Public Review Draft

# INTERSTATE 80/RICHARDS BOULEVARD INTERCHANGE IMPROVEMENTS PROJECT 

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Initial Study/Mitigated Negative Declaration


# INTERSTATE 80/RICHARDS BOULEVARD <br> INTERCHANGE IMPROVEMENTS PROJECT 

Initial Study/Mitigated Negative Declaration

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## Introduction

The City of Davis, in cooperation with the California Department of Transportation (Caltrans), proposes to reconstruct the westbound ramps at the Interstate 80 (I-80)/Richards Boulevard interchange in the City of Davis by converting from a cloverleaf to a tight diamond configuration, construct a grade-separated bicycle and pedestrian path along the west side of Richards Boulevard, close the isolated westbound off-ramp to Olive Drive, and make other related improvements to relieve existing congestion at the interchange to accommodate increased traffic demand generated by approved and/or proposed developments in the project area and to reduce conflicts between bicyclists, pedestrians, and vehicles. The City of Davis is the lead agency under California Environmental Quality Act (CEQA). Caltrans is a Responsible Agency for the proposed project under CEQA. As defined in Public Resources Code Section 21069, a Responsible Agency is a public agency, other than the lead agency, which has responsibility for carrying out or approving a project.

## Project Description

## Project Components

The proposed project would reconfigure the westbound I-80 ramps from a full cloverleaf to a tight diamond configuration by consolidating the two off-ramps into a single diagonal off-ramp and the two on-ramps into a single diagonal on-ramp. The resulting westbound I-80 ramp terminal intersection would include new traffic signals. The westbound I-80 on-ramp would require widening of I-80 over the existing bike and pedestrian tunnel. Figure 1 shows the project location, Figure 2 shows the project footprint, and Figure 3 shows the project design.

The eastbound I-80 ramp intersection would remain as a cloverleaf. Project improvements include widening the eastbound off-ramp to include a right-turn lane and two left-turn lanes. Richards Boulevard would be widened to provide two southbound through movements at the Research Park Drive/Richards Boulevard intersection.

The project would modify the Olive Drive/Richards Boulevard intersection providing the width, lane geometry, and right-of-way necessary for future developments on Olive Drive. The existing nearside bus stop on Richards Boulevard near Olive Drive would be relocated to the north of the Olive Drive/Richards Boulevard intersection. Along Eastbound Richards Boulevard, improvements would connect the mixed-use paths; include a left-turn lane, a through lane, and a combination through-right lane on the intersection entrance; and include two through lanes on the eastbound intersection egress.

Between the Olive Drive/Richards Boulevard intersection and the westbound I-80 ramp terminal intersection, improvements would include widening Richards Boulevard and installing a raised median to restrict let turn movements.


Figure 1



The project would include construction of a shared-use path along the west side of Richards Boulevard replacing the existing sidewalk, and serving both bicyclists and pedestrians. The shared-use path would connect to the existing path south of Olive Drive, diverge from Richards Boulevard to pass under the westbound I-80 on-ramp, then loop up to connect with the Richards Boulevard overcrossing. After passing over the existing structure, the shared-use path would terminate at the Research Park Drive/Richards Boulevard intersection. The project would widen the existing Class II bicycle lanes along Richards Boulevard between Olive Drive and Research Park Drive to a minimum of 7 feet.

The project would close the isolated westbound off-ramp to Olive Drive.
The elements of the interchange reconstruction and associated intersection widening are listed below.

- Install a traffic signal at the new westbound ramp terminal intersection
- Install a ramp meter signal on the new westbound on-ramp with two metered lanes and an HOV bypass lane
- At Richards Boulevard/Olive Drive, widen the northbound approach to provide a second leftturn lane, the southbound approach to provide a second through lane, and the east leg to provide two receiving lanes and eastbound left, through, and right lanes (one each)
- At Richards Boulevard/I 80 eastbound Ramps, widen the eastbound off-ramp approach to provide a second left-turn lane
- At Richards Boulevard/Cowell Boulevard/Research Park Drive, widen southbound Richards Boulevard to provide a second through lane.


## Construction Activities and Schedule

Construction is anticipated to last a total of approximately 18 months. The project would be completed in a single phase and construction activities would include clearing vegetation, grading, hauling materials, excavation, placing embankment, drainage, and paving roadway surfaces.

## ENVIRONMENTAL CHECKLIST Initial Study

\author{

1. Project Title: <br> 2. Lead Agency Name and Address: <br> 3. Contact Person and Phone Number: <br> 4. Project Location: <br> 5. Project Sponsor's Name and Address: <br> Interstate 80/Richards Boulevard Interchange Improvements Project <br> City of Davis <br> Department of Public Works <br> Engineering \& Transportation Department <br> 1717 Fifth Street <br> Davis, CA 95616 <br> Kevin Fong, P.E. <br> Senior Civil Engineer <br> 530-747-8285 <br> City of Davis <br> City of Davis <br> Department of Public Works <br> Engineering \& Transportation Department 1717 Fifth Street <br> Davis, CA 95616 <br> 6. General Plan Designation(s): <br> 7. Zoning: <br> Planned Development (PD) <br> \section*{8. Description of Project:}
}

The City of Davis, in cooperation with Caltrans, proposes to reconstruct the westbound ramps at the I-80/Richards Boulevard interchange in the City of Davis by converting from a cloverleaf to a tight diamond configuration, construct a grade-separated bicycle and pedestrian path along the west side of Richards Boulevard, close the isolated westbound off-ramp to Olive Drive, and make other related improvements to relieve existing congestion at the interchange to accommodate increased traffic demand generated by approved and/or proposed developments in the project area and to reduce conflicts between bicyclists, pedestrians, and vehicles.

## 9. Surrounding Land Uses and Setting:

Land uses to the south and south east of the project site include retail and commercial establishments, restaurants, hotels, and UC Davis Extension buildings. Land uses to the west and northwest of the project site include retail and commercial establishments, restaurants, a gas station, a hotel, and apartments, including Cesar Chavez Plaza Permanent Supportive Housing.
10. Other public agencies whose approval is required (e.g., permits, financing approval, or participation agreement.)

Caltrans is a Responsible Agency for the proposed project. As defined in Public Resources Code Section 21069, a Responsible Agency is a public agency, other than the lead agency, which has responsibility for carrying out or approving a project. Caltrans is a participant in the City of Davis CEQA process for the proposed project and will use the City's CEQA document when making decisions on the proposed project.
11. Have California Native American tribes traditionally and culturally affiliated with the project area requested consultation pursuant to Public Resources Code section 21080.3.1? If so, is there a plan for consultation that includes, for example, the determination of significance of impacts to tribal cultural resources, procedures regarding confidentiality, etc.?

The City of Davis has consulted with California Native American tribes pursuant to Public Resources Code section 21080.3.1. The details of this consultation are provided in the Cultural Resources and Tribal Cultural Resources sections of this initial study,

## Environmental Factors Potentially Affected

The environmental factors checked below would be potentially affected by this project, involving at least one impact that is a "Potentially Significant Impact" as indicated by the checklist on the following pages.

| $\square$ | Aesthetics | $\square$ | Agriculture and Forestry Resources | $\boxed{y}$ |
| :--- | :--- | :--- | :--- | :--- | Air Quality

## DETERMINATION: (To be completed by the Lead Agency) <br> On the basis of this initial study:

I find that the proposed project COULD NOT have a significant effect on the environment, and a NEGATIVE DECLARATION will be prepared.$\boxtimes$ I find that although the proposed project could have a significant effect on the environment, there will not be a significant effect in this case because revisions in the project have been made by or agreed to by the project proponent. A MITIGATED NEGATIVE DECLARATION will be prepared.
$\square \quad$ I find that the proposed project MAY have a significant effect on the environment, and an ENVIRONMENTAL IMPACT REPORT is required.I find that the proposed project MAY have a "potentially significant impact" or "potentially significant unless mitigated" impact on the environment, but at least one effect 1) has been adequately analyzed in an earlier document pursuant to applicable legal standards, and 2) has been addressed by mitigation measures based on the earlier analysis as described on attached sheets. An ENVIRONMENTAL IMPACT REPORT is required, but it must analyze only the effects that remain to be addressed.

I find that although the proposed project could have a significant effect on the environment, because all potentially significant effects (a) have been analyzed adequately in an earlier EIR or NEGATIVE DECLARATION pursuant to applicable standards, and (b) have been avoided or mitigated pursuant to that earlier EIR or NEGATIVE DECLARATION, including revisions or mitigation measures that are imposed upon the proposed project, nothing further is required.


## Signature

2/23/22
Date

## Environmental Checklist

## Aesthetics

| Issues（and Supporting Information Sources）： |  | Potentially <br> Significant Impact | Less Than Significant with Mitigation Incorporated | Less Than Significant Impact | No Impact |
| :---: | :---: | :---: | :---: | :---: | :---: |
| I． | AESTHETICS－Except as provided in Public Resources Code Section 21099，would the project： |  |  |  |  |
| a） | Have a substantial adverse effect on a scenic vista？ | $\square$ | $\square$ | $\square$ | 区 |
| b） | Substantially damage scenic resources，including， but not limited to，trees，rock outcroppings，and historic buildings within a state scenic highway？ | $\square$ | $\square$ | $\square$ | 区 |
| c） | Substantially degrade the existing visual character or quality of public views of the site and its surroundings？（Public views are those that are experienced from publicly accessible vantage point）． If the project is in an urbanized area，would the project conflict with applicable zoning and other regulations governing scenic Quality？ | $\square$ | $\square$ | 区 | $\square$ |
| d） | Create a new source of substantial light or glare which would adversely affect daytime or nighttime views in the area？ | $\square$ | $\square$ | 】 | $\square$ |

## Discussion

a，b）There are no known scenic resources visible from the project site nor are any of the roadways in the project area classified as scenic corridors by the State，the City of Davis， or any other entity with jurisdiction in this area（Caltrans，2018）．Implementation of the proposed project would result in no impact to a scenic vista or scenic resources．
c）The project site includes areas within the City of Davis at two primary locations：the intersection of Richards Boulevard and I－80 and the area between Olive Drive and I－80， just west of Pole Line Road．Figure 4 shows the locations photos taken of typical viewpoints of the project site．Figure 5 through Figure 7 show public views of the project site locations．Views are of urbanized areas，consisting of roads，street trees and other landscaping，street lights，fencing，street signs，commercial and industrial buildings， and a few residences．

Viewpoints 1 through 5 show typical public views of the project site from different viewpoints．The area is suburban with mostly commercial and transportation uses． Viewpoint 1 shows a view from the southeast corner of the Olive Drive／Richards Boulevard intersection，looking north．The view is urban，with wide asphalt right－of－way， cement sidewalks，light poles，a few commercial buildings，and associated landscaping． Viewpoint 2 shows a view towards the east from Olive Drive．The area is industrial in nature with street trees lining the road on one side and a chain link fence on the other． Views of the project site are limited due to the presence of trees．Viewpoint 3 shows the view of the I－80 north on－and off－ramps．Trees and other landscaping block views of the freeway from this location but the foreground views are dominated by asphalt，cement， and light poles．



Viewpoint 1: View looking north across Olive Drive intersection with Richards Boulevard.


Viewpoint 2: View from Olive Drive near Interstate 80 off-ramp looking east. -


Viewpoint 3: View from Richards Boulevard overpass looking north towards Interstate 80 north on-/off-ramp.


Viewpoint 4: View from Richards Boulevard overpass looking south towards Interstate 80 south off-ramp.


Figure 7

Viewpoint 4 shows the view from the Richards Boulevard overpass south over the I-80 south off-ramp. The interior of the off-ramp is planted with full-grown trees that block the view of the off-ramp and some farther views. The paved freeway is easily seen from this viewpoint, but further views are blocked by trees on either side. Viewpoint 5 shows the view of the Research Park Drive/Richards Boulevard intersection looking north from the southwest corner. Wide expanses of asphalt dominate the view, with trees blocking views of commercial buildings beyond. Light poles and cement sidewalks are also present.

Visual impacts are determined by assessing changes to the visual resources and predicting viewer response to those changes. The location of the proposed ramps would require the removal of some trees. This would constitute a change in the visual character as these trees would be removed. While removal of trees could affect the views experienced by travelers along I-80 and Richards Boulevard, the typical viewers of these areas are travelers in cars whose sensitivity to small changes in the aesthetic environment is low. Very few residences are within the project vicinity. As shown in Figure 3, the project would reduce the amount of asphalt by consolidating and reconfiguring on- and off-ramps. This would provide greater space for vegetation which generally softens the view and provides relief for the eye.

The visual character of the proposed project would be compatible with the existing visual character of the project site and vicinity. The existing on- and off-ramps are comprised of asphalt with high-visibility paint markings and metal light poles. The proposed on- and off-ramps would use the same types of materials. The project site does not include any elements of special visual character or design.

The visual quality of the project site and vicinity would not be altered by the proposed project. The same types of materials already present in the project site (e.g., asphalt, highvisibility paint, street signs) would be used to accomplish the project goals. The visual character of the proposed project would be compatible with the visual character of the project site and its surroundings. Consequently, implementation of the proposed project would not substantially degrade the existing visual character or quality of public views of the site and its surroundings or conflict with applicable zoning and other regulations governing scenic quality. The impact would be less than significant.
d) The materials used in the construction of the proposed project (e.g., asphalt, cement, paint) would not include any surfaces likely to produce glare. Future street lighting would comply with the City of Davis' Dark Sky Ordinance (Chapter 8, Buildings, of the Municipal Code. Article 8.17, Outdoor Lighting Control) which requires that outdoor light fixtures shall be fully shielded.

Construction of the proposed project could introduce new temporary sources of light, as construction may occur during nighttime hours. However, consistent with normal procedures, the City of Davis and Caltrans would require project contractors to direct lighting onto the immediate area under construction only and to avoid shining lights towards residences and towards traffic. Consequently, implementation of the proposed project would not create a new source of substantial light or glare which would adversely
affect daytime or nighttime views in the area, and this impact would be less than significant.

## References

California Department of Transportation (Caltrans), 2018. Visual Impact Assessment Technical Memorandum, Interstate 80/ Richards Boulevard Interchange Improvements Project. August 2018.

## Agriculture and Forestry Resources

| Issues (and Supporting Information Sources): | Potentially <br> Significant Impact | Less Than Significant with Mitigation Incorporated | Less Than Significant Impact | No Impact |
| :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |

II. AGRICULTURE AND FORESTRY RESOURCES -

In determining whether impacts to agricultural resources are significant environmental effects, lead agencies may refer to the California Agricultural Land Evaluation and Site Assessment Model (1997) prepared by the California Dept. of Conservation as an optional model to use in assessing impacts on agriculture and farmland. In determining whether impacts to forest resources, including timberland, are significant environmental effects, lead agencies may refer to information compiled by the California Department of Forestry and Fire Protection regarding the state's inventory of forest land, including the Forest and Range Assessment Project and the Forest Legacy Assessment project; and forest carbon measurement methodology provided in Forest Protocols adopted by the California Air Resources Board. Would the project:
a) Convert Prime Farmland, Unique Farmland, or Farmland of Statewide Importance (Farmland), as shown on the maps prepared pursuant to the Farmland Mapping and Monitoring Program of the California Resources Agency, to non-agricultural use?
b) Conflict with existing zoning for agricultural use, or a Williamson Act contract?
c) Conflict with existing zoning for, or cause rezoning of, forest land (as defined in Public Resources Code section 12220(g)), timberland (as defined by Public Resources Code section 4526), or timberland zoned Timberland Production (as defined by Government Code section 51104(g))?
d) Result in the loss of forest land or conversion of forest land to non-forest use?
e) Involve other changes in the existing environment which, due to their location or nature, could result in conversion of Farmland, to non-agricultural use or conversion of forest land to non-forest use?

## Discussion

a-e) The proposed project would reconstruct and reconfigure the I-80/Richards Boulevard interchange and make other related improvements to relieve existing congestion and reduce conflicts among bicyclists, pedestrians, and vehicles. There are no forested lands or lands being used for agriculture or forestry production on the project site or that would be affected by project construction or operation. For these reasons, there is no potential for the proposed project to cause loss to agriculture or forestry resources, and there would be no impact.

## Air Quality

|  | Potentially <br> Significant | Less Than <br> Significant with <br> Mitigation | Less Than <br> Significant |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Insues (and Supporting Information Sources): |  |  |  |  |  |  |  |

III. AIR QUALITY -

Where available, the significance criteria established by the applicable air quality management district or air pollution control district may be relied upon to make the following determinations. Would the project:
a) Conflict with or obstruct implementation of the applicable air quality plan?
b) Result in a cumulatively considerable net increase of any criteria pollutant for which the project region is non-attainment under an applicable federal or state ambient air quality standard?
c) Expose sensitive receptors to substantial pollutant concentrations?
d) Result in other emissions (such as those leading to odors) adversely affecting a substantial number of people?

## Environmental Setting

The project site is located in Yolo County within the Sacramento Valley Air Basin (SVAB). Air quality within Yolo County is regulated by the United States Environmental Protection Agency (U.S. EPA), and the California Air Resources Board (CARB) at the federal and state levels, respectively, and locally by the Yolo-Solano Air Quality Management District (YSAQMD). Yolo County is currently designated as a nonattainment area for the state and national ambient air quality standards for ozone $\left(\mathrm{O}_{3}\right)$. Yolo County is designated as unclassified and nonattainment for the national and state $\mathrm{PM}_{10}$ (i.e., respirable particulate matter with an aerodynamic diameter of 10 micrometers or less) standards, respectively. In addition, the eastern portion of Yolo County, including Davis, where the project site is located, is designated nonattainment for the national $\mathrm{PM}_{2.5}$ (i.e., respirable particulate matter with an aerodynamic diameter of 2.5 micrometers or less) standard (YSAQMD, 2019).

On October 11, 2017, the YSAQMD Board of Director's adopted the Sacramento Regional 2008 National Ambient Air Quality Standard (NAAQS) 8-Hour Ozone Attainment and Reasonable Further Progress Plan (Plan). The Plan geographically covers the Sacramento Federal Nonattainment Area (SFNA) which includes all of Yolo County. The Plan documents how the region is meeting requirements under the Clean Air Act (CAA) in demonstrating reasonable further progress and attainment of the 2008 NAAQS of 75 parts of ozone per billion.

In May 2019, the YSAQMD adopted its most recent Triennial Plan Update. The Triennial Plan Update is a requirement of the California Clean Air Act (CCAA). The document summarizes emission trends, forecasts future emissions, and reviews efforts made by the YSAQMD to improve air quality (YSAQMD, 2019).

Although the YSAQMD generally does not experience unhealthy levels of particulates, the U.S. EPA has included the YSAQMD in the Sacramento Federal Non-Attainment Area for fine particulate pollution. In order to show attainment of the 24 -hour fine particulate standard, an area must demonstrate that it has met the standard during three consecutive years. The Sacramento
region was able to show that the standard had been achieved during the 2010-2012 period. The YSAQMD and the other air districts of the region subsequently submitted a request to the U.S. EPA for a redesignation to attainment of the standard. The districts also developed and submitted a "clean data finding" and a maintenance plan to the U.S. EPA. The clean data finding demonstrates that the standard has been met during a given three-year period, and the maintenance plan demonstrates how the standard will continue to be met in future years.

Because operation of the proposed project can potentially generate additional air pollutant emissions within the region, this analysis estimates the net increase in operational air pollutants in comparison to the existing level of air pollutants from the project site. This analysis also evaluates construction-related impacts to air quality. YSAQMD has established the following standard for evaluating construction and operational impacts as shown below.

- 10 tons per year (tons/yr) of ROG,
- 10 tons $/ \mathrm{yr}$ of NOx,
- 80 pounds per day (lb/day) of $\mathrm{PM}_{10}$, and
- Violation of a state ambient air quality standard for carbon monoxide (CO)


## Discussion

a) In order to evaluate how a project would affect attainment of concentration-based ambient air quality standards, local air pollution control districts and air quality management districts frequently rely on mass-emission-based significance criteria. This is the case with YSAQMD's standard levels, as discussed above, as such are based on achieving concentration-based standards for these pollutants. For example, YSAQMD considers a project that would result in less than 10 tons/yr of ROG or NOx, and less than $80 \mathrm{lb} /$ day of $\mathrm{PM}_{10}$ to have a less-than-significant contribution to a violation of an ambient air quality standard. These mass-emission standards are tied to YSAQMD air quality attainment planning efforts of the ambient air quality standards. Thus, it is appropriate to use YSAQMD significance criteria to evaluate how emissions from the proposed project would affect attainment planning efforts.

The proposed project involves constructing improvements to the existing I-80/Richards Boulevard interchange. Proposed land uses would be similar to existing land uses on the project site and therefore would be consistent with the city General Plan land use designations. In addition, as shown in Tables AQ-2 and AQ-3, long-term operational emissions would not exceed applicable YSAQMD standard levels. As stated above, the YSAQMD emission standards are tied to attainment planning efforts, and projects resulting in emissions less than the standard levels would have a less than significant contribution to a violation of the NAAQS. Therefore, implementation of the proposed project would not conflict with or obstruct implementation of any air quality planning efforts. This impact would be less than significant.
b) On behalf of Caltrans District 3 and the City of Davis, ESA staff conducted an air quality analysis for the proposed project that included an emissions inventory estimation for the
construction and operation of the proposed project. The analysis was conducted in accordance with Caltrans guidance and requirements (Caltrans, 2019).

Construction and operational emissions of criteria air pollutants and precursors were modeled in accordance with Caltrans recommended methodologies using traffic volumes and truck percentages provided by the project's traffic engineers and construction schedule provided by the City. Caltrans CT-EMFAC2014 was utilized to conduct a precursor emissions burden analysis for NOx and reactive organic compounds (ROGs) (for ozone). In addition to its role in ozone formation, $\mathrm{NO}_{\mathrm{x}}$ forms $\mathrm{NO}_{2}$. Thus, modeling NOx emissions can serve as a useful analysis surrogate for $\mathrm{NO}_{2}$ emissions. For $\mathrm{PM}_{10}$, a comparative emissions analysis was conducted and relied on modeling exhaust emissions from CT-EMFAC and road dust emissions estimates. For $\mathrm{PM}_{2.5}$ direct vehicle emissions (exhaust, tire wear, and brake wear from on-road vehicles), follow the same requirements for $\mathrm{PM}_{10}$. Non-direct vehicle emissions of $\mathrm{PM}_{2.5}$ (road dust) are typically considered as well. $\mathrm{SO}_{2}$ and lead are not typically a concern for transportation sources and therefore were not analyzed.

## Construction

Site preparation and roadway construction would involve clearing, cut-and-fill activities, grading, removing or improving existing roadways, and paving roadway surfaces. During construction, short-term degradation of air quality is expected from the release of particulate emissions (airborne dust) generated from excavation, grading, hauling, and other activities related to construction. Emissions from construction equipment powered by gasoline and diesel engines are also anticipated and would include $\mathrm{CO}, \mathrm{NO}_{\mathrm{x}}$, ROGs, directly emitted $\mathrm{PM}_{10}$ and $\mathrm{PM}_{2.5}$, and toxic air contaminants (TACs) such as diesel exhaust particulate matter. Construction activities are expected to increase traffic congestion in the area, resulting in an increase in emissions from traffic delays. These emissions would be temporary and limited to the immediate area surrounding the construction site.

The construction period for the proposed project is expected to last for approximately 18 months. Construction emissions were estimated using the latest SMAQMD's Road Construction Emissions Model (RCEM), Version 8.1.0. Construction emissions were estimated for the proposed project using default equipment inventories provided in RCEM, project construction scheduling information provided by the City, and emissions factors from the EMFAC 2014 and OFFROAD models. Construction-related emissions for the proposed project are presented in Table AQ-1 below.

Based on the modeling conducted, short-term construction emissions would not exceed YSAQMD's applicable standard levels for ROGs and $\mathrm{PM}_{10}$. Although YSAQMD does not have a standard level for $\mathrm{PM}_{2.5}$, estimated emissions would be lower than estimated emissions of $\mathrm{PM}_{10}$, and are also included in Table AQ-1. However, $\mathrm{NO}_{\mathrm{x}}$ emissions generated by construction activities for the proposed project would exceed the YSAQMD standard level of 10 tons/yr. As a result, this impact would be potentially significant. Implementation of Mitigation Measure AQ-1 (see page 28) would ensure that $\mathrm{NO}_{\mathrm{x}}$
emissions generated from the construction of the proposed project would not exceed the YSAQMD standard levels and would result in a less-than-significant-impact.

TABLE AQ-1
Construction Emissions Inventory

| Construction Activity | ROG <br> (ton/yr) | $\mathbf{N O}_{\mathbf{x}}$ <br> (ton/yr) | $\mathbf{P M}_{10}$ <br> (Ib/day) | $\mathbf{P M}_{2.5}$ <br> (Ib/day) |
| :--- | :---: | :---: | :---: | :---: |
| Clearing/Grubbing | $>1$ | $>1$ | 21 | 5 |
| Grading/Excavation | 2 | 22 | 25 | 9 |
| Drainage/Utilities | $>1$ | 4 | 23 | 7 |
| Paving | $>1$ | $>1$ | $>1$ | $>1$ |
| Maximum daily or average daily | 2 | 27 | 25 | 9 |
| YSAQMD Standard Levels | $\mathbf{1 0}$ | $\mathbf{1 0}$ | $\mathbf{8 0}$ | NA |
| Exceed Standard Levels | No | Yes | No | NA |

NOTES:
Totals may not add up exactly due to rounding in the modeling calculations.
Standard levels established by the YSAQMD.
$\mathrm{lb} /$ day $=$ pounds per day; $\mathrm{NA}=\mathrm{No} ; \mathrm{NO}_{\mathrm{x}}=$ oxides of nitrogen; $\mathrm{PM}_{10}=$ particulate matter with aerodynamic diameter less than 10 microns; $\mathrm{PM}_{2.5}=$ particulate matter with aerodynamic diameter less than 2.5 microns; ROG $=$ reactive organic gases; YSAQMD = Yolo Solano Air Quality Management District; yr = year

SOURCE: ESA, 2019.

## Operation

The purpose of the proposed project is to reduce congestion, improve traffic operations, accommodate travel demand due to planned and approved developments, and improve safety for all modes of travel, including bicycles and pedestrians. An air quality analysis has been conducted to assess changes in air quality created by the operation of the project on the surrounding area. Potential air quality impacts from the operation of the project are primarily associated with the redistribution of vehicles on the new interchange along I-80 at Richards Boulevard, local street improvements, and the closing of the Olive Drive offramp. Impacts generated from the redistribution of traffic include incremental changes to VMT and average daily traffic (ADT). Changes in these traffic patterns along the roadway could potentially change the overall concentrations of pollutant levels from vehicle exhaust emissions throughout the project area.

Operation-related emissions have been assessed on a regional and project level. Operational emissions take into account long-term changes in emissions due to the project (excluding the construction phase). The operational emissions analysis compares forecasted emissions for existing/baseline and future analysis years 2022 (opening year) and 2042 (design year) with the proposed project. CT-EMFAC was used to calculate operational emissions. CT-EMFAC is a California-specific project-level analysis tool for modeling emissions of criteria pollutants, MSATs, and carbon dioxide from on-road vehicles. This model reflects CARB's current understanding of how vehicles travel and
how much they pollute. The results of the comparative emissions analysis are provided below in Table AQ-2 and Table AQ-3.

Table AQ-2
2022 Proposed Project Operational Emissions Inventory

| Scenario/Analysis Year | ROG <br> (ton/yr) | $\mathbf{N O}_{\mathbf{x}}$ <br> (ton/yr) | $\mathbf{P M}_{10}$ <br> (lb/day) | $\mathbf{P M}_{\mathbf{2 . 5}}$ <br> (lb/day) |
| :--- | :---: | :---: | :---: | :---: |
| Baseline (Existing Conditions) 2016 | 42 | 165 | 70 | 35 |
| 2022 with Project | 27 | 100 | 70 | 31 |
| Net Change in Emissions (With Project minus <br> Baseline) | $(15)$ | $(65)$ | 0 | $(3)$ |
| YSAMQD Standard Levels | $\mathbf{1 0}$ | $\mathbf{1 0}$ | $\mathbf{8 0}$ | NA |

NOTES:
Totals may not add up exactly due to rounding in the modeling calculations.
Standard levels established by the YSAQMD.
$\mathrm{lb} /$ day $=$ pounds per day; $\mathrm{NA}=\mathrm{No} ; \mathrm{NO}_{\mathrm{x}}=$ oxides of nitrogen; $\mathrm{PM}_{10}=$ particulate matter with aerodynamic diameter less than 10 microns; $\mathrm{PM}_{2.5}=$ particulate matter with aerodynamic diameter less than 2.5 microns; ROG = reactive organic gases; YSAQMD = Yolo Solano Air Quality Management District; yr = year
SOURCE: ESA, 2019.

Table AQ-3
2042 Proposed Project Operational Emissions Inventory

| Scenario/Analysis Year | ROG <br> (ton/yr) | $\mathbf{N O}_{\mathbf{x}}$ <br> (ton/yr) | $\mathbf{P M}_{10}$ <br> (Ib/day) | $\mathbf{P M}_{\mathbf{2 . 5}}$ <br> (Ib/day) |
| :--- | :---: | :---: | :---: | :---: |
| Baseline (Existing Conditions) 2016 | 42 | 165 | 70 | 35 |
| 2042 with Project | 18 | 58 | 82 | 34 |
| Net Change in Emissions (With Project minus <br> Baseline) | $(25)$ | $(107)$ | 12 | $(<1)$ |
| YSAMQD Standard Levels | $\mathbf{1 0}$ | $\mathbf{1 0}$ | $\mathbf{8 0}$ | NA |

## NOTES:

Totals may not add up exactly due to rounding in the modeling calculations.
Standard levels established by the YSAQMD.
$\mathrm{lb} /$ day $=$ pounds per day; $\mathrm{NA}=\mathrm{No} ; \mathrm{NO}_{\mathrm{x}}=$ oxides of nitrogen; $\mathrm{PM}_{10}=$ particulate matter with aerodynamic diameter less than 10 microns; $\mathrm{PM}_{2.5}=$ particulate matter with aerodynamic diameter less than 2.5 microns; ROG $=$ reactive organic gases; YSAQMD = Yolo Solano Air Quality Management District; yr = year

SOURCE: ESA, 2019.

Existing (2016) emissions in the project corridor were estimated using CT-EMFAC2014 emission factors, for comparison to the future analysis years 2022 and 2042. Based on the modeling conducted, the net increase in long-term operational emissions would not exceed YSAQMD's applicable standard levels. Although YSAQMD does not have a standard level for $\mathrm{PM}_{2.5}$, estimated emissions would be lower than estimated emissions of $\mathrm{PM}_{10}$ and would not contribute substantially to existing or projected air quality. Future with project emissions would be less than existing conditions for $\mathrm{ROG}, \mathrm{NO}_{2}$, and $\mathrm{PM}_{2.5}$. This decrease is due to the decrease in delays on the I-80 travel lanes and local roadway intersections, which generally result in lower emission rates. Thus, operational emissions
generated by the proposed project would not violate or contribute substantially to an existing or projected air quality violation, including the nonattainment status of Yolo County for ozone, $\mathrm{PM}_{10}$, and $\mathrm{PM}_{2.5}$. As a result, this impact would be less than significant.

## c) Construction

As previously discussed, the proposed project would not exceed the YSAQMD standard levels during construction with implementation of Mitigation Measure AQ-1 (see page 27) and would likely not cause or contribute to the exposure of sensitive receptors to ground-level concentrations in excess of health-protective levels.

## Toxic Air Contaminants

Intermittent construction activities associated with the proposed project would result in short-term emissions of diesel particulate matter, which the state has identified as a toxic air contaminant (TAC). During construction, the exhaust of off-road heavy-duty diesel equipment would emit diesel particulate matter during general construction activities, such as site grading, excavation, materials transport and handling, and paving.

Diesel particulate matter poses a carcinogenic health risk that is generally measured using an exposure period of 30 years for sensitive residential receptors, according to the California Environmental Protection Agency, Office of Environmental Health Hazard Assessment (OEHHA) Air Toxics Hot Spots Program Guidance Manual for Preparation of Health Risk Assessments (OEHHA Guidance), which was updated in 2015 with new exposure parameters including age sensitivity factors (OEHHA 2015). The closest sensitive receptors (multi-family residences) are located approximately 50 feet from the westbound I-80/Richards Boulevard off-ramp. However, as presented in Table AQ-1 above, diesel particulate matter emissions (strongly correlated with $\mathrm{PM}_{2.5}$ emissions) are less than significant. Although the localized analysis does not directly measure health risk impacts, it does provide data that can be used to evaluate the potential to cause health risk impacts. The very low level of $\mathrm{PM}_{2.5}$ emissions coupled with the short-term duration of construction activity resulted in an overall low level of diesel particulate matter concentrations in the project area. Furthermore, compliance with the CARB airborne toxic control measures (ATCM) anti-idling measure, which limits idling to no more than 5 minutes at any location for diesel-fueled commercial vehicles, would further minimize diesel particulate matter emissions in the project area. Sensitive receptors would be exposed to emissions below standard levels, and construction TAC impacts would be less than significant.

## Operation

## Carbon Monoxide Hotspot Analysis

The Caltrans CO Protocol has been recommended for use by several air pollution control districts in their CEQA analysis guidance documents and is used for the proposed project since the key criterion ( 8 -hour concentration) is similar: 9 ppm for the federal standard and 9.0 ppm for the state's standard. The CO Protocol was developed for project-level conformity (hot-spot) analysis and was approved for use by the U.S. EPA in 1997. It provides qualitative and quantitative screening procedures, as well as quantitative
(modeling) analysis methods to assess project-level CO impacts. The qualitative screening step is designed to avoid the use of detailed modeling for projects that clearly cannot cause a violation, or worsen an existing violation, of the CO standards.

The project is located in a CO attainment area. However, future traffic volumes would increase from existing conditions; therefore, a CO hot-spot analysis was conducted to demonstrate that the transportation activities associated with the project would not cause new air quality violations, worsen existing violations, or delay timely attainment of the NAAQS. The proposed project is not included in the exempt projects list from Table 2 of 40 CFR 93.126. Therefore, to determine the CO modeling requirements for new projects the proposed project must utilize the first flow chart provided in the Caltrans guidance document, Transportation Project-Level Carbon Monoxide Protocol (CO Protocol) (UCD, 1997).

Sections 3 and 4 of the CO Protocol describe the methodology for determining whether a CO hot-spot analysis is required. The Protocol provides two conformity requirement decision flowcharts that are designed to assist project sponsors in evaluating the requirements that apply to their project. The flowchart for the CO Protocol applies to new projects and was used for the proposed project. The flowchart can be found in Appendix C of the CO Protocol. Below is a step-by-step explanation of the applicable flowchart. Each level cited is followed by a response, which in turn determines the next applicable level of the flowchart for the project.

### 3.1.1: Is the project exempt from all emissions analysis?

Response: No, this project is not exempt from all emissions analysis. This proposed project type is not listed in Table 2 of the 40 CFR 93.126.

### 3.1.2: Is the project exempt from regional emissions analysis?

Response: Yes, this project is exempt from all regional emissions analysis. This proposed project type is listed in Table 3 of the 40 CFR 93.127.

### 3.1.9: Examine local impacts. Proceed to Section 4.

On the basis of the answers to the first flow chart, a second flow chart is used to determine the level of local CO impact analysis required for the project. The questions applicable to the project in the second flowchart and the answers to those questions are as follows:

## Level 1: Is the project in a CO nonattainment area?

Response: No, as shown previously stated, the Basin is classified as an attainment area for the federal CO standards.

Level 1: Was the area redesignated as "attainment" after the 1990 Clean Air Act?
Response: Yes, the Sacramento urbanized area was redesignated to attainment in 1998.

## Level 1: Has "continued attainment" been verified with the local Air District, if appropriate?

Response: Yes, "continued attainment" has been verified with the local Air District. (Proceed to Level 7)

## Level 7: Does the project worsen air quality?

Response: According to the CO Protocol, the following criteria should be used to determine whether a project is likely to worsen air quality for the area substantially affected by the project:

1. The project significantly increases the percentage of vehicles operating in cold start mode. Increasing the number of vehicles operating in cold start mode by as little as 2 percent should be considered potentially significant.
a. The proposed project is not expected to increase the percentage of vehicles operating in cold start mode. The traffic study developed for the proposed project found that the average annual daily traffic (AADT) for the no project and with project conditions in the future opening year (2022) will remain the same. Traffic volumes will increase from opening year to design year. However, no project and with project traffic volumes in the design year (2042) are the same. The proposed project is not expected to increase the number of vehicles traveling on the road; rather the proposed project is expected to relieve congestion, improve traffic flow, and provide safer travel through the I-80/Richards Boulevard Interchange area.
2. The project significantly increases traffic volumes. Increase in traffic volumes in excess of 5 percent should be considered potentially significant. Increasing the traffic volumes by less than 5 percent may still be potentially significant if there is also a reduction in average speeds.
a. The implementation of the proposed project would not increase traffic volumes within the proposed project area in comparison to the no project conditions. As stated previously, the AADT for the no project and with project conditions in the future opening year (2022) and design year (2042) are the same are the same.
3. The project worsens traffic flow. For uninterrupted roadway segments, a reduction in average speeds (within a range of 3 to 50 mph ) should be regarded as worsening traffic flow. For intersection segments, a reduction in average speed or an increase in average delay should be considered as worsening traffic flow.
a. According to the project's traffic analysis the traffic volumes for the with-project conditions are the same as the no project conditions except for reassigning traffic based on the new roadway configuration.

Compared to baseline (existing) conditions, the opening year volumes for the no project conditions show an increase of about 200 vehicles per hour during the peak hours for Richards Boulevard between I-80 and Olive Drive.

Under the no project conditions, the higher forecasted volumes at Richards Boulevard/Olive Drive would worsen operations from level of service (LOS) E to F during the AM peak hour for construction year conditions. The other study
intersections would continue to operate with the same LOS as under existing conditions. During the PM peak hour, increasing volume on the eastbound offramp would result in worse operations with LOS E degrading to LOS F at the I-80 Eastbound Ramps intersection. Similarly, the Research Park Drive intersection operations would worsen from LOS D to E, and the other study intersections would operate the same or better than under existing conditions.

Under the with-project conditions, additional capacity at the Richards Boulevard/ Olive Drive intersection would reduce vehicle delays compared to the proposed project. Operations would improve from LOS F to D during the AM peak hour and LOS E to D during the PM peak hour. The reconstructed and signalized I-80 Westbound Ramps intersection would operate with LOS C conditions during both peak hours. The addition of a second left-turn lane on the eastbound offramp would improve the I-80 Eastbound Ramps intersection from LOS F to C during the PM peak hour. All study intersections would have LOS D or better operations under the proposed project.

The results of the CO Protocol flowchart demonstrate that the proposed project does not require a quantitative hot-spot analysis to demonstrate conformity.

In addition, a PM Conformity Hot Spot Analysis Project Summary Form was drafted and submitted by email to Shengyi Gao of the Sacramento Area Council of Governments (SACOG) on June 25, 2018. Mr. Gao then distributed the PM Conformity Form to the members of the Interagency Group for review. The Interagency Group determined the proposed project is not a Project of Air Quality Concern (POAQC). Mr. Gao emailed the Interagency Group determination on September 10, 2018 (see Appendix A).

Thus, the project would not contribute considerably to the formation of CO hotspots and no further CO analysis is required. The project would result in a less-than-significant impact with respect to CO hotspots.

## Mobile Source Air Toxics Analysis (MSATs)

FHWA released updated guidance in October 2016 (FHWA, 2016) for determining when and how to address MSAT impacts in the NEPA process for transportation projects.
FHWA identified three levels of analysis:

- No analysis for exempt projects or projects with no potential for meaningful MSAT effects;
- Qualitative analysis for projects with low potential MSAT effects; and
- Quantitative analysis to differentiate alternatives for projects with higher potential MSAT effects.

Projects with high potential MSAT effects include those that:

- Create or significantly alter a major intermodal freight facility that has the potential to concentrate high levels of Diesel Particulate Matter in a single location; or
- Create new or add significant capacity to urban highways such as interstates, urban arterials, or urban collector-distributor routes with traffic volumes where the AADT
is projected to be in the range of 140,000 to 150,000 , or greater, by the design year; and
- Are proposed to be located in proximity to populated areas or, in rural areas, in proximity to concentrations of vulnerable populations (i.e., schools, nursing homes, hospitals).

Upon review of the traffic data from the project's traffic study and the FHWA guidance categories described above, the project could potentially have a high MSAT effect. The future design year (2042) AADT volumes remain the same between future No Build and Build conditions; however, AADT volumes increase from existing (2016) conditions to future design year (2042) by nearly 50,000 vehicles. Additionally, the AADT in the future design year conditions (2042) is estimated to be greater than 150,000 . Therefore, a quantitative analysis is appropriate for assessing air quality impacts from operation of the project.

The latest version of CT-EMFAC, CT-EMFAC2014 released in May 2017, was used to estimate emissions of benzene, 1,3-butadiene, formaldehyde, acrolein, naphthalene, DPM, and POM. Traffic activity data were estimated for each different period of a representative day in the baseline, opening (2022), and horizon (2042) years. Emissions were estimated for all MSATs using CT-EMFAC, based on EMFAC and speciation factors provided by CARB and U.S. EPA. The results of the comparative MSAT emissions analysis are provided below in Table AQ-4. The result of the comparative MSAT emission analysis show that future toxic emissions will decrease from baseline (existing) conditions. Thus, the project would result in a less-than-significant impact with respect to MSATs.

Table AQ-4
Summary of Comparative MSAT Emissions Analysis

| Scenario/ <br> Analysis Year | 1,3- <br> butadiene <br> (lbs/day) | Acetal- <br> dehyde <br> (lbs/day) | Acrolein <br> (lbs/day) | Benzene <br> (lbs/day) | Diesel <br> PM <br> (lbs/day) | Ethyl-- <br> benzene <br> (lbs/day) | Formal- <br> dehyde <br> (lbs/day) | Naph- <br> thalene <br> (lbs/day) | Polycyclic <br> Organic <br> Matter <br> (lbs/day) |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Baseline (Existing <br> Conditions) 2016 | 4 | 6 | 4 | 8 | 10 | 5 | 10 | 4 | 4 |
| 2022 with Project | 4 | 4 | 4 | 4 | 4 | 4 | 6 | 4 | 4 |
| 2042 with Project | 4 | 4 | 4 | 4 | 4 | 4 | 6 | 4 | 4 |

NOTES:
MSAT = mobile source air toxic; $\mathrm{Ib} / \mathrm{day}=$ pounds per day; PM = particulate matter
SOURCE: ESA, 2019.
d) Projects that are typically associated with odor complaints typically include agricultural uses, wastewater treatment plants, food processing plants, chemical plants, composting, refineries, landfills, dairies, and fiberglass molding. The proposed project does not include these elements that are typically associated with odor generation.

During construction, exhaust from equipment and activities associated with the application of pavement, finishes, or paints may produce discernible odors typical of most construction sites. Such odors would be temporary sources of nuisance to adjacent uses and would not affect a substantial number of people. Odors associated with construction would be temporary and intermittent in nature. Consequently, this impact would be less than significant.

## Mitigation Measures

## Mitigation Measure AQ-1: Construction Equipment Requirements.

All construction equipment shall be CARB Tier 4 Certified or better.

## References

California Department of Transportation (Caltrans), 2019. Air Quality Report for Richards Boulevard/Interstate-80 Interchange Improvements Project in the City of Davis, Yolo County (EA: 03-0H360; EFIS Project ID: 0315000148). Prepared by ESA for Caltrans District 3. June 2019.

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City of Davis, 2007. City of Davis General Plan. Available: https://www.cityofdavis.org/city-hall/ community-development-and-sustainability/planning-and-zoning/general-plan.

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Sacramento Area Council of Governments (SACOG), 2019. 2020 Metropolitan Transportation Plan/Sustainable Communities Strategy, Adopted November 18, 2019. Available: https://www.sacog.org/2020-metropolitan-transportation-plansustainable-communitiesstrategy.

University of California, Davis (UCD), 1997. Transportation Project-Level Carbon Monoxide Protocol. December 1997. Available: https://dot.ca.gov/-/media/dot-media/programs/ environmental-analysis/documents/env/co-protocol-searchable-a11y.pdf.

Yolo-Solano Air Quality Management District (YSAQMD), 2019. Triennial Assessment and Plan Update. May 2019. Available: https://www.ysaqmd.org/wp-content/uploads/2021/01/2015-17-Triennial-Plan-Final-Board-Approved.pdf.

## Biological Resources

| Sues and Supoorting Itormation Suuress) |  |  |  | No lmpa |
| :---: | :---: | :---: | :---: | :---: |
| Biolocical resources - Would the prije |  |  |  |  |
|  | $\square$ | ® | $\square$ | $\square$ |
|  | $\square$ | $\square$ | $\square$ | 区 |
| Heve a substanial adverse effect on state or <br>  diriect removal | $\square$ | $\square$ | $\square$ | ® |
| Interfere substantially with the movement of any native resident or migratory fish or wildlife species or with established native resident or migratory wildlife corridors, or impede the use of native wildlife nursery sites? | $\square$ | ® | $\square$ | $\square$ |
| any local policies or ordinances protecting biological resources, such as a tre preservation policy or ordinance? | $\square$ | ® | $\square$ | $\square$ |
| Conflict with the provisions of an adopted Habitat Conservation Plan, Natural Community Conserv Plan, or other approved local, regional, or state | $\square$ | ® | $\square$ | $\square$ |

## Study Methods

On May 4, 2018, an Environmental Science Associates biologist conducted a general biological survey within the Biological Study Area (BSA) for the proposed project. The BSA includes the Project Impact Area (PIA) and a surrounding 250 -foot area (see Figure 8). Prior to field surveys, satellite imagery and aerial photographs were analyzed to locate potential sensitive biological resources. Surveys were conducted by walking the entire BSA where entry was permitted and evaluating the potential for regionally occurring sensitive habitats (including jurisdictional waters of the U.S. and state) and special-status species to occur within the BSA. Plant communities and habitats were recorded onto a rectified aerial photograph, and all plant species encountered were identified and recorded. There were a number of locations within the BSA that were not accessible to biologists during the field surveys, including most private properties throughout the BSA. Biologists used a combination of aerial interpretation and binoculars to survey habitats within these locations.

Prior to field surveys, wetland spatial data was obtained from the portions of a previously U.S. Army Corps of Engineers (USACE)-verified wetland delineation for the USACE Six County Aquatic Resource Inventory (SCARI) (USACE, 2011). The boundaries of these features were then examined in the field to determine if they were present in the BSA.


Queries of the United States Fish and Wildlife Service (USFWS) Information, Planning, and Consultation System (IPaC); National Marine Fisheries Service (NMFS); California Natural Diversity Database (CNDDB); and California Native Plant Society (CNPS) databases were conducted to create a list of special-status species with the potential to occur in the project area and surrounding area. The results of the database inquiries are included in Appendix B to this initial study.

For the purposes of this initial study, special-status species are generally defined as follows:

- Plant and wildlife species listed or proposed for listing as threatened or endangered under the federal Endangered Species Act (FESA).
- Plant and wildlife species that are candidates for possible future listing as threatened or endangered under the FESA (80 FR 80584-80614, December 24, 2015).
- Plant and wildlife species that meet the definition of rare or endangered species under the California Environmental Quality Act (CEQA), or are considered sensitive or unique by the scientific community, or occur at the limits of its natural range (CEQA Guidelines, Section 15380).
- Plants considered by the CNPS and the California Department of Fish and Wildlife (CDFW) to be "rare, threatened, or endangered" in California (California Rare Plant Rank 1A, 1B and 2 [CNPS, 2022]).
- Plants listed or proposed for listing by the State of California as threatened or endangered under the California Endangered Species Act (CESA) (14 CCR 670.5).
- Plants listed under the California Native Plant Protection Act (California Fish and Game Code [CFGC] 1900 et seq.).
- Plants considered sensitive by other federal agencies (i.e., U.S. Forest Service, Bureau of Land Management) or state and local agencies or jurisdictions.
- Wildlife species that are listed or proposed for listing under CESA (CFGC 1992 Sections 2050 et seq.; 14 CCR Sections 670.1 et seq.).
- Wildlife species that are designated as Species of Special Concern (SSC) by CDFW.
- Wildlife species that are designated as Fully Protected by CDFW (CFGC, Section 3511, 4700, 5050, and 5515).
- Species addressed in the Yolo Habitat Conservation Plan/Natural Community Conservation Plan (Yolo HCP/NCCP) (Yolo Habitat Conservancy, 2018).


## Environmental Setting

The BSA is located within the southern portion of the City of Davis. Land uses within and adjacent to the BSA consist of a mix of residential, commercial, industrial, agriculture, and open space/public parks.

The BSA is situated on the broad, flat alluvial plain of the Sacramento River, and terrain is generally flat. Elevations of the BSA range from approximately 35 to 50 feet above mean sea level. Climate is typically hot and sub-humid. Data from the Western Regional Climate Center for the Davis 2 WSW Exp Farm weather station indicates that average annual precipitation is
17.55 inches. The average maximum annual temperature is 74.7 degrees $(\mathrm{F})$ and average minimum annual temperature is 46.0 degrees ( F ).

The project site is located in the City of Davis within the Sacramento Valley floristic province of the Great Central Valley. Historically, the region supported extensive marshes, riparian woodland intermixed with oak woodland, vernal pool complexes, and native grasslands. Intensive agricultural and urban development has resulted in substantial changes and conversions of these habitats. The remaining native vegetative communities exist now as isolated remnant patches within urban and agricultural landscapes.

## Habitat

Developed habitat comprises the majority of the BSA and consists of paved or otherwise developed areas where native vegetation does not grow. Ornamental vegetation associated with the BSA consists of trees and understory grassland along road shoulders and within undeveloped lots and open areas. In addition, some areas of agricultural land were noted within the BSA. Habitat types within the BSA are depicted on Figure 8. Acreages for habitat types within the BSA and project site are provided in Table BIO-1.

Table BIO-1
Habitat Types Within the BSA and Project Site

| Habitat Type | BSA $^{1}$ (acres) | Project Site (acres) |
| :--- | :---: | :---: |
| Developed | 85.21 | 18.48 |
| Ornamental | 34.97 | 11.75 |
| Agricultural | 4.74 | 0.00 |
| NOTES: |  |  |
| 1 Habitat acreages in the BSA include acreages from the project site. |  |  |
| SOURCE: Caltrans, 2019. |  |  |

## Special-Status Plants

Based on the review of existing information, including a search of the CNDDB, CNPS, and USFWS species lists, and species distribution and habitat requirements data, 21 special-status plant species were identified as having potential to occur in the vicinity of the project. Specialstatus plant species and rationale for their presence or absence and likelihood of occurrence within the BSA is provided in Table BIO-2. None of the species have the potential to occur within the project area or be affected by project construction. There is no critical habitat for any special-status plant species in the BSA.

## Special-Status Wildlife

Based on the review of existing information, including a search of the CNDDB, USFWS, and NMFS species lists, and species distribution and habitat requirements data, 42 special-status wildlife species were identified during the pre-field review as occurring or having the potential to occur within the BSA. The listing status, preferred habitat, and potential for occurrence in the BSA for each of these species are provided in Table BIO-3.

Table BIO-2
Special-status Plant Species with the Potential to Occur in the Biological Study Area

| Common and <br> Scientific Name | Legal Status <br> Federal/State/ <br> CRPR | Distribution |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |

Table BIO-2
Special-status Plant Species with the Potential to Occur in the Biological Study Area

| Common and Scientific Name | Legal Status ${ }^{1}$ Federal/State/ CRPR | Distribution | Habitat Association | Identification Period | Habitat <br> Present/ <br> Absent | Species <br> Present/ <br> Absent | Survey Results/Rationale |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| San Joaquin spearscale Extriplex joaquinana | --/--/1B. 2 | Alameda, Contra Costa, Colusa, Fresno, Glenn, Merced, Monterey, Napa, San Benito, Santa Clara, San Joaquin, San Luis Obispo, Solano, Tulare, and Yolo counties. | Alkaline soil in chenopod scrub, playas, meadows and seeps, and grasslands. 1-2750 feet. | April - October | Habitat Absent | Absent | No suitable habitat within the BSA. There are three CNDDB occurrences within five miles of the BSA. |
| Adobe-lily <br> Fritillaria pluriflora | ----/1B. 2 | Butte, Colusa, Glenn, Lake, Napa, Solano, Tehama, and Yolo counties. | Adobe soil in chaparral, cismontane woodland, and grasslands. 200-2300 feet. | February - <br> April | Habitat Absent | Absent | No suitable habitat within the BSA. There are no CNDDB occurrences within five miles of the BSA. |
| Woolly rosemallow Hibiscus lasiocarpos var. occidentalis | ----/1B. 2 | Butte, Contra Costa, Colusa, Glenn, Sacramento, San Joaquin, Solano, Sutter, and Yolo counties. | Marshes and swamps (freshwater). Moist, freshwater-soaked river banks \& low peat islands in sloughs; can also occur on riprap and levees). $0-390$ feet. | June September | Habitat Present | Absent | No suitable habitat within the BSA. There are no CNDDB occurrences within five miles of the BSA. |
| Heckard's peppergrass Lepidium latipes var. heckardii | --/--/1B. 2 | Glenn, Merced, Sacramento, Solano, and Yolo counties. | Alkaline flats in valley and foothill grasslands. 7 - 650 feet. | March - May | Habitat Absent | Absent | No suitable habitat within the BSA. There is one CNDDB occurrence within five miles of the BSA. |
| Mason's lilaeopsis Lilaeopsis masonii | --/SR/1B. 1 | Alameda, Contra Costa, Marin, Napa, Sacramento, San Joaquin, Solano, and Yolo counties. | Marshes and swamps (freshwater or brackish) and riparian scrub. 0-30 feet. | April November | Habitat Present | Absent | No suitable habitat within the BSA. There are no CNDDB occurrences within five miles of the BSA. |
| Baker's navarretia Navarretia leucocephala subsp. bakeri | ----/1B. 1 | Colusa, Glenn, Lake, Lassen, Mendocino, Marin, Napa, Solano, Sonoma, Sutter, Tehama, and Yolo counties. | Mesic sites in cismontane woodland, lower montane coniferous forest, meadows and seeps, vernal pools, and grasslands. $15-5700$ feet. | April - July | Habitat Present | Absent | No suitable habitat within the BSA. There are no CNDDB occurrences within five miles of the BSA. |
| Colusa grass <br> Neostapfia colusana | FT/SE/1B. 1 | Colusa, Glenn, Merced, Solano, Stanislaus, and Yolo counties | Large, adobe vernal pools. 15-600 feet. | May - August | Habitat Absent | Absent | No suitable habitat within the BSA. There are three CNDDB occurrences within five miles of the BSA. |

Table BIO-2
Special-status Plant Species with the Potential to Occur in the Biological Study Area

| Common and <br> Scientific Name | Legal Status ${ }^{1}$ <br> Federal/State/ <br> CRPR | Distribution |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |

Table BIO-2
Special-status Plant Species with the Potential to Occur in the Biological Study Area

NOTES:
1 Status explanations:

- $=$ no listing.
Federal
FE $=$ listed as endangered under the federal Endangered Species Act.
FT $=$ listed as threatened under the federal Endangered Species Act.
State
SE $=$ listed as endangered under the California Endangered Species Act.
SR $=$ listed as rare under the California Endangered Species Act.
ST $=$ listed as threatened under the California Endangered Species Act.


