LANDS OF BUTLER

New Vineyard Development Hydrologic Analysis

Property Information:

Owner: Jeff Butler Parcel No.: 033-190-006



Report Preparer Information:

Civil Engineer: Omar Reveles, PE R.C.E. 74723

Acme Engineering Inc.

Contact: 1700 Soscol Avenue, Suite 9

Napa, CA 94559 (707) 253-2263

Date: November 5, 2020



Project Narrative

Introduction and Scope of Project

This project proposes the development of approximately 5.1 acres of vineyard (comprised of 3.3 acres of vineyard and 1.8 acres of vineyard avenues) at APN: 033-190-006 in Napa, CA. The property is owned by Jeff Butler and measures approximately 10.1 acres. Vineyard development activities shall consist of: land clearing and tree removal, ripping, incorporation of soil amendments, disking, installation of deer fence, vineyard planting, trellising, installation of a drip irrigation system and cover cropping. The proposed development activities shall begin upon approval from the Napa County Department of Planning, Building & Environmental Services and shall be completed by October 15, 2021.

Existing Conditions

The project site is located within the Suisun Creek watershed. The project site lies immediately east and west of Twin Sisters Road. The project site currently consists mostly of oak woodland and non-native grassland. Portions of the property in the immediate vicinity consist mostly of trees, grasses and herbaceous weeds. The project site consists of moderate to strong sloping terrain (13-26%). Slopes surrounding the development areas are similar to those inside.

The project site is part of an overall watershed (watersheds A-H) that measures approximately 8.54 acres and consists of approximately 2.52 acres of tree canopy, approximately 5.77 acres of grass/weeds, and approximately 0.25 acres of gravel roadways. The overall watershed consists of three sub-watersheds that combine and drain into a seasonal drainage path downslope from the proposed development area. The remaining five watersheds leave the overall watershed separately, either as sheet flow, shallow concentrated flow or through existing culverts. Eventually runoff from the overall watershed makes its way to Wooden Valley Creek, then to Suisun Creek and finally drains into Suisun Marsh.

In watersheds A, B, C, E and F, runoff occurs as sheet flow, shallow concentrated flow and channel flow. Additionally, in watersheds D, G, and H, runoff occurs as sheet flow and shallow concentrated flow only. The runoff from watersheds A and F leaves through existing culverts. The runoff from watersheds D and H leaves the site as shallow concentrated flow. The runoff from watershed G leaves the site as sheet flow. The runoff from watersheds B, C and E combine and leave the site as channel flow.

Methodologies

In order to evaluate the hydrologic impact of the proposed development, two watershed runoff models were developed using the NRCS United States Department of Agriculture (USDA) Technical Release 55 (TR-55) methodology (USDA-NRCS 2003). WinTR-55 is single-event rainfall-runoff, small watershed hydrologic model. The model generates hydrographs from both urban and agricultural areas and at selected points along the stream system. Hydrographs are routed downstream through channels and/or reservoirs. Multiple sub-areas can be modeled within the watershed. The WinTR-55 methodology was used to generate peak flow estimates for the project site.

TR-55 only allows the modeling of reaches with trapezoidal flow areas. In order to model the drainage mainline addition, the bottom width and average side slopes for Reach 2 were modified such that the flow velocity at 0.5 ft depth matched the velocity of a 12" corrugated plastic pipe with a flow depth of 0.5 ft.

This methodology was applied to the entire effective watersheds. It was used to determine the predevelopment and post-development peak flow rates for the 2, 5, 10, 25, 50 and 100 year return period 24 hour storm events.

Assumptions

As previously mentioned there are several existing drainage swales and culverts along Twin Sisters Road. The intent of this project is to maintain the existing flow regimes to the maximum extent practicable. As a result all existing drainage swales and culverts shall be maintained or replaced if needed.

Hydrologic soil groups are based on estimates of runoff potential. This parameter is based on the type of soil encountered. Based on the interactive web soil survey found at:

https://websoilsurvey.sc.egov.usda.gov/App/HomePage.htm there is only one soil type within the project site. The soil type present is Hambright Loam (HaFso). Hambright Loam is classified as a soil in hydrologic group "D". Additionally, within the overall watershed boundaries there is an additional soil type present. This soil type is Sobrante Loam. Sobrante Loam is classified as a soil in hydrologic group "C". In an effort to simplify the analysis, hydrologic soil group "D" was used for the overall watershed, including the small portion that extends into the Sobrante Loam. This assumption is justified because the area in question is outside of the proposed development boundary and will remain unchanged between pre and post development conditions.

The determination of the hydrologic soil conditions was based on the observed canopy and surface cover conditions. For watersheds A, B, C and D a "good" hydrologic soil condition was selected for "pasture, grasslands or range" and "woods - grass combination" within the areas that are currently not developed. For watersheds E, F, G and H a "fair" hydrologic soil condition was selected for "pasture, grasslands or range" and "woods - grass combination" within the areas that are currently not developed. A "good" hydrologic soil condition was selected for "pasture, grasslands or range" within the areas of the proposed vineyard. A good hydrologic soil condition for the proposed and existing vineyard is justified by all the land preparation, cover cropping and straw mulching associated with the proposed development.

Finally, based on the hydrologic soil-cover complex definitions: "pasture, grasslands or range" land use was selected for the proposed vineyard areas. The selected land use is the one that most closely resembles the proposed cover crop seed mix and anticipated farming practices.

Impacts

The proposed development project shall not have any negative impacts on the project site. This is due to the fact that the proposed development shall not adversely affect any of the hydrologic characteristics. Currently, runoff flows across the project site as sheet flow, shallow concentrated flow and channel flow.

Currently, a culvert conveys runoff from watersheds B to watershed C and an additional culvert conveys runoff from watersheds B and C under Twin Sisters Road and discharges as shallow concentrated flow at watershed E. There is not any evidence of erosive cutting within the proposed development area. In order to prevent any long term erosion, a 12" S/W CPP pipe shall be installed to convey this runoff through the proposed vineyard. The installation of this drainage mainline shall result in no net increase in peak flow rates at the outfall of watersheds B, C and E or at the inlets of any of the existing culverts.

Finally, with all the land preparation, cover cropping and straw mulching associated with the proposed vineyard development, the hydrologic condition at the project site will actually improve at watersheds E,

G and H. The enhancement of hydrologic soil condition within the proposed development boundaries will result in no net increase in peak flow rates.

While the proposed vineyard development could potentially lead to pollutants entering the nearby waterways, the project incorporates several measures to minimize the potential for erosion and transport of pollutants during and after the proposed vineyard development. These measures include:

- Establishment of a 75% minimum ground cover, by means of a tilled cover crop in combination
 with straw roll installation and straw mulch, will minimize the amount of sediment leaving the
 project site during the soil building period. This will also maintain the volume and probability of
 rainfall generated runoff at or below pre-development conditions.
- 2. A no-till cover crop on all vineyard blocks will minimize the amount of sediment leaving the project site throughout the life of the proposed vineyard. This will also maintain the volume and probability of rainfall generated runoff at or below pre-development conditions.
- 3. Incorporation of setbacks to the nearby streams, and the use of grassy turnaround avenues shall help filter sediment from surface runoff before it enters the streams. These setbacks and grassy turnaround avenues shall also trap and hold dust and fertilizers (from vineyard operations), before they can enter the streams.
- 4. Proposed outfall locations shall have a rock apron installed to minimize erosion and ensure that runoff exits the project site as surface sheet flow.

Conclusions and statement addressing adequacy of design

Based on the results from TR-55, the proposed development will not have any adverse effects on the existing hydrology of the watershed. The majority of the runoff shall leave the project as sheet flow or through existing culverts, which shall be maintained and/or replaced. The proposed drainage improvement shall divert potential runoff away from the proposed vineyard area and direct it to more stabilized outfall location. This outfall location shall have rock outlet protection installed to minimize erosion and ensure that runoff exits the project site as surface sheet flow. The proposed cover crop, farming practices and drainage improvements shall maintain peak runoff flow rates at or below predevelopment conditions.

References

See the attached TR-55 report print outs for watersheds A-H pre-development and post-development.

See the attached sheets labeled "Pre-Development Site Plan and Curve Numbers" and "Post-Development Site Plan and Curve Numbers" for references to watershed areas and features mentioned in this report.

Land use selection was based on "Hydrologic Soil-Cover Complexes" National Engineering Handbook (NEH), Part 650, (EFH), Amend. IA50, Nov. 2007.

Hydrologic soil conditions are based on a field visits conducted by Omar Reveles of Acme Engineering, Inc. on March 20, 2019, April 1, 2019, and August 6, 2020.

Manning's roughness coefficients were obtained from Civil Engineering Reference Manual Appendix 19A and ADS product literature.

WinTR-55 Current Data Description

--- Identification Data ---

User: O. Reveles
Project: Butler Vineyards Date: 9/8/2020 Units: English SubTitle: Pre-Development Areal Units: Acres

State: California County: Napa

Filename: Z:\Jobs 2018\180901 Butler Vineyards\0121 New Vineyard Development ECP\Calc\01\TR-55\Butler Pre

--- Sub-Area Data ---

Name	Description	Reach	Area(ac)	RCN	Tc
A		Outlet	2.21	80	0.1
D		Outlet	0.42	80	0.1
F		Outlet	0.62	83	0.1
G		Outlet	0.63	82	0.1
H		Outlet	0.6	84	0.1

Total area: 4.48 (ac)

--- Storm Data --

Rainfall Depth by Rainfall Return Period

1-Yr	2-Yr	5-Yr	10-Yr	25-Yr	50-Yr	100-Yr
(in)	(in)	(in)	(in)	(in)	(in)	(in)
3.08	4.05	5.29	6.28	7.6	8.6	9.61

Storm Data Source: User-provided custom storm data Rainfall Distribution Type: Type IA
Dimensionless Unit Hydrograph: <standard>

Butler Vineyards Pre-Development Napa County, California

Storm Data

Rainfall Depth by Rainfall Return Period

1-Yr	2-Yr	5-Yr	10-Yr	25-Yr	50-Yr	100-Yr
(in)	(in)	(in)	(in)	(in)	(in)	(in)
3.08	4.05	5.29	6.28	7.6	8.6	9.61

Storm Data Source: User-provided custom storm data Rainfall Distribution Type: Type IA
Dimensionless Unit Hydrograph: <standard>

Butler Vineyards Pre-Development Napa County, California

Watershed Peak Table

Sub-Area Peak Flow by Rainfall Return Period								
or Reach	1-Yr	2-Yr	5-Yr	10-Yr	25-Yr	50-Yr	100-Yr	
Identifier	(cfs)							
SUBAREAS A	0.64	1.10	1.74	2.27	3.00	3.56	4.12	
D	0.12	0.21	0.33	0.43	0.57	0.68	0.79	
2	0.12	0.21	0.55	0.15	0.57	0.00	0.75	
F	0.22	0.36	0.55	0.70	0.91	1.06	1.22	
G	0.21	0.34	0.53	0.69	0.89	1.05	1.21	
Н	0.23	0.36	0.55	0.70	0.90	1.05	1.20	
REACHES								
OUTLET	1.41	2.37	3.69	4.79	6.27	7.40	8.55	

Butler Vineyards Pre-Development Napa County, California

Hydrograph Peak/Peak Time Table

Sub-Area or Reach Identifier	1-Yr (cfs)	2-Yr (cfs)	5-Yr (cfs)	10-Yr (cfs)	25-Yr	50-Yr (cfs)	100-Yr (cfs)
SUBAREAS A					3.00 7.93		
D					0.57 7.93		
F					0.91 7.92		
G					0.89 7.92		
Н					0.90 7.92		
REACHES							
OUTLET	1.41	2.37	3.69	4.79	6.27	7.40	8.55

