2@20'				- firm	17	101.7	27.4

Total depth of boring: 20.5 feet
Fill to 3 feet.
No groundwater encountered.
Backfilled with grout.

*Penetration resistance for 140-pound hammer falling 30 inches by auto-hammer.
NOTE: The stratification lines presented herein represent the approximate boundary between earth types; the transitions may be gradual.

W1301-06-01 BORING LOGS.GPJ

Figure A2,
Log of Boring 2, Page 1 of 1

SAMPLE SYMBOLS

- ☐ ... SAMPLING UNSUCCESSFUL
- ◧ ... STANDARD PENETRATION TEST
- ■ ... DRIVE SAMPLE (UNDISTURBED)
- ⊠ ... DISTURBED OR BAG SAMPLE
- ◪ ... CHUNK SAMPLE
- ▼ ... WATER TABLE OR SEEPAGE

NOTE: THE LOG OF SUBSURFACE CONDITIONS SHOWN HEREON APPLIES ONLY AT THE SPECIFIC BORING OR TRENCH LOCATION AND AT THE DATE INDICATED. IT IS NOT WARRANTED TO BE REPRESENTATIVE OF SUBSURFACE CONDITIONS AT OTHER LOCATIONS AND TIMES.

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PROJECT NO. W1301-06-01

BORING 3

ELEV. (MSL.) -- DATE COMPLETED **2/9/2021**

EQUIPMENT **HOLLOW STEM AUGER** BY: **JMH**

DEPTH IN FEET	SAMPLE NO.	LITHOLOGY	GROUNDWATER	SOIL CLASS (USCS)	MATERIAL DESCRIPTION	PENETRATION RESISTANCE (BLOWS/FT*)	DRY DENSITY (P.C.F.)	MOISTURE CONTENT (%)
0	BULK 0-5'				**ARTIFICIAL FILL** Sand, poorly graded, dense, moist, light brown, fine-grained, some medium-grained.			
2	B3@1.5'					50 (6")	107.1	4.0
4								
6	B3@5'					50 (6")		
8	B3@7'				- grayish brown, some fine gravel	50 (3")	103.4	8.7
10	B3@10'			MH	**ALLUVIUM** Silt, soft, moist, dark gray, high plasticity, some sand.	7		
12	B3@12.5'			CH	Clay, firm, moist, dark gray, high plasticity.	21	91.7	31.6
14								
16	B3@15'					10		
18	B3@17.5'		▼		Clay, firm, moist, dark gray.	14	103.7	26.1
20	B3@20'			CL	- soft, wet	3		
22	B3@22.5'				- firm, light brown	11	105.7	27.3
24								
26	B3@25'			CH	Clay, firm, moist, olive brown, some sand, trace gravel, high plasticity.	9		
28	B3@27.5'				- mottled calcium deposits, increase in sand	21	89.9	32.6

W1301-06-01 BORING LOGS.GPJ

Figure A3,
Log of Boring 3, Page 1 of 2

SAMPLE SYMBOLS

- ☐ ... SAMPLING UNSUCCESSFUL
- ◧ ... STANDARD PENETRATION TEST
- ■ ... DRIVE SAMPLE (UNDISTURBED)
- ⊠ ... DISTURBED OR BAG SAMPLE
- ◪ ... CHUNK SAMPLE
- ▼ ... WATER TABLE OR SEEPAGE

NOTE: THE LOG OF SUBSURFACE CONDITIONS SHOWN HEREON APPLIES ONLY AT THE SPECIFIC BORING OR TRENCH LOCATION AND AT THE DATE INDICATED. IT IS NOT WARRANTED TO BE REPRESENTATIVE OF SUBSURFACE CONDITIONS AT OTHER LOCATIONS AND TIMES.

GEOCON

PROJECT NO. W1301-06-01

BORING 3

ELEV. (MSL.) -- DATE COMPLETED **2/9/2021**

EQUIPMENT **HOLLOW STEM AUGER** BY: **JMH**

DEPTH IN FEET	SAMPLE NO.	LITHOLOGY	GROUNDWATER	SOIL CLASS (USCS)	MATERIAL DESCRIPTION	PENETRATION RESISTANCE (BLOWS/FT*)	DRY DENSITY (P.C.F.)	MOISTURE CONTENT (%)
30	B3@30'				- decrease in sand	11		
32	B3@32.5'			CH	- stiff	22	98.4	27.3
34	B3@35'				- firm, increase in sand	13		
36								
38	B3@37.5'				Silty Sand, poorly graded, dense, wet, olive brown, fine-grained.	67	117.6	16.4
40	B3@40'			SM		33		
42	B3@42.5'				- medium dense, trace shells	36	101.9	25.0
44				CL	Sandy Clay, soft, wet, olive brown.			
46	B3@45'					7		
48	B3@47.5'			SC	Clayey Sand, poorly graded, medium dense, saturated, olive brown with oxidation mottles, fine-grained.	20	100.0	25.4
50	B3@50'			SM	Silty Sand, poorly graded, medium dense, saturated, olive brown.	25		

Total depth of boring: 51 feet
Fill to 9 feet.
Groundwater encountered at 17.6 feet.
Backfilled with grout.

*Penetration resistance for 140-pound hammer falling 30 inches by auto-hammer.
NOTE: The stratification lines presented herein represent the approximate boundary between earth types; the transitions may be gradual.

W1301-06-01 BORING LOGS.GPJ

Figure A3,
Log of Boring 3, Page 2 of 2

SAMPLE SYMBOLS

- ... SAMPLING UNSUCCESSFUL
- ... STANDARD PENETRATION TEST
- ... DRIVE SAMPLE (UNDISTURBED)
- ... DISTURBED OR BAG SAMPLE
- ... CHUNK SAMPLE
- ... WATER TABLE OR SEEPAGE

NOTE: THE LOG OF SUBSURFACE CONDITIONS SHOWN HEREON APPLIES ONLY AT THE SPECIFIC BORING OR TRENCH LOCATION AND AT THE DATE INDICATED. IT IS NOT WARRANTED TO BE REPRESENTATIVE OF SUBSURFACE CONDITIONS AT OTHER LOCATIONS AND TIMES.

PROJECT NO. W1301-06-01

BORING 4

ELEV. (MSL.) -- DATE COMPLETED **2/9/2021**

EQUIPMENT **HOLLOW STEM AUGER** BY: **JMH**

DEPTH IN FEET	SAMPLE NO.	LITHOLOGY	GROUNDWATER	SOIL CLASS (USCS)	MATERIAL DESCRIPTION	PENETRATION RESISTANCE (BLOWS/FT*)	DRY DENSITY (P.C.F.)	MOISTURE CONTENT (%)
0	BULK 0-5'				**ARTIFICIAL FILL** Silty Sand, poorly graded, dense, moist, brown, fine-grained, some medium-grained, some gravel.			
2								
4	B4@3'					50 (6")		
6	B4@5'			ML	**ALLUVIUM** Sandy Silt, soft, moist, dark gray.	10	78.1	31.1
8	B4@7.5'				Clay, soft, wet, dark gray, high plasticity.	10	80.7	38.9
10	B4@10'					8	77.8	42.4
12				CH				
14								
16	B4@15'					10	85.0	38.5
18								
20	B4@20'					4	80.0	42.3

Total depth of boring: 20.5 feet
Fill to 5 feet.
No groundwater encountered.
Backfilled with grout.

*Penetration resistance for 140-pound hammer falling 30 inches by auto-hammer.
NOTE: The stratification lines presented herein represent the approximate boundary between earth types; the transitions may be gradual.

W1301-06-01 BORING LOGS.GPJ

Figure A4,
Log of Boring 4, Page 1 of 1

SAMPLE SYMBOLS

- ☐ ... SAMPLING UNSUCCESSFUL
- ◧ ... STANDARD PENETRATION TEST
- ■ ... DRIVE SAMPLE (UNDISTURBED)
- ⊠ ... DISTURBED OR BAG SAMPLE
- ◥ ... CHUNK SAMPLE
- ▼ ... WATER TABLE OR SEEPAGE

NOTE: THE LOG OF SUBSURFACE CONDITIONS SHOWN HEREON APPLIES ONLY AT THE SPECIFIC BORING OR TRENCH LOCATION AND AT THE DATE INDICATED. IT IS NOT WARRANTED TO BE REPRESENTATIVE OF SUBSURFACE CONDITIONS AT OTHER LOCATIONS AND TIMES.

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PROJECT NO. W1301-06-01

BORING 5

ELEV. (MSL.) -- DATE COMPLETED **2/9/2021**

EQUIPMENT **HOLLOW STEM AUGER** BY: **JMH**

DEPTH IN FEET	SAMPLE NO.	LITHOLOGY	GROUNDWATER	SOIL CLASS (USCS)	MATERIAL DESCRIPTION	PENETRATION RESISTANCE (BLOWS/FT*)	DRY DENSITY (P.C.F.)	MOISTURE CONTENT (%)
0					**ARTIFICIAL FILL** Silty Sand, poorly graded, loose, moist, brown, fine-grained, some medium-grained.			
2								
4								
6	B5@5'				**ALLUVIUM** Clay, soft, moist, dark gray, high plasticity.	11	79.5	42.3
8	B5@7.5'				- wet	10	82.2	38.4
10	B5@10'			CH		7	74.1	37.5
12								
14								
16	B5@15'				- saturated	11	97.9	47.5
18								
20	B5@20'				- firm, no recovery	17		

Total depth of boring: 20.5 feet
Fill to 5 feet.
No groundwater encountered.
Backfilled with grout.

*Penetration resistance for 140-pound hammer falling 30 inches by auto-hammer.
NOTE: The stratification lines presented herein represent the approx

W1301-06-01 BORING LOGS.GPJ

Figure A5,
Log of Boring 5, Page 1 of 1

SAMPLE SYMBOLS

- ☐ ... SAMPLING UNSUCCESSFUL
- ◧ ... STANDARD PENETRATION TEST
- ■ ... DRIVE SAMPLE (UNDISTURBED)
- ⊠ ... DISTURBED OR BAG SAMPLE
- ◪ ... CHUNK SAMPLE
- ▼ ... WATER TABLE OR SEEPAGE

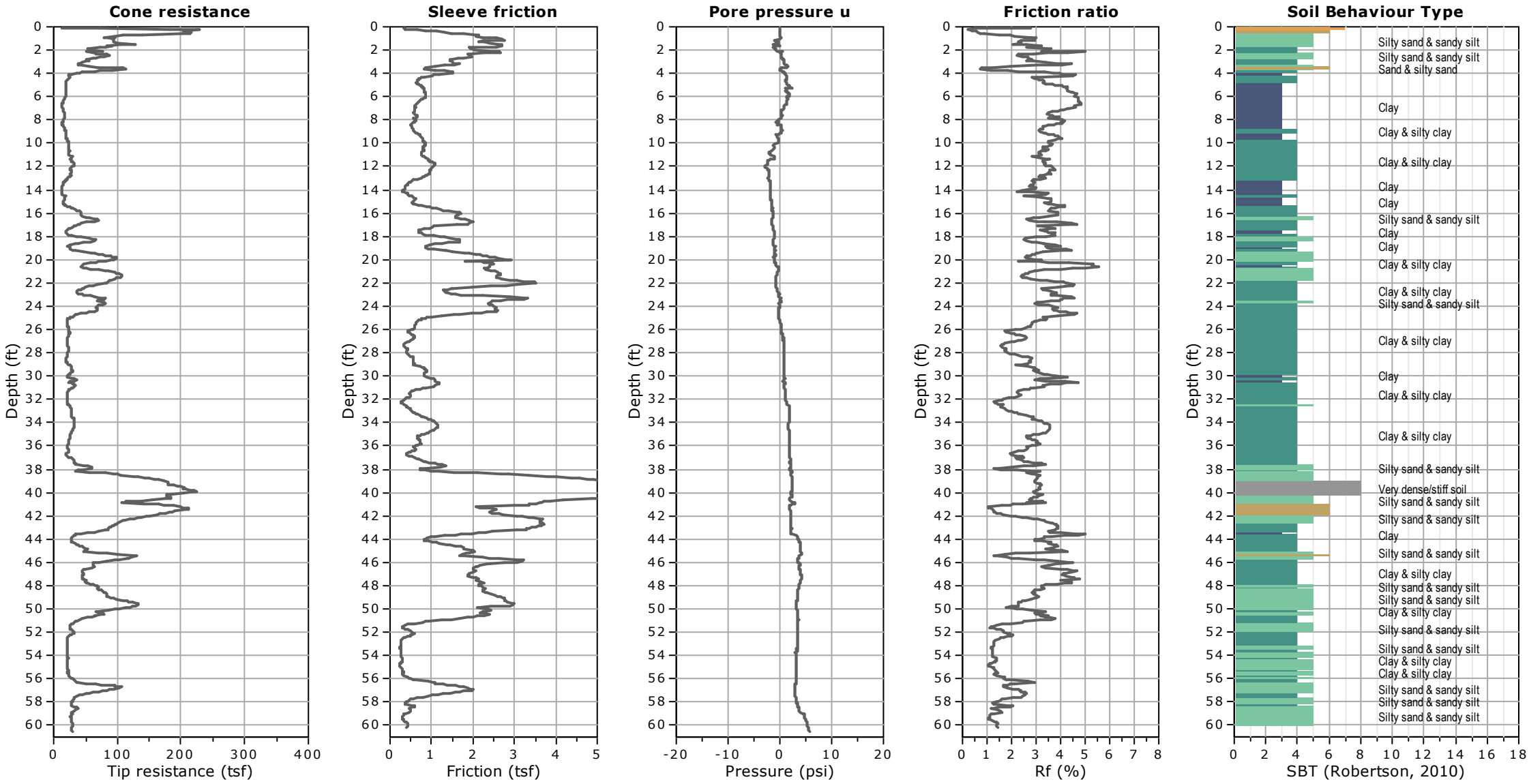
NOTE: THE LOG OF SUBSURFACE CONDITIONS SHOWN HEREON APPLIES ONLY AT THE SPECIFIC BORING OR TRENCH LOCATION AND AT THE DATE INDICATED. IT IS NOT WARRANTED TO BE REPRESENTATIVE OF SUBSURFACE CONDITIONS AT OTHER LOCATIONS AND TIMES.

GEOCON

Kehoe Testing and Engineering
714-901-7270
steve@kehoetesting.com
www.kehoetesting.com

Project: **Geocon West / Faring Perry Street**
Location: **Carson, CA**

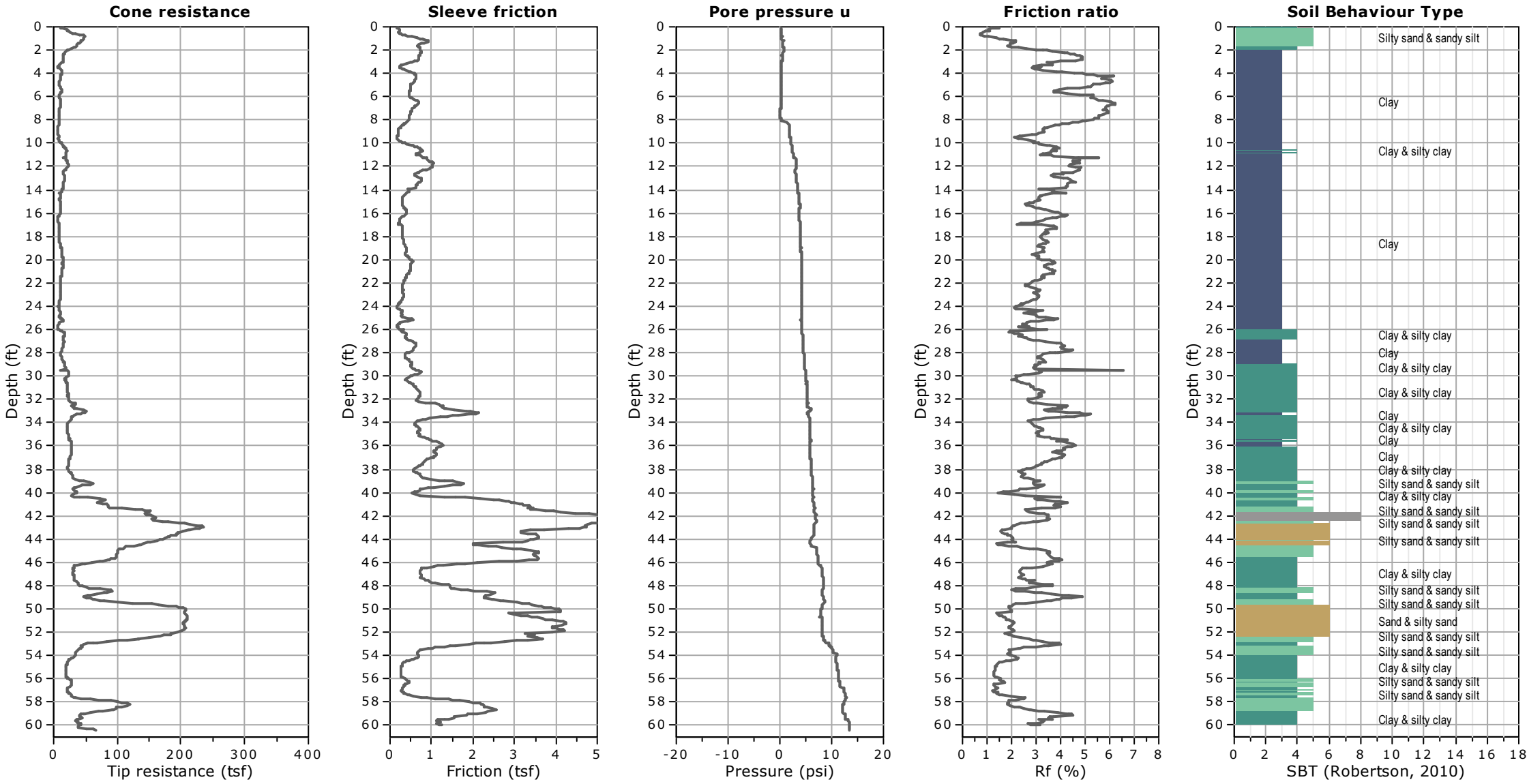
CPT-1
Total depth: 60.51 ft, Date: 2/9/2021



Kehoe Testing and Engineering
714-901-7270
steve@kehoetesting.com
www.kehoetesting.com

Project: Geocon West / Faring Perry Street
Location: Carson, CA

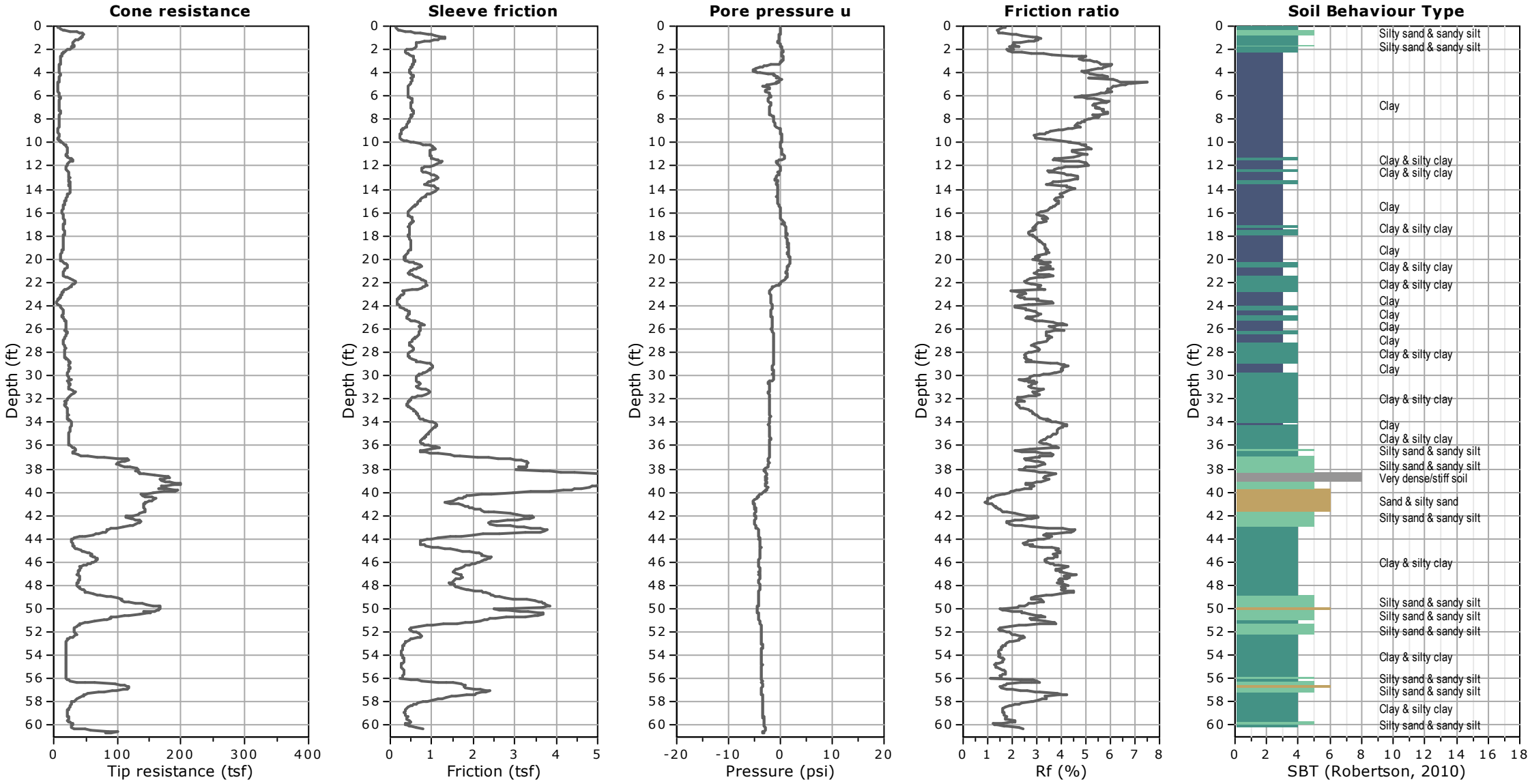
CPT-2
Total depth: 60.38 ft, Date: 2/9/2021



Kehoe Testing and Engineering
714-901-7270
steve@kehoetesting.com
www.kehoetesting.com

Project: Geocon West / Faring Perry Street
Location: Carson, CA

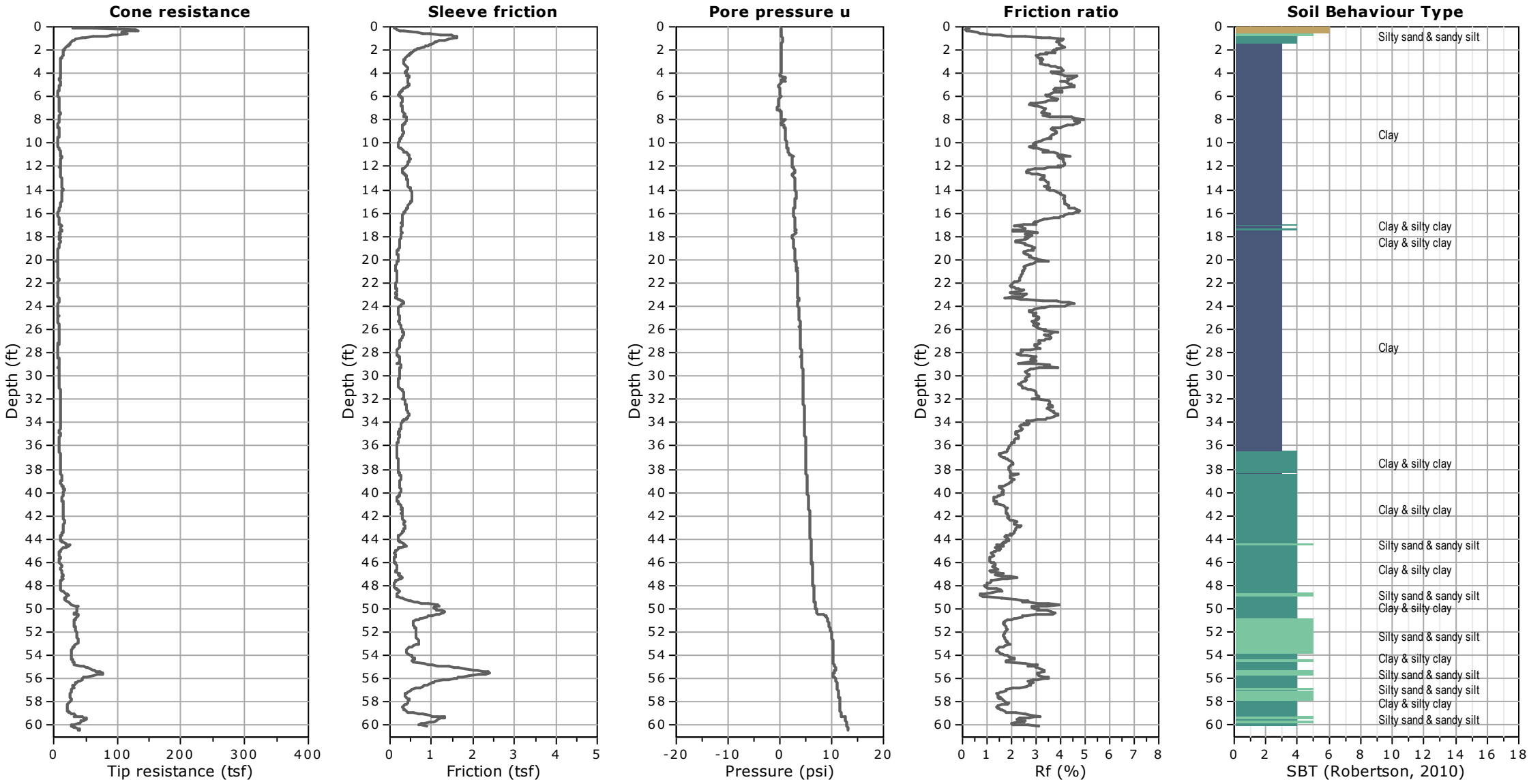
CPT-3
Total depth: 60.63 ft, Date: 2/9/2021



Kehoe Testing and Engineering
714-901-7270
steve@kehoetesting.com
www.kehoetesting.com

Project: Geocon West / Faring Perry Street
Location: Carson, CA

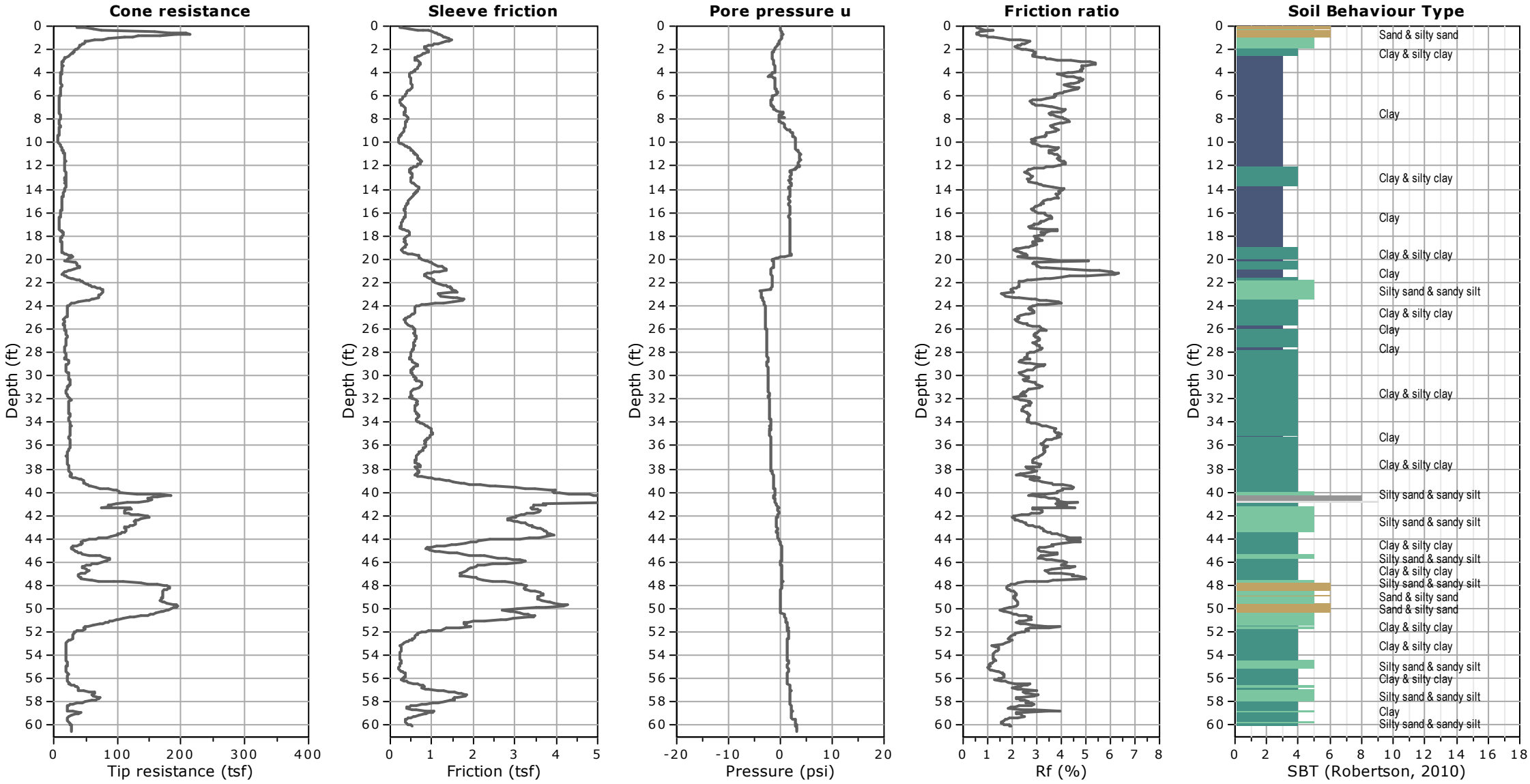
CPT-4
Total depth: 60.47 ft, Date: 2/9/2021



Kehoe Testing and Engineering
714-901-7270
steve@kehoetesting.com
www.kehoetesting.com

Project: **Geocon West / Faring Perry Street**
Location: **Carson, CA**

CPT-5
Total depth: 60.51 ft, Date: 2/9/2021

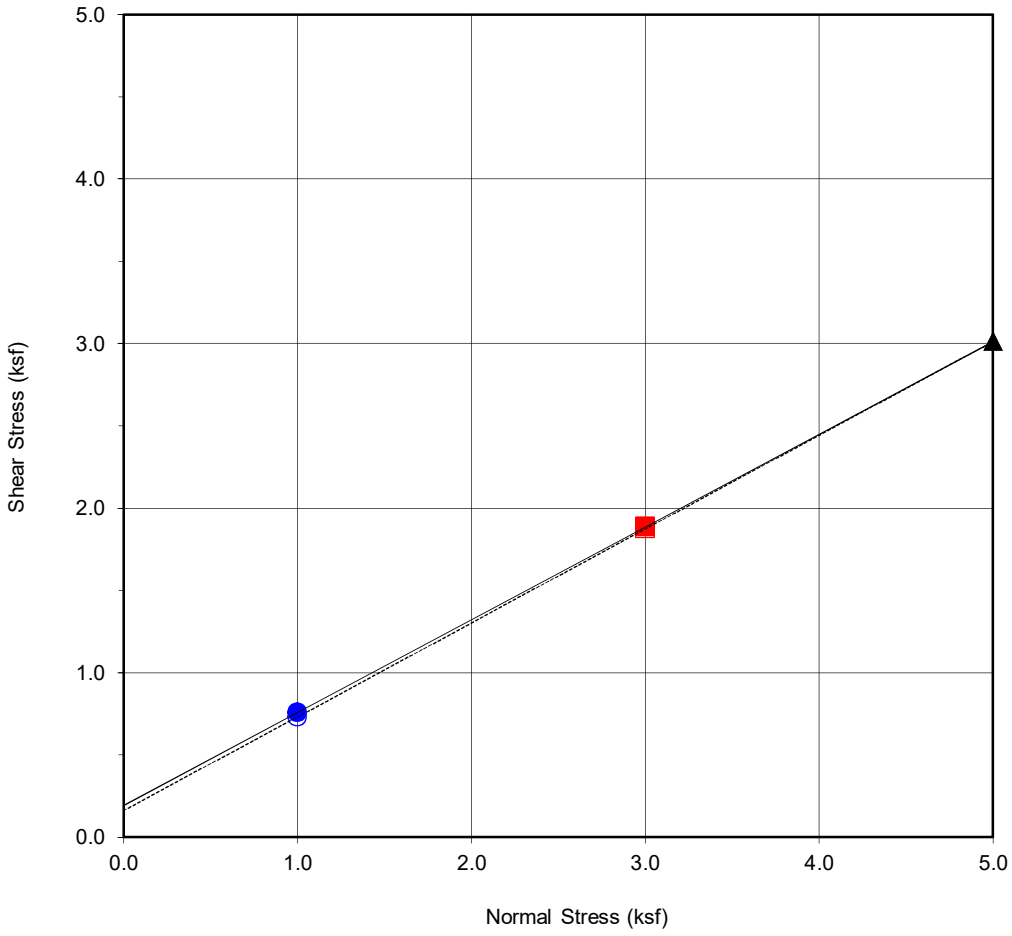


APPENDIX B

APPENDIX B

LABORATORY TESTING

Laboratory tests were performed in accordance with generally accepted test methods of the "American Society for Testing and Materials (ASTM)", or other suggested procedures. Selected samples were tested for direct shear strength, consolidation, plasticity indices, grain size, moisture density relationship, expansion characteristics, corrosivity and in-place dry density and moisture content. The results of the laboratory tests are summarized in Figures B1 through B23. The in-place dry density and moisture content of the samples tested are presented on the boring logs, Appendix A.



Boring No.	**B1 + B2**
Sample No.	**B1B2@0-5'**
Depth (ft)	**0-5'**
Sample Type:	Ring

Soil Identification:		
Brown Silty Sand (SM)		
Strength Parameters		
	C (psf)	ϕ (^{o})
Peak	192	29.4
Ultimate	162	29.7

Normal Strest (kip/ft2)	1	3	5
Peak Shear Stress (kip/ft²)	● 0.76	■ 1.88	▲ 3.01
Shear Stress @ End of Test (ksf)	○ 0.73	□ 1.87	△ 3.01
Deformation Rate (in./min.)	0.05	0.05	0.05
Initial Sample Height (in.)	1.0	1.0	1.0
Ring Inside Diameter (in.)	2.375	2.375	2.375
Initial Moisture Content (%)	13.6	14.5	14.1
Initial Dry Density (pcf)	101.0	101.0	101.0
Initial Degree of Saturation (%)	54.7	58.3	56.7
Soil Height Before Shearing (in.)	1.2	1.2	1.2
Final Moisture Content (%)	24.4	22.1	23.4

GEOCON

DIRECT SHEAR TEST RESULTS

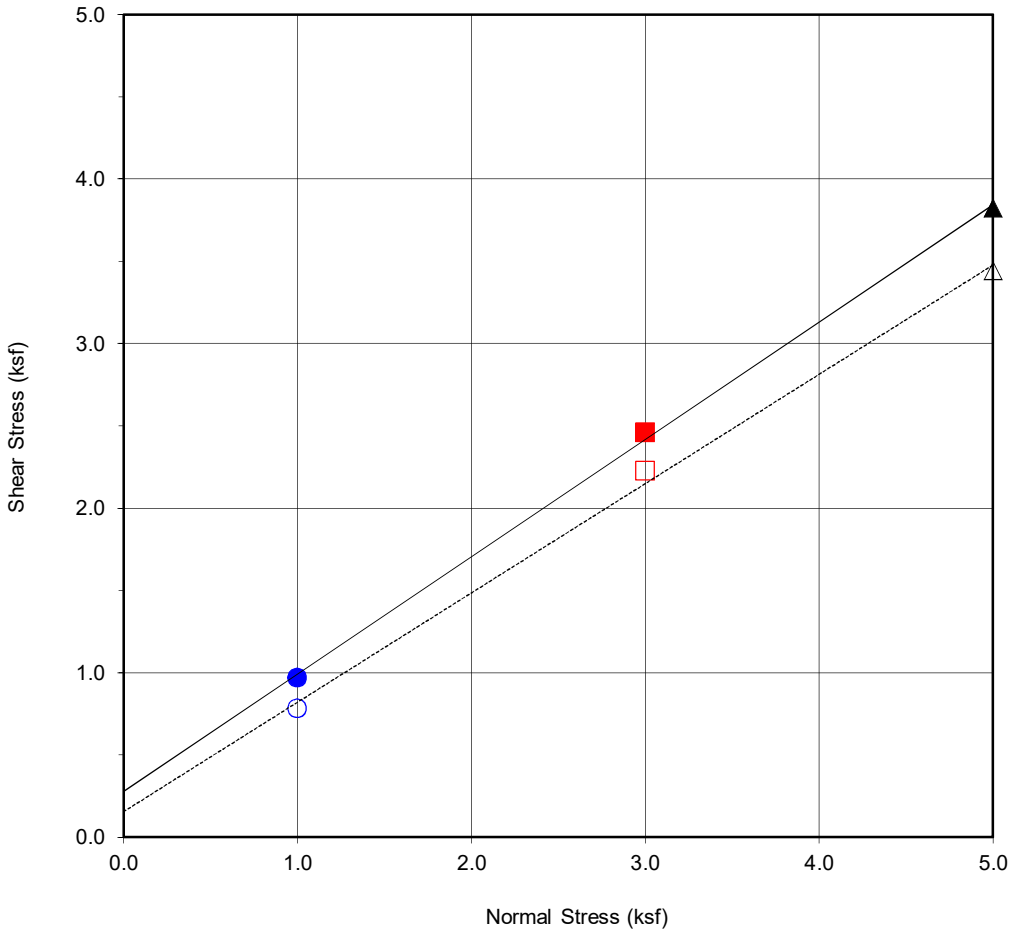
Consolidated Drained ASTM D-3080

Checked by: JMH

Project No.: W1301-06-01

21611 SOUTH PERRY STREET
CARSON, CALIFORNIA

APRIL 2021 Figure B1



Boring No.	**B3 + B4**
Sample No.	**B3B4@0-5'**
Depth (ft)	**0-5'**
Sample Type:	Ring

Soil Identification:		
Light Brown Silty Sand (SM)		
Strength Parameters		
	C (psf)	ϕ (^{o})
Peak	276	35.5
Ultimate	155	33.6

Normal Strest (kip/ft2)	1	3	5
Peak Shear Stress (kip/ft²)	● 0.97	■ 2.46	▲ 3.82
Shear Stress @ End of Test (ksf)	○ 0.78	□ 2.22	△ 3.44
Deformation Rate (in./min.)	0.05	0.05	0.05
Initial Sample Height (in.)	1.0	1.0	1.0
Ring Inside Diameter (in.)	2.375	2.375	2.375
Initial Moisture Content (%)	8.2	8.0	7.6
Initial Dry Density (pcf)	114.0	114.0	114.0
Initial Degree of Saturation (%)	46.3	44.9	42.7
Soil Height Before Shearing (in.)	1.2	1.2	1.2
Final Moisture Content (%)	14.2	14.9	14.1

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DIRECT SHEAR TEST RESULTS

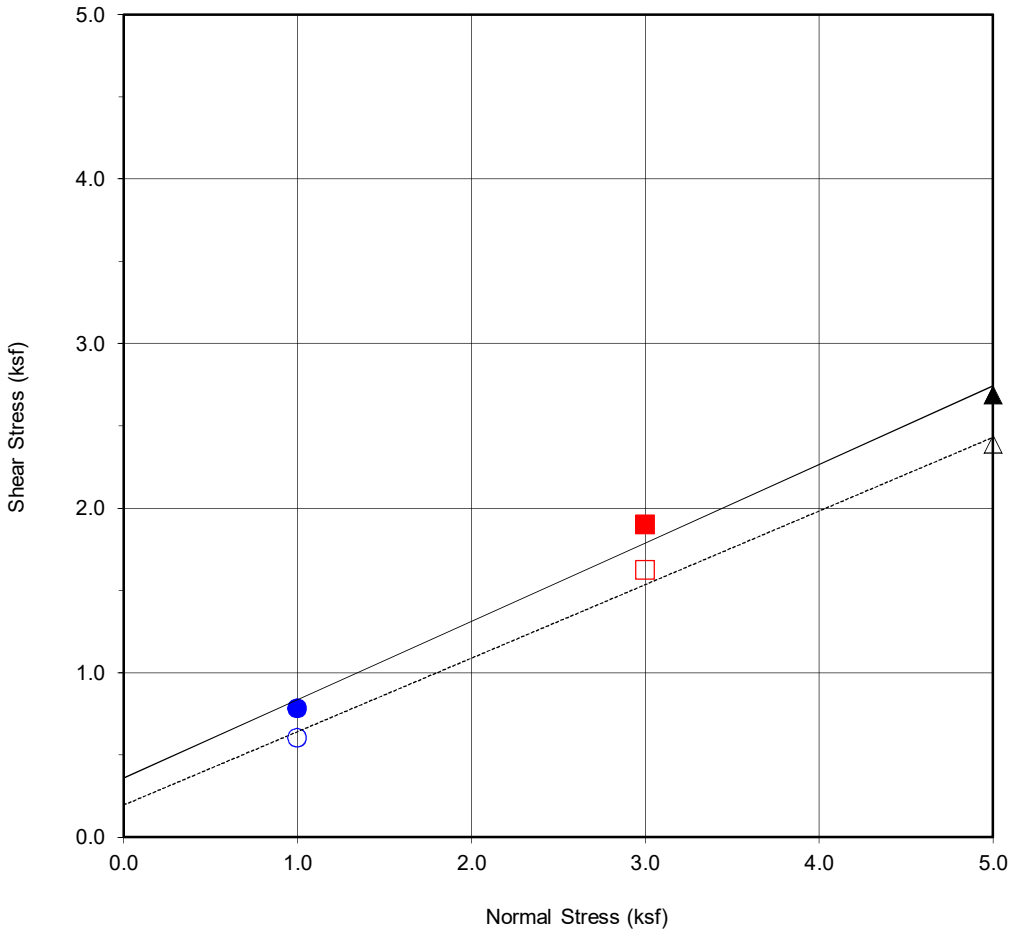
Consolidated Drained ASTM D-3080

Checked by: JMH

Project No.: W1301-06-01

21611 SOUTH PERRY STREET
CARSON, CALIFORNIA

APRIL 2021 Figure B2



Boring No.	**B2**
Sample No.	**B2@3'**
Depth (ft)	**3**
Sample Type:	Ring

Soil Identification:
Dark Gray Sandy Silt (ML)

Strength Parameters		
	C (psf)	ϕ (^{o})
Peak	357	25.5
Ultimate	195	24.1

Normal Strest (kip/ft2)	1	3	5
Peak Shear Stress (kip/ft²)	● 0.78	■ 1.90	▲ 2.69
Shear Stress @ End of Test (ksf)	○ 0.60	□ 1.62	△ 2.39
Deformation Rate (in./min.)	0.05	0.05	0.05
Initial Sample Height (in.)	1.0	1.0	1.0
Ring Inside Diameter (in.)	2.375	2.375	2.375
Initial Moisture Content (%)	34.1	36.8	37.9
Initial Dry Density (pcf)	80.3	83.9	82.9
Initial Degree of Saturation (%)	83.8	98.3	98.9
Soil Height Before Shearing (in.)	1.2	1.2	1.2
Final Moisture Content (%)	40.3	37.8	36.6

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DIRECT SHEAR TEST RESULTS

Consolidated Drained ASTM D-3080

Checked by: JMH

Project No.: W1301-06-01

21611 SOUTH PERRY STREET
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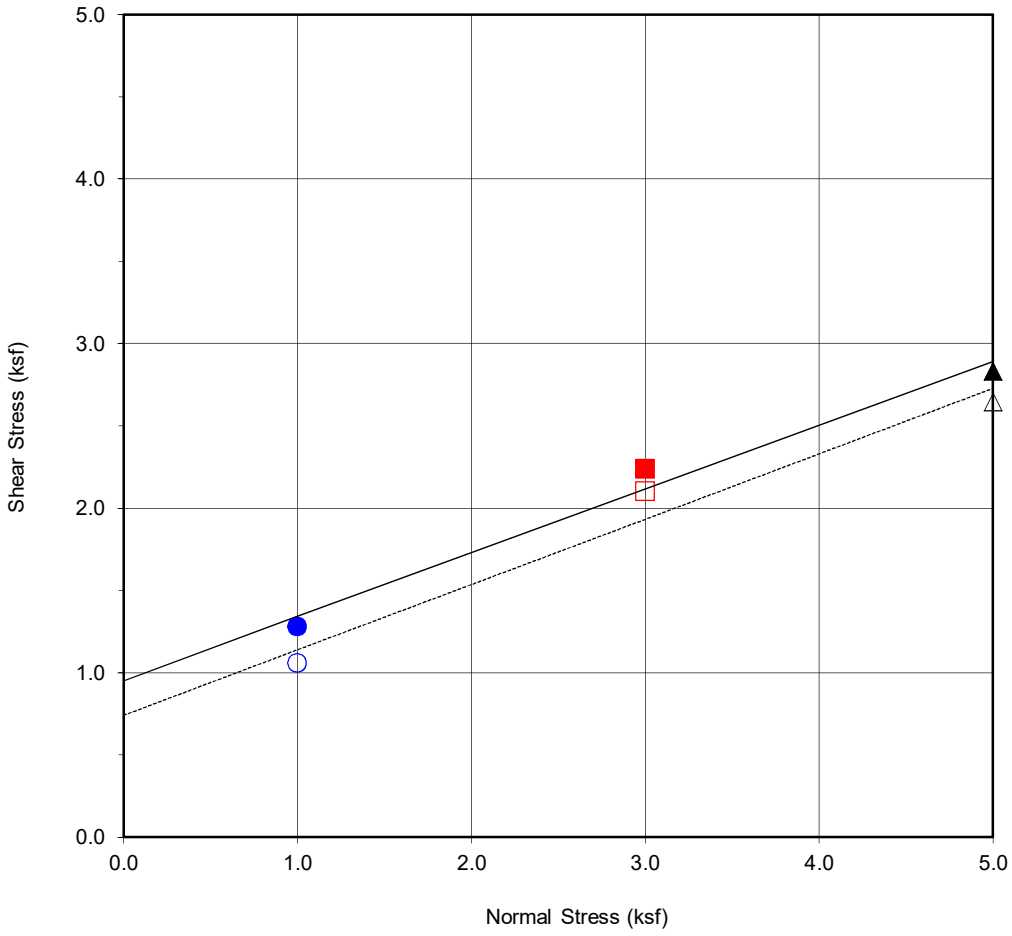
APRIL 2021 Figure B3



Boring No.	**B1**
Sample No.	**B1@5'**
Depth (ft)	**5**
Sample Type:	Ring

Soil Identification:		
Dark Gray Clay (CH)		
Strength Parameters		
	C (psf)	ϕ (^{o})
Peak	951	21.2
Ultimate	740	21.7

Normal Strest (kip/ft2)	1	3	5
Peak Shear Stress (kip/ft²)	● 1.28	■ 2.24	▲ 2.83
Shear Stress @ End of Test (ksf)	○ 1.06	□ 2.10	△ 2.65
Deformation Rate (in./min.)	0.05	0.05	0.05
Initial Sample Height (in.)	1.0	1.0	1.0
Ring Inside Diameter (in.)	2.375	2.375	2.375
Initial Moisture Content (%)	22.9	22.4	22.6
Initial Dry Density (pcf)	103.1	102.5	102.3
Initial Degree of Saturation (%)	97.2	93.9	94.3
Soil Height Before Shearing (in.)	1.2	1.2	1.2
Final Moisture Content (%)	26.0	24.1	23.0

GEOCON

DIRECT SHEAR TEST RESULTS

Consolidated Drained ASTM D-3080

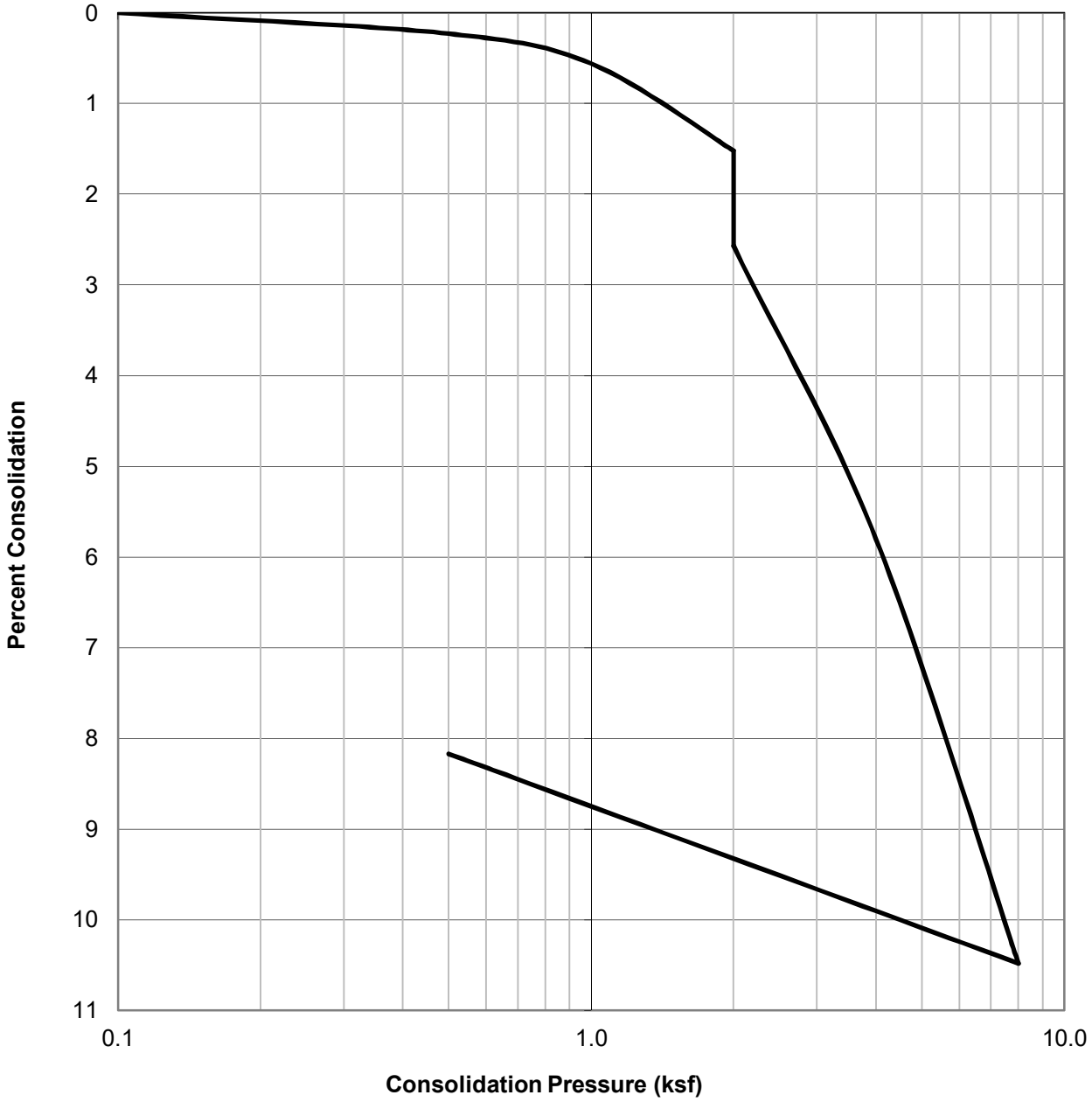
Checked by: JMH

Project No.: W1301-06-01

21611 SOUTH PERRY STREET
CARSON, CALIFORNIA

APRIL 2021 Figure B4

WATER ADDED AT 2.0 KSF



SAMPLE ID.	SOIL TYPE	DRY DENSITY (PCF)	INITIAL MOISTURE (%)	FINAL MOISTURE (%)
B2@3	Dark Gray Sandy Silt (ML)	76.2	32.7	37.3

GEOCON

CONSOLIDATION TEST RESULTS

ASTM D-2435

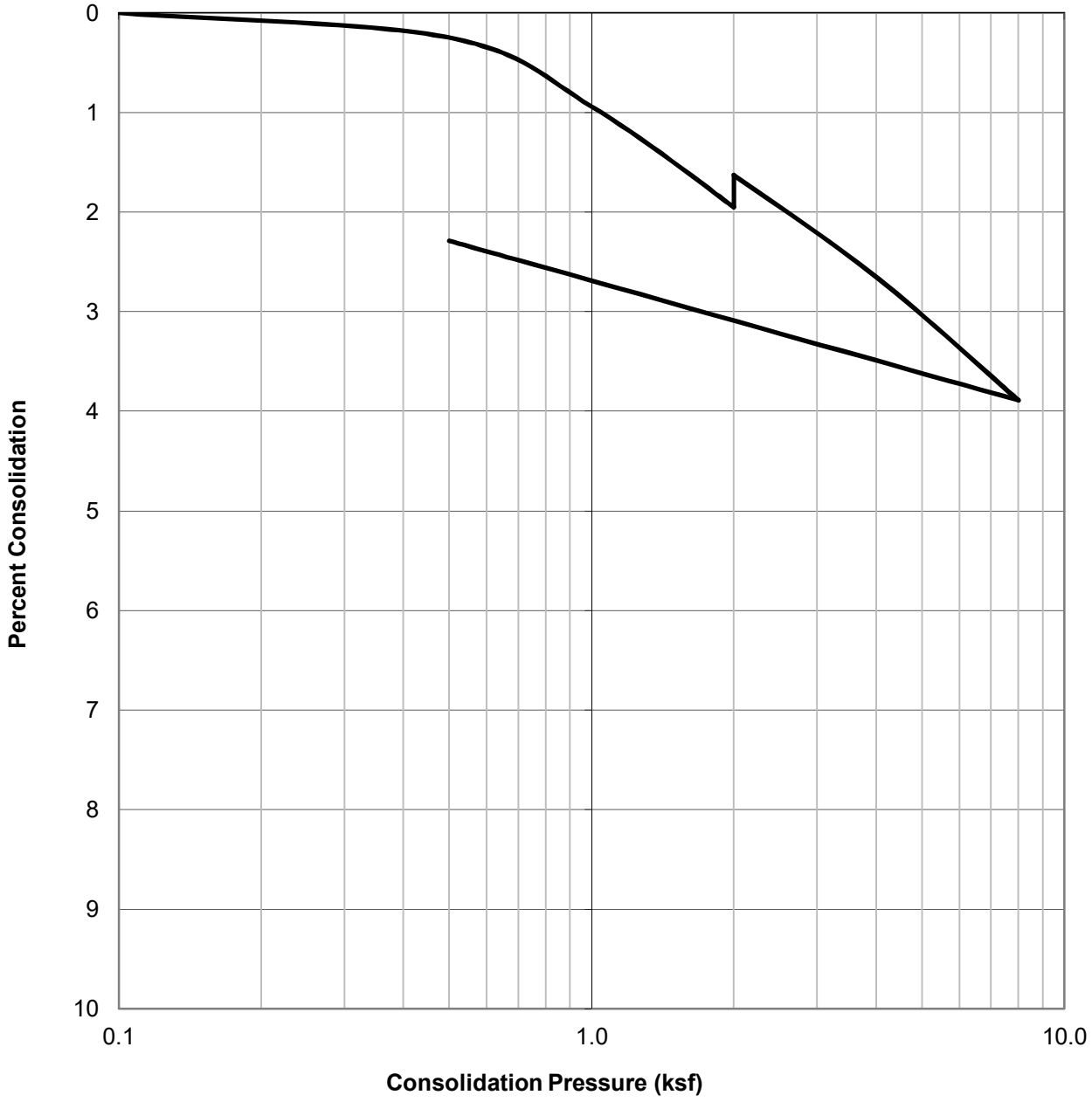
Checked by: JMH

Project No.: W1301-06-01

21611 SOUTH PERRY STREET
CARSON, CALIFORNIA

APRIL 2021 Figure B5

WATER ADDED AT 2.0 KSF



SAMPLE ID.	SOIL TYPE	DRY DENSITY (PCF)	INITIAL MOISTURE (%)	FINAL MOISTURE (%)
B1@5	Dark Gray Clay (CH)	101.8	24.0	24.3

GEOCON

CONSOLIDATION TEST RESULTS

ASTM D-2435

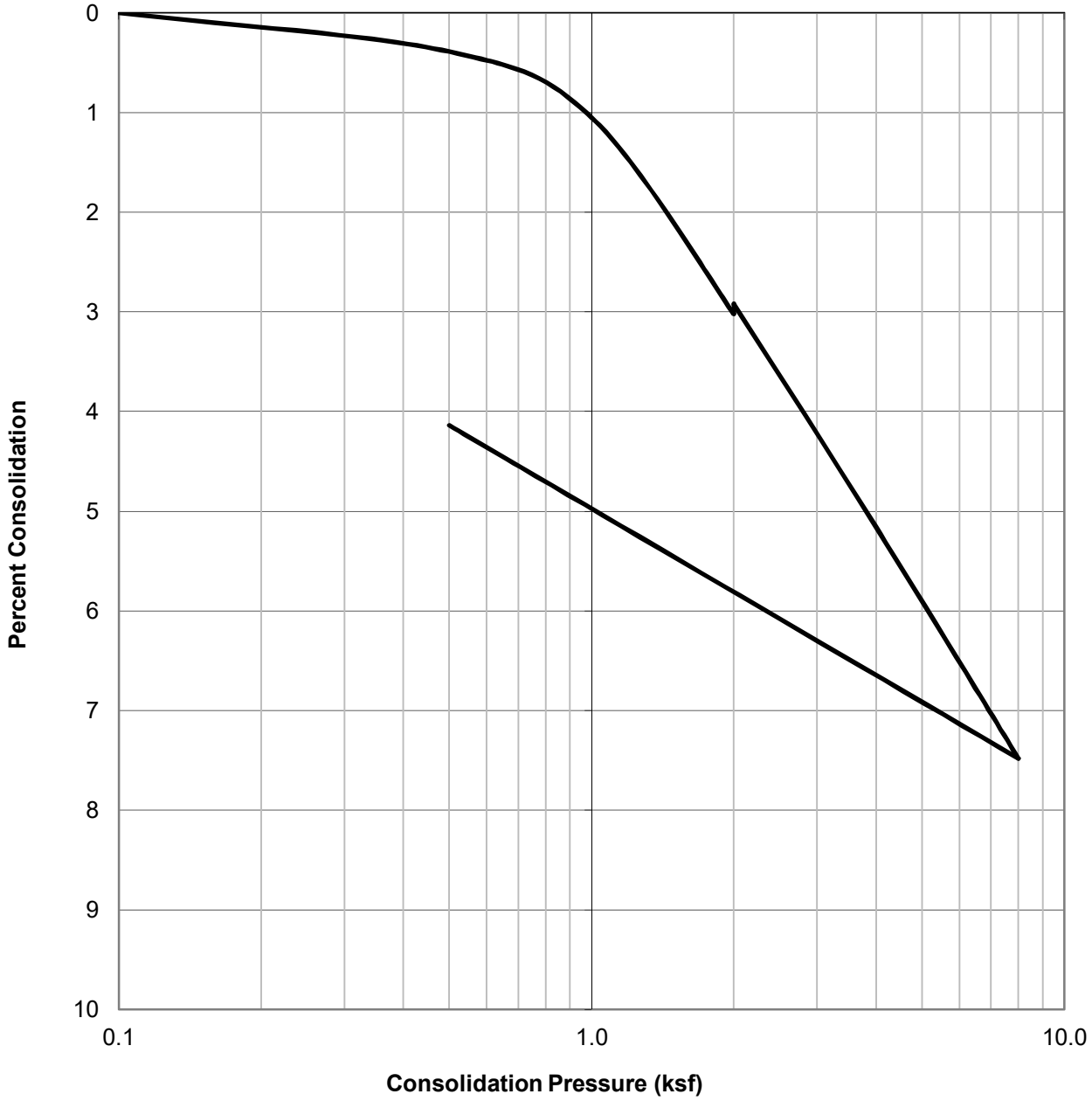
Checked by: JMH

Project No.: W1301-06-01

21611 SOUTH PERRY STREET
CARSON, CALIFORNIA

APRIL 2021 Figure B6

WATER ADDED AT 2.0 KSF



SAMPLE ID.	SOIL TYPE	DRY DENSITY (PCF)	INITIAL MOISTURE (%)	FINAL MOISTURE (%)
B5@5	Dark Gray Clay (CH)	81.9	38.4	39.2

GEOCON

CONSOLIDATION TEST RESULTS

ASTM D-2435

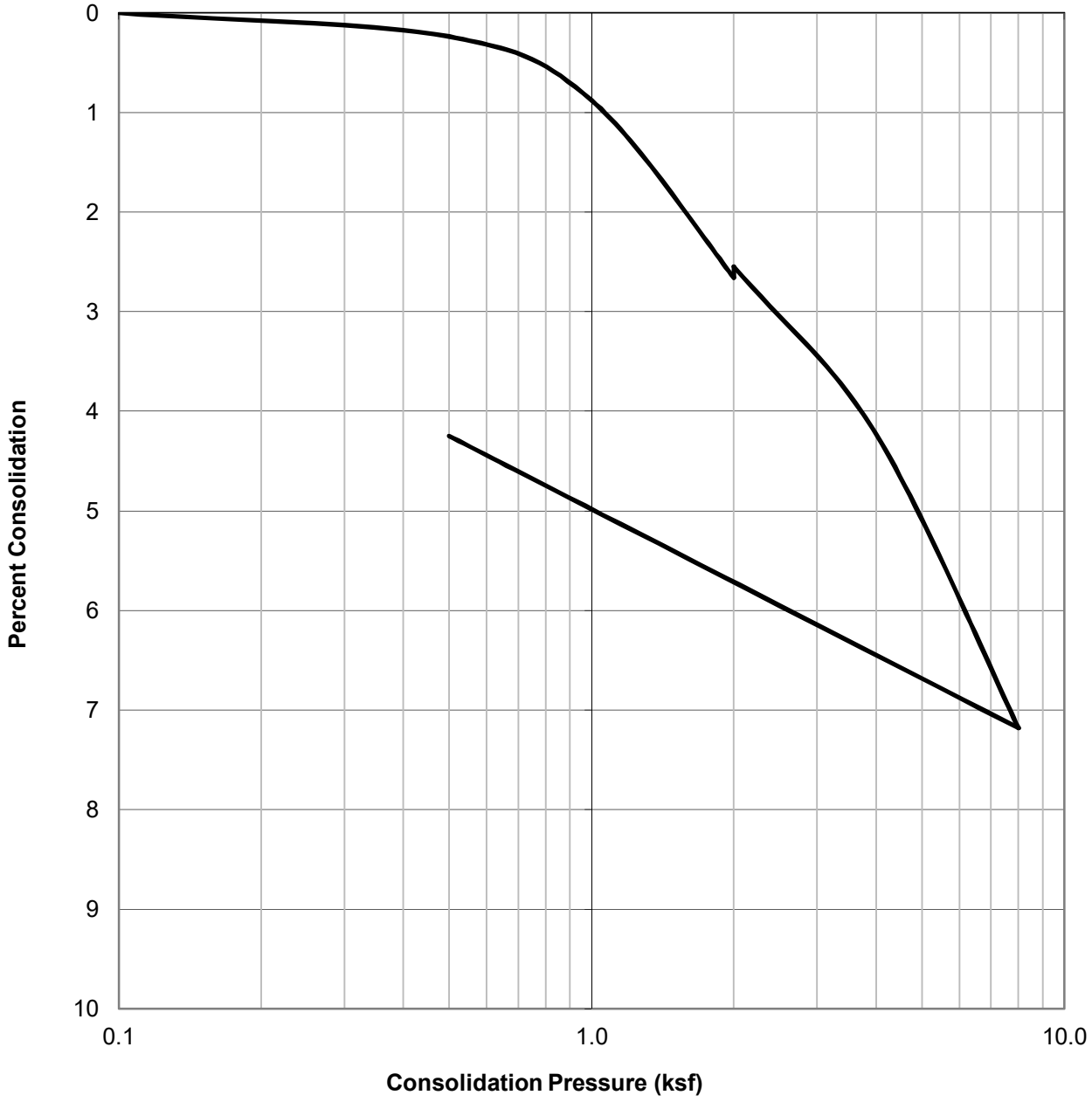
Checked by: JMH

Project No.: W1301-06-01

21611 SOUTH PERRY STREET
CARSON, CALIFORNIA

APRIL 2021 Figure B7

WATER ADDED AT 2.0 KSF



SAMPLE ID.	SOIL TYPE	DRY DENSITY (PCF)	INITIAL MOISTURE (%)	FINAL MOISTURE (%)
B4@7.5	Dark Gray Clay (CH)	80.9	38.9	38.0

GEOCON

CONSOLIDATION TEST RESULTS

ASTM D-2435

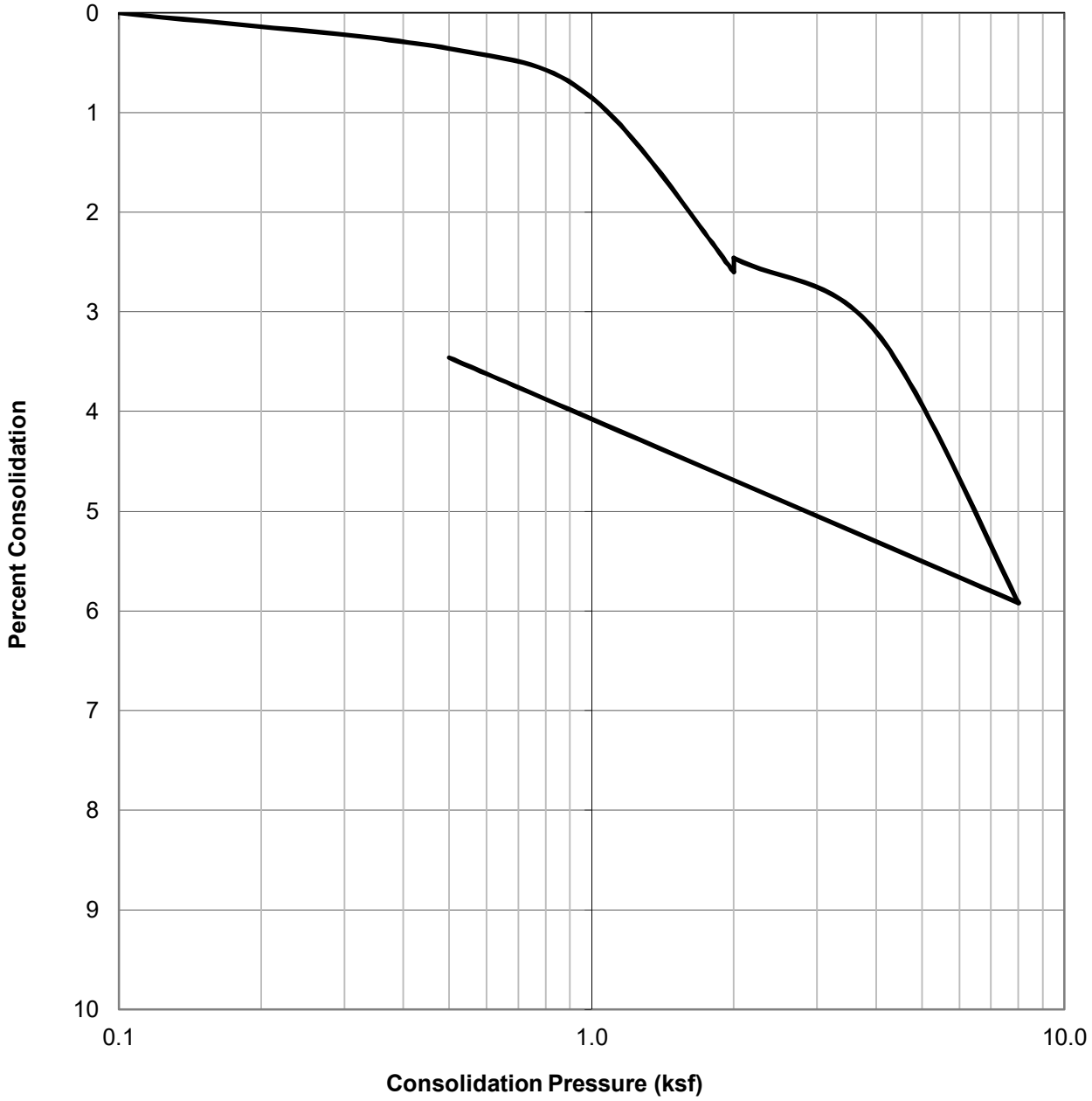
Checked by: JMH

Project No.: W1301-06-01

21611 SOUTH PERRY STREET
CARSON, CALIFORNIA

APRIL 2021 Figure B8

WATER ADDED AT 2.0 KSF



SAMPLE ID.	SOIL TYPE	DRY DENSITY (PCF)	INITIAL MOISTURE (%)	FINAL MOISTURE (%)
B2@9	Dark Gray Clay (CH)	70.9	49.8	48.8

GEOCON

CONSOLIDATION TEST RESULTS

ASTM D-2435

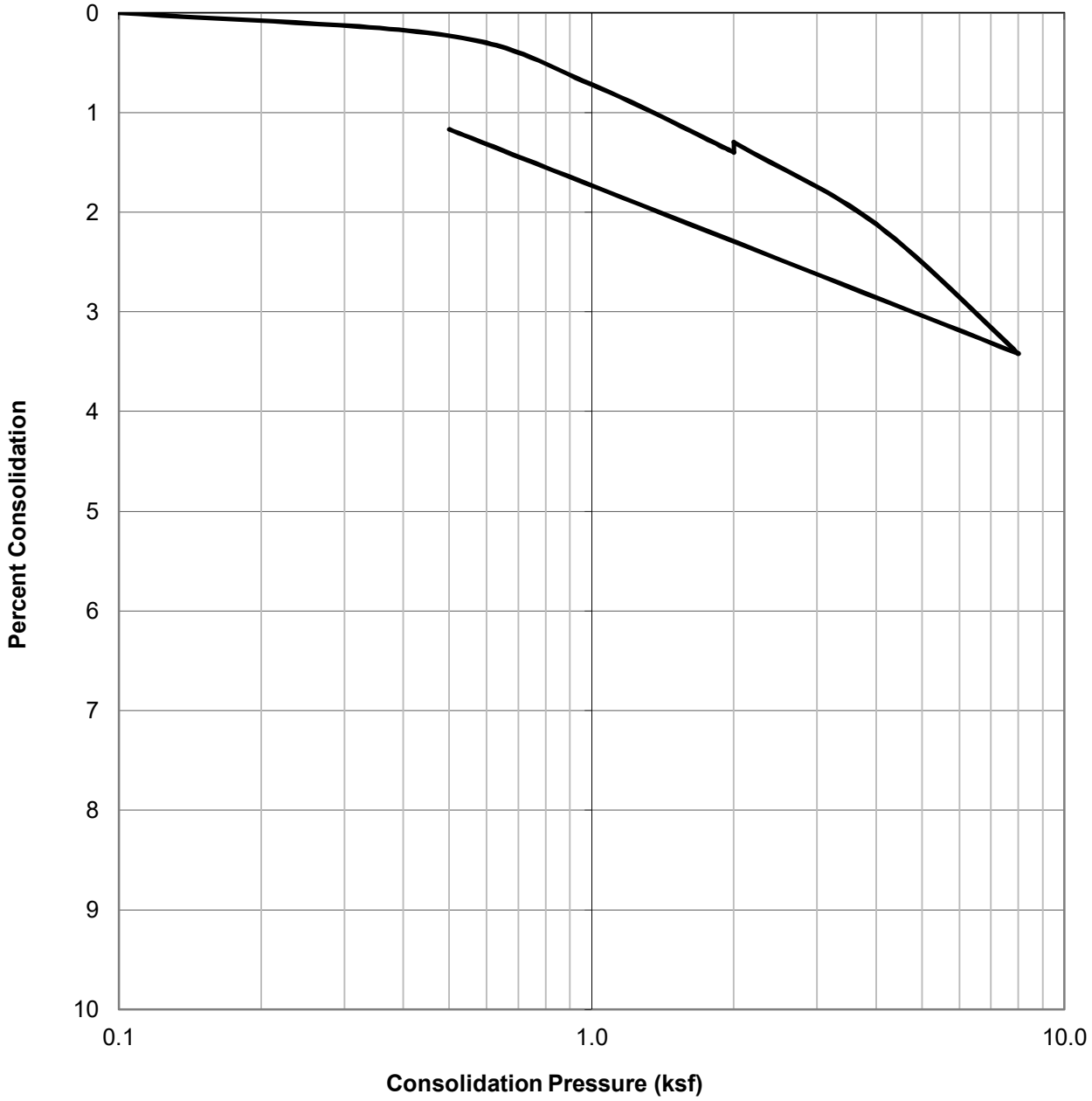
Checked by: JMH

Project No.: W1301-06-01

21611 SOUTH PERRY STREET
CARSON, CALIFORNIA

APRIL 2021 Figure B9

WATER ADDED AT 2.0 KSF



SAMPLE ID.	SOIL TYPE	DRY DENSITY (PCF)	INITIAL MOISTURE (%)	FINAL MOISTURE (%)
B1@10	Olive Brown Clay (CH)	105.4	22.0	22.8

GEOCON

CONSOLIDATION TEST RESULTS

ASTM D-2435

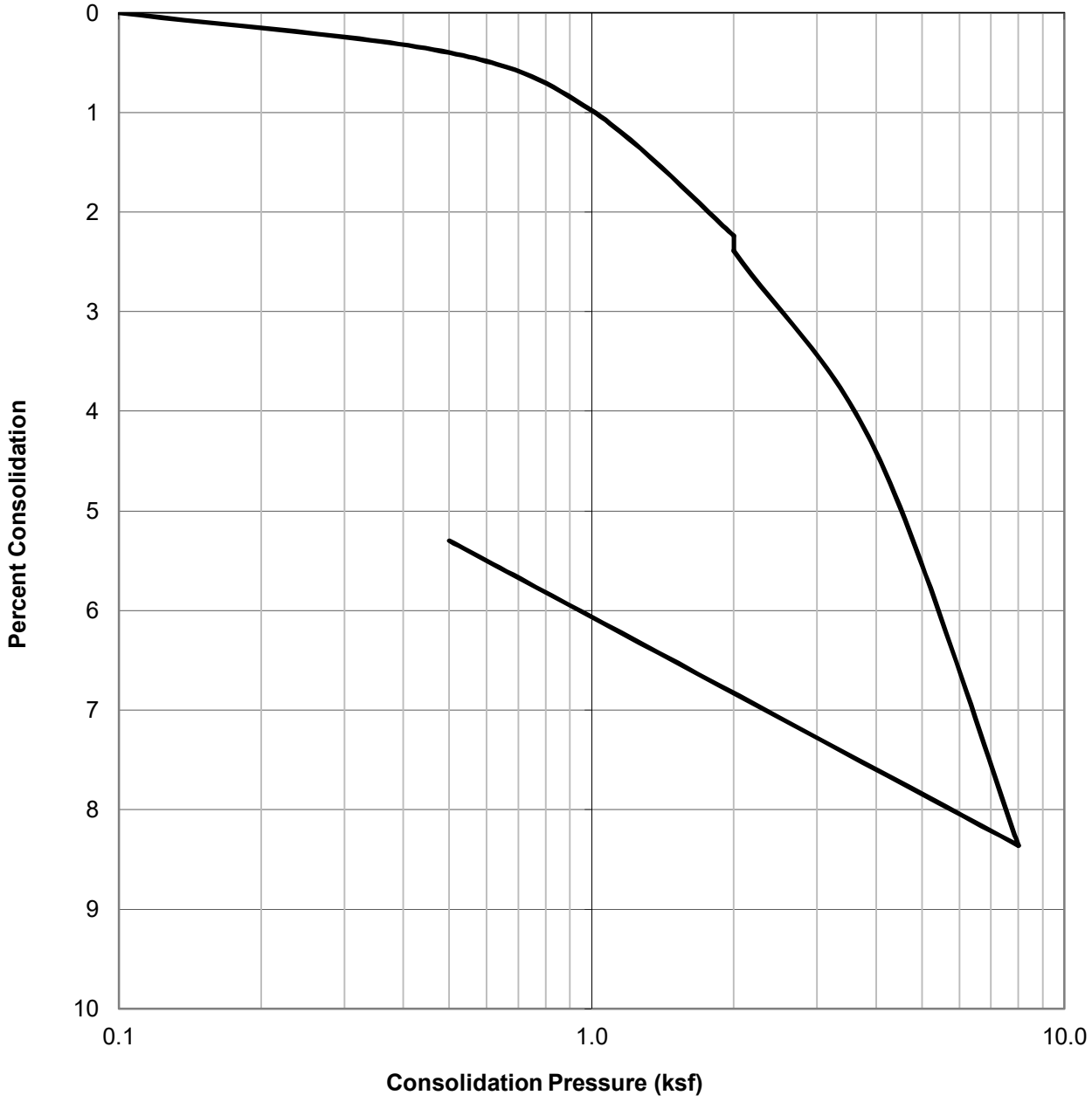
Checked by: JMH

Project No.: W1301-06-01

21611 SOUTH PERRY STREET
CARSON, CALIFORNIA

APRIL 2021 Figure B10

WATER ADDED AT 2.0 KSF



SAMPLE ID.	SOIL TYPE	DRY DENSITY (PCF)	INITIAL MOISTURE (%)	FINAL MOISTURE (%)
B5@10	Dark Gray Clay (CH)	71.6	47.5	46.1

GEOCON

CONSOLIDATION TEST RESULTS

ASTM D-2435

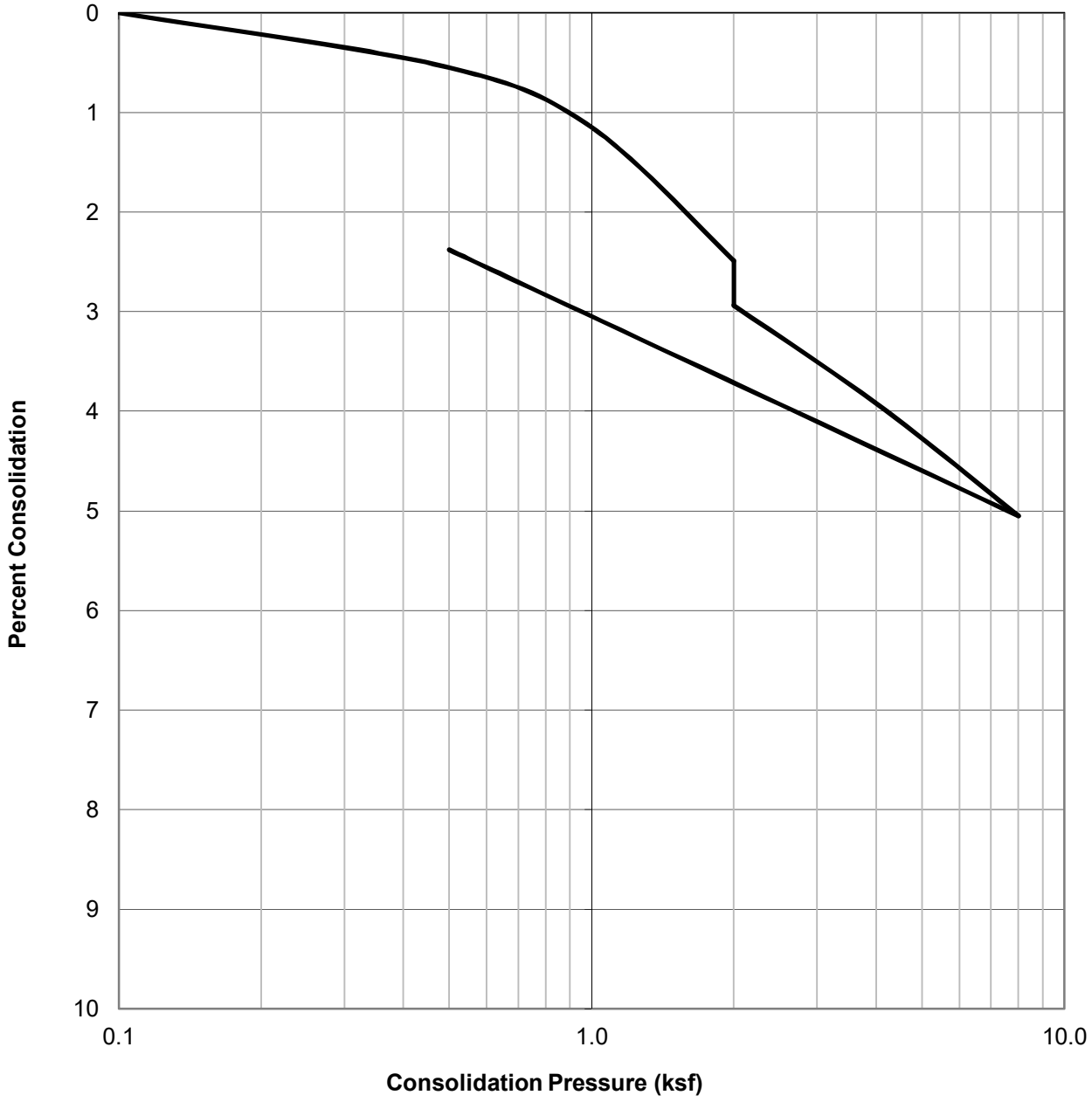
Checked by: JMH

Project No.: W1301-06-01

21611 SOUTH PERRY STREET
CARSON, CALIFORNIA

APRIL 2021 Figure B11

WATER ADDED AT 2.0 KSF



SAMPLE ID.	SOIL TYPE	DRY DENSITY (PCF)	INITIAL MOISTURE (%)	FINAL MOISTURE (%)
B3@12.5	Dark Gray Clay (CL)	90.9	31.6	31.3

GEOCON

CONSOLIDATION TEST RESULTS

ASTM D-2435

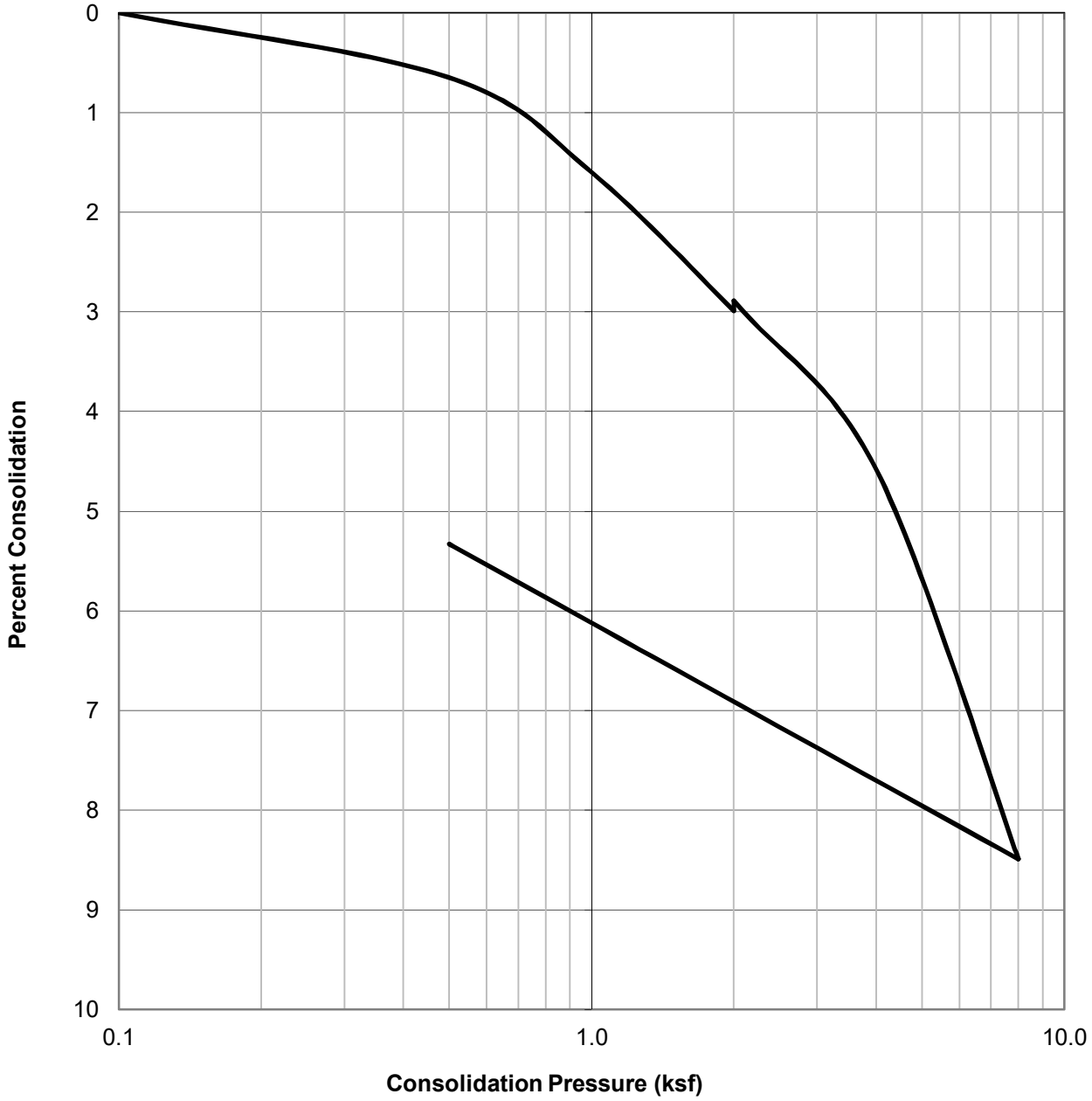
Checked by: JMH

Project No.: W1301-06-01

21611 SOUTH PERRY STREET
CARSON, CALIFORNIA

APRIL 2021 Figure B12

WATER ADDED AT 2.0 KSF



SAMPLE ID.	SOIL TYPE	DRY DENSITY (PCF)	INITIAL MOISTURE (%)	FINAL MOISTURE (%)
B2@15	Gray Clay (CH)	75.8	45.2	41.7

GEOCON

CONSOLIDATION TEST RESULTS

ASTM D-2435

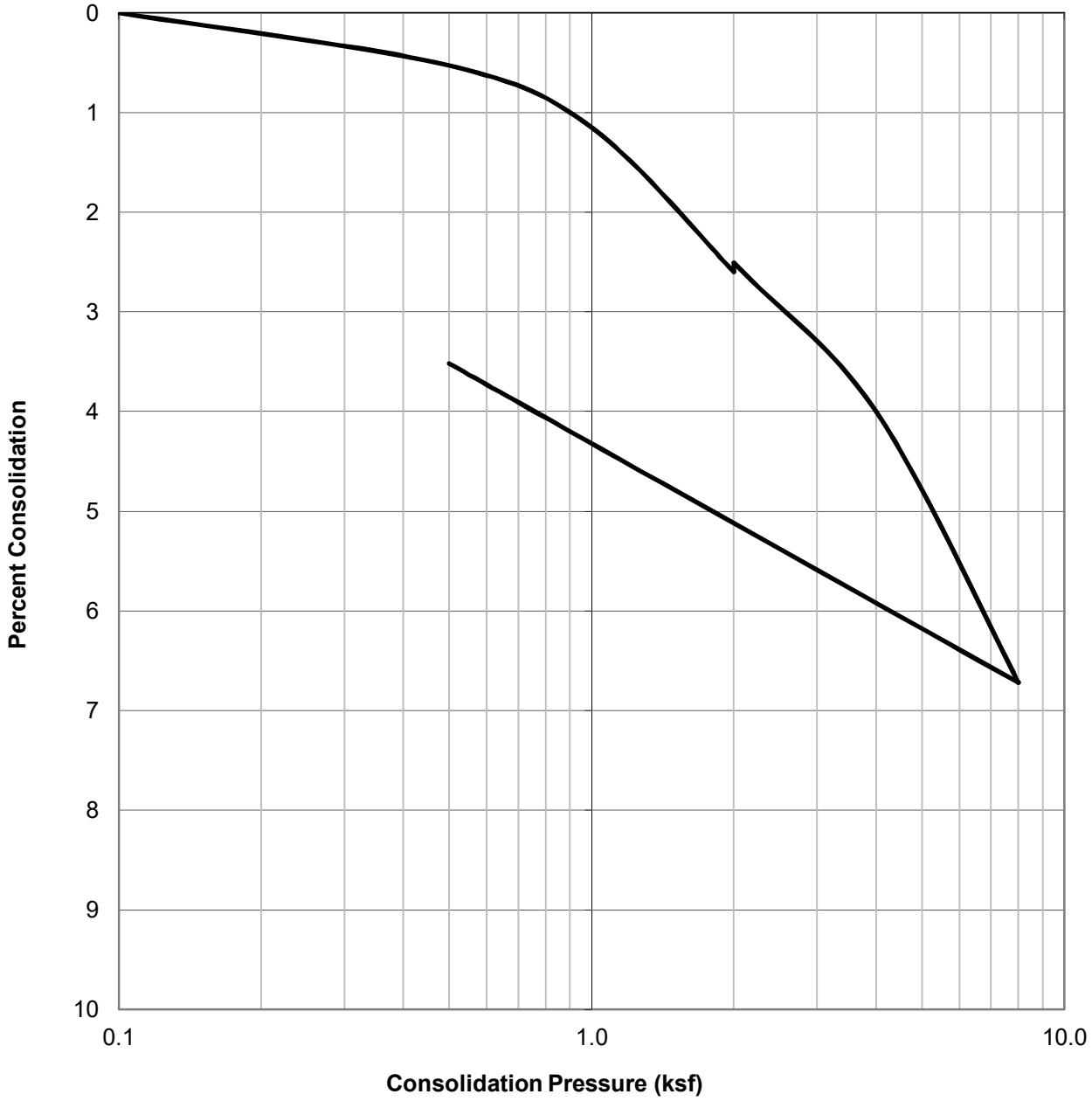
Checked by: JMH

Project No.: W1301-06-01

21611 SOUTH PERRY STREET
CARSON, CALIFORNIA

APRIL 2021 Figure B13

WATER ADDED AT 2.0 KSF



SAMPLE ID.	SOIL TYPE	DRY DENSITY (PCF)	INITIAL MOISTURE (%)	FINAL MOISTURE (%)
B4@15	Dark Gray Clay (CH)	83.1	38.5	37.0

GEOCON

CONSOLIDATION TEST RESULTS

ASTM D-2435

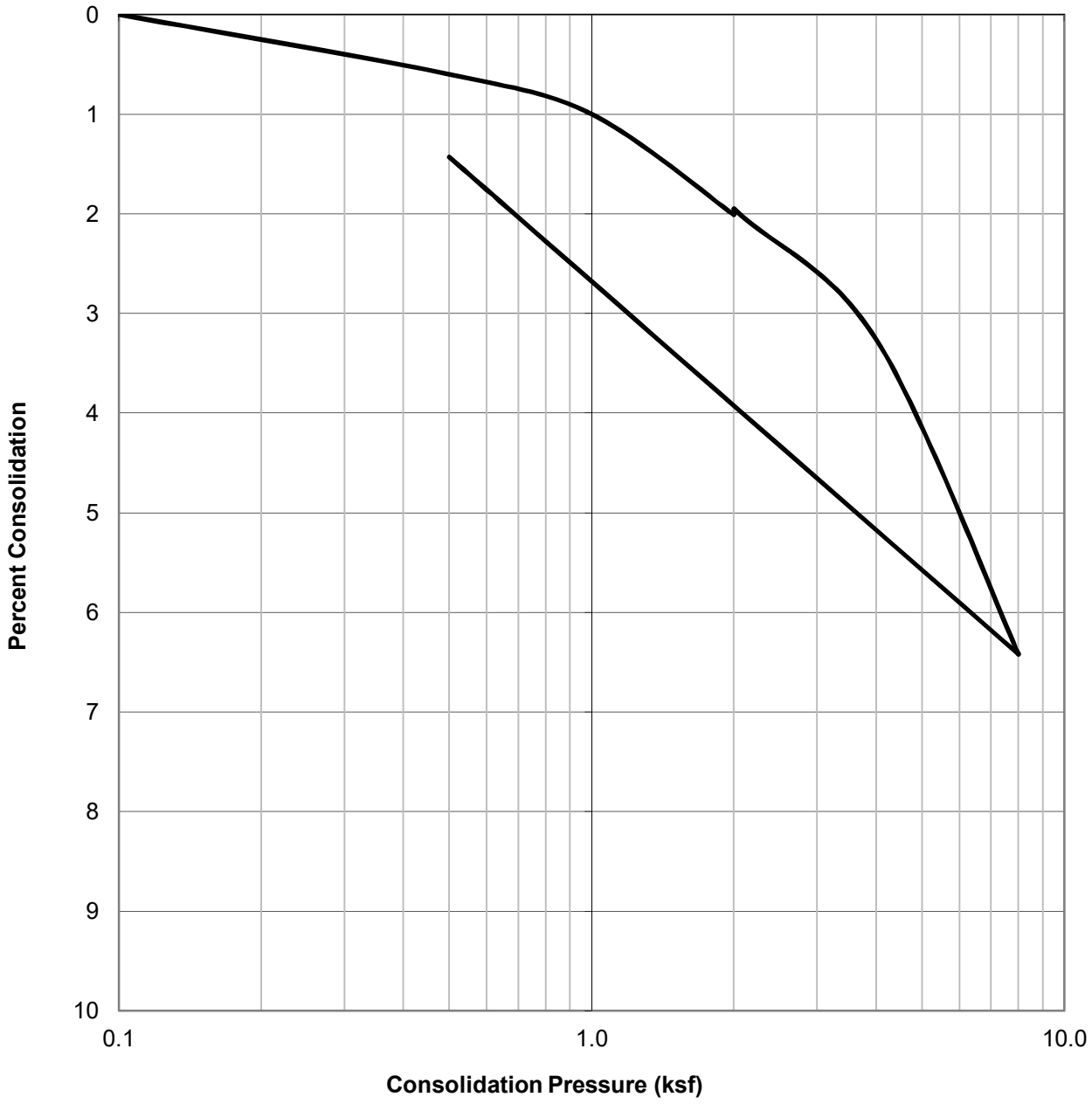
Checked by: JMH

Project No.: W1301-06-01

21611 SOUTH PERRY STREET
CARSON, CALIFORNIA

APRIL 2021 Figure B14

WATER ADDED AT 2.0 KSF



SAMPLE ID.	SOIL TYPE	DRY DENSITY (PCF)	INITIAL MOISTURE (%)	FINAL MOISTURE (%)
B5@15	Dark Gray Clay (CH)	96.3	29.6	29.7

GEOCON

CONSOLIDATION TEST RESULTS

ASTM D-2435

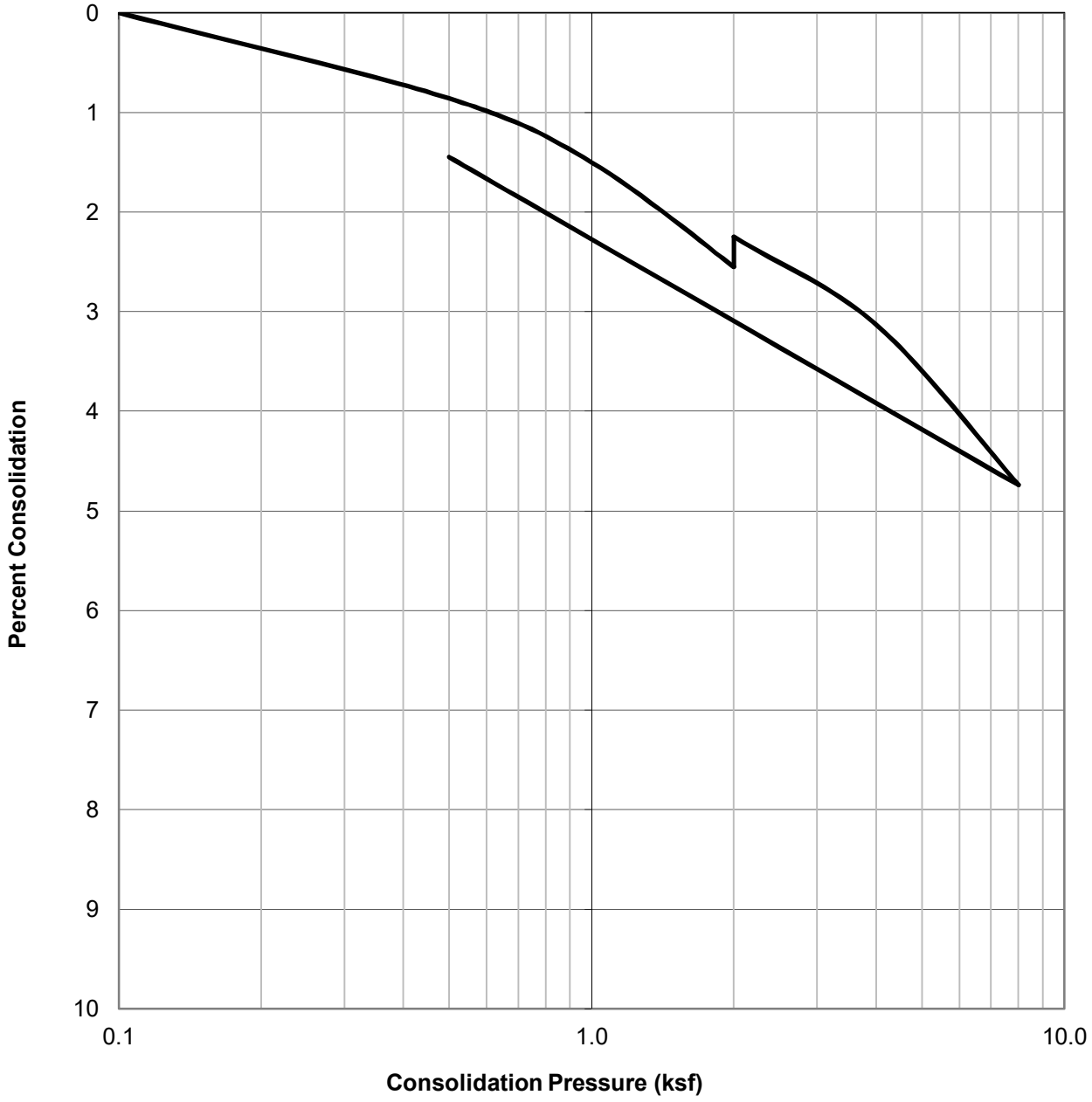
Checked by: JMH

Project No.: W1301-06-01

21611 SOUTH PERRY STREET
CARSON, CALIFORNIA

APRIL 2021 Figure B15

WATER ADDED AT 2.0 KSF



SAMPLE ID.	SOIL TYPE	DRY DENSITY (PCF)	INITIAL MOISTURE (%)	FINAL MOISTURE (%)
B3@17.5	Dark Gray Clay (CL)	100.2	26.1	25.9

GEOCON

CONSOLIDATION TEST RESULTS

ASTM D-2435

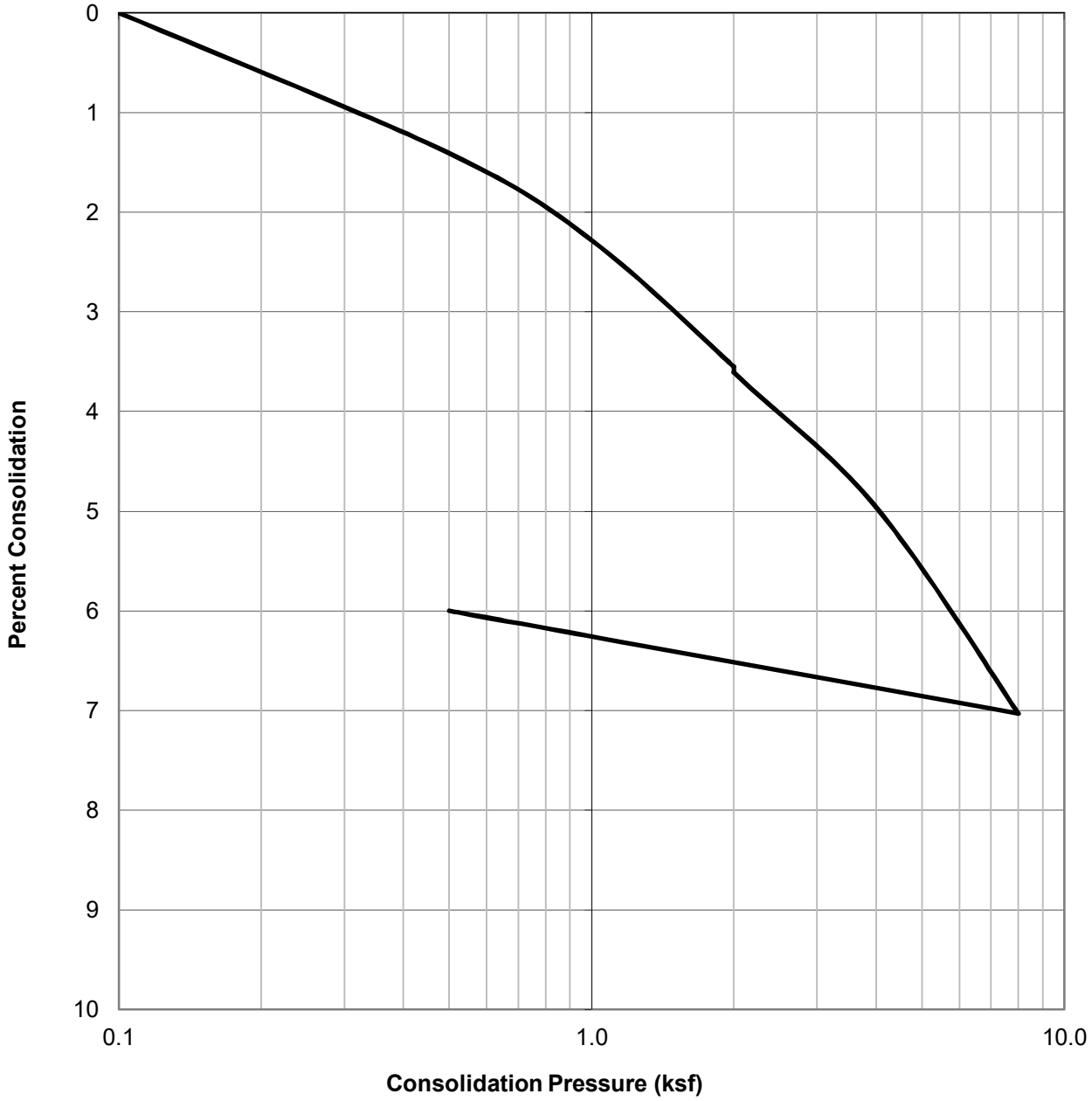
Checked by: JMH

Project No.: W1301-06-01

21611 SOUTH PERRY STREET
CARSON, CALIFORNIA

APRIL 2021 Figure B16

WATER ADDED AT 2.0 KSF



SAMPLE ID.	SOIL TYPE	DRY DENSITY (PCF)	INITIAL MOISTURE (%)	FINAL MOISTURE (%)
B3@22.5	Light Brown Clay (CL)	98.3	27.2	23.0

GEOCON

CONSOLIDATION TEST RESULTS

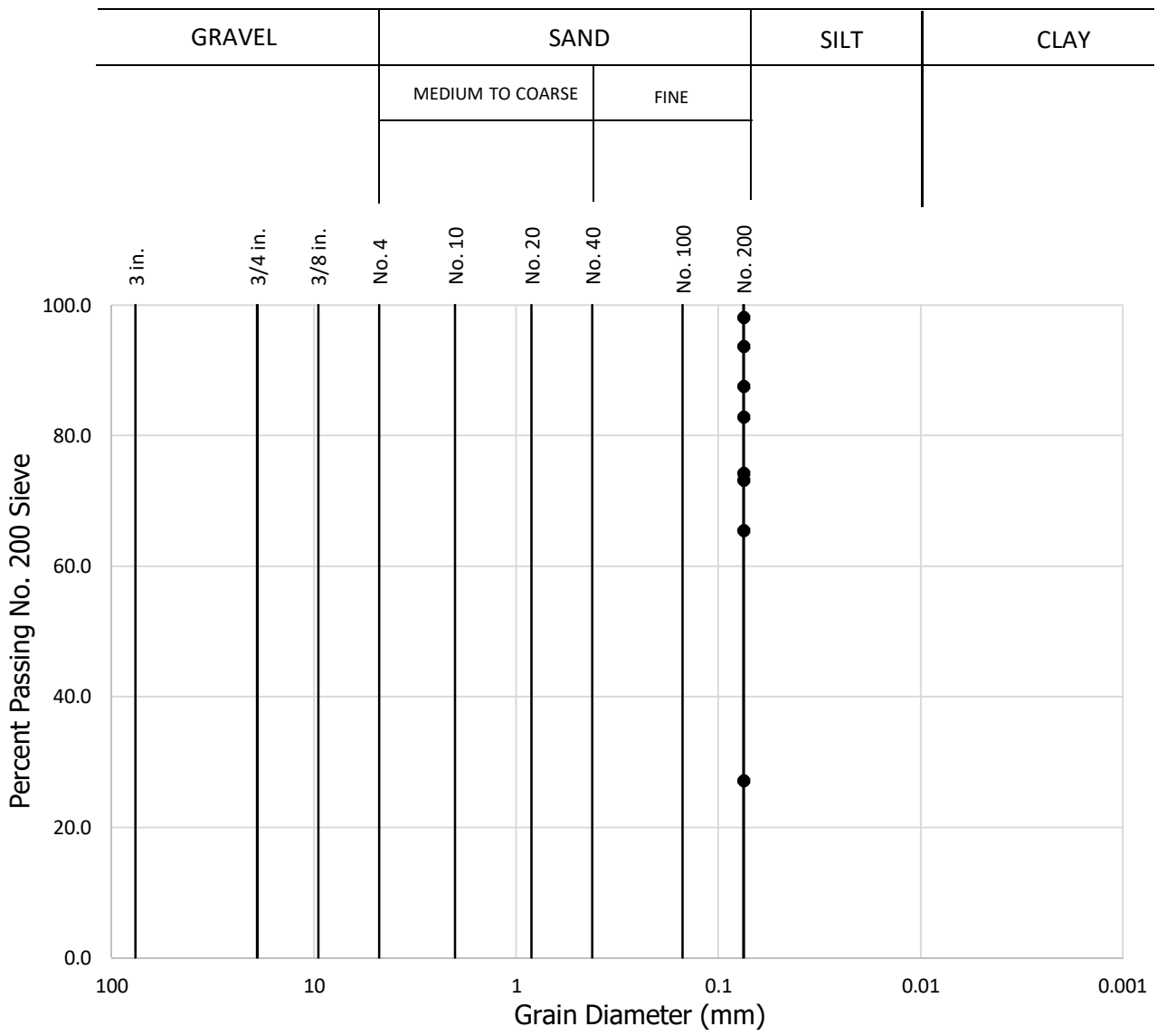
ASTM D-2435

Checked by: JMH

Project No.: W1301-06-01

21611 SOUTH PERRY STREET
CARSON, CALIFORNIA

APRIL 2021 Figure B17



Sample No.	Percent Passing No. 200 Sieve
B3 @ 10'	82.8
B3 @ 15'	87.6
B3 @ 20'	73.2
B3 @ 25'	98.1
B3 @ 30'	93.7
B3 @ 35'	74.2
B3 @ 40'	65.4
B3 @ 50'	27.1

GEOCON

GRAIN SIZE ANALYSIS

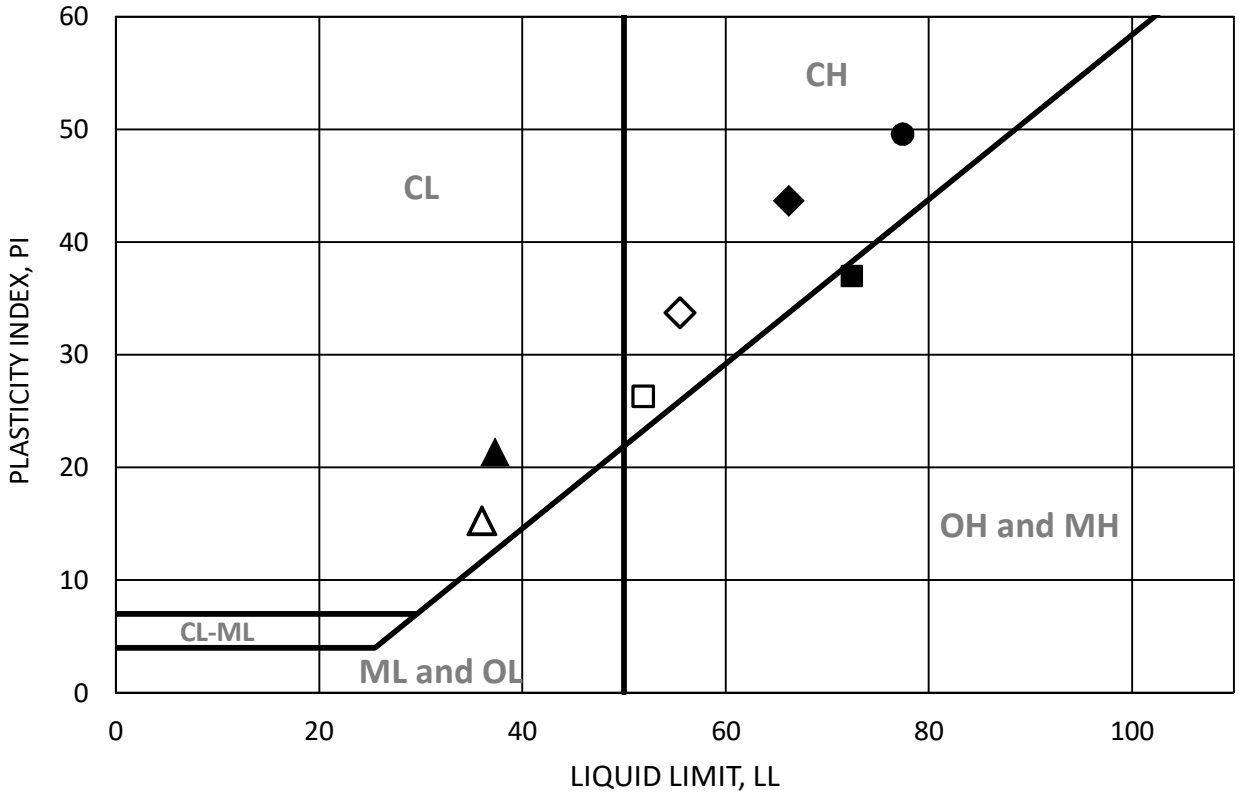
ASTM D-1140

Checked by: JMH

Project No.: W1301-06-01

21611 SOUTH PERRY STREET
CARSON, CALIFORNIA

APRIL 2021 Figure B18



SYMBOL	BORING	DEPTH (ft)	LL	PL	PI	MOISTURE CONTENT AT SATURATION	SOIL BEHAVIOR
■	B3	10'	72.5	36	37		MH
◆	B3	15'	66	23	44		CH
▲	B3	20'	37	16	21		CL
●	B3	25'	78	28	50		CH
□	B3	30'	52	26	26		CH
◇	B3	35'	56	22	34		CH
△	B3	45'	36	21	15		CL
○	B3	50'	N/P	N/P	N/P		SM

N/P = Non-Plastic

GEOCON

ATTERBERG LIMITS

ASTM D-4318

Checked by: JMH

Project No.: W1301-06-01

21611 SOUTH PERRY STREET
CARSON, CALIFORNIA

APRIL 2021 Figure B19

B1B2@0-5'

MOLDED SPECIMEN		BEFORE TEST	AFTER TEST
Specimen Diameter	(in.)	4.0	4.0
Specimen Height	(in.)	1.0	1.1
Wt. Comp. Soil + Mold	(gm)	740.3	787.1
Wt. of Mold	(gm)	367.6	367.6
Specific Gravity	(Assumed)	2.7	2.7
Wet Wt. of Soil + Cont.	(gm)	484.4	787.1
Dry Wt. of Soil + Cont.	(gm)	451.5	331.9
Wt. of Container	(gm)	184.4	367.6
Moisture Content	(%)	12.3	26.4
Wet Density	(pcf)	112.4	126.4
Dry Density	(pcf)	100.1	100.0
Void Ratio		0.7	0.8
Total Porosity		0.4	0.4
Pore Volume	(cc)	84.1	97.0
Degree of Saturation	(%) [S_{meas}]	49.0	90.3

Date	Time	Pressure (psi)	Elapsed Time (min)	Dial Readings (in.)
3/8/2021	10:00	1.0	0	0.3035
3/8/2021	10:10	1.0	10	0.302
Add Distilled Water to the Specimen				
3/9/2021	10:00	1.0	1430	0.3645
3/9/2021	11:00	1.0	1490	0.3645

Expansion Index (EI meas) =	62.5
Expansion Index (Report) =	**63**

Expansion Index, EI_{50}	CBC CLASSIFICATION *	UBC CLASSIFICATION **
0-20	Non-Expansive	Very Low
21-50	Expansive	Low
51-90	Expansive	Medium
91-130	Expansive	High
>130	Expansive	Very High

* Reference: 2019 California Building Code, Section 1803.5.3

** Reference: 1997 Uniform Building Code, Table 18-I-B.

GEOCON

EXPANSION INDEX TEST RESULTS

ASTM D-4829

Checked by: JMH

Project No.: W1301-06-01

21611 SOUTH PERRY STREET
CARSON, CALIFORNIA

APRIL 2021 Figure B20

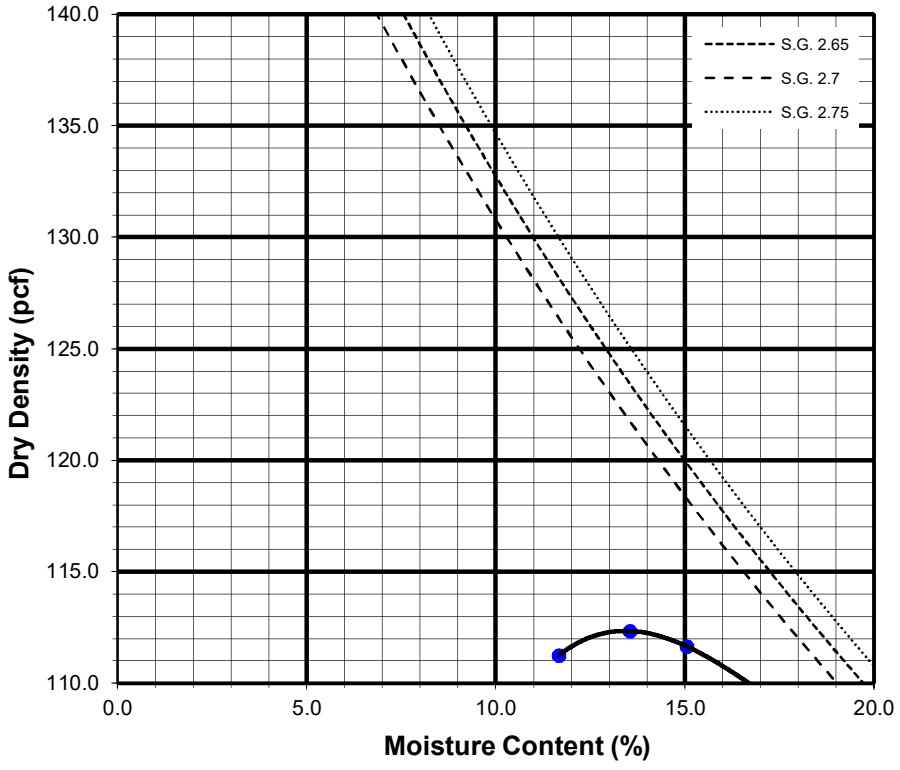
Sample No:

B1B2@0-5'	Brown Silty Sand (SM)

TEST NO.		1	2	3	4	5	6
Wt. Compacted Soil + Mold	(g)	6008	6058	6072	6069		
Weight of Mold	(g)	4132	4132	4132	4132		
Net Weight of Soil	(g)	1876	1927	1940	1937		
Wet Weight of Soil + Cont.	(g)	630.8	626.4	653.1	674.5		
Dry Weight of Soil + Cont.	(g)	580.0	569.3	585.6	594.2		
Weight of Container	(g)	144.4	147.6	137.1	125.4		
Moisture Content	(%)	11.7	13.5	15.1	17.1		
Wet Density	(pcf)	124.2	127.6	128.5	128.2		
Dry Density	(pcf)	111.2	112.3	111.7	109.5		

Maximum Dry Density (pcf)	**112.5**

Optimum Moisture Content (%)	**14.0**



Preparation Method: A

GEOCON

COMPACTION CHARACTERISTICS USING MODIFIED EFFORT TEST RESULTS

ASTM D-1557

Checked by: JMH

Project No.: W1301-06-01

21611 SOUTH PERRY STREET
CARSON, CALIFORNIA

APRIL 2021 Figure B21

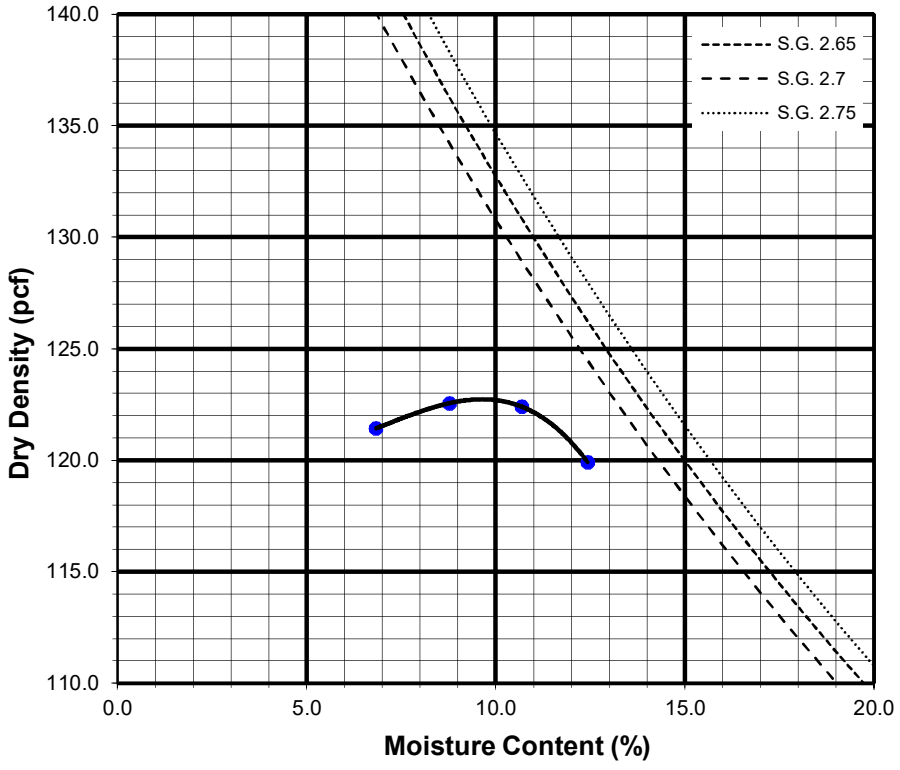
Sample No:

B3B4@0-5'	Light Brown Silty Sand (SM)

TEST NO.		1	2	3	4	5	6
Wt. Compacted Soil + Mold	(g)	6085	6139	6172	6162		
Weight of Mold	(g)	4132	4132	4132	4132		
Net Weight of Soil	(g)	1954	2008	2040	2030		
Wet Weight of Soil + Cont.	(g)	659.1	662.9	668.4	663.2		
Dry Weight of Soil + Cont.	(g)	626.4	619.6	618.1	606.0		
Weight of Container	(g)	148.0	126.1	147.5	145.6		
Moisture Content	(%)	6.8	8.8	10.7	12.4		
Wet Density	(pcf)	129.7	133.3	135.5	134.8		
Dry Density	(pcf)	121.4	122.6	122.4	119.9		

Maximum Dry Density (pcf)	**123.0**
Bulk Specific Gravity (dry)	**2.36**
Corrected Maximum Dry Density (pcf)	**127.0**

Optimum Moisture Content (%)	**10.0**
Oversized Fraction (%)	**18.0**
Corrected Moisture Content (%)	**8.0**



Preparation Method: A

GEOCON

COMPACTION CHARACTERISTICS USING MODIFIED EFFORT TEST RESULTS

ASTM D-1557

Checked by: JMH

Project No.: W1301-06-01

21611 SOUTH PERRY STREET
CARSON, CALIFORNIA

APRIL 2021 Figure B22

SUMMARY OF LABORATORY POTENTIAL
OF HYDROGEN (pH) AND RESISTIVITY TEST RESULTS
CALIFORNIA TEST NO. 643

Sample No.	pH	Resistivity (ohm centimeters)
B1 + B2 @ 0-5'	8.1	910 (Severely Corrosive)
B3 + B4 @ 0-5'	10.5	3900 (Moderately Corrosive)

SUMMARY OF LABORATORY CHLORIDE CONTENT TEST RESULTS
EPA NO. 325.3

Sample No.	Chloride Ion Content (%)
B1 + B2@0-5'	0.006
B3 + B4@0-5'	0.003

SUMMARY OF LABORATORY WATER SOLUBLE SULFATE TEST RESULTS
CALIFORNIA TEST NO. 417

Sample No.	Water Soluble Sulfate (% SO_4)	Sulfate Exposure*
B1 + B2@0-5'	0.070	S0
B3 + B4@0-5'	0.013	S0

GEOCON

CORROSIVITY TEST RESULTS

Checked by: JMH

Project No.: W1301-06-01

21611 SOUTH PERRY STREET
CARSON, CALIFORNIA

APRIL 2021 Figure B23

APPENDIX C

APPENDIX C

CPT LIQUEFACTION ANALYSIS

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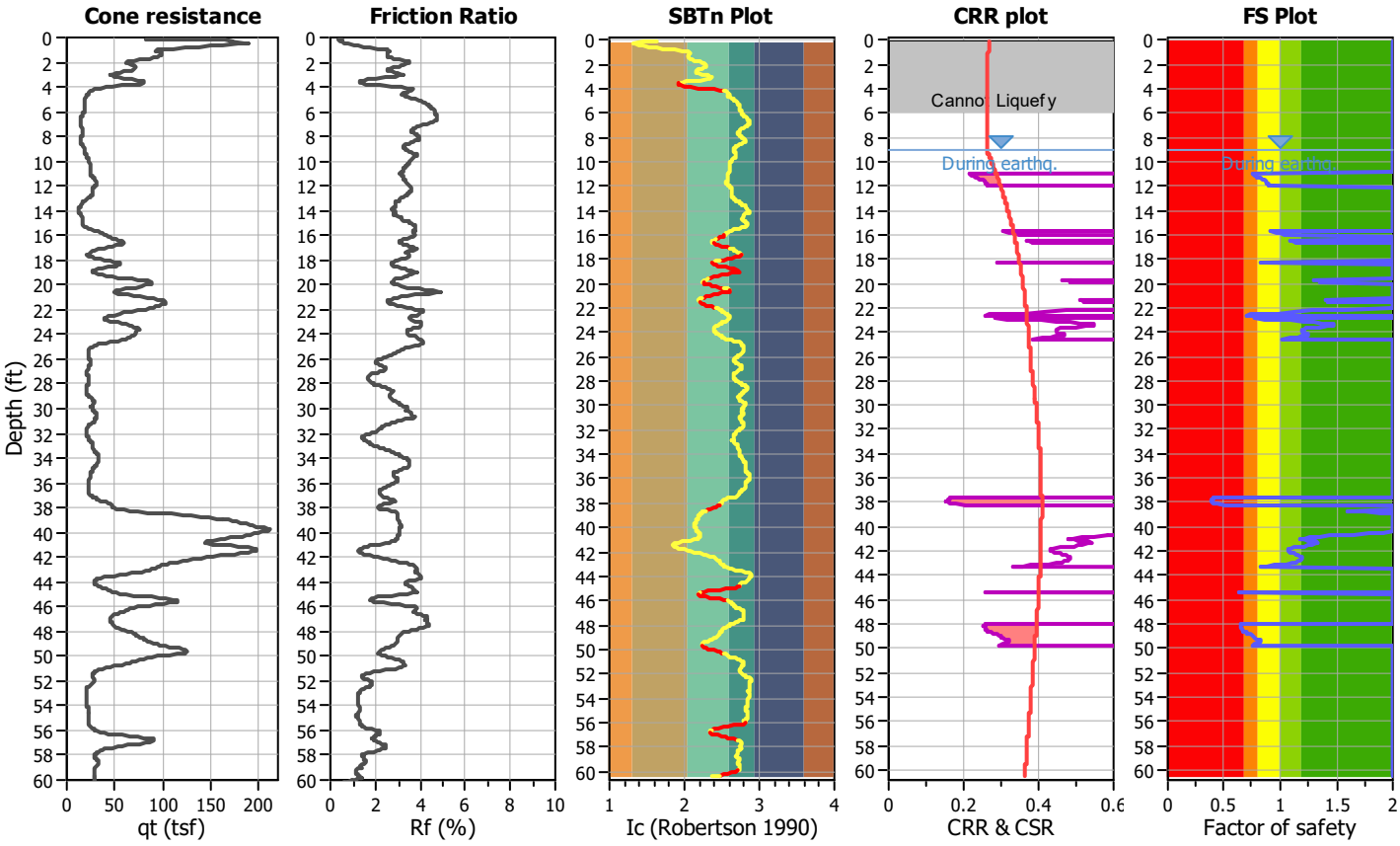
LIQUEFACTION ANALYSIS REPORT

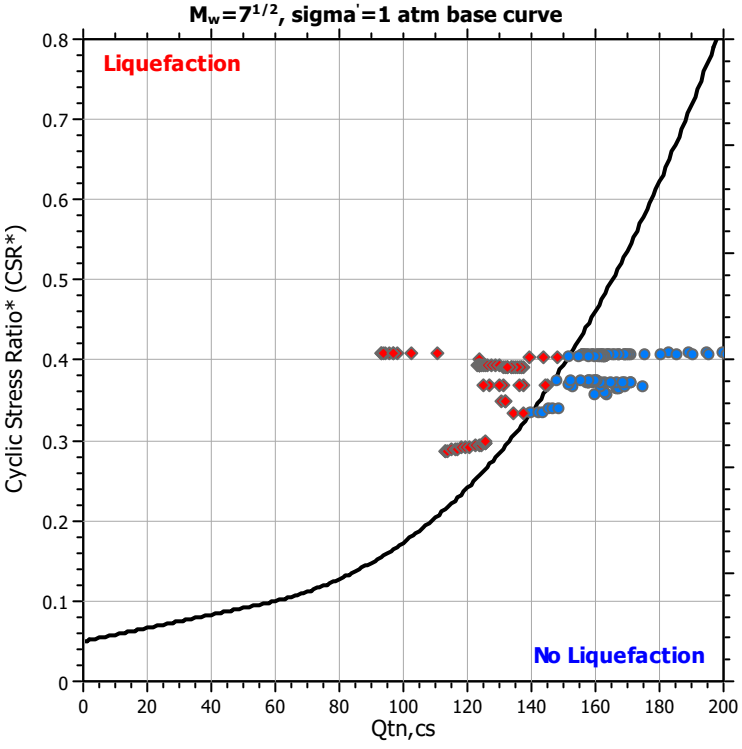
Project title : W1301-06-01 **Location : Perry Street**

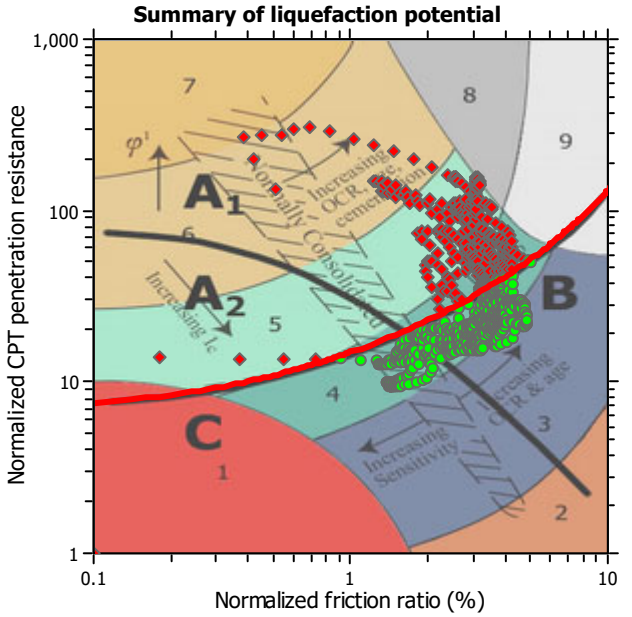
CPT file : CPT-1

Input parameters and analysis data

Analysis method:	NCEER (1998)	G.W.T. (in-situ):	12.00 ft	Use fill:	No	Clay like behavior applied:	Sands only
Fines correction method:	NCEER (1998)	G.W.T. (earthq.):	9.00 ft	Fill height:	N/A	Limit depth applied:	Yes
Points to test:	Based on Ic value	Average results interval:	.	Fill weight:	N/A	Limit depth:	50.00 ft
Earthquake magnitude M_w:	6.68	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	MSF method:	Method based
Peak ground acceleration:	0.55	Unit weight calculation:	Based on SBT	K_σ applied:	Yes		

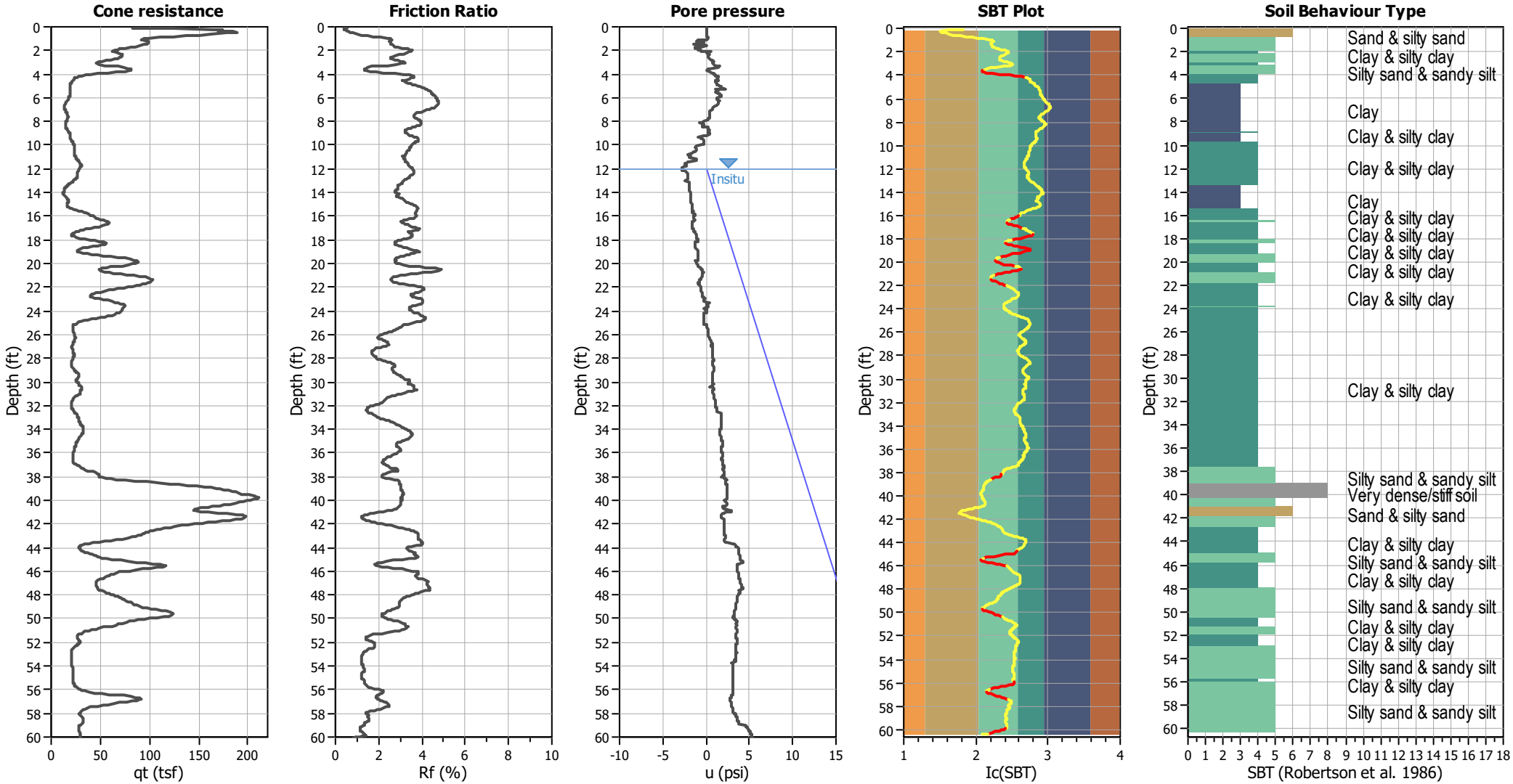






Zone A_1: Cyclic liquefaction likely depending on size and duration of cyclic loading
Zone A_2: Cyclic liquefaction and strength loss likely depending on loading and ground geometry
Zone B: Liquefaction and post-earthquake strength loss unlikely, check cyclic softening
Zone C: Cyclic liquefaction and strength loss possible depending on soil plasticity, brittleness/sensitivity, strain to peak undrained strength and ground geometry

CPT basic interpretation plots



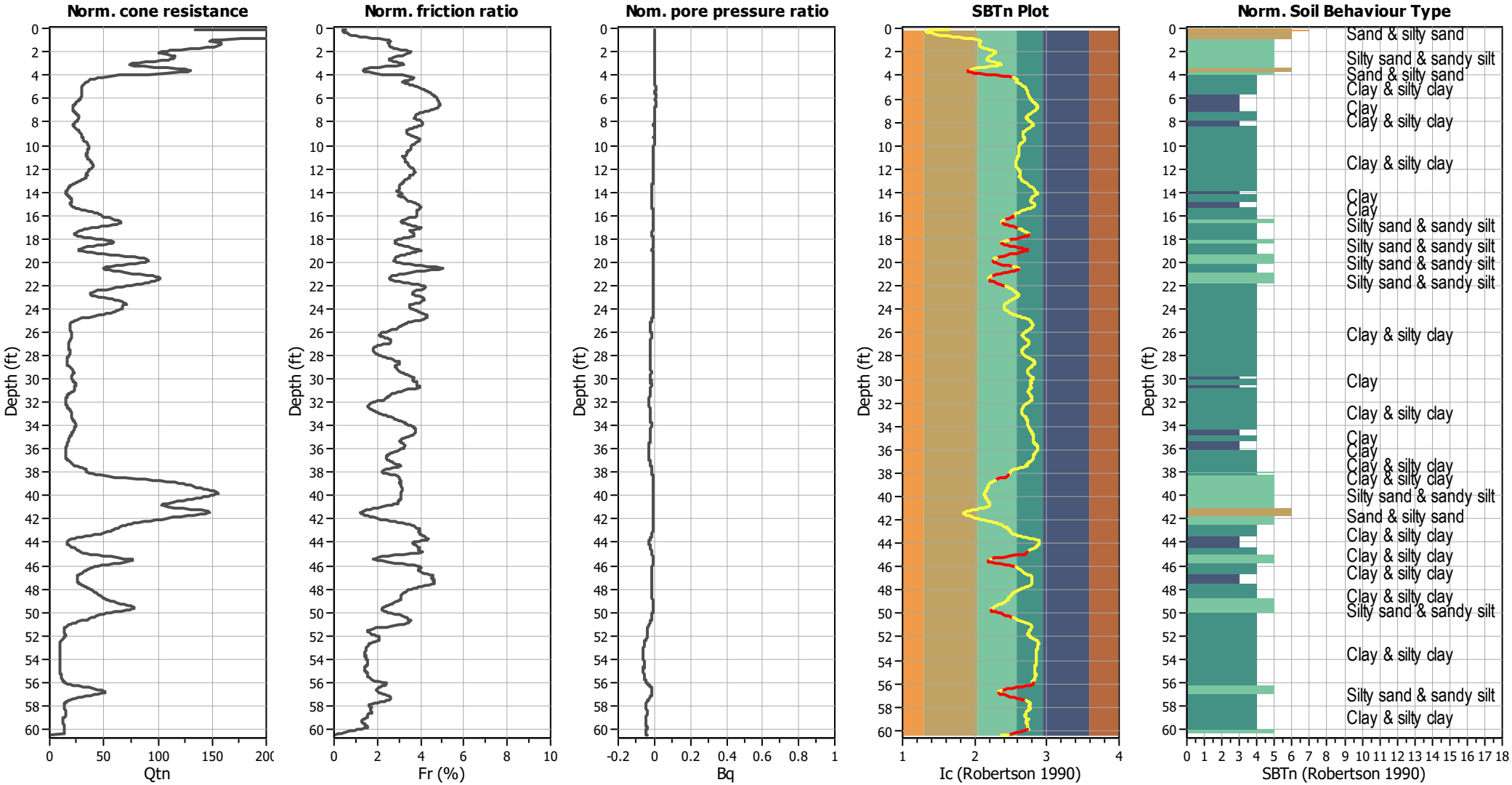
Input parameters and analysis data

Analysis method:	NCEER (1998)	Depth to water table (erthq.):	9.00 ft	Fill weight:	N/A
Fines correction method:	NCEER (1998)	Average results interval:	.	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.68	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.55	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	12.00 ft	Fill height:	N/A	Limit depth:	50.00 ft

SBT legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to
9. Very stiff fine grained

CPT basic interpretation plots (normalized)



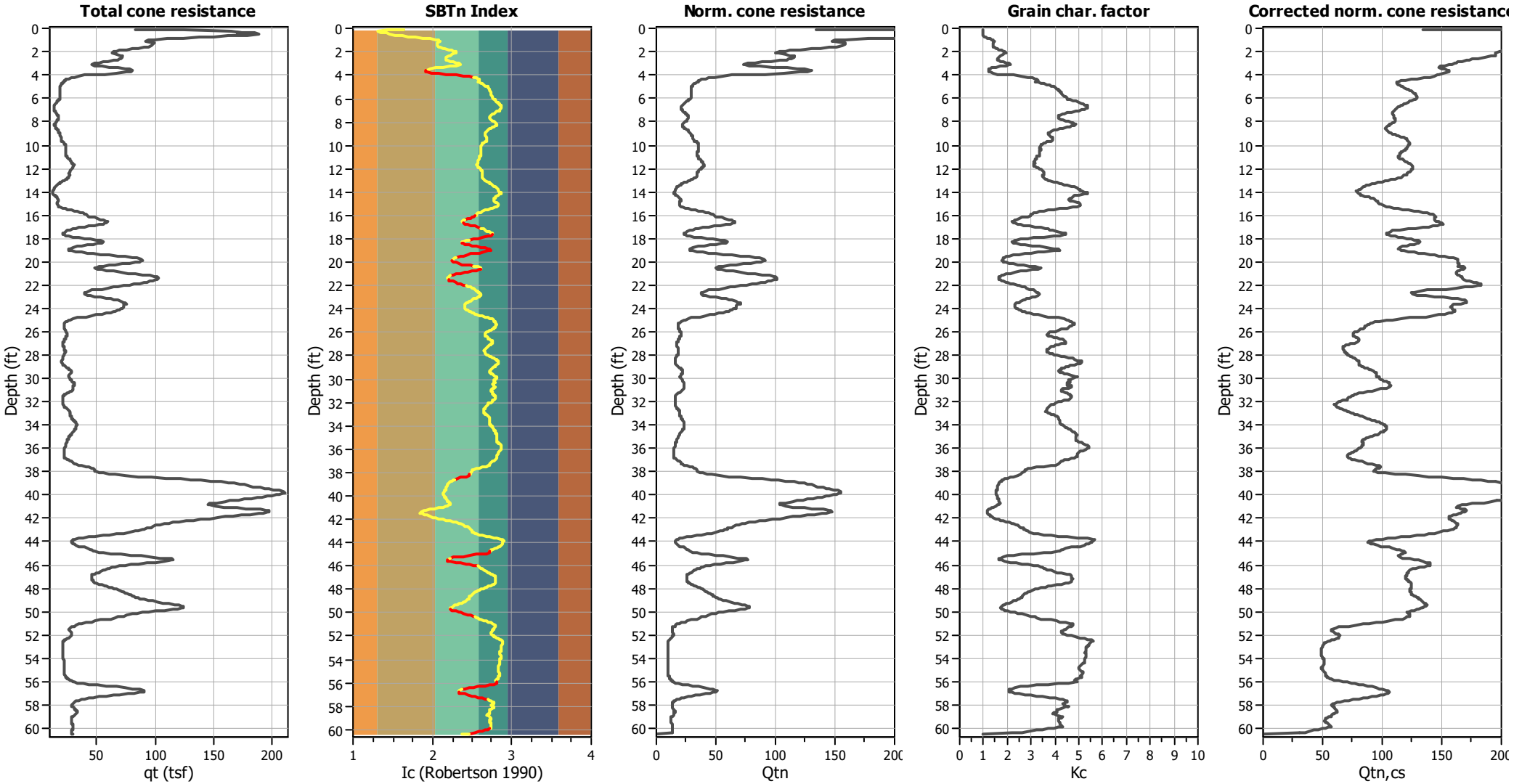
Input parameters and analysis data

Analysis method:	NCEER (1998)	Depth to water table (erthq.):	9.00 ft	Fill weight:	N/A
Fines correction method:	NCEER (1998)	Average results interval:	.	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.68	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.55	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	12.00 ft	Fill height:	N/A	Limit depth:	50.00 ft

SBTn legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to
9. Very stiff fine grained

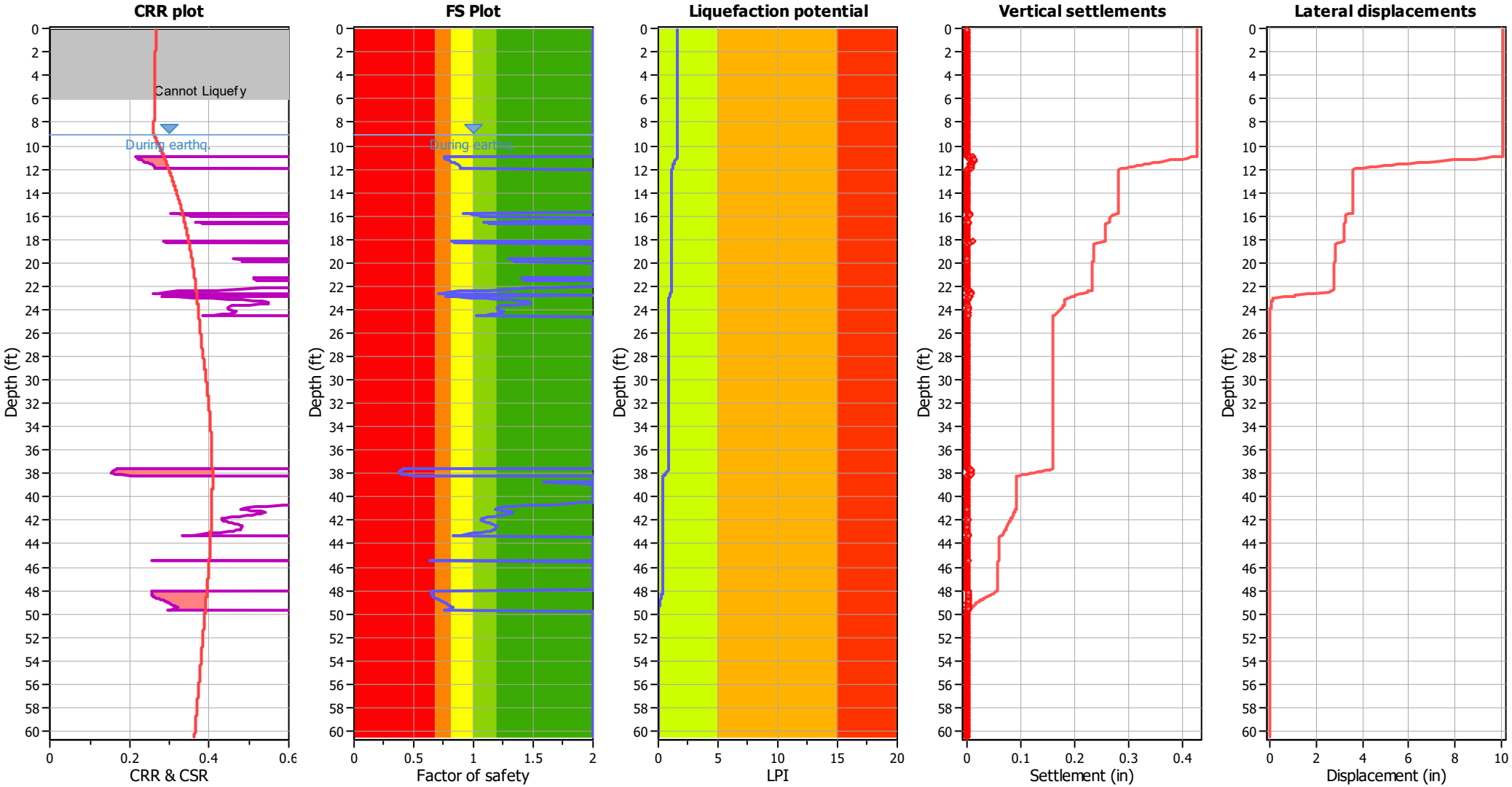
Liquefaction analysis overall plots (intermediate results)



Input parameters and analysis data

Analysis method:	NCEER (1998)	Depth to water table (erthq.):	9.00 ft	Fill weight:	N/A
Fines correction method:	NCEER (1998)	Average results interval:	.	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.68	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.55	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	12.00 ft	Fill height:	N/A	Limit depth:	50.00 ft

Liquefaction analysis overall plots



Input parameters and analysis data

Analysis method:	NCEER (1998)	Depth to water table (erthq.):	9.00 ft	Fill weight:	N/A
Fines correction method:	NCEER (1998)	Average results interval:	.	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.68	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.55	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	12.00 ft	Fill height:	N/A	Limit depth:	50.00 ft

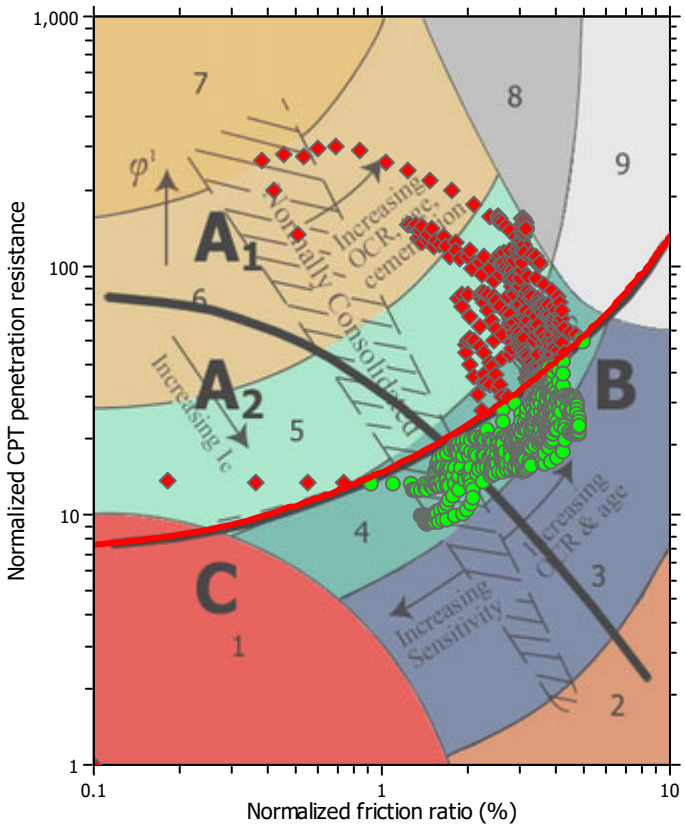
F.S. color scheme

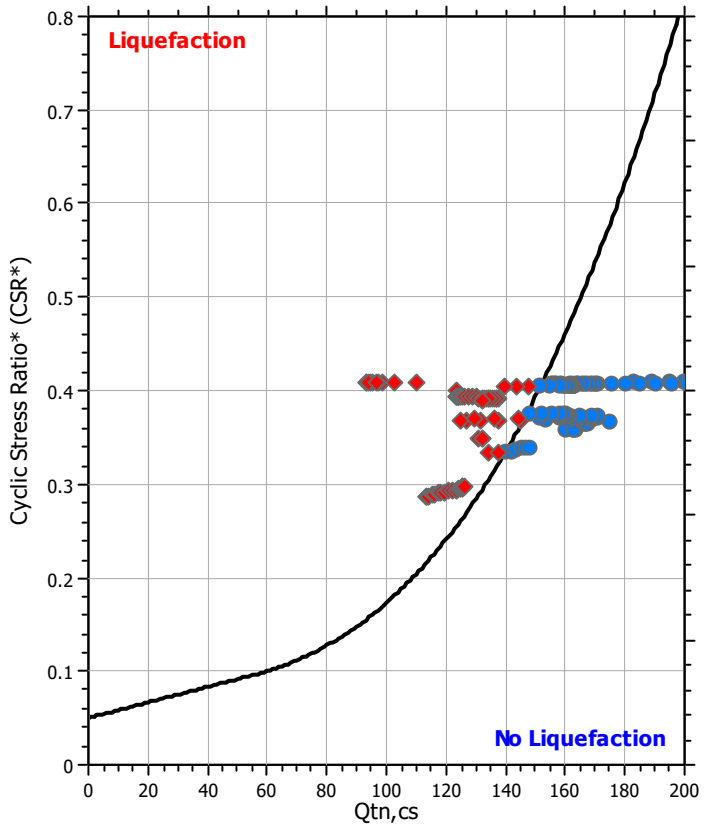
- Almost certain it will liquefy
- Very likely to liquefy
- Liquefaction and no liq. are equally likely
- Unlike to liquefy
- Almost certain it will not liquefy

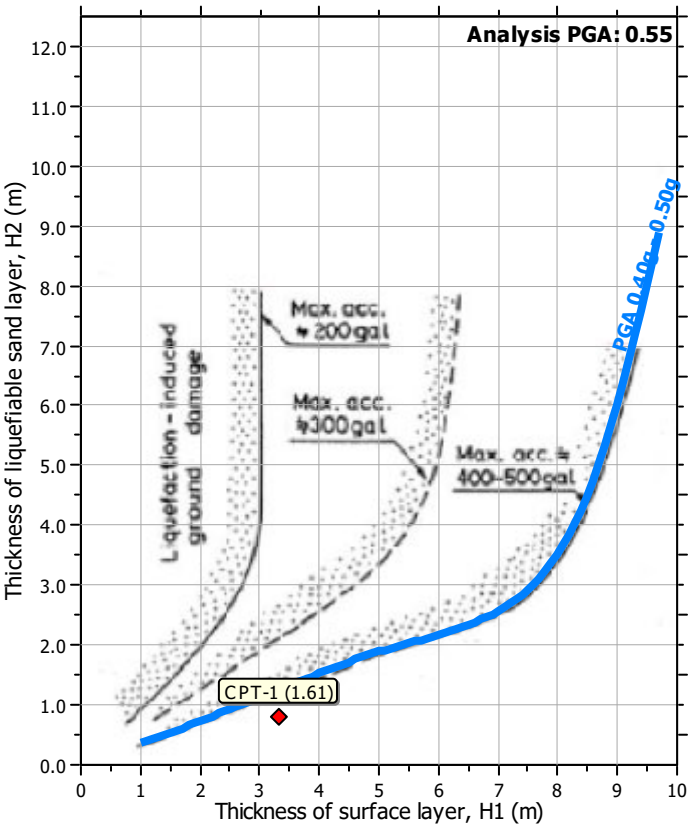
LPI color scheme

- Very high risk
- High risk
- Low risk

Liquefaction analysis summary plots



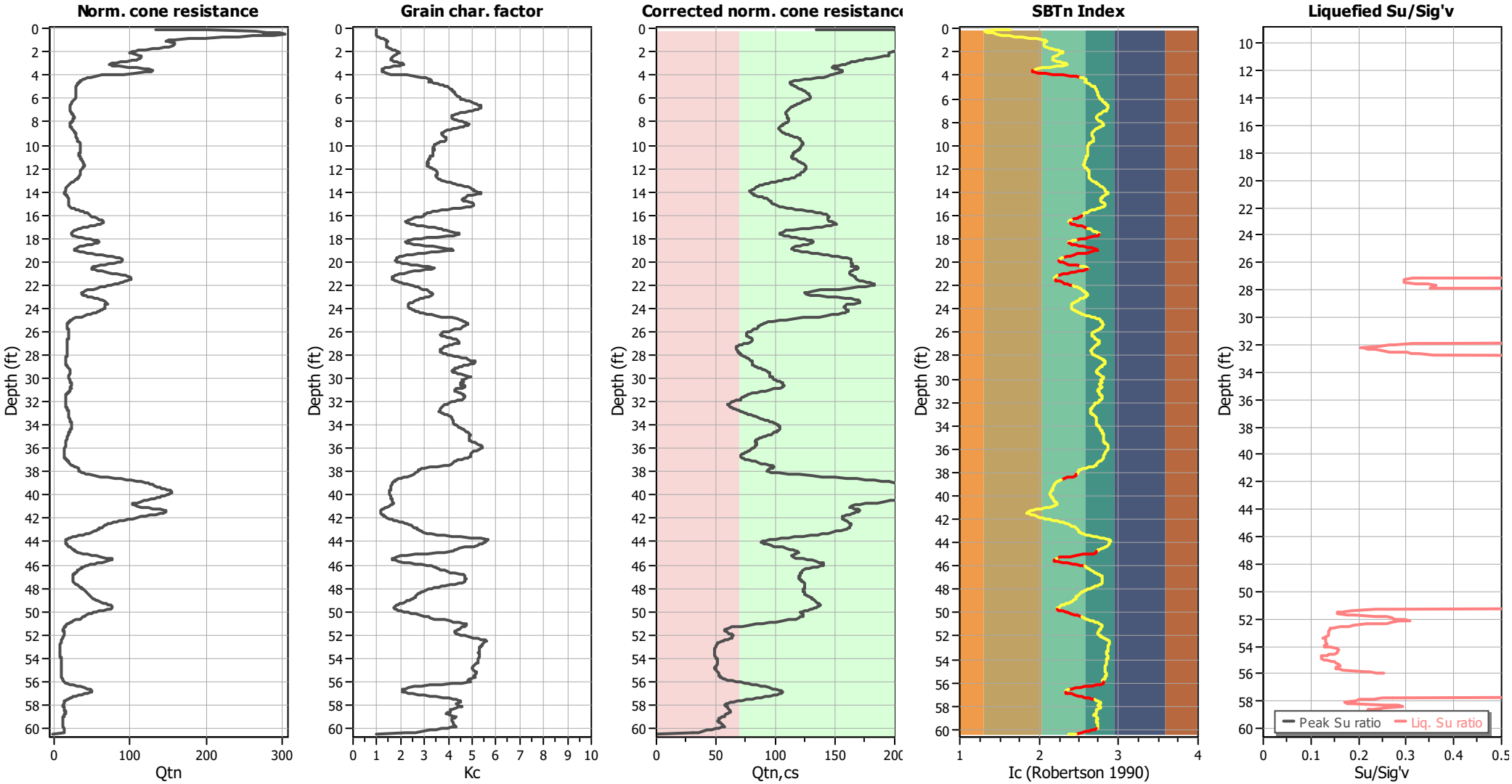




Input parameters and analysis data

Analysis method:	NCEER (1998)	Depth to water table (erthq.):	9.00 ft	Fill weight:	N/A
Fines correction method:	NCEER (1998)	Average results interval:	.	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.68	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.55	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	12.00 ft	Fill height:	N/A	Limit depth:	50.00 ft

Check for strength loss plots (Robertson (2010))



Input parameters and analysis data

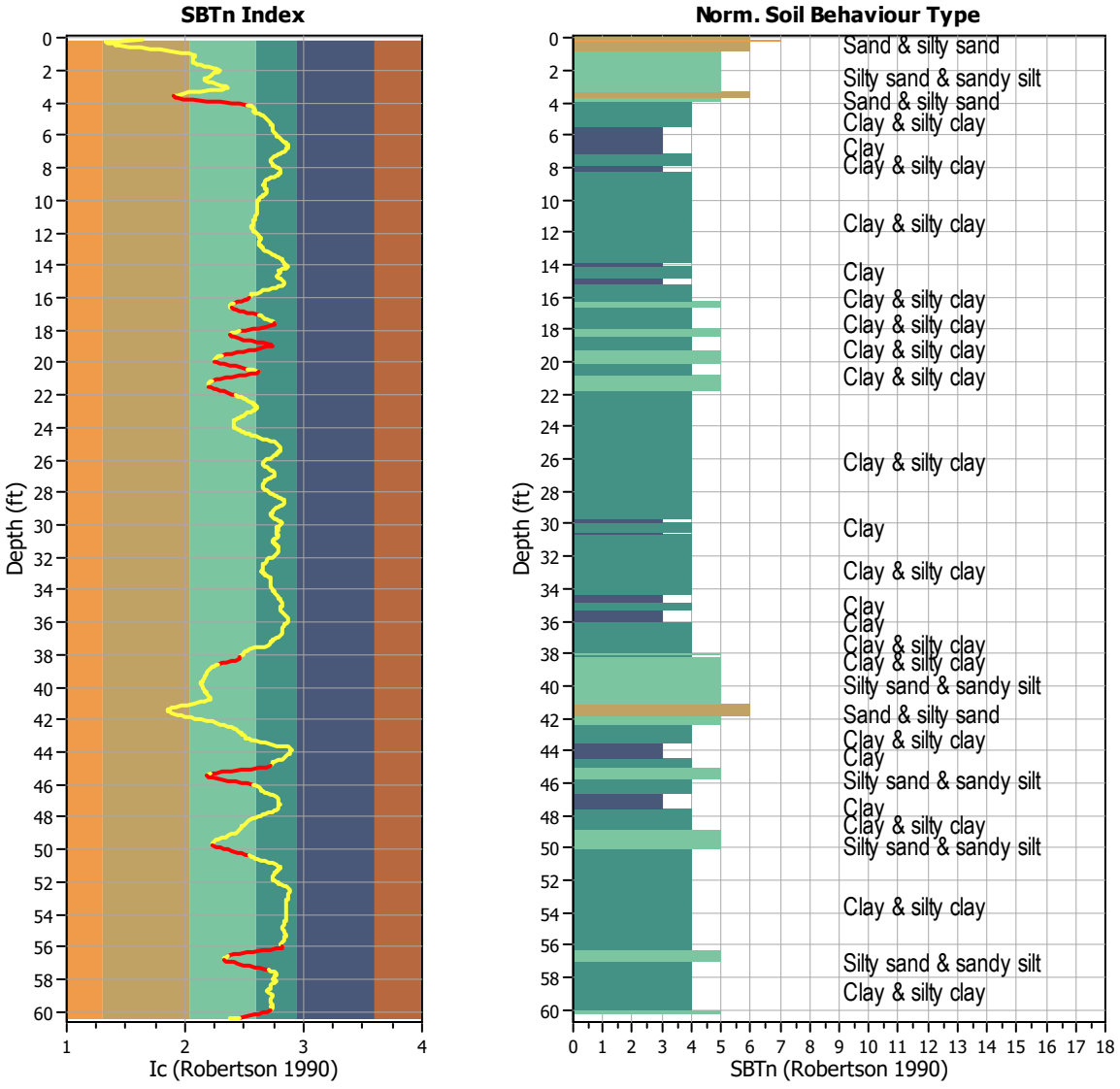
Analysis method:	NCEER (1998)	Depth to water table (erthq.):	9.00 ft	Fill weight:	N/A
Fines correction method:	NCEER (1998)	Average results interval:	.	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.68	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.55	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	12.00 ft	Fill height:	N/A	Limit depth:	50.00 ft

TRANSITION LAYER DETECTION ALGORITHM REPORT
Summary Details & Plots

Short description

The software will delete data when the cone is in transition from either clay to sand or vise-versa. To do this the software requires a range of I_c values over which the transition will be defined (typically somewhere between 1.80 < I_c < 3.0) and a rate of change of I_c. Transitions typically occur when the rate of change of I_c is fast (i.e. delta I_c is small).

The SBT_n plot below, displays in red the detected transition layers based on the parameters listed below the graphs.



Transition layer algorithm properties		General statistics	
I_c minimum check value:	1.70	Total points in CPT file:	922
I_c maximum check value:	3.00	Total points excluded:	144
I_c change ratio value:	0.0250	Exclusion percentage:	15.62%
Minimum number of points in layer:	4	Number of layers detected:	16

Transition layer No	Number of points	Depth	SBT_n number	SBT_n description
Transition layer 1	10	Start depth: 3.64 (ft)	6	Sand & silty sand
		End depth: 4.20 (ft)	4	Clay & silty clay
Transition layer 2	6	Start depth: 16.10 (ft)	4	Clay & silty clay
		End depth: 16.41 (ft)	5	Silty sand & sandy silt
Transition layer 3	8	Start depth: 16.70 (ft)	5	Silty sand & sandy silt
		End depth: 17.14 (ft)	4	Clay & silty clay
Transition layer 4	8	Start depth: 17.67 (ft)	4	Clay & silty clay
		End depth: 18.12 (ft)	5	Silty sand & sandy silt
Transition layer 5	9	Start depth: 18.40 (ft)	5	Silty sand & sandy silt
		End depth: 18.91 (ft)	4	Clay & silty clay
Transition layer 6	11	Start depth: 18.98 (ft)	4	Clay & silty clay
		End depth: 19.63 (ft)	5	Silty sand & sandy silt
Transition layer 7	8	Start depth: 19.99 (ft)	5	Silty sand & sandy silt
		End depth: 20.42 (ft)	4	Clay & silty clay
Transition layer 8	10	Start depth: 20.62 (ft)	4	Clay & silty clay
		End depth: 21.21 (ft)	5	Silty sand & sandy silt
Transition layer 9	9	Start depth: 21.56 (ft)	5	Silty sand & sandy silt
		End depth: 22.05 (ft)	4	Clay & silty clay
Transition layer 10	7	Start depth: 38.26 (ft)	4	Clay & silty clay
		End depth: 38.65 (ft)	5	Silty sand & sandy silt
Transition layer 11	10	Start depth: 44.84 (ft)	4	Clay & silty clay
		End depth: 45.43 (ft)	5	Silty sand & sandy silt
Transition layer 12	9	Start depth: 45.58 (ft)	5	Silty sand & sandy silt
		End depth: 46.07 (ft)	4	Clay & silty clay
Transition layer 13	11	Start depth: 49.77 (ft)	5	Silty sand & sandy silt
		End depth: 50.42 (ft)	4	Clay & silty clay
Transition layer 14	10	Start depth: 56.05 (ft)	4	Clay & silty clay
		End depth: 56.65 (ft)	5	Silty sand & sandy silt
Transition layer 15	11	Start depth: 56.87 (ft)	5	Silty sand & sandy silt
		End depth: 57.48 (ft)	4	Clay & silty clay
Transition layer 16	7	Start depth: 60.01 (ft)	4	Clay & silty clay
		End depth: 60.40 (ft)	5	Silty sand & sandy silt

Start depth: Depth where the transition layer begins
End depth: Depth where the transition layer ends

:: Field input data ::

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1	0.09	12.04	0.33	0.00	4.96	114.84
2	0.15	72.31	0.35	0.10	2.03	117.27
3	0.21	181.00	0.36	0.10	0.62	119.34
4	0.29	229.77	0.64	0.10	0.92	121.09
5	0.34	205.07	0.85	0.00	1.56	122.13
6	0.40	202.93	1.11	0.10	1.67	123.74
7	0.49	215.95	1.31	0.00	2.15	124.99
8	0.55	212.92	1.49	0.10	3.19	125.86
9	0.59	200.26	1.77	0.10	4.71	126.44
10	0.69	139.45	2.09	0.00	6.14	126.97
11	0.74	109.67	2.12	0.00	7.81	127.37
12	0.81	96.92	2.06	0.00	9.77	127.66
13	0.89	79.44	2.24	0.19	11.99	127.85
14	0.94	95.45	2.40	0.29	14.07	127.74
15	0.99	85.77	2.58	0.29	15.02	127.64
16	1.09	93.98	2.69	0.10	15.41	127.64
17	1.14	94.33	2.76	-0.95	15.51	127.76
18	1.19	94.33	2.26	-1.15	14.67	128.03
19	1.26	94.33	2.15	-0.29	14.63	128.15
20	1.34	94.33	2.25	-0.86	14.73	128.18
21	1.38	99.59	2.40	-0.33	14.75	128.18
22	1.50	128.21	2.64	-1.43	14.92	128.09
23	1.53	104.05	2.69	-0.38	15.22	127.90
24	1.59	83.37	2.69	0.10	15.95	127.72
25	1.68	92.99	2.70	-0.67	16.76	127.51
26	1.72	82.03	2.57	-1.34	17.68	127.24
27	1.78	72.13	1.90	-1.34	19.07	127.01
28	1.87	56.62	1.94	-0.86	20.70	126.79
29	1.93	54.39	1.97	-0.95	21.42	126.70
30	1.98	56.88	2.03	-0.67	22.17	126.44
31	2.06	76.59	2.48	-0.57	22.39	126.13
32	2.13	52.25	2.62	0.57	21.96	126.17
33	2.17	62.95	2.68	0.10	20.78	126.30
34	2.28	65.98	2.26	0.19	19.88	126.40
35	2.32	66.42	1.92	0.38	19.30	126.44
36	2.39	82.47	1.87	0.38	19.20	126.14
37	2.43	88.63	1.95	0.19	18.32	125.79
38	2.52	80.16	1.96	0.19	17.91	125.25
39	2.57	73.65	1.97	0.19	17.79	124.83
40	2.66	67.14	1.78	0.38	17.83	124.57
41	2.69	61.43	1.64	0.48	18.61	124.26
42	2.77	52.34	1.48	0.57	19.93	123.86
43	2.86	52.87	1.44	0.76	21.26	123.45
44	2.92	55.64	1.46	0.86	22.71	123.12
45	2.96	51.27	1.48	0.76	24.02	122.83
46	3.06	44.67	1.52	0.76	24.79	122.54
47	3.11	39.85	1.52	0.76	24.21	122.33
48	3.15	37.72	1.68	0.86	22.69	122.09

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
49	3.26	37.80	1.54	1.14	19.67	121.99
50	3.30	42.44	1.30	1.24	16.81	121.86
51	3.37	55.64	1.07	1.62	14.04	121.68
52	3.46	70.44	0.85	1.43	12.32	121.55
53	3.51	106.90	0.84	0.48	11.24	121.41
54	3.56	109.94	0.84	0.19	10.62	121.46
55	3.64	113.50	0.83	0.10	10.72	121.63
56	3.71	91.39	1.07	0.10	11.37	121.89
57	3.76	71.95	1.32	0.38	12.61	122.21
58	3.81	64.82	1.49	0.48	14.98	122.14
59	3.90	45.38	1.51	0.76	18.14	121.90
60	3.94	40.48	1.50	0.86	22.47	121.55
61	4.01	37.36	1.48	0.95	26.15	120.98
62	4.09	28.80	1.18	1.14	28.99	120.27
63	4.15	22.65	1.05	1.14	31.74	119.39
64	4.20	22.74	1.02	1.34	33.03	118.55
65	4.30	26.57	0.81	1.43	33.97	117.68
66	4.35	26.12	0.75	1.34	34.74	116.75
67	4.41	24.34	0.71	1.24	35.00	116.12
68	4.50	22.47	0.69	1.34	34.63	115.65
69	4.55	21.76	0.68	1.14	34.30	115.17
70	4.60	20.60	0.67	1.34	35.12	114.89
71	4.68	19.79	0.66	1.14	36.19	114.72
72	4.75	19.44	0.64	1.24	37.17	114.64
73	4.79	19.35	0.64	1.24	38.00	114.66
74	4.88	18.90	0.65	1.24	38.80	114.73
75	4.95	18.63	0.69	1.43	39.52	114.82
76	4.99	18.63	0.71	1.62	40.07	114.96
77	5.06	18.63	0.75	1.81	40.57	115.14
78	5.14	18.63	0.77	1.81	41.05	115.33
79	5.21	18.19	0.78	1.81	41.40	115.52
80	5.26	18.59	0.79	2.29	41.61	115.66
81	5.33	18.99	0.81	1.14	41.90	115.78
82	5.40	19.08	0.82	1.34	42.13	115.87
83	5.45	19.17	0.82	1.24	42.35	115.96
84	5.51	19.08	0.82	1.05	42.46	116.06
85	5.60	18.55	0.83	1.43	42.60	116.14
86	5.66	18.55	0.84	1.62	42.72	116.20
87	5.71	18.55	0.86	1.62	42.92	116.23
88	5.78	18.63	0.87	1.72	43.23	116.24
89	5.86	18.81	0.87	1.81	43.59	116.22
90	5.93	19.08	0.87	1.81	43.93	116.15
91	6.01	18.55	0.86	1.24	44.26	116.05
92	6.05	18.01	0.85	1.24	44.63	115.89
93	6.11	17.39	0.82	1.24	45.11	115.66
94	6.21	16.58	0.79	1.53	45.75	115.39
95	6.25	16.32	0.77	1.53	46.50	115.09
96	6.31	15.69	0.74	1.43	47.31	114.77

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
97	6.39	14.80	0.70	1.34	48.06	114.44
98	6.45	14.27	0.68	1.34	48.75	114.13
99	6.51	13.91	0.66	1.34	49.21	113.84
100	6.58	13.37	0.65	1.29	49.70	113.58
101	6.66	13.11	0.63	1.24	50.04	113.37
102	6.70	13.02	0.62	0.95	50.02	113.23
103	6.78	13.20	0.60	0.86	49.91	113.11
104	6.85	13.20	0.61	0.76	49.56	113.03
105	6.89	13.37	0.61	0.67	48.99	112.96
106	7.00	13.91	0.60	0.67	48.31	112.93
107	7.03	13.91	0.60	0.67	47.37	112.93
108	7.10	14.35	0.59	0.48	46.44	112.94
109	7.19	14.53	0.58	0.38	45.34	112.97
110	7.25	14.89	0.58	0.38	44.30	113.02
111	7.30	15.78	0.58	0.38	43.45	113.13
112	7.37	16.14	0.57	0.38	42.64	113.28
113	7.44	16.94	0.58	0.38	42.05	113.45
114	7.49	17.21	0.60	0.38	41.76	113.61
115	7.56	17.65	0.63	0.38	41.48	113.69
116	7.64	18.01	0.66	0.48	41.38	113.67
117	7.68	17.92	0.67	0.38	41.72	113.72
118	7.79	16.94	0.67	0.29	42.31	113.74
119	7.83	16.67	0.62	0.29	42.92	113.69
120	7.90	16.05	0.56	0.19	43.66	113.57
121	7.98	15.25	0.62	-0.19	44.43	113.35
122	8.02	14.89	0.62	-0.29	45.27	113.07
123	8.09	14.62	0.60	-0.48	45.76	112.80
124	8.15	14.00	0.58	-0.76	46.28	112.59
125	8.23	13.73	0.55	-0.27	46.56	112.49
126	8.29	13.11	0.53	-0.52	46.19	112.35
127	8.34	13.46	0.52	-0.27	45.58	112.21
128	8.41	13.64	0.51	-0.48	44.89	112.16
129	8.48	14.53	0.51	0.19	43.97	112.17
130	8.55	15.42	0.52	0.19	42.99	112.25
131	8.60	15.87	0.52	0.19	41.88	112.40
132	8.66	16.41	0.54	0.19	40.91	112.56
133	8.74	17.03	0.55	0.38	40.02	112.76
134	8.83	17.65	0.56	0.29	39.38	113.03
135	8.90	18.10	0.57	0.48	38.93	113.31
136	8.94	18.28	0.57	0.29	38.63	113.59
137	9.01	18.72	0.59	0.38	38.53	113.87
138	9.09	19.35	0.64	0.38	38.58	114.14
139	9.15	19.70	0.67	0.10	38.78	114.38
140	9.20	19.62	0.68	-0.29	39.05	114.63
141	9.29	19.44	0.72	-0.86	39.37	114.89
142	9.35	19.26	0.73	-0.57	39.64	115.15
143	9.39	19.08	0.74	-0.57	39.81	115.33
144	9.45	19.17	0.76	-0.48	39.87	115.46

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
145	9.55	19.35	0.78	-0.29	39.59	115.61
146	9.64	19.97	0.80	-0.19	39.12	115.75
147	9.65	20.33	0.79	-0.19	38.50	115.92
148	9.73	20.77	0.78	-0.19	37.86	116.09
149	9.79	22.38	0.78	-0.19	37.38	116.26
150	9.84	23.18	0.81	-0.19	36.94	116.38
151	9.91	23.98	0.83	-0.29	36.57	116.46
152	9.99	24.16	0.84	-0.38	36.26	116.53
153	10.08	23.72	0.87	-1.05	35.93	116.58
154	10.14	23.72	0.85	-1.24	35.79	116.61
155	10.19	23.72	0.84	-1.34	35.76	116.60
156	10.25	23.72	0.82	-1.15	35.75	116.56
157	10.34	24.16	0.79	-1.15	35.92	116.52
158	10.38	24.16	0.79	-1.15	35.85	116.47
159	10.44	23.63	0.79	-1.15	35.69	116.42
160	10.52	24.07	0.79	-1.34	35.59	116.33
161	10.59	23.36	0.81	-1.43	35.51	116.25
162	10.63	23.98	0.82	-1.53	35.58	116.20
163	10.70	24.61	0.79	-1.53	35.73	116.14
164	10.78	23.98	0.75	-2.10	35.80	116.09
165	10.87	23.90	0.74	-2.00	35.54	116.15
166	10.93	23.45	0.75	-1.81	34.88	116.22
167	10.97	23.00	0.74	-1.72	34.54	116.30
168	11.03	23.27	0.75	-1.91	34.55	116.45
169	11.12	27.10	0.81	-1.05	34.73	116.66
170	11.16	29.07	0.82	-1.05	34.52	116.89
171	11.23	27.64	0.86	-1.05	34.31	117.13
172	11.31	26.84	0.91	-1.05	34.11	117.39
173	11.37	26.04	0.93	-1.89	33.75	117.69
174	11.44	28.71	0.93	-2.14	33.71	117.96
175	11.51	28.71	0.94	-2.29	33.88	118.20
176	11.56	28.71	0.96	-2.38	33.77	118.42
177	11.63	30.67	1.00	-2.29	33.60	118.59
178	11.71	31.74	1.06	-2.48	33.53	118.73
179	11.76	31.83	1.07	-2.29	33.80	118.81
180	11.83	32.19	1.07	-2.48	34.12	118.84
181	11.91	31.47	1.07	-2.86	34.47	118.85
182	11.94	29.60	1.07	-2.77	34.99	118.78
183	12.05	28.00	1.03	-2.86	35.57	118.65
184	12.10	27.28	1.00	-2.86	35.98	118.50
185	12.14	26.66	0.99	-2.38	36.44	118.35
186	12.25	25.77	0.97	-2.29	36.85	118.21
187	12.29	26.04	0.96	-2.29	37.01	118.09
188	12.35	26.93	0.95	-2.19	37.11	118.01
189	12.44	26.93	0.95	-2.19	37.11	117.94
190	12.49	27.10	0.95	-2.19	36.89	117.86
191	12.55	26.93	0.95	-2.19	36.57	117.78
192	12.61	26.57	0.96	-2.19	36.33	117.65

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
193	12.70	26.66	0.92	-2.19	36.52	117.47
194	12.75	27.37	0.89	-2.19	36.82	117.24
195	12.81	27.10	0.86	-2.19	37.15	116.89
196	12.89	26.21	0.81	-2.19	37.47	116.43
197	12.94	23.63	0.79	-2.19	37.76	115.89
198	12.99	22.11	0.75	-2.38	38.26	115.33
199	13.08	20.77	0.65	-2.00	39.06	114.74
200	13.15	19.70	0.57	-2.00	40.07	114.10
201	13.20	18.72	0.53	-2.00	41.17	113.45
202	13.27	17.65	0.51	-1.91	41.96	112.77
203	13.32	17.12	0.50	-1.91	42.57	112.10
204	13.39	15.87	0.47	-1.91	43.31	111.52
205	13.48	15.16	0.44	-1.91	44.21	111.05
206	13.54	14.62	0.42	-1.91	45.28	110.62
207	13.59	14.35	0.40	-1.91	46.18	110.23
208	13.65	13.64	0.37	-1.91	47.03	109.85
209	13.74	13.29	0.37	-1.91	47.60	109.53
210	13.80	12.22	0.36	-1.91	47.85	109.20
211	13.89	12.30	0.36	-1.91	47.83	108.87
212	13.93	12.30	0.36	-1.81	48.20	108.69
213	13.99	12.48	0.35	-1.81	49.05	108.74
214	14.07	12.66	0.31	-1.81	49.73	108.86
215	14.12	13.02	0.29	-1.81	49.94	109.03
216	14.18	12.39	0.34	-1.81	49.09	109.31
217	14.26	11.77	0.41	-1.81	47.44	109.74
218	14.34	12.30	0.43	-1.72	46.06	110.20
219	14.38	12.66	0.43	-1.81	45.65	110.80
220	14.47	16.23	0.45	-1.81	45.75	111.44
221	14.53	19.62	0.49	-1.81	45.57	111.97
222	14.57	19.79	0.51	-1.81	45.00	112.37
223	14.64	18.01	0.57	-1.81	44.63	112.68
224	14.72	17.21	0.60	-1.72	44.38	112.94
225	14.80	16.94	0.61	-1.72	44.93	113.04
226	14.83	16.94	0.61	-1.72	45.96	113.03
227	14.92	16.23	0.59	-1.62	47.13	113.02
228	14.97	15.87	0.57	-1.62	47.59	113.04
229	15.06	15.07	0.53	-1.62	47.83	113.16
230	15.10	15.78	0.53	-1.62	47.97	113.40
231	15.17	15.69	0.55	-1.53	47.77	113.81
232	15.25	16.67	0.60	-1.53	46.87	114.41
233	15.31	17.48	0.68	-1.53	45.66	115.10
234	15.37	18.37	0.77	-1.53	43.93	115.94
235	15.44	20.95	0.87	-1.53	42.10	116.86
236	15.51	24.70	0.97	-1.53	40.31	117.76
237	15.56	26.84	1.02	-1.43	38.48	118.67
238	15.63	30.85	1.11	-1.53	36.98	119.59
239	15.71	34.86	1.23	-1.53	35.62	120.41
240	15.76	36.65	1.29	-1.53	34.51	121.11

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
241	15.82	40.48	1.41	-1.34	33.67	121.67
242	15.90	42.08	1.61	-1.34	33.11	122.14
243	15.95	43.06	1.67	-1.34	32.79	122.49
244	16.01	43.60	1.70	-1.43	32.40	122.74
245	16.10	43.78	1.68	-1.43	31.68	122.98
246	16.16	42.35	1.65	-1.43	30.85	123.18
247	16.21	41.91	1.62	-1.43	29.57	123.36
248	16.29	45.03	1.59	-1.34	28.18	123.58
249	16.36	51.09	1.59	-1.34	26.95	123.81
250	16.41	55.81	1.62	-1.43	26.17	124.07
251	16.49	63.93	1.72	-1.53	25.63	124.31
252	16.55	69.28	1.82	-1.62	25.49	124.52
253	16.60	69.90	1.90	-1.62	25.85	124.65
254	16.70	64.64	1.99	-1.62	26.60	124.74
255	16.74	60.01	2.00	-1.62	27.53	124.65
256	16.80	51.27	1.98	-1.62	28.60	124.20
257	16.89	42.80	1.91	-1.62	30.13	123.65
258	16.93	40.75	1.89	-1.53	32.06	122.98
259	17.00	37.45	1.63	-1.62	34.10	122.18
260	17.09	34.24	1.04	-1.43	36.18	121.24
261	17.14	32.99	1.05	-1.43	37.60	120.22
262	17.20	29.33	1.03	-1.43	38.27	119.19
263	17.28	25.05	0.95	-1.43	38.97	118.03
264	17.34	22.47	0.82	-1.24	39.73	117.00
265	17.41	22.29	0.73	-1.24	41.27	116.50
266	17.48	22.20	0.70	-1.24	42.83	116.03
267	17.56	20.06	0.68	-1.05	43.77	115.69
268	17.62	19.70	0.68	-1.05	43.79	115.59
269	17.67	19.79	0.70	-1.05	43.39	115.92
270	17.72	19.79	0.74	-1.05	42.12	116.58
271	17.78	21.40	0.80	-1.05	40.11	117.40
272	17.87	24.16	0.87	-1.05	36.88	118.40
273	17.94	27.82	1.06	-0.95	33.84	119.49
274	18.01	36.11	1.22	-0.95	31.30	120.47
275	18.06	43.60	1.32	-0.95	28.99	121.39
276	18.12	55.64	1.43	-0.95	27.28	122.18
277	18.21	62.23	1.60	-1.24	26.18	122.82
278	18.25	63.66	1.63	-1.24	25.54	123.11
279	18.31	67.05	1.67	-1.34	25.51	123.13
280	18.40	64.46	1.69	-1.34	25.86	122.96
281	18.44	58.67	1.67	-1.34	27.03	122.54
282	18.51	47.08	1.42	-1.34	28.73	121.89
283	18.58	37.63	1.25	-1.34	30.50	121.18
284	18.64	33.26	1.09	-1.24	32.96	120.37
285	18.71	25.59	0.96	-1.24	35.55	119.49
286	18.80	21.58	0.86	-1.05	38.15	118.63
287	18.86	25.46	0.86	-0.95	40.42	118.13
288	18.91	24.25	0.89	-0.86	41.68	118.11

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
289	18.98	25.32	0.87	-0.95	42.12	118.34
290	19.05	25.50	0.93	-0.95	40.21	118.97
291	19.10	25.14	1.07	-0.95	37.21	120.00
292	19.20	29.69	1.32	-0.95	34.90	120.98
293	19.23	33.70	1.36	-0.86	32.49	121.99
294	19.30	46.45	1.51	-0.95	30.23	123.00
295	19.39	59.38	1.82	-0.95	28.17	123.94
296	19.43	63.22	1.91	-0.95	26.01	124.82
297	19.50	69.55	2.06	-0.95	24.22	125.55
298	19.57	76.77	2.16	-0.86	22.66	126.25
299	19.63	80.78	2.23	-0.86	21.67	126.85
300	19.70	89.16	2.33	-0.95	21.22	127.32
301	19.77	91.30	2.42	-1.24	21.01	127.75
302	19.84	97.72	2.52	-1.15	20.60	127.70
303	19.90	98.34	2.63	-1.15	20.80	127.70
304	19.99	93.62	2.83	-1.05	21.28	127.67
305	20.02	90.05	2.92	-1.05	22.30	127.62
306	20.09	80.87	1.82	-0.95	23.77	127.49
307	20.19	70.70	2.20	-0.95	25.60	127.29
308	20.21	65.36	2.28	-0.95	27.62	127.00
309	20.29	57.42	2.48	-0.86	29.68	126.65
310	20.38	47.26	2.50	-0.68	31.85	126.25
311	20.42	46.27	2.46	-0.68	34.26	126.26
312	20.52	45.38	2.40	-0.68	35.69	126.18
313	20.55	43.96	2.40	-0.48	36.22	126.17
314	20.62	43.24	2.41	-0.38	35.29	126.18
315	20.68	46.99	2.34	-0.38	33.11	126.33
316	20.75	50.55	2.27	-0.29	30.92	126.55
317	20.81	58.67	2.36	-0.38	28.58	126.84
318	20.90	69.81	2.32	-0.38	26.41	127.14
319	20.96	81.23	2.42	-0.38	24.33	127.45
320	21.01	86.40	2.52	-0.38	22.59	127.75
321	21.09	95.76	2.60	-0.48	21.13	128.04
322	21.15	98.97	2.64	-0.48	19.98	128.26
323	21.21	103.60	2.67	-0.57	19.26	128.44
324	21.30	106.55	2.66	-0.57	18.90	128.54
325	21.36	107.97	2.61	-0.57	18.65	128.60
326	21.40	107.80	2.57	-0.76	18.67	128.63
327	21.49	105.30	2.58	-0.76	18.99	128.69
328	21.56	101.55	2.59	-0.76	19.52	128.77
329	21.60	99.41	2.59	-0.86	20.28	128.88
330	21.66	97.27	2.69	-0.76	21.29	129.07
331	21.75	90.77	2.90	-0.86	22.38	129.27
332	21.80	88.72	3.05	-0.76	23.47	129.44
333	21.85	85.51	3.22	-0.76	24.71	129.46
334	21.95	84.61	3.50	-0.67	26.03	129.40
335	21.99	83.72	3.53	-0.67	27.38	129.19
336	22.05	81.58	3.49	-0.67	28.49	128.79

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
337	22.14	67.41	3.05	-0.67	29.47	128.20
338	22.19	62.59	2.80	-0.67	30.37	127.52
339	22.26	55.73	2.42	-0.67	31.21	126.64
340	22.35	50.20	1.96	-0.67	32.11	125.65
341	22.44	46.54	1.51	-0.48	33.11	124.54
342	22.45	44.76	1.49	-0.48	33.70	123.59
343	22.54	41.82	1.37	-0.48	34.32	122.71
344	22.58	40.48	1.32	-0.48	34.79	122.02
345	22.65	38.07	1.29	-0.48	35.26	121.68
346	22.73	36.65	1.32	-0.48	35.59	121.70
347	22.79	35.75	1.35	-0.38	35.60	121.85
348	22.85	36.29	1.38	-0.29	35.20	122.44
349	22.93	38.78	1.50	-0.19	34.86	123.38
350	22.99	43.87	1.57	-0.10	34.22	124.47
351	23.04	47.97	1.72	-0.19	32.97	125.51
352	23.12	58.13	2.23	-0.19	31.84	126.40
353	23.19	65.18	2.88	-0.29	31.01	127.04
354	23.27	71.69	3.25	0.29	30.35	127.54
355	23.30	80.87	3.33	0.38	29.73	127.91
356	23.38	79.00	3.22	0.06	28.94	128.24
357	23.47	70.35	2.82	0.00	28.21	128.38
358	23.50	67.76	2.68	0.10	27.34	128.29
359	23.58	68.92	2.48	0.29	26.72	128.05
360	23.66	76.23	2.45	0.19	26.65	127.75
361	23.69	79.44	2.44	0.00	26.68	127.48
362	23.77	80.60	2.38	-0.19	26.73	127.38
363	23.84	76.41	2.39	0.00	26.66	127.35
364	23.92	70.70	2.46	-0.10	26.73	127.39
365	23.97	67.94	2.50	0.00	27.09	127.39
366	24.06	66.25	2.58	0.00	27.64	127.38
367	24.12	68.48	2.58	0.00	28.34	127.39
368	24.17	69.37	2.58	-0.19	28.98	127.40
369	24.23	68.74	2.53	-0.19	29.62	127.30
370	24.31	68.03	2.54	-0.19	30.30	127.13
371	24.36	67.41	2.59	-0.19	31.11	126.84
372	24.42	64.37	2.56	-0.29	32.22	126.39
373	24.51	55.28	2.33	-0.29	33.56	125.85
374	24.54	50.55	2.22	-0.29	34.93	125.18
375	24.62	42.71	1.99	-0.29	36.43	124.33
376	24.71	36.82	1.68	-0.29	38.19	123.30
377	24.74	34.24	1.54	-0.29	40.06	122.16
378	24.81	32.37	1.26	-0.29	41.76	121.03
379	24.89	29.60	0.99	-0.19	43.28	119.83
380	24.96	26.48	0.87	-0.19	44.17	118.67
381	25.01	25.14	0.84	-0.19	44.60	117.67
382	25.10	22.29	0.77	-0.19	44.86	116.71
383	25.14	21.76	0.74	-0.10	45.29	115.94
384	25.21	21.40	0.68	0.00	45.84	115.43

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
385	25.30	21.84	0.65	0.00	46.13	115.07
386	25.34	21.84	0.65	0.00	46.14	114.74
387	25.41	21.76	0.62	0.10	45.86	114.53
388	25.50	21.76	0.61	0.19	45.54	114.36
389	25.55	21.76	0.61	0.19	45.10	114.29
390	25.60	21.93	0.60	0.19	44.69	114.23
391	25.70	21.76	0.61	0.19	44.16	114.13
392	25.75	21.84	0.61	0.19	43.53	114.00
393	25.80	22.83	0.61	0.19	42.53	113.75
394	25.89	23.27	0.59	0.29	41.59	113.51
395	25.95	23.63	0.56	0.29	40.75	113.29
396	25.99	23.72	0.51	0.29	39.73	113.12
397	26.06	24.34	0.41	0.29	39.00	112.98
398	26.15	24.34	0.42	0.29	38.51	112.83
399	26.19	24.34	0.44	0.29	38.19	112.72
400	26.25	25.59	0.47	0.38	38.15	112.72
401	26.34	24.61	0.50	0.38	38.51	112.83
402	26.38	24.34	0.51	0.48	39.39	113.08
403	26.45	24.07	0.52	0.57	40.23	113.29
404	26.52	24.07	0.56	0.57	41.01	113.45
405	26.61	23.00	0.58	0.57	41.97	113.52
406	26.67	22.02	0.58	0.57	42.66	113.49
407	26.72	22.02	0.57	0.67	43.20	113.43
408	26.82	21.93	0.56	0.57	43.58	113.29
409	26.86	21.49	0.55	0.67	43.75	113.03
410	26.94	21.04	0.51	0.57	43.52	112.66
411	26.98	21.13	0.49	0.67	42.98	112.24
412	27.06	21.13	0.45	0.67	42.39	111.82
413	27.10	21.04	0.42	0.67	41.67	111.41
414	27.17	20.77	0.36	0.76	40.84	111.00
415	27.26	20.86	0.34	0.76	40.05	110.73
416	27.31	21.22	0.34	0.76	39.33	110.56
417	27.39	21.76	0.34	0.76	38.82	110.53
418	27.44	22.02	0.34	0.76	38.36	110.56
419	27.51	22.74	0.37	0.76	38.10	110.71
420	27.58	23.36	0.40	0.76	38.01	110.88
421	27.63	23.63	0.42	0.76	37.96	111.05
422	27.71	23.81	0.42	0.76	38.14	111.21
423	27.79	23.63	0.41	0.76	38.54	111.36
424	27.86	23.18	0.41	0.76	39.00	111.44
425	27.89	23.18	0.41	0.76	39.57	111.49
426	27.96	22.38	0.41	0.76	40.28	111.53
427	28.05	21.49	0.42	0.86	41.19	111.64
428	28.09	21.22	0.42	0.86	42.28	111.86
429	28.16	20.86	0.44	0.86	43.44	112.11
430	28.23	20.51	0.46	0.76	44.60	112.35
431	28.29	20.51	0.50	0.76	45.60	112.58
432	28.35	20.42	0.55	0.76	46.41	112.79

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
433	28.44	20.15	0.57	0.76	47.07	112.98
434	28.50	20.24	0.57	0.67	47.70	113.15
435	28.55	20.24	0.57	0.67	48.08	113.29
436	28.64	19.97	0.56	0.67	48.22	113.38
437	28.69	20.28	0.55	0.86	48.00	113.46
438	28.75	19.88	0.56	0.86	47.18	113.52
439	28.82	20.33	0.56	0.86	46.07	113.57
440	28.89	20.95	0.56	0.86	45.14	113.89
441	28.98	22.11	0.59	0.86	44.39	114.33
442	29.04	24.16	0.57	0.86	43.78	114.75
443	29.08	25.68	0.56	0.86	43.10	115.17
444	29.15	27.64	0.73	0.76	42.63	115.58
445	29.24	28.09	0.81	0.76	42.33	115.99
446	29.29	27.82	0.81	0.76	41.79	116.40
447	29.34	28.00	0.82	0.76	41.67	116.77
448	29.43	27.73	0.84	0.76	41.86	117.12
449	29.47	27.64	0.86	0.76	42.27	117.21
450	29.53	30.40	0.89	0.76	42.78	117.21
451	29.62	29.69	0.88	0.76	43.41	117.18
452	29.66	29.16	0.87	0.76	44.30	117.14
453	29.77	26.39	0.84	0.76	45.30	117.05
454	29.81	25.14	0.84	0.76	46.49	117.02
455	29.86	23.98	0.82	0.76	46.96	117.11
456	29.92	22.38	0.83	0.76	46.80	117.30
457	30.01	21.49	0.82	0.76	45.97	117.59
458	30.09	21.04	0.90	0.76	44.94	117.89
459	30.17	29.16	1.00	0.95	44.48	118.14
460	30.20	32.90	1.05	0.76	44.72	118.37
461	30.27	37.18	1.09	0.76	45.07	118.64
462	30.32	36.11	1.07	0.76	44.80	118.97
463	30.39	31.38	1.07	0.48	44.08	119.26
464	30.47	25.59	1.07	0.67	43.97	119.40
465	30.55	24.16	1.15	0.86	44.08	119.44
466	30.62	27.73	1.17	0.95	44.66	119.40
467	30.66	29.78	1.18	0.95	45.25	119.37
468	30.72	32.10	1.15	0.76	45.23	119.18
469	30.81	32.99	1.10	0.76	44.45	118.99
470	30.85	33.17	1.09	0.76	43.44	118.66
471	30.91	32.01	1.07	0.76	42.92	118.16
472	31.01	29.16	0.85	0.86	42.52	117.55
473	31.05	27.91	0.78	0.86	42.61	116.86
474	31.11	26.12	0.71	0.95	43.02	116.09
475	31.20	24.43	0.61	0.95	43.56	115.25
476	31.26	24.43	0.55	0.95	43.93	114.36
477	31.31	22.65	0.52	0.95	44.44	113.76
478	31.38	21.40	0.48	0.95	44.95	113.26
479	31.46	20.69	0.47	0.95	45.17	112.86
480	31.51	20.69	0.47	1.14	45.26	112.58

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
481	31.60	20.69	0.49	1.05	45.46	112.35
482	31.65	20.86	0.50	1.05	45.28	112.13
483	31.74	21.58	0.49	1.05	45.00	111.89
484	31.80	21.58	0.46	1.05	44.54	111.65
485	31.85	21.67	0.43	1.05	43.96	111.35
486	31.89	21.58	0.40	1.05	43.09	110.89
487	32.00	20.77	0.35	1.14	42.24	110.40
488	32.04	20.77	0.34	1.14	41.48	109.91
489	32.09	20.77	0.31	1.14	40.77	109.53
490	32.19	20.77	0.26	1.24	40.16	109.26
491	32.23	20.77	0.27	1.24	40.06	109.09
492	32.29	21.13	0.28	1.24	39.46	109.25
493	32.37	21.84	0.30	1.24	38.92	109.46
494	32.44	22.56	0.32	1.24	38.50	109.80
495	32.49	20.77	0.34	1.24	38.30	110.35
496	32.58	25.14	0.39	1.72	38.02	110.90
497	32.62	25.41	0.40	1.72	37.80	111.43
498	32.69	26.04	0.42	1.72	37.73	111.92
499	32.78	26.93	0.46	1.81	37.78	112.38
500	32.82	27.64	0.48	1.81	37.56	112.85
501	32.89	27.73	0.50	1.81	37.93	113.22
502	32.97	27.46	0.52	1.81	38.29	113.60
503	33.02	27.28	0.54	1.81	38.70	113.96
504	33.09	27.37	0.57	1.81	39.32	114.36
505	33.15	27.10	0.60	1.81	40.07	114.76
506	33.20	27.55	0.62	1.81	40.82	115.16
507	33.28	27.82	0.65	1.81	41.29	115.63
508	33.38	27.82	0.73	1.81	41.57	116.09
509	33.43	27.82	0.77	1.81	41.65	116.54
510	33.47	28.09	0.81	1.81	41.63	116.98
511	33.57	30.40	0.88	1.81	41.78	117.43
512	33.63	31.47	0.90	1.72	41.93	117.84
513	33.70	32.72	0.94	1.72	41.95	118.20
514	33.74	32.99	0.97	1.72	41.91	118.53
515	33.82	32.90	1.03	1.72	41.85	118.83
516	33.86	32.72	1.05	1.72	41.97	119.05
517	33.93	32.81	1.08	1.72	42.27	119.25
518	34.02	33.08	1.11	1.53	42.71	119.41
519	34.06	33.08	1.12	1.62	43.12	119.54
520	34.13	32.99	1.13	1.62	43.47	119.61
521	34.21	32.63	1.15	1.62	43.78	119.65
522	34.28	32.37	1.16	1.62	44.10	119.65
523	34.32	32.19	1.15	1.62	44.43	119.58
524	34.41	31.74	1.14	1.62	44.82	119.48
525	34.46	31.47	1.12	1.62	45.19	119.36
526	34.52	30.85	1.10	1.62	45.57	119.17
527	34.61	29.96	1.05	1.72	45.99	118.94
528	34.65	29.33	1.03	1.72	46.32	118.68

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
529	34.71	28.98	1.01	1.72	46.60	118.38
530	34.79	27.82	0.96	1.72	46.78	118.02
531	34.86	26.84	0.92	1.72	46.85	117.62
532	34.93	26.84	0.88	1.81	46.80	117.22
533	35.01	26.30	0.83	1.91	46.70	116.82
534	35.06	25.95	0.75	1.91	46.62	116.44
535	35.11	25.77	0.71	1.91	46.57	116.12
536	35.18	25.50	0.66	1.91	46.47	115.85
537	35.26	25.32	0.66	1.91	46.52	115.65
538	35.34	25.05	0.67	1.91	46.76	115.50
539	35.40	24.61	0.69	1.91	47.07	115.45
540	35.44	24.52	0.70	1.91	47.51	115.45
541	35.51	24.52	0.72	1.81	48.13	115.52
542	35.58	23.72	0.73	1.81	48.81	115.56
543	35.66	23.98	0.72	1.81	49.36	115.53
544	35.71	23.72	0.73	1.81	49.71	115.43
545	35.77	23.45	0.74	1.81	49.91	115.28
546	35.85	22.74	0.72	1.81	50.08	115.07
547	35.92	22.38	0.67	1.81	50.09	114.86
548	35.97	22.20	0.63	1.91	49.99	114.72
549	36.03	22.20	0.59	1.91	49.73	114.58
550	36.11	21.93	0.57	1.91	49.28	114.39
551	36.16	21.84	0.58	1.91	48.56	114.16
552	36.26	23.09	0.61	1.91	48.00	113.91
553	36.31	23.63	0.62	1.91	47.46	113.71
554	36.36	23.72	0.59	1.91	47.31	113.39
555	36.43	23.81	0.54	1.81	47.20	113.08
556	36.51	22.74	0.49	1.91	46.98	112.78
557	36.55	22.74	0.48	1.81	46.92	112.54
558	36.65	19.97	0.39	1.91	47.10	112.34
559	36.71	19.79	0.39	1.91	47.11	112.35
560	36.76	20.15	0.40	1.91	46.67	112.47
561	36.85	21.31	0.48	1.91	46.02	112.81
562	36.89	21.31	0.52	1.91	45.29	113.23
563	36.96	23.81	0.59	1.91	44.36	113.91
564	37.02	26.93	0.59	1.91	43.49	114.64
565	37.11	28.89	0.65	2.00	42.79	115.35
566	37.15	30.23	0.69	2.00	42.25	116.02
567	37.24	31.56	0.76	2.00	41.81	116.76
568	37.31	32.37	0.82	2.00	41.57	117.42
569	37.35	32.45	0.86	1.91	41.63	118.12
570	37.43	32.72	0.95	1.91	40.80	118.85
571	37.51	33.79	1.09	2.10	39.25	119.57
572	37.55	34.68	1.16	2.10	37.12	120.11
573	37.60	36.56	1.25	2.10	34.84	120.32
574	37.67	46.27	1.35	2.10	32.77	120.38
575	37.75	54.39	1.36	2.10	31.47	120.29
576	37.81	60.27	1.22	2.00	30.83	120.14

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
577	37.88	59.29	0.87	1.91	30.67	119.99
578	37.93	56.88	0.74	2.00	30.57	119.93
579	38.00	46.72	0.72	1.81	30.26	120.14
580	38.08	38.61	0.85	2.00	29.52	120.84
581	38.14	33.79	0.98	2.10	29.16	121.98
582	38.20	36.65	1.17	2.29	29.00	123.32
583	38.26	55.37	1.56	2.38	28.86	124.82
584	38.34	81.05	2.10	2.19	27.68	126.40
585	38.43	94.78	2.67	2.19	26.15	127.82
586	38.45	99.59	2.86	2.19	24.49	129.17
587	38.53	105.74	3.36	2.19	23.02	130.37
588	38.62	125.81	3.83	2.29	21.93	131.37
589	38.65	131.96	4.00	2.38	21.22	132.16
590	38.72	143.01	4.37	2.38	20.57	132.81
591	38.80	150.06	4.57	2.38	19.95	133.41
592	38.88	158.80	4.76	2.38	19.33	133.90
593	38.93	164.50	4.91	2.38	18.98	134.28
594	39.01	173.15	5.14	2.38	18.74	134.63
595	39.07	179.12	5.27	2.38	18.59	134.91
596	39.12	180.11	5.34	2.38	18.41	135.18
597	39.20	180.11	5.52	2.38	18.27	135.44
598	39.27	180.11	5.69	2.38	18.15	135.69
599	39.31	180.11	5.76	2.38	18.04	135.91
600	39.38	188.04	5.92	2.38	18.00	136.11
601	39.45	195.35	6.15	2.38	17.93	136.30
602	39.51	199.63	6.27	2.38	17.76	136.49
603	39.57	204.54	6.37	2.38	17.51	136.66
604	39.64	204.27	6.44	2.38	17.19	136.82
605	39.72	207.30	6.46	2.48	16.95	136.92
606	39.79	213.63	6.57	2.48	16.85	136.92
607	39.84	219.87	6.61	2.48	16.95	136.85
608	39.90	224.95	6.58	2.38	17.14	136.74
609	39.96	219.87	6.38	2.00	17.27	136.58
610	40.06	203.73	6.05	2.10	17.41	136.40
611	40.13	183.49	5.88	2.19	17.59	136.19
612	40.17	176.81	5.77	2.29	17.74	135.97
613	40.26	176.67	5.51	2.38	17.94	135.71
614	40.31	176.67	5.40	2.38	18.17	135.43
615	40.36	176.54	5.36	2.38	18.39	135.07
616	40.43	185.01	5.38	2.19	18.54	134.67
617	40.51	184.56	5.21	1.91	18.91	134.23
618	40.56	174.40	4.86	1.91	18.96	133.85
619	40.64	153.36	4.18	1.91	19.56	133.40
620	40.70	136.15	3.84	2.00	19.57	132.99
621	40.75	113.59	3.71	2.19	19.28	132.56
622	40.83	139.14	3.64	2.67	18.88	132.15
623	40.88	106.55	3.61	2.86	18.04	131.76
624	40.95	142.12	3.51	2.86	16.62	131.35

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
625	41.03	164.77	3.36	2.29	15.10	131.05
626	41.08	173.06	3.36	2.10	13.44	130.87
627	41.15	187.59	2.98	1.91	12.26	130.69
628	41.24	199.81	2.09	1.81	10.92	130.54
629	41.28	204.09	2.18	1.81	10.14	130.29
630	41.35	211.31	2.42	1.81	9.65	130.02
631	41.41	212.38	2.55	1.81	9.26	129.72
632	41.48	207.30	2.56	1.81	9.20	129.52
633	41.55	190.80	2.47	2.00	9.67	129.66
634	41.63	185.37	2.39	2.10	10.23	129.78
635	41.68	181.80	2.39	2.10	11.04	129.89
636	41.74	174.49	2.46	2.10	11.96	129.99
637	41.83	167.00	2.63	2.10	13.05	130.11
638	41.87	163.08	2.72	2.10	14.14	130.30
639	41.98	150.50	3.05	2.10	15.41	130.54
640	42.02	145.78	3.18	2.10	16.82	130.76
641	42.10	136.42	3.34	2.00	18.29	130.94
642	42.14	131.87	3.45	2.00	19.72	131.07
643	42.22	125.72	3.62	2.00	21.21	131.16
644	42.29	119.12	3.67	2.00	22.51	131.19
645	42.38	111.72	3.64	2.00	23.79	131.19
646	42.41	108.24	3.61	2.00	24.91	131.18
647	42.46	105.83	3.61	2.00	25.96	131.15
648	42.57	101.11	3.63	2.10	26.86	131.07
649	42.61	99.68	3.67	2.10	27.64	130.98
650	42.68	97.72	3.70	2.10	28.27	130.89
651	42.76	96.65	3.68	2.10	28.86	130.79
652	42.80	95.13	3.65	2.10	29.40	130.68
653	42.87	91.84	3.57	2.10	29.79	130.56
654	42.92	90.05	3.51	2.10	30.08	130.43
655	42.98	87.91	3.41	2.19	30.40	130.23
656	43.06	86.49	3.35	2.19	30.83	129.85
657	43.11	86.13	3.31	2.29	31.37	129.40
658	43.18	86.58	3.28	2.19	32.25	128.89
659	43.26	80.87	3.05	2.10	33.53	128.28
660	43.32	69.81	2.46	2.10	35.21	127.57
661	43.39	64.02	2.29	2.10	37.05	126.77
662	43.46	52.96	2.13	2.10	39.10	125.82
663	43.52	42.71	1.96	2.19	41.54	124.67
664	43.61	34.33	1.72	2.48	44.17	123.45
665	43.64	33.44	1.57	3.15	46.93	122.39
666	43.70	32.10	1.33	3.24	49.69	121.31
667	43.79	29.96	1.09	3.34	51.42	120.29
668	43.84	29.24	0.98	3.34	51.89	119.36
669	43.90	27.19	0.90	3.43	51.44	118.69
670	43.97	27.02	0.84	3.53	51.20	118.20
671	44.05	27.37	0.81	3.72	51.03	117.99
672	44.10	27.55	0.81	3.72	50.59	118.12

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
673	44.18	28.09	0.91	3.72	50.17	118.51
674	44.24	28.62	1.02	3.72	49.56	119.04
675	44.30	30.67	1.11	3.82	48.90	119.70
676	44.38	33.88	1.19	3.82	48.02	120.45
677	44.45	36.73	1.37	3.82	46.88	121.22
678	44.49	37.80	1.45	3.82	45.31	121.89
679	44.57	40.21	1.57	3.82	43.73	122.48
680	44.64	44.40	1.71	3.91	42.73	123.06
681	44.72	47.79	1.78	3.91	42.23	123.55
682	44.79	51.62	1.78	3.91	41.97	123.92
683	44.84	52.61	1.79	3.91	41.57	124.24
684	44.92	51.45	1.98	3.91	39.52	124.55
685	44.96	49.22	2.01	3.91	36.80	124.81
686	45.03	47.79	2.03	4.01	33.46	125.04
687	45.09	49.40	2.03	4.01	29.46	125.30
688	45.19	69.81	1.91	4.20	26.14	125.54
689	45.23	83.81	1.84	4.20	23.25	125.71
690	45.28	101.11	1.74	4.10	21.21	126.02
691	45.38	127.77	1.68	3.72	19.62	126.37
692	45.43	129.82	1.69	3.63	18.48	126.78
693	45.48	129.82	1.78	3.63	18.43	127.32
694	45.58	122.69	2.22	3.63	18.91	127.86
695	45.62	118.58	2.39	3.63	20.08	128.32
696	45.67	114.57	2.64	3.53	22.17	128.63
697	45.78	102.27	3.07	3.53	24.58	128.86
698	45.82	96.47	3.21	3.53	27.22	128.96
699	45.88	82.56	3.20	3.53	29.47	128.81
700	45.98	70.17	3.07	3.53	31.67	128.56
701	46.02	66.07	2.98	3.53	33.80	128.24
702	46.07	61.61	2.77	3.63	35.10	127.80
703	46.17	61.61	2.34	3.82	36.13	127.31
704	46.21	61.61	2.19	3.82	36.65	126.83
705	46.27	61.61	2.16	3.72	37.12	126.38
706	46.37	64.37	2.09	3.72	37.61	125.94
707	46.39	64.02	2.07	3.72	38.12	125.58
708	46.47	59.29	2.02	3.72	39.13	125.39
709	46.57	49.84	2.02	3.72	40.23	125.23
710	46.62	46.90	2.02	3.82	41.23	125.05
711	46.67	44.94	2.03	3.91	42.55	124.88
712	46.77	44.05	2.06	3.91	43.92	124.72
713	46.82	44.76	1.99	3.91	45.04	124.60
714	46.90	46.19	1.92	4.01	45.34	124.53
715	46.92	46.54	1.91	4.01	45.41	124.45
716	47.01	46.81	1.90	4.01	45.44	124.45
717	47.05	46.36	1.92	4.01	45.33	124.46
718	47.12	45.65	1.89	4.10	45.33	124.52
719	47.21	44.76	1.88	4.10	45.74	124.58
720	47.28	44.85	2.01	4.10	45.42	124.69

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
721	47.32	45.38	2.07	4.10	45.28	124.78
722	47.40	46.45	2.12	4.20	45.30	124.90
723	47.45	44.13	2.10	4.20	45.18	125.08
724	47.55	52.07	2.09	3.82	44.73	125.27
725	47.58	50.20	2.07	3.91	43.82	125.39
726	47.66	49.13	2.18	3.91	42.47	125.51
727	47.74	51.09	2.27	3.91	41.00	125.62
728	47.80	53.67	2.23	3.91	39.34	125.78
729	47.85	56.97	2.17	3.72	38.29	125.92
730	47.93	62.59	2.13	3.72	37.31	126.07
731	47.98	65.80	2.15	3.72	36.23	126.20
732	48.04	68.39	2.21	3.63	35.07	126.28
733	48.11	69.55	2.25	3.63	33.88	126.37
734	48.20	68.12	2.27	3.63	32.92	126.47
735	48.24	68.21	2.29	3.63	32.28	126.59
736	48.30	71.15	2.26	3.53	31.71	126.70
737	48.39	75.43	2.22	3.53	31.20	126.80
738	48.44	76.59	2.23	3.53	30.71	126.91
739	48.53	78.28	2.31	3.53	30.18	127.06
740	48.59	80.51	2.31	3.53	29.69	127.21
741	48.64	81.49	2.33	3.53	29.41	127.36
742	48.70	83.63	2.44	3.43	29.32	127.54
743	48.78	84.44	2.52	3.43	29.11	127.75
744	48.82	84.44	2.55	3.43	28.83	127.94
745	48.89	83.54	2.59	3.43	28.42	128.15
746	48.98	84.97	2.66	3.43	27.72	128.36
747	49.05	90.05	2.72	3.43	26.87	128.56
748	49.09	93.17	2.77	3.43	25.98	128.75
749	49.16	99.33	2.77	3.34	24.96	128.94
750	49.24	108.33	2.76	3.34	23.89	129.17
751	49.31	114.84	2.79	3.24	22.84	129.38
752	49.38	117.87	2.82	3.24	21.97	129.55
753	49.43	123.76	2.84	3.24	21.24	129.66
754	49.52	129.46	2.97	3.24	20.59	129.62
755	49.58	132.05	2.98	3.24	20.06	129.47
756	49.63	131.60	2.97	3.24	19.80	129.26
757	49.71	127.95	2.88	3.24	19.88	129.07
758	49.77	123.40	2.45	3.15	20.26	128.86
759	49.82	120.10	2.13	3.24	20.96	128.58
760	49.88	112.79	2.11	3.15	22.19	128.21
761	49.97	102.80	2.30	3.24	23.57	127.79
762	50.01	96.20	2.38	3.24	24.85	127.39
763	50.07	86.31	2.42	3.34	26.27	127.20
764	50.17	67.67	2.31	3.43	27.94	127.15
765	50.22	66.25	2.24	3.53	29.61	127.14
766	50.29	71.77	2.18	3.53	31.26	126.99
767	50.37	77.66	2.30	3.43	32.46	126.80
768	50.42	78.64	2.36	3.43	33.52	126.54

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
769	50.47	75.79	2.41	3.43	33.95	126.33
770	50.57	64.46	2.27	3.53	34.72	126.03
771	50.63	67.32	2.12	3.43	35.97	125.63
772	50.68	59.11	2.00	3.43	37.49	125.03
773	50.73	53.59	1.87	3.43	39.18	124.19
774	50.79	44.67	1.68	3.43	40.91	123.23
775	50.88	40.93	1.48	3.63	42.12	122.24
776	50.93	39.85	1.26	3.53	43.89	121.08
777	51.03	35.75	0.92	3.53	45.08	119.85
778	51.07	34.06	0.86	3.53	45.92	118.51
779	51.14	31.56	0.78	3.53	45.81	117.12
780	51.23	29.33	0.58	3.43	45.26	115.68
781	51.27	28.71	0.51	3.43	44.95	114.26
782	51.33	26.93	0.44	3.43	44.59	113.19
783	51.42	25.68	0.35	3.43	44.25	112.17
784	51.48	25.77	0.31	3.43	43.63	111.27
785	51.52	24.61	0.29	3.43	43.36	110.95
786	51.60	25.86	0.29	3.43	43.14	110.92
787	51.68	25.32	0.33	3.53	42.82	111.11
788	51.72	25.95	0.36	3.53	42.49	111.53
789	51.81	27.73	0.44	3.53	42.61	112.08
790	51.87	29.69	0.49	3.53	42.78	112.67
791	51.91	30.67	0.51	3.53	43.35	113.12
792	51.98	31.74	0.52	3.53	44.03	113.42
793	52.07	31.03	0.56	3.53	44.79	113.61
794	52.10	30.14	0.58	3.53	45.55	113.51
795	52.17	27.64	0.54	3.43	46.53	113.22
796	52.24	24.88	0.51	3.43	47.68	112.84
797	52.31	23.98	0.49	3.43	49.01	112.37
798	52.37	22.56	0.41	3.43	50.05	111.73
799	52.46	21.67	0.36	3.43	50.89	111.00
800	52.51	21.22	0.34	3.43	51.30	110.33
801	52.57	21.04	0.31	3.43	51.14	109.69
802	52.66	20.86	0.28	3.43	50.84	109.06
803	52.71	20.60	0.27	3.43	50.55	108.63
804	52.78	20.69	0.27	3.43	50.31	108.33
805	52.86	20.60	0.26	3.53	50.08	108.08
806	52.91	20.51	0.26	3.43	49.96	107.92
807	52.99	20.51	0.26	3.43	49.86	107.82
808	53.06	20.51	0.26	3.34	49.74	107.76
809	53.09	20.42	0.26	3.34	49.58	107.67
810	53.16	20.42	0.26	3.34	49.48	107.64
811	53.25	20.69	0.25	3.34	49.39	107.61
812	53.29	20.69	0.25	3.34	49.33	107.58
813	53.36	20.69	0.24	3.34	49.33	107.55
814	53.45	20.86	0.25	3.24	49.26	107.52
815	53.50	20.77	0.25	3.34	49.22	107.48
816	53.55	20.60	0.25	3.24	49.32	107.51

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
817	53.64	20.37	0.25	3.34	49.42	107.55
818	53.69	20.60	0.25	2.96	49.44	107.58
819	53.76	20.42	0.25	3.05	49.40	107.59
820	53.84	20.60	0.26	3.05	49.40	107.66
821	53.88	20.69	0.26	3.05	49.45	107.83
822	53.96	20.95	0.25	3.05	49.29	108.05
823	54.03	21.13	0.25	3.15	49.14	108.25
824	54.08	21.40	0.27	3.15	49.05	108.42
825	54.17	21.67	0.30	3.15	48.99	108.55
826	54.23	22.65	0.31	3.15	48.95	108.68
827	54.27	22.74	0.31	3.15	48.95	108.81
828	54.38	22.11	0.30	3.15	48.92	108.87
829	54.42	21.93	0.30	3.15	48.76	108.85
830	54.47	21.93	0.30	3.15	48.40	108.69
831	54.53	21.93	0.29	3.15	48.14	108.48
832	54.61	21.93	0.27	3.15	47.90	108.27
833	54.68	21.93	0.26	3.05	47.69	108.11
834	54.73	21.93	0.24	3.15	47.50	107.99
835	54.80	22.20	0.24	3.05	47.45	107.92
836	54.88	22.20	0.24	3.15	47.44	107.93
837	54.95	21.93	0.25	3.05	47.52	108.03
838	55.02	21.84	0.26	3.05	47.67	108.19
839	55.07	21.76	0.28	3.05	47.96	108.40
840	55.15	22.11	0.29	3.05	48.39	108.64
841	55.21	22.47	0.30	3.05	48.80	108.87
842	55.27	22.65	0.31	3.15	48.83	109.02
843	55.34	22.47	0.31	3.05	48.60	109.15
844	55.42	22.38	0.32	3.05	48.27	109.26
845	55.47	22.38	0.32	3.05	48.01	109.39
846	55.54	23.09	0.30	3.05	48.08	109.73
847	55.62	23.90	0.30	3.05	48.11	110.08
848	55.65	24.07	0.31	3.05	47.78	110.51
849	55.72	24.34	0.33	3.05	47.06	110.99
850	55.81	25.05	0.42	3.05	46.42	111.59
851	55.84	25.59	0.44	3.05	46.09	112.33
852	55.91	27.64	0.47	3.05	46.50	113.48
853	55.98	30.05	0.50	3.05	46.92	114.68
854	56.05	31.12	0.56	3.05	46.80	115.80
855	56.11	32.19	0.64	3.05	44.64	116.78
856	56.21	33.88	0.91	3.05	41.45	117.93
857	56.26	35.40	1.05	3.05	38.22	119.07
858	56.31	38.61	1.10	3.05	34.41	120.34
859	56.39	51.45	1.09	3.05	31.61	121.46
860	56.46	65.98	1.27	2.96	28.86	122.53
861	56.50	75.61	1.38	2.96	26.67	123.36
862	56.60	96.65	1.59	2.96	25.12	124.08
863	56.65	95.31	1.68	2.96	24.09	124.70
864	56.72	106.10	1.79	2.77	23.72	125.24

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
865	56.78	102.36	1.87	2.77	23.79	125.51
866	56.87	95.13	1.96	2.77	24.17	125.63
867	56.93	88.27	2.00	2.77	25.33	125.53
868	56.97	83.90	1.99	2.77	26.62	125.29
869	57.05	76.14	1.79	2.86	28.46	124.87
870	57.11	71.24	1.68	2.86	30.49	124.31
871	57.17	62.86	1.59	2.86	32.52	123.62
872	57.25	55.19	1.43	2.86	34.49	122.79
873	57.31	51.45	1.29	2.86	36.65	121.83
874	57.37	45.20	1.15	2.86	38.69	120.86
875	57.42	40.21	1.03	2.86	40.56	119.80
876	57.48	37.09	0.91	2.96	41.94	118.71
877	57.56	33.08	0.80	3.05	42.99	117.63
878	57.64	32.28	0.67	3.05	43.91	116.53
879	57.70	32.45	0.55	3.05	44.31	115.51
880	57.74	31.83	0.51	3.05	44.13	114.49
881	57.81	30.05	0.47	3.05	43.78	113.55
882	57.90	28.98	0.41	3.15	43.11	112.76
883	57.95	28.80	0.40	3.15	42.74	112.18
884	58.06	28.53	0.35	3.34	43.34	112.08
885	58.09	28.18	0.35	3.24	44.13	112.18
886	58.15	28.13	0.36	3.43	44.42	112.44
887	58.20	28.13	0.38	3.43	43.77	112.70
888	58.29	28.09	0.52	3.43	42.71	112.91
889	58.33	28.62	0.58	3.53	41.66	113.17
890	58.40	31.30	0.60	3.53	41.30	113.49
891	58.48	35.58	0.52	3.63	41.24	113.75
892	58.55	37.45	0.47	3.63	41.20	113.95
893	58.60	38.16	0.45	3.63	41.08	113.84
894	58.66	34.59	0.51	3.72	40.39	113.52
895	58.75	31.92	0.50	3.72	39.94	113.07
896	58.80	31.03	0.49	3.72	40.30	112.66
897	58.88	27.55	0.45	3.82	41.13	112.29
898	58.97	29.33	0.38	4.58	42.30	111.90
899	59.02	28.89	0.35	4.67	42.75	111.39
900	59.06	28.35	0.33	4.67	42.77	110.92
901	59.12	28.00	0.32	4.67	42.38	110.46
902	59.20	26.75	0.30	4.77	41.59	110.12
903	59.26	26.66	0.30	4.77	41.47	109.96
904	59.35	27.10	0.31	4.87	41.51	109.93
905	59.41	28.62	0.30	4.87	41.72	110.06
906	59.46	28.80	0.31	4.96	42.00	110.27
907	59.52	28.53	0.32	5.06	42.09	110.59
908	59.61	28.53	0.34	5.06	42.09	110.95
909	59.68	28.53	0.38	5.15	42.01	111.25
910	59.72	28.53	0.40	5.15	42.24	111.55
911	59.79	29.51	0.42	5.25	42.55	111.78
912	59.86	30.49	0.44	5.25	42.89	111.97

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
913	59.91	30.85	0.43	5.34	41.62	111.25
914	60.01	30.49	0.43	5.34	40.10	110.37
915	60.06	29.69	0.42	5.34	38.49	109.29
916	60.15	28.62	0.41	5.44	36.60	107.97
917	60.19	28.44	0.00	5.44	34.52	106.25
918	60.26	28.53	0.00	5.44	31.96	104.10
919	60.35	27.55	0.00	5.53	29.17	101.02
920	60.40	28.62	0.00	5.53	25.45	95.86
921	60.45	28.26	0.00	5.63	N/A	87.36
922	60.51	30.14	0.00	5.72	N/A	87.36

Abbreviations

Depth: Depth from free surface, at which CPT was performed (ft)
q_c: Measured cone resistance (tsf)
f_s: Sleeve friction resistance (tsf)
u: Pore pressure (tsf)
Fines content: Percentage of fines in soil (%)
Unit weight: Bulk soil unit weight (pcf)

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data ::

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
1	0.09	0.01	0.00	0.01	1.00	0.358	1.34	0.266	1.00	1.00	2.000	No
2	0.15	0.01	0.00	0.01	1.00	0.358	1.34	0.266	1.00	1.00	2.000	No
3	0.21	0.01	0.00	0.01	1.00	0.358	1.34	0.266	1.00	1.00	2.000	No
4	0.29	0.02	0.00	0.02	1.00	0.358	1.34	0.266	1.00	1.00	2.000	No
5	0.34	0.02	0.00	0.02	1.00	0.358	1.34	0.266	1.00	1.00	2.000	No
6	0.40	0.02	0.00	0.02	1.00	0.358	1.34	0.266	1.00	1.00	2.000	No
7	0.49	0.03	0.00	0.03	1.00	0.358	1.34	0.266	1.00	1.00	2.000	No
8	0.55	0.03	0.00	0.03	1.00	0.358	1.34	0.266	1.00	1.00	2.000	No
9	0.59	0.04	0.00	0.04	1.00	0.358	1.34	0.266	1.00	1.00	2.000	No
10	0.69	0.04	0.00	0.04	1.00	0.358	1.34	0.266	1.00	1.00	2.000	No
11	0.74	0.05	0.00	0.05	1.00	0.358	1.34	0.266	1.00	1.00	2.000	No
12	0.81	0.05	0.00	0.05	1.00	0.357	1.34	0.266	1.00	1.00	2.000	No
13	0.89	0.05	0.00	0.05	1.00	0.357	1.34	0.266	1.00	1.00	2.000	No
14	0.94	0.06	0.00	0.06	1.00	0.357	1.34	0.266	1.00	1.00	2.000	No
15	0.99	0.06	0.00	0.06	1.00	0.357	1.34	0.266	1.00	1.00	2.000	No
16	1.09	0.07	0.00	0.07	1.00	0.357	1.34	0.266	1.00	1.00	2.000	No
17	1.14	0.07	0.00	0.07	1.00	0.357	1.34	0.266	1.00	1.00	2.000	No
18	1.19	0.07	0.00	0.07	1.00	0.357	1.34	0.266	1.00	1.00	2.000	No
19	1.26	0.08	0.00	0.08	1.00	0.357	1.34	0.266	1.00	1.00	2.000	No
20	1.34	0.08	0.00	0.08	1.00	0.357	1.34	0.266	1.00	1.00	2.000	No
21	1.38	0.09	0.00	0.09	1.00	0.357	1.34	0.266	1.00	1.00	2.000	No
22	1.50	0.09	0.00	0.09	1.00	0.357	1.34	0.265	1.00	1.00	2.000	No
23	1.53	0.10	0.00	0.10	1.00	0.357	1.34	0.265	1.00	1.00	2.000	No
24	1.59	0.10	0.00	0.10	1.00	0.357	1.34	0.265	1.00	1.00	2.000	No
25	1.68	0.11	0.00	0.11	1.00	0.357	1.34	0.265	1.00	1.00	2.000	No
26	1.72	0.11	0.00	0.11	1.00	0.357	1.34	0.265	1.00	1.00	2.000	No
27	1.78	0.11	0.00	0.11	1.00	0.357	1.34	0.265	1.00	1.00	2.000	No
28	1.87	0.12	0.00	0.12	1.00	0.357	1.34	0.265	1.00	1.00	2.000	No
29	1.93	0.12	0.00	0.12	1.00	0.357	1.34	0.265	1.00	1.00	2.000	No
30	1.98	0.12	0.00	0.12	1.00	0.357	1.34	0.265	1.00	1.00	2.000	No
31	2.06	0.13	0.00	0.13	1.00	0.356	1.34	0.265	1.00	1.00	2.000	No
32	2.13	0.13	0.00	0.13	1.00	0.356	1.34	0.265	1.00	1.00	2.000	No
33	2.17	0.14	0.00	0.14	1.00	0.356	1.34	0.265	1.00	1.00	2.000	No
34	2.28	0.14	0.00	0.14	1.00	0.356	1.34	0.265	1.00	1.00	2.000	No
35	2.32	0.15	0.00	0.15	1.00	0.356	1.34	0.265	1.00	1.00	2.000	No
36	2.39	0.15	0.00	0.15	1.00	0.356	1.34	0.265	1.00	1.00	2.000	No
37	2.43	0.15	0.00	0.15	1.00	0.356	1.34	0.265	1.00	1.00	2.000	No
38	2.52	0.16	0.00	0.16	1.00	0.356	1.34	0.265	1.00	1.00	2.000	No
39	2.57	0.16	0.00	0.16	1.00	0.356	1.34	0.265	1.00	1.00	2.000	No
40	2.66	0.17	0.00	0.17	1.00	0.356	1.34	0.265	1.00	1.00	2.000	No
41	2.69	0.17	0.00	0.17	1.00	0.356	1.34	0.265	1.00	1.00	2.000	No
42	2.77	0.17	0.00	0.17	1.00	0.356	1.34	0.265	1.00	1.00	2.000	No
43	2.86	0.18	0.00	0.18	1.00	0.356	1.34	0.265	1.00	1.00	2.000	No
44	2.92	0.18	0.00	0.18	1.00	0.356	1.34	0.265	1.00	1.00	2.000	No
45	2.96	0.19	0.00	0.19	1.00	0.356	1.34	0.265	1.00	1.00	2.000	No
46	3.06	0.19	0.00	0.19	0.99	0.356	1.34	0.265	1.00	1.00	2.000	No
47	3.11	0.19	0.00	0.19	0.99	0.356	1.34	0.264	1.00	1.00	2.000	No
48	3.15	0.20	0.00	0.20	0.99	0.356	1.34	0.264	1.00	1.00	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
49	3.26	0.20	0.00	0.20	0.99	0.355	1.34	0.264	1.00	1.00	2.000	No
50	3.30	0.21	0.00	0.21	0.99	0.355	1.34	0.264	1.00	1.00	2.000	No
51	3.37	0.21	0.00	0.21	0.99	0.355	1.34	0.264	1.00	1.00	2.000	No
52	3.46	0.22	0.00	0.22	0.99	0.355	1.34	0.264	1.00	1.00	2.000	No
53	3.51	0.22	0.00	0.22	0.99	0.355	1.34	0.264	1.00	1.00	2.000	No
54	3.56	0.22	0.00	0.22	0.99	0.355	1.34	0.264	1.00	1.00	2.000	No
55	3.64	0.23	0.00	0.23	0.99	0.355	1.34	0.264	1.00	1.00	2.000	Yes
56	3.71	0.23	0.00	0.23	0.99	0.355	1.34	0.264	1.00	1.00	2.000	Yes
57	3.76	0.23	0.00	0.23	0.99	0.355	1.34	0.264	1.00	1.00	2.000	Yes
58	3.81	0.24	0.00	0.24	0.99	0.355	1.34	0.264	1.00	1.00	2.000	Yes
59	3.90	0.24	0.00	0.24	0.99	0.355	1.34	0.264	1.00	1.00	2.000	Yes
60	3.94	0.25	0.00	0.25	0.99	0.355	1.34	0.264	1.00	1.00	2.000	Yes
61	4.01	0.25	0.00	0.25	0.99	0.355	1.34	0.264	1.00	1.00	2.000	Yes
62	4.09	0.25	0.00	0.25	0.99	0.355	1.34	0.264	1.00	1.00	2.000	Yes
63	4.15	0.26	0.00	0.26	0.99	0.355	1.34	0.264	1.00	1.00	2.000	Yes
64	4.20	0.26	0.00	0.26	0.99	0.355	1.34	0.264	1.00	1.00	2.000	Yes
65	4.30	0.27	0.00	0.27	0.99	0.355	1.34	0.264	1.00	1.00	2.000	No
66	4.35	0.27	0.00	0.27	0.99	0.355	1.34	0.264	1.00	1.00	2.000	No
67	4.41	0.27	0.00	0.27	0.99	0.355	1.34	0.264	1.00	1.00	2.000	No
68	4.50	0.28	0.00	0.28	0.99	0.354	1.34	0.264	1.00	1.00	2.000	No
69	4.55	0.28	0.00	0.28	0.99	0.354	1.34	0.264	1.00	1.00	2.000	No
70	4.60	0.28	0.00	0.28	0.99	0.354	1.34	0.264	1.00	1.00	2.000	No
71	4.68	0.29	0.00	0.29	0.99	0.354	1.34	0.263	1.00	1.00	2.000	No
72	4.75	0.29	0.00	0.29	0.99	0.354	1.34	0.263	1.00	1.00	2.000	No
73	4.79	0.30	0.00	0.30	0.99	0.354	1.34	0.263	1.00	1.00	2.000	No
74	4.88	0.30	0.00	0.30	0.99	0.354	1.34	0.263	1.00	1.00	2.000	No
75	4.95	0.30	0.00	0.30	0.99	0.354	1.34	0.263	1.00	1.00	2.000	No
76	4.99	0.31	0.00	0.31	0.99	0.354	1.34	0.263	1.00	1.00	2.000	No
77	5.06	0.31	0.00	0.31	0.99	0.354	1.34	0.263	1.00	1.00	2.000	No
78	5.14	0.32	0.00	0.32	0.99	0.354	1.34	0.263	1.00	1.00	2.000	No
79	5.21	0.32	0.00	0.32	0.99	0.354	1.34	0.263	1.00	1.00	2.000	No
80	5.26	0.32	0.00	0.32	0.99	0.354	1.34	0.263	1.00	1.00	2.000	No
81	5.33	0.33	0.00	0.33	0.99	0.354	1.34	0.263	1.00	1.00	2.000	No
82	5.40	0.33	0.00	0.33	0.99	0.354	1.34	0.263	1.00	1.00	2.000	No
83	5.45	0.33	0.00	0.33	0.99	0.354	1.34	0.263	1.00	1.00	2.000	No
84	5.51	0.34	0.00	0.34	0.99	0.354	1.34	0.263	1.00	1.00	2.000	No
85	5.60	0.34	0.00	0.34	0.99	0.354	1.34	0.263	1.00	1.00	2.000	No
86	5.66	0.35	0.00	0.35	0.99	0.353	1.34	0.263	1.00	1.00	2.000	No
87	5.71	0.35	0.00	0.35	0.99	0.353	1.34	0.263	1.00	1.00	2.000	No
88	5.78	0.35	0.00	0.35	0.99	0.353	1.34	0.263	1.00	1.00	2.000	No
89	5.86	0.36	0.00	0.36	0.99	0.353	1.34	0.263	1.00	1.00	2.000	No
90	5.93	0.36	0.00	0.36	0.99	0.353	1.34	0.263	1.00	1.00	2.000	No
91	6.01	0.37	0.00	0.37	0.99	0.353	1.34	0.263	1.00	1.00	2.000	No
92	6.05	0.37	0.00	0.37	0.99	0.353	1.34	0.263	1.00	1.00	2.000	No
93	6.11	0.37	0.00	0.37	0.99	0.353	1.34	0.263	1.00	1.00	2.000	No
94	6.21	0.38	0.00	0.38	0.99	0.353	1.34	0.263	1.00	1.00	2.000	No
95	6.25	0.38	0.00	0.38	0.99	0.353	1.34	0.263	1.00	1.00	2.000	No
96	6.31	0.38	0.00	0.38	0.99	0.353	1.34	0.262	1.00	1.00	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
97	6.39	0.39	0.00	0.39	0.99	0.353	1.34	0.262	1.00	1.00	2.000	No
98	6.45	0.39	0.00	0.39	0.99	0.353	1.34	0.262	1.00	1.00	2.000	No
99	6.51	0.39	0.00	0.39	0.99	0.353	1.34	0.262	1.00	1.00	2.000	No
100	6.58	0.40	0.00	0.40	0.99	0.353	1.34	0.262	1.00	1.00	2.000	No
101	6.66	0.40	0.00	0.40	0.99	0.353	1.34	0.262	1.00	1.00	2.000	No
102	6.70	0.41	0.00	0.41	0.99	0.353	1.34	0.262	1.00	1.00	2.000	No
103	6.78	0.41	0.00	0.41	0.99	0.353	1.34	0.262	1.00	1.00	2.000	No
104	6.85	0.41	0.00	0.41	0.99	0.352	1.34	0.262	1.00	1.00	2.000	No
105	6.89	0.42	0.00	0.42	0.99	0.352	1.34	0.262	1.00	1.00	2.000	No
106	7.00	0.42	0.00	0.42	0.99	0.352	1.34	0.262	1.00	1.00	2.000	No
107	7.03	0.42	0.00	0.42	0.99	0.352	1.34	0.262	1.00	1.00	2.000	No
108	7.10	0.43	0.00	0.43	0.99	0.352	1.34	0.262	1.00	1.00	2.000	No
109	7.19	0.43	0.00	0.43	0.99	0.352	1.34	0.262	1.00	1.00	2.000	No
110	7.25	0.44	0.00	0.44	0.99	0.352	1.34	0.262	1.00	1.00	2.000	No
111	7.30	0.44	0.00	0.44	0.99	0.352	1.34	0.262	1.00	1.00	2.000	No
112	7.37	0.44	0.00	0.44	0.98	0.352	1.34	0.262	1.00	1.00	2.000	No
113	7.44	0.45	0.00	0.45	0.98	0.352	1.34	0.262	1.00	1.00	2.000	No
114	7.49	0.45	0.00	0.45	0.98	0.352	1.34	0.262	1.00	1.00	2.000	No
115	7.56	0.45	0.00	0.45	0.98	0.352	1.34	0.262	1.00	1.00	2.000	No
116	7.64	0.46	0.00	0.46	0.98	0.352	1.34	0.262	1.00	1.00	2.000	No
117	7.68	0.46	0.00	0.46	0.98	0.352	1.34	0.262	1.00	1.00	2.000	No
118	7.79	0.47	0.00	0.47	0.98	0.352	1.34	0.262	1.00	1.00	2.000	No
119	7.83	0.47	0.00	0.47	0.98	0.352	1.34	0.262	1.00	1.00	2.000	No
120	7.90	0.47	0.00	0.47	0.98	0.352	1.34	0.262	1.00	1.00	2.000	No
121	7.98	0.48	0.00	0.48	0.98	0.352	1.34	0.262	1.00	1.00	2.000	No
122	8.02	0.48	0.00	0.48	0.98	0.352	1.34	0.261	1.00	1.00	2.000	No
123	8.09	0.48	0.00	0.48	0.98	0.352	1.34	0.261	1.00	1.00	2.000	No
124	8.15	0.49	0.00	0.49	0.98	0.351	1.34	0.261	1.00	1.00	2.000	No
125	8.23	0.49	0.00	0.49	0.98	0.351	1.34	0.261	1.00	1.00	2.000	No
126	8.29	0.50	0.00	0.50	0.98	0.351	1.34	0.261	1.00	1.00	2.000	No
127	8.34	0.50	0.00	0.50	0.98	0.351	1.34	0.261	1.00	1.00	2.000	No
128	8.41	0.50	0.00	0.50	0.98	0.351	1.34	0.261	1.00	1.00	2.000	No
129	8.48	0.51	0.00	0.51	0.98	0.351	1.34	0.261	1.00	1.00	2.000	No
130	8.55	0.51	0.00	0.51	0.98	0.351	1.34	0.261	1.00	1.00	2.000	No
131	8.60	0.51	0.00	0.51	0.98	0.351	1.34	0.261	1.00	1.00	2.000	No
132	8.66	0.52	0.00	0.52	0.98	0.351	1.34	0.261	1.00	1.00	2.000	No
133	8.74	0.52	0.00	0.52	0.98	0.351	1.34	0.261	1.00	1.00	2.000	No
134	8.83	0.53	0.00	0.53	0.98	0.351	1.34	0.261	1.00	1.00	2.000	No
135	8.90	0.53	0.00	0.53	0.98	0.351	1.34	0.261	1.00	1.00	2.000	No
136	8.94	0.53	0.00	0.53	0.98	0.351	1.34	0.261	1.00	1.00	2.000	No
137	9.01	0.54	0.00	0.54	0.98	0.351	1.34	0.261	1.00	1.00	0.261	No
138	9.09	0.54	0.00	0.54	0.98	0.353	1.34	0.262	1.00	1.00	0.262	No
139	9.15	0.54	0.00	0.54	0.98	0.354	1.34	0.263	1.00	1.00	0.263	No
140	9.20	0.55	0.01	0.54	0.98	0.355	1.34	0.264	1.00	1.00	0.264	No
141	9.29	0.55	0.01	0.54	0.98	0.356	1.34	0.265	1.00	1.00	0.265	No
142	9.35	0.56	0.01	0.54	0.98	0.358	1.34	0.266	1.00	1.00	0.266	No
143	9.39	0.56	0.01	0.55	0.98	0.358	1.34	0.267	1.00	1.00	0.267	No
144	9.45	0.56	0.01	0.55	0.98	0.359	1.34	0.267	1.00	1.00	0.267	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
145	9.55	0.57	0.02	0.55	0.98	0.361	1.34	0.269	1.00	1.00	0.269	No
146	9.64	0.57	0.02	0.55	0.98	0.363	1.34	0.270	1.00	1.00	0.270	No
147	9.65	0.57	0.02	0.55	0.98	0.363	1.34	0.270	1.00	1.00	0.270	No
148	9.73	0.58	0.02	0.55	0.98	0.365	1.34	0.271	1.00	1.00	0.271	No
149	9.79	0.58	0.02	0.56	0.98	0.366	1.34	0.272	1.00	1.00	0.272	No
150	9.84	0.58	0.03	0.56	0.98	0.367	1.34	0.273	1.00	1.00	0.273	No
151	9.91	0.59	0.03	0.56	0.98	0.368	1.34	0.274	1.00	1.00	0.274	No
152	9.99	0.59	0.03	0.56	0.98	0.369	1.34	0.275	1.00	1.00	0.275	No
153	10.08	0.60	0.03	0.56	0.98	0.371	1.34	0.276	1.00	1.00	0.276	No
154	10.14	0.60	0.04	0.57	0.98	0.372	1.34	0.277	1.00	1.00	0.277	No
155	10.19	0.60	0.04	0.57	0.98	0.373	1.34	0.277	1.00	1.00	0.277	No
156	10.25	0.61	0.04	0.57	0.98	0.374	1.34	0.278	1.00	1.00	0.278	No
157	10.34	0.61	0.04	0.57	0.98	0.375	1.34	0.279	1.00	1.00	0.279	No
158	10.38	0.62	0.04	0.57	0.98	0.376	1.34	0.280	1.00	1.00	0.280	No
159	10.44	0.62	0.04	0.57	0.98	0.377	1.34	0.280	1.00	1.00	0.280	No
160	10.52	0.62	0.05	0.58	0.98	0.378	1.34	0.281	1.00	1.00	0.281	No
161	10.59	0.63	0.05	0.58	0.98	0.380	1.34	0.282	1.00	1.00	0.282	No
162	10.63	0.63	0.05	0.58	0.98	0.380	1.34	0.283	1.00	1.00	0.283	No
163	10.70	0.63	0.05	0.58	0.98	0.381	1.34	0.284	1.00	1.00	0.284	No
164	10.78	0.64	0.06	0.58	0.98	0.383	1.34	0.285	1.00	1.00	0.285	No
165	10.87	0.64	0.06	0.59	0.98	0.384	1.34	0.286	1.00	1.00	0.286	No
166	10.93	0.65	0.06	0.59	0.98	0.385	1.34	0.286	1.00	1.00	0.286	No
167	10.97	0.65	0.06	0.59	0.98	0.386	1.34	0.287	1.00	1.00	0.287	No
168	11.03	0.65	0.06	0.59	0.98	0.387	1.34	0.288	1.00	1.00	0.288	No
169	11.12	0.66	0.07	0.59	0.98	0.388	1.34	0.289	1.00	1.00	0.289	No
170	11.16	0.66	0.07	0.59	0.98	0.389	1.34	0.289	1.00	1.00	0.289	No
171	11.23	0.66	0.07	0.60	0.98	0.390	1.34	0.290	1.00	1.00	0.290	No
172	11.31	0.67	0.07	0.60	0.98	0.391	1.34	0.291	1.00	1.00	0.291	No
173	11.37	0.67	0.07	0.60	0.98	0.392	1.34	0.292	1.00	1.00	0.292	No
174	11.44	0.68	0.08	0.60	0.98	0.393	1.34	0.292	1.00	1.00	0.292	No
175	11.51	0.68	0.08	0.60	0.98	0.394	1.34	0.293	1.00	1.00	0.293	No
176	11.56	0.68	0.08	0.60	0.98	0.395	1.34	0.294	1.00	1.00	0.294	No
177	11.63	0.69	0.08	0.61	0.98	0.396	1.34	0.295	1.00	1.00	0.295	No
178	11.71	0.69	0.08	0.61	0.98	0.397	1.34	0.295	1.00	1.00	0.295	No
179	11.76	0.70	0.09	0.61	0.98	0.398	1.34	0.296	1.00	1.00	0.296	No
180	11.83	0.70	0.09	0.61	0.98	0.399	1.34	0.297	1.00	1.00	0.297	No
181	11.91	0.70	0.09	0.61	0.98	0.400	1.34	0.298	1.00	1.00	0.298	No
182	11.94	0.71	0.09	0.61	0.98	0.401	1.34	0.298	1.00	1.00	0.298	No
183	12.05	0.71	0.10	0.62	0.97	0.402	1.34	0.299	1.00	1.00	0.299	No
184	12.10	0.72	0.10	0.62	0.97	0.403	1.34	0.300	1.00	1.00	0.300	No
185	12.14	0.72	0.10	0.62	0.97	0.403	1.34	0.300	1.00	1.00	0.300	No
186	12.25	0.73	0.10	0.62	0.97	0.405	1.34	0.301	1.00	1.00	0.301	No
187	12.29	0.73	0.10	0.62	0.97	0.406	1.34	0.302	1.00	1.00	0.302	No
188	12.35	0.73	0.10	0.63	0.97	0.406	1.34	0.302	1.00	1.00	0.302	No
189	12.44	0.74	0.11	0.63	0.97	0.408	1.34	0.303	1.00	1.00	0.303	No
190	12.49	0.74	0.11	0.63	0.97	0.408	1.34	0.304	1.00	1.00	0.304	No
191	12.55	0.74	0.11	0.63	0.97	0.409	1.34	0.304	1.00	1.00	0.304	No
192	12.61	0.75	0.11	0.63	0.97	0.410	1.34	0.305	1.00	1.00	0.305	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
193	12.70	0.75	0.12	0.64	0.97	0.411	1.34	0.306	1.00	1.00	0.306	No
194	12.75	0.75	0.12	0.64	0.97	0.412	1.34	0.306	1.00	1.00	0.306	No
195	12.81	0.76	0.12	0.64	0.97	0.413	1.34	0.307	1.00	1.00	0.307	No
196	12.89	0.76	0.12	0.64	0.97	0.414	1.34	0.308	1.00	1.00	0.308	No
197	12.94	0.77	0.12	0.64	0.97	0.414	1.34	0.308	1.00	1.00	0.308	No
198	12.99	0.77	0.12	0.64	0.97	0.415	1.34	0.309	1.00	1.00	0.309	No
199	13.08	0.77	0.13	0.65	0.97	0.416	1.34	0.310	1.00	1.00	0.310	No
200	13.15	0.78	0.13	0.65	0.97	0.417	1.34	0.310	1.00	1.00	0.310	No
201	13.20	0.78	0.13	0.65	0.97	0.418	1.34	0.311	1.00	1.00	0.311	No
202	13.27	0.78	0.13	0.65	0.97	0.419	1.34	0.311	1.00	1.00	0.311	No
203	13.32	0.79	0.13	0.65	0.97	0.419	1.34	0.312	1.00	1.00	0.312	No
204	13.39	0.79	0.14	0.65	0.97	0.420	1.34	0.313	1.00	1.00	0.313	No
205	13.48	0.80	0.14	0.66	0.97	0.421	1.34	0.313	1.00	1.00	0.313	No
206	13.54	0.80	0.14	0.66	0.97	0.422	1.34	0.314	1.00	1.00	0.314	No
207	13.59	0.80	0.14	0.66	0.97	0.423	1.34	0.314	1.00	1.00	0.314	No
208	13.65	0.81	0.15	0.66	0.97	0.424	1.34	0.315	1.00	1.00	0.315	No
209	13.74	0.81	0.15	0.66	0.97	0.425	1.34	0.316	1.00	1.00	0.316	No
210	13.80	0.81	0.15	0.66	0.97	0.425	1.34	0.316	1.00	1.00	0.316	No
211	13.89	0.82	0.15	0.67	0.97	0.427	1.34	0.317	1.00	1.00	0.317	No
212	13.93	0.82	0.15	0.67	0.97	0.427	1.34	0.318	1.00	1.00	0.318	No
213	13.99	0.82	0.16	0.67	0.97	0.428	1.34	0.318	1.00	1.00	0.318	No
214	14.07	0.83	0.16	0.67	0.97	0.429	1.34	0.319	1.00	1.00	0.319	No
215	14.12	0.83	0.16	0.67	0.97	0.429	1.34	0.319	1.00	1.00	0.319	No
216	14.18	0.83	0.16	0.67	0.97	0.430	1.34	0.320	1.00	1.00	0.320	No
217	14.26	0.84	0.16	0.67	0.97	0.431	1.34	0.321	1.00	1.00	0.321	No
218	14.34	0.84	0.17	0.68	0.97	0.432	1.34	0.321	1.00	1.00	0.321	No
219	14.38	0.85	0.17	0.68	0.97	0.433	1.34	0.322	1.00	1.00	0.322	No
220	14.47	0.85	0.17	0.68	0.97	0.434	1.34	0.323	1.00	1.00	0.323	No
221	14.53	0.85	0.17	0.68	0.97	0.434	1.34	0.323	1.00	1.00	0.323	No
222	14.57	0.86	0.17	0.68	0.97	0.435	1.34	0.323	1.00	1.00	0.323	No
223	14.64	0.86	0.18	0.68	0.97	0.436	1.34	0.324	1.00	1.00	0.324	No
224	14.72	0.86	0.18	0.69	0.97	0.437	1.34	0.325	1.00	1.00	0.325	No
225	14.80	0.87	0.18	0.69	0.97	0.438	1.34	0.325	1.00	1.00	0.325	No
226	14.83	0.87	0.18	0.69	0.97	0.438	1.34	0.326	1.00	1.00	0.326	No
227	14.92	0.88	0.18	0.69	0.97	0.439	1.34	0.326	1.00	1.00	0.326	No
228	14.97	0.88	0.19	0.69	0.97	0.439	1.34	0.327	1.00	1.00	0.327	No
229	15.06	0.88	0.19	0.69	0.97	0.440	1.34	0.328	1.00	1.00	0.328	No
230	15.10	0.89	0.19	0.70	0.97	0.441	1.34	0.328	1.00	1.00	0.328	No
231	15.17	0.89	0.19	0.70	0.97	0.442	1.34	0.328	1.00	1.00	0.328	No
232	15.25	0.89	0.20	0.70	0.97	0.443	1.34	0.329	1.00	1.00	0.329	No
233	15.31	0.90	0.20	0.70	0.97	0.443	1.34	0.330	1.00	1.00	0.330	No
234	15.37	0.90	0.20	0.70	0.97	0.444	1.34	0.330	1.00	1.00	0.330	No
235	15.44	0.91	0.20	0.70	0.97	0.445	1.34	0.331	1.00	1.00	0.331	No
236	15.51	0.91	0.20	0.71	0.97	0.445	1.34	0.331	1.00	1.00	0.331	No
237	15.56	0.91	0.20	0.71	0.97	0.446	1.34	0.332	1.00	1.00	0.332	No
238	15.63	0.92	0.21	0.71	0.97	0.447	1.34	0.332	1.00	1.00	0.332	No
239	15.71	0.92	0.21	0.71	0.97	0.447	1.34	0.333	1.00	1.00	0.333	No
240	15.76	0.92	0.21	0.71	0.97	0.448	1.34	0.333	1.00	1.00	0.333	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
241	15.82	0.93	0.21	0.72	0.97	0.448	1.34	0.334	1.00	1.00	0.334	No
242	15.90	0.93	0.22	0.72	0.97	0.449	1.34	0.334	1.00	1.00	0.334	No
243	15.95	0.94	0.22	0.72	0.97	0.450	1.34	0.334	1.00	1.00	0.334	No
244	16.01	0.94	0.22	0.72	0.97	0.450	1.34	0.335	1.00	1.00	0.335	No
245	16.10	0.95	0.22	0.72	0.97	0.451	1.34	0.336	1.00	1.00	2.000	Yes
246	16.16	0.95	0.22	0.73	0.97	0.452	1.34	0.336	1.00	1.00	2.000	Yes
247	16.21	0.95	0.22	0.73	0.97	0.452	1.34	0.336	1.00	1.00	2.000	Yes
248	16.29	0.96	0.23	0.73	0.97	0.453	1.34	0.337	1.00	1.00	2.000	Yes
249	16.36	0.96	0.23	0.73	0.97	0.454	1.34	0.337	1.00	1.00	2.000	Yes
250	16.41	0.96	0.23	0.73	0.97	0.454	1.34	0.338	1.00	1.00	2.000	Yes
251	16.49	0.97	0.23	0.74	0.97	0.455	1.34	0.338	1.00	1.00	0.338	No
252	16.55	0.97	0.24	0.74	0.97	0.455	1.34	0.339	1.00	1.00	0.339	No
253	16.60	0.98	0.24	0.74	0.97	0.456	1.34	0.339	1.00	1.00	0.339	No
254	16.70	0.98	0.24	0.74	0.96	0.457	1.34	0.340	1.00	1.00	2.000	Yes
255	16.74	0.99	0.24	0.74	0.96	0.457	1.34	0.340	1.00	1.00	2.000	Yes
256	16.80	0.99	0.24	0.75	0.96	0.457	1.34	0.340	1.00	1.00	2.000	Yes
257	16.89	0.99	0.25	0.75	0.96	0.458	1.34	0.341	1.00	1.00	2.000	Yes
258	16.93	1.00	0.25	0.75	0.96	0.459	1.34	0.341	1.00	1.00	2.000	Yes
259	17.00	1.00	0.25	0.75	0.96	0.459	1.34	0.341	1.00	1.00	2.000	Yes
260	17.09	1.01	0.25	0.75	0.96	0.460	1.34	0.342	1.00	1.00	2.000	Yes
261	17.14	1.01	0.25	0.76	0.96	0.460	1.34	0.342	1.00	1.00	2.000	Yes
262	17.20	1.01	0.26	0.76	0.96	0.461	1.34	0.343	1.00	1.00	0.343	No
263	17.28	1.02	0.26	0.76	0.96	0.462	1.34	0.343	1.00	1.00	0.343	No
264	17.34	1.02	0.26	0.76	0.96	0.462	1.34	0.344	1.00	1.00	0.344	No
265	17.41	1.03	0.26	0.76	0.96	0.463	1.34	0.344	1.00	1.00	0.344	No
266	17.48	1.03	0.26	0.76	0.96	0.463	1.34	0.345	1.00	1.00	0.345	No
267	17.56	1.03	0.27	0.77	0.96	0.464	1.34	0.345	1.00	1.00	0.345	No
268	17.62	1.04	0.27	0.77	0.96	0.465	1.34	0.346	1.00	1.00	0.346	No
269	17.67	1.04	0.27	0.77	0.96	0.465	1.34	0.346	1.00	1.00	2.000	Yes
270	17.72	1.04	0.27	0.77	0.96	0.465	1.34	0.346	1.00	1.00	2.000	Yes
271	17.78	1.05	0.27	0.77	0.96	0.466	1.34	0.347	1.00	1.00	2.000	Yes
272	17.87	1.05	0.28	0.78	0.96	0.467	1.34	0.347	1.00	1.00	2.000	Yes
273	17.94	1.06	0.28	0.78	0.96	0.467	1.34	0.348	1.00	1.00	2.000	Yes
274	18.01	1.06	0.28	0.78	0.96	0.468	1.34	0.348	1.00	1.00	2.000	Yes
275	18.06	1.06	0.28	0.78	0.96	0.468	1.34	0.348	1.00	1.00	2.000	Yes
276	18.12	1.07	0.28	0.78	0.96	0.469	1.34	0.349	1.00	1.00	2.000	Yes
277	18.21	1.07	0.29	0.79	0.96	0.469	1.34	0.349	1.00	1.00	0.349	No
278	18.25	1.08	0.29	0.79	0.96	0.470	1.34	0.349	1.00	1.00	0.349	No
279	18.31	1.08	0.29	0.79	0.96	0.470	1.34	0.350	1.00	1.00	0.350	No
280	18.40	1.08	0.29	0.79	0.96	0.471	1.34	0.350	1.00	1.00	2.000	Yes
281	18.44	1.09	0.29	0.79	0.96	0.471	1.34	0.350	1.00	1.00	2.000	Yes
282	18.51	1.09	0.30	0.79	0.96	0.472	1.34	0.351	1.00	1.00	2.000	Yes
283	18.58	1.10	0.30	0.80	0.96	0.472	1.34	0.351	1.00	1.00	2.000	Yes
284	18.64	1.10	0.30	0.80	0.96	0.473	1.34	0.352	1.00	1.00	2.000	Yes
285	18.71	1.10	0.30	0.80	0.96	0.473	1.34	0.352	1.00	1.00	2.000	Yes
286	18.80	1.11	0.31	0.80	0.96	0.474	1.34	0.352	1.00	1.00	2.000	Yes
287	18.86	1.11	0.31	0.80	0.96	0.474	1.34	0.353	1.00	1.00	2.000	Yes
288	18.91	1.12	0.31	0.81	0.96	0.475	1.34	0.353	1.00	1.00	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
289	18.98	1.12	0.31	0.81	0.96	0.475	1.34	0.353	1.00	1.00	2.000	Yes
290	19.05	1.12	0.31	0.81	0.96	0.476	1.34	0.354	1.00	1.00	2.000	Yes
291	19.10	1.13	0.32	0.81	0.96	0.476	1.34	0.354	1.00	1.00	2.000	Yes
292	19.20	1.13	0.32	0.81	0.96	0.477	1.34	0.355	1.00	1.00	2.000	Yes
293	19.23	1.13	0.32	0.82	0.96	0.477	1.34	0.355	1.00	1.00	2.000	Yes
294	19.30	1.14	0.32	0.82	0.96	0.477	1.34	0.355	1.00	1.00	2.000	Yes
295	19.39	1.14	0.32	0.82	0.96	0.478	1.34	0.356	1.00	1.00	2.000	Yes
296	19.43	1.15	0.33	0.82	0.96	0.478	1.34	0.356	1.00	1.00	2.000	Yes
297	19.50	1.15	0.33	0.82	0.96	0.479	1.34	0.356	1.00	1.00	2.000	Yes
298	19.57	1.16	0.33	0.83	0.96	0.479	1.34	0.356	1.00	1.00	2.000	Yes
299	19.63	1.16	0.33	0.83	0.96	0.480	1.34	0.357	1.00	1.00	2.000	Yes
300	19.70	1.16	0.33	0.83	0.96	0.480	1.34	0.357	1.00	1.00	0.357	No
301	19.77	1.17	0.34	0.83	0.96	0.480	1.34	0.357	1.00	1.00	0.357	No
302	19.84	1.17	0.34	0.83	0.96	0.481	1.34	0.358	1.00	1.00	0.358	No
303	19.90	1.18	0.34	0.84	0.96	0.481	1.34	0.358	1.00	1.00	0.358	No
304	19.99	1.18	0.34	0.84	0.96	0.482	1.34	0.358	1.00	1.00	2.000	Yes
305	20.02	1.18	0.34	0.84	0.96	0.482	1.34	0.358	1.00	1.00	2.000	Yes
306	20.09	1.19	0.35	0.84	0.96	0.482	1.34	0.359	1.00	1.00	2.000	Yes
307	20.19	1.20	0.35	0.85	0.96	0.483	1.34	0.359	1.00	1.00	2.000	Yes
308	20.21	1.20	0.35	0.85	0.96	0.483	1.34	0.359	1.00	1.00	2.000	Yes
309	20.29	1.20	0.35	0.85	0.96	0.484	1.34	0.360	1.00	1.00	2.000	Yes
310	20.38	1.21	0.36	0.85	0.96	0.484	1.34	0.360	1.00	1.00	2.000	Yes
311	20.42	1.21	0.36	0.85	0.96	0.484	1.34	0.360	1.00	1.00	2.000	Yes
312	20.52	1.22	0.36	0.86	0.96	0.485	1.34	0.361	1.00	1.00	0.361	No
313	20.55	1.22	0.36	0.86	0.96	0.485	1.34	0.361	1.00	1.00	0.361	No
314	20.62	1.22	0.36	0.86	0.96	0.486	1.34	0.361	1.00	1.00	2.000	Yes
315	20.68	1.23	0.36	0.86	0.96	0.486	1.34	0.361	1.00	1.00	2.000	Yes
316	20.75	1.23	0.37	0.86	0.95	0.486	1.34	0.362	1.00	1.00	2.000	Yes
317	20.81	1.23	0.37	0.87	0.95	0.487	1.34	0.362	1.00	1.00	2.000	Yes
318	20.90	1.24	0.37	0.87	0.95	0.487	1.34	0.362	1.00	1.00	2.000	Yes
319	20.96	1.24	0.37	0.87	0.95	0.487	1.34	0.363	1.00	1.00	2.000	Yes
320	21.01	1.25	0.37	0.87	0.95	0.488	1.34	0.363	1.00	1.00	2.000	Yes
321	21.09	1.25	0.38	0.87	0.95	0.488	1.34	0.363	1.00	1.00	2.000	Yes
322	21.15	1.26	0.38	0.88	0.95	0.488	1.34	0.363	1.00	1.00	2.000	Yes
323	21.21	1.26	0.38	0.88	0.95	0.489	1.34	0.363	1.00	1.00	2.000	Yes
324	21.30	1.27	0.38	0.88	0.95	0.489	1.34	0.364	1.00	1.00	0.364	No
325	21.36	1.27	0.39	0.88	0.95	0.489	1.34	0.364	1.00	1.00	0.364	No
326	21.40	1.27	0.39	0.89	0.95	0.490	1.34	0.364	1.00	1.00	0.364	No
327	21.49	1.28	0.39	0.89	0.95	0.490	1.34	0.365	1.00	1.00	0.365	No
328	21.56	1.28	0.39	0.89	0.95	0.490	1.34	0.365	1.00	1.00	2.000	Yes
329	21.60	1.28	0.39	0.89	0.95	0.491	1.34	0.365	1.00	1.00	2.000	Yes
330	21.66	1.29	0.39	0.89	0.95	0.491	1.34	0.365	1.00	1.00	2.000	Yes
331	21.75	1.29	0.40	0.90	0.95	0.491	1.34	0.365	1.00	1.00	2.000	Yes
332	21.80	1.30	0.40	0.90	0.95	0.492	1.34	0.366	1.00	1.00	2.000	Yes
333	21.85	1.30	0.40	0.90	0.95	0.492	1.34	0.366	1.00	1.00	2.000	Yes
334	21.95	1.31	0.40	0.90	0.95	0.492	1.34	0.366	1.00	1.00	2.000	Yes
335	21.99	1.31	0.41	0.90	0.95	0.492	1.34	0.366	1.00	1.00	2.000	Yes
336	22.05	1.31	0.41	0.91	0.95	0.493	1.34	0.367	1.00	1.00	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
337	22.14	1.32	0.41	0.91	0.95	0.493	1.34	0.367	1.00	1.00	0.367	No
338	22.19	1.32	0.41	0.91	0.95	0.493	1.34	0.367	1.00	1.00	0.367	No
339	22.26	1.33	0.41	0.91	0.95	0.494	1.34	0.367	1.00	1.00	0.367	No
340	22.35	1.33	0.42	0.92	0.95	0.494	1.34	0.368	1.00	1.00	0.368	No
341	22.44	1.34	0.42	0.92	0.95	0.495	1.34	0.368	1.00	1.00	0.368	No
342	22.45	1.34	0.42	0.92	0.95	0.495	1.34	0.368	1.00	1.00	0.368	No
343	22.54	1.34	0.42	0.92	0.95	0.495	1.34	0.368	1.00	1.00	0.368	No
344	22.58	1.35	0.42	0.92	0.95	0.495	1.34	0.368	1.00	1.00	0.368	No
345	22.65	1.35	0.43	0.93	0.95	0.496	1.34	0.369	1.00	1.00	0.369	No
346	22.73	1.36	0.43	0.93	0.95	0.496	1.34	0.369	1.00	1.00	0.369	No
347	22.79	1.36	0.43	0.93	0.95	0.496	1.34	0.369	1.00	1.00	0.369	No
348	22.85	1.36	0.43	0.93	0.95	0.497	1.34	0.369	1.00	1.00	0.369	No
349	22.93	1.37	0.43	0.93	0.95	0.497	1.34	0.370	1.00	1.00	0.370	No
350	22.99	1.37	0.44	0.94	0.95	0.497	1.34	0.370	1.00	1.00	0.370	No
351	23.04	1.38	0.44	0.94	0.95	0.497	1.34	0.370	1.00	1.00	0.370	No
352	23.12	1.38	0.44	0.94	0.95	0.498	1.34	0.370	1.00	1.00	0.370	No
353	23.19	1.39	0.44	0.94	0.95	0.498	1.34	0.370	1.00	1.00	0.370	No
354	23.27	1.39	0.45	0.94	0.95	0.498	1.34	0.371	1.00	1.00	0.371	No
355	23.30	1.39	0.45	0.95	0.95	0.499	1.34	0.371	1.00	1.00	0.371	No
356	23.38	1.40	0.45	0.95	0.95	0.499	1.34	0.371	1.00	1.00	0.371	No
357	23.47	1.40	0.45	0.95	0.95	0.499	1.34	0.371	1.00	1.00	0.371	No
358	23.50	1.40	0.45	0.95	0.95	0.499	1.34	0.371	1.00	1.00	0.371	No
359	23.58	1.41	0.45	0.96	0.95	0.500	1.34	0.372	1.00	1.00	0.372	No
360	23.66	1.42	0.46	0.96	0.95	0.500	1.34	0.372	1.00	1.00	0.372	No
361	23.69	1.42	0.46	0.96	0.95	0.500	1.34	0.372	1.00	1.00	0.372	No
362	23.77	1.42	0.46	0.96	0.95	0.500	1.34	0.372	1.00	1.00	0.372	No
363	23.84	1.43	0.46	0.96	0.95	0.501	1.34	0.372	1.00	1.00	0.372	No
364	23.92	1.43	0.47	0.97	0.95	0.501	1.34	0.373	1.00	1.00	0.373	No
365	23.97	1.43	0.47	0.97	0.95	0.501	1.34	0.373	1.00	1.00	0.373	No
366	24.06	1.44	0.47	0.97	0.95	0.501	1.34	0.373	1.00	1.00	0.373	No
367	24.12	1.44	0.47	0.97	0.94	0.502	1.34	0.373	1.00	1.00	0.373	No
368	24.17	1.45	0.47	0.97	0.94	0.502	1.34	0.373	1.00	1.00	0.373	No
369	24.23	1.45	0.48	0.98	0.94	0.502	1.34	0.373	1.00	1.00	0.373	No
370	24.31	1.46	0.48	0.98	0.94	0.502	1.34	0.374	1.00	1.00	0.374	No
371	24.36	1.46	0.48	0.98	0.94	0.502	1.34	0.374	1.00	1.00	0.374	No
372	24.42	1.46	0.48	0.98	0.94	0.503	1.34	0.374	1.00	1.00	0.374	No
373	24.51	1.47	0.48	0.99	0.94	0.503	1.34	0.374	1.00	1.00	0.374	No
374	24.54	1.47	0.48	0.99	0.94	0.503	1.34	0.374	1.00	1.00	0.374	No
375	24.62	1.48	0.49	0.99	0.94	0.503	1.34	0.374	1.00	1.00	0.374	No
376	24.71	1.48	0.49	0.99	0.94	0.504	1.34	0.375	1.00	1.00	0.375	No
377	24.74	1.48	0.49	0.99	0.94	0.504	1.34	0.375	1.00	1.00	0.375	No
378	24.81	1.49	0.49	0.99	0.94	0.504	1.34	0.375	1.00	1.00	0.375	No
379	24.89	1.49	0.50	1.00	0.94	0.504	1.34	0.375	1.00	1.00	0.375	No
380	24.96	1.50	0.50	1.00	0.94	0.505	1.34	0.375	1.00	1.00	0.375	No
381	25.01	1.50	0.50	1.00	0.94	0.505	1.34	0.376	1.00	1.00	0.376	No
382	25.10	1.50	0.50	1.00	0.94	0.505	1.34	0.376	1.00	1.00	0.376	No
383	25.14	1.51	0.50	1.00	0.94	0.505	1.34	0.376	1.00	1.00	0.376	No
384	25.21	1.51	0.51	1.01	0.94	0.506	1.34	0.376	1.00	1.00	0.376	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
385	25.30	1.52	0.51	1.01	0.94	0.506	1.34	0.376	1.00	1.00	0.376	No
386	25.34	1.52	0.51	1.01	0.94	0.506	1.34	0.376	1.00	1.00	0.376	No
387	25.41	1.52	0.51	1.01	0.94	0.507	1.34	0.377	1.00	1.00	0.377	No
388	25.50	1.53	0.51	1.01	0.94	0.507	1.34	0.377	1.00	1.00	0.377	No
389	25.55	1.53	0.52	1.01	0.94	0.507	1.34	0.377	1.00	1.00	0.377	No
390	25.60	1.53	0.52	1.02	0.94	0.507	1.34	0.377	1.00	1.00	0.377	No
391	25.70	1.54	0.52	1.02	0.94	0.508	1.34	0.378	1.00	1.00	0.378	No
392	25.75	1.54	0.52	1.02	0.94	0.508	1.34	0.378	1.00	1.00	0.378	No
393	25.80	1.54	0.52	1.02	0.94	0.508	1.34	0.378	1.00	1.00	0.378	No
394	25.89	1.55	0.53	1.02	0.94	0.508	1.34	0.378	1.00	1.00	0.378	No
395	25.95	1.55	0.53	1.02	0.94	0.509	1.34	0.378	1.00	1.00	0.378	No
396	25.99	1.56	0.53	1.03	0.94	0.509	1.34	0.378	1.00	1.00	0.378	No
397	26.06	1.56	0.53	1.03	0.94	0.509	1.34	0.379	1.00	1.00	0.379	No
398	26.15	1.56	0.54	1.03	0.94	0.509	1.34	0.379	1.00	1.00	0.379	No
399	26.19	1.57	0.54	1.03	0.94	0.510	1.34	0.379	1.00	1.00	0.379	No
400	26.25	1.57	0.54	1.03	0.94	0.510	1.34	0.379	1.00	1.00	0.379	No
401	26.34	1.58	0.54	1.03	0.94	0.510	1.34	0.379	1.00	1.00	0.379	No
402	26.38	1.58	0.54	1.04	0.94	0.510	1.34	0.380	1.00	1.00	0.380	No
403	26.45	1.58	0.54	1.04	0.94	0.511	1.34	0.380	1.00	1.00	0.380	No
404	26.52	1.59	0.55	1.04	0.94	0.511	1.34	0.380	1.00	1.00	0.380	No
405	26.61	1.59	0.55	1.04	0.94	0.511	1.34	0.380	1.00	1.00	0.380	No
406	26.67	1.59	0.55	1.04	0.94	0.511	1.34	0.380	1.00	1.00	0.380	No
407	26.72	1.60	0.55	1.04	0.94	0.511	1.34	0.380	1.00	1.00	0.380	No
408	26.82	1.60	0.56	1.05	0.93	0.512	1.34	0.381	1.00	1.00	0.381	No
409	26.86	1.60	0.56	1.05	0.93	0.512	1.34	0.381	1.00	1.00	0.381	No
410	26.94	1.61	0.56	1.05	0.93	0.512	1.34	0.381	1.00	1.00	0.381	No
411	26.98	1.61	0.56	1.05	0.93	0.512	1.34	0.381	1.00	1.00	0.381	No
412	27.06	1.62	0.56	1.05	0.93	0.513	1.34	0.381	1.00	1.00	0.381	No
413	27.10	1.62	0.56	1.05	0.93	0.513	1.34	0.381	1.00	1.00	0.381	No
414	27.17	1.62	0.57	1.06	0.93	0.513	1.34	0.382	1.00	1.00	0.382	No
415	27.26	1.63	0.57	1.06	0.93	0.513	1.34	0.382	1.00	1.00	0.382	No
416	27.31	1.63	0.57	1.06	0.93	0.514	1.34	0.382	1.00	1.00	0.382	No
417	27.39	1.63	0.57	1.06	0.93	0.514	1.34	0.382	1.00	1.00	0.382	No
418	27.44	1.64	0.58	1.06	0.93	0.514	1.34	0.382	1.00	1.00	0.383	No
419	27.51	1.64	0.58	1.06	0.93	0.514	1.34	0.382	1.00	1.00	0.383	No
420	27.58	1.64	0.58	1.07	0.93	0.514	1.34	0.383	1.00	1.00	0.383	No
421	27.63	1.65	0.58	1.07	0.93	0.515	1.34	0.383	1.00	1.00	0.383	No
422	27.71	1.65	0.58	1.07	0.93	0.515	1.34	0.383	1.00	1.00	0.384	No
423	27.79	1.66	0.59	1.07	0.93	0.515	1.34	0.383	1.00	1.00	0.384	No
424	27.86	1.66	0.59	1.07	0.93	0.515	1.34	0.383	1.00	1.00	0.384	No
425	27.89	1.66	0.59	1.07	0.93	0.515	1.34	0.383	1.00	1.00	0.385	No
426	27.96	1.67	0.59	1.07	0.93	0.516	1.34	0.383	1.00	1.00	0.385	No
427	28.05	1.67	0.59	1.08	0.93	0.516	1.34	0.384	1.00	1.00	0.385	No
428	28.09	1.67	0.60	1.08	0.93	0.516	1.34	0.384	1.00	1.00	0.385	No
429	28.16	1.68	0.60	1.08	0.93	0.516	1.34	0.384	1.00	1.00	0.386	No
430	28.23	1.68	0.60	1.08	0.93	0.516	1.34	0.384	1.00	1.00	0.386	No
431	28.29	1.68	0.60	1.08	0.93	0.517	1.34	0.384	0.99	1.00	0.386	No
432	28.35	1.69	0.60	1.08	0.93	0.517	1.34	0.384	0.99	1.00	0.386	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
433	28.44	1.69	0.61	1.09	0.93	0.517	1.34	0.385	0.99	1.00	0.387	No
434	28.50	1.70	0.61	1.09	0.93	0.517	1.34	0.385	0.99	1.00	0.387	No
435	28.55	1.70	0.61	1.09	0.93	0.517	1.34	0.385	0.99	1.00	0.387	No
436	28.64	1.70	0.61	1.09	0.93	0.518	1.34	0.385	0.99	1.00	0.388	No
437	28.69	1.71	0.61	1.09	0.93	0.518	1.34	0.385	0.99	1.00	0.388	No
438	28.75	1.71	0.62	1.09	0.93	0.518	1.34	0.385	0.99	1.00	0.388	No
439	28.82	1.71	0.62	1.10	0.93	0.518	1.34	0.385	0.99	1.00	0.388	No
440	28.89	1.72	0.62	1.10	0.93	0.518	1.34	0.385	0.99	1.00	0.389	No
441	28.98	1.72	0.62	1.10	0.93	0.518	1.34	0.386	0.99	1.00	0.389	No
442	29.04	1.73	0.63	1.10	0.93	0.518	1.34	0.386	0.99	1.00	0.389	No
443	29.08	1.73	0.63	1.10	0.93	0.519	1.34	0.386	0.99	1.00	0.389	No
444	29.15	1.73	0.63	1.10	0.92	0.519	1.34	0.386	0.99	1.00	0.390	No
445	29.24	1.74	0.63	1.11	0.92	0.519	1.34	0.386	0.99	1.00	0.390	No
446	29.29	1.74	0.63	1.11	0.92	0.519	1.34	0.386	0.99	1.00	0.390	No
447	29.34	1.74	0.63	1.11	0.92	0.519	1.34	0.386	0.99	1.00	0.390	No
448	29.43	1.75	0.64	1.11	0.92	0.519	1.34	0.386	0.99	1.00	0.391	No
449	29.47	1.75	0.64	1.11	0.92	0.519	1.34	0.386	0.99	1.00	0.391	No
450	29.53	1.76	0.64	1.12	0.92	0.519	1.34	0.386	0.99	1.00	0.391	No
451	29.62	1.76	0.64	1.12	0.92	0.520	1.34	0.386	0.99	1.00	0.391	No
452	29.66	1.76	0.64	1.12	0.92	0.520	1.34	0.387	0.99	1.00	0.392	No
453	29.77	1.77	0.65	1.12	0.92	0.520	1.34	0.387	0.99	1.00	0.392	No
454	29.81	1.77	0.65	1.12	0.92	0.520	1.34	0.387	0.99	1.00	0.392	No
455	29.86	1.77	0.65	1.12	0.92	0.520	1.34	0.387	0.99	1.00	0.392	No
456	29.92	1.78	0.65	1.13	0.92	0.520	1.34	0.387	0.99	1.00	0.392	No
457	30.01	1.78	0.66	1.13	0.92	0.520	1.34	0.387	0.99	1.00	0.393	No
458	30.09	1.79	0.66	1.13	0.92	0.520	1.34	0.387	0.98	1.00	0.393	No
459	30.17	1.79	0.66	1.13	0.92	0.521	1.34	0.387	0.98	1.00	0.393	No
460	30.20	1.79	0.66	1.13	0.92	0.521	1.34	0.387	0.98	1.00	0.393	No
461	30.27	1.80	0.66	1.14	0.92	0.521	1.34	0.387	0.98	1.00	0.394	No
462	30.32	1.80	0.67	1.14	0.92	0.521	1.34	0.387	0.98	1.00	0.394	No
463	30.39	1.81	0.67	1.14	0.92	0.521	1.34	0.387	0.98	1.00	0.394	No
464	30.47	1.81	0.67	1.14	0.92	0.521	1.34	0.387	0.98	1.00	0.394	No
465	30.55	1.82	0.67	1.14	0.92	0.521	1.34	0.388	0.98	1.00	0.394	No
466	30.62	1.82	0.67	1.15	0.92	0.521	1.34	0.388	0.98	1.00	0.395	No
467	30.66	1.82	0.68	1.15	0.92	0.521	1.34	0.388	0.98	1.00	0.395	No
468	30.72	1.83	0.68	1.15	0.92	0.521	1.34	0.388	0.98	1.00	0.395	No
469	30.81	1.83	0.68	1.15	0.92	0.521	1.34	0.388	0.98	1.00	0.395	No
470	30.85	1.83	0.68	1.15	0.92	0.521	1.34	0.388	0.98	1.00	0.395	No
471	30.91	1.84	0.68	1.15	0.92	0.521	1.34	0.388	0.98	1.00	0.396	No
472	31.01	1.84	0.69	1.16	0.92	0.522	1.34	0.388	0.98	1.00	0.396	No
473	31.05	1.85	0.69	1.16	0.92	0.522	1.34	0.388	0.98	1.00	0.396	No
474	31.11	1.85	0.69	1.16	0.91	0.522	1.34	0.388	0.98	1.00	0.396	No
475	31.20	1.85	0.69	1.16	0.91	0.522	1.34	0.388	0.98	1.00	0.396	No
476	31.26	1.86	0.69	1.16	0.91	0.522	1.34	0.388	0.98	1.00	0.397	No
477	31.31	1.86	0.70	1.16	0.91	0.522	1.34	0.388	0.98	1.00	0.397	No
478	31.38	1.86	0.70	1.17	0.91	0.522	1.34	0.388	0.98	1.00	0.397	No
479	31.46	1.87	0.70	1.17	0.91	0.522	1.34	0.388	0.98	1.00	0.397	No
480	31.51	1.87	0.70	1.17	0.91	0.522	1.34	0.388	0.98	1.00	0.397	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
481	31.60	1.88	0.71	1.17	0.91	0.522	1.34	0.388	0.98	1.00	0.398	No
482	31.65	1.88	0.71	1.17	0.91	0.522	1.34	0.388	0.98	1.00	0.398	No
483	31.74	1.88	0.71	1.18	0.91	0.522	1.34	0.389	0.98	1.00	0.398	No
484	31.80	1.89	0.71	1.18	0.91	0.523	1.34	0.389	0.98	1.00	0.398	No
485	31.85	1.89	0.71	1.18	0.91	0.523	1.34	0.389	0.98	1.00	0.398	No
486	31.89	1.89	0.71	1.18	0.91	0.523	1.34	0.389	0.98	1.00	0.398	No
487	32.00	1.90	0.72	1.18	0.91	0.523	1.34	0.389	0.97	1.00	0.399	No
488	32.04	1.90	0.72	1.18	0.91	0.523	1.34	0.389	0.97	1.00	0.399	No
489	32.09	1.90	0.72	1.18	0.91	0.523	1.34	0.389	0.97	1.00	0.399	No
490	32.19	1.91	0.72	1.19	0.91	0.523	1.34	0.389	0.97	1.00	0.399	No
491	32.23	1.91	0.72	1.19	0.91	0.523	1.34	0.389	0.97	1.00	0.399	No
492	32.29	1.91	0.73	1.19	0.91	0.523	1.34	0.389	0.97	1.00	0.400	No
493	32.37	1.92	0.73	1.19	0.91	0.523	1.34	0.389	0.97	1.00	0.400	No
494	32.44	1.92	0.73	1.19	0.91	0.523	1.34	0.389	0.97	1.00	0.400	No
495	32.49	1.93	0.73	1.19	0.91	0.523	1.34	0.389	0.97	1.00	0.400	No
496	32.58	1.93	0.74	1.20	0.91	0.523	1.34	0.389	0.97	1.00	0.400	No
497	32.62	1.93	0.74	1.20	0.91	0.523	1.34	0.389	0.97	1.00	0.400	No
498	32.69	1.94	0.74	1.20	0.91	0.524	1.34	0.389	0.97	1.00	0.401	No
499	32.78	1.94	0.74	1.20	0.91	0.524	1.34	0.389	0.97	1.00	0.401	No
500	32.82	1.94	0.74	1.20	0.90	0.524	1.34	0.389	0.97	1.00	0.401	No
501	32.89	1.95	0.75	1.20	0.90	0.524	1.34	0.389	0.97	1.00	0.401	No
502	32.97	1.95	0.75	1.20	0.90	0.524	1.34	0.390	0.97	1.00	0.401	No
503	33.02	1.96	0.75	1.21	0.90	0.524	1.34	0.390	0.97	1.00	0.401	No
504	33.09	1.96	0.75	1.21	0.90	0.524	1.34	0.390	0.97	1.00	0.402	No
505	33.15	1.96	0.75	1.21	0.90	0.524	1.34	0.390	0.97	1.00	0.402	No
506	33.20	1.97	0.76	1.21	0.90	0.524	1.34	0.390	0.97	1.00	0.402	No
507	33.28	1.97	0.76	1.21	0.90	0.524	1.34	0.390	0.97	1.00	0.402	No
508	33.38	1.98	0.76	1.22	0.90	0.524	1.34	0.390	0.97	1.00	0.402	No
509	33.43	1.98	0.76	1.22	0.90	0.524	1.34	0.390	0.97	1.00	0.402	No
510	33.47	1.98	0.76	1.22	0.90	0.524	1.34	0.390	0.97	1.00	0.402	No
511	33.57	1.99	0.77	1.22	0.90	0.524	1.34	0.390	0.97	1.00	0.403	No
512	33.63	1.99	0.77	1.22	0.90	0.524	1.34	0.390	0.97	1.00	0.403	No
513	33.70	2.00	0.77	1.22	0.90	0.524	1.34	0.390	0.97	1.00	0.403	No
514	33.74	2.00	0.77	1.23	0.90	0.524	1.34	0.390	0.97	1.00	0.403	No
515	33.82	2.00	0.77	1.23	0.90	0.524	1.34	0.390	0.97	1.00	0.403	No
516	33.86	2.00	0.78	1.23	0.90	0.524	1.34	0.390	0.97	1.00	0.403	No
517	33.93	2.01	0.78	1.23	0.90	0.524	1.34	0.390	0.97	1.00	0.403	No
518	34.02	2.01	0.78	1.23	0.90	0.524	1.34	0.390	0.97	1.00	0.404	No
519	34.06	2.02	0.78	1.23	0.90	0.524	1.34	0.390	0.97	1.00	0.404	No
520	34.13	2.02	0.78	1.24	0.90	0.524	1.34	0.390	0.96	1.00	0.404	No
521	34.21	2.03	0.79	1.24	0.90	0.524	1.34	0.389	0.96	1.00	0.404	No
522	34.28	2.03	0.79	1.24	0.90	0.524	1.34	0.389	0.96	1.00	0.404	No
523	34.32	2.03	0.79	1.24	0.90	0.524	1.34	0.389	0.96	1.00	0.404	No
524	34.41	2.04	0.79	1.24	0.89	0.524	1.34	0.389	0.96	1.00	0.404	No
525	34.46	2.04	0.79	1.25	0.89	0.524	1.34	0.389	0.96	1.00	0.404	No
526	34.52	2.04	0.80	1.25	0.89	0.523	1.34	0.389	0.96	1.00	0.404	No
527	34.61	2.05	0.80	1.25	0.89	0.523	1.34	0.389	0.96	1.00	0.405	No
528	34.65	2.05	0.80	1.25	0.89	0.523	1.34	0.389	0.96	1.00	0.405	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
529	34.71	2.06	0.80	1.25	0.89	0.523	1.34	0.389	0.96	1.00	0.405	No
530	34.79	2.06	0.80	1.26	0.89	0.523	1.34	0.389	0.96	1.00	0.405	No
531	34.86	2.06	0.81	1.26	0.89	0.523	1.34	0.389	0.96	1.00	0.405	No
532	34.93	2.07	0.81	1.26	0.89	0.523	1.34	0.389	0.96	1.00	0.405	No
533	35.01	2.07	0.81	1.26	0.89	0.523	1.34	0.389	0.96	1.00	0.405	No
534	35.06	2.08	0.81	1.26	0.89	0.523	1.34	0.389	0.96	1.00	0.405	No
535	35.11	2.08	0.81	1.26	0.89	0.523	1.34	0.389	0.96	1.00	0.405	No
536	35.18	2.08	0.82	1.27	0.89	0.523	1.34	0.389	0.96	1.00	0.405	No
537	35.26	2.09	0.82	1.27	0.89	0.523	1.34	0.389	0.96	1.00	0.406	No
538	35.34	2.09	0.82	1.27	0.89	0.523	1.34	0.389	0.96	1.00	0.406	No
539	35.40	2.10	0.82	1.27	0.89	0.523	1.34	0.389	0.96	1.00	0.406	No
540	35.44	2.10	0.82	1.27	0.89	0.523	1.34	0.389	0.96	1.00	0.406	No
541	35.51	2.10	0.83	1.27	0.89	0.523	1.34	0.389	0.96	1.00	0.406	No
542	35.58	2.11	0.83	1.28	0.89	0.523	1.34	0.389	0.96	1.00	0.406	No
543	35.66	2.11	0.83	1.28	0.89	0.523	1.34	0.389	0.96	1.00	0.406	No
544	35.71	2.11	0.83	1.28	0.89	0.523	1.34	0.389	0.96	1.00	0.406	No
545	35.77	2.12	0.84	1.28	0.89	0.523	1.34	0.389	0.96	1.00	0.406	No
546	35.85	2.12	0.84	1.28	0.88	0.523	1.34	0.389	0.96	1.00	0.406	No
547	35.92	2.13	0.84	1.29	0.88	0.523	1.34	0.389	0.96	1.00	0.406	No
548	35.97	2.13	0.84	1.29	0.88	0.522	1.34	0.389	0.96	1.00	0.406	No
549	36.03	2.13	0.84	1.29	0.88	0.522	1.34	0.389	0.96	1.00	0.407	No
550	36.11	2.14	0.85	1.29	0.88	0.522	1.34	0.388	0.96	1.00	0.407	No
551	36.16	2.14	0.85	1.29	0.88	0.522	1.34	0.388	0.96	1.00	0.407	No
552	36.26	2.14	0.85	1.29	0.88	0.522	1.34	0.388	0.95	1.00	0.407	No
553	36.31	2.15	0.85	1.30	0.88	0.522	1.34	0.388	0.95	1.00	0.407	No
554	36.36	2.15	0.85	1.30	0.88	0.522	1.34	0.388	0.95	1.00	0.407	No
555	36.43	2.15	0.86	1.30	0.88	0.522	1.34	0.388	0.95	1.00	0.407	No
556	36.51	2.16	0.86	1.30	0.88	0.522	1.34	0.388	0.95	1.00	0.407	No
557	36.55	2.16	0.86	1.30	0.88	0.522	1.34	0.388	0.95	1.00	0.407	No
558	36.65	2.17	0.86	1.30	0.88	0.522	1.34	0.388	0.95	1.00	0.407	No
559	36.71	2.17	0.86	1.31	0.88	0.522	1.34	0.388	0.95	1.00	0.407	No
560	36.76	2.17	0.87	1.31	0.88	0.522	1.34	0.388	0.95	1.00	0.407	No
561	36.85	2.18	0.87	1.31	0.88	0.522	1.34	0.388	0.95	1.00	0.407	No
562	36.89	2.18	0.87	1.31	0.88	0.522	1.34	0.388	0.95	1.00	0.407	No
563	36.96	2.18	0.87	1.31	0.88	0.521	1.34	0.388	0.95	1.00	0.408	No
564	37.02	2.19	0.87	1.31	0.88	0.521	1.34	0.388	0.95	1.00	0.408	No
565	37.11	2.19	0.88	1.32	0.88	0.521	1.34	0.388	0.95	1.00	0.408	No
566	37.15	2.20	0.88	1.32	0.87	0.521	1.34	0.388	0.95	1.00	0.408	No
567	37.24	2.20	0.88	1.32	0.87	0.521	1.34	0.388	0.95	1.00	0.408	No
568	37.31	2.20	0.88	1.32	0.87	0.521	1.34	0.387	0.95	1.00	0.408	No
569	37.35	2.21	0.88	1.32	0.87	0.521	1.34	0.387	0.95	1.00	0.408	No
570	37.43	2.21	0.89	1.32	0.87	0.521	1.34	0.387	0.95	1.00	0.408	No
571	37.51	2.22	0.89	1.33	0.87	0.521	1.34	0.387	0.95	1.00	0.408	No
572	37.55	2.22	0.89	1.33	0.87	0.521	1.34	0.387	0.95	1.00	0.408	No
573	37.60	2.22	0.89	1.33	0.87	0.520	1.34	0.387	0.95	1.00	0.408	No
574	37.67	2.23	0.89	1.33	0.87	0.520	1.34	0.387	0.95	1.00	0.408	No
575	37.75	2.23	0.90	1.33	0.87	0.520	1.34	0.387	0.95	1.00	0.408	No
576	37.81	2.23	0.90	1.34	0.87	0.520	1.34	0.387	0.95	1.00	0.408	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
577	37.88	2.24	0.90	1.34	0.87	0.520	1.34	0.387	0.95	1.00	0.408	No
578	37.93	2.24	0.90	1.34	0.87	0.520	1.34	0.387	0.95	1.00	0.408	No
579	38.00	2.25	0.90	1.34	0.87	0.520	1.34	0.386	0.95	1.00	0.408	No
580	38.08	2.25	0.91	1.34	0.87	0.519	1.34	0.386	0.95	1.00	0.408	No
581	38.14	2.25	0.91	1.35	0.87	0.519	1.34	0.386	0.95	1.00	0.408	No
582	38.20	2.26	0.91	1.35	0.87	0.519	1.34	0.386	0.95	1.00	0.408	No
583	38.26	2.26	0.91	1.35	0.87	0.519	1.34	0.386	0.95	1.00	2.000	Yes
584	38.34	2.27	0.92	1.35	0.87	0.519	1.34	0.386	0.95	1.00	2.000	Yes
585	38.43	2.27	0.92	1.35	0.86	0.519	1.34	0.386	0.94	1.00	2.000	Yes
586	38.45	2.27	0.92	1.36	0.86	0.518	1.34	0.386	0.94	1.00	2.000	Yes
587	38.53	2.28	0.92	1.36	0.86	0.518	1.34	0.385	0.94	1.00	2.000	Yes
588	38.62	2.29	0.92	1.36	0.86	0.518	1.34	0.385	0.94	1.00	2.000	Yes
589	38.65	2.29	0.93	1.36	0.86	0.518	1.34	0.385	0.94	1.00	2.000	Yes
590	38.72	2.29	0.93	1.36	0.86	0.518	1.34	0.385	0.94	1.00	0.408	No
591	38.80	2.30	0.93	1.37	0.86	0.517	1.34	0.385	0.94	1.00	0.408	No
592	38.88	2.30	0.93	1.37	0.86	0.517	1.34	0.385	0.94	1.00	0.408	No
593	38.93	2.31	0.93	1.37	0.86	0.517	1.34	0.384	0.94	1.00	0.408	No
594	39.01	2.31	0.94	1.38	0.86	0.517	1.34	0.384	0.94	1.00	0.408	No
595	39.07	2.32	0.94	1.38	0.86	0.516	1.34	0.384	0.94	1.00	0.408	No
596	39.12	2.32	0.94	1.38	0.86	0.516	1.34	0.384	0.94	1.00	0.408	No
597	39.20	2.32	0.94	1.38	0.86	0.516	1.34	0.384	0.94	1.00	0.408	No
598	39.27	2.33	0.94	1.38	0.86	0.516	1.34	0.383	0.94	1.00	0.408	No
599	39.31	2.33	0.95	1.39	0.86	0.515	1.34	0.383	0.94	1.00	0.408	No
600	39.38	2.34	0.95	1.39	0.86	0.515	1.34	0.383	0.94	1.00	0.408	No
601	39.45	2.34	0.95	1.39	0.86	0.515	1.34	0.383	0.94	1.00	0.408	No
602	39.51	2.35	0.95	1.39	0.86	0.515	1.34	0.383	0.94	1.00	0.408	No
603	39.57	2.35	0.95	1.40	0.85	0.514	1.34	0.383	0.94	1.00	0.408	No
604	39.64	2.35	0.96	1.40	0.85	0.514	1.34	0.382	0.94	1.00	0.408	No
605	39.72	2.36	0.96	1.40	0.85	0.514	1.34	0.382	0.94	1.00	0.408	No
606	39.79	2.36	0.96	1.40	0.85	0.514	1.34	0.382	0.94	1.00	0.408	No
607	39.84	2.37	0.96	1.41	0.85	0.513	1.34	0.382	0.94	1.00	0.408	No
608	39.90	2.37	0.96	1.41	0.85	0.513	1.34	0.382	0.94	1.00	0.408	No
609	39.96	2.38	0.97	1.41	0.85	0.513	1.34	0.381	0.94	1.00	0.407	No
610	40.06	2.38	0.97	1.41	0.85	0.512	1.34	0.381	0.94	1.00	0.407	No
611	40.13	2.39	0.97	1.42	0.85	0.512	1.34	0.381	0.94	1.00	0.407	No
612	40.17	2.39	0.97	1.42	0.85	0.512	1.34	0.381	0.93	1.00	0.407	No
613	40.26	2.40	0.98	1.42	0.85	0.512	1.34	0.381	0.93	1.00	0.407	No
614	40.31	2.40	0.98	1.42	0.85	0.511	1.34	0.380	0.93	1.00	0.407	No
615	40.36	2.40	0.98	1.42	0.85	0.511	1.34	0.380	0.93	1.00	0.407	No
616	40.43	2.41	0.98	1.43	0.85	0.511	1.34	0.380	0.93	1.00	0.407	No
617	40.51	2.41	0.98	1.43	0.85	0.511	1.34	0.380	0.93	1.00	0.407	No
618	40.56	2.42	0.98	1.43	0.85	0.510	1.34	0.380	0.93	1.00	0.407	No
619	40.64	2.42	0.99	1.43	0.85	0.510	1.34	0.379	0.93	1.00	0.407	No
620	40.70	2.43	0.99	1.44	0.84	0.510	1.34	0.379	0.93	1.00	0.407	No
621	40.75	2.43	0.99	1.44	0.84	0.510	1.34	0.379	0.93	1.00	0.407	No
622	40.83	2.43	0.99	1.44	0.84	0.509	1.34	0.379	0.93	1.00	0.407	No
623	40.88	2.44	0.99	1.44	0.84	0.509	1.34	0.379	0.93	1.00	0.407	No
624	40.95	2.44	1.00	1.45	0.84	0.509	1.34	0.378	0.93	1.00	0.407	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
625	41.03	2.45	1.00	1.45	0.84	0.509	1.34	0.378	0.93	1.00	0.407	No
626	41.08	2.45	1.00	1.45	0.84	0.508	1.34	0.378	0.93	1.00	0.407	No
627	41.15	2.46	1.00	1.45	0.84	0.508	1.34	0.378	0.93	1.00	0.406	No
628	41.24	2.46	1.01	1.46	0.84	0.508	1.34	0.378	0.93	1.00	0.406	No
629	41.28	2.46	1.01	1.46	0.84	0.508	1.34	0.378	0.93	1.00	0.406	No
630	41.35	2.47	1.01	1.46	0.84	0.507	1.34	0.377	0.93	1.00	0.406	No
631	41.41	2.47	1.01	1.46	0.84	0.507	1.34	0.377	0.93	1.00	0.406	No
632	41.48	2.48	1.01	1.46	0.84	0.507	1.34	0.377	0.93	1.00	0.406	No
633	41.55	2.48	1.02	1.47	0.84	0.507	1.34	0.377	0.93	1.00	0.406	No
634	41.63	2.49	1.02	1.47	0.84	0.506	1.34	0.376	0.93	1.00	0.406	No
635	41.68	2.49	1.02	1.47	0.84	0.506	1.34	0.376	0.93	1.00	0.406	No
636	41.74	2.49	1.02	1.47	0.84	0.506	1.34	0.376	0.93	1.00	0.406	No
637	41.83	2.50	1.02	1.48	0.83	0.505	1.34	0.376	0.93	1.00	0.406	No
638	41.87	2.50	1.03	1.48	0.83	0.505	1.34	0.376	0.93	1.00	0.406	No
639	41.98	2.51	1.03	1.48	0.83	0.505	1.34	0.375	0.93	1.00	0.406	No
640	42.02	2.51	1.03	1.48	0.83	0.505	1.34	0.375	0.93	1.00	0.406	No
641	42.10	2.52	1.03	1.48	0.83	0.504	1.34	0.375	0.93	1.00	0.405	No
642	42.14	2.52	1.03	1.49	0.83	0.504	1.34	0.375	0.92	1.00	0.405	No
643	42.22	2.53	1.04	1.49	0.83	0.504	1.34	0.375	0.92	1.00	0.405	No
644	42.29	2.53	1.04	1.49	0.83	0.503	1.34	0.374	0.92	1.00	0.405	No
645	42.38	2.54	1.04	1.49	0.83	0.503	1.34	0.374	0.92	1.00	0.405	No
646	42.41	2.54	1.04	1.50	0.83	0.503	1.34	0.374	0.92	1.00	0.405	No
647	42.46	2.54	1.04	1.50	0.83	0.503	1.34	0.374	0.92	1.00	0.405	No
648	42.57	2.55	1.05	1.50	0.83	0.502	1.34	0.374	0.92	1.00	0.405	No
649	42.61	2.55	1.05	1.50	0.83	0.502	1.34	0.373	0.92	1.00	0.405	No
650	42.68	2.56	1.05	1.50	0.83	0.502	1.34	0.373	0.92	1.00	0.405	No
651	42.76	2.56	1.05	1.51	0.83	0.501	1.34	0.373	0.92	1.00	0.405	No
652	42.80	2.56	1.05	1.51	0.83	0.501	1.34	0.373	0.92	1.00	0.404	No
653	42.87	2.57	1.06	1.51	0.82	0.501	1.34	0.373	0.92	1.00	0.404	No
654	42.92	2.57	1.06	1.51	0.82	0.501	1.34	0.372	0.92	1.00	0.404	No
655	42.98	2.58	1.06	1.51	0.82	0.500	1.34	0.372	0.92	1.00	0.404	No
656	43.06	2.58	1.06	1.52	0.82	0.500	1.34	0.372	0.92	1.00	0.404	No
657	43.11	2.58	1.06	1.52	0.82	0.500	1.34	0.372	0.92	1.00	0.404	No
658	43.18	2.59	1.07	1.52	0.82	0.500	1.34	0.372	0.92	1.00	0.404	No
659	43.26	2.59	1.07	1.52	0.82	0.499	1.34	0.371	0.92	1.00	0.404	No
660	43.32	2.60	1.07	1.53	0.82	0.499	1.34	0.371	0.92	1.00	0.404	No
661	43.39	2.60	1.07	1.53	0.82	0.499	1.34	0.371	0.92	1.00	0.404	No
662	43.46	2.61	1.08	1.53	0.82	0.498	1.34	0.371	0.92	1.00	0.404	No
663	43.52	2.61	1.08	1.53	0.82	0.498	1.34	0.370	0.92	1.00	0.403	No
664	43.61	2.62	1.08	1.54	0.82	0.498	1.34	0.370	0.92	1.00	0.403	No
665	43.64	2.62	1.08	1.54	0.82	0.498	1.34	0.370	0.92	1.00	0.403	No
666	43.70	2.62	1.08	1.54	0.82	0.497	1.34	0.370	0.92	1.00	0.403	No
667	43.79	2.63	1.09	1.54	0.82	0.497	1.34	0.370	0.92	1.00	0.403	No
668	43.84	2.63	1.09	1.54	0.82	0.497	1.34	0.370	0.92	1.00	0.403	No
669	43.90	2.63	1.09	1.54	0.81	0.497	1.34	0.369	0.92	1.00	0.403	No
670	43.97	2.64	1.09	1.55	0.81	0.496	1.34	0.369	0.92	1.00	0.403	No
671	44.05	2.64	1.09	1.55	0.81	0.496	1.34	0.369	0.92	1.00	0.403	No
672	44.10	2.64	1.10	1.55	0.81	0.496	1.34	0.369	0.92	1.00	0.403	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
673	44.18	2.65	1.10	1.55	0.81	0.496	1.34	0.369	0.92	1.00	0.402	No
674	44.24	2.65	1.10	1.55	0.81	0.495	1.34	0.368	0.92	1.00	0.402	No
675	44.30	2.66	1.10	1.55	0.81	0.495	1.34	0.368	0.92	1.00	0.402	No
676	44.38	2.66	1.10	1.56	0.81	0.495	1.34	0.368	0.91	1.00	0.402	No
677	44.45	2.67	1.11	1.56	0.81	0.494	1.34	0.368	0.91	1.00	0.402	No
678	44.49	2.67	1.11	1.56	0.81	0.494	1.34	0.368	0.91	1.00	0.402	No
679	44.57	2.67	1.11	1.56	0.81	0.494	1.34	0.367	0.91	1.00	0.402	No
680	44.64	2.68	1.11	1.56	0.81	0.494	1.34	0.367	0.91	1.00	0.402	No
681	44.72	2.68	1.11	1.57	0.81	0.493	1.34	0.367	0.91	1.00	0.402	No
682	44.79	2.69	1.12	1.57	0.81	0.493	1.34	0.367	0.91	1.00	0.401	No
683	44.84	2.69	1.12	1.57	0.81	0.493	1.34	0.366	0.91	1.00	2.000	Yes
684	44.92	2.69	1.12	1.57	0.80	0.492	1.34	0.366	0.91	1.00	2.000	Yes
685	44.96	2.70	1.12	1.57	0.80	0.492	1.34	0.366	0.91	1.00	2.000	Yes
686	45.03	2.70	1.12	1.58	0.80	0.492	1.34	0.366	0.91	1.00	2.000	Yes
687	45.09	2.70	1.13	1.58	0.80	0.492	1.34	0.366	0.91	1.00	2.000	Yes
688	45.19	2.71	1.13	1.58	0.80	0.491	1.34	0.365	0.91	1.00	2.000	Yes
689	45.23	2.71	1.13	1.58	0.80	0.491	1.34	0.365	0.91	1.00	2.000	Yes
690	45.28	2.72	1.13	1.58	0.80	0.491	1.34	0.365	0.91	1.00	2.000	Yes
691	45.38	2.72	1.14	1.59	0.80	0.490	1.34	0.365	0.91	1.00	2.000	Yes
692	45.43	2.73	1.14	1.59	0.80	0.490	1.34	0.364	0.91	1.00	2.000	Yes
693	45.48	2.73	1.14	1.59	0.80	0.490	1.34	0.364	0.91	1.00	0.400	No
694	45.58	2.74	1.14	1.59	0.80	0.489	1.34	0.364	0.91	1.00	2.000	Yes
695	45.62	2.74	1.14	1.60	0.80	0.489	1.34	0.364	0.91	1.00	2.000	Yes
696	45.67	2.74	1.14	1.60	0.80	0.489	1.34	0.364	0.91	1.00	2.000	Yes
697	45.78	2.75	1.15	1.60	0.80	0.488	1.34	0.363	0.91	1.00	2.000	Yes
698	45.82	2.75	1.15	1.60	0.80	0.488	1.34	0.363	0.91	1.00	2.000	Yes
699	45.88	2.76	1.15	1.60	0.79	0.488	1.34	0.363	0.91	1.00	2.000	Yes
700	45.98	2.76	1.15	1.61	0.79	0.487	1.34	0.362	0.91	1.00	2.000	Yes
701	46.02	2.76	1.16	1.61	0.79	0.487	1.34	0.362	0.91	1.00	2.000	Yes
702	46.07	2.77	1.16	1.61	0.79	0.487	1.34	0.362	0.91	1.00	2.000	Yes
703	46.17	2.77	1.16	1.61	0.79	0.486	1.34	0.362	0.91	1.00	0.399	No
704	46.21	2.78	1.16	1.62	0.79	0.486	1.34	0.362	0.91	1.00	0.399	No
705	46.27	2.78	1.16	1.62	0.79	0.486	1.34	0.361	0.91	1.00	0.399	No
706	46.37	2.79	1.17	1.62	0.79	0.486	1.34	0.361	0.91	1.00	0.398	No
707	46.39	2.79	1.17	1.62	0.79	0.485	1.34	0.361	0.91	1.00	0.398	No
708	46.47	2.79	1.17	1.62	0.79	0.485	1.34	0.361	0.91	1.00	0.398	No
709	46.57	2.80	1.17	1.63	0.79	0.485	1.34	0.360	0.91	1.00	0.398	No
710	46.62	2.80	1.17	1.63	0.79	0.484	1.34	0.360	0.91	1.00	0.398	No
711	46.67	2.81	1.18	1.63	0.79	0.484	1.34	0.360	0.91	1.00	0.398	No
712	46.77	2.81	1.18	1.63	0.79	0.484	1.34	0.360	0.91	1.00	0.397	No
713	46.82	2.81	1.18	1.63	0.79	0.483	1.34	0.360	0.90	1.00	0.397	No
714	46.90	2.82	1.18	1.64	0.78	0.483	1.34	0.359	0.90	1.00	0.397	No
715	46.92	2.82	1.18	1.64	0.78	0.483	1.34	0.359	0.90	1.00	0.397	No
716	47.01	2.83	1.19	1.64	0.78	0.482	1.34	0.359	0.90	1.00	0.397	No
717	47.05	2.83	1.19	1.64	0.78	0.482	1.34	0.359	0.90	1.00	0.397	No
718	47.12	2.83	1.19	1.64	0.78	0.482	1.34	0.358	0.90	1.00	0.397	No
719	47.21	2.84	1.19	1.65	0.78	0.481	1.34	0.358	0.90	1.00	0.396	No
720	47.28	2.84	1.19	1.65	0.78	0.481	1.34	0.358	0.90	1.00	0.396	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
721	47.32	2.85	1.20	1.65	0.78	0.481	1.34	0.358	0.90	1.00	0.396	No
722	47.40	2.85	1.20	1.65	0.78	0.481	1.34	0.357	0.90	1.00	0.396	No
723	47.45	2.85	1.20	1.65	0.78	0.480	1.34	0.357	0.90	1.00	0.396	No
724	47.55	2.86	1.20	1.66	0.78	0.480	1.34	0.357	0.90	1.00	0.396	No
725	47.58	2.86	1.20	1.66	0.78	0.480	1.34	0.357	0.90	1.00	0.396	No
726	47.66	2.87	1.21	1.66	0.78	0.479	1.34	0.356	0.90	1.00	0.395	No
727	47.74	2.87	1.21	1.66	0.78	0.479	1.34	0.356	0.90	1.00	0.395	No
728	47.80	2.88	1.21	1.67	0.78	0.479	1.34	0.356	0.90	1.00	0.395	No
729	47.85	2.88	1.21	1.67	0.77	0.478	1.34	0.356	0.90	1.00	0.395	No
730	47.93	2.88	1.21	1.67	0.77	0.478	1.34	0.355	0.90	1.00	0.395	No
731	47.98	2.89	1.22	1.67	0.77	0.478	1.34	0.355	0.90	1.00	0.395	No
732	48.04	2.89	1.22	1.67	0.77	0.477	1.34	0.355	0.90	1.00	0.395	No
733	48.11	2.90	1.22	1.68	0.77	0.477	1.34	0.355	0.90	1.00	0.394	No
734	48.20	2.90	1.22	1.68	0.77	0.477	1.34	0.354	0.90	1.00	0.394	No
735	48.24	2.90	1.22	1.68	0.77	0.476	1.34	0.354	0.90	1.00	0.394	No
736	48.30	2.91	1.23	1.68	0.77	0.476	1.34	0.354	0.90	1.00	0.394	No
737	48.39	2.91	1.23	1.68	0.77	0.476	1.34	0.354	0.90	1.00	0.394	No
738	48.44	2.92	1.23	1.69	0.77	0.475	1.34	0.354	0.90	1.00	0.394	No
739	48.53	2.92	1.23	1.69	0.77	0.475	1.34	0.353	0.90	1.00	0.393	No
740	48.59	2.93	1.24	1.69	0.77	0.475	1.34	0.353	0.90	1.00	0.393	No
741	48.64	2.93	1.24	1.69	0.77	0.474	1.34	0.353	0.90	1.00	0.393	No
742	48.70	2.93	1.24	1.69	0.77	0.474	1.34	0.353	0.90	1.00	0.393	No
743	48.78	2.94	1.24	1.70	0.77	0.474	1.34	0.352	0.90	1.00	0.393	No
744	48.82	2.94	1.24	1.70	0.76	0.473	1.34	0.352	0.90	1.00	0.393	No
745	48.89	2.94	1.24	1.70	0.76	0.473	1.34	0.352	0.90	1.00	0.392	No
746	48.98	2.95	1.25	1.70	0.76	0.473	1.34	0.352	0.90	1.00	0.392	No
747	49.05	2.96	1.25	1.71	0.76	0.472	1.34	0.351	0.90	1.00	0.392	No
748	49.09	2.96	1.25	1.71	0.76	0.472	1.34	0.351	0.90	1.00	0.392	No
749	49.16	2.96	1.25	1.71	0.76	0.472	1.34	0.351	0.90	1.00	0.392	No
750	49.24	2.97	1.26	1.71	0.76	0.471	1.34	0.350	0.90	1.00	0.392	No
751	49.31	2.97	1.26	1.71	0.76	0.471	1.34	0.350	0.89	1.00	0.391	No
752	49.38	2.98	1.26	1.72	0.76	0.471	1.34	0.350	0.89	1.00	0.391	No
753	49.43	2.98	1.26	1.72	0.76	0.470	1.34	0.350	0.89	1.00	0.391	No
754	49.52	2.99	1.26	1.72	0.76	0.470	1.34	0.349	0.89	1.00	0.391	No
755	49.58	2.99	1.27	1.72	0.76	0.469	1.34	0.349	0.89	1.00	0.391	No
756	49.63	2.99	1.27	1.73	0.76	0.469	1.34	0.349	0.89	1.00	0.390	No
757	49.71	3.00	1.27	1.73	0.76	0.469	1.34	0.349	0.89	1.00	0.390	No
758	49.77	3.00	1.27	1.73	0.76	0.468	1.34	0.348	0.89	1.00	2.000	Yes
759	49.82	3.00	1.27	1.73	0.75	0.468	1.34	0.348	0.89	1.00	2.000	Yes
760	49.88	3.01	1.28	1.73	0.75	0.468	1.34	0.348	0.89	1.00	2.000	Yes
761	49.97	3.01	1.28	1.74	0.75	0.467	1.34	0.348	0.89	1.00	2.000	Yes
762	50.01	3.02	1.28	1.74	0.75	0.467	1.34	0.347	0.89	1.00	2.000	Yes
763	50.07	3.02	1.28	1.74	0.75	0.467	1.34	0.347	0.89	1.00	2.000	Yes
764	50.17	3.03	1.28	1.74	0.75	0.466	1.34	0.347	0.89	1.00	2.000	Yes
765	50.22	3.03	1.29	1.74	0.75	0.466	1.34	0.347	0.89	1.00	2.000	Yes
766	50.29	3.03	1.29	1.75	0.75	0.466	1.34	0.346	0.89	1.00	2.000	Yes
767	50.37	3.04	1.29	1.75	0.75	0.465	1.34	0.346	0.89	1.00	2.000	Yes
768	50.42	3.04	1.29	1.75	0.75	0.465	1.34	0.346	0.89	1.00	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
769	50.47	3.05	1.29	1.75	0.75	0.465	1.34	0.346	0.89	1.00	2.000	No
770	50.57	3.05	1.30	1.76	0.75	0.464	1.34	0.345	0.89	1.00	2.000	No
771	50.63	3.06	1.30	1.76	0.75	0.464	1.34	0.345	0.89	1.00	2.000	No
772	50.68	3.06	1.30	1.76	0.75	0.464	1.34	0.345	0.89	1.00	2.000	No
773	50.73	3.06	1.30	1.76	0.75	0.463	1.34	0.345	0.89	1.00	2.000	No
774	50.79	3.07	1.30	1.76	0.74	0.463	1.34	0.344	0.89	1.00	2.000	No
775	50.88	3.07	1.31	1.77	0.74	0.463	1.34	0.344	0.89	1.00	2.000	No
776	50.93	3.07	1.31	1.77	0.74	0.462	1.34	0.344	0.89	1.00	2.000	No
777	51.03	3.08	1.31	1.77	0.74	0.462	1.34	0.344	0.89	1.00	2.000	No
778	51.07	3.08	1.31	1.77	0.74	0.462	1.34	0.343	0.89	1.00	2.000	No
779	51.14	3.09	1.31	1.77	0.74	0.461	1.34	0.343	0.89	1.00	2.000	No
780	51.23	3.09	1.32	1.77	0.74	0.461	1.34	0.343	0.89	1.00	2.000	No
781	51.27	3.09	1.32	1.78	0.74	0.461	1.34	0.343	0.89	1.00	2.000	No
782	51.33	3.10	1.32	1.78	0.74	0.461	1.34	0.343	0.89	1.00	2.000	No
783	51.42	3.10	1.32	1.78	0.74	0.460	1.34	0.342	0.89	1.00	2.000	No
784	51.48	3.11	1.33	1.78	0.74	0.460	1.34	0.342	0.89	1.00	2.000	No
785	51.52	3.11	1.33	1.78	0.74	0.460	1.34	0.342	0.89	1.00	2.000	No
786	51.60	3.11	1.33	1.78	0.74	0.459	1.34	0.342	0.89	1.00	2.000	No
787	51.68	3.12	1.33	1.79	0.74	0.459	1.34	0.341	0.89	1.00	2.000	No
788	51.72	3.12	1.33	1.79	0.74	0.459	1.34	0.341	0.89	1.00	2.000	No
789	51.81	3.12	1.34	1.79	0.73	0.459	1.34	0.341	0.89	1.00	2.000	No
790	51.87	3.13	1.34	1.79	0.73	0.458	1.34	0.341	0.89	1.00	2.000	No
791	51.91	3.13	1.34	1.79	0.73	0.458	1.34	0.341	0.89	1.00	2.000	No
792	51.98	3.13	1.34	1.79	0.73	0.458	1.34	0.340	0.89	1.00	2.000	No
793	52.07	3.14	1.34	1.80	0.73	0.457	1.34	0.340	0.89	1.00	2.000	No
794	52.10	3.14	1.34	1.80	0.73	0.457	1.34	0.340	0.89	1.00	2.000	No
795	52.17	3.15	1.35	1.80	0.73	0.457	1.34	0.340	0.89	1.00	2.000	No
796	52.24	3.15	1.35	1.80	0.73	0.457	1.34	0.340	0.88	1.00	2.000	No
797	52.31	3.15	1.35	1.80	0.73	0.456	1.34	0.339	0.88	1.00	2.000	No
798	52.37	3.16	1.35	1.80	0.73	0.456	1.34	0.339	0.88	1.00	2.000	No
799	52.46	3.16	1.36	1.81	0.73	0.456	1.34	0.339	0.88	1.00	2.000	No
800	52.51	3.16	1.36	1.81	0.73	0.455	1.34	0.339	0.88	1.00	2.000	No
801	52.57	3.17	1.36	1.81	0.73	0.455	1.34	0.339	0.88	1.00	2.000	No
802	52.66	3.17	1.36	1.81	0.73	0.455	1.34	0.338	0.88	1.00	2.000	No
803	52.71	3.18	1.36	1.81	0.73	0.455	1.34	0.338	0.88	1.00	2.000	No
804	52.78	3.18	1.37	1.81	0.72	0.454	1.34	0.338	0.88	1.00	2.000	No
805	52.86	3.18	1.37	1.81	0.72	0.454	1.34	0.338	0.88	1.00	2.000	No
806	52.91	3.19	1.37	1.82	0.72	0.454	1.34	0.337	0.88	1.00	2.000	No
807	52.99	3.19	1.37	1.82	0.72	0.453	1.34	0.337	0.88	1.00	2.000	No
808	53.06	3.19	1.37	1.82	0.72	0.453	1.34	0.337	0.88	1.00	2.000	No
809	53.09	3.20	1.38	1.82	0.72	0.453	1.34	0.337	0.88	1.00	2.000	No
810	53.16	3.20	1.38	1.82	0.72	0.453	1.34	0.337	0.88	1.00	2.000	No
811	53.25	3.20	1.38	1.82	0.72	0.452	1.34	0.336	0.88	1.00	2.000	No
812	53.29	3.21	1.38	1.82	0.72	0.452	1.34	0.336	0.88	1.00	2.000	No
813	53.36	3.21	1.38	1.83	0.72	0.452	1.34	0.336	0.88	1.00	2.000	No
814	53.45	3.22	1.39	1.83	0.72	0.452	1.34	0.336	0.88	1.00	2.000	No
815	53.50	3.22	1.39	1.83	0.72	0.451	1.34	0.336	0.88	1.00	2.000	No
816	53.55	3.22	1.39	1.83	0.72	0.451	1.34	0.336	0.88	1.00	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
817	53.64	3.23	1.39	1.83	0.72	0.451	1.34	0.335	0.88	1.00	2.000	No
818	53.69	3.23	1.39	1.83	0.72	0.451	1.34	0.335	0.88	1.00	2.000	No
819	53.76	3.23	1.40	1.84	0.72	0.450	1.34	0.335	0.88	1.00	2.000	No
820	53.84	3.24	1.40	1.84	0.71	0.450	1.34	0.335	0.88	1.00	2.000	No
821	53.88	3.24	1.40	1.84	0.71	0.450	1.34	0.334	0.88	1.00	2.000	No
822	53.96	3.24	1.40	1.84	0.71	0.449	1.34	0.334	0.88	1.00	2.000	No
823	54.03	3.25	1.40	1.84	0.71	0.449	1.34	0.334	0.88	1.00	2.000	No
824	54.08	3.25	1.41	1.84	0.71	0.449	1.34	0.334	0.88	1.00	2.000	No
825	54.17	3.25	1.41	1.84	0.71	0.449	1.34	0.334	0.88	1.00	2.000	No
826	54.23	3.26	1.41	1.85	0.71	0.448	1.34	0.333	0.88	1.00	2.000	No
827	54.27	3.26	1.41	1.85	0.71	0.448	1.34	0.333	0.88	1.00	2.000	No
828	54.38	3.27	1.42	1.85	0.71	0.448	1.34	0.333	0.88	1.00	2.000	No
829	54.42	3.27	1.42	1.85	0.71	0.447	1.34	0.333	0.88	1.00	2.000	No
830	54.47	3.27	1.42	1.85	0.71	0.447	1.34	0.333	0.88	1.00	2.000	No
831	54.53	3.27	1.42	1.85	0.71	0.447	1.34	0.332	0.88	1.00	2.000	No
832	54.61	3.28	1.42	1.85	0.71	0.447	1.34	0.332	0.88	1.00	2.000	No
833	54.68	3.28	1.43	1.86	0.71	0.446	1.34	0.332	0.88	1.00	2.000	No
834	54.73	3.28	1.43	1.86	0.71	0.446	1.34	0.332	0.88	1.00	2.000	No
835	54.80	3.29	1.43	1.86	0.71	0.446	1.34	0.332	0.88	1.00	2.000	No
836	54.88	3.29	1.43	1.86	0.70	0.446	1.34	0.331	0.88	1.00	2.000	No
837	54.95	3.30	1.43	1.86	0.70	0.445	1.34	0.331	0.88	1.00	2.000	No
838	55.02	3.30	1.44	1.86	0.70	0.445	1.34	0.331	0.88	1.00	2.000	No
839	55.07	3.30	1.44	1.87	0.70	0.445	1.34	0.331	0.88	1.00	2.000	No
840	55.15	3.31	1.44	1.87	0.70	0.444	1.34	0.331	0.88	1.00	2.000	No
841	55.21	3.31	1.44	1.87	0.70	0.444	1.34	0.330	0.88	1.00	2.000	No
842	55.27	3.31	1.44	1.87	0.70	0.444	1.34	0.330	0.88	1.00	2.000	No
843	55.34	3.32	1.45	1.87	0.70	0.444	1.34	0.330	0.88	1.00	2.000	No
844	55.42	3.32	1.45	1.87	0.70	0.443	1.34	0.330	0.88	1.00	2.000	No
845	55.47	3.32	1.45	1.87	0.70	0.443	1.34	0.330	0.88	1.00	2.000	No
846	55.54	3.33	1.45	1.88	0.70	0.443	1.34	0.329	0.88	1.00	2.000	No
847	55.62	3.33	1.45	1.88	0.70	0.442	1.34	0.329	0.88	1.00	2.000	No
848	55.65	3.33	1.46	1.88	0.70	0.442	1.34	0.329	0.88	1.00	2.000	No
849	55.72	3.34	1.46	1.88	0.70	0.442	1.34	0.329	0.88	1.00	2.000	No
850	55.81	3.34	1.46	1.88	0.70	0.442	1.34	0.328	0.88	1.00	2.000	No
851	55.84	3.35	1.46	1.88	0.70	0.442	1.34	0.328	0.88	1.00	2.000	No
852	55.91	3.35	1.46	1.89	0.69	0.441	1.34	0.328	0.88	1.00	2.000	No
853	55.98	3.35	1.47	1.89	0.69	0.441	1.34	0.328	0.88	1.00	2.000	No
854	56.05	3.36	1.47	1.89	0.69	0.441	1.34	0.328	0.88	1.00	2.000	Yes
855	56.11	3.36	1.47	1.89	0.69	0.440	1.34	0.328	0.88	1.00	2.000	Yes
856	56.21	3.37	1.47	1.89	0.69	0.440	1.34	0.327	0.87	1.00	2.000	Yes
857	56.26	3.37	1.47	1.89	0.69	0.440	1.34	0.327	0.87	1.00	2.000	Yes
858	56.31	3.37	1.48	1.90	0.69	0.439	1.34	0.327	0.87	1.00	2.000	Yes
859	56.39	3.38	1.48	1.90	0.69	0.439	1.34	0.327	0.87	1.00	2.000	Yes
860	56.46	3.38	1.48	1.90	0.69	0.439	1.34	0.326	0.87	1.00	2.000	Yes
861	56.50	3.38	1.48	1.90	0.69	0.439	1.34	0.326	0.87	1.00	2.000	Yes
862	56.60	3.39	1.49	1.91	0.69	0.438	1.34	0.326	0.87	1.00	2.000	Yes
863	56.65	3.39	1.49	1.91	0.69	0.438	1.34	0.326	0.87	1.00	2.000	Yes
864	56.72	3.40	1.49	1.91	0.69	0.437	1.34	0.325	0.87	1.00	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
865	56.78	3.40	1.49	1.91	0.69	0.437	1.34	0.325	0.87	1.00	2.000	No
866	56.87	3.41	1.49	1.91	0.69	0.437	1.34	0.325	0.87	1.00	2.000	Yes
867	56.93	3.41	1.50	1.92	0.69	0.436	1.34	0.325	0.87	1.00	2.000	Yes
868	56.97	3.41	1.50	1.92	0.69	0.436	1.34	0.324	0.87	1.00	2.000	Yes
869	57.05	3.42	1.50	1.92	0.68	0.436	1.34	0.324	0.87	1.00	2.000	Yes
870	57.11	3.42	1.50	1.92	0.68	0.436	1.34	0.324	0.87	1.00	2.000	Yes
871	57.17	3.43	1.50	1.92	0.68	0.435	1.34	0.324	0.87	1.00	2.000	Yes
872	57.25	3.43	1.51	1.93	0.68	0.435	1.34	0.323	0.87	1.00	2.000	Yes
873	57.31	3.43	1.51	1.93	0.68	0.435	1.34	0.323	0.87	1.00	2.000	Yes
874	57.37	3.44	1.51	1.93	0.68	0.434	1.34	0.323	0.87	1.00	2.000	Yes
875	57.42	3.44	1.51	1.93	0.68	0.434	1.34	0.323	0.87	1.00	2.000	Yes
876	57.48	3.44	1.51	1.93	0.68	0.434	1.34	0.323	0.87	1.00	2.000	Yes
877	57.56	3.45	1.52	1.93	0.68	0.433	1.34	0.322	0.87	1.00	2.000	No
878	57.64	3.45	1.52	1.94	0.68	0.433	1.34	0.322	0.87	1.00	2.000	No
879	57.70	3.46	1.52	1.94	0.68	0.433	1.34	0.322	0.87	1.00	2.000	No
880	57.74	3.46	1.52	1.94	0.68	0.433	1.34	0.322	0.87	1.00	2.000	No
881	57.81	3.46	1.52	1.94	0.68	0.432	1.34	0.322	0.87	1.00	2.000	No
882	57.90	3.47	1.53	1.94	0.68	0.432	1.34	0.321	0.87	1.00	2.000	No
883	57.95	3.47	1.53	1.94	0.68	0.432	1.34	0.321	0.87	1.00	2.000	No
884	58.06	3.48	1.53	1.95	0.68	0.431	1.34	0.321	0.87	1.00	2.000	No
885	58.09	3.48	1.53	1.95	0.68	0.431	1.34	0.321	0.87	1.00	2.000	No
886	58.15	3.48	1.53	1.95	0.67	0.431	1.34	0.321	0.87	1.00	2.000	No
887	58.20	3.49	1.54	1.95	0.67	0.431	1.34	0.320	0.87	1.00	2.000	No
888	58.29	3.49	1.54	1.95	0.67	0.430	1.34	0.320	0.87	1.00	2.000	No
889	58.33	3.49	1.54	1.95	0.67	0.430	1.34	0.320	0.87	1.00	2.000	No
890	58.40	3.50	1.54	1.96	0.67	0.430	1.34	0.320	0.87	1.00	2.000	No
891	58.48	3.50	1.54	1.96	0.67	0.430	1.34	0.320	0.87	1.00	2.000	No
892	58.55	3.51	1.55	1.96	0.67	0.429	1.34	0.319	0.87	1.00	2.000	No
893	58.60	3.51	1.55	1.96	0.67	0.429	1.34	0.319	0.87	1.00	2.000	No
894	58.66	3.51	1.55	1.96	0.67	0.429	1.34	0.319	0.87	1.00	2.000	No
895	58.75	3.52	1.55	1.96	0.67	0.429	1.34	0.319	0.87	1.00	2.000	No
896	58.80	3.52	1.55	1.97	0.67	0.428	1.34	0.319	0.87	1.00	2.000	No
897	58.88	3.52	1.56	1.97	0.67	0.428	1.34	0.318	0.87	1.00	2.000	No
898	58.97	3.53	1.56	1.97	0.67	0.428	1.34	0.318	0.87	1.00	2.000	No
899	59.02	3.53	1.56	1.97	0.67	0.427	1.34	0.318	0.87	1.00	2.000	No
900	59.06	3.53	1.56	1.97	0.67	0.427	1.34	0.318	0.87	1.00	2.000	No
901	59.12	3.54	1.56	1.97	0.67	0.427	1.34	0.318	0.87	1.00	2.000	No
902	59.20	3.54	1.57	1.98	0.67	0.427	1.34	0.317	0.87	1.00	2.000	No
903	59.26	3.55	1.57	1.98	0.67	0.427	1.34	0.317	0.87	1.00	2.000	No
904	59.35	3.55	1.57	1.98	0.66	0.426	1.34	0.317	0.87	1.00	2.000	No
905	59.41	3.55	1.57	1.98	0.66	0.426	1.34	0.317	0.87	1.00	2.000	No
906	59.46	3.56	1.57	1.98	0.66	0.426	1.34	0.317	0.87	1.00	2.000	No
907	59.52	3.56	1.58	1.98	0.66	0.426	1.34	0.316	0.87	1.00	2.000	No
908	59.61	3.56	1.58	1.99	0.66	0.425	1.34	0.316	0.87	1.00	2.000	No
909	59.68	3.57	1.58	1.99	0.66	0.425	1.34	0.316	0.87	1.00	2.000	No
910	59.72	3.57	1.58	1.99	0.66	0.425	1.34	0.316	0.86	1.00	2.000	No
911	59.79	3.57	1.58	1.99	0.66	0.424	1.34	0.316	0.86	1.00	2.000	No
912	59.86	3.58	1.59	1.99	0.66	0.424	1.34	0.315	0.86	1.00	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
913	59.91	3.58	1.59	1.99	0.66	0.424	1.34	0.315	0.86	1.00	2.000	No
914	60.01	3.59	1.59	2.00	0.66	0.424	1.34	0.315	0.86	1.00	2.000	Yes
915	60.06	3.59	1.59	2.00	0.66	0.423	1.34	0.315	0.86	1.00	2.000	Yes
916	60.15	3.59	1.60	2.00	0.66	0.423	1.34	0.315	0.86	1.00	2.000	Yes
917	60.19	3.60	1.60	2.00	0.66	0.423	1.34	0.315	0.86	1.00	2.000	Yes
918	60.26	3.60	1.60	2.00	0.66	0.423	1.34	0.314	0.86	1.00	2.000	Yes
919	60.35	3.60	1.60	2.00	0.66	0.422	1.34	0.314	0.86	1.00	2.000	Yes
920	60.40	3.61	1.60	2.00	0.66	0.422	1.34	0.314	0.86	1.00	2.000	Yes
921	60.45	3.61	1.61	2.00	0.66	0.422	1.34	0.314	0.86	1.00	2.000	No
922	60.51	3.61	1.61	2.00	0.66	0.422	1.34	0.314	0.86	1.00	2.000	No

Abbreviations

Depth: Depth from free surface, at which CPT was performed (ft)
σ_v: Total overburden pressure at test point (tsf)
u_0: Water pressure at test point (tsf)
σ_v': Effective overburden pressure based on GWT during earthquake (tsf)
r_d: Nonlinear shear mass factor
CSR: Cyclic Stress Ratio
MSF: Magnitude Scaling Factor
CSR_{eq}: CSR adjusted for M=7.5
K_σ: Effective overburden stress factor
CSR^*: CSR fully adjusted

:: Cyclic Resistance Ratio (CRR) calculation data ::