## California Rare Plant Ranks

$1 \mathrm{~B}=$ Rank 1B species: rare, threatened, or endangered in California and elsewhere.
2B = Rank 2B species: rare, threatened, or endangered in California but more common elsewhere.
$0.1=$ Seriously threatened in California (over $80 \%$ of occurrences threatened/high degree and immediacy of threat)
$0.2=$ Moderately threatened in California ( $20 \%-80 \%$ occurrences threatened/moderate degree and immediacy of threat)
$0.3=$ Not very threatened in California (less than 20\% of occurrences threatened/low degree and immediacy of threat or no current threats known

Table BIO-3
Special-status Wildlife with the Potential to Occur in the Biological Study Area

| Common and Scientific Name | Legal Status ${ }^{1}$ |  | Distribution | Habitat Association | Identification Period | Habitat Present/ Absent | Species Present/ Absent | Rationale |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Federal | State |  |  |  |  |  |  |
| Invertebrates |  |  |  |  |  |  |  |  |
| Conservancy fairy shrimp Branchinecta conservatio | FE | -- | Northern two-thirds of the Central Valley. | Large, turbid vernal pools. | November-April for active shrimp, April-November for cysts | Habitat Absent | Absent | Habitat not present within the BSA. There are no CNDDB occurrences within five miles of the BSA. |
| Vernal pool fairy shrimp <br> Branchinecta lynchi | FT | -- | Central Valley, Central and South Coast Ranges from Tehama County to Santa Barbara County; isolated populations also in Riverside County and southern Oregon | Vernal pools and seasonal wetlands; also found in sandstone rock outcrop pools. | November-April for active shrimp, April-November for cysts | Habitat Absent | Absent | Habitat not present within the BSA. There are two CNDDB occurrences within five miles of the BSA. |
| Midvalley fairy shrimp Branchinecta mesovallensis | -- | -- | Central Valley. | Vernal pools in the Central Valley. | November-April for active shrimp, April-November for cysts | Habitat Absent | Absent | Habitat not present within the BSA. There are no CNDDB occurrences within five miles of the BSA. |
| Monarch - California overwintering population Danaus plexippus pop. 1 | FC | -- | Overwintering sites occur along the Pacific coast from Mendocino County, CA to Baja California, Mexico, typically within 1.5 miles of the Pacific Ocean or San Francisco Bay. Small aggregations inland have been reported in Inyo and Kern counties, CA. | Overwintering sites include dappled sunlight, high humidity, access to fresh water, and an absence of freezing temperatures or high winds. Tree species most commonly used for roosting are blue gum eucalyptus (Eucalyptus globulus), Monterey pine (Pinus radiata), and Monterey cypress (Cupressus macrocarpa). Milkweed (Asclepias spp.) is it obligate larval host plant during the breeding season. | Year-round for adults; spring and summer for larva and pupa | Habitat Absent | Absent | Habitat not present within the BSA. There are no CNDDB occurrences within five miles of the BSA. |

Table BIO-3
Special-status Wildlife with the Potential to Occur in the Biological Study Area

| Common and Scientific Name | Legal Status ${ }^{1}$ |  | Distribution | Habitat Association | Identification Period | Habitat Present/ Absent | Species Present/ Absent | Rationale |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Federal | State |  |  |  |  |  |  |
| Valley elderberry longhorn beetle Desmocerus californicus dimorphus ${ }^{2}$ | FT | -- | Central Valley and surrounding foothills below 1,500 feet elevations | Dependent on elderberry (Sambucus nigra) shrubs as a host plant; potential habitat is shrubs with stems one inch in diameter within Central Valley. | Year-round for host plant and exit holes | Habitat Present | Assumed Present | 17 elderberry shrubs and shrub clusters are known to occur within the BSA, with 13 occurring in the PIA. There is one CNDDB occurrence within five miles of the BSA. However, elderberry shrubs will not be impacted by the project. No ground disturbing activities are proposed within 30 feet of elderberry shrubs. |
| Vernal pool tadpole shrimp <br> Lepidurus packardi | FE | -- | Central Valley from Shasta County south to Merced County | Vernal pools, vernal lakes, and other seasonal wetlands. | November-April for active shrimp, April-November for cysts | Habitat Absent | Absent | Habitat not present within the BSA. There are three CNDDB occurrences within five miles of the BSA. |
| California linderiella Linderiella occidentalis | -- | -- | Sacramento Valley | Seasonal pools in unplowed grasslands with old alluvial soils underlain by hardpan or in sandstone depressions. Water in the pools has very low alkalinity, conductivity, and total dissolved solids (TDS). | November-April for active shrimp, April-November for cysts | Habitat Absent | Absent | Habitat not present within the BSA. There are three CNDDB occurrences within five miles of the BSA. |
| Amphibians |  |  |  |  |  |  |  |  |
| California tiger salamander <br> Ambystoma californiense pop. $1^{2}$ | FT | ST | Central Valley, including Sierra Nevada foothills up to 1,500 feet. The Cosumnes River marks the northern boundary of the species' range, with the exception of an isolated in the Dunnigan Hills in northern Yolo County. | Annual grasslands and valleyfoothill woodlands; breeds in seasonal wetlands such as vernal pools and swales. Burrows in underground refugia such as small mammal burrows. | January-May (aquatic) | Habitat Absent | Absent | Habitat is not present within the BSA. There is one CNDDB occurrence within five miles of the BSA. |
| California redlegged frog Rana draytonii | FT | ST | Along the coast and coastal mountain ranges of California from Marin County to San Diego County and in the Sierra Nevada from Tehama County to Fresno County. | Permanent and semipermanent aquatic habitats, such as creeks and ponds with emergent and submergent vegetation; may aestivate in upland burrow during dry periods. | Year-round | Habitat Absent | Absent | Habitat is not present within the BSA. Not within the known range for the species. There are no CNDDB occurrences within five miles of the BSA. |

Table BIO-3
Special-status Wildlife with the Potential to Occur in the Biological Study Area

| Common and Scientific Name | Legal Status ${ }^{1}$ |  | Distribution | Habitat Association | Identification Period | Habitat Present/ Absent | Species Present/ Absent | Rationale |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Federal | State |  |  |  |  |  |  |
| Western spadefoot Spea hammondii | -- | SSC | Historically occurred in the Central Valley and bordering foothills across southern California from Shasta County south into northwestern Baja California, including the Coast Ranges south of Monterey, from sea level to 4,500 feet. Today, virtually extirpated from the Sacramento Valley. | Occurs in grasslands, oak woodlands, coastal sage scrub, and chaparral vegetation in washes, floodplains, alluvial fans, playas, and alkali flats. Ephemeral pools lasting approximately 11.5 weeks are essential for breeding and egg-laying. | Eggs and larvae in ephemeral water bodies in spring and early summer, dependent on rain year; adults after rain events in late winter or spring, typically at night as species is nocturnal. | Habitat Absent | Absent | No suitable habitat is present within the BSA. There are no CNDDB occurrence within five miles of the BSA. |
| Reptiles |  |  |  |  |  |  |  |  |
| Western pond turtle Actineymys marmorata ${ }^{2}$ | -- | SSC | Populations extend throughout the coast and Central Valley of California. | Ponds, marshes, rivers, streams and irrigation ditches with aquatic vegetation below 6,000 feet in elevation. | Year-round | Habitat Absent | Absent | No suitable habitat is present within the BSA. There is one CNDDB occurrence within five miles of the BSA. |
| Giant garter snake Thamnophis gigas ${ }^{2}$ | FT | ST | Central Valley from Fresno County north to the Gridley/ Sutter Buttes area; has been extirpated from areas south of Fresno. | Sloughs, canals, and other small waterways where there is a prey base of small fish and amphibians; requires grassy banks and emergent vegetation for basking and areas of high ground protected from flooding during winter. Utilizes upland habitats within 200 feet from aquatic habitats. | April-October | Habitat Absent | Absent | No suitable habitat is present within the BSA. There are six CNDDB occurrences within five miles of the BSA. |

Table BIO-3
Special-status Wildlife with the Potential to Occur in the Biological Study Area

| Common and Scientific Name | Legal Status ${ }^{1}$ |  | Distribution | Habitat Association | Identification Period | Habitat Present/ Absent | Species Present/ Absent | Rationale |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Federal | State |  |  |  |  |  |  |
| Birds |  |  |  |  |  |  |  |  |
| Tricolored blackbird Agelaius tricolor ${ }^{2}$ | -- | $\begin{aligned} & \text { SCT, } \\ & \text { SSC } \end{aligned}$ | Largely endemic to California; permanent residents in the Central Valley from Butte County to Kern County; at scattered coastal locations from Marin County south to San Diego County; breeds at scattered locations in Lake, Sonoma, and Solano counties; rare nester in Siskiyou, Modoc, and Lassen counties. Sacramento-San Joaquin Valleys and low foothills of coast ranges and Sierra Nevada. | Nests in dense colonies in emergent marsh vegetation, such as tules and cattails, or upland sites with blackberries, nettles, thistles, and grain fields; nesting habitat must be large enough to support 50 pairs; probably requires water at or near the nesting colony; requires large foraging areas, including marshes, pastures, agricultural wetlands, dairies, and feedlots, where insect prey is abundant. | March-August | Habitat Absent | Absent | No suitable habitat is present within the BSA. There are three CNDDB occurrences within five miles of the BSA. |
| Grasshopper sparrow Ammodramus savannarum | -- | SSC | An uncommon and local, summer resident and breeder in foothills and lowlands west of the Cascade-Sierra Nevada crest from Trinity County south to San Diego County. | Dense grasslands on rolling hills, lowland plains, and in valleys and on hillsides on lower mountain slopes. Favors native grasslands with a mix of grasses, forbs and scattered shrubs. Loosely colonial when nesting. | March-August | Habitat Absent | Absent | No suitable habitat is present within the BSA. There are no CNDDB occurrences within five miles of the BSA. |
| Great egret Ardea alba (rookery sites) | -- | -- | The great egret is a common yearlong resident throughout California, except for high mountains and deserts. | Colonial nester in large trees. Rookery sites located near marshes, tide-flats, irrigated pastures, and margins of rivers and lakes. | Year-round | Habitat Absent | Absent | No suitable habitat is present within the BSA. There are no CNDDB occurrences within five miles of the BSA. |
| Great blue heron Ardea Herodias (rookery sites) | -- | -- | Fairly common throughout most of California. | Colonial nester in tall trees, cliff sides, and sequestered spots on marshes. Rookery sites in close proximity to foraging areas: marshes, lake margins, tide-flats, rivers and streams, wet meadows. | Year-round | Habitat Absent | Absent | No suitable rookery habitat is present within the BSA. <br> There are no CNDDB occurrences within five miles of the BSA. |

Table BIO-3
Special-status Wildlife with the Potential to Occur in the Biological Study Area

| Common and Scientific Name | Legal Status ${ }^{1}$ |  | Distribution | Habitat Association | Identification Period | Habitat Present/ Absent | Species Present/ Absent | Rationale |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Federal | State |  |  |  |  |  |  |
| Burrowing owl Athene cunicularia ${ }^{2}$ | -- | SSC | Lowlands throughout California, including the Central Valley, northeastern plateau, southeastern deserts, and coastal areas; rare along south coast. Central and southern coastal habitats, and Central Valley. | Open annual grasslands or perennial grasslands, deserts, and scrublands characterized by low-growing vegetation. Dependent upon burrowing mammals (especially California ground squirrel [Otospermophilus beecheyi]) for burrows. | Year-round | Habitat Present | Assumed Present | The annual grassland habitat within the PIA and surrounding BSA provides suitable nesting and foraging habitat for this species. There are 24 CNDDB occurrences within five miles of the BSA. |
| Swainson's hawk <br> Buteo swainsoni ${ }^{2}$ | -- | ST | Lower Sacramento and San Joaquin Valleys, the Klamath Basin, and Butte Valley; the state's highest nesting densities occur near Davis and Woodland, Yolo County. | Nests in oaks or cottonwoods in or near riparian habitats; requires adjacent suitable foraging areas such as grasslands, or alfalfa or grain fields supporting rodent populations. | March - <br> September | Habitat Present | Assumed Present | Suitable nest trees are present within the BSA and the PIA. No suitable foraging habitat within the BSA. Annual grasslands in the BSA are very disturbed, small in area, and fragmented. There are 143 CNDDB occurrences within five miles of the BSA, including several within one mile of the BSA. |
| Mountain plover Charadrius montanus | -- | SSC | Found in the Central Valley from Sutter County southward. Found in Imperial Valley, Los Angeles County, San Bernardino County, and along the central Colorado River valley. | Short grasslands, freshly plowed fields, newly sprouting grain fields, and sod farms. Short vegetation, bare ground, and flat topography. Prefers grazed areas and areas with burrowing rodents. | September March | Habitat Absent | Absent | No suitable habitat for this species within the BSA. There are no CNDDB occurrences within five miles of the BSA. |
| Western snowy plover Charadrius nivosus | FT | SSC | Nests on sandy marine and estuarine shores on coastal California. Inland nesting areas occur at the Salton Sea, Mono Lake, northeastern California, the Central Valley, and southeastern deserts. | Sandy beaches, salt pond levees, and shores of large alkali lakes. Needs sandy, gravelly, or friable soils for nesting. | Year-round | Habitat Absent | Absent | No suitable habitat for this species within the BSA. There is one CNDDB occurrence within five miles of the BSA. |

Table BIO-3
Special-status Wildlife with the Potential to Occur in the Biological Study Area

| Common and Scientific Name | Legal Status ${ }^{1}$ |  | Distribution | Habitat Association | Identification Period | Habitat Present/ Absent | Species Present/ Absent | Rationale |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Federal | State |  |  |  |  |  |  |
| Northern harrier Circus cyaneus | -- | SSC | Occurs throughout California as high as 10,000 feet. Breeds from sea level to 5,700 feet in the Central Valley and Sierra Nevada. | Coastal salt and freshwater marshes. Nests on ground in shrubby vegetation, usually at marsh edge; nest built of a large mound of stick in wet areas. | Year-round | Habitat Absent | Absent | No suitable habitat for this species within the BSA. There is one CNDDB occurrence within five miles of the BSA. |
| Western yellowbilled cuckoo Coccyzus americanus occidentalis ${ }^{2}$ | FT | SE | More common locations include Sacramento River from Red Bluff to Colusa and the South Fork Kern River from Isabella Reservoir to Canebrake Ecological Reserve. | This species is a riparian obligate, nesting in low to moderate elevation riparian woodlands with native broadleaf trees and shrubs that are 20 hectares (50 acres) or more in extent. | May - September | Habitat Absent | Absent | No suitable habitat for this species within the BSA. There is one CNDDB occurrence within five miles of the BSA. |
| Snowy egret Egretta thula (rookery sites) | -- | -- | In northern California, common March to November in coastal lowlands. Locally common in the Central Valley all year. | Colonial nester, with nest sites situated in protected beds of dense tule. Rookery sites situated close to foraging areas: marshes, tidal-flats, streams, wet meadows, and borders of lakes. | Year-round | Habitat Absent | Absent | No suitable rookery habitat for this species within the BSA. There are no CNDDB occurrences of rookeries within five miles of the BSA. |
| White-tailed kite Elanus leucurus ${ }^{2}$ | -- | FP | Lowland areas west of Sierra Nevada from head of Sacramento Valley south, including coastal valleys and foothills to western San Diego County at the Mexico border. Central Valley and low foothills of Sierra Nevadas. | Rolling foothills and valley margins with scattered oaks and river bottomlands or marshes next to deciduous woodland. Open grasslands, meadows, or marshes for foraging close to isolated, dense-topped trees for nesting and perching. | Year-round | Habitat Present | Assumed Present | Potential nesting and foraging habitat present within the BSA. There are six CNDDB occurrences within five miles of the BSA. |
| Merlin Falco columbarius | -- | WL | Common to uncommon, yearlong resident in coastal and valley lowlands; rarely found away from agricultural areas. Inhabits herbaceous and open stages of most habitats mostly in cismontane California. | Seacoast, tidal estuaries, open woodlands, savannahs, edges of grasslands \& deserts, farms \& ranches. Clumps of trees or windbreaks are required for roosting in open country. | Year-round | Habitat Absent | Absent | No suitable habitat for this species within the BSA. There are no CNDDB occurrences within five miles of the BSA. |

Table BIO-3
Special-status Wildlife with the Potential to Occur in the Biological Study Area

| Common and Scientific Name | Legal Status ${ }^{1}$ |  | Distribution | Habitat Association | Identification Period | Habitat Present/ Absent | Species Present/ Absent | Rationale |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Federal | State |  |  |  |  |  |  |
| California black rail Laterallus jamaicensis coturniculus | -- | ST, FP | Yearlong residence of saline, brackish, and freshwater wetlands in the San Francisco Bay area, Sacramento-San Joaquin Delta, coastal southern California, the Salton Sea, and lower Colorado River. | Inhabits freshwater marshes, wet meadows, and shallow margins of saltwater marshes bordering larger bays. Needs water depths of about one inch that do not fluctuate during the year and dense vegetation for nesting habitat. | Year-round | Habitat Absent | Absent | No suitable habitat for this species within the BSA. There are no CNDDB occurrences within five miles of the BSA. |
| Song sparrow <br> ("Modesto" population) Melospiza melodia | -- | SSC | A common resident of most of California, but avoids higher mountains and occurs only locally in southern deserts. | Emergent freshwater marshes dominated by tule (Scirpus spp., Schoenoplectus spp.) and cattail (Typha spp.) as well as riparian willow (Salix spp.) thickets. Also nest in riparian forests of valley oak (Quercus lobata) with a sufficient understory of blackberry (Rubus spp.), along vegetated irrigation canals and levees, and in recently planted valley oak restoration sites. | Year-round | Habitat Absent | Absent | No suitable habitat for this species within the BSA. There are no CNDDB occurrences within five miles of the BSA. |
| Black-crowned night heron <br> Nycticorax (rookery sites) | -- | -- | The black-crowned nightheron is a fairly common, yearlong resident in lowlands and foothills throughout most of California. | Forages in marshes swamps and wooded streams; nests in thickets, stands of trees or reedbeds. | Year-round | Habitat Absent | Absent | No suitable rookery habitat for this species within the BSA. There are no CNDDB occurrences of rookeries within five miles of the BSA. |
| White-faced ibis Plegadis chihi | -- | WL | Uncommon summer resident in southern California and Central Valley. | Shallow freshwater marsh. Uses dense tule thickets for nesting, interspersed with areas of shallow water for foraging. | May - September | Habitat Absent | Absent | No suitable habitat for this species within the BSA. There are no CNDDB occurrences within five miles of the BSA. |
| Purple martin Progne subis | -- | SSC | Nests in Sacramento County; uncommon or absent elsewhere in the Central Valley; breeds in coastal areas from Del Norte County south to Santa Barbara County; rare in southern California. | Abandoned woodpecker holes in valley oak and cottonwood (Populus spp.) forests for nesting; also nests in vertical drainage holes under elevated freeways and highway bridges; open areas required for feeding. | Year-round | Habitat Present | Assumed Present | Potential nesting and foraging habitat present within the BSA. There are no CNDDB occurrences within five miles of the BSA. |

Table BIO-3
Special-status Wildlife with the Potential to Occur in the Biological Study Area

| Common and Scientific Name | Legal Status ${ }^{1}$ |  | Distribution | Habitat Association | Identification Period | Habitat Present/ Absent | Species Present/ Absent | Rationale |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Federal | State |  |  |  |  |  |  |
| Bank swallow Riparia riparia ${ }^{2}$ | -- | ST | Nests primarily in riparian and other lowland habitats west of the desert. | Colonial nester. Requires vertical banks/cliffs with finetextured/sandy soils near streams, rivers, lakes, and oceans to dig nesting holes. | Spring - Fall | Habitat Absent | Absent | No suitable habitat is present within the BSA. There is one CNDDB occurrence within five miles of the BSA. |
| Least Bell's vireo Vireo bellii pusillus ${ }^{2}$ | FE | SE | Summer resident throughout Sacramento and San Joaquin valleys. | Summer resident of Southern California in low riparian in vicinity of water or in dry river bottoms; below 2000 ft . Nests placed along margins of bushes or on twigs projecting into pathways, usually willow, Baccharis sp., and mesquite. | March - August | Habitat Absent | Absent | No suitable nesting habitat for this species within the BSA. There are no CNDDB occurrences within five miles of the BSA. |
| Yellow-headed blackbird Xanthocephalus | -- | SSC | Throughout the Central Valley, and along the eastern side of the Sierra Nevada Mountains. Yearlong distribution follows a limited area along the Sacramento River, though summer range is larger, and incorporates much of the Central Valley. | Nests in freshwater emergent wetlands with dense vegetation and deep water. Often along borders of lakes or ponds. Nests only where large insects such as Odonata are abundant, nesting timed with maximum emergence of aquatic insects. | Year-round | Habitat Absent | Absent | No suitable nesting or foraging habitat for this species within the BSA. There are no CNDDB occurrences within five miles of the BSA. |
| Mammals |  |  |  |  |  |  |  |  |
| Pallid bat <br> Antrozous pallidus | -- | SSC | Throughout California except for the high Sierra Nevada. | Deserts, grasslands, shrublands, woodlands, and forests. Most common in open, dry habitats with rocky areas for roosting. Roosts must protect bats from high temperatures. Very sensitive to disturbance of roosting sites. | Year-round | Habitat Absent | Absent | No suitable habitat within the BSA. There is one CNDDB occurrence within five miles of the BSA. |
| American badger <br> Taxidea taxus | -- | SSC | Central Valley and surrounding foothills. | Grasslands with friable soils; near California ground squirrel populations. | Year-round | Habitat Absent | Absent | No suitable habitat within the BSA. There are two CNDDB occurrences within five miles of the BSA. |

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Special-status Wildlife with the Potential to Occur in the Biological Study Area

| Common and Scientific Name | Legal Status ${ }^{1}$ |  | Distribution | Habitat Association | Identification Period | Habitat Present/ Absent | Species Present/ Absent | Rationale |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Federal | State |  |  |  |  |  |  |
| Fish |  |  |  |  |  |  |  |  |
| Sacramento perch <br> Archoplites interruptus | -- | SSC | Historically found in the sloughs, slow-moving rivers, and lakes of the Central Valley. | Prefers warm water. Aquatic vegetation is essential for young. Tolerates wide range of physio-chemical water conditions. | Year-round | Habitat Absent | Absent | No suitable habitat within the BSA. There are no CNDDB occurrences within five miles of the BSA. |
| Delta smelt Hypomesus transpacificus | FT | SE | Sacramento-San Joaquin Delta and the lower reaches of the two rivers. Seasonally in Suisun Bay, Carquinez Strait and San Pablo Bay. | Found in Delta estuaries with dense aquatic vegetation and low occurrence of predators. Estuarine or brackish waters to 14 parts per thousand (ppt); spawn in shallow brackish water upstream of the mixing zone (zone of saltwaterfreshwater interface) where salinity is around 2 ppt. | Year-round | Habitat Absent | Absent | No suitable habitat within the BSA. There are no CNDDB occurrences within five miles of the BSA. |
| Central Valley steelhead Oncorhynchus mykiss | FT | -- | This ESU enters the Sacramento and San Joaquin Rivers and their tributaries from July to May; spawning from December to April. Young move to rearing areas in and through the Sacramento and San Joaquin Rivers, Delta, and San Pablo and San Francisco Bays. | Cool water with moderate size gravel for spawning and cover for rearing. | Year-round | Habitat Absent | Absent | No suitable habitat within the BSA. There are no CNDDB occurrences within five miles of the BSA. |
| Central Valley spring-run chinook salmon Oncorhynchus tshawytscha | FT | ST | Sacramento and San Joaquin Rivers and tributaries, Sacramento-San Joaquin Delta, San Francisco Bay. | Cool water with moderate size gravel for spawning and cover for rearing. | Year-round | Habitat Absent | Absent | No suitable habitat within the BSA. There are no CNDDB occurrences within five miles of the BSA. |
| Sacramento River winter-run chinook salmon Oncorhynchus tshawytscha | FE | SE | Sacramento and San Joaquin Rivers and tributaries, Sacramento-San Joaquin Delta, San Francisco Bay. | Cool water with moderate size gravel for spawning and cover for rearing. | Year-round | Habitat Absent | Absent | No suitable habitat within the BSA. There are no CNDDB occurrences within five miles of the BSA. |

Table BIO-3
Special-status Wildlife with the Potential to Occur in the Biological Study Area

| Common and Scientific Name | Legal Status ${ }^{1}$ |  | Distribution | Habitat Association | Identification Period | Habitat Present/ Absent | Species Present/ Absent | Rationale |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Federal | State |  |  |  |  |  |  |
| Sacramento splitttail gonichthys macrolepidotus | -- | SSC | Endemic to the lakes and rivers of the Central Valley, but now confined to the delta, Suisun Bay \& associated marshes. | Slow moving river sections, dead end sloughs. Requires flooded vegetation for spawning \& foraging for young. | Year-round | Habitat Absent | Absent | No suitable habitat within the BSA. There are no CNDDB occurrences within five miles of the BSA. |
| Longfin smelt <br> Spirinchus thaleichthys | FCT | $\begin{aligned} & \text { ST, } \\ & \text { SSC } \end{aligned}$ | Scattered populations of longfin smelt occur along the Pacific coast from Alaska to the San Francisco Estuary. Sacramento-San Joaquin Delta and the lower reaches of the two rivers. | Longfin smelt larvae and small juveniles are rarely found in water warmer than $71.6^{\circ} \mathrm{F}$ ( $22{ }^{\circ} \mathrm{C}$ ). Competent-swimming young juveniles disperse toward more-saline and deeper-water habitats. Mature longfin smelt require cool-tocold [less than $60.8^{\circ} \mathrm{F}\left(16{ }^{\circ} \mathrm{C}\right)$ ] freshwater habitats for spawning. | Year-round | Habitat Absent | Absent | No suitable habitat within the BSA. There are no CNDDB occurrences within five miles of the BSA. |

## NOTES:

Status explanations:
$-\quad=$ no listing.
Delisted = removed from federal or California Endangered Species Act list.
Federal
FC = federal candidate for listing under the federal Endangered Species Act.
FE $=$ listed as endangered under the federal Endangered Species Act
FT = listed as threatened under the federal Endangered Species Act.
L $=$ delisted
BGPA $=$ bald and golden eagle protection act
State $=\quad$ state candidate for listing as threatened under the California Endangered Species Act.
$\begin{array}{ll}\text { SCT } & =\text { state candidate for listing as threatened under the California Endang } \\ \text { SE } & =\text { listed as endangered under the California Endangered Species Act }\end{array}$
$\begin{array}{ll}\text { SE } & = \\ \text { SSC } & = \\ \text { listed as endangered under the } \\ \text { state species of special concern }\end{array}$
ST $=$ listed as threatened under the California Endangered Species Act
DL $=$ delisted
$\begin{array}{ll}\mathrm{FL} & =\text { species on the CDFW Watch Lis } \\ \mathrm{FP} & =\text { CDFW Fully Protected }\end{array}$
2 Species covered by the Yolo HCP/NCCP.

Of the 42 special-status wildlife species listed in Table BIO-3, 37 species were determined to not have potential to occur within the BSA, because the BSA lacks suitable habitat for the species or the BSA is outside the species' known range. There is no critical habitat or Essential Fish Habitat for any special-status wildlife species in the BSA. There is habitat within the BSA for the remaining five species: valley elderberry longhorn beetle (Desmocerus californicus dimorphus), burrowing owl (Athene cunicularia), Swainson's hawk (Buteo swainsoni), white-tailed kite (Elanus leucurus), and purple martin (Progne subis). These species are addressed in the discussion of project impacts below. Rationale for presence or absence and likelihood of occurrence in the BSA for special-status wildlife is provided in Table BIO-3.

## Wetlands and Other Waters

A formal delineation of potentially jurisdictional waters of the U.S. or state within the BSA has not been conducted. However, no potentially jurisdictional waters of the U.S. or state were noted during the reconnaissance survey of the BSA. The north fork of Putah Creek formerly flowed under Interstate 80 within the BSA. The north fork of Putah Creek was diverted to the south fork in 1948 to prevent flooding in the City of Davis. The remnant channel is still visible in the BSA, but no longer carries water. This remnant channel does not exhibit an ordinary high water mark or show any evidence of flowing water. This remnant channel does not meet the criteria as a jurisdictional water of the U.S or state.

## Discussion

a) Would the project have a substantial adverse effect, either directly or through habitat modifications, on any species identified as a candidate, sensitive, or special-status species in local or regional plans, policies, or regulations, or by the California Department of Fish and Wildlife, U.S. Fish and Wildlife Service, or NOAA Fisheries?

## Special-Status Plants Impacts

As shown in Table BIO-2, no special-status plant species have potential to be affected by the project because suitable habitat is not present within the project area. Consequently, the project would result in no impacts to special-status plant species

## Special-Status Wildlife Impacts

The biological study conducted for the proposed project determined that the proposed project could result in direct and indirect impacts to habitat for valley elderberry longhorn beetle, Swainson's hawk, and other migratory birds and raptors. The impacts and mitigation measures to address potentially significant impacts are discussed below.

## Valley Elderberry Longhorn Beetle

The valley elderberry longhorn beetle (Desmocerus californicus dimorphus) (VELB) occurs throughout the year in riparian woodlands and other Central Valley habitats containing elderberry shrubs (Sambucus spp.), upon which VELB is completely dependent for all stages of their life cycle. The females lay their eggs in crevices in the bark. After hatching, the larvae burrow into the stems of the tree where they feed on the interior wood for the next one to two years until they form pupae, from which the adults emerge. Prior to pupation, the larvae create an exit hole, plugs the hole with wood
shavings, and returns to the gallery where it pupates. Approximately one month later, the adult beetle emerges from the stem through the previously created exit hole (Burke 1921). As the larvae and adults are rarely seen, these borer holes are often the only evidence of this species' presence. After emergence from the stems, the adults remain in association with the elderberry shrub, where they will feed on the elderberry foliage and eventually reproduce.

VELB utilize elderberry shrubs with a stem diameter of at least one-inch (at ground level) as a host plant. All elderberry shrubs within the known range of the VELB that have one or more stems with diameters of one inch or greater at ground level are considered potential habitat for this species. In the Central Valley, elderberry shrubs are fairly common in remaining riparian forests and adjacent uplands. Elderberry shrubs are typically found growing in association with other riparian species, but they can also occur as isolated shrubs in upland areas. Historically, VELB ranged throughout the Central Valley. Currently, they are locally common in scattered populations from Redding to Bakersfield where historical riparian forests still exist.

ESA conducted a survey for of the entire BSA on May 4, 2018 for suitable habitat and evidence of presence for VELB. A total of 15 elderberry shrubs providing suitable VELB were identified within the BSA in several locations and one species occurrence has been recorded in the CNDDB within five miles of the project site. Subsequent to the aforementioned survey conducted by ESA, two additional elderberry shrubs were identified within the BSA by CDFW and USFW during field surveys for the Yolo Corridor Improvement Project in August 2021. Table BIO-4 details the 17 elderberry shrubs identified within the BSA.

A total of 13 elderberry shrubs occur within the project site within 100 feet of proposed project activities (see Figures 9, 10, and 11). However, none of these shrubs would be directly impacted based on current project design. No ground disturbing activities are proposed within 30 feet of any elderberry shrubs, and all but three of the 13 shrubs within the PIA are a minimum of 70 feet from proposed project activities. In addition, all of the elderberry shrubs within the PIA currently experience ongoing disturbance due to traffic and maintenance activities such as mowing (homeless encampments). The elderberry shrubs are not within riparian habitat, and no exit holes were observed on the shrubs. These shrubs are isolated from high quality suitable habitat for VELB. The nearest riparian habitat to the project site is associated with South Fork Putah Creek approximately 6,800 feet south of the project site. The nearest CNDDB occurrence of VELB is a 1934 collection of a single beetle with the location given as "Davis". No recent occurrences are documented in the CNDDB near the project site. According to the Framework for Assessing Impacts to the Valley Elderberry Longhorn Beetle (USFWS, 2017), isolated, nonriparian elderberry clumps are less likely to be occupied or become colonized by VELB, and those beyond 800 meters $(2,526$ feet) from the nearest elderberry clumps or nearest VELB occurrences become increasingly less likely to be occupied. The project would not directly impact shrubs, no ground disturbing activities would occur within 30 feet of any elderberry shrubs, and the elderberry shrubs are non-riparian and isolated.

Table BIO-4
Elderberry Shrubs (EB) within the Biological Study Area

| ID \# | Stems $\mathbf{\geq 1 "}$ <br> and $\leq 3^{\prime \prime}$ | Stems $>\mathbf{3}^{\prime \prime \prime}$ <br> and $<5 "$ | Stems $\geq 5^{\prime \prime}$ | Exit Holes (Y/N) | Riparian/ <br> Non-Riparian | Impacts |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| EB-1 | 3 | 0 | 0 | No | Non-Riparian | No |
| EB-2 | 4 | 1 | 1 | No | Non-Riparian | No |
| EB-3 | 2 | 0 | 0 | No | Non-Riparian | No |
| EB-4 | 7 | 2 | 5 | No | Non-Riparian | No |
| EB-5 | 0 | 1 | 2 | No | Non-Riparian | Indirect |
| EB-6 | 0 | 1 | 0 | No | Non-Riparian | Indirect |
| EB-7 | 0 | 1 | 2 | No | Non-Riparian | Indirect |
| EB-8 | 2 | 1 | 1 | No | Non-Riparian | Indirect |
| EB-9 | 4 | 2 | 3 | No | Non-Riparian | Indirect |
| EB-10 | 3 | 2 | 2 | No | Non-Riparian | Indirect |
| EB-11 | 4 | 2 | 4 | No | Non-Riparian | Indirect |
| EB-12 | 5 | 7 | 1 | No | Non-Riparian | Indirect |
| EB-13 | 2 | 0 | 2 | No | Non-Riparian | Indirect |
| EB-14 | 0 | 0 | 4 | No | Non-Riparian | Indirect |
| EB-15 | 0 | 3 | 0 | No | Non-Riparian | Indirect |
| EB-16* | 20 | 3 | 0 | No | Non-Riparian | Indirect |
| EB-17* | 24 | 0 | 0 | No | Non-Riparian | Indirect |
| NOTE |  |  |  |  |  |  |

NOTE:
EB-16 and EB-17 are the two elderberry shrubs identified within the BSA by CDFW and USFW during field surveys for the Yolo Corridor Improvement Project in August 2021.

SOURCE: ESA, 2021



SOURCE: USDA, 2018; ESRI, 2021; ESA, 2021
Interstate 80/Richards Boulevard Interchange Improvements Project
r ESA


SOURCE: USDA, 2016; ESRI, 2012; ESA, 2018

1

Therefore, the proposed project would have no direct impacts on VELB. While all of the elderberry shrubs are located outside of the project impact footprint, shrubs may potentially be indirectly affected by project construction, resulting in potentially significant impacts to elderberry shrubs. Implementation of Mitigation Measure BIO-1 (see page 58) would ensure that indirect impacts to elderberry shrubs would be less than significant.

## Burrowing Owl

Burrowing owl (Athene cunicularia), a California Species of Special Concern, is a small diurnal owl that nests underground in the burrows of small mammals, especially those of ground squirrels. Culverts and other human-made structures may also be suitable habitat for the burrowing owl. Often a burrowing owl will occupy several burrows in an area. In the Central Valley, the burrowing owl is a year-round resident of open spaces such as grasslands, agricultural fields, air fields, and levees. Vegetation must be very short or very sparse to be suitable habitat for burrowing owl. Breeding peaks from April to May but can occur from March to August. The burrowing owl forages on insects and small mammals and will also consume reptiles, birds, and carrion.

Suitable nesting habitat is present within the PIA and surrounding BSA, however no burrowing owls or active nests were observed in the BSA during the May 4, 2018 biological survey. Some soils within the BSA are sandy and friable and burrows and burrow complexes were noted during the survey. While no soil mounds were visible during the field survey, surrounding fence posts would provide suitable perches above potential nests within suitable habitat. There are 24 reported occurrences of burrowing owl in the CNDDB within five miles of the BSA. The closest occurrence is approximately 600 feet south of the BSA.

Accordingly, the proposed project could potentially impact individual burrowing owls if they occupied the BSA prior to construction. Indirect impacts to nesting birds during construction could extend up to 500 feet from the limits of construction. Potential impacts could include abandonment of nest sites and the mortality of young. The proposed project could also result in a permanent loss of foraging opportunities for burrowing owl in and adjacent to the PIA during construction. The loss of nesting and/or foraging habitat in and adjacent to the PIA is not expected to significantly impact burrowing owl because these habitats are abundant in the vicinity.

Because the BSA occurs within an urban area subject to ongoing noise disturbances and human presence, any burrowing owls nesting in this area would likely be habituated to these existing disturbances. Based on the existing level of disturbance/noise in the project vicinity, and limited ground disturbance associated with the project, the project is not likely to result in adverse effects (nest abandonment and/or death of developing burrowing owl eggs or young). Nonetheless, project ground-disturbing and noiseproducing construction activities could result in potentially significant impacts to nesting burrowing owls. Implementation of Mitigation Measure BIO-2 (see page 59) would ensure that impacts to burrowing owls would be less than significant.

## Swainson's Hawk

Swainson's hawk (Buteo swainsoni) is listed as a threatened species under CESA. This raptor is found primarily in open country, foraging in grasslands and agricultural fields, especially after disking or harvest. They use tall riparian trees (typically oaks or cottonwoods) for nesting but will occasionally nest in large eucalyptus or other large ornamental trees if there is suitable foraging habitat nearby. The species has lost much of its former nesting habitat as a result of the significant reduction in riparian woodland and forest habitat throughout the state over the last 100 years and is losing foraging habitat to urban development. Swainson's hawks can forage as far as 20 miles from the nest, but nests are generally more successful if suitable foraging habitat is present within an approximate ten-mile radius. Suitable foraging habitat is defined as annual grasslands, fallow fields, dry and irrigated pasture, and a variety of croplands including alfalfa, beet, tomato and other low growing row or field crops, rice (when not flooded), and cereal grain crops (including corn after harvest). When forced to travel greater distances from the nest, the adults must expend much more time and energy gathering food, leaving the eggs and young in the nests much more vulnerable to predation and the elements.

No Swainson's hawks were observed at or within 0.25 mile of the BSA during the May 4, 2018 field survey. Within the BSA, suitable nesting habitat occurs in larger trees. The BSA does not support suitable foraging areas for Swainson's hawk; however, suitable foraging habitat for this species is available adjacent to the BSA. Annual grassland in the BSA is highly disturbed, small in area, and fragmented. There are over one hundred CNDDB recorded occurrences of Swainson's hawk within five miles of the BSA, including several within one mile of the BSA (CDFW, 2019).

Noise associated with construction activities involving heavy equipment operation that occurs during the breeding season (generally between February 15 and August 31) could disturb nesting Swainson's hawk if an active nest is located near these activities. Within urban areas, CDFW considers 0.25 mile to be a sufficient buffer to avoid disturbance of nesting Swainson's hawks. Any disturbance that causes Swainson's hawk nest abandonment and subsequent loss of eggs or developing young at active nests located near the project area would violate the CESA; CFGC Sections 2800, 3503, and 3503.5; and the Migratory Bird Treaty Act (MBTA).

Because the BSA occurs within an urban area subject to ongoing noise disturbances and human presence, any Swainson's hawks nesting in this area would likely be habituated to these existing disturbances. Based on the existing level of disturbance/noise in the project vicinity, and limited ground disturbance associated with the project, the project is not likely to result in adverse effects (nest abandonment and/or death of developing Swainson's hawk eggs or young). Nonetheless, project ground-disturbing and noiseproducing construction activities could result in potentially significant impacts to nesting Swainson's hawks. Implementation of Mitigation Measure BIO-3 (see page 62) would ensure that impacts to Swainson's hawks would be less than significant.

## White-Tailed Kite

The white-tailed kite (Elanus leucurus) is listed as a "fully protected" raptor under Section 3511 of the California Fish and Game Code. The white-tailed kite is a year-round resident in central California. It typically nests in oak woodlands or trees, especially along marshes or river margins, and may use any suitable tree or shrub that is of moderate height. Its nesting season may begin as early as February and extends into August. This raptor forages during the day for rodents-especially voles-in wet or dry grasslands and fields. White-tailed kites forage characteristically by hovering over the location of a potential prey item. Although, like other raptors, kites build solitary nests, they often roost, and occasionally nest communally, especially during the non-breeding season.

Suitable nesting habitat is present within the PIA and surrounding BSA, however no white-tailed kites or active nests were observed in the BSA during the May 4, 2018 biological survey. Within the BSA, suitable nesting habitat occurs in larger trees. There are six reported occurrences of white-tailed kite in the CNDDB within five miles of the BSA. The closest occurrence is approximately 0.96 mile northeast of the BSA.

Disturbance of a relatively small roost or nesting area could affect a large number of birds. Noise associated with construction activities involving heavy equipment operation that occurs during the breeding season (generally between February 15 and August 31) could disturb nesting white-tailed kites if an active nest is located near these activities.

Because the BSA occurs within an urban area subject to ongoing noise disturbances and human presence, any white-tailed kites nesting in this area would likely be habituated to these existing disturbances. Based on the existing level of disturbance/noise in the project vicinity, and limited ground disturbance associated with the project, the project is not likely to result in adverse effects (nest abandonment and/or death of developing whitetailed kite eggs or young). Nonetheless, project ground-disturbing and noise-producing construction activities could result in potentially significant impacts to nesting whitetailed kites. Implementation of Mitigation Measure BIO-3 (see page 62) would ensure that impacts to white-tailed kites would be less than significant.

## Purple Martin

The purple martin (Progne subis) can be found throughout nearly the entire U.S. east of the Rocky Mountains. Although declining in many western states, it is also found in isolated areas of Canada, Oregon, Washington, California, Utah, Colorado, Arizona, New Mexico and Mexico. In California it is a Species of Special Concern. It is an early spring migrant from its wintering grounds in South America. Generally, purple martins inhabit open areas with an open water source nearby. Martins adapt well in and around people, but people are out-competed by starlings (Sturnus vulgaris) and sparrows in urban areas. Purple martins are colonial cavity nesters in abandoned woodpecker holes, human-made nest boxes, or cavities in other structures such as bridges and overpasses. Once established at a nest location, martins usually come back to the same site every year.

There are numerous potential nesting sites for this urban-adapted species throughout the BSA, in particular the I-80/Richards Boulevard overpass. There are no CNDDB recorded
occurrences of purple martin within five miles of the BSA. Disturbance of active nest sites which results in nest abandonment, loss of young, or reduced health and vigor of eggs and/or nestlings (resulting in reduced survival rates), or the direct removal of structures that supports nesting birds which result in killing of nestlings or fledgling bird species would be considered a potentially significant impact. Implementation of Mitigation Measure BIO-4 (see page 62) would ensure that impacts to purple martins would be less than significant.

## Other Nesting Migratory Birds and Raptors

Other migratory birds and raptors could nest within and surrounding the BSA in trees. The breeding season for most birds and raptors within the project region is generally from February 15 and August 31 . The occupied nests and eggs of these birds are protected by federal and state laws, including MBTA and CFGC Sections 3503 and 3503.5.

Migratory birds and raptors that could potentially nest within or adjacent to the BSA include, but are not limited to, American kestrel (Falco sparverius), California towhee (Melozone crissalis), red-tailed hawk (Buteo jamaicensis), northern harrier (Circus cyaneus), turkey vulture (Cathartes aura), American robin (Turdus migratorius), killdeer (Charadrius vociferus), mourning dove (Zenaida macroura), northern mockingbird (Mimus polyglottos), western meadowlark (Sturnella neglecta), and western scrub-jay (Aphelocoma californica).

Noise associated with construction activities involving heavy equipment operation that occurs during the breeding season (generally between February 1 and September 30) could disturb nesting migratory birds and raptors if an active nest is located near these activities. Any disturbance that causes migratory bird or raptor nest abandonment and subsequent loss of eggs or developing young at active nests located at or near the project area would violate CFGC Sections 3503 or 3503.5 and the MBTA. Consequently, impacts to other migratory birds and raptors are potentially significant. Implementation of Mitigation Measure BIO-4 (see page 62) would ensure that impacts to other migratory birds and raptors would be less than significant.
b) Would the project have a substantial adverse effect on any riparian habitat or other sensitive natural community identified in local or regional plans, policies, regulations or by the California Department of Fish and Wildlife or U.S. Fish and Wildlife Service?

Habitats and natural communities of special concern are those that are regulated by the federal, state, or local resource agencies. The BSA does not support any habitats that would be considered natural communities of special concern, including sensitive natural communities identified in local or regional plans, policies, regulations, or by the California Department of Fish and Game or U.S. Fish and Wildlife Service. Similarly, the BSA does not support any potentially jurisdictional wetlands and other waters of the U.S or state or riparian habitat. Therefore, project would result in no impact to these resources.
c) Would the project have a substantial adverse effect on state or federally protected wetlands (including, but not limited to, marsh, vernal pool, coastal, etc.) through direct removal, filling, hydrological interruption, or other means?

No state or federally protected wetlands or potentially jurisdictional waters of the U.S. or state were noted during the reconnaissance survey of the BSA. The north fork of Putah Creek formerly flowed under Interstate 80 within the BSA. The north fork of Putah Creek was diverted to the south fork in 1948 to prevent flooding in the City of Davis. The remnant channel is still visible in the BSA, but no longer carries water. This remnant channel does not exhibit an ordinary high water mark or show any evidence of flowing water. This remnant channel does not meet the criteria as a jurisdictional water of the U.S or state. Consequently, the project would result in no impacts to state or federally protected wetlands or potentially jurisdictional waters of the U.S. or state.
d) Would the project interfere substantially with the movement of any native resident or migratory fish or wildlife species or with established native resident or migratory wildlife corridors, or impede the use of native wildlife nursery sites?

Developed uses comprise the majority of the BSA and consists of paved or otherwise developed areas. Ornamental vegetation associated with the BSA consists of trees and understory grassland along road shoulders and within undeveloped lots and open areas. In addition, some areas of agricultural land were noted within the BSA. Habitat types within the BSA do not support fish or serve as significant wildlife corridors or linkages for special-status terrestrial species. Therefore, impacts on movement of terrestrial species associated with the proposed project would be considered less than significant.

As discussed above under question a) noise associated with construction activities involving heavy equipment operation that occurs during the breeding season could disturb Swainson's hawks and other nesting migratory birds and raptors if an active nest is located near these activities. Any disturbance that causes migratory bird or raptor nest abandonment and subsequent loss of eggs or developing young at active nests located at or near the project area would violate CFGC Sections 3503 or 3503.5 and the MBTA. Consequently, impacts to migratory birds and raptors are potentially significant. Implementation of Mitigation Measure BIO-4 (see page 62) would ensure that impacts to other migratory birds and raptors would be less than significant.
e) Would the project conflict with any local policies or ordinances protecting biological resources, such as a tree preservation policy or ordinance?

The City has acknowledged the importance of preserving mature trees through adoption of the City's tree preservation ordinance. The City adopted an ordinance on December 4, 2002 to protect landmark trees, trees of significance, street trees, city trees, and private trees. The loss of protected trees, including street trees, city trees (trees in parks, greenbelts, open spaces, or on city property or easements), landmark trees, and trees of significance is regulated by the City tree ordinance. The trees within the project area are ornamental trees within the Caltrans right-of-way and are not protected by the City's tree
ordinance. Nonetheless, implementation of Mitigation Measure BIO-5 (see page 63) would ensure that any unanticipated impacts to protected trees would be less than significant.
f) Would the project conflict with the provisions of an adopted Habitat Conservation Plan, Natural Community Conservation Plan, or other approved local, regional, or state habitat conservation plan?

The project site is located within the boundaries of the Yolo Habitat Conservation Plan/ Natural Community Conservation Plan (Yolo HCP/NCCP). The Yolo Habitat Conservancy (Conservancy), which consists of Yolo County and the incorporated cities of Davis, West Sacramento, Winters, and Woodland, completed the Yolo HCP/NCCP in 2018 and began implementation on January 11, 2019. The Yolo HCP/NCCP is a countywide conservation plan that ensures compliance with the Federal Endangered Species Act, the California Natural Community Conservation Planning Act, and the California Endangered Species Act for covered activities that may affect the covered species. The City of Davis is participatory to the Yolo HCP/NCCP and, consequently, the proposed project is considered a "covered activity" under the HCP/NCCP. Mitigation for incidental take of covered species occurring under the HCP/NCCP is provided through the establishment and management of a habitat reserve system and the restoration of natural communities within the HCP/NCCP area. Mitigation of impacts to covered species is accomplished through the payment of fees in order to obtain coverage under the Yolo HCP/NCCP.

The Yolo HCP/NCCP coordinates mitigation to maximize benefits to 12 covered species, including the following species potentially impacted by the proposed project: VELB, Swainson's hawk, white-tailed kite, and western burrowing owl. Therefore, implementation of the proposed project has the potential to result in impacts to covered species under the Yolo HCP/NCCP, and this impact is considered potentially significant. As described below, the project includes mitigation measures for impacts to these species that are consistent with the provisions of the Yolo HCP/NCCP (see Mitigation Measures BIO-1, BIO-2, and BIO-3). Implementation of these measures would reduce impacts to a less-than-significant level. In addition, implementation of Mitigation Measure BIO-6 (see page 63) would ensure that the proposed project would obtain coverage under the Yolo HCP/NCCP.

## Mitigation Measures

## Mitigation Measure BIO-1: Implement Yolo HCP/NCCP Avoidance and Minimization Measures 12: Minimize Take and Adverse Effects on Habitat of Valley Elderberry Longhorn Beetle.

The following measures shall be implemented during project construction.

- All suitable elderberry shrubs (i.e., shrubs with stem diameters of at least one inch when measured at ground level) shall be avoided. Shrubs shall not be removed or pruned.
- Shrubs shall be flagged or temporarily fenced, as needed, with guidance from a qualified biologist. These areas shall be avoided by all personnel and construction activities. When feasible, fencing shall be placed at least five feet from the dripline of each shrub.
- Timing of work near elderberry shrubs shall avoid the flight season of the beetle (March 15 - June 15) if feasible.
- The project proponent will maintain a buffer of at least 100 feet from any elderberry shrubs with stems greater than one inch in diameter at ground level. A lesser buffer may be approved by the Yolo Habitat Conservancy, USFWS, and CDFW if they determine that the shrubs are avoided to an extent that is consistent with the project purpose. In cases where the buffer is reduced, the maximum possible buffer will be implemented that accommodates project design, and consultation with the Conservancy, USFWS, and CDFW will occur to determine if further mitigation is required. Any temporarily disturbed habitat within the 100 -foot buffer will be restored upon completion of construction activities.


## Mitigation Measure BIO-2: Implement Yolo HCP/NCCP Avoidance and Minimization Measures 18: Minimize Take and Adverse Effects on Western Burrowing Owl.

The project proponent will retain a qualified biologist to conduct planning-level surveys and identify western burrowing owl habitat (as defined in Appendix A, Covered Species Accounts, of the Yolo $H C P / N C C P$ ) within or adjacent to (i.e., within 500 feet of) a covered activity. If habitat for this species is present, additional surveys for the species by a qualified biologist are required, consistent with CDFW guidelines (CDFW, 2012).

If burrowing owls are identified during the planning-level survey, the project proponent will minimize activities that will affect occupied habitat as follows. Occupied habitat is considered fully avoided if the project footprint does not impinge on a nondisturbance buffer around the suitable burrow. For occupied burrowing owl nest burrows, this nondisturbance buffer could range from 150 to 1,500 feet (Table BIO-5), depending on the time of year and the level of disturbance, based on current guidelines (CDFW, 2012). The Yolo HCP/NCCP generally defines low, medium, and high levels of disturbances of burrowing owls as follows.

- Low: Typically 71-80 dB, generally characterized by the presence of passenger vehicles, small gas-powered engines (e.g., lawn mowers, small chain saws, portable generators), and high-tension power lines. Includes electric hand tools (except circular saws, impact wrenches and similar). Management and enhancement activities would typically fall under this category. Human activity in the immediate vicinity of burrowing owls would also constitute a low level of disturbance, regardless of the noise levels.
- Moderate: Typically 81-90 dB, and would include medium- and large-sized construction equipment, such as backhoes, front end loaders, large pumps and generators, road graders, dozers, dump trucks, drill rigs, and other moderate to large diesel engines. Also includes power saws, large chainsaws, pneumatic drills and impact wrenches, and large gasoline-powered tools. Construction activities would normally fall under this category.
- High: Typically 91-100 dB, and is generally characterized by impacting devices, jackhammers, compression brakes on large trucks, and trains. This category includes both vibratory and impact pile drivers (smaller steel or wood piles) such as used to install piles and guard rails, and large pneumatic tools such as chipping machines. It may also include large diesel and gasoline engines, especially if in concert with other impacting devices. Felling of large trees (defined as dominant or subdominant trees in
mature forests), truck horns, yarding tower whistles, and muffled or underground explosives are also included. Very few covered activities are expected to fall under this category, but some construction activities may result in this level of disturbance.

The project proponent may qualify for a reduced buffer size, based on existing vegetation, human development, and land use, if agreed upon by CDFW and USFWS (CDFW, 2012).

Table BIO-5
Recommended Restricted Activity Dates and Setback Distances by Level of Disturbance for Burrowing Owls

| Time of Year | Level of Disturbance (feet) from Occupied Burrows |  |  |
| :--- | :---: | :---: | :---: |
|  | Low | Medium | High |
| April 1 - August 15 | 600 | 1,500 | 1,500 |
| August 16 - October 15 | 600 | 600 | 1,500 |
| October 16 - March 31 | 150 | 300 | 1,500 |
| SOURCE: Yolo Habitat Conservancy 2018 |  |  |  |

If the project does not fully avoid direct and indirect effects on nesting sites (i.e., if the project cannot adhere to the buffers described above), the project proponent will retain a qualified biologist to conduct preconstruction surveys and document the presence or absence of western burrowing owls that could be affected by the covered activity. Prior to any ground disturbance related to covered activities, the qualified biologist will conduct the preconstruction surveys within three days prior to ground disturbance in areas identified in the planning-level surveys as having suitable burrowing owl burrows, consistent with CDFW preconstruction survey guidelines (CDFW, 2012). The qualified biologist will conduct the preconstruction surveys three days prior to ground disturbance. Time lapses between ground disturbing activities will trigger subsequent surveys prior to ground disturbance.

If the biologist finds the site to be occupied ${ }^{1}$ by western burrowing owls during the breeding season (February 1 to August 31), the project proponent will avoid all nest sites, based on the buffer distances described above, during the remainder of the breeding season or while the nest is occupied by adults or young (occupation includes individuals or family groups that forage on or near the site following fledging). Construction may occur inside of the disturbance buffer during the breeding season if the nest is not disturbed and the project proponent develops an AMM plan that is approved by the Conservancy, CDFW, and USFWS prior to project construction, based on the following criteria:

- The Conservancy, CDFW, and USFWS approves the AMM plan provided by the project proponent.
- A qualified biologist monitors the owls for at least three days prior to construction to determine baseline nesting and foraging behavior (i.e., behavior without construction).
- The same qualified biologist monitors the owls during construction and finds no change in owl nesting and foraging behavior in response to construction activities.

[^0]- If the qualified biologist identifies a change in owl nesting and foraging behavior as a result of construction activities, the qualified biologist will have the authority to stop all construction related activities within the non-disturbance buffers described above. The qualified biologist will report this information to the Conservancy, CDFW, and USFWS within 24 hours, and the Conservancy will require that these activities immediately cease within the non-disturbance buffer. Construction cannot resume within the buffer until the adults and juveniles from the occupied burrows have moved out of the project site, and the Conservancy, CDFW, and USFWS agree.
- If monitoring indicates that the nest is abandoned prior to the end of nesting season and the burrow is no longer in use by owls, the project proponent may remove the nondisturbance buffer, only with concurrence from CDFW and USFWS. If the burrow cannot be avoided by construction activity, the biologist will excavate and collapse the burrow in accordance with CDFW's 2012 guidelines to prevent reoccupation after receiving approval from the wildlife agencies.

If evidence of western burrowing owl is detected outside the breeding season (September 1 to January 31), the project proponent will establish a non-disturbance buffer around occupied burrows, consistent with Table BIO-5, as determined by a qualified biologist. Construction activities within the disturbance buffer are allowed if the following criteria are met to prevent owls from abandoning important overwintering sites:

- A qualified biologist monitors the owls for at least three days prior to construction to determine baseline foraging behavior (i.e., behavior without construction).
- The same qualified biologist monitors the owls during construction and finds no change in owl foraging behavior in response to construction activities.
- If there is any change in owl roosting and foraging behavior as a result of construction activities, these activities will cease within the buffer.
- If the owls are gone for at least one week, the project proponent may request approval from the Conservancy, CDFW, and USFWS for a qualified biologist to excavate and collapse usable burrows to prevent owls from reoccupying the site if the burrow cannot be avoided by construction activities. The qualified biologist will install one-way doors for a 48-hour period prior to collapsing any potentially occupied burrows. After all usable burrows are excavated, the buffer will be removed and construction may continue.

Monitoring must continue as described above for the nonbreeding season as long as the burrow remains active.

A qualified biologist will monitor the site, consistent with the requirements described above, to ensure that buffers are enforced and owls are not disturbed. Passive relocation (i.e., exclusion) of owls has been used in the past in the Plan Area to remove and exclude owls from active burrows during the nonbreeding season (Trulio, 1995). Exclusion and burrow closure will not be conducted during the breeding season for any occupied burrow. If the Conservancy determines that passive relocation is necessary, the project proponent will develop a burrowing owl exclusion plan in consultation with CDFW biologists. The methods will be designed as described in the species monitoring guidelines (CDFW, 2012) and consistent with the most up-to-date checklist of passive relocation techniques. ${ }^{2}$ This may include the installation of one-way doors in

[^1]burrow entrances by a qualified biologist during the nonbreeding season. These doors will be in place for 48 hours and monitored twice daily to ensure that the owls have left the burrow, after which time the biologist will collapse the burrow to prevent reoccupation. Burrows will be excavated using hand tools. During excavation, an escape route will be maintained at all times. This may include inserting an artificial structure, such as piping, into the burrow to prevent collapsing until the entire burrow can be excavated and it can be determined that no owls are trapped inside the burrow. The Conservancy may allow other methods of passive or active relocation, based on best available science, if approved by the wildlife agencies. Artificial burrows will be constructed prior to exclusion and will be created less than 300 feet from the existing burrows on lands that are protected as part of the reserve system.

## Mitigation Measure BIO-3: Implement Yolo HCP/NCCP Avoidance and Minimization Measures 16: Minimize Take and Adverse Effects on Habitat of Swainson's Hawk and White-Tailed Kite.

The project proponent will retain a qualified biologist to conduct planning-level surveys and identify any nesting habitat present within 1,320 feet of the project footprint. Adjacent parcels under different land ownership will be surveyed only if access is granted or if the parcels are visible from authorized areas.

If a construction project cannot avoid potential nest trees (as determined by the qualified biologist) by 1,320 feet, the project proponent will retain a qualified biologist to conduct preconstruction surveys for active nests consistent, with guidelines provided by the Swanson's Hawk Technical Advisory Committee (2000), between March 15 and August 31, within 15 days prior to the beginning of the construction activity. The results of the survey will be submitted to the Conservancy and CDFW. If active nests are found during preconstruction surveys, a 1,320foot initial temporary nest disturbance buffer shall be established. If project related activities within the temporary nest disturbance buffer are determined to be necessary during the nesting season, then the qualified biologist will monitor the nest and will, along with the project proponent, consult with CDFW to determine the best course of action necessary to avoid nest abandonment or take of individuals. Work may be allowed only to proceed within the temporary nest disturbance buffer if Swanson's hawk or white-tailed kite are not exhibiting agitated behavior, such as defensive flights at intruders, getting up from a brooding position, or flying off the nest, and only with the agreement of CDFW and USFWS. The designated on-site biologist/monitor shall be on-site daily while construction-related activities are taking place within the 1,320-foot buffer and shall have the authority to stop work if raptors are exhibiting agitated behavior. Up to 20 Swanson's hawk nest trees (documented nesting within the last 5 years) may be removed during the permit term, but they must be removed when not occupied by Swanson's hawks.

For covered activities that involve pruning or removal of a potential Swanson's hawk or whitetailed kite nest tree, the project proponent will conduct preconstruction surveys that are consistent with the guidelines provided by the Swanson's Hawk Technical Advisory Committee (2000). If active nests are found during preconstruction surveys, no tree pruning or removal of the nest tree will occur during the period between March 1 and August 30 within 1,320 feet of an active nest, unless a qualified biologist determines that the young have fledged and the nest is no longer active.

## Mitigation Measure BIO-4: Conduct a Preconstruction Survey for other Nesting Migratory

 Birds and Raptors and Establish No-disturbance Buffers, if Necessary. If construction (including equipment staging and tree removal) will occur during the breeding season for migratory birds and raptors (generally between February 15 and August 31), the City shall retain a qualified biologist to conduct a preconstruction nesting bird and raptor survey before the onsetof construction activities. The preconstruction nesting bird and raptor surveys shall be conducted between February 1 and September 30 within suitable habitat at the project area. Surveys for migratory birds and raptor nests should extend 500 feet from the project area to ensure that nesting birds are not indirectly affected by construction noise. The survey shall be conducted no more than 14 days before the initiation of construction activities. If no active nests are detected during the survey, no additional mitigation is required and construction can proceed.

If migratory birds or raptors are found to be nesting in or adjacent to the project area, a 500-foot no-disturbance buffer shall be established around raptor nests and a 250-foot buffer around nonraptor nests to avoid disturbance of the nest area and to avoid take. The buffer shall be maintained around the nest area until the end of the breeding season or until a qualified biologist determines that the young have fledged and are foraging on their own. The extent of these buffers shall be determined by the biologist (coordinating with the CDFW) and shall depend on the species identified, level of noise or construction disturbance, line of sight between the nest and the disturbance, ambient levels of noise and other disturbances, and other topographical or artificial barriers.

Mitigation Measure BIO-5: Mitigate for Impacts to Protected Trees. If the proposed project would remove protected trees, the City shall submit a tree removal permit application for the removal of protected trees, as defined by City Code 37.01.020. The application shall include proposed mitigation measures to protect retained trees and propose replacement measures to mitigate for the loss of tree resources (replacement measures may be determined in consultation with the City's Director of Community Services). Any trees planted within the Caltrans right-ofway will need to meet Caltrans standards.

Mitigation Measure BIO-6: Obtain Coverage Under the Yolo HCP/NCCP. As a condition of approval for the proposed project, the City of Davis shall apply for and obtain coverage under the Yolo HCP/NCCP for impacts to covered species.

## References

Burke, H.E., 1921. Biological notes on Desmocerus, a genus of roundhead borers, the species of which infest various elders. Journal of Economic Entomology 14.

California Department of Transportation (Caltrans), 2019. Natural Environment Study (Minimal Impacts), Interstate 80/Richards Boulevard Interchange Improvements Project. April 2019.

California Department of Fish and Wildlife (CDFW), 2012. Staff Report on Burrowing Owl Mitigation. State of California Natural Resources Agency. Department of Fish and Game. March 7, 2012.
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U.S. Fish and Wildlife Service (USFWS), 2017. Framework for Assessing Impacts to the Valley Elderberry Longhorn Beetle (Desmocerus californicus dimporphus). U.S. Fish and Wildlife Service; Sacramento, California. 28 pp.

Western Regional Climate Center, 2018. Period of Record General Climate Summary for Davis 2 WSW Exp Farm, California (042294), 1893-2016. Available: www.wrcc.dri.edu/coopmap. Accessed August 8, 2018.

Yolo Habitat Conservancy, 2018. Yolo Habitat Conservation Plan/Natural Community Conservation Plan. Available: https://www.yolohabitatconservancy.org/documents. Accessed April 28, 2020.

## Cultural Resources

| Issues (and Supporting Information Sources): | Potentially Significant Impact | Less Than Significant with Mitigation Incorporated | Less Than Significant Impact | No Impact |
| :---: | :---: | :---: | :---: | :---: |
| V. CULTURAL RESOURCES - Would the project: |  |  |  |  |
| a) Cause a substantial adverse change in the significance of a historical resource pursuant to §15064.5? | $\square$ | Х | $\square$ | $\square$ |
| b) Cause a substantial adverse change in the significance of an archaeological resource pursuant to §15064.5? | $\square$ | Х | $\square$ | $\square$ |
| c) Disturb any human remains, including those interred outside of formal cemeteries? | $\square$ | Х | $\square$ | $\square$ |

## Discussion

a-c) On behalf of Caltrans District 3 and the City of Davis, ESA cultural resources staff conducted a cultural resources investigation for the proposed project that included a review of records from the Northwest Information Center (NWIC) of the California Historical Resources Information System (April 24, 2018; File No. 17-2544), a review of the proposed project design plans and methods of construction, and a pedestrian survey of the project site by an ESA Registered Professional Archaeologist. The investigation was conducted in support of the proposed project's compliance with the requirements of Section 106 of the National Historic Preservation Act and CEQA (ESA, 2018).