Butler Vineyards Pre-Development Napa County, California

Sub-Area Summary Table

Sub-Area Identifier	Drainage Area (ac)	Time of Concentration (hr)	Curve Number	Receiving Reach	Sub-Area Description
A	2.21	0.100	80	Outlet	
D	.42	0.100	80	Outlet	
F	.62	0.100	83	Outlet	
G	.63	0.100	82	Outlet	
H	.60	0.100	84	Outlet	

Total Area: 4.48 (ac)

Butler Vineyards Pre-Development Napa County, California

Sub-Area Time of Concentration Details

Sub- Ident	-Area cifier/	Length	Slope	Mannings's n	Area	Perimeter	Velocity	
	EET ALLOW ANNEL	100 692 164	0.3000	0.130 0.050 0.035	2.00	4.47	5.694	0.055 0.022 0.008
					Ti	me of Conce	ntration	0.1
	EET ALLOW	100 302		0.130 0.050				0.051 0.011
					Ti	me of Conce	ntration	0.1
SHA	ALLOW	100 111 233	0.1600	0.130 0.050 0.035	2.00	4.47	7.191	0.055 0.005 0.009
					Ti	me of Conce	ntration	0.1
G SHE	CET	100	0.2500	0.130				0.047
					Ti	me of Conce	ntration	0.1
	EET ALLOW	100 30		0.130 0.050				0.053 0.001
					Ti	me of Conce	ntration	0.1

Butler Vineyards Pre-Development Napa County, California

Sub-Area Land Use and Curve Number Details

Sub-Area Identifie			Hydrologic Soil Group	Sub-Area Area (ac)	Curve Number
A	Pasture, grassland or range Woods - grass combination) D) D	1.74 .47	80 79
	Total Area / Weighted Curve Number			2.21	80 ==
D		(good		.01 .27 .14	91 80 79
	Total Area / Weighted Curve Number			.42 ===	80
F	Pasture, grassland or range Woods - grass combination	(fair (fair		.38	84 82
	Total Area / Weighted Curve Number			.62 ===	83 ==
G	Pasture, grassland or range Woods - grass combination	(fair (fair	,	.12 .51	84 82
	Total Area / Weighted Curve Number			.63 ===	82 ==
Н	Gravel (w/ right-of-way) Pasture, grassland or range Woods - grass combination	(fair (fair		.01 .53 .06	91 84 82
	Total Area / Weighted Curve Number			.6 ==	84 ==

WinTR-55 Current Data Description

--- Identification Data ---

User: O. Reveles
Project: Butler Vineyards Date: 9/8/2020 Units: English SubTitle: Pre-Development Areal Units: Acres

State: California County: Napa

Filename: Z:\Jobs 2018\180901 Butler Vineyards\0121 New Vineyard Development ECP\Calc\01\TR-55\Butler Pre

--- Sub-Area Data ---

Name	Description	Reach	Area(ac)	RCN	Tc
B		Reach 1	1.31	80	0.1
C		Reach 2	0.38	81	0.1
E		Reach 3	2.37	84	0.1

Total area: 4.06 (ac)

--- Storm Data --

Rainfall Depth by Rainfall Return Period

1-Yr	2-Yr	5-Yr	10-Yr	25-Yr	50-Yr	100-Yr
(in)	(in)	(in)	(in)	(in)	(in)	(in)
3.08	4.05	5.29	6.28	7.6	8.6	9.61

Storm Data Source: User-provided custom storm data Rainfall Distribution Type: Type IA

Dimensionless Unit Hydrograph: <standard>

Butler Vineyards Pre-Development Napa County, California

Storm Data

Rainfall Depth by Rainfall Return Period

1-Yr	2-Yr	5-Yr	10-Yr	25-Yr	50-Yr	100-Yr
(in)	(in)	(in)	(in)	(in)	(in)	(in)
3.08	4.05	5.29	6.28	7.6	8.6	9.61

Storm Data Source: User-provided custom storm data Rainfall Distribution Type: Type IA
Dimensionless Unit Hydrograph: <standard>

Butler Vineyards Pre-Development Napa County, California

Watershed Peak Table

Sub-Area or Reach Identifier	1-Yr (cfs)	2-Yr (cfs)	5-Yr (cfs)		25-Yr (cfs)	(cfs)	
SUBAREAS B		0.65					2.45
C	0.12	0.20	0.31	0.40	0.53	0.62	0.72
E	0.89	1.43	2.15	2.74	3.53	4.14	4.74
REACHES Reach 1 Down	0.38 0.38	0.65 0.65	1.03	1.35 1.35		2.11 2.11	
Reach 2 Down	0.50 0.50	0.85 0.85	1.34 1.34	1.75 1.75	2.31 2.31	2.73 2.73	3.17 3.17
Reach 3 Down	1.39 1.39	2.28	3.49 3.49	4.49 4.49			
OUTLET	1.39	2.28	3.49	4.49	5.84	6.87	7.91

Butler Vineyards Pre-Development Napa County, California

Hydrograph Peak/Peak Time Table

Sub-Area or Reach Identifier	1-Yr (cfs) (hr)	(cfs)	5-Yr (cfs) (hr)	10-Yr (cfs) (hr)	25-Yr (cfs) (hr)	50-Yr (cfs) (hr)	100-Yr (cfs) (hr)
SUBAREAS B	0.38		1.03	1.35	1.78	2.11	2.45
С		0.20 7.94					
Е	0.89 7.93	1.43 7.93	2.15 7.92	2.74 7.92	3.53 7.92	4.14 7.91	4.74 7.92
	8.00	0.65 7.93 0.65 7.94	7.93 1.03	7.93 1.35	7.93 1.78	7.92 2.11	7.92 2.45
Reach 2 Down	8.01 0.50	0.85 7.94 0.85 7.95	7.93 1.34	7.93 1.75	7.93 2.31	7.92 2.73	7.92 3.17
Reach 3 Down	7.95 1.39	2.28 7.93 2.28 7.94	7.93 3.49	7.93 4.49	7.92 5.84	7.92 6.87	7.92 7.91
OUTLET	1.39	2.28	3.49	4.49	5.84	6.87	7.91

Butler Vineyards Pre-Development Napa County, California

Sub-Area Summary Table

Sub-Area Identifier	Drainage Area (ac)	Time of Concentration (hr)	Curve Number	Receiving Reach	Sub-Area Description
В	1.31	0.100	80	Reach 1	
C	.38	0.100	81	Reach 2	
E	2.37	0.100	84	Reach 3	

Total Area: 4.06 (ac)

Butler Vineyards Pre-Development Napa County, California

Reach Summary Table

Reach Identifier	Receiving Reach Identifier	Reach Length (ft)	Routing Method	
Reach 1	Reach 2	78	CHANNEL	
Reach 2	Reach 3	333	CHANNEL	
Reach 3	Outlet	1	CHANNEL	

Butler Vineyards Pre-Development Napa County, California

Sub-Area Time of Concentration Details

Sub-Area Identifier/	_			Area			
B SHEET SHALLOW CHANNEL	100 516 96	0.2200 0.2200 0.1300	0.130 0.050 0.035	2.00	4.47	8.889	0.050 0.019 0.003
				Ti	me of Conce	ntration :	0.1
C SHEET SHALLOW CHANNEL	100 400 78	0.2600 0.2130 0.1500	0.130 0.050 0.035	2.00	4.47	10.833	0.046 0.015 0.002
				Ti	me of Conce		0.1
E SHEET SHALLOW	100 324	0.1600 0.2400	0.130 0.050				0.056 0.011
				Ti	me of Conce		0.1

Butler Vineyards Pre-Development Napa County, California

Sub-Area Land Use and Curve Number Details

Sub-Area Identifie	-		Hydrologic Soil Group	Sub-Area Area (ac)	Curve Number
В	Pasture, grassland or range Woods - grass combination	(good) D) D	1.17	80 79
	Total Area / Weighted Curve Number			1.31	80 ==
С	Gravel (w/ right-of-way) Pasture, grassland or range Woods - grass combination	(good		.02 .33 .03	91 80 79
	Total Area / Weighted Curve Number			.38	81 ==
E	Gravel (w/ right-of-way) Pasture, grassland or range Woods - grass combination	(fair (fair	,	.21 1.23 .93	91 84 82
	Total Area / Weighted Curve Number			2.37	84 ==

Butler Vineyards Pre-Development Napa County, California

Reach Channel Rating Details

		Reach Manning's n		Width	Slope
Reach 1 Reach 2 Reach 3	78 333 1	0.035 0.035 0.035	0.14 0.15 0.15	0 0 0	2 :1 10 :1 2 :1
Reach Identifier	Stage (ft)	Flow (cfs)	Area	Top Width (ft)	Slope
	0.0 0.5 1.0 2.0 5.0 10.0		0 0.5 2 8 50.1 200.1	0 2 4 8 20 40 80	
Reach 2	0.5 1.0 2.0 5.0 10.0	0.000 16.304 103.383 656.003 7549.275 47928.508 304306.748	2.5 10 40 250.1 1000.1	0 10 20 40 100 200 400	0.15
Reach 3	0.5 1.0 2.0 5.0 10.0	19.364 122.537 1407.831	0 0.5 2 8 50.1 200.1 800.2	0 2 4 8 20 40 80	0.15

WinTR-55 Current Data Description

--- Identification Data ---

Date: 9/11/2020 Units: English User: O. Reveles Project: Butler Vineyards SubTitle: Post-Development Areal Units: Acres

State: California County: Napa

Filename: Z:\Jobs 2018\180901 Butler Vineyards\0121 New Vineyard Development ECP\Calc\01\TR-55\Butler Post

--- Sub-Area Data ---

Name	Description	Reach	Area(ac)	RCN	Tc
A		Outlet	2.21	80	0.1
D		Outlet	0.42	80	0.100
F		Outlet	0.62	83	0.1
G		Outlet	0.63	80	0.1
H		Outlet	0.6	80	0.1

Total area: 4.48 (ac)

--- Storm Data --

Rainfall Depth by Rainfall Return Period

1-Yr	2-Yr	5-Yr	10-Yr	25-Yr	50-Yr	100-Yr
(in)	(in)	(in)	(in)	(in)	(in)	(in)
3.08	4.05	5.29	6.28	7.6	8.6	9.61

Page 1

Storm Data Source: User-provided custom storm data Rainfall Distribution Type: Type IA
Dimensionless Unit Hydrograph: <standard>

Butler Vineyards Post-Development Napa County, California

Storm Data

Rainfall Depth by Rainfall Return Period

1-Yr	2-Yr	5-Yr	10-Yr	25-Yr	50-Yr	100-Yr
(in)	(in)	(in)	(in)	(in)	(in)	(in)
3.08	4.05	5.29	6.28	7.6	8.6	9.61

Storm Data Source: User-provided custom storm data Rainfall Distribution Type: Type IA
Dimensionless Unit Hydrograph: <standard>

Butler Vineyards Post-Development Napa County, California

Watershed Peak Table

Sub-Area or Reach Identifier	1-Yr	2-Yr	5-Yr	10-Yr	25-Yr		
SUBAREAS A	0.64	1.10	1.74	2.27	3.00	3.56	4.12
D	0.12	0.21	0.33	0.43	0.57	0.68	0.79
F	0.22	0.36	0.55	0.70	0.91	1.06	1.22
G	0.18	0.31	0.49	0.65	0.85	1.01	1.17
Н	0.17	0.30	0.47	0.62	0.82	0.97	1.12
REACHES							
OUTLET	1.34	2.28	3.58	4.67	6.15	7.28	8.43