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
1	0.09	83.15	1.64	0.51	0.50	133.58	1.00	133.58	4.000	No	No	2.00
2	0.15	124.45	1.44	0.42	0.50	199.93	1.00	199.93	4.000	No	No	2.00
3	0.21	164.56	1.32	0.38	0.50	264.38	1.00	264.38	4.000	No	No	2.00
4	0.29	173.53	1.35	0.45	0.50	278.77	1.00	278.77	4.000	No	No	2.00
5	0.34	170.25	1.40	0.54	0.50	273.50	1.00	273.50	4.000	No	No	2.00
6	0.40	184.41	1.41	0.60	0.50	296.24	1.00	296.24	4.000	No	No	2.00
7	0.49	188.56	1.45	0.69	0.50	302.90	1.00	302.90	4.000	No	No	2.00
8	0.55	179.22	1.52	0.83	0.50	287.88	1.00	287.88	4.000	No	No	2.00
9	0.59	162.51	1.62	1.03	0.50	261.04	1.00	261.04	4.000	No	No	2.00
10	0.69	150.33	1.70	1.23	0.52	241.46	1.04	250.82	4.000	No	No	2.00
11	0.74	137.32	1.79	1.46	0.56	220.54	1.10	241.72	4.000	No	No	2.00
12	0.81	123.76	1.87	1.75	0.59	198.76	1.16	231.55	4.000	No	No	2.00
13	0.89	110.59	1.96	2.08	0.62	177.58	1.26	222.96	4.000	No	No	2.00
14	0.94	98.81	2.04	2.39	0.65	158.66	1.36	215.26	4.000	No	No	2.00
15	0.99	93.80	2.07	2.52	0.67	150.60	1.41	212.11	4.000	No	No	2.00
16	1.09	92.09	2.09	2.58	0.67	147.85	1.43	211.59	4.000	No	No	2.00
17	1.14	92.39	2.09	2.62	0.67	148.32	1.44	213.14	4.000	No	No	2.00
18	1.19	97.81	2.06	2.52	0.66	157.02	1.39	218.13	4.000	No	No	2.00
19	1.26	98.76	2.06	2.52	0.66	158.55	1.39	219.88	4.000	No	No	2.00
20	1.34	98.49	2.06	2.54	0.66	158.11	1.39	220.12	4.000	No	No	2.00
21	1.38	98.38	2.06	2.55	0.66	157.93	1.39	220.09	4.000	No	No	2.00
22	1.50	97.02	2.07	2.56	0.66	155.72	1.40	218.45	4.000	No	No	2.00
23	1.53	94.55	2.08	2.59	0.67	151.75	1.42	215.48	4.000	No	No	2.00
24	1.59	90.36	2.10	2.68	0.68	145.01	1.46	212.18	4.000	No	No	2.00
25	1.68	85.92	2.13	2.78	0.69	137.87	1.51	208.71	4.000	No	No	2.00
26	1.72	81.17	2.16	2.90	0.70	130.24	1.57	205.01	4.000	No	No	2.00
27	1.78	75.44	2.20	3.09	0.71	121.02	1.67	202.37	4.000	No	No	2.00
28	1.87	69.69	2.25	3.34	0.73	111.77	1.80	200.88	4.000	No	No	2.00
29	1.93	67.42	2.27	3.45	0.74	108.12	1.86	200.61	4.000	No	No	2.00
30	1.98	64.42	2.29	3.53	0.75	103.29	1.92	198.19	4.000	No	No	2.00
31	2.06	62.68	2.30	3.52	0.75	100.50	1.94	194.72	4.000	No	No	2.00
32	2.13	63.84	2.28	3.45	0.75	102.35	1.90	194.57	4.000	No	No	2.00
33	2.17	67.39	2.25	3.27	0.73	108.06	1.80	194.87	4.000	No	No	2.00
34	2.28	70.26	2.23	3.13	0.72	112.65	1.73	195.27	4.000	No	No	2.00
35	2.32	72.12	2.21	3.04	0.72	115.64	1.69	195.38	4.000	No	No	2.00
36	2.39	71.08	2.21	2.98	0.72	113.95	1.68	191.64	4.000	No	No	2.00
37	2.43	72.10	2.18	2.78	0.71	115.59	1.62	187.09	4.000	No	No	2.00
38	2.52	70.92	2.17	2.64	0.70	113.69	1.59	180.76	4.000	No	No	2.00
39	2.57	69.46	2.16	2.57	0.70	111.34	1.58	176.14	4.000	No	No	2.00
40	2.66	68.27	2.16	2.54	0.70	109.41	1.58	173.38	4.000	No	No	2.00
41	2.69	64.80	2.19	2.61	0.71	103.84	1.64	170.20	4.000	No	No	2.00
42	2.77	59.92	2.23	2.74	0.72	95.98	1.74	166.69	4.000	No	No	2.00
43	2.86	55.44	2.27	2.87	0.74	88.78	1.84	163.61	4.000	No	No	2.00
44	2.92	51.45	2.30	3.03	0.75	82.36	1.96	161.82	4.000	No	No	2.00
45	2.96	48.19	2.34	3.19	0.77	77.12	2.08	160.64	4.000	No	No	2.00
46	3.06	46.08	2.36	3.25	0.77	73.72	2.15	158.82	4.000	No	No	2.00
47	3.11	46.45	2.34	3.13	0.77	74.31	2.10	156.09	4.000	No	No	2.00
48	3.15	48.40	2.30	2.86	0.75	77.45	1.96	152.07	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
49	3.26	54.10	2.22	2.43	0.72	86.58	1.72	148.68	4.000	No	No	2.00
50	3.30	60.61	2.13	2.05	0.69	97.05	1.52	147.19	4.000	No	No	2.00
51	3.37	68.26	2.04	1.71	0.65	109.33	1.36	148.15	4.000	No	No	2.00
52	3.46	73.99	1.98	1.51	0.63	118.52	1.27	150.56	4.000	No	No	2.00
53	3.51	77.79	1.93	1.38	0.61	124.63	1.22	152.41	4.000	No	No	2.00
54	3.56	80.79	1.91	1.33	0.60	129.44	1.20	155.05	4.000	No	No	2.00
55	3.64	81.12	1.91	1.35	0.60	129.96	1.20	156.20	4.000	Yes	No	2.00
56	3.71	79.43	1.94	1.44	0.61	127.24	1.23	156.34	4.000	Yes	No	2.00
57	3.76	75.75	1.99	1.60	0.63	121.33	1.28	155.78	4.000	Yes	No	2.00
58	3.81	67.08	2.07	1.87	0.66	107.39	1.41	151.01	4.000	Yes	No	2.00
59	3.90	57.38	2.17	2.22	0.70	91.80	1.61	147.39	4.000	Yes	No	2.00
60	3.94	47.30	2.30	2.74	0.75	75.59	1.94	146.95	4.000	Yes	No	2.00
61	4.01	40.10	2.39	3.17	0.79	64.02	2.29	146.35	4.000	Yes	No	2.00
62	4.09	35.01	2.46	3.45	0.81	55.83	2.58	144.12	4.000	Yes	No	2.00
63	4.15	30.51	2.52	3.68	0.84	48.60	2.89	140.47	4.000	Yes	No	2.00
64	4.20	27.97	2.55	3.69	0.85	44.51	3.04	135.41	4.000	Yes	No	2.00
65	4.30	25.89	2.57	3.63	0.85	41.16	3.15	129.86	4.000	No	No	2.00
66	4.35	24.02	2.59	3.54	0.86	38.16	3.25	124.00	4.000	No	No	2.00
67	4.41	23.02	2.59	3.44	0.86	36.55	3.28	119.96	4.000	No	No	2.00
68	4.50	22.67	2.58	3.29	0.86	35.97	3.24	116.38	4.000	No	No	2.00
69	4.55	22.29	2.58	3.16	0.86	35.36	3.20	113.01	4.000	No	No	2.00
70	4.60	21.44	2.60	3.20	0.86	33.98	3.30	112.03	4.000	No	No	2.00
71	4.68	20.60	2.62	3.30	0.87	32.64	3.43	112.02	4.000	No	Yes	2.00
72	4.75	19.97	2.64	3.40	0.88	31.62	3.56	112.48	4.000	No	Yes	2.00
73	4.79	19.55	2.65	3.52	0.89	30.93	3.67	113.38	4.000	No	Yes	2.00
74	4.88	19.20	2.67	3.63	0.89	30.36	3.77	114.53	4.000	No	Yes	2.00
75	4.95	18.93	2.68	3.75	0.90	29.93	3.87	115.81	4.000	No	Yes	2.00
76	4.99	18.80	2.69	3.86	0.90	29.71	3.94	117.17	4.000	No	Yes	2.00
77	5.06	18.75	2.70	3.97	0.90	29.62	4.01	118.85	4.000	No	Yes	2.00
78	5.14	18.72	2.71	4.09	0.91	29.57	4.08	120.60	4.000	No	Yes	2.00
79	5.21	18.75	2.72	4.18	0.91	29.61	4.13	122.18	4.000	No	Yes	2.00
80	5.26	18.80	2.72	4.25	0.91	29.69	4.16	123.37	4.000	No	Yes	2.00
81	5.33	18.79	2.73	4.33	0.91	29.66	4.20	124.49	4.000	No	Yes	2.00
82	5.40	18.78	2.73	4.38	0.92	29.64	4.23	125.33	4.000	No	Yes	2.00
83	5.45	18.77	2.74	4.44	0.92	29.62	4.26	126.17	4.000	No	Yes	2.00
84	5.51	18.82	2.74	4.48	0.92	29.70	4.28	126.96	4.000	No	Yes	2.00
85	5.60	18.84	2.74	4.53	0.92	29.73	4.30	127.68	4.000	No	Yes	2.00
86	5.66	18.86	2.74	4.56	0.92	29.74	4.31	128.22	4.000	No	Yes	2.00
87	5.71	18.80	2.75	4.60	0.92	29.64	4.34	128.62	4.000	No	Yes	2.00
88	5.78	18.67	2.75	4.65	0.92	29.43	4.38	128.99	4.000	No	Yes	2.00
89	5.86	18.48	2.76	4.70	0.93	29.12	4.44	129.14	4.000	No	Yes	2.00
90	5.93	18.26	2.76	4.74	0.93	28.76	4.48	128.94	4.000	No	Yes	2.00
91	6.01	18.01	2.77	4.76	0.93	28.35	4.53	128.49	4.000	No	Yes	2.00
92	6.05	17.70	2.78	4.77	0.93	27.84	4.58	127.63	4.000	No	Yes	2.00
93	6.11	17.27	2.78	4.78	0.94	27.15	4.66	126.38	4.000	No	Yes	2.00
94	6.21	16.76	2.80	4.80	0.94	26.33	4.75	124.99	4.000	No	Yes	2.00
95	6.25	16.19	2.81	4.83	0.95	25.40	4.86	123.43	4.000	No	Yes	2.00
96	6.31	15.61	2.82	4.86	0.95	24.47	4.98	121.84	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
97	6.39	15.07	2.84	4.87	0.96	23.59	5.09	120.11	4.000	No	Yes	2.00
98	6.45	14.58	2.85	4.89	0.96	22.80	5.20	118.49	4.000	No	Yes	2.00
99	6.51	14.21	2.85	4.87	0.96	22.19	5.27	116.87	4.000	No	Yes	2.00
100	6.58	13.86	2.86	4.86	0.97	21.62	5.34	115.50	4.000	No	Yes	2.00
101	6.66	13.60	2.87	4.85	0.97	21.20	5.39	114.37	4.000	No	Yes	2.00
102	6.70	13.50	2.87	4.80	0.97	21.04	5.39	113.43	4.000	No	Yes	2.00
103	6.78	13.46	2.87	4.75	0.97	20.96	5.37	112.65	4.000	No	Yes	2.00
104	6.85	13.51	2.86	4.68	0.96	21.03	5.32	111.91	4.000	No	Yes	2.00
105	6.89	13.63	2.85	4.57	0.96	21.23	5.23	111.13	4.000	No	Yes	2.00
106	7.00	13.83	2.84	4.47	0.96	21.54	5.13	110.50	4.000	No	Yes	2.00
107	7.03	14.14	2.82	4.34	0.95	22.03	4.99	109.89	4.000	No	Yes	2.00
108	7.10	14.46	2.81	4.21	0.94	22.55	4.85	109.37	4.000	No	Yes	2.00
109	7.19	14.88	2.79	4.07	0.94	23.20	4.69	108.77	4.000	No	Yes	2.00
110	7.25	15.30	2.77	3.95	0.93	23.88	4.54	108.37	4.000	No	Yes	2.00
111	7.30	15.72	2.76	3.86	0.92	24.55	4.42	108.39	4.000	No	Yes	2.00
112	7.37	16.17	2.74	3.79	0.92	25.27	4.30	108.69	4.000	No	Yes	2.00
113	7.44	16.57	2.73	3.76	0.92	25.90	4.22	109.23	4.000	No	Yes	2.00
114	7.49	16.84	2.72	3.76	0.91	26.33	4.18	109.96	4.000	No	Yes	2.00
115	7.56	17.03	2.72	3.74	0.91	26.64	4.14	110.23	4.000	No	Yes	2.00
116	7.64	17.06	2.72	3.72	0.91	26.68	4.12	110.01	4.000	No	Yes	2.00
117	7.68	16.96	2.72	3.78	0.91	26.52	4.17	110.59	4.000	No	Yes	2.00
118	7.79	16.74	2.73	3.86	0.92	26.14	4.25	111.18	4.000	No	Yes	2.00
119	7.83	16.45	2.75	3.93	0.92	25.67	4.34	111.39	4.000	No	Yes	2.00
120	7.90	16.04	2.76	4.00	0.93	25.01	4.45	111.18	4.000	No	Yes	2.00
121	7.98	15.56	2.77	4.04	0.93	24.23	4.56	110.40	4.000	No	Yes	2.00
122	8.02	15.03	2.79	4.09	0.94	23.37	4.68	109.33	4.000	No	Yes	2.00
123	8.09	14.64	2.80	4.08	0.94	22.74	4.75	108.03	4.000	No	Yes	2.00
124	8.15	14.30	2.80	4.09	0.94	22.19	4.83	107.10	4.000	No	Yes	2.00
125	8.23	14.13	2.81	4.11	0.95	21.91	4.87	106.69	4.000	No	Yes	2.00
126	8.29	14.15	2.80	4.02	0.94	21.94	4.81	105.61	4.000	No	Yes	2.00
127	8.34	14.26	2.79	3.91	0.94	22.11	4.72	104.46	4.000	No	Yes	2.00
128	8.41	14.46	2.78	3.80	0.93	22.43	4.62	103.67	4.000	No	Yes	2.00
129	8.48	14.80	2.76	3.69	0.93	22.96	4.49	103.11	4.000	No	Yes	2.00
130	8.55	15.24	2.75	3.59	0.92	23.66	4.35	102.91	4.000	No	Yes	2.00
131	8.60	15.79	2.73	3.49	0.91	24.55	4.19	102.94	4.000	No	Yes	2.00
132	8.66	16.33	2.71	3.41	0.91	25.40	4.06	103.10	4.000	No	Yes	2.00
133	8.74	16.89	2.69	3.35	0.90	26.31	3.94	103.55	4.000	No	Yes	2.00
134	8.83	17.43	2.68	3.33	0.90	27.16	3.85	104.55	4.000	No	Yes	2.00
135	8.90	17.91	2.67	3.33	0.89	27.92	3.79	105.79	4.000	No	Yes	2.00
136	8.94	18.32	2.67	3.35	0.89	28.58	3.75	107.17	4.000	No	Yes	2.00
137	9.01	18.66	2.66	3.40	0.89	29.11	3.74	108.78	4.000	No	Yes	2.00
138	9.09	18.90	2.66	3.47	0.89	29.50	3.74	110.44	4.000	No	Yes	2.00
139	9.15	19.06	2.67	3.55	0.89	29.75	3.77	112.13	4.000	No	Yes	2.00
140	9.20	19.18	2.67	3.64	0.89	29.93	3.81	113.94	4.000	No	Yes	2.00
141	9.29	19.30	2.68	3.74	0.90	30.11	3.85	115.92	4.000	No	Yes	2.00
142	9.35	19.43	2.68	3.84	0.90	30.33	3.89	117.85	4.000	No	Yes	2.00
143	9.39	19.54	2.69	3.90	0.90	30.50	3.91	119.21	4.000	No	Yes	2.00
144	9.45	19.66	2.69	3.94	0.90	30.68	3.92	120.17	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
145	9.55	19.97	2.68	3.94	0.90	31.17	3.88	120.89	4.000	No	Yes	2.00
146	9.64	20.38	2.67	3.91	0.89	31.83	3.81	121.43	4.000	No	Yes	2.00
147	9.65	20.91	2.66	3.86	0.89	32.67	3.73	121.97	4.000	No	Yes	2.00
148	9.73	21.47	2.65	3.81	0.88	33.57	3.65	122.48	4.000	No	Yes	2.00
149	9.79	21.98	2.64	3.78	0.88	34.31	3.59	123.03	4.000	No	Yes	2.00
150	9.84	22.46	2.63	3.73	0.88	34.86	3.53	122.99	4.000	No	Yes	2.00
151	9.91	22.88	2.62	3.68	0.88	35.24	3.48	122.67	4.000	No	Yes	2.00
152	9.99	23.25	2.62	3.64	0.87	35.53	3.44	122.26	4.000	No	Yes	2.00
153	10.08	23.63	2.61	3.58	0.87	35.78	3.40	121.63	4.000	No	Yes	2.00
154	10.14	23.82	2.61	3.56	0.87	35.88	3.38	121.31	4.000	No	Yes	2.00
155	10.19	23.87	2.61	3.54	0.87	35.79	3.38	120.88	4.000	No	Yes	2.00
156	10.25	23.88	2.61	3.52	0.87	35.62	3.38	120.28	4.000	No	Yes	2.00
157	10.34	23.79	2.61	3.52	0.87	35.24	3.40	119.75	4.000	No	Yes	2.00
158	10.38	23.82	2.61	3.50	0.87	35.15	3.39	119.11	4.000	No	Yes	2.00
159	10.44	23.92	2.61	3.45	0.87	35.10	3.37	118.25	4.000	No	Yes	2.00
160	10.52	23.94	2.60	3.41	0.87	34.89	3.36	117.11	4.000	No	Yes	2.00
161	10.59	23.96	2.60	3.37	0.87	34.70	3.35	116.11	4.000	No	Yes	2.00
162	10.63	23.88	2.60	3.36	0.87	34.48	3.35	115.67	4.000	No	Yes	2.00
163	10.70	23.75	2.61	3.35	0.87	34.11	3.37	115.08	4.000	No	Yes	2.00
164	10.78	23.71	2.61	3.34	0.87	33.84	3.38	114.48	4.000	No	Yes	2.00
165	10.87	24.05	2.60	3.30	0.87	34.05	3.35	114.07	4.000	No	Yes	2.00
166	10.93	24.68	2.59	3.22	0.86	34.72	3.27	113.43	0.216	No	No	0.75
167	10.97	25.09	2.58	3.19	0.86	35.14	3.22	113.33	0.215	No	No	0.75
168	11.03	25.34	2.58	3.21	0.86	35.34	3.23	114.00	0.218	No	No	0.76
169	11.12	25.57	2.59	3.26	0.86	35.43	3.25	115.11	0.222	No	No	0.77
170	11.16	26.10	2.58	3.28	0.86	36.05	3.22	116.20	0.226	No	No	0.78
171	11.23	26.69	2.58	3.28	0.86	36.65	3.20	117.14	0.229	No	No	0.79
172	11.31	27.32	2.57	3.30	0.86	37.28	3.17	118.24	0.234	No	No	0.80
173	11.37	28.14	2.57	3.30	0.85	38.20	3.13	119.49	0.239	No	No	0.82
174	11.44	28.65	2.57	3.34	0.85	38.70	3.12	120.91	0.244	No	No	0.84
175	11.51	28.96	2.57	3.40	0.85	38.94	3.14	122.45	0.251	No	No	0.86
176	11.56	29.46	2.57	3.42	0.85	39.47	3.13	123.56	0.255	No	No	0.87
177	11.63	29.97	2.56	3.43	0.85	39.93	3.11	124.20	0.258	No	No	0.88
178	11.71	30.37	2.56	3.43	0.85	40.22	3.10	124.71	0.260	No	No	0.88
179	11.76	30.29	2.57	3.48	0.85	39.99	3.13	125.36	0.263	No	No	0.89
180	11.83	30.13	2.57	3.52	0.86	39.61	3.17	125.68	0.265	No	No	0.89
181	11.91	29.90	2.58	3.56	0.86	39.12	3.22	125.79	0.265	No	No	0.89
182	11.94	29.36	2.59	3.62	0.86	38.36	3.28	125.85	0.265	No	No	0.89
183	12.05	28.72	2.60	3.66	0.87	37.35	3.35	125.25	4.000	No	Yes	2.00
184	12.10	28.18	2.61	3.69	0.87	36.60	3.41	124.65	4.000	No	Yes	2.00
185	12.14	27.59	2.62	3.72	0.87	35.82	3.46	124.10	4.000	No	Yes	2.00
186	12.25	27.11	2.63	3.74	0.88	35.08	3.52	123.36	4.000	No	Yes	2.00
187	12.29	26.81	2.63	3.73	0.88	34.65	3.54	122.58	4.000	No	Yes	2.00
188	12.35	26.66	2.64	3.72	0.88	34.38	3.55	122.06	4.000	No	Yes	2.00
189	12.44	26.59	2.64	3.70	0.88	34.17	3.55	121.34	4.000	No	Yes	2.00
190	12.49	26.67	2.63	3.64	0.88	34.20	3.52	120.41	4.000	No	Yes	2.00
191	12.55	26.82	2.62	3.58	0.88	34.29	3.48	119.34	4.000	No	Yes	2.00
192	12.61	26.84	2.62	3.51	0.87	34.21	3.45	118.04	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
193	12.70	26.47	2.62	3.49	0.88	33.64	3.47	116.91	4.000	No	Yes	2.00
194	12.75	25.93	2.63	3.48	0.88	32.91	3.51	115.62	4.000	No	Yes	2.00
195	12.81	25.23	2.64	3.44	0.88	31.96	3.56	113.61	4.000	No	Yes	2.00
196	12.89	24.43	2.64	3.38	0.88	30.85	3.60	110.95	4.000	No	Yes	2.00
197	12.94	23.55	2.65	3.30	0.88	29.68	3.63	107.89	4.000	No	Yes	2.00
198	12.99	22.55	2.66	3.24	0.89	28.37	3.70	105.01	4.000	No	Yes	2.00
199	13.08	21.42	2.67	3.21	0.89	26.86	3.81	102.27	4.000	No	Yes	2.00
200	13.15	20.17	2.69	3.20	0.90	25.24	3.94	99.55	4.000	No	Yes	2.00
201	13.20	18.94	2.71	3.19	0.91	23.67	4.09	96.93	4.000	No	Yes	2.00
202	13.27	17.94	2.73	3.13	0.91	22.36	4.20	94.01	4.000	No	Yes	2.00
203	13.32	17.08	2.74	3.06	0.92	21.23	4.29	91.09	4.000	No	Yes	2.00
204	13.39	16.29	2.75	3.02	0.92	20.19	4.39	88.71	4.000	No	Yes	2.00
205	13.48	15.57	2.77	3.01	0.93	19.24	4.52	87.03	4.000	No	Yes	2.00
206	13.54	14.85	2.79	3.04	0.94	18.31	4.68	85.67	4.000	No	Yes	2.00
207	13.59	14.26	2.80	3.05	0.94	17.54	4.81	84.40	4.000	No	Yes	2.00
208	13.65	13.72	2.82	3.05	0.95	16.84	4.94	83.16	4.000	No	Yes	2.00
209	13.74	13.35	2.83	3.04	0.95	16.32	5.02	81.98	4.000	No	Yes	2.00
210	13.80	13.07	2.83	2.99	0.95	15.93	5.06	80.63	4.000	No	Yes	2.00
211	13.89	12.89	2.83	2.92	0.95	15.65	5.06	79.16	4.000	No	Yes	2.00
212	13.93	12.67	2.84	2.92	0.96	15.36	5.11	78.57	4.000	No	Yes	2.00
213	13.99	12.47	2.85	3.01	0.96	15.09	5.24	79.11	4.000	No	Yes	2.00
214	14.07	12.36	2.86	3.09	0.97	14.93	5.35	79.81	4.000	No	Yes	2.00
215	14.12	12.41	2.87	3.15	0.97	14.97	5.38	80.54	4.000	No	Yes	2.00
216	14.18	12.84	2.85	3.12	0.96	15.48	5.25	81.24	4.000	No	Yes	2.00
217	14.26	13.66	2.82	3.03	0.95	16.43	5.00	82.12	4.000	No	Yes	2.00
218	14.34	14.47	2.80	2.98	0.94	17.37	4.79	83.28	4.000	No	Yes	2.00
219	14.38	15.06	2.79	3.06	0.94	18.09	4.73	85.64	4.000	No	Yes	2.00
220	14.47	15.53	2.80	3.20	0.94	18.63	4.75	88.46	4.000	No	Yes	2.00
221	14.53	16.03	2.79	3.29	0.94	19.23	4.72	90.78	4.000	No	Yes	2.00
222	14.57	16.61	2.78	3.32	0.94	19.90	4.64	92.32	4.000	No	Yes	2.00
223	14.64	17.04	2.78	3.34	0.93	20.39	4.59	93.50	4.000	No	Yes	2.00
224	14.72	17.40	2.77	3.36	0.93	20.77	4.55	94.50	4.000	No	Yes	2.00
225	14.80	17.27	2.78	3.44	0.94	20.58	4.63	95.26	4.000	No	Yes	2.00
226	14.83	16.85	2.80	3.56	0.94	20.07	4.78	95.90	4.000	No	Yes	2.00
227	14.92	16.39	2.82	3.70	0.95	19.48	4.95	96.48	4.000	No	Yes	2.00
228	14.97	16.24	2.83	3.75	0.95	19.28	5.02	96.80	4.000	No	Yes	2.00
229	15.06	16.27	2.83	3.80	0.95	19.26	5.06	97.42	4.000	No	Yes	2.00
230	15.10	16.43	2.83	3.88	0.95	19.44	5.08	98.73	4.000	No	Yes	2.00
231	15.17	16.88	2.83	3.95	0.95	19.94	5.05	100.69	4.000	No	Yes	2.00
232	15.25	17.82	2.82	3.98	0.95	21.02	4.91	103.31	4.000	No	Yes	2.00
233	15.31	19.04	2.79	3.99	0.94	22.44	4.73	106.25	4.000	No	Yes	2.00
234	15.37	20.79	2.76	3.97	0.93	24.48	4.48	109.75	4.000	No	Yes	2.00
235	15.44	22.91	2.73	3.94	0.92	26.92	4.22	113.74	4.000	No	Yes	2.00
236	15.51	25.24	2.70	3.90	0.90	29.60	3.98	117.67	4.000	No	Yes	2.00
237	15.56	27.89	2.66	3.85	0.89	32.64	3.73	121.72	4.000	No	Yes	2.00
238	15.63	30.62	2.63	3.85	0.88	35.75	3.53	126.33	4.000	No	Yes	2.00
239	15.71	33.36	2.61	3.83	0.87	38.84	3.36	130.50	4.000	No	Yes	2.00
240	15.76	35.88	2.58	3.82	0.86	41.68	3.22	134.26	0.305	No	No	0.92

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
241	15.82	38.00	2.56	3.81	0.85	44.04	3.12	137.37	0.321	No	No	0.96
242	15.90	39.72	2.55	3.82	0.85	45.92	3.05	140.10	0.336	No	No	1.00
243	15.95	40.95	2.55	3.85	0.85	47.26	3.01	142.38	0.348	No	No	1.04
244	16.01	42.08	2.54	3.84	0.84	48.46	2.97	143.78	0.356	No	No	1.06
245	16.10	43.69	2.52	3.77	0.84	50.12	2.88	144.51	4.000	Yes	No	2.00
246	16.16	45.39	2.50	3.68	0.83	51.93	2.79	144.76	4.000	Yes	No	2.00
247	16.21	47.82	2.47	3.52	0.82	54.52	2.64	144.17	4.000	Yes	No	2.00
248	16.29	50.73	2.44	3.35	0.81	57.59	2.49	143.67	4.000	Yes	No	2.00
249	16.36	53.65	2.41	3.20	0.79	60.67	2.37	143.61	4.000	Yes	No	2.00
250	16.41	55.97	2.39	3.13	0.79	63.12	2.29	144.46	4.000	Yes	No	2.00
251	16.49	57.93	2.38	3.09	0.78	65.13	2.24	145.59	0.367	No	No	1.09
252	16.55	58.97	2.38	3.11	0.78	66.18	2.22	147.05	0.376	No	No	1.11
253	16.60	58.73	2.39	3.18	0.78	65.85	2.26	148.63	0.385	No	No	1.14
254	16.70	57.58	2.40	3.30	0.79	64.45	2.33	150.28	4.000	Yes	No	2.00
255	16.74	55.54	2.43	3.43	0.80	62.18	2.43	150.89	4.000	Yes	No	2.00
256	16.80	52.24	2.45	3.50	0.81	58.44	2.54	148.41	4.000	Yes	No	2.00
257	16.89	48.21	2.49	3.62	0.82	53.86	2.71	145.75	4.000	Yes	No	2.00
258	16.93	43.70	2.53	3.78	0.84	48.84	2.93	142.95	4.000	Yes	No	2.00
259	17.00	39.30	2.57	3.91	0.86	43.87	3.17	139.12	4.000	Yes	No	2.00
260	17.09	35.13	2.62	4.01	0.87	39.12	3.43	134.22	4.000	Yes	Yes	2.00
261	17.14	31.91	2.65	3.97	0.88	35.46	3.61	128.18	4.000	Yes	Yes	2.00
262	17.20	29.62	2.66	3.82	0.89	32.81	3.70	121.48	4.000	No	Yes	2.00
263	17.28	27.32	2.67	3.65	0.89	30.13	3.80	114.37	4.000	No	Yes	2.00
264	17.34	25.35	2.69	3.51	0.90	27.85	3.90	108.56	4.000	No	Yes	2.00
265	17.41	23.75	2.72	3.59	0.91	26.02	4.11	106.90	4.000	No	Yes	2.00
266	17.48	22.28	2.74	3.68	0.92	24.34	4.33	105.33	4.000	No	Yes	2.00
267	17.56	21.40	2.76	3.71	0.93	23.31	4.46	103.98	4.000	No	Yes	2.00
268	17.62	21.30	2.76	3.68	0.93	23.15	4.46	103.34	4.000	No	Yes	2.00
269	17.67	21.90	2.75	3.71	0.92	23.78	4.41	104.80	4.000	Yes	Yes	2.00
270	17.72	23.43	2.73	3.70	0.92	25.45	4.23	107.56	4.000	Yes	Yes	2.00
271	17.78	25.81	2.69	3.62	0.90	28.02	3.95	110.64	4.000	Yes	Yes	2.00
272	17.87	29.76	2.63	3.41	0.88	32.25	3.52	113.53	4.000	Yes	Yes	2.00
273	17.94	34.49	2.57	3.24	0.85	37.30	3.14	117.09	4.000	Yes	No	2.00
274	18.01	39.36	2.51	3.10	0.83	42.48	2.84	120.59	4.000	Yes	No	2.00
275	18.06	44.61	2.46	2.96	0.81	48.05	2.58	124.00	4.000	Yes	No	2.00
276	18.12	49.40	2.42	2.87	0.80	53.08	2.40	127.40	4.000	Yes	No	2.00
277	18.21	53.23	2.39	2.83	0.79	57.04	2.29	130.57	0.287	No	No	0.82
278	18.25	55.37	2.38	2.79	0.78	59.24	2.23	131.91	0.293	No	No	0.84
279	18.31	55.54	2.38	2.79	0.78	59.32	2.22	131.93	0.294	No	No	0.84
280	18.40	54.39	2.39	2.80	0.78	57.96	2.26	130.84	4.000	Yes	No	2.00
281	18.44	51.05	2.42	2.89	0.80	54.37	2.37	129.13	4.000	Yes	No	2.00
282	18.51	46.53	2.46	2.99	0.81	49.50	2.55	126.35	4.000	Yes	No	2.00
283	18.58	42.29	2.50	3.09	0.83	44.90	2.75	123.40	4.000	Yes	No	2.00
284	18.64	37.54	2.55	3.26	0.85	39.79	3.03	120.70	4.000	Yes	No	2.00
285	18.71	33.19	2.60	3.42	0.87	35.09	3.35	117.60	4.000	Yes	Yes	2.00
286	18.80	29.50	2.66	3.57	0.89	31.08	3.69	114.60	4.000	Yes	Yes	2.00
287	18.86	27.07	2.70	3.76	0.90	28.44	3.99	113.53	4.000	Yes	Yes	2.00
288	18.91	26.18	2.72	3.92	0.91	27.47	4.17	114.45	4.000	Yes	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
289	18.98	26.23	2.73	4.03	0.92	27.48	4.23	116.18	4.000	Yes	Yes	2.00
290	19.05	28.55	2.70	3.92	0.90	29.89	3.96	118.43	4.000	Yes	Yes	2.00
291	19.10	32.75	2.64	3.73	0.88	34.30	3.56	122.20	4.000	Yes	Yes	2.00
292	19.20	36.95	2.59	3.62	0.86	38.62	3.27	126.30	4.000	Yes	No	2.00
293	19.23	41.98	2.54	3.50	0.84	43.88	2.98	130.67	4.000	Yes	No	2.00
294	19.30	47.70	2.49	3.37	0.82	49.78	2.72	135.29	4.000	Yes	No	2.00
295	19.39	53.84	2.44	3.26	0.81	56.05	2.49	139.78	4.000	Yes	No	2.00
296	19.43	60.95	2.39	3.10	0.79	63.36	2.27	144.00	4.000	Yes	No	2.00
297	19.50	67.80	2.34	2.97	0.77	70.30	2.10	147.71	4.000	Yes	No	2.00
298	19.57	74.91	2.30	2.86	0.75	77.48	1.96	151.93	4.000	Yes	No	2.00
299	19.63	80.68	2.28	2.81	0.74	83.29	1.88	156.25	4.000	Yes	No	2.00
300	19.70	84.48	2.26	2.81	0.74	87.05	1.84	160.14	0.462	No	No	1.29
301	19.77	87.46	2.26	2.85	0.74	89.97	1.82	163.96	0.490	No	No	1.37
302	19.84	88.72	2.25	2.77	0.73	91.06	1.79	162.94	0.482	No	No	1.35
303	19.90	88.05	2.25	2.80	0.73	90.24	1.81	162.93	0.482	No	No	1.35
304	19.99	86.33	2.27	2.86	0.74	88.30	1.84	162.87	4.000	Yes	No	2.00
305	20.02	82.81	2.29	3.01	0.75	84.69	1.93	163.44	4.000	Yes	No	2.00
306	20.09	77.91	2.33	3.21	0.76	79.61	2.06	163.98	4.000	Yes	No	2.00
307	20.19	72.20	2.38	3.46	0.78	73.64	2.23	164.40	4.000	Yes	No	2.00
308	20.21	66.31	2.43	3.74	0.80	67.65	2.44	164.76	4.000	Yes	No	2.00
309	20.29	60.80	2.48	4.00	0.82	61.90	2.66	164.43	4.000	Yes	No	2.00
310	20.38	55.60	2.53	4.28	0.84	56.47	2.90	163.92	4.000	Yes	No	2.00
311	20.42	51.83	2.58	4.71	0.86	52.62	3.19	167.91	4.000	Yes	No	2.00
312	20.52	49.59	2.61	4.95	0.87	50.20	3.37	169.09	4.000	No	Yes	2.00
313	20.55	48.85	2.62	5.04	0.87	49.41	3.44	169.77	4.000	No	Yes	2.00
314	20.62	50.23	2.60	4.87	0.87	50.69	3.32	168.19	4.000	Yes	No	2.00
315	20.68	54.00	2.55	4.50	0.85	54.40	3.05	165.95	4.000	Yes	No	2.00
316	20.75	58.46	2.51	4.16	0.83	58.77	2.79	164.25	4.000	Yes	No	2.00
317	20.81	64.06	2.45	3.83	0.81	64.27	2.54	163.09	4.000	Yes	No	2.00
318	20.90	70.17	2.40	3.53	0.79	70.22	2.31	162.34	4.000	Yes	No	2.00
319	20.96	76.88	2.35	3.25	0.77	76.78	2.11	162.12	4.000	Yes	No	2.00
320	21.01	83.50	2.30	3.03	0.75	83.25	1.95	162.71	4.000	Yes	No	2.00
321	21.09	89.88	2.26	2.86	0.74	89.40	1.83	163.78	4.000	Yes	No	2.00
322	21.15	95.34	2.23	2.72	0.72	94.66	1.74	164.75	4.000	Yes	No	2.00
323	21.21	99.28	2.21	2.64	0.72	98.41	1.69	165.97	4.000	Yes	No	2.00
324	21.30	101.54	2.20	2.60	0.71	100.41	1.66	166.66	0.511	No	No	1.40
325	21.36	102.98	2.19	2.57	0.71	101.69	1.64	166.99	0.513	No	No	1.41
326	21.40	103.15	2.19	2.57	0.71	101.76	1.64	167.23	0.515	No	No	1.41
327	21.49	102.24	2.20	2.63	0.71	100.65	1.67	167.75	0.519	No	No	1.42
328	21.56	100.58	2.22	2.71	0.72	98.87	1.71	168.66	4.000	Yes	No	2.00
329	21.60	98.24	2.24	2.84	0.73	96.51	1.76	170.27	4.000	Yes	No	2.00
330	21.66	95.65	2.27	3.03	0.74	93.85	1.84	173.11	4.000	Yes	No	2.00
331	21.75	92.97	2.30	3.23	0.75	91.05	1.94	176.31	4.000	Yes	No	2.00
332	21.80	90.34	2.33	3.44	0.76	88.38	2.03	179.61	4.000	Yes	No	2.00
333	21.85	86.54	2.36	3.65	0.77	84.57	2.15	181.57	4.000	Yes	No	2.00
334	21.95	82.45	2.39	3.87	0.79	80.35	2.27	182.77	4.000	Yes	No	2.00
335	21.99	77.84	2.42	4.06	0.80	75.75	2.41	182.63	4.000	Yes	No	2.00
336	22.05	73.33	2.45	4.17	0.81	71.22	2.53	179.99	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
337	22.14	68.64	2.47	4.21	0.82	66.45	2.63	175.01	0.579	No	No	1.58
338	22.19	64.12	2.49	4.20	0.82	61.92	2.73	169.22	0.531	No	No	1.45
339	22.26	59.36	2.51	4.14	0.83	57.14	2.83	161.62	0.473	No	No	1.29
340	22.35	54.56	2.53	4.05	0.84	52.30	2.93	153.37	0.415	No	No	1.13
341	22.44	49.73	2.55	3.95	0.85	47.45	3.05	144.80	0.362	No	No	0.99
342	22.45	46.31	2.57	3.82	0.85	44.10	3.12	137.69	0.323	No	No	0.88
343	22.54	43.33	2.58	3.71	0.86	41.08	3.20	131.39	0.291	No	No	0.79
344	22.58	41.17	2.59	3.62	0.86	38.93	3.26	126.75	0.269	No	No	0.73
345	22.65	39.90	2.60	3.61	0.86	37.63	3.31	124.71	0.260	No	No	0.71
346	22.73	39.60	2.60	3.66	0.87	37.26	3.36	125.06	4.000	No	Yes	2.00
347	22.79	39.96	2.61	3.69	0.87	37.55	3.36	126.08	4.000	No	Yes	2.00
348	22.85	41.77	2.60	3.76	0.86	39.25	3.31	129.80	0.283	No	No	0.77
349	22.93	44.52	2.59	3.92	0.86	41.82	3.27	136.54	0.317	No	No	0.86
350	22.99	48.25	2.58	4.08	0.86	45.36	3.19	144.50	0.361	No	No	0.98
351	23.04	53.17	2.55	4.12	0.85	50.03	3.03	151.83	0.405	No	No	1.10
352	23.12	57.97	2.53	4.14	0.84	54.54	2.90	158.22	0.448	No	No	1.21
353	23.19	61.76	2.51	4.14	0.83	58.07	2.81	162.95	0.482	No	No	1.30
354	23.27	64.98	2.49	4.14	0.82	61.03	2.73	166.65	0.510	No	No	1.38
355	23.30	67.76	2.48	4.12	0.82	63.65	2.66	169.44	0.532	No	No	1.44
356	23.38	70.90	2.46	4.05	0.81	66.51	2.58	171.29	0.547	No	No	1.48
357	23.47	73.27	2.44	3.95	0.81	68.60	2.50	171.31	0.548	No	No	1.47
358	23.50	74.99	2.42	3.78	0.80	70.18	2.41	168.91	0.528	No	No	1.42
359	23.58	75.51	2.41	3.63	0.79	70.53	2.34	165.30	0.500	No	No	1.35
360	23.66	74.38	2.41	3.55	0.79	69.31	2.34	161.96	0.475	No	No	1.28
361	23.69	73.15	2.41	3.50	0.79	68.09	2.34	159.30	0.456	No	No	1.23
362	23.77	72.69	2.41	3.49	0.79	67.52	2.34	158.28	0.449	No	No	1.21
363	23.84	72.77	2.41	3.47	0.79	67.48	2.34	157.74	0.445	No	No	1.20
364	23.92	72.82	2.41	3.48	0.79	67.39	2.34	157.99	0.447	No	No	1.20
365	23.97	71.99	2.42	3.53	0.80	66.52	2.38	158.38	0.449	No	No	1.21
366	24.06	70.72	2.43	3.61	0.80	65.17	2.44	158.89	0.453	No	No	1.21
367	24.12	69.26	2.45	3.73	0.81	63.69	2.51	159.96	0.461	No	No	1.23
368	24.17	67.92	2.46	3.83	0.81	62.35	2.58	160.90	0.467	No	No	1.25
369	24.23	66.21	2.48	3.91	0.82	60.65	2.65	160.73	0.466	No	No	1.25
370	24.31	64.27	2.49	3.98	0.82	58.71	2.73	160.00	0.461	No	No	1.23
371	24.36	61.66	2.51	4.05	0.83	56.19	2.82	158.28	0.449	No	No	1.20
372	24.42	58.14	2.53	4.12	0.84	52.82	2.95	155.55	0.430	No	No	1.15
373	24.51	54.24	2.56	4.21	0.85	49.05	3.10	152.30	0.409	No	No	1.09
374	24.54	50.19	2.59	4.27	0.86	45.25	3.27	148.14	0.382	No	No	1.02
375	24.62	45.92	2.62	4.29	0.87	41.19	3.46	142.60	4.000	No	Yes	2.00
376	24.71	41.38	2.66	4.30	0.89	36.87	3.69	136.14	4.000	No	Yes	2.00
377	24.74	37.02	2.69	4.29	0.90	32.81	3.94	129.34	4.000	No	Yes	2.00
378	24.81	33.35	2.72	4.24	0.91	29.36	4.18	122.62	4.000	No	Yes	2.00
379	24.89	30.15	2.75	4.14	0.92	26.35	4.39	115.71	4.000	No	Yes	2.00
380	24.96	27.79	2.77	3.96	0.93	24.12	4.52	109.01	4.000	No	Yes	2.00
381	25.01	26.12	2.78	3.76	0.93	22.57	4.58	103.36	4.000	No	Yes	2.00
382	25.10	24.74	2.78	3.56	0.93	21.25	4.62	98.16	4.000	No	Yes	2.00
383	25.14	23.57	2.79	3.43	0.94	20.15	4.68	94.33	4.000	No	Yes	2.00
384	25.21	22.70	2.80	3.37	0.94	19.32	4.76	92.00	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
385	25.30	22.17	2.80	3.32	0.94	18.80	4.80	90.31	4.000	No	Yes	2.00
386	25.34	21.82	2.80	3.25	0.94	18.46	4.81	88.71	4.000	No	Yes	2.00
387	25.41	21.76	2.80	3.17	0.94	18.37	4.76	87.53	4.000	No	Yes	2.00
388	25.50	21.77	2.79	3.10	0.94	18.34	4.72	86.53	4.000	No	Yes	2.00
389	25.55	21.93	2.78	3.03	0.94	18.47	4.65	85.93	4.000	No	Yes	2.00
390	25.60	22.09	2.78	2.98	0.93	18.59	4.59	85.40	4.000	No	Yes	2.00
391	25.70	22.29	2.77	2.90	0.93	18.73	4.52	84.60	4.000	No	Yes	2.00
392	25.75	22.50	2.76	2.81	0.93	18.90	4.43	83.67	4.000	No	Yes	2.00
393	25.80	22.79	2.74	2.67	0.92	19.15	4.28	82.04	4.000	No	Yes	2.00
394	25.89	23.08	2.72	2.54	0.91	19.37	4.15	80.44	4.000	No	Yes	2.00
395	25.95	23.34	2.71	2.43	0.91	19.59	4.04	79.07	4.000	No	Yes	2.00
396	25.99	23.77	2.69	2.31	0.90	19.96	3.90	77.81	4.000	No	Yes	2.00
397	26.06	24.08	2.67	2.23	0.89	20.21	3.80	76.79	4.000	No	Yes	2.00
398	26.15	24.25	2.66	2.16	0.89	20.33	3.73	75.89	4.000	No	Yes	2.00
399	26.19	24.34	2.66	2.12	0.89	20.39	3.69	75.28	4.000	No	Yes	2.00
400	26.25	24.39	2.66	2.11	0.89	20.41	3.69	75.23	4.000	No	Yes	2.00
401	26.34	24.31	2.66	2.16	0.89	20.30	3.73	75.77	4.000	No	Yes	2.00
402	26.38	24.05	2.68	2.26	0.90	20.04	3.85	77.18	4.000	No	Yes	2.00
403	26.45	23.79	2.70	2.37	0.90	19.77	3.97	78.40	4.000	No	Yes	2.00
404	26.52	23.52	2.71	2.46	0.91	19.49	4.07	79.37	4.000	No	Yes	2.00
405	26.61	23.07	2.73	2.55	0.91	19.04	4.21	80.09	4.000	No	Yes	2.00
406	26.67	22.67	2.74	2.60	0.92	18.66	4.30	80.27	4.000	No	Yes	2.00
407	26.72	22.32	2.75	2.64	0.92	18.31	4.38	80.21	4.000	No	Yes	2.00
408	26.82	21.99	2.76	2.64	0.93	17.98	4.43	79.73	4.000	No	Yes	2.00
409	26.86	21.65	2.76	2.61	0.93	17.67	4.46	78.75	4.000	No	Yes	2.00
410	26.94	21.41	2.76	2.52	0.93	17.42	4.43	77.07	4.000	No	Yes	2.00
411	26.98	21.28	2.75	2.40	0.92	17.29	4.35	75.19	4.000	No	Yes	2.00
412	27.06	21.19	2.74	2.28	0.92	17.19	4.27	73.31	4.000	No	Yes	2.00
413	27.10	21.17	2.72	2.16	0.91	17.16	4.16	71.47	4.000	No	Yes	2.00
414	27.17	21.23	2.71	2.03	0.91	17.20	4.05	69.64	4.000	No	Yes	2.00
415	27.26	21.42	2.69	1.94	0.90	17.34	3.94	68.32	4.000	No	Yes	2.00
416	27.31	21.67	2.68	1.86	0.90	17.54	3.84	67.44	4.000	No	Yes	2.00
417	27.39	21.94	2.67	1.82	0.89	17.76	3.77	67.05	4.000	No	Yes	2.00
418	27.44	22.25	2.66	1.79	0.89	18.02	3.71	66.93	4.000	No	Yes	2.00
419	27.51	22.57	2.65	1.79	0.89	18.27	3.68	67.24	4.000	No	Yes	2.00
420	27.58	22.83	2.65	1.81	0.89	18.47	3.67	67.74	4.000	No	Yes	2.00
421	27.63	23.05	2.65	1.83	0.89	18.64	3.66	68.26	4.000	No	Yes	2.00
422	27.71	23.11	2.66	1.86	0.89	18.67	3.69	68.80	4.000	No	Yes	2.00
423	27.79	23.06	2.66	1.91	0.89	18.58	3.74	69.46	4.000	No	Yes	2.00
424	27.86	22.89	2.67	1.95	0.89	18.40	3.80	69.90	4.000	No	Yes	2.00
425	27.89	22.61	2.68	1.99	0.90	18.14	3.88	70.31	4.000	No	Yes	2.00
426	27.96	22.26	2.70	2.05	0.90	17.80	3.97	70.72	4.000	No	Yes	2.00
427	28.05	21.90	2.71	2.13	0.91	17.44	4.10	71.46	4.000	No	Yes	2.00
428	28.09	21.54	2.73	2.25	0.92	17.11	4.25	72.69	4.000	No	Yes	2.00
429	28.16	21.20	2.75	2.38	0.92	16.78	4.41	74.05	4.000	No	Yes	2.00
430	28.23	20.88	2.78	2.51	0.93	16.46	4.58	75.37	4.000	No	Yes	2.00
431	28.29	20.64	2.79	2.64	0.94	16.22	4.73	76.64	4.000	No	Yes	2.00
432	28.35	20.47	2.81	2.75	0.94	16.04	4.85	77.72	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
433	28.44	20.36	2.82	2.84	0.95	15.91	4.94	78.67	4.000	No	Yes	2.00
434	28.50	20.26	2.83	2.93	0.95	15.79	5.04	79.55	4.000	No	Yes	2.00
435	28.55	20.24	2.84	2.99	0.96	15.75	5.10	80.26	4.000	No	Yes	2.00
436	28.64	20.28	2.84	3.02	0.96	15.76	5.12	80.62	4.000	No	Yes	2.00
437	28.69	20.47	2.83	3.01	0.96	15.90	5.08	80.83	4.000	No	Yes	2.00
438	28.75	20.92	2.82	2.94	0.95	16.26	4.96	80.68	4.000	No	Yes	2.00
439	28.82	21.52	2.80	2.85	0.94	16.76	4.80	80.40	4.000	No	Yes	2.00
440	28.89	22.35	2.79	2.82	0.94	17.44	4.66	81.27	4.000	No	Yes	2.00
441	28.98	23.25	2.77	2.83	0.93	18.18	4.55	82.71	4.000	No	Yes	2.00
442	29.04	24.09	2.76	2.86	0.93	18.87	4.46	84.22	4.000	No	Yes	2.00
443	29.08	24.99	2.75	2.87	0.92	19.62	4.37	85.67	4.000	No	Yes	2.00
444	29.15	25.81	2.74	2.90	0.92	20.29	4.30	87.23	4.000	No	Yes	2.00
445	29.24	26.55	2.73	2.95	0.92	20.88	4.26	88.89	4.000	No	Yes	2.00
446	29.29	27.47	2.72	2.98	0.91	21.64	4.18	90.48	4.000	No	Yes	2.00
447	29.34	28.09	2.72	3.04	0.91	22.14	4.16	92.19	4.000	No	Yes	2.00
448	29.43	28.47	2.73	3.12	0.91	22.41	4.19	93.91	4.000	No	Yes	2.00
449	29.47	28.34	2.73	3.18	0.92	22.27	4.25	94.60	4.000	No	Yes	2.00
450	29.53	28.01	2.74	3.24	0.92	21.95	4.32	94.84	4.000	No	Yes	2.00
451	29.62	27.58	2.75	3.30	0.92	21.54	4.41	94.97	4.000	No	Yes	2.00
452	29.66	26.96	2.77	3.38	0.93	20.98	4.54	95.20	4.000	No	Yes	2.00
453	29.77	26.26	2.79	3.47	0.94	20.33	4.68	95.20	4.000	No	Yes	2.00
454	29.81	25.53	2.81	3.60	0.95	19.68	4.86	95.62	4.000	No	Yes	2.00
455	29.86	25.39	2.82	3.67	0.95	19.54	4.93	96.27	4.000	No	Yes	2.00
456	29.92	25.75	2.81	3.69	0.95	19.81	4.90	97.12	4.000	No	Yes	2.00
457	30.01	26.64	2.80	3.66	0.94	20.51	4.78	98.08	4.000	No	Yes	2.00
458	30.09	27.72	2.78	3.61	0.93	21.39	4.63	99.03	4.000	No	Yes	2.00
459	30.17	28.41	2.77	3.61	0.93	21.93	4.56	100.07	4.000	No	Yes	2.00
460	30.20	28.59	2.78	3.69	0.93	22.05	4.60	101.40	4.000	No	Yes	2.00
461	30.27	28.79	2.78	3.80	0.94	22.17	4.65	103.06	4.000	No	Yes	2.00
462	30.32	29.48	2.78	3.84	0.93	22.72	4.61	104.73	4.000	No	Yes	2.00
463	30.39	30.45	2.77	3.82	0.93	23.50	4.51	105.88	4.000	No	Yes	2.00
464	30.47	30.78	2.76	3.84	0.93	23.72	4.49	106.51	4.000	No	Yes	2.00
465	30.55	30.79	2.77	3.85	0.93	23.68	4.51	106.70	4.000	No	Yes	2.00
466	30.62	30.35	2.78	3.91	0.93	23.27	4.59	106.77	4.000	No	Yes	2.00
467	30.66	29.89	2.79	3.98	0.94	22.86	4.67	106.87	4.000	No	Yes	2.00
468	30.72	29.64	2.79	3.93	0.94	22.63	4.67	105.71	4.000	No	Yes	2.00
469	30.81	29.90	2.77	3.78	0.93	22.81	4.56	103.99	4.000	No	Yes	2.00
470	30.85	30.12	2.75	3.57	0.92	22.99	4.41	101.48	4.000	No	Yes	2.00
471	30.91	29.75	2.75	3.40	0.92	22.67	4.34	98.41	4.000	No	Yes	2.00
472	31.01	29.16	2.74	3.22	0.92	22.15	4.28	94.88	4.000	No	Yes	2.00
473	31.05	28.11	2.74	3.08	0.92	21.28	4.30	91.42	4.000	No	Yes	2.00
474	31.11	26.82	2.75	2.96	0.92	20.20	4.35	87.95	4.000	No	Yes	2.00
475	31.20	25.44	2.76	2.85	0.93	19.03	4.43	84.32	4.000	No	Yes	2.00
476	31.26	24.18	2.76	2.71	0.93	17.98	4.48	80.64	4.000	No	Yes	2.00
477	31.31	23.24	2.77	2.64	0.93	17.20	4.56	78.37	4.000	No	Yes	2.00
478	31.38	22.45	2.78	2.59	0.94	16.53	4.63	76.56	4.000	No	Yes	2.00
479	31.46	21.95	2.79	2.53	0.94	16.09	4.66	75.05	4.000	No	Yes	2.00
480	31.51	21.63	2.79	2.49	0.94	15.82	4.68	74.00	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
481	31.60	21.33	2.79	2.46	0.94	15.54	4.71	73.14	4.000	No	Yes	2.00
482	31.65	21.21	2.79	2.41	0.94	15.44	4.68	72.24	4.000	No	Yes	2.00
483	31.74	21.14	2.78	2.34	0.94	15.36	4.64	71.22	4.000	No	Yes	2.00
484	31.80	21.15	2.77	2.27	0.93	15.35	4.57	70.19	4.000	No	Yes	2.00
485	31.85	21.16	2.76	2.17	0.93	15.35	4.49	68.91	4.000	No	Yes	2.00
486	31.89	21.17	2.75	2.04	0.92	15.37	4.36	67.05	4.000	No	Yes	2.00
487	32.00	21.16	2.73	1.91	0.92	15.34	4.24	65.11	4.000	No	Yes	2.00
488	32.04	21.11	2.72	1.79	0.91	15.30	4.14	63.32	4.000	No	Yes	2.00
489	32.09	21.14	2.71	1.70	0.91	15.33	4.04	61.91	4.000	No	Yes	2.00
490	32.19	21.23	2.69	1.63	0.90	15.39	3.96	60.88	4.000	No	Yes	2.00
491	32.23	21.15	2.69	1.60	0.90	15.31	3.94	60.35	4.000	No	Yes	2.00
492	32.29	21.63	2.68	1.58	0.90	15.69	3.86	60.57	4.000	No	Yes	2.00
493	32.37	22.15	2.67	1.58	0.89	16.09	3.79	60.95	4.000	No	Yes	2.00
494	32.44	22.73	2.66	1.59	0.89	16.54	3.73	61.75	4.000	No	Yes	2.00
495	32.49	23.42	2.66	1.64	0.89	17.08	3.71	63.28	4.000	No	Yes	2.00
496	32.58	24.18	2.65	1.69	0.89	17.66	3.67	64.80	4.000	No	Yes	2.00
497	32.62	24.92	2.65	1.75	0.88	18.23	3.64	66.38	4.000	No	Yes	2.00
498	32.69	25.54	2.65	1.80	0.88	18.71	3.63	67.92	4.000	No	Yes	2.00
499	32.78	26.07	2.65	1.87	0.88	19.09	3.64	69.43	4.000	No	Yes	2.00
500	32.82	26.80	2.64	1.91	0.88	19.66	3.61	70.95	4.000	No	Yes	2.00
501	32.89	27.02	2.65	1.99	0.89	19.79	3.66	72.39	4.000	No	Yes	2.00
502	32.97	27.26	2.66	2.07	0.89	19.94	3.70	73.87	4.000	No	Yes	2.00
503	33.02	27.46	2.67	2.15	0.89	20.06	3.76	75.41	4.000	No	Yes	2.00
504	33.09	27.56	2.68	2.26	0.90	20.09	3.84	77.21	4.000	No	Yes	2.00
505	33.15	27.58	2.69	2.39	0.90	20.06	3.94	79.12	4.000	No	Yes	2.00
506	33.20	27.62	2.71	2.52	0.91	20.05	4.05	81.12	4.000	No	Yes	2.00
507	33.28	27.94	2.72	2.64	0.91	20.26	4.11	83.29	4.000	No	Yes	2.00
508	33.38	28.41	2.72	2.75	0.91	20.57	4.15	85.36	4.000	No	Yes	2.00
509	33.43	29.00	2.72	2.84	0.91	21.01	4.16	87.41	4.000	No	Yes	2.00
510	33.47	29.66	2.72	2.92	0.91	21.50	4.16	89.41	4.000	No	Yes	2.00
511	33.57	30.25	2.72	3.02	0.91	21.91	4.18	91.56	4.000	No	Yes	2.00
512	33.63	30.80	2.73	3.12	0.91	22.30	4.20	93.64	4.000	No	Yes	2.00
513	33.70	31.35	2.73	3.19	0.91	22.69	4.20	95.39	4.000	No	Yes	2.00
514	33.74	31.93	2.73	3.26	0.91	23.12	4.20	97.06	4.000	No	Yes	2.00
515	33.82	32.49	2.73	3.31	0.91	23.51	4.19	98.51	4.000	No	Yes	2.00
516	33.86	32.78	2.73	3.37	0.91	23.71	4.21	99.73	4.000	No	Yes	2.00
517	33.93	32.90	2.73	3.45	0.92	23.76	4.25	100.95	4.000	No	Yes	2.00
518	34.02	32.86	2.74	3.53	0.92	23.67	4.31	102.03	4.000	No	Yes	2.00
519	34.06	32.78	2.75	3.61	0.92	23.57	4.37	102.94	4.000	No	Yes	2.00
520	34.13	32.65	2.76	3.66	0.93	23.42	4.42	103.48	4.000	No	Yes	2.00
521	34.21	32.51	2.76	3.70	0.93	23.26	4.46	103.80	4.000	No	Yes	2.00
522	34.28	32.29	2.77	3.74	0.93	23.05	4.51	103.90	4.000	No	Yes	2.00
523	34.32	31.94	2.77	3.76	0.93	22.75	4.56	103.65	4.000	No	Yes	2.00
524	34.41	31.53	2.78	3.78	0.93	22.38	4.61	103.23	4.000	No	Yes	2.00
525	34.46	31.08	2.79	3.79	0.94	22.00	4.67	102.68	4.000	No	Yes	2.00
526	34.52	30.55	2.79	3.79	0.94	21.56	4.72	101.80	4.000	No	Yes	2.00
527	34.61	29.93	2.80	3.78	0.94	21.04	4.78	100.63	4.000	No	Yes	2.00
528	34.65	29.34	2.81	3.75	0.94	20.56	4.83	99.34	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
529	34.71	28.73	2.81	3.71	0.95	20.07	4.87	97.80	4.000	No	Yes	2.00
530	34.79	28.12	2.81	3.64	0.95	19.57	4.90	95.91	4.000	No	Yes	2.00
531	34.86	27.56	2.81	3.55	0.95	19.11	4.91	93.87	4.000	No	Yes	2.00
532	34.93	27.06	2.81	3.45	0.95	18.72	4.90	91.78	4.000	No	Yes	2.00
533	35.01	26.62	2.81	3.34	0.95	18.35	4.89	89.74	4.000	No	Yes	2.00
534	35.06	26.18	2.81	3.25	0.95	18.01	4.88	87.84	4.000	No	Yes	2.00
535	35.11	25.82	2.81	3.17	0.95	17.73	4.87	86.31	4.000	No	Yes	2.00
536	35.18	25.57	2.81	3.10	0.95	17.51	4.85	85.02	4.000	No	Yes	2.00
537	35.26	25.31	2.81	3.06	0.95	17.29	4.86	84.06	4.000	No	Yes	2.00
538	35.34	25.02	2.81	3.05	0.95	17.04	4.90	83.47	4.000	No	Yes	2.00
539	35.40	24.80	2.82	3.06	0.95	16.85	4.94	83.29	4.000	No	Yes	2.00
540	35.44	24.58	2.83	3.10	0.95	16.65	5.01	83.43	4.000	No	Yes	2.00
541	35.51	24.35	2.84	3.18	0.96	16.44	5.10	83.91	4.000	No	Yes	2.00
542	35.58	24.06	2.85	3.25	0.96	16.19	5.21	84.27	4.000	No	Yes	2.00
543	35.66	23.76	2.86	3.29	0.96	15.93	5.29	84.26	4.000	No	Yes	2.00
544	35.71	23.50	2.86	3.30	0.97	15.70	5.34	83.91	4.000	No	Yes	2.00
545	35.77	23.24	2.87	3.29	0.97	15.49	5.37	83.26	4.000	No	Yes	2.00
546	35.85	22.95	2.87	3.25	0.97	15.25	5.40	82.35	4.000	No	Yes	2.00
547	35.92	22.74	2.87	3.21	0.97	15.07	5.40	81.42	4.000	No	Yes	2.00
548	35.97	22.64	2.87	3.16	0.97	14.99	5.39	80.74	4.000	No	Yes	2.00
549	36.03	22.63	2.86	3.11	0.97	14.97	5.35	80.03	4.000	No	Yes	2.00
550	36.11	22.66	2.86	3.02	0.96	14.98	5.28	79.05	4.000	No	Yes	2.00
551	36.16	22.78	2.84	2.91	0.96	15.07	5.17	77.87	4.000	No	Yes	2.00
552	36.26	22.82	2.83	2.80	0.96	15.08	5.08	76.66	4.000	No	Yes	2.00
553	36.31	22.88	2.83	2.72	0.95	15.12	5.00	75.65	4.000	No	Yes	2.00
554	36.36	22.63	2.82	2.64	0.95	14.93	4.98	74.35	4.000	No	Yes	2.00
555	36.43	22.40	2.82	2.57	0.95	14.74	4.96	73.14	4.000	No	Yes	2.00
556	36.51	22.21	2.82	2.50	0.95	14.58	4.93	71.91	4.000	No	Yes	2.00
557	36.55	22.01	2.82	2.45	0.95	14.43	4.92	71.02	4.000	No	Yes	2.00
558	36.65	21.75	2.82	2.43	0.95	14.21	4.95	70.32	4.000	No	Yes	2.00
559	36.71	21.76	2.82	2.43	0.95	14.20	4.95	70.29	4.000	No	Yes	2.00
560	36.76	22.11	2.81	2.41	0.95	14.45	4.88	70.57	4.000	No	Yes	2.00
561	36.85	22.79	2.80	2.42	0.94	14.94	4.79	71.52	4.000	No	Yes	2.00
562	36.89	23.63	2.79	2.44	0.94	15.55	4.68	72.78	4.000	No	Yes	2.00
563	36.96	24.91	2.77	2.48	0.93	16.49	4.55	74.96	4.000	No	Yes	2.00
564	37.02	26.31	2.76	2.53	0.93	17.51	4.42	77.41	4.000	No	Yes	2.00
565	37.11	27.68	2.74	2.60	0.92	18.50	4.32	79.93	4.000	No	Yes	2.00
566	37.15	28.95	2.73	2.67	0.92	19.42	4.25	82.45	4.000	No	Yes	2.00
567	37.24	30.33	2.73	2.76	0.91	20.41	4.18	85.40	4.000	No	Yes	2.00
568	37.31	31.54	2.72	2.87	0.91	21.27	4.15	88.27	4.000	No	Yes	2.00
569	37.35	32.61	2.72	3.01	0.91	22.02	4.16	91.57	4.000	No	Yes	2.00
570	37.43	34.54	2.71	3.07	0.91	23.43	4.04	94.72	4.000	No	Yes	2.00
571	37.51	37.23	2.68	3.05	0.90	25.41	3.83	97.40	4.000	No	Yes	2.00
572	37.55	40.42	2.64	2.93	0.88	27.84	3.55	98.85	4.000	No	Yes	2.00
573	37.60	43.41	2.59	2.73	0.86	30.14	3.26	98.34	0.168	No	No	0.41
574	37.67	46.12	2.55	2.53	0.85	32.25	3.01	97.10	0.165	No	No	0.40
575	37.75	47.68	2.52	2.39	0.83	33.45	2.86	95.62	0.161	No	No	0.40
576	37.81	48.21	2.50	2.30	0.83	33.86	2.79	94.32	0.158	No	No	0.39

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
577	37.88	48.12	2.50	2.26	0.83	33.76	2.77	93.42	0.156	No	No	0.38
578	37.93	48.13	2.50	2.24	0.83	33.75	2.76	93.00	0.155	No	No	0.38
579	38.00	49.14	2.49	2.24	0.82	34.47	2.72	93.80	0.157	No	No	0.38
580	38.08	52.10	2.47	2.28	0.82	36.67	2.64	96.77	0.164	No	No	0.40
581	38.14	55.93	2.47	2.41	0.81	39.49	2.60	102.67	0.181	No	No	0.44
582	38.20	60.41	2.46	2.61	0.81	42.75	2.58	110.38	0.205	No	No	0.50
583	38.26	65.84	2.46	2.84	0.81	46.71	2.57	119.90	4.000	Yes	No	2.00
584	38.34	74.63	2.43	2.98	0.80	53.26	2.44	130.07	4.000	Yes	No	2.00
585	38.43	85.00	2.39	3.03	0.79	61.06	2.29	139.63	4.000	Yes	No	2.00
586	38.45	97.14	2.35	3.04	0.77	70.35	2.13	149.58	4.000	Yes	No	2.00
587	38.53	109.74	2.31	3.03	0.76	79.94	1.99	159.28	4.000	Yes	No	2.00
588	38.62	121.23	2.28	3.04	0.75	88.66	1.90	168.28	4.000	Yes	No	2.00
589	38.65	130.51	2.26	3.06	0.74	95.75	1.84	176.10	4.000	Yes	No	2.00
590	38.72	139.21	2.25	3.07	0.73	102.35	1.79	182.90	0.649	No	No	1.59
591	38.80	148.05	2.23	3.07	0.72	109.03	1.74	189.51	0.713	No	No	1.75
592	38.88	156.31	2.21	3.04	0.72	115.30	1.69	195.08	0.770	No	No	1.89
593	38.93	162.35	2.20	3.05	0.71	119.87	1.67	199.70	0.821	No	No	2.00
594	39.01	167.70	2.19	3.06	0.71	123.81	1.65	204.11	4.000	No	No	2.00
595	39.07	171.82	2.19	3.08	0.71	126.83	1.64	207.67	4.000	No	No	2.00
596	39.12	176.04	2.18	3.09	0.71	129.96	1.62	211.17	4.000	No	No	2.00
597	39.20	180.10	2.18	3.11	0.71	132.88	1.62	214.63	4.000	No	No	2.00
598	39.27	184.00	2.17	3.12	0.70	135.69	1.61	217.99	4.000	No	No	2.00
599	39.31	187.49	2.17	3.14	0.70	138.26	1.60	221.07	4.000	No	No	2.00
600	39.38	190.29	2.17	3.16	0.70	140.19	1.60	223.77	4.000	No	No	2.00
601	39.45	193.31	2.17	3.18	0.70	142.31	1.59	226.42	4.000	No	No	2.00
602	39.51	197.03	2.16	3.17	0.70	145.04	1.58	229.13	4.000	No	No	2.00
603	39.57	201.45	2.15	3.16	0.70	148.33	1.56	231.77	4.000	No	No	2.00
604	39.64	206.43	2.14	3.12	0.69	152.05	1.54	234.36	4.000	No	No	2.00
605	39.72	209.97	2.14	3.10	0.69	154.62	1.53	235.92	4.000	No	No	2.00
606	39.79	210.90	2.13	3.08	0.69	155.19	1.52	235.81	4.000	No	No	2.00
607	39.84	209.11	2.14	3.08	0.69	153.65	1.53	234.48	4.000	No	No	2.00
608	39.90	206.02	2.14	3.10	0.69	151.08	1.54	232.41	4.000	No	No	2.00
609	39.96	202.96	2.15	3.09	0.69	148.57	1.55	229.77	4.000	No	No	2.00
610	40.06	199.55	2.15	3.09	0.69	145.71	1.56	226.70	4.000	No	No	2.00
611	40.13	195.43	2.16	3.08	0.70	142.38	1.57	223.26	4.000	No	No	2.00
612	40.17	191.56	2.16	3.07	0.70	139.34	1.58	219.92	4.000	No	No	2.00
613	40.26	187.07	2.17	3.06	0.70	135.71	1.59	216.05	4.000	No	No	2.00
614	40.31	182.02	2.18	3.06	0.70	131.75	1.61	211.86	4.000	No	No	2.00
615	40.36	176.42	2.18	3.04	0.71	127.42	1.62	206.86	4.000	No	No	2.00
616	40.43	171.16	2.19	3.00	0.71	123.34	1.63	201.52	4.000	No	No	2.00
617	40.51	164.14	2.20	2.99	0.71	117.86	1.66	195.74	0.777	No	No	1.91
618	40.56	159.97	2.20	2.93	0.71	114.70	1.66	190.93	0.727	No	No	1.79
619	40.64	152.18	2.22	2.95	0.72	108.61	1.71	185.56	0.674	No	No	1.66
620	40.70	148.35	2.22	2.89	0.72	105.73	1.71	180.74	0.629	No	No	1.55
621	40.75	146.10	2.21	2.78	0.72	104.13	1.69	175.76	0.585	No	No	1.44
622	40.83	144.83	2.20	2.66	0.71	103.24	1.66	171.24	0.547	No	No	1.34
623	40.88	146.29	2.17	2.49	0.70	104.60	1.60	167.25	0.515	No	No	1.27
624	40.95	151.45	2.13	2.24	0.69	108.92	1.50	163.89	0.489	No	No	1.20

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
625	41.03	159.00	2.08	2.02	0.67	115.12	1.41	162.69	0.480	No	No	1.18
626	41.08	169.86	2.02	1.80	0.64	124.05	1.32	164.27	0.492	No	No	1.21
627	41.15	178.00	1.97	1.65	0.63	130.77	1.27	165.80	0.504	No	No	1.24
628	41.24	189.19	1.92	1.49	0.61	140.00	1.21	169.37	0.532	No	No	1.31
629	41.28	194.60	1.89	1.39	0.60	144.65	1.18	170.54	0.541	No	No	1.33
630	41.35	196.88	1.87	1.31	0.59	146.68	1.16	170.24	0.539	No	No	1.33
631	41.41	197.86	1.85	1.25	0.58	147.66	1.15	169.29	0.531	No	No	1.31
632	41.48	196.40	1.85	1.23	0.58	146.49	1.14	167.63	0.518	No	No	1.28
633	41.55	192.75	1.87	1.29	0.59	143.17	1.16	166.29	0.508	No	No	1.25
634	41.63	188.20	1.89	1.35	0.60	139.10	1.18	164.51	0.494	No	No	1.22
635	41.68	181.44	1.93	1.44	0.61	133.30	1.21	161.92	0.475	No	No	1.17
636	41.74	174.04	1.96	1.54	0.62	127.00	1.25	159.25	0.456	No	No	1.12
637	41.83	166.17	2.00	1.67	0.64	120.27	1.30	156.93	0.439	No	No	1.08
638	41.87	159.62	2.04	1.81	0.65	114.71	1.36	156.04	0.433	No	No	1.07
639	41.98	152.99	2.09	1.98	0.67	108.97	1.43	155.95	0.433	No	No	1.07
640	42.02	146.03	2.13	2.18	0.69	103.14	1.52	156.49	0.436	No	No	1.08
641	42.10	139.05	2.18	2.38	0.71	97.32	1.62	157.32	0.442	No	No	1.09
642	42.14	132.52	2.22	2.59	0.72	92.01	1.72	158.36	0.449	No	No	1.11
643	42.22	126.16	2.26	2.80	0.74	86.83	1.84	159.59	0.458	No	No	1.13
644	42.29	120.67	2.30	2.99	0.75	82.42	1.95	160.51	0.465	No	No	1.15
645	42.38	115.55	2.33	3.17	0.76	78.32	2.06	161.46	0.471	No	No	1.16
646	42.41	111.25	2.36	3.33	0.78	74.95	2.17	162.34	0.478	No	No	1.18
647	42.46	107.34	2.39	3.48	0.79	71.90	2.27	163.00	0.483	No	No	1.19
648	42.57	103.94	2.41	3.60	0.79	69.19	2.36	163.11	0.484	No	No	1.19
649	42.61	100.91	2.43	3.70	0.80	66.88	2.44	163.01	0.483	No	No	1.19
650	42.68	98.50	2.44	3.78	0.81	65.01	2.50	162.77	0.481	No	No	1.19
651	42.76	96.24	2.46	3.85	0.81	63.25	2.57	162.34	0.478	No	No	1.18
652	42.80	94.09	2.47	3.91	0.82	61.63	2.63	161.80	0.474	No	No	1.17
653	42.87	92.43	2.48	3.94	0.82	60.35	2.67	161.02	0.468	No	No	1.16
654	42.92	90.98	2.49	3.95	0.82	59.26	2.70	160.04	0.461	No	No	1.14
655	42.98	89.10	2.49	3.96	0.83	57.87	2.74	158.36	0.449	No	No	1.11
656	43.06	86.12	2.50	3.94	0.83	55.71	2.79	155.17	0.427	No	No	1.06
657	43.11	82.66	2.52	3.92	0.83	53.25	2.85	151.63	0.404	No	No	1.00
658	43.18	78.34	2.53	3.93	0.84	50.16	2.95	147.91	0.381	No	No	0.94
659	43.26	73.08	2.56	3.98	0.85	46.41	3.10	143.94	0.357	No	No	0.88
660	43.32	67.13	2.60	4.05	0.86	42.20	3.31	139.61	0.333	No	No	0.82
661	43.39	61.24	2.63	4.13	0.88	38.07	3.54	134.85	4.000	No	Yes	2.00
662	43.46	55.24	2.67	4.18	0.89	33.90	3.81	129.27	4.000	No	Yes	2.00
663	43.52	48.95	2.72	4.22	0.91	29.60	4.15	122.72	4.000	No	Yes	2.00
664	43.61	43.21	2.77	4.25	0.93	25.69	4.52	116.06	4.000	No	Yes	2.00
665	43.64	38.48	2.82	4.33	0.95	22.50	4.92	110.79	4.000	No	Yes	2.00
666	43.70	34.37	2.86	4.38	0.97	19.75	5.34	105.47	4.000	No	Yes	2.00
667	43.79	31.53	2.89	4.31	0.98	17.87	5.61	100.21	4.000	No	Yes	2.00
668	43.84	29.85	2.90	4.10	0.98	16.79	5.68	95.39	4.000	No	Yes	2.00
669	43.90	29.16	2.89	3.87	0.98	16.37	5.61	91.83	4.000	No	Yes	2.00
670	43.97	28.62	2.89	3.72	0.98	16.03	5.57	89.31	4.000	No	Yes	2.00
671	44.05	28.46	2.88	3.64	0.97	15.91	5.55	88.25	4.000	No	Yes	2.00
672	44.10	28.90	2.88	3.63	0.97	16.18	5.48	88.67	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
673	44.18	29.73	2.87	3.68	0.97	16.69	5.41	90.36	4.000	No	Yes	2.00
674	44.24	30.91	2.86	3.74	0.97	17.43	5.32	92.72	4.000	No	Yes	2.00
675	44.30	32.38	2.85	3.83	0.96	18.35	5.22	95.76	4.000	No	Yes	2.00
676	44.38	34.27	2.83	3.92	0.96	19.53	5.09	99.36	4.000	No	Yes	2.00
677	44.45	36.52	2.82	3.97	0.95	20.96	4.92	103.06	4.000	No	Yes	2.00
678	44.49	39.14	2.79	3.95	0.94	22.67	4.68	106.18	4.000	No	Yes	2.00
679	44.57	41.80	2.76	3.90	0.93	24.41	4.46	108.75	4.000	No	Yes	2.00
680	44.64	44.11	2.74	3.92	0.92	25.89	4.31	111.67	4.000	No	Yes	2.00
681	44.72	45.81	2.73	3.98	0.92	26.96	4.24	114.40	4.000	No	Yes	2.00
682	44.79	47.04	2.73	4.03	0.91	27.72	4.21	116.56	4.000	No	Yes	2.00
683	44.84	48.33	2.72	4.06	0.91	28.53	4.15	118.40	4.000	Yes	Yes	2.00
684	44.92	51.62	2.68	3.87	0.90	30.75	3.87	118.97	4.000	Yes	Yes	2.00
685	44.96	56.00	2.63	3.57	0.88	33.79	3.51	118.61	4.000	Yes	Yes	2.00
686	45.03	61.93	2.56	3.21	0.85	37.94	3.09	117.38	4.000	Yes	No	2.00
687	45.09	70.39	2.47	2.79	0.82	43.99	2.63	115.79	4.000	Yes	No	2.00
688	45.19	78.97	2.39	2.46	0.79	50.19	2.29	114.70	4.000	Yes	No	2.00
689	45.23	87.67	2.32	2.19	0.76	56.61	2.01	113.97	4.000	Yes	No	2.00
690	45.28	95.84	2.26	2.02	0.74	62.61	1.84	115.12	4.000	Yes	No	2.00
691	45.38	103.70	2.22	1.90	0.72	68.35	1.71	117.08	4.000	Yes	No	2.00
692	45.43	110.94	2.18	1.84	0.71	73.64	1.63	119.99	4.000	Yes	No	2.00
693	45.48	114.55	2.18	1.89	0.71	76.05	1.63	123.69	0.256	No	No	0.64
694	45.58	115.95	2.20	2.00	0.71	76.70	1.66	127.38	4.000	Yes	No	2.00
695	45.62	113.89	2.23	2.19	0.73	74.81	1.75	130.77	4.000	Yes	No	2.00
696	45.67	107.49	2.29	2.47	0.75	69.71	1.92	133.73	4.000	Yes	No	2.00
697	45.78	100.41	2.35	2.79	0.77	64.15	2.13	136.92	4.000	Yes	No	2.00
698	45.82	92.83	2.42	3.15	0.80	58.44	2.39	139.92	4.000	Yes	No	2.00
699	45.88	86.04	2.47	3.42	0.82	53.46	2.63	140.77	4.000	Yes	No	2.00
700	45.98	79.71	2.52	3.68	0.84	48.88	2.88	140.84	4.000	Yes	No	2.00
701	46.02	73.83	2.57	3.91	0.85	44.74	3.13	140.23	4.000	Yes	No	2.00
702	46.07	69.62	2.59	3.99	0.86	41.84	3.29	137.86	4.000	Yes	No	2.00
703	46.17	66.01	2.62	4.02	0.87	39.37	3.42	134.82	4.000	No	Yes	2.00
704	46.21	63.43	2.63	3.97	0.88	37.66	3.49	131.48	4.000	No	Yes	2.00
705	46.27	61.17	2.64	3.93	0.88	36.16	3.55	128.41	4.000	No	Yes	2.00
706	46.37	59.04	2.65	3.89	0.88	34.72	3.62	125.52	4.000	No	Yes	2.00
707	46.39	57.19	2.66	3.87	0.89	33.50	3.68	123.35	4.000	No	Yes	2.00
708	46.47	55.24	2.67	3.95	0.89	32.14	3.82	122.66	4.000	No	Yes	2.00
709	46.57	53.36	2.70	4.06	0.90	30.82	3.97	122.21	4.000	No	Yes	2.00
710	46.62	51.65	2.71	4.14	0.91	29.64	4.10	121.62	4.000	No	Yes	2.00
711	46.67	49.67	2.74	4.28	0.92	28.29	4.29	121.27	4.000	No	Yes	2.00
712	46.77	47.76	2.76	4.42	0.93	26.96	4.48	120.87	4.000	No	Yes	2.00
713	46.82	46.32	2.78	4.54	0.94	25.98	4.64	120.67	4.000	No	Yes	2.00
714	46.90	45.86	2.79	4.55	0.94	25.64	4.69	120.21	4.000	No	Yes	2.00
715	46.92	45.62	2.79	4.54	0.94	25.48	4.70	119.75	4.000	No	Yes	2.00
716	47.01	45.61	2.79	4.54	0.94	25.43	4.70	119.60	4.000	No	Yes	2.00
717	47.05	45.76	2.79	4.53	0.94	25.51	4.69	119.58	4.000	No	Yes	2.00
718	47.12	45.95	2.79	4.54	0.94	25.59	4.69	119.93	4.000	No	Yes	2.00
719	47.21	45.72	2.80	4.61	0.94	25.38	4.75	120.48	4.000	No	Yes	2.00
720	47.28	46.33	2.79	4.59	0.94	25.74	4.70	120.95	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
721	47.32	46.71	2.79	4.60	0.94	25.95	4.68	121.44	4.000	No	Yes	2.00
722	47.40	47.02	2.79	4.63	0.94	26.10	4.68	122.19	4.000	No	Yes	2.00
723	47.45	47.62	2.79	4.66	0.94	26.44	4.66	123.33	4.000	No	Yes	2.00
724	47.55	48.61	2.78	4.65	0.93	27.01	4.60	124.26	4.000	No	Yes	2.00
725	47.58	49.96	2.76	4.55	0.93	27.88	4.47	124.59	4.000	No	Yes	2.00
726	47.66	51.87	2.74	4.39	0.92	29.11	4.28	124.45	4.000	No	Yes	2.00
727	47.74	54.02	2.71	4.21	0.91	30.50	4.07	124.17	4.000	No	Yes	2.00
728	47.80	56.71	2.68	4.02	0.90	32.27	3.84	124.05	4.000	No	Yes	2.00
729	47.85	58.65	2.66	3.92	0.89	33.53	3.70	124.22	4.000	No	Yes	2.00
730	47.93	60.64	2.64	3.82	0.88	34.81	3.58	124.49	4.000	No	Yes	2.00
731	47.98	62.76	2.62	3.71	0.87	36.21	3.44	124.46	4.000	No	Yes	2.00
732	48.04	64.99	2.59	3.57	0.86	37.69	3.29	124.03	0.257	No	No	0.65
733	48.11	67.41	2.57	3.44	0.85	39.30	3.14	123.57	0.255	No	No	0.65
734	48.20	69.59	2.55	3.33	0.85	40.73	3.03	123.38	0.255	No	No	0.65
735	48.24	71.33	2.54	3.28	0.84	41.88	2.95	123.68	0.256	No	No	0.65
736	48.30	72.97	2.52	3.23	0.84	42.95	2.89	123.93	0.257	No	No	0.65
737	48.39	74.42	2.51	3.18	0.83	43.87	2.83	124.05	0.258	No	No	0.65
738	48.44	75.99	2.50	3.14	0.83	44.91	2.77	124.44	0.259	No	No	0.66
739	48.53	77.80	2.49	3.10	0.82	46.06	2.71	124.94	0.261	No	No	0.66
740	48.59	79.60	2.48	3.07	0.82	47.23	2.66	125.51	0.264	No	No	0.67
741	48.64	80.98	2.47	3.06	0.82	48.11	2.63	126.34	0.268	No	No	0.68
742	48.70	82.04	2.47	3.08	0.82	48.73	2.62	127.52	0.273	No	No	0.69
743	48.78	83.53	2.46	3.09	0.81	49.64	2.59	128.78	0.279	No	No	0.71
744	48.82	85.19	2.46	3.09	0.81	50.69	2.56	129.97	0.284	No	No	0.72
745	48.89	87.28	2.45	3.08	0.81	52.03	2.52	131.08	0.289	No	No	0.74
746	48.98	90.26	2.43	3.03	0.80	53.97	2.45	132.03	0.294	No	No	0.75
747	49.05	93.73	2.41	2.95	0.79	56.28	2.36	132.78	0.298	No	No	0.76
748	49.09	97.44	2.39	2.87	0.79	58.81	2.27	133.45	0.301	No	No	0.77
749	49.16	101.81	2.36	2.78	0.78	61.78	2.17	134.12	0.304	No	No	0.78
750	49.24	106.91	2.34	2.68	0.77	65.26	2.07	135.13	0.309	No	No	0.79
751	49.31	112.14	2.31	2.59	0.75	68.86	1.98	136.11	0.315	No	No	0.80
752	49.38	116.76	2.29	2.51	0.75	72.05	1.90	137.00	0.319	No	No	0.82
753	49.43	120.62	2.26	2.43	0.74	74.75	1.84	137.59	0.322	No	No	0.82
754	49.52	123.30	2.25	2.35	0.73	76.64	1.79	137.04	0.319	No	No	0.82
755	49.58	124.61	2.23	2.27	0.73	77.65	1.75	135.66	0.312	No	No	0.80
756	49.63	124.38	2.22	2.21	0.72	77.57	1.73	133.96	0.304	No	No	0.78
757	49.71	122.70	2.23	2.19	0.72	76.38	1.73	132.38	0.296	No	No	0.76
758	49.77	119.64	2.24	2.21	0.73	74.19	1.76	130.76	4.000	Yes	No	2.00
759	49.82	114.85	2.26	2.25	0.74	70.80	1.82	128.74	4.000	Yes	No	2.00
760	49.88	107.69	2.29	2.33	0.75	65.75	1.92	126.27	4.000	Yes	No	2.00
761	49.97	100.43	2.33	2.42	0.76	60.65	2.04	123.80	4.000	Yes	No	2.00
762	50.01	94.19	2.36	2.50	0.77	56.34	2.16	121.67	4.000	Yes	No	2.00
763	50.07	89.11	2.40	2.63	0.79	52.76	2.30	121.25	4.000	Yes	No	2.00
764	50.17	84.50	2.44	2.81	0.80	49.44	2.47	122.07	4.000	Yes	No	2.00
765	50.22	80.39	2.48	3.00	0.82	46.53	2.65	123.24	4.000	Yes	No	2.00
766	50.29	76.13	2.51	3.17	0.83	43.58	2.83	123.52	4.000	Yes	No	2.00
767	50.37	72.92	2.54	3.28	0.84	41.37	2.97	123.02	4.000	Yes	No	2.00
768	50.42	69.90	2.56	3.36	0.85	39.36	3.10	122.05	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
769	50.47	68.34	2.57	3.36	0.86	38.34	3.15	120.84	4.000	No	No	2.00
770	50.57	65.94	2.59	3.39	0.86	36.74	3.25	119.31	4.000	No	No	2.00
771	50.63	62.51	2.61	3.46	0.87	34.52	3.40	117.49	4.000	No	Yes	2.00
772	50.68	58.31	2.64	3.51	0.88	31.85	3.60	114.64	4.000	No	Yes	2.00
773	50.73	53.55	2.68	3.52	0.90	28.88	3.82	110.42	4.000	No	Yes	2.00
774	50.79	48.91	2.71	3.50	0.91	26.02	4.06	105.58	4.000	No	Yes	2.00
775	50.88	45.25	2.73	3.42	0.92	23.79	4.23	100.57	4.000	No	Yes	2.00
776	50.93	41.03	2.76	3.35	0.93	21.25	4.48	95.16	4.000	No	Yes	2.00
777	51.03	37.66	2.78	3.19	0.94	19.24	4.65	89.48	4.000	No	Yes	2.00
778	51.07	34.69	2.80	2.99	0.94	17.53	4.77	83.65	4.000	No	Yes	2.00
779	51.14	32.58	2.80	2.70	0.94	16.34	4.76	77.75	4.000	No	Yes	2.00
780	51.23	30.90	2.79	2.40	0.94	15.42	4.68	72.12	4.000	No	Yes	2.00
781	51.27	29.21	2.78	2.14	0.94	14.49	4.63	67.10	4.000	No	Yes	2.00
782	51.33	28.11	2.78	1.96	0.93	13.89	4.58	63.59	4.000	No	Yes	2.00
783	51.42	27.14	2.77	1.79	0.93	13.35	4.53	60.46	4.000	No	Yes	2.00
784	51.48	26.51	2.76	1.64	0.93	13.02	4.44	57.82	4.000	No	Yes	2.00
785	51.52	26.33	2.75	1.59	0.92	12.93	4.40	56.91	4.000	No	Yes	2.00
786	51.60	26.44	2.75	1.57	0.92	12.98	4.37	56.75	4.000	No	Yes	2.00
787	51.68	26.86	2.74	1.58	0.92	13.22	4.32	57.16	4.000	No	Yes	2.00
788	51.72	27.53	2.74	1.61	0.92	13.60	4.28	58.21	4.000	No	Yes	2.00
789	51.81	28.12	2.74	1.68	0.92	13.90	4.30	59.73	4.000	No	Yes	2.00
790	51.87	28.73	2.74	1.77	0.92	14.22	4.32	61.44	4.000	No	Yes	2.00
791	51.91	28.93	2.75	1.86	0.92	14.29	4.40	62.90	4.000	No	Yes	2.00
792	51.98	28.88	2.77	1.95	0.93	14.21	4.50	63.93	4.000	No	Yes	2.00
793	52.07	28.66	2.78	2.02	0.93	14.03	4.61	64.66	4.000	No	Yes	2.00
794	52.10	28.09	2.79	2.05	0.94	13.67	4.72	64.51	4.000	No	Yes	2.00
795	52.17	27.20	2.81	2.07	0.95	13.12	4.86	63.79	4.000	No	Yes	2.00
796	52.24	26.15	2.83	2.08	0.95	12.48	5.03	62.82	4.000	No	Yes	2.00
797	52.31	24.96	2.85	2.09	0.96	11.76	5.24	61.59	4.000	No	Yes	2.00
798	52.37	23.83	2.87	2.05	0.97	11.10	5.40	59.89	4.000	No	Yes	2.00
799	52.46	22.77	2.88	1.99	0.97	10.48	5.52	57.92	4.000	No	Yes	2.00
800	52.51	21.99	2.89	1.91	0.98	10.05	5.59	56.16	4.000	No	Yes	2.00
801	52.57	21.52	2.89	1.81	0.97	9.79	5.56	54.48	4.000	No	Yes	2.00
802	52.66	21.13	2.88	1.71	0.97	9.58	5.52	52.88	4.000	No	Yes	2.00
803	52.71	20.91	2.88	1.64	0.97	9.46	5.47	51.80	4.000	No	Yes	2.00
804	52.78	20.78	2.87	1.58	0.97	9.39	5.44	51.06	4.000	No	Yes	2.00
805	52.86	20.69	2.87	1.54	0.97	9.34	5.40	50.46	4.000	No	Yes	2.00
806	52.91	20.62	2.87	1.52	0.97	9.30	5.38	50.07	4.000	No	Yes	2.00
807	52.99	20.60	2.87	1.50	0.97	9.29	5.37	49.83	4.000	No	Yes	2.00
808	53.06	20.61	2.86	1.49	0.97	9.29	5.35	49.67	4.000	No	Yes	2.00
809	53.09	20.61	2.86	1.47	0.97	9.29	5.32	49.44	4.000	No	Yes	2.00
810	53.16	20.64	2.86	1.46	0.96	9.30	5.31	49.35	4.000	No	Yes	2.00
811	53.25	20.67	2.86	1.45	0.96	9.30	5.29	49.26	4.000	No	Yes	2.00
812	53.29	20.68	2.86	1.44	0.96	9.31	5.28	49.17	4.000	No	Yes	2.00
813	53.36	20.66	2.86	1.44	0.96	9.29	5.28	49.08	4.000	No	Yes	2.00
814	53.45	20.68	2.86	1.43	0.96	9.29	5.27	48.99	4.000	No	Yes	2.00
815	53.50	20.68	2.85	1.43	0.96	9.28	5.27	48.90	4.000	No	Yes	2.00
816	53.55	20.67	2.86	1.43	0.96	9.27	5.28	48.97	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
817	53.64	20.67	2.86	1.44	0.96	9.25	5.30	49.03	4.000	No	Yes	2.00
818	53.69	20.70	2.86	1.44	0.96	9.26	5.30	49.09	4.000	No	Yes	2.00
819	53.76	20.73	2.86	1.44	0.96	9.27	5.30	49.08	4.000	No	Yes	2.00
820	53.84	20.80	2.86	1.45	0.96	9.29	5.30	49.22	4.000	No	Yes	2.00
821	53.88	20.91	2.86	1.47	0.96	9.35	5.30	49.59	4.000	No	Yes	2.00
822	53.96	21.17	2.86	1.49	0.96	9.48	5.28	50.03	4.000	No	Yes	2.00
823	54.03	21.41	2.85	1.51	0.96	9.60	5.26	50.46	4.000	No	Yes	2.00
824	54.08	21.59	2.85	1.52	0.96	9.69	5.24	50.82	4.000	No	Yes	2.00
825	54.17	21.74	2.85	1.53	0.96	9.76	5.23	51.09	4.000	No	Yes	2.00
826	54.23	21.88	2.85	1.55	0.96	9.83	5.23	51.37	4.000	No	Yes	2.00
827	54.27	21.99	2.85	1.56	0.96	9.88	5.23	51.65	4.000	No	Yes	2.00
828	54.38	22.08	2.85	1.57	0.96	9.91	5.22	51.77	4.000	No	Yes	2.00
829	54.42	22.14	2.85	1.55	0.96	9.94	5.20	51.69	4.000	No	Yes	2.00
830	54.47	22.17	2.84	1.52	0.96	9.97	5.14	51.26	4.000	No	Yes	2.00
831	54.53	22.12	2.84	1.48	0.96	9.94	5.10	50.74	4.000	No	Yes	2.00
832	54.61	22.06	2.83	1.44	0.95	9.91	5.07	50.22	4.000	No	Yes	2.00
833	54.68	22.03	2.83	1.42	0.95	9.90	5.04	49.84	4.000	No	Yes	2.00
834	54.73	22.02	2.83	1.39	0.95	9.89	5.01	49.53	4.000	No	Yes	2.00
835	54.80	22.01	2.82	1.38	0.95	9.87	5.00	49.37	4.000	No	Yes	2.00
836	54.88	22.03	2.82	1.38	0.95	9.87	5.00	49.35	4.000	No	Yes	2.00
837	54.95	22.09	2.83	1.40	0.95	9.89	5.01	49.56	4.000	No	Yes	2.00
838	55.02	22.17	2.83	1.42	0.95	9.92	5.03	49.92	4.000	No	Yes	2.00
839	55.07	22.23	2.83	1.46	0.96	9.93	5.08	50.42	4.000	No	Yes	2.00
840	55.15	22.25	2.84	1.50	0.96	9.91	5.14	50.97	4.000	No	Yes	2.00
841	55.21	22.27	2.85	1.55	0.96	9.90	5.20	51.52	4.000	No	Yes	2.00
842	55.27	22.39	2.85	1.57	0.96	9.96	5.21	51.86	4.000	No	Yes	2.00
843	55.34	22.62	2.84	1.57	0.96	10.08	5.17	52.13	4.000	No	Yes	2.00
844	55.42	22.88	2.84	1.57	0.96	10.21	5.12	52.33	4.000	No	Yes	2.00
845	55.47	23.13	2.83	1.57	0.96	10.34	5.08	52.59	4.000	No	Yes	2.00
846	55.54	23.41	2.84	1.62	0.96	10.48	5.09	53.39	4.000	No	Yes	2.00
847	55.62	23.74	2.84	1.66	0.96	10.64	5.10	54.24	4.000	No	Yes	2.00
848	55.65	24.32	2.83	1.70	0.95	10.95	5.05	55.28	4.000	No	Yes	2.00
849	55.72	25.17	2.82	1.73	0.95	11.41	4.94	56.41	4.000	No	Yes	2.00
850	55.81	26.14	2.81	1.77	0.95	11.94	4.85	57.86	4.000	No	Yes	2.00
851	55.84	27.15	2.80	1.85	0.94	12.48	4.80	59.87	4.000	No	Yes	2.00
852	55.91	28.26	2.81	2.04	0.95	13.02	4.86	63.28	4.000	No	Yes	2.00
853	55.98	29.52	2.82	2.26	0.95	13.64	4.92	67.15	4.000	No	Yes	2.00
854	56.05	31.10	2.81	2.44	0.95	14.46	4.90	70.92	4.000	Yes	Yes	2.00
855	56.11	34.04	2.78	2.45	0.93	16.12	4.59	73.94	4.000	Yes	Yes	2.00
856	56.21	38.52	2.72	2.40	0.91	18.71	4.13	77.33	4.000	Yes	Yes	2.00
857	56.26	43.85	2.66	2.33	0.89	21.85	3.70	80.74	4.000	Yes	Yes	2.00
858	56.31	51.25	2.58	2.23	0.86	26.31	3.21	84.44	4.000	Yes	No	2.00
859	56.39	58.39	2.52	2.16	0.84	30.64	2.88	88.08	4.000	Yes	No	2.00
860	56.46	66.60	2.46	2.08	0.81	35.71	2.57	91.68	4.000	Yes	No	2.00
861	56.50	74.21	2.41	2.01	0.79	40.49	2.34	94.69	4.000	Yes	No	2.00
862	56.60	80.84	2.37	1.97	0.78	44.64	2.19	97.58	4.000	Yes	No	2.00
863	56.65	86.36	2.34	1.96	0.77	48.10	2.09	100.49	4.000	Yes	No	2.00
864	56.72	89.96	2.33	1.99	0.76	50.26	2.06	103.30	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
865	56.78	91.09	2.33	2.03	0.76	50.86	2.06	104.84	4.000	No	No	2.00
866	56.87	90.61	2.34	2.08	0.77	50.39	2.10	105.65	4.000	Yes	No	2.00
867	56.93	86.85	2.37	2.18	0.78	47.84	2.21	105.54	4.000	Yes	No	2.00
868	56.97	82.39	2.41	2.26	0.79	44.91	2.33	104.79	4.000	Yes	No	2.00
869	57.05	76.32	2.45	2.38	0.81	40.97	2.52	103.41	4.000	Yes	No	2.00
870	57.11	69.97	2.50	2.48	0.83	36.95	2.75	101.47	4.000	Yes	No	2.00
871	57.17	63.87	2.54	2.56	0.84	33.16	2.98	98.86	4.000	Yes	No	2.00
872	57.25	58.18	2.58	2.61	0.86	29.71	3.22	95.61	4.000	Yes	No	2.00
873	57.31	52.54	2.63	2.64	0.88	26.32	3.49	91.87	4.000	Yes	Yes	2.00
874	57.37	47.66	2.67	2.65	0.89	23.46	3.76	88.15	4.000	Yes	Yes	2.00
875	57.42	43.35	2.70	2.62	0.91	20.97	4.01	84.11	4.000	Yes	Yes	2.00
876	57.48	39.91	2.73	2.54	0.91	19.02	4.20	79.93	4.000	Yes	Yes	2.00
877	57.56	37.11	2.75	2.44	0.92	17.46	4.35	75.95	4.000	No	Yes	2.00
878	57.64	34.62	2.76	2.32	0.93	16.08	4.48	72.08	4.000	No	Yes	2.00
879	57.70	32.80	2.77	2.18	0.93	15.10	4.54	68.55	4.000	No	Yes	2.00
880	57.74	31.50	2.77	2.01	0.93	14.44	4.51	65.16	4.000	No	Yes	2.00
881	57.81	30.51	2.76	1.85	0.93	13.94	4.46	62.19	4.000	No	Yes	2.00
882	57.90	29.96	2.75	1.71	0.92	13.68	4.37	59.72	4.000	No	Yes	2.00
883	57.95	29.50	2.74	1.61	0.92	13.45	4.31	58.04	4.000	No	Yes	2.00
884	58.06	29.02	2.75	1.63	0.92	13.15	4.40	57.86	4.000	No	Yes	2.00
885	58.09	28.66	2.77	1.69	0.93	12.92	4.51	58.28	4.000	No	Yes	2.00
886	58.15	28.80	2.77	1.73	0.93	12.96	4.55	59.02	4.000	No	Yes	2.00
887	58.20	29.53	2.76	1.73	0.93	13.36	4.46	59.61	4.000	No	Yes	2.00
888	58.29	30.50	2.74	1.70	0.92	13.91	4.31	59.94	4.000	No	Yes	2.00
889	58.33	31.57	2.72	1.67	0.91	14.52	4.16	60.44	4.000	No	Yes	2.00
890	58.40	32.28	2.72	1.69	0.91	14.90	4.11	61.27	4.000	No	Yes	2.00
891	58.48	32.70	2.71	1.72	0.91	15.11	4.10	62.00	4.000	No	Yes	2.00
892	58.55	33.02	2.71	1.75	0.91	15.26	4.10	62.56	4.000	No	Yes	2.00
893	58.60	32.96	2.71	1.72	0.91	15.23	4.08	62.16	4.000	No	Yes	2.00
894	58.66	33.04	2.70	1.64	0.90	15.31	3.99	61.04	4.000	No	Yes	2.00
895	58.75	32.78	2.69	1.56	0.90	15.19	3.93	59.62	4.000	No	Yes	2.00
896	58.80	31.98	2.70	1.53	0.90	14.73	3.98	58.57	4.000	No	Yes	2.00
897	58.88	30.93	2.71	1.53	0.91	14.12	4.09	57.74	4.000	No	Yes	2.00
898	58.97	29.66	2.73	1.54	0.92	13.38	4.25	56.89	4.000	No	Yes	2.00
899	59.02	28.78	2.74	1.50	0.92	12.89	4.32	55.64	4.000	No	Yes	2.00
900	59.06	28.25	2.74	1.45	0.92	12.61	4.32	54.47	4.000	No	Yes	2.00
901	59.12	27.98	2.74	1.38	0.92	12.49	4.26	53.25	4.000	No	Yes	2.00
902	59.20	28.12	2.72	1.31	0.91	12.60	4.15	52.31	4.000	No	Yes	2.00
903	59.26	28.04	2.72	1.29	0.91	12.55	4.14	51.90	4.000	No	Yes	2.00
904	59.35	28.00	2.72	1.29	0.91	12.51	4.14	51.82	4.000	No	Yes	2.00
905	59.41	28.02	2.72	1.31	0.91	12.50	4.17	52.14	4.000	No	Yes	2.00
906	59.46	28.08	2.73	1.34	0.92	12.51	4.21	52.66	4.000	No	Yes	2.00
907	59.52	28.38	2.73	1.38	0.92	12.65	4.22	53.41	4.000	No	Yes	2.00
908	59.61	28.81	2.73	1.42	0.92	12.85	4.22	54.27	4.000	No	Yes	2.00
909	59.68	29.23	2.73	1.45	0.92	13.06	4.21	54.99	4.000	No	Yes	2.00
910	59.72	29.44	2.73	1.49	0.92	13.14	4.24	55.77	4.000	No	Yes	2.00
911	59.79	29.54	2.74	1.53	0.92	13.16	4.29	56.42	4.000	No	Yes	2.00
912	59.86	29.55	2.75	1.57	0.92	13.13	4.34	56.94	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
913	59.91	29.54	2.72	1.43	0.91	13.20	4.16	54.87	4.000	No	Yes	2.00
914	60.01	29.54	2.69	1.26	0.90	13.28	3.95	52.42	4.000	Yes	Yes	2.00
915	60.06	29.43	2.66	1.10	0.89	13.32	3.73	49.70	4.000	Yes	Yes	2.00
916	60.15	29.33	2.63	0.92	0.88	13.39	3.48	46.66	4.000	Yes	Yes	2.00
917	60.19	29.08	2.58	0.74	0.86	13.40	3.22	43.20	4.000	Yes	No	2.00
918	60.26	29.01	2.53	0.55	0.84	13.54	2.91	39.48	4.000	Yes	No	2.00
919	60.35	28.68	2.47	0.37	0.81	13.58	2.60	35.31	4.000	Yes	No	2.00
920	60.40	28.68	2.38	0.18	0.78	13.89	2.22	30.80	4.000	Yes	No	2.00
921	60.45	28.56	N/A	0.00	1.00	-1.00	1.00	N/A	4.000	No	No	2.00
922	60.51	29.38	N/A	0.00	1.00	-1.00	1.00	N/A	4.000	No	No	2.00

Abbreviations

Depth: Depth from free surface, at which CPT was performed (ft)
q_t: Total cone resistance
I_c: Soil behavior type index
Fr: Normalized friction ratio (%)
n: Stress exponent
Q_{tn}: Normalized cone resistance
K_c: Cone resistance correction factor due to fines
$Q_{tn,cs}$: Normalized and adjusted cone resistance
$CRR_{7.5}$: Cyclic resistance ratio for M_w=7.5
FS: Factor of safety against soil liquefaction

:: Liquefaction Potential Index calculation data ::

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
0.09	2.00	0.00	0.00	0.02	0.00	0.15	2.00	0.00	0.00	0.02	0.00
0.21	2.00	0.00	0.00	0.02	0.00	0.29	2.00	0.00	0.00	0.02	0.00
0.34	2.00	0.00	0.00	0.02	0.00	0.40	2.00	0.00	0.00	0.02	0.00
0.49	2.00	0.00	0.00	0.03	0.00	0.55	2.00	0.00	0.00	0.02	0.00
0.59	2.00	0.00	0.00	0.01	0.00	0.69	2.00	0.00	0.00	0.03	0.00
0.74	2.00	0.00	0.00	0.02	0.00	0.81	2.00	0.00	0.00	0.02	0.00
0.89	2.00	0.00	0.00	0.02	0.00	0.94	2.00	0.00	0.00	0.02	0.00
0.99	2.00	0.00	0.00	0.02	0.00	1.09	2.00	0.00	0.00	0.03	0.00
1.14	2.00	0.00	0.00	0.02	0.00	1.19	2.00	0.00	0.00	0.02	0.00
1.26	2.00	0.00	0.00	0.02	0.00	1.34	2.00	0.00	0.00	0.02	0.00
1.38	2.00	0.00	0.00	0.01	0.00	1.50	2.00	0.00	0.00	0.04	0.00
1.53	2.00	0.00	0.00	0.01	0.00	1.59	2.00	0.00	0.00	0.02	0.00
1.68	2.00	0.00	0.00	0.03	0.00	1.72	2.00	0.00	0.00	0.01	0.00
1.78	2.00	0.00	0.00	0.02	0.00	1.87	2.00	0.00	0.00	0.03	0.00
1.93	2.00	0.00	0.00	0.02	0.00	1.98	2.00	0.00	0.00	0.02	0.00
2.06	2.00	0.00	0.00	0.02	0.00	2.13	2.00	0.00	0.00	0.02	0.00
2.17	2.00	0.00	0.00	0.01	0.00	2.28	2.00	0.00	0.00	0.03	0.00
2.32	2.00	0.00	0.00	0.01	0.00	2.39	2.00	0.00	0.00	0.02	0.00
2.43	2.00	0.00	0.00	0.01	0.00	2.52	2.00	0.00	0.00	0.03	0.00
2.57	2.00	0.00	0.00	0.02	0.00	2.66	2.00	0.00	0.00	0.03	0.00
2.69	2.00	0.00	0.00	0.01	0.00	2.77	2.00	0.00	0.00	0.02	0.00
2.86	2.00	0.00	0.00	0.03	0.00	2.92	2.00	0.00	0.00	0.02	0.00
2.96	2.00	0.00	0.00	0.01	0.00	3.06	2.00	0.00	0.00	0.03	0.00
3.11	2.00	0.00	0.00	0.02	0.00	3.15	2.00	0.00	0.00	0.01	0.00
3.26	2.00	0.00	0.00	0.03	0.00	3.30	2.00	0.00	0.00	0.01	0.00
3.37	2.00	0.00	0.00	0.02	0.00	3.46	2.00	0.00	0.00	0.03	0.00
3.51	2.00	0.00	0.00	0.02	0.00	3.56	2.00	0.00	0.00	0.02	0.00
3.64	2.00	0.00	0.00	0.02	0.00	3.71	2.00	0.00	0.00	0.02	0.00
3.76	2.00	0.00	0.00	0.02	0.00	3.81	2.00	0.00	0.00	0.02	0.00
3.90	2.00	0.00	0.00	0.03	0.00	3.94	2.00	0.00	0.00	0.01	0.00
4.01	2.00	0.00	0.00	0.02	0.00	4.09	2.00	0.00	0.00	0.02	0.00
4.15	2.00	0.00	0.00	0.02	0.00	4.20	2.00	0.00	0.00	0.02	0.00
4.30	2.00	0.00	0.00	0.03	0.00	4.35	2.00	0.00	0.00	0.02	0.00
4.41	2.00	0.00	0.00	0.02	0.00	4.50	2.00	0.00	0.00	0.03	0.00
4.55	2.00	0.00	0.00	0.02	0.00	4.60	2.00	0.00	0.00	0.02	0.00
4.68	2.00	0.00	0.00	0.02	0.00	4.75	2.00	0.00	0.00	0.02	0.00
4.79	2.00	0.00	0.00	0.01	0.00	4.88	2.00	0.00	0.00	0.03	0.00
4.95	2.00	0.00	0.00	0.02	0.00	4.99	2.00	0.00	0.00	0.01	0.00
5.06	2.00	0.00	0.00	0.02	0.00	5.14	2.00	0.00	0.00	0.02	0.00
5.21	2.00	0.00	0.00	0.02	0.00	5.26	2.00	0.00	0.00	0.02	0.00
5.33	2.00	0.00	0.00	0.02	0.00	5.40	2.00	0.00	0.00	0.02	0.00
5.45	2.00	0.00	0.00	0.02	0.00	5.51	2.00	0.00	0.00	0.02	0.00
5.60	2.00	0.00	0.00	0.03	0.00	5.66	2.00	0.00	0.00	0.02	0.00
5.71	2.00	0.00	0.00	0.02	0.00	5.78	2.00	0.00	0.00	0.02	0.00
5.86	2.00	0.00	0.00	0.02	0.00	5.93	2.00	0.00	0.00	0.02	0.00
6.01	2.00	0.00	0.00	0.02	0.00	6.05	2.00	0.00	0.00	0.01	0.00
6.11	2.00	0.00	0.00	0.02	0.00	6.21	2.00	0.00	0.00	0.03	0.00
6.25	2.00	0.00	0.00	0.01	0.00	6.31	2.00	0.00	0.00	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
6.39	2.00	0.00	0.00	0.02	0.00	6.45	2.00	0.00	0.00	0.02	0.00
6.51	2.00	0.00	0.00	0.02	0.00	6.58	2.00	0.00	0.00	0.02	0.00
6.66	2.00	0.00	0.00	0.02	0.00	6.70	2.00	0.00	0.00	0.01	0.00
6.78	2.00	0.00	0.00	0.02	0.00	6.85	2.00	0.00	0.00	0.02	0.00
6.89	2.00	0.00	0.00	0.01	0.00	7.00	2.00	0.00	0.00	0.03	0.00
7.03	2.00	0.00	0.00	0.01	0.00	7.10	2.00	0.00	0.00	0.02	0.00
7.19	2.00	0.00	0.00	0.03	0.00	7.25	2.00	0.00	0.00	0.02	0.00
7.30	2.00	0.00	0.00	0.02	0.00	7.37	2.00	0.00	0.00	0.02	0.00
7.44	2.00	0.00	0.00	0.02	0.00	7.49	2.00	0.00	0.00	0.02	0.00
7.56	2.00	0.00	0.00	0.02	0.00	7.64	2.00	0.00	0.00	0.02	0.00
7.68	2.00	0.00	0.00	0.01	0.00	7.79	2.00	0.00	0.00	0.03	0.00
7.83	2.00	0.00	0.00	0.01	0.00	7.90	2.00	0.00	0.00	0.02	0.00
7.98	2.00	0.00	0.00	0.02	0.00	8.02	2.00	0.00	0.00	0.01	0.00
8.09	2.00	0.00	0.00	0.02	0.00	8.15	2.00	0.00	0.00	0.02	0.00
8.23	2.00	0.00	0.00	0.02	0.00	8.29	2.00	0.00	0.00	0.02	0.00
8.34	2.00	0.00	0.00	0.02	0.00	8.41	2.00	0.00	0.00	0.02	0.00
8.48	2.00	0.00	0.00	0.02	0.00	8.55	2.00	0.00	0.00	0.02	0.00
8.60	2.00	0.00	0.00	0.02	0.00	8.66	2.00	0.00	0.00	0.02	0.00
8.74	2.00	0.00	0.00	0.02	0.00	8.83	2.00	0.00	0.00	0.03	0.00
8.90	2.00	0.00	0.00	0.02	0.00	8.94	2.00	0.00	0.00	0.01	0.00
9.01	2.00	0.00	0.00	0.02	0.00	9.09	2.00	0.00	0.00	0.02	0.00
9.15	2.00	0.00	0.00	0.02	0.00	9.20	2.00	0.00	0.00	0.02	0.00
9.29	2.00	0.00	0.00	0.03	0.00	9.35	2.00	0.00	0.00	0.02	0.00
9.39	2.00	0.00	0.00	0.01	0.00	9.45	2.00	0.00	0.00	0.02	0.00
9.55	2.00	0.00	0.00	0.03	0.00	9.64	2.00	0.00	0.00	0.03	0.00
9.65	2.00	0.00	0.00	0.00	0.00	9.73	2.00	0.00	0.00	0.02	0.00
9.79	2.00	0.00	0.00	0.02	0.00	9.84	2.00	0.00	0.00	0.02	0.00
9.91	2.00	0.00	0.00	0.02	0.00	9.99	2.00	0.00	0.00	0.02	0.00
10.08	2.00	0.00	0.00	0.03	0.00	10.14	2.00	0.00	0.00	0.02	0.00
10.19	2.00	0.00	0.00	0.02	0.00	10.25	2.00	0.00	0.00	0.02	0.00
10.34	2.00	0.00	0.00	0.03	0.00	10.38	2.00	0.00	0.00	0.01	0.00
10.44	2.00	0.00	0.00	0.02	0.00	10.52	2.00	0.00	0.00	0.02	0.00
10.59	2.00	0.00	0.00	0.02	0.00	10.63	2.00	0.00	0.00	0.01	0.00
10.70	2.00	0.00	0.00	0.02	0.00	10.78	2.00	0.00	0.00	0.02	0.00
10.87	2.00	0.00	0.00	0.03	0.00	10.93	0.75	0.00	0.00	0.02	0.04
10.97	0.75	0.00	0.00	0.01	0.03	11.03	0.76	0.00	0.00	0.02	0.04
11.12	0.77	0.00	0.00	0.03	0.05	11.16	0.78	0.00	0.00	0.01	0.02
11.23	0.79	0.00	0.00	0.02	0.04	11.31	0.80	0.00	0.00	0.02	0.04
11.37	0.82	0.00	0.00	0.02	0.03	11.44	0.84	0.00	0.00	0.02	0.03
11.51	0.86	0.00	0.00	0.02	0.03	11.56	0.87	0.00	0.00	0.02	0.02
11.63	0.88	0.00	0.00	0.02	0.02	11.71	0.88	0.00	0.00	0.02	0.02
11.76	0.89	0.00	0.00	0.02	0.01	11.83	0.89	0.00	0.00	0.02	0.02
11.91	0.89	0.00	0.00	0.02	0.02	11.94	0.89	0.00	0.00	0.01	0.01
12.05	2.00	0.00	0.00	0.03	0.00	12.10	2.00	0.00	0.00	0.02	0.00
12.14	2.00	0.00	0.00	0.01	0.00	12.25	2.00	0.00	0.00	0.03	0.00
12.29	2.00	0.00	0.00	0.01	0.00	12.35	2.00	0.00	0.00	0.02	0.00
12.44	2.00	0.00	0.00	0.03	0.00	12.49	2.00	0.00	0.00	0.02	0.00
12.55	2.00	0.00	0.00	0.02	0.00	12.61	2.00	0.00	0.00	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
12.70	2.00	0.00	0.00	0.03	0.00	12.75	2.00	0.00	0.00	0.02	0.00
12.81	2.00	0.00	0.00	0.02	0.00	12.89	2.00	0.00	0.00	0.02	0.00
12.94	2.00	0.00	0.00	0.02	0.00	12.99	2.00	0.00	0.00	0.02	0.00
13.08	2.00	0.00	0.00	0.03	0.00	13.15	2.00	0.00	0.00	0.02	0.00
13.20	2.00	0.00	0.00	0.02	0.00	13.27	2.00	0.00	0.00	0.02	0.00
13.32	2.00	0.00	0.00	0.02	0.00	13.39	2.00	0.00	0.00	0.02	0.00
13.48	2.00	0.00	0.00	0.03	0.00	13.54	2.00	0.00	0.00	0.02	0.00
13.59	2.00	0.00	0.00	0.02	0.00	13.65	2.00	0.00	0.00	0.02	0.00
13.74	2.00	0.00	0.00	0.03	0.00	13.80	2.00	0.00	0.00	0.02	0.00
13.89	2.00	0.00	0.00	0.03	0.00	13.93	2.00	0.00	0.00	0.01	0.00
13.99	2.00	0.00	0.00	0.02	0.00	14.07	2.00	0.00	0.00	0.02	0.00
14.12	2.00	0.00	0.00	0.02	0.00	14.18	2.00	0.00	0.00	0.02	0.00
14.26	2.00	0.00	0.00	0.02	0.00	14.34	2.00	0.00	0.00	0.02	0.00
14.38	2.00	0.00	0.00	0.01	0.00	14.47	2.00	0.00	0.00	0.03	0.00
14.53	2.00	0.00	0.00	0.02	0.00	14.57	2.00	0.00	0.00	0.01	0.00
14.64	2.00	0.00	0.00	0.02	0.00	14.72	2.00	0.00	0.00	0.02	0.00
14.80	2.00	0.00	0.00	0.02	0.00	14.83	2.00	0.00	0.00	0.01	0.00
14.92	2.00	0.00	0.00	0.03	0.00	14.97	2.00	0.00	0.00	0.02	0.00
15.06	2.00	0.00	0.00	0.03	0.00	15.10	2.00	0.00	0.00	0.01	0.00
15.17	2.00	0.00	0.00	0.02	0.00	15.25	2.00	0.00	0.00	0.02	0.00
15.31	2.00	0.00	0.00	0.02	0.00	15.37	2.00	0.00	0.00	0.02	0.00
15.44	2.00	0.00	0.00	0.02	0.00	15.51	2.00	0.00	0.00	0.02	0.00
15.56	2.00	0.00	0.00	0.02	0.00	15.63	2.00	0.00	0.00	0.02	0.00
15.71	2.00	0.00	0.00	0.02	0.00	15.76	0.92	0.00	0.00	0.02	0.01
15.82	0.96	0.00	0.00	0.02	0.01	15.90	1.00	0.00	0.00	0.02	0.00
15.95	1.04	0.00	0.00	0.02	0.00	16.01	1.06	0.00	0.00	0.02	0.00
16.10	2.00	0.00	0.00	0.03	0.00	16.16	2.00	0.00	0.00	0.02	0.00
16.21	2.00	0.00	0.00	0.02	0.00	16.29	2.00	0.00	0.00	0.02	0.00
16.36	2.00	0.00	0.00	0.02	0.00	16.41	2.00	0.00	0.00	0.02	0.00
16.49	1.09	0.00	0.00	0.02	0.00	16.55	1.11	0.00	0.00	0.02	0.00
16.60	1.14	0.00	0.00	0.02	0.00	16.70	2.00	0.00	0.00	0.03	0.00
16.74	2.00	0.00	0.00	0.01	0.00	16.80	2.00	0.00	0.00	0.02	0.00
16.89	2.00	0.00	0.00	0.03	0.00	16.93	2.00	0.00	0.00	0.01	0.00
17.00	2.00	0.00	0.00	0.02	0.00	17.09	2.00	0.00	0.00	0.03	0.00
17.14	2.00	0.00	0.00	0.02	0.00	17.20	2.00	0.00	0.00	0.02	0.00
17.28	2.00	0.00	0.00	0.02	0.00	17.34	2.00	0.00	0.00	0.02	0.00
17.41	2.00	0.00	0.00	0.02	0.00	17.48	2.00	0.00	0.00	0.02	0.00
17.56	2.00	0.00	0.00	0.02	0.00	17.62	2.00	0.00	0.00	0.02	0.00
17.67	2.00	0.00	0.00	0.02	0.00	17.72	2.00	0.00	0.00	0.02	0.00
17.78	2.00	0.00	0.00	0.02	0.00	17.87	2.00	0.00	0.00	0.03	0.00
17.94	2.00	0.00	0.00	0.02	0.00	18.01	2.00	0.00	0.00	0.02	0.00
18.06	2.00	0.00	0.00	0.02	0.00	18.12	2.00	0.00	0.00	0.02	0.00
18.21	0.82	0.00	0.00	0.03	0.04	18.25	0.84	0.00	0.00	0.01	0.01
18.31	0.84	0.00	0.00	0.02	0.02	18.40	2.00	0.00	0.00	0.03	0.00
18.44	2.00	0.00	0.00	0.01	0.00	18.51	2.00	0.00	0.00	0.02	0.00
18.58	2.00	0.00	0.00	0.02	0.00	18.64	2.00	0.00	0.00	0.02	0.00
18.71	2.00	0.00	0.00	0.02	0.00	18.80	2.00	0.00	0.00	0.03	0.00
18.86	2.00	0.00	0.00	0.02	0.00	18.91	2.00	0.00	0.00	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
18.98	2.00	0.00	0.00	0.02	0.00	19.05	2.00	0.00	0.00	0.02	0.00
19.10	2.00	0.00	0.00	0.02	0.00	19.20	2.00	0.00	0.00	0.03	0.00
19.23	2.00	0.00	0.00	0.01	0.00	19.30	2.00	0.00	0.00	0.02	0.00
19.39	2.00	0.00	0.00	0.03	0.00	19.43	2.00	0.00	0.00	0.01	0.00
19.50	2.00	0.00	0.00	0.02	0.00	19.57	2.00	0.00	0.00	0.02	0.00
19.63	2.00	0.00	0.00	0.02	0.00	19.70	1.29	0.00	0.00	0.02	0.00
19.77	1.37	0.00	0.00	0.02	0.00	19.84	1.35	0.00	0.00	0.02	0.00
19.90	1.35	0.00	0.00	0.02	0.00	19.99	2.00	0.00	0.00	0.03	0.00
20.02	2.00	0.00	0.00	0.01	0.00	20.09	2.00	0.00	0.00	0.02	0.00
20.19	2.00	0.00	0.00	0.03	0.00	20.21	2.00	0.00	0.00	0.01	0.00
20.29	2.00	0.00	0.00	0.02	0.00	20.38	2.00	0.00	0.00	0.03	0.00
20.42	2.00	0.00	0.00	0.01	0.00	20.52	2.00	0.00	0.00	0.03	0.00
20.55	2.00	0.00	0.00	0.01	0.00	20.62	2.00	0.00	0.00	0.02	0.00
20.68	2.00	0.00	0.00	0.02	0.00	20.75	2.00	0.00	0.00	0.02	0.00
20.81	2.00	0.00	0.00	0.02	0.00	20.90	2.00	0.00	0.00	0.03	0.00
20.96	2.00	0.00	0.00	0.02	0.00	21.01	2.00	0.00	0.00	0.02	0.00
21.09	2.00	0.00	0.00	0.02	0.00	21.15	2.00	0.00	0.00	0.02	0.00
21.21	2.00	0.00	0.00	0.02	0.00	21.30	1.40	0.00	0.00	0.03	0.00
21.36	1.41	0.00	0.00	0.02	0.00	21.40	1.41	0.00	0.00	0.01	0.00
21.49	1.42	0.00	0.00	0.03	0.00	21.56	2.00	0.00	0.00	0.02	0.00
21.60	2.00	0.00	0.00	0.01	0.00	21.66	2.00	0.00	0.00	0.02	0.00
21.75	2.00	0.00	0.00	0.03	0.00	21.80	2.00	0.00	0.00	0.02	0.00
21.85	2.00	0.00	0.00	0.02	0.00	21.95	2.00	0.00	0.00	0.03	0.00
21.99	2.00	0.00	0.00	0.01	0.00	22.05	2.00	0.00	0.00	0.02	0.00
22.14	1.58	0.00	0.00	0.03	0.00	22.19	1.45	0.00	0.00	0.02	0.00
22.26	1.29	0.00	0.00	0.02	0.00	22.35	1.13	0.00	0.00	0.03	0.00
22.44	0.99	0.00	0.00	0.03	0.00	22.45	0.88	0.00	0.00	0.00	0.00
22.54	0.79	0.00	0.00	0.03	0.04	22.58	0.73	0.00	0.00	0.01	0.02
22.65	0.71	0.00	0.00	0.02	0.04	22.73	2.00	0.00	0.00	0.02	0.00
22.79	2.00	0.00	0.00	0.02	0.00	22.85	0.77	0.00	0.00	0.02	0.03
22.93	0.86	0.00	0.00	0.02	0.02	22.99	0.98	0.00	0.00	0.02	0.00
23.04	1.10	0.00	0.00	0.02	0.00	23.12	1.21	0.00	0.00	0.02	0.00
23.19	1.30	0.00	0.00	0.02	0.00	23.27	1.38	0.00	0.00	0.02	0.00
23.30	1.44	0.00	0.00	0.01	0.00	23.38	1.48	0.00	0.00	0.02	0.00
23.47	1.47	0.00	0.00	0.03	0.00	23.50	1.42	0.00	0.00	0.01	0.00
23.58	1.35	0.00	0.00	0.02	0.00	23.66	1.28	0.00	0.00	0.02	0.00
23.69	1.23	0.00	0.00	0.01	0.00	23.77	1.21	0.00	0.00	0.02	0.00
23.84	1.20	0.00	0.00	0.02	0.00	23.92	1.20	0.00	0.00	0.02	0.00
23.97	1.21	0.00	0.00	0.02	0.00	24.06	1.21	0.00	0.00	0.03	0.00
24.12	1.23	0.00	0.00	0.02	0.00	24.17	1.25	0.00	0.00	0.02	0.00
24.23	1.25	0.00	0.00	0.02	0.00	24.31	1.23	0.00	0.00	0.02	0.00
24.36	1.20	0.00	0.00	0.02	0.00	24.42	1.15	0.00	0.00	0.02	0.00
24.51	1.09	0.00	0.00	0.03	0.00	24.54	1.02	0.00	0.00	0.01	0.00
24.62	2.00	0.00	0.00	0.02	0.00	24.71	2.00	0.00	0.00	0.03	0.00
24.74	2.00	0.00	0.00	0.01	0.00	24.81	2.00	0.00	0.00	0.02	0.00
24.89	2.00	0.00	0.00	0.02	0.00	24.96	2.00	0.00	0.00	0.02	0.00
25.01	2.00	0.00	0.00	0.02	0.00	25.10	2.00	0.00	0.00	0.03	0.00
25.14	2.00	0.00	0.00	0.01	0.00	25.21	2.00	0.00	0.00	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
25.30	2.00	0.00	0.00	0.03	0.00	25.34	2.00	0.00	0.00	0.01	0.00
25.41	2.00	0.00	0.00	0.02	0.00	25.50	2.00	0.00	0.00	0.03	0.00
25.55	2.00	0.00	0.00	0.02	0.00	25.60	2.00	0.00	0.00	0.02	0.00
25.70	2.00	0.00	0.00	0.03	0.00	25.75	2.00	0.00	0.00	0.02	0.00
25.80	2.00	0.00	0.00	0.02	0.00	25.89	2.00	0.00	0.00	0.03	0.00
25.95	2.00	0.00	0.00	0.02	0.00	25.99	2.00	0.00	0.00	0.01	0.00
26.06	2.00	0.00	0.00	0.02	0.00	26.15	2.00	0.00	0.00	0.03	0.00
26.19	2.00	0.00	0.00	0.01	0.00	26.25	2.00	0.00	0.00	0.02	0.00
26.34	2.00	0.00	0.00	0.03	0.00	26.38	2.00	0.00	0.00	0.01	0.00
26.45	2.00	0.00	0.00	0.02	0.00	26.52	2.00	0.00	0.00	0.02	0.00
26.61	2.00	0.00	0.00	0.03	0.00	26.67	2.00	0.00	0.00	0.02	0.00
26.72	2.00	0.00	0.00	0.02	0.00	26.82	2.00	0.00	0.00	0.03	0.00
26.86	2.00	0.00	0.00	0.01	0.00	26.94	2.00	0.00	0.00	0.02	0.00
26.98	2.00	0.00	0.00	0.01	0.00	27.06	2.00	0.00	0.00	0.02	0.00
27.10	2.00	0.00	0.00	0.01	0.00	27.17	2.00	0.00	0.00	0.02	0.00
27.26	2.00	0.00	0.00	0.03	0.00	27.31	2.00	0.00	0.00	0.02	0.00
27.39	2.00	0.00	0.00	0.02	0.00	27.44	2.00	0.00	0.00	0.02	0.00
27.51	2.00	0.00	0.00	0.02	0.00	27.58	2.00	0.00	0.00	0.02	0.00
27.63	2.00	0.00	0.00	0.02	0.00	27.71	2.00	0.00	0.00	0.02	0.00
27.79	2.00	0.00	0.00	0.02	0.00	27.86	2.00	0.00	0.00	0.02	0.00
27.89	2.00	0.00	0.00	0.01	0.00	27.96	2.00	0.00	0.00	0.02	0.00
28.05	2.00	0.00	0.00	0.03	0.00	28.09	2.00	0.00	0.00	0.01	0.00
28.16	2.00	0.00	0.00	0.02	0.00	28.23	2.00	0.00	0.00	0.02	0.00
28.29	2.00	0.00	0.00	0.02	0.00	28.35	2.00	0.00	0.00	0.02	0.00
28.44	2.00	0.00	0.00	0.03	0.00	28.50	2.00	0.00	0.00	0.02	0.00
28.55	2.00	0.00	0.00	0.02	0.00	28.64	2.00	0.00	0.00	0.03	0.00
28.69	2.00	0.00	0.00	0.02	0.00	28.75	2.00	0.00	0.00	0.02	0.00
28.82	2.00	0.00	0.00	0.02	0.00	28.89	2.00	0.00	0.00	0.02	0.00
28.98	2.00	0.00	0.00	0.03	0.00	29.04	2.00	0.00	0.00	0.02	0.00
29.08	2.00	0.00	0.00	0.01	0.00	29.15	2.00	0.00	0.00	0.02	0.00
29.24	2.00	0.00	0.00	0.03	0.00	29.29	2.00	0.00	0.00	0.02	0.00
29.34	2.00	0.00	0.00	0.02	0.00	29.43	2.00	0.00	0.00	0.03	0.00
29.47	2.00	0.00	0.00	0.01	0.00	29.53	2.00	0.00	0.00	0.02	0.00
29.62	2.00	0.00	0.00	0.03	0.00	29.66	2.00	0.00	0.00	0.01	0.00
29.77	2.00	0.00	0.00	0.03	0.00	29.81	2.00	0.00	0.00	0.01	0.00
29.86	2.00	0.00	0.00	0.02	0.00	29.92	2.00	0.00	0.00	0.02	0.00
30.01	2.00	0.00	0.00	0.03	0.00	30.09	2.00	0.00	0.00	0.02	0.00
30.17	2.00	0.00	0.00	0.02	0.00	30.20	2.00	0.00	0.00	0.01	0.00
30.27	2.00	0.00	0.00	0.02	0.00	30.32	2.00	0.00	0.00	0.02	0.00
30.39	2.00	0.00	0.00	0.02	0.00	30.47	2.00	0.00	0.00	0.02	0.00
30.55	2.00	0.00	0.00	0.02	0.00	30.62	2.00	0.00	0.00	0.02	0.00
30.66	2.00	0.00	0.00	0.01	0.00	30.72	2.00	0.00	0.00	0.02	0.00
30.81	2.00	0.00	0.00	0.03	0.00	30.85	2.00	0.00	0.00	0.01	0.00
30.91	2.00	0.00	0.00	0.02	0.00	31.01	2.00	0.00	0.00	0.03	0.00
31.05	2.00	0.00	0.00	0.01	0.00	31.11	2.00	0.00	0.00	0.02	0.00
31.20	2.00	0.00	0.00	0.03	0.00	31.26	2.00	0.00	0.00	0.02	0.00
31.31	2.00	0.00	0.00	0.02	0.00	31.38	2.00	0.00	0.00	0.02	0.00
31.46	2.00	0.00	0.00	0.02	0.00	31.51	2.00	0.00	0.00	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
31.60	2.00	0.00	0.00	0.03	0.00	31.65	2.00	0.00	0.00	0.02	0.00
31.74	2.00	0.00	0.00	0.03	0.00	31.80	2.00	0.00	0.00	0.02	0.00
31.85	2.00	0.00	0.00	0.02	0.00	31.89	2.00	0.00	0.00	0.01	0.00
32.00	2.00	0.00	0.00	0.03	0.00	32.04	2.00	0.00	0.00	0.01	0.00
32.09	2.00	0.00	0.00	0.02	0.00	32.19	2.00	0.00	0.00	0.03	0.00
32.23	2.00	0.00	0.00	0.01	0.00	32.29	2.00	0.00	0.00	0.02	0.00
32.37	2.00	0.00	0.00	0.02	0.00	32.44	2.00	0.00	0.00	0.02	0.00
32.49	2.00	0.00	0.00	0.02	0.00	32.58	2.00	0.00	0.00	0.03	0.00
32.62	2.00	0.00	0.00	0.01	0.00	32.69	2.00	0.00	0.00	0.02	0.00
32.78	2.00	0.00	0.00	0.03	0.00	32.82	2.00	0.00	0.00	0.01	0.00
32.89	2.00	0.00	0.00	0.02	0.00	32.97	2.00	0.00	0.00	0.02	0.00
33.02	2.00	0.00	0.00	0.02	0.00	33.09	2.00	0.00	0.00	0.02	0.00
33.15	2.00	0.00	0.00	0.02	0.00	33.20	2.00	0.00	0.00	0.02	0.00
33.28	2.00	0.00	0.00	0.02	0.00	33.38	2.00	0.00	0.00	0.03	0.00
33.43	2.00	0.00	0.00	0.02	0.00	33.47	2.00	0.00	0.00	0.01	0.00
33.57	2.00	0.00	0.00	0.03	0.00	33.63	2.00	0.00	0.00	0.02	0.00
33.70	2.00	0.00	0.00	0.02	0.00	33.74	2.00	0.00	0.00	0.01	0.00
33.82	2.00	0.00	0.00	0.02	0.00	33.86	2.00	0.00	0.00	0.01	0.00
33.93	2.00	0.00	0.00	0.02	0.00	34.02	2.00	0.00	0.00	0.03	0.00
34.06	2.00	0.00	0.00	0.01	0.00	34.13	2.00	0.00	0.00	0.02	0.00
34.21	2.00	0.00	0.00	0.02	0.00	34.28	2.00	0.00	0.00	0.02	0.00
34.32	2.00	0.00	0.00	0.01	0.00	34.41	2.00	0.00	0.00	0.03	0.00
34.46	2.00	0.00	0.00	0.02	0.00	34.52	2.00	0.00	0.00	0.02	0.00
34.61	2.00	0.00	0.00	0.03	0.00	34.65	2.00	0.00	0.00	0.01	0.00
34.71	2.00	0.00	0.00	0.02	0.00	34.79	2.00	0.00	0.00	0.02	0.00
34.86	2.00	0.00	0.00	0.02	0.00	34.93	2.00	0.00	0.00	0.02	0.00
35.01	2.00	0.00	0.00	0.02	0.00	35.06	2.00	0.00	0.00	0.02	0.00
35.11	2.00	0.00	0.00	0.02	0.00	35.18	2.00	0.00	0.00	0.02	0.00
35.26	2.00	0.00	0.00	0.02	0.00	35.34	2.00	0.00	0.00	0.02	0.00
35.40	2.00	0.00	0.00	0.02	0.00	35.44	2.00	0.00	0.00	0.01	0.00
35.51	2.00	0.00	0.00	0.02	0.00	35.58	2.00	0.00	0.00	0.02	0.00
35.66	2.00	0.00	0.00	0.02	0.00	35.71	2.00	0.00	0.00	0.02	0.00
35.77	2.00	0.00	0.00	0.02	0.00	35.85	2.00	0.00	0.00	0.02	0.00
35.92	2.00	0.00	0.00	0.02	0.00	35.97	2.00	0.00	0.00	0.02	0.00
36.03	2.00	0.00	0.00	0.02	0.00	36.11	2.00	0.00	0.00	0.02	0.00
36.16	2.00	0.00	0.00	0.02	0.00	36.26	2.00	0.00	0.00	0.03	0.00
36.31	2.00	0.00	0.00	0.02	0.00	36.36	2.00	0.00	0.00	0.02	0.00
36.43	2.00	0.00	0.00	0.02	0.00	36.51	2.00	0.00	0.00	0.02	0.00
36.55	2.00	0.00	0.00	0.01	0.00	36.65	2.00	0.00	0.00	0.03	0.00
36.71	2.00	0.00	0.00	0.02	0.00	36.76	2.00	0.00	0.00	0.02	0.00
36.85	2.00	0.00	0.00	0.03	0.00	36.89	2.00	0.00	0.00	0.01	0.00
36.96	2.00	0.00	0.00	0.02	0.00	37.02	2.00	0.00	0.00	0.02	0.00
37.11	2.00	0.00	0.00	0.03	0.00	37.15	2.00	0.00	0.00	0.01	0.00
37.24	2.00	0.00	0.00	0.03	0.00	37.31	2.00	0.00	0.00	0.02	0.00
37.35	2.00	0.00	0.00	0.01	0.00	37.43	2.00	0.00	0.00	0.02	0.00
37.51	2.00	0.00	0.00	0.02	0.00	37.55	2.00	0.00	0.00	0.01	0.00
37.60	0.41	0.59	0.40	0.05	0.04	37.67	0.40	0.60	0.39	0.07	0.05
37.75	0.40	0.60	0.38	0.08	0.06	37.81	0.39	0.61	0.38	0.06	0.05

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
37.88	0.38	0.62	0.37	0.07	0.06	37.93	0.38	0.62	0.37	0.05	0.04
38.00	0.38	0.62	0.37	0.07	0.06	38.08	0.40	0.60	0.39	0.08	0.06
38.14	0.44	0.56	0.42	0.06	0.04	38.20	0.50	0.50	0.48	0.06	0.04
38.26	2.00	0.00	0.00	0.02	0.00	38.34	2.00	0.00	0.00	0.02	0.00
38.43	2.00	0.00	0.00	0.03	0.00	38.45	2.00	0.00	0.00	0.01	0.00
38.53	2.00	0.00	0.00	0.02	0.00	38.62	2.00	0.00	0.00	0.03	0.00
38.65	2.00	0.00	0.00	0.01	0.00	38.72	1.59	0.00	0.00	0.02	0.00
38.80	1.75	0.00	0.00	0.02	0.00	38.88	1.89	0.00	0.00	0.02	0.00
38.93	2.00	0.00	0.00	0.02	0.00	39.01	2.00	0.00	0.00	0.02	0.00
39.07	2.00	0.00	0.00	0.02	0.00	39.12	2.00	0.00	0.00	0.02	0.00
39.20	2.00	0.00	0.00	0.02	0.00	39.27	2.00	0.00	0.00	0.02	0.00
39.31	2.00	0.00	0.00	0.01	0.00	39.38	2.00	0.00	0.00	0.02	0.00
39.45	2.00	0.00	0.00	0.02	0.00	39.51	2.00	0.00	0.00	0.02	0.00
39.57	2.00	0.00	0.00	0.02	0.00	39.64	2.00	0.00	0.00	0.02	0.00
39.72	2.00	0.00	0.00	0.02	0.00	39.79	2.00	0.00	0.00	0.02	0.00
39.84	2.00	0.00	0.00	0.02	0.00	39.90	2.00	0.00	0.00	0.02	0.00
39.96	2.00	0.00	0.00	0.02	0.00	40.06	2.00	0.00	0.00	0.03	0.00
40.13	2.00	0.00	0.00	0.02	0.00	40.17	2.00	0.00	0.00	0.01	0.00
40.26	2.00	0.00	0.00	0.03	0.00	40.31	2.00	0.00	0.00	0.02	0.00
40.36	2.00	0.00	0.00	0.02	0.00	40.43	2.00	0.00	0.00	0.02	0.00
40.51	1.91	0.00	0.00	0.02	0.00	40.56	1.79	0.00	0.00	0.02	0.00
40.64	1.66	0.00	0.00	0.02	0.00	40.70	1.55	0.00	0.00	0.02	0.00
40.75	1.44	0.00	0.00	0.02	0.00	40.83	1.34	0.00	0.00	0.02	0.00
40.88	1.27	0.00	0.00	0.02	0.00	40.95	1.20	0.00	0.00	0.02	0.00
41.03	1.18	0.00	0.00	0.02	0.00	41.08	1.21	0.00	0.00	0.02	0.00
41.15	1.24	0.00	0.00	0.02	0.00	41.24	1.31	0.00	0.00	0.03	0.00
41.28	1.33	0.00	0.00	0.01	0.00	41.35	1.33	0.00	0.00	0.02	0.00
41.41	1.31	0.00	0.00	0.02	0.00	41.48	1.28	0.00	0.00	0.02	0.00
41.55	1.25	0.00	0.00	0.02	0.00	41.63	1.22	0.00	0.00	0.02	0.00
41.68	1.17	0.00	0.00	0.02	0.00	41.74	1.12	0.00	0.00	0.02	0.00
41.83	1.08	0.00	0.00	0.03	0.00	41.87	1.07	0.00	0.00	0.01	0.00
41.98	1.07	0.00	0.00	0.03	0.00	42.02	1.08	0.00	0.00	0.01	0.00
42.10	1.09	0.00	0.00	0.02	0.00	42.14	1.11	0.00	0.00	0.01	0.00
42.22	1.13	0.00	0.00	0.02	0.00	42.29	1.15	0.00	0.00	0.02	0.00
42.38	1.16	0.00	0.00	0.03	0.00	42.41	1.18	0.00	0.00	0.01	0.00
42.46	1.19	0.00	0.00	0.02	0.00	42.57	1.19	0.00	0.00	0.03	0.00
42.61	1.19	0.00	0.00	0.01	0.00	42.68	1.19	0.00	0.00	0.02	0.00
42.76	1.18	0.00	0.00	0.02	0.00	42.80	1.17	0.00	0.00	0.01	0.00
42.87	1.16	0.00	0.00	0.02	0.00	42.92	1.14	0.00	0.00	0.02	0.00
42.98	1.11	0.00	0.00	0.02	0.00	43.06	1.06	0.00	0.00	0.02	0.00
43.11	1.00	0.00	0.00	0.02	0.00	43.18	0.94	0.00	0.00	0.02	0.00
43.26	0.88	0.00	0.00	0.02	0.01	43.32	0.82	0.00	0.00	0.02	0.01
43.39	2.00	0.00	0.00	0.02	0.00	43.46	2.00	0.00	0.00	0.02	0.00
43.52	2.00	0.00	0.00	0.02	0.00	43.61	2.00	0.00	0.00	0.03	0.00
43.64	2.00	0.00	0.00	0.01	0.00	43.70	2.00	0.00	0.00	0.02	0.00
43.79	2.00	0.00	0.00	0.03	0.00	43.84	2.00	0.00	0.00	0.02	0.00
43.90	2.00	0.00	0.00	0.02	0.00	43.97	2.00	0.00	0.00	0.02	0.00
44.05	2.00	0.00	0.00	0.02	0.00	44.10	2.00	0.00	0.00	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
44.18	2.00	0.00	0.00	0.02	0.00	44.24	2.00	0.00	0.00	0.02	0.00
44.30	2.00	0.00	0.00	0.02	0.00	44.38	2.00	0.00	0.00	0.02	0.00
44.45	2.00	0.00	0.00	0.02	0.00	44.49	2.00	0.00	0.00	0.01	0.00
44.57	2.00	0.00	0.00	0.02	0.00	44.64	2.00	0.00	0.00	0.02	0.00
44.72	2.00	0.00	0.00	0.02	0.00	44.79	2.00	0.00	0.00	0.02	0.00
44.84	2.00	0.00	0.00	0.02	0.00	44.92	2.00	0.00	0.00	0.02	0.00
44.96	2.00	0.00	0.00	0.01	0.00	45.03	2.00	0.00	0.00	0.02	0.00
45.09	2.00	0.00	0.00	0.02	0.00	45.19	2.00	0.00	0.00	0.03	0.00
45.23	2.00	0.00	0.00	0.01	0.00	45.28	2.00	0.00	0.00	0.02	0.00
45.38	2.00	0.00	0.00	0.03	0.00	45.43	2.00	0.00	0.00	0.02	0.00
45.48	0.64	0.36	0.72	0.05	0.02	45.58	2.00	0.00	0.00	0.03	0.00
45.62	2.00	0.00	0.00	0.01	0.00	45.67	2.00	0.00	0.00	0.02	0.00
45.78	2.00	0.00	0.00	0.03	0.00	45.82	2.00	0.00	0.00	0.01	0.00
45.88	2.00	0.00	0.00	0.02	0.00	45.98	2.00	0.00	0.00	0.03	0.00
46.02	2.00	0.00	0.00	0.01	0.00	46.07	2.00	0.00	0.00	0.02	0.00
46.17	2.00	0.00	0.00	0.03	0.00	46.21	2.00	0.00	0.00	0.01	0.00
46.27	2.00	0.00	0.00	0.02	0.00	46.37	2.00	0.00	0.00	0.03	0.00
46.39	2.00	0.00	0.00	0.01	0.00	46.47	2.00	0.00	0.00	0.02	0.00
46.57	2.00	0.00	0.00	0.03	0.00	46.62	2.00	0.00	0.00	0.02	0.00
46.67	2.00	0.00	0.00	0.02	0.00	46.77	2.00	0.00	0.00	0.03	0.00
46.82	2.00	0.00	0.00	0.02	0.00	46.90	2.00	0.00	0.00	0.02	0.00
46.92	2.00	0.00	0.00	0.01	0.00	47.01	2.00	0.00	0.00	0.03	0.00
47.05	2.00	0.00	0.00	0.01	0.00	47.12	2.00	0.00	0.00	0.02	0.00
47.21	2.00	0.00	0.00	0.03	0.00	47.28	2.00	0.00	0.00	0.02	0.00
47.32	2.00	0.00	0.00	0.01	0.00	47.40	2.00	0.00	0.00	0.02	0.00
47.45	2.00	0.00	0.00	0.02	0.00	47.55	2.00	0.00	0.00	0.03	0.00
47.58	2.00	0.00	0.00	0.01	0.00	47.66	2.00	0.00	0.00	0.02	0.00
47.74	2.00	0.00	0.00	0.02	0.00	47.80	2.00	0.00	0.00	0.02	0.00
47.85	2.00	0.00	0.00	0.02	0.00	47.93	2.00	0.00	0.00	0.02	0.00
47.98	2.00	0.00	0.00	0.02	0.00	48.04	0.65	0.35	0.76	0.06	0.02
48.11	0.65	0.35	0.74	0.07	0.02	48.20	0.65	0.35	0.74	0.09	0.03
48.24	0.65	0.35	0.75	0.04	0.01	48.30	0.65	0.35	0.76	0.06	0.02
48.39	0.65	0.35	0.76	0.09	0.02	48.44	0.66	0.34	0.77	0.05	0.01
48.53	0.66	0.34	0.79	0.09	0.02	48.59	0.67	0.33	0.81	0.06	0.02
48.64	0.68	0.32	0.85	0.05	0.01	48.70	0.69	0.31	0.90	0.06	0.01
48.78	0.71	0.00	0.00	0.02	0.02	48.82	0.72	0.00	0.00	0.01	0.01
48.89	0.74	0.00	0.00	0.02	0.01	48.98	0.75	0.00	0.00	0.03	0.02
49.05	0.76	0.00	0.00	0.02	0.01	49.09	0.77	0.00	0.00	0.01	0.01
49.16	0.78	0.00	0.00	0.02	0.01	49.24	0.79	0.00	0.00	0.02	0.01
49.31	0.80	0.00	0.00	0.02	0.01	49.38	0.82	0.00	0.00	0.02	0.01
49.43	0.82	0.00	0.00	0.02	0.01	49.52	0.82	0.00	0.00	0.03	0.01
49.58	0.80	0.00	0.00	0.02	0.01	49.63	0.78	0.00	0.00	0.02	0.01
49.71	0.76	0.00	0.00	0.02	0.01	49.77	2.00	0.00	0.00	0.02	0.00
49.82	2.00	0.00	0.00	0.02	0.00	49.88	2.00	0.00	0.00	0.02	0.00
49.97	2.00	0.00	0.00	0.03	0.00	50.01	2.00	0.00	0.00	0.01	0.00
50.07	2.00	0.00	0.00	0.02	0.00	50.17	2.00	0.00	0.00	0.03	0.00
50.22	2.00	0.00	0.00	0.02	0.00	50.29	2.00	0.00	0.00	0.02	0.00
50.37	2.00	0.00	0.00	0.02	0.00	50.42	2.00	0.00	0.00	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
50.47	2.00	0.00	0.00	0.02	0.00	50.57	2.00	0.00	0.00	0.03	0.00
50.63	2.00	0.00	0.00	0.02	0.00	50.68	2.00	0.00	0.00	0.02	0.00
50.73	2.00	0.00	0.00	0.02	0.00	50.79	2.00	0.00	0.00	0.02	0.00
50.88	2.00	0.00	0.00	0.03	0.00	50.93	2.00	0.00	0.00	0.02	0.00
51.03	2.00	0.00	0.00	0.03	0.00	51.07	2.00	0.00	0.00	0.01	0.00
51.14	2.00	0.00	0.00	0.02	0.00	51.23	2.00	0.00	0.00	0.03	0.00
51.27	2.00	0.00	0.00	0.01	0.00	51.33	2.00	0.00	0.00	0.02	0.00
51.42	2.00	0.00	0.00	0.03	0.00	51.48	2.00	0.00	0.00	0.02	0.00
51.52	2.00	0.00	0.00	0.01	0.00	51.60	2.00	0.00	0.00	0.02	0.00
51.68	2.00	0.00	0.00	0.02	0.00	51.72	2.00	0.00	0.00	0.01	0.00
51.81	2.00	0.00	0.00	0.03	0.00	51.87	2.00	0.00	0.00	0.02	0.00
51.91	2.00	0.00	0.00	0.01	0.00	51.98	2.00	0.00	0.00	0.02	0.00
52.07	2.00	0.00	0.00	0.03	0.00	52.10	2.00	0.00	0.00	0.01	0.00
52.17	2.00	0.00	0.00	0.02	0.00	52.24	2.00	0.00	0.00	0.02	0.00
52.31	2.00	0.00	0.00	0.02	0.00	52.37	2.00	0.00	0.00	0.02	0.00
52.46	2.00	0.00	0.00	0.03	0.00	52.51	2.00	0.00	0.00	0.02	0.00
52.57	2.00	0.00	0.00	0.02	0.00	52.66	2.00	0.00	0.00	0.03	0.00
52.71	2.00	0.00	0.00	0.02	0.00	52.78	2.00	0.00	0.00	0.02	0.00
52.86	2.00	0.00	0.00	0.02	0.00	52.91	2.00	0.00	0.00	0.02	0.00
52.99	2.00	0.00	0.00	0.02	0.00	53.06	2.00	0.00	0.00	0.02	0.00
53.09	2.00	0.00	0.00	0.01	0.00	53.16	2.00	0.00	0.00	0.02	0.00
53.25	2.00	0.00	0.00	0.03	0.00	53.29	2.00	0.00	0.00	0.01	0.00
53.36	2.00	0.00	0.00	0.02	0.00	53.45	2.00	0.00	0.00	0.03	0.00
53.50	2.00	0.00	0.00	0.02	0.00	53.55	2.00	0.00	0.00	0.02	0.00
53.64	2.00	0.00	0.00	0.03	0.00	53.69	2.00	0.00	0.00	0.02	0.00
53.76	2.00	0.00	0.00	0.02	0.00	53.84	2.00	0.00	0.00	0.02	0.00
53.88	2.00	0.00	0.00	0.01	0.00	53.96	2.00	0.00	0.00	0.02	0.00
54.03	2.00	0.00	0.00	0.02	0.00	54.08	2.00	0.00	0.00	0.02	0.00
54.17	2.00	0.00	0.00	0.03	0.00	54.23	2.00	0.00	0.00	0.02	0.00
54.27	2.00	0.00	0.00	0.01	0.00	54.38	2.00	0.00	0.00	0.03	0.00
54.42	2.00	0.00	0.00	0.01	0.00	54.47	2.00	0.00	0.00	0.02	0.00
54.53	2.00	0.00	0.00	0.02	0.00	54.61	2.00	0.00	0.00	0.02	0.00
54.68	2.00	0.00	0.00	0.02	0.00	54.73	2.00	0.00	0.00	0.02	0.00
54.80	2.00	0.00	0.00	0.02	0.00	54.88	2.00	0.00	0.00	0.02	0.00
54.95	2.00	0.00	0.00	0.02	0.00	55.02	2.00	0.00	0.00	0.02	0.00
55.07	2.00	0.00	0.00	0.02	0.00	55.15	2.00	0.00	0.00	0.02	0.00
55.21	2.00	0.00	0.00	0.02	0.00	55.27	2.00	0.00	0.00	0.02	0.00
55.34	2.00	0.00	0.00	0.02	0.00	55.42	2.00	0.00	0.00	0.02	0.00
55.47	2.00	0.00	0.00	0.02	0.00	55.54	2.00	0.00	0.00	0.02	0.00
55.62	2.00	0.00	0.00	0.02	0.00	55.65	2.00	0.00	0.00	0.01	0.00
55.72	2.00	0.00	0.00	0.02	0.00	55.81	2.00	0.00	0.00	0.03	0.00
55.84	2.00	0.00	0.00	0.01	0.00	55.91	2.00	0.00	0.00	0.02	0.00
55.98	2.00	0.00	0.00	0.02	0.00	56.05	2.00	0.00	0.00	0.02	0.00
56.11	2.00	0.00	0.00	0.02	0.00	56.21	2.00	0.00	0.00	0.03	0.00
56.26	2.00	0.00	0.00	0.02	0.00	56.31	2.00	0.00	0.00	0.02	0.00
56.39	2.00	0.00	0.00	0.02	0.00	56.46	2.00	0.00	0.00	0.02	0.00
56.50	2.00	0.00	0.00	0.01	0.00	56.60	2.00	0.00	0.00	0.03	0.00
56.65	2.00	0.00	0.00	0.02	0.00	56.72	2.00	0.00	0.00	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
56.78	2.00	0.00	0.00	0.02	0.00	56.87	2.00	0.00	0.00	0.03	0.00
56.93	2.00	0.00	0.00	0.02	0.00	56.97	2.00	0.00	0.00	0.01	0.00
57.05	2.00	0.00	0.00	0.02	0.00	57.11	2.00	0.00	0.00	0.02	0.00
57.17	2.00	0.00	0.00	0.02	0.00	57.25	2.00	0.00	0.00	0.02	0.00
57.31	2.00	0.00	0.00	0.02	0.00	57.37	2.00	0.00	0.00	0.02	0.00
57.42	2.00	0.00	0.00	0.02	0.00	57.48	2.00	0.00	0.00	0.02	0.00
57.56	2.00	0.00	0.00	0.02	0.00	57.64	2.00	0.00	0.00	0.02	0.00
57.70	2.00	0.00	0.00	0.02	0.00	57.74	2.00	0.00	0.00	0.01	0.00
57.81	2.00	0.00	0.00	0.02	0.00	57.90	2.00	0.00	0.00	0.03	0.00
57.95	2.00	0.00	0.00	0.02	0.00	58.06	2.00	0.00	0.00	0.03	0.00
58.09	2.00	0.00	0.00	0.01	0.00	58.15	2.00	0.00	0.00	0.02	0.00
58.20	2.00	0.00	0.00	0.02	0.00	58.29	2.00	0.00	0.00	0.03	0.00
58.33	2.00	0.00	0.00	0.01	0.00	58.40	2.00	0.00	0.00	0.02	0.00
58.48	2.00	0.00	0.00	0.02	0.00	58.55	2.00	0.00	0.00	0.02	0.00
58.60	2.00	0.00	0.00	0.02	0.00	58.66	2.00	0.00	0.00	0.02	0.00
58.75	2.00	0.00	0.00	0.03	0.00	58.80	2.00	0.00	0.00	0.02	0.00
58.88	2.00	0.00	0.00	0.02	0.00	58.97	2.00	0.00	0.00	0.03	0.00
59.02	2.00	0.00	0.00	0.02	0.00	59.06	2.00	0.00	0.00	0.01	0.00
59.12	2.00	0.00	0.00	0.02	0.00	59.20	2.00	0.00	0.00	0.02	0.00
59.26	2.00	0.00	0.00	0.02	0.00	59.35	2.00	0.00	0.00	0.03	0.00
59.41	2.00	0.00	0.00	0.02	0.00	59.46	2.00	0.00	0.00	0.02	0.00
59.52	2.00	0.00	0.00	0.02	0.00	59.61	2.00	0.00	0.00	0.03	0.00
59.68	2.00	0.00	0.00	0.02	0.00	59.72	2.00	0.00	0.00	0.01	0.00
59.79	2.00	0.00	0.00	0.02	0.00	59.86	2.00	0.00	0.00	0.02	0.00
59.91	2.00	0.00	0.00	0.02	0.00	60.01	2.00	0.00	0.00	0.03	0.00
60.06	2.00	0.00	0.00	0.02	0.00	60.15	2.00	0.00	0.00	0.03	0.00
60.19	2.00	0.00	0.00	0.01	0.00	60.26	2.00	0.00	0.00	0.02	0.00
60.35	2.00	0.00	0.00	0.03	0.00	60.40	2.00	0.00	0.00	0.02	0.00
60.45	2.00	0.00	0.00	0.02	0.00	60.51	2.00	0.00	0.00	0.02	0.00

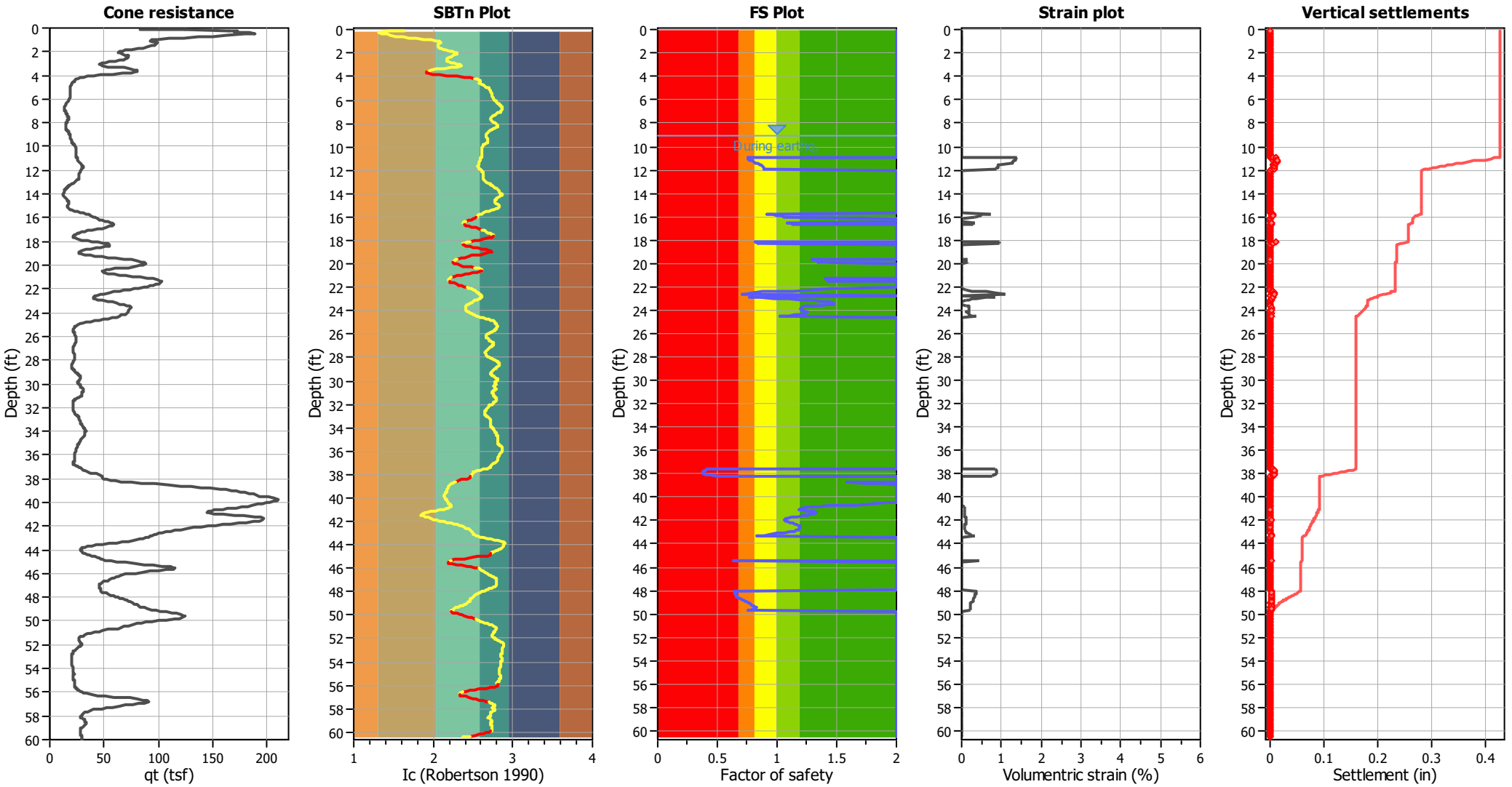
Overall liquefaction potential: 1.61

LPI = 0.00 - Liquefaction risk very low
LPI between 0.00 and 5.00 - Liquefaction risk low
LPI between 5.00 and 15.00 - Liquefaction risk high
LPI > 15.00 - Liquefaction risk very high

Abbreviations

FS: Calculated factor of safety for test point
F_L: 1 - FS
w_z: Function value of the extend of soil liquefaction according to depth
d_z: Layer thickness (ft)
LPI: Liquefaction potential index value for test point

Estimation of post-earthquake settlements



Abbreviations

q_t:	Total cone resistance (cone resistance q_c corrected for pore water effects)
I_c:	Soil Behaviour Type Index
FS:	Calculated Factor of Safety against liquefaction
Volumentric strain:	Post-liquefaction volumentric strain

:: Lateral displacement index calculation ::

Depth (ft)	q_t (tsf)	Q_{tn}	R_f (%)	$Q_{tn,cs}$	FS	D_r	$Gamma_{max}$ (%)	Lat. disp. (in)
9.01	18.66	29.11	3.31	108.78	2.00	26.27	0.00	0.00
9.09	18.90	29.50	3.37	110.44	2.00	26.71	0.00	0.00
9.15	19.06	29.75	3.45	112.13	2.00	26.98	0.00	0.00
9.20	19.18	29.93	3.53	113.94	2.00	27.19	0.00	0.00
9.29	19.30	30.11	3.63	115.92	2.00	27.39	0.00	0.00
9.35	19.43	30.33	3.73	117.85	2.00	27.62	0.00	0.00
9.39	19.54	30.50	3.79	119.21	2.00	27.81	0.00	0.00
9.45	19.66	30.68	3.83	120.17	2.00	28.01	0.00	0.00
9.55	19.97	31.17	3.83	120.89	2.00	28.52	0.00	0.00
9.64	20.38	31.83	3.80	121.43	2.00	29.21	0.00	0.00
9.65	20.91	32.67	3.76	121.97	2.00	30.08	0.00	0.00
9.73	21.47	33.57	3.71	122.48	2.00	30.97	0.00	0.00
9.79	21.98	34.31	3.68	123.03	2.00	31.69	0.00	0.00
9.84	22.46	34.86	3.64	122.99	2.00	32.21	0.00	0.00
9.91	22.88	35.24	3.59	122.67	2.00	32.57	0.00	0.00
9.99	23.25	35.53	3.55	122.26	2.00	32.85	0.00	0.00
10.08	23.63	35.78	3.49	121.63	2.00	33.08	0.00	0.00
10.14	23.82	35.88	3.47	121.31	2.00	33.17	0.00	0.00
10.19	23.87	35.79	3.45	120.88	2.00	33.09	0.00	0.00
10.25	23.88	35.62	3.43	120.28	2.00	32.93	0.00	0.00
10.34	23.79	35.24	3.43	119.75	2.00	32.57	0.00	0.00
10.38	23.82	35.15	3.41	119.11	2.00	32.49	0.00	0.00
10.44	23.92	35.10	3.36	118.25	2.00	32.44	0.00	0.00
10.52	23.94	34.89	3.32	117.11	2.00	32.25	0.00	0.00
10.59	23.96	34.70	3.28	116.11	2.00	32.07	0.00	0.00
10.63	23.88	34.48	3.27	115.67	2.00	31.86	0.00	0.00
10.70	23.75	34.11	3.27	115.08	2.00	31.50	0.00	0.00
10.78	23.71	33.84	3.25	114.48	2.00	31.24	0.00	0.00
10.87	24.05	34.05	3.22	114.07	2.00	31.44	0.00	0.00
10.93	24.68	34.72	3.14	113.43	0.75	32.08	51.20	0.44
10.97	25.09	35.14	3.10	113.33	0.75	32.49	51.20	0.29
11.03	25.34	35.34	3.13	114.00	0.76	32.66	51.20	0.44
11.12	25.57	35.43	3.18	115.11	0.77	32.76	51.20	0.66
11.16	26.10	36.05	3.19	116.20	0.78	33.33	51.20	0.29
11.23	26.69	36.65	3.20	117.14	0.79	33.87	51.20	0.51
11.31	27.32	37.28	3.22	118.24	0.80	34.43	51.20	0.59
11.37	28.14	38.20	3.22	119.49	0.82	35.24	48.90	0.42
11.44	28.65	38.70	3.26	120.91	0.84	35.67	44.57	0.45
11.51	28.96	38.94	3.32	122.45	0.86	35.87	39.72	0.40
11.56	29.46	39.47	3.35	123.56	0.87	36.31	36.11	0.26
11.63	29.97	39.93	3.35	124.20	0.88	36.70	34.38	0.35
11.71	30.37	40.22	3.36	124.71	0.88	36.93	33.15	0.38
11.76	30.29	39.99	3.40	125.36	0.89	36.75	31.18	0.22
11.83	30.13	39.61	3.44	125.68	0.89	36.43	30.56	0.31
11.91	29.90	39.12	3.48	125.79	0.89	36.02	30.81	0.35
11.94	29.36	38.36	3.53	125.85	0.89	35.38	30.83	0.13
12.05	28.72	37.35	3.57	125.25	2.00	34.49	0.00	0.00
12.10	28.18	36.60	3.59	124.65	2.00	33.83	0.00	0.00

:: Estimation of post-earthquake lateral Displacements :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	R_f (%)	$Q_{tn,cs}$	FS	D_r	$Gamma_{max}$ (%)	Lat. disp. (in)
12.14	27.59	35.82	3.62	124.10	2.00	33.12	0.00	0.00
12.25	27.11	35.08	3.64	123.36	2.00	32.42	0.00	0.00
12.29	26.81	34.65	3.63	122.58	2.00	32.02	0.00	0.00
12.35	26.66	34.38	3.62	122.06	2.00	31.76	0.00	0.00
12.44	26.59	34.17	3.59	121.34	2.00	31.56	0.00	0.00
12.49	26.67	34.20	3.54	120.41	2.00	31.58	0.00	0.00
12.55	26.82	34.29	3.48	119.34	2.00	31.67	0.00	0.00
12.61	26.84	34.21	3.41	118.04	2.00	31.60	0.00	0.00
12.70	26.47	33.64	3.39	116.91	2.00	31.05	0.00	0.00
12.75	25.93	32.91	3.38	115.62	2.00	30.32	0.00	0.00
12.81	25.23	31.96	3.34	113.61	2.00	29.35	0.00	0.00
12.89	24.43	30.85	3.28	110.95	2.00	28.18	0.00	0.00
12.94	23.55	29.68	3.19	107.89	2.00	26.91	0.00	0.00
12.99	22.55	28.37	3.13	105.01	2.00	25.42	0.00	0.00
13.08	21.42	26.86	3.10	102.27	2.00	23.61	0.00	0.00
13.15	20.17	25.24	3.07	99.55	2.00	21.56	0.00	0.00
13.20	18.94	23.67	3.06	96.93	2.00	19.44	0.00	0.00
13.27	17.94	22.36	3.00	94.01	2.00	17.56	0.00	0.00
13.32	17.08	21.23	2.92	91.09	2.00	15.85	0.00	0.00
13.39	16.29	20.19	2.87	88.71	2.00	14.18	0.00	0.00
13.48	15.57	19.24	2.86	87.03	2.00	12.60	0.00	0.00
13.54	14.85	18.31	2.87	85.67	2.00	10.96	0.00	0.00
13.59	14.26	17.54	2.88	84.40	2.00	9.55	0.00	0.00
13.65	13.72	16.84	2.87	83.16	2.00	8.20	0.00	0.00
13.74	13.35	16.32	2.86	81.98	2.00	7.16	0.00	0.00
13.80	13.07	15.93	2.81	80.63	2.00	6.37	0.00	0.00
13.89	12.89	15.65	2.73	79.16	2.00	5.79	0.00	0.00
13.93	12.67	15.36	2.73	78.57	2.00	5.17	0.00	0.00
13.99	12.47	15.09	2.81	79.11	2.00	4.58	0.00	0.00
14.07	12.36	14.93	2.89	79.81	2.00	4.22	0.00	0.00
14.12	12.41	14.97	2.94	80.54	2.00	4.32	0.00	0.00
14.18	12.84	15.48	2.92	81.24	2.00	5.42	0.00	0.00
14.26	13.66	16.43	2.85	82.12	2.00	7.38	0.00	0.00
14.34	14.47	17.37	2.81	83.28	2.00	9.23	0.00	0.00
14.38	15.06	18.09	2.89	85.64	2.00	10.56	0.00	0.00
14.47	15.53	18.63	3.03	88.46	2.00	11.54	0.00	0.00
14.53	16.03	19.23	3.12	90.78	2.00	12.57	0.00	0.00
14.57	16.61	19.90	3.14	92.32	2.00	13.72	0.00	0.00
14.64	17.04	20.39	3.17	93.50	2.00	14.52	0.00	0.00
14.72	17.40	20.77	3.19	94.50	2.00	15.13	0.00	0.00
14.80	17.27	20.58	3.27	95.26	2.00	14.82	0.00	0.00
14.83	16.85	20.07	3.38	95.90	2.00	13.99	0.00	0.00
14.92	16.39	19.48	3.50	96.48	2.00	13.01	0.00	0.00
14.97	16.24	19.28	3.55	96.80	2.00	12.66	0.00	0.00
15.06	16.27	19.26	3.60	97.42	2.00	12.64	0.00	0.00
15.10	16.43	19.44	3.67	98.73	2.00	12.94	0.00	0.00
15.17	16.88	19.94	3.75	100.69	2.00	13.78	0.00	0.00
15.25	17.82	21.02	3.78	103.31	2.00	15.52	0.00	0.00

:: Estimation of post-earthquake lateral Displacements :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	R_f (%)	$Q_{tn,cs}$	FS	D_r	$Gamma_{max}$ (%)	Lat. disp. (in)
15.31	19.04	22.44	3.81	106.25	2.00	17.68	0.00	0.00
15.37	20.79	24.48	3.79	109.75	2.00	20.54	0.00	0.00
15.44	22.91	26.92	3.78	113.74	2.00	23.69	0.00	0.00
15.51	25.24	29.60	3.76	117.67	2.00	26.82	0.00	0.00
15.56	27.89	32.64	3.73	121.72	2.00	30.04	0.00	0.00
15.63	30.62	35.75	3.73	126.33	2.00	33.05	0.00	0.00
15.71	33.36	38.84	3.72	130.50	2.00	35.78	0.00	0.00
15.76	35.88	41.68	3.72	134.26	0.92	38.12	24.52	0.18
15.82	38.00	44.04	3.72	137.37	0.96	39.94	12.83	0.11
15.90	39.72	45.92	3.73	140.10	1.00	41.31	0.00	0.00
15.95	40.95	47.26	3.76	142.38	1.04	42.26	0.00	0.00
16.01	42.08	48.46	3.75	143.78	1.06	43.09	0.00	0.00
16.10	43.69	50.12	3.69	144.51	2.00	44.20	0.00	0.00
16.16	45.39	51.93	3.61	144.76	2.00	45.37	0.00	0.00
16.21	47.82	54.52	3.45	144.17	2.00	46.98	0.00	0.00
16.29	50.73	57.59	3.28	143.67	2.00	48.78	0.00	0.00
16.36	53.65	60.67	3.15	143.61	2.00	50.50	0.00	0.00
16.41	55.97	63.12	3.08	144.46	2.00	51.81	0.00	0.00
16.49	57.93	65.13	3.04	145.59	1.09	52.85	2.50	0.03
16.55	58.97	66.18	3.05	147.05	1.11	53.38	2.17	0.02
16.60	58.73	65.85	3.13	148.63	1.14	53.21	1.86	0.01
16.70	57.58	64.45	3.25	150.28	2.00	52.50	0.00	0.00
16.74	55.54	62.18	3.37	150.89	2.00	51.32	0.00	0.00
16.80	52.24	58.44	3.44	148.41	2.00	49.27	0.00	0.00
16.89	48.21	53.86	3.55	145.75	2.00	46.57	0.00	0.00
16.93	43.70	48.84	3.69	142.95	2.00	43.34	0.00	0.00
17.00	39.30	43.87	3.81	139.12	2.00	39.81	0.00	0.00
17.09	35.13	39.12	3.89	134.22	2.00	36.03	0.00	0.00
17.14	31.91	35.46	3.85	128.18	2.00	32.78	0.00	0.00
17.20	29.62	32.81	3.69	121.48	2.00	30.22	0.00	0.00
17.28	27.32	30.13	3.51	114.37	2.00	27.41	0.00	0.00
17.34	25.35	27.85	3.37	108.56	2.00	24.81	0.00	0.00
17.41	23.75	26.02	3.43	106.90	2.00	22.56	0.00	0.00
17.48	22.28	24.34	3.51	105.33	2.00	20.37	0.00	0.00
17.56	21.40	23.31	3.53	103.98	2.00	18.93	0.00	0.00
17.62	21.30	23.15	3.51	103.34	2.00	18.71	0.00	0.00
17.67	21.90	23.78	3.53	104.80	2.00	19.59	0.00	0.00
17.72	23.43	25.45	3.53	107.56	2.00	21.83	0.00	0.00
17.78	25.81	28.02	3.47	110.64	2.00	25.00	0.00	0.00
17.87	29.76	32.25	3.29	113.53	2.00	29.65	0.00	0.00
17.94	34.49	37.30	3.14	117.09	2.00	34.45	0.00	0.00
18.01	39.36	42.48	3.01	120.59	2.00	38.74	0.00	0.00
18.06	44.61	48.05	2.89	124.00	2.00	42.81	0.00	0.00
18.12	49.40	53.08	2.81	127.40	2.00	46.10	0.00	0.00
18.21	53.23	57.04	2.77	130.57	0.82	48.47	14.74	0.19
18.25	55.37	59.24	2.74	131.91	0.84	49.72	12.86	0.07
18.31	55.54	59.32	2.74	131.93	0.84	49.77	12.90	0.11
18.40	54.39	57.96	2.75	130.84	2.00	49.00	0.00	0.00

:: Estimation of post-earthquake lateral Displacements :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	R_f (%)	$Q_{tn,cs}$	FS	D_r	$Gamma_{max}$ (%)	Lat. disp. (in)
18.44	51.05	54.37	2.83	129.13	2.00	46.89	0.00	0.00
18.51	46.53	49.50	2.92	126.35	2.00	43.79	0.00	0.00
18.58	42.29	44.90	3.01	123.40	2.00	40.57	0.00	0.00
18.64	37.54	39.79	3.16	120.70	2.00	36.58	0.00	0.00
18.71	33.19	35.09	3.30	117.60	2.00	32.44	0.00	0.00
18.80	29.50	31.08	3.44	114.60	2.00	28.43	0.00	0.00
18.86	27.07	28.44	3.60	113.53	2.00	25.50	0.00	0.00
18.91	26.18	27.47	3.76	114.45	2.00	24.36	0.00	0.00
18.98	26.23	27.48	3.86	116.18	2.00	24.37	0.00	0.00
19.05	28.55	29.89	3.76	118.43	2.00	27.14	0.00	0.00
19.10	32.75	34.30	3.61	122.20	2.00	31.68	0.00	0.00
19.20	36.95	38.62	3.51	126.30	2.00	35.60	0.00	0.00
19.23	41.98	43.88	3.40	130.67	2.00	39.81	0.00	0.00
19.30	47.70	49.78	3.29	135.29	2.00	43.98	0.00	0.00
19.39	53.84	56.05	3.19	139.78	2.00	47.89	0.00	0.00
19.43	60.95	63.36	3.04	144.00	2.00	51.94	0.00	0.00
19.50	67.80	70.30	2.92	147.71	2.00	55.37	0.00	0.00
19.57	74.91	77.48	2.81	151.93	2.00	58.58	0.00	0.00
19.63	80.68	83.29	2.77	156.25	2.00	60.96	0.00	0.00
19.70	84.48	87.05	2.77	160.14	1.29	62.42	1.15	0.01
19.77	87.46	89.97	2.81	163.96	1.37	63.51	0.89	0.01
19.84	88.72	91.06	2.74	162.94	1.35	63.91	0.96	0.01
19.90	88.05	90.24	2.76	162.93	1.35	63.61	0.96	0.01
19.99	86.33	88.30	2.83	162.87	2.00	62.89	0.00	0.00
20.02	82.81	84.69	2.97	163.44	2.00	61.52	0.00	0.00
20.09	77.91	79.61	3.16	163.98	2.00	59.47	0.00	0.00
20.19	72.20	73.64	3.40	164.40	2.00	56.90	0.00	0.00
20.21	66.31	67.65	3.67	164.76	2.00	54.10	0.00	0.00
20.29	60.80	61.90	3.92	164.43	2.00	51.17	0.00	0.00
20.38	55.60	56.47	4.19	163.92	2.00	48.14	0.00	0.00
20.42	51.83	52.62	4.60	167.91	2.00	45.81	0.00	0.00
20.52	49.59	50.20	4.83	169.09	2.00	44.25	0.00	0.00
20.55	48.85	49.41	4.92	169.77	2.00	43.73	0.00	0.00
20.62	50.23	50.69	4.75	168.19	2.00	44.57	0.00	0.00
20.68	54.00	54.40	4.40	165.95	2.00	46.90	0.00	0.00
20.75	58.46	58.77	4.07	164.25	2.00	49.45	0.00	0.00
20.81	64.06	64.27	3.75	163.09	2.00	52.41	0.00	0.00
20.90	70.17	70.22	3.46	162.34	2.00	55.33	0.00	0.00
20.96	76.88	76.78	3.20	162.12	2.00	58.28	0.00	0.00
21.01	83.50	83.25	2.99	162.71	2.00	60.95	0.00	0.00
21.09	89.88	89.40	2.82	163.78	2.00	63.30	0.00	0.00
21.15	95.34	94.66	2.68	164.75	2.00	65.19	0.00	0.00
21.21	99.28	98.41	2.60	165.97	2.00	66.47	0.00	0.00
21.30	101.54	100.41	2.57	166.66	1.40	67.14	1.20	0.02
21.36	102.98	101.69	2.54	166.99	1.41	67.55	1.19	0.01
21.40	103.15	101.76	2.54	167.23	1.41	67.57	1.18	0.01
21.49	102.24	100.65	2.59	167.75	1.42	67.21	1.15	0.01
21.56	100.58	98.87	2.68	168.66	2.00	66.63	0.00	0.00

:: Estimation of post-earthquake lateral Displacements :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	R_f (%)	$Q_{tn,cs}$	FS	D_r	$Gamma_{max}$ (%)	Lat. disp. (in)
21.60	98.24	96.51	2.80	170.27	2.00	65.83	0.00	0.00
21.66	95.65	93.85	2.98	173.11	2.00	64.90	0.00	0.00
21.75	92.97	91.05	3.18	176.31	2.00	63.90	0.00	0.00
21.80	90.34	88.38	3.39	179.61	2.00	62.92	0.00	0.00
21.85	86.54	84.57	3.60	181.57	2.00	61.47	0.00	0.00
21.95	82.45	80.35	3.80	182.77	2.00	59.78	0.00	0.00
21.99	77.84	75.75	3.99	182.63	2.00	57.84	0.00	0.00
22.05	73.33	71.22	4.09	179.99	2.00	55.80	0.00	0.00
22.14	68.64	66.45	4.12	175.01	1.58	53.51	0.23	0.00
22.19	64.12	61.92	4.12	169.22	1.45	51.18	0.40	0.00
22.26	59.36	57.14	4.05	161.62	1.29	48.53	0.84	0.01
22.35	54.56	52.30	3.95	153.37	1.13	45.61	1.93	0.02
22.44	49.73	47.45	3.85	144.80	0.99	42.40	7.23	0.09
22.45	46.31	44.10	3.71	137.69	0.88	39.98	34.16	0.05
22.54	43.33	41.08	3.60	131.39	0.79	37.64	51.20	0.66
22.58	41.17	38.93	3.51	126.75	0.73	35.86	51.20	0.29
22.65	39.90	37.63	3.49	124.71	0.71	34.74	51.20	0.51
22.73	39.60	37.26	3.53	125.06	2.00	34.42	0.00	0.00
22.79	39.96	37.55	3.56	126.08	2.00	34.67	0.00	0.00
22.85	41.77	39.25	3.64	129.80	0.77	36.13	51.20	0.44
22.93	44.52	41.82	3.80	136.54	0.86	38.22	39.27	0.45
22.99	48.25	45.36	3.96	144.50	0.98	40.91	9.74	0.08
23.04	53.17	50.03	4.01	151.83	1.10	44.14	0.00	0.00
23.12	57.97	54.54	4.04	158.22	1.21	46.99	1.24	0.01
23.19	61.76	58.07	4.05	162.95	1.30	49.06	0.78	0.01
23.27	64.98	61.03	4.05	166.65	1.38	50.70	0.55	0.01
23.30	67.76	63.65	4.04	169.44	1.44	52.09	0.42	0.00
23.38	70.90	66.51	3.97	171.29	1.48	53.54	0.35	0.00
23.47	73.27	68.60	3.87	171.31	1.47	54.56	0.35	0.00
23.50	74.99	70.18	3.71	168.91	1.42	55.31	0.75	0.00
23.58	75.51	70.53	3.56	165.30	1.35	55.48	0.96	0.01
23.66	74.38	69.31	3.48	161.96	1.28	54.90	0.88	0.01
23.69	73.15	68.09	3.43	159.30	1.23	54.31	1.15	0.00
23.77	72.69	67.52	3.42	158.28	1.21	54.04	1.27	0.01
23.84	72.77	67.48	3.40	157.74	1.20	54.02	1.35	0.01
23.92	72.82	67.39	3.41	157.99	1.20	53.97	1.32	0.02
23.97	71.99	66.52	3.46	158.38	1.21	53.54	1.27	0.01
24.06	70.72	65.17	3.54	158.89	1.21	52.87	1.22	0.00
24.12	69.26	63.69	3.65	159.96	1.23	52.11	1.10	0.00
24.17	67.92	62.35	3.75	160.90	1.25	51.41	1.00	0.00
24.23	66.21	60.65	3.82	160.73	1.25	50.49	1.02	0.00
24.31	64.27	58.71	3.89	160.00	1.23	49.42	1.10	0.00
24.36	61.66	56.19	3.95	158.28	1.20	47.97	1.31	0.00
24.42	58.14	52.82	4.02	155.55	1.15	45.93	1.73	0.00
24.51	54.24	49.05	4.09	152.30	1.09	43.49	0.00	0.00
24.54	50.19	45.25	4.14	148.14	1.02	40.83	0.00	0.00
24.62	45.92	41.19	4.15	142.60	2.00	37.72	0.00	0.00
24.71	41.38	36.87	4.15	136.14	2.00	34.07	0.00	0.00

:: Estimation of post-earthquake lateral Displacements :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	R_f (%)	$Q_{tn,cs}$	FS	D_r	$Gamma_{max}$ (%)	Lat. disp. (in)
24.74	37.02	32.81	4.12	129.34	2.00	30.21	0.00	0.00
24.81	33.35	29.36	4.05	122.62	2.00	26.55	0.00	0.00
24.89	30.15	26.35	3.94	115.71	2.00	22.98	0.00	0.00
24.96	27.79	24.12	3.75	109.01	2.00	20.07	0.00	0.00
25.01	26.12	22.57	3.55	103.36	2.00	17.86	0.00	0.00
25.10	24.74	21.25	3.35	98.16	2.00	15.88	0.00	0.00
25.14	23.57	20.15	3.21	94.33	2.00	14.13	0.00	0.00
25.21	22.70	19.32	3.15	92.00	2.00	12.74	0.00	0.00
25.30	22.17	18.80	3.09	90.31	2.00	11.83	0.00	0.00
25.34	21.82	18.46	3.02	88.71	2.00	11.23	0.00	0.00
25.41	21.76	18.37	2.95	87.53	2.00	11.08	0.00	0.00
25.50	21.77	18.34	2.88	86.53	2.00	11.02	0.00	0.00
25.55	21.93	18.47	2.82	85.93	2.00	11.24	0.00	0.00
25.60	22.09	18.59	2.77	85.40	2.00	11.46	0.00	0.00
25.70	22.29	18.73	2.70	84.60	2.00	11.71	0.00	0.00
25.75	22.50	18.90	2.62	83.67	2.00	12.02	0.00	0.00
25.80	22.79	19.15	2.49	82.04	2.00	12.44	0.00	0.00
25.89	23.08	19.37	2.37	80.44	2.00	12.82	0.00	0.00
25.95	23.34	19.59	2.27	79.07	2.00	13.20	0.00	0.00
25.99	23.77	19.96	2.16	77.81	2.00	13.82	0.00	0.00
26.06	24.08	20.21	2.08	76.79	2.00	14.23	0.00	0.00
26.15	24.25	20.33	2.02	75.89	2.00	14.42	0.00	0.00
26.19	24.34	20.39	1.98	75.28	2.00	14.52	0.00	0.00
26.25	24.39	20.41	1.98	75.23	2.00	14.55	0.00	0.00
26.34	24.31	20.30	2.02	75.77	2.00	14.36	0.00	0.00
26.38	24.05	20.04	2.12	77.18	2.00	13.94	0.00	0.00
26.45	23.79	19.77	2.21	78.40	2.00	13.50	0.00	0.00
26.52	23.52	19.49	2.29	79.37	2.00	13.03	0.00	0.00
26.61	23.07	19.04	2.37	80.09	2.00	12.26	0.00	0.00
26.67	22.67	18.66	2.42	80.27	2.00	11.58	0.00	0.00
26.72	22.32	18.31	2.45	80.21	2.00	10.97	0.00	0.00
26.82	21.99	17.98	2.45	79.73	2.00	10.36	0.00	0.00
26.86	21.65	17.67	2.42	78.75	2.00	9.78	0.00	0.00
26.94	21.41	17.42	2.33	77.07	2.00	9.31	0.00	0.00
26.98	21.28	17.29	2.22	75.19	2.00	9.08	0.00	0.00
27.06	21.19	17.19	2.11	73.31	2.00	8.88	0.00	0.00
27.10	21.17	17.16	1.99	71.47	2.00	8.83	0.00	0.00
27.17	21.23	17.20	1.88	69.64	2.00	8.90	0.00	0.00
27.26	21.42	17.34	1.79	68.32	2.00	9.16	0.00	0.00
27.31	21.67	17.54	1.72	67.44	2.00	9.55	0.00	0.00
27.39	21.94	17.76	1.69	67.05	2.00	9.96	0.00	0.00
27.44	22.25	18.02	1.66	66.93	2.00	10.43	0.00	0.00
27.51	22.57	18.27	1.66	67.24	2.00	10.90	0.00	0.00
27.58	22.83	18.47	1.68	67.74	2.00	11.25	0.00	0.00
27.63	23.05	18.64	1.70	68.26	2.00	11.56	0.00	0.00
27.71	23.11	18.67	1.73	68.80	2.00	11.60	0.00	0.00
27.79	23.06	18.58	1.77	69.46	2.00	11.45	0.00	0.00
27.86	22.89	18.40	1.81	69.90	2.00	11.13	0.00	0.00

:: Estimation of post-earthquake lateral Displacements :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	R_f (%)	$Q_{tn,cs}$	FS	D_r	$Gamma_{max}$ (%)	Lat. disp. (in)
27.89	22.61	18.14	1.85	70.31	2.00	10.66	0.00	0.00
27.96	22.26	17.80	1.90	70.72	2.00	10.04	0.00	0.00
28.05	21.90	17.44	1.97	71.46	2.00	9.36	0.00	0.00
28.09	21.54	17.11	2.07	72.69	2.00	8.72	0.00	0.00
28.16	21.20	16.78	2.19	74.05	2.00	8.08	0.00	0.00
28.23	20.88	16.46	2.31	75.37	2.00	7.44	0.00	0.00
28.29	20.64	16.22	2.42	76.64	2.00	6.96	0.00	0.00
28.35	20.47	16.04	2.52	77.72	2.00	6.60	0.00	0.00
28.44	20.36	15.91	2.60	78.67	2.00	6.33	0.00	0.00
28.50	20.26	15.79	2.68	79.55	2.00	6.07	0.00	0.00
28.55	20.24	15.75	2.74	80.26	2.00	5.99	0.00	0.00
28.64	20.28	15.76	2.77	80.62	2.00	6.00	0.00	0.00
28.69	20.47	15.90	2.76	80.83	2.00	6.30	0.00	0.00
28.75	20.92	16.26	2.70	80.68	2.00	7.05	0.00	0.00
28.82	21.52	16.76	2.62	80.40	2.00	8.05	0.00	0.00
28.89	22.35	17.44	2.61	81.27	2.00	9.36	0.00	0.00
28.98	23.25	18.18	2.62	82.71	2.00	10.73	0.00	0.00
29.04	24.09	18.87	2.65	84.22	2.00	11.96	0.00	0.00
29.08	24.99	19.62	2.67	85.67	2.00	13.25	0.00	0.00
29.15	25.81	20.29	2.71	87.23	2.00	14.36	0.00	0.00
29.24	26.55	20.88	2.76	88.89	2.00	15.30	0.00	0.00
29.29	27.47	21.64	2.79	90.48	2.00	16.49	0.00	0.00
29.34	28.09	22.14	2.85	92.19	2.00	17.23	0.00	0.00
29.43	28.47	22.41	2.93	93.91	2.00	17.64	0.00	0.00
29.47	28.34	22.27	2.99	94.60	2.00	17.42	0.00	0.00
29.53	28.01	21.95	3.03	94.84	2.00	16.95	0.00	0.00
29.62	27.58	21.54	3.09	94.97	2.00	16.32	0.00	0.00
29.66	26.96	20.98	3.16	95.20	2.00	15.46	0.00	0.00
29.77	26.26	20.33	3.24	95.20	2.00	14.42	0.00	0.00
29.81	25.53	19.68	3.35	95.62	2.00	13.35	0.00	0.00
29.86	25.39	19.54	3.41	96.27	2.00	13.10	0.00	0.00
29.92	25.75	19.81	3.44	97.12	2.00	13.56	0.00	0.00
30.01	26.64	20.51	3.42	98.08	2.00	14.72	0.00	0.00
30.09	27.72	21.39	3.38	99.03	2.00	16.09	0.00	0.00
30.17	28.41	21.93	3.38	100.07	2.00	16.91	0.00	0.00
30.20	28.59	22.05	3.46	101.40	2.00	17.10	0.00	0.00
30.27	28.79	22.17	3.56	103.06	2.00	17.28	0.00	0.00
30.32	29.48	22.72	3.61	104.73	2.00	18.09	0.00	0.00
30.39	30.45	23.50	3.59	105.88	2.00	19.20	0.00	0.00
30.47	30.78	23.72	3.61	106.51	2.00	19.51	0.00	0.00
30.55	30.79	23.68	3.63	106.70	2.00	19.46	0.00	0.00
30.62	30.35	23.27	3.68	106.77	2.00	18.87	0.00	0.00
30.66	29.89	22.86	3.74	106.87	2.00	18.29	0.00	0.00
30.72	29.64	22.63	3.68	105.71	2.00	17.95	0.00	0.00
30.81	29.90	22.81	3.54	103.99	2.00	18.22	0.00	0.00
30.85	30.12	22.99	3.36	101.48	2.00	18.48	0.00	0.00
30.91	29.75	22.67	3.19	98.41	2.00	18.02	0.00	0.00
31.01	29.16	22.15	3.01	94.88	2.00	17.25	0.00	0.00

:: Estimation of post-earthquake lateral Displacements :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	R_f (%)	$Q_{tn,cs}$	FS	D_r	$Gamma_{max}$ (%)	Lat. disp. (in)
31.05	28.11	21.28	2.88	91.42	2.00	15.92	0.00	0.00
31.11	26.82	20.20	2.76	87.95	2.00	14.21	0.00	0.00
31.20	25.44	19.03	2.64	84.32	2.00	12.24	0.00	0.00
31.26	24.18	17.98	2.50	80.64	2.00	10.37	0.00	0.00
31.31	23.24	17.20	2.43	78.37	2.00	8.89	0.00	0.00
31.38	22.45	16.53	2.38	76.56	2.00	7.59	0.00	0.00
31.46	21.95	16.09	2.32	75.05	2.00	6.71	0.00	0.00
31.51	21.63	15.82	2.28	74.00	2.00	6.14	0.00	0.00
31.60	21.33	15.54	2.25	73.14	2.00	5.56	0.00	0.00
31.65	21.21	15.44	2.20	72.24	2.00	5.33	0.00	0.00
31.74	21.14	15.36	2.13	71.22	2.00	5.16	0.00	0.00
31.80	21.15	15.35	2.06	70.19	2.00	5.15	0.00	0.00
31.85	21.16	15.35	1.98	68.91	2.00	5.15	0.00	0.00
31.89	21.17	15.37	1.86	67.05	2.00	5.18	0.00	0.00
32.00	21.16	15.34	1.74	65.11	2.00	5.12	0.00	0.00
32.04	21.11	15.30	1.63	63.32	2.00	5.05	0.00	0.00
32.09	21.14	15.33	1.55	61.91	2.00	5.09	0.00	0.00
32.19	21.23	15.39	1.48	60.88	2.00	5.23	0.00	0.00
32.23	21.15	15.31	1.46	60.35	2.00	5.05	0.00	0.00
32.29	21.63	15.69	1.44	60.57	2.00	5.87	0.00	0.00
32.37	22.15	16.09	1.44	60.95	2.00	6.69	0.00	0.00
32.44	22.73	16.54	1.46	61.75	2.00	7.61	0.00	0.00
32.49	23.42	17.08	1.51	63.28	2.00	8.66	0.00	0.00
32.58	24.18	17.66	1.56	64.80	2.00	9.77	0.00	0.00
32.62	24.92	18.23	1.61	66.38	2.00	10.83	0.00	0.00
32.69	25.54	18.71	1.67	67.92	2.00	11.67	0.00	0.00
32.78	26.07	19.09	1.73	69.43	2.00	12.34	0.00	0.00
32.82	26.80	19.66	1.77	70.95	2.00	13.31	0.00	0.00
32.89	27.02	19.79	1.85	72.39	2.00	13.54	0.00	0.00
32.97	27.26	19.94	1.92	73.87	2.00	13.78	0.00	0.00
33.02	27.46	20.06	2.00	75.41	2.00	13.98	0.00	0.00
33.09	27.56	20.09	2.10	77.21	2.00	14.03	0.00	0.00
33.15	27.58	20.06	2.22	79.12	2.00	13.98	0.00	0.00
33.20	27.62	20.05	2.34	81.12	2.00	13.96	0.00	0.00
33.28	27.94	20.26	2.45	83.29	2.00	14.30	0.00	0.00
33.38	28.41	20.57	2.55	85.36	2.00	14.81	0.00	0.00
33.43	29.00	21.01	2.64	87.41	2.00	15.50	0.00	0.00
33.47	29.66	21.50	2.72	89.41	2.00	16.26	0.00	0.00
33.57	30.25	21.91	2.82	91.56	2.00	16.89	0.00	0.00
33.63	30.80	22.30	2.92	93.64	2.00	17.47	0.00	0.00
33.70	31.35	22.69	2.99	95.39	2.00	18.05	0.00	0.00
33.74	31.93	23.12	3.05	97.06	2.00	18.67	0.00	0.00
33.82	32.49	23.51	3.11	98.51	2.00	19.22	0.00	0.00
33.86	32.78	23.71	3.16	99.73	2.00	19.50	0.00	0.00
33.93	32.90	23.76	3.24	100.95	2.00	19.57	0.00	0.00
34.02	32.86	23.67	3.31	102.03	2.00	19.44	0.00	0.00
34.06	32.78	23.57	3.38	102.94	2.00	19.30	0.00	0.00
34.13	32.65	23.42	3.43	103.48	2.00	19.09	0.00	0.00

:: Estimation of post-earthquake lateral Displacements :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	R_f (%)	$Q_{tn,cs}$	FS	D_r	$Gamma_{max}$ (%)	Lat. disp. (in)
34.21	32.51	23.26	3.47	103.80	2.00	18.86	0.00	0.00
34.28	32.29	23.05	3.50	103.90	2.00	18.56	0.00	0.00
34.32	31.94	22.75	3.52	103.65	2.00	18.13	0.00	0.00
34.41	31.53	22.38	3.53	103.23	2.00	17.59	0.00	0.00
34.46	31.08	22.00	3.54	102.68	2.00	17.03	0.00	0.00
34.52	30.55	21.56	3.54	101.80	2.00	16.35	0.00	0.00
34.61	29.93	21.04	3.52	100.63	2.00	15.55	0.00	0.00
34.65	29.34	20.56	3.49	99.34	2.00	14.79	0.00	0.00
34.71	28.73	20.07	3.44	97.80	2.00	13.99	0.00	0.00
34.79	28.12	19.57	3.37	95.91	2.00	13.16	0.00	0.00
34.86	27.56	19.11	3.28	93.87	2.00	12.38	0.00	0.00
34.93	27.06	18.72	3.18	91.78	2.00	11.69	0.00	0.00
35.01	26.62	18.35	3.08	89.74	2.00	11.04	0.00	0.00
35.06	26.18	18.01	2.99	87.84	2.00	10.42	0.00	0.00
35.11	25.82	17.73	2.91	86.31	2.00	9.90	0.00	0.00
35.18	25.57	17.51	2.85	85.02	2.00	9.49	0.00	0.00
35.26	25.31	17.29	2.81	84.06	2.00	9.07	0.00	0.00
35.34	25.02	17.04	2.79	83.47	2.00	8.59	0.00	0.00
35.40	24.80	16.85	2.80	83.29	2.00	8.22	0.00	0.00
35.44	24.58	16.65	2.84	83.43	2.00	7.83	0.00	0.00
35.51	24.35	16.44	2.90	83.91	2.00	7.41	0.00	0.00
35.58	24.06	16.19	2.96	84.27	2.00	6.90	0.00	0.00
35.66	23.76	15.93	3.00	84.26	2.00	6.36	0.00	0.00
35.71	23.50	15.70	3.01	83.91	2.00	5.90	0.00	0.00
35.77	23.24	15.49	2.99	83.26	2.00	5.44	0.00	0.00
35.85	22.95	15.25	2.95	82.35	2.00	4.93	0.00	0.00
35.92	22.74	15.07	2.91	81.42	2.00	4.54	0.00	0.00
35.97	22.64	14.99	2.87	80.74	2.00	4.36	0.00	0.00
36.03	22.63	14.97	2.81	80.03	2.00	4.31	0.00	0.00
36.11	22.66	14.98	2.74	79.05	2.00	4.33	0.00	0.00
36.16	22.78	15.07	2.63	77.87	2.00	4.53	0.00	0.00
36.26	22.82	15.08	2.54	76.66	2.00	4.56	0.00	0.00
36.31	22.88	15.12	2.46	75.65	2.00	4.65	0.00	0.00
36.36	22.63	14.93	2.39	74.35	2.00	4.23	0.00	0.00
36.43	22.40	14.74	2.33	73.14	2.00	3.80	0.00	0.00
36.51	22.21	14.58	2.26	71.91	2.00	3.46	0.00	0.00
36.55	22.01	14.43	2.21	71.02	2.00	3.11	0.00	0.00
36.65	21.75	14.21	2.19	70.32	2.00	2.60	0.00	0.00
36.71	21.76	14.20	2.19	70.29	2.00	2.58	0.00	0.00
36.76	22.11	14.45	2.18	70.57	2.00	3.15	0.00	0.00
36.85	22.79	14.94	2.19	71.52	2.00	4.24	0.00	0.00
36.89	23.63	15.55	2.21	72.78	2.00	5.57	0.00	0.00
36.96	24.91	16.49	2.26	74.96	2.00	7.51	0.00	0.00
37.02	26.31	17.51	2.32	77.41	2.00	9.49	0.00	0.00
37.11	27.68	18.50	2.39	79.93	2.00	11.30	0.00	0.00
37.15	28.95	19.42	2.47	82.45	2.00	12.91	0.00	0.00
37.24	30.33	20.41	2.56	85.40	2.00	14.55	0.00	0.00
37.31	31.54	21.27	2.67	88.27	2.00	15.91	0.00	0.00

:: Estimation of post-earthquake lateral Displacements :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	R_f (%)	$Q_{tn,cs}$	FS	D_r	$Gamma_{max}$ (%)	Lat. disp. (in)
37.35	32.61	22.02	2.80	91.57	2.00	17.06	0.00	0.00
37.43	34.54	23.43	2.87	94.72	2.00	19.10	0.00	0.00
37.51	37.23	25.41	2.87	97.40	2.00	21.79	0.00	0.00
37.55	40.42	27.84	2.77	98.85	2.00	24.79	0.00	0.00
37.60	43.41	30.14	2.59	98.34	0.41	27.42	51.20	0.00
37.67	46.12	32.25	2.41	97.10	0.40	29.65	51.20	0.00
37.75	47.68	33.45	2.27	95.62	0.40	30.85	51.20	0.00
37.81	48.21	33.86	2.19	94.32	0.39	31.26	51.20	0.00
37.88	48.12	33.76	2.16	93.42	0.38	31.16	51.20	0.00
37.93	48.13	33.75	2.14	93.00	0.38	31.14	51.20	0.00
38.00	49.14	34.47	2.14	93.80	0.38	31.85	51.20	0.00
38.08	52.10	36.67	2.18	96.77	0.40	33.89	51.20	0.00
38.14	55.93	39.49	2.32	102.67	0.44	36.33	51.20	0.00
38.20	60.41	42.75	2.51	110.38	0.50	38.95	51.20	0.00
38.26	65.84	46.71	2.75	119.90	2.00	41.88	0.00	0.00
38.34	74.63	53.26	2.89	130.07	2.00	46.21	0.00	0.00
38.43	85.00	61.06	2.94	139.63	2.00	50.72	0.00	0.00
38.45	97.14	70.35	2.96	149.58	2.00	55.39	0.00	0.00
38.53	109.74	79.94	2.97	159.28	2.00	59.61	0.00	0.00
38.62	121.23	88.66	2.98	168.28	2.00	63.03	0.00	0.00
38.65	130.51	95.75	3.01	176.10	2.00	65.57	0.00	0.00
38.72	139.21	102.35	3.02	182.90	1.59	67.77	0.84	0.00
38.80	148.05	109.03	3.02	189.51	1.75	69.85	0.64	0.00
38.88	156.31	115.30	3.00	195.08	1.89	71.70	0.51	0.00
38.93	162.35	119.87	3.00	199.70	2.00	72.98	0.00	0.00
39.01	167.70	123.81	3.02	204.11	2.00	74.05	0.00	0.00
39.07	171.82	126.83	3.04	207.67	2.00	74.85	0.00	0.00
39.12	176.04	129.96	3.05	211.17	2.00	75.65	0.00	0.00
39.20	180.10	132.88	3.07	214.63	2.00	76.38	0.00	0.00
39.27	184.00	135.69	3.08	217.99	2.00	77.07	0.00	0.00
39.31	187.49	138.26	3.10	221.07	2.00	77.69	0.00	0.00
39.38	190.29	140.19	3.12	223.77	2.00	78.15	0.00	0.00
39.45	193.31	142.31	3.14	226.42	2.00	78.65	0.00	0.00
39.51	197.03	145.04	3.14	229.13	2.00	79.27	0.00	0.00
39.57	201.45	148.33	3.12	231.77	2.00	80.01	0.00	0.00
39.64	206.43	152.05	3.09	234.36	2.00	80.83	0.00	0.00
39.72	209.97	154.62	3.06	235.92	2.00	81.38	0.00	0.00
39.79	210.90	155.19	3.04	235.81	2.00	81.50	0.00	0.00
39.84	209.11	153.65	3.05	234.48	2.00	81.18	0.00	0.00
39.90	206.02	151.08	3.06	232.41	2.00	80.62	0.00	0.00
39.96	202.96	148.57	3.06	229.77	2.00	80.07	0.00	0.00
40.06	199.55	145.71	3.05	226.70	2.00	79.43	0.00	0.00
40.13	195.43	142.38	3.04	223.26	2.00	78.66	0.00	0.00
40.17	191.56	139.34	3.03	219.92	2.00	77.95	0.00	0.00
40.26	187.07	135.71	3.03	216.05	2.00	77.08	0.00	0.00
40.31	182.02	131.75	3.02	211.86	2.00	76.10	0.00	0.00
40.36	176.42	127.42	2.99	206.86	2.00	75.00	0.00	0.00
40.43	171.16	123.34	2.95	201.52	2.00	73.93	0.00	0.00

:: Estimation of post-earthquake lateral Displacements :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	R_f (%)	$Q_{tn,cs}$	FS	D_r	$Gamma_{max}$ (%)	Lat. disp. (in)
40.51	164.14	117.86	2.94	195.74	1.91	72.42	0.49	0.00
40.56	159.97	114.70	2.89	190.93	1.79	71.53	0.60	0.00
40.64	152.18	108.61	2.91	185.56	1.66	69.73	0.74	0.00
40.70	148.35	105.73	2.84	180.74	1.55	68.84	0.91	0.00
40.75	146.10	104.13	2.73	175.76	1.44	68.34	1.12	0.00
40.83	144.83	103.24	2.61	171.24	1.34	68.05	1.36	0.00
40.88	146.29	104.60	2.44	167.25	1.27	68.48	1.62	0.00
40.95	151.45	108.92	2.21	163.89	1.20	69.82	1.87	0.00
41.03	159.00	115.12	1.99	162.69	1.18	71.65	1.97	0.00
41.08	169.86	124.05	1.78	164.27	1.21	74.11	1.84	0.00
41.15	178.00	130.77	1.63	165.80	1.24	75.85	2.06	0.00
41.24	189.19	140.00	1.47	169.37	1.31	78.11	1.84	0.00
41.28	194.60	144.65	1.37	170.54	1.33	79.18	1.77	0.00
41.35	196.88	146.68	1.30	170.24	1.33	79.64	1.79	0.00
41.41	197.86	147.66	1.24	169.29	1.31	79.86	1.84	0.00
41.48	196.40	146.49	1.22	167.63	1.28	79.60	1.94	0.00
41.55	192.75	143.17	1.27	166.29	1.25	78.84	2.02	0.00
41.63	188.20	139.10	1.33	164.51	1.22	77.89	2.14	0.00
41.68	181.44	133.30	1.42	161.92	1.17	76.49	2.32	0.00
41.74	174.04	127.00	1.52	159.25	1.12	74.89	2.29	0.00
41.83	166.17	120.27	1.65	156.93	1.08	73.09	2.54	0.00
41.87	159.62	114.71	1.78	156.04	1.07	71.53	2.65	0.00
41.98	152.99	108.97	1.95	155.95	1.07	69.84	2.65	0.00
42.02	146.03	103.14	2.14	156.49	1.08	68.02	2.59	0.00
42.10	139.05	97.32	2.34	157.32	1.09	66.10	2.49	0.00
42.14	132.52	92.01	2.54	158.36	1.11	64.25	2.27	0.00
42.22	126.16	86.83	2.75	159.59	1.13	62.34	2.08	0.00
42.29	120.67	82.42	2.92	160.51	1.15	60.62	1.96	0.00
42.38	115.55	78.32	3.10	161.46	1.16	58.93	1.83	0.00
42.41	111.25	74.95	3.26	162.34	1.18	57.48	1.72	0.00
42.46	107.34	71.90	3.40	163.00	1.19	56.11	1.65	0.00
42.57	103.94	69.19	3.51	163.11	1.19	54.84	1.35	0.00
42.61	100.91	66.88	3.61	163.01	1.19	53.72	1.37	0.00
42.68	98.50	65.01	3.68	162.77	1.19	52.78	1.40	0.00
42.76	96.24	63.25	3.74	162.34	1.18	51.88	1.46	0.00
42.80	94.09	61.63	3.80	161.80	1.17	51.03	1.53	0.00
42.87	92.43	60.35	3.83	161.02	1.16	50.33	1.65	0.00
42.92	90.98	59.26	3.84	160.04	1.14	49.73	1.82	0.00
42.98	89.10	57.87	3.84	158.36	1.11	48.95	2.15	0.00
43.06	86.12	55.71	3.82	155.17	1.06	47.69	2.95	0.00
43.11	82.66	53.25	3.79	151.63	1.00	46.20	4.21	0.00
43.18	78.34	50.16	3.80	147.91	0.94	44.23	17.73	0.00
43.26	73.08	46.41	3.84	143.94	0.88	41.66	32.26	0.00
43.32	67.13	42.20	3.90	139.61	0.82	38.52	47.25	0.00
43.39	61.24	38.07	3.95	134.85	2.00	35.12	0.00	0.00
43.46	55.24	33.90	3.98	129.27	2.00	31.30	0.00	0.00
43.52	48.95	29.60	4.00	122.72	2.00	26.81	0.00	0.00
43.61	43.21	25.69	3.99	116.06	2.00	22.14	0.00	0.00

:: Estimation of post-earthquake lateral Displacements :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	R_f (%)	$Q_{tn,cs}$	FS	D_r	$Gamma_{max}$ (%)	Lat. disp. (in)
43.64	38.48	22.50	4.03	110.79	2.00	17.77	0.00	0.00
43.70	34.37	19.75	4.05	105.47	2.00	13.46	0.00	0.00
43.79	31.53	17.87	3.95	100.21	2.00	10.16	0.00	0.00
43.84	29.85	16.79	3.74	95.39	2.00	8.11	0.00	0.00
43.90	29.16	16.37	3.52	91.83	2.00	7.26	0.00	0.00
43.97	28.62	16.03	3.37	89.31	2.00	6.57	0.00	0.00
44.05	28.46	15.91	3.31	88.25	2.00	6.33	0.00	0.00
44.10	28.90	16.18	3.29	88.67	2.00	6.89	0.00	0.00
44.18	29.73	16.69	3.35	90.36	2.00	7.91	0.00	0.00
44.24	30.91	17.43	3.42	92.72	2.00	9.34	0.00	0.00
44.30	32.38	18.35	3.51	95.76	2.00	11.03	0.00	0.00
44.38	34.27	19.53	3.61	99.36	2.00	13.10	0.00	0.00
44.45	36.52	20.96	3.68	103.06	2.00	15.43	0.00	0.00
44.49	39.14	22.67	3.69	106.18	2.00	18.02	0.00	0.00
44.57	41.80	24.41	3.65	108.75	2.00	20.45	0.00	0.00
44.64	44.11	25.89	3.68	111.67	2.00	22.40	0.00	0.00
44.72	45.81	26.96	3.74	114.40	2.00	23.74	0.00	0.00
44.79	47.04	27.72	3.80	116.56	2.00	24.65	0.00	0.00
44.84	48.33	28.53	3.83	118.40	2.00	25.61	0.00	0.00
44.92	51.62	30.75	3.66	118.97	2.00	28.07	0.00	0.00
44.96	56.00	33.79	3.40	118.61	2.00	31.18	0.00	0.00
45.03	61.93	37.94	3.07	117.38	2.00	35.02	0.00	0.00
45.09	70.39	43.99	2.69	115.79	2.00	39.90	0.00	0.00
45.19	78.97	50.19	2.38	114.70	2.00	44.24	0.00	0.00
45.23	87.67	56.61	2.12	113.97	2.00	48.22	0.00	0.00
45.28	95.84	62.61	1.96	115.12	2.00	51.55	0.00	0.00
45.38	103.70	68.35	1.85	117.08	2.00	54.44	0.00	0.00
45.43	110.94	73.64	1.79	119.99	2.00	56.90	0.00	0.00
45.48	114.55	76.05	1.85	123.69	0.64	57.97	22.70	0.00
45.58	115.95	76.70	1.96	127.38	2.00	58.25	0.00	0.00
45.62	113.89	74.81	2.13	130.77	2.00	57.42	0.00	0.00
45.67	107.49	69.71	2.41	133.73	2.00	55.09	0.00	0.00
45.78	100.41	64.15	2.72	136.92	2.00	52.35	0.00	0.00
45.82	92.83	58.44	3.06	139.92	2.00	49.27	0.00	0.00
45.88	86.04	53.46	3.31	140.77	2.00	46.33	0.00	0.00
45.98	79.71	48.88	3.55	140.84	2.00	43.37	0.00	0.00
46.02	73.83	44.74	3.76	140.23	2.00	40.45	0.00	0.00
46.07	69.62	41.84	3.83	137.86	2.00	38.24	0.00	0.00
46.17	66.01	39.37	3.85	134.82	2.00	36.23	0.00	0.00
46.21	63.43	37.66	3.80	131.48	2.00	34.77	0.00	0.00
46.27	61.17	36.16	3.75	128.41	2.00	33.42	0.00	0.00
46.37	59.04	34.72	3.70	125.52	2.00	32.08	0.00	0.00
46.39	57.19	33.50	3.68	123.35	2.00	30.90	0.00	0.00
46.47	55.24	32.14	3.75	122.66	2.00	29.53	0.00	0.00
46.57	53.36	30.82	3.84	122.21	2.00	28.15	0.00	0.00
46.62	51.65	29.64	3.92	121.62	2.00	26.87	0.00	0.00
46.67	49.67	28.29	4.04	121.27	2.00	25.32	0.00	0.00
46.77	47.76	26.96	4.16	120.87	2.00	23.74	0.00	0.00

:: Estimation of post-earthquake lateral Displacements :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	R_f (%)	$Q_{tn,cs}$	FS	D_r	$Gamma_{max}$ (%)	Lat. disp. (in)
46.82	46.32	25.98	4.26	120.67	2.00	22.51	0.00	0.00
46.90	45.86	25.64	4.27	120.21	2.00	22.08	0.00	0.00
46.92	45.62	25.48	4.26	119.75	2.00	21.88	0.00	0.00
47.01	45.61	25.43	4.26	119.60	2.00	21.81	0.00	0.00
47.05	45.76	25.51	4.25	119.58	2.00	21.91	0.00	0.00
47.12	45.95	25.59	4.26	119.93	2.00	22.01	0.00	0.00
47.21	45.72	25.38	4.33	120.48	2.00	21.74	0.00	0.00
47.28	46.33	25.74	4.31	120.95	2.00	22.20	0.00	0.00
47.32	46.71	25.95	4.32	121.44	2.00	22.48	0.00	0.00
47.40	47.02	26.10	4.35	122.19	2.00	22.66	0.00	0.00
47.45	47.62	26.44	4.38	123.33	2.00	23.09	0.00	0.00
47.55	48.61	27.01	4.37	124.26	2.00	23.80	0.00	0.00
47.58	49.96	27.88	4.29	124.59	2.00	24.84	0.00	0.00
47.66	51.87	29.11	4.15	124.45	2.00	26.26	0.00	0.00
47.74	54.02	30.50	3.99	124.17	2.00	27.81	0.00	0.00
47.80	56.71	32.27	3.82	124.05	2.00	29.67	0.00	0.00
47.85	58.65	33.53	3.72	124.22	2.00	30.94	0.00	0.00
47.93	60.64	34.81	3.64	124.49	2.00	32.17	0.00	0.00
47.98	62.76	36.21	3.54	124.46	2.00	33.47	0.00	0.00
48.04	64.99	37.69	3.41	124.03	0.65	34.80	51.20	0.00
48.11	67.41	39.30	3.29	123.57	0.65	36.18	51.20	0.00
48.20	69.59	40.73	3.19	123.38	0.65	37.36	51.20	0.00
48.24	71.33	41.88	3.14	123.68	0.65	38.28	51.20	0.00
48.30	72.97	42.95	3.10	123.93	0.65	39.10	51.20	0.00
48.39	74.42	43.87	3.06	124.05	0.65	39.81	51.20	0.00
48.44	75.99	44.91	3.02	124.44	0.66	40.58	51.20	0.00
48.53	77.80	46.06	2.99	124.94	0.66	41.42	51.20	0.00
48.59	79.60	47.23	2.95	125.51	0.67	42.24	51.20	0.00
48.64	80.98	48.11	2.95	126.34	0.68	42.85	51.20	0.00
48.70	82.04	48.73	2.97	127.52	0.69	43.27	51.20	0.00
48.78	83.53	49.64	2.98	128.78	0.71	43.88	51.20	0.00
48.82	85.19	50.69	2.99	129.97	0.72	44.58	51.20	0.00
48.89	87.28	52.03	2.97	131.08	0.74	45.43	29.49	0.00
48.98	90.26	53.97	2.93	132.03	0.75	46.64	26.57	0.00
49.05	93.73	56.28	2.86	132.78	0.76	48.03	24.49	0.00
49.09	97.44	58.81	2.79	133.45	0.77	49.48	22.78	0.00
49.16	101.81	61.78	2.70	134.12	0.78	51.11	21.16	0.00
49.24	106.91	65.26	2.61	135.13	0.79	52.91	18.96	0.00
49.31	112.14	68.86	2.52	136.11	0.80	54.69	17.05	0.00
49.38	116.76	72.05	2.44	137.00	0.82	56.18	8.80	0.00
49.43	120.62	74.75	2.37	137.59	0.82	57.39	8.42	0.00
49.52	123.30	76.64	2.29	137.04	0.82	58.22	8.74	0.00
49.58	124.61	77.65	2.21	135.66	0.80	58.65	9.64	0.00
49.63	124.38	77.57	2.16	133.96	0.78	58.62	10.89	0.00
49.71	122.70	76.38	2.14	132.38	0.76	58.11	12.19	0.00
49.77	119.64	74.19	2.15	130.76	2.00	57.15	0.00	0.00
49.82	114.85	70.80	2.19	128.74	2.00	55.60	0.00	0.00
49.88	107.69	65.75	2.26	126.27	2.00	53.16	0.00	0.00

:: Estimation of post-earthquake lateral Displacements :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	R_f (%)	$Q_{tn,cs}$	FS	D_r	$Gamma_{max}$ (%)	Lat. disp. (in)
49.97	100.43	60.65	2.35	123.80	2.00	50.49	0.00	0.00
50.01	94.19	56.34	2.42	121.67	2.00	48.06	0.00	0.00
50.07	89.11	52.76	2.54	121.25	2.00	45.89	0.00	0.00
50.17	84.50	49.44	2.71	122.07	2.00	43.75	0.00	0.00
50.22	80.39	46.53	2.89	123.24	2.00	41.75	0.00	0.00
50.29	76.13	43.58	3.05	123.52	2.00	39.58	0.00	0.00
50.37	72.92	41.37	3.14	123.02	2.00	37.87	0.00	0.00
50.42	69.90	39.36	3.21	122.05	2.00	36.22	0.00	0.00
50.47	68.34	38.34	3.21	120.84	2.00	35.35	0.00	0.00
50.57	65.94	36.74	3.23	119.31	2.00	33.95	0.00	0.00
50.63	62.51	34.52	3.29	117.49	2.00	31.89	0.00	0.00
50.68	58.31	31.85	3.33	114.64	2.00	29.24	0.00	0.00
50.73	53.55	28.88	3.32	110.42	2.00	26.00	0.00	0.00
50.79	48.91	26.02	3.28	105.58	2.00	22.56	0.00	0.00
50.88	45.25	23.79	3.18	100.57	2.00	19.61	0.00	0.00
50.93	41.03	21.25	3.10	95.16	2.00	15.88	0.00	0.00
51.03	37.66	19.24	2.93	89.48	2.00	12.60	0.00	0.00
51.07	34.69	17.53	2.73	83.65	2.00	9.52	0.00	0.00
51.14	32.58	16.34	2.45	77.75	2.00	7.21	0.00	0.00
51.23	30.90	15.42	2.16	72.12	2.00	5.30	0.00	0.00
51.27	29.21	14.49	1.92	67.10	2.00	3.24	0.00	0.00
51.33	28.11	13.89	1.74	63.59	2.00	1.84	0.00	0.00
51.42	27.14	13.35	1.59	60.46	2.00	0.53	0.00	0.00
51.48	26.51	13.02	1.45	57.82	2.00	0.00	0.00	0.00
51.52	26.33	12.93	1.40	56.91	2.00	0.00	0.00	0.00
51.60	26.44	12.98	1.39	56.75	2.00	0.00	0.00	0.00
51.68	26.86	13.22	1.39	57.16	2.00	0.21	0.00	0.00
51.72	27.53	13.60	1.43	58.21	2.00	1.15	0.00	0.00
51.81	28.12	13.90	1.50	59.73	2.00	1.88	0.00	0.00
51.87	28.73	14.22	1.58	61.44	2.00	2.63	0.00	0.00
51.91	28.93	14.29	1.66	62.90	2.00	2.79	0.00	0.00
51.98	28.88	14.21	1.74	63.93	2.00	2.60	0.00	0.00
52.07	28.66	14.03	1.80	64.66	2.00	2.18	0.00	0.00
52.10	28.09	13.67	1.82	64.51	2.00	1.32	0.00	0.00
52.17	27.20	13.12	1.83	63.79	2.00	0.00	0.00	0.00
52.24	26.15	12.48	1.83	62.82	2.00	0.00	0.00	0.00
52.31	24.96	11.76	1.83	61.59	2.00	0.00	0.00	0.00
52.37	23.83	11.10	1.78	59.89	2.00	0.00	0.00	0.00
52.46	22.77	10.48	1.71	57.92	2.00	0.00	0.00	0.00
52.51	21.99	10.05	1.64	56.16	2.00	0.00	0.00	0.00
52.57	21.52	9.79	1.54	54.48	2.00	0.00	0.00	0.00
52.66	21.13	9.58	1.45	52.88	2.00	0.00	0.00	0.00
52.71	20.91	9.46	1.39	51.80	2.00	0.00	0.00	0.00
52.78	20.78	9.39	1.34	51.06	2.00	0.00	0.00	0.00
52.86	20.69	9.34	1.31	50.46	2.00	0.00	0.00	0.00
52.91	20.62	9.30	1.28	50.07	2.00	0.00	0.00	0.00
52.99	20.60	9.29	1.27	49.83	2.00	0.00	0.00	0.00
53.06	20.61	9.29	1.26	49.67	2.00	0.00	0.00	0.00

:: Estimation of post-earthquake lateral Displacements :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	R_f (%)	$Q_{tn,cs}$	FS	D_r	$Gamma_{max}$ (%)	Lat. disp. (in)
53.09	20.61	9.29	1.24	49.44	2.00	0.00	0.00	0.00
53.16	20.64	9.30	1.23	49.35	2.00	0.00	0.00	0.00
53.25	20.67	9.30	1.23	49.26	2.00	0.00	0.00	0.00
53.29	20.68	9.31	1.22	49.17	2.00	0.00	0.00	0.00
53.36	20.66	9.29	1.22	49.08	2.00	0.00	0.00	0.00
53.45	20.68	9.29	1.21	48.99	2.00	0.00	0.00	0.00
53.50	20.68	9.28	1.20	48.90	2.00	0.00	0.00	0.00
53.55	20.67	9.27	1.21	48.97	2.00	0.00	0.00	0.00
53.64	20.67	9.25	1.21	49.03	2.00	0.00	0.00	0.00
53.69	20.70	9.26	1.22	49.09	2.00	0.00	0.00	0.00
53.76	20.73	9.27	1.22	49.08	2.00	0.00	0.00	0.00
53.84	20.80	9.29	1.22	49.22	2.00	0.00	0.00	0.00
53.88	20.91	9.35	1.24	49.59	2.00	0.00	0.00	0.00
53.96	21.17	9.48	1.26	50.03	2.00	0.00	0.00	0.00
54.03	21.41	9.60	1.28	50.46	2.00	0.00	0.00	0.00
54.08	21.59	9.69	1.29	50.82	2.00	0.00	0.00	0.00
54.17	21.74	9.76	1.30	51.09	2.00	0.00	0.00	0.00
54.23	21.88	9.83	1.32	51.37	2.00	0.00	0.00	0.00
54.27	21.99	9.88	1.33	51.65	2.00	0.00	0.00	0.00
54.38	22.08	9.91	1.33	51.77	2.00	0.00	0.00	0.00
54.42	22.14	9.94	1.33	51.69	2.00	0.00	0.00	0.00
54.47	22.17	9.97	1.29	51.26	2.00	0.00	0.00	0.00
54.53	22.12	9.94	1.26	50.74	2.00	0.00	0.00	0.00
54.61	22.06	9.91	1.23	50.22	2.00	0.00	0.00	0.00
54.68	22.03	9.90	1.21	49.84	2.00	0.00	0.00	0.00
54.73	22.02	9.89	1.19	49.53	2.00	0.00	0.00	0.00
54.80	22.01	9.87	1.18	49.37	2.00	0.00	0.00	0.00
54.88	22.03	9.87	1.18	49.35	2.00	0.00	0.00	0.00
54.95	22.09	9.89	1.19	49.56	2.00	0.00	0.00	0.00
55.02	22.17	9.92	1.21	49.92	2.00	0.00	0.00	0.00
55.07	22.23	9.93	1.24	50.42	2.00	0.00	0.00	0.00
55.15	22.25	9.91	1.28	50.97	2.00	0.00	0.00	0.00
55.21	22.27	9.90	1.32	51.52	2.00	0.00	0.00	0.00
55.27	22.39	9.96	1.33	51.86	2.00	0.00	0.00	0.00
55.34	22.62	10.08	1.34	52.13	2.00	0.00	0.00	0.00
55.42	22.88	10.21	1.34	52.33	2.00	0.00	0.00	0.00
55.47	23.13	10.34	1.35	52.59	2.00	0.00	0.00	0.00
55.54	23.41	10.48	1.39	53.39	2.00	0.00	0.00	0.00
55.62	23.74	10.64	1.43	54.24	2.00	0.00	0.00	0.00
55.65	24.32	10.95	1.47	55.28	2.00	0.00	0.00	0.00
55.72	25.17	11.41	1.50	56.41	2.00	0.00	0.00	0.00
55.81	26.14	11.94	1.54	57.86	2.00	0.00	0.00	0.00
55.84	27.15	12.48	1.62	59.87	2.00	0.00	0.00	0.00
55.91	28.26	13.02	1.80	63.28	2.00	0.00	0.00	0.00
55.98	29.52	13.64	2.00	67.15	2.00	1.25	0.00	0.00
56.05	31.10	14.46	2.18	70.92	2.00	3.18	0.00	0.00
56.11	34.04	16.12	2.21	73.94	2.00	6.76	0.00	0.00
56.21	38.52	18.71	2.19	77.33	2.00	11.67	0.00	0.00

:: Estimation of post-earthquake lateral Displacements :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	R_f (%)	$Q_{tn,cs}$	FS	D_r	$Gamma_{max}$ (%)	Lat. disp. (in)
56.26	43.85	21.85	2.15	80.74	2.00	16.79	0.00	0.00
56.31	51.25	26.31	2.08	84.44	2.00	22.93	0.00	0.00
56.39	58.39	30.64	2.04	88.08	2.00	27.95	0.00	0.00
56.46	66.60	35.71	1.98	91.68	2.00	33.01	0.00	0.00
56.50	74.21	40.49	1.92	94.69	2.00	37.16	0.00	0.00
56.60	80.84	44.64	1.89	97.58	2.00	40.38	0.00	0.00
56.65	86.36	48.10	1.88	100.49	2.00	42.84	0.00	0.00
56.72	89.96	50.26	1.92	103.30	2.00	44.29	0.00	0.00
56.78	91.09	50.86	1.96	104.84	2.00	44.68	0.00	0.00
56.87	90.61	50.39	2.00	105.65	2.00	44.38	0.00	0.00
56.93	86.85	47.84	2.09	105.54	2.00	42.66	0.00	0.00
56.97	82.39	44.91	2.17	104.79	2.00	40.58	0.00	0.00
57.05	76.32	40.97	2.27	103.41	2.00	37.55	0.00	0.00
57.11	69.97	36.95	2.36	101.47	2.00	34.14	0.00	0.00
57.17	63.87	33.16	2.43	98.86	2.00	30.57	0.00	0.00
57.25	58.18	29.71	2.46	95.61	2.00	26.94	0.00	0.00
57.31	52.54	26.32	2.47	91.87	2.00	22.94	0.00	0.00
57.37	47.66	23.46	2.46	88.15	2.00	19.14	0.00	0.00
57.42	43.35	20.97	2.41	84.11	2.00	15.44	0.00	0.00
57.48	39.91	19.02	2.32	79.93	2.00	12.22	0.00	0.00
57.56	37.11	17.46	2.21	75.95	2.00	9.40	0.00	0.00
57.64	34.62	16.08	2.09	72.08	2.00	6.68	0.00	0.00
57.70	32.80	15.10	1.95	68.55	2.00	4.61	0.00	0.00
57.74	31.50	14.44	1.79	65.16	2.00	3.13	0.00	0.00
57.81	30.51	13.94	1.64	62.19	2.00	1.96	0.00	0.00
57.90	29.96	13.68	1.51	59.72	2.00	1.34	0.00	0.00
57.95	29.50	13.45	1.42	58.04	2.00	0.79	0.00	0.00
58.06	29.02	13.15	1.44	57.86	2.00	0.03	0.00	0.00
58.09	28.66	12.92	1.48	58.28	2.00	0.00	0.00	0.00
58.15	28.80	12.96	1.52	59.02	2.00	0.00	0.00	0.00
58.20	29.53	13.36	1.53	59.61	2.00	0.57	0.00	0.00
58.29	30.50	13.91	1.50	59.94	2.00	1.89	0.00	0.00
58.33	31.57	14.52	1.49	60.44	2.00	3.31	0.00	0.00
58.40	32.28	14.90	1.51	61.27	2.00	4.16	0.00	0.00
58.48	32.70	15.11	1.54	62.00	2.00	4.62	0.00	0.00
58.55	33.02	15.26	1.56	62.56	2.00	4.95	0.00	0.00
58.60	32.96	15.23	1.54	62.16	2.00	4.88	0.00	0.00
58.66	33.04	15.31	1.47	61.04	2.00	5.06	0.00	0.00
58.75	32.78	15.19	1.40	59.62	2.00	4.79	0.00	0.00
58.80	31.98	14.73	1.37	58.57	2.00	3.79	0.00	0.00
58.88	30.93	14.12	1.36	57.74	2.00	2.39	0.00	0.00
58.97	29.66	13.38	1.36	56.89	2.00	0.61	0.00	0.00
59.02	28.78	12.89	1.32	55.64	2.00	0.00	0.00	0.00
59.06	28.25	12.61	1.27	54.47	2.00	0.00	0.00	0.00
59.12	27.98	12.49	1.21	53.25	2.00	0.00	0.00	0.00
59.20	28.12	12.60	1.15	52.31	2.00	0.00	0.00	0.00
59.26	28.04	12.55	1.13	51.90	2.00	0.00	0.00	0.00
59.35	28.00	12.51	1.12	51.82	2.00	0.00	0.00	0.00

:: Estimation of post-earthquake lateral Displacements :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	R_f (%)	$Q_{tn,cs}$	FS	D_r	$Gamma_{max}$ (%)	Lat. disp. (in)
59.41	28.02	12.50	1.14	52.14	2.00	0.00	0.00	0.00
59.46	28.08	12.51	1.17	52.66	2.00	0.00	0.00	0.00
59.52	28.38	12.65	1.21	53.41	2.00	0.00	0.00	0.00
59.61	28.81	12.85	1.24	54.27	2.00	0.00	0.00	0.00
59.68	29.23	13.06	1.27	54.99	2.00	0.00	0.00	0.00
59.72	29.44	13.14	1.31	55.77	2.00	0.02	0.00	0.00
59.79	29.54	13.16	1.35	56.42	2.00	0.07	0.00	0.00
59.86	29.55	13.13	1.38	56.94	2.00	0.00	0.00	0.00
59.91	29.54	13.20	1.25	54.87	2.00	0.16	0.00	0.00
60.01	29.54	13.28	1.11	52.42	2.00	0.36	0.00	0.00
60.06	29.43	13.32	0.96	49.70	2.00	0.46	0.00	0.00
60.15	29.33	13.39	0.81	46.66	2.00	0.64	0.00	0.00
60.19	29.08	13.40	0.65	43.20	2.00	0.67	0.00	0.00
60.26	29.01	13.54	0.48	39.48	2.00	1.01	0.00	0.00
60.35	28.68	13.58	0.32	35.31	2.00	1.09	0.00	0.00
60.40	28.68	13.89	0.16	30.80	2.00	1.85	0.00	0.00
60.45	28.56	N/A	0.00	-1.00	2.00	0.00	0.00	0.00
60.51	29.38	N/A	0.00	-1.00	2.00	0.00	0.00	0.00

Total estimated displacement: 10.07

Abbreviations

q_t: Total cone resistance
Q_{tn}: Adjusted cone resistance to an effective overburden stress of 1 atm
R_f: Friction ration
$Q_{tn,cs}$: Adjusted and corrected cone resistance due to fines
FS: Calculated factor of safety against liquefaction
D_r: Calculated relative density
$Gamma_{max}$: Calculated maximum cyclic shear strain
Lat. disp.: Lateral displacement

:: Strength loss calculation (Robertson (2009) ::

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
0.09	83.15	133.58	1.00	133.58	1.64	N/A	N/A
0.15	124.45	199.93	1.00	199.93	1.44	N/A	N/A
0.21	164.56	264.38	1.00	264.38	1.32	N/A	N/A
0.29	173.53	278.77	1.00	278.77	1.35	N/A	N/A
0.34	170.25	273.50	1.00	273.50	1.40	N/A	N/A
0.40	184.41	296.24	1.00	296.24	1.41	N/A	N/A
0.49	188.56	302.90	1.00	302.90	1.45	N/A	N/A
0.55	179.22	287.88	1.00	287.88	1.52	N/A	N/A
0.59	162.51	261.04	1.00	261.04	1.62	N/A	N/A
0.69	150.33	241.46	1.04	250.82	1.70	N/A	N/A
0.74	137.32	220.54	1.10	241.72	1.79	N/A	N/A
0.81	123.76	198.76	1.16	231.55	1.87	N/A	N/A
0.89	110.59	177.58	1.26	222.96	1.96	N/A	N/A
0.94	98.81	158.66	1.36	215.26	2.04	N/A	N/A
0.99	93.80	150.60	1.41	212.11	2.07	N/A	N/A
1.09	92.09	147.85	1.43	211.59	2.09	N/A	N/A
1.14	92.39	148.32	1.44	213.14	2.09	N/A	N/A
1.19	97.81	157.02	1.39	218.13	2.06	N/A	N/A
1.26	98.76	158.55	1.39	219.88	2.06	N/A	N/A
1.34	98.49	158.11	1.39	220.12	2.06	N/A	N/A
1.38	98.38	157.93	1.39	220.09	2.06	N/A	N/A
1.50	97.02	155.72	1.40	218.45	2.07	N/A	N/A
1.53	94.55	151.75	1.42	215.48	2.08	N/A	N/A
1.59	90.36	145.01	1.46	212.18	2.10	N/A	N/A
1.68	85.92	137.87	1.51	208.71	2.13	N/A	N/A
1.72	81.17	130.24	1.57	205.01	2.16	N/A	N/A
1.78	75.44	121.02	1.67	202.37	2.20	N/A	N/A
1.87	69.69	111.77	1.80	200.88	2.25	N/A	N/A
1.93	67.42	108.12	1.86	200.61	2.27	N/A	N/A
1.98	64.42	103.29	1.92	198.19	2.29	N/A	N/A
2.06	62.68	100.50	1.94	194.72	2.30	N/A	N/A
2.13	63.84	102.35	1.90	194.57	2.28	N/A	N/A
2.17	67.39	108.06	1.80	194.87	2.25	N/A	N/A
2.28	70.26	112.65	1.73	195.27	2.23	N/A	N/A
2.32	72.12	115.64	1.69	195.38	2.21	N/A	N/A
2.39	71.08	113.95	1.68	191.64	2.21	N/A	N/A
2.43	72.10	115.59	1.62	187.09	2.18	N/A	N/A
2.52	70.92	113.69	1.59	180.76	2.17	N/A	N/A
2.57	69.46	111.34	1.58	176.14	2.16	N/A	N/A
2.66	68.27	109.41	1.58	173.38	2.16	N/A	N/A
2.69	64.80	103.84	1.64	170.20	2.19	N/A	N/A
2.77	59.92	95.98	1.74	166.69	2.23	N/A	N/A
2.86	55.44	88.78	1.84	163.61	2.27	N/A	N/A
2.92	51.45	82.36	1.96	161.82	2.30	N/A	N/A
2.96	48.19	77.12	2.08	160.64	2.34	N/A	N/A
3.06	46.08	73.72	2.15	158.82	2.36	N/A	N/A
3.11	46.45	74.31	2.10	156.09	2.34	N/A	N/A
3.15	48.40	77.45	1.96	152.07	2.30	N/A	N/A

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
3.26	54.10	86.58	1.72	148.68	2.22	N/A	N/A
3.30	60.61	97.05	1.52	147.19	2.13	N/A	N/A
3.37	68.26	109.33	1.36	148.15	2.04	N/A	N/A
3.46	73.99	118.52	1.27	150.56	1.98	N/A	N/A
3.51	77.79	124.63	1.22	152.41	1.93	N/A	N/A
3.56	80.79	129.44	1.20	155.05	1.91	N/A	N/A
3.64	81.12	129.96	1.20	156.20	1.91	N/A	N/A
3.71	79.43	127.24	1.23	156.34	1.94	N/A	N/A
3.76	75.75	121.33	1.28	155.78	1.99	N/A	N/A
3.81	67.08	107.39	1.41	151.01	2.07	N/A	N/A
3.90	57.38	91.80	1.61	147.39	2.17	N/A	N/A
3.94	47.30	75.59	1.94	146.95	2.30	N/A	N/A
4.01	40.10	64.02	2.29	146.35	2.39	N/A	N/A
4.09	35.01	55.83	2.58	144.12	2.46	N/A	N/A
4.15	30.51	48.60	2.89	140.47	2.52	N/A	N/A
4.20	27.97	44.51	3.04	135.41	2.55	N/A	N/A
4.30	25.89	41.16	3.15	129.86	2.57	N/A	N/A
4.35	24.02	38.16	3.25	124.00	2.59	N/A	N/A
4.41	23.02	36.55	3.28	119.96	2.59	N/A	N/A
4.50	22.67	35.97	3.24	116.38	2.58	N/A	N/A
4.55	22.29	35.36	3.20	113.01	2.58	N/A	N/A
4.60	21.44	33.98	3.30	112.03	2.60	N/A	N/A
4.68	20.60	32.64	3.43	112.02	2.62	N/A	N/A
4.75	19.97	31.62	3.56	112.48	2.64	N/A	N/A
4.79	19.55	30.93	3.67	113.38	2.65	N/A	N/A
4.88	19.20	30.36	3.77	114.53	2.67	N/A	N/A
4.95	18.93	29.93	3.87	115.81	2.68	N/A	N/A
4.99	18.80	29.71	3.94	117.17	2.69	N/A	N/A
5.06	18.75	29.62	4.01	118.85	2.70	N/A	N/A
5.14	18.72	29.57	4.08	120.60	2.71	N/A	N/A
5.21	18.75	29.61	4.13	122.18	2.72	N/A	N/A
5.26	18.80	29.69	4.16	123.37	2.72	N/A	N/A
5.33	18.79	29.66	4.20	124.49	2.73	N/A	N/A
5.40	18.78	29.64	4.23	125.33	2.73	N/A	N/A
5.45	18.77	29.62	4.26	126.17	2.74	N/A	N/A
5.51	18.82	29.70	4.28	126.96	2.74	N/A	N/A
5.60	18.84	29.73	4.30	127.68	2.74	N/A	N/A
5.66	18.86	29.74	4.31	128.22	2.74	N/A	N/A
5.71	18.80	29.64	4.34	128.62	2.75	N/A	N/A
5.78	18.67	29.43	4.38	128.99	2.75	N/A	N/A
5.86	18.48	29.12	4.44	129.14	2.76	N/A	N/A
5.93	18.26	28.76	4.48	128.94	2.76	N/A	N/A
6.01	18.01	28.35	4.53	128.49	2.77	N/A	N/A
6.05	17.70	27.84	4.58	127.63	2.78	N/A	N/A
6.11	17.27	27.15	4.66	126.38	2.78	N/A	N/A
6.21	16.76	26.33	4.75	124.99	2.80	N/A	N/A
6.25	16.19	25.40	4.86	123.43	2.81	N/A	N/A
6.31	15.61	24.47	4.98	121.84	2.82	N/A	N/A

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
6.39	15.07	23.59	5.09	120.11	2.84	N/A	N/A
6.45	14.58	22.80	5.20	118.49	2.85	N/A	N/A
6.51	14.21	22.19	5.27	116.87	2.85	N/A	N/A
6.58	13.86	21.62	5.34	115.50	2.86	N/A	N/A
6.66	13.60	21.20	5.39	114.37	2.87	N/A	N/A
6.70	13.50	21.04	5.39	113.43	2.87	N/A	N/A
6.78	13.46	20.96	5.37	112.65	2.87	N/A	N/A
6.85	13.51	21.03	5.32	111.91	2.86	N/A	N/A
6.89	13.63	21.23	5.23	111.13	2.85	N/A	N/A
7.00	13.83	21.54	5.13	110.50	2.84	N/A	N/A
7.03	14.14	22.03	4.99	109.89	2.82	N/A	N/A
7.10	14.46	22.55	4.85	109.37	2.81	N/A	N/A
7.19	14.88	23.20	4.69	108.77	2.79	N/A	N/A
7.25	15.30	23.88	4.54	108.37	2.77	N/A	N/A
7.30	15.72	24.55	4.42	108.39	2.76	N/A	N/A
7.37	16.17	25.27	4.30	108.69	2.74	N/A	N/A
7.44	16.57	25.90	4.22	109.23	2.73	N/A	N/A
7.49	16.84	26.33	4.18	109.96	2.72	N/A	N/A
7.56	17.03	26.64	4.14	110.23	2.72	N/A	N/A
7.64	17.06	26.68	4.12	110.01	2.72	N/A	N/A
7.68	16.96	26.52	4.17	110.59	2.72	N/A	N/A
7.79	16.74	26.14	4.25	111.18	2.73	N/A	N/A
7.83	16.45	25.67	4.34	111.39	2.75	N/A	N/A
7.90	16.04	25.01	4.45	111.18	2.76	N/A	N/A
7.98	15.56	24.23	4.56	110.40	2.77	N/A	N/A
8.02	15.03	23.37	4.68	109.33	2.79	N/A	N/A
8.09	14.64	22.74	4.75	108.03	2.80	N/A	N/A
8.15	14.30	22.19	4.83	107.10	2.80	N/A	N/A
8.23	14.13	21.91	4.87	106.69	2.81	N/A	N/A
8.29	14.15	21.94	4.81	105.61	2.80	N/A	N/A
8.34	14.26	22.11	4.72	104.46	2.79	N/A	N/A
8.41	14.46	22.43	4.62	103.67	2.78	N/A	N/A
8.48	14.80	22.96	4.49	103.11	2.76	N/A	N/A
8.55	15.24	23.66	4.35	102.91	2.75	N/A	N/A
8.60	15.79	24.55	4.19	102.94	2.73	N/A	N/A
8.66	16.33	25.40	4.06	103.10	2.71	N/A	N/A
8.74	16.89	26.31	3.94	103.55	2.69	N/A	N/A
8.83	17.43	27.16	3.85	104.55	2.68	N/A	N/A
8.90	17.91	27.92	3.79	105.79	2.67	N/A	N/A
8.94	18.32	28.58	3.75	107.17	2.67	N/A	N/A
9.01	18.66	29.11	3.74	108.78	2.66	2.42	2.42
9.09	18.90	29.50	3.74	110.44	2.66	2.43	2.43
9.15	19.06	29.75	3.77	112.13	2.67	2.43	2.43
9.20	19.18	29.93	3.81	113.94	2.67	2.43	2.43
9.29	19.30	30.11	3.85	115.92	2.68	2.43	2.43
9.35	19.43	30.33	3.89	117.85	2.68	2.43	2.43
9.39	19.54	30.50	3.91	119.21	2.69	2.43	2.43
9.45	19.66	30.68	3.92	120.17	2.69	2.43	2.43

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
9.55	19.97	31.17	3.88	120.89	2.68	2.44	2.44
9.64	20.38	31.83	3.81	121.43	2.67	2.47	2.47
9.65	20.91	32.67	3.73	121.97	2.66	2.54	2.54
9.73	21.47	33.57	3.65	122.48	2.65	2.59	2.59
9.79	21.98	34.31	3.59	123.03	2.64	2.63	2.63
9.84	22.46	34.86	3.53	122.99	2.63	2.68	2.68
9.91	22.88	35.24	3.48	122.67	2.62	2.71	2.71
9.99	23.25	35.53	3.44	122.26	2.62	2.73	2.73
10.08	23.63	35.78	3.40	121.63	2.61	2.75	2.75
10.14	23.82	35.88	3.38	121.31	2.61	2.76	2.76
10.19	23.87	35.79	3.38	120.88	2.61	2.75	2.75
10.25	23.88	35.62	3.38	120.28	2.61	2.74	2.74
10.34	23.79	35.24	3.40	119.75	2.61	2.70	2.70
10.38	23.82	35.15	3.39	119.11	2.61	2.69	2.69
10.44	23.92	35.10	3.37	118.25	2.61	2.69	2.69
10.52	23.94	34.89	3.36	117.11	2.60	2.67	2.67
10.59	23.96	34.70	3.35	116.11	2.60	2.66	2.66
10.63	23.88	34.48	3.35	115.67	2.60	2.64	2.64
10.70	23.75	34.11	3.37	115.08	2.61	2.61	2.61
10.78	23.71	33.84	3.38	114.48	2.61	2.58	2.58
10.87	24.05	34.05	3.35	114.07	2.60	2.60	2.60
10.93	24.68	34.72	3.27	113.43	2.59	0.69	0.69
10.97	25.09	35.14	3.22	113.33	2.58	0.69	0.69
11.03	25.34	35.34	3.23	114.00	2.58	0.69	0.69
11.12	25.57	35.43	3.25	115.11	2.59	0.69	0.69
11.16	26.10	36.05	3.22	116.20	2.58	0.69	0.69
11.23	26.69	36.65	3.20	117.14	2.58	0.70	0.70
11.31	27.32	37.28	3.17	118.24	2.57	0.70	0.70
11.37	28.14	38.20	3.13	119.49	2.57	0.70	0.70
11.44	28.65	38.70	3.12	120.91	2.57	0.70	0.70
11.51	28.96	38.94	3.14	122.45	2.57	0.70	0.70
11.56	29.46	39.47	3.13	123.56	2.57	0.70	0.70
11.63	29.97	39.93	3.11	124.20	2.56	0.71	0.71
11.71	30.37	40.22	3.10	124.71	2.56	0.71	0.71
11.76	30.29	39.99	3.13	125.36	2.57	0.71	0.71
11.83	30.13	39.61	3.17	125.68	2.57	0.70	0.70
11.91	29.90	39.12	3.22	125.79	2.58	0.70	0.70
11.94	29.36	38.36	3.28	125.85	2.59	0.70	0.70
12.05	28.72	37.35	3.35	125.25	2.60	2.81	2.81
12.10	28.18	36.60	3.41	124.65	2.61	2.75	2.75
12.14	27.59	35.82	3.46	124.10	2.62	2.69	2.69
12.25	27.11	35.08	3.52	123.36	2.63	2.63	2.63
12.29	26.81	34.65	3.54	122.58	2.63	2.59	2.59
12.35	26.66	34.38	3.55	122.06	2.64	2.57	2.57
12.44	26.59	34.17	3.55	121.34	2.64	2.56	2.56
12.49	26.67	34.20	3.52	120.41	2.63	2.56	2.56
12.55	26.82	34.29	3.48	119.34	2.62	2.57	2.57
12.61	26.84	34.21	3.45	118.04	2.62	2.56	2.56

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
12.70	26.47	33.64	3.47	116.91	2.62	2.52	2.52
12.75	25.93	32.91	3.51	115.62	2.63	2.46	2.46
12.81	25.23	31.96	3.56	113.61	2.64	2.39	2.39
12.89	24.43	30.85	3.60	110.95	2.64	2.30	2.30
12.94	23.55	29.68	3.63	107.89	2.65	2.21	2.21
12.99	22.55	28.37	3.70	105.01	2.66	2.11	2.11
13.08	21.42	26.86	3.81	102.27	2.67	1.99	1.99
13.15	20.17	25.24	3.94	99.55	2.69	1.87	1.87
13.20	18.94	23.67	4.09	96.93	2.71	1.75	1.75
13.27	17.94	22.36	4.20	94.01	2.73	1.65	1.65
13.32	17.08	21.23	4.29	91.09	2.74	1.56	1.56
13.39	16.29	20.19	4.39	88.71	2.75	1.48	1.48
13.48	15.57	19.24	4.52	87.03	2.77	1.41	1.41
13.54	14.85	18.31	4.68	85.67	2.79	1.34	1.34
13.59	14.26	17.54	4.81	84.40	2.80	1.28	1.28
13.65	13.72	16.84	4.94	83.16	2.82	1.22	1.22
13.74	13.35	16.32	5.02	81.98	2.83	1.18	1.18
13.80	13.07	15.93	5.06	80.63	2.83	1.16	1.16
13.89	12.89	15.65	5.06	79.16	2.83	1.14	1.14
13.93	12.67	15.36	5.11	78.57	2.84	1.11	1.11
13.99	12.47	15.09	5.24	79.11	2.85	1.09	1.09
14.07	12.36	14.93	5.35	79.81	2.86	1.08	1.08
14.12	12.41	14.97	5.38	80.54	2.87	1.08	1.08
14.18	12.84	15.48	5.25	81.24	2.85	1.12	1.12
14.26	13.66	16.43	5.00	82.12	2.82	1.19	1.19
14.34	14.47	17.37	4.79	83.28	2.80	1.26	1.26
14.38	15.06	18.09	4.73	85.64	2.79	1.32	1.32
14.47	15.53	18.63	4.75	88.46	2.80	1.36	1.36
14.53	16.03	19.23	4.72	90.78	2.79	1.40	1.40
14.57	16.61	19.90	4.64	92.32	2.78	1.45	1.45
14.64	17.04	20.39	4.59	93.50	2.78	1.49	1.49
14.72	17.40	20.77	4.55	94.50	2.77	1.52	1.52
14.80	17.27	20.58	4.63	95.26	2.78	1.50	1.50
14.83	16.85	20.07	4.78	95.90	2.80	1.46	1.46
14.92	16.39	19.48	4.95	96.48	2.82	1.41	1.41
14.97	16.24	19.28	5.02	96.80	2.83	1.40	1.40
15.06	16.27	19.26	5.06	97.42	2.83	1.39	1.39
15.10	16.43	19.44	5.08	98.73	2.83	1.41	1.41
15.17	16.88	19.94	5.05	100.69	2.83	1.44	1.44
15.25	17.82	21.02	4.91	103.31	2.82	1.52	1.52
15.31	19.04	22.44	4.73	106.25	2.79	1.63	1.63
15.37	20.79	24.48	4.48	109.75	2.76	1.78	1.78
15.44	22.91	26.92	4.22	113.74	2.73	1.97	1.97
15.51	25.24	29.60	3.98	117.67	2.70	2.17	2.17
15.56	27.89	32.64	3.73	121.72	2.66	2.40	2.40
15.63	30.62	35.75	3.53	126.33	2.63	2.64	2.64
15.71	33.36	38.84	3.36	130.50	2.61	2.88	2.88
15.76	35.88	41.68	3.22	134.26	2.58	0.71	0.71

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
15.82	38.00	44.04	3.12	137.37	2.56	0.72	0.72
15.90	39.72	45.92	3.05	140.10	2.55	0.72	0.72
15.95	40.95	47.26	3.01	142.38	2.55	0.73	0.73
16.01	42.08	48.46	2.97	143.78	2.54	0.73	0.73
16.10	43.69	50.12	2.88	144.51	2.52	0.73	0.73
16.16	45.39	51.93	2.79	144.76	2.50	0.74	0.74
16.21	47.82	54.52	2.64	144.17	2.47	0.75	0.75
16.29	50.73	57.59	2.49	143.67	2.44	0.75	0.75
16.36	53.65	60.67	2.37	143.61	2.41	0.76	0.76
16.41	55.97	63.12	2.29	144.46	2.39	0.76	0.76
16.49	57.93	65.13	2.24	145.59	2.38	0.77	0.77
16.55	58.97	66.18	2.22	147.05	2.38	0.77	0.77
16.60	58.73	65.85	2.26	148.63	2.39	0.77	0.77
16.70	57.58	64.45	2.33	150.28	2.40	0.77	0.77
16.74	55.54	62.18	2.43	150.89	2.43	0.76	0.76
16.80	52.24	58.44	2.54	148.41	2.45	0.75	0.75
16.89	48.21	53.86	2.71	145.75	2.49	0.74	0.74
16.93	43.70	48.84	2.93	142.95	2.53	0.73	0.73
17.00	39.30	43.87	3.17	139.12	2.57	0.72	0.72
17.09	35.13	39.12	3.43	134.22	2.62	2.87	2.87
17.14	31.91	35.46	3.61	128.18	2.65	2.60	2.60
17.20	29.62	32.81	3.70	121.48	2.66	2.40	2.40
17.28	27.32	30.13	3.80	114.37	2.67	2.20	2.20
17.34	25.35	27.85	3.90	108.56	2.69	2.03	2.03
17.41	23.75	26.02	4.11	106.90	2.72	1.89	1.89
17.48	22.28	24.34	4.33	105.33	2.74	1.77	1.77
17.56	21.40	23.31	4.46	103.98	2.76	1.69	1.69
17.62	21.30	23.15	4.46	103.34	2.76	1.68	1.68
17.67	21.90	23.78	4.41	104.80	2.75	1.72	1.72
17.72	23.43	25.45	4.23	107.56	2.73	1.85	1.85
17.78	25.81	28.02	3.95	110.64	2.69	2.04	2.04
17.87	29.76	32.25	3.52	113.53	2.63	2.36	2.36
17.94	34.49	37.30	3.14	117.09	2.57	0.70	0.70
18.01	39.36	42.48	2.84	120.59	2.51	0.71	0.71
18.06	44.61	48.05	2.58	124.00	2.46	0.73	0.73
18.12	49.40	53.08	2.40	127.40	2.42	0.74	0.74
18.21	53.23	57.04	2.29	130.57	2.39	0.75	0.75
18.25	55.37	59.24	2.23	131.91	2.38	0.76	0.76
18.31	55.54	59.32	2.22	131.93	2.38	0.76	0.76
18.40	54.39	57.96	2.26	130.84	2.39	0.75	0.75
18.44	51.05	54.37	2.37	129.13	2.42	0.75	0.75
18.51	46.53	49.50	2.55	126.35	2.46	0.73	0.73
18.58	42.29	44.90	2.75	123.40	2.50	0.72	0.72
18.64	37.54	39.79	3.03	120.70	2.55	0.71	0.71
18.71	33.19	35.09	3.35	117.60	2.60	2.56	2.56
18.80	29.50	31.08	3.69	114.60	2.66	2.26	2.26
18.86	27.07	28.44	3.99	113.53	2.70	2.06	2.06
18.91	26.18	27.47	4.17	114.45	2.72	1.99	1.99

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
18.98	26.23	27.48	4.23	116.18	2.73	1.99	1.99
19.05	28.55	29.89	3.96	118.43	2.70	2.17	2.17
19.10	32.75	34.30	3.56	122.20	2.64	2.50	2.50
19.20	36.95	38.62	3.27	126.30	2.59	0.70	0.70
19.23	41.98	43.88	2.98	130.67	2.54	0.72	0.72
19.30	47.70	49.78	2.72	135.29	2.49	0.73	0.73
19.39	53.84	56.05	2.49	139.78	2.44	0.75	0.75
19.43	60.95	63.36	2.27	144.00	2.39	0.77	0.77
19.50	67.80	70.30	2.10	147.71	2.34	0.78	0.78
19.57	74.91	77.48	1.96	151.93	2.30	0.79	0.79
19.63	80.68	83.29	1.88	156.25	2.28	0.80	0.80
19.70	84.48	87.05	1.84	160.14	2.26	0.81	0.81
19.77	87.46	89.97	1.82	163.96	2.26	0.81	0.81
19.84	88.72	91.06	1.79	162.94	2.25	0.81	0.81
19.90	88.05	90.24	1.81	162.93	2.25	0.81	0.81
19.99	86.33	88.30	1.84	162.87	2.27	0.81	0.81
20.02	82.81	84.69	1.93	163.44	2.29	0.80	0.80
20.09	77.91	79.61	2.06	163.98	2.33	0.80	0.80
20.19	72.20	73.64	2.23	164.40	2.38	0.79	0.79
20.21	66.31	67.65	2.44	164.76	2.43	0.77	0.77
20.29	60.80	61.90	2.66	164.43	2.48	0.76	0.76
20.38	55.60	56.47	2.90	163.92	2.53	0.75	0.75
20.42	51.83	52.62	3.19	167.91	2.58	0.74	0.74
20.52	49.59	50.20	3.37	169.09	2.61	3.64	3.64
20.55	48.85	49.41	3.44	169.77	2.62	3.58	3.58
20.62	50.23	50.69	3.32	168.19	2.60	0.74	0.74
20.68	54.00	54.40	3.05	165.95	2.55	0.75	0.75
20.75	58.46	58.77	2.79	164.25	2.51	0.76	0.76
20.81	64.06	64.27	2.54	163.09	2.45	0.77	0.77
20.90	70.17	70.22	2.31	162.34	2.40	0.78	0.78
20.96	76.88	76.78	2.11	162.12	2.35	0.79	0.79
21.01	83.50	83.25	1.95	162.71	2.30	0.80	0.80
21.09	89.88	89.40	1.83	163.78	2.26	0.81	0.81
21.15	95.34	94.66	1.74	164.75	2.23	0.82	0.82
21.21	99.28	98.41	1.69	165.97	2.21	0.83	0.83
21.30	101.54	100.41	1.66	166.66	2.20	0.83	0.83
21.36	102.98	101.69	1.64	166.99	2.19	0.83	0.83
21.40	103.15	101.76	1.64	167.23	2.19	0.83	0.83
21.49	102.24	100.65	1.67	167.75	2.20	0.83	0.83
21.56	100.58	98.87	1.71	168.66	2.22	0.83	0.83
21.60	98.24	96.51	1.76	170.27	2.24	0.82	0.82
21.66	95.65	93.85	1.84	173.11	2.27	0.82	0.82
21.75	92.97	91.05	1.94	176.31	2.30	0.81	0.81
21.80	90.34	88.38	2.03	179.61	2.33	0.81	0.81
21.85	86.54	84.57	2.15	181.57	2.36	0.80	0.80
21.95	82.45	80.35	2.27	182.77	2.39	0.80	0.80
21.99	77.84	75.75	2.41	182.63	2.42	0.79	0.79
22.05	73.33	71.22	2.53	179.99	2.45	0.78	0.78

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
22.14	68.64	66.45	2.63	175.01	2.47	0.77	0.77
22.19	64.12	61.92	2.73	169.22	2.49	0.76	0.76
22.26	59.36	57.14	2.83	161.62	2.51	0.75	0.75
22.35	54.56	52.30	2.93	153.37	2.53	0.74	0.74
22.44	49.73	47.45	3.05	144.80	2.55	0.73	0.73
22.45	46.31	44.10	3.12	137.69	2.57	0.72	0.72
22.54	43.33	41.08	3.20	131.39	2.58	0.71	0.71
22.58	41.17	38.93	3.26	126.75	2.59	0.70	0.70
22.65	39.90	37.63	3.31	124.71	2.60	0.70	0.70
22.73	39.60	37.26	3.36	125.06	2.60	2.67	2.67
22.79	39.96	37.55	3.36	126.08	2.61	2.69	2.69
22.85	41.77	39.25	3.31	129.80	2.60	0.70	0.70
22.93	44.52	41.82	3.27	136.54	2.59	0.71	0.71
22.99	48.25	45.36	3.19	144.50	2.58	0.72	0.72
23.04	53.17	50.03	3.03	151.83	2.55	0.73	0.73
23.12	57.97	54.54	2.90	158.22	2.53	0.75	0.75
23.19	61.76	58.07	2.81	162.95	2.51	0.75	0.75
23.27	64.98	61.03	2.73	166.65	2.49	0.76	0.76
23.30	67.76	63.65	2.66	169.44	2.48	0.77	0.77
23.38	70.90	66.51	2.58	171.29	2.46	0.77	0.77
23.47	73.27	68.60	2.50	171.31	2.44	0.78	0.78
23.50	74.99	70.18	2.41	168.91	2.42	0.78	0.78
23.58	75.51	70.53	2.34	165.30	2.41	0.78	0.78
23.66	74.38	69.31	2.34	161.96	2.41	0.78	0.78
23.69	73.15	68.09	2.34	159.30	2.41	0.77	0.77
23.77	72.69	67.52	2.34	158.28	2.41	0.77	0.77
23.84	72.77	67.48	2.34	157.74	2.41	0.77	0.77
23.92	72.82	67.39	2.34	157.99	2.41	0.77	0.77
23.97	71.99	66.52	2.38	158.38	2.42	0.77	0.77
24.06	70.72	65.17	2.44	158.89	2.43	0.77	0.77
24.12	69.26	63.69	2.51	159.96	2.45	0.77	0.77
24.17	67.92	62.35	2.58	160.90	2.46	0.76	0.76
24.23	66.21	60.65	2.65	160.73	2.48	0.76	0.76
24.31	64.27	58.71	2.73	160.00	2.49	0.76	0.76
24.36	61.66	56.19	2.82	158.28	2.51	0.75	0.75
24.42	58.14	52.82	2.95	155.55	2.53	0.74	0.74
24.51	54.24	49.05	3.10	152.30	2.56	0.73	0.73
24.54	50.19	45.25	3.27	148.14	2.59	0.72	0.72
24.62	45.92	41.19	3.46	142.60	2.62	2.93	2.93
24.71	41.38	36.87	3.69	136.14	2.66	2.63	2.63
24.74	37.02	32.81	3.94	129.34	2.69	2.34	2.34
24.81	33.35	29.36	4.18	122.62	2.72	2.09	2.09
24.89	30.15	26.35	4.39	115.71	2.75	1.88	1.88
24.96	27.79	24.12	4.52	109.01	2.77	1.72	1.72
25.01	26.12	22.57	4.58	103.36	2.78	1.61	1.61
25.10	24.74	21.25	4.62	98.16	2.78	1.51	1.51
25.14	23.57	20.15	4.68	94.33	2.79	1.44	1.44
25.21	22.70	19.32	4.76	92.00	2.80	1.38	1.38

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
25.30	22.17	18.80	4.80	90.31	2.80	1.34	1.34
25.34	21.82	18.46	4.81	88.71	2.80	1.32	1.32
25.41	21.76	18.37	4.76	87.53	2.80	1.31	1.31
25.50	21.77	18.34	4.72	86.53	2.79	1.31	1.31
25.55	21.93	18.47	4.65	85.93	2.78	1.32	1.32
25.60	22.09	18.59	4.59	85.40	2.78	1.32	1.32
25.70	22.29	18.73	4.52	84.60	2.77	1.33	1.33
25.75	22.50	18.90	4.43	83.67	2.76	1.35	1.35
25.80	22.79	19.15	4.28	82.04	2.74	1.36	1.36
25.89	23.08	19.37	4.15	80.44	2.72	1.38	1.38
25.95	23.34	19.59	4.04	79.07	2.71	1.39	1.39
25.99	23.77	19.96	3.90	77.81	2.69	1.42	1.42
26.06	24.08	20.21	3.80	76.79	2.67	1.44	1.44
26.15	24.25	20.33	3.73	75.89	2.66	1.44	1.44
26.19	24.34	20.39	3.69	75.28	2.66	1.45	1.45
26.25	24.39	20.41	3.69	75.23	2.66	1.45	1.45
26.34	24.31	20.30	3.73	75.77	2.66	1.44	1.44
26.38	24.05	20.04	3.85	77.18	2.68	1.42	1.42
26.45	23.79	19.77	3.97	78.40	2.70	1.40	1.40
26.52	23.52	19.49	4.07	79.37	2.71	1.38	1.38
26.61	23.07	19.04	4.21	80.09	2.73	1.35	1.35
26.67	22.67	18.66	4.30	80.27	2.74	1.32	1.32
26.72	22.32	18.31	4.38	80.21	2.75	1.30	1.30
26.82	21.99	17.98	4.43	79.73	2.76	1.28	1.28
26.86	21.65	17.67	4.46	78.75	2.76	1.25	1.25
26.94	21.41	17.42	4.43	77.07	2.76	1.24	1.24
26.98	21.28	17.29	4.35	75.19	2.75	1.23	1.23
27.06	21.19	17.19	4.27	73.31	2.74	1.22	1.22
27.10	21.17	17.16	4.16	71.47	2.72	1.22	1.22
27.17	21.23	17.20	4.05	69.64	2.71	0.31	1.22
27.26	21.42	17.34	3.94	68.32	2.69	0.30	1.23
27.31	21.67	17.54	3.84	67.44	2.68	0.30	1.24
27.39	21.94	17.76	3.77	67.05	2.67	0.29	1.26
27.44	22.25	18.02	3.71	66.93	2.66	0.29	1.27
27.51	22.57	18.27	3.68	67.24	2.65	0.32	1.29
27.58	22.83	18.47	3.67	67.74	2.65	0.35	1.31
27.63	23.05	18.64	3.66	68.26	2.65	0.36	1.32
27.71	23.11	18.67	3.69	68.80	2.66	0.36	1.32
27.79	23.06	18.58	3.74	69.46	2.66	0.35	1.31
27.86	22.89	18.40	3.80	69.90	2.67	0.35	1.30
27.89	22.61	18.14	3.88	70.31	2.68	1.28	1.28
27.96	22.26	17.80	3.97	70.72	2.70	1.26	1.26
28.05	21.90	17.44	4.10	71.46	2.71	1.23	1.23
28.09	21.54	17.11	4.25	72.69	2.73	1.21	1.21
28.16	21.20	16.78	4.41	74.05	2.75	1.19	1.19
28.23	20.88	16.46	4.58	75.37	2.78	1.17	1.17
28.29	20.64	16.22	4.73	76.64	2.79	1.15	1.15
28.35	20.47	16.04	4.85	77.72	2.81	1.14	1.14

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
28.44	20.36	15.91	4.94	78.67	2.82	1.13	1.13
28.50	20.26	15.79	5.04	79.55	2.83	1.12	1.12
28.55	20.24	15.75	5.10	80.26	2.84	1.12	1.12
28.64	20.28	15.76	5.12	80.62	2.84	1.12	1.12
28.69	20.47	15.90	5.08	80.83	2.83	1.13	1.13
28.75	20.92	16.26	4.96	80.68	2.82	1.15	1.15
28.82	21.52	16.76	4.80	80.40	2.80	1.19	1.19
28.89	22.35	17.44	4.66	81.27	2.79	1.24	1.24
28.98	23.25	18.18	4.55	82.71	2.77	1.29	1.29
29.04	24.09	18.87	4.46	84.22	2.76	1.34	1.34
29.08	24.99	19.62	4.37	85.67	2.75	1.39	1.39
29.15	25.81	20.29	4.30	87.23	2.74	1.44	1.44
29.24	26.55	20.88	4.26	88.89	2.73	1.48	1.48
29.29	27.47	21.64	4.18	90.48	2.72	1.53	1.53
29.34	28.09	22.14	4.16	92.19	2.72	1.56	1.56
29.43	28.47	22.41	4.19	93.91	2.73	1.58	1.58
29.47	28.34	22.27	4.25	94.60	2.73	1.57	1.57
29.53	28.01	21.95	4.32	94.84	2.74	1.55	1.55
29.62	27.58	21.54	4.41	94.97	2.75	1.52	1.52
29.66	26.96	20.98	4.54	95.20	2.77	1.48	1.48
29.77	26.26	20.33	4.68	95.20	2.79	1.44	1.44
29.81	25.53	19.68	4.86	95.62	2.81	1.40	1.40
29.86	25.39	19.54	4.93	96.27	2.82	1.39	1.39
29.92	25.75	19.81	4.90	97.12	2.81	1.40	1.40
30.01	26.64	20.51	4.78	98.08	2.80	1.45	1.45
30.09	27.72	21.39	4.63	99.03	2.78	1.51	1.51
30.17	28.41	21.93	4.56	100.07	2.77	1.55	1.55
30.20	28.59	22.05	4.60	101.40	2.78	1.56	1.56
30.27	28.79	22.17	4.65	103.06	2.78	1.57	1.57
30.32	29.48	22.72	4.61	104.73	2.78	1.61	1.61
30.39	30.45	23.50	4.51	105.88	2.77	1.66	1.66
30.47	30.78	23.72	4.49	106.51	2.76	1.68	1.68
30.55	30.79	23.68	4.51	106.70	2.77	1.67	1.67
30.62	30.35	23.27	4.59	106.77	2.78	1.64	1.64
30.66	29.89	22.86	4.67	106.87	2.79	1.62	1.62
30.72	29.64	22.63	4.67	105.71	2.79	1.60	1.60
30.81	29.90	22.81	4.56	103.99	2.77	1.61	1.61
30.85	30.12	22.99	4.41	101.48	2.75	1.62	1.62
30.91	29.75	22.67	4.34	98.41	2.75	1.60	1.60
31.01	29.16	22.15	4.28	94.88	2.74	1.56	1.56
31.05	28.11	21.28	4.30	91.42	2.74	1.50	1.50
31.11	26.82	20.20	4.35	87.95	2.75	1.42	1.42
31.20	25.44	19.03	4.43	84.32	2.76	1.34	1.34
31.26	24.18	17.98	4.48	80.64	2.76	1.27	1.27
31.31	23.24	17.20	4.56	78.37	2.77	1.21	1.21
31.38	22.45	16.53	4.63	76.56	2.78	1.17	1.17
31.46	21.95	16.09	4.66	75.05	2.79	1.14	1.14
31.51	21.63	15.82	4.68	74.00	2.79	1.12	1.12

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
31.60	21.33	15.54	4.71	73.14	2.79	1.10	1.10
31.65	21.21	15.44	4.68	72.24	2.79	1.09	1.09
31.74	21.14	15.36	4.64	71.22	2.78	1.08	1.08
31.80	21.15	15.35	4.57	70.19	2.77	1.08	1.08
31.85	21.16	15.35	4.49	68.91	2.76	0.34	1.08
31.89	21.17	15.37	4.36	67.05	2.75	0.31	1.08
32.00	21.16	15.34	4.24	65.11	2.73	0.27	1.08
32.04	21.11	15.30	4.14	63.32	2.72	0.27	1.08
32.09	21.14	15.33	4.04	61.91	2.71	0.24	1.08
32.19	21.23	15.39	3.96	60.88	2.69	0.20	1.08
32.23	21.15	15.31	3.94	60.35	2.69	0.21	1.07
32.29	21.63	15.69	3.86	60.57	2.68	0.22	1.10
32.37	22.15	16.09	3.79	60.95	2.67	0.23	1.13
32.44	22.73	16.54	3.73	61.75	2.66	0.25	1.16
32.49	23.42	17.08	3.71	63.28	2.66	0.26	1.19
32.58	24.18	17.66	3.67	64.80	2.65	0.30	1.23
32.62	24.92	18.23	3.64	66.38	2.65	0.31	1.27
32.69	25.54	18.71	3.63	67.92	2.65	0.33	1.31
32.78	26.07	19.09	3.64	69.43	2.65	0.36	1.33
32.82	26.80	19.66	3.61	70.95	2.64	1.37	1.37
32.89	27.02	19.79	3.66	72.39	2.65	1.38	1.38
32.97	27.26	19.94	3.70	73.87	2.66	1.39	1.39
33.02	27.46	20.06	3.76	75.41	2.67	1.40	1.40
33.09	27.56	20.09	3.84	77.21	2.68	1.40	1.40
33.15	27.58	20.06	3.94	79.12	2.69	1.40	1.40
33.20	27.62	20.05	4.05	81.12	2.71	1.40	1.40
33.28	27.94	20.26	4.11	83.29	2.72	1.42	1.42
33.38	28.41	20.57	4.15	85.36	2.72	1.44	1.44
33.43	29.00	21.01	4.16	87.41	2.72	1.47	1.47
33.47	29.66	21.50	4.16	89.41	2.72	1.51	1.51
33.57	30.25	21.91	4.18	91.56	2.72	1.54	1.54
33.63	30.80	22.30	4.20	93.64	2.73	1.56	1.56
33.70	31.35	22.69	4.20	95.39	2.73	1.59	1.59
33.74	31.93	23.12	4.20	97.06	2.73	1.62	1.62
33.82	32.49	23.51	4.19	98.51	2.73	1.65	1.65
33.86	32.78	23.71	4.21	99.73	2.73	1.66	1.66
33.93	32.90	23.76	4.25	100.95	2.73	1.67	1.67
34.02	32.86	23.67	4.31	102.03	2.74	1.66	1.66
34.06	32.78	23.57	4.37	102.94	2.75	1.65	1.65
34.13	32.65	23.42	4.42	103.48	2.76	1.64	1.64
34.21	32.51	23.26	4.46	103.80	2.76	1.63	1.63
34.28	32.29	23.05	4.51	103.90	2.77	1.62	1.62
34.32	31.94	22.75	4.56	103.65	2.77	1.60	1.60
34.41	31.53	22.38	4.61	103.23	2.78	1.57	1.57
34.46	31.08	22.00	4.67	102.68	2.79	1.55	1.55
34.52	30.55	21.56	4.72	101.80	2.79	1.52	1.52
34.61	29.93	21.04	4.78	100.63	2.80	1.48	1.48
34.65	29.34	20.56	4.83	99.34	2.81	1.45	1.45

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
34.71	28.73	20.07	4.87	97.80	2.81	1.41	1.41
34.79	28.12	19.57	4.90	95.91	2.81	1.38	1.38
34.86	27.56	19.11	4.91	93.87	2.81	1.35	1.35
34.93	27.06	18.72	4.90	91.78	2.81	1.32	1.32
35.01	26.62	18.35	4.89	89.74	2.81	1.29	1.29
35.06	26.18	18.01	4.88	87.84	2.81	1.27	1.27
35.11	25.82	17.73	4.87	86.31	2.81	1.25	1.25
35.18	25.57	17.51	4.85	85.02	2.81	1.23	1.23
35.26	25.31	17.29	4.86	84.06	2.81	1.22	1.22
35.34	25.02	17.04	4.90	83.47	2.81	1.20	1.20
35.40	24.80	16.85	4.94	83.29	2.82	1.19	1.19
35.44	24.58	16.65	5.01	83.43	2.83	1.17	1.17
35.51	24.35	16.44	5.10	83.91	2.84	1.16	1.16
35.58	24.06	16.19	5.21	84.27	2.85	1.14	1.14
35.66	23.76	15.93	5.29	84.26	2.86	1.13	1.13
35.71	23.50	15.70	5.34	83.91	2.86	1.11	1.11
35.77	23.24	15.49	5.37	83.26	2.87	1.10	1.10
35.85	22.95	15.25	5.40	82.35	2.87	1.08	1.08
35.92	22.74	15.07	5.40	81.42	2.87	1.07	1.07
35.97	22.64	14.99	5.39	80.74	2.87	1.06	1.06
36.03	22.63	14.97	5.35	80.03	2.86	1.06	1.06
36.11	22.66	14.98	5.28	79.05	2.86	1.06	1.06
36.16	22.78	15.07	5.17	77.87	2.84	1.06	1.06
36.26	22.82	15.08	5.08	76.66	2.83	1.06	1.06
36.31	22.88	15.12	5.00	75.65	2.83	1.07	1.07
36.36	22.63	14.93	4.98	74.35	2.82	1.05	1.05
36.43	22.40	14.74	4.96	73.14	2.82	1.04	1.04
36.51	22.21	14.58	4.93	71.91	2.82	1.03	1.03
36.55	22.01	14.43	4.92	71.02	2.82	1.02	1.02
36.65	21.75	14.21	4.95	70.32	2.82	1.00	1.00
36.71	21.76	14.20	4.95	70.29	2.82	1.00	1.00
36.76	22.11	14.45	4.88	70.57	2.81	1.02	1.02
36.85	22.79	14.94	4.79	71.52	2.80	1.05	1.05
36.89	23.63	15.55	4.68	72.78	2.79	1.09	1.09
36.96	24.91	16.49	4.55	74.96	2.77	1.15	1.15
37.02	26.31	17.51	4.42	77.41	2.76	1.22	1.22
37.11	27.68	18.50	4.32	79.93	2.74	1.29	1.29
37.15	28.95	19.42	4.25	82.45	2.73	1.35	1.35
37.24	30.33	20.41	4.18	85.40	2.73	1.42	1.42
37.31	31.54	21.27	4.15	88.27	2.72	1.48	1.48
37.35	32.61	22.02	4.16	91.57	2.72	1.53	1.53
37.43	34.54	23.43	4.04	94.72	2.71	1.63	1.63
37.51	37.23	25.41	3.83	97.40	2.68	1.76	1.76
37.55	40.42	27.84	3.55	98.85	2.64	1.92	1.92
37.60	43.41	30.14	3.26	98.34	2.59	0.67	0.67
37.67	46.12	32.25	3.01	97.10	2.55	0.68	0.68
37.75	47.68	33.45	2.86	95.62	2.52	0.68	0.68
37.81	48.21	33.86	2.79	94.32	2.50	0.69	0.69

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
37.88	48.12	33.76	2.77	93.42	2.50	0.69	0.69
37.93	48.13	33.75	2.76	93.00	2.50	0.68	0.68
38.00	49.14	34.47	2.72	93.80	2.49	0.69	0.69
38.08	52.10	36.67	2.64	96.77	2.47	0.70	0.70
38.14	55.93	39.49	2.60	102.67	2.47	0.70	0.70
38.20	60.41	42.75	2.58	110.38	2.46	0.71	0.71
38.26	65.84	46.71	2.57	119.90	2.46	0.73	0.73
38.34	74.63	53.26	2.44	130.07	2.43	0.74	0.74
38.43	85.00	61.06	2.29	139.63	2.39	0.76	0.76
38.45	97.14	70.35	2.13	149.58	2.35	0.78	0.78
38.53	109.74	79.94	1.99	159.28	2.31	0.80	0.80
38.62	121.23	88.66	1.90	168.28	2.28	0.81	0.81
38.65	130.51	95.75	1.84	176.10	2.26	0.82	0.82
38.72	139.21	102.35	1.79	182.90	2.25	0.83	0.83
38.80	148.05	109.03	1.74	189.51	2.23	0.84	0.84
38.88	156.31	115.30	1.69	195.08	2.21	0.85	0.85
38.93	162.35	119.87	1.67	199.70	2.20	0.85	0.85
39.01	167.70	123.81	1.65	204.11	2.19	0.86	0.86
39.07	171.82	126.83	1.64	207.67	2.19	0.86	0.86
39.12	176.04	129.96	1.62	211.17	2.18	0.86	0.86
39.20	180.10	132.88	1.62	214.63	2.18	0.87	0.87
39.27	184.00	135.69	1.61	217.99	2.17	0.87	0.87
39.31	187.49	138.26	1.60	221.07	2.17	0.87	0.87
39.38	190.29	140.19	1.60	223.77	2.17	0.88	0.88
39.45	193.31	142.31	1.59	226.42	2.17	0.88	0.88
39.51	197.03	145.04	1.58	229.13	2.16	0.88	0.88
39.57	201.45	148.33	1.56	231.77	2.15	0.88	0.88
39.64	206.43	152.05	1.54	234.36	2.14	0.89	0.89
39.72	209.97	154.62	1.53	235.92	2.14	0.89	0.89
39.79	210.90	155.19	1.52	235.81	2.13	0.89	0.89
39.84	209.11	153.65	1.53	234.48	2.14	0.89	0.89
39.90	206.02	151.08	1.54	232.41	2.14	0.89	0.89
39.96	202.96	148.57	1.55	229.77	2.15	0.88	0.88
40.06	199.55	145.71	1.56	226.70	2.15	0.88	0.88
40.13	195.43	142.38	1.57	223.26	2.16	0.88	0.88
40.17	191.56	139.34	1.58	219.92	2.16	0.87	0.87
40.26	187.07	135.71	1.59	216.05	2.17	0.87	0.87
40.31	182.02	131.75	1.61	211.86	2.18	0.87	0.87
40.36	176.42	127.42	1.62	206.86	2.18	0.86	0.86
40.43	171.16	123.34	1.63	201.52	2.19	0.86	0.86
40.51	164.14	117.86	1.66	195.74	2.20	0.85	0.85
40.56	159.97	114.70	1.66	190.93	2.20	0.85	0.85
40.64	152.18	108.61	1.71	185.56	2.22	0.84	0.84
40.70	148.35	105.73	1.71	180.74	2.22	0.84	0.84
40.75	146.10	104.13	1.69	175.76	2.21	0.83	0.83
40.83	144.83	103.24	1.66	171.24	2.20	0.83	0.83
40.88	146.29	104.60	1.60	167.25	2.17	0.83	0.83
40.95	151.45	108.92	1.50	163.89	2.13	0.84	0.84

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
41.03	159.00	115.12	1.41	162.69	2.08	0.85	0.85
41.08	169.86	124.05	1.32	164.27	2.02	0.86	0.86
41.15	178.00	130.77	1.27	165.80	1.97	0.87	0.87
41.24	189.19	140.00	1.21	169.37	1.92	0.88	0.88
41.28	194.60	144.65	1.18	170.54	1.89	0.88	0.88
41.35	196.88	146.68	1.16	170.24	1.87	0.88	0.88
41.41	197.86	147.66	1.15	169.29	1.85	0.88	0.88
41.48	196.40	146.49	1.14	167.63	1.85	0.88	0.88
41.55	192.75	143.17	1.16	166.29	1.87	0.88	0.88
41.63	188.20	139.10	1.18	164.51	1.89	0.87	0.87
41.68	181.44	133.30	1.21	161.92	1.93	0.87	0.87
41.74	174.04	127.00	1.25	159.25	1.96	0.86	0.86
41.83	166.17	120.27	1.30	156.93	2.00	0.85	0.85
41.87	159.62	114.71	1.36	156.04	2.04	0.85	0.85
41.98	152.99	108.97	1.43	155.95	2.09	0.84	0.84
42.02	146.03	103.14	1.52	156.49	2.13	0.83	0.83
42.10	139.05	97.32	1.62	157.32	2.18	0.82	0.82
42.14	132.52	92.01	1.72	158.36	2.22	0.82	0.82
42.22	126.16	86.83	1.84	159.59	2.26	0.81	0.81
42.29	120.67	82.42	1.95	160.51	2.30	0.80	0.80
42.38	115.55	78.32	2.06	161.46	2.33	0.79	0.79
42.41	111.25	74.95	2.17	162.34	2.36	0.79	0.79
42.46	107.34	71.90	2.27	163.00	2.39	0.78	0.78
42.57	103.94	69.19	2.36	163.11	2.41	0.78	0.78
42.61	100.91	66.88	2.44	163.01	2.43	0.77	0.77
42.68	98.50	65.01	2.50	162.77	2.44	0.77	0.77
42.76	96.24	63.25	2.57	162.34	2.46	0.76	0.76
42.80	94.09	61.63	2.63	161.80	2.47	0.76	0.76
42.87	92.43	60.35	2.67	161.02	2.48	0.76	0.76
42.92	90.98	59.26	2.70	160.04	2.49	0.76	0.76
42.98	89.10	57.87	2.74	158.36	2.49	0.75	0.75
43.06	86.12	55.71	2.79	155.17	2.50	0.75	0.75
43.11	82.66	53.25	2.85	151.63	2.52	0.74	0.74
43.18	78.34	50.16	2.95	147.91	2.53	0.73	0.73
43.26	73.08	46.41	3.10	143.94	2.56	0.72	0.72
43.32	67.13	42.20	3.31	139.61	2.60	0.71	0.71
43.39	61.24	38.07	3.54	134.85	2.63	2.58	2.58
43.46	55.24	33.90	3.81	129.27	2.67	2.31	2.31
43.52	48.95	29.60	4.15	122.72	2.72	2.04	2.04
43.61	43.21	25.69	4.52	116.06	2.77	1.78	1.78
43.64	38.48	22.50	4.92	110.79	2.82	1.57	1.57
43.70	34.37	19.75	5.34	105.47	2.86	1.39	1.39
43.79	31.53	17.87	5.61	100.21	2.89	1.26	1.26
43.84	29.85	16.79	5.68	95.39	2.90	1.19	1.19
43.90	29.16	16.37	5.61	91.83	2.89	1.16	1.16
43.97	28.62	16.03	5.57	89.31	2.89	1.13	1.13
44.05	28.46	15.91	5.55	88.25	2.88	1.12	1.12
44.10	28.90	16.18	5.48	88.67	2.88	1.14	1.14

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
44.18	29.73	16.69	5.41	90.36	2.87	1.18	1.18
44.24	30.91	17.43	5.32	92.72	2.86	1.23	1.23
44.30	32.38	18.35	5.22	95.76	2.85	1.29	1.29
44.38	34.27	19.53	5.09	99.36	2.83	1.37	1.37
44.45	36.52	20.96	4.92	103.06	2.82	1.46	1.46
44.49	39.14	22.67	4.68	106.18	2.79	1.57	1.57
44.57	41.80	24.41	4.46	108.75	2.76	1.69	1.69
44.64	44.11	25.89	4.31	111.67	2.74	1.78	1.78
44.72	45.81	26.96	4.24	114.40	2.73	1.85	1.85
44.79	47.04	27.72	4.21	116.56	2.73	1.91	1.91
44.84	48.33	28.53	4.15	118.40	2.72	1.96	1.96
44.92	51.62	30.75	3.87	118.97	2.68	2.10	2.10
44.96	56.00	33.79	3.51	118.61	2.63	2.28	2.28
45.03	61.93	37.94	3.09	117.38	2.56	0.70	0.70
45.09	70.39	43.99	2.63	115.79	2.47	0.72	0.72
45.19	78.97	50.19	2.29	114.70	2.39	0.73	0.73
45.23	87.67	56.61	2.01	113.97	2.32	0.75	0.75
45.28	95.84	62.61	1.84	115.12	2.26	0.76	0.76
45.38	103.70	68.35	1.71	117.08	2.22	0.78	0.78
45.43	110.94	73.64	1.63	119.99	2.18	0.79	0.79
45.48	114.55	76.05	1.63	123.69	2.18	0.79	0.79
45.58	115.95	76.70	1.66	127.38	2.20	0.79	0.79
45.62	113.89	74.81	1.75	130.77	2.23	0.79	0.79
45.67	107.49	69.71	1.92	133.73	2.29	0.78	0.78
45.78	100.41	64.15	2.13	136.92	2.35	0.77	0.77
45.82	92.83	58.44	2.39	139.92	2.42	0.75	0.75
45.88	86.04	53.46	2.63	140.77	2.47	0.74	0.74
45.98	79.71	48.88	2.88	140.84	2.52	0.73	0.73
46.02	73.83	44.74	3.13	140.23	2.57	0.72	0.72
46.07	69.62	41.84	3.29	137.86	2.59	0.71	0.71
46.17	66.01	39.37	3.42	134.82	2.62	2.65	2.65
46.21	63.43	37.66	3.49	131.48	2.63	2.53	2.53
46.27	61.17	36.16	3.55	128.41	2.64	2.44	2.44
46.37	59.04	34.72	3.62	125.52	2.65	2.34	2.34
46.39	57.19	33.50	3.68	123.35	2.66	2.27	2.27
46.47	55.24	32.14	3.82	122.66	2.67	2.18	2.18
46.57	53.36	30.82	3.97	122.21	2.70	2.10	2.10
46.62	51.65	29.64	4.10	121.62	2.71	2.03	2.03
46.67	49.67	28.29	4.29	121.27	2.74	1.94	1.94
46.77	47.76	26.96	4.48	120.87	2.76	1.86	1.86
46.82	46.32	25.98	4.64	120.67	2.78	1.80	1.80
46.90	45.86	25.64	4.69	120.21	2.79	1.78	1.78
46.92	45.62	25.48	4.70	119.75	2.79	1.77	1.77
47.01	45.61	25.43	4.70	119.60	2.79	1.76	1.76
47.05	45.76	25.51	4.69	119.58	2.79	1.77	1.77
47.12	45.95	25.59	4.69	119.93	2.79	1.77	1.77
47.21	45.72	25.38	4.75	120.48	2.80	1.76	1.76
47.28	46.33	25.74	4.70	120.95	2.79	1.78	1.78

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
47.32	46.71	25.95	4.68	121.44	2.79	1.80	1.80
47.40	47.02	26.10	4.68	122.19	2.79	1.81	1.81
47.45	47.62	26.44	4.66	123.33	2.79	1.83	1.83
47.55	48.61	27.01	4.60	124.26	2.78	1.87	1.87
47.58	49.96	27.88	4.47	124.59	2.76	1.92	1.92
47.66	51.87	29.11	4.28	124.45	2.74	1.99	1.99
47.74	54.02	30.50	4.07	124.17	2.71	2.08	2.08
47.80	56.71	32.27	3.84	124.05	2.68	2.19	2.19
47.85	58.65	33.53	3.70	124.22	2.66	2.26	2.26
47.93	60.64	34.81	3.58	124.49	2.64	2.34	2.34
47.98	62.76	36.21	3.44	124.46	2.62	2.42	2.42
48.04	64.99	37.69	3.29	124.03	2.59	0.70	0.70
48.11	67.41	39.30	3.14	123.57	2.57	0.70	0.70
48.20	69.59	40.73	3.03	123.38	2.55	0.71	0.71
48.24	71.33	41.88	2.95	123.68	2.54	0.71	0.71
48.30	72.97	42.95	2.89	123.93	2.52	0.71	0.71
48.39	74.42	43.87	2.83	124.05	2.51	0.72	0.72
48.44	75.99	44.91	2.77	124.44	2.50	0.72	0.72
48.53	77.80	46.06	2.71	124.94	2.49	0.72	0.72
48.59	79.60	47.23	2.66	125.51	2.48	0.73	0.73
48.64	80.98	48.11	2.63	126.34	2.47	0.73	0.73
48.70	82.04	48.73	2.62	127.52	2.47	0.73	0.73
48.78	83.53	49.64	2.59	128.78	2.46	0.73	0.73
48.82	85.19	50.69	2.56	129.97	2.46	0.74	0.74
48.89	87.28	52.03	2.52	131.08	2.45	0.74	0.74
48.98	90.26	53.97	2.45	132.03	2.43	0.74	0.74
49.05	93.73	56.28	2.36	132.78	2.41	0.75	0.75
49.09	97.44	58.81	2.27	133.45	2.39	0.76	0.76
49.16	101.81	61.78	2.17	134.12	2.36	0.76	0.76
49.24	106.91	65.26	2.07	135.13	2.34	0.77	0.77
49.31	112.14	68.86	1.98	136.11	2.31	0.78	0.78
49.38	116.76	72.05	1.90	137.00	2.29	0.78	0.78
49.43	120.62	74.75	1.84	137.59	2.26	0.79	0.79
49.52	123.30	76.64	1.79	137.04	2.25	0.79	0.79
49.58	124.61	77.65	1.75	135.66	2.23	0.79	0.79
49.63	124.38	77.57	1.73	133.96	2.22	0.79	0.79
49.71	122.70	76.38	1.73	132.38	2.23	0.79	0.79
49.77	119.64	74.19	1.76	130.76	2.24	0.79	0.79
49.82	114.85	70.80	1.82	128.74	2.26	0.78	0.78
49.88	107.69	65.75	1.92	126.27	2.29	0.77	0.77
49.97	100.43	60.65	2.04	123.80	2.33	0.76	0.76
50.01	94.19	56.34	2.16	121.67	2.36	0.75	0.75
50.07	89.11	52.76	2.30	121.25	2.40	0.74	0.74
50.17	84.50	49.44	2.47	122.07	2.44	0.73	0.73
50.22	80.39	46.53	2.65	123.24	2.48	0.73	0.73
50.29	76.13	43.58	2.83	123.52	2.51	0.72	0.72
50.37	72.92	41.37	2.97	123.02	2.54	0.71	0.71
50.42	69.90	39.36	3.10	122.05	2.56	0.70	0.70

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
50.47	68.34	38.34	3.15	120.84	2.57	0.70	0.70
50.57	65.94	36.74	3.25	119.31	2.59	0.70	0.70
50.63	62.51	34.52	3.40	117.49	2.61	2.29	2.29
50.68	58.31	31.85	3.60	114.64	2.64	2.13	2.13
50.73	53.55	28.88	3.82	110.42	2.68	1.94	1.94
50.79	48.91	26.02	4.06	105.58	2.71	1.76	1.76
50.88	45.25	23.79	4.23	100.57	2.73	1.62	1.62
50.93	41.03	21.25	4.48	95.16	2.76	1.46	1.46
51.03	37.66	19.24	4.65	89.48	2.78	1.33	1.33
51.07	34.69	17.53	4.77	83.65	2.80	1.21	1.21
51.14	32.58	16.34	4.76	77.75	2.80	1.13	1.13
51.23	30.90	15.42	4.68	72.12	2.79	1.06	1.06
51.27	29.21	14.49	4.63	67.10	2.78	0.27	1.00
51.33	28.11	13.89	4.58	63.59	2.78	0.24	0.95
51.42	27.14	13.35	4.53	60.46	2.77	0.19	0.92
51.48	26.51	13.02	4.44	57.82	2.76	0.17	0.89
51.52	26.33	12.93	4.40	56.91	2.75	0.15	0.88
51.60	26.44	12.98	4.37	56.75	2.75	0.15	0.89
51.68	26.86	13.22	4.32	57.16	2.74	0.18	0.90
51.72	27.53	13.60	4.28	58.21	2.74	0.19	0.93
51.81	28.12	13.90	4.30	59.73	2.74	0.23	0.95
51.87	28.73	14.22	4.32	61.44	2.74	0.26	0.97
51.91	28.93	14.29	4.40	62.90	2.75	0.27	0.98
51.98	28.88	14.21	4.50	63.93	2.77	0.28	0.97
52.07	28.66	14.03	4.61	64.66	2.78	0.30	0.96
52.10	28.09	13.67	4.72	64.51	2.79	0.31	0.94
52.17	27.20	13.12	4.86	63.79	2.81	0.29	0.91
52.24	26.15	12.48	5.03	62.82	2.83	0.27	0.87
52.31	24.96	11.76	5.24	61.59	2.85	0.26	0.82
52.37	23.83	11.10	5.40	59.89	2.87	0.22	0.78
52.46	22.77	10.48	5.52	57.92	2.88	0.19	0.74
52.51	21.99	10.05	5.59	56.16	2.89	0.18	0.71
52.57	21.52	9.79	5.56	54.48	2.89	0.16	0.69
52.66	21.13	9.58	5.52	52.88	2.88	0.15	0.67
52.71	20.91	9.46	5.47	51.80	2.88	0.14	0.66
52.78	20.78	9.39	5.44	51.06	2.87	0.14	0.66
52.86	20.69	9.34	5.40	50.46	2.87	0.14	0.66
52.91	20.62	9.30	5.38	50.07	2.87	0.14	0.65
52.99	20.60	9.29	5.37	49.83	2.87	0.14	0.65
53.06	20.61	9.29	5.35	49.67	2.86	0.14	0.65
53.09	20.61	9.29	5.32	49.44	2.86	0.14	0.65
53.16	20.64	9.30	5.31	49.35	2.86	0.14	0.65
53.25	20.67	9.30	5.29	49.26	2.86	0.13	0.65
53.29	20.68	9.31	5.28	49.17	2.86	0.13	0.65
53.36	20.66	9.29	5.28	49.08	2.86	0.13	0.65
53.45	20.68	9.29	5.27	48.99	2.86	0.13	0.65
53.50	20.68	9.28	5.27	48.90	2.85	0.13	0.65
53.55	20.67	9.27	5.28	48.97	2.86	0.13	0.65

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
53.64	20.67	9.25	5.30	49.03	2.86	0.13	0.65
53.69	20.70	9.26	5.30	49.09	2.86	0.13	0.65
53.76	20.73	9.27	5.30	49.08	2.86	0.13	0.65
53.84	20.80	9.29	5.30	49.22	2.86	0.13	0.65
53.88	20.91	9.35	5.30	49.59	2.86	0.13	0.65
53.96	21.17	9.48	5.28	50.03	2.86	0.13	0.66
54.03	21.41	9.60	5.26	50.46	2.85	0.13	0.67
54.08	21.59	9.69	5.24	50.82	2.85	0.14	0.68
54.17	21.74	9.76	5.23	51.09	2.85	0.15	0.68
54.23	21.88	9.83	5.23	51.37	2.85	0.16	0.69
54.27	21.99	9.88	5.23	51.65	2.85	0.16	0.69
54.38	22.08	9.91	5.22	51.77	2.85	0.15	0.69
54.42	22.14	9.94	5.20	51.69	2.85	0.15	0.69
54.47	22.17	9.97	5.14	51.26	2.84	0.15	0.69
54.53	22.12	9.94	5.10	50.74	2.84	0.15	0.69
54.61	22.06	9.91	5.07	50.22	2.83	0.14	0.69
54.68	22.03	9.90	5.04	49.84	2.83	0.13	0.69
54.73	22.02	9.89	5.01	49.53	2.83	0.12	0.69
54.80	22.01	9.87	5.00	49.37	2.82	0.12	0.68
54.88	22.03	9.87	5.00	49.35	2.82	0.12	0.68
54.95	22.09	9.89	5.01	49.56	2.83	0.13	0.69
55.02	22.17	9.92	5.03	49.92	2.83	0.13	0.69
55.07	22.23	9.93	5.08	50.42	2.83	0.14	0.69
55.15	22.25	9.91	5.14	50.97	2.84	0.15	0.69
55.21	22.27	9.90	5.20	51.52	2.85	0.15	0.69
55.27	22.39	9.96	5.21	51.86	2.85	0.16	0.69
55.34	22.62	10.08	5.17	52.13	2.84	0.16	0.70
55.42	22.88	10.21	5.12	52.33	2.84	0.16	0.71
55.47	23.13	10.34	5.08	52.59	2.83	0.16	0.72
55.54	23.41	10.48	5.09	53.39	2.84	0.15	0.73
55.62	23.74	10.64	5.10	54.24	2.84	0.15	0.74
55.65	24.32	10.95	5.05	55.28	2.83	0.16	0.76
55.72	25.17	11.41	4.94	56.41	2.82	0.17	0.79
55.81	26.14	11.94	4.85	57.86	2.81	0.21	0.82
55.84	27.15	12.48	4.80	59.87	2.80	0.22	0.86
55.91	28.26	13.02	4.86	63.28	2.81	0.24	0.90
55.98	29.52	13.64	4.92	67.15	2.82	0.25	0.94
56.05	31.10	14.46	4.90	70.92	2.81	1.00	1.00
56.11	34.04	16.12	4.59	73.94	2.78	1.10	1.10
56.21	38.52	18.71	4.13	77.33	2.72	1.26	1.26
56.26	43.85	21.85	3.70	80.74	2.66	1.45	1.45
56.31	51.25	26.31	3.21	84.44	2.58	0.65	0.65
56.39	58.39	30.64	2.88	88.08	2.52	0.67	0.67
56.46	66.60	35.71	2.57	91.68	2.46	0.69	0.69
56.50	74.21	40.49	2.34	94.69	2.41	0.71	0.71
56.60	80.84	44.64	2.19	97.58	2.37	0.72	0.72
56.65	86.36	48.10	2.09	100.49	2.34	0.73	0.73
56.72	89.96	50.26	2.06	103.30	2.33	0.73	0.73

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
56.78	91.09	50.86	2.06	104.84	2.33	0.74	0.74
56.87	90.61	50.39	2.10	105.65	2.34	0.74	0.74
56.93	86.85	47.84	2.21	105.54	2.37	0.73	0.73
56.97	82.39	44.91	2.33	104.79	2.41	0.72	0.72
57.05	76.32	40.97	2.52	103.41	2.45	0.71	0.71
57.11	69.97	36.95	2.75	101.47	2.50	0.70	0.70
57.17	63.87	33.16	2.98	98.86	2.54	0.68	0.68
57.25	58.18	29.71	3.22	95.61	2.58	0.67	0.67
57.31	52.54	26.32	3.49	91.87	2.63	1.74	1.74
57.37	47.66	23.46	3.76	88.15	2.67	1.56	1.56
57.42	43.35	20.97	4.01	84.11	2.70	1.41	1.41
57.48	39.91	19.02	4.20	79.93	2.73	1.29	1.29
57.56	37.11	17.46	4.35	75.95	2.75	1.19	1.19
57.64	34.62	16.08	4.48	72.08	2.76	1.10	1.10
57.70	32.80	15.10	4.54	68.55	2.77	0.27	1.03
57.74	31.50	14.44	4.51	65.16	2.77	0.25	0.99
57.81	30.51	13.94	4.46	62.19	2.76	0.23	0.95
57.90	29.96	13.68	4.37	59.72	2.75	0.20	0.93
57.95	29.50	13.45	4.31	58.04	2.74	0.20	0.91
58.06	29.02	13.15	4.40	57.86	2.75	0.17	0.89
58.09	28.66	12.92	4.51	58.28	2.77	0.17	0.88
58.15	28.80	12.96	4.55	59.02	2.77	0.18	0.89
58.20	29.53	13.36	4.46	59.61	2.76	0.19	0.91
58.29	30.50	13.91	4.31	59.94	2.74	0.25	0.94
58.33	31.57	14.52	4.16	60.44	2.72	0.28	0.98
58.40	32.28	14.90	4.11	61.27	2.72	0.29	1.00
58.48	32.70	15.11	4.10	62.00	2.71	0.25	1.02
58.55	33.02	15.26	4.10	62.56	2.71	0.23	1.03
58.60	32.96	15.23	4.08	62.16	2.71	0.22	1.02
58.66	33.04	15.31	3.99	61.04	2.70	0.25	1.03
58.75	32.78	15.19	3.93	59.62	2.69	0.24	1.02
58.80	31.98	14.73	3.98	58.57	2.70	0.24	0.99
58.88	30.93	14.12	4.09	57.74	2.71	0.22	0.95
58.97	29.66	13.38	4.25	56.89	2.73	0.18	0.90
59.02	28.78	12.89	4.32	55.64	2.74	0.17	0.87
59.06	28.25	12.61	4.32	54.47	2.74	0.16	0.85
59.12	27.98	12.49	4.26	53.25	2.74	0.15	0.84
59.20	28.12	12.60	4.15	52.31	2.72	0.14	0.85
59.26	28.04	12.55	4.14	51.90	2.72	0.14	0.84
59.35	28.00	12.51	4.14	51.82	2.72	0.15	0.84
59.41	28.02	12.50	4.17	52.14	2.72	0.14	0.84
59.46	28.08	12.51	4.21	52.66	2.73	0.15	0.84
59.52	28.38	12.65	4.22	53.41	2.73	0.15	0.85
59.61	28.81	12.85	4.22	54.27	2.73	0.16	0.87
59.68	29.23	13.06	4.21	54.99	2.73	0.18	0.88
59.72	29.44	13.14	4.24	55.77	2.73	0.19	0.89
59.79	29.54	13.16	4.29	56.42	2.74	0.20	0.89
59.86	29.55	13.13	4.34	56.94	2.75	0.21	0.89

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
59.91	29.54	13.20	4.16	54.87	2.72	0.21	0.89
60.01	29.54	13.28	3.95	52.42	2.69	0.21	0.89
60.06	29.43	13.32	3.73	49.70	2.66	0.20	0.88
60.15	29.33	13.39	3.48	46.66	2.63	0.20	0.88
60.19	29.08	13.40	3.22	43.20	2.58	0.05	0.58
60.26	29.01	13.54	2.91	39.48	2.53	0.04	0.58
60.35	28.68	13.58	2.60	35.31	2.47	0.04	0.58
60.40	28.68	13.89	2.22	30.80	2.38	0.04	0.58
60.45	28.56	-1.00	1.00	-1.00	-1.00	N/A	N/A
60.51	29.38	-1.00	1.00	-1.00	-1.00	N/A	N/A

Abbreviations

q_t: Total cone resistance
K_c: Cone resistance correction factor due to fines
$Q_{tn,cs}$: Adjusted and corrected cone resistance due to fines
I_c: Soil behavior type index
$S_{u(liq)}/\sigma'_v$: Calculated liquefied undrained strength ratio
$S_{u(peak)}/\sigma'_v$: Calculated peak undrained strength ratio

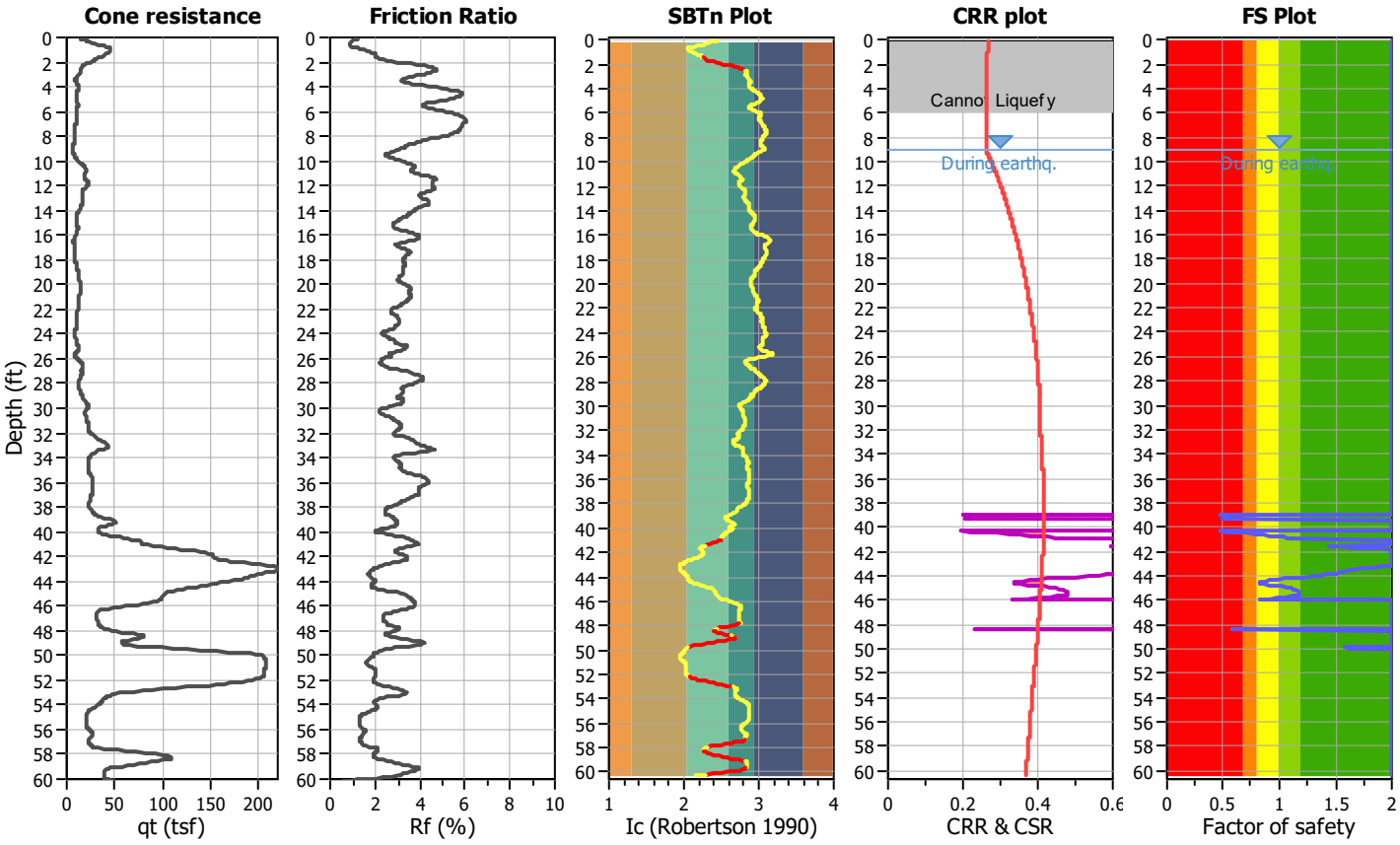
LIQUEFACTION ANALYSIS REPORT

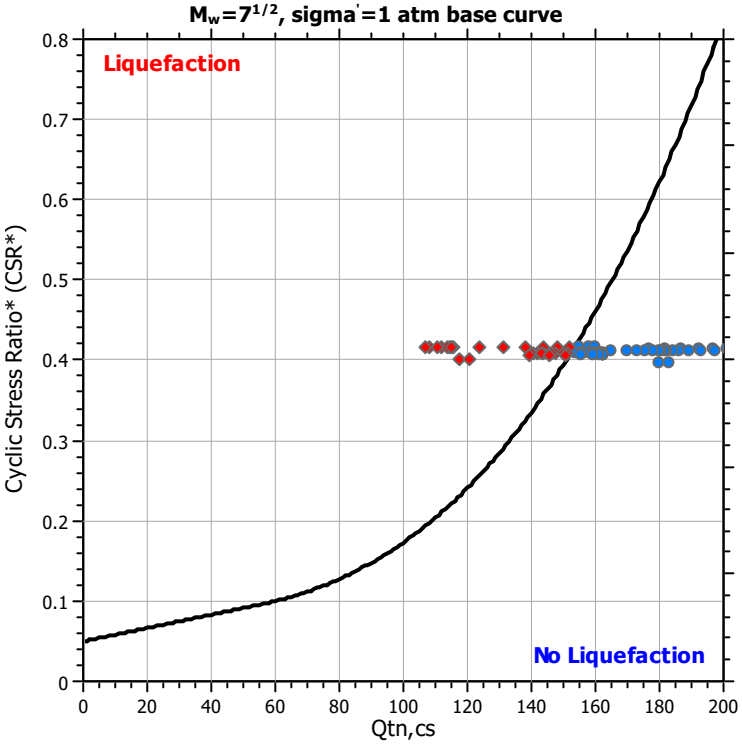
Project title : W1301-06-01 **Location : Perry Street**

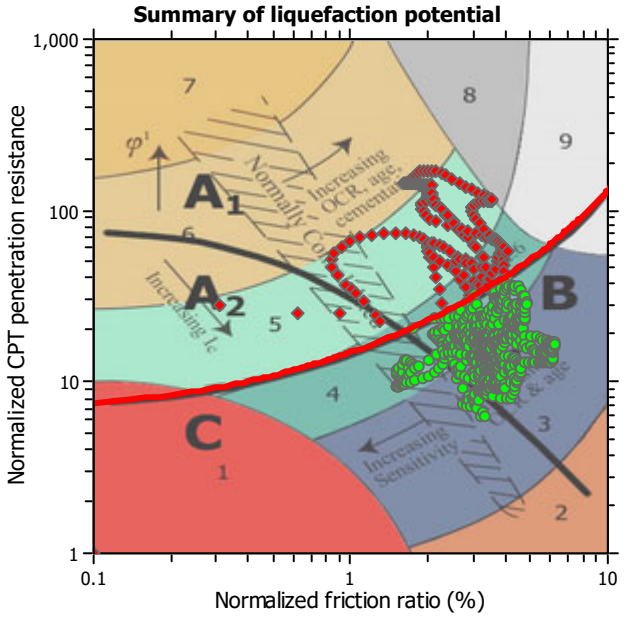
CPT file : CPT-2

Input parameters and analysis data

Analysis method:	NCEER (1998)	G.W.T. (in-situ):	12.00 ft	Use fill:	No	Clay like behavior applied:	Sands only
Fines correction method:	NCEER (1998)	G.W.T. (earthq.):	9.00 ft	Fill height:	N/A	Limit depth applied:	Yes
Points to test:	Based on Ic value	Average results interval:	.	Fill weight:	N/A	Limit depth:	50.00 ft
Earthquake magnitude M_w:	6.68	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	MSF method:	Method based
Peak ground acceleration:	0.55	Unit weight calculation:	Based on SBT	K_σ applied:	Yes		

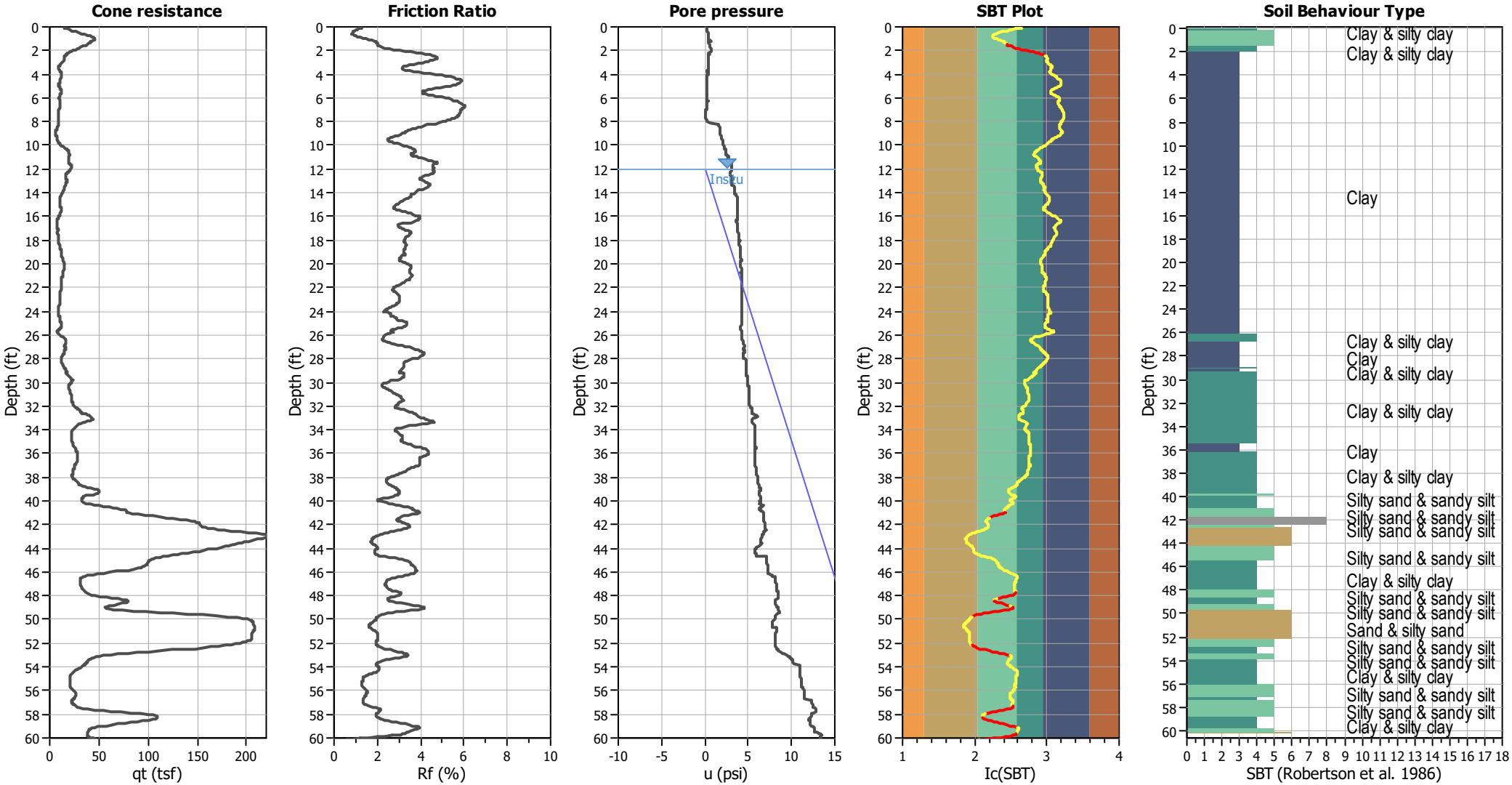






Zone A_1: Cyclic liquefaction likely depending on size and duration of cyclic loading
Zone A_2: Cyclic liquefaction and strength loss likely depending on loading and ground geometry
Zone B: Liquefaction and post-earthquake strength loss unlikely, check cyclic softening
Zone C: Cyclic liquefaction and strength loss possible depending on soil plasticity, brittleness/sensitivity, strain to peak undrained strength and ground geometry

CPT basic interpretation plots



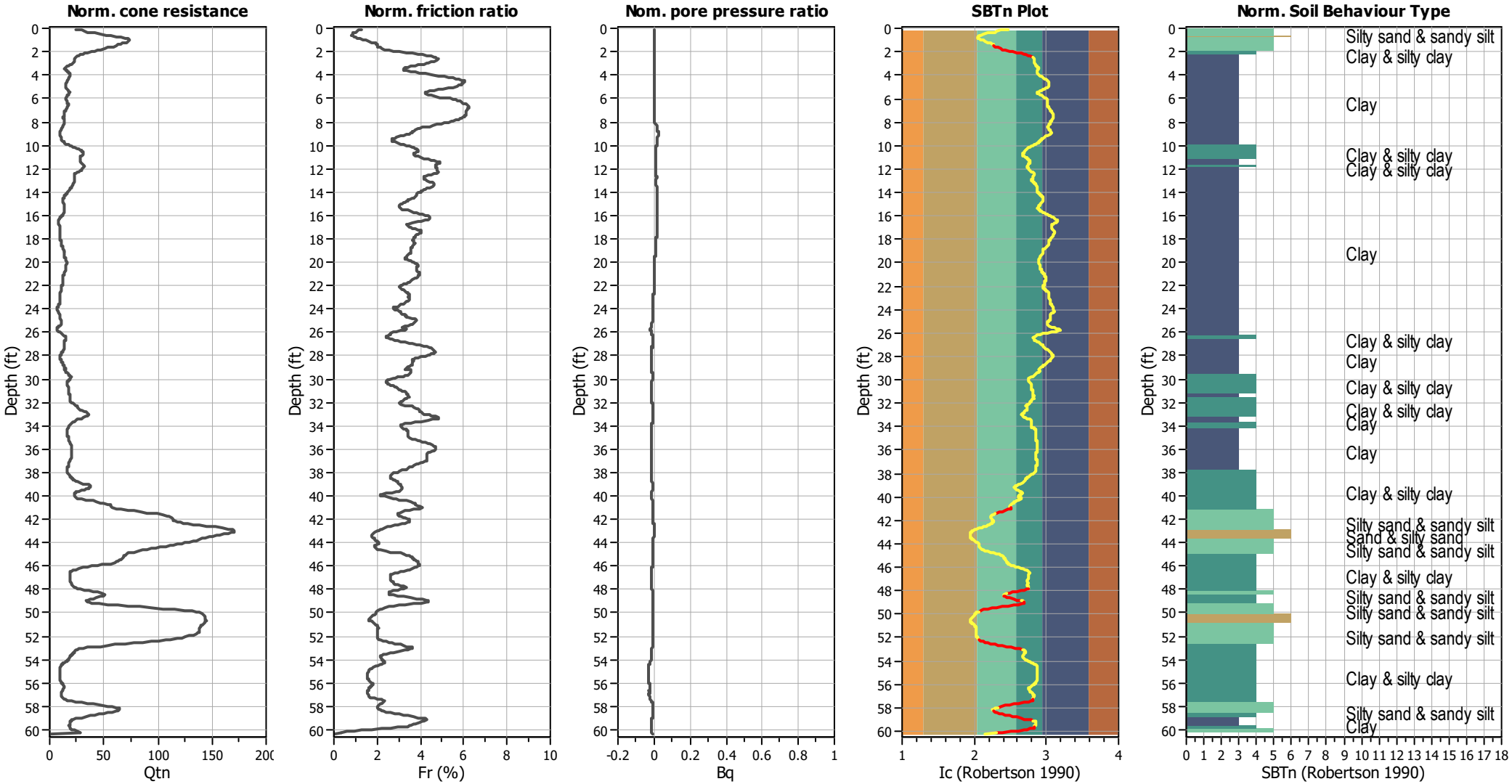
Input parameters and analysis data

Analysis method:	NCEER (1998)	Depth to water table (erthq.):	9.00 ft	Fill weight:	N/A
Fines correction method:	NCEER (1998)	Average results interval:	.	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.68	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.55	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	12.00 ft	Fill height:	N/A	Limit depth:	50.00 ft

SBT legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to
9. Very stiff fine grained

CPT basic interpretation plots (normalized)



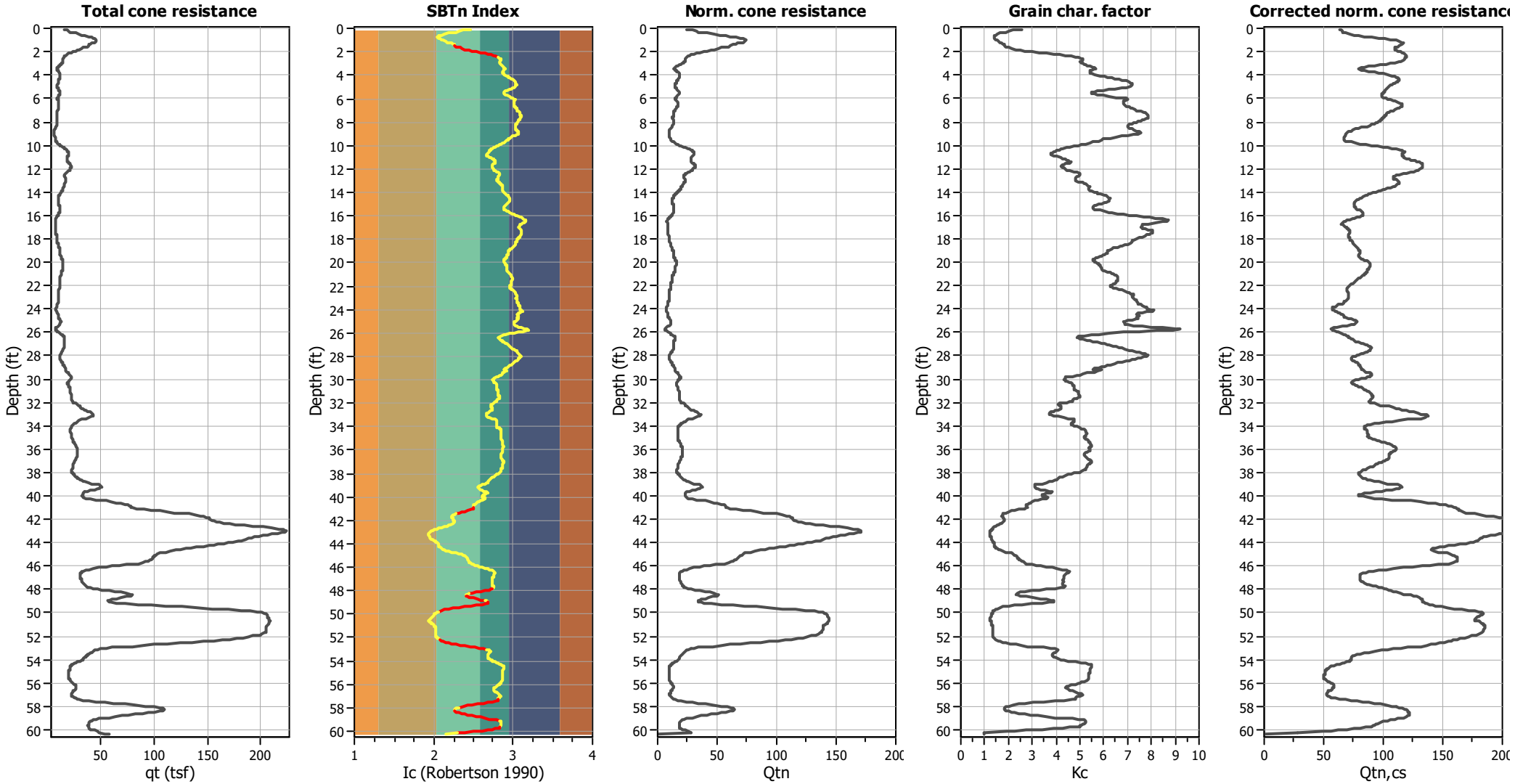
Input parameters and analysis data

Analysis method:	NCEER (1998)	Depth to water table (erthq.):	9.00 ft	Fill weight:	N/A
Fines correction method:	NCEER (1998)	Average results interval:	.	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.68	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.55	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	12.00 ft	Fill height:	N/A	Limit depth:	50.00 ft

SBTn legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to
9. Very stiff fine grained

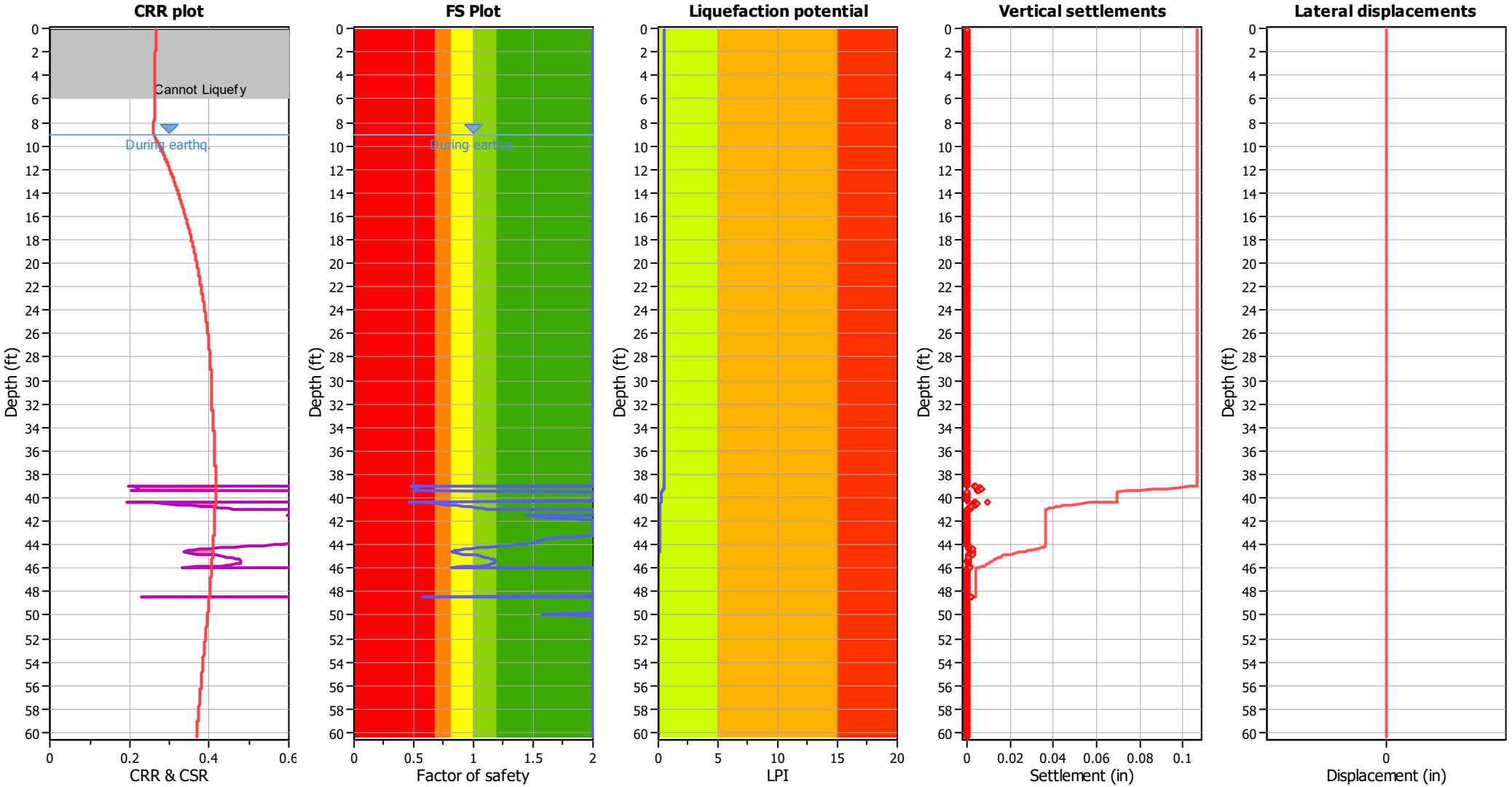
Liquefaction analysis overall plots (intermediate results)



Input parameters and analysis data

Analysis method:	NCEER (1998)	Depth to water table (erthq.):	9.00 ft	Fill weight:	N/A
Fines correction method:	NCEER (1998)	Average results interval:	.	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.68	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.55	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	12.00 ft	Fill height:	N/A	Limit depth:	50.00 ft

Liquefaction analysis overall plots



Input parameters and analysis data

Analysis method:	NCEER (1998)	Depth to water table (erthq.):	9.00 ft	Fill weight:	N/A
Fines correction method:	NCEER (1998)	Average results interval:	.	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.68	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.55	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	12.00 ft	Fill height:	N/A	Limit depth:	50.00 ft

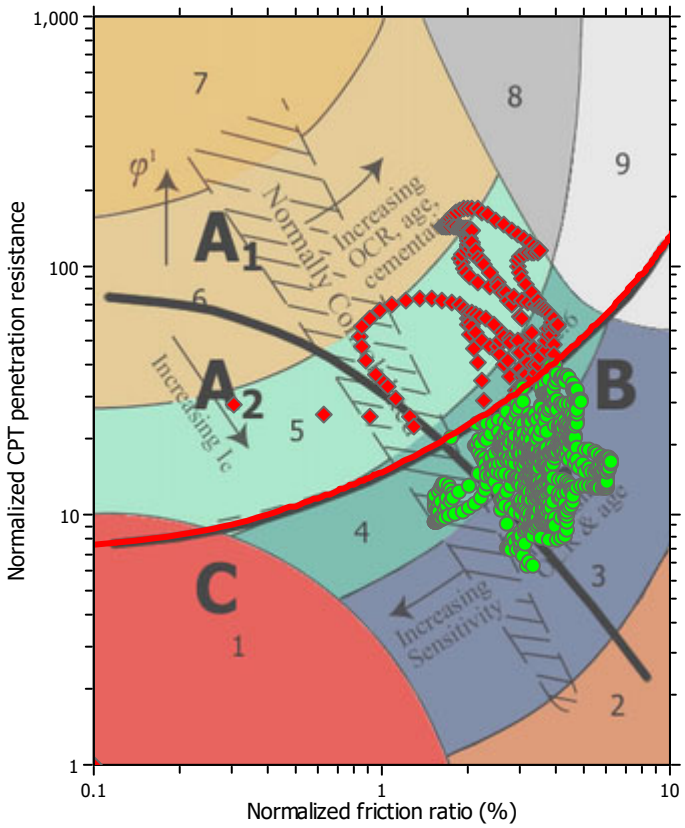
F.S. color scheme

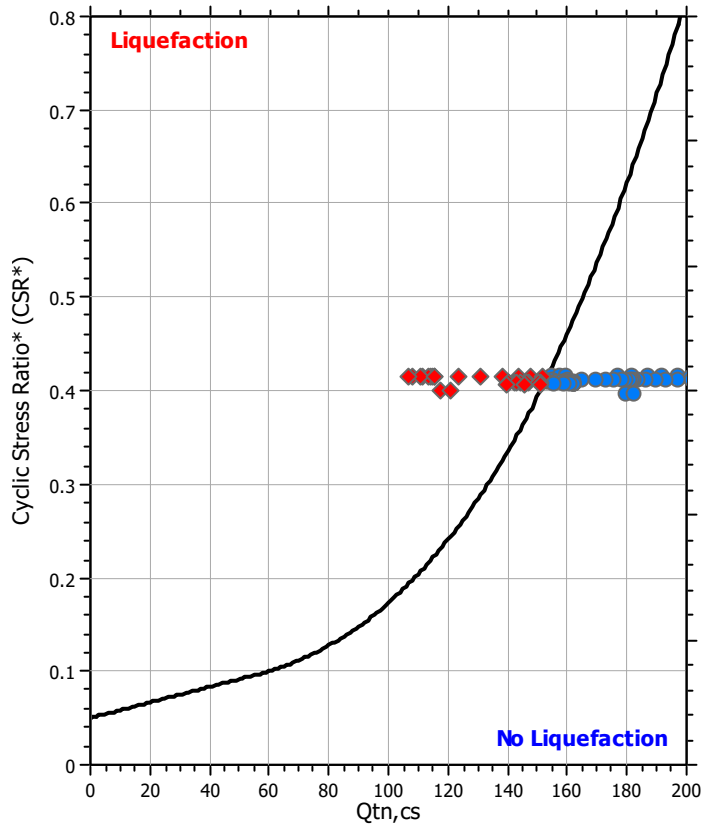
- Almost certain it will liquefy
- Very likely to liquefy
- Liquefaction and no liq. are equally likely
- Unlike to liquefy
- Almost certain it will not liquefy

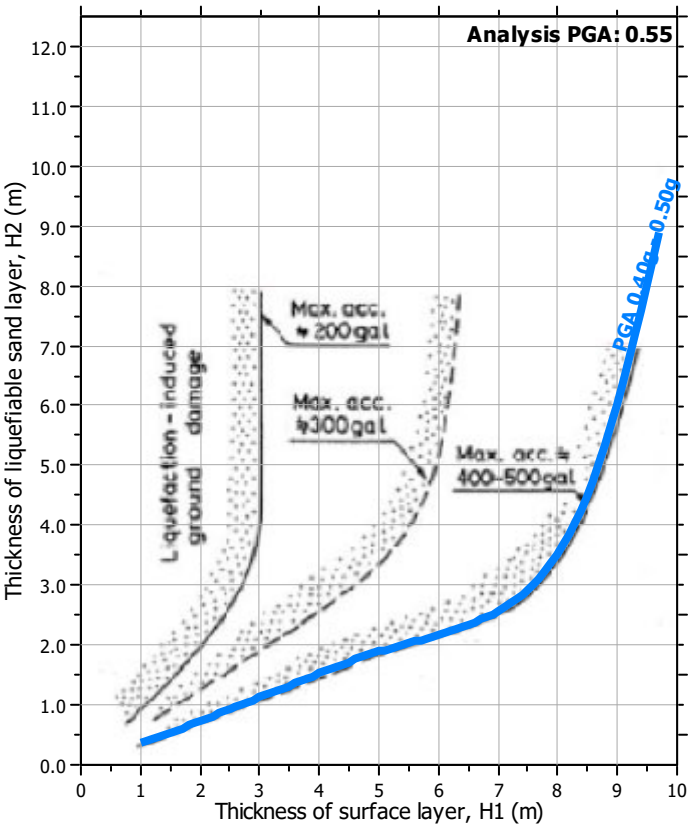
LPI color scheme

- Very high risk
- High risk
- Low risk

Liquefaction analysis summary plots



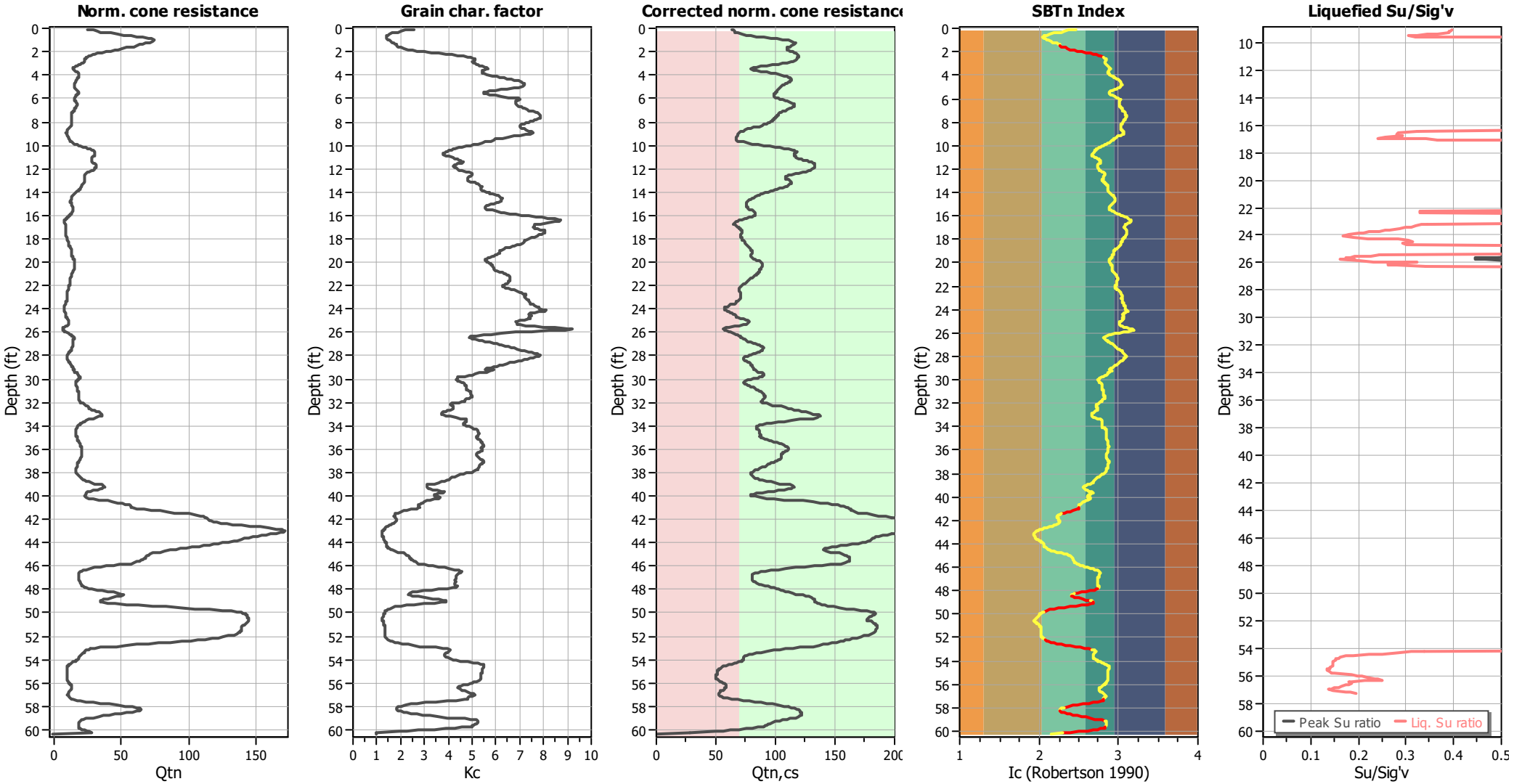




Input parameters and analysis data

Analysis method:	NCEER (1998)	Depth to water table (erthq.):	9.00 ft	Fill weight:	N/A
Fines correction method:	NCEER (1998)	Average results interval:	.	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.68	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.55	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	12.00 ft	Fill height:	N/A	Limit depth:	50.00 ft

Check for strength loss plots (Robertson (2010))



Input parameters and analysis data

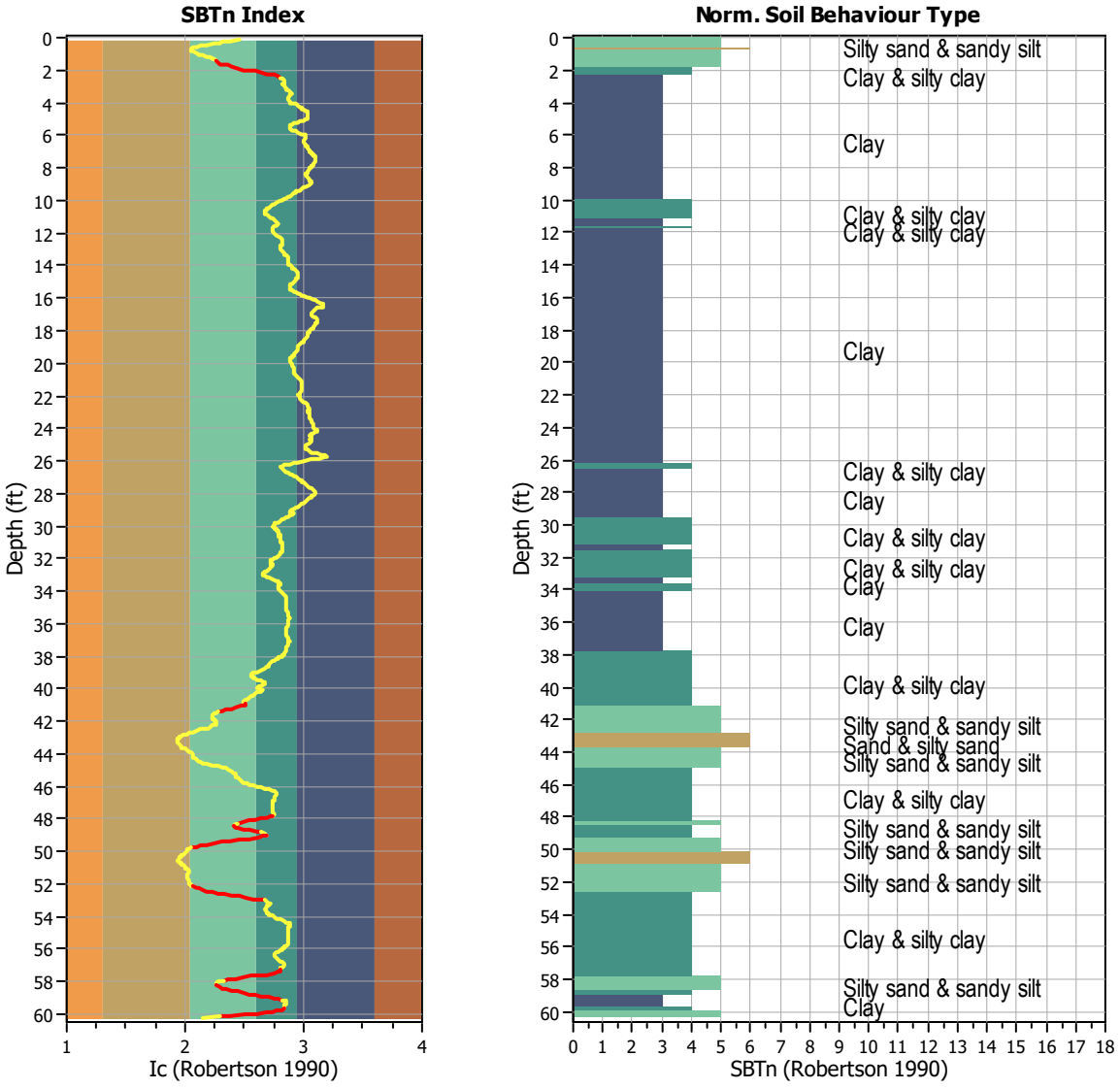
Analysis method:	NCEER (1998)	Depth to water table (erthq.):	9.00 ft	Fill weight:	N/A
Fines correction method:	NCEER (1998)	Average results interval:	.	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.68	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.55	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	12.00 ft	Fill height:	N/A	Limit depth:	50.00 ft

TRANSITION LAYER DETECTION ALGORITHM REPORT
Summary Details & Plots

Short description

The software will delete data when the cone is in transition from either clay to sand or vise-versa. To do this the software requires a range of I_c values over which the transition will be defined (typically somewhere between $1.80 < I_c < 3.0$) and a rate of change of I_c. Transitions typically occur when the rate of change of I_c is fast (i.e. delta I_c is small).

The SBT_n plot below, displays in red the detected transition layers based on the parameters listed below the graphs.