The investigation determined that there are no previously recorded archaeological or architectural resources in the proposed project Area of Potential Effects (APE), which comprises the geographic area within which a project may directly or indirectly cause changes in the character or use of historical or archaeological resources.

The nearest known prehistoric archaeological site is CA-YOL-118, which includes the remains of a large sweathouse, features, midden, and human remains. The site is approximately 0.25 mile west of the APE and would not be affected by the proposed project. There are also two sites informally recorded as "possible sites" further to the north on the University of California Davis campus. These sites would also not be affected by the proposed project.

The Richards Boulevard Underpass, located immediately adjacent to the APE, was constructed in 1917 and has been recommended eligible for listing in the National Register of Historic Places and California Register of Historical Resources. It is one of the oldest surviving examples of I-beam bridge construction on a railroad grade separation. The underpass would not be affected by the proposed project.

The pedestrian archaeological survey consisted of walking the paved and unpaved portions of the APE in narrow (no greater than 10-meter-wide) transects, where feasible, to observe the existing conditions and identify cultural resources, if present. The narrowness of the APE along the roadways made the use of parallel transects unnecessary, so inspection for cultural materials on one transect was sufficient. All areas
of the APE have been highly disturbed from construction of the existing overpass and roadways. Unpaved portions of the APE consisted of open, grassy areas between the onand off-ramps. Non-native grasses covered much of the unpaved areas, and grasses were periodically scraped back to expose ground surface. Some small trees and shrubs were also present. All soils in the APE consisted of light or medium brown gravelly loam, consistent with artificially-deposited fill and/or landscaping. Modern trash was lightly scattered throughout the APE adjacent to the on- and off-ramps. No prehistoric or historic-era cultural materials or other evidence of past human use or occupation were identified in the APE.

Pursuant to Public Resources Code section 21080.3.1, the City of Davis consulted with California Native American tribes regarding the proposed project. Letters that described the proposed project, provided formal notification of the proposed project, and requested a written response within 30 days if consultation was desired were sent to the Ione Band of Miwok Indians, the Yoche Dehe Wintun Nation, and the Cortina Indian Rancheria of Wintun Indians on August 28, 2019. The City received one response. In a letter dated September 12, 2018, the Yoche Dehe Wintun Nation stated that the project site is within the aboriginal territory of the Yoche Dehe Wintun Nation and therefore the tribe has cultural interest and authority in the project area. The letter stated that the tribe is not aware of any known cultural resources near the project site and monitoring is not needed. The letter included a recommendation that pre-construction cultural resource sensitivity training should be provided by members of the Yoche Dehe Wintun Nation. Records of tribal consultation are included in Appendix C of this initial study.

The cultural resources investigation determined that the proposed project has no potential to affect above-ground historical resources and a low potential to affect archaeological or resources or human remains due to the environmental setting and previous extensive disturbance of the area. Nonetheless, because there is a possibility that project construction and excavation activities could unearth previously undiscovered or unrecorded prehistoric or historic archaeological resources or human remains, if they are present, the impact is considered to be potentially significant. Implementation of Mitigation Measures CUL-1, CUL-2, and CUL-3 would ensure that impacts to archaeological resources or human remains would be less than significant.

## Mitigation Measures

## Mitigation Measure CUL-1: Conduct Pre-Construction Cultural Resources Sensitivity Training.

The City or its contractor shall coordinate with the Yoche Dehe Wintun Nation to provide preconstruction cultural sensitivity training for all construction personnel who will be involved in ground-disturbing construction activities.

## Mitigation Measure CUL-2: Measures to Protect Subsurface Cultural Resources.

In the event that any prehistoric or historic-era subsurface archaeological features or deposits, including locally darkened soil ("midden"), that could conceal cultural deposits, are discovered during project construction, all ground-disturbing activity within 100 feet of the resources shall
be halted and a qualified professional archaeologist shall be retained to assess the significance of the find. If the find is determined to be significant by the qualified archaeologist (i.e., because it is determined to constitute either an historical resource or a unique archaeological resource), the archaeologist shall develop appropriate procedures to protect the integrity of the resource and ensure that no additional resources are affected. Procedures could include but would not necessarily be limited to preservation in place, archival research, subsurface testing, or contiguous block-unit excavation and data recovery.

If the archaeologist determines that some or all of the affected property qualifies as a Native American Cultural Place, including a Native American sanctified cemetery, place of worship, religious or ceremonial site, or sacred shrine (Public Resources Code §5097.9) or a Native American historic, cultural, or sacred site, that is listed or may be eligible for listing in the California Register of Historical Resources pursuant to Public Resources Code §5024.1, including any historic or prehistoric ruins, any burial ground, any archaeological or historic site (Public Resources Code §5097.993), the archaeologist shall recommend to the City of Davis potentially feasible procedures that would preserve the integrity of the site or minimize impacts on it.

## Mitigation Measure CUL-3: Measures to Protect Human Burials and Associated Features.

California law recognizes the need to protect Native American human burials, skeletal remains, and items associated with Native American burials from vandalism and inadvertent destruction. The procedures for the treatment of Native American human remains are contained in California Health and Safety Code Sections 7050.5 and 7052 and California Public Resources Code Section 5097. If human remains are discovered during any demolition/construction activities, potentially damaging ground-disturbing activities in the area of the remains shall be halted immediately, and the City of Davis shall notify the Yolo County coroner and the Native American Heritage Commission (NAHC) immediately, according to Section 5097.98 of the State Public Resources Code and Section 7050.5 of California's Health and Safety Code. If the remains are determined by the NAHC to be Native American, the guidelines of the NAHC shall be adhered to in the treatment and disposition of the remains. The City of Davis shall also retain a professional archaeologist with Native American burial experience to conduct a field investigation of the specific site and consult with the Most Likely Descendant (MLD), if any, identified by the NAHC. Following the coroner's and NAHC's findings, the archaeologist, and the NAHC-designated MLD shall determine the ultimate treatment and disposition of the remains and take appropriate steps to ensure that additional human interments are not disturbed. The responsibilities for acting upon notification of a discovery of Native American human remains are identified in California Public Resources Code Section 5097.94.

## References

California Department of Transportation (Caltrans), 2018. Section 106 Compliance-Screened Undertaking for Richards Boulevard/Interstate-80 Interchange Improvements Project in the City of Davis, Yolo County (EA: 03-0H360; EFIS Project ID: 0315000148). Prepared by ESA for Caltrans District 3. August 9, 2018.

## Energy

| Issues (and Supporting Information Sources): | Potentially Significant Impact | Less Than Significant with Mitigation Incorporated | Less Than Significant Impact | No Impact |
| :---: | :---: | :---: | :---: | :---: |
| VI. ENERGY - Would the project: |  |  |  |  |
| a) Result in potentially significant environmental impact due to wasteful, inefficient, or unnecessary consumption of energy resources, during project construction or operation? | $\square$ | $\square$ | Х | $\square$ |
| b) Conflict with or obstruct a state or local plan for renewable energy or energy efficiency? | $\square$ | $\square$ | $\square$ | Х |

## Discussion

a) The proposed project would require construction activities, including but not limited to asphalt and concrete removal, grubbing, cut-and-fill activities, and grading. Construction energy consumption would result primarily from transportation fuels (e.g., diesel and gasoline) used for haul trucks, heavy-duty construction equipment, and construction workers traveling to and from the project limits. Project construction would be performed by professional contractors and would not be anticipated to result in inefficient or unnecessary consumption of fuel resources. While construction may occur during nighttime hours, electricity consumption for construction lighting would not be anticipated to have an adverse impact on available electricity supplies and infrastructure. Therefore, no impacts on electricity supply and infrastructure associated with short-term construction activities would occur. Natural gas is not anticipated to be consumed in any substantial quantities during construction of the proposed project. Therefore, project impacts on energy and gas associated with construction activities would be less than significant.

Operation of the proposed project would not result in changes to the existing land use (e.g., transportation facility) within the project limits and is not anticipated to increase the demand for electricity or natural resources. Therefore, operational impacts on energy and gas would be less than significant.
b) The proposed project is a transportation project that would improve an existing interchange. The proposed project does not propose any new structures that would subject to the goals and policies of the City's General Plan specific to development and new construction of buildings. In addition, the proposed project would support regional and statewide efforts to improve transportation energy efficiency and reduce transportation energy consumption with respect to private automobiles. The proposed project would be consistent with and support the goals and benefits of SACOG's MTP/SCS, which seeks to maximize mobility and accessibility for all people and goods in the region. Therefore, the proposed project would not conflict with or obstruct a state or local plan for renewable energy or energy efficiency, and there would be no impact.

## References

City of Davis, 2007. City of Davis General Plan. Available: https://www.cityofdavis.org/city-hall/ community-development-and-sustainability/planning-and-zoning/general-plan.

Fehr \& Peers, 2018. Transportation Analysis Report, Interstate 80 / Richards Boulevard Interchange. Prepared for City of Davis. June 2018.

Sacramento Area Council of Governments (SACOG), 2019. 2020 Metropolitan Transportation Plan/Sustainable Communities Strategy, Adopted November 18, 2019. Available: https://www.sacog.org/2020-metropolitan-transportation-plansustainable-communitiesstrategy.

## Geology and Soils

| Issues (and Supporting Information Sources): |  | Potentially Significant Impact | Less Than Significant with Mitigation Incorporated | Less Than Significant Impact | No Impact |
| :---: | :---: | :---: | :---: | :---: | :---: |
| VII. GEOLOGY AND SOILS - Would the project: |  |  |  |  |  |
| a) Directly or indirectly cause potential substantial adverse effects, including the risk of loss, injury, or death involving: |  |  |  |  |  |
|  | i) Rupture of a known earthquake fault, as delineated on the most recent Alquist-Priolo Earthquake Fault Zoning Map issued by the State Geologist for the area or based on other substantial evidence of a known fault? Refer to Division of Mines and Geology Special Publication 42. | $\square$ | $\square$ | $\square$ | 】 |
|  | ii) Strong seismic ground shaking? | $\square$ | $\square$ | $\square$ | Х |
|  | iii) Seismic-related ground failure, including liquefaction? | $\square$ | $\square$ | 区 | $\square$ |
|  | iv) Landslides? | $\square$ | $\square$ | Х | $\square$ |
| b) $R$ | Result in substantial soil erosion or the loss of topsoil? | $\square$ | $\square$ | Х | $\square$ |
| c) | Be located on a geologic unit or soil that is unstable, or that would become unstable as a result of the project, and potentially result in on- or off-site landslide, lateral spreading, subsidence, liquefaction, or collapse? | $\square$ | Х | $\square$ | $\square$ |
| d) <br> T | Be located on expansive soil, as defined in Table 18-1-B of the Uniform Building Code (1994), creating substantial direct or indirect risks to life or property? | $\square$ | Х | $\square$ | $\square$ |
| e) | Have soils incapable of adequately supporting the use of septic tanks or alternative waste water disposal systems where sewers are not available for the disposal of waste water? | $\square$ | $\square$ | $\square$ | Х |
| f) | Directly or indirectly destroy a unique paleontological resource or site or unique geologic feature? | $\square$ | Х | $\square$ | $\square$ |

## Discussion

a.i) There are no faults mapped in the immediate vicinity of the project site. The nearest faults include the Late Quaternary age Vaca fault approximately 18 miles to the westsouthwest and the Holcene-latest Pleistocene age Dunnigan Hills fault approximately 8.5 miles to the northwest. The project site is not located within an Alquist-Priolo earthquake fault zone (Crawford \& Associates, 2018). There would be no impact related to rupture of a known earthquake fault.
a.ii) The project area is not located within an Alquist-Priolo earthquake fault zone and surface evidence of faulting has not been observed (Crawford \& Associates, 2018). There would be no impact related to seismic ground shaking.
a.iii) Liquefaction can occur when saturated, loose- to medium-dense granular soils (generally within 50 feet of the surface), or specifically defined cohesive soils are subjected to ground shaking. Based on the medium-stiff to hard fine-grained silt/clay, medium-dense
coarse to fine-grain sand, and groundwater conditions observed on the project site during the geotechnical investigation conducted for the proposed project, the potential for liquefaction is expected to be low (Crawford \& Associates, 2018). In addition, all projectrelated work would be designed and constructed in accordance with the requirements of all applicable federal, state, and local safety regulations. Consequently, this impact would be less than significant.
a.iv) No significant erosion of the existing embankment fills, cut slopes, unlined drainage ditches, or swales in the project area were observed during the geotechnical investigation conducted for the proposed project (Crawford \& Associates, 2018). In addition, all project-related work would be designed and constructed in accordance with the requirements of all applicable federal, state, and local safety regulations. Consequently, the likelihood of slope failure is low, and this impact would be less than significant.
b) Construction of the proposed project would involve grading and excavation activities that may result in short-term wind and water driven erosion of soils. The project's required compliance with the National Pollutant Discharge Elimination System (NPDES) permit, Storm Water Pollution Prevention Plan (SWPPP), and the City's grading permit would ensure that necessary erosion control measures are applied to the project site during preparation and construction activities. As a result, impacts associated with soil erosion would be less than significant.
c, d) The United States Department of Agriculture (USDA) Web Soil Survey shows the surface soils on the project site as Sycamore Silt Loam and Sycamore Silty Clay Loam Both units are underlain by Silt Loam. These soils are indicated to have generally moderate to high shrink-swell potential, low to moderate corrosion potential to concrete, moderate to high corrosion potential to steel, and low to moderate bearing capacity (Crawford \& Associates, 2018). The geotechnical study prepared for the proposed project concluded that the site is adequately stable for the planned improvements provided that recommendations presented in the geotechnical study are followed, including retaining a Geotechnical Engineer of Record to review and provide comments on the civil plans and specifications prior to construction, and to monitor grading, foundation excavations (box culverts, retaining walls), wall backfill, and subgrade, aggregate based, and pavement placement and compaction. The proposed project would be designed and constructed in accordance with the requirements of all applicable federal, state, and local safety regulations (Crawford \& Associates, 2018). Compliance with these regulations and implementation of Mitigation Measure GEO-1 (see page 72) would ensure that potentially significant impacts related to soil stability would be less than significant.
e) The project does not propose the use or construction of septic tanks or alternative wastewater disposal systems. There would be no impact.
f) The project site been subject to substantial disturbance associated with construction of the existing interchange, and there is a low likelihood that paleontological resources or unique geological features would be encountered during construction of the proposed project. Despite this low likelihood, however, subsurface paleontological resources or
unique geological features could be damaged by ground-disturbing activities associated with construction of the proposed project. Implementation of Mitigation Measure GEO-2 would ensure that potentially significant impacts would be less than significant.

## Mitigation Measures

## Mitigation Measure GEO-1: Implement Recommendations Contained in the Site-Specific Geotechnical Report.

The City or its designated consultant shall retain a Geotechnical Engineer of Record to review and provide comments on the project plans and specifications prior to construction. The recommendations of the Geotechnical Engineer of Record shall be incorporated in the final design and construction of the project. Recommendations could include, but not be limited to, monitoring of grading, foundation excavations (box culverts, retaining walls), wall backfill, and subgrade, aggregate based, and pavement placement and compaction.

## Mitigation Measure GEO-2: Measures to Protect Paleontological Resources.

In the event that any suspected paleontological resources (e.g., fossilized remains) or unique geological features are discovered during project construction, all ground-disturbing activity within 100 feet of the resources shall be halted and a qualified paleontologist shall be retained to assess the significance of the find. If the find is determined to be significant, the paleontologist shall develop appropriate procedures to protect the integrity of the resource and ensure that no additional resources are affected. Procedures could include but would not necessarily be limited to preservation in place, archival research, subsurface testing, or data recovery.

## References

Crawford \& Associates, Inc., 2018. Draft Geotechnical Design and Materials Report, I-80 Richards Interchange T.O. \#10. Prepared for Mark Thomas. November 15, 2018.

## Greenhouse Gas Emissions

| Issues (and Supporting Information Sources): | Potentially Significant Impact | Less Than Significant with Mitigation Incorporated | Less Than Significant Impact | No Impact |
| :---: | :---: | :---: | :---: | :---: |
| VIII. GREENHOUSE GAS EMISSIONS Would the project: |  |  |  |  |
| a) Generate greenhouse gas emissions, either directly or indirectly, that may have a significant impact on the environment? | $\square$ | $\square$ | Х | $\square$ |
| b) Conflict with an applicable plan, policy or regulation adopted for the purpose of reducing the emissions of greenhouse gases? | $\square$ | $\square$ | Х | $\square$ |

## Discussion

The term greenhouse gas (GHG) is used to describe atmospheric gases that absorb solar radiation and subsequently emit radiation in the thermal infrared region of the energy spectrum, trapping heat in the Earth's atmosphere. These gases include carbon dioxide $\left(\mathrm{CO}_{2}\right)$, methane $\left(\mathrm{CH}_{4}\right)$, nitrous oxide ( $\mathrm{N}_{2} \mathrm{O}$ ), and water vapor, among others. $\mathrm{CO}_{2}$ is the most important GHG , so amounts of other gases are expressed relative to $\mathrm{CO}_{2}$, using a metric called "carbon dioxide equivalent" $\left(\mathrm{CO}_{2} \mathrm{e}\right)$. The global warming potential (GWP) of $\mathrm{CO}_{2}$ is assigned a value of 1 , and the warming potential of other gases is assessed as multiples of $\mathrm{CO}_{2}$. For example, the 2007 International Panel on Climate Change (IPCC) Fourth Assessment Report calculates the GWP of $\mathrm{CH}_{4}$ as 25 and the GWP of $\mathrm{N}_{2} \mathrm{O}$ as 298, over a 100 -year time horizon. ${ }^{3}$ Generally, estimates of all GHGs are summed to obtain total emissions for a project or given time period, usually expressed in metric tons ( $\mathrm{MTCO}_{2} \mathrm{e}$ ), or million metric tons ( $\mathrm{MMTCO}_{2} \mathrm{e}$ ). ${ }^{4}$

Emissions of GHGs have the potential to adversely affect the environment because such emissions contribute, on a cumulative basis, to global climate change. Although the emissions of one single project will not cause global climate change, GHG emissions from multiple projects throughout the world could result in a cumulative impact with respect to global climate change.

Legislation and executive orders on the subject of climate change in California have established a statewide context for and a process for developing an enforceable statewide cap on GHG emissions. Given the nature of environmental consequences from GHGs and global climate change, CEQA requires that lead agencies consider evaluating the cumulative impacts of GHGs, even relatively small (on a global basis) additions.

The proposed project would generate direct and indirect GHG emissions that contribute to global warming and climate change impacts. Although the contribution from an individual project may be minor, the cumulative impact can be substantial. While YSAQMD, the local agency in charge

[^2]of air quality considerations in Yolo County, has not established specific standard levels applicable to GHG emissions, CEQA still requires an evaluation of GHGs.

The California Global Warming Solution Act of 2006 (AB 32) was adopted establishing a state goal of reducing California's GHG emissions to 1990 levels by the year 2020. A subsequent Executive Order signed by the Governor establishes an additional target for State agencies of 80 percent below 1990 levels by 2050.

In June 2010, the City of Davis adopted a Climate Action and Adaptation Plan which included local reduction targets for greenhouse gas emissions. The targets are based on a range that uses the State targets as a minimum goal and identifies deeper reductions as the desired outcome. For example, the 2020 target reduction ranged from the State target of 1990 GHG emission levels to the desired target of 28 percent below 1990 levels. The 2050 emission targets ranged from the State target of 80 percent below 1990 levels to the desired outcome of being carbon neutral.

Recently, GHG and climate change impacts have been a major focus of federal and state regulatory agencies. One of the main strategies in the Climate Action Program (CAP) to reduce GHG emissions is to make California's transportation system more efficient. The highest levels of $\mathrm{CO}_{2}$ come from mobile sources, such as automobiles, and occur at stop-and-go speeds (zero to 25 mph ) and speeds over 55 mph . The most severe $\mathrm{CO}_{2}$ emissions occur from zero to 25 mph . The intent of a highway design project is to relieve traffic congestion by enhancing operations and improving travel times, thus reducing GHG emissions, particularly $\mathrm{CO}_{2}$.

Many studies show that an increase in traffic volume is related to higher overall $\mathrm{CO}_{2}$ emissions. Traffic volumes are expected to increase under future conditions; however, operation of the project would increase traffic speed and flow and decrease congestion. With these improvements, $\mathrm{CO}_{2}$ emissions are expected to decrease from the vehicles utilizing the roadway.
a) Implementation of the proposed project would result in short-term construction and longterm operational GHG emissions. GHG emissions generated by the proposed project would predominantly be in the form of $\mathrm{CO}_{2}$. While emissions of other GHGs such as methane $\left(\mathrm{CH}_{4}\right)$ and nitrous oxide $\left(\mathrm{N}_{2} \mathrm{O}\right)$ are important with respect to global climate change, the emission levels of these GHGs for the sources associated with project activities are nominal compared with $\mathrm{CO}_{2}$ emissions, even considering their higher global warming potential. Therefore, all GHG emissions for are reported as $\mathrm{CO}_{2}$.

Construction-related emissions would result from mobile-source exhaust from worker commute trips, haul truck trips, and equipment used on site (e.g., pavers, lifts). Long-term operational emissions would be associated with vehicular trips within the proposed project corridor.

As previously discussed in the Air Quality section of this initial study, construction emissions were estimated for the proposed project using default equipment inventories provided in RCEM, project construction scheduling information provided by the City and emissions factors from the EMFAC 2014 and OFFROAD models. GHG emissions generated from construction-related activities for the proposed project are presented
below in Table GHG-1. As shown in Table GHG-1, construction of the proposed project would result in a total of $126 \mathrm{MTCO}_{2}$ e per year. As previously stated, given the enormity of GHG emissions worldwide, the contributions of one project, such as the proposed project, are negligible.

| TABLE GHG-1 <br> Summary of Project Construction GHG Emissions |  |
| :---: | :---: |
| Construction Activity | $\mathrm{CO}_{2} \mathrm{e}$ (MT/phase) |
| Clearing/Grubbing | 21 |
| Grading/Excavation | 3091 |
| Drainage/Utilities | 626 |
| Paving | 53 |
| Total (tons/project) | 3,792 |
| Amortized Construction Emissions b | 126 |
| NOTES: |  |
| Totals may not add up exactly due to rounding in the modeling calculations. |  |
| For the purposes of the analysis, construction emissions were amortized over 30 years in accordance with industry standards. |  |
| $\mathrm{CO}_{2} \mathrm{e}=$ carbon dioxide equivalent; $\mathrm{MT}=$ metric ton |  |
| SOURCE: ESA, 2019. |  |

GHG emissions for baseline (existing) and future with project conditions was estimated utilizing Caltrans' CT-EMFAC, results of the emissions analysis are provided in
Table GHG-2. The results of the GHG emission analysis show that future $\mathrm{CO}_{2}$ emissions with the proposed project will decrease from baseline (existing) conditions. Operation of the proposed project would improve air quality throughout the Basin and would result in a less-than-significant impact.

Table GHG-2
Summary of Net Increase in GHG Emissions Associated with the Proposed Project

| Proposed Project | CO $_{2}$ Emissions (MT/Year) |
| :--- | ---: |
| Existing/Baseline [2016] | 130,025 |
| Open to Traffic [2022] | With Project |
| Net Change in Emissions (With Project minus Baseline) |  |
| 20-Year Horizon/Design-Year [2042] | 123,427 |
| Net Change in Emissions (With Project minus Baseline) |  |

NOTES:
$\mathrm{CO}_{2}$ emissions derived from CT-EMFAC were adjusted based on CARB's off-model adjustment factors for $\mathrm{CO}_{2}$. $\mathrm{CO}_{2}=$ carbon dioxide; $\mathrm{MT}=$ metric ton

SOURCE: ESA, 2021.
b) The proposed project is located in the City of Davis within the County of Yolo and is included in the Sacramento Area Council of Governments (SACOG) 2020 Metropolitan Transportation Plan/Sustainable Communities Strategy (MTP/SCS). The current 2020 MTP/SCS was adopted in November 2019.

In order to support attainment of air quality standards, the MTP/SCS must be analyzed as an overall package via technical modeling to verify that its implementation would meet federal air quality requirements. In addition, the MTP/SCS must achieve regional greenhouse gas emissions reduction targets set by the CARB. The MTP/SCS must demonstrate a reduction in GHG emissions via technical modeling of the forecasted land use pattern and supporting transportation network designed to serve the regional transportation needs.

As discussed under item a) above, the total GHG emissions associated with the proposed project would not be considered substantial. Additionally, the proposed project is included in SACOG’s 2020 MTP/SCS, which demonstrates a reduction in GHG emissions via technical modeling of the forecasted land use pattern and supporting transportation network designed to serve the regional transportation needs. For these reasons, the proposed project would not conflict with the reduction goals established by AB 32. As a result, this impact would be less than significant.

## References

City of Davis, 2007. City of Davis General Plan. Available: https://www.cityofdavis.org/city-hall/ community-development-and-sustainability/planning-and-zoning/general-plan.
—_, 2010. City Council Staff Report: Climate Action and Adaptation Plan Adoption. June 2010.

Fehr \& Peers, 2018. Transportation Analysis Report, Interstate 80 / Richards Boulevard Interchange. Prepared for City of Davis. June 2018.

International Panel on Climate Change (IPCC), 2007. IPCC Fourth Assessment Report: Climate Change 2007 (AR4): The Physical Science Basis. Contribution of Working Group I to the Fourth Assessment Report of the Intergovernmental Panel on Climate Change. September 2007.

Sacramento Area Council of Governments (SACOG), 2019. 2020 Metropolitan Transportation Plan/Sustainable Communities Strategy, Adopted November 18, 2019. Available: https://www.sacog.org/2020-metropolitan-transportation-plansustainable-communitiesstrategy.

## Hazards and Hazardous Materials

| Issues（and Supporting Information Sources）： |  | Potentially <br> Significant Impact | Less Than Significant with Mitigation Incorporated | Less Than Significant Impact | No Impact |
| :---: | :---: | :---: | :---: | :---: | :---: |
| IX． | HAZARDS AND HAZARDOUS MATERIALS－ Would the project： |  |  |  |  |
| a） | Create a significant hazard to the public or the environment through the routine transport，use，or disposal of hazardous materials？ | $\square$ | $\square$ | 区 | $\square$ |
| b） | Create a significant hazard to the public or the environment through reasonably foreseeable upset and accident conditions involving the release of hazardous materials into the environment？ | $\square$ | Х | $\square$ | $\square$ |
| c） | Emit hazardous emissions or handle hazardous or acutely hazardous materials，substances，or waste within one－quarter mile of an existing or proposed school？ | $\square$ | $\square$ | 区 | $\square$ |
| d） | Be located on a site which is included on a list of hazardous materials sites compiled pursuant to Government Code Section 65962.5 and，as a result， would it create a significant hazard to the public or the environment？ | $\square$ | $\square$ | $\square$ | Х |
| e） | For a project located within an airport land use plan or，where such a plan has not been adopted，within two miles of a public airport or public use airport， would the project result in a safety hazard or excessive noise for people residing or working in the project area？ | $\square$ | $\square$ | $\square$ | 】 |
| f） | Impair implementation of or physically interfere with an adopted emergency response plan or emergency evacuation plan？ | $\square$ | $\square$ | Х | $\square$ |
| g） | Expose people or structures，either directly or indirectly， to a significant risk of loss，injury，or death involving wildland fires？ | $\square$ | $\square$ | $\square$ | 区 |

## Discussion

a）Construction activities associated with the proposed project would involve the transport and use of limited quantities of fuels，lubricants，oils，solvents，and other potentially hazardous materials at the project site for the purposes of construction and equipment maintenance．The accidental release of hazardous materials due to the improper transport and handling of the common hazardous materials associated with the construction of the proposed could potentially occur．However，the transport，storage，and use of hazardous materials is regulated through various federal，state，and local laws and policies，enforced by an array of departments at local，municipal，and state levels．The use of hazardous materials associated with construction activities for their intended purposes in compliance with these regulations would therefore not represent a significant risk to public health or the environment，and this impact would be less than significant．

Operation of the completed interchange project would not result in material changes or increases related to the transport，storage，use，and／or disposal hazardous materials． Operation of the completed interchange project would occur in compliance with existing
hazardous materials regulations, and operational impacts related to the transport, use or disposal of hazardous materials would be less than significant.
b) Crawford \& Associates, Inc. prepared a Draft Initial Site Assessment (ISA) for the proposed project (Crawford \& Associates, 2018). The purpose of the ISA was to identify and provide a preliminary assessment of the potential impacts of known or potential Recognized Environmental Conditions (RECs) ${ }^{5}$ within the project area that may influence design and construction of the project. Crawford \& Associates performed the following tasks for preparation of the ISA.

- Reviewed geologic and groundwater conditions;
- Initiated a request with GeoSearch to search federal, state, and local regulatory agency databases to determine whether areas of environmental concern exist on or near the project site. Search distances ranged between $1 / 8$ and one mile from the project site, depending on the database;
- Reviewed available information to assess past and present activities conducted within the project study area and assessed the potential for hazardous materials impact;
- Reviewed historical aerial photographic coverage and topographic map coverage of the project site and vicinity for indications of potential sources of contamination;
- Reviewed the State of California's GeoTracker and EnviroStor websites for sites in the project vicinity;
- Conducted limited reconnaissance of the project site and vicinity on February 15, 2018; and
- Contracted with National Analytical Laboratory, Inc. (NAL) to perform a survey of the I-80 bridge for the presence of asbestos containing construction material (ACCM) and lead-containing material (LCM).

Based on the records reviewed and the site reconnaissance performed for the ISA, Crawford \& Associates made the following observations:

- The database records search did not identify any Recognized Environmental Conditions (RECs) or historical RECs (HRECs) that have potentially impacted shallow soil within the project site.
- A former service station in the vicinity of the eastern end of the I-80 off-ramp (HREC) was identified from review of aerial photographs.

[^3]- A REC was identified with respect to potential for petroleum hydrocarbons and volatile organic compounds (VOCs) in groundwater beneath the overpass structure, where proposed construction activities may encounter groundwater.
- Site reconnaissance identified a concrete box culvert that could potentially contain asbestos and subgrade transformers that may be impacted by the northward expansion of the I-80 bridge.
- Site reconnaissance identified guardrails and traffic signs mounted on treated wood posts at the I-80 bridge, on the Richards Boulevard overpass, at the westbound I-80 on and off-ramps for Richards Boulevard, and the Olive Drive off-ramp.
- Shallow soil along the proposed alignment of the new westbound I-80 on- and offramps has been tested for aerially deposited lead (ADL). ADL is reported below concentrations that require additional testing or special handling; this soil may be reused without restriction. Soil adjacent to Richards Boulevard between Olive Drive and the railroad underpass, and in the vicinity of the Olive Drive exit, has the potential for ADL impact.
- A REC was identified with respect to asbestos-containing construction material (ACCM) in the Putah Creek box culvert.
- A REC was identified with respect to lead-containing material (LCM) on the westbound I-80 bridge.

Based on the public records, historical aerial photographs, and historical aerial photographs reviewed for this project, and the site reconnaissance performed on February 15, 2018, Crawford \& Associates made the following recommendations:

- Fog line and lane striping material on Richards Boulevard, the Olive Drive off-ramp, the eastbound I-80 off-ramp, and the I-80 bridge should be evaluated for heavy metals (if they will be impacted by proposed construction activities, and the material will not be recycled).
- Groundwater upgradient of the overpass has been impacted by petroleum hydrocarbons and VOCs, which may have migrated beneath the overpass. If future construction activities include advancing borings (i.e., either by means of cast-in-drilled-holes or predrilling holes to assist driven piles) into groundwater, testing of extracted saturated soil and groundwater should be performed to minimize worker exposure and to properly classify the extracted material for disposal.
- Treated wood waste (TWW) will need to be handled and disposed of in accordance with alternative management standards (AMS) protocol.
- Soil adjacent to the Olive Drive exit and adjacent to Richards Boulevard between Olive Drive and the railroad underpass should be tested for the presence of ADL at concentrations in excess of the hazardous waste threshold if soil in these areas would be disturbed by proposed work.

Based on the findings of the ISA, without implementation of appropriate measures, construction of the proposed project could create a significant hazard to the public or the environment through reasonably foreseeable upset and accident conditions involving the
release of hazardous materials into the environment. Hazardous materials associated with the project site and vicinity identified in the ISA include, but are not limited to, contaminated groundwater, treated wood waste, asbestos-containing materials, aerially deposited lead, and lead-containing material, and heavy metals in paint and thermoplastic materials used for traffic striping. Consequently, impacts related to exposure or release of hazardous materials during project construction are potentially significant.

Implementation of Mitigation Measures HAZ-1, HAZ-2, and HAZ-3 (see page 81) would ensure there would not be a significant hazard to the public or the environment through reasonably foreseeable upset and accident conditions involving the release of hazardous materials into the environment and reduce the potentially significant impact to a less-than-significant level.

The project site is not located within one-quarter mile of an existing or proposed school. As discussed in item a) above, the transport, storage, and use of hazardous materials is regulated through various federal, state, and local laws and policies, enforced by an array of departments at local, municipal, and state levels. The use of hazardous materials associated with construction activities for their intended purposes in compliance with these regulations would therefore not represent a significant risk to public health or the environment, including school sites and attending students. This impact would be less than significant.
d) The ISA prepared for the proposed project included an extensive database records search for the project site and properties within a one-mile radius of the project site (Crawford \& Associates, 2018). Search distances ranged between $1 / 8$ and one mile from the project site, depending on the database. The ISA concluded that the project site was not identified in any of the databases searched, and the project site is not located on a site which is included on a list of hazardous materials sites compiled pursuant to Government Code Section 65962.5 (i.e., Cortese List). There would be no impact related to this significance criterion.
e) The Sacramento International Airport is located approximately 12 miles to the northeast of the project site, the Yolo County Airport is located approximately 7 miles to the northwest of the project site, and the University Airport is located approximately 2.5 miles west of the project site. The proposed project is not located within the airport influence areas of any airport. There would be no impact related to this significance criterion.
f) The proposed project would relieve existing congestion and reduce conflicts between bicyclists, pedestrians, and vehicles. Emergency access through the intersections would improve from conditions prior to the modifications.

A Transportation Management Plan (TMP) would be developed for use during project construction. The TMP would utilize strategies described in the California Manual of Traffic Control Devices and Caltrans Transportation Management Plan Guidelines. The TMP would direct the process and procedures for dissemination of information to the public and motorists, provide guidance for implementation of incident management,
describe construction strategies for traffic handling and guiding traffic through work zones, address traffic demand management during construction, and describe and direct the implementation of alternate routes or detours. Implementation of the TMP would ensure that impacts related to emergency access during construction of the proposed project would be less than significant.
g) The project site comprises an existing interchange and adjacent roadways and structures in an urban environment in the City of Davis. There are no wildlands within or adjacent to the project site. Construction and operation of the proposed project would not expose people or structures, either directly or indirectly, to a significant risk of loss, injury, or death involving wildland fires. There would be no impact related to this significance criterion.

## Mitigation Measures

## Mitigation Measure HAZ-1: Safe Removal and Proper Disposal of Hazardous Materials.

The City shall ensure, through the enforcement of contractual obligations, that work plans address procedures for the safe testing, removal, and proper disposal of hazardous materials that could be encountered and released with implementation of the project, including, but not limited to, treated wood waste, asbestos-containing materials, aerially deposited lead, and leadcontaining material, and heavy metals in paint and thermoplastic materials used for traffic striping, Hazardous materials shall be tested, handled, and disposed of in accordance with appropriate federal, state, and local regulations.

## Mitigation Measure HAZ-2: Contamination of Soil and/or Groundwater.

During construction activities for the proposed project, if contaminated soil and/or groundwater are encountered or suspected contamination is encountered, work shall be stopped in the suspected area of contamination and the type and extent of the contamination be identified. If necessary, a remediation plan shall be implemented in conjunction with continued construction of the proposed project.

## Mitigation Measure HAZ-3: Prepare and Implement a Health and Safety Plan (HASP).

The City shall ensure preparation and implement a Health and Safety Plan (HASP) that describes appropriate procedures to follow in the event that contaminated soil or groundwater or other hazardous materials or conditions are encountered during construction activities. Any unknown substances shall be tested, handled and disposed of in accordance with appropriate federal, state and local regulations.

## References

Crawford \& Associates, Inc., 2018. Draft Initial Site Assessment, I-80 Richards Interchange T.O. \#10. Prepared for Mark Thomas. August 21, 2018.

## Hydrology and Water Quality

| Issues（and Supporting Information Sources）： |  | Potentially <br> Significant Impact | Less Than Significant with Mitigation Incorporated | Less Than Significant Impact | No Impact |
| :---: | :---: | :---: | :---: | :---: | :---: |
| X． | HYDROLOGY AND WATER QUALITY－ Would the project： |  |  |  |  |
| a） | Violate any water quality standards or waste discharge requirements or otherwise substantially degrade surface or ground water quality？ | $\square$ | $\square$ | Х | $\square$ |
| b） | Substantially decrease groundwater supplies or interfere substantially with groundwater recharge such that the project may impede sustainable groundwater management of the basin？ | $\square$ | $\square$ | Х | $\square$ |
| c） | Substantially alter the existing drainage pattern of the site or area，including through the alteration of the course of a stream or river or through the addition of impervious surfaces，in a manner which would： |  |  |  |  |
|  | i）result in substantial erosion or siltation on－or off－ site； | $\square$ | $\square$ | 区 | $\square$ |
|  | ii）substantially increase the rate or amount of surface runoff in a manner which would result in flooding on－or offsite； | $\square$ | $\square$ | Х | $\square$ |
|  | iii）create or contribute runoff water which would exceed the capacity of existing or planned stormwater drainage systems or provide substantial additional sources of polluted runoff； or | $\square$ | $\square$ | Х | $\square$ |
|  | iv）impede or redirect flood flows？ | $\square$ | $\square$ | Х | $\square$ |
| d） | In flood hazard，tsunami，or seiche zones，risk release of pollutants due to project inundation？ | $\square$ | $\square$ | $\square$ | 区 |
| e） | Conflict with or obstruct implementation of a water quality control plan or sustainable groundwater management plan？ | $\square$ | $\square$ | 区 | $\square$ |

## Environmental Setting

The project site is located within the City of Davis，within a largely developed area in the southeastern portion of the City．The area has a generally flat or nearly flat topography，although there is an incline along Richards Boulevard to cross over the interstate．In the greater vicinity of the project site，the City lies on a relatively flat alluvial plain．Land uses that surround the project site include commercial，industrial，light industrial，residential，and agriculture．

The project site is located within what is known as the Great Valley geomorphic province．The geology of the Great Valley geomorphic province is classified by thick Jurassic through Holocene－aged sedimentary deposits．The majority of Davis consists of alluvial sediments from the Putah Creek Plain below which are metamorphic and igneous rocks．Soils in the area generally have a high proportion of silt and clay and as a result are only moderately or slowly permeable，which hinders drainage and groundwater recharge（USDA，2018）．

The proposed project is located within the Yolo Subbasin of the Sacramento Valley Groundwater Basin（Subbasin 5－021．67）of the Sacramento Valley aquifer system（CDWR，2004）．Aquifers in this area generally consist of younger alluvium，older alluvium，and the Tehama Formation which
can cumulatively range from a few hundred up to 3,000 feet. Groundwater in the subbasin is a sodium magnesium, calcium magnesium, or magnesium bicarbonate type. The geologic structure impedes subsurface groundwater flow from west to east. Subsurface groundwater outflow sometimes occurs from the Yolo subbasin into the Solano subbasin to the south. Subsurface outflow and inflow may also occur beneath the Sacramento River to the east with the South and North American subbasins. Subsurface groundwater inflow may occur from the west out of the Capay Valley Basin (CDWR, 2004).

Groundwater levels in the subbasin are impacted by periods of drought due to increased groundwater pumping and less surface water recharge, but recover quickly in high precipitation years. Long term trends for the subbasin do not indicate any significant declines except for localized depressions in areas including the City of Davis. The closest well for which groundwater level data were available was located just west of the study area, just south of Richards Boulevard (well number 08N02E15G004M), which indicated that groundwater levels are generally between 40 and 60 feet below ground surface (CDWR, 2018).

The project site and its immediate vicinity is mostly level. Drainage from Richards Boulevard is directed along curbside gutters into various catch basins. Runoff collected in the catch basins is presumably directed towards Putah Creek to the south of the site which is approximately 500 feet away. The Putah Creek watershed is approximately 225,301 acres and bounded by Putah Creek to the south and Cache Creek to the north.

The Federal Emergency Management Agency (FEMA), through its Flood Insurance Rate Maps (FIRMs), documents and delineates the occurrence of floodplains and flood hazard areas in populated areas of the US. In the Project vicinity, FEMA has delineated both the 100-year (i.e., 1 percent annual chance of return) and the 500 -year ( 0.2 percent annual chance of return) floodplain areas. Based on a review of current FEMA maps, the project site is located within Zone X, area of minimal flood potential, and not within any 100- or 500 -year flood zone (FEMA, 2018).

No potentially jurisdictional waters of the U.S. or state were identified within the project site during the biological investigation for the proposed project. The north fork of Putah Creek formerly flowed under Interstate 80 within the project area. The north fork of Putah Creek was diverted to the south fork in 1948 to prevent flooding in the City of Davis. The remnant channel is still visible within the project site but no longer carries water. This remnant channel does not exhibit an ordinary high water mark or show any evidence of flowing water. This remnant channel does not meet the criteria as a jurisdictional water of the U.S. or state (Caltrans, 2019).

Putah Creek is the primary natural drainage that flows south of the project site. Putah Creek ultimately discharges to the Sacramento River. Beneficial uses have not been specifically identified for Putah Creek. However, beneficial uses for the Sacramento River have been identified by the Central Valley RWQCB and include, municipal and domestic supply, irrigation and stock watering, process, power, contact recreation, other non-contact recreation, warm freshwater habitat, cold freshwater habitat, and wildlife habitat (SWRCB, 2017).

## Discussion

a) Project construction would involve removal of existing roadway improvements, widening existing roadways, and other roadway improvements such as creating a separation barrier for a multi-use pathway. During the construction process, these activities would require the use of heavy equipment on-site, including but not limited to grading equipment, excavators, bulldozers, semi-trucks, and paving equipment. Existing drainages would be filled, and re-excavated in their proposed locations. Existing culverts would be removed and, as warranted, re-excavated to support installation of the updated culverts. These activities would disturb existing surface vegetation, as well as surface sediments at the project site. This loosening of surficial soils could result, in the event of a storm, in increased erosion from the project site, as well as an increase in sedimentation downstream. Drainage potential to Putah Creek is enhanced during periods of high to very high stormflows. As a result, construction of the proposed project could result in increased sediment loads downstream. Increased sediment load in either of these areas could meaningfully impact water quality, resulting in water quality degradation.

In addition to sediment, the use of heavy machinery on site would increase potential for construction related water quality pollution during storm events. Construction related oils, greases, paint, fuels, and other potential construction-period water quality pollutants could become entrained in stormwater, resulting in degraded water quality downstream.

Construction of the proposed project would be performed in compliance with the state National Pollutant Discharge Elimination System (NPDES) General Construction Permit and any subsequent General Permit in effect at the time of project construction. The applicable permits authorize stormwater and authorized non-stormwater discharges from City and Caltrans construction activities and would be required prior to commencement of the construction phase of the project. As part of this permit requirement, a Stormwater Pollution Prevention Plan (SWPPP) that follows the City requirements and guidance in the current version of the Caltrans Stormwater Pollution Prevention Plan would be prepared prior to construction consistent with the requirements of the Regional Water Quality Control Board (RWQCB). The SWPPP would incorporate all applicable best management practices (BMPs) to ensure that adequate measures are taken during construction to minimize water quality impacts.

Operation of the proposed project would result in accumulation of oil, grease, and other chemicals used by motor vehicles that may be released during first rains and have the potential to degrade water quality. Operation of the proposed project would require compliance with the City of Davis stormwater program, which operates under a municipal separate storm sewer system (MS4) NPDES permit from the Central Valley RWQCB. This permit requires the City to enforce a post-construction stormwater management program for new development and redevelopment. The City's Stormwater Management Plan includes control measures to improve the quality and reduce the quantity of stormwater runoff to protect receiving waters.

Compliance with the above regulatory requirements would ensure that the project construction and operational impacts to water quality would be less than significant.
b) Project construction activities would include clearing vegetation, grading, excavation, placing embankment, drainage, and paving roadway surfaces. Project construction activities would not interfere with groundwater recharge. The completed project would result in a minor net increase (approximately 0.15 acre) in impervious surface in the project area and would not be anticipated to substantially decrease groundwater supplies or interfere substantially with groundwater recharge such that the project may impede sustainable groundwater management of the basin. The impact would be less than significant.
c) The completed project would result in a minor net increase (approximately 0.15 acre) in impervious surface in the project area and would not substantially alter the existing drainage pattern of the site or area or substantially increase the rate or amount of surface runoff in a manner which would result in flooding onsite or offsite. The proposed project would be designed and operated in compliance with the City of Davis stormwater program, which operates under a MS4 NPDES permit from the Central Valley RWQCB. This permit requires the City to enforce a post-construction stormwater management program for new development and redevelopment. The City's Stormwater Management Plan includes control measures to improve the quality and reduce the quantity of stormwater runoff to protect receiving waters. Compliance with the City's stormwater program would ensure that the proposed project would create or contribute runoff water which would exceed the capacity of existing or planned stormwater drainage systems or provide substantial additional sources of polluted runoff. The impact would be less than significant.
d) The project site is located within Zone X , area of minimal flood potential, and not within any 100 - or 500 -year flood zone (FEMA, 2018). Tsunamis are large waves created by earthquakes, undersea landslides, or volcanic eruptions. Low-lying coastal areas such as tidal flats, marshes, and former bay margins that have been artificially filled are susceptible to inundation. The California Department of Conservation prepares tsunami inundation maps for coastal areas and all populated areas at risk to tsunami within the state based on the maximum tsunami threat for that area, and no areas of Yolo County are at risk from tsunami (California Department of Conservation, 2009). Additionally, the project site is distant from any large water bodies that could create seiche waves and is located in level topography where the risk of mudflow is minimal. Consequently, there would be no impact related to risk of release of pollutants due to project inundation by flood, tsunami, or seiche.
e) As discussed in items a) and c) above, the proposed project would be constructed and operated in compliance with applicable regulations and permit requirements pertaining to water quality, including the requirements of the NPDES General Construction Permit and the City's Stormwater Management Plan. As discussed in item b) above, construction and operation of the proposed project would not impede sustainable groundwater
management of the within the Yolo Subbasin of the Sacramento Valley Groundwater Basin. Consequently, the proposed project would not conflict with or obstruct implementation of a water quality control plan or sustainable groundwater management plan. The impact would be less than significant.

## References

California Department of Conservation, 2009. Tsunami Inundation Map for Emergency Planning Available: https://www.conservation.ca.gov/cgs/tsunami/maps\#County. Accessed August 20, 2019.

California Department of Transportation (Caltrans), 2019. Natural Environment Study (Minimal Impacts), Interstate 80/Richards Boulevard Interchange Improvements Project. April 2019.

California Department of Water Resources (CDWR), 2004. California's Groundwater Bulletin 118, Sacramento Valley Groundwater Basin, South American Subbasin, Last update February 27, 2004.
——, 2018. Water Data Library, Groundwater Levels for Station 384092N1213447W00. Available: http://wdl.water.ca.gov/waterdatalibrary/groundwater/hydrographs/brr_ hydro.cfm?CFGRIDKEY=27854. Accessed June 27, 2018.

Central Valley Regional Water Quality Control Board (CVRWQCB), 2015. Order R5-2015-0023 NPDES No. CAS082597 Waste Discharge Requirements, Municipal Separate Storm Sewer System, 2015.
$\qquad$ , 2016. Water Quality Control Plan, Basin Plan, 2016.

Federal Emergency Management Agency (FEMA), 2018. National Flood Insurance Program: Flood Hazard Mapping. Available: https://www.fema.gov/national-flood-insurance-program-flood-hazard-mapping. Accessed June 28, 2018.

State Water Resources Control Board (SWRCB), 2017. Final 2014/2016 California Integrated Report (Clean Water Act Section 303(d) List/305(b) Report. Available:
https://www.waterboards.ca.gov/water_issues/programs/tmdl/2014_16state_ir_reports/ category5_report.shtml. Accessed June 28, 2018.
U.S. Department of Agriculture (USDA), Department of Conservation, 2018. Web Soil Survey, Sacramento County. Available: https://websoilsurvey.sc.egov.usda.gov/App/Home Page.htm. Accessed June 27, 2018.

## Land Use and Planning

| Issues (and Supporting Information Sources): | Potentially <br> Significant Impact | Less Than Significant with Mitigation Incorporated | Less Than Significant Impact | No Impact |
| :---: | :---: | :---: | :---: | :---: |
| XI. LAND USE AND PLANNING - Would the project: |  |  |  |  |
| a) Physically divide an established community? | $\square$ | $\square$ | $\square$ | Х |
| b) Cause a significant environmental impact due to a conflict with any land use plan, policy, or regulation adopted for the purpose of avoiding or mitigating an environmental effect? | $\square$ | $\square$ | $\square$ | Х |

## Discussion

a) The proposed project would reconstruct and reconfigure the I-80/Richards Boulevard interchange and make other related improvements to relieve existing congestion and reduce conflicts between bicyclists, pedestrians, and vehicles. The project would not install any additional barriers to movement between various segments of the community or physically divide an established community. There would be no impact related to this significance criterion.
b) The project is located within the City of Davis. The City of Davis General Plan and Gateway/Olive Drive Specific Plan together provide the land use designations for the project area (City of Davis, 2007 and 2018). The land southeast of I-80 is designated as Business Park and General Commercial. This area contains multiple retail establishments, including fast food and casual sit-down restaurants, a gas station, auto part store, several hotels, and UC Davis Extension buildings. To the northwest of I-80, the land is mainly designated as Commercial Service, with fast food restaurants, a coffee shop, a gas station, hotel, and other businesses. A small portion of the area (north of the westbound off-ramp) is designated as East Olive Mixed Use and includes apartments, including Cesar Chavez Plaza Permanent Supportive Housing. The proposed project would reconstruct and reconfigure the I-80/Richards Boulevard interchange and make other related improvements to relieve existing congestion and reduce conflicts between bicyclists, pedestrians, and vehicles. The proposed project is consistent with and would not conflict with any land use plan, policy, or regulation adopted for the purpose of avoiding or mitigating an environmental effect. There would be no impact related to this significance criterion.

## References

City of Davis, 2007. City of Davis General Plan. Available: https://www.cityofdavis.org/city-hall/ community-development-and-sustainability/planning-and-zoning/general-plan.
__ , 2018. Gateway/Olive Drive Specific Plan. Available:
https://www.cityofdavis.org/home/showpublisheddocument/608/636669010650870000.

## Mineral Resources



## Discussion

a, b) The proposed project would not use or extract any mineral or energy resources and would not restrict access to known mineral resource areas. The proposed project would not conflict with energy conservation plans, use non-renewable resources in a wasteful manner, or result in the loss of availability of a known mineral resource. There would be no impact.

## Noise

| Issues (and Supporting Information Sources): |  | Potentially Significant Impact | Less Than Significant with Mitigation Incorporated | Less Than Significant Impact | No Impact |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | NOISE - Would the project result in: |  |  |  |  |
| a) | Generation of a substantial temporary or permanent increase in ambient noise levels in the vicinity of the project in excess of standards established in the local general plan or noise ordinance, or applicable standards of other agencies? | $\square$ | $\square$ | Х | $\square$ |
| b) | Generation of excessive groundborne vibration or groundborne noise levels? | $\square$ | $\square$ | Х | $\square$ |
| c) | For a project located within the vicinity of a private airstrip or an airport land use plan or, where such a plan has not been adopted, within two miles of a public airport or public use airport, would the project expose people residing or working in the project area to excessive noise levels? | $\square$ | $\square$ | $\square$ | Х |

## Discussion

a) Noise associated with the proposed project would include noise during demolition and construction and traffic noise after operations commence. Noise associated with construction activities for the proposed project would be temporary and operational noise would be similar to existing noise levels within the project area.

## Construction

During construction of the project, noise from construction activities may intermittently dominate the noise environment in the immediate area of construction. Construction activities under the proposed project would include but not be limited to demolition, grubbing/land clearing, grading/excavation, paving, and pile driving for new pedestrian structures.

Table NOISE-1 summarizes noise levels produced by construction equipment that is commonly used on roadway construction projects. Construction equipment is expected to generate noise levels ranging from 70 to 90 decibels (dB) ${ }^{6}$ at a distance of 50 feet, and noise produced by construction equipment would be reduced over distance at a rate of about 6 dB per doubling of distance.

Noise sensitive land uses may include residential uses, schools, hospitals, nursing homes, religious institutions, libraries, and similar uses. The areas within and immediately adjacent to the project limits are predominantly developed and generally consist of multifamily residences, commercial/retail uses, hotels, and a school extension associated with UC Davis.

[^4]Table NOISE-1
Construction Equipment Noise Levels

| Equipment | Noise Level <br> (dB at $\mathbf{5 0}$ feet) |
| :--- | :---: |
| Bulldozers | 82 |
| Heavy Trucks | 81 |
| Backhoe | 78 |
| Pneumatic Tools | 85 |
| Concrete Pump | 81 |
| Loader | 79 |
| Roller | 80 |
| Compressor | 78 |
| Crane | 81 |
| Drill Rig | 79 |
| Paver | 77 |
| Hoe Ram | 90 |
| SOURCE: FHWA, 2006. |  |

Compliance with construction hours specified by the City would be required. Section 24.02.020 (Noise Limits) of the City's Municipal code allows construction between the hours of 7:00 a.m. and 7:00 p.m. on Mondays through Fridays, and between the hours of 8:00 a.m. and 8:00 p.m. on Saturdays and Sundays, if they meet at least one of the following noise limitations:

1. No individual piece of equipment shall produce a noise level exceeding eighty-three $\mathrm{dBA}^{7}$ at a distance of twenty-five feet. If the device is housed within a structure on the property, the measurement shall be made outside the structure at a distance as close to twenty feet from the equipment as possible.
2. The noise level at any point outside of the property plane of the project shall not exceed eighty-six dBA.
3. The provisions of subdivisions (1) and (2) of this subsection shall not be applicable to impact tools and equipment; provided, that such impact tools and equipment shall have intake and exhaust mufflers recommended by manufacturers thereof and approved by the director of public works as best accomplishing maximum noise attenuation, and that pavement breakers and jackhammers shall also be equipped with acoustically attenuating shields or shrouds recommended by the manufacturers thereof and approved by the director of public works as best accomplishing maximum noise attenuation. In the absence of manufacturer's recommendations, the director of public works may prescribe such means of accomplishing maximum noise attenuation as he or she may determine to be in the public interest.

[^5]4. Construction projects located more than two hundred feet from existing homes may request a special use permit to begin work at 6:00 a.m. on weekdays from June 15 until September 1. No percussion type tools (such as ramsets or jackhammers) can be used before 7:00 a.m. The permit shall be revoked if any noise complaint is received by the police department.
5. No individual powered blower shall produce a noise level exceeding seventy dBA measured at a distance of fifty feet.
6. No powered blower shall be operated within one hundred feet radius of another powered blower simultaneously.
7. On single-family residential property, the seventy dBA at fifty feet restriction shall not apply if operated for less than ten minutes per occurrence.

To minimize construction noise impacts on sensitive land uses adjacent to the project limits, construction noise is regulated by Caltrans Standard Specification Section 14-8.02, "Noise Control," and also by Standard Special Provisions (SSP) S5 310, which states the following:

- Do not exceed 86 dBA Lmax ${ }^{8}$ at 50 feet from the job site activities from 9:00 p.m. to 6:00 a.m.
- Equip an internal combustion engine with the manufacturer-recommended muffler. Do not operate an internal combustion engine on the job site without the appropriate muffler.

Adherence to the City and Caltrans requirements for construction would ensure that the proposed project's short-term construction noise impacts would be less than significant.

## Operation

As previously stated, permanent operational noise would be generated from vehicular traffic utilizing the new interchange. The City does not have specific noise requirements for transportation noise within the City limits. However, under CEQA, the baseline (existing) noise level is used as a comparison to the anticipated project noise level. The assessment of project noise impacts entails identifying the physical area and setting where the potential noise impact could occur and then determining how substantial and perceptible any noise increase would be in the given area. With respect to the community noise assessment, changes in noise levels of less than 3 dBA are generally not discernable to most people, while changes greater than 5 dBA are readily noticeable and would be considered a significant increase.

On behalf of Caltrans District 3 and the City of Davis, ESA staff conducted a noise study for the proposed project that included identifying existing ambient noise levels within the proposed project limits and calculating future noise levels with the proposed project. The analysis was conducted in accordance to Caltrans guidance and requirements (Caltrans, 2019).

[^6]Traffic noise levels were predicted using the Federal Highway Administration (FHWA) Traffic Noise Model Version 2.5. Key inputs to the traffic noise model were the locations of roadways, existing sound walls, ground type, and receptors. Three-dimensional representations of these inputs were developed using computer-aided design drawings, aerials, and topographic contours from the project design plans.

Traffic noise was evaluated under existing conditions future design year (2042) conditions with the project. Loudest-hour traffic volumes, vehicle classification percentages, and traffic speeds under existing (2016) and design year (2042) were used as input into the traffic noise model. The highest average traffic volumes on I-80 and Richards Boulevard are predicted to occur during the evening; therefore, evening peakhour traffic volumes were used in the model.

Existing and future predicted noise levels were computed for a total of 423 noise sensitive land use receivers, including residential communities to the northeast of the interchange. Existing noise levels ranged from 39 to 74 dBA Equivalent Sound Level $\left(\right.$ Leq) ${ }^{9}$ The noise modeling results indicated that predicted traffic noise levels for the future 2042 with-project conditions would range from 40 to 70 dBA Leq. The results show that the proposed project would increase the noise levels at some receiver locations by a maximum of 2 dB . Therefore, the traffic noise volumes associated with the proposed project would not exceed the 3 dB threshold (Caltrans, 2019). In addition, reconstruction of the interchange would shift traffic farther away from a number of noise-sensitive land uses within in the project area, which would result in a decrease in noise levels in the future with project conditions in comparison to the existing conditions. Consequently, operational noise impacts would be less than significant.
b) The project would include demolition, grubbing/land clearing, grading/excavation, paving, and pile driving for new pedestrian structures. Construction would be conducted in accordance with City and Caltrans requirements. Construction vibration would not be anticipated to occur beyond the construction site and would cease to occur once project construction is completed. Consequently, the proposed project would not be anticipated to generate excessive ground-borne vibration or ground-borne noise levels, and the impact would be less than significant.
c) The Sacramento International Airport is located approximately 12 miles to the northeast of the project site, the Yolo County Airport is located approximately 7 miles to the northwest of the project site, and the University Airport is located approximately 2.5 miles west of the project site. The proposed project is not located within the airport influence areas of any airport. There would be no impact related to this significance criterion.

9 Equivalent Sound Level (Leq) represents an average of the sound energy occurring over a specified period. In effect, Leq is the steady-state sound level containing the same acoustical energy as the time-varying sound that actually occurs during the same period. The 1-hour A-weighted equivalent sound level (Leq[h]) is the energy average of A-weighted sound levels occurring during a 1-hour period, and is the basis for noise abatement criteria (NAC) used by Caltrans and FHWA.

## References

California Department of Transportation (Caltrans), 2010. Noise Control. Standard Specifications Section 14-8.02.
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Federal Transit Administration (FTA), 2006. Transit Noise and Vibration Impact Assessment. May 2006.