Butler Vineyards Post-Development Napa County, California

Hydrograph Peak/Peak Time Table

Sub-Area or Reach Identifier	1-Yr (cfs) (hr)		5-Yr (cfs) (hr)	10-Yr (cfs) (hr)	25-Yr (cfs) (hr)	50-Yr (cfs) (hr)	100-Yr (cfs) (hr)
SUBAREAS							
A		1.10 7.93					
D		0.21 7.93					
F		0.36 7.93					
G		0.31 7.93					
Н		0.30 7.93					
REACHES							
OUTLET	1.34	2.28	3.58	4.67	6.15	7.28	8.43

Butler Vineyards Post-Development Napa County, California

Sub-Area Summary Table

Sub-Area Identifier	Drainage Area (ac)	Time of Concentration (hr)	Curve Number	Receiving Reach	Sub-Area Description
A	2.21	0.100	80	Outlet	
D	.42	0.100	80	Outlet	
F	.62	0.100	83	Outlet	
G	.63	0.100	80	Outlet	
H	.60	0.100	80	Outlet	

Total Area: 4.48 (ac)

Butler Vineyards Post-Development Napa County, California

Sub-Area Time of Concentration Details

Sub-Area Identifier/	Length	Slope (ft/ft)	Mannings's n	Area	Wetted Perimeter (ft)	Velocity	Travel / Time (hr)
A SHEET SHALLOW CHANNEL	100 692 164	0.3000	0.130 0.050 0.035	2.00	4.47	5.694	0.055 0.022 0.008
				Ti	me of Conce	ntration	0.1
D SHEET SHALLOW			0.130 0.050				0.051 0.011
				Ti	me of Conce	ntration	0.100
F SHEET SHALLOW CHANNEL		0.1600	0.050	2.00	4.47	7.191	0.055 0.005 0.009
				Ti	me of Conce	ntration	0.1
G SHEET	100	0.2500	0.170				0.058
				Ti	me of Conce	ntration	0.1
H SHEET SHALLOW	100 30	0.1900 0.3000	0.170 0.050				0.065 0.001
				Ti	me of Conce	ntration	0.1

Butler Vineyards Post-Development Napa County, California

Sub-Area Land Use and Curve Number Details

Sub-Area Identifie			Hydrologic Soil Group	Sub-Area Area (ac)	Curve Number
A	Pasture, grassland or range Woods - grass combination) D) D	1.74 .47	80 79
	Total Area / Weighted Curve Number			2.21	80 ==
D	Pasture, grassland or range Woods - grass combination	(good		.28 .14	80 79
	Total Area / Weighted Curve Number			.42 ===	80 ==
F	Pasture, grassland or range Pasture, grassland or range Woods - grass combination	(fair (good (fair) D	.37 .02 .23	84 80 82
	Total Area / Weighted Curve Number			.62 ===	83 ==
G	Pasture, grassland or range	(good) D	.63	80
	Total Area / Weighted Curve Number			.63 ===	80 ==
Н	Gravel (w/ right-of-way) Pasture, grassland or range Pasture, grassland or range	(fair (good	•	.01 .01 .58	91 84 80
	Total Area / Weighted Curve Number			.6 ==	80

WinTR-55 Current Data Description

--- Identification Data ---

User: O. Reveles
Project: Butler Vineyards Date: 9/11/2020 Units: English SubTitle: Post-Development Areal Units: Acres

State: California County: Napa

Filename: Z:\Jobs 2018\180901 Butler Vineyards\0121 New Vineyard Development ECP\Calc\01\TR-55\Butler Post

--- Sub-Area Data ---

Name	Description	Reach	Area(ac)	RCN	Tc
В С		Reach 1 Reach 2	1.31	80 80	0.100 0.1
E		Reach 4	2.37	81	0.1

Total area: 4.06 (ac)

--- Storm Data --

Rainfall Depth by Rainfall Return Period

1-Yr	2-Yr	5-Yr	10-Yr	25-Yr	50-Yr	100-Yr
(in)	(in)	(in)	(in)	(in)	(in)	(in)
3.08	4.05	5.29	6.28	7.6	8.6	9.61

Storm Data Source: User-provided custom storm data Rainfall Distribution Type: Type IA

Dimensionless Unit Hydrograph: <standard>

Butler Vineyards Post-Development Napa County, California

Storm Data

Rainfall Depth by Rainfall Return Period

1-Yr	2-Yr	5-Yr	10-Yr	25-Yr	50-Yr	100-Yr
(in)	(in)	(in)	(in)	(in)	(in)	(in)
3.08	4.05	5.29	6.28	7.6	8.6	9.61

Storm Data Source: User-provided custom storm data Rainfall Distribution Type: Type IA
Dimensionless Unit Hydrograph: <standard>

Butler Vineyards Post-Development Napa County, California

Watershed Peak Table

Sub-Area	Pea	k Flow by	Rainfall R	eturn Peri	iod		
or Reach	1-Yr	2-Yr	5-Yr	10-Yr	25-Yr	50-Yr	100-Yr
Identifier	(cfs)	(cfs)	(cfs)	(cfs)	(cfs)	(cfs)	(cfs)
SUBAREAS B	0.38	0.65	1.03	1.35	1.78	2.11	2.45
Б	0.30	0.65	1.03	1.33	1.70	2.11	2.45
С	0.11	0.19	0.30	0.39	0.51	0.61	0.70
	**						
E	0.73	1.24	1.94	2.51	3.30	3.90	4.50
REACHES	0 00	0.65	1 00	1 25	1 50	0 11	0.45
	0.38						
Down	0.38	0.65	1.03	1.35	1.78	2.11	2.45
Reach 2	0.49	0.84	1.33	1.74	2.29	2.72	3.15
Down	0.49	0.84	1.33	1.74	2.29	2.72	3.15
DOWII	0.15	0.01	1.33	1.71	2.27	2.72	3.13
Reach 3	0.49	0.84	1.33	1.74	2.29	2.72	3.15
Down	0.49	0.84	1.33	1.74	2.29	2.72	3.15
Reach 4	1.22	2.08	3.26	4.25	5.59	6.62	7.65
Down	1.22	2.08	3.26	4.25	5.59	6.62	7.65
OTTEL DE	1 00	0.00	2.06	4 05	F F0	6.60	D 65
OUTLET	1.22	∠.∪8	3.∠6	4.25	5.59	6.62	7.65

Butler Vineyards Post-Development Napa County, California

Hydrograph Peak/Peak Time Table

	1-Yr (cfs) (hr)	2-Yr	5-Yr (cfs) (hr)	10-Yr (cfs) (hr)	25-Yr (cfs) (hr)	50-Yr (cfs) (hr)	100-Yr (cfs) (hr)
SUBAREAS B	0.38	0.65 7.93	1.03	1.35	1.78	2.11	2.45
С	0.11	0.19 7.93	0.30 7.93	0.39 7.93	0.51 7.93	0.61 7.92	0.70 7.92
E	0.73	1.24 7.94	1.94 7.93	2.51 7.93	3.30 7.92	3.90 7.92	4.50 7.92
Down Reach 2 Down	8.00 0.38 8.01 0.49 8.01	7.94 0.84 7.94	7.93 1.03 7.94 1.33 7.93 1.33 7.94	7.93 1.35 7.93 1.74 7.93 1.74 7.93	7.93 1.78 7.93 2.29 7.93 2.29 7.93	7.92 2.11 7.92 2.72 7.92 2.72 7.93	7.92 2.45 7.92 3.15 7.92 3.15 7.93
Reach 3 Down	8.01 0.49	0.84 7.94 0.84 7.95	7.94 1.33	7.93 1.74	7.93 2.29	7.93 2.72	7.93 3.15
Reach 4 Down	8.01 1.22	2.08 7.94 2.08 7.94	7.93 3.26	7.93 4.25	7.93 5.59	7.92 6.62	7.92 7.65
OUTLET	1.22	2.08	3.26	4.25	5.59	6.62	7.65

Butler Vineyards Post-Development Napa County, California

Sub-Area Summary Table

Sub-Area Identifier	Drainage Area (ac)	Time of Concentration (hr)	Curve Number	Receiving Reach	Sub-Area Description
В	1.31	0.100	80	Reach 1	
C	.38	0.100	80	Reach 2	
E	2.37	0.100	81	Reach 4	

Total Area: 4.06 (ac)

Butler Vineyards Post-Development Napa County, California

Reach Summary Table

Reach Identifier	Receiving Reach Identifier	Reach Length (ft)	Routing Method	
Reach 1	Reach 2	78	CHANNEL	
Reach 2	Reach 3	206	CHANNEL	
Reach 3	Reach 4	118	CHANNEL	
Reach 4	Outlet	1	CHANNEL	

Page 1

Butler Vineyards Post-Development Napa County, California

Sub-Area Time of Concentration Details

Sub-Area Identifier/	Length	Slope	Mannings's n	Area	Perimeter	Velocity	
B SHEET SHALLOW CHANNEL	100 516 96	0.2200 0.2200 0.1300	0.130 0.050 0.035	2.00	4.47	8.889	0.050 0.019 0.003
				Ti	me of Conce	ntration :	0.100
C SHEET SHALLOW CHANNEL	100 400 78	0.2100	0.130 0.050 0.035	2.00	4.47	10.833	0.046 0.015 0.002
				Ti	me of Conce		0.1
E SHEET SHALLOW	100 324	0.1600 0.2400	0.170 0.050				0.070 0.011
				Ti	me of Conce		0.1

O. Reveles

Butler Vineyards Post-Development Napa County, California

Sub-Area Land Use and Curve Number Details

Sub-Area Identifia	-		Hydrologic Soil Group	Sub-Area Area (ac)	Curve Number
В	Pasture, grassland or range Woods - grass combination	(good) D) D	1.17	80 79
	Total Area / Weighted Curve Number			1.31	80 ==
С	Pasture, grassland or range Woods - grass combination	(good	•	.35	80 79
	Total Area / Weighted Curve Number			.38	80 ==
Е	Gravel (w/ right-of-way) Pasture, grassland or range Pasture, grassland or range Woods - grass combination	(fair (good (fair) D	.21 .13 1.72 .31	91 84 80 82
	Total Area / Weighted Curve Number			2.37	81 ==

O. Reveles

Butler Vineyards Post-Development Napa County, California

Reach Channel Rating Details

Reach Identifier	Reach Length (ft)	Reach Manning's n	Friction Slope (ft/ft)	Botto Widt (ft	m Side h Slope)
Reach 1 Reach 2 Reach 3 Reach 4	78 206 118 1	0.035 0.018 0.035 0.035	0.14 0.19 0.09 0.15	0 0. 0	2 :1 2 2.6 :1 10 :1 2 :1
Reach Identifier	Stage (ft)	Flow (cfs)	End Area (sq ft)	Width (ft)	Slope (ft/ft)
Reach 1	0.0 0.5 1.0 2.0 5.0 10.0	0.000 2.966 18.708	0 0.5 2 8 50.1 200.1	0	0.14
Reach 2	1.0 2.0 5.0	0.000 10.745 62.211 376.142 4200.856 26400.604 166767.272	2.8 10.8 66	0.2 2.8 5.4 10.6 26.2 52.2 104.2	0.19
Reach 3	0.5 1.0 2.0 5.0 10.0	0.000 12.629 80.080 508.138 5847.643 37125.263 235714.993	10 40 250.1 1000.1	0 10 20 40 100 200 400	0.09
Reach 4	0.5 1.0 2.0 5.0 10.0	0.000 3.070 19.364 122.537 1407.831 8933.058 56701.987	0 0.5 2 8 50.1 200.1 800.2	0 2 4 8 20 40 80	0.15

Subject: Lands of Butler - New Vineyard Development

Project #: 180901-0121 By: Omar Reveles Date: 11/5/2020

							Drop Inlet	Riser and Sump Design	
Point of Concentration	Deak Flow		Inlet Riser Diameter (ft)	Required (ft)	Inlet Sump Diameter (inches)	Inlet Sump Diameter (ft)	Head Required for Sump Inlet (ft)	Design	Remarks
1	3.15	8	0.67	0.62	15	1.3	0.41	8" riser 15" sump*	Set riser invert to 1' below sump invert. Use an earthen berm to create required head at sump.