Transition layer algorithm properties		General statistics	
I_c minimum check value:	1.70	Total points in CPT file:	920
I_c maximum check value:	3.00	Total points excluded:	100
I_c change ratio value:	0.0250	Exclusion percentage:	10.87%
Minimum number of points in layer:	4	Number of layers detected:	9

Transition layer No	Number of points	Depth	SBT_n number	SBT_n description
Transition layer 1	16	Start depth: 1.55 (ft)	5	Silty sand & sandy silt
		End depth: 2.50 (ft)	3	Clay
Transition layer 2	8	Start depth: 41.03 (ft)	4	Clay & silty clay
		End depth: 41.48 (ft)	5	Silty sand & sandy silt
Transition layer 3	8	Start depth: 47.86 (ft)	4	Clay & silty clay
		End depth: 48.34 (ft)	5	Silty sand & sandy silt
Transition layer 4	7	Start depth: 48.51 (ft)	5	Silty sand & sandy silt
		End depth: 48.90 (ft)	4	Clay & silty clay
Transition layer 5	13	Start depth: 49.03 (ft)	4	Clay & silty clay
		End depth: 49.83 (ft)	5	Silty sand & sandy silt
Transition layer 6	14	Start depth: 52.26 (ft)	5	Silty sand & sandy silt
		End depth: 53.10 (ft)	4	Clay & silty clay
Transition layer 7	11	Start depth: 57.38 (ft)	4	Clay & silty clay
		End depth: 58.02 (ft)	5	Silty sand & sandy silt
Transition layer 8	14	Start depth: 58.37 (ft)	5	Silty sand & sandy silt
		End depth: 59.19 (ft)	3	Clay
Transition layer 9	9	Start depth: 59.74 (ft)	3	Clay
		End depth: 60.25 (ft)	5	Silty sand & sandy silt

Start depth: Depth where the transition layer begins
End depth: Depth where the transition layer ends

:: Field input data ::

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1	0.10	11.46	0.17	0.19	28.94	104.87
2	0.16	15.94	0.19	0.19	25.35	105.73
3	0.21	21.31	0.22	0.29	23.07	106.28
4	0.29	21.76	0.24	0.29	22.11	106.51
5	0.36	21.94	0.23	0.29	20.78	106.71
6	0.40	23.37	0.22	0.29	18.55	107.47
7	0.51	24.80	0.20	0.38	16.79	108.34
8	0.57	30.08	0.23	0.38	15.63	109.20
9	0.61	34.47	0.25	0.38	14.78	110.22
10	0.70	40.38	0.29	0.38	14.48	111.48
11	0.76	46.29	0.36	0.38	14.37	112.72
12	0.81	48.26	0.42	0.38	14.46	113.95
13	0.87	49.51	0.52	0.48	14.96	115.09
14	0.96	47.54	0.66	0.38	15.64	116.10
15	1.00	47.45	0.72	0.38	16.49	116.88
16	1.05	46.92	0.78	0.38	17.42	117.37
17	1.16	44.32	0.89	0.57	18.33	117.72
18	1.20	43.25	0.93	0.67	19.21	117.90
19	1.26	41.72	0.91	0.48	19.90	117.84
20	1.35	40.38	0.82	0.48	20.53	117.71
21	1.40	40.11	0.79	0.48	21.05	117.51
22	1.45	38.77	0.76	0.57	21.37	117.22
23	1.55	35.37	0.68	0.57	21.82	116.90
24	1.60	35.37	0.67	0.57	22.49	116.58
25	1.64	35.46	0.66	0.57	23.54	116.34
26	1.71	34.29	0.68	0.57	24.88	116.12
27	1.79	31.25	0.71	0.67	26.37	115.93
28	1.87	27.58	0.72	0.67	27.98	115.87
29	1.95	24.00	0.72	0.67	30.04	115.79
30	2.00	22.38	0.73	0.67	32.45	115.68
31	2.04	21.49	0.73	0.67	35.06	115.52
32	2.11	20.32	0.75	0.67	37.58	115.32
33	2.19	18.00	0.75	0.48	39.79	115.14
34	2.24	17.28	0.74	0.48	41.60	114.98
35	2.30	16.39	0.72	0.57	43.26	114.80
36	2.38	15.58	0.71	0.48	44.87	114.64
37	2.45	15.22	0.71	0.38	46.25	114.45
38	2.50	14.68	0.70	0.48	47.13	114.31
39	2.58	14.24	0.69	0.48	47.86	114.19
40	2.64	14.15	0.69	0.48	48.30	114.08
41	2.69	14.06	0.68	0.48	48.25	113.90
42	2.79	14.06	0.69	0.48	48.00	113.65
43	2.85	14.06	0.68	0.48	47.59	113.36
44	2.90	14.24	0.66	0.48	47.74	112.89
45	2.98	14.50	0.58	0.38	48.23	112.24
46	3.05	14.24	0.52	0.38	48.67	111.47
47	3.09	13.88	0.48	0.38	48.95	110.56
48	3.17	10.57	0.39	0.38	49.56	109.55

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
49	3.24	8.51	0.31	0.38	50.23	108.46
50	3.29	8.15	0.26	0.38	50.84	107.52
51	3.36	8.06	0.23	0.38	51.38	106.86
52	3.44	7.16	0.23	0.38	51.87	106.35
53	3.48	7.34	0.23	0.38	51.28	106.38
54	3.56	8.95	0.25	0.38	50.61	106.91
55	3.64	10.39	0.31	0.38	50.26	107.62
56	3.69	10.92	0.33	0.29	50.31	108.48
57	3.76	11.82	0.39	0.38	50.11	109.35
58	3.84	12.00	0.46	0.29	50.06	110.20
59	3.88	12.00	0.49	0.38	50.59	110.92
60	3.98	12.00	0.55	0.38	51.44	111.45
61	4.03	11.91	0.58	0.38	52.81	111.87
62	4.08	11.91	0.61	0.29	53.99	112.20
63	4.14	11.64	0.62	0.29	54.94	112.41
64	4.23	11.37	0.62	0.29	55.91	112.56
65	4.27	10.12	0.62	0.19	56.89	112.59
66	4.36	11.01	0.63	0.19	57.82	112.56
67	4.41	11.10	0.63	0.19	58.78	112.45
68	4.46	10.74	0.62	0.19	59.63	112.31
69	4.55	10.12	0.61	0.19	60.33	112.15
70	4.61	9.85	0.59	0.19	60.36	111.99
71	4.66	9.49	0.58	0.19	60.71	111.75
72	4.75	9.31	0.56	0.19	61.03	111.50
73	4.80	9.31	0.54	0.19	61.24	111.28
74	4.86	9.31	0.52	0.19	61.04	111.10
75	4.96	9.22	0.49	0.19	60.69	110.96
76	5.01	9.40	0.49	0.19	59.87	110.86
77	5.06	9.40	0.50	0.19	58.49	110.82
78	5.16	9.67	0.50	0.29	56.83	110.82
79	5.21	9.85	0.50	0.19	55.13	110.85
80	5.26	10.48	0.50	0.19	53.60	110.92
81	5.32	11.55	0.49	0.19	52.28	110.94
82	5.41	12.45	0.49	0.19	51.32	110.91
83	5.46	12.80	0.48	0.19	50.83	110.84
84	5.52	12.80	0.48	0.19	50.77	110.75
85	5.60	12.45	0.46	0.19	51.33	110.64
86	5.66	11.46	0.45	0.19	52.37	110.51
87	5.71	10.48	0.45	0.19	53.80	110.38
88	5.81	9.49	0.45	0.29	55.38	110.31
89	5.89	8.60	0.46	0.29	57.00	110.28
90	5.91	8.60	0.46	0.29	58.53	110.37
91	6.00	8.77	0.47	0.29	59.56	110.54
92	6.06	9.31	0.49	0.29	60.00	110.82
93	6.11	9.58	0.51	0.29	59.94	111.18
94	6.20	10.12	0.55	0.29	59.53	111.60
95	6.24	10.48	0.57	0.38	59.15	112.02
96	6.30	11.01	0.61	0.29	58.91	112.36

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
97	6.38	11.28	0.65	0.19	58.89	112.64
98	6.46	11.37	0.69	0.19	58.91	112.85
99	6.50	11.37	0.70	0.19	59.04	112.94
100	6.60	11.01	0.68	0.19	59.32	112.97
101	6.63	10.83	0.67	0.19	59.75	112.90
102	6.72	10.65	0.65	0.19	60.28	112.71
103	6.80	10.39	0.62	0.19	60.79	112.45
104	6.84	10.12	0.60	0.19	61.22	112.15
105	6.90	9.85	0.58	0.19	61.75	111.85
106	7.00	9.31	0.54	0.19	62.26	111.56
107	7.04	9.13	0.53	0.10	62.85	111.29
108	7.09	9.13	0.52	0.10	63.45	111.04
109	7.20	8.68	0.51	0.10	64.02	110.81
110	7.24	8.68	0.51	0.10	64.48	110.61
111	7.30	8.51	0.51	0.10	64.77	110.47
112	7.39	8.33	0.49	0.10	64.96	110.33
113	7.43	8.33	0.49	0.10	65.18	110.20
114	7.50	8.33	0.48	0.10	65.18	110.11
115	7.59	8.33	0.47	0.10	65.19	110.01
116	7.64	8.33	0.46	0.10	64.97	109.92
117	7.70	8.33	0.46	0.10	64.68	109.86
118	7.79	8.33	0.46	0.10	64.21	109.77
119	7.83	8.33	0.46	0.19	63.76	109.65
120	7.90	8.51	0.46	0.19	63.32	109.53
121	7.94	8.51	0.45	0.19	62.76	109.43
122	8.03	8.68	0.43	0.19	62.22	109.27
123	8.11	8.51	0.41	0.57	61.67	109.03
124	8.17	8.51	0.40	1.44	61.05	108.75
125	8.21	8.77	0.40	1.44	60.55	108.39
126	8.28	8.51	0.37	1.53	60.19	107.96
127	8.37	8.24	0.34	1.63	60.00	107.50
128	8.41	8.15	0.32	1.73	59.93	107.00
129	8.48	7.88	0.30	1.82	60.12	106.42
130	8.57	7.43	0.27	1.82	60.57	105.76
131	8.61	7.25	0.25	1.82	61.03	105.15
132	8.67	6.80	0.23	1.82	61.59	104.56
133	8.77	6.27	0.21	1.82	62.21	104.02
134	8.81	6.00	0.20	1.82	62.88	103.57
135	8.87	6.00	0.20	1.82	63.19	103.25
136	8.96	5.82	0.19	1.82	63.26	103.03
137	8.99	5.91	0.19	1.82	62.68	102.92
138	9.07	5.91	0.20	1.82	61.50	102.89
139	9.16	6.27	0.20	1.92	60.08	102.88
140	9.21	6.63	0.20	1.92	58.54	102.82
141	9.27	7.16	0.20	1.92	57.01	102.76
142	9.36	7.52	0.19	1.92	55.81	102.73
143	9.40	7.61	0.18	1.92	54.70	102.70
144	9.48	7.70	0.17	1.92	53.93	102.75

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
145	9.52	7.61	0.16	2.01	53.37	103.03
146	9.61	7.43	0.17	2.01	52.59	103.41
147	9.65	7.34	0.18	2.01	51.93	103.94
148	9.72	7.52	0.20	2.01	51.10	104.83
149	9.81	8.33	0.25	2.11	50.15	105.79
150	9.86	9.58	0.27	2.11	49.11	107.06
151	9.91	10.39	0.30	2.11	47.99	108.23
152	10.00	12.18	0.38	2.20	46.99	109.32
153	10.05	13.16	0.41	2.20	45.83	110.44
154	10.16	15.04	0.52	2.30	44.69	111.45
155	10.20	15.40	0.55	2.30	43.64	112.32
156	10.25	15.40	0.58	2.30	42.61	113.13
157	10.31	17.01	0.66	2.40	41.93	113.78
158	10.40	18.00	0.71	2.40	41.34	114.36
159	10.44	18.98	0.71	2.40	40.62	114.79
160	10.51	19.97	0.74	2.40	40.18	115.04
161	10.59	19.97	0.77	2.40	39.63	115.17
162	10.65	20.41	0.78	2.40	39.25	115.18
163	10.71	21.94	0.80	2.40	38.89	115.10
164	10.80	19.61	0.71	2.49	38.90	115.12
165	10.85	19.16	0.65	2.59	39.00	115.13
166	10.90	19.43	0.64	2.59	39.65	115.10
167	10.96	19.43	0.62	2.68	40.86	115.07
168	11.04	19.79	0.72	2.68	41.80	115.10
169	11.10	19.97	0.75	2.68	42.47	115.30
170	11.18	16.74	0.78	2.59	43.17	115.59
171	11.24	14.77	0.83	2.97	43.67	115.89
172	11.30	18.44	0.87	2.97	44.14	116.22
173	11.35	18.80	0.90	3.07	44.49	116.52
174	11.42	19.25	0.92	3.07	44.80	116.82
175	11.51	20.41	0.92	3.07	44.38	117.13
176	11.55	20.86	0.94	3.07	43.27	117.40
177	11.62	21.40	1.01	3.07	42.74	117.59
178	11.71	21.94	1.05	3.16	42.31	117.74
179	11.75	22.29	1.05	3.16	42.06	117.85
180	11.85	23.10	1.02	3.16	42.33	117.91
181	11.90	23.46	1.01	3.16	42.58	117.91
182	11.94	23.37	1.02	3.16	42.85	117.79
183	12.02	22.03	1.01	3.16	43.34	117.57
184	12.10	20.41	0.99	3.07	43.89	117.29
185	12.15	19.97	0.96	3.07	44.73	116.94
186	12.24	18.98	0.90	2.97	45.78	116.53
187	12.30	17.64	0.85	2.97	46.63	116.07
188	12.35	16.83	0.79	2.97	47.40	115.55
189	12.44	15.85	0.73	2.97	47.60	115.06
190	12.50	15.22	0.69	2.97	47.60	114.60
191	12.55	15.85	0.65	2.97	47.36	114.27
192	12.63	14.68	0.60	3.07	46.97	114.04

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
193	12.70	15.85	0.59	3.26	46.68	113.96
194	12.74	16.47	0.60	3.26	46.38	114.01
195	12.84	17.37	0.64	3.26	46.14	114.15
196	12.86	17.46	0.66	3.16	46.09	114.32
197	12.94	17.46	0.72	3.16	46.02	114.53
198	13.01	17.46	0.75	3.16	46.40	114.70
199	13.09	17.46	0.77	3.16	46.96	114.82
200	13.14	17.46	0.77	3.16	47.54	114.83
201	13.20	16.92	0.75	3.16	48.12	114.79
202	13.29	15.94	0.73	3.16	48.58	114.66
203	13.33	15.58	0.72	3.16	48.98	114.49
204	13.39	15.49	0.68	3.26	49.36	114.28
205	13.49	15.13	0.65	3.45	49.77	114.06
206	13.53	15.04	0.64	3.45	50.10	113.86
207	13.59	14.86	0.64	3.45	49.96	113.53
208	13.69	14.77	0.63	3.45	49.69	113.11
209	13.73	14.77	0.63	3.45	49.74	112.77
210	13.79	14.50	0.62	3.45	49.98	112.44
211	13.89	14.15	0.49	3.45	50.34	112.10
212	13.94	13.79	0.43	3.45	50.60	111.71
213	13.99	13.07	0.46	3.45	51.51	111.23
214	14.08	12.36	0.46	3.45	52.11	110.70
215	14.13	12.00	0.45	3.54	52.37	110.17
216	14.18	11.82	0.43	3.54	53.09	109.80
217	14.27	9.49	0.40	3.54	54.07	109.52
218	14.32	10.39	0.38	3.74	54.65	109.16
219	14.37	11.01	0.37	3.74	55.04	108.74
220	14.48	10.57	0.34	3.74	55.39	108.35
221	14.52	10.30	0.33	3.74	55.76	107.98
222	14.58	10.12	0.32	3.74	55.23	107.71
223	14.68	9.67	0.30	3.74	55.33	107.48
224	14.72	9.67	0.30	3.74	55.37	107.27
225	14.77	9.58	0.30	3.74	55.18	107.17
226	14.83	9.40	0.29	3.74	54.68	107.14
227	14.92	9.40	0.30	3.74	54.04	107.12
228	14.98	10.12	0.30	3.74	53.31	107.17
229	15.07	10.57	0.30	3.74	52.63	107.22
230	15.11	11.28	0.31	3.74	51.95	107.29
231	15.17	11.46	0.30	3.74	51.44	107.45
232	15.27	11.46	0.30	3.83	51.00	107.60
233	15.31	11.46	0.30	3.83	50.86	107.76
234	15.38	11.46	0.31	3.83	51.10	107.97
235	15.47	11.37	0.33	3.83	51.48	108.18
236	15.52	11.28	0.34	3.83	52.17	108.41
237	15.56	11.28	0.35	3.74	53.08	108.62
238	15.64	11.19	0.38	3.74	54.10	108.82
239	15.71	11.55	0.39	3.74	55.13	108.96
240	15.75	11.10	0.40	3.74	56.21	109.04

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
241	15.87	10.48	0.40	3.74	57.53	109.02
242	15.91	10.30	0.40	3.74	59.02	108.94
243	15.96	10.03	0.39	3.74	60.52	108.72
244	16.01	9.67	0.39	3.74	62.40	108.38
245	16.11	8.86	0.36	3.74	64.16	107.96
246	16.15	8.24	0.35	3.74	65.59	107.49
247	16.22	7.70	0.32	3.74	67.02	106.92
248	16.31	7.16	0.29	3.64	68.51	106.34
249	16.36	6.98	0.27	3.74	69.64	105.75
250	16.41	6.80	0.25	3.64	70.03	105.26
251	16.51	6.54	0.22	3.74	69.73	104.82
252	16.54	6.45	0.22	3.74	68.62	104.53
253	16.61	6.63	0.22	3.74	66.89	104.27
254	16.70	7.07	0.22	3.83	65.16	104.03
255	16.75	7.43	0.22	3.83	64.26	104.16
256	16.81	8.15	0.23	3.83	63.84	104.47
257	16.91	8.42	0.20	3.83	63.55	104.80
258	16.95	8.42	0.19	3.83	63.39	105.11
259	17.01	8.33	0.27	3.83	63.54	105.40
260	17.11	8.06	0.29	3.83	63.87	105.63
261	17.13	7.97	0.30	3.83	64.27	105.78
262	17.21	7.88	0.30	3.83	65.12	106.01
263	17.29	7.88	0.30	3.83	66.04	106.26
264	17.34	7.88	0.29	3.83	66.17	106.29
265	17.43	8.15	0.28	3.93	66.19	106.26
266	17.48	8.15	0.28	3.93	66.09	106.20
267	17.54	8.15	0.28	3.93	65.76	106.16
268	17.63	8.33	0.28	3.93	65.34	106.12
269	17.68	8.06	0.28	3.93	64.78	106.12
270	17.73	7.97	0.28	3.93	64.37	106.14
271	17.83	8.24	0.28	3.93	63.84	106.20
272	17.85	8.42	0.28	3.93	63.27	106.30
273	17.93	8.68	0.28	3.93	62.84	106.42
274	17.98	8.86	0.28	3.93	62.23	106.55
275	18.07	9.22	0.29	4.02	61.69	106.71
276	18.12	9.31	0.30	3.93	61.39	106.85
277	18.18	9.49	0.31	3.93	61.26	107.01
278	18.24	9.49	0.31	3.93	61.14	107.17
279	18.33	9.49	0.32	3.93	60.99	107.32
280	18.38	9.31	0.32	3.93	60.70	107.49
281	18.47	9.31	0.33	4.02	60.14	107.66
282	18.53	9.58	0.33	4.02	59.50	107.81
283	18.57	9.85	0.33	4.02	58.79	107.99
284	18.67	10.39	0.34	4.02	58.23	108.21
285	18.72	11.10	0.35	4.02	57.50	108.46
286	18.78	11.28	0.35	4.02	56.59	108.69
287	18.85	11.55	0.36	4.02	55.84	108.91
288	18.93	11.64	0.39	4.02	55.33	109.12

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
289	18.97	11.91	0.40	4.12	55.04	109.28
290	19.08	12.27	0.40	4.02	55.00	109.39
291	19.12	12.27	0.40	4.02	54.97	109.46
292	19.22	12.09	0.40	4.02	54.92	109.49
293	19.27	11.91	0.40	4.02	54.37	109.46
294	19.32	11.91	0.39	4.12	53.99	109.38
295	19.37	11.82	0.38	4.12	53.68	109.38
296	19.43	12.00	0.37	4.12	53.38	109.43
297	19.52	12.80	0.36	4.12	52.97	109.53
298	19.57	12.53	0.36	4.12	52.35	109.68
299	19.67	13.07	0.39	4.22	51.75	109.86
300	19.72	13.34	0.41	4.22	51.24	110.12
301	19.77	13.79	0.43	4.12	51.05	110.49
302	19.82	14.41	0.45	4.12	51.19	110.86
303	19.92	14.68	0.45	4.12	51.32	111.24
304	19.97	14.77	0.48	4.12	51.47	111.50
305	20.04	14.77	0.53	4.12	51.79	111.69
306	20.08	14.77	0.54	4.12	52.07	111.80
307	20.16	14.68	0.55	4.12	52.42	111.88
308	20.24	14.41	0.53	4.12	52.75	111.92
309	20.28	13.79	0.52	4.12	52.98	111.90
310	20.37	13.79	0.50	4.22	53.06	111.81
311	20.41	14.06	0.50	4.22	53.13	111.72
312	20.50	14.15	0.48	4.22	53.23	111.59
313	20.57	14.15	0.48	4.22	53.38	111.49
314	20.61	14.15	0.48	4.22	53.53	111.41
315	20.70	14.06	0.49	4.22	53.82	111.36
316	20.76	13.79	0.48	4.12	54.26	111.27
317	20.81	13.52	0.48	4.31	54.83	111.20
318	20.89	12.98	0.48	4.31	55.51	111.11
319	20.95	12.89	0.48	4.31	56.11	110.98
320	21.00	12.53	0.47	4.31	56.52	110.78
321	21.10	12.36	0.46	4.31	56.95	110.58
322	21.14	12.09	0.45	4.31	57.22	110.36
323	21.21	12.09	0.43	4.31	57.45	110.16
324	21.30	12.09	0.40	4.31	57.65	109.94
325	21.34	11.91	0.39	4.31	57.67	109.74
326	21.40	11.82	0.38	4.31	57.70	109.53
327	21.48	11.55	0.39	4.31	57.55	109.33
328	21.54	11.46	0.38	4.31	57.38	109.13
329	21.60	11.55	0.38	4.31	57.30	108.96
330	21.68	11.37	0.37	4.22	57.21	108.82
331	21.75	11.55	0.36	4.22	57.10	108.65
332	21.80	11.55	0.34	4.22	56.73	108.44
333	21.88	11.55	0.33	4.22	56.34	108.22
334	21.92	11.55	0.33	4.22	55.95	107.99
335	21.99	11.37	0.31	4.31	55.72	107.81
336	22.08	11.37	0.30	4.31	55.79	107.64

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
337	22.15	11.37	0.29	4.31	55.96	107.51
338	22.19	11.37	0.29	4.31	56.46	107.42
339	22.28	11.10	0.30	4.31	57.14	107.33
340	22.34	10.74	0.30	4.22	57.91	107.32
341	22.39	10.74	0.30	4.31	58.69	107.31
342	22.47	10.21	0.31	4.22	59.43	107.31
343	22.54	9.94	0.31	4.31	60.24	107.33
344	22.58	9.94	0.32	4.31	60.61	107.34
345	22.68	9.94	0.31	4.31	60.98	107.36
346	22.74	10.12	0.30	4.31	61.38	107.40
347	22.79	10.12	0.31	4.31	61.39	107.43
348	22.84	10.57	0.31	4.31	61.31	107.46
349	22.94	10.30	0.31	4.31	61.21	107.47
350	22.99	10.30	0.32	4.31	61.16	107.48
351	23.04	10.39	0.32	4.31	61.43	107.47
352	23.11	10.30	0.32	4.31	61.60	107.40
353	23.18	10.30	0.32	4.31	61.97	107.30
354	23.23	10.12	0.31	4.31	62.14	107.17
355	23.34	9.67	0.30	4.31	62.27	106.96
356	23.37	9.67	0.29	4.31	62.40	106.70
357	23.44	9.63	0.28	4.31	62.50	106.41
358	23.54	9.58	0.27	4.31	62.77	106.03
359	23.60	9.40	0.25	4.31	63.05	105.63
360	23.64	9.22	0.24	4.22	63.47	105.21
361	23.71	9.13	0.23	4.22	63.80	104.73
362	23.79	8.60	0.21	4.22	64.37	104.21
363	23.84	8.33	0.20	4.22	64.67	103.72
364	23.89	7.61	0.19	4.22	64.66	103.40
365	23.99	7.66	0.17	4.22	64.77	103.26
366	24.03	7.25	0.16	4.31	65.69	103.41
367	24.10	7.70	0.16	4.31	66.47	103.74
368	24.18	8.51	0.18	4.31	66.14	104.19
369	24.23	8.77	0.21	4.31	64.92	104.70
370	24.31	8.42	0.27	4.22	63.67	105.19
371	24.36	8.68	0.29	4.22	62.52	105.69
372	24.45	10.21	0.30	4.22	62.43	106.15
373	24.49	10.92	0.30	4.22	62.59	106.51
374	24.57	11.19	0.28	4.22	62.87	106.70
375	24.61	10.83	0.28	4.22	62.50	106.78
376	24.69	9.67	0.29	4.22	62.27	106.95
377	24.74	9.67	0.29	4.22	62.47	107.31
378	24.82	9.13	0.27	4.31	62.55	107.96
379	24.89	9.40	0.29	4.31	62.18	108.72
380	24.94	9.85	0.34	4.31	61.29	109.37
381	25.01	11.37	0.42	4.31	60.13	109.78
382	25.09	13.61	0.53	4.22	59.20	109.99
383	25.13	15.22	0.56	4.22	59.09	109.93
384	25.22	15.58	0.53	4.02	59.31	109.76

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
385	25.28	14.06	0.44	4.12	59.50	109.41
386	25.34	12.80	0.36	4.12	60.17	108.79
387	25.44	9.13	0.24	4.12	61.44	107.77
388	25.48	8.24	0.22	4.12	63.53	106.54
389	25.53	7.79	0.19	4.12	65.99	105.13
390	25.59	7.16	0.18	4.22	68.60	104.05
391	25.68	6.80	0.17	4.22	71.70	103.35
392	25.73	6.80	0.19	4.31	72.62	103.67
393	25.79	6.98	0.16	4.22	70.95	103.92
394	25.88	7.34	0.20	4.31	67.35	104.37
395	25.93	7.34	0.23	4.22	63.11	104.98
396	25.99	9.04	0.32	4.31	59.09	105.82
397	26.08	10.83	0.26	4.31	55.23	106.70
398	26.14	13.61	0.26	4.31	52.62	107.65
399	26.19	15.13	0.28	4.31	50.58	108.39
400	26.28	16.65	0.34	4.31	48.56	108.93
401	26.34	18.18	0.38	4.31	46.95	109.19
402	26.39	17.64	0.41	4.31	46.50	109.54
403	26.45	16.65	0.41	4.41	46.85	109.82
404	26.53	16.47	0.38	4.41	47.53	110.04
405	26.58	15.85	0.38	4.41	48.34	110.25
406	26.68	14.68	0.38	4.50	49.47	110.42
407	26.73	14.41	0.38	4.50	50.36	110.57
408	26.78	14.50	0.39	4.50	51.12	110.83
409	26.88	15.49	0.45	4.60	52.31	111.23
410	26.93	15.85	0.48	4.60	53.43	111.64
411	26.98	15.94	0.50	4.60	54.17	112.04
412	27.04	16.12	0.55	4.60	54.80	112.45
413	27.13	15.76	0.61	4.50	55.45	112.81
414	27.22	15.31	0.62	4.60	56.32	113.06
415	27.24	15.31	0.62	4.50	57.10	113.20
416	27.33	15.40	0.63	4.60	57.87	113.29
417	27.37	15.31	0.63	4.60	58.72	113.27
418	27.43	14.86	0.63	4.60	59.55	113.15
419	27.52	14.68	0.60	4.50	60.39	113.02
420	27.57	14.59	0.58	4.50	61.26	112.82
421	27.63	13.88	0.57	4.50	62.13	112.51
422	27.72	12.98	0.56	4.50	63.06	112.14
423	27.76	12.53	0.56	4.50	63.68	111.71
424	27.84	12.09	0.52	4.50	64.27	111.27
425	27.93	11.64	0.46	4.50	64.88	110.85
426	27.97	11.28	0.43	4.60	65.17	110.44
427	28.02	11.28	0.40	4.60	64.86	110.06
428	28.12	11.28	0.37	4.69	64.17	109.68
429	28.17	11.37	0.37	4.69	63.45	109.39
430	28.23	11.37	0.37	4.69	62.70	109.32
431	28.32	11.82	0.37	4.69	61.88	109.38
432	28.37	12.18	0.37	4.69	61.14	109.54

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
433	28.42	12.18	0.38	4.69	60.44	109.81
434	28.48	12.80	0.41	4.69	59.74	110.14
435	28.57	13.34	0.44	4.69	58.51	110.50
436	28.61	13.61	0.45	4.69	57.53	110.87
437	28.69	14.15	0.47	4.69	56.72	111.21
438	28.77	14.68	0.50	4.79	55.82	111.52
439	28.83	16.30	0.51	4.79	54.93	111.72
440	28.88	16.30	0.52	4.79	54.18	111.86
441	28.97	16.39	0.52	4.79	53.42	112.00
442	29.02	16.56	0.51	4.79	52.46	112.16
443	29.08	16.65	0.49	4.79	51.49	112.33
444	29.17	16.47	0.49	4.79	50.96	112.49
445	29.21	16.92	0.50	4.79	53.21	112.57
446	29.28	18.35	0.53	4.79	52.21	112.93
447	29.37	19.07	0.56	4.69	51.27	113.36
448	29.41	19.43	0.58	4.79	50.43	113.83
449	29.47	9.67	0.64	4.89	49.47	114.26
450	29.56	22.38	0.70	4.89	48.35	114.53
451	29.62	23.19	0.74	4.89	47.37	114.69
452	29.68	23.46	0.76	4.89	46.50	114.72
453	29.76	23.82	0.74	4.89	45.58	114.67
454	29.83	24.00	0.64	4.89	43.17	114.56
455	29.87	24.08	0.60	4.89	43.08	114.11
456	29.96	23.28	0.54	4.89	43.14	113.53
457	30.01	23.28	0.50	4.89	42.92	112.88
458	30.07	20.32	0.45	4.98	43.06	112.20
459	30.16	18.44	0.40	4.98	43.45	111.74
460	30.20	17.55	0.38	4.98	43.91	111.38
461	30.27	18.49	0.37	4.98	44.46	111.20
462	30.34	17.19	0.38	5.08	45.12	111.16
463	30.42	18.53	0.42	5.08	45.45	111.31
464	30.46	19.16	0.44	5.17	45.58	111.61
465	30.52	19.70	0.47	5.17	45.58	111.99
466	30.58	20.41	0.50	5.17	45.79	112.40
467	30.66	20.41	0.53	5.13	45.70	112.83
468	30.71	20.41	0.55	5.17	45.72	113.19
469	30.81	20.77	0.57	5.17	45.83	113.52
470	30.87	21.13	0.59	5.17	45.95	113.80
471	30.91	21.31	0.61	5.17	46.23	114.05
472	31.01	21.76	0.63	5.17	46.56	114.29
473	31.06	21.85	0.64	5.17	46.84	114.52
474	31.11	21.85	0.65	5.17	47.09	114.72
475	31.19	21.58	0.67	5.17	47.15	114.90
476	31.26	21.40	0.70	5.17	47.15	115.03
477	31.35	21.49	0.72	5.17	47.16	115.14
478	31.37	21.67	0.72	5.17	47.30	115.23
479	31.46	22.74	0.72	5.17	47.28	115.31
480	31.55	22.83	0.71	5.17	47.34	115.36

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
481	31.59	23.01	0.71	5.17	47.07	115.38
482	31.66	22.12	0.71	5.17	46.58	115.34
483	31.70	22.97	0.71	5.17	45.91	115.27
484	31.79	22.03	0.71	5.17	45.54	115.19
485	31.86	22.92	0.70	5.17	45.20	115.11
486	31.91	23.46	0.66	5.17	44.72	115.14
487	31.99	24.26	0.64	5.27	43.83	115.41
488	32.06	23.91	0.64	5.27	42.93	115.81
489	32.10	23.82	0.63	5.27	41.75	116.33
490	32.20	25.79	0.71	5.36	41.18	116.95
491	32.26	29.64	0.86	5.36	41.62	117.54
492	32.30	32.41	0.97	5.46	41.77	118.18
493	32.35	35.01	1.07	5.36	42.04	118.76
494	32.46	34.38	1.19	5.36	42.03	119.31
495	32.49	28.56	1.23	5.36	42.14	119.80
496	32.58	31.96	1.28	5.36	42.01	120.20
497	32.62	30.26	1.27	5.36	41.21	120.70
498	32.69	32.19	1.25	5.56	40.38	121.30
499	32.78	32.41	1.31	5.84	39.57	121.87
500	32.82	37.07	1.36	5.94	38.65	122.47
501	32.89	46.47	1.56	6.04	38.48	122.98
502	32.98	52.02	1.83	5.84	38.34	123.44
503	33.02	51.93	1.96	5.65	38.62	123.78
504	33.08	48.53	2.08	5.46	38.94	123.93
505	33.18	44.23	2.12	5.36	39.64	123.96
506	33.21	41.81	2.07	5.46	40.97	123.77
507	33.29	36.80	1.92	5.36	42.69	123.33
508	33.37	32.77	1.64	5.46	44.21	122.69
509	33.42	31.16	1.51	5.46	45.24	121.91
510	33.47	29.99	1.37	5.56	45.70	121.02
511	33.53	28.56	1.21	5.65	45.94	120.01
512	33.62	28.29	0.97	5.84	45.72	119.00
513	33.67	27.93	0.87	5.84	45.46	118.10
514	33.73	27.31	0.79	5.84	45.27	117.19
515	33.82	25.61	0.69	5.84	45.15	116.32
516	33.87	24.62	0.66	5.84	45.08	115.57
517	33.93	22.74	0.63	5.84	45.43	115.09
518	34.02	21.31	0.60	5.84	45.99	114.73
519	34.06	20.77	0.59	5.84	46.70	114.52
520	34.13	20.77	0.60	5.84	47.41	114.48
521	34.22	21.58	0.62	5.84	48.04	114.50
522	34.26	21.85	0.64	5.84	48.50	114.60
523	34.32	22.03	0.67	5.84	48.79	114.74
524	34.42	22.20	0.69	5.75	49.01	114.87
525	34.46	22.29	0.70	5.75	49.09	114.96
526	34.52	21.85	0.72	5.75	49.21	115.01
527	34.61	21.49	0.71	5.75	49.27	115.04
528	34.70	21.31	0.69	5.75	49.31	115.05

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
529	34.76	21.40	0.67	5.75	49.25	115.10
530	34.82	21.67	0.66	5.84	49.19	115.13
531	34.86	22.03	0.66	5.84	48.94	115.12
532	34.92	22.20	0.68	5.84	48.83	115.22
533	35.02	23.01	0.72	5.84	48.85	115.42
534	35.06	23.01	0.72	5.84	48.85	115.68
535	35.11	22.92	0.70	5.84	48.92	116.01
536	35.19	23.10	0.78	5.84	49.57	116.33
537	35.25	23.37	0.84	5.84	50.03	116.65
538	35.31	24.17	0.88	5.84	49.99	117.00
539	35.40	24.80	0.93	5.84	50.04	117.40
540	35.45	22.56	0.96	5.84	50.21	117.86
541	35.50	23.64	0.99	5.94	50.35	118.28
542	35.56	26.95	1.03	5.94	50.40	118.64
543	35.64	27.40	1.11	5.84	50.58	118.97
544	35.72	27.31	1.17	5.84	50.72	119.25
545	35.81	27.40	1.24	5.84	50.35	119.50
546	35.85	27.58	1.25	5.84	50.05	119.66
547	35.90	27.40	1.27	5.84	50.17	119.74
548	35.96	27.76	1.28	5.84	50.30	119.73
549	36.04	27.67	1.23	5.75	50.32	119.68
550	36.11	27.49	1.18	5.84	50.21	119.57
551	36.16	27.40	1.13	5.75	49.91	119.44
552	36.25	26.77	1.11	5.84	49.42	119.29
553	36.31	26.77	1.10	5.84	48.99	119.13
554	36.36	26.77	1.09	5.84	48.78	119.04
555	36.44	27.67	1.06	5.84	48.68	119.01
556	36.50	28.38	1.05	5.84	48.75	119.00
557	36.56	28.11	1.05	5.84	48.80	118.98
558	36.65	27.85	1.11	5.84	48.87	118.95
559	36.68	27.85	1.13	5.84	49.00	118.90
560	36.76	27.04	1.12	5.84	49.40	118.81
561	36.84	26.41	1.09	5.84	49.85	118.68
562	36.91	26.32	1.07	5.84	50.27	118.51
563	36.96	25.52	1.04	5.84	50.49	118.27
564	37.04	24.71	0.98	5.84	50.62	117.99
565	37.10	24.71	0.93	5.84	50.54	117.71
566	37.15	24.08	0.88	5.94	50.34	117.43
567	37.23	24.08	0.86	5.94	50.17	117.15
568	37.30	24.17	0.83	5.94	49.92	116.88
569	37.35	24.35	0.82	5.94	49.63	116.65
570	37.45	24.44	0.80	5.94	49.48	116.41
571	37.51	24.26	0.79	5.94	49.35	116.19
572	37.55	23.91	0.77	5.94	49.26	115.94
573	37.62	23.64	0.75	5.94	49.20	115.66
574	37.70	23.10	0.71	5.94	49.08	115.37
575	37.75	22.47	0.68	5.94	48.84	115.08
576	37.80	22.03	0.65	5.94	48.53	114.79

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
577	37.90	21.76	0.60	6.04	48.04	114.50
578	37.95	22.20	0.59	6.04	47.39	114.25
579	38.05	22.74	0.57	6.04	46.69	114.15
580	38.06	22.83	0.56	6.04	45.71	114.18
581	38.15	23.55	0.55	6.04	44.78	114.32
582	38.19	24.17	0.55	6.04	44.02	114.55
583	38.27	25.61	0.62	6.13	43.21	114.83
584	38.34	27.40	0.66	6.13	42.41	115.14
585	38.39	28.20	0.70	6.13	41.68	115.44
586	38.46	28.11	0.72	6.13	41.20	115.77
587	38.55	29.73	0.74	6.13	40.92	116.16
588	38.59	30.89	0.75	6.23	40.58	116.64
589	38.68	30.71	0.74	6.23	40.03	117.29
590	38.75	30.71	0.77	6.23	39.41	118.01
591	38.80	30.98	0.83	6.32	38.58	118.84
592	38.87	34.20	0.99	6.32	37.33	119.73
593	38.95	40.38	1.19	6.42	35.96	120.68
594	38.99	43.25	1.32	6.42	34.70	121.55
595	39.04	47.63	1.50	6.42	33.73	122.26
596	39.11	55.78	1.63	6.42	33.47	122.73
597	39.19	61.78	1.78	6.32	33.39	122.94
598	39.27	62.23	1.79	6.23	33.71	122.83
599	39.33	58.02	1.69	6.23	34.17	122.55
600	39.39	45.66	1.53	6.23	34.70	122.06
601	39.45	40.65	1.31	6.23	35.62	121.35
602	39.53	33.75	1.04	6.32	36.92	120.46
603	39.57	31.43	0.94	6.32	38.31	119.47
604	39.64	30.26	0.80	6.42	39.25	118.45
605	39.72	30.80	0.72	6.51	38.74	117.50
606	39.79	31.16	0.72	6.42	37.70	116.68
607	39.84	32.14	0.73	6.42	36.52	116.11
608	39.93	33.93	0.66	6.42	36.01	115.74
609	39.98	35.37	0.59	6.42	36.09	115.65
610	40.05	36.71	0.54	6.32	37.17	116.36
611	40.09	34.92	0.53	6.42	37.81	117.34
612	40.19	30.35	0.64	6.32	37.49	118.51
613	40.23	28.56	0.74	6.42	36.08	119.99
614	40.34	32.59	1.30	6.61	34.75	121.57
615	40.38	40.83	1.57	6.71	33.86	123.02
616	40.43	53.36	1.80	6.61	33.39	124.34
617	40.50	72.97	2.17	6.42	32.74	125.48
618	40.58	81.57	2.49	6.23	32.19	126.48
619	40.63	80.85	2.64	6.42	31.50	127.20
620	40.70	75.57	2.80	6.32	30.77	127.84
621	40.75	72.88	2.86	6.42	30.28	128.36
622	40.84	69.12	2.92	6.51	30.33	128.71
623	40.88	69.39	2.99	6.61	30.68	128.97
624	40.95	77.81	3.11	6.71	30.93	129.18

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
625	41.03	83.89	3.19	6.71	30.70	129.35
626	41.08	86.58	3.24	6.71	29.71	129.61
627	41.15	84.97	3.36	6.71	27.82	129.91
628	41.23	84.70	3.38	6.71	25.89	130.25
629	41.28	88.37	3.32	6.80	24.34	130.58
630	41.35	105.92	3.44	6.80	22.97	130.92
631	41.43	128.84	3.38	6.71	21.88	131.28
632	41.48	138.60	3.53	6.71	21.07	131.66
633	41.54	143.43	3.75	6.71	20.44	132.08
634	41.62	151.13	3.94	6.71	19.98	132.55
635	41.68	150.06	4.13	6.71	19.79	133.01
636	41.77	143.70	4.49	6.80	19.97	133.45
637	41.82	142.81	4.79	6.90	20.19	133.84
638	41.88	145.49	5.03	6.99	20.42	134.16
639	41.97	152.39	5.37	6.90	20.74	134.42
640	42.01	155.97	5.44	6.90	21.04	134.64
641	42.10	160.62	5.52	6.90	21.07	134.81
642	42.17	159.55	5.50	6.90	20.99	134.92
643	42.22	158.21	5.48	6.90	20.65	135.00
644	42.28	154.00	5.46	6.90	20.19	135.01
645	42.33	157.67	5.43	6.99	19.48	135.02
646	42.41	157.13	5.34	7.09	18.71	134.99
647	42.48	171.19	5.25	6.99	17.82	134.96
648	42.52	179.34	5.18	6.99	16.82	134.93
649	42.60	197.07	5.01	6.80	15.74	134.93
650	42.66	204.41	4.86	6.80	14.77	134.93
651	42.72	213.63	4.77	6.71	13.88	134.91
652	42.81	224.37	4.71	6.71	13.20	134.87
653	42.87	232.88	4.73	6.61	12.64	134.78
654	42.92	235.30	4.74	6.61	12.21	134.57
655	43.00	233.15	4.67	6.61	11.83	134.31
656	43.06	229.39	4.56	6.61	11.55	134.00
657	43.11	221.96	4.31	6.61	11.41	133.66
658	43.18	214.88	3.71	6.51	11.35	133.29
659	43.25	211.12	3.38	6.51	11.35	132.93
660	43.31	203.69	3.17	6.51	11.39	132.62
661	43.39	197.07	3.17	6.51	11.46	132.34
662	43.45	194.56	3.16	6.51	11.60	132.11
663	43.51	194.38	3.32	6.51	11.88	132.03
664	43.61	193.48	3.51	6.61	12.25	132.04
665	43.65	192.05	3.55	6.51	12.65	132.10
666	43.72	184.26	3.55	6.51	13.02	132.13
667	43.81	180.95	3.57	6.32	13.39	132.14
668	43.85	180.68	3.59	6.23	13.75	132.10
669	43.92	176.02	3.59	5.94	14.15	131.96
670	44.01	170.92	3.47	5.94	14.56	131.81
671	44.05	167.43	3.38	5.94	14.76	131.55
672	44.10	161.70	3.33	5.84	14.75	131.09

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
673	44.20	151.58	3.19	5.84	14.78	130.59
674	44.25	149.43	3.20	5.84	14.83	130.11
675	44.30	147.37	2.72	5.84	15.06	129.70
676	44.40	141.37	1.99	5.84	15.54	129.35
677	44.45	137.79	1.99	5.94	16.07	129.04
678	44.50	133.85	2.14	5.94	16.69	128.88
679	44.57	125.53	2.37	5.94	17.42	128.74
680	44.63	113.71	2.55	5.94	18.48	128.78
681	44.69	111.92	2.68	7.19	20.00	129.12
682	44.79	109.32	2.96	7.19	21.58	129.47
683	44.84	105.65	3.06	7.19	23.08	129.79
684	44.89	102.79	3.14	7.19	24.29	130.05
685	44.96	100.10	3.38	7.19	25.09	130.25
686	45.04	99.83	3.52	7.19	25.83	130.40
687	45.09	100.19	3.59	7.19	26.40	130.50
688	45.17	100.55	3.58	7.19	26.83	130.59
689	45.24	100.28	3.48	7.19	27.18	130.68
690	45.28	98.49	3.45	7.19	27.33	130.71
691	45.38	98.49	3.50	7.28	27.50	130.72
692	45.42	98.76	3.53	7.28	27.81	130.69
693	45.49	98.04	3.56	7.28	28.22	130.65
694	45.57	97.86	3.56	7.28	28.67	130.58
695	45.63	96.07	3.58	7.28	29.22	130.42
696	45.69	90.43	3.59	7.28	29.74	130.14
697	45.78	87.74	3.54	7.28	30.49	129.67
698	45.84	85.51	3.36	7.28	31.54	129.05
699	45.89	77.45	3.06	7.28	32.79	128.32
700	45.93	72.34	2.62	7.28	34.27	127.40
701	46.02	60.35	2.10	7.28	35.80	126.34
702	46.08	49.51	1.81	7.28	37.40	125.13
703	46.13	44.77	1.61	7.38	39.14	123.77
704	46.22	37.43	1.29	7.57	40.74	122.36
705	46.28	33.13	1.15	7.86	42.47	121.00
706	46.33	32.14	1.06	7.86	43.82	119.87
707	46.43	31.25	0.89	8.05	44.33	118.91
708	46.47	30.71	0.81	8.14	44.50	118.06
709	46.53	31.25	0.77	8.14	44.28	117.47
710	46.63	30.98	0.75	8.14	43.77	117.02
711	46.67	31.25	0.74	8.14	43.29	116.67
712	46.73	31.34	0.73	8.14	43.13	116.52
713	46.83	30.89	0.72	8.14	43.01	116.47
714	46.87	30.53	0.72	8.14	42.99	116.46
715	46.93	30.53	0.73	8.14	42.90	116.49
716	47.02	30.53	0.76	8.24	42.80	116.51
717	47.08	30.98	0.76	8.24	42.67	116.53
718	47.12	31.34	0.76	8.24	42.63	116.65
719	47.18	32.14	0.77	8.24	42.62	116.79
720	47.27	32.41	0.75	8.33	42.65	116.94

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
721	47.31	32.59	0.74	8.33	42.88	117.12
722	47.39	32.77	0.81	8.33	42.75	117.36
723	47.48	32.77	0.84	8.33	42.48	117.67
724	47.52	32.50	0.85	8.33	42.30	118.02
725	47.59	31.61	0.93	8.33	42.51	118.52
726	47.66	35.37	0.96	8.53	43.01	119.14
727	47.74	37.96	1.03	8.53	43.27	119.70
728	47.79	38.59	1.09	8.53	42.94	120.22
729	47.86	38.68	1.26	8.53	41.89	120.75
730	47.94	38.77	1.43	8.53	40.18	121.27
731	47.99	39.93	1.46	8.53	37.69	121.87
732	48.05	44.14	1.45	8.53	34.89	122.53
733	48.13	50.41	1.45	8.53	32.35	123.21
734	48.19	56.50	1.48	8.53	30.05	123.86
735	48.26	71.99	1.56	8.53	28.27	124.52
736	48.34	85.06	1.72	8.14	27.19	125.16
737	48.39	90.34	1.87	8.05	26.64	125.75
738	48.43	92.94	2.03	8.05	26.70	126.23
739	48.51	91.77	2.33	8.05	27.25	126.58
740	48.58	84.25	2.50	8.05	28.52	126.79
741	48.63	78.25	2.53	8.05	30.57	126.87
742	48.72	67.96	2.48	8.05	32.91	126.85
743	48.78	58.47	2.36	8.24	35.36	126.77
744	48.83	53.27	2.31	8.24	37.45	126.61
745	48.90	46.92	2.31	8.33	38.86	126.50
746	48.99	47.81	2.28	8.43	39.77	126.43
747	49.03	51.03	2.28	8.53	39.58	126.52
748	49.08	56.85	2.31	8.53	38.46	126.74
749	49.17	62.76	2.48	8.43	36.17	127.19
750	49.23	65.18	2.51	8.43	32.73	127.77
751	49.32	72.70	2.65	8.62	28.94	128.46
752	49.35	79.69	2.73	8.62	25.71	129.12
753	49.43	99.92	3.05	8.62	22.94	129.80
754	49.50	124.54	3.20	8.43	20.51	130.40
755	49.58	153.10	3.34	8.33	18.51	130.97
756	49.63	164.47	3.42	8.24	16.87	131.52
757	49.72	180.59	3.57	8.14	15.55	132.03
758	49.78	193.39	3.64	8.14	14.55	132.42
759	49.83	197.78	3.70	8.05	13.89	132.74
760	49.90	203.69	3.88	8.05	13.57	132.98
761	49.98	206.91	4.00	8.05	13.35	133.17
762	50.02	207.90	4.06	7.95	13.24	133.30
763	50.08	207.72	4.10	7.95	12.96	133.19
764	50.18	205.39	4.12	7.86	12.67	133.02
765	50.23	204.32	4.08	7.86	12.40	132.84
766	50.27	204.76	4.01	7.86	12.15	132.65
767	50.36	205.66	3.03	7.86	11.95	132.49
768	50.40	206.38	2.86	7.86	11.75	132.33

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
769	50.47	207.72	3.00	7.86	11.57	132.20
770	50.55	209.15	3.16	7.86	11.42	132.11
771	50.63	209.24	3.34	7.86	11.32	132.06
772	50.67	208.93	3.43	7.76	11.55	132.27
773	50.72	208.93	3.55	8.24	11.90	132.57
774	50.83	208.62	3.68	8.24	12.26	132.83
775	50.88	208.88	3.76	8.24	12.59	133.06
776	50.93	208.35	3.91	8.24	12.89	133.25
777	51.02	207.18	4.12	8.24	13.16	133.40
778	51.08	206.02	4.19	8.24	13.39	133.53
779	51.12	205.12	4.23	8.14	13.55	133.61
780	51.21	203.69	4.25	8.14	13.66	133.65
781	51.27	203.78	4.23	8.14	13.69	133.65
782	51.32	203.96	4.21	8.05	13.65	133.62
783	51.39	204.32	4.13	8.05	13.61	133.58
784	51.47	204.94	3.99	8.05	13.57	133.55
785	51.55	206.38	3.92	8.05	13.55	133.54
786	51.60	206.65	3.93	8.05	13.57	133.53
787	51.67	206.38	4.00	8.05	13.62	133.52
788	51.72	206.02	4.08	8.05	13.66	133.47
789	51.79	204.32	4.19	8.05	13.66	133.29
790	51.87	201.72	4.20	8.05	13.73	133.13
791	51.91	200.02	4.20	8.05	13.86	133.01
792	51.98	194.74	3.91	8.05	14.03	132.83
793	52.06	186.41	3.25	8.05	14.30	132.64
794	52.12	183.81	3.31	8.05	14.51	132.39
795	52.17	183.10	3.50	8.05	14.93	132.16
796	52.26	174.06	3.36	8.05	15.60	131.93
797	52.31	165.82	3.46	8.05	16.35	131.78
798	52.38	164.21	3.33	8.33	17.40	131.68
799	52.47	149.79	3.55	8.33	18.61	131.48
800	52.51	132.51	3.64	8.43	20.11	131.12
801	52.56	134.30	3.69	8.43	21.88	130.67
802	52.66	116.48	3.34	8.43	23.82	130.13
803	52.70	102.96	3.07	8.72	26.33	129.51
804	52.77	83.63	2.77	8.81	28.86	128.76
805	52.87	68.94	2.44	9.00	31.13	127.85
806	52.92	62.14	2.27	9.10	33.94	126.77
807	52.97	52.47	2.08	9.39	36.53	125.73
808	53.02	47.90	1.91	9.48	38.82	124.63
809	53.10	44.95	1.58	9.58	40.24	123.61
810	53.16	43.25	1.44	9.77	40.99	122.68
811	53.22	44.05	1.33	9.87	41.28	121.68
812	53.31	42.98	1.07	9.96	40.84	120.71
813	53.36	42.62	1.00	9.96	40.23	119.77
814	53.42	40.47	0.93	10.06	39.83	118.95
815	53.51	38.59	0.75	10.15	39.41	118.18
816	53.56	37.78	0.72	10.15	39.23	117.47

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
817	53.62	35.81	0.71	10.15	39.25	116.97
818	53.71	34.02	0.66	10.25	39.46	116.57
819	53.75	33.98	0.65	10.35	39.64	116.26
820	53.83	33.93	0.67	11.02	40.33	116.16
821	53.91	35.10	0.65	11.02	41.15	116.04
822	53.98	35.10	0.69	11.02	42.08	115.86
823	54.01	34.56	0.70	11.02	42.96	115.69
824	54.11	32.23	0.71	10.92	44.08	115.44
825	54.15	30.35	0.67	10.92	45.12	115.07
826	54.21	27.13	0.62	10.92	46.42	114.64
827	54.27	25.88	0.57	10.92	47.77	114.03
828	54.35	24.00	0.52	10.92	49.06	113.31
829	54.42	23.37	0.46	10.92	49.94	112.51
830	54.46	22.92	0.41	10.92	50.58	111.71
831	54.55	21.49	0.35	10.92	50.75	110.95
832	54.60	21.22	0.32	10.92	50.77	110.25
833	54.67	20.77	0.30	11.02	50.47	109.61
834	54.74	20.59	0.29	11.02	50.26	109.08
835	54.79	20.23	0.28	11.02	50.17	108.67
836	54.86	20.23	0.28	11.02	50.09	108.42
837	54.96	20.32	0.27	11.11	50.12	108.27
838	55.03	20.32	0.27	11.11	50.13	108.17
839	55.06	20.32	0.27	11.11	50.14	108.10
840	55.14	20.15	0.27	11.11	50.10	108.04
841	55.21	20.15	0.27	11.11	50.05	107.98
842	55.25	20.15	0.27	11.11	50.04	107.91
843	55.32	20.15	0.27	11.21	50.02	107.85
844	55.41	20.06	0.26	11.21	50.02	107.78
845	55.45	20.06	0.26	11.21	50.00	107.75
846	55.52	19.97	0.25	11.21	50.03	107.75
847	55.61	20.06	0.25	11.21	50.02	107.79
848	55.65	19.97	0.25	11.21	49.96	108.06
849	55.71	20.06	0.26	11.30	49.75	108.43
850	55.80	20.15	0.27	11.30	49.33	108.86
851	55.86	20.59	0.28	11.30	48.59	109.37
852	55.95	22.29	0.35	11.40	47.99	109.93
853	56.00	23.55	0.37	11.40	47.42	110.48
854	56.05	24.89	0.39	11.40	46.94	111.02
855	56.11	26.86	0.41	11.40	46.06	111.37
856	56.20	27.13	0.44	11.40	45.09	111.59
857	56.24	27.13	0.45	11.49	44.18	111.62
858	56.31	27.04	0.47	11.49	43.58	111.61
859	56.39	27.58	0.40	11.49	43.34	111.52
860	56.43	27.58	0.35	11.49	43.42	111.33
861	56.50	27.31	0.34	11.49	44.00	110.98
862	56.60	26.77	0.35	11.49	44.54	110.58
863	56.66	25.34	0.34	11.49	44.87	110.07
864	56.70	24.62	0.33	11.49	45.53	109.67

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
865	56.79	20.86	0.31	12.17	46.32	109.37
866	56.84	20.86	0.30	12.26	47.17	109.15
867	56.92	20.86	0.28	12.26	47.98	109.04
868	56.99	21.13	0.27	12.36	48.35	109.06
869	57.03	21.67	0.26	12.36	48.23	109.18
870	57.09	21.94	0.28	12.36	47.24	109.55
871	57.18	22.74	0.33	12.45	46.58	110.01
872	57.23	24.00	0.35	12.55	46.33	110.77
873	57.31	26.14	0.37	12.55	46.35	111.91
874	57.38	28.02	0.42	12.55	46.30	113.17
875	57.43	27.67	0.45	12.65	45.29	114.60
876	57.50	28.74	0.57	12.74	42.99	116.26
877	57.58	31.87	0.77	12.84	40.03	117.84
878	57.62	34.74	0.89	12.84	36.29	119.42
879	57.68	43.42	1.09	12.74	33.01	120.96
880	57.78	58.38	1.40	12.74	30.13	122.36
881	57.82	69.84	1.51	12.74	27.45	123.64
882	57.89	89.18	1.67	12.55	25.13	124.69
883	57.97	99.92	1.91	12.26	23.27	125.58
884	58.02	106.28	2.01	12.36	21.94	126.30
885	58.09	116.39	2.17	12.26	21.20	126.80
886	58.17	120.24	2.20	12.26	20.90	127.18
887	58.23	119.89	2.22	12.17	21.05	127.45
888	58.28	116.22	2.27	12.07	21.42	127.65
889	58.37	107.44	2.29	11.97	22.04	127.81
890	58.43	100.46	2.28	12.07	22.92	127.88
891	58.48	99.03	2.32	11.97	24.25	127.82
892	58.57	97.86	2.46	12.07	25.87	127.73
893	58.62	94.55	2.55	12.07	27.88	127.57
894	58.67	91.68	2.55	12.07	30.00	127.33
895	58.78	76.46	2.36	12.17	32.21	127.05
896	58.82	70.19	2.35	12.17	34.75	126.68
897	58.88	58.82	2.31	12.17	37.58	126.23
898	58.97	49.78	2.11	12.36	40.34	125.62
899	59.01	46.47	2.01	12.45	43.15	124.98
900	59.07	41.99	1.88	12.55	45.18	124.48
901	59.12	40.74	1.85	12.65	47.24	123.90
902	59.19	41.19	1.55	12.65	48.60	123.28
903	59.27	43.69	1.55	12.65	48.89	122.73
904	59.32	44.50	1.56	12.65	49.24	122.18
905	59.42	39.22	1.43	12.65	48.90	121.78
906	59.47	35.46	1.30	12.65	48.51	121.37
907	59.52	37.25	1.16	13.03	48.35	121.11
908	59.58	33.93	1.13	13.12	47.90	120.83
909	59.68	37.60	1.22	13.32	47.63	120.55
910	59.74	36.44	1.20	13.41	47.29	120.44
911	59.78	37.96	1.16	13.41	44.73	119.52
912	59.88	42.17	1.12	13.32	42.58	118.56

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
913	59.93	42.08	1.17	13.32	39.80	117.52
914	60.00	39.93	1.26	13.32	35.84	116.24
915	60.05	38.77	0.00	13.32	30.73	114.75
916	60.13	38.05	0.00	13.41	25.69	112.85
917	60.18	39.22	0.00	13.41	22.61	110.06
918	60.25	51.03	0.00	13.51	5.00	105.37
919	60.33	62.94	0.00	13.41	N/A	87.36
920	60.38	66.70	0.00	13.32	N/A	87.36

Abbreviations

Depth: Depth from free surface, at which CPT was performed (ft)
q_c: Measured cone resistance (tsf)
f_s: Sleeve friction resistance (tsf)
u: Pore pressure (tsf)
Fines content: Percentage of fines in soil (%)
Unit weight: Bulk soil unit weight (pcf)

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data ::

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
1	0.10	0.01	0.00	0.01	1.00	0.358	1.34	0.266	1.00	1.00	2.000	No
2	0.16	0.01	0.00	0.01	1.00	0.358	1.34	0.266	1.00	1.00	2.000	No
3	0.21	0.01	0.00	0.01	1.00	0.358	1.34	0.266	1.00	1.00	2.000	No
4	0.29	0.02	0.00	0.02	1.00	0.358	1.34	0.266	1.00	1.00	2.000	No
5	0.36	0.02	0.00	0.02	1.00	0.358	1.34	0.266	1.00	1.00	2.000	No
6	0.40	0.02	0.00	0.02	1.00	0.358	1.34	0.266	1.00	1.00	2.000	No
7	0.51	0.03	0.00	0.03	1.00	0.358	1.34	0.266	1.00	1.00	2.000	No
8	0.57	0.03	0.00	0.03	1.00	0.358	1.34	0.266	1.00	1.00	2.000	No
9	0.61	0.03	0.00	0.03	1.00	0.358	1.34	0.266	1.00	1.00	2.000	No
10	0.70	0.04	0.00	0.04	1.00	0.358	1.34	0.266	1.00	1.00	2.000	No
11	0.76	0.04	0.00	0.04	1.00	0.358	1.34	0.266	1.00	1.00	2.000	No
12	0.81	0.04	0.00	0.04	1.00	0.357	1.34	0.266	1.00	1.00	2.000	No
13	0.87	0.05	0.00	0.05	1.00	0.357	1.34	0.266	1.00	1.00	2.000	No
14	0.96	0.05	0.00	0.05	1.00	0.357	1.34	0.266	1.00	1.00	2.000	No
15	1.00	0.05	0.00	0.05	1.00	0.357	1.34	0.266	1.00	1.00	2.000	No
16	1.05	0.06	0.00	0.06	1.00	0.357	1.34	0.266	1.00	1.00	2.000	No
17	1.16	0.06	0.00	0.06	1.00	0.357	1.34	0.266	1.00	1.00	2.000	No
18	1.20	0.07	0.00	0.07	1.00	0.357	1.34	0.266	1.00	1.00	2.000	No
19	1.26	0.07	0.00	0.07	1.00	0.357	1.34	0.266	1.00	1.00	2.000	No
20	1.35	0.08	0.00	0.08	1.00	0.357	1.34	0.266	1.00	1.00	2.000	No
21	1.40	0.08	0.00	0.08	1.00	0.357	1.34	0.266	1.00	1.00	2.000	No
22	1.45	0.08	0.00	0.08	1.00	0.357	1.34	0.266	1.00	1.00	2.000	No
23	1.55	0.09	0.00	0.09	1.00	0.357	1.34	0.265	1.00	1.00	2.000	Yes
24	1.60	0.09	0.00	0.09	1.00	0.357	1.34	0.265	1.00	1.00	2.000	Yes
25	1.64	0.09	0.00	0.09	1.00	0.357	1.34	0.265	1.00	1.00	2.000	Yes
26	1.71	0.10	0.00	0.10	1.00	0.357	1.34	0.265	1.00	1.00	2.000	Yes
27	1.79	0.10	0.00	0.10	1.00	0.357	1.34	0.265	1.00	1.00	2.000	Yes
28	1.87	0.11	0.00	0.11	1.00	0.357	1.34	0.265	1.00	1.00	2.000	Yes
29	1.95	0.11	0.00	0.11	1.00	0.357	1.34	0.265	1.00	1.00	2.000	Yes
30	2.00	0.11	0.00	0.11	1.00	0.357	1.34	0.265	1.00	1.00	2.000	Yes
31	2.04	0.12	0.00	0.12	1.00	0.357	1.34	0.265	1.00	1.00	2.000	Yes
32	2.11	0.12	0.00	0.12	1.00	0.356	1.34	0.265	1.00	1.00	2.000	Yes
33	2.19	0.12	0.00	0.12	1.00	0.356	1.34	0.265	1.00	1.00	2.000	Yes
34	2.24	0.13	0.00	0.13	1.00	0.356	1.34	0.265	1.00	1.00	2.000	Yes
35	2.30	0.13	0.00	0.13	1.00	0.356	1.34	0.265	1.00	1.00	2.000	Yes
36	2.38	0.14	0.00	0.14	1.00	0.356	1.34	0.265	1.00	1.00	2.000	Yes
37	2.45	0.14	0.00	0.14	1.00	0.356	1.34	0.265	1.00	1.00	2.000	Yes
38	2.50	0.14	0.00	0.14	1.00	0.356	1.34	0.265	1.00	1.00	2.000	Yes
39	2.58	0.15	0.00	0.15	1.00	0.356	1.34	0.265	1.00	1.00	2.000	No
40	2.64	0.15	0.00	0.15	1.00	0.356	1.34	0.265	1.00	1.00	2.000	No
41	2.69	0.15	0.00	0.15	1.00	0.356	1.34	0.265	1.00	1.00	2.000	No
42	2.79	0.16	0.00	0.16	1.00	0.356	1.34	0.265	1.00	1.00	2.000	No
43	2.85	0.16	0.00	0.16	1.00	0.356	1.34	0.265	1.00	1.00	2.000	No
44	2.90	0.16	0.00	0.16	1.00	0.356	1.34	0.265	1.00	1.00	2.000	No
45	2.98	0.17	0.00	0.17	1.00	0.356	1.34	0.265	1.00	1.00	2.000	No
46	3.05	0.17	0.00	0.17	0.99	0.356	1.34	0.265	1.00	1.00	2.000	No
47	3.09	0.18	0.00	0.18	0.99	0.356	1.34	0.264	1.00	1.00	2.000	No
48	3.17	0.18	0.00	0.18	0.99	0.356	1.34	0.264	1.00	1.00	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
49	3.24	0.18	0.00	0.18	0.99	0.355	1.34	0.264	1.00	1.00	2.000	No
50	3.29	0.19	0.00	0.19	0.99	0.355	1.34	0.264	1.00	1.00	2.000	No
51	3.36	0.19	0.00	0.19	0.99	0.355	1.34	0.264	1.00	1.00	2.000	No
52	3.44	0.19	0.00	0.19	0.99	0.355	1.34	0.264	1.00	1.00	2.000	No
53	3.48	0.20	0.00	0.20	0.99	0.355	1.34	0.264	1.00	1.00	2.000	No
54	3.56	0.20	0.00	0.20	0.99	0.355	1.34	0.264	1.00	1.00	2.000	No
55	3.64	0.20	0.00	0.20	0.99	0.355	1.34	0.264	1.00	1.00	2.000	No
56	3.69	0.21	0.00	0.21	0.99	0.355	1.34	0.264	1.00	1.00	2.000	No
57	3.76	0.21	0.00	0.21	0.99	0.355	1.34	0.264	1.00	1.00	2.000	No
58	3.84	0.22	0.00	0.22	0.99	0.355	1.34	0.264	1.00	1.00	2.000	No
59	3.88	0.22	0.00	0.22	0.99	0.355	1.34	0.264	1.00	1.00	2.000	No
60	3.98	0.22	0.00	0.22	0.99	0.355	1.34	0.264	1.00	1.00	2.000	No
61	4.03	0.23	0.00	0.23	0.99	0.355	1.34	0.264	1.00	1.00	2.000	No
62	4.08	0.23	0.00	0.23	0.99	0.355	1.34	0.264	1.00	1.00	2.000	No
63	4.14	0.23	0.00	0.23	0.99	0.355	1.34	0.264	1.00	1.00	2.000	No
64	4.23	0.24	0.00	0.24	0.99	0.355	1.34	0.264	1.00	1.00	2.000	No
65	4.27	0.24	0.00	0.24	0.99	0.355	1.34	0.264	1.00	1.00	2.000	No
66	4.36	0.25	0.00	0.25	0.99	0.355	1.34	0.264	1.00	1.00	2.000	No
67	4.41	0.25	0.00	0.25	0.99	0.355	1.34	0.264	1.00	1.00	2.000	No
68	4.46	0.25	0.00	0.25	0.99	0.354	1.34	0.264	1.00	1.00	2.000	No
69	4.55	0.26	0.00	0.26	0.99	0.354	1.34	0.264	1.00	1.00	2.000	No
70	4.61	0.26	0.00	0.26	0.99	0.354	1.34	0.264	1.00	1.00	2.000	No
71	4.66	0.26	0.00	0.26	0.99	0.354	1.34	0.264	1.00	1.00	2.000	No
72	4.75	0.27	0.00	0.27	0.99	0.354	1.34	0.263	1.00	1.00	2.000	No
73	4.80	0.27	0.00	0.27	0.99	0.354	1.34	0.263	1.00	1.00	2.000	No
74	4.86	0.27	0.00	0.27	0.99	0.354	1.34	0.263	1.00	1.00	2.000	No
75	4.96	0.28	0.00	0.28	0.99	0.354	1.34	0.263	1.00	1.00	2.000	No
76	5.01	0.28	0.00	0.28	0.99	0.354	1.34	0.263	1.00	1.00	2.000	No
77	5.06	0.28	0.00	0.28	0.99	0.354	1.34	0.263	1.00	1.00	2.000	No
78	5.16	0.29	0.00	0.29	0.99	0.354	1.34	0.263	1.00	1.00	2.000	No
79	5.21	0.29	0.00	0.29	0.99	0.354	1.34	0.263	1.00	1.00	2.000	No
80	5.26	0.30	0.00	0.30	0.99	0.354	1.34	0.263	1.00	1.00	2.000	No
81	5.32	0.30	0.00	0.30	0.99	0.354	1.34	0.263	1.00	1.00	2.000	No
82	5.41	0.30	0.00	0.30	0.99	0.354	1.34	0.263	1.00	1.00	2.000	No
83	5.46	0.31	0.00	0.31	0.99	0.354	1.34	0.263	1.00	1.00	2.000	No
84	5.52	0.31	0.00	0.31	0.99	0.354	1.34	0.263	1.00	1.00	2.000	No
85	5.60	0.31	0.00	0.31	0.99	0.354	1.34	0.263	1.00	1.00	2.000	No
86	5.66	0.32	0.00	0.32	0.99	0.353	1.34	0.263	1.00	1.00	2.000	No
87	5.71	0.32	0.00	0.32	0.99	0.353	1.34	0.263	1.00	1.00	2.000	No
88	5.81	0.33	0.00	0.33	0.99	0.353	1.34	0.263	1.00	1.00	2.000	No
89	5.89	0.33	0.00	0.33	0.99	0.353	1.34	0.263	1.00	1.00	2.000	No
90	5.91	0.33	0.00	0.33	0.99	0.353	1.34	0.263	1.00	1.00	2.000	No
91	6.00	0.34	0.00	0.34	0.99	0.353	1.34	0.263	1.00	1.00	2.000	No
92	6.06	0.34	0.00	0.34	0.99	0.353	1.34	0.263	1.00	1.00	2.000	No
93	6.11	0.34	0.00	0.34	0.99	0.353	1.34	0.263	1.00	1.00	2.000	No
94	6.20	0.35	0.00	0.35	0.99	0.353	1.34	0.263	1.00	1.00	2.000	No
95	6.24	0.35	0.00	0.35	0.99	0.353	1.34	0.263	1.00	1.00	2.000	No
96	6.30	0.35	0.00	0.35	0.99	0.353	1.34	0.263	1.00	1.00	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
97	6.38	0.36	0.00	0.36	0.99	0.353	1.34	0.262	1.00	1.00	2.000	No
98	6.46	0.36	0.00	0.36	0.99	0.353	1.34	0.262	1.00	1.00	2.000	No
99	6.50	0.36	0.00	0.36	0.99	0.353	1.34	0.262	1.00	1.00	2.000	No
100	6.60	0.37	0.00	0.37	0.99	0.353	1.34	0.262	1.00	1.00	2.000	No
101	6.63	0.37	0.00	0.37	0.99	0.353	1.34	0.262	1.00	1.00	2.000	No
102	6.72	0.38	0.00	0.38	0.99	0.353	1.34	0.262	1.00	1.00	2.000	No
103	6.80	0.38	0.00	0.38	0.99	0.353	1.34	0.262	1.00	1.00	2.000	No
104	6.84	0.38	0.00	0.38	0.99	0.353	1.34	0.262	1.00	1.00	2.000	No
105	6.90	0.39	0.00	0.39	0.99	0.352	1.34	0.262	1.00	1.00	2.000	No
106	7.00	0.39	0.00	0.39	0.99	0.352	1.34	0.262	1.00	1.00	2.000	No
107	7.04	0.39	0.00	0.39	0.99	0.352	1.34	0.262	1.00	1.00	2.000	No
108	7.09	0.40	0.00	0.40	0.99	0.352	1.34	0.262	1.00	1.00	2.000	No
109	7.20	0.40	0.00	0.40	0.99	0.352	1.34	0.262	1.00	1.00	2.000	No
110	7.24	0.41	0.00	0.41	0.99	0.352	1.34	0.262	1.00	1.00	2.000	No
111	7.30	0.41	0.00	0.41	0.99	0.352	1.34	0.262	1.00	1.00	2.000	No
112	7.39	0.41	0.00	0.41	0.98	0.352	1.34	0.262	1.00	1.00	2.000	No
113	7.43	0.42	0.00	0.42	0.98	0.352	1.34	0.262	1.00	1.00	2.000	No
114	7.50	0.42	0.00	0.42	0.98	0.352	1.34	0.262	1.00	1.00	2.000	No
115	7.59	0.42	0.00	0.42	0.98	0.352	1.34	0.262	1.00	1.00	2.000	No
116	7.64	0.43	0.00	0.43	0.98	0.352	1.34	0.262	1.00	1.00	2.000	No
117	7.70	0.43	0.00	0.43	0.98	0.352	1.34	0.262	1.00	1.00	2.000	No
118	7.79	0.44	0.00	0.44	0.98	0.352	1.34	0.262	1.00	1.00	2.000	No
119	7.83	0.44	0.00	0.44	0.98	0.352	1.34	0.262	1.00	1.00	2.000	No
120	7.90	0.44	0.00	0.44	0.98	0.352	1.34	0.262	1.00	1.00	2.000	No
121	7.94	0.44	0.00	0.44	0.98	0.352	1.34	0.262	1.00	1.00	2.000	No
122	8.03	0.45	0.00	0.45	0.98	0.352	1.34	0.261	1.00	1.00	2.000	No
123	8.11	0.45	0.00	0.45	0.98	0.352	1.34	0.261	1.00	1.00	2.000	No
124	8.17	0.46	0.00	0.46	0.98	0.351	1.34	0.261	1.00	1.00	2.000	No
125	8.21	0.46	0.00	0.46	0.98	0.351	1.34	0.261	1.00	1.00	2.000	No
126	8.28	0.46	0.00	0.46	0.98	0.351	1.34	0.261	1.00	1.00	2.000	No
127	8.37	0.47	0.00	0.47	0.98	0.351	1.34	0.261	1.00	1.00	2.000	No
128	8.41	0.47	0.00	0.47	0.98	0.351	1.34	0.261	1.00	1.00	2.000	No
129	8.48	0.47	0.00	0.47	0.98	0.351	1.34	0.261	1.00	1.00	2.000	No
130	8.57	0.48	0.00	0.48	0.98	0.351	1.34	0.261	1.00	1.00	2.000	No
131	8.61	0.48	0.00	0.48	0.98	0.351	1.34	0.261	1.00	1.00	2.000	No
132	8.67	0.48	0.00	0.48	0.98	0.351	1.34	0.261	1.00	1.00	2.000	No
133	8.77	0.49	0.00	0.49	0.98	0.351	1.34	0.261	1.00	1.00	2.000	No
134	8.81	0.49	0.00	0.49	0.98	0.351	1.34	0.261	1.00	1.00	2.000	No
135	8.87	0.49	0.00	0.49	0.98	0.351	1.34	0.261	1.00	1.00	2.000	No
136	8.96	0.50	0.00	0.50	0.98	0.351	1.34	0.261	1.00	1.00	2.000	No
137	8.99	0.50	0.00	0.50	0.98	0.351	1.34	0.261	1.00	1.00	2.000	No
138	9.07	0.50	0.00	0.50	0.98	0.352	1.34	0.262	1.00	1.00	0.262	No
139	9.16	0.51	0.00	0.50	0.98	0.354	1.34	0.263	1.00	1.00	0.263	No
140	9.21	0.51	0.01	0.50	0.98	0.355	1.34	0.264	1.00	1.00	0.264	No
141	9.27	0.51	0.01	0.51	0.98	0.356	1.34	0.265	1.00	1.00	0.265	No
142	9.36	0.52	0.01	0.51	0.98	0.358	1.34	0.266	1.00	1.00	0.266	No
143	9.40	0.52	0.01	0.51	0.98	0.359	1.34	0.267	1.00	1.00	0.267	No
144	9.48	0.52	0.01	0.51	0.98	0.361	1.34	0.268	1.00	1.00	0.268	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
145	9.52	0.53	0.02	0.51	0.98	0.362	1.34	0.269	1.00	1.00	0.269	No
146	9.61	0.53	0.02	0.51	0.98	0.363	1.34	0.270	1.00	1.00	0.270	No
147	9.65	0.53	0.02	0.51	0.98	0.364	1.34	0.271	1.00	1.00	0.271	No
148	9.72	0.54	0.02	0.51	0.98	0.366	1.34	0.272	1.00	1.00	0.272	No
149	9.81	0.54	0.03	0.52	0.98	0.367	1.34	0.273	1.00	1.00	0.273	No
150	9.86	0.54	0.03	0.52	0.98	0.368	1.34	0.274	1.00	1.00	0.274	No
151	9.91	0.55	0.03	0.52	0.98	0.369	1.34	0.275	1.00	1.00	0.275	No
152	10.00	0.55	0.03	0.52	0.98	0.371	1.34	0.276	1.00	1.00	0.276	No
153	10.05	0.56	0.03	0.52	0.98	0.372	1.34	0.277	1.00	1.00	0.277	No
154	10.16	0.56	0.04	0.53	0.98	0.374	1.34	0.278	1.00	1.00	0.278	No
155	10.20	0.56	0.04	0.53	0.98	0.375	1.34	0.279	1.00	1.00	0.279	No
156	10.25	0.57	0.04	0.53	0.98	0.376	1.34	0.279	1.00	1.00	0.279	No
157	10.31	0.57	0.04	0.53	0.98	0.377	1.34	0.280	1.00	1.00	0.280	No
158	10.40	0.57	0.04	0.53	0.98	0.378	1.34	0.282	1.00	1.00	0.282	No
159	10.44	0.58	0.04	0.53	0.98	0.379	1.34	0.282	1.00	1.00	0.282	No
160	10.51	0.58	0.05	0.53	0.98	0.380	1.34	0.283	1.00	1.00	0.283	No
161	10.59	0.59	0.05	0.54	0.98	0.382	1.34	0.284	1.00	1.00	0.284	No
162	10.65	0.59	0.05	0.54	0.98	0.383	1.34	0.285	1.00	1.00	0.285	No
163	10.71	0.59	0.05	0.54	0.98	0.384	1.34	0.286	1.00	1.00	0.286	No
164	10.80	0.60	0.06	0.54	0.98	0.386	1.34	0.287	1.00	1.00	0.287	No
165	10.85	0.60	0.06	0.54	0.98	0.387	1.34	0.287	1.00	1.00	0.287	No
166	10.90	0.60	0.06	0.54	0.98	0.387	1.34	0.288	1.00	1.00	0.288	No
167	10.96	0.61	0.06	0.55	0.98	0.388	1.34	0.289	1.00	1.00	0.289	No
168	11.04	0.61	0.06	0.55	0.98	0.390	1.34	0.290	1.00	1.00	0.290	No
169	11.10	0.62	0.07	0.55	0.98	0.391	1.34	0.291	1.00	1.00	0.291	No
170	11.18	0.62	0.07	0.55	0.98	0.392	1.34	0.292	1.00	1.00	0.292	No
171	11.24	0.62	0.07	0.55	0.98	0.393	1.34	0.292	1.00	1.00	0.292	No
172	11.30	0.63	0.07	0.56	0.98	0.394	1.34	0.293	1.00	1.00	0.293	No
173	11.35	0.63	0.07	0.56	0.98	0.395	1.34	0.294	1.00	1.00	0.294	No
174	11.42	0.63	0.08	0.56	0.98	0.396	1.34	0.295	1.00	1.00	0.295	No
175	11.51	0.64	0.08	0.56	0.98	0.398	1.34	0.296	1.00	1.00	0.296	No
176	11.55	0.64	0.08	0.56	0.98	0.398	1.34	0.296	1.00	1.00	0.296	No
177	11.62	0.65	0.08	0.56	0.98	0.399	1.34	0.297	1.00	1.00	0.297	No
178	11.71	0.65	0.08	0.57	0.98	0.401	1.34	0.298	1.00	1.00	0.298	No
179	11.75	0.65	0.09	0.57	0.98	0.401	1.34	0.299	1.00	1.00	0.299	No
180	11.85	0.66	0.09	0.57	0.98	0.403	1.34	0.300	1.00	1.00	0.300	No
181	11.90	0.66	0.09	0.57	0.98	0.404	1.34	0.300	1.00	1.00	0.300	No
182	11.94	0.66	0.09	0.57	0.98	0.404	1.34	0.301	1.00	1.00	0.301	No
183	12.02	0.67	0.09	0.57	0.97	0.406	1.34	0.302	1.00	1.00	0.302	No
184	12.10	0.67	0.10	0.58	0.97	0.407	1.34	0.303	1.00	1.00	0.303	No
185	12.15	0.68	0.10	0.58	0.97	0.408	1.34	0.303	1.00	1.00	0.303	No
186	12.24	0.68	0.10	0.58	0.97	0.409	1.34	0.304	1.00	1.00	0.304	No
187	12.30	0.69	0.10	0.58	0.97	0.410	1.34	0.305	1.00	1.00	0.305	No
188	12.35	0.69	0.10	0.58	0.97	0.411	1.34	0.305	1.00	1.00	0.305	No
189	12.44	0.69	0.11	0.59	0.97	0.412	1.34	0.306	1.00	1.00	0.306	No
190	12.50	0.70	0.11	0.59	0.97	0.413	1.34	0.307	1.00	1.00	0.307	No
191	12.55	0.70	0.11	0.59	0.97	0.414	1.34	0.308	1.00	1.00	0.308	No
192	12.63	0.70	0.11	0.59	0.97	0.415	1.34	0.308	1.00	1.00	0.308	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
193	12.70	0.71	0.12	0.59	0.97	0.416	1.34	0.309	1.00	1.00	0.309	No
194	12.74	0.71	0.12	0.59	0.97	0.416	1.34	0.310	1.00	1.00	0.310	No
195	12.84	0.72	0.12	0.60	0.97	0.418	1.34	0.311	1.00	1.00	0.311	No
196	12.86	0.72	0.12	0.60	0.97	0.418	1.34	0.311	1.00	1.00	0.311	No
197	12.94	0.72	0.12	0.60	0.97	0.419	1.34	0.312	1.00	1.00	0.312	No
198	13.01	0.73	0.13	0.60	0.97	0.420	1.34	0.313	1.00	1.00	0.313	No
199	13.09	0.73	0.13	0.60	0.97	0.421	1.34	0.313	1.00	1.00	0.313	No
200	13.14	0.73	0.13	0.60	0.97	0.422	1.34	0.314	1.00	1.00	0.314	No
201	13.20	0.74	0.13	0.61	0.97	0.423	1.34	0.314	1.00	1.00	0.314	No
202	13.29	0.74	0.13	0.61	0.97	0.424	1.34	0.315	1.00	1.00	0.315	No
203	13.33	0.74	0.14	0.61	0.97	0.425	1.34	0.316	1.00	1.00	0.316	No
204	13.39	0.75	0.14	0.61	0.97	0.425	1.34	0.316	1.00	1.00	0.316	No
205	13.49	0.75	0.14	0.61	0.97	0.427	1.34	0.317	1.00	1.00	0.317	No
206	13.53	0.76	0.14	0.61	0.97	0.427	1.34	0.318	1.00	1.00	0.318	No
207	13.59	0.76	0.14	0.62	0.97	0.428	1.34	0.318	1.00	1.00	0.318	No
208	13.69	0.76	0.15	0.62	0.97	0.429	1.34	0.319	1.00	1.00	0.319	No
209	13.73	0.77	0.15	0.62	0.97	0.430	1.34	0.320	1.00	1.00	0.320	No
210	13.79	0.77	0.15	0.62	0.97	0.431	1.34	0.320	1.00	1.00	0.320	No
211	13.89	0.78	0.15	0.62	0.97	0.432	1.34	0.321	1.00	1.00	0.321	No
212	13.94	0.78	0.15	0.62	0.97	0.433	1.34	0.322	1.00	1.00	0.322	No
213	13.99	0.78	0.16	0.63	0.97	0.433	1.34	0.322	1.00	1.00	0.322	No
214	14.08	0.79	0.16	0.63	0.97	0.434	1.34	0.323	1.00	1.00	0.323	No
215	14.13	0.79	0.16	0.63	0.97	0.435	1.34	0.324	1.00	1.00	0.324	No
216	14.18	0.79	0.16	0.63	0.97	0.436	1.34	0.324	1.00	1.00	0.324	No
217	14.27	0.80	0.16	0.63	0.97	0.437	1.34	0.325	1.00	1.00	0.325	No
218	14.32	0.80	0.17	0.63	0.97	0.438	1.34	0.325	1.00	1.00	0.325	No
219	14.37	0.80	0.17	0.64	0.97	0.438	1.34	0.326	1.00	1.00	0.326	No
220	14.48	0.81	0.17	0.64	0.97	0.440	1.34	0.327	1.00	1.00	0.327	No
221	14.52	0.81	0.17	0.64	0.97	0.440	1.34	0.327	1.00	1.00	0.327	No
222	14.58	0.81	0.17	0.64	0.97	0.441	1.34	0.328	1.00	1.00	0.328	No
223	14.68	0.82	0.18	0.64	0.97	0.442	1.34	0.329	1.00	1.00	0.329	No
224	14.72	0.82	0.18	0.64	0.97	0.443	1.34	0.329	1.00	1.00	0.329	No
225	14.77	0.82	0.18	0.64	0.97	0.443	1.34	0.330	1.00	1.00	0.330	No
226	14.83	0.83	0.18	0.65	0.97	0.444	1.34	0.330	1.00	1.00	0.330	No
227	14.92	0.83	0.18	0.65	0.97	0.445	1.34	0.331	1.00	1.00	0.331	No
228	14.98	0.84	0.19	0.65	0.97	0.446	1.34	0.332	1.00	1.00	0.332	No
229	15.07	0.84	0.19	0.65	0.97	0.447	1.34	0.332	1.00	1.00	0.332	No
230	15.11	0.84	0.19	0.65	0.97	0.447	1.34	0.333	1.00	1.00	0.333	No
231	15.17	0.85	0.19	0.65	0.97	0.448	1.34	0.333	1.00	1.00	0.333	No
232	15.27	0.85	0.20	0.66	0.97	0.449	1.34	0.334	1.00	1.00	0.334	No
233	15.31	0.85	0.20	0.66	0.97	0.450	1.34	0.335	1.00	1.00	0.335	No
234	15.38	0.86	0.20	0.66	0.97	0.451	1.34	0.335	1.00	1.00	0.335	No
235	15.47	0.86	0.20	0.66	0.97	0.452	1.34	0.336	1.00	1.00	0.336	No
236	15.52	0.86	0.20	0.66	0.97	0.452	1.34	0.336	1.00	1.00	0.336	No
237	15.56	0.87	0.20	0.66	0.97	0.453	1.34	0.337	1.00	1.00	0.337	No
238	15.64	0.87	0.21	0.66	0.97	0.454	1.34	0.337	1.00	1.00	0.337	No
239	15.71	0.87	0.21	0.67	0.97	0.454	1.34	0.338	1.00	1.00	0.338	No
240	15.75	0.88	0.21	0.67	0.97	0.455	1.34	0.338	1.00	1.00	0.338	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
241	15.87	0.88	0.21	0.67	0.97	0.456	1.34	0.339	1.00	1.00	0.339	No
242	15.91	0.89	0.22	0.67	0.97	0.457	1.34	0.340	1.00	1.00	0.340	No
243	15.96	0.89	0.22	0.67	0.97	0.457	1.34	0.340	1.00	1.00	0.340	No
244	16.01	0.89	0.22	0.67	0.97	0.458	1.34	0.341	1.00	1.00	0.341	No
245	16.11	0.90	0.22	0.67	0.97	0.459	1.34	0.341	1.00	1.00	0.341	No
246	16.15	0.90	0.22	0.68	0.97	0.459	1.34	0.342	1.00	1.00	0.342	No
247	16.22	0.90	0.23	0.68	0.97	0.460	1.34	0.342	1.00	1.00	0.342	No
248	16.31	0.91	0.23	0.68	0.97	0.461	1.34	0.343	1.00	1.00	0.343	No
249	16.36	0.91	0.23	0.68	0.97	0.462	1.34	0.343	1.00	1.00	0.343	No
250	16.41	0.91	0.23	0.68	0.97	0.462	1.34	0.344	1.00	1.00	0.344	No
251	16.51	0.92	0.23	0.68	0.97	0.463	1.34	0.345	1.00	1.00	0.345	No
252	16.54	0.92	0.24	0.68	0.97	0.464	1.34	0.345	1.00	1.00	0.345	No
253	16.61	0.92	0.24	0.69	0.97	0.464	1.34	0.345	1.00	1.00	0.345	No
254	16.70	0.93	0.24	0.69	0.96	0.465	1.34	0.346	1.00	1.00	0.346	No
255	16.75	0.93	0.24	0.69	0.96	0.466	1.34	0.347	1.00	1.00	0.347	No
256	16.81	0.93	0.24	0.69	0.96	0.467	1.34	0.347	1.00	1.00	0.347	No
257	16.91	0.94	0.25	0.69	0.96	0.468	1.34	0.348	1.00	1.00	0.348	No
258	16.95	0.94	0.25	0.69	0.96	0.468	1.34	0.348	1.00	1.00	0.348	No
259	17.01	0.94	0.25	0.69	0.96	0.469	1.34	0.349	1.00	1.00	0.349	No
260	17.11	0.95	0.25	0.70	0.96	0.470	1.34	0.349	1.00	1.00	0.349	No
261	17.13	0.95	0.25	0.70	0.96	0.470	1.34	0.350	1.00	1.00	0.350	No
262	17.21	0.95	0.26	0.70	0.96	0.471	1.34	0.350	1.00	1.00	0.350	No
263	17.29	0.96	0.26	0.70	0.96	0.472	1.34	0.351	1.00	1.00	0.351	No
264	17.34	0.96	0.26	0.70	0.96	0.472	1.34	0.351	1.00	1.00	0.351	No
265	17.43	0.97	0.26	0.70	0.96	0.473	1.34	0.352	1.00	1.00	0.352	No
266	17.48	0.97	0.26	0.70	0.96	0.474	1.34	0.352	1.00	1.00	0.352	No
267	17.54	0.97	0.27	0.71	0.96	0.474	1.34	0.353	1.00	1.00	0.353	No
268	17.63	0.98	0.27	0.71	0.96	0.475	1.34	0.353	1.00	1.00	0.353	No
269	17.68	0.98	0.27	0.71	0.96	0.476	1.34	0.354	1.00	1.00	0.354	No
270	17.73	0.98	0.27	0.71	0.96	0.476	1.34	0.354	1.00	1.00	0.354	No
271	17.83	0.99	0.28	0.71	0.96	0.477	1.34	0.355	1.00	1.00	0.355	No
272	17.85	0.99	0.28	0.71	0.96	0.477	1.34	0.355	1.00	1.00	0.355	No
273	17.93	0.99	0.28	0.71	0.96	0.478	1.34	0.356	1.00	1.00	0.356	No
274	17.98	1.00	0.28	0.72	0.96	0.479	1.34	0.356	1.00	1.00	0.356	No
275	18.07	1.00	0.28	0.72	0.96	0.479	1.34	0.357	1.00	1.00	0.357	No
276	18.12	1.00	0.28	0.72	0.96	0.480	1.34	0.357	1.00	1.00	0.357	No
277	18.18	1.01	0.29	0.72	0.96	0.480	1.34	0.357	1.00	1.00	0.357	No
278	18.24	1.01	0.29	0.72	0.96	0.481	1.34	0.358	1.00	1.00	0.358	No
279	18.33	1.01	0.29	0.72	0.96	0.482	1.34	0.358	1.00	1.00	0.358	No
280	18.38	1.02	0.29	0.72	0.96	0.482	1.34	0.359	1.00	1.00	0.359	No
281	18.47	1.02	0.30	0.73	0.96	0.483	1.34	0.359	1.00	1.00	0.359	No
282	18.53	1.02	0.30	0.73	0.96	0.484	1.34	0.360	1.00	1.00	0.360	No
283	18.57	1.03	0.30	0.73	0.96	0.484	1.34	0.360	1.00	1.00	0.360	No
284	18.67	1.03	0.30	0.73	0.96	0.485	1.34	0.361	1.00	1.00	0.361	No
285	18.72	1.04	0.30	0.73	0.96	0.485	1.34	0.361	1.00	1.00	0.361	No
286	18.78	1.04	0.31	0.73	0.96	0.486	1.34	0.361	1.00	1.00	0.361	No
287	18.85	1.04	0.31	0.73	0.96	0.487	1.34	0.362	1.00	1.00	0.362	No
288	18.93	1.05	0.31	0.74	0.96	0.487	1.34	0.362	1.00	1.00	0.362	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
289	18.97	1.05	0.31	0.74	0.96	0.488	1.34	0.363	1.00	1.00	0.363	No
290	19.08	1.05	0.31	0.74	0.96	0.489	1.34	0.363	1.00	1.00	0.363	No
291	19.12	1.06	0.32	0.74	0.96	0.489	1.34	0.364	1.00	1.00	0.364	No
292	19.22	1.06	0.32	0.74	0.96	0.490	1.34	0.364	1.00	1.00	0.364	No
293	19.27	1.07	0.32	0.74	0.96	0.490	1.34	0.365	1.00	1.00	0.365	No
294	19.32	1.07	0.32	0.75	0.96	0.491	1.34	0.365	1.00	1.00	0.365	No
295	19.37	1.07	0.32	0.75	0.96	0.491	1.34	0.365	1.00	1.00	0.365	No
296	19.43	1.07	0.33	0.75	0.96	0.492	1.34	0.366	1.00	1.00	0.366	No
297	19.52	1.08	0.33	0.75	0.96	0.492	1.34	0.366	1.00	1.00	0.366	No
298	19.57	1.08	0.33	0.75	0.96	0.493	1.34	0.366	1.00	1.00	0.366	No
299	19.67	1.09	0.33	0.75	0.96	0.494	1.34	0.367	1.00	1.00	0.367	No
300	19.72	1.09	0.33	0.76	0.96	0.494	1.34	0.367	1.00	1.00	0.367	No
301	19.77	1.09	0.34	0.76	0.96	0.494	1.34	0.368	1.00	1.00	0.368	No
302	19.82	1.10	0.34	0.76	0.96	0.495	1.34	0.368	1.00	1.00	0.368	No
303	19.92	1.10	0.34	0.76	0.96	0.496	1.34	0.369	1.00	1.00	0.369	No
304	19.97	1.10	0.34	0.76	0.96	0.496	1.34	0.369	1.00	1.00	0.369	No
305	20.04	1.11	0.34	0.76	0.96	0.496	1.34	0.369	1.00	1.00	0.369	No
306	20.08	1.11	0.35	0.76	0.96	0.497	1.34	0.369	1.00	1.00	0.369	No
307	20.16	1.11	0.35	0.77	0.96	0.497	1.34	0.370	1.00	1.00	0.370	No
308	20.24	1.12	0.35	0.77	0.96	0.498	1.34	0.370	1.00	1.00	0.370	No
309	20.28	1.12	0.35	0.77	0.96	0.498	1.34	0.371	1.00	1.00	0.371	No
310	20.37	1.13	0.35	0.77	0.96	0.499	1.34	0.371	1.00	1.00	0.371	No
311	20.41	1.13	0.36	0.77	0.96	0.499	1.34	0.371	1.00	1.00	0.371	No
312	20.50	1.13	0.36	0.77	0.96	0.500	1.34	0.372	1.00	1.00	0.372	No
313	20.57	1.14	0.36	0.78	0.96	0.500	1.34	0.372	1.00	1.00	0.372	No
314	20.61	1.14	0.36	0.78	0.96	0.501	1.34	0.372	1.00	1.00	0.372	No
315	20.70	1.14	0.37	0.78	0.96	0.501	1.34	0.373	1.00	1.00	0.373	No
316	20.76	1.15	0.37	0.78	0.95	0.502	1.34	0.373	1.00	1.00	0.373	No
317	20.81	1.15	0.37	0.78	0.95	0.502	1.34	0.373	1.00	1.00	0.373	No
318	20.89	1.16	0.37	0.78	0.95	0.503	1.34	0.374	1.00	1.00	0.374	No
319	20.95	1.16	0.37	0.79	0.95	0.503	1.34	0.374	1.00	1.00	0.374	No
320	21.00	1.16	0.37	0.79	0.95	0.503	1.34	0.374	1.00	1.00	0.374	No
321	21.10	1.17	0.38	0.79	0.95	0.504	1.34	0.375	1.00	1.00	0.375	No
322	21.14	1.17	0.38	0.79	0.95	0.504	1.34	0.375	1.00	1.00	0.375	No
323	21.21	1.17	0.38	0.79	0.95	0.505	1.34	0.376	1.00	1.00	0.376	No
324	21.30	1.18	0.38	0.79	0.95	0.506	1.34	0.376	1.00	1.00	0.376	No
325	21.34	1.18	0.39	0.79	0.95	0.506	1.34	0.376	1.00	1.00	0.376	No
326	21.40	1.18	0.39	0.80	0.95	0.506	1.34	0.377	1.00	1.00	0.377	No
327	21.48	1.19	0.39	0.80	0.95	0.507	1.34	0.377	1.00	1.00	0.377	No
328	21.54	1.19	0.39	0.80	0.95	0.507	1.34	0.377	1.00	1.00	0.377	No
329	21.60	1.19	0.39	0.80	0.95	0.508	1.34	0.378	1.00	1.00	0.378	No
330	21.68	1.20	0.40	0.80	0.95	0.508	1.34	0.378	1.00	1.00	0.378	No
331	21.75	1.20	0.40	0.80	0.95	0.509	1.34	0.378	1.00	1.00	0.378	No
332	21.80	1.20	0.40	0.81	0.95	0.509	1.34	0.379	1.00	1.00	0.379	No
333	21.88	1.21	0.40	0.81	0.95	0.510	1.34	0.379	1.00	1.00	0.379	No
334	21.92	1.21	0.40	0.81	0.95	0.510	1.34	0.379	1.00	1.00	0.379	No
335	21.99	1.22	0.41	0.81	0.95	0.510	1.34	0.380	1.00	1.00	0.380	No
336	22.08	1.22	0.41	0.81	0.95	0.511	1.34	0.380	1.00	1.00	0.380	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
337	22.15	1.22	0.41	0.81	0.95	0.511	1.34	0.380	1.00	1.00	0.380	No
338	22.19	1.23	0.41	0.81	0.95	0.512	1.34	0.381	1.00	1.00	0.381	No
339	22.28	1.23	0.41	0.82	0.95	0.512	1.34	0.381	1.00	1.00	0.381	No
340	22.34	1.23	0.42	0.82	0.95	0.513	1.34	0.381	1.00	1.00	0.381	No
341	22.39	1.24	0.42	0.82	0.95	0.513	1.34	0.382	1.00	1.00	0.382	No
342	22.47	1.24	0.42	0.82	0.95	0.514	1.34	0.382	1.00	1.00	0.382	No
343	22.54	1.24	0.42	0.82	0.95	0.514	1.34	0.382	1.00	1.00	0.382	No
344	22.58	1.25	0.42	0.82	0.95	0.514	1.34	0.382	1.00	1.00	0.382	No
345	22.68	1.25	0.43	0.83	0.95	0.515	1.34	0.383	1.00	1.00	0.383	No
346	22.74	1.26	0.43	0.83	0.95	0.515	1.34	0.383	1.00	1.00	0.383	No
347	22.79	1.26	0.43	0.83	0.95	0.516	1.34	0.383	1.00	1.00	0.383	No
348	22.84	1.26	0.43	0.83	0.95	0.516	1.34	0.384	1.00	1.00	0.384	No
349	22.94	1.27	0.43	0.83	0.95	0.517	1.34	0.384	1.00	1.00	0.384	No
350	22.99	1.27	0.44	0.83	0.95	0.517	1.34	0.384	1.00	1.00	0.384	No
351	23.04	1.27	0.44	0.83	0.95	0.517	1.34	0.385	1.00	1.00	0.385	No
352	23.11	1.28	0.44	0.84	0.95	0.518	1.34	0.385	1.00	1.00	0.385	No
353	23.18	1.28	0.44	0.84	0.95	0.518	1.34	0.385	1.00	1.00	0.385	No
354	23.23	1.28	0.44	0.84	0.95	0.518	1.34	0.386	1.00	1.00	0.386	No
355	23.34	1.29	0.45	0.84	0.95	0.519	1.34	0.386	1.00	1.00	0.386	No
356	23.37	1.29	0.45	0.84	0.95	0.519	1.34	0.386	1.00	1.00	0.386	No
357	23.44	1.29	0.45	0.84	0.95	0.520	1.34	0.386	1.00	1.00	0.386	No
358	23.54	1.30	0.45	0.84	0.95	0.520	1.34	0.387	1.00	1.00	0.387	No
359	23.60	1.30	0.46	0.85	0.95	0.521	1.34	0.387	1.00	1.00	0.387	No
360	23.64	1.30	0.46	0.85	0.95	0.521	1.34	0.387	1.00	1.00	0.387	No
361	23.71	1.31	0.46	0.85	0.95	0.521	1.34	0.388	1.00	1.00	0.388	No
362	23.79	1.31	0.46	0.85	0.95	0.522	1.34	0.388	1.00	1.00	0.388	No
363	23.84	1.31	0.46	0.85	0.95	0.522	1.34	0.388	1.00	1.00	0.388	No
364	23.89	1.32	0.46	0.85	0.95	0.522	1.34	0.389	1.00	1.00	0.389	No
365	23.99	1.32	0.47	0.85	0.95	0.523	1.34	0.389	1.00	1.00	0.389	No
366	24.03	1.32	0.47	0.85	0.95	0.523	1.34	0.389	1.00	1.00	0.389	No
367	24.10	1.33	0.47	0.86	0.94	0.524	1.34	0.389	1.00	1.00	0.389	No
368	24.18	1.33	0.47	0.86	0.94	0.524	1.34	0.390	1.00	1.00	0.390	No
369	24.23	1.33	0.48	0.86	0.94	0.524	1.34	0.390	1.00	1.00	0.390	No
370	24.31	1.34	0.48	0.86	0.94	0.525	1.34	0.390	1.00	1.00	0.390	No
371	24.36	1.34	0.48	0.86	0.94	0.525	1.34	0.391	1.00	1.00	0.391	No
372	24.45	1.35	0.48	0.86	0.94	0.526	1.34	0.391	1.00	1.00	0.391	No
373	24.49	1.35	0.48	0.86	0.94	0.526	1.34	0.391	1.00	1.00	0.391	No
374	24.57	1.35	0.49	0.87	0.94	0.526	1.34	0.391	1.00	1.00	0.391	No
375	24.61	1.35	0.49	0.87	0.94	0.527	1.34	0.392	1.00	1.00	0.392	No
376	24.69	1.36	0.49	0.87	0.94	0.527	1.34	0.392	1.00	1.00	0.392	No
377	24.74	1.36	0.49	0.87	0.94	0.527	1.34	0.392	1.00	1.00	0.392	No
378	24.82	1.37	0.49	0.87	0.94	0.528	1.34	0.392	1.00	1.00	0.392	No
379	24.89	1.37	0.50	0.87	0.94	0.528	1.34	0.393	1.00	1.00	0.393	No
380	24.94	1.37	0.50	0.87	0.94	0.528	1.34	0.393	1.00	1.00	0.393	No
381	25.01	1.38	0.50	0.88	0.94	0.529	1.34	0.393	1.00	1.00	0.393	No
382	25.09	1.38	0.50	0.88	0.94	0.529	1.34	0.393	1.00	1.00	0.393	No
383	25.13	1.38	0.50	0.88	0.94	0.529	1.34	0.394	1.00	1.00	0.394	No
384	25.22	1.39	0.51	0.88	0.94	0.530	1.34	0.394	1.00	1.00	0.394	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
385	25.28	1.39	0.51	0.88	0.94	0.530	1.34	0.394	1.00	1.00	0.394	No
386	25.34	1.39	0.51	0.88	0.94	0.530	1.34	0.394	1.00	1.00	0.394	No
387	25.44	1.40	0.51	0.89	0.94	0.531	1.34	0.395	1.00	1.00	0.395	No
388	25.48	1.40	0.51	0.89	0.94	0.531	1.34	0.395	1.00	1.00	0.395	No
389	25.53	1.40	0.52	0.89	0.94	0.531	1.34	0.395	1.00	1.00	0.395	No
390	25.59	1.41	0.52	0.89	0.94	0.531	1.34	0.395	1.00	1.00	0.395	No
391	25.68	1.41	0.52	0.89	0.94	0.532	1.34	0.396	1.00	1.00	0.396	No
392	25.73	1.41	0.52	0.89	0.94	0.532	1.34	0.396	1.00	1.00	0.396	No
393	25.79	1.42	0.52	0.89	0.94	0.532	1.34	0.396	1.00	1.00	0.396	No
394	25.88	1.42	0.53	0.90	0.94	0.533	1.34	0.396	1.00	1.00	0.396	No
395	25.93	1.43	0.53	0.90	0.94	0.533	1.34	0.396	1.00	1.00	0.396	No
396	25.99	1.43	0.53	0.90	0.94	0.533	1.34	0.397	1.00	1.00	0.397	No
397	26.08	1.43	0.53	0.90	0.94	0.534	1.34	0.397	1.00	1.00	0.397	No
398	26.14	1.44	0.53	0.90	0.94	0.534	1.34	0.397	1.00	1.00	0.397	No
399	26.19	1.44	0.54	0.90	0.94	0.534	1.34	0.397	1.00	1.00	0.397	No
400	26.28	1.44	0.54	0.90	0.94	0.535	1.34	0.398	1.00	1.00	0.398	No
401	26.34	1.45	0.54	0.91	0.94	0.535	1.34	0.398	1.00	1.00	0.398	No
402	26.39	1.45	0.54	0.91	0.94	0.535	1.34	0.398	1.00	1.00	0.398	No
403	26.45	1.45	0.54	0.91	0.94	0.535	1.34	0.398	1.00	1.00	0.398	No
404	26.53	1.46	0.55	0.91	0.94	0.536	1.34	0.398	1.00	1.00	0.398	No
405	26.58	1.46	0.55	0.91	0.94	0.536	1.34	0.399	1.00	1.00	0.399	No
406	26.68	1.47	0.55	0.91	0.94	0.536	1.34	0.399	1.00	1.00	0.399	No
407	26.73	1.47	0.55	0.92	0.94	0.536	1.34	0.399	1.00	1.00	0.399	No
408	26.78	1.47	0.55	0.92	0.94	0.537	1.34	0.399	1.00	1.00	0.399	No
409	26.88	1.48	0.56	0.92	0.93	0.537	1.34	0.399	1.00	1.00	0.399	No
410	26.93	1.48	0.56	0.92	0.93	0.537	1.34	0.400	1.00	1.00	0.400	No
411	26.98	1.48	0.56	0.92	0.93	0.537	1.34	0.400	1.00	1.00	0.400	No
412	27.04	1.49	0.56	0.92	0.93	0.538	1.34	0.400	1.00	1.00	0.400	No
413	27.13	1.49	0.57	0.93	0.93	0.538	1.34	0.400	1.00	1.00	0.400	No
414	27.22	1.50	0.57	0.93	0.93	0.538	1.34	0.400	1.00	1.00	0.400	No
415	27.24	1.50	0.57	0.93	0.93	0.538	1.34	0.400	1.00	1.00	0.400	No
416	27.33	1.50	0.57	0.93	0.93	0.538	1.34	0.400	1.00	1.00	0.400	No
417	27.37	1.50	0.57	0.93	0.93	0.539	1.34	0.401	1.00	1.00	0.401	No
418	27.43	1.51	0.58	0.93	0.93	0.539	1.34	0.401	1.00	1.00	0.401	No
419	27.52	1.51	0.58	0.94	0.93	0.539	1.34	0.401	1.00	1.00	0.401	No
420	27.57	1.52	0.58	0.94	0.93	0.539	1.34	0.401	1.00	1.00	0.401	No
421	27.63	1.52	0.58	0.94	0.93	0.539	1.34	0.401	1.00	1.00	0.401	No
422	27.72	1.52	0.58	0.94	0.93	0.540	1.34	0.401	1.00	1.00	0.401	No
423	27.76	1.53	0.59	0.94	0.93	0.540	1.34	0.401	1.00	1.00	0.401	No
424	27.84	1.53	0.59	0.94	0.93	0.540	1.34	0.402	1.00	1.00	0.402	No
425	27.93	1.54	0.59	0.95	0.93	0.540	1.34	0.402	1.00	1.00	0.402	No
426	27.97	1.54	0.59	0.95	0.93	0.540	1.34	0.402	1.00	1.00	0.402	No
427	28.02	1.54	0.59	0.95	0.93	0.541	1.34	0.402	1.00	1.00	0.402	No
428	28.12	1.55	0.60	0.95	0.93	0.541	1.34	0.402	1.00	1.00	0.402	No
429	28.17	1.55	0.60	0.95	0.93	0.541	1.34	0.402	1.00	1.00	0.402	No
430	28.23	1.55	0.60	0.95	0.93	0.541	1.34	0.403	1.00	1.00	0.403	No
431	28.32	1.56	0.60	0.95	0.93	0.542	1.34	0.403	1.00	1.00	0.403	No
432	28.37	1.56	0.60	0.96	0.93	0.542	1.34	0.403	1.00	1.00	0.403	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
433	28.42	1.56	0.61	0.96	0.93	0.542	1.34	0.403	1.00	1.00	0.403	No
434	28.48	1.57	0.61	0.96	0.93	0.542	1.34	0.403	1.00	1.00	0.403	No
435	28.57	1.57	0.61	0.96	0.93	0.542	1.34	0.403	1.00	1.00	0.403	No
436	28.61	1.57	0.61	0.96	0.93	0.542	1.34	0.403	1.00	1.00	0.403	No
437	28.69	1.58	0.61	0.96	0.93	0.543	1.34	0.404	1.00	1.00	0.404	No
438	28.77	1.58	0.62	0.97	0.93	0.543	1.34	0.404	1.00	1.00	0.404	No
439	28.83	1.59	0.62	0.97	0.93	0.543	1.34	0.404	1.00	1.00	0.404	No
440	28.88	1.59	0.62	0.97	0.93	0.543	1.34	0.404	1.00	1.00	0.404	No
441	28.97	1.59	0.62	0.97	0.93	0.543	1.34	0.404	1.00	1.00	0.404	No
442	29.02	1.60	0.62	0.97	0.93	0.543	1.34	0.404	1.00	1.00	0.404	No
443	29.08	1.60	0.63	0.97	0.93	0.544	1.34	0.404	1.00	1.00	0.404	No
444	29.17	1.60	0.63	0.98	0.92	0.544	1.34	0.404	1.00	1.00	0.404	No
445	29.21	1.61	0.63	0.98	0.92	0.544	1.34	0.405	1.00	1.00	0.405	No
446	29.28	1.61	0.63	0.98	0.92	0.544	1.34	0.405	1.00	1.00	0.405	No
447	29.37	1.62	0.64	0.98	0.92	0.544	1.34	0.405	1.00	1.00	0.405	No
448	29.41	1.62	0.64	0.98	0.92	0.544	1.34	0.405	1.00	1.00	0.405	No
449	29.47	1.62	0.64	0.98	0.92	0.544	1.34	0.405	1.00	1.00	0.405	No
450	29.56	1.63	0.64	0.99	0.92	0.545	1.34	0.405	1.00	1.00	0.405	No
451	29.62	1.63	0.64	0.99	0.92	0.545	1.34	0.405	1.00	1.00	0.405	No
452	29.68	1.63	0.65	0.99	0.92	0.545	1.34	0.405	1.00	1.00	0.405	No
453	29.76	1.64	0.65	0.99	0.92	0.545	1.34	0.405	1.00	1.00	0.405	No
454	29.83	1.64	0.65	0.99	0.92	0.545	1.34	0.405	1.00	1.00	0.405	No
455	29.87	1.64	0.65	0.99	0.92	0.545	1.34	0.405	1.00	1.00	0.405	No
456	29.96	1.65	0.65	1.00	0.92	0.545	1.34	0.406	1.00	1.00	0.406	No
457	30.01	1.65	0.66	1.00	0.92	0.545	1.34	0.406	1.00	1.00	0.406	No
458	30.07	1.66	0.66	1.00	0.92	0.546	1.34	0.406	1.00	1.00	0.406	No
459	30.16	1.66	0.66	1.00	0.92	0.546	1.34	0.406	1.00	1.00	0.406	No
460	30.20	1.66	0.66	1.00	0.92	0.546	1.34	0.406	1.00	1.00	0.406	No
461	30.27	1.67	0.66	1.00	0.92	0.546	1.34	0.406	1.00	1.00	0.406	No
462	30.34	1.67	0.67	1.01	0.92	0.546	1.34	0.406	1.00	1.00	0.406	No
463	30.42	1.68	0.67	1.01	0.92	0.546	1.34	0.406	1.00	1.00	0.406	No
464	30.46	1.68	0.67	1.01	0.92	0.546	1.34	0.406	1.00	1.00	0.406	No
465	30.52	1.68	0.67	1.01	0.92	0.546	1.34	0.406	1.00	1.00	0.406	No
466	30.58	1.68	0.67	1.01	0.92	0.546	1.34	0.406	1.00	1.00	0.406	No
467	30.66	1.69	0.68	1.01	0.92	0.547	1.34	0.407	1.00	1.00	0.407	No
468	30.71	1.69	0.68	1.01	0.92	0.547	1.34	0.407	1.00	1.00	0.407	No
469	30.81	1.70	0.68	1.02	0.92	0.547	1.34	0.407	1.00	1.00	0.407	No
470	30.87	1.70	0.68	1.02	0.92	0.547	1.34	0.407	1.00	1.00	0.407	No
471	30.91	1.70	0.68	1.02	0.92	0.547	1.34	0.407	1.00	1.00	0.407	No
472	31.01	1.71	0.69	1.02	0.92	0.547	1.34	0.407	1.00	1.00	0.407	No
473	31.06	1.71	0.69	1.02	0.92	0.547	1.34	0.407	1.00	1.00	0.407	No
474	31.11	1.71	0.69	1.02	0.91	0.547	1.34	0.407	1.00	1.00	0.407	No
475	31.19	1.72	0.69	1.03	0.91	0.547	1.34	0.407	1.00	1.00	0.407	No
476	31.26	1.72	0.69	1.03	0.91	0.547	1.34	0.407	1.00	1.00	0.407	No
477	31.35	1.73	0.70	1.03	0.91	0.547	1.34	0.407	1.00	1.00	0.407	No
478	31.37	1.73	0.70	1.03	0.91	0.547	1.34	0.407	1.00	1.00	0.407	No
479	31.46	1.73	0.70	1.03	0.91	0.547	1.34	0.407	1.00	1.00	0.407	No
480	31.55	1.74	0.70	1.04	0.91	0.548	1.34	0.407	1.00	1.00	0.407	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
481	31.59	1.74	0.70	1.04	0.91	0.548	1.34	0.407	1.00	1.00	0.407	No
482	31.66	1.75	0.71	1.04	0.91	0.548	1.34	0.407	1.00	1.00	0.407	No
483	31.70	1.75	0.71	1.04	0.91	0.548	1.34	0.407	1.00	1.00	0.407	No
484	31.79	1.75	0.71	1.04	0.91	0.548	1.34	0.407	1.00	1.00	0.407	No
485	31.86	1.76	0.71	1.04	0.91	0.548	1.34	0.407	1.00	1.00	0.407	No
486	31.91	1.76	0.71	1.05	0.91	0.548	1.34	0.407	1.00	1.00	0.407	No
487	31.99	1.77	0.72	1.05	0.91	0.548	1.34	0.407	1.00	1.00	0.407	No
488	32.06	1.77	0.72	1.05	0.91	0.548	1.34	0.408	1.00	1.00	0.408	No
489	32.10	1.77	0.72	1.05	0.91	0.548	1.34	0.408	1.00	1.00	0.408	No
490	32.20	1.78	0.72	1.05	0.91	0.548	1.34	0.408	1.00	1.00	0.408	No
491	32.26	1.78	0.73	1.06	0.91	0.548	1.34	0.408	1.00	1.00	0.408	No
492	32.30	1.78	0.73	1.06	0.91	0.548	1.34	0.408	1.00	1.00	0.408	No
493	32.35	1.79	0.73	1.06	0.91	0.548	1.34	0.408	1.00	1.00	0.408	No
494	32.46	1.79	0.73	1.06	0.91	0.548	1.34	0.408	1.00	1.00	0.408	No
495	32.49	1.79	0.73	1.06	0.91	0.548	1.34	0.408	1.00	1.00	0.408	No
496	32.58	1.80	0.74	1.06	0.91	0.548	1.34	0.408	1.00	1.00	0.408	No
497	32.62	1.80	0.74	1.07	0.91	0.548	1.34	0.408	1.00	1.00	0.408	No
498	32.69	1.81	0.74	1.07	0.91	0.548	1.34	0.408	1.00	1.00	0.408	No
499	32.78	1.81	0.74	1.07	0.91	0.548	1.34	0.407	1.00	1.00	0.409	No
500	32.82	1.81	0.74	1.07	0.90	0.548	1.34	0.407	1.00	1.00	0.409	No
501	32.89	1.82	0.75	1.07	0.90	0.548	1.34	0.407	1.00	1.00	0.409	No
502	32.98	1.82	0.75	1.08	0.90	0.548	1.34	0.407	1.00	1.00	0.409	No
503	33.02	1.83	0.75	1.08	0.90	0.548	1.34	0.407	1.00	1.00	0.409	No
504	33.08	1.83	0.75	1.08	0.90	0.548	1.34	0.407	1.00	1.00	0.409	No
505	33.18	1.84	0.75	1.08	0.90	0.548	1.34	0.407	0.99	1.00	0.409	No
506	33.21	1.84	0.76	1.08	0.90	0.548	1.34	0.407	0.99	1.00	0.409	No
507	33.29	1.84	0.76	1.09	0.90	0.547	1.34	0.407	0.99	1.00	0.410	No
508	33.37	1.85	0.76	1.09	0.90	0.547	1.34	0.407	0.99	1.00	0.410	No
509	33.42	1.85	0.76	1.09	0.90	0.547	1.34	0.407	0.99	1.00	0.410	No
510	33.47	1.85	0.76	1.09	0.90	0.547	1.34	0.407	0.99	1.00	0.410	No
511	33.53	1.86	0.77	1.09	0.90	0.547	1.34	0.407	0.99	1.00	0.410	No
512	33.62	1.86	0.77	1.10	0.90	0.547	1.34	0.407	0.99	1.00	0.410	No
513	33.67	1.87	0.77	1.10	0.90	0.547	1.34	0.407	0.99	1.00	0.410	No
514	33.73	1.87	0.77	1.10	0.90	0.547	1.34	0.407	0.99	1.00	0.411	No
515	33.82	1.88	0.77	1.10	0.90	0.547	1.34	0.407	0.99	1.00	0.411	No
516	33.87	1.88	0.78	1.10	0.90	0.547	1.34	0.407	0.99	1.00	0.411	No
517	33.93	1.88	0.78	1.10	0.90	0.547	1.34	0.407	0.99	1.00	0.411	No
518	34.02	1.89	0.78	1.11	0.90	0.547	1.34	0.407	0.99	1.00	0.411	No
519	34.06	1.89	0.78	1.11	0.90	0.547	1.34	0.407	0.99	1.00	0.411	No
520	34.13	1.89	0.78	1.11	0.90	0.547	1.34	0.407	0.99	1.00	0.411	No
521	34.22	1.90	0.79	1.11	0.90	0.547	1.34	0.407	0.99	1.00	0.411	No
522	34.26	1.90	0.79	1.11	0.90	0.547	1.34	0.407	0.99	1.00	0.412	No
523	34.32	1.90	0.79	1.11	0.90	0.547	1.34	0.407	0.99	1.00	0.412	No
524	34.42	1.91	0.79	1.12	0.89	0.547	1.34	0.407	0.99	1.00	0.412	No
525	34.46	1.91	0.79	1.12	0.89	0.547	1.34	0.407	0.99	1.00	0.412	No
526	34.52	1.92	0.80	1.12	0.89	0.547	1.34	0.407	0.99	1.00	0.412	No
527	34.61	1.92	0.80	1.12	0.89	0.547	1.34	0.407	0.99	1.00	0.412	No
528	34.70	1.93	0.80	1.12	0.89	0.547	1.34	0.407	0.99	1.00	0.412	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
529	34.76	1.93	0.80	1.13	0.89	0.547	1.34	0.407	0.99	1.00	0.412	No
530	34.82	1.93	0.81	1.13	0.89	0.547	1.34	0.407	0.99	1.00	0.413	No
531	34.86	1.94	0.81	1.13	0.89	0.547	1.34	0.407	0.99	1.00	0.413	No
532	34.92	1.94	0.81	1.13	0.89	0.547	1.34	0.407	0.99	1.00	0.413	No
533	35.02	1.94	0.81	1.13	0.89	0.547	1.34	0.406	0.98	1.00	0.413	No
534	35.06	1.95	0.81	1.13	0.89	0.547	1.34	0.406	0.98	1.00	0.413	No
535	35.11	1.95	0.81	1.13	0.89	0.546	1.34	0.406	0.98	1.00	0.413	No
536	35.19	1.95	0.82	1.14	0.89	0.546	1.34	0.406	0.98	1.00	0.413	No
537	35.25	1.96	0.82	1.14	0.89	0.546	1.34	0.406	0.98	1.00	0.413	No
538	35.31	1.96	0.82	1.14	0.89	0.546	1.34	0.406	0.98	1.00	0.413	No
539	35.40	1.97	0.82	1.14	0.89	0.546	1.34	0.406	0.98	1.00	0.413	No
540	35.45	1.97	0.83	1.14	0.89	0.546	1.34	0.406	0.98	1.00	0.414	No
541	35.50	1.97	0.83	1.15	0.89	0.546	1.34	0.406	0.98	1.00	0.414	No
542	35.56	1.98	0.83	1.15	0.89	0.546	1.34	0.406	0.98	1.00	0.414	No
543	35.64	1.98	0.83	1.15	0.89	0.546	1.34	0.406	0.98	1.00	0.414	No
544	35.72	1.99	0.83	1.15	0.89	0.546	1.34	0.406	0.98	1.00	0.414	No
545	35.81	1.99	0.84	1.15	0.88	0.546	1.34	0.406	0.98	1.00	0.414	No
546	35.85	1.99	0.84	1.16	0.88	0.545	1.34	0.406	0.98	1.00	0.414	No
547	35.90	2.00	0.84	1.16	0.88	0.545	1.34	0.406	0.98	1.00	0.414	No
548	35.96	2.00	0.84	1.16	0.88	0.545	1.34	0.406	0.98	1.00	0.414	No
549	36.04	2.00	0.84	1.16	0.88	0.545	1.34	0.405	0.98	1.00	0.414	No
550	36.11	2.01	0.85	1.16	0.88	0.545	1.34	0.405	0.98	1.00	0.414	No
551	36.16	2.01	0.85	1.16	0.88	0.545	1.34	0.405	0.98	1.00	0.414	No
552	36.25	2.02	0.85	1.17	0.88	0.545	1.34	0.405	0.98	1.00	0.414	No
553	36.31	2.02	0.85	1.17	0.88	0.545	1.34	0.405	0.98	1.00	0.414	No
554	36.36	2.02	0.85	1.17	0.88	0.545	1.34	0.405	0.98	1.00	0.415	No
555	36.44	2.03	0.86	1.17	0.88	0.544	1.34	0.405	0.98	1.00	0.415	No
556	36.50	2.03	0.86	1.17	0.88	0.544	1.34	0.405	0.98	1.00	0.415	No
557	36.56	2.04	0.86	1.18	0.88	0.544	1.34	0.405	0.98	1.00	0.415	No
558	36.65	2.04	0.86	1.18	0.88	0.544	1.34	0.405	0.98	1.00	0.415	No
559	36.68	2.04	0.86	1.18	0.88	0.544	1.34	0.405	0.98	1.00	0.415	No
560	36.76	2.05	0.87	1.18	0.88	0.544	1.34	0.404	0.97	1.00	0.415	No
561	36.84	2.05	0.87	1.18	0.88	0.544	1.34	0.404	0.97	1.00	0.415	No
562	36.91	2.06	0.87	1.19	0.88	0.544	1.34	0.404	0.97	1.00	0.415	No
563	36.96	2.06	0.87	1.19	0.88	0.543	1.34	0.404	0.97	1.00	0.415	No
564	37.04	2.06	0.87	1.19	0.88	0.543	1.34	0.404	0.97	1.00	0.415	No
565	37.10	2.07	0.88	1.19	0.88	0.543	1.34	0.404	0.97	1.00	0.415	No
566	37.15	2.07	0.88	1.19	0.87	0.543	1.34	0.404	0.97	1.00	0.415	No
567	37.23	2.08	0.88	1.19	0.87	0.543	1.34	0.404	0.97	1.00	0.415	No
568	37.30	2.08	0.88	1.20	0.87	0.543	1.34	0.404	0.97	1.00	0.415	No
569	37.35	2.08	0.88	1.20	0.87	0.543	1.34	0.404	0.97	1.00	0.415	No
570	37.45	2.09	0.89	1.20	0.87	0.542	1.34	0.403	0.97	1.00	0.415	No
571	37.51	2.09	0.89	1.20	0.87	0.542	1.34	0.403	0.97	1.00	0.415	No
572	37.55	2.09	0.89	1.20	0.87	0.542	1.34	0.403	0.97	1.00	0.415	No
573	37.62	2.10	0.89	1.20	0.87	0.542	1.34	0.403	0.97	1.00	0.415	No
574	37.70	2.10	0.90	1.21	0.87	0.542	1.34	0.403	0.97	1.00	0.416	No
575	37.75	2.11	0.90	1.21	0.87	0.542	1.34	0.403	0.97	1.00	0.416	No
576	37.80	2.11	0.90	1.21	0.87	0.542	1.34	0.403	0.97	1.00	0.416	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
577	37.90	2.11	0.90	1.21	0.87	0.542	1.34	0.403	0.97	1.00	0.416	No
578	37.95	2.12	0.90	1.21	0.87	0.541	1.34	0.403	0.97	1.00	0.416	No
579	38.05	2.12	0.91	1.22	0.87	0.541	1.34	0.403	0.97	1.00	0.416	No
580	38.06	2.12	0.91	1.22	0.87	0.541	1.34	0.403	0.97	1.00	0.416	No
581	38.15	2.13	0.91	1.22	0.87	0.541	1.34	0.402	0.97	1.00	0.416	No
582	38.19	2.13	0.91	1.22	0.87	0.541	1.34	0.402	0.97	1.00	0.416	No
583	38.27	2.14	0.91	1.22	0.87	0.541	1.34	0.402	0.97	1.00	0.416	No
584	38.34	2.14	0.92	1.22	0.87	0.541	1.34	0.402	0.97	1.00	0.416	No
585	38.39	2.14	0.92	1.23	0.86	0.541	1.34	0.402	0.97	1.00	0.416	No
586	38.46	2.15	0.92	1.23	0.86	0.540	1.34	0.402	0.97	1.00	0.416	No
587	38.55	2.15	0.92	1.23	0.86	0.540	1.34	0.402	0.97	1.00	0.416	No
588	38.59	2.15	0.92	1.23	0.86	0.540	1.34	0.402	0.97	1.00	0.416	No
589	38.68	2.16	0.93	1.23	0.86	0.540	1.34	0.402	0.97	1.00	0.416	No
590	38.75	2.16	0.93	1.23	0.86	0.540	1.34	0.401	0.97	1.00	0.416	No
591	38.80	2.17	0.93	1.24	0.86	0.540	1.34	0.401	0.96	1.00	0.416	No
592	38.87	2.17	0.93	1.24	0.86	0.539	1.34	0.401	0.96	1.00	0.416	No
593	38.95	2.18	0.93	1.24	0.86	0.539	1.34	0.401	0.96	1.00	0.416	No
594	38.99	2.18	0.94	1.24	0.86	0.539	1.34	0.401	0.96	1.00	0.416	No
595	39.04	2.18	0.94	1.24	0.86	0.539	1.34	0.401	0.96	1.00	0.416	No
596	39.11	2.18	0.94	1.25	0.86	0.539	1.34	0.401	0.96	1.00	0.416	No
597	39.19	2.19	0.94	1.25	0.86	0.538	1.34	0.400	0.96	1.00	0.416	No
598	39.27	2.19	0.94	1.25	0.86	0.538	1.34	0.400	0.96	1.00	0.416	No
599	39.33	2.20	0.95	1.25	0.86	0.538	1.34	0.400	0.96	1.00	0.416	No
600	39.39	2.20	0.95	1.25	0.86	0.538	1.34	0.400	0.96	1.00	0.416	No
601	39.45	2.21	0.95	1.26	0.86	0.537	1.34	0.400	0.96	1.00	0.416	No
602	39.53	2.21	0.95	1.26	0.86	0.537	1.34	0.400	0.96	1.00	0.416	No
603	39.57	2.21	0.95	1.26	0.85	0.537	1.34	0.399	0.96	1.00	0.416	No
604	39.64	2.22	0.96	1.26	0.85	0.537	1.34	0.399	0.96	1.00	0.416	No
605	39.72	2.22	0.96	1.26	0.85	0.537	1.34	0.399	0.96	1.00	0.416	No
606	39.79	2.23	0.96	1.27	0.85	0.536	1.34	0.399	0.96	1.00	0.416	No
607	39.84	2.23	0.96	1.27	0.85	0.536	1.34	0.399	0.96	1.00	0.416	No
608	39.93	2.23	0.97	1.27	0.85	0.536	1.34	0.399	0.96	1.00	0.416	No
609	39.98	2.24	0.97	1.27	0.85	0.536	1.34	0.399	0.96	1.00	0.416	No
610	40.05	2.24	0.97	1.27	0.85	0.536	1.34	0.398	0.96	1.00	0.416	No
611	40.09	2.24	0.97	1.27	0.85	0.536	1.34	0.398	0.96	1.00	0.416	No
612	40.19	2.25	0.97	1.28	0.85	0.535	1.34	0.398	0.96	1.00	0.416	No
613	40.23	2.25	0.97	1.28	0.85	0.535	1.34	0.398	0.96	1.00	0.416	No
614	40.34	2.26	0.98	1.28	0.85	0.535	1.34	0.398	0.96	1.00	0.416	No
615	40.38	2.26	0.98	1.28	0.85	0.535	1.34	0.398	0.96	1.00	0.415	No
616	40.43	2.26	0.98	1.28	0.85	0.534	1.34	0.397	0.96	1.00	0.415	No
617	40.50	2.27	0.98	1.29	0.85	0.534	1.34	0.397	0.96	1.00	0.415	No
618	40.58	2.27	0.99	1.29	0.85	0.534	1.34	0.397	0.96	1.00	0.415	No
619	40.63	2.28	0.99	1.29	0.85	0.534	1.34	0.397	0.96	1.00	0.415	No
620	40.70	2.28	0.99	1.29	0.84	0.533	1.34	0.397	0.96	1.00	0.415	No
621	40.75	2.28	0.99	1.29	0.84	0.533	1.34	0.396	0.95	1.00	0.415	No
622	40.84	2.29	0.99	1.30	0.84	0.533	1.34	0.396	0.95	1.00	0.415	No
623	40.88	2.29	0.99	1.30	0.84	0.532	1.34	0.396	0.95	1.00	0.415	No
624	40.95	2.30	1.00	1.30	0.84	0.532	1.34	0.396	0.95	1.00	0.415	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
625	41.03	2.30	1.00	1.30	0.84	0.532	1.34	0.396	0.95	1.00	2.000	Yes
626	41.08	2.31	1.00	1.30	0.84	0.532	1.34	0.395	0.95	1.00	2.000	Yes
627	41.15	2.31	1.00	1.31	0.84	0.531	1.34	0.395	0.95	1.00	2.000	Yes
628	41.23	2.32	1.01	1.31	0.84	0.531	1.34	0.395	0.95	1.00	2.000	Yes
629	41.28	2.32	1.01	1.31	0.84	0.531	1.34	0.395	0.95	1.00	2.000	Yes
630	41.35	2.32	1.01	1.31	0.84	0.530	1.34	0.394	0.95	1.00	2.000	Yes
631	41.43	2.33	1.01	1.32	0.84	0.530	1.34	0.394	0.95	1.00	2.000	Yes
632	41.48	2.33	1.01	1.32	0.84	0.530	1.34	0.394	0.95	1.00	2.000	Yes
633	41.54	2.34	1.02	1.32	0.84	0.529	1.34	0.394	0.95	1.00	0.414	No
634	41.62	2.34	1.02	1.32	0.84	0.529	1.34	0.393	0.95	1.00	0.414	No
635	41.68	2.34	1.02	1.33	0.84	0.529	1.34	0.393	0.95	1.00	0.414	No
636	41.77	2.35	1.02	1.33	0.83	0.528	1.34	0.393	0.95	1.00	0.414	No
637	41.82	2.35	1.02	1.33	0.83	0.528	1.34	0.393	0.95	1.00	0.414	No
638	41.88	2.36	1.03	1.33	0.83	0.528	1.34	0.392	0.95	1.00	0.414	No
639	41.97	2.36	1.03	1.34	0.83	0.527	1.34	0.392	0.95	1.00	0.414	No
640	42.01	2.37	1.03	1.34	0.83	0.527	1.34	0.392	0.95	1.00	0.414	No
641	42.10	2.37	1.03	1.34	0.83	0.527	1.34	0.392	0.95	1.00	0.413	No
642	42.17	2.38	1.03	1.34	0.83	0.526	1.34	0.391	0.95	1.00	0.413	No
643	42.22	2.38	1.04	1.34	0.83	0.526	1.34	0.391	0.95	1.00	0.413	No
644	42.28	2.39	1.04	1.35	0.83	0.526	1.34	0.391	0.95	1.00	0.413	No
645	42.33	2.39	1.04	1.35	0.83	0.525	1.34	0.391	0.95	1.00	0.413	No
646	42.41	2.39	1.04	1.35	0.83	0.525	1.34	0.390	0.95	1.00	0.413	No
647	42.48	2.40	1.04	1.35	0.83	0.525	1.34	0.390	0.94	1.00	0.413	No
648	42.52	2.40	1.05	1.36	0.83	0.524	1.34	0.390	0.94	1.00	0.413	No
649	42.60	2.41	1.05	1.36	0.83	0.524	1.34	0.390	0.94	1.00	0.413	No
650	42.66	2.41	1.05	1.36	0.83	0.524	1.34	0.389	0.94	1.00	0.413	No
651	42.72	2.41	1.05	1.36	0.83	0.523	1.34	0.389	0.94	1.00	0.412	No
652	42.81	2.42	1.05	1.37	0.83	0.523	1.34	0.389	0.94	1.00	0.412	No
653	42.87	2.43	1.06	1.37	0.82	0.522	1.34	0.389	0.94	1.00	0.412	No
654	42.92	2.43	1.06	1.37	0.82	0.522	1.34	0.388	0.94	1.00	0.412	No
655	43.00	2.43	1.06	1.37	0.82	0.522	1.34	0.388	0.94	1.00	0.412	No
656	43.06	2.44	1.06	1.38	0.82	0.521	1.34	0.388	0.94	1.00	0.412	No
657	43.11	2.44	1.06	1.38	0.82	0.521	1.34	0.388	0.94	1.00	0.412	No
658	43.18	2.45	1.07	1.38	0.82	0.521	1.34	0.387	0.94	1.00	0.412	No
659	43.25	2.45	1.07	1.38	0.82	0.520	1.34	0.387	0.94	1.00	0.412	No
660	43.31	2.45	1.07	1.38	0.82	0.520	1.34	0.387	0.94	1.00	0.411	No
661	43.39	2.46	1.07	1.39	0.82	0.520	1.34	0.387	0.94	1.00	0.411	No
662	43.45	2.46	1.07	1.39	0.82	0.519	1.34	0.386	0.94	1.00	0.411	No
663	43.51	2.47	1.08	1.39	0.82	0.519	1.34	0.386	0.94	1.00	0.411	No
664	43.61	2.47	1.08	1.39	0.82	0.519	1.34	0.386	0.94	1.00	0.411	No
665	43.65	2.48	1.08	1.40	0.82	0.518	1.34	0.385	0.94	1.00	0.411	No
666	43.72	2.48	1.08	1.40	0.82	0.518	1.34	0.385	0.94	1.00	0.411	No
667	43.81	2.49	1.09	1.40	0.82	0.517	1.34	0.385	0.94	1.00	0.411	No
668	43.85	2.49	1.09	1.40	0.82	0.517	1.34	0.385	0.94	1.00	0.410	No
669	43.92	2.49	1.09	1.41	0.81	0.517	1.34	0.384	0.94	1.00	0.410	No
670	44.01	2.50	1.09	1.41	0.81	0.516	1.34	0.384	0.94	1.00	0.410	No
671	44.05	2.50	1.09	1.41	0.81	0.516	1.34	0.384	0.94	1.00	0.410	No
672	44.10	2.51	1.10	1.41	0.81	0.516	1.34	0.384	0.94	1.00	0.410	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
673	44.20	2.51	1.10	1.41	0.81	0.515	1.34	0.383	0.94	1.00	0.410	No
674	44.25	2.52	1.10	1.42	0.81	0.515	1.34	0.383	0.94	1.00	0.410	No
675	44.30	2.52	1.10	1.42	0.81	0.515	1.34	0.383	0.93	1.00	0.410	No
676	44.40	2.53	1.10	1.42	0.81	0.514	1.34	0.383	0.93	1.00	0.409	No
677	44.45	2.53	1.11	1.42	0.81	0.514	1.34	0.382	0.93	1.00	0.409	No
678	44.50	2.53	1.11	1.42	0.81	0.514	1.34	0.382	0.93	1.00	0.409	No
679	44.57	2.54	1.11	1.43	0.81	0.513	1.34	0.382	0.93	1.00	0.409	No
680	44.63	2.54	1.11	1.43	0.81	0.513	1.34	0.382	0.93	1.00	0.409	No
681	44.69	2.54	1.11	1.43	0.81	0.513	1.34	0.381	0.93	1.00	0.409	No
682	44.79	2.55	1.12	1.43	0.81	0.512	1.34	0.381	0.93	1.00	0.409	No
683	44.84	2.55	1.12	1.44	0.81	0.512	1.34	0.381	0.93	1.00	0.409	No
684	44.89	2.56	1.12	1.44	0.80	0.512	1.34	0.381	0.93	1.00	0.408	No
685	44.96	2.56	1.12	1.44	0.80	0.511	1.34	0.380	0.93	1.00	0.408	No
686	45.04	2.57	1.12	1.44	0.80	0.511	1.34	0.380	0.93	1.00	0.408	No
687	45.09	2.57	1.13	1.44	0.80	0.511	1.34	0.380	0.93	1.00	0.408	No
688	45.17	2.58	1.13	1.45	0.80	0.510	1.34	0.379	0.93	1.00	0.408	No
689	45.24	2.58	1.13	1.45	0.80	0.510	1.34	0.379	0.93	1.00	0.408	No
690	45.28	2.58	1.13	1.45	0.80	0.510	1.34	0.379	0.93	1.00	0.408	No
691	45.38	2.59	1.14	1.45	0.80	0.509	1.34	0.379	0.93	1.00	0.407	No
692	45.42	2.59	1.14	1.46	0.80	0.509	1.34	0.378	0.93	1.00	0.407	No
693	45.49	2.60	1.14	1.46	0.80	0.508	1.34	0.378	0.93	1.00	0.407	No
694	45.57	2.60	1.14	1.46	0.80	0.508	1.34	0.378	0.93	1.00	0.407	No
695	45.63	2.61	1.14	1.46	0.80	0.508	1.34	0.378	0.93	1.00	0.407	No
696	45.69	2.61	1.14	1.47	0.80	0.507	1.34	0.377	0.93	1.00	0.407	No
697	45.78	2.62	1.15	1.47	0.80	0.507	1.34	0.377	0.93	1.00	0.406	No
698	45.84	2.62	1.15	1.47	0.80	0.507	1.34	0.377	0.93	1.00	0.406	No
699	45.89	2.62	1.15	1.47	0.79	0.506	1.34	0.377	0.93	1.00	0.406	No
700	45.93	2.63	1.15	1.47	0.79	0.506	1.34	0.376	0.93	1.00	0.406	No
701	46.02	2.63	1.16	1.48	0.79	0.506	1.34	0.376	0.93	1.00	0.406	No
702	46.08	2.63	1.16	1.48	0.79	0.505	1.34	0.376	0.93	1.00	0.406	No
703	46.13	2.64	1.16	1.48	0.79	0.505	1.34	0.376	0.93	1.00	0.406	No
704	46.22	2.64	1.16	1.48	0.79	0.505	1.34	0.375	0.93	1.00	0.406	No
705	46.28	2.65	1.16	1.48	0.79	0.504	1.34	0.375	0.93	1.00	0.405	No
706	46.33	2.65	1.16	1.49	0.79	0.504	1.34	0.375	0.92	1.00	0.405	No
707	46.43	2.66	1.17	1.49	0.79	0.504	1.34	0.375	0.92	1.00	0.405	No
708	46.47	2.66	1.17	1.49	0.79	0.503	1.34	0.374	0.92	1.00	0.405	No
709	46.53	2.66	1.17	1.49	0.79	0.503	1.34	0.374	0.92	1.00	0.405	No
710	46.63	2.67	1.17	1.49	0.79	0.503	1.34	0.374	0.92	1.00	0.405	No
711	46.67	2.67	1.18	1.49	0.79	0.502	1.34	0.374	0.92	1.00	0.405	No
712	46.73	2.67	1.18	1.50	0.79	0.502	1.34	0.373	0.92	1.00	0.404	No
713	46.83	2.68	1.18	1.50	0.79	0.502	1.34	0.373	0.92	1.00	0.404	No
714	46.87	2.68	1.18	1.50	0.78	0.501	1.34	0.373	0.92	1.00	0.404	No
715	46.93	2.69	1.18	1.50	0.78	0.501	1.34	0.373	0.92	1.00	0.404	No
716	47.02	2.69	1.19	1.50	0.78	0.501	1.34	0.372	0.92	1.00	0.404	No
717	47.08	2.69	1.19	1.51	0.78	0.501	1.34	0.372	0.92	1.00	0.404	No
718	47.12	2.70	1.19	1.51	0.78	0.500	1.34	0.372	0.92	1.00	0.404	No
719	47.18	2.70	1.19	1.51	0.78	0.500	1.34	0.372	0.92	1.00	0.404	No
720	47.27	2.71	1.19	1.51	0.78	0.500	1.34	0.372	0.92	1.00	0.403	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
721	47.31	2.71	1.20	1.51	0.78	0.499	1.34	0.371	0.92	1.00	0.403	No
722	47.39	2.71	1.20	1.51	0.78	0.499	1.34	0.371	0.92	1.00	0.403	No
723	47.48	2.72	1.20	1.52	0.78	0.499	1.34	0.371	0.92	1.00	0.403	No
724	47.52	2.72	1.20	1.52	0.78	0.498	1.34	0.371	0.92	1.00	0.403	No
725	47.59	2.72	1.20	1.52	0.78	0.498	1.34	0.370	0.92	1.00	0.403	No
726	47.66	2.73	1.21	1.52	0.78	0.498	1.34	0.370	0.92	1.00	0.402	No
727	47.74	2.73	1.21	1.52	0.78	0.497	1.34	0.370	0.92	1.00	0.402	No
728	47.79	2.74	1.21	1.53	0.78	0.497	1.34	0.370	0.92	1.00	0.402	No
729	47.86	2.74	1.21	1.53	0.77	0.497	1.34	0.369	0.92	1.00	2.000	Yes
730	47.94	2.74	1.21	1.53	0.77	0.496	1.34	0.369	0.92	1.00	2.000	Yes
731	47.99	2.75	1.22	1.53	0.77	0.496	1.34	0.369	0.92	1.00	2.000	Yes
732	48.05	2.75	1.22	1.53	0.77	0.496	1.34	0.369	0.92	1.00	2.000	Yes
733	48.13	2.76	1.22	1.54	0.77	0.495	1.34	0.368	0.92	1.00	2.000	Yes
734	48.19	2.76	1.22	1.54	0.77	0.495	1.34	0.368	0.92	1.00	2.000	Yes
735	48.26	2.76	1.22	1.54	0.77	0.495	1.34	0.368	0.92	1.00	2.000	Yes
736	48.34	2.77	1.23	1.54	0.77	0.494	1.34	0.368	0.92	1.00	2.000	Yes
737	48.39	2.77	1.23	1.54	0.77	0.494	1.34	0.367	0.92	1.00	0.401	No
738	48.43	2.78	1.23	1.55	0.77	0.494	1.34	0.367	0.92	1.00	0.401	No
739	48.51	2.78	1.23	1.55	0.77	0.493	1.34	0.367	0.92	1.00	2.000	Yes
740	48.58	2.78	1.23	1.55	0.77	0.493	1.34	0.367	0.92	1.00	2.000	Yes
741	48.63	2.79	1.24	1.55	0.77	0.493	1.34	0.366	0.92	1.00	2.000	Yes
742	48.72	2.79	1.24	1.55	0.77	0.492	1.34	0.366	0.92	1.00	2.000	Yes
743	48.78	2.80	1.24	1.56	0.77	0.492	1.34	0.366	0.92	1.00	2.000	Yes
744	48.83	2.80	1.24	1.56	0.76	0.491	1.34	0.365	0.91	1.00	2.000	Yes
745	48.90	2.81	1.24	1.56	0.76	0.491	1.34	0.365	0.91	1.00	2.000	Yes
746	48.99	2.81	1.25	1.56	0.76	0.491	1.34	0.365	0.91	1.00	0.399	No
747	49.03	2.81	1.25	1.56	0.76	0.490	1.34	0.365	0.91	1.00	2.000	Yes
748	49.08	2.82	1.25	1.57	0.76	0.490	1.34	0.364	0.91	1.00	2.000	Yes
749	49.17	2.82	1.25	1.57	0.76	0.490	1.34	0.364	0.91	1.00	2.000	Yes
750	49.23	2.83	1.26	1.57	0.76	0.489	1.34	0.364	0.91	1.00	2.000	Yes
751	49.32	2.83	1.26	1.57	0.76	0.489	1.34	0.363	0.91	1.00	2.000	Yes
752	49.35	2.83	1.26	1.57	0.76	0.488	1.34	0.363	0.91	1.00	2.000	Yes
753	49.43	2.84	1.26	1.58	0.76	0.488	1.34	0.363	0.91	1.00	2.000	Yes
754	49.50	2.84	1.26	1.58	0.76	0.488	1.34	0.363	0.91	1.00	2.000	Yes
755	49.58	2.85	1.27	1.58	0.76	0.487	1.34	0.362	0.91	1.00	2.000	Yes
756	49.63	2.85	1.27	1.58	0.76	0.487	1.34	0.362	0.91	1.00	2.000	Yes
757	49.72	2.86	1.27	1.59	0.76	0.486	1.34	0.362	0.91	1.00	2.000	Yes
758	49.78	2.86	1.27	1.59	0.75	0.486	1.34	0.361	0.91	1.00	2.000	Yes
759	49.83	2.87	1.27	1.59	0.75	0.486	1.34	0.361	0.91	1.00	2.000	Yes
760	49.90	2.87	1.28	1.59	0.75	0.485	1.34	0.361	0.91	1.00	0.397	No
761	49.98	2.88	1.28	1.60	0.75	0.485	1.34	0.361	0.91	1.00	0.396	No
762	50.02	2.88	1.28	1.60	0.75	0.484	1.34	0.360	0.91	1.00	2.000	No
763	50.08	2.88	1.28	1.60	0.75	0.484	1.34	0.360	0.91	1.00	2.000	No
764	50.18	2.89	1.28	1.60	0.75	0.483	1.34	0.360	0.91	1.00	2.000	No
765	50.23	2.89	1.29	1.61	0.75	0.483	1.34	0.359	0.91	1.00	2.000	No
766	50.27	2.89	1.29	1.61	0.75	0.483	1.34	0.359	0.91	1.00	2.000	No
767	50.36	2.90	1.29	1.61	0.75	0.482	1.34	0.359	0.91	1.00	2.000	No
768	50.40	2.90	1.29	1.61	0.75	0.482	1.34	0.359	0.91	1.00	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
769	50.47	2.91	1.29	1.61	0.75	0.482	1.34	0.358	0.91	1.00	2.000	No
770	50.55	2.91	1.30	1.62	0.75	0.481	1.34	0.358	0.91	1.00	2.000	No
771	50.63	2.92	1.30	1.62	0.75	0.481	1.34	0.358	0.91	1.00	2.000	No
772	50.67	2.92	1.30	1.62	0.75	0.481	1.34	0.357	0.91	1.00	2.000	No
773	50.72	2.92	1.30	1.62	0.75	0.480	1.34	0.357	0.91	1.00	2.000	No
774	50.83	2.93	1.31	1.63	0.74	0.480	1.34	0.357	0.91	1.00	2.000	No
775	50.88	2.93	1.31	1.63	0.74	0.479	1.34	0.356	0.91	1.00	2.000	No
776	50.93	2.94	1.31	1.63	0.74	0.479	1.34	0.356	0.91	1.00	2.000	No
777	51.02	2.94	1.31	1.63	0.74	0.478	1.34	0.356	0.90	1.00	2.000	No
778	51.08	2.95	1.31	1.64	0.74	0.478	1.34	0.356	0.90	1.00	2.000	No
779	51.12	2.95	1.31	1.64	0.74	0.478	1.34	0.355	0.90	1.00	2.000	No
780	51.21	2.96	1.32	1.64	0.74	0.477	1.34	0.355	0.90	1.00	2.000	No
781	51.27	2.96	1.32	1.64	0.74	0.477	1.34	0.355	0.90	1.00	2.000	No
782	51.32	2.96	1.32	1.64	0.74	0.477	1.34	0.354	0.90	1.00	2.000	No
783	51.39	2.97	1.32	1.65	0.74	0.476	1.34	0.354	0.90	1.00	2.000	No
784	51.47	2.97	1.33	1.65	0.74	0.476	1.34	0.354	0.90	1.00	2.000	No
785	51.55	2.98	1.33	1.65	0.74	0.475	1.34	0.353	0.90	1.00	2.000	No
786	51.60	2.98	1.33	1.65	0.74	0.475	1.34	0.353	0.90	1.00	2.000	No
787	51.67	2.99	1.33	1.66	0.74	0.474	1.34	0.353	0.90	1.00	2.000	No
788	51.72	2.99	1.33	1.66	0.74	0.474	1.34	0.353	0.90	1.00	2.000	No
789	51.79	3.00	1.34	1.66	0.73	0.474	1.34	0.352	0.90	1.00	2.000	No
790	51.87	3.00	1.34	1.66	0.73	0.473	1.34	0.352	0.90	1.00	2.000	No
791	51.91	3.00	1.34	1.66	0.73	0.473	1.34	0.352	0.90	1.00	2.000	No
792	51.98	3.01	1.34	1.67	0.73	0.473	1.34	0.352	0.90	1.00	2.000	No
793	52.06	3.01	1.34	1.67	0.73	0.472	1.34	0.351	0.90	1.00	2.000	No
794	52.12	3.02	1.35	1.67	0.73	0.472	1.34	0.351	0.90	1.00	2.000	No
795	52.17	3.02	1.35	1.67	0.73	0.471	1.34	0.351	0.90	1.00	2.000	No
796	52.26	3.03	1.35	1.68	0.73	0.471	1.34	0.350	0.90	1.00	2.000	Yes
797	52.31	3.03	1.35	1.68	0.73	0.471	1.34	0.350	0.90	1.00	2.000	Yes
798	52.38	3.03	1.35	1.68	0.73	0.470	1.34	0.350	0.90	1.00	2.000	Yes
799	52.47	3.04	1.36	1.68	0.73	0.470	1.34	0.349	0.90	1.00	2.000	Yes
800	52.51	3.04	1.36	1.69	0.73	0.469	1.34	0.349	0.90	1.00	2.000	Yes
801	52.56	3.05	1.36	1.69	0.73	0.469	1.34	0.349	0.90	1.00	2.000	Yes
802	52.66	3.05	1.36	1.69	0.73	0.469	1.34	0.349	0.90	1.00	2.000	Yes
803	52.70	3.06	1.36	1.69	0.73	0.468	1.34	0.348	0.90	1.00	2.000	Yes
804	52.77	3.06	1.37	1.69	0.72	0.468	1.34	0.348	0.90	1.00	2.000	Yes
805	52.87	3.07	1.37	1.70	0.72	0.467	1.34	0.348	0.90	1.00	2.000	Yes
806	52.92	3.07	1.37	1.70	0.72	0.467	1.34	0.347	0.90	1.00	2.000	Yes
807	52.97	3.07	1.37	1.70	0.72	0.467	1.34	0.347	0.90	1.00	2.000	Yes
808	53.02	3.08	1.37	1.70	0.72	0.467	1.34	0.347	0.90	1.00	2.000	Yes
809	53.10	3.08	1.38	1.70	0.72	0.466	1.34	0.347	0.90	1.00	2.000	Yes
810	53.16	3.08	1.38	1.71	0.72	0.466	1.34	0.346	0.90	1.00	2.000	No
811	53.22	3.09	1.38	1.71	0.72	0.466	1.34	0.346	0.90	1.00	2.000	No
812	53.31	3.09	1.38	1.71	0.72	0.465	1.34	0.346	0.90	1.00	2.000	No
813	53.36	3.10	1.38	1.71	0.72	0.465	1.34	0.346	0.90	1.00	2.000	No
814	53.42	3.10	1.39	1.71	0.72	0.465	1.34	0.345	0.89	1.00	2.000	No
815	53.51	3.11	1.39	1.72	0.72	0.464	1.34	0.345	0.89	1.00	2.000	No
816	53.56	3.11	1.39	1.72	0.72	0.464	1.34	0.345	0.89	1.00	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
817	53.62	3.11	1.39	1.72	0.72	0.464	1.34	0.345	0.89	1.00	2.000	No
818	53.71	3.12	1.39	1.72	0.72	0.463	1.34	0.344	0.89	1.00	2.000	No
819	53.75	3.12	1.40	1.72	0.72	0.463	1.34	0.344	0.89	1.00	2.000	No
820	53.83	3.12	1.40	1.73	0.71	0.462	1.34	0.344	0.89	1.00	2.000	No
821	53.91	3.13	1.40	1.73	0.71	0.462	1.34	0.344	0.89	1.00	2.000	No
822	53.98	3.13	1.40	1.73	0.71	0.462	1.34	0.343	0.89	1.00	2.000	No
823	54.01	3.13	1.40	1.73	0.71	0.462	1.34	0.343	0.89	1.00	2.000	No
824	54.11	3.14	1.41	1.73	0.71	0.461	1.34	0.343	0.89	1.00	2.000	No
825	54.15	3.14	1.41	1.73	0.71	0.461	1.34	0.343	0.89	1.00	2.000	No
826	54.21	3.15	1.41	1.74	0.71	0.461	1.34	0.343	0.89	1.00	2.000	No
827	54.27	3.15	1.41	1.74	0.71	0.460	1.34	0.342	0.89	1.00	2.000	No
828	54.35	3.15	1.41	1.74	0.71	0.460	1.34	0.342	0.89	1.00	2.000	No
829	54.42	3.16	1.42	1.74	0.71	0.460	1.34	0.342	0.89	1.00	2.000	No
830	54.46	3.16	1.42	1.74	0.71	0.459	1.34	0.342	0.89	1.00	2.000	No
831	54.55	3.17	1.42	1.74	0.71	0.459	1.34	0.341	0.89	1.00	2.000	No
832	54.60	3.17	1.42	1.75	0.71	0.459	1.34	0.341	0.89	1.00	2.000	No
833	54.67	3.17	1.42	1.75	0.71	0.459	1.34	0.341	0.89	1.00	2.000	No
834	54.74	3.18	1.43	1.75	0.71	0.458	1.34	0.341	0.89	1.00	2.000	No
835	54.79	3.18	1.43	1.75	0.71	0.458	1.34	0.341	0.89	1.00	2.000	No
836	54.86	3.18	1.43	1.75	0.70	0.458	1.34	0.340	0.89	1.00	2.000	No
837	54.96	3.19	1.43	1.75	0.70	0.457	1.34	0.340	0.89	1.00	2.000	No
838	55.03	3.19	1.44	1.76	0.70	0.457	1.34	0.340	0.89	1.00	2.000	No
839	55.06	3.19	1.44	1.76	0.70	0.457	1.34	0.340	0.89	1.00	2.000	No
840	55.14	3.20	1.44	1.76	0.70	0.457	1.34	0.340	0.89	1.00	2.000	No
841	55.21	3.20	1.44	1.76	0.70	0.456	1.34	0.339	0.89	1.00	2.000	No
842	55.25	3.20	1.44	1.76	0.70	0.456	1.34	0.339	0.89	1.00	2.000	No
843	55.32	3.21	1.45	1.76	0.70	0.456	1.34	0.339	0.89	1.00	2.000	No
844	55.41	3.21	1.45	1.76	0.70	0.455	1.34	0.339	0.89	1.00	2.000	No
845	55.45	3.21	1.45	1.76	0.70	0.455	1.34	0.339	0.89	1.00	2.000	No
846	55.52	3.22	1.45	1.77	0.70	0.455	1.34	0.338	0.89	1.00	2.000	No
847	55.61	3.22	1.45	1.77	0.70	0.454	1.34	0.338	0.89	1.00	2.000	No
848	55.65	3.22	1.46	1.77	0.70	0.454	1.34	0.338	0.89	1.00	2.000	No
849	55.71	3.23	1.46	1.77	0.70	0.454	1.34	0.338	0.89	1.00	2.000	No
850	55.80	3.23	1.46	1.77	0.70	0.454	1.34	0.337	0.89	1.00	2.000	No
851	55.86	3.24	1.46	1.77	0.70	0.453	1.34	0.337	0.89	1.00	2.000	No
852	55.95	3.24	1.46	1.78	0.69	0.453	1.34	0.337	0.89	1.00	2.000	No
853	56.00	3.24	1.47	1.78	0.69	0.453	1.34	0.337	0.89	1.00	2.000	No
854	56.05	3.25	1.47	1.78	0.69	0.453	1.34	0.337	0.89	1.00	2.000	No
855	56.11	3.25	1.47	1.78	0.69	0.452	1.34	0.336	0.89	1.00	2.000	No
856	56.20	3.26	1.47	1.78	0.69	0.452	1.34	0.336	0.89	1.00	2.000	No
857	56.24	3.26	1.47	1.78	0.69	0.452	1.34	0.336	0.89	1.00	2.000	No
858	56.31	3.26	1.48	1.79	0.69	0.451	1.34	0.336	0.89	1.00	2.000	No
859	56.39	3.27	1.48	1.79	0.69	0.451	1.34	0.335	0.89	1.00	2.000	No
860	56.43	3.27	1.48	1.79	0.69	0.451	1.34	0.335	0.89	1.00	2.000	No
861	56.50	3.27	1.48	1.79	0.69	0.451	1.34	0.335	0.89	1.00	2.000	No
862	56.60	3.28	1.49	1.79	0.69	0.450	1.34	0.335	0.89	1.00	2.000	No
863	56.66	3.28	1.49	1.79	0.69	0.450	1.34	0.335	0.89	1.00	2.000	No
864	56.70	3.28	1.49	1.79	0.69	0.450	1.34	0.334	0.89	1.00	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
865	56.79	3.29	1.49	1.80	0.69	0.449	1.34	0.334	0.89	1.00	2.000	No
866	56.84	3.29	1.49	1.80	0.69	0.449	1.34	0.334	0.89	1.00	2.000	No
867	56.92	3.29	1.50	1.80	0.69	0.449	1.34	0.334	0.89	1.00	2.000	No
868	56.99	3.30	1.50	1.80	0.69	0.448	1.34	0.334	0.88	1.00	2.000	No
869	57.03	3.30	1.50	1.80	0.68	0.448	1.34	0.333	0.88	1.00	2.000	No
870	57.09	3.30	1.50	1.80	0.68	0.448	1.34	0.333	0.88	1.00	2.000	No
871	57.18	3.31	1.50	1.81	0.68	0.448	1.34	0.333	0.88	1.00	2.000	No
872	57.23	3.31	1.50	1.81	0.68	0.447	1.34	0.333	0.88	1.00	2.000	No
873	57.31	3.32	1.51	1.81	0.68	0.447	1.34	0.332	0.88	1.00	2.000	No
874	57.38	3.32	1.51	1.81	0.68	0.447	1.34	0.332	0.88	1.00	2.000	Yes
875	57.43	3.32	1.51	1.81	0.68	0.447	1.34	0.332	0.88	1.00	2.000	Yes
876	57.50	3.33	1.51	1.81	0.68	0.446	1.34	0.332	0.88	1.00	2.000	Yes
877	57.58	3.33	1.52	1.82	0.68	0.446	1.34	0.332	0.88	1.00	2.000	Yes
878	57.62	3.33	1.52	1.82	0.68	0.446	1.34	0.331	0.88	1.00	2.000	Yes
879	57.68	3.34	1.52	1.82	0.68	0.445	1.34	0.331	0.88	1.00	2.000	Yes
880	57.78	3.34	1.52	1.82	0.68	0.445	1.34	0.331	0.88	1.00	2.000	Yes
881	57.82	3.35	1.52	1.82	0.68	0.445	1.34	0.331	0.88	1.00	2.000	Yes
882	57.89	3.35	1.53	1.83	0.68	0.444	1.34	0.330	0.88	1.00	2.000	Yes
883	57.97	3.36	1.53	1.83	0.68	0.444	1.34	0.330	0.88	1.00	2.000	Yes
884	58.02	3.36	1.53	1.83	0.68	0.444	1.34	0.330	0.88	1.00	2.000	Yes
885	58.09	3.36	1.53	1.83	0.68	0.443	1.34	0.330	0.88	1.00	2.000	No
886	58.17	3.37	1.53	1.83	0.67	0.443	1.34	0.329	0.88	1.00	2.000	No
887	58.23	3.37	1.54	1.84	0.67	0.443	1.34	0.329	0.88	1.00	2.000	No
888	58.28	3.38	1.54	1.84	0.67	0.442	1.34	0.329	0.88	1.00	2.000	No
889	58.37	3.38	1.54	1.84	0.67	0.442	1.34	0.329	0.88	1.00	2.000	Yes
890	58.43	3.39	1.54	1.84	0.67	0.442	1.34	0.328	0.88	1.00	2.000	Yes
891	58.48	3.39	1.54	1.84	0.67	0.441	1.34	0.328	0.88	1.00	2.000	Yes
892	58.57	3.39	1.55	1.85	0.67	0.441	1.34	0.328	0.88	1.00	2.000	Yes
893	58.62	3.40	1.55	1.85	0.67	0.441	1.34	0.328	0.88	1.00	2.000	Yes
894	58.67	3.40	1.55	1.85	0.67	0.440	1.34	0.327	0.88	1.00	2.000	Yes
895	58.78	3.41	1.55	1.85	0.67	0.440	1.34	0.327	0.88	1.00	2.000	Yes
896	58.82	3.41	1.55	1.86	0.67	0.440	1.34	0.327	0.88	1.00	2.000	Yes
897	58.88	3.41	1.56	1.86	0.67	0.439	1.34	0.327	0.88	1.00	2.000	Yes
898	58.97	3.42	1.56	1.86	0.67	0.439	1.34	0.326	0.88	1.00	2.000	Yes
899	59.01	3.42	1.56	1.86	0.67	0.439	1.34	0.326	0.88	1.00	2.000	Yes
900	59.07	3.43	1.56	1.86	0.67	0.438	1.34	0.326	0.88	1.00	2.000	Yes
901	59.12	3.43	1.56	1.87	0.67	0.438	1.34	0.326	0.88	1.00	2.000	Yes
902	59.19	3.43	1.57	1.87	0.67	0.438	1.34	0.326	0.88	1.00	2.000	Yes
903	59.27	3.44	1.57	1.87	0.67	0.437	1.34	0.325	0.88	1.00	2.000	No
904	59.32	3.44	1.57	1.87	0.66	0.437	1.34	0.325	0.88	1.00	2.000	No
905	59.42	3.45	1.57	1.87	0.66	0.437	1.34	0.325	0.88	1.00	2.000	No
906	59.47	3.45	1.57	1.88	0.66	0.436	1.34	0.325	0.88	1.00	2.000	No
907	59.52	3.45	1.58	1.88	0.66	0.436	1.34	0.324	0.88	1.00	2.000	No
908	59.58	3.46	1.58	1.88	0.66	0.436	1.34	0.324	0.88	1.00	2.000	No
909	59.68	3.46	1.58	1.88	0.66	0.435	1.34	0.324	0.88	1.00	2.000	No
910	59.74	3.47	1.58	1.88	0.66	0.435	1.34	0.324	0.88	1.00	2.000	Yes
911	59.78	3.47	1.58	1.88	0.66	0.435	1.34	0.324	0.88	1.00	2.000	Yes
912	59.88	3.47	1.59	1.89	0.66	0.435	1.34	0.323	0.88	1.00	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
913	59.93	3.48	1.59	1.89	0.66	0.434	1.34	0.323	0.88	1.00	2.000	Yes
914	60.00	3.48	1.59	1.89	0.66	0.434	1.34	0.323	0.88	1.00	2.000	Yes
915	60.05	3.48	1.59	1.89	0.66	0.434	1.34	0.323	0.87	1.00	2.000	Yes
916	60.13	3.49	1.60	1.89	0.66	0.433	1.34	0.322	0.87	1.00	2.000	Yes
917	60.18	3.49	1.60	1.90	0.66	0.433	1.34	0.322	0.87	1.00	2.000	Yes
918	60.25	3.50	1.60	1.90	0.66	0.433	1.34	0.322	0.87	1.00	2.000	Yes
919	60.33	3.50	1.60	1.90	0.66	0.433	1.34	0.322	0.87	1.00	2.000	No
920	60.38	3.50	1.60	1.90	0.66	0.433	1.34	0.322	0.87	1.00	2.000	No

Abbreviations

Depth: Depth from free surface, at which CPT was performed (ft)
σ_v: Total overburden pressure at test point (tsf)
u_0: Water pressure at test point (tsf)
σ_v': Effective overburden pressure based on GWT during earthquake (tsf)
r_d: Nonlinear shear mass factor
CSR: Cyclic Stress Ratio
MSF: Magnitude Scaling Factor
CSR_{eq}: CSR adjusted for M=7.5
K_σ: Effective overburden stress factor
CSR^*: CSR fully adjusted

:: Cyclic Resistance Ratio (CRR) calculation data ::

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
1	0.10	15.36	2.46	1.25	0.81	24.68	2.58	63.55	4.000	No	No	2.00
2	0.16	18.18	2.37	1.13	0.78	29.20	2.21	64.47	4.000	No	No	2.00
3	0.21	20.36	2.31	1.04	0.76	32.69	2.00	65.27	4.000	No	No	2.00
4	0.29	21.38	2.29	1.01	0.75	34.33	1.91	65.70	4.000	No	No	2.00
5	0.36	22.80	2.25	0.95	0.73	36.60	1.80	66.00	4.000	No	No	2.00
6	0.40	26.01	2.19	0.88	0.71	41.75	1.63	68.26	4.000	No	No	2.00
7	0.51	29.38	2.13	0.85	0.69	47.16	1.52	71.49	4.000	No	No	2.00
8	0.57	32.38	2.09	0.84	0.67	51.97	1.44	75.04	4.000	No	No	2.00
9	0.61	35.46	2.07	0.85	0.66	56.92	1.40	79.41	4.000	No	No	2.00
10	0.70	38.31	2.05	0.91	0.66	61.48	1.38	84.75	4.000	No	No	2.00
11	0.76	40.98	2.05	0.99	0.66	65.78	1.37	90.30	4.000	No	No	2.00
12	0.81	43.44	2.05	1.08	0.66	69.72	1.38	96.06	4.000	No	No	2.00
13	0.87	45.02	2.07	1.21	0.66	72.26	1.41	101.55	4.000	No	No	2.00
14	0.96	46.00	2.09	1.35	0.67	73.82	1.44	106.65	4.000	No	No	2.00
15	1.00	46.15	2.12	1.49	0.68	74.05	1.50	110.83	4.000	No	No	2.00
16	1.05	45.49	2.15	1.63	0.69	72.99	1.56	113.61	4.000	No	No	2.00
17	1.16	44.58	2.18	1.75	0.71	71.53	1.62	115.80	4.000	No	No	2.00
18	1.20	43.39	2.21	1.86	0.72	69.61	1.68	117.12	4.000	No	No	2.00
19	1.26	42.04	2.23	1.93	0.72	67.43	1.73	116.97	4.000	No	No	2.00
20	1.35	40.70	2.24	1.98	0.73	65.27	1.78	116.40	4.000	No	No	2.00
21	1.40	39.42	2.26	2.01	0.74	63.22	1.83	115.37	4.000	No	No	2.00
22	1.45	38.31	2.27	2.01	0.74	61.42	1.85	113.69	4.000	No	No	2.00
23	1.55	36.98	2.28	2.01	0.74	59.27	1.89	111.93	4.000	Yes	No	2.00
24	1.60	35.41	2.30	2.04	0.75	56.74	1.95	110.41	4.000	Yes	No	2.00
25	1.64	33.59	2.33	2.12	0.76	53.81	2.04	109.72	4.000	Yes	No	2.00
26	1.71	31.62	2.36	2.23	0.77	50.64	2.16	109.52	4.000	Yes	No	2.00
27	1.79	29.70	2.40	2.37	0.79	47.55	2.31	109.74	4.000	Yes	No	2.00
28	1.87	28.02	2.44	2.54	0.80	44.86	2.47	110.96	4.000	Yes	No	2.00
29	1.95	26.09	2.49	2.76	0.82	41.75	2.70	112.56	4.000	Yes	No	2.00
30	2.00	24.07	2.54	3.03	0.84	38.50	2.97	114.43	4.000	Yes	No	2.00
31	2.04	22.09	2.59	3.32	0.86	35.30	3.29	116.10	4.000	Yes	No	2.00
32	2.11	20.34	2.64	3.61	0.88	32.49	3.61	117.33	4.000	Yes	Yes	2.00
33	2.19	18.97	2.69	3.87	0.90	30.28	3.91	118.26	4.000	Yes	Yes	2.00
34	2.24	17.93	2.72	4.08	0.91	28.61	4.15	118.85	4.000	Yes	Yes	2.00
35	2.30	17.03	2.75	4.27	0.92	27.15	4.39	119.14	4.000	Yes	Yes	2.00
36	2.38	16.21	2.78	4.46	0.93	25.83	4.62	119.35	4.000	Yes	Yes	2.00
37	2.45	15.52	2.80	4.62	0.94	24.71	4.82	119.16	4.000	Yes	Yes	2.00
38	2.50	15.08	2.82	4.71	0.95	24.00	4.95	118.88	4.000	Yes	Yes	2.00
39	2.58	14.72	2.83	4.78	0.95	23.42	5.06	118.54	4.000	No	Yes	2.00
40	2.64	14.48	2.84	4.81	0.96	23.03	5.13	118.11	4.000	No	Yes	2.00
41	2.69	14.36	2.84	4.75	0.96	22.83	5.12	116.92	4.000	No	Yes	2.00
42	2.79	14.25	2.83	4.64	0.96	22.65	5.08	115.12	4.000	No	Yes	2.00
43	2.85	14.17	2.83	4.50	0.95	22.50	5.02	112.97	4.000	No	Yes	2.00
44	2.90	13.76	2.83	4.39	0.95	21.84	5.04	110.17	4.000	No	Yes	2.00
45	2.98	13.13	2.84	4.28	0.96	20.82	5.12	106.59	4.000	No	Yes	2.00
46	3.05	12.47	2.85	4.13	0.96	19.76	5.18	102.45	4.000	No	Yes	2.00
47	3.09	11.81	2.85	3.93	0.96	18.69	5.23	97.68	4.000	No	Yes	2.00
48	3.17	11.04	2.86	3.74	0.96	17.45	5.32	92.83	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
49	3.24	10.27	2.87	3.56	0.97	16.21	5.42	87.93	4.000	No	Yes	2.00
50	3.29	9.66	2.88	3.40	0.97	15.22	5.52	83.96	4.000	No	Yes	2.00
51	3.36	9.23	2.89	3.31	0.98	14.52	5.60	81.34	4.000	No	Yes	2.00
52	3.44	8.90	2.90	3.24	0.98	13.99	5.68	79.42	4.000	No	Yes	2.00
53	3.48	9.04	2.89	3.19	0.98	14.21	5.59	79.36	4.000	No	Yes	2.00
54	3.56	9.43	2.88	3.24	0.97	14.82	5.48	81.26	4.000	No	Yes	2.00
55	3.64	9.85	2.87	3.36	0.97	15.50	5.43	84.14	4.000	No	Yes	2.00
56	3.69	10.29	2.87	3.57	0.97	16.20	5.44	88.06	4.000	No	Yes	2.00
57	3.76	10.82	2.87	3.76	0.97	17.04	5.40	92.12	4.000	No	Yes	2.00
58	3.84	11.33	2.87	3.97	0.97	17.85	5.40	96.35	4.000	No	Yes	2.00
59	3.88	11.63	2.88	4.23	0.97	18.33	5.48	100.41	4.000	No	Yes	2.00
60	3.98	11.73	2.89	4.49	0.98	18.49	5.61	103.76	4.000	No	Yes	2.00
61	4.03	11.65	2.91	4.81	0.99	18.35	5.83	106.89	4.000	No	Yes	2.00
62	4.08	11.56	2.93	5.08	0.99	18.20	6.01	109.42	4.000	No	Yes	2.00
63	4.14	11.46	2.95	5.30	1.00	18.03	6.17	111.18	4.000	No	Yes	2.00
64	4.23	11.31	2.96	5.50	1.00	17.80	6.32	112.52	4.000	No	Yes	2.00
65	4.27	11.11	2.98	5.67	1.00	17.46	6.48	113.17	4.000	No	Yes	2.00
66	4.36	10.88	2.99	5.80	1.00	17.08	6.63	113.32	4.000	No	Yes	2.00
67	4.41	10.61	3.00	5.92	1.00	16.64	6.79	113.06	4.000	No	Yes	2.00
68	4.46	10.35	3.02	6.01	1.00	16.22	6.93	112.50	4.000	No	Yes	2.00
69	4.55	10.12	3.03	6.06	1.00	15.85	7.05	111.73	4.000	No	Yes	2.00
70	4.61	10.03	3.03	6.00	1.00	15.70	7.06	110.75	4.000	No	Yes	2.00
71	4.66	9.83	3.03	5.97	1.00	15.37	7.11	109.37	4.000	No	Yes	2.00
72	4.75	9.64	3.04	5.93	1.00	15.06	7.17	107.97	4.000	No	Yes	2.00
73	4.80	9.49	3.04	5.88	1.00	14.82	7.20	106.75	4.000	No	Yes	2.00
74	4.86	9.44	3.04	5.78	1.00	14.73	7.17	105.64	4.000	No	Yes	2.00
75	4.96	9.44	3.03	5.67	1.00	14.72	7.11	104.71	4.000	No	Yes	2.00
76	5.01	9.55	3.02	5.51	1.00	14.90	6.97	103.88	4.000	No	Yes	2.00
77	5.06	9.80	3.00	5.29	1.00	15.29	6.74	103.13	4.000	No	Yes	2.00
78	5.16	10.15	2.98	5.05	1.00	15.84	6.47	102.54	4.000	No	Yes	2.00
79	5.21	10.54	2.95	4.81	1.00	16.46	6.20	102.01	4.000	No	Yes	2.00
80	5.26	10.94	2.93	4.63	0.99	17.10	5.95	101.76	4.000	No	Yes	2.00
81	5.32	11.28	2.90	4.45	0.98	17.64	5.74	101.29	4.000	No	Yes	2.00
82	5.41	11.50	2.89	4.32	0.98	18.00	5.59	100.63	4.000	No	Yes	2.00
83	5.46	11.59	2.88	4.23	0.97	18.14	5.52	100.02	4.000	No	Yes	2.00
84	5.52	11.55	2.88	4.20	0.97	18.07	5.51	99.48	4.000	No	Yes	2.00
85	5.60	11.35	2.89	4.24	0.98	17.72	5.59	99.14	4.000	No	Yes	2.00
86	5.66	11.02	2.91	4.34	0.98	17.19	5.76	98.96	4.000	No	Yes	2.00
87	5.71	10.61	2.93	4.49	0.99	16.53	5.98	98.90	4.000	No	Yes	2.00
88	5.81	10.22	2.95	4.68	1.00	15.90	6.24	99.15	4.000	No	Yes	2.00
89	5.89	9.86	2.98	4.89	1.00	15.32	6.50	99.57	4.000	No	Yes	2.00
90	5.91	9.60	3.00	5.14	1.00	14.90	6.75	100.59	4.000	No	Yes	2.00
91	6.00	9.50	3.02	5.35	1.00	14.72	6.92	101.89	4.000	No	Yes	2.00
92	6.06	9.56	3.02	5.51	1.00	14.81	6.99	103.57	4.000	No	Yes	2.00
93	6.11	9.75	3.02	5.63	1.00	15.12	6.99	105.64	4.000	No	Yes	2.00
94	6.20	10.06	3.02	5.72	1.00	15.61	6.92	107.97	4.000	No	Yes	2.00
95	6.24	10.37	3.01	5.81	1.00	16.10	6.85	110.35	4.000	No	Yes	2.00
96	6.30	10.62	3.01	5.90	1.00	16.49	6.81	112.39	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
97	6.38	10.79	3.01	6.00	1.00	16.76	6.81	114.12	4.000	No	Yes	2.00
98	6.46	10.91	3.01	6.08	1.00	16.94	6.82	115.45	4.000	No	Yes	2.00
99	6.50	10.94	3.01	6.14	1.00	16.98	6.84	116.11	4.000	No	Yes	2.00
100	6.60	10.90	3.01	6.20	1.00	16.91	6.88	116.40	4.000	No	Yes	2.00
101	6.63	10.77	3.02	6.24	1.00	16.70	6.95	116.12	4.000	No	Yes	2.00
102	6.72	10.55	3.03	6.26	1.00	16.34	7.04	115.09	4.000	No	Yes	2.00
103	6.80	10.30	3.03	6.24	1.00	15.93	7.13	113.56	4.000	No	Yes	2.00
104	6.84	10.05	3.04	6.20	1.00	15.53	7.20	111.82	4.000	No	Yes	2.00
105	6.90	9.79	3.05	6.17	1.00	15.11	7.29	110.15	4.000	No	Yes	2.00
106	7.00	9.55	3.05	6.14	1.00	14.71	7.38	108.54	4.000	No	Yes	2.00
107	7.04	9.31	3.06	6.13	1.00	14.33	7.48	107.12	4.000	No	Yes	2.00
108	7.09	9.08	3.07	6.13	1.00	13.96	7.58	105.77	4.000	No	Yes	2.00
109	7.20	8.89	3.08	6.13	1.00	13.63	7.68	104.61	4.000	No	Yes	2.00
110	7.24	8.72	3.09	6.12	1.00	13.35	7.75	103.54	4.000	No	Yes	2.00
111	7.30	8.61	3.09	6.11	1.00	13.17	7.80	102.79	4.000	No	Yes	2.00
112	7.39	8.52	3.09	6.09	1.00	13.02	7.84	102.04	4.000	No	Yes	2.00
113	7.43	8.43	3.10	6.07	1.00	12.87	7.88	101.39	4.000	No	Yes	2.00
114	7.50	8.39	3.10	6.04	1.00	12.81	7.88	100.85	4.000	No	Yes	2.00
115	7.59	8.35	3.10	6.00	1.00	12.74	7.88	100.32	4.000	No	Yes	2.00
116	7.64	8.35	3.09	5.93	1.00	12.73	7.84	99.80	4.000	No	Yes	2.00
117	7.70	8.37	3.09	5.86	1.00	12.76	7.79	99.38	4.000	No	Yes	2.00
118	7.79	8.41	3.08	5.75	1.00	12.81	7.71	98.76	4.000	No	Yes	2.00
119	7.83	8.43	3.08	5.64	1.00	12.84	7.63	98.02	4.000	No	Yes	2.00
120	7.90	8.45	3.07	5.53	1.00	12.87	7.56	97.27	4.000	No	Yes	2.00
121	7.94	8.50	3.06	5.42	1.00	12.95	7.46	96.63	4.000	No	Yes	2.00
122	8.03	8.53	3.05	5.28	1.00	12.98	7.37	95.64	4.000	No	Yes	2.00
123	8.11	8.52	3.05	5.12	1.00	12.96	7.28	94.29	4.000	No	Yes	2.00
124	8.17	8.50	3.04	4.94	1.00	12.93	7.17	92.70	4.000	No	Yes	2.00
125	8.21	8.43	3.03	4.76	1.00	12.81	7.09	90.83	4.000	No	Yes	2.00
126	8.28	8.32	3.03	4.58	1.00	12.62	7.03	88.68	4.000	No	Yes	2.00
127	8.37	8.16	3.02	4.42	1.00	12.36	7.00	86.47	4.000	No	Yes	2.00
128	8.41	7.97	3.02	4.26	1.00	12.06	6.98	84.20	4.000	No	Yes	2.00
129	8.48	7.72	3.02	4.12	1.00	11.65	7.02	81.74	4.000	No	Yes	2.00
130	8.57	7.42	3.03	3.99	1.00	11.15	7.09	79.06	4.000	No	Yes	2.00
131	8.61	7.14	3.04	3.87	1.00	10.70	7.17	76.70	4.000	No	Yes	2.00
132	8.67	6.87	3.05	3.77	1.00	10.26	7.26	74.54	4.000	No	Yes	2.00
133	8.77	6.62	3.05	3.70	1.00	9.85	7.37	72.60	4.000	No	Yes	2.00
134	8.81	6.40	3.06	3.65	1.00	9.50	7.48	71.07	4.000	No	Yes	2.00
135	8.87	6.27	3.07	3.59	1.00	9.29	7.53	69.97	4.000	No	Yes	2.00
136	8.96	6.21	3.07	3.54	1.00	9.17	7.55	69.19	4.000	No	Yes	2.00
137	8.99	6.25	3.06	3.46	1.00	9.23	7.45	68.74	4.000	No	Yes	2.00
138	9.07	6.38	3.04	3.34	1.00	9.45	7.25	68.47	4.000	No	Yes	2.00
139	9.16	6.56	3.02	3.21	1.00	9.73	7.01	68.19	4.000	No	Yes	2.00
140	9.21	6.75	3.00	3.06	1.00	10.03	6.75	67.73	4.000	No	Yes	2.00
141	9.27	6.95	2.98	2.92	1.00	10.34	6.50	67.24	4.000	No	Yes	2.00
142	9.36	7.12	2.96	2.81	1.00	10.61	6.31	66.90	4.000	No	Yes	2.00
143	9.40	7.28	2.94	2.71	1.00	10.86	6.13	66.54	4.000	No	Yes	2.00
144	9.48	7.42	2.93	2.66	0.99	11.08	6.00	66.51	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
145	9.52	7.61	2.92	2.67	0.99	11.38	5.91	67.29	4.000	No	Yes	2.00
146	9.61	7.88	2.91	2.68	0.98	11.80	5.79	68.36	4.000	No	Yes	2.00
147	9.65	8.20	2.90	2.73	0.98	12.31	5.69	70.02	4.000	No	Yes	2.00
148	9.72	8.71	2.89	2.83	0.97	13.12	5.56	72.94	4.000	No	Yes	2.00
149	9.81	9.31	2.87	2.94	0.97	14.09	5.41	76.25	4.000	No	Yes	2.00
150	9.86	10.14	2.85	3.10	0.96	15.41	5.25	80.94	4.000	No	Yes	2.00
151	9.91	11.02	2.83	3.25	0.95	16.83	5.08	85.53	4.000	No	Yes	2.00
152	10.00	11.92	2.82	3.38	0.95	18.26	4.93	90.08	4.000	No	Yes	2.00
153	10.05	12.98	2.80	3.51	0.94	19.95	4.76	94.97	4.000	No	Yes	2.00
154	10.16	14.05	2.78	3.61	0.93	21.67	4.59	99.56	4.000	No	Yes	2.00
155	10.20	15.10	2.76	3.69	0.93	23.35	4.44	103.70	4.000	No	Yes	2.00
156	10.25	16.16	2.74	3.75	0.92	25.05	4.30	107.64	4.000	No	Yes	2.00
157	10.31	17.03	2.73	3.81	0.91	26.44	4.20	111.04	4.000	No	Yes	2.00
158	10.40	17.83	2.72	3.88	0.91	27.73	4.12	114.17	4.000	No	Yes	2.00
159	10.44	18.60	2.70	3.88	0.91	28.95	4.02	116.36	4.000	No	Yes	2.00
160	10.51	19.07	2.69	3.88	0.90	29.70	3.96	117.57	4.000	No	Yes	2.00
161	10.59	19.49	2.68	3.84	0.90	30.36	3.88	117.93	4.000	No	Yes	2.00
162	10.65	19.75	2.68	3.77	0.90	30.58	3.83	117.21	4.000	No	Yes	2.00
163	10.71	19.91	2.67	3.69	0.89	30.63	3.78	115.91	4.000	No	Yes	2.00
164	10.80	20.00	2.67	3.68	0.89	30.53	3.79	115.58	4.000	No	Yes	2.00
165	10.85	20.00	2.67	3.69	0.89	30.40	3.80	115.50	4.000	No	Yes	2.00
166	10.90	19.65	2.68	3.76	0.90	29.79	3.89	115.78	4.000	No	Yes	2.00
167	10.96	19.02	2.71	3.92	0.91	28.80	4.05	116.70	4.000	No	Yes	2.00
168	11.04	18.63	2.73	4.05	0.91	28.09	4.18	117.49	4.000	No	Yes	2.00
169	11.10	18.54	2.74	4.19	0.92	27.88	4.28	119.21	4.000	No	Yes	2.00
170	11.18	18.55	2.75	4.36	0.92	27.77	4.37	121.48	4.000	No	Yes	2.00
171	11.24	18.66	2.76	4.50	0.93	27.84	4.45	123.77	4.000	No	Yes	2.00
172	11.30	18.82	2.77	4.66	0.93	27.98	4.51	126.31	4.000	No	Yes	2.00
173	11.35	19.00	2.77	4.79	0.93	28.17	4.56	128.55	4.000	No	Yes	2.00
174	11.42	19.22	2.78	4.91	0.93	28.35	4.61	130.69	4.000	No	Yes	2.00
175	11.51	19.84	2.77	4.91	0.93	29.02	4.55	132.02	4.000	No	Yes	2.00
176	11.55	20.77	2.75	4.79	0.92	30.20	4.39	132.54	4.000	No	Yes	2.00
177	11.62	21.32	2.74	4.74	0.92	30.79	4.31	132.86	4.000	No	Yes	2.00
178	11.71	21.83	2.73	4.69	0.92	31.26	4.25	132.97	4.000	No	Yes	2.00
179	11.75	22.14	2.73	4.67	0.92	31.58	4.22	133.24	4.000	No	Yes	2.00
180	11.85	22.14	2.73	4.71	0.92	31.34	4.26	133.38	4.000	No	Yes	2.00
181	11.90	22.04	2.74	4.74	0.92	31.09	4.29	133.42	4.000	No	Yes	2.00
182	11.94	21.77	2.74	4.74	0.92	30.62	4.33	132.59	4.000	No	Yes	2.00
183	12.02	21.29	2.75	4.75	0.92	29.80	4.40	131.08	4.000	No	Yes	2.00
184	12.10	20.69	2.76	4.75	0.93	28.88	4.48	129.32	4.000	No	Yes	2.00
185	12.15	19.88	2.78	4.78	0.93	27.73	4.60	127.53	4.000	No	Yes	2.00
186	12.24	18.97	2.80	4.83	0.94	26.39	4.75	125.46	4.000	No	Yes	2.00
187	12.30	18.13	2.81	4.82	0.95	25.19	4.88	122.90	4.000	No	Yes	2.00
188	12.35	17.31	2.82	4.79	0.95	24.01	4.99	119.91	4.000	No	Yes	2.00
189	12.44	16.81	2.83	4.66	0.95	23.21	5.02	116.58	4.000	No	Yes	2.00
190	12.50	16.42	2.83	4.52	0.95	22.60	5.02	113.49	4.000	No	Yes	2.00
191	12.55	16.24	2.82	4.39	0.95	22.28	4.99	111.12	4.000	No	Yes	2.00
192	12.63	16.22	2.82	4.26	0.95	22.16	4.93	109.20	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
193	12.70	16.29	2.81	4.19	0.95	22.18	4.89	108.36	4.000	No	Yes	2.00
194	12.74	16.47	2.81	4.16	0.94	22.38	4.84	108.34	4.000	No	Yes	2.00
195	12.84	16.72	2.80	4.15	0.94	22.63	4.81	108.74	4.000	No	Yes	2.00
196	12.86	16.90	2.80	4.19	0.94	22.86	4.80	109.69	4.000	No	Yes	2.00
197	12.94	17.15	2.80	4.23	0.94	23.14	4.79	110.77	4.000	No	Yes	2.00
198	13.01	17.16	2.81	4.32	0.94	23.11	4.84	111.95	4.000	No	Yes	2.00
199	13.09	17.06	2.82	4.43	0.95	22.94	4.93	113.02	4.000	No	Yes	2.00
200	13.14	16.85	2.83	4.52	0.95	22.63	5.01	113.48	4.000	No	Yes	2.00
201	13.20	16.59	2.84	4.58	0.96	22.25	5.10	113.51	4.000	No	Yes	2.00
202	13.29	16.32	2.84	4.61	0.96	21.82	5.17	112.86	4.000	No	Yes	2.00
203	13.33	16.03	2.85	4.61	0.96	21.41	5.23	112.02	4.000	No	Yes	2.00
204	13.39	15.74	2.86	4.60	0.96	20.96	5.29	110.88	4.000	No	Yes	2.00
205	13.49	15.44	2.86	4.59	0.97	20.49	5.35	109.66	4.000	No	Yes	2.00
206	13.53	15.17	2.87	4.58	0.97	20.10	5.40	108.60	4.000	No	Yes	2.00
207	13.59	14.97	2.87	4.46	0.97	19.77	5.38	106.39	4.000	No	Yes	2.00
208	13.69	14.77	2.86	4.29	0.97	19.40	5.34	103.62	4.000	No	Yes	2.00
209	13.73	14.50	2.86	4.20	0.97	19.00	5.35	101.62	4.000	No	Yes	2.00
210	13.79	14.20	2.87	4.14	0.97	18.55	5.39	99.88	4.000	No	Yes	2.00
211	13.89	13.86	2.87	4.09	0.97	18.03	5.44	98.09	4.000	No	Yes	2.00
212	13.94	13.52	2.88	4.01	0.97	17.54	5.48	96.12	4.000	No	Yes	2.00
213	13.99	12.93	2.89	4.00	0.98	16.74	5.62	94.08	4.000	No	Yes	2.00
214	14.08	12.45	2.90	3.93	0.98	16.04	5.72	91.65	4.000	No	Yes	2.00
215	14.13	12.06	2.91	3.82	0.98	15.48	5.76	89.13	4.000	No	Yes	2.00
216	14.18	11.66	2.92	3.80	0.99	14.93	5.87	87.67	4.000	No	Yes	2.00
217	14.27	11.28	2.93	3.84	0.99	14.38	6.03	86.68	4.000	No	Yes	2.00
218	14.32	10.95	2.94	3.81	1.00	13.93	6.12	85.22	4.000	No	Yes	2.00
219	14.37	10.65	2.95	3.75	1.00	13.50	6.18	83.50	4.000	No	Yes	2.00
220	14.48	10.39	2.95	3.68	1.00	13.11	6.24	81.76	4.000	No	Yes	2.00
221	14.52	10.14	2.96	3.62	1.00	12.75	6.30	80.28	4.000	No	Yes	2.00
222	14.58	10.13	2.95	3.49	1.00	12.71	6.21	78.93	4.000	No	Yes	2.00
223	14.68	10.02	2.95	3.44	1.00	12.51	6.23	77.91	4.000	No	Yes	2.00
224	14.72	9.92	2.95	3.39	1.00	12.36	6.24	77.05	4.000	No	Yes	2.00
225	14.77	9.92	2.95	3.35	1.00	12.33	6.21	76.51	4.000	No	Yes	2.00
226	14.83	10.03	2.94	3.28	1.00	12.44	6.12	76.16	4.000	No	Yes	2.00
227	14.92	10.18	2.93	3.21	0.99	12.58	6.02	75.75	4.000	No	Yes	2.00
228	14.98	10.38	2.92	3.14	0.99	12.80	5.91	75.61	4.000	No	Yes	2.00
229	15.07	10.58	2.91	3.08	0.98	13.01	5.80	75.43	4.000	No	Yes	2.00
230	15.11	10.79	2.90	3.03	0.98	13.25	5.69	75.41	4.000	No	Yes	2.00
231	15.17	11.01	2.89	3.01	0.98	13.50	5.61	75.74	4.000	No	Yes	2.00
232	15.27	11.22	2.88	2.99	0.97	13.72	5.54	76.03	4.000	No	Yes	2.00
233	15.31	11.35	2.88	3.01	0.97	13.86	5.52	76.54	4.000	No	Yes	2.00
234	15.38	11.41	2.89	3.07	0.97	13.93	5.56	77.42	4.000	No	Yes	2.00
235	15.47	11.44	2.89	3.15	0.98	13.94	5.62	78.29	4.000	No	Yes	2.00
236	15.52	11.40	2.90	3.27	0.98	13.88	5.73	79.45	4.000	No	Yes	2.00
237	15.56	11.30	2.92	3.41	0.99	13.74	5.87	80.64	4.000	No	Yes	2.00
238	15.64	11.17	2.93	3.56	0.99	13.56	6.03	81.77	4.000	No	Yes	2.00
239	15.71	11.01	2.95	3.71	1.00	13.34	6.20	82.68	4.000	No	Yes	2.00
240	15.75	10.82	2.97	3.84	1.00	13.08	6.37	83.34	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
241	15.87	10.55	2.99	3.98	1.00	12.67	6.59	83.46	4.000	No	Yes	2.00
242	15.91	10.21	3.01	4.12	1.00	12.21	6.83	83.43	4.000	No	Yes	2.00
243	15.96	9.82	3.03	4.23	1.00	11.68	7.08	82.74	4.000	No	Yes	2.00
244	16.01	9.34	3.06	4.34	1.00	11.02	7.40	81.57	4.000	No	Yes	2.00
245	16.11	8.88	3.08	4.41	1.00	10.39	7.70	79.98	4.000	No	Yes	2.00
246	16.15	8.47	3.10	4.43	1.00	9.84	7.95	78.20	4.000	No	Yes	2.00
247	16.22	8.05	3.12	4.41	1.00	9.27	8.19	75.99	4.000	No	Yes	2.00
248	16.31	7.65	3.14	4.40	1.00	8.73	8.45	73.81	4.000	No	Yes	2.00
249	16.36	7.32	3.16	4.34	1.00	8.28	8.65	71.63	4.000	No	Yes	2.00
250	16.41	7.12	3.16	4.23	1.00	8.01	8.72	69.84	4.000	No	Yes	2.00
251	16.51	7.03	3.16	4.06	1.00	7.86	8.67	68.16	4.000	No	Yes	2.00
252	16.54	7.08	3.14	3.86	1.00	7.92	8.47	67.09	4.000	No	Yes	2.00
253	16.61	7.22	3.12	3.62	1.00	8.08	8.17	66.02	4.000	No	Yes	2.00
254	16.70	7.38	3.10	3.39	1.00	8.26	7.87	65.01	4.000	No	Yes	2.00
255	16.75	7.55	3.08	3.34	1.00	8.46	7.72	65.30	4.000	No	Yes	2.00
256	16.81	7.72	3.08	3.37	1.00	8.66	7.65	66.21	4.000	No	Yes	2.00
257	16.91	7.89	3.07	3.42	1.00	8.85	7.60	67.19	4.000	No	Yes	2.00
258	16.95	8.03	3.07	3.48	1.00	9.01	7.57	68.19	4.000	No	Yes	2.00
259	17.01	8.12	3.07	3.56	1.00	9.11	7.59	69.14	4.000	No	Yes	2.00
260	17.11	8.17	3.08	3.65	1.00	9.14	7.65	69.91	4.000	No	Yes	2.00
261	17.13	8.17	3.08	3.73	1.00	9.13	7.72	70.48	4.000	No	Yes	2.00
262	17.21	8.14	3.10	3.87	1.00	9.07	7.87	71.32	4.000	No	Yes	2.00
263	17.29	8.11	3.11	4.03	1.00	9.00	8.02	72.26	4.000	No	Yes	2.00
264	17.34	8.11	3.11	4.04	1.00	8.99	8.05	72.32	4.000	No	Yes	2.00
265	17.43	8.11	3.11	4.03	1.00	8.96	8.05	72.13	4.000	No	Yes	2.00
266	17.48	8.11	3.11	4.00	1.00	8.95	8.03	71.86	4.000	No	Yes	2.00
267	17.54	8.15	3.10	3.95	1.00	8.98	7.98	71.60	4.000	No	Yes	2.00
268	17.63	8.21	3.10	3.89	1.00	9.02	7.90	71.32	4.000	No	Yes	2.00
269	17.68	8.30	3.09	3.83	1.00	9.12	7.81	71.20	4.000	No	Yes	2.00
270	17.73	8.37	3.08	3.79	1.00	9.20	7.74	71.18	4.000	No	Yes	2.00
271	17.83	8.49	3.08	3.75	1.00	9.32	7.65	71.25	4.000	No	Yes	2.00
272	17.85	8.62	3.07	3.71	1.00	9.47	7.55	71.50	4.000	No	Yes	2.00
273	17.93	8.75	3.06	3.69	1.00	9.61	7.47	71.80	4.000	No	Yes	2.00
274	17.98	8.91	3.05	3.66	1.00	9.79	7.37	72.13	4.000	No	Yes	2.00
275	18.07	9.08	3.05	3.64	1.00	9.96	7.28	72.54	4.000	No	Yes	2.00
276	18.12	9.20	3.04	3.65	1.00	10.09	7.23	72.96	4.000	No	Yes	2.00
277	18.18	9.30	3.04	3.67	1.00	10.19	7.21	73.48	4.000	No	Yes	2.00
278	18.24	9.40	3.04	3.70	1.00	10.30	7.19	73.99	4.000	No	Yes	2.00
279	18.33	9.51	3.04	3.72	1.00	10.40	7.16	74.48	4.000	No	Yes	2.00
280	18.38	9.64	3.03	3.73	1.00	10.54	7.11	74.99	4.000	No	Yes	2.00
281	18.47	9.84	3.02	3.71	1.00	10.75	7.02	75.47	4.000	No	Yes	2.00
282	18.53	10.04	3.02	3.67	1.00	10.97	6.91	75.85	4.000	No	Yes	2.00
283	18.57	10.26	3.00	3.64	1.00	11.24	6.80	76.36	4.000	No	Yes	2.00
284	18.67	10.50	3.00	3.64	1.00	11.49	6.70	77.01	4.000	No	Yes	2.00
285	18.72	10.79	2.99	3.62	1.00	11.82	6.58	77.79	4.000	No	Yes	2.00
286	18.78	11.12	2.97	3.58	1.00	12.19	6.43	78.44	4.000	No	Yes	2.00
287	18.85	11.42	2.96	3.55	1.00	12.53	6.31	79.06	4.000	No	Yes	2.00
288	18.93	11.67	2.95	3.55	1.00	12.79	6.23	79.67	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
289	18.97	11.84	2.95	3.55	1.00	12.97	6.18	80.21	4.000	No	Yes	2.00
290	19.08	11.93	2.95	3.57	1.00	13.03	6.18	80.49	4.000	No	Yes	2.00
291	19.12	11.99	2.95	3.58	1.00	13.09	6.17	80.75	4.000	No	Yes	2.00
292	19.22	12.04	2.95	3.57	1.00	13.10	6.16	80.74	4.000	No	Yes	2.00
293	19.27	12.17	2.94	3.50	0.99	13.22	6.08	80.34	4.000	No	Yes	2.00
294	19.32	12.24	2.93	3.44	0.99	13.28	6.01	79.86	4.000	No	Yes	2.00
295	19.37	12.33	2.93	3.41	0.99	13.36	5.97	79.68	4.000	No	Yes	2.00
296	19.43	12.44	2.92	3.38	0.99	13.47	5.92	79.68	4.000	No	Yes	2.00
297	19.52	12.63	2.92	3.36	0.99	13.64	5.85	79.84	4.000	No	Yes	2.00
298	19.57	12.91	2.91	3.32	0.98	13.94	5.75	80.20	4.000	No	Yes	2.00
299	19.67	13.22	2.90	3.30	0.98	14.24	5.66	80.60	4.000	No	Yes	2.00
300	19.72	13.55	2.89	3.30	0.98	14.59	5.58	81.43	4.000	No	Yes	2.00
301	19.77	13.86	2.88	3.36	0.97	14.93	5.55	82.85	4.000	No	Yes	2.00
302	19.82	14.07	2.89	3.46	0.98	15.16	5.57	84.47	4.000	No	Yes	2.00
303	19.92	14.31	2.89	3.56	0.98	15.39	5.59	86.10	4.000	No	Yes	2.00
304	19.97	14.46	2.89	3.63	0.98	15.55	5.62	87.31	4.000	No	Yes	2.00
305	20.04	14.51	2.90	3.71	0.98	15.57	5.67	88.24	4.000	No	Yes	2.00
306	20.08	14.51	2.90	3.77	0.98	15.56	5.71	88.85	4.000	No	Yes	2.00
307	20.16	14.47	2.91	3.83	0.98	15.48	5.76	89.24	4.000	No	Yes	2.00
308	20.24	14.41	2.91	3.87	0.98	15.38	5.82	89.46	4.000	No	Yes	2.00
309	20.28	14.35	2.92	3.89	0.99	15.28	5.85	89.45	4.000	No	Yes	2.00
310	20.37	14.28	2.92	3.87	0.99	15.16	5.87	88.94	4.000	No	Yes	2.00
311	20.41	14.20	2.92	3.85	0.99	15.05	5.88	88.47	4.000	No	Yes	2.00
312	20.50	14.10	2.92	3.82	0.99	14.90	5.89	87.78	4.000	No	Yes	2.00
313	20.57	14.00	2.92	3.81	0.99	14.75	5.92	87.30	4.000	No	Yes	2.00
314	20.61	13.91	2.92	3.80	0.99	14.63	5.94	86.92	4.000	No	Yes	2.00
315	20.70	13.81	2.93	3.82	0.99	14.48	5.99	86.69	4.000	No	Yes	2.00
316	20.76	13.64	2.94	3.84	0.99	14.27	6.06	86.42	4.000	No	Yes	2.00
317	20.81	13.44	2.94	3.89	1.00	14.03	6.15	86.25	4.000	No	Yes	2.00
318	20.89	13.21	2.96	3.93	1.00	13.74	6.26	85.97	4.000	No	Yes	2.00
319	20.95	12.98	2.96	3.96	1.00	13.45	6.36	85.49	4.000	No	Yes	2.00
320	21.00	12.77	2.97	3.95	1.00	13.18	6.42	84.66	4.000	No	Yes	2.00
321	21.10	12.56	2.98	3.94	1.00	12.90	6.49	83.76	4.000	No	Yes	2.00
322	21.14	12.37	2.98	3.91	1.00	12.67	6.54	82.83	4.000	No	Yes	2.00
323	21.21	12.21	2.98	3.88	1.00	12.47	6.57	81.94	4.000	No	Yes	2.00
324	21.30	12.05	2.99	3.83	1.00	12.25	6.61	80.94	4.000	No	Yes	2.00
325	21.34	11.94	2.99	3.78	1.00	12.11	6.61	80.06	4.000	No	Yes	2.00
326	21.40	11.83	2.99	3.73	1.00	11.97	6.61	79.15	4.000	No	Yes	2.00
327	21.48	11.77	2.99	3.65	1.00	11.87	6.59	78.22	4.000	No	Yes	2.00
328	21.54	11.71	2.98	3.58	1.00	11.78	6.56	77.30	4.000	No	Yes	2.00
329	21.60	11.65	2.98	3.53	1.00	11.69	6.55	76.56	4.000	No	Yes	2.00
330	21.68	11.61	2.98	3.48	1.00	11.62	6.53	75.91	4.000	No	Yes	2.00
331	21.75	11.56	2.98	3.42	1.00	11.53	6.52	75.16	4.000	No	Yes	2.00
332	21.80	11.54	2.97	3.33	1.00	11.49	6.46	74.21	4.000	No	Yes	2.00
333	21.88	11.53	2.97	3.24	1.00	11.46	6.39	73.23	4.000	No	Yes	2.00
334	21.92	11.51	2.96	3.15	1.00	11.42	6.33	72.27	4.000	No	Yes	2.00
335	21.99	11.48	2.96	3.08	1.00	11.36	6.29	71.48	4.000	No	Yes	2.00
336	22.08	11.39	2.96	3.05	1.00	11.23	6.30	70.79	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
337	22.15	11.30	2.96	3.03	1.00	11.11	6.33	70.32	4.000	No	Yes	2.00
338	22.19	11.15	2.97	3.06	1.00	10.93	6.41	70.10	4.000	No	Yes	2.00
339	22.28	10.97	2.98	3.09	1.00	10.71	6.52	69.83	4.000	No	Yes	2.00
340	22.34	10.82	2.99	3.15	1.00	10.51	6.65	69.90	4.000	No	Yes	2.00
341	22.39	10.66	3.00	3.22	1.00	10.32	6.78	69.97	4.000	No	Yes	2.00
342	22.47	10.52	3.01	3.28	1.00	10.15	6.90	70.01	4.000	No	Yes	2.00
343	22.54	10.38	3.03	3.36	1.00	9.97	7.04	70.16	4.000	No	Yes	2.00
344	22.58	10.32	3.03	3.39	1.00	9.90	7.10	70.23	4.000	No	Yes	2.00
345	22.68	10.27	3.04	3.43	1.00	9.81	7.16	70.25	4.000	No	Yes	2.00
346	22.74	10.22	3.04	3.47	1.00	9.74	7.23	70.41	4.000	No	Yes	2.00
347	22.79	10.24	3.04	3.48	1.00	9.75	7.23	70.48	4.000	No	Yes	2.00
348	22.84	10.28	3.04	3.47	1.00	9.78	7.22	70.55	4.000	No	Yes	2.00
349	22.94	10.32	3.04	3.46	1.00	9.79	7.20	70.48	4.000	No	Yes	2.00
350	22.99	10.34	3.04	3.45	1.00	9.80	7.19	70.45	4.000	No	Yes	2.00
351	23.04	10.29	3.04	3.47	1.00	9.73	7.24	70.40	4.000	No	Yes	2.00
352	23.11	10.24	3.05	3.47	1.00	9.65	7.26	70.14	4.000	No	Yes	2.00
353	23.18	10.14	3.05	3.47	1.00	9.52	7.33	69.77	4.000	No	Yes	2.00
354	23.23	10.06	3.05	3.46	1.00	9.42	7.36	69.31	4.000	No	Yes	2.00
355	23.34	9.96	3.06	3.41	1.00	9.28	7.38	68.49	4.000	No	Yes	2.00
356	23.37	9.83	3.06	3.36	1.00	9.14	7.40	67.61	4.000	No	Yes	2.00
357	23.44	9.70	3.06	3.29	1.00	8.98	7.42	66.58	4.000	No	Yes	2.00
358	23.54	9.51	3.06	3.22	1.00	8.75	7.46	65.30	4.000	No	Yes	2.00
359	23.60	9.31	3.07	3.15	1.00	8.52	7.51	64.01	4.000	No	Yes	2.00
360	23.64	9.08	3.07	3.09	1.00	8.27	7.58	62.70	4.000	No	Yes	2.00
361	23.71	8.86	3.08	3.00	1.00	8.01	7.64	61.22	4.000	No	Yes	2.00
362	23.79	8.59	3.08	2.93	1.00	7.72	7.74	59.70	4.000	No	Yes	2.00
363	23.84	8.38	3.09	2.84	1.00	7.48	7.79	58.28	4.000	No	Yes	2.00
364	23.89	8.28	3.09	2.77	1.00	7.37	7.79	57.37	4.000	No	Yes	2.00
365	23.99	8.23	3.09	2.75	1.00	7.29	7.80	56.92	4.000	No	Yes	2.00
366	24.03	8.16	3.10	2.85	1.00	7.20	7.96	57.36	4.000	No	Yes	2.00
367	24.10	8.16	3.11	2.97	1.00	7.20	8.10	58.28	4.000	No	Yes	2.00
368	24.18	8.37	3.11	3.05	1.00	7.40	8.04	59.50	4.000	No	Yes	2.00
369	24.23	8.74	3.09	3.06	1.00	7.77	7.83	60.88	4.000	No	Yes	2.00
370	24.31	9.13	3.07	3.06	1.00	8.17	7.62	62.20	4.000	No	Yes	2.00
371	24.36	9.53	3.06	3.08	1.00	8.57	7.42	63.60	4.000	No	Yes	2.00
372	24.45	9.75	3.06	3.17	1.00	8.78	7.41	65.00	4.000	No	Yes	2.00
373	24.49	9.88	3.06	3.27	1.00	8.90	7.43	66.16	4.000	No	Yes	2.00
374	24.57	9.92	3.06	3.33	1.00	8.92	7.48	66.74	4.000	No	Yes	2.00
375	24.61	10.03	3.06	3.32	1.00	9.03	7.42	66.94	4.000	No	Yes	2.00
376	24.69	10.16	3.06	3.33	1.00	9.14	7.38	67.43	4.000	No	Yes	2.00
377	24.74	10.29	3.06	3.44	1.00	9.26	7.41	68.63	4.000	No	Yes	2.00
378	24.82	10.59	3.06	3.60	1.00	9.55	7.42	70.88	4.000	No	Yes	2.00
379	24.89	11.03	3.05	3.76	1.00	9.99	7.36	73.55	4.000	No	Yes	2.00
380	24.94	11.56	3.04	3.84	1.00	10.52	7.21	75.87	4.000	No	Yes	2.00
381	25.01	12.05	3.02	3.82	1.00	11.00	7.02	77.20	4.000	No	Yes	2.00
382	25.09	12.40	3.01	3.77	1.00	11.33	6.86	77.76	4.000	No	Yes	2.00
383	25.13	12.40	3.01	3.74	1.00	11.32	6.84	77.46	4.000	No	Yes	2.00
384	25.22	12.27	3.01	3.72	1.00	11.16	6.88	76.77	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
385	25.28	12.04	3.02	3.64	1.00	10.90	6.91	75.36	4.000	No	Yes	2.00
386	25.34	11.57	3.02	3.55	1.00	10.40	7.02	73.08	4.000	No	Yes	2.00
387	25.44	10.81	3.04	3.41	1.00	9.60	7.24	69.50	4.000	No	Yes	2.00
388	25.48	9.88	3.07	3.30	1.00	8.64	7.59	65.59	4.000	No	Yes	2.00
389	25.53	8.92	3.11	3.18	1.00	7.65	8.01	61.35	4.000	No	Yes	2.00
390	25.59	8.18	3.14	3.14	1.00	6.88	8.47	58.29	4.000	No	Yes	2.00
391	25.68	7.57	3.18	3.21	1.00	6.25	9.02	56.35	4.000	No	Yes	2.00
392	25.73	7.56	3.20	3.36	1.00	6.23	9.18	57.21	4.000	No	Yes	2.00
393	25.79	7.85	3.17	3.28	1.00	6.51	8.88	57.85	4.000	No	Yes	2.00
394	25.88	8.49	3.13	3.10	1.00	7.15	8.25	58.97	4.000	No	Yes	2.00
395	25.93	9.38	3.07	2.89	1.00	8.03	7.52	60.40	4.000	No	Yes	2.00
396	25.99	10.48	3.01	2.75	1.00	9.12	6.84	62.43	4.000	No	Yes	2.00
397	26.08	11.74	2.95	2.62	1.00	10.37	6.21	64.43	4.000	No	Yes	2.00
398	26.14	12.92	2.91	2.59	0.98	11.53	5.80	66.84	4.000	No	Yes	2.00
399	26.19	13.96	2.88	2.56	0.97	12.54	5.48	68.72	4.000	No	Yes	2.00
400	26.28	14.97	2.84	2.50	0.96	13.52	5.17	69.87	4.000	No	Yes	2.00
401	26.34	15.73	2.82	2.41	0.95	14.24	4.93	70.17	4.000	No	Yes	2.00
402	26.39	16.16	2.81	2.43	0.95	14.65	4.86	71.17	4.000	No	Yes	2.00
403	26.45	16.25	2.81	2.51	0.95	14.72	4.91	72.27	4.000	No	Yes	2.00
404	26.53	16.18	2.83	2.60	0.95	14.62	5.01	73.29	4.000	No	Yes	2.00
405	26.58	16.05	2.84	2.71	0.96	14.48	5.13	74.34	4.000	No	Yes	2.00
406	26.68	15.79	2.86	2.84	0.96	14.19	5.31	75.29	4.000	No	Yes	2.00
407	26.73	15.60	2.87	2.95	0.97	13.99	5.44	76.13	4.000	No	Yes	2.00
408	26.78	15.54	2.89	3.07	0.97	13.91	5.56	77.37	4.000	No	Yes	2.00
409	26.88	15.47	2.91	3.27	0.98	13.80	5.75	79.32	4.000	No	Yes	2.00
410	26.93	15.41	2.92	3.48	0.99	13.73	5.93	81.33	4.000	No	Yes	2.00
411	26.98	15.48	2.93	3.65	0.99	13.78	6.04	83.25	4.000	No	Yes	2.00
412	27.04	15.59	2.94	3.82	1.00	13.87	6.14	85.19	4.000	No	Yes	2.00
413	27.13	15.68	2.95	3.99	1.00	13.92	6.25	86.96	4.000	No	Yes	2.00
414	27.22	15.61	2.97	4.15	1.00	13.82	6.39	88.26	4.000	No	Yes	2.00
415	27.24	15.48	2.98	4.28	1.00	13.68	6.52	89.16	4.000	No	Yes	2.00
416	27.33	15.33	2.99	4.40	1.00	13.50	6.64	89.67	4.000	No	Yes	2.00
417	27.37	15.08	3.00	4.49	1.00	13.24	6.78	89.80	4.000	No	Yes	2.00
418	27.43	14.77	3.02	4.56	1.00	12.92	6.92	89.38	4.000	No	Yes	2.00
419	27.52	14.46	3.03	4.62	1.00	12.58	7.06	88.85	4.000	No	Yes	2.00
420	27.57	14.10	3.04	4.66	1.00	12.22	7.21	88.05	4.000	No	Yes	2.00
421	27.63	13.68	3.05	4.67	1.00	11.79	7.35	86.71	4.000	No	Yes	2.00
422	27.72	13.24	3.07	4.66	1.00	11.33	7.51	85.09	4.000	No	Yes	2.00
423	27.76	12.84	3.07	4.60	1.00	10.93	7.62	83.26	4.000	No	Yes	2.00
424	27.84	12.46	3.08	4.52	1.00	10.54	7.72	81.35	4.000	No	Yes	2.00
425	27.93	12.10	3.09	4.46	1.00	10.17	7.82	79.56	4.000	No	Yes	2.00
426	27.97	11.82	3.10	4.36	1.00	9.89	7.87	77.87	4.000	No	Yes	2.00
427	28.02	11.70	3.09	4.21	1.00	9.75	7.82	76.27	4.000	No	Yes	2.00
428	28.12	11.66	3.08	4.02	1.00	9.69	7.70	74.61	4.000	No	Yes	2.00
429	28.17	11.67	3.07	3.87	1.00	9.68	7.58	73.40	4.000	No	Yes	2.00
430	28.23	11.80	3.06	3.76	1.00	9.79	7.45	72.95	4.000	No	Yes	2.00
431	28.32	12.03	3.05	3.69	1.00	9.99	7.31	73.01	4.000	No	Yes	2.00
432	28.37	12.28	3.04	3.66	1.00	10.22	7.19	73.44	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
433	28.42	12.60	3.03	3.65	1.00	10.51	7.07	74.28	4.000	No	Yes	2.00
434	28.48	12.97	3.02	3.66	1.00	10.84	6.95	75.36	4.000	No	Yes	2.00
435	28.57	13.52	3.00	3.63	1.00	11.33	6.75	76.48	4.000	No	Yes	2.00
436	28.61	14.02	2.99	3.62	1.00	11.79	6.59	77.67	4.000	No	Yes	2.00
437	28.69	14.48	2.97	3.62	1.00	12.21	6.45	78.81	4.000	No	Yes	2.00
438	28.77	14.97	2.96	3.59	1.00	12.64	6.31	79.74	4.000	No	Yes	2.00
439	28.83	15.40	2.95	3.55	1.00	13.03	6.16	80.28	4.000	No	Yes	2.00
440	28.88	15.75	2.93	3.50	0.99	13.34	6.04	80.59	4.000	No	Yes	2.00
441	28.97	16.12	2.92	3.45	0.99	13.65	5.92	80.85	4.000	No	Yes	2.00
442	29.02	16.58	2.91	3.39	0.98	14.07	5.77	81.19	4.000	No	Yes	2.00
443	29.08	17.07	2.89	3.33	0.98	14.50	5.62	81.51	4.000	No	Yes	2.00
444	29.17	17.42	2.88	3.30	0.97	14.80	5.54	81.91	4.000	No	Yes	2.00
445	29.21	16.68	2.92	3.55	0.99	14.09	5.89	82.99	4.000	No	Yes	2.00
446	29.28	17.35	2.90	3.53	0.98	14.69	5.73	84.17	4.000	No	Yes	2.00
447	29.37	18.08	2.89	3.53	0.98	15.34	5.58	85.65	4.000	No	Yes	2.00
448	29.41	18.84	2.87	3.55	0.97	16.03	5.45	87.42	4.000	No	Yes	2.00
449	29.47	19.66	2.86	3.54	0.96	16.76	5.31	88.96	4.000	No	Yes	2.00
450	29.56	20.44	2.84	3.48	0.96	17.45	5.14	89.65	4.000	No	Yes	2.00
451	29.62	21.08	2.82	3.40	0.95	18.02	4.99	89.89	4.000	No	Yes	2.00
452	29.68	21.55	2.81	3.31	0.95	18.43	4.86	89.53	4.000	No	Yes	2.00
453	29.76	21.98	2.79	3.20	0.94	18.79	4.72	88.74	4.000	No	Yes	2.00
454	29.83	23.16	2.75	2.93	0.92	19.85	4.38	86.86	4.000	No	Yes	2.00
455	29.87	22.72	2.75	2.83	0.92	19.43	4.36	84.78	4.000	No	Yes	2.00
456	29.96	22.10	2.75	2.72	0.92	18.81	4.37	82.22	4.000	No	Yes	2.00
457	30.01	21.54	2.75	2.58	0.92	18.28	4.34	79.33	4.000	No	Yes	2.00
458	30.07	20.81	2.75	2.47	0.92	17.58	4.36	76.65	4.000	No	Yes	2.00
459	30.16	20.20	2.76	2.42	0.92	16.98	4.41	74.98	4.000	No	Yes	2.00
460	30.20	19.65	2.76	2.40	0.93	16.47	4.48	73.79	4.000	No	Yes	2.00
461	30.27	19.26	2.77	2.41	0.93	16.07	4.56	73.29	4.000	No	Yes	2.00
462	30.34	18.94	2.78	2.45	0.94	15.75	4.66	73.36	4.000	No	Yes	2.00
463	30.42	18.95	2.79	2.50	0.94	15.73	4.70	73.99	4.000	No	Yes	2.00
464	30.46	19.17	2.79	2.57	0.94	15.91	4.72	75.17	4.000	No	Yes	2.00
465	30.52	19.53	2.79	2.63	0.94	16.22	4.72	76.59	4.000	No	Yes	2.00
466	30.58	19.82	2.80	2.73	0.94	16.46	4.75	78.24	4.000	No	Yes	2.00
467	30.66	20.28	2.79	2.80	0.94	16.84	4.74	79.86	4.000	No	Yes	2.00
468	30.71	20.64	2.80	2.87	0.94	17.15	4.74	81.34	4.000	No	Yes	2.00
469	30.81	20.94	2.80	2.94	0.94	17.37	4.76	82.69	4.000	No	Yes	2.00
470	30.87	21.17	2.80	3.01	0.94	17.56	4.78	83.92	4.000	No	Yes	2.00
471	30.91	21.30	2.80	3.08	0.94	17.66	4.82	85.10	4.000	No	Yes	2.00
472	31.01	21.41	2.81	3.16	0.95	17.71	4.87	86.23	4.000	No	Yes	2.00
473	31.06	21.53	2.81	3.24	0.95	17.80	4.91	87.37	4.000	No	Yes	2.00
474	31.11	21.63	2.82	3.31	0.95	17.86	4.95	88.36	4.000	No	Yes	2.00
475	31.19	21.81	2.82	3.35	0.95	17.99	4.96	89.14	4.000	No	Yes	2.00
476	31.26	21.98	2.82	3.38	0.95	18.11	4.96	89.73	4.000	No	Yes	2.00
477	31.35	22.12	2.82	3.40	0.95	18.19	4.96	90.16	4.000	No	Yes	2.00
478	31.37	22.15	2.82	3.43	0.95	18.20	4.98	90.62	4.000	No	Yes	2.00
479	31.46	22.28	2.82	3.45	0.95	18.27	4.97	90.91	4.000	No	Yes	2.00
480	31.55	22.33	2.82	3.46	0.95	18.28	4.98	91.09	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
481	31.59	22.49	2.82	3.43	0.95	18.41	4.94	91.01	4.000	No	Yes	2.00
482	31.66	22.71	2.81	3.37	0.95	18.58	4.87	90.48	4.000	No	Yes	2.00
483	31.70	23.00	2.80	3.28	0.94	18.82	4.77	89.81	4.000	No	Yes	2.00
484	31.79	23.13	2.79	3.22	0.94	18.90	4.72	89.15	4.000	No	Yes	2.00
485	31.86	23.24	2.79	3.16	0.94	18.96	4.67	88.51	4.000	No	Yes	2.00
486	31.91	23.55	2.78	3.12	0.93	19.22	4.60	88.37	4.000	No	Yes	2.00
487	31.99	24.39	2.76	3.07	0.93	19.93	4.47	89.06	4.000	No	Yes	2.00
488	32.06	25.44	2.75	3.06	0.92	20.82	4.34	90.39	4.000	No	Yes	2.00
489	32.10	26.88	2.72	3.04	0.91	22.09	4.18	92.23	4.000	No	Yes	2.00
490	32.20	28.15	2.71	3.10	0.91	23.16	4.10	94.85	4.000	No	Yes	2.00
491	32.26	28.72	2.72	3.27	0.91	23.62	4.16	98.16	4.000	No	Yes	2.00
492	32.30	29.57	2.72	3.43	0.91	24.34	4.18	101.69	4.000	No	Yes	2.00
493	32.35	30.28	2.73	3.59	0.92	24.92	4.22	105.09	4.000	No	Yes	2.00
494	32.46	31.21	2.73	3.71	0.92	25.67	4.21	108.18	4.000	No	Yes	2.00
495	32.49	31.95	2.73	3.84	0.92	26.29	4.23	111.21	4.000	No	Yes	2.00
496	32.58	32.77	2.73	3.92	0.91	26.95	4.21	113.53	4.000	No	Yes	2.00
497	32.62	34.34	2.71	3.93	0.91	28.30	4.10	116.05	4.000	No	Yes	2.00
498	32.69	36.23	2.70	3.96	0.90	29.91	3.99	119.21	4.000	No	Yes	2.00
499	32.78	38.18	2.68	3.99	0.90	31.55	3.88	122.28	4.000	No	Yes	2.00
500	32.82	40.40	2.67	4.00	0.89	33.46	3.75	125.60	4.000	No	Yes	2.00
501	32.89	41.76	2.66	4.10	0.89	34.59	3.73	129.05	4.000	No	Yes	2.00
502	32.98	43.04	2.66	4.19	0.89	35.63	3.71	132.21	4.000	No	Yes	2.00
503	33.02	43.56	2.67	4.32	0.89	36.03	3.75	135.06	4.000	No	Yes	2.00
504	33.08	43.60	2.67	4.40	0.89	36.00	3.79	136.47	4.000	No	Yes	2.00
505	33.18	42.94	2.68	4.51	0.90	35.32	3.89	137.25	4.000	No	Yes	2.00
506	33.21	41.11	2.71	4.67	0.91	33.69	4.07	137.02	4.000	No	Yes	2.00
507	33.29	38.50	2.74	4.81	0.92	31.35	4.31	135.03	4.000	No	Yes	2.00
508	33.37	35.87	2.77	4.86	0.93	29.01	4.52	131.27	4.000	No	Yes	2.00
509	33.42	33.58	2.79	4.79	0.94	27.00	4.67	126.23	4.000	No	Yes	2.00
510	33.47	31.71	2.79	4.60	0.94	25.36	4.74	120.24	4.000	No	Yes	2.00
511	33.53	29.91	2.80	4.35	0.94	23.80	4.78	113.67	4.000	No	Yes	2.00
512	33.62	28.55	2.80	4.04	0.94	22.60	4.74	107.22	4.000	No	Yes	2.00
513	33.67	27.44	2.79	3.78	0.94	21.64	4.71	101.83	4.000	No	Yes	2.00
514	33.73	26.35	2.79	3.54	0.94	20.68	4.68	96.75	4.000	No	Yes	2.00
515	33.82	25.32	2.79	3.32	0.94	19.78	4.66	92.18	4.000	No	Yes	2.00
516	33.87	24.46	2.78	3.15	0.94	19.03	4.65	88.49	4.000	No	Yes	2.00
517	33.93	23.71	2.79	3.08	0.94	18.37	4.70	86.36	4.000	No	Yes	2.00
518	34.02	23.04	2.80	3.06	0.94	17.75	4.78	84.94	4.000	No	Yes	2.00
519	34.06	22.45	2.81	3.08	0.95	17.24	4.89	84.26	4.000	No	Yes	2.00
520	34.13	22.07	2.82	3.14	0.95	16.88	4.99	84.31	4.000	No	Yes	2.00
521	34.22	21.81	2.83	3.20	0.96	16.62	5.09	84.59	4.000	No	Yes	2.00
522	34.26	21.71	2.84	3.27	0.96	16.52	5.16	85.19	4.000	No	Yes	2.00
523	34.32	21.73	2.85	3.33	0.96	16.50	5.20	85.88	4.000	No	Yes	2.00
524	34.42	21.79	2.85	3.38	0.96	16.51	5.24	86.45	4.000	No	Yes	2.00
525	34.46	21.86	2.85	3.40	0.96	16.55	5.25	86.87	4.000	No	Yes	2.00
526	34.52	21.87	2.85	3.42	0.96	16.54	5.27	87.08	4.000	No	Yes	2.00
527	34.61	21.89	2.86	3.43	0.96	16.52	5.28	87.14	4.000	No	Yes	2.00
528	34.70	21.91	2.86	3.44	0.96	16.50	5.28	87.14	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
529	34.76	22.00	2.86	3.44	0.96	16.55	5.27	87.27	4.000	No	Yes	2.00
530	34.82	22.08	2.85	3.44	0.96	16.59	5.26	87.34	4.000	No	Yes	2.00
531	34.86	22.20	2.85	3.41	0.96	16.68	5.23	87.15	4.000	No	Yes	2.00
532	34.92	22.38	2.85	3.41	0.96	16.80	5.21	87.52	4.000	No	Yes	2.00
533	35.02	22.61	2.85	3.46	0.96	16.95	5.21	88.35	4.000	No	Yes	2.00
534	35.06	22.92	2.85	3.52	0.96	17.19	5.21	89.58	4.000	No	Yes	2.00
535	35.11	23.26	2.85	3.60	0.96	17.45	5.22	91.14	4.000	No	Yes	2.00
536	35.19	23.32	2.86	3.75	0.97	17.45	5.32	92.89	4.000	No	Yes	2.00
537	35.25	23.48	2.87	3.88	0.97	17.55	5.39	94.66	4.000	No	Yes	2.00
538	35.31	23.92	2.87	3.96	0.97	17.88	5.39	96.33	4.000	No	Yes	2.00
539	35.40	24.41	2.87	4.07	0.97	18.24	5.39	98.39	4.000	No	Yes	2.00
540	35.45	24.90	2.87	4.21	0.97	18.61	5.42	100.88	4.000	No	Yes	2.00
541	35.50	25.37	2.87	4.34	0.97	18.97	5.44	103.26	4.000	No	Yes	2.00
542	35.56	25.84	2.87	4.45	0.97	19.32	5.45	105.30	4.000	No	Yes	2.00
543	35.64	26.20	2.88	4.56	0.97	19.57	5.48	107.20	4.000	No	Yes	2.00
544	35.72	26.53	2.88	4.66	0.97	19.80	5.50	108.86	4.000	No	Yes	2.00
545	35.81	27.10	2.87	4.68	0.97	20.22	5.44	110.03	4.000	No	Yes	2.00
546	35.85	27.52	2.87	4.68	0.97	20.55	5.40	110.86	4.000	No	Yes	2.00
547	35.90	27.57	2.87	4.72	0.97	20.56	5.41	111.30	4.000	No	Yes	2.00
548	35.96	27.50	2.87	4.73	0.97	20.47	5.43	111.25	4.000	No	Yes	2.00
549	36.04	27.44	2.87	4.71	0.97	20.38	5.44	110.83	4.000	No	Yes	2.00
550	36.11	27.37	2.87	4.66	0.97	20.29	5.42	110.01	4.000	No	Yes	2.00
551	36.16	27.38	2.87	4.58	0.97	20.28	5.37	108.99	4.000	No	Yes	2.00
552	36.25	27.49	2.86	4.46	0.96	20.34	5.30	107.76	4.000	No	Yes	2.00
553	36.31	27.53	2.85	4.36	0.96	20.35	5.23	106.50	4.000	No	Yes	2.00
554	36.36	27.55	2.85	4.30	0.96	20.34	5.20	105.82	4.000	No	Yes	2.00
555	36.44	27.59	2.85	4.27	0.96	20.34	5.19	105.48	4.000	No	Yes	2.00
556	36.50	27.55	2.85	4.28	0.96	20.28	5.20	105.38	4.000	No	Yes	2.00
557	36.56	27.51	2.85	4.27	0.96	20.22	5.20	105.22	4.000	No	Yes	2.00
558	36.65	27.46	2.85	4.27	0.96	20.13	5.22	104.99	4.000	No	Yes	2.00
559	36.68	27.32	2.85	4.27	0.96	20.00	5.24	104.73	4.000	No	Yes	2.00
560	36.76	26.99	2.86	4.29	0.96	19.70	5.30	104.31	4.000	No	Yes	2.00
561	36.84	26.59	2.87	4.31	0.97	19.33	5.36	103.68	4.000	No	Yes	2.00
562	36.91	26.14	2.87	4.31	0.97	18.94	5.43	102.81	4.000	No	Yes	2.00
563	36.96	25.72	2.88	4.27	0.97	18.58	5.46	101.52	4.000	No	Yes	2.00
564	37.04	25.31	2.88	4.21	0.97	18.22	5.48	99.92	4.000	No	Yes	2.00
565	37.10	25.01	2.88	4.12	0.97	17.96	5.47	98.29	4.000	No	Yes	2.00
566	37.15	24.79	2.87	4.01	0.97	17.78	5.44	96.70	4.000	No	Yes	2.00
567	37.23	24.57	2.87	3.92	0.97	17.57	5.41	95.11	4.000	No	Yes	2.00
568	37.30	24.39	2.87	3.82	0.97	17.41	5.38	93.56	4.000	No	Yes	2.00
569	37.35	24.27	2.86	3.72	0.97	17.30	5.33	92.22	4.000	No	Yes	2.00
570	37.45	24.09	2.86	3.64	0.96	17.12	5.31	90.90	4.000	No	Yes	2.00
571	37.51	23.91	2.86	3.57	0.96	16.96	5.29	89.72	4.000	No	Yes	2.00
572	37.55	23.68	2.86	3.50	0.96	16.77	5.28	88.48	4.000	No	Yes	2.00
573	37.62	23.41	2.85	3.42	0.96	16.54	5.27	87.10	4.000	No	Yes	2.00
574	37.70	23.18	2.85	3.34	0.96	16.33	5.25	85.68	4.000	No	Yes	2.00
575	37.75	22.99	2.85	3.25	0.96	16.17	5.21	84.25	4.000	No	Yes	2.00
576	37.80	22.83	2.84	3.15	0.96	16.04	5.16	82.80	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
577	37.90	22.79	2.84	3.04	0.96	15.98	5.09	81.34	4.000	No	Yes	2.00
578	37.95	22.85	2.82	2.93	0.95	16.02	4.99	79.99	4.000	No	Yes	2.00
579	38.05	23.13	2.81	2.84	0.95	16.22	4.89	79.28	4.000	No	Yes	2.00
580	38.06	23.67	2.80	2.76	0.94	16.66	4.74	79.02	4.000	No	Yes	2.00
581	38.15	24.36	2.78	2.70	0.93	17.18	4.61	79.14	4.000	No	Yes	2.00
582	38.19	25.07	2.77	2.67	0.93	17.73	4.50	79.75	4.000	No	Yes	2.00
583	38.27	25.90	2.75	2.65	0.92	18.37	4.38	80.47	4.000	No	Yes	2.00
584	38.34	26.81	2.74	2.63	0.92	19.07	4.27	81.37	4.000	No	Yes	2.00
585	38.39	27.68	2.72	2.62	0.91	19.75	4.17	82.26	4.000	No	Yes	2.00
586	38.46	28.48	2.71	2.64	0.91	20.35	4.10	83.39	4.000	No	Yes	2.00
587	38.55	29.24	2.71	2.68	0.91	20.90	4.06	84.87	4.000	No	Yes	2.00
588	38.59	30.19	2.70	2.73	0.90	21.63	4.01	86.82	4.000	No	Yes	2.00
589	38.68	31.64	2.69	2.80	0.90	22.72	3.94	89.49	4.000	No	Yes	2.00
590	38.75	33.31	2.68	2.87	0.90	24.00	3.85	92.51	4.000	No	Yes	2.00
591	38.80	35.48	2.66	2.95	0.89	25.68	3.74	96.14	4.000	No	Yes	2.00
592	38.87	38.37	2.64	2.98	0.88	27.93	3.58	99.97	4.000	No	Yes	2.00
593	38.95	41.80	2.61	3.01	0.87	30.61	3.40	104.15	4.000	No	Yes	2.00
594	38.99	45.31	2.59	3.04	0.86	33.36	3.24	108.24	0.198	No	No	0.48
595	39.04	48.34	2.57	3.06	0.85	35.74	3.13	111.69	0.210	No	No	0.50
596	39.11	49.97	2.56	3.12	0.85	36.96	3.09	114.37	0.219	No	No	0.53
597	39.19	50.69	2.56	3.15	0.85	37.46	3.08	115.54	0.223	No	No	0.54
598	39.27	49.95	2.57	3.16	0.85	36.81	3.12	114.99	0.221	No	No	0.53
599	39.33	48.64	2.58	3.16	0.86	35.72	3.18	113.58	0.216	No	No	0.52
600	39.39	46.71	2.59	3.12	0.86	34.16	3.24	110.84	0.207	No	No	0.50
601	39.45	43.93	2.61	3.09	0.87	31.94	3.36	107.28	4.000	No	Yes	2.00
602	39.53	40.53	2.63	3.06	0.88	29.21	3.53	103.00	4.000	No	Yes	2.00
603	39.57	37.19	2.66	3.01	0.89	26.57	3.71	98.52	4.000	No	Yes	2.00
604	39.64	34.51	2.68	2.91	0.90	24.46	3.83	93.75	4.000	No	Yes	2.00
605	39.72	33.37	2.67	2.68	0.89	23.58	3.77	88.79	4.000	No	Yes	2.00
606	39.79	32.93	2.65	2.44	0.88	23.26	3.63	84.39	4.000	No	Yes	2.00
607	39.84	33.06	2.62	2.25	0.87	23.39	3.47	81.26	4.000	No	Yes	2.00
608	39.93	32.94	2.61	2.15	0.87	23.28	3.41	79.39	4.000	No	Yes	2.00
609	39.98	32.75	2.61	2.14	0.87	23.12	3.42	79.04	4.000	No	Yes	2.00
610	40.05	32.95	2.64	2.33	0.88	23.19	3.56	82.51	4.000	No	Yes	2.00
611	40.09	34.03	2.65	2.55	0.88	23.95	3.64	87.20	4.000	No	Yes	2.00
612	40.19	36.38	2.64	2.72	0.88	25.69	3.60	92.47	4.000	No	Yes	2.00
613	40.23	40.72	2.61	2.85	0.87	29.01	3.42	99.16	4.000	No	Yes	2.00
614	40.34	45.86	2.59	3.00	0.86	32.90	3.25	106.95	0.194	No	No	0.47
615	40.38	50.76	2.57	3.18	0.85	36.64	3.14	115.13	0.222	No	No	0.53
616	40.43	55.28	2.56	3.38	0.85	40.05	3.08	123.53	0.255	No	No	0.61
617	40.50	60.00	2.55	3.54	0.84	43.62	3.01	131.16	0.290	No	No	0.70
618	40.58	64.51	2.53	3.67	0.84	47.00	2.94	138.27	0.326	No	No	0.78
619	40.63	68.60	2.52	3.73	0.83	50.12	2.86	143.45	0.355	No	No	0.85
620	40.70	72.71	2.50	3.75	0.83	53.23	2.78	147.92	0.381	No	No	0.92
621	40.75	76.10	2.49	3.79	0.82	55.80	2.72	151.94	0.406	No	No	0.98
622	40.84	77.61	2.49	3.87	0.82	56.84	2.73	155.10	0.427	No	No	1.03
623	40.88	77.99	2.50	3.98	0.83	57.03	2.77	157.83	0.446	No	No	1.07
624	40.95	78.42	2.51	4.07	0.83	57.23	2.80	160.06	0.461	No	No	1.11

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
625	41.03	79.84	2.50	4.07	0.83	58.24	2.77	161.34	4.000	Yes	No	2.00
626	41.08	83.51	2.48	3.96	0.82	61.08	2.66	162.46	4.000	Yes	No	2.00
627	41.15	90.15	2.43	3.72	0.80	66.29	2.46	162.81	4.000	Yes	No	2.00
628	41.23	97.84	2.39	3.48	0.78	72.34	2.26	163.56	4.000	Yes	No	2.00
629	41.28	105.13	2.35	3.31	0.77	78.11	2.11	164.99	4.000	Yes	No	2.00
630	41.35	112.60	2.31	3.16	0.76	84.00	1.99	166.99	4.000	Yes	No	2.00
631	41.43	119.65	2.28	3.05	0.75	89.52	1.89	169.57	4.000	Yes	No	2.00
632	41.48	126.18	2.26	2.99	0.74	94.65	1.83	172.95	4.000	Yes	No	2.00
633	41.54	132.64	2.24	2.96	0.73	99.67	1.78	177.10	0.597	No	No	1.44
634	41.62	138.98	2.23	2.97	0.72	104.52	1.74	181.95	0.640	No	No	1.55
635	41.68	144.15	2.22	3.01	0.72	108.42	1.73	187.16	0.690	No	No	1.67
636	41.77	147.16	2.23	3.11	0.72	110.47	1.74	192.21	0.740	No	No	1.79
637	41.82	149.61	2.23	3.20	0.73	112.16	1.76	197.02	0.791	No	No	1.91
638	41.88	151.40	2.24	3.30	0.73	113.31	1.77	201.11	4.000	No	No	2.00
639	41.97	152.19	2.25	3.39	0.73	113.59	1.80	204.50	4.000	No	No	2.00
640	42.01	152.63	2.26	3.48	0.74	113.73	1.82	207.46	4.000	No	No	2.00
641	42.10	154.18	2.26	3.51	0.74	114.69	1.83	209.53	4.000	No	No	2.00
642	42.17	155.77	2.26	3.52	0.74	115.77	1.82	210.77	4.000	No	No	2.00
643	42.22	158.63	2.25	3.47	0.73	117.95	1.79	211.47	4.000	No	No	2.00
644	42.28	161.62	2.24	3.39	0.73	120.26	1.76	211.30	4.000	No	No	2.00
645	42.33	166.19	2.21	3.27	0.72	123.89	1.70	210.96	4.000	No	No	2.00
646	42.41	171.05	2.19	3.13	0.71	127.73	1.65	210.27	4.000	No	No	2.00
647	42.48	177.06	2.16	2.98	0.70	132.54	1.58	209.92	4.000	No	No	2.00
648	42.52	184.41	2.13	2.81	0.69	138.54	1.52	210.20	4.000	No	No	2.00
649	42.60	193.18	2.10	2.64	0.67	145.64	1.45	211.30	4.000	No	No	2.00
650	42.66	201.80	2.06	2.48	0.66	152.67	1.39	212.90	4.000	No	No	2.00
651	42.72	210.25	2.03	2.35	0.65	159.58	1.35	214.88	4.000	No	No	2.00
652	42.81	216.71	2.01	2.24	0.64	164.80	1.31	216.24	4.000	No	No	2.00
653	42.87	221.45	1.99	2.15	0.63	168.71	1.29	216.83	4.000	No	No	2.00
654	42.92	223.43	1.97	2.06	0.63	170.44	1.27	215.65	4.000	No	No	2.00
655	43.00	224.17	1.96	1.98	0.62	171.11	1.25	213.60	4.000	No	No	2.00
656	43.06	223.07	1.95	1.91	0.62	170.33	1.24	210.56	4.000	No	No	2.00
657	43.11	220.03	1.94	1.86	0.61	167.97	1.23	206.67	4.000	No	No	2.00
658	43.18	215.77	1.94	1.82	0.61	164.56	1.23	202.06	4.000	No	No	2.00
659	43.25	211.23	1.94	1.78	0.61	160.89	1.23	197.51	0.797	No	No	1.94
660	43.31	206.82	1.94	1.76	0.61	157.31	1.23	193.43	0.753	No	No	1.83
661	43.39	202.67	1.94	1.74	0.62	153.89	1.23	189.65	0.714	No	No	1.74
662	43.45	198.48	1.95	1.73	0.62	150.43	1.24	186.27	0.681	No	No	1.66
663	43.51	194.71	1.96	1.76	0.62	147.19	1.25	184.09	0.660	No	No	1.61
664	43.61	191.33	1.97	1.80	0.63	144.12	1.27	182.63	0.646	No	No	1.57
665	43.65	188.25	1.99	1.85	0.63	141.41	1.29	181.84	0.639	No	No	1.56
666	43.72	185.35	2.00	1.90	0.64	138.80	1.30	180.92	0.631	No	No	1.54
667	43.81	182.33	2.02	1.95	0.64	136.09	1.32	179.83	0.621	No	No	1.51
668	43.85	178.70	2.03	1.99	0.65	133.02	1.34	178.27	0.607	No	No	1.48
669	43.92	174.04	2.04	2.02	0.65	129.13	1.36	175.71	0.585	No	No	1.42
670	44.01	169.31	2.06	2.06	0.66	125.14	1.38	173.09	0.562	No	No	1.37
671	44.05	165.21	2.06	2.05	0.66	121.88	1.39	169.93	0.536	No	No	1.31
672	44.10	160.81	2.06	2.00	0.66	118.50	1.39	165.15	0.499	No	No	1.22

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
673	44.20	156.04	2.07	1.94	0.66	114.74	1.40	160.07	0.461	No	No	1.13
674	44.25	151.36	2.07	1.90	0.66	111.13	1.40	155.35	0.429	No	No	1.05
675	44.30	146.31	2.07	1.88	0.67	107.16	1.41	151.20	0.401	No	No	0.98
676	44.40	140.34	2.09	1.89	0.67	102.33	1.44	147.25	0.377	No	No	0.92
677	44.45	134.81	2.11	1.92	0.68	97.92	1.47	143.99	0.358	No	No	0.87
678	44.50	130.12	2.13	1.97	0.69	94.11	1.51	142.03	0.346	No	No	0.85
679	44.57	125.26	2.15	2.03	0.70	90.13	1.56	140.34	0.337	No	No	0.82
680	44.63	120.31	2.18	2.16	0.71	86.02	1.63	140.23	0.336	No	No	0.82
681	44.69	115.72	2.23	2.38	0.72	82.08	1.74	143.01	0.352	No	No	0.86
682	44.79	111.51	2.27	2.63	0.74	78.40	1.87	146.54	0.373	No	No	0.91
683	44.84	107.77	2.31	2.88	0.76	75.21	2.00	150.25	0.395	No	No	0.97
684	44.89	105.00	2.35	3.09	0.77	72.83	2.11	153.52	0.416	No	No	1.02
685	44.96	103.51	2.37	3.23	0.78	71.48	2.18	156.05	0.433	No	No	1.06
686	45.04	102.01	2.39	3.37	0.78	70.14	2.26	158.16	0.448	No	No	1.10
687	45.09	100.81	2.40	3.47	0.79	69.09	2.31	159.67	0.459	No	No	1.12
688	45.17	100.05	2.41	3.55	0.79	68.35	2.35	160.93	0.468	No	No	1.15
689	45.24	99.52	2.42	3.62	0.80	67.81	2.39	162.05	0.476	No	No	1.17
690	45.28	99.27	2.42	3.65	0.80	67.55	2.41	162.52	0.479	No	No	1.18
691	45.38	98.85	2.43	3.67	0.80	67.10	2.42	162.58	0.480	No	No	1.18
692	45.42	97.77	2.43	3.72	0.80	66.22	2.46	162.63	0.480	No	No	1.18
693	45.49	96.34	2.44	3.77	0.81	65.05	2.50	162.56	0.479	No	No	1.18
694	45.57	94.70	2.45	3.82	0.81	63.72	2.55	162.28	0.477	No	No	1.17
695	45.63	92.37	2.47	3.87	0.82	61.92	2.61	161.36	0.471	No	No	1.16
696	45.69	89.46	2.48	3.89	0.82	59.74	2.66	159.12	0.455	No	No	1.12
697	45.78	85.19	2.50	3.90	0.83	56.57	2.75	155.40	0.429	No	No	1.06
698	45.84	79.80	2.52	3.92	0.84	52.64	2.87	150.88	0.399	No	No	0.98
699	45.89	73.90	2.55	3.94	0.85	48.37	3.01	145.76	0.368	No	No	0.91
700	45.93	67.39	2.58	3.94	0.86	43.71	3.19	139.53	0.333	No	No	0.82
701	46.02	61.02	2.61	3.91	0.87	39.17	3.38	132.47	4.000	No	Yes	2.00
702	46.08	54.84	2.64	3.84	0.88	34.81	3.59	124.90	4.000	No	Yes	2.00
703	46.13	48.82	2.68	3.75	0.89	30.61	3.82	116.87	4.000	No	Yes	2.00
704	46.22	43.62	2.71	3.62	0.91	27.00	4.03	108.93	4.000	No	Yes	2.00
705	46.28	39.06	2.74	3.51	0.92	23.85	4.28	101.99	4.000	No	Yes	2.00
706	46.33	35.80	2.76	3.40	0.93	21.61	4.47	96.55	4.000	No	Yes	2.00
707	46.43	33.77	2.77	3.24	0.93	20.22	4.54	91.86	4.000	No	Yes	2.00
708	46.47	32.28	2.77	3.07	0.93	19.23	4.57	87.81	4.000	No	Yes	2.00
709	46.53	31.55	2.77	2.93	0.93	18.75	4.53	85.02	4.000	No	Yes	2.00
710	46.63	31.27	2.76	2.79	0.93	18.56	4.46	82.79	4.000	No	Yes	2.00
711	46.67	31.09	2.75	2.68	0.92	18.45	4.39	81.06	4.000	No	Yes	2.00
712	46.73	31.01	2.75	2.64	0.92	18.39	4.37	80.34	4.000	No	Yes	2.00
713	46.83	31.04	2.75	2.62	0.92	18.38	4.35	80.02	4.000	No	Yes	2.00
714	46.87	31.05	2.75	2.61	0.92	18.38	4.35	79.94	4.000	No	Yes	2.00
715	46.93	31.18	2.75	2.61	0.92	18.45	4.34	80.00	4.000	No	Yes	2.00
716	47.02	31.31	2.74	2.60	0.92	18.51	4.32	79.99	4.000	No	Yes	2.00
717	47.08	31.45	2.74	2.59	0.92	18.58	4.30	79.99	4.000	No	Yes	2.00
718	47.12	31.65	2.74	2.61	0.92	18.71	4.30	80.42	4.000	No	Yes	2.00
719	47.18	31.90	2.74	2.63	0.92	18.85	4.30	80.99	4.000	No	Yes	2.00
720	47.27	32.12	2.74	2.66	0.92	18.96	4.30	81.54	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
721	47.31	32.24	2.74	2.71	0.92	19.01	4.33	82.39	4.000	No	Yes	2.00
722	47.39	32.73	2.74	2.74	0.92	19.30	4.32	83.31	4.000	No	Yes	2.00
723	47.48	33.47	2.74	2.78	0.92	19.76	4.28	84.52	4.000	No	Yes	2.00
724	47.52	34.18	2.73	2.83	0.92	20.22	4.25	85.98	4.000	No	Yes	2.00
725	47.59	34.88	2.74	2.94	0.92	20.63	4.28	88.32	4.000	No	Yes	2.00
726	47.66	35.57	2.75	3.11	0.92	21.01	4.35	91.45	4.000	No	Yes	2.00
727	47.74	36.36	2.75	3.25	0.92	21.47	4.39	94.26	4.000	No	Yes	2.00
728	47.79	37.63	2.75	3.33	0.92	22.28	4.34	96.75	4.000	No	Yes	2.00
729	47.86	39.62	2.73	3.33	0.91	23.59	4.20	98.98	4.000	Yes	Yes	2.00
730	47.94	42.38	2.69	3.25	0.90	25.46	3.96	100.78	4.000	Yes	Yes	2.00
731	47.99	46.45	2.65	3.10	0.88	28.27	3.63	102.50	4.000	Yes	Yes	2.00
732	48.05	51.69	2.59	2.93	0.86	31.91	3.27	104.31	4.000	Yes	No	2.00
733	48.13	57.43	2.54	2.78	0.84	35.93	2.96	106.37	4.000	Yes	No	2.00
734	48.19	63.46	2.49	2.64	0.82	40.18	2.70	108.40	4.000	Yes	No	2.00
735	48.26	69.35	2.44	2.56	0.81	44.33	2.50	111.00	4.000	Yes	No	2.00
736	48.34	74.27	2.42	2.55	0.80	47.76	2.39	114.21	4.000	Yes	No	2.00
737	48.39	78.06	2.41	2.58	0.79	50.36	2.34	117.60	0.231	No	No	0.58
738	48.43	80.01	2.41	2.66	0.79	51.62	2.34	120.87	0.244	No	No	0.61
739	48.51	80.23	2.42	2.78	0.80	51.58	2.40	123.65	4.000	Yes	No	2.00
740	48.58	78.15	2.45	2.97	0.81	49.87	2.53	126.20	4.000	Yes	No	2.00
741	48.63	73.91	2.50	3.24	0.83	46.66	2.76	128.57	4.000	Yes	No	2.00
742	48.72	69.19	2.55	3.54	0.85	43.12	3.03	130.53	4.000	Yes	No	2.00
743	48.78	64.53	2.60	3.85	0.87	39.71	3.33	132.10	4.000	Yes	No	2.00
744	48.83	60.65	2.64	4.10	0.88	36.92	3.59	132.69	4.000	Yes	Yes	2.00
745	48.90	58.27	2.67	4.28	0.89	35.18	3.78	133.00	4.000	Yes	Yes	2.00
746	48.99	56.81	2.69	4.39	0.90	34.10	3.90	133.10	4.000	No	Yes	2.00
747	49.03	57.34	2.68	4.38	0.90	34.43	3.88	133.52	4.000	Yes	Yes	2.00
748	49.08	59.70	2.66	4.27	0.89	36.02	3.73	134.25	4.000	Yes	Yes	2.00
749	49.17	64.88	2.62	4.05	0.87	39.55	3.43	135.60	4.000	Yes	Yes	2.00
750	49.23	73.51	2.54	3.69	0.85	45.55	3.01	136.90	4.000	Yes	No	2.00
751	49.32	85.21	2.46	3.31	0.81	53.79	2.58	138.53	4.000	Yes	No	2.00
752	49.35	97.81	2.38	3.01	0.78	62.84	2.24	140.98	4.000	Yes	No	2.00
753	49.43	111.56	2.31	2.75	0.76	72.74	1.99	144.42	4.000	Yes	No	2.00
754	49.50	126.07	2.24	2.53	0.73	83.33	1.78	148.53	4.000	Yes	No	2.00
755	49.58	140.81	2.19	2.36	0.71	94.14	1.63	153.61	4.000	Yes	No	2.00
756	49.63	155.36	2.13	2.22	0.69	104.93	1.52	159.57	4.000	Yes	No	2.00
757	49.72	169.50	2.09	2.12	0.67	115.38	1.44	166.05	4.000	Yes	No	2.00
758	49.78	181.49	2.06	2.04	0.66	124.33	1.38	171.86	4.000	Yes	No	2.00
759	49.83	190.73	2.03	1.99	0.65	131.20	1.35	176.75	4.000	Yes	No	2.00
760	49.90	196.54	2.02	1.98	0.65	135.41	1.33	180.17	0.624	No	No	1.57
761	49.98	200.97	2.01	1.97	0.64	138.54	1.32	182.84	0.648	No	No	1.64
762	50.02	203.65	2.01	1.97	0.64	140.45	1.31	184.55	4.000	No	No	2.00
763	50.08	205.02	2.00	1.92	0.64	141.54	1.30	184.09	4.000	No	No	2.00
764	50.18	205.97	1.99	1.87	0.63	142.29	1.29	183.07	4.000	No	No	2.00
765	50.23	206.42	1.98	1.82	0.63	142.77	1.27	181.88	4.000	No	No	2.00
766	50.27	206.67	1.97	1.77	0.63	143.11	1.26	180.71	4.000	No	No	2.00
767	50.36	206.82	1.96	1.73	0.62	143.25	1.25	179.58	4.000	No	No	2.00
768	50.40	206.95	1.95	1.69	0.62	143.47	1.25	178.63	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
769	50.47	207.35	1.95	1.66	0.62	143.80	1.24	177.89	4.000	No	No	2.00
770	50.55	207.82	1.94	1.63	0.62	144.14	1.23	177.42	4.000	No	No	2.00
771	50.63	208.28	1.94	1.61	0.61	144.42	1.23	177.15	4.000	No	No	2.00
772	50.67	208.58	1.95	1.66	0.62	144.31	1.24	178.43	4.000	No	No	2.00
773	50.72	208.67	1.96	1.73	0.62	143.92	1.25	180.14	4.000	No	No	2.00
774	50.83	208.48	1.97	1.79	0.63	143.22	1.27	181.54	4.000	No	No	2.00
775	50.88	208.04	1.99	1.85	0.63	142.49	1.28	182.79	4.000	No	No	2.00
776	50.93	207.42	2.00	1.91	0.64	141.67	1.30	183.75	4.000	No	No	2.00
777	51.02	206.85	2.01	1.96	0.64	140.84	1.31	184.53	4.000	No	No	2.00
778	51.08	206.30	2.02	2.00	0.64	140.13	1.32	185.17	4.000	No	No	2.00
779	51.12	205.82	2.02	2.03	0.65	139.57	1.33	185.58	4.000	No	No	2.00
780	51.21	205.38	2.03	2.05	0.65	138.99	1.34	185.59	4.000	No	No	2.00
781	51.27	205.16	2.03	2.05	0.65	138.70	1.34	185.41	4.000	No	No	2.00
782	51.32	205.10	2.03	2.04	0.65	138.60	1.33	185.01	4.000	No	No	2.00
783	51.39	205.14	2.02	2.03	0.65	138.54	1.33	184.61	4.000	No	No	2.00
784	51.47	205.24	2.02	2.02	0.65	138.49	1.33	184.27	4.000	No	No	2.00
785	51.55	205.31	2.02	2.01	0.65	138.40	1.33	184.07	4.000	No	No	2.00
786	51.60	205.08	2.02	2.01	0.65	138.14	1.33	183.84	4.000	No	No	2.00
787	51.67	204.64	2.02	2.02	0.65	137.67	1.33	183.52	4.000	No	No	2.00
788	51.72	203.58	2.03	2.02	0.65	136.81	1.34	182.68	4.000	No	No	2.00
789	51.79	201.52	2.03	2.00	0.65	135.28	1.34	180.62	4.000	No	No	2.00
790	51.87	199.01	2.03	1.99	0.65	133.36	1.34	178.56	4.000	No	No	2.00
791	51.91	196.40	2.03	1.99	0.65	131.39	1.35	176.81	4.000	No	No	2.00
792	51.98	192.80	2.04	1.99	0.65	128.68	1.35	174.31	4.000	No	No	2.00
793	52.06	188.34	2.05	2.00	0.66	125.28	1.37	171.51	4.000	No	No	2.00
794	52.12	183.88	2.06	2.00	0.66	122.00	1.38	168.38	4.000	No	No	2.00
795	52.17	178.11	2.07	2.02	0.66	117.70	1.40	165.18	4.000	No	No	2.00
796	52.26	170.61	2.09	2.08	0.67	112.01	1.44	161.59	4.000	Yes	No	2.00
797	52.31	163.90	2.12	2.15	0.68	106.94	1.49	159.09	4.000	Yes	No	2.00
798	52.38	156.13	2.15	2.26	0.69	101.00	1.56	157.10	4.000	Yes	No	2.00
799	52.47	147.15	2.19	2.39	0.71	94.26	1.64	154.49	4.000	Yes	No	2.00
800	52.51	136.09	2.23	2.52	0.73	86.23	1.75	150.95	4.000	Yes	No	2.00
801	52.56	124.42	2.28	2.68	0.74	77.83	1.89	147.40	4.000	Yes	No	2.00
802	52.66	112.90	2.33	2.84	0.76	69.62	2.06	143.68	4.000	Yes	No	2.00
803	52.70	100.48	2.40	3.06	0.79	60.93	2.30	140.39	4.000	Yes	No	2.00
804	52.77	89.16	2.46	3.25	0.81	53.15	2.57	136.45	4.000	Yes	No	2.00
805	52.87	79.44	2.51	3.37	0.83	46.57	2.82	131.31	4.000	Yes	No	2.00
806	52.92	69.32	2.57	3.51	0.86	39.89	3.15	125.70	4.000	Yes	No	2.00
807	52.97	61.28	2.62	3.61	0.88	34.64	3.48	120.40	4.000	Yes	Yes	2.00
808	53.02	54.61	2.67	3.64	0.89	30.38	3.78	114.68	4.000	Yes	Yes	2.00
809	53.10	50.06	2.70	3.58	0.90	27.50	3.97	109.11	4.000	Yes	Yes	2.00
810	53.16	46.90	2.71	3.45	0.91	25.55	4.07	104.01	4.000	No	Yes	2.00
811	53.22	44.28	2.72	3.26	0.91	23.98	4.11	98.54	4.000	No	Yes	2.00
812	53.31	42.65	2.71	3.01	0.91	23.03	4.05	93.26	4.000	No	Yes	2.00
813	53.36	41.31	2.70	2.77	0.90	22.29	3.97	88.37	4.000	No	Yes	2.00
814	53.42	40.10	2.69	2.59	0.90	21.59	3.91	84.45	4.000	No	Yes	2.00
815	53.51	39.07	2.68	2.42	0.90	21.00	3.85	80.92	4.000	No	Yes	2.00
816	53.56	37.95	2.68	2.28	0.90	20.34	3.83	77.90	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
817	53.62	37.07	2.68	2.21	0.90	19.81	3.83	75.92	4.000	No	Yes	2.00
818	53.71	36.24	2.68	2.16	0.90	19.28	3.86	74.43	4.000	No	Yes	2.00
819	53.75	35.58	2.68	2.12	0.90	18.87	3.88	73.33	4.000	No	Yes	2.00
820	53.83	34.88	2.70	2.16	0.90	18.39	3.98	73.18	4.000	No	Yes	2.00
821	53.91	34.05	2.71	2.20	0.91	17.84	4.09	72.99	4.000	No	Yes	2.00
822	53.98	33.09	2.73	2.23	0.92	17.20	4.22	72.61	4.000	No	Yes	2.00
823	54.01	32.19	2.75	2.27	0.92	16.62	4.35	72.23	4.000	No	Yes	2.00
824	54.11	31.08	2.77	2.31	0.93	15.89	4.51	71.62	4.000	No	Yes	2.00
825	54.15	29.90	2.78	2.32	0.94	15.16	4.66	70.59	4.000	No	Yes	2.00
826	54.21	28.55	2.81	2.34	0.95	14.31	4.85	69.38	4.000	No	Yes	2.00
827	54.27	27.04	2.83	2.33	0.95	13.38	5.05	67.57	4.000	No	Yes	2.00
828	54.35	25.56	2.85	2.30	0.96	12.48	5.24	65.45	4.000	No	Yes	2.00
829	54.42	24.28	2.87	2.22	0.97	11.72	5.38	63.06	4.000	No	Yes	2.00
830	54.46	23.20	2.88	2.13	0.97	11.09	5.48	60.75	4.000	No	Yes	2.00
831	54.55	22.43	2.88	2.02	0.97	10.64	5.50	58.58	4.000	No	Yes	2.00
832	54.60	21.80	2.88	1.91	0.97	10.29	5.51	56.66	4.000	No	Yes	2.00
833	54.67	21.40	2.88	1.80	0.97	10.06	5.46	54.95	4.000	No	Yes	2.00
834	54.74	21.06	2.87	1.72	0.97	9.87	5.43	53.59	4.000	No	Yes	2.00
835	54.79	20.77	2.87	1.66	0.97	9.71	5.41	52.57	4.000	No	Yes	2.00
836	54.86	20.62	2.87	1.62	0.97	9.62	5.40	51.96	4.000	No	Yes	2.00
837	54.96	20.50	2.87	1.60	0.97	9.54	5.41	51.56	4.000	No	Yes	2.00
838	55.03	20.43	2.87	1.59	0.97	9.49	5.41	51.32	4.000	No	Yes	2.00
839	55.06	20.38	2.87	1.58	0.97	9.46	5.41	51.16	4.000	No	Yes	2.00
840	55.14	20.37	2.87	1.57	0.97	9.44	5.40	51.00	4.000	No	Yes	2.00
841	55.21	20.35	2.87	1.56	0.97	9.42	5.40	50.83	4.000	No	Yes	2.00
842	55.25	20.31	2.87	1.55	0.97	9.39	5.39	50.67	4.000	No	Yes	2.00
843	55.32	20.28	2.87	1.54	0.97	9.37	5.39	50.50	4.000	No	Yes	2.00
844	55.41	20.24	2.87	1.53	0.97	9.33	5.39	50.33	4.000	No	Yes	2.00
845	55.45	20.23	2.87	1.53	0.97	9.32	5.39	50.24	4.000	No	Yes	2.00
846	55.52	20.23	2.87	1.53	0.97	9.31	5.39	50.23	4.000	No	Yes	2.00
847	55.61	20.28	2.87	1.53	0.97	9.33	5.39	50.28	4.000	No	Yes	2.00
848	55.65	20.52	2.87	1.56	0.97	9.45	5.38	50.89	4.000	No	Yes	2.00
849	55.71	20.91	2.86	1.60	0.97	9.67	5.35	51.70	4.000	No	Yes	2.00
850	55.80	21.44	2.86	1.63	0.96	9.96	5.29	52.64	4.000	No	Yes	2.00
851	55.86	22.21	2.84	1.66	0.96	10.40	5.17	53.78	4.000	No	Yes	2.00
852	55.95	23.00	2.83	1.70	0.96	10.84	5.08	55.07	4.000	No	Yes	2.00
853	56.00	23.79	2.82	1.74	0.95	11.29	5.00	56.40	4.000	No	Yes	2.00
854	56.05	24.57	2.82	1.79	0.95	11.73	4.92	57.75	4.000	No	Yes	2.00
855	56.11	25.39	2.80	1.79	0.94	12.21	4.79	58.54	4.000	No	Yes	2.00
856	56.20	26.17	2.78	1.76	0.94	12.67	4.65	58.93	4.000	No	Yes	2.00
857	56.24	26.73	2.77	1.71	0.93	13.01	4.52	58.82	4.000	No	Yes	2.00
858	56.31	27.09	2.76	1.68	0.93	13.23	4.43	58.66	4.000	No	Yes	2.00
859	56.39	27.14	2.75	1.65	0.92	13.26	4.40	58.31	4.000	No	Yes	2.00
860	56.43	26.89	2.75	1.63	0.93	13.11	4.41	57.80	4.000	No	Yes	2.00
861	56.50	26.19	2.77	1.62	0.93	12.68	4.49	56.98	4.000	No	Yes	2.00
862	56.60	25.50	2.77	1.60	0.93	12.25	4.57	56.00	4.000	No	Yes	2.00
863	56.66	24.81	2.78	1.55	0.93	11.85	4.62	54.73	4.000	No	Yes	2.00
864	56.70	24.10	2.79	1.53	0.94	11.42	4.72	53.84	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
865	56.79	23.44	2.81	1.53	0.94	11.01	4.83	53.20	4.000	No	Yes	2.00
866	56.84	22.85	2.82	1.55	0.95	10.64	4.96	52.77	4.000	No	Yes	2.00
867	56.92	22.40	2.83	1.57	0.96	10.36	5.08	52.61	4.000	No	Yes	2.00
868	56.99	22.25	2.84	1.59	0.96	10.25	5.14	52.66	4.000	No	Yes	2.00
869	57.03	22.42	2.84	1.60	0.96	10.34	5.12	52.94	4.000	No	Yes	2.00
870	57.09	23.22	2.82	1.60	0.95	10.80	4.97	53.70	4.000	No	Yes	2.00
871	57.18	23.98	2.81	1.62	0.95	11.23	4.87	54.70	4.000	No	Yes	2.00
872	57.23	24.85	2.81	1.70	0.94	11.71	4.83	56.60	4.000	No	Yes	2.00
873	57.31	26.05	2.81	1.86	0.94	12.34	4.84	59.70	4.000	No	Yes	2.00
874	57.38	27.50	2.81	2.04	0.94	13.12	4.83	63.35	4.000	Yes	Yes	2.00
875	57.43	29.89	2.79	2.19	0.94	14.46	4.68	67.68	4.000	Yes	Yes	2.00
876	57.50	33.85	2.75	2.30	0.92	16.75	4.35	72.85	4.000	Yes	Yes	2.00
877	57.58	38.94	2.69	2.33	0.90	19.76	3.94	77.84	4.000	Yes	Yes	2.00
878	57.62	45.95	2.62	2.29	0.87	24.03	3.45	82.77	4.000	Yes	Yes	2.00
879	57.68	53.93	2.55	2.25	0.85	28.96	3.04	88.00	4.000	Yes	No	2.00
880	57.78	62.67	2.49	2.21	0.82	34.40	2.71	93.09	4.000	Yes	No	2.00
881	57.82	72.41	2.43	2.16	0.80	40.59	2.42	98.14	4.000	Yes	No	2.00
882	57.89	82.22	2.37	2.09	0.78	46.92	2.19	102.62	4.000	Yes	No	2.00
883	57.97	91.68	2.32	2.04	0.76	53.07	2.01	106.91	4.000	Yes	No	2.00
884	58.02	99.77	2.28	2.00	0.75	58.36	1.90	110.82	4.000	Yes	No	2.00
885	58.09	105.22	2.26	1.99	0.74	61.89	1.84	113.73	4.000	No	No	2.00
886	58.17	108.62	2.26	2.01	0.73	64.01	1.81	116.09	4.000	No	No	2.00
887	58.23	109.72	2.26	2.06	0.74	64.57	1.83	117.85	4.000	No	No	2.00
888	58.28	109.49	2.27	2.12	0.74	64.23	1.86	119.20	4.000	No	No	2.00
889	58.37	108.18	2.29	2.20	0.75	63.12	1.91	120.41	4.000	Yes	No	2.00
890	58.43	105.44	2.31	2.30	0.76	61.09	1.98	121.15	4.000	Yes	No	2.00
891	58.48	100.57	2.35	2.44	0.77	57.67	2.10	121.32	4.000	Yes	No	2.00
892	58.57	95.05	2.39	2.60	0.78	53.81	2.26	121.56	4.000	Yes	No	2.00
893	58.62	88.67	2.44	2.80	0.80	49.47	2.46	121.83	4.000	Yes	No	2.00
894	58.67	82.27	2.48	3.00	0.82	45.20	2.69	121.69	4.000	Yes	No	2.00
895	58.78	76.27	2.53	3.21	0.84	41.23	2.94	121.38	4.000	Yes	No	2.00
896	58.82	69.93	2.59	3.44	0.86	37.13	3.25	120.73	4.000	Yes	No	2.00
897	58.88	63.59	2.64	3.69	0.88	33.12	3.61	119.62	4.000	Yes	Yes	2.00
898	58.97	57.66	2.70	3.89	0.90	29.45	3.98	117.21	4.000	Yes	Yes	2.00
899	59.01	52.33	2.75	4.08	0.92	26.22	4.37	114.63	4.000	Yes	Yes	2.00
900	59.07	48.78	2.79	4.21	0.94	24.09	4.66	112.37	4.000	Yes	Yes	2.00
901	59.12	45.34	2.82	4.31	0.95	22.06	4.97	109.61	4.000	Yes	Yes	2.00
902	59.19	42.74	2.84	4.31	0.96	20.56	5.17	106.39	4.000	Yes	Yes	2.00
903	59.27	41.35	2.85	4.19	0.96	19.78	5.22	103.23	4.000	No	Yes	2.00
904	59.32	39.96	2.86	4.08	0.96	19.01	5.27	100.24	4.000	No	Yes	2.00
905	59.42	39.47	2.85	3.93	0.96	18.76	5.22	97.90	4.000	No	Yes	2.00
906	59.47	38.99	2.84	3.78	0.96	18.52	5.16	95.59	4.000	No	Yes	2.00
907	59.52	38.64	2.84	3.70	0.96	18.33	5.14	94.16	4.000	No	Yes	2.00
908	59.58	38.47	2.83	3.58	0.95	18.26	5.07	92.55	4.000	No	Yes	2.00
909	59.68	38.20	2.83	3.48	0.95	18.11	5.03	91.05	4.000	No	Yes	2.00
910	59.74	38.28	2.82	3.42	0.95	18.16	4.98	90.38	4.000	Yes	Yes	2.00
911	59.78	38.65	2.78	2.98	0.93	18.53	4.60	85.25	4.000	Yes	Yes	2.00
912	59.88	38.74	2.74	2.60	0.92	18.73	4.29	80.36	4.000	Yes	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
913	59.93	39.33	2.69	2.21	0.90	19.26	3.91	75.24	4.000	Yes	Yes	2.00
914	60.00	40.82	2.61	1.76	0.87	20.43	3.39	69.20	4.000	Yes	Yes	2.00
915	60.05	43.76	2.50	1.30	0.83	22.60	2.77	62.70	4.000	Yes	No	2.00
916	60.13	46.96	2.38	0.91	0.78	25.08	2.24	56.21	4.000	Yes	No	2.00
917	60.18	46.63	2.30	0.63	0.75	25.36	1.96	49.61	4.000	Yes	No	2.00
918	60.25	48.94	2.15	0.31	0.69	27.71	1.00	27.71	4.000	Yes	No	2.00
919	60.33	54.14	N/A	0.00	1.00	-1.00	1.00	N/A	4.000	No	No	2.00
920	60.38	58.50	N/A	0.00	1.00	-1.00	1.00	N/A	4.000	No	No	2.00

Abbreviations

Depth: Depth from free surface, at which CPT was performed (ft)
q_t: Total cone resistance
I_c: Soil behavior type index
Fr: Normalized friction ratio (%)
n: Stress exponent
Q_{tn}: Normalized cone resistance
K_c: Cone resistance correction factor due to fines
$Q_{tn,cs}$: Normalized and adjusted cone resistance
$CRR_{7.5}$: Cyclic resistance ratio for M_w=7.5
FS: Factor of safety against soil liquefaction

:: Liquefaction Potential Index calculation data ::

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
0.10	2.00	0.00	0.00	0.02	0.00	0.16	2.00	0.00	0.00	0.02	0.00
0.21	2.00	0.00	0.00	0.02	0.00	0.29	2.00	0.00	0.00	0.02	0.00
0.36	2.00	0.00	0.00	0.02	0.00	0.40	2.00	0.00	0.00	0.01	0.00
0.51	2.00	0.00	0.00	0.03	0.00	0.57	2.00	0.00	0.00	0.02	0.00
0.61	2.00	0.00	0.00	0.01	0.00	0.70	2.00	0.00	0.00	0.03	0.00
0.76	2.00	0.00	0.00	0.02	0.00	0.81	2.00	0.00	0.00	0.02	0.00
0.87	2.00	0.00	0.00	0.02	0.00	0.96	2.00	0.00	0.00	0.03	0.00
1.00	2.00	0.00	0.00	0.01	0.00	1.05	2.00	0.00	0.00	0.02	0.00
1.16	2.00	0.00	0.00	0.03	0.00	1.20	2.00	0.00	0.00	0.01	0.00
1.26	2.00	0.00	0.00	0.02	0.00	1.35	2.00	0.00	0.00	0.03	0.00
1.40	2.00	0.00	0.00	0.02	0.00	1.45	2.00	0.00	0.00	0.02	0.00
1.55	2.00	0.00	0.00	0.03	0.00	1.60	2.00	0.00	0.00	0.02	0.00
1.64	2.00	0.00	0.00	0.01	0.00	1.71	2.00	0.00	0.00	0.02	0.00
1.79	2.00	0.00	0.00	0.02	0.00	1.87	2.00	0.00	0.00	0.02	0.00
1.95	2.00	0.00	0.00	0.02	0.00	2.00	2.00	0.00	0.00	0.02	0.00
2.04	2.00	0.00	0.00	0.01	0.00	2.11	2.00	0.00	0.00	0.02	0.00
2.19	2.00	0.00	0.00	0.02	0.00	2.24	2.00	0.00	0.00	0.02	0.00
2.30	2.00	0.00	0.00	0.02	0.00	2.38	2.00	0.00	0.00	0.02	0.00
2.45	2.00	0.00	0.00	0.02	0.00	2.50	2.00	0.00	0.00	0.02	0.00
2.58	2.00	0.00	0.00	0.02	0.00	2.64	2.00	0.00	0.00	0.02	0.00
2.69	2.00	0.00	0.00	0.02	0.00	2.79	2.00	0.00	0.00	0.03	0.00
2.85	2.00	0.00	0.00	0.02	0.00	2.90	2.00	0.00	0.00	0.02	0.00
2.98	2.00	0.00	0.00	0.02	0.00	3.05	2.00	0.00	0.00	0.02	0.00
3.09	2.00	0.00	0.00	0.01	0.00	3.17	2.00	0.00	0.00	0.02	0.00
3.24	2.00	0.00	0.00	0.02	0.00	3.29	2.00	0.00	0.00	0.02	0.00
3.36	2.00	0.00	0.00	0.02	0.00	3.44	2.00	0.00	0.00	0.02	0.00
3.48	2.00	0.00	0.00	0.01	0.00	3.56	2.00	0.00	0.00	0.02	0.00
3.64	2.00	0.00	0.00	0.02	0.00	3.69	2.00	0.00	0.00	0.02	0.00
3.76	2.00	0.00	0.00	0.02	0.00	3.84	2.00	0.00	0.00	0.02	0.00
3.88	2.00	0.00	0.00	0.01	0.00	3.98	2.00	0.00	0.00	0.03	0.00
4.03	2.00	0.00	0.00	0.02	0.00	4.08	2.00	0.00	0.00	0.02	0.00
4.14	2.00	0.00	0.00	0.02	0.00	4.23	2.00	0.00	0.00	0.03	0.00
4.27	2.00	0.00	0.00	0.01	0.00	4.36	2.00	0.00	0.00	0.03	0.00
4.41	2.00	0.00	0.00	0.02	0.00	4.46	2.00	0.00	0.00	0.02	0.00
4.55	2.00	0.00	0.00	0.03	0.00	4.61	2.00	0.00	0.00	0.02	0.00
4.66	2.00	0.00	0.00	0.02	0.00	4.75	2.00	0.00	0.00	0.03	0.00
4.80	2.00	0.00	0.00	0.02	0.00	4.86	2.00	0.00	0.00	0.02	0.00
4.96	2.00	0.00	0.00	0.03	0.00	5.01	2.00	0.00	0.00	0.02	0.00
5.06	2.00	0.00	0.00	0.02	0.00	5.16	2.00	0.00	0.00	0.03	0.00
5.21	2.00	0.00	0.00	0.02	0.00	5.26	2.00	0.00	0.00	0.02	0.00
5.32	2.00	0.00	0.00	0.02	0.00	5.41	2.00	0.00	0.00	0.03	0.00
5.46	2.00	0.00	0.00	0.02	0.00	5.52	2.00	0.00	0.00	0.02	0.00
5.60	2.00	0.00	0.00	0.02	0.00	5.66	2.00	0.00	0.00	0.02	0.00
5.71	2.00	0.00	0.00	0.02	0.00	5.81	2.00	0.00	0.00	0.03	0.00
5.89	2.00	0.00	0.00	0.02	0.00	5.91	2.00	0.00	0.00	0.01	0.00
6.00	2.00	0.00	0.00	0.03	0.00	6.06	2.00	0.00	0.00	0.02	0.00
6.11	2.00	0.00	0.00	0.02	0.00	6.20	2.00	0.00	0.00	0.03	0.00
6.24	2.00	0.00	0.00	0.01	0.00	6.30	2.00	0.00	0.00	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
6.38	2.00	0.00	0.00	0.02	0.00	6.46	2.00	0.00	0.00	0.02	0.00
6.50	2.00	0.00	0.00	0.01	0.00	6.60	2.00	0.00	0.00	0.03	0.00
6.63	2.00	0.00	0.00	0.01	0.00	6.72	2.00	0.00	0.00	0.03	0.00
6.80	2.00	0.00	0.00	0.02	0.00	6.84	2.00	0.00	0.00	0.01	0.00
6.90	2.00	0.00	0.00	0.02	0.00	7.00	2.00	0.00	0.00	0.03	0.00
7.04	2.00	0.00	0.00	0.01	0.00	7.09	2.00	0.00	0.00	0.02	0.00
7.20	2.00	0.00	0.00	0.03	0.00	7.24	2.00	0.00	0.00	0.01	0.00
7.30	2.00	0.00	0.00	0.02	0.00	7.39	2.00	0.00	0.00	0.03	0.00
7.43	2.00	0.00	0.00	0.01	0.00	7.50	2.00	0.00	0.00	0.02	0.00
7.59	2.00	0.00	0.00	0.03	0.00	7.64	2.00	0.00	0.00	0.02	0.00
7.70	2.00	0.00	0.00	0.02	0.00	7.79	2.00	0.00	0.00	0.03	0.00
7.83	2.00	0.00	0.00	0.01	0.00	7.90	2.00	0.00	0.00	0.02	0.00
7.94	2.00	0.00	0.00	0.01	0.00	8.03	2.00	0.00	0.00	0.03	0.00
8.11	2.00	0.00	0.00	0.02	0.00	8.17	2.00	0.00	0.00	0.02	0.00
8.21	2.00	0.00	0.00	0.01	0.00	8.28	2.00	0.00	0.00	0.02	0.00
8.37	2.00	0.00	0.00	0.03	0.00	8.41	2.00	0.00	0.00	0.01	0.00
8.48	2.00	0.00	0.00	0.02	0.00	8.57	2.00	0.00	0.00	0.03	0.00
8.61	2.00	0.00	0.00	0.01	0.00	8.67	2.00	0.00	0.00	0.02	0.00
8.77	2.00	0.00	0.00	0.03	0.00	8.81	2.00	0.00	0.00	0.01	0.00
8.87	2.00	0.00	0.00	0.02	0.00	8.96	2.00	0.00	0.00	0.03	0.00
8.99	2.00	0.00	0.00	0.01	0.00	9.07	2.00	0.00	0.00	0.02	0.00
9.16	2.00	0.00	0.00	0.03	0.00	9.21	2.00	0.00	0.00	0.02	0.00
9.27	2.00	0.00	0.00	0.02	0.00	9.36	2.00	0.00	0.00	0.03	0.00
9.40	2.00	0.00	0.00	0.01	0.00	9.48	2.00	0.00	0.00	0.02	0.00
9.52	2.00	0.00	0.00	0.01	0.00	9.61	2.00	0.00	0.00	0.03	0.00
9.65	2.00	0.00	0.00	0.01	0.00	9.72	2.00	0.00	0.00	0.02	0.00
9.81	2.00	0.00	0.00	0.03	0.00	9.86	2.00	0.00	0.00	0.02	0.00
9.91	2.00	0.00	0.00	0.02	0.00	10.00	2.00	0.00	0.00	0.03	0.00
10.05	2.00	0.00	0.00	0.02	0.00	10.16	2.00	0.00	0.00	0.03	0.00
10.20	2.00	0.00	0.00	0.01	0.00	10.25	2.00	0.00	0.00	0.02	0.00
10.31	2.00	0.00	0.00	0.02	0.00	10.40	2.00	0.00	0.00	0.03	0.00
10.44	2.00	0.00	0.00	0.01	0.00	10.51	2.00	0.00	0.00	0.02	0.00
10.59	2.00	0.00	0.00	0.02	0.00	10.65	2.00	0.00	0.00	0.02	0.00
10.71	2.00	0.00	0.00	0.02	0.00	10.80	2.00	0.00	0.00	0.03	0.00
10.85	2.00	0.00	0.00	0.02	0.00	10.90	2.00	0.00	0.00	0.02	0.00
10.96	2.00	0.00	0.00	0.02	0.00	11.04	2.00	0.00	0.00	0.02	0.00
11.10	2.00	0.00	0.00	0.02	0.00	11.18	2.00	0.00	0.00	0.02	0.00
11.24	2.00	0.00	0.00	0.02	0.00	11.30	2.00	0.00	0.00	0.02	0.00
11.35	2.00	0.00	0.00	0.02	0.00	11.42	2.00	0.00	0.00	0.02	0.00
11.51	2.00	0.00	0.00	0.03	0.00	11.55	2.00	0.00	0.00	0.01	0.00
11.62	2.00	0.00	0.00	0.02	0.00	11.71	2.00	0.00	0.00	0.03	0.00
11.75	2.00	0.00	0.00	0.01	0.00	11.85	2.00	0.00	0.00	0.03	0.00
11.90	2.00	0.00	0.00	0.02	0.00	11.94	2.00	0.00	0.00	0.01	0.00
12.02	2.00	0.00	0.00	0.02	0.00	12.10	2.00	0.00	0.00	0.02	0.00
12.15	2.00	0.00	0.00	0.02	0.00	12.24	2.00	0.00	0.00	0.03	0.00
12.30	2.00	0.00	0.00	0.02	0.00	12.35	2.00	0.00	0.00	0.02	0.00
12.44	2.00	0.00	0.00	0.03	0.00	12.50	2.00	0.00	0.00	0.02	0.00
12.55	2.00	0.00	0.00	0.02	0.00	12.63	2.00	0.00	0.00	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
12.70	2.00	0.00	0.00	0.02	0.00	12.74	2.00	0.00	0.00	0.01	0.00
12.84	2.00	0.00	0.00	0.03	0.00	12.86	2.00	0.00	0.00	0.01	0.00
12.94	2.00	0.00	0.00	0.02	0.00	13.01	2.00	0.00	0.00	0.02	0.00
13.09	2.00	0.00	0.00	0.02	0.00	13.14	2.00	0.00	0.00	0.02	0.00
13.20	2.00	0.00	0.00	0.02	0.00	13.29	2.00	0.00	0.00	0.03	0.00
13.33	2.00	0.00	0.00	0.01	0.00	13.39	2.00	0.00	0.00	0.02	0.00
13.49	2.00	0.00	0.00	0.03	0.00	13.53	2.00	0.00	0.00	0.01	0.00
13.59	2.00	0.00	0.00	0.02	0.00	13.69	2.00	0.00	0.00	0.03	0.00
13.73	2.00	0.00	0.00	0.01	0.00	13.79	2.00	0.00	0.00	0.02	0.00
13.89	2.00	0.00	0.00	0.03	0.00	13.94	2.00	0.00	0.00	0.02	0.00
13.99	2.00	0.00	0.00	0.02	0.00	14.08	2.00	0.00	0.00	0.03	0.00
14.13	2.00	0.00	0.00	0.02	0.00	14.18	2.00	0.00	0.00	0.02	0.00
14.27	2.00	0.00	0.00	0.03	0.00	14.32	2.00	0.00	0.00	0.02	0.00
14.37	2.00	0.00	0.00	0.02	0.00	14.48	2.00	0.00	0.00	0.03	0.00
14.52	2.00	0.00	0.00	0.01	0.00	14.58	2.00	0.00	0.00	0.02	0.00
14.68	2.00	0.00	0.00	0.03	0.00	14.72	2.00	0.00	0.00	0.01	0.00
14.77	2.00	0.00	0.00	0.02	0.00	14.83	2.00	0.00	0.00	0.02	0.00
14.92	2.00	0.00	0.00	0.03	0.00	14.98	2.00	0.00	0.00	0.02	0.00
15.07	2.00	0.00	0.00	0.03	0.00	15.11	2.00	0.00	0.00	0.01	0.00
15.17	2.00	0.00	0.00	0.02	0.00	15.27	2.00	0.00	0.00	0.03	0.00
15.31	2.00	0.00	0.00	0.01	0.00	15.38	2.00	0.00	0.00	0.02	0.00
15.47	2.00	0.00	0.00	0.03	0.00	15.52	2.00	0.00	0.00	0.02	0.00
15.56	2.00	0.00	0.00	0.01	0.00	15.64	2.00	0.00	0.00	0.02	0.00
15.71	2.00	0.00	0.00	0.02	0.00	15.75	2.00	0.00	0.00	0.01	0.00
15.87	2.00	0.00	0.00	0.04	0.00	15.91	2.00	0.00	0.00	0.01	0.00
15.96	2.00	0.00	0.00	0.02	0.00	16.01	2.00	0.00	0.00	0.02	0.00
16.11	2.00	0.00	0.00	0.03	0.00	16.15	2.00	0.00	0.00	0.01	0.00
16.22	2.00	0.00	0.00	0.02	0.00	16.31	2.00	0.00	0.00	0.03	0.00
16.36	2.00	0.00	0.00	0.02	0.00	16.41	2.00	0.00	0.00	0.02	0.00
16.51	2.00	0.00	0.00	0.03	0.00	16.54	2.00	0.00	0.00	0.01	0.00
16.61	2.00	0.00	0.00	0.02	0.00	16.70	2.00	0.00	0.00	0.03	0.00
16.75	2.00	0.00	0.00	0.02	0.00	16.81	2.00	0.00	0.00	0.02	0.00
16.91	2.00	0.00	0.00	0.03	0.00	16.95	2.00	0.00	0.00	0.01	0.00
17.01	2.00	0.00	0.00	0.02	0.00	17.11	2.00	0.00	0.00	0.03	0.00
17.13	2.00	0.00	0.00	0.01	0.00	17.21	2.00	0.00	0.00	0.02	0.00
17.29	2.00	0.00	0.00	0.02	0.00	17.34	2.00	0.00	0.00	0.02	0.00
17.43	2.00	0.00	0.00	0.03	0.00	17.48	2.00	0.00	0.00	0.02	0.00
17.54	2.00	0.00	0.00	0.02	0.00	17.63	2.00	0.00	0.00	0.03	0.00
17.68	2.00	0.00	0.00	0.02	0.00	17.73	2.00	0.00	0.00	0.02	0.00
17.83	2.00	0.00	0.00	0.03	0.00	17.85	2.00	0.00	0.00	0.01	0.00
17.93	2.00	0.00	0.00	0.02	0.00	17.98	2.00	0.00	0.00	0.02	0.00
18.07	2.00	0.00	0.00	0.03	0.00	18.12	2.00	0.00	0.00	0.02	0.00
18.18	2.00	0.00	0.00	0.02	0.00	18.24	2.00	0.00	0.00	0.02	0.00
18.33	2.00	0.00	0.00	0.03	0.00	18.38	2.00	0.00	0.00	0.02	0.00
18.47	2.00	0.00	0.00	0.03	0.00	18.53	2.00	0.00	0.00	0.02	0.00
18.57	2.00	0.00	0.00	0.01	0.00	18.67	2.00	0.00	0.00	0.03	0.00
18.72	2.00	0.00	0.00	0.02	0.00	18.78	2.00	0.00	0.00	0.02	0.00
18.85	2.00	0.00	0.00	0.02	0.00	18.93	2.00	0.00	0.00	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
18.97	2.00	0.00	0.00	0.01	0.00	19.08	2.00	0.00	0.00	0.03	0.00
19.12	2.00	0.00	0.00	0.01	0.00	19.22	2.00	0.00	0.00	0.03	0.00
19.27	2.00	0.00	0.00	0.02	0.00	19.32	2.00	0.00	0.00	0.02	0.00
19.37	2.00	0.00	0.00	0.02	0.00	19.43	2.00	0.00	0.00	0.02	0.00
19.52	2.00	0.00	0.00	0.03	0.00	19.57	2.00	0.00	0.00	0.02	0.00
19.67	2.00	0.00	0.00	0.03	0.00	19.72	2.00	0.00	0.00	0.02	0.00
19.77	2.00	0.00	0.00	0.02	0.00	19.82	2.00	0.00	0.00	0.02	0.00
19.92	2.00	0.00	0.00	0.03	0.00	19.97	2.00	0.00	0.00	0.02	0.00
20.04	2.00	0.00	0.00	0.02	0.00	20.08	2.00	0.00	0.00	0.01	0.00
20.16	2.00	0.00	0.00	0.02	0.00	20.24	2.00	0.00	0.00	0.02	0.00
20.28	2.00	0.00	0.00	0.01	0.00	20.37	2.00	0.00	0.00	0.03	0.00
20.41	2.00	0.00	0.00	0.01	0.00	20.50	2.00	0.00	0.00	0.03	0.00
20.57	2.00	0.00	0.00	0.02	0.00	20.61	2.00	0.00	0.00	0.01	0.00
20.70	2.00	0.00	0.00	0.03	0.00	20.76	2.00	0.00	0.00	0.02	0.00
20.81	2.00	0.00	0.00	0.02	0.00	20.89	2.00	0.00	0.00	0.02	0.00
20.95	2.00	0.00	0.00	0.02	0.00	21.00	2.00	0.00	0.00	0.02	0.00
21.10	2.00	0.00	0.00	0.03	0.00	21.14	2.00	0.00	0.00	0.01	0.00
21.21	2.00	0.00	0.00	0.02	0.00	21.30	2.00	0.00	0.00	0.03	0.00
21.34	2.00	0.00	0.00	0.01	0.00	21.40	2.00	0.00	0.00	0.02	0.00
21.48	2.00	0.00	0.00	0.02	0.00	21.54	2.00	0.00	0.00	0.02	0.00
21.60	2.00	0.00	0.00	0.02	0.00	21.68	2.00	0.00	0.00	0.02	0.00
21.75	2.00	0.00	0.00	0.02	0.00	21.80	2.00	0.00	0.00	0.02	0.00
21.88	2.00	0.00	0.00	0.02	0.00	21.92	2.00	0.00	0.00	0.01	0.00
21.99	2.00	0.00	0.00	0.02	0.00	22.08	2.00	0.00	0.00	0.03	0.00
22.15	2.00	0.00	0.00	0.02	0.00	22.19	2.00	0.00	0.00	0.01	0.00
22.28	2.00	0.00	0.00	0.03	0.00	22.34	2.00	0.00	0.00	0.02	0.00
22.39	2.00	0.00	0.00	0.02	0.00	22.47	2.00	0.00	0.00	0.02	0.00
22.54	2.00	0.00	0.00	0.02	0.00	22.58	2.00	0.00	0.00	0.01	0.00
22.68	2.00	0.00	0.00	0.03	0.00	22.74	2.00	0.00	0.00	0.02	0.00
22.79	2.00	0.00	0.00	0.02	0.00	22.84	2.00	0.00	0.00	0.02	0.00
22.94	2.00	0.00	0.00	0.03	0.00	22.99	2.00	0.00	0.00	0.02	0.00
23.04	2.00	0.00	0.00	0.02	0.00	23.11	2.00	0.00	0.00	0.02	0.00
23.18	2.00	0.00	0.00	0.02	0.00	23.23	2.00	0.00	0.00	0.02	0.00
23.34	2.00	0.00	0.00	0.03	0.00	23.37	2.00	0.00	0.00	0.01	0.00
23.44	2.00	0.00	0.00	0.02	0.00	23.54	2.00	0.00	0.00	0.03	0.00
23.60	2.00	0.00	0.00	0.02	0.00	23.64	2.00	0.00	0.00	0.01	0.00
23.71	2.00	0.00	0.00	0.02	0.00	23.79	2.00	0.00	0.00	0.02	0.00
23.84	2.00	0.00	0.00	0.02	0.00	23.89	2.00	0.00	0.00	0.02	0.00
23.99	2.00	0.00	0.00	0.03	0.00	24.03	2.00	0.00	0.00	0.01	0.00
24.10	2.00	0.00	0.00	0.02	0.00	24.18	2.00	0.00	0.00	0.02	0.00
24.23	2.00	0.00	0.00	0.02	0.00	24.31	2.00	0.00	0.00	0.02	0.00
24.36	2.00	0.00	0.00	0.02	0.00	24.45	2.00	0.00	0.00	0.03	0.00
24.49	2.00	0.00	0.00	0.01	0.00	24.57	2.00	0.00	0.00	0.02	0.00
24.61	2.00	0.00	0.00	0.01	0.00	24.69	2.00	0.00	0.00	0.02	0.00
24.74	2.00	0.00	0.00	0.02	0.00	24.82	2.00	0.00	0.00	0.02	0.00
24.89	2.00	0.00	0.00	0.02	0.00	24.94	2.00	0.00	0.00	0.02	0.00
25.01	2.00	0.00	0.00	0.02	0.00	25.09	2.00	0.00	0.00	0.02	0.00
25.13	2.00	0.00	0.00	0.01	0.00	25.22	2.00	0.00	0.00	0.03	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
25.28	2.00	0.00	0.00	0.02	0.00	25.34	2.00	0.00	0.00	0.02	0.00
25.44	2.00	0.00	0.00	0.03	0.00	25.48	2.00	0.00	0.00	0.01	0.00
25.53	2.00	0.00	0.00	0.02	0.00	25.59	2.00	0.00	0.00	0.02	0.00
25.68	2.00	0.00	0.00	0.03	0.00	25.73	2.00	0.00	0.00	0.02	0.00
25.79	2.00	0.00	0.00	0.02	0.00	25.88	2.00	0.00	0.00	0.03	0.00
25.93	2.00	0.00	0.00	0.02	0.00	25.99	2.00	0.00	0.00	0.02	0.00
26.08	2.00	0.00	0.00	0.03	0.00	26.14	2.00	0.00	0.00	0.02	0.00
26.19	2.00	0.00	0.00	0.02	0.00	26.28	2.00	0.00	0.00	0.03	0.00
26.34	2.00	0.00	0.00	0.02	0.00	26.39	2.00	0.00	0.00	0.02	0.00
26.45	2.00	0.00	0.00	0.02	0.00	26.53	2.00	0.00	0.00	0.02	0.00
26.58	2.00	0.00	0.00	0.02	0.00	26.68	2.00	0.00	0.00	0.03	0.00
26.73	2.00	0.00	0.00	0.02	0.00	26.78	2.00	0.00	0.00	0.02	0.00
26.88	2.00	0.00	0.00	0.03	0.00	26.93	2.00	0.00	0.00	0.02	0.00
26.98	2.00	0.00	0.00	0.02	0.00	27.04	2.00	0.00	0.00	0.02	0.00
27.13	2.00	0.00	0.00	0.03	0.00	27.22	2.00	0.00	0.00	0.03	0.00
27.24	2.00	0.00	0.00	0.01	0.00	27.33	2.00	0.00	0.00	0.03	0.00
27.37	2.00	0.00	0.00	0.01	0.00	27.43	2.00	0.00	0.00	0.02	0.00
27.52	2.00	0.00	0.00	0.03	0.00	27.57	2.00	0.00	0.00	0.02	0.00
27.63	2.00	0.00	0.00	0.02	0.00	27.72	2.00	0.00	0.00	0.03	0.00
27.76	2.00	0.00	0.00	0.01	0.00	27.84	2.00	0.00	0.00	0.02	0.00
27.93	2.00	0.00	0.00	0.03	0.00	27.97	2.00	0.00	0.00	0.01	0.00
28.02	2.00	0.00	0.00	0.02	0.00	28.12	2.00	0.00	0.00	0.03	0.00
28.17	2.00	0.00	0.00	0.02	0.00	28.23	2.00	0.00	0.00	0.02	0.00
28.32	2.00	0.00	0.00	0.03	0.00	28.37	2.00	0.00	0.00	0.02	0.00
28.42	2.00	0.00	0.00	0.02	0.00	28.48	2.00	0.00	0.00	0.02	0.00
28.57	2.00	0.00	0.00	0.03	0.00	28.61	2.00	0.00	0.00	0.01	0.00
28.69	2.00	0.00	0.00	0.02	0.00	28.77	2.00	0.00	0.00	0.02	0.00
28.83	2.00	0.00	0.00	0.02	0.00	28.88	2.00	0.00	0.00	0.02	0.00
28.97	2.00	0.00	0.00	0.03	0.00	29.02	2.00	0.00	0.00	0.02	0.00
29.08	2.00	0.00	0.00	0.02	0.00	29.17	2.00	0.00	0.00	0.03	0.00
29.21	2.00	0.00	0.00	0.01	0.00	29.28	2.00	0.00	0.00	0.02	0.00
29.37	2.00	0.00	0.00	0.03	0.00	29.41	2.00	0.00	0.00	0.01	0.00
29.47	2.00	0.00	0.00	0.02	0.00	29.56	2.00	0.00	0.00	0.03	0.00
29.62	2.00	0.00	0.00	0.02	0.00	29.68	2.00	0.00	0.00	0.02	0.00
29.76	2.00	0.00	0.00	0.02	0.00	29.83	2.00	0.00	0.00	0.02	0.00
29.87	2.00	0.00	0.00	0.01	0.00	29.96	2.00	0.00	0.00	0.03	0.00
30.01	2.00	0.00	0.00	0.02	0.00	30.07	2.00	0.00	0.00	0.02	0.00
30.16	2.00	0.00	0.00	0.03	0.00	30.20	2.00	0.00	0.00	0.01	0.00
30.27	2.00	0.00	0.00	0.02	0.00	30.34	2.00	0.00	0.00	0.02	0.00
30.42	2.00	0.00	0.00	0.02	0.00	30.46	2.00	0.00	0.00	0.01	0.00
30.52	2.00	0.00	0.00	0.02	0.00	30.58	2.00	0.00	0.00	0.02	0.00
30.66	2.00	0.00	0.00	0.02	0.00	30.71	2.00	0.00	0.00	0.02	0.00
30.81	2.00	0.00	0.00	0.03	0.00	30.87	2.00	0.00	0.00	0.02	0.00
30.91	2.00	0.00	0.00	0.01	0.00	31.01	2.00	0.00	0.00	0.03	0.00
31.06	2.00	0.00	0.00	0.02	0.00	31.11	2.00	0.00	0.00	0.02	0.00
31.19	2.00	0.00	0.00	0.02	0.00	31.26	2.00	0.00	0.00	0.02	0.00
31.35	2.00	0.00	0.00	0.03	0.00	31.37	2.00	0.00	0.00	0.01	0.00
31.46	2.00	0.00	0.00	0.03	0.00	31.55	2.00	0.00	0.00	0.03	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
31.59	2.00	0.00	0.00	0.01	0.00	31.66	2.00	0.00	0.00	0.02	0.00
31.70	2.00	0.00	0.00	0.01	0.00	31.79	2.00	0.00	0.00	0.03	0.00
31.86	2.00	0.00	0.00	0.02	0.00	31.91	2.00	0.00	0.00	0.02	0.00
31.99	2.00	0.00	0.00	0.02	0.00	32.06	2.00	0.00	0.00	0.02	0.00
32.10	2.00	0.00	0.00	0.01	0.00	32.20	2.00	0.00	0.00	0.03	0.00
32.26	2.00	0.00	0.00	0.02	0.00	32.30	2.00	0.00	0.00	0.01	0.00
32.35	2.00	0.00	0.00	0.02	0.00	32.46	2.00	0.00	0.00	0.03	0.00
32.49	2.00	0.00	0.00	0.01	0.00	32.58	2.00	0.00	0.00	0.03	0.00
32.62	2.00	0.00	0.00	0.01	0.00	32.69	2.00	0.00	0.00	0.02	0.00
32.78	2.00	0.00	0.00	0.03	0.00	32.82	2.00	0.00	0.00	0.01	0.00
32.89	2.00	0.00	0.00	0.02	0.00	32.98	2.00	0.00	0.00	0.03	0.00
33.02	2.00	0.00	0.00	0.01	0.00	33.08	2.00	0.00	0.00	0.02	0.00
33.18	2.00	0.00	0.00	0.03	0.00	33.21	2.00	0.00	0.00	0.01	0.00
33.29	2.00	0.00	0.00	0.02	0.00	33.37	2.00	0.00	0.00	0.02	0.00
33.42	2.00	0.00	0.00	0.02	0.00	33.47	2.00	0.00	0.00	0.02	0.00
33.53	2.00	0.00	0.00	0.02	0.00	33.62	2.00	0.00	0.00	0.03	0.00
33.67	2.00	0.00	0.00	0.02	0.00	33.73	2.00	0.00	0.00	0.02	0.00
33.82	2.00	0.00	0.00	0.03	0.00	33.87	2.00	0.00	0.00	0.02	0.00
33.93	2.00	0.00	0.00	0.02	0.00	34.02	2.00	0.00	0.00	0.03	0.00
34.06	2.00	0.00	0.00	0.01	0.00	34.13	2.00	0.00	0.00	0.02	0.00
34.22	2.00	0.00	0.00	0.03	0.00	34.26	2.00	0.00	0.00	0.01	0.00
34.32	2.00	0.00	0.00	0.02	0.00	34.42	2.00	0.00	0.00	0.03	0.00
34.46	2.00	0.00	0.00	0.01	0.00	34.52	2.00	0.00	0.00	0.02	0.00
34.61	2.00	0.00	0.00	0.03	0.00	34.70	2.00	0.00	0.00	0.03	0.00
34.76	2.00	0.00	0.00	0.02	0.00	34.82	2.00	0.00	0.00	0.02	0.00
34.86	2.00	0.00	0.00	0.01	0.00	34.92	2.00	0.00	0.00	0.02	0.00
35.02	2.00	0.00	0.00	0.03	0.00	35.06	2.00	0.00	0.00	0.01	0.00
35.11	2.00	0.00	0.00	0.02	0.00	35.19	2.00	0.00	0.00	0.02	0.00
35.25	2.00	0.00	0.00	0.02	0.00	35.31	2.00	0.00	0.00	0.02	0.00
35.40	2.00	0.00	0.00	0.03	0.00	35.45	2.00	0.00	0.00	0.02	0.00
35.50	2.00	0.00	0.00	0.02	0.00	35.56	2.00	0.00	0.00	0.02	0.00
35.64	2.00	0.00	0.00	0.02	0.00	35.72	2.00	0.00	0.00	0.02	0.00
35.81	2.00	0.00	0.00	0.03	0.00	35.85	2.00	0.00	0.00	0.01	0.00
35.90	2.00	0.00	0.00	0.02	0.00	35.96	2.00	0.00	0.00	0.02	0.00
36.04	2.00	0.00	0.00	0.02	0.00	36.11	2.00	0.00	0.00	0.02	0.00
36.16	2.00	0.00	0.00	0.02	0.00	36.25	2.00	0.00	0.00	0.03	0.00
36.31	2.00	0.00	0.00	0.02	0.00	36.36	2.00	0.00	0.00	0.02	0.00
36.44	2.00	0.00	0.00	0.02	0.00	36.50	2.00	0.00	0.00	0.02	0.00
36.56	2.00	0.00	0.00	0.02	0.00	36.65	2.00	0.00	0.00	0.03	0.00
36.68	2.00	0.00	0.00	0.01	0.00	36.76	2.00	0.00	0.00	0.02	0.00
36.84	2.00	0.00	0.00	0.02	0.00	36.91	2.00	0.00	0.00	0.02	0.00
36.96	2.00	0.00	0.00	0.02	0.00	37.04	2.00	0.00	0.00	0.02	0.00
37.10	2.00	0.00	0.00	0.02	0.00	37.15	2.00	0.00	0.00	0.02	0.00
37.23	2.00	0.00	0.00	0.02	0.00	37.30	2.00	0.00	0.00	0.02	0.00
37.35	2.00	0.00	0.00	0.02	0.00	37.45	2.00	0.00	0.00	0.03	0.00
37.51	2.00	0.00	0.00	0.02	0.00	37.55	2.00	0.00	0.00	0.01	0.00
37.62	2.00	0.00	0.00	0.02	0.00	37.70	2.00	0.00	0.00	0.02	0.00
37.75	2.00	0.00	0.00	0.02	0.00	37.80	2.00	0.00	0.00	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
37.90	2.00	0.00	0.00	0.03	0.00	37.95	2.00	0.00	0.00	0.02	0.00
38.05	2.00	0.00	0.00	0.03	0.00	38.06	2.00	0.00	0.00	0.00	0.00
38.15	2.00	0.00	0.00	0.03	0.00	38.19	2.00	0.00	0.00	0.01	0.00
38.27	2.00	0.00	0.00	0.02	0.00	38.34	2.00	0.00	0.00	0.02	0.00
38.39	2.00	0.00	0.00	0.02	0.00	38.46	2.00	0.00	0.00	0.02	0.00
38.55	2.00	0.00	0.00	0.03	0.00	38.59	2.00	0.00	0.00	0.01	0.00
38.68	2.00	0.00	0.00	0.03	0.00	38.75	2.00	0.00	0.00	0.02	0.00
38.80	2.00	0.00	0.00	0.02	0.00	38.87	2.00	0.00	0.00	0.02	0.00
38.95	2.00	0.00	0.00	0.02	0.00	38.99	0.48	0.52	0.45	0.04	0.03
39.04	0.50	0.50	0.48	0.05	0.03	39.11	0.53	0.47	0.51	0.07	0.04
39.19	0.54	0.46	0.53	0.08	0.05	39.27	0.53	0.47	0.52	0.08	0.05
39.33	0.52	0.48	0.50	0.06	0.04	39.39	0.50	0.50	0.48	0.06	0.04
39.45	2.00	0.00	0.00	0.02	0.00	39.53	2.00	0.00	0.00	0.02	0.00
39.57	2.00	0.00	0.00	0.01	0.00	39.64	2.00	0.00	0.00	0.02	0.00
39.72	2.00	0.00	0.00	0.02	0.00	39.79	2.00	0.00	0.00	0.02	0.00
39.84	2.00	0.00	0.00	0.02	0.00	39.93	2.00	0.00	0.00	0.03	0.00
39.98	2.00	0.00	0.00	0.02	0.00	40.05	2.00	0.00	0.00	0.02	0.00
40.09	2.00	0.00	0.00	0.01	0.00	40.19	2.00	0.00	0.00	0.03	0.00
40.23	2.00	0.00	0.00	0.01	0.00	40.34	0.47	0.53	0.44	0.11	0.07
40.38	0.53	0.47	0.52	0.04	0.02	40.43	0.61	0.39	0.66	0.05	0.02
40.50	0.70	0.30	0.91	0.07	0.02	40.58	0.78	0.22	1.48	0.08	0.02
40.63	0.85	0.15	2.81	0.05	0.01	40.70	0.92	0.08	9.75	0.07	0.01
40.75	0.98	0.02	8683.83	0.05	0.00	40.84	1.03	0.00	0.00	0.03	0.00
40.88	1.07	0.00	0.00	0.01	0.00	40.95	1.11	0.00	0.00	0.02	0.00
41.03	2.00	0.00	0.00	0.02	0.00	41.08	2.00	0.00	0.00	0.02	0.00
41.15	2.00	0.00	0.00	0.02	0.00	41.23	2.00	0.00	0.00	0.02	0.00
41.28	2.00	0.00	0.00	0.02	0.00	41.35	2.00	0.00	0.00	0.02	0.00
41.43	2.00	0.00	0.00	0.02	0.00	41.48	2.00	0.00	0.00	0.02	0.00
41.54	1.44	0.00	0.00	0.02	0.00	41.62	1.55	0.00	0.00	0.02	0.00
41.68	1.67	0.00	0.00	0.02	0.00	41.77	1.79	0.00	0.00	0.03	0.00
41.82	1.91	0.00	0.00	0.02	0.00	41.88	2.00	0.00	0.00	0.02	0.00
41.97	2.00	0.00	0.00	0.03	0.00	42.01	2.00	0.00	0.00	0.01	0.00
42.10	2.00	0.00	0.00	0.03	0.00	42.17	2.00	0.00	0.00	0.02	0.00
42.22	2.00	0.00	0.00	0.02	0.00	42.28	2.00	0.00	0.00	0.02	0.00
42.33	2.00	0.00	0.00	0.02	0.00	42.41	2.00	0.00	0.00	0.02	0.00
42.48	2.00	0.00	0.00	0.02	0.00	42.52	2.00	0.00	0.00	0.01	0.00
42.60	2.00	0.00	0.00	0.02	0.00	42.66	2.00	0.00	0.00	0.02	0.00
42.72	2.00	0.00	0.00	0.02	0.00	42.81	2.00	0.00	0.00	0.03	0.00
42.87	2.00	0.00	0.00	0.02	0.00	42.92	2.00	0.00	0.00	0.02	0.00
43.00	2.00	0.00	0.00	0.02	0.00	43.06	2.00	0.00	0.00	0.02	0.00
43.11	2.00	0.00	0.00	0.02	0.00	43.18	2.00	0.00	0.00	0.02	0.00
43.25	1.94	0.00	0.00	0.02	0.00	43.31	1.83	0.00	0.00	0.02	0.00
43.39	1.74	0.00	0.00	0.02	0.00	43.45	1.66	0.00	0.00	0.02	0.00
43.51	1.61	0.00	0.00	0.02	0.00	43.61	1.57	0.00	0.00	0.03	0.00
43.65	1.56	0.00	0.00	0.01	0.00	43.72	1.54	0.00	0.00	0.02	0.00
43.81	1.51	0.00	0.00	0.03	0.00	43.85	1.48	0.00	0.00	0.01	0.00
43.92	1.42	0.00	0.00	0.02	0.00	44.01	1.37	0.00	0.00	0.03	0.00
44.05	1.31	0.00	0.00	0.01	0.00	44.10	1.22	0.00	0.00	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
44.20	1.13	0.00	0.00	0.03	0.00	44.25	1.05	0.00	0.00	0.02	0.00
44.30	0.98	0.02	19369.06	0.05	0.00	44.40	0.92	0.08	10.80	0.10	0.01
44.45	0.87	0.13	3.71	0.05	0.01	44.50	0.85	0.15	2.58	0.05	0.01
44.57	0.82	0.18	2.04	0.07	0.01	44.63	0.82	0.18	2.01	0.06	0.01
44.69	0.86	0.14	3.09	0.06	0.01	44.79	0.91	0.09	8.24	0.10	0.01
44.84	0.97	0.03	445.51	0.05	0.00	44.89	1.02	0.00	0.00	0.02	0.00
44.96	1.06	0.00	0.00	0.02	0.00	45.04	1.10	0.00	0.00	0.02	0.00
45.09	1.12	0.00	0.00	0.02	0.00	45.17	1.15	0.00	0.00	0.02	0.00
45.24	1.17	0.00	0.00	0.02	0.00	45.28	1.18	0.00	0.00	0.01	0.00
45.38	1.18	0.00	0.00	0.03	0.00	45.42	1.18	0.00	0.00	0.01	0.00
45.49	1.18	0.00	0.00	0.02	0.00	45.57	1.17	0.00	0.00	0.02	0.00
45.63	1.16	0.00	0.00	0.02	0.00	45.69	1.12	0.00	0.00	0.02	0.00
45.78	1.06	0.00	0.00	0.03	0.00	45.84	0.98	0.02	100523.05	0.06	0.00
45.89	0.91	0.09	7.00	0.05	0.00	45.93	0.82	0.18	1.95	0.04	0.01
46.02	2.00	0.00	0.00	0.03	0.00	46.08	2.00	0.00	0.00	0.02	0.00
46.13	2.00	0.00	0.00	0.02	0.00	46.22	2.00	0.00	0.00	0.03	0.00
46.28	2.00	0.00	0.00	0.02	0.00	46.33	2.00	0.00	0.00	0.02	0.00
46.43	2.00	0.00	0.00	0.03	0.00	46.47	2.00	0.00	0.00	0.01	0.00
46.53	2.00	0.00	0.00	0.02	0.00	46.63	2.00	0.00	0.00	0.03	0.00
46.67	2.00	0.00	0.00	0.01	0.00	46.73	2.00	0.00	0.00	0.02	0.00
46.83	2.00	0.00	0.00	0.03	0.00	46.87	2.00	0.00	0.00	0.01	0.00
46.93	2.00	0.00	0.00	0.02	0.00	47.02	2.00	0.00	0.00	0.03	0.00
47.08	2.00	0.00	0.00	0.02	0.00	47.12	2.00	0.00	0.00	0.01	0.00
47.18	2.00	0.00	0.00	0.02	0.00	47.27	2.00	0.00	0.00	0.03	0.00
47.31	2.00	0.00	0.00	0.01	0.00	47.39	2.00	0.00	0.00	0.02	0.00
47.48	2.00	0.00	0.00	0.03	0.00	47.52	2.00	0.00	0.00	0.01	0.00
47.59	2.00	0.00	0.00	0.02	0.00	47.66	2.00	0.00	0.00	0.02	0.00
47.74	2.00	0.00	0.00	0.02	0.00	47.79	2.00	0.00	0.00	0.02	0.00
47.86	2.00	0.00	0.00	0.02	0.00	47.94	2.00	0.00	0.00	0.02	0.00
47.99	2.00	0.00	0.00	0.02	0.00	48.05	2.00	0.00	0.00	0.02	0.00
48.13	2.00	0.00	0.00	0.02	0.00	48.19	2.00	0.00	0.00	0.02	0.00
48.26	2.00	0.00	0.00	0.02	0.00	48.34	2.00	0.00	0.00	0.02	0.00
48.39	0.58	0.42	0.59	0.05	0.02	48.43	0.61	0.39	0.65	0.04	0.01
48.51	2.00	0.00	0.00	0.02	0.00	48.58	2.00	0.00	0.00	0.02	0.00
48.63	2.00	0.00	0.00	0.02	0.00	48.72	2.00	0.00	0.00	0.03	0.00
48.78	2.00	0.00	0.00	0.02	0.00	48.83	2.00	0.00	0.00	0.02	0.00
48.90	2.00	0.00	0.00	0.02	0.00	48.99	2.00	0.00	0.00	0.03	0.00
49.03	2.00	0.00	0.00	0.01	0.00	49.08	2.00	0.00	0.00	0.02	0.00
49.17	2.00	0.00	0.00	0.03	0.00	49.23	2.00	0.00	0.00	0.02	0.00
49.32	2.00	0.00	0.00	0.03	0.00	49.35	2.00	0.00	0.00	0.01	0.00
49.43	2.00	0.00	0.00	0.02	0.00	49.50	2.00	0.00	0.00	0.02	0.00
49.58	2.00	0.00	0.00	0.02	0.00	49.63	2.00	0.00	0.00	0.02	0.00
49.72	2.00	0.00	0.00	0.03	0.00	49.78	2.00	0.00	0.00	0.02	0.00
49.83	2.00	0.00	0.00	0.02	0.00	49.90	1.57	0.00	0.00	0.02	0.00
49.98	1.64	0.00	0.00	0.02	0.00	50.02	2.00	0.00	0.00	0.01	0.00
50.08	2.00	0.00	0.00	0.02	0.00	50.18	2.00	0.00	0.00	0.03	0.00
50.23	2.00	0.00	0.00	0.02	0.00	50.27	2.00	0.00	0.00	0.01	0.00
50.36	2.00	0.00	0.00	0.03	0.00	50.40	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
50.47	2.00	0.00	0.00	0.02	0.00	50.55	2.00	0.00	0.00	0.02	0.00
50.63	2.00	0.00	0.00	0.02	0.00	50.67	2.00	0.00	0.00	0.01	0.00
50.72	2.00	0.00	0.00	0.02	0.00	50.83	2.00	0.00	0.00	0.03	0.00
50.88	2.00	0.00	0.00	0.02	0.00	50.93	2.00	0.00	0.00	0.02	0.00
51.02	2.00	0.00	0.00	0.03	0.00	51.08	2.00	0.00	0.00	0.02	0.00
51.12	2.00	0.00	0.00	0.01	0.00	51.21	2.00	0.00	0.00	0.03	0.00
51.27	2.00	0.00	0.00	0.02	0.00	51.32	2.00	0.00	0.00	0.02	0.00
51.39	2.00	0.00	0.00	0.02	0.00	51.47	2.00	0.00	0.00	0.02	0.00
51.55	2.00	0.00	0.00	0.02	0.00	51.60	2.00	0.00	0.00	0.02	0.00
51.67	2.00	0.00	0.00	0.02	0.00	51.72	2.00	0.00	0.00	0.02	0.00
51.79	2.00	0.00	0.00	0.02	0.00	51.87	2.00	0.00	0.00	0.02	0.00
51.91	2.00	0.00	0.00	0.01	0.00	51.98	2.00	0.00	0.00	0.02	0.00
52.06	2.00	0.00	0.00	0.02	0.00	52.12	2.00	0.00	0.00	0.02	0.00
52.17	2.00	0.00	0.00	0.02	0.00	52.26	2.00	0.00	0.00	0.03	0.00
52.31	2.00	0.00	0.00	0.02	0.00	52.38	2.00	0.00	0.00	0.02	0.00
52.47	2.00	0.00	0.00	0.03	0.00	52.51	2.00	0.00	0.00	0.01	0.00
52.56	2.00	0.00	0.00	0.02	0.00	52.66	2.00	0.00	0.00	0.03	0.00
52.70	2.00	0.00	0.00	0.01	0.00	52.77	2.00	0.00	0.00	0.02	0.00
52.87	2.00	0.00	0.00	0.03	0.00	52.92	2.00	0.00	0.00	0.02	0.00
52.97	2.00	0.00	0.00	0.02	0.00	53.02	2.00	0.00	0.00	0.02	0.00
53.10	2.00	0.00	0.00	0.02	0.00	53.16	2.00	0.00	0.00	0.02	0.00
53.22	2.00	0.00	0.00	0.02	0.00	53.31	2.00	0.00	0.00	0.03	0.00
53.36	2.00	0.00	0.00	0.02	0.00	53.42	2.00	0.00	0.00	0.02	0.00
53.51	2.00	0.00	0.00	0.03	0.00	53.56	2.00	0.00	0.00	0.02	0.00
53.62	2.00	0.00	0.00	0.02	0.00	53.71	2.00	0.00	0.00	0.03	0.00
53.75	2.00	0.00	0.00	0.01	0.00	53.83	2.00	0.00	0.00	0.02	0.00
53.91	2.00	0.00	0.00	0.02	0.00	53.98	2.00	0.00	0.00	0.02	0.00
54.01	2.00	0.00	0.00	0.01	0.00	54.11	2.00	0.00	0.00	0.03	0.00
54.15	2.00	0.00	0.00	0.01	0.00	54.21	2.00	0.00	0.00	0.02	0.00
54.27	2.00	0.00	0.00	0.02	0.00	54.35	2.00	0.00	0.00	0.02	0.00
54.42	2.00	0.00	0.00	0.02	0.00	54.46	2.00	0.00	0.00	0.01	0.00
54.55	2.00	0.00	0.00	0.03	0.00	54.60	2.00	0.00	0.00	0.02	0.00
54.67	2.00	0.00	0.00	0.02	0.00	54.74	2.00	0.00	0.00	0.02	0.00
54.79	2.00	0.00	0.00	0.02	0.00	54.86	2.00	0.00	0.00	0.02	0.00
54.96	2.00	0.00	0.00	0.03	0.00	55.03	2.00	0.00	0.00	0.02	0.00
55.06	2.00	0.00	0.00	0.01	0.00	55.14	2.00	0.00	0.00	0.02	0.00
55.21	2.00	0.00	0.00	0.02	0.00	55.25	2.00	0.00	0.00	0.01	0.00
55.32	2.00	0.00	0.00	0.02	0.00	55.41	2.00	0.00	0.00	0.03	0.00
55.45	2.00	0.00	0.00	0.01	0.00	55.52	2.00	0.00	0.00	0.02	0.00
55.61	2.00	0.00	0.00	0.03	0.00	55.65	2.00	0.00	0.00	0.01	0.00
55.71	2.00	0.00	0.00	0.02	0.00	55.80	2.00	0.00	0.00	0.03	0.00
55.86	2.00	0.00	0.00	0.02	0.00	55.95	2.00	0.00	0.00	0.03	0.00
56.00	2.00	0.00	0.00	0.02	0.00	56.05	2.00	0.00	0.00	0.02	0.00
56.11	2.00	0.00	0.00	0.02	0.00	56.20	2.00	0.00	0.00	0.03	0.00
56.24	2.00	0.00	0.00	0.01	0.00	56.31	2.00	0.00	0.00	0.02	0.00
56.39	2.00	0.00	0.00	0.02	0.00	56.43	2.00	0.00	0.00	0.01	0.00
56.50	2.00	0.00	0.00	0.02	0.00	56.60	2.00	0.00	0.00	0.03	0.00
56.66	2.00	0.00	0.00	0.02	0.00	56.70	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
56.79	2.00	0.00	0.00	0.03	0.00	56.84	2.00	0.00	0.00	0.02	0.00
56.92	2.00	0.00	0.00	0.02	0.00	56.99	2.00	0.00	0.00	0.02	0.00
57.03	2.00	0.00	0.00	0.01	0.00	57.09	2.00	0.00	0.00	0.02	0.00
57.18	2.00	0.00	0.00	0.03	0.00	57.23	2.00	0.00	0.00	0.02	0.00
57.31	2.00	0.00	0.00	0.02	0.00	57.38	2.00	0.00	0.00	0.02	0.00
57.43	2.00	0.00	0.00	0.02	0.00	57.50	2.00	0.00	0.00	0.02	0.00
57.58	2.00	0.00	0.00	0.02	0.00	57.62	2.00	0.00	0.00	0.01	0.00
57.68	2.00	0.00	0.00	0.02	0.00	57.78	2.00	0.00	0.00	0.03	0.00
57.82	2.00	0.00	0.00	0.01	0.00	57.89	2.00	0.00	0.00	0.02	0.00
57.97	2.00	0.00	0.00	0.02	0.00	58.02	2.00	0.00	0.00	0.02	0.00
58.09	2.00	0.00	0.00	0.02	0.00	58.17	2.00	0.00	0.00	0.02	0.00
58.23	2.00	0.00	0.00	0.02	0.00	58.28	2.00	0.00	0.00	0.02	0.00
58.37	2.00	0.00	0.00	0.03	0.00	58.43	2.00	0.00	0.00	0.02	0.00
58.48	2.00	0.00	0.00	0.02	0.00	58.57	2.00	0.00	0.00	0.03	0.00
58.62	2.00	0.00	0.00	0.02	0.00	58.67	2.00	0.00	0.00	0.02	0.00
58.78	2.00	0.00	0.00	0.03	0.00	58.82	2.00	0.00	0.00	0.01	0.00
58.88	2.00	0.00	0.00	0.02	0.00	58.97	2.00	0.00	0.00	0.03	0.00
59.01	2.00	0.00	0.00	0.01	0.00	59.07	2.00	0.00	0.00	0.02	0.00
59.12	2.00	0.00	0.00	0.02	0.00	59.19	2.00	0.00	0.00	0.02	0.00
59.27	2.00	0.00	0.00	0.02	0.00	59.32	2.00	0.00	0.00	0.02	0.00
59.42	2.00	0.00	0.00	0.03	0.00	59.47	2.00	0.00	0.00	0.02	0.00
59.52	2.00	0.00	0.00	0.02	0.00	59.58	2.00	0.00	0.00	0.02	0.00
59.68	2.00	0.00	0.00	0.03	0.00	59.74	2.00	0.00	0.00	0.02	0.00
59.78	2.00	0.00	0.00	0.01	0.00	59.88	2.00	0.00	0.00	0.03	0.00
59.93	2.00	0.00	0.00	0.02	0.00	60.00	2.00	0.00	0.00	0.02	0.00
60.05	2.00	0.00	0.00	0.02	0.00	60.13	2.00	0.00	0.00	0.02	0.00
60.18	2.00	0.00	0.00	0.02	0.00	60.25	2.00	0.00	0.00	0.02	0.00
60.33	2.00	0.00	0.00	0.02	0.00	60.38	2.00	0.00	0.00	0.02	0.00

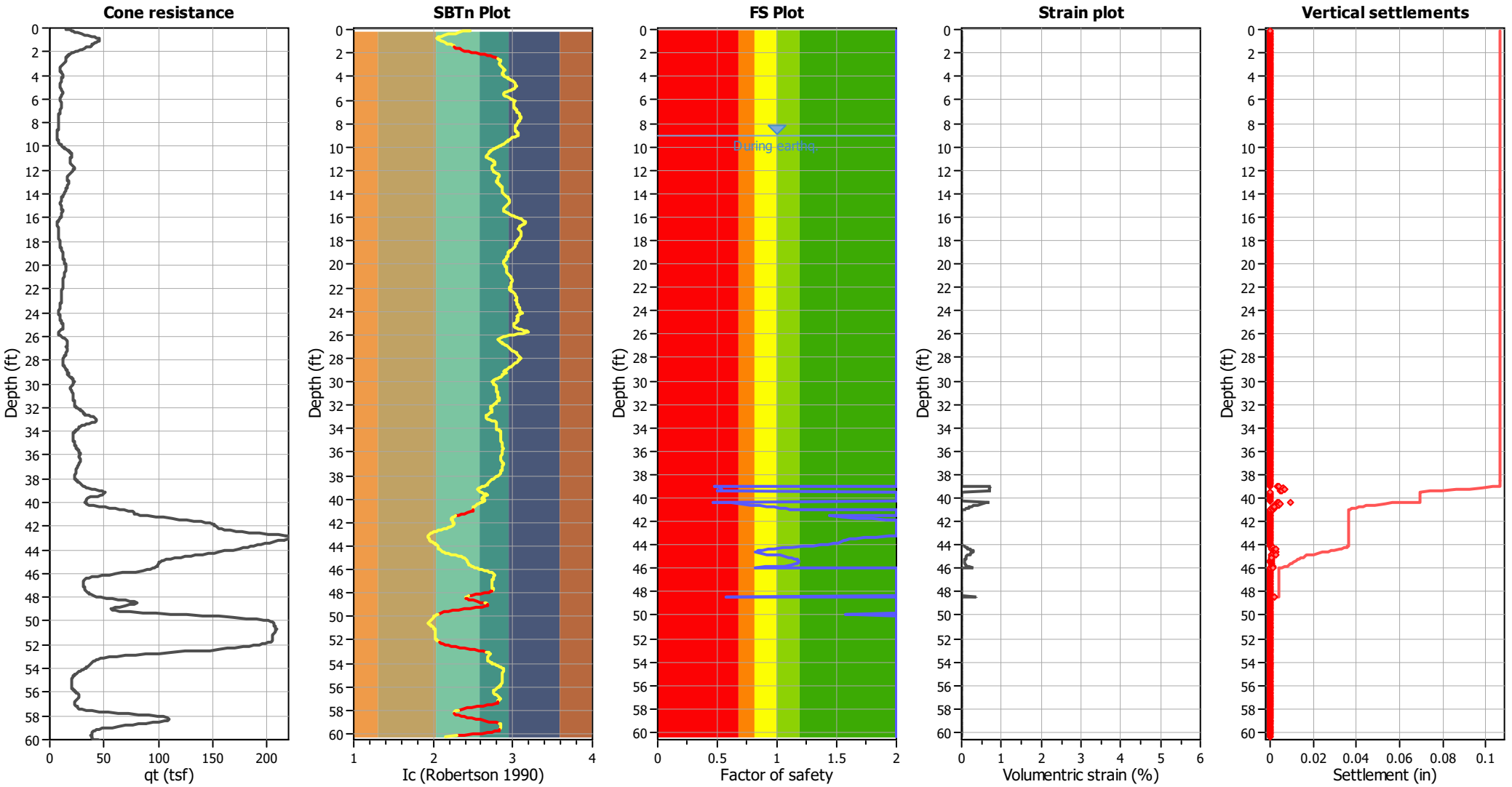
Overall liquefaction potential: 0.54

LPI = 0.00 - Liquefaction risk very low
LPI between 0.00 and 5.00 - Liquefaction risk low
LPI between 5.00 and 15.00 - Liquefaction risk high
LPI > 15.00 - Liquefaction risk very high

Abbreviations

FS: Calculated factor of safety for test point
F_L: 1 - FS
w_z: Function value of the extend of soil liquefaction according to depth
d_z: Layer thickness (ft)
LPI: Liquefaction potential index value for test point

Estimation of post-earthquake settlements



Abbreviations

q_t:	Total cone resistance (cone resistance q_c corrected for pore water effects)
I_c:	Soil Behaviour Type Index
FS:	Calculated Factor of Safety against liquefaction
Volumentric strain:	Post-liquefaction volumentric strain

:: Lateral displacement index calculation ::

Depth (ft)	q_t (tsf)	Q_{tn}	R_f (%)	$Q_{tn,cs}$	FS	D_r	$Gamma_{max}$ (%)	Lat. disp. (in)
9.07	6.38	9.45	3.08	68.47	2.00	0.00	0.00	0.00
9.16	6.56	9.73	2.96	68.19	2.00	0.00	0.00	0.00
9.21	6.75	10.03	2.83	67.73	2.00	0.00	0.00	0.00
9.27	6.95	10.34	2.70	67.24	2.00	0.00	0.00	0.00
9.36	7.12	10.61	2.61	66.90	2.00	0.00	0.00	0.00
9.40	7.28	10.86	2.52	66.54	2.00	0.00	0.00	0.00
9.48	7.42	11.08	2.47	66.51	2.00	0.00	0.00	0.00
9.52	7.61	11.38	2.48	67.29	2.00	0.00	0.00	0.00
9.61	7.88	11.80	2.50	68.36	2.00	0.00	0.00	0.00
9.65	8.20	12.31	2.55	70.02	2.00	0.00	0.00	0.00
9.72	8.71	13.12	2.65	72.94	2.00	0.00	0.00	0.00
9.81	9.31	14.09	2.77	76.25	2.00	2.32	0.00	0.00
9.86	10.14	15.41	2.94	80.94	2.00	5.28	0.00	0.00
9.91	11.02	16.83	3.08	85.53	2.00	8.19	0.00	0.00
10.00	11.92	18.26	3.23	90.08	2.00	10.88	0.00	0.00
10.05	12.98	19.95	3.36	94.97	2.00	13.80	0.00	0.00
10.16	14.05	21.67	3.46	99.56	2.00	16.53	0.00	0.00
10.20	15.10	23.35	3.55	103.70	2.00	18.99	0.00	0.00
10.25	16.16	25.05	3.62	107.64	2.00	21.31	0.00	0.00
10.31	17.03	26.44	3.69	111.04	2.00	23.09	0.00	0.00
10.40	17.83	27.73	3.75	114.17	2.00	24.66	0.00	0.00
10.44	18.60	28.95	3.76	116.36	2.00	26.09	0.00	0.00
10.51	19.07	29.70	3.76	117.57	2.00	26.93	0.00	0.00
10.59	19.49	30.36	3.72	117.93	2.00	27.66	0.00	0.00
10.65	19.75	30.58	3.66	117.21	2.00	27.90	0.00	0.00
10.71	19.91	30.63	3.58	115.91	2.00	27.94	0.00	0.00
10.80	20.00	30.53	3.57	115.58	2.00	27.84	0.00	0.00
10.85	20.00	30.40	3.58	115.50	2.00	27.70	0.00	0.00
10.90	19.65	29.79	3.65	115.78	2.00	27.03	0.00	0.00
10.96	19.02	28.80	3.80	116.70	2.00	25.91	0.00	0.00
11.04	18.63	28.09	3.92	117.49	2.00	25.09	0.00	0.00
11.10	18.54	27.88	4.05	119.21	2.00	24.84	0.00	0.00
11.18	18.55	27.77	4.21	121.48	2.00	24.71	0.00	0.00
11.24	18.66	27.84	4.35	123.77	2.00	24.79	0.00	0.00
11.30	18.82	27.98	4.50	126.31	2.00	24.96	0.00	0.00
11.35	19.00	28.17	4.63	128.55	2.00	25.18	0.00	0.00
11.42	19.22	28.35	4.75	130.69	2.00	25.40	0.00	0.00
11.51	19.84	29.02	4.75	132.02	2.00	26.17	0.00	0.00
11.55	20.77	30.20	4.64	132.54	2.00	27.48	0.00	0.00
11.62	21.32	30.79	4.60	132.86	2.00	28.12	0.00	0.00
11.71	21.83	31.26	4.55	132.97	2.00	28.62	0.00	0.00
11.75	22.14	31.58	4.53	133.24	2.00	28.96	0.00	0.00
11.85	22.14	31.34	4.57	133.38	2.00	28.70	0.00	0.00
11.90	22.04	31.09	4.60	133.42	2.00	28.44	0.00	0.00
11.94	21.77	30.62	4.60	132.59	2.00	27.94	0.00	0.00
12.02	21.29	29.80	4.60	131.08	2.00	27.04	0.00	0.00
12.10	20.69	28.88	4.59	129.32	2.00	26.00	0.00	0.00
12.15	19.88	27.73	4.62	127.53	2.00	24.66	0.00	0.00

:: Estimation of post-earthquake lateral Displacements :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	R_f (%)	$Q_{tn,cs}$	FS	D_r	$Gamma_{max}$ (%)	Lat. disp. (in)
12.24	18.97	26.39	4.65	125.46	2.00	23.03	0.00	0.00
12.30	18.13	25.19	4.64	122.90	2.00	21.49	0.00	0.00
12.35	17.31	24.01	4.60	119.91	2.00	19.91	0.00	0.00
12.44	16.81	23.21	4.47	116.58	2.00	18.79	0.00	0.00
12.50	16.42	22.60	4.33	113.49	2.00	17.91	0.00	0.00
12.55	16.24	22.28	4.20	111.12	2.00	17.44	0.00	0.00
12.63	16.22	22.16	4.08	109.20	2.00	17.26	0.00	0.00
12.70	16.29	22.18	4.01	108.36	2.00	17.29	0.00	0.00
12.74	16.47	22.38	3.98	108.34	2.00	17.59	0.00	0.00
12.84	16.72	22.63	3.97	108.74	2.00	17.95	0.00	0.00
12.86	16.90	22.86	4.01	109.69	2.00	18.29	0.00	0.00
12.94	17.15	23.14	4.05	110.77	2.00	18.69	0.00	0.00
13.01	17.16	23.11	4.14	111.95	2.00	18.65	0.00	0.00
13.09	17.06	22.94	4.24	113.02	2.00	18.40	0.00	0.00
13.14	16.85	22.63	4.32	113.48	2.00	17.96	0.00	0.00
13.20	16.59	22.25	4.38	113.51	2.00	17.40	0.00	0.00
13.29	16.32	21.82	4.40	112.86	2.00	16.76	0.00	0.00
13.33	16.03	21.41	4.40	112.02	2.00	16.12	0.00	0.00
13.39	15.74	20.96	4.39	110.88	2.00	15.43	0.00	0.00
13.49	15.44	20.49	4.37	109.66	2.00	14.67	0.00	0.00
13.53	15.17	20.10	4.35	108.60	2.00	14.04	0.00	0.00
13.59	14.97	19.77	4.23	106.39	2.00	13.49	0.00	0.00
13.69	14.77	19.40	4.07	103.62	2.00	12.88	0.00	0.00
13.73	14.50	19.00	3.98	101.62	2.00	12.19	0.00	0.00
13.79	14.20	18.55	3.91	99.88	2.00	11.39	0.00	0.00
13.89	13.86	18.03	3.86	98.09	2.00	10.45	0.00	0.00
13.94	13.52	17.54	3.78	96.12	2.00	9.55	0.00	0.00
13.99	12.93	16.74	3.75	94.08	2.00	8.00	0.00	0.00
14.08	12.45	16.04	3.68	91.65	2.00	6.59	0.00	0.00
14.13	12.06	15.48	3.57	89.13	2.00	5.43	0.00	0.00
14.18	11.66	14.93	3.54	87.67	2.00	4.24	0.00	0.00
14.27	11.28	14.38	3.57	86.68	2.00	3.00	0.00	0.00
14.32	10.95	13.93	3.53	85.22	2.00	1.93	0.00	0.00
14.37	10.65	13.50	3.46	83.50	2.00	0.92	0.00	0.00
14.48	10.39	13.11	3.39	81.76	2.00	0.00	0.00	0.00
14.52	10.14	12.75	3.33	80.28	2.00	0.00	0.00	0.00
14.58	10.13	12.71	3.21	78.93	2.00	0.00	0.00	0.00
14.68	10.02	12.51	3.16	77.91	2.00	0.00	0.00	0.00
14.72	9.92	12.36	3.11	77.05	2.00	0.00	0.00	0.00
14.77	9.92	12.33	3.07	76.51	2.00	0.00	0.00	0.00
14.83	10.03	12.44	3.01	76.16	2.00	0.00	0.00	0.00
14.92	10.18	12.58	2.95	75.75	2.00	0.00	0.00	0.00
14.98	10.38	12.80	2.89	75.61	2.00	0.00	0.00	0.00
15.07	10.58	13.01	2.84	75.43	2.00	0.00	0.00	0.00
15.11	10.79	13.25	2.79	75.41	2.00	0.29	0.00	0.00
15.17	11.01	13.50	2.78	75.74	2.00	0.90	0.00	0.00
15.27	11.22	13.72	2.76	76.03	2.00	1.43	0.00	0.00
15.31	11.35	13.86	2.78	76.54	2.00	1.78	0.00	0.00

:: Estimation of post-earthquake lateral Displacements :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	R_f (%)	$Q_{tn,cs}$	FS	D_r	$Gamma_{max}$ (%)	Lat. disp. (in)
15.38	11.41	13.93	2.84	77.42	2.00	1.94	0.00	0.00
15.47	11.44	13.94	2.91	78.29	2.00	1.95	0.00	0.00
15.52	11.40	13.88	3.02	79.45	2.00	1.82	0.00	0.00
15.56	11.30	13.74	3.15	80.64	2.00	1.49	0.00	0.00
15.64	11.17	13.56	3.28	81.77	2.00	1.05	0.00	0.00
15.71	11.01	13.34	3.41	82.68	2.00	0.52	0.00	0.00
15.75	10.82	13.08	3.53	83.34	2.00	0.00	0.00	0.00
15.87	10.55	12.67	3.64	83.46	2.00	0.00	0.00	0.00
15.91	10.21	12.21	3.76	83.43	2.00	0.00	0.00	0.00
15.96	9.82	11.68	3.85	82.74	2.00	0.00	0.00	0.00
16.01	9.34	11.02	3.93	81.57	2.00	0.00	0.00	0.00
16.11	8.88	10.39	3.97	79.98	2.00	0.00	0.00	0.00
16.15	8.47	9.84	3.96	78.20	2.00	0.00	0.00	0.00
16.22	8.05	9.27	3.92	75.99	2.00	0.00	0.00	0.00
16.31	7.65	8.73	3.88	73.81	2.00	0.00	0.00	0.00
16.36	7.32	8.28	3.80	71.63	2.00	0.00	0.00	0.00
16.41	7.12	8.01	3.68	69.84	2.00	0.00	0.00	0.00
16.51	7.03	7.86	3.53	68.16	2.00	0.00	0.00	0.00
16.54	7.08	7.92	3.36	67.09	2.00	0.00	0.00	0.00
16.61	7.22	8.08	3.16	66.02	2.00	0.00	0.00	0.00
16.70	7.38	8.26	2.97	65.01	2.00	0.00	0.00	0.00
16.75	7.55	8.46	2.93	65.30	2.00	0.00	0.00	0.00
16.81	7.72	8.66	2.97	66.21	2.00	0.00	0.00	0.00
16.91	7.89	8.85	3.02	67.19	2.00	0.00	0.00	0.00
16.95	8.03	9.01	3.07	68.19	2.00	0.00	0.00	0.00
17.01	8.12	9.11	3.15	69.14	2.00	0.00	0.00	0.00
17.11	8.17	9.14	3.23	69.91	2.00	0.00	0.00	0.00
17.13	8.17	9.13	3.29	70.48	2.00	0.00	0.00	0.00
17.21	8.14	9.07	3.41	71.32	2.00	0.00	0.00	0.00
17.29	8.11	9.00	3.55	72.26	2.00	0.00	0.00	0.00
17.34	8.11	8.99	3.56	72.32	2.00	0.00	0.00	0.00
17.43	8.11	8.96	3.55	72.13	2.00	0.00	0.00	0.00
17.48	8.11	8.95	3.52	71.86	2.00	0.00	0.00	0.00
17.54	8.15	8.98	3.48	71.60	2.00	0.00	0.00	0.00
17.63	8.21	9.02	3.43	71.32	2.00	0.00	0.00	0.00
17.68	8.30	9.12	3.38	71.20	2.00	0.00	0.00	0.00
17.73	8.37	9.20	3.34	71.18	2.00	0.00	0.00	0.00
17.83	8.49	9.32	3.31	71.25	2.00	0.00	0.00	0.00
17.85	8.62	9.47	3.29	71.50	2.00	0.00	0.00	0.00
17.93	8.75	9.61	3.28	71.80	2.00	0.00	0.00	0.00
17.98	8.91	9.79	3.25	72.13	2.00	0.00	0.00	0.00
18.07	9.08	9.96	3.24	72.54	2.00	0.00	0.00	0.00
18.12	9.20	10.09	3.25	72.96	2.00	0.00	0.00	0.00
18.18	9.30	10.19	3.27	73.48	2.00	0.00	0.00	0.00
18.24	9.40	10.30	3.30	73.99	2.00	0.00	0.00	0.00
18.33	9.51	10.40	3.32	74.48	2.00	0.00	0.00	0.00
18.38	9.64	10.54	3.33	74.99	2.00	0.00	0.00	0.00
18.47	9.84	10.75	3.32	75.47	2.00	0.00	0.00	0.00