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U.S. Department of Transportation, Federal Highway Administration, 1998. FHWA Traffic Noise Model User's Version 1 Guide. January. Available: https://www.fhwa.dot.gov/ environment/noise/traffic_noise_model/old_versions/tnm_version_10/users_guide/ index.cfm.
——, 2004. Traffic Noise Model User's Guide Version 2.5 Addendum. Final Report. April. Available: https://www.fhwa.dot.gov/environment/noise/traffic_noise_model/tnm_v25/ users_manual/index.cfm.
U.S. Department of Transportation, Federal Highway Administration, Office of Natural and Human Environment, (FHWA A-HEP-05-054), 2006. Roadway Construction Noise Model User's Guide. Washington, D.C. January.

## Population and Housing

| Issues (and Supporting Information Sources): | Potentially Significant Impact | Less Than Significant with Mitigation Incorporated | Less Than <br> Significant Impact | No Impact |
| :---: | :---: | :---: | :---: | :---: |
| XIV. POPULATION AND HOUSING - Would the project: |  |  |  |  |
| a) Induce substantial unplanned population growth in an area, either directly (for example, by proposing new homes and businesses) or indirectly (for example, through extension of roads or other infrastructure)? | $\square$ | $\square$ | $\square$ | 区 |
| b) Displace substantial numbers of existing people or housing, necessitating the construction of replacement housing elsewhere? | $\square$ | $\square$ | $\square$ | Х |

## Discussion

a) The proposed project would reconstruct and reconfigure the I-80/Richards Boulevard interchange and make other related improvements to relieve existing congestion and reduce conflicts between bicyclists, pedestrians, and vehicles. The project would involve the improvement of an existing interchange and would not in itself induce growth above that which is planned from development in the area. There would be no impact related to this significance criterion.
b) The proposed project would not involve the removal or relocation of any housing. There would be no impact related to this significance criterion.

## Public Services

| Issues (and Supporting Information Sources): |  | Less Than <br> Potentially <br> Significant <br> Impact | Significant with <br> Mitigation <br> Incorporated | Less Than <br> Significant <br> Impact |
| :--- | :--- | :--- | :--- | :--- | No Impact

## Discussion

a.i) The proposed project does not include a residential or commercial component that would increase human presence in the area. The project would not result in an increased demand for fire protection service or reduce response times. Traffic controls would be in place during construction and the dates and times of construction would be provided to the City Fire Department to avoid impacts to emergency. This impact would be less than significant.
a.ii) The proposed project does not include a residential or commercial component that would increase human presence in the area. The project would not result in an increased demand for police protection service or reduce response times. Traffic controls would be in place during construction and the dates and times of construction would be provided to the City Police Department to avoid impacts to emergency. This impact would be less than significant.
a.iii) The proposed project would not directly result in an increased demand for schools. There would be no impact related to this significance criterion.
a.iv) The proposed project would not directly result in an increased demand for parks. There would be no impact related to this significance criterion.
a.v) The proposed project would not require additional public facilities for construction of the proposed project or for maintenance of the interchange and roadway improvements. There would be no impact related to this significance criterion.

## Recreation

| Issues (and Supporting Information Sources): | Potentially Significant Impact | Less Than Significant with Mitigation Incorporated | Less Than Significant Impact | No Impact |
| :---: | :---: | :---: | :---: | :---: |
| XVI. RECREATION - |  |  |  |  |
| a) Would the project increase the use of existing neighborhood and regional parks or other recreational facilities such that substantial physical deterioration of the facility would occur or be accelerated? | $\square$ | $\square$ | $\square$ | Х |
| b) Does the project include recreational facilities or require the construction or expansion of recreational facilities which might have an adverse physical effect on the environment? | $\square$ | $\square$ | $\square$ | Х |

## Discussion

a) The nearest parks to the project are Central Park about three-quarters of a mile northwest of the interchange, Toad Hollow Dog Park about a mile northeast of the interchange, Playfields Park and Walnut Park, both a mile east and south of the interchange. The nearest recreational facilities to the site include the Putah Creek bike path, just west of the interchange. The proposed project does not include a residential or commercial component that would increase human presence and increase the use of existing neighborhood and regional parks or other recreational facilities such that substantial physical deterioration of the facility would occur or be accelerated. There would be no impact related to this significance criterion.
b) The project would include construction of a shared-use path along the west side of Richards Boulevard replacing the existing sidewalk, and serving both bicyclists and pedestrians. The project would also widen the existing Class II bicycle lanes along Richards Boulevard between Olive Drive and Research Park Drive to a minimum of 7 feet. The physical effects of construction and operation of these City transportation facilities are evaluated in this initial study. The project does not include recreational facilities or require the construction or expansion of recreational facilities which might have an adverse physical effect on the environment. There would be no impact related to this significance criterion.

## Transportation

| Issues（and Supporting Information Sources）： | Potentially Significant Impact | Less Than Significant with Mitigation Incorporated | Less Than Significant Impact | No Impact |
| :---: | :---: | :---: | :---: | :---: |
| XVII．TRANSPORTATION－Would the project： |  |  |  |  |
| a）Conflict with a program plan，ordinance or policy addressing the circulation system，including transit， roadway，bicycle and pedestrian facilities？ | $\square$ | $\square$ | $\square$ | 区 |
| b）Would the project conflict or be inconsistent with CEQA Guidelines section 15064.3 ，subdivision（b）？ | $\square$ | $\square$ | $\square$ | 】 |
| c）Substantially increase hazards due to a geometric design feature（e．g．，sharp curves or dangerous intersections）or incompatible uses（e．g．，farm equipment）？ | $\square$ | $\square$ | 】 | $\square$ |
| d）Result in inadequate emergency access？ | $\square$ | $\square$ | 区 | $\square$ |
| Transportation Analysis |  |  |  |  |

A transportation analysis report was prepared to analyze the effects of the proposed project on the transportation network，including roadways，intersections，transit systems，and bicycle and pedestrian facilities（Fehr \＆Peers，2018）．The transportation analysis report analyzed the transportation effects of the Build Alternative（i．e．，the proposed project）and the No Build Alternative．The No Build Alternative would maintain the current roadway configuration with the exception of planned future improvements to the Richards Boulevard／Olive Drive intersection， including restriping of approaches to extend bicycle lanes and addition of separate eastbound right turn to serve traffic from planned development east of Richards Boulevard．The transportation analysis report is included as Appendix D and is summarized below．

## Transportation Analysis Study Area

The transportation analysis study area is divided into a local street network and a freeway network．The local street network extends from First Street／D Street in downtown Davis along First Street and Richards Boulevard to Research Park Drive／Richards Boulevard／Cowell Boulevard in south Davis．The freeway network extends along I－80 from Old Davis Road to Mace Boulevard．Figure 12 shows the intersections and freeway segments in the study area．

## Study Intersections

1．First Street／D Street
2．First Street／E Street／Richards Boulevard
3．Olive Drive／Richards Boulevard
4．I－80 Westbound Ramps／Richards Boulevard
5．I－80 Eastbound Ramps／Richards Boulevard
6．Research Park Drive／Richards Boulevard／Cowell Boulevard


1 Study Intersection
Freeway Corridor
(N)

Not to scale

## Freeway Study Segments

Eastbound l-80

1. West of Old Davis Road On-ramp
2. Old Davis Road On-ramp
3. Old Davis Road to 1st Lane Drop
4. 1st Lane Drop to 2nd Lane Drop
5. Richards Boulevard Off-ramp
6. Richards Boulevard Off to On-ramp
7. Richards Boulevard On-ramp
8. Richards Boulevard to Chiles Road
9. Chiles Road Off-ramp
10. East of Chiles Road Off-ramp

Westbound I-80
11. East of Mace Boulevard On-ramp
12. Mace Boulevard to Lane Drop
13. Lane Drop to Olive Drive
14. Olive Drive Off-ramp
15. Olive Drive to Richards Boulevard
16. Richards Boulevard Northbound Off-ramp
17. Richards Boulevard Northbound Off to On-ramp
18. Richards Boulevard Northbound On-ramp to Southbound Off-ramp
19. Richards Boulevard Southbound Off to On-ramp
20. Richards Boulevard to Old Davis Road
21. Old Davis Road Off-ramp
22. West of Old Davis Road

## Evaluation Criteria

The intersection and freeway segment evaluation criteria used in the transportation analysis report were based on the policies of the City of Davis and Caltrans, both of which use level of service (LOS) as a metric for describing the operations of the segments and intersections of a roadway network. As described in the City of Davis General Plan Transportation Element, LOS is a semiquantitative description of an intersection's operation, ranging from LOS A (indicating free flow traffic conditions with little or no delay) to LOS F (representing oversaturated conditions with traffic flows exceeding design capacity, resulting in long queues and delays). LOS at roadway segments can be qualified by several methodologies. A daily LOS is a generalized approach where the volume-to-capacity based on a theoretical daily roadway capacity is based on the number of lanes and capacity class. Roadway congestion is generally represented by an
alphabetic level of service A through F. Level F is indicative of a roadway that has exceeded its theoretical maximum capacity, and therefore fully congested (City of Davis, 2013).

## City of Davis

The City of Davis General Plan Transportation Element identifies LOS E as the minimum acceptable LOS for intersections during peak hours although LOS F is acceptable for the "Core Area and Richards Boulevard/Olive Drive area." For the proposed project, a significant impact occurs when (1) an intersection worsens from LOS E or better under the No Build Alternative to LOS F or (2) intersection delay increases for an intersection operating at LOS F under the No Build Alternative.

## Caltrans

The Interstate 80 Transportation Concept Report (Caltrans, 2017) identifies LOS E as the concept LOS for urban areas in Caltrans District 3. For the proposed project, a significant impact occurs when (1) a freeway segment worsens from LOS E or better under the No Build Alternative to LOS F or (2) freeway segment density increases for a segment operating at LOS F under the No Build Alternative.

## Data Collection

To identify existing traffic conditions in the study area, intersection and freeway traffic counts were collected from 7:00 to 9:00 a.m. and 4:00 to 6:00 p.m. The peak period counts included heavy vehicles, bicycles, and pedestrians. The intersection turning movement counts were collected in May 2016 on a typical midweek day. Freeway mainline volumes were obtained from the Caltrans Performance Measurement System (PeMS). The data were averaged across weekdays in October 2016. Freeway ramp volumes for the Richards Boulevard and Old Davis Road interchanges come from intersection counts taken in October 2016. The Olive Drive offramp was counted in May 2016. For the Mace Boulevard/Chiles Road ramps, data collected in May 2014 was used. For the ramps, the peak hour volumes were determined using the mainline peak hour.

## Travel Demand Forecasting

## Base Year Model Development

The City of Davis travel demand forecasting model was used to prepare the traffic volumes for future conditions. A base year model validation was performed to determine how well the model replicates existing traffic volumes.

## Cumulative Year Model Development

Similar to the base year model, the cumulative year land use and roadway network inputs were reviewed. In addition to the roadway network adjustments identified for the base year model validation, the UC Davis land use growth was adjusted to the latest projections in the Long Range Development Plan (LRDP).

The cumulative year model includes build-out of the city's General Plan under 2035 conditions plus the following proposed projects.

- Aggie Research Campus - located north of I-80 and east of Mace Boulevard that would include 1.5 million square feet of research and development, 884,000 square feet of manufacturing, 160,000 square feet of hotel, and 100,000 square feet of retail and restaurant uses
- Davis Hotel and Conference Center - located west of Richards Boulevard between Olive Drive and I-80 that would replace the 43 -room University Inn \& Suites Hotel and Caffe Italia restaurant with a 132 -room Embassy Suites hotel, a restaurant, and a 14,900 square-foot conference center
- Nishi/West Olive Drive Development - located in the triangle formed by I-80, the Union Pacific Railroad, and Putah Creek with vehicle connections to Olive Drive and the UC Davis campus that would include 650 residential units, 325,000 square feet of research and development/office, and 20,000 square feet of retail uses
- Lincoln 40 Apartments - located on Olive Drive east of Richards Boulevard that would include 130 apartments oriented to students attending UC Davis
- Sterling Apartments - located on Fifth Street east of Pole Line Road that would include 198 apartments oriented to students attending UC Davis

The Aggie Research Campus has been approved, but is on hold, and the Davis Hotel and Conference Center was not approved by voters in an election. However, the properties are likely to be developed in some fashion by cumulative conditions. For the transportation analysis, the previously proposed projects were assumed although the actual development may be smaller in scope.

In addition, the forecasted growth was increased to account for growth between the cumulative model year of 2035 and the project design year of 2042. The design year represents an estimation of the future traffic demand and volume expected on the facility. For most locations, the growth rate from 2035 to 2042 was assumed to continue at the same rate predicted by the model from 2016 to 2035, which results in about 37 percent additional growth for the seven years from 2035 to 2042 . However, land uses along Olive Drive are assumed to be built out by 2035 conditions, so the additional growth from 2035 to 2042 was reduced from 37 to 10 percent. The construction year (2022) volumes were prepared using linear interpolation, which assumed a constant rate of traffic growth between existing and cumulative year (2035) conditions.

Bicycle and pedestrian volumes were assumed to grow proportionally to the land use growth in the study area. In the project vicinity, land use grows by about 17 percent between the base year and cumulative year models. Extrapolating this growth from the cumulative year of 2035 to the design year of 2042 conditions, increases the total growth to about 23 percent. This value was rounded up to 25 percent and used to generate the design year bicycle and pedestrian volumes. Additionally, the minimum bicycle turning movement volume was set to 2 bicycles per hour, and the bicycle volumes were balanced through the study intersections.

## Transportation Analysis Results and Findings

The findings of the transportation analysis report are summarized below. The complete transportation analysis report is included as Appendix D.

## Intersections and Freeway Segments

The study locations that operate or would operate over capacity (LOS F) are summarized below by alternative.

Existing Conditions

- Intersections
- I-80 Westbound Ramps/Richards Boulevard (AM)
- Freeway Segments
- I-80 Eastbound, Old Davis Road to Mace Boulevard (PM)

No Build Alternative, Construction Year Conditions

- Intersections
- Olive Drive/Richards Boulevard (AM)
- I-80 Westbound Ramps/Richards Boulevard (AM)
- I-80 Eastbound Ramps/Richards Boulevard (PM)
- Freeway Segments
- I-80 Eastbound, Old Davis Road to Mace Boulevard (PM)

Build Alternative, Construction Year Conditions

- Freeway Segments
- I-80 Eastbound, Old Davis Road to Mace Boulevard (PM)

No Build Alternative, Design Year Conditions

- Intersections
- First Street/D Street (AM)
- First Street/E Street/Richards Boulevard (AM)
- Olive Drive/Richards Boulevard (AM and PM)
- I-80 Westbound Ramps/Richards Boulevard (AM)
- I-80 Eastbound Ramps/Richards Boulevard (AM and PM)
- Research Park Drive/Richards Boulevard/Cowell Boulevard (AM and PM)

As discussed above, the intersection and freeway segment evaluation criteria used in the transportation analysis report were based on policies of the City of Davis and Caltrans. Under these criteria, a significant impact occurs where (1) the LOS threshold is exceeded and (2) the conditions are worse in Build Alternative than the No Build Alternative. Based on these evaluation
criteria, the transportation analysis report determined that the proposed project would not result in impacts to intersections or freeway segments, and, consequently, no mitigations were necessary.

## Roadway Safety

Using the forecasted daily volume, predicted collisions were calculated for design year conditions under the project alternatives. Under the No Build Alternative, the current five ramps in the westbound direction at Olive Drive and Richards Boulevard would be expected to have 5.7 collisions per year, with 2.2 fatality and injury-related collisions (see Table 18, Freeway Ramp Collision Rate - Construction Year Conditions, in Appendix D of this Initial Study). No Build Alternative Build Alternative. Under the proposed project, the westbound ramps would be reduced from 5 to 2 , and the ramp roadways would be reconfigured to have curves that are less sharp (that is, a higher radius). The expected total collision rate would be 2.1 collisions per year, with 1.0 fatality and injury-related collisions. The transportation analysis report determined that, under the proposed project, the expected total collision rate would be reduced by 63 percent of the No Build Alternative rate, and the fatality and injury-related rate would be reduced by about 55 percent.

## Bicycle System

The proposed project would provide a grade-separated two-way path for bicycles and pedestrians on the west side of the interchange. The path would function as an extension of the existing path on the west side of Richards Boulevard between First Street and Olive Drive that travels through a tunnel under the Union Pacific Railroad. South of Olive Drive, the path would run adjacent to Richards Boulevard. Approaching the interchange, the path would diverge from the roadway and then travel under the westbound on-ramp. Then, the path would loop around and travel over the path and adjacent to the westbound on-ramp to reach the freeway overcrossing. The path would continue adjacent to, but barrier-separated from, Richards Boulevard south to the Research Park Drive intersection. The existing Class II (on-street) bicycle lanes would be maintained on Richards Boulevard. The transportation analysis report determined that the reconstructed intersection at the I-80 Westbound Ramps would have slower speed turns than the existing configuration, which would provide a safer environment for on-street bicyclists.

## Pedestrian System

The proposed project would replace the sidewalk and crosswalks on the west side of the interchange with the grade-separated pathway for bicycles and pedestrians described in the previous section. At the loop on the pathway, stairs would be provided so that pedestrians can travel a shorter route.

At the Olive Drive and Research Park Drive intersections, crosswalks would be provided on all legs. At Olive Drive, the wider approaches would result in longer crossing distances on three of the four approaches. Longer crossing distance increases pedestrian exposure and therefore reduces pedestrian safety. The median bus stop on the northbound approach would be moved to the shoulder of the northbound departure. The transportation analysis report determined that pedestrians traveling to the bus stop would have less exposure to conflicting vehicles.

At Research Park Drive, the west leg (Richards Boulevard) would be reconstructed to provide an additional eastbound lane. However, the southwest corner would be rebuilt with a smaller radius such that the crosswalks on the west and south legs would be shorter than under existing
conditions. The transportation analysis report determined that the shorter crossing distance would reduce pedestrian exposure and therefore improve pedestrian safety.

## Transit System

The proposed project would relocate the Unitrans bus stop on northbound Richards Boulevard at Olive Drive from a near side to a far side location. This would move the boarding area from a median between two lanes of traffic to the roadway shoulder thereby improving the waiting experience for passengers. The far side location also would allow buses to more easily reenter the roadway compared to the near side location that requires buses to merge into traffic in the intersection. The transportation analysis report determined that the improvement in intersection operations with the proposed project would also improve bus operations and travel time.

## Performance Measures

To estimate the area-wide effect of the proposed project and the closure of the westbound offramp to Olive Drive, the design year (2042) performance measures of vehicle miles of travel (VMT), vehicle hours of travel (VHT), and vehicle hours of delay (VHD) were estimated using the cumulative year forecasting model. To capture the potential changes, performance was measured over the entire model area, which is the City of Davis. Under design year conditions, the same number of trips were assigned to the two different roadway alternatives.

The transportation analysis report determined that the proposed project would provide a small reduction in VMT by shifting trips originating in the City of Davis to shorter local routes with the closure of the Olive Drive westbound off-ramp. Network-wide delay would also be reduced by shifting trips from lower-speed Olive Drive to higher-speed I-80 and Richards Boulevard.

The transportation analysis report determined that the proposed project would provide more capacity along Richards Boulevard from Olive Drive to Research Park Drive. Intersections that would be over capacity under the No Build Alternative would operate with LOS E or better conditions.

The transportation analysis report determined that the reconfiguration of the westbound ramps at Richards Boulevard from a cloverleaf to a diamond design would remove the loop on-ramp and off-ramp, which have higher collision rates than slip or diagonal designs.

Even though the volume will be higher on the combined ramps, especially on the off-ramp with the closure of the Olive Drive off-ramp, the transportation analysis report determined that the combined westbound ramp collision rate for the proposed project is expected to be less than half the rate of the No Build Alternative under design year conditions.

Given the advantages in network efficiency, intersection operations, and freeway ramp safety, the transportation analysis report recommended the proposed project over the No Build Alternative to provide the best traffic operations and safety.

## Discussion

a) As discussed above, a transportation analysis report was prepared to analyze the effects of the proposed project on the transportation network, including roadways, intersections,
transit systems, and bicycle and pedestrian facilities (Appendix D). The evaluation criteria used in the transportation analysis report were based on the applicable transportation policies of the City of Davis and Caltrans. Based on these evaluation criteria, the transportation analysis report determined that the proposed project would not result in significant impacts to intersections or freeway segments; would improve safety for motorists, pedestrians and bicyclists; would improve bus operations and travel time. Consequently, the proposed project would not conflict with a program plan, ordinance, or policy addressing the circulation system, including transit, roadway, bicycle and pedestrian facilities. The transportation analysis report determined that the proposed project would improve network efficiency, intersection operations, and freeway ramp safety. There would be no impact related to this significance criterion.
b) CEQA Guidelines section 15064.3, Determining the Significance of Transportation Impacts, describes specific considerations for evaluating a project's transportation impacts and states that, generally, vehicle miles traveled (VMT), which refers to the amount and distance of automobile travel attributable to a project, is the most appropriate measure of transportation impacts. Section 15064.3, subdivision (b) (2) states that transportation projects that reduce, or have no impact on, vehicle miles traveled should be presumed to cause a less than significant transportation impact. As discussed above, the transportation analysis report determined that the proposed project would provide a small reduction in VMT by shifting trips originating in the City of Davis to shorter local routes with the closure of the Olive Drive westbound off-ramp. Consequently, the proposed project would not conflict or be inconsistent with CEQA Guidelines section 15064.3, subdivision (b). There would be no impact related to this significance criterion.
c) The proposed project would reconstruct and reconfigure the I-80/Richards Boulevard interchange and make other related improvements to relieve existing congestion and reduce conflicts between bicyclists, pedestrians, and vehicles. Under the proposed project, the westbound ramps would be reduced from 5 to 2 , and the ramp roadways would be reconfigured to have curves that are less sharp (that is, a higher radius). The transportation analysis report determined that, under the proposed project, the expected total collision rate would be reduced by 63 percent of the No Build Alternative rate, and the fatality and injury-related rate would be reduced by about 55 percent.

The proposed project would provide a grade-separated two-way path for bicycles and pedestrians on the west side of the interchange. The transportation analysis report determined that the reconstructed intersection at the I-80 westbound ramps would have slower speed turns than the existing configuration, which would provide a safer environment for on-street bicyclists.

At the Olive Drive and Research Park Drive intersections, crosswalks would be provided on all legs. At Olive Drive, the wider approaches would result in longer crossing distances on three of the four approaches.

At Research Park Drive, the west leg (Richards Boulevard) would be reconstructed to provide an additional eastbound lane. However, the southwest corner would be rebuilt
with a smaller radius such that the crosswalks on the west and south legs would be shorter than under existing conditions. The transportation analysis report determined that the shorter crossing distance would reduce pedestrian exposure and therefore improve pedestrian safety.

As described above, the proposed project includes numerous improvements that would improve operational safety and reduce conflicts between bicyclists, pedestrians, and vehicles. While the wider approaches at the Olive Drive intersection would result in longer crosswalk distances on three of the four approaches, the facilities would meet all applicable design requirements related to safety. The proposed project would not substantially increase hazards due to a geometric design feature or incompatible uses, and the impact would be less than significant.
d) The proposed project would relieve existing congestion and reduce conflicts between bicyclists, pedestrians, and vehicles. Emergency access through the intersections would improve from conditions prior to the modifications.

A Transportation Management Plan (TMP) would be developed for use during project construction. The TMP would utilize strategies described in the California Manual of Traffic Control Devices and Caltrans Transportation Management Plan Guidelines. The TMP would direct the process and procedures for dissemination of information to the public and motorists, provide guidance for implementation of incident management, describe construction strategies for traffic handling and guiding traffic through work zones, address traffic demand management during construction, and describe and direct the implementation of alternate routes or detours. Implementation of the TMP would ensure that impacts related to emergency access during construction of the proposed project would be less than significant.

## References

California Department of Transportation (Caltrans), 2017. Interstate 80 Transportation Concept Report. July 2017.

City of Davis, 2013. City of Davis General Plan Transportation Element. December 2013.
Fehr \& Peers, 2018. Transportation Analysis Report, Interstate 80/Richards Boulevard Interchange. Prepared for City of Davis. June 2018.

## Tribal Cultural Resources

| Issues (and Supporting Information Sources): |  | Potentially Significant Impact | Less Than Significant with Mitigation Incorporated | Less Than Significant Impact | No Impact |
| :---: | :---: | :---: | :---: | :---: | :---: |
| XVIII. TRIBAL CULTURAL RESOURCES - |  |  |  |  |  |
|  | uld the project cause a substantial adverse change he significance of a tribal cultural resource, defined Public Resources Code section 21074 as either a , feature, place, cultural landscape that is graphically defined in terms of the size and scope he landscape, sacred place, or object with cultural e to a California Native American tribe, and that is: |  |  |  |  |
| i) | Listed or eligible for listing in the California Register of Historical Resources, or in a local register of historical resources as defined in Public Resources. Code Section 5020.1(k), or | $\square$ | Х | $\square$ | $\square$ |
| ii) | A resource determined by the lead agency, in its discretion and supported by substantial evidence, to be significant pursuant to criteria set forth in subdivision (c) of Public Resources Code Section 5024.1. In applying the criteria set forth in subdivision (c) of Public Resources Code Section 5024.1, the lead agency shall consider the significance of the resource to a California Native American tribe. | $\square$ | Х | $\square$ | $\square$ |

## Discussion

a) A tribal cultural resource is defined in the Public Resources Code section 21074 and includes the following:

- Sites, features, places, cultural landscapes, sacred places, and objects with cultural value to a California Native American Tribe that are either of the following: included or determined to be eligible for inclusion in the California Register of Historical Resources or included in a local register of historical resources as defined in subdivision (k) of Section 5020.1;
- A resource determined by the lead agency, in its discretion and supported by substantial evidence, to be significant pursuant to criteria set forth in subdivision (c) of Section 5024.1. In applying the criteria set forth in subdivision (c) of Section 5024.1 for the purpose of this paragraph, the lead agency shall consider the significance of the resources to a California American tribe;
- A cultural landscape that meets the criteria of subdivision (a) is a tribal cultural resource to the extent that the landscape is geographically defined in terms of the size and scope of the landscape;
- A historical resource described in Section 21084.1, a unique archaeological resource as defined in subdivision (g) of Section 21083.2, or a "non-unique archaeological resource" as defined in subdivision (h) of Section 21083.2 may also be a tribal resource if it conforms with the criteria of subdivision (a).

As discussed in the Cultural Resources section of this initial study, the cultural resources investigation conducted for the proposed project determined that there are no previously recorded archaeological or tribal cultural resources in the proposed project Area of

Potential Effects (APE), and no evidence of archaeological or tribal cultural resources were encountered during the pedestrian archaeological survey of the APE.

Pursuant to Public Resources Code section 21080.3.1, the City of Davis consulted with California Native American tribes regarding the proposed project. Letters that described the proposed project, provided formal notification of the proposed project, and requested a written response within 30 days if consultation was desired were sent to the Ione Band of Miwok Indians, the Yoche Dehe Wintun Nation, and the Cortina Indian Rancheria of Wintun Indians on August 28, 2019. The City received one response. In a letter dated September 12, 2018, the Yoche Dehe Wintun Nation stated that the project site is within the aboriginal territory of the Yoche Dehe Wintun Nation and therefore the tribe has cultural interest and authority in the project area. The letter stated that the tribe is not aware of any known cultural resources near the project site and monitoring is not needed. The letter included a recommendation that pre-construction cultural resource sensitivity training should be provided by members of the Yoche Dehe Wintun Nation. Records of tribal consultation are included in Appendix C of this initial study.

As discussed in the Cultural Resources section of this initial study, the cultural resources investigation determined that the proposed project has a low potential to affect archaeological or resources or human remains due to the environmental setting and previous extensive disturbance of the area. Nonetheless, because there is a possibility that project construction and excavation activities could unearth previously undiscovered or unrecorded archaeological resources or human remains, if they are present, impacts to tribal cultural resources are considered to be potentially significant. Implementation of Mitigation Measures CUL-1, CUL-2, and CUL-3 included in the Cultural Resources section of this initial study would ensure that impacts to tribal cultural resource would be less than significant.

## Utilities and Service Systems

| Issues (and Supporting Information Sources): |  | Potentially Significant Impact | Less Than Significant with Mitigation Incorporated | Less Than Significant Impact | No Impact |
| :---: | :---: | :---: | :---: | :---: | :---: |
| XIX. | UTILITIES AND SERVICE SYSTEMS - <br> Would the project: |  |  |  |  |
| a) | Require or result in the relocation or construction of new or expanded water, wastewater treatment or storm water drainage, electric power, natural gas, or telecommunications facilities, the construction or relocation of which could cause significant environmental effects? | $\square$ | $\square$ | Х | $\square$ |
| b) | Have sufficient water supplies available to serve the project and reasonably foreseeable future development during normal, dry and multiple dry years? | $\square$ | $\square$ | Х | $\square$ |
| c) | Result in a determination by the wastewater treatment provider which serves or may serve the project that it has adequate capacity to serve the project's projected demand in addition to the provider's existing commitments? | $\square$ | $\square$ | 】 | $\square$ |
| d) | Generate solid waste in excess of State or local standards, or in excess of the capacity of local infrastructure, or otherwise impair the attainment of solid waste reduction goals? | $\square$ | $\square$ | Х | $\square$ |
| e) | Comply with federal, state, and local management and reduction statutes and regulations related to solid waste? | $\square$ | $\square$ | 】 | $\square$ |

## Discussion

a) The proposed project would reconstruct and reconfigure the I-80/Richards Boulevard interchange and make other related improvements to relieve existing congestion and reduce conflicts between bicyclists, pedestrians, and vehicles. Operation of the proposed project would not produce additional wastewater and it would not require or generate a demand for either water or wastewater service that would require or result in the relocation or construction of new or expanded water or wastewater facilities. Onsite drainage improvements would improve existing stormwater drainage and would not require relocation or construction of new or expanded offsite conveyance or treatment facilities. Water and electric power consumed for project construction activities would not result in demand levels that would require relocation or construction of new or expanded offsite facilities. The impact would be less than significant.
b) As an interchange modification project, no increase in demand for water would occur as a result of the completed project. Water use for project construction activities, such as dust control, would not be anticipated to have any adverse impact on available supplies. The impact would be less than significant.
c) The proposed project does not include any uses that would generate wastewater. The impact would be less than significant.
d) Solid waste generated by the project would be limited to demolition and construction debris, including asphalt and concrete. Disposal would occur at permitted landfills. The impact would be less than significant.
e) Solid waste disposal of demolition and construction materials, including the disposal of any hazardous wastes that may be encountered, would occur in accordance with federal, state and local regulations. The impact would be less than significant.

## Wildfire

| Issues（and Supporting Information Sources）： |  | Potentially Significant Impact | Less Than Significant with Mitigation Incorporated | Less Than <br> Significant Impact | No Impact |
| :---: | :---: | :---: | :---: | :---: | :---: |
| XX. | WILDFIRE－If located in or near state responsibility areas or lands classified as very high fire hazard severity zones，would the project： |  |  |  |  |
| a） | Substantially impair an adopted emergency response plan or emergency evacuation plan？ | $\square$ | $\square$ | $\square$ | 】 |
| b） | Due to slope，prevailing winds，and other factors， exacerbate wildfire risks，and thereby expose project occupants to，pollutant concentrations from a wildfire or the uncontrolled spread of a wildfire？ | $\square$ | $\square$ | $\square$ | 】 |
| c） | Require the installation or maintenance of associated infrastructure（such as roads，fuel breaks，emergency water sources，power lines or other utilities）that may exacerbate fire risk or that may result in temporary or ongoing impacts to the environment？ | $\square$ | $\square$ | $\square$ | 区 |
| d） | Expose people or structures to significant risks， including downslope or downstream flooding or landslides，as a result of runoff，post－fire slope instability，or drainage changes？ | $\square$ | $\square$ | $\square$ | 】 |

## Discussion

a－d）State Responsibility Areas are recognized by the Board of Forestry and Fire Protection as areas where Cal Fire is the primary emergency response agency responsible for fire suppression and prevention．The project site comprises an existing interchange and adjacent roadways and structures in an urban environment in the City of Davis．The project site is not located in or near state responsibility areas or lands classified as very high fire hazard severity zones（California State Board of Forestry and Fire Protection， 2019）．There would be no impact under these significance criteria．

## References

California State Board of Forestry and Fire Protection，2019．State Responsibility Area Viewer． Available：https：／／bof．fire．ca．gov／projects－and－programs／state－responsibility－area－viewer／． Accessed September 24， 2019.

# Mandatory Findings of Significance 

Issues (and Supporting Information Sources):

## Discussion

a) As discussed in this initial study, there are no historical resources within or adjacent to the project site, and Mitigation Measures CUL-1, CUL-2, and CUL-3 included in this initial study would ensure that unanticipated impacts to subsurface archaeological resources, human remains, or tribal cultural resources would be less than significant. Similarly, Mitigation Measures BIO-1 through BIO-6 included in this initial study would ensure that potential impacts to special-status wildlife species and habitat would be less than significant. Consequently, impacts related to degradation of the quality of the environment, reduction of species or habitat, and elimination of important examples of the major periods of California history or prehistory would be less than significant with mitigation incorporated.
b) The proposed project in conjunction with other development within the City of Davis could incrementally contribute to cumulative impacts in the area. However, the project's incremental contribution towards cumulative impacts would not be considered significant. Therefore, the proposed project would not have any impacts that would be cumulatively considerable, and impacts would be less than significant.
c) The proposed project would reconstruct and reconfigure the I-80/Richards Boulevard interchange and make other related improvements to relieve existing congestion and reduce conflicts between bicyclists, pedestrians, and vehicles. Substantial adverse effects on human beings are not anticipated with implementation of the proposed project. During construction activities, the project could result in temporary noise increases and rerouting of traffic. However, the proposed project would be designed and constructed in accordance with all applicable standards and codes to ensure adequate safety is provided for the
future residents of the proposed project. Therefore, impacts related to environmental effects that could cause adverse effects on human beings would be less than significant.

# Appendix A <br> Interagency Consultation 

| From: | Shengyi Gao [SGao@sacog.org](mailto:SGao@sacog.org) |
| :--- | :--- |
| Sent: | Monday, September 10, 2018 1:55 PM |
| To: | Alexander Fong; Dave Johnston; David Yang; Douglas Coleman; Heather Phillips ; Janice |
|  | Lam Snyder; Jason Lee; Jerry Barton; John Ungvarsky; Jose Luis Caceres; Joseph Vaughn; |
|  | Karina O'Connor; Ken Born; Lucas Sanchez; Mark Loutzenhiser; Matt Jones; Mcneel- |
|  | Caird; Paul Philley; Renee DeVere-Oki; Rodney Tavitas; Shalanda Christian; Sharon Tang; |
|  | Sondra Spaethe; Wright Molly; Yu-Shuo Chang |
| Cc: | clark.peri@dot.ca.gov; Joza Burnam |
| Subject: | RE: POAQC: City of Davis \& Caltrans Richards Blvd Project (YOL17140), Due 9/6 |

Hi all,
The Project Level Conformity Group has determined that the City of Davis and Caltrans Richards Blvd Project (YOL17140) is Not a Project of Air Quality Concern (POAQC).
EPA concurred on 09/06/2018 and FHWA concurred on 09/10/2018.

Thanks to you all!
Shengyi Gao
Sacramento Area Council of Governments
916.340.6239

From: Shengyi Gao
Sent: Friday, August 24, 2018 10:15 AM
To: Alexander Fong [alexander.fong@dot.ca.gov](mailto:alexander.fong@dot.ca.gov); Dave Johnston [dave.johnston@edcgov.us](mailto:dave.johnston@edcgov.us); David Yang [DYang@airquality.org](mailto:DYang@airquality.org); Douglas Coleman [douglas.coleman@dot.ca.gov](mailto:douglas.coleman@dot.ca.gov); Heather Phillips
[Heather.Phillips@arb.ca.gov](mailto:Heather.Phillips@arb.ca.gov); Janice Lam Snyder [JLam@airquality.org](mailto:JLam@airquality.org); Jason Lee [jason.lee@dot.ca.gov](mailto:jason.lee@dot.ca.gov); Jerry Barton [jbarton@edctc.org](mailto:jbarton@edctc.org); John Ungvarsky [Ungvarsky.John@epa.gov](mailto:Ungvarsky.John@epa.gov); Jose Luis Caceres [JCaceres@sacog.org](mailto:JCaceres@sacog.org); Joseph Vaughn [Joseph.Vaughn@dot.gov](mailto:Joseph.Vaughn@dot.gov); Karina O'Connor [oconnor.karina@epa.gov](mailto:oconnor.karina@epa.gov); Ken Born [kenneth.born@dot.gov](mailto:kenneth.born@dot.gov); Lucas Sanchez [lucas.sanchez@dot.ca.gov](mailto:lucas.sanchez@dot.ca.gov); Mark Loutzenhiser [mloutzenhiser@airquality.org](mailto:mloutzenhiser@airquality.org); Matt Jones [mjones@ysaqmd.org](mailto:mjones@ysaqmd.org); Mcneel-Caird [Imcneel-caird@pctpa.net](mailto:Imcneel-caird@pctpa.net); Paul Philley [pphilley@airquality.org](mailto:pphilley@airquality.org); Renee DeVere-Oki [RDeVere-Oki@sacog.org](mailto:RDeVere-Oki@sacog.org); Rodney Tavitas [rodney.tavitas@dot.ca.gov](mailto:rodney.tavitas@dot.ca.gov); Shalanda Christian [shalanda_christian@dot.ca.gov](mailto:shalanda_christian@dot.ca.gov); Sharon Tang [sharon.tang@dot.ca.gov](mailto:sharon.tang@dot.ca.gov); Sondra Spaethe [sspaethe@fraqmd.org](mailto:sspaethe@fraqmd.org); Wright Molly [mwright@airquality.org](mailto:mwright@airquality.org); Yu-Shuo Chang [YChang@placer.ca.gov](mailto:YChang@placer.ca.gov)
Cc: 'clark.peri@dot.ca.gov' [clark.peri@dot.ca.gov](mailto:clark.peri@dot.ca.gov); 'Joza Burnam' [jmburnam@esassoc.com](mailto:jmburnam@esassoc.com)
Subject: POAQC: City of Davis \& Caltrans Richards Blvd Project (YOL17140), Due 9/6

## Project Level Conformity Group,

Attached for interagency review is the City of Davis and Caltrans Richards Blvd Project (YOL17140) . As part of project level conformity under NEPA, it requires a determination of whether it is a project of air quality concern.

Please confirm that you concur that this is NOT a Project of Air Quality Concern (POAQC). Please email questions and comments by 5 p.m., Thursday, September 6.

This project falls under the 23 USC 327 (formerly 6005) federal process. As such, it requires written concurrence by EPA (Karina O'Conner) and FHWA (Joseph Vaughn). Please remember to use "reply all," to make comments to the group. Otherwise, you may also contact the sponsor directly:

Clark Peri
Caltrans
Tel: 916.274.0538
Email: clark.peri@dot.ca.gov

## Appendix B Species Lists



# United States Department of the Interior 

FISH AND WILDLIFE SERVICE<br>Sacramento Fish And Wildlife Office Federal Building<br>2800 Cottage Way, Room W-2605<br>Sacramento, CA 95825-1846<br>Phone: (916) 414-6600 Fax: (916) 414-6713

In Reply Refer To:
January 19, 2022
Consultation Code: 08ESMF00-2019-SLI-1525
Event Code: 08ESMF00-2022-E-02613
Project Name: 03-0H360 Richards Blvd Interchange Improvements

Subject: Updated list of threatened and endangered species that may occur in your proposed project location or may be affected by your proposed project

To Whom It May Concern:
The enclosed species list identifies threatened, endangered, proposed and candidate species, as well as proposed and final designated critical habitat, under the jurisdiction of the U.S. Fish and Wildlife Service (Service) that may occur within the boundary of your proposed project and/or may be affected by your proposed project. The species list fulfills the requirements of the Service under section 7(c) of the Endangered Species Act (Act) of 1973, as amended (16 U.S.C. 1531 et seq.).

Please follow the link below to see if your proposed project has the potential to affect other species or their habitats under the jurisdiction of the National Marine Fisheries Service:
http://www.nwr.noaa.gov/protected_species/species_list/species_lists.html
New information based on updated surveys, changes in the abundance and distribution of species, changed habitat conditions, or other factors could change this list. Please feel free to contact us if you need more current information or assistance regarding the potential impacts to federally proposed, listed, and candidate species and federally designated and proposed critical habitat. Please note that under 50 CFR 402.12(e) of the regulations implementing section 7 of the Act, the accuracy of this species list should be verified after 90 days. This verification can be completed formally or informally as desired. The Service recommends that verification be completed by visiting the ECOS-IPaC website at regular intervals during project planning and implementation for updates to species lists and information. An updated list may be requested through the ECOS-IPaC system by completing the same process used to receive the enclosed list.

The purpose of the Act is to provide a means whereby threatened and endangered species and the ecosystems upon which they depend may be conserved. Under sections 7(a)(1) and 7(a)(2) of the Act and its implementing regulations (50 CFR 402 et seq.), Federal agencies are required to
utilize their authorities to carry out programs for the conservation of threatened and endangered species and to determine whether projects may affect threatened and endangered species and/or designated critical habitat.

A Biological Assessment is required for construction projects (or other undertakings having similar physical impacts) that are major Federal actions significantly affecting the quality of the human environment as defined in the National Environmental Policy Act (42 U.S.C. 4332(2) (c)). For projects other than major construction activities, the Service suggests that a biological evaluation similar to a Biological Assessment be prepared to determine whether the project may affect listed or proposed species and/or designated or proposed critical habitat. Recommended contents of a Biological Assessment are described at 50 CFR 402.12.

If a Federal agency determines, based on the Biological Assessment or biological evaluation, that listed species and/or designated critical habitat may be affected by the proposed project, the agency is required to consult with the Service pursuant to 50 CFR 402. In addition, the Service recommends that candidate species, proposed species and proposed critical habitat be addressed within the consultation. More information on the regulations and procedures for section 7 consultation, including the role of permit or license applicants, can be found in the "Endangered Species Consultation Handbook" at:
http://www.fws.gov/endangered/esa-library/pdf/TOC-GLOS.PDF
Please be aware that bald and golden eagles are protected under the Bald and Golden Eagle Protection Act (16 U.S.C. 668 et seq.), and projects affecting these species may require development of an eagle conservation plan
(http://www.fws.gov/windenergy/eagle_guidance.html). Additionally, wind energy projects should follow the wind energy guidelines (http://www.fws.gov/windenergy/) for minimizing impacts to migratory birds and bats.

Guidance for minimizing impacts to migratory birds for projects including communications towers (e.g., cellular, digital television, radio, and emergency broadcast) can be found at: http://www.fws.gov/migratorybirds/CurrentBirdIssues/Hazards/towers/towers.htm; http://www.towerkill.com; and www.fws.gov/migratorybirds/CurrentBirdIssues/Hazards/towers/comtow.html.

We appreciate your concern for threatened and endangered species. The Service encourages Federal agencies to include conservation of threatened and endangered species into their project planning to further the purposes of the Act. Please include the Consultation Tracking Number in the header of this letter with any request for consultation or correspondence about your project that you submit to our office.

Attachment(s):

- Official Species List


## Official Species List

This list is provided pursuant to Section 7 of the Endangered Species Act, and fulfills the requirement for Federal agencies to "request of the Secretary of the Interior information whether any species which is listed or proposed to be listed may be present in the area of a proposed action".

This species list is provided by:
Sacramento Fish And Wildlife Office
Federal Building
2800 Cottage Way, Room W-2605
Sacramento, CA 95825-1846
(916) 414-6600

## Project Summary

Consultation Code: 08ESMF00-2019-SLI-1525
Event Code: Some(08ESMF00-2022-E-02613)
Project Name: 03-0H360 Richards Blvd Interchange Improvements
Project Type: TRANSPORTATION
Project Description: Change the westbound on- and off-ramps from a full cloverleaf configuration into a tight diamond configuration at the Richards Blvd Interchange.
Project Location:
Approximate location of the project can be viewed in Google Maps: https://
www.google.com/maps/@38.54205604437582,-121.73271990776217,14z


Counties: Solano and Yolo counties, California

## Endangered Species Act Species

There is a total of 10 threatened, endangered, or candidate species on this species list.
Species on this list should be considered in an effects analysis for your project and could include species that exist in another geographic area. For example, certain fish may appear on the species list because a project could affect downstream species.

IPaC does not display listed species or critical habitats under the sole jurisdiction of NOAA Fisheries ${ }^{\underline{1}}$, as USFWS does not have the authority to speak on behalf of NOAA and the Department of Commerce.

See the "Critical habitats" section below for those critical habitats that lie wholly or partially within your project area under this office's jurisdiction. Please contact the designated FWS office if you have questions.

1. NOAA Fisheries, also known as the National Marine Fisheries Service (NMFS), is an office of the National Oceanic and Atmospheric Administration within the Department of Commerce.

## Birds

NAME
STATUS
Western Snowy Plover Charadrius nivosus nivosus
Threatened
Population: Pacific Coast population DPS-U.S.A. (CA, OR, WA), Mexico (within 50 miles of Pacific coast)
There is final critical habitat for this species. The location of the critical habitat is not available.
Species profile: https://ecos.fws.gov/ecp/species/8035

## Reptiles

NAME STATUS
Giant Garter Snake Thamnophis gigas
Threatened
No critical habitat has been designated for this species.
Species profile: https://ecos.fws.gov/ecp/species/4482

## Amphibians

NAME
STATUS
California Red-legged Frog Rana draytonii
Threatened
There is final critical habitat for this species. The location of the critical habitat is not available.
Species profile: https://ecos.fws.gov/ecp/species/2891
California Tiger Salamander Ambystoma californiense Threatened
Population: U.S.A. (Central CA DPS)
There is final critical habitat for this species. The location of the critical habitat is not available. Species profile: https://ecos.fws.gov/ecp/species/2076

## Fishes

NAME
STATUS
Delta Smelt Hypomesus transpacificus
Threatened
There is final critical habitat for this species. The location of the critical habitat is not available. Species profile: https://ecos.fws.gov/ecp/species/321

## Insects

NAME STATUS

Monarch Butterfly Danaus plexippus
Candidate
No critical habitat has been designated for this species.
Species profile: https://ecos.fws.gov/ecp/species/9743
Valley Elderberry Longhorn Beetle Desmocerus californicus dimorphus Threatened
There is final critical habitat for this species. The location of the critical habitat is not available.
Species profile: https://ecos.fws.gov/ecp/species/7850

## Crustaceans

NAME
STATUS
Conservancy Fairy Shrimp Branchinecta conservatio
There is final critical habitat for this species. The location of the critical habitat is not available.
Species profile: https:///ecos.fws.gov/ecp/species/8246
Vernal Pool Fairy Shrimp Branchinecta lynchi Threatened
There is final critical habitat for this species. The location of the critical habitat is not available. Species profile: https://ecos.fws.gov/ecp/species/498

## Vernal Pool Tadpole Shrimp Lepidurus packardi

There is final critical habitat for this species. The location of the critical habitat is not available. Species profile: https://ecos.fws.gov/ecp/species/2246

## Critical habitats

THERE ARE NO CRITICAL HABITATS WITHIN YOUR PROJECT AREA UNDER THIS OFFICE'S JURISDICTION.

## Duffy, Shawn@DOT

$\begin{array}{ll}\text { From: } & \text { NMFS SpeciesList - NOAA Service Account <nmfs.wcrca.specieslist@noaa.gov> } \\ \text { Sent: } & \text { Wednesday, January 19, 2022 6:09 PM } \\ \text { To: } & \text { Duffy, Shawn@DOT } \\ \text { Subject: } & \text { Federal ESA - NOAA Fisheries Species List Re: 03-0H360 Richards Blvd Interchange }\end{array}$

EXTERNAL EMAIL. Links/attachments may not be safe.
Please retain a copy of each email request that you send to NOAA at nmfs.wcrca.specieslist@noaa.gov as proof of your official Endangered Species Act SPECIES LIST. The email you send to NOAA should include the following information: your first and last name; email address; phone number; federal agency name (or delegated state agency such as Caltrans); mailing address; project title; brief description of the project; and a copy of a list of threatened or endangered species identified within specified geographic areas derived from the NOAA Fisheries, West Coast Region, California Species List Tool. You may only receive this instruction once per week. If you have questions, contact your local NOAA Fisheries liaison.
From: Duffy, Shawn@DOT
Sent: Wednesday, January 19, 2022 6:08 PM
To: nmfs.wcrca.specieslist@noaa.gov
Subject: Re: 03-0H360 Richards Blvd Interchange
Quad Name Davis
Quad Number 38121-E6
ESA Anadromous Fish
SONCC Coho ESU (T) -
CCC Coho ESU (E) -
CC Chinook Salmon ESU (T) -
CVSR Chinook Salmon ESU (T) - X
SRWR Chinook Salmon ESU (E) - X
NC Steelhead DPS (T) -
CCC Steelhead DPS (T) -
SCCC Steelhead DPS (T) -
SC Steelhead DPS (E) -
CCV Steelhead DPS (T) - ..... X
Eulachon (T) -
sDPS Green Sturgeon (T) - ..... X
ESA Anadromous Fish Critical Habitat
SONCC Coho Critical Habitat -
CCC Coho Critical Habitat -CC Chinook Salmon Critical Habitat -
CVSR Chinook Salmon Critical Habitat -
SRWR Chinook Salmon Critical Habitat -NC Steelhead Critical Habitat -CCC Steelhead Critical Habitat -
SCCC Steelhead Critical Habitat -SC Steelhead Critical Habitat -

## ESA Marine Invertebrates

## ESA Marine Invertebrates Critical Habitat

Black Abalone Critical Habitat -

## ESA Sea Turtles

## East Pacific Green Sea Turtle (T) -

Olive Ridley Sea Turtle (T/E) -
Leatherback Sea Turtle (E) -
North Pacific Loggerhead Sea Turtle (E) -

## ESA Whales

Blue Whale (E) -
Fin Whale (E) -
Humpback Whale (E) -
Southern Resident Killer Whale (E) -
North Pacific Right Whale (E) -
Sei Whale (E) -
Sperm Whale (E) -

## ESA Pinnipeds

Guadalupe Fur Seal (T) -
Steller Sea Lion Critical Habitat -

## Essential Fish Habitat

Coho EFH -
Chinook Salmon EFH - X
Groundfish EFH -
Coastal Pelagics EFH -
Highly Migratory Species EFH -

## MMPA Species (See list at left)

## ESA and MMPA Cetaceans/Pinnipeds

## See list at left and consult the NMFS Long Beach office

 562-980-4000MMPA Cetaceans -
MMPA Pinnipeds -

Quad Number 38121-E5

## ESA Anadromous Fish

SONCC Coho ESU (T) -
CCC Coho ESU (E) -
CC Chinook Salmon ESU (T) -
CVSR Chinook Salmon ESU (T) - X
SRWR Chinook Salmon ESU (E) - X
NC Steelhead DPS (T) -
CCC Steelhead DPS (T) -
SCCC Steelhead DPS (T) -
SC Steelhead DPS (E) -
CCV Steelhead DPS (T) - X
Eulachon (T) -
sDPS Green Sturgeon (T) - X

## ESA Anadromous Fish Critical Habitat

SONCC Coho Critical Habitat -
CCC Coho Critical Habitat -
CC Chinook Salmon Critical Habitat -
CVSR Chinook Salmon Critical Habitat - X
SRWR Chinook Salmon Critical Habitat - X
NC Steelhead Critical Habitat -
CCC Steelhead Critical Habitat -
SCCC Steelhead Critical Habitat -
SC Steelhead Critical Habitat -
CCV Steelhead Critical Habitat - X
Eulachon Critical Habitat -
sDPS Green Sturgeon Critical Habitat - X

## ESA Marine Invertebrates

Range Black Abalone (E) -
Range White Abalone (E) -

## ESA Marine Invertebrates Critical Habitat

Black Abalone Critical Habitat -

## ESA Sea Turtles

East Pacific Green Sea Turtle (T) -
Olive Ridley Sea Turtle (T/E) -
Leatherback Sea Turtle (E) -
North Pacific Loggerhead Sea Turtle (E) -

## ESA Whales

Blue Whale (E)
Fin Whale (E) -
Humpback Whale (E) -
Southern Resident Killer Whale (E) -
North Pacific Right Whale (E) -
Sei Whale (E) -
Sperm Whale (E) -

## ESA Pinnipeds

Guadalupe Fur Seal (T) -
Steller Sea Lion Critical Habitat -

## Essential Fish Habitat

Coho EFH -
Chinook Salmon EFH - X

Groundfish EFH - X
Coastal Pelagics EFH -
Highly Migratory Species EFH -

## MMPA Species (See list at left)

## ESA and MMPA Cetaceans/Pinnipeds

See list at left and consult the NMFS Long Beach office
562-980-4000

MMPA Cetaceans -
MMPA Pinnipeds -

Shawn Duffy
Department of Transportation
North Region, Environmental Planning

Associate Environmental Planner/NS
Biologist
530-812-4313
Monday - Thursday, Fridays off

Selected Elements by Scientific Name
CALIFORNIA
California Department of Fish and Wildlife
California Natural Diversity Database

Query Criteria: Quad<span style='color:Red'> IS </span>(Davis (3812156)<span style='color:Red'> OR </span>Woodland (3812167)<span style='color:Red'> OR </span>Grays Bend (3812166)<span style='color:Red'> OR </span>Taylor Monument (3812165)<span style='color:Red'> OR </span>Sacramento West (3812155)<span style='color:Red'> OR </span>Clarksburg (3812145)<span style='color:Red'> OR </span>Saxon (3812146)<span style='color:Red'> OR </span>Dixon (3812147)<span style='color:Red'> OR </span>Merritt (3812157))

| Species | Element Code | Federal Status | State Status | Global Rank | State Rank | Rare Plant Rank/CDFW SSC or FP |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Agelaius tricolor tricolored blackbird | ABPBXB0020 | None | Threatened | G1G2 | S1S2 | SSC |
| Ambystoma californiense pop. 1 <br> California tiger salamander - central California DPS | AAAAA01181 | Threatened | Threatened | G2G3 | S3 | WL |
| Ammodramus savannarum <br> grasshopper sparrow | ABPBXA0020 | None | None | G5 | S3 | SSC |
| Antrozous pallidus pallid bat | AMACC10010 | None | None | G4 | S3 | SSC |
| Archoplites interruptus <br> Sacramento perch | AFCQB07010 | None | None | G2G3 | S1 | SSC |
| Ardea alba great egret | ABNGA04040 | None | None | G5 | S4 |  |
| Ardea herodias great blue heron | ABNGA04010 | None | None | G5 | S4 |  |


| Ferris' milk-vetch |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Astragalus tener var. tener alkali milk-vetch | PDFAB0F8R1 | None | None | G2T1 | S1 | 1B. 2 |
| Athene cunicularia burrowing owl | ABNSB10010 | None | None | G4 | S3 | SSC |
| Atriplex cordulata var. cordulata heartscale | PDCHE040B0 | None | None | G3T2 | S2 | 1B. 2 |
| Atriplex depressa brittlescale | PDCHE042LO | None | None | G2 | S2 | 1B. 2 |
| Bombus crotchii <br> Crotch bumble bee | IIHYM24480 | None | None | G3G4 | S1S2 |  |
| Bombus occidentalis western bumble bee | IIHYM24250 | None | None | G2G3 | S1 |  |
| Branchinecta conservatio Conservancy fairy shrimp | ICBRA03010 | Endangered | None | G2 | S2 |  |
| Branchinecta lynchi vernal pool fairy shrimp | ICBRA03030 | Threatened | None | G3 | S3 |  |
| Branchinecta mesovallensis midvalley fairy shrimp | ICBRA03150 | None | None | G2 | S2S3 |  |
| Buteo swainsoni | ABNKC19070 | None | Threatened | G5 | S3 |  |

California Natural Diversity Database

| Species | Element Code | Federal Status | State Status | Global Rank | State Rank | Rare Plant Rank/CDFW SSC or FP |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Carex comosa bristly sedge | PMCYP032Y0 | None | None | G5 | S2 | 2B. 1 |
| Centromadia parryi ssp. parryi pappose tarplant | PDAST4R0P2 | None | None | G3T2 | S2 | 1B. 2 |
| Charadrius montanus mountain plover | ABNNB03100 | None | None | G3 | S2S3 | SSC |
| Charadrius nivosus nivosus western snowy plover | ABNNB03031 | Threatened | None | G3T3 | S2 | SSC |
| Chloropyron palmatum palmate-bracted bird's-beak | PDSCROJOJO | Endangered | Endangered | G1 | S1 | 1B. 1 |
| Cicindela hirticollis abrupta <br> Sacramento Valley tiger beetle | IICOL02106 | None | None | G5TH | SH |  |
| Circus hudsonius northern harrier | ABNKC11011 | None | None | G5 | S3 | SSC |
| Coccyzus americanus occidentalis western yellow-billed cuckoo | ABNRB02022 | Threatened | Endangered | G5T2T3 | S1 |  |
| Desmocerus californicus dimorphus valley elderberry longhorn beetle | IICOL48011 | Threatened | None | G3T2 | S3 |  |
| Egretta thula snowy egret | ABNGA06030 | None | None | G5 | S4 |  |
| Elanus leucurus white-tailed kite | ABNKC06010 | None | None | G5 | S3S4 | FP |
| Elderberry Savanna <br> Elderberry Savanna | CTT63440CA | None | None | G2 | S2.1 |  |
| Emys marmorata western pond turtle | ARAAD02030 | None | None | G3G4 | S3 | SSC |
| Eryngium jepsonii Jepson's coyote-thistle | PDAPIOZ130 | None | None | G2 | S2 | 1B. 2 |
| Extriplex joaquinana <br> San Joaquin spearscale | PDCHE041F3 | None | None | G2 | S2 | 1B. 2 |
| Falco columbarius merlin | ABNKD06030 | None | None | G5 | S3S4 | WL |
| Fritillaria pluriflora adobe-lily | PMLILOVOFO | None | None | G2G3 | S2S3 | 1B. 2 |
| Gonidea angulata western ridged mussel | IMBIV19010 | None | None | G3 | S1S2 |  |
| Great Valley Cottonwood Riparian Forest Great Valley Cottonwood Riparian Forest | CTT61410CA | None | None | G2 | S2.1 |  |
| Hibiscus lasiocarpos var. occidentalis woolly rose-mallow | PDMALOH0R3 | None | None | G5T3 | S3 | 1B. 2 |
| Hypomesus transpacificus <br> Delta smelt | AFCHB01040 | Threatened | Endangered | G1 | S1 |  |


| Species | Element Code | Federal Status | State Status | Global Rank | State Rank | Rare Plant Rank/CDFW SSC or FP |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lasionycteris noctivagans silver-haired bat | AMACC02010 | None | None | G3G4 | S3S4 |  |
| Lasiurus cinereus hoary bat | AMACC05030 | None | None | G3G4 | S4 |  |
| Laterallus jamaicensis coturniculus California black rail | ABNME03041 | None | Threatened | G3G4T1 | S1 | FP |
| Lepidium latipes var. heckardii <br> Heckard's pepper-grass | PDBRA1M0K1 | None | None | G4T1 | S1 | 1B. 2 |
| Lepidurus packardi vernal pool tadpole shrimp | ICBRA10010 | Endangered | None | G4 | S3S4 |  |
| Lilaeopsis masonii <br> Mason's lilaeopsis | PDAPI19030 | None | Rare | G2 | S2 | 1B. 1 |
| Linderiella occidentalis California linderiella | ICBRA06010 | None | None | G2G3 | S2S3 |  |
| Melospiza melodia song sparrow ("Modesto" population) | ABPBXA3010 | None | None | G5 | S3? | SSC |
| Myrmosula pacifica <br> Antioch multilid wasp | IIHYM15010 | None | None | GH | SH |  |
| Navarretia leucocephala ssp. bakeri <br> Baker's navarretia | PDPLMOC0E1 | None | None | G4T2 | S2 | 1B. 1 |
| Neostapfia colusana Colusa grass | PMPOA4C010 | Threatened | Endangered | G1 | S1 | 1B. 1 |
| Nycticorax nycticorax <br> black-crowned night heron | ABNGA11010 | None | None | G5 | S4 |  |
| Oncorhynchus mykiss irideus pop. 11 steelhead - Central Valley DPS | AFCHA0209K | Threatened | None | G5T2Q | S2 |  |
| Oncorhynchus tshawytscha pop. 11 chinook salmon - Central Valley spring-run ESU | AFCHA0205L | Threatened | Threatened | G5T1T2Q | S2 |  |
| Oncorhynchus tshawytscha pop. 7 chinook salmon - Sacramento River winter-run ESU | AFCHA0205B | Endangered | Endangered | G5T1Q | S1 |  |
| Plagiobothrys hystriculus bearded popcornflower | PDBOROVOH0 | None | None | G2 | S2 | 1B. 1 |
| Plegadis chihi white-faced ibis | ABNGE02020 | None | None | G5 | S3S4 | WL |
| Pogonichthys macrolepidotus <br> Sacramento splittail | AFCJB34020 | None | None | GNR | S3 | SSC |
| Progne subis purple martin | ABPAU01010 | None | None | G5 | S3 | SSC |
| Puccinellia simplex <br> California alkali grass | PMPOA53110 | None | None | G3 | S2 | 1B. 2 |
| Sidalcea keckii <br> Keck's checkerbloom | PDMAL110D0 | Endangered | None | G2 | S2 | 1B. 1 |

Selected Elements by Scientific Name
CALIFORNIA
California Department of Fish and Wildlife
California Natural Diversity Database

| Species | Element Code | Federal Status | State Status | Global Rank | State Rank | Rare Plant Rank/CDFW SSC or FP |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Spea hammondii western spadefoot | AAABF02020 | None | None | G2G3 | S3 | SSC |
| Spirinchus thaleichthys longfin smelt | AFCHB03010 | Candidate | Threatened | G5 | S1 |  |
| Symphyotrichum lentum Suisun Marsh aster | PDASTE8470 | None | None | G2 | S2 | 1B. 2 |
| Taxidea taxus <br> American badger | AMAJF04010 | None | None | G5 | S3 | SSC |
| Thamnophis gigas giant gartersnake | ARADB36150 | Threatened | Threatened | G2 | S2 |  |
| Trifolium hydrophilum saline clover | PDFAB400R5 | None | None | G2 | S2 | 1B. 2 |
| Tuctoria mucronata <br> Crampton's tuctoria or Solano grass | PMPOA6N020 | Endangered | Endangered | G1 | S1 | 1B. 1 |
| Valley Oak Woodland Valley Oak Woodland | CTT71130CA | None | None | G3 | S2.1 |  |
| Vireo bellii pusillus least Bell's vireo | ABPBW01114 | Endangered | Endangered | G5T2 | S2 |  |
| Xanthocephalus xanthocephalus yellow-headed blackbird | ABPBXB3010 | None | None | G5 | S3 | SSC |

Record Count: 70

## Inventory of Rare and Endangered Plants of Califormia

## Search Results

28 matches found. Click on scientific name for details

Search Criteria: 9 -Quad include [3812155:3812165:3812145:3812147:3812167:3812157:3812166:3812156:3812146]

| - SCIENTIFIC |  |  |  |  |  |  |  |  | CA |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  | RARE |  |
|  |  |  |  | BLOOMING | FED | State | Global |  | PLANT |  |
| NAME | COMMON NAME | FAMILY | LIFEFORM | PERIOD | LIST | LIST | RANK | RANK | RANK | PHOTO |
| Astregalus | depauperate | Fabaceae | annual herb | Mar-Jun | None | None | G4 | S4 | 4.3 |  |
| pauperculus | milk-vetch |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  | 02012 |
|  |  |  |  |  |  |  |  |  |  | Tim |
|  |  |  |  |  |  |  |  |  |  | Kellison |
| Astragalus tener | Ferris' milk-vetch | Fabaceae | annual herb | Apr-May | None | None | G2T1 | S1 | 18.1 | No Photo |
| var. ferrisiae |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  | Available |
| Astragalus tener | alkali milk-vetch | Fabaceae | annual herb | Mar-Jun | None | None | G2T1 | S1 | 18.2 | No Photo |
| var. tener |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  | Available |
| Atriplex cordulato var. cordulata | heartscale | Chenopodiaceae | annual herb | Apr-Oct | None | None | G3T2 | S2 | 18.2 |  |
|  |  |  |  |  |  |  |  |  |  | (1) 1994 |
|  |  |  |  |  |  |  |  |  |  | Robert E. |
|  |  |  |  |  |  |  |  |  |  | Preston, |
|  |  |  |  |  |  |  |  |  |  | Ph.D. |
| Atriplex depressa | brittlescale | Chenopodiaceae | annual herb | Apr-Oct | None | None | G2 | S2 | 18.2 |  |
|  |  |  |  |  |  |  |  |  |  | (1)2009 |
|  |  |  |  |  |  |  |  |  |  | Zoya |
|  |  |  |  |  |  |  |  |  |  | Akulova |
| Carex comosa | bristly sedge | Cyperaceae | perennial | May-Sep | None | None | GS | S2 | 2 B .1 |  |
|  |  |  | rhizomatous |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  | Dean Wm. |
|  |  |  |  |  |  |  |  |  |  | Taylor 1997 |
| Centromadia | pappose | Asteraceae | annual herb | May-Nov | None | None | G3T2 | S2 | 18.2 |  |
| parryi ssp. parryi | tarplant |  |  |  |  |  |  |  |  | No Photo |


| Centromadia | Parry's rough | Asteraceae | annual herb | May-Oct | None None G3T3 | S3 | 4.2 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| parryissp. rudis | tarplant |  |  |  |  |  |  |


| Chloropypron poimatum | palmate-bracted | Orobanchaceae | annual herb | May-Oct | FE | CE | G1 | S1 | 1 B .1 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | bird's-beak |  | (hemiparasitic) |  |  |  |  |  |  | No Photo |
|  |  |  |  |  |  |  |  |  |  | Available |
| Eryngium jepsonii | Jepson's coyote- | Apiaceae | perennial herb | Apr-Aug | None | None | G2 | S2 | 18.2 |  |
|  | thistle |  |  |  |  |  |  |  |  | No Photo |
|  |  |  |  |  |  |  |  |  |  | Available |







Showing 1 to 28 of $2 B$ entries

## Suggested Citation:

California Native Plant Society, Rare Plant Program. 2022. Inventory of Rare and Endangered Piants of California (online edition, v9.01
1.0). Website https://www.rareplants.cnps.org [accessed 20 January 2022].