^{*} Sump shall be a runoff collector, therefore the whole circumference of the sump pipe shall funtion as a weir

Equations Used:

Circular Riser Weir Flow Equation: $Qw = 9.73 \times d \times h^{(3/2)}$

where Ow = weir flow, in cfs d = pipe diameter, in feet

h = height of water above riser, in feet

rearranging terms, and solving for h, yields: $h = (Qw/(9.73 \times d))^{(2/3)}$

when only half of the circumference of the circular riser behaves as a weir $h = (Qw/(4.87 \times d))^{2/3}$

Setting the Circular Riser Weir Flow Equation equal to the Standard Weir

Equation yields: $9.73 \times d \times h^{(3/2)} = C \times b \times h^{(3/2)}$

substituting circumference (π x d) for "b" yields:

 $9.73 \times d \times h^{(3/2)} = C \times (\pi \times d) \times h^{(3/2)}$

simplifying the equation yields: $9.73 = c \times \pi$

Solving for C yields: C = 3.10

Weir coefficient is on the conservative side of the acceptable range (3.0 - 3.9)

Standard Weir Equation: $Qw = C \times b \times h^{(3/2)}$

where C = weir coefficient (3.0 - 3.9)
b = effective weir length, in feet
h = height of water above weir, in feet

This equation calculates the flow in terms of the effective length of the weir and the height of the water above the weir. If a circular pipe riser is used, the effective weir length is equal to the circumference of that circular pipe

Subject: Lands of Butler - New Vineyard Development

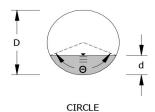
Project #: 180901-0121 By: Date: Omar Reveles 11/5/2020

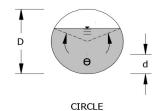
Drainage Mainline

Using Mannings Equation $Q=(((1.49/n) \times A \times R^{(2/3)}) \times s^{(1/2)})$

Q= flow, in cfs

n = Mannings Roughness Coefficient A =area in flow, in square feet R = hydraulic radius, in feet s = slope, in ft/ft





From the previous illustration:

 $\theta (RAD) = 2 \times \arccos((D/2-d)/(D/2))$

Area = $1/8(\theta-\sin\theta)D^2$ (θ in radians)

Wetted Perimeter = $\theta D/2$ (θ in radians)

Hydraulic Radius = $(1-(\sin(\theta)/\theta)) \times (D/4)$ (θ in radians)

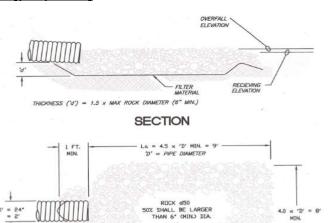
Drainage Mainline Sizing Table										
Section			HDPE Pipe Size (inches)	HDPE Pipe S/W or D/W	Mannings "n" value	% Full (d/D)	Flow Capacity (cfs)	Peak Anticipated Flow (cfs)	Notes	
Α	N/A	0.19	12	Single Wall	0.018	70%	9.42	3.15	OK	

Notes:
1.) Mannings roughness coefficients (n values) for smooth wall pipe were acquired from ADS product literature
2.) Peak anticipated flows were obtained from TR-55 hydrologic modeling for post-development conditions.

Subject: Lands of Butler - New Vineyard Development

Project #: 180901-0121 Omar Reveles 11/5/2020 By: Date:

Energy Dissipater Sizing



PLAN

- NOTES:

 1. "Lo" = LENGTH OF APRON. DISTANCE "Lo" SHALL BE OF SUFFICIENT LENGTH
 TO DISSIPATE ENERGY.

 2. APRON SHALL BE SET AT A ZERO GRADE AND ALIGNED STRAIGHT.

 3. FILTER MATERIAL SHALL BE FILTER FABRIC OR 6" THICK (MIN.) GRADED GRAVEL
 LAYER.

Pipe Geometry										
Diameter (in)	Diameter (ft)	Area (sq. ft.)								
3	0.25	0.05								
4	0.33	0.09								
6	0.50	0.20								
8	0.67	0.35								
10	0.83	0.55								
12	1.00	0.79								
15	1.25	1.23								
18	1.50	1.77								
24	2.00	3.14								

Channel Geometry (assuming 2:1 side slopes)												
Depth (in)	Depth (ft)	Width (ft)	Area (sq. ft.)	Equivalent Pipe Size (in)								
4	0.33	1.33	0.22	8								
6	0.50	2.00	0.50	10								
8	0.67	2.67	0.89	15								
10	0.83	3.33	1.39	18								
12	1.00	4.00	2.00	24								

4.0 x 'D' = 8' MIN.

			Energy	/ Dissipater G	eometry			
Outfall Location	Outfall Type	Channel Depth (in)	Equivalent Pipe Size (in)	Min Apron Width "Wa" (ft)	Min Apron Length "La" (ft)	d50 Rock Size (in)	Largest Stone Size (in)	Rock Layer Depth "d" (in)
Reach 3	Pipe	-	12	4.0	4.5	6	9	14

HYDROLOGIC SOIL-COVER COMPLEXES

A combination of the effects of hydrologic soil group (soil) and the land use and treatment class (cover) is used to determine the runoff curve number (CN). The CN indicates the runoff potential of a soil-cover complex during periods when the soil is not frozen. The higher the CN, the higher the potential for runoff.

Land Use

Fallow is the land use with the highest potential for runoff because the land is kept as bare as possible to conserve moisture for use by a succeeding crop.

A row crop is any field crop planted in rows far enough apart that most of the soil surface is exposed to rainfall impact during the early growing season (i.e.: corn, soybeans, sorghum).

Small grain is planted in rows close enough together that the soil surface is not exposed except during planting and shortly thereafter.

Close-seeded legumes or rotation meadow are either planted in close rows or broadcast. This cover may be allowed to remain for more than a year so that year-round protection is given to the soil.

Pasture is a long term stand of forage plants which gives year-round protection to the soil.

Meadow is a field in which grass is continually grown, protected from grazing, and generally mowed for hay.

Woods are forested areas that have at least 30 percent canopy coverage as viewed by aerial photography.

Farmsteads include the area surrounding the farm headquarters including buildings, lots, driveways, etc.

Roads are improved travelways (not farm lanes). Hard surface roads include any type of asphalt or concrete paving. Road right-of-way is included in the total road area used to determine CN.

Treatment or Practice

Straight row fields are those farmed in straight rows either up and down hill or across the slope.

Contoured fields are those farmed as nearly as possible on the contour. The hydrologic effect of contouring is due to the surface storage provided by the furrows because the storage prolongs the time during which infiltration can take place. The magnitude of the storage depends not only on the dimensions of the furrows but also on the land slope, crop, and manner of planting and cultivation. See Contour Farming (330) in the Field Office Technical Guide for additional guidance.

The contoured and terraced condition is to be used for systems containing open-end level or graded terraces with grassed waterway outlets where all tillage is done on the contour between the terraces. The area above closed-end level terraces and terraces with tile outlets is to be included with the contoured area for runoff curve number computations.

Hydrologic Condition

Ratings as to "poor" or "good" are based largely on the proportion of dense vegetation in the rotation.

Pasture is considered poor if it is heavily grazed and has no mulch or has plant cover on less than half of the area. Fair pasture has plant cover on 50 to 75 percent of the area. Heavily grazed pasture in lowa is generally considered to be fair pasture. Good pasture is lightly grazed and has plant cover on more than 75 percent of the area.

Poor woods are heavily grazed or are regularly burned and have no litter or new young growth. Fair woods are grazed but not burned. There may be some litter but these woods are not protected. Good woods are protected from grazing and have litter and shrubs covering the soil.

Table IA2-1 gives CN's for agricultural land uses and for selected suburban and urban land uses.

Effects of Conservation Tillage

Cropland with conservation tillage and residue management practices will be considered to be in good hydrologic condition.

RUNOFF CURVE NUMBERS^{1/} TABLE IA2-1

	<u> </u>	ABLE IAZ-1							—	
COVER TYPE	LAND USE AND TREATMENT ^{2/}	HYDROLOGIC CONDITION ^{3/}	Α	CN	В	CN	С	CN	D	CN
	ELLL V DEVELOPED LIPPAN AREAS (Vog Est					 			Н	⊢
2	FULLY DEVELOPED URBAN AREAS (Veg Est)				-	-		\vdash	⊢
	Open space (Lawns, parks, etc.) Poor condition; grass cover < 50%			60		79	1	96		90
3 4				68		_	-	86 79	\vdash	89
	Fair condition; grass cover 50% to 75%			49		69		79	Н	84
5	Good condition; grass cover > 75%			39		61	1	74		80
6	Immonutous Avess.					 			Н	<u> </u>
7	Impervious Areas:			00		- 00			Н	00
8	Paved parking lots, roofs, driveways		-	98		98		98	Н	98
10	Chroate and reader		-						Н	<u> </u>
_	Streets and roads:			00			<u> </u>	-00	Н	
11	Paved; curbs and storm sewers			98		98	<u> </u>	98	Ш	98
12	Paved; open ditches (w/ right-of-way)			83		89	<u> </u>	92	Ш	93
13	Gravel (w/ right-of-way)			76		85	├	89		91
14	Dirt (w/ right-of-way)			72		82	ــــــ	87		89
15									Ш	
16	Urban Districts	Avg % Imperv								L
17	Commercial & business	85		89		92		94		95
18	Industrial	72		81		88		91		93
19									Ш	_
20	Residential districts (by average lot size)	Avg % Imperv								
21	1/8 acre (town houses)	65		77		85		90		92
22	1/4 acre	38		61		75		83		87
23	1/3 acre	30		57		72		81		86
24	1/2 acre	25		54		70		80		85
25	1 acre	20		51		68		79		84
26	2 acre	12		46		65		77		82
27										
28	Western Desert Urban Areas									
29	Natural desert (pervious areas only)			63		77		85		88
30	Artificial desert landscaping			96		96		96		96
31	- managem de con namacoup m.g					 	1		П	
32	User defined urban (Click button to define)	Custom CN								
33	% Impervious Area:								П	
34	% Unconnected Impervious Area:			1		 	 		H	_
35	Pervious Curve Number:					 	1		H	
36	1 CIVIOUS GUIVE INGITIBET.					 	1		H	
37	DEVELOPING URBAN AREA (NO VEGETATIO	NA)				 	1		H	
38	Newly graded area (pervious only)	1		77		86		91	H	94
39	Newly graded area (pervious only)			- ' '		- 00	 	91	H	94
40	CULTIVATED AGRICULTURAL LANDS	+	-	\vdash		\vdash	 	$\vdash \vdash$	Н	-
41		+	-	77		86	+	91	Н	94
	Fallow Bare soil		-				+		Н	
42	Fallow Crop residue (CR)	poor		76		85	├─	90	Н	93
43	Fallow Crop residue (CR)	good		74		83	₩	88	Н	90
44	David and a 111 (05)	<u> </u>		7.		 	—		Н	<u> </u>
45	Row crop Straight row (SR)	poor		72		81	—	88	Н	91
46	Straight row (SR)	good		67		78	—	85	Ш	89
47	SR + Crop residue	poor		71		80	—	87	Щ	90
48	SR + Crop residue	good		64		75	Ļ	82	Щ	85
49	Contoured (C)	poor		70		79	<u> </u>	84	Ш	88
50	Contoured (C)	good		65		75	<u> </u>	82	Ш	86
51	C + Crop residue	poor		69		78		83	Ш	87
52	C + Crop residue	good		64		74		81	Ш	85
53	Cont & terraced (C&T)	poor		66		74		80		82
54	Cont & terraced (C&T)	good		62		71		78		81
55	C&T + Crop residue	poor		65		73		79		81
56	C&T + Crop residue	good		61		70		77		80
57									П	
		1		1		1 70	1	~ -	П	00
58	Small grain Straight row (SR)	poor		65	1	76	1	84	, ,	88
	Small grain Straight row (SR) Straight row (SR)	poor good		65		76	+	84	Н	87