:: Estimation of post-earthquake lateral Displacements :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	R_f (%)	$Q_{tn,cs}$	FS	D_r	$Gamma_{max}$ (%)	Lat. disp. (in)
18.53	10.04	10.97	3.30	75.85	2.00	0.00	0.00	0.00
18.57	10.26	11.24	3.28	76.36	2.00	0.00	0.00	0.00
18.67	10.50	11.49	3.28	77.01	2.00	0.00	0.00	0.00
18.72	10.79	11.82	3.27	77.79	2.00	0.00	0.00	0.00
18.78	11.12	12.19	3.25	78.44	2.00	0.00	0.00	0.00
18.85	11.42	12.53	3.23	79.06	2.00	0.00	0.00	0.00
18.93	11.67	12.79	3.23	79.67	2.00	0.00	0.00	0.00
18.97	11.84	12.97	3.24	80.21	2.00	0.00	0.00	0.00
19.08	11.93	13.03	3.25	80.49	2.00	0.00	0.00	0.00
19.12	11.99	13.09	3.26	80.75	2.00	0.00	0.00	0.00
19.22	12.04	13.10	3.26	80.74	2.00	0.00	0.00	0.00
19.27	12.17	13.22	3.20	80.34	2.00	0.23	0.00	0.00
19.32	12.24	13.28	3.14	79.86	2.00	0.36	0.00	0.00
19.37	12.33	13.36	3.11	79.68	2.00	0.55	0.00	0.00
19.43	12.44	13.47	3.09	79.68	2.00	0.82	0.00	0.00
19.52	12.63	13.64	3.07	79.84	2.00	1.25	0.00	0.00
19.57	12.91	13.94	3.05	80.20	2.00	1.96	0.00	0.00
19.67	13.22	14.24	3.03	80.60	2.00	2.67	0.00	0.00
19.72	13.55	14.59	3.03	81.43	2.00	3.48	0.00	0.00
19.77	13.86	14.93	3.10	82.85	2.00	4.22	0.00	0.00
19.82	14.07	15.16	3.19	84.47	2.00	4.74	0.00	0.00
19.92	14.31	15.39	3.28	86.10	2.00	5.24	0.00	0.00
19.97	14.46	15.55	3.36	87.31	2.00	5.56	0.00	0.00
20.04	14.51	15.57	3.43	88.24	2.00	5.62	0.00	0.00
20.08	14.51	15.56	3.48	88.85	2.00	5.59	0.00	0.00
20.16	14.47	15.48	3.53	89.24	2.00	5.43	0.00	0.00
20.24	14.41	15.38	3.57	89.46	2.00	5.21	0.00	0.00
20.28	14.35	15.28	3.59	89.45	2.00	5.00	0.00	0.00
20.37	14.28	15.16	3.56	88.94	2.00	4.74	0.00	0.00
20.41	14.20	15.05	3.55	88.47	2.00	4.50	0.00	0.00
20.50	14.10	14.90	3.51	87.78	2.00	4.16	0.00	0.00
20.57	14.00	14.75	3.50	87.30	2.00	3.84	0.00	0.00
20.61	13.91	14.63	3.49	86.92	2.00	3.57	0.00	0.00
20.70	13.81	14.48	3.50	86.69	2.00	3.22	0.00	0.00
20.76	13.64	14.27	3.52	86.42	2.00	2.73	0.00	0.00
20.81	13.44	14.03	3.55	86.25	2.00	2.17	0.00	0.00
20.89	13.21	13.74	3.59	85.97	2.00	1.48	0.00	0.00
20.95	12.98	13.45	3.61	85.49	2.00	0.79	0.00	0.00
21.00	12.77	13.18	3.59	84.66	2.00	0.12	0.00	0.00
21.10	12.56	12.90	3.57	83.76	2.00	0.00	0.00	0.00
21.14	12.37	12.67	3.54	82.83	2.00	0.00	0.00	0.00
21.21	12.21	12.47	3.50	81.94	2.00	0.00	0.00	0.00
21.30	12.05	12.25	3.46	80.94	2.00	0.00	0.00	0.00
21.34	11.94	12.11	3.41	80.06	2.00	0.00	0.00	0.00
21.40	11.83	11.97	3.35	79.15	2.00	0.00	0.00	0.00
21.48	11.77	11.87	3.28	78.22	2.00	0.00	0.00	0.00
21.54	11.71	11.78	3.22	77.30	2.00	0.00	0.00	0.00
21.60	11.65	11.69	3.17	76.56	2.00	0.00	0.00	0.00

:: Estimation of post-earthquake lateral Displacements :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	R_f (%)	$Q_{tn,cs}$	FS	D_r	$Gamma_{max}$ (%)	Lat. disp. (in)
21.68	11.61	11.62	3.12	75.91	2.00	0.00	0.00	0.00
21.75	11.56	11.53	3.07	75.16	2.00	0.00	0.00	0.00
21.80	11.54	11.49	2.98	74.21	2.00	0.00	0.00	0.00
21.88	11.53	11.46	2.90	73.23	2.00	0.00	0.00	0.00
21.92	11.51	11.42	2.82	72.27	2.00	0.00	0.00	0.00
21.99	11.48	11.36	2.76	71.48	2.00	0.00	0.00	0.00
22.08	11.39	11.23	2.72	70.79	2.00	0.00	0.00	0.00
22.15	11.30	11.11	2.70	70.32	2.00	0.00	0.00	0.00
22.19	11.15	10.93	2.72	70.10	2.00	0.00	0.00	0.00
22.28	10.97	10.71	2.74	69.83	2.00	0.00	0.00	0.00
22.34	10.82	10.51	2.79	69.90	2.00	0.00	0.00	0.00
22.39	10.66	10.32	2.85	69.97	2.00	0.00	0.00	0.00
22.47	10.52	10.15	2.89	70.01	2.00	0.00	0.00	0.00
22.54	10.38	9.97	2.95	70.16	2.00	0.00	0.00	0.00
22.58	10.32	9.90	2.98	70.23	2.00	0.00	0.00	0.00
22.68	10.27	9.81	3.01	70.25	2.00	0.00	0.00	0.00
22.74	10.22	9.74	3.04	70.41	2.00	0.00	0.00	0.00
22.79	10.24	9.75	3.05	70.48	2.00	0.00	0.00	0.00
22.84	10.28	9.78	3.05	70.55	2.00	0.00	0.00	0.00
22.94	10.32	9.79	3.04	70.48	2.00	0.00	0.00	0.00
22.99	10.34	9.80	3.03	70.45	2.00	0.00	0.00	0.00
23.04	10.29	9.73	3.04	70.40	2.00	0.00	0.00	0.00
23.11	10.24	9.65	3.04	70.14	2.00	0.00	0.00	0.00
23.18	10.14	9.52	3.04	69.77	2.00	0.00	0.00	0.00
23.23	10.06	9.42	3.02	69.31	2.00	0.00	0.00	0.00
23.34	9.96	9.28	2.97	68.49	2.00	0.00	0.00	0.00
23.37	9.83	9.14	2.92	67.61	2.00	0.00	0.00	0.00
23.44	9.70	8.98	2.85	66.58	2.00	0.00	0.00	0.00
23.54	9.51	8.75	2.78	65.30	2.00	0.00	0.00	0.00
23.60	9.31	8.52	2.71	64.01	2.00	0.00	0.00	0.00
23.64	9.08	8.27	2.64	62.70	2.00	0.00	0.00	0.00
23.71	8.86	8.01	2.56	61.22	2.00	0.00	0.00	0.00
23.79	8.59	7.72	2.48	59.70	2.00	0.00	0.00	0.00
23.84	8.38	7.48	2.40	58.28	2.00	0.00	0.00	0.00
23.89	8.28	7.37	2.33	57.37	2.00	0.00	0.00	0.00
23.99	8.23	7.29	2.31	56.92	2.00	0.00	0.00	0.00
24.03	8.16	7.20	2.38	57.36	2.00	0.00	0.00	0.00
24.10	8.16	7.20	2.49	58.28	2.00	0.00	0.00	0.00
24.18	8.37	7.40	2.56	59.50	2.00	0.00	0.00	0.00
24.23	8.74	7.77	2.59	60.88	2.00	0.00	0.00	0.00
24.31	9.13	8.17	2.62	62.20	2.00	0.00	0.00	0.00
24.36	9.53	8.57	2.65	63.60	2.00	0.00	0.00	0.00
24.45	9.75	8.78	2.74	65.00	2.00	0.00	0.00	0.00
24.49	9.88	8.90	2.82	66.16	2.00	0.00	0.00	0.00
24.57	9.92	8.92	2.88	66.74	2.00	0.00	0.00	0.00
24.61	10.03	9.03	2.87	66.94	2.00	0.00	0.00	0.00
24.69	10.16	9.14	2.89	67.43	2.00	0.00	0.00	0.00
24.74	10.29	9.26	2.98	68.63	2.00	0.00	0.00	0.00

:: Estimation of post-earthquake lateral Displacements :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	R_f (%)	$Q_{tn,cs}$	FS	D_r	$Gamma_{max}$ (%)	Lat. disp. (in)
24.82	10.59	9.55	3.14	70.88	2.00	0.00	0.00	0.00
24.89	11.03	9.99	3.29	73.55	2.00	0.00	0.00	0.00
24.94	11.56	10.52	3.38	75.87	2.00	0.00	0.00	0.00
25.01	12.05	11.00	3.38	77.20	2.00	0.00	0.00	0.00
25.09	12.40	11.33	3.35	77.76	2.00	0.00	0.00	0.00
25.13	12.40	11.32	3.33	77.46	2.00	0.00	0.00	0.00
25.22	12.27	11.16	3.30	76.77	2.00	0.00	0.00	0.00
25.28	12.04	10.90	3.22	75.36	2.00	0.00	0.00	0.00
25.34	11.57	10.40	3.12	73.08	2.00	0.00	0.00	0.00
25.44	10.81	9.60	2.97	69.50	2.00	0.00	0.00	0.00
25.48	9.88	8.64	2.83	65.59	2.00	0.00	0.00	0.00
25.53	8.92	7.65	2.68	61.35	2.00	0.00	0.00	0.00
25.59	8.18	6.88	2.60	58.29	2.00	0.00	0.00	0.00
25.68	7.57	6.25	2.61	56.35	2.00	0.00	0.00	0.00
25.73	7.56	6.23	2.73	57.21	2.00	0.00	0.00	0.00
25.79	7.85	6.51	2.69	57.85	2.00	0.00	0.00	0.00
25.88	8.49	7.15	2.58	58.97	2.00	0.00	0.00	0.00
25.93	9.38	8.03	2.45	60.40	2.00	0.00	0.00	0.00
25.99	10.48	9.12	2.38	62.43	2.00	0.00	0.00	0.00
26.08	11.74	10.37	2.30	64.43	2.00	0.00	0.00	0.00
26.14	12.92	11.53	2.30	66.84	2.00	0.00	0.00	0.00
26.19	13.96	12.54	2.30	68.72	2.00	0.00	0.00	0.00
26.28	14.97	13.52	2.26	69.87	2.00	0.95	0.00	0.00
26.34	15.73	14.24	2.19	70.17	2.00	2.68	0.00	0.00
26.39	16.16	14.65	2.21	71.17	2.00	3.60	0.00	0.00
26.45	16.25	14.72	2.28	72.27	2.00	3.75	0.00	0.00
26.53	16.18	14.62	2.37	73.29	2.00	3.54	0.00	0.00
26.58	16.05	14.48	2.46	74.34	2.00	3.21	0.00	0.00
26.68	15.79	14.19	2.58	75.29	2.00	2.55	0.00	0.00
26.73	15.60	13.99	2.67	76.13	2.00	2.07	0.00	0.00
26.78	15.54	13.91	2.78	77.37	2.00	1.90	0.00	0.00
26.88	15.47	13.80	2.96	79.32	2.00	1.63	0.00	0.00
26.93	15.41	13.73	3.14	81.33	2.00	1.46	0.00	0.00
26.98	15.48	13.78	3.30	83.25	2.00	1.58	0.00	0.00
27.04	15.59	13.87	3.46	85.19	2.00	1.79	0.00	0.00
27.13	15.68	13.92	3.61	86.96	2.00	1.92	0.00	0.00
27.22	15.61	13.82	3.75	88.26	2.00	1.67	0.00	0.00
27.24	15.48	13.68	3.87	89.16	2.00	1.34	0.00	0.00
27.33	15.33	13.50	3.97	89.67	2.00	0.90	0.00	0.00
27.37	15.08	13.24	4.05	89.80	2.00	0.26	0.00	0.00
27.43	14.77	12.92	4.09	89.38	2.00	0.00	0.00	0.00
27.52	14.46	12.58	4.13	88.85	2.00	0.00	0.00	0.00
27.57	14.10	12.22	4.16	88.05	2.00	0.00	0.00	0.00
27.63	13.68	11.79	4.15	86.71	2.00	0.00	0.00	0.00
27.72	13.24	11.33	4.12	85.09	2.00	0.00	0.00	0.00
27.76	12.84	10.93	4.05	83.26	2.00	0.00	0.00	0.00
27.84	12.46	10.54	3.97	81.35	2.00	0.00	0.00	0.00
27.93	12.10	10.17	3.89	79.56	2.00	0.00	0.00	0.00

:: Estimation of post-earthquake lateral Displacements :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	R_f (%)	$Q_{tn,cs}$	FS	D_r	$Gamma_{max}$ (%)	Lat. disp. (in)
27.97	11.82	9.89	3.80	77.87	2.00	0.00	0.00	0.00
28.02	11.70	9.75	3.66	76.27	2.00	0.00	0.00	0.00
28.12	11.66	9.69	3.49	74.61	2.00	0.00	0.00	0.00
28.17	11.67	9.68	3.35	73.40	2.00	0.00	0.00	0.00
28.23	11.80	9.79	3.27	72.95	2.00	0.00	0.00	0.00
28.32	12.03	9.99	3.22	73.01	2.00	0.00	0.00	0.00
28.37	12.28	10.22	3.19	73.44	2.00	0.00	0.00	0.00
28.42	12.60	10.51	3.20	74.28	2.00	0.00	0.00	0.00
28.48	12.97	10.84	3.22	75.36	2.00	0.00	0.00	0.00
28.57	13.52	11.33	3.21	76.48	2.00	0.00	0.00	0.00
28.61	14.02	11.79	3.21	77.67	2.00	0.00	0.00	0.00
28.69	14.48	12.21	3.22	78.81	2.00	0.00	0.00	0.00
28.77	14.97	12.64	3.21	79.74	2.00	0.00	0.00	0.00
28.83	15.40	13.03	3.18	80.28	2.00	0.00	0.00	0.00
28.88	15.75	13.34	3.15	80.59	2.00	0.50	0.00	0.00
28.97	16.12	13.65	3.11	80.85	2.00	1.27	0.00	0.00
29.02	16.58	14.07	3.06	81.19	2.00	2.27	0.00	0.00
29.08	17.07	14.50	3.01	81.51	2.00	3.27	0.00	0.00
29.17	17.42	14.80	3.00	81.91	2.00	3.93	0.00	0.00
29.21	16.68	14.09	3.21	82.99	2.00	2.32	0.00	0.00
29.28	17.35	14.69	3.20	84.17	2.00	3.68	0.00	0.00
29.37	18.08	15.34	3.21	85.65	2.00	5.12	0.00	0.00
29.41	18.84	16.03	3.24	87.42	2.00	6.57	0.00	0.00
29.47	19.66	16.76	3.25	88.96	2.00	8.05	0.00	0.00
29.56	20.44	17.45	3.20	89.65	2.00	9.38	0.00	0.00
29.62	21.08	18.02	3.14	89.89	2.00	10.43	0.00	0.00
29.68	21.55	18.43	3.06	89.53	2.00	11.17	0.00	0.00
29.76	21.98	18.79	2.96	88.74	2.00	11.81	0.00	0.00
29.83	23.16	19.85	2.72	86.86	2.00	13.63	0.00	0.00
29.87	22.72	19.43	2.63	84.78	2.00	12.92	0.00	0.00
29.96	22.10	18.81	2.52	82.22	2.00	11.85	0.00	0.00
30.01	21.54	18.28	2.38	79.33	2.00	10.91	0.00	0.00
30.07	20.81	17.58	2.27	76.65	2.00	9.62	0.00	0.00
30.16	20.20	16.98	2.22	74.98	2.00	8.48	0.00	0.00
30.20	19.65	16.47	2.19	73.79	2.00	7.46	0.00	0.00
30.27	19.26	16.07	2.20	73.29	2.00	6.66	0.00	0.00
30.34	18.94	15.75	2.24	73.36	2.00	6.00	0.00	0.00
30.42	18.95	15.73	2.28	73.99	2.00	5.95	0.00	0.00
30.46	19.17	15.91	2.34	75.17	2.00	6.34	0.00	0.00
30.52	19.53	16.22	2.41	76.59	2.00	6.96	0.00	0.00
30.58	19.82	16.46	2.49	78.24	2.00	7.45	0.00	0.00
30.66	20.28	16.84	2.56	79.86	2.00	8.20	0.00	0.00
30.71	20.64	17.15	2.63	81.34	2.00	8.80	0.00	0.00
30.81	20.94	17.37	2.70	82.69	2.00	9.23	0.00	0.00
30.87	21.17	17.56	2.77	83.92	2.00	9.59	0.00	0.00
30.91	21.30	17.66	2.84	85.10	2.00	9.77	0.00	0.00
31.01	21.41	17.71	2.91	86.23	2.00	9.87	0.00	0.00
31.06	21.53	17.80	2.98	87.37	2.00	10.03	0.00	0.00

:: Estimation of post-earthquake lateral Displacements :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	R_f (%)	$Q_{tn,cs}$	FS	D_r	$Gamma_{max}$ (%)	Lat. disp. (in)
31.11	21.63	17.86	3.05	88.36	2.00	10.15	0.00	0.00
31.19	21.81	17.99	3.09	89.14	2.00	10.38	0.00	0.00
31.26	21.98	18.11	3.11	89.73	2.00	10.59	0.00	0.00
31.35	22.12	18.19	3.13	90.16	2.00	10.74	0.00	0.00
31.37	22.15	18.20	3.17	90.62	2.00	10.77	0.00	0.00
31.46	22.28	18.27	3.18	90.91	2.00	10.90	0.00	0.00
31.55	22.33	18.28	3.19	91.09	2.00	10.91	0.00	0.00
31.59	22.49	18.41	3.17	91.01	2.00	11.15	0.00	0.00
31.66	22.71	18.58	3.11	90.48	2.00	11.44	0.00	0.00
31.70	23.00	18.82	3.03	89.81	2.00	11.87	0.00	0.00
31.79	23.13	18.90	2.97	89.15	2.00	12.00	0.00	0.00
31.86	23.24	18.96	2.92	88.51	2.00	12.12	0.00	0.00
31.91	23.55	19.22	2.88	88.37	2.00	12.56	0.00	0.00
31.99	24.39	19.93	2.85	89.06	2.00	13.75	0.00	0.00
32.06	25.44	20.82	2.85	90.39	2.00	15.21	0.00	0.00
32.10	26.88	22.09	2.84	92.23	2.00	17.15	0.00	0.00
32.20	28.15	23.16	2.91	94.85	2.00	18.72	0.00	0.00
32.26	28.72	23.62	3.07	98.16	2.00	19.37	0.00	0.00
32.30	29.57	24.34	3.22	101.69	2.00	20.36	0.00	0.00
32.35	30.28	24.92	3.38	105.09	2.00	21.14	0.00	0.00
32.46	31.21	25.67	3.50	108.18	2.00	22.12	0.00	0.00
32.49	31.95	26.29	3.63	111.21	2.00	22.90	0.00	0.00
32.58	32.77	26.95	3.71	113.53	2.00	23.73	0.00	0.00
32.62	34.34	28.30	3.73	116.05	2.00	25.34	0.00	0.00
32.69	36.23	29.91	3.77	119.21	2.00	27.16	0.00	0.00
32.78	38.18	31.55	3.80	122.28	2.00	28.93	0.00	0.00
32.82	40.40	33.46	3.82	125.60	2.00	30.87	0.00	0.00
32.89	41.76	34.59	3.92	129.05	2.00	31.96	0.00	0.00
32.98	43.04	35.63	4.01	132.21	2.00	32.94	0.00	0.00
33.02	43.56	36.03	4.14	135.06	2.00	33.30	0.00	0.00
33.08	43.60	36.00	4.22	136.47	2.00	33.28	0.00	0.00
33.18	42.94	35.32	4.32	137.25	2.00	32.65	0.00	0.00
33.21	41.11	33.69	4.46	137.02	2.00	31.09	0.00	0.00
33.29	38.50	31.35	4.58	135.03	2.00	28.71	0.00	0.00
33.37	35.87	29.01	4.61	131.27	2.00	26.15	0.00	0.00
33.42	33.58	27.00	4.53	126.23	2.00	23.79	0.00	0.00
33.47	31.71	25.36	4.33	120.24	2.00	21.72	0.00	0.00
33.53	29.91	23.80	4.08	113.67	2.00	19.61	0.00	0.00
33.62	28.55	22.60	3.78	107.22	2.00	17.91	0.00	0.00
33.67	27.44	21.64	3.52	101.83	2.00	16.47	0.00	0.00
33.73	26.35	20.68	3.29	96.75	2.00	14.99	0.00	0.00
33.82	25.32	19.78	3.08	92.18	2.00	13.51	0.00	0.00
33.87	24.46	19.03	2.91	88.49	2.00	12.23	0.00	0.00
33.93	23.71	18.37	2.84	86.36	2.00	11.07	0.00	0.00
34.02	23.04	17.75	2.81	84.94	2.00	9.95	0.00	0.00
34.06	22.45	17.24	2.82	84.26	2.00	8.97	0.00	0.00
34.13	22.07	16.88	2.87	84.31	2.00	8.28	0.00	0.00
34.22	21.81	16.62	2.92	84.59	2.00	7.77	0.00	0.00

:: Estimation of post-earthquake lateral Displacements :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	R_f (%)	$Q_{tn,cs}$	FS	D_r	$Gamma_{max}$ (%)	Lat. disp. (in)
34.26	21.71	16.52	2.98	85.19	2.00	7.56	0.00	0.00
34.32	21.73	16.50	3.04	85.88	2.00	7.54	0.00	0.00
34.42	21.79	16.51	3.08	86.45	2.00	7.55	0.00	0.00
34.46	21.86	16.55	3.11	86.87	2.00	7.63	0.00	0.00
34.52	21.87	16.54	3.12	87.08	2.00	7.60	0.00	0.00
34.61	21.89	16.52	3.13	87.14	2.00	7.56	0.00	0.00
34.70	21.91	16.50	3.13	87.14	2.00	7.52	0.00	0.00
34.76	22.00	16.55	3.14	87.27	2.00	7.62	0.00	0.00
34.82	22.08	16.59	3.14	87.34	2.00	7.71	0.00	0.00
34.86	22.20	16.68	3.11	87.15	2.00	7.88	0.00	0.00
34.92	22.38	16.80	3.12	87.52	2.00	8.13	0.00	0.00
35.02	22.61	16.95	3.16	88.35	2.00	8.42	0.00	0.00
35.06	22.92	17.19	3.22	89.58	2.00	8.87	0.00	0.00
35.11	23.26	17.45	3.30	91.14	2.00	9.38	0.00	0.00
35.19	23.32	17.45	3.44	92.89	2.00	9.38	0.00	0.00
35.25	23.48	17.55	3.56	94.66	2.00	9.57	0.00	0.00
35.31	23.92	17.88	3.64	96.33	2.00	10.19	0.00	0.00
35.40	24.41	18.24	3.74	98.39	2.00	10.84	0.00	0.00
35.45	24.90	18.61	3.88	100.88	2.00	11.50	0.00	0.00
35.50	25.37	18.97	4.01	103.26	2.00	12.14	0.00	0.00
35.56	25.84	19.32	4.11	105.30	2.00	12.74	0.00	0.00
35.64	26.20	19.57	4.22	107.20	2.00	13.16	0.00	0.00
35.72	26.53	19.80	4.31	108.86	2.00	13.54	0.00	0.00
35.81	27.10	20.22	4.33	110.03	2.00	14.23	0.00	0.00
35.85	27.52	20.55	4.34	110.86	2.00	14.77	0.00	0.00
35.90	27.57	20.56	4.38	111.30	2.00	14.79	0.00	0.00
35.96	27.50	20.47	4.39	111.25	2.00	14.64	0.00	0.00
36.04	27.44	20.38	4.37	110.83	2.00	14.50	0.00	0.00
36.11	27.37	20.29	4.32	110.01	2.00	14.36	0.00	0.00
36.16	27.38	20.28	4.24	108.99	2.00	14.34	0.00	0.00
36.25	27.49	20.34	4.13	107.76	2.00	14.43	0.00	0.00
36.31	27.53	20.35	4.04	106.50	2.00	14.45	0.00	0.00
36.36	27.55	20.34	3.98	105.82	2.00	14.44	0.00	0.00
36.44	27.59	20.34	3.96	105.48	2.00	14.43	0.00	0.00
36.50	27.55	20.28	3.96	105.38	2.00	14.33	0.00	0.00
36.56	27.51	20.22	3.96	105.22	2.00	14.23	0.00	0.00
36.65	27.46	20.13	3.95	104.99	2.00	14.09	0.00	0.00
36.68	27.32	20.00	3.95	104.73	2.00	13.89	0.00	0.00
36.76	26.99	19.70	3.97	104.31	2.00	13.38	0.00	0.00
36.84	26.59	19.33	3.98	103.68	2.00	12.75	0.00	0.00
36.91	26.14	18.94	3.97	102.81	2.00	12.07	0.00	0.00
36.96	25.72	18.58	3.93	101.52	2.00	11.45	0.00	0.00
37.04	25.31	18.22	3.86	99.92	2.00	10.80	0.00	0.00
37.10	25.01	17.96	3.78	98.29	2.00	10.33	0.00	0.00
37.15	24.79	17.78	3.68	96.70	2.00	9.99	0.00	0.00
37.23	24.57	17.57	3.59	95.11	2.00	9.60	0.00	0.00
37.30	24.39	17.41	3.49	93.56	2.00	9.29	0.00	0.00
37.35	24.27	17.30	3.40	92.22	2.00	9.09	0.00	0.00

:: Estimation of post-earthquake lateral Displacements :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	R_f (%)	$Q_{tn,cs}$	FS	D_r	$Gamma_{max}$ (%)	Lat. disp. (in)
37.45	24.09	17.12	3.33	90.90	2.00	8.75	0.00	0.00
37.51	23.91	16.96	3.26	89.72	2.00	8.44	0.00	0.00
37.55	23.68	16.77	3.19	88.48	2.00	8.07	0.00	0.00
37.62	23.41	16.54	3.12	87.10	2.00	7.61	0.00	0.00
37.70	23.18	16.33	3.04	85.68	2.00	7.19	0.00	0.00
37.75	22.99	16.17	2.95	84.25	2.00	6.86	0.00	0.00
37.80	22.83	16.04	2.86	82.80	2.00	6.59	0.00	0.00
37.90	22.79	15.98	2.76	81.34	2.00	6.47	0.00	0.00
37.95	22.85	16.02	2.66	79.99	2.00	6.56	0.00	0.00
38.05	23.13	16.22	2.58	79.28	2.00	6.96	0.00	0.00
38.06	23.67	16.66	2.51	79.02	2.00	7.85	0.00	0.00
38.15	24.36	17.18	2.46	79.14	2.00	8.87	0.00	0.00
38.19	25.07	17.73	2.45	79.75	2.00	9.91	0.00	0.00
38.27	25.90	18.37	2.43	80.47	2.00	11.07	0.00	0.00
38.34	26.81	19.07	2.42	81.37	2.00	12.30	0.00	0.00
38.39	27.68	19.75	2.42	82.26	2.00	13.46	0.00	0.00
38.46	28.48	20.35	2.44	83.39	2.00	14.45	0.00	0.00
38.55	29.24	20.90	2.48	84.87	2.00	15.33	0.00	0.00
38.59	30.19	21.63	2.54	86.82	2.00	16.47	0.00	0.00
38.68	31.64	22.72	2.61	89.49	2.00	18.09	0.00	0.00
38.75	33.31	24.00	2.69	92.51	2.00	19.90	0.00	0.00
38.80	35.48	25.68	2.77	96.14	2.00	22.13	0.00	0.00
38.87	38.37	27.93	2.81	99.97	2.00	24.91	0.00	0.00
38.95	41.80	30.61	2.86	104.15	2.00	27.92	0.00	0.00
38.99	45.31	33.36	2.89	108.24	0.48	30.77	51.20	0.00
39.04	48.34	35.74	2.92	111.69	0.50	33.04	51.20	0.00
39.11	49.97	36.96	2.98	114.37	0.53	34.15	51.20	0.00
39.19	50.69	37.46	3.01	115.54	0.54	34.59	51.20	0.00
39.27	49.95	36.81	3.02	114.99	0.53	34.01	51.20	0.00
39.33	48.64	35.72	3.02	113.58	0.52	33.02	51.20	0.00
39.39	46.71	34.16	2.98	110.84	0.50	31.55	51.20	0.00
39.45	43.93	31.94	2.93	107.28	2.00	29.32	0.00	0.00
39.53	40.53	29.21	2.89	103.00	2.00	26.38	0.00	0.00
39.57	37.19	26.57	2.83	98.52	2.00	23.26	0.00	0.00
39.64	34.51	24.46	2.72	93.75	2.00	20.53	0.00	0.00
39.72	33.37	23.58	2.50	88.79	2.00	19.32	0.00	0.00
39.79	32.93	23.26	2.27	84.39	2.00	18.87	0.00	0.00
39.84	33.06	23.39	2.09	81.26	2.00	19.05	0.00	0.00
39.93	32.94	23.28	2.00	79.39	2.00	18.90	0.00	0.00
39.98	32.75	23.12	1.99	79.04	2.00	18.66	0.00	0.00
40.05	32.95	23.19	2.17	82.51	2.00	18.76	0.00	0.00
40.09	34.03	23.95	2.38	87.20	2.00	19.83	0.00	0.00
40.19	36.38	25.69	2.56	92.47	2.00	22.14	0.00	0.00
40.23	40.72	29.01	2.70	99.16	2.00	26.16	0.00	0.00
40.34	45.86	32.90	2.85	106.95	0.47	30.31	51.20	0.00
40.38	50.76	36.64	3.04	115.13	0.53	33.86	51.20	0.00
40.43	55.28	40.05	3.25	123.53	0.61	36.80	51.20	0.00
40.50	60.00	43.62	3.40	131.16	0.70	39.62	51.20	0.00

:: Estimation of post-earthquake lateral Displacements :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	R_f (%)	$Q_{tn,cs}$	FS	D_r	$Gamma_{max}$ (%)	Lat. disp. (in)
40.58	64.51	47.00	3.54	138.27	0.78	42.08	51.20	0.00
40.63	68.60	50.12	3.60	143.45	0.85	44.20	40.07	0.00
40.70	72.71	53.23	3.63	147.92	0.92	46.19	7.31	0.00
40.75	76.10	55.80	3.68	151.94	0.98	47.75	4.85	0.00
40.84	77.61	56.84	3.76	155.10	1.03	48.35	3.52	0.00
40.88	77.99	57.03	3.86	157.83	1.07	48.46	2.68	0.00
40.95	78.42	57.23	3.95	160.06	1.11	48.58	2.15	0.00
41.03	79.84	58.24	3.95	161.34	2.00	49.16	0.00	0.00
41.08	83.51	61.08	3.85	162.46	2.00	50.73	0.00	0.00
41.15	90.15	66.29	3.62	162.81	2.00	53.43	0.00	0.00
41.23	97.84	72.34	3.40	163.56	2.00	56.31	0.00	0.00
41.28	105.13	78.11	3.23	164.99	2.00	58.85	0.00	0.00
41.35	112.60	84.00	3.09	166.99	2.00	61.25	0.00	0.00
41.43	119.65	89.52	2.99	169.57	2.00	63.35	0.00	0.00
41.48	126.18	94.65	2.94	172.95	2.00	65.18	0.00	0.00
41.54	132.64	99.67	2.91	177.10	1.44	66.89	1.12	0.00
41.62	138.98	104.52	2.92	181.95	1.55	68.46	0.91	0.00
41.68	144.15	108.42	2.96	187.16	1.67	69.67	0.73	0.00
41.77	147.16	110.47	3.06	192.21	1.79	70.29	0.60	0.00
41.82	149.61	112.16	3.15	197.02	1.91	70.79	0.49	0.00
41.88	151.40	113.31	3.24	201.11	2.00	71.12	0.00	0.00
41.97	152.19	113.59	3.34	204.50	2.00	71.21	0.00	0.00
42.01	152.63	113.73	3.43	207.46	2.00	71.25	0.00	0.00
42.10	154.18	114.69	3.46	209.53	2.00	71.53	0.00	0.00
42.17	155.77	115.77	3.46	210.77	2.00	71.83	0.00	0.00
42.22	158.63	117.95	3.42	211.47	2.00	72.45	0.00	0.00
42.28	161.62	120.26	3.34	211.30	2.00	73.09	0.00	0.00
42.33	166.19	123.89	3.22	210.96	2.00	74.07	0.00	0.00
42.41	171.05	127.73	3.09	210.27	2.00	75.08	0.00	0.00
42.48	177.06	132.54	2.94	209.92	2.00	76.30	0.00	0.00
42.52	184.41	138.54	2.77	210.20	2.00	77.76	0.00	0.00
42.60	193.18	145.64	2.60	211.30	2.00	79.41	0.00	0.00
42.66	201.80	152.67	2.46	212.90	2.00	80.97	0.00	0.00
42.72	210.25	159.58	2.32	214.88	2.00	82.43	0.00	0.00
42.81	216.71	164.80	2.22	216.24	2.00	83.49	0.00	0.00
42.87	221.45	168.71	2.13	216.83	2.00	84.26	0.00	0.00
42.92	223.43	170.44	2.04	215.65	2.00	84.60	0.00	0.00
43.00	224.17	171.11	1.96	213.60	2.00	84.73	0.00	0.00
43.06	223.07	170.33	1.89	210.56	2.00	84.58	0.00	0.00
43.11	220.03	167.97	1.84	206.67	2.00	84.12	0.00	0.00
43.18	215.77	164.56	1.80	202.06	2.00	83.44	0.00	0.00
43.25	211.23	160.89	1.76	197.51	1.94	82.70	0.82	0.00
43.31	206.82	157.31	1.73	193.43	1.83	81.95	0.92	0.00
43.39	202.67	153.89	1.71	189.65	1.74	81.23	1.02	0.00
43.45	198.48	150.43	1.71	186.27	1.66	80.48	1.13	0.00
43.51	194.71	147.19	1.73	184.09	1.61	79.76	1.20	0.00
43.61	191.33	144.12	1.78	182.63	1.57	79.06	1.25	0.00
43.65	188.25	141.41	1.83	181.84	1.56	78.44	1.28	0.00

:: Estimation of post-earthquake lateral Displacements :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	R_f (%)	$Q_{tn,cs}$	FS	D_r	$Gamma_{max}$ (%)	Lat. disp. (in)
43.72	185.35	138.80	1.88	180.92	1.54	77.82	1.32	0.00
43.81	182.33	136.09	1.92	179.83	1.51	77.17	1.36	0.00
43.85	178.70	133.02	1.96	178.27	1.48	76.42	1.43	0.00
43.92	174.04	129.13	1.99	175.71	1.42	75.44	1.54	0.00
44.01	169.31	125.14	2.03	173.09	1.37	74.40	1.29	0.00
44.05	165.21	121.88	2.02	169.93	1.31	73.53	1.47	0.00
44.10	160.81	118.50	1.97	165.15	1.22	72.60	1.81	0.00
44.20	156.04	114.74	1.91	160.07	1.13	71.54	2.27	0.00
44.25	151.36	111.13	1.87	155.35	1.05	70.48	2.81	0.00
44.30	146.31	107.16	1.85	151.20	0.98	69.28	3.39	0.00
44.40	140.34	102.33	1.86	147.25	0.92	67.76	4.06	0.00
44.45	134.81	97.92	1.88	143.99	0.87	66.31	4.73	0.00
44.50	130.12	94.11	1.93	142.03	0.85	65.00	7.47	0.00
44.57	125.26	90.13	1.99	140.34	0.82	63.57	8.42	0.00
44.63	120.31	86.02	2.11	140.23	0.82	62.03	8.48	0.00
44.69	115.72	82.08	2.33	143.01	0.86	60.48	6.93	0.00
44.79	111.51	78.40	2.57	146.54	0.91	58.97	5.38	0.00
44.84	107.77	75.21	2.81	150.25	0.97	57.60	4.13	0.00
44.89	105.00	72.83	3.01	153.52	1.02	56.54	3.28	0.00
44.96	103.51	71.48	3.15	156.05	1.06	55.92	2.75	0.00
45.04	102.01	70.14	3.28	158.16	1.10	55.29	2.37	0.00
45.09	100.81	69.09	3.38	159.67	1.12	54.79	2.00	0.00
45.17	100.05	68.35	3.46	160.93	1.15	54.44	1.76	0.00
45.24	99.52	67.81	3.53	162.05	1.17	54.18	1.57	0.00
45.28	99.27	67.55	3.56	162.52	1.18	54.05	1.50	0.00
45.38	98.85	67.10	3.58	162.58	1.18	53.83	1.49	0.00
45.42	97.77	66.22	3.62	162.63	1.18	53.39	1.48	0.00
45.49	96.34	65.05	3.67	162.56	1.18	52.81	1.48	0.00
45.57	94.70	63.72	3.72	162.28	1.17	52.13	1.52	0.00
45.63	92.37	61.92	3.76	161.36	1.16	51.18	1.66	0.00
45.69	89.46	59.74	3.78	159.12	1.12	50.00	2.07	0.00
45.78	85.19	56.57	3.78	155.40	1.06	48.20	2.99	0.00
45.84	79.80	52.64	3.79	150.88	0.98	45.82	4.71	0.00
45.89	73.90	48.37	3.80	145.76	0.91	43.03	27.02	0.00
45.93	67.39	43.71	3.79	139.53	0.82	39.69	48.74	0.00
46.02	61.02	39.17	3.74	132.47	2.00	36.06	0.00	0.00
46.08	54.84	34.81	3.66	124.90	2.00	32.17	0.00	0.00
46.13	48.82	30.61	3.55	116.87	2.00	27.92	0.00	0.00
46.22	43.62	27.00	3.40	108.93	2.00	23.78	0.00	0.00
46.28	39.06	23.85	3.27	101.99	2.00	19.69	0.00	0.00
46.33	35.80	21.61	3.15	96.55	2.00	16.44	0.00	0.00
46.43	33.77	20.22	2.98	91.86	2.00	14.25	0.00	0.00
46.47	32.28	19.23	2.82	87.81	2.00	12.59	0.00	0.00
46.53	31.55	18.75	2.68	85.02	2.00	11.75	0.00	0.00
46.63	31.27	18.56	2.56	82.79	2.00	11.41	0.00	0.00
46.67	31.09	18.45	2.45	81.06	2.00	11.22	0.00	0.00
46.73	31.01	18.39	2.41	80.34	2.00	11.11	0.00	0.00
46.83	31.04	18.38	2.39	80.02	2.00	11.09	0.00	0.00

:: Estimation of post-earthquake lateral Displacements :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	R_f (%)	$Q_{tn,cs}$	FS	D_r	$Gamma_{max}$ (%)	Lat. disp. (in)
46.87	31.05	18.38	2.39	79.94	2.00	11.08	0.00	0.00
46.93	31.18	18.45	2.38	80.00	2.00	11.21	0.00	0.00
47.02	31.31	18.51	2.38	79.99	2.00	11.31	0.00	0.00
47.08	31.45	18.58	2.37	79.99	2.00	11.45	0.00	0.00
47.12	31.65	18.71	2.39	80.42	2.00	11.67	0.00	0.00
47.18	31.90	18.85	2.41	80.99	2.00	11.92	0.00	0.00
47.27	32.12	18.96	2.44	81.54	2.00	12.11	0.00	0.00
47.31	32.24	19.01	2.48	82.39	2.00	12.20	0.00	0.00
47.39	32.73	19.30	2.52	83.31	2.00	12.71	0.00	0.00
47.48	33.47	19.76	2.55	84.52	2.00	13.48	0.00	0.00
47.52	34.18	20.22	2.60	85.98	2.00	14.24	0.00	0.00
47.59	34.88	20.63	2.71	88.32	2.00	14.90	0.00	0.00
47.66	35.57	21.01	2.87	91.45	2.00	15.51	0.00	0.00
47.74	36.36	21.47	3.01	94.26	2.00	16.22	0.00	0.00
47.79	37.63	22.28	3.09	96.75	2.00	17.44	0.00	0.00
47.86	39.62	23.59	3.10	98.98	2.00	19.33	0.00	0.00
47.94	42.38	25.46	3.04	100.78	2.00	21.84	0.00	0.00
47.99	46.45	28.27	2.92	102.50	2.00	25.30	0.00	0.00
48.05	51.69	31.91	2.77	104.31	2.00	29.30	0.00	0.00
48.13	57.43	35.93	2.65	106.37	2.00	33.21	0.00	0.00
48.19	63.46	40.18	2.53	108.40	2.00	36.91	0.00	0.00
48.26	69.35	44.33	2.46	111.00	2.00	40.15	0.00	0.00
48.34	74.27	47.76	2.45	114.21	2.00	42.61	0.00	0.00
48.39	78.06	50.36	2.49	117.60	0.58	44.36	51.20	0.00
48.43	80.01	51.62	2.57	120.87	0.61	45.17	34.10	0.00
48.51	80.23	51.58	2.68	123.65	2.00	45.15	0.00	0.00
48.58	78.15	49.87	2.86	126.20	2.00	44.04	0.00	0.00
48.63	73.91	46.66	3.11	128.57	2.00	41.84	0.00	0.00
48.72	69.19	43.12	3.39	130.53	2.00	39.24	0.00	0.00
48.78	64.53	39.71	3.68	132.10	2.00	36.52	0.00	0.00
48.83	60.65	36.92	3.91	132.69	2.00	34.11	0.00	0.00
48.90	58.27	35.18	4.07	133.00	2.00	32.52	0.00	0.00
48.99	56.81	34.10	4.17	133.10	2.00	31.49	0.00	0.00
49.03	57.34	34.43	4.16	133.52	2.00	31.81	0.00	0.00
49.08	59.70	36.02	4.07	134.25	2.00	33.30	0.00	0.00
49.17	64.88	39.55	3.87	135.60	2.00	36.38	0.00	0.00
49.23	73.51	45.55	3.55	136.90	2.00	41.05	0.00	0.00
49.32	85.21	53.79	3.20	138.53	2.00	46.53	0.00	0.00
49.35	97.81	62.84	2.92	140.98	2.00	51.67	0.00	0.00
49.43	111.56	72.74	2.68	144.42	2.00	56.50	0.00	0.00
49.50	126.07	83.33	2.48	148.53	2.00	60.98	0.00	0.00
49.58	140.81	94.14	2.31	153.61	2.00	65.01	0.00	0.00
49.63	155.36	104.93	2.18	159.57	2.00	68.59	0.00	0.00
49.72	169.50	115.38	2.08	166.05	2.00	71.72	0.00	0.00
49.78	181.49	124.33	2.01	171.86	2.00	74.19	0.00	0.00
49.83	190.73	131.20	1.96	176.75	2.00	75.96	0.00	0.00
49.90	196.54	135.41	1.95	180.17	1.57	77.00	1.25	0.00
49.98	200.97	138.54	1.94	182.84	1.64	77.76	1.16	0.00

:: Estimation of post-earthquake lateral Displacements :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	R_f (%)	$Q_{tn,cs}$	FS	D_r	$Gamma_{max}$ (%)	Lat. disp. (in)
50.02	203.65	140.45	1.94	184.55	2.00	78.21	0.00	0.00
50.08	205.02	141.54	1.90	184.09	2.00	78.47	0.00	0.00
50.18	205.97	142.29	1.84	183.07	2.00	78.64	0.00	0.00
50.23	206.42	142.77	1.79	181.88	2.00	78.75	0.00	0.00
50.27	206.67	143.11	1.74	180.71	2.00	78.83	0.00	0.00
50.36	206.82	143.25	1.70	179.58	2.00	78.86	0.00	0.00
50.40	206.95	143.47	1.67	178.63	2.00	78.91	0.00	0.00
50.47	207.35	143.80	1.63	177.89	2.00	78.99	0.00	0.00
50.55	207.82	144.14	1.61	177.42	2.00	79.07	0.00	0.00
50.63	208.28	144.42	1.59	177.15	2.00	79.13	0.00	0.00
50.67	208.58	144.31	1.63	178.43	2.00	79.11	0.00	0.00
50.72	208.67	143.92	1.70	180.14	2.00	79.02	0.00	0.00
50.83	208.48	143.22	1.77	181.54	2.00	78.86	0.00	0.00
50.88	208.04	142.49	1.83	182.79	2.00	78.69	0.00	0.00
50.93	207.42	141.67	1.88	183.75	2.00	78.50	0.00	0.00
51.02	206.85	140.84	1.93	184.53	2.00	78.30	0.00	0.00
51.08	206.30	140.13	1.97	185.17	2.00	78.14	0.00	0.00
51.12	205.82	139.57	2.00	185.58	2.00	78.00	0.00	0.00
51.21	205.38	138.99	2.02	185.59	2.00	77.87	0.00	0.00
51.27	205.16	138.70	2.02	185.41	2.00	77.80	0.00	0.00
51.32	205.10	138.60	2.01	185.01	2.00	77.77	0.00	0.00
51.39	205.14	138.54	2.00	184.61	2.00	77.76	0.00	0.00
51.47	205.24	138.49	1.99	184.27	2.00	77.75	0.00	0.00
51.55	205.31	138.40	1.99	184.07	2.00	77.73	0.00	0.00
51.60	205.08	138.14	1.99	183.84	2.00	77.66	0.00	0.00
51.67	204.64	137.67	1.99	183.52	2.00	77.55	0.00	0.00
51.72	203.58	136.81	1.99	182.68	2.00	77.34	0.00	0.00
51.79	201.52	135.28	1.97	180.62	2.00	76.97	0.00	0.00
51.87	199.01	133.36	1.96	178.56	2.00	76.50	0.00	0.00
51.91	196.40	131.39	1.96	176.81	2.00	76.01	0.00	0.00
51.98	192.80	128.68	1.96	174.31	2.00	75.32	0.00	0.00
52.06	188.34	125.28	1.97	171.51	2.00	74.44	0.00	0.00
52.12	183.88	122.00	1.97	168.38	2.00	73.56	0.00	0.00
52.17	178.11	117.70	1.99	165.18	2.00	72.38	0.00	0.00
52.26	170.61	112.01	2.04	161.59	2.00	70.74	0.00	0.00
52.31	163.90	106.94	2.11	159.09	2.00	69.21	0.00	0.00
52.38	156.13	101.00	2.22	157.10	2.00	67.33	0.00	0.00
52.47	147.15	94.26	2.34	154.49	2.00	65.05	0.00	0.00
52.51	136.09	86.23	2.47	150.95	2.00	62.11	0.00	0.00
52.56	124.42	77.83	2.62	147.40	2.00	58.73	0.00	0.00
52.66	112.90	69.62	2.77	143.68	2.00	55.05	0.00	0.00
52.70	100.48	60.93	2.97	140.39	2.00	50.65	0.00	0.00
52.77	89.16	53.15	3.14	136.45	2.00	46.14	0.00	0.00
52.87	79.44	46.57	3.24	131.31	2.00	41.78	0.00	0.00
52.92	69.32	39.89	3.35	125.70	2.00	36.66	0.00	0.00
52.97	61.28	34.64	3.43	120.40	2.00	32.01	0.00	0.00
53.02	54.61	30.38	3.44	114.68	2.00	27.67	0.00	0.00
53.10	50.06	27.50	3.36	109.11	2.00	24.39	0.00	0.00

:: Estimation of post-earthquake lateral Displacements :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	R_f (%)	$Q_{tn,cs}$	FS	D_r	$Gamma_{max}$ (%)	Lat. disp. (in)
53.16	46.90	25.55	3.22	104.01	2.00	21.97	0.00	0.00
53.22	44.28	23.98	3.03	98.54	2.00	19.87	0.00	0.00
53.31	42.65	23.03	2.80	93.26	2.00	18.54	0.00	0.00
53.36	41.31	22.29	2.56	88.37	2.00	17.45	0.00	0.00
53.42	40.10	21.59	2.39	84.45	2.00	16.41	0.00	0.00
53.51	39.07	21.00	2.22	80.92	2.00	15.48	0.00	0.00
53.56	37.95	20.34	2.10	77.90	2.00	14.43	0.00	0.00
53.62	37.07	19.81	2.02	75.92	2.00	13.56	0.00	0.00
53.71	36.24	19.28	1.97	74.43	2.00	12.67	0.00	0.00
53.75	35.58	18.87	1.94	73.33	2.00	11.97	0.00	0.00
53.83	34.88	18.39	1.96	73.18	2.00	11.11	0.00	0.00
53.91	34.05	17.84	1.99	72.99	2.00	10.10	0.00	0.00
53.98	33.09	17.20	2.02	72.61	2.00	8.90	0.00	0.00
54.01	32.19	16.62	2.05	72.23	2.00	7.77	0.00	0.00
54.11	31.08	15.89	2.07	71.62	2.00	6.30	0.00	0.00
54.15	29.90	15.16	2.08	70.59	2.00	4.73	0.00	0.00
54.21	28.55	14.31	2.08	69.38	2.00	2.83	0.00	0.00
54.27	27.04	13.38	2.06	67.57	2.00	0.62	0.00	0.00
54.35	25.56	12.48	2.01	65.45	2.00	0.00	0.00	0.00
54.42	24.28	11.72	1.93	63.06	2.00	0.00	0.00	0.00
54.46	23.20	11.09	1.84	60.75	2.00	0.00	0.00	0.00
54.55	22.43	10.64	1.73	58.58	2.00	0.00	0.00	0.00
54.60	21.80	10.29	1.64	56.66	2.00	0.00	0.00	0.00
54.67	21.40	10.06	1.54	54.95	2.00	0.00	0.00	0.00
54.74	21.06	9.87	1.46	53.59	2.00	0.00	0.00	0.00
54.79	20.77	9.71	1.41	52.57	2.00	0.00	0.00	0.00
54.86	20.62	9.62	1.37	51.96	2.00	0.00	0.00	0.00
54.96	20.50	9.54	1.35	51.56	2.00	0.00	0.00	0.00
55.03	20.43	9.49	1.34	51.32	2.00	0.00	0.00	0.00
55.06	20.38	9.46	1.34	51.16	2.00	0.00	0.00	0.00
55.14	20.37	9.44	1.33	51.00	2.00	0.00	0.00	0.00
55.21	20.35	9.42	1.32	50.83	2.00	0.00	0.00	0.00
55.25	20.31	9.39	1.31	50.67	2.00	0.00	0.00	0.00
55.32	20.28	9.37	1.30	50.50	2.00	0.00	0.00	0.00
55.41	20.24	9.33	1.29	50.33	2.00	0.00	0.00	0.00
55.45	20.23	9.32	1.29	50.24	2.00	0.00	0.00	0.00
55.52	20.23	9.31	1.29	50.23	2.00	0.00	0.00	0.00
55.61	20.28	9.33	1.29	50.28	2.00	0.00	0.00	0.00
55.65	20.52	9.45	1.32	50.89	2.00	0.00	0.00	0.00
55.71	20.91	9.67	1.35	51.70	2.00	0.00	0.00	0.00
55.80	21.44	9.96	1.38	52.64	2.00	0.00	0.00	0.00
55.86	22.21	10.40	1.42	53.78	2.00	0.00	0.00	0.00
55.95	23.00	10.84	1.46	55.07	2.00	0.00	0.00	0.00
56.00	23.79	11.29	1.50	56.40	2.00	0.00	0.00	0.00
56.05	24.57	11.73	1.55	57.75	2.00	0.00	0.00	0.00
56.11	25.39	12.21	1.56	58.54	2.00	0.00	0.00	0.00
56.20	26.17	12.67	1.54	58.93	2.00	0.00	0.00	0.00
56.24	26.73	13.01	1.50	58.82	2.00	0.00	0.00	0.00

:: Estimation of post-earthquake lateral Displacements :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	R_f (%)	$Q_{tn,cs}$	FS	D_r	$Gamma_{max}$ (%)	Lat. disp. (in)
56.31	27.09	13.23	1.48	58.66	2.00	0.24	0.00	0.00
56.39	27.14	13.26	1.45	58.31	2.00	0.30	0.00	0.00
56.43	26.89	13.11	1.43	57.80	2.00	0.00	0.00	0.00
56.50	26.19	12.68	1.42	56.98	2.00	0.00	0.00	0.00
56.60	25.50	12.25	1.39	56.00	2.00	0.00	0.00	0.00
56.66	24.81	11.85	1.34	54.73	2.00	0.00	0.00	0.00
56.70	24.10	11.42	1.32	53.84	2.00	0.00	0.00	0.00
56.79	23.44	11.01	1.32	53.20	2.00	0.00	0.00	0.00
56.84	22.85	10.64	1.32	52.77	2.00	0.00	0.00	0.00
56.92	22.40	10.36	1.34	52.61	2.00	0.00	0.00	0.00
56.99	22.25	10.25	1.35	52.66	2.00	0.00	0.00	0.00
57.03	22.42	10.34	1.36	52.94	2.00	0.00	0.00	0.00
57.09	23.22	10.80	1.37	53.70	2.00	0.00	0.00	0.00
57.18	23.98	11.23	1.39	54.70	2.00	0.00	0.00	0.00
57.23	24.85	11.71	1.48	56.60	2.00	0.00	0.00	0.00
57.31	26.05	12.34	1.62	59.70	2.00	0.00	0.00	0.00
57.38	27.50	13.12	1.79	63.35	2.00	0.00	0.00	0.00
57.43	29.89	14.46	1.95	67.68	2.00	3.17	0.00	0.00
57.50	33.85	16.75	2.07	72.85	2.00	8.03	0.00	0.00
57.58	38.94	19.76	2.13	77.84	2.00	13.48	0.00	0.00
57.62	45.95	24.03	2.12	82.77	2.00	19.93	0.00	0.00
57.68	53.93	28.96	2.11	88.00	2.00	26.09	0.00	0.00
57.78	62.67	34.40	2.10	93.09	2.00	31.78	0.00	0.00
57.82	72.41	40.59	2.06	98.14	2.00	37.24	0.00	0.00
57.89	82.22	46.92	2.01	102.62	2.00	42.02	0.00	0.00
57.97	91.68	53.07	1.96	106.91	2.00	46.09	0.00	0.00
58.02	99.77	58.36	1.93	110.82	2.00	49.23	0.00	0.00
58.09	105.22	61.89	1.93	113.73	2.00	51.16	0.00	0.00
58.17	108.62	64.01	1.95	116.09	2.00	52.28	0.00	0.00
58.23	109.72	64.57	1.99	117.85	2.00	52.56	0.00	0.00
58.28	109.49	64.23	2.05	119.20	2.00	52.39	0.00	0.00
58.37	108.18	63.12	2.13	120.41	2.00	51.81	0.00	0.00
58.43	105.44	61.09	2.23	121.15	2.00	50.73	0.00	0.00
58.48	100.57	57.67	2.35	121.32	2.00	48.83	0.00	0.00
58.57	95.05	53.81	2.51	121.56	2.00	46.55	0.00	0.00
58.62	88.67	49.47	2.69	121.83	2.00	43.77	0.00	0.00
58.67	82.27	45.20	2.88	121.69	2.00	40.79	0.00	0.00
58.78	76.27	41.23	3.06	121.38	2.00	37.75	0.00	0.00
58.82	69.93	37.13	3.27	120.73	2.00	34.30	0.00	0.00
58.88	63.59	33.12	3.49	119.62	2.00	30.53	0.00	0.00
58.97	57.66	29.45	3.66	117.21	2.00	26.65	0.00	0.00
59.01	52.33	26.22	3.82	114.63	2.00	22.82	0.00	0.00
59.07	48.78	24.09	3.91	112.37	2.00	20.02	0.00	0.00
59.12	45.34	22.06	3.98	109.61	2.00	17.11	0.00	0.00
59.19	42.74	20.56	3.96	106.39	2.00	14.79	0.00	0.00
59.27	41.35	19.78	3.84	103.23	2.00	13.52	0.00	0.00
59.32	39.96	19.01	3.73	100.24	2.00	12.21	0.00	0.00
59.42	39.47	18.76	3.59	97.90	2.00	11.76	0.00	0.00

:: Estimation of post-earthquake lateral Displacements :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	R_f (%)	$Q_{tn,cs}$	FS	D_r	$Gamma_{max}$ (%)	Lat. disp. (in)
59.47	38.99	18.52	3.45	95.59	2.00	11.34	0.00	0.00
59.52	38.64	18.33	3.37	94.16	2.00	11.00	0.00	0.00
59.58	38.47	18.26	3.26	92.55	2.00	10.87	0.00	0.00
59.68	38.20	18.11	3.17	91.05	2.00	10.60	0.00	0.00
59.74	38.28	18.16	3.11	90.38	2.00	10.69	0.00	0.00
59.78	38.65	18.53	2.71	85.25	2.00	11.37	0.00	0.00
59.88	38.74	18.73	2.37	80.36	2.00	11.70	0.00	0.00
59.93	39.33	19.26	2.01	75.24	2.00	12.63	0.00	0.00
60.00	40.82	20.43	1.61	69.20	2.00	14.57	0.00	0.00
60.05	43.76	22.60	1.20	62.70	2.00	17.92	0.00	0.00
60.13	46.96	25.08	0.84	56.21	2.00	21.35	0.00	0.00
60.18	46.63	25.36	0.58	49.61	2.00	21.71	0.00	0.00
60.25	48.94	27.71	0.29	27.71	2.00	24.64	0.00	0.00
60.33	54.14	N/A	0.00	-1.00	2.00	0.00	0.00	0.00
60.38	58.50	N/A	0.00	-1.00	2.00	0.00	0.00	0.00

Total estimated displacement: 0.00

Abbreviations

q_t: Total cone resistance
Q_{tn}: Adjusted cone resistance to an effective overburden stress of 1 atm
R_f: Friction ration
$Q_{tn,cs}$: Adjusted and corrected cone resistance due to fines
FS: Calculated factor of safety against liquefaction
D_r: Calculated relative density
$Gamma_{max}$: Calculated maximum cyclic shear strain
Lat. disp.: Lateral displacement

:: Strength loss calculation (Robertson (2009) ::

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
0.10	15.36	24.68	2.58	63.55	2.46	N/A	N/A
0.16	18.18	29.20	2.21	64.47	2.37	N/A	N/A
0.21	20.36	32.69	2.00	65.27	2.31	N/A	N/A
0.29	21.38	34.33	1.91	65.70	2.29	N/A	N/A
0.36	22.80	36.60	1.80	66.00	2.25	N/A	N/A
0.40	26.01	41.75	1.63	68.26	2.19	N/A	N/A
0.51	29.38	47.16	1.52	71.49	2.13	N/A	N/A
0.57	32.38	51.97	1.44	75.04	2.09	N/A	N/A
0.61	35.46	56.92	1.40	79.41	2.07	N/A	N/A
0.70	38.31	61.48	1.38	84.75	2.05	N/A	N/A
0.76	40.98	65.78	1.37	90.30	2.05	N/A	N/A
0.81	43.44	69.72	1.38	96.06	2.05	N/A	N/A
0.87	45.02	72.26	1.41	101.55	2.07	N/A	N/A
0.96	46.00	73.82	1.44	106.65	2.09	N/A	N/A
1.00	46.15	74.05	1.50	110.83	2.12	N/A	N/A
1.05	45.49	72.99	1.56	113.61	2.15	N/A	N/A
1.16	44.58	71.53	1.62	115.80	2.18	N/A	N/A
1.20	43.39	69.61	1.68	117.12	2.21	N/A	N/A
1.26	42.04	67.43	1.73	116.97	2.23	N/A	N/A
1.35	40.70	65.27	1.78	116.40	2.24	N/A	N/A
1.40	39.42	63.22	1.83	115.37	2.26	N/A	N/A
1.45	38.31	61.42	1.85	113.69	2.27	N/A	N/A
1.55	36.98	59.27	1.89	111.93	2.28	N/A	N/A
1.60	35.41	56.74	1.95	110.41	2.30	N/A	N/A
1.64	33.59	53.81	2.04	109.72	2.33	N/A	N/A
1.71	31.62	50.64	2.16	109.52	2.36	N/A	N/A
1.79	29.70	47.55	2.31	109.74	2.40	N/A	N/A
1.87	28.02	44.86	2.47	110.96	2.44	N/A	N/A
1.95	26.09	41.75	2.70	112.56	2.49	N/A	N/A
2.00	24.07	38.50	2.97	114.43	2.54	N/A	N/A
2.04	22.09	35.30	3.29	116.10	2.59	N/A	N/A
2.11	20.34	32.49	3.61	117.33	2.64	N/A	N/A
2.19	18.97	30.28	3.91	118.26	2.69	N/A	N/A
2.24	17.93	28.61	4.15	118.85	2.72	N/A	N/A
2.30	17.03	27.15	4.39	119.14	2.75	N/A	N/A
2.38	16.21	25.83	4.62	119.35	2.78	N/A	N/A
2.45	15.52	24.71	4.82	119.16	2.80	N/A	N/A
2.50	15.08	24.00	4.95	118.88	2.82	N/A	N/A
2.58	14.72	23.42	5.06	118.54	2.83	N/A	N/A
2.64	14.48	23.03	5.13	118.11	2.84	N/A	N/A
2.69	14.36	22.83	5.12	116.92	2.84	N/A	N/A
2.79	14.25	22.65	5.08	115.12	2.83	N/A	N/A
2.85	14.17	22.50	5.02	112.97	2.83	N/A	N/A
2.90	13.76	21.84	5.04	110.17	2.83	N/A	N/A
2.98	13.13	20.82	5.12	106.59	2.84	N/A	N/A
3.05	12.47	19.76	5.18	102.45	2.85	N/A	N/A
3.09	11.81	18.69	5.23	97.68	2.85	N/A	N/A
3.17	11.04	17.45	5.32	92.83	2.86	N/A	N/A

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
3.24	10.27	16.21	5.42	87.93	2.87	N/A	N/A
3.29	9.66	15.22	5.52	83.96	2.88	N/A	N/A
3.36	9.23	14.52	5.60	81.34	2.89	N/A	N/A
3.44	8.90	13.99	5.68	79.42	2.90	N/A	N/A
3.48	9.04	14.21	5.59	79.36	2.89	N/A	N/A
3.56	9.43	14.82	5.48	81.26	2.88	N/A	N/A
3.64	9.85	15.50	5.43	84.14	2.87	N/A	N/A
3.69	10.29	16.20	5.44	88.06	2.87	N/A	N/A
3.76	10.82	17.04	5.40	92.12	2.87	N/A	N/A
3.84	11.33	17.85	5.40	96.35	2.87	N/A	N/A
3.88	11.63	18.33	5.48	100.41	2.88	N/A	N/A
3.98	11.73	18.49	5.61	103.76	2.89	N/A	N/A
4.03	11.65	18.35	5.83	106.89	2.91	N/A	N/A
4.08	11.56	18.20	6.01	109.42	2.93	N/A	N/A
4.14	11.46	18.03	6.17	111.18	2.95	N/A	N/A
4.23	11.31	17.80	6.32	112.52	2.96	N/A	N/A
4.27	11.11	17.46	6.48	113.17	2.98	N/A	N/A
4.36	10.88	17.08	6.63	113.32	2.99	N/A	N/A
4.41	10.61	16.64	6.79	113.06	3.00	N/A	N/A
4.46	10.35	16.22	6.93	112.50	3.02	N/A	N/A
4.55	10.12	15.85	7.05	111.73	3.03	N/A	N/A
4.61	10.03	15.70	7.06	110.75	3.03	N/A	N/A
4.66	9.83	15.37	7.11	109.37	3.03	N/A	N/A
4.75	9.64	15.06	7.17	107.97	3.04	N/A	N/A
4.80	9.49	14.82	7.20	106.75	3.04	N/A	N/A
4.86	9.44	14.73	7.17	105.64	3.04	N/A	N/A
4.96	9.44	14.72	7.11	104.71	3.03	N/A	N/A
5.01	9.55	14.90	6.97	103.88	3.02	N/A	N/A
5.06	9.80	15.29	6.74	103.13	3.00	N/A	N/A
5.16	10.15	15.84	6.47	102.54	2.98	N/A	N/A
5.21	10.54	16.46	6.20	102.01	2.95	N/A	N/A
5.26	10.94	17.10	5.95	101.76	2.93	N/A	N/A
5.32	11.28	17.64	5.74	101.29	2.90	N/A	N/A
5.41	11.50	18.00	5.59	100.63	2.89	N/A	N/A
5.46	11.59	18.14	5.52	100.02	2.88	N/A	N/A
5.52	11.55	18.07	5.51	99.48	2.88	N/A	N/A
5.60	11.35	17.72	5.59	99.14	2.89	N/A	N/A
5.66	11.02	17.19	5.76	98.96	2.91	N/A	N/A
5.71	10.61	16.53	5.98	98.90	2.93	N/A	N/A
5.81	10.22	15.90	6.24	99.15	2.95	N/A	N/A
5.89	9.86	15.32	6.50	99.57	2.98	N/A	N/A
5.91	9.60	14.90	6.75	100.59	3.00	N/A	N/A
6.00	9.50	14.72	6.92	101.89	3.02	N/A	N/A
6.06	9.56	14.81	6.99	103.57	3.02	N/A	N/A
6.11	9.75	15.12	6.99	105.64	3.02	N/A	N/A
6.20	10.06	15.61	6.92	107.97	3.02	N/A	N/A
6.24	10.37	16.10	6.85	110.35	3.01	N/A	N/A
6.30	10.62	16.49	6.81	112.39	3.01	N/A	N/A

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
6.38	10.79	16.76	6.81	114.12	3.01	N/A	N/A
6.46	10.91	16.94	6.82	115.45	3.01	N/A	N/A
6.50	10.94	16.98	6.84	116.11	3.01	N/A	N/A
6.60	10.90	16.91	6.88	116.40	3.01	N/A	N/A
6.63	10.77	16.70	6.95	116.12	3.02	N/A	N/A
6.72	10.55	16.34	7.04	115.09	3.03	N/A	N/A
6.80	10.30	15.93	7.13	113.56	3.03	N/A	N/A
6.84	10.05	15.53	7.20	111.82	3.04	N/A	N/A
6.90	9.79	15.11	7.29	110.15	3.05	N/A	N/A
7.00	9.55	14.71	7.38	108.54	3.05	N/A	N/A
7.04	9.31	14.33	7.48	107.12	3.06	N/A	N/A
7.09	9.08	13.96	7.58	105.77	3.07	N/A	N/A
7.20	8.89	13.63	7.68	104.61	3.08	N/A	N/A
7.24	8.72	13.35	7.75	103.54	3.09	N/A	N/A
7.30	8.61	13.17	7.80	102.79	3.09	N/A	N/A
7.39	8.52	13.02	7.84	102.04	3.09	N/A	N/A
7.43	8.43	12.87	7.88	101.39	3.10	N/A	N/A
7.50	8.39	12.81	7.88	100.85	3.10	N/A	N/A
7.59	8.35	12.74	7.88	100.32	3.10	N/A	N/A
7.64	8.35	12.73	7.84	99.80	3.09	N/A	N/A
7.70	8.37	12.76	7.79	99.38	3.09	N/A	N/A
7.79	8.41	12.81	7.71	98.76	3.08	N/A	N/A
7.83	8.43	12.84	7.63	98.02	3.08	N/A	N/A
7.90	8.45	12.87	7.56	97.27	3.07	N/A	N/A
7.94	8.50	12.95	7.46	96.63	3.06	N/A	N/A
8.03	8.53	12.98	7.37	95.64	3.05	N/A	N/A
8.11	8.52	12.96	7.28	94.29	3.05	N/A	N/A
8.17	8.50	12.93	7.17	92.70	3.04	N/A	N/A
8.21	8.43	12.81	7.09	90.83	3.03	N/A	N/A
8.28	8.32	12.62	7.03	88.68	3.03	N/A	N/A
8.37	8.16	12.36	7.00	86.47	3.02	N/A	N/A
8.41	7.97	12.06	6.98	84.20	3.02	N/A	N/A
8.48	7.72	11.65	7.02	81.74	3.02	N/A	N/A
8.57	7.42	11.15	7.09	79.06	3.03	N/A	N/A
8.61	7.14	10.70	7.17	76.70	3.04	N/A	N/A
8.67	6.87	10.26	7.26	74.54	3.05	N/A	N/A
8.77	6.62	9.85	7.37	72.60	3.05	N/A	N/A
8.81	6.40	9.50	7.48	71.07	3.06	N/A	N/A
8.87	6.27	9.29	7.53	69.97	3.07	N/A	N/A
8.96	6.21	9.17	7.55	69.19	3.07	N/A	N/A
8.99	6.25	9.23	7.45	68.74	3.06	N/A	N/A
9.07	6.38	9.45	7.25	68.47	3.04	0.40	0.83
9.16	6.56	9.73	7.01	68.19	3.02	0.39	0.85
9.21	6.75	10.03	6.75	67.73	3.00	0.39	0.87
9.27	6.95	10.34	6.50	67.24	2.98	0.39	0.89
9.36	7.12	10.61	6.31	66.90	2.96	0.37	0.91
9.40	7.28	10.86	6.13	66.54	2.94	0.35	0.93
9.48	7.42	11.08	6.00	66.51	2.93	0.32	0.94

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
9.52	7.61	11.38	5.91	67.29	2.92	0.30	0.96
9.61	7.88	11.80	5.79	68.36	2.91	0.32	0.99
9.65	8.20	12.31	5.69	70.02	2.90	1.03	1.03
9.72	8.71	13.12	5.56	72.94	2.89	1.09	1.09
9.81	9.31	14.09	5.41	76.25	2.87	1.16	1.16
9.86	10.14	15.41	5.25	80.94	2.85	1.26	1.26
9.91	11.02	16.83	5.08	85.53	2.83	1.37	1.37
10.00	11.92	18.26	4.93	90.08	2.82	1.47	1.47
10.05	12.98	19.95	4.76	94.97	2.80	1.60	1.60
10.16	14.05	21.67	4.59	99.56	2.78	1.72	1.72
10.20	15.10	23.35	4.44	103.70	2.76	1.84	1.84
10.25	16.16	25.05	4.30	107.64	2.74	1.97	1.97
10.31	17.03	26.44	4.20	111.04	2.73	2.06	2.06
10.40	17.83	27.73	4.12	114.17	2.72	2.14	2.14
10.44	18.60	28.95	4.02	116.36	2.70	2.23	2.23
10.51	19.07	29.70	3.96	117.57	2.69	2.27	2.27
10.59	19.49	30.36	3.88	117.93	2.68	2.30	2.30
10.65	19.75	30.58	3.83	117.21	2.68	2.32	2.32
10.71	19.91	30.63	3.78	115.91	2.67	2.33	2.33
10.80	20.00	30.53	3.79	115.58	2.67	2.32	2.32
10.85	20.00	30.40	3.80	115.50	2.67	2.31	2.31
10.90	19.65	29.79	3.89	115.78	2.68	2.25	2.25
10.96	19.02	28.80	4.05	116.70	2.71	2.17	2.17
11.04	18.63	28.09	4.18	117.49	2.73	2.10	2.10
11.10	18.54	27.88	4.28	119.21	2.74	2.08	2.08
11.18	18.55	27.77	4.37	121.48	2.75	2.07	2.07
11.24	18.66	27.84	4.45	123.77	2.76	2.07	2.07
11.30	18.82	27.98	4.51	126.31	2.77	2.07	2.07
11.35	19.00	28.17	4.56	128.55	2.77	2.08	2.08
11.42	19.22	28.35	4.61	130.69	2.78	2.09	2.09
11.51	19.84	29.02	4.55	132.02	2.77	2.15	2.15
11.55	20.77	30.20	4.39	132.54	2.75	2.24	2.24
11.62	21.32	30.79	4.31	132.86	2.74	2.29	2.29
11.71	21.83	31.26	4.25	132.97	2.73	2.32	2.32
11.75	22.14	31.58	4.22	133.24	2.73	2.35	2.35
11.85	22.14	31.34	4.26	133.38	2.73	2.33	2.33
11.90	22.04	31.09	4.29	133.42	2.74	2.31	2.31
11.94	21.77	30.62	4.33	132.59	2.74	2.27	2.27
12.02	21.29	29.80	4.40	131.08	2.75	2.20	2.20
12.10	20.69	28.88	4.48	129.32	2.76	2.13	2.13
12.15	19.88	27.73	4.60	127.53	2.78	2.04	2.04
12.24	18.97	26.39	4.75	125.46	2.80	1.94	1.94
12.30	18.13	25.19	4.88	122.90	2.81	1.84	1.84
12.35	17.31	24.01	4.99	119.91	2.82	1.75	1.75
12.44	16.81	23.21	5.02	116.58	2.83	1.69	1.69
12.50	16.42	22.60	5.02	113.49	2.83	1.65	1.65
12.55	16.24	22.28	4.99	111.12	2.82	1.63	1.63
12.63	16.22	22.16	4.93	109.20	2.82	1.62	1.62

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
12.70	16.29	22.18	4.89	108.36	2.81	1.62	1.62
12.74	16.47	22.38	4.84	108.34	2.81	1.64	1.64
12.84	16.72	22.63	4.81	108.74	2.80	1.66	1.66
12.86	16.90	22.86	4.80	109.69	2.80	1.67	1.67
12.94	17.15	23.14	4.79	110.77	2.80	1.69	1.69
13.01	17.16	23.11	4.84	111.95	2.81	1.69	1.69
13.09	17.06	22.94	4.93	113.02	2.82	1.67	1.67
13.14	16.85	22.63	5.01	113.48	2.83	1.65	1.65
13.20	16.59	22.25	5.10	113.51	2.84	1.62	1.62
13.29	16.32	21.82	5.17	112.86	2.84	1.59	1.59
13.33	16.03	21.41	5.23	112.02	2.85	1.55	1.55
13.39	15.74	20.96	5.29	110.88	2.86	1.52	1.52
13.49	15.44	20.49	5.35	109.66	2.86	1.48	1.48
13.53	15.17	20.10	5.40	108.60	2.87	1.45	1.45
13.59	14.97	19.77	5.38	106.39	2.87	1.43	1.43
13.69	14.77	19.40	5.34	103.62	2.86	1.40	1.40
13.73	14.50	19.00	5.35	101.62	2.86	1.38	1.38
13.79	14.20	18.55	5.39	99.88	2.87	1.34	1.34
13.89	13.86	18.03	5.44	98.09	2.87	1.30	1.30
13.94	13.52	17.54	5.48	96.12	2.88	1.27	1.27
13.99	12.93	16.74	5.62	94.08	2.89	1.21	1.21
14.08	12.45	16.04	5.72	91.65	2.90	1.15	1.15
14.13	12.06	15.48	5.76	89.13	2.91	1.11	1.11
14.18	11.66	14.93	5.87	87.67	2.92	1.07	1.07
14.27	11.28	14.38	6.03	86.68	2.93	1.03	1.03
14.32	10.95	13.93	6.12	85.22	2.94	1.00	1.00
14.37	10.65	13.50	6.18	83.50	2.95	0.97	0.97
14.48	10.39	13.11	6.24	81.76	2.95	0.94	0.94
14.52	10.14	12.75	6.30	80.28	2.96	0.91	0.91
14.58	10.13	12.71	6.21	78.93	2.95	0.91	0.91
14.68	10.02	12.51	6.23	77.91	2.95	0.89	0.89
14.72	9.92	12.36	6.24	77.05	2.95	0.88	0.88
14.77	9.92	12.33	6.21	76.51	2.95	0.88	0.88
14.83	10.03	12.44	6.12	76.16	2.94	0.89	0.89
14.92	10.18	12.58	6.02	75.75	2.93	0.90	0.90
14.98	10.38	12.80	5.91	75.61	2.92	0.92	0.92
15.07	10.58	13.01	5.80	75.43	2.91	0.93	0.93
15.11	10.79	13.25	5.69	75.41	2.90	0.95	0.95
15.17	11.01	13.50	5.61	75.74	2.89	0.97	0.97
15.27	11.22	13.72	5.54	76.03	2.88	0.99	0.99
15.31	11.35	13.86	5.52	76.54	2.88	1.00	1.00
15.38	11.41	13.93	5.56	77.42	2.89	1.00	1.00
15.47	11.44	13.94	5.62	78.29	2.89	1.00	1.00
15.52	11.40	13.88	5.73	79.45	2.90	1.00	1.00
15.56	11.30	13.74	5.87	80.64	2.92	0.99	0.99
15.64	11.17	13.56	6.03	81.77	2.93	0.97	0.97
15.71	11.01	13.34	6.20	82.68	2.95	0.95	0.95
15.75	10.82	13.08	6.37	83.34	2.97	0.93	0.93

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
15.87	10.55	12.67	6.59	83.46	2.99	0.91	0.91
15.91	10.21	12.21	6.83	83.43	3.01	0.87	0.87
15.96	9.82	11.68	7.08	82.74	3.03	0.83	0.83
16.01	9.34	11.02	7.40	81.57	3.06	0.79	0.79
16.11	8.88	10.39	7.70	79.98	3.08	0.74	0.74
16.15	8.47	9.84	7.95	78.20	3.10	0.70	0.70
16.22	8.05	9.27	8.19	75.99	3.12	0.66	0.66
16.31	7.65	8.73	8.45	73.81	3.14	0.62	0.62
16.36	7.32	8.28	8.65	71.63	3.16	0.59	0.59
16.41	7.12	8.01	8.72	69.84	3.16	0.32	0.57
16.51	7.03	7.86	8.67	68.16	3.16	0.28	0.56
16.54	7.08	7.92	8.47	67.09	3.14	0.28	0.57
16.61	7.22	8.08	8.17	66.02	3.12	0.28	0.58
16.70	7.38	8.26	7.87	65.01	3.10	0.28	0.59
16.75	7.55	8.46	7.72	65.30	3.08	0.28	0.60
16.81	7.72	8.66	7.65	66.21	3.08	0.29	0.62
16.91	7.89	8.85	7.60	67.19	3.07	0.25	0.63
16.95	8.03	9.01	7.57	68.19	3.07	0.24	0.64
17.01	8.12	9.11	7.59	69.14	3.07	0.34	0.65
17.11	8.17	9.14	7.65	69.91	3.08	0.37	0.65
17.13	8.17	9.13	7.72	70.48	3.08	0.65	0.65
17.21	8.14	9.07	7.87	71.32	3.10	0.65	0.65
17.29	8.11	9.00	8.02	72.26	3.11	0.64	0.64
17.34	8.11	8.99	8.05	72.32	3.11	0.64	0.64
17.43	8.11	8.96	8.05	72.13	3.11	0.64	0.64
17.48	8.11	8.95	8.03	71.86	3.11	0.64	0.64
17.54	8.15	8.98	7.98	71.60	3.10	0.64	0.64
17.63	8.21	9.02	7.90	71.32	3.10	0.64	0.64
17.68	8.30	9.12	7.81	71.20	3.09	0.65	0.65
17.73	8.37	9.20	7.74	71.18	3.08	0.66	0.66
17.83	8.49	9.32	7.65	71.25	3.08	0.67	0.67
17.85	8.62	9.47	7.55	71.50	3.07	0.68	0.68
17.93	8.75	9.61	7.47	71.80	3.06	0.69	0.69
17.98	8.91	9.79	7.37	72.13	3.05	0.70	0.70
18.07	9.08	9.96	7.28	72.54	3.05	0.71	0.71
18.12	9.20	10.09	7.23	72.96	3.04	0.72	0.72
18.18	9.30	10.19	7.21	73.48	3.04	0.73	0.73
18.24	9.40	10.30	7.19	73.99	3.04	0.74	0.74
18.33	9.51	10.40	7.16	74.48	3.04	0.74	0.74
18.38	9.64	10.54	7.11	74.99	3.03	0.75	0.75
18.47	9.84	10.75	7.02	75.47	3.02	0.77	0.77
18.53	10.04	10.97	6.91	75.85	3.02	0.78	0.78
18.57	10.26	11.24	6.80	76.36	3.00	0.80	0.80
18.67	10.50	11.49	6.70	77.01	3.00	0.82	0.82
18.72	10.79	11.82	6.58	77.79	2.99	0.84	0.84
18.78	11.12	12.19	6.43	78.44	2.97	0.87	0.87
18.85	11.42	12.53	6.31	79.06	2.96	0.89	0.89
18.93	11.67	12.79	6.23	79.67	2.95	0.91	0.91

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
18.97	11.84	12.97	6.18	80.21	2.95	0.93	0.93
19.08	11.93	13.03	6.18	80.49	2.95	0.93	0.93
19.12	11.99	13.09	6.17	80.75	2.95	0.94	0.94
19.22	12.04	13.10	6.16	80.74	2.95	0.94	0.94
19.27	12.17	13.22	6.08	80.34	2.94	0.95	0.95
19.32	12.24	13.28	6.01	79.86	2.93	0.95	0.95
19.37	12.33	13.36	5.97	79.68	2.93	0.96	0.96
19.43	12.44	13.47	5.92	79.68	2.92	0.96	0.96
19.52	12.63	13.64	5.85	79.84	2.92	0.98	0.98
19.57	12.91	13.94	5.75	80.20	2.91	1.00	1.00
19.67	13.22	14.24	5.66	80.60	2.90	1.02	1.02
19.72	13.55	14.59	5.58	81.43	2.89	1.05	1.05
19.77	13.86	14.93	5.55	82.85	2.88	1.07	1.07
19.82	14.07	15.16	5.57	84.47	2.89	1.09	1.09
19.92	14.31	15.39	5.59	86.10	2.89	1.11	1.11
19.97	14.46	15.55	5.62	87.31	2.89	1.12	1.12
20.04	14.51	15.57	5.67	88.24	2.90	1.12	1.12
20.08	14.51	15.56	5.71	88.85	2.90	1.12	1.12
20.16	14.47	15.48	5.76	89.24	2.91	1.11	1.11
20.24	14.41	15.38	5.82	89.46	2.91	1.10	1.10
20.28	14.35	15.28	5.85	89.45	2.92	1.09	1.09
20.37	14.28	15.16	5.87	88.94	2.92	1.09	1.09
20.41	14.20	15.05	5.88	88.47	2.92	1.08	1.08
20.50	14.10	14.90	5.89	87.78	2.92	1.07	1.07
20.57	14.00	14.75	5.92	87.30	2.92	1.06	1.06
20.61	13.91	14.63	5.94	86.92	2.92	1.05	1.05
20.70	13.81	14.48	5.99	86.69	2.93	1.04	1.04
20.76	13.64	14.27	6.06	86.42	2.94	1.02	1.02
20.81	13.44	14.03	6.15	86.25	2.94	1.00	1.00
20.89	13.21	13.74	6.26	85.97	2.96	0.98	0.98
20.95	12.98	13.45	6.36	85.49	2.96	0.96	0.96
21.00	12.77	13.18	6.42	84.66	2.97	0.94	0.94
21.10	12.56	12.90	6.49	83.76	2.98	0.92	0.92
21.14	12.37	12.67	6.54	82.83	2.98	0.91	0.91
21.21	12.21	12.47	6.57	81.94	2.98	0.89	0.89
21.30	12.05	12.25	6.61	80.94	2.99	0.88	0.88
21.34	11.94	12.11	6.61	80.06	2.99	0.87	0.87
21.40	11.83	11.97	6.61	79.15	2.99	0.85	0.85
21.48	11.77	11.87	6.59	78.22	2.99	0.85	0.85
21.54	11.71	11.78	6.56	77.30	2.98	0.84	0.84
21.60	11.65	11.69	6.55	76.56	2.98	0.83	0.83
21.68	11.61	11.62	6.53	75.91	2.98	0.83	0.83
21.75	11.56	11.53	6.52	75.16	2.98	0.82	0.82
21.80	11.54	11.49	6.46	74.21	2.97	0.82	0.82
21.88	11.53	11.46	6.39	73.23	2.97	0.82	0.82
21.92	11.51	11.42	6.33	72.27	2.96	0.82	0.82
21.99	11.48	11.36	6.29	71.48	2.96	0.81	0.81
22.08	11.39	11.23	6.30	70.79	2.96	0.80	0.80

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
22.15	11.30	11.11	6.33	70.32	2.96	0.79	0.79
22.19	11.15	10.93	6.41	70.10	2.97	0.78	0.78
22.28	10.97	10.71	6.52	69.83	2.98	0.33	0.76
22.34	10.82	10.51	6.65	69.90	2.99	0.33	0.75
22.39	10.66	10.32	6.78	69.97	3.00	0.33	0.74
22.47	10.52	10.15	6.90	70.01	3.01	0.72	0.72
22.54	10.38	9.97	7.04	70.16	3.03	0.71	0.71
22.58	10.32	9.90	7.10	70.23	3.03	0.71	0.71
22.68	10.27	9.81	7.16	70.25	3.04	0.70	0.70
22.74	10.22	9.74	7.23	70.41	3.04	0.70	0.70
22.79	10.24	9.75	7.23	70.48	3.04	0.70	0.70
22.84	10.28	9.78	7.22	70.55	3.04	0.70	0.70
22.94	10.32	9.79	7.20	70.48	3.04	0.70	0.70
22.99	10.34	9.80	7.19	70.45	3.04	0.70	0.70
23.04	10.29	9.73	7.24	70.40	3.04	0.69	0.69
23.11	10.24	9.65	7.26	70.14	3.05	0.69	0.69
23.18	10.14	9.52	7.33	69.77	3.05	0.34	0.68
23.23	10.06	9.42	7.36	69.31	3.05	0.33	0.67
23.34	9.96	9.28	7.38	68.49	3.06	0.32	0.66
23.37	9.83	9.14	7.40	67.61	3.06	0.31	0.65
23.44	9.70	8.98	7.42	66.58	3.06	0.30	0.64
23.54	9.51	8.75	7.46	65.30	3.06	0.29	0.62
23.60	9.31	8.52	7.51	64.01	3.07	0.27	0.61
23.64	9.08	8.27	7.58	62.70	3.07	0.26	0.59
23.71	8.86	8.01	7.64	61.22	3.08	0.24	0.57
23.79	8.59	7.72	7.74	59.70	3.08	0.22	0.55
23.84	8.38	7.48	7.79	58.28	3.09	0.21	0.53
23.89	8.28	7.37	7.79	57.37	3.09	0.20	0.53
23.99	8.23	7.29	7.80	56.92	3.09	0.18	0.52
24.03	8.16	7.20	7.96	57.36	3.10	0.17	0.51
24.10	8.16	7.20	8.10	58.28	3.11	0.17	0.51
24.18	8.37	7.40	8.04	59.50	3.11	0.19	0.53
24.23	8.74	7.77	7.83	60.88	3.09	0.22	0.56
24.31	9.13	8.17	7.62	62.20	3.07	0.28	0.58
24.36	9.53	8.57	7.42	63.60	3.06	0.30	0.61
24.45	9.75	8.78	7.41	65.00	3.06	0.31	0.63
24.49	9.88	8.90	7.43	66.16	3.06	0.31	0.64
24.57	9.92	8.92	7.48	66.74	3.06	0.29	0.64
24.61	10.03	9.03	7.42	66.94	3.06	0.29	0.64
24.69	10.16	9.14	7.38	67.43	3.06	0.30	0.65
24.74	10.29	9.26	7.41	68.63	3.06	0.30	0.66
24.82	10.59	9.55	7.42	70.88	3.06	0.68	0.68
24.89	11.03	9.99	7.36	73.55	3.05	0.71	0.71
24.94	11.56	10.52	7.21	75.87	3.04	0.75	0.75
25.01	12.05	11.00	7.02	77.20	3.02	0.79	0.79
25.09	12.40	11.33	6.86	77.76	3.01	0.81	0.81
25.13	12.40	11.32	6.84	77.46	3.01	0.81	0.81
25.22	12.27	11.16	6.88	76.77	3.01	0.80	0.80

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
25.28	12.04	10.90	6.91	75.36	3.02	0.78	0.78
25.34	11.57	10.40	7.02	73.08	3.02	0.74	0.74
25.44	10.81	9.60	7.24	69.50	3.04	0.24	0.69
25.48	9.88	8.64	7.59	65.59	3.07	0.22	0.62
25.53	8.92	7.65	8.01	61.35	3.11	0.19	0.55
25.59	8.18	6.88	8.47	58.29	3.14	0.18	0.49
25.68	7.57	6.25	9.02	56.35	3.18	0.17	0.45
25.73	7.56	6.23	9.18	57.21	3.20	0.19	0.45
25.79	7.85	6.51	8.88	57.85	3.17	0.16	0.47
25.88	8.49	7.15	8.25	58.97	3.13	0.20	0.51
25.93	9.38	8.03	7.52	60.40	3.07	0.23	0.57
25.99	10.48	9.12	6.84	62.43	3.01	0.32	0.65
26.08	11.74	10.37	6.21	64.43	2.95	0.26	0.74
26.14	12.92	11.53	5.80	66.84	2.91	0.26	0.82
26.19	13.96	12.54	5.48	68.72	2.88	0.28	0.90
26.28	14.97	13.52	5.17	69.87	2.84	0.34	0.97
26.34	15.73	14.24	4.93	70.17	2.82	1.02	1.02
26.39	16.16	14.65	4.86	71.17	2.81	1.05	1.05
26.45	16.25	14.72	4.91	72.27	2.81	1.05	1.05
26.53	16.18	14.62	5.01	73.29	2.83	1.05	1.05
26.58	16.05	14.48	5.13	74.34	2.84	1.04	1.04
26.68	15.79	14.19	5.31	75.29	2.86	1.02	1.02
26.73	15.60	13.99	5.44	76.13	2.87	1.00	1.00
26.78	15.54	13.91	5.56	77.37	2.89	0.99	0.99
26.88	15.47	13.80	5.75	79.32	2.91	0.99	0.99
26.93	15.41	13.73	5.93	81.33	2.92	0.98	0.98
26.98	15.48	13.78	6.04	83.25	2.93	0.98	0.98
27.04	15.59	13.87	6.14	85.19	2.94	0.99	0.99
27.13	15.68	13.92	6.25	86.96	2.95	0.99	0.99
27.22	15.61	13.82	6.39	88.26	2.97	0.99	0.99
27.24	15.48	13.68	6.52	89.16	2.98	0.98	0.98
27.33	15.33	13.50	6.64	89.67	2.99	0.96	0.96
27.37	15.08	13.24	6.78	89.80	3.00	0.95	0.95
27.43	14.77	12.92	6.92	89.38	3.02	0.92	0.92
27.52	14.46	12.58	7.06	88.85	3.03	0.90	0.90
27.57	14.10	12.22	7.21	88.05	3.04	0.87	0.87
27.63	13.68	11.79	7.35	86.71	3.05	0.84	0.84
27.72	13.24	11.33	7.51	85.09	3.07	0.81	0.81
27.76	12.84	10.93	7.62	83.26	3.07	0.78	0.78
27.84	12.46	10.54	7.72	81.35	3.08	0.75	0.75
27.93	12.10	10.17	7.82	79.56	3.09	0.73	0.73
27.97	11.82	9.89	7.87	77.87	3.10	0.71	0.71
28.02	11.70	9.75	7.82	76.27	3.09	0.70	0.70
28.12	11.66	9.69	7.70	74.61	3.08	0.69	0.69
28.17	11.67	9.68	7.58	73.40	3.07	0.69	0.69
28.23	11.80	9.79	7.45	72.95	3.06	0.70	0.70
28.32	12.03	9.99	7.31	73.01	3.05	0.71	0.71
28.37	12.28	10.22	7.19	73.44	3.04	0.73	0.73

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
28.42	12.60	10.51	7.07	74.28	3.03	0.75	0.75
28.48	12.97	10.84	6.95	75.36	3.02	0.77	0.77
28.57	13.52	11.33	6.75	76.48	3.00	0.81	0.81
28.61	14.02	11.79	6.59	77.67	2.99	0.84	0.84
28.69	14.48	12.21	6.45	78.81	2.97	0.87	0.87
28.77	14.97	12.64	6.31	79.74	2.96	0.90	0.90
28.83	15.40	13.03	6.16	80.28	2.95	0.93	0.93
28.88	15.75	13.34	6.04	80.59	2.93	0.95	0.95
28.97	16.12	13.65	5.92	80.85	2.92	0.97	0.97
29.02	16.58	14.07	5.77	81.19	2.91	1.00	1.00
29.08	17.07	14.50	5.62	81.51	2.89	1.04	1.04
29.17	17.42	14.80	5.54	81.91	2.88	1.06	1.06
29.21	16.68	14.09	5.89	82.99	2.92	1.01	1.01
29.28	17.35	14.69	5.73	84.17	2.90	1.05	1.05
29.37	18.08	15.34	5.58	85.65	2.89	1.10	1.10
29.41	18.84	16.03	5.45	87.42	2.87	1.14	1.14
29.47	19.66	16.76	5.31	88.96	2.86	1.20	1.20
29.56	20.44	17.45	5.14	89.65	2.84	1.25	1.25
29.62	21.08	18.02	4.99	89.89	2.82	1.29	1.29
29.68	21.55	18.43	4.86	89.53	2.81	1.31	1.31
29.76	21.98	18.79	4.72	88.74	2.79	1.34	1.34
29.83	23.16	19.85	4.38	86.86	2.75	1.42	1.42
29.87	22.72	19.43	4.36	84.78	2.75	1.38	1.38
29.96	22.10	18.81	4.37	82.22	2.75	1.34	1.34
30.01	21.54	18.28	4.34	79.33	2.75	1.30	1.30
30.07	20.81	17.58	4.36	76.65	2.75	1.25	1.25
30.16	20.20	16.98	4.41	74.98	2.76	1.21	1.21
30.20	19.65	16.47	4.48	73.79	2.76	1.17	1.17
30.27	19.26	16.07	4.56	73.29	2.77	1.15	1.15
30.34	18.94	15.75	4.66	73.36	2.78	1.12	1.12
30.42	18.95	15.73	4.70	73.99	2.79	1.12	1.12
30.46	19.17	15.91	4.72	75.17	2.79	1.13	1.13
30.52	19.53	16.22	4.72	76.59	2.79	1.16	1.16
30.58	19.82	16.46	4.75	78.24	2.80	1.17	1.17
30.66	20.28	16.84	4.74	79.86	2.79	1.20	1.20
30.71	20.64	17.15	4.74	81.34	2.80	1.22	1.22
30.81	20.94	17.37	4.76	82.69	2.80	1.24	1.24
30.87	21.17	17.56	4.78	83.92	2.80	1.25	1.25
30.91	21.30	17.66	4.82	85.10	2.80	1.26	1.26
31.01	21.41	17.71	4.87	86.23	2.81	1.26	1.26
31.06	21.53	17.80	4.91	87.37	2.81	1.27	1.27
31.11	21.63	17.86	4.95	88.36	2.82	1.27	1.27
31.19	21.81	17.99	4.96	89.14	2.82	1.28	1.28
31.26	21.98	18.11	4.96	89.73	2.82	1.29	1.29
31.35	22.12	18.19	4.96	90.16	2.82	1.30	1.30
31.37	22.15	18.20	4.98	90.62	2.82	1.30	1.30
31.46	22.28	18.27	4.97	90.91	2.82	1.30	1.30
31.55	22.33	18.28	4.98	91.09	2.82	1.30	1.30

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
31.59	22.49	18.41	4.94	91.01	2.82	1.31	1.31
31.66	22.71	18.58	4.87	90.48	2.81	1.32	1.32
31.70	23.00	18.82	4.77	89.81	2.80	1.34	1.34
31.79	23.13	18.90	4.72	89.15	2.79	1.34	1.34
31.86	23.24	18.96	4.67	88.51	2.79	1.35	1.35
31.91	23.55	19.22	4.60	88.37	2.78	1.37	1.37
31.99	24.39	19.93	4.47	89.06	2.76	1.42	1.42
32.06	25.44	20.82	4.34	90.39	2.75	1.48	1.48
32.10	26.88	22.09	4.18	92.23	2.72	1.57	1.57
32.20	28.15	23.16	4.10	94.85	2.71	1.64	1.64
32.26	28.72	23.62	4.16	98.16	2.72	1.67	1.67
32.30	29.57	24.34	4.18	101.69	2.72	1.73	1.73
32.35	30.28	24.92	4.22	105.09	2.73	1.77	1.77
32.46	31.21	25.67	4.21	108.18	2.73	1.82	1.82
32.49	31.95	26.29	4.23	111.21	2.73	1.86	1.86
32.58	32.77	26.95	4.21	113.53	2.73	1.91	1.91
32.62	34.34	28.30	4.10	116.05	2.71	2.00	2.00
32.69	36.23	29.91	3.99	119.21	2.70	2.12	2.12
32.78	38.18	31.55	3.88	122.28	2.68	2.23	2.23
32.82	40.40	33.46	3.75	125.60	2.67	2.37	2.37
32.89	41.76	34.59	3.73	129.05	2.66	2.44	2.44
32.98	43.04	35.63	3.71	132.21	2.66	2.52	2.52
33.02	43.56	36.03	3.75	135.06	2.67	2.54	2.54
33.08	43.60	36.00	3.79	136.47	2.67	2.54	2.54
33.18	42.94	35.32	3.89	137.25	2.68	2.50	2.50
33.21	41.11	33.69	4.07	137.02	2.71	2.38	2.38
33.29	38.50	31.35	4.31	135.03	2.74	2.22	2.22
33.37	35.87	29.01	4.52	131.27	2.77	2.06	2.06
33.42	33.58	27.00	4.67	126.23	2.79	1.92	1.92
33.47	31.71	25.36	4.74	120.24	2.79	1.80	1.80
33.53	29.91	23.80	4.78	113.67	2.80	1.69	1.69
33.62	28.55	22.60	4.74	107.22	2.80	1.60	1.60
33.67	27.44	21.64	4.71	101.83	2.79	1.53	1.53
33.73	26.35	20.68	4.68	96.75	2.79	1.47	1.47
33.82	25.32	19.78	4.66	92.18	2.79	1.40	1.40
33.87	24.46	19.03	4.65	88.49	2.78	1.35	1.35
33.93	23.71	18.37	4.70	86.36	2.79	1.30	1.30
34.02	23.04	17.75	4.78	84.94	2.80	1.26	1.26
34.06	22.45	17.24	4.89	84.26	2.81	1.22	1.22
34.13	22.07	16.88	4.99	84.31	2.82	1.20	1.20
34.22	21.81	16.62	5.09	84.59	2.83	1.18	1.18
34.26	21.71	16.52	5.16	85.19	2.84	1.17	1.17
34.32	21.73	16.50	5.20	85.88	2.85	1.17	1.17
34.42	21.79	16.51	5.24	86.45	2.85	1.17	1.17
34.46	21.86	16.55	5.25	86.87	2.85	1.18	1.18
34.52	21.87	16.54	5.27	87.08	2.85	1.18	1.18
34.61	21.89	16.52	5.28	87.14	2.86	1.17	1.17
34.70	21.91	16.50	5.28	87.14	2.86	1.17	1.17

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
34.76	22.00	16.55	5.27	87.27	2.86	1.18	1.18
34.82	22.08	16.59	5.26	87.34	2.85	1.18	1.18
34.86	22.20	16.68	5.23	87.15	2.85	1.18	1.18
34.92	22.38	16.80	5.21	87.52	2.85	1.19	1.19
35.02	22.61	16.95	5.21	88.35	2.85	1.20	1.20
35.06	22.92	17.19	5.21	89.58	2.85	1.22	1.22
35.11	23.26	17.45	5.22	91.14	2.85	1.24	1.24
35.19	23.32	17.45	5.32	92.89	2.86	1.24	1.24
35.25	23.48	17.55	5.39	94.66	2.87	1.25	1.25
35.31	23.92	17.88	5.39	96.33	2.87	1.27	1.27
35.40	24.41	18.24	5.39	98.39	2.87	1.30	1.30
35.45	24.90	18.61	5.42	100.88	2.87	1.32	1.32
35.50	25.37	18.97	5.44	103.26	2.87	1.35	1.35
35.56	25.84	19.32	5.45	105.30	2.87	1.37	1.37
35.64	26.20	19.57	5.48	107.20	2.88	1.39	1.39
35.72	26.53	19.80	5.50	108.86	2.88	1.41	1.41
35.81	27.10	20.22	5.44	110.03	2.87	1.44	1.44
35.85	27.52	20.55	5.40	110.86	2.87	1.46	1.46
35.90	27.57	20.56	5.41	111.30	2.87	1.46	1.46
35.96	27.50	20.47	5.43	111.25	2.87	1.45	1.45
36.04	27.44	20.38	5.44	110.83	2.87	1.45	1.45
36.11	27.37	20.29	5.42	110.01	2.87	1.44	1.44
36.16	27.38	20.28	5.37	108.99	2.87	1.44	1.44
36.25	27.49	20.34	5.30	107.76	2.86	1.44	1.44
36.31	27.53	20.35	5.23	106.50	2.85	1.44	1.44
36.36	27.55	20.34	5.20	105.82	2.85	1.44	1.44
36.44	27.59	20.34	5.19	105.48	2.85	1.44	1.44
36.50	27.55	20.28	5.20	105.38	2.85	1.44	1.44
36.56	27.51	20.22	5.20	105.22	2.85	1.43	1.43
36.65	27.46	20.13	5.22	104.99	2.85	1.43	1.43
36.68	27.32	20.00	5.24	104.73	2.85	1.42	1.42
36.76	26.99	19.70	5.30	104.31	2.86	1.40	1.40
36.84	26.59	19.33	5.36	103.68	2.87	1.37	1.37
36.91	26.14	18.94	5.43	102.81	2.87	1.34	1.34
36.96	25.72	18.58	5.46	101.52	2.88	1.32	1.32
37.04	25.31	18.22	5.48	99.92	2.88	1.29	1.29
37.10	25.01	17.96	5.47	98.29	2.88	1.28	1.28
37.15	24.79	17.78	5.44	96.70	2.87	1.26	1.26
37.23	24.57	17.57	5.41	95.11	2.87	1.25	1.25
37.30	24.39	17.41	5.38	93.56	2.87	1.24	1.24
37.35	24.27	17.30	5.33	92.22	2.86	1.23	1.23
37.45	24.09	17.12	5.31	90.90	2.86	1.21	1.21
37.51	23.91	16.96	5.29	89.72	2.86	1.20	1.20
37.55	23.68	16.77	5.28	88.48	2.86	1.19	1.19
37.62	23.41	16.54	5.27	87.10	2.85	1.17	1.17
37.70	23.18	16.33	5.25	85.68	2.85	1.16	1.16
37.75	22.99	16.17	5.21	84.25	2.85	1.15	1.15
37.80	22.83	16.04	5.16	82.80	2.84	1.14	1.14

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
37.90	22.79	15.98	5.09	81.34	2.84	1.13	1.13
37.95	22.85	16.02	4.99	79.99	2.82	1.13	1.13
38.05	23.13	16.22	4.89	79.28	2.81	1.15	1.15
38.06	23.67	16.66	4.74	79.02	2.80	1.18	1.18
38.15	24.36	17.18	4.61	79.14	2.78	1.21	1.21
38.19	25.07	17.73	4.50	79.75	2.77	1.25	1.25
38.27	25.90	18.37	4.38	80.47	2.75	1.29	1.29
38.34	26.81	19.07	4.27	81.37	2.74	1.34	1.34
38.39	27.68	19.75	4.17	82.26	2.72	1.38	1.38
38.46	28.48	20.35	4.10	83.39	2.71	1.42	1.42
38.55	29.24	20.90	4.06	84.87	2.71	1.46	1.46
38.59	30.19	21.63	4.01	86.82	2.70	1.51	1.51
38.68	31.64	22.72	3.94	89.49	2.69	1.59	1.59
38.75	33.31	24.00	3.85	92.51	2.68	1.67	1.67
38.80	35.48	25.68	3.74	96.14	2.66	1.79	1.79
38.87	38.37	27.93	3.58	99.97	2.64	1.94	1.94
38.95	41.80	30.61	3.40	104.15	2.61	2.12	2.12
38.99	45.31	33.36	3.24	108.24	2.59	0.68	0.68
39.04	48.34	35.74	3.13	111.69	2.57	0.69	0.69
39.11	49.97	36.96	3.09	114.37	2.56	0.70	0.70
39.19	50.69	37.46	3.08	115.54	2.56	0.70	0.70
39.27	49.95	36.81	3.12	114.99	2.57	0.70	0.70
39.33	48.64	35.72	3.18	113.58	2.58	0.69	0.69
39.39	46.71	34.16	3.24	110.84	2.59	0.69	0.69
39.45	43.93	31.94	3.36	107.28	2.61	2.21	2.21
39.53	40.53	29.21	3.53	103.00	2.63	2.03	2.03
39.57	37.19	26.57	3.71	98.52	2.66	1.85	1.85
39.64	34.51	24.46	3.83	93.75	2.68	1.70	1.70
39.72	33.37	23.58	3.77	88.79	2.67	1.64	1.64
39.79	32.93	23.26	3.63	84.39	2.65	1.61	1.61
39.84	33.06	23.39	3.47	81.26	2.62	1.62	1.62
39.93	32.94	23.28	3.41	79.39	2.61	1.61	1.61
39.98	32.75	23.12	3.42	79.04	2.61	1.60	1.60
40.05	32.95	23.19	3.56	82.51	2.64	1.61	1.61
40.09	34.03	23.95	3.64	87.20	2.65	1.66	1.66
40.19	36.38	25.69	3.60	92.47	2.64	1.78	1.78
40.23	40.72	29.01	3.42	99.16	2.61	2.00	2.00
40.34	45.86	32.90	3.25	106.95	2.59	0.68	0.68
40.38	50.76	36.64	3.14	115.13	2.57	0.70	0.70
40.43	55.28	40.05	3.08	123.53	2.56	0.71	0.71
40.50	60.00	43.62	3.01	131.16	2.55	0.72	0.72
40.58	64.51	47.00	2.94	138.27	2.53	0.73	0.73
40.63	68.60	50.12	2.86	143.45	2.52	0.73	0.73
40.70	72.71	53.23	2.78	147.92	2.50	0.74	0.74
40.75	76.10	55.80	2.72	151.94	2.49	0.75	0.75
40.84	77.61	56.84	2.73	155.10	2.49	0.75	0.75
40.88	77.99	57.03	2.77	157.83	2.50	0.75	0.75
40.95	78.42	57.23	2.80	160.06	2.51	0.75	0.75

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
41.03	79.84	58.24	2.77	161.34	2.50	0.75	0.75
41.08	83.51	61.08	2.66	162.46	2.48	0.76	0.76
41.15	90.15	66.29	2.46	162.81	2.43	0.77	0.77
41.23	97.84	72.34	2.26	163.56	2.39	0.78	0.78
41.28	105.13	78.11	2.11	164.99	2.35	0.79	0.79
41.35	112.60	84.00	1.99	166.99	2.31	0.80	0.80
41.43	119.65	89.52	1.89	169.57	2.28	0.81	0.81
41.48	126.18	94.65	1.83	172.95	2.26	0.82	0.82
41.54	132.64	99.67	1.78	177.10	2.24	0.83	0.83
41.62	138.98	104.52	1.74	181.95	2.23	0.83	0.83
41.68	144.15	108.42	1.73	187.16	2.22	0.84	0.84
41.77	147.16	110.47	1.74	192.21	2.23	0.84	0.84
41.82	149.61	112.16	1.76	197.02	2.23	0.84	0.84
41.88	151.40	113.31	1.77	201.11	2.24	0.84	0.84
41.97	152.19	113.59	1.80	204.50	2.25	0.85	0.85
42.01	152.63	113.73	1.82	207.46	2.26	0.85	0.85
42.10	154.18	114.69	1.83	209.53	2.26	0.85	0.85
42.17	155.77	115.77	1.82	210.77	2.26	0.85	0.85
42.22	158.63	117.95	1.79	211.47	2.25	0.85	0.85
42.28	161.62	120.26	1.76	211.30	2.24	0.85	0.85
42.33	166.19	123.89	1.70	210.96	2.21	0.86	0.86
42.41	171.05	127.73	1.65	210.27	2.19	0.86	0.86
42.48	177.06	132.54	1.58	209.92	2.16	0.87	0.87
42.52	184.41	138.54	1.52	210.20	2.13	0.87	0.87
42.60	193.18	145.64	1.45	211.30	2.10	0.88	0.88
42.66	201.80	152.67	1.39	212.90	2.06	0.89	0.89
42.72	210.25	159.58	1.35	214.88	2.03	0.90	0.90
42.81	216.71	164.80	1.31	216.24	2.01	0.90	0.90
42.87	221.45	168.71	1.29	216.83	1.99	0.90	0.90
42.92	223.43	170.44	1.27	215.65	1.97	0.91	0.91
43.00	224.17	171.11	1.25	213.60	1.96	0.91	0.91
43.06	223.07	170.33	1.24	210.56	1.95	0.90	0.90
43.11	220.03	167.97	1.23	206.67	1.94	0.90	0.90
43.18	215.77	164.56	1.23	202.06	1.94	0.90	0.90
43.25	211.23	160.89	1.23	197.51	1.94	0.90	0.90
43.31	206.82	157.31	1.23	193.43	1.94	0.89	0.89
43.39	202.67	153.89	1.23	189.65	1.94	0.89	0.89
43.45	198.48	150.43	1.24	186.27	1.95	0.89	0.89
43.51	194.71	147.19	1.25	184.09	1.96	0.88	0.88
43.61	191.33	144.12	1.27	182.63	1.97	0.88	0.88
43.65	188.25	141.41	1.29	181.84	1.99	0.88	0.88
43.72	185.35	138.80	1.30	180.92	2.00	0.87	0.87
43.81	182.33	136.09	1.32	179.83	2.02	0.87	0.87
43.85	178.70	133.02	1.34	178.27	2.03	0.87	0.87
43.92	174.04	129.13	1.36	175.71	2.04	0.86	0.86
44.01	169.31	125.14	1.38	173.09	2.06	0.86	0.86
44.05	165.21	121.88	1.39	169.93	2.06	0.86	0.86
44.10	160.81	118.50	1.39	165.15	2.06	0.85	0.85

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
44.20	156.04	114.74	1.40	160.07	2.07	0.85	0.85
44.25	151.36	111.13	1.40	155.35	2.07	0.84	0.84
44.30	146.31	107.16	1.41	151.20	2.07	0.84	0.84
44.40	140.34	102.33	1.44	147.25	2.09	0.83	0.83
44.45	134.81	97.92	1.47	143.99	2.11	0.82	0.82
44.50	130.12	94.11	1.51	142.03	2.13	0.82	0.82
44.57	125.26	90.13	1.56	140.34	2.15	0.81	0.81
44.63	120.31	86.02	1.63	140.23	2.18	0.81	0.81
44.69	115.72	82.08	1.74	143.01	2.23	0.80	0.80
44.79	111.51	78.40	1.87	146.54	2.27	0.79	0.79
44.84	107.77	75.21	2.00	150.25	2.31	0.79	0.79
44.89	105.00	72.83	2.11	153.52	2.35	0.78	0.78
44.96	103.51	71.48	2.18	156.05	2.37	0.78	0.78
45.04	102.01	70.14	2.26	158.16	2.39	0.78	0.78
45.09	100.81	69.09	2.31	159.67	2.40	0.78	0.78
45.17	100.05	68.35	2.35	160.93	2.41	0.78	0.78
45.24	99.52	67.81	2.39	162.05	2.42	0.77	0.77
45.28	99.27	67.55	2.41	162.52	2.42	0.77	0.77
45.38	98.85	67.10	2.42	162.58	2.43	0.77	0.77
45.42	97.77	66.22	2.46	162.63	2.43	0.77	0.77
45.49	96.34	65.05	2.50	162.56	2.44	0.77	0.77
45.57	94.70	63.72	2.55	162.28	2.45	0.77	0.77
45.63	92.37	61.92	2.61	161.36	2.47	0.76	0.76
45.69	89.46	59.74	2.66	159.12	2.48	0.76	0.76
45.78	85.19	56.57	2.75	155.40	2.50	0.75	0.75
45.84	79.80	52.64	2.87	150.88	2.52	0.74	0.74
45.89	73.90	48.37	3.01	145.76	2.55	0.73	0.73
45.93	67.39	43.71	3.19	139.53	2.58	0.72	0.72
46.02	61.02	39.17	3.38	132.47	2.61	2.66	2.66
46.08	54.84	34.81	3.59	124.90	2.64	2.37	2.37
46.13	48.82	30.61	3.82	116.87	2.68	2.10	2.10
46.22	43.62	27.00	4.03	108.93	2.71	1.86	1.86
46.28	39.06	23.85	4.28	101.99	2.74	1.65	1.65
46.33	35.80	21.61	4.47	96.55	2.76	1.50	1.50
46.43	33.77	20.22	4.54	91.86	2.77	1.41	1.41
46.47	32.28	19.23	4.57	87.81	2.77	1.34	1.34
46.53	31.55	18.75	4.53	85.02	2.77	1.30	1.30
46.63	31.27	18.56	4.46	82.79	2.76	1.29	1.29
46.67	31.09	18.45	4.39	81.06	2.75	1.28	1.28
46.73	31.01	18.39	4.37	80.34	2.75	1.27	1.27
46.83	31.04	18.38	4.35	80.02	2.75	1.27	1.27
46.87	31.05	18.38	4.35	79.94	2.75	1.27	1.27
46.93	31.18	18.45	4.34	80.00	2.75	1.28	1.28
47.02	31.31	18.51	4.32	79.99	2.74	1.28	1.28
47.08	31.45	18.58	4.30	79.99	2.74	1.28	1.28
47.12	31.65	18.71	4.30	80.42	2.74	1.29	1.29
47.18	31.90	18.85	4.30	80.99	2.74	1.30	1.30
47.27	32.12	18.96	4.30	81.54	2.74	1.31	1.31

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
47.31	32.24	19.01	4.33	82.39	2.74	1.31	1.31
47.39	32.73	19.30	4.32	83.31	2.74	1.33	1.33
47.48	33.47	19.76	4.28	84.52	2.74	1.36	1.36
47.52	34.18	20.22	4.25	85.98	2.73	1.39	1.39
47.59	34.88	20.63	4.28	88.32	2.74	1.42	1.42
47.66	35.57	21.01	4.35	91.45	2.75	1.45	1.45
47.74	36.36	21.47	4.39	94.26	2.75	1.48	1.48
47.79	37.63	22.28	4.34	96.75	2.75	1.54	1.54
47.86	39.62	23.59	4.20	98.98	2.73	1.62	1.62
47.94	42.38	25.46	3.96	100.78	2.69	1.74	1.74
47.99	46.45	28.27	3.63	102.50	2.65	1.92	1.92
48.05	51.69	31.91	3.27	104.31	2.59	0.68	0.68
48.13	57.43	35.93	2.96	106.37	2.54	0.69	0.69
48.19	63.46	40.18	2.70	108.40	2.49	0.71	0.71
48.26	69.35	44.33	2.50	111.00	2.44	0.72	0.72
48.34	74.27	47.76	2.39	114.21	2.42	0.73	0.73
48.39	78.06	50.36	2.34	117.60	2.41	0.74	0.74
48.43	80.01	51.62	2.34	120.87	2.41	0.74	0.74
48.51	80.23	51.58	2.40	123.65	2.42	0.74	0.74
48.58	78.15	49.87	2.53	126.20	2.45	0.73	0.73
48.63	73.91	46.66	2.76	128.57	2.50	0.73	0.73
48.72	69.19	43.12	3.03	130.53	2.55	0.72	0.72
48.78	64.53	39.71	3.33	132.10	2.60	0.71	0.71
48.83	60.65	36.92	3.59	132.69	2.64	2.50	2.50
48.90	58.27	35.18	3.78	133.00	2.67	2.40	2.40
48.99	56.81	34.10	3.90	133.10	2.69	2.33	2.33
49.03	57.34	34.43	3.88	133.52	2.68	2.35	2.35
49.08	59.70	36.02	3.73	134.25	2.66	2.45	2.45
49.17	64.88	39.55	3.43	135.60	2.62	2.67	2.67
49.23	73.51	45.55	3.01	136.90	2.54	0.72	0.72
49.32	85.21	53.79	2.58	138.53	2.46	0.74	0.74
49.35	97.81	62.84	2.24	140.98	2.38	0.76	0.76
49.43	111.56	72.74	1.99	144.42	2.31	0.78	0.78
49.50	126.07	83.33	1.78	148.53	2.24	0.80	0.80
49.58	140.81	94.14	1.63	153.61	2.19	0.82	0.82
49.63	155.36	104.93	1.52	159.57	2.13	0.83	0.83
49.72	169.50	115.38	1.44	166.05	2.09	0.85	0.85
49.78	181.49	124.33	1.38	171.86	2.06	0.86	0.86
49.83	190.73	131.20	1.35	176.75	2.03	0.87	0.87
49.90	196.54	135.41	1.33	180.17	2.02	0.87	0.87
49.98	200.97	138.54	1.32	182.84	2.01	0.87	0.87
50.02	203.65	140.45	1.31	184.55	2.01	0.88	0.88
50.08	205.02	141.54	1.30	184.09	2.00	0.88	0.88
50.18	205.97	142.29	1.29	183.07	1.99	0.88	0.88
50.23	206.42	142.77	1.27	181.88	1.98	0.88	0.88
50.27	206.67	143.11	1.26	180.71	1.97	0.88	0.88
50.36	206.82	143.25	1.25	179.58	1.96	0.88	0.88
50.40	206.95	143.47	1.25	178.63	1.95	0.88	0.88

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
50.47	207.35	143.80	1.24	177.89	1.95	0.88	0.88
50.55	207.82	144.14	1.23	177.42	1.94	0.88	0.88
50.63	208.28	144.42	1.23	177.15	1.94	0.88	0.88
50.67	208.58	144.31	1.24	178.43	1.95	0.88	0.88
50.72	208.67	143.92	1.25	180.14	1.96	0.88	0.88
50.83	208.48	143.22	1.27	181.54	1.97	0.88	0.88
50.88	208.04	142.49	1.28	182.79	1.99	0.88	0.88
50.93	207.42	141.67	1.30	183.75	2.00	0.88	0.88
51.02	206.85	140.84	1.31	184.53	2.01	0.88	0.88
51.08	206.30	140.13	1.32	185.17	2.02	0.88	0.88
51.12	205.82	139.57	1.33	185.58	2.02	0.88	0.88
51.21	205.38	138.99	1.34	185.59	2.03	0.87	0.87
51.27	205.16	138.70	1.34	185.41	2.03	0.87	0.87
51.32	205.10	138.60	1.33	185.01	2.03	0.87	0.87
51.39	205.14	138.54	1.33	184.61	2.02	0.87	0.87
51.47	205.24	138.49	1.33	184.27	2.02	0.87	0.87
51.55	205.31	138.40	1.33	184.07	2.02	0.87	0.87
51.60	205.08	138.14	1.33	183.84	2.02	0.87	0.87
51.67	204.64	137.67	1.33	183.52	2.02	0.87	0.87
51.72	203.58	136.81	1.34	182.68	2.03	0.87	0.87
51.79	201.52	135.28	1.34	180.62	2.03	0.87	0.87
51.87	199.01	133.36	1.34	178.56	2.03	0.87	0.87
51.91	196.40	131.39	1.35	176.81	2.03	0.87	0.87
51.98	192.80	128.68	1.35	174.31	2.04	0.86	0.86
52.06	188.34	125.28	1.37	171.51	2.05	0.86	0.86
52.12	183.88	122.00	1.38	168.38	2.06	0.86	0.86
52.17	178.11	117.70	1.40	165.18	2.07	0.85	0.85
52.26	170.61	112.01	1.44	161.59	2.09	0.84	0.84
52.31	163.90	106.94	1.49	159.09	2.12	0.84	0.84
52.38	156.13	101.00	1.56	157.10	2.15	0.83	0.83
52.47	147.15	94.26	1.64	154.49	2.19	0.82	0.82
52.51	136.09	86.23	1.75	150.95	2.23	0.81	0.81
52.56	124.42	77.83	1.89	147.40	2.28	0.79	0.79
52.66	112.90	69.62	2.06	143.68	2.33	0.78	0.78
52.70	100.48	60.93	2.30	140.39	2.40	0.76	0.76
52.77	89.16	53.15	2.57	136.45	2.46	0.74	0.74
52.87	79.44	46.57	2.82	131.31	2.51	0.73	0.73
52.92	69.32	39.89	3.15	125.70	2.57	0.71	0.71
52.97	61.28	34.64	3.48	120.40	2.62	2.32	2.32
53.02	54.61	30.38	3.78	114.68	2.67	2.05	2.05
53.10	50.06	27.50	3.97	109.11	2.70	1.87	1.87
53.16	46.90	25.55	4.07	104.01	2.71	1.74	1.74
53.22	44.28	23.98	4.11	98.54	2.72	1.63	1.63
53.31	42.65	23.03	4.05	93.26	2.71	1.57	1.57
53.36	41.31	22.29	3.97	88.37	2.70	1.51	1.51
53.42	40.10	21.59	3.91	84.45	2.69	1.46	1.46
53.51	39.07	21.00	3.85	80.92	2.68	1.42	1.42
53.56	37.95	20.34	3.83	77.90	2.68	1.37	1.37

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
53.62	37.07	19.81	3.83	75.92	2.68	1.34	1.34
53.71	36.24	19.28	3.86	74.43	2.68	1.30	1.30
53.75	35.58	18.87	3.88	73.33	2.68	1.28	1.28
53.83	34.88	18.39	3.98	73.18	2.70	1.25	1.25
53.91	34.05	17.84	4.09	72.99	2.71	1.21	1.21
53.98	33.09	17.20	4.22	72.61	2.73	1.17	1.17
54.01	32.19	16.62	4.35	72.23	2.75	1.14	1.14
54.11	31.08	15.89	4.51	71.62	2.77	1.09	1.09
54.15	29.90	15.16	4.66	70.59	2.78	1.05	1.05
54.21	28.55	14.31	4.85	69.38	2.81	0.34	0.99
54.27	27.04	13.38	5.05	67.57	2.83	0.31	0.93
54.35	25.56	12.48	5.24	65.45	2.85	0.28	0.87
54.42	24.28	11.72	5.38	63.06	2.87	0.25	0.82
54.46	23.20	11.09	5.48	60.75	2.88	0.22	0.78
54.55	22.43	10.64	5.50	58.58	2.88	0.19	0.75
54.60	21.80	10.29	5.51	56.66	2.88	0.17	0.72
54.67	21.40	10.06	5.46	54.95	2.88	0.16	0.71
54.74	21.06	9.87	5.43	53.59	2.87	0.16	0.69
54.79	20.77	9.71	5.41	52.57	2.87	0.15	0.68
54.86	20.62	9.62	5.40	51.96	2.87	0.15	0.68
54.96	20.50	9.54	5.41	51.56	2.87	0.15	0.67
55.03	20.43	9.49	5.41	51.32	2.87	0.15	0.67
55.06	20.38	9.46	5.41	51.16	2.87	0.15	0.66
55.14	20.37	9.44	5.40	51.00	2.87	0.15	0.66
55.21	20.35	9.42	5.40	50.83	2.87	0.15	0.66
55.25	20.31	9.39	5.39	50.67	2.87	0.15	0.66
55.32	20.28	9.37	5.39	50.50	2.87	0.15	0.66
55.41	20.24	9.33	5.39	50.33	2.87	0.14	0.65
55.45	20.23	9.32	5.39	50.24	2.87	0.14	0.65
55.52	20.23	9.31	5.39	50.23	2.87	0.13	0.65
55.61	20.28	9.33	5.39	50.28	2.87	0.13	0.65
55.65	20.52	9.45	5.38	50.89	2.87	0.13	0.66
55.71	20.91	9.67	5.35	51.70	2.86	0.14	0.68
55.80	21.44	9.96	5.29	52.64	2.86	0.14	0.70
55.86	22.21	10.40	5.17	53.78	2.84	0.15	0.73
55.95	23.00	10.84	5.08	55.07	2.83	0.19	0.75
56.00	23.79	11.29	5.00	56.40	2.82	0.20	0.78
56.05	24.57	11.73	4.92	57.75	2.82	0.21	0.81
56.11	25.39	12.21	4.79	58.54	2.80	0.22	0.84
56.20	26.17	12.67	4.65	58.93	2.78	0.23	0.87
56.24	26.73	13.01	4.52	58.82	2.77	0.24	0.89
56.31	27.09	13.23	4.43	58.66	2.76	0.25	0.91
56.39	27.14	13.26	4.40	58.31	2.75	0.21	0.91
56.43	26.89	13.11	4.41	57.80	2.75	0.19	0.90
56.50	26.19	12.68	4.49	56.98	2.77	0.18	0.87
56.60	25.50	12.25	4.57	56.00	2.77	0.19	0.84
56.66	24.81	11.85	4.62	54.73	2.78	0.18	0.81
56.70	24.10	11.42	4.72	53.84	2.79	0.17	0.79

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
56.79	23.44	11.01	4.83	53.20	2.81	0.16	0.76
56.84	22.85	10.64	4.96	52.77	2.82	0.16	0.74
56.92	22.40	10.36	5.08	52.61	2.83	0.15	0.72
56.99	22.25	10.25	5.14	52.66	2.84	0.14	0.71
57.03	22.42	10.34	5.12	52.94	2.84	0.14	0.72
57.09	23.22	10.80	4.97	53.70	2.82	0.15	0.75
57.18	23.98	11.23	4.87	54.70	2.81	0.17	0.78
57.23	24.85	11.71	4.83	56.60	2.81	0.18	0.81
57.31	26.05	12.34	4.84	59.70	2.81	0.19	0.85
57.38	27.50	13.12	4.83	63.35	2.81	0.22	0.91
57.43	29.89	14.46	4.68	67.68	2.79	0.24	1.00
57.50	33.85	16.75	4.35	72.85	2.75	1.14	1.14
57.58	38.94	19.76	3.94	77.84	2.69	1.33	1.33
57.62	45.95	24.03	3.45	82.77	2.62	1.59	1.59
57.68	53.93	28.96	3.04	88.00	2.55	0.67	0.67
57.78	62.67	34.40	2.71	93.09	2.49	0.69	0.69
57.82	72.41	40.59	2.42	98.14	2.43	0.71	0.71
57.89	82.22	46.92	2.19	102.62	2.37	0.73	0.73
57.97	91.68	53.07	2.01	106.91	2.32	0.74	0.74
58.02	99.77	58.36	1.90	110.82	2.28	0.75	0.75
58.09	105.22	61.89	1.84	113.73	2.26	0.76	0.76
58.17	108.62	64.01	1.81	116.09	2.26	0.77	0.77
58.23	109.72	64.57	1.83	117.85	2.26	0.77	0.77
58.28	109.49	64.23	1.86	119.20	2.27	0.77	0.77
58.37	108.18	63.12	1.91	120.41	2.29	0.76	0.76
58.43	105.44	61.09	1.98	121.15	2.31	0.76	0.76
58.48	100.57	57.67	2.10	121.32	2.35	0.75	0.75
58.57	95.05	53.81	2.26	121.56	2.39	0.74	0.74
58.62	88.67	49.47	2.46	121.83	2.44	0.73	0.73
58.67	82.27	45.20	2.69	121.69	2.48	0.72	0.72
58.78	76.27	41.23	2.94	121.38	2.53	0.71	0.71
58.82	69.93	37.13	3.25	120.73	2.59	0.70	0.70
58.88	63.59	33.12	3.61	119.62	2.64	2.20	2.20
58.97	57.66	29.45	3.98	117.21	2.70	1.98	1.98
59.01	52.33	26.22	4.37	114.63	2.75	1.79	1.79
59.07	48.78	24.09	4.66	112.37	2.79	1.66	1.66
59.12	45.34	22.06	4.97	109.61	2.82	1.53	1.53
59.19	42.74	20.56	5.17	106.39	2.84	1.43	1.43
59.27	41.35	19.78	5.22	103.23	2.85	1.38	1.38
59.32	39.96	19.01	5.27	100.24	2.86	1.33	1.33
59.42	39.47	18.76	5.22	97.90	2.85	1.31	1.31
59.47	38.99	18.52	5.16	95.59	2.84	1.29	1.29
59.52	38.64	18.33	5.14	94.16	2.84	1.28	1.28
59.58	38.47	18.26	5.07	92.55	2.83	1.27	1.27
59.68	38.20	18.11	5.03	91.05	2.83	1.26	1.26
59.74	38.28	18.16	4.98	90.38	2.82	1.26	1.26
59.78	38.65	18.53	4.60	85.25	2.78	1.27	1.27
59.88	38.74	18.73	4.29	80.36	2.74	1.27	1.27

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
59.93	39.33	19.26	3.91	75.24	2.69	1.29	1.29
60.00	40.82	20.43	3.39	69.20	2.61	0.63	1.34
60.05	43.76	22.60	2.77	62.70	2.50	0.11	0.64
60.13	46.96	25.08	2.24	56.21	2.38	0.08	0.65
60.18	46.63	25.36	1.96	49.61	2.30	0.06	0.65
60.25	48.94	27.71	1.00	27.71	2.15	0.03	0.66
60.33	54.14	-1.00	1.00	-1.00	-1.00	N/A	N/A
60.38	58.50	-1.00	1.00	-1.00	-1.00	N/A	N/A

Abbreviations

q_t:	Total cone resistance
K_c:	Cone resistance correction factor due to fines
$Q_{tn,cs}$:	Adjusted and corrected cone resistance due to fines
I_c:	Soil behavior type index
$S_{u(liq)}/\sigma'_v$:	Calculated liquefied undrained strength ratio
$S_{u(peak)}/\sigma'_v$:	Calculated peak undrained strength ratio

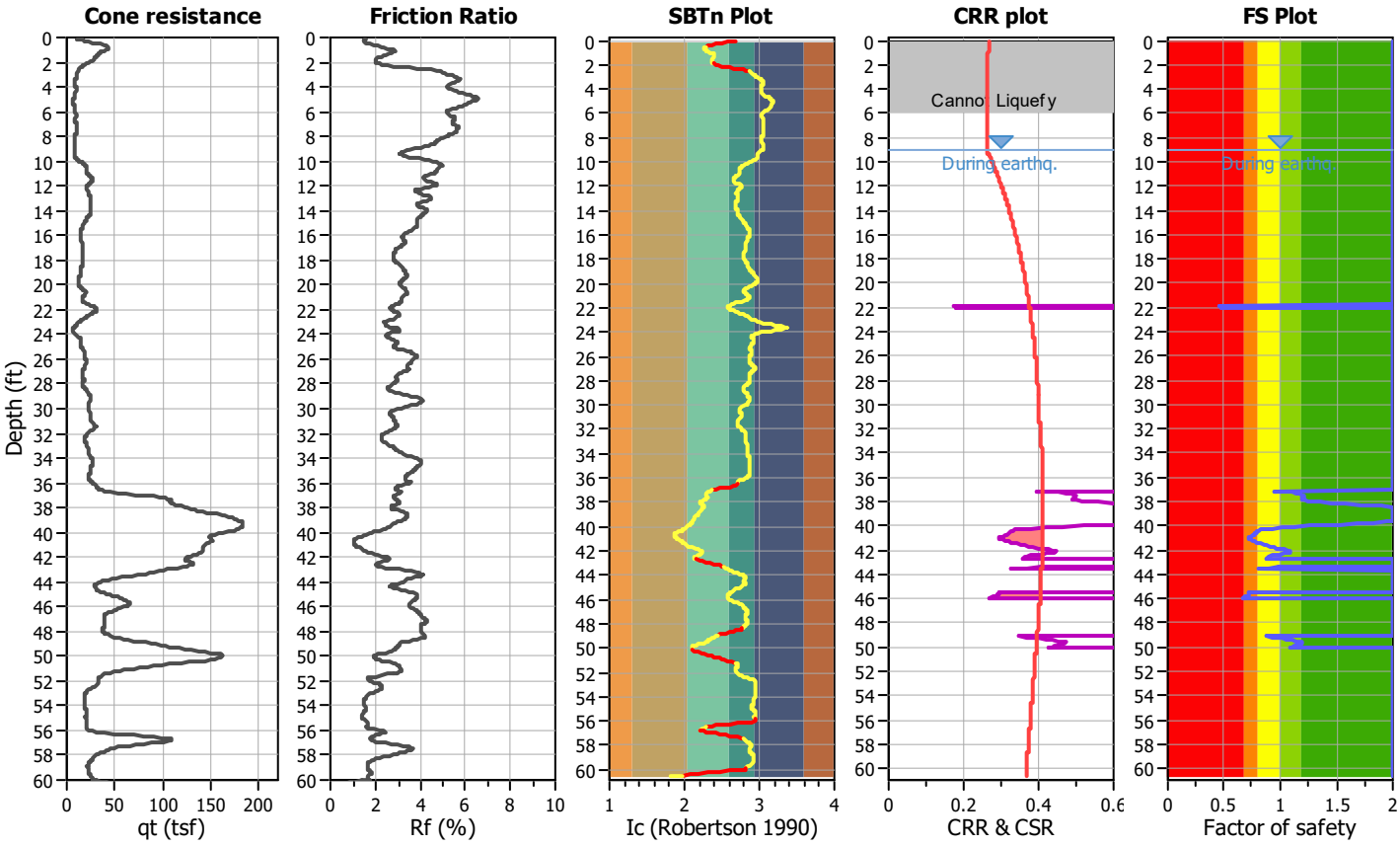
LIQUEFACTION ANALYSIS REPORT

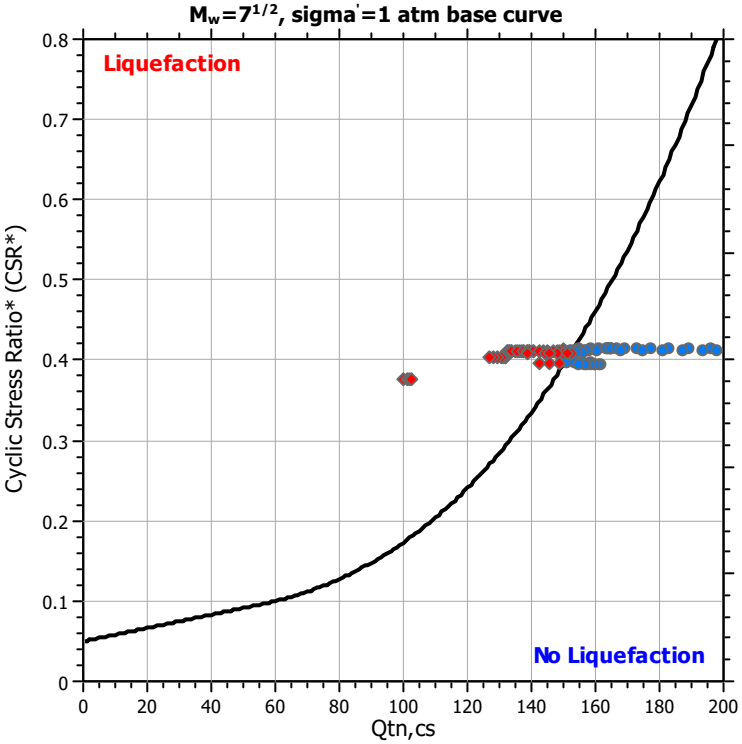
Project title : W1301-06-01 **Location : Perry Street**

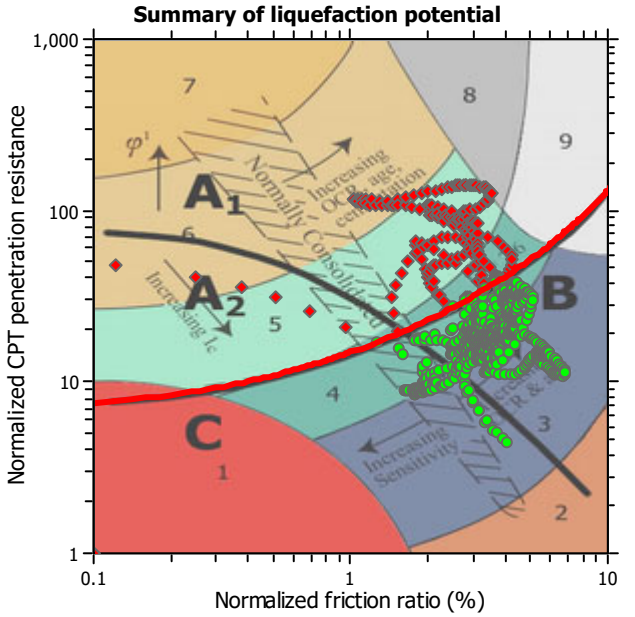
CPT file : CPT-3

Input parameters and analysis data

Analysis method:	NCEER (1998)	G.W.T. (in-situ):	12.00 ft	Use fill:	No	Clay like behavior applied:	Sands only
Fines correction method:	NCEER (1998)	G.W.T. (earthq.):	9.00 ft	Fill height:	N/A	Limit depth applied:	Yes
Points to test:	Based on Ic value	Average results interval:	.	Fill weight:	N/A	Limit depth:	50.00 ft
Earthquake magnitude M_w:	6.68	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	MSF method:	Method based
Peak ground acceleration:	0.55	Unit weight calculation:	Based on SBT	K_σ applied:	Yes		

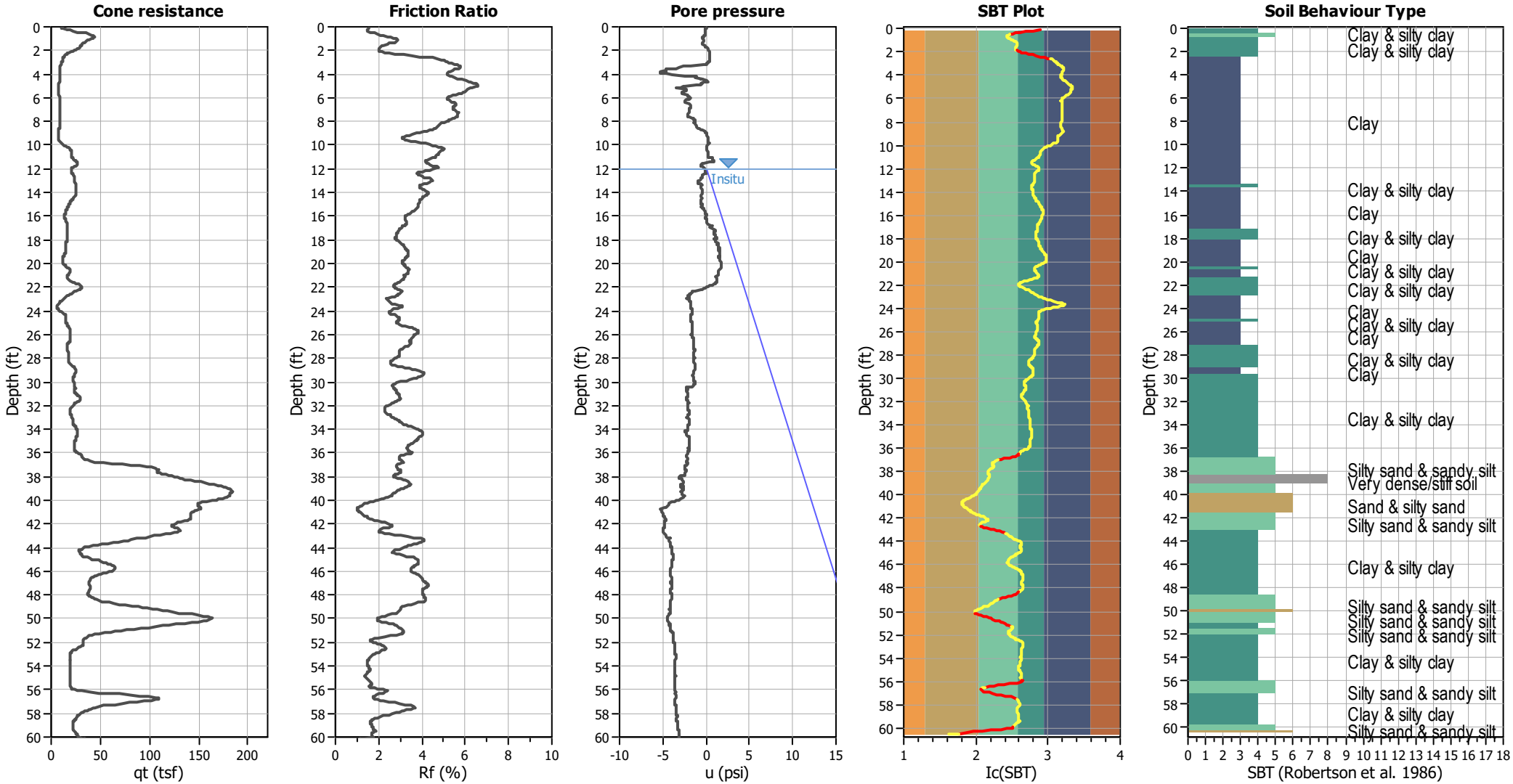






Zone A_1: Cyclic liquefaction likely depending on size and duration of cyclic loading
Zone A_2: Cyclic liquefaction and strength loss likely depending on loading and ground geometry
Zone B: Liquefaction and post-earthquake strength loss unlikely, check cyclic softening
Zone C: Cyclic liquefaction and strength loss possible depending on soil plasticity, brittleness/sensitivity, strain to peak undrained strength and ground geometry

CPT basic interpretation plots



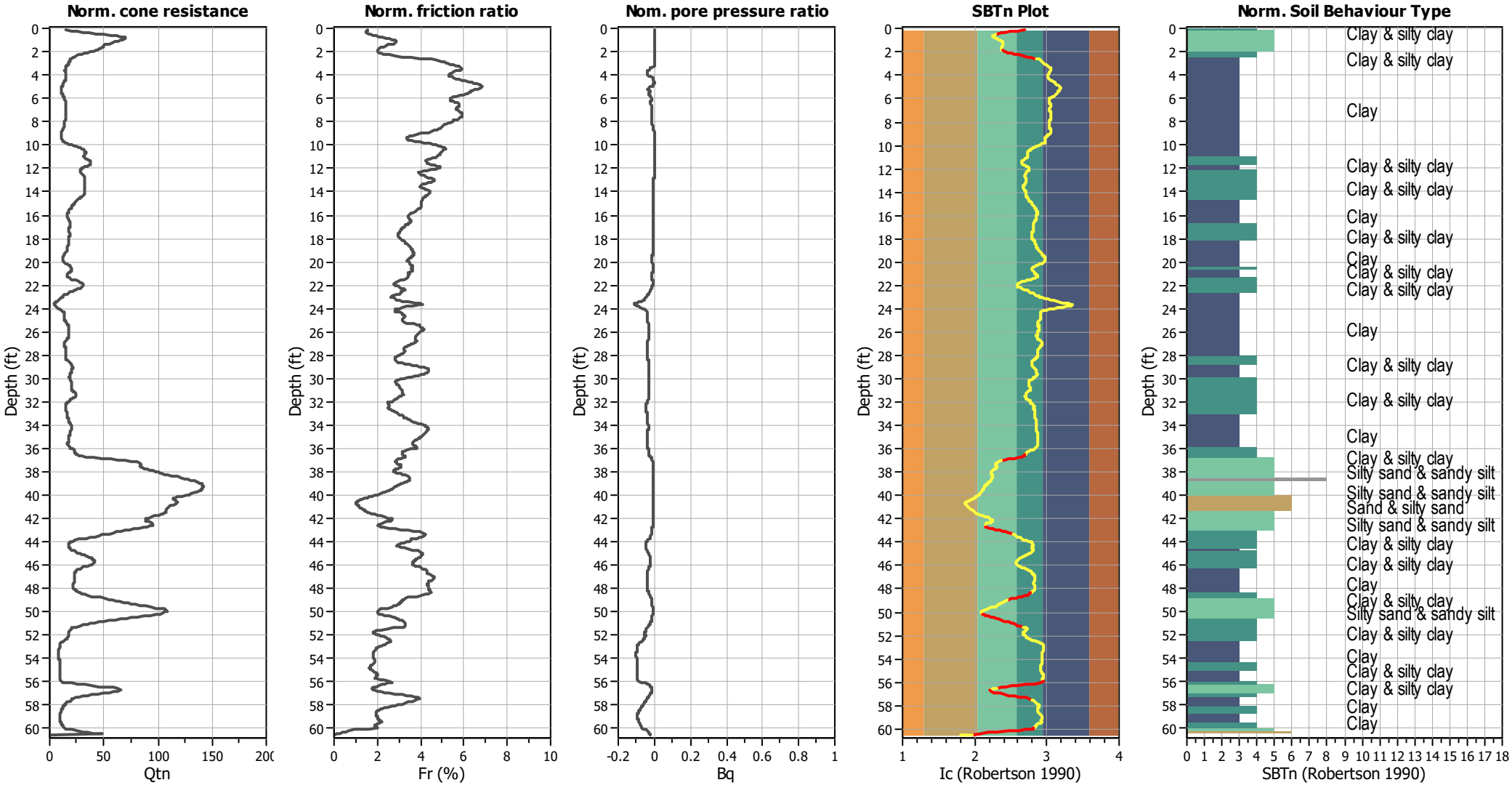
Input parameters and analysis data

Analysis method:	NCEER (1998)	Depth to water table (erthq.):	9.00 ft	Fill weight:	N/A
Fines correction method:	NCEER (1998)	Average results interval:	.	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.68	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.55	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	12.00 ft	Fill height:	N/A	Limit depth:	50.00 ft

SBT legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to
9. Very stiff fine grained

CPT basic interpretation plots (normalized)



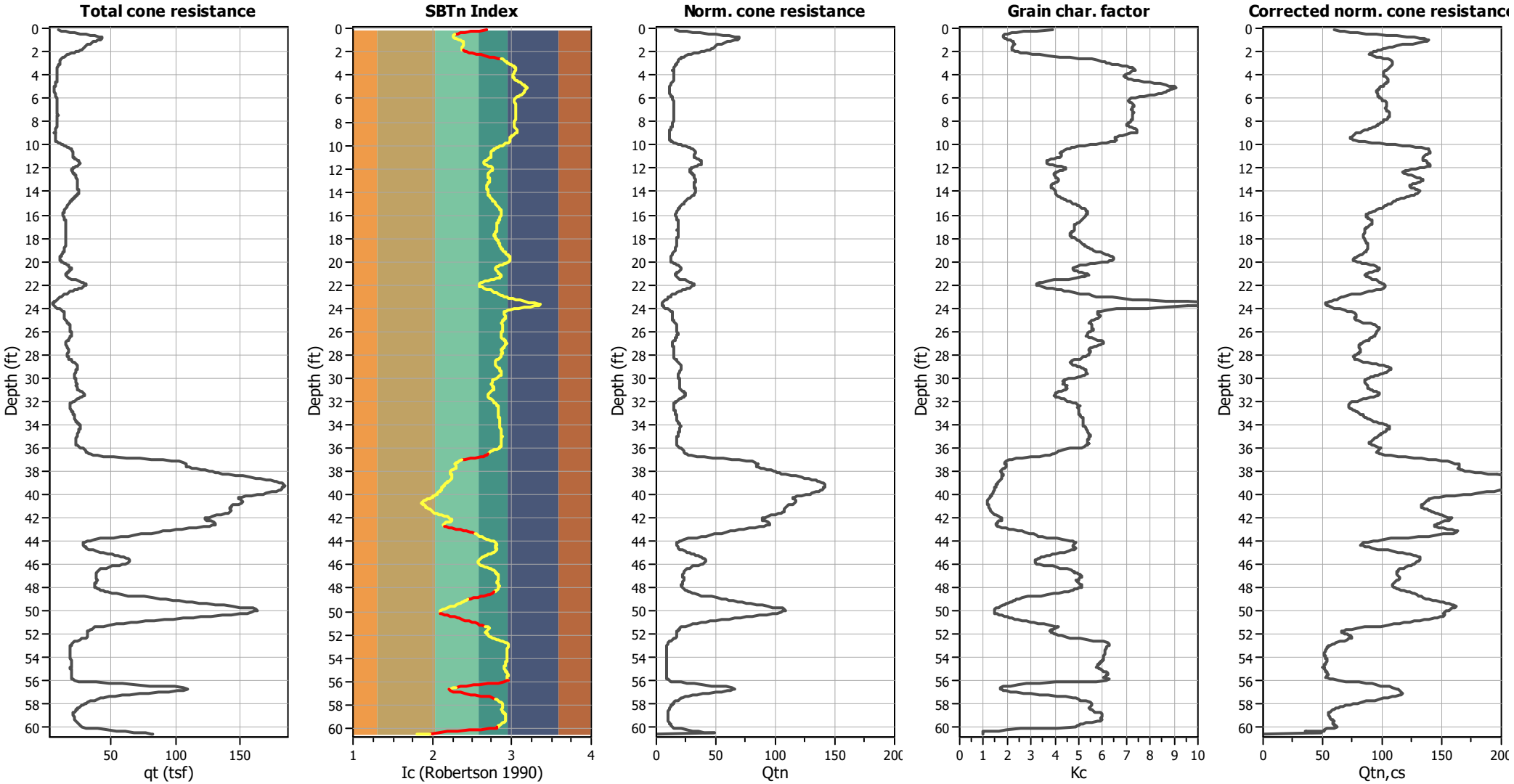
Input parameters and analysis data

Analysis method:	NCEER (1998)	Depth to water table (erthq.):	9.00 ft	Fill weight:	N/A
Fines correction method:	NCEER (1998)	Average results interval:	.	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.68	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.55	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	12.00 ft	Fill height:	N/A	Limit depth:	50.00 ft

SBTn legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to
9. Very stiff fine grained

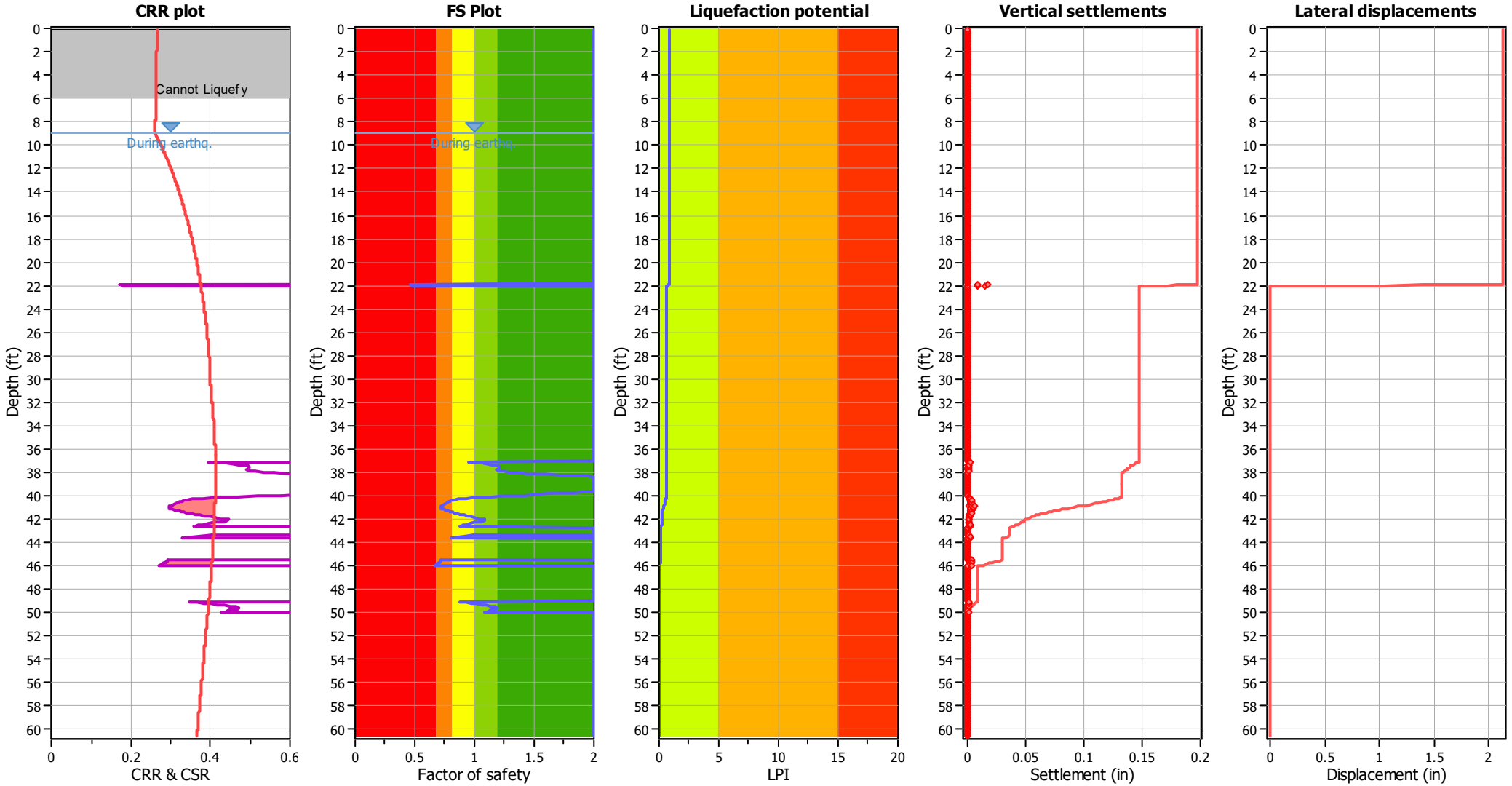
Liquefaction analysis overall plots (intermediate results)



Input parameters and analysis data

Analysis method:	NCEER (1998)	Depth to water table (erthq.):	9.00 ft	Fill weight:	N/A
Fines correction method:	NCEER (1998)	Average results interval:	.	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.68	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.55	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	12.00 ft	Fill height:	N/A	Limit depth:	50.00 ft

Liquefaction analysis overall plots



Input parameters and analysis data

Analysis method:	NCEER (1998)	Depth to water table (erthq.):	9.00 ft	Fill weight:	N/A
Fines correction method:	NCEER (1998)	Average results interval:	.	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.68	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.55	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	12.00 ft	Fill height:	N/A	Limit depth:	50.00 ft

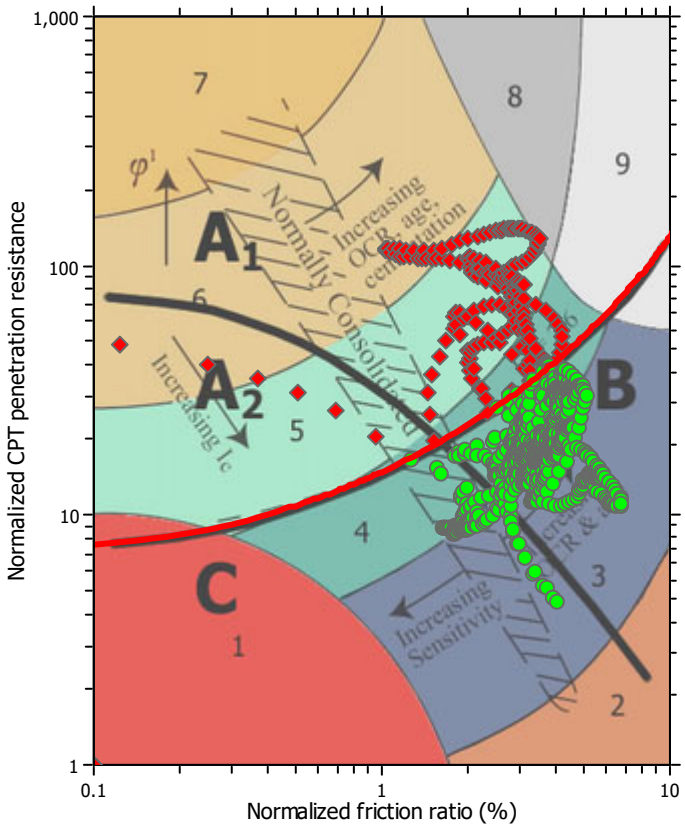
F.S. color scheme

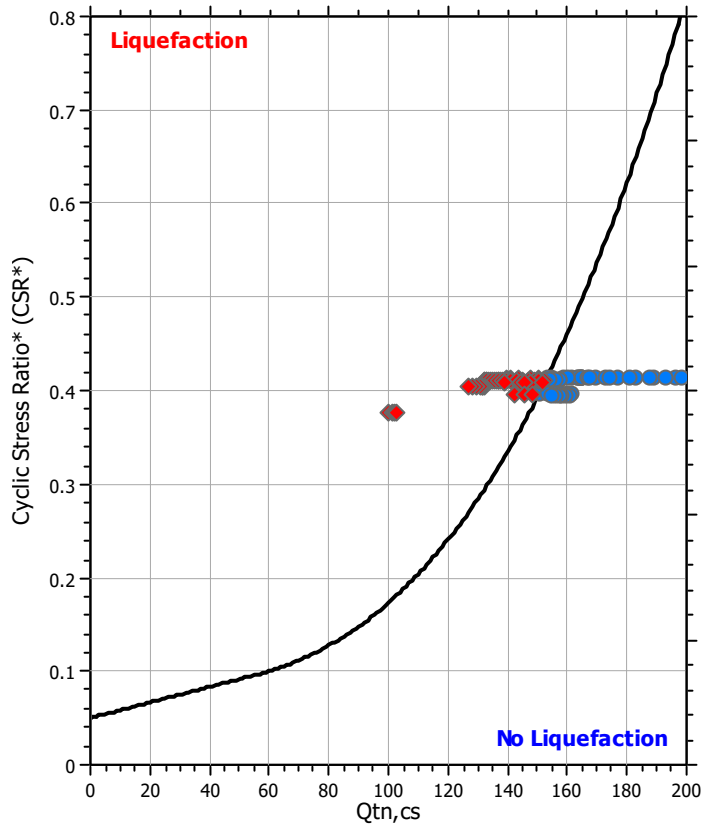
- Almost certain it will liquefy
- Very likely to liquefy
- Liquefaction and no liq. are equally likely
- Unlike to liquefy
- Almost certain it will not liquefy

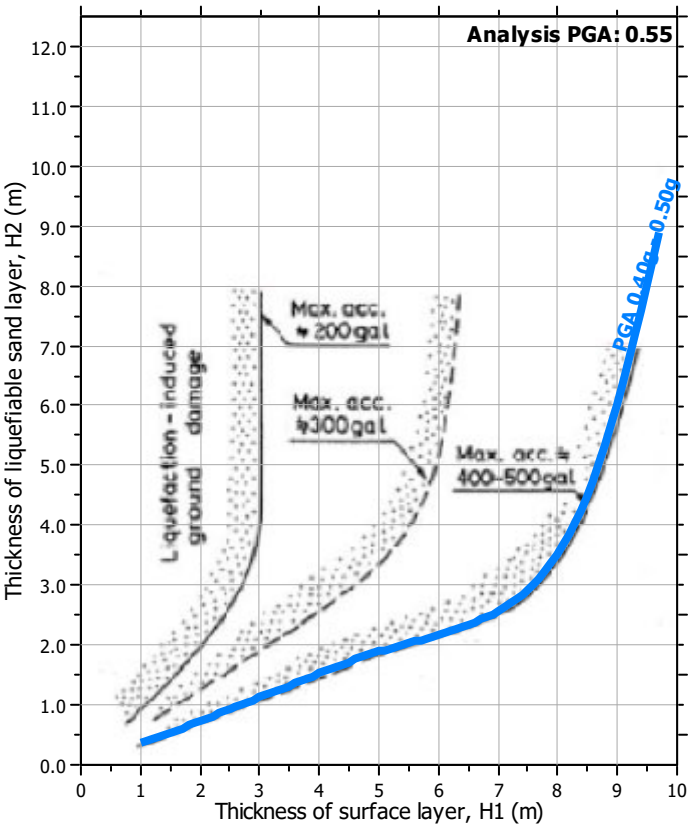
LPI color scheme

- Very high risk
- High risk
- Low risk

Liquefaction analysis summary plots



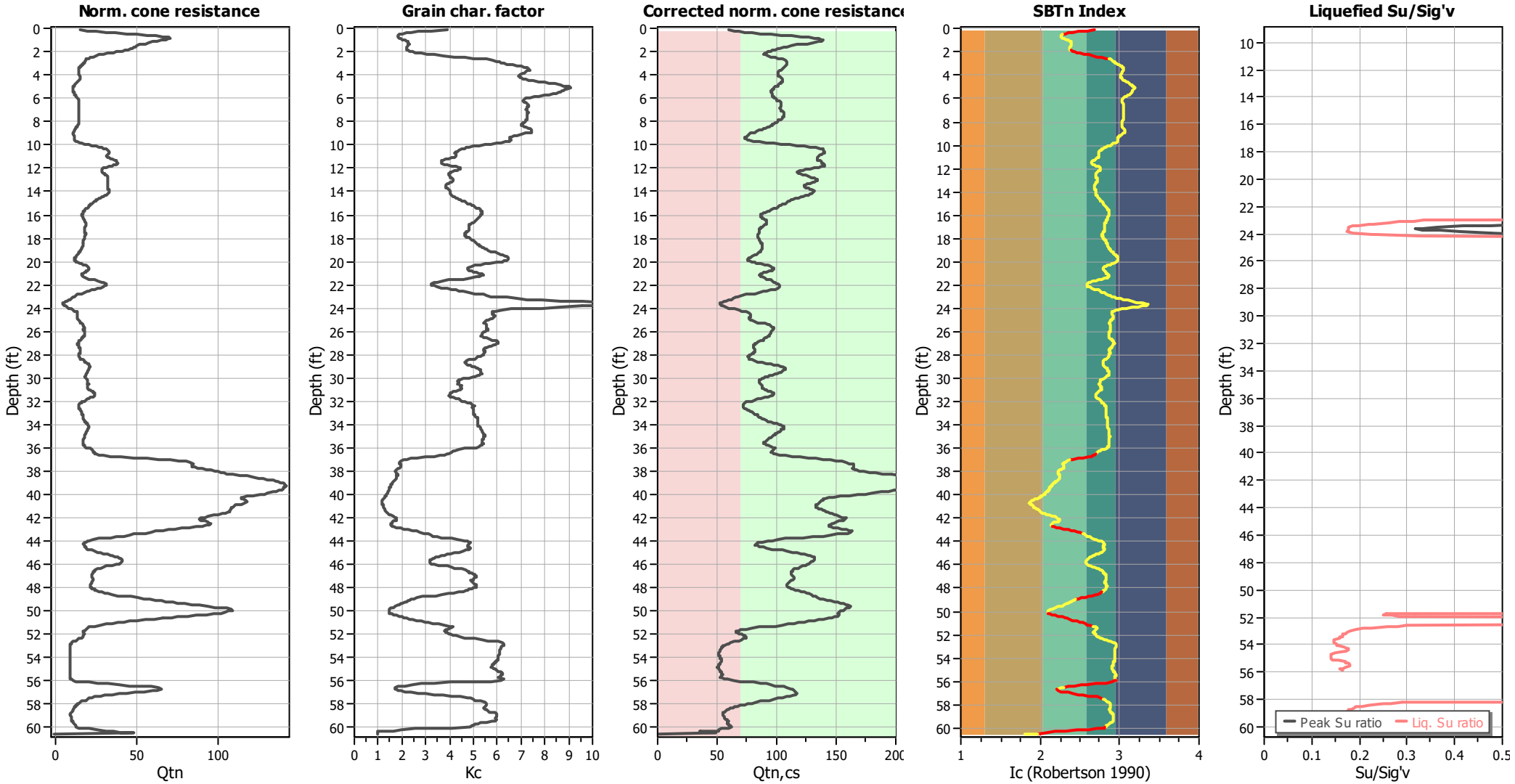




Input parameters and analysis data

Analysis method:	NCEER (1998)	Depth to water table (erthq.):	9.00 ft	Fill weight:	N/A
Fines correction method:	NCEER (1998)	Average results interval:	.	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.68	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.55	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	12.00 ft	Fill height:	N/A	Limit depth:	50.00 ft

Check for strength loss plots (Robertson (2010))



Input parameters and analysis data

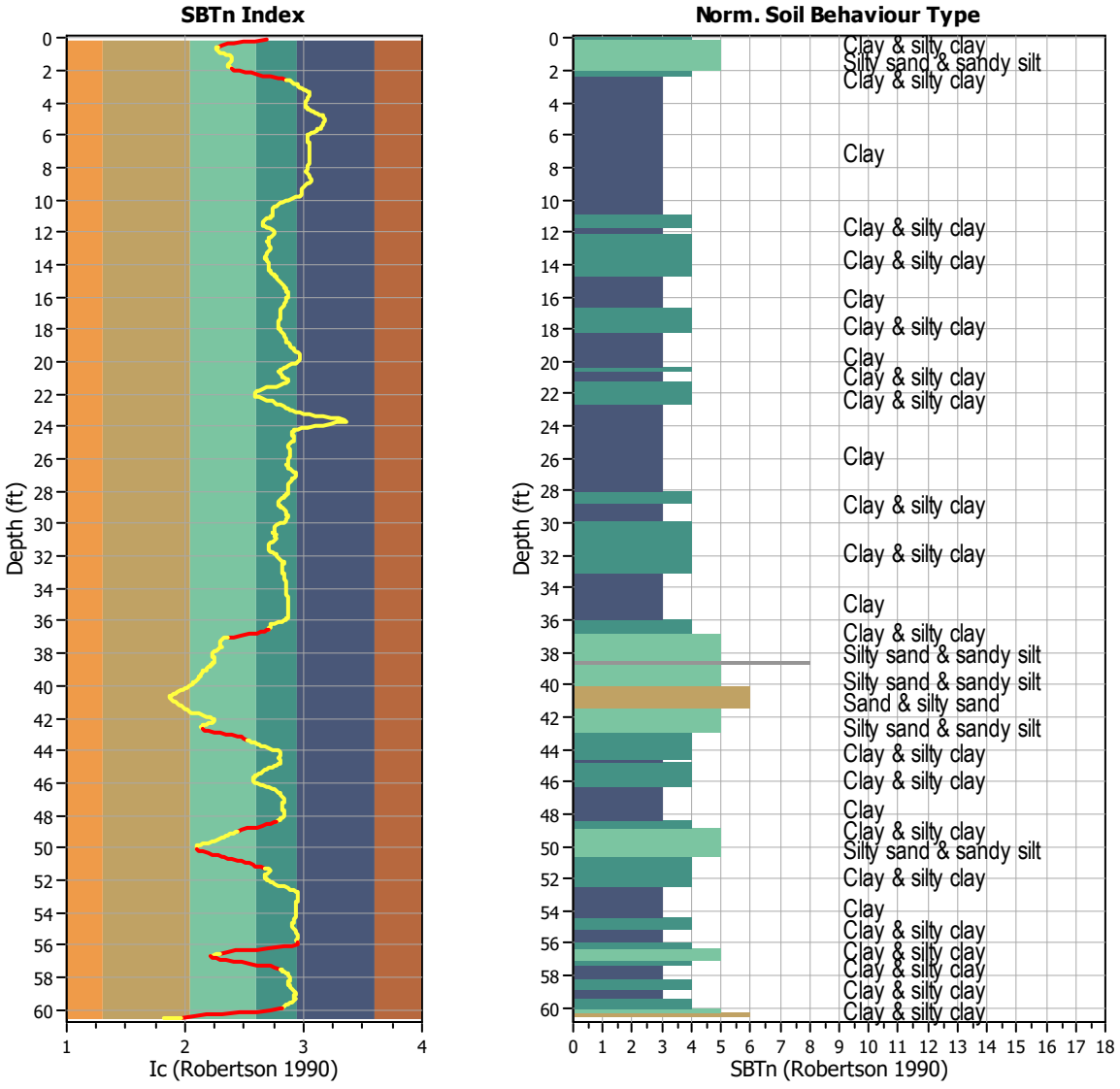
Analysis method:	NCEER (1998)	Depth to water table (erthq.):	9.00 ft	Fill weight:	N/A
Fines correction method:	NCEER (1998)	Average results interval:	.	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.68	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.55	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	12.00 ft	Fill height:	N/A	Limit depth:	50.00 ft

TRANSITION LAYER DETECTION ALGORITHM REPORT
Summary Details & Plots

Short description

The software will delete data when the cone is in transition from either clay to sand or vise-versa. To do this the software requires a range of I_c values over which the transition will be defined (typically somewhere between 1.80 < I_c < 3.0) and a rate of change of I_c. Transitions typically occur when the rate of change of I_c is fast (i.e. delta I_c is small).

The SBT_n plot below, displays in red the detected transition layers based on the parameters listed below the graphs.



Transition layer algorithm properties

I_c minimum check value:	1.70
I_c maximum check value:	3.00
I_c change ratio value:	0.0250
Minimum number of points in layer:	4

General statistics

Total points in CPT file:	924
Total points excluded:	101
Exclusion percentage:	10.93%
Number of layers detected:	9

Transition layer No	Number of points	Depth	SBT_n number	SBT_n description
Transition layer 1	8	Start depth: 0.08 (ft)	4	Clay & silty clay
		End depth: 0.55 (ft)	5	Silty sand & sandy silt
Transition layer 2	12	Start depth: 1.94 (ft)	5	Silty sand & sandy silt
		End depth: 2.63 (ft)	3	Clay
Transition layer 3	9	Start depth: 36.58 (ft)	4	Clay & silty clay
		End depth: 37.08 (ft)	5	Silty sand & sandy silt
Transition layer 4	11	Start depth: 42.73 (ft)	5	Silty sand & sandy silt
		End depth: 43.39 (ft)	4	Clay & silty clay
Transition layer 5	10	Start depth: 48.44 (ft)	3	Clay
		End depth: 49.03 (ft)	5	Silty sand & sandy silt
Transition layer 6	18	Start depth: 50.22 (ft)	5	Silty sand & sandy silt
		End depth: 51.34 (ft)	4	Clay & silty clay
Transition layer 7	11	Start depth: 55.93 (ft)	3	Clay
		End depth: 56.57 (ft)	5	Silty sand & sandy silt
Transition layer 8	13	Start depth: 56.78 (ft)	5	Silty sand & sandy silt
		End depth: 57.55 (ft)	3	Clay
Transition layer 9	9	Start depth: 59.99 (ft)	4	Clay & silty clay
		End depth: 60.53 (ft)	6	Sand & silty sand

Start depth: Depth where the transition layer begins
End depth: Depth where the transition layer ends

:: Field input data ::

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1	0.08	6.98	0.12	0.00	39.64	101.91
2	0.15	9.12	0.15	-0.10	34.72	104.11
3	0.23	11.45	0.17	-0.10	30.19	106.24
4	0.30	14.31	0.20	-0.10	27.00	108.14
5	0.35	16.63	0.23	-0.10	24.91	109.97
6	0.43	24.86	0.36	-0.10	23.15	112.11
7	0.50	35.32	0.50	-0.10	21.93	113.89
8	0.55	40.24	0.58	-0.10	21.22	115.50
9	0.61	45.70	0.74	-0.10	20.99	116.97
10	0.70	46.23	0.92	-0.10	20.93	118.25
11	0.73	46.05	0.99	-0.19	21.19	119.21
12	0.80	45.61	1.10	-0.19	21.77	119.80
13	0.89	44.09	1.25	-0.38	22.53	120.21
14	0.93	43.37	1.31	-0.38	23.57	120.37
15	1.01	41.94	1.32	-0.38	24.47	120.30
16	1.09	39.71	1.19	-0.29	25.28	120.07
17	1.13	38.45	1.14	-0.19	25.90	119.67
18	1.19	34.52	1.06	-0.19	26.10	119.10
19	1.29	32.46	0.94	-0.38	26.17	118.43
20	1.34	31.03	0.82	-0.43	26.12	117.70
21	1.39	30.14	0.70	-0.43	25.91	117.07
22	1.45	30.85	0.64	-0.48	26.00	116.42
23	1.54	30.49	0.63	-0.10	25.39	115.89
24	1.59	29.87	0.62	-0.10	25.05	115.42
25	1.67	31.39	0.62	-0.10	25.00	114.98
26	1.72	27.36	0.62	0.10	25.14	114.63
27	1.79	32.28	0.61	0.19	25.44	114.21
28	1.85	28.62	0.58	0.19	25.91	113.70
29	1.94	25.04	0.52	0.19	26.55	113.17
30	1.98	23.79	0.48	0.29	27.75	112.60
31	2.04	22.36	0.40	0.38	28.77	112.07
32	2.13	19.76	0.36	0.48	30.94	111.51
33	2.17	17.97	0.36	0.48	33.14	111.06
34	2.24	15.74	0.38	0.38	35.62	110.88
35	2.32	14.49	0.40	0.38	38.52	110.83
36	2.39	13.41	0.44	0.38	41.80	110.94
37	2.43	12.79	0.46	0.38	44.82	111.13
38	2.52	11.89	0.53	0.38	47.47	111.34
39	2.58	11.45	0.56	0.38	49.47	111.54
40	2.63	11.45	0.57	0.48	51.08	111.72
41	2.72	11.45	0.56	0.48	52.42	111.88
42	2.78	11.71	0.56	0.48	53.60	112.01
43	2.83	11.71	0.56	0.48	54.34	112.03
44	2.89	11.54	0.56	0.48	54.96	111.98
45	2.98	11.18	0.58	0.29	55.60	111.89
46	3.03	10.82	0.58	0.29	56.57	111.80
47	3.09	10.37	0.57	0.10	57.74	111.70
48	3.18	9.84	0.55	0.00	58.94	111.58

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
49	3.22	9.66	0.54	-0.19	60.02	111.43
50	3.32	9.03	0.54	-1.72	60.92	111.26
51	3.37	8.94	0.54	-2.58	61.61	111.08
52	3.42	8.94	0.53	-3.16	62.08	110.92
53	3.52	8.94	0.51	-3.54	62.25	110.76
54	3.57	8.94	0.51	-3.92	62.20	110.60
55	3.61	8.94	0.50	-4.69	61.70	110.46
56	3.68	8.94	0.49	-4.69	61.18	110.34
57	3.77	9.03	0.47	-5.26	60.70	110.27
58	3.83	9.12	0.45	-4.64	60.28	110.28
59	3.91	9.30	0.45	-5.26	59.86	110.28
60	3.95	9.30	0.46	-4.59	59.61	110.36
61	4.02	9.48	0.48	-3.92	59.50	110.48
62	4.12	9.66	0.50	-2.49	59.65	110.64
63	4.14	9.66	0.50	-1.34	59.87	110.80
64	4.22	9.66	0.53	-1.05	59.94	110.85
65	4.27	9.66	0.55	-1.24	60.48	110.97
66	4.37	9.48	0.56	-0.48	61.14	111.02
67	4.42	9.39	0.54	-0.67	61.98	110.99
68	4.46	9.39	0.48	-0.38	62.95	110.94
69	4.57	8.85	0.54	0.10	64.57	110.80
70	4.61	8.59	0.53	0.19	65.81	110.62
71	4.67	8.14	0.51	-0.19	66.92	110.42
72	4.76	7.87	0.50	-0.67	68.12	110.21
73	4.81	6.62	0.50	-0.38	69.61	110.08
74	4.90	7.15	0.49	-0.67	70.46	109.85
75	4.96	7.15	0.48	-1.15	71.23	109.60
76	5.00	7.06	0.46	-2.39	71.76	109.39
77	5.05	7.06	0.45	-2.58	72.00	109.24
78	5.14	7.06	0.44	-2.87	71.11	109.16
79	5.20	6.89	0.42	-3.45	70.63	109.06
80	5.30	6.89	0.42	-2.20	70.28	108.97
81	5.35	7.15	0.43	-2.20	69.94	108.93
82	5.39	7.42	0.44	-2.30	69.70	108.92
83	5.48	7.42	0.43	-2.78	69.32	108.94
84	5.55	7.33	0.43	-2.78	68.72	109.01
85	5.59	7.33	0.43	-2.78	68.01	109.09
86	5.64	7.33	0.44	-2.78	67.02	109.17
87	5.74	7.60	0.44	-2.11	65.97	109.22
88	5.79	7.87	0.44	-2.11	64.59	109.30
89	5.84	8.05	0.44	-2.11	63.30	109.45
90	5.94	8.67	0.44	-2.01	62.19	109.66
91	5.97	9.03	0.44	-1.91	61.21	109.86
92	6.05	9.57	0.43	-1.82	60.68	110.05
93	6.14	9.75	0.47	-2.01	60.40	110.25
94	6.19	9.84	0.50	-2.30	60.30	110.45
95	6.24	9.66	0.51	-2.39	60.47	110.61
96	6.33	9.30	0.52	-2.39	60.75	110.72

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
97	6.38	9.21	0.53	-2.39	61.26	110.81
98	6.44	9.12	0.54	-2.39	61.59	110.83
99	6.52	9.12	0.53	-2.01	61.80	110.82
100	6.59	9.12	0.51	-1.82	61.92	110.79
101	6.64	9.12	0.49	-1.82	61.79	110.76
102	6.70	9.30	0.49	-1.82	61.73	110.71
103	6.78	9.48	0.50	-1.82	61.43	110.66
104	6.83	9.39	0.50	-1.72	61.40	110.64
105	6.89	9.39	0.50	-2.01	61.36	110.68
106	6.98	9.12	0.50	-2.01	61.41	110.75
107	7.03	9.39	0.50	-2.01	61.44	110.86
108	7.09	9.12	0.52	-2.01	61.53	110.97
109	7.18	9.39	0.53	-2.01	61.66	111.08
110	7.23	9.39	0.53	-2.01	61.77	111.20
111	7.29	9.75	0.55	-2.01	61.72	111.26
112	7.38	9.84	0.56	-2.11	61.70	111.24
113	7.42	9.75	0.57	-2.11	61.62	111.23
114	7.48	9.75	0.57	-2.11	61.64	111.21
115	7.58	9.48	0.53	-2.11	61.67	111.18
116	7.62	9.39	0.49	-1.91	61.71	111.07
117	7.68	9.21	0.51	-1.63	61.68	110.91
118	7.78	9.30	0.52	-1.44	61.56	110.74
119	7.81	9.21	0.51	-1.44	61.33	110.53
120	7.88	9.21	0.49	-1.34	61.18	110.40
121	7.97	9.21	0.47	-1.35	61.12	110.31
122	8.01	9.21	0.47	-1.35	60.86	110.17
123	8.11	9.21	0.45	-1.36	60.57	109.99
124	8.14	9.21	0.46	-1.35	60.30	109.80
125	8.22	9.12	0.44	-1.34	60.14	109.62
126	8.31	9.03	0.43	-1.15	60.21	109.45
127	8.35	9.03	0.42	-1.15	60.41	109.24
128	8.41	8.85	0.41	-1.15	60.87	108.99
129	8.50	8.76	0.40	-1.15	61.30	108.67
130	8.56	8.41	0.39	-0.96	61.79	108.33
131	8.61	8.05	0.38	-0.77	62.17	107.96
132	8.68	7.51	0.35	-0.67	62.56	107.58
133	8.75	7.33	0.33	-0.38	62.70	107.14
134	8.80	7.15	0.31	-0.10	62.76	106.71
135	8.89	7.15	0.29	-0.10	62.58	106.30
136	8.94	7.15	0.28	-0.10	62.05	105.91
137	9.00	7.15	0.25	0.10	61.14	105.60
138	9.08	7.24	0.25	0.10	60.04	105.31
139	9.15	7.33	0.25	0.10	58.97	105.09
140	9.20	7.51	0.25	0.10	58.15	104.88
141	9.28	7.69	0.24	0.19	57.58	104.68
142	9.35	7.87	0.23	0.19	57.31	104.58
143	9.40	7.87	0.23	0.19	57.20	104.59
144	9.45	7.60	0.22	0.19	57.17	104.71

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
145	9.55	7.33	0.22	0.19	57.35	104.96
146	9.59	7.24	0.22	0.19	57.19	105.48
147	9.69	7.42	0.25	0.19	57.00	106.36
148	9.74	7.78	0.28	0.29	56.15	107.40
149	9.79	8.14	0.32	0.19	55.03	108.80
150	9.84	9.66	0.38	0.38	53.69	110.16
151	9.94	11.27	0.49	0.19	52.29	111.48
152	10.00	13.15	0.56	0.00	50.55	112.75
153	10.09	15.38	0.73	0.00	48.92	113.93
154	10.13	16.28	0.79	0.00	47.45	114.95
155	10.18	17.26	0.86	0.10	46.33	115.83
156	10.24	19.23	0.94	0.10	45.43	116.55
157	10.33	20.21	1.01	0.10	44.80	117.13
158	10.37	20.39	1.03	0.10	44.03	117.41
159	10.43	20.75	1.06	0.10	43.31	117.62
160	10.52	21.02	1.09	0.19	42.66	117.76
161	10.59	21.19	1.09	0.29	42.33	117.81
162	10.64	21.37	0.96	0.29	42.16	117.78
163	10.70	21.64	0.96	0.29	42.34	117.70
164	10.78	21.73	0.96	0.19	42.42	117.61
165	10.83	21.37	0.97	0.19	42.40	117.49
166	10.94	20.66	0.96	0.19	42.47	117.38
167	10.99	18.96	0.96	0.19	42.53	117.39
168	11.03	19.94	0.96	0.57	41.95	117.48
169	11.09	20.30	0.96	0.67	41.21	117.60
170	11.17	20.48	0.97	0.67	40.18	117.81
171	11.24	21.55	0.97	0.77	39.11	118.10
172	11.33	25.75	1.00	0.86	38.18	118.40
173	11.37	27.36	1.02	0.86	37.82	118.68
174	11.44	30.05	1.10	0.38	37.75	118.91
175	11.52	30.85	1.17	-0.19	37.77	119.11
176	11.57	29.15	1.19	-0.48	37.97	119.22
177	11.63	26.38	1.24	-0.67	38.69	119.21
178	11.72	24.41	1.21	-0.48	39.77	119.15
179	11.76	23.70	1.19	-0.67	41.00	118.93
180	11.83	22.18	1.12	-0.48	42.25	118.55
181	11.92	21.37	1.05	-0.29	43.28	118.12
182	11.94	20.39	1.04	-0.19	43.64	117.65
183	12.02	20.12	0.94	-0.10	43.65	117.22
184	12.11	19.67	0.82	-0.10	43.45	116.79
185	12.16	19.50	0.78	-0.10	42.79	116.45
186	12.22	19.58	0.76	-0.10	42.08	116.21
187	12.31	20.30	0.76	0.00	41.31	116.05
188	12.36	20.66	0.76	0.00	40.83	116.10
189	12.42	22.00	0.75	-0.10	40.58	116.33
190	12.50	22.62	0.79	-0.48	40.38	116.64
191	12.56	22.89	0.85	-0.38	40.26	116.98
192	12.62	23.25	0.95	-0.38	40.35	117.36

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
193	12.70	23.61	1.00	-0.38	40.49	117.73
194	12.77	24.23	1.04	-0.48	40.81	118.09
195	12.81	24.14	1.06	-0.57	41.13	118.38
196	12.91	24.32	1.13	-0.67	41.42	118.57
197	12.96	24.50	1.14	-0.77	41.46	118.66
198	13.01	24.68	1.15	-0.77	41.51	118.69
199	13.06	24.41	1.13	-0.96	41.38	118.62
200	13.16	23.88	1.08	-0.96	41.11	118.52
201	13.21	24.41	1.06	-0.96	40.69	118.35
202	13.26	23.79	1.03	-0.57	40.24	118.12
203	13.36	24.41	0.95	-0.48	39.76	117.87
204	13.40	24.86	0.92	-0.57	39.51	117.74
205	13.46	24.86	0.90	-0.67	39.34	117.72
206	13.55	24.59	0.85	-0.57	39.28	117.74
207	13.60	24.86	0.84	-0.67	39.21	117.82
208	13.67	24.50	0.98	-0.57	39.45	117.98
209	13.75	24.86	1.04	-0.48	39.86	118.16
210	13.80	25.31	1.07	-0.48	40.09	118.35
211	13.86	25.40	1.10	-0.48	40.30	118.57
212	13.95	25.13	1.13	-0.51	40.59	118.76
213	13.99	24.95	1.14	-0.51	40.63	118.80
214	14.06	26.11	1.13	-0.51	40.62	118.74
215	14.15	26.20	1.10	-0.48	40.72	118.62
216	14.19	25.84	1.08	-0.57	40.84	118.42
217	14.26	24.95	1.03	-0.57	40.96	118.17
218	14.35	24.50	0.97	-0.57	41.12	117.90
219	14.40	23.43	0.93	-0.57	41.48	117.57
220	14.45	22.45	0.89	-0.48	41.87	117.20
221	14.55	21.55	0.86	-0.57	42.31	116.82
222	14.58	21.10	0.86	-0.67	42.70	116.44
223	14.65	20.39	0.81	-0.57	43.22	116.11
224	14.74	20.03	0.76	-0.57	43.80	115.81
225	14.77	19.76	0.75	-0.57	44.29	115.53
226	14.84	19.14	0.71	-0.57	44.76	115.26
227	14.94	18.78	0.71	-0.57	45.19	114.97
228	15.00	17.97	0.70	-0.48	45.60	114.73
229	15.03	17.71	0.69	-0.57	46.06	114.53
230	15.11	17.26	0.67	-0.48	46.59	114.28
231	15.19	16.90	0.65	-0.57	47.10	114.08
232	15.24	16.81	0.65	-0.48	47.54	113.85
233	15.29	16.54	0.63	-0.38	47.87	113.58
234	15.39	15.83	0.59	-0.29	48.26	113.29
235	15.42	15.83	0.59	-0.29	48.59	113.01
236	15.49	15.47	0.57	-0.19	48.95	112.69
237	15.59	14.84	0.53	-0.10	49.35	112.35
238	15.63	14.49	0.52	-0.10	49.56	112.01
239	15.69	14.13	0.50	-0.10	49.72	111.71
240	15.78	13.68	0.47	-0.10	49.82	111.39

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
241	15.84	13.41	0.46	0.00	49.85	111.10
242	15.89	13.68	0.44	0.00	49.75	110.88
243	15.95	13.50	0.43	0.00	49.65	110.73
244	16.04	13.68	0.42	-0.10	49.61	110.65
245	16.08	13.68	0.42	-0.10	49.47	110.70
246	16.18	13.95	0.42	-0.10	49.25	110.83
247	16.24	13.95	0.44	0.10	49.20	111.00
248	16.28	13.95	0.46	0.10	48.83	111.20
249	16.36	14.49	0.49	0.10	48.52	111.44
250	16.43	15.02	0.51	0.10	48.22	111.69
251	16.47	15.02	0.52	0.10	48.08	111.95
252	16.54	16.01	0.52	0.10	47.74	112.13
253	16.63	16.36	0.53	0.19	47.27	112.26
254	16.68	16.45	0.54	0.19	46.87	112.27
255	16.78	16.19	0.55	0.57	46.64	112.20
256	16.83	16.54	0.53	0.57	46.37	112.09
257	16.87	16.63	0.51	0.67	46.37	111.97
258	16.93	16.05	0.48	0.38	46.33	111.81
259	17.01	15.56	0.46	0.77	46.28	111.62
260	17.09	15.29	0.45	0.77	46.15	111.44
261	17.15	15.20	0.45	1.05	46.17	111.28
262	17.20	15.47	0.44	1.05	46.35	111.17
263	17.27	15.47	0.44	1.05	46.31	111.13
264	17.35	15.56	0.45	0.96	46.16	111.15
265	17.40	15.47	0.45	0.96	45.73	111.18
266	17.45	15.38	0.46	0.96	45.38	111.20
267	17.55	16.10	0.46	0.96	45.19	111.24
268	17.59	16.36	0.46	1.05	45.05	111.27
269	17.65	17.08	0.45	1.05	45.04	111.26
270	17.75	16.72	0.45	1.15	45.09	111.24
271	17.79	16.63	0.45	1.24	45.04	111.20
272	17.87	16.28	0.45	1.24	45.23	111.17
273	17.94	15.65	0.44	0.96	45.52	111.16
274	17.98	15.38	0.44	1.05	46.03	111.16
275	18.05	15.38	0.44	1.15	46.51	111.20
276	18.14	15.38	0.45	1.15	46.98	111.23
277	18.18	15.38	0.46	1.15	47.31	111.27
278	18.24	15.47	0.47	1.34	47.55	111.36
279	18.34	15.47	0.48	1.34	47.83	111.46
280	18.39	15.47	0.48	1.24	48.11	111.56
281	18.44	15.56	0.48	1.44	48.33	111.63
282	18.54	15.56	0.49	1.44	48.64	111.69
283	18.59	15.38	0.50	1.44	48.90	111.73
284	18.64	15.29	0.50	1.63	49.17	111.73
285	18.74	15.20	0.49	1.53	49.52	111.73
286	18.79	15.02	0.50	1.44	49.92	111.73
287	18.84	15.02	0.50	1.53	50.28	111.69
288	18.92	14.76	0.49	1.44	50.63	111.64

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
289	18.97	14.58	0.49	1.53	51.07	111.55
290	19.04	14.40	0.49	1.53	51.56	111.43
291	19.14	14.31	0.48	1.63	52.18	111.26
292	19.17	14.13	0.48	1.63	52.78	111.05
293	19.24	13.59	0.47	1.63	53.48	110.81
294	19.34	13.15	0.44	1.63	54.23	110.57
295	19.39	12.43	0.43	1.44	54.80	110.24
296	19.43	12.16	0.41	1.63	55.38	109.88
297	19.52	11.63	0.39	1.44	56.00	109.53
298	19.56	11.45	0.39	1.63	56.47	109.22
299	19.63	11.27	0.35	1.63	56.73	108.94
300	19.73	11.09	0.33	1.63	56.82	108.74
301	19.78	11.09	0.34	1.63	56.77	108.54
302	19.83	11.09	0.35	1.72	56.76	108.46
303	19.90	11.36	0.33	1.72	56.35	108.54
304	19.96	11.45	0.35	1.72	55.72	108.91
305	20.03	11.40	0.33	1.72	55.09	109.51
306	20.09	11.36	0.36	1.72	53.80	110.15
307	20.16	12.79	0.41	1.82	51.96	110.86
308	20.23	14.49	0.48	1.82	50.54	111.73
309	20.31	15.65	0.56	1.72	49.27	112.55
310	20.35	17.80	0.59	1.72	48.02	113.32
311	20.42	20.21	0.63	1.72	46.89	113.89
312	20.50	21.19	0.73	1.63	45.95	114.31
313	20.55	21.37	0.76	1.53	45.81	114.53
314	20.62	21.64	0.75	1.34	45.70	114.56
315	20.70	20.39	0.68	1.34	45.87	114.46
316	20.75	20.39	0.65	1.34	46.39	114.23
317	20.82	17.17	0.63	1.44	46.99	113.80
318	20.90	16.54	0.57	1.44	47.56	113.28
319	20.96	16.45	0.53	1.44	48.20	112.73
320	21.01	16.19	0.49	1.44	48.87	112.31
321	21.11	15.29	0.46	1.15	49.94	112.03
322	21.15	15.20	0.45	1.15	50.26	111.87
323	21.21	15.20	0.44	1.24	49.83	111.99
324	21.27	15.11	0.46	1.24	49.13	112.25
325	21.36	15.11	0.53	1.24	48.27	112.63
326	21.40	15.11	0.55	1.24	46.50	113.18
327	21.51	18.87	0.62	1.24	44.40	113.81
328	21.55	20.75	0.65	1.24	42.42	114.49
329	21.60	22.09	0.67	1.15	40.27	115.21
330	21.69	26.20	0.72	1.05	38.24	115.80
331	21.75	29.51	0.76	0.86	36.45	116.33
332	21.80	30.76	0.80	0.77	35.44	116.70
333	21.90	33.80	0.86	0.38	34.81	117.01
334	21.95	34.07	0.86	0.19	34.59	117.26
335	22.00	33.71	0.86	0.10	34.74	117.40
336	22.09	31.30	0.86	-0.10	35.18	117.43

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
337	22.11	30.32	0.87	-0.19	35.77	117.37
338	22.19	27.54	0.87	-0.38	36.72	117.17
339	22.26	27.36	0.86	-0.67	38.13	116.83
340	22.35	26.74	0.81	-1.34	39.74	116.46
341	22.39	25.49	0.79	-1.63	41.16	115.96
342	22.44	24.23	0.74	-1.63	42.32	115.15
343	22.55	20.12	0.66	-1.91	43.44	114.31
344	22.58	19.14	0.64	-1.82	44.74	113.41
345	22.65	17.35	0.53	-1.91	46.35	112.49
346	22.74	15.56	0.30	-2.11	47.94	111.51
347	22.83	14.13	0.33	-2.01	49.49	110.49
348	22.85	13.41	0.33	-2.11	50.33	109.53
349	22.94	12.79	0.33	-1.98	51.09	108.47
350	23.00	12.61	0.32	-2.20	52.15	107.50
351	23.05	12.52	0.30	-1.95	54.34	107.10
352	23.10	11.71	0.27	-1.95	56.23	106.53
353	23.18	11.18	0.25	-1.95	58.83	105.87
354	23.25	9.66	0.22	-1.72	61.52	105.14
355	23.30	8.59	0.21	-1.72	65.15	104.37
356	23.38	7.69	0.19	-1.72	69.63	103.61
357	23.45	5.90	0.18	-1.72	74.72	102.93
358	23.50	5.63	0.17	-1.72	80.69	102.31
359	23.60	4.74	0.17	-1.72	84.62	101.92
360	23.65	4.74	0.17	-1.72	86.53	101.70
361	23.70	4.65	0.17	-1.72	84.28	101.94
362	23.76	4.56	0.17	-1.72	79.47	102.32
363	23.84	5.99	0.17	-1.63	74.79	102.81
364	23.89	6.89	0.18	-1.63	69.65	103.71
365	23.99	9.75	0.22	-1.63	65.07	104.64
366	24.03	10.46	0.22	-1.63	60.93	105.62
367	24.09	11.00	0.23	-1.63	57.45	106.60
368	24.19	12.61	0.32	-1.63	55.20	107.56
369	24.24	13.50	0.34	-1.63	53.41	108.44
370	24.30	14.40	0.37	-1.72	52.68	109.12
371	24.34	14.84	0.40	-1.72	52.46	109.73
372	24.44	15.11	0.43	-1.72	52.43	110.24
373	24.50	15.56	0.45	-1.72	52.50	110.50
374	24.58	15.38	0.46	-1.72	52.80	110.66
375	24.65	14.58	0.46	-1.72	53.16	110.69
376	24.69	14.31	0.45	-1.72	53.22	110.64
377	24.74	14.13	0.44	-1.72	53.03	110.57
378	24.84	13.77	0.42	-1.72	52.84	110.45
379	24.89	13.68	0.39	-1.72	52.62	110.47
380	24.95	14.49	0.38	-1.63	52.10	110.59
381	25.04	15.29	0.39	-1.63	51.55	110.82
382	25.08	15.56	0.39	-1.63	50.88	111.17
383	25.19	16.19	0.46	-1.63	50.50	111.75
384	25.24	16.90	0.50	-1.53	50.29	112.41

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
385	25.28	17.53	0.54	-1.63	50.40	113.06
386	25.35	18.51	0.59	-1.63	50.76	113.70
387	25.43	19.14	0.70	-1.63	50.97	114.21
388	25.48	19.14	0.74	-1.63	50.95	114.53
389	25.53	19.14	0.77	-1.63	50.89	114.78
390	25.63	19.14	0.81	-1.63	50.95	115.03
391	25.68	19.05	0.74	-1.63	51.09	115.20
392	25.74	19.05	0.69	-1.63	51.10	115.24
393	25.79	19.32	0.68	-1.63	51.46	115.20
394	25.88	19.67	0.73	-1.63	51.39	115.14
395	25.92	19.58	0.73	-1.63	50.88	115.04
396	25.99	19.58	0.73	-1.72	50.45	115.03
397	26.05	17.53	0.72	-1.56	50.13	115.07
398	26.13	19.14	0.72	-1.56	49.96	115.09
399	26.20	20.30	0.71	-1.56	49.79	115.03
400	26.26	20.75	0.71	-1.50	49.68	114.95
401	26.31	20.75	0.70	-1.44	49.73	114.85
402	26.40	20.39	0.69	-1.44	49.51	114.76
403	26.45	19.94	0.67	-1.44	49.72	114.59
404	26.54	19.41	0.66	-1.44	50.23	114.38
405	26.59	18.69	0.66	-1.44	50.89	114.14
406	26.65	17.80	0.64	-1.44	51.69	113.86
407	26.74	16.90	0.60	-1.44	52.50	113.58
408	26.78	16.81	0.58	-1.44	53.29	113.30
409	26.84	16.45	0.57	-1.44	53.85	112.97
410	26.94	15.83	0.54	-1.44	54.24	112.64
411	26.99	15.65	0.53	-1.44	54.20	112.33
412	27.04	15.38	0.52	-1.44	53.85	112.13
413	27.13	15.38	0.47	-1.44	53.46	111.97
414	27.18	15.38	0.47	-1.44	52.93	111.85
415	27.24	15.92	0.46	-1.34	52.30	111.86
416	27.34	16.63	0.47	-1.34	51.65	111.90
417	27.40	17.08	0.48	-1.34	51.01	111.99
418	27.44	17.35	0.49	-1.44	50.66	112.18
419	27.53	17.89	0.52	-1.44	50.42	112.33
420	27.57	18.15	0.53	-1.44	50.34	112.46
421	27.64	18.24	0.55	-1.44	50.44	112.54
422	27.72	17.97	0.56	-1.44	50.50	112.52
423	27.79	17.44	0.54	-1.44	50.52	112.45
424	27.83	17.26	0.53	-1.44	50.50	112.31
425	27.90	17.08	0.52	-1.44	50.43	112.14
426	27.98	16.90	0.47	-1.34	50.31	111.93
427	28.03	16.90	0.45	-1.44	50.08	111.71
428	28.09	16.99	0.44	-1.44	49.81	111.55
429	28.18	17.26	0.43	-1.44	49.44	111.42
430	28.22	17.26	0.43	-1.44	48.86	111.35
431	28.28	17.26	0.44	-1.44	48.29	111.49
432	28.38	17.35	0.45	-1.44	47.65	111.69

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
433	28.43	17.71	0.45	-1.34	46.99	112.11
434	28.48	18.69	0.47	-1.34	46.05	112.54
435	28.58	20.03	0.52	-1.24	45.42	113.09
436	28.62	20.93	0.53	-1.34	45.20	113.85
437	28.69	22.80	0.63	-1.34	45.17	114.61
438	28.77	24.59	0.63	-1.34	45.29	115.34
439	28.82	24.86	0.72	-1.34	45.56	115.99
440	28.88	25.13	0.89	-1.34	45.98	116.56
441	28.97	24.95	0.96	-1.34	46.49	117.08
442	29.01	24.59	0.98	-1.34	46.94	117.45
443	29.07	24.32	1.00	-1.40	47.69	117.77
444	29.15	24.32	1.03	-1.47	48.32	117.97
445	29.21	24.32	1.03	-1.47	48.73	118.00
446	29.30	24.77	1.01	-1.50	49.06	117.96
447	29.33	24.68	1.00	-1.50	49.29	117.87
448	29.41	24.32	0.97	-1.53	49.47	117.69
449	29.50	23.52	0.94	-1.53	49.62	117.46
450	29.53	23.25	0.94	-1.44	49.62	117.18
451	29.61	22.54	0.90	-1.44	49.69	116.86
452	29.70	21.73	0.82	-1.44	49.56	116.54
453	29.74	21.37	0.80	-1.44	49.24	116.18
454	29.80	21.37	0.75	-1.48	48.65	115.83
455	29.90	21.37	0.71	-1.44	48.05	115.47
456	29.93	22.18	0.69	-1.44	47.25	115.17
457	30.00	22.27	0.64	-1.34	46.15	114.98
458	30.09	22.71	0.61	-1.34	44.62	114.83
459	30.15	22.62	0.62	-1.34	43.75	114.69
460	30.19	23.25	0.63	-1.44	43.45	114.59
461	30.30	24.95	0.62	-1.44	43.02	114.56
462	30.33	27.36	0.62	-1.44	43.07	114.62
463	30.40	24.41	0.61	-1.53	43.07	114.77
464	30.49	22.00	0.63	-2.20	42.94	114.91
465	30.54	24.41	0.65	-2.30	42.88	115.01
466	30.59	22.71	0.68	-2.11	43.12	115.05
467	30.64	24.41	0.71	-2.30	43.77	115.04
468	30.72	25.04	0.71	-2.11	44.05	115.11
469	30.80	24.86	0.70	-2.20	43.83	115.17
470	30.88	24.23	0.66	-2.11	44.19	115.27
471	30.93	23.97	0.64	-2.11	44.08	115.50
472	31.00	23.92	0.67	-2.11	43.67	115.83
473	31.04	23.92	0.66	-2.11	43.10	116.18
474	31.13	23.88	0.74	-2.11	42.32	116.56
475	31.20	25.93	0.85	-2.11	41.57	116.96
476	31.29	30.32	0.94	-2.11	41.06	117.30
477	31.34	32.28	0.96	-2.20	40.86	117.53
478	31.38	34.07	0.97	-2.20	40.77	117.73
479	31.43	33.89	0.96	-2.30	40.60	117.76
480	31.51	31.93	0.92	-2.30	40.43	117.57

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
481	31.58	28.44	0.87	-2.11	40.55	117.17
482	31.63	27.28	0.84	-2.11	40.87	116.66
483	31.71	25.67	0.76	-2.11	41.56	116.04
484	31.78	24.68	0.65	-2.01	42.36	115.38
485	31.83	24.41	0.58	-2.11	43.16	114.71
486	31.90	23.70	0.53	-2.11	43.88	114.05
487	31.98	22.45	0.50	-2.11	44.20	113.38
488	32.03	21.73	0.49	-2.11	44.42	112.77
489	32.09	20.48	0.48	-2.11	44.90	112.27
490	32.16	18.15	0.46	-2.07	45.63	111.88
491	32.22	19.41	0.44	-2.07	46.45	111.56
492	32.30	19.14	0.42	-2.09	47.13	111.34
493	32.38	18.33	0.40	-2.11	47.64	111.16
494	32.42	18.06	0.40	-2.01	47.65	111.12
495	32.50	17.97	0.40	-2.01	47.22	111.19
496	32.56	18.15	0.41	-2.01	47.17	111.32
497	32.62	18.60	0.42	-2.01	47.34	111.58
498	32.72	20.21	0.46	-2.01	47.44	111.90
499	32.77	20.48	0.48	-2.11	47.48	112.25
500	32.82	20.75	0.50	-2.11	47.45	112.64
501	32.91	20.66	0.55	-2.11	47.39	113.02
502	32.97	20.66	0.56	-2.11	47.32	113.38
503	33.02	20.84	0.58	-2.20	47.45	113.68
504	33.11	21.46	0.61	-2.01	47.64	113.97
505	33.16	21.82	0.62	-2.01	47.82	114.22
506	33.22	22.18	0.63	-2.01	47.89	114.41
507	33.29	22.45	0.65	-2.01	47.97	114.58
508	33.37	22.54	0.67	-2.01	48.06	114.73
509	33.41	22.36	0.67	-2.01	48.25	114.88
510	33.47	22.27	0.68	-1.91	48.48	115.10
511	33.57	22.09	0.68	-2.01	48.85	115.33
512	33.60	22.09	0.69	-2.01	48.76	115.62
513	33.67	22.09	0.72	-2.11	48.66	115.99
514	33.76	23.07	0.79	-2.11	48.64	116.41
515	33.80	23.07	0.82	-2.11	48.63	116.87
516	33.86	25.75	0.87	-2.11	48.73	117.34
517	33.96	27.01	0.97	-2.11	48.85	117.78
518	34.00	27.01	1.02	-2.11	48.84	118.16
519	34.06	27.36	1.09	-2.11	48.79	118.44
520	34.16	27.01	1.13	-2.39	48.72	118.68
521	34.20	26.74	1.13	-2.39	48.97	118.83
522	34.26	26.74	1.12	-2.20	49.27	118.84
523	34.36	26.83	1.09	-2.20	49.47	118.80
524	34.39	26.65	1.08	-2.20	49.58	118.70
525	34.46	26.29	1.05	-2.20	49.64	118.55
526	34.56	25.75	1.00	-2.11	49.72	118.39
527	34.60	25.84	0.99	-2.01	49.84	118.21
528	34.65	25.67	0.98	-2.01	50.00	118.03

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
529	34.75	25.04	0.96	-2.01	50.15	117.85
530	34.80	24.68	0.95	-2.01	50.23	117.69
531	34.86	24.14	0.93	-2.01	50.33	117.55
532	34.95	24.14	0.91	-2.01	50.45	117.40
533	34.99	24.14	0.90	-2.02	50.46	117.24
534	35.06	24.14	0.88	-2.02	50.38	117.09
535	35.11	23.97	0.87	-2.03	50.31	116.93
536	35.19	23.79	0.84	-2.03	50.19	116.77
537	35.25	23.97	0.82	-2.03	50.11	116.61
538	35.31	23.97	0.81	-1.91	49.99	116.43
539	35.39	23.43	0.80	-1.91	49.94	116.25
540	35.49	23.16	0.77	-1.91	49.86	116.07
541	35.53	22.98	0.76	-2.01	49.88	115.96
542	35.60	22.89	0.73	-2.01	50.02	115.90
543	35.63	22.71	0.72	-2.11	50.20	115.93
544	35.70	22.71	0.71	-2.01	49.99	116.09
545	35.78	22.71	0.75	-2.06	49.69	116.39
546	35.84	22.98	0.78	-2.01	49.39	116.76
547	35.90	23.52	0.84	-2.11	49.02	117.25
548	35.98	26.11	0.92	-2.11	48.30	117.74
549	36.06	27.81	1.01	-2.11	46.77	118.08
550	36.09	28.44	1.07	-2.11	44.91	118.22
551	36.18	30.32	1.17	-2.20	43.21	118.27
552	36.23	32.10	1.15	-2.20	42.04	118.24
553	36.29	35.23	0.96	-2.20	41.55	118.23
554	36.38	35.23	0.77	-2.20	41.30	118.19
555	36.42	34.52	0.72	-2.11	40.99	118.29
556	36.49	30.94	0.73	-2.11	40.42	118.58
557	36.58	29.42	0.87	-2.11	39.83	119.00
558	36.62	29.24	0.95	-2.11	38.97	119.69
559	36.68	32.19	1.15	-2.20	37.62	120.84
560	36.77	38.99	1.43	-2.11	35.74	122.13
561	36.83	43.19	1.55	-2.20	32.71	123.51
562	36.88	53.48	1.67	-2.11	29.56	124.87
563	36.97	67.87	2.09	-2.11	27.07	126.08
564	37.02	79.86	2.36	-2.20	25.12	127.13
565	37.08	100.51	2.58	-2.39	23.83	127.98
566	37.17	116.16	2.90	-2.39	22.88	128.71
567	37.22	118.22	3.03	-2.39	22.40	129.32
568	37.27	117.95	3.15	-2.39	22.18	129.73
569	37.37	111.34	3.27	-2.39	22.09	130.03
570	37.41	107.85	3.30	-2.39	22.29	130.23
571	37.47	101.50	3.32	-2.20	22.58	130.31
572	37.57	98.73	3.29	-2.30	22.79	130.37
573	37.61	100.69	3.28	-2.39	22.71	130.36
574	37.67	105.43	3.30	-2.39	22.27	130.40
575	37.76	111.34	3.28	-2.39	21.70	130.44
576	37.81	115.09	3.30	-2.39	20.91	130.44

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
577	37.87	120.28	3.08	-2.49	20.43	130.61
578	37.97	130.29	3.27	-2.87	20.02	130.82
579	38.02	131.63	3.22	-3.06	19.80	131.08
580	38.07	131.90	3.02	-3.16	19.80	131.39
581	38.17	129.13	3.69	-3.16	20.07	131.83
582	38.20	132.44	3.85	-2.86	20.45	132.34
583	38.27	132.98	4.11	-2.86	20.71	132.87
584	38.33	134.05	4.44	-2.86	20.74	133.45
585	38.42	134.50	5.07	-2.58	20.77	134.05
586	38.46	140.67	5.31	-2.58	20.52	134.51
587	38.53	158.82	5.68	-2.58	20.36	134.91
588	38.62	175.63	5.90	-2.78	20.21	135.24
589	38.66	179.93	5.95	-2.87	20.04	135.50
590	38.73	181.09	5.95	-2.87	19.67	135.63
591	38.81	177.33	5.95	-2.68	19.27	135.72
592	38.86	173.04	5.90	-2.87	18.89	135.73
593	38.93	167.76	5.82	-2.68	18.59	135.67
594	39.02	170.00	5.62	-2.78	18.16	135.58
595	39.05	174.83	5.57	-2.68	17.73	135.48
596	39.12	182.79	5.43	-2.68	17.40	135.36
597	39.18	190.03	5.35	-2.68	17.16	135.23
598	39.27	199.69	5.13	-2.87	16.94	135.08
599	39.31	199.33	5.05	-2.78	16.67	134.96
600	39.37	188.51	5.04	-2.78	16.57	134.79
601	39.44	175.54	4.98	-2.78	16.41	134.62
602	39.50	169.28	4.88	-2.78	16.18	134.46
603	39.59	176.44	4.79	-2.49	16.02	134.28
604	39.65	165.08	4.60	-2.58	15.82	134.06
605	39.71	177.33	4.44	-2.58	15.57	133.74
606	39.77	189.31	4.36	-2.68	15.27	133.32
607	39.84	194.32	4.16	-2.87	14.89	132.79
608	39.91	190.92	3.84	-2.97	14.62	132.17
609	39.97	174.11	3.39	-3.16	14.05	131.50
610	40.03	156.85	2.96	-3.45	13.68	130.78
611	40.11	144.78	2.44	-3.64	13.35	129.97
612	40.17	136.82	2.21	-4.02	12.96	129.16
613	40.26	144.33	1.92	-4.31	12.55	128.37
614	40.30	138.25	1.86	-4.31	11.98	127.68
615	40.36	143.89	1.80	-4.31	11.36	127.10
616	40.45	154.35	1.77	-4.40	10.83	126.71
617	40.49	157.39	1.75	-4.40	10.35	126.40
618	40.57	159.71	1.64	-4.59	10.06	126.12
619	40.62	156.94	1.57	-4.88	9.74	125.85
620	40.70	153.90	1.52	-5.36	9.59	125.67
621	40.76	149.43	1.50	-5.36	9.68	125.58
622	40.86	145.85	1.33	-5.17	9.88	125.56
623	40.89	143.71	1.31	-5.17	10.17	125.62
624	40.95	142.54	1.46	-5.07	10.53	125.74

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
625	41.03	141.38	1.65	-5.17	10.89	125.91
626	41.11	141.47	1.76	-5.03	11.23	126.12
627	41.16	141.92	1.81	-4.99	11.62	126.46
628	41.23	140.18	1.86	-4.99	12.05	126.85
629	41.29	141.83	1.91	-4.89	12.40	127.18
630	41.35	141.74	1.96	-4.78	12.69	127.44
631	41.41	143.17	2.04	-4.78	12.98	127.69
632	41.49	144.24	2.18	-4.88	13.32	127.95
633	41.56	143.62	2.22	-4.69	13.85	128.32
634	41.64	142.28	2.27	-4.69	14.51	128.70
635	41.69	141.56	2.38	-4.69	15.33	129.08
636	41.73	140.76	2.49	-4.78	16.33	129.44
637	41.84	135.57	2.90	-4.88	17.38	129.74
638	41.89	131.72	3.05	-4.88	18.43	130.04
639	41.98	123.23	3.22	-4.88	19.29	130.29
640	42.04	115.72	3.36	-4.88	19.97	130.47
641	42.09	113.39	3.42	-4.78	20.47	130.59
642	42.16	114.11	3.47	-4.78	20.48	130.57
643	42.24	121.26	3.37	-4.78	20.21	130.46
644	42.28	124.84	3.23	-4.78	19.63	130.28
645	42.33	128.15	3.06	-4.88	18.87	130.06
646	42.39	133.87	2.82	-4.97	18.10	129.82
647	42.47	136.73	2.58	-4.97	17.42	129.54
648	42.53	136.46	2.44	-4.97	17.06	129.31
649	42.59	134.94	2.38	-4.97	17.01	129.19
650	42.66	132.53	2.40	-4.97	17.37	129.15
651	42.73	127.88	2.41	-4.97	17.99	129.22
652	42.83	123.14	2.58	-4.82	19.10	129.38
653	42.88	120.19	2.89	-4.82	20.62	129.61
654	42.93	108.29	3.06	-4.66	22.35	129.86
655	42.99	110.08	3.21	-4.66	24.25	130.11
656	43.07	98.99	3.39	-4.66	26.12	130.32
657	43.14	89.34	3.61	-4.43	27.87	130.45
658	43.19	86.39	3.72	-4.21	29.49	130.41
659	43.25	83.26	3.80	-4.31	30.68	130.19
660	43.34	82.81	3.73	-4.31	31.96	129.82
661	43.39	81.91	3.60	-4.31	32.85	129.35
662	43.45	77.35	3.27	-4.31	33.69	128.70
663	43.54	70.56	2.63	-4.21	34.54	127.93
664	43.59	66.35	2.25	-4.21	35.31	127.02
665	43.64	61.61	2.01	-4.21	36.43	125.89
666	43.74	48.29	1.70	-4.21	37.72	124.60
667	43.78	44.09	1.59	-4.21	39.16	123.22
668	43.83	40.60	1.45	-4.21	40.89	121.95
669	43.94	32.55	1.14	-4.02	42.94	120.75
670	43.98	30.76	1.00	-4.11	45.00	119.60
671	44.04	28.53	0.87	-3.92	45.87	118.69
672	44.14	27.10	0.75	-3.92	46.36	117.82

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
673	44.17	27.28	0.72	-3.92	46.58	117.05
674	44.23	27.90	0.72	-3.92	46.39	116.71
675	44.33	29.24	0.72	-3.92	46.22	116.56
676	44.37	29.51	0.73	-3.92	45.72	116.56
677	44.44	29.51	0.74	-3.92	45.68	116.90
678	44.53	29.51	0.83	-4.02	45.92	117.39
679	44.58	30.05	0.86	-3.83	46.29	117.97
680	44.64	31.57	0.85	-3.83	46.58	118.66
681	44.73	31.66	1.03	-3.83	46.34	119.47
682	44.78	32.37	1.17	-3.73	45.98	120.29
683	44.82	33.53	1.30	-3.83	45.29	121.12
684	44.90	37.11	1.45	-3.83	44.37	121.98
685	44.97	42.84	1.62	-3.83	43.46	122.84
686	45.03	44.71	1.74	-3.92	42.10	123.58
687	45.09	48.02	1.90	-3.92	40.87	124.21
688	45.17	52.58	2.06	-3.92	39.76	124.75
689	45.22	55.53	2.15	-3.92	38.78	125.25
690	45.29	59.47	2.19	-3.92	37.94	125.66
691	45.38	58.93	2.22	-3.92	37.09	126.02
692	45.42	58.66	2.25	-3.92	36.18	126.28
693	45.50	61.26	2.36	-3.92	35.43	126.43
694	45.57	64.74	2.42	-4.02	34.87	126.53
695	45.62	66.18	2.42	-4.02	34.54	126.56
696	45.69	68.32	2.36	-4.02	34.28	126.55
697	45.77	68.41	2.29	-4.11	34.07	126.51
698	45.82	67.16	2.28	-4.11	34.05	126.38
699	45.88	66.00	2.22	-4.11	34.35	126.17
700	45.97	62.87	2.13	-4.11	34.83	125.92
701	46.02	60.90	2.10	-4.11	35.69	125.62
702	46.10	57.68	2.05	-4.11	37.01	125.30
703	46.17	53.92	1.98	-4.11	38.40	124.96
704	46.21	51.60	1.92	-4.21	39.78	124.63
705	46.27	47.04	1.82	-4.11	41.01	124.28
706	46.36	41.94	1.79	-4.21	42.18	123.93
707	46.42	40.96	1.76	-4.11	43.25	123.60
708	46.46	41.81	1.72	-4.02	44.26	123.29
709	46.56	41.67	1.60	-3.92	45.19	123.02
710	46.61	41.49	1.56	-3.92	45.83	122.82
711	46.66	40.60	1.54	-3.92	46.10	122.69
712	46.74	38.81	1.54	-3.92	46.41	122.63
713	46.81	38.63	1.53	-3.92	46.88	122.61
714	46.87	38.18	1.53	-4.11	47.56	122.64
715	46.94	37.47	1.59	-3.92	47.79	122.71
716	47.01	37.74	1.69	-4.11	47.95	122.81
717	47.06	38.01	1.73	-3.92	48.08	122.91
718	47.12	37.38	1.72	-4.02	48.11	123.00
719	47.19	41.40	1.71	-4.02	47.91	123.04
720	47.25	41.31	1.72	-4.02	47.60	123.05

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
721	47.34	39.88	1.73	-4.02	47.32	122.99
722	47.39	40.24	1.69	-4.02	47.11	122.89
723	47.44	40.69	1.59	-3.92	46.80	122.78
724	47.54	40.06	1.56	-4.11	46.99	122.60
725	47.59	39.08	1.55	-4.11	47.27	122.43
726	47.65	37.92	1.53	-4.11	47.37	122.31
727	47.74	37.83	1.49	-4.11	47.72	122.20
728	47.81	37.02	1.42	-4.11	48.11	122.15
729	47.85	36.22	1.46	-3.92	48.25	122.16
730	47.94	37.11	1.53	-4.02	48.21	122.19
731	47.98	36.13	1.55	-4.02	48.07	122.32
732	48.04	37.20	1.54	-4.02	47.64	122.55
733	48.13	39.26	1.58	-4.02	47.06	122.85
734	48.17	40.24	1.60	-4.02	46.29	123.21
735	48.24	41.23	1.72	-4.02	45.79	123.60
736	48.32	45.25	1.83	-4.02	45.19	124.00
737	48.37	47.22	1.88	-4.02	44.40	124.44
738	48.44	49.27	2.02	-4.21	43.25	124.90
739	48.53	49.27	2.20	-4.11	41.74	125.37
740	48.56	49.81	2.25	-4.11	40.04	125.80
741	48.64	53.83	2.32	-4.11	37.94	126.24
742	48.72	61.08	2.40	-4.11	35.90	126.69
743	48.78	67.61	2.42	-4.11	33.68	127.15
744	48.83	71.81	2.45	-4.11	31.47	127.61
745	48.90	84.24	2.53	-4.11	29.59	128.05
746	48.97	89.96	2.63	-4.11	28.25	128.51
747	49.03	99.98	2.77	-4.11	27.24	128.96
748	49.12	106.24	2.96	-4.21	26.48	129.41
749	49.16	106.24	3.03	-4.11	25.72	129.86
750	49.23	104.45	3.29	-4.31	25.05	130.27
751	49.31	107.67	3.47	-4.11	24.26	130.66
752	49.36	110.26	3.58	-4.11	23.57	131.00
753	49.43	117.06	3.66	-4.11	22.81	131.32
754	49.52	127.79	3.69	-4.21	21.90	131.63
755	49.58	139.33	3.73	-4.31	20.86	131.87
756	49.62	145.32	3.77	-4.31	19.86	132.03
757	49.71	155.33	3.84	-4.31	18.66	131.96
758	49.78	164.19	3.86	-4.40	17.51	131.79
759	49.81	166.87	3.80	-4.40	16.60	131.60
760	49.88	166.87	3.69	-4.40	15.97	131.43
761	49.97	166.33	2.81	-4.40	15.60	131.29
762	50.00	165.71	2.51	-4.40	15.62	131.13
763	50.07	165.35	2.63	-4.40	15.71	131.03
764	50.14	162.67	2.83	-4.40	15.93	130.97
765	50.22	157.39	3.13	-4.39	16.41	130.91
766	50.27	140.13	3.31	-4.37	17.43	131.02
767	50.35	151.58	3.58	-4.37	18.71	131.16
768	50.40	148.36	3.68	-4.29	20.17	131.18

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
769	50.47	133.96	3.67	-4.21	21.63	131.02
770	50.55	118.40	3.57	-4.21	22.94	130.72
771	50.59	110.62	3.48	-4.31	23.79	130.37
772	50.66	97.83	3.25	-4.11	25.02	129.89
773	50.75	89.34	2.79	-4.11	26.40	129.32
774	50.79	87.73	2.53	-4.11	27.87	128.69
775	50.86	88.89	2.41	-4.11	29.36	127.99
776	50.94	83.79	2.34	-4.11	30.91	127.24
777	50.99	78.16	2.26	-4.11	32.34	126.46
778	51.05	65.10	2.17	-4.02	33.72	125.69
779	51.14	52.67	1.94	-4.02	35.25	124.86
780	51.18	48.56	1.82	-3.83	37.12	123.93
781	51.25	43.28	1.63	-3.83	38.95	122.86
782	51.34	41.05	1.28	-3.83	40.76	121.60
783	51.41	40.06	1.01	-3.73	41.64	120.27
784	51.44	39.26	0.90	-3.73	41.46	118.99
785	51.52	36.84	0.70	-3.73	40.87	117.62
786	51.67	33.00	0.50	-3.73	39.81	116.30
787	51.70	32.19	0.48	-3.73	39.16	115.26
788	51.75	31.84	0.46	-3.73	39.05	114.59
789	51.78	31.39	0.45	-3.73	39.16	114.10
790	51.88	31.84	0.48	-3.73	39.39	114.05
791	51.92	31.21	0.51	-3.73	39.68	114.39
792	51.99	31.84	0.57	-3.73	40.07	114.77
793	52.04	32.10	0.61	-3.68	40.77	115.20
794	52.14	34.88	0.68	-3.68	41.59	115.58
795	52.19	35.41	0.71	-3.68	42.54	115.87
796	52.26	34.61	0.73	-3.64	43.63	116.00
797	52.33	32.82	0.77	-3.64	44.82	115.89
798	52.38	31.21	0.75	-3.64	46.10	115.68
799	52.43	29.42	0.73	-3.64	47.88	115.29
800	52.51	25.93	0.65	-3.64	49.76	114.75
801	52.58	23.25	0.54	-3.64	51.52	114.13
802	52.63	22.09	0.51	-3.64	52.93	113.37
803	52.69	20.66	0.47	-3.64	54.17	112.56
804	52.77	20.30	0.41	-3.64	55.16	111.73
805	52.83	20.30	0.38	-3.62	55.56	111.00
806	52.90	19.76	0.35	-3.62	55.69	110.47
807	52.99	19.41	0.33	-3.62	55.59	109.96
808	53.05	19.23	0.33	-3.54	55.26	109.54
809	53.10	19.05	0.32	-3.54	55.08	109.25
810	53.16	18.96	0.31	-3.54	55.01	109.00
811	53.25	18.96	0.30	-3.54	54.96	108.83
812	53.29	18.96	0.30	-3.54	54.89	108.72
813	53.38	18.96	0.30	-3.54	54.67	108.55
814	53.44	18.96	0.29	-3.64	54.48	108.41
815	53.50	18.91	0.29	-3.64	54.36	108.29
816	53.55	18.96	0.29	-3.64	54.33	108.20

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
817	53.64	18.96	0.27	-3.64	54.44	108.13
818	53.72	18.78	0.27	-3.64	54.54	108.07
819	53.74	18.69	0.27	-3.64	54.49	108.04
820	53.82	18.51	0.27	-3.64	54.33	108.05
821	53.90	18.33	0.28	-3.64	54.26	108.12
822	53.94	18.33	0.28	-3.64	54.24	108.28
823	54.01	18.96	0.28	-3.64	54.23	108.46
824	54.09	19.58	0.29	-3.64	54.23	108.65
825	54.19	19.76	0.31	-3.64	54.15	108.80
826	54.24	20.12	0.32	-3.64	54.00	108.93
827	54.29	20.12	0.33	-3.64	53.84	109.02
828	54.35	20.03	0.33	-3.64	53.69	109.03
829	54.44	19.94	0.32	-3.64	53.55	108.96
830	54.49	19.76	0.32	-3.64	53.31	108.82
831	54.53	19.58	0.31	-3.64	53.09	108.65
832	54.63	19.58	0.28	-3.64	52.86	108.45
833	54.68	19.67	0.26	-3.64	52.59	108.25
834	54.74	19.67	0.26	-3.64	52.41	108.07
835	54.83	19.76	0.26	-3.54	52.20	107.91
836	54.88	19.67	0.26	-3.64	52.17	107.85
837	54.94	19.58	0.26	-3.64	52.44	107.97
838	55.03	19.41	0.26	-3.64	52.82	108.15
839	55.07	19.58	0.27	-3.64	53.20	108.35
840	55.13	19.32	0.29	-3.64	53.70	108.58
841	55.23	19.58	0.32	-3.64	54.17	108.80
842	55.28	19.76	0.32	-3.64	54.58	109.01
843	55.32	19.85	0.33	-3.64	54.94	109.22
844	55.42	19.76	0.34	-3.64	55.19	109.35
845	55.50	19.76	0.34	-3.64	55.10	109.41
846	55.53	19.76	0.34	-3.64	54.85	109.37
847	55.58	19.76	0.34	-3.64	54.80	109.34
848	55.66	19.85	0.32	-3.64	54.72	109.27
849	55.73	20.12	0.31	-3.64	54.10	108.96
850	55.78	20.12	0.30	-3.64	54.62	109.41
851	55.86	19.85	0.31	-3.64	55.35	110.19
852	55.93	19.67	0.30	-3.64	55.76	111.17
853	55.97	19.76	0.22	-3.64	54.85	112.87
854	56.08	21.28	0.51	-3.64	52.24	114.70
855	56.12	22.98	0.65	-3.64	47.69	116.55
856	56.17	25.67	0.77	-3.54	40.66	118.53
857	56.28	37.11	1.15	-3.60	35.33	120.26
858	56.32	48.20	1.35	-3.60	31.24	121.84
859	56.37	64.21	1.50	-3.60	27.66	123.01
860	56.47	97.30	1.72	-3.54	24.80	123.99
861	56.52	104.27	1.77	-3.54	22.49	124.82
862	56.57	110.44	1.81	-3.54	20.88	125.48
863	56.67	115.54	1.77	-3.54	19.85	126.02
864	56.72	116.88	1.78	-3.54	19.53	126.46

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
865	56.78	118.31	1.81	-3.64	20.09	126.72
866	56.87	114.55	2.04	-3.64	21.06	126.88
867	56.91	110.08	2.17	-3.64	22.36	126.93
868	56.97	98.91	2.31	-3.64	24.36	126.88
869	57.03	91.75	2.39	-3.64	26.77	126.77
870	57.11	78.78	2.31	-3.64	29.69	126.62
871	57.17	70.91	2.21	-3.64	32.65	126.30
872	57.26	54.37	2.07	-3.64	35.65	125.81
873	57.32	49.99	2.03	-3.64	38.36	125.25
874	57.35	47.57	2.01	-3.54	41.20	124.56
875	57.42	46.77	1.83	-3.45	43.69	123.86
876	57.51	46.23	1.57	-3.45	45.93	123.14
877	57.55	44.89	1.48	-3.45	46.82	122.48
878	57.62	40.06	1.36	-3.45	47.44	121.72
879	57.71	36.75	1.25	-3.45	47.93	120.88
880	57.78	35.41	1.14	-3.45	48.62	120.05
881	57.82	34.07	1.03	-3.45	49.58	119.25
882	57.90	31.12	0.88	-3.45	50.55	118.42
883	57.96	29.60	0.84	-3.45	50.94	117.60
884	58.01	28.80	0.80	-3.45	50.99	116.79
885	58.11	27.99	0.67	-3.45	50.99	116.00
886	58.15	27.63	0.63	-3.35	50.90	115.22
887	58.21	27.28	0.57	-3.35	50.73	114.53
888	58.31	26.47	0.52	-3.35	50.50	113.81
889	58.35	26.29	0.49	-3.45	50.25	113.07
890	58.42	25.75	0.44	-3.45	50.38	112.48
891	58.50	24.59	0.40	-3.45	50.54	111.91
892	58.55	23.43	0.38	-3.45	50.90	111.42
893	58.61	22.71	0.37	-3.45	51.26	110.99
894	58.70	21.91	0.36	-3.35	51.84	110.61
895	58.75	21.82	0.35	-3.35	52.57	110.35
896	58.81	21.55	0.35	-3.35	53.20	110.22
897	58.89	21.46	0.34	-3.35	53.61	110.17
898	58.95	21.02	0.34	-3.35	53.87	110.21
899	59.00	21.02	0.35	-3.35	53.83	110.34
900	59.10	21.37	0.36	-3.35	53.71	110.47
901	59.15	21.82	0.37	-3.35	53.57	110.60
902	59.20	22.18	0.39	-3.35	53.51	110.75
903	59.28	23.07	0.41	-3.25	53.41	110.90
904	59.35	23.43	0.40	-3.35	53.65	111.16
905	59.38	23.16	0.40	-3.19	53.75	111.47
906	59.46	22.89	0.40	-3.19	53.55	111.71
907	59.53	22.62	0.40	-3.19	52.49	111.89
908	59.59	22.45	0.47	-3.06	50.91	111.89
909	59.67	23.52	0.50	-3.06	49.64	111.92
910	59.73	24.77	0.48	-3.06	48.60	111.95
911	59.79	27.90	0.45	-3.06	47.99	112.09
912	59.89	29.60	0.37	-3.06	47.37	112.33

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
913	59.94	29.24	0.38	-3.06	46.97	112.68
914	59.99	28.26	0.39	-3.06	46.47	113.29
915	60.07	27.19	0.45	-3.06	41.22	112.67
916	60.12	28.12	0.50	-3.06	35.84	112.04
917	60.19	27.99	0.63	-2.97	29.05	111.64
918	60.25	32.64	0.81	-2.97	22.89	111.14
919	60.33	48.20	0.00	-2.97	18.61	110.35
920	60.38	57.77	0.00	-2.97	5.00	109.08
921	60.48	86.03	0.00	-3.06	5.00	107.14
922	60.53	99.62	0.00	-3.35	5.00	103.25
923	60.61	88.89	0.00	-3.35	N/A	87.36
924	60.63	81.65	0.00	-3.25	N/A	87.36

Abbreviations

Depth: Depth from free surface, at which CPT was performed (ft)
q_c: Measured cone resistance (tsf)
f_s: Sleeve friction resistance (tsf)
u: Pore pressure (tsf)
Fines content: Percentage of fines in soil (%)
Unit weight: Bulk soil unit weight (pcf)

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data ::

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
1	0.08	0.00	0.00	0.00	1.00	0.358	1.34	0.266	1.00	1.00	2.000	Yes
2	0.15	0.01	0.00	0.01	1.00	0.358	1.34	0.266	1.00	1.00	2.000	Yes
3	0.23	0.01	0.00	0.01	1.00	0.358	1.34	0.266	1.00	1.00	2.000	Yes
4	0.30	0.02	0.00	0.02	1.00	0.358	1.34	0.266	1.00	1.00	2.000	Yes
5	0.35	0.02	0.00	0.02	1.00	0.358	1.34	0.266	1.00	1.00	2.000	Yes
6	0.43	0.02	0.00	0.02	1.00	0.358	1.34	0.266	1.00	1.00	2.000	Yes
7	0.50	0.03	0.00	0.03	1.00	0.358	1.34	0.266	1.00	1.00	2.000	Yes
8	0.55	0.03	0.00	0.03	1.00	0.358	1.34	0.266	1.00	1.00	2.000	Yes
9	0.61	0.03	0.00	0.03	1.00	0.358	1.34	0.266	1.00	1.00	2.000	No
10	0.70	0.04	0.00	0.04	1.00	0.358	1.34	0.266	1.00	1.00	2.000	No
11	0.73	0.04	0.00	0.04	1.00	0.358	1.34	0.266	1.00	1.00	2.000	No
12	0.80	0.04	0.00	0.04	1.00	0.357	1.34	0.266	1.00	1.00	2.000	No
13	0.89	0.05	0.00	0.05	1.00	0.357	1.34	0.266	1.00	1.00	2.000	No
14	0.93	0.05	0.00	0.05	1.00	0.357	1.34	0.266	1.00	1.00	2.000	No
15	1.01	0.06	0.00	0.06	1.00	0.357	1.34	0.266	1.00	1.00	2.000	No
16	1.09	0.06	0.00	0.06	1.00	0.357	1.34	0.266	1.00	1.00	2.000	No
17	1.13	0.06	0.00	0.06	1.00	0.357	1.34	0.266	1.00	1.00	2.000	No
18	1.19	0.07	0.00	0.07	1.00	0.357	1.34	0.266	1.00	1.00	2.000	No
19	1.29	0.07	0.00	0.07	1.00	0.357	1.34	0.266	1.00	1.00	2.000	No
20	1.34	0.08	0.00	0.08	1.00	0.357	1.34	0.266	1.00	1.00	2.000	No
21	1.39	0.08	0.00	0.08	1.00	0.357	1.34	0.266	1.00	1.00	2.000	No
22	1.45	0.08	0.00	0.08	1.00	0.357	1.34	0.266	1.00	1.00	2.000	No
23	1.54	0.09	0.00	0.09	1.00	0.357	1.34	0.265	1.00	1.00	2.000	No
24	1.59	0.09	0.00	0.09	1.00	0.357	1.34	0.265	1.00	1.00	2.000	No
25	1.67	0.10	0.00	0.10	1.00	0.357	1.34	0.265	1.00	1.00	2.000	No
26	1.72	0.10	0.00	0.10	1.00	0.357	1.34	0.265	1.00	1.00	2.000	No
27	1.79	0.10	0.00	0.10	1.00	0.357	1.34	0.265	1.00	1.00	2.000	No
28	1.85	0.11	0.00	0.11	1.00	0.357	1.34	0.265	1.00	1.00	2.000	No
29	1.94	0.11	0.00	0.11	1.00	0.357	1.34	0.265	1.00	1.00	2.000	Yes
30	1.98	0.11	0.00	0.11	1.00	0.357	1.34	0.265	1.00	1.00	2.000	Yes
31	2.04	0.12	0.00	0.12	1.00	0.357	1.34	0.265	1.00	1.00	2.000	Yes
32	2.13	0.12	0.00	0.12	1.00	0.356	1.34	0.265	1.00	1.00	2.000	Yes
33	2.17	0.12	0.00	0.12	1.00	0.356	1.34	0.265	1.00	1.00	2.000	Yes
34	2.24	0.13	0.00	0.13	1.00	0.356	1.34	0.265	1.00	1.00	2.000	Yes
35	2.32	0.13	0.00	0.13	1.00	0.356	1.34	0.265	1.00	1.00	2.000	Yes
36	2.39	0.14	0.00	0.14	1.00	0.356	1.34	0.265	1.00	1.00	2.000	Yes
37	2.43	0.14	0.00	0.14	1.00	0.356	1.34	0.265	1.00	1.00	2.000	Yes
38	2.52	0.14	0.00	0.14	1.00	0.356	1.34	0.265	1.00	1.00	2.000	Yes
39	2.58	0.15	0.00	0.15	1.00	0.356	1.34	0.265	1.00	1.00	2.000	Yes
40	2.63	0.15	0.00	0.15	1.00	0.356	1.34	0.265	1.00	1.00	2.000	Yes
41	2.72	0.15	0.00	0.15	1.00	0.356	1.34	0.265	1.00	1.00	2.000	No
42	2.78	0.16	0.00	0.16	1.00	0.356	1.34	0.265	1.00	1.00	2.000	No
43	2.83	0.16	0.00	0.16	1.00	0.356	1.34	0.265	1.00	1.00	2.000	No
44	2.89	0.16	0.00	0.16	1.00	0.356	1.34	0.265	1.00	1.00	2.000	No
45	2.98	0.17	0.00	0.17	1.00	0.356	1.34	0.265	1.00	1.00	2.000	No
46	3.03	0.17	0.00	0.17	0.99	0.356	1.34	0.265	1.00	1.00	2.000	No
47	3.09	0.18	0.00	0.18	0.99	0.356	1.34	0.264	1.00	1.00	2.000	No
48	3.18	0.18	0.00	0.18	0.99	0.356	1.34	0.264	1.00	1.00	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
49	3.22	0.18	0.00	0.18	0.99	0.356	1.34	0.264	1.00	1.00	2.000	No
50	3.32	0.19	0.00	0.19	0.99	0.355	1.34	0.264	1.00	1.00	2.000	No
51	3.37	0.19	0.00	0.19	0.99	0.355	1.34	0.264	1.00	1.00	2.000	No
52	3.42	0.19	0.00	0.19	0.99	0.355	1.34	0.264	1.00	1.00	2.000	No
53	3.52	0.20	0.00	0.20	0.99	0.355	1.34	0.264	1.00	1.00	2.000	No
54	3.57	0.20	0.00	0.20	0.99	0.355	1.34	0.264	1.00	1.00	2.000	No
55	3.61	0.20	0.00	0.20	0.99	0.355	1.34	0.264	1.00	1.00	2.000	No
56	3.68	0.21	0.00	0.21	0.99	0.355	1.34	0.264	1.00	1.00	2.000	No
57	3.77	0.21	0.00	0.21	0.99	0.355	1.34	0.264	1.00	1.00	2.000	No
58	3.83	0.22	0.00	0.22	0.99	0.355	1.34	0.264	1.00	1.00	2.000	No
59	3.91	0.22	0.00	0.22	0.99	0.355	1.34	0.264	1.00	1.00	2.000	No
60	3.95	0.22	0.00	0.22	0.99	0.355	1.34	0.264	1.00	1.00	2.000	No
61	4.02	0.23	0.00	0.23	0.99	0.355	1.34	0.264	1.00	1.00	2.000	No
62	4.12	0.23	0.00	0.23	0.99	0.355	1.34	0.264	1.00	1.00	2.000	No
63	4.14	0.23	0.00	0.23	0.99	0.355	1.34	0.264	1.00	1.00	2.000	No
64	4.22	0.24	0.00	0.24	0.99	0.355	1.34	0.264	1.00	1.00	2.000	No
65	4.27	0.24	0.00	0.24	0.99	0.355	1.34	0.264	1.00	1.00	2.000	No
66	4.37	0.25	0.00	0.25	0.99	0.355	1.34	0.264	1.00	1.00	2.000	No
67	4.42	0.25	0.00	0.25	0.99	0.354	1.34	0.264	1.00	1.00	2.000	No
68	4.46	0.25	0.00	0.25	0.99	0.354	1.34	0.264	1.00	1.00	2.000	No
69	4.57	0.26	0.00	0.26	0.99	0.354	1.34	0.264	1.00	1.00	2.000	No
70	4.61	0.26	0.00	0.26	0.99	0.354	1.34	0.264	1.00	1.00	2.000	No
71	4.67	0.26	0.00	0.26	0.99	0.354	1.34	0.263	1.00	1.00	2.000	No
72	4.76	0.27	0.00	0.27	0.99	0.354	1.34	0.263	1.00	1.00	2.000	No
73	4.81	0.27	0.00	0.27	0.99	0.354	1.34	0.263	1.00	1.00	2.000	No
74	4.90	0.28	0.00	0.28	0.99	0.354	1.34	0.263	1.00	1.00	2.000	No
75	4.96	0.28	0.00	0.28	0.99	0.354	1.34	0.263	1.00	1.00	2.000	No
76	5.00	0.28	0.00	0.28	0.99	0.354	1.34	0.263	1.00	1.00	2.000	No
77	5.05	0.28	0.00	0.28	0.99	0.354	1.34	0.263	1.00	1.00	2.000	No
78	5.14	0.29	0.00	0.29	0.99	0.354	1.34	0.263	1.00	1.00	2.000	No
79	5.20	0.29	0.00	0.29	0.99	0.354	1.34	0.263	1.00	1.00	2.000	No
80	5.30	0.30	0.00	0.30	0.99	0.354	1.34	0.263	1.00	1.00	2.000	No
81	5.35	0.30	0.00	0.30	0.99	0.354	1.34	0.263	1.00	1.00	2.000	No
82	5.39	0.30	0.00	0.30	0.99	0.354	1.34	0.263	1.00	1.00	2.000	No
83	5.48	0.31	0.00	0.31	0.99	0.354	1.34	0.263	1.00	1.00	2.000	No
84	5.55	0.31	0.00	0.31	0.99	0.354	1.34	0.263	1.00	1.00	2.000	No
85	5.59	0.31	0.00	0.31	0.99	0.354	1.34	0.263	1.00	1.00	2.000	No
86	5.64	0.32	0.00	0.32	0.99	0.353	1.34	0.263	1.00	1.00	2.000	No
87	5.74	0.32	0.00	0.32	0.99	0.353	1.34	0.263	1.00	1.00	2.000	No
88	5.79	0.32	0.00	0.32	0.99	0.353	1.34	0.263	1.00	1.00	2.000	No
89	5.84	0.33	0.00	0.33	0.99	0.353	1.34	0.263	1.00	1.00	2.000	No
90	5.94	0.33	0.00	0.33	0.99	0.353	1.34	0.263	1.00	1.00	2.000	No
91	5.97	0.33	0.00	0.33	0.99	0.353	1.34	0.263	1.00	1.00	2.000	No
92	6.05	0.34	0.00	0.34	0.99	0.353	1.34	0.263	1.00	1.00	2.000	No
93	6.14	0.34	0.00	0.34	0.99	0.353	1.34	0.263	1.00	1.00	2.000	No
94	6.19	0.35	0.00	0.35	0.99	0.353	1.34	0.263	1.00	1.00	2.000	No
95	6.24	0.35	0.00	0.35	0.99	0.353	1.34	0.263	1.00	1.00	2.000	No
96	6.33	0.35	0.00	0.35	0.99	0.353	1.34	0.262	1.00	1.00	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
97	6.38	0.36	0.00	0.36	0.99	0.353	1.34	0.262	1.00	1.00	2.000	No
98	6.44	0.36	0.00	0.36	0.99	0.353	1.34	0.262	1.00	1.00	2.000	No
99	6.52	0.36	0.00	0.36	0.99	0.353	1.34	0.262	1.00	1.00	2.000	No
100	6.59	0.37	0.00	0.37	0.99	0.353	1.34	0.262	1.00	1.00	2.000	No
101	6.64	0.37	0.00	0.37	0.99	0.353	1.34	0.262	1.00	1.00	2.000	No
102	6.70	0.37	0.00	0.37	0.99	0.353	1.34	0.262	1.00	1.00	2.000	No
103	6.78	0.38	0.00	0.38	0.99	0.353	1.34	0.262	1.00	1.00	2.000	No
104	6.83	0.38	0.00	0.38	0.99	0.353	1.34	0.262	1.00	1.00	2.000	No
105	6.89	0.39	0.00	0.39	0.99	0.352	1.34	0.262	1.00	1.00	2.000	No
106	6.98	0.39	0.00	0.39	0.99	0.352	1.34	0.262	1.00	1.00	2.000	No
107	7.03	0.39	0.00	0.39	0.99	0.352	1.34	0.262	1.00	1.00	2.000	No
108	7.09	0.40	0.00	0.40	0.99	0.352	1.34	0.262	1.00	1.00	2.000	No
109	7.18	0.40	0.00	0.40	0.99	0.352	1.34	0.262	1.00	1.00	2.000	No
110	7.23	0.40	0.00	0.40	0.99	0.352	1.34	0.262	1.00	1.00	2.000	No
111	7.29	0.41	0.00	0.41	0.99	0.352	1.34	0.262	1.00	1.00	2.000	No
112	7.38	0.41	0.00	0.41	0.98	0.352	1.34	0.262	1.00	1.00	2.000	No
113	7.42	0.41	0.00	0.41	0.98	0.352	1.34	0.262	1.00	1.00	2.000	No
114	7.48	0.42	0.00	0.42	0.98	0.352	1.34	0.262	1.00	1.00	2.000	No
115	7.58	0.42	0.00	0.42	0.98	0.352	1.34	0.262	1.00	1.00	2.000	No
116	7.62	0.43	0.00	0.43	0.98	0.352	1.34	0.262	1.00	1.00	2.000	No
117	7.68	0.43	0.00	0.43	0.98	0.352	1.34	0.262	1.00	1.00	2.000	No
118	7.78	0.43	0.00	0.43	0.98	0.352	1.34	0.262	1.00	1.00	2.000	No
119	7.81	0.44	0.00	0.44	0.98	0.352	1.34	0.262	1.00	1.00	2.000	No
120	7.88	0.44	0.00	0.44	0.98	0.352	1.34	0.262	1.00	1.00	2.000	No
121	7.97	0.44	0.00	0.44	0.98	0.352	1.34	0.262	1.00	1.00	2.000	No
122	8.01	0.45	0.00	0.45	0.98	0.352	1.34	0.261	1.00	1.00	2.000	No
123	8.11	0.45	0.00	0.45	0.98	0.352	1.34	0.261	1.00	1.00	2.000	No
124	8.14	0.45	0.00	0.45	0.98	0.351	1.34	0.261	1.00	1.00	2.000	No
125	8.22	0.46	0.00	0.46	0.98	0.351	1.34	0.261	1.00	1.00	2.000	No
126	8.31	0.46	0.00	0.46	0.98	0.351	1.34	0.261	1.00	1.00	2.000	No
127	8.35	0.47	0.00	0.47	0.98	0.351	1.34	0.261	1.00	1.00	2.000	No
128	8.41	0.47	0.00	0.47	0.98	0.351	1.34	0.261	1.00	1.00	2.000	No
129	8.50	0.47	0.00	0.47	0.98	0.351	1.34	0.261	1.00	1.00	2.000	No
130	8.56	0.48	0.00	0.48	0.98	0.351	1.34	0.261	1.00	1.00	2.000	No
131	8.61	0.48	0.00	0.48	0.98	0.351	1.34	0.261	1.00	1.00	2.000	No
132	8.68	0.48	0.00	0.48	0.98	0.351	1.34	0.261	1.00	1.00	2.000	No
133	8.75	0.49	0.00	0.49	0.98	0.351	1.34	0.261	1.00	1.00	2.000	No
134	8.80	0.49	0.00	0.49	0.98	0.351	1.34	0.261	1.00	1.00	2.000	No
135	8.89	0.49	0.00	0.49	0.98	0.351	1.34	0.261	1.00	1.00	2.000	No
136	8.94	0.50	0.00	0.50	0.98	0.351	1.34	0.261	1.00	1.00	2.000	No
137	9.00	0.50	0.00	0.50	0.98	0.351	1.34	0.261	1.00	1.00	2.000	No
138	9.08	0.50	0.00	0.50	0.98	0.352	1.34	0.262	1.00	1.00	0.262	No
139	9.15	0.51	0.00	0.50	0.98	0.354	1.34	0.263	1.00	1.00	0.263	No
140	9.20	0.51	0.01	0.50	0.98	0.355	1.34	0.264	1.00	1.00	0.264	No
141	9.28	0.52	0.01	0.51	0.98	0.357	1.34	0.265	1.00	1.00	0.265	No
142	9.35	0.52	0.01	0.51	0.98	0.358	1.34	0.266	1.00	1.00	0.266	No
143	9.40	0.52	0.01	0.51	0.98	0.359	1.34	0.267	1.00	1.00	0.267	No
144	9.45	0.52	0.01	0.51	0.98	0.360	1.34	0.268	1.00	1.00	0.268	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
145	9.55	0.53	0.02	0.51	0.98	0.362	1.34	0.269	1.00	1.00	0.269	No
146	9.59	0.53	0.02	0.51	0.98	0.363	1.34	0.270	1.00	1.00	0.270	No
147	9.69	0.54	0.02	0.52	0.98	0.365	1.34	0.271	1.00	1.00	0.271	No
148	9.74	0.54	0.02	0.52	0.98	0.366	1.34	0.272	1.00	1.00	0.272	No
149	9.79	0.54	0.02	0.52	0.98	0.367	1.34	0.273	1.00	1.00	0.273	No
150	9.84	0.55	0.03	0.52	0.98	0.368	1.34	0.274	1.00	1.00	0.274	No
151	9.94	0.55	0.03	0.52	0.98	0.370	1.34	0.275	1.00	1.00	0.275	No
152	10.00	0.55	0.03	0.52	0.98	0.371	1.34	0.276	1.00	1.00	0.276	No
153	10.09	0.56	0.03	0.53	0.98	0.373	1.34	0.277	1.00	1.00	0.277	No
154	10.13	0.56	0.04	0.53	0.98	0.373	1.34	0.278	1.00	1.00	0.278	No
155	10.18	0.56	0.04	0.53	0.98	0.374	1.34	0.278	1.00	1.00	0.278	No
156	10.24	0.57	0.04	0.53	0.98	0.375	1.34	0.279	1.00	1.00	0.279	No
157	10.33	0.57	0.04	0.53	0.98	0.377	1.34	0.280	1.00	1.00	0.280	No
158	10.37	0.58	0.04	0.53	0.98	0.378	1.34	0.281	1.00	1.00	0.281	No
159	10.43	0.58	0.04	0.53	0.98	0.379	1.34	0.282	1.00	1.00	0.282	No
160	10.52	0.58	0.05	0.54	0.98	0.381	1.34	0.283	1.00	1.00	0.283	No
161	10.59	0.59	0.05	0.54	0.98	0.382	1.34	0.284	1.00	1.00	0.284	No
162	10.64	0.59	0.05	0.54	0.98	0.383	1.34	0.285	1.00	1.00	0.285	No
163	10.70	0.59	0.05	0.54	0.98	0.384	1.34	0.285	1.00	1.00	0.285	No
164	10.78	0.60	0.06	0.54	0.98	0.385	1.34	0.286	1.00	1.00	0.286	No
165	10.83	0.60	0.06	0.55	0.98	0.386	1.34	0.287	1.00	1.00	0.287	No
166	10.94	0.61	0.06	0.55	0.98	0.388	1.34	0.288	1.00	1.00	0.288	No
167	10.99	0.61	0.06	0.55	0.98	0.389	1.34	0.289	1.00	1.00	0.289	No
168	11.03	0.61	0.06	0.55	0.98	0.389	1.34	0.290	1.00	1.00	0.290	No
169	11.09	0.62	0.07	0.55	0.98	0.390	1.34	0.290	1.00	1.00	0.290	No
170	11.17	0.62	0.07	0.55	0.98	0.392	1.34	0.291	1.00	1.00	0.291	No
171	11.24	0.63	0.07	0.56	0.98	0.393	1.34	0.292	1.00	1.00	0.292	No
172	11.33	0.63	0.07	0.56	0.98	0.394	1.34	0.293	1.00	1.00	0.293	No
173	11.37	0.63	0.07	0.56	0.98	0.395	1.34	0.294	1.00	1.00	0.294	No
174	11.44	0.64	0.08	0.56	0.98	0.396	1.34	0.295	1.00	1.00	0.295	No
175	11.52	0.64	0.08	0.56	0.98	0.397	1.34	0.296	1.00	1.00	0.296	No
176	11.57	0.65	0.08	0.57	0.98	0.398	1.34	0.296	1.00	1.00	0.296	No
177	11.63	0.65	0.08	0.57	0.98	0.399	1.34	0.297	1.00	1.00	0.297	No
178	11.72	0.66	0.08	0.57	0.98	0.401	1.34	0.298	1.00	1.00	0.298	No
179	11.76	0.66	0.09	0.57	0.98	0.401	1.34	0.298	1.00	1.00	0.298	No
180	11.83	0.66	0.09	0.57	0.98	0.402	1.34	0.299	1.00	1.00	0.299	No
181	11.92	0.67	0.09	0.58	0.98	0.404	1.34	0.300	1.00	1.00	0.300	No
182	11.94	0.67	0.09	0.58	0.98	0.404	1.34	0.301	1.00	1.00	0.301	No
183	12.02	0.67	0.09	0.58	0.97	0.405	1.34	0.301	1.00	1.00	0.301	No
184	12.11	0.68	0.10	0.58	0.97	0.407	1.34	0.302	1.00	1.00	0.302	No
185	12.16	0.68	0.10	0.58	0.97	0.407	1.34	0.303	1.00	1.00	0.303	No
186	12.22	0.68	0.10	0.58	0.97	0.408	1.34	0.304	1.00	1.00	0.304	No
187	12.31	0.69	0.10	0.59	0.97	0.410	1.34	0.305	1.00	1.00	0.305	No
188	12.36	0.69	0.10	0.59	0.97	0.410	1.34	0.305	1.00	1.00	0.305	No
189	12.42	0.70	0.11	0.59	0.97	0.411	1.34	0.306	1.00	1.00	0.306	No
190	12.50	0.70	0.11	0.59	0.97	0.412	1.34	0.307	1.00	1.00	0.307	No
191	12.56	0.70	0.11	0.59	0.97	0.413	1.34	0.307	1.00	1.00	0.307	No
192	12.62	0.71	0.11	0.59	0.97	0.414	1.34	0.308	1.00	1.00	0.308	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
193	12.70	0.71	0.12	0.60	0.97	0.415	1.34	0.309	1.00	1.00	0.309	No
194	12.77	0.72	0.12	0.60	0.97	0.416	1.34	0.310	1.00	1.00	0.310	No
195	12.81	0.72	0.12	0.60	0.97	0.417	1.34	0.310	1.00	1.00	0.310	No
196	12.91	0.73	0.12	0.60	0.97	0.418	1.34	0.311	1.00	1.00	0.311	No
197	12.96	0.73	0.12	0.60	0.97	0.419	1.34	0.312	1.00	1.00	0.312	No
198	13.01	0.73	0.13	0.61	0.97	0.420	1.34	0.312	1.00	1.00	0.312	No
199	13.06	0.73	0.13	0.61	0.97	0.420	1.34	0.313	1.00	1.00	0.313	No
200	13.16	0.74	0.13	0.61	0.97	0.422	1.34	0.314	1.00	1.00	0.314	No
201	13.21	0.74	0.13	0.61	0.97	0.422	1.34	0.314	1.00	1.00	0.314	No
202	13.26	0.75	0.13	0.61	0.97	0.423	1.34	0.315	1.00	1.00	0.315	No
203	13.36	0.75	0.14	0.62	0.97	0.424	1.34	0.316	1.00	1.00	0.316	No
204	13.40	0.75	0.14	0.62	0.97	0.425	1.34	0.316	1.00	1.00	0.316	No
205	13.46	0.76	0.14	0.62	0.97	0.426	1.34	0.317	1.00	1.00	0.317	No
206	13.55	0.76	0.14	0.62	0.97	0.427	1.34	0.317	1.00	1.00	0.317	No
207	13.60	0.77	0.14	0.62	0.97	0.427	1.34	0.318	1.00	1.00	0.318	No
208	13.67	0.77	0.15	0.62	0.97	0.428	1.34	0.319	1.00	1.00	0.319	No
209	13.75	0.77	0.15	0.63	0.97	0.429	1.34	0.319	1.00	1.00	0.319	No
210	13.80	0.78	0.15	0.63	0.97	0.430	1.34	0.320	1.00	1.00	0.320	No
211	13.86	0.78	0.15	0.63	0.97	0.431	1.34	0.320	1.00	1.00	0.320	No
212	13.95	0.79	0.15	0.63	0.97	0.432	1.34	0.321	1.00	1.00	0.321	No
213	13.99	0.79	0.16	0.63	0.97	0.432	1.34	0.322	1.00	1.00	0.322	No
214	14.06	0.79	0.16	0.64	0.97	0.433	1.34	0.322	1.00	1.00	0.322	No
215	14.15	0.80	0.16	0.64	0.97	0.434	1.34	0.323	1.00	1.00	0.323	No
216	14.19	0.80	0.16	0.64	0.97	0.435	1.34	0.323	1.00	1.00	0.323	No
217	14.26	0.80	0.16	0.64	0.97	0.436	1.34	0.324	1.00	1.00	0.324	No
218	14.35	0.81	0.17	0.64	0.97	0.437	1.34	0.325	1.00	1.00	0.325	No
219	14.40	0.81	0.17	0.64	0.97	0.437	1.34	0.325	1.00	1.00	0.325	No
220	14.45	0.82	0.17	0.65	0.97	0.438	1.34	0.326	1.00	1.00	0.326	No
221	14.55	0.82	0.17	0.65	0.97	0.439	1.34	0.327	1.00	1.00	0.327	No
222	14.58	0.82	0.17	0.65	0.97	0.439	1.34	0.327	1.00	1.00	0.327	No
223	14.65	0.83	0.18	0.65	0.97	0.440	1.34	0.327	1.00	1.00	0.327	No
224	14.74	0.83	0.18	0.65	0.97	0.441	1.34	0.328	1.00	1.00	0.328	No
225	14.77	0.83	0.18	0.65	0.97	0.442	1.34	0.329	1.00	1.00	0.329	No
226	14.84	0.84	0.18	0.66	0.97	0.443	1.34	0.329	1.00	1.00	0.329	No
227	14.94	0.84	0.19	0.66	0.97	0.444	1.34	0.330	1.00	1.00	0.330	No
228	15.00	0.85	0.19	0.66	0.97	0.444	1.34	0.331	1.00	1.00	0.331	No
229	15.03	0.85	0.19	0.66	0.97	0.445	1.34	0.331	1.00	1.00	0.331	No
230	15.11	0.85	0.19	0.66	0.97	0.446	1.34	0.331	1.00	1.00	0.331	No
231	15.19	0.86	0.19	0.67	0.97	0.447	1.34	0.332	1.00	1.00	0.332	No
232	15.24	0.86	0.19	0.67	0.97	0.447	1.34	0.333	1.00	1.00	0.333	No
233	15.29	0.86	0.20	0.67	0.97	0.448	1.34	0.333	1.00	1.00	0.333	No
234	15.39	0.87	0.20	0.67	0.97	0.449	1.34	0.334	1.00	1.00	0.334	No
235	15.42	0.87	0.20	0.67	0.97	0.449	1.34	0.334	1.00	1.00	0.334	No
236	15.49	0.88	0.20	0.67	0.97	0.450	1.34	0.335	1.00	1.00	0.335	No
237	15.59	0.88	0.21	0.68	0.97	0.451	1.34	0.335	1.00	1.00	0.335	No
238	15.63	0.88	0.21	0.68	0.97	0.451	1.34	0.336	1.00	1.00	0.336	No
239	15.69	0.89	0.21	0.68	0.97	0.452	1.34	0.336	1.00	1.00	0.336	No
240	15.78	0.89	0.21	0.68	0.97	0.453	1.34	0.337	1.00	1.00	0.337	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
241	15.84	0.90	0.21	0.68	0.97	0.454	1.34	0.337	1.00	1.00	0.337	No
242	15.89	0.90	0.21	0.68	0.97	0.454	1.34	0.338	1.00	1.00	0.338	No
243	15.95	0.90	0.22	0.68	0.97	0.455	1.34	0.338	1.00	1.00	0.338	No
244	16.04	0.91	0.22	0.69	0.97	0.456	1.34	0.339	1.00	1.00	0.339	No
245	16.08	0.91	0.22	0.69	0.97	0.456	1.34	0.339	1.00	1.00	0.339	No
246	16.18	0.91	0.22	0.69	0.97	0.457	1.34	0.340	1.00	1.00	0.340	No
247	16.24	0.92	0.23	0.69	0.97	0.458	1.34	0.341	1.00	1.00	0.341	No
248	16.28	0.92	0.23	0.69	0.97	0.458	1.34	0.341	1.00	1.00	0.341	No
249	16.36	0.92	0.23	0.69	0.97	0.459	1.34	0.342	1.00	1.00	0.342	No
250	16.43	0.93	0.23	0.70	0.97	0.460	1.34	0.342	1.00	1.00	0.342	No
251	16.47	0.93	0.23	0.70	0.97	0.460	1.34	0.342	1.00	1.00	0.342	No
252	16.54	0.93	0.24	0.70	0.97	0.461	1.34	0.343	1.00	1.00	0.343	No
253	16.63	0.94	0.24	0.70	0.96	0.462	1.34	0.344	1.00	1.00	0.344	No
254	16.68	0.94	0.24	0.70	0.96	0.463	1.34	0.344	1.00	1.00	0.344	No
255	16.78	0.95	0.24	0.70	0.96	0.464	1.34	0.345	1.00	1.00	0.345	No
256	16.83	0.95	0.24	0.71	0.96	0.464	1.34	0.345	1.00	1.00	0.345	No
257	16.87	0.95	0.25	0.71	0.96	0.465	1.34	0.345	1.00	1.00	0.345	No
258	16.93	0.96	0.25	0.71	0.96	0.465	1.34	0.346	1.00	1.00	0.346	No
259	17.01	0.96	0.25	0.71	0.96	0.466	1.34	0.347	1.00	1.00	0.347	No
260	17.09	0.96	0.25	0.71	0.96	0.467	1.34	0.347	1.00	1.00	0.347	No
261	17.15	0.97	0.25	0.71	0.96	0.467	1.34	0.348	1.00	1.00	0.348	No
262	17.20	0.97	0.26	0.72	0.96	0.468	1.34	0.348	1.00	1.00	0.348	No
263	17.27	0.97	0.26	0.72	0.96	0.468	1.34	0.348	1.00	1.00	0.348	No
264	17.35	0.98	0.26	0.72	0.96	0.469	1.34	0.349	1.00	1.00	0.349	No
265	17.40	0.98	0.26	0.72	0.96	0.470	1.34	0.349	1.00	1.00	0.349	No
266	17.45	0.98	0.26	0.72	0.96	0.470	1.34	0.350	1.00	1.00	0.350	No
267	17.55	0.99	0.27	0.72	0.96	0.471	1.34	0.350	1.00	1.00	0.350	No
268	17.59	0.99	0.27	0.72	0.96	0.471	1.34	0.351	1.00	1.00	0.351	No
269	17.65	1.00	0.27	0.73	0.96	0.472	1.34	0.351	1.00	1.00	0.351	No
270	17.75	1.00	0.27	0.73	0.96	0.473	1.34	0.352	1.00	1.00	0.352	No
271	17.79	1.00	0.27	0.73	0.96	0.473	1.34	0.352	1.00	1.00	0.352	No
272	17.87	1.01	0.28	0.73	0.96	0.474	1.34	0.353	1.00	1.00	0.353	No
273	17.94	1.01	0.28	0.73	0.96	0.475	1.34	0.353	1.00	1.00	0.353	No
274	17.98	1.01	0.28	0.73	0.96	0.475	1.34	0.353	1.00	1.00	0.353	No
275	18.05	1.02	0.28	0.74	0.96	0.476	1.34	0.354	1.00	1.00	0.354	No
276	18.14	1.02	0.29	0.74	0.96	0.477	1.34	0.354	1.00	1.00	0.354	No
277	18.18	1.03	0.29	0.74	0.96	0.477	1.34	0.355	1.00	1.00	0.355	No
278	18.24	1.03	0.29	0.74	0.96	0.477	1.34	0.355	1.00	1.00	0.355	No
279	18.34	1.03	0.29	0.74	0.96	0.478	1.34	0.356	1.00	1.00	0.356	No
280	18.39	1.04	0.29	0.74	0.96	0.479	1.34	0.356	1.00	1.00	0.356	No
281	18.44	1.04	0.29	0.75	0.96	0.479	1.34	0.356	1.00	1.00	0.356	No
282	18.54	1.05	0.30	0.75	0.96	0.480	1.34	0.357	1.00	1.00	0.357	No
283	18.59	1.05	0.30	0.75	0.96	0.480	1.34	0.357	1.00	1.00	0.357	No
284	18.64	1.05	0.30	0.75	0.96	0.481	1.34	0.358	1.00	1.00	0.358	No
285	18.74	1.06	0.30	0.75	0.96	0.482	1.34	0.358	1.00	1.00	0.358	No
286	18.79	1.06	0.31	0.75	0.96	0.482	1.34	0.359	1.00	1.00	0.359	No
287	18.84	1.06	0.31	0.76	0.96	0.483	1.34	0.359	1.00	1.00	0.359	No
288	18.92	1.07	0.31	0.76	0.96	0.483	1.34	0.359	1.00	1.00	0.359	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
289	18.97	1.07	0.31	0.76	0.96	0.484	1.34	0.360	1.00	1.00	0.360	No
290	19.04	1.07	0.31	0.76	0.96	0.484	1.34	0.360	1.00	1.00	0.360	No
291	19.14	1.08	0.32	0.76	0.96	0.485	1.34	0.361	1.00	1.00	0.361	No
292	19.17	1.08	0.32	0.76	0.96	0.485	1.34	0.361	1.00	1.00	0.361	No
293	19.24	1.08	0.32	0.77	0.96	0.486	1.34	0.361	1.00	1.00	0.361	No
294	19.34	1.09	0.32	0.77	0.96	0.487	1.34	0.362	1.00	1.00	0.362	No
295	19.39	1.09	0.32	0.77	0.96	0.487	1.34	0.362	1.00	1.00	0.362	No
296	19.43	1.10	0.33	0.77	0.96	0.487	1.34	0.363	1.00	1.00	0.363	No
297	19.52	1.10	0.33	0.77	0.96	0.488	1.34	0.363	1.00	1.00	0.363	No
298	19.56	1.10	0.33	0.77	0.96	0.489	1.34	0.363	1.00	1.00	0.363	No
299	19.63	1.11	0.33	0.77	0.96	0.489	1.34	0.364	1.00	1.00	0.364	No
300	19.73	1.11	0.33	0.78	0.96	0.490	1.34	0.364	1.00	1.00	0.364	No
301	19.78	1.11	0.34	0.78	0.96	0.490	1.34	0.365	1.00	1.00	0.365	No
302	19.83	1.12	0.34	0.78	0.96	0.491	1.34	0.365	1.00	1.00	0.365	No
303	19.90	1.12	0.34	0.78	0.96	0.491	1.34	0.365	1.00	1.00	0.365	No
304	19.96	1.12	0.34	0.78	0.96	0.492	1.34	0.366	1.00	1.00	0.366	No
305	20.03	1.13	0.34	0.78	0.96	0.492	1.34	0.366	1.00	1.00	0.366	No
306	20.09	1.13	0.35	0.79	0.96	0.493	1.34	0.366	1.00	1.00	0.366	No
307	20.16	1.14	0.35	0.79	0.96	0.493	1.34	0.367	1.00	1.00	0.367	No
308	20.23	1.14	0.35	0.79	0.96	0.494	1.34	0.367	1.00	1.00	0.367	No
309	20.31	1.14	0.35	0.79	0.96	0.494	1.34	0.368	1.00	1.00	0.368	No
310	20.35	1.15	0.35	0.79	0.96	0.495	1.34	0.368	1.00	1.00	0.368	No
311	20.42	1.15	0.36	0.79	0.96	0.495	1.34	0.368	1.00	1.00	0.368	No
312	20.50	1.15	0.36	0.80	0.96	0.496	1.34	0.369	1.00	1.00	0.369	No
313	20.55	1.16	0.36	0.80	0.96	0.496	1.34	0.369	1.00	1.00	0.369	No
314	20.62	1.16	0.36	0.80	0.96	0.497	1.34	0.369	1.00	1.00	0.369	No
315	20.70	1.17	0.37	0.80	0.96	0.497	1.34	0.370	1.00	1.00	0.370	No
316	20.75	1.17	0.37	0.80	0.95	0.497	1.34	0.370	1.00	1.00	0.370	No
317	20.82	1.17	0.37	0.80	0.95	0.498	1.34	0.370	1.00	1.00	0.370	No
318	20.90	1.18	0.37	0.81	0.95	0.498	1.34	0.371	1.00	1.00	0.371	No
319	20.96	1.18	0.37	0.81	0.95	0.499	1.34	0.371	1.00	1.00	0.371	No
320	21.01	1.18	0.37	0.81	0.95	0.499	1.34	0.371	1.00	1.00	0.371	No
321	21.11	1.19	0.38	0.81	0.95	0.500	1.34	0.372	1.00	1.00	0.372	No
322	21.15	1.19	0.38	0.81	0.95	0.500	1.34	0.372	1.00	1.00	0.372	No
323	21.21	1.19	0.38	0.81	0.95	0.501	1.34	0.372	1.00	1.00	0.372	No
324	21.27	1.20	0.38	0.82	0.95	0.501	1.34	0.373	1.00	1.00	0.373	No
325	21.36	1.20	0.39	0.82	0.95	0.502	1.34	0.373	1.00	1.00	0.373	No
326	21.40	1.21	0.39	0.82	0.95	0.502	1.34	0.373	1.00	1.00	0.373	No
327	21.51	1.21	0.39	0.82	0.95	0.503	1.34	0.374	1.00	1.00	0.374	No
328	21.55	1.21	0.39	0.82	0.95	0.503	1.34	0.374	1.00	1.00	0.374	No
329	21.60	1.22	0.39	0.82	0.95	0.503	1.34	0.374	1.00	1.00	0.374	No
330	21.69	1.22	0.40	0.83	0.95	0.504	1.34	0.375	1.00	1.00	0.375	No
331	21.75	1.23	0.40	0.83	0.95	0.504	1.34	0.375	1.00	1.00	0.375	No
332	21.80	1.23	0.40	0.83	0.95	0.504	1.34	0.375	1.00	1.00	0.375	No
333	21.90	1.23	0.40	0.83	0.95	0.505	1.34	0.376	1.00	1.00	0.376	No
334	21.95	1.24	0.40	0.83	0.95	0.505	1.34	0.376	1.00	1.00	0.376	No
335	22.00	1.24	0.41	0.83	0.95	0.505	1.34	0.376	1.00	1.00	0.376	No
336	22.09	1.25	0.41	0.84	0.95	0.506	1.34	0.376	1.00	1.00	0.376	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
337	22.11	1.25	0.41	0.84	0.95	0.506	1.34	0.376	1.00	1.00	0.376	No
338	22.19	1.25	0.41	0.84	0.95	0.507	1.34	0.377	1.00	1.00	0.377	No
339	22.26	1.26	0.41	0.84	0.95	0.507	1.34	0.377	1.00	1.00	0.377	No
340	22.35	1.26	0.42	0.84	0.95	0.507	1.34	0.377	1.00	1.00	0.377	No
341	22.39	1.26	0.42	0.84	0.95	0.508	1.34	0.378	1.00	1.00	0.378	No
342	22.44	1.27	0.42	0.85	0.95	0.508	1.34	0.378	1.00	1.00	0.378	No
343	22.55	1.27	0.42	0.85	0.95	0.509	1.34	0.378	1.00	1.00	0.378	No
344	22.58	1.27	0.42	0.85	0.95	0.509	1.34	0.378	1.00	1.00	0.378	No
345	22.65	1.28	0.43	0.85	0.95	0.509	1.34	0.379	1.00	1.00	0.379	No
346	22.74	1.28	0.43	0.85	0.95	0.510	1.34	0.379	1.00	1.00	0.379	No
347	22.83	1.29	0.43	0.86	0.95	0.510	1.34	0.380	1.00	1.00	0.380	No
348	22.85	1.29	0.43	0.86	0.95	0.510	1.34	0.380	1.00	1.00	0.380	No
349	22.94	1.29	0.43	0.86	0.95	0.511	1.34	0.380	1.00	1.00	0.380	No
350	23.00	1.30	0.44	0.86	0.95	0.511	1.34	0.380	1.00	1.00	0.380	No
351	23.05	1.30	0.44	0.86	0.95	0.512	1.34	0.381	1.00	1.00	0.381	No
352	23.10	1.30	0.44	0.86	0.95	0.512	1.34	0.381	1.00	1.00	0.381	No
353	23.18	1.31	0.44	0.86	0.95	0.512	1.34	0.381	1.00	1.00	0.381	No
354	23.25	1.31	0.44	0.87	0.95	0.513	1.34	0.381	1.00	1.00	0.381	No
355	23.30	1.31	0.45	0.87	0.95	0.513	1.34	0.382	1.00	1.00	0.382	No
356	23.38	1.32	0.45	0.87	0.95	0.514	1.34	0.382	1.00	1.00	0.382	No
357	23.45	1.32	0.45	0.87	0.95	0.514	1.34	0.382	1.00	1.00	0.382	No
358	23.50	1.32	0.45	0.87	0.95	0.514	1.34	0.383	1.00	1.00	0.383	No
359	23.60	1.33	0.46	0.87	0.95	0.515	1.34	0.383	1.00	1.00	0.383	No
360	23.65	1.33	0.46	0.87	0.95	0.515	1.34	0.383	1.00	1.00	0.383	No
361	23.70	1.33	0.46	0.87	0.95	0.516	1.34	0.384	1.00	1.00	0.384	No
362	23.76	1.34	0.46	0.88	0.95	0.516	1.34	0.384	1.00	1.00	0.384	No
363	23.84	1.34	0.46	0.88	0.95	0.517	1.34	0.384	1.00	1.00	0.384	No
364	23.89	1.34	0.46	0.88	0.95	0.517	1.34	0.384	1.00	1.00	0.384	No
365	23.99	1.35	0.47	0.88	0.95	0.517	1.34	0.385	1.00	1.00	0.385	No
366	24.03	1.35	0.47	0.88	0.95	0.518	1.34	0.385	1.00	1.00	0.385	No
367	24.09	1.35	0.47	0.88	0.94	0.518	1.34	0.385	1.00	1.00	0.385	No
368	24.19	1.36	0.47	0.88	0.94	0.519	1.34	0.386	1.00	1.00	0.386	No
369	24.24	1.36	0.48	0.89	0.94	0.519	1.34	0.386	1.00	1.00	0.386	No
370	24.30	1.36	0.48	0.89	0.94	0.519	1.34	0.386	1.00	1.00	0.386	No
371	24.34	1.37	0.48	0.89	0.94	0.519	1.34	0.386	1.00	1.00	0.386	No
372	24.44	1.37	0.48	0.89	0.94	0.520	1.34	0.387	1.00	1.00	0.387	No
373	24.50	1.38	0.48	0.89	0.94	0.520	1.34	0.387	1.00	1.00	0.387	No
374	24.58	1.38	0.49	0.89	0.94	0.521	1.34	0.387	1.00	1.00	0.387	No
375	24.65	1.38	0.49	0.90	0.94	0.521	1.34	0.387	1.00	1.00	0.387	No
376	24.69	1.39	0.49	0.90	0.94	0.521	1.34	0.388	1.00	1.00	0.388	No
377	24.74	1.39	0.49	0.90	0.94	0.521	1.34	0.388	1.00	1.00	0.388	No
378	24.84	1.39	0.49	0.90	0.94	0.522	1.34	0.388	1.00	1.00	0.388	No
379	24.89	1.40	0.50	0.90	0.94	0.522	1.34	0.388	1.00	1.00	0.388	No
380	24.95	1.40	0.50	0.90	0.94	0.522	1.34	0.388	1.00	1.00	0.388	No
381	25.04	1.41	0.50	0.91	0.94	0.523	1.34	0.389	1.00	1.00	0.389	No
382	25.08	1.41	0.50	0.91	0.94	0.523	1.34	0.389	1.00	1.00	0.389	No
383	25.19	1.41	0.51	0.91	0.94	0.523	1.34	0.389	1.00	1.00	0.389	No
384	25.24	1.42	0.51	0.91	0.94	0.524	1.34	0.389	1.00	1.00	0.389	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
385	25.28	1.42	0.51	0.91	0.94	0.524	1.34	0.390	1.00	1.00	0.390	No
386	25.35	1.42	0.51	0.91	0.94	0.524	1.34	0.390	1.00	1.00	0.390	No
387	25.43	1.43	0.51	0.92	0.94	0.524	1.34	0.390	1.00	1.00	0.390	No
388	25.48	1.43	0.51	0.92	0.94	0.525	1.34	0.390	1.00	1.00	0.390	No
389	25.53	1.43	0.52	0.92	0.94	0.525	1.34	0.390	1.00	1.00	0.390	No
390	25.63	1.44	0.52	0.92	0.94	0.525	1.34	0.391	1.00	1.00	0.391	No
391	25.68	1.44	0.52	0.92	0.94	0.525	1.34	0.391	1.00	1.00	0.391	No
392	25.74	1.45	0.52	0.92	0.94	0.526	1.34	0.391	1.00	1.00	0.391	No
393	25.79	1.45	0.52	0.92	0.94	0.526	1.34	0.391	1.00	1.00	0.391	No
394	25.88	1.45	0.53	0.93	0.94	0.526	1.34	0.391	1.00	1.00	0.391	No
395	25.92	1.46	0.53	0.93	0.94	0.526	1.34	0.391	1.00	1.00	0.391	No
396	25.99	1.46	0.53	0.93	0.94	0.527	1.34	0.392	1.00	1.00	0.392	No
397	26.05	1.46	0.53	0.93	0.94	0.527	1.34	0.392	1.00	1.00	0.392	No
398	26.13	1.47	0.53	0.93	0.94	0.527	1.34	0.392	1.00	1.00	0.392	No
399	26.20	1.47	0.54	0.94	0.94	0.527	1.34	0.392	1.00	1.00	0.392	No
400	26.26	1.48	0.54	0.94	0.94	0.528	1.34	0.392	1.00	1.00	0.392	No
401	26.31	1.48	0.54	0.94	0.94	0.528	1.34	0.393	1.00	1.00	0.393	No
402	26.40	1.48	0.54	0.94	0.94	0.528	1.34	0.393	1.00	1.00	0.393	No
403	26.45	1.49	0.54	0.94	0.94	0.528	1.34	0.393	1.00	1.00	0.393	No
404	26.54	1.49	0.55	0.94	0.94	0.529	1.34	0.393	1.00	1.00	0.393	No
405	26.59	1.49	0.55	0.95	0.94	0.529	1.34	0.393	1.00	1.00	0.393	No
406	26.65	1.50	0.55	0.95	0.94	0.529	1.34	0.393	1.00	1.00	0.393	No
407	26.74	1.50	0.55	0.95	0.94	0.529	1.34	0.394	1.00	1.00	0.394	No
408	26.78	1.51	0.55	0.95	0.94	0.529	1.34	0.394	1.00	1.00	0.394	No
409	26.84	1.51	0.56	0.95	0.93	0.530	1.34	0.394	1.00	1.00	0.394	No
410	26.94	1.51	0.56	0.95	0.93	0.530	1.34	0.394	1.00	1.00	0.394	No
411	26.99	1.52	0.56	0.96	0.93	0.530	1.34	0.394	1.00	1.00	0.394	No
412	27.04	1.52	0.56	0.96	0.93	0.530	1.34	0.394	1.00	1.00	0.394	No
413	27.13	1.52	0.57	0.96	0.93	0.531	1.34	0.395	1.00	1.00	0.395	No
414	27.18	1.53	0.57	0.96	0.93	0.531	1.34	0.395	1.00	1.00	0.395	No
415	27.24	1.53	0.57	0.96	0.93	0.531	1.34	0.395	1.00	1.00	0.395	No
416	27.34	1.54	0.57	0.96	0.93	0.531	1.34	0.395	1.00	1.00	0.395	No
417	27.40	1.54	0.57	0.97	0.93	0.532	1.34	0.395	1.00	1.00	0.395	No
418	27.44	1.54	0.58	0.97	0.93	0.532	1.34	0.395	1.00	1.00	0.395	No
419	27.53	1.55	0.58	0.97	0.93	0.532	1.34	0.396	1.00	1.00	0.396	No
420	27.57	1.55	0.58	0.97	0.93	0.532	1.34	0.396	1.00	1.00	0.396	No
421	27.64	1.55	0.58	0.97	0.93	0.532	1.34	0.396	1.00	1.00	0.396	No
422	27.72	1.56	0.58	0.97	0.93	0.533	1.34	0.396	1.00	1.00	0.396	No
423	27.79	1.56	0.59	0.98	0.93	0.533	1.34	0.396	1.00	1.00	0.396	No
424	27.83	1.56	0.59	0.98	0.93	0.533	1.34	0.396	1.00	1.00	0.396	No
425	27.90	1.57	0.59	0.98	0.93	0.533	1.34	0.397	1.00	1.00	0.397	No
426	27.98	1.57	0.59	0.98	0.93	0.533	1.34	0.397	1.00	1.00	0.397	No
427	28.03	1.58	0.59	0.98	0.93	0.534	1.34	0.397	1.00	1.00	0.397	No
428	28.09	1.58	0.60	0.98	0.93	0.534	1.34	0.397	1.00	1.00	0.397	No
429	28.18	1.58	0.60	0.99	0.93	0.534	1.34	0.397	1.00	1.00	0.397	No
430	28.22	1.59	0.60	0.99	0.93	0.534	1.34	0.397	1.00	1.00	0.397	No
431	28.28	1.59	0.60	0.99	0.93	0.534	1.34	0.397	1.00	1.00	0.397	No
432	28.38	1.59	0.60	0.99	0.93	0.535	1.34	0.398	1.00	1.00	0.398	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
433	28.43	1.60	0.61	0.99	0.93	0.535	1.34	0.398	1.00	1.00	0.398	No
434	28.48	1.60	0.61	0.99	0.93	0.535	1.34	0.398	1.00	1.00	0.398	No
435	28.58	1.61	0.61	1.00	0.93	0.535	1.34	0.398	1.00	1.00	0.398	No
436	28.62	1.61	0.61	1.00	0.93	0.535	1.34	0.398	1.00	1.00	0.398	No
437	28.69	1.61	0.61	1.00	0.93	0.535	1.34	0.398	1.00	1.00	0.398	No
438	28.77	1.62	0.62	1.00	0.93	0.536	1.34	0.398	1.00	1.00	0.398	No
439	28.82	1.62	0.62	1.00	0.93	0.536	1.34	0.398	1.00	1.00	0.398	No
440	28.88	1.62	0.62	1.00	0.93	0.536	1.34	0.398	1.00	1.00	0.398	No
441	28.97	1.63	0.62	1.01	0.93	0.536	1.34	0.399	1.00	1.00	0.399	No
442	29.01	1.63	0.62	1.01	0.93	0.536	1.34	0.399	1.00	1.00	0.399	No
443	29.07	1.63	0.63	1.01	0.93	0.536	1.34	0.399	1.00	1.00	0.399	No
444	29.15	1.64	0.63	1.01	0.92	0.536	1.34	0.399	1.00	1.00	0.399	No
445	29.21	1.64	0.63	1.01	0.92	0.536	1.34	0.399	1.00	1.00	0.399	No
446	29.30	1.65	0.63	1.01	0.92	0.537	1.34	0.399	1.00	1.00	0.399	No
447	29.33	1.65	0.63	1.02	0.92	0.537	1.34	0.399	1.00	1.00	0.399	No
448	29.41	1.65	0.64	1.02	0.92	0.537	1.34	0.399	1.00	1.00	0.399	No
449	29.50	1.66	0.64	1.02	0.92	0.537	1.34	0.399	1.00	1.00	0.399	No
450	29.53	1.66	0.64	1.02	0.92	0.537	1.34	0.399	1.00	1.00	0.399	No
451	29.61	1.67	0.64	1.02	0.92	0.537	1.34	0.399	1.00	1.00	0.399	No
452	29.70	1.67	0.65	1.03	0.92	0.537	1.34	0.400	1.00	1.00	0.400	No
453	29.74	1.67	0.65	1.03	0.92	0.537	1.34	0.400	1.00	1.00	0.400	No
454	29.80	1.68	0.65	1.03	0.92	0.537	1.34	0.400	1.00	1.00	0.400	No
455	29.90	1.68	0.65	1.03	0.92	0.538	1.34	0.400	1.00	1.00	0.400	No
456	29.93	1.68	0.65	1.03	0.92	0.538	1.34	0.400	1.00	1.00	0.400	No
457	30.00	1.69	0.66	1.03	0.92	0.538	1.34	0.400	1.00	1.00	0.400	No
458	30.09	1.69	0.66	1.04	0.92	0.538	1.34	0.400	1.00	1.00	0.400	No
459	30.15	1.70	0.66	1.04	0.92	0.538	1.34	0.400	1.00	1.00	0.400	No
460	30.19	1.70	0.66	1.04	0.92	0.538	1.34	0.400	1.00	1.00	0.400	No
461	30.30	1.71	0.66	1.04	0.92	0.538	1.34	0.400	1.00	1.00	0.400	No
462	30.33	1.71	0.67	1.04	0.92	0.538	1.34	0.400	1.00	1.00	0.400	No
463	30.40	1.71	0.67	1.04	0.92	0.538	1.34	0.400	1.00	1.00	0.400	No
464	30.49	1.72	0.67	1.05	0.92	0.539	1.34	0.401	1.00	1.00	0.401	No
465	30.54	1.72	0.67	1.05	0.92	0.539	1.34	0.401	1.00	1.00	0.401	No
466	30.59	1.72	0.67	1.05	0.92	0.539	1.34	0.401	1.00	1.00	0.401	No
467	30.64	1.73	0.68	1.05	0.92	0.539	1.34	0.401	1.00	1.00	0.401	No
468	30.72	1.73	0.68	1.05	0.92	0.539	1.34	0.401	1.00	1.00	0.401	No
469	30.80	1.73	0.68	1.05	0.92	0.539	1.34	0.401	1.00	1.00	0.401	No
470	30.88	1.74	0.68	1.06	0.92	0.539	1.34	0.401	1.00	1.00	0.401	No
471	30.93	1.74	0.68	1.06	0.92	0.539	1.34	0.401	1.00	1.00	0.401	No
472	31.00	1.75	0.69	1.06	0.92	0.539	1.34	0.401	1.00	1.00	0.401	No
473	31.04	1.75	0.69	1.06	0.92	0.539	1.34	0.401	1.00	1.00	0.401	No
474	31.13	1.75	0.69	1.06	0.91	0.539	1.34	0.401	1.00	1.00	0.402	No
475	31.20	1.76	0.69	1.07	0.91	0.539	1.34	0.401	1.00	1.00	0.402	No
476	31.29	1.76	0.70	1.07	0.91	0.539	1.34	0.401	1.00	1.00	0.402	No
477	31.34	1.77	0.70	1.07	0.91	0.539	1.34	0.401	1.00	1.00	0.402	No
478	31.38	1.77	0.70	1.07	0.91	0.539	1.34	0.401	1.00	1.00	0.402	No
479	31.43	1.77	0.70	1.07	0.91	0.540	1.34	0.401	1.00	1.00	0.402	No
480	31.51	1.78	0.70	1.07	0.91	0.540	1.34	0.401	1.00	1.00	0.403	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
481	31.58	1.78	0.70	1.08	0.91	0.540	1.34	0.401	1.00	1.00	0.403	No
482	31.63	1.78	0.71	1.08	0.91	0.540	1.34	0.401	1.00	1.00	0.403	No
483	31.71	1.79	0.71	1.08	0.91	0.540	1.34	0.401	1.00	1.00	0.403	No
484	31.78	1.79	0.71	1.08	0.91	0.540	1.34	0.401	1.00	1.00	0.403	No
485	31.83	1.79	0.71	1.08	0.91	0.540	1.34	0.401	0.99	1.00	0.404	No
486	31.90	1.80	0.71	1.08	0.91	0.540	1.34	0.402	0.99	1.00	0.404	No
487	31.98	1.80	0.72	1.09	0.91	0.540	1.34	0.402	0.99	1.00	0.404	No
488	32.03	1.81	0.72	1.09	0.91	0.540	1.34	0.402	0.99	1.00	0.404	No
489	32.09	1.81	0.72	1.09	0.91	0.540	1.34	0.402	0.99	1.00	0.404	No
490	32.16	1.81	0.72	1.09	0.91	0.540	1.34	0.402	0.99	1.00	0.405	No
491	32.22	1.82	0.72	1.09	0.91	0.540	1.34	0.402	0.99	1.00	0.405	No
492	32.30	1.82	0.73	1.09	0.91	0.540	1.34	0.402	0.99	1.00	0.405	No
493	32.38	1.83	0.73	1.10	0.91	0.540	1.34	0.402	0.99	1.00	0.405	No
494	32.42	1.83	0.73	1.10	0.91	0.540	1.34	0.402	0.99	1.00	0.405	No
495	32.50	1.83	0.73	1.10	0.91	0.540	1.34	0.402	0.99	1.00	0.405	No
496	32.56	1.84	0.74	1.10	0.91	0.540	1.34	0.402	0.99	1.00	0.406	No
497	32.62	1.84	0.74	1.10	0.91	0.541	1.34	0.402	0.99	1.00	0.406	No
498	32.72	1.84	0.74	1.10	0.91	0.541	1.34	0.402	0.99	1.00	0.406	No
499	32.77	1.85	0.74	1.11	0.91	0.541	1.34	0.402	0.99	1.00	0.406	No
500	32.82	1.85	0.74	1.11	0.90	0.541	1.34	0.402	0.99	1.00	0.406	No
501	32.91	1.86	0.75	1.11	0.90	0.541	1.34	0.402	0.99	1.00	0.407	No
502	32.97	1.86	0.75	1.11	0.90	0.541	1.34	0.402	0.99	1.00	0.407	No
503	33.02	1.86	0.75	1.11	0.90	0.541	1.34	0.402	0.99	1.00	0.407	No
504	33.11	1.87	0.75	1.11	0.90	0.541	1.34	0.402	0.99	1.00	0.407	No
505	33.16	1.87	0.75	1.12	0.90	0.541	1.34	0.402	0.99	1.00	0.407	No
506	33.22	1.87	0.76	1.12	0.90	0.541	1.34	0.402	0.99	1.00	0.407	No
507	33.29	1.88	0.76	1.12	0.90	0.541	1.34	0.402	0.99	1.00	0.407	No
508	33.37	1.88	0.76	1.12	0.90	0.541	1.34	0.402	0.99	1.00	0.408	No
509	33.41	1.88	0.76	1.12	0.90	0.541	1.34	0.402	0.99	1.00	0.408	No
510	33.47	1.89	0.76	1.12	0.90	0.541	1.34	0.402	0.99	1.00	0.408	No
511	33.57	1.89	0.77	1.13	0.90	0.541	1.34	0.402	0.99	1.00	0.408	No
512	33.60	1.89	0.77	1.13	0.90	0.541	1.34	0.402	0.99	1.00	0.408	No
513	33.67	1.90	0.77	1.13	0.90	0.541	1.34	0.402	0.99	1.00	0.408	No
514	33.76	1.90	0.77	1.13	0.90	0.541	1.34	0.402	0.98	1.00	0.408	No
515	33.80	1.91	0.77	1.13	0.90	0.541	1.34	0.402	0.98	1.00	0.409	No
516	33.86	1.91	0.78	1.13	0.90	0.541	1.34	0.402	0.98	1.00	0.409	No
517	33.96	1.92	0.78	1.14	0.90	0.541	1.34	0.402	0.98	1.00	0.409	No
518	34.00	1.92	0.78	1.14	0.90	0.541	1.34	0.402	0.98	1.00	0.409	No
519	34.06	1.92	0.78	1.14	0.90	0.541	1.34	0.402	0.98	1.00	0.409	No
520	34.16	1.93	0.78	1.14	0.90	0.541	1.34	0.402	0.98	1.00	0.409	No
521	34.20	1.93	0.79	1.14	0.90	0.541	1.34	0.402	0.98	1.00	0.409	No
522	34.26	1.93	0.79	1.15	0.90	0.540	1.34	0.402	0.98	1.00	0.409	No
523	34.36	1.94	0.79	1.15	0.89	0.540	1.34	0.402	0.98	1.00	0.410	No
524	34.39	1.94	0.79	1.15	0.89	0.540	1.34	0.402	0.98	1.00	0.410	No
525	34.46	1.95	0.79	1.15	0.89	0.540	1.34	0.402	0.98	1.00	0.410	No
526	34.56	1.95	0.80	1.15	0.89	0.540	1.34	0.402	0.98	1.00	0.410	No
527	34.60	1.95	0.80	1.16	0.89	0.540	1.34	0.402	0.98	1.00	0.410	No
528	34.65	1.96	0.80	1.16	0.89	0.540	1.34	0.402	0.98	1.00	0.410	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
529	34.75	1.96	0.80	1.16	0.89	0.540	1.34	0.402	0.98	1.00	0.410	No
530	34.80	1.97	0.80	1.16	0.89	0.540	1.34	0.402	0.98	1.00	0.410	No
531	34.86	1.97	0.81	1.16	0.89	0.540	1.34	0.402	0.98	1.00	0.410	No
532	34.95	1.97	0.81	1.16	0.89	0.540	1.34	0.402	0.98	1.00	0.411	No
533	34.99	1.98	0.81	1.17	0.89	0.540	1.34	0.402	0.98	1.00	0.411	No
534	35.06	1.98	0.81	1.17	0.89	0.540	1.34	0.402	0.98	1.00	0.411	No
535	35.11	1.98	0.81	1.17	0.89	0.540	1.34	0.401	0.98	1.00	0.411	No
536	35.19	1.99	0.82	1.17	0.89	0.540	1.34	0.401	0.98	1.00	0.411	No
537	35.25	1.99	0.82	1.17	0.89	0.540	1.34	0.401	0.98	1.00	0.411	No
538	35.31	2.00	0.82	1.17	0.89	0.540	1.34	0.401	0.98	1.00	0.411	No
539	35.39	2.00	0.82	1.18	0.89	0.540	1.34	0.401	0.98	1.00	0.411	No
540	35.49	2.01	0.83	1.18	0.89	0.539	1.34	0.401	0.98	1.00	0.411	No
541	35.53	2.01	0.83	1.18	0.89	0.539	1.34	0.401	0.98	1.00	0.411	No
542	35.60	2.01	0.83	1.18	0.89	0.539	1.34	0.401	0.97	1.00	0.411	No
543	35.63	2.01	0.83	1.18	0.89	0.539	1.34	0.401	0.97	1.00	0.412	No
544	35.70	2.02	0.83	1.18	0.89	0.539	1.34	0.401	0.97	1.00	0.412	No
545	35.78	2.02	0.84	1.19	0.89	0.539	1.34	0.401	0.97	1.00	0.412	No
546	35.84	2.03	0.84	1.19	0.88	0.539	1.34	0.401	0.97	1.00	0.412	No
547	35.90	2.03	0.84	1.19	0.88	0.539	1.34	0.401	0.97	1.00	0.412	No
548	35.98	2.03	0.84	1.19	0.88	0.539	1.34	0.401	0.97	1.00	0.412	No
549	36.06	2.04	0.84	1.19	0.88	0.539	1.34	0.401	0.97	1.00	0.412	No
550	36.09	2.04	0.85	1.20	0.88	0.539	1.34	0.401	0.97	1.00	0.412	No
551	36.18	2.05	0.85	1.20	0.88	0.539	1.34	0.401	0.97	1.00	0.412	No
552	36.23	2.05	0.85	1.20	0.88	0.538	1.34	0.400	0.97	1.00	0.412	No
553	36.29	2.05	0.85	1.20	0.88	0.538	1.34	0.400	0.97	1.00	0.412	No
554	36.38	2.06	0.85	1.20	0.88	0.538	1.34	0.400	0.97	1.00	0.412	No
555	36.42	2.06	0.86	1.20	0.88	0.538	1.34	0.400	0.97	1.00	0.412	No
556	36.49	2.06	0.86	1.21	0.88	0.538	1.34	0.400	0.97	1.00	0.412	No
557	36.58	2.07	0.86	1.21	0.88	0.538	1.34	0.400	0.97	1.00	2.000	Yes
558	36.62	2.07	0.86	1.21	0.88	0.538	1.34	0.400	0.97	1.00	2.000	Yes
559	36.68	2.08	0.86	1.21	0.88	0.538	1.34	0.400	0.97	1.00	2.000	Yes
560	36.77	2.08	0.87	1.22	0.88	0.538	1.34	0.400	0.97	1.00	2.000	Yes
561	36.83	2.09	0.87	1.22	0.88	0.537	1.34	0.400	0.97	1.00	2.000	Yes
562	36.88	2.09	0.87	1.22	0.88	0.537	1.34	0.400	0.97	1.00	2.000	Yes
563	36.97	2.09	0.87	1.22	0.88	0.537	1.34	0.399	0.97	1.00	2.000	Yes
564	37.02	2.10	0.87	1.22	0.88	0.537	1.34	0.399	0.97	1.00	2.000	Yes
565	37.08	2.10	0.88	1.22	0.88	0.537	1.34	0.399	0.97	1.00	2.000	Yes
566	37.17	2.11	0.88	1.23	0.87	0.536	1.34	0.399	0.97	1.00	0.413	No
567	37.22	2.11	0.88	1.23	0.87	0.536	1.34	0.399	0.97	1.00	0.413	No
568	37.27	2.11	0.88	1.23	0.87	0.536	1.34	0.399	0.97	1.00	0.413	No
569	37.37	2.12	0.89	1.23	0.87	0.536	1.34	0.399	0.97	1.00	0.413	No
570	37.41	2.12	0.89	1.24	0.87	0.536	1.34	0.398	0.96	1.00	0.413	No
571	37.47	2.13	0.89	1.24	0.87	0.536	1.34	0.398	0.96	1.00	0.413	No
572	37.57	2.13	0.89	1.24	0.87	0.535	1.34	0.398	0.96	1.00	0.413	No
573	37.61	2.14	0.89	1.24	0.87	0.535	1.34	0.398	0.96	1.00	0.413	No
574	37.67	2.14	0.89	1.24	0.87	0.535	1.34	0.398	0.96	1.00	0.413	No
575	37.76	2.15	0.90	1.25	0.87	0.535	1.34	0.398	0.96	1.00	0.413	No
576	37.81	2.15	0.90	1.25	0.87	0.534	1.34	0.398	0.96	1.00	0.413	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
577	37.87	2.15	0.90	1.25	0.87	0.534	1.34	0.397	0.96	1.00	0.413	No
578	37.97	2.16	0.90	1.26	0.87	0.534	1.34	0.397	0.96	1.00	0.413	No
579	38.02	2.16	0.91	1.26	0.87	0.534	1.34	0.397	0.96	1.00	0.413	No
580	38.07	2.17	0.91	1.26	0.87	0.534	1.34	0.397	0.96	1.00	0.413	No
581	38.17	2.17	0.91	1.26	0.87	0.533	1.34	0.397	0.96	1.00	0.413	No
582	38.20	2.17	0.91	1.26	0.87	0.533	1.34	0.397	0.96	1.00	0.413	No
583	38.27	2.18	0.91	1.27	0.87	0.533	1.34	0.396	0.96	1.00	0.413	No
584	38.33	2.18	0.92	1.27	0.87	0.533	1.34	0.396	0.96	1.00	0.413	No
585	38.42	2.19	0.92	1.27	0.86	0.532	1.34	0.396	0.96	1.00	0.413	No
586	38.46	2.19	0.92	1.27	0.86	0.532	1.34	0.396	0.96	1.00	0.413	No
587	38.53	2.20	0.92	1.27	0.86	0.532	1.34	0.396	0.96	1.00	0.413	No
588	38.62	2.20	0.92	1.28	0.86	0.532	1.34	0.395	0.96	1.00	0.413	No
589	38.66	2.20	0.93	1.28	0.86	0.531	1.34	0.395	0.96	1.00	0.413	No
590	38.73	2.21	0.93	1.28	0.86	0.531	1.34	0.395	0.96	1.00	0.413	No
591	38.81	2.22	0.93	1.29	0.86	0.531	1.34	0.395	0.96	1.00	0.413	No
592	38.86	2.22	0.93	1.29	0.86	0.531	1.34	0.395	0.96	1.00	0.413	No
593	38.93	2.22	0.93	1.29	0.86	0.530	1.34	0.394	0.96	1.00	0.413	No
594	39.02	2.23	0.94	1.29	0.86	0.530	1.34	0.394	0.95	1.00	0.413	No
595	39.05	2.23	0.94	1.29	0.86	0.530	1.34	0.394	0.95	1.00	0.413	No
596	39.12	2.24	0.94	1.30	0.86	0.529	1.34	0.394	0.95	1.00	0.413	No
597	39.18	2.24	0.94	1.30	0.86	0.529	1.34	0.394	0.95	1.00	0.413	No
598	39.27	2.25	0.94	1.30	0.86	0.529	1.34	0.393	0.95	1.00	0.413	No
599	39.31	2.25	0.95	1.30	0.86	0.529	1.34	0.393	0.95	1.00	0.413	No
600	39.37	2.25	0.95	1.31	0.86	0.528	1.34	0.393	0.95	1.00	0.413	No
601	39.44	2.26	0.95	1.31	0.86	0.528	1.34	0.393	0.95	1.00	0.412	No
602	39.50	2.26	0.95	1.31	0.86	0.528	1.34	0.393	0.95	1.00	0.412	No
603	39.59	2.27	0.95	1.31	0.85	0.528	1.34	0.392	0.95	1.00	0.412	No
604	39.65	2.27	0.96	1.32	0.85	0.527	1.34	0.392	0.95	1.00	0.412	No
605	39.71	2.28	0.96	1.32	0.85	0.527	1.34	0.392	0.95	1.00	0.412	No
606	39.77	2.28	0.96	1.32	0.85	0.527	1.34	0.392	0.95	1.00	0.412	No
607	39.84	2.28	0.96	1.32	0.85	0.527	1.34	0.392	0.95	1.00	0.412	No
608	39.91	2.29	0.96	1.32	0.85	0.526	1.34	0.391	0.95	1.00	0.412	No
609	39.97	2.29	0.97	1.33	0.85	0.526	1.34	0.391	0.95	1.00	0.412	No
610	40.03	2.30	0.97	1.33	0.85	0.526	1.34	0.391	0.95	1.00	0.412	No
611	40.11	2.30	0.97	1.33	0.85	0.525	1.34	0.391	0.95	1.00	0.412	No
612	40.17	2.31	0.97	1.33	0.85	0.525	1.34	0.391	0.95	1.00	0.412	No
613	40.26	2.31	0.98	1.34	0.85	0.525	1.34	0.390	0.95	1.00	0.412	No
614	40.30	2.31	0.98	1.34	0.85	0.525	1.34	0.390	0.95	1.00	0.412	No
615	40.36	2.32	0.98	1.34	0.85	0.524	1.34	0.390	0.95	1.00	0.412	No
616	40.45	2.32	0.98	1.34	0.85	0.524	1.34	0.390	0.95	1.00	0.412	No
617	40.49	2.33	0.98	1.34	0.85	0.524	1.34	0.390	0.95	1.00	0.412	No
618	40.57	2.33	0.98	1.35	0.85	0.524	1.34	0.389	0.95	1.00	0.412	No
619	40.62	2.33	0.99	1.35	0.85	0.523	1.34	0.389	0.95	1.00	0.412	No
620	40.70	2.34	0.99	1.35	0.84	0.523	1.34	0.389	0.95	1.00	0.412	No
621	40.76	2.34	0.99	1.35	0.84	0.523	1.34	0.389	0.95	1.00	0.412	No
622	40.86	2.35	0.99	1.36	0.84	0.523	1.34	0.389	0.94	1.00	0.411	No
623	40.89	2.35	0.99	1.36	0.84	0.522	1.34	0.389	0.94	1.00	0.411	No
624	40.95	2.36	1.00	1.36	0.84	0.522	1.34	0.388	0.94	1.00	0.411	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
625	41.03	2.36	1.00	1.36	0.84	0.522	1.34	0.388	0.94	1.00	0.411	No
626	41.11	2.37	1.00	1.36	0.84	0.522	1.34	0.388	0.94	1.00	0.411	No
627	41.16	2.37	1.00	1.37	0.84	0.521	1.34	0.388	0.94	1.00	0.411	No
628	41.23	2.37	1.01	1.37	0.84	0.521	1.34	0.388	0.94	1.00	0.411	No
629	41.29	2.38	1.01	1.37	0.84	0.521	1.34	0.387	0.94	1.00	0.411	No
630	41.35	2.38	1.01	1.37	0.84	0.521	1.34	0.387	0.94	1.00	0.411	No
631	41.41	2.38	1.01	1.37	0.84	0.520	1.34	0.387	0.94	1.00	0.411	No
632	41.49	2.39	1.01	1.38	0.84	0.520	1.34	0.387	0.94	1.00	0.411	No
633	41.56	2.39	1.02	1.38	0.84	0.520	1.34	0.387	0.94	1.00	0.411	No
634	41.64	2.40	1.02	1.38	0.84	0.519	1.34	0.386	0.94	1.00	0.411	No
635	41.69	2.40	1.02	1.38	0.84	0.519	1.34	0.386	0.94	1.00	0.411	No
636	41.73	2.41	1.02	1.38	0.84	0.519	1.34	0.386	0.94	1.00	0.411	No
637	41.84	2.41	1.02	1.39	0.83	0.519	1.34	0.386	0.94	1.00	0.410	No
638	41.89	2.42	1.03	1.39	0.83	0.518	1.34	0.385	0.94	1.00	0.410	No
639	41.98	2.42	1.03	1.39	0.83	0.518	1.34	0.385	0.94	1.00	0.410	No
640	42.04	2.43	1.03	1.39	0.83	0.518	1.34	0.385	0.94	1.00	0.410	No
641	42.09	2.43	1.03	1.40	0.83	0.517	1.34	0.385	0.94	1.00	0.410	No
642	42.16	2.43	1.03	1.40	0.83	0.517	1.34	0.385	0.94	1.00	0.410	No
643	42.24	2.44	1.04	1.40	0.83	0.517	1.34	0.384	0.94	1.00	0.410	No
644	42.28	2.44	1.04	1.40	0.83	0.517	1.34	0.384	0.94	1.00	0.410	No
645	42.33	2.44	1.04	1.40	0.83	0.516	1.34	0.384	0.94	1.00	0.410	No
646	42.39	2.45	1.04	1.41	0.83	0.516	1.34	0.384	0.94	1.00	0.410	No
647	42.47	2.45	1.04	1.41	0.83	0.516	1.34	0.384	0.94	1.00	0.410	No
648	42.53	2.46	1.05	1.41	0.83	0.515	1.34	0.383	0.94	1.00	0.410	No
649	42.59	2.46	1.05	1.41	0.83	0.515	1.34	0.383	0.94	1.00	0.409	No
650	42.66	2.47	1.05	1.42	0.83	0.515	1.34	0.383	0.94	1.00	0.409	No
651	42.73	2.47	1.05	1.42	0.83	0.514	1.34	0.383	0.93	1.00	2.000	Yes
652	42.83	2.48	1.06	1.42	0.82	0.514	1.34	0.382	0.93	1.00	2.000	Yes
653	42.88	2.48	1.06	1.42	0.82	0.514	1.34	0.382	0.93	1.00	2.000	Yes
654	42.93	2.48	1.06	1.42	0.82	0.514	1.34	0.382	0.93	1.00	2.000	Yes
655	42.99	2.49	1.06	1.43	0.82	0.513	1.34	0.382	0.93	1.00	2.000	Yes
656	43.07	2.49	1.06	1.43	0.82	0.513	1.34	0.381	0.93	1.00	2.000	Yes
657	43.14	2.50	1.07	1.43	0.82	0.513	1.34	0.381	0.93	1.00	2.000	Yes
658	43.19	2.50	1.07	1.43	0.82	0.512	1.34	0.381	0.93	1.00	2.000	Yes
659	43.25	2.50	1.07	1.44	0.82	0.512	1.34	0.381	0.93	1.00	2.000	Yes
660	43.34	2.51	1.07	1.44	0.82	0.512	1.34	0.380	0.93	1.00	2.000	Yes
661	43.39	2.51	1.07	1.44	0.82	0.511	1.34	0.380	0.93	1.00	2.000	Yes
662	43.45	2.52	1.07	1.44	0.82	0.511	1.34	0.380	0.93	1.00	0.408	No
663	43.54	2.52	1.08	1.44	0.82	0.511	1.34	0.380	0.93	1.00	0.408	No
664	43.59	2.53	1.08	1.45	0.82	0.510	1.34	0.380	0.93	1.00	0.408	No
665	43.64	2.53	1.08	1.45	0.82	0.510	1.34	0.379	0.93	1.00	0.408	No
666	43.74	2.54	1.08	1.45	0.82	0.510	1.34	0.379	0.93	1.00	0.408	No
667	43.78	2.54	1.09	1.45	0.82	0.510	1.34	0.379	0.93	1.00	0.408	No
668	43.83	2.54	1.09	1.45	0.82	0.509	1.34	0.379	0.93	1.00	0.407	No
669	43.94	2.55	1.09	1.46	0.81	0.509	1.34	0.378	0.93	1.00	0.407	No
670	43.98	2.55	1.09	1.46	0.81	0.509	1.34	0.378	0.93	1.00	0.407	No
671	44.04	2.55	1.09	1.46	0.81	0.508	1.34	0.378	0.93	1.00	0.407	No
672	44.14	2.56	1.10	1.46	0.81	0.508	1.34	0.378	0.93	1.00	0.407	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
673	44.17	2.56	1.10	1.46	0.81	0.508	1.34	0.378	0.93	1.00	0.407	No
674	44.23	2.56	1.10	1.47	0.81	0.508	1.34	0.378	0.93	1.00	0.407	No
675	44.33	2.57	1.10	1.47	0.81	0.507	1.34	0.377	0.93	1.00	0.407	No
676	44.37	2.57	1.10	1.47	0.81	0.507	1.34	0.377	0.93	1.00	0.407	No
677	44.44	2.58	1.11	1.47	0.81	0.507	1.34	0.377	0.93	1.00	0.407	No
678	44.53	2.58	1.11	1.47	0.81	0.506	1.34	0.377	0.93	1.00	0.406	No
679	44.58	2.58	1.11	1.47	0.81	0.506	1.34	0.376	0.93	1.00	0.406	No
680	44.64	2.59	1.11	1.48	0.81	0.506	1.34	0.376	0.93	1.00	0.406	No
681	44.73	2.59	1.11	1.48	0.81	0.506	1.34	0.376	0.93	1.00	0.406	No
682	44.78	2.60	1.12	1.48	0.81	0.505	1.34	0.376	0.93	1.00	0.406	No
683	44.82	2.60	1.12	1.48	0.81	0.505	1.34	0.376	0.93	1.00	0.406	No
684	44.90	2.60	1.12	1.48	0.80	0.505	1.34	0.375	0.93	1.00	0.406	No
685	44.97	2.61	1.12	1.49	0.80	0.504	1.34	0.375	0.92	1.00	0.406	No
686	45.03	2.61	1.12	1.49	0.80	0.504	1.34	0.375	0.92	1.00	0.406	No
687	45.09	2.62	1.13	1.49	0.80	0.504	1.34	0.375	0.92	1.00	0.405	No
688	45.17	2.62	1.13	1.49	0.80	0.503	1.34	0.374	0.92	1.00	0.405	No
689	45.22	2.62	1.13	1.49	0.80	0.503	1.34	0.374	0.92	1.00	0.405	No
690	45.29	2.63	1.13	1.50	0.80	0.503	1.34	0.374	0.92	1.00	0.405	No
691	45.38	2.63	1.14	1.50	0.80	0.502	1.34	0.374	0.92	1.00	0.405	No
692	45.42	2.64	1.14	1.50	0.80	0.502	1.34	0.374	0.92	1.00	0.405	No
693	45.50	2.64	1.14	1.50	0.80	0.502	1.34	0.373	0.92	1.00	0.405	No
694	45.57	2.65	1.14	1.50	0.80	0.502	1.34	0.373	0.92	1.00	0.404	No
695	45.62	2.65	1.14	1.51	0.80	0.501	1.34	0.373	0.92	1.00	0.404	No
696	45.69	2.65	1.14	1.51	0.80	0.501	1.34	0.373	0.92	1.00	0.404	No
697	45.77	2.66	1.15	1.51	0.80	0.501	1.34	0.372	0.92	1.00	0.404	No
698	45.82	2.66	1.15	1.51	0.80	0.500	1.34	0.372	0.92	1.00	0.404	No
699	45.88	2.67	1.15	1.51	0.79	0.500	1.34	0.372	0.92	1.00	0.404	No
700	45.97	2.67	1.15	1.52	0.79	0.499	1.34	0.372	0.92	1.00	0.404	No
701	46.02	2.67	1.16	1.52	0.79	0.499	1.34	0.371	0.92	1.00	0.404	No
702	46.10	2.68	1.16	1.52	0.79	0.499	1.34	0.371	0.92	1.00	0.403	No
703	46.17	2.68	1.16	1.52	0.79	0.498	1.34	0.371	0.92	1.00	0.403	No
704	46.21	2.69	1.16	1.53	0.79	0.498	1.34	0.371	0.92	1.00	0.403	No
705	46.27	2.69	1.16	1.53	0.79	0.498	1.34	0.370	0.92	1.00	0.403	No
706	46.36	2.70	1.17	1.53	0.79	0.498	1.34	0.370	0.92	1.00	0.403	No
707	46.42	2.70	1.17	1.53	0.79	0.497	1.34	0.370	0.92	1.00	0.403	No
708	46.46	2.70	1.17	1.53	0.79	0.497	1.34	0.370	0.92	1.00	0.403	No
709	46.56	2.71	1.17	1.54	0.79	0.497	1.34	0.369	0.92	1.00	0.402	No
710	46.61	2.71	1.17	1.54	0.79	0.496	1.34	0.369	0.92	1.00	0.402	No
711	46.66	2.71	1.17	1.54	0.79	0.496	1.34	0.369	0.92	1.00	0.402	No
712	46.74	2.72	1.18	1.54	0.79	0.496	1.34	0.369	0.92	1.00	0.402	No
713	46.81	2.72	1.18	1.54	0.79	0.495	1.34	0.368	0.92	1.00	0.402	No
714	46.87	2.73	1.18	1.55	0.78	0.495	1.34	0.368	0.92	1.00	0.402	No
715	46.94	2.73	1.18	1.55	0.78	0.495	1.34	0.368	0.92	1.00	0.402	No
716	47.01	2.74	1.19	1.55	0.78	0.494	1.34	0.368	0.92	1.00	0.401	No
717	47.06	2.74	1.19	1.55	0.78	0.494	1.34	0.367	0.92	1.00	0.401	No
718	47.12	2.74	1.19	1.55	0.78	0.494	1.34	0.367	0.92	1.00	0.401	No
719	47.19	2.75	1.19	1.56	0.78	0.493	1.34	0.367	0.92	1.00	0.401	No
720	47.25	2.75	1.19	1.56	0.78	0.493	1.34	0.367	0.92	1.00	0.401	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
721	47.34	2.76	1.20	1.56	0.78	0.493	1.34	0.366	0.91	1.00	0.401	No
722	47.39	2.76	1.20	1.56	0.78	0.492	1.34	0.366	0.91	1.00	0.401	No
723	47.44	2.76	1.20	1.56	0.78	0.492	1.34	0.366	0.91	1.00	0.400	No
724	47.54	2.77	1.20	1.57	0.78	0.492	1.34	0.366	0.91	1.00	0.400	No
725	47.59	2.77	1.20	1.57	0.78	0.491	1.34	0.366	0.91	1.00	0.400	No
726	47.65	2.77	1.21	1.57	0.78	0.491	1.34	0.365	0.91	1.00	0.400	No
727	47.74	2.78	1.21	1.57	0.78	0.491	1.34	0.365	0.91	1.00	0.400	No
728	47.81	2.78	1.21	1.57	0.78	0.490	1.34	0.365	0.91	1.00	0.400	No
729	47.85	2.79	1.21	1.57	0.77	0.490	1.34	0.365	0.91	1.00	0.399	No
730	47.94	2.79	1.21	1.58	0.77	0.490	1.34	0.364	0.91	1.00	0.399	No
731	47.98	2.79	1.22	1.58	0.77	0.489	1.34	0.364	0.91	1.00	0.399	No
732	48.04	2.80	1.22	1.58	0.77	0.489	1.34	0.364	0.91	1.00	0.399	No
733	48.13	2.80	1.22	1.58	0.77	0.489	1.34	0.363	0.91	1.00	0.399	No
734	48.17	2.81	1.22	1.58	0.77	0.488	1.34	0.363	0.91	1.00	0.399	No
735	48.24	2.81	1.22	1.59	0.77	0.488	1.34	0.363	0.91	1.00	0.399	No
736	48.32	2.82	1.23	1.59	0.77	0.488	1.34	0.363	0.91	1.00	0.398	No
737	48.37	2.82	1.23	1.59	0.77	0.487	1.34	0.363	0.91	1.00	0.398	No
738	48.44	2.82	1.23	1.59	0.77	0.487	1.34	0.362	0.91	1.00	2.000	Yes
739	48.53	2.83	1.23	1.60	0.77	0.487	1.34	0.362	0.91	1.00	2.000	Yes
740	48.56	2.83	1.23	1.60	0.77	0.486	1.34	0.362	0.91	1.00	2.000	Yes
741	48.64	2.84	1.24	1.60	0.77	0.486	1.34	0.361	0.91	1.00	2.000	Yes
742	48.72	2.84	1.24	1.60	0.77	0.486	1.34	0.361	0.91	1.00	2.000	Yes
743	48.78	2.84	1.24	1.60	0.77	0.485	1.34	0.361	0.91	1.00	2.000	Yes
744	48.83	2.85	1.24	1.61	0.76	0.485	1.34	0.361	0.91	1.00	2.000	Yes
745	48.90	2.85	1.24	1.61	0.76	0.485	1.34	0.360	0.91	1.00	2.000	Yes
746	48.97	2.86	1.25	1.61	0.76	0.484	1.34	0.360	0.91	1.00	2.000	Yes
747	49.03	2.86	1.25	1.61	0.76	0.484	1.34	0.360	0.91	1.00	2.000	Yes
748	49.12	2.87	1.25	1.61	0.76	0.483	1.34	0.360	0.91	1.00	0.396	No
749	49.16	2.87	1.25	1.62	0.76	0.483	1.34	0.359	0.91	1.00	0.396	No
750	49.23	2.87	1.26	1.62	0.76	0.483	1.34	0.359	0.91	1.00	0.396	No
751	49.31	2.88	1.26	1.62	0.76	0.482	1.34	0.359	0.91	1.00	0.396	No
752	49.36	2.88	1.26	1.62	0.76	0.482	1.34	0.358	0.91	1.00	0.396	No
753	49.43	2.89	1.26	1.63	0.76	0.482	1.34	0.358	0.91	1.00	0.395	No
754	49.52	2.89	1.26	1.63	0.76	0.481	1.34	0.358	0.91	1.00	0.395	No
755	49.58	2.90	1.27	1.63	0.76	0.481	1.34	0.358	0.91	1.00	0.395	No
756	49.62	2.90	1.27	1.63	0.76	0.481	1.34	0.357	0.91	1.00	0.395	No
757	49.71	2.91	1.27	1.64	0.76	0.480	1.34	0.357	0.90	1.00	0.395	No
758	49.78	2.91	1.27	1.64	0.75	0.480	1.34	0.357	0.90	1.00	0.394	No
759	49.81	2.91	1.27	1.64	0.75	0.479	1.34	0.357	0.90	1.00	0.394	No
760	49.88	2.92	1.28	1.64	0.75	0.479	1.34	0.356	0.90	1.00	0.394	No
761	49.97	2.92	1.28	1.64	0.75	0.478	1.34	0.356	0.90	1.00	0.394	No
762	50.00	2.92	1.28	1.65	0.75	0.478	1.34	0.356	0.90	1.00	0.394	No
763	50.07	2.93	1.28	1.65	0.75	0.478	1.34	0.355	0.90	1.00	2.000	No
764	50.14	2.93	1.28	1.65	0.75	0.478	1.34	0.355	0.90	1.00	2.000	No
765	50.22	2.94	1.29	1.65	0.75	0.477	1.34	0.355	0.90	1.00	2.000	Yes
766	50.27	2.94	1.29	1.65	0.75	0.477	1.34	0.355	0.90	1.00	2.000	Yes
767	50.35	2.95	1.29	1.66	0.75	0.476	1.34	0.354	0.90	1.00	2.000	Yes
768	50.40	2.95	1.29	1.66	0.75	0.476	1.34	0.354	0.90	1.00	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
769	50.47	2.96	1.29	1.66	0.75	0.476	1.34	0.354	0.90	1.00	2.000	Yes
770	50.55	2.96	1.30	1.66	0.75	0.475	1.34	0.353	0.90	1.00	2.000	Yes
771	50.59	2.96	1.30	1.67	0.75	0.475	1.34	0.353	0.90	1.00	2.000	Yes
772	50.66	2.97	1.30	1.67	0.75	0.475	1.34	0.353	0.90	1.00	2.000	Yes
773	50.75	2.97	1.30	1.67	0.75	0.474	1.34	0.353	0.90	1.00	2.000	Yes
774	50.79	2.98	1.30	1.67	0.74	0.474	1.34	0.352	0.90	1.00	2.000	Yes
775	50.86	2.98	1.31	1.67	0.74	0.473	1.34	0.352	0.90	1.00	2.000	Yes
776	50.94	2.99	1.31	1.68	0.74	0.473	1.34	0.352	0.90	1.00	2.000	Yes
777	50.99	2.99	1.31	1.68	0.74	0.473	1.34	0.352	0.90	1.00	2.000	Yes
778	51.05	2.99	1.31	1.68	0.74	0.472	1.34	0.351	0.90	1.00	2.000	Yes
779	51.14	3.00	1.31	1.68	0.74	0.472	1.34	0.351	0.90	1.00	2.000	Yes
780	51.18	3.00	1.32	1.68	0.74	0.472	1.34	0.351	0.90	1.00	2.000	Yes
781	51.25	3.00	1.32	1.69	0.74	0.471	1.34	0.351	0.90	1.00	2.000	Yes
782	51.34	3.01	1.32	1.69	0.74	0.471	1.34	0.350	0.90	1.00	2.000	Yes
783	51.41	3.01	1.32	1.69	0.74	0.471	1.34	0.350	0.90	1.00	2.000	No
784	51.44	3.02	1.32	1.69	0.74	0.470	1.34	0.350	0.90	1.00	2.000	No
785	51.52	3.02	1.33	1.69	0.74	0.470	1.34	0.350	0.90	1.00	2.000	No
786	51.67	3.03	1.33	1.70	0.74	0.469	1.34	0.349	0.90	1.00	2.000	No
787	51.70	3.03	1.33	1.70	0.74	0.469	1.34	0.349	0.90	1.00	2.000	No
788	51.75	3.03	1.33	1.70	0.74	0.469	1.34	0.349	0.90	1.00	2.000	No
789	51.78	3.04	1.33	1.70	0.73	0.469	1.34	0.349	0.90	1.00	2.000	No
790	51.88	3.04	1.34	1.70	0.73	0.468	1.34	0.348	0.90	1.00	2.000	No
791	51.92	3.04	1.34	1.71	0.73	0.468	1.34	0.348	0.90	1.00	2.000	No
792	51.99	3.05	1.34	1.71	0.73	0.468	1.34	0.348	0.90	1.00	2.000	No
793	52.04	3.05	1.34	1.71	0.73	0.467	1.34	0.348	0.90	1.00	2.000	No
794	52.14	3.06	1.35	1.71	0.73	0.467	1.34	0.347	0.90	1.00	2.000	No
795	52.19	3.06	1.35	1.71	0.73	0.467	1.34	0.347	0.90	1.00	2.000	No
796	52.26	3.06	1.35	1.71	0.73	0.466	1.34	0.347	0.89	1.00	2.000	No
797	52.33	3.07	1.35	1.72	0.73	0.466	1.34	0.347	0.89	1.00	2.000	No
798	52.38	3.07	1.35	1.72	0.73	0.466	1.34	0.346	0.89	1.00	2.000	No
799	52.43	3.07	1.36	1.72	0.73	0.466	1.34	0.346	0.89	1.00	2.000	No
800	52.51	3.08	1.36	1.72	0.73	0.465	1.34	0.346	0.89	1.00	2.000	No
801	52.58	3.08	1.36	1.72	0.73	0.465	1.34	0.346	0.89	1.00	2.000	No
802	52.63	3.08	1.36	1.72	0.73	0.465	1.34	0.346	0.89	1.00	2.000	No
803	52.69	3.09	1.36	1.73	0.73	0.464	1.34	0.345	0.89	1.00	2.000	No
804	52.77	3.09	1.37	1.73	0.72	0.464	1.34	0.345	0.89	1.00	2.000	No
805	52.83	3.10	1.37	1.73	0.72	0.464	1.34	0.345	0.89	1.00	2.000	No
806	52.90	3.10	1.37	1.73	0.72	0.463	1.34	0.345	0.89	1.00	2.000	No
807	52.99	3.10	1.37	1.73	0.72	0.463	1.34	0.344	0.89	1.00	2.000	No
808	53.05	3.11	1.37	1.73	0.72	0.463	1.34	0.344	0.89	1.00	2.000	No
809	53.10	3.11	1.38	1.74	0.72	0.463	1.34	0.344	0.89	1.00	2.000	No
810	53.16	3.11	1.38	1.74	0.72	0.462	1.34	0.344	0.89	1.00	2.000	No
811	53.25	3.12	1.38	1.74	0.72	0.462	1.34	0.344	0.89	1.00	2.000	No
812	53.29	3.12	1.38	1.74	0.72	0.462	1.34	0.343	0.89	1.00	2.000	No
813	53.38	3.13	1.38	1.74	0.72	0.461	1.34	0.343	0.89	1.00	2.000	No
814	53.44	3.13	1.39	1.74	0.72	0.461	1.34	0.343	0.89	1.00	2.000	No
815	53.50	3.13	1.39	1.74	0.72	0.461	1.34	0.343	0.89	1.00	2.000	No
816	53.55	3.14	1.39	1.75	0.72	0.461	1.34	0.343	0.89	1.00	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
817	53.64	3.14	1.39	1.75	0.72	0.460	1.34	0.342	0.89	1.00	2.000	No
818	53.72	3.14	1.40	1.75	0.72	0.460	1.34	0.342	0.89	1.00	2.000	No
819	53.74	3.15	1.40	1.75	0.72	0.460	1.34	0.342	0.89	1.00	2.000	No
820	53.82	3.15	1.40	1.75	0.71	0.459	1.34	0.342	0.89	1.00	2.000	No
821	53.90	3.15	1.40	1.75	0.71	0.459	1.34	0.341	0.89	1.00	2.000	No
822	53.94	3.16	1.40	1.75	0.71	0.459	1.34	0.341	0.89	1.00	2.000	No
823	54.01	3.16	1.40	1.76	0.71	0.459	1.34	0.341	0.89	1.00	2.000	No
824	54.09	3.16	1.41	1.76	0.71	0.458	1.34	0.341	0.89	1.00	2.000	No
825	54.19	3.17	1.41	1.76	0.71	0.458	1.34	0.340	0.89	1.00	2.000	No
826	54.24	3.17	1.41	1.76	0.71	0.458	1.34	0.340	0.89	1.00	2.000	No
827	54.29	3.18	1.41	1.76	0.71	0.457	1.34	0.340	0.89	1.00	2.000	No
828	54.35	3.18	1.41	1.76	0.71	0.457	1.34	0.340	0.89	1.00	2.000	No
829	54.44	3.18	1.42	1.77	0.71	0.457	1.34	0.340	0.89	1.00	2.000	No
830	54.49	3.19	1.42	1.77	0.71	0.457	1.34	0.340	0.89	1.00	2.000	No
831	54.53	3.19	1.42	1.77	0.71	0.456	1.34	0.339	0.89	1.00	2.000	No
832	54.63	3.19	1.42	1.77	0.71	0.456	1.34	0.339	0.89	1.00	2.000	No
833	54.68	3.20	1.43	1.77	0.71	0.456	1.34	0.339	0.89	1.00	2.000	No
834	54.74	3.20	1.43	1.77	0.71	0.455	1.34	0.339	0.89	1.00	2.000	No
835	54.83	3.20	1.43	1.77	0.70	0.455	1.34	0.338	0.89	1.00	2.000	No
836	54.88	3.21	1.43	1.78	0.70	0.455	1.34	0.338	0.89	1.00	2.000	No
837	54.94	3.21	1.43	1.78	0.70	0.455	1.34	0.338	0.89	1.00	2.000	No
838	55.03	3.22	1.44	1.78	0.70	0.454	1.34	0.338	0.89	1.00	2.000	No
839	55.07	3.22	1.44	1.78	0.70	0.454	1.34	0.338	0.89	1.00	2.000	No
840	55.13	3.22	1.44	1.78	0.70	0.454	1.34	0.337	0.89	1.00	2.000	No
841	55.23	3.23	1.44	1.78	0.70	0.453	1.34	0.337	0.89	1.00	2.000	No
842	55.28	3.23	1.44	1.79	0.70	0.453	1.34	0.337	0.89	1.00	2.000	No
843	55.32	3.23	1.45	1.79	0.70	0.453	1.34	0.337	0.89	1.00	2.000	No
844	55.42	3.24	1.45	1.79	0.70	0.452	1.34	0.337	0.89	1.00	2.000	No
845	55.50	3.24	1.45	1.79	0.70	0.452	1.34	0.336	0.89	1.00	2.000	No
846	55.53	3.24	1.45	1.79	0.70	0.452	1.34	0.336	0.89	1.00	2.000	No
847	55.58	3.25	1.45	1.79	0.70	0.452	1.34	0.336	0.89	1.00	2.000	No
848	55.66	3.25	1.46	1.79	0.70	0.451	1.34	0.336	0.89	1.00	2.000	No
849	55.73	3.25	1.46	1.80	0.70	0.451	1.34	0.336	0.89	1.00	2.000	No
850	55.78	3.26	1.46	1.80	0.70	0.451	1.34	0.335	0.89	1.00	2.000	No
851	55.86	3.26	1.46	1.80	0.70	0.451	1.34	0.335	0.89	1.00	2.000	No
852	55.93	3.26	1.46	1.80	0.69	0.450	1.34	0.335	0.88	1.00	2.000	Yes
853	55.97	3.27	1.47	1.80	0.69	0.450	1.34	0.335	0.88	1.00	2.000	Yes
854	56.08	3.27	1.47	1.80	0.69	0.450	1.34	0.334	0.88	1.00	2.000	Yes
855	56.12	3.28	1.47	1.81	0.69	0.449	1.34	0.334	0.88	1.00	2.000	Yes
856	56.17	3.28	1.47	1.81	0.69	0.449	1.34	0.334	0.88	1.00	2.000	Yes
857	56.28	3.29	1.48	1.81	0.69	0.449	1.34	0.334	0.88	1.00	2.000	Yes
858	56.32	3.29	1.48	1.81	0.69	0.448	1.34	0.334	0.88	1.00	2.000	Yes
859	56.37	3.29	1.48	1.81	0.69	0.448	1.34	0.333	0.88	1.00	2.000	Yes
860	56.47	3.30	1.48	1.82	0.69	0.448	1.34	0.333	0.88	1.00	2.000	Yes
861	56.52	3.30	1.48	1.82	0.69	0.447	1.34	0.333	0.88	1.00	2.000	Yes
862	56.57	3.30	1.48	1.82	0.69	0.447	1.34	0.333	0.88	1.00	2.000	Yes
863	56.67	3.31	1.49	1.82	0.69	0.447	1.34	0.332	0.88	1.00	2.000	No
864	56.72	3.31	1.49	1.82	0.69	0.446	1.34	0.332	0.88	1.00	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
865	56.78	3.32	1.49	1.83	0.69	0.446	1.34	0.332	0.88	1.00	2.000	Yes
866	56.87	3.32	1.49	1.83	0.69	0.446	1.34	0.331	0.88	1.00	2.000	Yes
867	56.91	3.32	1.49	1.83	0.69	0.445	1.34	0.331	0.88	1.00	2.000	Yes
868	56.97	3.33	1.50	1.83	0.69	0.445	1.34	0.331	0.88	1.00	2.000	Yes
869	57.03	3.33	1.50	1.83	0.68	0.445	1.34	0.331	0.88	1.00	2.000	Yes
870	57.11	3.34	1.50	1.84	0.68	0.444	1.34	0.330	0.88	1.00	2.000	Yes
871	57.17	3.34	1.50	1.84	0.68	0.444	1.34	0.330	0.88	1.00	2.000	Yes
872	57.26	3.35	1.51	1.84	0.68	0.444	1.34	0.330	0.88	1.00	2.000	Yes
873	57.32	3.35	1.51	1.84	0.68	0.443	1.34	0.330	0.88	1.00	2.000	Yes
874	57.35	3.35	1.51	1.84	0.68	0.443	1.34	0.330	0.88	1.00	2.000	Yes
875	57.42	3.36	1.51	1.85	0.68	0.443	1.34	0.329	0.88	1.00	2.000	Yes
876	57.51	3.36	1.51	1.85	0.68	0.442	1.34	0.329	0.88	1.00	2.000	Yes
877	57.55	3.36	1.51	1.85	0.68	0.442	1.34	0.329	0.88	1.00	2.000	Yes
878	57.62	3.37	1.52	1.85	0.68	0.442	1.34	0.329	0.88	1.00	2.000	No
879	57.71	3.37	1.52	1.85	0.68	0.441	1.34	0.328	0.88	1.00	2.000	No
880	57.78	3.38	1.52	1.86	0.68	0.441	1.34	0.328	0.88	1.00	2.000	No
881	57.82	3.38	1.52	1.86	0.68	0.441	1.34	0.328	0.88	1.00	2.000	No
882	57.90	3.39	1.53	1.86	0.68	0.440	1.34	0.328	0.88	1.00	2.000	No
883	57.96	3.39	1.53	1.86	0.68	0.440	1.34	0.327	0.88	1.00	2.000	No
884	58.01	3.39	1.53	1.86	0.68	0.440	1.34	0.327	0.88	1.00	2.000	No
885	58.11	3.40	1.53	1.87	0.68	0.440	1.34	0.327	0.88	1.00	2.000	No
886	58.15	3.40	1.53	1.87	0.67	0.439	1.34	0.327	0.88	1.00	2.000	No
887	58.21	3.40	1.54	1.87	0.67	0.439	1.34	0.327	0.88	1.00	2.000	No
888	58.31	3.41	1.54	1.87	0.67	0.439	1.34	0.326	0.88	1.00	2.000	No
889	58.35	3.41	1.54	1.87	0.67	0.439	1.34	0.326	0.88	1.00	2.000	No
890	58.42	3.42	1.54	1.87	0.67	0.438	1.34	0.326	0.88	1.00	2.000	No
891	58.50	3.42	1.54	1.88	0.67	0.438	1.34	0.326	0.88	1.00	2.000	No
892	58.55	3.42	1.55	1.88	0.67	0.438	1.34	0.326	0.88	1.00	2.000	No
893	58.61	3.43	1.55	1.88	0.67	0.437	1.34	0.325	0.88	1.00	2.000	No
894	58.70	3.43	1.55	1.88	0.67	0.437	1.34	0.325	0.88	1.00	2.000	No
895	58.75	3.43	1.55	1.88	0.67	0.437	1.34	0.325	0.88	1.00	2.000	No
896	58.81	3.44	1.55	1.88	0.67	0.437	1.34	0.325	0.88	1.00	2.000	No
897	58.89	3.44	1.56	1.89	0.67	0.436	1.34	0.324	0.88	1.00	2.000	No
898	58.95	3.45	1.56	1.89	0.67	0.436	1.34	0.324	0.88	1.00	2.000	No
899	59.00	3.45	1.56	1.89	0.67	0.436	1.34	0.324	0.88	1.00	2.000	No
900	59.10	3.45	1.56	1.89	0.67	0.435	1.34	0.324	0.88	1.00	2.000	No
901	59.15	3.46	1.56	1.89	0.67	0.435	1.34	0.324	0.87	1.00	2.000	No
902	59.20	3.46	1.57	1.89	0.67	0.435	1.34	0.324	0.87	1.00	2.000	No
903	59.28	3.46	1.57	1.89	0.67	0.435	1.34	0.323	0.87	1.00	2.000	No
904	59.35	3.47	1.57	1.90	0.66	0.434	1.34	0.323	0.87	1.00	2.000	No
905	59.38	3.47	1.57	1.90	0.66	0.434	1.34	0.323	0.87	1.00	2.000	No
906	59.46	3.47	1.57	1.90	0.66	0.434	1.34	0.323	0.87	1.00	2.000	No
907	59.53	3.48	1.58	1.90	0.66	0.434	1.34	0.323	0.87	1.00	2.000	No
908	59.59	3.48	1.58	1.90	0.66	0.433	1.34	0.322	0.87	1.00	2.000	No
909	59.67	3.49	1.58	1.90	0.66	0.433	1.34	0.322	0.87	1.00	2.000	No
910	59.73	3.49	1.58	1.91	0.66	0.433	1.34	0.322	0.87	1.00	2.000	No
911	59.79	3.49	1.58	1.91	0.66	0.433	1.34	0.322	0.87	1.00	2.000	No
912	59.89	3.50	1.59	1.91	0.66	0.432	1.34	0.321	0.87	1.00	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
913	59.94	3.50	1.59	1.91	0.66	0.432	1.34	0.321	0.87	1.00	2.000	No
914	59.99	3.50	1.59	1.91	0.66	0.432	1.34	0.321	0.87	1.00	2.000	Yes
915	60.07	3.51	1.59	1.91	0.66	0.431	1.34	0.321	0.87	1.00	2.000	Yes
916	60.12	3.51	1.59	1.92	0.66	0.431	1.34	0.321	0.87	1.00	2.000	Yes
917	60.19	3.51	1.60	1.92	0.66	0.431	1.34	0.321	0.87	1.00	2.000	Yes
918	60.25	3.52	1.60	1.92	0.66	0.431	1.34	0.320	0.87	1.00	2.000	Yes
919	60.33	3.52	1.60	1.92	0.66	0.430	1.34	0.320	0.87	1.00	2.000	Yes
920	60.38	3.52	1.60	1.92	0.66	0.430	1.34	0.320	0.87	1.00	2.000	Yes
921	60.48	3.53	1.61	1.92	0.66	0.430	1.34	0.320	0.87	1.00	2.000	Yes
922	60.53	3.53	1.61	1.93	0.65	0.430	1.34	0.320	0.87	1.00	2.000	Yes
923	60.61	3.54	1.61	1.93	0.65	0.429	1.34	0.319	0.87	1.00	2.000	No
924	60.63	3.54	1.61	1.93	0.65	0.429	1.34	0.319	0.87	1.00	2.000	No

Abbreviations

Depth: Depth from free surface, at which CPT was performed (ft)
σ_v: Total overburden pressure at test point (tsf)
u_0: Water pressure at test point (tsf)
σ_v': Effective overburden pressure based on GWT during earthquake (tsf)
r_d: Nonlinear shear mass factor
CSR: Cyclic Stress Ratio
MSF: Magnitude Scaling Factor
CSR_{eq}: CSR adjusted for M=7.5
K_σ: Effective overburden stress factor
CSR^*: CSR fully adjusted

:: Cyclic Resistance Ratio (CRR) calculation data ::