Appendix C
Tribal Consultation Letters

# 23 Russell Boulevard - Davis, California 95616 <br> 530/757-5610 - FAX: 530/757-5660 - TDD: 530/757-5666 <br>  

August 28, 2018

Cultural Committee
Ione Band of Miwok Indians
PO Box 699
9252 Bush St, Suite 2
Plymouth, CA 95669

## Re: Formal Notification of I-80/Richards Boulevard Interchange Improvements Project

In response to your request for formal notification of projects for which the City of Davis will prepare a negative declaration, mitigated negative declaration, or environmental impact report pursuant to Public Resources Code section 21080.3.1(b), this letter serves as formal notification of the City's consideration of the I-80/Richards Boulevard Interchange Improvements Project (Project).

Accordingly, as required by Public Resources Code section 21080.3.1(d), this letter provides a brief description of the Project and its location.

The Project would reconfigure the westbound I-80 ramps from a full cloverleaf (Type L10) to a tight diamond (Type L-1) by consolidating the two off-ramps of the I-80/Richards Boulevard interchange into a single diagonal off-ramp; and the two on-ramps into a single diagonal on-ramp. The resulting westbound I-80 ramp terminal intersection would include signals optimized for the design year traffic forecast. The westbound I-80 on-ramp would require widening of I-80 over the existing bike and pedestrian tunnel.

The eastbound I-80 ramp intersection would remain as a cloverleaf (Type L-8). Project improvements include widening the eastbound off-ramp to include a right-turn lane and two leftturn lanes. Outside the State access control limits, Richards Boulevard would be widened to provide two southbound through movements at the Research Park Drive/Richards Boulevard intersection.

The Project would modify the Olive Drive/Richards Boulevard intersection providing the width, lane geometry, and right-of-way necessary for future developments on Olive Drive. The existing nearside bus stop on Richards Boulevard near Olive Drive would be relocated to the north of the Olive Drive/Richards Boulevard intersection. Along eastbound Richards Boulevard, improvements would connect the mixed-use paths; include a left-turn lane, a through lane, and a combination through-right lane on the intersection entrance; and include two through lanes on the eastbound intersection egress.

Between the Olive Drive/Richards Boulevard intersection and the westbound I-80 ramp terminal intersection, improvements would include widening Richards Boulevard and installing a raised median to restrict left turn movements.

The Project would include construction of a shared-use path along the west side of Richards Boulevard replacing the existing sidewalk, and serving both bicyclists and pedestrians. The shared-use path would connect to the existing path south of Olive Drive, diverge from Richards Boulevard to pass under the westbound I-80 on-ramp, then loop up to connect with the Richards Boulevard overcrossing. After passing over the existing structure, the shared-use path would terminate at the Research Park Drive/Richards Boulevard intersection. The Project would widen the existing Class II bicycle lanes along Richards Boulevard between Olive Drive and Research Park Drive to a minimum of 7 feet. A map identifying the Project is attached to this letter.

Environmental Science Associates (ESA) cultural resources staff conducted a records search for the Project at the Northwest Information Center (NWIC) of the California Historical Resources Information System (April 24, 2018; File No. 17-2544). The results indicate that there are no previously recorded archaeological or architectural resources in the project Area of Potential Effects (APE). The nearest known prehistoric archaeological site is approximately 0.25 mile west of the APE and would not be affected by the proposed project. There are also two sites informally recorded as "possible sites" further to the north on the University of California Davis campus. These sites would also not be affected by the proposed project.

An ESA Registered Professional Archaeologist completed a surface survey of the APE on August 8, 2018. The survey consisted of walking the paved and unpaved portions of the APE in narrow (no greater than 10 -meter-wide) transects, where feasible, to observe the existing conditions and identify cultural resources, if present. No prehistoric or historic-era cultural materials or other evidence of past human use or occupation were identified in the APE. The APE has a low archaeological sensitivity due to the environmental setting and previous extensive disturbance of the area.

Pursuant to Public Resources Code section 21080.3.1 (b) and (d), the Ione Band of Miwok Indians now has 30 days to inform the City, in writing, of its request to consult with the City on the Project. Such a request must provide the name of the Tribe's designated lead contact person and should be directed to lead agency contact information Katherine Hess, Community Development Administrator, at (530)757-5652 or khess@cityofdavis.org.

Please do not hesitate to contact me with any questions or concerns regarding the above.
Sincerely,


Katherine Hess, AICP
Community Development Administrator
Attachment: Project Map


August 28, 2018

Laverne Bill, Cultural Resources Department Manager
Yocha Dehe Wintun Nation
PO Box 18
Brooks, CA 95606
Re: Formal Notification of I-80/Richards Boulevard Interchange Improvements Project
Dear Mr. Bill:
This letter serves as formal notification of the City's consideration of the I-80/Richards Boulevard Interchange Improvements Project (Project).

Accordingly, as required by Public Resources Code section 21080.3.1(d), this letter provides a brief description of the Project and its location.

The Project would reconfigure the westbound I-80 ramps from a full cloverleaf (Type L10) to a tight diamond (Type L-1) by consolidating the two off-ramps of the I-80/Richards Boulevard interchange into a single diagonal off-ramp; and the two on-ramps into a single diagonal on-ramp. The resulting westbound I-80 ramp terminal intersection would include signals optimized for the design year traffic forecast. The westbound I-80 on-ramp would require widening of I-80 over the existing bike and pedestrian tunnel.

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Pursuant to Public Resources Code section 21080.3.1 (b) and (d), the Yocha Dehe Wintun Nation now has 30 days to inform the City, in writing, of its request to consult with the City on the Project. Such a request must provide the name of the Tribe's designated lead contact person and should be directed to lead agency contact information Katherine Hess, Community Development Administrator, at (530)757-5652 or khess@cityofdavis.org.

Please do not hesitate to contact me with any questions or concerns regarding the above.
Sincerely,


Katherine Hess, AICP
Community Development Administrator
Attachment: Project Map

August 28, 2018

Cortina Indian Rancheria of Wintun Indians
Charlie Wright, Chairperson
P.O. Box 1630

Williams, CA 95987
Re: Formal Notification of I-80/Richards Boulevard Interchange Improvements Project
Dear Mr. Wright:
This letter serves as formal notification of the City's consideration of the I-80/Richards Boulevard Interchange Improvements Project (Project).

Accordingly, as required by Public Resources Code section 21080.3.1(d), this letter provides a brief description of the Project and its location.

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Pursuant to Public Resources Code section 21080.3.1 (b) and (d), the Cortina Indian Rancheria of Wintun Indians now has 30 days to inform the City, in writing, of its request to consult with the City on the Project. Such a request must provide the name of the Tribe's designated lead contact person and should be directed to lead agency contact information Katherine Hess, Community Development Administrator, at (530)757-5652 or khess@cityofdavis.org.

Please do not hesitate to contact me with any questions or concerns regarding the above.
Sincerely,


Katherine Hess, AJCP
Community Development Administrator
Attachment: Project Map

## Yocha Dehe <br> (.iltural Risculircis

September 12, 2018

City of Davis - Community Development Attn: Katherine Hess, Administrator
23 Russell Boulevard
Davis, CA 95616
RE: I-80 Richards Boulevard Interchange Improvements Project
Dear Ms. Hess:
Thank you for your project notification letter dated, August 28, 2018, regarding cultural information on or near the proposed I-80 Richards Boulevard Interchange Improvements Project, Davis, Yolo County. We appreciate your effort to contact us and wish to respond.

The Cultural Resources Department has reviewed the project and concluded that it is within the aboriginal territories of the Yocha Dehe Wintun Nation. Therefore, we have a cultural interest and authority in the proposed project area.

Based on the information provided, Yocha Dehe Wintun Nation is not aware of any known cultural resources near this project site and a cultural monitor is not needed. However, we recommend cultural sensitivity training for any pre-project personnel. Please contact one of the individuals listed below to schedule the cultural sensitivity training, prior to the start of the project.

Lawrence Longee, Tribal Monitor<br>Yocha Dehe Wintun Nation<br>Office: (530) 605-6655<br>Email: Ilongee (olyochadehe-nsn.gov<br>Robert Geary, Tribal Monitor<br>Yocha Dehe Wintun Nation<br>Office: (530) 215-6180<br>Email: rgearyeayochadehe-nsn.gov

Please refer to identification number YD - 09062018-01 in correspondence concerning this project.
Thank you for providing us the opportunity to comment.
Sincerely,


Leland Kinter
Tribal Historic Preservation Officer

Appendix D Traffic Study

## Interstate 80 / Richards Boulevard Interchange

## Transportation Analysis Report



Prepared for:
City of Davis

June 2018

FehrłPEERS

# Transportation Analysis Report 

Interstate 80 / Richards Boulevard Interchange

03-YOL-80-PM 0.0/0.5, 04-SOL-80 PM 44.5/44.7

EA 03-0H360
Project ID 0315000148

June 2018

Prepared By:
David Stanek, PE
Date: 6/1/18

| Phone Number | 916-329-7332 |
| :--- | :--- |
| Firm Name | Fehr \& Peers |
| Location | Sacramento, CA |

Planning
Approved By: $\qquad$ Date: $\qquad$

Name
Title
Phone Number $\qquad$
Office Name
District/Region $\qquad$

Traffic Operations Approved By: $\qquad$ Date: $\qquad$

Name
Title $\qquad$
Phone Number $\qquad$
Office Name $\qquad$
District/Region $\qquad$

# Transportation Analysis Report 

Interstate 80 / Richards Boulevard Interchange

03-YOL-80-PM 0.0/0.5, 04-SOL-80 PM 44.5/44.7

EA 03-0H360
Project ID 0315000148

## June 2018

This report was prepared under my direction and responsible charge. I attest to the technical information contained herein and have judged the qualification of any technical specialists providing engineering data upon which recommendations, conclusions, and decisions are based.


6/1/18

David Stanek, P.E.
Date
Registered Professional Civil Engineer
Fehr \& Peers

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## Chapter 1. Introduction

This transportation analysis report was prepared for the Interstate $80(I-80)$ / Richards Boulevard Interchange project. The report contains the results and findings of the transportation operations analyses, while the detailed analysis calculations are compiled in a separately bound appendix.

### 1.1 Report Purpose

The purpose of this report is to analyze project design alternatives and their effects on the transportation network. The report focuses on a comparison of alternatives that are each designed to improve current and future traffic operations for intersections and roadways in City of Davis. Portions of the analysis results will also be used to comply with environmental impact analysis requirements for the California Environmental Quality Act (CEQA) and National Environmental Policy Act (NEPA).

### 1.2 Project Description

The project proposes to reconstruct the westbound ramps at the I-80/Richards Boulevard interchange by converting from a cloverleaf (Type L-12) to a tight diamond (Type L-1) configuration, construct a gradeseparated bicycle and pedestrian path along the west side of Richards Boulevard, and close the isolated westbound off-ramp to Olive Drive. The elements of the interchange reconstruction and associated intersection widening are listed below.

- Install a traffic signal at the new westbound ramp terminal intersection
- Install a ramp meter signal on the new westbound on-ramp with two metered lanes and an HOV bypass lane
- At Richards Boulevard/Olive Drive, widen the northbound approach to provide a second left-turn lane, the southbound approach to provide a second through lane, and the east leg to provide two receiving lanes and eastbound left, through, and right lanes (one each)
- At Richards Boulevard/I-80 Eastbound Ramps, widen the eastbound off-ramp approach to provide a second left-turn lane
- At Richards Boulevard/Cowell Boulevard/Research Park Drive, widen southbound Richards Boulevard to provide a second through lane


### 1.3 Project Alternatives

Figure 1 shows an initial design layout for the Build Alternative at the I-80/Richards Boulevard interchange. The No Build Alternative would maintain the current roadway configuration with the following exceptions at the Richards Boulevard/Olive Drive intersection.

- Under future year conditions, the westbound approach will be re-striped so that the bicycle lane extends to the intersection under a separate project.
- Under design year conditions, the eastbound approach is assumed to be restriped to provide bike lanes in both directions. and a separate eastbound right turn lane is assumed to be added to serve traffic from planned development east of Richards Boulevard.



## Chapter 2. Analysis Methodology

This chapter describes the study area and the methods used to analyze the transportation facilities.

### 2.1 Study Area

The transportation analysis study area is divided into a local street network and a freeway network. The local street network extends from First Street/D Street in downtown Davis along First Street and Richards Boulevard to Research Park Drive/Richards Boulevard/Cowell Boulevard in south Davis. The freeway network extends along I-80 from Old Davis Road to Mace Boulevard. Figure 2 shows the intersections, and freeway segments in the study area.

The study intersections are listed below.

1. First Street/D Street
2. First Street/E Street/Richards Boulevard
3. Olive Drive/Richards Boulevard
4. I-80 Westbound Ramps/Richards Boulevard
5. I-80 Eastbound Ramps/Richards Boulevard
6. Research Park Drive/Richards Boulevard/Cowell Boulevard

The freeway study segments are listed below.

Eastbound I-80

1. West of Old Davis Road On-ramp
2. Old Davis Road On-ramp
3. Old Davis Road to 1st Lane Drop
4. 1st Lane Drop to 2nd Lane Drop
5. Richards Boulevard Off-ramp
6. Richards Boulevard Off to On-ramp
7. Richards Boulevard On-ramp
8. Richards Boulevard to Chiles Road
9. Chiles Road Off-ramp
10. East of Chiles Road Off-ramp

(1)Study Intersection

Freeway Corridor
11. East of Mace Boulevard On-ramp
12. Mace Boulevard to Lane Drop
13. Lane Drop to Olive Drive
14. Olive Drive Off-ramp
15. Olive Drive to Richards Boulevard
16. Richards Boulevard Northbound Off-ramp
17. Richards Boulevard Northbound Off to On-ramp
18. Richards Boulevard Northbound On-ramp to Southbound Off-ramp
19. Richards Boulevard Southbound Off to On-ramp
20. Richards Boulevard to Old Davis Road
21. Old Davis Road Off-ramp
22. West of Old Davis Road

No new study intersections are added with the Build Alternative or under future analysis years. The freeway segments are modified in the westbound direction with the Build Alternative. The planned HOV lanes on I80 also modify the freeway study segments under design year conditions.

### 2.2 Data Collection

The intersection and freeway traffic counts were collected from 7:00 to 9:00 AM and 4:00 to 6:00 PM. The peak period counts included heavy vehicles, bicycles, and pedestrians. The intersection turning movement counts were collected in May 2016 on a typical midweek day.

The morning peak hour occurred from 8:00 to 9:00 AM, and the evening peak hour occurred from 5:00 to 6:00 PM. The network-wide peak hour factors were 0.92 and 0.94 during the morning and evening peak hours. The average network heavy vehicle percentages were 3 and 1 percent during the morning and evening peak hours, respectively. Figure 3 shows the peak hour vehicle turning movement volumes and lane configurations for the study intersections. Figure 4 shows the peak hour bicycle and pedestrian volumes.

Signal timing plans were obtained from the signal controllers under a previous project that developed optimized signal timings. New signal timings were implemented in January 2017 after the counts were collected, so the previous signal timing plans will be used for the existing conditions analysis. Existing traffic conditions, including peak hour vehicle queuing, were also observed under the previous project.

Existing lane configurations, turn pocket lengths, and intersection spacing were taken from Bing Maps. The lane configurations were confirmed in the field concurrent with the collection of posted speeds, bus stop locations, and parking restrictions. The intersection and roadway configuration for the Build Alternative was provided via the draft geometric approval drawing. The proposed project has a design exception for corner sight distance at the Richards Boulevard/I-80 Westbound Ramps intersection. The operations analysis model includes a 1 -second all-red time for the signal phases to offset the reduced corner sight distance.

Freeway mainline volumes were obtained from the Caltrans Performance Measurement System (PeMS). The data were averaged across weekdays in October 2016. Table 1 lists the peak hours and peak hour factors by direction. The AM and PM peak hour heavy vehicle percentages were assumed to be the same as the daily percentage of 9 percent as reported in the Caltrans Annual Average Daily Truck Traffic publication (http://www.dot.ca.gov/trafficops/census/docs/2015 aadt truck.pdf).

Table 1: Freeway Mainline Volume Data

|  | AM Peak Hour |  |  | PM Peak Hour |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Peak Hour | Peak Hour <br> Factor | Heavy Vehicle <br> Percentage | Peak Hour | Peak Hour <br> Factor | Heavy Vehicle <br> Percentage |
| Eastbound I-80 | $7: 15$ to 8:15 | 0.95 | $9 \%$ | $4: 00$ to $5: 00$ | 0.96 | $9 \%$ |
| Westbound I-80 | $8: 00$ to 9:00 | 0.98 | $9 \%$ | $4: 15$ to $5: 15$ | 0.99 | $9 \%$ |

Source: Caltrans PeMS (October 2016), Caltrans Annual Average Daily Truck Traffic (2015)

Freeway ramp volumes for the Richards Boulevard and Old Davis Road interchanges come from intersection counts taken in October 2016. The Olive Drive off-ramp was counted in May 2016. For the Mace Boulevard/Chiles Road ramps, data collected in May 2014 was used. For the ramps, the peak hour volumes were determined using the mainline peak hour. The freeway mainline and ramp volumes for the AM and PM peak hours are shown in Figure 5.

### 2.3 Travel Demand Forecasting

### 2.3.1 Base Year Model Development

The City of Davis travel demand forecasting model was used to prepare the traffic volumes for future conditions. A base year model validation was performed to determine how well the model replicates existing traffic volumes. We reviewed base year model land uses, roadway network, link properties (speed, functional classification, etc.), and model traffic analysis zone (TAZ) centroid connections in the study area. Based on the review, land uses, network connections, and link speed and capacity were adjusted (see appendix for a list of model changes).

The model validation process involved running the model, checking the results against existing traffic volumes, and then adjusting input parameters in an iterative manner. This static sub-area validation method was performed on roadways near or parallel to the I-80/Richards Boulevard interchange.

The sub-area validation results were compared to the following validation thresholds discussed in 2017 California Regional Transportation Plan Guidelines (CTC, January 2017):

- The two-way sum of the volumes on all roadway links for which counts are available should be within 10 percent of the counts.
- At least 75 percent of the roadway links for which counts are available should be within the maximum desirable deviation, which ranges from approximately 14 to 68 percent depending on total volume (the larger the volume, the less deviation is permitted).
- The percent root mean square error ( $\mathrm{RMSE}^{1}$ ) should not exceed 40 percent.
- The correlation coefficient ${ }^{2}$ between the actual ground counts and the estimated traffic volumes should be greater than 88 percent.

Table 2 presents the results of the base year forecast model validation. See the appendix for detailed results.

- Mainline model volumes compare well to I-80 mainline count volumes in the peak directions: the westbound direction under AM peak hour and in the eastbound direction under PM peak hour.
- The overall model was improved; however, a few links could not be validated within the Caltrans standard deviation. This includes the I-80 Westbound off-ramp to southbound Richards Boulevard in the AM peak hour, the I-80 Eastbound on-ramp at Old Davis Road in the PM peak hour, and the I-80 Westbound off-ramp at Olive Drive in the PM peak hour.
- The model is overly sensitive to the balance of traffic between I-80 eastbound off ramp at Olive Drive and at Richards Boulevard with only minor changes in speed.
- The model generally overestimates traffic on study intersections in downtown Davis, especially during the AM peak hour.

Table 2: Base Year Forecast Model Validation

| Validation Statistic | Acceptance Criterion ${ }^{1}$ | Model Result |  |
| :---: | :---: | :---: | :---: |
|  |  | AM Peak Hour | PM Peak Hour |
| Model/Count Ratio | - | 1.03 | 0.97 |
| Percent of Links within Caltrans Standard Deviations | > $75 \%$ | 83\% | 87\% |
| Percent RMSE | $\leq 30 \%$ | 24\% | 25\% |
| Correlation Coefficient | > 0.88 | 0.99 | 0.99 |

Note: 1. 2017 California Regional Transportation Plan Guidelines (CTC, January 2017)
Source: Fehr \& Peers, 2018

A dynamic validation test was also performed to evaluate the model's sensitivity to changes in the roadway network. Pole Line Road at the I-80 overcrossing was increased to 4 lanes between Fifth Street and Cowell

[^7]Boulevard. The overall screen line of volumes at Richards Boulevard, Pole Line Road, and Mace Boulevard over I-80 increased by 3 percent in the AM peak hour and 5 percent in the PM peak hour. Volumes appropriately shifted from Richards Boulevard and Mace Boulevard to Pole Line Road with the increase in capacity.

### 2.3.2 Cumulative Year Model Development

Similar to the base year model, the cumulative year land use and roadway network inputs were reviewed. In addition to the roadway network adjustments identified for the base year model validation, the UC Davis land use growth was adjusted to the latest projections in the Long Range Development Plan (LRDP).

As directed by Caltrans staff, the planned I-80 HOV lanes were assumed to extend through the study area. This was accounted for by adding the capacity of the HOV lane (assumed to be 900 vehicles per hour) to the capacity of the three mainline travel lanes (an additional 300 vehicles per hour per lane).

The cumulative year model includes build-out of the city's general plan under 2035 conditions plus the following proposed projects.

- Mace Ranch Innovation Center - located north of I-80 and east of Mace Boulevard that would include 1.51 million square feet of research and development/office, 884,000 square feet of manufacturing, 150,000 square feet of hotel/conference center, and 100,000 square feet of retail land uses
- Davis Hotel and Conference Center - located west of Richards Boulevard between Olive Drive and I-80 that would replace the 43 -room University Inn \& Suites Hotel and Caffe Italia restaurant with a 132 -room Embassy Suites hotel, a restaurant, and a 14,900 square-foot conference center
- Nishi/West Olive Drive Development - located in the triangle formed by I-80, the Union Pacific Railroad, and Putah Creek with vehicle connections to Olive Drive and the UC Davis campus that would include 650 residential units, 325,000 square feet of research and development/office, and 20,000 square feet of retail uses
- Lincoln40 Apartments - located on Olive Drive east of Richards Boulevard that would include 130 apartments oriented to students attending UC Davis
- Sterling Apartments - located on Fifth Street east of Pole Line Road that would include 198 apartments oriented to students attending UC Davis

The Mace Ranch Innovation Center and Nishi/West Olive Drive projects have not been approved. The first is on hold and the second was not approved by the voters in an election. However, the properties are likely to be developed in some fashion by cumulative conditions. For this analysis, the previously proposed projects were assumed although the actual development may be smaller in scope.

Forecasting future traffic volumes is inherently uncertain. In addition to the assumptions for land use and roadway network changes, the following limitations are noted below.

- The effect of transportation network companies (such as Uber or Lyft) on trip making patterns is not included in the model.
- The effect of internet shopping on passenger or freight travel is not included.


### 2.3.3 Analysis Year Forecasts

To account for model error, the cumulative year model volumes for the freeway and ramps were adjusted using a process known as the "difference method," which adjusts model output volume forecasts based on incremental growth from existing conditions using the following formula:

> Forecast Volume $=$ Existing Traffic Count +
> (Cumulative Year Raw Model Volume - Base Year Raw Model Volume)

In addition, the forecasted growth was increased to account for growth between the cumulative model year of 2035 and the project design year of 2042. For most locations, the growth rate from 2035 to 2042 was assumed to continue at the same rate predicted by the model from 2016 to 2035 , which results in about 37 percent additional growth for the seven years from 2035 to 2042. However, land uses along Olive Drive are assumed to be built out by 2035 conditions, so the additional growth from 2035 to 2042 was reduced from 37 to 10 percent. The construction year (2022) volumes were prepared using linear interpolation, which assumed a constant rate of traffic growth between existing and cumulative year (2035) conditions.

For the intersection forecasts, the difference method was applied using trip tables. An origin-destination trip table was estimated from the existing conditions peak hour counts using the base year model trip table as a seed matrix. Then, subarea trip tables were extracted from the base year and cumulative year models. The difference between the model matrices, factored to extrapolate to design year conditions, was added to the existing conditions matrix to generate the design year trip table, which was then assigned to the project area network. For the freeway forecasts, the difference method was applied to the link counts.

As part of the forecasting process, all peak hour volumes were rounded to the nearest ten vehicles per hour to acknowledge that these volumes are estimated projections. In general, decreases in turning movement volumes greater than 10 vehicles per hour were not allowed between existing and design year conditions with the following exception. During the PM peak hour, the eastbound through at First Street/D Street, eastbound right turn at First Street/E Street/Richards Boulevard, and southbound through at Olive Drive/Richards Boulevard were allowed to decrease due to the new connection to UC Davis via Olive Drive and the Nishi/West Olive development. Additionally, volumes were balanced through the study area.

Bicycle and pedestrian volumes were assumed to grow proportionally to the land use growth in the study area. In the project vicinity, land use grows by about 17 percent between the base year and cumulative year models. Extrapolating this growth from the cumulative year of 2035 to the design year of 2042 conditions, increases the total growth to about 23 percent. This value was rounded up to 25 percent and used to generate the design year bicycle and pedestrian volumes. Additionally, the minimum bicycle turning
movement volume was set to 2 bicycles per hour, and the bicycle volumes were balanced through the study intersections.

The traffic volumes for the Build Alternative will be the same as the No Build Alternative except for reassigning traffic based on the new roadway configuration. For example, the reconfiguration of the westbound ramps from four to two at the l-80/Richards Boulevard interchange will shift the loop off-ramp volumes to become off-ramp left-turn movements at the new signalized intersection. The closure of the Olive Drive westbound off-ramp will shift the traffic to the westbound off-ramp to northbound Richards Boulevard. The distribution of the Olive Drive off-ramp traffic destinations were determined using a selectlink model run so that the volumes were assigned to the appropriate turning movements at the study intersections.

Under design year conditions, turning volumes at the Richards Boulevard/Cowell Boulevard/Research Park Drive intersection were adjusted based on preliminary intersection operations. The initial forecasted volume for the left turn from Richards Boulevard to Research Park Drive would have resulted in queues exceeding the storage length. Drivers could easily avoid this queue by continuing through onto Cowell Boulevard to make a left turn midblock or at Drew Avenue. As a result, 50 vph was shifted during the AM peak hour, and 150 vph was shifted during the PM peak hour from the left turn to the through movement. Similarly, 100 vph was shifted during the PM peak hour from the right turn from Research Park Drive to Richards Boulevard to the through movement from Cowell Boulevard to Richards Boulevard.

### 2.4 Traffic Operations Analysis

### 2.4.1 Intersections

The study intersections were analyzed using the performance measures of intersection delay and level of service (LOS). LOS is a qualitative measure of traffic operating conditions that assigns a letter rating, from A (the best) to $F$ (the worst). These ratings represent the perspective of drivers and are an indication of the comfort and convenience associated with driving. The descriptions of letter ratings and the delay thresholds for signalized and unsignalized intersections are provided in Table 3. For unsignalized intersections with some movements uncontrolled, the intersection LOS is determined by the controlled movement with the highest delay.

Intersection operations were analyzed under AM and PM peak period conditions (7:00 to 9:00 AM and 4:00 to 6:00 PM) using the Vissim (Version 9) microsimulation software. Traffic simulation analysis allows for the direct modeling of vehicle, bicycle, and pedestrian interactions, delays due to queues that block turn pockets or adjacent lanes, bus routes and stops, and congestion that either constrains vehicles from reaching downstream intersections or causes queues that create additional delay at upstream intersections. The Vissim software was applied consistent with the methodology presented in the Highway Capacity Manual, 6th Edition (Transportation Research Board, 2016). The analysis results are an average of ten model runs
using different random seed values. Intersection delay and LOS are based on the Vissim results, and the average maximum queue lengths from Vissim are reported.

Table 3: Intersection LOS Thresholds

| LOS | Description | Delay ${ }^{1}$ |  |
| :---: | :---: | :---: | :---: |
|  |  | Signalized | Unsignalized |
| A | Operations with very low delay occurring with favorable progression and/or short cycle length. | $\leq 10$ | $\leq 10$ |
| B | Operations with low delay occurring with good progression and/or short cycle lengths. | > 10 to 20 | $>10$ to 15 |
| C | Operations with average delays resulting from fair progression and/or longer cycle lengths. Individual cycle failures begin to appear. | > 20 to 35 | > 15 to 25 |
| D | Operations with longer delays due to a combination of unfavorable progression, long cycle lengths, or high V/C ratios. Many vehicles stop and individual cycle failures are noticeable. | > 35 to 55 | >25 to 35 |
| E | Operations with high delay values indicating poor progression, long cycle lengths, and high V/C ratios. Individual cycle failures are frequent occurrences. | > 55 to 80 | > 35 to 50 |
| F | Operation with delays unacceptable to most drivers occurring due to over saturation, poor progression, or very long cycle lengths. | $\begin{gathered} >80 \text { or } \\ \mathrm{v} / \mathrm{c}>1^{2} \end{gathered}$ | $\begin{gathered} >50 \text { or } \\ \mathrm{v} / \mathrm{c}>1^{2} \end{gathered}$ |
| Notes: | elay is reported in seconds per vehicle. <br> olume-to-capacity ratio is greater than 1 (demand exceeds capacity). way Capacity Manual (Transportation Research Board, 2010) |  |  |

The following key assumptions were included in the intersection operations analysis.

- The truck percentages collected during the May 2016 counts were used for to develop a networkwide value. The existing values were used for all future analysis years.
- For existing conditions, bicycle and pedestrian volumes are based on observed data. For future conditions, the minimum conflicting bicycle volume was set to 2 bicycles per hour, and the minimum pedestrian volume was 5 pedestrians per hour.
- Input volumes for vehicles, bicycles and pedestrians are based on the 15 -minute flow rates collected during the traffic counts. Although traffic volumes change between analysis years, the arrival distribution of volumes across the peak period is assumed to stay the same as existing conditions for the one-hour seeding period. For the one-hour analysis period, the input volumes were adjusted to have a peak hour factor of 0.92 for the AM peak hour and 0.95 for the PM peak hour under future years. The 15 -minute interval in the peak hour with the highest flow rate was kept the same for all analysis scenarios.


### 2.4.2 Simulation Model Development

Development of the street network and traffic volumes that comprise the Vissim models required the input of geometric, traffic control and traffic flow data, each of which is described in this section. An overview of the micro-simulation model development process is described below.

Roadway geometric data (traffic lanes, turn pockets, bus lanes, bus stop locations, etc.) were gathered using aerial photographs and field observations. Lane configurations were initially taken from aerial photographs and were then confirmed or revised based on field observations.

City staff provided signal timing plans for the traffic signals in the study area. The signal timing settings include vehicle and pedestrian signal phases. The posted speed limits for streets in the study area were collected during field observations. Maximum vehicle speeds in the model are consistent with posted speed limits, although random speed variability is assigned to each vehicle, causing them to drive above or below the speed limit, to mimic prevailing driver behavior.

For each peak period, the analysis period is two hours with a 15 -minute seeding period. The volume inputs vary each 15 minutes based on the traffic counts. The peak hour was determined based on the highest consecutive four 15 -minute interval period based on the overall network volume. The routing decisions for the two-hour analysis period are based on the peak hour volumes. That is, the travel patterns during the peak hour are assumed to be the same for the two-hour peak period. When developing the peak hour volumes, the volumes were balanced between intersections to reduce unexpected changes in through volumes between adjacent intersections. Where balancing was performed, the volumes were balanced to the higher volume to provide for a conservative analysis.

The pedestrian and bicycle volumes were directly modeled through use of pedestrian crossing counts and bicycle turning movement counts taken at the same time as the intersection vehicle turning movement counts. Bicycle peak hour volumes were also balanced through the network.

The Vissim models were validated to existing conditions using criteria suggested by the Federal Highway Administration (FHWA) and additional criteria developed by Fehr \& Peers. A number of iterations were required to successively adjust the default Vissim parameters for driver behavior until the model was validated to observed conditions.

Because micro-simulation models like Vissim rely on the random arrival of vehicles, multiple runs are needed to provide a reasonable level of statistical accuracy and validity. The models are run up to twenty times (each using a different random seed number). Starting with the first ten runs, runs that are clear outliers are reviewed to determine if coding errors are present. If no obvious error is found, the run is discarded and replaced with a subsequent run. This process is repeated until ten acceptable runs remain. The final results are based on an average of the ten acceptable runs.

### 2.4.2.1 Model Calibration

During calibration of a microsimulation model, individual components are adjusted to match collected and field-observed data. Calibration of a model is necessary to ensure that the model provides a visually accurate depiction of the field-observed condition and that model outputs can be trusted to inform the best possible analysis.

Adjustments to the Vissim models focus on the model components related to driver behavior including yielding right-of-way at intersections, driver performance such as aggressiveness, vehicle fleet mix, and vehicle performance. In particular, roadway links with bicycles traveling in the regular traffic lane have been adjusted so that bikes can be overtaken on the left if the lane is wide enough to provide acceptable clearance.

### 2.4.2.2 Model Validation

During validation, the VISSIM model output is compared against field data to determine if the output is within acceptable levels. FHWA (Traffic Analysis Toolbox Volume III - Guidelines for Applying Traffic Microsimulation Modeling Software, 2003) suggests the following validation criteria:

- Link volumes for more than 85 percent of cases meet the following criteria:
o For volumes less than 700 vph , within 100 vph
o For volumes between 700 and 2,700 vph, within 15 percent
o For volumes greater than 2,700 vph, within 400 vph
- Link volumes for more than 85 percent of cases have a GEH statistic less than 5 (a measure of how well the model replicates actual conditions)
- Sum of link volumes within 5 percent
- Sum of link volumes have a GEH statistic less than 4
- Signals create visually acceptable queuing and agree with observed conditions

Fehr \& Peers has developed the following additional validation criterion, which has a narrower tolerance for intersection volumes (which are aggregated link volumes) than the criteria suggested by FHWA.

- Peak-hour volumes for more than 85 percent of intersections within 5 percent of traffic counts

Table 4: Validation Criteria Thresholds Comparison shows how the results for the existing conditions Vissim models compare to the validation criteria thresholds. The results reflect the average of 10 micro-simulation model runs.

As noted above, the Vissim analysis used a 15-minute seeding interval followed by a 2 -hour modeling period corresponding to the 2-hour peak period. Measures of effectiveness (network throughput,
intersection delay, queue length, etc.) were recorded for the 60-minute period corresponding to the peak hour.

### 2.4.3 Freeway Segments

Freeway operations were analyzed under AM and PM peak hour conditions according to the methodology presented in the Highway Capacity Manual, 6th Edition (Transportation Research Board, 2016). As with intersections, LOS is used to describe the operating condition of freeway segments. Table 5 lists the descriptions of the letter ratings and thresholds for each category.

Table 4: Validation Criteria Thresholds Comparison

| Criteria | Criteria Threshold | Target for \% Met | Peak Hour | \% Met / Value | Pass/Fail |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Link Volumes |  |  |  |  |  |
| $<700 \mathrm{vph}$ | $\pm 100 \mathrm{vph}$ |  |  |  |  |
| 700 to $2,700 \mathrm{vph}$ | $\pm 15 \%$ | $>85 \%$ | AM | $100 \%$ | Pass |
| $>2,700 \mathrm{vph}$ | $\pm 400 \mathrm{vph}$ |  | PM | $100 \%$ | Pass |
| GEH statistic | $<5.0$ | $>85 \%$ | AM | $100 \%$ | Pass |

## Sum of Link Volumes

| Sum of all links | $\pm 5 \%$ | - | $\begin{aligned} & \text { AM } \\ & \text { PM } \end{aligned}$ | $\begin{aligned} & -0.4 \% \\ & -1.7 \% \end{aligned}$ | Pass <br> Pass |
| :---: | :---: | :---: | :---: | :---: | :---: |
| GEH statistic | < 4.0 | - | $\begin{aligned} & \text { AM } \\ & \text { PM } \end{aligned}$ | $\begin{aligned} & 0.5 \\ & 2.3 \end{aligned}$ | $\begin{aligned} & \text { Pass } \\ & \text { Pass } \end{aligned}$ |
| Aggregated Volumes |  |  |  |  |  |
| Intersections | $\pm 5 \%$ | > 85\% | $\begin{aligned} & \text { AM } \\ & \text { PM } \end{aligned}$ | $\begin{aligned} & 100 \% \\ & 100 \% \end{aligned}$ | Pass <br> Pass |
| Visual Inspection |  |  |  |  |  |
| Queuing | ma | ons | $\begin{aligned} & \text { AM } \\ & \text { PM } \end{aligned}$ |  | Pass <br> Pass |

Source: FHWA, 2003 and Fehr \& Peers, 2018

The HCM method for freeway capacity analysis has the following limitations that may apply in one or more analysis scenario.

- The methodology does not account for the influence of a downstream bottleneck that causes queuing to extend into the study area.
- The methodology does not account for the influence of an upstream bottleneck that constrains traffic demand from reaching the study area.
- The capacity-enhancing effects of ramp metering and intelligent transportation system features (for example, electronic dynamic message signs) are not captured.
- The effect of the posted speed limit and enforcement practices on actual vehicle speed is not modeled.
- The effect of a ramp HOV (high-occupancy vehicle) lane on merge segment capacity is not captured.
- The effect of a mainline HOV lane on freeway segment capacity is not modeled directly.


## Table 5: Freeway LOS Thresholds

|  |  | Density ${ }^{1}$ |  |
| :---: | :---: | :---: | :---: |
| LOS | Description | Basic | Merge, Diverge and Weave |
| A | Free-flow speeds prevail. Vehicles are almost completely unimpeded in their ability to maneuver. | < 11 | < 10 |
| B | Free-flow speeds are maintained. The ability to maneuver with the traffic stream is only slightly restricted. | > 11 to 18 | > 10 to 20 |
| C | Flow with speeds at or near free-flow speeds. Freedom to maneuver within the traffic stream is noticeably restricted, and lane changes require more care and vigilance on the part of the driver. | > 18 to 26 | > 20 to 28 |
| D | Speeds decline slightly with increasing flows. Freedom to maneuver with the traffic stream is more noticeably limited, and the driver experiences reduced physical and psychological comfort. | > 26 to 35 | > 28 to 35 |
| E | Operation at capacity. There are virtually no usable gaps within the traffic stream, leaving little room to maneuver. Any disruption can be expected to produce a breakdown with queuing. | > 35 to 45 | > 35 to 43 |
| F | Represents a breakdown in flow. | > 45 or $\mathrm{V} / \mathrm{c}>1^{2}$ | $>43^{3}$ or $\mathrm{v} / \mathrm{c}>1^{2}$ |

Notes: 1. Density is reported in vehicles per lane per mile.
2. Volume-to-capacity ratio is greater than 1 (demand exceeds capacity).
3. Threshold of 43 vehicles per lane per mile applies to weave segments only. Merge and diverge segments do not have a density threshold for LOS F.
Source: Highway Capacity Manual (Transportation Research Board, 2016)
To address the last limitation, the mainline HOV lane volume and lane will be removed from the segment analysis to estimate operations in the general purpose lanes under design year conditions. The HOV percentage was assumed to be 14 percent under both peak hours based on forecasted volumes for I-80 between Davis and West Sacramento from the cumulative year SACMET regional traffic demand model.

For weave segments, capacity is also analyzed according the Leisch Method as described in the Highway Design Manual (Caltrans, 2012) Section 504.7.

The freeway mainline peak hour factors and heavy vehicle percentages are provided in Table 1. For ramps, the peak hour factor and heavy vehicle percentage come from the appropriate ramp terminal intersection count. These values were used for all future analysis years with the following exception. The minimum value of 0.92 peak hour factor and 3 percent heavy vehicles was applied.

The lane configuration for the ramp meter proposed for the new westbound on-ramp was evaluated according to the arrival distribution and practical metering rates as described in the Ramp Meter Design Manual (Caltrans, 2016). The HOV percentage for on-ramp traffic was assumed to be 15 percent.

### 2.5 Evaluation Criteria

The intersection and freeway segment evaluation criteria were based on policies of the respective jurisdictions.

The City of Davis General Plan (December 2013) identifies LOS E as the minimum acceptable LOS for intersections during peak hours although LOS F is acceptable for the "Core Area and Richards Boulevard/Olive Drive area." For this project, a project impact for the Build Alternative occurs when (1) an intersection worsens from LOS E or better under the No Build Alternative to LOS F or (2) intersection delay increases for an intersection operating at LOS F under the No Build Alternative.

The Interstate 80 Transportation Concept Report (July 2017) identifies LOS E as the concept LOS for urban areas in Caltrans District 3. For this project, a project impact for the Build Alternative occurs when (1) a freeway segment worsens from LOS E or better under the No Build Alternative to LOS F or (2) freeway segment density increases for a segment operating at LOS F under the No Build Alternative.

### 2.6 Safety Analysis

The Highway Safety Manual (American Association of State Highway and Transportation Officials, 2010) methodology was used to predict the expected number of collisions for the westbound I-80 freeway ramps at Richards Boulevard and Olive Drive. The methodology uses daily volume, roadway geometry, and other characteristics to predict collisions for a given roadway. The collision history is also a model input that can improve the statistical reliability of the prediction. Although this methodology estimates collisions, it does not ensure or imply that the actual number of collisions will match the predicted value.

The Enhanced Interchange Safety Analysis Tool spreadsheet (Texas Transportation Institute, 2013) was used to estimate collisions to apply the Highway Safety Manual methodology.

## Chapter 3. Existing Conditions

The existing conditions chapter presents the operations and safety of the roadway system. The operations analysis is a detailed evaluation of individual facilities with separate discussions for intersections and freeway segments. Crash history for roadways adjacent and parallel to the proposed project are presented. The existing transit, bicycle, and pedestrian systems are also discussed.

### 3.1 Study Facilities

The roadway study area extends along the First Street/Richards Boulevard corridor from D Street in the north to Research Park Drive in the south and along I-80 from Old Davis Road in the west to Mace Boulevard in the east. The study locations are in Yolo and Solano Counties and the City of Davis. The major roadways are described below.

- Richards Boulevard is a north-south arterial that extends from First Street/E Street in downtown Davis under the Union Pacific Railroad and over I-80 to Research Park Drive/Cowell Boulevard in south Davis. The roadway is one of three crossings of the railroad and the freeway in the City of Davis.
- First Street is an east-west arterial that runs from A Street at the University of California at Davis (UC Davis) campus to G Street and serves as the southernmost street in downtown Davis.
- Olive Drive is an east-west collector street that provides access to parcels located in the triangle formed by the Union Pacific Railroad on the north, I-80 on the south, and Putah Creek on the west. Land uses in this area include highway commercial, light industrial, and residential (student) apartment complexes.
- Cowell Boulevard is an east-west arterial serving south Davis that runs from Richards Boulevard/Research Park Drive to the El Macero neighborhood east of Mace Boulevard.
- Old Davis Road is a north-south roadway that serves as the south entrance to UC Davis and the main access point from I-80.
- Mace Boulevard is a north-south roadway that serves east and south Davis. It is the easternmost of three crossings of the railroads and has one of two I-80 interchanges in the City of Davis.
- I-80 is an east-west freeway that traverses the United States from San Francisco to New York. In the study area, the freeway has three lanes in each direction and serves regional traffic between the Sacramento metropolitan area and the Bay Area.

Five of the six study intersections are signalized and operate as a coordinated corridor during the AM and PM peak periods. The cycle length was 120 seconds during both peak hours when the traffic counts and
field observations were conducted in October 2016. The unsignalized intersection at the I-80 Westbound Ramps is uncontrolled; that is, turning vehicles either have free movements or must merge (westbound I80 to southbound Richards Boulevard) or weave (westbound I-80 to northbound Richards Boulevard) with conflicting vehicles.

Marked, on-street parallel parking is provided on westbound First Street. Parking is restricted to 90 minutes for vehicles without a residential permit. On-street parking is also allowed on the north legs of the D and E Street intersections at First Street. Elsewhere in the study area, on-street parking is prohibited. The effect of on-street parking on traffic operations was not directly modeled in Vissim.

The I-80/Richards Boulevard interchange has a loop off-ramp and slip on-ramp in the eastbound direction and a full cloverleaf configuration in the westbound direction. West of the interchange, the freeway widens out approaching the Old Davis Road and State Route 113 interchanges. The next interchange to the east is at Mace Boulevard. Further west is the three-mile long causeway at the Yolo Bypass.

The causeway is a bottleneck in the westbound direction that constrains traffic demand from reaching the Richards Boulevard interchange during both peak periods. The measured peak hour factors for the westbound mainline freeway ( 0.98 and 0.99 ) are close to 1.0 due to this upstream constraint. If the bottleneck were removed, the westbound peak hour volumes would be higher than measured.

In the eastbound direction, the causeway is a bottleneck during the PM peak hour only. Congestion from this bottleneck has grown in recent years until the queue regularly extends through the Richards Boulevard interchange during the PM peak period. If this bottleneck were removed, the congested, stop-and-go conditions observed for the eastbound freeway at Richards Boulevard would be improved, and the observed PM peak hour freeway volume would increase.

Due to the congested conditions, the freeway count measured at Richards Boulevard via PeMS does not reflect the actual demand volume. To estimate the eastbound PM peak hour demand, the additional congested length during the PM peak hour was assumed to extend upstream to the Union Pacific Railroad Overhead, a distance of about 1.1 miles. Assuming three lanes of queued vehicles and 50 feet per vehicle, the unserved volume during the PM peak hour was estimated as 350 vehicles. This additional volume was added to the mainline volume for the eastbound PM peak hour freeway capacity analysis.

Figure 3 shows the peak hour vehicle turning movement volumes, traffic control, and lane configurations for the study intersections. Figure 4 shows the intersection peak hour bicycle and pedestrian volumes. The freeway mainline and ramp peak hour volumes are shown in Figure 5.

### 3.2 Intersection Operations

Intersection operations were analyzed for existing (2016) conditions under AM and PM peak hour conditions using the Vissim software. Table 6 shows the intersection LOS and average delay under existing conditions.


| 1. D St/First St | 2. Richards Blvd/E St/First St | 3. Richards Blvd/Olive Dr | 4. Richards Blvd/l-80 WB Ramps |
| :---: | :---: | :---: | :---: |
|  |  |  |  |
| 5. Richards Blvd/I-80 EB Ramps | 6. Research Park Dr/Richards Blvd | 1 Study Intersection <br> Bike Path <br> Turn Lane <br> AM (PM) Peak Hour Traffic Volume Traffic Signal |  |
|  |  |  |  |



Figure 4
Note: These volumes are based on the mainline peak hours:


## AM (PM) [PM Demand] <br> Mainline Volume

AM (PM)
Note: The traffic volumes are based on counts collected in October 2016.

Ramp Volume

\[

\]

Table 6: Intersection Operations - Existing Conditions

| Intersection | Control | LOS / Delay ${ }^{1}$ |  |
| :---: | :---: | :---: | :---: |
|  |  | AM | PM |
| 1. First St/D St | Signal | B / 13 | D / 43 |
| 2. First St/E St/Richards Blvd | Signal | C / 29 | D / 41 |
| 3. Olive Dr/Richards Blvd | Signal | E / 69 | E / 64 |
| 4. I-80 Westbound Ramps/Richards Blvd | Side Street Yield | F/51 (WB RT) | A / 1 (WB RT) |
| 5. I-80 Eastbound Ramps/Richards Blvd | Signal | D / 37 | E/ 62 |
| 6. Research Park Dr/Richards Blvd/Cowell Blvd | Signal | D / 35 | C / 29 |

Notes: Bold and underline font indicate LOS F conditions: that is, volume exceeds capacity. For the side street yield intersection, the highest controlled movement delay is reported with the movement listed in parentheses. Vehicle delay includes delay for bicycles traveling in regular lanes but excludes delay for bicycles traveling in bicycle-only lanes. 1. Delay is reported in seconds per vehicle.

Source: Fehr \& Peers, 2018
During the AM peak hour, the First Street intersections have LOS C or better conditions, but Olive Drive/Richards Boulevard operates at LOS E with high delays on the northbound and westbound approaches. The southern intersections at the l-80 Eastbound Ramps and Research Park Drive have LOS D conditions. The LOS F on the westbound right turn on the I-80 off-ramp is caused by traffic queuing back from the downstream Olive Drive intersection. During the PM peak hour, the First Street intersections have LOS D conditions, and the Olive Drive/Richards Boulevard and I-80 Eastbound Ramps/Richards Boulevard intersections have the highest delays (similar to the AM peak hour) with LOS E conditions.

Table 7 reports the average maximum queue length under existing conditions from the Vissim models. During the AM peak hour, field observations showed long queues on the westbound and northbound approaches at Olive Drive/Richards Boulevard. The bottleneck at the First Street/E Street intersection backs up along Richards Boulevard and extends onto the I-80 overcrossing and the westbound I-80 off-ramp. This is reflected in the 625 -foot queue on northbound Richards Boulevard at Olive Drive and the 250 -foot queue on the westbound off-ramp to northbound Richards Boulevard. During the PM peak hour, queues extend to the upstream intersection on all approaches at the First Street/E Street/Richards Boulevard intersection. At the I-80 Eastbound Ramps, the queue on the off-ramp approach can extend back to the Richards Boulevard overcrossing.

It should be noted that the signal timing plans for the study area were updated in February 2017. The signal timing changes reduced the cycle length for most study intersections resulting in improved operations. In particular, the cycle length at the I-80 Eastbound Ramps/Richards Boulevard intersection was reduced from 120 to 60 seconds, which resulted in shorter off-ramp queues. As a result, the existing conditions operations results reported above no longer reflect current conditions.

Table 7: Average Maximum Queue Length - Existing Conditions

| Intersection | Approach | Storage Length | Queue Length |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  |  | AM Peak Hour | PM Peak Hour |
| 1. First St / D St | Eastbound | 250 | 150 | 475 |
| 2. First St / E St / Richards Blvd | Northbound | 625 | 775 | 650 |
|  | Eastbound | 225 | 200 | 300 |
|  | Westbound | 225 | 175 | 275 |
| 3. Olive Dr / Richards Blvd | Northbound | 300 | 625 | 425 |
|  | Southbound | 625 | 400 | 500 |
|  | Westbound | > 1,500 | 475 | 575 |
| 4. I-80 Westbound Ramps / Richards Blvd | Eastbound | 530 | 25 | 25 |
|  | Westbound | 1,470 | 250 | 25 |
| 5. I-80 Eastbound Ramps / Richards Blvd | Northbound | 445 | 325 | 275 |
|  | Southbound | 1,010 | 175 | 175 |
|  | Westbound | 1,625 | 650 | 1,150 |
| 6. Research Park Dr / Richards Blvd / Cowell Blvd | Eastbound | 445 | 425 | 500 |

Note: The storage length and average maximum queue length is reported in feet.
Source: Fehr \& Peers, 2018

### 3.3 Freeway Operations

Freeway operations were analyzed for existing (2016) conditions under AM and PM peak hour conditions using the HCM analysis method. Tables 8 and 9 present freeway operations under existing conditions for I80 between Old Davis Road and Mace Boulevard for the eastbound and westbound directions, respectively.

During the AM peak hour, both eastbound and westbound freeway study segments would have LOS D or better conditions. The eastbound off-ramp at Richards Boulevard and the westbound off-ramps at Olive Drive and northbound Richards Boulevard have the highest densities (and LOS D conditions).

During the PM peak hour, the HCM analysis showed similar conditions with LOS D or better conditions in both directions. The eastbound PM peak hour conditions are actually congested as shown in Exhibit 1. Slow speeds are shown on eastbound I-80 starting from the Old Davis Road on-ramp and extending to the east. Given the observed congested conditions, the eastbound I-80 study segments are reported as having LOS F conditions in Table 8.

## Table 8: Eastbound Freeway Operations - Existing Conditions

| Segment |  | LOS / Density |  |
| :--- | :---: | :---: | :---: |
|  | Facility Type | AM | PM |
|  | Basic | $\mathrm{B} / 14$ | $\mathrm{~F}^{2}$ |
| Old Davis Road to 1st Lane Drop | Basic $^{1}$ | $\mathrm{~B} / 12$ | $\mathrm{~F}^{2}$ |
| 1st Lane Drop to 2nd Lane Drop | Basic | $\mathrm{B} / 14$ | $\mathrm{~F}^{2}$ |
| Richards Blvd Off-ramp | Basic | $\mathrm{B} / 18$ | $\mathrm{~F}^{2}$ |
| Richards Blvd Off-ramp to On-ramp | Diverge | $\mathrm{D} / 31$ | $\mathrm{~F}^{2}$ |
| Richards Blvd On-ramp | Basic | $\mathrm{C} / 22$ | $\mathrm{~F}^{2}$ |
| Richards Blvd to Chiles Rd | Merge | $\mathrm{C} / 26$ | $\mathrm{~F}^{2}$ |
| Chiles Rd Off-ramp | Basic | $\mathrm{C} / 24$ | $\mathrm{~F}^{2}$ |
| East of Chiles Rd Off-ramp | Diverge | $\mathrm{B} / 15$ | $\mathrm{~F}^{2}$ |

Notes: Density is reported in passenger car equivalents per lane per mile.

1. Since the acceleration lane is greater than 1,500 feet, the location is classified as a basic segment according to the HCM.
2. HCM analysis indicates LOS C/D conditions in the study area. However, actual conditions are LOS F due to a
downstream bottleneck at the Yolo Causeway, which causes congestion that extends through the study area.
Source: Fehr \& Peers, 2018


Exhibit 1 - Google Maps Typical Traffic Conditions for Wednesday at 4:45 PM

Table 9: Westbound Freeway Operations - Existing Conditions

| Segment | Facility Type | LOS / Density |  |
| :---: | :---: | :---: | :---: |
|  |  | AM | PM |
| East of Mace Blvd On-ramp | Basic | C / 23 | C / 21 |
| Mace Blvd to Lane Drop | Basic ${ }^{1}$ | C / 19 | B / 18 |
| Lane Drop to Olive Dr | Basic | D / 27 | C / 24 |
| Olive Dr Off-ramp | Diverge | D / 32 | D / 30 |
| Olive Dr to Richards Blvd | Basic | C / 26 | C / 24 |
| Richards Blvd NB Off-ramp | Diverge | D / 32 | D / 30 |
| Richards Blvd NB Off-ramp to On-ramp | Basic | C / 24 | C / 22 |
| Richards Blvd NB On-ramp to SB Off-ramp | Weave ${ }^{2}$ | C / 23 (C) | C / 23 (C) |
| Richards Blvd SB Off-ramp to On-ramp | Basic | C / 25 | C / 25 |
| Richards Blvd to Old Davis Rd | Basic | C / 18 | C / 19 |
| Old Davis Rd Off-ramp | Diverge | C / 25 | C / 24 |
| West of Old Davis Rd Off-ramp | Basic | B / 13 | B / 15 |

Notes: Density is reported in passenger car equivalents per lane per mile.