RUNOFF CURVE NUMBERS^{1/} TABLE IA2-1

		IIVADAL ASIA		_		T			_	
COVER TYPE	LAND USE AND TREATMENT ^{2/}	HYDROLOGIC CONDITION ^{3/}	Α	CN	В	CN	С	CN	D	CN
61	SR + Crop residue	poor		64		75		83		86
62	SR + Crop residue	good		60		72		80		84
63	Contoured (C)	poor		63		74		82		85
64	Contoured (C)	good		61		73		81		84
65	C + Crop residue	poor		62		73		81		84
66	C + Crop residue	good		60		72		80		83
67	Cont & terraced (C&T)	poor		61		72		79		82
68	Cont & terraced (C&T)	good		59		70		78		81
69	C&T + Crop residue	poor		60		71		78		81
70	C&T + Crop residue	good		58		69		77		80
71										
72	Close-seeded Straight Row	poor		66		77		85		89
73	legumes or Straight Row	good		58		72		81		85
74	rotation Contoured	poor		64		75		83		85
75	meadow Contoured	good		55		69		78		83
76	Cont & terraced	poor		63		73		80		83
77	Cont & terraced	good		51		67		76		80
78										
79	OTHER AGRICULTURAL LANDS									
80	Pasture, grassland or range⁴′	poor		68		79		86		89
81	Pasture, grassland or range	fair		49		69		79		84
82	Pasture, grassland or range	good		39		61		74		80
83										
84	Meadow - cont. grass (non grazed)			30		58		71		78
85										
86	Brush - brush, weed, grass mix ^{5/}	poor		48		67		77		83
87	Brush - brush, weed, grass mix	fair		35		56		70		77
88	Brush - brush, weed, grass mix	good		30 ^{6/}		48		65		73
89										
90	Woods - grass combination"	poor		57		73		82		86
91	Woods - grass combination	fair		43		65		76		82
92	Woods - grass combination	good		32		58		72		79
93	W								Ш	
94	Woods ^{8/}	poor		45		66		77	Ш	83
95	Woods	fair		36		60		73	Ш	79
96	Woods	good		30		55		70	Ш	77
97										
98	Farmsteads			59		74		82		86
99	Feedlots									
100	Earthen			90		90		90		90
101	Paved			98		98		98		98

Average runoff condition, and I_a =0.2s.

Crop residue cover applies only if residue is on at least 5% of the surface throughout the year.

Poor: factors impair infiltration and tend to increase runoff.

Factors encourage average and better than average infiltration and tend to decrease runoff.

For conservation tillage poor hydrologic condition, 5 to 20% of the surface is covered with residue (less than 750 pounds per acre for row crops or 300 pounds per acre for small grain).

For conservation tillage good hydrologic condition, more than 20% of the surface is covered with residue (greater than 750 pounds per acre for row crops or 300 pounds per acre for small grain).
Poor: <50% ground cove

<50% ground cover or heavily grazed with no mulch. Fair: 50 to 75% ground cover and not heavily grazed.

>75% ground cover and lightly or only occasionally grazed. Good:

Poor: <50% ground cover. 50 to 75% ground cover. Fair: Good: >75% ground cover.

If actual curve number is less than 30, use CN = 30 for runoff computation.

CNs shown were computed for areas with 50% woods and 50% grass (pasture) cover. Other combinations of conditions may be computed from the CNs for woods and pasture.

Forest litter, small trees, and brush are destroyed by heavy grazing or regular burning. Poor:

Fair: Woods are grazed, but not burned, and some forest litter covers the soil.

Good: Woods are protected from grazing, and letter and brush adequately cover the soil.

Hydrologic condition is based on combinations of factors that affect infiltration and runoff, including (a) density and canopy of vegetative areas, (b) amount of year-round cover, (c) amount of grass or close-seeded legumes, (d) percent of residue cover on the land surface (good ≥20%), and (e) degree of surface toughness.

APPENDIX 19.A

Manning's Roughness Coefficient a,b (design use)

channel material	n
plastic (PVC and ABS)	0.009
clean, uncoated cast iron	0.013 - 0.015
clean, coated cast iron	0.012 - 0.014
dirty, tuberculated cast iron	0.015 - 0.035
riveted steel	0.015 - 0.017
lock-bar and welded steel pipe	0.012 - 0.013
galvanized iron	0.015 - 0.017
brass and glass	0.009 - 0.013
wood stave	
small diameter	0.011 - 0.012
large diameter	0.012 - 0.013
concrete	
average value used	0.013
typical commercial, ball and spigot	
rubber gasketed end connections	
 full (pressurized and wet) 	0.010
– partially full	0.0085
with rough joints	0.016 - 0.017
dry mix, rough forms	0.015 - 0.016
wet mix, steel forms	0.012 - 0.014
very smooth, finished	0.011 - 0.012
vitrified sewer	0.013 - 0.015
common-clay drainage tile	0.012 - 0.014
ashestos	0.011
planed timber (flume)	0.012 (0.010-0.014)
canvas	0.012
unplaned timber (flume)	0.013 (0.011-0.015)
brick	0.016
rubble masonry	0.017
smooth earth	0.018
firm gravel	0.023
corrugated metal pipe (CMP)	0.024 (see App. 17.F)
natural channels, good condition	0.025
rip rap	0.035
natural channels with stones and weeds	0.035
very poor natural channels	0.060

 aC ompiled from various sources. bV alues outside these ranges have been observed, but these values are typical.

Conveyance Factors (Standard Units) Table 3-1

Design Mannin	Design Manning's Values for ADS Thermoplastic Pipe *	*
Product	Diameter	Design Manning's "n"
N-12, MEGA GREEN, N-12 STIB, N-12 WTIB, HP STORM, SaniTite, SaniTite HP, N-12 Low Head	4" - 60"	"n" = 0.012
Single Wall Highway and Heavy Duty *	18" - 24"	"n" = 0.020
	12" - 15"	"n" = 0.018
	10"	"n" = 0.017
		"n" = 0.016
	3" - 6"	"n" = 0.015
TripleWall and Smoothwall Sewer & Drain	3" - 6"	"n" = 0.009 **
Conveyance	Conveyance Equations: $k = Q/(s^{\wedge}0.5)$ Q = $k s^{\wedge}0.5$	

| | | | |

 |

 | | | | |
 | ,- | | ~~ |
 | ~~ | ۲. | ~~ | _
 | ഗ | က | ~ |
|------------|----------------------|-----------------------------------------------------------------------------------------------------|---------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------

-------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|---------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|---------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|---------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|---------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|-----------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|---------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------

------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|--------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|-----------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|----------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------
------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|---------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|
| | 0.025 | 0.5 | 1.0 | 2.9

 | 6.3

 | 11.4 | 18.5 | 33.6 | 54.6 | 82.4
 | 117.6 | 161.0 | 213.3 | 275.0
 | 346.8 | 523.2 | 628.8 | 746.5
 | 1022. | 1354. | 2202.2 |
| | 0.024 | 0.5 | 1.0 | 3.0

 | 6.5

 | 11.9 | 19.3 | 35.0 | 56.9 | 82.8
 | 122.5 | 167.8 | 222.2 | 286.5
 | 361.3 | 545.0 | 655.0 | 778.1
 | 1065.2 | 1410.7 | 2294.0 |
| | 0.023 | 0.5 | 1.1 | 3.2

 | 6.8

 | 12.4 | 20.1 | 36.5 | 59.4 | 9.68
 | 127.9 | 175.0 | 231.8 | 298.9
 | 377.0 | 568.7 | 683.5 | 811.9
 | 1111.5 | 1472.1 | 2393.7 |
| | 0.022 | 0.5 | 1.1 | 3.3

 | 7.1

 | 12.9 | 21.1 | 38.2 | 62.1 | 93.6
 | 133.7 | 183.0 | 242.4 | 312.5
 | 394.1 | 594.5 | 714.6 | 848.8
 | 1162.0 | 1539.0 | 2502.5 |
| | 0.021 | 0.5 | 1.2 | 3.5

 | 7.5

 | 13.6 | 22.1 | 40.0 | 65.0 | 98.1
 | 140.0 | 191.7 | 253.9 | 327.4
 | 412.9 | 622.8 | 748.6 | 889.2
 | 1217.4 | 1612.3 | 2621.7 |
| | 0.020 | 9.0 | 1.2 | 3.6

 | 7.9

 | 14.2 | 23.2 | 42.0 | 68.3 | 103.0
 | 147.0 | 201.3 | 266.6 | 343.8
 | 433.5 | 654.0 | 786.1 | 933.7
 | 1278.2 | 1692.9 | 2752.8 |
| | 0.019 | 9.0 | 1.3 | 3.8

 | 8.3

 | 15.0 | 24.4 | 44.2 | 71.9 | 108.4
 | 154.8 | 211.9 | 280.6 | 361.9
 | 456.4 | 688.4 | 827.4 | 982.8
 | 1345.5 | 1782.0 | 2897.7 |
| | 0.018 | 9.0 | 1.4 | 4.1

 | 8.7

 | 15.8 | 25.7 | 46.7 | 75.9 | 114.4
 | 163.4 | 223.7 | 296.2 | 382.0
 | 481.7 | 726.6 | 873.4 | 1037.4
 | 1420.2 | 1881.0 | 3058.7 |
| les | 0.017 | 0.7 | 1.5 | 4.3

 | 9.5

 | 16.8 | 27.2 | 49.4 | 80.3 | 121.2
 | 173.0 | 236.8 | 313.7 | 404.4
 | 510.0 | 769.4 | 924.8 | 1098.4
 | 1503.8 | 1991.6 | 3238.6 |
| s "n" Valu | 0.016 | 0.7 | 1.5 | 4.6

 | 9.8

 | 17.8 | 28.9 | 52.5 | 85.3 | 128.7
 | 183.8 | 251.6 | 333.3 | 429.7
 | 541.9 | 817.5 | 982.6 | 1167.1
 | 1597.8 | 2116.1 | 3441.0 |
| Manning' | 0.015 | 9.0 | 1.6 | 4.9