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
1	0.08	9.60	2.68	1.56	0.90	15.42	3.88	59.90	4.000	Yes	Yes	2.00
2	0.15	12.30	2.59	1.52	0.86	19.75	3.25	64.14	4.000	Yes	No	2.00
3	0.23	15.73	2.49	1.46	0.82	25.25	2.71	68.51	4.000	Yes	No	2.00
4	0.30	19.25	2.41	1.45	0.80	30.90	2.37	73.28	4.000	Yes	No	2.00
5	0.35	22.73	2.36	1.49	0.78	36.49	2.17	79.06	4.000	Yes	No	2.00
6	0.43	27.09	2.32	1.58	0.76	43.49	2.00	87.15	4.000	Yes	No	2.00
7	0.50	31.20	2.28	1.67	0.75	50.08	1.90	95.08	4.000	Yes	No	2.00
8	0.55	34.99	2.26	1.79	0.74	56.17	1.84	103.30	4.000	Yes	No	2.00
9	0.61	38.30	2.26	1.94	0.74	61.48	1.82	111.93	4.000	No	No	2.00
10	0.70	41.27	2.26	2.09	0.73	66.25	1.82	120.26	4.000	No	No	2.00
11	0.73	43.17	2.26	2.24	0.74	69.29	1.84	127.26	4.000	No	No	2.00
12	0.80	43.66	2.28	2.39	0.74	70.07	1.88	132.08	4.000	No	No	2.00
13	0.89	43.46	2.30	2.55	0.75	69.74	1.95	135.95	4.000	No	No	2.00
14	0.93	42.22	2.33	2.71	0.76	67.74	2.04	138.27	4.000	No	No	2.00
15	1.01	40.68	2.35	2.82	0.77	65.27	2.12	138.64	4.000	No	No	2.00
16	1.09	39.02	2.37	2.89	0.78	62.58	2.20	137.77	4.000	No	No	2.00
17	1.13	37.30	2.39	2.90	0.78	59.82	2.26	135.26	4.000	No	No	2.00
18	1.19	35.82	2.39	2.83	0.79	57.45	2.28	131.07	4.000	No	No	2.00
19	1.29	34.39	2.39	2.73	0.79	55.14	2.29	126.20	4.000	No	No	2.00
20	1.34	33.05	2.39	2.61	0.79	52.98	2.28	120.97	4.000	No	No	2.00
21	1.39	32.13	2.39	2.49	0.78	51.49	2.26	116.52	4.000	No	No	2.00
22	1.45	30.90	2.39	2.40	0.79	49.51	2.27	112.45	4.000	No	No	2.00
23	1.54	30.65	2.37	2.25	0.78	49.10	2.21	108.60	4.000	No	No	2.00
24	1.59	30.22	2.37	2.15	0.78	48.41	2.18	105.51	4.000	No	No	2.00
25	1.67	29.56	2.36	2.09	0.78	47.34	2.17	102.95	4.000	No	No	2.00
26	1.72	28.85	2.37	2.06	0.78	46.20	2.19	101.08	4.000	No	No	2.00
27	1.79	27.91	2.38	2.03	0.78	44.68	2.22	99.05	4.000	No	No	2.00
28	1.85	26.72	2.39	2.01	0.78	42.76	2.26	96.74	4.000	No	No	2.00
29	1.94	25.40	2.40	2.00	0.79	40.63	2.33	94.54	4.000	Yes	No	2.00
30	1.98	23.66	2.43	2.03	0.80	37.83	2.45	92.65	4.000	Yes	No	2.00
31	2.04	22.23	2.46	2.05	0.81	35.53	2.56	90.86	4.000	Yes	No	2.00
32	2.13	20.14	2.51	2.18	0.83	32.16	2.80	89.96	4.000	Yes	No	2.00
33	2.17	18.38	2.55	2.31	0.85	29.33	3.05	89.57	4.000	Yes	No	2.00
34	2.24	16.92	2.61	2.52	0.87	26.97	3.36	90.61	4.000	Yes	Yes	2.00
35	2.32	15.55	2.66	2.80	0.89	24.76	3.74	92.51	4.000	Yes	Yes	2.00
36	2.39	14.33	2.72	3.18	0.91	22.81	4.18	95.38	4.000	Yes	Yes	2.00
37	2.43	13.41	2.78	3.57	0.93	21.32	4.61	98.35	4.000	Yes	Yes	2.00
38	2.52	12.71	2.83	3.94	0.95	20.20	5.00	101.07	4.000	Yes	Yes	2.00
39	2.58	12.27	2.86	4.25	0.96	19.47	5.31	103.33	4.000	Yes	Yes	2.00
40	2.63	11.94	2.89	4.52	0.97	18.94	5.56	105.23	4.000	Yes	Yes	2.00
41	2.72	11.69	2.91	4.76	0.98	18.54	5.76	106.84	4.000	No	Yes	2.00
42	2.78	11.47	2.93	4.97	0.99	18.18	5.95	108.19	4.000	No	Yes	2.00
43	2.83	11.30	2.94	5.09	0.99	17.90	6.07	108.67	4.000	No	Yes	2.00
44	2.89	11.12	2.95	5.16	1.00	17.61	6.17	108.63	4.000	No	Yes	2.00
45	2.98	10.92	2.96	5.23	1.00	17.28	6.27	108.39	4.000	No	Yes	2.00
46	3.03	10.65	2.97	5.34	1.00	16.84	6.43	108.26	4.000	No	Yes	2.00
47	3.09	10.34	2.99	5.49	1.00	16.33	6.62	108.12	4.000	No	Yes	2.00
48	3.18	10.03	3.01	5.63	1.00	15.82	6.82	107.86	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
49	3.22	9.73	3.02	5.75	1.00	15.34	7.00	107.37	4.000	No	Yes	2.00
50	3.32	9.47	3.04	5.83	1.00	14.92	7.15	106.66	4.000	No	Yes	2.00
51	3.37	9.26	3.05	5.87	1.00	14.57	7.27	105.83	4.000	No	Yes	2.00
52	3.42	9.09	3.05	5.88	1.00	14.29	7.35	105.00	4.000	No	Yes	2.00
53	3.52	8.99	3.05	5.85	1.00	14.13	7.37	104.17	4.000	No	Yes	2.00
54	3.57	8.93	3.05	5.78	1.00	14.01	7.37	103.23	4.000	No	Yes	2.00
55	3.61	8.95	3.05	5.65	1.00	14.05	7.28	102.30	4.000	No	Yes	2.00
56	3.68	8.99	3.04	5.53	1.00	14.10	7.19	101.46	4.000	No	Yes	2.00
57	3.77	9.05	3.03	5.43	1.00	14.19	7.11	100.93	4.000	No	Yes	2.00
58	3.83	9.13	3.03	5.37	1.00	14.32	7.04	100.83	4.000	No	Yes	2.00
59	3.91	9.21	3.02	5.31	1.00	14.44	6.97	100.72	4.000	No	Yes	2.00
60	3.95	9.30	3.02	5.30	1.00	14.58	6.93	101.04	4.000	No	Yes	2.00
61	4.02	9.38	3.01	5.33	1.00	14.71	6.91	101.68	4.000	No	Yes	2.00
62	4.12	9.44	3.02	5.41	1.00	14.79	6.94	102.63	4.000	No	Yes	2.00
63	4.14	9.48	3.02	5.49	1.00	14.85	6.97	103.57	4.000	No	Yes	2.00
64	4.22	9.49	3.02	5.52	1.00	14.87	6.99	103.89	4.000	No	Yes	2.00
65	4.27	9.45	3.03	5.65	1.00	14.80	7.08	104.71	4.000	No	Yes	2.00
66	4.37	9.36	3.04	5.77	1.00	14.64	7.19	105.22	4.000	No	Yes	2.00
67	4.42	9.19	3.05	5.89	1.00	14.37	7.33	105.31	4.000	No	Yes	2.00
68	4.46	9.00	3.06	6.02	1.00	14.05	7.49	105.28	4.000	No	Yes	2.00
69	4.57	8.66	3.09	6.23	1.00	13.50	7.77	104.88	4.000	No	Yes	2.00
70	4.61	8.38	3.10	6.36	1.00	13.05	7.98	104.17	4.000	No	Yes	2.00
71	4.67	8.12	3.12	6.46	1.00	12.63	8.18	103.24	4.000	No	Yes	2.00
72	4.76	7.86	3.14	6.57	1.00	12.20	8.39	102.28	4.000	No	Yes	2.00
73	4.81	7.60	3.16	6.76	1.00	11.77	8.65	101.79	4.000	No	Yes	2.00
74	4.90	7.39	3.17	6.81	1.00	11.44	8.80	100.62	4.000	No	Yes	2.00
75	4.96	7.20	3.18	6.82	1.00	11.12	8.94	99.34	4.000	No	Yes	2.00
76	5.00	7.06	3.18	6.82	1.00	10.89	9.03	98.30	4.000	No	Yes	2.00
77	5.05	6.97	3.19	6.79	1.00	10.75	9.07	97.51	4.000	No	Yes	2.00
78	5.14	7.06	3.18	6.61	1.00	10.88	8.91	96.98	4.000	No	Yes	2.00
79	5.20	7.09	3.17	6.49	1.00	10.92	8.83	96.38	4.000	No	Yes	2.00
80	5.30	7.10	3.16	6.40	1.00	10.94	8.77	95.87	4.000	No	Yes	2.00
81	5.35	7.13	3.16	6.32	1.00	10.98	8.71	95.58	4.000	No	Yes	2.00
82	5.39	7.16	3.16	6.28	1.00	11.02	8.66	95.50	4.000	No	Yes	2.00
83	5.48	7.22	3.15	6.23	1.00	11.11	8.60	95.54	4.000	No	Yes	2.00
84	5.55	7.34	3.14	6.17	1.00	11.29	8.49	95.84	4.000	No	Yes	2.00
85	5.59	7.46	3.13	6.09	1.00	11.49	8.37	96.14	4.000	No	Yes	2.00
86	5.64	7.63	3.12	5.97	1.00	11.76	8.19	96.34	4.000	No	Yes	2.00
87	5.74	7.81	3.11	5.83	1.00	12.04	8.01	96.43	4.000	No	Yes	2.00
88	5.79	8.05	3.09	5.65	1.00	12.42	7.77	96.53	4.000	No	Yes	2.00
89	5.84	8.32	3.07	5.52	1.00	12.85	7.55	97.05	4.000	No	Yes	2.00
90	5.94	8.60	3.05	5.43	1.00	13.29	7.36	97.86	4.000	No	Yes	2.00
91	5.97	8.86	3.04	5.35	1.00	13.70	7.20	98.66	4.000	No	Yes	2.00
92	6.05	9.05	3.03	5.34	1.00	14.00	7.11	99.53	4.000	No	Yes	2.00
93	6.14	9.20	3.03	5.37	1.00	14.23	7.06	100.50	4.000	No	Yes	2.00
94	6.19	9.32	3.03	5.42	1.00	14.42	7.05	101.57	4.000	No	Yes	2.00
95	6.24	9.37	3.03	5.51	1.00	14.49	7.07	102.52	4.000	No	Yes	2.00
96	6.33	9.38	3.03	5.59	1.00	14.50	7.12	103.26	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
97	6.38	9.33	3.04	5.70	1.00	14.41	7.21	103.88	4.000	No	Yes	2.00
98	6.44	9.28	3.05	5.76	1.00	14.33	7.26	104.08	4.000	No	Yes	2.00
99	6.52	9.24	3.05	5.78	1.00	14.26	7.30	104.07	4.000	No	Yes	2.00
100	6.59	9.21	3.05	5.79	1.00	14.21	7.32	103.97	4.000	No	Yes	2.00
101	6.64	9.22	3.05	5.76	1.00	14.22	7.30	103.76	4.000	No	Yes	2.00
102	6.70	9.21	3.05	5.73	1.00	14.20	7.29	103.45	4.000	No	Yes	2.00
103	6.78	9.24	3.04	5.67	1.00	14.24	7.24	103.04	4.000	No	Yes	2.00
104	6.83	9.24	3.04	5.66	1.00	14.24	7.23	102.93	4.000	No	Yes	2.00
105	6.89	9.27	3.04	5.66	1.00	14.28	7.22	103.14	4.000	No	Yes	2.00
106	6.98	9.30	3.04	5.70	1.00	14.32	7.23	103.56	4.000	No	Yes	2.00
107	7.03	9.35	3.04	5.74	1.00	14.39	7.24	104.19	4.000	No	Yes	2.00
108	7.09	9.39	3.04	5.79	1.00	14.45	7.25	104.80	4.000	No	Yes	2.00
109	7.18	9.43	3.05	5.86	1.00	14.51	7.27	105.52	4.000	No	Yes	2.00
110	7.23	9.47	3.05	5.92	1.00	14.57	7.29	106.24	4.000	No	Yes	2.00
111	7.29	9.51	3.05	5.93	1.00	14.63	7.28	106.54	4.000	No	Yes	2.00
112	7.38	9.51	3.05	5.92	1.00	14.62	7.28	106.44	4.000	No	Yes	2.00
113	7.42	9.52	3.05	5.91	1.00	14.63	7.27	106.34	4.000	No	Yes	2.00
114	7.48	9.51	3.05	5.90	1.00	14.61	7.27	106.24	4.000	No	Yes	2.00
115	7.58	9.49	3.05	5.89	1.00	14.57	7.28	106.03	4.000	No	Yes	2.00
116	7.62	9.43	3.05	5.86	1.00	14.47	7.28	105.42	4.000	No	Yes	2.00
117	7.68	9.37	3.05	5.79	1.00	14.36	7.28	104.49	4.000	No	Yes	2.00
118	7.78	9.31	3.04	5.71	1.00	14.25	7.26	103.45	4.000	No	Yes	2.00
119	7.81	9.25	3.04	5.60	1.00	14.16	7.22	102.20	4.000	No	Yes	2.00
120	7.88	9.22	3.04	5.53	1.00	14.10	7.19	101.46	4.000	No	Yes	2.00
121	7.97	9.19	3.04	5.49	1.00	14.05	7.18	100.93	4.000	No	Yes	2.00
122	8.01	9.17	3.03	5.40	1.00	14.02	7.14	100.07	4.000	No	Yes	2.00
123	8.11	9.14	3.03	5.29	1.00	13.96	7.09	98.99	4.000	No	Yes	2.00
124	8.14	9.10	3.03	5.19	1.00	13.89	7.05	97.90	4.000	No	Yes	2.00
125	8.22	9.05	3.02	5.11	1.00	13.81	7.02	96.90	4.000	No	Yes	2.00
126	8.31	8.96	3.03	5.06	1.00	13.66	7.03	96.01	4.000	No	Yes	2.00
127	8.35	8.84	3.03	5.02	1.00	13.45	7.06	95.00	4.000	No	Yes	2.00
128	8.41	8.65	3.04	5.00	1.00	13.14	7.14	93.85	4.000	No	Yes	2.00
129	8.50	8.44	3.04	4.95	1.00	12.80	7.21	92.34	4.000	No	Yes	2.00
130	8.56	8.22	3.05	4.91	1.00	12.45	7.30	90.80	4.000	No	Yes	2.00
131	8.61	8.02	3.05	4.84	1.00	12.11	7.36	89.12	4.000	No	Yes	2.00
132	8.68	7.81	3.06	4.76	1.00	11.77	7.43	87.40	4.000	No	Yes	2.00
133	8.75	7.62	3.06	4.64	1.00	11.46	7.45	85.41	4.000	No	Yes	2.00
134	8.80	7.46	3.06	4.51	1.00	11.19	7.46	83.50	4.000	No	Yes	2.00
135	8.89	7.34	3.06	4.37	1.00	10.99	7.43	81.68	4.000	No	Yes	2.00
136	8.94	7.28	3.05	4.19	1.00	10.89	7.34	79.97	4.000	No	Yes	2.00
137	9.00	7.30	3.04	4.00	1.00	10.92	7.19	78.50	4.000	No	Yes	2.00
138	9.08	7.36	3.02	3.81	1.00	11.01	7.00	77.13	4.000	No	Yes	2.00
139	9.15	7.44	3.01	3.64	1.00	11.14	6.82	76.02	4.000	No	Yes	2.00
140	9.20	7.49	3.00	3.50	1.00	11.22	6.69	75.01	4.000	No	Yes	2.00
141	9.28	7.51	2.99	3.40	1.00	11.24	6.60	74.14	4.000	No	Yes	2.00
142	9.35	7.52	2.98	3.35	1.00	11.25	6.55	73.70	4.000	No	Yes	2.00
143	9.40	7.54	2.98	3.34	1.00	11.28	6.53	73.70	4.000	No	Yes	2.00
144	9.45	7.59	2.98	3.36	1.00	11.36	6.53	74.13	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
145	9.55	7.66	2.98	3.44	1.00	11.46	6.56	75.15	4.000	No	Yes	2.00
146	9.59	7.88	2.98	3.55	1.00	11.81	6.53	77.12	4.000	No	Yes	2.00
147	9.69	8.26	2.98	3.76	1.00	12.41	6.50	80.66	4.000	No	Yes	2.00
148	9.74	8.85	2.96	3.93	1.00	13.35	6.36	84.90	4.000	No	Yes	2.00
149	9.79	9.71	2.95	4.18	1.00	14.73	6.18	91.03	4.000	No	Yes	2.00
150	9.84	10.70	2.93	4.40	0.99	16.32	5.97	97.37	4.000	No	Yes	2.00
151	9.94	11.82	2.90	4.60	0.98	18.10	5.74	103.99	4.000	No	Yes	2.00
152	10.00	13.13	2.88	4.73	0.97	20.20	5.47	110.57	4.000	No	Yes	2.00
153	10.09	14.51	2.85	4.84	0.96	22.41	5.22	117.08	4.000	No	Yes	2.00
154	10.13	15.87	2.83	4.93	0.95	24.60	5.00	123.02	4.000	No	Yes	2.00
155	10.18	17.10	2.81	5.02	0.94	26.57	4.83	128.46	4.000	No	Yes	2.00
156	10.24	18.19	2.79	5.09	0.94	28.31	4.70	133.07	4.000	No	Yes	2.00
157	10.33	19.08	2.78	5.16	0.93	29.73	4.61	137.04	4.000	No	Yes	2.00
158	10.37	19.75	2.77	5.12	0.93	30.80	4.50	138.53	4.000	No	Yes	2.00
159	10.43	20.34	2.75	5.06	0.92	31.75	4.39	139.54	4.000	No	Yes	2.00
160	10.52	20.84	2.74	4.99	0.92	32.54	4.30	140.02	4.000	No	Yes	2.00
161	10.59	21.08	2.73	4.95	0.92	32.92	4.26	140.09	4.000	No	Yes	2.00
162	10.64	21.13	2.73	4.91	0.92	32.99	4.23	139.63	4.000	No	Yes	2.00
163	10.70	20.97	2.73	4.91	0.92	32.65	4.26	139.01	4.000	No	Yes	2.00
164	10.78	20.88	2.74	4.88	0.92	32.28	4.27	137.82	4.000	No	Yes	2.00
165	10.83	20.80	2.74	4.83	0.92	32.00	4.27	136.50	4.000	No	Yes	2.00
166	10.94	20.72	2.74	4.78	0.92	31.57	4.28	134.99	4.000	No	Yes	2.00
167	10.99	20.74	2.74	4.79	0.92	31.46	4.28	134.82	4.000	No	Yes	2.00
168	11.03	21.20	2.73	4.70	0.91	31.99	4.20	134.49	4.000	No	Yes	2.00
169	11.09	21.83	2.71	4.59	0.91	32.70	4.10	134.07	4.000	No	Yes	2.00
170	11.17	22.79	2.69	4.46	0.90	33.81	3.96	133.84	4.000	No	Yes	2.00
171	11.24	23.92	2.67	4.34	0.89	35.18	3.81	134.18	4.000	No	Yes	2.00
172	11.33	25.05	2.66	4.25	0.89	36.47	3.69	134.60	4.000	No	Yes	2.00
173	11.37	25.77	2.65	4.25	0.88	37.35	3.64	136.05	4.000	No	Yes	2.00
174	11.44	26.22	2.65	4.29	0.88	37.80	3.63	137.34	4.000	No	Yes	2.00
175	11.52	26.58	2.65	4.32	0.88	38.07	3.64	138.41	4.000	No	Yes	2.00
176	11.57	26.65	2.65	4.38	0.89	38.03	3.66	139.31	4.000	No	Yes	2.00
177	11.63	26.16	2.67	4.48	0.89	37.23	3.76	139.89	4.000	No	Yes	2.00
178	11.72	25.38	2.69	4.63	0.90	35.96	3.90	140.36	4.000	No	Yes	2.00
179	11.76	24.28	2.71	4.77	0.91	34.38	4.07	139.96	4.000	No	Yes	2.00
180	11.83	23.04	2.73	4.87	0.92	32.52	4.25	138.03	4.000	No	Yes	2.00
181	11.92	21.96	2.75	4.90	0.92	30.82	4.39	135.33	4.000	No	Yes	2.00
182	11.94	21.21	2.76	4.82	0.93	29.72	4.44	132.01	4.000	No	Yes	2.00
183	12.02	20.75	2.76	4.68	0.93	28.89	4.44	128.38	4.000	No	Yes	2.00
184	12.11	20.42	2.76	4.52	0.93	28.28	4.42	124.87	4.000	No	Yes	2.00
185	12.16	20.40	2.74	4.32	0.92	28.14	4.32	121.60	4.000	No	Yes	2.00
186	12.22	20.54	2.73	4.14	0.92	28.21	4.22	119.09	4.000	No	Yes	2.00
187	12.31	20.81	2.72	3.98	0.91	28.44	4.11	117.01	4.000	No	Yes	2.00
188	12.36	21.16	2.71	3.92	0.91	28.83	4.05	116.71	4.000	No	Yes	2.00
189	12.42	21.60	2.70	3.93	0.91	29.35	4.01	117.81	4.000	No	Yes	2.00
190	12.50	22.12	2.70	3.97	0.90	29.98	3.99	119.47	4.000	No	Yes	2.00
191	12.56	22.63	2.70	4.03	0.90	30.60	3.97	121.49	4.000	No	Yes	2.00
192	12.62	23.07	2.70	4.14	0.90	31.16	3.98	124.10	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
193	12.70	23.50	2.70	4.25	0.90	31.67	4.00	126.72	4.000	No	Yes	2.00
194	12.77	23.80	2.71	4.39	0.91	32.03	4.05	129.56	4.000	No	Yes	2.00
195	12.81	23.99	2.71	4.51	0.91	32.28	4.09	132.01	4.000	No	Yes	2.00
196	12.91	24.10	2.72	4.60	0.91	32.33	4.13	133.52	4.000	No	Yes	2.00
197	12.96	24.23	2.72	4.63	0.91	32.45	4.13	134.17	4.000	No	Yes	2.00
198	13.01	24.25	2.72	4.64	0.91	32.42	4.14	134.28	4.000	No	Yes	2.00
199	13.06	24.27	2.72	4.59	0.91	32.37	4.12	133.47	4.000	No	Yes	2.00
200	13.16	24.35	2.71	4.51	0.91	32.33	4.09	132.12	4.000	No	Yes	2.00
201	13.21	24.41	2.70	4.39	0.91	32.31	4.03	130.18	4.000	No	Yes	2.00
202	13.26	24.42	2.70	4.26	0.90	32.22	3.97	127.80	4.000	No	Yes	2.00
203	13.36	24.44	2.69	4.11	0.90	32.08	3.90	125.14	4.000	No	Yes	2.00
204	13.40	24.45	2.68	4.04	0.90	32.02	3.87	123.86	4.000	No	Yes	2.00
205	13.46	24.56	2.68	4.00	0.90	32.08	3.84	123.35	4.000	No	Yes	2.00
206	13.55	24.66	2.68	3.99	0.90	32.11	3.84	123.20	4.000	No	Yes	2.00
207	13.60	24.84	2.68	3.99	0.90	32.28	3.83	123.53	4.000	No	Yes	2.00
208	13.67	24.92	2.68	4.06	0.90	32.33	3.86	124.78	4.000	No	Yes	2.00
209	13.75	24.93	2.69	4.16	0.90	32.28	3.91	126.36	4.000	No	Yes	2.00
210	13.80	25.07	2.69	4.24	0.90	32.43	3.95	127.94	4.000	No	Yes	2.00
211	13.86	25.25	2.70	4.33	0.90	32.61	3.97	129.61	4.000	No	Yes	2.00
212	13.95	25.36	2.70	4.42	0.91	32.67	4.02	131.18	4.000	No	Yes	2.00
213	13.99	25.41	2.70	4.43	0.91	32.69	4.02	131.45	4.000	No	Yes	2.00
214	14.06	25.37	2.70	4.41	0.91	32.55	4.02	130.82	4.000	No	Yes	2.00
215	14.15	25.16	2.71	4.38	0.91	32.18	4.03	129.77	4.000	No	Yes	2.00
216	14.19	24.83	2.71	4.35	0.91	31.70	4.05	128.37	4.000	No	Yes	2.00
217	14.26	24.43	2.71	4.29	0.91	31.11	4.07	126.50	4.000	No	Yes	2.00
218	14.35	24.01	2.71	4.24	0.91	30.46	4.09	124.52	4.000	No	Yes	2.00
219	14.40	23.37	2.72	4.20	0.91	29.60	4.14	122.43	4.000	No	Yes	2.00
220	14.45	22.69	2.73	4.16	0.91	28.67	4.19	120.19	4.000	No	Yes	2.00
221	14.55	22.01	2.73	4.12	0.92	27.72	4.25	117.90	4.000	No	Yes	2.00
222	14.58	21.36	2.74	4.08	0.92	26.87	4.31	115.74	4.000	No	Yes	2.00
223	14.65	20.73	2.75	4.06	0.92	26.00	4.38	113.97	4.000	No	Yes	2.00
224	14.74	20.12	2.76	4.06	0.93	25.16	4.47	112.38	4.000	No	Yes	2.00
225	14.77	19.60	2.77	4.06	0.93	24.48	4.54	111.04	4.000	No	Yes	2.00
226	14.84	19.12	2.78	4.05	0.93	23.82	4.60	109.67	4.000	No	Yes	2.00
227	14.94	18.65	2.79	4.02	0.94	23.15	4.67	108.06	4.000	No	Yes	2.00
228	15.00	18.25	2.79	4.02	0.94	22.61	4.73	106.87	4.000	No	Yes	2.00
229	15.03	17.87	2.80	4.02	0.94	22.10	4.79	105.97	4.000	No	Yes	2.00
230	15.11	17.43	2.81	4.02	0.95	21.50	4.87	104.76	4.000	No	Yes	2.00
231	15.19	17.06	2.82	4.03	0.95	20.99	4.95	103.84	4.000	No	Yes	2.00
232	15.24	16.70	2.83	4.03	0.95	20.50	5.01	102.77	4.000	No	Yes	2.00
233	15.29	16.35	2.83	4.00	0.95	20.02	5.06	101.39	4.000	No	Yes	2.00
234	15.39	15.99	2.84	3.97	0.96	19.51	5.12	99.95	4.000	No	Yes	2.00
235	15.42	15.64	2.84	3.93	0.96	19.05	5.17	98.56	4.000	No	Yes	2.00
236	15.49	15.29	2.85	3.89	0.96	18.56	5.23	97.01	4.000	No	Yes	2.00
237	15.59	14.91	2.86	3.85	0.96	18.03	5.29	95.32	4.000	No	Yes	2.00
238	15.63	14.59	2.86	3.78	0.96	17.60	5.32	93.63	4.000	No	Yes	2.00
239	15.69	14.34	2.86	3.73	0.97	17.24	5.35	92.15	4.000	No	Yes	2.00
240	15.78	14.10	2.86	3.65	0.97	16.88	5.36	90.51	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
241	15.84	13.90	2.87	3.58	0.97	16.60	5.37	89.04	4.000	No	Yes	2.00
242	15.89	13.80	2.86	3.51	0.97	16.44	5.35	87.93	4.000	No	Yes	2.00
243	15.95	13.74	2.86	3.46	0.97	16.32	5.33	87.08	4.000	No	Yes	2.00
244	16.04	13.72	2.86	3.43	0.97	16.25	5.33	86.58	4.000	No	Yes	2.00
245	16.08	13.81	2.86	3.43	0.96	16.34	5.31	86.70	4.000	No	Yes	2.00
246	16.18	13.99	2.86	3.42	0.96	16.50	5.27	87.01	4.000	No	Yes	2.00
247	16.24	14.14	2.85	3.45	0.96	16.65	5.27	87.68	4.000	No	Yes	2.00
248	16.28	14.42	2.85	3.46	0.96	16.97	5.21	88.39	4.000	No	Yes	2.00
249	16.36	14.72	2.84	3.47	0.96	17.29	5.16	89.23	4.000	No	Yes	2.00
250	16.43	15.02	2.84	3.49	0.96	17.62	5.12	90.16	4.000	No	Yes	2.00
251	16.47	15.27	2.84	3.53	0.96	17.90	5.10	91.24	4.000	No	Yes	2.00
252	16.54	15.56	2.83	3.53	0.95	18.21	5.04	91.86	4.000	No	Yes	2.00
253	16.63	15.86	2.82	3.50	0.95	18.51	4.97	92.06	4.000	No	Yes	2.00
254	16.68	16.03	2.82	3.45	0.95	18.68	4.91	91.80	4.000	No	Yes	2.00
255	16.78	16.10	2.81	3.40	0.95	18.69	4.88	91.18	4.000	No	Yes	2.00
256	16.83	16.13	2.81	3.35	0.94	18.68	4.84	90.44	4.000	No	Yes	2.00
257	16.87	16.04	2.81	3.31	0.94	18.55	4.84	89.77	4.000	No	Yes	2.00
258	16.93	15.94	2.81	3.27	0.94	18.39	4.83	88.90	4.000	No	Yes	2.00
259	17.01	15.83	2.81	3.22	0.94	18.21	4.83	87.90	4.000	No	Yes	2.00
260	17.09	15.76	2.80	3.16	0.94	18.07	4.81	86.88	4.000	No	Yes	2.00
261	17.15	15.65	2.80	3.13	0.94	17.90	4.81	86.10	4.000	No	Yes	2.00
262	17.20	15.51	2.81	3.12	0.94	17.70	4.84	85.64	4.000	No	Yes	2.00
263	17.27	15.51	2.81	3.10	0.94	17.67	4.83	85.37	4.000	No	Yes	2.00
264	17.35	15.60	2.80	3.08	0.94	17.73	4.81	85.24	4.000	No	Yes	2.00
265	17.40	15.80	2.80	3.04	0.94	17.93	4.75	85.08	4.000	No	Yes	2.00
266	17.45	15.97	2.79	3.01	0.94	18.09	4.69	84.93	4.000	No	Yes	2.00
267	17.55	16.10	2.79	2.99	0.94	18.19	4.67	84.87	4.000	No	Yes	2.00
268	17.59	16.19	2.78	2.98	0.94	18.27	4.65	84.88	4.000	No	Yes	2.00
269	17.65	16.20	2.78	2.97	0.94	18.24	4.64	84.72	4.000	No	Yes	2.00
270	17.75	16.19	2.78	2.97	0.94	18.18	4.65	84.55	4.000	No	Yes	2.00
271	17.79	16.19	2.78	2.96	0.94	18.15	4.64	84.31	4.000	No	Yes	2.00
272	17.87	16.11	2.79	2.96	0.94	18.02	4.67	84.19	4.000	No	Yes	2.00
273	17.94	16.00	2.79	2.99	0.94	17.86	4.72	84.20	4.000	No	Yes	2.00
274	17.98	15.82	2.80	3.04	0.94	17.64	4.79	84.47	4.000	No	Yes	2.00
275	18.05	15.69	2.81	3.09	0.95	17.45	4.86	84.79	4.000	No	Yes	2.00
276	18.14	15.56	2.82	3.14	0.95	17.26	4.93	85.08	4.000	No	Yes	2.00
277	18.18	15.48	2.82	3.18	0.95	17.15	4.98	85.39	4.000	No	Yes	2.00
278	18.24	15.47	2.83	3.22	0.95	17.11	5.02	85.83	4.000	No	Yes	2.00
279	18.34	15.47	2.83	3.27	0.95	17.07	5.06	86.33	4.000	No	Yes	2.00
280	18.39	15.46	2.84	3.32	0.96	17.03	5.10	86.87	4.000	No	Yes	2.00
281	18.44	15.44	2.84	3.36	0.96	16.99	5.13	87.21	4.000	No	Yes	2.00
282	18.54	15.40	2.85	3.40	0.96	16.90	5.18	87.53	4.000	No	Yes	2.00
283	18.59	15.35	2.85	3.43	0.96	16.82	5.22	87.79	4.000	No	Yes	2.00
284	18.64	15.27	2.85	3.46	0.96	16.71	5.26	87.88	4.000	No	Yes	2.00
285	18.74	15.17	2.86	3.49	0.96	16.55	5.31	87.93	4.000	No	Yes	2.00
286	18.79	15.04	2.87	3.54	0.97	16.38	5.38	88.05	4.000	No	Yes	2.00
287	18.84	14.91	2.87	3.56	0.97	16.20	5.43	87.97	4.000	No	Yes	2.00
288	18.92	14.77	2.88	3.58	0.97	16.00	5.49	87.78	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
289	18.97	14.58	2.89	3.61	0.97	15.76	5.55	87.54	4.000	No	Yes	2.00
290	19.04	14.35	2.89	3.63	0.98	15.47	5.63	87.11	4.000	No	Yes	2.00
291	19.14	14.06	2.90	3.65	0.98	15.10	5.73	86.48	4.000	No	Yes	2.00
292	19.17	13.75	2.91	3.67	0.98	14.73	5.82	85.74	4.000	No	Yes	2.00
293	19.24	13.40	2.92	3.68	0.99	14.31	5.93	84.86	4.000	No	Yes	2.00
294	19.34	13.05	2.94	3.70	0.99	13.87	6.05	83.94	4.000	No	Yes	2.00
295	19.39	12.70	2.94	3.68	1.00	13.45	6.14	82.65	4.000	No	Yes	2.00
296	19.43	12.35	2.95	3.64	1.00	13.03	6.24	81.26	4.000	No	Yes	2.00
297	19.52	12.01	2.96	3.62	1.00	12.60	6.34	79.86	4.000	No	Yes	2.00
298	19.56	11.73	2.97	3.59	1.00	12.27	6.41	78.68	4.000	No	Yes	2.00
299	19.63	11.53	2.97	3.54	1.00	12.01	6.46	77.54	4.000	No	Yes	2.00
300	19.73	11.42	2.98	3.49	1.00	11.85	6.47	76.65	4.000	No	Yes	2.00
301	19.78	11.34	2.97	3.43	1.00	11.73	6.46	75.80	4.000	No	Yes	2.00
302	19.83	11.31	2.97	3.41	1.00	11.68	6.46	75.46	4.000	No	Yes	2.00
303	19.90	11.46	2.97	3.39	1.00	11.82	6.39	75.59	4.000	No	Yes	2.00
304	19.96	11.82	2.96	3.41	1.00	12.21	6.29	76.82	4.000	No	Yes	2.00
305	20.03	12.32	2.95	3.48	1.00	12.76	6.19	78.97	4.000	No	Yes	2.00
306	20.09	13.07	2.93	3.50	0.99	13.56	5.98	81.14	4.000	No	Yes	2.00
307	20.16	14.08	2.90	3.47	0.98	14.65	5.69	83.40	4.000	No	Yes	2.00
308	20.23	15.17	2.88	3.52	0.97	15.83	5.47	86.60	4.000	No	Yes	2.00
309	20.31	16.28	2.86	3.56	0.96	17.00	5.28	89.70	4.000	No	Yes	2.00
310	20.35	17.41	2.83	3.60	0.96	18.23	5.09	92.74	4.000	No	Yes	2.00
311	20.42	18.42	2.82	3.60	0.95	19.29	4.92	94.85	4.000	No	Yes	2.00
312	20.50	19.26	2.80	3.58	0.94	20.16	4.78	96.30	4.000	No	Yes	2.00
313	20.55	19.56	2.80	3.61	0.94	20.45	4.76	97.31	4.000	No	Yes	2.00
314	20.62	19.65	2.79	3.60	0.94	20.52	4.74	97.27	4.000	No	Yes	2.00
315	20.70	19.50	2.80	3.59	0.94	20.30	4.77	96.78	4.000	No	Yes	2.00
316	20.75	19.06	2.81	3.60	0.94	19.79	4.84	95.83	4.000	No	Yes	2.00
317	20.82	18.40	2.82	3.56	0.95	19.04	4.93	93.87	4.000	No	Yes	2.00
318	20.90	17.71	2.83	3.50	0.95	18.24	5.02	91.54	4.000	No	Yes	2.00
319	20.96	17.00	2.84	3.44	0.96	17.44	5.11	89.17	4.000	No	Yes	2.00
320	21.01	16.41	2.85	3.41	0.96	16.77	5.21	87.47	4.000	No	Yes	2.00
321	21.11	15.83	2.87	3.46	0.97	16.10	5.38	86.58	4.000	No	Yes	2.00
322	21.15	15.60	2.87	3.46	0.97	15.83	5.43	85.93	4.000	No	Yes	2.00
323	21.21	15.85	2.86	3.43	0.97	16.08	5.36	86.21	4.000	No	Yes	2.00
324	21.27	16.33	2.85	3.41	0.96	16.56	5.25	87.01	4.000	No	Yes	2.00
325	21.36	16.99	2.84	3.40	0.96	17.22	5.12	88.21	4.000	No	Yes	2.00
326	21.40	18.20	2.81	3.33	0.95	18.49	4.86	89.82	4.000	No	Yes	2.00
327	21.51	19.79	2.77	3.23	0.93	20.11	4.55	91.52	4.000	No	Yes	2.00
328	21.55	21.52	2.74	3.15	0.92	21.91	4.27	93.52	4.000	No	Yes	2.00
329	21.60	23.59	2.70	3.06	0.90	24.06	3.97	95.55	4.000	No	Yes	2.00
330	21.69	25.70	2.66	2.95	0.89	26.20	3.70	96.90	4.000	No	Yes	2.00
331	21.75	27.76	2.62	2.85	0.87	28.31	3.47	98.12	4.000	No	Yes	2.00
332	21.80	29.14	2.60	2.80	0.87	29.71	3.34	99.15	4.000	No	Yes	2.00
333	21.90	30.20	2.59	2.78	0.86	30.73	3.26	100.14	0.173	No	No	0.46
334	21.95	30.81	2.58	2.80	0.86	31.32	3.23	101.22	0.176	No	No	0.47
335	22.00	30.93	2.59	2.84	0.86	31.42	3.25	102.10	0.179	No	No	0.48
336	22.09	30.62	2.60	2.89	0.86	31.03	3.30	102.52	0.180	No	No	0.48

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
337	22.11	30.03	2.61	2.95	0.87	30.40	3.38	102.71	4.000	No	Yes	2.00
338	22.19	28.96	2.63	3.02	0.88	29.24	3.50	102.32	4.000	No	Yes	2.00
339	22.26	27.41	2.66	3.11	0.89	27.58	3.68	101.61	4.000	No	Yes	2.00
340	22.35	25.79	2.69	3.22	0.90	25.84	3.90	100.78	4.000	No	Yes	2.00
341	22.39	24.24	2.71	3.27	0.91	24.21	4.09	99.12	4.000	No	Yes	2.00
342	22.44	22.59	2.73	3.23	0.92	22.47	4.25	95.60	4.000	No	Yes	2.00
343	22.55	21.10	2.75	3.17	0.92	20.85	4.41	92.02	4.000	No	Yes	2.00
344	22.58	19.55	2.78	3.12	0.93	19.22	4.60	88.43	4.000	No	Yes	2.00
345	22.65	18.00	2.81	3.09	0.94	17.58	4.84	85.03	4.000	No	Yes	2.00
346	22.74	16.57	2.83	3.04	0.95	16.05	5.07	81.44	4.000	No	Yes	2.00
347	22.83	15.26	2.86	2.97	0.96	14.66	5.31	77.84	4.000	No	Yes	2.00
348	22.85	14.33	2.87	2.85	0.97	13.68	5.44	74.41	4.000	No	Yes	2.00
349	22.94	13.44	2.89	2.71	0.97	12.73	5.56	70.71	4.000	No	Yes	2.00
350	23.00	12.59	2.90	2.61	0.98	11.82	5.72	67.64	4.000	No	Yes	2.00
351	23.05	11.82	2.94	2.70	0.99	11.01	6.07	66.82	4.000	No	Yes	2.00
352	23.10	11.10	2.97	2.74	1.00	10.25	6.37	65.35	4.000	No	Yes	2.00
353	23.18	10.27	3.01	2.81	1.00	9.36	6.80	63.65	4.000	No	Yes	2.00
354	23.25	9.47	3.04	2.87	1.00	8.51	7.25	61.72	4.000	No	Yes	2.00
355	23.30	8.60	3.10	2.99	1.00	7.59	7.87	59.72	4.000	No	Yes	2.00
356	23.38	7.73	3.16	3.17	1.00	6.67	8.65	57.73	4.000	No	Yes	2.00
357	23.45	6.95	3.22	3.41	1.00	5.85	9.56	55.88	4.000	No	Yes	2.00
358	23.50	6.22	3.30	3.75	1.00	5.07	10.65	54.03	4.000	No	Yes	2.00
359	23.60	5.81	3.34	3.97	1.00	4.64	11.37	52.74	4.000	No	Yes	2.00
360	23.65	5.62	3.36	4.07	1.00	4.43	11.73	52.02	4.000	No	Yes	2.00
361	23.70	5.85	3.34	3.94	1.00	4.66	11.31	52.75	4.000	No	Yes	2.00
362	23.76	6.35	3.28	3.63	1.00	5.18	10.42	53.96	4.000	No	Yes	2.00
363	23.84	6.95	3.22	3.37	1.00	5.78	9.57	55.32	4.000	No	Yes	2.00
364	23.89	7.83	3.16	3.17	1.00	6.67	8.65	57.73	4.000	No	Yes	2.00
365	23.99	8.80	3.09	3.01	1.00	7.65	7.86	60.10	4.000	No	Yes	2.00
366	24.03	9.88	3.04	2.89	1.00	8.75	7.15	62.59	4.000	No	Yes	2.00
367	24.09	11.03	2.98	2.81	1.00	9.91	6.57	65.13	4.000	No	Yes	2.00
368	24.19	12.04	2.95	2.82	1.00	10.91	6.21	67.75	4.000	No	Yes	2.00
369	24.24	13.00	2.92	2.84	0.99	11.87	5.92	70.30	4.000	No	Yes	2.00
370	24.30	13.63	2.91	2.92	0.98	12.48	5.81	72.49	4.000	No	Yes	2.00
371	24.34	14.08	2.91	3.02	0.98	12.93	5.77	74.64	4.000	No	Yes	2.00
372	24.44	14.45	2.91	3.13	0.98	13.27	5.77	76.52	4.000	No	Yes	2.00
373	24.50	14.62	2.91	3.19	0.98	13.42	5.78	77.53	4.000	No	Yes	2.00
374	24.58	14.65	2.91	3.25	0.98	13.42	5.83	78.18	4.000	No	Yes	2.00
375	24.65	14.57	2.92	3.29	0.99	13.32	5.88	78.33	4.000	No	Yes	2.00
376	24.69	14.53	2.92	3.28	0.99	13.26	5.89	78.13	4.000	No	Yes	2.00
377	24.74	14.55	2.92	3.24	0.99	13.26	5.86	77.73	4.000	No	Yes	2.00
378	24.84	14.55	2.91	3.19	0.99	13.22	5.83	77.12	4.000	No	Yes	2.00
379	24.89	14.64	2.91	3.17	0.98	13.30	5.80	77.06	4.000	No	Yes	2.00
380	24.95	14.90	2.90	3.14	0.98	13.53	5.71	77.31	4.000	No	Yes	2.00
381	25.04	15.26	2.89	3.14	0.98	13.85	5.63	77.95	4.000	No	Yes	2.00
382	25.08	15.75	2.88	3.15	0.97	14.32	5.52	79.10	4.000	No	Yes	2.00
383	25.19	16.34	2.88	3.23	0.97	14.87	5.46	81.25	4.000	No	Yes	2.00
384	25.24	16.95	2.87	3.36	0.97	15.45	5.43	83.94	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
385	25.28	17.47	2.87	3.52	0.97	15.95	5.45	86.89	4.000	No	Yes	2.00
386	25.35	17.89	2.88	3.71	0.97	16.34	5.51	89.97	4.000	No	Yes	2.00
387	25.43	18.28	2.88	3.86	0.97	16.69	5.54	92.42	4.000	No	Yes	2.00
388	25.48	18.60	2.88	3.93	0.97	16.98	5.53	93.96	4.000	No	Yes	2.00
389	25.53	18.87	2.88	3.99	0.97	17.22	5.53	95.14	4.000	No	Yes	2.00
390	25.63	19.11	2.88	4.06	0.97	17.40	5.53	96.33	4.000	No	Yes	2.00
391	25.68	19.22	2.89	4.12	0.97	17.50	5.56	97.23	4.000	No	Yes	2.00
392	25.74	19.27	2.89	4.13	0.97	17.52	5.56	97.37	4.000	No	Yes	2.00
393	25.79	19.09	2.89	4.16	0.98	17.32	5.61	97.23	4.000	No	Yes	2.00
394	25.88	19.09	2.89	4.13	0.98	17.27	5.60	96.79	4.000	No	Yes	2.00
395	25.92	19.22	2.88	4.03	0.97	17.38	5.52	96.00	4.000	No	Yes	2.00
396	25.99	19.41	2.88	3.97	0.97	17.53	5.46	95.66	4.000	No	Yes	2.00
397	26.05	19.60	2.87	3.94	0.97	17.68	5.41	95.60	4.000	No	Yes	2.00
398	26.13	19.72	2.87	3.92	0.97	17.75	5.38	95.56	4.000	No	Yes	2.00
399	26.20	19.75	2.86	3.88	0.97	17.75	5.36	95.05	4.000	No	Yes	2.00
400	26.26	19.73	2.86	3.84	0.97	17.70	5.34	94.50	4.000	No	Yes	2.00
401	26.31	19.63	2.86	3.82	0.97	17.58	5.35	93.99	4.000	No	Yes	2.00
402	26.40	19.66	2.86	3.76	0.96	17.57	5.31	93.32	4.000	No	Yes	2.00
403	26.45	19.42	2.86	3.74	0.97	17.30	5.35	92.49	4.000	No	Yes	2.00
404	26.54	19.03	2.87	3.74	0.97	16.89	5.42	91.59	4.000	No	Yes	2.00
405	26.59	18.55	2.88	3.76	0.97	16.41	5.53	90.67	4.000	No	Yes	2.00
406	26.65	18.00	2.90	3.78	0.98	15.86	5.65	89.59	4.000	No	Yes	2.00
407	26.74	17.48	2.91	3.79	0.98	15.31	5.78	88.46	4.000	No	Yes	2.00
408	26.78	16.97	2.92	3.81	0.99	14.81	5.90	87.42	4.000	No	Yes	2.00
409	26.84	16.52	2.93	3.78	0.99	14.36	5.99	86.03	4.000	No	Yes	2.00
410	26.94	16.15	2.94	3.73	0.99	13.97	6.05	84.56	4.000	No	Yes	2.00
411	26.99	15.95	2.93	3.65	0.99	13.75	6.05	83.16	4.000	No	Yes	2.00
412	27.04	15.92	2.93	3.56	0.99	13.70	5.99	82.10	4.000	No	Yes	2.00
413	27.13	15.95	2.92	3.47	0.99	13.70	5.93	81.22	4.000	No	Yes	2.00
414	27.18	16.05	2.91	3.39	0.99	13.77	5.85	80.52	4.000	No	Yes	2.00
415	27.24	16.28	2.90	3.32	0.98	13.97	5.75	80.26	4.000	No	Yes	2.00
416	27.34	16.55	2.89	3.26	0.98	14.19	5.64	80.12	4.000	No	Yes	2.00
417	27.40	16.87	2.88	3.22	0.97	14.47	5.54	80.24	4.000	No	Yes	2.00
418	27.44	17.16	2.88	3.22	0.97	14.73	5.49	80.86	4.000	No	Yes	2.00
419	27.53	17.39	2.87	3.23	0.97	14.91	5.45	81.30	4.000	No	Yes	2.00
420	27.57	17.54	2.87	3.25	0.97	15.03	5.44	81.78	4.000	No	Yes	2.00
421	27.64	17.59	2.87	3.27	0.97	15.05	5.46	82.11	4.000	No	Yes	2.00
422	27.72	17.57	2.88	3.27	0.97	15.00	5.47	81.98	4.000	No	Yes	2.00
423	27.79	17.52	2.88	3.25	0.97	14.93	5.47	81.63	4.000	No	Yes	2.00
424	27.83	17.42	2.88	3.22	0.97	14.82	5.47	80.99	4.000	No	Yes	2.00
425	27.90	17.32	2.87	3.17	0.97	14.70	5.45	80.17	4.000	No	Yes	2.00
426	27.98	17.21	2.87	3.11	0.97	14.57	5.44	79.17	4.000	No	Yes	2.00
427	28.03	17.13	2.87	3.04	0.97	14.48	5.40	78.18	4.000	No	Yes	2.00
428	28.09	17.12	2.86	2.97	0.97	14.44	5.36	77.40	4.000	No	Yes	2.00
429	28.18	17.17	2.86	2.91	0.96	14.46	5.30	76.66	4.000	No	Yes	2.00
430	28.22	17.35	2.85	2.84	0.96	14.61	5.21	76.16	4.000	No	Yes	2.00
431	28.28	17.70	2.84	2.81	0.96	14.91	5.13	76.45	4.000	No	Yes	2.00
432	28.38	18.14	2.83	2.79	0.95	15.29	5.03	76.91	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
433	28.43	18.79	2.82	2.81	0.95	15.87	4.93	78.24	4.000	No	Yes	2.00
434	28.48	19.60	2.80	2.81	0.94	16.60	4.79	79.56	4.000	No	Yes	2.00
435	28.58	20.45	2.79	2.85	0.94	17.34	4.70	81.50	4.000	No	Yes	2.00
436	28.62	21.32	2.79	2.98	0.94	18.13	4.67	84.61	4.000	No	Yes	2.00
437	28.69	22.17	2.79	3.14	0.94	18.87	4.66	88.01	4.000	No	Yes	2.00
438	28.77	22.93	2.79	3.30	0.94	19.53	4.68	91.42	4.000	No	Yes	2.00
439	28.82	23.56	2.79	3.47	0.94	20.08	4.72	94.77	4.000	No	Yes	2.00
440	28.88	24.03	2.80	3.65	0.94	20.48	4.78	97.92	4.000	No	Yes	2.00
441	28.97	24.41	2.81	3.84	0.95	20.77	4.86	100.91	4.000	No	Yes	2.00
442	29.01	24.63	2.82	3.99	0.95	20.95	4.93	103.16	4.000	No	Yes	2.00
443	29.07	24.64	2.83	4.16	0.95	20.92	5.04	105.36	4.000	No	Yes	2.00
444	29.15	24.58	2.84	4.30	0.96	20.82	5.13	106.80	4.000	No	Yes	2.00
445	29.21	24.40	2.85	4.36	0.96	20.62	5.19	107.09	4.000	No	Yes	2.00
446	29.30	24.21	2.85	4.38	0.96	20.39	5.24	106.94	4.000	No	Yes	2.00
447	29.33	23.98	2.86	4.39	0.96	20.17	5.28	106.50	4.000	No	Yes	2.00
448	29.41	23.70	2.86	4.36	0.96	19.87	5.31	105.43	4.000	No	Yes	2.00
449	29.50	23.37	2.86	4.30	0.97	19.52	5.33	104.05	4.000	No	Yes	2.00
450	29.53	23.04	2.86	4.23	0.97	19.21	5.33	102.41	4.000	No	Yes	2.00
451	29.61	22.66	2.86	4.14	0.97	18.83	5.34	100.59	4.000	No	Yes	2.00
452	29.70	22.38	2.86	4.03	0.96	18.54	5.32	98.65	4.000	No	Yes	2.00
453	29.74	22.16	2.85	3.90	0.96	18.32	5.27	96.58	4.000	No	Yes	2.00
454	29.80	22.07	2.85	3.74	0.96	18.22	5.18	94.41	4.000	No	Yes	2.00
455	29.90	22.00	2.84	3.58	0.96	18.11	5.09	92.22	4.000	No	Yes	2.00
456	29.93	22.08	2.82	3.42	0.95	18.18	4.97	90.35	4.000	No	Yes	2.00
457	30.00	22.43	2.80	3.25	0.94	18.47	4.81	88.80	4.000	No	Yes	2.00
458	30.09	23.10	2.78	3.06	0.93	19.03	4.58	87.25	4.000	No	Yes	2.00
459	30.15	23.44	2.76	2.94	0.93	19.31	4.46	86.11	4.000	No	Yes	2.00
460	30.19	23.51	2.76	2.89	0.92	19.36	4.42	85.48	4.000	No	Yes	2.00
461	30.30	23.75	2.75	2.84	0.92	19.53	4.35	85.04	4.000	No	Yes	2.00
462	30.33	23.80	2.75	2.85	0.92	19.56	4.36	85.29	4.000	No	Yes	2.00
463	30.40	23.99	2.75	2.88	0.92	19.69	4.36	85.88	4.000	No	Yes	2.00
464	30.49	24.26	2.75	2.89	0.92	19.89	4.34	86.36	4.000	No	Yes	2.00
465	30.54	24.43	2.74	2.90	0.92	20.02	4.33	86.75	4.000	No	Yes	2.00
466	30.59	24.35	2.75	2.93	0.92	19.92	4.37	87.03	4.000	No	Yes	2.00
467	30.64	23.97	2.76	2.99	0.93	19.56	4.46	87.26	4.000	No	Yes	2.00
468	30.72	23.92	2.77	3.03	0.93	19.47	4.50	87.64	4.000	No	Yes	2.00
469	30.80	24.13	2.76	3.02	0.93	19.62	4.47	87.72	4.000	No	Yes	2.00
470	30.88	24.07	2.77	3.07	0.93	19.53	4.52	88.30	4.000	No	Yes	2.00
471	30.93	24.43	2.77	3.10	0.93	19.82	4.51	89.29	4.000	No	Yes	2.00
472	31.00	25.09	2.76	3.13	0.93	20.36	4.45	90.55	4.000	No	Yes	2.00
473	31.04	25.89	2.75	3.14	0.92	21.05	4.36	91.89	4.000	No	Yes	2.00
474	31.13	26.92	2.73	3.13	0.92	21.91	4.25	93.21	4.000	No	Yes	2.00
475	31.20	27.99	2.72	3.13	0.91	22.82	4.15	94.69	4.000	No	Yes	2.00
476	31.29	28.87	2.71	3.14	0.91	23.54	4.08	96.05	4.000	No	Yes	2.00
477	31.34	29.38	2.71	3.17	0.91	23.95	4.05	97.07	4.000	No	Yes	2.00
478	31.38	29.75	2.71	3.20	0.91	24.26	4.04	98.00	4.000	No	Yes	2.00
479	31.43	29.95	2.70	3.18	0.90	24.40	4.02	98.01	4.000	No	Yes	2.00
480	31.51	29.81	2.70	3.12	0.90	24.24	3.99	96.77	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
481	31.58	29.15	2.70	3.05	0.90	23.63	4.01	94.73	4.000	No	Yes	2.00
482	31.63	28.20	2.71	2.98	0.91	22.78	4.05	92.32	4.000	No	Yes	2.00
483	31.71	26.91	2.72	2.92	0.91	21.61	4.15	89.67	4.000	No	Yes	2.00
484	31.78	25.56	2.74	2.87	0.92	20.41	4.26	86.95	4.000	No	Yes	2.00
485	31.83	24.29	2.75	2.82	0.92	19.28	4.37	84.32	4.000	No	Yes	2.00
486	31.90	23.14	2.76	2.75	0.93	18.26	4.48	81.74	4.000	No	Yes	2.00
487	31.98	22.27	2.77	2.66	0.93	17.48	4.52	79.05	4.000	No	Yes	2.00
488	32.03	21.54	2.77	2.56	0.93	16.84	4.55	76.69	4.000	No	Yes	2.00
489	32.09	20.84	2.78	2.51	0.93	16.21	4.62	74.93	4.000	No	Yes	2.00
490	32.16	20.13	2.79	2.50	0.94	15.57	4.73	73.67	4.000	No	Yes	2.00
491	32.22	19.49	2.81	2.51	0.94	15.00	4.85	72.78	4.000	No	Yes	2.00
492	32.30	19.02	2.82	2.52	0.95	14.56	4.95	72.13	4.000	No	Yes	2.00
493	32.38	18.67	2.83	2.53	0.95	14.24	5.03	71.60	4.000	No	Yes	2.00
494	32.42	18.64	2.83	2.52	0.95	14.20	5.03	71.43	4.000	No	Yes	2.00
495	32.50	18.90	2.82	2.49	0.95	14.39	4.97	71.49	4.000	No	Yes	2.00
496	32.56	19.05	2.82	2.51	0.95	14.50	4.96	71.91	4.000	No	Yes	2.00
497	32.62	19.22	2.82	2.57	0.95	14.62	4.98	72.88	4.000	No	Yes	2.00
498	32.72	19.47	2.82	2.63	0.95	14.80	5.00	74.02	4.000	No	Yes	2.00
499	32.77	19.78	2.83	2.70	0.95	15.05	5.01	75.31	4.000	No	Yes	2.00
500	32.82	20.17	2.82	2.77	0.95	15.35	5.00	76.77	4.000	No	Yes	2.00
501	32.91	20.58	2.82	2.84	0.95	15.66	4.99	78.18	4.000	No	Yes	2.00
502	32.97	20.98	2.82	2.90	0.95	15.98	4.98	79.57	4.000	No	Yes	2.00
503	33.02	21.23	2.83	2.97	0.95	16.16	5.00	80.83	4.000	No	Yes	2.00
504	33.11	21.45	2.83	3.05	0.95	16.32	5.03	82.05	4.000	No	Yes	2.00
505	33.16	21.63	2.83	3.11	0.95	16.44	5.06	83.15	4.000	No	Yes	2.00
506	33.22	21.81	2.83	3.16	0.95	16.57	5.07	83.95	4.000	No	Yes	2.00
507	33.29	21.97	2.83	3.20	0.95	16.67	5.08	84.67	4.000	No	Yes	2.00
508	33.37	22.11	2.84	3.24	0.96	16.76	5.09	85.32	4.000	No	Yes	2.00
509	33.41	22.18	2.84	3.29	0.96	16.79	5.12	86.01	4.000	No	Yes	2.00
510	33.47	22.32	2.84	3.36	0.96	16.88	5.16	87.04	4.000	No	Yes	2.00
511	33.57	22.42	2.85	3.45	0.96	16.92	5.21	88.17	4.000	No	Yes	2.00
512	33.60	22.79	2.85	3.51	0.96	17.21	5.20	89.47	4.000	No	Yes	2.00
513	33.67	23.28	2.85	3.58	0.96	17.59	5.18	91.17	4.000	No	Yes	2.00
514	33.76	23.80	2.85	3.67	0.96	17.98	5.18	93.12	4.000	No	Yes	2.00
515	33.80	24.36	2.84	3.79	0.96	18.42	5.18	95.41	4.000	No	Yes	2.00
516	33.86	24.91	2.85	3.91	0.96	18.84	5.19	97.86	4.000	No	Yes	2.00
517	33.96	25.43	2.85	4.04	0.96	19.22	5.21	100.16	4.000	No	Yes	2.00
518	34.00	25.94	2.85	4.13	0.96	19.62	5.21	102.23	4.000	No	Yes	2.00
519	34.06	26.36	2.85	4.20	0.96	19.93	5.20	103.72	4.000	No	Yes	2.00
520	34.16	26.76	2.85	4.25	0.96	20.21	5.19	104.93	4.000	No	Yes	2.00
521	34.20	26.82	2.85	4.32	0.96	20.23	5.23	105.84	4.000	No	Yes	2.00
522	34.26	26.68	2.86	4.36	0.96	20.09	5.28	105.97	4.000	No	Yes	2.00
523	34.36	26.55	2.86	4.37	0.96	19.93	5.31	105.74	4.000	No	Yes	2.00
524	34.39	26.36	2.86	4.35	0.97	19.76	5.32	105.17	4.000	No	Yes	2.00
525	34.46	26.14	2.86	4.32	0.97	19.55	5.33	104.24	4.000	No	Yes	2.00
526	34.56	25.91	2.86	4.28	0.97	19.31	5.34	103.23	4.000	No	Yes	2.00
527	34.60	25.62	2.86	4.24	0.97	19.06	5.36	102.22	4.000	No	Yes	2.00
528	34.65	25.33	2.87	4.21	0.97	18.80	5.39	101.26	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
529	34.75	25.05	2.87	4.17	0.97	18.52	5.41	100.23	4.000	No	Yes	2.00
530	34.80	24.81	2.87	4.13	0.97	18.31	5.42	99.30	4.000	No	Yes	2.00
531	34.86	24.61	2.87	4.11	0.97	18.12	5.44	98.56	4.000	No	Yes	2.00
532	34.95	24.38	2.87	4.08	0.97	17.90	5.46	97.68	4.000	No	Yes	2.00
533	34.99	24.19	2.88	4.03	0.97	17.73	5.46	96.78	4.000	No	Yes	2.00
534	35.06	24.08	2.87	3.98	0.97	17.61	5.45	95.90	4.000	No	Yes	2.00
535	35.11	23.94	2.87	3.93	0.97	17.48	5.44	95.02	4.000	No	Yes	2.00
536	35.19	23.83	2.87	3.87	0.97	17.36	5.42	94.06	4.000	No	Yes	2.00
537	35.25	23.70	2.87	3.81	0.97	17.24	5.40	93.16	4.000	No	Yes	2.00
538	35.31	23.56	2.87	3.75	0.97	17.10	5.39	92.15	4.000	No	Yes	2.00
539	35.39	23.40	2.87	3.70	0.97	16.95	5.38	91.17	4.000	No	Yes	2.00
540	35.49	23.26	2.87	3.64	0.97	16.80	5.37	90.16	4.000	No	Yes	2.00
541	35.53	23.14	2.87	3.61	0.97	16.69	5.37	89.62	4.000	No	Yes	2.00
542	35.60	23.03	2.87	3.61	0.97	16.57	5.39	89.34	4.000	No	Yes	2.00
543	35.63	22.98	2.87	3.64	0.97	16.52	5.42	89.51	4.000	No	Yes	2.00
544	35.70	23.28	2.87	3.65	0.97	16.73	5.39	90.12	4.000	No	Yes	2.00
545	35.78	23.79	2.86	3.68	0.97	17.11	5.34	91.39	4.000	No	Yes	2.00
546	35.84	24.40	2.86	3.74	0.96	17.57	5.29	93.03	4.000	No	Yes	2.00
547	35.90	25.23	2.85	3.82	0.96	18.20	5.24	95.32	4.000	No	Yes	2.00
548	35.98	26.27	2.84	3.85	0.96	19.00	5.13	97.44	4.000	No	Yes	2.00
549	36.06	27.66	2.81	3.75	0.95	20.09	4.90	98.43	4.000	No	Yes	2.00
550	36.09	29.05	2.78	3.57	0.93	21.22	4.63	98.16	4.000	No	Yes	2.00
551	36.18	30.33	2.75	3.38	0.92	22.24	4.38	97.40	4.000	No	Yes	2.00
552	36.23	31.16	2.73	3.24	0.92	22.90	4.22	96.52	4.000	No	Yes	2.00
553	36.29	31.53	2.72	3.19	0.91	23.17	4.15	96.09	4.000	No	Yes	2.00
554	36.38	31.68	2.72	3.15	0.91	23.26	4.11	95.64	4.000	No	Yes	2.00
555	36.42	32.10	2.71	3.13	0.91	23.58	4.07	95.94	4.000	No	Yes	2.00
556	36.49	33.06	2.70	3.13	0.90	24.32	3.99	97.04	4.000	No	Yes	2.00
557	36.58	34.30	2.69	3.15	0.90	25.26	3.91	98.78	4.000	Yes	Yes	2.00
558	36.62	36.32	2.67	3.19	0.89	26.86	3.79	101.91	4.000	Yes	Yes	2.00
559	36.68	39.95	2.65	3.27	0.88	29.72	3.62	107.49	4.000	Yes	Yes	2.00
560	36.77	44.99	2.61	3.31	0.87	33.72	3.38	113.80	4.000	Yes	Yes	2.00
561	36.83	52.72	2.54	3.21	0.84	39.94	3.00	119.98	4.000	Yes	No	2.00
562	36.88	62.36	2.47	3.08	0.82	47.77	2.64	126.28	4.000	Yes	No	2.00
563	36.97	72.24	2.42	2.97	0.80	55.77	2.38	132.66	4.000	Yes	No	2.00
564	37.02	81.77	2.37	2.90	0.78	63.53	2.19	138.89	4.000	Yes	No	2.00
565	37.08	89.81	2.33	2.86	0.76	70.05	2.07	144.68	4.000	Yes	No	2.00
566	37.17	96.99	2.31	2.85	0.76	75.82	1.98	150.13	0.395	No	No	0.96
567	37.22	102.33	2.30	2.88	0.75	80.09	1.94	155.26	0.428	No	No	1.04
568	37.27	105.76	2.29	2.92	0.75	82.79	1.92	158.89	0.453	No	No	1.10
569	37.37	108.07	2.29	2.95	0.75	84.49	1.91	161.53	0.472	No	No	1.14
570	37.41	108.62	2.29	3.01	0.75	84.82	1.93	163.58	0.487	No	No	1.18
571	37.47	108.08	2.30	3.06	0.75	84.24	1.95	164.56	0.494	No	No	1.20
572	37.57	107.73	2.31	3.10	0.75	83.75	1.97	165.17	0.499	No	No	1.21
573	37.61	107.99	2.31	3.09	0.75	83.91	1.97	164.91	0.497	No	No	1.20
574	37.67	110.10	2.29	3.03	0.75	85.56	1.93	164.87	0.497	No	No	1.20
575	37.76	112.74	2.28	2.95	0.74	87.63	1.88	164.62	0.495	No	No	1.20
576	37.81	116.12	2.26	2.83	0.73	90.39	1.81	163.96	0.490	No	No	1.19

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
577	37.87	119.49	2.24	2.79	0.73	93.08	1.78	165.30	0.500	No	No	1.21
578	37.97	123.02	2.23	2.76	0.73	95.80	1.74	167.09	0.514	No	No	1.24
579	38.02	126.08	2.22	2.76	0.72	98.19	1.73	169.55	0.533	No	No	1.29
580	38.07	128.60	2.22	2.81	0.72	100.10	1.73	172.82	0.560	No	No	1.36
581	38.17	130.76	2.23	2.92	0.73	101.53	1.75	177.46	0.600	No	No	1.45
582	38.20	133.02	2.24	3.06	0.73	103.16	1.78	183.33	0.653	No	No	1.58
583	38.27	136.19	2.25	3.18	0.73	105.44	1.80	189.57	0.714	No	No	1.73
584	38.33	141.08	2.25	3.29	0.73	109.15	1.80	196.53	0.786	No	No	1.90
585	38.42	146.42	2.25	3.39	0.73	113.13	1.80	203.92	4.000	No	No	2.00
586	38.46	152.19	2.24	3.43	0.73	117.65	1.78	209.76	4.000	No	No	2.00
587	38.53	157.18	2.24	3.47	0.73	121.44	1.77	215.00	4.000	No	No	2.00
588	38.62	161.63	2.24	3.50	0.73	124.77	1.76	219.36	4.000	No	No	2.00
589	38.66	165.38	2.23	3.51	0.73	127.66	1.75	222.81	4.000	No	No	2.00
590	38.73	169.32	2.22	3.46	0.72	130.70	1.72	224.42	4.000	No	No	2.00
591	38.81	173.12	2.21	3.40	0.72	133.62	1.69	225.39	4.000	No	No	2.00
592	38.86	175.78	2.20	3.33	0.71	135.72	1.66	225.22	4.000	No	No	2.00
593	38.93	177.38	2.19	3.27	0.71	136.92	1.64	224.21	4.000	No	No	2.00
594	39.02	179.58	2.17	3.18	0.70	138.58	1.61	222.75	4.000	No	No	2.00
595	39.05	181.60	2.16	3.09	0.70	140.28	1.58	221.31	4.000	No	No	2.00
596	39.12	182.85	2.15	3.01	0.69	141.22	1.56	219.61	4.000	No	No	2.00
597	39.18	183.12	2.14	2.95	0.69	141.38	1.54	217.70	4.000	No	No	2.00
598	39.27	183.29	2.14	2.89	0.69	141.39	1.53	215.65	4.000	No	No	2.00
599	39.31	184.01	2.13	2.83	0.69	141.97	1.51	214.11	4.000	No	No	2.00
600	39.37	182.93	2.12	2.78	0.68	141.02	1.50	211.74	4.000	No	No	2.00
601	39.44	182.32	2.12	2.73	0.68	140.45	1.49	209.45	4.000	No	No	2.00
602	39.50	182.24	2.11	2.67	0.68	140.34	1.48	207.34	4.000	No	No	2.00
603	39.59	181.64	2.11	2.62	0.68	139.74	1.47	205.04	4.000	No	No	2.00
604	39.65	180.71	2.10	2.56	0.68	138.96	1.46	202.25	4.000	No	No	2.00
605	39.71	179.11	2.09	2.48	0.67	137.69	1.44	198.38	0.806	No	No	1.96
606	39.77	177.03	2.08	2.38	0.67	136.09	1.42	193.62	0.755	No	No	1.83
607	39.84	174.31	2.07	2.26	0.66	134.01	1.40	187.78	0.696	No	No	1.69
608	39.91	169.90	2.06	2.15	0.66	130.56	1.39	181.00	0.631	No	No	1.53
609	39.97	167.59	2.04	2.00	0.65	128.92	1.36	174.76	0.576	No	No	1.40
610	40.03	163.25	2.03	1.87	0.65	125.60	1.34	167.87	0.520	No	No	1.26
611	40.11	158.20	2.01	1.75	0.64	121.67	1.32	160.59	0.465	No	No	1.13
612	40.17	153.76	2.00	1.63	0.64	118.29	1.30	153.83	0.419	No	No	1.02
613	40.26	150.03	1.99	1.51	0.63	115.42	1.28	147.85	0.381	No	No	0.92
614	40.30	148.43	1.96	1.40	0.62	114.38	1.26	143.56	0.355	No	No	0.86
615	40.36	148.43	1.94	1.29	0.61	114.61	1.23	140.76	0.339	No	No	0.82
616	40.45	149.44	1.92	1.21	0.61	115.54	1.21	139.38	0.332	No	No	0.81
617	40.49	150.84	1.90	1.15	0.60	116.84	1.19	138.73	0.328	No	No	0.80
618	40.57	151.01	1.89	1.10	0.59	117.01	1.18	137.62	0.322	No	No	0.78
619	40.62	151.62	1.87	1.06	0.59	117.60	1.16	136.87	0.318	No	No	0.77
620	40.70	151.46	1.87	1.03	0.59	117.45	1.16	136.06	0.314	No	No	0.76
621	40.76	150.02	1.87	1.03	0.59	116.16	1.16	134.96	0.309	No	No	0.75
622	40.86	148.25	1.88	1.05	0.59	114.50	1.17	133.87	0.303	No	No	0.74
623	40.89	146.27	1.89	1.07	0.60	112.74	1.18	133.07	0.299	No	No	0.73
624	40.95	144.41	1.91	1.11	0.60	110.99	1.19	132.55	0.297	No	No	0.72

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
625	41.03	143.07	1.92	1.15	0.61	109.63	1.21	132.49	0.296	No	No	0.72
626	41.11	142.22	1.93	1.20	0.61	108.67	1.22	132.84	0.298	No	No	0.72
627	41.16	141.92	1.95	1.25	0.62	108.15	1.24	134.04	0.304	No	No	0.74
628	41.23	141.98	1.97	1.32	0.62	107.87	1.26	135.72	0.312	No	No	0.76
629	41.29	142.10	1.98	1.38	0.63	107.69	1.27	137.23	0.320	No	No	0.78
630	41.35	142.20	1.99	1.43	0.63	107.53	1.29	138.47	0.327	No	No	0.80
631	41.41	142.21	2.00	1.48	0.64	107.30	1.30	139.67	0.333	No	No	0.81
632	41.49	142.08	2.01	1.54	0.64	106.91	1.32	140.92	0.340	No	No	0.83
633	41.56	141.57	2.03	1.62	0.65	106.15	1.35	142.81	0.351	No	No	0.85
634	41.64	140.45	2.06	1.73	0.66	104.86	1.38	144.72	0.362	No	No	0.88
635	41.69	138.39	2.08	1.86	0.67	102.85	1.43	146.71	0.374	No	No	0.91
636	41.73	135.34	2.12	2.01	0.68	100.06	1.49	148.72	0.386	No	No	0.94
637	41.84	131.91	2.15	2.17	0.69	96.89	1.55	150.57	0.397	No	No	0.97
638	41.89	128.64	2.18	2.34	0.71	93.97	1.63	152.81	0.412	No	No	1.00
639	41.98	126.30	2.21	2.48	0.72	91.79	1.69	154.98	0.426	No	No	1.04
640	42.04	124.44	2.23	2.60	0.72	90.08	1.74	156.76	0.438	No	No	1.07
641	42.09	123.04	2.24	2.68	0.73	88.81	1.78	157.96	0.447	No	No	1.09
642	42.16	122.85	2.24	2.68	0.73	88.56	1.78	157.62	0.444	No	No	1.08
643	42.24	123.41	2.24	2.62	0.73	88.94	1.76	156.37	0.436	No	No	1.06
644	42.28	124.88	2.22	2.52	0.72	90.15	1.71	154.54	0.423	No	No	1.03
645	42.33	127.01	2.20	2.39	0.71	91.92	1.66	152.37	0.409	No	No	1.00
646	42.39	129.14	2.17	2.26	0.70	93.69	1.60	150.19	0.395	No	No	0.96
647	42.47	130.67	2.15	2.14	0.70	94.96	1.56	147.85	0.381	No	No	0.93
648	42.53	130.88	2.14	2.07	0.69	95.17	1.53	145.93	0.369	No	No	0.90
649	42.59	130.36	2.14	2.05	0.69	94.72	1.53	144.89	0.363	No	No	0.89
650	42.66	128.15	2.15	2.08	0.69	92.84	1.55	144.24	0.359	No	No	0.88
651	42.73	125.51	2.17	2.16	0.70	90.55	1.60	144.49	4.000	Yes	No	2.00
652	42.83	121.32	2.20	2.31	0.71	86.92	1.67	145.58	4.000	Yes	No	2.00
653	42.88	116.08	2.25	2.54	0.73	82.53	1.79	147.81	4.000	Yes	No	2.00
654	42.93	110.69	2.30	2.80	0.75	78.01	1.93	150.89	4.000	Yes	No	2.00
655	42.99	105.22	2.35	3.10	0.77	73.48	2.10	154.56	4.000	Yes	No	2.00
656	43.07	100.21	2.39	3.41	0.79	69.35	2.28	158.34	4.000	Yes	No	2.00
657	43.14	95.63	2.44	3.70	0.80	65.62	2.46	161.52	4.000	Yes	No	2.00
658	43.19	90.87	2.47	3.95	0.82	61.88	2.64	163.11	4.000	Yes	No	2.00
659	43.25	86.68	2.50	4.09	0.83	58.66	2.77	162.37	4.000	Yes	No	2.00
660	43.34	81.82	2.53	4.20	0.84	54.96	2.91	160.19	4.000	Yes	No	2.00
661	43.39	77.67	2.55	4.23	0.85	51.89	3.02	156.69	4.000	Yes	No	2.00
662	43.45	73.11	2.57	4.20	0.85	48.56	3.12	151.56	0.404	No	No	0.99
663	43.54	68.41	2.58	4.15	0.86	45.14	3.22	145.56	0.367	No	No	0.90
664	43.59	63.67	2.60	4.04	0.87	41.76	3.32	138.68	0.328	No	No	0.80
665	43.64	58.08	2.62	3.93	0.87	37.78	3.46	130.82	4.000	No	Yes	2.00
666	43.74	52.40	2.65	3.80	0.88	33.73	3.63	122.45	4.000	No	Yes	2.00
667	43.78	46.98	2.68	3.66	0.89	29.92	3.82	114.29	4.000	No	Yes	2.00
668	43.83	42.15	2.71	3.58	0.91	26.52	4.06	107.56	4.000	No	Yes	2.00
669	43.94	37.81	2.75	3.54	0.92	23.43	4.34	101.74	4.000	No	Yes	2.00
670	43.98	34.06	2.78	3.50	0.94	20.82	4.64	96.56	4.000	No	Yes	2.00
671	44.04	31.95	2.80	3.39	0.94	19.35	4.77	92.25	4.000	No	Yes	2.00
672	44.14	30.33	2.81	3.24	0.94	18.23	4.84	88.21	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
673	44.17	29.10	2.81	3.09	0.95	17.40	4.87	84.75	4.000	No	Yes	2.00
674	44.23	28.76	2.81	3.00	0.94	17.17	4.84	83.14	4.000	No	Yes	2.00
675	44.33	28.68	2.80	2.95	0.94	17.09	4.82	82.35	4.000	No	Yes	2.00
676	44.37	29.02	2.80	2.91	0.94	17.32	4.74	82.18	4.000	No	Yes	2.00
677	44.44	29.52	2.79	2.97	0.94	17.63	4.74	83.55	4.000	No	Yes	2.00
678	44.53	30.09	2.80	3.09	0.94	17.96	4.77	85.75	4.000	No	Yes	2.00
679	44.58	30.72	2.81	3.25	0.94	18.34	4.83	88.54	4.000	No	Yes	2.00
680	44.64	31.59	2.81	3.43	0.95	18.87	4.87	91.92	4.000	No	Yes	2.00
681	44.73	33.07	2.81	3.59	0.94	19.81	4.84	95.80	4.000	No	Yes	2.00
682	44.78	34.76	2.80	3.75	0.94	20.91	4.78	100.00	4.000	No	Yes	2.00
683	44.82	36.82	2.79	3.87	0.94	22.27	4.68	104.27	4.000	No	Yes	2.00
684	44.90	39.32	2.77	3.97	0.93	23.92	4.55	108.78	4.000	No	Yes	2.00
685	44.97	41.98	2.76	4.07	0.93	25.69	4.42	113.46	4.000	No	Yes	2.00
686	45.03	45.07	2.73	4.08	0.92	27.77	4.22	117.33	4.000	No	Yes	2.00
687	45.09	48.02	2.71	4.07	0.91	29.77	4.05	120.66	4.000	No	Yes	2.00
688	45.17	50.82	2.69	4.05	0.90	31.66	3.90	123.53	4.000	No	Yes	2.00
689	45.22	53.50	2.67	4.04	0.89	33.49	3.77	126.23	4.000	No	Yes	2.00
690	45.29	55.93	2.65	4.02	0.89	35.13	3.66	128.50	4.000	No	Yes	2.00
691	45.38	58.32	2.63	3.98	0.88	36.73	3.55	130.31	4.000	No	Yes	2.00
692	45.42	60.57	2.62	3.92	0.87	38.30	3.43	131.40	4.000	No	Yes	2.00
693	45.50	62.33	2.60	3.85	0.87	39.50	3.34	131.76	4.000	No	Yes	2.00
694	45.57	63.62	2.59	3.79	0.86	40.38	3.27	131.88	0.293	No	No	0.73
695	45.62	64.35	2.58	3.75	0.86	40.86	3.23	131.80	0.293	No	No	0.72
696	45.69	64.79	2.58	3.71	0.86	41.14	3.19	131.34	0.291	No	No	0.72
697	45.77	65.03	2.57	3.67	0.86	41.27	3.17	130.71	0.288	No	No	0.71
698	45.82	64.64	2.57	3.63	0.86	40.97	3.17	129.68	0.283	No	No	0.70
699	45.88	63.43	2.58	3.63	0.86	40.09	3.20	128.34	0.277	No	No	0.68
700	45.97	61.81	2.59	3.63	0.86	38.90	3.26	126.83	0.270	No	No	0.67
701	46.02	59.45	2.61	3.68	0.87	37.20	3.37	125.35	4.000	No	Yes	2.00
702	46.10	56.51	2.63	3.78	0.88	35.08	3.54	124.07	4.000	No	Yes	2.00
703	46.17	53.60	2.66	3.88	0.89	32.99	3.72	122.72	4.000	No	Yes	2.00
704	46.21	50.91	2.69	3.98	0.90	31.09	3.90	121.40	4.000	No	Yes	2.00
705	46.27	48.55	2.71	4.06	0.91	29.43	4.07	119.86	4.000	No	Yes	2.00
706	46.36	46.40	2.73	4.12	0.92	27.90	4.24	118.19	4.000	No	Yes	2.00
707	46.42	44.50	2.75	4.17	0.92	26.58	4.39	116.57	4.000	No	Yes	2.00
708	46.46	42.82	2.77	4.22	0.93	25.41	4.53	115.16	4.000	No	Yes	2.00
709	46.56	41.38	2.79	4.27	0.94	24.39	4.67	113.82	4.000	No	Yes	2.00
710	46.61	40.40	2.80	4.30	0.94	23.70	4.76	112.81	4.000	No	Yes	2.00
711	46.66	39.90	2.80	4.29	0.94	23.35	4.80	112.07	4.000	No	Yes	2.00
712	46.74	39.54	2.81	4.31	0.94	23.07	4.85	111.78	4.000	No	Yes	2.00
713	46.81	39.12	2.82	4.37	0.95	22.74	4.92	111.81	4.000	No	Yes	2.00
714	46.87	38.64	2.83	4.46	0.95	22.38	5.02	112.27	4.000	No	Yes	2.00
715	46.94	38.63	2.83	4.51	0.95	22.33	5.05	112.77	4.000	No	Yes	2.00
716	47.01	38.71	2.83	4.56	0.95	22.33	5.08	113.37	4.000	No	Yes	2.00
717	47.06	38.83	2.84	4.60	0.96	22.38	5.10	114.02	4.000	No	Yes	2.00
718	47.12	39.01	2.84	4.63	0.96	22.46	5.10	114.54	4.000	No	Yes	2.00
719	47.19	39.29	2.83	4.61	0.95	22.62	5.07	114.67	4.000	No	Yes	2.00
720	47.25	39.58	2.83	4.57	0.95	22.79	5.02	114.47	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
721	47.34	39.73	2.82	4.51	0.95	22.86	4.98	113.86	4.000	No	Yes	2.00
722	47.39	39.72	2.82	4.45	0.95	22.85	4.95	113.08	4.000	No	Yes	2.00
723	47.44	39.77	2.81	4.38	0.95	22.88	4.90	112.17	4.000	No	Yes	2.00
724	47.54	39.28	2.82	4.35	0.95	22.52	4.93	111.05	4.000	No	Yes	2.00
725	47.59	38.71	2.82	4.33	0.95	22.13	4.97	110.09	4.000	No	Yes	2.00
726	47.65	38.41	2.82	4.31	0.95	21.91	4.99	109.31	4.000	No	Yes	2.00
727	47.74	37.95	2.83	4.32	0.95	21.57	5.04	108.75	4.000	No	Yes	2.00
728	47.81	37.56	2.84	4.35	0.96	21.28	5.10	108.54	4.000	No	Yes	2.00
729	47.85	37.47	2.84	4.37	0.96	21.20	5.12	108.59	4.000	No	Yes	2.00
730	47.94	37.60	2.84	4.37	0.96	21.25	5.12	108.69	4.000	No	Yes	2.00
731	47.98	37.97	2.84	4.39	0.96	21.46	5.09	109.34	4.000	No	Yes	2.00
732	48.04	38.79	2.83	4.39	0.95	21.97	5.03	110.49	4.000	No	Yes	2.00
733	48.13	39.93	2.82	4.40	0.95	22.66	4.94	112.01	4.000	No	Yes	2.00
734	48.17	41.38	2.81	4.39	0.94	23.58	4.83	113.87	4.000	No	Yes	2.00
735	48.24	42.73	2.80	4.43	0.94	24.42	4.75	116.08	4.000	No	Yes	2.00
736	48.32	44.25	2.79	4.46	0.94	25.35	4.67	118.31	4.000	No	Yes	2.00
737	48.37	46.09	2.77	4.47	0.93	26.53	4.55	120.75	4.000	No	Yes	2.00
738	48.44	48.52	2.75	4.43	0.92	28.08	4.39	123.16	4.000	Yes	Yes	2.00
739	48.53	51.56	2.72	4.34	0.91	30.04	4.17	125.39	4.000	Yes	Yes	2.00
740	48.56	54.96	2.69	4.21	0.90	32.30	3.94	127.24	4.000	Yes	Yes	2.00
741	48.64	59.29	2.65	4.03	0.89	35.19	3.66	128.73	4.000	Yes	Yes	2.00
742	48.72	64.04	2.61	3.85	0.87	38.37	3.40	130.28	4.000	Yes	Yes	2.00
743	48.78	69.67	2.57	3.65	0.85	42.21	3.12	131.70	4.000	Yes	No	2.00
744	48.83	76.00	2.52	3.45	0.83	46.56	2.86	133.11	4.000	Yes	No	2.00
745	48.90	82.27	2.48	3.29	0.82	50.88	2.65	134.67	4.000	Yes	No	2.00
746	48.97	87.90	2.44	3.20	0.81	54.74	2.50	136.96	4.000	Yes	No	2.00
747	49.03	93.07	2.42	3.15	0.80	58.27	2.40	139.62	4.000	Yes	No	2.00
748	49.12	97.81	2.40	3.13	0.79	61.45	2.32	142.53	0.349	No	No	0.88
749	49.16	102.84	2.38	3.10	0.78	64.88	2.24	145.62	0.367	No	No	0.93
750	49.23	107.68	2.37	3.08	0.78	68.15	2.18	148.54	0.385	No	No	0.97
751	49.31	113.16	2.35	3.04	0.77	71.90	2.10	151.31	0.402	No	No	1.02
752	49.36	118.20	2.33	3.00	0.76	75.37	2.04	153.88	0.419	No	No	1.06
753	49.43	123.66	2.31	2.95	0.75	79.14	1.97	156.19	0.434	No	No	1.10
754	49.52	130.09	2.28	2.87	0.75	83.63	1.90	158.50	0.450	No	No	1.14
755	49.58	137.03	2.25	2.77	0.73	88.58	1.81	160.30	0.463	No	No	1.17
756	49.62	143.61	2.23	2.65	0.72	93.36	1.73	161.63	0.473	No	No	1.20
757	49.71	149.84	2.19	2.48	0.71	98.02	1.64	160.96	0.468	No	No	1.19
758	49.78	155.24	2.15	2.31	0.70	102.19	1.56	159.69	0.459	No	No	1.16
759	49.81	159.41	2.13	2.18	0.69	105.51	1.50	158.62	0.451	No	No	1.14
760	49.88	162.01	2.11	2.08	0.68	107.57	1.46	157.54	0.444	No	No	1.13
761	49.97	163.35	2.09	2.02	0.67	108.59	1.44	156.61	0.437	No	No	1.11
762	50.00	161.66	2.09	2.00	0.67	107.39	1.44	155.04	0.427	No	No	1.08
763	50.07	160.26	2.10	2.00	0.67	106.28	1.45	153.97	4.000	No	No	2.00
764	50.14	158.20	2.10	2.02	0.68	104.64	1.46	153.02	4.000	No	No	2.00
765	50.22	154.55	2.12	2.06	0.68	101.76	1.49	151.80	4.000	Yes	No	2.00
766	50.27	149.22	2.15	2.20	0.70	97.52	1.56	151.87	4.000	Yes	No	2.00
767	50.35	143.10	2.19	2.37	0.71	92.63	1.65	152.47	4.000	Yes	No	2.00
768	50.40	135.60	2.23	2.55	0.73	86.89	1.76	152.50	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
769	50.47	127.45	2.28	2.72	0.74	80.82	1.87	151.35	4.000	Yes	No	2.00
770	50.55	119.71	2.31	2.84	0.76	75.19	1.98	149.24	4.000	Yes	No	2.00
771	50.59	114.02	2.33	2.90	0.76	71.17	2.06	146.72	4.000	Yes	No	2.00
772	50.66	106.49	2.37	2.98	0.78	65.86	2.18	143.35	4.000	Yes	No	2.00
773	50.75	98.69	2.40	3.05	0.79	60.41	2.31	139.61	4.000	Yes	No	2.00
774	50.79	91.04	2.44	3.13	0.80	55.16	2.46	135.79	4.000	Yes	No	2.00
775	50.86	83.73	2.47	3.19	0.82	50.19	2.62	131.58	4.000	Yes	No	2.00
776	50.94	76.84	2.51	3.24	0.83	45.52	2.79	127.20	4.000	Yes	No	2.00
777	50.99	70.78	2.54	3.26	0.84	41.49	2.96	122.83	4.000	Yes	No	2.00
778	51.05	65.41	2.57	3.27	0.85	37.95	3.12	118.60	4.000	Yes	No	2.00
779	51.14	60.12	2.60	3.28	0.87	34.47	3.31	114.18	4.000	Yes	No	2.00
780	51.18	54.60	2.64	3.31	0.88	30.89	3.55	109.70	4.000	Yes	Yes	2.00
781	51.25	49.39	2.67	3.28	0.89	27.54	3.79	104.45	4.000	Yes	Yes	2.00
782	51.34	44.37	2.71	3.21	0.91	24.36	4.04	98.37	4.000	Yes	Yes	2.00
783	51.41	40.71	2.72	3.02	0.91	22.11	4.16	91.95	4.000	No	Yes	2.00
784	51.44	38.40	2.72	2.76	0.91	20.75	4.14	85.82	4.000	No	Yes	2.00
785	51.52	36.49	2.71	2.46	0.91	19.65	4.05	79.66	4.000	No	Yes	2.00
786	51.67	35.22	2.69	2.16	0.90	18.94	3.91	74.02	4.000	No	Yes	2.00
787	51.70	34.13	2.68	1.96	0.90	18.33	3.82	70.04	4.000	No	Yes	2.00
788	51.75	33.21	2.67	1.86	0.89	17.79	3.81	67.69	4.000	No	Yes	2.00
789	51.78	32.42	2.68	1.80	0.90	17.30	3.82	66.11	4.000	No	Yes	2.00
790	51.88	32.20	2.68	1.81	0.90	17.13	3.85	65.99	4.000	No	Yes	2.00
791	51.92	32.47	2.69	1.87	0.90	17.26	3.89	67.16	4.000	No	Yes	2.00
792	51.99	32.74	2.69	1.95	0.90	17.38	3.94	68.52	4.000	No	Yes	2.00
793	52.04	32.85	2.71	2.05	0.91	17.38	4.04	70.20	4.000	No	Yes	2.00
794	52.14	32.83	2.72	2.17	0.91	17.29	4.15	71.79	4.000	No	Yes	2.00
795	52.19	32.56	2.74	2.28	0.92	17.06	4.29	73.12	4.000	No	Yes	2.00
796	52.26	31.97	2.76	2.38	0.93	16.63	4.44	73.88	4.000	No	Yes	2.00
797	52.33	31.02	2.78	2.45	0.93	16.00	4.61	73.79	4.000	No	Yes	2.00
798	52.38	29.91	2.80	2.51	0.94	15.28	4.80	73.35	4.000	No	Yes	2.00
799	52.43	28.33	2.83	2.58	0.95	14.28	5.07	72.33	4.000	No	Yes	2.00
800	52.51	26.65	2.86	2.62	0.97	13.23	5.35	70.78	4.000	No	Yes	2.00
801	52.58	25.06	2.89	2.63	0.98	12.25	5.62	68.88	4.000	No	Yes	2.00
802	52.63	23.61	2.91	2.59	0.99	11.38	5.85	66.51	4.000	No	Yes	2.00
803	52.69	22.29	2.93	2.53	0.99	10.60	6.04	64.03	4.000	No	Yes	2.00
804	52.77	21.16	2.95	2.44	1.00	9.93	6.20	61.57	4.000	No	Yes	2.00
805	52.83	20.40	2.96	2.34	1.00	9.49	6.27	59.49	4.000	No	Yes	2.00
806	52.90	19.92	2.96	2.25	1.00	9.22	6.29	57.98	4.000	No	Yes	2.00
807	52.99	19.57	2.96	2.16	1.00	9.02	6.27	56.56	4.000	No	Yes	2.00
808	53.05	19.39	2.95	2.07	1.00	8.91	6.22	55.38	4.000	No	Yes	2.00
809	53.10	19.24	2.95	2.01	1.00	8.82	6.19	54.61	4.000	No	Yes	2.00
810	53.16	19.09	2.95	1.97	1.00	8.74	6.18	53.96	4.000	No	Yes	2.00
811	53.25	18.99	2.95	1.94	1.00	8.67	6.17	53.51	4.000	No	Yes	2.00
812	53.29	18.94	2.95	1.92	1.00	8.64	6.16	53.22	4.000	No	Yes	2.00
813	53.38	18.91	2.94	1.88	1.00	8.62	6.12	52.77	4.000	No	Yes	2.00
814	53.44	18.88	2.94	1.85	1.00	8.60	6.09	52.39	4.000	No	Yes	2.00
815	53.50	18.85	2.94	1.82	0.99	8.58	6.07	52.09	4.000	No	Yes	2.00
816	53.55	18.80	2.94	1.81	0.99	8.54	6.07	51.85	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
817	53.64	18.73	2.94	1.80	1.00	8.49	6.09	51.68	4.000	No	Yes	2.00
818	53.72	18.66	2.94	1.80	1.00	8.44	6.10	51.50	4.000	No	Yes	2.00
819	53.74	18.66	2.94	1.79	1.00	8.44	6.09	51.43	4.000	No	Yes	2.00
820	53.82	18.74	2.94	1.78	0.99	8.47	6.07	51.42	4.000	No	Yes	2.00
821	53.90	18.83	2.94	1.79	0.99	8.51	6.06	51.55	4.000	No	Yes	2.00
822	53.94	18.95	2.94	1.81	0.99	8.58	6.05	51.92	4.000	No	Yes	2.00
823	54.01	19.10	2.94	1.83	0.99	8.65	6.05	52.34	4.000	No	Yes	2.00
824	54.09	19.25	2.94	1.86	0.99	8.72	6.05	52.76	4.000	No	Yes	2.00
825	54.19	19.41	2.93	1.87	0.99	8.79	6.04	53.10	4.000	No	Yes	2.00
826	54.24	19.57	2.93	1.88	0.99	8.88	6.01	53.39	4.000	No	Yes	2.00
827	54.29	19.71	2.93	1.89	0.99	8.95	5.99	53.60	4.000	No	Yes	2.00
828	54.35	19.78	2.93	1.88	0.99	8.98	5.97	53.59	4.000	No	Yes	2.00
829	54.44	19.79	2.92	1.86	0.99	8.98	5.94	53.36	4.000	No	Yes	2.00
830	54.49	19.78	2.92	1.83	0.99	8.98	5.90	53.01	4.000	No	Yes	2.00
831	54.53	19.74	2.92	1.79	0.99	8.96	5.87	52.57	4.000	No	Yes	2.00
832	54.63	19.69	2.91	1.75	0.99	8.92	5.83	52.05	4.000	No	Yes	2.00
833	54.68	19.64	2.91	1.71	0.98	8.90	5.79	51.53	4.000	No	Yes	2.00
834	54.74	19.58	2.91	1.68	0.98	8.86	5.76	51.08	4.000	No	Yes	2.00
835	54.83	19.56	2.90	1.64	0.98	8.85	5.73	50.69	4.000	No	Yes	2.00
836	54.88	19.53	2.90	1.63	0.98	8.82	5.73	50.52	4.000	No	Yes	2.00
837	54.94	19.53	2.91	1.66	0.98	8.81	5.77	50.80	4.000	No	Yes	2.00
838	55.03	19.54	2.91	1.70	0.99	8.79	5.83	51.22	4.000	No	Yes	2.00
839	55.07	19.56	2.92	1.75	0.99	8.78	5.89	51.71	4.000	No	Yes	2.00
840	55.13	19.56	2.93	1.80	0.99	8.76	5.97	52.25	4.000	No	Yes	2.00
841	55.23	19.57	2.93	1.86	0.99	8.74	6.04	52.78	4.000	No	Yes	2.00
842	55.28	19.59	2.94	1.91	1.00	8.73	6.11	53.32	4.000	No	Yes	2.00
843	55.32	19.63	2.95	1.96	1.00	8.73	6.17	53.85	4.000	No	Yes	2.00
844	55.42	19.66	2.95	1.99	1.00	8.72	6.21	54.15	4.000	No	Yes	2.00
845	55.50	19.75	2.95	1.99	1.00	8.77	6.19	54.28	4.000	No	Yes	2.00
846	55.53	19.81	2.94	1.97	1.00	8.80	6.15	54.15	4.000	No	Yes	2.00
847	55.58	19.82	2.94	1.96	1.00	8.80	6.14	54.07	4.000	No	Yes	2.00
848	55.66	19.80	2.94	1.95	1.00	8.78	6.13	53.84	4.000	No	Yes	2.00
849	55.73	19.80	2.93	1.87	0.99	8.79	6.03	53.02	4.000	No	Yes	2.00
850	55.78	19.97	2.94	1.96	1.00	8.86	6.11	54.17	4.000	No	Yes	2.00
851	55.86	20.32	2.95	2.12	1.00	9.02	6.23	56.19	4.000	No	Yes	2.00
852	55.93	20.98	2.96	2.31	1.00	9.35	6.30	58.91	4.000	Yes	Yes	2.00
853	55.97	22.90	2.94	2.56	1.00	10.37	6.15	63.82	4.000	Yes	Yes	2.00
854	56.08	26.02	2.90	2.72	0.98	12.11	5.74	69.47	4.000	Yes	Yes	2.00
855	56.12	30.92	2.83	2.72	0.95	14.96	5.04	75.34	4.000	Yes	Yes	2.00
856	56.17	39.52	2.70	2.50	0.91	20.15	4.02	81.08	4.000	Yes	Yes	2.00
857	56.28	48.92	2.60	2.35	0.87	25.93	3.32	86.19	4.000	Yes	No	2.00
858	56.32	59.00	2.51	2.24	0.83	32.27	2.83	91.38	4.000	Yes	No	2.00
859	56.37	69.47	2.43	2.10	0.80	39.03	2.44	95.22	4.000	Yes	No	2.00
860	56.47	79.91	2.36	1.98	0.77	45.84	2.16	98.82	4.000	Yes	No	2.00
861	56.52	90.20	2.30	1.87	0.75	52.68	1.95	102.49	4.000	Yes	No	2.00
862	56.57	98.80	2.25	1.81	0.73	58.43	1.81	105.88	4.000	Yes	No	2.00
863	56.67	105.68	2.23	1.78	0.72	62.98	1.73	109.00	4.000	No	No	2.00
864	56.72	109.54	2.22	1.80	0.72	65.45	1.71	111.70	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
865	56.78	108.92	2.23	1.88	0.73	64.78	1.75	113.30	4.000	Yes	No	2.00
866	56.87	106.09	2.26	1.99	0.74	62.58	1.83	114.28	4.000	Yes	No	2.00
867	56.91	101.69	2.30	2.12	0.75	59.38	1.94	114.91	4.000	Yes	No	2.00
868	56.97	94.90	2.35	2.32	0.77	54.58	2.11	115.36	4.000	Yes	No	2.00
869	57.03	87.46	2.41	2.55	0.79	49.42	2.35	116.07	4.000	Yes	No	2.00
870	57.11	79.60	2.48	2.85	0.82	44.05	2.66	117.05	4.000	Yes	No	2.00
871	57.17	72.07	2.54	3.12	0.84	39.08	3.00	117.09	4.000	Yes	No	2.00
872	57.26	64.98	2.61	3.38	0.87	34.48	3.36	115.99	4.000	Yes	Yes	2.00
873	57.32	58.98	2.66	3.58	0.89	30.71	3.71	114.08	4.000	Yes	Yes	2.00
874	57.35	53.23	2.71	3.76	0.91	27.19	4.10	111.44	4.000	Yes	Yes	2.00
875	57.42	48.56	2.76	3.89	0.93	24.36	4.45	108.40	4.000	Yes	Yes	2.00
876	57.51	44.62	2.80	3.97	0.94	22.00	4.78	105.07	4.000	Yes	Yes	2.00
877	57.55	42.37	2.81	3.90	0.95	20.71	4.91	101.63	4.000	Yes	Yes	2.00
878	57.62	40.27	2.82	3.78	0.95	19.53	5.00	97.64	4.000	No	Yes	2.00
879	57.71	38.27	2.83	3.62	0.95	18.41	5.07	93.40	4.000	No	Yes	2.00
880	57.78	36.28	2.84	3.50	0.96	17.29	5.18	89.53	4.000	No	Yes	2.00
881	57.82	34.25	2.86	3.40	0.97	16.16	5.32	86.01	4.000	No	Yes	2.00
882	57.90	32.33	2.88	3.30	0.97	15.08	5.47	82.51	4.000	No	Yes	2.00
883	57.96	30.91	2.88	3.15	0.97	14.30	5.53	79.14	4.000	No	Yes	2.00
884	58.01	29.77	2.88	2.98	0.97	13.70	5.54	75.90	4.000	No	Yes	2.00
885	58.11	28.76	2.88	2.82	0.97	13.15	5.54	72.86	4.000	No	Yes	2.00
886	58.15	27.83	2.88	2.66	0.97	12.67	5.53	70.01	4.000	No	Yes	2.00
887	58.21	27.11	2.88	2.51	0.97	12.29	5.50	67.59	4.000	No	Yes	2.00
888	58.31	26.42	2.88	2.37	0.97	11.92	5.46	65.17	4.000	No	Yes	2.00
889	58.35	25.74	2.87	2.22	0.97	11.58	5.43	62.82	4.000	No	Yes	2.00
890	58.42	25.07	2.87	2.13	0.97	11.21	5.45	61.05	4.000	No	Yes	2.00
891	58.50	24.42	2.88	2.05	0.97	10.86	5.47	59.40	4.000	No	Yes	2.00
892	58.55	23.79	2.88	2.00	0.97	10.51	5.53	58.05	4.000	No	Yes	2.00
893	58.61	23.23	2.89	1.95	0.98	10.19	5.58	56.92	4.000	No	Yes	2.00
894	58.70	22.64	2.90	1.93	0.98	9.86	5.67	55.93	4.000	No	Yes	2.00
895	58.75	22.12	2.91	1.93	0.98	9.56	5.79	55.31	4.000	No	Yes	2.00
896	58.81	21.76	2.92	1.94	0.99	9.34	5.89	55.01	4.000	No	Yes	2.00
897	58.89	21.58	2.93	1.95	0.99	9.22	5.95	54.89	4.000	No	Yes	2.00
898	58.95	21.52	2.93	1.97	0.99	9.18	5.99	54.99	4.000	No	Yes	2.00
899	59.00	21.65	2.93	1.99	0.99	9.23	5.99	55.30	4.000	No	Yes	2.00
900	59.10	21.83	2.93	2.00	0.99	9.32	5.97	55.60	4.000	No	Yes	2.00
901	59.15	22.01	2.92	2.01	0.99	9.40	5.95	55.91	4.000	No	Yes	2.00
902	59.20	22.17	2.92	2.03	0.99	9.48	5.94	56.28	4.000	No	Yes	2.00
903	59.28	22.35	2.92	2.05	0.99	9.57	5.92	56.65	4.000	No	Yes	2.00
904	59.35	22.51	2.93	2.10	0.99	9.62	5.96	57.35	4.000	No	Yes	2.00
905	59.38	22.75	2.93	2.16	0.99	9.74	5.98	58.18	4.000	No	Yes	2.00
906	59.46	23.08	2.92	2.18	0.99	9.90	5.94	58.82	4.000	No	Yes	2.00
907	59.53	23.71	2.91	2.15	0.98	10.25	5.78	59.22	4.000	No	Yes	2.00
908	59.59	24.44	2.88	2.05	0.97	10.68	5.53	59.03	4.000	No	Yes	2.00
909	59.67	25.08	2.86	1.98	0.97	11.05	5.33	58.93	4.000	No	Yes	2.00
910	59.73	25.65	2.84	1.93	0.96	11.38	5.17	58.87	4.000	No	Yes	2.00
911	59.79	26.13	2.83	1.91	0.96	11.64	5.08	59.15	4.000	No	Yes	2.00
912	59.89	26.74	2.82	1.91	0.95	11.97	4.99	59.70	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
913	59.94	27.35	2.82	1.93	0.95	12.30	4.93	60.60	4.000	No	Yes	2.00
914	59.99	28.37	2.81	1.99	0.95	12.84	4.85	62.31	4.000	Yes	Yes	2.00
915	60.07	30.97	2.71	1.61	0.91	14.49	4.10	59.42	4.000	Yes	Yes	2.00
916	60.12	34.29	2.61	1.27	0.87	16.66	3.39	56.43	4.000	Yes	Yes	2.00
917	60.19	40.56	2.46	0.95	0.81	20.76	2.59	53.74	4.000	Yes	No	2.00
918	60.25	48.38	2.31	0.69	0.76	26.09	1.98	51.69	4.000	Yes	No	2.00
919	60.33	55.12	2.19	0.51	0.71	30.89	1.64	50.62	4.000	Yes	No	2.00
920	60.38	61.17	2.08	0.37	0.67	35.45	1.00	35.45	4.000	Yes	No	2.00
921	60.48	67.60	1.96	0.25	0.62	40.50	1.00	40.50	4.000	Yes	No	2.00
922	60.53	77.07	1.81	0.12	0.57	48.20	1.00	48.20	4.000	Yes	No	2.00
923	60.61	80.93	N/A	0.00	1.00	-1.00	1.00	N/A	4.000	No	No	2.00
924	60.63	82.24	N/A	0.00	1.00	-1.00	1.00	N/A	4.000	No	No	2.00

Abbreviations

Depth: Depth from free surface, at which CPT was performed (ft)
q_t: Total cone resistance
I_c: Soil behavior type index
Fr: Normalized friction ratio (%)
n: Stress exponent
Q_{tn}: Normalized cone resistance
K_c: Cone resistance correction factor due to fines
$Q_{tn,cs}$: Normalized and adjusted cone resistance
$CRR_{7.5}$: Cyclic resistance ratio for M_w=7.5
FS: Factor of safety against soil liquefaction

:: Liquefaction Potential Index calculation data ::

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
0.08	2.00	0.00	0.00	0.02	0.00	0.15	2.00	0.00	0.00	0.02	0.00
0.23	2.00	0.00	0.00	0.02	0.00	0.30	2.00	0.00	0.00	0.02	0.00
0.35	2.00	0.00	0.00	0.02	0.00	0.43	2.00	0.00	0.00	0.02	0.00
0.50	2.00	0.00	0.00	0.02	0.00	0.55	2.00	0.00	0.00	0.02	0.00
0.61	2.00	0.00	0.00	0.02	0.00	0.70	2.00	0.00	0.00	0.03	0.00
0.73	2.00	0.00	0.00	0.01	0.00	0.80	2.00	0.00	0.00	0.02	0.00
0.89	2.00	0.00	0.00	0.03	0.00	0.93	2.00	0.00	0.00	0.01	0.00
1.01	2.00	0.00	0.00	0.02	0.00	1.09	2.00	0.00	0.00	0.02	0.00
1.13	2.00	0.00	0.00	0.01	0.00	1.19	2.00	0.00	0.00	0.02	0.00
1.29	2.00	0.00	0.00	0.03	0.00	1.34	2.00	0.00	0.00	0.02	0.00
1.39	2.00	0.00	0.00	0.02	0.00	1.45	2.00	0.00	0.00	0.02	0.00
1.54	2.00	0.00	0.00	0.03	0.00	1.59	2.00	0.00	0.00	0.02	0.00
1.67	2.00	0.00	0.00	0.02	0.00	1.72	2.00	0.00	0.00	0.02	0.00
1.79	2.00	0.00	0.00	0.02	0.00	1.85	2.00	0.00	0.00	0.02	0.00
1.94	2.00	0.00	0.00	0.03	0.00	1.98	2.00	0.00	0.00	0.01	0.00
2.04	2.00	0.00	0.00	0.02	0.00	2.13	2.00	0.00	0.00	0.03	0.00
2.17	2.00	0.00	0.00	0.01	0.00	2.24	2.00	0.00	0.00	0.02	0.00
2.32	2.00	0.00	0.00	0.02	0.00	2.39	2.00	0.00	0.00	0.02	0.00
2.43	2.00	0.00	0.00	0.01	0.00	2.52	2.00	0.00	0.00	0.03	0.00
2.58	2.00	0.00	0.00	0.02	0.00	2.63	2.00	0.00	0.00	0.02	0.00
2.72	2.00	0.00	0.00	0.03	0.00	2.78	2.00	0.00	0.00	0.02	0.00
2.83	2.00	0.00	0.00	0.02	0.00	2.89	2.00	0.00	0.00	0.02	0.00
2.98	2.00	0.00	0.00	0.03	0.00	3.03	2.00	0.00	0.00	0.02	0.00
3.09	2.00	0.00	0.00	0.02	0.00	3.18	2.00	0.00	0.00	0.03	0.00
3.22	2.00	0.00	0.00	0.01	0.00	3.32	2.00	0.00	0.00	0.03	0.00
3.37	2.00	0.00	0.00	0.02	0.00	3.42	2.00	0.00	0.00	0.02	0.00
3.52	2.00	0.00	0.00	0.03	0.00	3.57	2.00	0.00	0.00	0.02	0.00
3.61	2.00	0.00	0.00	0.01	0.00	3.68	2.00	0.00	0.00	0.02	0.00
3.77	2.00	0.00	0.00	0.03	0.00	3.83	2.00	0.00	0.00	0.02	0.00
3.91	2.00	0.00	0.00	0.02	0.00	3.95	2.00	0.00	0.00	0.01	0.00
4.02	2.00	0.00	0.00	0.02	0.00	4.12	2.00	0.00	0.00	0.03	0.00
4.14	2.00	0.00	0.00	0.01	0.00	4.22	2.00	0.00	0.00	0.02	0.00
4.27	2.00	0.00	0.00	0.02	0.00	4.37	2.00	0.00	0.00	0.03	0.00
4.42	2.00	0.00	0.00	0.02	0.00	4.46	2.00	0.00	0.00	0.01	0.00
4.57	2.00	0.00	0.00	0.03	0.00	4.61	2.00	0.00	0.00	0.01	0.00
4.67	2.00	0.00	0.00	0.02	0.00	4.76	2.00	0.00	0.00	0.03	0.00
4.81	2.00	0.00	0.00	0.02	0.00	4.90	2.00	0.00	0.00	0.03	0.00
4.96	2.00	0.00	0.00	0.02	0.00	5.00	2.00	0.00	0.00	0.01	0.00
5.05	2.00	0.00	0.00	0.02	0.00	5.14	2.00	0.00	0.00	0.03	0.00
5.20	2.00	0.00	0.00	0.02	0.00	5.30	2.00	0.00	0.00	0.03	0.00
5.35	2.00	0.00	0.00	0.02	0.00	5.39	2.00	0.00	0.00	0.01	0.00
5.48	2.00	0.00	0.00	0.03	0.00	5.55	2.00	0.00	0.00	0.02	0.00
5.59	2.00	0.00	0.00	0.01	0.00	5.64	2.00	0.00	0.00	0.02	0.00
5.74	2.00	0.00	0.00	0.03	0.00	5.79	2.00	0.00	0.00	0.02	0.00
5.84	2.00	0.00	0.00	0.02	0.00	5.94	2.00	0.00	0.00	0.03	0.00
5.97	2.00	0.00	0.00	0.01	0.00	6.05	2.00	0.00	0.00	0.02	0.00
6.14	2.00	0.00	0.00	0.03	0.00	6.19	2.00	0.00	0.00	0.02	0.00
6.24	2.00	0.00	0.00	0.02	0.00	6.33	2.00	0.00	0.00	0.03	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
6.38	2.00	0.00	0.00	0.02	0.00	6.44	2.00	0.00	0.00	0.02	0.00
6.52	2.00	0.00	0.00	0.02	0.00	6.59	2.00	0.00	0.00	0.02	0.00
6.64	2.00	0.00	0.00	0.02	0.00	6.70	2.00	0.00	0.00	0.02	0.00
6.78	2.00	0.00	0.00	0.02	0.00	6.83	2.00	0.00	0.00	0.02	0.00
6.89	2.00	0.00	0.00	0.02	0.00	6.98	2.00	0.00	0.00	0.03	0.00
7.03	2.00	0.00	0.00	0.02	0.00	7.09	2.00	0.00	0.00	0.02	0.00
7.18	2.00	0.00	0.00	0.03	0.00	7.23	2.00	0.00	0.00	0.02	0.00
7.29	2.00	0.00	0.00	0.02	0.00	7.38	2.00	0.00	0.00	0.03	0.00
7.42	2.00	0.00	0.00	0.01	0.00	7.48	2.00	0.00	0.00	0.02	0.00
7.58	2.00	0.00	0.00	0.03	0.00	7.62	2.00	0.00	0.00	0.01	0.00
7.68	2.00	0.00	0.00	0.02	0.00	7.78	2.00	0.00	0.00	0.03	0.00
7.81	2.00	0.00	0.00	0.01	0.00	7.88	2.00	0.00	0.00	0.02	0.00
7.97	2.00	0.00	0.00	0.03	0.00	8.01	2.00	0.00	0.00	0.01	0.00
8.11	2.00	0.00	0.00	0.03	0.00	8.14	2.00	0.00	0.00	0.01	0.00
8.22	2.00	0.00	0.00	0.02	0.00	8.31	2.00	0.00	0.00	0.03	0.00
8.35	2.00	0.00	0.00	0.01	0.00	8.41	2.00	0.00	0.00	0.02	0.00
8.50	2.00	0.00	0.00	0.03	0.00	8.56	2.00	0.00	0.00	0.02	0.00
8.61	2.00	0.00	0.00	0.02	0.00	8.68	2.00	0.00	0.00	0.02	0.00
8.75	2.00	0.00	0.00	0.02	0.00	8.80	2.00	0.00	0.00	0.02	0.00
8.89	2.00	0.00	0.00	0.03	0.00	8.94	2.00	0.00	0.00	0.02	0.00
9.00	2.00	0.00	0.00	0.02	0.00	9.08	2.00	0.00	0.00	0.02	0.00
9.15	2.00	0.00	0.00	0.02	0.00	9.20	2.00	0.00	0.00	0.02	0.00
9.28	2.00	0.00	0.00	0.02	0.00	9.35	2.00	0.00	0.00	0.02	0.00
9.40	2.00	0.00	0.00	0.02	0.00	9.45	2.00	0.00	0.00	0.02	0.00
9.55	2.00	0.00	0.00	0.03	0.00	9.59	2.00	0.00	0.00	0.01	0.00
9.69	2.00	0.00	0.00	0.03	0.00	9.74	2.00	0.00	0.00	0.02	0.00
9.79	2.00	0.00	0.00	0.02	0.00	9.84	2.00	0.00	0.00	0.02	0.00
9.94	2.00	0.00	0.00	0.03	0.00	10.00	2.00	0.00	0.00	0.02	0.00
10.09	2.00	0.00	0.00	0.03	0.00	10.13	2.00	0.00	0.00	0.01	0.00
10.18	2.00	0.00	0.00	0.02	0.00	10.24	2.00	0.00	0.00	0.02	0.00
10.33	2.00	0.00	0.00	0.03	0.00	10.37	2.00	0.00	0.00	0.01	0.00
10.43	2.00	0.00	0.00	0.02	0.00	10.52	2.00	0.00	0.00	0.03	0.00
10.59	2.00	0.00	0.00	0.02	0.00	10.64	2.00	0.00	0.00	0.02	0.00
10.70	2.00	0.00	0.00	0.02	0.00	10.78	2.00	0.00	0.00	0.02	0.00
10.83	2.00	0.00	0.00	0.02	0.00	10.94	2.00	0.00	0.00	0.03	0.00
10.99	2.00	0.00	0.00	0.02	0.00	11.03	2.00	0.00	0.00	0.01	0.00
11.09	2.00	0.00	0.00	0.02	0.00	11.17	2.00	0.00	0.00	0.02	0.00
11.24	2.00	0.00	0.00	0.02	0.00	11.33	2.00	0.00	0.00	0.03	0.00
11.37	2.00	0.00	0.00	0.01	0.00	11.44	2.00	0.00	0.00	0.02	0.00
11.52	2.00	0.00	0.00	0.02	0.00	11.57	2.00	0.00	0.00	0.02	0.00
11.63	2.00	0.00	0.00	0.02	0.00	11.72	2.00	0.00	0.00	0.03	0.00
11.76	2.00	0.00	0.00	0.01	0.00	11.83	2.00	0.00	0.00	0.02	0.00
11.92	2.00	0.00	0.00	0.03	0.00	11.94	2.00	0.00	0.00	0.01	0.00
12.02	2.00	0.00	0.00	0.02	0.00	12.11	2.00	0.00	0.00	0.03	0.00
12.16	2.00	0.00	0.00	0.02	0.00	12.22	2.00	0.00	0.00	0.02	0.00
12.31	2.00	0.00	0.00	0.03	0.00	12.36	2.00	0.00	0.00	0.02	0.00
12.42	2.00	0.00	0.00	0.02	0.00	12.50	2.00	0.00	0.00	0.02	0.00
12.56	2.00	0.00	0.00	0.02	0.00	12.62	2.00	0.00	0.00	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
12.70	2.00	0.00	0.00	0.02	0.00	12.77	2.00	0.00	0.00	0.02	0.00
12.81	2.00	0.00	0.00	0.01	0.00	12.91	2.00	0.00	0.00	0.03	0.00
12.96	2.00	0.00	0.00	0.02	0.00	13.01	2.00	0.00	0.00	0.02	0.00
13.06	2.00	0.00	0.00	0.02	0.00	13.16	2.00	0.00	0.00	0.03	0.00
13.21	2.00	0.00	0.00	0.02	0.00	13.26	2.00	0.00	0.00	0.02	0.00
13.36	2.00	0.00	0.00	0.03	0.00	13.40	2.00	0.00	0.00	0.01	0.00
13.46	2.00	0.00	0.00	0.02	0.00	13.55	2.00	0.00	0.00	0.03	0.00
13.60	2.00	0.00	0.00	0.02	0.00	13.67	2.00	0.00	0.00	0.02	0.00
13.75	2.00	0.00	0.00	0.02	0.00	13.80	2.00	0.00	0.00	0.02	0.00
13.86	2.00	0.00	0.00	0.02	0.00	13.95	2.00	0.00	0.00	0.03	0.00
13.99	2.00	0.00	0.00	0.01	0.00	14.06	2.00	0.00	0.00	0.02	0.00
14.15	2.00	0.00	0.00	0.03	0.00	14.19	2.00	0.00	0.00	0.01	0.00
14.26	2.00	0.00	0.00	0.02	0.00	14.35	2.00	0.00	0.00	0.03	0.00
14.40	2.00	0.00	0.00	0.02	0.00	14.45	2.00	0.00	0.00	0.02	0.00
14.55	2.00	0.00	0.00	0.03	0.00	14.58	2.00	0.00	0.00	0.01	0.00
14.65	2.00	0.00	0.00	0.02	0.00	14.74	2.00	0.00	0.00	0.03	0.00
14.77	2.00	0.00	0.00	0.01	0.00	14.84	2.00	0.00	0.00	0.02	0.00
14.94	2.00	0.00	0.00	0.03	0.00	15.00	2.00	0.00	0.00	0.02	0.00
15.03	2.00	0.00	0.00	0.01	0.00	15.11	2.00	0.00	0.00	0.02	0.00
15.19	2.00	0.00	0.00	0.02	0.00	15.24	2.00	0.00	0.00	0.02	0.00
15.29	2.00	0.00	0.00	0.02	0.00	15.39	2.00	0.00	0.00	0.03	0.00
15.42	2.00	0.00	0.00	0.01	0.00	15.49	2.00	0.00	0.00	0.02	0.00
15.59	2.00	0.00	0.00	0.03	0.00	15.63	2.00	0.00	0.00	0.01	0.00
15.69	2.00	0.00	0.00	0.02	0.00	15.78	2.00	0.00	0.00	0.03	0.00
15.84	2.00	0.00	0.00	0.02	0.00	15.89	2.00	0.00	0.00	0.02	0.00
15.95	2.00	0.00	0.00	0.02	0.00	16.04	2.00	0.00	0.00	0.03	0.00
16.08	2.00	0.00	0.00	0.01	0.00	16.18	2.00	0.00	0.00	0.03	0.00
16.24	2.00	0.00	0.00	0.02	0.00	16.28	2.00	0.00	0.00	0.01	0.00
16.36	2.00	0.00	0.00	0.02	0.00	16.43	2.00	0.00	0.00	0.02	0.00
16.47	2.00	0.00	0.00	0.01	0.00	16.54	2.00	0.00	0.00	0.02	0.00
16.63	2.00	0.00	0.00	0.03	0.00	16.68	2.00	0.00	0.00	0.02	0.00
16.78	2.00	0.00	0.00	0.03	0.00	16.83	2.00	0.00	0.00	0.02	0.00
16.87	2.00	0.00	0.00	0.01	0.00	16.93	2.00	0.00	0.00	0.02	0.00
17.01	2.00	0.00	0.00	0.02	0.00	17.09	2.00	0.00	0.00	0.02	0.00
17.15	2.00	0.00	0.00	0.02	0.00	17.20	2.00	0.00	0.00	0.02	0.00
17.27	2.00	0.00	0.00	0.02	0.00	17.35	2.00	0.00	0.00	0.02	0.00
17.40	2.00	0.00	0.00	0.02	0.00	17.45	2.00	0.00	0.00	0.02	0.00
17.55	2.00	0.00	0.00	0.03	0.00	17.59	2.00	0.00	0.00	0.01	0.00
17.65	2.00	0.00	0.00	0.02	0.00	17.75	2.00	0.00	0.00	0.03	0.00
17.79	2.00	0.00	0.00	0.01	0.00	17.87	2.00	0.00	0.00	0.02	0.00
17.94	2.00	0.00	0.00	0.02	0.00	17.98	2.00	0.00	0.00	0.01	0.00
18.05	2.00	0.00	0.00	0.02	0.00	18.14	2.00	0.00	0.00	0.03	0.00
18.18	2.00	0.00	0.00	0.01	0.00	18.24	2.00	0.00	0.00	0.02	0.00
18.34	2.00	0.00	0.00	0.03	0.00	18.39	2.00	0.00	0.00	0.02	0.00
18.44	2.00	0.00	0.00	0.02	0.00	18.54	2.00	0.00	0.00	0.03	0.00
18.59	2.00	0.00	0.00	0.02	0.00	18.64	2.00	0.00	0.00	0.02	0.00
18.74	2.00	0.00	0.00	0.03	0.00	18.79	2.00	0.00	0.00	0.02	0.00
18.84	2.00	0.00	0.00	0.02	0.00	18.92	2.00	0.00	0.00	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
18.97	2.00	0.00	0.00	0.02	0.00	19.04	2.00	0.00	0.00	0.02	0.00
19.14	2.00	0.00	0.00	0.03	0.00	19.17	2.00	0.00	0.00	0.01	0.00
19.24	2.00	0.00	0.00	0.02	0.00	19.34	2.00	0.00	0.00	0.03	0.00
19.39	2.00	0.00	0.00	0.02	0.00	19.43	2.00	0.00	0.00	0.01	0.00
19.52	2.00	0.00	0.00	0.03	0.00	19.56	2.00	0.00	0.00	0.01	0.00
19.63	2.00	0.00	0.00	0.02	0.00	19.73	2.00	0.00	0.00	0.03	0.00
19.78	2.00	0.00	0.00	0.02	0.00	19.83	2.00	0.00	0.00	0.02	0.00
19.90	2.00	0.00	0.00	0.02	0.00	19.96	2.00	0.00	0.00	0.02	0.00
20.03	2.00	0.00	0.00	0.02	0.00	20.09	2.00	0.00	0.00	0.02	0.00
20.16	2.00	0.00	0.00	0.02	0.00	20.23	2.00	0.00	0.00	0.02	0.00
20.31	2.00	0.00	0.00	0.02	0.00	20.35	2.00	0.00	0.00	0.01	0.00
20.42	2.00	0.00	0.00	0.02	0.00	20.50	2.00	0.00	0.00	0.02	0.00
20.55	2.00	0.00	0.00	0.02	0.00	20.62	2.00	0.00	0.00	0.02	0.00
20.70	2.00	0.00	0.00	0.02	0.00	20.75	2.00	0.00	0.00	0.02	0.00
20.82	2.00	0.00	0.00	0.02	0.00	20.90	2.00	0.00	0.00	0.02	0.00
20.96	2.00	0.00	0.00	0.02	0.00	21.01	2.00	0.00	0.00	0.02	0.00
21.11	2.00	0.00	0.00	0.03	0.00	21.15	2.00	0.00	0.00	0.01	0.00
21.21	2.00	0.00	0.00	0.02	0.00	21.27	2.00	0.00	0.00	0.02	0.00
21.36	2.00	0.00	0.00	0.03	0.00	21.40	2.00	0.00	0.00	0.01	0.00
21.51	2.00	0.00	0.00	0.03	0.00	21.55	2.00	0.00	0.00	0.01	0.00
21.60	2.00	0.00	0.00	0.02	0.00	21.69	2.00	0.00	0.00	0.03	0.00
21.75	2.00	0.00	0.00	0.02	0.00	21.80	2.00	0.00	0.00	0.02	0.00
21.90	0.46	0.00	0.00	0.03	0.11	21.95	0.47	0.00	0.00	0.02	0.05
22.00	0.48	0.00	0.00	0.02	0.05	22.09	0.48	0.00	0.00	0.03	0.09
22.11	2.00	0.00	0.00	0.01	0.00	22.19	2.00	0.00	0.00	0.02	0.00
22.26	2.00	0.00	0.00	0.02	0.00	22.35	2.00	0.00	0.00	0.03	0.00
22.39	2.00	0.00	0.00	0.01	0.00	22.44	2.00	0.00	0.00	0.02	0.00
22.55	2.00	0.00	0.00	0.03	0.00	22.58	2.00	0.00	0.00	0.01	0.00
22.65	2.00	0.00	0.00	0.02	0.00	22.74	2.00	0.00	0.00	0.03	0.00
22.83	2.00	0.00	0.00	0.03	0.00	22.85	2.00	0.00	0.00	0.01	0.00
22.94	2.00	0.00	0.00	0.03	0.00	23.00	2.00	0.00	0.00	0.02	0.00
23.05	2.00	0.00	0.00	0.02	0.00	23.10	2.00	0.00	0.00	0.02	0.00
23.18	2.00	0.00	0.00	0.02	0.00	23.25	2.00	0.00	0.00	0.02	0.00
23.30	2.00	0.00	0.00	0.02	0.00	23.38	2.00	0.00	0.00	0.02	0.00
23.45	2.00	0.00	0.00	0.02	0.00	23.50	2.00	0.00	0.00	0.02	0.00
23.60	2.00	0.00	0.00	0.03	0.00	23.65	2.00	0.00	0.00	0.02	0.00
23.70	2.00	0.00	0.00	0.02	0.00	23.76	2.00	0.00	0.00	0.02	0.00
23.84	2.00	0.00	0.00	0.02	0.00	23.89	2.00	0.00	0.00	0.02	0.00
23.99	2.00	0.00	0.00	0.03	0.00	24.03	2.00	0.00	0.00	0.01	0.00
24.09	2.00	0.00	0.00	0.02	0.00	24.19	2.00	0.00	0.00	0.03	0.00
24.24	2.00	0.00	0.00	0.02	0.00	24.30	2.00	0.00	0.00	0.02	0.00
24.34	2.00	0.00	0.00	0.01	0.00	24.44	2.00	0.00	0.00	0.03	0.00
24.50	2.00	0.00	0.00	0.02	0.00	24.58	2.00	0.00	0.00	0.02	0.00
24.65	2.00	0.00	0.00	0.02	0.00	24.69	2.00	0.00	0.00	0.01	0.00
24.74	2.00	0.00	0.00	0.02	0.00	24.84	2.00	0.00	0.00	0.03	0.00
24.89	2.00	0.00	0.00	0.02	0.00	24.95	2.00	0.00	0.00	0.02	0.00
25.04	2.00	0.00	0.00	0.03	0.00	25.08	2.00	0.00	0.00	0.01	0.00
25.19	2.00	0.00	0.00	0.03	0.00	25.24	2.00	0.00	0.00	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
25.28	2.00	0.00	0.00	0.01	0.00	25.35	2.00	0.00	0.00	0.02	0.00
25.43	2.00	0.00	0.00	0.02	0.00	25.48	2.00	0.00	0.00	0.02	0.00
25.53	2.00	0.00	0.00	0.02	0.00	25.63	2.00	0.00	0.00	0.03	0.00
25.68	2.00	0.00	0.00	0.02	0.00	25.74	2.00	0.00	0.00	0.02	0.00
25.79	2.00	0.00	0.00	0.02	0.00	25.88	2.00	0.00	0.00	0.03	0.00
25.92	2.00	0.00	0.00	0.01	0.00	25.99	2.00	0.00	0.00	0.02	0.00
26.05	2.00	0.00	0.00	0.02	0.00	26.13	2.00	0.00	0.00	0.02	0.00
26.20	2.00	0.00	0.00	0.02	0.00	26.26	2.00	0.00	0.00	0.02	0.00
26.31	2.00	0.00	0.00	0.02	0.00	26.40	2.00	0.00	0.00	0.03	0.00
26.45	2.00	0.00	0.00	0.02	0.00	26.54	2.00	0.00	0.00	0.03	0.00
26.59	2.00	0.00	0.00	0.02	0.00	26.65	2.00	0.00	0.00	0.02	0.00
26.74	2.00	0.00	0.00	0.03	0.00	26.78	2.00	0.00	0.00	0.01	0.00
26.84	2.00	0.00	0.00	0.02	0.00	26.94	2.00	0.00	0.00	0.03	0.00
26.99	2.00	0.00	0.00	0.02	0.00	27.04	2.00	0.00	0.00	0.02	0.00
27.13	2.00	0.00	0.00	0.03	0.00	27.18	2.00	0.00	0.00	0.02	0.00
27.24	2.00	0.00	0.00	0.02	0.00	27.34	2.00	0.00	0.00	0.03	0.00
27.40	2.00	0.00	0.00	0.02	0.00	27.44	2.00	0.00	0.00	0.01	0.00
27.53	2.00	0.00	0.00	0.03	0.00	27.57	2.00	0.00	0.00	0.01	0.00
27.64	2.00	0.00	0.00	0.02	0.00	27.72	2.00	0.00	0.00	0.02	0.00
27.79	2.00	0.00	0.00	0.02	0.00	27.83	2.00	0.00	0.00	0.01	0.00
27.90	2.00	0.00	0.00	0.02	0.00	27.98	2.00	0.00	0.00	0.02	0.00
28.03	2.00	0.00	0.00	0.02	0.00	28.09	2.00	0.00	0.00	0.02	0.00
28.18	2.00	0.00	0.00	0.03	0.00	28.22	2.00	0.00	0.00	0.01	0.00
28.28	2.00	0.00	0.00	0.02	0.00	28.38	2.00	0.00	0.00	0.03	0.00
28.43	2.00	0.00	0.00	0.02	0.00	28.48	2.00	0.00	0.00	0.02	0.00
28.58	2.00	0.00	0.00	0.03	0.00	28.62	2.00	0.00	0.00	0.01	0.00
28.69	2.00	0.00	0.00	0.02	0.00	28.77	2.00	0.00	0.00	0.02	0.00
28.82	2.00	0.00	0.00	0.02	0.00	28.88	2.00	0.00	0.00	0.02	0.00
28.97	2.00	0.00	0.00	0.03	0.00	29.01	2.00	0.00	0.00	0.01	0.00
29.07	2.00	0.00	0.00	0.02	0.00	29.15	2.00	0.00	0.00	0.02	0.00
29.21	2.00	0.00	0.00	0.02	0.00	29.30	2.00	0.00	0.00	0.03	0.00
29.33	2.00	0.00	0.00	0.01	0.00	29.41	2.00	0.00	0.00	0.02	0.00
29.50	2.00	0.00	0.00	0.03	0.00	29.53	2.00	0.00	0.00	0.01	0.00
29.61	2.00	0.00	0.00	0.02	0.00	29.70	2.00	0.00	0.00	0.03	0.00
29.74	2.00	0.00	0.00	0.01	0.00	29.80	2.00	0.00	0.00	0.02	0.00
29.90	2.00	0.00	0.00	0.03	0.00	29.93	2.00	0.00	0.00	0.01	0.00
30.00	2.00	0.00	0.00	0.02	0.00	30.09	2.00	0.00	0.00	0.03	0.00
30.15	2.00	0.00	0.00	0.02	0.00	30.19	2.00	0.00	0.00	0.01	0.00
30.30	2.00	0.00	0.00	0.03	0.00	30.33	2.00	0.00	0.00	0.01	0.00
30.40	2.00	0.00	0.00	0.02	0.00	30.49	2.00	0.00	0.00	0.03	0.00
30.54	2.00	0.00	0.00	0.02	0.00	30.59	2.00	0.00	0.00	0.02	0.00
30.64	2.00	0.00	0.00	0.02	0.00	30.72	2.00	0.00	0.00	0.02	0.00
30.80	2.00	0.00	0.00	0.02	0.00	30.88	2.00	0.00	0.00	0.02	0.00
30.93	2.00	0.00	0.00	0.02	0.00	31.00	2.00	0.00	0.00	0.02	0.00
31.04	2.00	0.00	0.00	0.01	0.00	31.13	2.00	0.00	0.00	0.03	0.00
31.20	2.00	0.00	0.00	0.02	0.00	31.29	2.00	0.00	0.00	0.03	0.00
31.34	2.00	0.00	0.00	0.02	0.00	31.38	2.00	0.00	0.00	0.01	0.00
31.43	2.00	0.00	0.00	0.02	0.00	31.51	2.00	0.00	0.00	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
31.58	2.00	0.00	0.00	0.02	0.00	31.63	2.00	0.00	0.00	0.02	0.00
31.71	2.00	0.00	0.00	0.02	0.00	31.78	2.00	0.00	0.00	0.02	0.00
31.83	2.00	0.00	0.00	0.02	0.00	31.90	2.00	0.00	0.00	0.02	0.00
31.98	2.00	0.00	0.00	0.02	0.00	32.03	2.00	0.00	0.00	0.02	0.00
32.09	2.00	0.00	0.00	0.02	0.00	32.16	2.00	0.00	0.00	0.02	0.00
32.22	2.00	0.00	0.00	0.02	0.00	32.30	2.00	0.00	0.00	0.02	0.00
32.38	2.00	0.00	0.00	0.02	0.00	32.42	2.00	0.00	0.00	0.01	0.00
32.50	2.00	0.00	0.00	0.02	0.00	32.56	2.00	0.00	0.00	0.02	0.00
32.62	2.00	0.00	0.00	0.02	0.00	32.72	2.00	0.00	0.00	0.03	0.00
32.77	2.00	0.00	0.00	0.02	0.00	32.82	2.00	0.00	0.00	0.02	0.00
32.91	2.00	0.00	0.00	0.03	0.00	32.97	2.00	0.00	0.00	0.02	0.00
33.02	2.00	0.00	0.00	0.02	0.00	33.11	2.00	0.00	0.00	0.03	0.00
33.16	2.00	0.00	0.00	0.02	0.00	33.22	2.00	0.00	0.00	0.02	0.00
33.29	2.00	0.00	0.00	0.02	0.00	33.37	2.00	0.00	0.00	0.02	0.00
33.41	2.00	0.00	0.00	0.01	0.00	33.47	2.00	0.00	0.00	0.02	0.00
33.57	2.00	0.00	0.00	0.03	0.00	33.60	2.00	0.00	0.00	0.01	0.00
33.67	2.00	0.00	0.00	0.02	0.00	33.76	2.00	0.00	0.00	0.03	0.00
33.80	2.00	0.00	0.00	0.01	0.00	33.86	2.00	0.00	0.00	0.02	0.00
33.96	2.00	0.00	0.00	0.03	0.00	34.00	2.00	0.00	0.00	0.01	0.00
34.06	2.00	0.00	0.00	0.02	0.00	34.16	2.00	0.00	0.00	0.03	0.00
34.20	2.00	0.00	0.00	0.01	0.00	34.26	2.00	0.00	0.00	0.02	0.00
34.36	2.00	0.00	0.00	0.03	0.00	34.39	2.00	0.00	0.00	0.01	0.00
34.46	2.00	0.00	0.00	0.02	0.00	34.56	2.00	0.00	0.00	0.03	0.00
34.60	2.00	0.00	0.00	0.01	0.00	34.65	2.00	0.00	0.00	0.02	0.00
34.75	2.00	0.00	0.00	0.03	0.00	34.80	2.00	0.00	0.00	0.02	0.00
34.86	2.00	0.00	0.00	0.02	0.00	34.95	2.00	0.00	0.00	0.03	0.00
34.99	2.00	0.00	0.00	0.01	0.00	35.06	2.00	0.00	0.00	0.02	0.00
35.11	2.00	0.00	0.00	0.02	0.00	35.19	2.00	0.00	0.00	0.02	0.00
35.25	2.00	0.00	0.00	0.02	0.00	35.31	2.00	0.00	0.00	0.02	0.00
35.39	2.00	0.00	0.00	0.02	0.00	35.49	2.00	0.00	0.00	0.03	0.00
35.53	2.00	0.00	0.00	0.01	0.00	35.60	2.00	0.00	0.00	0.02	0.00
35.63	2.00	0.00	0.00	0.01	0.00	35.70	2.00	0.00	0.00	0.02	0.00
35.78	2.00	0.00	0.00	0.02	0.00	35.84	2.00	0.00	0.00	0.02	0.00
35.90	2.00	0.00	0.00	0.02	0.00	35.98	2.00	0.00	0.00	0.02	0.00
36.06	2.00	0.00	0.00	0.02	0.00	36.09	2.00	0.00	0.00	0.01	0.00
36.18	2.00	0.00	0.00	0.03	0.00	36.23	2.00	0.00	0.00	0.02	0.00
36.29	2.00	0.00	0.00	0.02	0.00	36.38	2.00	0.00	0.00	0.03	0.00
36.42	2.00	0.00	0.00	0.01	0.00	36.49	2.00	0.00	0.00	0.02	0.00
36.58	2.00	0.00	0.00	0.03	0.00	36.62	2.00	0.00	0.00	0.01	0.00
36.68	2.00	0.00	0.00	0.02	0.00	36.77	2.00	0.00	0.00	0.03	0.00
36.83	2.00	0.00	0.00	0.02	0.00	36.88	2.00	0.00	0.00	0.02	0.00
36.97	2.00	0.00	0.00	0.03	0.00	37.02	2.00	0.00	0.00	0.02	0.00
37.08	2.00	0.00	0.00	0.02	0.00	37.17	0.96	0.00	0.00	0.03	0.01
37.22	1.04	0.00	0.00	0.02	0.00	37.27	1.10	0.00	0.00	0.02	0.00
37.37	1.14	0.00	0.00	0.03	0.00	37.41	1.18	0.00	0.00	0.01	0.00
37.47	1.20	0.00	0.00	0.02	0.00	37.57	1.21	0.00	0.00	0.03	0.00
37.61	1.20	0.00	0.00	0.01	0.00	37.67	1.20	0.00	0.00	0.02	0.00
37.76	1.20	0.00	0.00	0.03	0.00	37.81	1.19	0.00	0.00	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
37.87	1.21	0.00	0.00	0.02	0.00	37.97	1.24	0.00	0.00	0.03	0.00
38.02	1.29	0.00	0.00	0.02	0.00	38.07	1.36	0.00	0.00	0.02	0.00
38.17	1.45	0.00	0.00	0.03	0.00	38.20	1.58	0.00	0.00	0.01	0.00
38.27	1.73	0.00	0.00	0.02	0.00	38.33	1.90	0.00	0.00	0.02	0.00
38.42	2.00	0.00	0.00	0.03	0.00	38.46	2.00	0.00	0.00	0.01	0.00
38.53	2.00	0.00	0.00	0.02	0.00	38.62	2.00	0.00	0.00	0.03	0.00
38.66	2.00	0.00	0.00	0.01	0.00	38.73	2.00	0.00	0.00	0.02	0.00
38.81	2.00	0.00	0.00	0.02	0.00	38.86	2.00	0.00	0.00	0.02	0.00
38.93	2.00	0.00	0.00	0.02	0.00	39.02	2.00	0.00	0.00	0.03	0.00
39.05	2.00	0.00	0.00	0.01	0.00	39.12	2.00	0.00	0.00	0.02	0.00
39.18	2.00	0.00	0.00	0.02	0.00	39.27	2.00	0.00	0.00	0.03	0.00
39.31	2.00	0.00	0.00	0.01	0.00	39.37	2.00	0.00	0.00	0.02	0.00
39.44	2.00	0.00	0.00	0.02	0.00	39.50	2.00	0.00	0.00	0.02	0.00
39.59	2.00	0.00	0.00	0.03	0.00	39.65	2.00	0.00	0.00	0.02	0.00
39.71	1.96	0.00	0.00	0.02	0.00	39.77	1.83	0.00	0.00	0.02	0.00
39.84	1.69	0.00	0.00	0.02	0.00	39.91	1.53	0.00	0.00	0.02	0.00
39.97	1.40	0.00	0.00	0.02	0.00	40.03	1.26	0.00	0.00	0.02	0.00
40.11	1.13	0.00	0.00	0.02	0.00	40.17	1.02	0.00	0.00	0.02	0.00
40.26	0.92	0.00	0.00	0.03	0.01	40.30	0.86	0.00	0.00	0.01	0.01
40.36	0.82	0.00	0.00	0.02	0.01	40.45	0.81	0.00	0.00	0.03	0.02
40.49	0.80	0.00	0.00	0.01	0.01	40.57	0.78	0.00	0.00	0.02	0.02
40.62	0.77	0.00	0.00	0.02	0.01	40.70	0.76	0.00	0.00	0.02	0.02
40.76	0.75	0.00	0.00	0.02	0.02	40.86	0.74	0.00	0.00	0.03	0.03
40.89	0.73	0.00	0.00	0.01	0.01	40.95	0.72	0.00	0.00	0.02	0.02
41.03	0.72	0.00	0.00	0.02	0.03	41.11	0.72	0.00	0.00	0.02	0.03
41.16	0.74	0.00	0.00	0.02	0.01	41.23	0.76	0.00	0.00	0.02	0.02
41.29	0.78	0.00	0.00	0.02	0.01	41.35	0.80	0.00	0.00	0.02	0.01
41.41	0.81	0.00	0.00	0.02	0.01	41.49	0.83	0.00	0.00	0.02	0.02
41.56	0.85	0.00	0.00	0.02	0.01	41.64	0.88	0.00	0.00	0.02	0.01
41.69	0.91	0.00	0.00	0.02	0.00	41.73	0.94	0.00	0.00	0.01	0.00
41.84	0.97	0.00	0.00	0.03	0.00	41.89	1.00	0.00	0.00	0.02	0.00
41.98	1.04	0.00	0.00	0.03	0.00	42.04	1.07	0.00	0.00	0.02	0.00
42.09	1.09	0.00	0.00	0.02	0.00	42.16	1.08	0.00	0.00	0.02	0.00
42.24	1.06	0.00	0.00	0.02	0.00	42.28	1.03	0.00	0.00	0.01	0.00
42.33	1.00	0.00	0.00	0.02	0.00	42.39	0.96	0.00	0.00	0.02	0.00
42.47	0.93	0.00	0.00	0.02	0.01	42.53	0.90	0.00	0.00	0.02	0.01
42.59	0.89	0.00	0.00	0.02	0.01	42.66	0.88	0.00	0.00	0.02	0.01
42.73	2.00	0.00	0.00	0.02	0.00	42.83	2.00	0.00	0.00	0.03	0.00
42.88	2.00	0.00	0.00	0.02	0.00	42.93	2.00	0.00	0.00	0.02	0.00
42.99	2.00	0.00	0.00	0.02	0.00	43.07	2.00	0.00	0.00	0.02	0.00
43.14	2.00	0.00	0.00	0.02	0.00	43.19	2.00	0.00	0.00	0.02	0.00
43.25	2.00	0.00	0.00	0.02	0.00	43.34	2.00	0.00	0.00	0.03	0.00
43.39	2.00	0.00	0.00	0.02	0.00	43.45	0.99	0.00	0.00	0.02	0.00
43.54	0.90	0.00	0.00	0.03	0.01	43.59	0.80	0.00	0.00	0.02	0.01
43.64	2.00	0.00	0.00	0.02	0.00	43.74	2.00	0.00	0.00	0.03	0.00
43.78	2.00	0.00	0.00	0.01	0.00	43.83	2.00	0.00	0.00	0.02	0.00
43.94	2.00	0.00	0.00	0.03	0.00	43.98	2.00	0.00	0.00	0.01	0.00
44.04	2.00	0.00	0.00	0.02	0.00	44.14	2.00	0.00	0.00	0.03	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
44.17	2.00	0.00	0.00	0.01	0.00	44.23	2.00	0.00	0.00	0.02	0.00
44.33	2.00	0.00	0.00	0.03	0.00	44.37	2.00	0.00	0.00	0.01	0.00
44.44	2.00	0.00	0.00	0.02	0.00	44.53	2.00	0.00	0.00	0.03	0.00
44.58	2.00	0.00	0.00	0.02	0.00	44.64	2.00	0.00	0.00	0.02	0.00
44.73	2.00	0.00	0.00	0.03	0.00	44.78	2.00	0.00	0.00	0.02	0.00
44.82	2.00	0.00	0.00	0.01	0.00	44.90	2.00	0.00	0.00	0.02	0.00
44.97	2.00	0.00	0.00	0.02	0.00	45.03	2.00	0.00	0.00	0.02	0.00
45.09	2.00	0.00	0.00	0.02	0.00	45.17	2.00	0.00	0.00	0.02	0.00
45.22	2.00	0.00	0.00	0.02	0.00	45.29	2.00	0.00	0.00	0.02	0.00
45.38	2.00	0.00	0.00	0.03	0.00	45.42	2.00	0.00	0.00	0.01	0.00
45.50	2.00	0.00	0.00	0.02	0.00	45.57	0.73	0.00	0.00	0.02	0.02
45.62	0.72	0.00	0.00	0.02	0.01	45.69	0.72	0.00	0.00	0.02	0.02
45.77	0.71	0.00	0.00	0.02	0.02	45.82	0.70	0.00	0.00	0.02	0.01
45.88	0.68	0.00	0.00	0.02	0.02	45.97	0.67	0.00	0.00	0.03	0.03
46.02	2.00	0.00	0.00	0.02	0.00	46.10	2.00	0.00	0.00	0.02	0.00
46.17	2.00	0.00	0.00	0.02	0.00	46.21	2.00	0.00	0.00	0.01	0.00
46.27	2.00	0.00	0.00	0.02	0.00	46.36	2.00	0.00	0.00	0.03	0.00
46.42	2.00	0.00	0.00	0.02	0.00	46.46	2.00	0.00	0.00	0.01	0.00
46.56	2.00	0.00	0.00	0.03	0.00	46.61	2.00	0.00	0.00	0.02	0.00
46.66	2.00	0.00	0.00	0.02	0.00	46.74	2.00	0.00	0.00	0.02	0.00
46.81	2.00	0.00	0.00	0.02	0.00	46.87	2.00	0.00	0.00	0.02	0.00
46.94	2.00	0.00	0.00	0.02	0.00	47.01	2.00	0.00	0.00	0.02	0.00
47.06	2.00	0.00	0.00	0.02	0.00	47.12	2.00	0.00	0.00	0.02	0.00
47.19	2.00	0.00	0.00	0.02	0.00	47.25	2.00	0.00	0.00	0.02	0.00
47.34	2.00	0.00	0.00	0.03	0.00	47.39	2.00	0.00	0.00	0.02	0.00
47.44	2.00	0.00	0.00	0.02	0.00	47.54	2.00	0.00	0.00	0.03	0.00
47.59	2.00	0.00	0.00	0.02	0.00	47.65	2.00	0.00	0.00	0.02	0.00
47.74	2.00	0.00	0.00	0.03	0.00	47.81	2.00	0.00	0.00	0.02	0.00
47.85	2.00	0.00	0.00	0.01	0.00	47.94	2.00	0.00	0.00	0.03	0.00
47.98	2.00	0.00	0.00	0.01	0.00	48.04	2.00	0.00	0.00	0.02	0.00
48.13	2.00	0.00	0.00	0.03	0.00	48.17	2.00	0.00	0.00	0.01	0.00
48.24	2.00	0.00	0.00	0.02	0.00	48.32	2.00	0.00	0.00	0.02	0.00
48.37	2.00	0.00	0.00	0.02	0.00	48.44	2.00	0.00	0.00	0.02	0.00
48.53	2.00	0.00	0.00	0.03	0.00	48.56	2.00	0.00	0.00	0.01	0.00
48.64	2.00	0.00	0.00	0.02	0.00	48.72	2.00	0.00	0.00	0.02	0.00
48.78	2.00	0.00	0.00	0.02	0.00	48.83	2.00	0.00	0.00	0.02	0.00
48.90	2.00	0.00	0.00	0.02	0.00	48.97	2.00	0.00	0.00	0.02	0.00
49.03	2.00	0.00	0.00	0.02	0.00	49.12	0.88	0.00	0.00	0.03	0.01
49.16	0.93	0.00	0.00	0.01	0.00	49.23	0.97	0.00	0.00	0.02	0.00
49.31	1.02	0.00	0.00	0.02	0.00	49.36	1.06	0.00	0.00	0.02	0.00
49.43	1.10	0.00	0.00	0.02	0.00	49.52	1.14	0.00	0.00	0.03	0.00
49.58	1.17	0.00	0.00	0.02	0.00	49.62	1.20	0.00	0.00	0.01	0.00
49.71	1.19	0.00	0.00	0.03	0.00	49.78	1.16	0.00	0.00	0.02	0.00
49.81	1.14	0.00	0.00	0.01	0.00	49.88	1.13	0.00	0.00	0.02	0.00
49.97	1.11	0.00	0.00	0.03	0.00	50.00	1.08	0.00	0.00	0.01	0.00
50.07	2.00	0.00	0.00	0.02	0.00	50.14	2.00	0.00	0.00	0.02	0.00
50.22	2.00	0.00	0.00	0.02	0.00	50.27	2.00	0.00	0.00	0.02	0.00
50.35	2.00	0.00	0.00	0.02	0.00	50.40	2.00	0.00	0.00	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
50.47	2.00	0.00	0.00	0.02	0.00	50.55	2.00	0.00	0.00	0.02	0.00
50.59	2.00	0.00	0.00	0.01	0.00	50.66	2.00	0.00	0.00	0.02	0.00
50.75	2.00	0.00	0.00	0.03	0.00	50.79	2.00	0.00	0.00	0.01	0.00
50.86	2.00	0.00	0.00	0.02	0.00	50.94	2.00	0.00	0.00	0.02	0.00
50.99	2.00	0.00	0.00	0.02	0.00	51.05	2.00	0.00	0.00	0.02	0.00
51.14	2.00	0.00	0.00	0.03	0.00	51.18	2.00	0.00	0.00	0.01	0.00
51.25	2.00	0.00	0.00	0.02	0.00	51.34	2.00	0.00	0.00	0.03	0.00
51.41	2.00	0.00	0.00	0.02	0.00	51.44	2.00	0.00	0.00	0.01	0.00
51.52	2.00	0.00	0.00	0.02	0.00	51.67	2.00	0.00	0.00	0.05	0.00
51.70	2.00	0.00	0.00	0.01	0.00	51.75	2.00	0.00	0.00	0.02	0.00
51.78	2.00	0.00	0.00	0.01	0.00	51.88	2.00	0.00	0.00	0.03	0.00
51.92	2.00	0.00	0.00	0.01	0.00	51.99	2.00	0.00	0.00	0.02	0.00
52.04	2.00	0.00	0.00	0.02	0.00	52.14	2.00	0.00	0.00	0.03	0.00
52.19	2.00	0.00	0.00	0.02	0.00	52.26	2.00	0.00	0.00	0.02	0.00
52.33	2.00	0.00	0.00	0.02	0.00	52.38	2.00	0.00	0.00	0.02	0.00
52.43	2.00	0.00	0.00	0.02	0.00	52.51	2.00	0.00	0.00	0.02	0.00
52.58	2.00	0.00	0.00	0.02	0.00	52.63	2.00	0.00	0.00	0.02	0.00
52.69	2.00	0.00	0.00	0.02	0.00	52.77	2.00	0.00	0.00	0.02	0.00
52.83	2.00	0.00	0.00	0.02	0.00	52.90	2.00	0.00	0.00	0.02	0.00
52.99	2.00	0.00	0.00	0.03	0.00	53.05	2.00	0.00	0.00	0.02	0.00
53.10	2.00	0.00	0.00	0.02	0.00	53.16	2.00	0.00	0.00	0.02	0.00
53.25	2.00	0.00	0.00	0.03	0.00	53.29	2.00	0.00	0.00	0.01	0.00
53.38	2.00	0.00	0.00	0.03	0.00	53.44	2.00	0.00	0.00	0.02	0.00
53.50	2.00	0.00	0.00	0.02	0.00	53.55	2.00	0.00	0.00	0.02	0.00
53.64	2.00	0.00	0.00	0.03	0.00	53.72	2.00	0.00	0.00	0.02	0.00
53.74	2.00	0.00	0.00	0.01	0.00	53.82	2.00	0.00	0.00	0.02	0.00
53.90	2.00	0.00	0.00	0.02	0.00	53.94	2.00	0.00	0.00	0.01	0.00
54.01	2.00	0.00	0.00	0.02	0.00	54.09	2.00	0.00	0.00	0.02	0.00
54.19	2.00	0.00	0.00	0.03	0.00	54.24	2.00	0.00	0.00	0.02	0.00
54.29	2.00	0.00	0.00	0.02	0.00	54.35	2.00	0.00	0.00	0.02	0.00
54.44	2.00	0.00	0.00	0.03	0.00	54.49	2.00	0.00	0.00	0.02	0.00
54.53	2.00	0.00	0.00	0.01	0.00	54.63	2.00	0.00	0.00	0.03	0.00
54.68	2.00	0.00	0.00	0.02	0.00	54.74	2.00	0.00	0.00	0.02	0.00
54.83	2.00	0.00	0.00	0.03	0.00	54.88	2.00	0.00	0.00	0.02	0.00
54.94	2.00	0.00	0.00	0.02	0.00	55.03	2.00	0.00	0.00	0.03	0.00
55.07	2.00	0.00	0.00	0.01	0.00	55.13	2.00	0.00	0.00	0.02	0.00
55.23	2.00	0.00	0.00	0.03	0.00	55.28	2.00	0.00	0.00	0.02	0.00
55.32	2.00	0.00	0.00	0.01	0.00	55.42	2.00	0.00	0.00	0.03	0.00
55.50	2.00	0.00	0.00	0.02	0.00	55.53	2.00	0.00	0.00	0.01	0.00
55.58	2.00	0.00	0.00	0.02	0.00	55.66	2.00	0.00	0.00	0.02	0.00
55.73	2.00	0.00	0.00	0.02	0.00	55.78	2.00	0.00	0.00	0.02	0.00
55.86	2.00	0.00	0.00	0.02	0.00	55.93	2.00	0.00	0.00	0.02	0.00
55.97	2.00	0.00	0.00	0.01	0.00	56.08	2.00	0.00	0.00	0.03	0.00
56.12	2.00	0.00	0.00	0.01	0.00	56.17	2.00	0.00	0.00	0.02	0.00
56.28	2.00	0.00	0.00	0.03	0.00	56.32	2.00	0.00	0.00	0.01	0.00
56.37	2.00	0.00	0.00	0.02	0.00	56.47	2.00	0.00	0.00	0.03	0.00
56.52	2.00	0.00	0.00	0.02	0.00	56.57	2.00	0.00	0.00	0.02	0.00
56.67	2.00	0.00	0.00	0.03	0.00	56.72	2.00	0.00	0.00	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
56.78	2.00	0.00	0.00	0.02	0.00	56.87	2.00	0.00	0.00	0.03	0.00
56.91	2.00	0.00	0.00	0.01	0.00	56.97	2.00	0.00	0.00	0.02	0.00
57.03	2.00	0.00	0.00	0.02	0.00	57.11	2.00	0.00	0.00	0.02	0.00
57.17	2.00	0.00	0.00	0.02	0.00	57.26	2.00	0.00	0.00	0.03	0.00
57.32	2.00	0.00	0.00	0.02	0.00	57.35	2.00	0.00	0.00	0.01	0.00
57.42	2.00	0.00	0.00	0.02	0.00	57.51	2.00	0.00	0.00	0.03	0.00
57.55	2.00	0.00	0.00	0.01	0.00	57.62	2.00	0.00	0.00	0.02	0.00
57.71	2.00	0.00	0.00	0.03	0.00	57.78	2.00	0.00	0.00	0.02	0.00
57.82	2.00	0.00	0.00	0.01	0.00	57.90	2.00	0.00	0.00	0.02	0.00
57.96	2.00	0.00	0.00	0.02	0.00	58.01	2.00	0.00	0.00	0.02	0.00
58.11	2.00	0.00	0.00	0.03	0.00	58.15	2.00	0.00	0.00	0.01	0.00
58.21	2.00	0.00	0.00	0.02	0.00	58.31	2.00	0.00	0.00	0.03	0.00
58.35	2.00	0.00	0.00	0.01	0.00	58.42	2.00	0.00	0.00	0.02	0.00
58.50	2.00	0.00	0.00	0.02	0.00	58.55	2.00	0.00	0.00	0.02	0.00
58.61	2.00	0.00	0.00	0.02	0.00	58.70	2.00	0.00	0.00	0.03	0.00
58.75	2.00	0.00	0.00	0.02	0.00	58.81	2.00	0.00	0.00	0.02	0.00
58.89	2.00	0.00	0.00	0.02	0.00	58.95	2.00	0.00	0.00	0.02	0.00
59.00	2.00	0.00	0.00	0.02	0.00	59.10	2.00	0.00	0.00	0.03	0.00
59.15	2.00	0.00	0.00	0.02	0.00	59.20	2.00	0.00	0.00	0.02	0.00
59.28	2.00	0.00	0.00	0.02	0.00	59.35	2.00	0.00	0.00	0.02	0.00
59.38	2.00	0.00	0.00	0.01	0.00	59.46	2.00	0.00	0.00	0.02	0.00
59.53	2.00	0.00	0.00	0.02	0.00	59.59	2.00	0.00	0.00	0.02	0.00
59.67	2.00	0.00	0.00	0.02	0.00	59.73	2.00	0.00	0.00	0.02	0.00
59.79	2.00	0.00	0.00	0.02	0.00	59.89	2.00	0.00	0.00	0.03	0.00
59.94	2.00	0.00	0.00	0.02	0.00	59.99	2.00	0.00	0.00	0.02	0.00
60.07	2.00	0.00	0.00	0.02	0.00	60.12	2.00	0.00	0.00	0.02	0.00
60.19	2.00	0.00	0.00	0.02	0.00	60.25	2.00	0.00	0.00	0.02	0.00
60.33	2.00	0.00	0.00	0.02	0.00	60.38	2.00	0.00	0.00	0.02	0.00
60.48	2.00	0.00	0.00	0.03	0.00	60.53	2.00	0.00	0.00	0.02	0.00
60.61	2.00	0.00	0.00	0.02	0.00	60.63	2.00	0.00	0.00	0.01	0.00

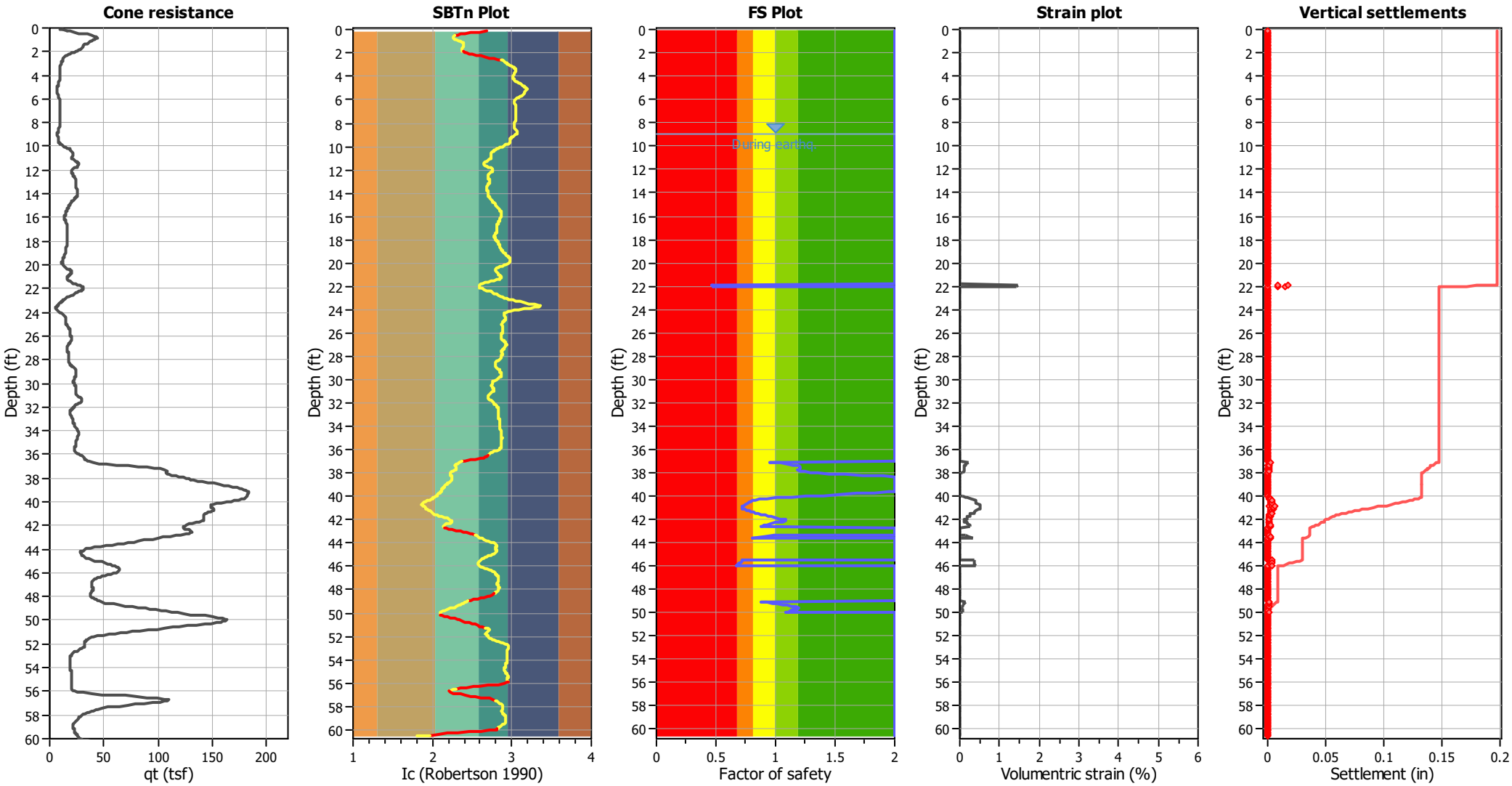
Overall liquefaction potential: 0.87

LPI = 0.00 - Liquefaction risk very low
LPI between 0.00 and 5.00 - Liquefaction risk low
LPI between 5.00 and 15.00 - Liquefaction risk high
LPI > 15.00 - Liquefaction risk very high

Abbreviations

FS: Calculated factor of safety for test point
F_L: 1 - FS
w_z: Function value of the extend of soil liquefaction according to depth
d_z: Layer thickness (ft)
LPI: Liquefaction potential index value for test point

Estimation of post-earthquake settlements



Abbreviations

q_t:	Total cone resistance (cone resistance q_c corrected for pore water effects)
I_c:	Soil Behaviour Type Index
FS:	Calculated Factor of Safety against liquefaction
Volumentric strain:	Post-liquefaction volumentric strain

:: Lateral displacement index calculation ::

Depth (ft)	q_t (tsf)	Q_{tn}	R_f (%)	$Q_{tn,cs}$	FS	D_r	$Gamma_{max}$ (%)	Lat. disp. (in)
9.00	7.30	10.92	3.73	78.50	2.00	0.00	0.00	0.00
9.08	7.36	11.01	3.55	77.13	2.00	0.00	0.00	0.00
9.15	7.44	11.14	3.39	76.02	2.00	0.00	0.00	0.00
9.20	7.49	11.22	3.26	75.01	2.00	0.00	0.00	0.00
9.28	7.51	11.24	3.17	74.14	2.00	0.00	0.00	0.00
9.35	7.52	11.25	3.12	73.70	2.00	0.00	0.00	0.00
9.40	7.54	11.28	3.11	73.70	2.00	0.00	0.00	0.00
9.45	7.59	11.36	3.13	74.13	2.00	0.00	0.00	0.00
9.55	7.66	11.46	3.20	75.15	2.00	0.00	0.00	0.00
9.59	7.88	11.81	3.31	77.12	2.00	0.00	0.00	0.00
9.69	8.26	12.41	3.51	80.66	2.00	0.00	0.00	0.00
9.74	8.85	13.35	3.69	84.90	2.00	0.53	0.00	0.00
9.79	9.71	14.73	3.95	91.03	2.00	3.78	0.00	0.00
9.84	10.70	16.32	4.17	97.37	2.00	7.17	0.00	0.00
9.94	11.82	18.10	4.38	103.99	2.00	10.59	0.00	0.00
10.00	13.13	20.20	4.53	110.57	2.00	14.21	0.00	0.00
10.09	14.51	22.41	4.66	117.08	2.00	17.64	0.00	0.00
10.13	15.87	24.60	4.75	123.02	2.00	20.71	0.00	0.00
10.18	17.10	26.57	4.85	128.46	2.00	23.26	0.00	0.00
10.24	18.19	28.31	4.93	133.07	2.00	25.34	0.00	0.00
10.33	19.08	29.73	5.01	137.04	2.00	26.97	0.00	0.00
10.37	19.75	30.80	4.97	138.53	2.00	28.13	0.00	0.00
10.43	20.34	31.75	4.92	139.54	2.00	29.14	0.00	0.00
10.52	20.84	32.54	4.85	140.02	2.00	29.95	0.00	0.00
10.59	21.08	32.92	4.81	140.09	2.00	30.33	0.00	0.00
10.64	21.13	32.99	4.78	139.63	2.00	30.40	0.00	0.00
10.70	20.97	32.65	4.77	139.01	2.00	30.06	0.00	0.00
10.78	20.88	32.28	4.74	137.82	2.00	29.68	0.00	0.00
10.83	20.80	32.00	4.69	136.50	2.00	29.39	0.00	0.00
10.94	20.72	31.57	4.64	134.99	2.00	28.94	0.00	0.00
10.99	20.74	31.46	4.64	134.82	2.00	28.83	0.00	0.00
11.03	21.20	31.99	4.56	134.49	2.00	29.38	0.00	0.00
11.09	21.83	32.70	4.46	134.07	2.00	30.10	0.00	0.00
11.17	22.79	33.81	4.34	133.84	2.00	31.21	0.00	0.00
11.24	23.92	35.18	4.23	134.18	2.00	32.52	0.00	0.00
11.33	25.05	36.47	4.14	134.60	2.00	33.71	0.00	0.00
11.37	25.77	37.35	4.15	136.05	2.00	34.50	0.00	0.00
11.44	26.22	37.80	4.18	137.34	2.00	34.89	0.00	0.00
11.52	26.58	38.07	4.22	138.41	2.00	35.12	0.00	0.00
11.57	26.65	38.03	4.27	139.31	2.00	35.09	0.00	0.00
11.63	26.16	37.23	4.37	139.89	2.00	34.39	0.00	0.00
11.72	25.38	35.96	4.51	140.36	2.00	33.24	0.00	0.00
11.76	24.28	34.38	4.65	139.96	2.00	31.76	0.00	0.00
11.83	23.04	32.52	4.73	138.03	2.00	29.92	0.00	0.00
11.92	21.96	30.82	4.75	135.33	2.00	28.16	0.00	0.00
11.94	21.21	29.72	4.67	132.01	2.00	26.95	0.00	0.00
12.02	20.75	28.89	4.53	128.38	2.00	26.01	0.00	0.00
12.11	20.42	28.28	4.37	124.87	2.00	25.32	0.00	0.00

:: Estimation of post-earthquake lateral Displacements :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	R_f (%)	$Q_{tn,cs}$	FS	D_r	$Gamma_{max}$ (%)	Lat. disp. (in)
12.16	20.40	28.14	4.17	121.60	2.00	25.15	0.00	0.00
12.22	20.54	28.21	4.00	119.09	2.00	25.23	0.00	0.00
12.31	20.81	28.44	3.85	117.01	2.00	25.50	0.00	0.00
12.36	21.16	28.83	3.79	116.71	2.00	25.95	0.00	0.00
12.42	21.60	29.35	3.81	117.81	2.00	26.54	0.00	0.00
12.50	22.12	29.98	3.85	119.47	2.00	27.24	0.00	0.00
12.56	22.63	30.60	3.91	121.49	2.00	27.92	0.00	0.00
12.62	23.07	31.16	4.01	124.10	2.00	28.52	0.00	0.00
12.70	23.50	31.67	4.12	126.72	2.00	29.05	0.00	0.00
12.77	23.80	32.03	4.25	129.56	2.00	29.42	0.00	0.00
12.81	23.99	32.28	4.38	132.01	2.00	29.68	0.00	0.00
12.91	24.10	32.33	4.46	133.52	2.00	29.73	0.00	0.00
12.96	24.23	32.45	4.49	134.17	2.00	29.85	0.00	0.00
13.01	24.25	32.42	4.50	134.28	2.00	29.82	0.00	0.00
13.06	24.27	32.37	4.45	133.47	2.00	29.77	0.00	0.00
13.16	24.35	32.33	4.38	132.12	2.00	29.73	0.00	0.00
13.21	24.41	32.31	4.26	130.18	2.00	29.71	0.00	0.00
13.26	24.42	32.22	4.13	127.80	2.00	29.62	0.00	0.00
13.36	24.44	32.08	3.98	125.14	2.00	29.47	0.00	0.00
13.40	24.45	32.02	3.91	123.86	2.00	29.42	0.00	0.00
13.46	24.56	32.08	3.88	123.35	2.00	29.48	0.00	0.00
13.55	24.66	32.11	3.87	123.20	2.00	29.50	0.00	0.00
13.60	24.84	32.28	3.87	123.53	2.00	29.68	0.00	0.00
13.67	24.92	32.33	3.94	124.78	2.00	29.73	0.00	0.00
13.75	24.93	32.28	4.03	126.36	2.00	29.68	0.00	0.00
13.80	25.07	32.43	4.11	127.94	2.00	29.83	0.00	0.00
13.86	25.25	32.61	4.19	129.61	2.00	30.01	0.00	0.00
13.95	25.36	32.67	4.28	131.18	2.00	30.08	0.00	0.00
13.99	25.41	32.69	4.29	131.45	2.00	30.10	0.00	0.00
14.06	25.37	32.55	4.27	130.82	2.00	29.96	0.00	0.00
14.15	25.16	32.18	4.24	129.77	2.00	29.57	0.00	0.00
14.19	24.83	31.70	4.21	128.37	2.00	29.09	0.00	0.00
14.26	24.43	31.11	4.15	126.50	2.00	28.46	0.00	0.00
14.35	24.01	30.46	4.10	124.52	2.00	27.76	0.00	0.00
14.40	23.37	29.60	4.06	122.43	2.00	26.81	0.00	0.00
14.45	22.69	28.67	4.01	120.19	2.00	25.77	0.00	0.00
14.55	22.01	27.72	3.97	117.90	2.00	24.65	0.00	0.00
14.58	21.36	26.87	3.92	115.74	2.00	23.62	0.00	0.00
14.65	20.73	26.00	3.90	113.97	2.00	22.54	0.00	0.00
14.74	20.12	25.16	3.89	112.38	2.00	21.46	0.00	0.00
14.77	19.60	24.48	3.88	111.04	2.00	20.55	0.00	0.00
14.84	19.12	23.82	3.87	109.67	2.00	19.65	0.00	0.00
14.94	18.65	23.15	3.84	108.06	2.00	18.71	0.00	0.00
15.00	18.25	22.61	3.83	106.87	2.00	17.93	0.00	0.00
15.03	17.87	22.10	3.83	105.97	2.00	17.18	0.00	0.00
15.11	17.43	21.50	3.82	104.76	2.00	16.27	0.00	0.00
15.19	17.06	20.99	3.83	103.84	2.00	15.47	0.00	0.00
15.24	16.70	20.50	3.82	102.77	2.00	14.69	0.00	0.00

:: Estimation of post-earthquake lateral Displacements :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	R_f (%)	$Q_{tn,cs}$	FS	D_r	$Gamma_{max}$ (%)	Lat. disp. (in)
15.29	16.35	20.02	3.79	101.39	2.00	13.92	0.00	0.00
15.39	15.99	19.51	3.75	99.95	2.00	13.06	0.00	0.00
15.42	15.64	19.05	3.71	98.56	2.00	12.28	0.00	0.00
15.49	15.29	18.56	3.67	97.01	2.00	11.41	0.00	0.00
15.59	14.91	18.03	3.62	95.32	2.00	10.45	0.00	0.00
15.63	14.59	17.60	3.56	93.63	2.00	9.66	0.00	0.00
15.69	14.34	17.24	3.50	92.15	2.00	8.97	0.00	0.00
15.78	14.10	16.88	3.42	90.51	2.00	8.29	0.00	0.00
15.84	13.90	16.60	3.35	89.04	2.00	7.72	0.00	0.00
15.89	13.80	16.44	3.29	87.93	2.00	7.40	0.00	0.00
15.95	13.74	16.32	3.23	87.08	2.00	7.18	0.00	0.00
16.04	13.72	16.25	3.21	86.58	2.00	7.02	0.00	0.00
16.08	13.81	16.34	3.20	86.70	2.00	7.20	0.00	0.00
16.18	13.99	16.50	3.20	87.01	2.00	7.53	0.00	0.00
16.24	14.14	16.65	3.23	87.68	2.00	7.83	0.00	0.00
16.28	14.42	16.97	3.24	88.39	2.00	8.45	0.00	0.00
16.36	14.72	17.29	3.25	89.23	2.00	9.07	0.00	0.00
16.43	15.02	17.62	3.28	90.16	2.00	9.70	0.00	0.00
16.47	15.27	17.90	3.32	91.24	2.00	10.23	0.00	0.00
16.54	15.56	18.21	3.32	91.86	2.00	10.78	0.00	0.00
16.63	15.86	18.51	3.29	92.06	2.00	11.32	0.00	0.00
16.68	16.03	18.68	3.25	91.80	2.00	11.62	0.00	0.00
16.78	16.10	18.69	3.20	91.18	2.00	11.63	0.00	0.00
16.83	16.13	18.68	3.15	90.44	2.00	11.63	0.00	0.00
16.87	16.04	18.55	3.12	89.77	2.00	11.39	0.00	0.00
16.93	15.94	18.39	3.07	88.90	2.00	11.11	0.00	0.00
17.01	15.83	18.21	3.02	87.90	2.00	10.79	0.00	0.00
17.09	15.76	18.07	2.97	86.88	2.00	10.54	0.00	0.00
17.15	15.65	17.90	2.93	86.10	2.00	10.21	0.00	0.00
17.20	15.51	17.70	2.92	85.64	2.00	9.85	0.00	0.00
17.27	15.51	17.67	2.91	85.37	2.00	9.79	0.00	0.00
17.35	15.60	17.73	2.89	85.24	2.00	9.90	0.00	0.00
17.40	15.80	17.93	2.85	85.08	2.00	10.27	0.00	0.00
17.45	15.97	18.09	2.82	84.93	2.00	10.57	0.00	0.00
17.55	16.10	18.19	2.81	84.87	2.00	10.74	0.00	0.00
17.59	16.19	18.27	2.80	84.88	2.00	10.89	0.00	0.00
17.65	16.20	18.24	2.79	84.72	2.00	10.85	0.00	0.00
17.75	16.19	18.18	2.79	84.55	2.00	10.72	0.00	0.00
17.79	16.19	18.15	2.77	84.31	2.00	10.68	0.00	0.00
17.87	16.11	18.02	2.78	84.19	2.00	10.43	0.00	0.00
17.94	16.00	17.86	2.80	84.20	2.00	10.14	0.00	0.00
17.98	15.82	17.64	2.84	84.47	2.00	9.73	0.00	0.00
18.05	15.69	17.45	2.89	84.79	2.00	9.37	0.00	0.00
18.14	15.56	17.26	2.94	85.08	2.00	9.01	0.00	0.00
18.18	15.48	17.15	2.97	85.39	2.00	8.80	0.00	0.00
18.24	15.47	17.11	3.01	85.83	2.00	8.73	0.00	0.00
18.34	15.47	17.07	3.05	86.33	2.00	8.64	0.00	0.00
18.39	15.46	17.03	3.10	86.87	2.00	8.58	0.00	0.00

:: Estimation of post-earthquake lateral Displacements :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	R_f (%)	$Q_{tn,cs}$	FS	D_r	$Gamma_{max}$ (%)	Lat. disp. (in)
18.44	15.44	16.99	3.13	87.21	2.00	8.50	0.00	0.00
18.54	15.40	16.90	3.17	87.53	2.00	8.31	0.00	0.00
18.59	15.35	16.82	3.20	87.79	2.00	8.16	0.00	0.00
18.64	15.27	16.71	3.22	87.88	2.00	7.94	0.00	0.00
18.74	15.17	16.55	3.25	87.93	2.00	7.62	0.00	0.00
18.79	15.04	16.38	3.29	88.05	2.00	7.28	0.00	0.00
18.84	14.91	16.20	3.31	87.97	2.00	6.92	0.00	0.00
18.92	14.77	16.00	3.33	87.78	2.00	6.52	0.00	0.00
18.97	14.58	15.76	3.35	87.54	2.00	6.02	0.00	0.00
19.04	14.35	15.47	3.36	87.11	2.00	5.41	0.00	0.00
19.14	14.06	15.10	3.37	86.48	2.00	4.61	0.00	0.00
19.17	13.75	14.73	3.38	85.74	2.00	3.78	0.00	0.00
19.24	13.40	14.31	3.38	84.86	2.00	2.82	0.00	0.00
19.34	13.05	13.87	3.39	83.94	2.00	1.79	0.00	0.00
19.39	12.70	13.45	3.36	82.65	2.00	0.79	0.00	0.00
19.43	12.35	13.03	3.32	81.26	2.00	0.00	0.00	0.00
19.52	12.01	12.60	3.29	79.86	2.00	0.00	0.00	0.00
19.56	11.73	12.27	3.25	78.68	2.00	0.00	0.00	0.00
19.63	11.53	12.01	3.20	77.54	2.00	0.00	0.00	0.00
19.73	11.42	11.85	3.15	76.65	2.00	0.00	0.00	0.00
19.78	11.34	11.73	3.10	75.80	2.00	0.00	0.00	0.00
19.83	11.31	11.68	3.08	75.46	2.00	0.00	0.00	0.00
19.90	11.46	11.82	3.05	75.59	2.00	0.00	0.00	0.00
19.96	11.82	12.21	3.08	76.82	2.00	0.00	0.00	0.00
20.03	12.32	12.76	3.16	78.97	2.00	0.00	0.00	0.00
20.09	13.07	13.56	3.20	81.14	2.00	1.05	0.00	0.00
20.16	14.08	14.65	3.19	83.40	2.00	3.60	0.00	0.00
20.23	15.17	15.83	3.25	86.60	2.00	6.15	0.00	0.00
20.31	16.28	17.00	3.31	89.70	2.00	8.52	0.00	0.00
20.35	17.41	18.23	3.36	92.74	2.00	10.82	0.00	0.00
20.42	18.42	19.29	3.37	94.85	2.00	12.68	0.00	0.00
20.50	19.26	20.16	3.36	96.30	2.00	14.14	0.00	0.00
20.55	19.56	20.45	3.40	97.31	2.00	14.62	0.00	0.00
20.62	19.65	20.52	3.39	97.27	2.00	14.72	0.00	0.00
20.70	19.50	20.30	3.38	96.78	2.00	14.38	0.00	0.00
20.75	19.06	19.79	3.38	95.83	2.00	13.53	0.00	0.00
20.82	18.40	19.04	3.33	93.87	2.00	12.25	0.00	0.00
20.90	17.71	18.24	3.27	91.54	2.00	10.85	0.00	0.00
20.96	17.00	17.44	3.20	89.17	2.00	9.35	0.00	0.00
21.01	16.41	16.77	3.17	87.47	2.00	8.07	0.00	0.00
21.11	15.83	16.10	3.20	86.58	2.00	6.71	0.00	0.00
21.15	15.60	15.83	3.19	85.93	2.00	6.16	0.00	0.00
21.21	15.85	16.08	3.17	86.21	2.00	6.67	0.00	0.00
21.27	16.33	16.56	3.16	87.01	2.00	7.65	0.00	0.00
21.36	16.99	17.22	3.16	88.21	2.00	8.93	0.00	0.00
21.40	18.20	18.49	3.11	89.82	2.00	11.28	0.00	0.00
21.51	19.79	20.11	3.03	91.52	2.00	14.05	0.00	0.00
21.55	21.52	21.91	2.97	93.52	2.00	16.89	0.00	0.00

:: Estimation of post-earthquake lateral Displacements :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	R_f (%)	$Q_{tn,cs}$	FS	D_r	$Gamma_{max}$ (%)	Lat. disp. (in)
21.60	23.59	24.06	2.90	95.55	2.00	19.98	0.00	0.00
21.69	25.70	26.20	2.81	96.90	2.00	22.79	0.00	0.00
21.75	27.76	28.31	2.72	98.12	2.00	25.35	0.00	0.00
21.80	29.14	29.71	2.68	99.15	2.00	26.94	0.00	0.00
21.90	30.20	30.73	2.67	100.14	0.46	28.06	51.20	0.74
21.95	30.81	31.32	2.69	101.22	0.47	28.69	51.20	0.37
22.00	30.93	31.42	2.73	102.10	0.48	28.79	51.20	0.37
22.09	30.62	31.03	2.78	102.52	0.48	28.37	51.20	0.66
22.11	30.03	30.40	2.83	102.71	2.00	27.70	0.00	0.00
22.19	28.96	29.24	2.88	102.32	2.00	26.41	0.00	0.00
22.26	27.41	27.58	2.97	101.61	2.00	24.49	0.00	0.00
22.35	25.79	25.84	3.06	100.78	2.00	22.34	0.00	0.00
22.39	24.24	24.21	3.10	99.12	2.00	20.18	0.00	0.00
22.44	22.59	22.47	3.05	95.60	2.00	17.72	0.00	0.00
22.55	21.10	20.85	2.98	92.02	2.00	15.25	0.00	0.00
22.58	19.55	19.22	2.92	88.43	2.00	12.57	0.00	0.00
22.65	18.00	17.58	2.87	85.03	2.00	9.62	0.00	0.00
22.74	16.57	16.05	2.80	81.44	2.00	6.61	0.00	0.00
22.83	15.26	14.66	2.72	77.84	2.00	3.63	0.00	0.00
22.85	14.33	13.68	2.60	74.41	2.00	1.34	0.00	0.00
22.94	13.44	12.73	2.45	70.71	2.00	0.00	0.00	0.00
23.00	12.59	11.82	2.34	67.64	2.00	0.00	0.00	0.00
23.05	11.82	11.01	2.41	66.82	2.00	0.00	0.00	0.00
23.10	11.10	10.25	2.42	65.35	2.00	0.00	0.00	0.00
23.18	10.27	9.36	2.46	63.65	2.00	0.00	0.00	0.00
23.25	9.47	8.51	2.48	61.72	2.00	0.00	0.00	0.00
23.30	8.60	7.59	2.53	59.72	2.00	0.00	0.00	0.00
23.38	7.73	6.67	2.63	57.73	2.00	0.00	0.00	0.00
23.45	6.95	5.85	2.77	55.88	2.00	0.00	0.00	0.00
23.50	6.22	5.07	2.95	54.03	2.00	0.00	0.00	0.00
23.60	5.81	4.64	3.06	52.74	2.00	0.00	0.00	0.00
23.65	5.62	4.43	3.10	52.02	2.00	0.00	0.00	0.00
23.70	5.85	4.66	3.04	52.75	2.00	0.00	0.00	0.00
23.76	6.35	5.18	2.87	53.96	2.00	0.00	0.00	0.00
23.84	6.95	5.78	2.72	55.32	2.00	0.00	0.00	0.00
23.89	7.83	6.67	2.63	57.73	2.00	0.00	0.00	0.00
23.99	8.80	7.65	2.55	60.10	2.00	0.00	0.00	0.00
24.03	9.88	8.75	2.50	62.59	2.00	0.00	0.00	0.00
24.09	11.03	9.91	2.47	65.13	2.00	0.00	0.00	0.00
24.19	12.04	10.91	2.50	67.75	2.00	0.00	0.00	0.00
24.24	13.00	11.87	2.55	70.30	2.00	0.00	0.00	0.00
24.30	13.63	12.48	2.63	72.49	2.00	0.00	0.00	0.00
24.34	14.08	12.93	2.73	74.64	2.00	0.00	0.00	0.00
24.44	14.45	13.27	2.83	76.52	2.00	0.34	0.00	0.00
24.50	14.62	13.42	2.89	77.53	2.00	0.71	0.00	0.00
24.58	14.65	13.42	2.94	78.18	2.00	0.71	0.00	0.00
24.65	14.57	13.32	2.97	78.33	2.00	0.45	0.00	0.00
24.69	14.53	13.26	2.97	78.13	2.00	0.32	0.00	0.00

:: Estimation of post-earthquake lateral Displacements :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	R_f (%)	$Q_{tn,cs}$	FS	D_r	$Gamma_{max}$ (%)	Lat. disp. (in)
24.74	14.55	13.26	2.93	77.73	2.00	0.32	0.00	0.00
24.84	14.55	13.22	2.89	77.12	2.00	0.23	0.00	0.00
24.89	14.64	13.30	2.87	77.06	2.00	0.40	0.00	0.00
24.95	14.90	13.53	2.85	77.31	2.00	0.98	0.00	0.00
25.04	15.26	13.85	2.85	77.95	2.00	1.75	0.00	0.00
25.08	15.75	14.32	2.87	79.10	2.00	2.85	0.00	0.00
25.19	16.34	14.87	2.95	81.25	2.00	4.09	0.00	0.00
25.24	16.95	15.45	3.07	83.94	2.00	5.36	0.00	0.00
25.28	17.47	15.95	3.23	86.89	2.00	6.40	0.00	0.00
25.35	17.89	16.34	3.42	89.97	2.00	7.21	0.00	0.00
25.43	18.28	16.69	3.56	92.42	2.00	7.90	0.00	0.00
25.48	18.60	16.98	3.63	93.96	2.00	8.47	0.00	0.00
25.53	18.87	17.22	3.69	95.14	2.00	8.94	0.00	0.00
25.63	19.11	17.40	3.75	96.33	2.00	9.29	0.00	0.00
25.68	19.22	17.50	3.81	97.23	2.00	9.47	0.00	0.00
25.74	19.27	17.52	3.82	97.37	2.00	9.50	0.00	0.00
25.79	19.09	17.32	3.84	97.23	2.00	9.12	0.00	0.00
25.88	19.09	17.27	3.81	96.79	2.00	9.04	0.00	0.00
25.92	19.22	17.38	3.73	96.00	2.00	9.24	0.00	0.00
25.99	19.41	17.53	3.67	95.66	2.00	9.52	0.00	0.00
26.05	19.60	17.68	3.64	95.60	2.00	9.81	0.00	0.00
26.13	19.72	17.75	3.63	95.56	2.00	9.95	0.00	0.00
26.20	19.75	17.75	3.59	95.05	2.00	9.94	0.00	0.00
26.26	19.73	17.70	3.55	94.50	2.00	9.85	0.00	0.00
26.31	19.63	17.58	3.53	93.99	2.00	9.62	0.00	0.00
26.40	19.66	17.57	3.48	93.32	2.00	9.60	0.00	0.00
26.45	19.42	17.30	3.46	92.49	2.00	9.10	0.00	0.00
26.54	19.03	16.89	3.45	91.59	2.00	8.30	0.00	0.00
26.59	18.55	16.41	3.46	90.67	2.00	7.34	0.00	0.00
26.65	18.00	15.86	3.46	89.59	2.00	6.21	0.00	0.00
26.74	17.48	15.31	3.46	88.46	2.00	5.06	0.00	0.00
26.78	16.97	14.81	3.47	87.42	2.00	3.97	0.00	0.00
26.84	16.52	14.36	3.44	86.03	2.00	2.94	0.00	0.00
26.94	16.15	13.97	3.38	84.56	2.00	2.03	0.00	0.00
26.99	15.95	13.75	3.30	83.16	2.00	1.51	0.00	0.00
27.04	15.92	13.70	3.22	82.10	2.00	1.40	0.00	0.00
27.13	15.95	13.70	3.14	81.22	2.00	1.39	0.00	0.00
27.18	16.05	13.77	3.07	80.52	2.00	1.57	0.00	0.00
27.24	16.28	13.97	3.01	80.26	2.00	2.03	0.00	0.00
27.34	16.55	14.19	2.96	80.12	2.00	2.56	0.00	0.00
27.40	16.87	14.47	2.92	80.24	2.00	3.20	0.00	0.00
27.44	17.16	14.73	2.93	80.86	2.00	3.78	0.00	0.00
27.53	17.39	14.91	2.94	81.30	2.00	4.18	0.00	0.00
27.57	17.54	15.03	2.96	81.78	2.00	4.45	0.00	0.00
27.64	17.59	15.05	2.98	82.11	2.00	4.50	0.00	0.00
27.72	17.57	15.00	2.98	81.98	2.00	4.39	0.00	0.00
27.79	17.52	14.93	2.96	81.63	2.00	4.22	0.00	0.00
27.83	17.42	14.82	2.93	80.99	2.00	3.98	0.00	0.00

:: Estimation of post-earthquake lateral Displacements :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	R_f (%)	$Q_{tn,cs}$	FS	D_r	$Gamma_{max}$ (%)	Lat. disp. (in)
27.90	17.32	14.70	2.88	80.17	2.00	3.71	0.00	0.00
27.98	17.21	14.57	2.82	79.17	2.00	3.42	0.00	0.00
28.03	17.13	14.48	2.76	78.18	2.00	3.21	0.00	0.00
28.09	17.12	14.44	2.70	77.40	2.00	3.14	0.00	0.00
28.18	17.17	14.46	2.64	76.66	2.00	3.17	0.00	0.00
28.22	17.35	14.61	2.58	76.16	2.00	3.51	0.00	0.00
28.28	17.70	14.91	2.56	76.45	2.00	4.19	0.00	0.00
28.38	18.14	15.29	2.55	76.91	2.00	5.01	0.00	0.00
28.43	18.79	15.87	2.57	78.24	2.00	6.24	0.00	0.00
28.48	19.60	16.60	2.58	79.56	2.00	7.73	0.00	0.00
28.58	20.45	17.34	2.63	81.50	2.00	9.16	0.00	0.00
28.62	21.32	18.13	2.76	84.61	2.00	10.63	0.00	0.00
28.69	22.17	18.87	2.91	88.01	2.00	11.96	0.00	0.00
28.77	22.93	19.53	3.07	91.42	2.00	13.09	0.00	0.00
28.82	23.56	20.08	3.24	94.77	2.00	14.00	0.00	0.00
28.88	24.03	20.48	3.41	97.92	2.00	14.66	0.00	0.00
28.97	24.41	20.77	3.58	100.91	2.00	15.13	0.00	0.00
29.01	24.63	20.95	3.72	103.16	2.00	15.40	0.00	0.00
29.07	24.64	20.92	3.89	105.36	2.00	15.36	0.00	0.00
29.15	24.58	20.82	4.01	106.80	2.00	15.20	0.00	0.00
29.21	24.40	20.62	4.06	107.09	2.00	14.88	0.00	0.00
29.30	24.21	20.39	4.08	106.94	2.00	14.52	0.00	0.00
29.33	23.98	20.17	4.09	106.50	2.00	14.16	0.00	0.00
29.41	23.70	19.87	4.05	105.43	2.00	13.66	0.00	0.00
29.50	23.37	19.52	4.00	104.05	2.00	13.08	0.00	0.00
29.53	23.04	19.21	3.92	102.41	2.00	12.56	0.00	0.00
29.61	22.66	18.83	3.84	100.59	2.00	11.90	0.00	0.00
29.70	22.38	18.54	3.73	98.65	2.00	11.38	0.00	0.00
29.74	22.16	18.32	3.61	96.58	2.00	10.99	0.00	0.00
29.80	22.07	18.22	3.45	94.41	2.00	10.80	0.00	0.00
29.90	22.00	18.11	3.30	92.22	2.00	10.61	0.00	0.00
29.93	22.08	18.18	3.16	90.35	2.00	10.72	0.00	0.00
30.00	22.43	18.47	3.01	88.80	2.00	11.25	0.00	0.00
30.09	23.10	19.03	2.83	87.25	2.00	12.24	0.00	0.00
30.15	23.44	19.31	2.73	86.11	2.00	12.73	0.00	0.00
30.19	23.51	19.36	2.68	85.48	2.00	12.80	0.00	0.00
30.30	23.75	19.53	2.63	85.04	2.00	13.09	0.00	0.00
30.33	23.80	19.56	2.65	85.29	2.00	13.14	0.00	0.00
30.40	23.99	19.69	2.67	85.88	2.00	13.36	0.00	0.00
30.49	24.26	19.89	2.68	86.36	2.00	13.69	0.00	0.00
30.54	24.43	20.02	2.70	86.75	2.00	13.91	0.00	0.00
30.59	24.35	19.92	2.72	87.03	2.00	13.75	0.00	0.00
30.64	23.97	19.56	2.78	87.26	2.00	13.14	0.00	0.00
30.72	23.92	19.47	2.81	87.64	2.00	12.99	0.00	0.00
30.80	24.13	19.62	2.80	87.72	2.00	13.25	0.00	0.00
30.88	24.07	19.53	2.85	88.30	2.00	13.09	0.00	0.00
30.93	24.43	19.82	2.88	89.29	2.00	13.58	0.00	0.00
31.00	25.09	20.36	2.91	90.55	2.00	14.48	0.00	0.00

:: Estimation of post-earthquake lateral Displacements :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	R_f (%)	$Q_{tn,cs}$	FS	D_r	$Gamma_{max}$ (%)	Lat. disp. (in)
31.04	25.89	21.05	2.93	91.89	2.00	15.57	0.00	0.00
31.13	26.92	21.91	2.93	93.21	2.00	16.89	0.00	0.00
31.20	27.99	22.82	2.93	94.69	2.00	18.23	0.00	0.00
31.29	28.87	23.54	2.95	96.05	2.00	19.26	0.00	0.00
31.34	29.38	23.95	2.98	97.07	2.00	19.83	0.00	0.00
31.38	29.75	24.26	3.01	98.00	2.00	20.25	0.00	0.00
31.43	29.95	24.40	2.99	98.01	2.00	20.45	0.00	0.00
31.51	29.81	24.24	2.93	96.77	2.00	20.22	0.00	0.00
31.58	29.15	23.63	2.86	94.73	2.00	19.39	0.00	0.00
31.63	28.20	22.78	2.79	92.32	2.00	18.17	0.00	0.00
31.71	26.91	21.61	2.73	89.67	2.00	16.44	0.00	0.00
31.78	25.56	20.41	2.67	86.95	2.00	14.54	0.00	0.00
31.83	24.29	19.28	2.61	84.32	2.00	12.67	0.00	0.00
31.90	23.14	18.26	2.54	81.74	2.00	10.88	0.00	0.00
31.98	22.27	17.48	2.44	79.05	2.00	9.43	0.00	0.00
32.03	21.54	16.84	2.35	76.69	2.00	8.19	0.00	0.00
32.09	20.84	16.21	2.29	74.93	2.00	6.93	0.00	0.00
32.16	20.13	15.57	2.27	73.67	2.00	5.62	0.00	0.00
32.22	19.49	15.00	2.27	72.78	2.00	4.39	0.00	0.00
32.30	19.02	14.56	2.28	72.13	2.00	3.40	0.00	0.00
32.38	18.67	14.24	2.28	71.60	2.00	2.66	0.00	0.00
32.42	18.64	14.20	2.27	71.43	2.00	2.57	0.00	0.00
32.50	18.90	14.39	2.25	71.49	2.00	3.02	0.00	0.00
32.56	19.05	14.50	2.27	71.91	2.00	3.27	0.00	0.00
32.62	19.22	14.62	2.32	72.88	2.00	3.54	0.00	0.00
32.72	19.47	14.80	2.38	74.02	2.00	3.95	0.00	0.00
32.77	19.78	15.05	2.45	75.31	2.00	4.48	0.00	0.00
32.82	20.17	15.35	2.52	76.77	2.00	5.15	0.00	0.00
32.91	20.58	15.66	2.58	78.18	2.00	5.81	0.00	0.00
32.97	20.98	15.98	2.64	79.57	2.00	6.46	0.00	0.00
33.02	21.23	16.16	2.71	80.83	2.00	6.85	0.00	0.00
33.11	21.45	16.32	2.78	82.05	2.00	7.16	0.00	0.00
33.16	21.63	16.44	2.85	83.15	2.00	7.42	0.00	0.00
33.22	21.81	16.57	2.89	83.95	2.00	7.67	0.00	0.00
33.29	21.97	16.67	2.93	84.67	2.00	7.87	0.00	0.00
33.37	22.11	16.76	2.96	85.32	2.00	8.04	0.00	0.00
33.41	22.18	16.79	3.01	86.01	2.00	8.11	0.00	0.00
33.47	22.32	16.88	3.08	87.04	2.00	8.28	0.00	0.00
33.57	22.42	16.92	3.16	88.17	2.00	8.35	0.00	0.00
33.60	22.79	17.21	3.21	89.47	2.00	8.92	0.00	0.00
33.67	23.28	17.59	3.29	91.17	2.00	9.64	0.00	0.00
33.76	23.80	17.98	3.38	93.12	2.00	10.36	0.00	0.00
33.80	24.36	18.42	3.49	95.41	2.00	11.17	0.00	0.00
33.86	24.91	18.84	3.61	97.86	2.00	11.91	0.00	0.00
33.96	25.43	19.22	3.73	100.16	2.00	12.56	0.00	0.00
34.00	25.94	19.62	3.83	102.23	2.00	13.25	0.00	0.00
34.06	26.36	19.93	3.89	103.72	2.00	13.77	0.00	0.00
34.16	26.76	20.21	3.94	104.93	2.00	14.22	0.00	0.00

:: Estimation of post-earthquake lateral Displacements :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	R_f (%)	$Q_{tn,cs}$	FS	D_r	$Gamma_{max}$ (%)	Lat. disp. (in)
34.20	26.82	20.23	4.01	105.84	2.00	14.26	0.00	0.00
34.26	26.68	20.09	4.04	105.97	2.00	14.02	0.00	0.00
34.36	26.55	19.93	4.05	105.74	2.00	13.76	0.00	0.00
34.39	26.36	19.76	4.03	105.17	2.00	13.48	0.00	0.00
34.46	26.14	19.55	4.00	104.24	2.00	13.12	0.00	0.00
34.56	25.91	19.31	3.95	103.23	2.00	12.73	0.00	0.00
34.60	25.62	19.06	3.92	102.22	2.00	12.29	0.00	0.00
34.65	25.33	18.80	3.88	101.26	2.00	11.83	0.00	0.00
34.75	25.05	18.52	3.85	100.23	2.00	11.35	0.00	0.00
34.80	24.81	18.31	3.81	99.30	2.00	10.96	0.00	0.00
34.86	24.61	18.12	3.78	98.56	2.00	10.62	0.00	0.00
34.95	24.38	17.90	3.75	97.68	2.00	10.22	0.00	0.00
34.99	24.19	17.73	3.70	96.78	2.00	9.90	0.00	0.00
35.06	24.08	17.61	3.65	95.90	2.00	9.68	0.00	0.00
35.11	23.94	17.48	3.60	95.02	2.00	9.43	0.00	0.00
35.19	23.83	17.36	3.54	94.06	2.00	9.21	0.00	0.00
35.25	23.70	17.24	3.49	93.16	2.00	8.97	0.00	0.00
35.31	23.56	17.10	3.43	92.15	2.00	8.72	0.00	0.00
35.39	23.40	16.95	3.38	91.17	2.00	8.41	0.00	0.00
35.49	23.26	16.80	3.32	90.16	2.00	8.12	0.00	0.00
35.53	23.14	16.69	3.30	89.62	2.00	7.91	0.00	0.00
35.60	23.03	16.57	3.30	89.34	2.00	7.67	0.00	0.00
35.63	22.98	16.52	3.32	89.51	2.00	7.57	0.00	0.00
35.70	23.28	16.73	3.33	90.12	2.00	7.99	0.00	0.00
35.78	23.79	17.11	3.37	91.39	2.00	8.73	0.00	0.00
35.84	24.40	17.57	3.43	93.03	2.00	9.60	0.00	0.00
35.90	25.23	18.20	3.51	95.32	2.00	10.77	0.00	0.00
35.98	26.27	19.00	3.55	97.44	2.00	12.19	0.00	0.00
36.06	27.66	20.09	3.47	98.43	2.00	14.03	0.00	0.00
36.09	29.05	21.22	3.32	98.16	2.00	15.83	0.00	0.00
36.18	30.33	22.24	3.15	97.40	2.00	17.38	0.00	0.00
36.23	31.16	22.90	3.03	96.52	2.00	18.34	0.00	0.00
36.29	31.53	23.17	2.98	96.09	2.00	18.73	0.00	0.00
36.38	31.68	23.26	2.94	95.64	2.00	18.86	0.00	0.00
36.42	32.10	23.58	2.93	95.94	2.00	19.31	0.00	0.00
36.49	33.06	24.32	2.93	97.04	2.00	20.33	0.00	0.00
36.58	34.30	25.26	2.96	98.78	2.00	21.58	0.00	0.00
36.62	36.32	26.86	3.01	101.91	2.00	23.61	0.00	0.00
36.68	39.95	29.72	3.10	107.49	2.00	26.96	0.00	0.00
36.77	44.99	33.72	3.16	113.80	2.00	31.11	0.00	0.00
36.83	52.72	39.94	3.09	119.98	2.00	36.71	0.00	0.00
36.88	62.36	47.77	2.97	126.28	2.00	42.61	0.00	0.00
36.97	72.24	55.77	2.89	132.66	2.00	47.73	0.00	0.00
37.02	81.77	63.53	2.82	138.89	2.00	52.03	0.00	0.00
37.08	89.81	70.05	2.80	144.68	2.00	55.25	0.00	0.00
37.17	96.99	75.82	2.79	150.13	0.96	57.86	4.37	0.00
37.22	102.33	80.09	2.82	155.26	1.04	59.67	3.05	0.00
37.27	105.76	82.79	2.86	158.89	1.10	60.77	2.38	0.00

:: Estimation of post-earthquake lateral Displacements :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	R_f (%)	$Q_{tn,cs}$	FS	D_r	$Gamma_{max}$ (%)	Lat. disp. (in)
37.37	108.07	84.49	2.89	161.53	1.14	61.44	1.98	0.00
37.41	108.62	84.82	2.95	163.58	1.18	61.57	1.73	0.00
37.47	108.08	84.24	3.00	164.56	1.20	61.34	1.61	0.00
37.57	107.73	83.75	3.04	165.17	1.21	61.15	1.55	0.00
37.61	107.99	83.91	3.03	164.91	1.20	61.21	1.58	0.00
37.67	110.10	85.56	2.97	164.87	1.20	61.85	1.58	0.00
37.76	112.74	87.63	2.89	164.62	1.20	62.64	1.61	0.00
37.81	116.12	90.39	2.78	163.96	1.19	63.67	1.68	0.00
37.87	119.49	93.08	2.74	165.30	1.21	64.63	1.54	0.00
37.97	123.02	95.80	2.71	167.09	1.24	65.58	1.70	0.00
38.02	126.08	98.19	2.72	169.55	1.29	66.40	1.53	0.00
38.07	128.60	100.10	2.76	172.82	1.36	67.03	1.33	0.00
38.17	130.76	101.53	2.87	177.46	1.45	67.50	1.09	0.00
38.20	133.02	103.16	3.01	183.33	1.58	68.03	0.85	0.00
38.27	136.19	105.44	3.13	189.57	1.73	68.75	0.66	0.00
38.33	141.08	109.15	3.23	196.53	1.90	69.89	0.50	0.00
38.42	146.42	113.13	3.34	203.92	2.00	71.07	0.00	0.00
38.46	152.19	117.65	3.38	209.76	2.00	72.36	0.00	0.00
38.53	157.18	121.44	3.42	215.00	2.00	73.41	0.00	0.00
38.62	161.63	124.77	3.45	219.36	2.00	74.30	0.00	0.00
38.66	165.38	127.66	3.46	222.81	2.00	75.06	0.00	0.00
38.73	169.32	130.70	3.42	224.42	2.00	75.84	0.00	0.00
38.81	173.12	133.62	3.36	225.39	2.00	76.57	0.00	0.00
38.86	175.78	135.72	3.29	225.22	2.00	77.08	0.00	0.00
38.93	177.38	136.92	3.23	224.21	2.00	77.37	0.00	0.00
39.02	179.58	138.58	3.14	222.75	2.00	77.77	0.00	0.00
39.05	181.60	140.28	3.05	221.31	2.00	78.17	0.00	0.00
39.12	182.85	141.22	2.97	219.61	2.00	78.39	0.00	0.00
39.18	183.12	141.38	2.91	217.70	2.00	78.43	0.00	0.00
39.27	183.29	141.39	2.85	215.65	2.00	78.43	0.00	0.00
39.31	184.01	141.97	2.79	214.11	2.00	78.57	0.00	0.00
39.37	182.93	141.02	2.75	211.74	2.00	78.35	0.00	0.00
39.44	182.32	140.45	2.70	209.45	2.00	78.21	0.00	0.00
39.50	182.24	140.34	2.64	207.34	2.00	78.19	0.00	0.00
39.59	181.64	139.74	2.59	205.04	2.00	78.04	0.00	0.00
39.65	180.71	138.96	2.53	202.25	2.00	77.86	0.00	0.00
39.71	179.11	137.69	2.45	198.38	1.96	77.56	0.80	0.00
39.77	177.03	136.09	2.35	193.62	1.83	77.17	0.91	0.00
39.84	174.31	134.01	2.23	187.78	1.69	76.66	1.08	0.00
39.91	169.90	130.56	2.12	181.00	1.53	75.80	1.33	0.00
39.97	167.59	128.92	1.97	174.76	1.40	75.39	1.60	0.00
40.03	163.25	125.60	1.85	167.87	1.26	74.52	1.63	0.00
40.11	158.20	121.67	1.73	160.59	1.13	73.47	2.25	0.00
40.17	153.76	118.29	1.60	153.83	1.02	72.54	3.06	0.00
40.26	150.03	115.42	1.49	147.85	0.92	71.73	4.02	0.00
40.30	148.43	114.38	1.37	143.56	0.86	71.44	4.91	0.00
40.36	148.43	114.61	1.27	140.76	0.82	71.50	5.60	0.00
40.45	149.44	115.54	1.19	139.38	0.81	71.77	5.97	0.00

:: Estimation of post-earthquake lateral Displacements :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	R_f (%)	$Q_{tn,cs}$	FS	D_r	$Gamma_{max}$ (%)	Lat. disp. (in)
40.49	150.84	116.84	1.13	138.73	0.80	72.14	6.16	0.00
40.57	151.01	117.01	1.08	137.62	0.78	72.19	6.49	0.00
40.62	151.62	117.60	1.04	136.87	0.77	72.35	6.72	0.00
40.70	151.46	117.45	1.02	136.06	0.76	72.31	6.98	0.00
40.76	150.02	116.16	1.02	134.96	0.75	71.95	7.35	0.00
40.86	148.25	114.50	1.03	133.87	0.74	71.47	7.74	0.00
40.89	146.27	112.74	1.06	133.07	0.73	70.96	8.04	0.00
40.95	144.41	110.99	1.09	132.55	0.72	70.44	8.24	0.00
41.03	143.07	109.63	1.13	132.49	0.72	70.03	8.26	0.00
41.11	142.22	108.67	1.18	132.84	0.72	69.74	8.11	0.00
41.16	141.92	108.15	1.23	134.04	0.74	69.59	7.66	0.00
41.23	141.98	107.87	1.30	135.72	0.76	69.50	7.07	0.00
41.29	142.10	107.69	1.36	137.23	0.78	69.45	6.58	0.00
41.35	142.20	107.53	1.41	138.47	0.80	69.40	6.20	0.00
41.41	142.21	107.30	1.46	139.67	0.81	69.33	5.86	0.00
41.49	142.08	106.91	1.51	140.92	0.83	69.21	5.52	0.00
41.56	141.57	106.15	1.60	142.81	0.85	68.97	5.05	0.00
41.64	140.45	104.86	1.70	144.72	0.88	68.57	4.61	0.00
41.69	138.39	102.85	1.83	146.71	0.91	67.93	4.20	0.00
41.73	135.34	100.06	1.98	148.72	0.94	67.02	3.83	0.00
41.84	131.91	96.89	2.13	150.57	0.97	65.96	3.51	0.00
41.89	128.64	93.97	2.29	152.81	1.00	64.95	3.52	0.00
41.98	126.30	91.79	2.43	154.98	1.04	64.17	3.02	0.00
42.04	124.44	90.08	2.55	156.76	1.07	63.55	2.67	0.00
42.09	123.04	88.81	2.63	157.96	1.09	63.08	2.46	0.00
42.16	122.85	88.56	2.62	157.62	1.08	62.99	2.51	0.00
42.24	123.41	88.94	2.57	156.37	1.06	63.13	2.74	0.00
42.28	124.88	90.15	2.47	154.54	1.03	63.58	3.11	0.00
42.33	127.01	91.92	2.34	152.37	1.00	64.22	3.61	0.00
42.39	129.14	93.69	2.22	150.19	0.96	64.85	4.21	0.00
42.47	130.67	94.96	2.10	147.85	0.93	65.29	3.96	0.00
42.53	130.88	95.17	2.03	145.93	0.90	65.37	4.33	0.00
42.59	130.36	94.72	2.01	144.89	0.89	65.21	4.54	0.00
42.66	128.15	92.84	2.04	144.24	0.88	64.55	6.39	0.00
42.73	125.51	90.55	2.12	144.49	2.00	63.72	0.00	0.00
42.83	121.32	86.92	2.27	145.58	2.00	62.37	0.00	0.00
42.88	116.08	82.53	2.48	147.81	2.00	60.66	0.00	0.00
42.93	110.69	78.01	2.74	150.89	2.00	58.81	0.00	0.00
42.99	105.22	73.48	3.03	154.56	2.00	56.83	0.00	0.00
43.07	100.21	69.35	3.33	158.34	2.00	54.92	0.00	0.00
43.14	95.63	65.62	3.60	161.52	2.00	53.10	0.00	0.00
43.19	90.87	61.88	3.84	163.11	2.00	51.16	0.00	0.00
43.25	86.68	58.66	3.97	162.37	2.00	49.39	0.00	0.00
43.34	81.82	54.96	4.07	160.19	2.00	47.24	0.00	0.00
43.39	77.67	51.89	4.09	156.69	2.00	45.35	0.00	0.00
43.45	73.11	48.56	4.06	151.56	0.99	43.16	6.17	0.00
43.54	68.41	45.14	3.99	145.56	0.90	40.75	28.70	0.00
43.59	63.67	41.76	3.88	138.68	0.80	38.17	51.20	0.00

:: Estimation of post-earthquake lateral Displacements :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	R_f (%)	$Q_{tn,cs}$	FS	D_r	$Gamma_{max}$ (%)	Lat. disp. (in)
43.64	58.08	37.78	3.76	130.82	2.00	34.87	0.00	0.00
43.74	52.40	33.73	3.61	122.45	2.00	31.13	0.00	0.00
43.78	46.98	29.92	3.46	114.29	2.00	27.17	0.00	0.00
43.83	42.15	26.52	3.36	107.56	2.00	23.19	0.00	0.00
43.94	37.81	23.43	3.30	101.74	2.00	19.11	0.00	0.00
43.98	34.06	20.82	3.24	96.56	2.00	15.20	0.00	0.00
44.04	31.95	19.35	3.12	92.25	2.00	12.79	0.00	0.00
44.14	30.33	18.23	2.97	88.21	2.00	10.82	0.00	0.00
44.17	29.10	17.40	2.82	84.75	2.00	9.29	0.00	0.00
44.23	28.76	17.17	2.74	83.14	2.00	8.84	0.00	0.00
44.33	28.68	17.09	2.69	82.35	2.00	8.69	0.00	0.00
44.37	29.02	17.32	2.65	82.18	2.00	9.14	0.00	0.00
44.44	29.52	17.63	2.71	83.55	2.00	9.72	0.00	0.00
44.53	30.09	17.96	2.82	85.75	2.00	10.33	0.00	0.00
44.58	30.72	18.34	2.98	88.54	2.00	11.01	0.00	0.00
44.64	31.59	18.87	3.15	91.92	2.00	11.96	0.00	0.00
44.73	33.07	19.81	3.31	95.80	2.00	13.57	0.00	0.00
44.78	34.76	20.91	3.47	100.00	2.00	15.35	0.00	0.00
44.82	36.82	22.27	3.60	104.27	2.00	17.43	0.00	0.00
44.90	39.32	23.92	3.71	108.78	2.00	19.79	0.00	0.00
44.97	41.98	25.69	3.82	113.46	2.00	22.14	0.00	0.00
45.03	45.07	27.77	3.84	117.33	2.00	24.72	0.00	0.00
45.09	48.02	29.77	3.85	120.66	2.00	27.01	0.00	0.00
45.17	50.82	31.66	3.84	123.53	2.00	29.04	0.00	0.00
45.22	53.50	33.49	3.84	126.23	2.00	30.89	0.00	0.00
45.29	55.93	35.13	3.83	128.50	2.00	32.47	0.00	0.00
45.38	58.32	36.73	3.80	130.31	2.00	33.95	0.00	0.00
45.42	60.57	38.30	3.75	131.40	2.00	35.33	0.00	0.00
45.50	62.33	39.50	3.68	131.76	2.00	36.34	0.00	0.00
45.57	63.62	40.38	3.63	131.88	0.73	37.06	51.20	0.00
45.62	64.35	40.86	3.59	131.80	0.72	37.46	51.20	0.00
45.69	64.79	41.14	3.56	131.34	0.72	37.68	51.20	0.00
45.77	65.03	41.27	3.52	130.71	0.71	37.79	51.20	0.00
45.82	64.64	40.97	3.48	129.68	0.70	37.55	51.20	0.00
45.88	63.43	40.09	3.47	128.34	0.68	36.83	51.20	0.00
45.97	61.81	38.90	3.47	126.83	0.67	35.83	51.20	0.00
46.02	59.45	37.20	3.51	125.35	2.00	34.36	0.00	0.00
46.10	56.51	35.08	3.60	124.07	2.00	32.42	0.00	0.00
46.17	53.60	32.99	3.68	122.72	2.00	30.40	0.00	0.00
46.21	50.91	31.09	3.77	121.40	2.00	28.44	0.00	0.00
46.27	48.55	29.43	3.83	119.86	2.00	26.63	0.00	0.00
46.36	46.40	27.90	3.88	118.19	2.00	24.87	0.00	0.00
46.42	44.50	26.58	3.92	116.57	2.00	23.26	0.00	0.00
46.46	42.82	25.41	3.96	115.16	2.00	21.78	0.00	0.00
46.56	41.38	24.39	3.99	113.82	2.00	20.43	0.00	0.00
46.61	40.40	23.70	4.01	112.81	2.00	19.48	0.00	0.00
46.66	39.90	23.35	4.00	112.07	2.00	18.99	0.00	0.00
46.74	39.54	23.07	4.02	111.78	2.00	18.59	0.00	0.00

:: Estimation of post-earthquake lateral Displacements :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	R_f (%)	$Q_{tn,cs}$	FS	D_r	$Gamma_{max}$ (%)	Lat. disp. (in)
46.81	39.12	22.74	4.06	111.81	2.00	18.12	0.00	0.00
46.87	38.64	22.38	4.15	112.27	2.00	17.58	0.00	0.00
46.94	38.63	22.33	4.19	112.77	2.00	17.51	0.00	0.00
47.01	38.71	22.33	4.24	113.37	2.00	17.52	0.00	0.00
47.06	38.83	22.38	4.28	114.02	2.00	17.59	0.00	0.00
47.12	39.01	22.46	4.30	114.54	2.00	17.71	0.00	0.00
47.19	39.29	22.62	4.29	114.67	2.00	17.94	0.00	0.00
47.25	39.58	22.79	4.25	114.47	2.00	18.19	0.00	0.00
47.34	39.73	22.86	4.20	113.86	2.00	18.29	0.00	0.00
47.39	39.72	22.85	4.14	113.08	2.00	18.27	0.00	0.00
47.44	39.77	22.88	4.07	112.17	2.00	18.31	0.00	0.00
47.54	39.28	22.52	4.04	111.05	2.00	17.79	0.00	0.00
47.59	38.71	22.13	4.02	110.09	2.00	17.22	0.00	0.00
47.65	38.41	21.91	4.00	109.31	2.00	16.89	0.00	0.00
47.74	37.95	21.57	4.01	108.75	2.00	16.37	0.00	0.00
47.81	37.56	21.28	4.03	108.54	2.00	15.93	0.00	0.00
47.85	37.47	21.20	4.05	108.59	2.00	15.80	0.00	0.00
47.94	37.60	21.25	4.05	108.69	2.00	15.87	0.00	0.00
47.98	37.97	21.46	4.06	109.34	2.00	16.21	0.00	0.00
48.04	38.79	21.97	4.08	110.49	2.00	16.98	0.00	0.00
48.13	39.93	22.66	4.09	112.01	2.00	18.00	0.00	0.00
48.17	41.38	23.58	4.10	113.87	2.00	19.32	0.00	0.00
48.24	42.73	24.42	4.14	116.08	2.00	20.46	0.00	0.00
48.32	44.25	25.35	4.17	118.31	2.00	21.71	0.00	0.00
48.37	46.09	26.53	4.19	120.75	2.00	23.20	0.00	0.00
48.44	48.52	28.08	4.17	123.16	2.00	25.07	0.00	0.00
48.53	51.56	30.04	4.10	125.39	2.00	27.31	0.00	0.00
48.56	54.96	32.30	4.00	127.24	2.00	29.70	0.00	0.00
48.64	59.29	35.19	3.84	128.73	2.00	32.53	0.00	0.00
48.72	64.04	38.37	3.68	130.28	2.00	35.39	0.00	0.00
48.78	69.67	42.21	3.50	131.70	2.00	38.53	0.00	0.00
48.83	76.00	46.56	3.32	133.11	2.00	41.77	0.00	0.00
48.90	82.27	50.88	3.18	134.67	2.00	44.70	0.00	0.00
48.97	87.90	54.74	3.09	136.96	2.00	47.11	0.00	0.00
49.03	93.07	58.27	3.05	139.62	2.00	49.17	0.00	0.00
49.12	97.81	61.45	3.03	142.53	0.88	50.93	9.44	0.00
49.16	102.84	64.88	3.02	145.62	0.93	52.72	6.85	0.00
49.23	107.68	68.15	3.00	148.54	0.97	54.35	5.06	0.00
49.31	113.16	71.90	2.96	151.31	1.02	56.11	3.33	0.00
49.36	118.20	75.37	2.93	153.88	1.06	57.67	2.78	0.00
49.43	123.66	79.14	2.88	156.19	1.10	59.28	2.36	0.00
49.52	130.09	83.63	2.81	158.50	1.14	61.10	2.01	0.00
49.58	137.03	88.58	2.71	160.30	1.17	63.00	1.77	0.00
49.62	143.61	93.36	2.60	161.63	1.20	64.73	1.62	0.00
49.71	149.84	98.02	2.44	160.96	1.19	66.34	1.96	0.00
49.78	155.24	102.19	2.27	159.69	1.16	67.71	2.07	0.00
49.81	159.41	105.51	2.14	158.62	1.14	68.77	2.17	0.00
49.88	162.01	107.57	2.04	157.54	1.13	69.41	2.27	0.00

:: Estimation of post-earthquake lateral Displacements :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	R_f (%)	$Q_{tn,cs}$	FS	D_r	$Gamma_{max}$ (%)	Lat. disp. (in)
49.97	163.35	108.59	1.98	156.61	1.11	69.72	2.37	0.00
50.00	161.66	107.39	1.96	155.04	1.08	69.35	2.54	0.00
50.07	160.26	106.28	1.96	153.97	2.00	69.01	0.00	0.00
50.14	158.20	104.64	1.98	153.02	2.00	68.50	0.00	0.00
50.22	154.55	101.76	2.02	151.80	2.00	67.58	0.00	0.00
50.27	149.22	97.52	2.15	151.87	2.00	66.17	0.00	0.00
50.35	143.10	92.63	2.32	152.47	2.00	64.47	0.00	0.00
50.40	135.60	86.89	2.50	152.50	2.00	62.36	0.00	0.00
50.47	127.45	80.82	2.66	151.35	2.00	59.97	0.00	0.00
50.55	119.71	75.19	2.77	149.24	2.00	57.59	0.00	0.00
50.59	114.02	71.17	2.82	146.72	2.00	55.77	0.00	0.00
50.66	106.49	65.86	2.89	143.35	2.00	53.22	0.00	0.00
50.75	98.69	60.41	2.96	139.61	2.00	50.36	0.00	0.00
50.79	91.04	55.16	3.03	135.79	2.00	47.37	0.00	0.00
50.86	83.73	50.19	3.07	131.58	2.00	44.25	0.00	0.00
50.94	76.84	45.52	3.11	127.20	2.00	41.02	0.00	0.00
50.99	70.78	41.49	3.12	122.83	2.00	37.97	0.00	0.00
51.05	65.41	37.95	3.12	118.60	2.00	35.02	0.00	0.00
51.14	60.12	34.47	3.12	114.18	2.00	31.84	0.00	0.00
51.18	54.60	30.89	3.12	109.70	2.00	28.22	0.00	0.00
51.25	49.39	27.54	3.08	104.45	2.00	24.44	0.00	0.00
51.34	44.37	24.36	2.99	98.37	2.00	20.38	0.00	0.00
51.41	40.71	22.11	2.80	91.95	2.00	17.18	0.00	0.00
51.44	38.40	20.75	2.54	85.82	2.00	15.10	0.00	0.00
51.52	36.49	19.65	2.26	79.66	2.00	13.30	0.00	0.00
51.67	35.22	18.94	1.97	74.02	2.00	12.08	0.00	0.00
51.70	34.13	18.33	1.79	70.04	2.00	11.00	0.00	0.00
51.75	33.21	17.79	1.69	67.69	2.00	10.01	0.00	0.00
51.78	32.42	17.30	1.63	66.11	2.00	9.10	0.00	0.00
51.88	32.20	17.13	1.64	65.99	2.00	8.77	0.00	0.00
51.92	32.47	17.26	1.69	67.16	2.00	9.02	0.00	0.00
51.99	32.74	17.38	1.76	68.52	2.00	9.24	0.00	0.00
52.04	32.85	17.38	1.86	70.20	2.00	9.24	0.00	0.00
52.14	32.83	17.29	1.97	71.79	2.00	9.07	0.00	0.00
52.19	32.56	17.06	2.07	73.12	2.00	8.63	0.00	0.00
52.26	31.97	16.63	2.15	73.88	2.00	7.80	0.00	0.00
52.33	31.02	16.00	2.21	73.79	2.00	6.51	0.00	0.00
52.38	29.91	15.28	2.26	73.35	2.00	4.99	0.00	0.00
52.43	28.33	14.28	2.30	72.33	2.00	2.76	0.00	0.00
52.51	26.65	13.23	2.32	70.78	2.00	0.23	0.00	0.00
52.58	25.06	12.25	2.31	68.88	2.00	0.00	0.00	0.00
52.63	23.61	11.38	2.25	66.51	2.00	0.00	0.00	0.00
52.69	22.29	10.60	2.18	64.03	2.00	0.00	0.00	0.00
52.77	21.16	9.93	2.08	61.57	2.00	0.00	0.00	0.00
52.83	20.40	9.49	1.98	59.49	2.00	0.00	0.00	0.00
52.90	19.92	9.22	1.90	57.98	2.00	0.00	0.00	0.00
52.99	19.57	9.02	1.82	56.56	2.00	0.00	0.00	0.00
53.05	19.39	8.91	1.74	55.38	2.00	0.00	0.00	0.00

:: Estimation of post-earthquake lateral Displacements :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	R_f (%)	$Q_{tn,cs}$	FS	D_r	$Gamma_{max}$ (%)	Lat. disp. (in)
53.10	19.24	8.82	1.69	54.61	2.00	0.00	0.00	0.00
53.16	19.09	8.74	1.65	53.96	2.00	0.00	0.00	0.00
53.25	18.99	8.67	1.62	53.51	2.00	0.00	0.00	0.00
53.29	18.94	8.64	1.60	53.22	2.00	0.00	0.00	0.00
53.38	18.91	8.62	1.57	52.77	2.00	0.00	0.00	0.00
53.44	18.88	8.60	1.54	52.39	2.00	0.00	0.00	0.00
53.50	18.85	8.58	1.52	52.09	2.00	0.00	0.00	0.00
53.55	18.80	8.54	1.51	51.85	2.00	0.00	0.00	0.00
53.64	18.73	8.49	1.50	51.68	2.00	0.00	0.00	0.00
53.72	18.66	8.44	1.49	51.50	2.00	0.00	0.00	0.00
53.74	18.66	8.44	1.49	51.43	2.00	0.00	0.00	0.00
53.82	18.74	8.47	1.48	51.42	2.00	0.00	0.00	0.00
53.90	18.83	8.51	1.49	51.55	2.00	0.00	0.00	0.00
53.94	18.95	8.58	1.51	51.92	2.00	0.00	0.00	0.00
54.01	19.10	8.65	1.53	52.34	2.00	0.00	0.00	0.00
54.09	19.25	8.72	1.55	52.76	2.00	0.00	0.00	0.00
54.19	19.41	8.79	1.57	53.10	2.00	0.00	0.00	0.00
54.24	19.57	8.88	1.58	53.39	2.00	0.00	0.00	0.00
54.29	19.71	8.95	1.58	53.60	2.00	0.00	0.00	0.00
54.35	19.78	8.98	1.58	53.59	2.00	0.00	0.00	0.00
54.44	19.79	8.98	1.56	53.36	2.00	0.00	0.00	0.00
54.49	19.78	8.98	1.53	53.01	2.00	0.00	0.00	0.00
54.53	19.74	8.96	1.50	52.57	2.00	0.00	0.00	0.00
54.63	19.69	8.92	1.47	52.05	2.00	0.00	0.00	0.00
54.68	19.64	8.90	1.43	51.53	2.00	0.00	0.00	0.00
54.74	19.58	8.86	1.40	51.08	2.00	0.00	0.00	0.00
54.83	19.56	8.85	1.37	50.69	2.00	0.00	0.00	0.00
54.88	19.53	8.82	1.37	50.52	2.00	0.00	0.00	0.00
54.94	19.53	8.81	1.39	50.80	2.00	0.00	0.00	0.00
55.03	19.54	8.79	1.42	51.22	2.00	0.00	0.00	0.00
55.07	19.56	8.78	1.46	51.71	2.00	0.00	0.00	0.00
55.13	19.56	8.76	1.51	52.25	2.00	0.00	0.00	0.00
55.23	19.57	8.74	1.55	52.78	2.00	0.00	0.00	0.00
55.28	19.59	8.73	1.59	53.32	2.00	0.00	0.00	0.00
55.32	19.63	8.73	1.64	53.85	2.00	0.00	0.00	0.00
55.42	19.66	8.72	1.66	54.15	2.00	0.00	0.00	0.00
55.50	19.75	8.77	1.67	54.28	2.00	0.00	0.00	0.00
55.53	19.81	8.80	1.65	54.15	2.00	0.00	0.00	0.00
55.58	19.82	8.80	1.64	54.07	2.00	0.00	0.00	0.00
55.66	19.80	8.78	1.63	53.84	2.00	0.00	0.00	0.00
55.73	19.80	8.79	1.56	53.02	2.00	0.00	0.00	0.00
55.78	19.97	8.86	1.64	54.17	2.00	0.00	0.00	0.00
55.86	20.32	9.02	1.78	56.19	2.00	0.00	0.00	0.00
55.93	20.98	9.35	1.95	58.91	2.00	0.00	0.00	0.00
55.97	22.90	10.37	2.19	63.82	2.00	0.00	0.00	0.00
56.08	26.02	12.11	2.37	69.47	2.00	0.00	0.00	0.00
56.12	30.92	14.96	2.43	75.34	2.00	4.29	0.00	0.00
56.17	39.52	20.15	2.30	81.08	2.00	14.13	0.00	0.00

:: Estimation of post-earthquake lateral Displacements :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	R_f (%)	$Q_{tn,cs}$	FS	D_r	$Gamma_{max}$ (%)	Lat. disp. (in)
56.28	48.92	25.93	2.19	86.19	2.00	22.45	0.00	0.00
56.32	59.00	32.27	2.11	91.38	2.00	29.67	0.00	0.00
56.37	69.47	39.03	2.00	95.22	2.00	35.94	0.00	0.00
56.47	79.91	45.84	1.89	98.82	2.00	41.25	0.00	0.00
56.52	90.20	52.68	1.81	102.49	2.00	45.84	0.00	0.00
56.57	98.80	58.43	1.75	105.88	2.00	49.27	0.00	0.00
56.67	105.68	62.98	1.72	109.00	2.00	51.74	0.00	0.00
56.72	109.54	65.45	1.74	111.70	2.00	53.01	0.00	0.00
56.78	108.92	64.78	1.82	113.30	2.00	52.67	0.00	0.00
56.87	106.09	62.58	1.93	114.28	2.00	51.53	0.00	0.00
56.91	101.69	59.38	2.05	114.91	2.00	49.80	0.00	0.00
56.97	94.90	54.58	2.24	115.36	2.00	47.01	0.00	0.00
57.03	87.46	49.42	2.46	116.07	2.00	43.74	0.00	0.00
57.11	79.60	44.05	2.73	117.05	2.00	39.94	0.00	0.00
57.17	72.07	39.08	2.98	117.09	2.00	35.98	0.00	0.00
57.26	64.98	34.48	3.20	115.99	2.00	31.86	0.00	0.00
57.32	58.98	30.71	3.37	114.08	2.00	28.04	0.00	0.00
57.35	53.23	27.19	3.52	111.44	2.00	24.02	0.00	0.00
57.42	48.56	24.36	3.62	108.40	2.00	20.39	0.00	0.00
57.51	44.62	22.00	3.67	105.07	2.00	17.03	0.00	0.00
57.55	42.37	20.71	3.59	101.63	2.00	15.04	0.00	0.00
57.62	40.27	19.53	3.46	97.64	2.00	13.09	0.00	0.00
57.71	38.27	18.41	3.30	93.40	2.00	11.15	0.00	0.00
57.78	36.28	17.29	3.17	89.53	2.00	9.08	0.00	0.00
57.82	34.25	16.16	3.07	86.01	2.00	6.83	0.00	0.00
57.90	32.33	15.08	2.96	82.51	2.00	4.55	0.00	0.00
57.96	30.91	14.30	2.81	79.14	2.00	2.81	0.00	0.00
58.01	29.77	13.70	2.64	75.90	2.00	1.38	0.00	0.00
58.11	28.76	13.15	2.48	72.86	2.00	0.04	0.00	0.00
58.15	27.83	12.67	2.33	70.01	2.00	0.00	0.00	0.00
58.21	27.11	12.29	2.20	67.59	2.00	0.00	0.00	0.00
58.31	26.42	11.92	2.06	65.17	2.00	0.00	0.00	0.00
58.35	25.74	11.58	1.93	62.82	2.00	0.00	0.00	0.00
58.42	25.07	11.21	1.84	61.05	2.00	0.00	0.00	0.00
58.50	24.42	10.86	1.77	59.40	2.00	0.00	0.00	0.00
58.55	23.79	10.51	1.71	58.05	2.00	0.00	0.00	0.00
58.61	23.23	10.19	1.66	56.92	2.00	0.00	0.00	0.00
58.70	22.64	9.86	1.63	55.93	2.00	0.00	0.00	0.00
58.75	22.12	9.56	1.63	55.31	2.00	0.00	0.00	0.00
58.81	21.76	9.34	1.63	55.01	2.00	0.00	0.00	0.00
58.89	21.58	9.22	1.64	54.89	2.00	0.00	0.00	0.00
58.95	21.52	9.18	1.66	54.99	2.00	0.00	0.00	0.00
59.00	21.65	9.23	1.67	55.30	2.00	0.00	0.00	0.00
59.10	21.83	9.32	1.68	55.60	2.00	0.00	0.00	0.00
59.15	22.01	9.40	1.70	55.91	2.00	0.00	0.00	0.00
59.20	22.17	9.48	1.71	56.28	2.00	0.00	0.00	0.00
59.28	22.35	9.57	1.73	56.65	2.00	0.00	0.00	0.00
59.35	22.51	9.62	1.78	57.35	2.00	0.00	0.00	0.00

:: Estimation of post-earthquake lateral Displacements :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	R_f (%)	$Q_{tn,cs}$	FS	D_r	$Gamma_{max}$ (%)	Lat. disp. (in)
59.38	22.75	9.74	1.83	58.18	2.00	0.00	0.00	0.00
59.46	23.08	9.90	1.85	58.82	2.00	0.00	0.00	0.00
59.53	23.71	10.25	1.83	59.22	2.00	0.00	0.00	0.00
59.59	24.44	10.68	1.76	59.03	2.00	0.00	0.00	0.00
59.67	25.08	11.05	1.71	58.93	2.00	0.00	0.00	0.00
59.73	25.65	11.38	1.66	58.87	2.00	0.00	0.00	0.00
59.79	26.13	11.64	1.65	59.15	2.00	0.00	0.00	0.00
59.89	26.74	11.97	1.66	59.70	2.00	0.00	0.00	0.00
59.94	27.35	12.30	1.69	60.60	2.00	0.00	0.00	0.00
59.99	28.37	12.84	1.75	62.31	2.00	0.00	0.00	0.00
60.07	30.97	14.49	1.43	59.42	2.00	3.24	0.00	0.00
60.12	34.29	16.66	1.14	56.43	2.00	7.84	0.00	0.00
60.19	40.56	20.76	0.87	53.74	2.00	15.12	0.00	0.00
60.25	48.38	26.09	0.64	51.69	2.00	22.65	0.00	0.00
60.33	55.12	30.89	0.48	50.62	2.00	28.23	0.00	0.00
60.38	61.17	35.45	0.35	35.45	2.00	32.77	0.00	0.00
60.48	67.60	40.50	0.24	40.50	2.00	37.17	0.00	0.00
60.53	77.07	48.20	0.12	48.20	2.00	42.91	0.00	0.00
60.61	80.93	N/A	0.00	-1.00	2.00	0.00	0.00	0.00
60.63	82.24	N/A	0.00	-1.00	2.00	0.00	0.00	0.00

Total estimated displacement: 2.13

Abbreviations

q_t: Total cone resistance
Q_{tn}: Adjusted cone resistance to an effective overburden stress of 1 atm
R_f: Friction ration
$Q_{tn,cs}$: Adjusted and corrected cone resistance due to fines
FS: Calculated factor of safety against liquefaction
D_r: Calculated relative density
$Gamma_{max}$: Calculated maximum cyclic shear strain
Lat. disp.: Lateral displacement

:: Strength loss calculation (Robertson (2009) ::

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
0.08	9.60	15.42	3.88	59.90	2.68	N/A	N/A
0.15	12.30	19.75	3.25	64.14	2.59	N/A	N/A
0.23	15.73	25.25	2.71	68.51	2.49	N/A	N/A
0.30	19.25	30.90	2.37	73.28	2.41	N/A	N/A
0.35	22.73	36.49	2.17	79.06	2.36	N/A	N/A
0.43	27.09	43.49	2.00	87.15	2.32	N/A	N/A
0.50	31.20	50.08	1.90	95.08	2.28	N/A	N/A
0.55	34.99	56.17	1.84	103.30	2.26	N/A	N/A
0.61	38.30	61.48	1.82	111.93	2.26	N/A	N/A
0.70	41.27	66.25	1.82	120.26	2.26	N/A	N/A
0.73	43.17	69.29	1.84	127.26	2.26	N/A	N/A
0.80	43.66	70.07	1.88	132.08	2.28	N/A	N/A
0.89	43.46	69.74	1.95	135.95	2.30	N/A	N/A
0.93	42.22	67.74	2.04	138.27	2.33	N/A	N/A
1.01	40.68	65.27	2.12	138.64	2.35	N/A	N/A
1.09	39.02	62.58	2.20	137.77	2.37	N/A	N/A
1.13	37.30	59.82	2.26	135.26	2.39	N/A	N/A
1.19	35.82	57.45	2.28	131.07	2.39	N/A	N/A
1.29	34.39	55.14	2.29	126.20	2.39	N/A	N/A
1.34	33.05	52.98	2.28	120.97	2.39	N/A	N/A
1.39	32.13	51.49	2.26	116.52	2.39	N/A	N/A
1.45	30.90	49.51	2.27	112.45	2.39	N/A	N/A
1.54	30.65	49.10	2.21	108.60	2.37	N/A	N/A
1.59	30.22	48.41	2.18	105.51	2.37	N/A	N/A
1.67	29.56	47.34	2.17	102.95	2.36	N/A	N/A
1.72	28.85	46.20	2.19	101.08	2.37	N/A	N/A
1.79	27.91	44.68	2.22	99.05	2.38	N/A	N/A
1.85	26.72	42.76	2.26	96.74	2.39	N/A	N/A
1.94	25.40	40.63	2.33	94.54	2.40	N/A	N/A
1.98	23.66	37.83	2.45	92.65	2.43	N/A	N/A
2.04	22.23	35.53	2.56	90.86	2.46	N/A	N/A
2.13	20.14	32.16	2.80	89.96	2.51	N/A	N/A
2.17	18.38	29.33	3.05	89.57	2.55	N/A	N/A
2.24	16.92	26.97	3.36	90.61	2.61	N/A	N/A
2.32	15.55	24.76	3.74	92.51	2.66	N/A	N/A
2.39	14.33	22.81	4.18	95.38	2.72	N/A	N/A
2.43	13.41	21.32	4.61	98.35	2.78	N/A	N/A
2.52	12.71	20.20	5.00	101.07	2.83	N/A	N/A
2.58	12.27	19.47	5.31	103.33	2.86	N/A	N/A
2.63	11.94	18.94	5.56	105.23	2.89	N/A	N/A
2.72	11.69	18.54	5.76	106.84	2.91	N/A	N/A
2.78	11.47	18.18	5.95	108.19	2.93	N/A	N/A
2.83	11.30	17.90	6.07	108.67	2.94	N/A	N/A
2.89	11.12	17.61	6.17	108.63	2.95	N/A	N/A
2.98	10.92	17.28	6.27	108.39	2.96	N/A	N/A
3.03	10.65	16.84	6.43	108.26	2.97	N/A	N/A
3.09	10.34	16.33	6.62	108.12	2.99	N/A	N/A
3.18	10.03	15.82	6.82	107.86	3.01	N/A	N/A

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
3.22	9.73	15.34	7.00	107.37	3.02	N/A	N/A
3.32	9.47	14.92	7.15	106.66	3.04	N/A	N/A
3.37	9.26	14.57	7.27	105.83	3.05	N/A	N/A
3.42	9.09	14.29	7.35	105.00	3.05	N/A	N/A
3.52	8.99	14.13	7.37	104.17	3.05	N/A	N/A
3.57	8.93	14.01	7.37	103.23	3.05	N/A	N/A
3.61	8.95	14.05	7.28	102.30	3.05	N/A	N/A
3.68	8.99	14.10	7.19	101.46	3.04	N/A	N/A
3.77	9.05	14.19	7.11	100.93	3.03	N/A	N/A
3.83	9.13	14.32	7.04	100.83	3.03	N/A	N/A
3.91	9.21	14.44	6.97	100.72	3.02	N/A	N/A
3.95	9.30	14.58	6.93	101.04	3.02	N/A	N/A
4.02	9.38	14.71	6.91	101.68	3.01	N/A	N/A
4.12	9.44	14.79	6.94	102.63	3.02	N/A	N/A
4.14	9.48	14.85	6.97	103.57	3.02	N/A	N/A
4.22	9.49	14.87	6.99	103.89	3.02	N/A	N/A
4.27	9.45	14.80	7.08	104.71	3.03	N/A	N/A
4.37	9.36	14.64	7.19	105.22	3.04	N/A	N/A
4.42	9.19	14.37	7.33	105.31	3.05	N/A	N/A
4.46	9.00	14.05	7.49	105.28	3.06	N/A	N/A
4.57	8.66	13.50	7.77	104.88	3.09	N/A	N/A
4.61	8.38	13.05	7.98	104.17	3.10	N/A	N/A
4.67	8.12	12.63	8.18	103.24	3.12	N/A	N/A
4.76	7.86	12.20	8.39	102.28	3.14	N/A	N/A
4.81	7.60	11.77	8.65	101.79	3.16	N/A	N/A
4.90	7.39	11.44	8.80	100.62	3.17	N/A	N/A
4.96	7.20	11.12	8.94	99.34	3.18	N/A	N/A
5.00	7.06	10.89	9.03	98.30	3.18	N/A	N/A
5.05	6.97	10.75	9.07	97.51	3.19	N/A	N/A
5.14	7.06	10.88	8.91	96.98	3.18	N/A	N/A
5.20	7.09	10.92	8.83	96.38	3.17	N/A	N/A
5.30	7.10	10.94	8.77	95.87	3.16	N/A	N/A
5.35	7.13	10.98	8.71	95.58	3.16	N/A	N/A
5.39	7.16	11.02	8.66	95.50	3.16	N/A	N/A
5.48	7.22	11.11	8.60	95.54	3.15	N/A	N/A
5.55	7.34	11.29	8.49	95.84	3.14	N/A	N/A
5.59	7.46	11.49	8.37	96.14	3.13	N/A	N/A
5.64	7.63	11.76	8.19	96.34	3.12	N/A	N/A
5.74	7.81	12.04	8.01	96.43	3.11	N/A	N/A
5.79	8.05	12.42	7.77	96.53	3.09	N/A	N/A
5.84	8.32	12.85	7.55	97.05	3.07	N/A	N/A
5.94	8.60	13.29	7.36	97.86	3.05	N/A	N/A
5.97	8.86	13.70	7.20	98.66	3.04	N/A	N/A
6.05	9.05	14.00	7.11	99.53	3.03	N/A	N/A
6.14	9.20	14.23	7.06	100.50	3.03	N/A	N/A
6.19	9.32	14.42	7.05	101.57	3.03	N/A	N/A
6.24	9.37	14.49	7.07	102.52	3.03	N/A	N/A
6.33	9.38	14.50	7.12	103.26	3.03	N/A	N/A

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
6.38	9.33	14.41	7.21	103.88	3.04	N/A	N/A
6.44	9.28	14.33	7.26	104.08	3.05	N/A	N/A
6.52	9.24	14.26	7.30	104.07	3.05	N/A	N/A
6.59	9.21	14.21	7.32	103.97	3.05	N/A	N/A
6.64	9.22	14.22	7.30	103.76	3.05	N/A	N/A
6.70	9.21	14.20	7.29	103.45	3.05	N/A	N/A
6.78	9.24	14.24	7.24	103.04	3.04	N/A	N/A
6.83	9.24	14.24	7.23	102.93	3.04	N/A	N/A
6.89	9.27	14.28	7.22	103.14	3.04	N/A	N/A
6.98	9.30	14.32	7.23	103.56	3.04	N/A	N/A
7.03	9.35	14.39	7.24	104.19	3.04	N/A	N/A
7.09	9.39	14.45	7.25	104.80	3.04	N/A	N/A
7.18	9.43	14.51	7.27	105.52	3.05	N/A	N/A
7.23	9.47	14.57	7.29	106.24	3.05	N/A	N/A
7.29	9.51	14.63	7.28	106.54	3.05	N/A	N/A
7.38	9.51	14.62	7.28	106.44	3.05	N/A	N/A
7.42	9.52	14.63	7.27	106.34	3.05	N/A	N/A
7.48	9.51	14.61	7.27	106.24	3.05	N/A	N/A
7.58	9.49	14.57	7.28	106.03	3.05	N/A	N/A
7.62	9.43	14.47	7.28	105.42	3.05	N/A	N/A
7.68	9.37	14.36	7.28	104.49	3.05	N/A	N/A
7.78	9.31	14.25	7.26	103.45	3.04	N/A	N/A
7.81	9.25	14.16	7.22	102.20	3.04	N/A	N/A
7.88	9.22	14.10	7.19	101.46	3.04	N/A	N/A
7.97	9.19	14.05	7.18	100.93	3.04	N/A	N/A
8.01	9.17	14.02	7.14	100.07	3.03	N/A	N/A
8.11	9.14	13.96	7.09	98.99	3.03	N/A	N/A
8.14	9.10	13.89	7.05	97.90	3.03	N/A	N/A
8.22	9.05	13.81	7.02	96.90	3.02	N/A	N/A
8.31	8.96	13.66	7.03	96.01	3.03	N/A	N/A
8.35	8.84	13.45	7.06	95.00	3.03	N/A	N/A
8.41	8.65	13.14	7.14	93.85	3.04	N/A	N/A
8.50	8.44	12.80	7.21	92.34	3.04	N/A	N/A
8.56	8.22	12.45	7.30	90.80	3.05	N/A	N/A
8.61	8.02	12.11	7.36	89.12	3.05	N/A	N/A
8.68	7.81	11.77	7.43	87.40	3.06	N/A	N/A
8.75	7.62	11.46	7.45	85.41	3.06	N/A	N/A
8.80	7.46	11.19	7.46	83.50	3.06	N/A	N/A
8.89	7.34	10.99	7.43	81.68	3.06	N/A	N/A
8.94	7.28	10.89	7.34	79.97	3.05	N/A	N/A
9.00	7.30	10.92	7.19	78.50	3.04	N/A	N/A
9.08	7.36	11.01	7.00	77.13	3.02	0.97	0.97
9.15	7.44	11.14	6.82	76.02	3.01	0.97	0.97
9.20	7.49	11.22	6.69	75.01	3.00	0.98	0.98
9.28	7.51	11.24	6.60	74.14	2.99	0.97	0.97
9.35	7.52	11.25	6.55	73.70	2.98	0.96	0.96
9.40	7.54	11.28	6.53	73.70	2.98	0.96	0.96
9.45	7.59	11.36	6.53	74.13	2.98	0.96	0.96

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
9.55	7.66	11.46	6.56	75.15	2.98	0.96	0.96
9.59	7.88	11.81	6.53	77.12	2.98	0.99	0.99
9.69	8.26	12.41	6.50	80.66	2.98	1.03	1.03
9.74	8.85	13.35	6.36	84.90	2.96	1.10	1.10
9.79	9.71	14.73	6.18	91.03	2.95	1.21	1.21
9.84	10.70	16.32	5.97	97.37	2.93	1.33	1.33
9.94	11.82	18.10	5.74	103.99	2.90	1.46	1.46
10.00	13.13	20.20	5.47	110.57	2.88	1.62	1.62
10.09	14.51	22.41	5.22	117.08	2.85	1.78	1.78
10.13	15.87	24.60	5.00	123.02	2.83	1.95	1.95
10.18	17.10	26.57	4.83	128.46	2.81	2.09	2.09
10.24	18.19	28.31	4.70	133.07	2.79	2.22	2.22
10.33	19.08	29.73	4.61	137.04	2.78	2.31	2.31
10.37	19.75	30.80	4.50	138.53	2.77	2.38	2.38
10.43	20.34	31.75	4.39	139.54	2.75	2.44	2.44
10.52	20.84	32.54	4.30	140.02	2.74	2.48	2.48
10.59	21.08	32.92	4.26	140.09	2.73	2.49	2.49
10.64	21.13	32.99	4.23	139.63	2.73	2.48	2.48
10.70	20.97	32.65	4.26	139.01	2.73	2.45	2.45
10.78	20.88	32.28	4.27	137.82	2.74	2.42	2.42
10.83	20.80	32.00	4.27	136.50	2.74	2.39	2.39
10.94	20.72	31.57	4.28	134.99	2.74	2.36	2.36
10.99	20.74	31.46	4.28	134.82	2.74	2.35	2.35
11.03	21.20	31.99	4.20	134.49	2.73	2.39	2.39
11.09	21.83	32.70	4.10	134.07	2.71	2.45	2.45
11.17	22.79	33.81	3.96	133.84	2.69	2.54	2.54
11.24	23.92	35.18	3.81	134.18	2.67	2.66	2.66
11.33	25.05	36.47	3.69	134.60	2.66	2.76	2.76
11.37	25.77	37.35	3.64	136.05	2.65	2.83	2.83
11.44	26.22	37.80	3.63	137.34	2.65	2.86	2.86
11.52	26.58	38.07	3.64	138.41	2.65	2.88	2.88
11.57	26.65	38.03	3.66	139.31	2.65	2.87	2.87
11.63	26.16	37.23	3.76	139.89	2.67	2.80	2.80
11.72	25.38	35.96	3.90	140.36	2.69	2.70	2.70
11.76	24.28	34.38	4.07	139.96	2.71	2.57	2.57
11.83	23.04	32.52	4.25	138.03	2.73	2.41	2.41
11.92	21.96	30.82	4.39	135.33	2.75	2.28	2.28
11.94	21.21	29.72	4.44	132.01	2.76	2.20	2.20
12.02	20.75	28.89	4.44	128.38	2.76	2.13	2.13
12.11	20.42	28.28	4.42	124.87	2.76	2.09	2.09
12.16	20.40	28.14	4.32	121.60	2.74	2.08	2.08
12.22	20.54	28.21	4.22	119.09	2.73	2.09	2.09
12.31	20.81	28.44	4.11	117.01	2.72	2.11	2.11
12.36	21.16	28.83	4.05	116.71	2.71	2.15	2.15
12.42	21.60	29.35	4.01	117.81	2.70	2.19	2.19
12.50	22.12	29.98	3.99	119.47	2.70	2.23	2.23
12.56	22.63	30.60	3.97	121.49	2.70	2.28	2.28
12.62	23.07	31.16	3.98	124.10	2.70	2.32	2.32

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
12.70	23.50	31.67	4.00	126.72	2.70	2.36	2.36
12.77	23.80	32.03	4.05	129.56	2.71	2.38	2.38
12.81	23.99	32.28	4.09	132.01	2.71	2.40	2.40
12.91	24.10	32.33	4.13	133.52	2.72	2.40	2.40
12.96	24.23	32.45	4.13	134.17	2.72	2.41	2.41
13.01	24.25	32.42	4.14	134.28	2.72	2.40	2.40
13.06	24.27	32.37	4.12	133.47	2.72	2.40	2.40
13.16	24.35	32.33	4.09	132.12	2.71	2.40	2.40
13.21	24.41	32.31	4.03	130.18	2.70	2.40	2.40
13.26	24.42	32.22	3.97	127.80	2.70	2.39	2.39
13.36	24.44	32.08	3.90	125.14	2.69	2.39	2.39
13.40	24.45	32.02	3.87	123.86	2.68	2.38	2.38
13.46	24.56	32.08	3.84	123.35	2.68	2.39	2.39
13.55	24.66	32.11	3.84	123.20	2.68	2.39	2.39
13.60	24.84	32.28	3.83	123.53	2.68	2.40	2.40
13.67	24.92	32.33	3.86	124.78	2.68	2.40	2.40
13.75	24.93	32.28	3.91	126.36	2.69	2.40	2.40
13.80	25.07	32.43	3.95	127.94	2.69	2.41	2.41
13.86	25.25	32.61	3.97	129.61	2.70	2.42	2.42
13.95	25.36	32.67	4.02	131.18	2.70	2.42	2.42
13.99	25.41	32.69	4.02	131.45	2.70	2.42	2.42
14.06	25.37	32.55	4.02	130.82	2.70	2.41	2.41
14.15	25.16	32.18	4.03	129.77	2.71	2.38	2.38
14.19	24.83	31.70	4.05	128.37	2.71	2.34	2.34
14.26	24.43	31.11	4.07	126.50	2.71	2.30	2.30
14.35	24.01	30.46	4.09	124.52	2.71	2.25	2.25
14.40	23.37	29.60	4.14	122.43	2.72	2.18	2.18
14.45	22.69	28.67	4.19	120.19	2.73	2.11	2.11
14.55	22.01	27.72	4.25	117.90	2.73	2.04	2.04
14.58	21.36	26.87	4.31	115.74	2.74	1.97	1.97
14.65	20.73	26.00	4.38	113.97	2.75	1.91	1.91
14.74	20.12	25.16	4.47	112.38	2.76	1.84	1.84
14.77	19.60	24.48	4.54	111.04	2.77	1.79	1.79
14.84	19.12	23.82	4.60	109.67	2.78	1.74	1.74
14.94	18.65	23.15	4.67	108.06	2.79	1.69	1.69
15.00	18.25	22.61	4.73	106.87	2.79	1.65	1.65
15.03	17.87	22.10	4.79	105.97	2.80	1.61	1.61
15.11	17.43	21.50	4.87	104.76	2.81	1.56	1.56
15.19	17.06	20.99	4.95	103.84	2.82	1.52	1.52
15.24	16.70	20.50	5.01	102.77	2.83	1.49	1.49
15.29	16.35	20.02	5.06	101.39	2.83	1.45	1.45
15.39	15.99	19.51	5.12	99.95	2.84	1.41	1.41
15.42	15.64	19.05	5.17	98.56	2.84	1.38	1.38
15.49	15.29	18.56	5.23	97.01	2.85	1.34	1.34
15.59	14.91	18.03	5.29	95.32	2.86	1.30	1.30
15.63	14.59	17.60	5.32	93.63	2.86	1.27	1.27
15.69	14.34	17.24	5.35	92.15	2.86	1.24	1.24
15.78	14.10	16.88	5.36	90.51	2.86	1.22	1.22

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
15.84	13.90	16.60	5.37	89.04	2.87	1.20	1.20
15.89	13.80	16.44	5.35	87.93	2.86	1.19	1.19
15.95	13.74	16.32	5.33	87.08	2.86	1.18	1.18
16.04	13.72	16.25	5.33	86.58	2.86	1.17	1.17
16.08	13.81	16.34	5.31	86.70	2.86	1.18	1.18
16.18	13.99	16.50	5.27	87.01	2.86	1.19	1.19
16.24	14.14	16.65	5.27	87.68	2.85	1.20	1.20
16.28	14.42	16.97	5.21	88.39	2.85	1.23	1.23
16.36	14.72	17.29	5.16	89.23	2.84	1.25	1.25
16.43	15.02	17.62	5.12	90.16	2.84	1.27	1.27
16.47	15.27	17.90	5.10	91.24	2.84	1.30	1.30
16.54	15.56	18.21	5.04	91.86	2.83	1.32	1.32
16.63	15.86	18.51	4.97	92.06	2.82	1.34	1.34
16.68	16.03	18.68	4.91	91.80	2.82	1.35	1.35
16.78	16.10	18.69	4.88	91.18	2.81	1.35	1.35
16.83	16.13	18.68	4.84	90.44	2.81	1.36	1.36
16.87	16.04	18.55	4.84	89.77	2.81	1.35	1.35
16.93	15.94	18.39	4.83	88.90	2.81	1.33	1.33
17.01	15.83	18.21	4.83	87.90	2.81	1.32	1.32
17.09	15.76	18.07	4.81	86.88	2.80	1.31	1.31
17.15	15.65	17.90	4.81	86.10	2.80	1.30	1.30
17.20	15.51	17.70	4.84	85.64	2.81	1.28	1.28
17.27	15.51	17.67	4.83	85.37	2.81	1.28	1.28
17.35	15.60	17.73	4.81	85.24	2.80	1.29	1.29
17.40	15.80	17.93	4.75	85.08	2.80	1.30	1.30
17.45	15.97	18.09	4.69	84.93	2.79	1.31	1.31
17.55	16.10	18.19	4.67	84.87	2.79	1.32	1.32
17.59	16.19	18.27	4.65	84.88	2.78	1.33	1.33
17.65	16.20	18.24	4.64	84.72	2.78	1.32	1.32
17.75	16.19	18.18	4.65	84.55	2.78	1.32	1.32
17.79	16.19	18.15	4.64	84.31	2.78	1.32	1.32
17.87	16.11	18.02	4.67	84.19	2.79	1.31	1.31
17.94	16.00	17.86	4.72	84.20	2.79	1.29	1.29
17.98	15.82	17.64	4.79	84.47	2.80	1.28	1.28
18.05	15.69	17.45	4.86	84.79	2.81	1.26	1.26
18.14	15.56	17.26	4.93	85.08	2.82	1.25	1.25
18.18	15.48	17.15	4.98	85.39	2.82	1.24	1.24
18.24	15.47	17.11	5.02	85.83	2.83	1.24	1.24
18.34	15.47	17.07	5.06	86.33	2.83	1.23	1.23
18.39	15.46	17.03	5.10	86.87	2.84	1.23	1.23
18.44	15.44	16.99	5.13	87.21	2.84	1.23	1.23
18.54	15.40	16.90	5.18	87.53	2.85	1.22	1.22
18.59	15.35	16.82	5.22	87.79	2.85	1.21	1.21
18.64	15.27	16.71	5.26	87.88	2.85	1.20	1.20
18.74	15.17	16.55	5.31	87.93	2.86	1.19	1.19
18.79	15.04	16.38	5.38	88.05	2.87	1.18	1.18
18.84	14.91	16.20	5.43	87.97	2.87	1.16	1.16
18.92	14.77	16.00	5.49	87.78	2.88	1.15	1.15

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
18.97	14.58	15.76	5.55	87.54	2.89	1.13	1.13
19.04	14.35	15.47	5.63	87.11	2.89	1.11	1.11
19.14	14.06	15.10	5.73	86.48	2.90	1.08	1.08
19.17	13.75	14.73	5.82	85.74	2.91	1.06	1.06
19.24	13.40	14.31	5.93	84.86	2.92	1.02	1.02
19.34	13.05	13.87	6.05	83.94	2.94	0.99	0.99
19.39	12.70	13.45	6.14	82.65	2.94	0.96	0.96
19.43	12.35	13.03	6.24	81.26	2.95	0.93	0.93
19.52	12.01	12.60	6.34	79.86	2.96	0.90	0.90
19.56	11.73	12.27	6.41	78.68	2.97	0.88	0.88
19.63	11.53	12.01	6.46	77.54	2.97	0.86	0.86
19.73	11.42	11.85	6.47	76.65	2.98	0.85	0.85
19.78	11.34	11.73	6.46	75.80	2.97	0.84	0.84
19.83	11.31	11.68	6.46	75.46	2.97	0.83	0.83
19.90	11.46	11.82	6.39	75.59	2.97	0.84	0.84
19.96	11.82	12.21	6.29	76.82	2.96	0.87	0.87
20.03	12.32	12.76	6.19	78.97	2.95	0.91	0.91
20.09	13.07	13.56	5.98	81.14	2.93	0.97	0.97
20.16	14.08	14.65	5.69	83.40	2.90	1.05	1.05
20.23	15.17	15.83	5.47	86.60	2.88	1.14	1.14
20.31	16.28	17.00	5.28	89.70	2.86	1.22	1.22
20.35	17.41	18.23	5.09	92.74	2.83	1.31	1.31
20.42	18.42	19.29	4.92	94.85	2.82	1.39	1.39
20.50	19.26	20.16	4.78	96.30	2.80	1.45	1.45
20.55	19.56	20.45	4.76	97.31	2.80	1.48	1.48
20.62	19.65	20.52	4.74	97.27	2.79	1.48	1.48
20.70	19.50	20.30	4.77	96.78	2.80	1.46	1.46
20.75	19.06	19.79	4.84	95.83	2.81	1.43	1.43
20.82	18.40	19.04	4.93	93.87	2.82	1.37	1.37
20.90	17.71	18.24	5.02	91.54	2.83	1.31	1.31
20.96	17.00	17.44	5.11	89.17	2.84	1.25	1.25
21.01	16.41	16.77	5.21	87.47	2.85	1.21	1.21
21.11	15.83	16.10	5.38	86.58	2.87	1.16	1.16
21.15	15.60	15.83	5.43	85.93	2.87	1.14	1.14
21.21	15.85	16.08	5.36	86.21	2.86	1.15	1.15
21.27	16.33	16.56	5.25	87.01	2.85	1.19	1.19
21.36	16.99	17.22	5.12	88.21	2.84	1.24	1.24
21.40	18.20	18.49	4.86	89.82	2.81	1.33	1.33
21.51	19.79	20.11	4.55	91.52	2.77	1.45	1.45
21.55	21.52	21.91	4.27	93.52	2.74	1.58	1.58
21.60	23.59	24.06	3.97	95.55	2.70	1.74	1.74
21.69	25.70	26.20	3.70	96.90	2.66	1.90	1.90
21.75	27.76	28.31	3.47	98.12	2.62	2.06	2.06
21.80	29.14	29.71	3.34	99.15	2.60	2.16	2.16
21.90	30.20	30.73	3.26	100.14	2.59	0.67	0.67
21.95	30.81	31.32	3.23	101.22	2.58	0.68	0.68
22.00	30.93	31.42	3.25	102.10	2.59	0.68	0.68
22.09	30.62	31.03	3.30	102.52	2.60	0.67	0.67

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
22.11	30.03	30.40	3.38	102.71	2.61	2.21	2.21
22.19	28.96	29.24	3.50	102.32	2.63	2.12	2.12
22.26	27.41	27.58	3.68	101.61	2.66	2.00	2.00
22.35	25.79	25.84	3.90	100.78	2.69	1.87	1.87
22.39	24.24	24.21	4.09	99.12	2.71	1.75	1.75
22.44	22.59	22.47	4.25	95.60	2.73	1.62	1.62
22.55	21.10	20.85	4.41	92.02	2.75	1.50	1.50
22.58	19.55	19.22	4.60	88.43	2.78	1.38	1.38
22.65	18.00	17.58	4.84	85.03	2.81	1.26	1.26
22.74	16.57	16.05	5.07	81.44	2.83	1.15	1.15
22.83	15.26	14.66	5.31	77.84	2.86	1.05	1.05
22.85	14.33	13.68	5.44	74.41	2.87	0.98	0.98
22.94	13.44	12.73	5.56	70.71	2.89	0.91	0.91
23.00	12.59	11.82	5.72	67.64	2.90	0.34	0.85
23.05	11.82	11.01	6.07	66.82	2.94	0.31	0.79
23.10	11.10	10.25	6.37	65.35	2.97	0.28	0.73
23.18	10.27	9.36	6.80	63.65	3.01	0.26	0.67
23.25	9.47	8.51	7.25	61.72	3.04	0.23	0.61
23.30	8.60	7.59	7.87	59.72	3.10	0.22	0.54
23.38	7.73	6.67	8.65	57.73	3.16	0.20	0.48
23.45	6.95	5.85	9.56	55.88	3.22	0.19	0.42
23.50	6.22	5.07	10.65	54.03	3.30	0.18	0.36
23.60	5.81	4.64	11.37	52.74	3.34	0.18	0.33
23.65	5.62	4.43	11.73	52.02	3.36	0.18	0.32
23.70	5.85	4.66	11.31	52.75	3.34	0.18	0.33
23.76	6.35	5.18	10.42	53.96	3.28	0.18	0.37
23.84	6.95	5.78	9.57	55.32	3.22	0.18	0.41
23.89	7.83	6.67	8.65	57.73	3.16	0.19	0.48
23.99	8.80	7.65	7.86	60.10	3.09	0.23	0.55
24.03	9.88	8.75	7.15	62.59	3.04	0.23	0.63
24.09	11.03	9.91	6.57	65.13	2.98	0.24	0.71
24.19	12.04	10.91	6.21	67.75	2.95	0.33	0.78
24.24	13.00	11.87	5.92	70.30	2.92	0.85	0.85
24.30	13.63	12.48	5.81	72.49	2.91	0.89	0.89
24.34	14.08	12.93	5.77	74.64	2.91	0.93	0.93
24.44	14.45	13.27	5.77	76.52	2.91	0.95	0.95
24.50	14.62	13.42	5.78	77.53	2.91	0.96	0.96
24.58	14.65	13.42	5.83	78.18	2.91	0.96	0.96
24.65	14.57	13.32	5.88	78.33	2.92	0.95	0.95
24.69	14.53	13.26	5.89	78.13	2.92	0.95	0.95
24.74	14.55	13.26	5.86	77.73	2.92	0.95	0.95
24.84	14.55	13.22	5.83	77.12	2.91	0.95	0.95
24.89	14.64	13.30	5.80	77.06	2.91	0.95	0.95
24.95	14.90	13.53	5.71	77.31	2.90	0.97	0.97
25.04	15.26	13.85	5.63	77.95	2.89	0.99	0.99
25.08	15.75	14.32	5.52	79.10	2.88	1.02	1.02
25.19	16.34	14.87	5.46	81.25	2.88	1.06	1.06
25.24	16.95	15.45	5.43	83.94	2.87	1.11	1.11

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
25.28	17.47	15.95	5.45	86.89	2.87	1.14	1.14
25.35	17.89	16.34	5.51	89.97	2.88	1.17	1.17
25.43	18.28	16.69	5.54	92.42	2.88	1.19	1.19
25.48	18.60	16.98	5.53	93.96	2.88	1.21	1.21
25.53	18.87	17.22	5.53	95.14	2.88	1.23	1.23
25.63	19.11	17.40	5.53	96.33	2.88	1.24	1.24
25.68	19.22	17.50	5.56	97.23	2.89	1.25	1.25
25.74	19.27	17.52	5.56	97.37	2.89	1.25	1.25
25.79	19.09	17.32	5.61	97.23	2.89	1.24	1.24
25.88	19.09	17.27	5.60	96.79	2.89	1.23	1.23
25.92	19.22	17.38	5.52	96.00	2.88	1.24	1.24
25.99	19.41	17.53	5.46	95.66	2.88	1.25	1.25
26.05	19.60	17.68	5.41	95.60	2.87	1.26	1.26
26.13	19.72	17.75	5.38	95.56	2.87	1.27	1.27
26.20	19.75	17.75	5.36	95.05	2.86	1.27	1.27
26.26	19.73	17.70	5.34	94.50	2.86	1.27	1.27
26.31	19.63	17.58	5.35	93.99	2.86	1.26	1.26
26.40	19.66	17.57	5.31	93.32	2.86	1.26	1.26
26.45	19.42	17.30	5.35	92.49	2.86	1.24	1.24
26.54	19.03	16.89	5.42	91.59	2.87	1.21	1.21
26.59	18.55	16.41	5.53	90.67	2.88	1.17	1.17
26.65	18.00	15.86	5.65	89.59	2.90	1.13	1.13
26.74	17.48	15.31	5.78	88.46	2.91	1.09	1.09
26.78	16.97	14.81	5.90	87.42	2.92	1.06	1.06
26.84	16.52	14.36	5.99	86.03	2.93	1.03	1.03
26.94	16.15	13.97	6.05	84.56	2.94	1.00	1.00
26.99	15.95	13.75	6.05	83.16	2.93	0.98	0.98
27.04	15.92	13.70	5.99	82.10	2.93	0.98	0.98
27.13	15.95	13.70	5.93	81.22	2.92	0.98	0.98
27.18	16.05	13.77	5.85	80.52	2.91	0.98	0.98
27.24	16.28	13.97	5.75	80.26	2.90	1.00	1.00
27.34	16.55	14.19	5.64	80.12	2.89	1.01	1.01
27.40	16.87	14.47	5.54	80.24	2.88	1.03	1.03
27.44	17.16	14.73	5.49	80.86	2.88	1.05	1.05
27.53	17.39	14.91	5.45	81.30	2.87	1.06	1.06
27.57	17.54	15.03	5.44	81.78	2.87	1.07	1.07
27.64	17.59	15.05	5.46	82.11	2.87	1.07	1.07
27.72	17.57	15.00	5.47	81.98	2.88	1.07	1.07
27.79	17.52	14.93	5.47	81.63	2.88	1.07	1.07
27.83	17.42	14.82	5.47	80.99	2.88	1.06	1.06
27.90	17.32	14.70	5.45	80.17	2.87	1.05	1.05
27.98	17.21	14.57	5.44	79.17	2.87	1.04	1.04
28.03	17.13	14.48	5.40	78.18	2.87	1.03	1.03
28.09	17.12	14.44	5.36	77.40	2.86	1.03	1.03
28.18	17.17	14.46	5.30	76.66	2.86	1.03	1.03
28.22	17.35	14.61	5.21	76.16	2.85	1.04	1.04
28.28	17.70	14.91	5.13	76.45	2.84	1.06	1.06
28.38	18.14	15.29	5.03	76.91	2.83	1.09	1.09

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
28.43	18.79	15.87	4.93	78.24	2.82	1.13	1.13
28.48	19.60	16.60	4.79	79.56	2.80	1.18	1.18
28.58	20.45	17.34	4.70	81.50	2.79	1.24	1.24
28.62	21.32	18.13	4.67	84.61	2.79	1.29	1.29
28.69	22.17	18.87	4.66	88.01	2.79	1.35	1.35
28.77	22.93	19.53	4.68	91.42	2.79	1.39	1.39
28.82	23.56	20.08	4.72	94.77	2.79	1.43	1.43
28.88	24.03	20.48	4.78	97.92	2.80	1.46	1.46
28.97	24.41	20.77	4.86	100.91	2.81	1.48	1.48
29.01	24.63	20.95	4.93	103.16	2.82	1.49	1.49
29.07	24.64	20.92	5.04	105.36	2.83	1.49	1.49
29.15	24.58	20.82	5.13	106.80	2.84	1.48	1.48
29.21	24.40	20.62	5.19	107.09	2.85	1.47	1.47
29.30	24.21	20.39	5.24	106.94	2.85	1.45	1.45
29.33	23.98	20.17	5.28	106.50	2.86	1.44	1.44
29.41	23.70	19.87	5.31	105.43	2.86	1.42	1.42
29.50	23.37	19.52	5.33	104.05	2.86	1.39	1.39
29.53	23.04	19.21	5.33	102.41	2.86	1.37	1.37
29.61	22.66	18.83	5.34	100.59	2.86	1.34	1.34
29.70	22.38	18.54	5.32	98.65	2.86	1.32	1.32
29.74	22.16	18.32	5.27	96.58	2.85	1.31	1.31
29.80	22.07	18.22	5.18	94.41	2.85	1.30	1.30
29.90	22.00	18.11	5.09	92.22	2.84	1.29	1.29
29.93	22.08	18.18	4.97	90.35	2.82	1.29	1.29
30.00	22.43	18.47	4.81	88.80	2.80	1.31	1.31
30.09	23.10	19.03	4.58	87.25	2.78	1.35	1.35
30.15	23.44	19.31	4.46	86.11	2.76	1.37	1.37
30.19	23.51	19.36	4.42	85.48	2.76	1.38	1.38
30.30	23.75	19.53	4.35	85.04	2.75	1.39	1.39
30.33	23.80	19.56	4.36	85.29	2.75	1.39	1.39
30.40	23.99	19.69	4.36	85.88	2.75	1.40	1.40
30.49	24.26	19.89	4.34	86.36	2.75	1.41	1.41
30.54	24.43	20.02	4.33	86.75	2.74	1.42	1.42
30.59	24.35	19.92	4.37	87.03	2.75	1.41	1.41
30.64	23.97	19.56	4.46	87.26	2.76	1.39	1.39
30.72	23.92	19.47	4.50	87.64	2.77	1.38	1.38
30.80	24.13	19.62	4.47	87.72	2.76	1.39	1.39
30.88	24.07	19.53	4.52	88.30	2.77	1.39	1.39
30.93	24.43	19.82	4.51	89.29	2.77	1.41	1.41
31.00	25.09	20.36	4.45	90.55	2.76	1.45	1.45
31.04	25.89	21.05	4.36	91.89	2.75	1.49	1.49
31.13	26.92	21.91	4.25	93.21	2.73	1.55	1.55
31.20	27.99	22.82	4.15	94.69	2.72	1.62	1.62
31.29	28.87	23.54	4.08	96.05	2.71	1.67	1.67
31.34	29.38	23.95	4.05	97.07	2.71	1.70	1.70
31.38	29.75	24.26	4.04	98.00	2.71	1.72	1.72
31.43	29.95	24.40	4.02	98.01	2.70	1.73	1.73
31.51	29.81	24.24	3.99	96.77	2.70	1.72	1.72

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
31.58	29.15	23.63	4.01	94.73	2.70	1.67	1.67
31.63	28.20	22.78	4.05	92.32	2.71	1.61	1.61
31.71	26.91	21.61	4.15	89.67	2.72	1.53	1.53
31.78	25.56	20.41	4.26	86.95	2.74	1.45	1.45
31.83	24.29	19.28	4.37	84.32	2.75	1.37	1.37
31.90	23.14	18.26	4.48	81.74	2.76	1.29	1.29
31.98	22.27	17.48	4.52	79.05	2.77	1.24	1.24
32.03	21.54	16.84	4.55	76.69	2.77	1.19	1.19
32.09	20.84	16.21	4.62	74.93	2.78	1.15	1.15
32.16	20.13	15.57	4.73	73.67	2.79	1.10	1.10
32.22	19.49	15.00	4.85	72.78	2.81	1.06	1.06
32.30	19.02	14.56	4.95	72.13	2.82	1.03	1.03
32.38	18.67	14.24	5.03	71.60	2.83	1.01	1.01
32.42	18.64	14.20	5.03	71.43	2.83	1.01	1.01
32.50	18.90	14.39	4.97	71.49	2.82	1.02	1.02
32.56	19.05	14.50	4.96	71.91	2.82	1.03	1.03
32.62	19.22	14.62	4.98	72.88	2.82	1.04	1.04
32.72	19.47	14.80	5.00	74.02	2.82	1.05	1.05
32.77	19.78	15.05	5.01	75.31	2.83	1.07	1.07
32.82	20.17	15.35	5.00	76.77	2.82	1.09	1.09
32.91	20.58	15.66	4.99	78.18	2.82	1.11	1.11
32.97	20.98	15.98	4.98	79.57	2.82	1.13	1.13
33.02	21.23	16.16	5.00	80.83	2.83	1.15	1.15
33.11	21.45	16.32	5.03	82.05	2.83	1.16	1.16
33.16	21.63	16.44	5.06	83.15	2.83	1.17	1.17
33.22	21.81	16.57	5.07	83.95	2.83	1.18	1.18
33.29	21.97	16.67	5.08	84.67	2.83	1.18	1.18
33.37	22.11	16.76	5.09	85.32	2.84	1.19	1.19
33.41	22.18	16.79	5.12	86.01	2.84	1.19	1.19
33.47	22.32	16.88	5.16	87.04	2.84	1.20	1.20
33.57	22.42	16.92	5.21	88.17	2.85	1.20	1.20
33.60	22.79	17.21	5.20	89.47	2.85	1.22	1.22
33.67	23.28	17.59	5.18	91.17	2.85	1.25	1.25
33.76	23.80	17.98	5.18	93.12	2.85	1.28	1.28
33.80	24.36	18.42	5.18	95.41	2.84	1.31	1.31
33.86	24.91	18.84	5.19	97.86	2.85	1.34	1.34
33.96	25.43	19.22	5.21	100.16	2.85	1.36	1.36
34.00	25.94	19.62	5.21	102.23	2.85	1.39	1.39
34.06	26.36	19.93	5.20	103.72	2.85	1.42	1.42
34.16	26.76	20.21	5.19	104.93	2.85	1.43	1.43
34.20	26.82	20.23	5.23	105.84	2.85	1.44	1.44
34.26	26.68	20.09	5.28	105.97	2.86	1.43	1.43
34.36	26.55	19.93	5.31	105.74	2.86	1.42	1.42
34.39	26.36	19.76	5.32	105.17	2.86	1.40	1.40
34.46	26.14	19.55	5.33	104.24	2.86	1.39	1.39
34.56	25.91	19.31	5.34	103.23	2.86	1.37	1.37
34.60	25.62	19.06	5.36	102.22	2.86	1.35	1.35
34.65	25.33	18.80	5.39	101.26	2.87	1.34	1.34

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
34.75	25.05	18.52	5.41	100.23	2.87	1.32	1.32
34.80	24.81	18.31	5.42	99.30	2.87	1.30	1.30
34.86	24.61	18.12	5.44	98.56	2.87	1.29	1.29
34.95	24.38	17.90	5.46	97.68	2.87	1.27	1.27
34.99	24.19	17.73	5.46	96.78	2.88	1.26	1.26
35.06	24.08	17.61	5.45	95.90	2.87	1.25	1.25
35.11	23.94	17.48	5.44	95.02	2.87	1.24	1.24
35.19	23.83	17.36	5.42	94.06	2.87	1.23	1.23
35.25	23.70	17.24	5.40	93.16	2.87	1.22	1.22
35.31	23.56	17.10	5.39	92.15	2.87	1.21	1.21
35.39	23.40	16.95	5.38	91.17	2.87	1.20	1.20
35.49	23.26	16.80	5.37	90.16	2.87	1.19	1.19
35.53	23.14	16.69	5.37	89.62	2.87	1.18	1.18
35.60	23.03	16.57	5.39	89.34	2.87	1.18	1.18
35.63	22.98	16.52	5.42	89.51	2.87	1.17	1.17
35.70	23.28	16.73	5.39	90.12	2.87	1.19	1.19
35.78	23.79	17.11	5.34	91.39	2.86	1.21	1.21
35.84	24.40	17.57	5.29	93.03	2.86	1.25	1.25
35.90	25.23	18.20	5.24	95.32	2.85	1.29	1.29
35.98	26.27	19.00	5.13	97.44	2.84	1.35	1.35
36.06	27.66	20.09	4.90	98.43	2.81	1.42	1.42
36.09	29.05	21.22	4.63	98.16	2.78	1.50	1.50
36.18	30.33	22.24	4.38	97.40	2.75	1.56	1.56
36.23	31.16	22.90	4.22	96.52	2.73	1.61	1.61
36.29	31.53	23.17	4.15	96.09	2.72	1.63	1.63
36.38	31.68	23.26	4.11	95.64	2.72	1.63	1.63
36.42	32.10	23.58	4.07	95.94	2.71	1.65	1.65
36.49	33.06	24.32	3.99	97.04	2.70	1.70	1.70
36.58	34.30	25.26	3.91	98.78	2.69	1.77	1.77
36.62	36.32	26.86	3.79	101.91	2.67	1.88	1.88
36.68	39.95	29.72	3.62	107.49	2.65	2.07	2.07
36.77	44.99	33.72	3.38	113.80	2.61	2.34	2.34
36.83	52.72	39.94	3.00	119.98	2.54	0.71	0.71
36.88	62.36	47.77	2.64	126.28	2.47	0.73	0.73
36.97	72.24	55.77	2.38	132.66	2.42	0.75	0.75
37.02	81.77	63.53	2.19	138.89	2.37	0.77	0.77
37.08	89.81	70.05	2.07	144.68	2.33	0.78	0.78
37.17	96.99	75.82	1.98	150.13	2.31	0.79	0.79
37.22	102.33	80.09	1.94	155.26	2.30	0.80	0.80
37.27	105.76	82.79	1.92	158.89	2.29	0.80	0.80
37.37	108.07	84.49	1.91	161.53	2.29	0.80	0.80
37.41	108.62	84.82	1.93	163.58	2.29	0.80	0.80
37.47	108.08	84.24	1.95	164.56	2.30	0.80	0.80
37.57	107.73	83.75	1.97	165.17	2.31	0.80	0.80
37.61	107.99	83.91	1.97	164.91	2.31	0.80	0.80
37.67	110.10	85.56	1.93	164.87	2.29	0.81	0.81
37.76	112.74	87.63	1.88	164.62	2.28	0.81	0.81
37.81	116.12	90.39	1.81	163.96	2.26	0.81	0.81

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
37.87	119.49	93.08	1.78	165.30	2.24	0.82	0.82
37.97	123.02	95.80	1.74	167.09	2.23	0.82	0.82
38.02	126.08	98.19	1.73	169.55	2.22	0.82	0.82
38.07	128.60	100.10	1.73	172.82	2.22	0.83	0.83
38.17	130.76	101.53	1.75	177.46	2.23	0.83	0.83
38.20	133.02	103.16	1.78	183.33	2.24	0.83	0.83
38.27	136.19	105.44	1.80	189.57	2.25	0.83	0.83
38.33	141.08	109.15	1.80	196.53	2.25	0.84	0.84
38.42	146.42	113.13	1.80	203.92	2.25	0.84	0.84
38.46	152.19	117.65	1.78	209.76	2.24	0.85	0.85
38.53	157.18	121.44	1.77	215.00	2.24	0.85	0.85
38.62	161.63	124.77	1.76	219.36	2.24	0.86	0.86
38.66	165.38	127.66	1.75	222.81	2.23	0.86	0.86
38.73	169.32	130.70	1.72	224.42	2.22	0.87	0.87
38.81	173.12	133.62	1.69	225.39	2.21	0.87	0.87
38.86	175.78	135.72	1.66	225.22	2.20	0.87	0.87
38.93	177.38	136.92	1.64	224.21	2.19	0.87	0.87
39.02	179.58	138.58	1.61	222.75	2.17	0.87	0.87
39.05	181.60	140.28	1.58	221.31	2.16	0.88	0.88
39.12	182.85	141.22	1.56	219.61	2.15	0.88	0.88
39.18	183.12	141.38	1.54	217.70	2.14	0.88	0.88
39.27	183.29	141.39	1.53	215.65	2.14	0.88	0.88
39.31	184.01	141.97	1.51	214.11	2.13	0.88	0.88
39.37	182.93	141.02	1.50	211.74	2.12	0.88	0.88
39.44	182.32	140.45	1.49	209.45	2.12	0.88	0.88
39.50	182.24	140.34	1.48	207.34	2.11	0.88	0.88
39.59	181.64	139.74	1.47	205.04	2.11	0.88	0.88
39.65	180.71	138.96	1.46	202.25	2.10	0.87	0.87
39.71	179.11	137.69	1.44	198.38	2.09	0.87	0.87
39.77	177.03	136.09	1.42	193.62	2.08	0.87	0.87
39.84	174.31	134.01	1.40	187.78	2.07	0.87	0.87
39.91	169.90	130.56	1.39	181.00	2.06	0.87	0.87
39.97	167.59	128.92	1.36	174.76	2.04	0.86	0.86
40.03	163.25	125.60	1.34	167.87	2.03	0.86	0.86
40.11	158.20	121.67	1.32	160.59	2.01	0.86	0.86
40.17	153.76	118.29	1.30	153.83	2.00	0.85	0.85
40.26	150.03	115.42	1.28	147.85	1.99	0.85	0.85
40.30	148.43	114.38	1.26	143.56	1.96	0.85	0.85
40.36	148.43	114.61	1.23	140.76	1.94	0.85	0.85
40.45	149.44	115.54	1.21	139.38	1.92	0.85	0.85
40.49	150.84	116.84	1.19	138.73	1.90	0.85	0.85
40.57	151.01	117.01	1.18	137.62	1.89	0.85	0.85
40.62	151.62	117.60	1.16	136.87	1.87	0.85	0.85
40.70	151.46	117.45	1.16	136.06	1.87	0.85	0.85
40.76	150.02	116.16	1.16	134.96	1.87	0.85	0.85
40.86	148.25	114.50	1.17	133.87	1.88	0.85	0.85
40.89	146.27	112.74	1.18	133.07	1.89	0.84	0.84
40.95	144.41	110.99	1.19	132.55	1.91	0.84	0.84

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
41.03	143.07	109.63	1.21	132.49	1.92	0.84	0.84
41.11	142.22	108.67	1.22	132.84	1.93	0.84	0.84
41.16	141.92	108.15	1.24	134.04	1.95	0.84	0.84
41.23	141.98	107.87	1.26	135.72	1.97	0.84	0.84
41.29	142.10	107.69	1.27	137.23	1.98	0.84	0.84
41.35	142.20	107.53	1.29	138.47	1.99	0.84	0.84
41.41	142.21	107.30	1.30	139.67	2.00	0.84	0.84
41.49	142.08	106.91	1.32	140.92	2.01	0.84	0.84
41.56	141.57	106.15	1.35	142.81	2.03	0.84	0.84
41.64	140.45	104.86	1.38	144.72	2.06	0.83	0.83
41.69	138.39	102.85	1.43	146.71	2.08	0.83	0.83
41.73	135.34	100.06	1.49	148.72	2.12	0.83	0.83
41.84	131.91	96.89	1.55	150.57	2.15	0.82	0.82
41.89	128.64	93.97	1.63	152.81	2.18	0.82	0.82
41.98	126.30	91.79	1.69	154.98	2.21	0.82	0.82
42.04	124.44	90.08	1.74	156.76	2.23	0.81	0.81
42.09	123.04	88.81	1.78	157.96	2.24	0.81	0.81
42.16	122.85	88.56	1.78	157.62	2.24	0.81	0.81
42.24	123.41	88.94	1.76	156.37	2.24	0.81	0.81
42.28	124.88	90.15	1.71	154.54	2.22	0.81	0.81
42.33	127.01	91.92	1.66	152.37	2.20	0.82	0.82
42.39	129.14	93.69	1.60	150.19	2.17	0.82	0.82
42.47	130.67	94.96	1.56	147.85	2.15	0.82	0.82
42.53	130.88	95.17	1.53	145.93	2.14	0.82	0.82
42.59	130.36	94.72	1.53	144.89	2.14	0.82	0.82
42.66	128.15	92.84	1.55	144.24	2.15	0.82	0.82
42.73	125.51	90.55	1.60	144.49	2.17	0.81	0.81
42.83	121.32	86.92	1.67	145.58	2.20	0.81	0.81
42.88	116.08	82.53	1.79	147.81	2.25	0.80	0.80
42.93	110.69	78.01	1.93	150.89	2.30	0.79	0.79
42.99	105.22	73.48	2.10	154.56	2.35	0.78	0.78
43.07	100.21	69.35	2.28	158.34	2.39	0.78	0.78
43.14	95.63	65.62	2.46	161.52	2.44	0.77	0.77
43.19	90.87	61.88	2.64	163.11	2.47	0.76	0.76
43.25	86.68	58.66	2.77	162.37	2.50	0.75	0.75
43.34	81.82	54.96	2.91	160.19	2.53	0.75	0.75
43.39	77.67	51.89	3.02	156.69	2.55	0.74	0.74
43.45	73.11	48.56	3.12	151.56	2.57	0.73	0.73
43.54	68.41	45.14	3.22	145.56	2.58	0.72	0.72
43.59	63.67	41.76	3.32	138.68	2.60	0.71	0.71
43.64	58.08	37.78	3.46	130.82	2.62	2.57	2.57
43.74	52.40	33.73	3.63	122.45	2.65	2.31	2.31
43.78	46.98	29.92	3.82	114.29	2.68	2.05	2.05
43.83	42.15	26.52	4.06	107.56	2.71	1.83	1.83
43.94	37.81	23.43	4.34	101.74	2.75	1.62	1.62
43.98	34.06	20.82	4.64	96.56	2.78	1.45	1.45
44.04	31.95	19.35	4.77	92.25	2.80	1.35	1.35
44.14	30.33	18.23	4.84	88.21	2.81	1.27	1.27

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
44.17	29.10	17.40	4.87	84.75	2.81	1.22	1.22
44.23	28.76	17.17	4.84	83.14	2.81	1.20	1.20
44.33	28.68	17.09	4.82	82.35	2.80	1.19	1.19
44.37	29.02	17.32	4.74	82.18	2.80	1.21	1.21
44.44	29.52	17.63	4.74	83.55	2.79	1.23	1.23
44.53	30.09	17.96	4.77	85.75	2.80	1.25	1.25
44.58	30.72	18.34	4.83	88.54	2.81	1.28	1.28
44.64	31.59	18.87	4.87	91.92	2.81	1.32	1.32
44.73	33.07	19.81	4.84	95.80	2.81	1.38	1.38
44.78	34.76	20.91	4.78	100.00	2.80	1.46	1.46
44.82	36.82	22.27	4.68	104.27	2.79	1.55	1.55
44.90	39.32	23.92	4.55	108.78	2.77	1.66	1.66
44.97	41.98	25.69	4.42	113.46	2.76	1.78	1.78
45.03	45.07	27.77	4.22	117.33	2.73	1.92	1.92
45.09	48.02	29.77	4.05	120.66	2.71	2.05	2.05
45.17	50.82	31.66	3.90	123.53	2.69	2.17	2.17
45.22	53.50	33.49	3.77	126.23	2.67	2.29	2.29
45.29	55.93	35.13	3.66	128.50	2.65	2.40	2.40
45.38	58.32	36.73	3.55	130.31	2.63	2.50	2.50
45.42	60.57	38.30	3.43	131.40	2.62	2.60	2.60
45.50	62.33	39.50	3.34	131.76	2.60	2.67	2.67
45.57	63.62	40.38	3.27	131.88	2.59	0.71	0.71
45.62	64.35	40.86	3.23	131.80	2.58	0.71	0.71
45.69	64.79	41.14	3.19	131.34	2.58	0.71	0.71
45.77	65.03	41.27	3.17	130.71	2.57	0.71	0.71
45.82	64.64	40.97	3.17	129.68	2.57	0.71	0.71
45.88	63.43	40.09	3.20	128.34	2.58	0.71	0.71
45.97	61.81	38.90	3.26	126.83	2.59	0.70	0.70
46.02	59.45	37.20	3.37	125.35	2.61	2.51	2.51
46.10	56.51	35.08	3.54	124.07	2.63	2.38	2.38
46.17	53.60	32.99	3.72	122.72	2.66	2.25	2.25
46.21	50.91	31.09	3.90	121.40	2.69	2.13	2.13
46.27	48.55	29.43	4.07	119.86	2.71	2.02	2.02
46.36	46.40	27.90	4.24	118.19	2.73	1.92	1.92
46.42	44.50	26.58	4.39	116.57	2.75	1.84	1.84
46.46	42.82	25.41	4.53	115.16	2.77	1.76	1.76
46.56	41.38	24.39	4.67	113.82	2.79	1.70	1.70
46.61	40.40	23.70	4.76	112.81	2.80	1.65	1.65
46.66	39.90	23.35	4.80	112.07	2.80	1.63	1.63
46.74	39.54	23.07	4.85	111.78	2.81	1.61	1.61
46.81	39.12	22.74	4.92	111.81	2.82	1.59	1.59
46.87	38.64	22.38	5.02	112.27	2.83	1.57	1.57
46.94	38.63	22.33	5.05	112.77	2.83	1.56	1.56
47.01	38.71	22.33	5.08	113.37	2.83	1.56	1.56
47.06	38.83	22.38	5.10	114.02	2.84	1.57	1.57
47.12	39.01	22.46	5.10	114.54	2.84	1.57	1.57
47.19	39.29	22.62	5.07	114.67	2.83	1.58	1.58
47.25	39.58	22.79	5.02	114.47	2.83	1.59	1.59

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
47.34	39.73	22.86	4.98	113.86	2.82	1.60	1.60
47.39	39.72	22.85	4.95	113.08	2.82	1.60	1.60
47.44	39.77	22.88	4.90	112.17	2.81	1.60	1.60
47.54	39.28	22.52	4.93	111.05	2.82	1.57	1.57
47.59	38.71	22.13	4.97	110.09	2.82	1.55	1.55
47.65	38.41	21.91	4.99	109.31	2.82	1.53	1.53
47.74	37.95	21.57	5.04	108.75	2.83	1.51	1.51
47.81	37.56	21.28	5.10	108.54	2.84	1.49	1.49
47.85	37.47	21.20	5.12	108.59	2.84	1.48	1.48
47.94	37.60	21.25	5.12	108.69	2.84	1.49	1.49
47.98	37.97	21.46	5.09	109.34	2.84	1.50	1.50
48.04	38.79	21.97	5.03	110.49	2.83	1.54	1.54
48.13	39.93	22.66	4.94	112.01	2.82	1.58	1.58
48.17	41.38	23.58	4.83	113.87	2.81	1.64	1.64
48.24	42.73	24.42	4.75	116.08	2.80	1.70	1.70
48.32	44.25	25.35	4.67	118.31	2.79	1.76	1.76
48.37	46.09	26.53	4.55	120.75	2.77	1.84	1.84
48.44	48.52	28.08	4.39	123.16	2.75	1.94	1.94
48.53	51.56	30.04	4.17	125.39	2.72	2.06	2.06
48.56	54.96	32.30	3.94	127.24	2.69	2.20	2.20
48.64	59.29	35.19	3.66	128.73	2.65	2.38	2.38
48.72	64.04	38.37	3.40	130.28	2.61	2.58	2.58
48.78	69.67	42.21	3.12	131.70	2.57	0.71	0.71
48.83	76.00	46.56	2.86	133.11	2.52	0.73	0.73
48.90	82.27	50.88	2.65	134.67	2.48	0.74	0.74
48.97	87.90	54.74	2.50	136.96	2.44	0.75	0.75
49.03	93.07	58.27	2.40	139.62	2.42	0.75	0.75
49.12	97.81	61.45	2.32	142.53	2.40	0.76	0.76
49.16	102.84	64.88	2.24	145.62	2.38	0.77	0.77
49.23	107.68	68.15	2.18	148.54	2.37	0.77	0.77
49.31	113.16	71.90	2.10	151.31	2.35	0.78	0.78
49.36	118.20	75.37	2.04	153.88	2.33	0.79	0.79
49.43	123.66	79.14	1.97	156.19	2.31	0.79	0.79
49.52	130.09	83.63	1.90	158.50	2.28	0.80	0.80
49.58	137.03	88.58	1.81	160.30	2.25	0.81	0.81
49.62	143.61	93.36	1.73	161.63	2.23	0.82	0.82
49.71	149.84	98.02	1.64	160.96	2.19	0.82	0.82
49.78	155.24	102.19	1.56	159.69	2.15	0.83	0.83
49.81	159.41	105.51	1.50	158.62	2.13	0.83	0.83
49.88	162.01	107.57	1.46	157.54	2.11	0.84	0.84
49.97	163.35	108.59	1.44	156.61	2.09	0.84	0.84
50.00	161.66	107.39	1.44	155.04	2.09	0.84	0.84
50.07	160.26	106.28	1.45	153.97	2.10	0.84	0.84
50.14	158.20	104.64	1.46	153.02	2.10	0.83	0.83
50.22	154.55	101.76	1.49	151.80	2.12	0.83	0.83
50.27	149.22	97.52	1.56	151.87	2.15	0.82	0.82
50.35	143.10	92.63	1.65	152.47	2.19	0.82	0.82
50.40	135.60	86.89	1.76	152.50	2.23	0.81	0.81

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
50.47	127.45	80.82	1.87	151.35	2.28	0.80	0.80
50.55	119.71	75.19	1.98	149.24	2.31	0.79	0.79
50.59	114.02	71.17	2.06	146.72	2.33	0.78	0.78
50.66	106.49	65.86	2.18	143.35	2.37	0.77	0.77
50.75	98.69	60.41	2.31	139.61	2.40	0.76	0.76
50.79	91.04	55.16	2.46	135.79	2.44	0.75	0.75
50.86	83.73	50.19	2.62	131.58	2.47	0.73	0.73
50.94	76.84	45.52	2.79	127.20	2.51	0.72	0.72
50.99	70.78	41.49	2.96	122.83	2.54	0.71	0.71
51.05	65.41	37.95	3.12	118.60	2.57	0.70	0.70
51.14	60.12	34.47	3.31	114.18	2.60	0.69	0.69
51.18	54.60	30.89	3.55	109.70	2.64	2.07	2.07
51.25	49.39	27.54	3.79	104.45	2.67	1.86	1.86
51.34	44.37	24.36	4.04	98.37	2.71	1.66	1.66
51.41	40.71	22.11	4.16	91.95	2.72	1.51	1.51
51.44	38.40	20.75	4.14	85.82	2.72	1.42	1.42
51.52	36.49	19.65	4.05	79.66	2.71	1.34	1.34
51.67	35.22	18.94	3.91	74.02	2.69	1.28	1.28
51.70	34.13	18.33	3.82	70.04	2.68	1.24	1.24
51.75	33.21	17.79	3.81	67.69	2.67	0.26	1.20
51.78	32.42	17.30	3.82	66.11	2.68	0.25	1.17
51.88	32.20	17.13	3.85	65.99	2.68	0.27	1.16
51.92	32.47	17.26	3.89	67.16	2.69	0.28	1.17
51.99	32.74	17.38	3.94	68.52	2.69	0.32	1.18
52.04	32.85	17.38	4.04	70.20	2.71	1.18	1.18
52.14	32.83	17.29	4.15	71.79	2.72	1.18	1.18
52.19	32.56	17.06	4.29	73.12	2.74	1.17	1.17
52.26	31.97	16.63	4.44	73.88	2.76	1.14	1.14
52.33	31.02	16.00	4.61	73.79	2.78	1.10	1.10
52.38	29.91	15.28	4.80	73.35	2.80	1.06	1.06
52.43	28.33	14.28	5.07	72.33	2.83	1.00	1.00
52.51	26.65	13.23	5.35	70.78	2.86	0.93	0.93
52.58	25.06	12.25	5.62	68.88	2.89	0.30	0.86
52.63	23.61	11.38	5.85	66.51	2.91	0.28	0.81
52.69	22.29	10.60	6.04	64.03	2.93	0.26	0.75
52.77	21.16	9.93	6.20	61.57	2.95	0.23	0.71
52.83	20.40	9.49	6.27	59.49	2.96	0.21	0.68
52.90	19.92	9.22	6.29	57.98	2.96	0.19	0.66
52.99	19.57	9.02	6.27	56.56	2.96	0.18	0.64
53.05	19.39	8.91	6.22	55.38	2.95	0.18	0.64
53.10	19.24	8.82	6.19	54.61	2.95	0.17	0.63
53.16	19.09	8.74	6.18	53.96	2.95	0.17	0.62
53.25	18.99	8.67	6.17	53.51	2.95	0.16	0.62
53.29	18.94	8.64	6.16	53.22	2.95	0.16	0.62
53.38	18.91	8.62	6.12	52.77	2.94	0.16	0.61
53.44	18.88	8.60	6.09	52.39	2.94	0.16	0.61
53.50	18.85	8.58	6.07	52.09	2.94	0.16	0.61
53.55	18.80	8.54	6.07	51.85	2.94	0.16	0.61

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
53.64	18.73	8.49	6.09	51.68	2.94	0.15	0.60
53.72	18.66	8.44	6.10	51.50	2.94	0.15	0.60
53.74	18.66	8.44	6.09	51.43	2.94	0.15	0.60
53.82	18.74	8.47	6.07	51.42	2.94	0.15	0.60
53.90	18.83	8.51	6.06	51.55	2.94	0.15	0.61
53.94	18.95	8.58	6.05	51.92	2.94	0.15	0.61
54.01	19.10	8.65	6.05	52.34	2.94	0.15	0.62
54.09	19.25	8.72	6.05	52.76	2.94	0.16	0.62
54.19	19.41	8.79	6.04	53.10	2.93	0.17	0.63
54.24	19.57	8.88	6.01	53.39	2.93	0.17	0.63
54.29	19.71	8.95	5.99	53.60	2.93	0.18	0.64
54.35	19.78	8.98	5.97	53.59	2.93	0.18	0.64
54.44	19.79	8.98	5.94	53.36	2.92	0.17	0.64
54.49	19.78	8.98	5.90	53.01	2.92	0.17	0.64
54.53	19.74	8.96	5.87	52.57	2.92	0.17	0.63
54.63	19.69	8.92	5.83	52.05	2.91	0.15	0.63
54.68	19.64	8.90	5.79	51.53	2.91	0.14	0.63
54.74	19.58	8.86	5.76	51.08	2.91	0.14	0.63
54.83	19.56	8.85	5.73	50.69	2.90	0.14	0.63
54.88	19.53	8.82	5.73	50.52	2.90	0.14	0.62
54.94	19.53	8.81	5.77	50.80	2.91	0.14	0.62
55.03	19.54	8.79	5.83	51.22	2.91	0.14	0.62
55.07	19.56	8.78	5.89	51.71	2.92	0.14	0.62
55.13	19.56	8.76	5.97	52.25	2.93	0.15	0.62
55.23	19.57	8.74	6.04	52.78	2.93	0.17	0.62
55.28	19.59	8.73	6.11	53.32	2.94	0.17	0.62
55.32	19.63	8.73	6.17	53.85	2.95	0.18	0.62
55.42	19.66	8.72	6.21	54.15	2.95	0.18	0.62
55.50	19.75	8.77	6.19	54.28	2.95	0.18	0.63
55.53	19.81	8.80	6.15	54.15	2.94	0.18	0.63
55.58	19.82	8.80	6.14	54.07	2.94	0.18	0.63
55.66	19.80	8.78	6.13	53.84	2.94	0.17	0.63
55.73	19.80	8.79	6.03	53.02	2.93	0.16	0.63
55.78	19.97	8.86	6.11	54.17	2.94	0.16	0.63
55.86	20.32	9.02	6.23	56.19	2.95	0.16	0.64
55.93	20.98	9.35	6.30	58.91	2.96	0.16	0.67
55.97	22.90	10.37	6.15	63.82	2.94	0.12	0.74
56.08	26.02	12.11	5.74	69.47	2.90	0.27	0.86
56.12	30.92	14.96	5.04	75.34	2.83	1.04	1.04
56.17	39.52	20.15	4.02	81.08	2.70	1.36	1.36
56.28	48.92	25.93	3.32	86.19	2.60	0.65	0.65
56.32	59.00	32.27	2.83	91.38	2.51	0.68	0.68
56.37	69.47	39.03	2.44	95.22	2.43	0.70	0.70
56.47	79.91	45.84	2.16	98.82	2.36	0.72	0.72
56.52	90.20	52.68	1.95	102.49	2.30	0.74	0.74
56.57	98.80	58.43	1.81	105.88	2.25	0.75	0.75
56.67	105.68	62.98	1.73	109.00	2.23	0.76	0.76
56.72	109.54	65.45	1.71	111.70	2.22	0.77	0.77

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
56.78	108.92	64.78	1.75	113.30	2.23	0.77	0.77
56.87	106.09	62.58	1.83	114.28	2.26	0.76	0.76
56.91	101.69	59.38	1.94	114.91	2.30	0.76	0.76
56.97	94.90	54.58	2.11	115.36	2.35	0.75	0.75
57.03	87.46	49.42	2.35	116.07	2.41	0.73	0.73
57.11	79.60	44.05	2.66	117.05	2.48	0.72	0.72
57.17	72.07	39.08	3.00	117.09	2.54	0.70	0.70
57.26	64.98	34.48	3.36	115.99	2.61	2.28	2.28
57.32	58.98	30.71	3.71	114.08	2.66	2.05	2.05
57.35	53.23	27.19	4.10	111.44	2.71	1.84	1.84
57.42	48.56	24.36	4.45	108.40	2.76	1.66	1.66
57.51	44.62	22.00	4.78	105.07	2.80	1.52	1.52
57.55	42.37	20.71	4.91	101.63	2.81	1.43	1.43
57.62	40.27	19.53	5.00	97.64	2.82	1.35	1.35
57.71	38.27	18.41	5.07	93.40	2.83	1.28	1.28
57.78	36.28	17.29	5.18	89.53	2.84	1.20	1.20
57.82	34.25	16.16	5.32	86.01	2.86	1.13	1.13
57.90	32.33	15.08	5.47	82.51	2.88	1.06	1.06
57.96	30.91	14.30	5.53	79.14	2.88	1.01	1.01
58.01	29.77	13.70	5.54	75.90	2.88	0.96	0.96
58.11	28.76	13.15	5.54	72.86	2.88	0.92	0.92
58.15	27.83	12.67	5.53	70.01	2.88	0.89	0.89
58.21	27.11	12.29	5.50	67.59	2.88	0.29	0.86
58.31	26.42	11.92	5.46	65.17	2.88	0.26	0.84
58.35	25.74	11.58	5.43	62.82	2.87	0.25	0.81
58.42	25.07	11.21	5.45	61.05	2.87	0.22	0.79
58.50	24.42	10.86	5.47	59.40	2.88	0.20	0.76
58.55	23.79	10.51	5.53	58.05	2.88	0.19	0.74
58.61	23.23	10.19	5.58	56.92	2.89	0.19	0.72
58.70	22.64	9.86	5.67	55.93	2.90	0.18	0.70
58.75	22.12	9.56	5.79	55.31	2.91	0.18	0.68
58.81	21.76	9.34	5.89	55.01	2.92	0.18	0.66
58.89	21.58	9.22	5.95	54.89	2.93	0.17	0.65
58.95	21.52	9.18	5.99	54.99	2.93	0.17	0.65
59.00	21.65	9.23	5.99	55.30	2.93	0.18	0.66
59.10	21.83	9.32	5.97	55.60	2.93	0.18	0.66
59.15	22.01	9.40	5.95	55.91	2.92	0.19	0.67
59.20	22.17	9.48	5.94	56.28	2.92	0.20	0.67
59.28	22.35	9.57	5.92	56.65	2.92	0.21	0.68
59.35	22.51	9.62	5.96	57.35	2.93	0.20	0.68
59.38	22.75	9.74	5.98	58.18	2.93	0.20	0.69
59.46	23.08	9.90	5.94	58.82	2.92	0.20	0.70
59.53	23.71	10.25	5.78	59.22	2.91	0.20	0.72
59.59	24.44	10.68	5.53	59.03	2.88	0.24	0.75
59.67	25.08	11.05	5.33	58.93	2.86	0.25	0.77
59.73	25.65	11.38	5.17	58.87	2.84	0.24	0.79
59.79	26.13	11.64	5.08	59.15	2.83	0.22	0.81
59.89	26.74	11.97	4.99	59.70	2.82	0.18	0.83

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
59.94	27.35	12.30	4.93	60.60	2.82	0.19	0.85
59.99	28.37	12.84	4.85	62.31	2.81	0.19	0.89
60.07	30.97	14.49	4.10	59.42	2.71	0.22	0.98
60.12	34.29	16.66	3.39	56.43	2.61	0.25	1.09
60.19	40.56	20.76	2.59	53.74	2.46	0.07	0.63
60.25	48.38	26.09	1.98	51.69	2.31	0.06	0.65
60.33	55.12	30.89	1.64	50.62	2.19	0.06	0.67
60.38	61.17	35.45	1.00	35.45	2.08	0.04	0.69
60.48	67.60	40.50	1.00	40.50	1.96	0.04	0.71
60.53	77.07	48.20	1.00	48.20	1.81	0.06	0.73
60.61	80.93	-1.00	1.00	-1.00	-1.00	N/A	N/A
60.63	82.24	-1.00	1.00	-1.00	-1.00	N/A	N/A

Abbreviations

q_t:	Total cone resistance
K_c:	Cone resistance correction factor due to fines
$Q_{tn,cs}$:	Adjusted and corrected cone resistance due to fines
I_c:	Soil behavior type index
$S_{u(liq)}/\sigma'_v$:	Calculated liquefied undrained strength ratio
$S_{u(peak)}/\sigma'_v$:	Calculated peak undrained strength ratio

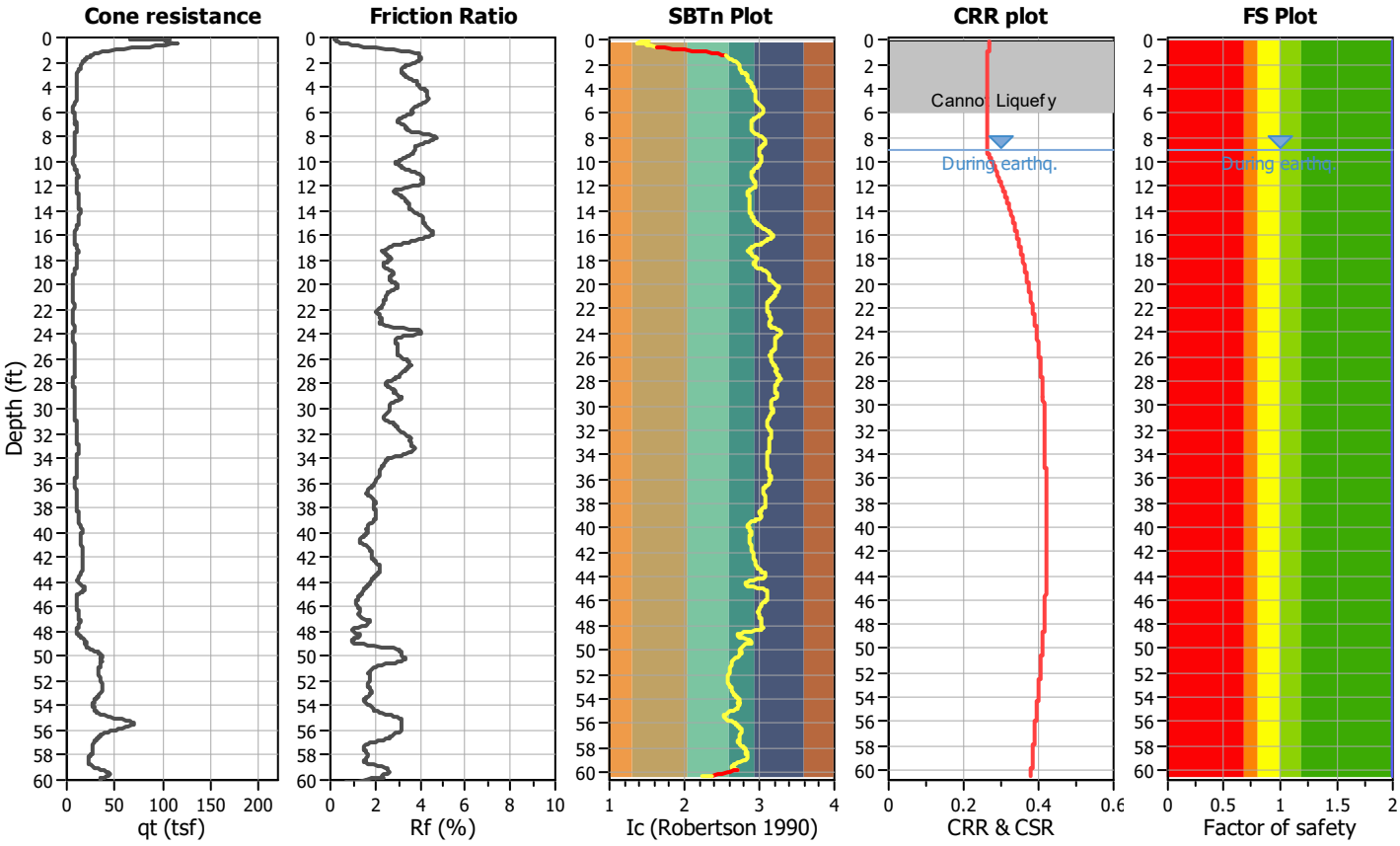
LIQUEFACTION ANALYSIS REPORT

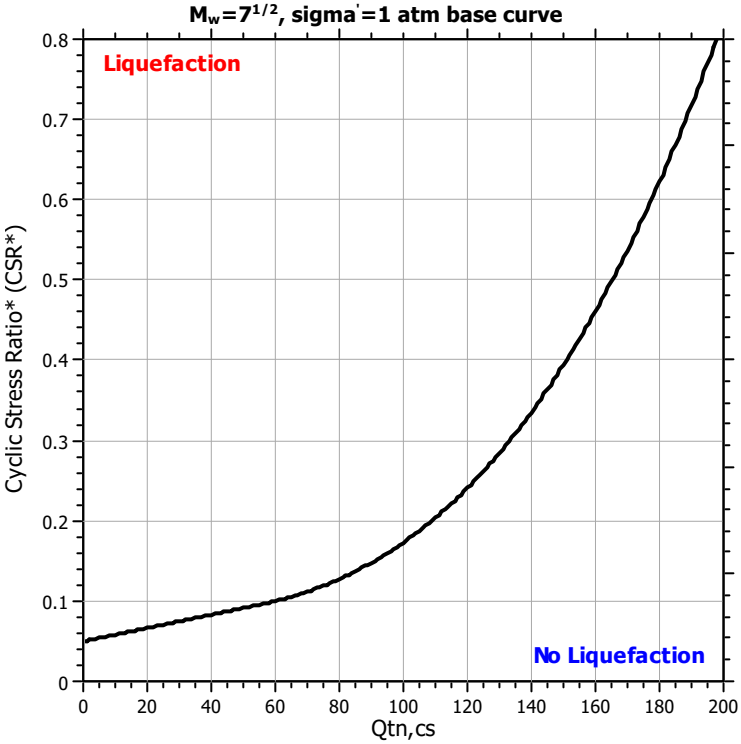
Project title : W1301-06-01 **Location : Perry Street**

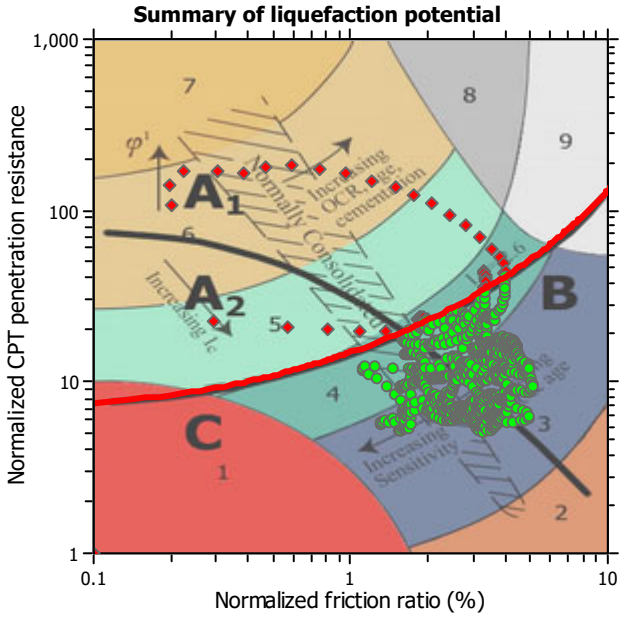
CPT file : CPT-4

Input parameters and analysis data

Analysis method:	NCEER (1998)	G.W.T. (in-situ):	12.00 ft	Use fill:	No	Clay like behavior applied:	Sands only
Fines correction method:	NCEER (1998)	G.W.T. (earthq.):	9.00 ft	Fill height:	N/A	Limit depth applied:	Yes
Points to test:	Based on Ic value	Average results interval:	.	Fill weight:	N/A	Limit depth:	50.00 ft
Earthquake magnitude M_w:	6.68	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	MSF method:	Method based
Peak ground acceleration:	0.55	Unit weight calculation:	Based on SBT	K_σ applied:	Yes		

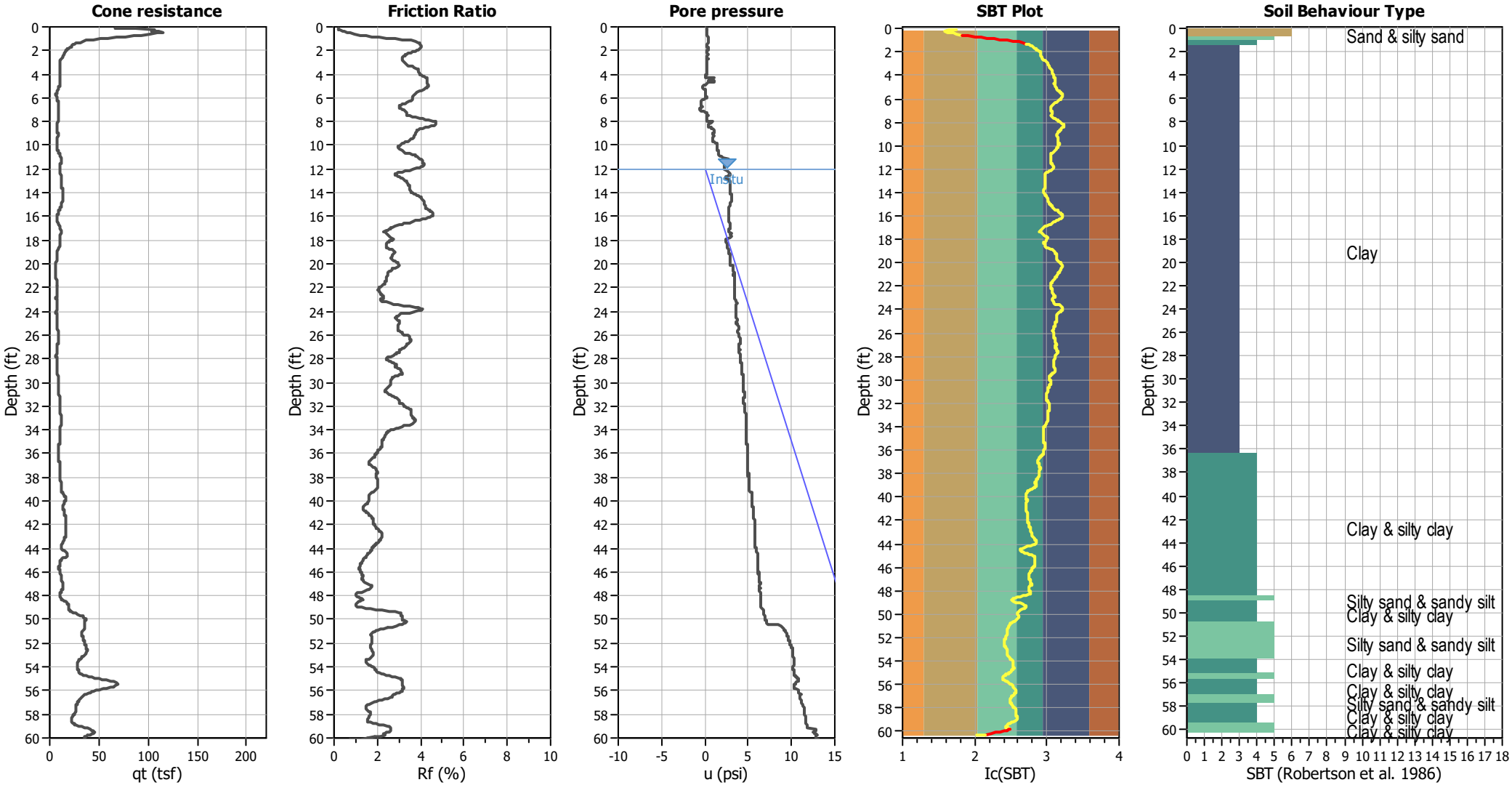






Zone A_1: Cyclic liquefaction likely depending on size and duration of cyclic loading
Zone A_2: Cyclic liquefaction and strength loss likely depending on loading and ground geometry
Zone B: Liquefaction and post-earthquake strength loss unlikely, check cyclic softening
Zone C: Cyclic liquefaction and strength loss possible depending on soil plasticity, brittleness/sensitivity, strain to peak undrained strength and ground geometry

CPT basic interpretation plots



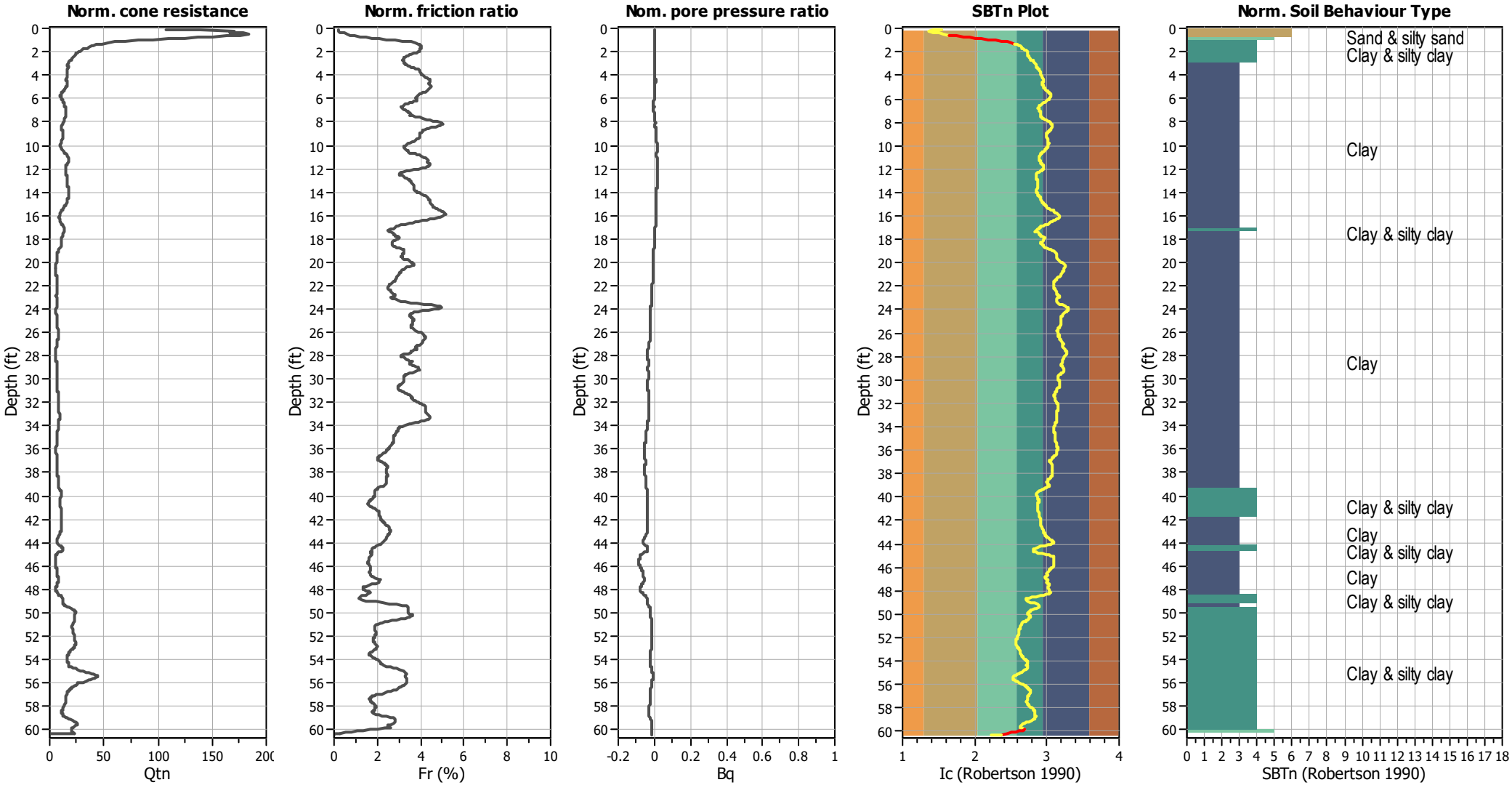
Input parameters and analysis data

Analysis method:	NCEER (1998)	Depth to water table (erthq.):	9.00 ft	Fill weight:	N/A
Fines correction method:	NCEER (1998)	Average results interval:	.	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.68	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.55	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	12.00 ft	Fill height:	N/A	Limit depth:	50.00 ft

SBT legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to
9. Very stiff fine grained

CPT basic interpretation plots (normalized)



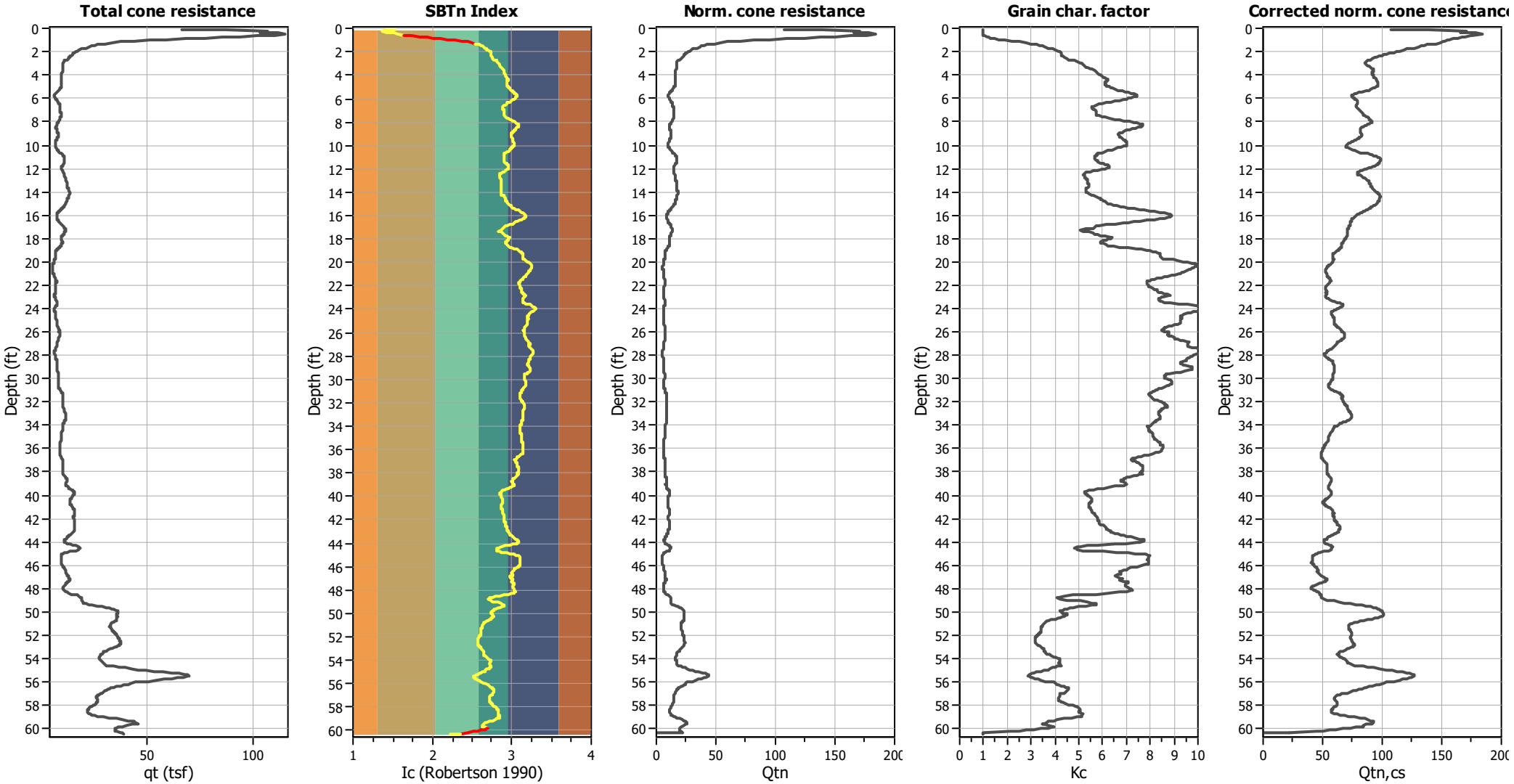
Input parameters and analysis data

Analysis method:	NCEER (1998)	Depth to water table (erthq.):	9.00 ft	Fill weight:	N/A
Fines correction method:	NCEER (1998)	Average results interval:	.	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.68	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.55	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	12.00 ft	Fill height:	N/A	Limit depth:	50.00 ft

SBTn legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to
9. Very stiff fine grained

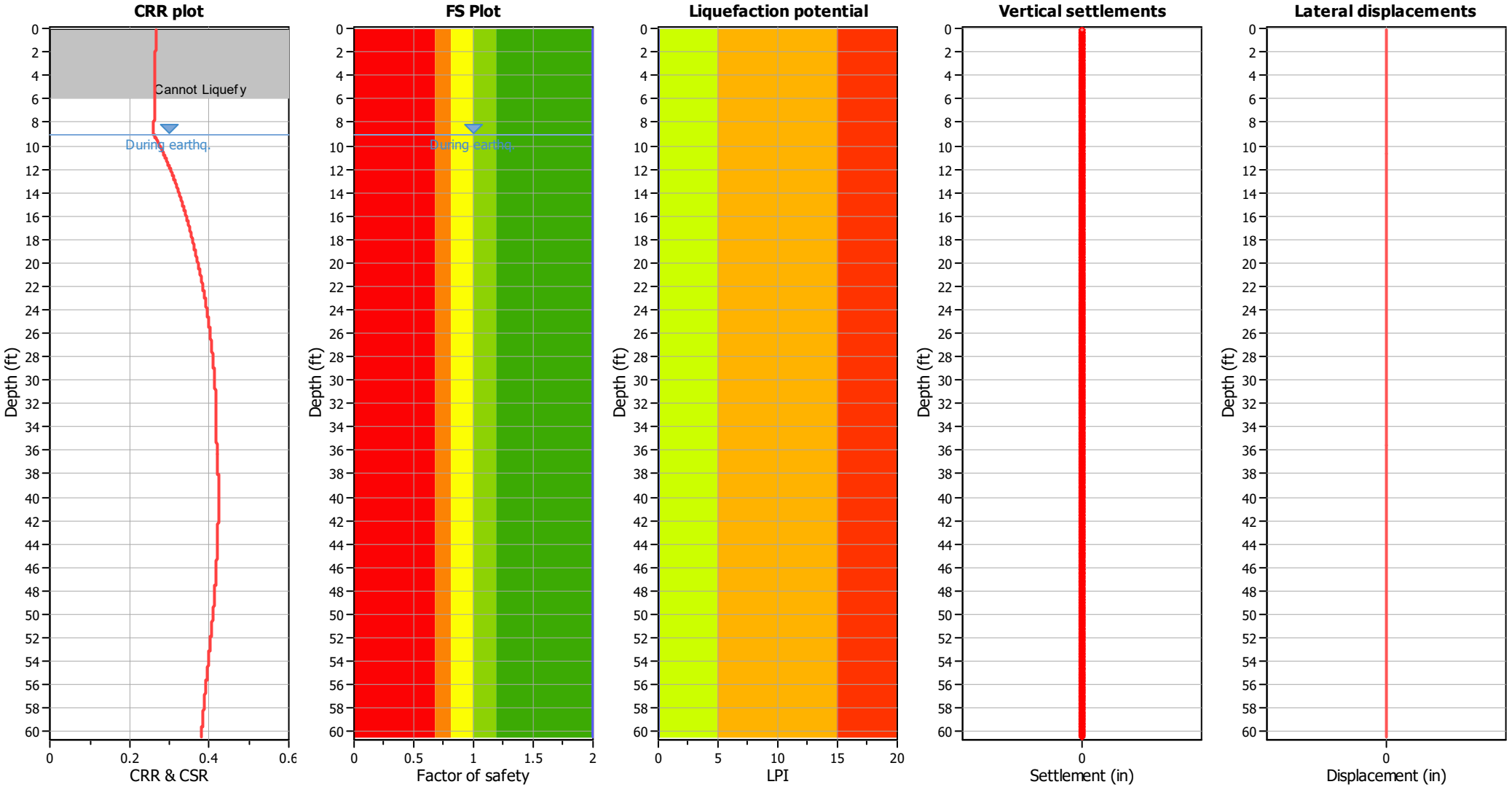
Liquefaction analysis overall plots (intermediate results)



Input parameters and analysis data

Analysis method:	NCEER (1998)	Depth to water table (erthq.):	9.00 ft	Fill weight:	N/A
Fines correction method:	NCEER (1998)	Average results interval:	.	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.68	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.55	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	12.00 ft	Fill height:	N/A	Limit depth:	50.00 ft

Liquefaction analysis overall plots



Input parameters and analysis data

Analysis method:	NCEER (1998)	Depth to water table (erthq.):	9.00 ft	Fill weight:	N/A
Fines correction method:	NCEER (1998)	Average results interval:	.	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.68	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.55	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	12.00 ft	Fill height:	N/A	Limit depth:	50.00 ft

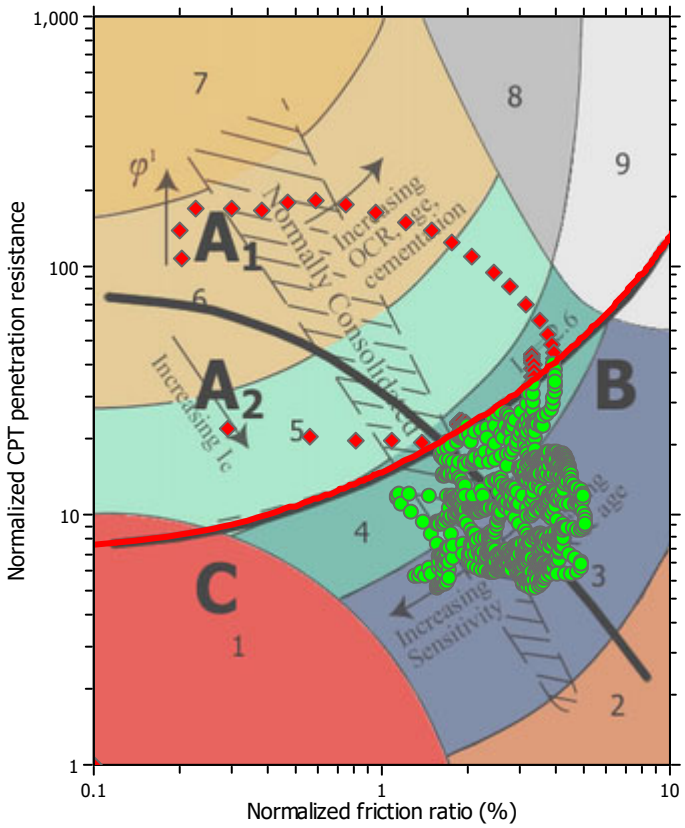
F.S. color scheme

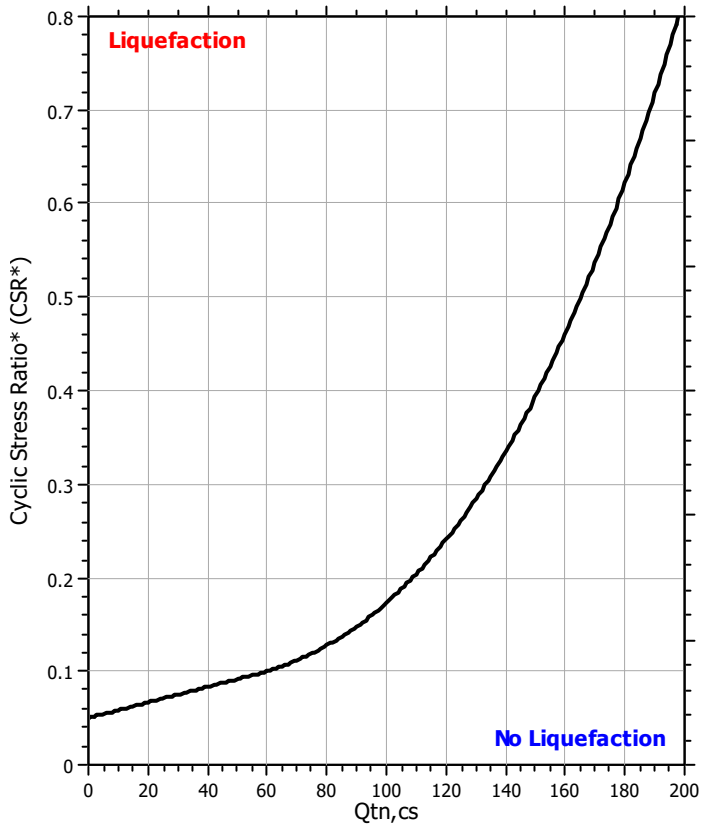
- Almost certain it will liquefy
- Very likely to liquefy
- Liquefaction and no liq. are equally likely
- Unlike to liquefy
- Almost certain it will not liquefy

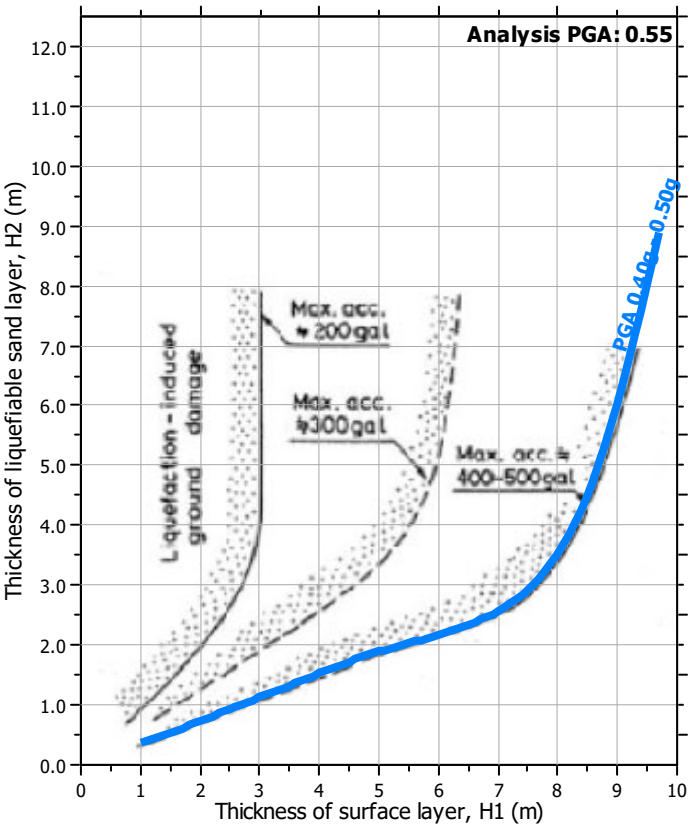
LPI color scheme

- Very high risk
- High risk
- Low risk

Liquefaction analysis summary plots



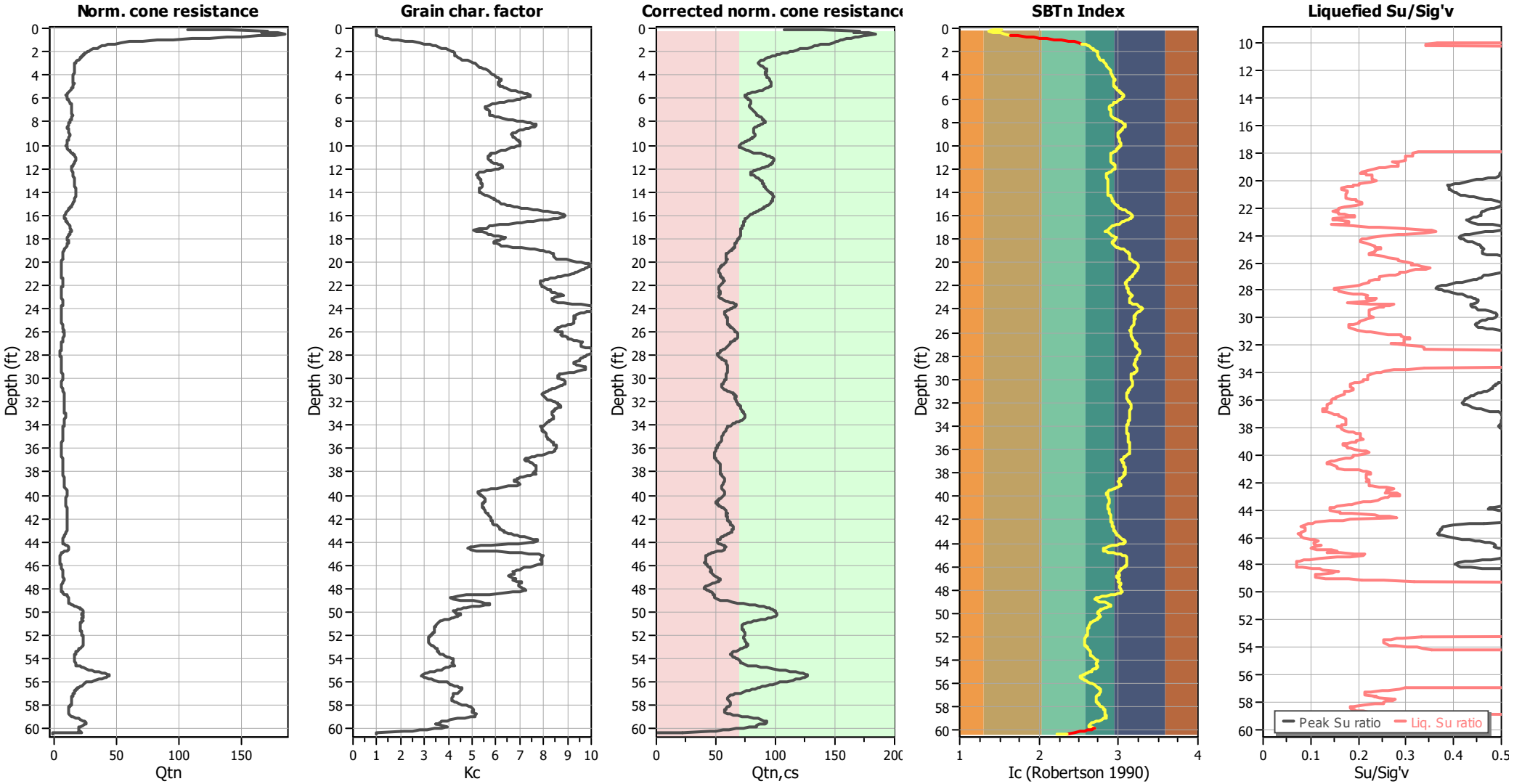




Input parameters and analysis data

Analysis method:	NCEER (1998)	Depth to water table (erthq.):	9.00 ft	Fill weight:	N/A
Fines correction method:	NCEER (1998)	Average results interval:	.	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.68	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.55	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	12.00 ft	Fill height:	N/A	Limit depth:	50.00 ft

Check for strength loss plots (Robertson (2010))



Input parameters and analysis data

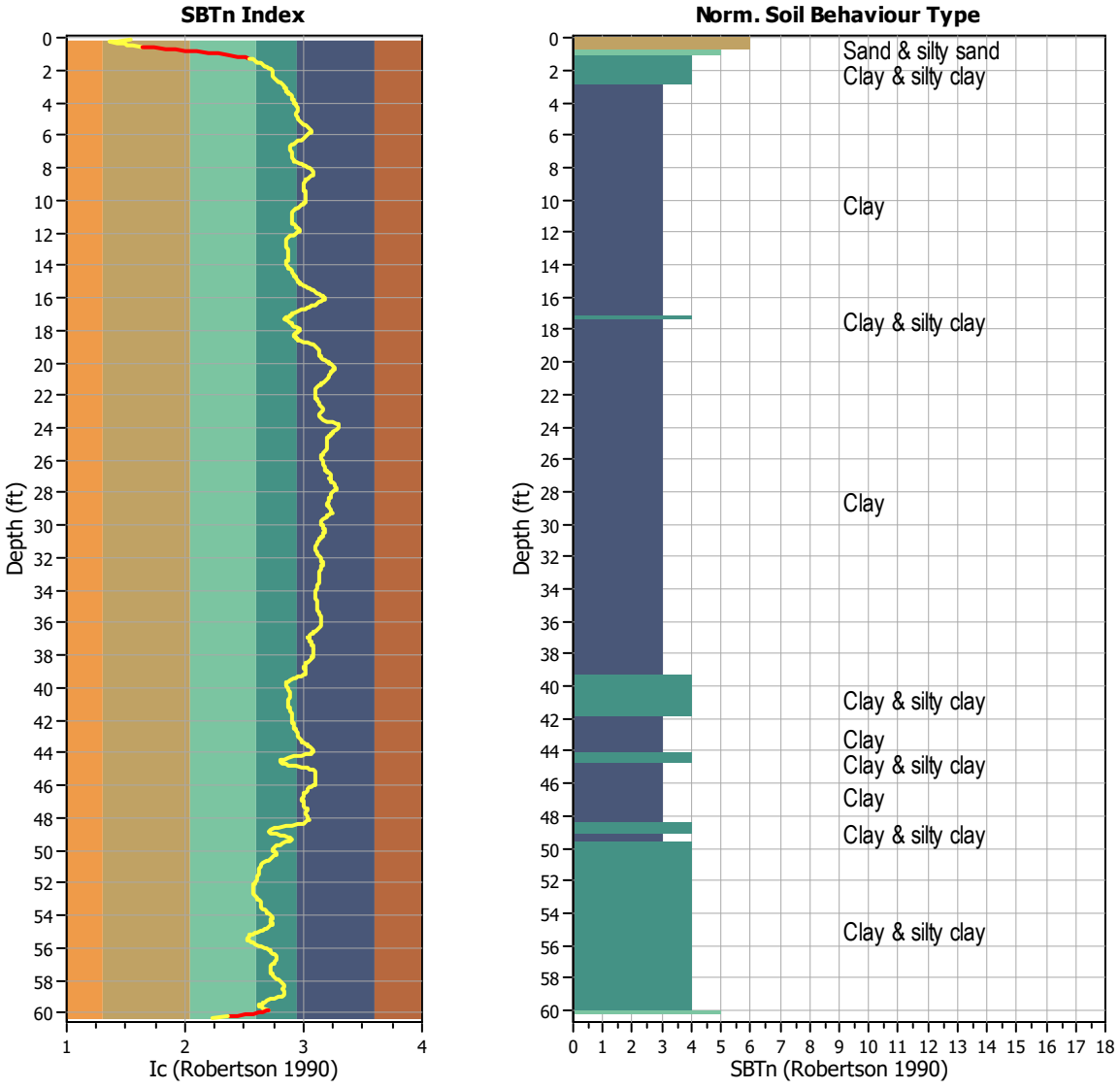
Analysis method:	NCEER (1998)	Depth to water table (erthq.):	9.00 ft	Fill weight:	N/A
Fines correction method:	NCEER (1998)	Average results interval:	.	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.68	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.55	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	12.00 ft	Fill height:	N/A	Limit depth:	50.00 ft

TRANSITION LAYER DETECTION ALGORITHM REPORT
Summary Details & Plots

Short description

The software will delete data when the cone is in transition from either clay to sand or vise-versa. To do this the software requires a range of I_c values over which the transition will be defined (typically somewhere between $1.80 < I_c < 3.0$) and a rate of change of I_c. Transitions typically occur when the rate of change of I_c is fast (i.e. delta I_c is small).