1. Since the acceleration lane is greater than 1,500 feet, the location is classified as a basic segment according to the HCM .
2. For the weave segment, the LOS from the Leisch Method is also reported in parentheses.

Source: Fehr \& Peers, 2018

### 3.4 Roadway Safety

The California Highway Patrol's Statewide Integrated Traffic Records System (SWITRS) was queried to find crashes on Richards Boulevard in the City of Davis. Table 10 lists the crashes by type on Richards Boulevard at or near Olive Drive and Research Park Drive/Cowell Boulevard (collisions at the I-80 ramp terminal intersections are reported in Table 11). The crashes occurred between January 1, 2012 and December 31, 2014. This three-year period was chosen to match the most recent three-year period available from Caltrans' Traffic Accident Surveillance and Analysis System (TASAS) for the freeway and ramp facilities.

More collisions occurred at or near the Olive Drive intersection, 14, compared to the Research Park Drive intersection, 2. The most common collision type was a rear-end collision (43 percent), which is consistent with the observed congested conditions. The next most common type are bicycle-related collisions ( 29 percent). Of the 16 reported crashes, a majority (9) were injury-related, but none were fatality-related.

Table 10: Collision History - Richards Boulevard

| Collision Type | Intersection |  |
| :--- | :---: | :---: |
|  | Olive Dr | Research Park Dr |
| Broadside | 0 | 0 |
| Head On | 1 | 0 |
| Hit Object | 2 | 1 |
| Overturn | 0 | 0 |
| Pedestrian/Bicycle | 4 | 1 |
| Rear End | 6 | 0 |
| Sideswipe | 1 | 0 |
| Fatality | 0 | 0 |
| Injury | 8 | 1 |
| Total | 14 | 2 |

Note: Collisions occurred from January 2012 through December 2014.
Source: SWITRS, 2017
Table 11 shows reported collisions for the I-80 freeway mainline from Old Davis Road to Mace Boulevard from the TASAS database for January 2012 through December 2014. For this three-year period, 262 collisions occurred with one fatality. On an overall basis, the collision rate is lower than the statewide collision rate for similar facilities. However, the pattern is different when separated by direction. About threequarters of the collisions occurred in the eastbound direction. This is consistent with the congested conditions observed during the weekday PM peak hour. In the eastbound direction, the actual collision rate for fatality and injury-related collisions and total collisions exceeds the statewide average collision rate.

Table 11 also shows the collision rate for the freeway ramps at Richards Boulevard and Olive Drive including the ramp terminal intersections. The collision rate for most ramps was below the statewide average rate. No collisions were reported in the three-year period for the westbound on-ramp from southbound Richards Boulevard and the westbound off-ramp to Olive Drive. However, two ramps have collision rates that exceed the statewide average. The collision rate for the westbound off-ramp to southbound Richards Boulevard is about double the statewide average for fatality and injury-related collisions and total collisions. The fatality and injury-related collision rate for the eastbound on-ramp from Richards Boulevard is about 50 percent higher than the statewide average. The most common collision types were rear end (5) and hit object (5), each 36 percent of the 14 total ramp collisions.

Using the Highway Safety Manual (AASHTO, 2010), the number of collisions were predicted for existing (2016) conditions for the freeway ramps that will be modified by the project. For all ramps, no fatality and injury collisions were recorded in the most recent three-year period although the analysis predicts an
average of 1.6 such collisions per year. Similarly, the actual property damage only rate is lower than the predicted rate for most ramps. Overall, the observed total collision rate was 2.0 compared with the predicted rate of 4.0 collisions per year.

Table 11: I-80 Collision History

| Facility | Total Collisions | Total <br> Fatalities | Actual Collision Rate ${ }^{1}$ |  |  | Average Collision Rate ${ }^{1}$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | F | F8! | Total | F | F\&1 | Total |
| Mainline | 262 | 1 | 0.002 | 0.18 | 0.51 | 0.005 | 0.24 | 0.75 |
| Eastbound Mainline | 197 | 1 | 0.004 | $\underline{0.27}$ | 0.77 | 0.005 | 0.24 | 0.75 |
| Westbound Mainline | 65 | 0 | 0.000 | 0.08 | 0.25 | 0.005 | 0.24 | 0.75 |
| WB On from SB Richards Blvd | 0 | 0 | 0.000 | 0.00 | 0.00 | 0.003 | 0.18 | 0.57 |
| WB Off to SB Richards Blvd | 3 | 0 | 0.000 | $\underline{0.65}$ | 1.96 | 0.003 | 0.30 | 1.06 |
| EB Off to Richards Blvd | 5 | 0 | 0.000 | 0.29 | 0.74 | 0.004 | 0.33 | 1.00 |
| WB On from NB Richards Blvd | 2 | 0 | 0.000 | 0.00 | 0.42 | 0.002 | 0.21 | 0.73 |
| WB Off to NB Richards Blvd | 1 | 0 | 0.000 | 0.00 | 0.26 | 0.004 | 0.24 | 0.75 |
| EB On from Richards Blvd | 3 | 0 | 0.000 | 0.34 | 0.51 | 0.002 | 0.22 | 0.63 |
| WB Off to Olive Dr | 0 | 0 | 0.000 | 0.00 | 0.00 | 0.004 | 0.24 | 0.75 |

Note: 1. The collision rate is in collisions per million vehicle-miles. "F" refers to the fatality collision rate, and "F\&l" refers to the fatality and injury collision rate.
Source: Caltrans TASAS Table B, January 2012 to December 2014
Table 12: Freeway Ramp Collision Rate - Existing Conditions

| Location | Fatality and Injury |  | Property Damage Only | Total |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Observed | Predicted | Observed | Predicted | Observed | Predicted |
| WB On from SB Richards Blvd | 0 | 0.271 | 0 | 0.311 | 0 | 0.582 |
| WB Off to SB Richards Blvd | 0 | 0.437 | 1.000 | 0.663 | 1.000 | 1.100 |
| WB On from NB Richards Blvd | 0 | 0.467 | 0.667 | 0.958 | 0.667 | 1.425 |
| WB Off to NB Richards Blvd | 0 | 0.341 | 0.333 | 0.442 | 0.333 | 0.784 |
| WB Off to Olive Dr | 0 | 0.052 | 0 | 0.053 | 0 | 0.106 |
| Total | 0 | 1.568 | 2.0 | 2.427 | 2.0 | 3.997 |

[^8]
### 3.5 Multimodal Facilities

### 3.5.1 Transit System

Two transit agencies serve the study area. Unitrans, operated by UC Davis, provides weekday bus service on M (hourly) and W (twice per hour) lines that travels both directions between along First Street west of Richards Boulevard, Richards Boulevard, and Cowell Boulevard east of Research Park Drive.

Yolobus has three express routes in the study area. Route 43 R is an express route between downtown Sacramento and UC Davis that has one bus westbound during the AM peak hour and one bus eastbound during the PM peak hour. Route 44 has three eastbound AM and three westbound PM buses that travel along First Street and Richards Boulevard. Route 242 is an express route between Woodland and Davis with one northbound AM bus and one southbound PM bus. It travels the same path as Route 44 but in the opposite direction.

### 3.5.2 Bicycle System

The existing bicycle facilities are listed below.

- Along First Street, a buffered bicycle lane is provided in the eastbound direction. The westbound lane has sharrow markings indicating that vehicles and bicycles share the travel lane. A shared-use path (bicycles and pedestrians) exists on the south side of First Street that continues along the west side of Richards Boulevard to Olive Drive.
- Class II (on-street) bicycle lanes are provided on Olive Drive east of Richards Boulevard, on Richards Boulevard south of Olive Drive, and on all legs of the Research Park Drive/Richards Boulevard/Cowell Boulevard intersection.
- Importantly, the Putah Creek bicycle trail parallels Richards Boulevard to the west and provides a grade separated crossing on I-80. Connections to the trail exist at the south end of D Street, the west end of Olive Drive, and Chiles Road, which connects to the south end of Research Park Drive.

During the AM peak hour, intersection bicycle volume was highest at Richards Boulevard/Olive Drive (115), with the majority (63) heading west on Olive Drive towards the Putah Creek trail and the UC Davis campus. During the PM peak hour, the First Street/D Street and Richards Boulevard/Olive Drive intersections had about the same total bicycle volume: 128 and 126, respectively. At First Street/D Street, the northbound, eastbound and westbound through volume were all between 32 and 34 bicycles per hour. At Richards Boulevard/Olive Drive, the peak direction was eastbound through away from the UC Davis campus. The bicycle volume using the Richards Boulevard overcrossing was 28 during the AM peak hour and 23 during the PM peak hour.

### 3.5.3 Pedestrian System

In the study area, crosswalks are provided on all four approaches at First Street/D Street, Richards Boulevard/Olive Drive, and Research Park Drive/Richards Boulevard/Cowell Boulevard. At First Street/E Street/Richards Boulevard, pedestrians are allowed to cross only the west and north legs. At I-80 Westbound Ramps/Richards Boulevard, no marked crossings are provided, but a pedestrian path with sidewalks and curb ramps exists on the west side of the intersection. No pedestrian crossings are provided at I-80 Eastbound Ramps/Richards Boulevard.

Pedestrians are accommodated on a shared-use path (bicycles and pedestrians) on the west side of Richards Boulevard between First Street and Olive Drive. A sidewalk is provided on the west side of Richards Boulevard through the interchange. Sidewalks are provided on the east side of Richards Boulevard only south of Olive Drive and north of Research Park Drive along the frontage of gas stations.

The highest total crosswalk volume during the AM peak hour occurred at First Street/D Street (70) although Richards Boulevard/Olive Drive (61) and First Street/E Street/Richards Boulevard (60) also have substantial pedestrian volume. During the PM peak hour, 215 pedestrians were observed using the First Street/E Street/Richards Boulevard crosswalks. First Street/D Street (120) and Richards Boulevard/Olive Drive (92) also had substantial PM peak hour pedestrian volumes. During the peak hours, 12 (AM) and 14 (PM) pedestrians traveled across the Richards Boulevard overcrossing.

### 3.5.4 Freight System

The I-80/Richards Boulevard interchange provides access for trucks to retail and commercial businesses along Richards Boulevard, Olive Drive, and Research Park Drive. However, the Richards Boulevard underpass at the Union Pacific Railroad has a low clearance of 13.5 feet, which restricts some trucks from reaching downtown Davis from the interchange. As noted above, heavy vehicle percentages at the study intersections are relatively low at 3 and 1 percent during the AM and PM peak hours.

I-80 is an important route for freight traffic. It is part of the National Highway Freight Network and included in the Primary Highway Freight System established by USDOT in December 2015, which includes approximately 41,518 miles across the nation. I-80 is on the Strategic Highway Network (STRAHNET), National Truck Network, the Interregional Road System, the Extra Legal Load Network (ELLN), and is a Surface Transportation Assistance Act (STAA) route. I-80 also connects the Bay Area and Sacramento metropolitan areas, the two largest economic and population centers in Northern California.

## chapter 4. Travel Demand Forecasts

This chapter presents the construction and design year forecasts.

### 4.1 Construction Year Forecasts

Figures 6 and 7 show the study intersection peak hour volumes for construction year (2022) conditions under the No Build and Build Alternatives, respectively. These volumes represent traffic demand volumes that may not be fully accommodated during the peak hour due to bottlenecks outside the study area. The figures also show the assumed intersection traffic control and lane configurations.

The traffic volumes for the Build Alternative (Figure 7) are the same as the No Build Alternative (Figure 6) except for reassigning traffic based on the new roadway configuration. At the I-80/Richards Boulevard interchange, the reconfiguration of the westbound ramps from four to two would shift the loop ramp volumes (both loop on-ramp and loop off-ramp) to become left-turn movements at the new signalized intersection. The closure of the Olive Drive westbound off-ramp would shift traffic to the westbound offramp to northbound Richards Boulevard. The distribution of the Olive Drive off-ramp traffic destinations were determined using a select-link model run so that the volumes could be assigned to the appropriate turning movements at the study intersections.

Compared to existing conditions, the construction year volumes for the No Build Alternative show an increase of about 200 vehicles per hour during the peak hours for Richards Boulevard between I-80 and Olive Drive. This is a growth of 14 (PM) to 17 (AM) percent over existing volumes. With the closure of the Olive Drive off-ramp in the Build Alternative, the volume change would increase to about 570 vehicles per hour during the AM peak hour and 270 vehicles per hour during the PM peak hour.

Figure 8 shows the bicycle and pedestrian volumes for construction year conditions. Similar to the vehicle volumes, the bicycle and pedestrian volumes are estimated by linear interpolation of the existing and design year volumes. The bicycle and pedestrian connections are the same for the project alternatives, so the forecasted volumes are also the same.

Figure 9 shows the freeway volumes for construction year conditions. The difference between the project alternatives is shown for westbound I-80 at Olive Drive and Richards Boulevard. On westbound I-80 east of Olive Drive, traffic volume would grow by about 300 vehicles per hour during the peak hours, a 6 (AM) to 8 (PM) percent growth over existing volumes.


Vehicle Volume, Traffic Control, and Lane Configurations -


Figure 7

## Vehicle Volume, Traffic Control, and Lane Configurations Construction Year Conditions Build Alternative



Figure 8

## Bicycle and Pedestrian Volume Construction Year Conditions



### 4.2 Design Year Forecasts

Figures 10 and 11 show the study intersection peak hour volumes for design year (2042) conditions under the No Build and Build Alternatives, respectively. These volumes represent traffic demand volumes that may not be fully accommodated during the peak hour due to bottlenecks outside the study area. The figures also show the assumed intersection traffic control and lane configurations. For the Olive Drive/Richards Boulevard intersection, additional widening on the west leg was assumed to serve the traffic generated from the Nishi and Hotel Conference Center projects.

The traffic volumes for the Build Alternative (Figure 11) are the same as the No Build Alternative (Figure 10) except for reassigning traffic based on the new roadway configuration. At the I-80/Richards Boulevard interchange, the reconfiguration of the westbound ramps from four to two would shift the loop ramp volumes (both loop on-ramp and loop off-ramp) to become left-turn movements at the new signalized intersection. The closure of the Olive Drive westbound off-ramp would shift traffic to the westbound offramp to northbound Richards Boulevard. The distribution of the Olive Drive off-ramp traffic destinations were determined using a select-link model run so that the volumes could be assigned to the appropriate turning movements at the study intersections.

Compared to existing conditions, the design year volumes for the No Build Alternative show an increase of about 800 vehicles per hour during the peak hours for Richards Boulevard between I-80 and Olive Drive. This is a growth of 52 (PM) to 62 (AM) percent over existing volumes. With the closure of the Olive Drive off-ramp in the Build Alternative, the volume change would increase to about 1,100 vehicles per hour during the AM peak hour and 940 vehicles per hour during the PM peak hour.

Figure 12 shows the bicycle and pedestrian volumes for design year conditions. Similar to the vehicle volumes, the bicycle and pedestrian volumes are estimated by linear interpolation of the existing and design year volumes. The bicycle and pedestrian connections are the same for the project alternatives, so the forecasted volumes are also the same.

Figure 13 shows the freeway volumes for design year conditions. The difference between the project alternatives is shown for westbound I-80 at Olive Drive and Richards Boulevard. On westbound I-80 east of Olive Drive, traffic volume would grow by about 1,500 vehicles per hour during the peak hours, a 30 (AM) to 33 (PM) percent growth over existing volumes.



Figure 11

## Vehicle Volume, Traffic Control, and Lane Configurations Design Year Conditions Build Alternative



Figure 12

## Bicycle and Pedestrian Volume Design Year Conditions



### 4.3 Design Year Performance Measures

To estimate the area-wide effect of the reconstruction of the I-80/Richards Boulevard interchange and the closure of the westbound off-ramp to Olive Drive, the design year performance measures of vehicle miles of travel (VMT), vehicle hours of travel (VHT), and vehicle hours of delay (VHD) were estimated using the cumulative year forecasting model. To capture the potential changes, performance was measured over the entire model area, which is the City of Davis. Under design year conditions, the same number of trips were assigned to the two different roadway alternatives.

Table 13 shows the local area-wide performance measures (see the appendix for VMT by 5 -mph speed bin).

Table 13: Area-wide Performance Measures

| Statistic |  | Design Year Conditions |  | Change from No <br> Build |
| :--- | :---: | :---: | :---: | :---: |
|  | Existing | No Build | Build Alternative |  |
| Vehicle Miles of Travel (VMT) | $2,360,828$ | $2,980,219$ | $2,979,159$ | $-1,060(-0.04 \%)$ |
| Vehicle Hours of Travel (VHT) | 69,583 | 101,513 | 101,451 | $-62(-0.06 \%)$ |
| Vehicle Hours of Delay (VHD) | 7,148 | 21,965 | 21,911 | $-54(-0.25 \%)$ |

Source: Fehr \& Peers, 2018
Compared to existing conditions, the No Build Alternative under design year conditions would have 26 percent more VMT, 46 percent more VHT, and 207 percent more VHD. Compared to the No Build Alternative, the Build Alternative would have a lower VMT by about 1,060 vehicle-miles, or 0.04 percent. Although closing the Olive Drive off-ramp would increase trip lengths from westbound I-80 to the east Olive Drive area, trips originating in the City of Davis and destined to east Olive Drive would shift from using the freeway to shorter local street routes, which would result in an overall VMT decrease.

The change in VHT and VHD would both be marginal with the project: 0.06 percent fewer vehicle-hours of travel and 0.25 percent vehicle-hours of delay. The travel time would be improved by shifting regional trips destined to east Olive Drive from the lower-speed Olive Drive via the westbound off-ramp closure to the higher speed I-80 and Richards Boulevard. This improvement would be offset by the local trips using lower speed local streets to access east Olive Drive.

## Chapter 5. Construction Year Conditions

This chapter presents the operations and safety analysis under construction year (2022) conditions.

### 5.1 Intersection Operations

Intersection operations were analyzed for construction year (2022) conditions during the AM and PM peak hours. Table 14 shows the intersection LOS and average delay for the AM and PM peak hours (see the appendix for detailed analysis results).

Table 14: Intersection Operations - Construction Year Conditions

| Intersection | Control | No Build Alternative |  | Build Alternative |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | AM | PM | AM | PM |
| 1. First St/D St | Signal | B / 15 | C / 29 | B / 13 | D / 36 |
| 2. First St/E St/Richards Blvd | Signal | C / 31 | C / 34 | B / 18 | C / 26 |
| 3. Olive Dr/Richards Blvd | Signal | F/93 | E/ 65 | D / 38 | D / 52 |
| 4. I-80 Westbound Ramps/Richards Blvd | Side Street Yield/ Signal ${ }^{1}$ | $\frac{F / 121}{(N B T H)}$ | A/9 <br> (NB TH) | C / 35 | C / 23 |
| 5. I-80 Eastbound Ramps/Richards Blvd | Signal | D / 40 | F/109 | C/26 | C/ 24 |
| 6. Research Park Dr/Richards Blvd/Cowell Blvd | Signal | D / 47 | D / 42 | C / 27 | C / 30 |

Notes: Bold and underline font indicate LOS F conditions: that is, volume exceeds capacity. For the side street yield intersection, the highest controlled movement delay is reported with the movement listed in parentheses. Vehicle delay includes delay for bicycles traveling in regular lanes but excludes delay for bicycles traveling in bicycle-only lanes. Delay is reported in seconds per vehicle.

1. The intersection would have signal control under the Build Alternative

Source: Fehr \& Peers, 2018
Under the No Build Alternative, the higher forecasted volumes at Richards Boulevard/Olive Drive would worsen operations from LOS E to F during the AM peak hour for construction year conditions. The northbound queue at the intersection would extend through the I-80 Westbound Ramps intersection resulting in higher delay for the westbound to northbound off-ramp approach than under existing conditions. The other study intersections would continue to operate with the same LOS as under existing conditions.

During the PM peak hour, increasing volume on the eastbound off-ramp would result in worse operations with LOS E degrading to LOS F at the I-80 Eastbound Ramps intersection. Similarly, the Research Park Drive intersection operations would worsen from LOS D to E , and the other study intersections would operate the same or better than under existing conditions.

Under the Build Alternative, additional capacity at the Richards Boulevard/Olive Drive intersection would reduce vehicle delay compared to the No Build Alternative. Operations would improve from LOS F to D during the AM peak hour and LOS E to D during the PM peak hour. The reconstructed and signalized I-80 Westbound Ramps intersection would operate with LOS C conditions during both peak hours. The addition of a second left-turn lane on the eastbound off-ramp would improve the I-80 Eastbound Ramps intersection from LOS F to C during the PM peak hour. All study intersections would have LOS D or better operations under the Build Alternative.

Table 15 presents the average maximum queue length for selected approaches to the study intersection under the Build Alternative (see the appendix for detailed analysis results). During the AM peak hour, the queues would be less than the storage length except for northbound Richards Boulevard at Olive Drive. The constraint would be the single lane for northbound through vehicles. Despite this, the upstream I-80 Westbound Ramps intersection would operate acceptably, and the westbound off-ramp queue would be contained on the ramp.

Table 15: Average Maximum Queue Length - Construction Year Conditions

| Intersection | Approach | Storage Length | Queue Length |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  |  | AM Peak Hour | PM Peak Hour |
| 1. First St / D St | Eastbound | 250 | 150 | 400 |
| 2. First St / E St / Richards Blvd | Northbound | 625 | 425 | 250 |
|  | Eastbound | 225 | 200 | 275 |
|  | Westbound | 225 | 175 | 250 |
| 3. Olive Dr / Richards Blvd | Northbound | 525 | 550 | 475 |
|  | Southbound | 625 | 475 | 700 |
|  | Westbound | >1,500 | 50 | 275 |
| 4. I-80 Westbound Ramps / Richards Blvd | Northbound | 815 | 450 | 300 |
|  | Southbound | 500 | 200 | 150 |
|  | Westbound | 1,250 | 575 | 275 |
| 5. I-80 Eastbound Ramps / Richards Blvd | Northbound | 440 | 275 | 300 |
|  | Southbound | 850 | 175 | 225 |
|  | Westbound | 1,270 | 250 | 300 |
| 6. Research Park Dr / Richards Blvd / Cowell Blvd | Eastbound | 440 | 325 | 375 |

Notes: Bold and underline font indicate a queue length that is greater than the storage length. The storage length and average maximum queue length is reported in feet.
Source: Fehr \& Peers, 2018

During the PM peak hour, the average maximum queue would exceed the storage on southbound Richards Boulevard at Olive Drive. The queue would extend upstream and affect other approaches to the First Street
intersections. These queues reflect the high traffic demand from downtown Davis to I-80 and south Davis. As during the AM peak hour, the freeway off-ramp queues ( 300 feet or less) would be contained on the offramps.

### 5.2 Freeway Operations

Freeway operations were analyzed for construction year (2022) conditions under AM and PM peak hour conditions. Table 16 and Table 17 show the freeway LOS and density for the study segments (see the appendix for detailed analysis results).

Although density would increase with the increasing volumes compared to existing conditions, freeway segments would operate at LOS D or better under the No Build Alternative. The eastbound freeway segments are listed as LOS F during the PM peak hour since no improvements are planned to occur at the Yolo Bypass bottleneck by construction year conditions.

Table 16: Eastbound Freeway Operations - Construction Year Conditions

| Segment | Facility Type | No Build Alternative |  | Build Alternative |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | AM | PM | AM | PM |
| West of Old Davis Rd On-ramp | Basic | B / 15 | $\mathrm{F}^{2}$ | Same as No Build Alternative |  |
| Old Davis Road On-ramp | Basic ${ }^{1}$ | B / 13 | $\mathrm{F}^{2}$ |  |  |
| Old Davis Road to 1st Lane Drop | Basic | B / 16 | $\mathrm{F}^{2}$ |  |  |
| 1st Lane Drop to 2nd Lane Drop | Basic | C / 20 | $\mathrm{F}^{2}$ |  |  |
| Richards Blvd Off-ramp | Diverge | D / 33 | $\mathrm{F}^{2}$ |  |  |
| Richards Blvd Off-ramp to On-ramp | Basic | C / 24 | $\mathrm{F}^{2}$ |  |  |
| Richards Blvd On-ramp | Merge | C / 27 | $\mathrm{F}^{2}$ |  |  |
| Richards Blvd to Chiles Rd | Basic | C / 26 | $\mathrm{F}^{2}$ |  |  |
| Chiles Rd Off-ramp | Diverge | B / 16 | $\mathrm{F}^{2}$ |  |  |
| East of Chiles Rd Off-ramp | Basic | C / 23 | $\mathrm{F}^{2}$ |  |  |

Notes: Density is reported in passenger car equivalents per lane per mile.

1. Since the acceleration lane is greater than 1,500 feet, the location is classified as a basic segment according to the HCM . 2. HCM analysis indicates LOS C/D conditions in the study area. However, actual conditions are likely to be LOS F since no improvements are planned by the construction year at the downstream bottleneck at the Yolo Causeway, which causes congestion that extends through the study area under existing conditions.
Source: Fehr \& Peers, 2018
For the Build Alternative, the eastbound freeway configuration and volumes would be the same as the No Build Alternative since no improvements to eastbound I-80 are included in the proposed project. In the westbound direction, the closure of the Olive Drive off-ramp and consolidation of ramps at Richards

Boulevard provide different configurations and volumes. Near Olive Drive, the Build Alternative would provide a lower density due to the ramp removal. The combined Richards Boulevard off-ramp would have a higher density due to the higher exiting volume compared to existing conditions. Operations between the on and off-ramps would be the same or better under the No Build Alternative since the weaving section would be removed. Similar to the combined off-ramp, the combined on-ramp would have higher densities. Despite these changes, no freeway segments would have project impacts under construction year conditions.

Table 17: Westbound Freeway Operations - Construction Year Conditions

| Segment | Facility Type | No Build Alternative |  | Build Alternative |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | AM | PM | AM | PM |
| East of Mace Blvd On-ramp | Basic | C / 25 | C / 23 | C / 25 | C / 23 |
| Mace Blvd to Lane Drop | Basic | C / 20 | C / 19 | C / 20 | C / 18 |
| Lane Drop to Olive Dr | Basic | D / 29 | D / 26 | D / 29 | D / 26 |
| Olive Dr Off-ramp | Diverge | D / 33 | D / 32 |  |  |
| Olive Dr to Richards Blvd | Basic | D / 28 | C / 26 |  |  |
| Richards Blvd NB Off-ramp | Diverge | D / 33 | D / 31 | D / 34 | D / 32 |
| Richards Blvd NB Off-ramp to On-ramp | Basic | C / 25 | C / 24 | C / 26 | C / 23 |
| Richards Blvd NB On-ramp to SB Off-ramp | Weave ${ }^{1}$ | C/25 (D) | C / 25 (D) |  |  |
| Richards Blvd SB Off-ramp to On-ramp | Basic | D / 26 | D / 27 |  |  |
| Richards Blvd to Old Davis Rd | Basic | C / 19 | C / 21 | C / 21 | D / 30 |
| Old Davis Rd Off-ramp | Diverge | C / 24 | C / 25 | C / 24 | C / 22 |
| West of Old Davis Rd | Basic | B / 14 | B / 16 | B / 15 | B / 15 |

Notes: Density is reported in passenger car equivalents per lane per mile.

1. For the weave segment, the LOS from the Leisch Method is also reported in parentheses.

Source: Fehr \& Peers, 2018

### 5.3 Roadway Safety

Using the forecasted daily volume, predicted collisions were calculated for construction year conditions under the project alternatives as shown in Table 18 (see the appendix for detailed analysis results). Under the No Build Alternative, the current five ramps in the westbound direction at Olive Drive and Richards Boulevard would be expected to have 4.3 collisions per year, with 1.7 fatality and injury-related collisions. With the Build Alternative, the number of westbound ramps is reduced from 5 to 2 , and the ramp roadways are reconfigured to have less sharp curves (a higher radius). The expected total collision rate would be 1.6
collisions per year, with 0.8 fatality and injury-related collisions. Under the Build Alternative, the expected total collision rate would be less than one-third of the No Build Alternative rate, and the fatality and injuryrelated rate would be less than one-half.

Table 18: Freeway Ramp Collision Rate - Construction Year Conditions

| Location | No Build Alternative |  |  | Build Alternative |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
|  | F+I | PDO | Total | F+I | PDO | Total |
| WB On from SB Richards Blvd | 0.293 | 0.338 | 0.631 | 0.422 | 0.411 | 0.833 |
| WB Off to SB Richards Blvd | 0.459 | 0.695 | 1.155 | - | - | - |
| WB On from NB Richards Blvd | 0.522 | 1.072 | 1.593 | - | - | - |
| WB Off to NB Richards Blvd | 0.355 | 0.460 | 0.815 | 0.347 | 0.398 | 0.745 |
| WB Off to Olive Dr | 0.072 | 0.073 | 0.145 | - | - | - |
| Total | 1.701 | 2.638 | 4.339 | 0.769 | 0.809 | 1.578 |

Note: Values are in collisions per year.
Source: Fehr \& Peers, 2018

## chapter 6. Design Year Conditions

This chapter presents the operations and safety analysis of the roadway system under design year (2042) conditions and an assessment of multimodal systems affected by the proposed project.

### 6.1 Intersection Operations

Intersection operations were analyzed for design year (2042) conditions during the AM and PM peak hours. Table 19 shows the intersection LOS and average delay for the AM and PM peak hours (see the appendix for detailed analysis results).

Table 19: Intersection Operations - Design Year Conditions

| Intersection | Control | No Build Alternative |  | Build Alternative |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | AM | PM | AM | PM |
| 1. First St/D St | Signal | F/224 | D / 41 | C / 27 | D / 36 |
| 2. First St/E St/Richards Blvd | Signal | F/123 | C / 32 | C / 28 | C / 27 |
| 3. Olive Dr/Richards Blvd | Signal | F/142 | F/183 | D / 44 | D / 44 |
| 4. I-80 Westbound Ramps/Richards Blvd | Side Street <br> Yield/ Signal ${ }^{1}$ | $\frac{\mathbf{F} / 267}{(W B R T)}$ | $\begin{gathered} \text { A / } 3 \\ \text { (WB RT) } \end{gathered}$ | D / 42 | D / 39 |
| 5. I-80 Eastbound Ramps/Richards Blvd | Signal | F/182 | F/131 | C/ 30 | D / 53 |
| 6. Research Park Dr/Richards Blvd/Cowell Blvd | Signal | F/122 | F/101 | D / 48 | E/78 |

Notes: Bold and underline font indicate LOS F conditions: that is, volume exceeds capacity. For the side street yield intersection, the highest controlled movement delay is reported with the movement listed in parentheses. Vehicle delay includes delay for bicycles traveling in regular lanes but excludes delay for bicycles traveling in bicycle-only lanes. Delay is reported in seconds per vehicle.

1. The intersection would have signal control under the Build Alternative.

Source: Fehr \& Peers, 2018
Under the No Build Alternative, the design year forecasts would not be accommodated during the AM peak hour. All study intersections would have LOS F conditions. Bottlenecks at the Olive Drive and I-80 Eastbound Ramps intersections would extend into the adjacent intersections resulting in poor operations overall. During the PM peak hour, the corridor bottlenecks would also result in LOS F conditions at Olive Drive, I-80 Eastbound Ramps, and Research Park Drive. The First Street intersections would have lower overall delays compared to the AM peak hour due to upstream congestion that constrains demand volume from reaching the intersection.

The Build Alternative would reduce intersection delay and improve operations to LOS D or better during the AM peak hour. Average delay at the Olive Drive and I-80 Eastbound Ramps intersection would be less than under existing conditions.

During the PM peak hour, all study intersections would operate acceptably at LOS E or better. Operations on the north side of the interchange would be similar to the AM peak hour with LOS D or better conditions. The Research Park Drive intersection would have the worst overall operations at LOS E with two approaches at LOS F: southbound Research Park Drive and westbound Cowell Boulevard. These approaches would have high demand volumes heading towards I-80. Intersection efficiency could be improved by prohibiting the U-turn movement on the Richards Boulevard approach. The U-turning traffic could be re-routed to northbound Research Park Drive to access the highway commercial properties adjacent to the interchange.

Table 20: Average Maximum Queue Length - Design Year Conditions

| Intersection | Approach | Storage <br> Length | Queue Length |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  |  | AM Peak Hour | PM Peak Hour |
| 1. First St / D St | Eastbound | 250 | 200 | 275 |
| 2. First St / E St / Richards Blvd | Northbound | 625 | 400 | 250 |
|  | Eastbound | 225 | 275 | 300 |
|  | Westbound | 225 | 250 | 250 |
| 3. Olive Dr / Richards Blvd | Northbound | 525 | 600 | 675 |
|  | Southbound | 625 | $\underline{675}$ | 625 |
|  | Westbound | >1,500 | 100 | 200 |
| 4. I-80 Westbound Ramps / Richards Blvd | Northbound | 815 | 575 | 675 |
|  | Southbound | 500 | 300 | 325 |
|  | Westbound | 1,250 | 600 | 275 |
| 5. I-80 Eastbound Ramps / Richards Blvd | Northbound | 440 | 300 | 400 |
|  | Southbound | 850 | 225 | 225 |
|  | Westbound | 1,270 | 500 | 775 |
| 6. Research Park Dr / Richards Blvd / Cowell Blvd | Eastbound | 440 | 475 | 450 |
| Notes: Bold and underline font indicate a queue length that is greater than the storage length. The storage length and average maximum queue length is reported in feet. <br> Source: Fehr \& Peers, 2018 |  |  |  |  |

Table 20 presents the average maximum queue length for selected approaches to the study intersection under the Build Alternative (see the appendix for detailed analysis results). The off-ramp queues would be contained on the ramps during both peak hours. The results show three areas with queues that exceed the storage length.

- At Richards Boulevard/Olive Drive, queues on the southbound approach extend to First Street during both peak hours. This queuing would extend upstream on the eastbound and westbound approaches to the First Street/E Street intersection.
- Also, the northbound approach at Richards Boulevard/Olive Drive would extend back to the I-80 Westbound Ramps during both peak hours. However, this queue would not cause upstream queuing issues.
- The third location is the eastbound approach at Research Park Drive (southbound Richards Boulevard), which would have a queue that extends into the upstream intersection. Although the queue would cause additional delay at the upstream intersection, the queues would be contained.


### 6.2 Freeway Operations

Freeway operations were analyzed for design year (2042) conditions under AM and PM peak hour conditions. Table 21 and Table 22 show the freeway LOS and density for the study segments (see the appendix for detailed analysis results).

Table 21: Eastbound Freeway Operations - Design Year Conditions

| Segment | Facility Type | No Build Alternative |  | Build Alternative |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | AM | PM | AM | AM |
| West of Old Davis Rd On-ramp | Basic | C / 22 | C / $21^{2}$ | Same as No Build Alternative |  |
| Old Davis Road On-ramp | Basic ${ }^{1}$ | B / 17 | B/ $17^{2}$ |  |  |
| Old Davis Road to Lane Drop | Basic | C / 22 | B/ $22^{2}$ |  |  |
| Lane Drop to Richards Blvd | Basic | D / 33 | D / 33 ${ }^{2}$ |  |  |
| Richards Blvd Off-ramp | Diverge | E/36 | E/ $36{ }^{2}$ |  |  |
| Richards Blvd Off-ramp to On-ramp | Basic | C / 26 | D / $26^{2}$ |  |  |
| Richards Blvd On-ramp | Merge | D / 30 | D / $31^{2}$ |  |  |
| Richards Blvd to Chiles Rd | Basic | D / 29 | D / $29{ }^{2}$ |  |  |
| Chiles Rd Off-ramp | Diverge | B / 18 | B/ $19{ }^{2}$ |  |  |
| East of Chiles Rd Off-ramp | Basic | C / 24 | C / $26^{2}$ |  |  |

Note: Density is reported in passenger car equivalents per lane per mile.

1. Since the acceleration lane is greater than 1,500 feet, the location is classified as a basic segment according to the HCM .
2. Actual design year conditions may be worse if planned improvements (HOV lane, ramp metering, and other active traffic management strategies) are unable to prevent downstream congestion from extending into the study area.
Source: Fehr \& Peers, 2018
With the increased volumes, some freeway segments that operated at LOS D under construction year conditions worsen to LOS E. Since I-80 is assumed to be widened to provide HOV lanes at the Yolo Bypass bottleneck, the eastbound freeway segments no longer listed as LOS F during the PM peak hour. However,
congested conditions may still occur under design year conditions if the planned improvements are unable to prevent downstream congestion from extending into the study area.

In the westbound direction, the Richards Boulevard off-ramp segment would have the highest density and would be the only segment with LOS E conditions. In the westbound direction, all segments would have LOS D or better conditions for the No Build Alternative. For the Build Alternative, the consolidation of the westbound off-ramps results in LOS E conditions at Richards Boulevard during the AM peak hour. Despite this, no freeway segments would have project impacts under design year conditions since LOS E is considered acceptable.

Table 22: Westbound Freeway Operations - Design Year Conditions

| Segment | Facility Type | No Build Alternative |  | Build Alternative |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | AM | PM | AM | PM |
| East of Mace Blvd On-ramp | Basic | D / 28 | C / 23 | D / 28 | C / 23 |
| Mace Blvd to Lane Drop | Basic | C / 22 | C / 21 | C / 22 | C / 21 |
| Lane Drop to Olive Dr | Basic | D / 32 | D / 29 | D / 32 | D / 29 |
| Olive Dr Off-ramp | Diverge | D / 35 | D / 33 |  |  |
| Olive Dr to Richards Blvd | Basic | D / 30 | D / 28 |  |  |
| Richards Blvd NB Off-ramp | Diverge | D / 34 | D / 33 | E / 36 | D / 34 |
| Richards Blvd NB Off-ramp to On-ramp | Basic | C / 26 | D / 26 | C / 24 | C / 25 |
| Richards Blvd NB On-ramp to SB Off-ramp | Weave ${ }^{1}$ | C / 26 (D) | C / 28 (D) |  |  |
| Richards Blvd SB Off-ramp to On-ramp | Basic | D / 27 | D / 30 |  |  |
| Richards Blvd SB On-ramp | Merge | D / 29 | D / 33 | D / 31 | E/35 |
| Richards Blvd to Old Davis Rd | Basic | D / 28 | D / 33 | D / 28 | D / 33 |
| Old Davis Rd Off-ramp | Diverge | D / 33 | C / 28 | D / 33 | C / 28 |
| West of Old Davis Rd Off-ramp | Basic | B / 18 | C / 21 | B / 18 | C / 21 |

Notes: Density is reported in passenger car equivalents per lane per mile.

1. For the weave segment, the LOS from the Leisch Method is also reported in parentheses.

Source: Fehr \& Peers, 2018

### 6.3 Roadway Safety

Using the forecasted daily volume, predicted collisions were calculated for design year conditions under the project alternatives as shown in Table 23 (see the appendix for detailed analysis results). Under the No Build Alternative, the current five ramps in the westbound direction at Olive Drive and Richards Boulevard would
be expected to have 5.7 collisions per year, with 2.2 fatality and injury-related collisions. With the Build Alternative, the westbound ramps are reduced from 5 to 2 and the ramp roadways are reconfigured to have curves that are less sharp (that is, a higher radius). The expected total collision rate would be 2.1 collisions per year, with 1.0 fatality and injury-related collisions. Under the Build Alternative, the expected total collision rate would be reduced by 63 percent of the No Build Alternative rate, and the fatality and injuryrelated rate would be reduced by about 55 percent.

Table 23: Freeway Ramp Collision Rate - Design Year Conditions

|  | No Build Alternative |  |  | Build Alternative |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Focation | PDO | Total | F+I | PDO | Total |
| WB On from SB Richards Blvd | 0.357 | 0.416 | 0.773 | 0.557 | 0.548 | 1.105 |
| WB Off to SB Richards Blvd | 0.585 | 0.878 | 1.463 | - | - | - |
| WB On from NB Richards Blvd | 0.696 | 1.421 | 2.117 | - | - | - |
| WB Off to NB Richards Blvd | 0.510 | 0.659 | 1.169 | 0.456 | 0.524 | 0.980 |
| WB Off to Olive Dr | 0.082 | 0.084 | 0.166 | - | - | - |
| Total | 2.230 | 3.458 | 5.688 | 1.013 | 1.072 | 2.085 |

Note: Values are in collisions per year.
Source: Fehr \& Peers, 2018

### 6.4 Ramp Meter Storage

The Build Alternative includes the construction of a ramp meter signal on the proposed diagonal westbound on-ramp. An HOV preferential lane is required at ramp meter locations according to the Ramp Meter Design Manual (Caltrans 2016). To confirm that two general purpose lanes would provide adequate storage, the expected arrival rate and practical discharge rate were compared under design year (2042) conditions. The arrival rate was based on the arrival rate as counted in May 2016. The HOV percentage was assumed to 15 percent.

Table 24 shows the maximum metering rates and corresponding maximum queues for one and two general purpose lanes. The storage length was measured at 630 feet from the stop bar to the end of the HOV lane using the draft geometric approval drawing. With one lane for storage at the ramp meter, the AM peak period demand volume under design year conditions could be stored on the ramp. However, the PM peak period demand would exceed the available storage at the maximum practical metering rate of 900 vehicles per hour per lane. As a result, two general purpose lanes would be needed to serve the design year peak period demand.

Table 24: Ramp Meter Storage Analysis - Design Year Conditions

| Configuration | Storage Length | Maximum Metering Rate |  | Maximum Queue |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | AM | PM | AM | PM |
| 1 general purpose lane and 1 HOV lane | 630 ft | 575 vph | 900 vph | 606 ft | $\underline{\mathbf{3 , 2 6 1 ~ f t}}$ |
| 2 general purpose lanes and 1 HOV lane | $\begin{gathered} 630 \mathrm{ft} \\ \text { (each lane) } \end{gathered}$ | 540 vph | 990 vph | 566 ft | 618 ft |

Note: Bold and underline font indicate that the queue would not be contained on the ramp. The maximum practical metering rate is 900 vehicles per hour (vph) per lane.
Source: Fehr \& Peers, 2018
The Ramp Meter Design Manual also states that the "minimum storage length should be designed based on seven percent ( $7 \%$ ) of the peak hour demand for the design year" for new or reconstructed on-ramps. Seven percent of the peak hour design year volume ( $1,080 \mathrm{vph}$ during the PM peak hour) is 76 vehicles. Assuming 30 feet per vehicle, 15 percent HOV volume, and two storage lanes, the required storage length general purpose would be about 965 feet. As noted in Table 24, the proposed ramp storage is 630 feet, which is 335 feet short.

As noted in the manual, additional storage capacity can be provided on the local street. At the ramp terminal intersection, the right-turn pocket length is 150 feet (one lane), and the left-turn pocket length is 400 feet (two lanes). Under peak hour conditions, the northbound left turn volume onto the ramp is about twice the southbound right turn volume ( 810 versus 420 vehicles per hour). The additional needed 335 feet for two lanes of storage can then be allocated one-third to the right turn pocket ( 112 feet of two-lane storage or about 225 feet of one-lane storage) and two-thirds to the left turn pocket (about 225 feet). The northbound left turn pocket would have sufficient storage, but the southbound right turn pocket would need to be lengthened by about 75 feet to meet the 7 percent storage requirement.

### 6.5 Multimodal Facilities

### 6.5.1 Transit System

The Build Alternative will relocate the Unitrans bus stop on northbound Richards Boulevard at Olive Drive from a near side to a far side location. This will move the boarding area from a median between two lanes of traffic to the roadway shoulder thereby improving the waiting experience for passengers. The far side location also would allow buses to more easily reenter the roadway compared to the near side location that requires buses to merge into traffic in the intersection.

The improvement in intersection operations with the Build Alternative will also improve bus operations and travel time.

### 6.5.2 Bicycle System

The Build Alternative will provide a grade-separated two-way path for bicycles and pedestrians on the west side of the interchange. The path will function as an extension of the existing path on the west side of Richards Boulevard between First Street and Olive Drive that travels through a tunnel under the Union Pacific Railroad. South of Olive Drive, the path will run adjacent to Richards Boulevard. Approaching the interchange, the path will diverge from the roadway and then travel under the westbound on-ramp. Then, the path will loop around and travel over the path and adjacent to the westbound on-ramp to reach the freeway overcrossing. The path will continue adjacent to, but barrier-separated from, Richards Boulevard south to the Research Park Drive intersection.

The existing Class II (on-street) bicycle lanes will be maintained on Richards Boulevard. The reconstructed intersection at the I-80 Westbound Ramps will have slower speed turns than the existing configuration, which will provide a safer environment for on-street bicyclists.

### 6.5.3 Pedestrian System

The Build Alternative will replace the sidewalk and crosswalks on the west side of the interchange with the grade-separated pathway for bicycles and pedestrians described in the previous section. At the loop on the pathway, stairs will be provided so that pedestrians can travel a shorter route.

At the Olive Drive and Research Park Drive intersections, crosswalks would be provided on all legs. At Olive Drive, the wider approaches would result in longer crossing distances on three of the four approaches. Longer crossing distance increases pedestrian exposure and therefore reduces pedestrian safety. As noted above, the median bus stop on the northbound approach would be moved to the shoulder of the northbound departure. Pedestrians traveling to the bus stop would have less exposure to conflicting vehicles.

At Research Park Drive, the west leg (Richards Boulevard) would be reconstructed to provide an additional eastbound lane. However, the southwest corner would be rebuilt with a smaller radius such that the crosswalks on the west and south legs would be shorter than under existing conditions. The shorter crossing distance would reduce pedestrian exposure and therefore improve pedestrian safety.

### 6.5.4 Freight System

As noted above, the intersection curb returns would be reconstructed with a smaller radius at some study intersections. However, all turning movements will be designed to accommodate a California legal 65-foot design vehicle so that heavy vehicles can safely travel through the study area.

## Chapter 7. Summary and Conclusions

### 7.1 Deficiencies

The study locations that operate or would operate over capacity (LOS F) are summarized below by alternative.

## Existing Conditions

- Intersections
- I-80 Westbound Ramps/Richards Boulevard (AM)
- Freeway Segments
- I-80 Eastbound, Old Davis Road to Mace Boulevard (PM)

No Build Alternative, Construction Year Conditions

- Intersections
- Olive Drive/Richards Boulevard (AM)
- I-80 Westbound Ramps/Richards Boulevard (AM)
- I-80 Eastbound Ramps/Richards Boulevard (PM)
- Freeway Segments
- I-80 Eastbound, Old Davis Road to Mace Boulevard (PM)


## Build Alternative, Construction Year Conditions

- Freeway Segments
- I-80 Eastbound, Old Davis Road to Mace Boulevard (PM)

No Build Alternative, Design Year Conditions

- Intersections
- First Street/D Street (AM)
- First Street/E Street/Richards Boulevard (AM)
- Olive Drive/Richards Boulevard (AM and PM)
- I-80 Westbound Ramps/Richards Boulevard (AM)


### 7.2 Project Impacts

A project impact occurs where (1) the LOS threshold is exceeded and (2) the conditions are worse in Build Alternative than the No Build Alternative. The LOS thresholds are provided in Section 2.5.

The proposed project does not have impacts to intersections or freeway segments.

### 7.3 Potential Mitigation Measures

Since the proposed project does not have impacts, no mitigation measures were identified.

### 7.4 Design Designation

Table 25 shows the traffic data needed for the design designation for project roadways per the Highway Design Manual (Caltrans, 2012). The existing daily volume for I-80 comes from the traffic volumes published by Caltrans (http://www.dot.ca.gov/trafficops/census/). The existing daily volume estimate for Richards Boulevard uses the ratio of daily volume to peak hour volume for the segment of Richards Boulevard between First Street and Olive Drive. The future year volumes are based on the Build Alternative and use the existing ratio of daily to peak hour volume to estimate daily volume.

Table 25: Traffic Data for Design Designation

| Scenario |  | I-80 east of Olive Dr |  | Richards Blvd at I-80 |  |
| :--- | :---: | :---: | :---: | :---: | :---: |
|  | Year | Annual ADT | Peak Hour | Annual ADT | Peak Hour |
|  |  | 133,600 | 8,898 | 23,950 | 1,609 |
| Construction Year | 2022 | 144,350 | 9,620 | 27,920 | 1,890 |
| Design Year | 2042 | 180,180 | 12,000 | 41,160 | 2,800 |

Source: Fehr \& Peers, 2018
Table 26 provides the traffic index for roadway pavement design according the Highway Design Manual (see the appendix for detailed calculations). For I-80, the distribution of trucks based on the number of axles come from a truck classification count collected at Richards Boulevard in 2000 as shown in the 2015 Daily Truck Traffic (http://www.dot.ca.gov/trafficops/census/docs/2015 aadt truck.pdf).

## Table 26: Traffic Index

| Parameter | Roadway |  |
| :--- | :---: | :---: |
|  | I-80 | Richards Boulevard |
| Directional Split (\%) | $50 \%$ | $50 \%$ |
| Trucks (\%) | $9 \%$ | $2 \%$ |
| 10-Year Traffic Index | $13.5 / 11.5$ (Outside/Inside) | 10.0 |
| 20-Year Traffic Index | $14.5 / 12.5$ (Outside/Inside) | 10.0 |

Source: Fehr \& Peers, 2018

### 7.5 Alternative Comparison

Table 27 compares the alternatives based on the design year performance measures reported above. The performance measures are the network-wide VMT (vehicle miles of travel) and VHD (vehicle hours of delay); intersection operations deficiencies; and expected collisions.

Table 27: Alternative Comparison Summary - Design Year Conditions

| Category | No Build <br> Alternative | Build Alternative | Difference |
| :--- | :---: | :---: | :---: |
| Vehicle Miles of Travel (VMT) | $2,980,219$ | $2,979,159$ | $-1,060(-0.04 \%)$ |
| Vehicle Hours of Delay (VHD) | 21,965 | 21,911 | $-54(-0.25 \%)$ |
| Intersection Operations Deficiencies | 9 of 12 | 0 | -9 |
| Expected Total Collisions on Westbound Ramps | 5.7 per year | 2.1 per year | -3.6 per year |

Source: Fehr \& Peers, 2018
The Build Alternative would provide a small reduction in VMT by shifting trips originating in the City of Davis to shorter local routes with the closure of the Olive Drive westbound off-ramp. Network-wide delay would also be reduced by shifting trips from lower-speed Olive Drive to higher-speed I-80 and Richards Boulevard.

The Build Alternative would provide more capacity along Richards Boulevard from Olive Drive to Research Park Drive. Intersections that would be over capacity under the No Build Alternative would operate with LOS E or better conditions.

The reconfiguration of the westbound ramps at Richards Boulevard from a cloverleaf to a diamond design will remove the loop on-ramp and off-ramp, which have higher collision rates than slip or diagonal rates.

Even though the volume will be higher on the combined ramps, especially on the off-ramp with the closure of the Olive Drive off-ramp, the combined westbound ramp collision rate for the Build Alternative is expected to be less than half the rate of the No Build Alternative under design year conditions.

Given the advantages in network efficiency, intersection operations, and freeway ramp safety, the Build Alternative is recommended to provide the best traffic operations and safety.

## Chapter 8. References

The references cited in the Transportation Analysis Report are listed below.