 | 10.5

 | 19.0 | 30.9 | 26.0 | 91.0 | 137.3
 | 196.1 | 268.4 | 355.5 | 458.3
 | 578.0 | 871.9 | 1048.1 | 1244.9
 | 1704.3 | H | 3670.4 |
| | 0.014 | 8.0 | 1.8 | 5.2

 | 11.2

 | 20.3 | 33.1 | 0.09 | 97.5 | 147.1
 | 210.1 | 287.6 | 380.9 | 491.1
 | 619.3 | 934.2 | 1122.9 | 1333.8
 | 1826.0 | 2418.4 | 3932.6 |
| | 0.013 | 6.0 | 1.9 | 9.9

 | 12.1

 | 21.9 | 35.6 | 64.6 | 105.0 | 158.4
 | 226.2 | 309.7 | 410.2 | 528.9
 | 0.799 | 1006.1 | 1209.3 | 1436.4
 | 1966.5 | 4 | 4235.1 |
| | 0.012 | 1.0 | 2.1 | 6.1

 | 13.1

 | 23.7 | 38.6 | 70.0 | 113.8 | 171.6
 | 245.1 | 335.5 | 444.3 | 572.9
 | 722.6 | 1089.9 | 1310.1 | 1556.1
 | 2130.4 | 2821.5 | 4588.0 |
| | 0.011 | 1.0 | 2.2 | 9.9

 | 14.3

 | 25.9 | 42.1 | 26.3 | 124.1 | 187.3
 | 267.3 | 366.0 | 484.7 | 625.0
 | 788.2 | 1189.0 | 1429.2 | 1697.6
 | 2324.0 | 3078.0 | 5005.1 |
| | 0.010 | 1.1 | 2.5 | 7.3

 | 15.7

 | 28.5 | 46.3 | 84.0 | 136.6 | 206.0
 | 294.1 | 402.6 | 533.2 | 687.5
 | 867.1 | 1307.9 | 1572.1 | 1867.4
 | 2556.4 | 3385.8 | 5505.6 |
| | 0.009 | 1.3 | 2.7 | 8.1

 | 17.5

 | 31.6 | 51.5 | 93.3 | 151.7 | 228.9
 | 326.8 | 447.3 | 592.5 | 763.9
 | 963.4 | | |
 | | - | 6117.3 |
| | Area
iq. ft.) | 0.05 | 60.0 | 0.20

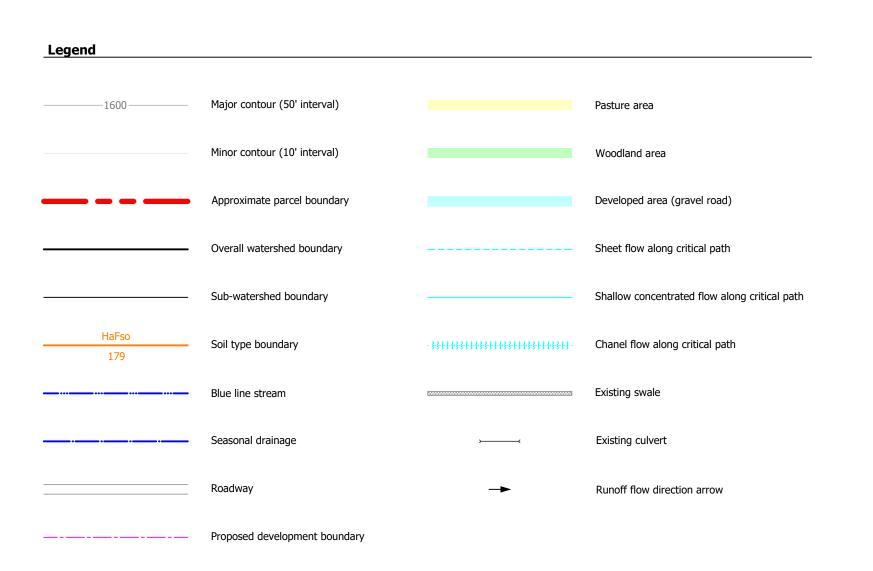
 | 0.35

 | 0.55 | 0.79 | 1.23 | 1.77 | H
 | | | |
 | 7.07 | | |
 | | H | 28.27 |
| | Dia.
(in.) | က | 4 | 9