The SBT_n plot below, displays in red the detected transition layers based on the parameters listed below the graphs.



Transition layer algorithm properties	
I_c minimum check value:	1.70
I_c maximum check value:	3.00
I_c change ratio value:	0.0250
Minimum number of points in layer:	4

General statistics	
Total points in CPT file:	921
Total points excluded:	20
Exclusion percentage:	2.17%
Number of layers detected:	2

Transition layer No	Number of points	Depth	SBT_n number	SBT_n description
Transition layer 1	12	Start depth: 0.60 (ft)	6	Sand & silty sand
		End depth: 1.33 (ft)	4	Clay & silty clay
Transition layer 2	8	Start depth: 59.85 (ft)	4	Clay & silty clay
		End depth: 60.33 (ft)	5	Silty sand & sandy silt

Start depth: Depth where the transition layer begins
End depth: Depth where the transition layer ends

:: Field input data ::

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1	0.10	29.65	0.09	0.19	3.34	105.82
2	0.16	61.45	0.12	0.29	1.84	108.28
3	0.23	127.29	0.16	0.29	1.11	111.21
4	0.30	132.22	0.22	0.29	1.84	113.21
5	0.34	128.99	0.26	0.29	2.65	114.82
6	0.40	114.03	0.34	0.29	2.98	117.01
7	0.50	107.76	0.65	0.29	3.70	118.93
8	0.54	112.51	0.79	0.29	5.09	120.34
9	0.60	115.47	0.94	0.29	6.86	121.41
10	0.68	100.86	1.22	0.29	8.93	122.24
11	0.73	92.89	1.47	0.29	11.03	122.87
12	0.80	83.40	1.55	0.38	13.16	123.09
13	0.87	62.61	1.60	0.38	15.70	123.10
14	0.95	50.25	1.62	0.48	18.79	122.88
15	0.99	44.88	1.59	0.48	21.81	122.46
16	1.09	33.86	1.40	0.48	24.99	121.87
17	1.14	32.34	1.31	0.48	28.40	121.18
18	1.22	30.37	1.19	0.48	30.87	120.51
19	1.29	28.84	1.11	0.48	32.57	119.85
20	1.33	27.86	1.08	0.48	34.07	119.16
21	1.39	26.25	1.04	0.38	34.77	118.63
22	1.48	24.99	0.99	0.29	35.62	118.11
23	1.52	24.28	0.96	0.29	36.50	117.65
24	1.59	22.66	0.91	0.29	37.41	117.17
25	1.66	21.32	0.86	0.29	38.32	116.64
26	1.73	19.80	0.83	0.38	39.17	116.10
27	1.78	19.08	0.79	0.38	39.97	115.55
28	1.84	17.74	0.70	0.38	40.81	114.97
29	1.93	16.93	0.65	0.38	41.66	114.39
30	1.98	16.21	0.62	0.29	42.14	113.86
31	2.04	15.68	0.58	0.29	42.46	113.34
32	2.13	15.05	0.55	0.29	42.52	112.82
33	2.18	14.06	0.53	0.29	42.50	112.40
34	2.25	14.96	0.51	0.29	42.45	112.02
35	2.30	14.42	0.50	0.38	42.52	111.62
36	2.38	14.87	0.47	0.38	42.77	111.22
37	2.44	14.69	0.45	0.29	43.09	110.81
38	2.51	14.33	0.43	0.29	43.26	110.41
39	2.57	13.17	0.41	0.29	43.94	109.99
40	2.66	12.09	0.38	0.29	44.49	109.55
41	2.72	11.29	0.36	0.38	45.34	109.16
42	2.76	11.02	0.35	0.29	46.28	108.79
43	2.84	10.30	0.34	0.29	47.14	108.47
44	2.92	10.30	0.33	0.29	47.74	108.24
45	2.95	10.30	0.33	0.19	48.20	108.19
46	3.07	10.30	0.33	0.19	48.54	108.22
47	3.11	10.57	0.33	0.19	48.82	108.31
48	3.16	10.66	0.34	0.19	48.97	108.48

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
49	3.26	10.75	0.37	0.29	49.23	108.70
50	3.30	10.75	0.38	0.29	49.53	108.91
51	3.36	10.84	0.39	0.29	49.97	109.10
52	3.44	10.84	0.41	0.29	50.58	109.25
53	3.50	10.84	0.42	0.29	51.23	109.35
54	3.56	10.66	0.42	0.29	51.74	109.36
55	3.62	10.30	0.42	0.29	52.00	109.30
56	3.71	10.03	0.41	0.19	52.25	109.22
57	3.76	9.76	0.40	0.19	52.39	109.14
58	3.82	9.76	0.39	0.19	52.63	109.10
59	3.90	9.94	0.36	0.19	52.91	109.06
60	3.95	9.94	0.36	0.19	53.06	109.01
61	4.00	10.21	0.38	0.19	53.43	109.08
62	4.09	10.21	0.41	0.10	53.68	109.18
63	4.16	9.94	0.41	0.10	53.96	109.26
64	4.20	9.76	0.40	0.10	54.33	109.37
65	4.27	9.67	0.45	0.10	54.74	109.46
66	4.34	9.76	0.45	1.05	55.14	109.50
67	4.44	9.59	0.43	0.57	55.08	109.53
68	4.48	9.76	0.42	1.10	54.98	109.60
69	4.58	9.59	0.41	0.38	54.90	109.70
70	4.63	9.67	0.41	1.15	54.63	109.71
71	4.68	10.48	0.42	0.38	54.49	109.72
72	4.73	10.48	0.44	0.29	54.36	109.78
73	4.80	10.39	0.44	0.19	54.55	109.81
74	4.86	10.30	0.45	0.10	54.73	109.82
75	4.93	10.12	0.45	-0.10	55.03	109.76
76	5.00	10.12	0.45	-0.19	55.55	109.58
77	5.07	9.59	0.44	-0.19	55.88	109.29
78	5.12	9.32	0.42	-0.19	56.39	108.94
79	5.20	8.87	0.39	-0.19	56.99	108.52
80	5.27	8.69	0.35	-0.10	57.84	108.02
81	5.33	8.60	0.32	0.00	58.97	107.42
82	5.41	7.97	0.30	0.10	59.80	106.78
83	5.45	7.52	0.29	0.10	60.54	106.12
84	5.52	6.72	0.27	0.00	61.14	105.50
85	5.60	6.09	0.25	0.10	61.82	105.01
86	5.67	6.09	0.23	0.00	62.58	104.64
87	5.71	6.09	0.22	0.10	62.80	104.48
88	5.80	6.09	0.21	0.10	62.60	104.41
89	5.85	6.36	0.22	0.10	61.97	104.49
90	5.91	6.63	0.23	0.19	61.22	104.72
91	6.01	7.26	0.26	0.19	60.61	105.01
92	6.06	7.61	0.27	0.00	60.07	105.33
93	6.11	7.70	0.28	-0.10	59.27	105.65
94	6.18	7.70	0.30	-0.29	58.41	105.90
95	6.26	7.79	0.30	-0.38	57.20	106.10
96	6.30	7.79	0.30	-0.38	55.98	106.17

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
97	6.37	8.24	0.29	-0.38	54.94	106.20
98	6.45	8.42	0.28	-0.38	53.91	106.20
99	6.51	9.14	0.27	-0.38	52.89	106.16
100	6.60	9.41	0.26	-0.38	52.07	106.15
101	6.64	9.41	0.26	-0.38	51.35	106.16
102	6.70	9.41	0.26	-0.29	51.01	106.22
103	6.80	9.32	0.27	-0.38	50.88	106.33
104	6.83	9.23	0.28	-0.38	51.10	106.44
105	6.90	9.14	0.29	-0.57	51.51	106.58
106	6.98	9.14	0.30	-0.57	51.88	106.72
107	7.04	9.14	0.31	-0.57	52.15	106.86
108	7.09	9.23	0.31	-0.48	52.21	107.01
109	7.16	9.23	0.31	-0.10	52.22	107.16
110	7.24	9.32	0.31	0.10	52.30	107.33
111	7.30	9.50	0.31	0.29	52.32	107.45
112	7.39	9.85	0.32	0.29	52.17	107.46
113	7.43	9.85	0.33	0.38	52.25	107.51
114	7.50	9.76	0.35	0.29	52.85	107.73
115	7.59	9.59	0.34	0.29	53.58	107.94
116	7.63	9.50	0.31	0.29	54.43	108.12
117	7.70	9.32	0.33	0.29	55.80	108.23
118	7.78	9.05	0.40	0.29	57.16	108.30
119	7.83	8.87	0.40	0.29	58.10	108.32
120	7.89	8.78	0.40	0.29	59.28	108.36
121	7.95	7.88	0.39	0.29	60.66	108.43
122	8.02	7.88	0.39	0.96	61.91	108.41
123	8.11	8.33	0.38	0.67	62.77	108.20
124	8.16	7.88	0.38	0.48	63.48	107.93
125	8.21	7.70	0.37	0.38	64.10	107.65
126	8.30	7.44	0.35	0.38	64.12	107.38
127	8.36	7.08	0.33	0.38	64.01	107.12
128	8.41	6.99	0.31	0.38	63.81	106.84
129	8.47	6.99	0.30	0.67	63.16	106.59
130	8.56	6.99	0.29	0.77	62.39	106.39
131	8.61	7.17	0.29	0.86	61.65	106.31
132	8.70	7.70	0.28	1.05	60.82	106.29
133	8.75	7.88	0.28	1.05	60.14	106.36
134	8.81	8.06	0.29	1.05	59.50	106.46
135	8.90	8.15	0.31	1.05	58.83	106.56
136	8.94	8.15	0.31	0.96	58.27	106.65
137	9.01	8.15	0.32	0.96	58.05	106.73
138	9.09	8.24	0.32	0.96	58.04	106.79
139	9.13	8.33	0.31	0.96	58.11	106.79
140	9.20	8.33	0.31	1.05	58.15	106.69
141	9.27	8.33	0.30	0.96	58.38	106.56
142	9.35	8.15	0.30	0.96	58.60	106.36
143	9.39	7.97	0.29	0.96	58.84	106.09
144	9.45	7.79	0.28	0.96	59.14	105.81

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
145	9.54	7.35	0.27	0.96	59.38	105.50
146	9.59	7.17	0.26	0.96	59.68	105.20
147	9.65	6.99	0.24	0.96	59.79	104.87
148	9.73	6.99	0.23	1.15	59.95	104.52
149	9.81	6.99	0.22	1.25	60.11	104.15
150	9.85	6.99	0.22	1.34	60.07	103.82
151	9.94	6.99	0.21	1.34	60.00	103.53
152	10.00	6.72	0.20	1.34	59.95	103.31
153	10.04	6.54	0.19	1.34	59.65	103.15
154	10.12	6.45	0.19	1.34	59.22	103.17
155	10.19	6.45	0.19	1.44	58.65	103.39
156	10.24	6.45	0.19	1.44	58.01	103.77
157	10.31	6.90	0.19	1.44	57.26	104.40
158	10.39	7.61	0.22	1.44	56.50	105.02
159	10.48	8.33	0.26	1.53	55.39	105.60
160	10.53	8.96	0.29	1.53	54.38	106.20
161	10.63	9.67	0.34	1.53	53.60	106.88
162	10.67	9.67	0.34	1.53	53.01	107.63
163	10.71	10.12	0.33	1.53	52.52	108.25
164	10.79	10.30	0.35	1.53	52.29	108.78
165	10.83	10.48	0.39	1.53	52.47	109.18
166	10.93	11.02	0.43	1.73	52.10	109.48
167	10.98	11.29	0.44	1.92	51.74	109.79
168	11.06	11.20	0.46	2.11	51.77	110.12
169	11.11	10.48	0.46	2.68	51.83	110.38
170	11.16	11.91	0.46	2.49	51.85	110.55
171	11.23	12.00	0.47	2.40	51.99	110.60
172	11.31	11.73	0.48	2.40	52.29	110.61
173	11.36	11.56	0.48	2.40	52.54	110.56
174	11.42	11.29	0.47	2.40	52.58	110.50
175	11.51	11.02	0.46	2.40	53.28	110.41
176	11.56	10.84	0.45	2.40	53.98	110.25
177	11.65	10.57	0.44	2.40	54.66	110.05
178	11.71	10.39	0.43	2.30	55.10	109.84
179	11.75	10.21	0.43	2.30	55.61	109.62
180	11.84	9.85	0.41	2.30	55.81	109.37
181	11.89	9.67	0.40	2.30	55.80	109.10
182	11.96	9.85	0.39	2.30	55.36	108.80
183	12.03	9.41	0.38	2.30	54.70	108.50
184	12.11	9.85	0.35	2.59	53.82	108.17
185	12.16	9.85	0.33	2.59	52.78	107.91
186	12.21	10.30	0.30	2.68	51.59	107.71
187	12.30	10.57	0.29	2.78	50.55	107.55
188	12.35	10.66	0.28	2.88	49.49	107.47
189	12.41	10.93	0.29	2.97	48.97	107.51
190	12.49	11.38	0.30	2.97	48.68	107.65
191	12.56	11.56	0.31	2.68	48.76	107.89
192	12.60	11.56	0.33	2.59	48.93	108.16

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
193	12.67	11.38	0.35	2.40	49.11	108.45
194	12.75	11.38	0.37	2.40	49.18	108.71
195	12.80	11.38	0.38	2.49	49.27	108.96
196	12.90	11.56	0.39	2.68	49.53	109.20
197	12.95	11.82	0.39	2.78	49.69	109.41
198	13.02	12.27	0.39	2.97	49.78	109.59
199	13.06	12.54	0.40	2.97	49.77	109.74
200	13.14	12.36	0.41	2.88	49.77	109.85
201	13.19	12.36	0.42	2.88	49.77	109.95
202	13.29	12.27	0.43	2.88	49.89	110.03
203	13.33	12.27	0.43	2.88	50.12	110.11
204	13.39	12.18	0.43	2.97	50.31	110.14
205	13.48	12.18	0.43	2.97	50.39	110.16
206	13.54	12.18	0.43	2.97	50.36	110.25
207	13.59	12.18	0.43	2.97	50.18	110.38
208	13.67	12.36	0.42	2.97	49.84	110.53
209	13.72	12.45	0.42	2.97	49.54	110.70
210	13.78	13.08	0.46	2.97	49.44	110.87
211	13.86	13.53	0.48	2.97	49.39	111.05
212	13.93	14.24	0.49	2.97	49.37	111.26
213	14.01	14.06	0.50	2.97	49.52	111.46
214	14.05	13.62	0.51	2.97	49.75	111.65
215	14.14	13.62	0.52	3.07	50.06	111.76
216	14.21	13.62	0.53	3.16	50.43	111.83
217	14.24	13.35	0.53	3.16	51.04	111.87
218	14.31	13.08	0.53	3.07	51.60	111.89
219	14.39	13.08	0.53	3.16	52.03	111.90
220	14.44	13.08	0.53	3.07	52.39	111.88
221	14.54	12.81	0.53	3.16	52.83	111.84
222	14.59	12.81	0.53	3.07	53.18	111.80
223	14.64	12.72	0.53	3.07	53.43	111.75
224	14.70	12.63	0.52	3.07	53.76	111.70
225	14.79	12.45	0.52	2.97	54.14	111.63
226	14.83	12.36	0.52	2.97	54.44	111.52
227	14.93	12.27	0.51	2.88	54.89	111.37
228	14.98	12.09	0.51	2.88	55.41	111.22
229	15.03	11.91	0.50	2.88	56.11	111.03
230	15.10	11.56	0.48	2.88	56.82	110.84
231	15.18	11.11	0.46	2.78	57.64	110.62
232	15.23	10.75	0.46	2.78	58.49	110.38
233	15.33	10.21	0.44	2.78	59.39	110.13
234	15.37	10.12	0.44	2.78	60.50	109.89
235	15.44	9.76	0.43	2.78	61.75	109.63
236	15.52	9.50	0.41	2.78	63.18	109.39
237	15.56	9.41	0.41	2.68	64.40	109.11
238	15.63	8.87	0.41	2.68	65.66	108.84
239	15.71	8.42	0.39	2.68	67.00	108.54
240	15.77	7.88	0.38	2.68	68.16	108.25

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
241	15.82	7.79	0.36	2.68	69.24	107.98
242	15.89	7.44	0.35	2.68	70.21	107.68
243	15.97	7.26	0.34	2.68	70.74	107.37
244	16.02	7.26	0.33	2.68	71.03	107.12
245	16.10	7.26	0.32	2.68	70.87	106.90
246	16.17	7.35	0.31	2.68	70.46	106.73
247	16.22	7.35	0.30	2.68	69.47	106.57
248	16.28	7.35	0.30	2.68	68.23	106.45
249	16.37	7.52	0.30	2.78	66.74	106.40
250	16.42	7.79	0.29	2.78	65.09	106.39
251	16.52	8.15	0.28	2.88	63.50	106.38
252	16.55	8.42	0.28	2.88	61.98	106.40
253	16.62	9.05	0.29	2.88	60.56	106.41
254	16.70	9.41	0.29	2.88	59.38	106.45
255	16.74	9.59	0.28	2.88	57.33	106.56
256	16.82	9.59	0.28	2.88	54.73	106.74
257	16.91	9.59	0.28	2.88	53.15	106.84
258	16.94	9.59	0.29	2.88	52.31	106.83
259	17.01	11.65	0.29	2.88	51.70	106.81
260	17.10	13.71	0.29	2.78	51.25	106.81
261	17.15	12.18	0.28	2.78	50.77	106.81
262	17.21	10.84	0.27	2.78	49.37	106.86
263	17.30	10.75	0.27	2.78	48.04	106.89
264	17.34	10.75	0.27	2.78	48.52	106.79
265	17.41	10.75	0.27	3.07	50.20	106.65
266	17.49	13.26	0.27	2.97	51.27	106.59
267	17.53	13.17	0.27	2.97	51.40	106.62
268	17.59	10.03	0.27	2.97	51.86	106.56
269	17.67	9.14	0.28	3.07	52.56	106.49
270	17.73	9.59	0.28	3.16	53.18	106.39
271	17.79	10.75	0.28	2.88	54.62	106.23
272	17.87	9.59	0.26	2.40	56.15	106.08
273	17.92	9.05	0.26	2.40	56.38	106.00
274	17.99	9.14	0.25	2.49	56.03	105.88
275	18.07	9.85	0.25	2.49	55.16	105.79
276	18.14	9.85	0.25	2.49	54.99	105.66
277	18.19	9.41	0.25	2.49	54.18	105.64
278	18.26	9.41	0.24	2.59	53.41	105.61
279	18.34	10.93	0.24	2.59	53.37	105.54
280	18.38	10.66	0.24	2.59	53.77	105.41
281	18.45	11.11	0.24	2.59	54.26	105.31
282	18.53	10.57	0.24	2.59	54.74	105.21
283	18.60	9.05	0.23	2.59	55.33	105.14
284	18.68	8.60	0.22	2.59	56.82	105.02
285	18.72	8.60	0.23	2.68	58.39	104.86
286	18.79	8.24	0.23	2.68	60.49	104.63
287	18.84	8.15	0.23	2.68	62.50	104.37
288	18.92	8.06	0.23	2.68	63.88	104.14

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
289	18.98	7.61	0.22	2.68	65.00	103.92
290	19.06	7.26	0.21	2.78	66.00	103.62
291	19.11	6.99	0.20	2.78	66.65	103.32
292	19.18	6.63	0.19	2.88	67.28	103.02
293	19.25	6.63	0.18	2.88	67.94	102.75
294	19.33	6.63	0.17	2.88	68.28	102.54
295	19.37	6.72	0.17	2.88	68.26	102.45
296	19.47	6.72	0.17	2.88	68.34	102.40
297	19.52	6.72	0.18	2.88	68.15	102.41
298	19.57	6.81	0.18	2.88	68.16	102.46
299	19.62	7.08	0.19	2.88	68.51	102.55
300	19.71	6.90	0.19	2.97	69.05	102.63
301	19.77	6.90	0.19	2.97	69.99	102.73
302	19.82	6.81	0.19	2.97	71.46	102.72
303	19.91	6.54	0.19	2.97	72.47	102.63
304	19.96	6.45	0.19	2.97	73.62	102.49
305	20.02	6.09	0.20	2.97	74.65	102.35
306	20.11	5.29	0.19	2.97	75.64	102.16
307	20.18	5.73	0.17	3.26	76.64	101.97
308	20.23	5.73	0.17	3.26	77.23	101.75
309	20.28	5.73	0.17	3.26	77.59	101.47
310	20.37	5.73	0.16	3.26	77.34	101.16
311	20.42	5.64	0.16	3.26	76.33	100.92
312	20.48	5.64	0.15	3.26	76.23	100.81
313	20.56	5.64	0.14	3.26	75.95	100.70
314	20.63	5.73	0.14	3.26	75.55	100.61
315	20.67	5.64	0.14	3.26	75.05	100.57
316	20.74	5.64	0.15	3.35	74.39	100.54
317	20.83	5.82	0.15	3.26	73.89	100.56
318	20.90	5.91	0.15	3.35	73.52	100.64
319	20.97	6.09	0.15	3.26	73.26	100.72
320	21.02	6.18	0.15	3.35	72.69	100.80
321	21.10	6.18	0.15	3.35	71.89	100.90
322	21.17	6.18	0.15	3.35	71.06	101.06
323	21.22	6.18	0.15	3.35	70.16	101.22
324	21.27	6.36	0.15	3.35	69.33	101.43
325	21.37	6.63	0.16	3.35	68.59	101.63
326	21.43	6.99	0.17	3.35	67.76	101.84
327	21.46	7.17	0.17	3.35	67.01	102.04
328	21.55	7.44	0.18	3.35	66.23	102.18
329	21.62	7.52	0.18	3.35	65.66	102.32
330	21.66	7.61	0.18	3.35	65.17	102.29
331	21.74	7.52	0.18	3.35	64.99	102.14
332	21.81	7.52	0.17	3.35	65.00	101.99
333	21.85	7.44	0.17	3.35	65.08	101.76
334	21.93	7.17	0.15	3.35	65.21	101.48
335	22.00	6.90	0.14	3.35	65.31	101.18
336	22.07	6.81	0.14	3.35	65.39	100.94

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
337	22.16	6.81	0.14	3.35	65.68	100.74
338	22.19	6.72	0.13	3.35	65.98	100.60
339	22.26	6.81	0.13	3.45	66.48	100.64
340	22.33	6.90	0.14	3.45	67.02	100.81
341	22.40	6.81	0.14	3.45	67.47	100.98
342	22.45	6.81	0.15	3.45	67.61	101.09
343	22.53	6.81	0.16	3.45	67.69	101.09
344	22.60	6.81	0.17	3.45	67.92	101.09
345	22.64	6.81	0.17	3.45	68.51	101.06
346	22.70	6.99	0.16	3.45	69.39	101.14
347	22.80	6.72	0.13	3.45	69.95	101.18
348	22.84	6.63	0.13	3.45	70.62	101.10
349	22.90	6.27	0.14	3.45	70.38	100.93
350	23.00	6.18	0.16	3.45	69.13	100.75
351	23.05	6.45	0.16	3.55	68.58	100.83
352	23.14	6.00	0.15	3.55	68.29	101.27
353	23.18	6.72	0.14	3.55	68.03	101.80
354	23.24	7.70	0.13	3.55	67.99	102.49
355	23.32	7.79	0.17	3.74	68.19	103.21
356	23.39	8.15	0.20	3.64	68.76	103.90
357	23.44	8.24	0.22	3.64	69.27	104.61
358	23.53	8.15	0.27	3.64	70.63	105.26
359	23.59	7.97	0.31	3.55	72.71	105.79
360	23.63	7.79	0.32	3.55	74.78	106.03
361	23.69	7.52	0.33	3.55	76.93	106.13
362	23.77	7.17	0.33	3.55	78.80	106.09
363	23.82	6.99	0.31	3.55	80.08	105.85
364	23.93	6.27	0.27	3.55	80.97	105.50
365	23.95	6.27	0.26	3.55	81.13	105.09
366	24.03	6.36	0.23	3.55	80.69	104.61
367	24.12	6.36	0.21	3.64	79.74	104.12
368	24.16	6.36	0.21	3.64	78.67	103.68
369	24.22	6.63	0.20	3.64	77.27	103.40
370	24.30	6.81	0.19	3.64	76.10	103.19
371	24.37	6.90	0.19	3.64	75.43	103.13
372	24.43	6.90	0.19	3.64	74.72	103.16
373	24.50	6.90	0.19	3.64	73.88	103.24
374	24.57	6.90	0.20	3.64	73.42	103.35
375	24.62	6.90	0.21	3.74	73.24	103.54
376	24.69	7.17	0.21	3.74	73.23	103.72
377	24.77	7.44	0.22	3.74	73.31	103.89
378	24.83	7.44	0.22	3.74	73.35	104.01
379	24.88	7.52	0.23	3.64	73.20	104.10
380	24.97	7.44	0.23	3.74	73.15	104.15
381	25.02	7.35	0.23	3.64	73.05	104.16
382	25.11	7.26	0.22	3.74	73.12	104.12
383	25.17	7.35	0.22	3.74	73.18	104.12
384	25.21	7.17	0.22	3.74	73.19	104.08

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
385	25.29	7.35	0.21	3.93	73.06	104.13
386	25.36	7.35	0.21	3.93	72.49	104.23
387	25.40	7.44	0.22	3.93	71.70	104.39
388	25.46	7.44	0.22	3.93	71.06	104.62
389	25.54	7.79	0.24	3.93	70.33	104.85
390	25.62	8.33	0.25	3.83	69.84	105.10
391	25.66	8.60	0.25	3.83	69.49	105.40
392	25.75	8.78	0.27	3.83	69.25	105.70
393	25.80	8.78	0.27	3.74	68.92	105.99
394	25.85	8.78	0.27	3.93	68.55	106.20
395	25.96	8.78	0.29	3.93	69.47	106.36
396	26.01	8.78	0.30	3.93	70.08	106.56
397	26.05	8.87	0.30	3.93	70.24	106.77
398	26.12	9.05	0.30	3.93	70.29	106.95
399	26.19	7.79	0.31	3.93	70.21	107.10
400	26.25	8.51	0.32	4.03	69.98	107.17
401	26.33	9.32	0.34	4.03	70.30	107.16
402	26.42	9.41	0.33	4.03	70.99	107.10
403	26.46	9.50	0.32	4.03	71.77	107.01
404	26.52	9.41	0.31	4.03	71.62	106.93
405	26.61	8.42	0.30	4.03	71.87	106.78
406	26.67	7.88	0.29	4.03	72.47	106.51
407	26.71	7.79	0.28	4.03	72.98	106.21
408	26.79	7.79	0.28	3.93	73.84	105.91
409	26.87	7.79	0.27	3.93	74.74	105.65
410	26.92	7.79	0.26	3.93	75.11	105.43
411	26.98	7.88	0.24	3.93	74.96	105.22
412	27.06	7.70	0.24	3.93	74.82	105.02
413	27.11	7.70	0.24	3.93	74.64	104.80
414	27.21	7.44	0.24	3.93	74.74	104.61
415	27.26	7.52	0.23	4.03	74.95	104.41
416	27.32	7.44	0.22	3.93	75.90	104.22
417	27.40	7.44	0.22	3.93	76.83	104.02
418	27.45	7.26	0.22	3.93	77.64	103.74
419	27.52	7.08	0.21	3.93	77.83	103.35
420	27.60	6.45	0.20	4.03	78.49	102.97
421	27.65	6.36	0.20	4.03	78.87	102.63
422	27.71	6.27	0.18	4.12	79.19	102.32
423	27.80	6.36	0.15	4.12	78.85	102.04
424	27.84	6.09	0.15	4.12	78.27	101.80
425	27.90	6.36	0.15	4.12	77.11	101.68
426	27.99	6.54	0.16	4.12	76.15	101.67
427	28.05	6.99	0.16	4.12	75.68	101.85
428	28.10	7.08	0.16	4.12	75.60	102.23
429	28.17	7.26	0.17	4.12	75.27	102.59
430	28.25	7.26	0.19	4.12	74.87	102.95
431	28.30	7.17	0.21	4.03	74.34	103.25
432	28.39	7.35	0.22	4.22	74.39	103.61

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
433	28.44	7.35	0.22	4.22	74.36	103.92
434	28.49	7.70	0.22	4.22	74.39	104.21
435	28.54	7.88	0.22	4.22	74.12	104.34
436	28.62	7.97	0.24	4.22	73.25	104.26
437	28.68	7.97	0.23	4.22	73.04	104.31
438	28.74	8.06	0.24	4.22	73.29	104.54
439	28.83	7.97	0.22	4.22	73.76	104.72
440	28.89	7.97	0.18	4.22	74.24	104.85
441	28.98	7.79	0.23	4.22	75.63	104.88
442	29.03	7.79	0.28	4.22	75.89	104.94
443	29.09	7.79	0.27	4.22	75.86	104.91
444	29.14	7.79	0.26	4.22	75.85	104.95
445	29.22	6.63	0.26	4.22	75.98	105.13
446	29.27	7.93	0.25	4.31	75.34	105.16
447	29.38	8.06	0.23	4.41	74.27	105.02
448	29.43	8.15	0.23	4.41	73.18	104.92
449	29.48	8.42	0.23	4.50	72.12	104.85
450	29.57	8.60	0.23	4.50	70.39	104.82
451	29.62	8.69	0.23	4.50	69.77	104.77
452	29.68	8.78	0.23	4.50	69.53	104.82
453	29.73	8.87	0.23	4.50	69.25	104.83
454	29.82	8.69	0.23	4.41	69.21	104.84
455	29.87	8.60	0.23	4.41	69.23	104.80
456	29.94	8.60	0.24	4.41	69.40	104.76
457	30.02	8.60	0.23	4.41	69.74	104.67
458	30.07	8.60	0.23	4.41	70.26	104.57
459	30.16	8.51	0.22	4.41	70.70	104.47
460	30.19	8.42	0.22	4.50	70.92	104.34
461	30.26	8.15	0.21	4.50	71.00	104.13
462	30.36	7.97	0.21	4.50	71.06	103.96
463	30.41	7.97	0.21	4.50	70.92	103.80
464	30.46	7.97	0.20	4.50	70.81	103.67
465	30.53	7.97	0.19	4.50	70.68	103.59
466	30.61	8.15	0.19	4.50	70.37	103.56
467	30.65	8.33	0.19	4.50	69.86	103.58
468	30.71	8.33	0.19	4.50	69.24	103.70
469	30.81	8.42	0.20	4.50	68.66	103.91
470	30.84	8.51	0.20	4.60	68.08	104.24
471	30.91	8.69	0.21	4.60	67.66	104.63
472	30.99	9.14	0.23	4.60	67.39	105.12
473	31.04	9.41	0.24	4.60	67.03	105.58
474	31.11	9.76	0.26	4.60	66.57	106.03
475	31.19	10.03	0.28	4.60	66.20	106.49
476	31.25	10.39	0.31	4.60	65.84	106.89
477	31.30	10.48	0.31	4.50	65.63	107.18
478	31.39	10.75	0.32	4.50	65.59	107.42
479	31.45	10.84	0.33	4.50	65.68	107.59
480	31.50	10.84	0.33	4.50	65.87	107.70

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
481	31.60	10.66	0.32	4.50	66.11	107.72
482	31.65	10.57	0.32	4.50	66.18	107.66
483	31.73	10.39	0.32	4.50	66.49	107.65
484	31.80	10.21	0.32	4.50	67.04	107.71
485	31.84	10.21	0.32	4.60	67.57	107.78
486	31.91	10.21	0.29	4.60	68.14	107.89
487	31.99	10.30	0.32	4.60	68.68	108.00
488	32.03	10.30	0.36	4.60	69.04	108.12
489	32.09	10.30	0.36	4.60	69.29	108.25
490	32.19	10.30	0.37	4.60	69.46	108.37
491	32.25	10.30	0.37	4.60	69.84	108.58
492	32.29	10.35	0.37	4.60	70.12	108.75
493	32.38	10.39	0.37	4.60	70.10	108.82
494	32.43	10.57	0.37	4.60	69.85	108.91
495	32.48	10.57	0.38	4.60	69.44	108.98
496	32.58	10.57	0.39	4.70	69.08	109.07
497	32.63	10.75	0.39	4.70	68.78	109.18
498	32.69	11.11	0.39	4.70	68.56	109.31
499	32.74	11.29	0.39	4.70	68.43	109.45
500	32.83	11.38	0.40	4.70	68.20	109.58
501	32.88	11.38	0.41	4.70	67.88	109.68
502	32.97	11.38	0.42	4.70	67.80	109.82
503	33.01	11.47	0.43	4.70	67.86	109.97
504	33.07	11.65	0.43	4.70	68.03	110.10
505	33.16	11.65	0.43	4.70	68.26	110.19
506	33.20	11.65	0.45	4.70	68.29	110.24
507	33.27	11.73	0.46	4.70	68.26	110.22
508	33.36	11.65	0.45	4.70	68.18	110.16
509	33.42	11.56	0.45	4.70	68.17	110.06
510	33.51	11.56	0.43	4.70	68.06	109.88
511	33.56	11.47	0.41	4.70	67.71	109.58
512	33.61	11.47	0.40	4.70	67.31	109.21
513	33.67	11.29	0.38	4.70	67.07	108.81
514	33.76	11.11	0.34	4.70	67.01	108.36
515	33.81	11.02	0.31	4.70	66.63	107.92
516	33.86	10.84	0.29	4.70	66.55	107.50
517	33.94	10.39	0.28	4.70	66.17	107.07
518	34.02	9.85	0.27	4.70	65.74	106.68
519	34.06	10.44	0.26	4.70	65.39	106.40
520	34.14	9.94	0.26	4.70	65.27	106.21
521	34.21	10.48	0.25	4.70	65.38	106.07
522	34.25	10.57	0.25	4.70	65.42	105.93
523	34.33	10.66	0.25	4.70	65.35	105.82
524	34.41	10.57	0.25	4.70	65.67	105.70
525	34.49	10.21	0.25	4.70	65.62	105.56
526	34.56	9.85	0.24	4.70	65.88	105.40
527	34.59	9.67	0.24	4.79	66.16	105.24
528	34.67	9.59	0.23	4.79	66.44	105.07

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
529	34.76	9.59	0.22	4.79	66.66	104.91
530	34.80	9.59	0.21	4.79	66.69	104.75
531	34.85	9.59	0.21	4.79	66.67	104.67
532	34.93	9.76	0.21	4.79	66.55	104.59
533	34.98	9.76	0.21	4.79	66.59	104.55
534	35.05	9.67	0.21	4.79	66.78	104.50
535	35.13	9.67	0.22	4.79	66.81	104.46
536	35.18	9.67	0.22	4.79	66.88	104.42
537	35.24	9.45	0.22	4.89	67.11	104.37
538	35.32	9.23	0.21	4.89	67.48	104.31
539	35.41	9.50	0.20	4.89	67.83	104.21
540	35.46	9.41	0.20	4.89	68.12	104.07
541	35.51	9.32	0.20	4.89	68.31	103.88
542	35.58	9.14	0.20	4.89	68.44	103.70
543	35.66	8.96	0.19	4.89	68.42	103.52
544	35.71	8.87	0.19	4.89	68.66	103.37
545	35.76	8.87	0.18	4.89	68.83	103.21
546	35.86	8.78	0.18	4.89	68.92	103.07
547	35.91	8.78	0.17	4.89	68.90	102.92
548	36.01	8.78	0.17	4.89	68.90	102.82
549	36.05	8.78	0.17	4.89	68.67	102.68
550	36.12	8.87	0.17	4.89	68.57	102.58
551	36.20	8.78	0.17	4.89	68.61	102.47
552	36.23	8.78	0.17	4.89	68.46	102.43
553	36.31	8.78	0.16	4.89	68.09	102.39
554	36.35	8.78	0.16	4.89	67.28	102.32
555	36.45	8.51	0.16	4.98	66.40	102.25
556	36.51	8.87	0.16	4.98	65.33	102.19
557	36.58	9.23	0.16	4.98	64.41	102.18
558	36.66	9.67	0.15	4.98	63.63	102.21
559	36.70	9.94	0.15	4.98	62.95	102.30
560	36.80	10.12	0.15	4.98	62.13	102.46
561	36.85	10.12	0.16	4.98	61.55	102.65
562	36.89	10.12	0.16	4.98	61.19	102.83
563	36.96	10.12	0.17	4.98	61.34	103.09
564	37.03	10.39	0.18	4.98	61.62	103.34
565	37.09	10.48	0.19	4.98	62.14	103.61
566	37.15	10.48	0.19	4.98	62.54	103.83
567	37.23	10.39	0.20	4.98	62.96	104.05
568	37.27	10.39	0.20	4.98	63.24	104.22
569	37.34	10.30	0.21	4.98	63.51	104.34
570	37.43	10.30	0.21	4.98	63.70	104.42
571	37.49	10.30	0.21	4.98	63.92	104.50
572	37.54	10.30	0.21	4.98	63.90	104.50
573	37.62	10.48	0.21	4.98	64.01	104.50
574	37.69	10.57	0.21	5.08	63.93	104.42
575	37.74	10.48	0.21	4.98	63.93	104.38
576	37.82	10.48	0.20	5.08	63.95	104.34

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
577	37.89	10.30	0.20	4.98	63.96	104.29
578	37.93	10.21	0.19	5.08	63.84	104.30
579	38.02	10.21	0.20	5.08	63.69	104.35
580	38.08	10.21	0.20	5.08	63.41	104.46
581	38.13	10.21	0.20	5.08	63.89	104.61
582	38.23	10.75	0.21	5.08	63.50	104.84
583	38.28	11.11	0.22	5.08	62.70	105.13
584	38.35	11.38	0.23	5.08	61.78	105.37
585	38.42	10.30	0.24	5.08	60.85	105.61
586	38.47	11.91	0.25	5.18	59.99	105.85
587	38.52	12.72	0.25	5.18	59.66	106.05
588	38.61	12.90	0.25	5.18	59.48	106.21
589	38.67	12.99	0.25	5.18	59.28	106.26
590	38.72	12.90	0.25	5.18	58.69	106.29
591	38.82	12.36	0.26	5.18	58.76	106.22
592	38.86	12.27	0.26	5.18	59.16	106.09
593	38.96	12.09	0.24	5.18	59.66	105.92
594	39.01	11.73	0.24	5.18	60.09	105.75
595	39.05	11.56	0.23	5.18	60.15	105.59
596	39.13	11.38	0.22	5.18	59.44	105.47
597	39.21	11.29	0.21	5.27	58.54	105.36
598	39.24	11.47	0.21	5.27	57.27	105.38
599	39.31	12.18	0.21	5.37	55.65	105.47
600	39.40	13.35	0.22	5.37	54.17	105.67
601	39.44	13.71	0.22	5.37	52.68	105.95
602	39.51	14.87	0.23	5.37	51.39	106.29
603	39.60	15.77	0.24	5.37	50.31	106.62
604	39.66	16.03	0.26	5.37	49.52	106.88
605	39.70	16.39	0.27	5.37	49.07	107.01
606	39.80	16.48	0.28	5.37	48.87	107.10
607	39.85	16.30	0.28	5.37	49.01	107.13
608	39.90	16.03	0.27	5.37	49.38	107.07
609	39.98	15.50	0.25	5.37	49.70	106.91
610	40.05	14.96	0.24	5.37	50.05	106.64
611	40.10	14.69	0.24	5.37	50.44	106.29
612	40.20	14.42	0.23	5.37	50.75	105.88
613	40.25	14.33	0.22	5.46	50.95	105.46
614	40.30	13.97	0.20	5.46	51.10	105.11
615	40.40	13.53	0.19	5.46	51.15	104.80
616	40.45	13.44	0.18	5.46	51.09	104.52
617	40.50	13.44	0.17	5.56	50.89	104.35
618	40.59	13.44	0.17	5.56	50.80	104.26
619	40.64	13.44	0.17	5.56	50.70	104.26
620	40.69	13.62	0.18	5.56	50.43	104.33
621	40.79	14.15	0.19	5.56	50.31	104.53
622	40.83	14.24	0.20	5.56	50.44	104.94
623	40.92	14.33	0.20	5.56	50.42	105.38
624	40.98	14.60	0.20	5.56	50.37	105.84

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
625	41.03	14.87	0.22	5.56	50.39	106.28
626	41.08	15.14	0.26	5.56	50.50	106.65
627	41.18	15.86	0.27	5.56	50.55	106.94
628	41.22	16.03	0.28	5.56	50.67	107.21
629	41.31	15.94	0.29	5.66	50.92	107.47
630	41.36	15.94	0.29	5.66	51.10	107.66
631	41.42	15.86	0.28	5.66	51.14	107.72
632	41.50	15.59	0.28	5.66	51.35	107.74
633	41.54	15.50	0.28	5.75	51.60	107.76
634	41.61	15.50	0.28	5.75	51.71	107.73
635	41.70	15.50	0.28	5.75	51.90	107.72
636	41.75	15.50	0.28	5.75	52.13	107.74
637	41.80	15.50	0.29	5.75	52.28	107.77
638	41.87	15.50	0.28	5.75	52.40	107.79
639	41.95	15.50	0.29	5.75	52.45	107.83
640	42.01	15.41	0.29	5.75	52.51	107.89
641	42.10	15.41	0.29	5.75	52.56	108.01
642	42.14	15.41	0.29	5.75	52.59	108.16
643	42.21	15.68	0.29	5.75	52.82	108.39
644	42.27	15.77	0.30	5.75	52.92	108.56
645	42.34	16.21	0.32	5.75	52.98	108.70
646	42.39	16.39	0.34	5.75	53.11	108.84
647	42.49	16.30	0.36	5.75	53.28	108.97
648	42.54	16.30	0.35	5.75	53.67	109.17
649	42.59	16.21	0.34	5.85	54.07	109.36
650	42.69	15.94	0.34	5.85	54.49	109.49
651	42.74	15.86	0.34	5.85	54.71	109.51
652	42.80	15.86	0.37	5.85	54.81	109.48
653	42.89	15.86	0.38	5.85	54.99	109.45
654	42.93	16.03	0.38	5.85	55.31	109.41
655	42.99	15.94	0.35	5.85	55.56	109.34
656	43.08	15.94	0.35	5.85	55.85	109.23
657	43.11	15.77	0.34	5.85	56.08	109.03
658	43.18	15.14	0.33	5.85	56.48	108.74
659	43.28	14.96	0.32	5.85	57.10	108.37
660	43.35	14.51	0.30	5.85	57.81	108.05
661	43.38	14.15	0.30	5.85	58.70	107.67
662	43.45	13.26	0.28	5.85	59.54	107.22
663	43.53	12.54	0.26	5.85	60.26	106.75
664	43.58	12.54	0.25	5.85	61.15	106.25
665	43.64	11.91	0.24	5.85	62.32	105.79
666	43.73	11.73	0.21	5.85	63.44	105.31
667	43.78	11.47	0.20	5.85	64.11	104.91
668	43.84	10.93	0.19	5.85	64.43	104.69
669	43.92	10.30	0.19	5.85	64.47	104.56
670	43.98	10.21	0.19	5.94	63.48	104.52
671	44.07	10.57	0.19	5.94	62.65	104.73
672	44.12	11.20	0.21	5.94	59.78	105.37

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
673	44.17	12.09	0.22	5.94	57.19	106.06
674	44.23	13.53	0.22	5.94	52.78	106.91
675	44.29	14.15	0.25	5.94	49.94	107.71
676	44.39	19.71	0.32	6.13	48.01	108.02
677	44.43	19.71	0.33	6.13	47.15	108.13
678	44.49	25.71	0.36	6.04	46.40	108.15
679	44.57	23.11	0.38	6.04	46.57	108.04
680	44.67	18.90	0.25	6.04	47.03	107.69
681	44.73	14.96	0.23	6.04	48.61	106.97
682	44.78	14.96	0.21	6.04	50.29	106.12
683	44.82	12.36	0.19	6.04	54.12	104.91
684	44.93	10.39	0.15	6.04	57.45	103.44
685	44.97	10.12	0.14	6.13	60.57	102.52
686	45.02	9.85	0.13	6.13	62.40	101.78
687	45.09	9.59	0.12	6.13	64.66	101.10
688	45.17	9.41	0.11	6.13	65.62	100.58
689	45.22	9.41	0.11	6.13	65.67	100.36
690	45.30	9.32	0.12	6.13	65.49	100.15
691	45.37	9.32	0.12	6.13	65.32	100.01
692	45.42	9.50	0.12	6.13	65.33	99.93
693	45.50	9.76	0.12	6.13	65.30	99.86
694	45.57	9.85	0.11	6.13	65.47	99.85
695	45.61	9.76	0.11	6.13	65.41	99.78
696	45.72	9.41	0.11	6.13	65.40	99.70
697	45.77	9.32	0.10	6.13	65.61	99.69
698	45.80	9.23	0.11	6.13	65.50	99.86
699	45.88	9.23	0.11	6.13	65.41	100.17
700	45.96	9.23	0.11	6.23	64.82	100.56
701	46.01	9.23	0.12	6.13	63.80	100.96
702	46.11	10.39	0.14	6.23	62.71	101.35
703	46.14	10.93	0.15	6.13	61.71	101.65
704	46.21	11.82	0.16	6.23	61.11	101.93
705	46.26	12.18	0.16	6.23	60.62	102.26
706	46.35	12.36	0.15	6.23	60.17	102.58
707	46.41	11.91	0.15	6.23	59.40	102.67
708	46.49	11.29	0.15	6.23	58.58	102.66
709	46.55	11.29	0.16	6.23	58.21	102.56
710	46.59	11.29	0.17	6.23	58.23	102.56
711	46.68	12.27	0.15	6.33	58.74	102.83
712	46.74	12.54	0.14	6.33	58.71	103.22
713	46.80	12.27	0.14	6.33	57.80	103.47
714	46.85	12.18	0.16	6.33	57.31	103.86
715	46.93	12.45	0.20	6.42	57.24	104.35
716	47.00	13.53	0.22	6.42	57.95	105.00
717	47.10	14.24	0.19	6.33	58.79	105.63
718	47.15	13.97	0.23	6.33	58.92	106.09
719	47.20	13.62	0.27	6.33	58.79	106.32
720	47.25	13.62	0.30	6.33	58.15	106.24

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
721	47.31	13.62	0.30	6.42	58.33	105.93
722	47.40	14.15	0.26	6.33	59.44	105.60
723	47.44	13.62	0.22	6.33	60.31	105.07
724	47.52	13.62	0.17	6.33	60.38	104.31
725	47.58	11.73	0.14	6.33	60.23	103.33
726	47.67	10.39	0.12	6.42	59.78	102.22
727	47.73	9.85	0.11	6.42	59.86	101.19
728	47.78	10.44	0.10	6.42	59.76	100.33
729	47.86	10.12	0.10	6.42	60.31	99.75
730	47.92	10.48	0.10	6.42	60.51	99.58
731	47.98	10.48	0.10	6.42	60.76	99.82
732	48.05	11.02	0.10	6.52	61.11	100.27
733	48.12	10.93	0.10	6.52	61.50	100.85
734	48.19	10.93	0.12	6.52	61.13	101.74
735	48.27	10.75	0.15	6.52	60.13	102.52
736	48.32	10.75	0.17	6.52	58.22	103.23
737	48.39	11.65	0.18	6.52	55.23	103.75
738	48.47	13.80	0.23	6.52	52.37	104.20
739	48.52	15.14	0.22	6.52	48.97	104.58
740	48.57	17.02	0.21	6.52	45.63	104.82
741	48.67	19.89	0.17	6.52	43.20	104.92
742	48.71	19.89	0.16	6.52	41.55	105.08
743	48.76	22.13	0.16	6.52	41.23	105.24
744	48.82	22.57	0.16	6.52	40.94	105.63
745	48.93	20.07	0.16	6.52	42.02	106.27
746	48.97	19.08	0.19	6.52	43.97	107.28
747	49.05	16.21	0.26	6.61	46.09	108.31
748	49.08	19.04	0.30	6.61	47.92	109.44
749	49.16	16.93	0.37	6.71	49.82	110.62
750	49.25	18.99	0.46	6.71	51.13	111.87
751	49.29	18.99	0.50	6.71	52.10	113.14
752	49.36	23.38	0.58	6.71	52.05	114.52
753	49.43	24.46	0.67	6.81	51.21	115.77
754	49.48	25.08	0.77	6.81	49.34	116.81
755	49.55	25.98	0.91	6.81	47.43	117.60
756	49.64	28.75	1.14	6.90	45.79	118.25
757	49.70	34.76	1.19	6.90	44.94	118.78
758	49.75	37.00	1.16	6.90	44.24	119.23
759	49.81	38.52	1.09	6.90	43.43	119.56
760	49.90	37.17	1.05	6.90	42.73	119.90
761	49.94	36.19	1.08	6.90	42.13	120.10
762	50.01	35.74	1.12	7.00	42.39	120.15
763	50.08	36.01	1.10	7.09	43.00	120.18
764	50.15	36.73	1.26	7.09	43.93	120.19
765	50.24	36.55	1.33	7.09	44.06	120.24
766	50.30	33.95	1.28	7.19	43.61	120.23
767	50.34	33.05	1.24	7.19	43.10	120.11
768	50.41	31.98	1.17	7.28	42.71	119.97

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
769	50.47	37.44	1.13	8.53	42.19	119.58
770	50.54	39.32	1.02	8.72	41.50	119.10
771	50.62	37.71	0.93	8.91	40.55	118.60
772	50.66	36.73	0.89	9.01	39.44	118.04
773	50.77	34.58	0.76	9.11	38.30	117.47
774	50.81	34.22	0.73	9.20	37.79	116.82
775	50.87	33.41	0.68	9.20	37.58	116.23
776	50.92	32.96	0.61	9.30	37.40	115.71
777	51.01	32.34	0.57	9.30	37.12	115.22
778	51.07	31.71	0.55	9.30	36.85	114.92
779	51.15	32.34	0.54	9.39	36.63	114.67
780	51.21	31.89	0.54	9.49	36.47	114.52
781	51.26	32.34	0.54	9.49	36.38	114.50
782	51.32	32.70	0.55	9.49	36.26	114.56
783	51.39	32.70	0.56	9.49	36.13	114.67
784	51.46	32.70	0.58	9.58	36.12	114.80
785	51.53	33.50	0.59	9.58	36.09	114.94
786	51.61	34.13	0.60	9.68	36.06	115.08
787	51.65	34.40	0.61	9.68	35.98	115.20
788	51.72	34.40	0.62	9.68	35.85	115.30
789	51.81	34.31	0.63	9.68	35.61	115.38
790	51.84	34.76	0.63	9.78	35.39	115.44
791	51.92	35.03	0.62	9.78	35.17	115.47
792	52.01	35.38	0.62	9.87	34.96	115.49
793	52.06	36.01	0.62	9.87	34.72	115.49
794	52.11	36.28	0.62	9.87	34.44	115.49
795	52.19	36.64	0.61	9.97	34.28	115.48
796	52.25	36.73	0.61	9.97	34.15	115.51
797	52.30	36.64	0.61	9.97	34.03	115.56
798	52.38	36.68	0.61	9.97	33.96	115.66
799	52.45	36.37	0.62	10.06	33.91	115.77
800	52.49	36.73	0.63	10.06	33.88	115.90
801	52.57	37.44	0.65	10.06	33.95	116.02
802	52.65	38.34	0.68	10.16	34.08	116.14
803	52.70	38.61	0.69	10.16	34.44	116.21
804	52.79	39.06	0.70	10.16	34.78	116.24
805	52.85	38.25	0.70	10.16	35.12	116.22
806	52.89	37.53	0.70	10.16	35.45	116.09
807	52.99	34.67	0.68	10.16	35.82	115.84
808	53.04	34.13	0.66	10.16	36.13	115.49
809	53.08	33.50	0.63	10.16	36.57	115.07
810	53.17	32.61	0.57	10.16	36.93	114.60
811	53.24	31.80	0.52	10.26	37.21	114.09
812	53.33	30.99	0.46	10.26	37.23	113.59
813	53.39	29.74	0.44	10.26	37.22	113.10
814	53.42	29.38	0.42	10.26	37.37	112.64
815	53.49	28.84	0.40	10.26	37.62	112.29
816	53.58	28.49	0.40	10.26	37.98	112.05

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
817	53.63	28.31	0.40	10.26	38.48	111.98
818	53.68	27.05	0.40	10.26	38.93	112.03
819	53.77	27.05	0.41	10.26	39.46	112.19
820	53.83	27.05	0.42	10.26	40.10	112.42
821	53.88	27.05	0.44	10.26	40.78	112.70
822	53.97	27.68	0.48	10.16	41.50	113.01
823	54.03	28.13	0.51	10.16	42.02	113.33
824	54.08	27.59	0.53	10.16	42.14	113.61
825	54.18	27.63	0.56	10.16	42.12	113.82
826	54.22	27.63	0.58	10.16	41.98	114.00
827	54.27	27.68	0.59	10.26	41.78	114.13
828	54.38	29.56	0.57	10.26	41.54	114.24
829	54.42	29.74	0.54	10.26	41.81	114.67
830	54.47	30.01	0.54	10.26	42.05	115.21
831	54.57	30.46	0.55	10.35	42.43	115.78
832	54.61	31.17	0.57	10.35	41.62	116.57
833	54.68	31.17	0.81	10.35	41.14	117.57
834	54.75	32.88	0.93	10.45	40.50	118.66
835	54.79	32.61	1.00	10.45	39.78	119.73
836	54.86	43.45	1.16	10.64	39.03	120.80
837	54.95	47.39	1.40	10.64	38.29	121.91
838	55.01	51.69	1.55	10.73	37.14	122.83
839	55.06	54.02	1.65	10.73	36.02	123.68
840	55.12	57.15	1.80	10.73	34.71	124.52
841	55.21	61.27	2.04	10.73	33.76	125.22
842	55.25	64.14	2.11	10.64	32.87	125.75
843	55.32	66.91	2.23	10.54	32.18	126.15
844	55.40	72.29	2.38	10.54	31.81	126.39
845	55.50	77.75	2.42	10.45	31.72	126.45
846	55.52	77.93	2.40	10.35	31.96	126.30
847	55.60	76.23	2.31	10.26	32.50	126.07
848	55.67	68.89	2.13	10.35	33.16	125.74
849	55.72	61.18	1.92	10.26	33.98	125.28
850	55.79	52.40	1.75	10.35	35.08	124.70
851	55.86	47.48	1.66	10.45	36.27	124.04
852	55.95	45.68	1.60	10.73	37.65	123.26
853	56.00	45.95	1.53	10.73	38.96	122.53
854	56.05	45.51	1.40	10.73	40.16	121.88
855	56.11	44.61	1.29	10.73	40.86	121.32
856	56.19	40.85	1.09	10.73	41.22	120.78
857	56.24	38.34	1.08	10.73	41.64	120.18
858	56.34	35.74	1.04	11.12	42.32	119.54
859	56.37	35.03	1.01	11.02	43.11	118.95
860	56.43	34.31	0.95	10.93	43.79	118.37
861	56.54	31.53	0.87	10.93	44.39	117.93
862	56.59	30.01	0.82	10.93	44.58	117.44
863	56.64	30.10	0.79	10.93	44.42	116.85
864	56.73	31.17	0.73	11.02	44.27	116.23

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
865	56.79	30.73	0.69	11.12	44.22	115.62
866	56.84	30.37	0.63	11.12	43.79	115.04
867	56.93	28.84	0.51	11.12	43.16	114.47
868	56.96	28.22	0.50	11.21	42.56	113.83
869	57.03	27.05	0.48	11.21	42.19	113.19
870	57.13	27.14	0.44	11.31	41.98	112.57
871	57.16	27.14	0.42	11.31	41.84	112.02
872	57.23	26.34	0.38	11.31	41.87	111.70
873	57.29	26.34	0.36	11.31	41.94	111.47
874	57.38	25.44	0.36	11.41	41.75	111.27
875	57.42	25.44	0.36	11.41	41.56	111.22
876	57.49	25.44	0.36	11.41	41.52	111.34
877	57.57	25.71	0.40	11.41	41.66	111.51
878	57.62	26.34	0.39	11.50	42.09	111.67
879	57.68	27.68	0.41	11.50	42.48	111.80
880	57.77	28.67	0.47	11.50	43.04	111.92
881	57.85	27.50	0.46	11.50	43.82	112.03
882	57.92	25.62	0.44	11.50	44.48	111.99
883	57.97	24.81	0.43	11.50	45.20	111.88
884	58.02	23.83	0.43	11.50	45.91	111.65
885	58.07	22.57	0.43	11.50	46.56	111.26
886	58.16	22.13	0.40	11.60	47.09	110.88
887	58.23	21.86	0.36	11.60	47.42	110.58
888	58.31	22.22	0.32	11.60	47.72	110.31
889	58.37	22.22	0.31	11.60	47.78	110.05
890	58.42	22.04	0.31	11.60	47.67	109.88
891	58.50	21.77	0.32	11.60	47.59	109.83
892	58.57	21.50	0.33	11.69	47.59	109.91
893	58.61	21.59	0.33	11.69	47.77	110.16
894	58.68	21.68	0.36	11.69	48.12	110.74
895	58.76	22.22	0.38	11.69	48.53	111.58
896	58.80	22.66	0.39	11.69	48.38	112.57
897	58.87	23.56	0.42	11.79	48.09	113.70
898	58.95	25.62	0.55	11.79	48.27	114.79
899	59.01	27.68	0.69	11.88	46.93	116.17
900	59.06	31.35	0.80	11.88	45.24	117.35
901	59.16	33.95	0.95	11.88	43.13	118.35
902	59.19	32.25	1.03	11.88	41.20	119.16
903	59.29	44.52	1.31	12.75	40.00	119.76
904	59.33	47.57	1.30	12.75	39.12	120.19
905	59.39	51.33	1.21	12.75	38.51	120.44
906	59.47	51.24	1.14	12.56	37.77	120.49
907	59.54	46.40	1.13	12.65	36.79	120.38
908	59.58	43.45	1.12	12.65	36.60	119.93
909	59.65	42.01	1.05	12.84	36.97	119.35
910	59.73	42.46	0.95	12.94	38.40	118.82
911	59.81	40.22	0.82	12.84	40.33	118.46
912	59.85	37.53	0.76	12.84	39.79	117.27

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
913	59.92	32.88	0.69	12.84	38.45	115.93
914	59.99	28.67	0.76	12.84	36.19	114.48
915	60.08	28.84	0.90	12.94	33.75	112.89
916	60.13	31.80	0.00	13.13	31.17	111.17
917	60.18	34.04	0.00	13.13	28.28	109.13
918	60.27	39.24	0.00	13.13	24.82	106.64
919	60.33	40.76	0.00	13.03	5.00	102.26
920	60.38	40.04	0.00	13.03	N/A	87.36
921	60.47	38.88	0.00	13.03	N/A	87.36

Abbreviations

Depth:	Depth from free surface, at which CPT was performed (ft)
q_c:	Measured cone resistance (tsf)
f_s:	Sleeve friction resistance (tsf)
u:	Pore pressure (tsf)
Fines content:	Percentage of fines in soil (%)
Unit weight:	Bulk soil unit weight (pcf)

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data ::

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
1	0.10	0.01	0.00	0.01	1.00	0.358	1.34	0.266	1.00	1.00	2.000	No
2	0.16	0.01	0.00	0.01	1.00	0.358	1.34	0.266	1.00	1.00	2.000	No
3	0.23	0.01	0.00	0.01	1.00	0.358	1.34	0.266	1.00	1.00	2.000	No
4	0.30	0.02	0.00	0.02	1.00	0.358	1.34	0.266	1.00	1.00	2.000	No
5	0.34	0.02	0.00	0.02	1.00	0.358	1.34	0.266	1.00	1.00	2.000	No
6	0.40	0.02	0.00	0.02	1.00	0.358	1.34	0.266	1.00	1.00	2.000	No
7	0.50	0.03	0.00	0.03	1.00	0.358	1.34	0.266	1.00	1.00	2.000	No
8	0.54	0.03	0.00	0.03	1.00	0.358	1.34	0.266	1.00	1.00	2.000	No
9	0.60	0.03	0.00	0.03	1.00	0.358	1.34	0.266	1.00	1.00	2.000	Yes
10	0.68	0.04	0.00	0.04	1.00	0.358	1.34	0.266	1.00	1.00	2.000	Yes
11	0.73	0.04	0.00	0.04	1.00	0.358	1.34	0.266	1.00	1.00	2.000	Yes
12	0.80	0.05	0.00	0.05	1.00	0.357	1.34	0.266	1.00	1.00	2.000	Yes
13	0.87	0.05	0.00	0.05	1.00	0.357	1.34	0.266	1.00	1.00	2.000	Yes
14	0.95	0.06	0.00	0.06	1.00	0.357	1.34	0.266	1.00	1.00	2.000	Yes
15	0.99	0.06	0.00	0.06	1.00	0.357	1.34	0.266	1.00	1.00	2.000	Yes
16	1.09	0.06	0.00	0.06	1.00	0.357	1.34	0.266	1.00	1.00	2.000	Yes
17	1.14	0.07	0.00	0.07	1.00	0.357	1.34	0.266	1.00	1.00	2.000	Yes
18	1.22	0.07	0.00	0.07	1.00	0.357	1.34	0.266	1.00	1.00	2.000	Yes
19	1.29	0.08	0.00	0.08	1.00	0.357	1.34	0.266	1.00	1.00	2.000	Yes
20	1.33	0.08	0.00	0.08	1.00	0.357	1.34	0.266	1.00	1.00	2.000	Yes
21	1.39	0.08	0.00	0.08	1.00	0.357	1.34	0.266	1.00	1.00	2.000	No
22	1.48	0.09	0.00	0.09	1.00	0.357	1.34	0.265	1.00	1.00	2.000	No
23	1.52	0.09	0.00	0.09	1.00	0.357	1.34	0.265	1.00	1.00	2.000	No
24	1.59	0.09	0.00	0.09	1.00	0.357	1.34	0.265	1.00	1.00	2.000	No
25	1.66	0.10	0.00	0.10	1.00	0.357	1.34	0.265	1.00	1.00	2.000	No
26	1.73	0.10	0.00	0.10	1.00	0.357	1.34	0.265	1.00	1.00	2.000	No
27	1.78	0.11	0.00	0.11	1.00	0.357	1.34	0.265	1.00	1.00	2.000	No
28	1.84	0.11	0.00	0.11	1.00	0.357	1.34	0.265	1.00	1.00	2.000	No
29	1.93	0.11	0.00	0.11	1.00	0.357	1.34	0.265	1.00	1.00	2.000	No
30	1.98	0.12	0.00	0.12	1.00	0.357	1.34	0.265	1.00	1.00	2.000	No
31	2.04	0.12	0.00	0.12	1.00	0.357	1.34	0.265	1.00	1.00	2.000	No
32	2.13	0.12	0.00	0.12	1.00	0.356	1.34	0.265	1.00	1.00	2.000	No
33	2.18	0.13	0.00	0.13	1.00	0.356	1.34	0.265	1.00	1.00	2.000	No
34	2.25	0.13	0.00	0.13	1.00	0.356	1.34	0.265	1.00	1.00	2.000	No
35	2.30	0.13	0.00	0.13	1.00	0.356	1.34	0.265	1.00	1.00	2.000	No
36	2.38	0.14	0.00	0.14	1.00	0.356	1.34	0.265	1.00	1.00	2.000	No
37	2.44	0.14	0.00	0.14	1.00	0.356	1.34	0.265	1.00	1.00	2.000	No
38	2.51	0.15	0.00	0.15	1.00	0.356	1.34	0.265	1.00	1.00	2.000	No
39	2.57	0.15	0.00	0.15	1.00	0.356	1.34	0.265	1.00	1.00	2.000	No
40	2.66	0.15	0.00	0.15	1.00	0.356	1.34	0.265	1.00	1.00	2.000	No
41	2.72	0.16	0.00	0.16	1.00	0.356	1.34	0.265	1.00	1.00	2.000	No
42	2.76	0.16	0.00	0.16	1.00	0.356	1.34	0.265	1.00	1.00	2.000	No
43	2.84	0.16	0.00	0.16	1.00	0.356	1.34	0.265	1.00	1.00	2.000	No
44	2.92	0.17	0.00	0.17	1.00	0.356	1.34	0.265	1.00	1.00	2.000	No
45	2.95	0.17	0.00	0.17	1.00	0.356	1.34	0.265	1.00	1.00	2.000	No
46	3.07	0.18	0.00	0.18	0.99	0.356	1.34	0.265	1.00	1.00	2.000	No
47	3.11	0.18	0.00	0.18	0.99	0.356	1.34	0.264	1.00	1.00	2.000	No
48	3.16	0.18	0.00	0.18	0.99	0.356	1.34	0.264	1.00	1.00	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
49	3.26	0.19	0.00	0.19	0.99	0.355	1.34	0.264	1.00	1.00	2.000	No
50	3.30	0.19	0.00	0.19	0.99	0.355	1.34	0.264	1.00	1.00	2.000	No
51	3.36	0.19	0.00	0.19	0.99	0.355	1.34	0.264	1.00	1.00	2.000	No
52	3.44	0.20	0.00	0.20	0.99	0.355	1.34	0.264	1.00	1.00	2.000	No
53	3.50	0.20	0.00	0.20	0.99	0.355	1.34	0.264	1.00	1.00	2.000	No
54	3.56	0.20	0.00	0.20	0.99	0.355	1.34	0.264	1.00	1.00	2.000	No
55	3.62	0.21	0.00	0.21	0.99	0.355	1.34	0.264	1.00	1.00	2.000	No
56	3.71	0.21	0.00	0.21	0.99	0.355	1.34	0.264	1.00	1.00	2.000	No
57	3.76	0.21	0.00	0.21	0.99	0.355	1.34	0.264	1.00	1.00	2.000	No
58	3.82	0.22	0.00	0.22	0.99	0.355	1.34	0.264	1.00	1.00	2.000	No
59	3.90	0.22	0.00	0.22	0.99	0.355	1.34	0.264	1.00	1.00	2.000	No
60	3.95	0.22	0.00	0.22	0.99	0.355	1.34	0.264	1.00	1.00	2.000	No
61	4.00	0.23	0.00	0.23	0.99	0.355	1.34	0.264	1.00	1.00	2.000	No
62	4.09	0.23	0.00	0.23	0.99	0.355	1.34	0.264	1.00	1.00	2.000	No
63	4.16	0.24	0.00	0.24	0.99	0.355	1.34	0.264	1.00	1.00	2.000	No
64	4.20	0.24	0.00	0.24	0.99	0.355	1.34	0.264	1.00	1.00	2.000	No
65	4.27	0.24	0.00	0.24	0.99	0.355	1.34	0.264	1.00	1.00	2.000	No
66	4.34	0.25	0.00	0.25	0.99	0.355	1.34	0.264	1.00	1.00	2.000	No
67	4.44	0.25	0.00	0.25	0.99	0.354	1.34	0.264	1.00	1.00	2.000	No
68	4.48	0.25	0.00	0.25	0.99	0.354	1.34	0.264	1.00	1.00	2.000	No
69	4.58	0.26	0.00	0.26	0.99	0.354	1.34	0.264	1.00	1.00	2.000	No
70	4.63	0.26	0.00	0.26	0.99	0.354	1.34	0.264	1.00	1.00	2.000	No
71	4.68	0.26	0.00	0.26	0.99	0.354	1.34	0.263	1.00	1.00	2.000	No
72	4.73	0.27	0.00	0.27	0.99	0.354	1.34	0.263	1.00	1.00	2.000	No
73	4.80	0.27	0.00	0.27	0.99	0.354	1.34	0.263	1.00	1.00	2.000	No
74	4.86	0.27	0.00	0.27	0.99	0.354	1.34	0.263	1.00	1.00	2.000	No
75	4.93	0.28	0.00	0.28	0.99	0.354	1.34	0.263	1.00	1.00	2.000	No
76	5.00	0.28	0.00	0.28	0.99	0.354	1.34	0.263	1.00	1.00	2.000	No
77	5.07	0.29	0.00	0.29	0.99	0.354	1.34	0.263	1.00	1.00	2.000	No
78	5.12	0.29	0.00	0.29	0.99	0.354	1.34	0.263	1.00	1.00	2.000	No
79	5.20	0.29	0.00	0.29	0.99	0.354	1.34	0.263	1.00	1.00	2.000	No
80	5.27	0.30	0.00	0.30	0.99	0.354	1.34	0.263	1.00	1.00	2.000	No
81	5.33	0.30	0.00	0.30	0.99	0.354	1.34	0.263	1.00	1.00	2.000	No
82	5.41	0.30	0.00	0.30	0.99	0.354	1.34	0.263	1.00	1.00	2.000	No
83	5.45	0.31	0.00	0.31	0.99	0.354	1.34	0.263	1.00	1.00	2.000	No
84	5.52	0.31	0.00	0.31	0.99	0.354	1.34	0.263	1.00	1.00	2.000	No
85	5.60	0.31	0.00	0.31	0.99	0.354	1.34	0.263	1.00	1.00	2.000	No
86	5.67	0.32	0.00	0.32	0.99	0.353	1.34	0.263	1.00	1.00	2.000	No
87	5.71	0.32	0.00	0.32	0.99	0.353	1.34	0.263	1.00	1.00	2.000	No
88	5.80	0.32	0.00	0.32	0.99	0.353	1.34	0.263	1.00	1.00	2.000	No
89	5.85	0.33	0.00	0.33	0.99	0.353	1.34	0.263	1.00	1.00	2.000	No
90	5.91	0.33	0.00	0.33	0.99	0.353	1.34	0.263	1.00	1.00	2.000	No
91	6.01	0.34	0.00	0.34	0.99	0.353	1.34	0.263	1.00	1.00	2.000	No
92	6.06	0.34	0.00	0.34	0.99	0.353	1.34	0.263	1.00	1.00	2.000	No
93	6.11	0.34	0.00	0.34	0.99	0.353	1.34	0.263	1.00	1.00	2.000	No
94	6.18	0.34	0.00	0.34	0.99	0.353	1.34	0.263	1.00	1.00	2.000	No
95	6.26	0.35	0.00	0.35	0.99	0.353	1.34	0.263	1.00	1.00	2.000	No
96	6.30	0.35	0.00	0.35	0.99	0.353	1.34	0.263	1.00	1.00	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
97	6.37	0.35	0.00	0.35	0.99	0.353	1.34	0.262	1.00	1.00	2.000	No
98	6.45	0.36	0.00	0.36	0.99	0.353	1.34	0.262	1.00	1.00	2.000	No
99	6.51	0.36	0.00	0.36	0.99	0.353	1.34	0.262	1.00	1.00	2.000	No
100	6.60	0.37	0.00	0.37	0.99	0.353	1.34	0.262	1.00	1.00	2.000	No
101	6.64	0.37	0.00	0.37	0.99	0.353	1.34	0.262	1.00	1.00	2.000	No
102	6.70	0.37	0.00	0.37	0.99	0.353	1.34	0.262	1.00	1.00	2.000	No
103	6.80	0.38	0.00	0.38	0.99	0.353	1.34	0.262	1.00	1.00	2.000	No
104	6.83	0.38	0.00	0.38	0.99	0.353	1.34	0.262	1.00	1.00	2.000	No
105	6.90	0.38	0.00	0.38	0.99	0.352	1.34	0.262	1.00	1.00	2.000	No
106	6.98	0.39	0.00	0.39	0.99	0.352	1.34	0.262	1.00	1.00	2.000	No
107	7.04	0.39	0.00	0.39	0.99	0.352	1.34	0.262	1.00	1.00	2.000	No
108	7.09	0.39	0.00	0.39	0.99	0.352	1.34	0.262	1.00	1.00	2.000	No
109	7.16	0.40	0.00	0.40	0.99	0.352	1.34	0.262	1.00	1.00	2.000	No
110	7.24	0.40	0.00	0.40	0.99	0.352	1.34	0.262	1.00	1.00	2.000	No
111	7.30	0.40	0.00	0.40	0.99	0.352	1.34	0.262	1.00	1.00	2.000	No
112	7.39	0.41	0.00	0.41	0.98	0.352	1.34	0.262	1.00	1.00	2.000	No
113	7.43	0.41	0.00	0.41	0.98	0.352	1.34	0.262	1.00	1.00	2.000	No
114	7.50	0.42	0.00	0.42	0.98	0.352	1.34	0.262	1.00	1.00	2.000	No
115	7.59	0.42	0.00	0.42	0.98	0.352	1.34	0.262	1.00	1.00	2.000	No
116	7.63	0.42	0.00	0.42	0.98	0.352	1.34	0.262	1.00	1.00	2.000	No
117	7.70	0.43	0.00	0.43	0.98	0.352	1.34	0.262	1.00	1.00	2.000	No
118	7.78	0.43	0.00	0.43	0.98	0.352	1.34	0.262	1.00	1.00	2.000	No
119	7.83	0.43	0.00	0.43	0.98	0.352	1.34	0.262	1.00	1.00	2.000	No
120	7.89	0.44	0.00	0.44	0.98	0.352	1.34	0.262	1.00	1.00	2.000	No
121	7.95	0.44	0.00	0.44	0.98	0.352	1.34	0.262	1.00	1.00	2.000	No
122	8.02	0.44	0.00	0.44	0.98	0.352	1.34	0.261	1.00	1.00	2.000	No
123	8.11	0.45	0.00	0.45	0.98	0.352	1.34	0.261	1.00	1.00	2.000	No
124	8.16	0.45	0.00	0.45	0.98	0.351	1.34	0.261	1.00	1.00	2.000	No
125	8.21	0.45	0.00	0.45	0.98	0.351	1.34	0.261	1.00	1.00	2.000	No
126	8.30	0.46	0.00	0.46	0.98	0.351	1.34	0.261	1.00	1.00	2.000	No
127	8.36	0.46	0.00	0.46	0.98	0.351	1.34	0.261	1.00	1.00	2.000	No
128	8.41	0.46	0.00	0.46	0.98	0.351	1.34	0.261	1.00	1.00	2.000	No
129	8.47	0.47	0.00	0.47	0.98	0.351	1.34	0.261	1.00	1.00	2.000	No
130	8.56	0.47	0.00	0.47	0.98	0.351	1.34	0.261	1.00	1.00	2.000	No
131	8.61	0.47	0.00	0.47	0.98	0.351	1.34	0.261	1.00	1.00	2.000	No
132	8.70	0.48	0.00	0.48	0.98	0.351	1.34	0.261	1.00	1.00	2.000	No
133	8.75	0.48	0.00	0.48	0.98	0.351	1.34	0.261	1.00	1.00	2.000	No
134	8.81	0.49	0.00	0.49	0.98	0.351	1.34	0.261	1.00	1.00	2.000	No
135	8.90	0.49	0.00	0.49	0.98	0.351	1.34	0.261	1.00	1.00	2.000	No
136	8.94	0.49	0.00	0.49	0.98	0.351	1.34	0.261	1.00	1.00	2.000	No
137	9.01	0.50	0.00	0.50	0.98	0.351	1.34	0.261	1.00	1.00	0.261	No
138	9.09	0.50	0.00	0.50	0.98	0.353	1.34	0.262	1.00	1.00	0.262	No
139	9.13	0.50	0.00	0.50	0.98	0.354	1.34	0.263	1.00	1.00	0.263	No
140	9.20	0.51	0.01	0.50	0.98	0.355	1.34	0.264	1.00	1.00	0.264	No
141	9.27	0.51	0.01	0.50	0.98	0.356	1.34	0.265	1.00	1.00	0.265	No
142	9.35	0.51	0.01	0.50	0.98	0.358	1.34	0.266	1.00	1.00	0.266	No
143	9.39	0.52	0.01	0.50	0.98	0.359	1.34	0.267	1.00	1.00	0.267	No
144	9.45	0.52	0.01	0.51	0.98	0.360	1.34	0.268	1.00	1.00	0.268	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
145	9.54	0.52	0.02	0.51	0.98	0.362	1.34	0.269	1.00	1.00	0.269	No
146	9.59	0.53	0.02	0.51	0.98	0.363	1.34	0.270	1.00	1.00	0.270	No
147	9.65	0.53	0.02	0.51	0.98	0.364	1.34	0.271	1.00	1.00	0.271	No
148	9.73	0.53	0.02	0.51	0.98	0.366	1.34	0.272	1.00	1.00	0.272	No
149	9.81	0.54	0.03	0.51	0.98	0.367	1.34	0.273	1.00	1.00	0.273	No
150	9.85	0.54	0.03	0.51	0.98	0.368	1.34	0.274	1.00	1.00	0.274	No
151	9.94	0.55	0.03	0.52	0.98	0.370	1.34	0.275	1.00	1.00	0.275	No
152	10.00	0.55	0.03	0.52	0.98	0.371	1.34	0.276	1.00	1.00	0.276	No
153	10.04	0.55	0.03	0.52	0.98	0.372	1.34	0.277	1.00	1.00	0.277	No
154	10.12	0.55	0.03	0.52	0.98	0.373	1.34	0.278	1.00	1.00	0.278	No
155	10.19	0.56	0.04	0.52	0.98	0.375	1.34	0.279	1.00	1.00	0.279	No
156	10.24	0.56	0.04	0.52	0.98	0.376	1.34	0.279	1.00	1.00	0.279	No
157	10.31	0.56	0.04	0.52	0.98	0.377	1.34	0.280	1.00	1.00	0.280	No
158	10.39	0.57	0.04	0.53	0.98	0.379	1.34	0.282	1.00	1.00	0.282	No
159	10.48	0.57	0.05	0.53	0.98	0.380	1.34	0.283	1.00	1.00	0.283	No
160	10.53	0.58	0.05	0.53	0.98	0.381	1.34	0.284	1.00	1.00	0.284	No
161	10.63	0.58	0.05	0.53	0.98	0.383	1.34	0.285	1.00	1.00	0.285	No
162	10.67	0.58	0.05	0.53	0.98	0.384	1.34	0.285	1.00	1.00	0.285	No
163	10.71	0.59	0.05	0.53	0.98	0.385	1.34	0.286	1.00	1.00	0.286	No
164	10.79	0.59	0.06	0.53	0.98	0.386	1.34	0.287	1.00	1.00	0.287	No
165	10.83	0.59	0.06	0.54	0.98	0.387	1.34	0.288	1.00	1.00	0.288	No
166	10.93	0.60	0.06	0.54	0.98	0.388	1.34	0.289	1.00	1.00	0.289	No
167	10.98	0.60	0.06	0.54	0.98	0.389	1.34	0.290	1.00	1.00	0.290	No
168	11.06	0.60	0.06	0.54	0.98	0.391	1.34	0.291	1.00	1.00	0.291	No
169	11.11	0.61	0.07	0.54	0.98	0.392	1.34	0.291	1.00	1.00	0.291	No
170	11.16	0.61	0.07	0.54	0.98	0.393	1.34	0.292	1.00	1.00	0.292	No
171	11.23	0.61	0.07	0.54	0.98	0.394	1.34	0.293	1.00	1.00	0.293	No
172	11.31	0.62	0.07	0.55	0.98	0.395	1.34	0.294	1.00	1.00	0.294	No
173	11.36	0.62	0.07	0.55	0.98	0.396	1.34	0.294	1.00	1.00	0.294	No
174	11.42	0.62	0.08	0.55	0.98	0.397	1.34	0.295	1.00	1.00	0.295	No
175	11.51	0.63	0.08	0.55	0.98	0.398	1.34	0.296	1.00	1.00	0.296	No
176	11.56	0.63	0.08	0.55	0.98	0.399	1.34	0.297	1.00	1.00	0.297	No
177	11.65	0.64	0.08	0.55	0.98	0.401	1.34	0.298	1.00	1.00	0.298	No
178	11.71	0.64	0.08	0.56	0.98	0.402	1.34	0.299	1.00	1.00	0.299	No
179	11.75	0.64	0.09	0.56	0.98	0.402	1.34	0.299	1.00	1.00	0.299	No
180	11.84	0.65	0.09	0.56	0.98	0.404	1.34	0.300	1.00	1.00	0.300	No
181	11.89	0.65	0.09	0.56	0.98	0.405	1.34	0.301	1.00	1.00	0.301	No
182	11.96	0.65	0.09	0.56	0.98	0.406	1.34	0.302	1.00	1.00	0.302	No
183	12.03	0.66	0.09	0.56	0.97	0.407	1.34	0.303	1.00	1.00	0.303	No
184	12.11	0.66	0.10	0.57	0.97	0.408	1.34	0.304	1.00	1.00	0.304	No
185	12.16	0.67	0.10	0.57	0.97	0.409	1.34	0.304	1.00	1.00	0.304	No
186	12.21	0.67	0.10	0.57	0.97	0.410	1.34	0.305	1.00	1.00	0.305	No
187	12.30	0.67	0.10	0.57	0.97	0.411	1.34	0.306	1.00	1.00	0.306	No
188	12.35	0.68	0.10	0.57	0.97	0.412	1.34	0.306	1.00	1.00	0.306	No
189	12.41	0.68	0.11	0.57	0.97	0.413	1.34	0.307	1.00	1.00	0.307	No
190	12.49	0.68	0.11	0.57	0.97	0.414	1.34	0.308	1.00	1.00	0.308	No
191	12.56	0.69	0.11	0.58	0.97	0.415	1.34	0.309	1.00	1.00	0.309	No
192	12.60	0.69	0.11	0.58	0.97	0.416	1.34	0.309	1.00	1.00	0.309	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
193	12.67	0.69	0.11	0.58	0.97	0.417	1.34	0.310	1.00	1.00	0.310	No
194	12.75	0.70	0.12	0.58	0.97	0.418	1.34	0.311	1.00	1.00	0.311	No
195	12.80	0.70	0.12	0.58	0.97	0.419	1.34	0.312	1.00	1.00	0.312	No
196	12.90	0.71	0.12	0.58	0.97	0.420	1.34	0.313	1.00	1.00	0.313	No
197	12.95	0.71	0.12	0.58	0.97	0.421	1.34	0.313	1.00	1.00	0.313	No
198	13.02	0.71	0.13	0.59	0.97	0.422	1.34	0.314	1.00	1.00	0.314	No
199	13.06	0.71	0.13	0.59	0.97	0.423	1.34	0.314	1.00	1.00	0.314	No
200	13.14	0.72	0.13	0.59	0.97	0.424	1.34	0.315	1.00	1.00	0.315	No
201	13.19	0.72	0.13	0.59	0.97	0.425	1.34	0.316	1.00	1.00	0.316	No
202	13.29	0.73	0.13	0.59	0.97	0.426	1.34	0.317	1.00	1.00	0.317	No
203	13.33	0.73	0.14	0.59	0.97	0.427	1.34	0.317	1.00	1.00	0.317	No
204	13.39	0.73	0.14	0.60	0.97	0.427	1.34	0.318	1.00	1.00	0.318	No
205	13.48	0.74	0.14	0.60	0.97	0.429	1.34	0.319	1.00	1.00	0.319	No
206	13.54	0.74	0.14	0.60	0.97	0.430	1.34	0.319	1.00	1.00	0.319	No
207	13.59	0.74	0.14	0.60	0.97	0.430	1.34	0.320	1.00	1.00	0.320	No
208	13.67	0.75	0.15	0.60	0.97	0.431	1.34	0.321	1.00	1.00	0.321	No
209	13.72	0.75	0.15	0.60	0.97	0.432	1.34	0.321	1.00	1.00	0.321	No
210	13.78	0.75	0.15	0.60	0.97	0.433	1.34	0.322	1.00	1.00	0.322	No
211	13.86	0.76	0.15	0.61	0.97	0.434	1.34	0.323	1.00	1.00	0.323	No
212	13.93	0.76	0.15	0.61	0.97	0.435	1.34	0.323	1.00	1.00	0.323	No
213	14.01	0.77	0.16	0.61	0.97	0.436	1.34	0.324	1.00	1.00	0.324	No
214	14.05	0.77	0.16	0.61	0.97	0.436	1.34	0.325	1.00	1.00	0.325	No
215	14.14	0.77	0.16	0.61	0.97	0.438	1.34	0.325	1.00	1.00	0.325	No
216	14.21	0.78	0.16	0.62	0.97	0.439	1.34	0.326	1.00	1.00	0.326	No
217	14.24	0.78	0.16	0.62	0.97	0.439	1.34	0.326	1.00	1.00	0.326	No
218	14.31	0.78	0.17	0.62	0.97	0.440	1.34	0.327	1.00	1.00	0.327	No
219	14.39	0.79	0.17	0.62	0.97	0.441	1.34	0.328	1.00	1.00	0.328	No
220	14.44	0.79	0.17	0.62	0.97	0.441	1.34	0.328	1.00	1.00	0.328	No
221	14.54	0.80	0.17	0.62	0.97	0.443	1.34	0.329	1.00	1.00	0.329	No
222	14.59	0.80	0.17	0.62	0.97	0.443	1.34	0.330	1.00	1.00	0.330	No
223	14.64	0.80	0.18	0.63	0.97	0.444	1.34	0.330	1.00	1.00	0.330	No
224	14.70	0.80	0.18	0.63	0.97	0.445	1.34	0.331	1.00	1.00	0.331	No
225	14.79	0.81	0.18	0.63	0.97	0.446	1.34	0.332	1.00	1.00	0.332	No
226	14.83	0.81	0.18	0.63	0.97	0.446	1.34	0.332	1.00	1.00	0.332	No
227	14.93	0.82	0.19	0.63	0.97	0.448	1.34	0.333	1.00	1.00	0.333	No
228	14.98	0.82	0.19	0.63	0.97	0.448	1.34	0.333	1.00	1.00	0.333	No
229	15.03	0.82	0.19	0.64	0.97	0.449	1.34	0.334	1.00	1.00	0.334	No
230	15.10	0.83	0.19	0.64	0.97	0.450	1.34	0.334	1.00	1.00	0.334	No
231	15.18	0.83	0.19	0.64	0.97	0.451	1.34	0.335	1.00	1.00	0.335	No
232	15.23	0.83	0.19	0.64	0.97	0.451	1.34	0.336	1.00	1.00	0.336	No
233	15.33	0.84	0.20	0.64	0.97	0.452	1.34	0.336	1.00	1.00	0.336	No
234	15.37	0.84	0.20	0.64	0.97	0.453	1.34	0.337	1.00	1.00	0.337	No
235	15.44	0.85	0.20	0.65	0.97	0.454	1.34	0.337	1.00	1.00	0.337	No
236	15.52	0.85	0.20	0.65	0.97	0.455	1.34	0.338	1.00	1.00	0.338	No
237	15.56	0.85	0.20	0.65	0.97	0.455	1.34	0.338	1.00	1.00	0.338	No
238	15.63	0.86	0.21	0.65	0.97	0.456	1.34	0.339	1.00	1.00	0.339	No
239	15.71	0.86	0.21	0.65	0.97	0.457	1.34	0.340	1.00	1.00	0.340	No
240	15.77	0.86	0.21	0.65	0.97	0.458	1.34	0.340	1.00	1.00	0.340	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
241	15.82	0.87	0.21	0.65	0.97	0.458	1.34	0.341	1.00	1.00	0.341	No
242	15.89	0.87	0.21	0.66	0.97	0.459	1.34	0.341	1.00	1.00	0.341	No
243	15.97	0.87	0.22	0.66	0.97	0.460	1.34	0.342	1.00	1.00	0.342	No
244	16.02	0.88	0.22	0.66	0.97	0.460	1.34	0.342	1.00	1.00	0.342	No
245	16.10	0.88	0.22	0.66	0.97	0.461	1.34	0.343	1.00	1.00	0.343	No
246	16.17	0.89	0.22	0.66	0.97	0.462	1.34	0.344	1.00	1.00	0.344	No
247	16.22	0.89	0.23	0.66	0.97	0.463	1.34	0.344	1.00	1.00	0.344	No
248	16.28	0.89	0.23	0.66	0.97	0.463	1.34	0.345	1.00	1.00	0.345	No
249	16.37	0.90	0.23	0.67	0.97	0.464	1.34	0.345	1.00	1.00	0.345	No
250	16.42	0.90	0.23	0.67	0.97	0.465	1.34	0.346	1.00	1.00	0.346	No
251	16.52	0.90	0.23	0.67	0.97	0.466	1.34	0.347	1.00	1.00	0.347	No
252	16.55	0.91	0.24	0.67	0.97	0.466	1.34	0.347	1.00	1.00	0.347	No
253	16.62	0.91	0.24	0.67	0.96	0.467	1.34	0.347	1.00	1.00	0.347	No
254	16.70	0.91	0.24	0.67	0.96	0.468	1.34	0.348	1.00	1.00	0.348	No
255	16.74	0.92	0.24	0.67	0.96	0.468	1.34	0.348	1.00	1.00	0.348	No
256	16.82	0.92	0.24	0.68	0.96	0.469	1.34	0.349	1.00	1.00	0.349	No
257	16.91	0.92	0.25	0.68	0.96	0.470	1.34	0.350	1.00	1.00	0.350	No
258	16.94	0.93	0.25	0.68	0.96	0.471	1.34	0.350	1.00	1.00	0.350	No
259	17.01	0.93	0.25	0.68	0.96	0.471	1.34	0.351	1.00	1.00	0.351	No
260	17.10	0.93	0.25	0.68	0.96	0.472	1.34	0.351	1.00	1.00	0.351	No
261	17.15	0.94	0.25	0.68	0.96	0.473	1.34	0.352	1.00	1.00	0.352	No
262	17.21	0.94	0.26	0.68	0.96	0.473	1.34	0.352	1.00	1.00	0.352	No
263	17.30	0.95	0.26	0.69	0.96	0.474	1.34	0.353	1.00	1.00	0.353	No
264	17.34	0.95	0.26	0.69	0.96	0.475	1.34	0.353	1.00	1.00	0.353	No
265	17.41	0.95	0.26	0.69	0.96	0.475	1.34	0.354	1.00	1.00	0.354	No
266	17.49	0.96	0.26	0.69	0.96	0.476	1.34	0.354	1.00	1.00	0.354	No
267	17.53	0.96	0.27	0.69	0.96	0.477	1.34	0.355	1.00	1.00	0.355	No
268	17.59	0.96	0.27	0.69	0.96	0.477	1.34	0.355	1.00	1.00	0.355	No
269	17.67	0.97	0.27	0.69	0.96	0.478	1.34	0.356	1.00	1.00	0.356	No
270	17.73	0.97	0.27	0.70	0.96	0.479	1.34	0.356	1.00	1.00	0.356	No
271	17.79	0.97	0.27	0.70	0.96	0.479	1.34	0.356	1.00	1.00	0.356	No
272	17.87	0.98	0.28	0.70	0.96	0.480	1.34	0.357	1.00	1.00	0.357	No
273	17.92	0.98	0.28	0.70	0.96	0.481	1.34	0.357	1.00	1.00	0.357	No
274	17.99	0.98	0.28	0.70	0.96	0.481	1.34	0.358	1.00	1.00	0.358	No
275	18.07	0.99	0.28	0.70	0.96	0.482	1.34	0.359	1.00	1.00	0.359	No
276	18.14	0.99	0.29	0.71	0.96	0.483	1.34	0.359	1.00	1.00	0.359	No
277	18.19	0.99	0.29	0.71	0.96	0.483	1.34	0.359	1.00	1.00	0.359	No
278	18.26	1.00	0.29	0.71	0.96	0.484	1.34	0.360	1.00	1.00	0.360	No
279	18.34	1.00	0.29	0.71	0.96	0.485	1.34	0.360	1.00	1.00	0.360	No
280	18.38	1.00	0.29	0.71	0.96	0.485	1.34	0.361	1.00	1.00	0.361	No
281	18.45	1.01	0.29	0.71	0.96	0.486	1.34	0.361	1.00	1.00	0.361	No
282	18.53	1.01	0.30	0.71	0.96	0.487	1.34	0.362	1.00	1.00	0.362	No
283	18.60	1.01	0.30	0.71	0.96	0.487	1.34	0.362	1.00	1.00	0.362	No
284	18.68	1.02	0.30	0.72	0.96	0.488	1.34	0.363	1.00	1.00	0.363	No
285	18.72	1.02	0.30	0.72	0.96	0.488	1.34	0.363	1.00	1.00	0.363	No
286	18.79	1.02	0.31	0.72	0.96	0.489	1.34	0.364	1.00	1.00	0.364	No
287	18.84	1.03	0.31	0.72	0.96	0.489	1.34	0.364	1.00	1.00	0.364	No
288	18.92	1.03	0.31	0.72	0.96	0.490	1.34	0.365	1.00	1.00	0.365	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
289	18.98	1.03	0.31	0.72	0.96	0.491	1.34	0.365	1.00	1.00	0.365	No
290	19.06	1.04	0.31	0.72	0.96	0.491	1.34	0.366	1.00	1.00	0.366	No
291	19.11	1.04	0.32	0.73	0.96	0.492	1.34	0.366	1.00	1.00	0.366	No
292	19.18	1.04	0.32	0.73	0.96	0.493	1.34	0.366	1.00	1.00	0.366	No
293	19.25	1.05	0.32	0.73	0.96	0.493	1.34	0.367	1.00	1.00	0.367	No
294	19.33	1.05	0.32	0.73	0.96	0.494	1.34	0.367	1.00	1.00	0.367	No
295	19.37	1.05	0.32	0.73	0.96	0.494	1.34	0.368	1.00	1.00	0.368	No
296	19.47	1.06	0.33	0.73	0.96	0.495	1.34	0.368	1.00	1.00	0.368	No
297	19.52	1.06	0.33	0.73	0.96	0.496	1.34	0.369	1.00	1.00	0.369	No
298	19.57	1.06	0.33	0.73	0.96	0.496	1.34	0.369	1.00	1.00	0.369	No
299	19.62	1.07	0.33	0.74	0.96	0.497	1.34	0.369	1.00	1.00	0.369	No
300	19.71	1.07	0.33	0.74	0.96	0.497	1.34	0.370	1.00	1.00	0.370	No
301	19.77	1.07	0.34	0.74	0.96	0.498	1.34	0.370	1.00	1.00	0.370	No
302	19.82	1.08	0.34	0.74	0.96	0.498	1.34	0.371	1.00	1.00	0.371	No
303	19.91	1.08	0.34	0.74	0.96	0.499	1.34	0.371	1.00	1.00	0.371	No
304	19.96	1.08	0.34	0.74	0.96	0.500	1.34	0.372	1.00	1.00	0.372	No
305	20.02	1.09	0.34	0.74	0.96	0.500	1.34	0.372	1.00	1.00	0.372	No
306	20.11	1.09	0.35	0.75	0.96	0.501	1.34	0.373	1.00	1.00	0.373	No
307	20.18	1.10	0.35	0.75	0.96	0.502	1.34	0.373	1.00	1.00	0.373	No
308	20.23	1.10	0.35	0.75	0.96	0.502	1.34	0.373	1.00	1.00	0.373	No
309	20.28	1.10	0.35	0.75	0.96	0.502	1.34	0.374	1.00	1.00	0.374	No
310	20.37	1.11	0.35	0.75	0.96	0.503	1.34	0.374	1.00	1.00	0.374	No
311	20.42	1.11	0.36	0.75	0.96	0.504	1.34	0.375	1.00	1.00	0.375	No
312	20.48	1.11	0.36	0.75	0.96	0.504	1.34	0.375	1.00	1.00	0.375	No
313	20.56	1.12	0.36	0.75	0.96	0.505	1.34	0.375	1.00	1.00	0.375	No
314	20.63	1.12	0.36	0.76	0.96	0.505	1.34	0.376	1.00	1.00	0.376	No
315	20.67	1.12	0.36	0.76	0.96	0.506	1.34	0.376	1.00	1.00	0.376	No
316	20.74	1.12	0.37	0.76	0.95	0.506	1.34	0.377	1.00	1.00	0.377	No
317	20.83	1.13	0.37	0.76	0.95	0.507	1.34	0.377	1.00	1.00	0.377	No
318	20.90	1.13	0.37	0.76	0.95	0.508	1.34	0.378	1.00	1.00	0.378	No
319	20.97	1.14	0.37	0.76	0.95	0.508	1.34	0.378	1.00	1.00	0.378	No
320	21.02	1.14	0.38	0.76	0.95	0.509	1.34	0.378	1.00	1.00	0.378	No
321	21.10	1.14	0.38	0.76	0.95	0.509	1.34	0.379	1.00	1.00	0.379	No
322	21.17	1.15	0.38	0.77	0.95	0.510	1.34	0.379	1.00	1.00	0.379	No
323	21.22	1.15	0.38	0.77	0.95	0.510	1.34	0.380	1.00	1.00	0.380	No
324	21.27	1.15	0.38	0.77	0.95	0.511	1.34	0.380	1.00	1.00	0.380	No
325	21.37	1.16	0.39	0.77	0.95	0.512	1.34	0.380	1.00	1.00	0.380	No
326	21.43	1.16	0.39	0.77	0.95	0.512	1.34	0.381	1.00	1.00	0.381	No
327	21.46	1.16	0.39	0.77	0.95	0.512	1.34	0.381	1.00	1.00	0.381	No
328	21.55	1.17	0.39	0.77	0.95	0.513	1.34	0.382	1.00	1.00	0.382	No
329	21.62	1.17	0.39	0.77	0.95	0.514	1.34	0.382	1.00	1.00	0.382	No
330	21.66	1.17	0.39	0.78	0.95	0.514	1.34	0.382	1.00	1.00	0.382	No
331	21.74	1.17	0.40	0.78	0.95	0.514	1.34	0.383	1.00	1.00	0.383	No
332	21.81	1.18	0.40	0.78	0.95	0.515	1.34	0.383	1.00	1.00	0.383	No
333	21.85	1.18	0.40	0.78	0.95	0.515	1.34	0.383	1.00	1.00	0.383	No
334	21.93	1.18	0.40	0.78	0.95	0.516	1.34	0.384	1.00	1.00	0.384	No
335	22.00	1.19	0.41	0.78	0.95	0.516	1.34	0.384	1.00	1.00	0.384	No
336	22.07	1.19	0.41	0.78	0.95	0.517	1.34	0.385	1.00	1.00	0.385	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
337	22.16	1.20	0.41	0.79	0.95	0.518	1.34	0.385	1.00	1.00	0.385	No
338	22.19	1.20	0.41	0.79	0.95	0.518	1.34	0.385	1.00	1.00	0.385	No
339	22.26	1.20	0.41	0.79	0.95	0.518	1.34	0.386	1.00	1.00	0.386	No
340	22.33	1.20	0.42	0.79	0.95	0.519	1.34	0.386	1.00	1.00	0.386	No
341	22.40	1.21	0.42	0.79	0.95	0.519	1.34	0.386	1.00	1.00	0.386	No
342	22.45	1.21	0.42	0.79	0.95	0.520	1.34	0.387	1.00	1.00	0.387	No
343	22.53	1.21	0.42	0.79	0.95	0.520	1.34	0.387	1.00	1.00	0.387	No
344	22.60	1.22	0.42	0.79	0.95	0.521	1.34	0.387	1.00	1.00	0.387	No
345	22.64	1.22	0.43	0.79	0.95	0.521	1.34	0.388	1.00	1.00	0.388	No
346	22.70	1.22	0.43	0.80	0.95	0.522	1.34	0.388	1.00	1.00	0.388	No
347	22.80	1.23	0.43	0.80	0.95	0.522	1.34	0.389	1.00	1.00	0.389	No
348	22.84	1.23	0.43	0.80	0.95	0.523	1.34	0.389	1.00	1.00	0.389	No
349	22.90	1.23	0.43	0.80	0.95	0.523	1.34	0.389	1.00	1.00	0.389	No
350	23.00	1.24	0.44	0.80	0.95	0.524	1.34	0.390	1.00	1.00	0.390	No
351	23.05	1.24	0.44	0.80	0.95	0.524	1.34	0.390	1.00	1.00	0.390	No
352	23.14	1.25	0.44	0.80	0.95	0.525	1.34	0.390	1.00	1.00	0.390	No
353	23.18	1.25	0.44	0.81	0.95	0.525	1.34	0.391	1.00	1.00	0.391	No
354	23.24	1.25	0.44	0.81	0.95	0.525	1.34	0.391	1.00	1.00	0.391	No
355	23.32	1.25	0.45	0.81	0.95	0.526	1.34	0.391	1.00	1.00	0.391	No
356	23.39	1.26	0.45	0.81	0.95	0.526	1.34	0.392	1.00	1.00	0.392	No
357	23.44	1.26	0.45	0.81	0.95	0.527	1.34	0.392	1.00	1.00	0.392	No
358	23.53	1.27	0.45	0.81	0.95	0.527	1.34	0.392	1.00	1.00	0.392	No
359	23.59	1.27	0.46	0.81	0.95	0.528	1.34	0.392	1.00	1.00	0.392	No
360	23.63	1.27	0.46	0.81	0.95	0.528	1.34	0.393	1.00	1.00	0.393	No
361	23.69	1.27	0.46	0.82	0.95	0.528	1.34	0.393	1.00	1.00	0.393	No
362	23.77	1.28	0.46	0.82	0.95	0.529	1.34	0.393	1.00	1.00	0.393	No
363	23.82	1.28	0.46	0.82	0.95	0.529	1.34	0.394	1.00	1.00	0.394	No
364	23.93	1.29	0.47	0.82	0.95	0.530	1.34	0.394	1.00	1.00	0.394	No
365	23.95	1.29	0.47	0.82	0.95	0.530	1.34	0.394	1.00	1.00	0.394	No
366	24.03	1.29	0.47	0.82	0.95	0.530	1.34	0.394	1.00	1.00	0.394	No
367	24.12	1.30	0.47	0.83	0.94	0.531	1.34	0.395	1.00	1.00	0.395	No
368	24.16	1.30	0.47	0.83	0.94	0.531	1.34	0.395	1.00	1.00	0.395	No
369	24.22	1.30	0.47	0.83	0.94	0.531	1.34	0.395	1.00	1.00	0.395	No
370	24.30	1.31	0.48	0.83	0.94	0.532	1.34	0.396	1.00	1.00	0.396	No
371	24.37	1.31	0.48	0.83	0.94	0.532	1.34	0.396	1.00	1.00	0.396	No
372	24.43	1.31	0.48	0.83	0.94	0.533	1.34	0.396	1.00	1.00	0.396	No
373	24.50	1.32	0.48	0.83	0.94	0.533	1.34	0.397	1.00	1.00	0.397	No
374	24.57	1.32	0.49	0.83	0.94	0.534	1.34	0.397	1.00	1.00	0.397	No
375	24.62	1.32	0.49	0.84	0.94	0.534	1.34	0.397	1.00	1.00	0.397	No
376	24.69	1.33	0.49	0.84	0.94	0.534	1.34	0.397	1.00	1.00	0.397	No
377	24.77	1.33	0.49	0.84	0.94	0.535	1.34	0.398	1.00	1.00	0.398	No
378	24.83	1.33	0.49	0.84	0.94	0.535	1.34	0.398	1.00	1.00	0.398	No
379	24.88	1.34	0.50	0.84	0.94	0.535	1.34	0.398	1.00	1.00	0.398	No
380	24.97	1.34	0.50	0.84	0.94	0.536	1.34	0.399	1.00	1.00	0.399	No
381	25.02	1.34	0.50	0.84	0.94	0.536	1.34	0.399	1.00	1.00	0.399	No
382	25.11	1.35	0.50	0.85	0.94	0.537	1.34	0.399	1.00	1.00	0.399	No
383	25.17	1.35	0.50	0.85	0.94	0.537	1.34	0.399	1.00	1.00	0.399	No
384	25.21	1.35	0.51	0.85	0.94	0.537	1.34	0.400	1.00	1.00	0.400	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
385	25.29	1.36	0.51	0.85	0.94	0.538	1.34	0.400	1.00	1.00	0.400	No
386	25.36	1.36	0.51	0.85	0.94	0.538	1.34	0.400	1.00	1.00	0.400	No
387	25.40	1.36	0.51	0.85	0.94	0.538	1.34	0.400	1.00	1.00	0.400	No
388	25.46	1.37	0.51	0.85	0.94	0.538	1.34	0.401	1.00	1.00	0.401	No
389	25.54	1.37	0.52	0.85	0.94	0.539	1.34	0.401	1.00	1.00	0.401	No
390	25.62	1.37	0.52	0.86	0.94	0.539	1.34	0.401	1.00	1.00	0.401	No
391	25.66	1.38	0.52	0.86	0.94	0.540	1.34	0.401	1.00	1.00	0.401	No
392	25.75	1.38	0.52	0.86	0.94	0.540	1.34	0.402	1.00	1.00	0.402	No
393	25.80	1.38	0.52	0.86	0.94	0.540	1.34	0.402	1.00	1.00	0.402	No
394	25.85	1.39	0.53	0.86	0.94	0.540	1.34	0.402	1.00	1.00	0.402	No
395	25.96	1.39	0.53	0.86	0.94	0.541	1.34	0.402	1.00	1.00	0.402	No
396	26.01	1.40	0.53	0.86	0.94	0.541	1.34	0.403	1.00	1.00	0.403	No
397	26.05	1.40	0.53	0.87	0.94	0.541	1.34	0.403	1.00	1.00	0.403	No
398	26.12	1.40	0.53	0.87	0.94	0.542	1.34	0.403	1.00	1.00	0.403	No
399	26.19	1.41	0.54	0.87	0.94	0.542	1.34	0.403	1.00	1.00	0.403	No
400	26.25	1.41	0.54	0.87	0.94	0.542	1.34	0.403	1.00	1.00	0.403	No
401	26.33	1.41	0.54	0.87	0.94	0.543	1.34	0.404	1.00	1.00	0.404	No
402	26.42	1.42	0.54	0.87	0.94	0.543	1.34	0.404	1.00	1.00	0.404	No
403	26.46	1.42	0.54	0.87	0.94	0.543	1.34	0.404	1.00	1.00	0.404	No
404	26.52	1.42	0.55	0.88	0.94	0.543	1.34	0.404	1.00	1.00	0.404	No
405	26.61	1.43	0.55	0.88	0.94	0.544	1.34	0.404	1.00	1.00	0.404	No
406	26.67	1.43	0.55	0.88	0.94	0.544	1.34	0.405	1.00	1.00	0.405	No
407	26.71	1.43	0.55	0.88	0.94	0.544	1.34	0.405	1.00	1.00	0.405	No
408	26.79	1.44	0.56	0.88	0.94	0.545	1.34	0.405	1.00	1.00	0.405	No
409	26.87	1.44	0.56	0.88	0.93	0.545	1.34	0.405	1.00	1.00	0.405	No
410	26.92	1.44	0.56	0.88	0.93	0.545	1.34	0.405	1.00	1.00	0.405	No
411	26.98	1.45	0.56	0.89	0.93	0.545	1.34	0.406	1.00	1.00	0.406	No
412	27.06	1.45	0.56	0.89	0.93	0.546	1.34	0.406	1.00	1.00	0.406	No
413	27.11	1.45	0.57	0.89	0.93	0.546	1.34	0.406	1.00	1.00	0.406	No
414	27.21	1.46	0.57	0.89	0.93	0.546	1.34	0.406	1.00	1.00	0.406	No
415	27.26	1.46	0.57	0.89	0.93	0.547	1.34	0.407	1.00	1.00	0.407	No
416	27.32	1.47	0.57	0.89	0.93	0.547	1.34	0.407	1.00	1.00	0.407	No
417	27.40	1.47	0.57	0.90	0.93	0.547	1.34	0.407	1.00	1.00	0.407	No
418	27.45	1.47	0.58	0.90	0.93	0.547	1.34	0.407	1.00	1.00	0.407	No
419	27.52	1.48	0.58	0.90	0.93	0.548	1.34	0.407	1.00	1.00	0.407	No
420	27.60	1.48	0.58	0.90	0.93	0.548	1.34	0.408	1.00	1.00	0.408	No
421	27.65	1.48	0.58	0.90	0.93	0.548	1.34	0.408	1.00	1.00	0.408	No
422	27.71	1.49	0.58	0.90	0.93	0.549	1.34	0.408	1.00	1.00	0.408	No
423	27.80	1.49	0.59	0.90	0.93	0.549	1.34	0.408	1.00	1.00	0.408	No
424	27.84	1.49	0.59	0.90	0.93	0.549	1.34	0.408	1.00	1.00	0.408	No
425	27.90	1.49	0.59	0.91	0.93	0.549	1.34	0.409	1.00	1.00	0.409	No
426	27.99	1.50	0.59	0.91	0.93	0.550	1.34	0.409	1.00	1.00	0.409	No
427	28.05	1.50	0.59	0.91	0.93	0.550	1.34	0.409	1.00	1.00	0.409	No
428	28.10	1.51	0.60	0.91	0.93	0.550	1.34	0.409	1.00	1.00	0.409	No
429	28.17	1.51	0.60	0.91	0.93	0.550	1.34	0.409	1.00	1.00	0.409	No
430	28.25	1.51	0.60	0.91	0.93	0.551	1.34	0.410	1.00	1.00	0.410	No
431	28.30	1.52	0.60	0.91	0.93	0.551	1.34	0.410	1.00	1.00	0.410	No
432	28.39	1.52	0.60	0.92	0.93	0.551	1.34	0.410	1.00	1.00	0.410	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
433	28.44	1.52	0.61	0.92	0.93	0.551	1.34	0.410	1.00	1.00	0.410	No
434	28.49	1.53	0.61	0.92	0.93	0.552	1.34	0.410	1.00	1.00	0.410	No
435	28.54	1.53	0.61	0.92	0.93	0.552	1.34	0.410	1.00	1.00	0.410	No
436	28.62	1.53	0.61	0.92	0.93	0.552	1.34	0.411	1.00	1.00	0.411	No
437	28.68	1.54	0.61	0.92	0.93	0.552	1.34	0.411	1.00	1.00	0.411	No
438	28.74	1.54	0.62	0.92	0.93	0.553	1.34	0.411	1.00	1.00	0.411	No
439	28.83	1.54	0.62	0.92	0.93	0.553	1.34	0.411	1.00	1.00	0.411	No
440	28.89	1.55	0.62	0.93	0.93	0.553	1.34	0.411	1.00	1.00	0.411	No
441	28.98	1.55	0.62	0.93	0.93	0.553	1.34	0.412	1.00	1.00	0.412	No
442	29.03	1.55	0.62	0.93	0.93	0.553	1.34	0.412	1.00	1.00	0.412	No
443	29.09	1.56	0.63	0.93	0.93	0.554	1.34	0.412	1.00	1.00	0.412	No
444	29.14	1.56	0.63	0.93	0.92	0.554	1.34	0.412	1.00	1.00	0.412	No
445	29.22	1.56	0.63	0.93	0.92	0.554	1.34	0.412	1.00	1.00	0.412	No
446	29.27	1.57	0.63	0.93	0.92	0.554	1.34	0.412	1.00	1.00	0.412	No
447	29.38	1.57	0.64	0.94	0.92	0.555	1.34	0.412	1.00	1.00	0.412	No
448	29.43	1.57	0.64	0.94	0.92	0.555	1.34	0.413	1.00	1.00	0.413	No
449	29.48	1.58	0.64	0.94	0.92	0.555	1.34	0.413	1.00	1.00	0.413	No
450	29.57	1.58	0.64	0.94	0.92	0.555	1.34	0.413	1.00	1.00	0.413	No
451	29.62	1.58	0.64	0.94	0.92	0.555	1.34	0.413	1.00	1.00	0.413	No
452	29.68	1.59	0.65	0.94	0.92	0.555	1.34	0.413	1.00	1.00	0.413	No
453	29.73	1.59	0.65	0.94	0.92	0.556	1.34	0.413	1.00	1.00	0.413	No
454	29.82	1.59	0.65	0.95	0.92	0.556	1.34	0.413	1.00	1.00	0.413	No
455	29.87	1.60	0.65	0.95	0.92	0.556	1.34	0.413	1.00	1.00	0.413	No
456	29.94	1.60	0.65	0.95	0.92	0.556	1.34	0.414	1.00	1.00	0.414	No
457	30.02	1.61	0.66	0.95	0.92	0.556	1.34	0.414	1.00	1.00	0.414	No
458	30.07	1.61	0.66	0.95	0.92	0.556	1.34	0.414	1.00	1.00	0.414	No
459	30.16	1.61	0.66	0.95	0.92	0.557	1.34	0.414	1.00	1.00	0.414	No
460	30.19	1.61	0.66	0.95	0.92	0.557	1.34	0.414	1.00	1.00	0.414	No
461	30.26	1.62	0.66	0.95	0.92	0.557	1.34	0.414	1.00	1.00	0.414	No
462	30.36	1.62	0.67	0.96	0.92	0.557	1.34	0.414	1.00	1.00	0.414	No
463	30.41	1.63	0.67	0.96	0.92	0.557	1.34	0.415	1.00	1.00	0.415	No
464	30.46	1.63	0.67	0.96	0.92	0.558	1.34	0.415	1.00	1.00	0.415	No
465	30.53	1.63	0.67	0.96	0.92	0.558	1.34	0.415	1.00	1.00	0.415	No
466	30.61	1.64	0.67	0.96	0.92	0.558	1.34	0.415	1.00	1.00	0.415	No
467	30.65	1.64	0.68	0.96	0.92	0.558	1.34	0.415	1.00	1.00	0.415	No
468	30.71	1.64	0.68	0.96	0.92	0.558	1.34	0.415	1.00	1.00	0.415	No
469	30.81	1.65	0.68	0.97	0.92	0.558	1.34	0.415	1.00	1.00	0.415	No
470	30.84	1.65	0.68	0.97	0.92	0.558	1.34	0.415	1.00	1.00	0.415	No
471	30.91	1.65	0.68	0.97	0.92	0.559	1.34	0.415	1.00	1.00	0.415	No
472	30.99	1.66	0.69	0.97	0.92	0.559	1.34	0.416	1.00	1.00	0.416	No
473	31.04	1.66	0.69	0.97	0.92	0.559	1.34	0.416	1.00	1.00	0.416	No
474	31.11	1.66	0.69	0.97	0.91	0.559	1.34	0.416	1.00	1.00	0.416	No
475	31.19	1.67	0.69	0.97	0.91	0.559	1.34	0.416	1.00	1.00	0.416	No
476	31.25	1.67	0.69	0.98	0.91	0.559	1.34	0.416	1.00	1.00	0.416	No
477	31.30	1.67	0.70	0.98	0.91	0.559	1.34	0.416	1.00	1.00	0.416	No
478	31.39	1.68	0.70	0.98	0.91	0.560	1.34	0.416	1.00	1.00	0.416	No
479	31.45	1.68	0.70	0.98	0.91	0.560	1.34	0.416	1.00	1.00	0.416	No
480	31.50	1.68	0.70	0.98	0.91	0.560	1.34	0.416	1.00	1.00	0.416	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
481	31.60	1.69	0.71	0.98	0.91	0.560	1.34	0.416	1.00	1.00	0.416	No
482	31.65	1.69	0.71	0.98	0.91	0.560	1.34	0.416	1.00	1.00	0.416	No
483	31.73	1.70	0.71	0.99	0.91	0.560	1.34	0.417	1.00	1.00	0.417	No
484	31.80	1.70	0.71	0.99	0.91	0.560	1.34	0.417	1.00	1.00	0.417	No
485	31.84	1.70	0.71	0.99	0.91	0.560	1.34	0.417	1.00	1.00	0.417	No
486	31.91	1.71	0.71	0.99	0.91	0.560	1.34	0.417	1.00	1.00	0.417	No
487	31.99	1.71	0.72	0.99	0.91	0.560	1.34	0.417	1.00	1.00	0.417	No
488	32.03	1.71	0.72	0.99	0.91	0.560	1.34	0.417	1.00	1.00	0.417	No
489	32.09	1.71	0.72	0.99	0.91	0.561	1.34	0.417	1.00	1.00	0.417	No
490	32.19	1.72	0.72	1.00	0.91	0.561	1.34	0.417	1.00	1.00	0.417	No
491	32.25	1.72	0.73	1.00	0.91	0.561	1.34	0.417	1.00	1.00	0.417	No
492	32.29	1.73	0.73	1.00	0.91	0.561	1.34	0.417	1.00	1.00	0.417	No
493	32.38	1.73	0.73	1.00	0.91	0.561	1.34	0.417	1.00	1.00	0.417	No
494	32.43	1.73	0.73	1.00	0.91	0.561	1.34	0.417	1.00	1.00	0.417	No
495	32.48	1.74	0.73	1.00	0.91	0.561	1.34	0.417	1.00	1.00	0.417	No
496	32.58	1.74	0.74	1.01	0.91	0.561	1.34	0.417	1.00	1.00	0.417	No
497	32.63	1.74	0.74	1.01	0.91	0.561	1.34	0.417	1.00	1.00	0.417	No
498	32.69	1.75	0.74	1.01	0.91	0.561	1.34	0.417	1.00	1.00	0.417	No
499	32.74	1.75	0.74	1.01	0.91	0.561	1.34	0.417	1.00	1.00	0.417	No
500	32.83	1.76	0.74	1.01	0.90	0.561	1.34	0.417	1.00	1.00	0.417	No
501	32.88	1.76	0.75	1.01	0.90	0.561	1.34	0.417	1.00	1.00	0.417	No
502	32.97	1.76	0.75	1.02	0.90	0.561	1.34	0.417	1.00	1.00	0.417	No
503	33.01	1.77	0.75	1.02	0.90	0.561	1.34	0.417	1.00	1.00	0.417	No
504	33.07	1.77	0.75	1.02	0.90	0.561	1.34	0.417	1.00	1.00	0.417	No
505	33.16	1.77	0.75	1.02	0.90	0.561	1.34	0.418	1.00	1.00	0.418	No
506	33.20	1.78	0.76	1.02	0.90	0.561	1.34	0.418	1.00	1.00	0.418	No
507	33.27	1.78	0.76	1.02	0.90	0.561	1.34	0.418	1.00	1.00	0.418	No
508	33.36	1.78	0.76	1.02	0.90	0.561	1.34	0.418	1.00	1.00	0.418	No
509	33.42	1.79	0.76	1.03	0.90	0.561	1.34	0.418	1.00	1.00	0.418	No
510	33.51	1.79	0.76	1.03	0.90	0.561	1.34	0.418	1.00	1.00	0.418	No
511	33.56	1.80	0.77	1.03	0.90	0.561	1.34	0.418	1.00	1.00	0.418	No
512	33.61	1.80	0.77	1.03	0.90	0.561	1.34	0.418	1.00	1.00	0.418	No
513	33.67	1.80	0.77	1.03	0.90	0.562	1.34	0.418	1.00	1.00	0.418	No
514	33.76	1.81	0.77	1.03	0.90	0.562	1.34	0.418	1.00	1.00	0.418	No
515	33.81	1.81	0.77	1.03	0.90	0.562	1.34	0.418	1.00	1.00	0.418	No
516	33.86	1.81	0.78	1.04	0.90	0.562	1.34	0.418	1.00	1.00	0.418	No
517	33.94	1.82	0.78	1.04	0.90	0.562	1.34	0.418	1.00	1.00	0.418	No
518	34.02	1.82	0.78	1.04	0.90	0.562	1.34	0.418	1.00	1.00	0.418	No
519	34.06	1.82	0.78	1.04	0.90	0.562	1.34	0.418	1.00	1.00	0.418	No
520	34.14	1.83	0.78	1.04	0.90	0.562	1.34	0.418	1.00	1.00	0.418	No
521	34.21	1.83	0.79	1.04	0.90	0.562	1.34	0.418	1.00	1.00	0.418	No
522	34.25	1.83	0.79	1.04	0.90	0.562	1.34	0.418	1.00	1.00	0.418	No
523	34.33	1.84	0.79	1.05	0.90	0.562	1.34	0.418	1.00	1.00	0.418	No
524	34.41	1.84	0.79	1.05	0.89	0.562	1.34	0.418	1.00	1.00	0.418	No
525	34.49	1.85	0.80	1.05	0.89	0.562	1.34	0.418	1.00	1.00	0.418	No
526	34.56	1.85	0.80	1.05	0.89	0.562	1.34	0.418	1.00	1.00	0.418	No
527	34.59	1.85	0.80	1.05	0.89	0.562	1.34	0.418	1.00	1.00	0.418	No
528	34.67	1.85	0.80	1.05	0.89	0.562	1.34	0.418	1.00	1.00	0.418	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
529	34.76	1.86	0.80	1.06	0.89	0.562	1.34	0.418	1.00	1.00	0.418	No
530	34.80	1.86	0.80	1.06	0.89	0.562	1.34	0.418	1.00	1.00	0.418	No
531	34.85	1.86	0.81	1.06	0.89	0.562	1.34	0.418	1.00	1.00	0.418	No
532	34.93	1.87	0.81	1.06	0.89	0.562	1.34	0.418	1.00	1.00	0.418	No
533	34.98	1.87	0.81	1.06	0.89	0.562	1.34	0.418	1.00	1.00	0.418	No
534	35.05	1.87	0.81	1.06	0.89	0.562	1.34	0.418	1.00	1.00	0.418	No
535	35.13	1.88	0.82	1.06	0.89	0.562	1.34	0.418	1.00	1.00	0.418	No
536	35.18	1.88	0.82	1.06	0.89	0.562	1.34	0.418	1.00	1.00	0.419	No
537	35.24	1.88	0.82	1.07	0.89	0.562	1.34	0.418	1.00	1.00	0.419	No
538	35.32	1.89	0.82	1.07	0.89	0.562	1.34	0.418	1.00	1.00	0.419	No
539	35.41	1.89	0.82	1.07	0.89	0.562	1.34	0.418	1.00	1.00	0.419	No
540	35.46	1.90	0.83	1.07	0.89	0.562	1.34	0.418	1.00	1.00	0.419	No
541	35.51	1.90	0.83	1.07	0.89	0.562	1.34	0.418	1.00	1.00	0.419	No
542	35.58	1.90	0.83	1.07	0.89	0.562	1.34	0.418	1.00	1.00	0.419	No
543	35.66	1.91	0.83	1.07	0.89	0.562	1.34	0.418	1.00	1.00	0.419	No
544	35.71	1.91	0.83	1.08	0.89	0.562	1.34	0.418	1.00	1.00	0.419	No
545	35.76	1.91	0.83	1.08	0.89	0.562	1.34	0.418	1.00	1.00	0.420	No
546	35.86	1.92	0.84	1.08	0.88	0.562	1.34	0.418	1.00	1.00	0.420	No
547	35.91	1.92	0.84	1.08	0.88	0.562	1.34	0.418	1.00	1.00	0.420	No
548	36.01	1.92	0.84	1.08	0.88	0.562	1.34	0.418	0.99	1.00	0.420	No
549	36.05	1.93	0.84	1.08	0.88	0.562	1.34	0.418	0.99	1.00	0.420	No
550	36.12	1.93	0.85	1.08	0.88	0.562	1.34	0.418	0.99	1.00	0.420	No
551	36.20	1.93	0.85	1.09	0.88	0.562	1.34	0.418	0.99	1.00	0.420	No
552	36.23	1.94	0.85	1.09	0.88	0.562	1.34	0.418	0.99	1.00	0.420	No
553	36.31	1.94	0.85	1.09	0.88	0.562	1.34	0.418	0.99	1.00	0.421	No
554	36.35	1.94	0.85	1.09	0.88	0.562	1.34	0.418	0.99	1.00	0.421	No
555	36.45	1.95	0.86	1.09	0.88	0.562	1.34	0.418	0.99	1.00	0.421	No
556	36.51	1.95	0.86	1.09	0.88	0.562	1.34	0.418	0.99	1.00	0.421	No
557	36.58	1.95	0.86	1.09	0.88	0.562	1.34	0.418	0.99	1.00	0.421	No
558	36.66	1.96	0.86	1.09	0.88	0.562	1.34	0.418	0.99	1.00	0.421	No
559	36.70	1.96	0.86	1.10	0.88	0.562	1.34	0.418	0.99	1.00	0.421	No
560	36.80	1.96	0.87	1.10	0.88	0.562	1.34	0.418	0.99	1.00	0.421	No
561	36.85	1.97	0.87	1.10	0.88	0.562	1.34	0.418	0.99	1.00	0.421	No
562	36.89	1.97	0.87	1.10	0.88	0.562	1.34	0.418	0.99	1.00	0.421	No
563	36.96	1.97	0.87	1.10	0.88	0.562	1.34	0.418	0.99	1.00	0.421	No
564	37.03	1.98	0.87	1.10	0.88	0.562	1.34	0.418	0.99	1.00	0.422	No
565	37.09	1.98	0.88	1.10	0.88	0.561	1.34	0.418	0.99	1.00	0.422	No
566	37.15	1.98	0.88	1.10	0.87	0.561	1.34	0.418	0.99	1.00	0.422	No
567	37.23	1.99	0.88	1.11	0.87	0.561	1.34	0.417	0.99	1.00	0.422	No
568	37.27	1.99	0.88	1.11	0.87	0.561	1.34	0.417	0.99	1.00	0.422	No
569	37.34	1.99	0.88	1.11	0.87	0.561	1.34	0.417	0.99	1.00	0.422	No
570	37.43	2.00	0.89	1.11	0.87	0.561	1.34	0.417	0.99	1.00	0.422	No
571	37.49	2.00	0.89	1.11	0.87	0.561	1.34	0.417	0.99	1.00	0.422	No
572	37.54	2.00	0.89	1.11	0.87	0.561	1.34	0.417	0.99	1.00	0.422	No
573	37.62	2.01	0.89	1.11	0.87	0.561	1.34	0.417	0.99	1.00	0.422	No
574	37.69	2.01	0.90	1.12	0.87	0.561	1.34	0.417	0.99	1.00	0.422	No
575	37.74	2.01	0.90	1.12	0.87	0.561	1.34	0.417	0.99	1.00	0.422	No
576	37.82	2.02	0.90	1.12	0.87	0.561	1.34	0.417	0.99	1.00	0.422	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
577	37.89	2.02	0.90	1.12	0.87	0.561	1.34	0.417	0.99	1.00	0.422	No
578	37.93	2.02	0.90	1.12	0.87	0.561	1.34	0.417	0.99	1.00	0.422	No
579	38.02	2.03	0.91	1.12	0.87	0.560	1.34	0.417	0.99	1.00	0.423	No
580	38.08	2.03	0.91	1.12	0.87	0.560	1.34	0.417	0.99	1.00	0.423	No
581	38.13	2.03	0.91	1.12	0.87	0.560	1.34	0.417	0.99	1.00	0.423	No
582	38.23	2.04	0.91	1.13	0.87	0.560	1.34	0.417	0.99	1.00	0.423	No
583	38.28	2.04	0.91	1.13	0.87	0.560	1.34	0.417	0.99	1.00	0.423	No
584	38.35	2.05	0.92	1.13	0.87	0.560	1.34	0.416	0.99	1.00	0.423	No
585	38.42	2.05	0.92	1.13	0.86	0.560	1.34	0.416	0.98	1.00	0.423	No
586	38.47	2.05	0.92	1.13	0.86	0.560	1.34	0.416	0.98	1.00	0.423	No
587	38.52	2.05	0.92	1.13	0.86	0.560	1.34	0.416	0.98	1.00	0.423	No
588	38.61	2.06	0.92	1.14	0.86	0.560	1.34	0.416	0.98	1.00	0.423	No
589	38.67	2.06	0.93	1.14	0.86	0.559	1.34	0.416	0.98	1.00	0.423	No
590	38.72	2.07	0.93	1.14	0.86	0.559	1.34	0.416	0.98	1.00	0.423	No
591	38.82	2.07	0.93	1.14	0.86	0.559	1.34	0.416	0.98	1.00	0.423	No
592	38.86	2.07	0.93	1.14	0.86	0.559	1.34	0.416	0.98	1.00	0.423	No
593	38.96	2.08	0.93	1.14	0.86	0.559	1.34	0.416	0.98	1.00	0.423	No
594	39.01	2.08	0.94	1.14	0.86	0.559	1.34	0.416	0.98	1.00	0.423	No
595	39.05	2.08	0.94	1.14	0.86	0.559	1.34	0.416	0.98	1.00	0.423	No
596	39.13	2.09	0.94	1.15	0.86	0.559	1.34	0.415	0.98	1.00	0.423	No
597	39.21	2.09	0.94	1.15	0.86	0.558	1.34	0.415	0.98	1.00	0.423	No
598	39.24	2.09	0.94	1.15	0.86	0.558	1.34	0.415	0.98	1.00	0.423	No
599	39.31	2.10	0.95	1.15	0.86	0.558	1.34	0.415	0.98	1.00	0.423	No
600	39.40	2.10	0.95	1.15	0.86	0.558	1.34	0.415	0.98	1.00	0.423	No
601	39.44	2.10	0.95	1.15	0.86	0.558	1.34	0.415	0.98	1.00	0.423	No
602	39.51	2.11	0.95	1.15	0.86	0.558	1.34	0.415	0.98	1.00	0.423	No
603	39.60	2.11	0.95	1.16	0.85	0.558	1.34	0.415	0.98	1.00	0.423	No
604	39.66	2.11	0.96	1.16	0.85	0.557	1.34	0.415	0.98	1.00	0.423	No
605	39.70	2.12	0.96	1.16	0.85	0.557	1.34	0.415	0.98	1.00	0.423	No
606	39.80	2.12	0.96	1.16	0.85	0.557	1.34	0.414	0.98	1.00	0.423	No
607	39.85	2.12	0.96	1.16	0.85	0.557	1.34	0.414	0.98	1.00	0.423	No
608	39.90	2.13	0.96	1.16	0.85	0.557	1.34	0.414	0.98	1.00	0.423	No
609	39.98	2.13	0.97	1.17	0.85	0.557	1.34	0.414	0.98	1.00	0.423	No
610	40.05	2.14	0.97	1.17	0.85	0.557	1.34	0.414	0.98	1.00	0.423	No
611	40.10	2.14	0.97	1.17	0.85	0.556	1.34	0.414	0.98	1.00	0.423	No
612	40.20	2.14	0.97	1.17	0.85	0.556	1.34	0.414	0.98	1.00	0.423	No
613	40.25	2.15	0.98	1.17	0.85	0.556	1.34	0.414	0.98	1.00	0.423	No
614	40.30	2.15	0.98	1.17	0.85	0.556	1.34	0.413	0.98	1.00	0.423	No
615	40.40	2.15	0.98	1.17	0.85	0.556	1.34	0.413	0.98	1.00	0.423	No
616	40.45	2.16	0.98	1.18	0.85	0.556	1.34	0.413	0.98	1.00	0.423	No
617	40.50	2.16	0.98	1.18	0.85	0.555	1.34	0.413	0.98	1.00	0.423	No
618	40.59	2.16	0.99	1.18	0.85	0.555	1.34	0.413	0.98	1.00	0.423	No
619	40.64	2.17	0.99	1.18	0.85	0.555	1.34	0.413	0.98	1.00	0.423	No
620	40.69	2.17	0.99	1.18	0.84	0.555	1.34	0.413	0.98	1.00	0.423	No
621	40.79	2.17	0.99	1.18	0.84	0.555	1.34	0.413	0.97	1.00	0.423	No
622	40.83	2.18	0.99	1.18	0.84	0.555	1.34	0.413	0.97	1.00	0.423	No
623	40.92	2.18	1.00	1.19	0.84	0.554	1.34	0.412	0.97	1.00	0.423	No
624	40.98	2.18	1.00	1.19	0.84	0.554	1.34	0.412	0.97	1.00	0.423	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
625	41.03	2.19	1.00	1.19	0.84	0.554	1.34	0.412	0.97	1.00	0.423	No
626	41.08	2.19	1.00	1.19	0.84	0.554	1.34	0.412	0.97	1.00	0.423	No
627	41.18	2.20	1.00	1.19	0.84	0.554	1.34	0.412	0.97	1.00	0.423	No
628	41.22	2.20	1.01	1.19	0.84	0.554	1.34	0.412	0.97	1.00	0.423	No
629	41.31	2.20	1.01	1.19	0.84	0.553	1.34	0.412	0.97	1.00	0.423	No
630	41.36	2.20	1.01	1.20	0.84	0.553	1.34	0.411	0.97	1.00	0.423	No
631	41.42	2.21	1.01	1.20	0.84	0.553	1.34	0.411	0.97	1.00	0.423	No
632	41.50	2.21	1.01	1.20	0.84	0.553	1.34	0.411	0.97	1.00	0.423	No
633	41.54	2.21	1.02	1.20	0.84	0.553	1.34	0.411	0.97	1.00	0.423	No
634	41.61	2.22	1.02	1.20	0.84	0.552	1.34	0.411	0.97	1.00	0.423	No
635	41.70	2.22	1.02	1.20	0.84	0.552	1.34	0.411	0.97	1.00	0.423	No
636	41.75	2.23	1.02	1.20	0.84	0.552	1.34	0.411	0.97	1.00	0.423	No
637	41.80	2.23	1.02	1.21	0.83	0.552	1.34	0.410	0.97	1.00	0.423	No
638	41.87	2.23	1.03	1.21	0.83	0.552	1.34	0.410	0.97	1.00	0.423	No
639	41.95	2.24	1.03	1.21	0.83	0.551	1.34	0.410	0.97	1.00	0.423	No
640	42.01	2.24	1.03	1.21	0.83	0.551	1.34	0.410	0.97	1.00	0.423	No
641	42.10	2.24	1.03	1.21	0.83	0.551	1.34	0.410	0.97	1.00	0.423	No
642	42.14	2.25	1.03	1.21	0.83	0.551	1.34	0.410	0.97	1.00	0.423	No
643	42.21	2.25	1.04	1.21	0.83	0.550	1.34	0.409	0.97	1.00	0.423	No
644	42.27	2.25	1.04	1.22	0.83	0.550	1.34	0.409	0.97	1.00	0.423	No
645	42.34	2.26	1.04	1.22	0.83	0.550	1.34	0.409	0.97	1.00	0.422	No
646	42.39	2.26	1.04	1.22	0.83	0.550	1.34	0.409	0.97	1.00	0.422	No
647	42.49	2.27	1.04	1.22	0.83	0.549	1.34	0.409	0.97	1.00	0.422	No
648	42.54	2.27	1.05	1.22	0.83	0.549	1.34	0.409	0.97	1.00	0.422	No
649	42.59	2.27	1.05	1.22	0.83	0.549	1.34	0.408	0.97	1.00	0.422	No
650	42.69	2.28	1.05	1.23	0.83	0.549	1.34	0.408	0.97	1.00	0.422	No
651	42.74	2.28	1.05	1.23	0.83	0.549	1.34	0.408	0.97	1.00	0.422	No
652	42.80	2.28	1.05	1.23	0.83	0.548	1.34	0.408	0.97	1.00	0.422	No
653	42.89	2.29	1.06	1.23	0.82	0.548	1.34	0.408	0.97	1.00	0.422	No
654	42.93	2.29	1.06	1.23	0.82	0.548	1.34	0.407	0.97	1.00	0.422	No
655	42.99	2.29	1.06	1.23	0.82	0.548	1.34	0.407	0.97	1.00	0.422	No
656	43.08	2.30	1.06	1.23	0.82	0.547	1.34	0.407	0.97	1.00	0.422	No
657	43.11	2.30	1.06	1.24	0.82	0.547	1.34	0.407	0.96	1.00	0.422	No
658	43.18	2.30	1.07	1.24	0.82	0.547	1.34	0.407	0.96	1.00	0.422	No
659	43.28	2.31	1.07	1.24	0.82	0.546	1.34	0.406	0.96	1.00	0.422	No
660	43.35	2.31	1.07	1.24	0.82	0.546	1.34	0.406	0.96	1.00	0.421	No
661	43.38	2.31	1.07	1.24	0.82	0.546	1.34	0.406	0.96	1.00	0.421	No
662	43.45	2.32	1.07	1.24	0.82	0.546	1.34	0.406	0.96	1.00	0.421	No
663	43.53	2.32	1.08	1.25	0.82	0.546	1.34	0.406	0.96	1.00	0.421	No
664	43.58	2.33	1.08	1.25	0.82	0.545	1.34	0.406	0.96	1.00	0.421	No
665	43.64	2.33	1.08	1.25	0.82	0.545	1.34	0.405	0.96	1.00	0.421	No
666	43.73	2.33	1.08	1.25	0.82	0.545	1.34	0.405	0.96	1.00	0.421	No
667	43.78	2.34	1.09	1.25	0.82	0.545	1.34	0.405	0.96	1.00	0.421	No
668	43.84	2.34	1.09	1.25	0.82	0.544	1.34	0.405	0.96	1.00	0.421	No
669	43.92	2.34	1.09	1.25	0.81	0.544	1.34	0.405	0.96	1.00	0.421	No
670	43.98	2.35	1.09	1.25	0.81	0.544	1.34	0.405	0.96	1.00	0.421	No
671	44.07	2.35	1.09	1.26	0.81	0.544	1.34	0.404	0.96	1.00	0.421	No
672	44.12	2.35	1.10	1.26	0.81	0.543	1.34	0.404	0.96	1.00	0.421	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
673	44.17	2.36	1.10	1.26	0.81	0.543	1.34	0.404	0.96	1.00	0.421	No
674	44.23	2.36	1.10	1.26	0.81	0.543	1.34	0.404	0.96	1.00	0.420	No
675	44.29	2.36	1.10	1.26	0.81	0.543	1.34	0.404	0.96	1.00	0.420	No
676	44.39	2.37	1.10	1.26	0.81	0.542	1.34	0.403	0.96	1.00	0.420	No
677	44.43	2.37	1.11	1.26	0.81	0.542	1.34	0.403	0.96	1.00	0.420	No
678	44.49	2.37	1.11	1.27	0.81	0.542	1.34	0.403	0.96	1.00	0.420	No
679	44.57	2.38	1.11	1.27	0.81	0.542	1.34	0.403	0.96	1.00	0.420	No
680	44.67	2.38	1.11	1.27	0.81	0.541	1.34	0.403	0.96	1.00	0.420	No
681	44.73	2.39	1.11	1.27	0.81	0.541	1.34	0.402	0.96	1.00	0.420	No
682	44.78	2.39	1.12	1.27	0.81	0.541	1.34	0.402	0.96	1.00	0.420	No
683	44.82	2.39	1.12	1.27	0.81	0.541	1.34	0.402	0.96	1.00	0.420	No
684	44.93	2.40	1.12	1.28	0.80	0.540	1.34	0.402	0.96	1.00	0.419	No
685	44.97	2.40	1.12	1.28	0.80	0.540	1.34	0.402	0.96	1.00	0.419	No
686	45.02	2.40	1.12	1.28	0.80	0.540	1.34	0.402	0.96	1.00	0.419	No
687	45.09	2.40	1.13	1.28	0.80	0.540	1.34	0.401	0.96	1.00	0.419	No
688	45.17	2.41	1.13	1.28	0.80	0.539	1.34	0.401	0.96	1.00	0.419	No
689	45.22	2.41	1.13	1.28	0.80	0.539	1.34	0.401	0.96	1.00	0.419	No
690	45.30	2.42	1.13	1.28	0.80	0.539	1.34	0.401	0.96	1.00	0.419	No
691	45.37	2.42	1.13	1.28	0.80	0.539	1.34	0.401	0.96	1.00	0.419	No
692	45.42	2.42	1.14	1.29	0.80	0.538	1.34	0.401	0.96	1.00	0.419	No
693	45.50	2.43	1.14	1.29	0.80	0.538	1.34	0.400	0.96	1.00	0.419	No
694	45.57	2.43	1.14	1.29	0.80	0.538	1.34	0.400	0.96	1.00	0.419	No
695	45.61	2.43	1.14	1.29	0.80	0.538	1.34	0.400	0.96	1.00	0.419	No
696	45.72	2.44	1.15	1.29	0.80	0.537	1.34	0.400	0.96	1.00	0.418	No
697	45.77	2.44	1.15	1.29	0.80	0.537	1.34	0.400	0.96	1.00	0.418	No
698	45.80	2.44	1.15	1.29	0.80	0.537	1.34	0.400	0.96	1.00	0.418	No
699	45.88	2.44	1.15	1.29	0.79	0.537	1.34	0.399	0.95	1.00	0.418	No
700	45.96	2.45	1.15	1.30	0.79	0.537	1.34	0.399	0.95	1.00	0.418	No
701	46.01	2.45	1.15	1.30	0.79	0.536	1.34	0.399	0.95	1.00	0.418	No
702	46.11	2.46	1.16	1.30	0.79	0.536	1.34	0.399	0.95	1.00	0.418	No
703	46.14	2.46	1.16	1.30	0.79	0.536	1.34	0.399	0.95	1.00	0.418	No
704	46.21	2.46	1.16	1.30	0.79	0.536	1.34	0.398	0.95	1.00	0.418	No
705	46.26	2.46	1.16	1.30	0.79	0.535	1.34	0.398	0.95	1.00	0.418	No
706	46.35	2.47	1.17	1.30	0.79	0.535	1.34	0.398	0.95	1.00	0.417	No
707	46.41	2.47	1.17	1.30	0.79	0.535	1.34	0.398	0.95	1.00	0.417	No
708	46.49	2.48	1.17	1.31	0.79	0.534	1.34	0.398	0.95	1.00	0.417	No
709	46.55	2.48	1.17	1.31	0.79	0.534	1.34	0.397	0.95	1.00	0.417	No
710	46.59	2.48	1.17	1.31	0.79	0.534	1.34	0.397	0.95	1.00	0.417	No
711	46.68	2.49	1.18	1.31	0.79	0.534	1.34	0.397	0.95	1.00	0.417	No
712	46.74	2.49	1.18	1.31	0.79	0.533	1.34	0.397	0.95	1.00	0.417	No
713	46.80	2.49	1.18	1.31	0.79	0.533	1.34	0.397	0.95	1.00	0.417	No
714	46.85	2.49	1.18	1.31	0.78	0.533	1.34	0.396	0.95	1.00	0.417	No
715	46.93	2.50	1.18	1.31	0.78	0.533	1.34	0.396	0.95	1.00	0.416	No
716	47.00	2.50	1.19	1.32	0.78	0.532	1.34	0.396	0.95	1.00	0.416	No
717	47.10	2.51	1.19	1.32	0.78	0.532	1.34	0.396	0.95	1.00	0.416	No
718	47.15	2.51	1.19	1.32	0.78	0.532	1.34	0.395	0.95	1.00	0.416	No
719	47.20	2.51	1.19	1.32	0.78	0.531	1.34	0.395	0.95	1.00	0.416	No
720	47.25	2.52	1.19	1.32	0.78	0.531	1.34	0.395	0.95	1.00	0.416	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
721	47.31	2.52	1.20	1.32	0.78	0.531	1.34	0.395	0.95	1.00	0.416	No
722	47.40	2.52	1.20	1.32	0.78	0.531	1.34	0.395	0.95	1.00	0.416	No
723	47.44	2.53	1.20	1.33	0.78	0.530	1.34	0.394	0.95	1.00	0.415	No
724	47.52	2.53	1.20	1.33	0.78	0.530	1.34	0.394	0.95	1.00	0.415	No
725	47.58	2.53	1.20	1.33	0.78	0.530	1.34	0.394	0.95	1.00	0.415	No
726	47.67	2.54	1.21	1.33	0.78	0.529	1.34	0.394	0.95	1.00	0.415	No
727	47.73	2.54	1.21	1.33	0.78	0.529	1.34	0.394	0.95	1.00	0.415	No
728	47.78	2.54	1.21	1.33	0.78	0.529	1.34	0.393	0.95	1.00	0.415	No
729	47.86	2.55	1.21	1.33	0.77	0.529	1.34	0.393	0.95	1.00	0.415	No
730	47.92	2.55	1.21	1.34	0.77	0.528	1.34	0.393	0.95	1.00	0.415	No
731	47.98	2.55	1.22	1.34	0.77	0.528	1.34	0.393	0.95	1.00	0.414	No
732	48.05	2.56	1.22	1.34	0.77	0.528	1.34	0.393	0.95	1.00	0.414	No
733	48.12	2.56	1.22	1.34	0.77	0.528	1.34	0.392	0.95	1.00	0.414	No
734	48.19	2.56	1.22	1.34	0.77	0.527	1.34	0.392	0.95	1.00	0.414	No
735	48.27	2.57	1.23	1.34	0.77	0.527	1.34	0.392	0.95	1.00	0.414	No
736	48.32	2.57	1.23	1.34	0.77	0.527	1.34	0.392	0.95	1.00	0.414	No
737	48.39	2.57	1.23	1.34	0.77	0.526	1.34	0.391	0.95	1.00	0.414	No
738	48.47	2.58	1.23	1.35	0.77	0.526	1.34	0.391	0.95	1.00	0.413	No
739	48.52	2.58	1.23	1.35	0.77	0.526	1.34	0.391	0.95	1.00	0.413	No
740	48.57	2.58	1.23	1.35	0.77	0.526	1.34	0.391	0.95	1.00	0.413	No
741	48.67	2.59	1.24	1.35	0.77	0.525	1.34	0.391	0.95	1.00	0.413	No
742	48.71	2.59	1.24	1.35	0.77	0.525	1.34	0.390	0.95	1.00	0.413	No
743	48.76	2.59	1.24	1.35	0.77	0.525	1.34	0.390	0.95	1.00	0.413	No
744	48.82	2.60	1.24	1.35	0.76	0.524	1.34	0.390	0.94	1.00	0.413	No
745	48.93	2.60	1.25	1.36	0.76	0.524	1.34	0.390	0.94	1.00	0.412	No
746	48.97	2.60	1.25	1.36	0.76	0.524	1.34	0.389	0.94	1.00	0.412	No
747	49.05	2.61	1.25	1.36	0.76	0.523	1.34	0.389	0.94	1.00	0.412	No
748	49.08	2.61	1.25	1.36	0.76	0.523	1.34	0.389	0.94	1.00	0.412	No
749	49.16	2.61	1.25	1.36	0.76	0.523	1.34	0.389	0.94	1.00	0.412	No
750	49.25	2.62	1.26	1.36	0.76	0.522	1.34	0.388	0.94	1.00	0.412	No
751	49.29	2.62	1.26	1.36	0.76	0.522	1.34	0.388	0.94	1.00	0.412	No
752	49.36	2.63	1.26	1.37	0.76	0.522	1.34	0.388	0.94	1.00	0.411	No
753	49.43	2.63	1.26	1.37	0.76	0.521	1.34	0.388	0.94	1.00	0.411	No
754	49.48	2.63	1.26	1.37	0.76	0.521	1.34	0.387	0.94	1.00	0.411	No
755	49.55	2.64	1.27	1.37	0.76	0.520	1.34	0.387	0.94	1.00	0.411	No
756	49.64	2.64	1.27	1.37	0.76	0.520	1.34	0.387	0.94	1.00	0.411	No
757	49.70	2.65	1.27	1.38	0.76	0.520	1.34	0.386	0.94	1.00	0.410	No
758	49.75	2.65	1.27	1.38	0.76	0.519	1.34	0.386	0.94	1.00	0.410	No
759	49.81	2.65	1.27	1.38	0.75	0.519	1.34	0.386	0.94	1.00	0.410	No
760	49.90	2.66	1.28	1.38	0.75	0.518	1.34	0.386	0.94	1.00	0.410	No
761	49.94	2.66	1.28	1.38	0.75	0.518	1.34	0.385	0.94	1.00	0.410	No
762	50.01	2.66	1.28	1.38	0.75	0.518	1.34	0.385	0.94	1.00	2.000	No
763	50.08	2.67	1.28	1.39	0.75	0.517	1.34	0.385	0.94	1.00	2.000	No
764	50.15	2.67	1.28	1.39	0.75	0.517	1.34	0.384	0.94	1.00	2.000	No
765	50.24	2.68	1.29	1.39	0.75	0.516	1.34	0.384	0.94	1.00	2.000	No
766	50.30	2.68	1.29	1.39	0.75	0.516	1.34	0.384	0.94	1.00	2.000	No
767	50.34	2.68	1.29	1.39	0.75	0.516	1.34	0.384	0.94	1.00	2.000	No
768	50.41	2.69	1.29	1.40	0.75	0.515	1.34	0.383	0.94	1.00	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
769	50.47	2.69	1.29	1.40	0.75	0.515	1.34	0.383	0.94	1.00	2.000	No
770	50.54	2.70	1.30	1.40	0.75	0.514	1.34	0.383	0.94	1.00	2.000	No
771	50.62	2.70	1.30	1.40	0.75	0.514	1.34	0.382	0.94	1.00	2.000	No
772	50.66	2.70	1.30	1.40	0.75	0.514	1.34	0.382	0.94	1.00	2.000	No
773	50.77	2.71	1.30	1.41	0.74	0.513	1.34	0.382	0.94	1.00	2.000	No
774	50.81	2.71	1.30	1.41	0.74	0.513	1.34	0.381	0.94	1.00	2.000	No
775	50.87	2.72	1.31	1.41	0.74	0.512	1.34	0.381	0.94	1.00	2.000	No
776	50.92	2.72	1.31	1.41	0.74	0.512	1.34	0.381	0.94	1.00	2.000	No
777	51.01	2.72	1.31	1.41	0.74	0.512	1.34	0.381	0.94	1.00	2.000	No
778	51.07	2.73	1.31	1.41	0.74	0.511	1.34	0.380	0.94	1.00	2.000	No
779	51.15	2.73	1.32	1.42	0.74	0.511	1.34	0.380	0.94	1.00	2.000	No
780	51.21	2.73	1.32	1.42	0.74	0.511	1.34	0.380	0.93	1.00	2.000	No
781	51.26	2.74	1.32	1.42	0.74	0.510	1.34	0.380	0.93	1.00	2.000	No
782	51.32	2.74	1.32	1.42	0.74	0.510	1.34	0.379	0.93	1.00	2.000	No
783	51.39	2.75	1.32	1.42	0.74	0.510	1.34	0.379	0.93	1.00	2.000	No
784	51.46	2.75	1.32	1.42	0.74	0.509	1.34	0.379	0.93	1.00	2.000	No
785	51.53	2.75	1.33	1.43	0.74	0.509	1.34	0.378	0.93	1.00	2.000	No
786	51.61	2.76	1.33	1.43	0.74	0.508	1.34	0.378	0.93	1.00	2.000	No
787	51.65	2.76	1.33	1.43	0.74	0.508	1.34	0.378	0.93	1.00	2.000	No
788	51.72	2.76	1.33	1.43	0.74	0.508	1.34	0.378	0.93	1.00	2.000	No
789	51.81	2.77	1.34	1.43	0.73	0.507	1.34	0.377	0.93	1.00	2.000	No
790	51.84	2.77	1.34	1.43	0.73	0.507	1.34	0.377	0.93	1.00	2.000	No
791	51.92	2.78	1.34	1.44	0.73	0.507	1.34	0.377	0.93	1.00	2.000	No
792	52.01	2.78	1.34	1.44	0.73	0.506	1.34	0.376	0.93	1.00	2.000	No
793	52.06	2.78	1.34	1.44	0.73	0.506	1.34	0.376	0.93	1.00	2.000	No
794	52.11	2.79	1.35	1.44	0.73	0.505	1.34	0.376	0.93	1.00	2.000	No
795	52.19	2.79	1.35	1.44	0.73	0.505	1.34	0.376	0.93	1.00	2.000	No
796	52.25	2.79	1.35	1.45	0.73	0.505	1.34	0.375	0.93	1.00	2.000	No
797	52.30	2.80	1.35	1.45	0.73	0.504	1.34	0.375	0.93	1.00	2.000	No
798	52.38	2.80	1.35	1.45	0.73	0.504	1.34	0.375	0.93	1.00	2.000	No
799	52.45	2.81	1.36	1.45	0.73	0.503	1.34	0.374	0.93	1.00	2.000	No
800	52.49	2.81	1.36	1.45	0.73	0.503	1.34	0.374	0.93	1.00	2.000	No
801	52.57	2.81	1.36	1.45	0.73	0.503	1.34	0.374	0.93	1.00	2.000	No
802	52.65	2.82	1.36	1.46	0.73	0.502	1.34	0.374	0.93	1.00	2.000	No
803	52.70	2.82	1.36	1.46	0.73	0.502	1.34	0.373	0.93	1.00	2.000	No
804	52.79	2.83	1.37	1.46	0.72	0.502	1.34	0.373	0.93	1.00	2.000	No
805	52.85	2.83	1.37	1.46	0.72	0.501	1.34	0.373	0.93	1.00	2.000	No
806	52.89	2.83	1.37	1.46	0.72	0.501	1.34	0.373	0.93	1.00	2.000	No
807	52.99	2.84	1.37	1.47	0.72	0.500	1.34	0.372	0.93	1.00	2.000	No
808	53.04	2.84	1.37	1.47	0.72	0.500	1.34	0.372	0.93	1.00	2.000	No
809	53.08	2.84	1.38	1.47	0.72	0.500	1.34	0.372	0.93	1.00	2.000	No
810	53.17	2.85	1.38	1.47	0.72	0.499	1.34	0.371	0.93	1.00	2.000	No
811	53.24	2.85	1.38	1.47	0.72	0.499	1.34	0.371	0.93	1.00	2.000	No
812	53.33	2.86	1.38	1.47	0.72	0.498	1.34	0.371	0.93	1.00	2.000	No
813	53.39	2.86	1.38	1.48	0.72	0.498	1.34	0.371	0.93	1.00	2.000	No
814	53.42	2.86	1.39	1.48	0.72	0.498	1.34	0.370	0.93	1.00	2.000	No
815	53.49	2.87	1.39	1.48	0.72	0.498	1.34	0.370	0.93	1.00	2.000	No
816	53.58	2.87	1.39	1.48	0.72	0.497	1.34	0.370	0.93	1.00	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
817	53.63	2.87	1.39	1.48	0.72	0.497	1.34	0.370	0.93	1.00	2.000	No
818	53.68	2.88	1.39	1.48	0.72	0.497	1.34	0.369	0.93	1.00	2.000	No
819	53.77	2.88	1.40	1.49	0.72	0.496	1.34	0.369	0.93	1.00	2.000	No
820	53.83	2.89	1.40	1.49	0.71	0.496	1.34	0.369	0.92	1.00	2.000	No
821	53.88	2.89	1.40	1.49	0.71	0.496	1.34	0.369	0.92	1.00	2.000	No
822	53.97	2.89	1.40	1.49	0.71	0.495	1.34	0.368	0.92	1.00	2.000	No
823	54.03	2.90	1.40	1.49	0.71	0.495	1.34	0.368	0.92	1.00	2.000	No
824	54.08	2.90	1.41	1.49	0.71	0.494	1.34	0.368	0.92	1.00	2.000	No
825	54.18	2.91	1.41	1.50	0.71	0.494	1.34	0.367	0.92	1.00	2.000	No
826	54.22	2.91	1.41	1.50	0.71	0.494	1.34	0.367	0.92	1.00	2.000	No
827	54.27	2.91	1.41	1.50	0.71	0.493	1.34	0.367	0.92	1.00	2.000	No
828	54.38	2.92	1.42	1.50	0.71	0.493	1.34	0.366	0.92	1.00	2.000	No
829	54.42	2.92	1.42	1.50	0.71	0.493	1.34	0.366	0.92	1.00	2.000	No
830	54.47	2.92	1.42	1.50	0.71	0.492	1.34	0.366	0.92	1.00	2.000	No
831	54.57	2.93	1.42	1.51	0.71	0.492	1.34	0.366	0.92	1.00	2.000	No
832	54.61	2.93	1.42	1.51	0.71	0.491	1.34	0.366	0.92	1.00	2.000	No
833	54.68	2.93	1.43	1.51	0.71	0.491	1.34	0.365	0.92	1.00	2.000	No
834	54.75	2.94	1.43	1.51	0.71	0.491	1.34	0.365	0.92	1.00	2.000	No
835	54.79	2.94	1.43	1.51	0.71	0.490	1.34	0.365	0.92	1.00	2.000	No
836	54.86	2.94	1.43	1.51	0.70	0.490	1.34	0.364	0.92	1.00	2.000	No
837	54.95	2.95	1.43	1.52	0.70	0.489	1.34	0.364	0.92	1.00	2.000	No
838	55.01	2.95	1.44	1.52	0.70	0.489	1.34	0.364	0.92	1.00	2.000	No
839	55.06	2.96	1.44	1.52	0.70	0.489	1.34	0.364	0.92	1.00	2.000	No
840	55.12	2.96	1.44	1.52	0.70	0.488	1.34	0.363	0.92	1.00	2.000	No
841	55.21	2.97	1.44	1.52	0.70	0.488	1.34	0.363	0.92	1.00	2.000	No
842	55.25	2.97	1.44	1.53	0.70	0.488	1.34	0.363	0.92	1.00	2.000	No
843	55.32	2.97	1.45	1.53	0.70	0.487	1.34	0.362	0.92	1.00	2.000	No
844	55.40	2.98	1.45	1.53	0.70	0.487	1.34	0.362	0.92	1.00	2.000	No
845	55.50	2.98	1.45	1.53	0.70	0.486	1.34	0.361	0.92	1.00	2.000	No
846	55.52	2.99	1.45	1.53	0.70	0.486	1.34	0.361	0.92	1.00	2.000	No
847	55.60	2.99	1.45	1.54	0.70	0.485	1.34	0.361	0.92	1.00	2.000	No
848	55.67	3.00	1.46	1.54	0.70	0.485	1.34	0.361	0.92	1.00	2.000	No
849	55.72	3.00	1.46	1.54	0.70	0.485	1.34	0.360	0.92	1.00	2.000	No
850	55.79	3.00	1.46	1.54	0.70	0.484	1.34	0.360	0.92	1.00	2.000	No
851	55.86	3.01	1.46	1.55	0.70	0.484	1.34	0.360	0.92	1.00	2.000	No
852	55.95	3.01	1.46	1.55	0.69	0.483	1.34	0.359	0.92	1.00	2.000	No
853	56.00	3.02	1.47	1.55	0.69	0.483	1.34	0.359	0.92	1.00	2.000	No
854	56.05	3.02	1.47	1.55	0.69	0.483	1.34	0.359	0.92	1.00	2.000	No
855	56.11	3.02	1.47	1.55	0.69	0.482	1.34	0.359	0.92	1.00	2.000	No
856	56.19	3.03	1.47	1.55	0.69	0.482	1.34	0.358	0.92	1.00	2.000	No
857	56.24	3.03	1.47	1.56	0.69	0.482	1.34	0.358	0.92	1.00	2.000	No
858	56.34	3.04	1.48	1.56	0.69	0.481	1.34	0.358	0.91	1.00	2.000	No
859	56.37	3.04	1.48	1.56	0.69	0.481	1.34	0.358	0.91	1.00	2.000	No
860	56.43	3.04	1.48	1.56	0.69	0.480	1.34	0.357	0.91	1.00	2.000	No
861	56.54	3.05	1.48	1.56	0.69	0.480	1.34	0.357	0.91	1.00	2.000	No
862	56.59	3.05	1.48	1.57	0.69	0.480	1.34	0.357	0.91	1.00	2.000	No
863	56.64	3.05	1.49	1.57	0.69	0.479	1.34	0.356	0.91	1.00	2.000	No
864	56.73	3.06	1.49	1.57	0.69	0.479	1.34	0.356	0.91	1.00	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
865	56.79	3.06	1.49	1.57	0.69	0.478	1.34	0.356	0.91	1.00	2.000	No
866	56.84	3.07	1.49	1.57	0.69	0.478	1.34	0.356	0.91	1.00	2.000	No
867	56.93	3.07	1.50	1.58	0.69	0.478	1.34	0.355	0.91	1.00	2.000	No
868	56.96	3.07	1.50	1.58	0.69	0.478	1.34	0.355	0.91	1.00	2.000	No
869	57.03	3.08	1.50	1.58	0.68	0.477	1.34	0.355	0.91	1.00	2.000	No
870	57.13	3.08	1.50	1.58	0.68	0.477	1.34	0.355	0.91	1.00	2.000	No
871	57.16	3.08	1.50	1.58	0.68	0.477	1.34	0.354	0.91	1.00	2.000	No
872	57.23	3.09	1.50	1.58	0.68	0.476	1.34	0.354	0.91	1.00	2.000	No
873	57.29	3.09	1.51	1.58	0.68	0.476	1.34	0.354	0.91	1.00	2.000	No
874	57.38	3.10	1.51	1.59	0.68	0.475	1.34	0.354	0.91	1.00	2.000	No
875	57.42	3.10	1.51	1.59	0.68	0.475	1.34	0.353	0.91	1.00	2.000	No
876	57.49	3.10	1.51	1.59	0.68	0.475	1.34	0.353	0.91	1.00	2.000	No
877	57.57	3.11	1.52	1.59	0.68	0.475	1.34	0.353	0.91	1.00	2.000	No
878	57.62	3.11	1.52	1.59	0.68	0.474	1.34	0.353	0.91	1.00	2.000	No
879	57.68	3.11	1.52	1.59	0.68	0.474	1.34	0.353	0.91	1.00	2.000	No
880	57.77	3.12	1.52	1.60	0.68	0.474	1.34	0.352	0.91	1.00	2.000	No
881	57.85	3.12	1.52	1.60	0.68	0.473	1.34	0.352	0.91	1.00	2.000	No
882	57.92	3.13	1.53	1.60	0.68	0.473	1.34	0.352	0.91	1.00	2.000	No
883	57.97	3.13	1.53	1.60	0.68	0.473	1.34	0.351	0.91	1.00	2.000	No
884	58.02	3.13	1.53	1.60	0.68	0.472	1.34	0.351	0.91	1.00	2.000	No
885	58.07	3.13	1.53	1.60	0.68	0.472	1.34	0.351	0.91	1.00	2.000	No
886	58.16	3.14	1.53	1.61	0.67	0.472	1.34	0.351	0.91	1.00	2.000	No
887	58.23	3.14	1.54	1.61	0.67	0.471	1.34	0.351	0.91	1.00	2.000	No
888	58.31	3.15	1.54	1.61	0.67	0.471	1.34	0.350	0.91	1.00	2.000	No
889	58.37	3.15	1.54	1.61	0.67	0.471	1.34	0.350	0.91	1.00	2.000	No
890	58.42	3.15	1.54	1.61	0.67	0.470	1.34	0.350	0.91	1.00	2.000	No
891	58.50	3.16	1.54	1.61	0.67	0.470	1.34	0.350	0.91	1.00	2.000	No
892	58.57	3.16	1.55	1.62	0.67	0.470	1.34	0.349	0.91	1.00	2.000	No
893	58.61	3.16	1.55	1.62	0.67	0.469	1.34	0.349	0.91	1.00	2.000	No
894	58.68	3.17	1.55	1.62	0.67	0.469	1.34	0.349	0.91	1.00	2.000	No
895	58.76	3.17	1.55	1.62	0.67	0.469	1.34	0.349	0.91	1.00	2.000	No
896	58.80	3.17	1.55	1.62	0.67	0.469	1.34	0.348	0.91	1.00	2.000	No
897	58.87	3.18	1.56	1.62	0.67	0.468	1.34	0.348	0.91	1.00	2.000	No
898	58.95	3.18	1.56	1.62	0.67	0.468	1.34	0.348	0.91	1.00	2.000	No
899	59.01	3.19	1.56	1.63	0.67	0.467	1.34	0.348	0.91	1.00	2.000	No
900	59.06	3.19	1.56	1.63	0.67	0.467	1.34	0.348	0.91	1.00	2.000	No
901	59.16	3.20	1.56	1.63	0.67	0.467	1.34	0.347	0.91	1.00	2.000	No
902	59.19	3.20	1.57	1.63	0.67	0.467	1.34	0.347	0.91	1.00	2.000	No
903	59.29	3.20	1.57	1.63	0.67	0.466	1.34	0.347	0.90	1.00	2.000	No
904	59.33	3.21	1.57	1.64	0.66	0.466	1.34	0.346	0.90	1.00	2.000	No
905	59.39	3.21	1.57	1.64	0.66	0.465	1.34	0.346	0.90	1.00	2.000	No
906	59.47	3.21	1.57	1.64	0.66	0.465	1.34	0.346	0.90	1.00	2.000	No
907	59.54	3.22	1.58	1.64	0.66	0.465	1.34	0.346	0.90	1.00	2.000	No
908	59.58	3.22	1.58	1.64	0.66	0.464	1.34	0.345	0.90	1.00	2.000	No
909	59.65	3.23	1.58	1.64	0.66	0.464	1.34	0.345	0.90	1.00	2.000	No
910	59.73	3.23	1.58	1.65	0.66	0.464	1.34	0.345	0.90	1.00	2.000	No
911	59.81	3.23	1.59	1.65	0.66	0.463	1.34	0.345	0.90	1.00	2.000	No
912	59.85	3.24	1.59	1.65	0.66	0.463	1.34	0.344	0.90	1.00	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
913	59.92	3.24	1.59	1.65	0.66	0.463	1.34	0.344	0.90	1.00	2.000	Yes
914	59.99	3.25	1.59	1.65	0.66	0.462	1.34	0.344	0.90	1.00	2.000	Yes
915	60.08	3.25	1.59	1.66	0.66	0.462	1.34	0.344	0.90	1.00	2.000	Yes
916	60.13	3.25	1.60	1.66	0.66	0.462	1.34	0.343	0.90	1.00	2.000	Yes
917	60.18	3.26	1.60	1.66	0.66	0.462	1.34	0.343	0.90	1.00	2.000	Yes
918	60.27	3.26	1.60	1.66	0.66	0.461	1.34	0.343	0.90	1.00	2.000	Yes
919	60.33	3.26	1.60	1.66	0.66	0.461	1.34	0.343	0.90	1.00	2.000	Yes
920	60.38	3.27	1.60	1.66	0.66	0.461	1.34	0.343	0.90	1.00	2.000	No
921	60.47	3.27	1.61	1.66	0.66	0.460	1.34	0.342	0.90	1.00	2.000	No

Abbreviations

Depth: Depth from free surface, at which CPT was performed (ft)
σ_v: Total overburden pressure at test point (tsf)
u_0: Water pressure at test point (tsf)
σ_v': Effective overburden pressure based on GWT during earthquake (tsf)
r_d: Nonlinear shear mass factor
CSR: Cyclic Stress Ratio
MSF: Magnitude Scaling Factor
CSR_{eq}: CSR adjusted for M=7.5
K_σ: Effective overburden stress factor
CSR^*: CSR fully adjusted

:: Cyclic Resistance Ratio (CRR) calculation data ::

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
1	0.10	66.47	1.53	0.20	0.50	106.79	1.00	106.79	4.000	No	No	2.00
2	0.16	86.45	1.43	0.20	0.50	138.87	1.00	138.87	4.000	No	No	2.00
3	0.23	106.22	1.36	0.23	0.50	170.64	1.00	170.64	4.000	No	No	2.00
4	0.30	105.13	1.43	0.30	0.50	168.88	1.00	168.88	4.000	No	No	2.00
5	0.34	103.27	1.49	0.38	0.50	165.88	1.00	165.88	4.000	No	No	2.00
6	0.40	111.18	1.51	0.47	0.50	178.59	1.00	178.59	4.000	No	No	2.00
7	0.50	114.67	1.56	0.59	0.50	184.19	1.00	184.19	4.000	No	No	2.00
8	0.54	109.80	1.64	0.75	0.50	176.35	1.00	176.09	4.000	No	No	2.00
9	0.60	102.06	1.74	0.96	0.54	163.92	1.06	174.37	4.000	Yes	No	2.00
10	0.68	93.31	1.84	1.21	0.58	149.86	1.13	170.05	4.000	Yes	No	2.00
11	0.73	85.63	1.93	1.48	0.61	137.51	1.21	166.98	4.000	Yes	No	2.00
12	0.80	77.42	2.01	1.75	0.64	124.31	1.31	162.91	4.000	Yes	No	2.00
13	0.87	68.51	2.10	2.06	0.67	109.99	1.45	159.28	4.000	Yes	No	2.00
14	0.95	59.06	2.19	2.44	0.71	94.79	1.65	156.57	4.000	Yes	No	2.00
15	0.99	51.06	2.28	2.80	0.74	81.93	1.89	154.68	4.000	Yes	No	2.00
16	1.09	43.83	2.36	3.16	0.78	70.32	2.17	152.86	4.000	Yes	No	2.00
17	1.14	37.48	2.45	3.55	0.81	60.11	2.52	151.36	4.000	Yes	No	2.00
18	1.22	33.30	2.50	3.79	0.83	53.38	2.79	148.94	4.000	Yes	No	2.00
19	1.29	30.41	2.54	3.91	0.84	48.74	2.99	145.59	4.000	Yes	No	2.00
20	1.33	27.94	2.57	3.98	0.86	44.77	3.17	141.81	4.000	Yes	No	2.00
21	1.39	26.55	2.59	3.97	0.86	42.53	3.25	138.36	4.000	No	No	2.00
22	1.48	25.16	2.61	3.98	0.87	40.28	3.36	135.34	4.000	No	Yes	2.00
23	1.52	23.90	2.62	4.00	0.87	38.26	3.47	132.83	4.000	No	Yes	2.00
24	1.59	22.67	2.64	4.02	0.88	36.27	3.59	130.17	4.000	No	Yes	2.00
25	1.66	21.45	2.66	4.02	0.89	34.31	3.71	127.25	4.000	No	Yes	2.00
26	1.73	20.34	2.68	4.01	0.89	32.51	3.82	124.27	4.000	No	Yes	2.00
27	1.78	19.30	2.69	3.99	0.90	30.85	3.93	121.23	4.000	No	Yes	2.00
28	1.84	18.28	2.71	3.97	0.91	29.19	4.05	118.09	4.000	No	Yes	2.00
29	1.93	17.32	2.72	3.94	0.91	27.65	4.16	115.10	4.000	No	Yes	2.00
30	1.98	16.62	2.73	3.88	0.92	26.51	4.23	112.12	4.000	No	Yes	2.00
31	2.04	16.02	2.74	3.79	0.92	25.54	4.27	109.19	4.000	No	Yes	2.00
32	2.13	15.55	2.74	3.68	0.92	24.78	4.28	106.17	4.000	No	Yes	2.00
33	2.18	15.21	2.74	3.58	0.92	24.24	4.28	103.74	4.000	No	Yes	2.00
34	2.25	14.92	2.74	3.49	0.92	23.76	4.27	101.54	4.000	No	Yes	2.00
35	2.30	14.59	2.74	3.41	0.92	23.22	4.28	99.44	4.000	No	Yes	2.00
36	2.38	14.19	2.74	3.35	0.92	22.57	4.32	97.46	4.000	No	Yes	2.00
37	2.44	13.77	2.75	3.29	0.92	21.89	4.36	95.56	4.000	No	Yes	2.00
38	2.51	13.43	2.75	3.23	0.92	21.34	4.39	93.67	4.000	No	Yes	2.00
39	2.57	12.91	2.76	3.21	0.93	20.51	4.49	91.99	4.000	No	Yes	2.00
40	2.66	12.46	2.77	3.18	0.93	19.76	4.56	90.22	4.000	No	Yes	2.00
41	2.72	11.95	2.79	3.19	0.94	18.94	4.69	88.81	4.000	No	Yes	2.00
42	2.76	11.46	2.80	3.21	0.94	18.15	4.83	87.61	4.000	No	Yes	2.00
43	2.84	11.04	2.82	3.23	0.95	17.48	4.95	86.59	4.000	No	Yes	2.00
44	2.92	10.76	2.83	3.24	0.95	17.02	5.04	85.86	4.000	No	Yes	2.00
45	2.95	10.61	2.84	3.28	0.96	16.78	5.11	85.81	4.000	No	Yes	2.00
46	3.07	10.55	2.84	3.32	0.96	16.67	5.16	86.11	4.000	No	Yes	2.00
47	3.11	10.53	2.85	3.37	0.96	16.64	5.21	86.64	4.000	No	Yes	2.00
48	3.16	10.59	2.85	3.43	0.96	16.73	5.23	87.50	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
49	3.26	10.65	2.85	3.50	0.96	16.82	5.27	88.61	4.000	No	Yes	2.00
50	3.30	10.69	2.86	3.59	0.96	16.88	5.32	89.72	4.000	No	Yes	2.00
51	3.36	10.69	2.87	3.68	0.97	16.87	5.38	90.83	4.000	No	Yes	2.00
52	3.44	10.63	2.88	3.79	0.97	16.77	5.48	91.84	4.000	No	Yes	2.00
53	3.50	10.53	2.89	3.89	0.98	16.60	5.58	92.62	4.000	No	Yes	2.00
54	3.56	10.42	2.90	3.96	0.98	16.42	5.66	92.91	4.000	No	Yes	2.00
55	3.62	10.33	2.90	3.97	0.98	16.27	5.70	92.71	4.000	No	Yes	2.00
56	3.71	10.23	2.90	3.98	0.98	16.10	5.74	92.40	4.000	No	Yes	2.00
57	3.76	10.16	2.91	3.98	0.98	15.98	5.76	92.07	4.000	No	Yes	2.00
58	3.82	10.09	2.91	3.99	0.98	15.87	5.80	91.98	4.000	No	Yes	2.00
59	3.90	10.01	2.91	4.02	0.99	15.73	5.84	91.90	4.000	No	Yes	2.00
60	3.95	9.95	2.92	4.02	0.99	15.63	5.87	91.68	4.000	No	Yes	2.00
61	4.00	9.91	2.92	4.08	0.99	15.56	5.92	92.18	4.000	No	Yes	2.00
62	4.09	9.91	2.93	4.14	0.99	15.55	5.96	92.78	4.000	No	Yes	2.00
63	4.16	9.90	2.93	4.20	0.99	15.52	6.01	93.26	4.000	No	Yes	2.00
64	4.20	9.88	2.94	4.28	0.99	15.49	6.07	93.97	4.000	No	Yes	2.00
65	4.27	9.84	2.94	4.35	1.00	15.42	6.13	94.57	4.000	No	Yes	2.00
66	4.34	9.78	2.95	4.42	1.00	15.32	6.20	94.94	4.000	No	Yes	2.00
67	4.44	9.81	2.95	4.42	1.00	15.36	6.19	95.05	4.000	No	Yes	2.00
68	4.48	9.87	2.95	4.43	1.00	15.45	6.17	95.38	4.000	No	Yes	2.00
69	4.58	9.94	2.95	4.44	1.00	15.55	6.16	95.82	4.000	No	Yes	2.00
70	4.63	10.01	2.94	4.41	1.00	15.66	6.12	95.80	4.000	No	Yes	2.00
71	4.68	10.05	2.94	4.39	1.00	15.72	6.09	95.79	4.000	No	Yes	2.00
72	4.73	10.11	2.94	4.39	0.99	15.81	6.07	96.00	4.000	No	Yes	2.00
73	4.80	10.09	2.94	4.43	1.00	15.77	6.10	96.24	4.000	No	Yes	2.00
74	4.86	10.05	2.94	4.45	1.00	15.71	6.13	96.36	4.000	No	Yes	2.00
75	4.93	9.96	2.95	4.47	1.00	15.56	6.18	96.16	4.000	No	Yes	2.00
76	5.00	9.76	2.96	4.49	1.00	15.23	6.26	95.42	4.000	No	Yes	2.00
77	5.07	9.55	2.96	4.45	1.00	14.89	6.32	94.09	4.000	No	Yes	2.00
78	5.12	9.29	2.97	4.41	1.00	14.45	6.40	92.51	4.000	No	Yes	2.00
79	5.20	8.98	2.98	4.36	1.00	13.95	6.50	90.66	4.000	No	Yes	2.00
80	5.27	8.60	2.99	4.32	1.00	13.34	6.64	88.54	4.000	No	Yes	2.00
81	5.33	8.15	3.01	4.29	1.00	12.61	6.82	86.10	4.000	No	Yes	2.00
82	5.41	7.76	3.02	4.20	1.00	11.98	6.96	83.44	4.000	No	Yes	2.00
83	5.45	7.40	3.03	4.10	1.00	11.40	7.09	80.81	4.000	No	Yes	2.00
84	5.52	7.10	3.04	4.00	1.00	10.90	7.19	78.36	4.000	No	Yes	2.00
85	5.60	6.84	3.05	3.93	1.00	10.48	7.30	76.53	4.000	No	Yes	2.00
86	5.67	6.62	3.06	3.91	1.00	10.12	7.43	75.22	4.000	No	Yes	2.00
87	5.71	6.54	3.06	3.89	1.00	9.99	7.47	74.64	4.000	No	Yes	2.00
88	5.80	6.55	3.06	3.86	1.00	10.00	7.43	74.36	4.000	No	Yes	2.00
89	5.85	6.66	3.05	3.81	1.00	10.17	7.33	74.53	4.000	No	Yes	2.00
90	5.91	6.84	3.04	3.79	1.00	10.45	7.20	75.27	4.000	No	Yes	2.00
91	6.01	7.03	3.03	3.80	1.00	10.75	7.10	76.28	4.000	No	Yes	2.00
92	6.06	7.21	3.02	3.83	1.00	11.05	7.01	77.41	4.000	No	Yes	2.00
93	6.11	7.45	3.01	3.83	1.00	11.42	6.87	78.52	4.000	No	Yes	2.00
94	6.18	7.68	3.00	3.80	1.00	11.78	6.73	79.34	4.000	No	Yes	2.00
95	6.26	7.96	2.98	3.72	1.00	12.22	6.53	79.86	4.000	No	Yes	2.00
96	6.30	8.20	2.96	3.61	1.00	12.60	6.33	79.82	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
97	6.37	8.40	2.95	3.51	1.00	12.92	6.17	79.64	4.000	No	Yes	2.00
98	6.45	8.58	2.93	3.40	0.99	13.22	6.00	79.31	4.000	No	Yes	2.00
99	6.51	8.76	2.91	3.29	0.99	13.50	5.84	78.83	4.000	No	Yes	2.00
100	6.60	8.92	2.90	3.21	0.98	13.75	5.71	78.49	4.000	No	Yes	2.00
101	6.64	9.07	2.89	3.14	0.98	13.99	5.60	78.29	4.000	No	Yes	2.00
102	6.70	9.17	2.88	3.12	0.97	14.14	5.54	78.39	4.000	No	Yes	2.00
103	6.80	9.25	2.88	3.13	0.97	14.26	5.52	78.78	4.000	No	Yes	2.00
104	6.83	9.26	2.89	3.18	0.97	14.27	5.56	79.34	4.000	No	Yes	2.00
105	6.90	9.24	2.89	3.25	0.98	14.24	5.62	80.05	4.000	No	Yes	2.00
106	6.98	9.23	2.90	3.32	0.98	14.21	5.68	80.74	4.000	No	Yes	2.00
107	7.04	9.25	2.90	3.38	0.98	14.23	5.72	81.42	4.000	No	Yes	2.00
108	7.09	9.31	2.90	3.42	0.98	14.32	5.73	82.07	4.000	No	Yes	2.00
109	7.16	9.38	2.90	3.45	0.98	14.43	5.73	82.72	4.000	No	Yes	2.00
110	7.24	9.45	2.90	3.50	0.98	14.53	5.75	83.49	4.000	No	Yes	2.00
111	7.30	9.50	2.91	3.53	0.98	14.61	5.75	84.00	4.000	No	Yes	2.00
112	7.39	9.54	2.90	3.52	0.98	14.67	5.73	83.98	4.000	No	Yes	2.00
113	7.43	9.55	2.90	3.54	0.98	14.68	5.74	84.24	4.000	No	Yes	2.00
114	7.50	9.53	2.91	3.66	0.99	14.65	5.83	85.43	4.000	No	Yes	2.00
115	7.59	9.48	2.93	3.79	0.99	14.56	5.95	86.60	4.000	No	Yes	2.00
116	7.63	9.40	2.94	3.94	0.99	14.43	6.08	87.77	4.000	No	Yes	2.00
117	7.70	9.18	2.96	4.12	1.00	14.07	6.30	88.70	4.000	No	Yes	2.00
118	7.78	8.96	2.98	4.31	1.00	13.71	6.53	89.48	4.000	No	Yes	2.00
119	7.83	8.81	2.99	4.43	1.00	13.45	6.68	89.86	4.000	No	Yes	2.00
120	7.89	8.62	3.01	4.59	1.00	13.14	6.88	90.36	4.000	No	Yes	2.00
121	7.95	8.42	3.03	4.79	1.00	12.82	7.11	91.06	4.000	No	Yes	2.00
122	8.02	8.21	3.05	4.95	1.00	12.47	7.32	91.27	4.000	No	Yes	2.00
123	8.11	7.99	3.06	5.00	1.00	12.12	7.46	90.42	4.000	No	Yes	2.00
124	8.16	7.78	3.07	5.00	1.00	11.78	7.58	89.31	4.000	No	Yes	2.00
125	8.21	7.58	3.08	4.99	1.00	11.45	7.69	88.06	4.000	No	Yes	2.00
126	8.30	7.48	3.08	4.90	1.00	11.29	7.69	86.84	4.000	No	Yes	2.00
127	8.36	7.40	3.08	4.80	1.00	11.16	7.67	85.60	4.000	No	Yes	2.00
128	8.41	7.34	3.08	4.69	1.00	11.04	7.64	84.34	4.000	No	Yes	2.00
129	8.47	7.34	3.07	4.53	1.00	11.04	7.53	83.09	4.000	No	Yes	2.00
130	8.56	7.38	3.06	4.38	1.00	11.09	7.40	82.08	4.000	No	Yes	2.00
131	8.61	7.46	3.05	4.26	1.00	11.22	7.27	81.58	4.000	No	Yes	2.00
132	8.70	7.58	3.03	4.16	1.00	11.40	7.13	81.34	4.000	No	Yes	2.00
133	8.75	7.71	3.02	4.11	1.00	11.61	7.02	81.48	4.000	No	Yes	2.00
134	8.81	7.85	3.01	4.06	1.00	11.83	6.91	81.75	4.000	No	Yes	2.00
135	8.90	8.00	3.01	4.01	1.00	12.06	6.80	82.01	4.000	No	Yes	2.00
136	8.94	8.12	3.00	3.97	1.00	12.26	6.71	82.26	4.000	No	Yes	2.00
137	9.01	8.19	2.99	3.97	1.00	12.37	6.67	82.52	4.000	No	Yes	2.00
138	9.09	8.22	2.99	3.98	1.00	12.41	6.67	82.78	4.000	No	Yes	2.00
139	9.13	8.21	2.99	3.99	1.00	12.39	6.68	82.78	4.000	No	Yes	2.00
140	9.20	8.17	2.99	3.97	1.00	12.32	6.69	82.39	4.000	No	Yes	2.00
141	9.27	8.09	3.00	3.96	1.00	12.17	6.73	81.87	4.000	No	Yes	2.00
142	9.35	7.98	3.00	3.93	1.00	11.99	6.76	81.08	4.000	No	Yes	2.00
143	9.39	7.84	3.01	3.89	1.00	11.76	6.80	80.02	4.000	No	Yes	2.00
144	9.45	7.69	3.01	3.84	1.00	11.52	6.85	78.94	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
145	9.54	7.54	3.01	3.79	1.00	11.27	6.89	77.70	4.000	No	Yes	2.00
146	9.59	7.39	3.02	3.74	1.00	11.03	6.94	76.58	4.000	No	Yes	2.00
147	9.65	7.26	3.02	3.66	1.00	10.82	6.96	75.30	4.000	No	Yes	2.00
148	9.73	7.13	3.02	3.59	1.00	10.59	6.99	73.99	4.000	No	Yes	2.00
149	9.81	6.99	3.02	3.51	1.00	10.36	7.01	72.66	4.000	No	Yes	2.00
150	9.85	6.89	3.02	3.43	1.00	10.20	7.01	71.46	4.000	No	Yes	2.00
151	9.94	6.81	3.02	3.35	1.00	10.06	7.00	70.39	4.000	No	Yes	2.00
152	10.00	6.75	3.02	3.30	1.00	9.96	6.99	69.61	4.000	No	Yes	2.00
153	10.04	6.74	3.02	3.23	1.00	9.94	6.94	68.99	4.000	No	Yes	2.00
154	10.12	6.81	3.01	3.20	1.00	10.05	6.87	69.00	4.000	No	Yes	2.00
155	10.19	6.96	3.00	3.19	1.00	10.28	6.77	69.63	4.000	No	Yes	2.00
156	10.24	7.18	2.99	3.22	1.00	10.63	6.67	70.86	4.000	No	Yes	2.00
157	10.31	7.51	2.98	3.30	1.00	11.15	6.54	72.96	4.000	No	Yes	2.00
158	10.39	7.85	2.97	3.37	1.00	11.70	6.42	75.13	4.000	No	Yes	2.00
159	10.48	8.26	2.95	3.40	1.00	12.35	6.24	77.07	4.000	No	Yes	2.00
160	10.53	8.69	2.94	3.44	0.99	13.04	6.08	79.21	4.000	No	Yes	2.00
161	10.63	9.14	2.93	3.52	0.99	13.75	5.95	81.80	4.000	No	Yes	2.00
162	10.67	9.60	2.92	3.64	0.99	14.48	5.86	84.82	4.000	No	Yes	2.00
163	10.71	10.01	2.91	3.74	0.98	15.13	5.78	87.48	4.000	No	Yes	2.00
164	10.79	10.33	2.90	3.85	0.98	15.64	5.74	89.85	4.000	No	Yes	2.00
165	10.83	10.50	2.91	3.97	0.98	15.91	5.77	91.85	4.000	No	Yes	2.00
166	10.93	10.75	2.90	4.01	0.98	16.31	5.71	93.18	4.000	No	Yes	2.00
167	10.98	11.01	2.90	4.05	0.98	16.72	5.66	94.60	4.000	No	Yes	2.00
168	11.06	11.19	2.90	4.14	0.98	17.00	5.66	96.27	4.000	No	Yes	2.00
169	11.11	11.33	2.90	4.22	0.98	17.22	5.67	97.70	4.000	No	Yes	2.00
170	11.16	11.42	2.90	4.27	0.98	17.37	5.68	98.57	4.000	No	Yes	2.00
171	11.23	11.42	2.90	4.30	0.98	17.36	5.70	98.91	4.000	No	Yes	2.00
172	11.31	11.37	2.90	4.33	0.98	17.21	5.75	98.90	4.000	No	Yes	2.00
173	11.36	11.30	2.91	4.34	0.98	17.04	5.78	98.56	4.000	No	Yes	2.00
174	11.42	11.29	2.91	4.31	0.98	16.93	5.79	98.01	4.000	No	Yes	2.00
175	11.51	11.10	2.92	4.36	0.99	16.53	5.90	97.52	4.000	No	Yes	2.00
176	11.56	10.86	2.93	4.40	0.99	16.11	6.01	96.84	4.000	No	Yes	2.00
177	11.65	10.63	2.94	4.41	1.00	15.65	6.12	95.79	4.000	No	Yes	2.00
178	11.71	10.44	2.95	4.40	1.00	15.29	6.19	94.68	4.000	No	Yes	2.00
179	11.75	10.23	2.96	4.39	1.00	14.92	6.27	93.61	4.000	No	Yes	2.00
180	11.84	10.11	2.96	4.32	1.00	14.60	6.31	92.08	4.000	No	Yes	2.00
181	11.89	10.00	2.96	4.23	1.00	14.37	6.30	90.56	4.000	No	Yes	2.00
182	11.96	9.97	2.95	4.08	1.00	14.23	6.23	88.71	4.000	No	Yes	2.00
183	12.03	9.99	2.94	3.91	1.00	14.17	6.13	86.82	4.000	No	Yes	2.00
184	12.11	10.04	2.93	3.71	0.99	14.16	5.99	84.80	4.000	No	Yes	2.00
185	12.16	10.16	2.91	3.52	0.98	14.28	5.82	83.13	4.000	No	Yes	2.00
186	12.21	10.35	2.89	3.34	0.98	14.49	5.63	81.63	4.000	No	Yes	2.00
187	12.30	10.54	2.88	3.19	0.97	14.68	5.47	80.34	4.000	No	Yes	2.00
188	12.35	10.78	2.86	3.06	0.96	14.96	5.31	79.44	4.000	No	Yes	2.00
189	12.41	10.95	2.85	3.01	0.96	15.15	5.23	79.26	4.000	No	Yes	2.00
190	12.49	11.12	2.85	3.00	0.96	15.34	5.19	79.58	4.000	No	Yes	2.00
191	12.56	11.24	2.85	3.05	0.96	15.48	5.20	80.48	4.000	No	Yes	2.00
192	12.60	11.35	2.85	3.13	0.96	15.63	5.22	81.65	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
193	12.67	11.48	2.85	3.20	0.96	15.78	5.25	82.89	4.000	No	Yes	2.00
194	12.75	11.63	2.85	3.26	0.96	15.96	5.26	83.95	4.000	No	Yes	2.00
195	12.80	11.76	2.86	3.33	0.96	16.12	5.28	85.04	4.000	No	Yes	2.00
196	12.90	11.84	2.86	3.40	0.96	16.20	5.32	86.09	4.000	No	Yes	2.00
197	12.95	11.93	2.86	3.46	0.97	16.30	5.34	87.05	4.000	No	Yes	2.00
198	13.02	12.03	2.86	3.51	0.97	16.41	5.35	87.86	4.000	No	Yes	2.00
199	13.06	12.13	2.86	3.54	0.97	16.53	5.35	88.44	4.000	No	Yes	2.00
200	13.14	12.22	2.86	3.56	0.97	16.60	5.35	88.87	4.000	No	Yes	2.00
201	13.19	12.29	2.86	3.58	0.97	16.67	5.35	89.23	4.000	No	Yes	2.00
202	13.29	12.33	2.87	3.61	0.97	16.67	5.37	89.55	4.000	No	Yes	2.00
203	13.33	12.32	2.87	3.65	0.97	16.64	5.41	89.97	4.000	No	Yes	2.00
204	13.39	12.30	2.87	3.68	0.97	16.58	5.44	90.15	4.000	No	Yes	2.00
205	13.48	12.31	2.87	3.69	0.97	16.54	5.45	90.15	4.000	No	Yes	2.00
206	13.54	12.39	2.87	3.70	0.97	16.62	5.44	90.48	4.000	No	Yes	2.00
207	13.59	12.53	2.87	3.70	0.97	16.78	5.42	90.88	4.000	No	Yes	2.00
208	13.67	12.75	2.86	3.69	0.97	17.02	5.36	91.29	4.000	No	Yes	2.00
209	13.72	12.96	2.86	3.69	0.96	17.27	5.32	91.86	4.000	No	Yes	2.00
210	13.78	13.12	2.86	3.72	0.96	17.46	5.30	92.55	4.000	No	Yes	2.00
211	13.86	13.28	2.86	3.75	0.96	17.63	5.29	93.31	4.000	No	Yes	2.00
212	13.93	13.44	2.86	3.79	0.96	17.80	5.29	94.19	4.000	No	Yes	2.00
213	14.01	13.55	2.86	3.86	0.96	17.91	5.31	95.18	4.000	No	Yes	2.00
214	14.05	13.62	2.86	3.93	0.97	17.99	5.35	96.24	4.000	No	Yes	2.00
215	14.14	13.62	2.87	4.00	0.97	17.94	5.40	96.86	4.000	No	Yes	2.00
216	14.21	13.57	2.87	4.06	0.97	17.84	5.45	97.32	4.000	No	Yes	2.00
217	14.24	13.41	2.88	4.14	0.97	17.63	5.55	97.81	4.000	No	Yes	2.00
218	14.31	13.27	2.89	4.22	0.98	17.41	5.64	98.13	4.000	No	Yes	2.00
219	14.39	13.17	2.90	4.27	0.98	17.24	5.70	98.30	4.000	No	Yes	2.00
220	14.44	13.06	2.91	4.31	0.98	17.07	5.76	98.31	4.000	No	Yes	2.00
221	14.54	12.93	2.91	4.35	0.99	16.84	5.83	98.16	4.000	No	Yes	2.00
222	14.59	12.82	2.92	4.38	0.99	16.67	5.88	98.07	4.000	No	Yes	2.00
223	14.64	12.73	2.92	4.40	0.99	16.52	5.92	97.86	4.000	No	Yes	2.00
224	14.70	12.62	2.93	4.42	0.99	16.34	5.98	97.64	4.000	No	Yes	2.00
225	14.79	12.49	2.93	4.44	0.99	16.12	6.04	97.30	4.000	No	Yes	2.00
226	14.83	12.35	2.94	4.45	0.99	15.91	6.09	96.83	4.000	No	Yes	2.00
227	14.93	12.16	2.95	4.46	1.00	15.61	6.16	96.10	4.000	No	Yes	2.00
228	14.98	11.95	2.95	4.47	1.00	15.29	6.24	95.44	4.000	No	Yes	2.00
229	15.03	11.68	2.96	4.50	1.00	14.89	6.36	94.64	4.000	No	Yes	2.00
230	15.10	11.42	2.98	4.53	1.00	14.50	6.47	93.80	4.000	No	Yes	2.00
231	15.18	11.13	2.99	4.57	1.00	14.06	6.60	92.84	4.000	No	Yes	2.00
232	15.23	10.82	3.00	4.60	1.00	13.61	6.75	91.81	4.000	No	Yes	2.00
233	15.33	10.52	3.01	4.63	1.00	13.15	6.89	90.69	4.000	No	Yes	2.00
234	15.37	10.18	3.03	4.69	1.00	12.68	7.08	89.73	4.000	No	Yes	2.00
235	15.44	9.83	3.05	4.76	1.00	12.17	7.29	88.70	4.000	No	Yes	2.00
236	15.52	9.47	3.07	4.86	1.00	11.65	7.53	87.73	4.000	No	Yes	2.00
237	15.56	9.15	3.09	4.92	1.00	11.19	7.74	86.58	4.000	No	Yes	2.00
238	15.63	8.84	3.10	4.98	1.00	10.74	7.96	85.48	4.000	No	Yes	2.00
239	15.71	8.52	3.12	5.05	1.00	10.28	8.19	84.22	4.000	No	Yes	2.00
240	15.77	8.24	3.14	5.09	1.00	9.89	8.39	82.98	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
241	15.82	7.99	3.15	5.13	1.00	9.53	8.58	81.84	4.000	No	Yes	2.00
242	15.89	7.76	3.16	5.14	1.00	9.20	8.75	80.56	4.000	No	Yes	2.00
243	15.97	7.60	3.17	5.09	1.00	8.95	8.85	79.20	4.000	No	Yes	2.00
244	16.02	7.48	3.17	5.03	1.00	8.78	8.90	78.11	4.000	No	Yes	2.00
245	16.10	7.44	3.17	4.93	1.00	8.70	8.87	77.14	4.000	No	Yes	2.00
246	16.17	7.44	3.17	4.82	1.00	8.67	8.80	76.32	4.000	No	Yes	2.00
247	16.22	7.52	3.15	4.64	1.00	8.76	8.62	75.56	4.000	No	Yes	2.00
248	16.28	7.65	3.14	4.46	1.00	8.91	8.41	74.93	4.000	No	Yes	2.00
249	16.37	7.84	3.12	4.27	1.00	9.15	8.15	74.50	4.000	No	Yes	2.00
250	16.42	8.08	3.09	4.08	1.00	9.44	7.86	74.22	4.000	No	Yes	2.00
251	16.52	8.33	3.07	3.90	1.00	9.74	7.59	73.87	4.000	No	Yes	2.00
252	16.55	8.58	3.05	3.75	1.00	10.05	7.33	73.67	4.000	No	Yes	2.00
253	16.62	8.83	3.03	3.60	1.00	10.35	7.09	73.40	4.000	No	Yes	2.00
254	16.70	9.06	3.01	3.49	1.00	10.62	6.89	73.23	4.000	No	Yes	2.00
255	16.74	9.49	2.98	3.32	1.00	11.17	6.55	73.19	4.000	No	Yes	2.00
256	16.82	10.11	2.94	3.11	1.00	11.93	6.13	73.13	4.000	No	Yes	2.00
257	16.91	10.53	2.92	2.97	0.99	12.39	5.88	72.87	4.000	No	Yes	2.00
258	16.94	10.72	2.90	2.89	0.98	12.62	5.75	72.51	4.000	No	Yes	2.00
259	17.01	10.87	2.90	2.83	0.98	12.76	5.65	72.13	4.000	No	Yes	2.00
260	17.10	11.00	2.89	2.78	0.98	12.88	5.58	71.87	4.000	No	Yes	2.00
261	17.15	11.13	2.88	2.74	0.97	13.01	5.51	71.64	4.000	No	Yes	2.00
262	17.21	11.54	2.86	2.62	0.96	13.47	5.29	71.26	4.000	No	Yes	2.00
263	17.30	11.94	2.83	2.51	0.96	13.90	5.09	70.72	4.000	No	Yes	2.00
264	17.34	11.76	2.84	2.53	0.96	13.66	5.16	70.54	4.000	No	Yes	2.00
265	17.41	11.25	2.87	2.64	0.97	13.04	5.42	70.64	4.000	No	Yes	2.00
266	17.49	10.96	2.89	2.72	0.98	12.66	5.59	70.73	4.000	No	Yes	2.00
267	17.53	10.95	2.89	2.73	0.98	12.64	5.60	70.83	4.000	No	Yes	2.00
268	17.59	10.82	2.90	2.76	0.98	12.46	5.68	70.73	4.000	No	Yes	2.00
269	17.67	10.63	2.91	2.80	0.98	12.20	5.79	70.63	4.000	No	Yes	2.00
270	17.73	10.45	2.92	2.83	0.99	11.97	5.88	70.41	4.000	No	Yes	2.00
271	17.79	10.07	2.94	2.93	1.00	11.49	6.11	70.27	4.000	No	Yes	2.00
272	17.87	9.70	2.96	3.03	1.00	11.01	6.36	70.05	4.000	No	Yes	2.00
273	17.92	9.63	2.97	3.03	1.00	10.90	6.40	69.77	4.000	No	Yes	2.00
274	17.99	9.66	2.96	2.97	1.00	10.91	6.34	69.22	4.000	No	Yes	2.00
275	18.07	9.81	2.95	2.87	1.00	11.07	6.20	68.63	4.000	No	Yes	2.00
276	18.14	9.80	2.95	2.82	1.00	11.03	6.17	68.07	4.000	No	Yes	2.00
277	18.19	9.97	2.93	2.75	0.99	11.20	6.04	67.72	4.000	No	Yes	2.00
278	18.26	10.14	2.92	2.67	0.99	11.38	5.92	67.35	4.000	No	Yes	2.00
279	18.34	10.13	2.92	2.65	0.99	11.33	5.92	67.04	4.000	No	Yes	2.00
280	18.38	9.99	2.93	2.66	0.99	11.15	5.98	66.67	4.000	No	Yes	2.00
281	18.45	9.85	2.94	2.68	0.99	10.96	6.06	66.41	4.000	No	Yes	2.00
282	18.53	9.72	2.94	2.69	1.00	10.78	6.13	66.14	4.000	No	Yes	2.00
283	18.60	9.58	2.95	2.72	1.00	10.60	6.23	66.01	4.000	No	Yes	2.00
284	18.68	9.26	2.98	2.82	1.00	10.18	6.47	65.85	4.000	No	Yes	2.00
285	18.72	8.93	3.00	2.91	1.00	9.75	6.73	65.57	4.000	No	Yes	2.00
286	18.79	8.50	3.03	3.03	1.00	9.20	7.08	65.11	4.000	No	Yes	2.00
287	18.84	8.10	3.06	3.14	1.00	8.69	7.42	64.48	4.000	No	Yes	2.00
288	18.92	7.83	3.08	3.20	1.00	8.34	7.65	63.84	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
289	18.98	7.61	3.09	3.24	1.00	8.06	7.84	63.20	4.000	No	Yes	2.00
290	19.06	7.40	3.11	3.25	1.00	7.77	8.02	62.28	4.000	No	Yes	2.00
291	19.11	7.23	3.12	3.23	1.00	7.55	8.13	61.39	4.000	No	Yes	2.00
292	19.18	7.07	3.12	3.21	1.00	7.34	8.24	60.47	4.000	No	Yes	2.00
293	19.25	6.92	3.13	3.20	1.00	7.14	8.36	59.68	4.000	No	Yes	2.00
294	19.33	6.83	3.14	3.17	1.00	7.02	8.41	59.04	4.000	No	Yes	2.00
295	19.37	6.81	3.14	3.15	1.00	6.98	8.41	58.73	4.000	No	Yes	2.00
296	19.47	6.80	3.14	3.13	1.00	6.95	8.42	58.53	4.000	No	Yes	2.00
297	19.52	6.83	3.14	3.12	1.00	6.97	8.39	58.52	4.000	No	Yes	2.00
298	19.57	6.85	3.14	3.13	1.00	6.99	8.39	58.63	4.000	No	Yes	2.00
299	19.62	6.84	3.14	3.17	1.00	6.96	8.45	58.85	4.000	No	Yes	2.00
300	19.71	6.81	3.15	3.23	1.00	6.91	8.55	59.04	4.000	No	Yes	2.00
301	19.77	6.74	3.16	3.33	1.00	6.81	8.71	59.33	4.000	No	Yes	2.00
302	19.82	6.58	3.18	3.45	1.00	6.61	8.97	59.29	4.000	No	Yes	2.00
303	19.91	6.46	3.19	3.51	1.00	6.44	9.15	58.99	4.000	No	Yes	2.00
304	19.96	6.31	3.21	3.57	1.00	6.25	9.36	58.55	4.000	No	Yes	2.00
305	20.02	6.19	3.22	3.62	1.00	6.09	9.55	58.11	4.000	No	Yes	2.00
306	20.11	6.06	3.23	3.65	1.00	5.91	9.73	57.52	4.000	No	Yes	2.00
307	20.18	5.93	3.25	3.68	1.00	5.75	9.91	56.93	4.000	No	Yes	2.00
308	20.23	5.83	3.25	3.67	1.00	5.62	10.01	56.25	4.000	No	Yes	2.00
309	20.28	5.74	3.26	3.62	1.00	5.50	10.08	55.46	4.000	No	Yes	2.00
310	20.37	5.70	3.25	3.51	1.00	5.44	10.03	54.57	4.000	No	Yes	2.00
311	20.42	5.74	3.24	3.36	1.00	5.48	9.85	53.93	4.000	No	Yes	2.00
312	20.48	5.73	3.24	3.32	1.00	5.45	9.83	53.62	4.000	No	Yes	2.00
313	20.56	5.74	3.24	3.27	1.00	5.45	9.78	53.31	4.000	No	Yes	2.00
314	20.63	5.76	3.23	3.21	1.00	5.46	9.71	53.02	4.000	No	Yes	2.00
315	20.67	5.80	3.23	3.16	1.00	5.50	9.62	52.91	4.000	No	Yes	2.00
316	20.74	5.86	3.22	3.10	1.00	5.56	9.50	52.80	4.000	No	Yes	2.00
317	20.83	5.92	3.21	3.06	1.00	5.61	9.41	52.82	4.000	No	Yes	2.00
318	20.90	5.98	3.21	3.05	1.00	5.67	9.34	52.98	4.000	No	Yes	2.00
319	20.97	6.03	3.20	3.04	1.00	5.72	9.30	53.14	4.000	No	Yes	2.00
320	21.02	6.11	3.20	3.02	1.00	5.80	9.19	53.33	4.000	No	Yes	2.00
321	21.10	6.22	3.19	2.98	1.00	5.91	9.05	53.53	4.000	No	Yes	2.00
322	21.17	6.35	3.17	2.95	1.00	6.05	8.90	53.88	4.000	No	Yes	2.00
323	21.22	6.49	3.16	2.91	1.00	6.20	8.74	54.25	4.000	No	Yes	2.00
324	21.27	6.64	3.15	2.90	1.00	6.37	8.60	54.75	4.000	No	Yes	2.00
325	21.37	6.79	3.14	2.88	1.00	6.52	8.47	55.21	4.000	No	Yes	2.00
326	21.43	6.95	3.13	2.86	1.00	6.69	8.32	55.69	4.000	No	Yes	2.00
327	21.46	7.09	3.12	2.85	1.00	6.86	8.19	56.17	4.000	No	Yes	2.00
328	21.55	7.24	3.11	2.81	1.00	7.01	8.06	56.47	4.000	No	Yes	2.00
329	21.62	7.36	3.10	2.80	1.00	7.13	7.96	56.76	4.000	No	Yes	2.00
330	21.66	7.42	3.10	2.75	1.00	7.19	7.87	56.63	4.000	No	Yes	2.00
331	21.74	7.41	3.09	2.71	1.00	7.16	7.84	56.18	4.000	No	Yes	2.00
332	21.81	7.37	3.09	2.67	1.00	7.10	7.84	55.71	4.000	No	Yes	2.00
333	21.85	7.30	3.09	2.63	1.00	7.01	7.86	55.11	4.000	No	Yes	2.00
334	21.93	7.21	3.10	2.58	1.00	6.89	7.88	54.32	4.000	No	Yes	2.00
335	22.00	7.13	3.10	2.53	1.00	6.78	7.90	53.54	4.000	No	Yes	2.00
336	22.07	7.06	3.10	2.48	1.00	6.69	7.91	52.89	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
337	22.16	6.98	3.10	2.46	1.00	6.58	7.96	52.37	4.000	No	Yes	2.00
338	22.19	6.91	3.11	2.45	1.00	6.49	8.01	52.03	4.000	No	Yes	2.00
339	22.26	6.87	3.11	2.49	1.00	6.43	8.10	52.11	4.000	No	Yes	2.00
340	22.33	6.86	3.12	2.55	1.00	6.41	8.19	52.50	4.000	No	Yes	2.00
341	22.40	6.86	3.13	2.62	1.00	6.39	8.27	52.89	4.000	No	Yes	2.00
342	22.45	6.88	3.13	2.65	1.00	6.41	8.30	53.16	4.000	No	Yes	2.00
343	22.53	6.88	3.13	2.65	1.00	6.39	8.31	53.12	4.000	No	Yes	2.00
344	22.60	6.86	3.13	2.66	1.00	6.36	8.35	53.07	4.000	No	Yes	2.00
345	22.64	6.79	3.14	2.69	1.00	6.27	8.45	53.00	4.000	No	Yes	2.00
346	22.70	6.72	3.15	2.77	1.00	6.18	8.61	53.20	4.000	No	Yes	2.00
347	22.80	6.68	3.16	2.81	1.00	6.11	8.71	53.25	4.000	No	Yes	2.00
348	22.84	6.59	3.17	2.84	1.00	6.01	8.83	53.02	4.000	No	Yes	2.00
349	22.90	6.58	3.17	2.78	1.00	5.98	8.78	52.57	4.000	No	Yes	2.00
350	23.00	6.68	3.15	2.65	1.00	6.08	8.56	52.04	4.000	No	Yes	2.00
351	23.05	6.77	3.14	2.63	1.00	6.17	8.47	52.22	4.000	No	Yes	2.00
352	23.14	6.93	3.14	2.70	1.00	6.33	8.42	53.25	4.000	No	Yes	2.00
353	23.18	7.11	3.13	2.79	1.00	6.52	8.37	54.56	4.000	No	Yes	2.00
354	23.24	7.32	3.13	2.93	1.00	6.74	8.36	56.36	4.000	No	Yes	2.00
355	23.32	7.52	3.14	3.11	1.00	6.94	8.40	58.31	4.000	No	Yes	2.00
356	23.39	7.66	3.14	3.31	1.00	7.09	8.50	60.28	4.000	No	Yes	2.00
357	23.44	7.83	3.15	3.53	1.00	7.27	8.59	62.42	4.000	No	Yes	2.00
358	23.53	7.88	3.17	3.83	1.00	7.30	8.83	64.47	4.000	No	Yes	2.00
359	23.59	7.80	3.20	4.18	1.00	7.20	9.20	66.24	4.000	No	Yes	2.00
360	23.63	7.63	3.22	4.47	1.00	7.01	9.57	67.05	4.000	No	Yes	2.00
361	23.69	7.43	3.25	4.73	1.00	6.76	9.96	67.36	4.000	No	Yes	2.00
362	23.77	7.22	3.27	4.92	1.00	6.52	10.30	67.12	4.000	No	Yes	2.00
363	23.82	7.02	3.29	4.98	1.00	6.29	10.54	66.24	4.000	No	Yes	2.00
364	23.93	6.84	3.30	4.94	1.00	6.07	10.70	64.93	4.000	No	Yes	2.00
365	23.95	6.71	3.30	4.82	1.00	5.92	10.73	63.57	4.000	No	Yes	2.00
366	24.03	6.63	3.30	4.60	1.00	5.82	10.65	62.00	4.000	No	Yes	2.00
367	24.12	6.60	3.28	4.34	1.00	5.77	10.47	60.46	4.000	No	Yes	2.00
368	24.16	6.59	3.27	4.09	1.00	5.76	10.28	59.15	4.000	No	Yes	2.00
369	24.22	6.66	3.25	3.88	1.00	5.82	10.02	58.33	4.000	No	Yes	2.00
370	24.30	6.73	3.24	3.71	1.00	5.88	9.81	57.69	4.000	No	Yes	2.00
371	24.37	6.79	3.23	3.63	1.00	5.93	9.69	57.49	4.000	No	Yes	2.00
372	24.43	6.88	3.22	3.57	1.00	6.02	9.56	57.55	4.000	No	Yes	2.00
373	24.50	7.00	3.21	3.52	1.00	6.14	9.41	57.74	4.000	No	Yes	2.00
374	24.57	7.09	3.21	3.50	1.00	6.22	9.33	58.01	4.000	No	Yes	2.00
375	24.62	7.17	3.20	3.53	1.00	6.30	9.29	58.51	4.000	No	Yes	2.00
376	24.69	7.23	3.20	3.57	1.00	6.35	9.29	58.98	4.000	No	Yes	2.00
377	24.77	7.28	3.20	3.62	1.00	6.39	9.31	59.42	4.000	No	Yes	2.00
378	24.83	7.32	3.20	3.66	1.00	6.42	9.31	59.75	4.000	No	Yes	2.00
379	24.88	7.37	3.20	3.66	1.00	6.46	9.29	59.98	4.000	No	Yes	2.00
380	24.97	7.40	3.20	3.67	1.00	6.47	9.28	60.06	4.000	No	Yes	2.00
381	25.02	7.42	3.20	3.66	1.00	6.49	9.26	60.05	4.000	No	Yes	2.00
382	25.11	7.41	3.20	3.65	1.00	6.46	9.27	59.87	4.000	No	Yes	2.00
383	25.17	7.41	3.20	3.65	1.00	6.45	9.28	59.83	4.000	No	Yes	2.00
384	25.21	7.40	3.20	3.64	1.00	6.43	9.28	59.69	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
385	25.29	7.44	3.20	3.63	1.00	6.45	9.26	59.78	4.000	No	Yes	2.00
386	25.36	7.55	3.19	3.61	1.00	6.56	9.16	60.05	4.000	No	Yes	2.00
387	25.40	7.70	3.18	3.58	1.00	6.71	9.02	60.47	4.000	No	Yes	2.00
388	25.46	7.86	3.17	3.58	1.00	6.86	8.90	61.10	4.000	No	Yes	2.00
389	25.54	8.04	3.17	3.57	1.00	7.03	8.77	61.72	4.000	No	Yes	2.00
390	25.62	8.20	3.16	3.58	1.00	7.18	8.69	62.42	4.000	No	Yes	2.00
391	25.66	8.36	3.15	3.63	1.00	7.34	8.63	63.34	4.000	No	Yes	2.00
392	25.75	8.51	3.15	3.68	1.00	7.48	8.58	64.20	4.000	No	Yes	2.00
393	25.80	8.67	3.15	3.72	1.00	7.63	8.53	65.08	4.000	No	Yes	2.00
394	25.85	8.81	3.14	3.74	1.00	7.77	8.46	65.74	4.000	No	Yes	2.00
395	25.96	8.75	3.15	3.87	1.00	7.68	8.62	66.22	4.000	No	Yes	2.00
396	26.01	8.74	3.16	3.98	1.00	7.66	8.73	66.87	4.000	No	Yes	2.00
397	26.05	8.80	3.16	4.05	1.00	7.71	8.76	67.56	4.000	No	Yes	2.00
398	26.12	8.87	3.16	4.11	1.00	7.77	8.77	68.13	4.000	No	Yes	2.00
399	26.19	8.95	3.16	4.14	1.00	7.84	8.75	68.60	4.000	No	Yes	2.00
400	26.25	9.02	3.16	4.13	1.00	7.89	8.71	68.79	4.000	No	Yes	2.00
401	26.33	8.98	3.16	4.16	1.00	7.83	8.77	68.70	4.000	No	Yes	2.00
402	26.42	8.87	3.17	4.21	1.00	7.70	8.89	68.46	4.000	No	Yes	2.00
403	26.46	8.73	3.18	4.26	1.00	7.55	9.03	68.15	4.000	No	Yes	2.00
404	26.52	8.73	3.18	4.21	1.00	7.53	9.00	67.82	4.000	No	Yes	2.00
405	26.61	8.65	3.19	4.19	1.00	7.43	9.05	67.22	4.000	No	Yes	2.00
406	26.67	8.48	3.19	4.16	1.00	7.24	9.15	66.29	4.000	No	Yes	2.00
407	26.71	8.31	3.20	4.12	1.00	7.06	9.25	65.26	4.000	No	Yes	2.00
408	26.79	8.11	3.21	4.11	1.00	6.84	9.40	64.26	4.000	No	Yes	2.00
409	26.87	7.92	3.22	4.12	1.00	6.62	9.56	63.35	4.000	No	Yes	2.00
410	26.92	7.81	3.23	4.09	1.00	6.50	9.63	62.62	4.000	No	Yes	2.00
411	26.98	7.77	3.23	4.01	1.00	6.45	9.60	61.94	4.000	No	Yes	2.00
412	27.06	7.73	3.22	3.93	1.00	6.40	9.58	61.25	4.000	No	Yes	2.00
413	27.11	7.69	3.22	3.85	1.00	6.35	9.54	60.57	4.000	No	Yes	2.00
414	27.21	7.63	3.22	3.80	1.00	6.27	9.56	59.94	4.000	No	Yes	2.00
415	27.26	7.55	3.22	3.76	1.00	6.18	9.60	59.31	4.000	No	Yes	2.00
416	27.32	7.39	3.24	3.79	1.00	6.01	9.77	58.70	4.000	No	Yes	2.00
417	27.40	7.24	3.25	3.81	1.00	5.84	9.94	58.07	4.000	No	Yes	2.00
418	27.45	7.09	3.26	3.80	1.00	5.67	10.09	57.22	4.000	No	Yes	2.00
419	27.52	6.97	3.26	3.70	1.00	5.54	10.12	56.08	4.000	No	Yes	2.00
420	27.60	6.81	3.27	3.65	1.00	5.37	10.24	54.98	4.000	No	Yes	2.00
421	27.65	6.69	3.27	3.59	1.00	5.24	10.31	54.03	4.000	No	Yes	2.00
422	27.71	6.59	3.28	3.53	1.00	5.13	10.37	53.20	4.000	No	Yes	2.00
423	27.80	6.56	3.27	3.42	1.00	5.09	10.31	52.43	4.000	No	Yes	2.00
424	27.84	6.56	3.27	3.31	1.00	5.08	10.20	51.83	4.000	No	Yes	2.00
425	27.90	6.65	3.25	3.19	1.00	5.16	9.99	51.56	4.000	No	Yes	2.00
426	27.99	6.75	3.24	3.11	1.00	5.25	9.82	51.51	4.000	No	Yes	2.00
427	28.05	6.85	3.23	3.12	1.00	5.34	9.73	51.95	4.000	No	Yes	2.00
428	28.10	6.96	3.23	3.20	1.00	5.44	9.72	52.86	4.000	No	Yes	2.00
429	28.17	7.10	3.23	3.26	1.00	5.57	9.66	53.77	4.000	No	Yes	2.00
430	28.25	7.25	3.22	3.31	1.00	5.70	9.59	54.67	4.000	No	Yes	2.00
431	28.30	7.40	3.22	3.34	1.00	5.84	9.49	55.46	4.000	No	Yes	2.00
432	28.39	7.51	3.22	3.43	1.00	5.94	9.50	56.38	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
433	28.44	7.61	3.22	3.51	1.00	6.03	9.49	57.20	4.000	No	Yes	2.00
434	28.49	7.69	3.22	3.58	1.00	6.10	9.50	57.99	4.000	No	Yes	2.00
435	28.54	7.77	3.21	3.59	1.00	6.17	9.45	58.34	4.000	No	Yes	2.00
436	28.62	7.86	3.20	3.49	1.00	6.25	9.29	58.06	4.000	No	Yes	2.00
437	28.68	7.91	3.20	3.48	1.00	6.28	9.26	58.18	4.000	No	Yes	2.00
438	28.74	7.96	3.20	3.56	1.00	6.32	9.30	58.81	4.000	No	Yes	2.00
439	28.83	7.97	3.21	3.65	1.00	6.32	9.39	59.27	4.000	No	Yes	2.00
440	28.89	7.96	3.22	3.72	1.00	6.29	9.47	59.63	4.000	No	Yes	2.00
441	28.98	7.81	3.23	3.85	1.00	6.13	9.72	59.63	4.000	No	Yes	2.00
442	29.03	7.81	3.24	3.89	1.00	6.12	9.77	59.79	4.000	No	Yes	2.00
443	29.09	7.81	3.24	3.87	1.00	6.11	9.77	59.65	4.000	No	Yes	2.00
444	29.14	7.83	3.24	3.88	1.00	6.12	9.76	59.74	4.000	No	Yes	2.00
445	29.22	7.88	3.24	3.94	1.00	6.15	9.79	60.23	4.000	No	Yes	2.00
446	29.27	7.97	3.23	3.89	1.00	6.23	9.67	60.29	4.000	No	Yes	2.00
447	29.38	8.07	3.22	3.74	1.00	6.31	9.48	59.82	4.000	No	Yes	2.00
448	29.43	8.18	3.20	3.62	1.00	6.41	9.28	59.49	4.000	No	Yes	2.00
449	29.48	8.30	3.19	3.50	1.00	6.52	9.09	59.25	4.000	No	Yes	2.00
450	29.57	8.53	3.17	3.34	1.00	6.72	8.79	59.06	4.000	No	Yes	2.00
451	29.62	8.60	3.16	3.28	1.00	6.78	8.68	58.87	4.000	No	Yes	2.00
452	29.68	8.66	3.15	3.27	1.00	6.83	8.63	58.98	4.000	No	Yes	2.00
453	29.73	8.71	3.15	3.24	1.00	6.87	8.58	58.98	4.000	No	Yes	2.00
454	29.82	8.73	3.15	3.24	1.00	6.87	8.58	58.94	4.000	No	Yes	2.00
455	29.87	8.72	3.15	3.23	1.00	6.85	8.58	58.80	4.000	No	Yes	2.00
456	29.94	8.69	3.15	3.23	1.00	6.81	8.61	58.64	4.000	No	Yes	2.00
457	30.02	8.62	3.16	3.23	1.00	6.73	8.67	58.34	4.000	No	Yes	2.00
458	30.07	8.52	3.16	3.25	1.00	6.62	8.76	58.04	4.000	No	Yes	2.00
459	30.16	8.44	3.17	3.25	1.00	6.53	8.84	57.73	4.000	No	Yes	2.00
460	30.19	8.37	3.17	3.24	1.00	6.46	8.88	57.35	4.000	No	Yes	2.00
461	30.26	8.30	3.17	3.19	1.00	6.38	8.89	56.73	4.000	No	Yes	2.00
462	30.36	8.25	3.17	3.15	1.00	6.31	8.90	56.22	4.000	No	Yes	2.00
463	30.41	8.22	3.17	3.10	1.00	6.28	8.88	55.74	4.000	No	Yes	2.00
464	30.46	8.20	3.17	3.06	1.00	6.25	8.86	55.37	4.000	No	Yes	2.00
465	30.53	8.20	3.17	3.03	1.00	6.24	8.84	55.12	4.000	No	Yes	2.00
466	30.61	8.24	3.17	2.99	1.00	6.26	8.78	55.00	4.000	No	Yes	2.00
467	30.65	8.33	3.16	2.96	1.00	6.33	8.69	55.03	4.000	No	Yes	2.00
468	30.71	8.46	3.15	2.94	1.00	6.44	8.58	55.30	4.000	No	Yes	2.00
469	30.81	8.62	3.14	2.93	1.00	6.58	8.48	55.79	4.000	No	Yes	2.00
470	30.84	8.81	3.14	2.96	1.00	6.76	8.38	56.64	4.000	No	Yes	2.00
471	30.91	9.02	3.13	3.01	1.00	6.94	8.31	57.68	4.000	No	Yes	2.00
472	30.99	9.25	3.13	3.10	1.00	7.14	8.26	59.00	4.000	No	Yes	2.00
473	31.04	9.49	3.12	3.18	1.00	7.36	8.20	60.31	4.000	No	Yes	2.00
474	31.11	9.75	3.11	3.24	1.00	7.59	8.12	61.58	4.000	No	Yes	2.00
475	31.19	10.01	3.11	3.32	1.00	7.81	8.05	62.91	4.000	No	Yes	2.00
476	31.25	10.25	3.11	3.38	1.00	8.02	7.99	64.11	4.000	No	Yes	2.00
477	31.30	10.42	3.10	3.43	1.00	8.17	7.95	64.99	4.000	No	Yes	2.00
478	31.39	10.55	3.10	3.48	1.00	8.27	7.95	65.72	4.000	No	Yes	2.00
479	31.45	10.62	3.10	3.53	1.00	8.32	7.96	66.25	4.000	No	Yes	2.00
480	31.50	10.63	3.11	3.57	1.00	8.33	7.99	66.59	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
481	31.60	10.61	3.11	3.60	1.00	8.29	8.04	66.61	4.000	No	Yes	2.00
482	31.65	10.59	3.11	3.59	1.00	8.25	8.05	66.39	4.000	No	Yes	2.00
483	31.73	10.54	3.11	3.61	1.00	8.19	8.10	66.32	4.000	No	Yes	2.00
484	31.80	10.48	3.12	3.67	1.00	8.12	8.20	66.52	4.000	No	Yes	2.00
485	31.84	10.42	3.13	3.74	1.00	8.05	8.29	66.74	4.000	No	Yes	2.00
486	31.91	10.38	3.14	3.82	1.00	8.00	8.39	67.11	4.000	No	Yes	2.00
487	31.99	10.35	3.14	3.90	1.00	7.95	8.48	67.48	4.000	No	Yes	2.00
488	32.03	10.34	3.15	3.97	1.00	7.94	8.55	67.88	4.000	No	Yes	2.00
489	32.09	10.36	3.15	4.02	1.00	7.95	8.59	68.27	4.000	No	Yes	2.00
490	32.19	10.40	3.15	4.07	1.00	7.96	8.62	68.65	4.000	No	Yes	2.00
491	32.25	10.44	3.16	4.17	1.00	7.99	8.69	69.37	4.000	No	Yes	2.00
492	32.29	10.47	3.16	4.24	1.00	8.00	8.74	69.94	4.000	No	Yes	2.00
493	32.38	10.52	3.16	4.26	1.00	8.03	8.73	70.14	4.000	No	Yes	2.00
494	32.43	10.61	3.16	4.25	1.00	8.10	8.69	70.40	4.000	No	Yes	2.00
495	32.48	10.72	3.15	4.23	1.00	8.19	8.62	70.58	4.000	No	Yes	2.00
496	32.58	10.84	3.15	4.21	1.00	8.28	8.55	70.82	4.000	No	Yes	2.00
497	32.63	10.96	3.14	4.21	1.00	8.37	8.50	71.16	4.000	No	Yes	2.00
498	32.69	11.07	3.14	4.22	1.00	8.46	8.46	71.57	4.000	No	Yes	2.00
499	32.74	11.17	3.14	4.25	1.00	8.54	8.44	72.05	4.000	No	Yes	2.00
500	32.83	11.29	3.14	4.25	1.00	8.62	8.40	72.44	4.000	No	Yes	2.00
501	32.88	11.41	3.13	4.25	1.00	8.72	8.34	72.77	4.000	No	Yes	2.00
502	32.97	11.51	3.13	4.28	1.00	8.79	8.33	73.21	4.000	No	Yes	2.00
503	33.01	11.58	3.13	4.33	1.00	8.84	8.34	73.76	4.000	No	Yes	2.00
504	33.07	11.62	3.13	4.38	1.00	8.86	8.37	74.19	4.000	No	Yes	2.00
505	33.16	11.64	3.14	4.43	1.00	8.86	8.41	74.51	4.000	No	Yes	2.00
506	33.20	11.66	3.14	4.44	1.00	8.87	8.42	74.64	4.000	No	Yes	2.00
507	33.27	11.67	3.14	4.43	1.00	8.86	8.41	74.52	4.000	No	Yes	2.00
508	33.36	11.67	3.14	4.40	1.00	8.84	8.40	74.22	4.000	No	Yes	2.00
509	33.42	11.63	3.14	4.36	1.00	8.79	8.39	73.78	4.000	No	Yes	2.00
510	33.51	11.57	3.14	4.29	1.00	8.71	8.38	73.00	4.000	No	Yes	2.00
511	33.56	11.50	3.13	4.16	1.00	8.64	8.31	71.84	4.000	No	Yes	2.00
512	33.61	11.40	3.12	4.00	1.00	8.54	8.24	70.41	4.000	No	Yes	2.00
513	33.67	11.26	3.12	3.87	1.00	8.40	8.20	68.94	4.000	No	Yes	2.00
514	33.76	11.07	3.12	3.73	1.00	8.22	8.19	67.30	4.000	No	Yes	2.00
515	33.81	10.94	3.12	3.58	1.00	8.09	8.13	65.77	4.000	No	Yes	2.00
516	33.86	10.77	3.11	3.46	1.00	7.93	8.11	64.36	4.000	No	Yes	2.00
517	33.94	10.66	3.11	3.32	1.00	7.82	8.05	62.93	4.000	No	Yes	2.00
518	34.02	10.58	3.10	3.18	1.00	7.73	7.97	61.65	4.000	No	Yes	2.00
519	34.06	10.53	3.10	3.09	1.00	7.68	7.91	60.77	4.000	No	Yes	2.00
520	34.14	10.48	3.10	3.03	1.00	7.62	7.89	60.14	4.000	No	Yes	2.00
521	34.21	10.41	3.10	3.00	1.00	7.55	7.91	59.69	4.000	No	Yes	2.00
522	34.25	10.35	3.10	2.97	1.00	7.49	7.92	59.26	4.000	No	Yes	2.00
523	34.33	10.33	3.10	2.94	1.00	7.45	7.90	58.92	4.000	No	Yes	2.00
524	34.41	10.24	3.10	2.94	1.00	7.36	7.96	58.55	4.000	No	Yes	2.00
525	34.49	10.20	3.10	2.90	1.00	7.31	7.95	58.11	4.000	No	Yes	2.00
526	34.56	10.10	3.11	2.88	1.00	7.21	8.00	57.64	4.000	No	Yes	2.00
527	34.59	9.99	3.11	2.87	1.00	7.11	8.04	57.18	4.000	No	Yes	2.00
528	34.67	9.89	3.11	2.85	1.00	7.01	8.09	56.70	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
529	34.76	9.80	3.12	2.83	1.00	6.91	8.13	56.22	4.000	No	Yes	2.00
530	34.80	9.74	3.12	2.79	1.00	6.85	8.14	55.76	4.000	No	Yes	2.00
531	34.85	9.72	3.12	2.77	1.00	6.83	8.13	55.53	4.000	No	Yes	2.00
532	34.93	9.72	3.11	2.74	1.00	6.81	8.11	55.28	4.000	No	Yes	2.00
533	34.98	9.71	3.12	2.74	1.00	6.79	8.12	55.15	4.000	No	Yes	2.00
534	35.05	9.67	3.12	2.74	1.00	6.75	8.15	55.00	4.000	No	Yes	2.00
535	35.13	9.66	3.12	2.73	1.00	6.72	8.16	54.86	4.000	No	Yes	2.00
536	35.18	9.64	3.12	2.72	1.00	6.70	8.17	54.72	4.000	No	Yes	2.00
537	35.24	9.59	3.12	2.73	1.00	6.65	8.21	54.57	4.000	No	Yes	2.00
538	35.32	9.52	3.13	2.74	1.00	6.57	8.27	54.40	4.000	No	Yes	2.00
539	35.41	9.44	3.13	2.74	1.00	6.49	8.34	54.11	4.000	No	Yes	2.00
540	35.46	9.35	3.14	2.73	1.00	6.41	8.39	53.73	4.000	No	Yes	2.00
541	35.51	9.26	3.14	2.70	1.00	6.32	8.42	53.25	4.000	No	Yes	2.00
542	35.58	9.19	3.14	2.67	1.00	6.25	8.44	52.75	4.000	No	Yes	2.00
543	35.66	9.14	3.14	2.63	1.00	6.19	8.44	52.26	4.000	No	Yes	2.00
544	35.71	9.06	3.14	2.61	1.00	6.12	8.48	51.88	4.000	No	Yes	2.00
545	35.76	8.99	3.15	2.59	1.00	6.05	8.51	51.49	4.000	No	Yes	2.00
546	35.86	8.94	3.15	2.56	1.00	5.99	8.53	51.09	4.000	No	Yes	2.00
547	35.91	8.90	3.15	2.53	1.00	5.95	8.52	50.72	4.000	No	Yes	2.00
548	36.01	8.88	3.15	2.51	1.00	5.92	8.52	50.45	4.000	No	Yes	2.00
549	36.05	8.87	3.14	2.46	1.00	5.91	8.48	50.09	4.000	No	Yes	2.00
550	36.12	8.86	3.14	2.44	1.00	5.89	8.47	49.84	4.000	No	Yes	2.00
551	36.20	8.83	3.14	2.42	1.00	5.85	8.47	49.56	4.000	No	Yes	2.00
552	36.23	8.84	3.14	2.40	1.00	5.85	8.45	49.44	4.000	No	Yes	2.00
553	36.31	8.89	3.14	2.37	1.00	5.89	8.38	49.32	4.000	No	Yes	2.00
554	36.35	8.99	3.12	2.30	1.00	5.96	8.24	49.13	4.000	No	Yes	2.00
555	36.45	9.11	3.11	2.23	1.00	6.05	8.09	48.92	4.000	No	Yes	2.00
556	36.51	9.26	3.10	2.16	1.00	6.17	7.90	48.73	4.000	No	Yes	2.00
557	36.58	9.41	3.09	2.10	1.00	6.28	7.74	48.64	4.000	No	Yes	2.00
558	36.66	9.56	3.07	2.06	1.00	6.40	7.61	48.67	4.000	No	Yes	2.00
559	36.70	9.71	3.06	2.04	1.00	6.52	7.49	48.82	4.000	No	Yes	2.00
560	36.80	9.91	3.05	2.01	1.00	6.68	7.35	49.08	4.000	No	Yes	2.00
561	36.85	10.09	3.04	2.01	1.00	6.82	7.26	49.47	4.000	No	Yes	2.00
562	36.89	10.23	3.04	2.02	1.00	6.93	7.19	49.84	4.000	No	Yes	2.00
563	36.96	10.31	3.04	2.07	1.00	6.98	7.22	50.42	4.000	No	Yes	2.00
564	37.03	10.36	3.05	2.12	1.00	7.01	7.27	50.98	4.000	No	Yes	2.00
565	37.09	10.38	3.05	2.20	1.00	7.02	7.35	51.64	4.000	No	Yes	2.00
566	37.15	10.40	3.06	2.26	1.00	7.03	7.42	52.17	4.000	No	Yes	2.00
567	37.23	10.42	3.06	2.32	1.00	7.03	7.49	52.69	4.000	No	Yes	2.00
568	37.27	10.44	3.07	2.37	1.00	7.04	7.54	53.11	4.000	No	Yes	2.00
569	37.34	10.45	3.07	2.40	1.00	7.04	7.59	53.40	4.000	No	Yes	2.00
570	37.43	10.46	3.08	2.43	1.00	7.03	7.62	53.58	4.000	No	Yes	2.00
571	37.49	10.46	3.08	2.46	1.00	7.02	7.66	53.77	4.000	No	Yes	2.00
572	37.54	10.47	3.08	2.45	1.00	7.02	7.66	53.75	4.000	No	Yes	2.00
573	37.62	10.46	3.08	2.46	1.00	7.00	7.67	53.71	4.000	No	Yes	2.00
574	37.69	10.45	3.08	2.44	1.00	6.98	7.66	53.47	4.000	No	Yes	2.00
575	37.74	10.44	3.08	2.43	1.00	6.96	7.66	53.35	4.000	No	Yes	2.00
576	37.82	10.43	3.08	2.42	1.00	6.94	7.66	53.21	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
577	37.89	10.42	3.08	2.41	1.00	6.92	7.67	53.07	4.000	No	Yes	2.00
578	37.93	10.45	3.08	2.40	1.00	6.94	7.65	53.07	4.000	No	Yes	2.00
579	38.02	10.51	3.08	2.40	1.00	6.98	7.62	53.15	4.000	No	Yes	2.00
580	38.08	10.61	3.07	2.40	1.00	7.05	7.57	53.37	4.000	No	Yes	2.00
581	38.13	10.59	3.08	2.45	1.00	7.02	7.65	53.76	4.000	No	Yes	2.00
582	38.23	10.77	3.07	2.47	1.00	7.15	7.59	54.28	4.000	No	Yes	2.00
583	38.28	11.05	3.06	2.47	1.00	7.37	7.45	54.94	4.000	No	Yes	2.00
584	38.35	11.35	3.05	2.45	1.00	7.61	7.29	55.48	4.000	No	Yes	2.00
585	38.42	11.66	3.03	2.43	1.00	7.85	7.14	56.01	4.000	No	Yes	2.00
586	38.47	11.96	3.02	2.41	1.00	8.08	6.99	56.53	4.000	No	Yes	2.00
587	38.52	12.14	3.02	2.42	1.00	8.22	6.94	57.02	4.000	No	Yes	2.00
588	38.61	12.27	3.01	2.44	1.00	8.31	6.91	57.39	4.000	No	Yes	2.00
589	38.67	12.35	3.01	2.43	1.00	8.36	6.88	57.47	4.000	No	Yes	2.00
590	38.72	12.50	3.00	2.39	1.00	8.48	6.78	57.46	4.000	No	Yes	2.00
591	38.82	12.47	3.00	2.38	1.00	8.43	6.79	57.22	4.000	No	Yes	2.00
592	38.86	12.32	3.01	2.39	1.00	8.30	6.86	56.90	4.000	No	Yes	2.00
593	38.96	12.14	3.02	2.39	1.00	8.14	6.94	56.45	4.000	No	Yes	2.00
594	39.01	11.97	3.02	2.38	1.00	7.99	7.01	56.01	4.000	No	Yes	2.00
595	39.05	11.89	3.02	2.36	1.00	7.92	7.02	55.59	4.000	No	Yes	2.00
596	39.13	12.00	3.01	2.29	1.00	7.99	6.90	55.17	4.000	No	Yes	2.00
597	39.21	12.16	3.00	2.21	1.00	8.11	6.75	54.75	4.000	No	Yes	2.00
598	39.24	12.47	2.98	2.13	1.00	8.35	6.54	54.65	4.000	No	Yes	2.00
599	39.31	12.92	2.96	2.04	1.00	8.70	6.28	54.63	4.000	No	Yes	2.00
600	39.40	13.42	2.93	1.98	0.99	9.09	6.04	54.92	4.000	No	Yes	2.00
601	39.44	13.97	2.91	1.94	0.98	9.54	5.81	55.41	4.000	No	Yes	2.00
602	39.51	14.55	2.89	1.91	0.98	10.01	5.60	56.06	4.000	No	Yes	2.00
603	39.60	15.09	2.87	1.89	0.97	10.43	5.44	56.69	4.000	No	Yes	2.00
604	39.66	15.51	2.86	1.88	0.96	10.77	5.31	57.21	4.000	No	Yes	2.00
605	39.70	15.75	2.85	1.87	0.96	10.96	5.25	57.47	4.000	No	Yes	2.00
606	39.80	15.89	2.85	1.87	0.96	11.05	5.22	57.61	4.000	No	Yes	2.00
607	39.85	15.87	2.85	1.88	0.96	11.02	5.24	57.69	4.000	No	Yes	2.00
608	39.90	15.72	2.86	1.90	0.96	10.88	5.29	57.60	4.000	No	Yes	2.00
609	39.98	15.53	2.86	1.89	0.97	10.71	5.34	57.20	4.000	No	Yes	2.00
610	40.05	15.26	2.87	1.87	0.97	10.47	5.40	56.51	4.000	No	Yes	2.00
611	40.10	14.94	2.87	1.84	0.97	10.20	5.46	55.63	4.000	No	Yes	2.00
612	40.20	14.62	2.88	1.80	0.97	9.92	5.50	54.60	4.000	No	Yes	2.00
613	40.25	14.33	2.88	1.75	0.97	9.68	5.53	53.57	4.000	No	Yes	2.00
614	40.30	14.10	2.89	1.71	0.97	9.49	5.56	52.72	4.000	No	Yes	2.00
615	40.40	13.93	2.89	1.67	0.97	9.33	5.57	51.94	4.000	No	Yes	2.00
616	40.45	13.82	2.89	1.63	0.97	9.23	5.56	51.28	4.000	No	Yes	2.00
617	40.50	13.79	2.88	1.60	0.97	9.20	5.52	50.82	4.000	No	Yes	2.00
618	40.59	13.78	2.88	1.58	0.97	9.17	5.51	50.57	4.000	No	Yes	2.00
619	40.64	13.82	2.88	1.57	0.97	9.20	5.50	50.56	4.000	No	Yes	2.00
620	40.69	13.94	2.87	1.57	0.97	9.29	5.45	50.65	4.000	No	Yes	2.00
621	40.79	14.09	2.87	1.58	0.97	9.39	5.44	51.06	4.000	No	Yes	2.00
622	40.83	14.28	2.87	1.64	0.97	9.53	5.46	52.01	4.000	No	Yes	2.00
623	40.92	14.55	2.87	1.70	0.97	9.73	5.45	53.03	4.000	No	Yes	2.00
624	40.98	14.84	2.87	1.76	0.97	9.94	5.45	54.14	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
625	41.03	15.10	2.87	1.82	0.97	10.13	5.45	55.21	4.000	No	Yes	2.00
626	41.08	15.30	2.88	1.87	0.97	10.28	5.47	56.17	4.000	No	Yes	2.00
627	41.18	15.48	2.88	1.92	0.97	10.40	5.47	56.90	4.000	No	Yes	2.00
628	41.22	15.62	2.88	1.96	0.97	10.50	5.49	57.63	4.000	No	Yes	2.00
629	41.31	15.72	2.88	2.01	0.97	10.55	5.53	58.34	4.000	No	Yes	2.00
630	41.36	15.79	2.89	2.05	0.97	10.59	5.56	58.87	4.000	No	Yes	2.00
631	41.42	15.83	2.89	2.06	0.97	10.61	5.56	59.03	4.000	No	Yes	2.00
632	41.50	15.79	2.89	2.08	0.98	10.56	5.60	59.10	4.000	No	Yes	2.00
633	41.54	15.73	2.89	2.10	0.98	10.50	5.64	59.18	4.000	No	Yes	2.00
634	41.61	15.68	2.90	2.10	0.98	10.45	5.65	59.06	4.000	No	Yes	2.00
635	41.70	15.63	2.90	2.10	0.98	10.39	5.68	59.03	4.000	No	Yes	2.00
636	41.75	15.58	2.90	2.12	0.98	10.33	5.72	59.10	4.000	No	Yes	2.00
637	41.80	15.56	2.90	2.13	0.98	10.31	5.74	59.18	4.000	No	Yes	2.00
638	41.87	15.55	2.91	2.14	0.98	10.28	5.76	59.24	4.000	No	Yes	2.00
639	41.95	15.57	2.91	2.15	0.98	10.28	5.77	59.30	4.000	No	Yes	2.00
640	42.01	15.60	2.91	2.16	0.98	10.29	5.78	59.45	4.000	No	Yes	2.00
641	42.10	15.68	2.91	2.18	0.98	10.33	5.79	59.77	4.000	No	Yes	2.00
642	42.14	15.78	2.91	2.21	0.98	10.39	5.79	60.19	4.000	No	Yes	2.00
643	42.21	15.87	2.91	2.26	0.99	10.44	5.83	60.86	4.000	No	Yes	2.00
644	42.27	15.96	2.91	2.29	0.99	10.50	5.84	61.35	4.000	No	Yes	2.00
645	42.34	16.05	2.92	2.32	0.99	10.55	5.85	61.74	4.000	No	Yes	2.00
646	42.39	16.11	2.92	2.35	0.99	10.58	5.87	62.14	4.000	No	Yes	2.00
647	42.49	16.16	2.92	2.38	0.99	10.59	5.90	62.52	4.000	No	Yes	2.00
648	42.54	16.18	2.93	2.44	0.99	10.59	5.96	63.15	4.000	No	Yes	2.00
649	42.59	16.19	2.93	2.51	0.99	10.58	6.03	63.79	4.000	No	Yes	2.00
650	42.69	16.17	2.94	2.56	1.00	10.54	6.09	64.22	4.000	No	Yes	2.00
651	42.74	16.12	2.94	2.58	1.00	10.49	6.13	64.28	4.000	No	Yes	2.00
652	42.80	16.08	2.94	2.58	1.00	10.44	6.15	64.17	4.000	No	Yes	2.00
653	42.89	16.02	2.95	2.58	1.00	10.38	6.17	64.05	4.000	No	Yes	2.00
654	42.93	15.90	2.95	2.60	1.00	10.27	6.23	63.95	4.000	No	Yes	2.00
655	42.99	15.79	2.96	2.60	1.00	10.18	6.27	63.77	4.000	No	Yes	2.00
656	43.08	15.64	2.96	2.60	1.00	10.04	6.31	63.41	4.000	No	Yes	2.00
657	43.11	15.45	2.96	2.58	1.00	9.89	6.35	62.83	4.000	No	Yes	2.00
658	43.18	15.16	2.97	2.55	1.00	9.66	6.41	61.98	4.000	No	Yes	2.00
659	43.28	14.77	2.98	2.52	1.00	9.35	6.52	60.93	4.000	No	Yes	2.00
660	43.35	14.40	2.99	2.51	1.00	9.05	6.63	60.05	4.000	No	Yes	2.00
661	43.38	13.95	3.00	2.50	1.00	8.71	6.78	59.07	4.000	No	Yes	2.00
662	43.45	13.50	3.02	2.47	1.00	8.36	6.92	57.87	4.000	No	Yes	2.00
663	43.53	13.09	3.03	2.43	1.00	8.04	7.04	56.63	4.000	No	Yes	2.00
664	43.58	12.64	3.04	2.40	1.00	7.70	7.19	55.36	4.000	No	Yes	2.00
665	43.64	12.18	3.06	2.39	1.00	7.34	7.39	54.23	4.000	No	Yes	2.00
666	43.73	11.74	3.07	2.37	1.00	7.00	7.58	53.06	4.000	No	Yes	2.00
667	43.78	11.44	3.08	2.34	1.00	6.77	7.69	52.10	4.000	No	Yes	2.00
668	43.84	11.29	3.09	2.32	1.00	6.65	7.75	51.55	4.000	No	Yes	2.00
669	43.92	11.24	3.09	2.30	1.00	6.61	7.75	51.21	4.000	No	Yes	2.00
670	43.98	11.42	3.07	2.23	1.00	6.73	7.58	51.04	4.000	No	Yes	2.00
671	44.07	11.69	3.06	2.21	1.00	6.92	7.44	51.48	4.000	No	Yes	2.00
672	44.12	12.61	3.02	2.15	1.00	7.59	6.96	52.80	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
673	44.17	13.58	2.98	2.10	1.00	8.30	6.53	54.21	4.000	No	Yes	2.00
674	44.23	15.30	2.91	1.97	0.98	9.59	5.82	55.83	4.000	No	Yes	2.00
675	44.29	16.73	2.87	1.92	0.97	10.69	5.38	57.49	4.000	No	Yes	2.00
676	44.39	17.65	2.83	1.85	0.96	11.39	5.08	57.91	4.000	No	Yes	2.00
677	44.43	18.07	2.82	1.81	0.95	11.71	4.96	58.02	4.000	No	Yes	2.00
678	44.49	18.39	2.81	1.77	0.94	11.95	4.84	57.87	4.000	No	Yes	2.00
679	44.57	18.26	2.81	1.76	0.95	11.83	4.87	57.59	4.000	No	Yes	2.00
680	44.67	17.84	2.82	1.74	0.95	11.49	4.94	56.71	4.000	No	Yes	2.00
681	44.73	16.78	2.84	1.73	0.96	10.65	5.18	55.13	4.000	No	Yes	2.00
682	44.78	15.68	2.87	1.71	0.97	9.81	5.43	53.28	4.000	No	Yes	2.00
683	44.82	13.89	2.93	1.74	0.99	8.43	6.03	50.86	4.000	No	Yes	2.00
684	44.93	12.37	2.98	1.70	1.00	7.28	6.57	47.87	4.000	No	Yes	2.00
685	44.97	11.32	3.03	1.73	1.00	6.51	7.09	46.15	4.000	No	Yes	2.00
686	45.02	10.69	3.06	1.72	1.00	6.04	7.40	44.73	4.000	No	Yes	2.00
687	45.09	10.06	3.09	1.73	1.00	5.58	7.79	43.44	4.000	No	Yes	2.00
688	45.17	9.74	3.10	1.70	1.00	5.34	7.95	42.46	4.000	No	Yes	2.00
689	45.22	9.67	3.10	1.67	1.00	5.28	7.96	42.05	4.000	No	Yes	2.00
690	45.30	9.64	3.10	1.63	1.00	5.25	7.93	41.64	4.000	No	Yes	2.00
691	45.37	9.63	3.10	1.60	1.00	5.24	7.90	41.37	4.000	No	Yes	2.00
692	45.42	9.61	3.10	1.59	1.00	5.22	7.90	41.23	4.000	No	Yes	2.00
693	45.50	9.60	3.10	1.58	1.00	5.20	7.90	41.08	4.000	No	Yes	2.00
694	45.57	9.58	3.10	1.58	1.00	5.18	7.92	41.05	4.000	No	Yes	2.00
695	45.61	9.57	3.10	1.57	1.00	5.17	7.92	40.91	4.000	No	Yes	2.00
696	45.72	9.57	3.10	1.56	1.00	5.15	7.91	40.75	4.000	No	Yes	2.00
697	45.77	9.54	3.10	1.57	1.00	5.12	7.95	40.73	4.000	No	Yes	2.00
698	45.80	9.61	3.10	1.58	1.00	5.17	7.93	41.00	4.000	No	Yes	2.00
699	45.88	9.73	3.10	1.62	1.00	5.25	7.91	41.54	4.000	No	Yes	2.00
700	45.96	9.95	3.09	1.64	1.00	5.40	7.81	42.23	4.000	No	Yes	2.00
701	46.01	10.26	3.08	1.65	1.00	5.62	7.64	42.93	4.000	No	Yes	2.00
702	46.11	10.60	3.06	1.65	1.00	5.85	7.45	43.61	4.000	No	Yes	2.00
703	46.14	10.90	3.05	1.65	1.00	6.06	7.28	44.16	4.000	No	Yes	2.00
704	46.21	11.13	3.04	1.65	1.00	6.22	7.18	44.66	4.000	No	Yes	2.00
705	46.26	11.36	3.03	1.67	1.00	6.38	7.10	45.27	4.000	No	Yes	2.00
706	46.35	11.59	3.02	1.69	1.00	6.53	7.02	45.86	4.000	No	Yes	2.00
707	46.41	11.79	3.01	1.67	1.00	6.67	6.90	45.99	4.000	No	Yes	2.00
708	46.49	11.97	3.00	1.63	1.00	6.79	6.76	45.89	4.000	No	Yes	2.00
709	46.55	12.02	3.00	1.59	1.00	6.82	6.70	45.65	4.000	No	Yes	2.00
710	46.59	12.02	3.00	1.60	1.00	6.81	6.70	45.64	4.000	No	Yes	2.00
711	46.68	12.03	3.00	1.65	1.00	6.81	6.79	46.18	4.000	No	Yes	2.00
712	46.74	12.21	3.00	1.70	1.00	6.93	6.78	46.96	4.000	No	Yes	2.00
713	46.80	12.54	2.99	1.69	1.00	7.15	6.63	47.42	4.000	No	Yes	2.00
714	46.85	12.84	2.98	1.72	1.00	7.36	6.55	48.18	4.000	No	Yes	2.00
715	46.93	13.10	2.98	1.78	1.00	7.53	6.54	49.23	4.000	No	Yes	2.00
716	47.00	13.25	2.99	1.91	1.00	7.62	6.66	50.73	4.000	No	Yes	2.00
717	47.10	13.37	3.00	2.06	1.00	7.69	6.79	52.26	4.000	No	Yes	2.00
718	47.15	13.58	3.01	2.14	1.00	7.83	6.82	53.39	4.000	No	Yes	2.00
719	47.20	13.74	3.00	2.17	1.00	7.94	6.80	53.94	4.000	No	Yes	2.00
720	47.25	13.87	3.00	2.11	1.00	8.02	6.69	53.66	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
721	47.31	13.67	3.00	2.07	1.00	7.87	6.72	52.88	4.000	No	Yes	2.00
722	47.40	13.24	3.01	2.08	1.00	7.56	6.90	52.16	4.000	No	Yes	2.00
723	47.44	12.78	3.03	2.05	1.00	7.23	7.05	50.94	4.000	No	Yes	2.00
724	47.52	12.43	3.03	1.93	1.00	6.97	7.06	49.18	4.000	No	Yes	2.00
725	47.58	12.04	3.03	1.78	1.00	6.69	7.03	47.03	4.000	No	Yes	2.00
726	47.67	11.69	3.02	1.60	1.00	6.43	6.96	44.74	4.000	No	Yes	2.00
727	47.73	11.28	3.02	1.47	1.00	6.14	6.97	42.78	4.000	No	Yes	2.00
728	47.78	11.00	3.02	1.37	1.00	5.93	6.95	41.22	4.000	No	Yes	2.00
729	47.86	10.70	3.03	1.32	1.00	5.71	7.05	40.24	4.000	No	Yes	2.00
730	47.92	10.61	3.03	1.31	1.00	5.64	7.08	39.94	4.000	No	Yes	2.00
731	47.98	10.65	3.03	1.34	1.00	5.66	7.12	40.33	4.000	No	Yes	2.00
732	48.05	10.75	3.04	1.41	1.00	5.72	7.18	41.11	4.000	No	Yes	2.00
733	48.12	10.88	3.04	1.50	1.00	5.81	7.25	42.11	4.000	No	Yes	2.00
734	48.19	11.29	3.04	1.59	1.00	6.09	7.18	43.74	4.000	No	Yes	2.00
735	48.27	11.81	3.02	1.65	1.00	6.44	7.02	45.19	4.000	No	Yes	2.00
736	48.32	12.54	3.00	1.65	1.00	6.94	6.70	46.49	4.000	No	Yes	2.00
737	48.39	13.52	2.95	1.57	1.00	7.61	6.21	47.30	4.000	No	Yes	2.00
738	48.47	14.52	2.91	1.50	0.98	8.34	5.76	48.00	4.000	No	Yes	2.00
739	48.52	15.76	2.85	1.39	0.96	9.26	5.23	48.43	4.000	No	Yes	2.00
740	48.57	17.08	2.79	1.27	0.94	10.24	4.73	48.45	4.000	No	Yes	2.00
741	48.67	18.11	2.75	1.18	0.92	11.01	4.38	48.22	4.000	No	Yes	2.00
742	48.71	18.94	2.72	1.13	0.91	11.63	4.15	48.22	4.000	No	Yes	2.00
743	48.76	19.21	2.71	1.13	0.91	11.82	4.10	48.49	4.000	No	Yes	2.00
744	48.82	19.64	2.71	1.15	0.91	12.12	4.06	49.25	4.000	No	Yes	2.00
745	48.93	19.63	2.73	1.26	0.92	12.06	4.21	50.82	4.000	No	Yes	2.00
746	48.97	19.53	2.76	1.46	0.93	11.93	4.49	53.58	4.000	No	Yes	2.00
747	49.05	19.43	2.80	1.69	0.94	11.79	4.80	56.59	4.000	No	Yes	2.00
748	49.08	19.57	2.83	1.95	0.95	11.84	5.07	60.05	4.000	No	Yes	2.00
749	49.16	19.78	2.86	2.26	0.97	11.92	5.36	63.92	4.000	No	Yes	2.00
750	49.25	20.34	2.89	2.57	0.97	12.26	5.56	68.19	4.000	No	Yes	2.00
751	49.29	21.10	2.90	2.90	0.98	12.75	5.71	72.88	4.000	No	Yes	2.00
752	49.36	22.50	2.90	3.19	0.98	13.70	5.71	78.16	4.000	No	Yes	2.00
753	49.43	24.24	2.89	3.39	0.98	14.90	5.58	83.10	4.000	No	Yes	2.00
754	49.48	26.47	2.86	3.44	0.96	16.49	5.29	87.16	4.000	No	Yes	2.00
755	49.55	28.64	2.82	3.42	0.95	18.03	5.00	90.13	4.000	No	Yes	2.00
756	49.64	30.67	2.80	3.39	0.94	19.47	4.75	92.56	4.000	No	Yes	2.00
757	49.70	32.09	2.78	3.42	0.94	20.47	4.63	94.76	4.000	No	Yes	2.00
758	49.75	33.34	2.77	3.44	0.93	21.35	4.53	96.70	4.000	No	Yes	2.00
759	49.81	34.56	2.75	3.43	0.92	22.21	4.41	98.00	4.000	No	Yes	2.00
760	49.90	35.75	2.74	3.42	0.92	23.04	4.31	99.36	4.000	No	Yes	2.00
761	49.94	36.62	2.73	3.40	0.92	23.66	4.23	100.04	4.000	No	Yes	2.00
762	50.01	36.53	2.74	3.44	0.92	23.55	4.26	100.43	4.000	No	Yes	2.00
763	50.08	36.09	2.75	3.51	0.92	23.18	4.35	100.85	4.000	No	Yes	2.00
764	50.15	35.37	2.76	3.61	0.93	22.60	4.48	101.32	4.000	No	Yes	2.00
765	50.24	35.40	2.77	3.64	0.93	22.57	4.50	101.61	4.000	No	Yes	2.00
766	50.30	35.75	2.76	3.58	0.93	22.81	4.44	101.22	4.000	No	Yes	2.00
767	50.34	35.97	2.75	3.49	0.92	22.97	4.36	100.26	4.000	No	Yes	2.00
768	50.41	36.05	2.74	3.41	0.92	23.02	4.31	99.21	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
769	50.47	35.82	2.73	3.27	0.92	22.86	4.24	96.84	4.000	No	Yes	2.00
770	50.54	35.56	2.72	3.09	0.91	22.69	4.14	93.92	4.000	No	Yes	2.00
771	50.62	35.51	2.70	2.90	0.90	22.67	4.01	90.88	4.000	No	Yes	2.00
772	50.66	35.50	2.68	2.68	0.90	22.71	3.86	87.61	4.000	No	Yes	2.00
773	50.77	35.54	2.66	2.48	0.89	22.76	3.71	84.35	4.000	No	Yes	2.00
774	50.81	34.91	2.65	2.33	0.88	22.33	3.64	81.27	4.000	No	Yes	2.00
775	50.87	34.13	2.64	2.21	0.88	21.78	3.61	78.68	4.000	No	Yes	2.00
776	50.92	33.49	2.64	2.12	0.88	21.33	3.59	76.51	4.000	No	Yes	2.00
777	51.01	33.00	2.64	2.03	0.88	20.97	3.55	74.48	4.000	No	Yes	2.00
778	51.07	32.79	2.63	1.96	0.88	20.82	3.52	73.21	4.000	No	Yes	2.00
779	51.15	32.62	2.63	1.91	0.88	20.69	3.49	72.16	4.000	No	Yes	2.00
780	51.21	32.54	2.62	1.88	0.87	20.62	3.47	71.53	4.000	No	Yes	2.00
781	51.26	32.61	2.62	1.87	0.87	20.65	3.46	71.37	4.000	No	Yes	2.00
782	51.32	32.80	2.62	1.87	0.87	20.78	3.44	71.50	4.000	No	Yes	2.00
783	51.39	33.10	2.62	1.87	0.87	20.97	3.42	71.79	4.000	No	Yes	2.00
784	51.46	33.33	2.62	1.89	0.87	21.10	3.42	72.21	4.000	No	Yes	2.00
785	51.53	33.60	2.61	1.90	0.87	21.26	3.42	72.69	4.000	No	Yes	2.00
786	51.61	33.87	2.61	1.92	0.87	21.42	3.42	73.16	4.000	No	Yes	2.00
787	51.65	34.13	2.61	1.93	0.87	21.59	3.41	73.51	4.000	No	Yes	2.00
788	51.72	34.43	2.61	1.93	0.87	21.78	3.39	73.79	4.000	No	Yes	2.00
789	51.81	34.80	2.61	1.92	0.87	22.01	3.36	73.92	4.000	No	Yes	2.00
790	51.84	35.11	2.60	1.91	0.87	22.23	3.33	74.03	4.000	No	Yes	2.00
791	51.92	35.39	2.60	1.90	0.86	22.40	3.30	74.01	4.000	No	No	2.00
792	52.01	35.65	2.59	1.89	0.86	22.56	3.28	73.92	4.000	No	No	2.00
793	52.06	35.90	2.59	1.87	0.86	22.73	3.25	73.80	4.000	No	No	2.00
794	52.11	36.16	2.58	1.85	0.86	22.91	3.21	73.61	4.000	No	No	2.00
795	52.19	36.34	2.58	1.83	0.86	23.01	3.19	73.49	4.000	No	No	2.00
796	52.25	36.53	2.58	1.83	0.86	23.13	3.18	73.49	4.000	No	No	2.00
797	52.30	36.76	2.57	1.83	0.86	23.27	3.16	73.61	4.000	No	No	2.00
798	52.38	37.02	2.57	1.83	0.86	23.43	3.15	73.88	4.000	No	No	2.00
799	52.45	37.28	2.57	1.84	0.85	23.58	3.15	74.22	4.000	No	No	2.00
800	52.49	37.54	2.57	1.86	0.85	23.75	3.14	74.68	4.000	No	No	2.00
801	52.57	37.71	2.57	1.88	0.86	23.83	3.15	75.13	4.000	No	No	2.00
802	52.65	37.81	2.57	1.90	0.86	23.86	3.17	75.60	4.000	No	No	2.00
803	52.70	37.59	2.58	1.93	0.86	23.66	3.21	76.02	4.000	No	No	2.00
804	52.79	37.34	2.59	1.96	0.86	23.43	3.25	76.26	4.000	No	No	2.00
805	52.85	36.98	2.60	1.98	0.86	23.14	3.30	76.30	4.000	No	No	2.00
806	52.89	36.45	2.60	1.99	0.87	22.74	3.34	75.93	4.000	No	Yes	2.00
807	52.99	35.72	2.61	1.98	0.87	22.19	3.38	75.10	4.000	No	Yes	2.00
808	53.04	34.87	2.62	1.95	0.87	21.58	3.42	73.90	4.000	No	Yes	2.00
809	53.08	33.84	2.62	1.92	0.88	20.84	3.48	72.53	4.000	No	Yes	2.00
810	53.17	32.85	2.63	1.88	0.88	20.12	3.53	70.98	4.000	No	Yes	2.00
811	53.24	31.89	2.64	1.83	0.88	19.44	3.56	69.26	4.000	No	Yes	2.00
812	53.33	31.20	2.64	1.76	0.88	18.95	3.57	67.56	4.000	No	Yes	2.00
813	53.39	30.55	2.64	1.70	0.88	18.50	3.57	65.95	4.000	No	Yes	2.00
814	53.42	29.84	2.64	1.65	0.88	18.00	3.58	64.53	4.000	No	Yes	2.00
815	53.49	29.22	2.65	1.62	0.88	17.56	3.62	63.51	4.000	No	Yes	2.00
816	53.58	28.69	2.65	1.61	0.89	17.16	3.66	62.88	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
817	53.63	28.25	2.66	1.63	0.89	16.83	3.73	62.80	4.000	No	Yes	2.00
818	53.68	28.03	2.67	1.67	0.89	16.65	3.79	63.10	4.000	No	Yes	2.00
819	53.77	27.89	2.68	1.72	0.90	16.51	3.86	63.72	4.000	No	Yes	2.00
820	53.83	27.75	2.69	1.78	0.90	16.37	3.95	64.62	4.000	No	Yes	2.00
821	53.88	27.65	2.71	1.86	0.91	16.26	4.04	65.69	4.000	No	Yes	2.00
822	53.97	27.58	2.72	1.95	0.91	16.15	4.14	66.86	4.000	No	Yes	2.00
823	54.03	27.65	2.73	2.03	0.92	16.16	4.21	68.06	4.000	No	Yes	2.00
824	54.08	27.92	2.73	2.08	0.92	16.32	4.23	69.02	4.000	No	Yes	2.00
825	54.18	28.22	2.73	2.11	0.92	16.49	4.23	69.69	4.000	No	Yes	2.00
826	54.22	28.55	2.73	2.12	0.91	16.70	4.21	70.24	4.000	No	Yes	2.00
827	54.27	28.86	2.72	2.13	0.91	16.89	4.18	70.60	4.000	No	Yes	2.00
828	54.38	29.20	2.72	2.13	0.91	17.09	4.15	70.87	4.000	No	Yes	2.00
829	54.42	29.60	2.73	2.21	0.91	17.33	4.18	72.48	4.000	No	Yes	2.00
830	54.47	30.18	2.73	2.32	0.92	17.68	4.22	74.54	4.000	No	Yes	2.00
831	54.57	30.74	2.74	2.44	0.92	17.99	4.27	76.80	4.000	No	Yes	2.00
832	54.61	32.49	2.72	2.51	0.91	19.15	4.16	79.62	4.000	No	Yes	2.00
833	54.68	34.47	2.71	2.64	0.91	20.44	4.09	83.61	4.000	No	Yes	2.00
834	54.75	36.91	2.70	2.78	0.90	22.04	4.00	88.19	4.000	No	Yes	2.00
835	54.79	39.58	2.69	2.92	0.90	23.80	3.90	92.93	4.000	No	Yes	2.00
836	54.86	42.54	2.67	3.05	0.89	25.75	3.80	97.96	4.000	No	Yes	2.00
837	54.95	45.89	2.66	3.19	0.89	27.95	3.70	103.54	4.000	No	Yes	2.00
838	55.01	49.55	2.64	3.25	0.88	30.41	3.55	108.09	4.000	No	Yes	2.00
839	55.06	53.33	2.61	3.30	0.87	32.97	3.41	112.42	4.000	No	Yes	2.00
840	55.12	57.74	2.59	3.31	0.86	35.97	3.25	116.75	4.000	No	No	2.00
841	55.21	61.55	2.57	3.33	0.85	38.53	3.13	120.57	4.000	No	No	2.00
842	55.25	64.95	2.55	3.33	0.85	40.86	3.02	123.48	4.000	No	No	2.00
843	55.32	67.67	2.53	3.32	0.84	42.71	2.94	125.59	4.000	No	No	2.00
844	55.40	69.32	2.52	3.32	0.84	43.79	2.90	126.89	4.000	No	No	2.00
845	55.50	69.77	2.52	3.32	0.84	44.02	2.89	127.13	4.000	No	No	2.00
846	55.52	68.79	2.53	3.32	0.84	43.32	2.91	126.29	4.000	No	No	2.00
847	55.60	66.93	2.54	3.34	0.84	41.97	2.98	124.98	4.000	No	No	2.00
848	55.67	64.58	2.55	3.35	0.85	40.27	3.06	123.13	4.000	No	No	2.00
849	55.72	61.65	2.57	3.36	0.86	38.22	3.16	120.61	4.000	No	No	2.00
850	55.79	58.07	2.59	3.37	0.86	35.70	3.29	117.52	4.000	No	No	2.00
851	55.86	54.37	2.62	3.37	0.87	33.13	3.44	114.05	4.000	No	Yes	2.00
852	55.95	50.44	2.65	3.37	0.88	30.41	3.62	110.07	4.000	No	Yes	2.00
853	56.00	47.04	2.67	3.36	0.89	28.08	3.79	106.54	4.000	No	Yes	2.00
854	56.05	44.22	2.69	3.36	0.90	26.16	3.96	103.47	4.000	No	Yes	2.00
855	56.11	42.29	2.71	3.31	0.91	24.85	4.05	100.71	4.000	No	Yes	2.00
856	56.19	40.82	2.71	3.23	0.91	23.87	4.10	97.89	4.000	No	Yes	2.00
857	56.24	39.25	2.72	3.15	0.91	22.82	4.16	94.95	4.000	No	Yes	2.00
858	56.34	37.48	2.73	3.08	0.92	21.62	4.25	92.00	4.000	No	Yes	2.00
859	56.37	35.77	2.75	3.03	0.92	20.49	4.37	89.45	4.000	No	Yes	2.00
860	56.43	34.28	2.76	2.98	0.93	19.49	4.46	87.00	4.000	No	Yes	2.00
861	56.54	33.15	2.77	2.95	0.93	18.72	4.55	85.17	4.000	No	Yes	2.00
862	56.59	32.27	2.78	2.86	0.93	18.14	4.58	83.05	4.000	No	Yes	2.00
863	56.64	31.50	2.77	2.73	0.93	17.66	4.56	80.45	4.000	No	Yes	2.00
864	56.73	30.75	2.77	2.60	0.93	17.17	4.53	77.84	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
865	56.79	29.94	2.77	2.49	0.93	16.66	4.53	75.39	4.000	No	Yes	2.00
866	56.84	29.45	2.76	2.35	0.93	16.36	4.46	73.04	4.000	No	Yes	2.00
867	56.93	29.13	2.75	2.21	0.92	16.17	4.37	70.74	4.000	No	Yes	2.00
868	56.96	28.72	2.74	2.07	0.92	15.94	4.29	68.35	4.000	No	Yes	2.00
869	57.03	28.18	2.73	1.95	0.92	15.60	4.24	66.11	4.000	No	Yes	2.00
870	57.13	27.59	2.73	1.85	0.91	15.23	4.21	64.05	4.000	No	Yes	2.00
871	57.16	27.05	2.73	1.77	0.91	14.88	4.19	62.33	4.000	No	Yes	2.00
872	57.23	26.67	2.73	1.72	0.91	14.63	4.19	61.35	4.000	No	Yes	2.00
873	57.29	26.39	2.73	1.70	0.91	14.44	4.20	60.68	4.000	No	Yes	2.00
874	57.38	26.31	2.72	1.66	0.91	14.38	4.17	60.04	4.000	No	Yes	2.00
875	57.42	26.37	2.72	1.64	0.91	14.42	4.15	59.82	4.000	No	Yes	2.00
876	57.49	26.54	2.72	1.65	0.91	14.51	4.14	60.12	4.000	No	Yes	2.00
877	57.57	26.67	2.72	1.68	0.91	14.57	4.16	60.64	4.000	No	Yes	2.00
878	57.62	26.59	2.73	1.73	0.92	14.49	4.22	61.18	4.000	No	Yes	2.00
879	57.68	26.52	2.74	1.77	0.92	14.41	4.28	61.64	4.000	No	Yes	2.00
880	57.77	26.34	2.75	1.81	0.92	14.25	4.36	62.10	4.000	No	Yes	2.00
881	57.85	26.02	2.76	1.87	0.93	14.01	4.47	62.58	4.000	No	Yes	2.00
882	57.92	25.63	2.77	1.91	0.93	13.72	4.56	62.60	4.000	No	Yes	2.00
883	57.97	25.13	2.79	1.93	0.94	13.37	4.67	62.43	4.000	No	Yes	2.00
884	58.02	24.52	2.80	1.94	0.94	12.97	4.77	61.87	4.000	No	Yes	2.00
885	58.07	23.81	2.81	1.92	0.95	12.50	4.87	60.83	4.000	No	Yes	2.00
886	58.16	23.20	2.82	1.90	0.95	12.09	4.95	59.82	4.000	No	Yes	2.00
887	58.23	22.77	2.82	1.87	0.95	11.81	5.00	59.00	4.000	No	Yes	2.00
888	58.31	22.40	2.83	1.85	0.95	11.56	5.04	58.29	4.000	No	Yes	2.00
889	58.37	22.16	2.83	1.82	0.95	11.40	5.05	57.57	4.000	No	Yes	2.00
890	58.42	22.06	2.83	1.79	0.95	11.33	5.03	57.06	4.000	No	Yes	2.00
891	58.50	22.07	2.83	1.77	0.95	11.33	5.02	56.90	4.000	No	Yes	2.00
892	58.57	22.16	2.83	1.78	0.95	11.37	5.02	57.09	4.000	No	Yes	2.00
893	58.61	22.31	2.83	1.83	0.95	11.45	5.05	57.78	4.000	No	Yes	2.00
894	58.68	22.68	2.84	1.93	0.96	11.65	5.10	59.42	4.000	No	Yes	2.00
895	58.76	23.31	2.84	2.08	0.96	11.99	5.16	61.90	4.000	No	Yes	2.00
896	58.80	24.38	2.84	2.23	0.96	12.62	5.14	64.88	4.000	No	Yes	2.00
897	58.87	25.76	2.84	2.40	0.96	13.44	5.10	68.50	4.000	No	Yes	2.00
898	58.95	26.94	2.84	2.60	0.96	14.12	5.12	72.34	4.000	No	Yes	2.00
899	59.01	29.48	2.82	2.75	0.95	15.68	4.92	77.17	4.000	No	Yes	2.00
900	59.06	32.30	2.79	2.84	0.94	17.44	4.67	81.48	4.000	No	Yes	2.00
901	59.16	35.49	2.75	2.84	0.92	19.45	4.37	84.96	4.000	No	Yes	2.00
902	59.19	38.57	2.71	2.82	0.91	21.43	4.10	87.83	4.000	No	Yes	2.00
903	59.29	40.88	2.69	2.82	0.90	22.89	3.93	90.03	4.000	No	Yes	2.00
904	59.33	42.63	2.67	2.82	0.89	24.01	3.82	91.61	4.000	No	Yes	2.00
905	59.39	43.82	2.66	2.80	0.89	24.76	3.73	92.47	4.000	No	Yes	2.00
906	59.47	44.76	2.65	2.74	0.88	25.38	3.64	92.27	4.000	No	Yes	2.00
907	59.54	45.65	2.63	2.63	0.88	25.98	3.51	91.18	4.000	No	Yes	2.00
908	59.58	44.87	2.63	2.53	0.88	25.51	3.48	88.87	4.000	No	Yes	2.00
909	59.65	43.24	2.63	2.46	0.88	24.45	3.53	86.35	4.000	No	Yes	2.00
910	59.73	40.72	2.66	2.50	0.89	22.76	3.72	84.64	4.000	No	Yes	2.00
911	59.81	38.24	2.70	2.60	0.90	21.07	3.98	83.87	4.000	No	Yes	2.00
912	59.85	36.61	2.69	2.35	0.90	20.12	3.91	78.60	4.000	Yes	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
913	59.92	35.57	2.66	2.04	0.89	19.57	3.73	72.90	4.000	Yes	Yes	2.00
914	59.99	35.26	2.62	1.69	0.87	19.53	3.43	67.02	4.000	Yes	Yes	2.00
915	60.08	35.07	2.57	1.37	0.85	19.57	3.13	61.24	4.000	Yes	No	2.00
916	60.13	35.05	2.51	1.09	0.83	19.76	2.82	55.82	4.000	Yes	No	2.00
917	60.18	35.20	2.44	0.82	0.81	20.10	2.51	50.35	4.000	Yes	No	2.00
918	60.27	35.91	2.36	0.56	0.77	20.86	2.16	44.99	4.000	Yes	No	2.00
919	60.33	37.42	2.23	0.29	0.72	22.37	1.00	22.37	4.000	Yes	No	2.00
920	60.38	38.51	N/A	0.00	1.00	-1.00	1.00	N/A	4.000	No	No	2.00
921	60.47	38.91	N/A	0.00	1.00	-1.00	1.00	N/A	4.000	No	No	2.00

Abbreviations

Depth: Depth from free surface, at which CPT was performed (ft)
q_t: Total cone resistance
I_c: Soil behavior type index
Fr: Normalized friction ratio (%)
n: Stress exponent
Q_{tn}: Normalized cone resistance
K_c: Cone resistance correction factor due to fines
$Q_{tn,cs}$: Normalized and adjusted cone resistance
$CRR_{7.5}$: Cyclic resistance ratio for M_w=7.5
FS: Factor of safety against soil liquefaction

:: Liquefaction Potential Index calculation data ::

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
0.10	2.00	0.00	0.00	0.02	0.00	0.16	2.00	0.00	0.00	0.02	0.00
0.23	2.00	0.00	0.00	0.02	0.00	0.30	2.00	0.00	0.00	0.02	0.00
0.34	2.00	0.00	0.00	0.01	0.00	0.40	2.00	0.00	0.00	0.02	0.00
0.50	2.00	0.00	0.00	0.03	0.00	0.54	2.00	0.00	0.00	0.01	0.00
0.60	2.00	0.00	0.00	0.02	0.00	0.68	2.00	0.00	0.00	0.02	0.00
0.73	2.00	0.00	0.00	0.02	0.00	0.80	2.00	0.00	0.00	0.02	0.00
0.87	2.00	0.00	0.00	0.02	0.00	0.95	2.00	0.00	0.00	0.02	0.00
0.99	2.00	0.00	0.00	0.01	0.00	1.09	2.00	0.00	0.00	0.03	0.00
1.14	2.00	0.00	0.00	0.02	0.00	1.22	2.00	0.00	0.00	0.02	0.00
1.29	2.00	0.00	0.00	0.02	0.00	1.33	2.00	0.00	0.00	0.01	0.00
1.39	2.00	0.00	0.00	0.02	0.00	1.48	2.00	0.00	0.00	0.03	0.00
1.52	2.00	0.00	0.00	0.01	0.00	1.59	2.00	0.00	0.00	0.02	0.00
1.66	2.00	0.00	0.00	0.02	0.00	1.73	2.00	0.00	0.00	0.02	0.00
1.78	2.00	0.00	0.00	0.02	0.00	1.84	2.00	0.00	0.00	0.02	0.00
1.93	2.00	0.00	0.00	0.03	0.00	1.98	2.00	0.00	0.00	0.02	0.00
2.04	2.00	0.00	0.00	0.02	0.00	2.13	2.00	0.00	0.00	0.03	0.00
2.18	2.00	0.00	0.00	0.02	0.00	2.25	2.00	0.00	0.00	0.02	0.00
2.30	2.00	0.00	0.00	0.02	0.00	2.38	2.00	0.00	0.00	0.02	0.00
2.44	2.00	0.00	0.00	0.02	0.00	2.51	2.00	0.00	0.00	0.02	0.00
2.57	2.00	0.00	0.00	0.02	0.00	2.66	2.00	0.00	0.00	0.03	0.00
2.72	2.00	0.00	0.00	0.02	0.00	2.76	2.00	0.00	0.00	0.01	0.00
2.84	2.00	0.00	0.00	0.02	0.00	2.92	2.00	0.00	0.00	0.02	0.00
2.95	2.00	0.00	0.00	0.01	0.00	3.07	2.00	0.00	0.00	0.04	0.00
3.11	2.00	0.00	0.00	0.01	0.00	3.16	2.00	0.00	0.00	0.02	0.00
3.26	2.00	0.00	0.00	0.03	0.00	3.30	2.00	0.00	0.00	0.01	0.00
3.36	2.00	0.00	0.00	0.02	0.00	3.44	2.00	0.00	0.00	0.02	0.00
3.50	2.00	0.00	0.00	0.02	0.00	3.56	2.00	0.00	0.00	0.02	0.00
3.62	2.00	0.00	0.00	0.02	0.00	3.71	2.00	0.00	0.00	0.03	0.00
3.76	2.00	0.00	0.00	0.02	0.00	3.82	2.00	0.00	0.00	0.02	0.00
3.90	2.00	0.00	0.00	0.02	0.00	3.95	2.00	0.00	0.00	0.02	0.00
4.00	2.00	0.00	0.00	0.02	0.00	4.09	2.00	0.00	0.00	0.03	0.00
4.16	2.00	0.00	0.00	0.02	0.00	4.20	2.00	0.00	0.00	0.01	0.00
4.27	2.00	0.00	0.00	0.02	0.00	4.34	2.00	0.00	0.00	0.02	0.00
4.44	2.00	0.00	0.00	0.03	0.00	4.48	2.00	0.00	0.00	0.01	0.00
4.58	2.00	0.00	0.00	0.03	0.00	4.63	2.00	0.00	0.00	0.02	0.00
4.68	2.00	0.00	0.00	0.02	0.00	4.73	2.00	0.00	0.00	0.02	0.00
4.80	2.00	0.00	0.00	0.02	0.00	4.86	2.00	0.00	0.00	0.02	0.00
4.93	2.00	0.00	0.00	0.02	0.00	5.00	2.00	0.00	0.00	0.02	0.00
5.07	2.00	0.00	0.00	0.02	0.00	5.12	2.00	0.00	0.00	0.02	0.00
5.20	2.00	0.00	0.00	0.02	0.00	5.27	2.00	0.00	0.00	0.02	0.00
5.33	2.00	0.00	0.00	0.02	0.00	5.41	2.00	0.00	0.00	0.02	0.00
5.45	2.00	0.00	0.00	0.01	0.00	5.52	2.00	0.00	0.00	0.02	0.00
5.60	2.00	0.00	0.00	0.02	0.00	5.67	2.00	0.00	0.00	0.02	0.00
5.71	2.00	0.00	0.00	0.01	0.00	5.80	2.00	0.00	0.00	0.03	0.00
5.85	2.00	0.00	0.00	0.02	0.00	5.91	2.00	0.00	0.00	0.02	0.00
6.01	2.00	0.00	0.00	0.03	0.00	6.06	2.00	0.00	0.00	0.02	0.00
6.11	2.00	0.00	0.00	0.02	0.00	6.18	2.00	0.00	0.00	0.02	0.00
6.26	2.00	0.00	0.00	0.02	0.00	6.30	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
6.37	2.00	0.00	0.00	0.02	0.00	6.45	2.00	0.00	0.00	0.02	0.00
6.51	2.00	0.00	0.00	0.02	0.00	6.60	2.00	0.00	0.00	0.03	0.00
6.64	2.00	0.00	0.00	0.01	0.00	6.70	2.00	0.00	0.00	0.02	0.00
6.80	2.00	0.00	0.00	0.03	0.00	6.83	2.00	0.00	0.00	0.01	0.00
6.90	2.00	0.00	0.00	0.02	0.00	6.98	2.00	0.00	0.00	0.02	0.00
7.04	2.00	0.00	0.00	0.02	0.00	7.09	2.00	0.00	0.00	0.02	0.00
7.16	2.00	0.00	0.00	0.02	0.00	7.24	2.00	0.00	0.00	0.02	0.00
7.30	2.00	0.00	0.00	0.02	0.00	7.39	2.00	0.00	0.00	0.03	0.00
7.43	2.00	0.00	0.00	0.01	0.00	7.50	2.00	0.00	0.00	0.02	0.00
7.59	2.00	0.00	0.00	0.03	0.00	7.63	2.00	0.00	0.00	0.01	0.00
7.70	2.00	0.00	0.00	0.02	0.00	7.78	2.00	0.00	0.00	0.02	0.00
7.83	2.00	0.00	0.00	0.02	0.00	7.89	2.00	0.00	0.00	0.02	0.00
7.95	2.00	0.00	0.00	0.02	0.00	8.02	2.00	0.00	0.00	0.02	0.00
8.11	2.00	0.00	0.00	0.03	0.00	8.16	2.00	0.00	0.00	0.02	0.00
8.21	2.00	0.00	0.00	0.02	0.00	8.30	2.00	0.00	0.00	0.03	0.00
8.36	2.00	0.00	0.00	0.02	0.00	8.41	2.00	0.00	0.00	0.02	0.00
8.47	2.00	0.00	0.00	0.02	0.00	8.56	2.00	0.00	0.00	0.03	0.00
8.61	2.00	0.00	0.00	0.02	0.00	8.70	2.00	0.00	0.00	0.03	0.00
8.75	2.00	0.00	0.00	0.02	0.00	8.81	2.00	0.00	0.00	0.02	0.00
8.90	2.00	0.00	0.00	0.03	0.00	8.94	2.00	0.00	0.00	0.01	0.00
9.01	2.00	0.00	0.00	0.02	0.00	9.09	2.00	0.00	0.00	0.02	0.00
9.13	2.00	0.00	0.00	0.01	0.00	9.20	2.00	0.00	0.00	0.02	0.00
9.27	2.00	0.00	0.00	0.02	0.00	9.35	2.00	0.00	0.00	0.02	0.00
9.39	2.00	0.00	0.00	0.01	0.00	9.45	2.00	0.00	0.00	0.02	0.00
9.54	2.00	0.00	0.00	0.03	0.00	9.59	2.00	0.00	0.00	0.02	0.00
9.65	2.00	0.00	0.00	0.02	0.00	9.73	2.00	0.00	0.00	0.02	0.00
9.81	2.00	0.00	0.00	0.02	0.00	9.85	2.00	0.00	0.00	0.01	0.00
9.94	2.00	0.00	0.00	0.03	0.00	10.00	2.00	0.00	0.00	0.02	0.00
10.04	2.00	0.00	0.00	0.01	0.00	10.12	2.00	0.00	0.00	0.02	0.00
10.19	2.00	0.00	0.00	0.02	0.00	10.24	2.00	0.00	0.00	0.02	0.00
10.31	2.00	0.00	0.00	0.02	0.00	10.39	2.00	0.00	0.00	0.02	0.00
10.48	2.00	0.00	0.00	0.03	0.00	10.53	2.00	0.00	0.00	0.02	0.00
10.63	2.00	0.00	0.00	0.03	0.00	10.67	2.00	0.00	0.00	0.01	0.00
10.71	2.00	0.00	0.00	0.01	0.00	10.79	2.00	0.00	0.00	0.02	0.00
10.83	2.00	0.00	0.00	0.01	0.00	10.93	2.00	0.00	0.00	0.03	0.00
10.98	2.00	0.00	0.00	0.02	0.00	11.06	2.00	0.00	0.00	0.02	0.00
11.11	2.00	0.00	0.00	0.02	0.00	11.16	2.00	0.00	0.00	0.02	0.00
11.23	2.00	0.00	0.00	0.02	0.00	11.31	2.00	0.00	0.00	0.02	0.00
11.36	2.00	0.00	0.00	0.02	0.00	11.42	2.00	0.00	0.00	0.02	0.00
11.51	2.00	0.00	0.00	0.03	0.00	11.56	2.00	0.00	0.00	0.02	0.00
11.65	2.00	0.00	0.00	0.03	0.00	11.71	2.00	0.00	0.00	0.02	0.00
11.75	2.00	0.00	0.00	0.01	0.00	11.84	2.00	0.00	0.00	0.03	0.00
11.89	2.00	0.00	0.00	0.02	0.00	11.96	2.00	0.00	0.00	0.02	0.00
12.03	2.00	0.00	0.00	0.02	0.00	12.11	2.00	0.00	0.00	0.02	0.00
12.16	2.00	0.00	0.00	0.02	0.00	12.21	2.00	0.00	0.00	0.02	0.00
12.30	2.00	0.00	0.00	0.03	0.00	12.35	2.00	0.00	0.00	0.02	0.00
12.41	2.00	0.00	0.00	0.02	0.00	12.49	2.00	0.00	0.00	0.02	0.00
12.56	2.00	0.00	0.00	0.02	0.00	12.60	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
12.67	2.00	0.00	0.00	0.02	0.00	12.75	2.00	0.00	0.00	0.02	0.00
12.80	2.00	0.00	0.00	0.02	0.00	12.90	2.00	0.00	0.00	0.03	0.00
12.95	2.00	0.00	0.00	0.02	0.00	13.02	2.00	0.00	0.00	0.02	0.00
13.06	2.00	0.00	0.00	0.01	0.00	13.14	2.00	0.00	0.00	0.02	0.00
13.19	2.00	0.00	0.00	0.02	0.00	13.29	2.00	0.00	0.00	0.03	0.00
13.33	2.00	0.00	0.00	0.01	0.00	13.39	2.00	0.00	0.00	0.02	0.00
13.48	2.00	0.00	0.00	0.03	0.00	13.54	2.00	0.00	0.00	0.02	0.00
13.59	2.00	0.00	0.00	0.02	0.00	13.67	2.00	0.00	0.00	0.02	0.00
13.72	2.00	0.00	0.00	0.02	0.00	13.78	2.00	0.00	0.00	0.02	0.00
13.86	2.00	0.00	0.00	0.02	0.00	13.93	2.00	0.00	0.00	0.02	0.00
14.01	2.00	0.00	0.00	0.02	0.00	14.05	2.00	0.00	0.00	0.01	0.00
14.14	2.00	0.00	0.00	0.03	0.00	14.21	2.00	0.00	0.00	0.02	0.00
14.24	2.00	0.00	0.00	0.01	0.00	14.31	2.00	0.00	0.00	0.02	0.00
14.39	2.00	0.00	0.00	0.02	0.00	14.44	2.00	0.00	0.00	0.02	0.00
14.54	2.00	0.00	0.00	0.03	0.00	14.59	2.00	0.00	0.00	0.02	0.00
14.64	2.00	0.00	0.00	0.02	0.00	14.70	2.00	0.00	0.00	0.02	0.00
14.79	2.00	0.00	0.00	0.03	0.00	14.83	2.00	0.00	0.00	0.01	0.00
14.93	2.00	0.00	0.00	0.03	0.00	14.98	2.00	0.00	0.00	0.02	0.00
15.03	2.00	0.00	0.00	0.02	0.00	15.10	2.00	0.00	0.00	0.02	0.00
15.18	2.00	0.00	0.00	0.02	0.00	15.23	2.00	0.00	0.00	0.02	0.00
15.33	2.00	0.00	0.00	0.03	0.00	15.37	2.00	0.00	0.00	0.01	0.00
15.44	2.00	0.00	0.00	0.02	0.00	15.52	2.00	0.00	0.00	0.02	0.00
15.56	2.00	0.00	0.00	0.01	0.00	15.63	2.00	0.00	0.00	0.02	0.00
15.71	2.00	0.00	0.00	0.02	0.00	15.77	2.00	0.00	0.00	0.02	0.00
15.82	2.00	0.00	0.00	0.02	0.00	15.89	2.00	0.00	0.00	0.02	0.00
15.97	2.00	0.00	0.00	0.02	0.00	16.02	2.00	0.00	0.00	0.02	0.00
16.10	2.00	0.00	0.00	0.02	0.00	16.17	2.00	0.00	0.00	0.02	0.00
16.22	2.00	0.00	0.00	0.02	0.00	16.28	2.00	0.00	0.00	0.02	0.00
16.37	2.00	0.00	0.00	0.03	0.00	16.42	2.00	0.00	0.00	0.02	0.00
16.52	2.00	0.00	0.00	0.03	0.00	16.55	2.00	0.00	0.00	0.01	0.00
16.62	2.00	0.00	0.00	0.02	0.00	16.70	2.00	0.00	0.00	0.02	0.00
16.74	2.00	0.00	0.00	0.01	0.00	16.82	2.00	0.00	0.00	0.02	0.00
16.91	2.00	0.00	0.00	0.03	0.00	16.94	2.00	0.00	0.00	0.01	0.00
17.01	2.00	0.00	0.00	0.02	0.00	17.10	2.00	0.00	0.00	0.03	0.00
17.15	2.00	0.00	0.00	0.02	0.00	17.21	2.00	0.00	0.00	0.02	0.00
17.30	2.00	0.00	0.00	0.03	0.00	17.34	2.00	0.00	0.00	0.01	0.00
17.41	2.00	0.00	0.00	0.02	0.00	17.49	2.00	0.00	0.00	0.02	0.00
17.53	2.00	0.00	0.00	0.01	0.00	17.59	2.00	0.00	0.00	0.02	0.00
17.67	2.00	0.00	0.00	0.02	0.00	17.73	2.00	0.00	0.00	0.02	0.00
17.79	2.00	0.00	0.00	0.02	0.00	17.87	2.00	0.00	0.00	0.02	0.00
17.92	2.00	0.00	0.00	0.02	0.00	17.99	2.00	0.00	0.00	0.02	0.00
18.07	2.00	0.00	0.00	0.02	0.00	18.14	2.00	0.00	0.00	0.02	0.00
18.19	2.00	0.00	0.00	0.02	0.00	18.26	2.00	0.00	0.00	0.02	0.00
18.34	2.00	0.00	0.00	0.02	0.00	18.38	2.00	0.00	0.00	0.01	0.00
18.45	2.00	0.00	0.00	0.02	0.00	18.53	2.00	0.00	0.00	0.02	0.00
18.60	2.00	0.00	0.00	0.02	0.00	18.68	2.00	0.00	0.00	0.02	0.00
18.72	2.00	0.00	0.00	0.01	0.00	18.79	2.00	0.00	0.00	0.02	0.00
18.84	2.00	0.00	0.00	0.02	0.00	18.92	2.00	0.00	0.00	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
18.98	2.00	0.00	0.00	0.02	0.00	19.06	2.00	0.00	0.00	0.02	0.00
19.11	2.00	0.00	0.00	0.02	0.00	19.18	2.00	0.00	0.00	0.02	0.00
19.25	2.00	0.00	0.00	0.02	0.00	19.33	2.00	0.00	0.00	0.02	0.00
19.37	2.00	0.00	0.00	0.01	0.00	19.47	2.00	0.00	0.00	0.03	0.00
19.52	2.00	0.00	0.00	0.02	0.00	19.57	2.00	0.00	0.00	0.02	0.00
19.62	2.00	0.00	0.00	0.02	0.00	19.71	2.00	0.00	0.00	0.03	0.00
19.77	2.00	0.00	0.00	0.02	0.00	19.82	2.00	0.00	0.00	0.02	0.00
19.91	2.00	0.00	0.00	0.03	0.00	19.96	2.00	0.00	0.00	0.02	0.00
20.02	2.00	0.00	0.00	0.02	0.00	20.11	2.00	0.00	0.00	0.03	0.00
20.18	2.00	0.00	0.00	0.02	0.00	20.23	2.00	0.00	0.00	0.02	0.00
20.28	2.00	0.00	0.00	0.02	0.00	20.37	2.00	0.00	0.00	0.03	0.00
20.42	2.00	0.00	0.00	0.02	0.00	20.48	2.00	0.00	0.00	0.02	0.00
20.56	2.00	0.00	0.00	0.02	0.00	20.63	2.00	0.00	0.00	0.02	0.00
20.67	2.00	0.00	0.00	0.01	0.00	20.74	2.00	0.00	0.00	0.02	0.00
20.83	2.00	0.00	0.00	0.03	0.00	20.90	2.00	0.00	0.00	0.02	0.00
20.97	2.00	0.00	0.00	0.02	0.00	21.02	2.00	0.00	0.00	0.02	0.00
21.10	2.00	0.00	0.00	0.02	0.00	21.17	2.00	0.00	0.00	0.02	0.00
21.22	2.00	0.00	0.00	0.02	0.00	21.27	2.00	0.00	0.00	0.02	0.00
21.37	2.00	0.00	0.00	0.03	0.00	21.43	2.00	0.00	0.00	0.02	0.00
21.46	2.00	0.00	0.00	0.01	0.00	21.55	2.00	0.00	0.00	0.03	0.00
21.62	2.00	0.00	0.00	0.02	0.00	21.66	2.00	0.00	0.00	0.01	0.00
21.74	2.00	0.00	0.00	0.02	0.00	21.81	2.00	0.00	0.00	0.02	0.00
21.85	2.00	0.00	0.00	0.01	0.00	21.93	2.00	0.00	0.00	0.02	0.00
22.00	2.00	0.00	0.00	0.02	0.00	22.07	2.00	0.00	0.00	0.02	0.00
22.16	2.00	0.00	0.00	0.03	0.00	22.19	2.00	0.00	0.00	0.01	0.00
22.26	2.00	0.00	0.00	0.02	0.00	22.33	2.00	0.00	0.00	0.02	0.00
22.40	2.00	0.00	0.00	0.02	0.00	22.45	2.00	0.00	0.00	0.02	0.00
22.53	2.00	0.00	0.00	0.02	0.00	22.60	2.00	0.00	0.00	0.02	0.00
22.64	2.00	0.00	0.00	0.01	0.00	22.70	2.00	0.00	0.00	0.02	0.00
22.80	2.00	0.00	0.00	0.03	0.00	22.84	2.00	0.00	0.00	0.01	0.00
22.90	2.00	0.00	0.00	0.02	0.00	23.00	2.00	0.00	0.00	0.03	0.00
23.05	2.00	0.00	0.00	0.02	0.00	23.14	2.00	0.00	0.00	0.03	0.00
23.18	2.00	0.00	0.00	0.01	0.00	23.24	2.00	0.00	0.00	0.02	0.00
23.32	2.00	0.00	0.00	0.02	0.00	23.39	2.00	0.00	0.00	0.02	0.00
23.44	2.00	0.00	0.00	0.02	0.00	23.53	2.00	0.00	0.00	0.03	0.00
23.59	2.00	0.00	0.00	0.02	0.00	23.63	2.00	0.00	0.00	0.01	0.00
23.69	2.00	0.00	0.00	0.02	0.00	23.77	2.00	0.00	0.00	0.02	0.00
23.82	2.00	0.00	0.00	0.02	0.00	23.93	2.00	0.00	0.00	0.03	0.00
23.95	2.00	0.00	0.00	0.01	0.00	24.03	2.00	0.00	0.00	0.02	0.00
24.12	2.00	0.00	0.00	0.03	0.00	24.16	2.00	0.00	0.00	0.01	0.00
24.22	2.00	0.00	0.00	0.02	0.00	24.30	2.00	0.00	0.00	0.02	0.00
24.37	2.00	0.00	0.00	0.02	0.00	24.43	2.00	0.00	0.00	0.02	0.00
24.50	2.00	0.00	0.00	0.02	0.00	24.57	2.00	0.00	0.00	0.02	0.00
24.62	2.00	0.00	0.00	0.02	0.00	24.69	2.00	0.00	0.00	0.02	0.00
24.77	2.00	0.00	0.00	0.02	0.00	24.83	2.00	0.00	0.00	0.02	0.00
24.88	2.00	0.00	0.00	0.02	0.00	24.97	2.00	0.00	0.00	0.03	0.00
25.02	2.00	0.00	0.00	0.02	0.00	25.11	2.00	0.00	0.00	0.03	0.00
25.17	2.00	0.00	0.00	0.02	0.00	25.21	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
25.29	2.00	0.00	0.00	0.02	0.00	25.36	2.00	0.00	0.00	0.02	0.00
25.40	2.00	0.00	0.00	0.01	0.00	25.46	2.00	0.00	0.00	0.02	0.00
25.54	2.00	0.00	0.00	0.02	0.00	25.62	2.00	0.00	0.00	0.02	0.00
25.66	2.00	0.00	0.00	0.01	0.00	25.75	2.00	0.00	0.00	0.03	0.00
25.80	2.00	0.00	0.00	0.02	0.00	25.85	2.00	0.00	0.00	0.02	0.00
25.96	2.00	0.00	0.00	0.03	0.00	26.01	2.00	0.00	0.00	0.02	0.00
26.05	2.00	0.00	0.00	0.01	0.00	26.12	2.00	0.00	0.00	0.02	0.00
26.19	2.00	0.00	0.00	0.02	0.00	26.25	2.00	0.00	0.00	0.02	0.00
26.33	2.00	0.00	0.00	0.02	0.00	26.42	2.00	0.00	0.00	0.03	0.00
26.46	2.00	0.00	0.00	0.01	0.00	26.52	2.00	0.00	0.00	0.02	0.00
26.61	2.00	0.00	0.00	0.03	0.00	26.67	2.00	0.00	0.00	0.02	0.00
26.71	2.00	0.00	0.00	0.01	0.00	26.79	2.00	0.00	0.00	0.02	0.00
26.87	2.00	0.00	0.00	0.02	0.00	26.92	2.00	0.00	0.00	0.02	0.00
26.98	2.00	0.00	0.00	0.02	0.00	27.06	2.00	0.00	0.00	0.02	0.00
27.11	2.00	0.00	0.00	0.02	0.00	27.21	2.00	0.00	0.00	0.03	0.00
27.26	2.00	0.00	0.00	0.02	0.00	27.32	2.00	0.00	0.00	0.02	0.00
27.40	2.00	0.00	0.00	0.02	0.00	27.45	2.00	0.00	0.00	0.02	0.00
27.52	2.00	0.00	0.00	0.02	0.00	27.60	2.00	0.00	0.00	0.02	0.00
27.65	2.00	0.00	0.00	0.02	0.00	27.71	2.00	0.00	0.00	0.02	0.00
27.80	2.00	0.00	0.00	0.03	0.00	27.84	2.00	0.00	0.00	0.01	0.00
27.90	2.00	0.00	0.00	0.02	0.00	27.99	2.00	0.00	0.00	0.03	0.00
28.05	2.00	0.00	0.00	0.02	0.00	28.10	2.00	0.00	0.00	0.02	0.00
28.17	2.00	0.00	0.00	0.02	0.00	28.25	2.00	0.00	0.00	0.02	0.00
28.30	2.00	0.00	0.00	0.02	0.00	28.39	2.00	0.00	0.00	0.03	0.00
28.44	2.00	0.00	0.00	0.02	0.00	28.49	2.00	0.00	0.00	0.02	0.00
28.54	2.00	0.00	0.00	0.02	0.00	28.62	2.00	0.00	0.00	0.02	0.00
28.68	2.00	0.00	0.00	0.02	0.00	28.74	2.00	0.00	0.00	0.02	0.00
28.83	2.00	0.00	0.00	0.03	0.00	28.89	2.00	0.00	0.00	0.02	0.00
28.98	2.00	0.00	0.00	0.03	0.00	29.03	2.00	0.00	0.00	0.02	0.00
29.09	2.00	0.00	0.00	0.02	0.00	29.14	2.00	0.00	0.00	0.02	0.00
29.22	2.00	0.00	0.00	0.02	0.00	29.27	2.00	0.00	0.00	0.02	0.00
29.38	2.00	0.00	0.00	0.03	0.00	29.43	2.00	0.00	0.00	0.02	0.00
29.48	2.00	0.00	0.00	0.02	0.00	29.57	2.00	0.00	0.00	0.03	0.00
29.62	2.00	0.00	0.00	0.02	0.00	29.68	2.00	0.00	0.00	0.02	0.00
29.73	2.00	0.00	0.00	0.02	0.00	29.82	2.00	0.00	0.00	0.03	0.00
29.87	2.00	0.00	0.00	0.02	0.00	29.94	2.00	0.00	0.00	0.02	0.00
30.02	2.00	0.00	0.00	0.02	0.00	30.07	2.00	0.00	0.00	0.02	0.00
30.16	2.00	0.00	0.00	0.03	0.00	30.19	2.00	0.00	0.00	0.01	0.00
30.26	2.00	0.00	0.00	0.02	0.00	30.36	2.00	0.00	0.00	0.03	0.00
30.41	2.00	0.00	0.00	0.02	0.00	30.46	2.00	0.00	0.00	0.02	0.00
30.53	2.00	0.00	0.00	0.02	0.00	30.61	2.00	0.00	0.00	0.02	0.00
30.65	2.00	0.00	0.00	0.01	0.00	30.71	2.00	0.00	0.00	0.02	0.00
30.81	2.00	0.00	0.00	0.03	0.00	30.84	2.00	0.00	0.00	0.01	0.00
30.91	2.00	0.00	0.00	0.02	0.00	30.99	2.00	0.00	0.00	0.02	0.00
31.04	2.00	0.00	0.00	0.02	0.00	31.11	2.00	0.00	0.00	0.02	0.00
31.19	2.00	0.00	0.00	0.02	0.00	31.25	2.00	0.00	0.00	0.02	0.00
31.30	2.00	0.00	0.00	0.02	0.00	31.39	2.00	0.00	0.00	0.03	0.00
31.45	2.00	0.00	0.00	0.02	0.00	31.50	2.00	0.00	0.00	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
31.60	2.00	0.00	0.00	0.03	0.00	31.65	2.00	0.00	0.00	0.02	0.00
31.73	2.00	0.00	0.00	0.02	0.00	31.80	2.00	0.00	0.00	0.02	0.00
31.84	2.00	0.00	0.00	0.01	0.00	31.91	2.00	0.00	0.00	0.02	0.00
31.99	2.00	0.00	0.00	0.02	0.00	32.03	2.00	0.00	0.00	0.01	0.00
32.09	2.00	0.00	0.00	0.02	0.00	32.19	2.00	0.00	0.00	0.03	0.00
32.25	2.00	0.00	0.00	0.02	0.00	32.29	2.00	0.00	0.00	0.01	0.00
32.38	2.00	0.00	0.00	0.03	0.00	32.43	2.00	0.00	0.00	0.02	0.00
32.48	2.00	0.00	0.00	0.02	0.00	32.58	2.00	0.00	0.00	0.03	0.00
32.63	2.00	0.00	0.00	0.02	0.00	32.69	2.00	0.00	0.00	0.02	0.00
32.74	2.00	0.00	0.00	0.02	0.00	32.83	2.00	0.00	0.00	0.03	0.00
32.88	2.00	0.00	0.00	0.02	0.00	32.97	2.00	0.00	0.00	0.03	0.00
33.01	2.00	0.00	0.00	0.01	0.00	33.07	2.00	0.00	0.00	0.02	0.00
33.16	2.00	0.00	0.00	0.03	0.00	33.20	2.00	0.00	0.00	0.01	0.00
33.27	2.00	0.00	0.00	0.02	0.00	33.36	2.00	0.00	0.00	0.03	0.00
33.42	2.00	0.00	0.00	0.02	0.00	33.51	2.00	0.00	0.00	0.03	0.00
33.56	2.00	0.00	0.00	0.02	0.00	33.61	2.00	0.00	0.00	0.02	0.00
33.67	2.00	0.00	0.00	0.02	0.00	33.76	2.00	0.00	0.00	0.03	0.00
33.81	2.00	0.00	0.00	0.02	0.00	33.86	2.00	0.00	0.00	0.02	0.00
33.94	2.00	0.00	0.00	0.02	0.00	34.02	2.00	0.00	0.00	0.02	0.00
34.06	2.00	0.00	0.00	0.01	0.00	34.14	2.00	0.00	0.00	0.02	0.00
34.21	2.00	0.00	0.00	0.02	0.00	34.25	2.00	0.00	0.00	0.01	0.00
34.33	2.00	0.00	0.00	0.02	0.00	34.41	2.00	0.00	0.00	0.02	0.00
34.49	2.00	0.00	0.00	0.02	0.00	34.56	2.00	0.00	0.00	0.02	0.00
34.59	2.00	0.00	0.00	0.01	0.00	34.67	2.00	0.00	0.00	0.02	0.00
34.76	2.00	0.00	0.00	0.03	0.00	34.80	2.00	0.00	0.00	0.01	0.00
34.85	2.00	0.00	0.00	0.02	0.00	34.93	2.00	0.00	0.00	0.02	0.00
34.98	2.00	0.00	0.00	0.02	0.00	35.05	2.00	0.00	0.00	0.02	0.00
35.13	2.00	0.00	0.00	0.02	0.00	35.18	2.00	0.00	0.00	0.02	0.00
35.24	2.00	0.00	0.00	0.02	0.00	35.32	2.00	0.00	0.00	0.02	0.00
35.41	2.00	0.00	0.00	0.03	0.00	35.46	2.00	0.00	0.00	0.02	0.00
35.51	2.00	0.00	0.00	0.02	0.00	35.58	2.00	0.00	0.00	0.02	0.00
35.66	2.00	0.00	0.00	0.02	0.00	35.71	2.00	0.00	0.00	0.02	0.00
35.76	2.00	0.00	0.00	0.02	0.00	35.86	2.00	0.00	0.00	0.03	0.00
35.91	2.00	0.00	0.00	0.02	0.00	36.01	2.00	0.00	0.00	0.03	0.00
36.05	2.00	0.00	0.00	0.01	0.00	36.12	2.00	0.00	0.00	0.02	0.00
36.20	2.00	0.00	0.00	0.02	0.00	36.23	2.00	0.00	0.00	0.01	0.00
36.31	2.00	0.00	0.00	0.02	0.00	36.35	2.00	0.00	0.00	0.01	0.00
36.45	2.00	0.00	0.00	0.03	0.00	36.51	2.00	0.00	0.00	0.02	0.00
36.58	2.00	0.00	0.00	0.02	0.00	36.66	2.00	0.00	0.00	0.02	0.00
36.70	2.00	0.00	0.00	0.01	0.00	36.80	2.00	0.00	0.00	0.03	0.00
36.85	2.00	0.00	0.00	0.02	0.00	36.89	2.00	0.00	0.00	0.01	0.00
36.96	2.00	0.00	0.00	0.02	0.00	37.03	2.00	0.00	0.00	0.02	0.00
37.09	2.00	0.00	0.00	0.02	0.00	37.15	2.00	0.00	0.00	0.02	0.00
37.23	2.00	0.00	0.00	0.02	0.00	37.27	2.00	0.00	0.00	0.01	0.00
37.34	2.00	0.00	0.00	0.02	0.00	37.43	2.00	0.00	0.00	0.03	0.00
37.49	2.00	0.00	0.00	0.02	0.00	37.54	2.00	0.00	0.00	0.02	0.00
37.62	2.00	0.00	0.00	0.02	0.00	37.69	2.00	0.00	0.00	0.02	0.00
37.74	2.00	0.00	0.00	0.02	0.00	37.82	2.00	0.00	0.00	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
37.89	2.00	0.00	0.00	0.02	0.00	37.93	2.00	0.00	0.00	0.01	0.00
38.02	2.00	0.00	0.00	0.03	0.00	38.08	2.00	0.00	0.00	0.02	0.00
38.13	2.00	0.00	0.00	0.02	0.00	38.23	2.00	0.00	0.00	0.03	0.00
38.28	2.00	0.00	0.00	0.02	0.00	38.35	2.00	0.00	0.00	0.02	0.00
38.42	2.00	0.00	0.00	0.02	0.00	38.47	2.00	0.00	0.00	0.02	0.00
38.52	2.00	0.00	0.00	0.02	0.00	38.61	2.00	0.00	0.00	0.03	0.00
38.67	2.00	0.00	0.00	0.02	0.00	38.72	2.00	0.00	0.00	0.02	0.00
38.82	2.00	0.00	0.00	0.03	0.00	38.86	2.00	0.00	0.00	0.01	0.00
38.96	2.00	0.00	0.00	0.03	0.00	39.01	2.00	0.00	0.00	0.02	0.00
39.05	2.00	0.00	0.00	0.01	0.00	39.13	2.00	0.00	0.00	0.02	0.00
39.21	2.00	0.00	0.00	0.02	0.00	39.24	2.00	0.00	0.00	0.01	0.00
39.31	2.00	0.00	0.00	0.02	0.00	39.40	2.00	0.00	0.00	0.03	0.00
39.44	2.00	0.00	0.00	0.01	0.00	39.51	2.00	0.00	0.00	0.02	0.00
39.60	2.00	0.00	0.00	0.03	0.00	39.66	2.00	0.00	0.00	0.02	0.00
39.70	2.00	0.00	0.00	0.01	0.00	39.80	2.00	0.00	0.00	0.03	0.00
39.85	2.00	0.00	0.00	0.02	0.00	39.90	2.00	0.00	0.00	0.02	0.00
39.98	2.00	0.00	0.00	0.02	0.00	40.05	2.00	0.00	0.00	0.02	0.00
40.10	2.00	0.00	0.00	0.02	0.00	40.20	2.00	0.00	0.00	0.03	0.00
40.25	2.00	0.00	0.00	0.02	0.00	40.30	2.00	0.00	0.00	0.02	0.00
40.40	2.00	0.00	0.00	0.03	0.00	40.45	2.00	0.00	0.00	0.02	0.00
40.50	2.00	0.00	0.00	0.02	0.00	40.59	2.00	0.00	0.00	0.03	0.00
40.64	2.00	0.00	0.00	0.02	0.00	40.69	2.00	0.00	0.00	0.02	0.00
40.79	2.00	0.00	0.00	0.03	0.00	40.83	2.00	0.00	0.00	0.01	0.00
40.92	2.00	0.00	0.00	0.03	0.00	40.98	2.00	0.00	0.00	0.02	0.00
41.03	2.00	0.00	0.00	0.02	0.00	41.08	2.00	0.00	0.00	0.02	0.00
41.18	2.00	0.00	0.00	0.03	0.00	41.22	2.00	0.00	0.00	0.01	0.00
41.31	2.00	0.00	0.00	0.03	0.00	41.36	2.00	0.00	0.00	0.02	0.00
41.42	2.00	0.00	0.00	0.02	0.00	41.50	2.00	0.00	0.00	0.02	0.00
41.54	2.00	0.00	0.00	0.01	0.00	41.61	2.00	0.00	0.00	0.02	0.00
41.70	2.00	0.00	0.00	0.03	0.00	41.75	2.00	0.00	0.00	0.02	0.00
41.80	2.00	0.00	0.00	0.02	0.00	41.87	2.00	0.00	0.00	0.02	0.00
41.95	2.00	0.00	0.00	0.02	0.00	42.01	2.00	0.00	0.00	0.02	0.00
42.10	2.00	0.00	0.00	0.03	0.00	42.14	2.00	0.00	0.00	0.01	0.00
42.21	2.00	0.00	0.00	0.02	0.00	42.27	2.00	0.00	0.00	0.02	0.00
42.34	2.00	0.00	0.00	0.02	0.00	42.39	2.00	0.00	0.00	0.02	0.00
42.49	2.00	0.00	0.00	0.03	0.00	42.54	2.00	0.00	0.00	0.02	0.00
42.59	2.00	0.00	0.00	0.02	0.00	42.69	2.00	0.00	0.00	0.03	0.00
42.74	2.00	0.00	0.00	0.02	0.00	42.80	2.00	0.00	0.00	0.02	0.00
42.89	2.00	0.00	0.00	0.03	0.00	42.93	2.00	0.00	0.00	0.01	0.00
42.99	2.00	0.00	0.00	0.02	0.00	43.08	2.00	0.00	0.00	0.03	0.00
43.11	2.00	0.00	0.00	0.01	0.00	43.18	2.00	0.00	0.00	0.02	0.00
43.28	2.00	0.00	0.00	0.03	0.00	43.35	2.00	0.00	0.00	0.02	0.00
43.38	2.00	0.00	0.00	0.01	0.00	43.45	2.00	0.00	0.00	0.02	0.00
43.53	2.00	0.00	0.00	0.02	0.00	43.58	2.00	0.00	0.00	0.02	0.00
43.64	2.00	0.00	0.00	0.02	0.00	43.73	2.00	0.00	0.00	0.03	0.00
43.78	2.00	0.00	0.00	0.02	0.00	43.84	2.00	0.00	0.00	0.02	0.00
43.92	2.00	0.00	0.00	0.02	0.00	43.98	2.00	0.00	0.00	0.02	0.00
44.07	2.00	0.00	0.00	0.03	0.00	44.12	2.00	0.00	0.00	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
44.17	2.00	0.00	0.00	0.02	0.00	44.23	2.00	0.00	0.00	0.02	0.00
44.29	2.00	0.00	0.00	0.02	0.00	44.39	2.00	0.00	0.00	0.03	0.00
44.43	2.00	0.00	0.00	0.01	0.00	44.49	2.00	0.00	0.00	0.02	0.00
44.57	2.00	0.00	0.00	0.02	0.00	44.67	2.00	0.00	0.00	0.03	0.00
44.73	2.00	0.00	0.00	0.02	0.00	44.78	2.00	0.00	0.00	0.02	0.00
44.82	2.00	0.00	0.00	0.01	0.00	44.93	2.00	0.00	0.00	0.03	0.00
44.97	2.00	0.00	0.00	0.01	0.00	45.02	2.00	0.00	0.00	0.02	0.00
45.09	2.00	0.00	0.00	0.02	0.00	45.17	2.00	0.00	0.00	0.02	0.00
45.22	2.00	0.00	0.00	0.02	0.00	45.30	2.00	0.00	0.00	0.02	0.00
45.37	2.00	0.00	0.00	0.02	0.00	45.42	2.00	0.00	0.00	0.02	0.00
45.50	2.00	0.00	0.00	0.02	0.00	45.57	2.00	0.00	0.00	0.02	0.00
45.61	2.00	0.00	0.00	0.01	0.00	45.72	2.00	0.00	0.00	0.03	0.00
45.77	2.00	0.00	0.00	0.02	0.00	45.80	2.00	0.00	0.00	0.01	0.00
45.88	2.00	0.00	0.00	0.02	0.00	45.96	2.00	0.00	0.00	0.02	0.00
46.01	2.00	0.00	0.00	0.02	0.00	46.11	2.00	0.00	0.00	0.03	0.00
46.14	2.00	0.00	0.00	0.01	0.00	46.21	2.00	0.00	0.00	0.02	0.00
46.26	2.00	0.00	0.00	0.02	0.00	46.35	2.00	0.00	0.00	0.03	0.00
46.41	2.00	0.00	0.00	0.02	0.00	46.49	2.00	0.00	0.00	0.02	0.00
46.55	2.00	0.00	0.00	0.02	0.00	46.59	2.00	0.00	0.00	0.01	0.00
46.68	2.00	0.00	0.00	0.03	0.00	46.74	2.00	0.00	0.00	0.02	0.00
46.80	2.00	0.00	0.00	0.02	0.00	46.85	2.00	0.00	0.00	0.02	0.00
46.93	2.00	0.00	0.00	0.02	0.00	47.00	2.00	0.00	0.00	0.02	0.00
47.10	2.00	0.00	0.00	0.03	0.00	47.15	2.00	0.00	0.00	0.02	0.00
47.20	2.00	0.00	0.00	0.02	0.00	47.25	2.00	0.00	0.00	0.02	0.00
47.31	2.00	0.00	0.00	0.02	0.00	47.40	2.00	0.00	0.00	0.03	0.00
47.44	2.00	0.00	0.00	0.01	0.00	47.52	2.00	0.00	0.00	0.02	0.00
47.58	2.00	0.00	0.00	0.02	0.00	47.67	2.00	0.00	0.00	0.03	0.00
47.73	2.00	0.00	0.00	0.02	0.00	47.78	2.00	0.00	0.00	0.02	0.00
47.86	2.00	0.00	0.00	0.02	0.00	47.92	2.00	0.00	0.00	0.02	0.00
47.98	2.00	0.00	0.00	0.02	0.00	48.05	2.00	0.00	0.00	0.02	0.00
48.12	2.00	0.00	0.00	0.02	0.00	48.19	2.00	0.00	0.00	0.02	0.00
48.27	2.00	0.00	0.00	0.02	0.00	48.32	2.00	0.00	0.00	0.02	0.00
48.39	2.00	0.00	0.00	0.02	0.00	48.47	2.00	0.00	0.00	0.02	0.00
48.52	2.00	0.00	0.00	0.02	0.00	48.57	2.00	0.00	0.00	0.02	0.00
48.67	2.00	0.00	0.00	0.03	0.00	48.71	2.00	0.00	0.00	0.01	0.00
48.76	2.00	0.00	0.00	0.02	0.00	48.82	2.00	0.00	0.00	0.02	0.00
48.93	2.00	0.00	0.00	0.03	0.00	48.97	2.00	0.00	0.00	0.01	0.00
49.05	2.00	0.00	0.00	0.02	0.00	49.08	2.00	0.00	0.00	0.01	0.00
49.16	2.00	0.00	0.00	0.02	0.00	49.25	2.00	0.00	0.00	0.03	0.00
49.29	2.00	0.00	0.00	0.01	0.00	49.36	2.00	0.00	0.00	0.02	0.00
49.43	2.00	0.00	0.00	0.02	0.00	49.48	2.00	0.00	0.00	0.02	0.00
49.55	2.00	0.00	0.00	0.02	0.00	49.64	2.00	0.00	0.00	0.03	0.00
49.70	2.00	0.00	0.00	0.02	0.00	49.75	2.00	0.00	0.00	0.02	0.00
49.81	2.00	0.00	0.00	0.02	0.00	49.90	2.00	0.00	0.00	0.03	0.00
49.94	2.00	0.00	0.00	0.01	0.00	50.01	2.00	0.00	0.00	0.02	0.00
50.08	2.00	0.00	0.00	0.02	0.00	50.15	2.00	0.00	0.00	0.02	0.00
50.24	2.00	0.00	0.00	0.03	0.00	50.30	2.00	0.00	0.00	0.02	0.00
50.34	2.00	0.00	0.00	0.01	0.00	50.41	2.00	0.00	0.00	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
50.47	2.00	0.00	0.00	0.02	0.00	50.54	2.00	0.00	0.00	0.02	0.00
50.62	2.00	0.00	0.00	0.02	0.00	50.66	2.00	0.00	0.00	0.01	0.00
50.77	2.00	0.00	0.00	0.03	0.00	50.81	2.00	0.00	0.00	0.01	0.00
50.87	2.00	0.00	0.00	0.02	0.00	50.92	2.00	0.00	0.00	0.02	0.00
51.01	2.00	0.00	0.00	0.03	0.00	51.07	2.00	0.00	0.00	0.02	0.00
51.15	2.00	0.00	0.00	0.02	0.00	51.21	2.00	0.00	0.00	0.02	0.00
51.26	2.00	0.00	0.00	0.02	0.00	51.32	2.00	0.00	0.00	0.02	0.00
51.39	2.00	0.00	0.00	0.02	0.00	51.46	2.00	0.00	0.00	0.02	0.00
51.53	2.00	0.00	0.00	0.02	0.00	51.61	2.00	0.00	0.00	0.02	0.00
51.65	2.00	0.00	0.00	0.01	0.00	51.72	2.00	0.00	0.00	0.02	0.00
51.81	2.00	0.00	0.00	0.03	0.00	51.84	2.00	0.00	0.00	0.01	0.00
51.92	2.00	0.00	0.00	0.02	0.00	52.01	2.00	0.00	0.00	0.03	0.00
52.06	2.00	0.00	0.00	0.02	0.00	52.11	2.00	0.00	0.00	0.02	0.00
52.19	2.00	0.00	0.00	0.02	0.00	52.25	2.00	0.00	0.00	0.02	0.00
52.30	2.00	0.00	0.00	0.02	0.00	52.38	2.00	0.00	0.00	0.02	0.00
52.45	2.00	0.00	0.00	0.02	0.00	52.49	2.00	0.00	0.00	0.01	0.00
52.57	2.00	0.00	0.00	0.02	0.00	52.65	2.00	0.00	0.00	0.02	0.00
52.70	2.00	0.00	0.00	0.02	0.00	52.79	2.00	0.00	0.00	0.03	0.00
52.85	2.00	0.00	0.00	0.02	0.00	52.89	2.00	0.00	0.00	0.01	0.00
52.99	2.00	0.00	0.00	0.03	0.00	53.04	2.00	0.00	0.00	0.02	0.00
53.08	2.00	0.00	0.00	0.01	0.00	53.17	2.00	0.00	0.00	0.03	0.00
53.24	2.00	0.00	0.00	0.02	0.00	53.33	2.00	0.00	0.00	0.03	0.00
53.39	2.00	0.00	0.00	0.02	0.00	53.42	2.00	0.00	0.00	0.01	0.00
53.49	2.00	0.00	0.00	0.02	0.00	53.58	2.00	0.00	0.00	0.03	0.00
53.63	2.00	0.00	0.00	0.02	0.00	53.68	2.00	0.00	0.00	0.02	0.00
53.77	2.00	0.00	0.00	0.03	0.00	53.83	2.00	0.00	0.00	0.02	0.00
53.88	2.00	0.00	0.00	0.02	0.00	53.97	2.00	0.00	0.00	0.03	0.00
54.03	2.00	0.00	0.00	0.02	0.00	54.08	2.00	0.00	0.00	0.02	0.00
54.18	2.00	0.00	0.00	0.03	0.00	54.22	2.00	0.00	0.00	0.01	0.00
54.27	2.00	0.00	0.00	0.02	0.00	54.38	2.00	0.00	0.00	0.03	0.00
54.42	2.00	0.00	0.00	0.01	0.00	54.47	2.00	0.00	0.00	0.02	0.00
54.57	2.00	0.00	0.00	0.03	0.00	54.61	2.00	0.00	0.00	0.01	0.00
54.68	2.00	0.00	0.00	0.02	0.00	54.75	2.00	0.00	0.00	0.02	0.00
54.79	2.00	0.00	0.00	0.01	0.00	54.86	2.00	0.00	0.00	0.02	0.00
54.95	2.00	0.00	0.00	0.03	0.00	55.01	2.00	0.00	0.00	0.02	0.00
55.06	2.00	0.00	0.00	0.02	0.00	55.12	2.00	0.00	0.00	0.02	0.00
55.21	2.00	0.00	0.00	0.03	0.00	55.25	2.00	0.00	0.00	0.01	0.00
55.32	2.00	0.00	0.00	0.02	0.00	55.40	2.00	0.00	0.00	0.02	0.00
55.50	2.00	0.00	0.00	0.03	0.00	55.52	2.00	0.00	0.00	0.01	0.00
55.60	2.00	0.00	0.00	0.02	0.00	55.67	2.00	0.00	0.00	0.02	0.00
55.72	2.00	0.00	0.00	0.02	0.00	55.79	2.00	0.00	0.00	0.02	0.00
55.86	2.00	0.00	0.00	0.02	0.00	55.95	2.00	0.00	0.00	0.03	0.00
56.00	2.00	0.00	0.00	0.02	0.00	56.05	2.00	0.00	0.00	0.02	0.00
56.11	2.00	0.00	0.00	0.02	0.00	56.19	2.00	0.00	0.00	0.02	0.00
56.24	2.00	0.00	0.00	0.02	0.00	56.34	2.00	0.00	0.00	0.03	0.00
56.37	2.00	0.00	0.00	0.01	0.00	56.43	2.00	0.00	0.00	0.02	0.00
56.54	2.00	0.00	0.00	0.03	0.00	56.59	2.00	0.00	0.00	0.02	0.00
56.64	2.00	0.00	0.00	0.02	0.00	56.73	2.00	0.00	0.00	0.03	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
56.79	2.00	0.00	0.00	0.02	0.00	56.84	2.00	0.00	0.00	0.02	0.00
56.93	2.00	0.00	0.00	0.03	0.00	56.96	2.00	0.00	0.00	0.01	0.00
57.03	2.00	0.00	0.00	0.02	0.00	57.13	2.00	0.00	0.00	0.03	0.00
57.16	2.00	0.00	0.00	0.01	0.00	57.23	2.00	0.00	0.00	0.02	0.00
57.29	2.00	0.00	0.00	0.02	0.00	57.38	2.00	0.00	0.00	0.03	0.00
57.42	2.00	0.00	0.00	0.01	0.00	57.49	2.00	0.00	0.00	0.02	0.00
57.57	2.00	0.00	0.00	0.02	0.00	57.62	2.00	0.00	0.00	0.02	0.00
57.68	2.00	0.00	0.00	0.02	0.00	57.77	2.00	0.00	0.00	0.03	0.00
57.85	2.00	0.00	0.00	0.02	0.00	57.92	2.00	0.00	0.00	0.02	0.00
57.97	2.00	0.00	0.00	0.02	0.00	58.02	2.00	0.00	0.00	0.02	0.00
58.07	2.00	0.00	0.00	0.02	0.00	58.16	2.00	0.00	0.00	0.03	0.00
58.23	2.00	0.00	0.00	0.02	0.00	58.31	2.00	0.00	0.00	0.02	0.00
58.37	2.00	0.00	0.00	0.02	0.00	58.42	2.00	0.00	0.00	0.02	0.00
58.50	2.00	0.00	0.00	0.02	0.00	58.57	2.00	0.00	0.00	0.02	0.00
58.61	2.00	0.00	0.00	0.01	0.00	58.68	2.00	0.00	0.00	0.02	0.00
58.76	2.00	0.00	0.00	0.02	0.00	58.80	2.00	0.00	0.00	0.01	0.00
58.87	2.00	0.00	0.00	0.02	0.00	58.95	2.00	0.00	0.00	0.02	0.00
59.01	2.00	0.00	0.00	0.02	0.00	59.06	2.00	0.00	0.00	0.02	0.00
59.16	2.00	0.00	0.00	0.03	0.00	59.19	2.00	0.00	0.00	0.01	0.00
59.29	2.00	0.00	0.00	0.03	0.00	59.33	2.00	0.00	0.00	0.01	0.00
59.39	2.00	0.00	0.00	0.02	0.00	59.47	2.00	0.00	0.00	0.02	0.00
59.54	2.00	0.00	0.00	0.02	0.00	59.58	2.00	0.00	0.00	0.01	0.00
59.65	2.00	0.00	0.00	0.02	0.00	59.73	2.00	0.00	0.00	0.02	0.00
59.81	2.00	0.00	0.00	0.02	0.00	59.85	2.00	0.00	0.00	0.01	0.00
59.92	2.00	0.00	0.00	0.02	0.00	59.99	2.00	0.00	0.00	0.02	0.00
60.08	2.00	0.00	0.00	0.03	0.00	60.13	2.00	0.00	0.00	0.02	0.00
60.18	2.00	0.00	0.00	0.02	0.00	60.27	2.00	0.00	0.00	0.03	0.00
60.33	2.00	0.00	0.00	0.02	0.00	60.38	2.00	0.00	0.00	0.02	0.00
60.47	2.00	0.00	0.00	0.03	0.00						

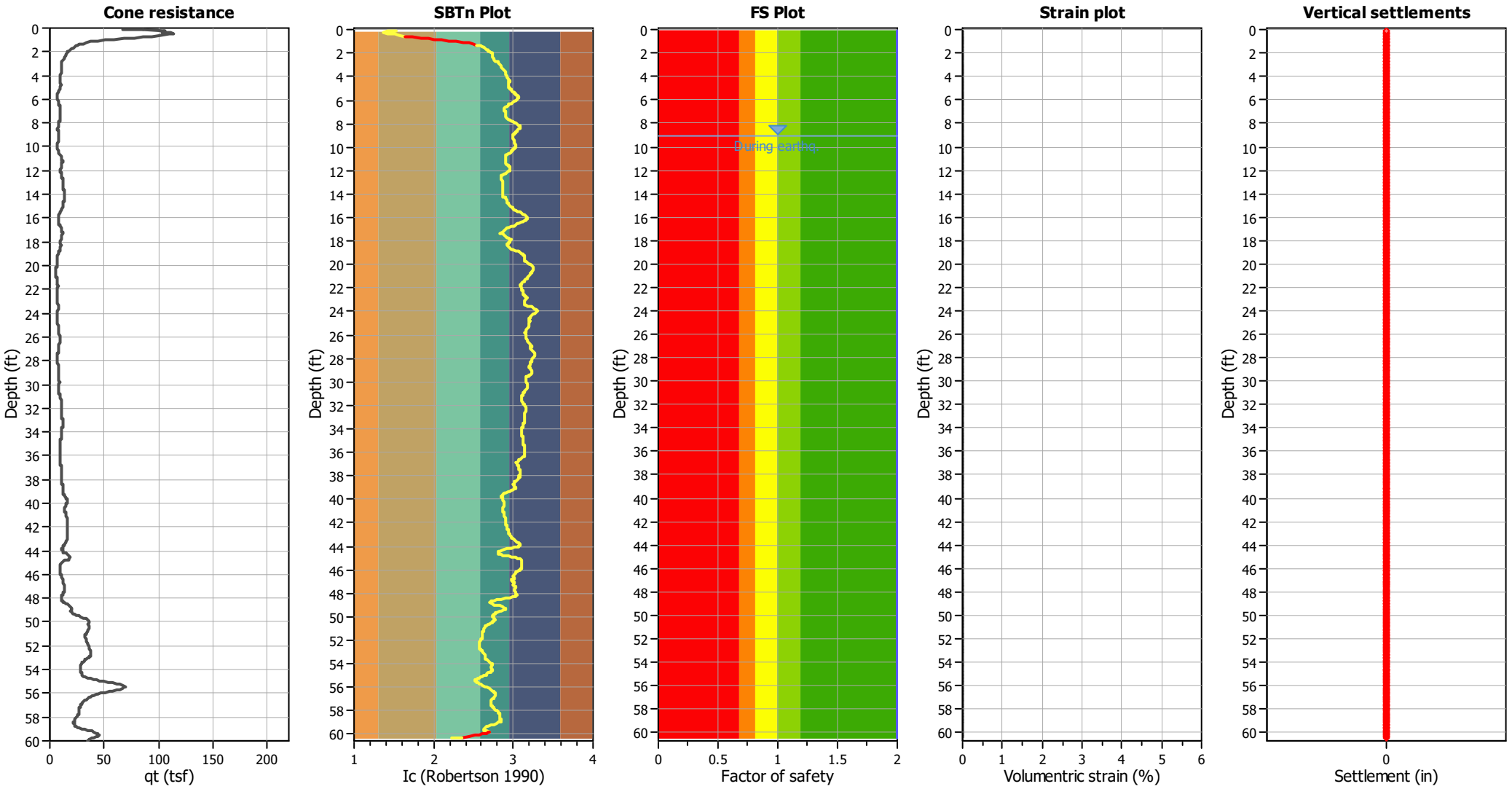
Overall liquefaction potential: 0.00

LPI = 0.00 - Liquefaction risk very low
LPI between 0.00 and 5.00 - Liquefaction risk low
LPI between 5.00 and 15.00 - Liquefaction risk high
LPI > 15.00 - Liquefaction risk very high

Abbreviations

FS: Calculated factor of safety for test point
F_L: 1 - FS
w_z: Function value of the extend of soil liquefaction according to depth
d_z: Layer thickness (ft)
LPI: Liquefaction potential index value for test point

Estimation of post-earthquake settlements



Abbreviations

q_t:	Total cone resistance (cone resistance q_c corrected for pore water effects)
I_c:	Soil Behaviour Type Index
FS:	Calculated Factor of Safety against liquefaction
Volumentric strain:	Post-liquefaction volumentric strain

:: Lateral displacement index calculation ::

Depth (ft)	q_t (tsf)	Q_{tn}	R_f (%)	$Q_{tn,cs}$	FS	D_r	$Gamma_{max}$ (%)	Lat. disp. (in)
9.01	8.19	12.37	3.73	82.52	2.00	0.00	0.00	0.00
9.09	8.22	12.41	3.74	82.78	2.00	0.00	0.00	0.00
9.13	8.21	12.39	3.75	82.78	2.00	0.00	0.00	0.00
9.20	8.17	12.32	3.72	82.39	2.00	0.00	0.00	0.00
9.27	8.09	12.17	3.71	81.87	2.00	0.00	0.00	0.00
9.35	7.98	11.99	3.68	81.08	2.00	0.00	0.00	0.00
9.39	7.84	11.76	3.63	80.02	2.00	0.00	0.00	0.00
9.45	7.69	11.52	3.58	78.94	2.00	0.00	0.00	0.00
9.54	7.54	11.27	3.52	77.70	2.00	0.00	0.00	0.00
9.59	7.39	11.03	3.47	76.58	2.00	0.00	0.00	0.00
9.65	7.26	10.82	3.40	75.30	2.00	0.00	0.00	0.00
9.73	7.13	10.59	3.32	73.99	2.00	0.00	0.00	0.00
9.81	6.99	10.36	3.24	72.66	2.00	0.00	0.00	0.00
9.85	6.89	10.20	3.16	71.46	2.00	0.00	0.00	0.00
9.94	6.81	10.06	3.08	70.39	2.00	0.00	0.00	0.00
10.00	6.75	9.96	3.03	69.61	2.00	0.00	0.00	0.00
10.04	6.74	9.94	2.97	68.99	2.00	0.00	0.00	0.00
10.12	6.81	10.05	2.94	69.00	2.00	0.00	0.00	0.00
10.19	6.96	10.28	2.94	69.63	2.00	0.00	0.00	0.00
10.24	7.18	10.63	2.97	70.86	2.00	0.00	0.00	0.00
10.31	7.51	11.15	3.05	72.96	2.00	0.00	0.00	0.00
10.39	7.85	11.70	3.13	75.13	2.00	0.00	0.00	0.00
10.48	8.26	12.35	3.16	77.07	2.00	0.00	0.00	0.00
10.53	8.69	13.04	3.21	79.21	2.00	0.00	0.00	0.00
10.63	9.14	13.75	3.30	81.80	2.00	1.50	0.00	0.00
10.67	9.60	14.48	3.42	84.82	2.00	3.22	0.00	0.00
10.71	10.01	15.13	3.52	87.48	2.00	4.68	0.00	0.00
10.79	10.33	15.64	3.63	89.85	2.00	5.76	0.00	0.00
10.83	10.50	15.91	3.75	91.85	2.00	6.33	0.00	0.00
10.93	10.75	16.31	3.78	93.18	2.00	7.14	0.00	0.00
10.98	11.01	16.72	3.83	94.60	2.00	7.96	0.00	0.00
11.06	11.19	17.00	3.91	96.27	2.00	8.52	0.00	0.00
11.11	11.33	17.22	3.99	97.70	2.00	8.95	0.00	0.00
11.16	11.42	17.37	4.04	98.57	2.00	9.22	0.00	0.00
11.23	11.42	17.36	4.07	98.91	2.00	9.21	0.00	0.00
11.31	11.37	17.21	4.09	98.90	2.00	8.93	0.00	0.00
11.36	11.30	17.04	4.10	98.56	2.00	8.59	0.00	0.00
11.42	11.29	16.93	4.07	98.01	2.00	8.38	0.00	0.00
11.51	11.10	16.53	4.11	97.52	2.00	7.58	0.00	0.00
11.56	10.86	16.11	4.14	96.84	2.00	6.73	0.00	0.00
11.65	10.63	15.65	4.15	95.79	2.00	5.79	0.00	0.00
11.71	10.44	15.29	4.13	94.68	2.00	5.02	0.00	0.00
11.75	10.23	14.92	4.11	93.61	2.00	4.21	0.00	0.00
11.84	10.11	14.60	4.05	92.08	2.00	3.49	0.00	0.00
11.89	10.00	14.37	3.96	90.56	2.00	2.96	0.00	0.00
11.96	9.97	14.23	3.81	88.71	2.00	2.65	0.00	0.00
12.03	9.99	14.17	3.65	86.82	2.00	2.50	0.00	0.00
12.11	10.04	14.16	3.46	84.80	2.00	2.49	0.00	0.00

:: Estimation of post-earthquake lateral Displacements :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	R_f (%)	$Q_{tn,cs}$	FS	D_r	$Gamma_{max}$ (%)	Lat. disp. (in)
12.16	10.16	14.28	3.29	83.13	2.00	2.76	0.00	0.00
12.21	10.35	14.49	3.12	81.63	2.00	3.24	0.00	0.00
12.30	10.54	14.68	2.98	80.34	2.00	3.67	0.00	0.00
12.35	10.78	14.96	2.87	79.44	2.00	4.29	0.00	0.00
12.41	10.95	15.15	2.82	79.26	2.00	4.72	0.00	0.00
12.49	11.12	15.34	2.82	79.58	2.00	5.13	0.00	0.00
12.56	11.24	15.48	2.87	80.48	2.00	5.43	0.00	0.00
12.60	11.35	15.63	2.94	81.65	2.00	5.74	0.00	0.00
12.67	11.48	15.78	3.01	82.89	2.00	6.06	0.00	0.00
12.75	11.63	15.96	3.07	83.95	2.00	6.42	0.00	0.00
12.80	11.76	16.12	3.13	85.04	2.00	6.75	0.00	0.00
12.90	11.84	16.20	3.20	86.09	2.00	6.92	0.00	0.00
12.95	11.93	16.30	3.26	87.05	2.00	7.13	0.00	0.00
13.02	12.03	16.41	3.31	87.86	2.00	7.34	0.00	0.00
13.06	12.13	16.53	3.33	88.44	2.00	7.58	0.00	0.00
13.14	12.22	16.60	3.35	88.87	2.00	7.74	0.00	0.00
13.19	12.29	16.67	3.37	89.23	2.00	7.87	0.00	0.00
13.29	12.33	16.67	3.40	89.55	2.00	7.87	0.00	0.00
13.33	12.32	16.64	3.44	89.97	2.00	7.81	0.00	0.00
13.39	12.30	16.58	3.46	90.15	2.00	7.70	0.00	0.00
13.48	12.31	16.54	3.47	90.15	2.00	7.62	0.00	0.00
13.54	12.39	16.62	3.48	90.48	2.00	7.77	0.00	0.00
13.59	12.53	16.78	3.48	90.88	2.00	8.08	0.00	0.00
13.67	12.75	17.02	3.48	91.29	2.00	8.56	0.00	0.00
13.72	12.96	17.27	3.48	91.86	2.00	9.04	0.00	0.00
13.78	13.12	17.46	3.51	92.55	2.00	9.39	0.00	0.00
13.86	13.28	17.63	3.54	93.31	2.00	9.71	0.00	0.00
13.93	13.44	17.80	3.58	94.19	2.00	10.04	0.00	0.00
14.01	13.55	17.91	3.64	95.18	2.00	10.24	0.00	0.00
14.05	13.62	17.99	3.71	96.24	2.00	10.38	0.00	0.00
14.14	13.62	17.94	3.77	96.86	2.00	10.30	0.00	0.00
14.21	13.57	17.84	3.82	97.32	2.00	10.11	0.00	0.00
14.24	13.41	17.63	3.90	97.81	2.00	9.71	0.00	0.00
14.31	13.27	17.41	3.97	98.13	2.00	9.30	0.00	0.00
14.39	13.17	17.24	4.01	98.30	2.00	8.97	0.00	0.00
14.44	13.06	17.07	4.05	98.31	2.00	8.64	0.00	0.00
14.54	12.93	16.84	4.08	98.16	2.00	8.20	0.00	0.00
14.59	12.82	16.67	4.11	98.07	2.00	7.86	0.00	0.00
14.64	12.73	16.52	4.12	97.86	2.00	7.57	0.00	0.00
14.70	12.62	16.34	4.14	97.64	2.00	7.20	0.00	0.00
14.79	12.49	16.12	4.15	97.30	2.00	6.75	0.00	0.00
14.83	12.35	15.91	4.16	96.83	2.00	6.33	0.00	0.00
14.93	12.16	15.61	4.16	96.10	2.00	5.69	0.00	0.00
14.98	11.95	15.29	4.17	95.44	2.00	5.01	0.00	0.00
15.03	11.68	14.89	4.19	94.64	2.00	4.14	0.00	0.00
15.10	11.42	14.50	4.20	93.80	2.00	3.26	0.00	0.00
15.18	11.13	14.06	4.22	92.84	2.00	2.24	0.00	0.00
15.23	10.82	13.61	4.24	91.81	2.00	1.17	0.00	0.00