- 2017 California Regional Transportation Plan Guidelines (CTC, January 2017)
- Caltrans Traffic Census Program, http://www.dot.ca.gov/trafficops/census/ accessed October 2017
- Caltrans Performance Measurement System (PeMS), http://pems.dot.ca.gov/, accessed October 2017.
- City of Davis General Plan (City of Davis, December 2013)
- Enhanced Interchange Safety Analysis Tool: User Manual. Texas Transportation Institute, Texas A\&M University, College Station, Texas, July 2013.
- Highway Capacity Manual, 6th Edition (Transportation Research Board, 2016)
- Highway Design Manual (Caltrans, 2012)
- Highway Safety Manual (American Association of State Highway and Transportation Officials, 2010)
- Interstate 80 Transportation Concept Report (Caltrans, July 2017)
- Ramp Meter Design Manual (Caltrans, 2016)
- Statewide Integrated Taffic Records System (SWITRS), California Highway Patrol, http://iswitrs.chp.ca.gov, accessed December 2017
- Traffic Accident Surveillance and Analysis System (TASAS), Caltrans, accessed November 2017
- Traffic Analysis Toolbox Volume III - Guidelines for Applying Traffic Microsimulation Modeling Software (FHWA, 2003)

FehrłPeers

# Interstate 80 / Richards Boulevard Interchange 

# Transportation Analysis Report APPENDIX 

Prepared for:<br>City of Davis

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I-80 / Richards Blvd PDT
VISSIM Calibration

| Existing AM Peak Hour |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Measured Volumes | Modeled Conditions |  |  |  | Link Flow Criteria |  | Link GEH Criteria |  |
|  |  |  | DemandVolume (vph) | Served Volume (vph) | Difference |  |  | Measure | Meets Target? | Target | Meets Target? |
| ID | Link | Direction |  |  | vph | \% | GEH |  |  |  |  |
| 19 | D St S. of 1st St | NB | 55 | 54.7 | -0.3 | -0.5\% | 0.0 | +/-100 vph | Yes | < 5 | Yes |
| 20 | D St S. of 1st St | SB | 82 | 76.3 | -5.7 | -7.0\% | 0.6 | +/-100 vph | Yes | < 5 | Yes |
| 21 | D St between 1st St and 2nd St | NB | 68 | 59.3 | -8.7 | -12.8\% | 1.1 | +/-100 vph | Yes | < 5 | Yes |
| 22 | D St between 2nd St and 1st St | SB | 59 | 58.8 | -0.2 | -0.3\% | 0.0 | +/-100 vph | Yes | < 5 | Yes |
| 23 | 1st St between C St and D St | EB | 296 | 301.5 | 5.5 | 1.9\% | 0.3 | +/-100 vph | Yes | < 5 | Yes |
| 24 | 1st St between D St and C St | WB | 464 | 465.6 | 1.6 | 0.3\% | 0.1 | +/-100 vph | Yes | < 5 | Yes |
| 25 | 1st St between D St and E St / Richards Blvd | EB | 314 | 319.7 | 5.7 | 1.8\% | 0.3 | +/-100 vph | Yes | < 5 | Yes |
| 26 | 1st St between E St / Richards Blvd and D St | WB | 518 | 507.4 | -10.6 | -2.0\% | 0.5 | +/-100 vph | Yes | < 5 | Yes |
| 27 | Richards Blvd between Olive Dr and 1st St | NB | 806 | 785.9 | -20.1 | -2.5\% | 0.7 | +/-400 vph | Yes | < 5 | Yes |
| 28 | Richards Blvd between 1st St and Olive Dr | SB | 497 | 502.1 | 5.1 | 1.0\% | 0.2 | +/-100 vph | Yes | < 5 | Yes |
| 29 | E St between 1st St and 2nd St | NB | 98 | 101.2 | 3.2 | 3.3\% | 0.3 | +/-100 vph | Yes | < 5 | Yes |
| 30 | E St between 2nd St and 1st St | SB | 96 | 95.3 | -0.7 | -0.7\% | 0.1 | +/-100 vph | Yes | < 5 | Yes |
| 31 | 1st St between E St / Richards Blvd and F St | EB | 253 | 238.5 | -14.5 | -5.7\% | 0.9 | +/-100 vph | Yes | < 5 | Yes |
| 32 | 1st St between F St and E St / Richards Blvd | WB | 150 | 148.6 | -1.4 | -0.9\% | 0.1 | +/-100 vph | Yes | < 5 | Yes |
| 33 | Richards Blvd between Hotel and Olive Dr | NB | 723 | 714.6 | -8.4 | -1.2\% | 0.3 | +/-400 vph | Yes | < 5 | Yes |
| 34 | Richards Blvd between Olive Dr and Hotel | SB | 604 | 607.2 | 3.2 | 0.5\% | 0.1 | +/-100 vph | Yes | < 5 | Yes |
| 35 | Olive Dr west of Richards Blvd | EB | 102 | 101.6 | -0.4 | -0.4\% | 0.0 | +/-100 vph | Yes | < 5 | Yes |
| 36 | Olive Dr west of Richards Blvd | WB | 124 | 121.9 | -2.1 | -1.7\% | 0.2 | +/-100 vph | Yes | < 5 | Yes |
| 37 | Olive Dr between Richards Blvd and Dwy | EB | 69 | 69.2 | 0.2 | 0.3\% | 0.0 | +/-100 vph | Yes | < 5 | Yes |
| 38 | Olive Dr between Dwy and Richards Blvd | WB | 281 | 268.6 | -12.4 | -4.4\% | 0.7 | +/-100 vph | Yes | < 5 | Yes |
| 39 | Richards Blvd between Olive Dr and I-80 WB Ramps | SB | 617 | 617.5 | 0.5 | 0.1\% | 0.0 | +/-100 vph | Yes | < 5 | Yes |
| 40 | Richards Blvd between I-80 WB Ramps and Olive Dr | NB | 789 | 778.6 | -10.4 | -1.3\% | 0.4 | +/-400 vph | Yes | < 5 | Yes |
| 41 | I-80 WB Off-Ramp to Richards Blvd NB | WB | 389 | 380.2 | -8.8 | -2.3\% | 0.4 | +/-100 vph | Yes | < 5 | Yes |
| 42 | I-80 WB On-Ramp from Richards Blvd NB | EB | 359 | 357.5 | -1.5 | -0.4\% | 0.1 | +/-100 vph | Yes | < 5 | Yes |
| 43 | I-80 WB Off-Ramp to Richards Blvd SB | EB | 179 | 178.5 | -0.5 | -0.3\% | 0.0 | +/-100 vph | Yes | < 5 | Yes |
| 44 | I-80 WB On-Ramp to Richards Blvd SB | WB | 195 | 189.8 | -5.2 | -2.7\% | 0.4 | +/-100 vph | Yes | < 5 | Yes |
| 45 | Richards Blvd from I-80 WB Ramps to I-80 EB Ramps | SB | 601 | 606.2 | 5.2 | 0.9\% | 0.2 | +/-100 vph | Yes | < 5 | Yes |
| 46 | Richards Blvd from I-80 EB Ramps to I-80 WB Ramps | NB | 759 | 755.9 | -3.1 | -0.4\% | 0.1 | +/-400 vph | Yes | < 5 | Yes |
| 47 | I-80 EB Off-Ramp to Richards Blvd | WB | 613 | 611.9 | -1.1 | -0.2\% | 0.0 | +/-100 vph | Yes | < 5 | Yes |
| 48 | I-80 EB On-Ramp from Richards Blvd | EB | 334 | 338 | 4 | 1.2\% | 0.2 | +/-100 vph | Yes | < 5 | Yes |
| 49 | Richards Blvd from I-80 EB Ramps to KFC | SB | 789 | 793.1 | 4.1 | 0.5\% | 0.1 | +/-400 vph | Yes | < 5 | Yes |
| 50 | Richards Blvd from KFC to I-80 EB Ramps | NB | 668 | 672.9 | 4.9 | 0.7\% | 0.2 | +/-100 vph | Yes | < 5 | Yes |
| 51 | Richards Blvd from KFC to Research Park Dr | EB | 789 | 790.8 | 1.8 | 0.2\% | 0.1 | +/-400 vph | Yes | < 5 | Yes |
| 52 | Richards Blvd from Research Park Dr to KFC | WB | 663 | 667.8 | 4.8 | 0.7\% | 0.2 | +/-100 vph | Yes | < 5 | Yes |
| 53 | Cowell Blvd from Research Park Dr to Drew Ave | EB | 521 | 522.1 | 1.1 | 0.2\% | 0.0 | +/-100 vph | Yes | < 5 | Yes |
| 54 | Cowell Blvd from Drew Ave to Research Park Dr | WB | 537 | 543.2 | 6.2 | 1.2\% | 0.3 | +/-100 vph | Yes | < 5 | Yes |
| 55 | Research Park Dr from Richards Blvd / Cowell Blvd to Drew A | NB | 183 | 186.6 | 3.6 | 2.0\% | 0.3 | +/-100 vph | Yes | < 5 | Yes |
| 56 | Research Park Dr from Drew Ave to Richards Blvd / Cowell Bl | SB | 123 | 123.1 | 0.1 | 0.1\% | 0.0 | +/-100 vph | Yes | < 5 | Yes |
| 57 | Research Park Dr from to Richards Blvd / Cowell Blvd | NB | 100 | 99.9 | -0.1 | -0.1\% | 0.0 | +/-100 vph | Yes | < 5 | Yes |
| 58 | Research Park Dr from Richards Blvd / Cowell Blvd to | SB | 182 | 180.5 | -1.5 | -0.8\% | 0.1 | +/-100 vph | Yes | < 5 | Yes |
|  | Total |  | 15049 | 14992.1 | -56.9 | -0.4\% | 0.5 | +/-5\% | Yes | <4 | Yes |


| All Link Flows |  |  |  |
| :---: | :---: | :---: | :---: |
| Link Flow Criteria |  | Link GEH Criteria |  |
| Measure | \% Cases | Measure | \% Cases |
| $>85 \%$ | $100 \%$ | $>85 \%$ | $100 \%$ |
| Met Target |  | Met Target |  |

I-80 / Richards Blvd PDT
VISSIM Calibration

| Existing PM Peak Hour |  |  |  |  |  |  |  |  |  | Link GEH Criteria |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Measured Volumes | Modeled Conditions |  |  |  | Link Flow Criteria |  |  |  |
|  |  |  | DemandVolume (vph) | Served Volume(vph) | Difference |  |  | Measure | Meets Target? | Target | Meets Target? |
| ID | Link | Direction |  |  | vph | \% | GEH |  |  |  |  |
| 19 | D St S. of 1st St | NB | 129 | 129 | 0 | 0.0\% | 0.0 | +/-100 vph | Yes | < 5 | Yes |
| 20 | D St S. of 1st St | SB | 165 | 163 | -2 | -1.2\% | 0.2 | +/-100 vph | Yes | < 5 | Yes |
| 21 | D St between 1st St and 2nd St | NB | 103 | 104.9 | 1.9 | 1.8\% | 0.2 | +/-100 vph | Yes | < 5 | Yes |
| 22 | D St between 2nd St and 1st St | SB | 135 | 134.4 | -0.6 | -0.4\% | 0.1 | +/-100 vph | Yes | < 5 | Yes |
| 23 | 1st St between C St and D St | EB | 447 | 449.7 | 2.7 | 0.6\% | 0.1 | +/-100 vph | Yes | < 5 | Yes |
| 24 | 1st St between D St and C St | WB | 356 | 351.1 | -4.9 | -1.4\% | 0.3 | +/-100 vph | Yes | < 5 | Yes |
| 25 | 1st St between D St and E St / Richards Blvd | EB | 520 | 530.5 | 10.5 | 2.0\% | 0.5 | +/-100 vph | Yes | < 5 | Yes |
| 26 | 1st St between E St / Richards Blvd and D St | WB | 433 | 431.1 | -1.9 | -0.4\% | 0.1 | +/-100 vph | Yes | < 5 | Yes |
| 27 | Richards Blvd between Olive Dr and 1st St | NB | 734 | 728.6 | -5.4 | -0.7\% | 0.2 | +/-400 vph | Yes | < 5 | Yes |
| 28 | Richards Blvd between 1st St and Olive Dr | SB | 824 | 823.2 | -0.8 | -0.1\% | 0.0 | +/-400 vph | Yes | < 5 | Yes |
| 29 | E St between 1st St and 2nd St | NB | 124 | 125.4 | 1.4 | 1.1\% | 0.1 | +/-100 vph | Yes | < 5 | Yes |
| 30 | E St between 2nd St and 1st St | SB | 193 | 188.1 | -4.9 | -2.5\% | 0.4 | +/-100 vph | Yes | < 5 | Yes |
| 31 | 1st St between E St / Richards Blvd and F St | EB | 309 | 302.5 | -6.5 | -2.1\% | 0.4 | +/-100 vph | Yes | < 5 | Yes |
| 32 | 1st St between F St and E St / Richards Blvd | WB | 243 | 238.8 | -4.2 | -1.7\% | 0.3 | +/-100 vph | Yes | < 5 | Yes |
| 33 | Richards Blvd between Hotel and Olive Dr | NB | 634 | 621.5 | -12.5 | -2.0\% | 0.5 | +/-100 vph | Yes | < 5 | Yes |
| 34 | Richards Blvd between Olive Dr and Hotel | SB | 914 | 904.2 | -9.8 | -1.1\% | 0.3 | +/-400 vph | Yes | < 5 | Yes |
| 35 | Olive Dr west of Richards Blvd | EB | 111 | 111.2 | 0.2 | 0.2\% | 0.0 | +/-100 vph | Yes | < 5 | Yes |
| 36 | Olive Dr west of Richards Blvd | WB | 97 | 95 | -2 | -2.1\% | 0.2 | +/-100 vph | Yes | < 5 | Yes |
| 37 | Olive Dr between Richards Blvd and Dwy | EB | 149 | 148.3 | -0.7 | -0.5\% | 0.1 | +/-100 vph | Yes | < 5 | Yes |
| 38 | Olive Dr between Dwy and Richards Blvd | WB | 325 | 316.2 | -8.8 | -2.7\% | 0.5 | +/-100 vph | Yes | < 5 | Yes |
| 39 | Richards Blvd between Olive Dr and I-80 WB Ramps | SB | 956 | 929.3 | -26.7 | -2.8\% | 0.9 | +/-400 vph | Yes | < 5 | Yes |
| 40 | Richards Blvd between I-80 WB Ramps and Olive Dr | NB | 668 | 656.5 | -11.5 | -1.7\% | 0.4 | +/-100 vph | Yes | < 5 | Yes |
| 41 | I-80 WB Off-Ramp to Richards Blvd NB | WB | 221 | 217.9 | -3.1 | -1.4\% | 0.2 | +/-100 vph | Yes | < 5 | Yes |
| 42 | I-80 WB On-Ramp from Richards Blvd NB | EB | 437 | 413.6 | -23.4 | -5.4\% | 1.1 | +/-100 vph | Yes | < 5 | Yes |
| 43 | I-80 WB Off-Ramp to Richards Blvd SB | EB | 90 | 89.5 | -0.5 | -0.6\% | 0.1 | +/-100 vph | Yes | < 5 | Yes |
| 44 | I-80 WB On-Ramp to Richards Blvd SB | WB | 321 | 307.2 | -13.8 | -4.3\% | 0.8 | +/-100 vph | Yes | < 5 | Yes |
| 45 | Richards Blvd from I-80 WB Ramps to I-80 EB Ramps | SB | 725 | 711.6 | -13.4 | -1.8\% | 0.5 | +/-400 vph | Yes | < 5 | Yes |
| 46 | Richards Blvd from I-80 EB Ramps to I-80 WB Ramps | NB | 884 | 852.2 | -31.8 | -3.6\% | 1.1 | +/-400 vph | Yes | < 5 | Yes |
| 47 | I-80 EB Off-Ramp to Richards Blvd | WB | 730 | 702.1 | -27.9 | -3.8\% | 1.0 | +/-400 vph | Yes | < 5 | Yes |
| 48 | I-80 EB On-Ramp from Richards Blvd | EB | 315 | 306.5 | -8.5 | -2.7\% | 0.5 | +/-100 vph | Yes | < 5 | Yes |
| 49 | Richards Blvd from I-80 EB Ramps to KFC | SB | 1088 | 1052 | -36 | -3.3\% | 1.1 | +/-400 vph | Yes | < 5 | Yes |
| 50 | Richards Blvd from KFC to l-80 EB Ramps | NB | 832 | 802.3 | -29.7 | -3.6\% | 1.0 | +/-400 vph | Yes | < 5 | Yes |
| 51 | Richards Blvd from KFC to Research Park Dr | EB | 1088 | 1056.6 | -31.4 | -2.9\% | 1.0 | +/-400 vph | Yes | < 5 | Yes |
| 52 | Richards Blvd from Research Park Dr to KFC | WB | 814 | 819.1 | 5.1 | 0.6\% | 0.2 | +/-400 vph | Yes | < 5 | Yes |
| 53 | Cowell Blvd from Research Park Dr to Drew Ave | EB | 803 | 794.3 | -8.7 | -1.1\% | 0.3 | +/-400 vph | Yes | < 5 | Yes |
| 54 | Cowell Blvd from Drew Ave to Research Park Dr | WB | 590 | 602.1 | 12.1 | 2.1\% | 0.5 | +/-100 vph | Yes | < 5 | Yes |
| 55 | Research Park Dr from Richards Blvd / Cowell Blvd to Drew A | NB | 298 | 288.7 | -9.3 | -3.1\% | 0.5 | +/-100 vph | Yes | < 5 | Yes |
| 56 | Research Park Dr from Drew Ave to Richards Blvd / Cowell Bl | SB | 173 | 173.5 | 0.5 | 0.3\% | 0.0 | +/-100 vph | Yes | < 5 | Yes |
| 57 | Research Park Dr from to Richards Blvd / Cowell Blvd | NB | 157 | 157.7 | 0.7 | 0.4\% | 0.1 | +/-100 vph | Yes | < 5 | Yes |
| 58 | Research Park Dr from Richards Blvd / Cowell Blvd to | SB | 93 | 87.8 | -5.2 | -5.6\% | 0.5 | +/-100 vph | Yes | < 5 | Yes |
|  | Total |  | 18228 | 17917.2 | -310.8 | -1.7\% | 2.3 | +/-5\% | Yes | <4 | Yes |


| All Link Flows |  |  |  |
| :---: | :---: | :---: | :---: |
| Link Flow Criteria |  | Link GEH Criteria |  |
| Measure | \% Cases | Measure | \% Cases |
| $>85 \%$ | $100 \%$ | $>85 \%$ | $100 \%$ |
| Met Target |  | Met Target |  |

## Volume and Delay by Movement

AM Peak Hour

Intersection 1
D St/First St
Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) |  |  |  |  |  | Total Delay (sec/veh) |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Average | Percent | Std. Dev. | Minimum | Maximum | GEH | Average | Std. Dev. | Minimum | Maximum | LOS |
| NB | Left Turn | 12 | 11 | 93.3\% | 2.7 | 7 | 15 | 0.2 | 51.2 | 27.6 | 4.5 | 84.5 | D |
|  | Through | 15 | 14 | 94.7\% | 1.9 | 12 | 17 | 0.2 | 52.1 | 29.6 | 28.7 | 90.5 | D |
|  | Right Turn | 28 | 29 | 104.6\% | 2.9 | 25 | 33 | 0.2 | 5.9 | 0.6 | 3.6 | 7.4 | A |
|  | Subtotal | 55 | 55 | 99.5\% | 0.7 | 54 | 56 | 0.0 | 30.4 | 14.0 | 15.7 | 47.5 | C |
| SB | Left Turn | 24 | 23 | 95.4\% | 2.6 | 20 | 28 | 0.2 | 51.0 | 17.4 | 28.5 | 86.9 | D |
|  | Through | 20 | 20 | 98.0\% | 2.5 | 16 | 24 | 0.1 | 55.4 | 10.2 | 29.7 | 65.8 | E |
|  | Right Turn | 15 | 16 | 108.7\% | 2.5 | 13 | 21 | 0.3 | 16.0 | 11.1 | 6.7 | 41.3 | B |
|  | Subtotal | 59 | 59 | 99.7\% | 0.4 | 58 | 59 | 0.0 | 45.5 | 9.6 | 24.1 | 68.5 | D |
| EB | Left Turn | 3 | 3 | 90.0\% | 1.4 | 0 | 5 | 0.2 | 33.7 | 40.6 | 0.0 | 126.2 | C |
|  | Through | 262 | 269 | 102.7\% | 7.1 | 258 | 280 | 0.4 | 10.5 | 2.9 | 8.7 | 14.4 | B |
|  | Right Turn | 31 | 30 | 96.1\% | 5.9 | 21 | 40 | 0.2 | 11.5 | 10.0 | 2.7 | 32.1 | B |
|  | Subtotal | 296 | 302 | 101.9\% | 2.1 | 297 | 305 | 0.3 | 11.0 | 3.4 | 8.9 | 15.1 | B |
| WB | Left Turn | 31 | 27 | 86.8\% | 5.3 | 17 | 32 | 0.8 | 68.5 | 9.8 | 48.4 | 87.7 | E |
|  | Through | 437 | 438 | 100.3\% | 13.1 | 417 | 456 | 0.1 | 2.6 | 1.5 | 0.5 | 5.1 | A |
|  | Right Turn | 50 | 42 | 84.8\% | 7.4 | 30 | 53 | 1.1 | 2.4 | 1.9 | 0.6 | 6.2 | A |
|  | Subtotal | 518 | 507 | 98.0\% | 16.6 | 486 | 526 | 0.5 | 6.9 | 2.1 | 2.9 | 8.8 | A |
| Total |  | 928 | 922 | 99.4\% | 17.6 | 898 | 942 | 0.2 | 12.7 | 2.5 | 8.3 | 15.7 | B |

## Volume and Delay by Movement

AM Peak Hour

Intersection 2
E St-Richards Blvd/First St
Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) |  |  |  |  |  | Total Delay (sec/veh) |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Average | Percent | Std. Dev. | Minimum | Maximum | GEH | Average | Std. Dev. | Minimum | Maximum | LOS |
| NB | Left Turn | 491 | 482 | 98.1\% | 14.5 | 461 | 501 | 0.4 | 29.6 | 2.9 | 25.5 | 34.1 | C |
|  | Through | 86 | 89 | 102.9\% | 12.6 | 70 | 108 | 0.3 | 29.0 | 6.6 | 11.5 | 35.9 | C |
|  | Right Turn | 229 | 216 | 94.3\% | 16.5 | 184 | 248 | 0.9 | 15.1 | 3.7 | 9.3 | 20.9 | B |
|  | Subtotal | 806 | 786 | 97.5\% | 16.7 | 750 | 811 | 0.7 | 25.6 | 2.9 | 19.2 | 28.0 | C |
| SB | Left Turn | 1 | 1 | 100.0\% | 1.1 | 0 | 3 | 0.0 | 11.9 | 33.2 | 0.0 | 105.7 | B |
|  | Through | 85 | 84 | 99.1\% | 4.3 | 76 | 90 | 0.1 | 44.0 | 9.5 | 26.9 | 55.7 | D |
|  | Right Turn | 10 | 10 | 101.0\% | 2.9 | 6 | 17 | 0.0 | 12.4 | 7.7 | 0.0 | 24.0 | B |
|  | Subtotal | 96 | 95 | 99.3\% | 1.5 | 93 | 98 | 0.1 | 40.2 | 9.3 | 24.8 | 52.9 | D |
| EB | Left Turn | 9 | 9 | 104.4\% | 3.4 | 4 | 14 | 0.1 | 67.7 | 32.5 | 12.2 | 116.1 | E |
|  | Through | 23 | 22 | 93.9\% | 4.8 | 14 | 31 | 0.3 | 75.5 | 29.9 | 41.2 | 139.5 | E |
|  | Right Turn | 282 | 289 | 102.4\% | 9.6 | 277 | 305 | 0.4 | 11.9 | 2.1 | 8.7 | 16.2 | B |
|  | Subtotal | 314 | 320 | 101.8\% | 8.6 | 308 | 332 | 0.3 | 17.2 | 3.3 | 12.1 | 21.2 | B |
| WB | Left Turn | 130 | 129 | 99.4\% | 2.5 | 126 | 134 | 0.1 | 61.7 | 11.3 | 42.4 | 86.5 | E |
|  | Through | 17 | 16 | 94.7\% | 1.9 | 13 | 19 | 0.2 | 42.0 | 12.7 | 23.5 | 60.2 | D |
|  | Right Turn | 3 | 3 | 110.0\% | 1.6 | 1 | 6 | 0.2 | 20.5 | 28.5 | 0.0 | 74.9 | C |
|  | Subtotal | 150 | 149 | 99.1\% | 1.0 | 147 | 150 | 0.1 | 59.0 | 10.7 | 39.2 | 81.3 | E |
| Total |  | 1,366 | 1,350 | 98.8\% | 17.1 | 1,318 | 1,367 | 0.4 | 28.8 | 2.2 | 24.1 | 32.5 | C |

## Volume and Delay by Movement

AM Peak Hour

Intersection 3
Richards Blvd/Olive Dr
Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) |  |  |  |  |  | Total Delay (sec/veh) |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Average | Percent | Std. Dev. | Minimum | Maximum | GEH | Average | Std. Dev. | Minimum | Maximum | LOS |
| NB | Left Turn | 80 | 81 | 100.6\% | 10.3 | 66 | 97 | 0.1 | 138.1 | 44.3 | 81.4 | 242.7 | F |
|  | Through | 612 | 604 | 98.7\% | 17.7 | 571 | 625 | 0.3 | 94.8 | 33.2 | 39.4 | 154.7 | F |
|  | Right Turn | 31 | 30 | 96.8\% | 4.0 | 23 | 34 | 0.2 | 34.0 | 18.1 | 10.5 | 71.0 | C |
|  | Subtotal | 723 | 715 | 98.8\% | 26.3 | 668 | 752 | 0.3 | 97.2 | 30.8 | 43.6 | 150.8 | F |
| SB | Left Turn | 31 | 31 | 100.6\% | 6.6 | 20 | 38 | 0.0 | 38.3 | 19.0 | 11.4 | 74.1 | D |
|  | Through | 440 | 447 | 101.5\% | 9.7 | 426 | 460 | 0.3 | 13.1 | 3.2 | 8.2 | 17.0 | B |
|  | Right Turn | 26 | 24 | 91.2\% | 4.8 | 18 | 32 | 0.5 | 12.7 | 6.9 | 4.4 | 28.4 | B |
|  | Subtotal | 497 | 501 | 100.9\% | 10.9 | 487 | 521 | 0.2 | 14.5 | 3.0 | 10.4 | 18.0 | B |
| EB | Left Turn | 37 | 36 | 96.8\% | 3.0 | 32 | 40 | 0.2 | 42.2 | 15.1 | 18.2 | 68.2 | D |
|  | Through | 7 | 8 | 114.3\% | 2.0 | 5 | 11 | 0.4 | 28.6 | 17.7 | 0.0 | 49.7 | C |
|  | Right Turn | 58 | 58 | 99.7\% | 2.3 | 55 | 62 | 0.0 | 17.6 | 9.5 | 6.9 | 33.8 | B |
|  | Subtotal | 102 | 102 | 99.6\% | 1.6 | 99 | 104 | 0.0 | 28.0 | 10.9 | 13.0 | 44.4 | C |
| WB | Left Turn | 106 | 103 | 97.1\% | 7.1 | 88 | 110 | 0.3 | 86.9 | 33.1 | 42.0 | 134.2 | F |
|  | Through | 18 | 18 | 98.3\% | 4.1 | 13 | 24 | 0.1 | 144.6 | 71.8 | 52.3 | 298.5 | F |
|  | Right Turn | 157 | 148 | 94.3\% | 7.5 | 134 | 157 | 0.7 | 138.9 | 58.3 | 53.4 | 242.6 | F |
|  | Subtotal | 281 | 269 | 95.6\% | 7.5 | 256 | 279 | 0.7 | 118.9 | 47.2 | 48.3 | 195.3 | F |
| Total |  | 1,603 | 1,586 | 99.0\% | 29.6 | 1,528 | 1,617 | 0.4 | 69.2 | 12.6 | 52.6 | 94.9 | E |

## Volume and Delay by Movement

AM Peak Hour

Intersection 4
I-80 WB Ramps/Richards Blvd
Uncontrolled

| Direction |  | Demand | Served Volume (vph) |  |  |  |  |  | Total Delay (sec/veh) |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Movement | Volume (vph) | Average | Percent | Std. Dev. | Minimum | Maximum | GEH | Average | Std. Dev. | Minimum | Maximum | LOS |
| NB | Left Turn | 64 | 62 | 96.4\% | 6.5 | 51 | 75 | 0.3 | 18.4 | 16.9 | 2.7 | 55.2 | C |
|  | Through | 336 | 337 | 100.2\% | 18.1 | 302 | 361 | 0.0 | 38.6 | 21.6 | 8.1 | 76.0 | E |
|  | Right Turn | 359 | 358 | 99.6\% | 11.1 | 337 | 374 | 0.1 | 2.9 | 0.8 | 1.7 | 4.4 | A |
|  | Subtotal | 759 | 756 | 99.6\% | 15.4 | 729 | 775 | 0.1 | 19.0 | 10.6 | 5.2 | 37.9 | C |
| SB | Left Turn |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Through | 422 | 428 | 101.4\% | 15.1 | 403 | 450 | 0.3 | 1.3 | 0.4 | 0.7 | 2.1 | A |
|  | Right Turn | 195 | 190 | 97.3\% | 10.6 | 175 | 210 | 0.4 | 4.4 | 0.7 | 3.1 | 5.2 | A |
|  | Subtotal | 617 | 618 | 100.1\% | 15.0 | 587 | 633 | 0.0 | 2.2 | 0.4 | 1.5 | 2.9 | A |
| EB | Left Turn |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Through |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Right Turn | 179 | 179 | 99.7\% | 1.3 | 177 | 181 | 0.0 | 0.8 | 0.2 | 0.6 | 1.1 | A |
|  | Subtotal | 179 | 179 | 99.7\% | 1.3 | 177 | 181 | 0.0 | 0.8 | 0.2 | 0.6 | 1.1 | A |
| WB | Left Turn |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Through |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Right Turn | 389 | 380 | 97.7\% | 5.9 | 371 | 388 | 0.4 | 51.3 | 38.6 | 8.6 | 126.2 | F |
|  | Subtotal | 389 | 380 | 97.7\% | 5.9 | 371 | 388 | 0.4 | 51.3 | 38.6 | 8.6 | 126.2 | F |
| Total |  | 1,944 | 1,932 | 99.4\% | 24.3 | 1,900 | 1,970 | 0.3 | 18.0 | 10.2 | 4.7 | 39.2 | C |

## Volume and Delay by Movement

AM Peak Hour


## Volume and Delay by Movement

AM Peak Hour

Intersection 6
Research Park Dr/Richards Blvd-Cowell Blvd
Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) |  |  |  |  |  | Total Delay (sec/veh) |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Average | Percent | Std. Dev. | Minimum | Maximum | GEH | Average | Std. Dev. | Minimum | Maximum | LOS |
| NB | Left Turn | 64 | 63 | 98.6\% | 6.6 | 51 | 72 | 0.1 | 53.7 | 11.4 | 39.4 | 75.6 | D |
|  | Through | 6 | 6 | 98.3\% | 2.9 | 2 | 10 | 0.0 | 36.7 | 23.1 | 0.0 | 73.3 | D |
|  | Right Turn | 30 | 31 | 103.0\% | 6.4 | 24 | 44 | 0.2 | 10.9 | 4.2 | 6.8 | 18.0 | B |
|  | Subtotal | 100 | 100 | 99.9\% | 1.7 | 97 | 102 | 0.0 | 42.1 | 7.9 | 32.4 | 56.5 | D |
| SB | Left Turn | 22 | 26 | 116.8\% | 3.9 | 20 | 32 | 0.8 | 57.5 | 14.3 | 37.2 | 75.1 | E |
|  | Through | 19 | 18 | 96.8\% | 3.4 | 14 | 23 | 0.1 | 36.7 | 16.6 | 1.1 | 57.5 | D |
|  | Right Turn | 82 | 79 | 96.3\% | 3.6 | 72 | 84 | 0.3 | 11.1 | 5.7 | 4.3 | 21.8 | B |
|  | Subtotal | 123 | 123 | 100.1\% | 3.2 | 116 | 127 | 0.0 | 26.0 | 7.0 | 15.3 | 36.8 | C |
| EB | Left Turn | 187 | 191 | 102.0\% | 7.0 | 178 | 201 | 0.3 | 49.7 | 6.2 | 38.0 | 57.5 | D |
|  | Through | 469 | 466 | 99.3\% | 19.1 | 427 | 492 | 0.2 | 31.4 | 5.0 | 22.7 | 37.9 | C |
|  | Right Turn | 133 | 135 | 101.2\% | 9.6 | 119 | 148 | 0.1 | 27.2 | 6.1 | 14.8 | 34.3 | C |
|  | Subtotal | 789 | 791 | 100.2\% | 18.8 | 758 | 826 | 0.1 | 35.1 | 4.4 | 27.4 | 42.6 | D |
| WB | Left Turn | 30 | 28 | 91.7\% | 5.7 | 19 | 36 | 0.5 | 76.8 | 17.8 | 53.5 | 107.9 | E |
|  | Through | 487 | 495 | 101.6\% | 8.3 | 478 | 505 | 0.4 | 35.2 | 11.7 | 22.4 | 58.8 | D |
|  | Right Turn | 20 | 21 | 103.5\% | 4.6 | 12 | 27 | 0.2 | 13.8 | 10.9 | 3.2 | 34.9 | B |
|  | Subtotal | 537 | 543 | 101.2\% | 2.7 | 537 | 547 | 0.3 | 36.6 | 11.4 | 24.3 | 59.0 | D |
| Total |  | 1,549 | 1,557 | 100.5\% | 21.0 | 1,519 | 1,593 | 0.2 | 35.3 | 5.9 | 26.5 | 45.5 | D |

## Volume and Delay by Movement

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) |  |  |  |  |  | Total Delay (sec/veh) |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Average | Percent | Std. Dev. | Minimum | Maximum | GEH | Average | Std. Dev. | Minimum | Maximum | LOS |
| NB | Left Turn | 27 | 26 | 96.7\% | 5.4 | 19 | 33 | 0.2 | 20.8 | 6.3 | 11.6 | 30.1 | C |
|  | Through | 41 | 40 | 97.3\% | 5.6 | 33 | 51 | 0.2 | 24.4 | 6.4 | 17.2 | 33.7 | C |
|  | Right Turn | 61 | 63 | 103.3\% | 5.7 | 54 | 73 | 0.3 | 15.2 | 6.9 | 6.2 | 29.7 | B |
|  | Subtotal | 129 | 129 | 100.0\% | 1.9 | 124 | 130 | 0.0 | 19.1 | 5.0 | 10.6 | 30.1 | B |
| SB | Left Turn | 85 | 86 | 100.6\% | 7.2 | 68 | 94 | 0.1 | 43.6 | 18.8 | 23.8 | 88.9 | D |
|  | Through | 29 | 28 | 97.6\% | 5.4 | 21 | 38 | 0.1 | 44.3 | 17.1 | 16.6 | 87.1 | D |
|  | Right Turn | 21 | 21 | 98.1\% | 2.6 | 18 | 25 | 0.1 | 15.7 | 11.7 | 3.3 | 37.1 | B |
|  | Subtotal | 135 | 134 | 99.6\% | 2.4 | 129 | 137 | 0.1 | 40.1 | 17.2 | 18.5 | 84.0 | D |
| EB | Left Turn | 14 | 14 | 100.7\% | 3.8 | 9 | 21 | 0.0 | 91.1 | 35.8 | 45.6 | 172.9 | F |
|  | Through | 374 | 377 | 100.7\% | 14.7 | 356 | 398 | 0.1 | 75.9 | 27.3 | 27.6 | 120.1 | E |
|  | Right Turn | 59 | 59 | 99.8\% | 7.8 | 48 | 70 | 0.0 | 69.7 | 24.1 | 22.2 | 109.2 | E |
|  | Subtotal | 447 | 450 | 100.6\% | 12.9 | 423 | 467 | 0.1 | 75.5 | 26.8 | 27.7 | 117.6 | E |
| WB | Left Turn | 77 | 76 | 98.4\% | 7.6 | 67 | 90 | 0.1 | 38.1 | 8.4 | 24.0 | 52.5 | D |
|  | Through | 308 | 304 | 98.8\% | 18.4 | 270 | 335 | 0.2 | 12.0 | 3.8 | 8.2 | 17.7 | B |
|  | Right Turn | 48 | 51 | 106.0\% | 8.8 | 35 | 65 | 0.4 | 7.9 | 2.7 | 4.8 | 13.4 | A |
|  | Subtotal | 433 | 431 | 99.6\% | 23.6 | 383 | 471 | 0.1 | 16.2 | 5.1 | 11.9 | 24.6 | B |
| Total |  | 1,144 | 1,144 | 100.0\% | 27.0 | 1,111 | 1,201 | 0.0 | 43.3 | 11.9 | 19.4 | 63.5 | D |

## Volume and Delay by Movement

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) |  |  |  |  |  | Total Delay (sec/veh) |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Average | Percent | Std. Dev. | Minimum | Maximum | GEH | Average | Std. Dev. | Minimum | Maximum | LOS |
| NB | Left Turn | 376 | 379 | 100.7\% | 22.9 | 328 | 416 | 0.1 | 29.6 | 4.9 | 23.4 | 37.8 | C |
|  | Through | 108 | 109 | 101.2\% | 7.8 | 96 | 118 | 0.1 | 26.0 | 5.6 | 18.0 | 35.6 | C |
|  | Right Turn | 250 | 241 | 96.2\% | 16.7 | 212 | 258 | 0.6 | 10.4 | 2.3 | 6.6 | 14.4 | B |
|  | Subtotal | 734 | 729 | 99.3\% | 35.7 | 636 | 765 | 0.2 | 22.8 | 4.4 | 17.8 | 30.2 | C |
| SB | Left Turn | 6 | 6 | 106.7\% | 1.4 | 5 | 9 | 0.2 | 58.2 | 37.6 | 0.0 | 106.1 | E |
|  | Through | 166 | 160 | 96.4\% | 6.7 | 146 | 169 | 0.5 | 59.3 | 5.5 | 53.4 | 70.6 | E |
|  | Right Turn | 21 | 22 | 102.9\% | 6.3 | 14 | 35 | 0.1 | 32.6 | 30.1 | 5.4 | 101.6 | C |
|  | Subtotal | 193 | 188 | 97.5\% | 2.0 | 186 | 191 | 0.4 | 56.2 | 5.3 | 49.0 | 66.4 | E |
| EB | Left Turn | 10 | 11 | 106.0\% | 2.9 | 7 | 15 | 0.2 | 91.7 | 44.6 | 0.0 | 179.0 | F |
|  | Through | 53 | 56 | 104.7\% | 8.1 | 42 | 69 | 0.3 | 103.2 | 15.7 | 76.2 | 123.0 | F |
|  | Right Turn | 457 | 464 | 101.6\% | 19.7 | 426 | 490 | 0.3 | 14.1 | 1.7 | 11.9 | 17.3 | B |
|  | Subtotal | 520 | 531 | 102.0\% | 19.8 | 488 | 551 | 0.5 | 26.3 | 4.1 | 17.4 | 31.5 | C |
| WB | Left Turn | 201 | 199 | 98.9\% | 5.5 | 192 | 209 | 0.2 | 121.6 | 35.7 | 72.2 | 195.2 | F |
|  | Through | 36 | 35 | 96.1\% | 5.5 | 25 | 42 | 0.2 | 88.1 | 29.4 | 57.5 | 153.2 | F |
|  | Right Turn | 6 | 6 | 91.7\% | 1.8 | 3 | 8 | 0.2 | 25.3 | 42.9 | 0.0 | 135.6 | C |
|  | Subtotal | 243 | 239 | 98.3\% | 4.5 | 234 | 250 | 0.3 | 115.2 | 34.0 | 71.0 | 188.2 | F |
| Total |  | 1,690 | 1,686 | 99.8\% | 33.8 | 1,614 | 1,731 | 0.1 | 41.0 | 5.1 | 35.5 | 52.8 | D |

Volume and Delay by Movement

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) |  |  |  |  |  | Total Delay (sec/veh) |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Average | Percent | Std. Dev. | Minimum | Maximum | GEH | Average | Std. Dev. | Minimum | Maximum | LOS |
| NB | Left Turn | 46 | 43 | 93.3\% | 5.6 | 37 | 55 | 0.5 | 71.7 | 14.7 | 39.2 | 90.5 | E |
|  | Through | 536 | 530 | 98.9\% | 31.6 | 443 | 552 | 0.3 | 26.5 | 6.8 | 19.1 | 43.3 | C |
|  | Right Turn | 52 | 49 | 93.5\% | 9.2 | 31 | 58 | 0.5 | 8.8 | 3.5 | 4.5 | 14.7 | A |
|  | Subtotal | 634 | 622 | 98.0\% | 30.1 | 543 | 652 | 0.5 | 28.4 | 7.0 | 19.4 | 44.7 | C |
| SB | Left Turn | 92 | 96 | 104.6\% | 9.2 | 75 | 107 | 0.4 | 43.6 | 6.0 | 34.3 | 52.8 | D |
|  | Through | 698 | 692 | 99.1\% | 15.2 | 664 | 719 | 0.2 | 12.9 | 1.7 | 8.1 | 15.2 | B |
|  | Right Turn | 34 | 35 | 101.5\% | 4.0 | 26 | 40 | 0.1 | 12.6 | 4.7 | 4.9 | 18.4 | B |
|  | Subtotal | 824 | 823 | 99.8\% | 17.5 | 788 | 845 | 0.1 | 16.4 | 2.0 | 10.8 | 19.7 | B |
| EB | Left Turn | 32 | 32 | 99.7\% | 5.4 | 20 | 38 | 0.0 | 86.6 | 39.4 | 22.4 | 160.8 | F |
|  | Through | 5 | 4 | 70.0\% | 2.8 | 0 | 8 | 0.7 | 25.3 | 33.6 | 0.0 | 92.5 | C |
|  | Right Turn | 74 | 76 | 102.4\% | 7.0 | 68 | 91 | 0.2 | 49.6 | 22.7 | 13.3 | 94.2 | D |
|  | Subtotal | 111 | 111 | 100.2\% | 1.4 | 108 | 113 | 0.0 | 60.7 | 27.0 | 17.6 | 106.9 | E |
| WB | Left Turn | 142 | 137 | 96.2\% | 7.8 | 119 | 146 | 0.5 | 285.3 | 105.2 | 70.0 | 473.9 | F |
|  | Through | 17 | 18 | 103.5\% | 3.5 | 11 | 22 | 0.1 | 217.3 | 83.0 | 73.9 | 401.4 | F |
|  | Right Turn | 166 | 162 | 97.6\% | 12.2 | 143 | 186 | 0.3 | 195.0 | 77.4 | 45.3 | 367.7 | F |
|  | Subtotal | 325 | 316 | 97.3\% | 7.4 | 303 | 325 | 0.5 | 239.6 | 87.3 | 60.7 | 426.3 | F |
| Total |  | 1,894 | 1,871 | 98.8\% | 27.1 | 1,818 | 1,906 | 0.5 | 64.1 | 17.9 | 28.1 | 103.0 | E |

## Volume and Delay by Movement

PM Peak Hour

Intersection 4
I-80 WB Ramps/Richards Blvd
Uncontrolled

|  |  | Demand | Served Volume (vph) |  |  |  |  |  | Total Delay (sec/veh) |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Direction | Movement | Volume (vph) | Average | Percent | Std. Dev. | Minimum | Maximum | GEH | Average | Std. Dev. | Minimum | Maximum | LOS |
| NB | Left Turn | 29 | 28 | 97.9\% | 3.8 | 22 | 34 | 0.1 | 4.7 | 3.0 | 0.4 | 12.5 | A |
|  | Through | 418 | 410 | 98.1\% | 18.4 | 368 | 429 | 0.4 | 6.9 | 2.0 | 2.4 | 11.0 | A |
|  | Right Turn | 437 | 414 | 94.6\% | 19.4 | 382 | 455 | 1.1 | 2.9 | 0.6 | 1.5 | 4.0 | A |
|  | Subtotal | 884 | 852 | 96.4\% | 27.4 | 803 | 893 | 1.1 | 4.8 | 1.1 | 2.3 | 7.1 | A |
| SB | Left Turn |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Through | 635 | 622 | 98.0\% | 14.8 | 595 | 651 | 0.5 | 2.4 | 0.7 | 1.0 | 4.3 | A |
|  | Right Turn | 321 | 307 | 95.7\% | 15.4 | 283 | 330 | 0.8 | 5.6 | 1.1 | 3.9 | 7.1 | A |
|  | Subtotal | 956 | 929 | 97.2\% | 21.6 | 896 | 973 | 0.9 | 3.5 | 0.8 | 2.1 | 5.2 | A |
| EB | Left Turn |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Through |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Right Turn | 90 | 90 | 99.4\% | 0.8 | 88 | 91 | 0.1 | 0.7 | 0.2 | 0.6 | 1.1 | A |
|  | Subtotal | 90 | 90 | 99.4\% | 0.8 | 88 | 91 | 0.1 | 0.7 | 0.2 | 0.6 | 1.1 | A |
| WB | Left Turn |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Through |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Right Turn | 221 | 218 | 98.6\% | 9.2 | 192 | 223 | 0.2 | 0.8 | 0.2 | 0.6 | 1.2 | A |
|  | Subtotal | 221 | 218 | 98.6\% | 9.2 | 192 | 223 | 0.2 | 0.8 | 0.2 | 0.6 | 1.2 | A |
| Total |  | 2,151 | 2,089 | 97.1\% | 27.9 | 2,057 | 2,145 | 1.3 | 3.7 | 0.6 | 2.5 | 4.8 | A |

## Volume and Delay by Movement



## Volume and Delay by Movement

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) |  |  |  |  |  | Total Delay (sec/veh) |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Average | Percent | Std. Dev. | Minimum | Maximum | GEH | Average | Std. Dev. | Minimum | Maximum | LOS |
| NB | Left Turn | 92 | 92 | 100.0\% | 6.6 | 81 | 99 | 0.0 | 50.8 | 13.1 | 36.4 | 63.3 | D |
|  | Through | 25 | 24 | 94.8\% | 4.6 | 17 | 32 | 0.3 | 39.4 | 16.6 | 13.6 | 57.3 | D |
|  | Right Turn | 40 | 42 | 105.0\% | 5.5 | 36 | 54 | 0.3 | 12.6 | 7.1 | 7.4 | 30.8 | B |
|  | Subtotal | 157 | 158 | 100.4\% | 1.3 | 156 | 161 | 0.1 | 40.5 | 8.5 | 29.0 | 51.9 | D |
| SB | Left Turn | 37 | 36 | 98.4\% | 5.5 | 27 | 45 | 0.1 | 57.9 | 14.2 | 26.6 | 83.2 | E |
|  | Through | 10 | 10 | 104.0\% | 2.8 | 7 | 16 | 0.1 | 44.7 | 36.7 | 0.0 | 123.9 | D |
|  | Right Turn | 126 | 127 | 100.6\% | 4.5 | 122 | 133 | 0.1 | 10.5 | 4.0 | 5.3 | 19.3 | B |
|  | Subtotal | 173 | 174 | 100.3\% | 2.6 | 170 | 179 | 0.0 | 21.9 | 5.7 | 10.1 | 34.5 | C |
| EB | Left Turn | 304 | 287 | 94.5\% | 21.6 | 250 | 317 | 1.0 | 52.3 | 5.6 | 44.5 | 60.7 | D |
|  | Through | 726 | 716 | 98.6\% | 19.0 | 685 | 752 | 0.4 | 16.9 | 6.1 | 7.3 | 27.3 | B |
|  | Right Turn | 58 | 53 | 91.9\% | 5.5 | 43 | 61 | 0.6 | 12.5 | 7.9 | 1.3 | 28.1 | B |
|  | Subtotal | 1,088 | 1,057 | 97.1\% | 16.1 | 1,018 | 1,076 | 1.0 | 27.0 | 5.5 | 20.3 | 35.1 | C |
| WB | Left Turn | 25 | 24 | 96.4\% | 4.7 | 17 | 32 | 0.2 | 66.2 | 19.5 | 49.7 | 100.8 | E |
|  | Through | 530 | 543 | 102.4\% | 13.2 | 525 | 565 | 0.6 | 32.2 | 6.0 | 19.3 | 43.4 | C |
|  | Right Turn | 35 | 35 | 100.3\% | 5.7 | 29 | 44 | 0.0 | 11.5 | 5.9 | 2.8 | 26.8 | B |
|  | Subtotal | 590 | 602 | 102.1\% | 10.2 | 584 | 615 | 0.5 | 32.2 | 5.8 | 20.2 | 43.1 | C |
| Total |  | 2,008 | 1,990 | 99.1\% | 19.8 | 1,946 | 2,021 | 0.4 | 29.1 | 4.4 | 22.5 | 34.3 | C |

Intersection 1
D St/First St
Signal

| Direction | Movement | Storage | Average Queue (ft) |  |  |  | Maximum Queue (ft) |  |  |  | Exceeds Storage? |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | (ft) | Average | Std. Dev. | Minimum | Maximum | Average | Std. Dev. | Minimum | Maximum |  |
| NB | U Turn |  |  |  |  |  |  |  |  |  |  |
|  | Second Left |  |  |  |  |  |  |  |  |  |  |
|  | Left Turn | 100 | 7 | 1 | 5 | 9 | 50 | 10 | 37 | 67 | NO |
|  | Through | 100 | 7 | 1 | 5 | 9 | 50 | 10 | 37 | 67 | NO |
|  | Right Turn | 400 | 1 | 0 | 0 | 1 | 33 | 7 | 23 | 43 | NO |
|  | Second Right |  |  |  |  |  |  |  |  |  |  |
| SB | U Turn |  |  |  |  |  |  |  |  |  |  |
|  | Second Left |  |  |  |  |  |  |  |  |  |  |
|  | Left Turn | 400 | 12 | 1 | 11 | 14 | 70 | 13 | 46 | 94 | NO |
|  | Through | 400 | 12 | 1 | 11 | 14 | 70 | 13 | 46 | 94 | NO |
|  | Right Turn | 400 | 0 | 0 | 0 | 0 | 37 | 15 | 22 | 64 | NO |
|  | Second Right |  |  |  |  |  |  |  |  |  |  |
| EB | U Turn |  |  |  |  |  |  |  |  |  |  |
|  | Second Left |  |  |  |  |  |  |  |  |  |  |
|  | Left Turn | 80 | 1 | 1 | 0 | 2 | 12 | 7 | 0 | 25 | NO |
|  | Through | 560 | 8 | 2 | 7 | 13 | 133 | 27 | 91 | 168 | NO |
|  | Right Turn | 560 | 10 | 2 | 8 | 15 | 142 | 27 | 101 | 178 | NO |
|  | Second Right |  |  |  |  |  |  |  |  |  |  |
| WB | U Turn |  |  |  |  |  |  |  |  |  |  |
|  | Second Left |  |  |  |  |  |  |  |  |  |  |
|  | Left Turn | 100 | 10 | 2 | 6 | 13 | 55 | 13 | 31 | 76 | NO |
|  | Through | 240 | 4 | 3 | 0 | 7 | 109 | 63 | 30 | 239 | NO |
|  | Right Turn | 240 | 4 | 3 | 0 | 7 | 109 | 67 | 16 | 241 | NO |
|  | Second Right |  |  |  |  |  |  |  |  |  |  |

Intersection 2
E St-Richards Blvd/First St
Signal

| Direction | Movement | Storage | Average Queue ( ft ) |  |  |  | Maximum Queue (ft) |  |  |  | Exceeds <br> Storage? |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | (ft) | Average | Std. Dev. | Minimum | Maximum | Average | Std. Dev. | Minimum | Maximum |  |
| NB | U Turn |  |  |  |  |  |  |  |  |  |  |
|  | Second Left |  |  |  |  |  |  |  |  |  |  |
|  | Left Turn | 640 | 303 | 47 | 209 | 364 | 774 | 2 | 773 | 779 | MAX |
|  | Through | 640 | 303 | 47 | 209 | 364 | 774 | 2 | 773 | 779 | MAX |
|  | Right Turn | 180 | 0 | 0 | 0 | 0 | 3 | 4 | 0 | 8 | NO |
|  | Second Right |  |  |  |  |  |  |  |  |  |  |
| SB | U Turn |  |  |  |  |  |  |  |  |  |  |
|  | Second Left |  |  |  |  |  |  |  |  |  |  |
|  | Left Turn |  |  |  |  |  |  |  |  |  |  |
|  | Through | 400 | 22 | 4 | 18 | 29 | 114 | 19 | 89 | 148 | NO |
|  | Right Turn | 400 | 0 | 0 | 0 | 1 | 23 | 8 | 14 | 43 | NO |
|  | Second Right |  |  |  |  |  |  |  |  |  |  |
| EB | U Turn |  |  |  |  |  |  |  |  |  |  |
|  | Second Left |  |  |  |  |  |  |  |  |  |  |
|  | Left Turn | 100 | 13 | 2 | 10 | 16 | 68 | 19 | 39 | 101 | NO |
|  | Through | 220 | 13 | 2 | 10 | 16 | 68 | 19 | 39 | 101 | NO |
|  | Right Turn | 200 | 22 | 1 | 20 | 24 | 195 | 24 | 166 | 242 | NO |
|  | Second Right |  |  |  |  |  |  |  |  |  |  |
| WB | U Turn |  |  |  |  |  |  |  |  |  |  |
|  | Second Left |  |  |  |  |  |  |  |  |  |  |
|  | Left Turn | 220 | 44 | 6 | 36 | 55 | 165 | 21 | 135 | 197 | NO |
|  | Through | 240 | 44 | 6 | 36 | 55 | 165 | 21 | 135 | 197 | NO |
|  | Right Turn | 240 | 44 | 6 | 36 | 55 | 165 | 21 | 135 | 197 | NO |
|  | Second Right |  |  |  |  |  |  |  |  |  |  |

Intersection 3
Richards Blvd/Olive Dr
Signal

| Direction | Movement | Storage <br> (ft) | Average Queue ( ft ) |  |  |  | Maximum Queue (ft) |  |  |  | Exceeds Storage? |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Average | Std. Dev. | Minimum | Maximum | Average | Std. Dev. | Minimum | Maximum |  |
| NB | U Turn |  |  |  |  |  |  |  |  |  |  |
|  | Second Left |  |  |  |  |  |  |  |  |  |  |
|  | Left Turn | 100 | 75 | 39 | 35 | 169 | 310 | 117 | 115 | 548 | MAX |
|  | Through | 1,540 | 152 | 63 | 78 | 263 | 603 | 100 | 489 | 801 | NO |
|  | Right Turn | 160 | 0 | 0 | 0 | 0 | 6 | 4 | 0 | 13 | NO |
|  | Second Right |  |  |  |  |  |  |  |  |  |  |
| SB | U Turn |  |  |  |  |  |  |  |  |  |  |
|  | Second Left |  |  |  |  |  |  |  |  |  |  |
|  | Left Turn | 640 | 6 | 2 | 3 | 9 | 51 | 14 | 30 | 82 | NO |
|  | Through | 640 | 41 | 13 | 20 | 59 | 395 | 98 | 247 | 557 | NO |
|  | Right Turn | 640 | 39 | 13 | 18 | 57 | 393 | 98 | 245 | 555 | NO |
|  | Second Right |  |  |  |  |  |  |  |  |  |  |
| EB | U Turn |  |  |  |  |  |  |  |  |  |  |
|  | Second Left |  |  |  |  |  |  |  |  |  |  |
|  | Left Turn | 600 | 14 | 4 | 9 | 22 | 101 | 24 | 72 | 142 | NO |
|  | Through | 600 | 14 | 4 | 9 | 22 | 101 | 24 | 72 | 142 | NO |
|  | Right Turn | 600 | 13 | 4 | 7 | 21 | 104 | 24 | 77 | 144 | NO |
|  | Second Right |  |  |  |  |  |  |  |  |  |  |
| WB | U Turn |  |  |  |  |  |  |  |  |  |  |
|  | Second Left |  |  |  |  |  |  |  |  |  |  |
|  | Left Turn | 200 | 32 | 12 | 23 | 63 | 159 | 55 | 120 | 279 | NO |
|  | Through | 4,000 | 133 | 39 | 64 | 197 | 453 | 86 | 295 | 586 | NO |
|  | Right Turn | 4,000 | 136 | 38 | 67 | 200 | 456 | 86 | 298 | 589 | NO |
|  | Second Right |  |  |  |  |  |  |  |  |  |  |

Average Results from 10 Runs
Queue Length

Intersection 4 I-80 WB Ramps/Richards Blvd
Uncontrolled


Intersection 5
Richards Blvd/I-80 EB Ramps
Signal

| Direction | Movement | Storage <br> (ft) | Average Queue (ft) |  |  |  | Maximum Queue (ft) |  |  |  | Exceeds <br> Storage? |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| NB | U Turn Second Left Left Turn Through Right Turn Second Right | $\begin{aligned} & 500 \\ & 500 \end{aligned}$ | $\begin{aligned} & 55 \\ & 42 \end{aligned}$ | $\begin{aligned} & 4 \\ & 4 \end{aligned}$ | $\begin{aligned} & 51 \\ & 38 \end{aligned}$ | $\begin{aligned} & 63 \\ & 50 \end{aligned}$ | $\begin{aligned} & 308 \\ & 280 \end{aligned}$ | $\begin{aligned} & 29 \\ & 29 \end{aligned}$ | $\begin{aligned} & 269 \\ & 241 \end{aligned}$ | $\begin{aligned} & 364 \\ & 336 \end{aligned}$ | $\begin{aligned} & \text { NO } \\ & \text { NO } \end{aligned}$ |
| SB | U Turn Second Left Left Turn Through Right Turn Second Right | $\begin{gathered} 360 \\ 1,300 \end{gathered}$ | $\begin{aligned} & 48 \\ & 12 \end{aligned}$ | $\begin{aligned} & 3 \\ & 1 \end{aligned}$ | $\begin{aligned} & 44 \\ & 10 \end{aligned}$ | $\begin{aligned} & 52 \\ & 14 \end{aligned}$ | $\begin{aligned} & 159 \\ & 121 \end{aligned}$ | $\begin{aligned} & 18 \\ & 13 \end{aligned}$ | $\begin{aligned} & 130 \\ & 100 \end{aligned}$ | $\begin{aligned} & 187 \\ & 137 \end{aligned}$ | $\begin{aligned} & \text { NO } \\ & \text { NO } \end{aligned}$ |
| EB | U Turn Second Left Left Turn <br> Through <br> Right Turn <br> Second Right |  |  |  |  |  |  |  |  |  |  |
| WB | U Turn Second Left Left Turn Through Right Turn Second Right | $\begin{gathered} 160 \\ 1,260 \end{gathered}$ | $\begin{gathered} 174 \\ 8 \end{gathered}$ | $25$ <br> 1 | $131$ <br> 7 | 214 <br> 10 | $\begin{aligned} & 636 \\ & 96 \end{aligned}$ | $\begin{aligned} & 78 \\ & 17 \end{aligned}$ | $\begin{aligned} & 550 \\ & 66 \end{aligned}$ | $\begin{aligned} & 818 \\ & 121 \end{aligned}$ | $\begin{aligned} & \text { AVG } \\ & \text { NO } \end{aligned}$ |

Research Park Dr/Richards Blvd-Cowell Blvd
Signal


Intersection 1 D St/First St Signal

| Direction | Movement | Storage | Average Queue (ft) |  |  |  | Maximum Queue (ft) |  |  |  | Exceeds Storage? |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | (ft) | Average | Std. Dev. | Minimum | Maximum | Average | Std. Dev. | Minimum | Maximum |  |
| NB | U Turn |  |  |  |  |  |  |  |  |  |  |
|  | Second Left |  |  |  |  |  |  |  |  |  |  |
|  | Left Turn | 100 | 8 | 1 | 6 | 11 | 71 | 9 | 59 | 89 | NO |
|  | Through | 100 | 8 | 1 | 6 | 11 | 71 | 9 | 59 | 89 | NO |
|  | Right Turn | 400 | 2 | 1 | 1 | 4 | 41 | 7 | 31 | 53 | NO |
|  | Second Right |  |  |  |  |  |  |  |  |  |  |
| SB | U Turn |  |  |  |  |  |  |  |  |  |  |
|  | Second Left |  |  |  |  |  |  |  |  |  |  |
|  | Left Turn | 400 | 23 | 6 | 18 | 34 | 134 | 39 | 89 | 233 | NO |
|  | Through | 400 | 23 | 6 | 18 | 34 | 134 | 39 | 89 | 233 | NO |
|  | Right Turn | 400 | 4 | 3 | 0 | 11 | 105 | 48 | 61 | 236 | NO |
|  | Second Right |  |  |  |  |  |  |  |  |  |  |
| EB | U Turn |  |  |  |  |  |  |  |  |  |  |
|  | Second Left |  |  |  |  |  |  |  |  |  |  |
|  | Left Turn | 80 | 8 | 13 | 2 | 43 | 65 | 66 | 24 | 231 | NO |
|  | Through | 560 | 158 | 44 | 61 | 210 | 457 | 95 | 306 | 638 | NO |
|  | Right Turn | 560 | 164 | 45 | 65 | 217 | 466 | 95 | 316 | 647 | NO |
|  | Second Right |  |  |  |  |  |  |  |  |  |  |
| WB | U Turn |  |  |  |  |  |  |  |  |  |  |
|  | Second Left |  |  |  |  |  |  |  |  |  |  |
|  | Left Turn | 100 | 15 | 3 | 9 | 20 | 96 | 22 | 72 | 148 | NO |
|  | Through | 240 | 18 | 5 | 11 | 26 | 259 | 54 | 141 | 322 | MAX |
|  | Right Turn | 240 | 17 | 5 | 10 | 25 | 262 | 54 | 143 | 324 | MAX |
|  | Second Right |  |  |  |  |  |  |  |  |  |  |

E St-Richards Blvd/First St
Signa

| Direction | Movement | Storage <br> (ft) | Average Queue (ft) |  |  |  | Maximum Queue (ft) |  |  |  | Exceeds Storage? |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Average | Std. Dev. | Minimum | Maximum | Average | Std. Dev. | Minimum | Maximum |  |
| NB | U Turn |  |  |  |  |  |  |  |  |  |  |
|  | Second Left |  |  |  |  |  |  |  |  |  |  |
|  | Left Turn | 640 | 119 | 15 | 106 | 148 | 635 | 52 | 548 | 728 | NO |
|  | Through | 640 | 119 | 15 | 106 | 148 | 635 | 52 | 548 | 728 | NO |
|  | Right Turn | 180 | 0 | 0 | 0 | 1 | 32 | 11 | 22 | 51 | NO |
|  | Second Right |  |  |  |  |  |  |  |  |  |  |
| SB | U Turn |  |  |  |  |  |  |  |  |  |  |
|  | Second Left |  |  |  |  |  |  |  |  |  |  |
|  | Left Turn |  |  |  |  |  |  |  |  |  |  |
|  | Through | 400 | 57 | 6 | 47 | 66 | 237 | 21 | 204 | 275 | NO |
|  | Right Turn | 400 | 1 | 0 | 0 | 1 | 26 | 5 | 18 | 37 | NO |
|  | Second Right |  |  |  |  |  |  |  |  |  |  |
| EB | U Turn |  |  |  |  |  |  |  |  |  |  |
|  | Second Left |  |  |  |  |  |  |  |  |  |  |
|  | Left Turn | 100 | 51 | 11 | 36 | 68 | 232 | 47 | 140 | 291 | MAX |
|  | Through | 220 | 51 | 11 | 36 | 68 | 232 | 47 | 140 | 291 | MAX |
|  | Right Turn | 200 | 47 | 3 | 44 | 52 | 284 | 12 | 269 | 306 | MAX |
|  | Second Right |  |  |  |  |  |  |  |  |  |  |
| WB | U Turn |  |  |  |  |  |  |  |  |  |  |
|  | Second Left |  |  |  |  |  |  |  |  |  |  |
|  | Left Turn | 220 | 152 | 43 | 91 | 239 | 361 | 57 | 258 | 438 | MAX |
|  | Through | 240 | 152 | 43 | 91 | 239 | 361 | 57 | 258 | 438 | MAX |
|  | Right Turn | 240 | 152 | 43 | 91 | 239 | 361 | 57 | 258 | 438 | MAX |
|  | Second Right |  |  |  |  |  |  |  |  |  |  |

Intersection 3
Richards Blvd/Olive Dr
Signal


Average Results from 10 Runs
Queue Length

Intersection 4 I-80 WB Ramps/Richards Blvd
Uncontrolled


Intersection 5
Richards Blvd/I-80 EB Ramps
Signal

| Direction | Movement | Storage <br> (ft) | Average Queue (ft) |  |  |  | Maximum Queue (ft) |  |  |  | Exceeds Storage? |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| NB | U Turn Second Left Left Turn Through Right Turn Second Right | $\begin{aligned} & 500 \\ & 500 \end{aligned}$ | $\begin{aligned} & 35 \\ & 24 \end{aligned}$ | $\begin{aligned} & 3 \\ & 3 \end{aligned}$ | $\begin{aligned} & 31 \\ & 21 \end{aligned}$ | $\begin{aligned} & 41 \\ & 30 \end{aligned}$ | $\begin{aligned} & 266 \\ & 238 \end{aligned}$ | $\begin{aligned} & 29 \\ & 29 \end{aligned}$ | $\begin{aligned} & 215 \\ & 187 \end{aligned}$ | $\begin{aligned} & 326 \\ & 298 \end{aligned}$ | $\begin{aligned} & \text { NO } \\ & \text { NO } \end{aligned}$ |
| SB | U Turn Second Left Left Turn Through Right Turn Second Right | $\begin{gathered} 360 \\ 1,300 \end{gathered}$ | $\begin{aligned} & 44 \\ & 13 \end{aligned}$ | $\begin{aligned} & 3 \\ & 2 \end{aligned}$ | $\begin{aligned} & 38 \\ & 11 \end{aligned}$ | $\begin{aligned} & 48 \\ & 16 \end{aligned}$ | $\begin{aligned} & 124 \\ & 155 \end{aligned}$ | $\begin{gathered} 8 \\ 33 \end{gathered}$ | $\begin{aligned} & 113 \\ & 113 \end{aligned}$ | $\begin{aligned} & 136 \\ & 203 \end{aligned}$ | $\begin{aligned} & \text { NO } \\ & \text { NO } \end{aligned}$ |
| EB | U Turn Second Left Left Turn <br> Through <br> Right Turn <br> Second Right |  |  |  |  |  |  |  |  |  |  |
| WB | U Turn Second Left Left Turn Through Right Turn Second Right | $\begin{gathered} 160 \\ 1,260 \end{gathered}$ | $\begin{gathered} 607 \\ 10 \end{gathered}$ | $\begin{gathered} 151 \\ 5 \end{gathered}$ | $\begin{gathered} 418 \\ 6 \end{gathered}$ | $944$ | $\begin{gathered} 1,134 \\ 126 \end{gathered}$ | $\begin{aligned} & 118 \\ & 88 \end{aligned}$ | $\begin{aligned} & 929 \\ & 76 \end{aligned}$ | $\begin{gathered} 1,291 \\ 371 \end{gathered}$ | $\begin{aligned} & \text { AVG } \\ & \text { NO } \end{aligned}$ |