 | 8

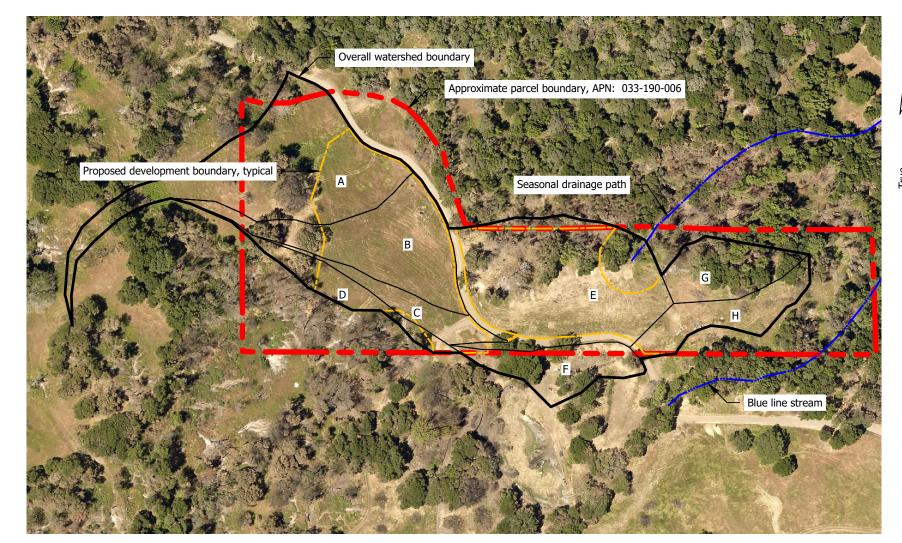
 | 10 | 12 | 15 | 18 | 21
 | 24 | 27 | 30 | 33
 | 36 | 42 | 45 | 48
 | 54 | 09 | 72 2 |
| | Manning's "n" Values | Area Area 0.009 0.010 0.011 0.012 0.013 0.014 0.015 0.016 0.017 0.018 0.019 0.020 0.021 0.022 0.023 | Area Area 0.009 0.010 0.011 0.012 0.013 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0 | Area Accidental Seq. ft.) 0.009 0.010 0.011 0.012 0.013 0.014 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.020 0.020 0.020 0.020 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 <th>Area Accidental Seq. ft.) 0.009 0.010 0.011 0.012 0.013 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014<th>Area Acea (sq. ft.) 0.009 0.010 0.011 0.012 0.013 0.014 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020</th><th>Area Acea 0.009 0.010 0.011 0.012 0.013 0.014 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0</th><th>Area O.009 O.010 O.011 O.012 O.014 O.015 O.014 O.015 O.014 O.015 O.014 O.015 O.016 O.017 O.016 O.016 O.017 O.016 O.016 O.017 O.016 O.016 O.020 O.020</th><th>Area Acea 0.009 0.010 0.011 0.012 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.014 0.015 0.014 0.015 0.014 0.014 0.015 0.014 0.015 0.014 0.015 0.015 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0</th><th>Area Acea 0.009 0.010 0.011 0.012 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.014 0.015 0.014 0.015 0.014 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.014 0.015 0.014 0.015 0.014 0.015 0.015 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0</th><th>Area Accidentes Co.00 0.010 0.011 0.014 0.015 0.016 0.017 0.018 0.019 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020
0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020</th><th>Area Acea 0.010 0.011 0.012 0.014 0.015 0.016 0.017 0.018 0.010 0.012 0.012 0.012 0.023 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0</th><th>Area O.009 0.011 0.012 0.014 0.015 0.017 0.018 0.019 0.020 0.021 0.023 0.024 0.05 1.3 1.1 1.0 0.01 0.014 0.015 0.017 0.018 0.019 0.019 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020</th><th>Area 6.009 0.010 0.010 0.011 0.012 0.013 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 <th< th=""><th>Area O.009 O.010 O.011 O.012 O.014 O.015 O.014 O.015 O.014 O.015 O.014 O.015 O.014 O.015 O.014 O.015 O.016 O.016 O.020 O.020 O.016 O.016 O.020 O.020 O.016 O.016 O.020 O.020 O.016 O.016 O.020 O.020</th><th>Area 6cg. ft. b) 0.009 0.011 0.012 0.014 0.015 0.015 0.019 0.019 0.019 0.019 0.019 0.019 0.019 0.019 0.019 0.019 0.019 0.019 0.019 0.019 0.019 0.019 0.019 0.019 0.019 0.019 0.019 0.019 0.019 0.019 0.019 0.019 0.019 0.019 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0</th><th>Advata Aga, ft. 0.009 0.010 0.011 0.012 0.014 0.014 0.015 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.015 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024</th><th>Area O.09 O.010 O.011 O.012 O.014 O.015 O.017 O.018 O.019 O.020 O.020 O.021 O.024 O.024 O.017 O.016 O.018 O.020 O.021 O.025 O.024 O.02 O.017 O.016 O.016 O.02 O.025 O.025 O.025 O.025 O.025 O.025 O.025 O.025 O.025 O.026 O.026 O.026 O.027 O.06 O.07 O.07 O.06 O.06 O.07 O.07 O.06 O.06 O.07 O.07 O.06 O.06 O.07 O.07 O.06 O.07 O.07 O.06 O.07 O.07 O.07 O.07 O.09 O.09 O.07 O.07 O.07 O.06 O.07 O.07<th>Aveal O.009 O.010 O.011 O.012 O.013 O.014 O.015 O.014 <th< th=""><th>Area O.009 0.010 0.011 0.012 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.02 0.02 0.02 0.02 0.02 0.02 0.014 0.014 0.014 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02</th><th>Area Loo 0.010 0.011 0.012 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.015 0.017 0.016 0.019 0.020 0.021 0.025 0.025 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02
0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02</th></th<></th></th></th<></th></th> | Area Accidental Seq. ft.) 0.009 0.010 0.011 0.012 0.013 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 <th>Area Acea (sq. ft.) 0.009 0.010 0.011 0.012 0.013 0.014 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020</th> <th>Area Acea 0.009 0.010 0.011 0.012 0.013 0.014 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0</th> <th>Area O.009 O.010 O.011 O.012 O.014 O.015 O.014 O.015 O.014 O.015 O.014 O.015 O.016 O.017 O.016 O.016 O.017 O.016 O.016 O.017 O.016 O.016 O.020 O.020</th> <th>Area Acea 0.009 0.010 0.011 0.012 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.014 0.015 0.014 0.015 0.014 0.014 0.015 0.014 0.015 0.014 0.015 0.015 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0</th> <th>Area Acea 0.009 0.010 0.011 0.012 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.014 0.015 0.014 0.015 0.014 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.014 0.015 0.014 0.015 0.014 0.015 0.015 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0</th> <th>Area Accidentes Co.00 0.010 0.011 0.014 0.015 0.016 0.017 0.018 0.019 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020</th> <th>Area Acea 0.010 0.011 0.012 0.014 0.015 0.016 0.017 0.018 0.010 0.012 0.012 0.012 0.023 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0</th> <th>Area O.009 0.011 0.012 0.014 0.015 0.017 0.018 0.019 0.020 0.021 0.023 0.024 0.05 1.3 1.1 1.0 0.01 0.014 0.015 0.017 0.018 0.019 0.019 0.020 0.020 0.020
0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020</th> <th>Area 6.009 0.010 0.010 0.011 0.012 0.013 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 <th< th=""><th>Area O.009 O.010 O.011 O.012 O.014 O.015 O.014 O.015 O.014 O.015 O.014 O.015 O.014 O.015 O.014 O.015 O.016 O.016 O.020 O.020 O.016 O.016 O.020 O.020 O.016 O.016 O.020 O.020 O.016 O.016 O.020 O.020</th><th>Area 6cg. ft. b) 0.009 0.011 0.012 0.014 0.015 0.015 0.019 0.019 0.019 0.019 0.019 0.019 0.019 0.019 0.019 0.019 0.019 0.019 0.019 0.019 0.019 0.019 0.019 0.019 0.019 0.019 0.019 0.019 0.019 0.019 0.019 0.019 0.019 0.019 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0</th><th>Advata Aga, ft. 0.009 0.010 0.011 0.012 0.014 0.014 0.015 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.015 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024</th><th>Area O.09 O.010 O.011 O.012 O.014 O.015 O.017 O.018 O.019 O.020 O.020 O.021 O.024 O.024 O.017 O.016 O.018 O.020 O.021 O.025 O.024 O.02 O.017 O.016 O.016 O.02 O.025 O.025 O.025 O.025 O.025 O.025 O.025 O.025 O.025 O.026 O.026 O.026 O.027 O.06 O.07 O.07 O.06 O.06 O.07 O.07 O.06 O.06 O.07 O.07 O.06 O.06 O.07 O.07 O.06 O.07 O.07 O.06 O.07 O.07 O.07 O.07 O.09 O.09 O.07 O.07 O.07 O.06 O.07 O.07<th>Aveal O.009 O.010 O.011 O.012 O.013 O.014 O.015 O.014 <th< th=""><th>Area O.009 0.010 0.011 0.012 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.02 0.02 0.02 0.02 0.02 0.02 0.014 0.014 0.014 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02</th><th>Area Loo 0.010 0.011 0.012 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.015 0.017 0.016 0.019 0.020 0.021 0.025 0.025 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02</th></th<></th></th></th<></th> | Area Acea (sq. ft.) 0.009 0.010 0.011 0.012 0.013 0.014 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 | Area Acea 0.009 0.010 0.011 0.012 0.013 0.014 0.015 0.015 0.015 0.015 0.015 0.015
0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0 | Area O.009 O.010 O.011 O.012 O.014 O.015 O.014 O.015 O.014 O.015 O.014 O.015 O.016 O.017 O.016 O.016 O.017 O.016 O.016 O.017 O.016 O.016 O.020 O.020 | Area Acea 0.009 0.010 0.011 0.012 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.014 0.015 0.014 0.015 0.014 0.014 0.015 0.014 0.015 0.014 0.015 0.015 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0 | Area Acea 0.009 0.010 0.011 0.012 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.014 0.015 0.014 0.015 0.014 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.014 0.015 0.014 0.015 0.014 0.015 0.015 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0 | Area Accidentes Co.00 0.010 0.011 0.014 0.015 0.016 0.017 0.018 0.019 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 | Area Acea 0.010 0.011 0.012 0.014 0.015 0.016 0.017 0.018 0.010 0.012 0.012 0.012 0.023 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0 | Area O.009 0.011 0.012 0.014 0.015 0.017 0.018 0.019 0.020 0.021 0.023 0.024 0.05 1.3 1.1 1.0 0.01 0.014 0.015 0.017 0.018 0.019 0.019 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 | Area 6.009 0.010 0.010 0.011 0.012 0.013 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 <th< th=""><th>Area O.009 O.010 O.011 O.012 O.014 O.015 O.014 O.015 O.014 O.015 O.014 O.015 O.014 O.015 O.014 O.015 O.016 O.016 O.020 O.020 O.016 O.016 O.020 O.020 O.016 O.016 O.020 O.020 O.016 O.016 O.020 O.020</th><th>Area 6cg. ft. b) 0.009 0.011 0.012 0.014 0.015 0.015 0.019 0.019 0.019 0.019 0.019 0.019 0.019 0.019 0.019 0.019 0.019 0.019 0.019 0.019 0.019 0.019 0.019 0.019 0.019 0.019 0.019 0.019 0.019 0.019 0.019 0.019 0.019 0.019 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02
 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0</th><th>Advata Aga, ft. 0.009 0.010 0.011 0.012 0.014 0.014 0.015 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.015 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024</th><th>Area O.09 O.010 O.011 O.012 O.014 O.015 O.017 O.018 O.019 O.020 O.020 O.021 O.024 O.024 O.017 O.016 O.018 O.020 O.021 O.025 O.024 O.02 O.017 O.016 O.016 O.02 O.025 O.025 O.025 O.025 O.025 O.025 O.025 O.025 O.025 O.026 O.026 O.026 O.027 O.06 O.07 O.07 O.06 O.06 O.07 O.07 O.06 O.06 O.07 O.07 O.06 O.06 O.07 O.07 O.06 O.07 O.07 O.06 O.07 O.07 O.07 O.07 O.09 O.09 O.07 O.07 O.07 O.06 O.07 O.07<th>Aveal O.009 O.010 O.011 O.012 O.013 O.014 O.015 O.014 <th< th=""><th>Area O.009 0.010 0.011 0.012 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.02 0.02 0.02 0.02 0.02 0.02 0.014 0.014 0.014 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02</th><th>Area Loo 0.010 0.011 0.012 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.015 0.017 0.016 0.019 0.020 0.021 0.025 0.025 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02</th></th<></th></th></th<> | Area O.009 O.010 O.011 O.012 O.014 O.015 O.014 O.015 O.014 O.015 O.014 O.015 O.014 O.015 O.014 O.015 O.016 O.016 O.020 O.020 O.016 O.016 O.020 O.020 O.016 O.016 O.020 O.020 O.016 O.016 O.020 O.020 | Area 6cg. ft. b) 0.009 0.011 0.012 0.014 0.015 0.015 0.019 0.019 0.019 0.019 0.019 0.019 0.019 0.019 0.019 0.019 0.019 0.019 0.019 0.019 0.019 0.019 0.019 0.019 0.019 0.019 0.019 0.019 0.019 0.019 0.019 0.019 0.019 0.019 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0 | Advata Aga, ft. 0.009 0.010 0.011 0.012 0.014 0.014 0.015 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.015 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 | Area O.09 O.010 O.011 O.012 O.014 O.015 O.017 O.018 O.019 O.020 O.020 O.021 O.024 O.024 O.017 O.016 O.018 O.020 O.021 O.025 O.024 O.02 O.017 O.016 O.016 O.02 O.025 O.025 O.025 O.025 O.025 O.025 O.025 O.025 O.025 O.026 O.026 O.026 O.027 O.06 O.07 O.07 O.06 O.06 O.07 O.07 O.06 O.06 O.07 O.07 O.06 O.06 O.07 O.07 O.06 O.07 O.07 O.06 O.07 O.07 O.07 O.07 O.09 O.09 O.07 O.07 O.07 O.06 O.07 O.07 <th>Aveal O.009 O.010 O.011 O.012 O.013 O.014 O.015 O.014 <th< th=""><th>Area O.009 0.010 0.011 0.012 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.02 0.02 0.02 0.02 0.02 0.02 0.014 0.014 0.014
 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02</th><th>Area Loo 0.010 0.011 0.012 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.015 0.017 0.016 0.019 0.020 0.021 0.025 0.025 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02</th></th<></th> | Aveal O.009 O.010 O.011 O.012 O.013 O.014 O.015 O.014 O.014 <th< th=""><th>Area O.009 0.010 0.011 0.012 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.02 0.02 0.02 0.02 0.02 0.02 0.014 0.014 0.014 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02</th><th>Area Loo 0.010 0.011 0.012 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.015 0.017 0.016 0.019 0.020 0.021 0.025 0.025 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02</th></th<> | Area O.009 0.010 0.011 0.012 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.014 0.02 0.02 0.02 0.02 0.02 0.02 0.014 0.014 0.014 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 | Area Loo 0.010 0.011 0.012 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.015 0.014 0.015 0.017 0.016 0.019 0.020 0.021 0.025 0.025 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 |

^{*} Corrugated Polyethylene Pipe Association (2000) "Hydraulic Considerations for Corrugated Polyethylene Pipe" ** "Lingedburg, Michael, "Civil Engineer Reference Manual"⁴



Watershed	Land Use	Hydrologic Condition	Hydrologic Soil Group	Acres	Curve Number
А	Pasture, grassland or range	Good	D*	1.74	80
	Woods - grass combination	Good	D*	0.47	79
	Total			2.21	80
В	Pasture, grassland or range	Good	D	1.17	80
	Woods - grass combination	Good	D	0.14	79
	Total			1.31	80
С	Gravel (w/ right-of-way)		D	0.02	91
	Pasture, grassland or range	Good	D	0.33	80
	Woods - grass combination	Good	D	0.03	79
	Total			0.38	81
D	Gravel (w/ right-of-way)		D	0.01	91
	Pasture, grassland or range	Good	D	0.27	80
	Woods - grass combination	Good	D	0.14	79
	Total			0.42	80
	Gravel (w/ right-of-way)	200 100	D	0.21	91
Е	Pasture, grassland or range	Fair	D	1.23	84
	Woods - grass combination	Fair	D	0.93	82
	Total			2.37	84
F	Pasture, grassland or range	Fair	D	0.38	84
	Woods - grass combination	Fair	D	0.24	82
	Total			0.62	83
	Pasture, grassland or range	Fair	D	0.12	84
G	Woods - grass combination	Fair	D	0.51	82
	Total			0.63	82
Н	Gravel (w/ right-of-way)		D	0.01	91
	Pasture, grassland or range	Fair	D	0.53	84
	Woods - grass combination	Fair	D	0.06	82
	Total			0.60	84