:: Estimation of post-earthquake lateral Displacements :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	R_f (%)	$Q_{tn,cs}$	FS	D_r	$Gamma_{max}$ (%)	Lat. disp. (in)
15.33	10.52	13.15	4.26	90.69	2.00	0.05	0.00	0.00
15.37	10.18	12.68	4.30	89.73	2.00	0.00	0.00	0.00
15.44	9.83	12.17	4.35	88.70	2.00	0.00	0.00	0.00
15.52	9.47	11.65	4.42	87.73	2.00	0.00	0.00	0.00
15.56	9.15	11.19	4.46	86.58	2.00	0.00	0.00	0.00
15.63	8.84	10.74	4.50	85.48	2.00	0.00	0.00	0.00
15.71	8.52	10.28	4.54	84.22	2.00	0.00	0.00	0.00
15.77	8.24	9.89	4.56	82.98	2.00	0.00	0.00	0.00
15.82	7.99	9.53	4.57	81.84	2.00	0.00	0.00	0.00
15.89	7.76	9.20	4.57	80.56	2.00	0.00	0.00	0.00
15.97	7.60	8.95	4.51	79.20	2.00	0.00	0.00	0.00
16.02	7.48	8.78	4.44	78.11	2.00	0.00	0.00	0.00
16.10	7.44	8.70	4.35	77.14	2.00	0.00	0.00	0.00
16.17	7.44	8.67	4.24	76.32	2.00	0.00	0.00	0.00
16.22	7.52	8.76	4.10	75.56	2.00	0.00	0.00	0.00
16.28	7.65	8.91	3.94	74.93	2.00	0.00	0.00	0.00
16.37	7.84	9.15	3.78	74.50	2.00	0.00	0.00	0.00
16.42	8.08	9.44	3.63	74.22	2.00	0.00	0.00	0.00
16.52	8.33	9.74	3.48	73.87	2.00	0.00	0.00	0.00
16.55	8.58	10.05	3.35	73.67	2.00	0.00	0.00	0.00
16.62	8.83	10.35	3.23	73.40	2.00	0.00	0.00	0.00
16.70	9.06	10.62	3.14	73.23	2.00	0.00	0.00	0.00
16.74	9.49	11.17	3.00	73.19	2.00	0.00	0.00	0.00
16.82	10.11	11.93	2.83	73.13	2.00	0.00	0.00	0.00
16.91	10.53	12.39	2.71	72.87	2.00	0.00	0.00	0.00
16.94	10.72	12.62	2.64	72.51	2.00	0.00	0.00	0.00
17.01	10.87	12.76	2.59	72.13	2.00	0.00	0.00	0.00
17.10	11.00	12.88	2.55	71.87	2.00	0.00	0.00	0.00
17.15	11.13	13.01	2.51	71.64	2.00	0.00	0.00	0.00
17.21	11.54	13.47	2.41	71.26	2.00	0.83	0.00	0.00
17.30	11.94	13.90	2.31	70.72	2.00	1.86	0.00	0.00
17.34	11.76	13.66	2.32	70.54	2.00	1.31	0.00	0.00
17.41	11.25	13.04	2.42	70.64	2.00	0.00	0.00	0.00
17.49	10.96	12.66	2.48	70.73	2.00	0.00	0.00	0.00
17.53	10.95	12.64	2.50	70.83	2.00	0.00	0.00	0.00
17.59	10.82	12.46	2.52	70.73	2.00	0.00	0.00	0.00
17.67	10.63	12.20	2.55	70.63	2.00	0.00	0.00	0.00
17.73	10.45	11.97	2.57	70.41	2.00	0.00	0.00	0.00
17.79	10.07	11.49	2.65	70.27	2.00	0.00	0.00	0.00
17.87	9.70	11.01	2.72	70.05	2.00	0.00	0.00	0.00
17.92	9.63	10.90	2.72	69.77	2.00	0.00	0.00	0.00
17.99	9.66	10.91	2.67	69.22	2.00	0.00	0.00	0.00
18.07	9.81	11.07	2.58	68.63	2.00	0.00	0.00	0.00
18.14	9.80	11.03	2.54	68.07	2.00	0.00	0.00	0.00
18.19	9.97	11.20	2.47	67.72	2.00	0.00	0.00	0.00
18.26	10.14	11.38	2.41	67.35	2.00	0.00	0.00	0.00
18.34	10.13	11.33	2.39	67.04	2.00	0.00	0.00	0.00
18.38	9.99	11.15	2.39	66.67	2.00	0.00	0.00	0.00

:: Estimation of post-earthquake lateral Displacements :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	R_f (%)	$Q_{tn,cs}$	FS	D_r	$Gamma_{max}$ (%)	Lat. disp. (in)
18.45	9.85	10.96	2.40	66.41	2.00	0.00	0.00	0.00
18.53	9.72	10.78	2.41	66.14	2.00	0.00	0.00	0.00
18.60	9.58	10.60	2.43	66.01	2.00	0.00	0.00	0.00
18.68	9.26	10.18	2.51	65.85	2.00	0.00	0.00	0.00
18.72	8.93	9.75	2.58	65.57	2.00	0.00	0.00	0.00
18.79	8.50	9.20	2.67	65.11	2.00	0.00	0.00	0.00
18.84	8.10	8.69	2.74	64.48	2.00	0.00	0.00	0.00
18.92	7.83	8.34	2.78	63.84	2.00	0.00	0.00	0.00
18.98	7.61	8.06	2.80	63.20	2.00	0.00	0.00	0.00
19.06	7.40	7.77	2.79	62.28	2.00	0.00	0.00	0.00
19.11	7.23	7.55	2.77	61.39	2.00	0.00	0.00	0.00
19.18	7.07	7.34	2.74	60.47	2.00	0.00	0.00	0.00
19.25	6.92	7.14	2.71	59.68	2.00	0.00	0.00	0.00
19.33	6.83	7.02	2.68	59.04	2.00	0.00	0.00	0.00
19.37	6.81	6.98	2.66	58.73	2.00	0.00	0.00	0.00
19.47	6.80	6.95	2.65	58.53	2.00	0.00	0.00	0.00
19.52	6.83	6.97	2.63	58.52	2.00	0.00	0.00	0.00
19.57	6.85	6.99	2.64	58.63	2.00	0.00	0.00	0.00
19.62	6.84	6.96	2.68	58.85	2.00	0.00	0.00	0.00
19.71	6.81	6.91	2.72	59.04	2.00	0.00	0.00	0.00
19.77	6.74	6.81	2.80	59.33	2.00	0.00	0.00	0.00
19.82	6.58	6.61	2.89	59.29	2.00	0.00	0.00	0.00
19.91	6.46	6.44	2.92	58.99	2.00	0.00	0.00	0.00
19.96	6.31	6.25	2.96	58.55	2.00	0.00	0.00	0.00
20.02	6.19	6.09	2.98	58.11	2.00	0.00	0.00	0.00
20.11	6.06	5.91	2.99	57.52	2.00	0.00	0.00	0.00
20.18	5.93	5.75	3.00	56.93	2.00	0.00	0.00	0.00
20.23	5.83	5.62	2.97	56.25	2.00	0.00	0.00	0.00
20.28	5.74	5.50	2.92	55.46	2.00	0.00	0.00	0.00
20.37	5.70	5.44	2.83	54.57	2.00	0.00	0.00	0.00
20.42	5.74	5.48	2.71	53.93	2.00	0.00	0.00	0.00
20.48	5.73	5.45	2.68	53.62	2.00	0.00	0.00	0.00
20.56	5.74	5.45	2.63	53.31	2.00	0.00	0.00	0.00
20.63	5.76	5.46	2.59	53.02	2.00	0.00	0.00	0.00
20.67	5.80	5.50	2.55	52.91	2.00	0.00	0.00	0.00
20.74	5.86	5.56	2.50	52.80	2.00	0.00	0.00	0.00
20.83	5.92	5.61	2.48	52.82	2.00	0.00	0.00	0.00
20.90	5.98	5.67	2.47	52.98	2.00	0.00	0.00	0.00
20.97	6.03	5.72	2.47	53.14	2.00	0.00	0.00	0.00
21.02	6.11	5.80	2.46	53.33	2.00	0.00	0.00	0.00
21.10	6.22	5.91	2.43	53.53	2.00	0.00	0.00	0.00
21.17	6.35	6.05	2.42	53.88	2.00	0.00	0.00	0.00
21.22	6.49	6.20	2.40	54.25	2.00	0.00	0.00	0.00
21.27	6.64	6.37	2.39	54.75	2.00	0.00	0.00	0.00
21.37	6.79	6.52	2.39	55.21	2.00	0.00	0.00	0.00
21.43	6.95	6.69	2.38	55.69	2.00	0.00	0.00	0.00
21.46	7.09	6.86	2.38	56.17	2.00	0.00	0.00	0.00
21.55	7.24	7.01	2.36	56.47	2.00	0.00	0.00	0.00

:: Estimation of post-earthquake lateral Displacements :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	R_f (%)	$Q_{tn,cs}$	FS	D_r	$Gamma_{max}$ (%)	Lat. disp. (in)
21.62	7.36	7.13	2.35	56.76	2.00	0.00	0.00	0.00
21.66	7.42	7.19	2.32	56.63	2.00	0.00	0.00	0.00
21.74	7.41	7.16	2.28	56.18	2.00	0.00	0.00	0.00
21.81	7.37	7.10	2.25	55.71	2.00	0.00	0.00	0.00
21.85	7.30	7.01	2.21	55.11	2.00	0.00	0.00	0.00
21.93	7.21	6.89	2.16	54.32	2.00	0.00	0.00	0.00
22.00	7.13	6.78	2.10	53.54	2.00	0.00	0.00	0.00
22.07	7.06	6.69	2.06	52.89	2.00	0.00	0.00	0.00
22.16	6.98	6.58	2.04	52.37	2.00	0.00	0.00	0.00
22.19	6.91	6.49	2.03	52.03	2.00	0.00	0.00	0.00
22.26	6.87	6.43	2.05	52.11	2.00	0.00	0.00	0.00
22.33	6.86	6.41	2.11	52.50	2.00	0.00	0.00	0.00
22.40	6.86	6.39	2.15	52.89	2.00	0.00	0.00	0.00
22.45	6.88	6.41	2.18	53.16	2.00	0.00	0.00	0.00
22.53	6.88	6.39	2.18	53.12	2.00	0.00	0.00	0.00
22.60	6.86	6.36	2.19	53.07	2.00	0.00	0.00	0.00
22.64	6.79	6.27	2.21	53.00	2.00	0.00	0.00	0.00
22.70	6.72	6.18	2.27	53.20	2.00	0.00	0.00	0.00
22.80	6.68	6.11	2.30	53.25	2.00	0.00	0.00	0.00
22.84	6.59	6.01	2.31	53.02	2.00	0.00	0.00	0.00
22.90	6.58	5.98	2.26	52.57	2.00	0.00	0.00	0.00
23.00	6.68	6.08	2.16	52.04	2.00	0.00	0.00	0.00
23.05	6.77	6.17	2.15	52.22	2.00	0.00	0.00	0.00
23.14	6.93	6.33	2.21	53.25	2.00	0.00	0.00	0.00
23.18	7.11	6.52	2.30	54.56	2.00	0.00	0.00	0.00
23.24	7.32	6.74	2.43	56.36	2.00	0.00	0.00	0.00
23.32	7.52	6.94	2.59	58.31	2.00	0.00	0.00	0.00
23.39	7.66	7.09	2.77	60.28	2.00	0.00	0.00	0.00
23.44	7.83	7.27	2.96	62.42	2.00	0.00	0.00	0.00
23.53	7.88	7.30	3.21	64.47	2.00	0.00	0.00	0.00
23.59	7.80	7.20	3.50	66.24	2.00	0.00	0.00	0.00
23.63	7.63	7.01	3.73	67.05	2.00	0.00	0.00	0.00
23.69	7.43	6.76	3.92	67.36	2.00	0.00	0.00	0.00
23.77	7.22	6.52	4.05	67.12	2.00	0.00	0.00	0.00
23.82	7.02	6.29	4.07	66.24	2.00	0.00	0.00	0.00
23.93	6.84	6.07	4.01	64.93	2.00	0.00	0.00	0.00
23.95	6.71	5.92	3.89	63.57	2.00	0.00	0.00	0.00
24.03	6.63	5.82	3.70	62.00	2.00	0.00	0.00	0.00
24.12	6.60	5.77	3.48	60.46	2.00	0.00	0.00	0.00
24.16	6.59	5.76	3.29	59.15	2.00	0.00	0.00	0.00
24.22	6.66	5.82	3.12	58.33	2.00	0.00	0.00	0.00
24.30	6.73	5.88	2.99	57.69	2.00	0.00	0.00	0.00
24.37	6.79	5.93	2.93	57.49	2.00	0.00	0.00	0.00
24.43	6.88	6.02	2.89	57.55	2.00	0.00	0.00	0.00
24.50	7.00	6.14	2.86	57.74	2.00	0.00	0.00	0.00
24.57	7.09	6.22	2.85	58.01	2.00	0.00	0.00	0.00
24.62	7.17	6.30	2.88	58.51	2.00	0.00	0.00	0.00
24.69	7.23	6.35	2.92	58.98	2.00	0.00	0.00	0.00

:: Estimation of post-earthquake lateral Displacements :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	R_f (%)	$Q_{tn,cs}$	FS	D_r	$Gamma_{max}$ (%)	Lat. disp. (in)
24.77	7.28	6.39	2.96	59.42	2.00	0.00	0.00	0.00
24.83	7.32	6.42	2.99	59.75	2.00	0.00	0.00	0.00
24.88	7.37	6.46	3.00	59.98	2.00	0.00	0.00	0.00
24.97	7.40	6.47	3.00	60.06	2.00	0.00	0.00	0.00
25.02	7.42	6.49	2.99	60.05	2.00	0.00	0.00	0.00
25.11	7.41	6.46	2.98	59.87	2.00	0.00	0.00	0.00
25.17	7.41	6.45	2.98	59.83	2.00	0.00	0.00	0.00
25.21	7.40	6.43	2.97	59.69	2.00	0.00	0.00	0.00
25.29	7.44	6.45	2.97	59.78	2.00	0.00	0.00	0.00
25.36	7.55	6.56	2.96	60.05	2.00	0.00	0.00	0.00
25.40	7.70	6.71	2.94	60.47	2.00	0.00	0.00	0.00
25.46	7.86	6.86	2.95	61.10	2.00	0.00	0.00	0.00
25.54	8.04	7.03	2.96	61.72	2.00	0.00	0.00	0.00
25.62	8.20	7.18	2.98	62.42	2.00	0.00	0.00	0.00
25.66	8.36	7.34	3.03	63.34	2.00	0.00	0.00	0.00
25.75	8.51	7.48	3.08	64.20	2.00	0.00	0.00	0.00
25.80	8.67	7.63	3.13	65.08	2.00	0.00	0.00	0.00
25.85	8.81	7.77	3.15	65.74	2.00	0.00	0.00	0.00
25.96	8.75	7.68	3.25	66.22	2.00	0.00	0.00	0.00
26.01	8.74	7.66	3.34	66.87	2.00	0.00	0.00	0.00
26.05	8.80	7.71	3.41	67.56	2.00	0.00	0.00	0.00
26.12	8.87	7.77	3.46	68.13	2.00	0.00	0.00	0.00
26.19	8.95	7.84	3.49	68.60	2.00	0.00	0.00	0.00
26.25	9.02	7.89	3.49	68.79	2.00	0.00	0.00	0.00
26.33	8.98	7.83	3.50	68.70	2.00	0.00	0.00	0.00
26.42	8.87	7.70	3.53	68.46	2.00	0.00	0.00	0.00
26.46	8.73	7.55	3.56	68.15	2.00	0.00	0.00	0.00
26.52	8.73	7.53	3.53	67.82	2.00	0.00	0.00	0.00
26.61	8.65	7.43	3.49	67.22	2.00	0.00	0.00	0.00
26.67	8.48	7.24	3.46	66.29	2.00	0.00	0.00	0.00
26.71	8.31	7.06	3.41	65.26	2.00	0.00	0.00	0.00
26.79	8.11	6.84	3.39	64.26	2.00	0.00	0.00	0.00
26.87	7.92	6.62	3.37	63.35	2.00	0.00	0.00	0.00
26.92	7.81	6.50	3.33	62.62	2.00	0.00	0.00	0.00
26.98	7.77	6.45	3.26	61.94	2.00	0.00	0.00	0.00
27.06	7.73	6.40	3.19	61.25	2.00	0.00	0.00	0.00
27.11	7.69	6.35	3.12	60.57	2.00	0.00	0.00	0.00
27.21	7.63	6.27	3.07	59.94	2.00	0.00	0.00	0.00
27.26	7.55	6.18	3.03	59.31	2.00	0.00	0.00	0.00
27.32	7.39	6.01	3.04	58.70	2.00	0.00	0.00	0.00
27.40	7.24	5.84	3.04	58.07	2.00	0.00	0.00	0.00
27.45	7.09	5.67	3.01	57.22	2.00	0.00	0.00	0.00
27.52	6.97	5.54	2.92	56.08	2.00	0.00	0.00	0.00
27.60	6.81	5.37	2.86	54.98	2.00	0.00	0.00	0.00
27.65	6.69	5.24	2.79	54.03	2.00	0.00	0.00	0.00
27.71	6.59	5.13	2.73	53.20	2.00	0.00	0.00	0.00
27.80	6.56	5.09	2.64	52.43	2.00	0.00	0.00	0.00
27.84	6.56	5.08	2.56	51.83	2.00	0.00	0.00	0.00

:: Estimation of post-earthquake lateral Displacements :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	R_f (%)	$Q_{tn,cs}$	FS	D_r	$Gamma_{max}$ (%)	Lat. disp. (in)
27.90	6.65	5.16	2.47	51.56	2.00	0.00	0.00	0.00
27.99	6.75	5.25	2.42	51.51	2.00	0.00	0.00	0.00
28.05	6.85	5.34	2.43	51.95	2.00	0.00	0.00	0.00
28.10	6.96	5.44	2.51	52.86	2.00	0.00	0.00	0.00
28.17	7.10	5.57	2.57	53.77	2.00	0.00	0.00	0.00
28.25	7.25	5.70	2.62	54.67	2.00	0.00	0.00	0.00
28.30	7.40	5.84	2.66	55.46	2.00	0.00	0.00	0.00
28.39	7.51	5.94	2.74	56.38	2.00	0.00	0.00	0.00
28.44	7.61	6.03	2.80	57.20	2.00	0.00	0.00	0.00
28.49	7.69	6.10	2.87	57.99	2.00	0.00	0.00	0.00
28.54	7.77	6.17	2.89	58.34	2.00	0.00	0.00	0.00
28.62	7.86	6.25	2.81	58.06	2.00	0.00	0.00	0.00
28.68	7.91	6.28	2.81	58.18	2.00	0.00	0.00	0.00
28.74	7.96	6.32	2.88	58.81	2.00	0.00	0.00	0.00
28.83	7.97	6.32	2.94	59.27	2.00	0.00	0.00	0.00
28.89	7.96	6.29	3.00	59.63	2.00	0.00	0.00	0.00
28.98	7.81	6.13	3.09	59.63	2.00	0.00	0.00	0.00
29.03	7.81	6.12	3.12	59.79	2.00	0.00	0.00	0.00
29.09	7.81	6.11	3.10	59.65	2.00	0.00	0.00	0.00
29.14	7.83	6.12	3.11	59.74	2.00	0.00	0.00	0.00
29.22	7.88	6.15	3.16	60.23	2.00	0.00	0.00	0.00
29.27	7.97	6.23	3.12	60.29	2.00	0.00	0.00	0.00
29.38	8.07	6.31	3.02	59.82	2.00	0.00	0.00	0.00
29.43	8.18	6.41	2.92	59.49	2.00	0.00	0.00	0.00
29.48	8.30	6.52	2.84	59.25	2.00	0.00	0.00	0.00
29.57	8.53	6.72	2.72	59.06	2.00	0.00	0.00	0.00
29.62	8.60	6.78	2.67	58.87	2.00	0.00	0.00	0.00
29.68	8.66	6.83	2.67	58.98	2.00	0.00	0.00	0.00
29.73	8.71	6.87	2.65	58.98	2.00	0.00	0.00	0.00
29.82	8.73	6.87	2.65	58.94	2.00	0.00	0.00	0.00
29.87	8.72	6.85	2.64	58.80	2.00	0.00	0.00	0.00
29.94	8.69	6.81	2.63	58.64	2.00	0.00	0.00	0.00
30.02	8.62	6.73	2.63	58.34	2.00	0.00	0.00	0.00
30.07	8.52	6.62	2.63	58.04	2.00	0.00	0.00	0.00
30.16	8.44	6.53	2.63	57.73	2.00	0.00	0.00	0.00
30.19	8.37	6.46	2.61	57.35	2.00	0.00	0.00	0.00
30.26	8.30	6.38	2.57	56.73	2.00	0.00	0.00	0.00
30.36	8.25	6.31	2.53	56.22	2.00	0.00	0.00	0.00
30.41	8.22	6.28	2.49	55.74	2.00	0.00	0.00	0.00
30.46	8.20	6.25	2.45	55.37	2.00	0.00	0.00	0.00
30.53	8.20	6.24	2.42	55.12	2.00	0.00	0.00	0.00
30.61	8.24	6.26	2.40	55.00	2.00	0.00	0.00	0.00
30.65	8.33	6.33	2.38	55.03	2.00	0.00	0.00	0.00
30.71	8.46	6.44	2.37	55.30	2.00	0.00	0.00	0.00
30.81	8.62	6.58	2.37	55.79	2.00	0.00	0.00	0.00
30.84	8.81	6.76	2.41	56.64	2.00	0.00	0.00	0.00
30.91	9.02	6.94	2.46	57.68	2.00	0.00	0.00	0.00
30.99	9.25	7.14	2.55	59.00	2.00	0.00	0.00	0.00

:: Estimation of post-earthquake lateral Displacements :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	R_f (%)	$Q_{tn,cs}$	FS	D_r	$Gamma_{max}$ (%)	Lat. disp. (in)
31.04	9.49	7.36	2.62	60.31	2.00	0.00	0.00	0.00
31.11	9.75	7.59	2.69	61.58	2.00	0.00	0.00	0.00
31.19	10.01	7.81	2.76	62.91	2.00	0.00	0.00	0.00
31.25	10.25	8.02	2.83	64.11	2.00	0.00	0.00	0.00
31.30	10.42	8.17	2.88	64.99	2.00	0.00	0.00	0.00
31.39	10.55	8.27	2.93	65.72	2.00	0.00	0.00	0.00
31.45	10.62	8.32	2.97	66.25	2.00	0.00	0.00	0.00
31.50	10.63	8.33	3.01	66.59	2.00	0.00	0.00	0.00
31.60	10.61	8.29	3.03	66.61	2.00	0.00	0.00	0.00
31.65	10.59	8.25	3.01	66.39	2.00	0.00	0.00	0.00
31.73	10.54	8.19	3.03	66.32	2.00	0.00	0.00	0.00
31.80	10.48	8.12	3.08	66.52	2.00	0.00	0.00	0.00
31.84	10.42	8.05	3.13	66.74	2.00	0.00	0.00	0.00
31.91	10.38	8.00	3.19	67.11	2.00	0.00	0.00	0.00
31.99	10.35	7.95	3.25	67.48	2.00	0.00	0.00	0.00
32.03	10.34	7.94	3.31	67.88	2.00	0.00	0.00	0.00
32.09	10.36	7.95	3.36	68.27	2.00	0.00	0.00	0.00
32.19	10.40	7.96	3.40	68.65	2.00	0.00	0.00	0.00
32.25	10.44	7.99	3.48	69.37	2.00	0.00	0.00	0.00
32.29	10.47	8.00	3.54	69.94	2.00	0.00	0.00	0.00
32.38	10.52	8.03	3.56	70.14	2.00	0.00	0.00	0.00
32.43	10.61	8.10	3.56	70.40	2.00	0.00	0.00	0.00
32.48	10.72	8.19	3.54	70.58	2.00	0.00	0.00	0.00
32.58	10.84	8.28	3.54	70.82	2.00	0.00	0.00	0.00
32.63	10.96	8.37	3.54	71.16	2.00	0.00	0.00	0.00
32.69	11.07	8.46	3.55	71.57	2.00	0.00	0.00	0.00
32.74	11.17	8.54	3.58	72.05	2.00	0.00	0.00	0.00
32.83	11.29	8.62	3.59	72.44	2.00	0.00	0.00	0.00
32.88	11.41	8.72	3.59	72.77	2.00	0.00	0.00	0.00
32.97	11.51	8.79	3.62	73.21	2.00	0.00	0.00	0.00
33.01	11.58	8.84	3.67	73.76	2.00	0.00	0.00	0.00
33.07	11.62	8.86	3.71	74.19	2.00	0.00	0.00	0.00
33.16	11.64	8.86	3.75	74.51	2.00	0.00	0.00	0.00
33.20	11.66	8.87	3.77	74.64	2.00	0.00	0.00	0.00
33.27	11.67	8.86	3.75	74.52	2.00	0.00	0.00	0.00
33.36	11.67	8.84	3.72	74.22	2.00	0.00	0.00	0.00
33.42	11.63	8.79	3.69	73.78	2.00	0.00	0.00	0.00
33.51	11.57	8.71	3.62	73.00	2.00	0.00	0.00	0.00
33.56	11.50	8.64	3.51	71.84	2.00	0.00	0.00	0.00
33.61	11.40	8.54	3.37	70.41	2.00	0.00	0.00	0.00
33.67	11.26	8.40	3.25	68.94	2.00	0.00	0.00	0.00
33.76	11.07	8.22	3.12	67.30	2.00	0.00	0.00	0.00
33.81	10.94	8.09	2.99	65.77	2.00	0.00	0.00	0.00
33.86	10.77	7.93	2.88	64.36	2.00	0.00	0.00	0.00
33.94	10.66	7.82	2.75	62.93	2.00	0.00	0.00	0.00
34.02	10.58	7.73	2.64	61.65	2.00	0.00	0.00	0.00
34.06	10.53	7.68	2.55	60.77	2.00	0.00	0.00	0.00
34.14	10.48	7.62	2.50	60.14	2.00	0.00	0.00	0.00

:: Estimation of post-earthquake lateral Displacements :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	R_f (%)	$Q_{tn,cs}$	FS	D_r	$Gamma_{max}$ (%)	Lat. disp. (in)
34.21	10.41	7.55	2.48	59.69	2.00	0.00	0.00	0.00
34.25	10.35	7.49	2.45	59.26	2.00	0.00	0.00	0.00
34.33	10.33	7.45	2.42	58.92	2.00	0.00	0.00	0.00
34.41	10.24	7.36	2.41	58.55	2.00	0.00	0.00	0.00
34.49	10.20	7.31	2.37	58.11	2.00	0.00	0.00	0.00
34.56	10.10	7.21	2.35	57.64	2.00	0.00	0.00	0.00
34.59	9.99	7.11	2.34	57.18	2.00	0.00	0.00	0.00
34.67	9.89	7.01	2.31	56.70	2.00	0.00	0.00	0.00
34.76	9.80	6.91	2.29	56.22	2.00	0.00	0.00	0.00
34.80	9.74	6.85	2.26	55.76	2.00	0.00	0.00	0.00
34.85	9.72	6.83	2.24	55.53	2.00	0.00	0.00	0.00
34.93	9.72	6.81	2.22	55.28	2.00	0.00	0.00	0.00
34.98	9.71	6.79	2.21	55.15	2.00	0.00	0.00	0.00
35.05	9.67	6.75	2.21	55.00	2.00	0.00	0.00	0.00
35.13	9.66	6.72	2.20	54.86	2.00	0.00	0.00	0.00
35.18	9.64	6.70	2.19	54.72	2.00	0.00	0.00	0.00
35.24	9.59	6.65	2.19	54.57	2.00	0.00	0.00	0.00
35.32	9.52	6.57	2.19	54.40	2.00	0.00	0.00	0.00
35.41	9.44	6.49	2.19	54.11	2.00	0.00	0.00	0.00
35.46	9.35	6.41	2.17	53.73	2.00	0.00	0.00	0.00
35.51	9.26	6.32	2.15	53.25	2.00	0.00	0.00	0.00
35.58	9.19	6.25	2.12	52.75	2.00	0.00	0.00	0.00
35.66	9.14	6.19	2.08	52.26	2.00	0.00	0.00	0.00
35.71	9.06	6.12	2.06	51.88	2.00	0.00	0.00	0.00
35.76	8.99	6.05	2.04	51.49	2.00	0.00	0.00	0.00
35.86	8.94	5.99	2.01	51.09	2.00	0.00	0.00	0.00
35.91	8.90	5.95	1.98	50.72	2.00	0.00	0.00	0.00
36.01	8.88	5.92	1.96	50.45	2.00	0.00	0.00	0.00
36.05	8.87	5.91	1.93	50.09	2.00	0.00	0.00	0.00
36.12	8.86	5.89	1.91	49.84	2.00	0.00	0.00	0.00
36.20	8.83	5.85	1.89	49.56	2.00	0.00	0.00	0.00
36.23	8.84	5.85	1.87	49.44	2.00	0.00	0.00	0.00
36.31	8.89	5.89	1.85	49.32	2.00	0.00	0.00	0.00
36.35	8.99	5.96	1.80	49.13	2.00	0.00	0.00	0.00
36.45	9.11	6.05	1.76	48.92	2.00	0.00	0.00	0.00
36.51	9.26	6.17	1.70	48.73	2.00	0.00	0.00	0.00
36.58	9.41	6.28	1.67	48.64	2.00	0.00	0.00	0.00
36.66	9.56	6.40	1.64	48.67	2.00	0.00	0.00	0.00
36.70	9.71	6.52	1.63	48.82	2.00	0.00	0.00	0.00
36.80	9.91	6.68	1.61	49.08	2.00	0.00	0.00	0.00
36.85	10.09	6.82	1.62	49.47	2.00	0.00	0.00	0.00
36.89	10.23	6.93	1.63	49.84	2.00	0.00	0.00	0.00
36.96	10.31	6.98	1.67	50.42	2.00	0.00	0.00	0.00
37.03	10.36	7.01	1.72	50.98	2.00	0.00	0.00	0.00
37.09	10.38	7.02	1.78	51.64	2.00	0.00	0.00	0.00
37.15	10.40	7.03	1.83	52.17	2.00	0.00	0.00	0.00
37.23	10.42	7.03	1.88	52.69	2.00	0.00	0.00	0.00
37.27	10.44	7.04	1.92	53.11	2.00	0.00	0.00	0.00

:: Estimation of post-earthquake lateral Displacements :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	R_f (%)	$Q_{tn,cs}$	FS	D_r	$Gamma_{max}$ (%)	Lat. disp. (in)
37.34	10.45	7.04	1.95	53.40	2.00	0.00	0.00	0.00
37.43	10.46	7.03	1.96	53.58	2.00	0.00	0.00	0.00
37.49	10.46	7.02	1.99	53.77	2.00	0.00	0.00	0.00
37.54	10.47	7.02	1.98	53.75	2.00	0.00	0.00	0.00
37.62	10.46	7.00	1.99	53.71	2.00	0.00	0.00	0.00
37.69	10.45	6.98	1.97	53.47	2.00	0.00	0.00	0.00
37.74	10.44	6.96	1.96	53.35	2.00	0.00	0.00	0.00
37.82	10.43	6.94	1.95	53.21	2.00	0.00	0.00	0.00
37.89	10.42	6.92	1.94	53.07	2.00	0.00	0.00	0.00
37.93	10.45	6.94	1.93	53.07	2.00	0.00	0.00	0.00
38.02	10.51	6.98	1.93	53.15	2.00	0.00	0.00	0.00
38.08	10.61	7.05	1.94	53.37	2.00	0.00	0.00	0.00
38.13	10.59	7.02	1.98	53.76	2.00	0.00	0.00	0.00
38.23	10.77	7.15	2.00	54.28	2.00	0.00	0.00	0.00
38.28	11.05	7.37	2.01	54.94	2.00	0.00	0.00	0.00
38.35	11.35	7.61	2.01	55.48	2.00	0.00	0.00	0.00
38.42	11.66	7.85	2.00	56.01	2.00	0.00	0.00	0.00
38.47	11.96	8.08	2.00	56.53	2.00	0.00	0.00	0.00
38.52	12.14	8.22	2.01	57.02	2.00	0.00	0.00	0.00
38.61	12.27	8.31	2.03	57.39	2.00	0.00	0.00	0.00
38.67	12.35	8.36	2.03	57.47	2.00	0.00	0.00	0.00
38.72	12.50	8.48	2.00	57.46	2.00	0.00	0.00	0.00
38.82	12.47	8.43	1.99	57.22	2.00	0.00	0.00	0.00
38.86	12.32	8.30	1.98	56.90	2.00	0.00	0.00	0.00
38.96	12.14	8.14	1.98	56.45	2.00	0.00	0.00	0.00
39.01	11.97	7.99	1.97	56.01	2.00	0.00	0.00	0.00
39.05	11.89	7.92	1.94	55.59	2.00	0.00	0.00	0.00
39.13	12.00	7.99	1.89	55.17	2.00	0.00	0.00	0.00
39.21	12.16	8.11	1.83	54.75	2.00	0.00	0.00	0.00
39.24	12.47	8.35	1.77	54.65	2.00	0.00	0.00	0.00
39.31	12.92	8.70	1.71	54.63	2.00	0.00	0.00	0.00
39.40	13.42	9.09	1.67	54.92	2.00	0.00	0.00	0.00
39.44	13.97	9.54	1.65	55.41	2.00	0.00	0.00	0.00
39.51	14.55	10.01	1.63	56.06	2.00	0.00	0.00	0.00
39.60	15.09	10.43	1.63	56.69	2.00	0.00	0.00	0.00
39.66	15.51	10.77	1.63	57.21	2.00	0.00	0.00	0.00
39.70	15.75	10.96	1.62	57.47	2.00	0.00	0.00	0.00
39.80	15.89	11.05	1.62	57.61	2.00	0.00	0.00	0.00
39.85	15.87	11.02	1.63	57.69	2.00	0.00	0.00	0.00
39.90	15.72	10.88	1.64	57.60	2.00	0.00	0.00	0.00
39.98	15.53	10.71	1.63	57.20	2.00	0.00	0.00	0.00
40.05	15.26	10.47	1.61	56.51	2.00	0.00	0.00	0.00
40.10	14.94	10.20	1.58	55.63	2.00	0.00	0.00	0.00
40.20	14.62	9.92	1.54	54.60	2.00	0.00	0.00	0.00
40.25	14.33	9.68	1.49	53.57	2.00	0.00	0.00	0.00
40.30	14.10	9.49	1.45	52.72	2.00	0.00	0.00	0.00
40.40	13.93	9.33	1.41	51.94	2.00	0.00	0.00	0.00
40.45	13.82	9.23	1.38	51.28	2.00	0.00	0.00	0.00

:: Estimation of post-earthquake lateral Displacements :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	R_f (%)	$Q_{tn,cs}$	FS	D_r	$Gamma_{max}$ (%)	Lat. disp. (in)
40.50	13.79	9.20	1.35	50.82	2.00	0.00	0.00	0.00
40.59	13.78	9.17	1.33	50.57	2.00	0.00	0.00	0.00
40.64	13.82	9.20	1.33	50.56	2.00	0.00	0.00	0.00
40.69	13.94	9.29	1.32	50.65	2.00	0.00	0.00	0.00
40.79	14.09	9.39	1.34	51.06	2.00	0.00	0.00	0.00
40.83	14.28	9.53	1.39	52.01	2.00	0.00	0.00	0.00
40.92	14.55	9.73	1.44	53.03	2.00	0.00	0.00	0.00
40.98	14.84	9.94	1.50	54.14	2.00	0.00	0.00	0.00
41.03	15.10	10.13	1.55	55.21	2.00	0.00	0.00	0.00
41.08	15.30	10.28	1.61	56.17	2.00	0.00	0.00	0.00
41.18	15.48	10.40	1.64	56.90	2.00	0.00	0.00	0.00
41.22	15.62	10.50	1.69	57.63	2.00	0.00	0.00	0.00
41.31	15.72	10.55	1.73	58.34	2.00	0.00	0.00	0.00
41.36	15.79	10.59	1.77	58.87	2.00	0.00	0.00	0.00
41.42	15.83	10.61	1.78	59.03	2.00	0.00	0.00	0.00
41.50	15.79	10.56	1.79	59.10	2.00	0.00	0.00	0.00
41.54	15.73	10.50	1.80	59.18	2.00	0.00	0.00	0.00
41.61	15.68	10.45	1.80	59.06	2.00	0.00	0.00	0.00
41.70	15.63	10.39	1.81	59.03	2.00	0.00	0.00	0.00
41.75	15.58	10.33	1.82	59.10	2.00	0.00	0.00	0.00
41.80	15.56	10.31	1.83	59.18	2.00	0.00	0.00	0.00
41.87	15.55	10.28	1.84	59.24	2.00	0.00	0.00	0.00
41.95	15.57	10.28	1.84	59.30	2.00	0.00	0.00	0.00
42.01	15.60	10.29	1.85	59.45	2.00	0.00	0.00	0.00
42.10	15.68	10.33	1.87	59.77	2.00	0.00	0.00	0.00
42.14	15.78	10.39	1.89	60.19	2.00	0.00	0.00	0.00
42.21	15.87	10.44	1.94	60.86	2.00	0.00	0.00	0.00
42.27	15.96	10.50	1.97	61.35	2.00	0.00	0.00	0.00
42.34	16.05	10.55	1.99	61.74	2.00	0.00	0.00	0.00
42.39	16.11	10.58	2.02	62.14	2.00	0.00	0.00	0.00
42.49	16.16	10.59	2.05	62.52	2.00	0.00	0.00	0.00
42.54	16.18	10.59	2.10	63.15	2.00	0.00	0.00	0.00
42.59	16.19	10.58	2.16	63.79	2.00	0.00	0.00	0.00
42.69	16.17	10.54	2.20	64.22	2.00	0.00	0.00	0.00
42.74	16.12	10.49	2.21	64.28	2.00	0.00	0.00	0.00
42.80	16.08	10.44	2.21	64.17	2.00	0.00	0.00	0.00
42.89	16.02	10.38	2.21	64.05	2.00	0.00	0.00	0.00
42.93	15.90	10.27	2.22	63.95	2.00	0.00	0.00	0.00
42.99	15.79	10.18	2.22	63.77	2.00	0.00	0.00	0.00
43.08	15.64	10.04	2.22	63.41	2.00	0.00	0.00	0.00
43.11	15.45	9.89	2.19	62.83	2.00	0.00	0.00	0.00
43.18	15.16	9.66	2.16	61.98	2.00	0.00	0.00	0.00
43.28	14.77	9.35	2.13	60.93	2.00	0.00	0.00	0.00
43.35	14.40	9.05	2.11	60.05	2.00	0.00	0.00	0.00
43.38	13.95	8.71	2.09	59.07	2.00	0.00	0.00	0.00
43.45	13.50	8.36	2.05	57.87	2.00	0.00	0.00	0.00
43.53	13.09	8.04	2.00	56.63	2.00	0.00	0.00	0.00
43.58	12.64	7.70	1.96	55.36	2.00	0.00	0.00	0.00

:: Estimation of post-earthquake lateral Displacements :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	R_f (%)	$Q_{tn,cs}$	FS	D_r	$Gamma_{max}$ (%)	Lat. disp. (in)
43.64	12.18	7.34	1.93	54.23	2.00	0.00	0.00	0.00
43.73	11.74	7.00	1.90	53.06	2.00	0.00	0.00	0.00
43.78	11.44	6.77	1.86	52.10	2.00	0.00	0.00	0.00
43.84	11.29	6.65	1.84	51.55	2.00	0.00	0.00	0.00
43.92	11.24	6.61	1.82	51.21	2.00	0.00	0.00	0.00
43.98	11.42	6.73	1.77	51.04	2.00	0.00	0.00	0.00
44.07	11.69	6.92	1.77	51.48	2.00	0.00	0.00	0.00
44.12	12.61	7.59	1.75	52.80	2.00	0.00	0.00	0.00
44.17	13.58	8.30	1.73	54.21	2.00	0.00	0.00	0.00
44.23	15.30	9.59	1.66	55.83	2.00	0.00	0.00	0.00
44.29	16.73	10.69	1.65	57.49	2.00	0.00	0.00	0.00
44.39	17.65	11.39	1.60	57.91	2.00	0.00	0.00	0.00
44.43	18.07	11.71	1.57	58.02	2.00	0.00	0.00	0.00
44.49	18.39	11.95	1.54	57.87	2.00	0.00	0.00	0.00
44.57	18.26	11.83	1.53	57.59	2.00	0.00	0.00	0.00
44.67	17.84	11.49	1.51	56.71	2.00	0.00	0.00	0.00
44.73	16.78	10.65	1.48	55.13	2.00	0.00	0.00	0.00
44.78	15.68	9.81	1.45	53.28	2.00	0.00	0.00	0.00
44.82	13.89	8.43	1.44	50.86	2.00	0.00	0.00	0.00
44.93	12.37	7.28	1.37	47.87	2.00	0.00	0.00	0.00
44.97	11.32	6.51	1.36	46.15	2.00	0.00	0.00	0.00
45.02	10.69	6.04	1.33	44.73	2.00	0.00	0.00	0.00
45.09	10.06	5.58	1.31	43.44	2.00	0.00	0.00	0.00
45.17	9.74	5.34	1.28	42.46	2.00	0.00	0.00	0.00
45.22	9.67	5.28	1.25	42.05	2.00	0.00	0.00	0.00
45.30	9.64	5.25	1.22	41.64	2.00	0.00	0.00	0.00
45.37	9.63	5.24	1.20	41.37	2.00	0.00	0.00	0.00
45.42	9.61	5.22	1.19	41.23	2.00	0.00	0.00	0.00
45.50	9.60	5.20	1.18	41.08	2.00	0.00	0.00	0.00
45.57	9.58	5.18	1.18	41.05	2.00	0.00	0.00	0.00
45.61	9.57	5.17	1.17	40.91	2.00	0.00	0.00	0.00
45.72	9.57	5.15	1.16	40.75	2.00	0.00	0.00	0.00
45.77	9.54	5.12	1.17	40.73	2.00	0.00	0.00	0.00
45.80	9.61	5.17	1.18	41.00	2.00	0.00	0.00	0.00
45.88	9.73	5.25	1.21	41.54	2.00	0.00	0.00	0.00
45.96	9.95	5.40	1.24	42.23	2.00	0.00	0.00	0.00
46.01	10.26	5.62	1.26	42.93	2.00	0.00	0.00	0.00
46.11	10.60	5.85	1.27	43.61	2.00	0.00	0.00	0.00
46.14	10.90	6.06	1.27	44.16	2.00	0.00	0.00	0.00
46.21	11.13	6.22	1.29	44.66	2.00	0.00	0.00	0.00
46.26	11.36	6.38	1.31	45.27	2.00	0.00	0.00	0.00
46.35	11.59	6.53	1.33	45.86	2.00	0.00	0.00	0.00
46.41	11.79	6.67	1.32	45.99	2.00	0.00	0.00	0.00
46.49	11.97	6.79	1.29	45.89	2.00	0.00	0.00	0.00
46.55	12.02	6.82	1.27	45.65	2.00	0.00	0.00	0.00
46.59	12.02	6.81	1.27	45.64	2.00	0.00	0.00	0.00
46.68	12.03	6.81	1.31	46.18	2.00	0.00	0.00	0.00
46.74	12.21	6.93	1.36	46.96	2.00	0.00	0.00	0.00

:: Estimation of post-earthquake lateral Displacements :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	R_f (%)	$Q_{tn,cs}$	FS	D_r	$Gamma_{max}$ (%)	Lat. disp. (in)
46.80	12.54	7.15	1.36	47.42	2.00	0.00	0.00	0.00
46.85	12.84	7.36	1.38	48.18	2.00	0.00	0.00	0.00
46.93	13.10	7.53	1.44	49.23	2.00	0.00	0.00	0.00
47.00	13.25	7.62	1.55	50.73	2.00	0.00	0.00	0.00
47.10	13.37	7.69	1.67	52.26	2.00	0.00	0.00	0.00
47.15	13.58	7.83	1.74	53.39	2.00	0.00	0.00	0.00
47.20	13.74	7.94	1.77	53.94	2.00	0.00	0.00	0.00
47.25	13.87	8.02	1.73	53.66	2.00	0.00	0.00	0.00
47.31	13.67	7.87	1.69	52.88	2.00	0.00	0.00	0.00
47.40	13.24	7.56	1.69	52.16	2.00	0.00	0.00	0.00
47.44	12.78	7.23	1.64	50.94	2.00	0.00	0.00	0.00
47.52	12.43	6.97	1.54	49.18	2.00	0.00	0.00	0.00
47.58	12.04	6.69	1.40	47.03	2.00	0.00	0.00	0.00
47.67	11.69	6.43	1.25	44.74	2.00	0.00	0.00	0.00
47.73	11.28	6.14	1.14	42.78	2.00	0.00	0.00	0.00
47.78	11.00	5.93	1.05	41.22	2.00	0.00	0.00	0.00
47.86	10.70	5.71	1.01	40.24	2.00	0.00	0.00	0.00
47.92	10.61	5.64	1.00	39.94	2.00	0.00	0.00	0.00
47.98	10.65	5.66	1.02	40.33	2.00	0.00	0.00	0.00
48.05	10.75	5.72	1.08	41.11	2.00	0.00	0.00	0.00
48.12	10.88	5.81	1.14	42.11	2.00	0.00	0.00	0.00
48.19	11.29	6.09	1.23	43.74	2.00	0.00	0.00	0.00
48.27	11.81	6.44	1.29	45.19	2.00	0.00	0.00	0.00
48.32	12.54	6.94	1.31	46.49	2.00	0.00	0.00	0.00
48.39	13.52	7.61	1.27	47.30	2.00	0.00	0.00	0.00
48.47	14.52	8.34	1.23	48.00	2.00	0.00	0.00	0.00
48.52	15.76	9.26	1.16	48.43	2.00	0.00	0.00	0.00
48.57	17.08	10.24	1.08	48.45	2.00	0.00	0.00	0.00
48.67	18.11	11.01	1.01	48.22	2.00	0.00	0.00	0.00
48.71	18.94	11.63	0.97	48.22	2.00	0.00	0.00	0.00
48.76	19.21	11.82	0.98	48.49	2.00	0.00	0.00	0.00
48.82	19.64	12.12	1.00	49.25	2.00	0.00	0.00	0.00
48.93	19.63	12.06	1.09	50.82	2.00	0.00	0.00	0.00
48.97	19.53	11.93	1.26	53.58	2.00	0.00	0.00	0.00
49.05	19.43	11.79	1.46	56.59	2.00	0.00	0.00	0.00
49.08	19.57	11.84	1.69	60.05	2.00	0.00	0.00	0.00
49.16	19.78	11.92	1.96	63.92	2.00	0.00	0.00	0.00
49.25	20.34	12.26	2.24	68.19	2.00	0.00	0.00	0.00
49.29	21.10	12.75	2.54	72.88	2.00	0.00	0.00	0.00
49.36	22.50	13.70	2.82	78.16	2.00	1.38	0.00	0.00
49.43	24.24	14.90	3.02	83.10	2.00	4.17	0.00	0.00
49.48	26.47	16.49	3.10	87.16	2.00	7.50	0.00	0.00
49.55	28.64	18.03	3.11	90.13	2.00	10.46	0.00	0.00
49.64	30.67	19.47	3.10	92.56	2.00	12.99	0.00	0.00
49.70	32.09	20.47	3.14	94.76	2.00	14.65	0.00	0.00
49.75	33.34	21.35	3.17	96.70	2.00	16.04	0.00	0.00
49.81	34.56	22.21	3.16	98.00	2.00	17.34	0.00	0.00
49.90	35.75	23.04	3.17	99.36	2.00	18.55	0.00	0.00

:: Estimation of post-earthquake lateral Displacements :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	R_f (%)	$Q_{tn,cs}$	FS	D_r	$Gamma_{max}$ (%)	Lat. disp. (in)
49.94	36.62	23.66	3.15	100.04	2.00	19.42	0.00	0.00
50.01	36.53	23.55	3.18	100.43	2.00	19.27	0.00	0.00
50.08	36.09	23.18	3.25	100.85	2.00	18.75	0.00	0.00
50.15	35.37	22.60	3.34	101.32	2.00	17.90	0.00	0.00
50.24	35.40	22.57	3.36	101.61	2.00	17.87	0.00	0.00
50.30	35.75	22.81	3.31	101.22	2.00	18.22	0.00	0.00
50.34	35.97	22.97	3.23	100.26	2.00	18.45	0.00	0.00
50.41	36.05	23.02	3.16	99.21	2.00	18.52	0.00	0.00
50.47	35.82	22.86	3.02	96.84	2.00	18.29	0.00	0.00
50.54	35.56	22.69	2.86	93.92	2.00	18.04	0.00	0.00
50.62	35.51	22.67	2.68	90.88	2.00	18.01	0.00	0.00
50.66	35.50	22.71	2.48	87.61	2.00	18.07	0.00	0.00
50.77	35.54	22.76	2.29	84.35	2.00	18.14	0.00	0.00
50.81	34.91	22.33	2.15	81.27	2.00	17.52	0.00	0.00
50.87	34.13	21.78	2.04	78.68	2.00	16.70	0.00	0.00
50.92	33.49	21.33	1.95	76.51	2.00	16.00	0.00	0.00
51.01	33.00	20.97	1.86	74.48	2.00	15.45	0.00	0.00
51.07	32.79	20.82	1.80	73.21	2.00	15.21	0.00	0.00
51.15	32.62	20.69	1.75	72.16	2.00	15.00	0.00	0.00
51.21	32.54	20.62	1.72	71.53	2.00	14.89	0.00	0.00
51.26	32.61	20.65	1.71	71.37	2.00	14.94	0.00	0.00
51.32	32.80	20.78	1.71	71.50	2.00	15.13	0.00	0.00
51.39	33.10	20.97	1.72	71.79	2.00	15.43	0.00	0.00
51.46	33.33	21.10	1.73	72.21	2.00	15.65	0.00	0.00
51.53	33.60	21.26	1.75	72.69	2.00	15.90	0.00	0.00
51.61	33.87	21.42	1.76	73.16	2.00	16.14	0.00	0.00
51.65	34.13	21.59	1.77	73.51	2.00	16.40	0.00	0.00
51.72	34.43	21.78	1.77	73.79	2.00	16.69	0.00	0.00
51.81	34.80	22.01	1.77	73.92	2.00	17.04	0.00	0.00
51.84	35.11	22.23	1.76	74.03	2.00	17.36	0.00	0.00
51.92	35.39	22.40	1.75	74.01	2.00	17.62	0.00	0.00
52.01	35.65	22.56	1.74	73.92	2.00	17.85	0.00	0.00
52.06	35.90	22.73	1.72	73.80	2.00	18.10	0.00	0.00
52.11	36.16	22.91	1.71	73.61	2.00	18.36	0.00	0.00
52.19	36.34	23.01	1.69	73.49	2.00	18.51	0.00	0.00
52.25	36.53	23.13	1.69	73.49	2.00	18.68	0.00	0.00
52.30	36.76	23.27	1.69	73.61	2.00	18.88	0.00	0.00
52.38	37.02	23.43	1.69	73.88	2.00	19.10	0.00	0.00
52.45	37.28	23.58	1.70	74.22	2.00	19.31	0.00	0.00
52.49	37.54	23.75	1.72	74.68	2.00	19.55	0.00	0.00
52.57	37.71	23.83	1.74	75.13	2.00	19.66	0.00	0.00
52.65	37.81	23.86	1.76	75.60	2.00	19.70	0.00	0.00
52.70	37.59	23.66	1.79	76.02	2.00	19.42	0.00	0.00
52.79	37.34	23.43	1.81	76.26	2.00	19.10	0.00	0.00
52.85	36.98	23.14	1.83	76.30	2.00	18.69	0.00	0.00
52.89	36.45	22.74	1.83	75.93	2.00	18.12	0.00	0.00
52.99	35.72	22.19	1.82	75.10	2.00	17.30	0.00	0.00
53.04	34.87	21.58	1.79	73.90	2.00	16.38	0.00	0.00

:: Estimation of post-earthquake lateral Displacements :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	R_f (%)	$Q_{tn,cs}$	FS	D_r	$Gamma_{max}$ (%)	Lat. disp. (in)
53.08	33.84	20.84	1.76	72.53	2.00	15.23	0.00	0.00
53.17	32.85	20.12	1.72	70.98	2.00	14.08	0.00	0.00
53.24	31.89	19.44	1.67	69.26	2.00	12.94	0.00	0.00
53.33	31.20	18.95	1.60	67.56	2.00	12.10	0.00	0.00
53.39	30.55	18.50	1.54	65.95	2.00	11.30	0.00	0.00
53.42	29.84	18.00	1.49	64.53	2.00	10.41	0.00	0.00
53.49	29.22	17.56	1.46	63.51	2.00	9.58	0.00	0.00
53.58	28.69	17.16	1.45	62.88	2.00	8.83	0.00	0.00
53.63	28.25	16.83	1.47	62.80	2.00	8.19	0.00	0.00
53.68	28.03	16.65	1.49	63.10	2.00	7.82	0.00	0.00
53.77	27.89	16.51	1.54	63.72	2.00	7.54	0.00	0.00
53.83	27.75	16.37	1.60	64.62	2.00	7.26	0.00	0.00
53.88	27.65	16.26	1.67	65.69	2.00	7.04	0.00	0.00
53.97	27.58	16.15	1.74	66.86	2.00	6.82	0.00	0.00
54.03	27.65	16.16	1.82	68.06	2.00	6.84	0.00	0.00
54.08	27.92	16.32	1.86	69.02	2.00	7.17	0.00	0.00
54.18	28.22	16.49	1.89	69.69	2.00	7.50	0.00	0.00
54.22	28.55	16.70	1.91	70.24	2.00	7.92	0.00	0.00
54.27	28.86	16.89	1.91	70.60	2.00	8.31	0.00	0.00
54.38	29.20	17.09	1.91	70.87	2.00	8.69	0.00	0.00
54.42	29.60	17.33	1.99	72.48	2.00	9.14	0.00	0.00
54.47	30.18	17.68	2.09	74.54	2.00	9.81	0.00	0.00
54.57	30.74	17.99	2.21	76.80	2.00	10.38	0.00	0.00
54.61	32.49	19.15	2.28	79.62	2.00	12.45	0.00	0.00
54.68	34.47	20.44	2.42	83.61	2.00	14.60	0.00	0.00
54.75	36.91	22.04	2.56	88.19	2.00	17.08	0.00	0.00
54.79	39.58	23.80	2.70	92.93	2.00	19.62	0.00	0.00
54.86	42.54	25.75	2.84	97.96	2.00	22.22	0.00	0.00
54.95	45.89	27.95	2.99	103.54	2.00	24.92	0.00	0.00
55.01	49.55	30.41	3.06	108.09	2.00	27.71	0.00	0.00
55.06	53.33	32.97	3.11	112.42	2.00	30.37	0.00	0.00
55.12	57.74	35.97	3.14	116.75	2.00	33.25	0.00	0.00
55.21	61.55	38.53	3.17	120.57	2.00	35.52	0.00	0.00
55.25	64.95	40.86	3.18	123.48	2.00	37.46	0.00	0.00
55.32	67.67	42.71	3.18	125.59	2.00	38.92	0.00	0.00
55.40	69.32	43.79	3.18	126.89	2.00	39.75	0.00	0.00
55.50	69.77	44.02	3.18	127.13	2.00	39.92	0.00	0.00
55.52	68.79	43.32	3.17	126.29	2.00	39.39	0.00	0.00
55.60	66.93	41.97	3.19	124.98	2.00	38.34	0.00	0.00
55.67	64.58	40.27	3.20	123.13	2.00	36.98	0.00	0.00
55.72	61.65	38.22	3.19	120.61	2.00	35.25	0.00	0.00
55.79	58.07	35.70	3.20	117.52	2.00	33.01	0.00	0.00
55.86	54.37	33.13	3.19	114.05	2.00	30.53	0.00	0.00
55.95	50.44	30.41	3.17	110.07	2.00	27.70	0.00	0.00
56.00	47.04	28.08	3.15	106.54	2.00	25.08	0.00	0.00
56.05	44.22	26.16	3.13	103.47	2.00	22.74	0.00	0.00
56.11	42.29	24.85	3.07	100.71	2.00	21.05	0.00	0.00
56.19	40.82	23.87	2.99	97.89	2.00	19.71	0.00	0.00

:: Estimation of post-earthquake lateral Displacements :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	R_f (%)	$Q_{tn,cs}$	FS	D_r	$Gamma_{max}$ (%)	Lat. disp. (in)
56.24	39.25	22.82	2.90	94.95	2.00	18.24	0.00	0.00
56.34	37.48	21.62	2.83	92.00	2.00	16.45	0.00	0.00
56.37	35.77	20.49	2.78	89.45	2.00	14.67	0.00	0.00
56.43	34.28	19.49	2.72	87.00	2.00	13.03	0.00	0.00
56.54	33.15	18.72	2.67	85.17	2.00	11.70	0.00	0.00
56.59	32.27	18.14	2.59	83.05	2.00	10.66	0.00	0.00
56.64	31.50	17.66	2.47	80.45	2.00	9.77	0.00	0.00
56.73	30.75	17.17	2.35	77.84	2.00	8.85	0.00	0.00
56.79	29.94	16.66	2.23	75.39	2.00	7.84	0.00	0.00
56.84	29.45	16.36	2.11	73.04	2.00	7.26	0.00	0.00
56.93	29.13	16.17	1.98	70.74	2.00	6.87	0.00	0.00
56.96	28.72	15.94	1.85	68.35	2.00	6.38	0.00	0.00
57.03	28.18	15.60	1.74	66.11	2.00	5.69	0.00	0.00
57.13	27.59	15.23	1.64	64.05	2.00	4.88	0.00	0.00
57.16	27.05	14.88	1.57	62.33	2.00	4.13	0.00	0.00
57.23	26.67	14.63	1.52	61.35	2.00	3.56	0.00	0.00
57.29	26.39	14.44	1.50	60.68	2.00	3.13	0.00	0.00
57.38	26.31	14.38	1.47	60.04	2.00	3.00	0.00	0.00
57.42	26.37	14.42	1.45	59.82	2.00	3.08	0.00	0.00
57.49	26.54	14.51	1.46	60.12	2.00	3.29	0.00	0.00
57.57	26.67	14.57	1.49	60.64	2.00	3.42	0.00	0.00
57.62	26.59	14.49	1.53	61.18	2.00	3.23	0.00	0.00
57.68	26.52	14.41	1.56	61.64	2.00	3.06	0.00	0.00
57.77	26.34	14.25	1.60	62.10	2.00	2.70	0.00	0.00
57.85	26.02	14.01	1.65	62.58	2.00	2.12	0.00	0.00
57.92	25.63	13.72	1.67	62.60	2.00	1.44	0.00	0.00
57.97	25.13	13.37	1.69	62.43	2.00	0.60	0.00	0.00
58.02	24.52	12.97	1.69	61.87	2.00	0.00	0.00	0.00
58.07	23.81	12.50	1.67	60.83	2.00	0.00	0.00	0.00
58.16	23.20	12.09	1.64	59.82	2.00	0.00	0.00	0.00
58.23	22.77	11.81	1.62	59.00	2.00	0.00	0.00	0.00
58.31	22.40	11.56	1.59	58.29	2.00	0.00	0.00	0.00
58.37	22.16	11.40	1.56	57.57	2.00	0.00	0.00	0.00
58.42	22.06	11.33	1.53	57.06	2.00	0.00	0.00	0.00
58.50	22.07	11.33	1.52	56.90	2.00	0.00	0.00	0.00
58.57	22.16	11.37	1.53	57.09	2.00	0.00	0.00	0.00
58.61	22.31	11.45	1.57	57.78	2.00	0.00	0.00	0.00
58.68	22.68	11.65	1.66	59.42	2.00	0.00	0.00	0.00
58.76	23.31	11.99	1.80	61.90	2.00	0.00	0.00	0.00
58.80	24.38	12.62	1.94	64.88	2.00	0.00	0.00	0.00
58.87	25.76	13.44	2.10	68.50	2.00	0.76	0.00	0.00
58.95	26.94	14.12	2.30	72.34	2.00	2.38	0.00	0.00
59.01	29.48	15.68	2.46	77.17	2.00	5.84	0.00	0.00
59.06	32.30	17.44	2.56	81.48	2.00	9.35	0.00	0.00
59.16	35.49	19.45	2.59	84.96	2.00	12.95	0.00	0.00
59.19	38.57	21.43	2.59	87.83	2.00	16.16	0.00	0.00
59.29	40.88	22.89	2.60	90.03	2.00	18.33	0.00	0.00
59.33	42.63	24.01	2.60	91.61	2.00	19.91	0.00	0.00

:: Estimation of post-earthquake lateral Displacements :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	R_f (%)	$Q_{tn,cs}$	FS	D_r	$Gamma_{max}$ (%)	Lat. disp. (in)
59.39	43.82	24.76	2.60	92.47	2.00	20.93	0.00	0.00
59.47	44.76	25.38	2.54	92.27	2.00	21.74	0.00	0.00
59.54	45.65	25.98	2.44	91.18	2.00	22.52	0.00	0.00
59.58	44.87	25.51	2.35	88.87	2.00	21.91	0.00	0.00
59.65	43.24	24.45	2.28	86.35	2.00	20.51	0.00	0.00
59.73	40.72	22.76	2.30	84.64	2.00	18.15	0.00	0.00
59.81	38.24	21.07	2.38	83.87	2.00	15.60	0.00	0.00
59.85	36.61	20.12	2.14	78.60	2.00	14.08	0.00	0.00
59.92	35.57	19.57	1.85	72.90	2.00	13.16	0.00	0.00
59.99	35.26	19.53	1.54	67.02	2.00	13.09	0.00	0.00
60.08	35.07	19.57	1.25	61.24	2.00	13.17	0.00	0.00
60.13	35.05	19.76	0.99	55.82	2.00	13.49	0.00	0.00
60.18	35.20	20.10	0.74	50.35	2.00	14.04	0.00	0.00
60.27	35.91	20.86	0.51	44.99	2.00	15.27	0.00	0.00
60.33	37.42	22.37	0.27	22.37	2.00	17.58	0.00	0.00
60.38	38.51	N/A	0.00	-1.00	2.00	0.00	0.00	0.00
60.47	38.91	N/A	0.00	-1.00	2.00	0.00	0.00	0.00

Total estimated displacement: 0.00

Abbreviations

q_t: Total cone resistance
Q_{tn}: Adjusted cone resistance to an effective overburden stress of 1 atm
R_f: Friction ration
$Q_{tn,cs}$: Adjusted and corrected cone resistance due to fines
FS: Calculated factor of safety against liquefaction
D_r: Calculated relative density
$Gamma_{max}$: Calculated maximum cyclic shear strain
Lat. disp.: Lateral displacement

:: Strength loss calculation (Robertson (2009) ::

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
0.10	66.47	106.79	1.00	106.79	1.53	N/A	N/A
0.16	86.45	138.87	1.00	138.87	1.43	N/A	N/A
0.23	106.22	170.64	1.00	170.64	1.36	N/A	N/A
0.30	105.13	168.88	1.00	168.88	1.43	N/A	N/A
0.34	103.27	165.88	1.00	165.88	1.49	N/A	N/A
0.40	111.18	178.59	1.00	178.59	1.51	N/A	N/A
0.50	114.67	184.19	1.00	184.19	1.56	N/A	N/A
0.54	109.80	176.35	1.00	176.09	1.64	N/A	N/A
0.60	102.06	163.92	1.06	174.37	1.74	N/A	N/A
0.68	93.31	149.86	1.13	170.05	1.84	N/A	N/A
0.73	85.63	137.51	1.21	166.98	1.93	N/A	N/A
0.80	77.42	124.31	1.31	162.91	2.01	N/A	N/A
0.87	68.51	109.99	1.45	159.28	2.10	N/A	N/A
0.95	59.06	94.79	1.65	156.57	2.19	N/A	N/A
0.99	51.06	81.93	1.89	154.68	2.28	N/A	N/A
1.09	43.83	70.32	2.17	152.86	2.36	N/A	N/A
1.14	37.48	60.11	2.52	151.36	2.45	N/A	N/A
1.22	33.30	53.38	2.79	148.94	2.50	N/A	N/A
1.29	30.41	48.74	2.99	145.59	2.54	N/A	N/A
1.33	27.94	44.77	3.17	141.81	2.57	N/A	N/A
1.39	26.55	42.53	3.25	138.36	2.59	N/A	N/A
1.48	25.16	40.28	3.36	135.34	2.61	N/A	N/A
1.52	23.90	38.26	3.47	132.83	2.62	N/A	N/A
1.59	22.67	36.27	3.59	130.17	2.64	N/A	N/A
1.66	21.45	34.31	3.71	127.25	2.66	N/A	N/A
1.73	20.34	32.51	3.82	124.27	2.68	N/A	N/A
1.78	19.30	30.85	3.93	121.23	2.69	N/A	N/A
1.84	18.28	29.19	4.05	118.09	2.71	N/A	N/A
1.93	17.32	27.65	4.16	115.10	2.72	N/A	N/A
1.98	16.62	26.51	4.23	112.12	2.73	N/A	N/A
2.04	16.02	25.54	4.27	109.19	2.74	N/A	N/A
2.13	15.55	24.78	4.28	106.17	2.74	N/A	N/A
2.18	15.21	24.24	4.28	103.74	2.74	N/A	N/A
2.25	14.92	23.76	4.27	101.54	2.74	N/A	N/A
2.30	14.59	23.22	4.28	99.44	2.74	N/A	N/A
2.38	14.19	22.57	4.32	97.46	2.74	N/A	N/A
2.44	13.77	21.89	4.36	95.56	2.75	N/A	N/A
2.51	13.43	21.34	4.39	93.67	2.75	N/A	N/A
2.57	12.91	20.51	4.49	91.99	2.76	N/A	N/A
2.66	12.46	19.76	4.56	90.22	2.77	N/A	N/A
2.72	11.95	18.94	4.69	88.81	2.79	N/A	N/A
2.76	11.46	18.15	4.83	87.61	2.80	N/A	N/A
2.84	11.04	17.48	4.95	86.59	2.82	N/A	N/A
2.92	10.76	17.02	5.04	85.86	2.83	N/A	N/A
2.95	10.61	16.78	5.11	85.81	2.84	N/A	N/A
3.07	10.55	16.67	5.16	86.11	2.84	N/A	N/A
3.11	10.53	16.64	5.21	86.64	2.85	N/A	N/A
3.16	10.59	16.73	5.23	87.50	2.85	N/A	N/A

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
3.26	10.65	16.82	5.27	88.61	2.85	N/A	N/A
3.30	10.69	16.88	5.32	89.72	2.86	N/A	N/A
3.36	10.69	16.87	5.38	90.83	2.87	N/A	N/A
3.44	10.63	16.77	5.48	91.84	2.88	N/A	N/A
3.50	10.53	16.60	5.58	92.62	2.89	N/A	N/A
3.56	10.42	16.42	5.66	92.91	2.90	N/A	N/A
3.62	10.33	16.27	5.70	92.71	2.90	N/A	N/A
3.71	10.23	16.10	5.74	92.40	2.90	N/A	N/A
3.76	10.16	15.98	5.76	92.07	2.91	N/A	N/A
3.82	10.09	15.87	5.80	91.98	2.91	N/A	N/A
3.90	10.01	15.73	5.84	91.90	2.91	N/A	N/A
3.95	9.95	15.63	5.87	91.68	2.92	N/A	N/A
4.00	9.91	15.56	5.92	92.18	2.92	N/A	N/A
4.09	9.91	15.55	5.96	92.78	2.93	N/A	N/A
4.16	9.90	15.52	6.01	93.26	2.93	N/A	N/A
4.20	9.88	15.49	6.07	93.97	2.94	N/A	N/A
4.27	9.84	15.42	6.13	94.57	2.94	N/A	N/A
4.34	9.78	15.32	6.20	94.94	2.95	N/A	N/A
4.44	9.81	15.36	6.19	95.05	2.95	N/A	N/A
4.48	9.87	15.45	6.17	95.38	2.95	N/A	N/A
4.58	9.94	15.55	6.16	95.82	2.95	N/A	N/A
4.63	10.01	15.66	6.12	95.80	2.94	N/A	N/A
4.68	10.05	15.72	6.09	95.79	2.94	N/A	N/A
4.73	10.11	15.81	6.07	96.00	2.94	N/A	N/A
4.80	10.09	15.77	6.10	96.24	2.94	N/A	N/A
4.86	10.05	15.71	6.13	96.36	2.94	N/A	N/A
4.93	9.96	15.56	6.18	96.16	2.95	N/A	N/A
5.00	9.76	15.23	6.26	95.42	2.96	N/A	N/A
5.07	9.55	14.89	6.32	94.09	2.96	N/A	N/A
5.12	9.29	14.45	6.40	92.51	2.97	N/A	N/A
5.20	8.98	13.95	6.50	90.66	2.98	N/A	N/A
5.27	8.60	13.34	6.64	88.54	2.99	N/A	N/A
5.33	8.15	12.61	6.82	86.10	3.01	N/A	N/A
5.41	7.76	11.98	6.96	83.44	3.02	N/A	N/A
5.45	7.40	11.40	7.09	80.81	3.03	N/A	N/A
5.52	7.10	10.90	7.19	78.36	3.04	N/A	N/A
5.60	6.84	10.48	7.30	76.53	3.05	N/A	N/A
5.67	6.62	10.12	7.43	75.22	3.06	N/A	N/A
5.71	6.54	9.99	7.47	74.64	3.06	N/A	N/A
5.80	6.55	10.00	7.43	74.36	3.06	N/A	N/A
5.85	6.66	10.17	7.33	74.53	3.05	N/A	N/A
5.91	6.84	10.45	7.20	75.27	3.04	N/A	N/A
6.01	7.03	10.75	7.10	76.28	3.03	N/A	N/A
6.06	7.21	11.05	7.01	77.41	3.02	N/A	N/A
6.11	7.45	11.42	6.87	78.52	3.01	N/A	N/A
6.18	7.68	11.78	6.73	79.34	3.00	N/A	N/A
6.26	7.96	12.22	6.53	79.86	2.98	N/A	N/A
6.30	8.20	12.60	6.33	79.82	2.96	N/A	N/A

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
6.37	8.40	12.92	6.17	79.64	2.95	N/A	N/A
6.45	8.58	13.22	6.00	79.31	2.93	N/A	N/A
6.51	8.76	13.50	5.84	78.83	2.91	N/A	N/A
6.60	8.92	13.75	5.71	78.49	2.90	N/A	N/A
6.64	9.07	13.99	5.60	78.29	2.89	N/A	N/A
6.70	9.17	14.14	5.54	78.39	2.88	N/A	N/A
6.80	9.25	14.26	5.52	78.78	2.88	N/A	N/A
6.83	9.26	14.27	5.56	79.34	2.89	N/A	N/A
6.90	9.24	14.24	5.62	80.05	2.89	N/A	N/A
6.98	9.23	14.21	5.68	80.74	2.90	N/A	N/A
7.04	9.25	14.23	5.72	81.42	2.90	N/A	N/A
7.09	9.31	14.32	5.73	82.07	2.90	N/A	N/A
7.16	9.38	14.43	5.73	82.72	2.90	N/A	N/A
7.24	9.45	14.53	5.75	83.49	2.90	N/A	N/A
7.30	9.50	14.61	5.75	84.00	2.91	N/A	N/A
7.39	9.54	14.67	5.73	83.98	2.90	N/A	N/A
7.43	9.55	14.68	5.74	84.24	2.90	N/A	N/A
7.50	9.53	14.65	5.83	85.43	2.91	N/A	N/A
7.59	9.48	14.56	5.95	86.60	2.93	N/A	N/A
7.63	9.40	14.43	6.08	87.77	2.94	N/A	N/A
7.70	9.18	14.07	6.30	88.70	2.96	N/A	N/A
7.78	8.96	13.71	6.53	89.48	2.98	N/A	N/A
7.83	8.81	13.45	6.68	89.86	2.99	N/A	N/A
7.89	8.62	13.14	6.88	90.36	3.01	N/A	N/A
7.95	8.42	12.82	7.11	91.06	3.03	N/A	N/A
8.02	8.21	12.47	7.32	91.27	3.05	N/A	N/A
8.11	7.99	12.12	7.46	90.42	3.06	N/A	N/A
8.16	7.78	11.78	7.58	89.31	3.07	N/A	N/A
8.21	7.58	11.45	7.69	88.06	3.08	N/A	N/A
8.30	7.48	11.29	7.69	86.84	3.08	N/A	N/A
8.36	7.40	11.16	7.67	85.60	3.08	N/A	N/A
8.41	7.34	11.04	7.64	84.34	3.08	N/A	N/A
8.47	7.34	11.04	7.53	83.09	3.07	N/A	N/A
8.56	7.38	11.09	7.40	82.08	3.06	N/A	N/A
8.61	7.46	11.22	7.27	81.58	3.05	N/A	N/A
8.70	7.58	11.40	7.13	81.34	3.03	N/A	N/A
8.75	7.71	11.61	7.02	81.48	3.02	N/A	N/A
8.81	7.85	11.83	6.91	81.75	3.01	N/A	N/A
8.90	8.00	12.06	6.80	82.01	3.01	N/A	N/A
8.94	8.12	12.26	6.71	82.26	3.00	N/A	N/A
9.01	8.19	12.37	6.67	82.52	2.99	1.11	1.11
9.09	8.22	12.41	6.67	82.78	2.99	1.10	1.10
9.13	8.21	12.39	6.68	82.78	2.99	1.10	1.10
9.20	8.17	12.32	6.69	82.39	2.99	1.08	1.08
9.27	8.09	12.17	6.73	81.87	3.00	1.06	1.06
9.35	7.98	11.99	6.76	81.08	3.00	1.04	1.04
9.39	7.84	11.76	6.80	80.02	3.01	1.01	1.01
9.45	7.69	11.52	6.85	78.94	3.01	0.99	0.99

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
9.54	7.54	11.27	6.89	77.70	3.01	0.96	0.96
9.59	7.39	11.03	6.94	76.58	3.02	0.93	0.93
9.65	7.26	10.82	6.96	75.30	3.02	0.91	0.91
9.73	7.13	10.59	6.99	73.99	3.02	0.88	0.88
9.81	6.99	10.36	7.01	72.66	3.02	0.86	0.86
9.85	6.89	10.20	7.01	71.46	3.02	0.84	0.84
9.94	6.81	10.06	7.00	70.39	3.02	0.82	0.82
10.00	6.75	9.96	6.99	69.61	3.02	0.36	0.81
10.04	6.74	9.94	6.94	68.99	3.02	0.35	0.80
10.12	6.81	10.05	6.87	69.00	3.01	0.34	0.81
10.19	6.96	10.28	6.77	69.63	3.00	0.34	0.82
10.24	7.18	10.63	6.67	70.86	2.99	0.84	0.84
10.31	7.51	11.15	6.54	72.96	2.98	0.88	0.88
10.39	7.85	11.70	6.42	75.13	2.97	0.92	0.92
10.48	8.26	12.35	6.24	77.07	2.95	0.96	0.96
10.53	8.69	13.04	6.08	79.21	2.94	1.01	1.01
10.63	9.14	13.75	5.95	81.80	2.93	1.05	1.05
10.67	9.60	14.48	5.86	84.82	2.92	1.10	1.10
10.71	10.01	15.13	5.78	87.48	2.91	1.15	1.15
10.79	10.33	15.64	5.74	89.85	2.90	1.18	1.18
10.83	10.50	15.91	5.77	91.85	2.91	1.19	1.19
10.93	10.75	16.31	5.71	93.18	2.90	1.21	1.21
10.98	11.01	16.72	5.66	94.60	2.90	1.24	1.24
11.06	11.19	17.00	5.66	96.27	2.90	1.25	1.25
11.11	11.33	17.22	5.67	97.70	2.90	1.26	1.26
11.16	11.42	17.37	5.68	98.57	2.90	1.27	1.27
11.23	11.42	17.36	5.70	98.91	2.90	1.26	1.26
11.31	11.37	17.21	5.75	98.90	2.90	1.24	1.24
11.36	11.30	17.04	5.78	98.56	2.91	1.23	1.23
11.42	11.29	16.93	5.79	98.01	2.91	1.22	1.22
11.51	11.10	16.53	5.90	97.52	2.92	1.19	1.19
11.56	10.86	16.11	6.01	96.84	2.93	1.16	1.16
11.65	10.63	15.65	6.12	95.79	2.94	1.12	1.12
11.71	10.44	15.29	6.19	94.68	2.95	1.09	1.09
11.75	10.23	14.92	6.27	93.61	2.96	1.07	1.07
11.84	10.11	14.60	6.31	92.08	2.96	1.04	1.04
11.89	10.00	14.37	6.30	90.56	2.96	1.03	1.03
11.96	9.97	14.23	6.23	88.71	2.95	1.02	1.02
12.03	9.99	14.17	6.13	86.82	2.94	1.01	1.01
12.11	10.04	14.16	5.99	84.80	2.93	1.02	1.02
12.16	10.16	14.28	5.82	83.13	2.91	1.03	1.03
12.21	10.35	14.49	5.63	81.63	2.89	1.05	1.05
12.30	10.54	14.68	5.47	80.34	2.88	1.06	1.06
12.35	10.78	14.96	5.31	79.44	2.86	1.09	1.09
12.41	10.95	15.15	5.23	79.26	2.85	1.10	1.10
12.49	11.12	15.34	5.19	79.58	2.85	1.12	1.12
12.56	11.24	15.48	5.20	80.48	2.85	1.13	1.13
12.60	11.35	15.63	5.22	81.65	2.85	1.14	1.14

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
12.67	11.48	15.78	5.25	82.89	2.85	1.15	1.15
12.75	11.63	15.96	5.26	83.95	2.85	1.16	1.16
12.80	11.76	16.12	5.28	85.04	2.86	1.17	1.17
12.90	11.84	16.20	5.32	86.09	2.86	1.18	1.18
12.95	11.93	16.30	5.34	87.05	2.86	1.18	1.18
13.02	12.03	16.41	5.35	87.86	2.86	1.19	1.19
13.06	12.13	16.53	5.35	88.44	2.86	1.20	1.20
13.14	12.22	16.60	5.35	88.87	2.86	1.20	1.20
13.19	12.29	16.67	5.35	89.23	2.86	1.21	1.21
13.29	12.33	16.67	5.37	89.55	2.87	1.21	1.21
13.33	12.32	16.64	5.41	89.97	2.87	1.20	1.20
13.39	12.30	16.58	5.44	90.15	2.87	1.20	1.20
13.48	12.31	16.54	5.45	90.15	2.87	1.20	1.20
13.54	12.39	16.62	5.44	90.48	2.87	1.20	1.20
13.59	12.53	16.78	5.42	90.88	2.87	1.21	1.21
13.67	12.75	17.02	5.36	91.29	2.86	1.23	1.23
13.72	12.96	17.27	5.32	91.86	2.86	1.25	1.25
13.78	13.12	17.46	5.30	92.55	2.86	1.27	1.27
13.86	13.28	17.63	5.29	93.31	2.86	1.28	1.28
13.93	13.44	17.80	5.29	94.19	2.86	1.29	1.29
14.01	13.55	17.91	5.31	95.18	2.86	1.30	1.30
14.05	13.62	17.99	5.35	96.24	2.86	1.30	1.30
14.14	13.62	17.94	5.40	96.86	2.87	1.30	1.30
14.21	13.57	17.84	5.45	97.32	2.87	1.29	1.29
14.24	13.41	17.63	5.55	97.81	2.88	1.27	1.27
14.31	13.27	17.41	5.64	98.13	2.89	1.25	1.25
14.39	13.17	17.24	5.70	98.30	2.90	1.24	1.24
14.44	13.06	17.07	5.76	98.31	2.91	1.23	1.23
14.54	12.93	16.84	5.83	98.16	2.91	1.21	1.21
14.59	12.82	16.67	5.88	98.07	2.92	1.20	1.20
14.64	12.73	16.52	5.92	97.86	2.92	1.19	1.19
14.70	12.62	16.34	5.98	97.64	2.93	1.17	1.17
14.79	12.49	16.12	6.04	97.30	2.93	1.15	1.15
14.83	12.35	15.91	6.09	96.83	2.94	1.14	1.14
14.93	12.16	15.61	6.16	96.10	2.95	1.12	1.12
14.98	11.95	15.29	6.24	95.44	2.95	1.09	1.09
15.03	11.68	14.89	6.36	94.64	2.96	1.06	1.06
15.10	11.42	14.50	6.47	93.80	2.98	1.04	1.04
15.18	11.13	14.06	6.60	92.84	2.99	1.00	1.00
15.23	10.82	13.61	6.75	91.81	3.00	0.97	0.97
15.33	10.52	13.15	6.89	90.69	3.01	0.94	0.94
15.37	10.18	12.68	7.08	89.73	3.03	0.91	0.91
15.44	9.83	12.17	7.29	88.70	3.05	0.87	0.87
15.52	9.47	11.65	7.53	87.73	3.07	0.83	0.83
15.56	9.15	11.19	7.74	86.58	3.09	0.80	0.80
15.63	8.84	10.74	7.96	85.48	3.10	0.77	0.77
15.71	8.52	10.28	8.19	84.22	3.12	0.73	0.73
15.77	8.24	9.89	8.39	82.98	3.14	0.71	0.71

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
15.82	7.99	9.53	8.58	81.84	3.15	0.68	0.68
15.89	7.76	9.20	8.75	80.56	3.16	0.66	0.66
15.97	7.60	8.95	8.85	79.20	3.17	0.64	0.64
16.02	7.48	8.78	8.90	78.11	3.17	0.63	0.63
16.10	7.44	8.70	8.87	77.14	3.17	0.62	0.62
16.17	7.44	8.67	8.80	76.32	3.17	0.62	0.62
16.22	7.52	8.76	8.62	75.56	3.15	0.63	0.63
16.28	7.65	8.91	8.41	74.93	3.14	0.64	0.64
16.37	7.84	9.15	8.15	74.50	3.12	0.65	0.65
16.42	8.08	9.44	7.86	74.22	3.09	0.67	0.67
16.52	8.33	9.74	7.59	73.87	3.07	0.70	0.70
16.55	8.58	10.05	7.33	73.67	3.05	0.72	0.72
16.62	8.83	10.35	7.09	73.40	3.03	0.74	0.74
16.70	9.06	10.62	6.89	73.23	3.01	0.76	0.76
16.74	9.49	11.17	6.55	73.19	2.98	0.80	0.80
16.82	10.11	11.93	6.13	73.13	2.94	0.85	0.85
16.91	10.53	12.39	5.88	72.87	2.92	0.89	0.89
16.94	10.72	12.62	5.75	72.51	2.90	0.91	0.91
17.01	10.87	12.76	5.65	72.13	2.90	0.92	0.92
17.10	11.00	12.88	5.58	71.87	2.89	0.93	0.93
17.15	11.13	13.01	5.51	71.64	2.88	0.94	0.94
17.21	11.54	13.47	5.29	71.26	2.86	0.97	0.97
17.30	11.94	13.90	5.09	70.72	2.83	1.01	1.01
17.34	11.76	13.66	5.16	70.54	2.84	0.99	0.99
17.41	11.25	13.04	5.42	70.64	2.87	0.94	0.94
17.49	10.96	12.66	5.59	70.73	2.89	0.91	0.91
17.53	10.95	12.64	5.60	70.83	2.89	0.91	0.91
17.59	10.82	12.46	5.68	70.73	2.90	0.90	0.90
17.67	10.63	12.20	5.79	70.63	2.91	0.88	0.88
17.73	10.45	11.97	5.88	70.41	2.92	0.86	0.86
17.79	10.07	11.49	6.11	70.27	2.94	0.82	0.82
17.87	9.70	11.01	6.36	70.05	2.96	0.79	0.79
17.92	9.63	10.90	6.40	69.77	2.97	0.33	0.78
17.99	9.66	10.91	6.34	69.22	2.96	0.31	0.78
18.07	9.81	11.07	6.20	68.63	2.95	0.31	0.79
18.14	9.80	11.03	6.17	68.07	2.95	0.31	0.79
18.19	9.97	11.20	6.04	67.72	2.93	0.31	0.80
18.26	10.14	11.38	5.92	67.35	2.92	0.30	0.82
18.34	10.13	11.33	5.92	67.04	2.92	0.30	0.81
18.38	9.99	11.15	5.98	66.67	2.93	0.30	0.80
18.45	9.85	10.96	6.06	66.41	2.94	0.30	0.78
18.53	9.72	10.78	6.13	66.14	2.94	0.30	0.77
18.60	9.58	10.60	6.23	66.01	2.95	0.28	0.76
18.68	9.26	10.18	6.47	65.85	2.98	0.27	0.73
18.72	8.93	9.75	6.73	65.57	3.00	0.28	0.70
18.79	8.50	9.20	7.08	65.11	3.03	0.28	0.66
18.84	8.10	8.69	7.42	64.48	3.06	0.28	0.62
18.92	7.83	8.34	7.65	63.84	3.08	0.28	0.60

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
18.98	7.61	8.06	7.84	63.20	3.09	0.27	0.58
19.06	7.40	7.77	8.02	62.28	3.11	0.26	0.55
19.11	7.23	7.55	8.13	61.39	3.12	0.24	0.54
19.18	7.07	7.34	8.24	60.47	3.12	0.23	0.52
19.25	6.92	7.14	8.36	59.68	3.13	0.22	0.51
19.33	6.83	7.02	8.41	59.04	3.14	0.21	0.50
19.37	6.81	6.98	8.41	58.73	3.14	0.21	0.50
19.47	6.80	6.95	8.42	58.53	3.14	0.21	0.50
19.52	6.83	6.97	8.39	58.52	3.14	0.22	0.50
19.57	6.85	6.99	8.39	58.63	3.14	0.22	0.50
19.62	6.84	6.96	8.45	58.85	3.14	0.23	0.50
19.71	6.81	6.91	8.55	59.04	3.15	0.23	0.49
19.77	6.74	6.81	8.71	59.33	3.16	0.23	0.49
19.82	6.58	6.61	8.97	59.29	3.18	0.23	0.47
19.91	6.46	6.44	9.15	58.99	3.19	0.23	0.46
19.96	6.31	6.25	9.36	58.55	3.21	0.23	0.45
20.02	6.19	6.09	9.55	58.11	3.22	0.24	0.43
20.11	6.06	5.91	9.73	57.52	3.23	0.23	0.42
20.18	5.93	5.75	9.91	56.93	3.25	0.20	0.41
20.23	5.83	5.62	10.01	56.25	3.25	0.20	0.40
20.28	5.74	5.50	10.08	55.46	3.26	0.20	0.39
20.37	5.70	5.44	10.03	54.57	3.25	0.19	0.39
20.42	5.74	5.48	9.85	53.93	3.24	0.19	0.39
20.48	5.73	5.45	9.83	53.62	3.24	0.18	0.39
20.56	5.74	5.45	9.78	53.31	3.24	0.17	0.39
20.63	5.76	5.46	9.71	53.02	3.23	0.16	0.39
20.67	5.80	5.50	9.62	52.91	3.23	0.16	0.39
20.74	5.86	5.56	9.50	52.80	3.22	0.18	0.40
20.83	5.92	5.61	9.41	52.82	3.21	0.18	0.40
20.90	5.98	5.67	9.34	52.98	3.21	0.18	0.41
20.97	6.03	5.72	9.30	53.14	3.20	0.18	0.41
21.02	6.11	5.80	9.19	53.33	3.20	0.18	0.41
21.10	6.22	5.91	9.05	53.53	3.19	0.17	0.42
21.17	6.35	6.05	8.90	53.88	3.17	0.17	0.43
21.22	6.49	6.20	8.74	54.25	3.16	0.17	0.44
21.27	6.64	6.37	8.60	54.75	3.15	0.17	0.45
21.37	6.79	6.52	8.47	55.21	3.14	0.19	0.47
21.43	6.95	6.69	8.32	55.69	3.13	0.20	0.48
21.46	7.09	6.86	8.19	56.17	3.12	0.20	0.49
21.55	7.24	7.01	8.06	56.47	3.11	0.21	0.50
21.62	7.36	7.13	7.96	56.76	3.10	0.21	0.51
21.66	7.42	7.19	7.87	56.63	3.10	0.21	0.51
21.74	7.41	7.16	7.84	56.18	3.09	0.21	0.51
21.81	7.37	7.10	7.84	55.71	3.09	0.19	0.51
21.85	7.30	7.01	7.86	55.11	3.09	0.19	0.50
21.93	7.21	6.89	7.88	54.32	3.10	0.17	0.49
22.00	7.13	6.78	7.90	53.54	3.10	0.16	0.48
22.07	7.06	6.69	7.91	52.89	3.10	0.16	0.48

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
22.16	6.98	6.58	7.96	52.37	3.10	0.16	0.47
22.19	6.91	6.49	8.01	52.03	3.11	0.15	0.46
22.26	6.87	6.43	8.10	52.11	3.11	0.15	0.46
22.33	6.86	6.41	8.19	52.50	3.12	0.16	0.46
22.40	6.86	6.39	8.27	52.89	3.13	0.16	0.46
22.45	6.88	6.41	8.30	53.16	3.13	0.17	0.46
22.53	6.88	6.39	8.31	53.12	3.13	0.18	0.46
22.60	6.86	6.36	8.35	53.07	3.13	0.19	0.45
22.64	6.79	6.27	8.45	53.00	3.14	0.19	0.45
22.70	6.72	6.18	8.61	53.20	3.15	0.18	0.44
22.80	6.68	6.11	8.71	53.25	3.16	0.15	0.44
22.84	6.59	6.01	8.83	53.02	3.17	0.15	0.43
22.90	6.58	5.98	8.78	52.57	3.17	0.16	0.43
23.00	6.68	6.08	8.56	52.04	3.15	0.18	0.43
23.05	6.77	6.17	8.47	52.22	3.14	0.18	0.44
23.14	6.93	6.33	8.42	53.25	3.14	0.17	0.45
23.18	7.11	6.52	8.37	54.56	3.13	0.16	0.47
23.24	7.32	6.74	8.36	56.36	3.13	0.14	0.48
23.32	7.52	6.94	8.40	58.31	3.14	0.19	0.50
23.39	7.66	7.09	8.50	60.28	3.14	0.22	0.51
23.44	7.83	7.27	8.59	62.42	3.15	0.24	0.52
23.53	7.88	7.30	8.83	64.47	3.17	0.30	0.52
23.59	7.80	7.20	9.20	66.24	3.20	0.34	0.51
23.63	7.63	7.01	9.57	67.05	3.22	0.35	0.50
23.69	7.43	6.76	9.96	67.36	3.25	0.36	0.48
23.77	7.22	6.52	10.30	67.12	3.27	0.36	0.47
23.82	7.02	6.29	10.54	66.24	3.29	0.34	0.45
23.93	6.84	6.07	10.70	64.93	3.30	0.30	0.43
23.95	6.71	5.92	10.73	63.57	3.30	0.28	0.42
24.03	6.63	5.82	10.65	62.00	3.30	0.25	0.42
24.12	6.60	5.77	10.47	60.46	3.28	0.23	0.41
24.16	6.59	5.76	10.28	59.15	3.27	0.23	0.41
24.22	6.66	5.82	10.02	58.33	3.25	0.22	0.42
24.30	6.73	5.88	9.81	57.69	3.24	0.21	0.42
24.37	6.79	5.93	9.69	57.49	3.23	0.21	0.42
24.43	6.88	6.02	9.56	57.55	3.22	0.21	0.43
24.50	7.00	6.14	9.41	57.74	3.21	0.21	0.44
24.57	7.09	6.22	9.33	58.01	3.21	0.22	0.44
24.62	7.17	6.30	9.29	58.51	3.20	0.23	0.45
24.69	7.23	6.35	9.29	58.98	3.20	0.23	0.45
24.77	7.28	6.39	9.31	59.42	3.20	0.24	0.46
24.83	7.32	6.42	9.31	59.75	3.20	0.24	0.46
24.88	7.37	6.46	9.29	59.98	3.20	0.25	0.46
24.97	7.40	6.47	9.28	60.06	3.20	0.25	0.46
25.02	7.42	6.49	9.26	60.05	3.20	0.25	0.46
25.11	7.41	6.46	9.27	59.87	3.20	0.23	0.46
25.17	7.41	6.45	9.28	59.83	3.20	0.23	0.46
25.21	7.40	6.43	9.28	59.69	3.20	0.23	0.46

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
25.29	7.44	6.45	9.26	59.78	3.20	0.22	0.46
25.36	7.55	6.56	9.16	60.05	3.19	0.22	0.47
25.40	7.70	6.71	9.02	60.47	3.18	0.23	0.48
25.46	7.86	6.86	8.90	61.10	3.17	0.23	0.49
25.54	8.04	7.03	8.77	61.72	3.17	0.25	0.50
25.62	8.20	7.18	8.69	62.42	3.16	0.26	0.51
25.66	8.36	7.34	8.63	63.34	3.15	0.26	0.52
25.75	8.51	7.48	8.58	64.20	3.15	0.28	0.53
25.80	8.67	7.63	8.53	65.08	3.15	0.28	0.55
25.85	8.81	7.77	8.46	65.74	3.14	0.28	0.55
25.96	8.75	7.68	8.62	66.22	3.15	0.30	0.55
26.01	8.74	7.66	8.73	66.87	3.16	0.31	0.55
26.05	8.80	7.71	8.76	67.56	3.16	0.31	0.55
26.12	8.87	7.77	8.77	68.13	3.16	0.31	0.55
26.19	8.95	7.84	8.75	68.60	3.16	0.32	0.56
26.25	9.02	7.89	8.71	68.79	3.16	0.33	0.56
26.33	8.98	7.83	8.77	68.70	3.16	0.35	0.56
26.42	8.87	7.70	8.89	68.46	3.17	0.34	0.55
26.46	8.73	7.55	9.03	68.15	3.18	0.33	0.54
26.52	8.73	7.53	9.00	67.82	3.18	0.32	0.54
26.61	8.65	7.43	9.05	67.22	3.19	0.31	0.53
26.67	8.48	7.24	9.15	66.29	3.19	0.30	0.52
26.71	8.31	7.06	9.25	65.26	3.20	0.29	0.50
26.79	8.11	6.84	9.40	64.26	3.21	0.29	0.49
26.87	7.92	6.62	9.56	63.35	3.22	0.28	0.47
26.92	7.81	6.50	9.63	62.62	3.23	0.27	0.46
26.98	7.77	6.45	9.60	61.94	3.23	0.24	0.46
27.06	7.73	6.40	9.58	61.25	3.22	0.24	0.46
27.11	7.69	6.35	9.54	60.57	3.22	0.24	0.45
27.21	7.63	6.27	9.56	59.94	3.22	0.24	0.45
27.26	7.55	6.18	9.60	59.31	3.22	0.23	0.44
27.32	7.39	6.01	9.77	58.70	3.24	0.22	0.43
27.40	7.24	5.84	9.94	58.07	3.25	0.22	0.42
27.45	7.09	5.67	10.09	57.22	3.26	0.22	0.41
27.52	6.97	5.54	10.12	56.08	3.26	0.21	0.40
27.60	6.81	5.37	10.24	54.98	3.27	0.20	0.38
27.65	6.69	5.24	10.31	54.03	3.27	0.20	0.37
27.71	6.59	5.13	10.37	53.20	3.28	0.18	0.37
27.80	6.56	5.09	10.31	52.43	3.27	0.15	0.36
27.84	6.56	5.08	10.20	51.83	3.27	0.15	0.36
27.90	6.65	5.16	9.99	51.56	3.25	0.15	0.37
27.99	6.75	5.25	9.82	51.51	3.24	0.16	0.37
28.05	6.85	5.34	9.73	51.95	3.23	0.16	0.38
28.10	6.96	5.44	9.72	52.86	3.23	0.16	0.39
28.17	7.10	5.57	9.66	53.77	3.23	0.17	0.40
28.25	7.25	5.70	9.59	54.67	3.22	0.19	0.41
28.30	7.40	5.84	9.49	55.46	3.22	0.21	0.42
28.39	7.51	5.94	9.50	56.38	3.22	0.22	0.42

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
28.44	7.61	6.03	9.49	57.20	3.22	0.22	0.43
28.49	7.69	6.10	9.50	57.99	3.22	0.22	0.44
28.54	7.77	6.17	9.45	58.34	3.21	0.22	0.44
28.62	7.86	6.25	9.29	58.06	3.20	0.24	0.45
28.68	7.91	6.28	9.26	58.18	3.20	0.23	0.45
28.74	7.96	6.32	9.30	58.81	3.20	0.24	0.45
28.83	7.97	6.32	9.39	59.27	3.21	0.22	0.45
28.89	7.96	6.29	9.47	59.63	3.22	0.18	0.45
28.98	7.81	6.13	9.72	59.63	3.23	0.23	0.44
29.03	7.81	6.12	9.77	59.79	3.24	0.27	0.44
29.09	7.81	6.11	9.77	59.65	3.24	0.26	0.44
29.14	7.83	6.12	9.76	59.74	3.24	0.25	0.44
29.22	7.88	6.15	9.79	60.23	3.24	0.25	0.44
29.27	7.97	6.23	9.67	60.29	3.23	0.24	0.45
29.38	8.07	6.31	9.48	59.82	3.22	0.22	0.45
29.43	8.18	6.41	9.28	59.49	3.20	0.22	0.46
29.48	8.30	6.52	9.09	59.25	3.19	0.22	0.47
29.57	8.53	6.72	8.79	59.06	3.17	0.22	0.48
29.62	8.60	6.78	8.68	58.87	3.16	0.22	0.48
29.68	8.66	6.83	8.63	58.98	3.15	0.22	0.49
29.73	8.71	6.87	8.58	58.98	3.15	0.22	0.49
29.82	8.73	6.87	8.58	58.94	3.15	0.22	0.49
29.87	8.72	6.85	8.58	58.80	3.15	0.22	0.49
29.94	8.69	6.81	8.61	58.64	3.15	0.23	0.49
30.02	8.62	6.73	8.67	58.34	3.16	0.22	0.48
30.07	8.52	6.62	8.76	58.04	3.16	0.22	0.47
30.16	8.44	6.53	8.84	57.73	3.17	0.21	0.47
30.19	8.37	6.46	8.88	57.35	3.17	0.21	0.46
30.26	8.30	6.38	8.89	56.73	3.17	0.20	0.46
30.36	8.25	6.31	8.90	56.22	3.17	0.20	0.45
30.41	8.22	6.28	8.88	55.74	3.17	0.20	0.45
30.46	8.20	6.25	8.86	55.37	3.17	0.19	0.45
30.53	8.20	6.24	8.84	55.12	3.17	0.18	0.45
30.61	8.24	6.26	8.78	55.00	3.17	0.18	0.45
30.65	8.33	6.33	8.69	55.03	3.16	0.18	0.45
30.71	8.46	6.44	8.58	55.30	3.15	0.18	0.46
30.81	8.62	6.58	8.48	55.79	3.14	0.19	0.47
30.84	8.81	6.76	8.38	56.64	3.14	0.19	0.48
30.91	9.02	6.94	8.31	57.68	3.13	0.20	0.50
30.99	9.25	7.14	8.26	59.00	3.13	0.22	0.51
31.04	9.49	7.36	8.20	60.31	3.12	0.23	0.53
31.11	9.75	7.59	8.12	61.58	3.11	0.24	0.54
31.19	10.01	7.81	8.05	62.91	3.11	0.26	0.56
31.25	10.25	8.02	7.99	64.11	3.11	0.29	0.57
31.30	10.42	8.17	7.95	64.99	3.10	0.29	0.58
31.39	10.55	8.27	7.95	65.72	3.10	0.30	0.59
31.45	10.62	8.32	7.96	66.25	3.10	0.31	0.59
31.50	10.63	8.33	7.99	66.59	3.11	0.31	0.59

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
31.60	10.61	8.29	8.04	66.61	3.11	0.30	0.59
31.65	10.59	8.25	8.05	66.39	3.11	0.30	0.59
31.73	10.54	8.19	8.10	66.32	3.11	0.30	0.58
31.80	10.48	8.12	8.20	66.52	3.12	0.30	0.58
31.84	10.42	8.05	8.29	66.74	3.13	0.30	0.58
31.91	10.38	8.00	8.39	67.11	3.14	0.27	0.57
31.99	10.35	7.95	8.48	67.48	3.14	0.29	0.57
32.03	10.34	7.94	8.55	67.88	3.15	0.33	0.57
32.09	10.36	7.95	8.59	68.27	3.15	0.33	0.57
32.19	10.40	7.96	8.62	68.65	3.15	0.34	0.57
32.25	10.44	7.99	8.69	69.37	3.16	0.34	0.57
32.29	10.47	8.00	8.74	69.94	3.16	0.34	0.57
32.38	10.52	8.03	8.73	70.14	3.16	0.57	0.57
32.43	10.61	8.10	8.69	70.40	3.16	0.58	0.58
32.48	10.72	8.19	8.62	70.58	3.15	0.59	0.59
32.58	10.84	8.28	8.55	70.82	3.15	0.59	0.59
32.63	10.96	8.37	8.50	71.16	3.14	0.60	0.60
32.69	11.07	8.46	8.46	71.57	3.14	0.60	0.60
32.74	11.17	8.54	8.44	72.05	3.14	0.61	0.61
32.83	11.29	8.62	8.40	72.44	3.14	0.62	0.62
32.88	11.41	8.72	8.34	72.77	3.13	0.62	0.62
32.97	11.51	8.79	8.33	73.21	3.13	0.63	0.63
33.01	11.58	8.84	8.34	73.76	3.13	0.63	0.63
33.07	11.62	8.86	8.37	74.19	3.13	0.63	0.63
33.16	11.64	8.86	8.41	74.51	3.14	0.63	0.63
33.20	11.66	8.87	8.42	74.64	3.14	0.63	0.63
33.27	11.67	8.86	8.41	74.52	3.14	0.63	0.63
33.36	11.67	8.84	8.40	74.22	3.14	0.63	0.63
33.42	11.63	8.79	8.39	73.78	3.14	0.63	0.63
33.51	11.57	8.71	8.38	73.00	3.14	0.62	0.62
33.56	11.50	8.64	8.31	71.84	3.13	0.62	0.62
33.61	11.40	8.54	8.24	70.41	3.12	0.61	0.61
33.67	11.26	8.40	8.20	68.94	3.12	0.34	0.60
33.76	11.07	8.22	8.19	67.30	3.12	0.30	0.59
33.81	10.94	8.09	8.13	65.77	3.12	0.27	0.58
33.86	10.77	7.93	8.11	64.36	3.11	0.26	0.57
33.94	10.66	7.82	8.05	62.93	3.11	0.25	0.56
34.02	10.58	7.73	7.97	61.65	3.10	0.24	0.55
34.06	10.53	7.68	7.91	60.77	3.10	0.23	0.55
34.14	10.48	7.62	7.89	60.14	3.10	0.23	0.54
34.21	10.41	7.55	7.91	59.69	3.10	0.22	0.54
34.25	10.35	7.49	7.92	59.26	3.10	0.22	0.53
34.33	10.33	7.45	7.90	58.92	3.10	0.22	0.53
34.41	10.24	7.36	7.96	58.55	3.10	0.22	0.53
34.49	10.20	7.31	7.95	58.11	3.10	0.22	0.52
34.56	10.10	7.21	8.00	57.64	3.11	0.21	0.51
34.59	9.99	7.11	8.04	57.18	3.11	0.21	0.51
34.67	9.89	7.01	8.09	56.70	3.11	0.20	0.50

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
34.76	9.80	6.91	8.13	56.22	3.12	0.19	0.49
34.80	9.74	6.85	8.14	55.76	3.12	0.18	0.49
34.85	9.72	6.83	8.13	55.53	3.12	0.18	0.49
34.93	9.72	6.81	8.11	55.28	3.11	0.18	0.49
34.98	9.71	6.79	8.12	55.15	3.12	0.18	0.49
35.05	9.67	6.75	8.15	55.00	3.12	0.18	0.48
35.13	9.66	6.72	8.16	54.86	3.12	0.19	0.48
35.18	9.64	6.70	8.17	54.72	3.12	0.19	0.48
35.24	9.59	6.65	8.21	54.57	3.12	0.19	0.47
35.32	9.52	6.57	8.27	54.40	3.13	0.18	0.47
35.41	9.44	6.49	8.34	54.11	3.13	0.17	0.46
35.46	9.35	6.41	8.39	53.73	3.14	0.17	0.46
35.51	9.26	6.32	8.42	53.25	3.14	0.17	0.45
35.58	9.19	6.25	8.44	52.75	3.14	0.17	0.45
35.66	9.14	6.19	8.44	52.26	3.14	0.16	0.44
35.71	9.06	6.12	8.48	51.88	3.14	0.16	0.44
35.76	8.99	6.05	8.51	51.49	3.15	0.15	0.43
35.86	8.94	5.99	8.53	51.09	3.15	0.15	0.43
35.91	8.90	5.95	8.52	50.72	3.15	0.14	0.43
36.01	8.88	5.92	8.52	50.45	3.15	0.14	0.42
36.05	8.87	5.91	8.48	50.09	3.14	0.14	0.42
36.12	8.86	5.89	8.47	49.84	3.14	0.14	0.42
36.20	8.83	5.85	8.47	49.56	3.14	0.14	0.42
36.23	8.84	5.85	8.45	49.44	3.14	0.14	0.42
36.31	8.89	5.89	8.38	49.32	3.14	0.14	0.42
36.35	8.99	5.96	8.24	49.13	3.12	0.14	0.43
36.45	9.11	6.05	8.09	48.92	3.11	0.14	0.43
36.51	9.26	6.17	7.90	48.73	3.10	0.14	0.44
36.58	9.41	6.28	7.74	48.64	3.09	0.13	0.45
36.66	9.56	6.40	7.61	48.67	3.07	0.13	0.46
36.70	9.71	6.52	7.49	48.82	3.06	0.13	0.47
36.80	9.91	6.68	7.35	49.08	3.05	0.13	0.48
36.85	10.09	6.82	7.26	49.47	3.04	0.13	0.49
36.89	10.23	6.93	7.19	49.84	3.04	0.13	0.49
36.96	10.31	6.98	7.22	50.42	3.04	0.14	0.50
37.03	10.36	7.01	7.27	50.98	3.05	0.15	0.50
37.09	10.38	7.02	7.35	51.64	3.05	0.16	0.50
37.15	10.40	7.03	7.42	52.17	3.06	0.16	0.50
37.23	10.42	7.03	7.49	52.69	3.06	0.17	0.50
37.27	10.44	7.04	7.54	53.11	3.07	0.17	0.50
37.34	10.45	7.04	7.59	53.40	3.07	0.17	0.50
37.43	10.46	7.03	7.62	53.58	3.08	0.17	0.50
37.49	10.46	7.02	7.66	53.77	3.08	0.17	0.50
37.54	10.47	7.02	7.66	53.75	3.08	0.17	0.50
37.62	10.46	7.00	7.67	53.71	3.08	0.17	0.50
37.69	10.45	6.98	7.66	53.47	3.08	0.17	0.50
37.74	10.44	6.96	7.66	53.35	3.08	0.17	0.50
37.82	10.43	6.94	7.66	53.21	3.08	0.17	0.50

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
37.89	10.42	6.92	7.67	53.07	3.08	0.16	0.49
37.93	10.45	6.94	7.65	53.07	3.08	0.16	0.50
38.02	10.51	6.98	7.62	53.15	3.08	0.16	0.50
38.08	10.61	7.05	7.57	53.37	3.07	0.16	0.50
38.13	10.59	7.02	7.65	53.76	3.08	0.16	0.50
38.23	10.77	7.15	7.59	54.28	3.07	0.17	0.51
38.28	11.05	7.37	7.45	54.94	3.06	0.18	0.53
38.35	11.35	7.61	7.29	55.48	3.05	0.19	0.54
38.42	11.66	7.85	7.14	56.01	3.03	0.20	0.56
38.47	11.96	8.08	6.99	56.53	3.02	0.20	0.58
38.52	12.14	8.22	6.94	57.02	3.02	0.20	0.59
38.61	12.27	8.31	6.91	57.39	3.01	0.20	0.59
38.67	12.35	8.36	6.88	57.47	3.01	0.20	0.60
38.72	12.50	8.48	6.78	57.46	3.00	0.20	0.61
38.82	12.47	8.43	6.79	57.22	3.00	0.21	0.60
38.86	12.32	8.30	6.86	56.90	3.01	0.21	0.59
38.96	12.14	8.14	6.94	56.45	3.02	0.19	0.58
39.01	11.97	7.99	7.01	56.01	3.02	0.19	0.57
39.05	11.89	7.92	7.02	55.59	3.02	0.19	0.57
39.13	12.00	7.99	6.90	55.17	3.01	0.18	0.57
39.21	12.16	8.11	6.75	54.75	3.00	0.17	0.58
39.24	12.47	8.35	6.54	54.65	2.98	0.17	0.60
39.31	12.92	8.70	6.28	54.63	2.96	0.17	0.62
39.40	13.42	9.09	6.04	54.92	2.93	0.18	0.65
39.44	13.97	9.54	5.81	55.41	2.91	0.18	0.68
39.51	14.55	10.01	5.60	56.06	2.89	0.18	0.71
39.60	15.09	10.43	5.44	56.69	2.87	0.19	0.74
39.66	15.51	10.77	5.31	57.21	2.86	0.21	0.76
39.70	15.75	10.96	5.25	57.47	2.85	0.22	0.78
39.80	15.89	11.05	5.22	57.61	2.85	0.22	0.78
39.85	15.87	11.02	5.24	57.69	2.85	0.22	0.78
39.90	15.72	10.88	5.29	57.60	2.86	0.21	0.77
39.98	15.53	10.71	5.34	57.20	2.86	0.20	0.76
40.05	15.26	10.47	5.40	56.51	2.87	0.19	0.74
40.10	14.94	10.20	5.46	55.63	2.87	0.19	0.72
40.20	14.62	9.92	5.50	54.60	2.88	0.18	0.71
40.25	14.33	9.68	5.53	53.57	2.88	0.17	0.69
40.30	14.10	9.49	5.56	52.72	2.89	0.16	0.67
40.40	13.93	9.33	5.57	51.94	2.89	0.15	0.66
40.45	13.82	9.23	5.56	51.28	2.89	0.14	0.66
40.50	13.79	9.20	5.52	50.82	2.88	0.13	0.65
40.59	13.78	9.17	5.51	50.57	2.88	0.13	0.65
40.64	13.82	9.20	5.50	50.56	2.88	0.13	0.65
40.69	13.94	9.29	5.45	50.65	2.87	0.14	0.66
40.79	14.09	9.39	5.44	51.06	2.87	0.15	0.67
40.83	14.28	9.53	5.46	52.01	2.87	0.16	0.68
40.92	14.55	9.73	5.45	53.03	2.87	0.16	0.69
40.98	14.84	9.94	5.45	54.14	2.87	0.16	0.71

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
41.03	15.10	10.13	5.45	55.21	2.87	0.17	0.72
41.08	15.30	10.28	5.47	56.17	2.88	0.20	0.73
41.18	15.48	10.40	5.47	56.90	2.88	0.21	0.74
41.22	15.62	10.50	5.49	57.63	2.88	0.22	0.75
41.31	15.72	10.55	5.53	58.34	2.88	0.23	0.75
41.36	15.79	10.59	5.56	58.87	2.89	0.23	0.75
41.42	15.83	10.61	5.56	59.03	2.89	0.22	0.75
41.50	15.79	10.56	5.60	59.10	2.89	0.22	0.75
41.54	15.73	10.50	5.64	59.18	2.89	0.22	0.75
41.61	15.68	10.45	5.65	59.06	2.90	0.22	0.74
41.70	15.63	10.39	5.68	59.03	2.90	0.22	0.74
41.75	15.58	10.33	5.72	59.10	2.90	0.22	0.74
41.80	15.56	10.31	5.74	59.18	2.90	0.22	0.73
41.87	15.55	10.28	5.76	59.24	2.91	0.22	0.73
41.95	15.57	10.28	5.77	59.30	2.91	0.22	0.73
42.01	15.60	10.29	5.78	59.45	2.91	0.22	0.73
42.10	15.68	10.33	5.79	59.77	2.91	0.22	0.74
42.14	15.78	10.39	5.79	60.19	2.91	0.22	0.74
42.21	15.87	10.44	5.83	60.86	2.91	0.22	0.74
42.27	15.96	10.50	5.84	61.35	2.91	0.23	0.75
42.34	16.05	10.55	5.85	61.74	2.92	0.24	0.75
42.39	16.11	10.58	5.87	62.14	2.92	0.26	0.75
42.49	16.16	10.59	5.90	62.52	2.92	0.27	0.75
42.54	16.18	10.59	5.96	63.15	2.93	0.27	0.76
42.59	16.19	10.58	6.03	63.79	2.93	0.26	0.75
42.69	16.17	10.54	6.09	64.22	2.94	0.26	0.75
42.74	16.12	10.49	6.13	64.28	2.94	0.26	0.75
42.80	16.08	10.44	6.15	64.17	2.94	0.28	0.75
42.89	16.02	10.38	6.17	64.05	2.95	0.29	0.74
42.93	15.90	10.27	6.23	63.95	2.95	0.29	0.73
42.99	15.79	10.18	6.27	63.77	2.96	0.26	0.73
43.08	15.64	10.04	6.31	63.41	2.96	0.26	0.72
43.11	15.45	9.89	6.35	62.83	2.96	0.26	0.71
43.18	15.16	9.66	6.41	61.98	2.97	0.25	0.69
43.28	14.77	9.35	6.52	60.93	2.98	0.24	0.67
43.35	14.40	9.05	6.63	60.05	2.99	0.22	0.65
43.38	13.95	8.71	6.78	59.07	3.00	0.22	0.62
43.45	13.50	8.36	6.92	57.87	3.02	0.21	0.60
43.53	13.09	8.04	7.04	56.63	3.03	0.19	0.57
43.58	12.64	7.70	7.19	55.36	3.04	0.19	0.55
43.64	12.18	7.34	7.39	54.23	3.06	0.18	0.52
43.73	11.74	7.00	7.58	53.06	3.07	0.16	0.50
43.78	11.44	6.77	7.69	52.10	3.08	0.15	0.48
43.84	11.29	6.65	7.75	51.55	3.09	0.14	0.48
43.92	11.24	6.61	7.75	51.21	3.09	0.14	0.47
43.98	11.42	6.73	7.58	51.04	3.07	0.14	0.48
44.07	11.69	6.92	7.44	51.48	3.06	0.14	0.49
44.12	12.61	7.59	6.96	52.80	3.02	0.16	0.54

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
44.17	13.58	8.30	6.53	54.21	2.98	0.16	0.59
44.23	15.30	9.59	5.82	55.83	2.91	0.16	0.68
44.29	16.73	10.69	5.38	57.49	2.87	0.18	0.76
44.39	17.65	11.39	5.08	57.91	2.83	0.24	0.80
44.43	18.07	11.71	4.96	58.02	2.82	0.24	0.83
44.49	18.39	11.95	4.84	57.87	2.81	0.26	0.84
44.57	18.26	11.83	4.87	57.59	2.81	0.28	0.83
44.67	17.84	11.49	4.94	56.71	2.82	0.18	0.81
44.73	16.78	10.65	5.18	55.13	2.84	0.17	0.75
44.78	15.68	9.81	5.43	53.28	2.87	0.15	0.70
44.82	13.89	8.43	6.03	50.86	2.93	0.14	0.60
44.93	12.37	7.28	6.57	47.87	2.98	0.11	0.52
44.97	11.32	6.51	7.09	46.15	3.03	0.10	0.46
45.02	10.69	6.04	7.40	44.73	3.06	0.09	0.43
45.09	10.06	5.58	7.79	43.44	3.09	0.09	0.40
45.17	9.74	5.34	7.95	42.46	3.10	0.08	0.38
45.22	9.67	5.28	7.96	42.05	3.10	0.08	0.38
45.30	9.64	5.25	7.93	41.64	3.10	0.09	0.38
45.37	9.63	5.24	7.90	41.37	3.10	0.09	0.37
45.42	9.61	5.22	7.90	41.23	3.10	0.09	0.37
45.50	9.60	5.20	7.90	41.08	3.10	0.09	0.37
45.57	9.58	5.18	7.92	41.05	3.10	0.08	0.37
45.61	9.57	5.17	7.92	40.91	3.10	0.08	0.37
45.72	9.57	5.15	7.91	40.75	3.10	0.08	0.37
45.77	9.54	5.12	7.95	40.73	3.10	0.07	0.37
45.80	9.61	5.17	7.93	41.00	3.10	0.08	0.37
45.88	9.73	5.25	7.91	41.54	3.10	0.08	0.37
45.96	9.95	5.40	7.81	42.23	3.09	0.08	0.39
46.01	10.26	5.62	7.64	42.93	3.08	0.09	0.40
46.11	10.60	5.85	7.45	43.61	3.06	0.10	0.42
46.14	10.90	6.06	7.28	44.16	3.05	0.11	0.43
46.21	11.13	6.22	7.18	44.66	3.04	0.11	0.44
46.26	11.36	6.38	7.10	45.27	3.03	0.11	0.46
46.35	11.59	6.53	7.02	45.86	3.02	0.11	0.47
46.41	11.79	6.67	6.90	45.99	3.01	0.11	0.48
46.49	11.97	6.79	6.76	45.89	3.00	0.11	0.48
46.55	12.02	6.82	6.70	45.65	3.00	0.11	0.49
46.59	12.02	6.81	6.70	45.64	3.00	0.12	0.49
46.68	12.03	6.81	6.79	46.18	3.00	0.11	0.49
46.74	12.21	6.93	6.78	46.96	3.00	0.10	0.49
46.80	12.54	7.15	6.63	47.42	2.99	0.10	0.51
46.85	12.84	7.36	6.55	48.18	2.98	0.11	0.53
46.93	13.10	7.53	6.54	49.23	2.98	0.14	0.54
47.00	13.25	7.62	6.66	50.73	2.99	0.16	0.54
47.10	13.37	7.69	6.79	52.26	3.00	0.13	0.55
47.15	13.58	7.83	6.82	53.39	3.01	0.16	0.56
47.20	13.74	7.94	6.80	53.94	3.00	0.19	0.57
47.25	13.87	8.02	6.69	53.66	3.00	0.21	0.57

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
47.31	13.67	7.87	6.72	52.88	3.00	0.21	0.56
47.40	13.24	7.56	6.90	52.16	3.01	0.18	0.54
47.44	12.78	7.23	7.05	50.94	3.03	0.15	0.52
47.52	12.43	6.97	7.06	49.18	3.03	0.12	0.50
47.58	12.04	6.69	7.03	47.03	3.03	0.10	0.48
47.67	11.69	6.43	6.96	44.74	3.02	0.08	0.46
47.73	11.28	6.14	6.97	42.78	3.02	0.08	0.44
47.78	11.00	5.93	6.95	41.22	3.02	0.07	0.42
47.86	10.70	5.71	7.05	40.24	3.03	0.07	0.41
47.92	10.61	5.64	7.08	39.94	3.03	0.07	0.40
47.98	10.65	5.66	7.12	40.33	3.03	0.07	0.40
48.05	10.75	5.72	7.18	41.11	3.04	0.07	0.41
48.12	10.88	5.81	7.25	42.11	3.04	0.07	0.42
48.19	11.29	6.09	7.18	43.74	3.04	0.08	0.43
48.27	11.81	6.44	7.02	45.19	3.02	0.10	0.46
48.32	12.54	6.94	6.70	46.49	3.00	0.12	0.50
48.39	13.52	7.61	6.21	47.30	2.95	0.13	0.54
48.47	14.52	8.34	5.76	48.00	2.91	0.16	0.59
48.52	15.76	9.26	5.23	48.43	2.85	0.15	0.65
48.57	17.08	10.24	4.73	48.45	2.79	0.15	0.72
48.67	18.11	11.01	4.38	48.22	2.75	0.12	0.77
48.71	18.94	11.63	4.15	48.22	2.72	0.11	0.81
48.76	19.21	11.82	4.10	48.49	2.71	0.11	0.82
48.82	19.64	12.12	4.06	49.25	2.71	0.11	0.84
48.93	19.63	12.06	4.21	50.82	2.73	0.11	0.84
48.97	19.53	11.93	4.49	53.58	2.76	0.13	0.83
49.05	19.43	11.79	4.80	56.59	2.80	0.18	0.83
49.08	19.57	11.84	5.07	60.05	2.83	0.21	0.83
49.16	19.78	11.92	5.36	63.92	2.86	0.25	0.84
49.25	20.34	12.26	5.56	68.19	2.89	0.32	0.87
49.29	21.10	12.75	5.71	72.88	2.90	0.91	0.91
49.36	22.50	13.70	5.71	78.16	2.90	0.97	0.97
49.43	24.24	14.90	5.58	83.10	2.89	1.06	1.06
49.48	26.47	16.49	5.29	87.16	2.86	1.16	1.16
49.55	28.64	18.03	5.00	90.13	2.82	1.27	1.27
49.64	30.67	19.47	4.75	92.56	2.80	1.36	1.36
49.70	32.09	20.47	4.63	94.76	2.78	1.43	1.43
49.75	33.34	21.35	4.53	96.70	2.77	1.49	1.49
49.81	34.56	22.21	4.41	98.00	2.75	1.55	1.55
49.90	35.75	23.04	4.31	99.36	2.74	1.60	1.60
49.94	36.62	23.66	4.23	100.04	2.73	1.64	1.64
50.01	36.53	23.55	4.26	100.43	2.74	1.64	1.64
50.08	36.09	23.18	4.35	100.85	2.75	1.61	1.61
50.15	35.37	22.60	4.48	101.32	2.76	1.58	1.58
50.24	35.40	22.57	4.50	101.61	2.77	1.57	1.57
50.30	35.75	22.81	4.44	101.22	2.76	1.59	1.59
50.34	35.97	22.97	4.36	100.26	2.75	1.60	1.60
50.41	36.05	23.02	4.31	99.21	2.74	1.60	1.60

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
50.47	35.82	22.86	4.24	96.84	2.73	1.59	1.59
50.54	35.56	22.69	4.14	93.92	2.72	1.57	1.57
50.62	35.51	22.67	4.01	90.88	2.70	1.57	1.57
50.66	35.50	22.71	3.86	87.61	2.68	1.56	1.56
50.77	35.54	22.76	3.71	84.35	2.66	1.56	1.56
50.81	34.91	22.33	3.64	81.27	2.65	1.53	1.53
50.87	34.13	21.78	3.61	78.68	2.64	1.49	1.49
50.92	33.49	21.33	3.59	76.51	2.64	1.46	1.46
51.01	33.00	20.97	3.55	74.48	2.64	1.44	1.44
51.07	32.79	20.82	3.52	73.21	2.63	1.42	1.42
51.15	32.62	20.69	3.49	72.16	2.63	1.41	1.41
51.21	32.54	20.62	3.47	71.53	2.62	1.41	1.41
51.26	32.61	20.65	3.46	71.37	2.62	1.41	1.41
51.32	32.80	20.78	3.44	71.50	2.62	1.42	1.42
51.39	33.10	20.97	3.42	71.79	2.62	1.43	1.43
51.46	33.33	21.10	3.42	72.21	2.62	1.44	1.44
51.53	33.60	21.26	3.42	72.69	2.61	1.45	1.45
51.61	33.87	21.42	3.42	73.16	2.61	1.46	1.46
51.65	34.13	21.59	3.41	73.51	2.61	1.47	1.47
51.72	34.43	21.78	3.39	73.79	2.61	1.48	1.48
51.81	34.80	22.01	3.36	73.92	2.61	1.50	1.50
51.84	35.11	22.23	3.33	74.03	2.60	1.51	1.51
51.92	35.39	22.40	3.30	74.01	2.60	0.64	0.64
52.01	35.65	22.56	3.28	73.92	2.59	0.64	0.64
52.06	35.90	22.73	3.25	73.80	2.59	0.64	0.64
52.11	36.16	22.91	3.21	73.61	2.58	0.64	0.64
52.19	36.34	23.01	3.19	73.49	2.58	0.64	0.64
52.25	36.53	23.13	3.18	73.49	2.58	0.64	0.64
52.30	36.76	23.27	3.16	73.61	2.57	0.64	0.64
52.38	37.02	23.43	3.15	73.88	2.57	0.64	0.64
52.45	37.28	23.58	3.15	74.22	2.57	0.64	0.64
52.49	37.54	23.75	3.14	74.68	2.57	0.64	0.64
52.57	37.71	23.83	3.15	75.13	2.57	0.64	0.64
52.65	37.81	23.86	3.17	75.60	2.57	0.64	0.64
52.70	37.59	23.66	3.21	76.02	2.58	0.64	0.64
52.79	37.34	23.43	3.25	76.26	2.59	0.64	0.64
52.85	36.98	23.14	3.30	76.30	2.60	0.64	0.64
52.89	36.45	22.74	3.34	75.93	2.60	1.54	1.54
52.99	35.72	22.19	3.38	75.10	2.61	1.51	1.51
53.04	34.87	21.58	3.42	73.90	2.62	1.47	1.47
53.08	33.84	20.84	3.48	72.53	2.62	1.42	1.42
53.17	32.85	20.12	3.53	70.98	2.63	1.37	1.37
53.24	31.89	19.44	3.56	69.26	2.64	0.33	1.32
53.33	31.20	18.95	3.57	67.56	2.64	0.29	1.29
53.39	30.55	18.50	3.57	65.95	2.64	0.28	1.26
53.42	29.84	18.00	3.58	64.53	2.64	0.27	1.23
53.49	29.22	17.56	3.62	63.51	2.65	0.25	1.20
53.58	28.69	17.16	3.66	62.88	2.65	0.25	1.17

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
53.63	28.25	16.83	3.73	62.80	2.66	0.25	1.15
53.68	28.03	16.65	3.79	63.10	2.67	0.25	1.14
53.77	27.89	16.51	3.86	63.72	2.68	0.26	1.13
53.83	27.75	16.37	3.95	64.62	2.69	0.27	1.12
53.88	27.65	16.26	4.04	65.69	2.71	0.28	1.12
53.97	27.58	16.15	4.14	66.86	2.72	0.30	1.11
54.03	27.65	16.16	4.21	68.06	2.73	0.32	1.12
54.08	27.92	16.32	4.23	69.02	2.73	0.33	1.13
54.18	28.22	16.49	4.23	69.69	2.73	0.35	1.14
54.22	28.55	16.70	4.21	70.24	2.73	1.15	1.15
54.27	28.86	16.89	4.18	70.60	2.72	1.16	1.16
54.38	29.20	17.09	4.15	70.87	2.72	1.18	1.18
54.42	29.60	17.33	4.18	72.48	2.73	1.19	1.19
54.47	30.18	17.68	4.22	74.54	2.73	1.22	1.22
54.57	30.74	17.99	4.27	76.80	2.74	1.24	1.24
54.61	32.49	19.15	4.16	79.62	2.72	1.32	1.32
54.68	34.47	20.44	4.09	83.61	2.71	1.41	1.41
54.75	36.91	22.04	4.00	88.19	2.70	1.51	1.51
54.79	39.58	23.80	3.90	92.93	2.69	1.63	1.63
54.86	42.54	25.75	3.80	97.96	2.67	1.76	1.76
54.95	45.89	27.95	3.70	103.54	2.66	1.90	1.90
55.01	49.55	30.41	3.55	108.09	2.64	2.06	2.06
55.06	53.33	32.97	3.41	112.42	2.61	2.23	2.23
55.12	57.74	35.97	3.25	116.75	2.59	0.69	0.69
55.21	61.55	38.53	3.13	120.57	2.57	0.70	0.70
55.25	64.95	40.86	3.02	123.48	2.55	0.71	0.71
55.32	67.67	42.71	2.94	125.59	2.53	0.71	0.71
55.40	69.32	43.79	2.90	126.89	2.52	0.72	0.72
55.50	69.77	44.02	2.89	127.13	2.52	0.72	0.72
55.52	68.79	43.32	2.91	126.29	2.53	0.72	0.72
55.60	66.93	41.97	2.98	124.98	2.54	0.71	0.71
55.67	64.58	40.27	3.06	123.13	2.55	0.71	0.71
55.72	61.65	38.22	3.16	120.61	2.57	0.70	0.70
55.79	58.07	35.70	3.29	117.52	2.59	0.69	0.69
55.86	54.37	33.13	3.44	114.05	2.62	2.24	2.24
55.95	50.44	30.41	3.62	110.07	2.65	2.06	2.06
56.00	47.04	28.08	3.79	106.54	2.67	1.91	1.91
56.05	44.22	26.16	3.96	103.47	2.69	1.79	1.79
56.11	42.29	24.85	4.05	100.71	2.71	1.70	1.70
56.19	40.82	23.87	4.10	97.89	2.71	1.64	1.64
56.24	39.25	22.82	4.16	94.95	2.72	1.57	1.57
56.34	37.48	21.62	4.25	92.00	2.73	1.49	1.49
56.37	35.77	20.49	4.37	89.45	2.75	1.41	1.41
56.43	34.28	19.49	4.46	87.00	2.76	1.35	1.35
56.54	33.15	18.72	4.55	85.17	2.77	1.30	1.30
56.59	32.27	18.14	4.58	83.05	2.78	1.26	1.26
56.64	31.50	17.66	4.56	80.45	2.77	1.22	1.22
56.73	30.75	17.17	4.53	77.84	2.77	1.19	1.19

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
56.79	29.94	16.66	4.53	75.39	2.77	1.15	1.15
56.84	29.45	16.36	4.46	73.04	2.76	1.13	1.13
56.93	29.13	16.17	4.37	70.74	2.75	1.12	1.12
56.96	28.72	15.94	4.29	68.35	2.74	0.30	1.10
57.03	28.18	15.60	4.24	66.11	2.73	0.29	1.07
57.13	27.59	15.23	4.21	64.05	2.73	0.26	1.05
57.16	27.05	14.88	4.19	62.33	2.73	0.25	1.02
57.23	26.67	14.63	4.19	61.35	2.73	0.23	1.00
57.29	26.39	14.44	4.20	60.68	2.73	0.21	0.99
57.38	26.31	14.38	4.17	60.04	2.72	0.21	0.99
57.42	26.37	14.42	4.15	59.82	2.72	0.21	0.99
57.49	26.54	14.51	4.14	60.12	2.72	0.21	0.99
57.57	26.67	14.57	4.16	60.64	2.72	0.24	1.00
57.62	26.59	14.49	4.22	61.18	2.73	0.23	0.99
57.68	26.52	14.41	4.28	61.64	2.74	0.24	0.99
57.77	26.34	14.25	4.36	62.10	2.75	0.28	0.98
57.85	26.02	14.01	4.47	62.58	2.76	0.27	0.97
57.92	25.63	13.72	4.56	62.60	2.77	0.26	0.95
57.97	25.13	13.37	4.67	62.43	2.79	0.25	0.93
58.02	24.52	12.97	4.77	61.87	2.80	0.25	0.90
58.07	23.81	12.50	4.87	60.83	2.81	0.25	0.87
58.16	23.20	12.09	4.95	59.82	2.82	0.24	0.84
58.23	22.77	11.81	5.00	59.00	2.82	0.21	0.82
58.31	22.40	11.56	5.04	58.29	2.83	0.19	0.81
58.37	22.16	11.40	5.05	57.57	2.83	0.18	0.80
58.42	22.06	11.33	5.03	57.06	2.83	0.18	0.79
58.50	22.07	11.33	5.02	56.90	2.83	0.19	0.79
58.57	22.16	11.37	5.02	57.09	2.83	0.19	0.79
58.61	22.31	11.45	5.05	57.78	2.83	0.19	0.80
58.68	22.68	11.65	5.10	59.42	2.84	0.21	0.81
58.76	23.31	11.99	5.16	61.90	2.84	0.22	0.84
58.80	24.38	12.62	5.14	64.88	2.84	0.23	0.88
58.87	25.76	13.44	5.10	68.50	2.84	0.24	0.94
58.95	26.94	14.12	5.12	72.34	2.84	0.99	0.99
59.01	29.48	15.68	4.92	77.17	2.82	1.09	1.09
59.06	32.30	17.44	4.67	81.48	2.79	1.21	1.21
59.16	35.49	19.45	4.37	84.96	2.75	1.34	1.34
59.19	38.57	21.43	4.10	87.83	2.71	1.46	1.46
59.29	40.88	22.89	3.93	90.03	2.69	1.56	1.56
59.33	42.63	24.01	3.82	91.61	2.67	1.63	1.63
59.39	43.82	24.76	3.73	92.47	2.66	1.68	1.68
59.47	44.76	25.38	3.64	92.27	2.65	1.71	1.71
59.54	45.65	25.98	3.51	91.18	2.63	1.75	1.75
59.58	44.87	25.51	3.48	88.87	2.63	1.71	1.71
59.65	43.24	24.45	3.53	86.35	2.63	1.64	1.64
59.73	40.72	22.76	3.72	84.64	2.66	1.54	1.54
59.81	38.24	21.07	3.98	83.87	2.70	1.43	1.43
59.85	36.61	20.12	3.91	78.60	2.69	1.37	1.37

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
59.92	35.57	19.57	3.73	72.90	2.66	1.32	1.32
59.99	35.26	19.53	3.43	67.02	2.62	0.43	1.31
60.08	35.07	19.57	3.13	61.24	2.57	0.10	0.62
60.13	35.05	19.76	2.82	55.82	2.51	0.07	0.62
60.18	35.20	20.10	2.51	50.35	2.44	0.06	0.62
60.27	35.91	20.86	2.16	44.99	2.36	0.05	0.63
60.33	37.42	22.37	1.00	22.37	2.23	0.03	0.64
60.38	38.51	-1.00	1.00	-1.00	-1.00	N/A	N/A
60.47	38.91	-1.00	1.00	-1.00	-1.00	N/A	N/A

Abbreviations

q_t:	Total cone resistance
K_c:	Cone resistance correction factor due to fines
$Q_{tn,cs}$:	Adjusted and corrected cone resistance due to fines
I_c:	Soil behavior type index
$S_{u(liq)}/\sigma'_v$:	Calculated liquefied undrained strength ratio
$S_{u(peak)}/\sigma'_v$:	Calculated peak undrained strength ratio

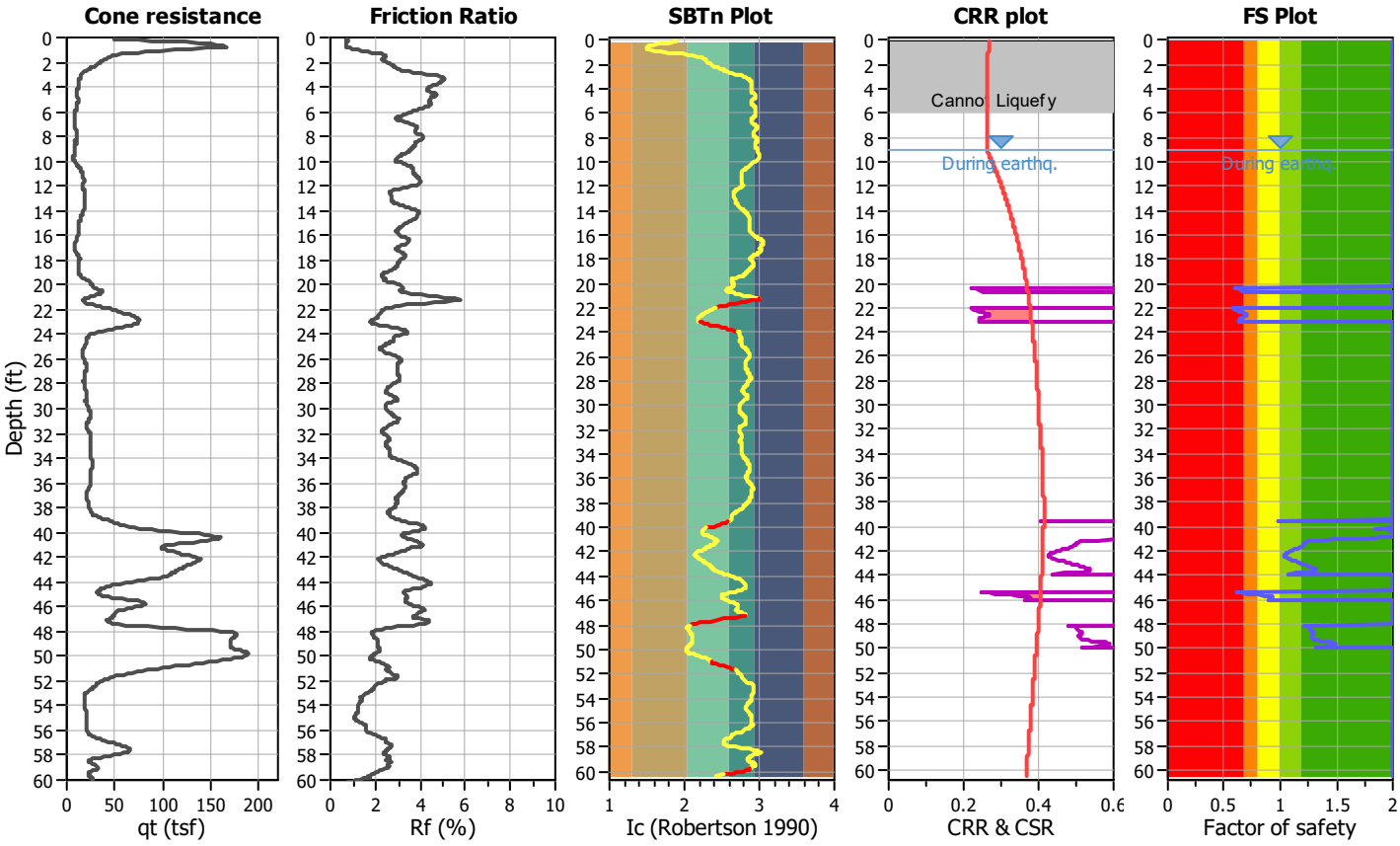
LIQUEFACTION ANALYSIS REPORT

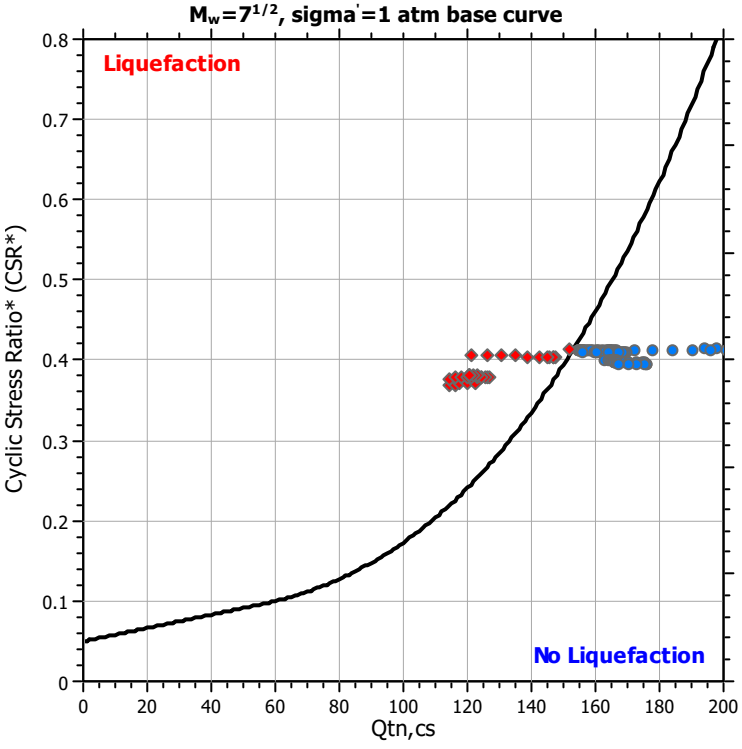
Project title : W1301-06-01 **Location : Perry Street**

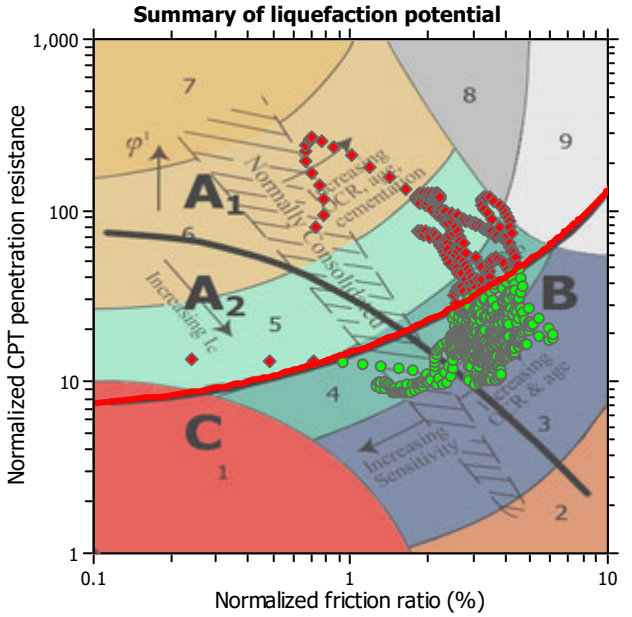
CPT file : CPT-5

Input parameters and analysis data

Analysis method:	NCEER (1998)	G.W.T. (in-situ):	12.00 ft	Use fill:	No	Clay like behavior applied:	Sands only
Fines correction method:	NCEER (1998)	G.W.T. (earthq.):	9.00 ft	Fill height:	N/A	Limit depth applied:	Yes
Points to test:	Based on Ic value	Average results interval:	.	Fill weight:	N/A	Limit depth:	50.00 ft
Earthquake magnitude M_w:	6.68	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	MSF method:	Method based
Peak ground acceleration:	0.55	Unit weight calculation:	Based on SBT	K_σ applied:	Yes		

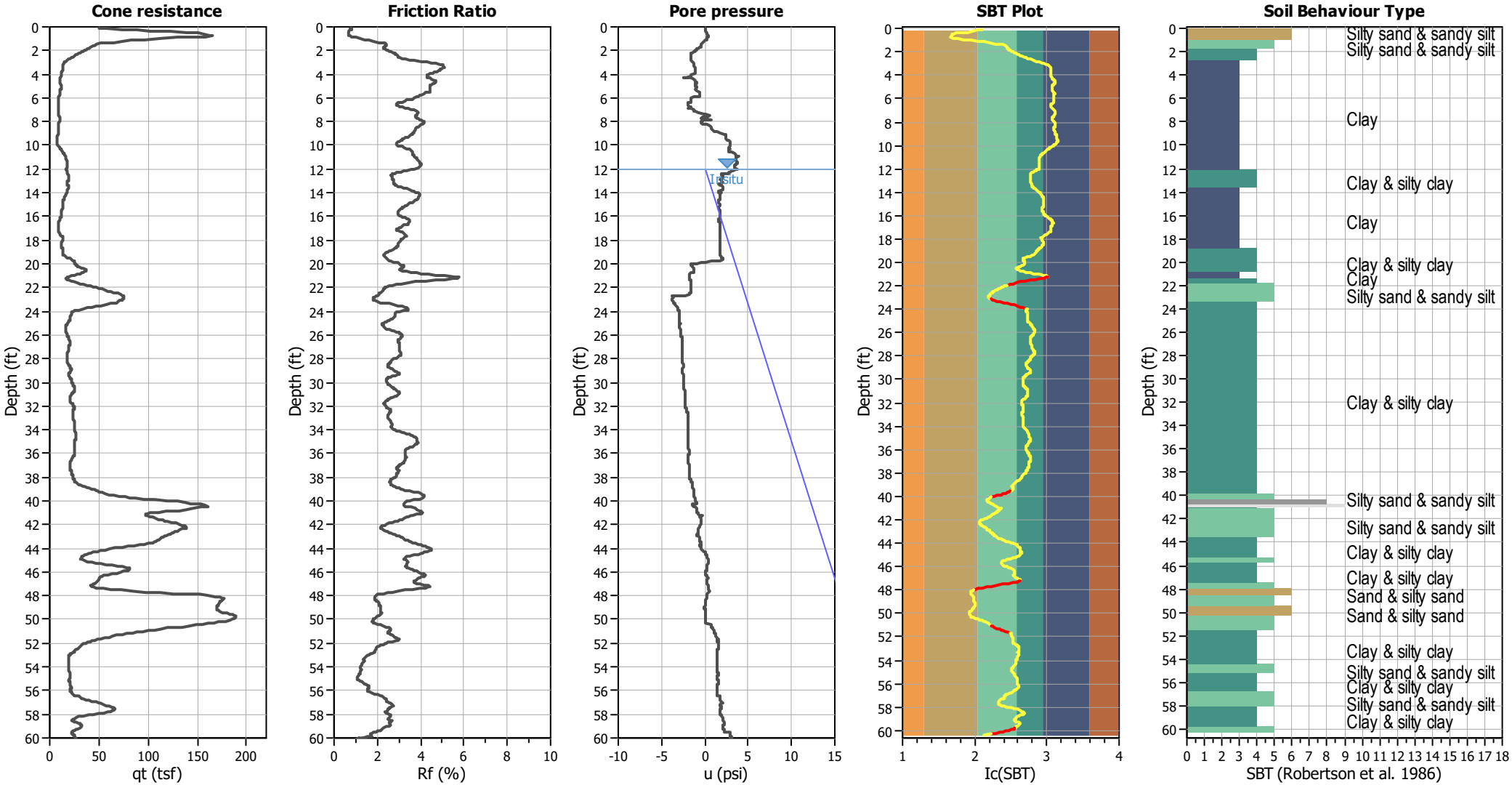






Zone A_1: Cyclic liquefaction likely depending on size and duration of cyclic loading
Zone A_2: Cyclic liquefaction and strength loss likely depending on loading and ground geometry
Zone B: Liquefaction and post-earthquake strength loss unlikely, check cyclic softening
Zone C: Cyclic liquefaction and strength loss possible depending on soil plasticity, brittleness/sensitivity, strain to peak undrained strength and ground geometry

CPT basic interpretation plots



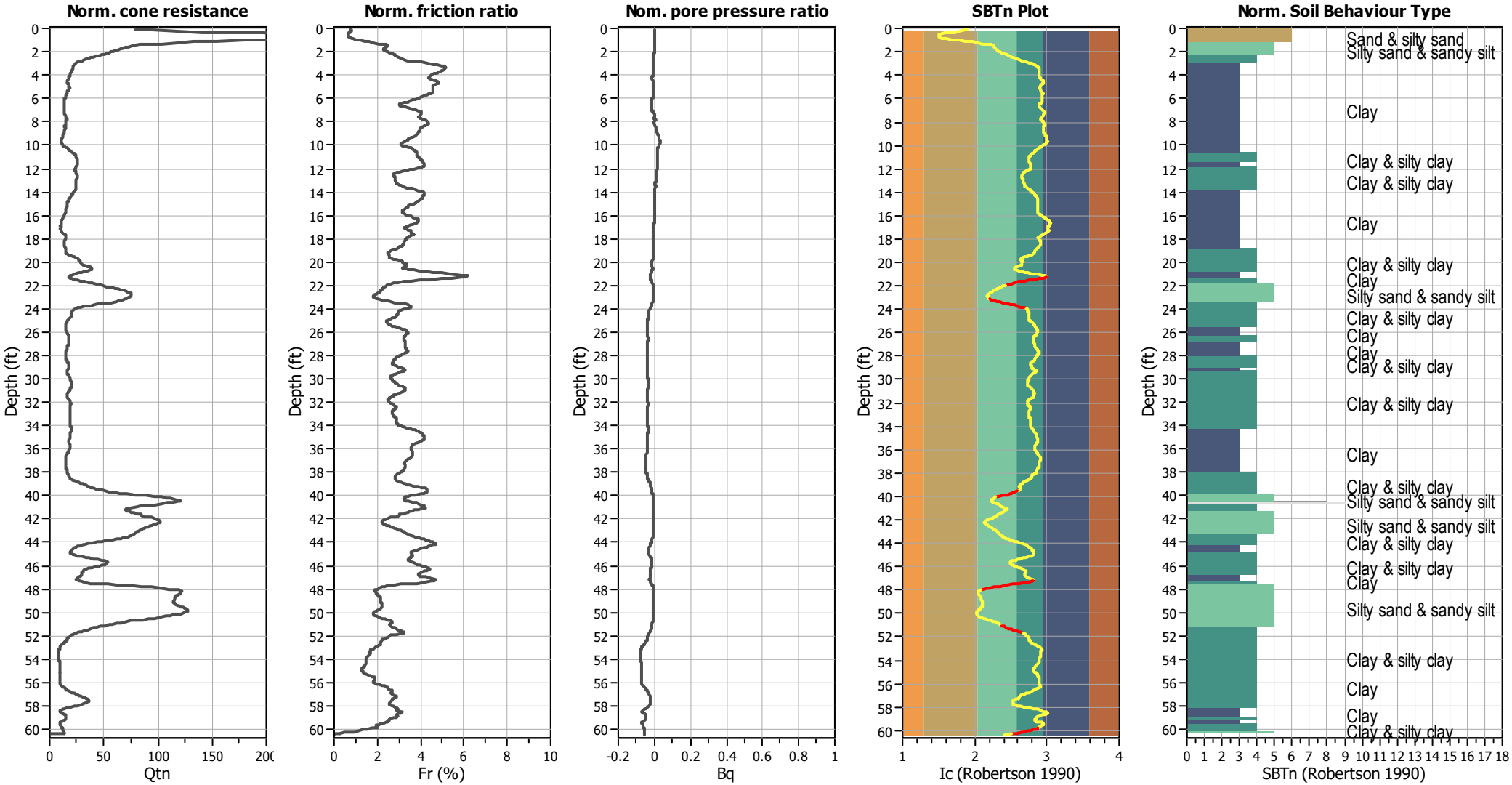
Input parameters and analysis data

Analysis method:	NCEER (1998)	Depth to water table (erthq.):	9.00 ft	Fill weight:	N/A
Fines correction method:	NCEER (1998)	Average results interval:	.	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.68	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.55	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	12.00 ft	Fill height:	N/A	Limit depth:	50.00 ft

SBT legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to
9. Very stiff fine grained

CPT basic interpretation plots (normalized)



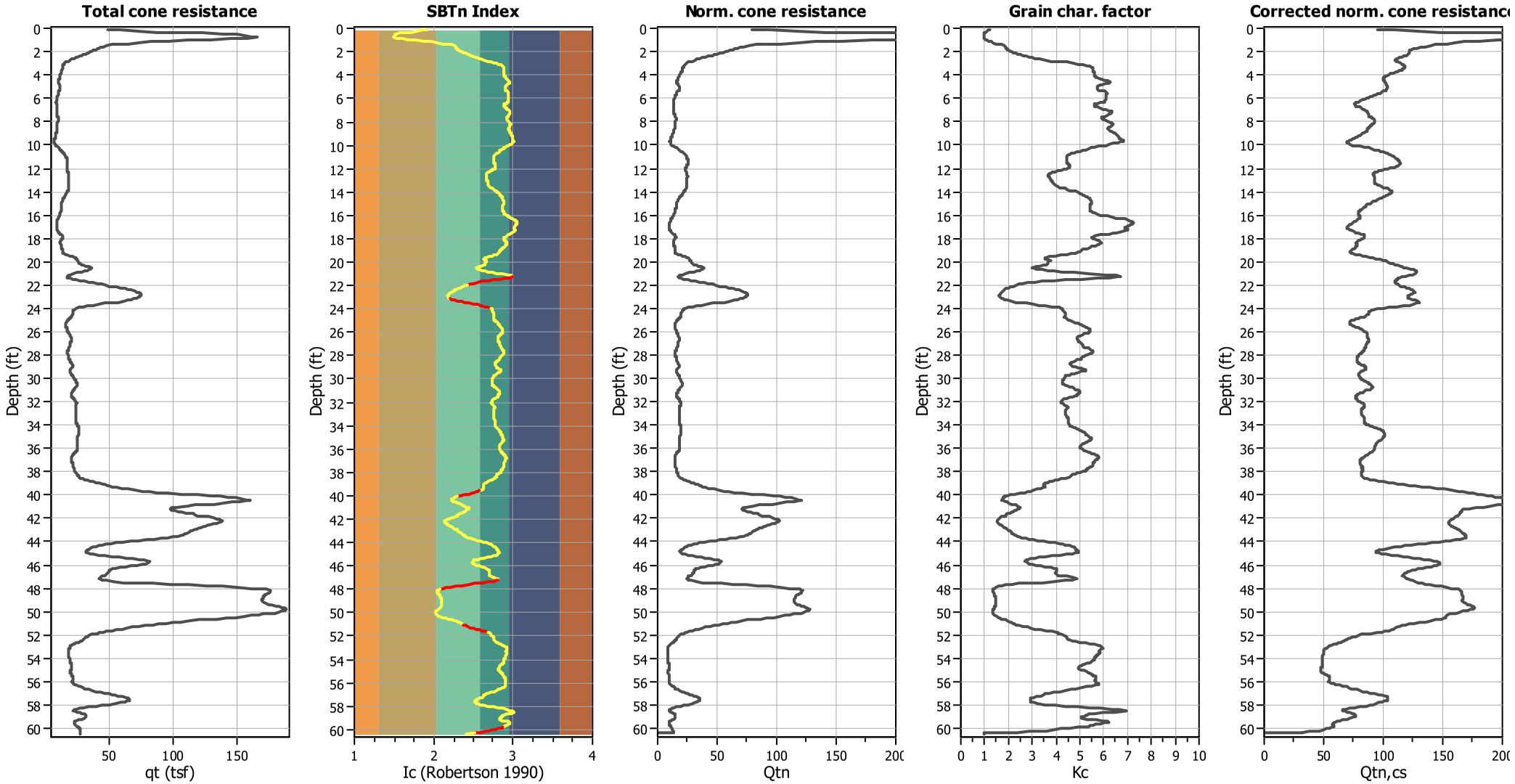
Input parameters and analysis data

Analysis method:	NCEER (1998)	Depth to water table (erthq.):	9.00 ft	Fill weight:	N/A
Fines correction method:	NCEER (1998)	Average results interval:	.	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.68	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.55	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	12.00 ft	Fill height:	N/A	Limit depth:	50.00 ft

SBTn legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to
9. Very stiff fine grained

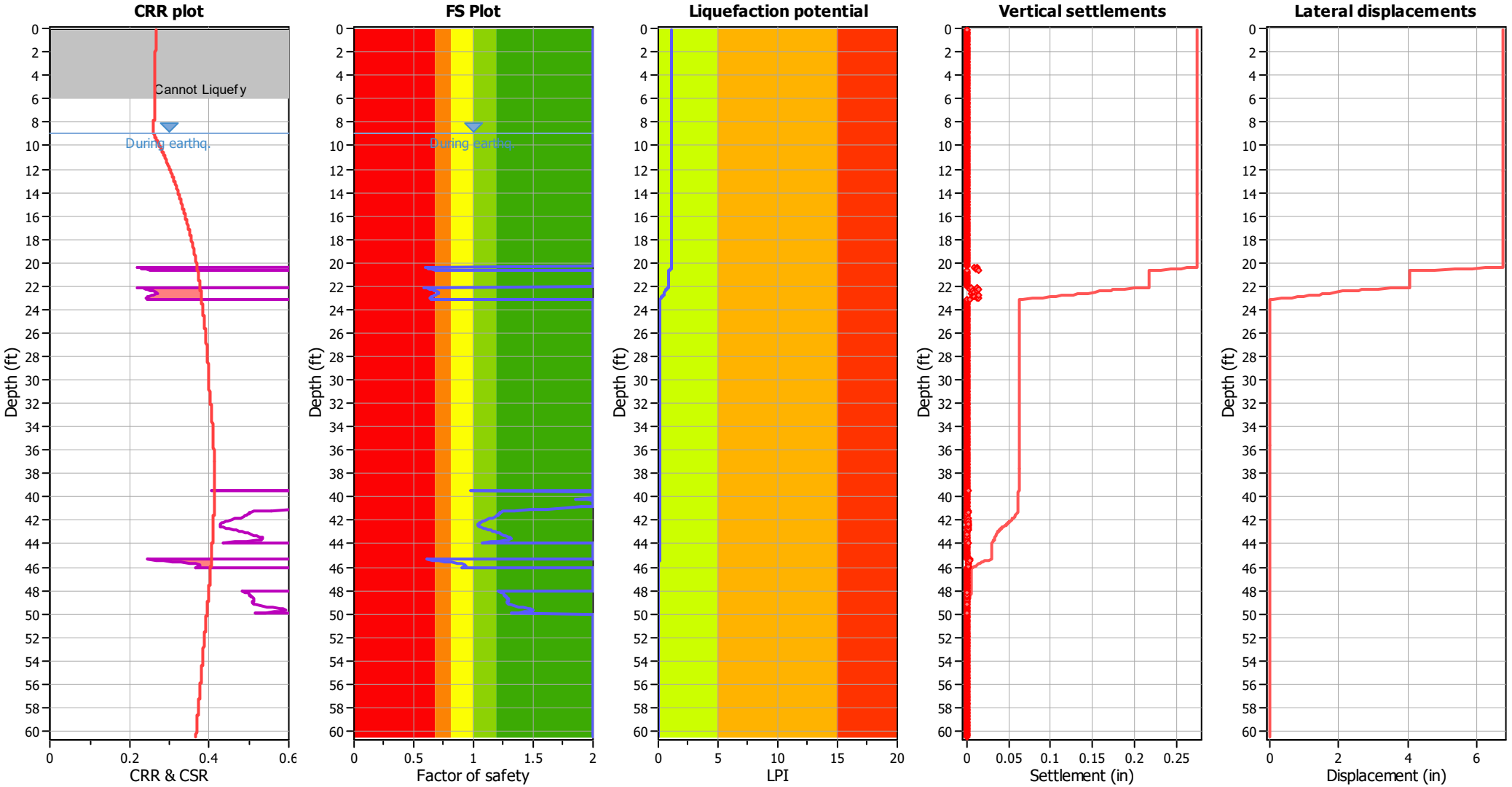
Liquefaction analysis overall plots (intermediate results)



Input parameters and analysis data

Analysis method:	NCEER (1998)	Depth to water table (erthq.):	9.00 ft	Fill weight:	N/A
Fines correction method:	NCEER (1998)	Average results interval:	.	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.68	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.55	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	12.00 ft	Fill height:	N/A	Limit depth:	50.00 ft

Liquefaction analysis overall plots



Input parameters and analysis data

Analysis method:	NCEER (1998)	Depth to water table (erthq.):	9.00 ft	Fill weight:	N/A
Fines correction method:	NCEER (1998)	Average results interval:	.	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.68	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.55	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	12.00 ft	Fill height:	N/A	Limit depth:	50.00 ft

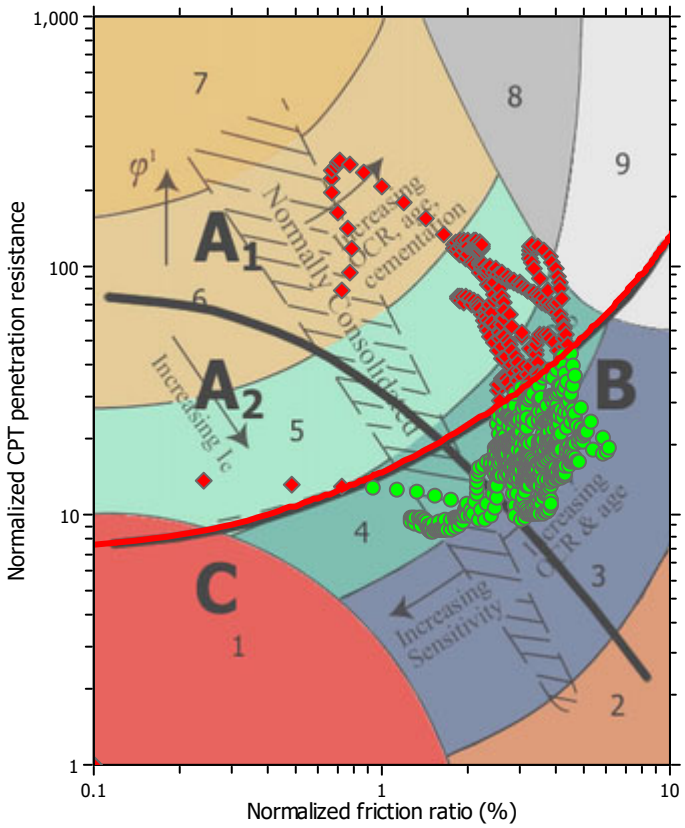
F.S. color scheme

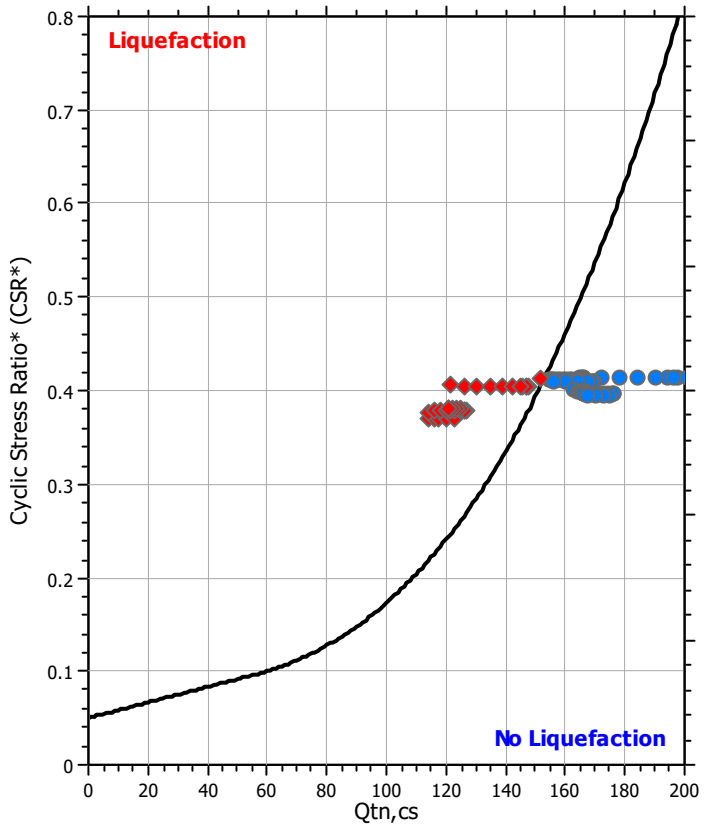
- Almost certain it will liquefy
- Very likely to liquefy
- Liquefaction and no liq. are equally likely
- Unlike to liquefy
- Almost certain it will not liquefy

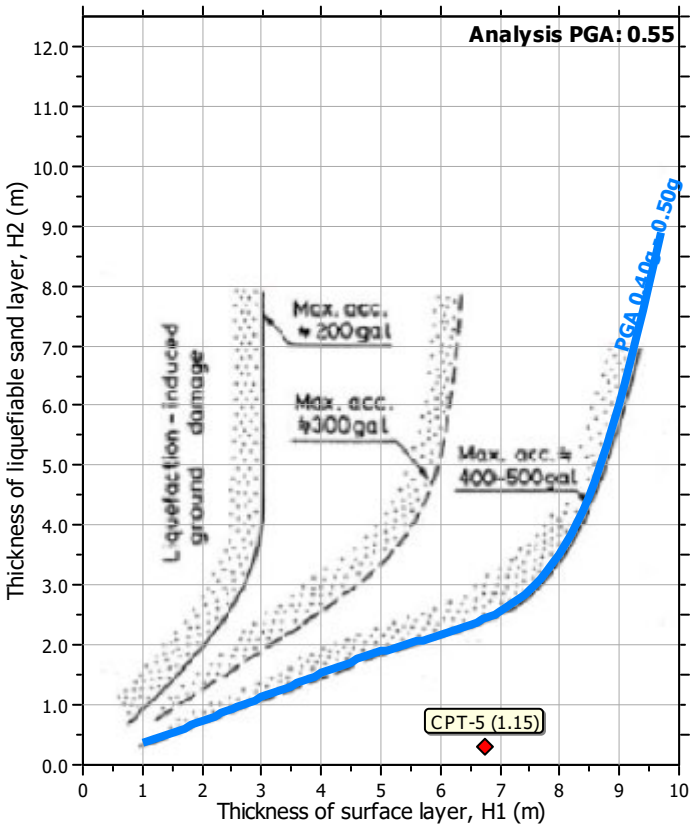
LPI color scheme

- Very high risk
- High risk
- Low risk

Liquefaction analysis summary plots



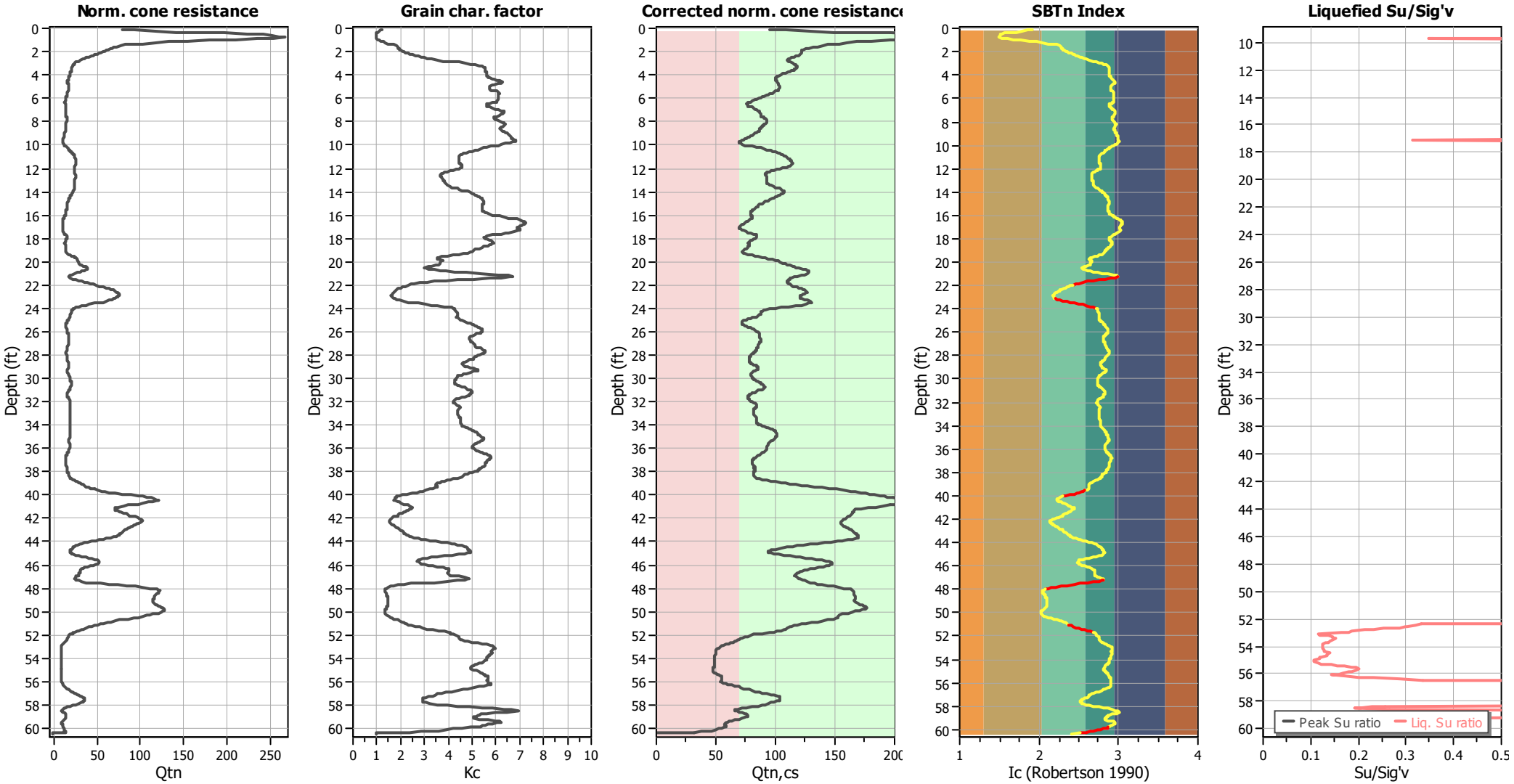




Input parameters and analysis data

Analysis method:	NCEER (1998)	Depth to water table (erthq.):	9.00 ft	Fill weight:	N/A
Fines correction method:	NCEER (1998)	Average results interval:	.	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.68	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.55	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	12.00 ft	Fill height:	N/A	Limit depth:	50.00 ft

Check for strength loss plots (Robertson (2010))



Input parameters and analysis data

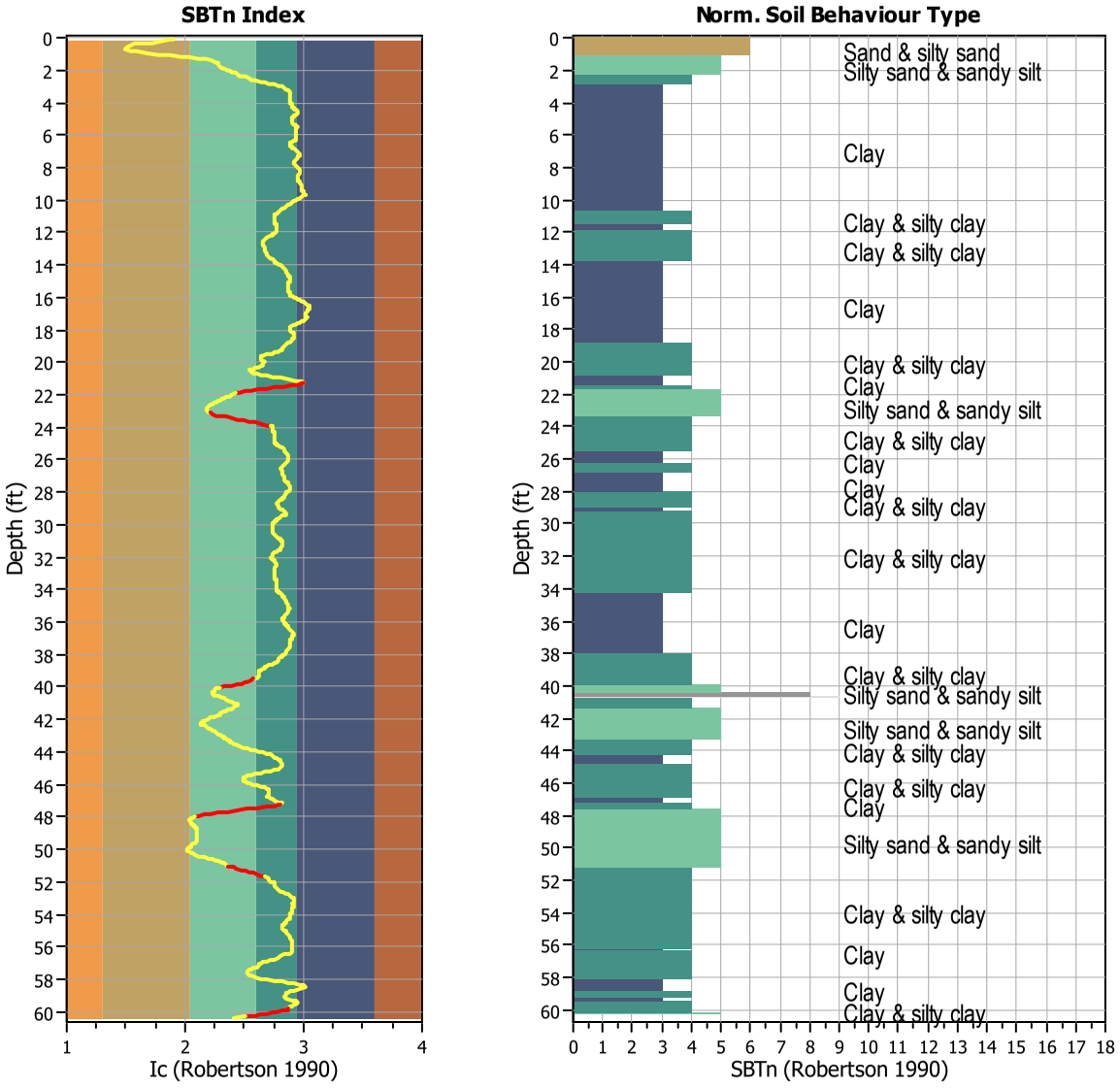
Analysis method:	NCEER (1998)	Depth to water table (erthq.):	9.00 ft	Fill weight:	N/A
Fines correction method:	NCEER (1998)	Average results interval:	.	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.68	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.55	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	12.00 ft	Fill height:	N/A	Limit depth:	50.00 ft

TRANSITION LAYER DETECTION ALGORITHM REPORT
Summary Details & Plots

Short description

The software will delete data when the cone is in transition from either clay to sand or vise-versa. To do this the software requires a range of I_c values over which the transition will be defined (typically somewhere between 1.80 < I_c < 3.0) and a rate of change of I_c. Transitions typically occur when the rate of change of I_c is fast (i.e. delta I_c is small).

The SBT_n plot below, displays in red the detected transition layers based on the parameters listed below the graphs.



Transition layer algorithm properties		General statistics	
I_c minimum check value:	1.70	Total points in CPT file:	922
I_c maximum check value:	3.00	Total points excluded:	67
I_c change ratio value:	0.0250	Exclusion percentage:	7.27%
Minimum number of points in layer:	4	Number of layers detected:	6

Transition layer No	Number of points	Depth	SBT_n number	SBT_n description
Transition layer 1	12	Start depth: 21.26 (ft)	3	Clay
		End depth: 22.01 (ft)	5	Silty sand & sandy silt
Transition layer 2	13	Start depth: 23.18 (ft)	5	Silty sand & sandy silt
		End depth: 23.96 (ft)	4	Clay & silty clay
Transition layer 3	9	Start depth: 39.60 (ft)	4	Clay & silty clay
		End depth: 40.11 (ft)	5	Silty sand & sandy silt
Transition layer 4	13	Start depth: 47.28 (ft)	3	Clay
		End depth: 48.04 (ft)	5	Silty sand & sandy silt
Transition layer 5	11	Start depth: 51.09 (ft)	5	Silty sand & sandy silt
		End depth: 51.73 (ft)	4	Clay & silty clay
Transition layer 6	9	Start depth: 59.87 (ft)	4	Clay & silty clay
		End depth: 60.40 (ft)	5	Silty sand & sandy silt

Start depth: Depth where the transition layer begins
End depth: Depth where the transition layer ends

:: Field input data ::

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1	0.10	36.51	0.22	0.10	10.56	112.36
2	0.15	49.40	0.26	0.10	9.61	114.37
3	0.23	63.09	0.45	0.10	7.92	116.73
4	0.30	75.89	0.67	0.10	6.50	118.27
5	0.34	75.08	0.78	0.10	5.12	119.15
6	0.39	74.72	0.91	0.10	3.95	120.55
7	0.50	158.13	1.01	0.29	3.32	121.70
8	0.53	182.65	1.07	0.29	3.00	122.56
9	0.60	207.98	1.10	0.29	2.90	123.12
10	0.69	214.78	1.14	0.48	2.82	123.56
11	0.72	192.58	1.17	0.48	2.78	123.92
12	0.80	167.26	1.24	0.38	3.39	124.07
13	0.87	133.34	1.25	0.29	4.29	124.13
14	0.92	124.30	1.27	0.29	5.70	124.09
15	1.00	110.97	1.33	0.19	7.64	123.90
16	1.08	86.45	1.41	0.19	9.81	123.65
17	1.12	76.96	1.44	0.00	12.06	123.30
18	1.20	64.25	1.49	-0.10	14.06	122.93
19	1.30	52.44	1.43	-0.19	16.25	122.49
20	1.34	50.20	1.36	-0.29	18.41	121.99
21	1.40	48.33	1.26	-0.29	19.85	121.45
22	1.49	46.00	1.14	-0.38	21.03	120.87
23	1.54	44.21	1.07	-0.48	21.61	120.25
24	1.59	43.31	1.01	-0.48	21.73	119.72
25	1.68	41.70	0.92	-0.48	21.92	119.23
26	1.74	40.45	0.87	-0.67	22.21	118.82
27	1.79	39.73	0.83	-0.77	22.60	118.52
28	1.87	38.21	0.84	-0.96	23.18	118.29
29	1.94	36.51	0.86	-0.96	23.86	118.11
30	1.98	35.62	0.88	-1.05	24.64	118.00
31	2.04	34.54	0.89	-1.15	25.48	117.88
32	2.13	32.13	0.91	-1.34	26.44	117.75
33	2.17	31.50	0.91	-1.44	27.31	117.57
34	2.24	30.61	0.89	-1.63	28.26	117.28
35	2.33	28.91	0.83	-1.63	29.13	116.95
36	2.36	27.56	0.80	-1.63	30.23	116.54
37	2.43	26.67	0.75	-1.63	31.29	116.05
38	2.52	23.27	0.68	-1.53	32.43	115.56
39	2.56	23.27	0.66	-1.53	33.70	115.07
40	2.64	19.96	0.63	-1.53	35.18	114.63
41	2.74	17.90	0.59	-1.63	36.96	114.27
42	2.78	17.63	0.60	-1.63	39.08	114.01
43	2.83	17.09	0.61	-1.63	41.13	113.88
44	2.90	15.75	0.60	-1.44	43.58	113.78
45	2.98	14.77	0.65	-1.44	45.50	113.76
46	3.03	14.32	0.68	-1.34	47.06	113.82
47	3.10	13.60	0.70	-1.34	48.41	113.84
48	3.18	13.16	0.71	-1.25	49.54	113.86

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
49	3.23	13.16	0.71	-1.25	50.34	113.91
50	3.29	13.24	0.70	-1.25	50.80	113.89
51	3.38	13.69	0.68	-1.15	51.07	113.84
52	3.42	13.96	0.68	-1.15	51.09	113.71
53	3.51	13.78	0.67	-1.15	51.04	113.56
54	3.58	13.42	0.66	-1.15	51.01	113.39
55	3.62	13.24	0.65	-1.15	51.05	113.18
56	3.69	12.71	0.61	-1.15	51.21	112.94
57	3.77	12.35	0.60	-1.15	51.42	112.63
58	3.82	12.17	0.59	-1.15	51.47	112.29
59	3.89	11.81	0.56	-1.05	51.33	111.96
60	3.97	11.72	0.52	-1.15	51.36	111.61
61	4.03	11.54	0.49	-1.69	51.46	111.32
62	4.10	11.63	0.46	-1.69	51.71	111.06
63	4.15	11.90	0.46	-1.69	52.01	110.85
64	4.24	11.19	0.45	-2.04	52.34	110.70
65	4.29	10.83	0.45	-2.39	52.83	110.63
66	4.35	10.38	0.47	-1.63	53.43	110.61
67	4.44	10.38	0.49	-1.25	54.16	110.63
68	4.48	10.29	0.49	-1.15	54.98	110.62
69	4.54	10.29	0.50	-1.05	55.46	110.67
70	4.61	10.20	0.50	-1.05	55.64	110.73
71	4.69	10.20	0.49	-0.96	55.31	110.81
72	4.74	10.20	0.48	-0.96	54.45	110.92
73	4.82	10.47	0.49	-1.05	53.55	111.05
74	4.86	10.83	0.49	-1.05	52.79	111.17
75	4.94	11.45	0.50	-1.05	52.34	111.26
76	5.02	12.71	0.52	-1.05	52.16	111.32
77	5.09	12.89	0.53	-0.96	52.05	111.37
78	5.13	12.62	0.54	-0.96	52.05	111.35
79	5.23	11.72	0.53	-1.05	52.19	111.27
80	5.28	11.01	0.52	-1.05	52.54	111.14
81	5.33	10.74	0.50	-1.05	53.25	110.89
82	5.39	10.38	0.48	-0.86	53.98	110.59
83	5.48	10.11	0.45	-0.67	54.59	110.28
84	5.52	9.93	0.44	-0.67	54.81	109.97
85	5.58	9.84	0.41	-0.67	54.58	109.67
86	5.67	9.84	0.40	-0.57	54.43	109.37
87	5.73	9.84	0.40	-0.57	54.35	109.07
88	5.78	9.84	0.39	-0.57	54.42	108.73
89	5.88	10.02	0.37	-0.67	54.59	108.40
90	5.92	9.66	0.36	-1.25	54.63	108.09
91	5.97	9.22	0.35	-1.53	54.64	107.74
92	6.08	8.50	0.31	-1.63	54.54	107.36
93	6.11	8.23	0.31	-1.63	54.34	106.93
94	6.18	8.46	0.29	-1.63	54.25	106.54
95	6.27	8.41	0.27	-1.63	54.01	106.16
96	6.33	8.50	0.26	-1.63	53.55	105.85

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
97	6.38	8.50	0.24	-1.72	52.94	105.72
98	6.44	8.68	0.24	-1.92	52.10	105.59
99	6.50	8.68	0.24	-1.92	51.55	105.55
100	6.57	8.86	0.25	-1.92	51.37	105.67
101	6.67	9.04	0.26	-1.92	51.49	105.88
102	6.72	9.22	0.26	-1.82	51.79	106.17
103	6.76	9.31	0.27	-1.63	52.32	106.50
104	6.83	9.22	0.30	-1.92	52.99	106.84
105	6.92	9.13	0.32	-1.53	53.76	107.13
106	6.97	9.13	0.33	-1.34	54.53	107.34
107	7.04	9.04	0.35	-1.25	55.29	107.55
108	7.12	8.86	0.36	-1.34	55.88	107.71
109	7.16	8.68	0.36	-1.15	56.05	107.81
110	7.25	8.59	0.35	-0.77	55.94	107.87
111	7.32	8.77	0.35	-0.10	55.73	107.91
112	7.37	8.95	0.34	0.10	55.35	107.99
113	7.43	9.31	0.34	0.57	54.81	108.10
114	7.52	9.58	0.34	0.57	54.16	108.22
115	7.56	9.66	0.34	0.29	53.66	108.43
116	7.63	10.02	0.37	-0.29	53.31	108.65
117	7.71	10.29	0.39	-0.38	53.21	108.86
118	7.75	10.38	0.39	-0.24	53.29	109.02
119	7.83	10.43	0.42	0.77	53.69	109.14
120	7.88	10.47	0.43	-0.24	54.27	109.22
121	7.97	10.11	0.42	-0.29	54.91	109.21
122	8.01	9.93	0.41	-0.38	55.49	109.11
123	8.08	9.40	0.40	-0.38	55.95	108.99
124	8.18	8.95	0.39	-0.19	56.17	108.81
125	8.22	8.77	0.38	-0.10	56.30	108.61
126	8.28	8.77	0.36	0.29	56.12	108.45
127	8.35	9.04	0.35	0.57	55.94	108.31
128	8.43	9.31	0.35	0.67	55.64	108.20
129	8.48	9.40	0.35	0.67	55.28	108.09
130	8.56	9.75	0.35	0.67	55.02	108.00
131	8.63	9.66	0.35	0.67	55.01	107.95
132	8.68	9.49	0.35	0.86	55.18	107.89
133	8.76	9.13	0.34	0.96	55.48	107.79
134	8.80	8.86	0.34	1.15	55.64	107.62
135	8.88	8.59	0.34	1.34	55.99	107.40
136	8.94	8.50	0.33	1.72	56.33	107.15
137	8.99	8.41	0.32	1.82	56.68	106.90
138	9.07	8.41	0.29	2.20	56.99	106.64
139	9.14	8.32	0.28	2.39	57.34	106.34
140	9.22	8.14	0.27	2.39	57.58	106.00
141	9.27	7.96	0.27	2.39	57.75	105.66
142	9.37	7.70	0.26	2.39	57.74	105.27
143	9.42	7.25	0.25	2.39	57.92	104.93
144	9.47	7.07	0.24	2.49	58.20	104.57

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
145	9.52	7.07	0.23	2.59	58.64	104.23
146	9.62	7.16	0.21	2.78	59.03	103.88
147	9.67	7.07	0.20	2.87	59.10	103.53
148	9.73	6.80	0.19	2.87	58.43	103.48
149	9.82	6.53	0.19	2.87	57.56	103.58
150	9.86	6.44	0.19	2.87	56.52	103.77
151	9.92	6.62	0.18	2.87	55.39	104.30
152	10.02	7.96	0.23	2.87	54.38	104.95
153	10.06	8.50	0.25	2.97	53.43	105.74
154	10.12	9.04	0.26	2.97	52.41	106.64
155	10.21	10.47	0.32	2.78	51.52	107.51
156	10.25	10.83	0.35	2.87	50.62	108.39
157	10.31	11.19	0.39	2.78	49.79	109.12
158	10.41	11.81	0.44	2.78	48.98	109.76
159	10.45	11.81	0.46	2.78	48.08	110.36
160	10.52	12.44	0.48	2.78	47.33	110.89
161	10.61	13.33	0.50	3.16	46.55	111.35
162	10.64	13.69	0.50	3.35	45.77	111.77
163	10.71	14.59	0.51	3.45	45.06	112.13
164	10.81	15.48	0.55	3.54	44.50	112.47
165	10.85	15.84	0.56	3.64	44.05	112.77
166	10.91	16.20	0.59	3.64	43.83	113.04
167	10.96	16.33	0.61	3.93	43.64	113.30
168	11.03	16.47	0.63	3.64	43.57	113.56
169	11.10	16.47	0.64	3.64	43.59	113.76
170	11.20	16.47	0.65	3.64	43.67	113.97
171	11.24	16.65	0.65	3.64	43.61	114.15
172	11.30	17.27	0.67	3.64	43.59	114.33
173	11.36	17.45	0.68	3.73	43.61	114.50
174	11.43	17.81	0.70	3.83	43.70	114.63
175	11.50	18.17	0.71	3.73	43.86	114.71
176	11.58	18.26	0.73	3.64	44.05	114.73
177	11.63	18.17	0.75	3.64	44.19	114.71
178	11.70	17.72	0.74	3.45	44.39	114.67
179	11.79	16.91	0.71	3.45	44.55	114.56
180	11.84	16.56	0.67	3.45	44.61	114.37
181	11.90	16.87	0.66	3.45	44.65	114.11
182	11.98	16.65	0.65	3.73	44.29	113.79
183	12.02	16.82	0.62	3.64	43.69	113.44
184	12.09	16.65	0.57	3.26	42.90	113.12
185	12.14	16.29	0.54	3.06	42.08	112.86
186	12.21	17.54	0.51	2.87	41.25	112.60
187	12.29	17.45	0.48	2.78	40.24	112.37
188	12.34	17.72	0.47	2.68	39.44	112.22
189	12.44	17.90	0.47	1.92	38.86	112.17
190	12.49	18.43	0.47	1.92	38.28	112.18
191	12.57	19.42	0.48	2.01	38.16	112.24
192	12.64	19.24	0.50	2.01	38.14	112.33

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
193	12.68	19.24	0.52	2.01	38.16	112.41
194	12.73	19.24	0.52	2.01	38.27	112.48
195	12.84	18.79	0.53	1.82	38.48	112.50
196	12.89	18.61	0.53	1.92	38.71	112.49
197	12.98	18.43	0.51	1.92	38.89	112.44
198	13.00	18.08	0.51	1.92	39.00	112.36
199	13.08	17.99	0.49	2.01	39.15	112.30
200	13.14	18.35	0.48	2.01	39.34	112.28
201	13.23	18.26	0.48	1.82	39.52	112.31
202	13.27	18.08	0.48	1.63	39.69	112.43
203	13.34	18.26	0.49	1.72	39.82	112.60
204	13.43	17.99	0.53	1.92	40.03	112.82
205	13.47	18.26	0.55	2.01	40.32	113.07
206	13.54	18.79	0.58	2.01	40.90	113.36
207	13.63	19.15	0.61	2.01	41.67	113.66
208	13.67	19.15	0.62	2.01	42.42	113.92
209	13.72	19.33	0.64	2.01	43.09	114.13
210	13.83	18.35	0.68	1.63	43.82	114.25
211	13.88	17.45	0.70	1.63	44.53	114.30
212	13.94	17.45	0.70	1.63	45.27	114.30
213	13.98	17.00	0.70	1.92	46.08	114.24
214	14.06	16.56	0.67	1.82	47.01	114.14
215	14.14	16.47	0.65	1.82	47.58	113.98
216	14.18	16.29	0.64	1.82	47.86	113.78
217	14.26	15.66	0.62	1.82	48.24	113.53
218	14.33	15.30	0.61	1.82	48.60	113.25
219	14.37	15.21	0.59	1.82	48.95	113.00
220	14.45	15.03	0.57	1.82	49.50	112.74
221	14.54	14.50	0.55	1.82	49.99	112.47
222	14.61	13.96	0.53	1.82	50.28	112.20
223	14.65	13.69	0.52	1.63	50.42	111.91
224	14.74	13.16	0.51	1.63	50.59	111.63
225	14.80	13.16	0.49	1.63	50.72	111.36
226	14.85	13.16	0.47	1.63	50.77	111.11
227	14.90	13.16	0.45	1.63	50.76	110.90
228	15.00	13.16	0.44	1.72	50.70	110.68
229	15.05	13.16	0.43	1.72	50.46	110.47
230	15.10	12.98	0.42	1.72	50.33	110.27
231	15.17	12.80	0.42	1.63	50.25	110.08
232	15.25	12.80	0.41	1.63	50.21	109.90
233	15.30	12.71	0.40	1.63	50.15	109.73
234	15.36	12.44	0.39	1.63	50.15	109.54
235	15.45	12.44	0.38	1.72	50.13	109.36
236	15.49	12.44	0.37	1.72	50.14	109.16
237	15.57	12.44	0.36	1.72	50.25	108.98
238	15.64	12.26	0.35	1.72	50.41	108.85
239	15.69	12.17	0.34	1.72	50.59	108.76
240	15.77	11.81	0.34	1.72	50.91	108.69

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
241	15.85	11.72	0.34	1.72	51.53	108.66
242	15.89	11.72	0.35	1.72	52.19	108.62
243	15.99	11.63	0.36	1.72	53.04	108.60
244	16.05	11.45	0.36	1.72	54.05	108.59
245	16.09	10.92	0.37	1.72	54.98	108.57
246	16.16	10.74	0.36	1.72	56.09	108.50
247	16.24	10.38	0.36	1.63	57.30	108.39
248	16.30	10.02	0.36	1.63	58.39	108.23
249	16.34	9.75	0.35	1.63	59.45	108.02
250	16.44	9.31	0.34	1.63	60.21	107.76
251	16.48	9.04	0.33	1.72	60.84	107.51
252	16.54	9.04	0.32	1.72	61.30	107.26
253	16.63	8.77	0.30	1.72	61.55	107.02
254	16.69	8.77	0.29	1.72	61.55	106.78
255	16.74	8.77	0.28	1.72	61.22	106.55
256	16.82	8.77	0.28	1.72	60.87	106.35
257	16.90	8.86	0.28	1.72	60.56	106.14
258	16.94	8.95	0.27	1.72	59.99	106.00
259	17.03	9.04	0.26	1.72	59.58	105.89
260	17.07	8.95	0.26	1.72	59.28	105.77
261	17.13	8.86	0.25	1.82	59.51	105.80
262	17.21	9.22	0.25	1.82	60.04	105.94
263	17.26	9.13	0.25	1.82	60.25	106.30
264	17.33	8.86	0.24	1.82	59.79	106.84
265	17.41	8.59	0.29	1.82	58.81	107.43
266	17.48	8.68	0.33	1.82	57.32	108.11
267	17.53	10.02	0.38	1.82	56.26	108.74
268	17.61	11.90	0.42	1.82	55.21	109.32
269	17.67	13.07	0.44	1.82	54.15	109.87
270	17.72	14.50	0.46	1.82	52.82	110.19
271	17.82	14.23	0.47	1.82	51.58	110.38
272	17.88	14.23	0.46	1.82	50.88	110.40
273	17.92	14.23	0.45	1.82	50.71	110.26
274	18.02	13.69	0.40	1.82	51.01	110.03
275	18.07	13.16	0.38	1.82	51.47	109.73
276	18.14	12.17	0.37	1.82	52.23	109.40
277	18.20	11.63	0.35	1.72	52.62	109.09
278	18.27	11.10	0.34	1.82	52.89	108.82
279	18.32	11.68	0.34	1.72	53.06	108.71
280	18.38	10.65	0.35	1.82	53.23	108.68
281	18.47	11.72	0.34	1.82	53.15	108.71
282	18.51	12.35	0.35	1.82	52.67	108.79
283	18.57	12.80	0.36	1.82	52.08	108.91
284	18.67	12.71	0.37	1.72	51.65	108.96
285	18.71	12.71	0.38	1.72	50.71	108.97
286	18.81	13.24	0.37	1.72	50.07	108.94
287	18.86	13.24	0.37	1.72	49.41	108.83
288	18.91	13.24	0.35	1.72	48.87	108.62

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
289	18.97	13.16	0.33	1.82	48.38	108.41
290	19.06	13.42	0.31	1.82	47.85	108.19
291	19.11	13.60	0.29	1.82	47.49	108.10
292	19.21	13.24	0.27	1.82	46.84	108.12
293	19.27	12.98	0.28	1.82	46.13	108.40
294	19.31	13.16	0.29	1.82	45.11	108.99
295	19.41	13.87	0.33	1.92	43.72	109.93
296	19.46	15.39	0.36	1.92	42.18	110.99
297	19.51	17.09	0.43	1.92	40.10	111.99
298	19.56	20.05	0.52	2.01	38.26	112.88
299	19.63	24.52	0.64	2.01	37.43	113.63
300	19.71	27.21	0.70	1.82	36.94	114.30
301	19.80	30.52	0.68	0.67	37.08	114.90
302	19.82	30.34	0.68	0.10	37.42	115.44
303	19.91	25.42	0.69	-0.48	38.66	115.83
304	19.95	24.07	0.72	-0.86	38.28	116.25
305	20.02	21.57	0.77	-1.63	37.99	116.59
306	20.11	21.30	0.84	-1.63	38.01	116.96
307	20.15	17.36	0.89	-1.36	38.01	117.36
308	20.24	31.86	0.95	-1.36	37.41	117.81
309	20.29	33.56	0.97	-1.36	36.44	118.32
310	20.36	35.35	1.00	-1.34	35.13	118.88
311	20.41	35.62	1.04	-1.34	33.89	119.38
312	20.48	35.98	1.08	-1.34	32.57	119.84
313	20.56	38.57	1.15	-1.34	33.12	120.13
314	20.66	40.72	1.25	-1.34	34.33	120.33
315	20.71	40.45	1.28	-1.34	35.87	120.45
316	20.74	38.39	1.30	-1.63	37.71	120.42
317	20.82	31.95	1.35	-1.72	39.84	120.24
318	20.91	25.95	1.34	-1.72	42.53	119.91
319	20.95	23.63	1.31	-1.72	45.95	119.39
320	21.03	19.87	1.20	-1.72	50.00	118.77
321	21.11	17.09	1.04	-1.72	54.40	118.12
322	21.15	15.75	0.97	-1.72	57.33	117.50
323	21.22	13.96	0.88	-1.72	58.13	117.00
324	21.26	13.60	0.84	-1.72	57.68	116.61
325	21.34	14.05	0.84	-1.72	55.24	116.49
326	21.41	16.47	0.84	-1.63	52.03	116.63
327	21.48	19.51	0.85	-1.63	47.67	116.98
328	21.52	21.92	0.88	-1.63	43.41	117.42
329	21.61	26.76	0.95	-1.63	39.61	117.87
330	21.66	29.71	0.98	-1.63	36.14	118.33
331	21.76	37.14	1.04	-1.63	33.35	118.81
332	21.81	39.82	1.03	-1.63	31.04	119.30
333	21.85	42.15	1.02	-1.63	29.08	119.77
334	21.92	45.37	1.03	-1.63	27.51	120.19
335	22.01	48.06	1.10	-1.63	26.21	120.64
336	22.09	51.28	1.17	-1.63	25.30	121.01

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
337	22.12	53.16	1.20	-1.63	24.45	121.43
338	22.20	56.20	1.27	-1.63	23.69	121.84
339	22.29	58.80	1.36	-1.63	22.94	122.24
340	22.31	60.59	1.38	-1.63	22.13	122.59
341	22.40	64.88	1.45	-1.63	21.46	122.90
342	22.45	67.39	1.46	-1.72	20.86	123.20
343	22.51	71.95	1.47	-1.72	20.41	123.48
344	22.60	75.71	1.48	-1.82	19.93	123.62
345	22.64	76.25	1.50	-2.20	19.30	123.54
346	22.75	77.86	1.56	-3.83	18.81	123.41
347	22.80	77.50	1.61	-3.64	18.48	123.26
348	22.85	76.87	1.49	-3.64	18.30	123.10
349	22.91	75.17	1.15	-3.74	18.25	122.93
350	22.99	74.01	1.15	-3.74	18.44	122.92
351	23.08	71.77	1.18	-3.74	18.75	122.92
352	23.10	71.32	1.19	-3.74	19.34	122.94
353	23.18	71.10	1.23	-3.59	20.13	123.05
354	23.26	70.88	1.51	-3.59	21.30	123.32
355	23.30	69.98	1.61	-3.46	22.66	123.54
356	23.37	62.46	1.74	-3.46	24.31	123.59
357	23.46	60.85	1.78	-3.46	26.22	123.46
358	23.51	56.38	1.75	-3.35	28.40	123.17
359	23.56	51.10	1.74	-3.35	30.58	122.57
360	23.63	39.20	1.53	-3.16	32.91	121.82
361	23.72	32.22	1.28	-3.16	34.95	120.91
362	23.79	27.74	1.09	-3.06	37.22	119.84
363	23.87	25.15	0.85	-3.06	39.47	118.67
364	23.91	25.15	0.77	-3.06	41.35	117.41
365	23.96	23.54	0.68	-2.97	42.20	116.31
366	24.02	22.19	0.63	-2.97	42.33	115.46
367	24.11	21.66	0.59	-2.97	42.31	114.80
368	24.20	22.24	0.59	-2.97	42.44	114.43
369	24.22	21.30	0.59	-2.87	42.77	114.15
370	24.31	22.28	0.60	-2.97	43.05	114.00
371	24.39	21.21	0.60	-2.97	43.25	113.94
372	24.42	21.03	0.60	-2.97	43.29	113.91
373	24.51	20.85	0.60	-2.97	43.38	113.83
374	24.55	20.94	0.59	-2.87	43.13	113.71
375	24.63	20.94	0.60	-2.87	43.10	113.47
376	24.71	21.21	0.57	-2.87	43.06	113.19
377	24.75	21.30	0.54	-2.87	43.09	112.82
378	24.81	21.39	0.50	-2.87	43.30	112.41
379	24.90	20.40	0.45	-2.87	43.59	111.96
380	24.94	19.06	0.43	-2.97	43.77	111.42
381	25.01	17.72	0.39	-2.87	44.10	110.93
382	25.07	16.47	0.38	-2.78	44.56	110.47
383	25.15	16.02	0.36	-2.87	45.33	110.11
384	25.20	15.93	0.34	-2.87	46.22	109.91

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
385	25.28	16.20	0.35	-2.87	47.02	109.82
386	25.35	16.20	0.35	-2.87	47.64	109.85
387	25.40	16.11	0.37	-2.87	47.91	109.96
388	25.48	15.93	0.39	-2.78	48.23	110.23
389	25.55	15.84	0.41	-2.78	48.74	110.65
390	25.60	16.02	0.42	-2.78	49.19	111.08
391	25.67	16.38	0.43	-2.78	49.62	111.50
392	25.75	16.91	0.48	-2.78	50.01	111.89
393	25.79	17.27	0.54	-2.78	50.37	112.22
394	25.90	17.72	0.56	-2.78	50.28	112.53
395	25.95	17.90	0.57	-2.78	50.06	112.82
396	26.01	17.72	0.58	-2.73	49.90	113.08
397	26.09	17.18	0.58	-2.73	49.67	113.26
398	26.13	18.70	0.58	-2.73	49.20	113.34
399	26.19	19.06	0.58	-2.68	48.75	113.40
400	26.27	19.06	0.58	-2.68	48.22	113.48
401	26.34	19.33	0.58	-2.68	47.65	113.57
402	26.39	19.69	0.57	-2.68	46.91	113.68
403	26.47	20.05	0.58	-2.68	46.67	113.76
404	26.54	20.76	0.60	-2.68	46.56	113.83
405	26.58	20.85	0.61	-2.68	46.55	113.90
406	26.67	21.21	0.62	-2.68	46.67	113.94
407	26.73	20.58	0.62	-2.68	46.84	113.98
408	26.78	20.31	0.62	-2.68	47.01	113.97
409	26.85	19.78	0.62	-2.68	47.20	113.90
410	26.93	19.42	0.61	-2.68	47.39	113.81
411	26.98	19.42	0.60	-2.68	47.70	113.72
412	27.03	19.42	0.58	-2.68	47.92	113.63
413	27.13	19.51	0.56	-2.68	48.13	113.54
414	27.17	19.51	0.56	-2.68	48.28	113.47
415	27.24	19.24	0.57	-2.59	48.45	113.38
416	27.33	19.06	0.57	-2.59	48.82	113.29
417	27.36	18.97	0.57	-2.59	49.28	113.23
418	27.43	18.70	0.58	-2.59	49.80	113.17
419	27.53	18.17	0.56	-2.59	50.35	113.11
420	27.60	17.54	0.56	-2.59	50.73	113.01
421	27.63	17.27	0.56	-2.59	50.97	112.86
422	27.72	17.27	0.54	-2.59	51.14	112.70
423	27.77	17.27	0.54	-2.59	51.07	112.53
424	27.84	17.27	0.52	-2.59	50.75	112.42
425	27.93	17.18	0.49	-2.59	50.22	112.31
426	27.97	17.36	0.48	-2.59	49.60	112.20
427	28.02	17.81	0.48	-2.59	49.10	112.12
428	28.12	18.52	0.48	-2.59	48.66	112.04
429	28.17	18.70	0.48	-2.59	48.15	111.96
430	28.22	18.70	0.48	-2.59	47.80	111.90
431	28.32	18.52	0.48	-2.59	47.78	111.89
432	28.36	18.43	0.48	-2.59	47.50	111.91

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
433	28.42	18.61	0.46	-2.49	46.77	112.05
434	28.48	18.17	0.45	-2.49	46.08	112.17
435	28.57	17.54	0.47	-2.49	45.43	112.29
436	28.62	19.06	0.48	-2.49	44.84	112.54
437	28.72	22.55	0.53	-2.49	44.49	112.80
438	28.75	22.55	0.52	-2.49	44.55	113.11
439	28.82	22.55	0.52	-2.59	44.89	113.45
440	28.87	23.18	0.59	-2.68	45.00	113.73
441	28.95	22.46	0.61	-2.68	45.32	113.93
442	29.02	21.21	0.64	-2.68	46.08	113.95
443	29.07	19.87	0.66	-2.62	46.91	113.93
444	29.16	19.78	0.65	-2.62	47.80	113.91
445	29.21	19.69	0.62	-2.55	48.59	113.77
446	29.29	19.51	0.57	-2.49	48.98	113.59
447	29.36	18.88	0.54	-2.49	48.88	113.38
448	29.40	18.88	0.54	-2.49	47.95	113.17
449	29.47	18.88	0.53	-2.39	46.96	113.00
450	29.56	19.60	0.51	-2.49	46.00	112.89
451	29.60	19.96	0.50	-2.39	45.13	112.88
452	29.71	21.84	0.50	-2.49	44.46	112.94
453	29.75	22.46	0.51	-2.39	43.85	113.04
454	29.79	22.91	0.52	-2.39	43.32	113.16
455	29.86	23.18	0.53	-2.39	43.08	113.33
456	29.95	22.64	0.55	-2.39	42.92	113.53
457	30.04	22.60	0.57	-2.39	42.85	113.72
458	30.06	22.60	0.58	-2.39	42.69	113.91
459	30.15	22.55	0.60	-2.39	42.61	114.11
460	30.20	22.91	0.61	-2.39	42.52	114.35
461	30.28	24.25	0.61	-2.39	42.46	114.65
462	30.35	25.15	0.62	-2.39	42.47	114.93
463	30.39	25.59	0.64	-2.39	42.47	115.17
464	30.45	26.22	0.68	-2.39	42.49	115.36
465	30.54	26.31	0.75	-2.49	42.63	115.52
466	30.60	25.68	0.76	-2.39	43.18	115.66
467	30.67	25.33	0.75	-2.30	43.89	115.73
468	30.74	24.70	0.74	-2.30	44.61	115.75
469	30.79	24.25	0.74	-2.30	45.42	115.70
470	30.86	22.91	0.74	-2.30	45.96	115.45
471	30.95	22.37	0.71	-2.30	46.40	115.16
472	30.99	22.19	0.69	-2.30	46.82	114.83
473	31.05	21.75	0.68	-2.30	47.20	114.49
474	31.14	21.21	0.58	-2.30	47.39	114.12
475	31.19	20.85	0.56	-2.30	47.38	113.74
476	31.26	20.31	0.53	-2.30	47.21	113.40
477	31.34	19.78	0.51	-2.30	46.96	113.06
478	31.39	20.27	0.50	-2.30	46.58	112.76
479	31.45	19.60	0.49	-2.20	46.49	112.68
480	31.54	20.22	0.49	-2.20	46.24	112.60

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
481	31.57	20.49	0.48	-2.20	45.49	112.54
482	31.63	20.76	0.49	-2.20	44.57	112.64
483	31.73	21.03	0.53	-2.30	43.79	112.82
484	31.77	21.48	0.51	-2.20	42.90	113.11
485	31.84	23.00	0.47	-2.30	42.23	113.42
486	31.93	24.79	0.53	-2.20	42.18	113.73
487	31.98	25.68	0.57	-2.20	42.06	114.01
488	32.05	26.67	0.62	-2.20	41.94	114.20
489	32.09	26.76	0.64	-2.20	42.01	114.39
490	32.17	24.07	0.66	-2.15	42.38	114.63
491	32.22	24.43	0.66	-2.15	42.95	114.72
492	32.32	23.80	0.64	-2.15	43.44	114.75
493	32.35	23.27	0.64	-2.11	43.87	114.70
494	32.43	23.71	0.64	-2.11	44.20	114.60
495	32.52	22.91	0.62	-2.11	43.99	114.52
496	32.57	23.63	0.61	-2.01	43.86	114.42
497	32.62	23.98	0.60	-2.01	43.67	114.35
498	32.71	24.34	0.59	-2.01	43.44	114.27
499	32.76	24.43	0.59	-2.01	43.24	114.20
500	32.82	24.25	0.59	-2.01	43.09	114.19
501	32.90	24.07	0.58	-2.01	43.08	114.21
502	32.96	23.89	0.58	-2.01	43.14	114.25
503	33.02	24.07	0.58	-2.01	43.27	114.36
504	33.11	23.80	0.61	-2.01	43.45	114.47
505	33.17	24.07	0.62	-2.01	43.55	114.60
506	33.22	24.25	0.63	-2.01	43.63	114.72
507	33.31	24.88	0.66	-2.01	43.78	114.82
508	33.34	24.88	0.67	-2.01	43.91	114.90
509	33.41	25.24	0.68	-2.01	43.96	114.91
510	33.49	25.15	0.67	-2.01	44.08	114.93
511	33.57	24.34	0.65	-2.01	44.21	114.94
512	33.61	24.25	0.64	-2.01	44.26	114.90
513	33.68	23.89	0.62	-2.01	44.24	114.87
514	33.76	23.89	0.64	-1.92	44.25	114.87
515	33.81	23.89	0.64	-1.92	44.28	114.94
516	33.88	24.25	0.63	-1.92	44.29	115.11
517	33.95	24.88	0.65	-1.92	44.39	115.37
518	34.01	25.42	0.68	-1.92	44.53	115.69
519	34.06	25.86	0.72	-1.92	44.75	116.01
520	34.13	26.22	0.77	-1.92	45.09	116.33
521	34.21	26.67	0.83	-1.92	45.62	116.71
522	34.25	26.85	0.87	-1.92	46.14	117.04
523	34.35	26.40	0.90	-2.01	46.68	117.33
524	34.40	25.95	0.92	-1.92	47.18	117.57
525	34.49	25.95	0.98	-2.01	47.62	117.75
526	34.53	26.13	0.98	-1.92	48.02	117.87
527	34.60	26.22	0.98	-1.92	48.39	117.96
528	34.65	26.22	0.98	-2.01	48.74	118.03

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
529	34.74	26.22	0.97	-2.01	49.06	118.12
530	34.80	26.22	0.98	-2.01	49.21	118.13
531	34.85	26.13	0.98	-2.01	49.41	118.09
532	34.93	25.68	1.00	-2.01	49.67	118.04
533	34.98	25.59	1.03	-2.01	50.04	117.99
534	35.05	25.50	1.00	-2.01	50.32	117.92
535	35.15	24.79	0.95	-2.01	50.56	117.84
536	35.20	24.57	0.94	-1.96	50.67	117.74
537	35.25	23.89	0.94	-1.96	50.50	117.61
538	35.33	24.34	0.92	-1.96	50.22	117.44
539	35.40	24.34	0.90	-1.92	49.98	117.29
540	35.44	24.70	0.89	-1.92	49.59	117.21
541	35.50	25.06	0.85	-1.92	49.14	117.13
542	35.59	25.24	0.84	-1.92	48.53	117.06
543	35.64	25.15	0.84	-1.92	48.06	117.00
544	35.70	25.86	0.85	-1.82	47.72	116.97
545	35.79	26.04	0.84	-1.82	47.54	116.95
546	35.83	26.22	0.83	-1.82	47.57	116.97
547	35.94	26.13	0.84	-1.82	47.64	116.96
548	35.98	25.86	0.85	-1.82	47.66	116.93
549	36.03	25.59	0.86	-1.82	47.83	116.85
550	36.09	25.24	0.87	-1.92	48.14	116.76
551	36.17	25.06	0.83	-1.92	48.65	116.64
552	36.23	24.79	0.81	-1.92	49.20	116.49
553	36.29	24.25	0.79	-1.92	49.78	116.30
554	36.38	23.63	0.77	-1.92	50.32	116.07
555	36.44	22.64	0.75	-1.92	50.83	115.81
556	36.49	22.10	0.74	-1.92	51.37	115.56
557	36.59	21.30	0.71	-1.92	51.90	115.32
558	36.63	21.03	0.69	-1.92	52.36	115.08
559	36.69	20.58	0.68	-1.92	52.71	114.88
560	36.78	20.40	0.65	-1.92	52.79	114.70
561	36.82	20.58	0.64	-1.92	52.65	114.54
562	36.88	20.31	0.63	-1.82	52.35	114.42
563	36.98	20.58	0.63	-1.82	52.08	114.32
564	37.02	20.94	0.62	-1.82	51.75	114.24
565	37.11	21.30	0.62	-1.82	51.51	114.18
566	37.18	21.48	0.61	-1.82	51.32	114.13
567	37.22	21.39	0.61	-1.82	51.13	114.13
568	37.28	21.21	0.61	-1.82	51.06	114.20
569	37.38	21.03	0.60	-1.82	51.07	114.32
570	37.42	21.03	0.60	-1.82	51.00	114.47
571	37.48	21.12	0.62	-1.82	50.96	114.63
572	37.57	21.57	0.67	-1.82	50.70	114.72
573	37.62	22.19	0.70	-1.82	50.18	114.73
574	37.68	23.00	0.72	-1.72	49.78	114.77
575	37.77	23.27	0.72	-1.72	49.55	114.87
576	37.82	23.45	0.66	-1.72	49.29	114.96

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
577	37.88	23.63	0.60	-1.72	49.00	114.98
578	37.96	23.18	0.61	-1.72	48.90	114.96
579	38.00	23.18	0.66	-1.72	48.43	114.94
580	38.08	23.18	0.67	-1.72	47.58	114.91
581	38.12	23.18	0.67	-1.72	46.78	114.92
582	38.20	22.64	0.68	-1.60	46.04	114.97
583	38.27	25.06	0.69	-1.60	45.54	115.03
584	38.36	27.03	0.66	-1.60	45.09	115.06
585	38.40	27.38	0.63	-1.53	44.88	115.19
586	38.46	27.92	0.60	-1.44	44.41	115.57
587	38.56	26.49	0.63	-1.44	43.41	116.01
588	38.59	26.04	0.66	-1.44	42.12	116.59
589	38.66	25.77	0.75	-1.44	41.03	117.28
590	38.76	30.07	0.93	-1.44	40.01	118.13
591	38.79	33.74	0.97	-1.44	39.28	118.98
592	38.87	40.09	1.09	-1.44	38.58	119.81
593	38.91	43.49	1.19	-1.44	37.95	120.69
594	39.00	47.16	1.36	-1.34	37.20	121.50
595	39.04	46.80	1.42	-1.34	36.56	122.20
596	39.11	46.53	1.51	-1.34	36.35	122.97
597	39.20	47.79	1.70	-1.34	36.59	123.71
598	39.24	48.95	1.77	-1.34	36.83	124.40
599	39.31	51.55	1.90	-1.34	36.90	125.19
600	39.38	53.43	2.18	-1.34	36.61	126.02
601	39.46	54.95	2.40	-1.25	35.65	126.89
602	39.51	57.81	2.54	-1.25	34.43	127.77
603	39.60	66.94	3.01	-1.25	33.29	128.59
604	39.66	73.47	3.27	-1.25	32.11	129.31
605	39.71	85.64	3.49	-1.15	30.93	129.92
606	39.79	95.04	3.86	-1.15	29.80	130.48
607	39.85	97.81	3.96	-1.15	28.13	131.08
608	39.91	101.84	3.92	-1.15	25.89	131.73
609	39.99	103.54	3.94	-1.15	23.75	132.32
610	40.05	106.32	4.07	-1.05	22.31	132.82
611	40.11	130.21	4.31	-0.96	21.42	133.20
612	40.20	167.88	4.79	-0.96	20.77	133.54
613	40.25	184.17	4.91	-1.15	20.35	133.87
614	40.30	176.92	5.04	-1.44	20.06	134.21
615	40.40	162.52	5.17	-1.44	19.87	134.57
616	40.43	155.45	5.21	-1.34	19.95	134.86
617	40.49	150.25	5.29	-1.25	20.49	134.97
618	40.55	148.29	5.50	-1.05	21.49	134.98
619	40.64	149.00	5.82	-0.96	22.67	134.93
620	40.69	153.12	5.95	-0.96	23.50	134.58
621	40.80	148.38	5.71	-0.96	24.47	134.22
622	40.84	133.52	5.57	-0.96	25.39	133.81
623	40.89	116.25	5.43	-0.96	26.20	133.33
624	40.96	97.63	3.70	-0.86	26.94	132.77

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
625	41.04	87.88	3.73	-0.77	28.25	132.10
626	41.10	85.46	3.57	-0.77	28.21	131.57
627	41.15	87.52	3.44	-0.77	27.74	131.08
628	41.24	89.85	3.44	-0.64	27.01	130.65
629	41.28	74.72	3.42	-0.19	26.55	130.66
630	41.38	120.54	3.40	-0.64	25.84	130.70
631	41.41	121.08	3.44	-0.57	25.12	130.77
632	41.49	114.55	3.54	-0.48	24.49	130.84
633	41.54	111.24	3.58	-0.48	23.72	130.88
634	41.61	111.60	3.62	-0.48	22.54	130.95
635	41.69	111.60	3.57	-0.38	22.17	130.92
636	41.77	111.95	3.46	-0.38	21.51	130.88
637	41.84	117.95	3.30	-0.38	20.63	130.83
638	41.88	121.80	3.24	-0.48	19.64	130.78
639	41.94	133.52	3.17	-0.48	18.72	130.70
640	42.04	144.62	3.05	-0.57	18.02	130.56
641	42.08	147.21	3.03	-0.57	17.43	130.44
642	42.17	150.43	3.02	-0.57	17.11	130.35
643	42.19	148.38	2.98	-0.67	16.93	130.30
644	42.28	136.20	2.84	-0.77	17.00	130.26
645	42.33	132.71	2.84	-0.77	17.33	130.26
646	42.39	129.14	2.90	-0.77	17.75	130.29
647	42.48	127.08	3.00	-0.77	18.27	130.32
648	42.53	127.97	3.07	-0.77	18.86	130.37
649	42.59	128.02	3.17	-0.77	19.41	130.48
650	42.67	128.87	3.27	-0.77	19.96	130.60
651	42.73	128.06	3.30	-0.77	20.54	130.70
652	42.81	124.84	3.36	-0.86	21.10	130.80
653	42.88	119.83	3.41	-0.77	21.65	130.90
654	42.92	116.96	3.42	-0.86	22.20	130.99
655	43.00	111.86	3.46	-0.77	22.75	131.06
656	43.08	111.86	3.56	-0.57	23.28	131.13
657	43.12	112.85	3.61	-0.57	23.80	131.19
658	43.21	112.58	3.69	-0.57	24.28	131.24
659	43.27	113.74	3.73	-0.67	24.76	131.29
660	43.32	113.56	3.76	-0.67	25.22	131.35
661	43.39	110.70	3.78	-0.67	25.70	131.40
662	43.47	106.76	3.77	-0.48	26.25	131.43
663	43.52	104.44	3.78	-0.48	26.93	131.38
664	43.59	100.50	3.85	-0.48	27.80	131.27
665	43.67	99.78	3.93	-0.48	29.01	131.07
666	43.72	98.08	3.91	-0.57	30.28	130.79
667	43.80	89.76	3.75	-0.48	31.54	130.33
668	43.85	82.87	3.59	-0.57	33.00	129.76
669	43.92	70.70	3.37	-0.48	34.54	129.14
670	43.97	65.42	3.11	-0.38	36.40	128.43
671	44.04	56.56	2.40	-0.38	38.38	127.63
672	44.13	49.85	2.16	-0.19	40.06	126.81

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
673	44.17	47.25	2.13	-0.19	41.47	125.92
674	44.24	43.22	2.08	-0.10	42.31	125.04
675	44.31	43.04	1.93	0.00	43.28	124.12
676	44.37	44.12	1.79	0.10	44.46	123.38
677	44.45	42.87	1.57	0.10	45.29	122.67
678	44.50	40.54	1.46	0.10	45.87	121.88
679	44.56	35.53	1.31	0.19	46.05	121.05
680	44.65	30.78	1.11	0.19	46.31	120.26
681	44.71	29.62	0.99	0.29	46.71	119.56
682	44.76	28.64	0.89	0.29	47.07	119.13
683	44.85	27.92	0.85	0.38	47.19	118.89
684	44.88	28.73	0.87	0.38	46.86	118.99
685	44.96	31.14	0.95	0.38	46.20	119.45
686	45.05	34.54	1.09	0.38	45.39	120.13
687	45.10	36.60	1.19	0.38	43.65	121.00
688	45.17	39.02	1.40	0.38	41.45	122.06
689	45.25	41.97	1.60	0.38	39.19	123.07
690	45.30	45.55	1.75	0.38	37.07	124.04
691	45.37	56.11	1.91	0.29	35.10	124.96
692	45.45	66.04	2.18	0.29	33.49	125.84
693	45.49	72.13	2.27	0.29	32.10	126.62
694	45.54	77.95	2.42	0.19	31.06	127.31
695	45.61	84.57	2.61	0.19	30.38	127.93
696	45.68	86.81	2.81	0.19	30.18	128.42
697	45.75	87.70	2.97	0.19	30.40	128.73
698	45.80	86.18	3.13	0.19	30.89	128.86
699	45.89	82.96	3.25	0.19	31.69	128.82
700	45.93	80.72	3.26	0.10	32.73	128.63
701	46.01	74.64	3.16	0.10	34.03	128.30
702	46.08	67.65	2.79	0.10	35.55	127.88
703	46.15	59.96	2.47	0.10	37.18	127.39
704	46.20	57.01	2.28	0.10	38.65	126.81
705	46.29	51.10	2.11	0.19	39.99	126.20
706	46.34	47.97	2.08	0.19	40.64	125.62
707	46.41	45.37	2.06	0.29	40.85	125.19
708	46.49	45.37	1.98	0.38	40.71	124.90
709	46.53	46.98	1.94	0.38	40.64	124.68
710	46.60	51.82	1.87	0.29	40.51	124.48
711	46.69	54.41	1.83	0.29	40.36	124.30
712	46.73	54.77	1.83	0.29	40.25	124.12
713	46.79	52.35	1.79	0.29	40.60	123.96
714	46.89	48.15	1.69	0.29	41.16	123.79
715	46.94	45.46	1.69	0.29	42.31	123.67
716	46.99	42.60	1.70	0.29	43.81	123.66
717	47.09	37.94	1.70	0.38	45.31	123.71
718	47.13	37.85	1.69	0.38	46.71	123.79
719	47.19	38.03	1.78	0.38	46.24	124.09
720	47.28	40.72	2.00	0.38	45.31	124.42

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
721	47.34	42.87	2.09	0.38	43.39	124.89
722	47.38	42.60	2.12	0.38	39.77	125.58
723	47.50	58.26	2.22	0.38	35.97	126.30
724	47.51	60.67	2.24	0.38	31.66	127.12
725	47.60	71.23	2.45	0.57	27.92	127.84
726	47.69	93.79	2.69	0.48	24.55	128.54
727	47.70	108.46	2.75	0.38	21.64	129.22
728	47.80	135.85	3.00	0.29	19.53	129.80
729	47.84	147.39	3.08	0.29	17.73	130.33
730	47.91	163.41	3.16	0.19	16.29	130.74
731	48.00	174.24	3.25	0.19	15.28	131.04
732	48.04	178.36	3.28	0.19	14.57	131.28
733	48.11	181.76	3.26	0.19	14.20	131.41
734	48.19	181.13	3.23	0.19	14.02	131.52
735	48.23	180.32	3.23	0.19	14.03	131.62
736	48.30	177.10	3.25	0.10	14.20	131.70
737	48.40	174.24	3.30	0.10	14.42	131.78
738	48.45	172.18	3.37	0.00	14.70	131.86
739	48.50	171.20	3.48	0.00	14.99	131.96
740	48.59	170.48	3.60	0.00	15.24	132.04
741	48.66	170.84	3.67	0.00	15.43	132.11
742	48.69	170.30	3.69	0.00	15.56	132.16
743	48.78	170.21	3.69	0.00	15.65	132.19
744	48.85	171.64	3.65	0.00	15.69	132.20
745	48.89	171.64	3.59	0.00	15.71	132.19
746	48.98	170.66	3.54	-0.10	15.73	132.17
747	49.03	170.03	3.54	0.00	15.76	132.16
748	49.09	170.39	3.54	-0.10	15.78	132.18
749	49.19	168.42	3.57	0.00	15.82	132.23
750	49.23	167.97	3.59	0.00	15.87	132.32
751	49.28	167.71	3.64	0.00	15.85	132.48
752	49.39	171.91	3.80	0.00	15.80	132.66
753	49.42	174.24	3.84	0.10	15.74	132.85
754	49.49	177.01	3.95	0.10	15.60	133.01
755	49.59	187.75	4.16	0.10	15.36	133.08
756	49.62	190.79	4.20	0.10	15.10	133.10
757	49.69	193.03	4.27	0.10	14.86	133.07
758	49.74	194.73	4.19	0.10	14.53	132.92
759	49.83	192.58	3.74	0.10	14.14	132.66
760	49.88	189.18	3.59	0.10	13.83	132.32
761	49.93	187.30	3.53	0.10	13.64	131.98
762	50.03	184.26	3.06	0.10	13.51	131.63
763	50.13	180.68	2.69	0.10	13.55	131.31
764	50.14	177.91	2.71	0.10	13.80	131.12
765	50.23	172.18	2.89	0.10	14.16	130.99
766	50.27	168.96	2.95	0.10	14.61	130.89
767	50.34	161.35	3.12	0.10	15.39	130.92
768	50.43	156.16	3.24	0.77	16.45	131.02

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
769	50.49	152.22	3.31	0.77	17.57	131.07
770	50.53	147.48	3.39	0.77	18.63	130.97
771	50.62	137.01	3.47	0.77	19.81	130.80
772	50.68	125.47	3.44	0.86	20.90	130.55
773	50.73	119.65	3.33	0.86	21.89	130.16
774	50.82	110.07	2.95	0.96	22.85	129.65
775	50.88	101.12	2.79	1.05	23.73	129.06
776	50.93	97.46	2.68	1.05	24.41	128.40
777	51.02	91.73	2.26	1.15	24.99	127.72
778	51.09	86.99	2.00	1.15	25.65	127.06
779	51.12	85.02	1.88	1.15	26.55	126.48
780	51.19	81.53	1.78	1.25	27.73	125.93
781	51.28	76.25	1.79	1.25	29.26	125.45
782	51.32	72.22	1.86	1.25	30.88	125.03
783	51.39	62.82	1.79	1.25	32.29	124.59
784	51.48	53.25	1.82	1.34	33.78	124.15
785	51.53	49.04	1.95	1.44	35.53	123.71
786	51.62	47.70	1.67	1.44	37.37	123.13
787	51.68	49.85	1.36	1.53	39.16	122.43
788	51.73	49.94	1.28	1.44	40.50	121.72
789	51.82	45.55	1.22	1.53	41.13	120.90
790	51.87	39.02	1.01	1.44	41.02	119.87
791	51.92	36.51	0.93	1.53	41.15	118.95
792	51.97	34.36	0.85	1.63	41.99	118.17
793	52.04	31.41	0.74	1.63	43.00	117.38
794	52.12	31.14	0.66	1.63	43.61	116.61
795	52.18	30.78	0.66	1.63	43.77	116.05
796	52.23	30.78	0.63	1.63	43.82	115.53
797	52.31	30.78	0.60	1.63	43.81	115.09
798	52.37	30.78	0.60	1.63	44.01	114.75
799	52.44	30.70	0.58	1.53	44.64	114.40
800	52.53	29.62	0.55	1.53	45.33	113.97
801	52.57	29.08	0.54	1.44	46.33	113.50
802	52.64	26.13	0.52	1.44	47.55	112.96
803	52.72	23.54	0.46	1.44	48.89	112.37
804	52.78	22.28	0.42	1.44	50.37	111.72
805	52.83	20.49	0.39	1.44	51.45	110.92
806	52.93	19.42	0.34	1.44	52.56	110.08
807	52.96	19.06	0.33	1.44	53.16	109.34
808	53.04	18.70	0.30	1.44	53.44	108.78
809	53.12	18.70	0.21	1.44	53.64	108.32
810	53.17	18.70	0.22	1.44	53.49	107.98
811	53.22	18.70	0.25	1.44	53.24	107.76
812	53.29	18.88	0.27	1.44	52.83	107.54
813	53.37	18.70	0.27	1.44	52.54	107.42
814	53.42	18.79	0.28	1.44	52.76	107.55
815	53.49	18.88	0.27	1.44	52.89	107.61
816	53.58	19.06	0.26	1.44	52.81	107.55

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
817	53.63	18.97	0.26	1.44	52.60	107.42
818	53.68	18.88	0.25	1.44	52.37	107.29
819	53.78	18.79	0.24	1.44	52.09	107.13
820	53.84	18.70	0.23	1.44	51.88	106.99
821	53.88	18.79	0.23	1.44	51.75	106.89
822	53.94	18.70	0.23	1.44	51.55	106.78
823	54.03	18.79	0.23	1.44	51.42	106.75
824	54.08	18.79	0.23	1.44	51.27	106.76
825	54.16	18.88	0.23	1.44	51.28	106.88
826	54.20	19.06	0.23	1.44	51.19	107.00
827	54.28	19.24	0.24	1.44	50.77	107.10
828	54.35	19.42	0.24	1.44	50.14	107.20
829	54.43	19.51	0.26	1.44	49.44	107.31
830	54.48	19.87	0.26	1.53	48.72	107.35
831	54.55	20.85	0.25	1.53	48.22	107.35
832	54.63	21.75	0.25	1.53	47.81	107.30
833	54.67	22.10	0.25	1.53	47.57	107.24
834	54.74	21.84	0.23	1.44	47.18	107.03
835	54.82	20.94	0.22	1.44	46.90	106.82
836	54.87	20.58	0.22	1.44	46.89	106.62
837	54.92	19.96	0.22	1.44	47.23	106.48
838	55.02	19.69	0.20	1.44	47.75	106.37
839	55.06	19.60	0.20	1.44	48.59	106.49
840	55.14	19.60	0.20	1.53	49.28	106.73
841	55.22	19.60	0.22	1.53	49.96	107.08
842	55.27	19.60	0.23	1.53	50.29	107.54
843	55.37	19.60	0.27	1.53	50.62	108.10
844	55.42	20.22	0.29	1.53	50.87	108.66
845	55.47	20.58	0.32	1.44	51.18	109.15
846	55.53	21.92	0.35	1.44	51.50	109.51
847	55.58	22.55	0.37	1.44	51.77	109.79
848	55.67	22.73	0.38	1.44	51.82	109.92
849	55.72	22.10	0.37	1.44	51.80	109.95
850	55.81	21.12	0.35	1.44	51.69	109.88
851	55.86	20.85	0.34	1.44	51.62	109.67
852	55.92	20.58	0.32	1.44	51.73	109.56
853	56.01	20.58	0.30	1.44	51.93	109.55
854	56.05	20.58	0.29	1.44	51.83	109.75
855	56.11	20.67	0.27	1.44	51.74	110.27
856	56.21	21.39	0.33	1.44	52.45	110.96
857	56.26	22.10	0.38	1.34	52.51	111.81
858	56.32	23.98	0.44	1.34	51.84	112.81
859	56.41	25.59	0.55	1.34	50.69	113.80
860	56.46	23.80	0.64	1.34	49.37	114.72
861	56.50	27.47	0.71	1.72	47.76	115.44
862	56.59	32.13	0.79	1.82	46.42	116.14
863	56.65	35.17	0.82	1.82	45.50	116.78
864	56.70	36.60	0.81	1.82	45.11	117.48

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
865	56.78	38.03	0.77	1.82	43.36	118.28
866	56.85	38.30	0.84	1.82	41.52	119.08
867	56.89	38.03	0.91	1.92	39.64	119.90
868	56.98	38.03	1.14	1.92	38.22	120.67
869	57.04	48.06	1.29	2.01	37.23	121.43
870	57.09	55.04	1.41	1.92	36.74	122.19
871	57.16	63.27	1.56	1.72	36.34	122.87
872	57.24	64.43	1.63	1.92	35.69	123.46
873	57.29	63.36	1.70	1.82	34.18	123.85
874	57.37	61.39	1.80	1.92	33.05	124.09
875	57.42	59.87	1.83	1.92	32.26	124.22
876	57.49	61.75	1.80	1.92	31.97	124.24
877	57.59	69.62	1.63	1.82	31.83	124.21
878	57.64	71.95	1.56	1.82	31.85	124.07
879	57.69	71.41	1.53	1.82	32.07	123.77
880	57.77	68.64	1.55	1.82	32.27	123.34
881	57.82	66.22	1.55	1.82	32.97	122.78
882	57.89	58.88	1.46	1.82	34.71	122.12
883	57.97	49.04	1.31	1.82	37.10	121.39
884	58.03	44.39	1.14	1.82	40.03	120.50
885	58.09	36.15	1.01	1.92	43.22	119.41
886	58.17	29.08	0.84	1.92	46.83	118.15
887	58.21	26.49	0.77	1.92	50.30	116.81
888	58.28	23.09	0.64	2.01	53.05	115.50
889	58.37	21.48	0.50	2.01	55.93	114.49
890	58.40	21.12	0.45	2.11	57.94	113.81
891	58.48	20.67	0.40	2.11	59.77	113.77
892	58.53	20.67	0.38	2.11	59.68	114.24
893	58.63	21.84	0.52	2.20	56.74	114.93
894	58.67	21.84	0.64	2.20	53.60	115.67
895	58.73	21.92	0.87	2.20	51.26	116.31
896	58.82	30.87	1.07	2.30	49.88	116.88
897	58.89	41.34	1.01	2.20	49.34	117.25
898	58.93	42.96	0.93	2.11	49.11	117.34
899	59.00	39.55	0.86	2.01	48.86	117.28
900	59.06	34.90	0.81	2.11	47.97	116.90
901	59.13	28.55	0.68	2.01	47.79	116.10
902	59.22	24.43	0.59	2.11	49.44	115.18
903	59.28	22.64	0.57	2.20	51.77	114.23
904	59.33	22.28	0.50	2.20	53.92	113.30
905	59.41	21.84	0.41	2.20	55.08	112.42
906	59.47	21.66	0.39	2.30	55.16	111.80
907	59.52	21.66	0.38	2.87	54.26	111.42
908	59.61	21.48	0.36	2.87	52.83	111.14
909	59.67	22.73	0.36	2.97	51.73	111.06
910	59.72	23.18	0.37	2.97	51.04	111.30
911	59.78	24.70	0.39	2.97	50.45	111.66
912	59.87	25.77	0.41	2.97	49.85	111.99

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
913	59.92	25.95	0.44	3.06	47.09	111.35
914	60.00	26.76	0.50	2.97	44.67	110.62
915	60.05	27.38	0.54	3.06	42.16	109.76
916	60.11	27.38	0.52	2.97	39.88	108.69
917	60.21	28.19	0.00	3.06	37.59	107.34
918	60.25	27.74	0.00	3.06	34.86	105.53
919	60.31	28.28	0.00	3.06	31.28	102.72
920	60.40	27.38	0.00	3.06	26.86	97.50
921	60.43	26.94	0.00	3.06	N/A	87.36
922	60.51	27.12	0.00	3.16	N/A	87.36

Abbreviations

Depth: Depth from free surface, at which CPT was performed (ft)
q_c: Measured cone resistance (tsf)
f_s: Sleeve friction resistance (tsf)
u: Pore pressure (tsf)
Fines content: Percentage of fines in soil (%)
Unit weight: Bulk soil unit weight (pcf)

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data ::

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
1	0.10	0.01	0.00	0.01	1.00	0.358	1.34	0.266	1.00	1.00	2.000	No
2	0.15	0.01	0.00	0.01	1.00	0.358	1.34	0.266	1.00	1.00	2.000	No
3	0.23	0.01	0.00	0.01	1.00	0.358	1.34	0.266	1.00	1.00	2.000	No
4	0.30	0.02	0.00	0.02	1.00	0.358	1.34	0.266	1.00	1.00	2.000	No
5	0.34	0.02	0.00	0.02	1.00	0.358	1.34	0.266	1.00	1.00	2.000	No
6	0.39	0.02	0.00	0.02	1.00	0.358	1.34	0.266	1.00	1.00	2.000	No
7	0.50	0.03	0.00	0.03	1.00	0.358	1.34	0.266	1.00	1.00	2.000	No
8	0.53	0.03	0.00	0.03	1.00	0.358	1.34	0.266	1.00	1.00	2.000	No
9	0.60	0.04	0.00	0.04	1.00	0.358	1.34	0.266	1.00	1.00	2.000	No
10	0.69	0.04	0.00	0.04	1.00	0.358	1.34	0.266	1.00	1.00	2.000	No
11	0.72	0.04	0.00	0.04	1.00	0.358	1.34	0.266	1.00	1.00	2.000	No
12	0.80	0.05	0.00	0.05	1.00	0.357	1.34	0.266	1.00	1.00	2.000	No
13	0.87	0.05	0.00	0.05	1.00	0.357	1.34	0.266	1.00	1.00	2.000	No
14	0.92	0.06	0.00	0.06	1.00	0.357	1.34	0.266	1.00	1.00	2.000	No
15	1.00	0.06	0.00	0.06	1.00	0.357	1.34	0.266	1.00	1.00	2.000	No
16	1.08	0.07	0.00	0.07	1.00	0.357	1.34	0.266	1.00	1.00	2.000	No
17	1.12	0.07	0.00	0.07	1.00	0.357	1.34	0.266	1.00	1.00	2.000	No
18	1.20	0.07	0.00	0.07	1.00	0.357	1.34	0.266	1.00	1.00	2.000	No
19	1.30	0.08	0.00	0.08	1.00	0.357	1.34	0.266	1.00	1.00	2.000	No
20	1.34	0.08	0.00	0.08	1.00	0.357	1.34	0.266	1.00	1.00	2.000	No
21	1.40	0.08	0.00	0.08	1.00	0.357	1.34	0.266	1.00	1.00	2.000	No
22	1.49	0.09	0.00	0.09	1.00	0.357	1.34	0.265	1.00	1.00	2.000	No
23	1.54	0.09	0.00	0.09	1.00	0.357	1.34	0.265	1.00	1.00	2.000	No
24	1.59	0.10	0.00	0.10	1.00	0.357	1.34	0.265	1.00	1.00	2.000	No
25	1.68	0.10	0.00	0.10	1.00	0.357	1.34	0.265	1.00	1.00	2.000	No
26	1.74	0.11	0.00	0.11	1.00	0.357	1.34	0.265	1.00	1.00	2.000	No
27	1.79	0.11	0.00	0.11	1.00	0.357	1.34	0.265	1.00	1.00	2.000	No
28	1.87	0.11	0.00	0.11	1.00	0.357	1.34	0.265	1.00	1.00	2.000	No
29	1.94	0.12	0.00	0.12	1.00	0.357	1.34	0.265	1.00	1.00	2.000	No
30	1.98	0.12	0.00	0.12	1.00	0.357	1.34	0.265	1.00	1.00	2.000	No
31	2.04	0.12	0.00	0.12	1.00	0.357	1.34	0.265	1.00	1.00	2.000	No
32	2.13	0.13	0.00	0.13	1.00	0.356	1.34	0.265	1.00	1.00	2.000	No
33	2.17	0.13	0.00	0.13	1.00	0.356	1.34	0.265	1.00	1.00	2.000	No
34	2.24	0.13	0.00	0.13	1.00	0.356	1.34	0.265	1.00	1.00	2.000	No
35	2.33	0.14	0.00	0.14	1.00	0.356	1.34	0.265	1.00	1.00	2.000	No
36	2.36	0.14	0.00	0.14	1.00	0.356	1.34	0.265	1.00	1.00	2.000	No
37	2.43	0.15	0.00	0.15	1.00	0.356	1.34	0.265	1.00	1.00	2.000	No
38	2.52	0.15	0.00	0.15	1.00	0.356	1.34	0.265	1.00	1.00	2.000	No
39	2.56	0.15	0.00	0.15	1.00	0.356	1.34	0.265	1.00	1.00	2.000	No
40	2.64	0.16	0.00	0.16	1.00	0.356	1.34	0.265	1.00	1.00	2.000	No
41	2.74	0.16	0.00	0.16	1.00	0.356	1.34	0.265	1.00	1.00	2.000	No
42	2.78	0.17	0.00	0.17	1.00	0.356	1.34	0.265	1.00	1.00	2.000	No
43	2.83	0.17	0.00	0.17	1.00	0.356	1.34	0.265	1.00	1.00	2.000	No
44	2.90	0.17	0.00	0.17	1.00	0.356	1.34	0.265	1.00	1.00	2.000	No
45	2.98	0.18	0.00	0.18	1.00	0.356	1.34	0.265	1.00	1.00	2.000	No
46	3.03	0.18	0.00	0.18	0.99	0.356	1.34	0.265	1.00	1.00	2.000	No
47	3.10	0.18	0.00	0.18	0.99	0.356	1.34	0.264	1.00	1.00	2.000	No
48	3.18	0.19	0.00	0.19	0.99	0.356	1.34	0.264	1.00	1.00	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
49	3.23	0.19	0.00	0.19	0.99	0.356	1.34	0.264	1.00	1.00	2.000	No
50	3.29	0.19	0.00	0.19	0.99	0.355	1.34	0.264	1.00	1.00	2.000	No
51	3.38	0.20	0.00	0.20	0.99	0.355	1.34	0.264	1.00	1.00	2.000	No
52	3.42	0.20	0.00	0.20	0.99	0.355	1.34	0.264	1.00	1.00	2.000	No
53	3.51	0.21	0.00	0.21	0.99	0.355	1.34	0.264	1.00	1.00	2.000	No
54	3.58	0.21	0.00	0.21	0.99	0.355	1.34	0.264	1.00	1.00	2.000	No
55	3.62	0.21	0.00	0.21	0.99	0.355	1.34	0.264	1.00	1.00	2.000	No
56	3.69	0.22	0.00	0.22	0.99	0.355	1.34	0.264	1.00	1.00	2.000	No
57	3.77	0.22	0.00	0.22	0.99	0.355	1.34	0.264	1.00	1.00	2.000	No
58	3.82	0.22	0.00	0.22	0.99	0.355	1.34	0.264	1.00	1.00	2.000	No
59	3.89	0.23	0.00	0.23	0.99	0.355	1.34	0.264	1.00	1.00	2.000	No
60	3.97	0.23	0.00	0.23	0.99	0.355	1.34	0.264	1.00	1.00	2.000	No
61	4.03	0.24	0.00	0.24	0.99	0.355	1.34	0.264	1.00	1.00	2.000	No
62	4.10	0.24	0.00	0.24	0.99	0.355	1.34	0.264	1.00	1.00	2.000	No
63	4.15	0.24	0.00	0.24	0.99	0.355	1.34	0.264	1.00	1.00	2.000	No
64	4.24	0.25	0.00	0.25	0.99	0.355	1.34	0.264	1.00	1.00	2.000	No
65	4.29	0.25	0.00	0.25	0.99	0.355	1.34	0.264	1.00	1.00	2.000	No
66	4.35	0.25	0.00	0.25	0.99	0.355	1.34	0.264	1.00	1.00	2.000	No
67	4.44	0.26	0.00	0.26	0.99	0.354	1.34	0.264	1.00	1.00	2.000	No
68	4.48	0.26	0.00	0.26	0.99	0.354	1.34	0.264	1.00	1.00	2.000	No
69	4.54	0.26	0.00	0.26	0.99	0.354	1.34	0.264	1.00	1.00	2.000	No
70	4.61	0.27	0.00	0.27	0.99	0.354	1.34	0.264	1.00	1.00	2.000	No
71	4.69	0.27	0.00	0.27	0.99	0.354	1.34	0.263	1.00	1.00	2.000	No
72	4.74	0.28	0.00	0.28	0.99	0.354	1.34	0.263	1.00	1.00	2.000	No
73	4.82	0.28	0.00	0.28	0.99	0.354	1.34	0.263	1.00	1.00	2.000	No
74	4.86	0.28	0.00	0.28	0.99	0.354	1.34	0.263	1.00	1.00	2.000	No
75	4.94	0.29	0.00	0.29	0.99	0.354	1.34	0.263	1.00	1.00	2.000	No
76	5.02	0.29	0.00	0.29	0.99	0.354	1.34	0.263	1.00	1.00	2.000	No
77	5.09	0.30	0.00	0.30	0.99	0.354	1.34	0.263	1.00	1.00	2.000	No
78	5.13	0.30	0.00	0.30	0.99	0.354	1.34	0.263	1.00	1.00	2.000	No
79	5.23	0.30	0.00	0.30	0.99	0.354	1.34	0.263	1.00	1.00	2.000	No
80	5.28	0.31	0.00	0.31	0.99	0.354	1.34	0.263	1.00	1.00	2.000	No
81	5.33	0.31	0.00	0.31	0.99	0.354	1.34	0.263	1.00	1.00	2.000	No
82	5.39	0.31	0.00	0.31	0.99	0.354	1.34	0.263	1.00	1.00	2.000	No
83	5.48	0.32	0.00	0.32	0.99	0.354	1.34	0.263	1.00	1.00	2.000	No
84	5.52	0.32	0.00	0.32	0.99	0.354	1.34	0.263	1.00	1.00	2.000	No
85	5.58	0.32	0.00	0.32	0.99	0.354	1.34	0.263	1.00	1.00	2.000	No
86	5.67	0.33	0.00	0.33	0.99	0.353	1.34	0.263	1.00	1.00	2.000	No
87	5.73	0.33	0.00	0.33	0.99	0.353	1.34	0.263	1.00	1.00	2.000	No
88	5.78	0.33	0.00	0.33	0.99	0.353	1.34	0.263	1.00	1.00	2.000	No
89	5.88	0.34	0.00	0.34	0.99	0.353	1.34	0.263	1.00	1.00	2.000	No
90	5.92	0.34	0.00	0.34	0.99	0.353	1.34	0.263	1.00	1.00	2.000	No
91	5.97	0.34	0.00	0.34	0.99	0.353	1.34	0.263	1.00	1.00	2.000	No
92	6.08	0.35	0.00	0.35	0.99	0.353	1.34	0.263	1.00	1.00	2.000	No
93	6.11	0.35	0.00	0.35	0.99	0.353	1.34	0.263	1.00	1.00	2.000	No
94	6.18	0.35	0.00	0.35	0.99	0.353	1.34	0.263	1.00	1.00	2.000	No
95	6.27	0.36	0.00	0.36	0.99	0.353	1.34	0.263	1.00	1.00	2.000	No
96	6.33	0.36	0.00	0.36	0.99	0.353	1.34	0.262	1.00	1.00	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
97	6.38	0.37	0.00	0.37	0.99	0.353	1.34	0.262	1.00	1.00	2.000	No
98	6.44	0.37	0.00	0.37	0.99	0.353	1.34	0.262	1.00	1.00	2.000	No
99	6.50	0.37	0.00	0.37	0.99	0.353	1.34	0.262	1.00	1.00	2.000	No
100	6.57	0.38	0.00	0.38	0.99	0.353	1.34	0.262	1.00	1.00	2.000	No
101	6.67	0.38	0.00	0.38	0.99	0.353	1.34	0.262	1.00	1.00	2.000	No
102	6.72	0.38	0.00	0.38	0.99	0.353	1.34	0.262	1.00	1.00	2.000	No
103	6.76	0.39	0.00	0.39	0.99	0.353	1.34	0.262	1.00	1.00	2.000	No
104	6.83	0.39	0.00	0.39	0.99	0.353	1.34	0.262	1.00	1.00	2.000	No
105	6.92	0.39	0.00	0.39	0.99	0.352	1.34	0.262	1.00	1.00	2.000	No
106	6.97	0.40	0.00	0.40	0.99	0.352	1.34	0.262	1.00	1.00	2.000	No
107	7.04	0.40	0.00	0.40	0.99	0.352	1.34	0.262	1.00	1.00	2.000	No
108	7.12	0.40	0.00	0.40	0.99	0.352	1.34	0.262	1.00	1.00	2.000	No
109	7.16	0.41	0.00	0.41	0.99	0.352	1.34	0.262	1.00	1.00	2.000	No
110	7.25	0.41	0.00	0.41	0.99	0.352	1.34	0.262	1.00	1.00	2.000	No
111	7.32	0.42	0.00	0.42	0.98	0.352	1.34	0.262	1.00	1.00	2.000	No
112	7.37	0.42	0.00	0.42	0.98	0.352	1.34	0.262	1.00	1.00	2.000	No
113	7.43	0.42	0.00	0.42	0.98	0.352	1.34	0.262	1.00	1.00	2.000	No
114	7.52	0.43	0.00	0.43	0.98	0.352	1.34	0.262	1.00	1.00	2.000	No
115	7.56	0.43	0.00	0.43	0.98	0.352	1.34	0.262	1.00	1.00	2.000	No
116	7.63	0.43	0.00	0.43	0.98	0.352	1.34	0.262	1.00	1.00	2.000	No
117	7.71	0.44	0.00	0.44	0.98	0.352	1.34	0.262	1.00	1.00	2.000	No
118	7.75	0.44	0.00	0.44	0.98	0.352	1.34	0.262	1.00	1.00	2.000	No
119	7.83	0.44	0.00	0.44	0.98	0.352	1.34	0.262	1.00	1.00	2.000	No
120	7.88	0.45	0.00	0.45	0.98	0.352	1.34	0.262	1.00	1.00	2.000	No
121	7.97	0.45	0.00	0.45	0.98	0.352	1.34	0.262	1.00	1.00	2.000	No
122	8.01	0.45	0.00	0.45	0.98	0.352	1.34	0.261	1.00	1.00	2.000	No
123	8.08	0.46	0.00	0.46	0.98	0.352	1.34	0.261	1.00	1.00	2.000	No
124	8.18	0.46	0.00	0.46	0.98	0.351	1.34	0.261	1.00	1.00	2.000	No
125	8.22	0.46	0.00	0.46	0.98	0.351	1.34	0.261	1.00	1.00	2.000	No
126	8.28	0.47	0.00	0.47	0.98	0.351	1.34	0.261	1.00	1.00	2.000	No
127	8.35	0.47	0.00	0.47	0.98	0.351	1.34	0.261	1.00	1.00	2.000	No
128	8.43	0.48	0.00	0.48	0.98	0.351	1.34	0.261	1.00	1.00	2.000	No
129	8.48	0.48	0.00	0.48	0.98	0.351	1.34	0.261	1.00	1.00	2.000	No
130	8.56	0.48	0.00	0.48	0.98	0.351	1.34	0.261	1.00	1.00	2.000	No
131	8.63	0.49	0.00	0.49	0.98	0.351	1.34	0.261	1.00	1.00	2.000	No
132	8.68	0.49	0.00	0.49	0.98	0.351	1.34	0.261	1.00	1.00	2.000	No
133	8.76	0.49	0.00	0.49	0.98	0.351	1.34	0.261	1.00	1.00	2.000	No
134	8.80	0.50	0.00	0.50	0.98	0.351	1.34	0.261	1.00	1.00	2.000	No
135	8.88	0.50	0.00	0.50	0.98	0.351	1.34	0.261	1.00	1.00	2.000	No
136	8.94	0.50	0.00	0.50	0.98	0.351	1.34	0.261	1.00	1.00	2.000	No
137	8.99	0.51	0.00	0.51	0.98	0.351	1.34	0.261	1.00	1.00	2.000	No
138	9.07	0.51	0.00	0.51	0.98	0.352	1.34	0.262	1.00	1.00	0.262	No
139	9.14	0.51	0.00	0.51	0.98	0.354	1.34	0.263	1.00	1.00	0.263	No
140	9.22	0.52	0.01	0.51	0.98	0.355	1.34	0.264	1.00	1.00	0.264	No
141	9.27	0.52	0.01	0.51	0.98	0.356	1.34	0.265	1.00	1.00	0.265	No
142	9.37	0.53	0.01	0.51	0.98	0.358	1.34	0.267	1.00	1.00	0.267	No
143	9.42	0.53	0.01	0.52	0.98	0.359	1.34	0.267	1.00	1.00	0.267	No
144	9.47	0.53	0.01	0.52	0.98	0.360	1.34	0.268	1.00	1.00	0.268	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
145	9.52	0.53	0.02	0.52	0.98	0.361	1.34	0.269	1.00	1.00	0.269	No
146	9.62	0.54	0.02	0.52	0.98	0.363	1.34	0.270	1.00	1.00	0.270	No
147	9.67	0.54	0.02	0.52	0.98	0.364	1.34	0.271	1.00	1.00	0.271	No
148	9.73	0.55	0.02	0.52	0.98	0.366	1.34	0.272	1.00	1.00	0.272	No
149	9.82	0.55	0.03	0.52	0.98	0.367	1.34	0.273	1.00	1.00	0.273	No
150	9.86	0.55	0.03	0.52	0.98	0.368	1.34	0.274	1.00	1.00	0.274	No
151	9.92	0.55	0.03	0.53	0.98	0.369	1.34	0.275	1.00	1.00	0.275	No
152	10.02	0.56	0.03	0.53	0.98	0.371	1.34	0.276	1.00	1.00	0.276	No
153	10.06	0.56	0.03	0.53	0.98	0.372	1.34	0.277	1.00	1.00	0.277	No
154	10.12	0.57	0.03	0.53	0.98	0.373	1.34	0.277	1.00	1.00	0.277	No
155	10.21	0.57	0.04	0.53	0.98	0.375	1.34	0.279	1.00	1.00	0.279	No
156	10.25	0.57	0.04	0.53	0.98	0.375	1.34	0.279	1.00	1.00	0.279	No
157	10.31	0.58	0.04	0.53	0.98	0.377	1.34	0.280	1.00	1.00	0.280	No
158	10.41	0.58	0.04	0.54	0.98	0.378	1.34	0.281	1.00	1.00	0.281	No
159	10.45	0.58	0.05	0.54	0.98	0.379	1.34	0.282	1.00	1.00	0.282	No
160	10.52	0.59	0.05	0.54	0.98	0.380	1.34	0.283	1.00	1.00	0.283	No
161	10.61	0.59	0.05	0.54	0.98	0.382	1.34	0.284	1.00	1.00	0.284	No
162	10.64	0.59	0.05	0.54	0.98	0.383	1.34	0.284	1.00	1.00	0.284	No
163	10.71	0.60	0.05	0.54	0.98	0.384	1.34	0.285	1.00	1.00	0.285	No
164	10.81	0.60	0.06	0.55	0.98	0.385	1.34	0.287	1.00	1.00	0.287	No
165	10.85	0.61	0.06	0.55	0.98	0.386	1.34	0.287	1.00	1.00	0.287	No
166	10.91	0.61	0.06	0.55	0.98	0.387	1.34	0.288	1.00	1.00	0.288	No
167	10.96	0.61	0.06	0.55	0.98	0.388	1.34	0.289	1.00	1.00	0.289	No
168	11.03	0.62	0.06	0.55	0.98	0.389	1.34	0.290	1.00	1.00	0.290	No
169	11.10	0.62	0.07	0.55	0.98	0.390	1.34	0.290	1.00	1.00	0.290	No
170	11.20	0.63	0.07	0.56	0.98	0.392	1.34	0.292	1.00	1.00	0.292	No
171	11.24	0.63	0.07	0.56	0.98	0.393	1.34	0.292	1.00	1.00	0.292	No
172	11.30	0.63	0.07	0.56	0.98	0.394	1.34	0.293	1.00	1.00	0.293	No
173	11.36	0.63	0.07	0.56	0.98	0.395	1.34	0.294	1.00	1.00	0.294	No
174	11.43	0.64	0.08	0.56	0.98	0.396	1.34	0.294	1.00	1.00	0.294	No
175	11.50	0.64	0.08	0.56	0.98	0.397	1.34	0.295	1.00	1.00	0.295	No
176	11.58	0.65	0.08	0.57	0.98	0.398	1.34	0.296	1.00	1.00	0.296	No
177	11.63	0.65	0.08	0.57	0.98	0.399	1.34	0.297	1.00	1.00	0.297	No
178	11.70	0.65	0.08	0.57	0.98	0.400	1.34	0.298	1.00	1.00	0.298	No
179	11.79	0.66	0.09	0.57	0.98	0.402	1.34	0.299	1.00	1.00	0.299	No
180	11.84	0.66	0.09	0.57	0.98	0.402	1.34	0.299	1.00	1.00	0.299	No
181	11.90	0.67	0.09	0.58	0.98	0.403	1.34	0.300	1.00	1.00	0.300	No
182	11.98	0.67	0.09	0.58	0.97	0.405	1.34	0.301	1.00	1.00	0.301	No
183	12.02	0.67	0.09	0.58	0.97	0.405	1.34	0.301	1.00	1.00	0.301	No
184	12.09	0.68	0.10	0.58	0.97	0.406	1.34	0.302	1.00	1.00	0.302	No
185	12.14	0.68	0.10	0.58	0.97	0.407	1.34	0.303	1.00	1.00	0.303	No
186	12.21	0.68	0.10	0.58	0.97	0.408	1.34	0.304	1.00	1.00	0.304	No
187	12.29	0.69	0.10	0.59	0.97	0.409	1.34	0.305	1.00	1.00	0.305	No
188	12.34	0.69	0.10	0.59	0.97	0.410	1.34	0.305	1.00	1.00	0.305	No
189	12.44	0.70	0.11	0.59	0.97	0.412	1.34	0.306	1.00	1.00	0.306	No
190	12.49	0.70	0.11	0.59	0.97	0.412	1.34	0.307	1.00	1.00	0.307	No
191	12.57	0.70	0.11	0.59	0.97	0.414	1.34	0.308	1.00	1.00	0.308	No
192	12.64	0.71	0.11	0.59	0.97	0.415	1.34	0.308	1.00	1.00	0.308	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
193	12.68	0.71	0.11	0.59	0.97	0.415	1.34	0.309	1.00	1.00	0.309	No
194	12.73	0.71	0.12	0.60	0.97	0.416	1.34	0.309	1.00	1.00	0.309	No
195	12.84	0.72	0.12	0.60	0.97	0.417	1.34	0.311	1.00	1.00	0.311	No
196	12.89	0.72	0.12	0.60	0.97	0.418	1.34	0.311	1.00	1.00	0.311	No
197	12.98	0.73	0.12	0.60	0.97	0.419	1.34	0.312	1.00	1.00	0.312	No
198	13.00	0.73	0.12	0.60	0.97	0.420	1.34	0.312	1.00	1.00	0.312	No
199	13.08	0.73	0.13	0.60	0.97	0.421	1.34	0.313	1.00	1.00	0.313	No
200	13.14	0.74	0.13	0.61	0.97	0.422	1.34	0.314	1.00	1.00	0.314	No
201	13.23	0.74	0.13	0.61	0.97	0.423	1.34	0.315	1.00	1.00	0.315	No
202	13.27	0.74	0.13	0.61	0.97	0.424	1.34	0.315	1.00	1.00	0.315	No
203	13.34	0.75	0.14	0.61	0.97	0.424	1.34	0.316	1.00	1.00	0.316	No
204	13.43	0.75	0.14	0.61	0.97	0.426	1.34	0.317	1.00	1.00	0.317	No
205	13.47	0.75	0.14	0.61	0.97	0.426	1.34	0.317	1.00	1.00	0.317	No
206	13.54	0.76	0.14	0.62	0.97	0.427	1.34	0.318	1.00	1.00	0.318	No
207	13.63	0.76	0.14	0.62	0.97	0.428	1.34	0.319	1.00	1.00	0.319	No
208	13.67	0.77	0.15	0.62	0.97	0.429	1.34	0.319	1.00	1.00	0.319	No
209	13.72	0.77	0.15	0.62	0.97	0.430	1.34	0.319	1.00	1.00	0.319	No
210	13.83	0.77	0.15	0.62	0.97	0.431	1.34	0.321	1.00	1.00	0.321	No
211	13.88	0.78	0.15	0.63	0.97	0.432	1.34	0.321	1.00	1.00	0.321	No
212	13.94	0.78	0.15	0.63	0.97	0.432	1.34	0.322	1.00	1.00	0.322	No
213	13.98	0.78	0.16	0.63	0.97	0.433	1.34	0.322	1.00	1.00	0.322	No
214	14.06	0.79	0.16	0.63	0.97	0.434	1.34	0.323	1.00	1.00	0.323	No
215	14.14	0.79	0.16	0.63	0.97	0.435	1.34	0.323	1.00	1.00	0.323	No
216	14.18	0.79	0.16	0.63	0.97	0.435	1.34	0.324	1.00	1.00	0.324	No
217	14.26	0.80	0.16	0.64	0.97	0.436	1.34	0.325	1.00	1.00	0.325	No
218	14.33	0.80	0.17	0.64	0.97	0.437	1.34	0.325	1.00	1.00	0.325	No
219	14.37	0.81	0.17	0.64	0.97	0.438	1.34	0.326	1.00	1.00	0.326	No
220	14.45	0.81	0.17	0.64	0.97	0.439	1.34	0.326	1.00	1.00	0.326	No
221	14.54	0.81	0.17	0.64	0.97	0.440	1.34	0.327	1.00	1.00	0.327	No
222	14.61	0.82	0.18	0.64	0.97	0.441	1.34	0.328	1.00	1.00	0.328	No
223	14.65	0.82	0.18	0.64	0.97	0.441	1.34	0.328	1.00	1.00	0.328	No
224	14.74	0.83	0.18	0.65	0.97	0.442	1.34	0.329	1.00	1.00	0.329	No
225	14.80	0.83	0.18	0.65	0.97	0.443	1.34	0.330	1.00	1.00	0.330	No
226	14.85	0.83	0.18	0.65	0.97	0.444	1.34	0.330	1.00	1.00	0.330	No
227	14.90	0.84	0.18	0.65	0.97	0.444	1.34	0.330	1.00	1.00	0.330	No
228	15.00	0.84	0.19	0.65	0.97	0.445	1.34	0.331	1.00	1.00	0.331	No
229	15.05	0.84	0.19	0.65	0.97	0.446	1.34	0.332	1.00	1.00	0.332	No
230	15.10	0.85	0.19	0.66	0.97	0.447	1.34	0.332	1.00	1.00	0.332	No
231	15.17	0.85	0.19	0.66	0.97	0.447	1.34	0.333	1.00	1.00	0.333	No
232	15.25	0.85	0.20	0.66	0.97	0.448	1.34	0.334	1.00	1.00	0.334	No
233	15.30	0.86	0.20	0.66	0.97	0.449	1.34	0.334	1.00	1.00	0.334	No
234	15.36	0.86	0.20	0.66	0.97	0.450	1.34	0.334	1.00	1.00	0.334	No
235	15.45	0.87	0.20	0.66	0.97	0.451	1.34	0.335	1.00	1.00	0.335	No
236	15.49	0.87	0.20	0.66	0.97	0.451	1.34	0.336	1.00	1.00	0.336	No
237	15.57	0.87	0.20	0.67	0.97	0.452	1.34	0.336	1.00	1.00	0.336	No
238	15.64	0.88	0.21	0.67	0.97	0.453	1.34	0.337	1.00	1.00	0.337	No
239	15.69	0.88	0.21	0.67	0.97	0.453	1.34	0.337	1.00	1.00	0.337	No
240	15.77	0.88	0.21	0.67	0.97	0.454	1.34	0.338	1.00	1.00	0.338	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
241	15.85	0.89	0.21	0.67	0.97	0.455	1.34	0.339	1.00	1.00	0.339	No
242	15.89	0.89	0.21	0.67	0.97	0.456	1.34	0.339	1.00	1.00	0.339	No
243	15.99	0.89	0.22	0.68	0.97	0.457	1.34	0.340	1.00	1.00	0.340	No
244	16.05	0.90	0.22	0.68	0.97	0.458	1.34	0.340	1.00	1.00	0.340	No
245	16.09	0.90	0.22	0.68	0.97	0.458	1.34	0.341	1.00	1.00	0.341	No
246	16.16	0.90	0.22	0.68	0.97	0.459	1.34	0.341	1.00	1.00	0.341	No
247	16.24	0.91	0.23	0.68	0.97	0.460	1.34	0.342	1.00	1.00	0.342	No
248	16.30	0.91	0.23	0.68	0.97	0.460	1.34	0.342	1.00	1.00	0.342	No
249	16.34	0.91	0.23	0.68	0.97	0.461	1.34	0.343	1.00	1.00	0.343	No
250	16.44	0.92	0.23	0.69	0.97	0.462	1.34	0.343	1.00	1.00	0.343	No
251	16.48	0.92	0.23	0.69	0.97	0.462	1.34	0.344	1.00	1.00	0.344	No
252	16.54	0.92	0.24	0.69	0.97	0.463	1.34	0.344	1.00	1.00	0.344	No
253	16.63	0.93	0.24	0.69	0.96	0.464	1.34	0.345	1.00	1.00	0.345	No
254	16.69	0.93	0.24	0.69	0.96	0.464	1.34	0.345	1.00	1.00	0.345	No
255	16.74	0.94	0.24	0.69	0.96	0.465	1.34	0.346	1.00	1.00	0.346	No
256	16.82	0.94	0.24	0.70	0.96	0.466	1.34	0.346	1.00	1.00	0.346	No
257	16.90	0.94	0.25	0.70	0.96	0.467	1.34	0.347	1.00	1.00	0.347	No
258	16.94	0.95	0.25	0.70	0.96	0.467	1.34	0.347	1.00	1.00	0.347	No
259	17.03	0.95	0.25	0.70	0.96	0.468	1.34	0.348	1.00	1.00	0.348	No
260	17.07	0.95	0.25	0.70	0.96	0.468	1.34	0.348	1.00	1.00	0.348	No
261	17.13	0.96	0.25	0.70	0.96	0.469	1.34	0.349	1.00	1.00	0.349	No
262	17.21	0.96	0.26	0.70	0.96	0.470	1.34	0.349	1.00	1.00	0.349	No
263	17.26	0.96	0.26	0.70	0.96	0.470	1.34	0.350	1.00	1.00	0.350	No
264	17.33	0.97	0.26	0.71	0.96	0.471	1.34	0.350	1.00	1.00	0.350	No
265	17.41	0.97	0.26	0.71	0.96	0.472	1.34	0.351	1.00	1.00	0.351	No
266	17.48	0.97	0.26	0.71	0.96	0.473	1.34	0.351	1.00	1.00	0.351	No
267	17.53	0.98	0.27	0.71	0.96	0.473	1.34	0.352	1.00	1.00	0.352	No
268	17.61	0.98	0.27	0.71	0.96	0.474	1.34	0.352	1.00	1.00	0.352	No
269	17.67	0.98	0.27	0.71	0.96	0.474	1.34	0.353	1.00	1.00	0.353	No
270	17.72	0.99	0.27	0.72	0.96	0.475	1.34	0.353	1.00	1.00	0.353	No
271	17.82	0.99	0.28	0.72	0.96	0.476	1.34	0.354	1.00	1.00	0.354	No
272	17.88	1.00	0.28	0.72	0.96	0.476	1.34	0.354	1.00	1.00	0.354	No
273	17.92	1.00	0.28	0.72	0.96	0.477	1.34	0.355	1.00	1.00	0.355	No
274	18.02	1.00	0.28	0.72	0.96	0.478	1.34	0.355	1.00	1.00	0.355	No
275	18.07	1.01	0.28	0.72	0.96	0.478	1.34	0.356	1.00	1.00	0.356	No
276	18.14	1.01	0.29	0.73	0.96	0.479	1.34	0.356	1.00	1.00	0.356	No
277	18.20	1.01	0.29	0.73	0.96	0.479	1.34	0.357	1.00	1.00	0.357	No
278	18.27	1.02	0.29	0.73	0.96	0.480	1.34	0.357	1.00	1.00	0.357	No
279	18.32	1.02	0.29	0.73	0.96	0.480	1.34	0.357	1.00	1.00	0.357	No
280	18.38	1.02	0.29	0.73	0.96	0.481	1.34	0.358	1.00	1.00	0.358	No
281	18.47	1.03	0.30	0.73	0.96	0.482	1.34	0.358	1.00	1.00	0.358	No
282	18.51	1.03	0.30	0.73	0.96	0.482	1.34	0.359	1.00	1.00	0.359	No
283	18.57	1.03	0.30	0.74	0.96	0.483	1.34	0.359	1.00	1.00	0.359	No
284	18.67	1.04	0.30	0.74	0.96	0.484	1.34	0.360	1.00	1.00	0.360	No
285	18.71	1.04	0.30	0.74	0.96	0.484	1.34	0.360	1.00	1.00	0.360	No
286	18.81	1.05	0.31	0.74	0.96	0.485	1.34	0.361	1.00	1.00	0.361	No
287	18.86	1.05	0.31	0.74	0.96	0.485	1.34	0.361	1.00	1.00	0.361	No
288	18.91	1.05	0.31	0.74	0.96	0.486	1.34	0.361	1.00	1.00	0.361	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
289	18.97	1.06	0.31	0.74	0.96	0.486	1.34	0.362	1.00	1.00	0.362	No
290	19.06	1.06	0.31	0.75	0.96	0.487	1.34	0.362	1.00	1.00	0.362	No
291	19.11	1.06	0.32	0.75	0.96	0.487	1.34	0.363	1.00	1.00	0.363	No
292	19.21	1.07	0.32	0.75	0.96	0.488	1.34	0.363	1.00	1.00	0.363	No
293	19.27	1.07	0.32	0.75	0.96	0.489	1.34	0.364	1.00	1.00	0.364	No
294	19.31	1.07	0.32	0.75	0.96	0.489	1.34	0.364	1.00	1.00	0.364	No
295	19.41	1.08	0.32	0.75	0.96	0.490	1.34	0.364	1.00	1.00	0.364	No
296	19.46	1.08	0.33	0.76	0.96	0.490	1.34	0.365	1.00	1.00	0.365	No
297	19.51	1.09	0.33	0.76	0.96	0.491	1.34	0.365	1.00	1.00	0.365	No
298	19.56	1.09	0.33	0.76	0.96	0.491	1.34	0.365	1.00	1.00	0.365	No
299	19.63	1.09	0.33	0.76	0.96	0.492	1.34	0.366	1.00	1.00	0.366	No
300	19.71	1.10	0.33	0.76	0.96	0.492	1.34	0.366	1.00	1.00	0.366	No
301	19.80	1.10	0.34	0.76	0.96	0.493	1.34	0.367	1.00	1.00	0.367	No
302	19.82	1.10	0.34	0.77	0.96	0.493	1.34	0.367	1.00	1.00	0.367	No
303	19.91	1.11	0.34	0.77	0.96	0.494	1.34	0.367	1.00	1.00	0.367	No
304	19.95	1.11	0.34	0.77	0.96	0.494	1.34	0.368	1.00	1.00	0.368	No
305	20.02	1.11	0.34	0.77	0.96	0.495	1.34	0.368	1.00	1.00	0.368	No
306	20.11	1.12	0.35	0.77	0.96	0.495	1.34	0.368	1.00	1.00	0.368	No
307	20.15	1.12	0.35	0.77	0.96	0.496	1.34	0.369	1.00	1.00	0.369	No
308	20.24	1.13	0.35	0.78	0.96	0.496	1.34	0.369	1.00	1.00	0.369	No
309	20.29	1.13	0.35	0.78	0.96	0.497	1.34	0.369	1.00	1.00	0.369	No
310	20.36	1.13	0.35	0.78	0.96	0.497	1.34	0.370	1.00	1.00	0.370	No
311	20.41	1.14	0.36	0.78	0.96	0.497	1.34	0.370	1.00	1.00	0.370	No
312	20.48	1.14	0.36	0.78	0.96	0.498	1.34	0.370	1.00	1.00	0.370	No
313	20.56	1.15	0.36	0.79	0.96	0.498	1.34	0.371	1.00	1.00	0.371	No
314	20.66	1.15	0.36	0.79	0.96	0.499	1.34	0.371	1.00	1.00	0.371	No
315	20.71	1.16	0.37	0.79	0.96	0.499	1.34	0.371	1.00	1.00	0.371	No
316	20.74	1.16	0.37	0.79	0.95	0.499	1.34	0.371	1.00	1.00	0.371	No
317	20.82	1.16	0.37	0.79	0.95	0.500	1.34	0.372	1.00	1.00	0.372	No
318	20.91	1.17	0.37	0.80	0.95	0.500	1.34	0.372	1.00	1.00	0.372	No
319	20.95	1.17	0.37	0.80	0.95	0.501	1.34	0.372	1.00	1.00	0.372	No
320	21.03	1.17	0.38	0.80	0.95	0.501	1.34	0.373	1.00	1.00	0.373	No
321	21.11	1.18	0.38	0.80	0.95	0.502	1.34	0.373	1.00	1.00	0.373	No
322	21.15	1.18	0.38	0.80	0.95	0.502	1.34	0.373	1.00	1.00	0.373	No
323	21.22	1.19	0.38	0.80	0.95	0.502	1.34	0.374	1.00	1.00	0.374	No
324	21.26	1.19	0.38	0.81	0.95	0.503	1.34	0.374	1.00	1.00	2.000	Yes
325	21.34	1.19	0.39	0.81	0.95	0.503	1.34	0.374	1.00	1.00	2.000	Yes
326	21.41	1.20	0.39	0.81	0.95	0.504	1.34	0.375	1.00	1.00	2.000	Yes
327	21.48	1.20	0.39	0.81	0.95	0.504	1.34	0.375	1.00	1.00	2.000	Yes
328	21.52	1.20	0.39	0.81	0.95	0.504	1.34	0.375	1.00	1.00	2.000	Yes
329	21.61	1.21	0.39	0.82	0.95	0.505	1.34	0.375	1.00	1.00	2.000	Yes
330	21.66	1.21	0.39	0.82	0.95	0.505	1.34	0.376	1.00	1.00	2.000	Yes
331	21.76	1.22	0.40	0.82	0.95	0.506	1.34	0.376	1.00	1.00	2.000	Yes
332	21.81	1.22	0.40	0.82	0.95	0.506	1.34	0.376	1.00	1.00	2.000	Yes
333	21.85	1.22	0.40	0.82	0.95	0.506	1.34	0.377	1.00	1.00	2.000	Yes
334	21.92	1.23	0.40	0.82	0.95	0.507	1.34	0.377	1.00	1.00	2.000	Yes
335	22.01	1.23	0.41	0.83	0.95	0.507	1.34	0.377	1.00	1.00	2.000	Yes
336	22.09	1.24	0.41	0.83	0.95	0.508	1.34	0.377	1.00	1.00	0.377	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
337	22.12	1.24	0.41	0.83	0.95	0.508	1.34	0.378	1.00	1.00	0.378	No
338	22.20	1.24	0.41	0.83	0.95	0.508	1.34	0.378	1.00	1.00	0.378	No
339	22.29	1.25	0.41	0.84	0.95	0.509	1.34	0.378	1.00	1.00	0.378	No
340	22.31	1.25	0.42	0.84	0.95	0.509	1.34	0.378	1.00	1.00	0.378	No
341	22.40	1.26	0.42	0.84	0.95	0.509	1.34	0.379	1.00	1.00	0.379	No
342	22.45	1.26	0.42	0.84	0.95	0.509	1.34	0.379	1.00	1.00	0.379	No
343	22.51	1.26	0.42	0.84	0.95	0.510	1.34	0.379	1.00	1.00	0.379	No
344	22.60	1.27	0.42	0.84	0.95	0.510	1.34	0.379	1.00	1.00	0.379	No
345	22.64	1.27	0.43	0.85	0.95	0.510	1.34	0.380	1.00	1.00	0.380	No
346	22.75	1.28	0.43	0.85	0.95	0.511	1.34	0.380	1.00	1.00	0.380	No
347	22.80	1.28	0.43	0.85	0.95	0.511	1.34	0.380	1.00	1.00	0.380	No
348	22.85	1.28	0.43	0.85	0.95	0.511	1.34	0.380	1.00	1.00	0.380	No
349	22.91	1.29	0.43	0.85	0.95	0.512	1.34	0.380	1.00	1.00	0.380	No
350	22.99	1.29	0.44	0.86	0.95	0.512	1.34	0.381	1.00	1.00	0.381	No
351	23.08	1.30	0.44	0.86	0.95	0.512	1.34	0.381	1.00	1.00	0.381	No
352	23.10	1.30	0.44	0.86	0.95	0.512	1.34	0.381	1.00	1.00	0.381	No
353	23.18	1.30	0.44	0.86	0.95	0.513	1.34	0.381	1.00	1.00	2.000	Yes
354	23.26	1.31	0.44	0.86	0.95	0.513	1.34	0.382	1.00	1.00	2.000	Yes
355	23.30	1.31	0.45	0.87	0.95	0.513	1.34	0.382	1.00	1.00	2.000	Yes
356	23.37	1.32	0.45	0.87	0.95	0.514	1.34	0.382	1.00	1.00	2.000	Yes
357	23.46	1.32	0.45	0.87	0.95	0.514	1.34	0.382	1.00	1.00	2.000	Yes
358	23.51	1.32	0.45	0.87	0.95	0.514	1.34	0.382	1.00	1.00	2.000	Yes
359	23.56	1.33	0.45	0.87	0.95	0.514	1.34	0.383	1.00	1.00	2.000	Yes
360	23.63	1.33	0.46	0.88	0.95	0.515	1.34	0.383	1.00	1.00	2.000	Yes
361	23.72	1.34	0.46	0.88	0.95	0.515	1.34	0.383	1.00	1.00	2.000	Yes
362	23.79	1.34	0.46	0.88	0.95	0.515	1.34	0.383	1.00	1.00	2.000	Yes
363	23.87	1.35	0.46	0.88	0.95	0.516	1.34	0.384	1.00	1.00	2.000	Yes
364	23.91	1.35	0.47	0.88	0.95	0.516	1.34	0.384	1.00	1.00	2.000	Yes
365	23.96	1.35	0.47	0.89	0.95	0.516	1.34	0.384	1.00	1.00	2.000	Yes
366	24.02	1.36	0.47	0.89	0.95	0.516	1.34	0.384	1.00	1.00	0.384	No
367	24.11	1.36	0.47	0.89	0.94	0.517	1.34	0.384	1.00	1.00	0.384	No
368	24.20	1.37	0.47	0.89	0.94	0.517	1.34	0.385	1.00	1.00	0.385	No
369	24.22	1.37	0.47	0.89	0.94	0.517	1.34	0.385	1.00	1.00	0.385	No
370	24.31	1.37	0.48	0.89	0.94	0.518	1.34	0.385	1.00	1.00	0.385	No
371	24.39	1.38	0.48	0.90	0.94	0.518	1.34	0.385	1.00	1.00	0.385	No
372	24.42	1.38	0.48	0.90	0.94	0.518	1.34	0.386	1.00	1.00	0.386	No
373	24.51	1.38	0.48	0.90	0.94	0.519	1.34	0.386	1.00	1.00	0.386	No
374	24.55	1.39	0.49	0.90	0.94	0.519	1.34	0.386	1.00	1.00	0.386	No
375	24.63	1.39	0.49	0.90	0.94	0.519	1.34	0.386	1.00	1.00	0.386	No
376	24.71	1.39	0.49	0.90	0.94	0.520	1.34	0.387	1.00	1.00	0.387	No
377	24.75	1.40	0.49	0.91	0.94	0.520	1.34	0.387	1.00	1.00	0.387	No
378	24.81	1.40	0.49	0.91	0.94	0.520	1.34	0.387	1.00	1.00	0.387	No
379	24.90	1.41	0.50	0.91	0.94	0.521	1.34	0.387	1.00	1.00	0.387	No
380	24.94	1.41	0.50	0.91	0.94	0.521	1.34	0.387	1.00	1.00	0.387	No
381	25.01	1.41	0.50	0.91	0.94	0.521	1.34	0.388	1.00	1.00	0.388	No
382	25.07	1.41	0.50	0.91	0.94	0.521	1.34	0.388	1.00	1.00	0.388	No
383	25.15	1.42	0.50	0.92	0.94	0.522	1.34	0.388	1.00	1.00	0.388	No
384	25.20	1.42	0.51	0.92	0.94	0.522	1.34	0.388	1.00	1.00	0.388	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
385	25.28	1.43	0.51	0.92	0.94	0.522	1.34	0.389	1.00	1.00	0.389	No
386	25.35	1.43	0.51	0.92	0.94	0.523	1.34	0.389	1.00	1.00	0.389	No
387	25.40	1.43	0.51	0.92	0.94	0.523	1.34	0.389	1.00	1.00	0.389	No
388	25.48	1.44	0.51	0.92	0.94	0.523	1.34	0.389	1.00	1.00	0.389	No
389	25.55	1.44	0.52	0.92	0.94	0.524	1.34	0.389	1.00	1.00	0.389	No
390	25.60	1.44	0.52	0.93	0.94	0.524	1.34	0.390	1.00	1.00	0.390	No
391	25.67	1.45	0.52	0.93	0.94	0.524	1.34	0.390	1.00	1.00	0.390	No
392	25.75	1.45	0.52	0.93	0.94	0.524	1.34	0.390	1.00	1.00	0.390	No
393	25.79	1.45	0.52	0.93	0.94	0.525	1.34	0.390	1.00	1.00	0.390	No
394	25.90	1.46	0.53	0.93	0.94	0.525	1.34	0.391	1.00	1.00	0.391	No
395	25.95	1.46	0.53	0.93	0.94	0.525	1.34	0.391	1.00	1.00	0.391	No
396	26.01	1.47	0.53	0.94	0.94	0.525	1.34	0.391	1.00	1.00	0.391	No
397	26.09	1.47	0.53	0.94	0.94	0.526	1.34	0.391	1.00	1.00	0.391	No
398	26.13	1.47	0.53	0.94	0.94	0.526	1.34	0.391	1.00	1.00	0.391	No
399	26.19	1.48	0.54	0.94	0.94	0.526	1.34	0.391	1.00	1.00	0.391	No
400	26.27	1.48	0.54	0.94	0.94	0.526	1.34	0.392	1.00	1.00	0.392	No
401	26.34	1.49	0.54	0.94	0.94	0.527	1.34	0.392	1.00	1.00	0.392	No
402	26.39	1.49	0.54	0.95	0.94	0.527	1.34	0.392	1.00	1.00	0.392	No
403	26.47	1.49	0.55	0.95	0.94	0.527	1.34	0.392	1.00	1.00	0.392	No
404	26.54	1.50	0.55	0.95	0.94	0.527	1.34	0.392	1.00	1.00	0.392	No
405	26.58	1.50	0.55	0.95	0.94	0.528	1.34	0.392	1.00	1.00	0.392	No
406	26.67	1.50	0.55	0.95	0.94	0.528	1.34	0.393	1.00	1.00	0.393	No
407	26.73	1.51	0.55	0.95	0.94	0.528	1.34	0.393	1.00	1.00	0.393	No
408	26.78	1.51	0.55	0.96	0.94	0.528	1.34	0.393	1.00	1.00	0.393	No
409	26.85	1.51	0.56	0.96	0.93	0.529	1.34	0.393	1.00	1.00	0.393	No
410	26.93	1.52	0.56	0.96	0.93	0.529	1.34	0.393	1.00	1.00	0.393	No
411	26.98	1.52	0.56	0.96	0.93	0.529	1.34	0.393	1.00	1.00	0.393	No
412	27.03	1.53	0.56	0.96	0.93	0.529	1.34	0.394	1.00	1.00	0.394	No
413	27.13	1.53	0.57	0.97	0.93	0.529	1.34	0.394	1.00	1.00	0.394	No
414	27.17	1.53	0.57	0.97	0.93	0.530	1.34	0.394	1.00	1.00	0.394	No
415	27.24	1.54	0.57	0.97	0.93	0.530	1.34	0.394	1.00	1.00	0.394	No
416	27.33	1.54	0.57	0.97	0.93	0.530	1.34	0.394	1.00	1.00	0.394	No
417	27.36	1.54	0.57	0.97	0.93	0.530	1.34	0.394	1.00	1.00	0.394	No
418	27.43	1.55	0.58	0.97	0.93	0.530	1.34	0.395	1.00	1.00	0.395	No
419	27.53	1.55	0.58	0.98	0.93	0.531	1.34	0.395	1.00	1.00	0.395	No
420	27.60	1.56	0.58	0.98	0.93	0.531	1.34	0.395	1.00	1.00	0.395	No
421	27.63	1.56	0.58	0.98	0.93	0.531	1.34	0.395	1.00	1.00	0.395	No
422	27.72	1.56	0.58	0.98	0.93	0.531	1.34	0.395	1.00	1.00	0.395	No
423	27.77	1.57	0.59	0.98	0.93	0.531	1.34	0.395	1.00	1.00	0.395	No
424	27.84	1.57	0.59	0.98	0.93	0.532	1.34	0.395	1.00	1.00	0.395	No
425	27.93	1.58	0.59	0.99	0.93	0.532	1.34	0.396	1.00	1.00	0.396	No
426	27.97	1.58	0.59	0.99	0.93	0.532	1.34	0.396	1.00	1.00	0.396	No
427	28.02	1.58	0.59	0.99	0.93	0.532	1.34	0.396	1.00	1.00	0.396	No
428	28.12	1.59	0.60	0.99	0.93	0.533	1.34	0.396	1.00	1.00	0.396	No
429	28.17	1.59	0.60	0.99	0.93	0.533	1.34	0.396	1.00	1.00	0.396	No
430	28.22	1.59	0.60	0.99	0.93	0.533	1.34	0.396	1.00	1.00	0.396	No
431	28.32	1.60	0.60	0.99	0.93	0.533	1.34	0.396	1.00	1.00	0.396	No
432	28.36	1.60	0.60	1.00	0.93	0.533	1.34	0.397	1.00	1.00	0.397	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
433	28.42	1.60	0.61	1.00	0.93	0.533	1.34	0.397	1.00	1.00	0.397	No
434	28.48	1.61	0.61	1.00	0.93	0.534	1.34	0.397	1.00	1.00	0.397	No
435	28.57	1.61	0.61	1.00	0.93	0.534	1.34	0.397	1.00	1.00	0.397	No
436	28.62	1.61	0.61	1.00	0.93	0.534	1.34	0.397	1.00	1.00	0.397	No
437	28.72	1.62	0.62	1.00	0.93	0.534	1.34	0.397	1.00	1.00	0.397	No
438	28.75	1.62	0.62	1.01	0.93	0.534	1.34	0.397	1.00	1.00	0.397	No
439	28.82	1.63	0.62	1.01	0.93	0.534	1.34	0.397	1.00	1.00	0.397	No
440	28.87	1.63	0.62	1.01	0.93	0.535	1.34	0.398	1.00	1.00	0.398	No
441	28.95	1.63	0.62	1.01	0.93	0.535	1.34	0.398	1.00	1.00	0.398	No
442	29.02	1.64	0.62	1.01	0.93	0.535	1.34	0.398	1.00	1.00	0.398	No
443	29.07	1.64	0.63	1.01	0.93	0.535	1.34	0.398	1.00	1.00	0.398	No
444	29.16	1.65	0.63	1.02	0.92	0.535	1.34	0.398	1.00	1.00	0.398	No
445	29.21	1.65	0.63	1.02	0.92	0.535	1.34	0.398	1.00	1.00	0.398	No
446	29.29	1.65	0.63	1.02	0.92	0.535	1.34	0.398	1.00	1.00	0.398	No
447	29.36	1.66	0.64	1.02	0.92	0.536	1.34	0.398	1.00	1.00	0.398	No
448	29.40	1.66	0.64	1.02	0.92	0.536	1.34	0.398	1.00	1.00	0.398	No
449	29.47	1.66	0.64	1.02	0.92	0.536	1.34	0.399	1.00	1.00	0.399	No
450	29.56	1.67	0.64	1.03	0.92	0.536	1.34	0.399	1.00	1.00	0.399	No
451	29.60	1.67	0.64	1.03	0.92	0.536	1.34	0.399	1.00	1.00	0.399	No
452	29.71	1.68	0.65	1.03	0.92	0.536	1.34	0.399	1.00	1.00	0.399	No
453	29.75	1.68	0.65	1.03	0.92	0.536	1.34	0.399	1.00	1.00	0.399	No
454	29.79	1.68	0.65	1.03	0.92	0.537	1.34	0.399	1.00	1.00	0.399	No
455	29.86	1.68	0.65	1.03	0.92	0.537	1.34	0.399	1.00	1.00	0.399	No
456	29.95	1.69	0.65	1.04	0.92	0.537	1.34	0.399	1.00	1.00	0.399	No
457	30.04	1.70	0.66	1.04	0.92	0.537	1.34	0.399	1.00	1.00	0.399	No
458	30.06	1.70	0.66	1.04	0.92	0.537	1.34	0.399	1.00	1.00	0.399	No
459	30.15	1.70	0.66	1.04	0.92	0.537	1.34	0.400	1.00	1.00	0.400	No
460	30.20	1.70	0.66	1.04	0.92	0.537	1.34	0.400	1.00	1.00	0.400	No
461	30.28	1.71	0.66	1.04	0.92	0.537	1.34	0.400	1.00	1.00	0.400	No
462	30.35	1.71	0.67	1.05	0.92	0.538	1.34	0.400	1.00	1.00	0.400	No
463	30.39	1.72	0.67	1.05	0.92	0.538	1.34	0.400	1.00	1.00	0.400	No
464	30.45	1.72	0.67	1.05	0.92	0.538	1.34	0.400	1.00	1.00	0.400	No
465	30.54	1.72	0.67	1.05	0.92	0.538	1.34	0.400	1.00	1.00	0.400	No
466	30.60	1.73	0.67	1.05	0.92	0.538	1.34	0.400	1.00	1.00	0.400	No
467	30.67	1.73	0.68	1.06	0.92	0.538	1.34	0.400	1.00	1.00	0.400	No
468	30.74	1.74	0.68	1.06	0.92	0.538	1.34	0.400	1.00	1.00	0.400	No
469	30.79	1.74	0.68	1.06	0.92	0.538	1.34	0.400	1.00	1.00	0.400	No
470	30.86	1.74	0.68	1.06	0.92	0.538	1.34	0.400	1.00	1.00	0.400	No
471	30.95	1.75	0.68	1.06	0.92	0.538	1.34	0.400	1.00	1.00	0.401	No
472	30.99	1.75	0.69	1.06	0.92	0.538	1.34	0.400	1.00	1.00	0.401	No
473	31.05	1.75	0.69	1.07	0.92	0.538	1.34	0.400	1.00	1.00	0.401	No
474	31.14	1.76	0.69	1.07	0.91	0.539	1.34	0.401	1.00	1.00	0.401	No
475	31.19	1.76	0.69	1.07	0.91	0.539	1.34	0.401	1.00	1.00	0.402	No
476	31.26	1.77	0.69	1.07	0.91	0.539	1.34	0.401	1.00	1.00	0.402	No
477	31.34	1.77	0.70	1.07	0.91	0.539	1.34	0.401	1.00	1.00	0.402	No
478	31.39	1.77	0.70	1.07	0.91	0.539	1.34	0.401	1.00	1.00	0.402	No
479	31.45	1.78	0.70	1.08	0.91	0.539	1.34	0.401	1.00	1.00	0.402	No
480	31.54	1.78	0.70	1.08	0.91	0.539	1.34	0.401	1.00	1.00	0.403	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
481	31.57	1.78	0.70	1.08	0.91	0.539	1.34	0.401	1.00	1.00	0.403	No
482	31.63	1.79	0.71	1.08	0.91	0.539	1.34	0.401	1.00	1.00	0.403	No
483	31.73	1.79	0.71	1.08	0.91	0.539	1.34	0.401	0.99	1.00	0.403	No
484	31.77	1.79	0.71	1.08	0.91	0.539	1.34	0.401	0.99	1.00	0.403	No
485	31.84	1.80	0.71	1.09	0.91	0.539	1.34	0.401	0.99	1.00	0.403	No
486	31.93	1.80	0.72	1.09	0.91	0.539	1.34	0.401	0.99	1.00	0.404	No
487	31.98	1.81	0.72	1.09	0.91	0.539	1.34	0.401	0.99	1.00	0.404	No
488	32.05	1.81	0.72	1.09	0.91	0.540	1.34	0.401	0.99	1.00	0.404	No
489	32.09	1.81	0.72	1.09	0.91	0.540	1.34	0.401	0.99	1.00	0.404	No
490	32.17	1.82	0.72	1.09	0.91	0.540	1.34	0.401	0.99	1.00	0.404	No
491	32.22	1.82	0.72	1.10	0.91	0.540	1.34	0.401	0.99	1.00	0.405	No
492	32.32	1.83	0.73	1.10	0.91	0.540	1.34	0.401	0.99	1.00	0.405	No
493	32.35	1.83	0.73	1.10	0.91	0.540	1.34	0.401	0.99	1.00	0.405	No
494	32.43	1.83	0.73	1.10	0.91	0.540	1.34	0.401	0.99	1.00	0.405	No
495	32.52	1.84	0.73	1.10	0.91	0.540	1.34	0.401	0.99	1.00	0.405	No
496	32.57	1.84	0.74	1.10	0.91	0.540	1.34	0.401	0.99	1.00	0.405	No
497	32.62	1.84	0.74	1.11	0.91	0.540	1.34	0.402	0.99	1.00	0.406	No
498	32.71	1.85	0.74	1.11	0.91	0.540	1.34	0.402	0.99	1.00	0.406	No
499	32.76	1.85	0.74	1.11	0.91	0.540	1.34	0.402	0.99	1.00	0.406	No
500	32.82	1.85	0.74	1.11	0.90	0.540	1.34	0.402	0.99	1.00	0.406	No
501	32.90	1.86	0.75	1.11	0.90	0.540	1.34	0.402	0.99	1.00	0.406	No
502	32.96	1.86	0.75	1.11	0.90	0.540	1.34	0.402	0.99	1.00	0.406	No
503	33.02	1.87	0.75	1.12	0.90	0.540	1.34	0.402	0.99	1.00	0.407	No
504	33.11	1.87	0.75	1.12	0.90	0.540	1.34	0.402	0.99	1.00	0.407	No
505	33.17	1.87	0.75	1.12	0.90	0.540	1.34	0.402	0.99	1.00	0.407	No
506	33.22	1.88	0.76	1.12	0.90	0.540	1.34	0.402	0.99	1.00	0.407	No
507	33.31	1.88	0.76	1.12	0.90	0.540	1.34	0.402	0.99	1.00	0.407	No
508	33.34	1.88	0.76	1.12	0.90	0.540	1.34	0.402	0.99	1.00	0.407	No
509	33.41	1.89	0.76	1.13	0.90	0.540	1.34	0.402	0.99	1.00	0.407	No
510	33.49	1.89	0.76	1.13	0.90	0.540	1.34	0.402	0.99	1.00	0.408	No
511	33.57	1.90	0.77	1.13	0.90	0.540	1.34	0.402	0.98	1.00	0.408	No
512	33.61	1.90	0.77	1.13	0.90	0.540	1.34	0.402	0.98	1.00	0.408	No
513	33.68	1.90	0.77	1.13	0.90	0.540	1.34	0.402	0.98	1.00	0.408	No
514	33.76	1.91	0.77	1.14	0.90	0.540	1.34	0.402	0.98	1.00	0.408	No
515	33.81	1.91	0.77	1.14	0.90	0.540	1.34	0.402	0.98	1.00	0.408	No
516	33.88	1.91	0.78	1.14	0.90	0.540	1.34	0.402	0.98	1.00	0.408	No
517	33.95	1.92	0.78	1.14	0.90	0.540	1.34	0.402	0.98	1.00	0.409	No
518	34.01	1.92	0.78	1.14	0.90	0.540	1.34	0.402	0.98	1.00	0.409	No
519	34.06	1.93	0.78	1.14	0.90	0.540	1.34	0.402	0.98	1.00	0.409	No
520	34.13	1.93	0.78	1.15	0.90	0.540	1.34	0.402	0.98	1.00	0.409	No
521	34.21	1.93	0.79	1.15	0.90	0.540	1.34	0.402	0.98	1.00	0.409	No
522	34.25	1.94	0.79	1.15	0.90	0.540	1.34	0.402	0.98	1.00	0.409	No
523	34.35	1.94	0.79	1.15	0.90	0.540	1.34	0.402	0.98	1.00	0.409	No
524	34.40	1.94	0.79	1.15	0.89	0.540	1.34	0.401	0.98	1.00	0.409	No
525	34.49	1.95	0.80	1.15	0.89	0.540	1.34	0.401	0.98	1.00	0.410	No
526	34.53	1.95	0.80	1.16	0.89	0.540	1.34	0.401	0.98	1.00	0.410	No
527	34.60	1.96	0.80	1.16	0.89	0.540	1.34	0.401	0.98	1.00	0.410	No
528	34.65	1.96	0.80	1.16	0.89	0.540	1.34	0.401	0.98	1.00	0.410	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
529	34.74	1.97	0.80	1.16	0.89	0.540	1.34	0.401	0.98	1.00	0.410	No
530	34.80	1.97	0.80	1.16	0.89	0.539	1.34	0.401	0.98	1.00	0.410	No
531	34.85	1.97	0.81	1.17	0.89	0.539	1.34	0.401	0.98	1.00	0.410	No
532	34.93	1.98	0.81	1.17	0.89	0.539	1.34	0.401	0.98	1.00	0.410	No
533	34.98	1.98	0.81	1.17	0.89	0.539	1.34	0.401	0.98	1.00	0.410	No
534	35.05	1.98	0.81	1.17	0.89	0.539	1.34	0.401	0.98	1.00	0.410	No
535	35.15	1.99	0.82	1.17	0.89	0.539	1.34	0.401	0.98	1.00	0.411	No
536	35.20	1.99	0.82	1.17	0.89	0.539	1.34	0.401	0.98	1.00	0.411	No
537	35.25	2.00	0.82	1.18	0.89	0.539	1.34	0.401	0.98	1.00	0.411	No
538	35.33	2.00	0.82	1.18	0.89	0.539	1.34	0.401	0.98	1.00	0.411	No
539	35.40	2.00	0.82	1.18	0.89	0.539	1.34	0.401	0.98	1.00	0.411	No
540	35.44	2.01	0.82	1.18	0.89	0.539	1.34	0.401	0.97	1.00	0.411	No
541	35.50	2.01	0.83	1.18	0.89	0.539	1.34	0.401	0.97	1.00	0.411	No
542	35.59	2.02	0.83	1.19	0.89	0.539	1.34	0.401	0.97	1.00	0.411	No
543	35.64	2.02	0.83	1.19	0.89	0.539	1.34	0.401	0.97	1.00	0.411	No
544	35.70	2.02	0.83	1.19	0.89	0.539	1.34	0.401	0.97	1.00	0.411	No
545	35.79	2.03	0.84	1.19	0.88	0.538	1.34	0.400	0.97	1.00	0.412	No
546	35.83	2.03	0.84	1.19	0.88	0.538	1.34	0.400	0.97	1.00	0.412	No
547	35.94	2.04	0.84	1.19	0.88	0.538	1.34	0.400	0.97	1.00	0.412	No
548	35.98	2.04	0.84	1.20	0.88	0.538	1.34	0.400	0.97	1.00	0.412	No
549	36.03	2.04	0.84	1.20	0.88	0.538	1.34	0.400	0.97	1.00	0.412	No
550	36.09	2.04	0.85	1.20	0.88	0.538	1.34	0.400	0.97	1.00	0.412	No
551	36.17	2.05	0.85	1.20	0.88	0.538	1.34	0.400	0.97	1.00	0.412	No
552	36.23	2.05	0.85	1.20	0.88	0.538	1.34	0.400	0.97	1.00	0.412	No
553	36.29	2.06	0.85	1.20	0.88	0.538	1.34	0.400	0.97	1.00	0.412	No
554	36.38	2.06	0.85	1.21	0.88	0.538	1.34	0.400	0.97	1.00	0.412	No
555	36.44	2.06	0.86	1.21	0.88	0.538	1.34	0.400	0.97	1.00	0.412	No
556	36.49	2.07	0.86	1.21	0.88	0.538	1.34	0.400	0.97	1.00	0.412	No
557	36.59	2.07	0.86	1.21	0.88	0.537	1.34	0.400	0.97	1.00	0.412	No
558	36.63	2.08	0.86	1.21	0.88	0.537	1.34	0.400	0.97	1.00	0.412	No
559	36.69	2.08	0.86	1.22	0.88	0.537	1.34	0.400	0.97	1.00	0.412	No
560	36.78	2.08	0.87	1.22	0.88	0.537	1.34	0.399	0.97	1.00	0.413	No
561	36.82	2.09	0.87	1.22	0.88	0.537	1.34	0.399	0.97	1.00	0.413	No
562	36.88	2.09	0.87	1.22	0.88	0.537	1.34	0.399	0.97	1.00	0.413	No
563	36.98	2.10	0.87	1.22	0.88	0.537	1.34	0.399	0.97	1.00	0.413	No
564	37.02	2.10	0.87	1.22	0.88	0.537	1.34	0.399	0.97	1.00	0.413	No
565	37.11	2.10	0.88	1.23	0.88	0.537	1.34	0.399	0.97	1.00	0.413	No
566	37.18	2.11	0.88	1.23	0.87	0.537	1.34	0.399	0.97	1.00	0.413	No
567	37.22	2.11	0.88	1.23	0.87	0.536	1.34	0.399	0.97	1.00	0.413	No
568	37.28	2.11	0.88	1.23	0.87	0.536	1.34	0.399	0.97	1.00	0.413	No
569	37.38	2.12	0.89	1.23	0.87	0.536	1.34	0.399	0.97	1.00	0.413	No
570	37.42	2.12	0.89	1.23	0.87	0.536	1.34	0.399	0.97	1.00	0.413	No
571	37.48	2.12	0.89	1.24	0.87	0.536	1.34	0.399	0.96	1.00	0.413	No
572	37.57	2.13	0.89	1.24	0.87	0.536	1.34	0.399	0.96	1.00	0.413	No
573	37.62	2.13	0.89	1.24	0.87	0.536	1.34	0.398	0.96	1.00	0.413	No
574	37.68	2.14	0.89	1.24	0.87	0.536	1.34	0.398	0.96	1.00	0.413	No
575	37.77	2.14	0.90	1.24	0.87	0.535	1.34	0.398	0.96	1.00	0.413	No
576	37.82	2.14	0.90	1.24	0.87	0.535	1.34	0.398	0.96	1.00	0.413	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
577	37.88	2.15	0.90	1.25	0.87	0.535	1.34	0.398	0.96	1.00	0.413	No
578	37.96	2.15	0.90	1.25	0.87	0.535	1.34	0.398	0.96	1.00	0.413	No
579	38.00	2.15	0.90	1.25	0.87	0.535	1.34	0.398	0.96	1.00	0.413	No
580	38.08	2.16	0.91	1.25	0.87	0.535	1.34	0.398	0.96	1.00	0.413	No
581	38.12	2.16	0.91	1.25	0.87	0.535	1.34	0.398	0.96	1.00	0.413	No
582	38.20	2.17	0.91	1.25	0.87	0.535	1.34	0.398	0.96	1.00	0.414	No
583	38.27	2.17	0.91	1.26	0.87	0.534	1.34	0.398	0.96	1.00	0.414	No
584	38.36	2.17	0.92	1.26	0.87	0.534	1.34	0.397	0.96	1.00	0.414	No
585	38.40	2.18	0.92	1.26	0.86	0.534	1.34	0.397	0.96	1.00	0.414	No
586	38.46	2.18	0.92	1.26	0.86	0.534	1.34	0.397	0.96	1.00	0.414	No
587	38.56	2.19	0.92	1.26	0.86	0.534	1.34	0.397	0.96	1.00	0.414	No
588	38.59	2.19	0.92	1.26	0.86	0.534	1.34	0.397	0.96	1.00	0.414	No
589	38.66	2.19	0.93	1.27	0.86	0.534	1.34	0.397	0.96	1.00	0.414	No
590	38.76	2.20	0.93	1.27	0.86	0.533	1.34	0.397	0.96	1.00	0.414	No
591	38.79	2.20	0.93	1.27	0.86	0.533	1.34	0.397	0.96	1.00	0.414	No
592	38.87	2.20	0.93	1.27	0.86	0.533	1.34	0.396	0.96	1.00	0.414	No
593	38.91	2.21	0.93	1.27	0.86	0.533	1.34	0.396	0.96	1.00	0.414	No
594	39.00	2.21	0.94	1.28	0.86	0.533	1.34	0.396	0.96	1.00	0.414	No
595	39.04	2.21	0.94	1.28	0.86	0.533	1.34	0.396	0.96	1.00	0.414	No
596	39.11	2.22	0.94	1.28	0.86	0.532	1.34	0.396	0.96	1.00	0.414	No
597	39.20	2.22	0.94	1.28	0.86	0.532	1.34	0.396	0.96	1.00	0.414	No
598	39.24	2.23	0.94	1.28	0.86	0.532	1.34	0.396	0.96	1.00	0.414	No
599	39.31	2.23	0.95	1.29	0.86	0.532	1.34	0.395	0.96	1.00	0.414	No
600	39.38	2.24	0.95	1.29	0.86	0.531	1.34	0.395	0.96	1.00	0.414	No
601	39.46	2.24	0.95	1.29	0.86	0.531	1.34	0.395	0.96	1.00	0.414	No
602	39.51	2.24	0.95	1.29	0.86	0.531	1.34	0.395	0.96	1.00	0.414	No
603	39.60	2.25	0.95	1.30	0.85	0.531	1.34	0.395	0.95	1.00	2.000	Yes
604	39.66	2.25	0.96	1.30	0.85	0.530	1.34	0.394	0.95	1.00	2.000	Yes
605	39.71	2.26	0.96	1.30	0.85	0.530	1.34	0.394	0.95	1.00	2.000	Yes
606	39.79	2.26	0.96	1.30	0.85	0.530	1.34	0.394	0.95	1.00	2.000	Yes
607	39.85	2.27	0.96	1.30	0.85	0.530	1.34	0.394	0.95	1.00	2.000	Yes
608	39.91	2.27	0.96	1.31	0.85	0.529	1.34	0.394	0.95	1.00	2.000	Yes
609	39.99	2.28	0.97	1.31	0.85	0.529	1.34	0.393	0.95	1.00	2.000	Yes
610	40.05	2.28	0.97	1.31	0.85	0.529	1.34	0.393	0.95	1.00	2.000	Yes
611	40.11	2.28	0.97	1.31	0.85	0.529	1.34	0.393	0.95	1.00	2.000	Yes
612	40.20	2.29	0.97	1.32	0.85	0.528	1.34	0.393	0.95	1.00	0.413	No
613	40.25	2.29	0.98	1.32	0.85	0.528	1.34	0.393	0.95	1.00	0.413	No
614	40.30	2.30	0.98	1.32	0.85	0.528	1.34	0.392	0.95	1.00	0.413	No
615	40.40	2.30	0.98	1.32	0.85	0.527	1.34	0.392	0.95	1.00	0.413	No
616	40.43	2.31	0.98	1.32	0.85	0.527	1.34	0.392	0.95	1.00	0.413	No
617	40.49	2.31	0.98	1.33	0.85	0.527	1.34	0.392	0.95	1.00	0.413	No
618	40.55	2.31	0.98	1.33	0.85	0.527	1.34	0.392	0.95	1.00	0.413	No
619	40.64	2.32	0.99	1.33	0.85	0.526	1.34	0.391	0.95	1.00	0.413	No
620	40.69	2.32	0.99	1.33	0.84	0.526	1.34	0.391	0.95	1.00	0.413	No
621	40.80	2.33	0.99	1.34	0.84	0.525	1.34	0.391	0.95	1.00	0.412	No
622	40.84	2.33	0.99	1.34	0.84	0.525	1.34	0.391	0.95	1.00	0.412	No
623	40.89	2.34	0.99	1.34	0.84	0.525	1.34	0.390	0.95	1.00	0.412	No
624	40.96	2.34	1.00	1.34	0.84	0.525	1.34	0.390	0.95	1.00	0.412	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
625	41.04	2.35	1.00	1.35	0.84	0.524	1.34	0.390	0.95	1.00	0.412	No
626	41.10	2.35	1.00	1.35	0.84	0.524	1.34	0.390	0.95	1.00	0.412	No
627	41.15	2.35	1.00	1.35	0.84	0.524	1.34	0.390	0.95	1.00	0.412	No
628	41.24	2.36	1.01	1.35	0.84	0.523	1.34	0.389	0.94	1.00	0.412	No
629	41.28	2.36	1.01	1.35	0.84	0.523	1.34	0.389	0.94	1.00	0.412	No
630	41.38	2.37	1.01	1.36	0.84	0.523	1.34	0.389	0.94	1.00	0.412	No
631	41.41	2.37	1.01	1.36	0.84	0.523	1.34	0.389	0.94	1.00	0.412	No
632	41.49	2.38	1.01	1.36	0.84	0.522	1.34	0.388	0.94	1.00	0.412	No
633	41.54	2.38	1.02	1.36	0.84	0.522	1.34	0.388	0.94	1.00	0.412	No
634	41.61	2.38	1.02	1.37	0.84	0.522	1.34	0.388	0.94	1.00	0.412	No
635	41.69	2.39	1.02	1.37	0.84	0.521	1.34	0.388	0.94	1.00	0.411	No
636	41.77	2.39	1.02	1.37	0.83	0.521	1.34	0.388	0.94	1.00	0.411	No
637	41.84	2.40	1.02	1.37	0.83	0.521	1.34	0.387	0.94	1.00	0.411	No
638	41.88	2.40	1.03	1.38	0.83	0.521	1.34	0.387	0.94	1.00	0.411	No
639	41.94	2.40	1.03	1.38	0.83	0.520	1.34	0.387	0.94	1.00	0.411	No
640	42.04	2.41	1.03	1.38	0.83	0.520	1.34	0.387	0.94	1.00	0.411	No
641	42.08	2.41	1.03	1.38	0.83	0.520	1.34	0.386	0.94	1.00	0.411	No
642	42.17	2.42	1.03	1.38	0.83	0.519	1.34	0.386	0.94	1.00	0.411	No
643	42.19	2.42	1.04	1.39	0.83	0.519	1.34	0.386	0.94	1.00	0.411	No
644	42.28	2.43	1.04	1.39	0.83	0.519	1.34	0.386	0.94	1.00	0.411	No
645	42.33	2.43	1.04	1.39	0.83	0.518	1.34	0.386	0.94	1.00	0.411	No
646	42.39	2.43	1.04	1.39	0.83	0.518	1.34	0.385	0.94	1.00	0.411	No
647	42.48	2.44	1.04	1.40	0.83	0.518	1.34	0.385	0.94	1.00	0.410	No
648	42.53	2.44	1.05	1.40	0.83	0.518	1.34	0.385	0.94	1.00	0.410	No
649	42.59	2.45	1.05	1.40	0.83	0.517	1.34	0.385	0.94	1.00	0.410	No
650	42.67	2.45	1.05	1.40	0.83	0.517	1.34	0.384	0.94	1.00	0.410	No
651	42.73	2.46	1.05	1.40	0.83	0.517	1.34	0.384	0.94	1.00	0.410	No
652	42.81	2.46	1.05	1.41	0.83	0.516	1.34	0.384	0.94	1.00	0.410	No
653	42.88	2.47	1.06	1.41	0.82	0.516	1.34	0.384	0.94	1.00	0.410	No
654	42.92	2.47	1.06	1.41	0.82	0.516	1.34	0.384	0.94	1.00	0.410	No
655	43.00	2.47	1.06	1.41	0.82	0.515	1.34	0.383	0.94	1.00	0.410	No
656	43.08	2.48	1.06	1.42	0.82	0.515	1.34	0.383	0.94	1.00	0.409	No
657	43.12	2.48	1.06	1.42	0.82	0.515	1.34	0.383	0.93	1.00	0.409	No
658	43.21	2.49	1.07	1.42	0.82	0.514	1.34	0.382	0.93	1.00	0.409	No
659	43.27	2.49	1.07	1.42	0.82	0.514	1.34	0.382	0.93	1.00	0.409	No
660	43.32	2.50	1.07	1.42	0.82	0.514	1.34	0.382	0.93	1.00	0.409	No
661	43.39	2.50	1.07	1.43	0.82	0.513	1.34	0.382	0.93	1.00	0.409	No
662	43.47	2.50	1.08	1.43	0.82	0.513	1.34	0.381	0.93	1.00	0.409	No
663	43.52	2.51	1.08	1.43	0.82	0.513	1.34	0.381	0.93	1.00	0.409	No
664	43.59	2.51	1.08	1.43	0.82	0.512	1.34	0.381	0.93	1.00	0.409	No
665	43.67	2.52	1.08	1.44	0.82	0.512	1.34	0.381	0.93	1.00	0.408	No
666	43.72	2.52	1.08	1.44	0.82	0.512	1.34	0.381	0.93	1.00	0.408	No
667	43.80	2.53	1.09	1.44	0.82	0.511	1.34	0.380	0.93	1.00	0.408	No
668	43.85	2.53	1.09	1.44	0.82	0.511	1.34	0.380	0.93	1.00	0.408	No
669	43.92	2.53	1.09	1.44	0.81	0.511	1.34	0.380	0.93	1.00	0.408	No
670	43.97	2.54	1.09	1.45	0.81	0.510	1.34	0.380	0.93	1.00	0.408	No
671	44.04	2.54	1.09	1.45	0.81	0.510	1.34	0.379	0.93	1.00	0.408	No
672	44.13	2.55	1.10	1.45	0.81	0.510	1.34	0.379	0.93	1.00	0.408	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
673	44.17	2.55	1.10	1.45	0.81	0.509	1.34	0.379	0.93	1.00	0.408	No
674	44.24	2.55	1.10	1.46	0.81	0.509	1.34	0.379	0.93	1.00	0.407	No
675	44.31	2.56	1.10	1.46	0.81	0.509	1.34	0.378	0.93	1.00	0.407	No
676	44.37	2.56	1.10	1.46	0.81	0.509	1.34	0.378	0.93	1.00	0.407	No
677	44.45	2.57	1.11	1.46	0.81	0.508	1.34	0.378	0.93	1.00	0.407	No
678	44.50	2.57	1.11	1.46	0.81	0.508	1.34	0.378	0.93	1.00	0.407	No
679	44.56	2.57	1.11	1.46	0.81	0.508	1.34	0.378	0.93	1.00	0.407	No
680	44.65	2.58	1.11	1.47	0.81	0.507	1.34	0.377	0.93	1.00	0.407	No
681	44.71	2.58	1.11	1.47	0.81	0.507	1.34	0.377	0.93	1.00	0.407	No
682	44.76	2.59	1.12	1.47	0.81	0.507	1.34	0.377	0.93	1.00	0.407	No
683	44.85	2.59	1.12	1.47	0.81	0.506	1.34	0.377	0.93	1.00	0.406	No
684	44.88	2.59	1.12	1.47	0.80	0.506	1.34	0.377	0.93	1.00	0.406	No
685	44.96	2.60	1.12	1.48	0.80	0.506	1.34	0.376	0.93	1.00	0.406	No
686	45.05	2.60	1.12	1.48	0.80	0.506	1.34	0.376	0.93	1.00	0.406	No
687	45.10	2.61	1.13	1.48	0.80	0.505	1.34	0.376	0.93	1.00	0.406	No
688	45.17	2.61	1.13	1.48	0.80	0.505	1.34	0.376	0.93	1.00	0.406	No
689	45.25	2.62	1.13	1.48	0.80	0.505	1.34	0.375	0.93	1.00	0.406	No
690	45.30	2.62	1.13	1.49	0.80	0.504	1.34	0.375	0.92	1.00	0.406	No
691	45.37	2.62	1.13	1.49	0.80	0.504	1.34	0.375	0.92	1.00	0.405	No
692	45.45	2.63	1.14	1.49	0.80	0.504	1.34	0.375	0.92	1.00	0.405	No
693	45.49	2.63	1.14	1.49	0.80	0.503	1.34	0.374	0.92	1.00	0.405	No
694	45.54	2.63	1.14	1.49	0.80	0.503	1.34	0.374	0.92	1.00	0.405	No
695	45.61	2.64	1.14	1.50	0.80	0.503	1.34	0.374	0.92	1.00	0.405	No
696	45.68	2.64	1.14	1.50	0.80	0.502	1.34	0.374	0.92	1.00	0.405	No
697	45.75	2.65	1.15	1.50	0.80	0.502	1.34	0.373	0.92	1.00	0.405	No
698	45.80	2.65	1.15	1.50	0.80	0.502	1.34	0.373	0.92	1.00	0.405	No
699	45.89	2.66	1.15	1.51	0.79	0.501	1.34	0.373	0.92	1.00	0.404	No
700	45.93	2.66	1.15	1.51	0.79	0.501	1.34	0.373	0.92	1.00	0.404	No
701	46.01	2.66	1.15	1.51	0.79	0.501	1.34	0.372	0.92	1.00	0.404	No
702	46.08	2.67	1.16	1.51	0.79	0.500	1.34	0.372	0.92	1.00	0.404	No
703	46.15	2.67	1.16	1.51	0.79	0.500	1.34	0.372	0.92	1.00	0.404	No
704	46.20	2.68	1.16	1.52	0.79	0.500	1.34	0.372	0.92	1.00	0.404	No
705	46.29	2.68	1.16	1.52	0.79	0.499	1.34	0.371	0.92	1.00	0.403	No
706	46.34	2.69	1.17	1.52	0.79	0.499	1.34	0.371	0.92	1.00	0.403	No
707	46.41	2.69	1.17	1.52	0.79	0.499	1.34	0.371	0.92	1.00	0.403	No
708	46.49	2.69	1.17	1.52	0.79	0.498	1.34	0.371	0.92	1.00	0.403	No
709	46.53	2.70	1.17	1.53	0.79	0.498	1.34	0.370	0.92	1.00	0.403	No
710	46.60	2.70	1.17	1.53	0.79	0.498	1.34	0.370	0.92	1.00	0.403	No
711	46.69	2.71	1.18	1.53	0.79	0.497	1.34	0.370	0.92	1.00	0.403	No
712	46.73	2.71	1.18	1.53	0.79	0.497	1.34	0.370	0.92	1.00	0.402	No
713	46.79	2.71	1.18	1.53	0.79	0.497	1.34	0.369	0.92	1.00	0.402	No
714	46.89	2.72	1.18	1.54	0.78	0.496	1.34	0.369	0.92	1.00	0.402	No
715	46.94	2.72	1.18	1.54	0.78	0.496	1.34	0.369	0.92	1.00	0.402	No
716	46.99	2.73	1.19	1.54	0.78	0.496	1.34	0.369	0.92	1.00	0.402	No
717	47.09	2.73	1.19	1.54	0.78	0.495	1.34	0.368	0.92	1.00	0.402	No
718	47.13	2.73	1.19	1.54	0.78	0.495	1.34	0.368	0.92	1.00	0.402	No
719	47.19	2.74	1.19	1.55	0.78	0.495	1.34	0.368	0.92	1.00	0.401	No
720	47.28	2.74	1.19	1.55	0.78	0.494	1.34	0.368	0.92	1.00	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
721	47.34	2.75	1.20	1.55	0.78	0.494	1.34	0.367	0.92	1.00	2.000	Yes
722	47.38	2.75	1.20	1.55	0.78	0.494	1.34	0.367	0.92	1.00	2.000	Yes
723	47.50	2.76	1.20	1.56	0.78	0.493	1.34	0.367	0.92	1.00	2.000	Yes
724	47.51	2.76	1.20	1.56	0.78	0.493	1.34	0.367	0.92	1.00	2.000	Yes
725	47.60	2.76	1.20	1.56	0.78	0.492	1.34	0.366	0.91	1.00	2.000	Yes
726	47.69	2.77	1.21	1.56	0.78	0.492	1.34	0.366	0.91	1.00	2.000	Yes
727	47.70	2.77	1.21	1.56	0.78	0.492	1.34	0.366	0.91	1.00	2.000	Yes
728	47.80	2.78	1.21	1.57	0.78	0.491	1.34	0.365	0.91	1.00	2.000	Yes
729	47.84	2.78	1.21	1.57	0.77	0.491	1.34	0.365	0.91	1.00	2.000	Yes
730	47.91	2.78	1.21	1.57	0.77	0.491	1.34	0.365	0.91	1.00	2.000	Yes
731	48.00	2.79	1.22	1.57	0.77	0.490	1.34	0.365	0.91	1.00	2.000	Yes
732	48.04	2.79	1.22	1.57	0.77	0.490	1.34	0.364	0.91	1.00	2.000	Yes
733	48.11	2.80	1.22	1.58	0.77	0.490	1.34	0.364	0.91	1.00	0.399	No
734	48.19	2.80	1.22	1.58	0.77	0.489	1.34	0.364	0.91	1.00	0.399	No
735	48.23	2.80	1.22	1.58	0.77	0.489	1.34	0.364	0.91	1.00	0.399	No
736	48.30	2.81	1.23	1.58	0.77	0.489	1.34	0.363	0.91	1.00	0.399	No
737	48.40	2.82	1.23	1.59	0.77	0.488	1.34	0.363	0.91	1.00	0.398	No
738	48.45	2.82	1.23	1.59	0.77	0.488	1.34	0.363	0.91	1.00	0.398	No
739	48.50	2.82	1.23	1.59	0.77	0.487	1.34	0.362	0.91	1.00	0.398	No
740	48.59	2.83	1.24	1.59	0.77	0.487	1.34	0.362	0.91	1.00	0.398	No
741	48.66	2.83	1.24	1.60	0.77	0.486	1.34	0.362	0.91	1.00	0.398	No
742	48.69	2.84	1.24	1.60	0.77	0.486	1.34	0.362	0.91	1.00	0.398	No
743	48.78	2.84	1.24	1.60	0.77	0.486	1.34	0.361	0.91	1.00	0.397	No
744	48.85	2.85	1.24	1.60	0.76	0.485	1.34	0.361	0.91	1.00	0.397	No
745	48.89	2.85	1.24	1.60	0.76	0.485	1.34	0.361	0.91	1.00	0.397	No
746	48.98	2.85	1.25	1.61	0.76	0.485	1.34	0.360	0.91	1.00	0.397	No
747	49.03	2.86	1.25	1.61	0.76	0.484	1.34	0.360	0.91	1.00	0.397	No
748	49.09	2.86	1.25	1.61	0.76	0.484	1.34	0.360	0.91	1.00	0.396	No
749	49.19	2.87	1.25	1.61	0.76	0.483	1.34	0.360	0.91	1.00	0.396	No
750	49.23	2.87	1.26	1.62	0.76	0.483	1.34	0.359	0.91	1.00	0.396	No
751	49.28	2.87	1.26	1.62	0.76	0.483	1.34	0.359	0.91	1.00	0.396	No
752	49.39	2.88	1.26	1.62	0.76	0.482	1.34	0.359	0.91	1.00	0.396	No
753	49.42	2.88	1.26	1.62	0.76	0.482	1.34	0.359	0.91	1.00	0.396	No
754	49.49	2.89	1.26	1.62	0.76	0.482	1.34	0.358	0.91	1.00	0.395	No
755	49.59	2.89	1.27	1.63	0.76	0.481	1.34	0.358	0.91	1.00	0.395	No
756	49.62	2.90	1.27	1.63	0.76	0.481	1.34	0.358	0.91	1.00	0.395	No
757	49.69	2.90	1.27	1.63	0.76	0.480	1.34	0.357	0.91	1.00	0.395	No
758	49.74	2.90	1.27	1.63	0.76	0.480	1.34	0.357	0.90	1.00	0.395	No
759	49.83	2.91	1.27	1.64	0.75	0.480	1.34	0.357	0.90	1.00	0.394	No
760	49.88	2.91	1.28	1.64	0.75	0.479	1.34	0.357	0.90	1.00	0.394	No
761	49.93	2.92	1.28	1.64	0.75	0.479	1.34	0.356	0.90	1.00	0.394	No
762	50.03	2.92	1.28	1.64	0.75	0.478	1.34	0.356	0.90	1.00	2.000	No
763	50.13	2.93	1.28	1.65	0.75	0.478	1.34	0.355	0.90	1.00	2.000	No
764	50.14	2.93	1.28	1.65	0.75	0.478	1.34	0.355	0.90	1.00	2.000	No
765	50.23	2.94	1.29	1.65	0.75	0.477	1.34	0.355	0.90	1.00	2.000	No
766	50.27	2.94	1.29	1.65	0.75	0.477	1.34	0.355	0.90	1.00	2.000	No
767	50.34	2.94	1.29	1.65	0.75	0.477	1.34	0.355	0.90	1.00	2.000	No
768	50.43	2.95	1.29	1.66	0.75	0.476	1.34	0.354	0.90	1.00	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
769	50.49	2.95	1.29	1.66	0.75	0.476	1.34	0.354	0.90	1.00	2.000	No
770	50.53	2.96	1.30	1.66	0.75	0.476	1.34	0.354	0.90	1.00	2.000	No
771	50.62	2.96	1.30	1.66	0.75	0.475	1.34	0.353	0.90	1.00	2.000	No
772	50.68	2.97	1.30	1.67	0.75	0.475	1.34	0.353	0.90	1.00	2.000	No
773	50.73	2.97	1.30	1.67	0.75	0.474	1.34	0.353	0.90	1.00	2.000	No
774	50.82	2.98	1.30	1.67	0.74	0.474	1.34	0.352	0.90	1.00	2.000	No
775	50.88	2.98	1.31	1.67	0.74	0.474	1.34	0.352	0.90	1.00	2.000	No
776	50.93	2.98	1.31	1.67	0.74	0.473	1.34	0.352	0.90	1.00	2.000	No
777	51.02	2.99	1.31	1.68	0.74	0.473	1.34	0.352	0.90	1.00	2.000	No
778	51.09	2.99	1.31	1.68	0.74	0.472	1.34	0.351	0.90	1.00	2.000	Yes
779	51.12	2.99	1.31	1.68	0.74	0.472	1.34	0.351	0.90	1.00	2.000	Yes
780	51.19	3.00	1.32	1.68	0.74	0.472	1.34	0.351	0.90	1.00	2.000	Yes
781	51.28	3.00	1.32	1.69	0.74	0.471	1.34	0.351	0.90	1.00	2.000	Yes
782	51.32	3.01	1.32	1.69	0.74	0.471	1.34	0.350	0.90	1.00	2.000	Yes
783	51.39	3.01	1.32	1.69	0.74	0.471	1.34	0.350	0.90	1.00	2.000	Yes
784	51.48	3.02	1.33	1.69	0.74	0.470	1.34	0.350	0.90	1.00	2.000	Yes
785	51.53	3.02	1.33	1.69	0.74	0.470	1.34	0.350	0.90	1.00	2.000	Yes
786	51.62	3.03	1.33	1.70	0.74	0.470	1.34	0.349	0.90	1.00	2.000	Yes
787	51.68	3.03	1.33	1.70	0.74	0.469	1.34	0.349	0.90	1.00	2.000	Yes
788	51.73	3.03	1.33	1.70	0.74	0.469	1.34	0.349	0.90	1.00	2.000	Yes
789	51.82	3.04	1.34	1.70	0.73	0.469	1.34	0.349	0.90	1.00	2.000	No
790	51.87	3.04	1.34	1.70	0.73	0.468	1.34	0.348	0.90	1.00	2.000	No
791	51.92	3.04	1.34	1.70	0.73	0.468	1.34	0.348	0.90	1.00	2.000	No
792	51.97	3.05	1.34	1.71	0.73	0.468	1.34	0.348	0.90	1.00	2.000	No
793	52.04	3.05	1.34	1.71	0.73	0.467	1.34	0.348	0.90	1.00	2.000	No
794	52.12	3.06	1.35	1.71	0.73	0.467	1.34	0.347	0.90	1.00	2.000	No
795	52.18	3.06	1.35	1.71	0.73	0.467	1.34	0.347	0.90	1.00	2.000	No
796	52.23	3.06	1.35	1.71	0.73	0.467	1.34	0.347	0.90	1.00	2.000	No
797	52.31	3.07	1.35	1.72	0.73	0.466	1.34	0.347	0.89	1.00	2.000	No
798	52.37	3.07	1.35	1.72	0.73	0.466	1.34	0.347	0.89	1.00	2.000	No
799	52.44	3.07	1.36	1.72	0.73	0.466	1.34	0.346	0.89	1.00	2.000	No
800	52.53	3.08	1.36	1.72	0.73	0.465	1.34	0.346	0.89	1.00	2.000	No
801	52.57	3.08	1.36	1.72	0.73	0.465	1.34	0.346	0.89	1.00	2.000	No
802	52.64	3.09	1.36	1.72	0.73	0.465	1.34	0.346	0.89	1.00	2.000	No
803	52.72	3.09	1.36	1.73	0.73	0.464	1.34	0.345	0.89	1.00	2.000	No
804	52.78	3.09	1.37	1.73	0.72	0.464	1.34	0.345	0.89	1.00	2.000	No
805	52.83	3.10	1.37	1.73	0.72	0.464	1.34	0.345	0.89	1.00	2.000	No
806	52.93	3.10	1.37	1.73	0.72	0.463	1.34	0.345	0.89	1.00	2.000	No
807	52.96	3.10	1.37	1.73	0.72	0.463	1.34	0.345	0.89	1.00	2.000	No
808	53.04	3.11	1.37	1.73	0.72	0.463	1.34	0.344	0.89	1.00	2.000	No
809	53.12	3.11	1.38	1.74	0.72	0.462	1.34	0.344	0.89	1.00	2.000	No
810	53.17	3.11	1.38	1.74	0.72	0.462	1.34	0.344	0.89	1.00	2.000	No
811	53.22	3.12	1.38	1.74	0.72	0.462	1.34	0.344	0.89	1.00	2.000	No
812	53.29	3.12	1.38	1.74	0.72	0.462	1.34	0.343	0.89	1.00	2.000	No
813	53.37	3.13	1.38	1.74	0.72	0.461	1.34	0.343	0.89	1.00	2.000	No
814	53.42	3.13	1.39	1.74	0.72	0.461	1.34	0.343	0.89	1.00	2.000	No
815	53.49	3.13	1.39	1.74	0.72	0.461	1.34	0.343	0.89	1.00	2.000	No
816	53.58	3.14	1.39	1.75	0.72	0.461	1.34	0.343	0.89	1.00	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
817	53.63	3.14	1.39	1.75	0.72	0.460	1.34	0.342	0.89	1.00	2.000	No
818	53.68	3.14	1.39	1.75	0.72	0.460	1.34	0.342	0.89	1.00	2.000	No
819	53.78	3.15	1.40	1.75	0.71	0.460	1.34	0.342	0.89	1.00	2.000	No
820	53.84	3.15	1.40	1.75	0.71	0.459	1.34	0.342	0.89	1.00	2.000	No
821	53.88	3.15	1.40	1.75	0.71	0.459	1.34	0.342	0.89	1.00	2.000	No
822	53.94	3.16	1.40	1.75	0.71	0.459	1.34	0.341	0.89	1.00	2.000	No
823	54.03	3.16	1.40	1.76	0.71	0.459	1.34	0.341	0.89	1.00	2.000	No
824	54.08	3.16	1.41	1.76	0.71	0.458	1.34	0.341	0.89	1.00	2.000	No
825	54.16	3.17	1.41	1.76	0.71	0.458	1.34	0.341	0.89	1.00	2.000	No
826	54.20	3.17	1.41	1.76	0.71	0.458	1.34	0.341	0.89	1.00	2.000	No
827	54.28	3.17	1.41	1.76	0.71	0.458	1.34	0.340	0.89	1.00	2.000	No
828	54.35	3.18	1.41	1.76	0.71	0.457	1.34	0.340	0.89	1.00	2.000	No
829	54.43	3.18	1.42	1.76	0.71	0.457	1.34	0.340	0.89	1.00	2.000	No
830	54.48	3.18	1.42	1.77	0.71	0.457	1.34	0.340	0.89	1.00	2.000	No
831	54.55	3.19	1.42	1.77	0.71	0.456	1.34	0.339	0.89	1.00	2.000	No
832	54.63	3.19	1.42	1.77	0.71	0.456	1.34	0.339	0.89	1.00	2.000	No
833	54.67	3.20	1.42	1.77	0.71	0.456	1.34	0.339	0.89	1.00	2.000	No
834	54.74	3.20	1.43	1.77	0.71	0.456	1.34	0.339	0.89	1.00	2.000	No
835	54.82	3.20	1.43	1.77	0.71	0.455	1.34	0.339	0.89	1.00	2.000	No
836	54.87	3.21	1.43	1.77	0.70	0.455	1.34	0.338	0.89	1.00	2.000	No
837	54.92	3.21	1.43	1.78	0.70	0.455	1.34	0.338	0.89	1.00	2.000	No
838	55.02	3.21	1.44	1.78	0.70	0.454	1.34	0.338	0.89	1.00	2.000	No
839	55.06	3.22	1.44	1.78	0.70	0.454	1.34	0.338	0.89	1.00	2.000	No
840	55.14	3.22	1.44	1.78	0.70	0.454	1.34	0.338	0.89	1.00	2.000	No
841	55.22	3.22	1.44	1.78	0.70	0.454	1.34	0.337	0.89	1.00	2.000	No
842	55.27	3.23	1.44	1.78	0.70	0.453	1.34	0.337	0.89	1.00	2.000	No
843	55.37	3.23	1.45	1.79	0.70	0.453	1.34	0.337	0.89	1.00	2.000	No
844	55.42	3.24	1.45	1.79	0.70	0.453	1.34	0.337	0.89	1.00	2.000	No
845	55.47	3.24	1.45	1.79	0.70	0.452	1.34	0.337	0.89	1.00	2.000	No
846	55.53	3.24	1.45	1.79	0.70	0.452	1.34	0.336	0.89	1.00	2.000	No
847	55.58	3.24	1.45	1.79	0.70	0.452	1.34	0.336	0.89	1.00	2.000	No
848	55.67	3.25	1.46	1.79	0.70	0.452	1.34	0.336	0.89	1.00	2.000	No
849	55.72	3.25	1.46	1.79	0.70	0.451	1.34	0.336	0.89	1.00	2.000	No
850	55.81	3.26	1.46	1.80	0.70	0.451	1.34	0.335	0.89	1.00	2.000	No
851	55.86	3.26	1.46	1.80	0.70	0.451	1.34	0.335	0.89	1.00	2.000	No
852	55.92	3.26	1.46	1.80	0.69	0.451	1.34	0.335	0.89	1.00	2.000	No
853	56.01	3.27	1.47	1.80	0.69	0.450	1.34	0.335	0.88	1.00	2.000	No
854	56.05	3.27	1.47	1.80	0.69	0.450	1.34	0.335	0.88	1.00	2.000	No
855	56.11	3.27	1.47	1.80	0.69	0.450	1.34	0.334	0.88	1.00	2.000	No
856	56.21	3.28	1.47	1.81	0.69	0.449	1.34	0.334	0.88	1.00	2.000	No
857	56.26	3.28	1.47	1.81	0.69	0.449	1.34	0.334	0.88	1.00	2.000	No
858	56.32	3.28	1.48	1.81	0.69	0.449	1.34	0.334	0.88	1.00	2.000	No
859	56.41	3.29	1.48	1.81	0.69	0.448	1.34	0.333	0.88	1.00	2.000	No
860	56.46	3.29	1.48	1.81	0.69	0.448	1.34	0.333	0.88	1.00	2.000	No
861	56.50	3.30	1.48	1.81	0.69	0.448	1.34	0.333	0.88	1.00	2.000	No
862	56.59	3.30	1.48	1.82	0.69	0.448	1.34	0.333	0.88	1.00	2.000	No
863	56.65	3.30	1.49	1.82	0.69	0.447	1.34	0.333	0.88	1.00	2.000	No
864	56.70	3.31	1.49	1.82	0.69	0.447	1.34	0.332	0.88	1.00	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
865	56.78	3.31	1.49	1.82	0.69	0.447	1.34	0.332	0.88	1.00	2.000	No
866	56.85	3.32	1.49	1.82	0.69	0.446	1.34	0.332	0.88	1.00	2.000	No
867	56.89	3.32	1.49	1.82	0.69	0.446	1.34	0.332	0.88	1.00	2.000	No
868	56.98	3.32	1.50	1.83	0.69	0.446	1.34	0.331	0.88	1.00	2.000	No
869	57.04	3.33	1.50	1.83	0.68	0.445	1.34	0.331	0.88	1.00	2.000	No
870	57.09	3.33	1.50	1.83	0.68	0.445	1.34	0.331	0.88	1.00	2.000	No
871	57.16	3.33	1.50	1.83	0.68	0.445	1.34	0.331	0.88	1.00	2.000	No
872	57.24	3.34	1.51	1.83	0.68	0.444	1.34	0.330	0.88	1.00	2.000	No
873	57.29	3.34	1.51	1.84	0.68	0.444	1.34	0.330	0.88	1.00	2.000	No
874	57.37	3.35	1.51	1.84	0.68	0.444	1.34	0.330	0.88	1.00	2.000	No
875	57.42	3.35	1.51	1.84	0.68	0.443	1.34	0.330	0.88	1.00	2.000	No
876	57.49	3.35	1.51	1.84	0.68	0.443	1.34	0.330	0.88	1.00	2.000	No
877	57.59	3.36	1.52	1.85	0.68	0.443	1.34	0.329	0.88	1.00	2.000	No
878	57.64	3.36	1.52	1.85	0.68	0.442	1.34	0.329	0.88	1.00	2.000	No
879	57.69	3.37	1.52	1.85	0.68	0.442	1.34	0.329	0.88	1.00	2.000	No
880	57.77	3.37	1.52	1.85	0.68	0.442	1.34	0.329	0.88	1.00	2.000	No
881	57.82	3.38	1.52	1.85	0.68	0.441	1.34	0.328	0.88	1.00	2.000	No
882	57.89	3.38	1.53	1.85	0.68	0.441	1.34	0.328	0.88	1.00	2.000	No
883	57.97	3.38	1.53	1.86	0.68	0.441	1.34	0.328	0.88	1.00	2.000	No
884	58.03	3.39	1.53	1.86	0.68	0.440	1.34	0.328	0.88	1.00	2.000	No
885	58.09	3.39	1.53	1.86	0.68	0.440	1.34	0.327	0.88	1.00	2.000	No
886	58.17	3.40	1.53	1.86	0.67	0.440	1.34	0.327	0.88	1.00	2.000	No
887	58.21	3.40	1.54	1.86	0.67	0.440	1.34	0.327	0.88	1.00	2.000	No
888	58.28	3.40	1.54	1.87	0.67	0.439	1.34	0.327	0.88	1.00	2.000	No
889	58.37	3.41	1.54	1.87	0.67	0.439	1.34	0.326	0.88	1.00	2.000	No
890	58.40	3.41	1.54	1.87	0.67	0.439	1.34	0.326	0.88	1.00	2.000	No
891	58.48	3.41	1.54	1.87	0.67	0.438	1.34	0.326	0.88	1.00	2.000	No
892	58.53	3.42	1.55	1.87	0.67	0.438	1.34	0.326	0.88	1.00	2.000	No
893	58.63	3.42	1.55	1.87	0.67	0.438	1.34	0.326	0.88	1.00	2.000	No
894	58.67	3.43	1.55	1.88	0.67	0.438	1.34	0.326	0.88	1.00	2.000	No
895	58.73	3.43	1.55	1.88	0.67	0.437	1.34	0.325	0.88	1.00	2.000	No
896	58.82	3.43	1.55	1.88	0.67	0.437	1.34	0.325	0.88	1.00	2.000	No
897	58.89	3.44	1.56	1.88	0.67	0.437	1.34	0.325	0.88	1.00	2.000	No
898	58.93	3.44	1.56	1.88	0.67	0.437	1.34	0.325	0.88	1.00	2.000	No
899	59.00	3.44	1.56	1.88	0.67	0.436	1.34	0.324	0.88	1.00	2.000	No
900	59.06	3.45	1.56	1.89	0.67	0.436	1.34	0.324	0.88	1.00	2.000	No
901	59.13	3.45	1.56	1.89	0.67	0.436	1.34	0.324	0.88	1.00	2.000	No
902	59.22	3.46	1.57	1.89	0.67	0.435	1.34	0.324	0.88	1.00	2.000	No
903	59.28	3.46	1.57	1.89	0.67	0.435	1.34	0.324	0.87	1.00	2.000	No
904	59.33	3.46	1.57	1.89	0.66	0.435	1.34	0.323	0.87	1.00	2.000	No
905	59.41	3.47	1.57	1.90	0.66	0.434	1.34	0.323	0.87	1.00	2.000	No
906	59.47	3.47	1.57	1.90	0.66	0.434	1.34	0.323	0.87	1.00	2.000	No
907	59.52	3.47	1.58	1.90	0.66	0.434	1.34	0.323	0.87	1.00	2.000	No
908	59.61	3.48	1.58	1.90	0.66	0.434	1.34	0.323	0.87	1.00	2.000	No
909	59.67	3.48	1.58	1.90	0.66	0.433	1.34	0.322	0.87	1.00	2.000	No
910	59.72	3.49	1.58	1.90	0.66	0.433	1.34	0.322	0.87	1.00	2.000	No
911	59.78	3.49	1.58	1.90	0.66	0.433	1.34	0.322	0.87	1.00	2.000	No
912	59.87	3.49	1.59	1.91	0.66	0.433	1.34	0.322	0.87	1.00	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
913	59.92	3.50	1.59	1.91	0.66	0.432	1.34	0.322	0.87	1.00	2.000	Yes
914	60.00	3.50	1.59	1.91	0.66	0.432	1.34	0.321	0.87	1.00	2.000	Yes
915	60.05	3.50	1.59	1.91	0.66	0.432	1.34	0.321	0.87	1.00	2.000	Yes
916	60.11	3.51	1.59	1.91	0.66	0.432	1.34	0.321	0.87	1.00	2.000	Yes
917	60.21	3.51	1.60	1.91	0.66	0.431	1.34	0.321	0.87	1.00	2.000	Yes
918	60.25	3.51	1.60	1.92	0.66	0.431	1.34	0.321	0.87	1.00	2.000	Yes
919	60.31	3.52	1.60	1.92	0.66	0.431	1.34	0.320	0.87	1.00	2.000	Yes
920	60.40	3.52	1.60	1.92	0.66	0.431	1.34	0.320	0.87	1.00	2.000	Yes
921	60.43	3.52	1.60	1.92	0.66	0.431	1.34	0.320	0.87	1.00	2.000	No
922	60.51	3.53	1.61	1.92	0.66	0.430	1.34	0.320	0.87	1.00	2.000	No