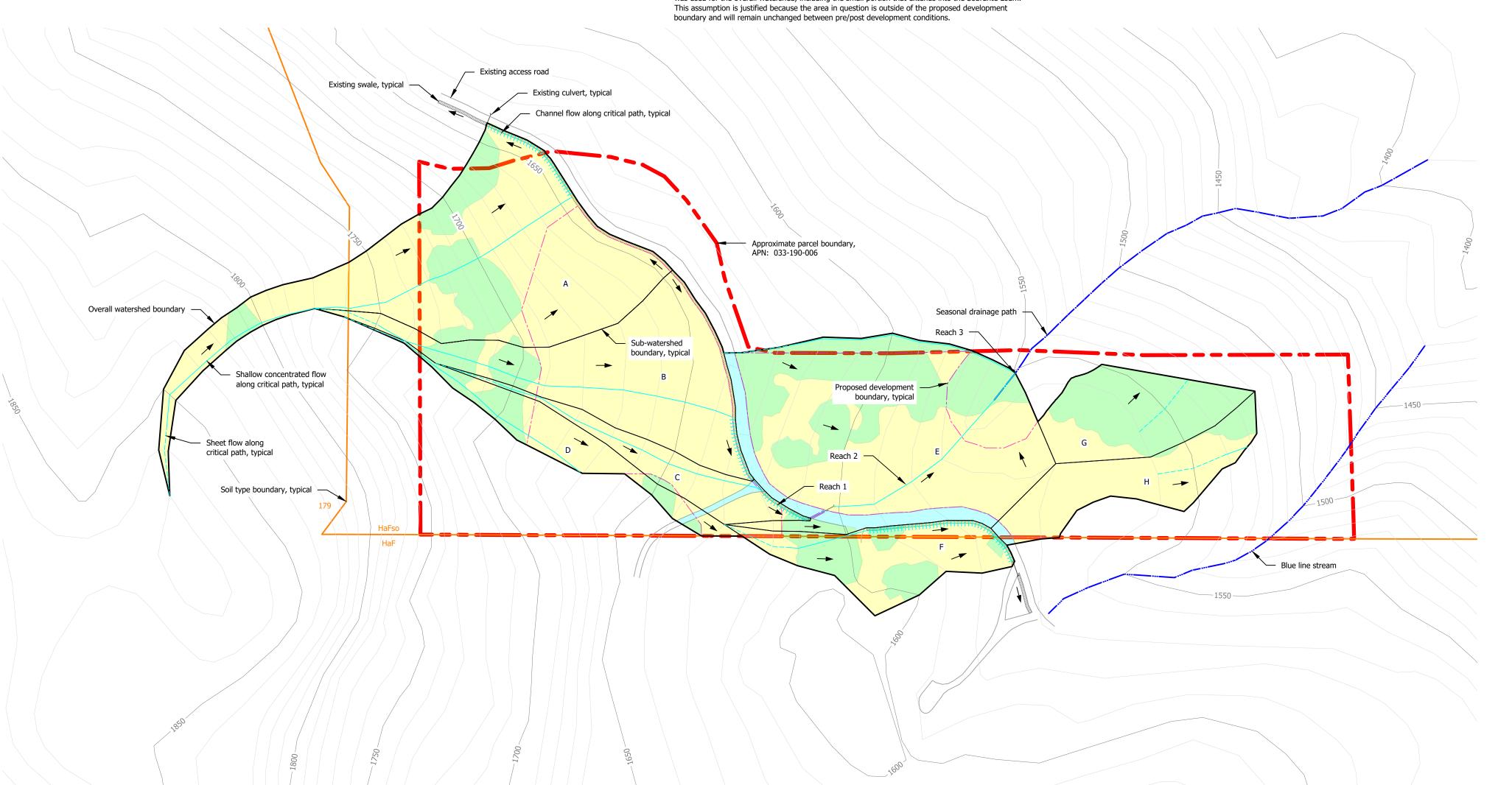
* The majority of the overall watershed rests on Hambright Loam. Hambright Loam is classified as Hydrologic Soil Group D. A small portion of sub-watershed A extends into the Sobrante Loam. Sobrante Loam is classified as Hydrologic Soil Group C. In an effort to simplify the analysis hydrologic soil group D was used for the overall watershed, including the small portion that extends into the Sobrante Loam.



Watershed Aerial Map
Scale: 1" = 200'

Topographic information provided by Napa County GIS database from 2002.
 Datum: North American Vertical Datum of 1988 (NAVD 88).
 Aerial image is from 2018 and was provided by Napa County.

<u>Soil Types on Site:</u> 179 - Sobrante loam, Hydrologic Soil Group C HaFso, HaF - Hambright loam, Hydrologic Soil Group D



Pre-Development Site Plan
Scale: 1" = 100'

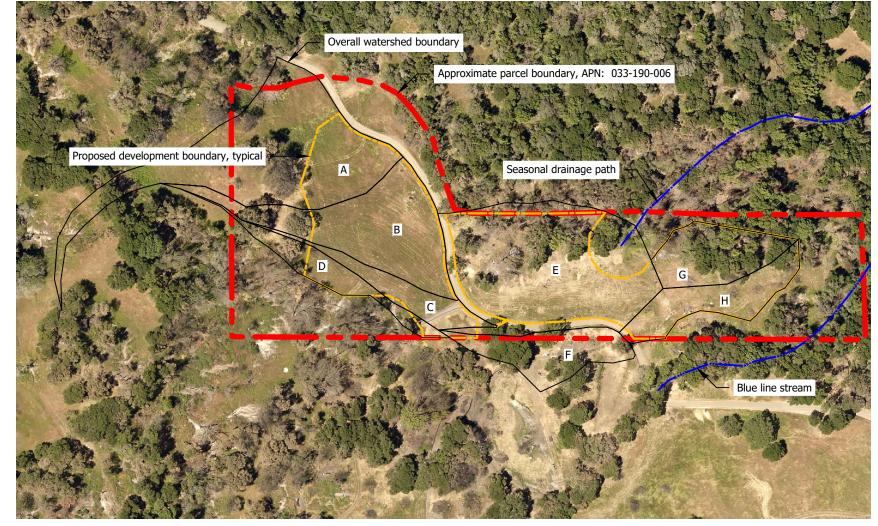
NEW VINEYARD DEVELOPMENT PRE-DEVELOPMENT SITE PLAN AND CURCVE NUMBERS LANDS OF BUTLER

Legend				
1600	Major contour (50' interval)		Pasture area	
	Minor contour (10' interval)		Woodland area	
	Approximate parcel boundary		Developed area (gravel road)	
	Watershed area boundary		Sheet flow along critical path	
	Watershed sub-area boundary		Shallow concentrated flow along critical path	
HaFso 179	Soil type boundary	·#####################################	Chanel flow along critical path	
	Blue line stream		Existing swale	
	Seasonal drainage		Existing culvert	
	Roadway		Runoff flow direction arrow	
	Proposed development area (vineyard)			

Watershed	Land Use	Hydrologic Condition	Hydrologic Soil Group	Acres	Curve Number
А	Pasture, grassland or range	Good	D*	1.74	80
	Woods - grass combination	Good	D*	0.47	79
	Total			2.21	80
В	Pasture, grassland or range	Good	D	1.17	80
	Woods - grass combination	Good	D	0.14	79
	Total			1.31	80
	Pasture, grassland or range	Good	D	0.35	80
С	Woods - grass combination	Good	D	0.03	79
	Total			0.38	80
D	Pasture, grassland or range	Good	D	0.28	80
	Woods - grass combination	Good	D	0.14	79
	Total		_	0.42	80
	Gravel (w/ right-of-way)	S-10	D	0.21	91
_	Pasture, grassland or range	Fair	D	0.13	84
Е	Pasture, grassland or range	Good	D	1.72	80
	Woods - grass combination	Fair	D	0.31	82
	Total			2.37	81
	Pasture, grassland or range	Fair	D	0.37	84
F	Pasture, grassland or range	Good	D	0.02	80
F	Woods - grass combination	Fair	D	0.23	82
	Total			0.62	83
G	Pasture, grassland or range	Good	D	0.63	80
	Total			0.63	80
Н	Gravel (w/ right-of-way)		D	0.01	91
	Pasture, grassland or range	Fair	D	0.01	84
	Pasture, grassland or range	Good	D	0.58	80
	Total	0000		0.60	80

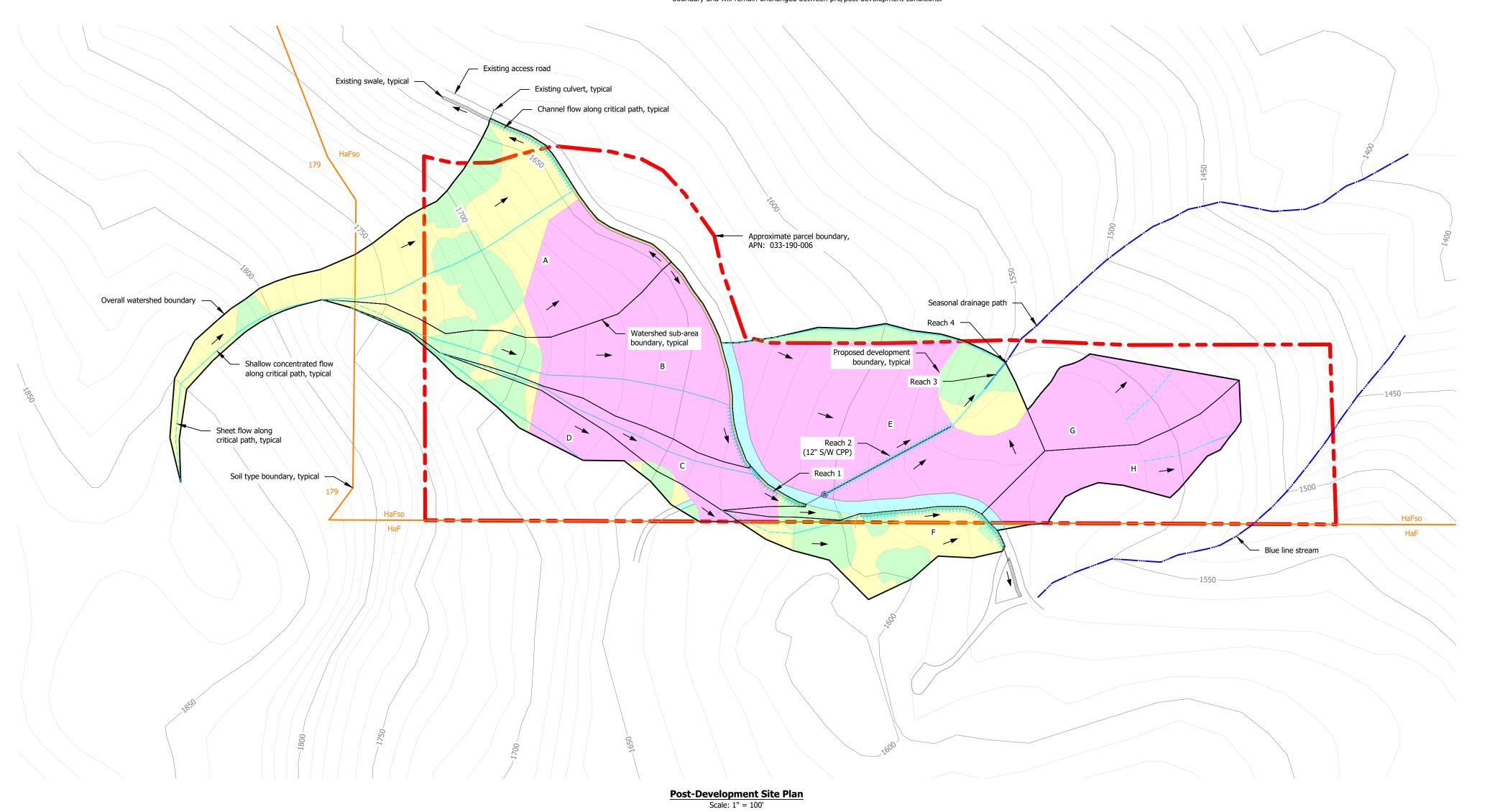
* The majority of the overall watershed rests on Hambright Loam. Hambright Loam is classified as Hydrologic Soil Group D. A small portion of sub-watershed A extends into the Sobrante Loam is classified as Hydrologic Soil Group C. In an effort to simplify the analysis hydrologic soil group D was used for the overall watershed, including the small portion that extends into the Sobrante Loam.

This assumption is justified because the area in question is outside of the proposed development boundary and will remain unchanged between pre/post development conditions.



Notes:
 Topographic information provided by Napa County GIS database from 2002.
 Datum: North American Vertical Datum of 1988 (NAVD 88).
 Aerial image is from 2018 and was provided by Napa County.

<u>Soil Types on Site:</u> 179 - Sobrante Ioam, Hydrologic Soil Group C HaFso, HaF - Hambright Ioam, Hydrologic Soil Group D



LANDS OF BUTLER

NEW VINEYARD DEVELOPMENT POST-DEVELOPMENT SITE PLAN AND CURVE NUMBERS