Abbreviations

Depth: Depth from free surface, at which CPT was performed (ft)
σ_v: Total overburden pressure at test point (tsf)
u_0: Water pressure at test point (tsf)
σ_v': Effective overburden pressure based on GWT during earthquake (tsf)
r_d: Nonlinear shear mass factor
CSR: Cyclic Stress Ratio
MSF: Magnitude Scaling Factor
CSR_{eq}: CSR adjusted for M=7.5
K_σ: Effective overburden stress factor
CSR^*: CSR fully adjusted

:: Cyclic Resistance Ratio (CRR) calculation data ::

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
1	0.10	49.56	1.91	0.73	0.60	79.61	1.20	95.18	4.000	No	No	2.00
2	0.15	58.10	1.87	0.78	0.59	93.33	1.16	108.18	4.000	No	No	2.00
3	0.23	73.22	1.79	0.79	0.56	117.62	1.10	129.38	4.000	No	No	2.00
4	0.30	87.93	1.72	0.76	0.53	141.25	1.05	148.50	4.000	No	No	2.00
5	0.34	102.61	1.64	0.70	0.50	164.82	1.00	164.76	4.000	No	No	2.00
6	0.39	122.42	1.57	0.67	0.50	196.64	1.00	196.64	4.000	No	No	2.00
7	0.50	138.33	1.53	0.67	0.50	222.19	1.00	222.19	4.000	No	No	2.00
8	0.53	149.90	1.51	0.67	0.50	240.79	1.00	240.79	4.000	No	No	2.00
9	0.60	156.28	1.50	0.69	0.50	251.04	1.00	251.04	4.000	No	No	2.00
10	0.69	161.75	1.50	0.70	0.50	259.81	1.00	259.81	4.000	No	No	2.00
11	0.72	165.78	1.50	0.71	0.50	266.28	1.00	266.28	4.000	No	No	2.00
12	0.80	157.82	1.54	0.77	0.50	253.48	1.00	253.48	4.000	No	No	2.00
13	0.87	146.07	1.60	0.86	0.50	234.60	1.00	234.60	4.000	No	No	2.00
14	0.92	130.10	1.68	1.00	0.51	208.94	1.02	213.65	4.000	No	No	2.00
15	1.00	112.06	1.78	1.19	0.55	179.95	1.09	196.18	4.000	No	No	2.00
16	1.08	96.24	1.88	1.41	0.59	154.52	1.17	180.26	4.000	No	No	2.00
17	1.12	83.03	1.97	1.64	0.62	133.29	1.26	167.79	4.000	No	No	2.00
18	1.20	73.32	2.04	1.84	0.65	117.68	1.36	159.61	4.000	No	No	2.00
19	1.30	64.42	2.11	2.06	0.68	103.38	1.48	153.19	4.000	No	No	2.00
20	1.34	56.90	2.18	2.27	0.71	91.29	1.62	148.32	4.000	No	No	2.00
21	1.40	51.93	2.23	2.38	0.72	83.30	1.73	144.16	4.000	No	No	2.00
22	1.49	47.87	2.26	2.45	0.74	76.77	1.82	140.01	4.000	No	No	2.00
23	1.54	45.15	2.28	2.44	0.74	72.38	1.87	135.47	4.000	No	No	2.00
24	1.59	43.56	2.28	2.38	0.74	69.84	1.88	131.38	4.000	No	No	2.00
25	1.68	42.04	2.28	2.33	0.75	67.38	1.90	127.84	4.000	No	No	2.00
26	1.74	40.63	2.29	2.31	0.75	65.11	1.92	125.10	4.000	No	No	2.00
27	1.79	39.35	2.30	2.31	0.75	63.05	1.96	123.29	4.000	No	No	2.00
28	1.87	38.01	2.32	2.35	0.76	60.89	2.01	122.18	4.000	No	No	2.00
29	1.94	36.70	2.34	2.40	0.77	58.77	2.07	121.55	4.000	No	No	2.00
30	1.98	35.46	2.36	2.48	0.77	56.78	2.14	121.52	4.000	No	No	2.00
31	2.04	34.18	2.38	2.56	0.78	54.71	2.22	121.49	4.000	No	No	2.00
32	2.13	32.82	2.40	2.65	0.79	52.53	2.32	121.63	4.000	No	No	2.00
33	2.17	31.54	2.42	2.73	0.80	50.47	2.40	121.32	4.000	No	No	2.00
34	2.24	30.07	2.44	2.80	0.81	48.09	2.50	120.38	4.000	No	No	2.00
35	2.33	28.70	2.46	2.85	0.81	45.88	2.60	119.10	4.000	No	No	2.00
36	2.36	27.08	2.49	2.91	0.82	43.27	2.72	117.61	4.000	No	No	2.00
37	2.43	25.49	2.51	2.95	0.83	40.73	2.84	115.57	4.000	No	No	2.00
38	2.52	23.95	2.54	3.00	0.84	38.24	2.97	113.59	4.000	No	No	2.00
39	2.56	22.45	2.57	3.06	0.85	35.82	3.12	111.86	4.000	No	No	2.00
40	2.64	20.99	2.60	3.16	0.86	33.47	3.30	110.58	4.000	No	No	2.00
41	2.74	19.57	2.63	3.30	0.88	31.18	3.53	110.08	4.000	No	Yes	2.00
42	2.78	18.20	2.67	3.51	0.89	28.97	3.81	110.38	4.000	No	Yes	2.00
43	2.83	17.12	2.71	3.75	0.91	27.24	4.09	111.38	4.000	No	Yes	2.00
44	2.90	16.00	2.76	4.05	0.93	25.43	4.43	112.72	4.000	No	Yes	2.00
45	2.98	15.24	2.79	4.31	0.94	24.21	4.71	114.07	4.000	No	Yes	2.00
46	3.03	14.73	2.82	4.55	0.95	23.37	4.94	115.52	4.000	No	Yes	2.00
47	3.10	14.29	2.84	4.76	0.96	22.66	5.14	116.59	4.000	No	Yes	2.00
48	3.18	13.94	2.86	4.94	0.96	22.10	5.32	117.49	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
49	3.23	13.72	2.87	5.07	0.97	21.74	5.44	118.30	4.000	No	Yes	2.00
50	3.29	13.57	2.88	5.14	0.97	21.50	5.51	118.48	4.000	No	Yes	2.00
51	3.38	13.45	2.89	5.16	0.97	21.30	5.55	118.25	4.000	No	Yes	2.00
52	3.42	13.36	2.89	5.13	0.97	21.13	5.56	117.44	4.000	No	Yes	2.00
53	3.51	13.27	2.88	5.07	0.97	20.98	5.55	116.42	4.000	No	Yes	2.00
54	3.58	13.16	2.88	5.01	0.97	20.80	5.54	115.30	4.000	No	Yes	2.00
55	3.62	13.00	2.88	4.95	0.97	20.54	5.55	114.00	4.000	No	Yes	2.00
56	3.69	12.78	2.89	4.90	0.98	20.18	5.57	112.51	4.000	No	Yes	2.00
57	3.77	12.51	2.89	4.84	0.98	19.74	5.61	110.72	4.000	No	Yes	2.00
58	3.82	12.27	2.89	4.74	0.98	19.35	5.62	108.69	4.000	No	Yes	2.00
59	3.89	12.10	2.89	4.62	0.98	19.07	5.59	106.68	4.000	No	Yes	2.00
60	3.97	11.87	2.89	4.53	0.98	18.70	5.60	104.67	4.000	No	Yes	2.00
61	4.03	11.66	2.89	4.45	0.98	18.35	5.61	103.05	4.000	No	Yes	2.00
62	4.10	11.44	2.90	4.41	0.98	17.99	5.65	101.73	4.000	No	Yes	2.00
63	4.15	11.24	2.90	4.39	0.98	17.67	5.70	100.72	4.000	No	Yes	2.00
64	4.24	11.07	2.91	4.39	0.98	17.39	5.75	100.03	4.000	No	Yes	2.00
65	4.29	10.91	2.91	4.44	0.99	17.13	5.83	99.87	4.000	No	Yes	2.00
66	4.35	10.77	2.92	4.51	0.99	16.89	5.92	100.05	4.000	No	Yes	2.00
67	4.44	10.61	2.93	4.62	0.99	16.63	6.04	100.44	4.000	No	Yes	2.00
68	4.48	10.42	2.95	4.73	1.00	16.32	6.17	100.73	4.000	No	Yes	2.00
69	4.54	10.34	2.95	4.81	1.00	16.19	6.25	101.19	4.000	No	Yes	2.00
70	4.61	10.34	2.96	4.85	1.00	16.19	6.28	101.63	4.000	No	Yes	2.00
71	4.69	10.46	2.95	4.83	1.00	16.37	6.22	101.92	4.000	No	Yes	2.00
72	4.74	10.72	2.94	4.74	0.99	16.78	6.09	102.16	4.000	No	Yes	2.00
73	4.82	11.01	2.92	4.66	0.99	17.24	5.94	102.49	4.000	No	Yes	2.00
74	4.86	11.27	2.91	4.59	0.98	17.65	5.82	102.81	4.000	No	Yes	2.00
75	4.94	11.44	2.91	4.55	0.98	17.92	5.75	103.07	4.000	No	Yes	2.00
76	5.02	11.53	2.90	4.55	0.98	18.06	5.72	103.35	4.000	No	Yes	2.00
77	5.09	11.59	2.90	4.55	0.98	18.15	5.71	103.54	4.000	No	Yes	2.00
78	5.13	11.58	2.90	4.54	0.98	18.13	5.71	103.44	4.000	No	Yes	2.00
79	5.23	11.50	2.90	4.53	0.98	17.99	5.73	103.05	4.000	No	Yes	2.00
80	5.28	11.33	2.91	4.54	0.98	17.72	5.78	102.47	4.000	No	Yes	2.00
81	5.33	11.01	2.92	4.57	0.99	17.20	5.90	101.40	4.000	No	Yes	2.00
82	5.39	10.68	2.93	4.58	0.99	16.65	6.01	100.10	4.000	No	Yes	2.00
83	5.48	10.37	2.94	4.57	1.00	16.15	6.11	98.65	4.000	No	Yes	2.00
84	5.52	10.16	2.94	4.51	1.00	15.81	6.14	97.14	4.000	No	Yes	2.00
85	5.58	10.05	2.94	4.39	1.00	15.63	6.11	95.46	4.000	No	Yes	2.00
86	5.67	9.93	2.94	4.28	0.99	15.43	6.08	93.87	4.000	No	Yes	2.00
87	5.73	9.80	2.94	4.19	0.99	15.21	6.07	92.37	4.000	No	Yes	2.00
88	5.78	9.62	2.94	4.10	0.99	14.92	6.08	90.75	4.000	No	Yes	2.00
89	5.88	9.43	2.94	4.03	1.00	14.60	6.11	89.22	4.000	No	Yes	2.00
90	5.92	9.27	2.94	3.96	1.00	14.35	6.12	87.78	4.000	No	Yes	2.00
91	5.97	9.11	2.94	3.86	1.00	14.09	6.12	86.19	4.000	No	Yes	2.00
92	6.08	8.96	2.94	3.75	1.00	13.84	6.10	84.43	4.000	No	Yes	2.00
93	6.11	8.81	2.94	3.62	0.99	13.59	6.07	82.50	4.000	No	Yes	2.00
94	6.18	8.66	2.94	3.52	0.99	13.35	6.05	80.80	4.000	No	Yes	2.00
95	6.27	8.55	2.93	3.40	0.99	13.16	6.02	79.18	4.000	No	Yes	2.00
96	6.33	8.51	2.92	3.29	0.99	13.09	5.94	77.79	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
97	6.38	8.57	2.91	3.20	0.99	13.18	5.85	77.06	4.000	No	Yes	2.00
98	6.44	8.68	2.90	3.09	0.98	13.35	5.71	76.30	4.000	No	Yes	2.00
99	6.50	8.77	2.89	3.03	0.98	13.50	5.63	75.97	4.000	No	Yes	2.00
100	6.57	8.86	2.89	3.04	0.98	13.64	5.60	76.38	4.000	No	Yes	2.00
101	6.67	8.93	2.89	3.09	0.98	13.74	5.62	77.22	4.000	No	Yes	2.00
102	6.72	9.00	2.90	3.18	0.98	13.85	5.67	78.47	4.000	No	Yes	2.00
103	6.76	9.05	2.91	3.31	0.98	13.91	5.75	79.99	4.000	No	Yes	2.00
104	6.83	9.07	2.92	3.46	0.99	13.94	5.85	81.62	4.000	No	Yes	2.00
105	6.92	9.05	2.93	3.61	0.99	13.90	5.98	83.10	4.000	No	Yes	2.00
106	6.97	9.00	2.94	3.75	1.00	13.82	6.10	84.30	4.000	No	Yes	2.00
107	7.04	8.95	2.95	3.88	1.00	13.74	6.22	85.48	4.000	No	Yes	2.00
108	7.12	8.92	2.96	4.00	1.00	13.67	6.32	86.38	4.000	No	Yes	2.00
109	7.16	8.93	2.96	4.04	1.00	13.69	6.35	86.88	4.000	No	Yes	2.00
110	7.25	8.98	2.96	4.04	1.00	13.77	6.33	87.12	4.000	No	Yes	2.00
111	7.32	9.04	2.96	4.03	1.00	13.86	6.29	87.24	4.000	No	Yes	2.00
112	7.37	9.15	2.95	4.01	1.00	14.04	6.23	87.46	4.000	No	Yes	2.00
113	7.43	9.31	2.94	3.97	1.00	14.29	6.14	87.79	4.000	No	Yes	2.00
114	7.52	9.51	2.93	3.93	0.99	14.59	6.04	88.11	4.000	No	Yes	2.00
115	7.56	9.71	2.93	3.93	0.99	14.92	5.96	88.91	4.000	No	Yes	2.00
116	7.63	9.90	2.92	3.94	0.99	15.21	5.91	89.83	4.000	No	Yes	2.00
117	7.71	10.03	2.92	3.98	0.99	15.41	5.89	90.76	4.000	No	Yes	2.00
118	7.75	10.10	2.92	4.04	0.99	15.52	5.90	91.59	4.000	No	Yes	2.00
119	7.83	10.07	2.93	4.12	0.99	15.47	5.97	92.32	4.000	No	Yes	2.00
120	7.88	10.00	2.94	4.21	0.99	15.34	6.06	92.94	4.000	No	Yes	2.00
121	7.97	9.86	2.95	4.29	1.00	15.11	6.16	93.11	4.000	No	Yes	2.00
122	8.01	9.69	2.95	4.33	1.00	14.84	6.25	92.80	4.000	No	Yes	2.00
123	8.08	9.54	2.96	4.35	1.00	14.59	6.33	92.37	4.000	No	Yes	2.00
124	8.18	9.42	2.97	4.33	1.00	14.39	6.36	91.57	4.000	No	Yes	2.00
125	8.22	9.30	2.97	4.29	1.00	14.19	6.39	90.63	4.000	No	Yes	2.00
126	8.28	9.26	2.96	4.22	1.00	14.13	6.36	89.79	4.000	No	Yes	2.00
127	8.35	9.23	2.96	4.16	1.00	14.08	6.33	89.07	4.000	No	Yes	2.00
128	8.43	9.24	2.96	4.09	1.00	14.09	6.28	88.45	4.000	No	Yes	2.00
129	8.48	9.27	2.95	4.02	1.00	14.12	6.22	87.82	4.000	No	Yes	2.00
130	8.56	9.28	2.95	3.97	1.00	14.13	6.18	87.32	4.000	No	Yes	2.00
131	8.63	9.26	2.95	3.95	1.00	14.10	6.18	87.07	4.000	No	Yes	2.00
132	8.68	9.20	2.95	3.95	1.00	14.00	6.20	86.84	4.000	No	Yes	2.00
133	8.76	9.10	2.95	3.96	1.00	13.83	6.25	86.49	4.000	No	Yes	2.00
134	8.80	9.00	2.96	3.93	1.00	13.66	6.28	85.75	4.000	No	Yes	2.00
135	8.88	8.84	2.96	3.92	1.00	13.40	6.34	84.89	4.000	No	Yes	2.00
136	8.94	8.67	2.97	3.89	1.00	13.13	6.39	83.89	4.000	No	Yes	2.00
137	8.99	8.51	2.97	3.86	1.00	12.85	6.45	82.88	4.000	No	Yes	2.00
138	9.07	8.35	2.98	3.83	1.00	12.59	6.50	81.85	4.000	No	Yes	2.00
139	9.14	8.17	2.98	3.79	1.00	12.30	6.56	80.67	4.000	No	Yes	2.00
140	9.22	8.01	2.99	3.72	1.00	12.03	6.59	79.33	4.000	No	Yes	2.00
141	9.27	7.85	2.99	3.65	1.00	11.77	6.62	77.97	4.000	No	Yes	2.00
142	9.37	7.71	2.99	3.56	1.00	11.54	6.62	76.43	4.000	No	Yes	2.00
143	9.42	7.56	2.99	3.49	1.00	11.30	6.65	75.16	4.000	No	Yes	2.00
144	9.47	7.39	3.00	3.43	1.00	11.03	6.70	73.85	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
145	9.52	7.22	3.00	3.39	1.00	10.74	6.77	72.68	4.000	No	Yes	2.00
146	9.62	7.05	3.01	3.35	1.00	10.46	6.83	71.47	4.000	No	Yes	2.00
147	9.67	6.93	3.01	3.27	1.00	10.26	6.85	70.25	4.000	No	Yes	2.00
148	9.73	7.01	3.00	3.20	1.00	10.39	6.73	69.94	4.000	No	Yes	2.00
149	9.82	7.17	2.99	3.14	1.00	10.63	6.59	70.09	4.000	No	Yes	2.00
150	9.86	7.39	2.97	3.09	1.00	10.98	6.42	70.54	4.000	No	Yes	2.00
151	9.92	7.76	2.95	3.10	1.00	11.57	6.24	72.17	4.000	No	Yes	2.00
152	10.02	8.17	2.94	3.15	0.99	12.23	6.08	74.33	4.000	No	Yes	2.00
153	10.06	8.66	2.92	3.24	0.99	13.01	5.92	77.10	4.000	No	Yes	2.00
154	10.12	9.25	2.91	3.34	0.98	13.95	5.76	80.39	4.000	No	Yes	2.00
155	10.21	9.84	2.89	3.45	0.98	14.90	5.62	83.79	4.000	No	Yes	2.00
156	10.25	10.49	2.88	3.56	0.97	15.94	5.48	87.38	4.000	No	Yes	2.00
157	10.31	11.09	2.86	3.65	0.97	16.89	5.36	90.46	4.000	No	Yes	2.00
158	10.41	11.67	2.85	3.71	0.96	17.81	5.23	93.18	4.000	No	Yes	2.00
159	10.45	12.28	2.84	3.75	0.96	18.80	5.10	95.78	4.000	No	Yes	2.00
160	10.52	12.84	2.82	3.79	0.95	19.69	4.98	98.11	4.000	No	Yes	2.00
161	10.61	13.40	2.81	3.81	0.95	20.57	4.87	100.13	4.000	No	Yes	2.00
162	10.64	13.96	2.80	3.82	0.94	21.47	4.75	101.99	4.000	No	Yes	2.00
163	10.71	14.46	2.78	3.82	0.94	22.27	4.65	103.52	4.000	No	Yes	2.00
164	10.81	14.98	2.77	3.81	0.93	22.93	4.57	104.69	4.000	No	Yes	2.00
165	10.85	15.43	2.77	3.82	0.93	23.52	4.50	105.85	4.000	No	Yes	2.00
166	10.91	15.78	2.76	3.84	0.93	23.92	4.47	106.92	4.000	No	Yes	2.00
167	10.96	16.11	2.76	3.86	0.93	24.32	4.44	108.02	4.000	No	Yes	2.00
168	11.03	16.41	2.76	3.91	0.93	24.63	4.43	109.16	4.000	No	Yes	2.00
169	11.10	16.63	2.76	3.94	0.93	24.81	4.43	110.05	4.000	No	Yes	2.00
170	11.20	16.84	2.76	3.99	0.93	24.94	4.45	110.91	4.000	No	Yes	2.00
171	11.24	17.06	2.76	4.02	0.93	25.18	4.44	111.77	4.000	No	Yes	2.00
172	11.30	17.28	2.76	4.05	0.93	25.38	4.43	112.54	4.000	No	Yes	2.00
173	11.36	17.47	2.76	4.08	0.93	25.53	4.44	113.33	4.000	No	Yes	2.00
174	11.43	17.60	2.76	4.11	0.93	25.59	4.45	113.92	4.000	No	Yes	2.00
175	11.50	17.65	2.76	4.14	0.93	25.53	4.47	114.20	4.000	No	Yes	2.00
176	11.58	17.64	2.77	4.16	0.93	25.35	4.50	114.11	4.000	No	Yes	2.00
177	11.63	17.60	2.77	4.16	0.93	25.19	4.52	113.88	4.000	No	Yes	2.00
178	11.70	17.51	2.77	4.17	0.93	24.92	4.55	113.42	4.000	No	Yes	2.00
179	11.79	17.40	2.77	4.14	0.93	24.59	4.57	112.43	4.000	No	Yes	2.00
180	11.84	17.23	2.78	4.09	0.93	24.24	4.58	111.06	4.000	No	Yes	2.00
181	11.90	17.01	2.78	4.02	0.93	23.80	4.59	109.21	4.000	No	Yes	2.00
182	11.98	16.94	2.77	3.87	0.93	23.51	4.54	106.65	4.000	No	Yes	2.00
183	12.02	16.91	2.76	3.70	0.93	23.37	4.45	103.99	4.000	No	Yes	2.00
184	12.09	17.00	2.75	3.52	0.92	23.38	4.34	101.38	4.000	No	Yes	2.00
185	12.14	17.14	2.73	3.35	0.92	23.48	4.22	99.12	4.000	No	Yes	2.00
186	12.21	17.31	2.71	3.19	0.91	23.60	4.11	96.91	4.000	No	Yes	2.00
187	12.29	17.62	2.70	3.03	0.90	23.89	3.97	94.76	4.000	No	Yes	2.00
188	12.34	17.88	2.68	2.90	0.90	24.16	3.86	93.21	4.000	No	Yes	2.00
189	12.44	18.17	2.67	2.82	0.89	24.43	3.78	92.34	4.000	No	Yes	2.00
190	12.49	18.50	2.66	2.76	0.89	24.79	3.70	91.81	4.000	No	Yes	2.00
191	12.57	18.63	2.66	2.75	0.89	24.90	3.69	91.83	4.000	No	Yes	2.00
192	12.64	18.76	2.66	2.76	0.89	25.02	3.69	92.19	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
193	12.68	18.84	2.66	2.78	0.89	25.09	3.69	92.51	4.000	No	Yes	2.00
194	12.73	18.86	2.66	2.80	0.89	25.08	3.70	92.86	4.000	No	Yes	2.00
195	12.84	18.81	2.66	2.82	0.89	24.93	3.73	92.99	4.000	No	Yes	2.00
196	12.89	18.69	2.67	2.84	0.89	24.74	3.76	93.03	4.000	No	Yes	2.00
197	12.98	18.58	2.67	2.84	0.89	24.53	3.78	92.82	4.000	No	Yes	2.00
198	13.00	18.45	2.67	2.84	0.89	24.34	3.80	92.48	4.000	No	Yes	2.00
199	13.08	18.34	2.68	2.84	0.89	24.13	3.82	92.17	4.000	No	Yes	2.00
200	13.14	18.25	2.68	2.85	0.90	23.98	3.84	92.18	4.000	No	Yes	2.00
201	13.23	18.22	2.68	2.87	0.90	23.86	3.87	92.33	4.000	No	Yes	2.00
202	13.27	18.26	2.69	2.91	0.90	23.89	3.89	92.99	4.000	No	Yes	2.00
203	13.34	18.38	2.69	2.96	0.90	24.01	3.91	93.85	4.000	No	Yes	2.00
204	13.43	18.50	2.69	3.02	0.90	24.12	3.94	94.98	4.000	No	Yes	2.00
205	13.47	18.61	2.70	3.10	0.90	24.25	3.98	96.47	4.000	No	Yes	2.00
206	13.54	18.62	2.71	3.22	0.91	24.25	4.06	98.37	4.000	No	Yes	2.00
207	13.63	18.55	2.72	3.37	0.91	24.12	4.16	100.47	4.000	No	Yes	2.00
208	13.67	18.46	2.74	3.52	0.92	24.02	4.27	102.51	4.000	No	Yes	2.00
209	13.72	18.35	2.75	3.65	0.92	23.87	4.36	104.15	4.000	No	Yes	2.00
210	13.83	18.16	2.76	3.77	0.93	23.56	4.47	105.29	4.000	No	Yes	2.00
211	13.88	17.91	2.77	3.87	0.93	23.21	4.57	106.09	4.000	No	Yes	2.00
212	13.94	17.59	2.79	3.97	0.94	22.77	4.68	106.54	4.000	No	Yes	2.00
213	13.98	17.20	2.80	4.06	0.94	22.26	4.80	106.80	4.000	No	Yes	2.00
214	14.06	16.75	2.82	4.16	0.95	21.64	4.93	106.76	4.000	No	Yes	2.00
215	14.14	16.40	2.83	4.19	0.95	21.13	5.02	106.09	4.000	No	Yes	2.00
216	14.18	16.13	2.83	4.17	0.95	20.75	5.06	105.03	4.000	No	Yes	2.00
217	14.26	15.81	2.84	4.15	0.96	20.27	5.12	103.76	4.000	No	Yes	2.00
218	14.33	15.47	2.84	4.11	0.96	19.77	5.17	102.31	4.000	No	Yes	2.00
219	14.37	15.15	2.85	4.09	0.96	19.33	5.23	101.05	4.000	No	Yes	2.00
220	14.45	14.78	2.86	4.09	0.96	18.80	5.31	99.86	4.000	No	Yes	2.00
221	14.54	14.43	2.87	4.07	0.97	18.29	5.39	98.53	4.000	No	Yes	2.00
222	14.61	14.15	2.87	4.03	0.97	17.89	5.43	97.16	4.000	No	Yes	2.00
223	14.65	13.92	2.87	3.97	0.97	17.55	5.45	95.67	4.000	No	Yes	2.00
224	14.74	13.69	2.88	3.91	0.97	17.19	5.48	94.20	4.000	No	Yes	2.00
225	14.80	13.48	2.88	3.86	0.97	16.88	5.50	92.84	4.000	No	Yes	2.00
226	14.85	13.31	2.88	3.79	0.97	16.63	5.51	91.55	4.000	No	Yes	2.00
227	14.90	13.18	2.88	3.73	0.97	16.42	5.51	90.43	4.000	No	Yes	2.00
228	15.00	13.08	2.88	3.67	0.97	16.23	5.50	89.23	4.000	No	Yes	2.00
229	15.05	13.03	2.88	3.58	0.97	16.13	5.46	88.03	4.000	No	Yes	2.00
230	15.10	12.95	2.87	3.51	0.97	15.99	5.44	86.96	4.000	No	Yes	2.00
231	15.17	12.87	2.87	3.46	0.97	15.84	5.43	85.96	4.000	No	Yes	2.00
232	15.25	12.79	2.87	3.41	0.97	15.69	5.42	85.06	4.000	No	Yes	2.00
233	15.30	12.71	2.87	3.35	0.97	15.56	5.41	84.17	4.000	No	Yes	2.00
234	15.36	12.61	2.87	3.31	0.97	15.39	5.41	83.29	4.000	No	Yes	2.00
235	15.45	12.52	2.87	3.26	0.97	15.23	5.41	82.36	4.000	No	Yes	2.00
236	15.49	12.41	2.87	3.21	0.97	15.06	5.41	81.49	4.000	No	Yes	2.00
237	15.57	12.29	2.87	3.18	0.97	14.87	5.43	80.69	4.000	No	Yes	2.00
238	15.64	12.18	2.87	3.16	0.97	14.70	5.45	80.12	4.000	No	Yes	2.00
239	15.69	12.09	2.88	3.16	0.97	14.56	5.48	79.78	4.000	No	Yes	2.00
240	15.77	11.98	2.88	3.17	0.97	14.39	5.53	79.54	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
241	15.85	11.82	2.89	3.22	0.98	14.15	5.62	79.57	4.000	No	Yes	2.00
242	15.89	11.63	2.90	3.28	0.98	13.90	5.73	79.64	4.000	No	Yes	2.00
243	15.99	11.42	2.92	3.36	0.99	13.60	5.86	79.77	4.000	No	Yes	2.00
244	16.05	11.18	2.93	3.46	0.99	13.29	6.02	80.06	4.000	No	Yes	2.00
245	16.09	10.95	2.95	3.55	1.00	13.00	6.17	80.24	4.000	No	Yes	2.00
246	16.16	10.68	2.96	3.65	1.00	12.63	6.35	80.24	4.000	No	Yes	2.00
247	16.24	10.38	2.98	3.74	1.00	12.21	6.55	79.98	4.000	No	Yes	2.00
248	16.30	10.10	3.00	3.81	1.00	11.82	6.73	79.51	4.000	No	Yes	2.00
249	16.34	9.80	3.01	3.86	1.00	11.42	6.90	78.82	4.000	No	Yes	2.00
250	16.44	9.56	3.03	3.87	1.00	11.07	7.03	77.83	4.000	No	Yes	2.00
251	16.48	9.34	3.03	3.87	1.00	10.78	7.14	76.90	4.000	No	Yes	2.00
252	16.54	9.16	3.04	3.84	1.00	10.52	7.21	75.93	4.000	No	Yes	2.00
253	16.63	9.03	3.04	3.80	1.00	10.33	7.26	74.93	4.000	No	Yes	2.00
254	16.69	8.94	3.04	3.73	1.00	10.19	7.26	73.96	4.000	No	Yes	2.00
255	16.74	8.91	3.04	3.63	1.00	10.14	7.20	72.99	4.000	No	Yes	2.00
256	16.82	8.90	3.03	3.54	1.00	10.10	7.14	72.11	4.000	No	Yes	2.00
257	16.90	8.88	3.03	3.46	1.00	10.04	7.09	71.21	4.000	No	Yes	2.00
258	16.94	8.94	3.02	3.37	1.00	10.09	6.99	70.59	4.000	No	Yes	2.00
259	17.03	8.98	3.02	3.30	1.00	10.11	6.93	70.04	4.000	No	Yes	2.00
260	17.07	8.99	3.01	3.24	1.00	10.11	6.88	69.52	4.000	No	Yes	2.00
261	17.13	8.97	3.02	3.26	1.00	10.07	6.91	69.59	4.000	No	Yes	2.00
262	17.21	8.95	3.02	3.34	1.00	10.01	7.00	70.13	4.000	No	Yes	2.00
263	17.26	9.06	3.03	3.44	1.00	10.15	7.04	71.40	4.000	No	Yes	2.00
264	17.33	9.38	3.02	3.52	1.00	10.52	6.96	73.22	4.000	No	Yes	2.00
265	17.41	9.84	3.00	3.57	1.00	11.06	6.80	75.19	4.000	No	Yes	2.00
266	17.48	10.47	2.98	3.58	1.00	11.81	6.55	77.41	4.000	No	Yes	2.00
267	17.53	11.02	2.97	3.63	1.00	12.49	6.38	79.66	4.000	No	Yes	2.00
268	17.61	11.59	2.95	3.66	1.00	13.15	6.21	81.69	4.000	No	Yes	2.00
269	17.67	12.19	2.93	3.67	0.99	13.84	6.04	83.58	4.000	No	Yes	2.00
270	17.72	12.75	2.91	3.60	0.99	14.48	5.83	84.41	4.000	No	Yes	2.00
271	17.82	13.25	2.89	3.50	0.98	15.02	5.63	84.59	4.000	No	Yes	2.00
272	17.88	13.49	2.88	3.42	0.97	15.26	5.52	84.31	4.000	No	Yes	2.00
273	17.92	13.46	2.88	3.37	0.97	15.20	5.50	83.57	4.000	No	Yes	2.00
274	18.02	13.24	2.88	3.34	0.97	14.89	5.54	82.55	4.000	No	Yes	2.00
275	18.07	12.93	2.89	3.32	0.98	14.50	5.62	81.41	4.000	No	Yes	2.00
276	18.14	12.53	2.90	3.32	0.98	14.00	5.73	80.27	4.000	No	Yes	2.00
277	18.20	12.25	2.91	3.28	0.98	13.64	5.80	79.05	4.000	No	Yes	2.00
278	18.27	12.04	2.91	3.25	0.99	13.36	5.84	78.00	4.000	No	Yes	2.00
279	18.32	11.94	2.92	3.23	0.99	13.22	5.87	77.57	4.000	No	Yes	2.00
280	18.38	11.89	2.92	3.24	0.99	13.14	5.89	77.43	4.000	No	Yes	2.00
281	18.47	11.95	2.92	3.23	0.99	13.17	5.88	77.44	4.000	No	Yes	2.00
282	18.51	12.13	2.91	3.20	0.98	13.36	5.80	77.55	4.000	No	Yes	2.00
283	18.57	12.37	2.90	3.17	0.98	13.61	5.71	77.73	4.000	No	Yes	2.00
284	18.67	12.54	2.89	3.13	0.98	13.76	5.64	77.68	4.000	No	Yes	2.00
285	18.71	12.82	2.88	3.04	0.97	14.06	5.50	77.30	4.000	No	Yes	2.00
286	18.81	13.01	2.87	2.96	0.97	14.23	5.40	76.81	4.000	No	Yes	2.00
287	18.86	13.15	2.86	2.87	0.96	14.35	5.30	76.04	4.000	No	Yes	2.00
288	18.91	13.20	2.85	2.78	0.96	14.38	5.22	74.98	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
289	18.97	13.23	2.84	2.69	0.96	14.38	5.14	73.92	4.000	No	Yes	2.00
290	19.06	13.28	2.83	2.60	0.95	14.39	5.06	72.81	4.000	No	Yes	2.00
291	19.11	13.35	2.83	2.55	0.95	14.44	5.01	72.28	4.000	No	Yes	2.00
292	19.21	13.59	2.81	2.49	0.95	14.66	4.91	71.98	4.000	No	Yes	2.00
293	19.27	14.02	2.80	2.48	0.94	15.12	4.80	72.63	4.000	No	Yes	2.00
294	19.31	14.78	2.78	2.50	0.94	15.97	4.65	74.33	4.000	No	Yes	2.00
295	19.41	16.02	2.76	2.54	0.93	17.32	4.45	77.15	4.000	No	Yes	2.00
296	19.46	17.53	2.73	2.58	0.92	19.00	4.24	80.48	4.000	No	Yes	2.00
297	19.51	19.45	2.69	2.56	0.90	21.12	3.95	83.35	4.000	No	Yes	2.00
298	19.56	21.37	2.66	2.54	0.89	23.23	3.70	85.96	4.000	No	Yes	2.00
299	19.63	22.73	2.64	2.58	0.88	24.70	3.59	88.73	4.000	No	Yes	2.00
300	19.71	23.86	2.63	2.65	0.88	25.91	3.53	91.41	4.000	No	Yes	2.00
301	19.80	24.54	2.63	2.76	0.88	26.62	3.55	94.40	4.000	No	Yes	2.00
302	19.82	25.00	2.64	2.90	0.88	27.14	3.59	97.46	4.000	No	Yes	2.00
303	19.91	24.70	2.67	3.11	0.89	26.78	3.75	100.50	4.000	No	Yes	2.00
304	19.95	25.51	2.66	3.15	0.89	27.65	3.70	102.41	4.000	No	Yes	2.00
305	20.02	26.21	2.65	3.18	0.89	28.37	3.67	103.99	4.000	No	Yes	2.00
306	20.11	26.74	2.65	3.26	0.89	28.89	3.67	105.99	4.000	No	Yes	2.00
307	20.15	27.33	2.65	3.34	0.89	29.52	3.67	108.26	4.000	No	Yes	2.00
308	20.24	28.50	2.64	3.35	0.88	30.73	3.59	110.30	4.000	No	Yes	2.00
309	20.29	30.11	2.62	3.33	0.87	32.44	3.46	112.35	4.000	No	Yes	2.00
310	20.36	32.24	2.60	3.28	0.86	34.68	3.30	114.39	0.219	No	No	0.59
311	20.41	34.37	2.57	3.21	0.85	36.93	3.15	116.15	0.226	No	No	0.61
312	20.48	36.70	2.54	3.13	0.84	39.36	2.99	117.57	0.231	No	No	0.62
313	20.56	36.71	2.55	3.26	0.85	39.31	3.05	120.01	0.241	No	No	0.65
314	20.66	35.87	2.58	3.45	0.86	38.33	3.20	122.64	0.252	No	No	0.68
315	20.71	34.56	2.61	3.69	0.87	36.92	3.39	125.21	4.000	No	Yes	2.00
316	20.74	32.81	2.65	3.95	0.88	35.04	3.63	127.16	4.000	No	Yes	2.00
317	20.82	30.71	2.69	4.22	0.90	32.73	3.91	128.02	4.000	No	Yes	2.00
318	20.91	28.18	2.74	4.54	0.92	29.93	4.29	128.26	4.000	No	Yes	2.00
319	20.95	25.20	2.80	4.93	0.94	26.71	4.78	127.59	4.000	No	Yes	2.00
320	21.03	22.22	2.87	5.40	0.97	23.43	5.39	126.25	4.000	No	Yes	2.00
321	21.11	19.51	2.94	5.92	0.99	20.46	6.08	124.37	4.000	No	Yes	2.00
322	21.15	17.79	2.98	6.19	1.00	18.53	6.55	121.46	4.000	No	Yes	2.00
323	21.22	17.08	2.99	6.13	1.00	17.69	6.69	118.28	4.000	No	Yes	2.00
324	21.26	16.89	2.99	5.90	1.00	17.46	6.61	115.41	4.000	Yes	Yes	2.00
325	21.34	17.65	2.95	5.46	1.00	18.26	6.21	113.47	4.000	Yes	Yes	2.00
326	21.41	19.06	2.90	5.00	0.98	19.71	5.70	112.40	4.000	Yes	Yes	2.00
327	21.48	21.43	2.83	4.45	0.95	22.18	5.03	111.65	4.000	Yes	Yes	2.00
328	21.52	24.31	2.75	3.97	0.92	25.19	4.41	111.09	4.000	Yes	Yes	2.00
329	21.61	27.48	2.68	3.57	0.90	28.46	3.88	110.44	4.000	Yes	Yes	2.00
330	21.66	30.96	2.62	3.22	0.87	32.05	3.43	109.80	4.000	Yes	Yes	2.00
331	21.76	34.47	2.56	2.97	0.85	35.62	3.08	109.70	4.000	Yes	No	2.00
332	21.81	38.00	2.51	2.78	0.83	39.23	2.81	110.19	4.000	Yes	No	2.00
333	21.85	41.47	2.46	2.63	0.81	42.78	2.59	110.86	4.000	Yes	No	2.00
334	21.92	44.74	2.43	2.51	0.80	46.08	2.42	111.70	4.000	Yes	No	2.00
335	22.01	47.97	2.39	2.43	0.79	49.30	2.29	113.00	4.000	Yes	No	2.00
336	22.09	50.58	2.37	2.38	0.78	51.88	2.20	114.29	0.219	No	No	0.58

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
337	22.12	53.36	2.35	2.34	0.77	54.70	2.12	116.09	0.225	No	No	0.60
338	22.20	56.17	2.33	2.31	0.76	57.47	2.05	117.96	0.233	No	No	0.62
339	22.29	59.12	2.31	2.28	0.76	60.36	1.99	119.83	0.240	No	No	0.63
340	22.31	62.19	2.29	2.23	0.75	63.46	1.91	121.53	0.247	No	No	0.65
341	22.40	64.97	2.27	2.19	0.74	66.14	1.86	122.95	0.253	No	No	0.67
342	22.45	67.71	2.25	2.16	0.73	68.85	1.81	124.62	0.260	No	No	0.69
343	22.51	70.07	2.24	2.14	0.73	71.14	1.77	126.20	0.267	No	No	0.70
344	22.60	72.08	2.23	2.10	0.72	73.01	1.74	126.79	0.270	No	No	0.71
345	22.64	73.69	2.21	2.02	0.72	74.54	1.69	125.89	0.266	No	No	0.70
346	22.75	74.70	2.19	1.95	0.71	75.33	1.65	124.57	0.260	No	No	0.68
347	22.80	75.19	2.18	1.89	0.71	75.71	1.63	123.38	0.255	No	No	0.67
348	22.85	75.11	2.18	1.85	0.71	75.52	1.62	122.10	0.249	No	No	0.66
349	22.91	74.60	2.18	1.83	0.70	74.89	1.61	120.84	0.244	No	No	0.64
350	22.99	74.00	2.18	1.84	0.71	74.15	1.63	120.66	0.243	No	No	0.64
351	23.08	73.13	2.19	1.87	0.71	73.14	1.65	120.60	0.243	No	No	0.64
352	23.10	71.45	2.21	1.94	0.72	71.45	1.69	120.90	0.244	No	No	0.64
353	23.18	69.67	2.23	2.04	0.73	69.57	1.75	121.90	4.000	Yes	No	2.00
354	23.26	67.59	2.27	2.20	0.74	67.40	1.85	124.40	4.000	Yes	No	2.00
355	23.30	65.04	2.30	2.39	0.75	64.84	1.96	127.10	4.000	Yes	No	2.00
356	23.37	61.42	2.35	2.60	0.77	61.15	2.11	128.98	4.000	Yes	No	2.00
357	23.46	57.08	2.40	2.82	0.79	56.69	2.29	130.03	4.000	Yes	No	2.00
358	23.51	52.26	2.45	3.06	0.81	51.82	2.52	130.48	4.000	Yes	No	2.00
359	23.56	47.18	2.50	3.24	0.83	46.67	2.76	128.64	4.000	Yes	No	2.00
360	23.63	42.20	2.55	3.41	0.85	41.60	3.03	125.94	4.000	Yes	No	2.00
361	23.72	37.88	2.59	3.49	0.86	37.16	3.28	121.71	4.000	Yes	No	2.00
362	23.79	33.58	2.64	3.56	0.88	32.77	3.56	116.82	4.000	Yes	Yes	2.00
363	23.87	29.73	2.68	3.59	0.90	28.83	3.86	111.37	4.000	Yes	Yes	2.00
364	23.91	26.52	2.72	3.54	0.91	25.57	4.12	105.33	4.000	Yes	Yes	2.00
365	23.96	24.53	2.73	3.39	0.92	23.53	4.24	99.72	4.000	Yes	Yes	2.00
366	24.02	23.43	2.73	3.22	0.92	22.37	4.26	95.24	4.000	No	Yes	2.00
367	24.11	22.70	2.73	3.07	0.92	21.59	4.25	91.81	4.000	No	Yes	2.00
368	24.20	22.25	2.74	3.01	0.92	21.07	4.27	90.02	4.000	No	Yes	2.00
369	24.22	21.77	2.74	2.98	0.92	20.58	4.32	88.89	4.000	No	Yes	2.00
370	24.31	21.48	2.75	2.98	0.92	20.25	4.36	88.24	4.000	No	Yes	2.00
371	24.39	21.34	2.75	2.98	0.92	20.06	4.39	88.00	4.000	No	Yes	2.00
372	24.42	21.29	2.75	2.98	0.92	20.00	4.39	87.84	4.000	No	Yes	2.00
373	24.51	21.19	2.75	2.97	0.92	19.85	4.40	87.42	4.000	No	Yes	2.00
374	24.55	21.20	2.75	2.92	0.92	19.83	4.37	86.67	4.000	No	Yes	2.00
375	24.63	20.99	2.75	2.86	0.92	19.58	4.37	85.49	4.000	No	Yes	2.00
376	24.71	20.75	2.75	2.80	0.92	19.30	4.36	84.15	4.000	No	Yes	2.00
377	24.75	20.38	2.75	2.73	0.92	18.92	4.36	82.54	4.000	No	Yes	2.00
378	24.81	19.90	2.75	2.67	0.92	18.40	4.39	80.85	4.000	No	Yes	2.00
379	24.90	19.35	2.76	2.61	0.93	17.82	4.44	79.04	4.000	No	Yes	2.00
380	24.94	18.79	2.76	2.53	0.93	17.25	4.46	76.96	4.000	No	Yes	2.00
381	25.01	18.24	2.77	2.47	0.93	16.67	4.51	75.15	4.000	No	Yes	2.00
382	25.07	17.67	2.77	2.43	0.93	16.09	4.57	73.59	4.000	No	Yes	2.00
383	25.15	17.08	2.79	2.43	0.94	15.48	4.69	72.54	4.000	No	Yes	2.00
384	25.20	16.59	2.80	2.46	0.94	14.97	4.82	72.13	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
385	25.28	16.23	2.82	2.51	0.95	14.59	4.94	72.03	4.000	No	Yes	2.00
386	25.35	16.04	2.83	2.56	0.95	14.38	5.03	72.34	4.000	No	Yes	2.00
387	25.40	16.03	2.83	2.60	0.95	14.36	5.07	72.78	4.000	No	Yes	2.00
388	25.48	16.13	2.84	2.68	0.96	14.42	5.12	73.82	4.000	No	Yes	2.00
389	25.55	16.28	2.85	2.80	0.96	14.54	5.19	75.56	4.000	No	Yes	2.00
390	25.60	16.45	2.85	2.93	0.96	14.69	5.26	77.34	4.000	No	Yes	2.00
391	25.67	16.64	2.86	3.05	0.97	14.85	5.33	79.14	4.000	No	Yes	2.00
392	25.75	16.81	2.87	3.17	0.97	15.00	5.39	80.81	4.000	No	Yes	2.00
393	25.79	16.95	2.87	3.28	0.97	15.12	5.45	82.31	4.000	No	Yes	2.00
394	25.90	17.27	2.87	3.33	0.97	15.38	5.43	83.51	4.000	No	Yes	2.00
395	25.95	17.61	2.87	3.37	0.97	15.69	5.40	84.65	4.000	No	Yes	2.00
396	26.01	17.91	2.87	3.41	0.97	15.95	5.37	85.69	4.000	No	Yes	2.00
397	26.09	18.18	2.86	3.43	0.97	16.17	5.34	86.33	4.000	No	Yes	2.00
398	26.13	18.45	2.85	3.39	0.96	16.42	5.27	86.44	4.000	No	Yes	2.00
399	26.19	18.70	2.85	3.35	0.96	16.64	5.20	86.46	4.000	No	Yes	2.00
400	26.27	19.02	2.84	3.31	0.96	16.91	5.12	86.51	4.000	No	Yes	2.00
401	26.34	19.37	2.83	3.27	0.95	17.21	5.03	86.57	4.000	No	Yes	2.00
402	26.39	19.82	2.82	3.21	0.95	17.61	4.92	86.67	4.000	No	Yes	2.00
403	26.47	20.03	2.81	3.20	0.95	17.78	4.88	86.84	4.000	No	Yes	2.00
404	26.54	20.17	2.81	3.20	0.95	17.88	4.87	87.04	4.000	No	Yes	2.00
405	26.58	20.25	2.81	3.21	0.95	17.94	4.87	87.28	4.000	No	Yes	2.00
406	26.67	20.26	2.81	3.23	0.95	17.90	4.88	87.44	4.000	No	Yes	2.00
407	26.73	20.23	2.81	3.25	0.95	17.85	4.91	87.63	4.000	No	Yes	2.00
408	26.78	20.16	2.82	3.27	0.95	17.76	4.93	87.62	4.000	No	Yes	2.00
409	26.85	20.02	2.82	3.27	0.95	17.59	4.96	87.31	4.000	No	Yes	2.00
410	26.93	19.87	2.82	3.26	0.95	17.41	4.99	86.92	4.000	No	Yes	2.00
411	26.98	19.65	2.83	3.27	0.95	17.18	5.04	86.58	4.000	No	Yes	2.00
412	27.03	19.48	2.83	3.27	0.95	17.00	5.07	86.22	4.000	No	Yes	2.00
413	27.13	19.33	2.84	3.27	0.96	16.82	5.10	85.81	4.000	No	Yes	2.00
414	27.17	19.21	2.84	3.27	0.96	16.68	5.13	85.52	4.000	No	Yes	2.00
415	27.24	19.07	2.84	3.26	0.96	16.52	5.15	85.13	4.000	No	Yes	2.00
416	27.33	18.86	2.85	3.28	0.96	16.29	5.21	84.82	4.000	No	Yes	2.00
417	27.36	18.63	2.86	3.31	0.96	16.05	5.28	84.72	4.000	No	Yes	2.00
418	27.43	18.38	2.86	3.35	0.97	15.79	5.36	84.58	4.000	No	Yes	2.00
419	27.53	18.13	2.87	3.39	0.97	15.51	5.44	84.43	4.000	No	Yes	2.00
420	27.60	17.91	2.88	3.40	0.97	15.28	5.50	84.05	4.000	No	Yes	2.00
421	27.63	17.70	2.88	3.39	0.97	15.07	5.54	83.47	4.000	No	Yes	2.00
422	27.72	17.52	2.89	3.36	0.97	14.87	5.57	82.75	4.000	No	Yes	2.00
423	27.77	17.42	2.89	3.31	0.97	14.76	5.55	81.96	4.000	No	Yes	2.00
424	27.84	17.46	2.88	3.25	0.97	14.77	5.50	81.27	4.000	No	Yes	2.00
425	27.93	17.59	2.87	3.17	0.97	14.85	5.42	80.54	4.000	No	Yes	2.00
426	27.97	17.75	2.86	3.09	0.97	14.99	5.33	79.83	4.000	No	Yes	2.00
427	28.02	17.89	2.85	3.02	0.96	15.10	5.25	79.27	4.000	No	Yes	2.00
428	28.12	18.02	2.85	2.96	0.96	15.18	5.18	78.68	4.000	No	Yes	2.00
429	28.17	18.17	2.84	2.89	0.96	15.30	5.11	78.11	4.000	No	Yes	2.00
430	28.22	18.28	2.83	2.84	0.95	15.38	5.05	77.72	4.000	No	Yes	2.00
431	28.32	18.30	2.83	2.83	0.95	15.36	5.05	77.57	4.000	No	Yes	2.00
432	28.36	18.44	2.83	2.81	0.95	15.47	5.01	77.50	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
433	28.42	18.88	2.81	2.77	0.95	15.86	4.90	77.73	4.000	No	Yes	2.00
434	28.48	19.31	2.80	2.73	0.94	16.24	4.80	77.88	4.000	No	Yes	2.00
435	28.57	19.74	2.79	2.69	0.94	16.59	4.70	78.01	4.000	No	Yes	2.00
436	28.62	20.26	2.78	2.68	0.93	17.05	4.62	78.69	4.000	No	Yes	2.00
437	28.72	20.70	2.77	2.70	0.93	17.42	4.56	79.51	4.000	No	Yes	2.00
438	28.75	20.99	2.77	2.76	0.93	17.67	4.57	80.80	4.000	No	Yes	2.00
439	28.82	21.18	2.78	2.85	0.93	17.81	4.62	82.31	4.000	No	Yes	2.00
440	28.87	21.43	2.78	2.92	0.94	18.01	4.64	83.55	4.000	No	Yes	2.00
441	28.95	21.50	2.79	2.99	0.94	18.04	4.69	84.52	4.000	No	Yes	2.00
442	29.02	21.16	2.80	3.06	0.94	17.70	4.80	84.88	4.000	No	Yes	2.00
443	29.07	20.75	2.82	3.14	0.95	17.30	4.92	85.13	4.000	No	Yes	2.00
444	29.16	20.35	2.83	3.22	0.95	16.89	5.05	85.34	4.000	No	Yes	2.00
445	29.21	19.87	2.84	3.27	0.96	16.43	5.17	85.00	4.000	No	Yes	2.00
446	29.29	19.55	2.85	3.27	0.96	16.11	5.23	84.30	4.000	No	Yes	2.00
447	29.36	19.41	2.85	3.20	0.96	15.96	5.22	83.25	4.000	No	Yes	2.00
448	29.40	19.63	2.83	3.07	0.95	16.15	5.08	81.96	4.000	No	Yes	2.00
449	29.47	19.93	2.82	2.93	0.95	16.39	4.93	80.76	4.000	No	Yes	2.00
450	29.56	20.29	2.80	2.82	0.94	16.68	4.78	79.82	4.000	No	Yes	2.00
451	29.60	20.70	2.78	2.73	0.94	17.04	4.66	79.35	4.000	No	Yes	2.00
452	29.71	21.12	2.77	2.68	0.93	17.37	4.56	79.22	4.000	No	Yes	2.00
453	29.75	21.53	2.76	2.64	0.93	17.73	4.47	79.29	4.000	No	Yes	2.00
454	29.79	21.94	2.75	2.62	0.92	18.08	4.40	79.51	4.000	No	Yes	2.00
455	29.86	22.27	2.75	2.62	0.92	18.35	4.36	80.05	4.000	No	Yes	2.00
456	29.95	22.60	2.75	2.64	0.92	18.60	4.34	80.71	4.000	No	Yes	2.00
457	30.04	22.87	2.74	2.67	0.92	18.80	4.33	81.39	4.000	No	Yes	2.00
458	30.06	23.16	2.74	2.69	0.92	19.06	4.31	82.09	4.000	No	Yes	2.00
459	30.15	23.46	2.74	2.71	0.92	19.28	4.30	82.82	4.000	No	Yes	2.00
460	30.20	23.80	2.74	2.75	0.92	19.56	4.28	83.76	4.000	No	Yes	2.00
461	30.28	24.21	2.74	2.80	0.92	19.88	4.28	85.00	4.000	No	Yes	2.00
462	30.35	24.55	2.74	2.85	0.92	20.15	4.28	86.18	4.000	No	Yes	2.00
463	30.39	24.85	2.74	2.89	0.92	20.40	4.28	87.23	4.000	No	Yes	2.00
464	30.45	25.09	2.74	2.93	0.92	20.58	4.28	88.07	4.000	No	Yes	2.00
465	30.54	25.24	2.74	2.97	0.92	20.67	4.30	88.84	4.000	No	Yes	2.00
466	30.60	25.09	2.75	3.05	0.92	20.50	4.38	89.73	4.000	No	Yes	2.00
467	30.67	24.78	2.76	3.14	0.93	20.19	4.48	90.39	4.000	No	Yes	2.00
468	30.74	24.41	2.78	3.22	0.93	19.81	4.58	90.80	4.000	No	Yes	2.00
469	30.79	23.91	2.79	3.29	0.94	19.35	4.70	90.92	4.000	No	Yes	2.00
470	30.86	23.34	2.80	3.29	0.94	18.82	4.78	89.92	4.000	No	Yes	2.00
471	30.95	22.81	2.81	3.27	0.94	18.30	4.84	88.68	4.000	No	Yes	2.00
472	30.99	22.25	2.81	3.24	0.95	17.80	4.91	87.32	4.000	No	Yes	2.00
473	31.05	21.70	2.82	3.20	0.95	17.29	4.96	85.85	4.000	No	Yes	2.00
474	31.14	21.26	2.82	3.13	0.95	16.87	4.99	84.23	4.000	No	Yes	2.00
475	31.19	20.89	2.82	3.05	0.95	16.53	4.99	82.51	4.000	No	Yes	2.00
476	31.26	20.65	2.82	2.96	0.95	16.30	4.96	80.93	4.000	No	Yes	2.00
477	31.34	20.47	2.82	2.86	0.95	16.11	4.93	79.38	4.000	No	Yes	2.00
478	31.39	20.36	2.81	2.77	0.95	16.00	4.87	77.95	4.000	No	Yes	2.00
479	31.45	20.34	2.81	2.74	0.95	15.96	4.86	77.54	4.000	No	Yes	2.00
480	31.54	20.41	2.80	2.70	0.94	15.99	4.82	77.08	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
481	31.57	20.70	2.79	2.62	0.94	16.25	4.71	76.52	4.000	No	Yes	2.00
482	31.63	21.26	2.78	2.56	0.93	16.71	4.58	76.48	4.000	No	Yes	2.00
483	31.73	21.86	2.76	2.52	0.93	17.20	4.46	76.78	4.000	No	Yes	2.00
484	31.77	22.65	2.75	2.50	0.92	17.87	4.34	77.50	4.000	No	Yes	2.00
485	31.84	23.37	2.73	2.49	0.92	18.47	4.24	78.35	4.000	No	Yes	2.00
486	31.93	23.77	2.73	2.54	0.92	18.77	4.24	79.51	4.000	No	Yes	2.00
487	31.98	24.18	2.73	2.58	0.92	19.10	4.22	80.58	4.000	No	Yes	2.00
488	32.05	24.49	2.73	2.60	0.91	19.34	4.20	81.23	4.000	No	Yes	2.00
489	32.09	24.69	2.73	2.64	0.91	19.49	4.21	82.07	4.000	No	Yes	2.00
490	32.17	24.77	2.74	2.71	0.92	19.51	4.26	83.19	4.000	No	Yes	2.00
491	32.22	24.56	2.75	2.78	0.92	19.30	4.34	83.85	4.000	No	Yes	2.00
492	32.32	24.33	2.75	2.83	0.92	19.06	4.41	84.14	4.000	No	Yes	2.00
493	32.35	24.03	2.76	2.86	0.93	18.79	4.47	84.07	4.000	No	Yes	2.00
494	32.43	23.76	2.77	2.87	0.93	18.52	4.52	83.76	4.000	No	Yes	2.00
495	32.52	23.80	2.76	2.83	0.93	18.52	4.49	83.20	4.000	No	Yes	2.00
496	32.57	23.78	2.76	2.79	0.93	18.49	4.47	82.69	4.000	No	Yes	2.00
497	32.62	23.81	2.76	2.76	0.93	18.49	4.45	82.23	4.000	No	Yes	2.00
498	32.71	23.88	2.75	2.72	0.92	18.52	4.41	81.74	4.000	No	Yes	2.00
499	32.76	23.92	2.75	2.69	0.92	18.53	4.39	81.27	4.000	No	Yes	2.00
500	32.82	24.02	2.75	2.67	0.92	18.59	4.36	81.13	4.000	No	Yes	2.00
501	32.90	24.07	2.75	2.67	0.92	18.60	4.36	81.14	4.000	No	Yes	2.00
502	32.96	24.10	2.75	2.68	0.92	18.60	4.37	81.31	4.000	No	Yes	2.00
503	33.02	24.16	2.75	2.71	0.92	18.62	4.39	81.74	4.000	No	Yes	2.00
504	33.11	24.21	2.76	2.75	0.92	18.62	4.42	82.23	4.000	No	Yes	2.00
505	33.17	24.32	2.76	2.78	0.93	18.69	4.43	82.78	4.000	No	Yes	2.00
506	33.22	24.44	2.76	2.81	0.93	18.77	4.44	83.33	4.000	No	Yes	2.00
507	33.31	24.49	2.76	2.84	0.93	18.77	4.46	83.74	4.000	No	Yes	2.00
508	33.34	24.51	2.76	2.86	0.93	18.77	4.48	84.12	4.000	No	Yes	2.00
509	33.41	24.52	2.76	2.87	0.93	18.75	4.49	84.14	4.000	No	Yes	2.00
510	33.49	24.50	2.77	2.88	0.93	18.69	4.51	84.23	4.000	No	Yes	2.00
511	33.57	24.46	2.77	2.89	0.93	18.63	4.52	84.25	4.000	No	Yes	2.00
512	33.61	24.39	2.77	2.88	0.93	18.55	4.53	84.05	4.000	No	Yes	2.00
513	33.68	24.39	2.77	2.88	0.93	18.52	4.53	83.87	4.000	No	Yes	2.00
514	33.76	24.41	2.77	2.87	0.93	18.50	4.53	83.81	4.000	No	Yes	2.00
515	33.81	24.49	2.77	2.89	0.93	18.55	4.53	84.09	4.000	No	Yes	2.00
516	33.88	24.70	2.77	2.92	0.93	18.69	4.54	84.79	4.000	No	Yes	2.00
517	33.95	24.97	2.77	2.98	0.93	18.88	4.55	85.91	4.000	No	Yes	2.00
518	34.01	25.30	2.77	3.06	0.93	19.12	4.57	87.39	4.000	No	Yes	2.00
519	34.06	25.58	2.78	3.14	0.93	19.32	4.60	88.93	4.000	No	Yes	2.00
520	34.13	25.81	2.78	3.24	0.94	19.47	4.65	90.56	4.000	No	Yes	2.00
521	34.21	25.99	2.79	3.38	0.94	19.58	4.73	92.59	4.000	No	Yes	2.00
522	34.25	26.13	2.80	3.51	0.94	19.66	4.81	94.49	4.000	No	Yes	2.00
523	34.35	26.22	2.81	3.64	0.95	19.68	4.89	96.14	4.000	No	Yes	2.00
524	34.40	26.26	2.82	3.75	0.95	19.68	4.96	97.59	4.000	No	Yes	2.00
525	34.49	26.26	2.83	3.84	0.95	19.62	5.03	98.65	4.000	No	Yes	2.00
526	34.53	26.21	2.83	3.92	0.96	19.56	5.09	99.47	4.000	No	Yes	2.00
527	34.60	26.13	2.84	3.98	0.96	19.45	5.14	100.04	4.000	No	Yes	2.00
528	34.65	26.05	2.85	4.04	0.96	19.36	5.19	100.56	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
529	34.74	26.01	2.85	4.10	0.96	19.28	5.24	101.09	4.000	No	Yes	2.00
530	34.80	25.96	2.85	4.12	0.96	19.21	5.27	101.16	4.000	No	Yes	2.00
531	34.85	25.81	2.86	4.13	0.96	19.06	5.30	100.98	4.000	No	Yes	2.00
532	34.93	25.63	2.86	4.15	0.97	18.87	5.34	100.73	4.000	No	Yes	2.00
533	34.98	25.37	2.87	4.18	0.97	18.64	5.39	100.52	4.000	No	Yes	2.00
534	35.05	25.16	2.87	4.19	0.97	18.43	5.44	100.22	4.000	No	Yes	2.00
535	35.15	24.95	2.88	4.19	0.97	18.22	5.47	99.73	4.000	No	Yes	2.00
536	35.20	24.79	2.88	4.18	0.97	18.07	5.49	99.23	4.000	No	Yes	2.00
537	35.25	24.73	2.88	4.12	0.97	18.00	5.47	98.37	4.000	No	Yes	2.00
538	35.33	24.69	2.87	4.03	0.97	17.94	5.42	97.25	4.000	No	Yes	2.00
539	35.40	24.65	2.87	3.96	0.97	17.88	5.39	96.31	4.000	No	Yes	2.00
540	35.44	24.77	2.86	3.89	0.97	17.97	5.33	95.69	4.000	No	Yes	2.00
541	35.50	24.93	2.85	3.82	0.96	18.08	5.26	95.04	4.000	No	Yes	2.00
542	35.59	25.19	2.84	3.72	0.96	18.26	5.16	94.29	4.000	No	Yes	2.00
543	35.64	25.39	2.84	3.65	0.96	18.41	5.09	93.74	4.000	No	Yes	2.00
544	35.70	25.56	2.83	3.60	0.95	18.52	5.04	93.37	4.000	No	Yes	2.00
545	35.79	25.66	2.83	3.57	0.95	18.57	5.01	93.11	4.000	No	Yes	2.00
546	35.83	25.68	2.83	3.58	0.95	18.57	5.02	93.19	4.000	No	Yes	2.00
547	35.94	25.66	2.83	3.58	0.95	18.50	5.03	93.05	4.000	No	Yes	2.00
548	35.98	25.62	2.83	3.57	0.95	18.45	5.03	92.86	4.000	No	Yes	2.00
549	36.03	25.44	2.83	3.57	0.95	18.29	5.06	92.51	4.000	No	Yes	2.00
550	36.09	25.17	2.84	3.58	0.96	18.05	5.10	92.12	4.000	No	Yes	2.00
551	36.17	24.77	2.85	3.60	0.96	17.69	5.18	91.67	4.000	No	Yes	2.00
552	36.23	24.32	2.85	3.63	0.96	17.31	5.27	91.14	4.000	No	Yes	2.00
553	36.29	23.82	2.86	3.64	0.97	16.88	5.35	90.37	4.000	No	Yes	2.00
554	36.38	23.31	2.87	3.64	0.97	16.44	5.44	89.39	4.000	No	Yes	2.00
555	36.44	22.79	2.88	3.63	0.97	16.01	5.52	88.30	4.000	No	Yes	2.00
556	36.49	22.27	2.89	3.62	0.98	15.58	5.60	87.26	4.000	No	Yes	2.00
557	36.59	21.81	2.90	3.61	0.98	15.17	5.68	86.23	4.000	No	Yes	2.00
558	36.63	21.37	2.91	3.61	0.98	14.82	5.76	85.28	4.000	No	Yes	2.00
559	36.69	21.03	2.91	3.59	0.98	14.53	5.81	84.42	4.000	No	Yes	2.00
560	36.78	20.84	2.91	3.55	0.98	14.35	5.82	83.57	4.000	No	Yes	2.00
561	36.82	20.75	2.91	3.49	0.98	14.28	5.80	82.81	4.000	No	Yes	2.00
562	36.88	20.77	2.91	3.43	0.98	14.28	5.75	82.14	4.000	No	Yes	2.00
563	36.98	20.81	2.90	3.38	0.98	14.28	5.71	81.57	4.000	No	Yes	2.00
564	37.02	20.88	2.90	3.32	0.98	14.33	5.66	81.09	4.000	No	Yes	2.00
565	37.11	20.95	2.89	3.28	0.98	14.36	5.62	80.71	4.000	No	Yes	2.00
566	37.18	21.00	2.89	3.25	0.98	14.38	5.59	80.40	4.000	No	Yes	2.00
567	37.22	21.09	2.89	3.23	0.97	14.44	5.56	80.31	4.000	No	Yes	2.00
568	37.28	21.20	2.88	3.24	0.97	14.50	5.55	80.51	4.000	No	Yes	2.00
569	37.38	21.34	2.89	3.26	0.97	14.58	5.55	80.94	4.000	No	Yes	2.00
570	37.42	21.53	2.88	3.29	0.97	14.71	5.54	81.52	4.000	No	Yes	2.00
571	37.48	21.73	2.88	3.32	0.97	14.84	5.54	82.15	4.000	No	Yes	2.00
572	37.57	21.96	2.88	3.31	0.97	14.99	5.50	82.37	4.000	No	Yes	2.00
573	37.62	22.23	2.87	3.26	0.97	15.19	5.42	82.24	4.000	No	Yes	2.00
574	37.68	22.47	2.86	3.22	0.97	15.36	5.35	82.23	4.000	No	Yes	2.00
575	37.77	22.71	2.86	3.22	0.96	15.51	5.32	82.51	4.000	No	Yes	2.00
576	37.82	22.94	2.86	3.21	0.96	15.67	5.28	82.75	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
577	37.88	23.12	2.85	3.18	0.96	15.79	5.24	82.68	4.000	No	Yes	2.00
578	37.96	23.17	2.85	3.17	0.96	15.81	5.22	82.50	4.000	No	Yes	2.00
579	38.00	23.39	2.84	3.12	0.96	15.98	5.15	82.25	4.000	No	Yes	2.00
580	38.08	23.81	2.83	3.03	0.95	16.29	5.02	81.76	4.000	No	Yes	2.00
581	38.12	24.25	2.81	2.95	0.95	16.62	4.90	81.46	4.000	No	Yes	2.00
582	38.20	24.73	2.80	2.89	0.94	16.97	4.79	81.32	4.000	No	Yes	2.00
583	38.27	25.09	2.79	2.85	0.94	17.24	4.72	81.32	4.000	No	Yes	2.00
584	38.36	25.41	2.78	2.82	0.94	17.46	4.65	81.20	4.000	No	Yes	2.00
585	38.40	25.70	2.78	2.82	0.93	17.66	4.62	81.62	4.000	No	Yes	2.00
586	38.46	26.47	2.77	2.85	0.93	18.23	4.55	83.02	4.000	No	Yes	2.00
587	38.56	27.70	2.75	2.84	0.92	19.15	4.41	84.43	4.000	No	Yes	2.00
588	38.59	29.37	2.73	2.83	0.92	20.44	4.23	86.38	4.000	No	Yes	2.00
589	38.66	31.20	2.71	2.85	0.91	21.82	4.08	88.94	4.000	No	Yes	2.00
590	38.76	33.40	2.69	2.91	0.90	23.47	3.94	92.37	4.000	No	Yes	2.00
591	38.79	35.50	2.68	3.00	0.90	25.07	3.84	96.19	4.000	No	Yes	2.00
592	38.87	37.72	2.66	3.09	0.89	26.74	3.74	100.07	4.000	No	Yes	2.00
593	38.91	40.14	2.65	3.20	0.89	28.57	3.66	104.53	4.000	No	Yes	2.00
594	39.00	42.72	2.64	3.28	0.88	30.49	3.56	108.61	4.000	No	Yes	2.00
595	39.04	45.10	2.62	3.34	0.88	32.30	3.48	112.39	4.000	No	Yes	2.00
596	39.11	47.29	2.62	3.48	0.87	33.92	3.45	117.11	4.000	No	Yes	2.00
597	39.20	48.94	2.62	3.67	0.88	35.08	3.48	122.18	4.000	No	Yes	2.00
598	39.24	50.53	2.63	3.86	0.88	36.22	3.51	127.28	4.000	No	Yes	2.00
599	39.31	52.73	2.63	4.06	0.88	37.81	3.52	133.19	4.000	No	Yes	2.00
600	39.38	55.69	2.63	4.22	0.88	39.99	3.49	139.41	4.000	No	Yes	2.00
601	39.46	60.04	2.61	4.28	0.87	43.26	3.36	145.48	4.000	No	Yes	2.00
602	39.51	65.29	2.58	4.30	0.86	47.26	3.21	151.76	0.405	No	No	0.98
603	39.60	70.72	2.56	4.32	0.85	51.35	3.07	157.81	4.000	Yes	No	2.00
604	39.66	76.31	2.53	4.30	0.84	55.62	2.93	163.13	4.000	Yes	No	2.00
605	39.71	81.88	2.51	4.24	0.83	59.90	2.80	167.53	4.000	Yes	No	2.00
606	39.79	87.58	2.48	4.18	0.82	64.26	2.67	171.54	4.000	Yes	No	2.00
607	39.85	95.63	2.44	4.03	0.81	70.52	2.49	175.53	4.000	Yes	No	2.00
608	39.91	106.85	2.39	3.78	0.78	79.35	2.26	179.41	4.000	Yes	No	2.00
609	39.99	119.15	2.33	3.54	0.76	89.06	2.06	183.29	4.000	Yes	No	2.00
610	40.05	129.29	2.29	3.39	0.75	97.07	1.93	187.43	4.000	Yes	No	2.00
611	40.11	136.78	2.27	3.31	0.74	102.96	1.86	191.07	4.000	Yes	No	2.00
612	40.20	143.19	2.25	3.26	0.73	107.89	1.80	194.51	0.764	No	No	1.85
613	40.25	148.57	2.24	3.25	0.73	112.05	1.77	198.24	0.805	No	No	1.95
614	40.30	153.54	2.23	3.25	0.73	115.86	1.75	202.36	4.000	No	No	2.00
615	40.40	158.28	2.23	3.28	0.72	119.33	1.73	206.73	4.000	No	No	2.00
616	40.43	160.83	2.23	3.34	0.72	121.18	1.74	210.64	4.000	No	No	2.00
617	40.49	158.66	2.24	3.45	0.73	119.18	1.78	212.23	4.000	No	No	2.00
618	40.55	153.03	2.27	3.63	0.74	114.40	1.86	212.96	4.000	No	No	2.00
619	40.64	146.29	2.30	3.83	0.75	108.69	1.96	213.19	4.000	No	No	2.00
620	40.69	139.08	2.33	3.91	0.76	102.89	2.04	209.39	4.000	No	No	2.00
621	40.80	131.58	2.35	4.01	0.77	96.75	2.12	205.56	4.000	No	No	2.00
622	40.84	124.38	2.37	4.09	0.78	91.04	2.21	201.42	4.000	No	No	2.00
623	40.89	117.63	2.39	4.14	0.79	85.72	2.29	196.43	0.785	No	No	1.90
624	40.96	111.06	2.41	4.14	0.79	80.55	2.37	190.55	0.723	No	No	1.75

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
625	41.04	102.35	2.44	4.22	0.81	73.71	2.50	184.44	0.663	No	No	1.61
626	41.10	99.25	2.44	4.09	0.81	71.35	2.50	178.24	0.607	No	No	1.47
627	41.15	97.87	2.43	3.91	0.80	70.36	2.45	172.25	0.555	No	No	1.35
628	41.24	97.68	2.41	3.69	0.80	70.24	2.37	166.66	0.511	No	No	1.24
629	41.28	99.20	2.40	3.62	0.79	71.40	2.33	166.12	0.506	No	No	1.23
630	41.38	101.83	2.39	3.51	0.78	73.35	2.26	165.46	0.501	No	No	1.22
631	41.41	104.74	2.37	3.41	0.78	75.62	2.19	165.26	0.500	No	No	1.21
632	41.49	107.45	2.35	3.33	0.77	77.66	2.13	165.11	0.499	No	No	1.21
633	41.54	110.57	2.33	3.22	0.76	80.08	2.06	164.61	0.495	No	No	1.20
634	41.61	115.81	2.30	3.05	0.75	84.17	1.95	164.14	0.491	No	No	1.19
635	41.69	117.25	2.29	2.99	0.75	85.22	1.92	163.47	0.486	No	No	1.18
636	41.77	119.86	2.27	2.89	0.74	87.23	1.86	162.49	0.479	No	No	1.16
637	41.84	123.49	2.25	2.75	0.73	90.09	1.79	161.41	0.471	No	No	1.15
638	41.88	127.85	2.22	2.61	0.72	93.59	1.71	160.50	0.465	No	No	1.13
639	41.94	131.93	2.19	2.47	0.71	96.89	1.65	159.54	0.458	No	No	1.11
640	42.04	134.67	2.17	2.36	0.70	99.03	1.60	158.18	0.448	No	No	1.09
641	42.08	136.97	2.15	2.27	0.70	100.92	1.56	157.19	0.441	No	No	1.07
642	42.17	138.21	2.14	2.21	0.69	101.83	1.54	156.42	0.436	No	No	1.06
643	42.19	138.80	2.14	2.19	0.69	102.31	1.52	155.99	0.433	No	No	1.05
644	42.28	138.18	2.14	2.19	0.69	101.67	1.53	155.46	0.429	No	No	1.05
645	42.33	136.34	2.15	2.23	0.69	100.08	1.55	155.19	0.428	No	No	1.04
646	42.39	134.30	2.16	2.28	0.70	98.29	1.58	155.17	0.427	No	No	1.04
647	42.48	131.81	2.18	2.35	0.71	96.09	1.61	155.16	0.427	No	No	1.04
648	42.53	129.20	2.20	2.43	0.71	93.85	1.66	155.50	0.430	No	No	1.05
649	42.59	127.38	2.21	2.52	0.72	92.22	1.70	156.51	0.437	No	No	1.06
650	42.67	125.63	2.23	2.61	0.72	90.61	1.74	157.58	0.444	No	No	1.08
651	42.73	123.71	2.25	2.70	0.73	88.91	1.78	158.66	0.451	No	No	1.10
652	42.81	122.02	2.26	2.79	0.74	87.35	1.83	159.78	0.459	No	No	1.12
653	42.88	120.34	2.28	2.88	0.74	85.85	1.87	160.92	0.468	No	No	1.14
654	42.92	118.62	2.29	2.97	0.75	84.36	1.92	162.09	0.476	No	No	1.16
655	43.00	116.94	2.31	3.06	0.75	82.86	1.97	163.09	0.483	No	No	1.18
656	43.08	115.33	2.32	3.15	0.76	81.42	2.02	164.14	0.491	No	No	1.20
657	43.12	113.76	2.33	3.24	0.76	80.08	2.06	165.17	0.499	No	No	1.22
658	43.21	112.31	2.35	3.32	0.77	78.78	2.11	165.99	0.505	No	No	1.23
659	43.27	110.92	2.36	3.40	0.77	77.57	2.15	166.88	0.512	No	No	1.25
660	43.32	109.66	2.37	3.48	0.78	76.47	2.20	167.89	0.520	No	No	1.27
661	43.39	108.32	2.38	3.56	0.78	75.29	2.24	168.83	0.528	No	No	1.29
662	43.47	106.67	2.40	3.65	0.79	73.88	2.30	169.61	0.534	No	No	1.31
663	43.52	104.14	2.41	3.75	0.79	71.84	2.36	169.87	0.536	No	No	1.31
664	43.59	100.71	2.43	3.86	0.80	69.13	2.45	169.67	0.534	No	No	1.31
665	43.67	95.95	2.46	4.01	0.81	65.41	2.58	168.99	0.529	No	No	1.29
666	43.72	90.92	2.49	4.16	0.82	61.58	2.72	167.69	0.519	No	No	1.27
667	43.80	85.34	2.52	4.25	0.84	57.38	2.87	164.49	0.494	No	No	1.21
668	43.85	79.27	2.55	4.35	0.85	52.89	3.04	160.68	0.466	No	No	1.14
669	43.92	73.36	2.58	4.45	0.86	48.52	3.23	156.49	0.436	No	No	1.07
670	43.97	67.07	2.62	4.56	0.87	43.93	3.46	151.94	4.000	No	Yes	2.00
671	44.04	60.96	2.66	4.66	0.89	39.49	3.72	146.78	4.000	No	Yes	2.00
672	44.13	55.89	2.69	4.70	0.90	35.84	3.94	141.26	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
673	44.17	51.45	2.72	4.67	0.91	32.70	4.14	135.24	4.000	No	Yes	2.00
674	44.24	48.10	2.73	4.55	0.92	30.35	4.25	129.08	4.000	No	Yes	2.00
675	44.31	44.77	2.75	4.43	0.92	28.03	4.39	123.05	4.000	No	Yes	2.00
676	44.37	41.91	2.77	4.39	0.93	26.01	4.56	118.63	4.000	No	Yes	2.00
677	44.45	39.66	2.79	4.30	0.94	24.44	4.68	114.39	4.000	No	Yes	2.00
678	44.50	37.60	2.80	4.17	0.94	23.02	4.77	109.69	4.000	No	Yes	2.00
679	44.56	35.90	2.80	3.97	0.94	21.87	4.79	104.78	4.000	No	Yes	2.00
680	44.65	34.31	2.81	3.80	0.94	20.77	4.83	100.36	4.000	No	Yes	2.00
681	44.71	32.87	2.81	3.67	0.95	19.79	4.89	96.76	4.000	No	Yes	2.00
682	44.76	31.94	2.82	3.60	0.95	19.15	4.94	94.64	4.000	No	Yes	2.00
683	44.85	31.50	2.82	3.55	0.95	18.82	4.96	93.38	4.000	No	Yes	2.00
684	44.88	31.89	2.81	3.54	0.95	19.08	4.91	93.73	4.000	No	Yes	2.00
685	44.96	33.14	2.80	3.58	0.94	19.89	4.81	95.77	4.000	No	Yes	2.00
686	45.05	34.91	2.79	3.64	0.94	21.05	4.70	98.87	4.000	No	Yes	2.00
687	45.10	37.96	2.76	3.65	0.93	23.13	4.44	102.79	4.000	No	Yes	2.00
688	45.17	42.19	2.72	3.63	0.91	26.02	4.13	107.56	4.000	No	Yes	2.00
689	45.25	47.02	2.68	3.59	0.89	29.34	3.82	112.20	4.000	No	Yes	2.00
690	45.30	52.22	2.63	3.54	0.88	32.95	3.55	116.82	4.000	No	Yes	2.00
691	45.37	57.78	2.59	3.49	0.86	36.82	3.30	121.32	0.246	No	No	0.61
692	45.45	63.35	2.56	3.47	0.85	40.70	3.10	126.01	0.266	No	No	0.66
693	45.49	68.76	2.53	3.45	0.84	44.49	2.93	130.44	0.286	No	No	0.71
694	45.54	73.67	2.51	3.45	0.83	47.92	2.81	134.70	0.307	No	No	0.76
695	45.61	77.83	2.49	3.48	0.83	50.78	2.73	138.84	0.329	No	No	0.81
696	45.68	80.57	2.49	3.55	0.82	52.60	2.71	142.61	0.350	No	No	0.86
697	45.75	81.52	2.49	3.65	0.83	53.13	2.74	145.41	0.366	No	No	0.90
698	45.80	81.02	2.50	3.74	0.83	52.66	2.79	147.01	0.375	No	No	0.93
699	45.89	79.02	2.52	3.85	0.84	51.09	2.88	147.36	0.378	No	No	0.93
700	45.93	75.96	2.54	3.96	0.85	48.83	3.01	146.80	0.374	No	No	0.93
701	46.01	71.99	2.57	4.07	0.86	45.92	3.16	145.23	0.365	No	No	0.90
702	46.08	67.58	2.60	4.20	0.87	42.73	3.35	143.16	4.000	No	Yes	2.00
703	46.15	63.04	2.64	4.32	0.88	39.49	3.56	140.53	4.000	No	Yes	2.00
704	46.20	58.87	2.67	4.39	0.89	36.55	3.75	137.15	4.000	No	Yes	2.00
705	46.29	55.12	2.69	4.42	0.90	33.92	3.93	133.38	4.000	No	Yes	2.00
706	46.34	52.58	2.70	4.36	0.91	32.18	4.02	129.41	4.000	No	Yes	2.00
707	46.41	51.11	2.71	4.27	0.91	31.17	4.05	126.27	4.000	No	Yes	2.00
708	46.49	50.54	2.70	4.18	0.91	30.77	4.03	124.04	4.000	No	Yes	2.00
709	46.53	50.02	2.70	4.11	0.91	30.42	4.02	122.34	4.000	No	Yes	2.00
710	46.60	49.69	2.70	4.04	0.90	30.18	4.00	120.82	4.000	No	Yes	2.00
711	46.69	49.41	2.70	3.97	0.90	29.96	3.98	119.37	4.000	No	Yes	2.00
712	46.73	49.11	2.70	3.91	0.90	29.76	3.97	118.07	4.000	No	Yes	2.00
713	46.79	48.28	2.70	3.91	0.91	29.16	4.02	117.13	4.000	No	Yes	2.00
714	46.89	47.27	2.71	3.94	0.91	28.41	4.09	116.30	4.000	No	Yes	2.00
715	46.94	45.73	2.73	4.06	0.92	27.31	4.25	116.20	4.000	No	Yes	2.00
716	46.99	44.21	2.76	4.25	0.93	26.21	4.47	117.04	4.000	No	Yes	2.00
717	47.09	42.89	2.79	4.46	0.94	25.21	4.68	118.10	4.000	No	Yes	2.00
718	47.13	41.81	2.81	4.68	0.95	24.41	4.89	119.40	4.000	No	Yes	2.00
719	47.19	42.93	2.80	4.70	0.94	25.12	4.82	121.09	4.000	No	Yes	2.00
720	47.28	44.62	2.79	4.65	0.94	26.20	4.68	122.72	4.000	Yes	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
721	47.34	47.80	2.75	4.51	0.92	28.32	4.41	124.80	4.000	Yes	Yes	2.00
722	47.38	54.01	2.69	4.18	0.90	32.56	3.90	127.10	4.000	Yes	Yes	2.00
723	47.50	61.85	2.61	3.82	0.87	37.94	3.40	129.13	4.000	Yes	Yes	2.00
724	47.51	72.72	2.52	3.42	0.84	45.60	2.88	131.32	4.000	Yes	No	2.00
725	47.60	84.57	2.44	3.07	0.80	54.02	2.47	133.24	4.000	Yes	No	2.00
726	47.69	97.97	2.35	2.77	0.77	63.68	2.13	135.74	4.000	Yes	No	2.00
727	47.70	112.59	2.28	2.51	0.74	74.42	1.87	139.45	4.000	Yes	No	2.00
728	47.80	125.94	2.22	2.34	0.72	84.20	1.71	143.67	4.000	Yes	No	2.00
729	47.84	139.39	2.16	2.19	0.70	94.21	1.58	148.64	4.000	Yes	No	2.00
730	47.91	151.60	2.12	2.07	0.68	103.34	1.48	153.39	4.000	Yes	No	2.00
731	48.00	161.22	2.08	1.98	0.67	110.51	1.42	157.32	4.000	Yes	No	2.00
732	48.04	168.84	2.06	1.92	0.66	116.26	1.38	160.83	4.000	Yes	No	2.00
733	48.11	173.11	2.05	1.89	0.65	119.39	1.36	162.82	0.481	No	No	1.21
734	48.19	175.86	2.04	1.88	0.65	121.33	1.35	164.25	0.492	No	No	1.23
735	48.23	176.73	2.04	1.89	0.65	121.85	1.35	165.07	0.498	No	No	1.25
736	48.30	176.31	2.04	1.92	0.65	121.32	1.36	165.40	0.501	No	No	1.26
737	48.40	175.47	2.05	1.96	0.66	120.40	1.38	165.61	0.502	No	No	1.26
738	48.45	174.20	2.06	2.00	0.66	119.22	1.39	165.83	0.504	No	No	1.27
739	48.50	172.99	2.07	2.04	0.66	118.09	1.41	166.15	0.507	No	No	1.27
740	48.59	172.02	2.08	2.08	0.67	117.09	1.42	166.44	0.509	No	No	1.28
741	48.66	171.41	2.09	2.11	0.67	116.42	1.43	166.75	0.511	No	No	1.29
742	48.69	171.02	2.09	2.13	0.67	116.01	1.44	167.02	0.513	No	No	1.29
743	48.78	170.78	2.09	2.15	0.67	115.63	1.45	167.11	0.514	No	No	1.29
744	48.85	170.69	2.10	2.15	0.67	115.43	1.45	167.08	0.514	No	No	1.29
745	48.89	170.46	2.10	2.15	0.67	115.19	1.45	166.89	0.512	No	No	1.29
746	48.98	170.14	2.10	2.15	0.67	114.81	1.45	166.50	0.509	No	No	1.28
747	49.03	169.85	2.10	2.15	0.67	114.51	1.45	166.24	0.507	No	No	1.28
748	49.09	170.04	2.10	2.16	0.67	114.53	1.45	166.41	0.509	No	No	1.28
749	49.19	170.33	2.10	2.17	0.68	114.54	1.46	166.69	0.511	No	No	1.29
750	49.23	170.93	2.10	2.18	0.68	114.85	1.46	167.48	0.517	No	No	1.30
751	49.28	172.83	2.10	2.20	0.68	116.08	1.46	169.12	0.530	No	No	1.34
752	49.39	175.13	2.10	2.21	0.68	117.50	1.45	170.85	0.544	No	No	1.37
753	49.42	177.65	2.10	2.23	0.67	119.21	1.45	172.90	0.561	No	No	1.42
754	49.49	180.57	2.09	2.23	0.67	121.19	1.44	174.81	0.577	No	No	1.46
755	49.59	183.31	2.09	2.20	0.67	123.06	1.43	175.79	0.585	No	No	1.48
756	49.62	185.69	2.08	2.17	0.67	124.84	1.41	176.44	0.591	No	No	1.50
757	49.69	187.40	2.07	2.14	0.66	126.08	1.40	176.46	0.591	No	No	1.50
758	49.74	188.52	2.06	2.08	0.66	127.02	1.38	175.46	0.582	No	No	1.48
759	49.83	188.92	2.04	2.00	0.65	127.47	1.36	173.39	0.565	No	No	1.43
760	49.88	187.83	2.03	1.92	0.65	126.90	1.34	170.54	0.541	No	No	1.37
761	49.93	185.76	2.03	1.86	0.65	125.55	1.33	167.52	0.517	No	No	1.31
762	50.03	183.09	2.02	1.81	0.64	123.66	1.33	164.16	4.000	No	No	2.00
763	50.13	179.38	2.02	1.78	0.65	120.92	1.33	160.78	4.000	No	No	2.00
764	50.14	175.33	2.03	1.79	0.65	117.93	1.34	158.34	4.000	No	No	2.00
765	50.23	171.23	2.04	1.82	0.65	114.71	1.36	156.17	4.000	No	No	2.00
766	50.27	166.80	2.06	1.86	0.66	111.30	1.39	154.26	4.000	No	No	2.00
767	50.34	161.56	2.09	1.95	0.67	107.09	1.43	153.13	4.000	No	No	2.00
768	50.43	155.42	2.12	2.08	0.68	102.13	1.49	152.59	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
769	50.49	148.95	2.16	2.22	0.70	97.05	1.57	152.09	4.000	No	No	2.00
770	50.53	142.05	2.19	2.33	0.71	91.83	1.64	150.66	4.000	No	No	2.00
771	50.62	134.51	2.22	2.45	0.72	86.16	1.73	148.86	4.000	No	No	2.00
772	50.68	127.42	2.26	2.55	0.73	80.95	1.81	146.80	4.000	No	No	2.00
773	50.73	120.26	2.28	2.62	0.74	75.84	1.89	143.66	4.000	No	No	2.00
774	50.82	113.01	2.31	2.66	0.75	70.70	1.98	139.77	4.000	No	No	2.00
775	50.88	106.07	2.33	2.67	0.76	65.87	2.06	135.47	4.000	No	No	2.00
776	50.93	99.91	2.35	2.65	0.77	61.68	2.12	130.70	4.000	No	No	2.00
777	51.02	94.44	2.36	2.61	0.78	57.95	2.17	125.94	4.000	No	No	2.00
778	51.09	89.17	2.38	2.58	0.78	54.38	2.24	121.63	4.000	Yes	No	2.00
779	51.12	83.92	2.40	2.59	0.79	50.82	2.33	118.24	4.000	Yes	No	2.00
780	51.19	78.60	2.43	2.62	0.80	47.16	2.45	115.41	4.000	Yes	No	2.00
781	51.28	73.22	2.47	2.71	0.82	43.44	2.61	113.38	4.000	Yes	No	2.00
782	51.32	68.33	2.50	2.81	0.83	40.10	2.79	111.88	4.000	Yes	No	2.00
783	51.39	64.21	2.54	2.89	0.84	37.28	2.95	110.12	4.000	Yes	No	2.00
784	51.48	60.31	2.57	2.97	0.85	34.64	3.13	108.49	4.000	Yes	No	2.00
785	51.53	56.31	2.60	3.07	0.87	31.96	3.35	107.03	4.000	Yes	Yes	2.00
786	51.62	52.17	2.64	3.16	0.88	29.22	3.58	104.75	4.000	Yes	Yes	2.00
787	51.68	48.21	2.68	3.20	0.89	26.65	3.82	101.81	4.000	Yes	Yes	2.00
788	51.73	45.05	2.70	3.20	0.90	24.64	4.00	98.61	4.000	Yes	Yes	2.00
789	51.82	42.62	2.71	3.09	0.91	23.13	4.09	94.59	4.000	No	Yes	2.00
790	51.87	40.63	2.71	2.87	0.91	21.96	4.07	89.44	4.000	No	Yes	2.00
791	51.92	38.75	2.71	2.71	0.91	20.83	4.09	85.24	4.000	No	Yes	2.00
792	51.97	36.63	2.73	2.64	0.92	19.52	4.21	82.16	4.000	No	Yes	2.00
793	52.04	34.50	2.75	2.58	0.92	18.20	4.35	79.17	4.000	No	Yes	2.00
794	52.12	32.86	2.76	2.49	0.93	17.19	4.44	76.28	4.000	No	Yes	2.00
795	52.18	31.94	2.76	2.40	0.93	16.63	4.46	74.17	4.000	No	Yes	2.00
796	52.23	31.17	2.76	2.32	0.93	16.17	4.47	72.25	4.000	No	Yes	2.00
797	52.31	30.59	2.76	2.24	0.93	15.81	4.47	70.63	4.000	No	Yes	2.00
798	52.37	30.00	2.77	2.20	0.93	15.45	4.50	69.47	4.000	No	Yes	2.00
799	52.44	29.15	2.78	2.19	0.93	14.92	4.59	68.42	4.000	No	Yes	2.00
800	52.53	28.21	2.79	2.17	0.94	14.32	4.69	67.11	4.000	No	Yes	2.00
801	52.57	27.07	2.81	2.16	0.94	13.61	4.83	65.80	4.000	No	Yes	2.00
802	52.64	25.80	2.83	2.15	0.95	12.83	5.02	64.33	4.000	No	Yes	2.00
803	52.72	24.50	2.85	2.14	0.96	12.02	5.22	62.73	4.000	No	Yes	2.00
804	52.78	23.17	2.87	2.13	0.97	11.20	5.44	61.00	4.000	No	Yes	2.00
805	52.83	21.95	2.89	2.07	0.98	10.48	5.61	58.82	4.000	No	Yes	2.00
806	52.93	20.80	2.91	2.00	0.98	9.79	5.79	56.64	4.000	No	Yes	2.00
807	52.96	19.98	2.92	1.92	0.99	9.31	5.88	54.75	4.000	No	Yes	2.00
808	53.04	19.46	2.92	1.86	0.99	9.00	5.93	53.36	4.000	No	Yes	2.00
809	53.12	19.06	2.93	1.80	0.99	8.76	5.96	52.22	4.000	No	Yes	2.00
810	53.17	18.87	2.92	1.74	0.99	8.66	5.93	51.39	4.000	No	Yes	2.00
811	53.22	18.81	2.92	1.70	0.99	8.63	5.89	50.85	4.000	No	Yes	2.00
812	53.29	18.81	2.91	1.65	0.99	8.63	5.83	50.31	4.000	No	Yes	2.00
813	53.37	18.84	2.91	1.62	0.98	8.64	5.78	49.99	4.000	No	Yes	2.00
814	53.42	18.86	2.91	1.65	0.98	8.64	5.82	50.29	4.000	No	Yes	2.00
815	53.49	18.87	2.91	1.66	0.99	8.63	5.84	50.42	4.000	No	Yes	2.00
816	53.58	18.87	2.91	1.65	0.99	8.62	5.83	50.25	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
817	53.63	18.86	2.91	1.62	0.98	8.62	5.79	49.93	4.000	No	Yes	2.00
818	53.68	18.86	2.91	1.59	0.98	8.62	5.76	49.62	4.000	No	Yes	2.00
819	53.78	18.86	2.90	1.56	0.98	8.61	5.71	49.21	4.000	No	Yes	2.00
820	53.84	18.85	2.90	1.53	0.98	8.61	5.68	48.88	4.000	No	Yes	2.00
821	53.88	18.83	2.90	1.51	0.98	8.59	5.66	48.64	4.000	No	Yes	2.00
822	53.94	18.84	2.89	1.49	0.98	8.60	5.63	48.39	4.000	No	Yes	2.00
823	54.03	18.88	2.89	1.48	0.98	8.61	5.61	48.30	4.000	No	Yes	2.00
824	54.08	18.95	2.89	1.47	0.98	8.65	5.58	48.29	4.000	No	Yes	2.00
825	54.16	19.04	2.89	1.48	0.98	8.69	5.59	48.52	4.000	No	Yes	2.00
826	54.20	19.16	2.89	1.49	0.98	8.75	5.57	48.76	4.000	No	Yes	2.00
827	54.28	19.40	2.88	1.49	0.97	8.88	5.51	48.91	4.000	No	Yes	2.00
828	54.35	19.73	2.87	1.47	0.97	9.07	5.41	49.08	4.000	No	Yes	2.00
829	54.43	20.10	2.86	1.45	0.96	9.29	5.30	49.24	4.000	No	Yes	2.00
830	54.48	20.43	2.85	1.42	0.96	9.48	5.19	49.24	4.000	No	Yes	2.00
831	54.55	20.63	2.84	1.40	0.96	9.61	5.12	49.16	4.000	No	Yes	2.00
832	54.63	20.78	2.83	1.38	0.95	9.69	5.05	48.99	4.000	No	Yes	2.00
833	54.67	20.84	2.83	1.36	0.95	9.73	5.02	48.82	4.000	No	Yes	2.00
834	54.74	20.86	2.82	1.32	0.95	9.74	4.96	48.33	4.000	No	Yes	2.00
835	54.82	20.83	2.82	1.29	0.95	9.72	4.92	47.83	4.000	No	Yes	2.00
836	54.87	20.69	2.82	1.26	0.95	9.64	4.92	47.41	4.000	No	Yes	2.00
837	54.92	20.46	2.82	1.26	0.95	9.49	4.97	47.15	4.000	No	Yes	2.00
838	55.02	20.18	2.83	1.27	0.95	9.31	5.05	46.96	4.000	No	Yes	2.00
839	55.06	19.93	2.84	1.32	0.96	9.14	5.17	47.27	4.000	No	Yes	2.00
840	55.14	19.85	2.86	1.37	0.96	9.06	5.28	47.81	4.000	No	Yes	2.00
841	55.22	19.85	2.87	1.44	0.97	9.03	5.38	48.59	4.000	No	Yes	2.00
842	55.27	20.07	2.87	1.50	0.97	9.13	5.43	49.60	4.000	No	Yes	2.00
843	55.37	20.38	2.88	1.59	0.97	9.28	5.48	50.87	4.000	No	Yes	2.00
844	55.42	20.73	2.88	1.67	0.97	9.45	5.52	52.18	4.000	No	Yes	2.00
845	55.47	21.01	2.89	1.75	0.98	9.58	5.57	53.37	4.000	No	Yes	2.00
846	55.53	21.18	2.89	1.81	0.98	9.65	5.62	54.26	4.000	No	Yes	2.00
847	55.58	21.32	2.90	1.87	0.98	9.71	5.66	54.99	4.000	No	Yes	2.00
848	55.67	21.43	2.90	1.89	0.98	9.75	5.67	55.30	4.000	No	Yes	2.00
849	55.72	21.47	2.90	1.89	0.98	9.77	5.67	55.36	4.000	No	Yes	2.00
850	55.81	21.47	2.90	1.87	0.98	9.76	5.65	55.13	4.000	No	Yes	2.00
851	55.86	21.33	2.89	1.84	0.98	9.68	5.64	54.58	4.000	No	Yes	2.00
852	55.92	21.20	2.90	1.83	0.98	9.60	5.66	54.29	4.000	No	Yes	2.00
853	56.01	21.13	2.90	1.84	0.98	9.54	5.69	54.26	4.000	No	Yes	2.00
854	56.05	21.34	2.90	1.86	0.98	9.65	5.67	54.73	4.000	No	Yes	2.00
855	56.11	21.83	2.90	1.93	0.98	9.91	5.66	56.06	4.000	No	Yes	2.00
856	56.21	22.16	2.91	2.07	0.98	10.04	5.77	57.94	4.000	No	Yes	2.00
857	56.26	22.93	2.91	2.21	0.98	10.44	5.78	60.32	4.000	No	Yes	2.00
858	56.32	24.21	2.90	2.34	0.98	11.14	5.67	63.19	4.000	No	Yes	2.00
859	56.41	25.83	2.88	2.43	0.97	12.03	5.50	66.12	4.000	No	Yes	2.00
860	56.46	27.60	2.86	2.50	0.96	13.03	5.29	68.96	4.000	No	Yes	2.00
861	56.50	29.45	2.83	2.51	0.95	14.10	5.05	71.15	4.000	No	Yes	2.00
862	56.59	31.25	2.81	2.53	0.95	15.12	4.85	73.31	4.000	No	Yes	2.00
863	56.65	32.82	2.79	2.58	0.94	16.01	4.71	75.45	4.000	No	Yes	2.00
864	56.70	34.20	2.78	2.67	0.94	16.78	4.65	78.08	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
865	56.78	36.90	2.75	2.67	0.92	18.34	4.40	80.75	4.000	No	Yes	2.00
866	56.85	39.96	2.72	2.66	0.91	20.15	4.14	83.47	4.000	No	Yes	2.00
867	56.89	43.42	2.68	2.65	0.90	22.21	3.89	86.30	4.000	No	Yes	2.00
868	56.98	46.67	2.66	2.66	0.89	24.13	3.70	89.17	4.000	No	Yes	2.00
869	57.04	49.64	2.64	2.70	0.88	25.88	3.57	92.28	4.000	No	Yes	2.00
870	57.09	52.24	2.63	2.79	0.88	27.37	3.50	95.85	4.000	No	Yes	2.00
871	57.16	54.64	2.62	2.87	0.87	28.73	3.45	99.15	4.000	No	Yes	2.00
872	57.24	57.27	2.61	2.92	0.87	30.26	3.37	101.95	4.000	No	Yes	2.00
873	57.29	60.78	2.58	2.83	0.86	32.45	3.18	103.21	4.000	No	No	2.00
874	57.37	63.44	2.55	2.76	0.85	34.10	3.04	103.78	4.000	No	No	2.00
875	57.42	65.25	2.53	2.70	0.84	35.24	2.95	103.95	4.000	No	No	2.00
876	57.49	65.85	2.53	2.67	0.84	35.59	2.92	103.82	4.000	No	No	2.00
877	57.59	66.05	2.53	2.65	0.84	35.68	2.90	103.46	4.000	No	No	2.00
878	57.64	65.55	2.53	2.63	0.84	35.37	2.90	102.67	4.000	No	No	2.00
879	57.69	64.18	2.53	2.60	0.84	34.52	2.93	101.10	4.000	No	No	2.00
880	57.77	62.46	2.54	2.54	0.84	33.48	2.95	98.82	4.000	No	No	2.00
881	57.82	59.62	2.55	2.52	0.85	31.73	3.03	96.27	4.000	No	No	2.00
882	57.89	55.11	2.59	2.57	0.86	28.91	3.25	93.85	4.000	No	No	2.00
883	57.97	50.06	2.64	2.66	0.88	25.76	3.55	91.40	4.000	No	Yes	2.00
884	58.03	44.69	2.69	2.76	0.90	22.48	3.94	88.53	4.000	No	Yes	2.00
885	58.09	39.45	2.75	2.84	0.92	19.34	4.38	84.77	4.000	No	Yes	2.00
886	58.17	34.44	2.81	2.91	0.95	16.39	4.91	80.43	4.000	No	Yes	2.00
887	58.21	30.20	2.87	2.93	0.97	13.95	5.43	75.82	4.000	No	Yes	2.00
888	58.28	27.04	2.92	2.88	0.99	12.17	5.86	71.37	4.000	No	Yes	2.00
889	58.37	24.54	2.96	2.90	1.00	10.77	6.33	68.16	4.000	No	Yes	2.00
890	58.40	22.95	2.99	2.92	1.00	9.96	6.65	66.27	4.000	No	Yes	2.00
891	58.48	22.15	3.02	3.07	1.00	9.54	6.96	66.39	4.000	No	Yes	2.00
892	58.53	22.64	3.02	3.16	1.00	9.78	6.94	67.91	4.000	No	Yes	2.00
893	58.63	24.67	2.97	3.05	1.00	10.80	6.46	69.73	4.000	No	Yes	2.00
894	58.67	27.06	2.93	2.95	0.99	12.07	5.95	71.85	4.000	No	Yes	2.00
895	58.73	29.10	2.89	2.89	0.98	13.23	5.58	73.85	4.000	No	Yes	2.00
896	58.82	30.69	2.87	2.89	0.97	14.10	5.37	75.70	4.000	No	Yes	2.00
897	58.89	31.56	2.86	2.92	0.96	14.56	5.29	77.01	4.000	No	Yes	2.00
898	58.93	31.85	2.85	2.92	0.96	14.72	5.25	77.30	4.000	No	Yes	2.00
899	59.00	31.94	2.85	2.88	0.96	14.76	5.21	76.96	4.000	No	Yes	2.00
900	59.06	31.98	2.83	2.73	0.96	14.82	5.08	75.29	4.000	No	Yes	2.00
901	59.13	30.97	2.83	2.57	0.95	14.30	5.05	72.23	4.000	No	Yes	2.00
902	59.22	28.79	2.86	2.52	0.96	13.06	5.30	69.22	4.000	No	Yes	2.00
903	59.28	26.42	2.90	2.51	0.98	11.72	5.66	66.38	4.000	No	Yes	2.00
904	59.33	24.42	2.93	2.49	0.99	10.60	6.00	63.61	4.000	No	Yes	2.00
905	59.41	23.06	2.95	2.40	1.00	9.86	6.19	61.04	4.000	No	Yes	2.00
906	59.47	22.47	2.95	2.30	1.00	9.55	6.20	59.23	4.000	No	Yes	2.00
907	59.52	22.50	2.94	2.18	0.99	9.59	6.06	58.08	4.000	No	Yes	2.00
908	59.61	22.85	2.91	2.05	0.99	9.81	5.83	57.18	4.000	No	Yes	2.00
909	59.67	23.26	2.90	1.97	0.98	10.05	5.66	56.84	4.000	No	Yes	2.00
910	59.72	23.81	2.88	1.97	0.97	10.35	5.55	57.41	4.000	No	Yes	2.00
911	59.78	24.44	2.87	1.99	0.97	10.69	5.46	58.31	4.000	No	Yes	2.00
912	59.87	25.08	2.87	2.00	0.97	11.02	5.36	59.13	4.000	Yes	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
913	59.92	25.83	2.82	1.76	0.95	11.52	4.95	57.00	4.000	Yes	Yes	2.00
914	60.00	26.38	2.78	1.54	0.93	11.92	4.59	54.71	4.000	Yes	Yes	2.00
915	60.05	26.95	2.73	1.33	0.92	12.34	4.23	52.22	4.000	Yes	Yes	2.00
916	60.11	27.25	2.69	1.13	0.90	12.61	3.92	49.42	4.000	Yes	Yes	2.00
917	60.21	27.38	2.64	0.93	0.88	12.81	3.61	46.28	4.000	Yes	Yes	2.00
918	60.25	27.51	2.59	0.72	0.86	13.05	3.26	42.60	4.000	Yes	No	2.00
919	60.31	27.68	2.51	0.49	0.83	13.38	2.84	37.95	4.000	Yes	No	2.00
920	60.40	27.58	2.41	0.24	0.79	13.65	2.36	32.18	4.000	Yes	No	2.00
921	60.43	27.43	N/A	0.00	1.00	-1.00	1.00	N/A	4.000	No	No	2.00
922	60.51	27.37	N/A	0.00	1.00	-1.00	1.00	N/A	4.000	No	No	2.00

Abbreviations

Depth: Depth from free surface, at which CPT was performed (ft)
q_t: Total cone resistance
I_c: Soil behavior type index
Fr: Normalized friction ratio (%)
n: Stress exponent
Q_{tn}: Normalized cone resistance
K_c: Cone resistance correction factor due to fines
$Q_{tn,cs}$: Normalized and adjusted cone resistance
$CRR_{7.5}$: Cyclic resistance ratio for M_w=7.5
FS: Factor of safety against soil liquefaction

:: Liquefaction Potential Index calculation data ::

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
0.10	2.00	0.00	0.00	0.02	0.00	0.15	2.00	0.00	0.00	0.02	0.00
0.23	2.00	0.00	0.00	0.02	0.00	0.30	2.00	0.00	0.00	0.02	0.00
0.34	2.00	0.00	0.00	0.01	0.00	0.39	2.00	0.00	0.00	0.02	0.00
0.50	2.00	0.00	0.00	0.03	0.00	0.53	2.00	0.00	0.00	0.01	0.00
0.60	2.00	0.00	0.00	0.02	0.00	0.69	2.00	0.00	0.00	0.03	0.00
0.72	2.00	0.00	0.00	0.01	0.00	0.80	2.00	0.00	0.00	0.02	0.00
0.87	2.00	0.00	0.00	0.02	0.00	0.92	2.00	0.00	0.00	0.02	0.00
1.00	2.00	0.00	0.00	0.02	0.00	1.08	2.00	0.00	0.00	0.02	0.00
1.12	2.00	0.00	0.00	0.01	0.00	1.20	2.00	0.00	0.00	0.02	0.00
1.30	2.00	0.00	0.00	0.03	0.00	1.34	2.00	0.00	0.00	0.01	0.00
1.40	2.00	0.00	0.00	0.02	0.00	1.49	2.00	0.00	0.00	0.03	0.00
1.54	2.00	0.00	0.00	0.02	0.00	1.59	2.00	0.00	0.00	0.02	0.00
1.68	2.00	0.00	0.00	0.03	0.00	1.74	2.00	0.00	0.00	0.02	0.00
1.79	2.00	0.00	0.00	0.02	0.00	1.87	2.00	0.00	0.00	0.02	0.00
1.94	2.00	0.00	0.00	0.02	0.00	1.98	2.00	0.00	0.00	0.01	0.00
2.04	2.00	0.00	0.00	0.02	0.00	2.13	2.00	0.00	0.00	0.03	0.00
2.17	2.00	0.00	0.00	0.01	0.00	2.24	2.00	0.00	0.00	0.02	0.00
2.33	2.00	0.00	0.00	0.03	0.00	2.36	2.00	0.00	0.00	0.01	0.00
2.43	2.00	0.00	0.00	0.02	0.00	2.52	2.00	0.00	0.00	0.03	0.00
2.56	2.00	0.00	0.00	0.01	0.00	2.64	2.00	0.00	0.00	0.02	0.00
2.74	2.00	0.00	0.00	0.03	0.00	2.78	2.00	0.00	0.00	0.01	0.00
2.83	2.00	0.00	0.00	0.02	0.00	2.90	2.00	0.00	0.00	0.02	0.00
2.98	2.00	0.00	0.00	0.02	0.00	3.03	2.00	0.00	0.00	0.02	0.00
3.10	2.00	0.00	0.00	0.02	0.00	3.18	2.00	0.00	0.00	0.02	0.00
3.23	2.00	0.00	0.00	0.02	0.00	3.29	2.00	0.00	0.00	0.02	0.00
3.38	2.00	0.00	0.00	0.03	0.00	3.42	2.00	0.00	0.00	0.01	0.00
3.51	2.00	0.00	0.00	0.03	0.00	3.58	2.00	0.00	0.00	0.02	0.00
3.62	2.00	0.00	0.00	0.01	0.00	3.69	2.00	0.00	0.00	0.02	0.00
3.77	2.00	0.00	0.00	0.02	0.00	3.82	2.00	0.00	0.00	0.02	0.00
3.89	2.00	0.00	0.00	0.02	0.00	3.97	2.00	0.00	0.00	0.02	0.00
4.03	2.00	0.00	0.00	0.02	0.00	4.10	2.00	0.00	0.00	0.02	0.00
4.15	2.00	0.00	0.00	0.02	0.00	4.24	2.00	0.00	0.00	0.03	0.00
4.29	2.00	0.00	0.00	0.02	0.00	4.35	2.00	0.00	0.00	0.02	0.00
4.44	2.00	0.00	0.00	0.03	0.00	4.48	2.00	0.00	0.00	0.01	0.00
4.54	2.00	0.00	0.00	0.02	0.00	4.61	2.00	0.00	0.00	0.02	0.00
4.69	2.00	0.00	0.00	0.02	0.00	4.74	2.00	0.00	0.00	0.02	0.00
4.82	2.00	0.00	0.00	0.02	0.00	4.86	2.00	0.00	0.00	0.01	0.00
4.94	2.00	0.00	0.00	0.02	0.00	5.02	2.00	0.00	0.00	0.02	0.00
5.09	2.00	0.00	0.00	0.02	0.00	5.13	2.00	0.00	0.00	0.01	0.00
5.23	2.00	0.00	0.00	0.03	0.00	5.28	2.00	0.00	0.00	0.02	0.00
5.33	2.00	0.00	0.00	0.02	0.00	5.39	2.00	0.00	0.00	0.02	0.00
5.48	2.00	0.00	0.00	0.03	0.00	5.52	2.00	0.00	0.00	0.01	0.00
5.58	2.00	0.00	0.00	0.02	0.00	5.67	2.00	0.00	0.00	0.03	0.00
5.73	2.00	0.00	0.00	0.02	0.00	5.78	2.00	0.00	0.00	0.02	0.00
5.88	2.00	0.00	0.00	0.03	0.00	5.92	2.00	0.00	0.00	0.01	0.00
5.97	2.00	0.00	0.00	0.02	0.00	6.08	2.00	0.00	0.00	0.03	0.00
6.11	2.00	0.00	0.00	0.01	0.00	6.18	2.00	0.00	0.00	0.02	0.00
6.27	2.00	0.00	0.00	0.03	0.00	6.33	2.00	0.00	0.00	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
6.38	2.00	0.00	0.00	0.02	0.00	6.44	2.00	0.00	0.00	0.02	0.00
6.50	2.00	0.00	0.00	0.02	0.00	6.57	2.00	0.00	0.00	0.02	0.00
6.67	2.00	0.00	0.00	0.03	0.00	6.72	2.00	0.00	0.00	0.02	0.00
6.76	2.00	0.00	0.00	0.01	0.00	6.83	2.00	0.00	0.00	0.02	0.00
6.92	2.00	0.00	0.00	0.03	0.00	6.97	2.00	0.00	0.00	0.02	0.00
7.04	2.00	0.00	0.00	0.02	0.00	7.12	2.00	0.00	0.00	0.02	0.00
7.16	2.00	0.00	0.00	0.01	0.00	7.25	2.00	0.00	0.00	0.03	0.00
7.32	2.00	0.00	0.00	0.02	0.00	7.37	2.00	0.00	0.00	0.02	0.00
7.43	2.00	0.00	0.00	0.02	0.00	7.52	2.00	0.00	0.00	0.03	0.00
7.56	2.00	0.00	0.00	0.01	0.00	7.63	2.00	0.00	0.00	0.02	0.00
7.71	2.00	0.00	0.00	0.02	0.00	7.75	2.00	0.00	0.00	0.01	0.00
7.83	2.00	0.00	0.00	0.02	0.00	7.88	2.00	0.00	0.00	0.02	0.00
7.97	2.00	0.00	0.00	0.03	0.00	8.01	2.00	0.00	0.00	0.01	0.00
8.08	2.00	0.00	0.00	0.02	0.00	8.18	2.00	0.00	0.00	0.03	0.00
8.22	2.00	0.00	0.00	0.01	0.00	8.28	2.00	0.00	0.00	0.02	0.00
8.35	2.00	0.00	0.00	0.02	0.00	8.43	2.00	0.00	0.00	0.02	0.00
8.48	2.00	0.00	0.00	0.02	0.00	8.56	2.00	0.00	0.00	0.02	0.00
8.63	2.00	0.00	0.00	0.02	0.00	8.68	2.00	0.00	0.00	0.02	0.00
8.76	2.00	0.00	0.00	0.02	0.00	8.80	2.00	0.00	0.00	0.01	0.00
8.88	2.00	0.00	0.00	0.02	0.00	8.94	2.00	0.00	0.00	0.02	0.00
8.99	2.00	0.00	0.00	0.02	0.00	9.07	2.00	0.00	0.00	0.02	0.00
9.14	2.00	0.00	0.00	0.02	0.00	9.22	2.00	0.00	0.00	0.02	0.00
9.27	2.00	0.00	0.00	0.02	0.00	9.37	2.00	0.00	0.00	0.03	0.00
9.42	2.00	0.00	0.00	0.02	0.00	9.47	2.00	0.00	0.00	0.02	0.00
9.52	2.00	0.00	0.00	0.02	0.00	9.62	2.00	0.00	0.00	0.03	0.00
9.67	2.00	0.00	0.00	0.02	0.00	9.73	2.00	0.00	0.00	0.02	0.00
9.82	2.00	0.00	0.00	0.03	0.00	9.86	2.00	0.00	0.00	0.01	0.00
9.92	2.00	0.00	0.00	0.02	0.00	10.02	2.00	0.00	0.00	0.03	0.00
10.06	2.00	0.00	0.00	0.01	0.00	10.12	2.00	0.00	0.00	0.02	0.00
10.21	2.00	0.00	0.00	0.03	0.00	10.25	2.00	0.00	0.00	0.01	0.00
10.31	2.00	0.00	0.00	0.02	0.00	10.41	2.00	0.00	0.00	0.03	0.00
10.45	2.00	0.00	0.00	0.01	0.00	10.52	2.00	0.00	0.00	0.02	0.00
10.61	2.00	0.00	0.00	0.03	0.00	10.64	2.00	0.00	0.00	0.01	0.00
10.71	2.00	0.00	0.00	0.02	0.00	10.81	2.00	0.00	0.00	0.03	0.00
10.85	2.00	0.00	0.00	0.01	0.00	10.91	2.00	0.00	0.00	0.02	0.00
10.96	2.00	0.00	0.00	0.02	0.00	11.03	2.00	0.00	0.00	0.02	0.00
11.10	2.00	0.00	0.00	0.02	0.00	11.20	2.00	0.00	0.00	0.03	0.00
11.24	2.00	0.00	0.00	0.01	0.00	11.30	2.00	0.00	0.00	0.02	0.00
11.36	2.00	0.00	0.00	0.02	0.00	11.43	2.00	0.00	0.00	0.02	0.00
11.50	2.00	0.00	0.00	0.02	0.00	11.58	2.00	0.00	0.00	0.02	0.00
11.63	2.00	0.00	0.00	0.02	0.00	11.70	2.00	0.00	0.00	0.02	0.00
11.79	2.00	0.00	0.00	0.03	0.00	11.84	2.00	0.00	0.00	0.02	0.00
11.90	2.00	0.00	0.00	0.02	0.00	11.98	2.00	0.00	0.00	0.02	0.00
12.02	2.00	0.00	0.00	0.01	0.00	12.09	2.00	0.00	0.00	0.02	0.00
12.14	2.00	0.00	0.00	0.02	0.00	12.21	2.00	0.00	0.00	0.02	0.00
12.29	2.00	0.00	0.00	0.02	0.00	12.34	2.00	0.00	0.00	0.02	0.00
12.44	2.00	0.00	0.00	0.03	0.00	12.49	2.00	0.00	0.00	0.02	0.00
12.57	2.00	0.00	0.00	0.02	0.00	12.64	2.00	0.00	0.00	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
12.68	2.00	0.00	0.00	0.01	0.00	12.73	2.00	0.00	0.00	0.02	0.00
12.84	2.00	0.00	0.00	0.03	0.00	12.89	2.00	0.00	0.00	0.02	0.00
12.98	2.00	0.00	0.00	0.03	0.00	13.00	2.00	0.00	0.00	0.01	0.00
13.08	2.00	0.00	0.00	0.02	0.00	13.14	2.00	0.00	0.00	0.02	0.00
13.23	2.00	0.00	0.00	0.03	0.00	13.27	2.00	0.00	0.00	0.01	0.00
13.34	2.00	0.00	0.00	0.02	0.00	13.43	2.00	0.00	0.00	0.03	0.00
13.47	2.00	0.00	0.00	0.01	0.00	13.54	2.00	0.00	0.00	0.02	0.00
13.63	2.00	0.00	0.00	0.03	0.00	13.67	2.00	0.00	0.00	0.01	0.00
13.72	2.00	0.00	0.00	0.02	0.00	13.83	2.00	0.00	0.00	0.03	0.00
13.88	2.00	0.00	0.00	0.02	0.00	13.94	2.00	0.00	0.00	0.02	0.00
13.98	2.00	0.00	0.00	0.01	0.00	14.06	2.00	0.00	0.00	0.02	0.00
14.14	2.00	0.00	0.00	0.02	0.00	14.18	2.00	0.00	0.00	0.01	0.00
14.26	2.00	0.00	0.00	0.02	0.00	14.33	2.00	0.00	0.00	0.02	0.00
14.37	2.00	0.00	0.00	0.01	0.00	14.45	2.00	0.00	0.00	0.02	0.00
14.54	2.00	0.00	0.00	0.03	0.00	14.61	2.00	0.00	0.00	0.02	0.00
14.65	2.00	0.00	0.00	0.01	0.00	14.74	2.00	0.00	0.00	0.03	0.00
14.80	2.00	0.00	0.00	0.02	0.00	14.85	2.00	0.00	0.00	0.02	0.00
14.90	2.00	0.00	0.00	0.02	0.00	15.00	2.00	0.00	0.00	0.03	0.00
15.05	2.00	0.00	0.00	0.02	0.00	15.10	2.00	0.00	0.00	0.02	0.00
15.17	2.00	0.00	0.00	0.02	0.00	15.25	2.00	0.00	0.00	0.02	0.00
15.30	2.00	0.00	0.00	0.02	0.00	15.36	2.00	0.00	0.00	0.02	0.00
15.45	2.00	0.00	0.00	0.03	0.00	15.49	2.00	0.00	0.00	0.01	0.00
15.57	2.00	0.00	0.00	0.02	0.00	15.64	2.00	0.00	0.00	0.02	0.00
15.69	2.00	0.00	0.00	0.02	0.00	15.77	2.00	0.00	0.00	0.02	0.00
15.85	2.00	0.00	0.00	0.02	0.00	15.89	2.00	0.00	0.00	0.01	0.00
15.99	2.00	0.00	0.00	0.03	0.00	16.05	2.00	0.00	0.00	0.02	0.00
16.09	2.00	0.00	0.00	0.01	0.00	16.16	2.00	0.00	0.00	0.02	0.00
16.24	2.00	0.00	0.00	0.02	0.00	16.30	2.00	0.00	0.00	0.02	0.00
16.34	2.00	0.00	0.00	0.01	0.00	16.44	2.00	0.00	0.00	0.03	0.00
16.48	2.00	0.00	0.00	0.01	0.00	16.54	2.00	0.00	0.00	0.02	0.00
16.63	2.00	0.00	0.00	0.03	0.00	16.69	2.00	0.00	0.00	0.02	0.00
16.74	2.00	0.00	0.00	0.02	0.00	16.82	2.00	0.00	0.00	0.02	0.00
16.90	2.00	0.00	0.00	0.02	0.00	16.94	2.00	0.00	0.00	0.01	0.00
17.03	2.00	0.00	0.00	0.03	0.00	17.07	2.00	0.00	0.00	0.01	0.00
17.13	2.00	0.00	0.00	0.02	0.00	17.21	2.00	0.00	0.00	0.02	0.00
17.26	2.00	0.00	0.00	0.02	0.00	17.33	2.00	0.00	0.00	0.02	0.00
17.41	2.00	0.00	0.00	0.02	0.00	17.48	2.00	0.00	0.00	0.02	0.00
17.53	2.00	0.00	0.00	0.02	0.00	17.61	2.00	0.00	0.00	0.02	0.00
17.67	2.00	0.00	0.00	0.02	0.00	17.72	2.00	0.00	0.00	0.02	0.00
17.82	2.00	0.00	0.00	0.03	0.00	17.88	2.00	0.00	0.00	0.02	0.00
17.92	2.00	0.00	0.00	0.01	0.00	18.02	2.00	0.00	0.00	0.03	0.00
18.07	2.00	0.00	0.00	0.02	0.00	18.14	2.00	0.00	0.00	0.02	0.00
18.20	2.00	0.00	0.00	0.02	0.00	18.27	2.00	0.00	0.00	0.02	0.00
18.32	2.00	0.00	0.00	0.02	0.00	18.38	2.00	0.00	0.00	0.02	0.00
18.47	2.00	0.00	0.00	0.03	0.00	18.51	2.00	0.00	0.00	0.01	0.00
18.57	2.00	0.00	0.00	0.02	0.00	18.67	2.00	0.00	0.00	0.03	0.00
18.71	2.00	0.00	0.00	0.01	0.00	18.81	2.00	0.00	0.00	0.03	0.00
18.86	2.00	0.00	0.00	0.02	0.00	18.91	2.00	0.00	0.00	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
18.97	2.00	0.00	0.00	0.02	0.00	19.06	2.00	0.00	0.00	0.03	0.00
19.11	2.00	0.00	0.00	0.02	0.00	19.21	2.00	0.00	0.00	0.03	0.00
19.27	2.00	0.00	0.00	0.02	0.00	19.31	2.00	0.00	0.00	0.01	0.00
19.41	2.00	0.00	0.00	0.03	0.00	19.46	2.00	0.00	0.00	0.02	0.00
19.51	2.00	0.00	0.00	0.02	0.00	19.56	2.00	0.00	0.00	0.02	0.00
19.63	2.00	0.00	0.00	0.02	0.00	19.71	2.00	0.00	0.00	0.02	0.00
19.80	2.00	0.00	0.00	0.03	0.00	19.82	2.00	0.00	0.00	0.01	0.00
19.91	2.00	0.00	0.00	0.03	0.00	19.95	2.00	0.00	0.00	0.01	0.00
20.02	2.00	0.00	0.00	0.02	0.00	20.11	2.00	0.00	0.00	0.03	0.00
20.15	2.00	0.00	0.00	0.01	0.00	20.24	2.00	0.00	0.00	0.03	0.00
20.29	2.00	0.00	0.00	0.02	0.00	20.36	0.59	0.00	0.00	0.02	0.06
20.41	0.61	0.00	0.00	0.02	0.04	20.48	0.62	0.00	0.00	0.02	0.06
20.56	0.65	0.00	0.00	0.02	0.06	20.66	0.68	0.00	0.00	0.03	0.07
20.71	2.00	0.00	0.00	0.02	0.00	20.74	2.00	0.00	0.00	0.01	0.00
20.82	2.00	0.00	0.00	0.02	0.00	20.91	2.00	0.00	0.00	0.03	0.00
20.95	2.00	0.00	0.00	0.01	0.00	21.03	2.00	0.00	0.00	0.02	0.00
21.11	2.00	0.00	0.00	0.02	0.00	21.15	2.00	0.00	0.00	0.01	0.00
21.22	2.00	0.00	0.00	0.02	0.00	21.26	2.00	0.00	0.00	0.01	0.00
21.34	2.00	0.00	0.00	0.02	0.00	21.41	2.00	0.00	0.00	0.02	0.00
21.48	2.00	0.00	0.00	0.02	0.00	21.52	2.00	0.00	0.00	0.01	0.00
21.61	2.00	0.00	0.00	0.03	0.00	21.66	2.00	0.00	0.00	0.02	0.00
21.76	2.00	0.00	0.00	0.03	0.00	21.81	2.00	0.00	0.00	0.02	0.00
21.85	2.00	0.00	0.00	0.01	0.00	21.92	2.00	0.00	0.00	0.02	0.00
22.01	2.00	0.00	0.00	0.03	0.00	22.09	0.58	0.00	0.00	0.02	0.07
22.12	0.60	0.00	0.00	0.01	0.02	22.20	0.62	0.00	0.00	0.02	0.06
22.29	0.63	0.00	0.00	0.03	0.07	22.31	0.65	0.00	0.00	0.01	0.01
22.40	0.67	0.00	0.00	0.03	0.06	22.45	0.69	0.00	0.00	0.02	0.03
22.51	0.70	0.00	0.00	0.02	0.04	22.60	0.71	0.00	0.00	0.03	0.05
22.64	0.70	0.00	0.00	0.01	0.02	22.75	0.68	0.00	0.00	0.03	0.07
22.80	0.67	0.00	0.00	0.02	0.03	22.85	0.66	0.00	0.00	0.02	0.03
22.91	0.64	0.00	0.00	0.02	0.04	22.99	0.64	0.00	0.00	0.02	0.06
23.08	0.64	0.00	0.00	0.03	0.06	23.10	0.64	0.00	0.00	0.01	0.01
23.18	2.00	0.00	0.00	0.02	0.00	23.26	2.00	0.00	0.00	0.02	0.00
23.30	2.00	0.00	0.00	0.01	0.00	23.37	2.00	0.00	0.00	0.02	0.00
23.46	2.00	0.00	0.00	0.03	0.00	23.51	2.00	0.00	0.00	0.02	0.00
23.56	2.00	0.00	0.00	0.02	0.00	23.63	2.00	0.00	0.00	0.02	0.00
23.72	2.00	0.00	0.00	0.03	0.00	23.79	2.00	0.00	0.00	0.02	0.00
23.87	2.00	0.00	0.00	0.02	0.00	23.91	2.00	0.00	0.00	0.01	0.00
23.96	2.00	0.00	0.00	0.02	0.00	24.02	2.00	0.00	0.00	0.02	0.00
24.11	2.00	0.00	0.00	0.03	0.00	24.20	2.00	0.00	0.00	0.03	0.00
24.22	2.00	0.00	0.00	0.01	0.00	24.31	2.00	0.00	0.00	0.03	0.00
24.39	2.00	0.00	0.00	0.02	0.00	24.42	2.00	0.00	0.00	0.01	0.00
24.51	2.00	0.00	0.00	0.03	0.00	24.55	2.00	0.00	0.00	0.01	0.00
24.63	2.00	0.00	0.00	0.02	0.00	24.71	2.00	0.00	0.00	0.02	0.00
24.75	2.00	0.00	0.00	0.01	0.00	24.81	2.00	0.00	0.00	0.02	0.00
24.90	2.00	0.00	0.00	0.03	0.00	24.94	2.00	0.00	0.00	0.01	0.00
25.01	2.00	0.00	0.00	0.02	0.00	25.07	2.00	0.00	0.00	0.02	0.00
25.15	2.00	0.00	0.00	0.02	0.00	25.20	2.00	0.00	0.00	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
25.28	2.00	0.00	0.00	0.02	0.00	25.35	2.00	0.00	0.00	0.02	0.00
25.40	2.00	0.00	0.00	0.02	0.00	25.48	2.00	0.00	0.00	0.02	0.00
25.55	2.00	0.00	0.00	0.02	0.00	25.60	2.00	0.00	0.00	0.02	0.00
25.67	2.00	0.00	0.00	0.02	0.00	25.75	2.00	0.00	0.00	0.02	0.00
25.79	2.00	0.00	0.00	0.01	0.00	25.90	2.00	0.00	0.00	0.03	0.00
25.95	2.00	0.00	0.00	0.02	0.00	26.01	2.00	0.00	0.00	0.02	0.00
26.09	2.00	0.00	0.00	0.02	0.00	26.13	2.00	0.00	0.00	0.01	0.00
26.19	2.00	0.00	0.00	0.02	0.00	26.27	2.00	0.00	0.00	0.02	0.00
26.34	2.00	0.00	0.00	0.02	0.00	26.39	2.00	0.00	0.00	0.02	0.00
26.47	2.00	0.00	0.00	0.02	0.00	26.54	2.00	0.00	0.00	0.02	0.00
26.58	2.00	0.00	0.00	0.01	0.00	26.67	2.00	0.00	0.00	0.03	0.00
26.73	2.00	0.00	0.00	0.02	0.00	26.78	2.00	0.00	0.00	0.02	0.00
26.85	2.00	0.00	0.00	0.02	0.00	26.93	2.00	0.00	0.00	0.02	0.00
26.98	2.00	0.00	0.00	0.02	0.00	27.03	2.00	0.00	0.00	0.02	0.00
27.13	2.00	0.00	0.00	0.03	0.00	27.17	2.00	0.00	0.00	0.01	0.00
27.24	2.00	0.00	0.00	0.02	0.00	27.33	2.00	0.00	0.00	0.03	0.00
27.36	2.00	0.00	0.00	0.01	0.00	27.43	2.00	0.00	0.00	0.02	0.00
27.53	2.00	0.00	0.00	0.03	0.00	27.60	2.00	0.00	0.00	0.02	0.00
27.63	2.00	0.00	0.00	0.01	0.00	27.72	2.00	0.00	0.00	0.03	0.00
27.77	2.00	0.00	0.00	0.02	0.00	27.84	2.00	0.00	0.00	0.02	0.00
27.93	2.00	0.00	0.00	0.03	0.00	27.97	2.00	0.00	0.00	0.01	0.00
28.02	2.00	0.00	0.00	0.02	0.00	28.12	2.00	0.00	0.00	0.03	0.00
28.17	2.00	0.00	0.00	0.02	0.00	28.22	2.00	0.00	0.00	0.02	0.00
28.32	2.00	0.00	0.00	0.03	0.00	28.36	2.00	0.00	0.00	0.01	0.00
28.42	2.00	0.00	0.00	0.02	0.00	28.48	2.00	0.00	0.00	0.02	0.00
28.57	2.00	0.00	0.00	0.03	0.00	28.62	2.00	0.00	0.00	0.02	0.00
28.72	2.00	0.00	0.00	0.03	0.00	28.75	2.00	0.00	0.00	0.01	0.00
28.82	2.00	0.00	0.00	0.02	0.00	28.87	2.00	0.00	0.00	0.02	0.00
28.95	2.00	0.00	0.00	0.02	0.00	29.02	2.00	0.00	0.00	0.02	0.00
29.07	2.00	0.00	0.00	0.02	0.00	29.16	2.00	0.00	0.00	0.03	0.00
29.21	2.00	0.00	0.00	0.02	0.00	29.29	2.00	0.00	0.00	0.02	0.00
29.36	2.00	0.00	0.00	0.02	0.00	29.40	2.00	0.00	0.00	0.01	0.00
29.47	2.00	0.00	0.00	0.02	0.00	29.56	2.00	0.00	0.00	0.03	0.00
29.60	2.00	0.00	0.00	0.01	0.00	29.71	2.00	0.00	0.00	0.03	0.00
29.75	2.00	0.00	0.00	0.01	0.00	29.79	2.00	0.00	0.00	0.01	0.00
29.86	2.00	0.00	0.00	0.02	0.00	29.95	2.00	0.00	0.00	0.03	0.00
30.04	2.00	0.00	0.00	0.03	0.00	30.06	2.00	0.00	0.00	0.01	0.00
30.15	2.00	0.00	0.00	0.03	0.00	30.20	2.00	0.00	0.00	0.02	0.00
30.28	2.00	0.00	0.00	0.02	0.00	30.35	2.00	0.00	0.00	0.02	0.00
30.39	2.00	0.00	0.00	0.01	0.00	30.45	2.00	0.00	0.00	0.02	0.00
30.54	2.00	0.00	0.00	0.03	0.00	30.60	2.00	0.00	0.00	0.02	0.00
30.67	2.00	0.00	0.00	0.02	0.00	30.74	2.00	0.00	0.00	0.02	0.00
30.79	2.00	0.00	0.00	0.02	0.00	30.86	2.00	0.00	0.00	0.02	0.00
30.95	2.00	0.00	0.00	0.03	0.00	30.99	2.00	0.00	0.00	0.01	0.00
31.05	2.00	0.00	0.00	0.02	0.00	31.14	2.00	0.00	0.00	0.03	0.00
31.19	2.00	0.00	0.00	0.02	0.00	31.26	2.00	0.00	0.00	0.02	0.00
31.34	2.00	0.00	0.00	0.02	0.00	31.39	2.00	0.00	0.00	0.02	0.00
31.45	2.00	0.00	0.00	0.02	0.00	31.54	2.00	0.00	0.00	0.03	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
31.57	2.00	0.00	0.00	0.01	0.00	31.63	2.00	0.00	0.00	0.02	0.00
31.73	2.00	0.00	0.00	0.03	0.00	31.77	2.00	0.00	0.00	0.01	0.00
31.84	2.00	0.00	0.00	0.02	0.00	31.93	2.00	0.00	0.00	0.03	0.00
31.98	2.00	0.00	0.00	0.02	0.00	32.05	2.00	0.00	0.00	0.02	0.00
32.09	2.00	0.00	0.00	0.01	0.00	32.17	2.00	0.00	0.00	0.02	0.00
32.22	2.00	0.00	0.00	0.02	0.00	32.32	2.00	0.00	0.00	0.03	0.00
32.35	2.00	0.00	0.00	0.01	0.00	32.43	2.00	0.00	0.00	0.02	0.00
32.52	2.00	0.00	0.00	0.03	0.00	32.57	2.00	0.00	0.00	0.02	0.00
32.62	2.00	0.00	0.00	0.02	0.00	32.71	2.00	0.00	0.00	0.03	0.00
32.76	2.00	0.00	0.00	0.02	0.00	32.82	2.00	0.00	0.00	0.02	0.00
32.90	2.00	0.00	0.00	0.02	0.00	32.96	2.00	0.00	0.00	0.02	0.00
33.02	2.00	0.00	0.00	0.02	0.00	33.11	2.00	0.00	0.00	0.03	0.00
33.17	2.00	0.00	0.00	0.02	0.00	33.22	2.00	0.00	0.00	0.02	0.00
33.31	2.00	0.00	0.00	0.03	0.00	33.34	2.00	0.00	0.00	0.01	0.00
33.41	2.00	0.00	0.00	0.02	0.00	33.49	2.00	0.00	0.00	0.02	0.00
33.57	2.00	0.00	0.00	0.02	0.00	33.61	2.00	0.00	0.00	0.01	0.00
33.68	2.00	0.00	0.00	0.02	0.00	33.76	2.00	0.00	0.00	0.02	0.00
33.81	2.00	0.00	0.00	0.02	0.00	33.88	2.00	0.00	0.00	0.02	0.00
33.95	2.00	0.00	0.00	0.02	0.00	34.01	2.00	0.00	0.00	0.02	0.00
34.06	2.00	0.00	0.00	0.02	0.00	34.13	2.00	0.00	0.00	0.02	0.00
34.21	2.00	0.00	0.00	0.02	0.00	34.25	2.00	0.00	0.00	0.01	0.00
34.35	2.00	0.00	0.00	0.03	0.00	34.40	2.00	0.00	0.00	0.02	0.00
34.49	2.00	0.00	0.00	0.03	0.00	34.53	2.00	0.00	0.00	0.01	0.00
34.60	2.00	0.00	0.00	0.02	0.00	34.65	2.00	0.00	0.00	0.02	0.00
34.74	2.00	0.00	0.00	0.03	0.00	34.80	2.00	0.00	0.00	0.02	0.00
34.85	2.00	0.00	0.00	0.02	0.00	34.93	2.00	0.00	0.00	0.02	0.00
34.98	2.00	0.00	0.00	0.02	0.00	35.05	2.00	0.00	0.00	0.02	0.00
35.15	2.00	0.00	0.00	0.03	0.00	35.20	2.00	0.00	0.00	0.02	0.00
35.25	2.00	0.00	0.00	0.02	0.00	35.33	2.00	0.00	0.00	0.02	0.00
35.40	2.00	0.00	0.00	0.02	0.00	35.44	2.00	0.00	0.00	0.01	0.00
35.50	2.00	0.00	0.00	0.02	0.00	35.59	2.00	0.00	0.00	0.03	0.00
35.64	2.00	0.00	0.00	0.02	0.00	35.70	2.00	0.00	0.00	0.02	0.00
35.79	2.00	0.00	0.00	0.03	0.00	35.83	2.00	0.00	0.00	0.01	0.00
35.94	2.00	0.00	0.00	0.03	0.00	35.98	2.00	0.00	0.00	0.01	0.00
36.03	2.00	0.00	0.00	0.02	0.00	36.09	2.00	0.00	0.00	0.02	0.00
36.17	2.00	0.00	0.00	0.02	0.00	36.23	2.00	0.00	0.00	0.02	0.00
36.29	2.00	0.00	0.00	0.02	0.00	36.38	2.00	0.00	0.00	0.03	0.00
36.44	2.00	0.00	0.00	0.02	0.00	36.49	2.00	0.00	0.00	0.02	0.00
36.59	2.00	0.00	0.00	0.03	0.00	36.63	2.00	0.00	0.00	0.01	0.00
36.69	2.00	0.00	0.00	0.02	0.00	36.78	2.00	0.00	0.00	0.03	0.00
36.82	2.00	0.00	0.00	0.01	0.00	36.88	2.00	0.00	0.00	0.02	0.00
36.98	2.00	0.00	0.00	0.03	0.00	37.02	2.00	0.00	0.00	0.01	0.00
37.11	2.00	0.00	0.00	0.03	0.00	37.18	2.00	0.00	0.00	0.02	0.00
37.22	2.00	0.00	0.00	0.01	0.00	37.28	2.00	0.00	0.00	0.02	0.00
37.38	2.00	0.00	0.00	0.03	0.00	37.42	2.00	0.00	0.00	0.01	0.00
37.48	2.00	0.00	0.00	0.02	0.00	37.57	2.00	0.00	0.00	0.03	0.00
37.62	2.00	0.00	0.00	0.02	0.00	37.68	2.00	0.00	0.00	0.02	0.00
37.77	2.00	0.00	0.00	0.03	0.00	37.82	2.00	0.00	0.00	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
37.88	2.00	0.00	0.00	0.02	0.00	37.96	2.00	0.00	0.00	0.02	0.00
38.00	2.00	0.00	0.00	0.01	0.00	38.08	2.00	0.00	0.00	0.02	0.00
38.12	2.00	0.00	0.00	0.01	0.00	38.20	2.00	0.00	0.00	0.02	0.00
38.27	2.00	0.00	0.00	0.02	0.00	38.36	2.00	0.00	0.00	0.03	0.00
38.40	2.00	0.00	0.00	0.01	0.00	38.46	2.00	0.00	0.00	0.02	0.00
38.56	2.00	0.00	0.00	0.03	0.00	38.59	2.00	0.00	0.00	0.01	0.00
38.66	2.00	0.00	0.00	0.02	0.00	38.76	2.00	0.00	0.00	0.03	0.00
38.79	2.00	0.00	0.00	0.01	0.00	38.87	2.00	0.00	0.00	0.02	0.00
38.91	2.00	0.00	0.00	0.01	0.00	39.00	2.00	0.00	0.00	0.03	0.00
39.04	2.00	0.00	0.00	0.01	0.00	39.11	2.00	0.00	0.00	0.02	0.00
39.20	2.00	0.00	0.00	0.03	0.00	39.24	2.00	0.00	0.00	0.01	0.00
39.31	2.00	0.00	0.00	0.02	0.00	39.38	2.00	0.00	0.00	0.02	0.00
39.46	2.00	0.00	0.00	0.02	0.00	39.51	0.98	0.00	0.00	0.02	0.00
39.60	2.00	0.00	0.00	0.03	0.00	39.66	2.00	0.00	0.00	0.02	0.00
39.71	2.00	0.00	0.00	0.02	0.00	39.79	2.00	0.00	0.00	0.02	0.00
39.85	2.00	0.00	0.00	0.02	0.00	39.91	2.00	0.00	0.00	0.02	0.00
39.99	2.00	0.00	0.00	0.02	0.00	40.05	2.00	0.00	0.00	0.02	0.00
40.11	2.00	0.00	0.00	0.02	0.00	40.20	1.85	0.00	0.00	0.03	0.00
40.25	1.95	0.00	0.00	0.02	0.00	40.30	2.00	0.00	0.00	0.02	0.00
40.40	2.00	0.00	0.00	0.03	0.00	40.43	2.00	0.00	0.00	0.01	0.00
40.49	2.00	0.00	0.00	0.02	0.00	40.55	2.00	0.00	0.00	0.02	0.00
40.64	2.00	0.00	0.00	0.03	0.00	40.69	2.00	0.00	0.00	0.02	0.00
40.80	2.00	0.00	0.00	0.03	0.00	40.84	2.00	0.00	0.00	0.01	0.00
40.89	1.90	0.00	0.00	0.02	0.00	40.96	1.75	0.00	0.00	0.02	0.00
41.04	1.61	0.00	0.00	0.02	0.00	41.10	1.47	0.00	0.00	0.02	0.00
41.15	1.35	0.00	0.00	0.02	0.00	41.24	1.24	0.00	0.00	0.03	0.00
41.28	1.23	0.00	0.00	0.01	0.00	41.38	1.22	0.00	0.00	0.03	0.00
41.41	1.21	0.00	0.00	0.01	0.00	41.49	1.21	0.00	0.00	0.02	0.00
41.54	1.20	0.00	0.00	0.02	0.00	41.61	1.19	0.00	0.00	0.02	0.00
41.69	1.18	0.00	0.00	0.02	0.00	41.77	1.16	0.00	0.00	0.02	0.00
41.84	1.15	0.00	0.00	0.02	0.00	41.88	1.13	0.00	0.00	0.01	0.00
41.94	1.11	0.00	0.00	0.02	0.00	42.04	1.09	0.00	0.00	0.03	0.00
42.08	1.07	0.00	0.00	0.01	0.00	42.17	1.06	0.00	0.00	0.03	0.00
42.19	1.05	0.00	0.00	0.01	0.00	42.28	1.05	0.00	0.00	0.03	0.00
42.33	1.04	0.00	0.00	0.02	0.00	42.39	1.04	0.00	0.00	0.02	0.00
42.48	1.04	0.00	0.00	0.03	0.00	42.53	1.05	0.00	0.00	0.02	0.00
42.59	1.06	0.00	0.00	0.02	0.00	42.67	1.08	0.00	0.00	0.02	0.00
42.73	1.10	0.00	0.00	0.02	0.00	42.81	1.12	0.00	0.00	0.02	0.00
42.88	1.14	0.00	0.00	0.02	0.00	42.92	1.16	0.00	0.00	0.01	0.00
43.00	1.18	0.00	0.00	0.02	0.00	43.08	1.20	0.00	0.00	0.02	0.00
43.12	1.22	0.00	0.00	0.01	0.00	43.21	1.23	0.00	0.00	0.03	0.00
43.27	1.25	0.00	0.00	0.02	0.00	43.32	1.27	0.00	0.00	0.02	0.00
43.39	1.29	0.00	0.00	0.02	0.00	43.47	1.31	0.00	0.00	0.02	0.00
43.52	1.31	0.00	0.00	0.02	0.00	43.59	1.31	0.00	0.00	0.02	0.00
43.67	1.29	0.00	0.00	0.02	0.00	43.72	1.27	0.00	0.00	0.02	0.00
43.80	1.21	0.00	0.00	0.02	0.00	43.85	1.14	0.00	0.00	0.02	0.00
43.92	1.07	0.00	0.00	0.02	0.00	43.97	2.00	0.00	0.00	0.02	0.00
44.04	2.00	0.00	0.00	0.02	0.00	44.13	2.00	0.00	0.00	0.03	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
44.17	2.00	0.00	0.00	0.01	0.00	44.24	2.00	0.00	0.00	0.02	0.00
44.31	2.00	0.00	0.00	0.02	0.00	44.37	2.00	0.00	0.00	0.02	0.00
44.45	2.00	0.00	0.00	0.02	0.00	44.50	2.00	0.00	0.00	0.02	0.00
44.56	2.00	0.00	0.00	0.02	0.00	44.65	2.00	0.00	0.00	0.03	0.00
44.71	2.00	0.00	0.00	0.02	0.00	44.76	2.00	0.00	0.00	0.02	0.00
44.85	2.00	0.00	0.00	0.03	0.00	44.88	2.00	0.00	0.00	0.01	0.00
44.96	2.00	0.00	0.00	0.02	0.00	45.05	2.00	0.00	0.00	0.03	0.00
45.10	2.00	0.00	0.00	0.02	0.00	45.17	2.00	0.00	0.00	0.02	0.00
45.25	2.00	0.00	0.00	0.02	0.00	45.30	2.00	0.00	0.00	0.02	0.00
45.37	0.61	0.00	0.00	0.02	0.03	45.45	0.66	0.00	0.00	0.02	0.03
45.49	0.71	0.00	0.00	0.01	0.01	45.54	0.76	0.00	0.00	0.02	0.01
45.61	0.81	0.00	0.00	0.02	0.01	45.68	0.86	0.00	0.00	0.02	0.01
45.75	0.90	0.00	0.00	0.02	0.01	45.80	0.93	0.00	0.00	0.02	0.00
45.89	0.93	0.00	0.00	0.03	0.01	45.93	0.93	0.00	0.00	0.01	0.00
46.01	0.90	0.00	0.00	0.02	0.01	46.08	2.00	0.00	0.00	0.02	0.00
46.15	2.00	0.00	0.00	0.02	0.00	46.20	2.00	0.00	0.00	0.02	0.00
46.29	2.00	0.00	0.00	0.03	0.00	46.34	2.00	0.00	0.00	0.02	0.00
46.41	2.00	0.00	0.00	0.02	0.00	46.49	2.00	0.00	0.00	0.02	0.00
46.53	2.00	0.00	0.00	0.01	0.00	46.60	2.00	0.00	0.00	0.02	0.00
46.69	2.00	0.00	0.00	0.03	0.00	46.73	2.00	0.00	0.00	0.01	0.00
46.79	2.00	0.00	0.00	0.02	0.00	46.89	2.00	0.00	0.00	0.03	0.00
46.94	2.00	0.00	0.00	0.02	0.00	46.99	2.00	0.00	0.00	0.02	0.00
47.09	2.00	0.00	0.00	0.03	0.00	47.13	2.00	0.00	0.00	0.01	0.00
47.19	2.00	0.00	0.00	0.02	0.00	47.28	2.00	0.00	0.00	0.03	0.00
47.34	2.00	0.00	0.00	0.02	0.00	47.38	2.00	0.00	0.00	0.01	0.00
47.50	2.00	0.00	0.00	0.04	0.00	47.51	2.00	0.00	0.00	0.00	0.00
47.60	2.00	0.00	0.00	0.03	0.00	47.69	2.00	0.00	0.00	0.03	0.00
47.70	2.00	0.00	0.00	0.00	0.00	47.80	2.00	0.00	0.00	0.03	0.00
47.84	2.00	0.00	0.00	0.01	0.00	47.91	2.00	0.00	0.00	0.02	0.00
48.00	2.00	0.00	0.00	0.03	0.00	48.04	2.00	0.00	0.00	0.01	0.00
48.11	1.21	0.00	0.00	0.02	0.00	48.19	1.23	0.00	0.00	0.02	0.00
48.23	1.25	0.00	0.00	0.01	0.00	48.30	1.26	0.00	0.00	0.02	0.00
48.40	1.26	0.00	0.00	0.03	0.00	48.45	1.27	0.00	0.00	0.02	0.00
48.50	1.27	0.00	0.00	0.02	0.00	48.59	1.28	0.00	0.00	0.03	0.00
48.66	1.29	0.00	0.00	0.02	0.00	48.69	1.29	0.00	0.00	0.01	0.00
48.78	1.29	0.00	0.00	0.03	0.00	48.85	1.29	0.00	0.00	0.02	0.00
48.89	1.29	0.00	0.00	0.01	0.00	48.98	1.28	0.00	0.00	0.03	0.00
49.03	1.28	0.00	0.00	0.02	0.00	49.09	1.28	0.00	0.00	0.02	0.00
49.19	1.29	0.00	0.00	0.03	0.00	49.23	1.30	0.00	0.00	0.01	0.00
49.28	1.34	0.00	0.00	0.02	0.00	49.39	1.37	0.00	0.00	0.03	0.00
49.42	1.42	0.00	0.00	0.01	0.00	49.49	1.46	0.00	0.00	0.02	0.00
49.59	1.48	0.00	0.00	0.03	0.00	49.62	1.50	0.00	0.00	0.01	0.00
49.69	1.50	0.00	0.00	0.02	0.00	49.74	1.48	0.00	0.00	0.02	0.00
49.83	1.43	0.00	0.00	0.03	0.00	49.88	1.37	0.00	0.00	0.02	0.00
49.93	1.31	0.00	0.00	0.02	0.00	50.03	2.00	0.00	0.00	0.03	0.00
50.13	2.00	0.00	0.00	0.03	0.00	50.14	2.00	0.00	0.00	0.00	0.00
50.23	2.00	0.00	0.00	0.03	0.00	50.27	2.00	0.00	0.00	0.01	0.00
50.34	2.00	0.00	0.00	0.02	0.00	50.43	2.00	0.00	0.00	0.03	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
50.49	2.00	0.00	0.00	0.02	0.00	50.53	2.00	0.00	0.00	0.01	0.00
50.62	2.00	0.00	0.00	0.03	0.00	50.68	2.00	0.00	0.00	0.02	0.00
50.73	2.00	0.00	0.00	0.02	0.00	50.82	2.00	0.00	0.00	0.03	0.00
50.88	2.00	0.00	0.00	0.02	0.00	50.93	2.00	0.00	0.00	0.02	0.00
51.02	2.00	0.00	0.00	0.03	0.00	51.09	2.00	0.00	0.00	0.02	0.00
51.12	2.00	0.00	0.00	0.01	0.00	51.19	2.00	0.00	0.00	0.02	0.00
51.28	2.00	0.00	0.00	0.03	0.00	51.32	2.00	0.00	0.00	0.01	0.00
51.39	2.00	0.00	0.00	0.02	0.00	51.48	2.00	0.00	0.00	0.03	0.00
51.53	2.00	0.00	0.00	0.02	0.00	51.62	2.00	0.00	0.00	0.03	0.00
51.68	2.00	0.00	0.00	0.02	0.00	51.73	2.00	0.00	0.00	0.02	0.00
51.82	2.00	0.00	0.00	0.03	0.00	51.87	2.00	0.00	0.00	0.02	0.00
51.92	2.00	0.00	0.00	0.02	0.00	51.97	2.00	0.00	0.00	0.02	0.00
52.04	2.00	0.00	0.00	0.02	0.00	52.12	2.00	0.00	0.00	0.02	0.00
52.18	2.00	0.00	0.00	0.02	0.00	52.23	2.00	0.00	0.00	0.02	0.00
52.31	2.00	0.00	0.00	0.02	0.00	52.37	2.00	0.00	0.00	0.02	0.00
52.44	2.00	0.00	0.00	0.02	0.00	52.53	2.00	0.00	0.00	0.03	0.00
52.57	2.00	0.00	0.00	0.01	0.00	52.64	2.00	0.00	0.00	0.02	0.00
52.72	2.00	0.00	0.00	0.02	0.00	52.78	2.00	0.00	0.00	0.02	0.00
52.83	2.00	0.00	0.00	0.02	0.00	52.93	2.00	0.00	0.00	0.03	0.00
52.96	2.00	0.00	0.00	0.01	0.00	53.04	2.00	0.00	0.00	0.02	0.00
53.12	2.00	0.00	0.00	0.02	0.00	53.17	2.00	0.00	0.00	0.02	0.00
53.22	2.00	0.00	0.00	0.02	0.00	53.29	2.00	0.00	0.00	0.02	0.00
53.37	2.00	0.00	0.00	0.02	0.00	53.42	2.00	0.00	0.00	0.02	0.00
53.49	2.00	0.00	0.00	0.02	0.00	53.58	2.00	0.00	0.00	0.03	0.00
53.63	2.00	0.00	0.00	0.02	0.00	53.68	2.00	0.00	0.00	0.02	0.00
53.78	2.00	0.00	0.00	0.03	0.00	53.84	2.00	0.00	0.00	0.02	0.00
53.88	2.00	0.00	0.00	0.01	0.00	53.94	2.00	0.00	0.00	0.02	0.00
54.03	2.00	0.00	0.00	0.03	0.00	54.08	2.00	0.00	0.00	0.02	0.00
54.16	2.00	0.00	0.00	0.02	0.00	54.20	2.00	0.00	0.00	0.01	0.00
54.28	2.00	0.00	0.00	0.02	0.00	54.35	2.00	0.00	0.00	0.02	0.00
54.43	2.00	0.00	0.00	0.02	0.00	54.48	2.00	0.00	0.00	0.02	0.00
54.55	2.00	0.00	0.00	0.02	0.00	54.63	2.00	0.00	0.00	0.02	0.00
54.67	2.00	0.00	0.00	0.01	0.00	54.74	2.00	0.00	0.00	0.02	0.00
54.82	2.00	0.00	0.00	0.02	0.00	54.87	2.00	0.00	0.00	0.02	0.00
54.92	2.00	0.00	0.00	0.02	0.00	55.02	2.00	0.00	0.00	0.03	0.00
55.06	2.00	0.00	0.00	0.01	0.00	55.14	2.00	0.00	0.00	0.02	0.00
55.22	2.00	0.00	0.00	0.02	0.00	55.27	2.00	0.00	0.00	0.02	0.00
55.37	2.00	0.00	0.00	0.03	0.00	55.42	2.00	0.00	0.00	0.02	0.00
55.47	2.00	0.00	0.00	0.02	0.00	55.53	2.00	0.00	0.00	0.02	0.00
55.58	2.00	0.00	0.00	0.02	0.00	55.67	2.00	0.00	0.00	0.03	0.00
55.72	2.00	0.00	0.00	0.02	0.00	55.81	2.00	0.00	0.00	0.03	0.00
55.86	2.00	0.00	0.00	0.02	0.00	55.92	2.00	0.00	0.00	0.02	0.00
56.01	2.00	0.00	0.00	0.03	0.00	56.05	2.00	0.00	0.00	0.01	0.00
56.11	2.00	0.00	0.00	0.02	0.00	56.21	2.00	0.00	0.00	0.03	0.00
56.26	2.00	0.00	0.00	0.02	0.00	56.32	2.00	0.00	0.00	0.02	0.00
56.41	2.00	0.00	0.00	0.03	0.00	56.46	2.00	0.00	0.00	0.02	0.00
56.50	2.00	0.00	0.00	0.01	0.00	56.59	2.00	0.00	0.00	0.03	0.00
56.65	2.00	0.00	0.00	0.02	0.00	56.70	2.00	0.00	0.00	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
56.78	2.00	0.00	0.00	0.02	0.00	56.85	2.00	0.00	0.00	0.02	0.00
56.89	2.00	0.00	0.00	0.01	0.00	56.98	2.00	0.00	0.00	0.03	0.00
57.04	2.00	0.00	0.00	0.02	0.00	57.09	2.00	0.00	0.00	0.02	0.00
57.16	2.00	0.00	0.00	0.02	0.00	57.24	2.00	0.00	0.00	0.02	0.00
57.29	2.00	0.00	0.00	0.02	0.00	57.37	2.00	0.00	0.00	0.02	0.00
57.42	2.00	0.00	0.00	0.02	0.00	57.49	2.00	0.00	0.00	0.02	0.00
57.59	2.00	0.00	0.00	0.03	0.00	57.64	2.00	0.00	0.00	0.02	0.00
57.69	2.00	0.00	0.00	0.02	0.00	57.77	2.00	0.00	0.00	0.02	0.00
57.82	2.00	0.00	0.00	0.02	0.00	57.89	2.00	0.00	0.00	0.02	0.00
57.97	2.00	0.00	0.00	0.02	0.00	58.03	2.00	0.00	0.00	0.02	0.00
58.09	2.00	0.00	0.00	0.02	0.00	58.17	2.00	0.00	0.00	0.02	0.00
58.21	2.00	0.00	0.00	0.01	0.00	58.28	2.00	0.00	0.00	0.02	0.00
58.37	2.00	0.00	0.00	0.03	0.00	58.40	2.00	0.00	0.00	0.01	0.00
58.48	2.00	0.00	0.00	0.02	0.00	58.53	2.00	0.00	0.00	0.02	0.00
58.63	2.00	0.00	0.00	0.03	0.00	58.67	2.00	0.00	0.00	0.01	0.00
58.73	2.00	0.00	0.00	0.02	0.00	58.82	2.00	0.00	0.00	0.03	0.00
58.89	2.00	0.00	0.00	0.02	0.00	58.93	2.00	0.00	0.00	0.01	0.00
59.00	2.00	0.00	0.00	0.02	0.00	59.06	2.00	0.00	0.00	0.02	0.00
59.13	2.00	0.00	0.00	0.02	0.00	59.22	2.00	0.00	0.00	0.03	0.00
59.28	2.00	0.00	0.00	0.02	0.00	59.33	2.00	0.00	0.00	0.02	0.00
59.41	2.00	0.00	0.00	0.02	0.00	59.47	2.00	0.00	0.00	0.02	0.00
59.52	2.00	0.00	0.00	0.02	0.00	59.61	2.00	0.00	0.00	0.03	0.00
59.67	2.00	0.00	0.00	0.02	0.00	59.72	2.00	0.00	0.00	0.02	0.00
59.78	2.00	0.00	0.00	0.02	0.00	59.87	2.00	0.00	0.00	0.03	0.00
59.92	2.00	0.00	0.00	0.02	0.00	60.00	2.00	0.00	0.00	0.02	0.00
60.05	2.00	0.00	0.00	0.02	0.00	60.11	2.00	0.00	0.00	0.02	0.00
60.21	2.00	0.00	0.00	0.03	0.00	60.25	2.00	0.00	0.00	0.01	0.00
60.31	2.00	0.00	0.00	0.02	0.00	60.40	2.00	0.00	0.00	0.03	0.00
60.43	2.00	0.00	0.00	0.01	0.00	60.51	2.00	0.00	0.00	0.02	0.00

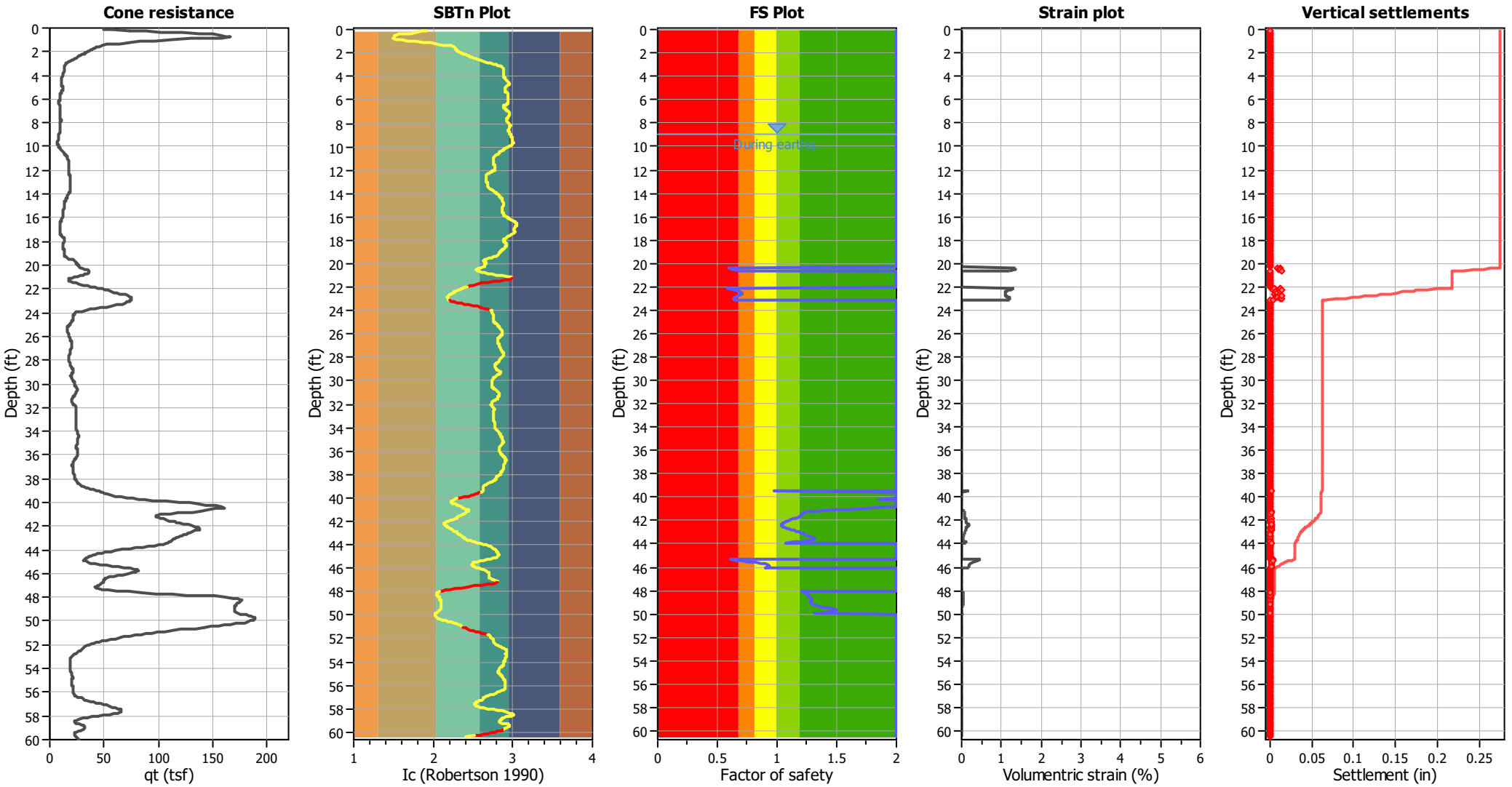
Overall liquefaction potential: 1.15

LPI = 0.00 - Liquefaction risk very low
LPI between 0.00 and 5.00 - Liquefaction risk low
LPI between 5.00 and 15.00 - Liquefaction risk high
LPI > 15.00 - Liquefaction risk very high

Abbreviations

FS: Calculated factor of safety for test point
F_L: 1 - FS
w_z: Function value of the extend of soil liquefaction according to depth
d_z: Layer thickness (ft)
LPI: Liquefaction potential index value for test point

Estimation of post-earthquake settlements



Abbreviations

q_t:	Total cone resistance (cone resistance q_c corrected for pore water effects)
I_c:	Soil Behaviour Type Index
FS:	Calculated Factor of Safety against liquefaction
Volumentric strain:	Post-liquefaction volumentric strain

:: Lateral displacement index calculation ::

Depth (ft)	q_t (tsf)	Q_{tn}	R_f (%)	$Q_{tn,cs}$	FS	D_r	$Gamma_{max}$ (%)	Lat. disp. (in)
9.07	8.35	12.59	3.59	81.85	2.00	0.00	0.00	0.00
9.14	8.17	12.30	3.55	80.67	2.00	0.00	0.00	0.00
9.22	8.01	12.03	3.48	79.33	2.00	0.00	0.00	0.00
9.27	7.85	11.77	3.41	77.97	2.00	0.00	0.00	0.00
9.37	7.71	11.54	3.31	76.43	2.00	0.00	0.00	0.00
9.42	7.56	11.30	3.25	75.16	2.00	0.00	0.00	0.00
9.47	7.39	11.03	3.19	73.85	2.00	0.00	0.00	0.00
9.52	7.22	10.74	3.14	72.68	2.00	0.00	0.00	0.00
9.62	7.05	10.46	3.09	71.47	2.00	0.00	0.00	0.00
9.67	6.93	10.26	3.01	70.25	2.00	0.00	0.00	0.00
9.73	7.01	10.39	2.95	69.94	2.00	0.00	0.00	0.00
9.82	7.17	10.63	2.90	70.09	2.00	0.00	0.00	0.00
9.86	7.39	10.98	2.86	70.54	2.00	0.00	0.00	0.00
9.92	7.76	11.57	2.88	72.17	2.00	0.00	0.00	0.00
10.02	8.17	12.23	2.94	74.33	2.00	0.00	0.00	0.00
10.06	8.66	13.01	3.03	77.10	2.00	0.00	0.00	0.00
10.12	9.25	13.95	3.14	80.39	2.00	1.99	0.00	0.00
10.21	9.84	14.90	3.25	83.79	2.00	4.16	0.00	0.00
10.25	10.49	15.94	3.37	87.38	2.00	6.38	0.00	0.00
10.31	11.09	16.89	3.46	90.46	2.00	8.30	0.00	0.00
10.41	11.67	17.81	3.52	93.18	2.00	10.05	0.00	0.00
10.45	12.28	18.80	3.57	95.78	2.00	11.83	0.00	0.00
10.52	12.84	19.69	3.62	98.11	2.00	13.36	0.00	0.00
10.61	13.40	20.57	3.64	100.13	2.00	14.81	0.00	0.00
10.64	13.96	21.47	3.65	101.99	2.00	16.22	0.00	0.00
10.71	14.46	22.27	3.66	103.52	2.00	17.43	0.00	0.00
10.81	14.98	22.93	3.66	104.69	2.00	18.39	0.00	0.00
10.85	15.43	23.52	3.67	105.85	2.00	19.23	0.00	0.00
10.91	15.78	23.92	3.69	106.92	2.00	19.79	0.00	0.00
10.96	16.11	24.32	3.72	108.02	2.00	20.33	0.00	0.00
11.03	16.41	24.63	3.76	109.16	2.00	20.75	0.00	0.00
11.10	16.63	24.81	3.80	110.05	2.00	21.00	0.00	0.00
11.20	16.84	24.94	3.84	110.91	2.00	21.17	0.00	0.00
11.24	17.06	25.18	3.87	111.77	2.00	21.49	0.00	0.00
11.30	17.28	25.38	3.90	112.54	2.00	21.74	0.00	0.00
11.36	17.47	25.53	3.93	113.33	2.00	21.94	0.00	0.00
11.43	17.60	25.59	3.96	113.92	2.00	22.02	0.00	0.00
11.50	17.65	25.53	3.99	114.20	2.00	21.93	0.00	0.00
11.58	17.64	25.35	4.01	114.11	2.00	21.71	0.00	0.00
11.63	17.60	25.19	4.01	113.88	2.00	21.49	0.00	0.00
11.70	17.51	24.92	4.01	113.42	2.00	21.14	0.00	0.00
11.79	17.40	24.59	3.98	112.43	2.00	20.69	0.00	0.00
11.84	17.23	24.24	3.93	111.06	2.00	20.22	0.00	0.00
11.90	17.01	23.80	3.86	109.21	2.00	19.62	0.00	0.00
11.98	16.94	23.51	3.72	106.65	2.00	19.22	0.00	0.00
12.02	16.91	23.37	3.56	103.99	2.00	19.02	0.00	0.00
12.09	17.00	23.38	3.38	101.38	2.00	19.03	0.00	0.00
12.14	17.14	23.48	3.22	99.12	2.00	19.18	0.00	0.00

:: Estimation of post-earthquake lateral Displacements :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	R_f (%)	$Q_{tn,cs}$	FS	D_r	$Gamma_{max}$ (%)	Lat. disp. (in)
12.21	17.31	23.60	3.07	96.91	2.00	19.34	0.00	0.00
12.29	17.62	23.89	2.91	94.76	2.00	19.74	0.00	0.00
12.34	17.88	24.16	2.79	93.21	2.00	20.11	0.00	0.00
12.44	18.17	24.43	2.71	92.34	2.00	20.48	0.00	0.00
12.49	18.50	24.79	2.66	91.81	2.00	20.97	0.00	0.00
12.57	18.63	24.90	2.65	91.83	2.00	21.11	0.00	0.00
12.64	18.76	25.02	2.66	92.19	2.00	21.26	0.00	0.00
12.68	18.84	25.09	2.67	92.51	2.00	21.36	0.00	0.00
12.73	18.86	25.08	2.69	92.86	2.00	21.35	0.00	0.00
12.84	18.81	24.93	2.71	92.99	2.00	21.15	0.00	0.00
12.89	18.69	24.74	2.73	93.03	2.00	20.90	0.00	0.00
12.98	18.58	24.53	2.73	92.82	2.00	20.61	0.00	0.00
13.00	18.45	24.34	2.73	92.48	2.00	20.36	0.00	0.00
13.08	18.34	24.13	2.73	92.17	2.00	20.08	0.00	0.00
13.14	18.25	23.98	2.74	92.18	2.00	19.86	0.00	0.00
13.23	18.22	23.86	2.76	92.33	2.00	19.70	0.00	0.00
13.27	18.26	23.89	2.79	92.99	2.00	19.75	0.00	0.00
13.34	18.38	24.01	2.84	93.85	2.00	19.90	0.00	0.00
13.43	18.50	24.12	2.89	94.98	2.00	20.06	0.00	0.00
13.47	18.61	24.25	2.97	96.47	2.00	20.24	0.00	0.00
13.54	18.62	24.25	3.09	98.37	2.00	20.23	0.00	0.00
13.63	18.55	24.12	3.23	100.47	2.00	20.07	0.00	0.00
13.67	18.46	24.02	3.38	102.51	2.00	19.92	0.00	0.00
13.72	18.35	23.87	3.50	104.15	2.00	19.71	0.00	0.00
13.83	18.16	23.56	3.61	105.29	2.00	19.29	0.00	0.00
13.88	17.91	23.21	3.70	106.09	2.00	18.79	0.00	0.00
13.94	17.59	22.77	3.79	106.54	2.00	18.16	0.00	0.00
13.98	17.20	22.26	3.88	106.80	2.00	17.41	0.00	0.00
14.06	16.75	21.64	3.96	106.76	2.00	16.48	0.00	0.00
14.14	16.40	21.13	3.98	106.09	2.00	15.69	0.00	0.00
14.18	16.13	20.75	3.96	105.03	2.00	15.09	0.00	0.00
14.26	15.81	20.27	3.94	103.76	2.00	14.31	0.00	0.00
14.33	15.47	19.77	3.90	102.31	2.00	13.50	0.00	0.00
14.37	15.15	19.33	3.87	101.05	2.00	12.76	0.00	0.00
14.45	14.78	18.80	3.86	99.86	2.00	11.84	0.00	0.00
14.54	14.43	18.29	3.84	98.53	2.00	10.94	0.00	0.00
14.61	14.15	17.89	3.80	97.16	2.00	10.19	0.00	0.00
14.65	13.92	17.55	3.74	95.67	2.00	9.56	0.00	0.00
14.74	13.69	17.19	3.68	94.20	2.00	8.88	0.00	0.00
14.80	13.48	16.88	3.62	92.84	2.00	8.28	0.00	0.00
14.85	13.31	16.63	3.56	91.55	2.00	7.78	0.00	0.00
14.90	13.18	16.42	3.50	90.43	2.00	7.38	0.00	0.00
15.00	13.08	16.23	3.43	89.23	2.00	6.99	0.00	0.00
15.05	13.03	16.13	3.35	88.03	2.00	6.78	0.00	0.00
15.10	12.95	15.99	3.29	86.96	2.00	6.49	0.00	0.00
15.17	12.87	15.84	3.23	85.96	2.00	6.19	0.00	0.00
15.25	12.79	15.69	3.18	85.06	2.00	5.87	0.00	0.00
15.30	12.71	15.56	3.13	84.17	2.00	5.59	0.00	0.00

:: Estimation of post-earthquake lateral Displacements :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	R_f (%)	$Q_{tn,cs}$	FS	D_r	$Gamma_{max}$ (%)	Lat. disp. (in)
15.36	12.61	15.39	3.08	83.29	2.00	5.24	0.00	0.00
15.45	12.52	15.23	3.03	82.36	2.00	4.88	0.00	0.00
15.49	12.41	15.06	2.99	81.49	2.00	4.52	0.00	0.00
15.57	12.29	14.87	2.96	80.69	2.00	4.09	0.00	0.00
15.64	12.18	14.70	2.94	80.12	2.00	3.71	0.00	0.00
15.69	12.09	14.56	2.93	79.78	2.00	3.40	0.00	0.00
15.77	11.98	14.39	2.94	79.54	2.00	3.00	0.00	0.00
15.85	11.82	14.15	2.98	79.57	2.00	2.45	0.00	0.00
15.89	11.63	13.90	3.03	79.64	2.00	1.87	0.00	0.00
15.99	11.42	13.60	3.09	79.77	2.00	1.16	0.00	0.00
16.05	11.18	13.29	3.18	80.06	2.00	0.39	0.00	0.00
16.09	10.95	13.00	3.26	80.24	2.00	0.00	0.00	0.00
16.16	10.68	12.63	3.34	80.24	2.00	0.00	0.00	0.00
16.24	10.38	12.21	3.41	79.98	2.00	0.00	0.00	0.00
16.30	10.10	11.82	3.47	79.51	2.00	0.00	0.00	0.00
16.34	9.80	11.42	3.50	78.82	2.00	0.00	0.00	0.00
16.44	9.56	11.07	3.50	77.83	2.00	0.00	0.00	0.00
16.48	9.34	10.78	3.49	76.90	2.00	0.00	0.00	0.00
16.54	9.16	10.52	3.46	75.93	2.00	0.00	0.00	0.00
16.63	9.03	10.33	3.41	74.93	2.00	0.00	0.00	0.00
16.69	8.94	10.19	3.34	73.96	2.00	0.00	0.00	0.00
16.74	8.91	10.14	3.25	72.99	2.00	0.00	0.00	0.00
16.82	8.90	10.10	3.17	72.11	2.00	0.00	0.00	0.00
16.90	8.88	10.04	3.09	71.21	2.00	0.00	0.00	0.00
16.94	8.94	10.09	3.01	70.59	2.00	0.00	0.00	0.00
17.03	8.98	10.11	2.95	70.04	2.00	0.00	0.00	0.00
17.07	8.99	10.11	2.89	69.52	2.00	0.00	0.00	0.00
17.13	8.97	10.07	2.91	69.59	2.00	0.00	0.00	0.00
17.21	8.95	10.01	2.98	70.13	2.00	0.00	0.00	0.00
17.26	9.06	10.15	3.08	71.40	2.00	0.00	0.00	0.00
17.33	9.38	10.52	3.16	73.22	2.00	0.00	0.00	0.00
17.41	9.84	11.06	3.22	75.19	2.00	0.00	0.00	0.00
17.48	10.47	11.81	3.25	77.41	2.00	0.00	0.00	0.00
17.53	11.02	12.49	3.31	79.66	2.00	0.00	0.00	0.00
17.61	11.59	13.15	3.35	81.69	2.00	0.05	0.00	0.00
17.67	12.19	13.84	3.37	83.58	2.00	1.72	0.00	0.00
17.72	12.75	14.48	3.32	84.41	2.00	3.23	0.00	0.00
17.82	13.25	15.02	3.24	84.59	2.00	4.42	0.00	0.00
17.88	13.49	15.26	3.17	84.31	2.00	4.95	0.00	0.00
17.92	13.46	15.20	3.12	83.57	2.00	4.82	0.00	0.00
18.02	13.24	14.89	3.09	82.55	2.00	4.14	0.00	0.00
18.07	12.93	14.50	3.06	81.41	2.00	3.25	0.00	0.00
18.14	12.53	14.00	3.05	80.27	2.00	2.10	0.00	0.00
18.20	12.25	13.64	3.01	79.05	2.00	1.24	0.00	0.00
18.27	12.04	13.36	2.97	78.00	2.00	0.56	0.00	0.00
18.32	11.94	13.22	2.96	77.57	2.00	0.22	0.00	0.00
18.38	11.89	13.14	2.96	77.43	2.00	0.01	0.00	0.00
18.47	11.95	13.17	2.96	77.44	2.00	0.09	0.00	0.00

:: Estimation of post-earthquake lateral Displacements :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	R_f (%)	$Q_{tn,cs}$	FS	D_r	$Gamma_{max}$ (%)	Lat. disp. (in)
18.51	12.13	13.36	2.93	77.55	2.00	0.56	0.00	0.00
18.57	12.37	13.61	2.90	77.73	2.00	1.17	0.00	0.00
18.67	12.54	13.76	2.87	77.68	2.00	1.54	0.00	0.00
18.71	12.82	14.06	2.79	77.30	2.00	2.24	0.00	0.00
18.81	13.01	14.23	2.72	76.81	2.00	2.63	0.00	0.00
18.86	13.15	14.35	2.64	76.04	2.00	2.93	0.00	0.00
18.91	13.20	14.38	2.56	74.98	2.00	2.99	0.00	0.00
18.97	13.23	14.38	2.48	73.92	2.00	2.98	0.00	0.00
19.06	13.28	14.39	2.39	72.81	2.00	3.00	0.00	0.00
19.11	13.35	14.44	2.35	72.28	2.00	3.12	0.00	0.00
19.21	13.59	14.66	2.30	71.98	2.00	3.63	0.00	0.00
19.27	14.02	15.12	2.29	72.63	2.00	4.64	0.00	0.00
19.31	14.78	15.97	2.32	74.33	2.00	6.45	0.00	0.00
19.41	16.02	17.32	2.37	77.15	2.00	9.13	0.00	0.00
19.46	17.53	19.00	2.42	80.48	2.00	12.19	0.00	0.00
19.51	19.45	21.12	2.42	83.35	2.00	15.67	0.00	0.00
19.56	21.37	23.23	2.41	85.96	2.00	18.82	0.00	0.00
19.63	22.73	24.70	2.46	88.73	2.00	20.85	0.00	0.00
19.71	23.86	25.91	2.52	91.41	2.00	22.42	0.00	0.00
19.80	24.54	26.62	2.64	94.40	2.00	23.32	0.00	0.00
19.82	25.00	27.14	2.77	97.46	2.00	23.96	0.00	0.00
19.91	24.70	26.78	2.97	100.50	2.00	23.51	0.00	0.00
19.95	25.51	27.65	3.01	102.41	2.00	24.57	0.00	0.00
20.02	26.21	28.37	3.05	103.99	2.00	25.42	0.00	0.00
20.11	26.74	28.89	3.12	105.99	2.00	26.02	0.00	0.00
20.15	27.33	29.52	3.20	108.26	2.00	26.73	0.00	0.00
20.24	28.50	30.73	3.22	110.30	2.00	28.05	0.00	0.00
20.29	30.11	32.44	3.21	112.35	2.00	29.84	0.00	0.00
20.36	32.24	34.68	3.16	114.39	0.59	32.05	51.20	0.51
20.41	34.37	36.93	3.11	116.15	0.61	34.12	51.20	0.37
20.48	36.70	39.36	3.03	117.57	0.62	36.23	51.20	0.51
20.56	36.71	39.31	3.15	120.01	0.65	36.19	51.20	0.59
20.66	35.87	38.33	3.34	122.64	0.68	35.35	51.20	0.74
20.71	34.56	36.92	3.57	125.21	2.00	34.11	0.00	0.00
20.74	32.81	35.04	3.81	127.16	2.00	32.39	0.00	0.00
20.82	30.71	32.73	4.06	128.02	2.00	30.13	0.00	0.00
20.91	28.18	29.93	4.35	128.26	2.00	27.19	0.00	0.00
20.95	25.20	26.71	4.70	127.59	2.00	23.42	0.00	0.00
21.03	22.22	23.43	5.12	126.25	2.00	19.11	0.00	0.00
21.11	19.51	20.46	5.56	124.37	2.00	14.63	0.00	0.00
21.15	17.79	18.53	5.78	121.46	2.00	11.36	0.00	0.00
21.22	17.08	17.69	5.71	118.28	2.00	9.83	0.00	0.00
21.26	16.89	17.46	5.49	115.41	2.00	9.39	0.00	0.00
21.34	17.65	18.26	5.09	113.47	2.00	10.87	0.00	0.00
21.41	19.06	19.71	4.68	112.40	2.00	13.39	0.00	0.00
21.48	21.43	22.18	4.20	111.65	2.00	17.30	0.00	0.00
21.52	24.31	25.19	3.77	111.09	2.00	21.49	0.00	0.00
21.61	27.48	28.46	3.41	110.44	2.00	25.52	0.00	0.00

:: Estimation of post-earthquake lateral Displacements :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	R_f (%)	$Q_{tn,cs}$	FS	D_r	$Gamma_{max}$ (%)	Lat. disp. (in)
21.66	30.96	32.05	3.09	109.80	2.00	29.45	0.00	0.00
21.76	34.47	35.62	2.86	109.70	2.00	32.92	0.00	0.00
21.81	38.00	39.23	2.69	110.19	2.00	36.12	0.00	0.00
21.85	41.47	42.78	2.55	110.86	2.00	38.98	0.00	0.00
21.92	44.74	46.08	2.44	111.70	2.00	41.43	0.00	0.00
22.01	47.97	49.30	2.37	113.00	2.00	43.66	0.00	0.00
22.09	50.58	51.88	2.32	114.29	0.58	45.34	34.10	0.39
22.12	53.36	54.70	2.29	116.09	0.60	47.09	34.10	0.15
22.20	56.17	57.47	2.26	117.96	0.62	48.72	34.10	0.39
22.29	59.12	60.36	2.23	119.83	0.63	50.34	34.10	0.44
22.31	62.19	63.46	2.19	121.53	0.65	51.99	34.10	0.10
22.40	64.97	66.14	2.15	122.95	0.67	53.36	34.10	0.44
22.45	67.71	68.85	2.12	124.62	0.69	54.68	34.10	0.24
22.51	70.07	71.14	2.10	126.20	0.70	55.76	16.87	0.15
22.60	72.08	73.01	2.07	126.79	0.71	56.62	16.21	0.21
22.64	73.69	74.54	1.99	125.89	0.70	57.30	17.35	0.10
22.75	74.70	75.33	1.91	124.57	0.68	57.65	19.20	0.30
22.80	75.19	75.71	1.86	123.38	0.67	57.81	21.01	0.15
22.85	75.11	75.52	1.82	122.10	0.66	57.73	22.70	0.16
22.91	74.60	74.89	1.80	120.84	0.64	57.45	22.70	0.20
22.99	74.00	74.15	1.81	120.66	0.64	57.13	22.70	0.26
23.08	73.13	73.14	1.84	120.60	0.64	56.67	22.70	0.29
23.10	71.45	71.45	1.90	120.90	0.64	55.90	22.70	0.07
23.18	69.67	69.57	2.00	121.90	2.00	55.02	0.00	0.00
23.26	67.59	67.40	2.16	124.40	2.00	53.98	0.00	0.00
23.30	65.04	64.84	2.35	127.10	2.00	52.70	0.00	0.00
23.37	61.42	61.15	2.55	128.98	2.00	50.76	0.00	0.00
23.46	57.08	56.69	2.76	130.03	2.00	48.27	0.00	0.00
23.51	52.26	51.82	2.98	130.48	2.00	45.30	0.00	0.00
23.56	47.18	46.67	3.15	128.64	2.00	41.85	0.00	0.00
23.63	42.20	41.60	3.30	125.94	2.00	38.05	0.00	0.00
23.72	37.88	37.16	3.36	121.71	2.00	34.32	0.00	0.00
23.79	33.58	32.77	3.41	116.82	2.00	30.18	0.00	0.00
23.87	29.73	28.83	3.42	111.37	2.00	25.95	0.00	0.00
23.91	26.52	25.57	3.36	105.33	2.00	21.99	0.00	0.00
23.96	24.53	23.53	3.20	99.72	2.00	19.24	0.00	0.00
24.02	23.43	22.37	3.03	95.24	2.00	17.58	0.00	0.00
24.11	22.70	21.59	2.89	91.81	2.00	16.40	0.00	0.00
24.20	22.25	21.07	2.82	90.02	2.00	15.60	0.00	0.00
24.22	21.77	20.58	2.80	88.89	2.00	14.83	0.00	0.00
24.31	21.48	20.25	2.79	88.24	2.00	14.28	0.00	0.00
24.39	21.34	20.06	2.79	88.00	2.00	13.98	0.00	0.00
24.42	21.29	20.00	2.79	87.84	2.00	13.88	0.00	0.00
24.51	21.19	19.85	2.77	87.42	2.00	13.62	0.00	0.00
24.55	21.20	19.83	2.73	86.67	2.00	13.60	0.00	0.00
24.63	20.99	19.58	2.67	85.49	2.00	13.18	0.00	0.00
24.71	20.75	19.30	2.61	84.15	2.00	12.71	0.00	0.00
24.75	20.38	18.92	2.55	82.54	2.00	12.04	0.00	0.00

:: Estimation of post-earthquake lateral Displacements :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	R_f (%)	$Q_{tn,cs}$	FS	D_r	$Gamma_{max}$ (%)	Lat. disp. (in)
24.81	19.90	18.40	2.49	80.85	2.00	11.13	0.00	0.00
24.90	19.35	17.82	2.42	79.04	2.00	10.07	0.00	0.00
24.94	18.79	17.25	2.34	76.96	2.00	9.00	0.00	0.00
25.01	18.24	16.67	2.28	75.15	2.00	7.87	0.00	0.00
25.07	17.67	16.09	2.23	73.59	2.00	6.69	0.00	0.00
25.15	17.08	15.48	2.22	72.54	2.00	5.42	0.00	0.00
25.20	16.59	14.97	2.25	72.13	2.00	4.32	0.00	0.00
25.28	16.23	14.59	2.29	72.03	2.00	3.47	0.00	0.00
25.35	16.04	14.38	2.33	72.34	2.00	3.00	0.00	0.00
25.40	16.03	14.36	2.37	72.78	2.00	2.93	0.00	0.00
25.48	16.13	14.42	2.44	73.82	2.00	3.09	0.00	0.00
25.55	16.28	14.54	2.55	75.56	2.00	3.37	0.00	0.00
25.60	16.45	14.69	2.67	77.34	2.00	3.70	0.00	0.00
25.67	16.64	14.85	2.79	79.14	2.00	4.05	0.00	0.00
25.75	16.81	15.00	2.89	80.81	2.00	4.37	0.00	0.00
25.79	16.95	15.12	3.00	82.31	2.00	4.64	0.00	0.00
25.90	17.27	15.38	3.05	83.51	2.00	5.21	0.00	0.00
25.95	17.61	15.69	3.09	84.65	2.00	5.86	0.00	0.00
26.01	17.91	15.95	3.13	85.69	2.00	6.41	0.00	0.00
26.09	18.18	16.17	3.15	86.33	2.00	6.87	0.00	0.00
26.13	18.45	16.42	3.12	86.44	2.00	7.36	0.00	0.00
26.19	18.70	16.64	3.09	86.46	2.00	7.80	0.00	0.00
26.27	19.02	16.91	3.05	86.51	2.00	8.33	0.00	0.00
26.34	19.37	17.21	3.02	86.57	2.00	8.92	0.00	0.00
26.39	19.82	17.61	2.97	86.67	2.00	9.69	0.00	0.00
26.47	20.03	17.78	2.96	86.84	2.00	9.99	0.00	0.00
26.54	20.17	17.88	2.96	87.04	2.00	10.18	0.00	0.00
26.58	20.25	17.94	2.97	87.28	2.00	10.28	0.00	0.00
26.67	20.26	17.90	2.99	87.44	2.00	10.22	0.00	0.00
26.73	20.23	17.85	3.01	87.63	2.00	10.12	0.00	0.00
26.78	20.16	17.76	3.02	87.62	2.00	9.95	0.00	0.00
26.85	20.02	17.59	3.02	87.31	2.00	9.64	0.00	0.00
26.93	19.87	17.41	3.01	86.92	2.00	9.31	0.00	0.00
26.98	19.65	17.18	3.02	86.58	2.00	8.87	0.00	0.00
27.03	19.48	17.00	3.02	86.22	2.00	8.52	0.00	0.00
27.13	19.33	16.82	3.01	85.81	2.00	8.15	0.00	0.00
27.17	19.21	16.68	3.01	85.52	2.00	7.90	0.00	0.00
27.24	19.07	16.52	3.00	85.13	2.00	7.58	0.00	0.00
27.33	18.86	16.29	3.01	84.82	2.00	7.10	0.00	0.00
27.36	18.63	16.05	3.04	84.72	2.00	6.62	0.00	0.00
27.43	18.38	15.79	3.07	84.58	2.00	6.07	0.00	0.00
27.53	18.13	15.51	3.10	84.43	2.00	5.49	0.00	0.00
27.60	17.91	15.28	3.10	84.05	2.00	4.99	0.00	0.00
27.63	17.70	15.07	3.09	83.47	2.00	4.54	0.00	0.00
27.72	17.52	14.87	3.06	82.75	2.00	4.09	0.00	0.00
27.77	17.42	14.76	3.02	81.96	2.00	3.85	0.00	0.00
27.84	17.46	14.77	2.96	81.27	2.00	3.87	0.00	0.00
27.93	17.59	14.85	2.89	80.54	2.00	4.06	0.00	0.00

:: Estimation of post-earthquake lateral Displacements :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	R_f (%)	$Q_{tn,cs}$	FS	D_r	$Gamma_{max}$ (%)	Lat. disp. (in)
27.97	17.75	14.99	2.81	79.83	2.00	4.35	0.00	0.00
28.02	17.89	15.10	2.75	79.27	2.00	4.59	0.00	0.00
28.12	18.02	15.18	2.69	78.68	2.00	4.77	0.00	0.00
28.17	18.17	15.30	2.64	78.11	2.00	5.03	0.00	0.00
28.22	18.28	15.38	2.60	77.72	2.00	5.21	0.00	0.00
28.32	18.30	15.36	2.59	77.57	2.00	5.17	0.00	0.00
28.36	18.44	15.47	2.57	77.50	2.00	5.41	0.00	0.00
28.42	18.88	15.86	2.54	77.73	2.00	6.23	0.00	0.00
28.48	19.31	16.24	2.50	77.88	2.00	7.00	0.00	0.00
28.57	19.74	16.59	2.47	78.01	2.00	7.72	0.00	0.00
28.62	20.26	17.05	2.47	78.69	2.00	8.61	0.00	0.00
28.72	20.70	17.42	2.48	79.51	2.00	9.31	0.00	0.00
28.75	20.99	17.67	2.55	80.80	2.00	9.79	0.00	0.00
28.82	21.18	17.81	2.63	82.31	2.00	10.05	0.00	0.00
28.87	21.43	18.01	2.70	83.55	2.00	10.42	0.00	0.00
28.95	21.50	18.04	2.76	84.52	2.00	10.47	0.00	0.00
29.02	21.16	17.70	2.82	84.88	2.00	9.84	0.00	0.00
29.07	20.75	17.30	2.89	85.13	2.00	9.09	0.00	0.00
29.16	20.35	16.89	2.96	85.34	2.00	8.30	0.00	0.00
29.21	19.87	16.43	3.00	85.00	2.00	7.39	0.00	0.00
29.29	19.55	16.11	2.99	84.30	2.00	6.74	0.00	0.00
29.36	19.41	15.96	2.93	83.25	2.00	6.43	0.00	0.00
29.40	19.63	16.15	2.81	81.96	2.00	6.81	0.00	0.00
29.47	19.93	16.39	2.69	80.76	2.00	7.31	0.00	0.00
29.56	20.29	16.68	2.58	79.82	2.00	7.89	0.00	0.00
29.60	20.70	17.04	2.51	79.35	2.00	8.58	0.00	0.00
29.71	21.12	17.37	2.47	79.22	2.00	9.22	0.00	0.00
29.75	21.53	17.73	2.44	79.29	2.00	9.89	0.00	0.00
29.79	21.94	18.08	2.42	79.51	2.00	10.55	0.00	0.00
29.86	22.27	18.35	2.42	80.05	2.00	11.03	0.00	0.00
29.95	22.60	18.60	2.44	80.71	2.00	11.48	0.00	0.00
30.04	22.87	18.80	2.47	81.39	2.00	11.83	0.00	0.00
30.06	23.16	19.06	2.49	82.09	2.00	12.28	0.00	0.00
30.15	23.46	19.28	2.51	82.82	2.00	12.67	0.00	0.00
30.20	23.80	19.56	2.55	83.76	2.00	13.14	0.00	0.00
30.28	24.21	19.88	2.60	85.00	2.00	13.68	0.00	0.00
30.35	24.55	20.15	2.65	86.18	2.00	14.13	0.00	0.00
30.39	24.85	20.40	2.69	87.23	2.00	14.53	0.00	0.00
30.45	25.09	20.58	2.73	88.07	2.00	14.82	0.00	0.00
30.54	25.24	20.67	2.77	88.84	2.00	14.96	0.00	0.00
30.60	25.09	20.50	2.84	89.73	2.00	14.69	0.00	0.00
30.67	24.78	20.19	2.92	90.39	2.00	14.19	0.00	0.00
30.74	24.41	19.81	2.99	90.80	2.00	13.57	0.00	0.00
30.79	23.91	19.35	3.05	90.92	2.00	12.78	0.00	0.00
30.86	23.34	18.82	3.04	89.92	2.00	11.86	0.00	0.00
30.95	22.81	18.30	3.02	88.68	2.00	10.95	0.00	0.00
30.99	22.25	17.80	2.98	87.32	2.00	10.03	0.00	0.00
31.05	21.70	17.29	2.94	85.85	2.00	9.08	0.00	0.00

:: Estimation of post-earthquake lateral Displacements :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	R_f (%)	$Q_{tn,cs}$	FS	D_r	$Gamma_{max}$ (%)	Lat. disp. (in)
31.14	21.26	16.87	2.87	84.23	2.00	8.27	0.00	0.00
31.19	20.89	16.53	2.79	82.51	2.00	7.60	0.00	0.00
31.26	20.65	16.30	2.71	80.93	2.00	7.13	0.00	0.00
31.34	20.47	16.11	2.62	79.38	2.00	6.74	0.00	0.00
31.39	20.36	16.00	2.53	77.95	2.00	6.52	0.00	0.00
31.45	20.34	15.96	2.50	77.54	2.00	6.44	0.00	0.00
31.54	20.41	15.99	2.47	77.08	2.00	6.50	0.00	0.00
31.57	20.70	16.25	2.40	76.52	2.00	7.02	0.00	0.00
31.63	21.26	16.71	2.35	76.48	2.00	7.95	0.00	0.00
31.73	21.86	17.20	2.32	76.78	2.00	8.90	0.00	0.00
31.77	22.65	17.87	2.30	77.50	2.00	10.16	0.00	0.00
31.84	23.37	18.47	2.30	78.35	2.00	11.25	0.00	0.00
31.93	23.77	18.77	2.35	79.51	2.00	11.79	0.00	0.00
31.98	24.18	19.10	2.38	80.58	2.00	12.36	0.00	0.00
32.05	24.49	19.34	2.40	81.23	2.00	12.76	0.00	0.00
32.09	24.69	19.49	2.44	82.07	2.00	13.02	0.00	0.00
32.17	24.77	19.51	2.51	83.19	2.00	13.06	0.00	0.00
32.22	24.56	19.30	2.57	83.85	2.00	12.71	0.00	0.00
32.32	24.33	19.06	2.62	84.14	2.00	12.29	0.00	0.00
32.35	24.03	18.79	2.64	84.07	2.00	11.82	0.00	0.00
32.43	23.76	18.52	2.65	83.76	2.00	11.34	0.00	0.00
32.52	23.80	18.52	2.61	83.20	2.00	11.34	0.00	0.00
32.57	23.78	18.49	2.58	82.69	2.00	11.28	0.00	0.00
32.62	23.81	18.49	2.55	82.23	2.00	11.29	0.00	0.00
32.71	23.88	18.52	2.51	81.74	2.00	11.33	0.00	0.00
32.76	23.92	18.53	2.48	81.27	2.00	11.36	0.00	0.00
32.82	24.02	18.59	2.47	81.13	2.00	11.47	0.00	0.00
32.90	24.07	18.60	2.46	81.14	2.00	11.49	0.00	0.00
32.96	24.10	18.60	2.48	81.31	2.00	11.48	0.00	0.00
33.02	24.16	18.62	2.50	81.74	2.00	11.52	0.00	0.00
33.11	24.21	18.62	2.53	82.23	2.00	11.53	0.00	0.00
33.17	24.32	18.69	2.56	82.78	2.00	11.64	0.00	0.00
33.22	24.44	18.77	2.59	83.33	2.00	11.78	0.00	0.00
33.31	24.49	18.77	2.62	83.74	2.00	11.78	0.00	0.00
33.34	24.51	18.77	2.64	84.12	2.00	11.78	0.00	0.00
33.41	24.52	18.75	2.65	84.14	2.00	11.74	0.00	0.00
33.49	24.50	18.69	2.66	84.23	2.00	11.65	0.00	0.00
33.57	24.46	18.63	2.67	84.25	2.00	11.53	0.00	0.00
33.61	24.39	18.55	2.66	84.05	2.00	11.39	0.00	0.00
33.68	24.39	18.52	2.65	83.87	2.00	11.34	0.00	0.00
33.76	24.41	18.50	2.65	83.81	2.00	11.31	0.00	0.00
33.81	24.49	18.55	2.66	84.09	2.00	11.39	0.00	0.00
33.88	24.70	18.69	2.69	84.79	2.00	11.64	0.00	0.00
33.95	24.97	18.88	2.75	85.91	2.00	11.97	0.00	0.00
34.01	25.30	19.12	2.82	87.39	2.00	12.39	0.00	0.00
34.06	25.58	19.32	2.91	88.93	2.00	12.74	0.00	0.00
34.13	25.81	19.47	3.00	90.56	2.00	12.99	0.00	0.00
34.21	25.99	19.58	3.13	92.59	2.00	13.17	0.00	0.00

:: Estimation of post-earthquake lateral Displacements :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	R_f (%)	$Q_{tn,cs}$	FS	D_r	$Gamma_{max}$ (%)	Lat. disp. (in)
34.25	26.13	19.66	3.25	94.49	2.00	13.32	0.00	0.00
34.35	26.22	19.68	3.37	96.14	2.00	13.34	0.00	0.00
34.40	26.26	19.68	3.47	97.59	2.00	13.34	0.00	0.00
34.49	26.26	19.62	3.56	98.65	2.00	13.25	0.00	0.00
34.53	26.21	19.56	3.63	99.47	2.00	13.14	0.00	0.00
34.60	26.13	19.45	3.69	100.04	2.00	12.96	0.00	0.00
34.65	26.05	19.36	3.74	100.56	2.00	12.80	0.00	0.00
34.74	26.01	19.28	3.79	101.09	2.00	12.66	0.00	0.00
34.80	25.96	19.21	3.81	101.16	2.00	12.54	0.00	0.00
34.85	25.81	19.06	3.82	100.98	2.00	12.29	0.00	0.00
34.93	25.63	18.87	3.83	100.73	2.00	11.96	0.00	0.00
34.98	25.37	18.64	3.85	100.52	2.00	11.55	0.00	0.00
35.05	25.16	18.43	3.86	100.22	2.00	11.19	0.00	0.00
35.15	24.95	18.22	3.86	99.73	2.00	10.80	0.00	0.00
35.20	24.79	18.07	3.84	99.23	2.00	10.53	0.00	0.00
35.25	24.73	18.00	3.78	98.37	2.00	10.40	0.00	0.00
35.33	24.69	17.94	3.70	97.25	2.00	10.29	0.00	0.00
35.40	24.65	17.88	3.64	96.31	2.00	10.19	0.00	0.00
35.44	24.77	17.97	3.58	95.69	2.00	10.34	0.00	0.00
35.50	24.93	18.08	3.51	95.04	2.00	10.55	0.00	0.00
35.59	25.19	18.26	3.42	94.29	2.00	10.88	0.00	0.00
35.64	25.39	18.41	3.36	93.74	2.00	11.14	0.00	0.00
35.70	25.56	18.52	3.32	93.37	2.00	11.35	0.00	0.00
35.79	25.66	18.57	3.29	93.11	2.00	11.43	0.00	0.00
35.83	25.68	18.57	3.30	93.19	2.00	11.42	0.00	0.00
35.94	25.66	18.50	3.30	93.05	2.00	11.31	0.00	0.00
35.98	25.62	18.45	3.29	92.86	2.00	11.22	0.00	0.00
36.03	25.44	18.29	3.28	92.51	2.00	10.93	0.00	0.00
36.09	25.17	18.05	3.29	92.12	2.00	10.49	0.00	0.00
36.17	24.77	17.69	3.31	91.67	2.00	9.84	0.00	0.00
36.23	24.32	17.31	3.32	91.14	2.00	9.11	0.00	0.00
36.29	23.82	16.88	3.33	90.37	2.00	8.28	0.00	0.00
36.38	23.31	16.44	3.32	89.39	2.00	7.41	0.00	0.00
36.44	22.79	16.01	3.30	88.30	2.00	6.53	0.00	0.00
36.49	22.27	15.58	3.29	87.26	2.00	5.64	0.00	0.00
36.59	21.81	15.17	3.27	86.23	2.00	4.77	0.00	0.00
36.63	21.37	14.82	3.25	85.28	2.00	3.98	0.00	0.00
36.69	21.03	14.53	3.23	84.42	2.00	3.33	0.00	0.00
36.78	20.84	14.35	3.19	83.57	2.00	2.93	0.00	0.00
36.82	20.75	14.28	3.14	82.81	2.00	2.75	0.00	0.00
36.88	20.77	14.28	3.09	82.14	2.00	2.75	0.00	0.00
36.98	20.81	14.28	3.04	81.57	2.00	2.76	0.00	0.00
37.02	20.88	14.33	2.99	81.09	2.00	2.87	0.00	0.00
37.11	20.95	14.36	2.95	80.71	2.00	2.94	0.00	0.00
37.18	21.00	14.38	2.93	80.40	2.00	2.98	0.00	0.00
37.22	21.09	14.44	2.91	80.31	2.00	3.12	0.00	0.00
37.28	21.20	14.50	2.91	80.51	2.00	3.27	0.00	0.00
37.38	21.34	14.58	2.94	80.94	2.00	3.44	0.00	0.00

:: Estimation of post-earthquake lateral Displacements :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	R_f (%)	$Q_{tn,cs}$	FS	D_r	$Gamma_{max}$ (%)	Lat. disp. (in)
37.42	21.53	14.71	2.96	81.52	2.00	3.73	0.00	0.00
37.48	21.73	14.84	2.99	82.15	2.00	4.03	0.00	0.00
37.57	21.96	14.99	2.99	82.37	2.00	4.36	0.00	0.00
37.62	22.23	15.19	2.94	82.24	2.00	4.79	0.00	0.00
37.68	22.47	15.36	2.92	82.23	2.00	5.16	0.00	0.00
37.77	22.71	15.51	2.92	82.51	2.00	5.49	0.00	0.00
37.82	22.94	15.67	2.91	82.75	2.00	5.83	0.00	0.00
37.88	23.12	15.79	2.89	82.68	2.00	6.09	0.00	0.00
37.96	23.17	15.81	2.87	82.50	2.00	6.11	0.00	0.00
38.00	23.39	15.98	2.83	82.25	2.00	6.47	0.00	0.00
38.08	23.81	16.29	2.75	81.76	2.00	7.10	0.00	0.00
38.12	24.25	16.62	2.69	81.46	2.00	7.77	0.00	0.00
38.20	24.73	16.97	2.64	81.32	2.00	8.46	0.00	0.00
38.27	25.09	17.24	2.61	81.32	2.00	8.97	0.00	0.00
38.36	25.41	17.46	2.58	81.20	2.00	9.39	0.00	0.00
38.40	25.70	17.66	2.58	81.62	2.00	9.78	0.00	0.00
38.46	26.47	18.23	2.62	83.02	2.00	10.82	0.00	0.00
38.56	27.70	19.15	2.62	84.43	2.00	12.44	0.00	0.00
38.59	29.37	20.44	2.62	86.38	2.00	14.59	0.00	0.00
38.66	31.20	21.82	2.65	88.94	2.00	16.76	0.00	0.00
38.76	33.40	23.47	2.72	92.37	2.00	19.16	0.00	0.00
38.79	35.50	25.07	2.82	96.19	2.00	21.33	0.00	0.00
38.87	37.72	26.74	2.91	100.07	2.00	23.46	0.00	0.00
38.91	40.14	28.57	3.02	104.53	2.00	25.64	0.00	0.00
39.00	42.72	30.49	3.11	108.61	2.00	27.80	0.00	0.00
39.04	45.10	32.30	3.18	112.39	2.00	29.70	0.00	0.00
39.11	47.29	33.92	3.32	117.11	2.00	31.31	0.00	0.00
39.20	48.94	35.08	3.50	122.18	2.00	32.42	0.00	0.00
39.24	50.53	36.22	3.69	127.28	2.00	33.48	0.00	0.00
39.31	52.73	37.81	3.88	133.19	2.00	34.90	0.00	0.00
39.38	55.69	39.99	4.05	139.41	2.00	36.75	0.00	0.00
39.46	60.04	43.26	4.12	145.48	2.00	39.34	0.00	0.00
39.51	65.29	47.26	4.16	151.76	0.98	42.26	8.63	0.00
39.60	70.72	51.35	4.18	157.81	2.00	45.00	0.00	0.00
39.66	76.31	55.62	4.17	163.13	2.00	47.64	0.00	0.00
39.71	81.88	59.90	4.12	167.53	2.00	50.09	0.00	0.00
39.79	87.58	64.26	4.07	171.54	2.00	52.40	0.00	0.00
39.85	95.63	70.52	3.93	175.53	2.00	55.47	0.00	0.00
39.91	106.85	79.35	3.70	179.41	2.00	59.37	0.00	0.00
39.99	119.15	89.06	3.47	183.29	2.00	63.18	0.00	0.00
40.05	129.29	97.07	3.33	187.43	2.00	66.02	0.00	0.00
40.11	136.78	102.96	3.26	191.07	2.00	67.96	0.00	0.00
40.20	143.19	107.89	3.21	194.51	1.85	69.51	0.54	0.00
40.25	148.57	112.05	3.20	198.24	1.95	70.76	0.47	0.00
40.30	153.54	115.86	3.21	202.36	2.00	71.86	0.00	0.00
40.40	158.28	119.33	3.23	206.73	2.00	72.83	0.00	0.00
40.43	160.83	121.18	3.29	210.64	2.00	73.34	0.00	0.00
40.49	158.66	119.18	3.40	212.23	2.00	72.79	0.00	0.00

:: Estimation of post-earthquake lateral Displacements :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	R_f (%)	$Q_{tn,cs}$	FS	D_r	$Gamma_{max}$ (%)	Lat. disp. (in)
40.55	153.03	114.40	3.58	212.96	2.00	71.44	0.00	0.00
40.64	146.29	108.69	3.77	213.19	2.00	69.75	0.00	0.00
40.69	139.08	102.89	3.85	209.39	2.00	67.94	0.00	0.00
40.80	131.58	96.75	3.94	205.56	2.00	65.91	0.00	0.00
40.84	124.38	91.04	4.02	201.42	2.00	63.90	0.00	0.00
40.89	117.63	85.72	4.05	196.43	1.90	61.91	0.21	0.00
40.96	111.06	80.55	4.06	190.55	1.75	59.86	0.30	0.00
41.04	102.35	73.71	4.13	184.44	1.61	56.93	0.44	0.00
41.10	99.25	71.35	4.00	178.24	1.47	55.86	0.65	0.00
41.15	97.87	70.36	3.81	172.25	1.35	55.40	0.96	0.00
41.24	97.68	70.24	3.60	166.66	1.24	55.34	1.39	0.00
41.28	99.20	71.40	3.54	166.12	1.23	55.88	1.44	0.00
41.38	101.83	73.35	3.43	165.46	1.22	56.77	1.50	0.00
41.41	104.74	75.62	3.34	165.26	1.21	57.78	1.52	0.00
41.49	107.45	77.66	3.25	165.11	1.21	58.65	1.54	0.00
41.54	110.57	80.08	3.15	164.61	1.20	59.67	1.59	0.00
41.61	115.81	84.17	2.99	164.14	1.19	61.31	1.64	0.00
41.69	117.25	85.22	2.93	163.47	1.18	61.72	1.71	0.00
41.77	119.86	87.23	2.83	162.49	1.16	62.49	1.83	0.00
41.84	123.49	90.09	2.70	161.41	1.15	63.55	1.96	0.00
41.88	127.85	93.59	2.56	160.50	1.13	64.81	2.09	0.00
41.94	131.93	96.89	2.43	159.54	1.11	65.96	2.35	0.00
42.04	134.67	99.03	2.32	158.18	1.09	66.68	2.49	0.00
42.08	136.97	100.92	2.23	157.19	1.07	67.30	2.61	0.00
42.17	138.21	101.83	2.18	156.42	1.06	67.60	2.70	0.00
42.19	138.80	102.31	2.15	155.99	1.05	67.76	2.75	0.00
42.28	138.18	101.67	2.15	155.46	1.05	67.55	2.81	0.00
42.33	136.34	100.08	2.19	155.19	1.04	67.02	2.85	0.00
42.39	134.30	98.29	2.24	155.17	1.04	66.43	2.85	0.00
42.48	131.81	96.09	2.31	155.16	1.04	65.68	2.85	0.00
42.53	129.20	93.85	2.39	155.50	1.05	64.91	2.92	0.00
42.59	127.38	92.22	2.47	156.51	1.06	64.33	2.72	0.00
42.67	125.63	90.61	2.56	157.58	1.08	63.74	2.52	0.00
42.73	123.71	88.91	2.65	158.66	1.10	63.12	2.34	0.00
42.81	122.02	87.35	2.73	159.78	1.12	62.54	2.16	0.00
42.88	120.34	85.85	2.82	160.92	1.14	61.96	2.00	0.00
42.92	118.62	84.36	2.91	162.09	1.16	61.39	1.84	0.00
43.00	116.94	82.86	3.00	163.09	1.18	60.80	1.72	0.00
43.08	115.33	81.42	3.08	164.14	1.20	60.22	1.60	0.00
43.12	113.76	80.08	3.17	165.17	1.22	59.67	1.49	0.00
43.21	112.31	78.78	3.24	165.99	1.23	59.13	1.41	0.00
43.27	110.92	77.57	3.32	166.88	1.25	58.61	1.33	0.00
43.32	109.66	76.47	3.40	167.89	1.27	58.15	1.24	0.00
43.39	108.32	75.29	3.48	168.83	1.29	57.63	1.16	0.00
43.47	106.67	73.88	3.56	169.61	1.31	57.01	1.10	0.00
43.52	104.14	71.84	3.66	169.87	1.31	56.09	1.08	0.00
43.59	100.71	69.13	3.76	169.67	1.31	54.81	0.76	0.00
43.67	95.95	65.41	3.91	168.99	1.29	52.99	0.81	0.00

:: Estimation of post-earthquake lateral Displacements :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	R_f (%)	$Q_{tn,cs}$	FS	D_r	$Gamma_{max}$ (%)	Lat. disp. (in)
43.72	90.92	61.58	4.04	167.69	1.27	51.00	0.92	0.00
43.80	85.34	57.38	4.13	164.49	1.21	48.67	1.25	0.00
43.85	79.27	52.89	4.21	160.68	1.14	45.98	1.81	0.00
43.92	73.36	48.52	4.29	156.49	1.07	43.13	0.00	0.00
43.97	67.07	43.93	4.39	151.94	2.00	39.85	0.00	0.00
44.04	60.96	39.49	4.47	146.78	2.00	36.34	0.00	0.00
44.13	55.89	35.84	4.49	141.26	2.00	33.13	0.00	0.00
44.17	51.45	32.70	4.44	135.24	2.00	30.11	0.00	0.00
44.24	48.10	30.35	4.30	129.08	2.00	27.64	0.00	0.00
44.31	44.77	28.03	4.18	123.05	2.00	25.01	0.00	0.00
44.37	41.91	26.01	4.12	118.63	2.00	22.55	0.00	0.00
44.45	39.66	24.44	4.03	114.39	2.00	20.49	0.00	0.00
44.50	37.60	23.02	3.88	109.69	2.00	18.52	0.00	0.00
44.56	35.90	21.87	3.68	104.78	2.00	16.82	0.00	0.00
44.65	34.31	20.77	3.51	100.36	2.00	15.13	0.00	0.00
44.71	32.87	19.79	3.38	96.76	2.00	13.52	0.00	0.00
44.76	31.94	19.15	3.31	94.64	2.00	12.44	0.00	0.00
44.85	31.50	18.82	3.26	93.38	2.00	11.87	0.00	0.00
44.88	31.89	19.08	3.25	93.73	2.00	12.32	0.00	0.00
44.96	33.14	19.89	3.30	95.77	2.00	13.70	0.00	0.00
45.05	34.91	21.05	3.37	98.87	2.00	15.57	0.00	0.00
45.10	37.96	23.13	3.40	102.79	2.00	18.68	0.00	0.00
45.17	42.19	26.02	3.41	107.56	2.00	22.57	0.00	0.00
45.25	47.02	29.34	3.39	112.20	2.00	26.52	0.00	0.00
45.30	52.22	32.95	3.36	116.82	2.00	30.36	0.00	0.00
45.37	57.78	36.82	3.33	121.32	0.61	34.02	51.20	0.00
45.45	63.35	40.70	3.32	126.01	0.66	37.33	51.20	0.00
45.49	68.76	44.49	3.32	130.44	0.71	40.27	51.20	0.00
45.54	73.67	47.92	3.33	134.70	0.76	42.72	51.20	0.00
45.61	77.83	50.78	3.36	138.84	0.81	44.63	50.44	0.00
45.68	80.57	52.60	3.43	142.61	0.86	45.79	10.74	0.00
45.75	81.52	53.13	3.53	145.41	0.90	46.13	8.02	0.00
45.80	81.02	52.66	3.62	147.01	0.93	45.83	6.79	0.00
45.89	79.02	51.09	3.72	147.36	0.93	44.83	20.04	0.00
45.93	75.96	48.83	3.82	146.80	0.93	43.34	22.08	0.00
46.01	71.99	45.92	3.92	145.23	0.90	41.31	27.76	0.00
46.08	67.58	42.73	4.03	143.16	2.00	38.94	0.00	0.00
46.15	63.04	39.49	4.13	140.53	2.00	36.33	0.00	0.00
46.20	58.87	36.55	4.19	137.15	2.00	33.78	0.00	0.00
46.29	55.12	33.92	4.21	133.38	2.00	31.31	0.00	0.00
46.34	52.58	32.18	4.14	129.41	2.00	29.58	0.00	0.00
46.41	51.11	31.17	4.05	126.27	2.00	28.53	0.00	0.00
46.49	50.54	30.77	3.95	124.04	2.00	28.10	0.00	0.00
46.53	50.02	30.42	3.89	122.34	2.00	27.72	0.00	0.00
46.60	49.69	30.18	3.82	120.82	2.00	27.46	0.00	0.00
46.69	49.41	29.96	3.75	119.37	2.00	27.22	0.00	0.00
46.73	49.11	29.76	3.69	118.07	2.00	26.99	0.00	0.00
46.79	48.28	29.16	3.69	117.13	2.00	26.33	0.00	0.00

:: Estimation of post-earthquake lateral Displacements :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	R_f (%)	$Q_{tn,cs}$	FS	D_r	$Gamma_{max}$ (%)	Lat. disp. (in)
46.89	47.27	28.41	3.71	116.30	2.00	25.47	0.00	0.00
46.94	45.73	27.31	3.81	116.20	2.00	24.16	0.00	0.00
46.99	44.21	26.21	3.99	117.04	2.00	22.80	0.00	0.00
47.09	42.89	25.21	4.18	118.10	2.00	21.52	0.00	0.00
47.13	41.81	24.41	4.37	119.40	2.00	20.46	0.00	0.00
47.19	42.93	25.12	4.40	121.09	2.00	21.40	0.00	0.00
47.28	44.62	26.20	4.37	122.72	2.00	22.79	0.00	0.00
47.34	47.80	28.32	4.25	124.80	2.00	25.36	0.00	0.00
47.38	54.01	32.56	3.97	127.10	2.00	29.97	0.00	0.00
47.50	61.85	37.94	3.65	129.13	2.00	35.01	0.00	0.00
47.51	72.72	45.60	3.29	131.32	2.00	41.08	0.00	0.00
47.60	84.57	54.02	2.97	133.24	2.00	46.67	0.00	0.00
47.69	97.97	63.68	2.69	135.74	2.00	52.10	0.00	0.00
47.70	112.59	74.42	2.45	139.45	2.00	57.25	0.00	0.00
47.80	125.94	84.20	2.29	143.67	2.00	61.32	0.00	0.00
47.84	139.39	94.21	2.15	148.64	2.00	65.03	0.00	0.00
47.91	151.60	103.34	2.03	153.39	2.00	68.08	0.00	0.00
48.00	161.22	110.51	1.95	157.32	2.00	70.30	0.00	0.00
48.04	168.84	116.26	1.89	160.83	2.00	71.97	0.00	0.00
48.11	173.11	119.39	1.86	162.82	1.21	72.85	1.86	0.00
48.19	175.86	121.33	1.85	164.25	1.23	73.38	1.74	0.00
48.23	176.73	121.85	1.86	165.07	1.25	73.52	1.68	0.00
48.30	176.31	121.32	1.89	165.40	1.26	73.38	1.65	0.00
48.40	175.47	120.40	1.92	165.61	1.26	73.13	1.64	0.00
48.45	174.20	119.22	1.97	165.83	1.27	72.80	1.62	0.00
48.50	172.99	118.09	2.01	166.15	1.27	72.49	1.59	0.00
48.59	172.02	117.09	2.05	166.44	1.28	72.21	1.57	0.00
48.66	171.41	116.42	2.08	166.75	1.29	72.02	1.55	0.00
48.69	171.02	116.01	2.10	167.02	1.29	71.90	1.53	0.00
48.78	170.78	115.63	2.11	167.11	1.29	71.79	1.52	0.00
48.85	170.69	115.43	2.12	167.08	1.29	71.74	1.52	0.00
48.89	170.46	115.19	2.12	166.89	1.29	71.67	1.53	0.00
48.98	170.14	114.81	2.12	166.50	1.28	71.56	1.56	0.00
49.03	169.85	114.51	2.12	166.24	1.28	71.47	1.57	0.00
49.09	170.04	114.53	2.12	166.41	1.28	71.48	1.56	0.00
49.19	170.33	114.54	2.13	166.69	1.29	71.48	1.54	0.00
49.23	170.93	114.85	2.15	167.48	1.30	71.57	1.48	0.00
49.28	172.83	116.08	2.16	169.12	1.34	71.92	1.38	0.00
49.39	175.13	117.50	2.18	170.85	1.37	72.32	1.28	0.00
49.42	177.65	119.21	2.19	172.90	1.42	72.80	1.17	0.00
49.49	180.57	121.19	2.19	174.81	1.46	73.34	1.07	0.00
49.59	183.31	123.06	2.17	175.79	1.48	73.85	1.03	0.00
49.62	185.69	124.84	2.14	176.44	1.50	74.32	1.00	0.00
49.69	187.40	126.08	2.10	176.46	1.50	74.65	1.00	0.00
49.74	188.52	127.02	2.04	175.46	1.48	74.89	1.04	0.00
49.83	188.92	127.47	1.97	173.39	1.43	75.01	1.53	0.00
49.88	187.83	126.90	1.89	170.54	1.37	74.86	1.28	0.00
49.93	185.76	125.55	1.83	167.52	1.31	74.51	1.46	0.00

:: Estimation of post-earthquake lateral Displacements :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	R_f (%)	$Q_{tn,cs}$	FS	D_r	$Gamma_{max}$ (%)	Lat. disp. (in)
50.03	183.09	123.66	1.78	164.16	2.00	74.01	0.00	0.00
50.13	179.38	120.92	1.75	160.78	2.00	73.27	0.00	0.00
50.14	175.33	117.93	1.76	158.34	2.00	72.44	0.00	0.00
50.23	171.23	114.71	1.78	156.17	2.00	71.53	0.00	0.00
50.27	166.80	111.30	1.82	154.26	2.00	70.53	0.00	0.00
50.34	161.56	107.09	1.91	153.13	2.00	69.26	0.00	0.00
50.43	155.42	102.13	2.04	152.59	2.00	67.70	0.00	0.00
50.49	148.95	97.05	2.17	152.09	2.00	66.01	0.00	0.00
50.53	142.05	91.83	2.28	150.66	2.00	64.19	0.00	0.00
50.62	134.51	86.16	2.40	148.86	2.00	62.08	0.00	0.00
50.68	127.42	80.95	2.49	146.80	2.00	60.02	0.00	0.00
50.73	120.26	75.84	2.55	143.66	2.00	57.87	0.00	0.00
50.82	113.01	70.70	2.59	139.77	2.00	55.55	0.00	0.00
50.88	106.07	65.87	2.60	135.47	2.00	53.22	0.00	0.00
50.93	99.91	61.68	2.57	130.70	2.00	51.05	0.00	0.00
51.02	94.44	57.95	2.52	125.94	2.00	48.99	0.00	0.00
51.09	89.17	54.38	2.49	121.63	2.00	46.89	0.00	0.00
51.12	83.92	50.82	2.49	118.24	2.00	44.66	0.00	0.00
51.19	78.60	47.16	2.52	115.41	2.00	42.20	0.00	0.00
51.28	73.22	43.44	2.60	113.38	2.00	39.48	0.00	0.00
51.32	68.33	40.10	2.69	111.88	2.00	36.84	0.00	0.00
51.39	64.21	37.28	2.75	110.12	2.00	34.43	0.00	0.00
51.48	60.31	34.64	2.82	108.49	2.00	32.01	0.00	0.00
51.53	56.31	31.96	2.91	107.03	2.00	29.35	0.00	0.00
51.62	52.17	29.22	2.97	104.75	2.00	26.40	0.00	0.00
51.68	48.21	26.65	3.00	101.81	2.00	23.36	0.00	0.00
51.73	45.05	24.64	2.98	98.61	2.00	20.77	0.00	0.00
51.82	42.62	23.13	2.87	94.59	2.00	18.68	0.00	0.00
51.87	40.63	21.96	2.66	89.44	2.00	16.96	0.00	0.00
51.92	38.75	20.83	2.50	85.24	2.00	15.23	0.00	0.00
51.97	36.63	19.52	2.42	82.16	2.00	13.08	0.00	0.00
52.04	34.50	18.20	2.35	79.17	2.00	10.76	0.00	0.00
52.12	32.86	17.19	2.26	76.28	2.00	8.87	0.00	0.00
52.18	31.94	16.63	2.17	74.17	2.00	7.78	0.00	0.00
52.23	31.17	16.17	2.09	72.25	2.00	6.86	0.00	0.00
52.31	30.59	15.81	2.02	70.63	2.00	6.13	0.00	0.00
52.37	30.00	15.45	1.98	69.47	2.00	5.36	0.00	0.00
52.44	29.15	14.92	1.96	68.42	2.00	4.20	0.00	0.00
52.53	28.21	14.32	1.93	67.11	2.00	2.85	0.00	0.00
52.57	27.07	13.61	1.91	65.80	2.00	1.18	0.00	0.00
52.64	25.80	12.83	1.89	64.33	2.00	0.00	0.00	0.00
52.72	24.50	12.02	1.87	62.73	2.00	0.00	0.00	0.00
52.78	23.17	11.20	1.85	61.00	2.00	0.00	0.00	0.00
52.83	21.95	10.48	1.78	58.82	2.00	0.00	0.00	0.00
52.93	20.80	9.79	1.70	56.64	2.00	0.00	0.00	0.00
52.96	19.98	9.31	1.62	54.75	2.00	0.00	0.00	0.00
53.04	19.46	9.00	1.56	53.36	2.00	0.00	0.00	0.00
53.12	19.06	8.76	1.50	52.22	2.00	0.00	0.00	0.00

:: Estimation of post-earthquake lateral Displacements :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	R_f (%)	$Q_{tn,cs}$	FS	D_r	$Gamma_{max}$ (%)	Lat. disp. (in)
53.17	18.87	8.66	1.45	51.39	2.00	0.00	0.00	0.00
53.22	18.81	8.63	1.42	50.85	2.00	0.00	0.00	0.00
53.29	18.81	8.63	1.38	50.31	2.00	0.00	0.00	0.00
53.37	18.84	8.64	1.35	49.99	2.00	0.00	0.00	0.00
53.42	18.86	8.64	1.37	50.29	2.00	0.00	0.00	0.00
53.49	18.87	8.63	1.38	50.42	2.00	0.00	0.00	0.00
53.58	18.87	8.62	1.37	50.25	2.00	0.00	0.00	0.00
53.63	18.86	8.62	1.35	49.93	2.00	0.00	0.00	0.00
53.68	18.86	8.62	1.33	49.62	2.00	0.00	0.00	0.00
53.78	18.86	8.61	1.30	49.21	2.00	0.00	0.00	0.00
53.84	18.85	8.61	1.27	48.88	2.00	0.00	0.00	0.00
53.88	18.83	8.59	1.26	48.64	2.00	0.00	0.00	0.00
53.94	18.84	8.60	1.24	48.39	2.00	0.00	0.00	0.00
54.03	18.88	8.61	1.23	48.30	2.00	0.00	0.00	0.00
54.08	18.95	8.65	1.23	48.29	2.00	0.00	0.00	0.00
54.16	19.04	8.69	1.24	48.52	2.00	0.00	0.00	0.00
54.20	19.16	8.75	1.25	48.76	2.00	0.00	0.00	0.00
54.28	19.40	8.88	1.24	48.91	2.00	0.00	0.00	0.00
54.35	19.73	9.07	1.23	49.08	2.00	0.00	0.00	0.00
54.43	20.10	9.29	1.22	49.24	2.00	0.00	0.00	0.00
54.48	20.43	9.48	1.20	49.24	2.00	0.00	0.00	0.00
54.55	20.63	9.61	1.18	49.16	2.00	0.00	0.00	0.00
54.63	20.78	9.69	1.17	48.99	2.00	0.00	0.00	0.00
54.67	20.84	9.73	1.15	48.82	2.00	0.00	0.00	0.00
54.74	20.86	9.74	1.12	48.33	2.00	0.00	0.00	0.00
54.82	20.83	9.72	1.09	47.83	2.00	0.00	0.00	0.00
54.87	20.69	9.64	1.07	47.41	2.00	0.00	0.00	0.00
54.92	20.46	9.49	1.06	47.15	2.00	0.00	0.00	0.00
55.02	20.18	9.31	1.07	46.96	2.00	0.00	0.00	0.00
55.06	19.93	9.14	1.10	47.27	2.00	0.00	0.00	0.00
55.14	19.85	9.06	1.15	47.81	2.00	0.00	0.00	0.00
55.22	19.85	9.03	1.20	48.59	2.00	0.00	0.00	0.00
55.27	20.07	9.13	1.26	49.60	2.00	0.00	0.00	0.00
55.37	20.38	9.28	1.34	50.87	2.00	0.00	0.00	0.00
55.42	20.73	9.45	1.41	52.18	2.00	0.00	0.00	0.00
55.47	21.01	9.58	1.48	53.37	2.00	0.00	0.00	0.00
55.53	21.18	9.65	1.54	54.26	2.00	0.00	0.00	0.00
55.58	21.32	9.71	1.58	54.99	2.00	0.00	0.00	0.00
55.67	21.43	9.75	1.60	55.30	2.00	0.00	0.00	0.00
55.72	21.47	9.77	1.60	55.36	2.00	0.00	0.00	0.00
55.81	21.47	9.76	1.59	55.13	2.00	0.00	0.00	0.00
55.86	21.33	9.68	1.56	54.58	2.00	0.00	0.00	0.00
55.92	21.20	9.60	1.55	54.29	2.00	0.00	0.00	0.00
56.01	21.13	9.54	1.55	54.26	2.00	0.00	0.00	0.00
56.05	21.34	9.65	1.57	54.73	2.00	0.00	0.00	0.00
56.11	21.83	9.91	1.64	56.06	2.00	0.00	0.00	0.00
56.21	22.16	10.04	1.76	57.94	2.00	0.00	0.00	0.00
56.26	22.93	10.44	1.89	60.32	2.00	0.00	0.00	0.00

:: Estimation of post-earthquake lateral Displacements :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	R_f (%)	$Q_{tn,cs}$	FS	D_r	$Gamma_{max}$ (%)	Lat. disp. (in)
56.32	24.21	11.14	2.02	63.19	2.00	0.00	0.00	0.00
56.41	25.83	12.03	2.12	66.12	2.00	0.00	0.00	0.00
56.46	27.60	13.03	2.20	68.96	2.00	0.00	0.00	0.00
56.50	29.45	14.10	2.23	71.15	2.00	2.34	0.00	0.00
56.59	31.25	15.12	2.26	73.31	2.00	4.66	0.00	0.00
56.65	32.82	16.01	2.32	75.45	2.00	6.54	0.00	0.00
56.70	34.20	16.78	2.41	78.08	2.00	8.07	0.00	0.00
56.78	36.90	18.34	2.43	80.75	2.00	11.03	0.00	0.00
56.85	39.96	20.15	2.44	83.47	2.00	14.12	0.00	0.00
56.89	43.42	22.21	2.44	86.30	2.00	17.34	0.00	0.00
56.98	46.67	24.13	2.47	89.17	2.00	20.08	0.00	0.00
57.04	49.64	25.88	2.52	92.28	2.00	22.38	0.00	0.00
57.09	52.24	27.37	2.61	95.85	2.00	24.23	0.00	0.00
57.16	54.64	28.73	2.70	99.15	2.00	25.83	0.00	0.00
57.24	57.27	30.26	2.75	101.95	2.00	27.55	0.00	0.00
57.29	60.78	32.45	2.68	103.21	2.00	29.85	0.00	0.00
57.37	63.44	34.10	2.61	103.78	2.00	31.48	0.00	0.00
57.42	65.25	35.24	2.56	103.95	2.00	32.57	0.00	0.00
57.49	65.85	35.59	2.54	103.82	2.00	32.90	0.00	0.00
57.59	66.05	35.68	2.51	103.46	2.00	32.99	0.00	0.00
57.64	65.55	35.37	2.49	102.67	2.00	32.69	0.00	0.00
57.69	64.18	34.52	2.46	101.10	2.00	31.90	0.00	0.00
57.77	62.46	33.48	2.41	98.82	2.00	30.88	0.00	0.00
57.82	59.62	31.73	2.37	96.27	2.00	29.11	0.00	0.00
57.89	55.11	28.91	2.41	93.85	2.00	26.04	0.00	0.00
57.97	50.06	25.76	2.48	91.40	2.00	22.23	0.00	0.00
58.03	44.69	22.48	2.55	88.53	2.00	17.73	0.00	0.00
58.09	39.45	19.34	2.60	84.77	2.00	12.77	0.00	0.00
58.17	34.44	16.39	2.62	80.43	2.00	7.31	0.00	0.00
58.21	30.20	13.95	2.60	75.82	2.00	1.99	0.00	0.00
58.28	27.04	12.17	2.52	71.37	2.00	0.00	0.00	0.00
58.37	24.54	10.77	2.49	68.16	2.00	0.00	0.00	0.00
58.40	22.95	9.96	2.49	66.27	2.00	0.00	0.00	0.00
58.48	22.15	9.54	2.59	66.39	2.00	0.00	0.00	0.00
58.53	22.64	9.78	2.68	67.91	2.00	0.00	0.00	0.00
58.63	24.67	10.80	2.63	69.73	2.00	0.00	0.00	0.00
58.67	27.06	12.07	2.57	71.85	2.00	0.00	0.00	0.00
58.73	29.10	13.23	2.55	73.85	2.00	0.23	0.00	0.00
58.82	30.69	14.10	2.57	75.70	2.00	2.33	0.00	0.00
58.89	31.56	14.56	2.60	77.01	2.00	3.41	0.00	0.00
58.93	31.85	14.72	2.60	77.30	2.00	3.76	0.00	0.00
59.00	31.94	14.76	2.57	76.96	2.00	3.86	0.00	0.00
59.06	31.98	14.82	2.44	75.29	2.00	3.99	0.00	0.00
59.13	30.97	14.30	2.28	72.23	2.00	2.80	0.00	0.00
59.22	28.79	13.06	2.22	69.22	2.00	0.00	0.00	0.00
59.28	26.42	11.72	2.18	66.38	2.00	0.00	0.00	0.00
59.33	24.42	10.60	2.13	63.61	2.00	0.00	0.00	0.00
59.41	23.06	9.86	2.04	61.04	2.00	0.00	0.00	0.00

:: Estimation of post-earthquake lateral Displacements :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	R_f (%)	$Q_{tn,cs}$	FS	D_r	$Gamma_{max}$ (%)	Lat. disp. (in)
59.47	22.47	9.55	1.94	59.23	2.00	0.00	0.00	0.00
59.52	22.50	9.59	1.84	58.08	2.00	0.00	0.00	0.00
59.61	22.85	9.81	1.74	57.18	2.00	0.00	0.00	0.00
59.67	23.26	10.05	1.68	56.84	2.00	0.00	0.00	0.00
59.72	23.81	10.35	1.68	57.41	2.00	0.00	0.00	0.00
59.78	24.44	10.69	1.70	58.31	2.00	0.00	0.00	0.00
59.87	25.08	11.02	1.72	59.13	2.00	0.00	0.00	0.00
59.92	25.83	11.52	1.52	57.00	2.00	0.00	0.00	0.00
60.00	26.38	11.92	1.34	54.71	2.00	0.00	0.00	0.00
60.05	26.95	12.34	1.15	52.22	2.00	0.00	0.00	0.00
60.11	27.25	12.61	0.98	49.42	2.00	0.00	0.00	0.00
60.21	27.38	12.81	0.81	46.28	2.00	0.00	0.00	0.00
60.25	27.51	13.05	0.63	42.60	2.00	0.00	0.00	0.00
60.31	27.68	13.38	0.43	37.95	2.00	0.61	0.00	0.00
60.40	27.58	13.65	0.21	32.18	2.00	1.27	0.00	0.00
60.43	27.43	N/A	0.00	-1.00	2.00	0.00	0.00	0.00
60.51	27.37	N/A	0.00	-1.00	2.00	0.00	0.00	0.00

Total estimated displacement: 6.76

Abbreviations

q_t: Total cone resistance
Q_{tn}: Adjusted cone resistance to an effective overburden stress of 1 atm
R_f: Friction ration
$Q_{tn,cs}$: Adjusted and corrected cone resistance due to fines
FS: Calculated factor of safety against liquefaction
D_r: Calculated relative density
$Gamma_{max}$: Calculated maximum cyclic shear strain
Lat. disp.: Lateral displacement

:: Strength loss calculation (Robertson (2009) ::

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
0.10	49.56	79.61	1.20	95.18	1.91	N/A	N/A
0.15	58.10	93.33	1.16	108.18	1.87	N/A	N/A
0.23	73.22	117.62	1.10	129.38	1.79	N/A	N/A
0.30	87.93	141.25	1.05	148.50	1.72	N/A	N/A
0.34	102.61	164.82	1.00	164.76	1.64	N/A	N/A
0.39	122.42	196.64	1.00	196.64	1.57	N/A	N/A
0.50	138.33	222.19	1.00	222.19	1.53	N/A	N/A
0.53	149.90	240.79	1.00	240.79	1.51	N/A	N/A
0.60	156.28	251.04	1.00	251.04	1.50	N/A	N/A
0.69	161.75	259.81	1.00	259.81	1.50	N/A	N/A
0.72	165.78	266.28	1.00	266.28	1.50	N/A	N/A
0.80	157.82	253.48	1.00	253.48	1.54	N/A	N/A
0.87	146.07	234.60	1.00	234.60	1.60	N/A	N/A
0.92	130.10	208.94	1.02	213.65	1.68	N/A	N/A
1.00	112.06	179.95	1.09	196.18	1.78	N/A	N/A
1.08	96.24	154.52	1.17	180.26	1.88	N/A	N/A
1.12	83.03	133.29	1.26	167.79	1.97	N/A	N/A
1.20	73.32	117.68	1.36	159.61	2.04	N/A	N/A
1.30	64.42	103.38	1.48	153.19	2.11	N/A	N/A
1.34	56.90	91.29	1.62	148.32	2.18	N/A	N/A
1.40	51.93	83.30	1.73	144.16	2.23	N/A	N/A
1.49	47.87	76.77	1.82	140.01	2.26	N/A	N/A
1.54	45.15	72.38	1.87	135.47	2.28	N/A	N/A
1.59	43.56	69.84	1.88	131.38	2.28	N/A	N/A
1.68	42.04	67.38	1.90	127.84	2.28	N/A	N/A
1.74	40.63	65.11	1.92	125.10	2.29	N/A	N/A
1.79	39.35	63.05	1.96	123.29	2.30	N/A	N/A
1.87	38.01	60.89	2.01	122.18	2.32	N/A	N/A
1.94	36.70	58.77	2.07	121.55	2.34	N/A	N/A
1.98	35.46	56.78	2.14	121.52	2.36	N/A	N/A
2.04	34.18	54.71	2.22	121.49	2.38	N/A	N/A
2.13	32.82	52.53	2.32	121.63	2.40	N/A	N/A
2.17	31.54	50.47	2.40	121.32	2.42	N/A	N/A
2.24	30.07	48.09	2.50	120.38	2.44	N/A	N/A
2.33	28.70	45.88	2.60	119.10	2.46	N/A	N/A
2.36	27.08	43.27	2.72	117.61	2.49	N/A	N/A
2.43	25.49	40.73	2.84	115.57	2.51	N/A	N/A
2.52	23.95	38.24	2.97	113.59	2.54	N/A	N/A
2.56	22.45	35.82	3.12	111.86	2.57	N/A	N/A
2.64	20.99	33.47	3.30	110.58	2.60	N/A	N/A
2.74	19.57	31.18	3.53	110.08	2.63	N/A	N/A
2.78	18.20	28.97	3.81	110.38	2.67	N/A	N/A
2.83	17.12	27.24	4.09	111.38	2.71	N/A	N/A
2.90	16.00	25.43	4.43	112.72	2.76	N/A	N/A
2.98	15.24	24.21	4.71	114.07	2.79	N/A	N/A
3.03	14.73	23.37	4.94	115.52	2.82	N/A	N/A
3.10	14.29	22.66	5.14	116.59	2.84	N/A	N/A
3.18	13.94	22.10	5.32	117.49	2.86	N/A	N/A

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
3.23	13.72	21.74	5.44	118.30	2.87	N/A	N/A
3.29	13.57	21.50	5.51	118.48	2.88	N/A	N/A
3.38	13.45	21.30	5.55	118.25	2.89	N/A	N/A
3.42	13.36	21.13	5.56	117.44	2.89	N/A	N/A
3.51	13.27	20.98	5.55	116.42	2.88	N/A	N/A
3.58	13.16	20.80	5.54	115.30	2.88	N/A	N/A
3.62	13.00	20.54	5.55	114.00	2.88	N/A	N/A
3.69	12.78	20.18	5.57	112.51	2.89	N/A	N/A
3.77	12.51	19.74	5.61	110.72	2.89	N/A	N/A
3.82	12.27	19.35	5.62	108.69	2.89	N/A	N/A
3.89	12.10	19.07	5.59	106.68	2.89	N/A	N/A
3.97	11.87	18.70	5.60	104.67	2.89	N/A	N/A
4.03	11.66	18.35	5.61	103.05	2.89	N/A	N/A
4.10	11.44	17.99	5.65	101.73	2.90	N/A	N/A
4.15	11.24	17.67	5.70	100.72	2.90	N/A	N/A
4.24	11.07	17.39	5.75	100.03	2.91	N/A	N/A
4.29	10.91	17.13	5.83	99.87	2.91	N/A	N/A
4.35	10.77	16.89	5.92	100.05	2.92	N/A	N/A
4.44	10.61	16.63	6.04	100.44	2.93	N/A	N/A
4.48	10.42	16.32	6.17	100.73	2.95	N/A	N/A
4.54	10.34	16.19	6.25	101.19	2.95	N/A	N/A
4.61	10.34	16.19	6.28	101.63	2.96	N/A	N/A
4.69	10.46	16.37	6.22	101.92	2.95	N/A	N/A
4.74	10.72	16.78	6.09	102.16	2.94	N/A	N/A
4.82	11.01	17.24	5.94	102.49	2.92	N/A	N/A
4.86	11.27	17.65	5.82	102.81	2.91	N/A	N/A
4.94	11.44	17.92	5.75	103.07	2.91	N/A	N/A
5.02	11.53	18.06	5.72	103.35	2.90	N/A	N/A
5.09	11.59	18.15	5.71	103.54	2.90	N/A	N/A
5.13	11.58	18.13	5.71	103.44	2.90	N/A	N/A
5.23	11.50	17.99	5.73	103.05	2.90	N/A	N/A
5.28	11.33	17.72	5.78	102.47	2.91	N/A	N/A
5.33	11.01	17.20	5.90	101.40	2.92	N/A	N/A
5.39	10.68	16.65	6.01	100.10	2.93	N/A	N/A
5.48	10.37	16.15	6.11	98.65	2.94	N/A	N/A
5.52	10.16	15.81	6.14	97.14	2.94	N/A	N/A
5.58	10.05	15.63	6.11	95.46	2.94	N/A	N/A
5.67	9.93	15.43	6.08	93.87	2.94	N/A	N/A
5.73	9.80	15.21	6.07	92.37	2.94	N/A	N/A
5.78	9.62	14.92	6.08	90.75	2.94	N/A	N/A
5.88	9.43	14.60	6.11	89.22	2.94	N/A	N/A
5.92	9.27	14.35	6.12	87.78	2.94	N/A	N/A
5.97	9.11	14.09	6.12	86.19	2.94	N/A	N/A
6.08	8.96	13.84	6.10	84.43	2.94	N/A	N/A
6.11	8.81	13.59	6.07	82.50	2.94	N/A	N/A
6.18	8.66	13.35	6.05	80.80	2.94	N/A	N/A
6.27	8.55	13.16	6.02	79.18	2.93	N/A	N/A
6.33	8.51	13.09	5.94	77.79	2.92	N/A	N/A

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
6.38	8.57	13.18	5.85	77.06	2.91	N/A	N/A
6.44	8.68	13.35	5.71	76.30	2.90	N/A	N/A
6.50	8.77	13.50	5.63	75.97	2.89	N/A	N/A
6.57	8.86	13.64	5.60	76.38	2.89	N/A	N/A
6.67	8.93	13.74	5.62	77.22	2.89	N/A	N/A
6.72	9.00	13.85	5.67	78.47	2.90	N/A	N/A
6.76	9.05	13.91	5.75	79.99	2.91	N/A	N/A
6.83	9.07	13.94	5.85	81.62	2.92	N/A	N/A
6.92	9.05	13.90	5.98	83.10	2.93	N/A	N/A
6.97	9.00	13.82	6.10	84.30	2.94	N/A	N/A
7.04	8.95	13.74	6.22	85.48	2.95	N/A	N/A
7.12	8.92	13.67	6.32	86.38	2.96	N/A	N/A
7.16	8.93	13.69	6.35	86.88	2.96	N/A	N/A
7.25	8.98	13.77	6.33	87.12	2.96	N/A	N/A
7.32	9.04	13.86	6.29	87.24	2.96	N/A	N/A
7.37	9.15	14.04	6.23	87.46	2.95	N/A	N/A
7.43	9.31	14.29	6.14	87.79	2.94	N/A	N/A
7.52	9.51	14.59	6.04	88.11	2.93	N/A	N/A
7.56	9.71	14.92	5.96	88.91	2.93	N/A	N/A
7.63	9.90	15.21	5.91	89.83	2.92	N/A	N/A
7.71	10.03	15.41	5.89	90.76	2.92	N/A	N/A
7.75	10.10	15.52	5.90	91.59	2.92	N/A	N/A
7.83	10.07	15.47	5.97	92.32	2.93	N/A	N/A
7.88	10.00	15.34	6.06	92.94	2.94	N/A	N/A
7.97	9.86	15.11	6.16	93.11	2.95	N/A	N/A
8.01	9.69	14.84	6.25	92.80	2.95	N/A	N/A
8.08	9.54	14.59	6.33	92.37	2.96	N/A	N/A
8.18	9.42	14.39	6.36	91.57	2.97	N/A	N/A
8.22	9.30	14.19	6.39	90.63	2.97	N/A	N/A
8.28	9.26	14.13	6.36	89.79	2.96	N/A	N/A
8.35	9.23	14.08	6.33	89.07	2.96	N/A	N/A
8.43	9.24	14.09	6.28	88.45	2.96	N/A	N/A
8.48	9.27	14.12	6.22	87.82	2.95	N/A	N/A
8.56	9.28	14.13	6.18	87.32	2.95	N/A	N/A
8.63	9.26	14.10	6.18	87.07	2.95	N/A	N/A
8.68	9.20	14.00	6.20	86.84	2.95	N/A	N/A
8.76	9.10	13.83	6.25	86.49	2.95	N/A	N/A
8.80	9.00	13.66	6.28	85.75	2.96	N/A	N/A
8.88	8.84	13.40	6.34	84.89	2.96	N/A	N/A
8.94	8.67	13.13	6.39	83.89	2.97	N/A	N/A
8.99	8.51	12.85	6.45	82.88	2.97	N/A	N/A
9.07	8.35	12.59	6.50	81.85	2.98	1.10	1.10
9.14	8.17	12.30	6.56	80.67	2.98	1.06	1.06
9.22	8.01	12.03	6.59	79.33	2.99	1.03	1.03
9.27	7.85	11.77	6.62	77.97	2.99	1.00	1.00
9.37	7.71	11.54	6.62	76.43	2.99	0.98	0.98
9.42	7.56	11.30	6.65	75.16	2.99	0.95	0.95
9.47	7.39	11.03	6.70	73.85	3.00	0.92	0.92

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
9.52	7.22	10.74	6.77	72.68	3.00	0.89	0.89
9.62	7.05	10.46	6.83	71.47	3.01	0.86	0.86
9.67	6.93	10.26	6.85	70.25	3.01	0.84	0.84
9.73	7.01	10.39	6.73	69.94	3.00	0.35	0.85
9.82	7.17	10.63	6.59	70.09	2.99	0.86	0.86
9.86	7.39	10.98	6.42	70.54	2.97	0.88	0.88
9.92	7.76	11.57	6.24	72.17	2.95	0.93	0.93
10.02	8.17	12.23	6.08	74.33	2.94	0.97	0.97
10.06	8.66	13.01	5.92	77.10	2.92	1.03	1.03
10.12	9.25	13.95	5.76	80.39	2.91	1.10	1.10
10.21	9.84	14.90	5.62	83.79	2.89	1.16	1.16
10.25	10.49	15.94	5.48	87.38	2.88	1.24	1.24
10.31	11.09	16.89	5.36	90.46	2.86	1.30	1.30
10.41	11.67	17.81	5.23	93.18	2.85	1.36	1.36
10.45	12.28	18.80	5.10	95.78	2.84	1.43	1.43
10.52	12.84	19.69	4.98	98.11	2.82	1.49	1.49
10.61	13.40	20.57	4.87	100.13	2.81	1.54	1.54
10.64	13.96	21.47	4.75	101.99	2.80	1.61	1.61
10.71	14.46	22.27	4.65	103.52	2.78	1.66	1.66
10.81	14.98	22.93	4.57	104.69	2.77	1.70	1.70
10.85	15.43	23.52	4.50	105.85	2.77	1.75	1.75
10.91	15.78	23.92	4.47	106.92	2.76	1.78	1.78
10.96	16.11	24.32	4.44	108.02	2.76	1.81	1.81
11.03	16.41	24.63	4.43	109.16	2.76	1.83	1.83
11.10	16.63	24.81	4.43	110.05	2.76	1.84	1.84
11.20	16.84	24.94	4.45	110.91	2.76	1.85	1.85
11.24	17.06	25.18	4.44	111.77	2.76	1.87	1.87
11.30	17.28	25.38	4.43	112.54	2.76	1.88	1.88
11.36	17.47	25.53	4.44	113.33	2.76	1.89	1.89
11.43	17.60	25.59	4.45	113.92	2.76	1.90	1.90
11.50	17.65	25.53	4.47	114.20	2.76	1.89	1.89
11.58	17.64	25.35	4.50	114.11	2.77	1.87	1.87
11.63	17.60	25.19	4.52	113.88	2.77	1.86	1.86
11.70	17.51	24.92	4.55	113.42	2.77	1.84	1.84
11.79	17.40	24.59	4.57	112.43	2.77	1.81	1.81
11.84	17.23	24.24	4.58	111.06	2.78	1.79	1.79
11.90	17.01	23.80	4.59	109.21	2.78	1.75	1.75
11.98	16.94	23.51	4.54	106.65	2.77	1.73	1.73
12.02	16.91	23.37	4.45	103.99	2.76	1.73	1.73
12.09	17.00	23.38	4.34	101.38	2.75	1.73	1.73
12.14	17.14	23.48	4.22	99.12	2.73	1.74	1.74
12.21	17.31	23.60	4.11	96.91	2.71	1.76	1.76
12.29	17.62	23.89	3.97	94.76	2.70	1.78	1.78
12.34	17.88	24.16	3.86	93.21	2.68	1.81	1.81
12.44	18.17	24.43	3.78	92.34	2.67	1.83	1.83
12.49	18.50	24.79	3.70	91.81	2.66	1.86	1.86
12.57	18.63	24.90	3.69	91.83	2.66	1.87	1.87
12.64	18.76	25.02	3.69	92.19	2.66	1.88	1.88

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
12.68	18.84	25.09	3.69	92.51	2.66	1.88	1.88
12.73	18.86	25.08	3.70	92.86	2.66	1.88	1.88
12.84	18.81	24.93	3.73	92.99	2.66	1.87	1.87
12.89	18.69	24.74	3.76	93.03	2.67	1.85	1.85
12.98	18.58	24.53	3.78	92.82	2.67	1.83	1.83
13.00	18.45	24.34	3.80	92.48	2.67	1.82	1.82
13.08	18.34	24.13	3.82	92.17	2.68	1.80	1.80
13.14	18.25	23.98	3.84	92.18	2.68	1.79	1.79
13.23	18.22	23.86	3.87	92.33	2.68	1.78	1.78
13.27	18.26	23.89	3.89	92.99	2.69	1.78	1.78
13.34	18.38	24.01	3.91	93.85	2.69	1.79	1.79
13.43	18.50	24.12	3.94	94.98	2.69	1.79	1.79
13.47	18.61	24.25	3.98	96.47	2.70	1.80	1.80
13.54	18.62	24.25	4.06	98.37	2.71	1.80	1.80
13.63	18.55	24.12	4.16	100.47	2.72	1.78	1.78
13.67	18.46	24.02	4.27	102.51	2.74	1.77	1.77
13.72	18.35	23.87	4.36	104.15	2.75	1.76	1.76
13.83	18.16	23.56	4.47	105.29	2.76	1.73	1.73
13.88	17.91	23.21	4.57	106.09	2.77	1.70	1.70
13.94	17.59	22.77	4.68	106.54	2.79	1.67	1.67
13.98	17.20	22.26	4.80	106.80	2.80	1.63	1.63
14.06	16.75	21.64	4.93	106.76	2.82	1.58	1.58
14.14	16.40	21.13	5.02	106.09	2.83	1.54	1.54
14.18	16.13	20.75	5.06	105.03	2.83	1.51	1.51
14.26	15.81	20.27	5.12	103.76	2.84	1.47	1.47
14.33	15.47	19.77	5.17	102.31	2.84	1.43	1.43
14.37	15.15	19.33	5.23	101.05	2.85	1.40	1.40
14.45	14.78	18.80	5.31	99.86	2.86	1.36	1.36
14.54	14.43	18.29	5.39	98.53	2.87	1.32	1.32
14.61	14.15	17.89	5.43	97.16	2.87	1.29	1.29
14.65	13.92	17.55	5.45	95.67	2.87	1.27	1.27
14.74	13.69	17.19	5.48	94.20	2.88	1.24	1.24
14.80	13.48	16.88	5.50	92.84	2.88	1.22	1.22
14.85	13.31	16.63	5.51	91.55	2.88	1.20	1.20
14.90	13.18	16.42	5.51	90.43	2.88	1.18	1.18
15.00	13.08	16.23	5.50	89.23	2.88	1.17	1.17
15.05	13.03	16.13	5.46	88.03	2.88	1.16	1.16
15.10	12.95	15.99	5.44	86.96	2.87	1.15	1.15
15.17	12.87	15.84	5.43	85.96	2.87	1.14	1.14
15.25	12.79	15.69	5.42	85.06	2.87	1.13	1.13
15.30	12.71	15.56	5.41	84.17	2.87	1.12	1.12
15.36	12.61	15.39	5.41	83.29	2.87	1.11	1.11
15.45	12.52	15.23	5.41	82.36	2.87	1.10	1.10
15.49	12.41	15.06	5.41	81.49	2.87	1.09	1.09
15.57	12.29	14.87	5.43	80.69	2.87	1.07	1.07
15.64	12.18	14.70	5.45	80.12	2.87	1.06	1.06
15.69	12.09	14.56	5.48	79.78	2.88	1.05	1.05
15.77	11.98	14.39	5.53	79.54	2.88	1.04	1.04

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
15.85	11.82	14.15	5.62	79.57	2.89	1.02	1.02
15.89	11.63	13.90	5.73	79.64	2.90	1.00	1.00
15.99	11.42	13.60	5.86	79.77	2.92	0.98	0.98
16.05	11.18	13.29	6.02	80.06	2.93	0.95	0.95
16.09	10.95	13.00	6.17	80.24	2.95	0.93	0.93
16.16	10.68	12.63	6.35	80.24	2.96	0.90	0.90
16.24	10.38	12.21	6.55	79.98	2.98	0.87	0.87
16.30	10.10	11.82	6.73	79.51	3.00	0.84	0.84
16.34	9.80	11.42	6.90	78.82	3.01	0.82	0.82
16.44	9.56	11.07	7.03	77.83	3.03	0.79	0.79
16.48	9.34	10.78	7.14	76.90	3.03	0.77	0.77
16.54	9.16	10.52	7.21	75.93	3.04	0.75	0.75
16.63	9.03	10.33	7.26	74.93	3.04	0.74	0.74
16.69	8.94	10.19	7.26	73.96	3.04	0.73	0.73
16.74	8.91	10.14	7.20	72.99	3.04	0.72	0.72
16.82	8.90	10.10	7.14	72.11	3.03	0.72	0.72
16.90	8.88	10.04	7.09	71.21	3.03	0.72	0.72
16.94	8.94	10.09	6.99	70.59	3.02	0.72	0.72
17.03	8.98	10.11	6.93	70.04	3.02	0.72	0.72
17.07	8.99	10.11	6.88	69.52	3.01	0.33	0.72
17.13	8.97	10.07	6.91	69.59	3.02	0.31	0.72
17.21	8.95	10.01	7.00	70.13	3.02	0.72	0.72
17.26	9.06	10.15	7.04	71.40	3.03	0.72	0.72
17.33	9.38	10.52	6.96	73.22	3.02	0.75	0.75
17.41	9.84	11.06	6.80	75.19	3.00	0.79	0.79
17.48	10.47	11.81	6.55	77.41	2.98	0.84	0.84
17.53	11.02	12.49	6.38	79.66	2.97	0.89	0.89
17.61	11.59	13.15	6.21	81.69	2.95	0.94	0.94
17.67	12.19	13.84	6.04	83.58	2.93	0.99	0.99
17.72	12.75	14.48	5.83	84.41	2.91	1.04	1.04
17.82	13.25	15.02	5.63	84.59	2.89	1.08	1.08
17.88	13.49	15.26	5.52	84.31	2.88	1.10	1.10
17.92	13.46	15.20	5.50	83.57	2.88	1.09	1.09
18.02	13.24	14.89	5.54	82.55	2.88	1.07	1.07
18.07	12.93	14.50	5.62	81.41	2.89	1.04	1.04
18.14	12.53	14.00	5.73	80.27	2.90	1.00	1.00
18.20	12.25	13.64	5.80	79.05	2.91	0.98	0.98
18.27	12.04	13.36	5.84	78.00	2.91	0.96	0.96
18.32	11.94	13.22	5.87	77.57	2.92	0.95	0.95
18.38	11.89	13.14	5.89	77.43	2.92	0.94	0.94
18.47	11.95	13.17	5.88	77.44	2.92	0.94	0.94
18.51	12.13	13.36	5.80	77.55	2.91	0.96	0.96
18.57	12.37	13.61	5.71	77.73	2.90	0.98	0.98
18.67	12.54	13.76	5.64	77.68	2.89	0.99	0.99
18.71	12.82	14.06	5.50	77.30	2.88	1.01	1.01
18.81	13.01	14.23	5.40	76.81	2.87	1.02	1.02
18.86	13.15	14.35	5.30	76.04	2.86	1.03	1.03
18.91	13.20	14.38	5.22	74.98	2.85	1.04	1.04

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
18.97	13.23	14.38	5.14	73.92	2.84	1.04	1.04
19.06	13.28	14.39	5.06	72.81	2.83	1.04	1.04
19.11	13.35	14.44	5.01	72.28	2.83	1.04	1.04
19.21	13.59	14.66	4.91	71.98	2.81	1.06	1.06
19.27	14.02	15.12	4.80	72.63	2.80	1.09	1.09
19.31	14.78	15.97	4.65	74.33	2.78	1.16	1.16
19.41	16.02	17.32	4.45	77.15	2.76	1.26	1.26
19.46	17.53	19.00	4.24	80.48	2.73	1.38	1.38
19.51	19.45	21.12	3.95	83.35	2.69	1.54	1.54
19.56	21.37	23.23	3.70	85.96	2.66	1.70	1.70
19.63	22.73	24.70	3.59	88.73	2.64	1.81	1.81
19.71	23.86	25.91	3.53	91.41	2.63	1.90	1.90
19.80	24.54	26.62	3.55	94.40	2.63	1.95	1.95
19.82	25.00	27.14	3.59	97.46	2.64	1.99	1.99
19.91	24.70	26.78	3.75	100.50	2.67	1.96	1.96
19.95	25.51	27.65	3.70	102.41	2.66	2.02	2.02
20.02	26.21	28.37	3.67	103.99	2.65	2.07	2.07
20.11	26.74	28.89	3.67	105.99	2.65	2.11	2.11
20.15	27.33	29.52	3.67	108.26	2.65	2.16	2.16
20.24	28.50	30.73	3.59	110.30	2.64	2.25	2.25
20.29	30.11	32.44	3.46	112.35	2.62	2.37	2.37
20.36	32.24	34.68	3.30	114.39	2.60	0.69	0.69
20.41	34.37	36.93	3.15	116.15	2.57	0.70	0.70
20.48	36.70	39.36	2.99	117.57	2.54	0.70	0.70
20.56	36.71	39.31	3.05	120.01	2.55	0.70	0.70
20.66	35.87	38.33	3.20	122.64	2.58	0.70	0.70
20.71	34.56	36.92	3.39	125.21	2.61	2.70	2.70
20.74	32.81	35.04	3.63	127.16	2.65	2.56	2.56
20.82	30.71	32.73	3.91	128.02	2.69	2.38	2.38
20.91	28.18	29.93	4.29	128.26	2.74	2.17	2.17
20.95	25.20	26.71	4.78	127.59	2.80	1.93	1.93
21.03	22.22	23.43	5.39	126.25	2.87	1.68	1.68
21.11	19.51	20.46	6.08	124.37	2.94	1.46	1.46
21.15	17.79	18.53	6.55	121.46	2.98	1.32	1.32
21.22	17.08	17.69	6.69	118.28	2.99	1.26	1.26
21.26	16.89	17.46	6.61	115.41	2.99	1.25	1.25
21.34	17.65	18.26	6.21	113.47	2.95	1.30	1.30
21.41	19.06	19.71	5.70	112.40	2.90	1.41	1.41
21.48	21.43	22.18	5.03	111.65	2.83	1.60	1.60
21.52	24.31	25.19	4.41	111.09	2.75	1.82	1.82
21.61	27.48	28.46	3.88	110.44	2.68	2.06	2.06
21.66	30.96	32.05	3.43	109.80	2.62	2.33	2.33
21.76	34.47	35.62	3.08	109.70	2.56	0.69	0.69
21.81	38.00	39.23	2.81	110.19	2.51	0.70	0.70
21.85	41.47	42.78	2.59	110.86	2.46	0.71	0.71
21.92	44.74	46.08	2.42	111.70	2.43	0.72	0.72
22.01	47.97	49.30	2.29	113.00	2.39	0.73	0.73
22.09	50.58	51.88	2.20	114.29	2.37	0.74	0.74

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
22.12	53.36	54.70	2.12	116.09	2.35	0.75	0.75
22.20	56.17	57.47	2.05	117.96	2.33	0.75	0.75
22.29	59.12	60.36	1.99	119.83	2.31	0.76	0.76
22.31	62.19	63.46	1.91	121.53	2.29	0.77	0.77
22.40	64.97	66.14	1.86	122.95	2.27	0.77	0.77
22.45	67.71	68.85	1.81	124.62	2.25	0.78	0.78
22.51	70.07	71.14	1.77	126.20	2.24	0.78	0.78
22.60	72.08	73.01	1.74	126.79	2.23	0.78	0.78
22.64	73.69	74.54	1.69	125.89	2.21	0.79	0.79
22.75	74.70	75.33	1.65	124.57	2.19	0.79	0.79
22.80	75.19	75.71	1.63	123.38	2.18	0.79	0.79
22.85	75.11	75.52	1.62	122.10	2.18	0.79	0.79
22.91	74.60	74.89	1.61	120.84	2.18	0.79	0.79
22.99	74.00	74.15	1.63	120.66	2.18	0.79	0.79
23.08	73.13	73.14	1.65	120.60	2.19	0.78	0.78
23.10	71.45	71.45	1.69	120.90	2.21	0.78	0.78
23.18	69.67	69.57	1.75	121.90	2.23	0.78	0.78
23.26	67.59	67.40	1.85	124.40	2.27	0.77	0.77
23.30	65.04	64.84	1.96	127.10	2.30	0.77	0.77
23.37	61.42	61.15	2.11	128.98	2.35	0.76	0.76
23.46	57.08	56.69	2.29	130.03	2.40	0.75	0.75
23.51	52.26	51.82	2.52	130.48	2.45	0.74	0.74
23.56	47.18	46.67	2.76	128.64	2.50	0.73	0.73
23.63	42.20	41.60	3.03	125.94	2.55	0.71	0.71
23.72	37.88	37.16	3.28	121.71	2.59	0.70	0.70
23.79	33.58	32.77	3.56	116.82	2.64	2.36	2.36
23.87	29.73	28.83	3.86	111.37	2.68	2.08	2.08
23.91	26.52	25.57	4.12	105.33	2.72	1.84	1.84
23.96	24.53	23.53	4.24	99.72	2.73	1.69	1.69
24.02	23.43	22.37	4.26	95.24	2.73	1.61	1.61
24.11	22.70	21.59	4.25	91.81	2.73	1.55	1.55
24.20	22.25	21.07	4.27	90.02	2.74	1.51	1.51
24.22	21.77	20.58	4.32	88.89	2.74	1.48	1.48
24.31	21.48	20.25	4.36	88.24	2.75	1.45	1.45
24.39	21.34	20.06	4.39	88.00	2.75	1.44	1.44
24.42	21.29	20.00	4.39	87.84	2.75	1.44	1.44
24.51	21.19	19.85	4.40	87.42	2.75	1.42	1.42
24.55	21.20	19.83	4.37	86.67	2.75	1.42	1.42
24.63	20.99	19.58	4.37	85.49	2.75	1.41	1.41
24.71	20.75	19.30	4.36	84.15	2.75	1.39	1.39
24.75	20.38	18.92	4.36	82.54	2.75	1.36	1.36
24.81	19.90	18.40	4.39	80.85	2.75	1.32	1.32
24.90	19.35	17.82	4.44	79.04	2.76	1.28	1.28
24.94	18.79	17.25	4.46	76.96	2.76	1.24	1.24
25.01	18.24	16.67	4.51	75.15	2.77	1.20	1.20
25.07	17.67	16.09	4.57	73.59	2.77	1.15	1.15
25.15	17.08	15.48	4.69	72.54	2.79	1.11	1.11
25.20	16.59	14.97	4.82	72.13	2.80	1.07	1.07

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
25.28	16.23	14.59	4.94	72.03	2.82	1.04	1.04
25.35	16.04	14.38	5.03	72.34	2.83	1.03	1.03
25.40	16.03	14.36	5.07	72.78	2.83	1.03	1.03
25.48	16.13	14.42	5.12	73.82	2.84	1.03	1.03
25.55	16.28	14.54	5.19	75.56	2.85	1.04	1.04
25.60	16.45	14.69	5.26	77.34	2.85	1.05	1.05
25.67	16.64	14.85	5.33	79.14	2.86	1.06	1.06
25.75	16.81	15.00	5.39	80.81	2.87	1.07	1.07
25.79	16.95	15.12	5.45	82.31	2.87	1.08	1.08
25.90	17.27	15.38	5.43	83.51	2.87	1.10	1.10
25.95	17.61	15.69	5.40	84.65	2.87	1.12	1.12
26.01	17.91	15.95	5.37	85.69	2.87	1.14	1.14
26.09	18.18	16.17	5.34	86.33	2.86	1.16	1.16
26.13	18.45	16.42	5.27	86.44	2.85	1.17	1.17
26.19	18.70	16.64	5.20	86.46	2.85	1.19	1.19
26.27	19.02	16.91	5.12	86.51	2.84	1.21	1.21
26.34	19.37	17.21	5.03	86.57	2.83	1.23	1.23
26.39	19.82	17.61	4.92	86.67	2.82	1.26	1.26
26.47	20.03	17.78	4.88	86.84	2.81	1.27	1.27
26.54	20.17	17.88	4.87	87.04	2.81	1.28	1.28
26.58	20.25	17.94	4.87	87.28	2.81	1.28	1.28
26.67	20.26	17.90	4.88	87.44	2.81	1.28	1.28
26.73	20.23	17.85	4.91	87.63	2.81	1.28	1.28
26.78	20.16	17.76	4.93	87.62	2.82	1.27	1.27
26.85	20.02	17.59	4.96	87.31	2.82	1.26	1.26
26.93	19.87	17.41	4.99	86.92	2.82	1.24	1.24
26.98	19.65	17.18	5.04	86.58	2.83	1.23	1.23
27.03	19.48	17.00	5.07	86.22	2.83	1.21	1.21
27.13	19.33	16.82	5.10	85.81	2.84	1.20	1.20
27.17	19.21	16.68	5.13	85.52	2.84	1.19	1.19
27.24	19.07	16.52	5.15	85.13	2.84	1.18	1.18
27.33	18.86	16.29	5.21	84.82	2.85	1.16	1.16
27.36	18.63	16.05	5.28	84.72	2.86	1.15	1.15
27.43	18.38	15.79	5.36	84.58	2.86	1.13	1.13
27.53	18.13	15.51	5.44	84.43	2.87	1.11	1.11
27.60	17.91	15.28	5.50	84.05	2.88	1.09	1.09
27.63	17.70	15.07	5.54	83.47	2.88	1.08	1.08
27.72	17.52	14.87	5.57	82.75	2.89	1.06	1.06
27.77	17.42	14.76	5.55	81.96	2.89	1.05	1.05
27.84	17.46	14.77	5.50	81.27	2.88	1.05	1.05
27.93	17.59	14.85	5.42	80.54	2.87	1.06	1.06
27.97	17.75	14.99	5.33	79.83	2.86	1.07	1.07
28.02	17.89	15.10	5.25	79.27	2.85	1.08	1.08
28.12	18.02	15.18	5.18	78.68	2.85	1.08	1.08
28.17	18.17	15.30	5.11	78.11	2.84	1.09	1.09
28.22	18.28	15.38	5.05	77.72	2.83	1.10	1.10
28.32	18.30	15.36	5.05	77.57	2.83	1.10	1.10
28.36	18.44	15.47	5.01	77.50	2.83	1.10	1.10

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
28.42	18.88	15.86	4.90	77.73	2.81	1.13	1.13
28.48	19.31	16.24	4.80	77.88	2.80	1.16	1.16
28.57	19.74	16.59	4.70	78.01	2.79	1.18	1.18
28.62	20.26	17.05	4.62	78.69	2.78	1.21	1.21
28.72	20.70	17.42	4.56	79.51	2.77	1.24	1.24
28.75	20.99	17.67	4.57	80.80	2.77	1.26	1.26
28.82	21.18	17.81	4.62	82.31	2.78	1.27	1.27
28.87	21.43	18.01	4.64	83.55	2.78	1.28	1.28
28.95	21.50	18.04	4.69	84.52	2.79	1.28	1.28
29.02	21.16	17.70	4.80	84.88	2.80	1.26	1.26
29.07	20.75	17.30	4.92	85.13	2.82	1.23	1.23
29.16	20.35	16.89	5.05	85.34	2.83	1.20	1.20
29.21	19.87	16.43	5.17	85.00	2.84	1.17	1.17
29.29	19.55	16.11	5.23	84.30	2.85	1.15	1.15
29.36	19.41	15.96	5.22	83.25	2.85	1.14	1.14
29.40	19.63	16.15	5.08	81.96	2.83	1.15	1.15
29.47	19.93	16.39	4.93	80.76	2.82	1.17	1.17
29.56	20.29	16.68	4.78	79.82	2.80	1.19	1.19
29.60	20.70	17.04	4.66	79.35	2.78	1.21	1.21
29.71	21.12	17.37	4.56	79.22	2.77	1.24	1.24
29.75	21.53	17.73	4.47	79.29	2.76	1.26	1.26
29.79	21.94	18.08	4.40	79.51	2.75	1.29	1.29
29.86	22.27	18.35	4.36	80.05	2.75	1.30	1.30
29.95	22.60	18.60	4.34	80.71	2.75	1.32	1.32
30.04	22.87	18.80	4.33	81.39	2.74	1.34	1.34
30.06	23.16	19.06	4.31	82.09	2.74	1.35	1.35
30.15	23.46	19.28	4.30	82.82	2.74	1.37	1.37
30.20	23.80	19.56	4.28	83.76	2.74	1.39	1.39
30.28	24.21	19.88	4.28	85.00	2.74	1.41	1.41
30.35	24.55	20.15	4.28	86.18	2.74	1.43	1.43
30.39	24.85	20.40	4.28	87.23	2.74	1.45	1.45
30.45	25.09	20.58	4.28	88.07	2.74	1.46	1.46
30.54	25.24	20.67	4.30	88.84	2.74	1.47	1.47
30.60	25.09	20.50	4.38	89.73	2.75	1.46	1.46
30.67	24.78	20.19	4.48	90.39	2.76	1.43	1.43
30.74	24.41	19.81	4.58	90.80	2.78	1.41	1.41
30.79	23.91	19.35	4.70	90.92	2.79	1.37	1.37
30.86	23.34	18.82	4.78	89.92	2.80	1.34	1.34
30.95	22.81	18.30	4.84	88.68	2.81	1.30	1.30
30.99	22.25	17.80	4.91	87.32	2.81	1.27	1.27
31.05	21.70	17.29	4.96	85.85	2.82	1.23	1.23
31.14	21.26	16.87	4.99	84.23	2.82	1.20	1.20
31.19	20.89	16.53	4.99	82.51	2.82	1.18	1.18
31.26	20.65	16.30	4.96	80.93	2.82	1.16	1.16
31.34	20.47	16.11	4.93	79.38	2.82	1.15	1.15
31.39	20.36	16.00	4.87	77.95	2.81	1.14	1.14
31.45	20.34	15.96	4.86	77.54	2.81	1.13	1.13
31.54	20.41	15.99	4.82	77.08	2.80	1.14	1.14

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
31.57	20.70	16.25	4.71	76.52	2.79	1.15	1.15
31.63	21.26	16.71	4.58	76.48	2.78	1.19	1.19
31.73	21.86	17.20	4.46	76.78	2.76	1.22	1.22
31.77	22.65	17.87	4.34	77.50	2.75	1.27	1.27
31.84	23.37	18.47	4.24	78.35	2.73	1.31	1.31
31.93	23.77	18.77	4.24	79.51	2.73	1.33	1.33
31.98	24.18	19.10	4.22	80.58	2.73	1.35	1.35
32.05	24.49	19.34	4.20	81.23	2.73	1.37	1.37
32.09	24.69	19.49	4.21	82.07	2.73	1.38	1.38
32.17	24.77	19.51	4.26	83.19	2.74	1.38	1.38
32.22	24.56	19.30	4.34	83.85	2.75	1.37	1.37
32.32	24.33	19.06	4.41	84.14	2.75	1.35	1.35
32.35	24.03	18.79	4.47	84.07	2.76	1.33	1.33
32.43	23.76	18.52	4.52	83.76	2.77	1.31	1.31
32.52	23.80	18.52	4.49	83.20	2.76	1.31	1.31
32.57	23.78	18.49	4.47	82.69	2.76	1.31	1.31
32.62	23.81	18.49	4.45	82.23	2.76	1.31	1.31
32.71	23.88	18.52	4.41	81.74	2.75	1.31	1.31
32.76	23.92	18.53	4.39	81.27	2.75	1.31	1.31
32.82	24.02	18.59	4.36	81.13	2.75	1.31	1.31
32.90	24.07	18.60	4.36	81.14	2.75	1.32	1.32
32.96	24.10	18.60	4.37	81.31	2.75	1.32	1.32
33.02	24.16	18.62	4.39	81.74	2.75	1.32	1.32
33.11	24.21	18.62	4.42	82.23	2.76	1.32	1.32
33.17	24.32	18.69	4.43	82.78	2.76	1.32	1.32
33.22	24.44	18.77	4.44	83.33	2.76	1.33	1.33
33.31	24.49	18.77	4.46	83.74	2.76	1.33	1.33
33.34	24.51	18.77	4.48	84.12	2.76	1.33	1.33
33.41	24.52	18.75	4.49	84.14	2.76	1.33	1.33
33.49	24.50	18.69	4.51	84.23	2.77	1.32	1.32
33.57	24.46	18.63	4.52	84.25	2.77	1.32	1.32
33.61	24.39	18.55	4.53	84.05	2.77	1.31	1.31
33.68	24.39	18.52	4.53	83.87	2.77	1.31	1.31
33.76	24.41	18.50	4.53	83.81	2.77	1.31	1.31
33.81	24.49	18.55	4.53	84.09	2.77	1.31	1.31
33.88	24.70	18.69	4.54	84.79	2.77	1.32	1.32
33.95	24.97	18.88	4.55	85.91	2.77	1.33	1.33
34.01	25.30	19.12	4.57	87.39	2.77	1.35	1.35
34.06	25.58	19.32	4.60	88.93	2.78	1.37	1.37
34.13	25.81	19.47	4.65	90.56	2.78	1.38	1.38
34.21	25.99	19.58	4.73	92.59	2.79	1.38	1.38
34.25	26.13	19.66	4.81	94.49	2.80	1.39	1.39
34.35	26.22	19.68	4.89	96.14	2.81	1.39	1.39
34.40	26.26	19.68	4.96	97.59	2.82	1.39	1.39
34.49	26.26	19.62	5.03	98.65	2.83	1.39	1.39
34.53	26.21	19.56	5.09	99.47	2.83	1.39	1.39
34.60	26.13	19.45	5.14	100.04	2.84	1.38	1.38
34.65	26.05	19.36	5.19	100.56	2.85	1.37	1.37

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
34.74	26.01	19.28	5.24	101.09	2.85	1.37	1.37
34.80	25.96	19.21	5.27	101.16	2.85	1.36	1.36
34.85	25.81	19.06	5.30	100.98	2.86	1.35	1.35
34.93	25.63	18.87	5.34	100.73	2.86	1.34	1.34
34.98	25.37	18.64	5.39	100.52	2.87	1.32	1.32
35.05	25.16	18.43	5.44	100.22	2.87	1.31	1.31
35.15	24.95	18.22	5.47	99.73	2.88	1.29	1.29
35.20	24.79	18.07	5.49	99.23	2.88	1.28	1.28
35.25	24.73	18.00	5.47	98.37	2.88	1.28	1.28
35.33	24.69	17.94	5.42	97.25	2.87	1.27	1.27
35.40	24.65	17.88	5.39	96.31	2.87	1.27	1.27
35.44	24.77	17.97	5.33	95.69	2.86	1.28	1.28
35.50	24.93	18.08	5.26	95.04	2.85	1.28	1.28
35.59	25.19	18.26	5.16	94.29	2.84	1.29	1.29
35.64	25.39	18.41	5.09	93.74	2.84	1.30	1.30
35.70	25.56	18.52	5.04	93.37	2.83	1.31	1.31
35.79	25.66	18.57	5.01	93.11	2.83	1.31	1.31
35.83	25.68	18.57	5.02	93.19	2.83	1.31	1.31
35.94	25.66	18.50	5.03	93.05	2.83	1.31	1.31
35.98	25.62	18.45	5.03	92.86	2.83	1.31	1.31
36.03	25.44	18.29	5.06	92.51	2.83	1.29	1.29
36.09	25.17	18.05	5.10	92.12	2.84	1.28	1.28
36.17	24.77	17.69	5.18	91.67	2.85	1.25	1.25
36.23	24.32	17.31	5.27	91.14	2.85	1.23	1.23
36.29	23.82	16.88	5.35	90.37	2.86	1.20	1.20
36.38	23.31	16.44	5.44	89.39	2.87	1.17	1.17
36.44	22.79	16.01	5.52	88.30	2.88	1.14	1.14
36.49	22.27	15.58	5.60	87.26	2.89	1.11	1.11
36.59	21.81	15.17	5.68	86.23	2.90	1.08	1.08
36.63	21.37	14.82	5.76	85.28	2.91	1.05	1.05
36.69	21.03	14.53	5.81	84.42	2.91	1.03	1.03
36.78	20.84	14.35	5.82	83.57	2.91	1.02	1.02
36.82	20.75	14.28	5.80	82.81	2.91	1.02	1.02
36.88	20.77	14.28	5.75	82.14	2.91	1.02	1.02
36.98	20.81	14.28	5.71	81.57	2.90	1.02	1.02
37.02	20.88	14.33	5.66	81.09	2.90	1.02	1.02
37.11	20.95	14.36	5.62	80.71	2.89	1.02	1.02
37.18	21.00	14.38	5.59	80.40	2.89	1.02	1.02
37.22	21.09	14.44	5.56	80.31	2.89	1.03	1.03
37.28	21.20	14.50	5.55	80.51	2.88	1.03	1.03
37.38	21.34	14.58	5.55	80.94	2.89	1.04	1.04
37.42	21.53	14.71	5.54	81.52	2.88	1.04	1.04
37.48	21.73	14.84	5.54	82.15	2.88	1.05	1.05
37.57	21.96	14.99	5.50	82.37	2.88	1.06	1.06
37.62	22.23	15.19	5.42	82.24	2.87	1.08	1.08
37.68	22.47	15.36	5.35	82.23	2.86	1.09	1.09
37.77	22.71	15.51	5.32	82.51	2.86	1.10	1.10
37.82	22.94	15.67	5.28	82.75	2.86	1.11	1.11

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
37.88	23.12	15.79	5.24	82.68	2.85	1.12	1.12
37.96	23.17	15.81	5.22	82.50	2.85	1.12	1.12
38.00	23.39	15.98	5.15	82.25	2.84	1.13	1.13
38.08	23.81	16.29	5.02	81.76	2.83	1.15	1.15
38.12	24.25	16.62	4.90	81.46	2.81	1.17	1.17
38.20	24.73	16.97	4.79	81.32	2.80	1.20	1.20
38.27	25.09	17.24	4.72	81.32	2.79	1.21	1.21
38.36	25.41	17.46	4.65	81.20	2.78	1.23	1.23
38.40	25.70	17.66	4.62	81.62	2.78	1.24	1.24
38.46	26.47	18.23	4.55	83.02	2.77	1.28	1.28
38.56	27.70	19.15	4.41	84.43	2.75	1.34	1.34
38.59	29.37	20.44	4.23	86.38	2.73	1.43	1.43
38.66	31.20	21.82	4.08	88.94	2.71	1.52	1.52
38.76	33.40	23.47	3.94	92.37	2.69	1.63	1.63
38.79	35.50	25.07	3.84	96.19	2.68	1.74	1.74
38.87	37.72	26.74	3.74	100.07	2.66	1.86	1.86
38.91	40.14	28.57	3.66	104.53	2.65	1.98	1.98
39.00	42.72	30.49	3.56	108.61	2.64	2.11	2.11
39.04	45.10	32.30	3.48	112.39	2.62	2.23	2.23
39.11	47.29	33.92	3.45	117.11	2.62	2.34	2.34
39.20	48.94	35.08	3.48	122.18	2.62	2.42	2.42
39.24	50.53	36.22	3.51	127.28	2.63	2.50	2.50
39.31	52.73	37.81	3.52	133.19	2.63	2.61	2.61
39.38	55.69	39.99	3.49	139.41	2.63	2.76	2.76
39.46	60.04	43.26	3.36	145.48	2.61	2.98	2.98
39.51	65.29	47.26	3.21	151.76	2.58	0.73	0.73
39.60	70.72	51.35	3.07	157.81	2.56	0.74	0.74
39.66	76.31	55.62	2.93	163.13	2.53	0.75	0.75
39.71	81.88	59.90	2.80	167.53	2.51	0.76	0.76
39.79	87.58	64.26	2.67	171.54	2.48	0.77	0.77
39.85	95.63	70.52	2.49	175.53	2.44	0.78	0.78
39.91	106.85	79.35	2.26	179.41	2.39	0.80	0.80
39.99	119.15	89.06	2.06	183.29	2.33	0.81	0.81
40.05	129.29	97.07	1.93	187.43	2.29	0.82	0.82
40.11	136.78	102.96	1.86	191.07	2.27	0.83	0.83
40.20	143.19	107.89	1.80	194.51	2.25	0.84	0.84
40.25	148.57	112.05	1.77	198.24	2.24	0.84	0.84
40.30	153.54	115.86	1.75	202.36	2.23	0.85	0.85
40.40	158.28	119.33	1.73	206.73	2.23	0.85	0.85
40.43	160.83	121.18	1.74	210.64	2.23	0.85	0.85
40.49	158.66	119.18	1.78	212.23	2.24	0.85	0.85
40.55	153.03	114.40	1.86	212.96	2.27	0.85	0.85
40.64	146.29	108.69	1.96	213.19	2.30	0.84	0.84
40.69	139.08	102.89	2.04	209.39	2.33	0.83	0.83
40.80	131.58	96.75	2.12	205.56	2.35	0.82	0.82
40.84	124.38	91.04	2.21	201.42	2.37	0.81	0.81
40.89	117.63	85.72	2.29	196.43	2.39	0.81	0.81
40.96	111.06	80.55	2.37	190.55	2.41	0.80	0.80

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
41.04	102.35	73.71	2.50	184.44	2.44	0.79	0.79
41.10	99.25	71.35	2.50	178.24	2.44	0.78	0.78
41.15	97.87	70.36	2.45	172.25	2.43	0.78	0.78
41.24	97.68	70.24	2.37	166.66	2.41	0.78	0.78
41.28	99.20	71.40	2.33	166.12	2.40	0.78	0.78
41.38	101.83	73.35	2.26	165.46	2.39	0.78	0.78
41.41	104.74	75.62	2.19	165.26	2.37	0.79	0.79
41.49	107.45	77.66	2.13	165.11	2.35	0.79	0.79
41.54	110.57	80.08	2.06	164.61	2.33	0.80	0.80
41.61	115.81	84.17	1.95	164.14	2.30	0.80	0.80
41.69	117.25	85.22	1.92	163.47	2.29	0.81	0.81
41.77	119.86	87.23	1.86	162.49	2.27	0.81	0.81
41.84	123.49	90.09	1.79	161.41	2.25	0.81	0.81
41.88	127.85	93.59	1.71	160.50	2.22	0.82	0.82
41.94	131.93	96.89	1.65	159.54	2.19	0.82	0.82
42.04	134.67	99.03	1.60	158.18	2.17	0.83	0.83
42.08	136.97	100.92	1.56	157.19	2.15	0.83	0.83
42.17	138.21	101.83	1.54	156.42	2.14	0.83	0.83
42.19	138.80	102.31	1.52	155.99	2.14	0.83	0.83
42.28	138.18	101.67	1.53	155.46	2.14	0.83	0.83
42.33	136.34	100.08	1.55	155.19	2.15	0.83	0.83
42.39	134.30	98.29	1.58	155.17	2.16	0.82	0.82
42.48	131.81	96.09	1.61	155.16	2.18	0.82	0.82
42.53	129.20	93.85	1.66	155.50	2.20	0.82	0.82
42.59	127.38	92.22	1.70	156.51	2.21	0.82	0.82
42.67	125.63	90.61	1.74	157.58	2.23	0.81	0.81
42.73	123.71	88.91	1.78	158.66	2.25	0.81	0.81
42.81	122.02	87.35	1.83	159.78	2.26	0.81	0.81
42.88	120.34	85.85	1.87	160.92	2.28	0.81	0.81
42.92	118.62	84.36	1.92	162.09	2.29	0.80	0.80
43.00	116.94	82.86	1.97	163.09	2.31	0.80	0.80
43.08	115.33	81.42	2.02	164.14	2.32	0.80	0.80
43.12	113.76	80.08	2.06	165.17	2.33	0.80	0.80
43.21	112.31	78.78	2.11	165.99	2.35	0.79	0.79
43.27	110.92	77.57	2.15	166.88	2.36	0.79	0.79
43.32	109.66	76.47	2.20	167.89	2.37	0.79	0.79
43.39	108.32	75.29	2.24	168.83	2.38	0.79	0.79
43.47	106.67	73.88	2.30	169.61	2.40	0.79	0.79
43.52	104.14	71.84	2.36	169.87	2.41	0.78	0.78
43.59	100.71	69.13	2.45	169.67	2.43	0.78	0.78
43.67	95.95	65.41	2.58	168.99	2.46	0.77	0.77
43.72	90.92	61.58	2.72	167.69	2.49	0.76	0.76
43.80	85.34	57.38	2.87	164.49	2.52	0.75	0.75
43.85	79.27	52.89	3.04	160.68	2.55	0.74	0.74
43.92	73.36	48.52	3.23	156.49	2.58	0.73	0.73
43.97	67.07	43.93	3.46	151.94	2.62	2.99	2.99
44.04	60.96	39.49	3.72	146.78	2.66	2.71	2.71
44.13	55.89	35.84	3.94	141.26	2.69	2.47	2.47

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
44.17	51.45	32.70	4.14	135.24	2.72	2.26	2.26
44.24	48.10	30.35	4.25	129.08	2.73	2.10	2.10
44.31	44.77	28.03	4.39	123.05	2.75	1.94	1.94
44.37	41.91	26.01	4.56	118.63	2.77	1.81	1.81
44.45	39.66	24.44	4.68	114.39	2.79	1.70	1.70
44.50	37.60	23.02	4.77	109.69	2.80	1.61	1.61
44.56	35.90	21.87	4.79	104.78	2.80	1.53	1.53
44.65	34.31	20.77	4.83	100.36	2.81	1.45	1.45
44.71	32.87	19.79	4.89	96.76	2.81	1.38	1.38
44.76	31.94	19.15	4.94	94.64	2.82	1.34	1.34
44.85	31.50	18.82	4.96	93.38	2.82	1.32	1.32
44.88	31.89	19.08	4.91	93.73	2.81	1.34	1.34
44.96	33.14	19.89	4.81	95.77	2.80	1.39	1.39
45.05	34.91	21.05	4.70	98.87	2.79	1.47	1.47
45.10	37.96	23.13	4.44	102.79	2.76	1.60	1.60
45.17	42.19	26.02	4.13	107.56	2.72	1.79	1.79
45.25	47.02	29.34	3.82	112.20	2.68	2.01	2.01
45.30	52.22	32.95	3.55	116.82	2.63	2.24	2.24
45.37	57.78	36.82	3.30	121.32	2.59	0.70	0.70
45.45	63.35	40.70	3.10	126.01	2.56	0.71	0.71
45.49	68.76	44.49	2.93	130.44	2.53	0.72	0.72
45.54	73.67	47.92	2.81	134.70	2.51	0.73	0.73
45.61	77.83	50.78	2.73	138.84	2.49	0.74	0.74
45.68	80.57	52.60	2.71	142.61	2.49	0.74	0.74
45.75	81.52	53.13	2.74	145.41	2.49	0.74	0.74
45.80	81.02	52.66	2.79	147.01	2.50	0.74	0.74
45.89	79.02	51.09	2.88	147.36	2.52	0.74	0.74
45.93	75.96	48.83	3.01	146.80	2.54	0.73	0.73
46.01	71.99	45.92	3.16	145.23	2.57	0.72	0.72
46.08	67.58	42.73	3.35	143.16	2.60	2.89	2.89
46.15	63.04	39.49	3.56	140.53	2.64	2.68	2.68
46.20	58.87	36.55	3.75	137.15	2.67	2.49	2.49
46.29	55.12	33.92	3.93	133.38	2.69	2.32	2.32
46.34	52.58	32.18	4.02	129.41	2.70	2.21	2.21
46.41	51.11	31.17	4.05	126.27	2.71	2.14	2.14
46.49	50.54	30.77	4.03	124.04	2.70	2.11	2.11
46.53	50.02	30.42	4.02	122.34	2.70	2.09	2.09
46.60	49.69	30.18	4.00	120.82	2.70	2.07	2.07
46.69	49.41	29.96	3.98	119.37	2.70	2.05	2.05
46.73	49.11	29.76	3.97	118.07	2.70	2.04	2.04
46.79	48.28	29.16	4.02	117.13	2.70	2.00	2.00
46.89	47.27	28.41	4.09	116.30	2.71	1.95	1.95
46.94	45.73	27.31	4.25	116.20	2.73	1.88	1.88
46.99	44.21	26.21	4.47	117.04	2.76	1.81	1.81
47.09	42.89	25.21	4.68	118.10	2.79	1.75	1.75
47.13	41.81	24.41	4.89	119.40	2.81	1.70	1.70
47.19	42.93	25.12	4.82	121.09	2.80	1.75	1.75
47.28	44.62	26.20	4.68	122.72	2.79	1.82	1.82

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
47.34	47.80	28.32	4.41	124.80	2.75	1.96	1.96
47.38	54.01	32.56	3.90	127.10	2.69	2.22	2.22
47.50	61.85	37.94	3.40	129.13	2.61	2.56	2.56
47.51	72.72	45.60	2.88	131.32	2.52	0.72	0.72
47.60	84.57	54.02	2.47	133.24	2.44	0.74	0.74
47.69	97.97	63.68	2.13	135.74	2.35	0.77	0.77
47.70	112.59	74.42	1.87	139.45	2.28	0.79	0.79
47.80	125.94	84.20	1.71	143.67	2.22	0.80	0.80
47.84	139.39	94.21	1.58	148.64	2.16	0.82	0.82
47.91	151.60	103.34	1.48	153.39	2.12	0.83	0.83
48.00	161.22	110.51	1.42	157.32	2.08	0.84	0.84
48.04	168.84	116.26	1.38	160.83	2.06	0.85	0.85
48.11	173.11	119.39	1.36	162.82	2.05	0.85	0.85
48.19	175.86	121.33	1.35	164.25	2.04	0.85	0.85
48.23	176.73	121.85	1.35	165.07	2.04	0.86	0.86
48.30	176.31	121.32	1.36	165.40	2.04	0.85	0.85
48.40	175.47	120.40	1.38	165.61	2.05	0.85	0.85
48.45	174.20	119.22	1.39	165.83	2.06	0.85	0.85
48.50	172.99	118.09	1.41	166.15	2.07	0.85	0.85
48.59	172.02	117.09	1.42	166.44	2.08	0.85	0.85
48.66	171.41	116.42	1.43	166.75	2.09	0.85	0.85
48.69	171.02	116.01	1.44	167.02	2.09	0.85	0.85
48.78	170.78	115.63	1.45	167.11	2.09	0.85	0.85
48.85	170.69	115.43	1.45	167.08	2.10	0.85	0.85
48.89	170.46	115.19	1.45	166.89	2.10	0.85	0.85
48.98	170.14	114.81	1.45	166.50	2.10	0.85	0.85
49.03	169.85	114.51	1.45	166.24	2.10	0.85	0.85
49.09	170.04	114.53	1.45	166.41	2.10	0.85	0.85
49.19	170.33	114.54	1.46	166.69	2.10	0.85	0.85
49.23	170.93	114.85	1.46	167.48	2.10	0.85	0.85
49.28	172.83	116.08	1.46	169.12	2.10	0.85	0.85
49.39	175.13	117.50	1.45	170.85	2.10	0.85	0.85
49.42	177.65	119.21	1.45	172.90	2.10	0.85	0.85
49.49	180.57	121.19	1.44	174.81	2.09	0.85	0.85
49.59	183.31	123.06	1.43	175.79	2.09	0.86	0.86
49.62	185.69	124.84	1.41	176.44	2.08	0.86	0.86
49.69	187.40	126.08	1.40	176.46	2.07	0.86	0.86
49.74	188.52	127.02	1.38	175.46	2.06	0.86	0.86
49.83	188.92	127.47	1.36	173.39	2.04	0.86	0.86
49.88	187.83	126.90	1.34	170.54	2.03	0.86	0.86
49.93	185.76	125.55	1.33	167.52	2.03	0.86	0.86
50.03	183.09	123.66	1.33	164.16	2.02	0.86	0.86
50.13	179.38	120.92	1.33	160.78	2.02	0.85	0.85
50.14	175.33	117.93	1.34	158.34	2.03	0.85	0.85
50.23	171.23	114.71	1.36	156.17	2.04	0.85	0.85
50.27	166.80	111.30	1.39	154.26	2.06	0.84	0.84
50.34	161.56	107.09	1.43	153.13	2.09	0.84	0.84
50.43	155.42	102.13	1.49	152.59	2.12	0.83	0.83

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
50.49	148.95	97.05	1.57	152.09	2.16	0.82	0.82
50.53	142.05	91.83	1.64	150.66	2.19	0.82	0.82
50.62	134.51	86.16	1.73	148.86	2.22	0.81	0.81
50.68	127.42	80.95	1.81	146.80	2.26	0.80	0.80
50.73	120.26	75.84	1.89	143.66	2.28	0.79	0.79
50.82	113.01	70.70	1.98	139.77	2.31	0.78	0.78
50.88	106.07	65.87	2.06	135.47	2.33	0.77	0.77
50.93	99.91	61.68	2.12	130.70	2.35	0.76	0.76
51.02	94.44	57.95	2.17	125.94	2.36	0.75	0.75
51.09	89.17	54.38	2.24	121.63	2.38	0.75	0.75
51.12	83.92	50.82	2.33	118.24	2.40	0.74	0.74
51.19	78.60	47.16	2.45	115.41	2.43	0.73	0.73
51.28	73.22	43.44	2.61	113.38	2.47	0.72	0.72
51.32	68.33	40.10	2.79	111.88	2.50	0.71	0.71
51.39	64.21	37.28	2.95	110.12	2.54	0.70	0.70
51.48	60.31	34.64	3.13	108.49	2.57	0.69	0.69
51.53	56.31	31.96	3.35	107.03	2.60	2.13	2.13
51.62	52.17	29.22	3.58	104.75	2.64	1.96	1.96
51.68	48.21	26.65	3.82	101.81	2.68	1.80	1.80
51.73	45.05	24.64	4.00	98.61	2.70	1.67	1.67
51.82	42.62	23.13	4.09	94.59	2.71	1.57	1.57
51.87	40.63	21.96	4.07	89.44	2.71	1.49	1.49
51.92	38.75	20.83	4.09	85.24	2.71	1.42	1.42
51.97	36.63	19.52	4.21	82.16	2.73	1.33	1.33
52.04	34.50	18.20	4.35	79.17	2.75	1.25	1.25
52.12	32.86	17.19	4.44	76.28	2.76	1.18	1.18
52.18	31.94	16.63	4.46	74.17	2.76	1.14	1.14
52.23	31.17	16.17	4.47	72.25	2.76	1.11	1.11
52.31	30.59	15.81	4.47	70.63	2.76	1.09	1.09
52.37	30.00	15.45	4.50	69.47	2.77	0.33	1.06
52.44	29.15	14.92	4.59	68.42	2.78	0.32	1.03
52.53	28.21	14.32	4.69	67.11	2.79	0.30	0.99
52.57	27.07	13.61	4.83	65.80	2.81	0.30	0.94
52.64	25.80	12.83	5.02	64.33	2.83	0.29	0.89
52.72	24.50	12.02	5.22	62.73	2.85	0.25	0.84
52.78	23.17	11.20	5.44	61.00	2.87	0.23	0.79
52.83	21.95	10.48	5.61	58.82	2.89	0.21	0.74
52.93	20.80	9.79	5.79	56.64	2.91	0.19	0.69
52.96	19.98	9.31	5.88	54.75	2.92	0.18	0.66
53.04	19.46	9.00	5.93	53.36	2.92	0.16	0.64
53.12	19.06	8.76	5.96	52.22	2.93	0.11	0.62
53.17	18.87	8.66	5.93	51.39	2.92	0.12	0.61
53.22	18.81	8.63	5.89	50.85	2.92	0.14	0.61
53.29	18.81	8.63	5.83	50.31	2.91	0.15	0.61
53.37	18.84	8.64	5.78	49.99	2.91	0.15	0.61
53.42	18.86	8.64	5.82	50.29	2.91	0.15	0.61
53.49	18.87	8.63	5.84	50.42	2.91	0.15	0.61
53.58	18.87	8.62	5.83	50.25	2.91	0.14	0.61

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
53.63	18.86	8.62	5.79	49.93	2.91	0.14	0.61
53.68	18.86	8.62	5.76	49.62	2.91	0.14	0.61
53.78	18.86	8.61	5.71	49.21	2.90	0.13	0.61
53.84	18.85	8.61	5.68	48.88	2.90	0.12	0.61
53.88	18.83	8.59	5.66	48.64	2.90	0.12	0.61
53.94	18.84	8.60	5.63	48.39	2.89	0.12	0.61
54.03	18.88	8.61	5.61	48.30	2.89	0.12	0.61
54.08	18.95	8.65	5.58	48.29	2.89	0.12	0.61
54.16	19.04	8.69	5.59	48.52	2.89	0.12	0.61
54.20	19.16	8.75	5.57	48.76	2.89	0.12	0.62
54.28	19.40	8.88	5.51	48.91	2.88	0.13	0.62
54.35	19.73	9.07	5.41	49.08	2.87	0.13	0.64
54.43	20.10	9.29	5.30	49.24	2.86	0.14	0.65
54.48	20.43	9.48	5.19	49.24	2.85	0.14	0.66
54.55	20.63	9.61	5.12	49.16	2.84	0.13	0.67
54.63	20.78	9.69	5.05	48.99	2.83	0.13	0.67
54.67	20.84	9.73	5.02	48.82	2.83	0.13	0.68
54.74	20.86	9.74	4.96	48.33	2.82	0.12	0.68
54.82	20.83	9.72	4.92	47.83	2.82	0.12	0.67
54.87	20.69	9.64	4.92	47.41	2.82	0.12	0.67
54.92	20.46	9.49	4.97	47.15	2.82	0.12	0.66
55.02	20.18	9.31	5.05	46.96	2.83	0.11	0.65
55.06	19.93	9.14	5.17	47.27	2.84	0.11	0.64
55.14	19.85	9.06	5.28	47.81	2.86	0.11	0.63
55.22	19.85	9.03	5.38	48.59	2.87	0.12	0.63
55.27	20.07	9.13	5.43	49.60	2.87	0.12	0.64
55.37	20.38	9.28	5.48	50.87	2.88	0.14	0.65
55.42	20.73	9.45	5.52	52.18	2.88	0.15	0.66
55.47	21.01	9.58	5.57	53.37	2.89	0.17	0.67
55.53	21.18	9.65	5.62	54.26	2.89	0.19	0.68
55.58	21.32	9.71	5.66	54.99	2.90	0.20	0.69
55.67	21.43	9.75	5.67	55.30	2.90	0.20	0.69
55.72	21.47	9.77	5.67	55.36	2.90	0.20	0.69
55.81	21.47	9.76	5.65	55.13	2.90	0.19	0.69
55.86	21.33	9.68	5.64	54.58	2.89	0.18	0.68
55.92	21.20	9.60	5.66	54.29	2.90	0.17	0.68
56.01	21.13	9.54	5.69	54.26	2.90	0.16	0.67
56.05	21.34	9.65	5.67	54.73	2.90	0.15	0.68
56.11	21.83	9.91	5.66	56.06	2.90	0.14	0.70
56.21	22.16	10.04	5.77	57.94	2.91	0.17	0.71
56.26	22.93	10.44	5.78	60.32	2.91	0.20	0.74
56.32	24.21	11.14	5.67	63.19	2.90	0.23	0.79
56.41	25.83	12.03	5.50	66.12	2.88	0.29	0.85
56.46	27.60	13.03	5.29	68.96	2.86	0.34	0.91
56.50	29.45	14.10	5.05	71.15	2.83	0.98	0.98
56.59	31.25	15.12	4.85	73.31	2.81	1.05	1.05
56.65	32.82	16.01	4.71	75.45	2.79	1.10	1.10
56.70	34.20	16.78	4.65	78.08	2.78	1.15	1.15

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
56.78	36.90	18.34	4.40	80.75	2.75	1.25	1.25
56.85	39.96	20.15	4.14	83.47	2.72	1.37	1.37
56.89	43.42	22.21	3.89	86.30	2.68	1.49	1.49
56.98	46.67	24.13	3.70	89.17	2.66	1.61	1.61
57.04	49.64	25.88	3.57	92.28	2.64	1.72	1.72
57.09	52.24	27.37	3.50	95.85	2.63	1.82	1.82
57.16	54.64	28.73	3.45	99.15	2.62	1.90	1.90
57.24	57.27	30.26	3.37	101.95	2.61	2.00	2.00
57.29	60.78	32.45	3.18	103.21	2.58	0.68	0.68
57.37	63.44	34.10	3.04	103.78	2.55	0.69	0.69
57.42	65.25	35.24	2.95	103.95	2.53	0.69	0.69
57.49	65.85	35.59	2.92	103.82	2.53	0.69	0.69
57.59	66.05	35.68	2.90	103.46	2.53	0.69	0.69
57.64	65.55	35.37	2.90	102.67	2.53	0.69	0.69
57.69	64.18	34.52	2.93	101.10	2.53	0.69	0.69
57.77	62.46	33.48	2.95	98.82	2.54	0.68	0.68
57.82	59.62	31.73	3.03	96.27	2.55	0.68	0.68
57.89	55.11	28.91	3.25	93.85	2.59	0.67	0.67
57.97	50.06	25.76	3.55	91.40	2.64	1.71	1.71
58.03	44.69	22.48	3.94	88.53	2.69	1.51	1.51
58.09	39.45	19.34	4.38	84.77	2.75	1.32	1.32
58.17	34.44	16.39	4.91	80.43	2.81	1.13	1.13
58.21	30.20	13.95	5.43	75.82	2.87	0.98	0.98
58.28	27.04	12.17	5.86	71.37	2.92	0.86	0.86
58.37	24.54	10.77	6.33	68.16	2.96	0.25	0.77
58.40	22.95	9.96	6.65	66.27	2.99	0.23	0.71
58.48	22.15	9.54	6.96	66.39	3.02	0.20	0.68
58.53	22.64	9.78	6.94	67.91	3.02	0.19	0.70
58.63	24.67	10.80	6.46	69.73	2.97	0.26	0.77
58.67	27.06	12.07	5.95	71.85	2.93	0.86	0.86
58.73	29.10	13.23	5.58	73.85	2.89	0.93	0.93
58.82	30.69	14.10	5.37	75.70	2.87	0.99	0.99
58.89	31.56	14.56	5.29	77.01	2.86	1.02	1.02
58.93	31.85	14.72	5.25	77.30	2.85	1.03	1.03
59.00	31.94	14.76	5.21	76.96	2.85	1.03	1.03
59.06	31.98	14.82	5.08	75.29	2.83	1.03	1.03
59.13	30.97	14.30	5.05	72.23	2.83	0.99	0.99
59.22	28.79	13.06	5.30	69.22	2.86	0.30	0.91
59.28	26.42	11.72	5.66	66.38	2.90	0.29	0.83
59.33	24.42	10.60	6.00	63.61	2.93	0.25	0.75
59.41	23.06	9.86	6.19	61.04	2.95	0.21	0.70
59.47	22.47	9.55	6.20	59.23	2.95	0.20	0.68
59.52	22.50	9.59	6.06	58.08	2.94	0.19	0.68
59.61	22.85	9.81	5.83	57.18	2.91	0.18	0.69
59.67	23.26	10.05	5.66	56.84	2.90	0.18	0.71
59.72	23.81	10.35	5.55	57.41	2.88	0.19	0.73
59.78	24.44	10.69	5.46	58.31	2.87	0.20	0.75
59.87	25.08	11.02	5.36	59.13	2.87	0.20	0.77

:: Strength loss calculation (Robertson (2009) :: (continued)

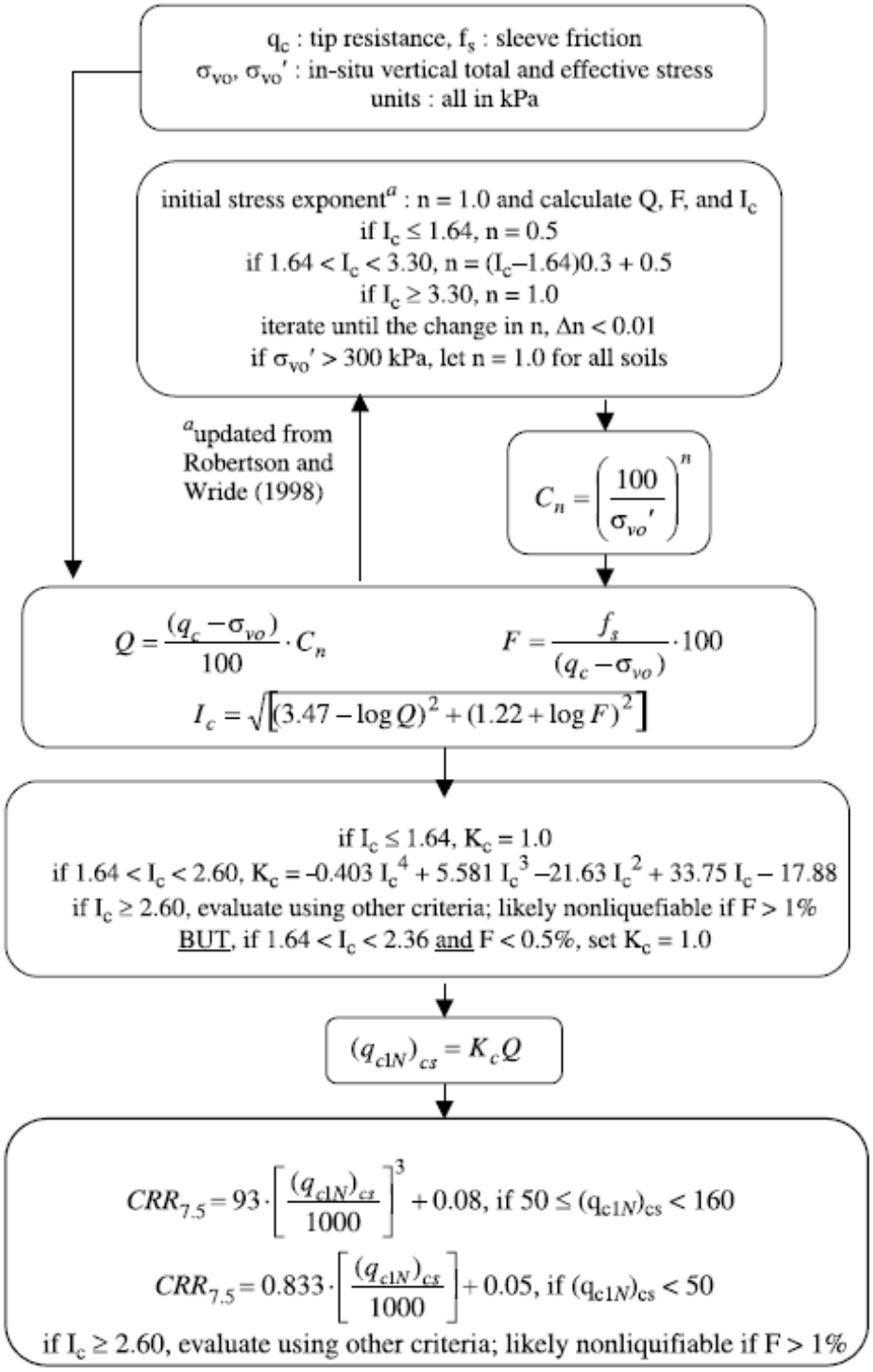
Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
59.92	25.83	11.52	4.95	57.00	2.82	0.22	0.80
60.00	26.38	11.92	4.59	54.71	2.78	0.25	0.82
60.05	26.95	12.34	4.23	52.22	2.73	0.27	0.84
60.11	27.25	12.61	3.92	49.42	2.69	0.26	0.85
60.21	27.38	12.81	3.61	46.28	2.64	0.00	0.85
60.25	27.51	13.05	3.26	42.60	2.59	0.05	0.57
60.31	27.68	13.38	2.84	37.95	2.51	0.04	0.58
60.40	27.58	13.65	2.36	32.18	2.41	0.04	0.58
60.43	27.43	-1.00	1.00	-1.00	-1.00	N/A	N/A
60.51	27.37	-1.00	1.00	-1.00	-1.00	N/A	N/A

Abbreviations

q_t: Total cone resistance
K_c: Cone resistance correction factor due to fines
$Q_{tn,cs}$: Adjusted and corrected cone resistance due to fines
I_c: Soil behavior type index
$S_{u(liq)}/\sigma'_v$: Calculated liquefied undrained strength ratio
$S_{u(peak)}/\sigma'_v$: Calculated peak undrained strength ratio

Procedure for the evaluation of soil liquefaction resistance, NCEER (1998)

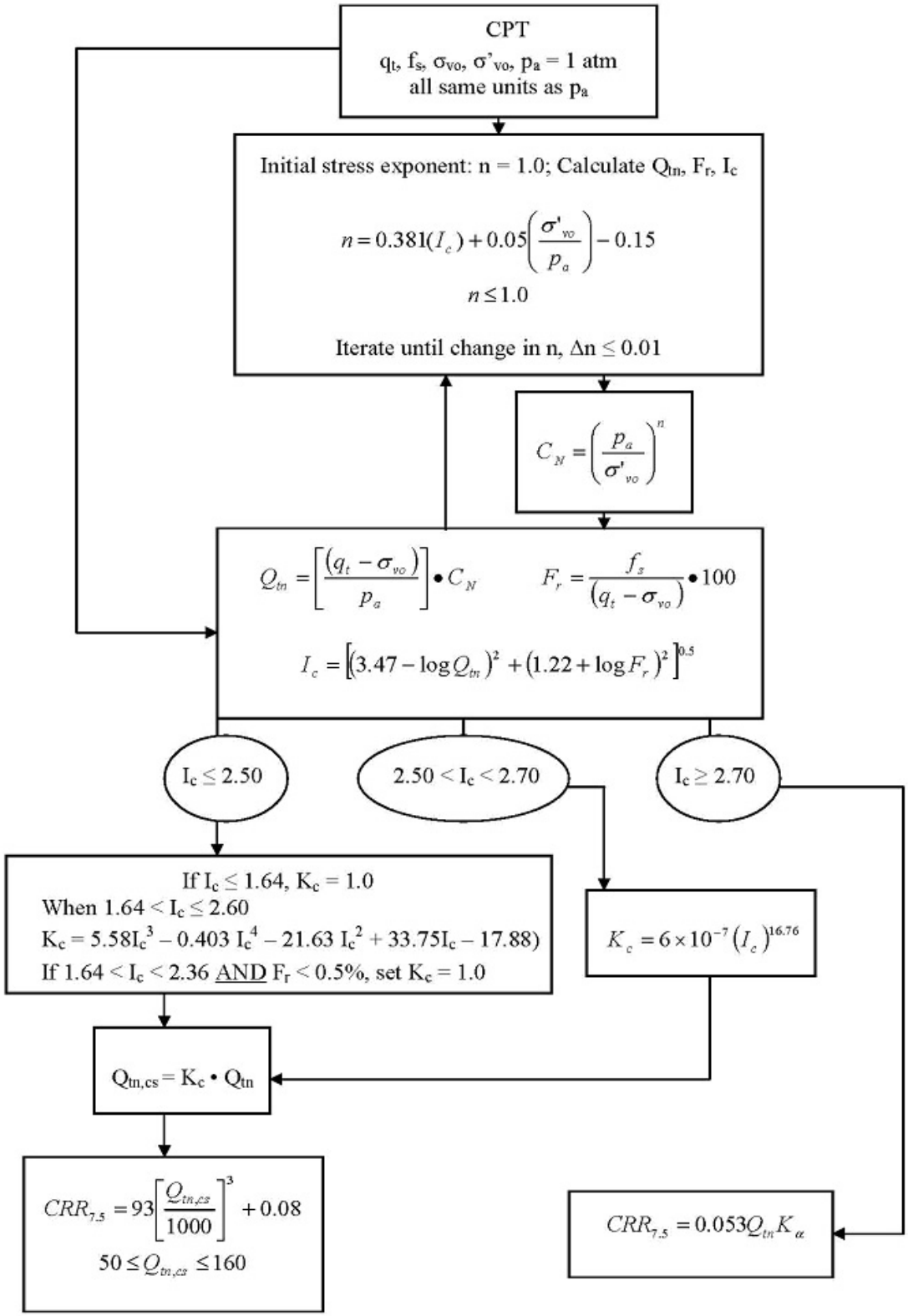
Calculation of soil resistance against liquefaction is performed according to the Robertson & Wride (1998) procedure. The procedure used in the software, slightly differs from the one originally published in NCEER-97-0022 (Proceedings of the NCEER Workshop on Evaluation of Liquefaction Resistance of Soils). The revised procedure is presented below in the form of a flowchart[1]:



[1] "Estimating liquefaction-induced ground settlements from CPT for level ground", G. Zhang, P.K. Robertson, and R.W.I. Brachman

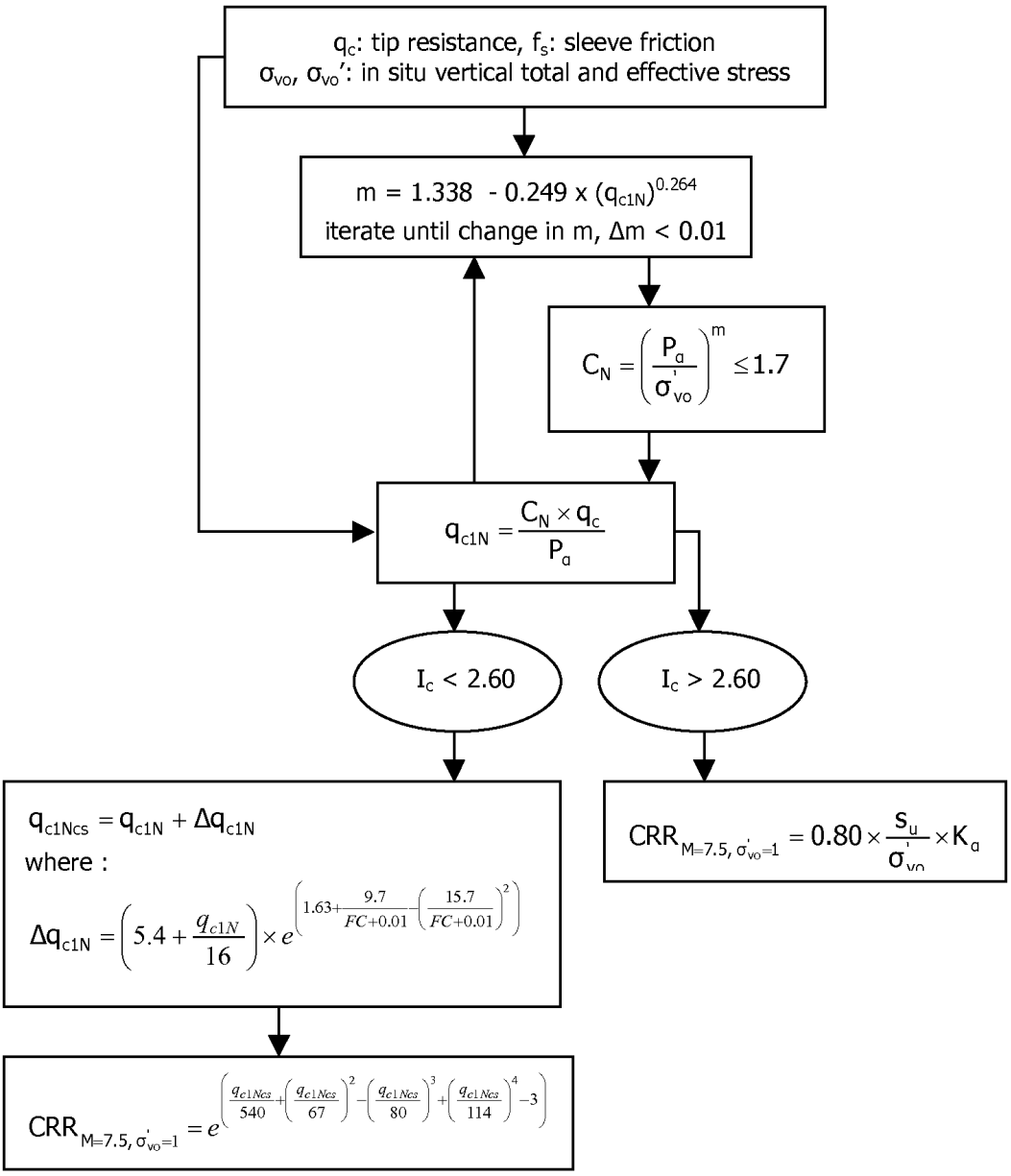
Procedure for the evaluation of soil liquefaction resistance (all soils), Robertson (2010)

Calculation of soil resistance against liquefaction is performed according to the Robertson & Wride (1998) procedure. This procedure used in the software, slightly differs from the one originally published in NCEER-97-0022 (Proceedings of the NCEER Workshop on Evaluation of Liquefaction Resistance of Soils). The revised procedure is presented below in the form of a flowchart[1]:

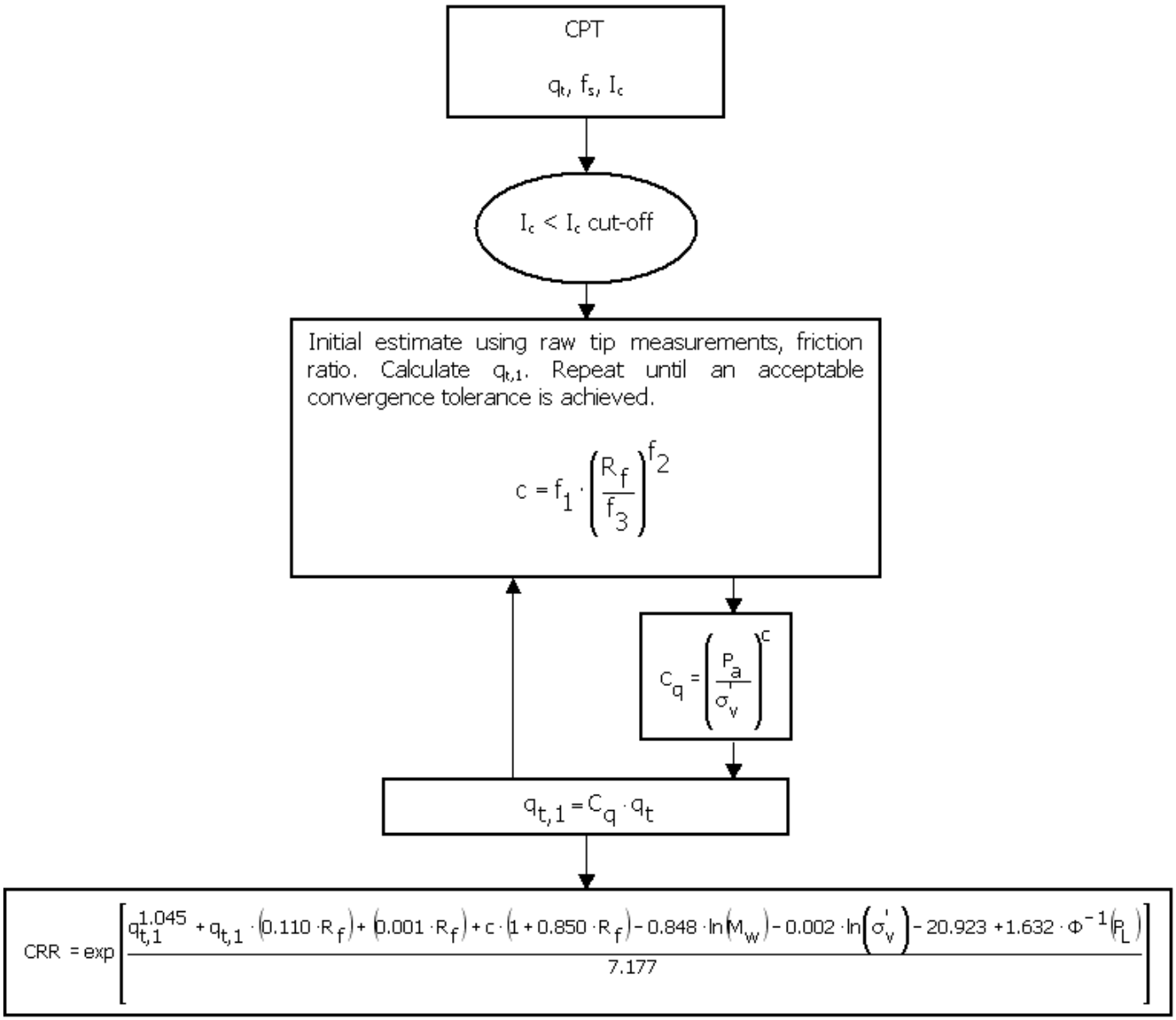


[1] P.K. Robertson, 2009. "Performance based earthquake design using the CPT", Keynote Lecture, International Conference on Performance-based Design in Earthquake Geotechnical Engineering – from case history to practice, IS-Tokyo, June 2009

Procedure for the evaluation of soil liquefaction resistance, Idriss & Boulanger (2008)



Procedure for the evaluation of soil liquefaction resistance (sandy soils), Moss et al. (2006)



Procedure for the evaluation of soil liquefaction resistance, Boulanger & Idriss(2014)

$$FS_{liq} = \frac{CRR_{M=7.5,\sigma'_v=1atm}}{CSR_{M=7.5,\sigma'_v=1atm}}$$

$$CSR_{M=7.5,\sigma'_v=1atm} = 0.65 \frac{\sigma_v}{\sigma'_v} \frac{a_{max}}{g} r_d \frac{1}{MSF} \frac{1}{K_\sigma}$$

$$r_d = \exp\left[\alpha(z) + \beta(z) \cdot M\right]$$

$$\alpha(z) = -1.012 - 1.126 \sin\left(\frac{z}{11.73} + 5.133\right)$$

$$\beta(z) = 0.106 + 0.118 \sin\left(\frac{z}{11.28} + 5.142\right)$$

$$K_\sigma = 1 - C_\sigma \ln\left(\frac{\sigma'_v}{P_a}\right) \le 1.1$$

$$C_\sigma = \frac{1}{37.3 - 8.27\left(q_{c1Ncs}\right)^{0.264}} \le 0.3$$

$$MSF = 1 + \left(MSF_{max} - 1\right)\left(8.64 \exp\left(\frac{-M}{4}\right) - 1.325\right)$$

$$MSF_{max} = 1.09 + \left(\frac{q_{C1Ncs}}{180}\right)^3 \le 2.2$$

σ'_v *and* σ_v *at start of earthquake shaking*

$$CRR_{M=7.5,\sigma'_v=1atm} = \exp\left(\frac{q_{c1Ncs}}{113} + \left(\frac{q_{c1Ncs}}{1000}\right)^2 - \left(\frac{q_{c1Ncs}}{140}\right)^3 + \left(\frac{q_{c1Ncs}}{137}\right)^4 - 2.80\right)$$

$$q_{c1Ncs} = q_{c1N} + \Delta q_{c1N}$$

$$\Delta q_{c1N} = \left(11.9 + \frac{q_{c1N}}{14.6}\right) \exp\left(1.63 - \frac{9.7}{FC+2} - \left(\frac{15.7}{FC+2}\right)^2\right)$$

$$q_{c1N} = C_{Ne} \frac{q_c}{P_a}$$

$$C_{Ne} = \left(\frac{P_a}{\sigma'_v}\right)^m \le 1.7$$

$$m = 1.338 - 0.249\left(q_{c1Ncs}\right)^{0.264} \quad with \quad 0.264 \le m \le 0.782$$

$$FC = 80\left(I_C + C_{FC}\right) - 137 \quad with \quad 0\% \le FC \le 100\%$$

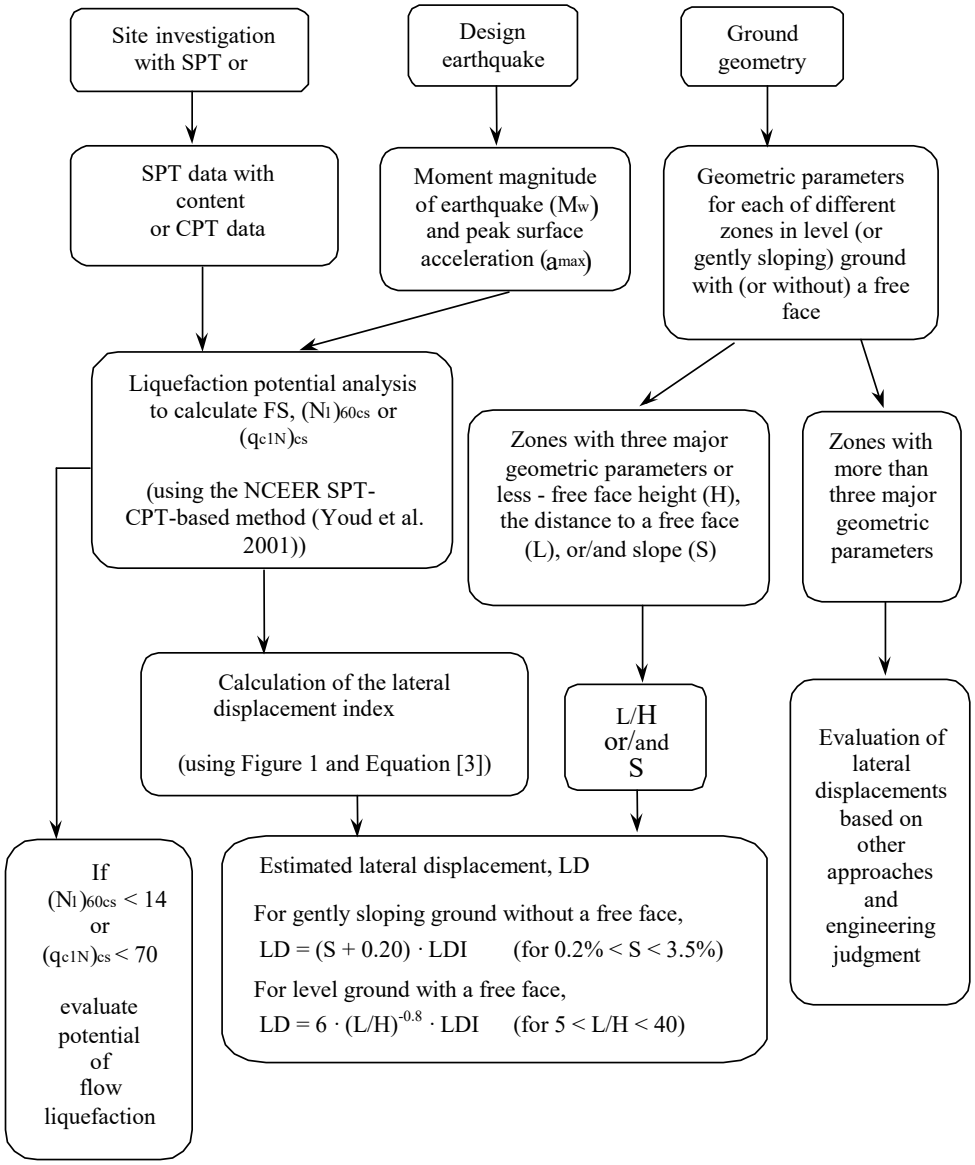
$$I_c = \left[\left(3.47 - \log\left(Q\right)\right)^2 + \left(1.22 + \log\left(F\right)\right)^2\right]^{0.5}$$

$$Q = \left(\frac{q_c - \sigma_{vc}}{P_a}\right)\left(\frac{P_a}{\sigma'_{vc}}\right)^n \; with \; 0.5 \le n \le 1.0 \; per \; Robertson \; \& \; Wride \; (1998)$$

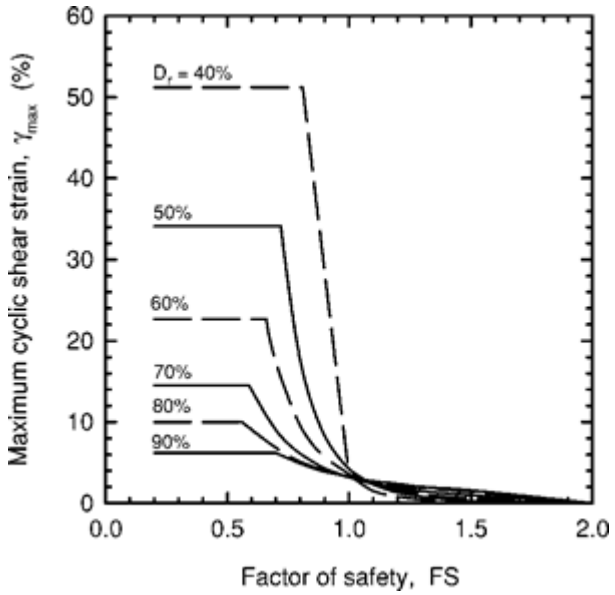
$$F = \left(\frac{f_s}{q_c - \sigma_{vc}}\right) \cdot 100\%$$

σ'_v *at time of CPT sounding*

Procedure for the evaluation of liquefaction-induced lateral spreading displacements



[1] Flow chart illustrating major steps in estimating liquefaction-induced lateral spreading displacements using the proposed approach



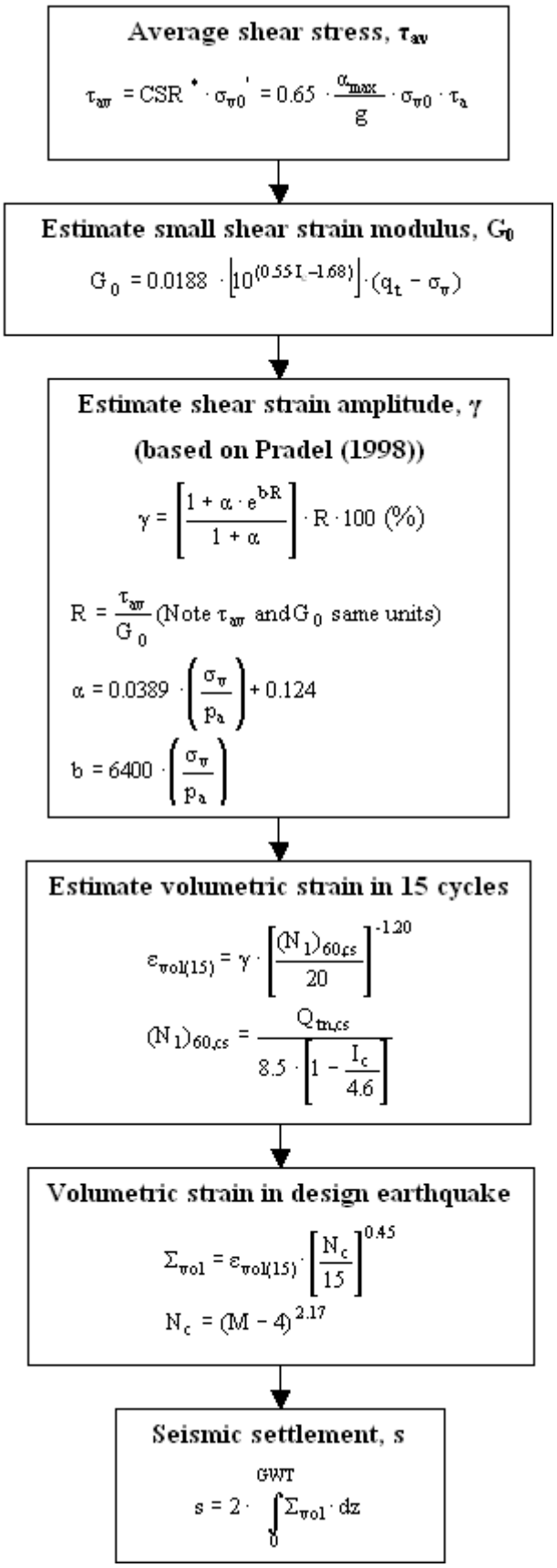
[1] Figure 1

$$LDI = \int_0^{z_{max}} \gamma_{max} dz$$

[1] Equation [3]

[1] "Estimating liquefaction-induced ground settlements from CPT for level ground", G. Zhang, P.K. Robertson, and R.W.I. Brachman

Procedure for the estimation of seismic induced settlements in dry sands



Robertson, P.K. and Lisheng, S., 2010, "Estimation of seismic compression in dry soils using the CPT" FIFTH INTERNATIONAL CONFERENCE ON RECENT ADVANCES IN GEOTECHNICAL EARTHQUAKE ENGINEERING AND SOIL DYNAMICS, Symposium in honor of professor I. M. Idriss, San Diego, CA

Liquefaction Potential Index (LPI) calculation procedure

Calculation of the Liquefaction Potential Index (LPI) is used to interpret the liquefaction assessment calculations in terms of severity over depth. The calculation procedure is based on the methology developed by Iwasaki (1982) and is adopted by AFPS.

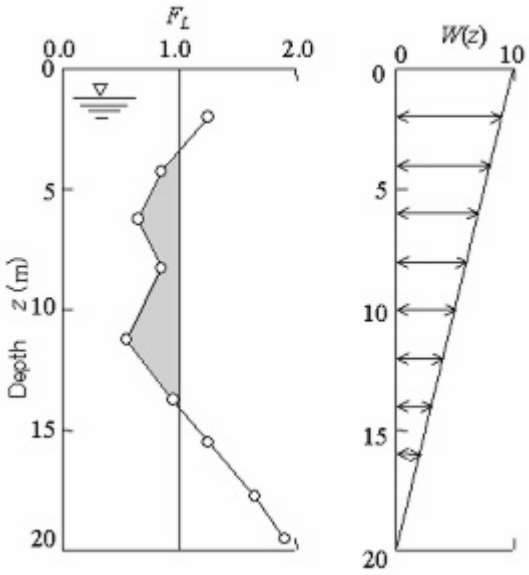
To estimate the severity of liquefaction extent at a given site, LPI is calculated based on the following equation:

$$\mathbf{LPI} = \int_0^{20} (10 - 0{,}5z) \times F_L \times dz$$

where:
F_L = 1 - F.S. when F.S. less than 1
F_L = 0 when F.S. greater than 1
z depth of measurment in meters

Values of LPI range between zero (0) when no test point is characterized as liquefiable and 100 when all points are characterized as susceptible to liquefaction. Iwasaki proposed four (4) discrete categories based on the numeric value of LPI:

- LPI = 0 : Liquefaction risk is very low
- 0 < LPI <= 5 : Liquefaction risk is low
- 5 < LPI <= 15 : Liquefaction risk is high
- LPI > 15 : Liquefaction risk is very high



Graphical presentation of the LPI calculation procedure

Shear-Induced Building Settlement (Ds) calculation procedure

The shear-induced building settlement (Ds) due to liquefaction below the building can be estimated using the relationship developed by Bray and Macedo (2017):

$$Ln(Ds) = c1 + c2 * LBS + 0.58 * Ln\left(Tanh\left(\frac{HL}{6}\right)\right) + 4.59 * Ln(Q) - 0.42 * Ln(Q)^2 - 0.02 * B + 0.84 * Ln(CAVdp) + 0.41 * Ln(Sa1) + \varepsilon$$

where Ds is in the units of mm, c1= -8.35 and c2= 0.072 for LBS ≤ 16, and c1= -7.48 and c2= 0.014 otherwise. Q is the building contact pressure in units of kPa, HL is the cumulative thickness of the liquefiable layers in the units of m, B is the building width in the units of m, CAVdp is a standardized version of the cumulative absolute velocity in the units of g-s, Sa1 is 5%-damped pseudo-acceleration response spectral value at a period of 1 s in the units of g, and ε is a normal random variable with zero mean and 0.50 standard deviation in Ln units. The liquefaction-induced building settlement index (LBS) is:

$$LBS = \sum W * \frac{\varepsilon_{shear}}{z} dz$$

where z (m) is the depth measured from the ground surface > 0, W is a foundation-weighting factor wherein W = 0.0 for z less than Df, which is the embedment depth of the foundation, and W = 1.0 otherwise. The shear strain parameter (ε_shear) is the liquefaction-induced free-field shear strain (in %) estimated using Zhang et al. (2004). It is calculated based on the estimated Dr of the liquefied soil layer and the calculated safety factor against liquefaction triggering (FSL).

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