Research Park Dr/Richards Blvd-Cowell Blvd
Signal

| Direction | Movement | Storage <br> (ft) | Average Queue (ft) |  |  |  | Maximum Queue (ft) |  |  |  | Exceeds Storage? |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Average | Std. Dev. | Minimum | Maximum | Average | Std. Dev. | Minimum | Maximum |  |
| NB | U Turn | $\begin{aligned} & 100 \\ & 620 \end{aligned}$ | 227 | 32 | $\begin{gathered} 17 \\ 4 \end{gathered}$ | $\begin{aligned} & 26 \\ & 10 \end{aligned}$ | $\begin{aligned} & 88 \\ & 71 \end{aligned}$ | $\begin{aligned} & 21 \\ & 13 \end{aligned}$ | $\begin{aligned} & 66 \\ & 52 \end{aligned}$ | $\begin{gathered} 129 \\ 89 \end{gathered}$ | $\begin{aligned} & \text { NO } \\ & \text { NO } \end{aligned}$ |
|  | Second Left |  |  |  |  |  |  |  |  |  |  |
|  | Left Turn |  |  |  |  |  |  |  |  |  |  |
|  | Through |  |  |  |  |  |  |  |  |  |  |
|  | Right Turn |  |  |  |  |  |  |  |  |  |  |
|  | Second Right |  |  |  |  |  |  |  |  |  |  |
| SB | U Turn | 1203,940 | 116 | 32 | 63 | $\begin{gathered} 14 \\ 9 \end{gathered}$ | $\begin{aligned} & 66 \\ & 87 \end{aligned}$ | $\begin{aligned} & 16 \\ & 21 \end{aligned}$ | $\begin{aligned} & 45 \\ & 61 \end{aligned}$ | $\begin{gathered} 85 \\ 121 \end{gathered}$ | $\begin{aligned} & \text { NO } \\ & \text { NO } \end{aligned}$ |
|  | Second Left |  |  |  |  |  |  |  |  |  |  |
|  | Left Turn |  |  |  |  |  |  |  |  |  |  |
|  | Through |  |  |  |  |  |  |  |  |  |  |
|  | Right Turn |  |  |  |  |  |  |  |  |  |  |
|  | Second Right |  |  |  |  |  |  |  |  |  |  |
| EB | U Turn | 440 | 121 | 11 | 100 | 137 | 485 | 70 | 392 | 564 | MAX |
|  | Second Left |  |  |  |  |  |  |  |  |  |  |
|  | Left Turn | 440 | 121 | 11 | 100 | 137 | 485 | 70 | 392 | 564 | MAX |
|  | Through | 440 | 121 | 11 | 100 | 137 | 485 | 70 | 392 | 564 | MAX |
|  | Right Turn |  |  |  |  |  |  |  |  |  |  |
|  | Second Right |  |  |  |  |  |  |  |  |  |  |
| WB | U Turn |  |  |  |  |  |  |  |  |  |  |
|  | Second Left |  |  |  |  |  |  |  |  |  |  |
|  | Left Turn | 80 | 7 | 2 | 4 | 12 | 187 | 36 | 127 | 228 | MAX |
|  | Through | 180 | 7 | 2 | 4 | 12 | 187 | 36 | 127 | 228 | MAX |
|  | Right Turn |  |  |  |  |  |  |  |  |  |  |
|  | Second Right |  |  |  |  |  |  |  |  |  |  |


|  | Freeway Basic Report |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Eastbound I-80 |
| Segment | West of Old Davis Rd |
| Alternative | Existing Conditions |
| Time Period | AM Peak Hour |


|  |  |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
|  | General | Purpose Lanes - Geometric Data |  |  |  |  |
| General Purpose Lanes, N | 5 | ln | Terrain Type | Level |  |  |
| Segment Length, L | 1,500 | ft | Percent Grade | - |  |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |  |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 1.67 | $\mathrm{ramps} / \mathrm{mi}$ |  |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 70.5 | mph |  |


| General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


|  | General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | ---: | :---: |
| Volume, V | 4,372 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |  |
| Peak Hour Factor, PHF | 0.95 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,003 | pcphpl |  |
| Total Trucks | $9.0 \%$ |  | Capacity, c | 2,400 | pcphpl |  |
| Single Unit/Tractor-Trailer Mix | - | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |  |  |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.42 |  |  |


| General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS ${ }_{\text {adj }}$ | 70.5 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 70.5 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 14.2 | pcpmpl |
| Total Ramp Density Adjustment | 4.9 | mph | Level of Service, LOS | B |  |

$\qquad$


| Entering General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :--- | :---: | :--- | :--- | :--- | :--- |
| Volume, V | 4,372 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.95 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,003 | pcphpl |
| Total Trucks | $9.0 \%$ |  | Capacity, c | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |  |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.42 |  |


| Entering General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 70.5 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 70.5 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 14.2 | pcpmpl |
| Total Ramp Density Adjustment | 4.9 | mph | Level of Service, LOS | B |  |


| Segment General Purpose Lanes - Capacity, Speed, and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| General Purpose Lanes, N | 6 | $\ln$ | Average Speed, S | 70.5 | mph |
| Adjusted Capacity, cadj | 2,400 | pcphpl | Density, D | 12.0 | pcphpl |
| Flow Rate, vp | 844 | pcphpl | Level of Service, LOS | B |  |
| Volume-to-Capacity Ratio, v/c | 0.35 |  |  |  |  |

## Freeway Merge Report



## Freeway Merge Report



| Ramp Influence Area Density and Level of Service |  |  |
| :--- | :--- | :---: |
|  | pcpmpl |  |
| Density in Ramp Influence Area, $D_{R}$ |  |  |

## Segment Speed, Flow, and Density

Speed Adjustment Factor, SAF
Speed Index, $\mathrm{M}_{\mathrm{S}}$ or $\mathrm{D}_{\mathrm{S}}$
Average Speed in Ramp Influence Area, $\mathrm{S}_{\mathrm{R}} \mathrm{mph}$

Average Flow in Outer Lanes, $\mathrm{v}_{\mathrm{OA}}$
pcphpl
mph
Average Speed in Outer Lanes, $\mathrm{S}_{0}$
mph
Density across All Lanes, D
pcpmpl

|  | Freeway Basic Report |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Eastbound I-80 |
| Segment | Old Davis Rd to Lane Drop 1 |
| Alternative | Existing Conditions |
| Time Period | AM Peak Hour |


|  | General |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
|  | Purpose Lanes - Geometric Data |  |  |  |  |  |
| General Purpose Lanes, N | 5 | ln | Terrain Type | Level |  |  |
| Segment Length, L | 820 | ft | Percent Grade | - |  |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |  |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 1.67 | $\mathrm{ramps} / \mathrm{mi}$ |  |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 70.5 | mph |  |


| General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


|  | General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | ---: | :---: |
| Volume, V | 4,415 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |  |
| Peak Hour Factor, PHF | 0.95 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,013 | pcphpl |  |
| Total Trucks | $9.0 \%$ |  | Capacity, c | 2,400 | pcphpl |  |
| Single Unit/Tractor-Trailer Mix | - | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |  |  |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.42 |  |  |


| General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS ${ }_{\text {adj }}$ | 70.5 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 70.5 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 14.4 | pcpmpl |
| Total Ramp Density Adjustment | 4.9 | mph | Level of Service, LOS | B |  |

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|  | Freeway Basic Report |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Eastbound I-80 |
| Segment | Lane Drop 1 to Lane Drop 2 |
| Alternative | Existing Conditions |
| Time Period | AM Peak Hour |


|  | General |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
|  | Purpose Lanes - Geometric Data |  |  |  |  |  |
| General Purpose Lanes, N | 4 | ln | Terrain Type | Level |  |  |
| Segment Length, L | 1,480 | ft | Percent Grade | - |  |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |  |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 1.50 | $\mathrm{ramps} / \mathrm{mi}$ |  |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 70.9 | mph |  |


| General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


| General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Volume, V | 4,415 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.95 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,266 | pcphpl |
| Total Trucks | 9.0\% |  | Capacity, c | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - |  | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.53 |  |


| General Purpose Lanes - Speed and Density |  |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 70.9 | mph |  |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 70.8 | mph |  |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 17.9 | pcpmpl |  |
| Total Ramp Density Adjustment | 4.5 | mph | Level of Service, LOS | B |  |  |

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## Freeway Diverge Report

| Freeway Diverge Report |  |  |  |
| :---: | :---: | :---: | :---: |
| Project I-80/Richards B <br> Freeway Eastbound I-80 <br> Segment Richards Blvd O <br> Alternative Existing Conditi <br> Time Period AM Peak Hour |  |  |  |
| Geometric Data |  |  |  |
|  | Freeway | Off Ramp |  |
| Number of Lanes, N | 3 | 1 |  |
| Free-Flow Speed, FFS | 70.9 | 25 | mph |
| Segment Length, L / Deceleration Length, LD | 1,240 | 150 | ft |
| Terrain Type | Level | Level |  |
| Percent Grade | - | - |  |
| Grade Length | - | - | ft |
| Segment Type / Ramp Type | Freeway | Right |  |
| Adjustment Factors |  |  |  |
|  | Freeway | Off Ramp |  |
| Driver Population | Familiar | Familiar |  |
| Weather Type | Non-severe | Non-severe |  |
| Incident Type | No incident | No incident |  |
| Capacity Adjustment Factor, CAF | 1.00 | 1.00 |  |
| Demand Adjustment Factor, DAF | 1.00 | 1.00 |  |
| Volume Data |  |  |  |
| Junction Components | Freeway | Off Ramp |  |
| Volume, V | 4,415 | 483 | vph |
| Peak Hour Factor, PHF | 0.95 | 0.88 |  |
| Total Trucks | 9.0\% | 3.3\% |  |
| Single Unit/Tractor-Trailer Mix | - | - |  |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 | 2.0 |  |
| Heavy Vehicle Adjustment, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 | 0.968 |  |
| Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 5,066 | 567 | pcph |

## Adjacent Ramp Data

Adjacent Ramp Meeting Criteria
Upstream Downstream

Type of Adjacent Ramp
Distance to Adjacent Ramp
Volume on Adjacent Ramp

| No | Yes |  |
| :---: | :---: | :---: |
|  | On |  |
|  | 2,740 | ft |
|  | 348 | pcph |

## Freeway Diverge Report

| Freeway Diverge Report |  |  |
| :---: | :---: | :---: |
| Project I-80/Richards Blvd Interchange <br> Freeway Eastbound I-80 <br> Segment Richards Blvd Off Ramp <br> Alternative Existing Conditions <br> Time Period AM Peak Hour |  |  |
| Estimation of Volume in Ramp Influence Area |  |  |
| Adjacent Upstream On-ramp Equilibrium Distance, $\mathrm{L}_{\mathrm{EQ}}$ <br> Adjacent Downstream On-ramp Equilibrium Distance, $\mathrm{L}_{\mathrm{EQ}}$ <br> Proportion of Freeway Vehicles in Lanes 1 and 2, $\mathrm{P}_{\mathrm{FM}}$ or $\mathrm{P}_{\mathrm{FD}}$ <br> Flow Rate in Lanes 1 and 2, $\mathrm{v}_{12}$ | $\begin{gathered} 447 \\ 0.607 \\ 3,299 \end{gathered}$ | ft <br> ft pcph |
| Capacity Checks |  |  |
|  Flow  Capacity <br> Entering General Purpose Lanes 5,066  7,200 <br> Exiting General Purpose Lanes 4,499 7,200  | pcph <br> pcph | $\begin{gathered} \text { V/C Ratio } \\ \hline 0.70 \\ 0.62 \end{gathered}$ |
| Off Ramp 567 1,900 <br> Ramp Influence Area 3,299 4,400 | pcph pcph | $\begin{aligned} & 0.30 \\ & 0.75 \end{aligned}$ |
| Ramp Influence Area Density and Level of Service |  |  |
| Density in Ramp Influence Area, $D_{R}$ Level of Service, LOS | $\begin{gathered} 31.3 \\ D \end{gathered}$ | pcpmpl |
| Segment Speed, Flow, and Density |  |  |
| Speed Adjustment Factor, SAF <br> Speed Index, $\mathrm{M}_{\mathrm{S}}$ or $\mathrm{D}_{\mathrm{S}}$ <br> Average Speed in Ramp Influence Area, $\mathrm{S}_{\mathrm{R}}$ <br> Average Flow in Outer Lanes, $\mathrm{v}_{\mathrm{OA}}$ <br> Average Speed in Outer Lanes, $\mathrm{S}_{\mathrm{O}}$ <br> Average Speed for Segment, S <br> Density across All Lanes, D | $\begin{gathered} 1.00 \\ 0.609 \\ 53.3 \\ 1,767 \\ 74.8 \\ 59.2 \\ 28.8 \end{gathered}$ | mph <br> pcphpl <br> mph <br> mph <br> pcpmpl |


|  | Freeway Basic Report |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Eastbound I-80 |
| Segment | Richards Blvd Off to On |
| Alternative | Existing Conditions |
| Time Period | AM Peak Hour |


|  | General |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
|  | Purpose Lanes - Geometric Data |  |  |  |  |  |
| General Purpose Lanes, N | 3 | ln | Terrain Type | Level |  |  |
| Segment Length, L | 1,500 | ft | Percent Grade | - |  |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |  |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 1.67 | $\mathrm{ramps} / \mathrm{mi}$ |  |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 70.5 | mph |  |


| General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


| General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | ---: |
| Volume, V | 3,932 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.95 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,504 | pcphpl |
| Total Trucks | $9.0 \%$ |  | Capacity, c | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |  |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.63 |  |


| General Purpose Lanes - Speed and Density |  |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 70.5 | mph |  |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 69.3 | mph |  |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 21.7 | pcpmpl |  |
| Total Ramp Density Adjustment | 4.9 | mph | Level of Service, LOS | C |  |  |

$\qquad$

| Freeway Merge Report |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Project I-80/Richards B <br> Freeway Eastbound I-80 <br> Segment Richards Blvd O <br> Alternative Existing Condit <br> Time Period AM Peak Hour |  |  |  |  |
| Geometric Data |  |  |  |  |
|  | Freeway | On Ramp |  |  |
| Number of Lanes, N | 3 | 1 |  |  |
| Free-Flow Speed, FFS | 70.5 | 45 |  | mph |
| Segment Length, L / Acceleration Length, LA | 1,500 | 500 |  | ft |
| Terrain Type | Level | Level |  |  |
| Percent Grade | - | - |  |  |
| Grade Length | - |  |  | ft |
| Segment Type / Ramp Type | Freeway | Right |  |  |
| Adjustment Factors |  |  |  |  |
|  | Freeway | On Ramp |  |  |
| Driver Population | Familiar | Familiar |  |  |
| Weather Type | Non-severe | Non-severe |  |  |
| Incident Type | No incident | No incident |  |  |
| Capacity Adjustment Factor, CAF | 1.00 | 1.00 |  |  |
| Demand Adjustment Factor, DAF | 1.00 | 1.00 |  |  |
| Volume Data |  |  |  |  |
| Junction Components | Freeway | On Ramp |  |  |
| Volume, V | 3,932 | 300 |  | vph |
| Peak Hour Factor, PHF | 0.95 | 0.88 |  |  |
| Total Trucks | 9.0\% | 1.7\% |  |  |
| Single Unit/Tractor-Trailer Mix | - | - |  |  |
| Passenger Car Equivalent, $\mathrm{E}_{T}$ | 2.0 | 2.0 |  |  |
| Heavy Vehicle Adjustment, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 | 0.983 |  |  |
| Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 4,511 | 347 |  | pcph |
| Adjacent Ramp Data |  |  |  |  |
|  |  | Upstream | Downstream |  |
| Adjacent Ramp Meeting Criteria |  | Yes | No |  |
| Type of Adjacent Ramp |  | Off |  |  |
| Distance to Adjacent Ramp |  | 2,740 |  | ft |
| Volume on Adjacent Ramp |  | 567 |  | pcph |



|  | Freeway Basic Report |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Eastbound I-80 |
| Segment | Richards Blvd to Chiles Rd |
| Alternative | Existing Conditions |
| Time Period | AM Peak Hour |


|  | General |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
|  | Purpose Lanes - Geometric Data |  |  |  |  |  |
| General Purpose Lanes, N | 3 | ln | Terrain Type | Level |  |  |
| Segment Length, L | 5,710 | ft | Percent Grade | - |  |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |  |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 1.50 | $\mathrm{ramps} / \mathrm{mi}$ |  |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 70.9 | mph |  |


| General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


| General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Volume, V | 4,232 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.95 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,619 | pcphpl |
| Total Trucks | 9.0\% |  | Capacity, c | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - |  | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.67 |  |


| General Purpose Lanes - Speed and Density |  |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 70.9 | mph |  |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 68.5 | mph |  |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 23.6 | pcpmpl |  |
| Total Ramp Density Adjustment | 4.5 | mph | Level of Service, LOS | C |  |  |

$\qquad$

## Freeway Diverge Report

| Freeway Diverge Report |  |  |  |
| :---: | :---: | :---: | :---: |
| Project I-80/Richards B <br> Freeway Eastbound I-80 <br> Segment Chiles Rd Off Ra <br> Alternative Existing Conditi <br> Time Period AM Peak Hour |  |  |  |
| Geometric Data |  |  |  |
|  | Freeway | Off Ramp |  |
| Number of Lanes, N | 3 | 2 |  |
| Free-Flow Speed, FFS | 70.9 | 25 | mph |
| Segment Length, L / Deceleration Length, LD | 1,500 | 1,500 | ft |
| Terrain Type | Level | Level |  |
| Percent Grade | - | - |  |
| Grade Length | - | - | ft |
| Segment Type / Ramp Type | Freeway | Right |  |
| Adjustment Factors |  |  |  |
|  | Freeway | Off Ramp |  |
| Driver Population | Familiar | Familiar |  |
| Weather Type | Non-severe | Non-severe |  |
| Incident Type | No incident | No incident |  |
| Capacity Adjustment Factor, CAF | 1.00 | 1.00 |  |
| Demand Adjustment Factor, DAF | 1.00 | 1.00 |  |
| Volume Data |  |  |  |
| Junction Components | Freeway | Off Ramp |  |
| Volume, V | 4,232 | 299 | vph |
| Peak Hour Factor, PHF | 0.95 | 0.78 |  |
| Total Trucks | 9.0\% | 3.0\% |  |
| Single Unit/Tractor-Trailer Mix | - | - |  |
| Passenger Car Equivalent, $\mathrm{E}_{T}$ | 2.0 | 2.0 |  |
| Heavy Vehicle Adjustment, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 | 0.971 |  |
| Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 4,856 | 395 | pcph |

## Adjacent Ramp Data

Adjacent Ramp Meeting Criteria
Upstream Downstream

Type of Adjacent Ramp
Distance to Adjacent Ramp ft
Volume on Adjacent Ramp pcph

## Freeway Diverge Report



|  | Freeway Basic Repor |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Eastbound I-80 |
| Segment | Chiles Rd Off to Mace Rd On |
| Alternative | Existing Conditions |
| Time Period | AM Peak Hour |


|  | General |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
|  | Purpose Lanes - Geometric Data |  |  |  |  |  |
| General Purpose Lanes, N | 3 | ln | Terrain Type | Level |  |  |
| Segment Length, L | 1,000 | ft | Percent Grade | - |  |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |  |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 1.50 | $\mathrm{ramps} / \mathrm{mi}$ |  |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 70.9 | mph |  |


| General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


| General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | ---: |
| Volume, V | 3,933 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.95 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,504 | pcphpl |
| Total Trucks | $9.0 \%$ |  | Capacity, c | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |  |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.63 |  |


| General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 70.9 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 69.6 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 21.6 | pcpmpl |
| Total Ramp Density Adjustment | 4.5 | mph | Level of Service, LOS | C |  |

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|  | Freeway Basic Report |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Eastbound I-80 |
| Segment | West of Old Davis Rd |
| Alternative | Existing Conditions |
| Time Period | PM Peak Hour |


|  | General Purpose Lanes - Geometric Data |  |  |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: | :---: | :---: |
| General Purpose Lanes, N | 5 | In | Terrain Type | Level |  |  |  |  |
| Segment Length, L | 1,500 | ft | Percent Grade | - |  |  |  |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |  |  |  |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 1.67 | $\mathrm{ramps} / \mathrm{mi}$ |  |  |  |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 70.5 | mph |  |  |  |


| General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


| General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Volume, V | 4,622 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.99 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,018 | pcphpl |
| Total Trucks | 9.0\% |  | Capacity, c | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - |  | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.42 |  |


| General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS ${ }_{\text {adj }}$ | 70.5 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 70.5 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 14.4 | pcpmpl |
| Total Ramp Density Adjustment | 4.9 | mph | Level of Service, LOS | B |  |

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| Entering General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :--- | :---: | :--- | :--- | :--- | :--- |
| Volume, V | 4,622 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.99 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,018 | pcphpl |
| Total Trucks | $9.0 \%$ |  | Capacity, c | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |  |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.42 |  |


| Entering General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 70.5 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 70.5 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 14.4 | pcpmpl |
| Total Ramp Density Adjustment | 4.9 | mph | Level of Service, LOS | B |  |


| Segment General Purpose Lanes - Capacity, Speed, and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| General Purpose Lanes, N | 6 | $\ln$ | Average Speed, S | 70.5 | mph |
| Adjusted Capacity, cadj | 2,400 | pcphpl | Density, D | 12.8 | pcphpl |
| Flow Rate, vp | 903 | pcphpl | Level of Service, LOS | B |  |
| Volume-to-Capacity Ratio, v/c | 0.38 |  |  |  |  |

## Freeway Merge Report



## Adjacent Ramp Data

Adjacent Ramp Meeting Criteria
Upstream Downstream

Type of Adjacent Ramp
Distance to Adjacent Ramp ft
Volume on Adjacent Ramp pcph

## Freeway Merge Report



| Ramp Influence Area Density and Level of Service |  |  |
| :--- | :--- | :---: |
|  | pcpmpl |  |
| Density in Ramp Influence Area, $D_{R}$ |  |  |

## Segment Speed, Flow, and Density

Speed Adjustment Factor, SAF
Speed Index, $\mathrm{M}_{\mathrm{S}}$ or $\mathrm{D}_{\mathrm{S}}$
Average Speed in Ramp Influence Area, $\mathrm{S}_{\mathrm{R}} \mathrm{mph}$

Average Flow in Outer Lanes, $\mathrm{v}_{\mathrm{OA}}$
pcphpl
mph
Average Speed in Outer Lanes, $\mathrm{S}_{0}$
Average Speed for Segment, S
mph
Density across All Lanes, D
pcpmpl

|  | Freeway Basic Report |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Eastbound I-80 |
| Segment | Old Davis Rd to Lane Drop 1 |
| Alternative | Existing Conditions |
| Time Period | PM Peak Hour |


|  | General |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
|  | Purpose Lanes - Geometric Data |  |  |  |  |  |
| General Purpose Lanes, N | 5 | ln | Terrain Type | Level |  |  |
| Segment Length, L | 820 | ft | Percent Grade | - |  |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |  |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 1.67 | $\mathrm{ramps} / \mathrm{mi}$ |  |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 70.5 | mph |  |


| General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


|  | General Purpose Lanes - Demand and Capacity |  |  |  |  |
| :--- | :---: | :--- | :--- | :--- | :--- |
| Volume, V | 4,874 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.99 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,073 | pcphpl |
| Total Trucks | $9.0 \%$ |  | Capacity, c | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |  |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.45 |  |


| General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 70.5 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 70.5 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 15.2 | pcpmpl |
| Total Ramp Density Adjustment | 4.9 | mph | Level of Service, LOS | B |  |

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|  | Freeway Basic Report |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Eastbound I-80 |
| Segment | Lane Drop 1 to Lane Drop 2 |
| Alternative | Existing Conditions |
| Time Period | PM Peak Hour |


|  | General |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
|  | Purpose Lanes - Geometric Data |  |  |  |  |  |
| General Purpose Lanes, N | 4 | ln | Terrain Type | Level |  |  |
| Segment Length, L | 1,480 | ft | Percent Grade | - |  |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |  |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 1.50 | $\mathrm{ramps} / \mathrm{mi}$ |  |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 70.9 | mph |  |


| General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


| General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | ---: |
| Volume, V | 4,874 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.99 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,342 | pcphpl |
| Total Trucks | $9.0 \%$ |  | Capacity, c | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |  |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.56 |  |


| General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 70.9 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 70.5 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 19.0 | pcpmpl |
| Total Ramp Density Adjustment | 4.5 | mph | Level of Service, LOS | C |  |

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## Freeway Diverge Report

| Freeway Diverge Report |  |  |  |
| :---: | :---: | :---: | :---: |
| Project I-80/Richards B <br> Freeway Eastbound I-80 <br> Segment Richards Blvd O <br> Alternative Existing Conditi <br> Time Period PM Peak Hour |  |  |  |
| Geometric Data |  |  |  |
|  | Freeway | Off Ramp |  |
| Number of Lanes, N | 3 | 1 |  |
| Free-Flow Speed, FFS | 70.9 | 25 | mph |
| Segment Length, L / Deceleration Length, LD | 1,240 | 150 | ft |
| Terrain Type | Level | Level |  |
| Percent Grade | - | - |  |
| Grade Length | - |  | ft |
| Segment Type / Ramp Type | Freeway | Right |  |
| Adjustment Factors |  |  |  |
|  | Freeway | Off Ramp |  |
| Driver Population | Familiar | Familiar |  |
| Weather Type | Non-severe | Non-severe |  |
| Incident Type | No incident | No incident |  |
| Capacity Adjustment Factor, CAF | 1.00 | 1.00 |  |
| Demand Adjustment Factor, DAF | 1.00 | 1.00 |  |
| Volume Data |  |  |  |
| Junction Components | Freeway | Off Ramp |  |
| Volume, V | 4,874 | 593 | vph |
| Peak Hour Factor, PHF | 0.99 | 0.86 |  |
| Total Trucks | 9.0\% | 2.4\% |  |
| Single Unit/Tractor-Trailer Mix | - | - |  |
| Passenger Car Equivalent, $\mathrm{E}_{T}$ | 2.0 | 2.0 |  |
| Heavy Vehicle Adjustment, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 | 0.977 |  |
| Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 5,366 | 706 | pcph |

## Adjacent Ramp Data

Adjacent Ramp Meeting Criteria

| Upstream | Downstream |
| :---: | :---: |
| No | Yes |
|  | On |
|  | 2,740 |
|  | 389 |

Type of Adjacent Ramp
Distance to Adjacent Ramp
Volume on Adjacent Ramp

## Freeway Diverge Report



|  | Freeway Basic Report |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Eastbound I-80 |
| Segment | Richards Blvd Off to On |
| Alternative | Existing Conditions |
| Time Period | PM Peak Hour |


|  | General |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
|  | Purpose Lanes - Geometric Data |  |  |  |  |  |
| General Purpose Lanes, N | 3 | ln | Terrain Type | Level |  |  |
| Segment Length, L | 1,500 | ft | Percent Grade | - |  |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |  |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 1.67 | $\mathrm{ramps} / \mathrm{mi}$ |  |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 70.5 | mph |  |


| General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


| General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Volume, V | 4,281 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.99 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,571 | pcphpl |
| Total Trucks | 9.0\% |  | Capacity, c | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - |  | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |
| Passenger Car Equivalent, $\mathrm{E}_{T}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.65 |  |


| General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 70.5 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 68.7 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 22.9 | pcpmpl |
| Total Ramp Density Adjustment | 4.9 | mph | Level of Service, LOS | C |  |

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## Freeway Merge Report

| Freeway Merge Report |  |  |  |
| :---: | :---: | :---: | :---: |
| Project I-80/Richards B |  |  |  |
| Freeway Eastbound I-80 |  |  |  |
| Segment Richards Blvd O |  |  |  |
| Alternative Existing Conditi |  |  |  |
| Time Period PM Peak Hour |  |  |  |
| Geometric Data |  |  |  |
|  | Freeway | On Ramp |  |
| Number of Lanes, N | 3 | 1 |  |
| Free-Flow Speed, FFS | 70.5 | 45 | mph |
| Segment Length, L / Acceleration Length, LA | 1,500 | 500 | ft |
| Terrain Type | Level | Level |  |
| Percent Grade | - | - |  |
| Grade Length | - |  | ft |
| Segment Type / Ramp Type | Freeway | Right |  |
| Adjustment Factors |  |  |  |
|  | Freeway | On Ramp |  |
| Driver Population | Familiar | Familiar |  |
| Weather Type | Non-severe | Non-severe |  |
| Incident Type | No incident | No incident |  |
| Capacity Adjustment Factor, CAF | 1.00 | 1.00 |  |
| Demand Adjustment Factor, DAF | 1.00 | 1.00 |  |
| Volume Data |  |  |  |
| Junction Components | Freeway | On Ramp |  |
| Volume, V | 4,281 | 320 | vph |
| Peak Hour Factor, PHF | 0.99 | 0.84 |  |
| Total Trucks | 9.0\% | 2.2\% |  |
| Single Unit/Tractor-Trailer Mix | - | - |  |
| Passenger Car Equivalent, $\mathrm{E}_{T}$ | 2.0 | 2.0 |  |
| Heavy Vehicle Adjustment, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 | 0.978 |  |
| Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 4,713 | 389 | pcph |

## Adjacent Ramp Data

Adjacent Ramp Meeting Criteria

| Upstream | Downstream |
| :---: | :---: |
| Yes | No |
| Off |  |
| 2,740 |  |
| 706 |  |

## Freeway Merge Report



|  | Freeway Basic Report |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Eastbound I-80 |
| Segment | Richards Blvd to Chiles Rd |
| Alternative | Existing Conditions |
| Time Period | PM Peak Hour |


|  | General |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
|  | Purpose Lanes - Geometric Data |  |  |  |  |  |
| General Purpose Lanes, N | 3 | ln | Terrain Type | Level |  |  |
| Segment Length, L | 5,710 | ft | Percent Grade | - |  |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |  |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 1.50 | $\mathrm{ramps} / \mathrm{mi}$ |  |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 70.9 | mph |  |


| General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


|  | General Purpose Lanes - Demand and Capacity |  |  |  |  |
| :--- | :---: | :--- | :--- | :--- | :--- |
| Volume, V | 4,601 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.99 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,689 | pcphpl |
| Total Trucks | $9.0 \%$ |  | Capacity, c | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |  |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.70 |  |


| General Purpose Lanes - Speed and Density |  |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 70.9 | mph |  |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 67.7 | mph |  |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 24.9 | pcpmpl |  |
| Total Ramp Density Adjustment | 4.5 | mph | Level of Service, LOS | C |  |  |

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## Freeway Diverge Report

| Freeway Diverge Report |  |  |  |
| :---: | :---: | :---: | :---: |
| Project I-80/Richards B <br> Freeway Eastbound I-80 <br> Segment Chiles Rd Off Ra <br> Alternative Existing Conditi <br> Time Period PM Peak Hour |  |  |  |
| Geometric Data |  |  |  |
|  | Freeway | Off Ramp |  |
| Number of Lanes, N | 3 | 2 |  |
| Free-Flow Speed, FFS | 70.9 | 25 | mph |
| Segment Length, L / Deceleration Length, LD | 1,500 | 1,500 | ft |
| Terrain Type | Level | Level |  |
| Percent Grade | - | - |  |
| Grade Length | - | - | ft |
| Segment Type / Ramp Type | Freeway | Right |  |
| Adjustment Factors |  |  |  |
|  | Freeway | Off Ramp |  |
| Driver Population | Familiar | Familiar |  |
| Weather Type | Non-severe | Non-severe |  |
| Incident Type | No incident | No incident |  |
| Capacity Adjustment Factor, CAF | 1.00 | 1.00 |  |
| Demand Adjustment Factor, DAF | 1.00 | 1.00 |  |
| Volume Data |  |  |  |
| Junction Components | Freeway | Off Ramp |  |
| Volume, V | 4,601 | 411 | vph |
| Peak Hour Factor, PHF | 0.99 | 0.76 |  |
| Total Trucks | 9.0\% | 3.0\% |  |
| Single Unit/Tractor-Trailer Mix | - | - |  |
| Passenger Car Equivalent, $\mathrm{E}_{T}$ | 2.0 | 2.0 |  |
| Heavy Vehicle Adjustment, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 | 0.971 |  |
| Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 5,066 | 557 | pcph |

## Adjacent Ramp Data

Adjacent Ramp Meeting Criteria
Upstream Downstream

Type of Adjacent Ramp
Distance to Adjacent Ramp ft
Volume on Adjacent Ramp pcph

## Freeway Diverge Report



|  | Freeway Basic Report |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Eastbound I-80 |
| Segment | Chiles Rd Off to Mace Rd On |
| Alternative | Existing Conditions |
| Time Period | PM Peak Hour |


|  | General |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
|  | Purpose Lanes - Geometric Data |  |  |  |  |  |
| General Purpose Lanes, N | 3 | ln | Terrain Type | Level |  |  |
| Segment Length, L | 1,000 | ft | Percent Grade | - |  |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |  |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 1.50 | $\mathrm{ramps} / \mathrm{mi}$ |  |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 70.9 | mph |  |


| General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


| General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Volume, V | 4,190 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.99 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,538 | pcphpl |
| Total Trucks | 9.0\% |  | Capacity, c | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - |  | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.64 |  |


| General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 70.9 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 69.3 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 22.2 | pcpmpl |
| Total Ramp Density Adjustment | 4.5 | mph | Level of Service, LOS | C |  |

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|  | Freeway Basic Report |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Westbound I-80 |
| Segment | East of Mace Blvd |
| Alternative | Existing Conditions |
| Time Period | AM Peak Hour |


|  | General |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
|  | Purpose Lanes - Geometric Data |  |  |  |  |  |
| General Purpose Lanes, N | 3 | ln | Terrain Type | Level |  |  |
| Segment Length, L | 2,590 | ft | Percent Grade | - |  |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |  |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 1.50 | $\mathrm{ramps} / \mathrm{mi}$ |  |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 70.9 | mph |  |


| General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


| General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Volume, V | 4,270 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.98 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,583 | pcphpl |
| Total Trucks | 9.0\% |  | Capacity, c | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - |  | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.66 |  |


| General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 70.9 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 68.9 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 23.0 | pcpmpl |
| Total Ramp Density Adjustment | 4.5 | mph | Level of Service, LOS | C |  |

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| Entering General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Volume, V | 4,270 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.98 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,583 | pcphpl |
| Total Trucks | 9.0\% |  | Capacity, c | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - |  | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.66 |  |


| Entering General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 71.3 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 69.1 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 22.9 | pcpmpl |
| Total Ramp Density Adjustment | 4.1 | mph | Level of Service, LOS | C |  |


| Segment General Purpose Lanes - Capacity, Speed, and Density |  |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
| General Purpose Lanes, N | 4 | $\ln$ | Average Speed, S | 70.8 | mph |  |
| Adjusted Capacity, cadj | 2,400 | pcphpl | Density, D | 19.1 | pcphpl |  |
| Flow Rate, vp | 1,351 | pcphpl | Level of Service, LOS | C |  |  |
| Volume-to-Capacity Ratio, v/c | 0.56 |  |  |  |  |  |

## Freeway Merge Report



## Freeway Merge Report



| Ramp Influence Area Density and Level of Service |  |  |
| :--- | :--- | :---: |
|  | pcpmpl |  |
| Density in Ramp Influence Area, $D_{R}$ |  |  |

## Segment Speed, Flow, and Density

Speed Adjustment Factor, SAF
Speed Index, $\mathrm{M}_{\mathrm{S}}$ or $\mathrm{D}_{\mathrm{S}}$
Average Speed in Ramp Influence Area, $\mathrm{S}_{\mathrm{R}} \mathrm{mph}$

Average Flow in Outer Lanes, $\mathrm{v}_{\mathrm{OA}}$
pcphpl
mph
Average Speed in Outer Lanes, $\mathrm{S}_{0}$
mph
Density across All Lanes, D
pcpmpl

|  | Freeway Basic Report |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Westbound I-80 |
| Segment | Lane Drop to Olive Dr |
| Alternative | Existing Conditions |
| Time Period | AM Peak Hour |


|  | General |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
|  | Purpose Lanes - Geometric Data |  |  |  |  |  |
| General Purpose Lanes, N | 3 | ln | Terrain Type | Level |  |  |
| Segment Length, L | 4,780 | ft | Percent Grade | - |  |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |  |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 1.33 | $\mathrm{ramps} / \mathrm{mi}$ |  |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 71.3 | mph |  |


| General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


| General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Volume, V | 4,815 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.98 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,785 | pcphpl |
| Total Trucks | 9.0\% |  | Capacity, c | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - |  | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.74 |  |


| General Purpose Lanes - Speed and Density |  |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 71.3 | mph |  |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 66.6 | mph |  |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 26.8 | pcpmpl |  |
| Total Ramp Density Adjustment | 4.1 | mph | Level of Service, LOS | D |  |  |

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## Freeway Diverge Report



|  | Volume Data |  |  |  |
| :--- | :---: | :---: | :---: | :---: |
|  |  |  |  |  |
| Junction Components | $\underline{\text { Freeway }}$ | $\underline{\text { Off Ramp }}$ |  |  |
| Volume, V | 4,815 | 149 | vph |  |
| Peak Hour Factor, PHF | 0.98 | 0.81 |  |  |
| Total Trucks | $9.0 \%$ | $0.7 \%$ |  |  |
| Single Unit/Tractor-Trailer Mix | - | - |  |  |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 | 2.0 |  |  |
| Heavy Vehicle Adjustment, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 | 0.993 |  |  |
| Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 5,355 | 185 | pcph |  |

Adjacent Ramp Meeting Criteria

| Upstream | Downstream |
| :---: | :---: |
| No | Yes |
|  | Off |
|  | 2,390 |
|  | 400 |

## Freeway Diverge Report



|  | Freeway Basic Report |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Westbound I-80 |
| Segment | Olive Dr to Richards Blvd |
| Alternative | Existing Conditions |
| Time Period | AM Peak Hour |


|  | General |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
|  | Purpose Lanes - Geometric Data |  |  |  |  |  |
| General Purpose Lanes, N | 3 | ln | Terrain Type | Level |  |  |
| Segment Length, L | 890 | ft | Percent Grade | - |  |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |  |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 1.83 | $\mathrm{ramps} / \mathrm{mi}$ |  |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 70.0 | mph |  |


| General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


| General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Volume, V | 4,666 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.98 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,730 | pcphpl |
| Total Trucks | 9.0\% |  | Capacity, c | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - |  | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.72 |  |


| General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 70.0 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 66.8 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 25.9 | pcpmpl |
| Total Ramp Density Adjustment | 5.4 | mph | Level of Service, LOS | C |  |

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## Freeway Diverge Report

|  | Freeway Diverg |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Westbound I-80 |
| Segment | Richards Blvd NB Off |
| Alternative | Existing Conditions |
| Time Period | AM Peak Hour |


| Geometric Data |  |  |  |
| :---: | :---: | :---: | :---: |
|  | Freeway | Off Ramp |  |
| Number of Lanes, N | 3 | 1 |  |
| Free-Flow Speed, FFS | 70.0 | 45 | mph |
| Segment Length, L / Deceleration Length, LD | 1,500 | 150 | ft |
| Terrain Type | Level | Level |  |
| Percent Grade | - | - |  |
| Grade Length | - | - | ft |
| Segment Type / Ramp Type | Freeway | Right |  |
| Adjustment Factors |  |  |  |
|  | Freeway | Off Ramp |  |
| Driver Population | Familiar | Familiar |  |
| Weather Type | Non-severe | Non-severe |  |
| Incident Type | No incident | No incident |  |
| Capacity Adjustment Factor, CAF | 1.00 | 1.00 |  |
| Demand Adjustment Factor, DAF | 1.00 | 1.00 |  |
| Volume Data |  |  |  |
| Junction Components | Freeway | Off Ramp |  |
| Volume, V | 4,666 | 345 | vph |
| Peak Hour Factor, PHF | 0.98 | 0.87 |  |
| Total Trucks | 9.0\% | 0.9\% |  |
| Single Unit/Tractor-Trailer Mix | - | - |  |
| Passenger Car Equivalent, $\mathrm{E}_{T}$ | 2.0 | 2.0 |  |
| Heavy Vehicle Adjustment, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 | 0.991 |  |
| Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 5,190 | 400 | pcph |

Adjacent Ramp Meeting Criteria
Type of Adjacent Ramp
Distance to Adjacent Ramp
Volume on Adjacent Ramp

| Upstream | Downstream |
| :---: | :---: |
| Yes | No |
| Off |  |
| 2,390 |  |
| 185 |  |

## Freeway Diverge Report



|  | Freeway Basic Report |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Westbound I-80 |
| Segment | Richards Blvd NB Off to On |
| Alternative | Existing Conditions |
| Time Period | AM Peak Hour |


|  | General |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
|  | Purpose Lanes - Geometric Data |  |  |  |  |  |
| General Purpose Lanes, N | 3 | ln | Terrain Type | Level |  |  |
| Segment Length, L | 430 | ft | Percent Grade | - |  |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |  |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 1.83 | $\mathrm{ramps} / \mathrm{mi}$ |  |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 70.0 | mph |  |


| General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


| General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Volume, V | 4,321 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.98 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,602 | pcphpl |
| Total Trucks | 9.0\% |  | Capacity, c | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - |  | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.67 |  |


| General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 70.0 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 68.2 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 23.5 | pcpmpl |
| Total Ramp Density Adjustment | 5.4 | mph | Level of Service, LOS | C |  |

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## Freeway Weave Report

|  | Freeway Weave Report |  |
| :--- | :--- | :--- | :--- |
|  |  |  |

## Freeway Weave Report

| Project | I-80/Richards Blvd Interchange |
| :--- | :--- |
| Freeway | Westbound I-80 |
| Segment | Richards Blvd NB On to SB Off |
| Alternative | Existing Conditions |
| Time period | AM Peak Hour |


|  | Capacity |  |
| :--- | :---: | :---: |
|  |  |  |
|  |  |  |
| Maximum Weaving Length, $\mathrm{L}_{\mathrm{MAX}}$ | 3,925 | ft |
| Weaving Length Check | OK |  |
| Freeway Maximum Capacity, $\mathrm{c}_{\mathrm{IFL}}$ | 2,400 | pchpl |
| Density-Based Capacity, $\mathrm{c}_{\mathrm{IWL}}$ | 9,338 | pchpl |
| Demand Flow-Based Capacity, $\mathrm{c}_{\mathrm{IW}}$ | 15,966 | pch |
| Weaving Segment Capacity, $\mathrm{c}_{\mathrm{w}}$ | 15,966 | vph |
| Adjusted Weaving Area Capacity, $\mathrm{c}_{\mathrm{wa}}$ | 15,966 | vph |
| Volume-to-Capacity Ratio, $\mathrm{v} / \mathrm{c}$ | 0.31 |  |


| Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |
| Minimum Lane Change Rate, $\mathrm{LC}_{\mathrm{MIN}}$ | 744 | $\mathrm{Ic} / \mathrm{h}$ |  |  |  |
| Weaving Lane Change Rate, $\mathrm{LC}_{\mathrm{W}}$ | 763 | $\mathrm{Ic} / \mathrm{h}$ |  |  |  |
| Non-weaving Vehicle Index, $\mathrm{I}_{\mathrm{NW}}$ | 191 |  |  |  |  |
| Non-weaving Lane Change Rate, $\mathrm{LC}_{\mathrm{NW}}$ | 447 | $\mathrm{Ic} / \mathrm{h}$ |  |  |  |
| Total Lane Change Rate, $\mathrm{LC}_{\mathrm{ALL}}$ | 1,210 | $\mathrm{Ic} / \mathrm{h}$ |  |  |  |
| Weaving Intensity Factor, W | 0.454 |  |  |  |  |
| Average Weaving Speed, $\mathrm{S}_{\mathrm{W}}$ | 52.9 | mph |  |  |  |
| Average Non-Weaving Speed, $\mathrm{S}_{\mathrm{NW}}$ | 58.3 | mph |  |  |  |
| Average Speed, S | 57.5 | mph |  |  |  |
| Density, D | 23.2 | pcpmpl |  |  |  |
| Level of Service, LOS | C |  |  |  |  |

## Capacity Checks

Entering General Purpose Lanes
Exiting General Purpose Lanes
On Ramp
Off Ramp
$\left.\begin{array}{ccccc}\begin{array}{c}\text { Flow }\end{array} & & \text { Capacity } & & \text { V/C Ratio } \\ \hline 4,806 & & 7,200 & & \text { pcph }\end{array}\right)$

## Leisch Method for Weaving Analysis

## Data Input

Number of Entering Mainline Lanes
Number of Lanes in Weaving Section Length of Weaving Section (feet)

| $N_{b}$ | 3 |
| :---: | :---: |
| $N$ | 4 |
|  | 500 |

Mainline to Off-ramp ( $\mathrm{W}_{2}$ )

| 364 |
| :---: |
| $2.2 \%$ |
| 2.0 |
| 372 |

Volume (vph)
Truck Percentage
PCE for Trucks
Volume (pcph)


The LOS in the chart above refers to the capacity of weaving traffic only; through and ramp to ramp traffic is not included.

* Note: Do not adjust by a Peak Hour Factor (PHF). The methodology incorporates the PHF in the Service Volume tables.

Sources: Completion of Procedures for Analysis and Design of Traffic Weaving Sections, Jack E. Leisch \& Associates, September 1983 and
Highway Design Manual , California Department of Transportation, 2014

|  | Freeway Basic Report |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Westbound I-80 |
| Segment | Richards Blvd SB Off to On |
| Alternative | Existing Conditions |
| Time Period | AM Peak Hour |


|  | General |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
|  | Purpose Lanes - Geometric Data |  |  |  |  |  |
| General Purpose Lanes, N | 3 | ln | Terrain Type | Level |  |  |
| Segment Length, L | 210 | ft | Percent Grade | - |  |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |  |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 1.83 | $\mathrm{ramps} / \mathrm{mi}$ |  |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 70.0 | mph |  |


| General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


| General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Volume, V | 4,494 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.98 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,666 | pcphpl |
| Total Trucks | 9.0\% |  | Capacity, c | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - |  | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.69 |  |


| General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 70.0 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 67.5 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 24.7 | pcpmpl |
| Total Ramp Density Adjustment | 5.4 | mph | Level of Service, LOS | C |  |

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| Entering General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :--- | :---: | :--- | :--- | :--- | :--- |
| Volume, V | 4,494 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.98 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,666 | pcphpl |
| Total Trucks | $9.0 \%$ |  | Capacity, c | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |  |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.69 |  |


| Entering General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 70.4 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 67.7 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 24.6 | pcpmpl |
| Total Ramp Density Adjustment | 5.0 | mph | Level of Service, LOS | C |  |


| Segment General Purpose Lanes - Capacity, Speed, and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| General Purpose Lanes, N | 4 | In | Average Speed, S | 70.3 | mph |
| Adjusted Capacity, cadj | 2,400 | pcphpl | Density, D | 18.4 | pcphpl |
| Flow Rate, vp | 1,290 | pcphpl | Level of Service, LOS | C |  |
| Volume-to-Capacity Ratio, v/c | 0.54 |  |  |  |  |

## Freeway Diverge Report

|  | Freeway Diverg |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Westbound I-80 |
| Segment | Lane Add to Old Davis Off |
| Alternative | Existing Conditions |
| Time Period | AM Peak Hour |


| Geometric Data |  |  |  |
| :---: | :---: | :---: | :---: |
|  | Freeway | Off Ramp |  |
| Number of Lanes, N | 4 | 1 |  |
| Free-Flow Speed, FFS | 70.0 | 45 | mph |
| Segment Length, L / Deceleration Length, LD | 1,190 | 150 | ft |
| Terrain Type | Level | Level |  |
| Percent Grade | - | - |  |
| Grade Length | - | - | ft |
| Segment Type / Ramp Type | Freeway | Right |  |
| Adjustment Factors |  |  |  |
|  | Freeway | Off Ramp |  |
| Driver Population | Familiar | Familiar |  |
| Weather Type | Non-severe | Non-severe |  |
| Incident Type | No incident | No incident |  |
| Capacity Adjustment Factor, CAF | 1.00 | 1.00 |  |
| Demand Adjustment Factor, DAF | 1.00 | 1.00 |  |
| Volume Data |  |  |  |
| Junction Components | Freeway | Off Ramp |  |
| Volume, V | 4,618 | 481 | vph |
| Peak Hour Factor, PHF | 0.98 | 0.83 |  |
| Total Trucks | 9.0\% | 1.0\% |  |
| Single Unit/Tractor-Trailer Mix | - | - |  |
| Passenger Car Equivalent, $\mathrm{E}_{T}$ | 2.0 | 2.0 |  |
| Heavy Vehicle Adjustment, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 | 0.990 |  |
| Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 5,136 | 585 | pcph |

Adjacent Ramp Meeting Criteria
Upstream Downstream

Type of Adjacent Ramp
Distance to Adjacent Ramp ft
Volume on Adjacent Ramp
pcph

## Freeway Diverge Report



|  | Freeway Basic Report |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Westbound I-80 |
| Segment | West of Old Davis Rd |
| Alternative | Existing Conditions |
| Time Period | AM Peak Hour |


|  | General |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
|  | Purpose Lanes - Geometric Data |  |  |  |  |  |
| General Purpose Lanes, N | 5 | ln | Terrain Type | Level |  |  |
| Segment Length, L | 1,350 | ft | Percent Grade | - |  |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |  |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 1.83 | $\mathrm{ramps} / \mathrm{mi}$ |  |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 70.0 | mph |  |


| General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


| General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Volume, V | 4,137 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.98 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 920 | pcphpl |
| Total Trucks | 9.0\% |  | Capacity, c | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - |  | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.38 |  |


| General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 70.0 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 70.0 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 13.1 | pcpmpl |
| Total Ramp Density Adjustment | 5.4 | mph | Level of Service, LOS | B |  |

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|  | Freeway Basic Report |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Westbound I-80 |
| Segment | East of Mace Blvd |
| Alternative | Existing Conditions |
| Time Period | PM Peak Hour |


|  | General |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
|  | Purpose Lanes - Geometric Data |  |  |  |  |  |
| General Purpose Lanes, N | 3 | ln | Terrain Type | Level |  |  |
| Segment Length, L | 2,590 | ft | Percent Grade | - |  |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |  |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 1.50 | $\mathrm{ramps} / \mathrm{mi}$ |  |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 70.9 | mph |  |


| General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


| General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Volume, V | 4,063 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.99 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,491 | pcphpl |
| Total Trucks | 9.0\% |  | Capacity, c | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - |  | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.62 |  |


| General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 70.9 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 69.7 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 21.4 | pcpmpl |
| Total Ramp Density Adjustment | 4.5 | mph | Level of Service, LOS | C |  |

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| Entering General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :--- | :---: | :--- | :--- | :--- | :--- |
| Volume, V | 4,063 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.99 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,491 | pcphpl |
| Total Trucks | $9.0 \%$ |  | Capacity, c | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |  |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.62 |  |


| Entering General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 71.3 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 70.0 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 21.3 | pcpmpl |
| Total Ramp Density Adjustment | 4.1 | mph | Level of Service, LOS | C |  |

## Segment General Purpose Lanes - Capacity, Speed, and Density

| General Purpose Lanes, N | 4 | $\ln$ | Average Speed, S | 71.2 | mph |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Adjusted Capacity, cadj | 2,400 | pcphpl | Density, D | 17.7 | pcphpl |
| Flow Rate, vp | 1,260 | pcphpl | Level of Service, LOS | B |  |
| Volume-to-Capacity Ratio, v/c | 0.52 |  |  |  |  |

## Freeway Merge Report



## Freeway Merge Report



| Ramp Influence Area Density and Level of Service |  |  |
| :--- | :--- | :---: |
|  |  |  |
| Density in Ramp Influence Area, $D_{R}$ | pcpmpl |  |
| Level of Service, LOS |  |  |

## Segment Speed, Flow, and Density

Speed Adjustment Factor, SAF
Speed Index, $\mathrm{M}_{\mathrm{S}}$ or $\mathrm{D}_{\mathrm{S}}$
Average Speed in Ramp Influence Area, $\mathrm{S}_{\mathrm{R}} \mathrm{mph}$

Average Flow in Outer Lanes, $\mathrm{v}_{\mathrm{OA}}$
pcphpl
mph
Average Speed in Outer Lanes, $\mathrm{S}_{0}$
Average Speed for Segment, S
mph
Density across All Lanes, D
pcpmpl

|  | Freeway Basic Report |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Westbound I-80 |
| Segment | Lane Drop to Olive Dr |
| Alternative | Existing Conditions |
| Time Period | PM Peak Hour |


|  | General |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
|  | Purpose Lanes - Geometric Data |  |  |  |  |  |
| General Purpose Lanes, N | 3 | ln | Terrain Type | Level |  |  |
| Segment Length, L | 4,780 | ft | Percent Grade | - |  |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |  |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 1.33 | $\mathrm{ramps} / \mathrm{mi}$ |  |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 71.3 | mph |  |


| General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


| General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Volume, V | 4,492 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.99 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,649 | pcphpl |
| Total Trucks | 9.0\% |  | Capacity, c | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - |  | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.69 |  |


| General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 71.3 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 68.4 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 24.1 | pcpmpl |
| Total Ramp Density Adjustment | 4.1 | mph | Level of Service, LOS | C |  |

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## Freeway Diverge Report

|  | Freeway Diverg |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Westbound I-80 |
| Segment | Olive Dr Off |
| Alternative | Existing Conditions |
| Time Period | PM Peak Hour |


| Geometric Data |  |  |  |
| :---: | :---: | :---: | :---: |
|  | Freeway | Off Ramp |  |
| Number of Lanes, N | 3 | 1 |  |
| Free-Flow Speed, FFS | 70.5 | 35 | mph |
| Segment Length, L / Deceleration Length, LD | 1,500 | 150 | ft |
| Terrain Type | Level | Level |  |
| Percent Grade | - | - |  |
| Grade Length | - | - | ft |
| Segment Type / Ramp Type | Freeway | Right |  |
| Adjustment Factors |  |  |  |
|  | Freeway | Off Ramp |  |
| Driver Population | Familiar | Familiar |  |
| Weather Type | Non-severe | Non-severe |  |
| Incident Type | No incident | No incident |  |
| Capacity Adjustment Factor, CAF | 1.00 | 1.00 |  |
| Demand Adjustment Factor, DAF | 1.00 | 1.00 |  |


|  | Volume Data |  |  |  |
| :--- | :---: | :---: | :---: | :---: |
|  |  |  |  |  |
| Junction Components | $\underline{\text { Freeway }}$ | $\underline{\text { Off Ramp }}$ |  |  |
| Volume, V | 4,492 | 125 | vph |  |
| Peak Hour Factor, PHF | 0.99 | 0.84 |  |  |
| Total Trucks | $9.0 \%$ | $0.8 \%$ |  |  |
| Single Unit/Tractor-Trailer Mix | - | - |  |  |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 | 2.0 |  |  |
| Heavy Vehicle Adjustment, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 | 0.992 |  |  |
| Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 4,946 | 150 | pcph |  |

Adjacent Ramp Meeting Criteria

| Upstream | Downstream |
| :---: | :---: |
| No | Yes |
|  | Off |
|  | 2,390 |
|  | 255 |

## Freeway Diverge Report



|  | Freeway Basic Report |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Westbound I-80 |
| Segment | Olive Dr to Richards Blvd |
| Alternative | Existing Conditions |
| Time Period | PM Peak Hour |


|  | General |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
|  | Purpose Lanes - Geometric Data |  |  |  |  |  |
| General Purpose Lanes, N | 3 | ln | Terrain Type | Level |  |  |
| Segment Length, L | 890 | ft | Percent Grade | - |  |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |  |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 1.83 | $\mathrm{ramps} / \mathrm{mi}$ |  |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 70.0 | mph |  |


| General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


| General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Volume, V | 4,367 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.99 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,603 | pcphpl |
| Total Trucks | 9.0\% |  | Capacity, c | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - |  | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.67 |  |


| General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 70.0 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 68.2 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 23.5 | pcpmpl |
| Total Ramp Density Adjustment | 5.4 | mph | Level of Service, LOS | C |  |

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## Freeway Diverge Report

| Freeway Diverge Report |  |  |  |
| :---: | :---: | :---: | :---: |
| Project I-80/Richards B <br> Freeway Westbound I-80 <br> Segment Richards Blvd N <br> Alternative Existing Conditi <br> Time Period PM Peak Hour |  |  |  |
| Geometric Data |  |  |  |
|  | Freeway | Off Ramp |  |
| Number of Lanes, N | 3 | 1 |  |
| Free-Flow Speed, FFS | 70.0 | 45 | mph |
| Segment Length, L / Deceleration Length, LD | 1,500 | 150 | ft |
| Terrain Type | Level | Level |  |
| Percent Grade | - | - |  |
| Grade Length | - | - | ft |
| Segment Type / Ramp Type | Freeway | Right |  |
| Adjustment Factors |  |  |  |
|  | Freeway | Off Ramp |  |
| Driver Population | Familiar | Familiar |  |
| Weather Type | Non-severe | Non-severe |  |
| Incident Type | No incident | No incident |  |
| Capacity Adjustment Factor, CAF | 1.00 | 1.00 |  |
| Demand Adjustment Factor, DAF | 1.00 | 1.00 |  |
| Volume Data |  |  |  |
| Junction Components | Freeway | Off Ramp |  |
| Volume, V | 4,367 | 214 | vph |
| Peak Hour Factor, PHF | 0.99 | 0.85 |  |
| Total Trucks | 9.0\% | 1.4\% |  |
| Single Unit/Tractor-Trailer Mix | - | - |  |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 | 2.0 |  |
| Heavy Vehicle Adjustment, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 | 0.986 |  |
| Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 4,808 | 255 | pcph |

## Adjacent Ramp Data

Adjacent Ramp Meeting Criteria

| Upstream | Downstream |
| :---: | :---: |
| Yes | No |
| Off |  |
| 2,390 |  |
| 150 |  |

## Freeway Diverge Report



|  | Freeway Basic Report |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Westbound I-80 |
| Segment | Richards Blvd NB Off to On |
| Alternative | Existing Conditions |
| Time Period | PM Peak Hour |


|  | General |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
|  | Purpose Lanes - Geometric Data |  |  |  |  |  |
| General Purpose Lanes, N | 3 | ln | Terrain Type | Level |  |  |
| Segment Length, L | 430 | ft | Percent Grade | - |  |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |  |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 1.83 | $\mathrm{ramps} / \mathrm{mi}$ |  |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 70.0 | mph |  |


| General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


| General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :--- | :---: | :--- | :--- | :--- | :--- |
| Volume, V | 4,153 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.99 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,524 | pcphpl |
| Total Trucks | $9.0 \%$ |  | Capacity, | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |  |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.64 |  |


| General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 70.0 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 68.8 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 22.1 | pcpmpl |
| Total Ramp Density Adjustment | 5.4 | mph | Level of Service, LOS | C |  |

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## Freeway Weave Report

|  | Freeway Weave Report |  |  |
| :--- | :--- | :--- | :---: |
|  |  |  |  |
| Project | I-80/Richards Blvd Interchange |  |  |
| Freeway | Westbound I-80 |  |  |
| Segment | Richards Blvd NB On to SB Off |  |  |
| Alternative | Existing Conditions |  |  |
| Time period | PM Peak Hour |  |  |
|  |  |  |  |
|  |  |  |  |

## Adjustment Factors

| Driver Population | Familiar |
| :--- | :---: |
| Weather Type | Non-severe |
| Incident Type | No incident |
| Capacity Adjustment Factor, CAF |  |
| Demand Adjustment Factor, DAF |  |


| Volume Data |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Frwy to Frwy | On to Frwy | Frwy to Off | Frwy to Off | vph |
| Volume, V | 4,084 | 452 | 69 | 0 |  |
| Peak-hour factor, PHF | 0.99 | 0.74 | 0.78 | 0.95 |  |
| Total Trucks | 9.0\% | 1.8\% | 0.5\% | 3.0\% |  |
| Terrain Type | Level | Level | Level | Level | mi |
| Grade |  |  |  |  |  |
| Length |  |  |  |  |  |
| SUT/TT Mix |  |  |  |  |  |
| Passenger Car Equivalent, $\mathrm{E}_{T}$ | 2.0 | 2.0 | 2.0 | 2.0 | pcph |
| Heavy Vehicle Adjustment, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 | 0.982 | 0.995 | 0.971 |  |
| Demand Adjustment Factor, DAF | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 4,497 | 622 | 89 | 0 |  |
| Weaving Flow Rate, vW | 711 | Total Flow Rate, v |  |  | 5,207 |
| Non-Weaving Flow Rate, vNW | 4,497 | Volume Ratio, VR |  |  | 0.136 |

## Freeway Weave Report

| Project | I-80/Richards Blvd Interchange |
| :--- | :--- |
| Freeway | Westbound I-80 |
| Segment | Richards Blvd NB On to SB Off |
| Alternative | Existing Conditions |
| Time period | PM Peak Hour |


|  | Capacity |  |
| :--- | :---: | :---: |
|  |  |  |
|  |  |  |
| Maximum Weaving Length, $\mathrm{L}_{\mathrm{MAX}}$ | 3,897 | ft |
| Weaving Length Check | OK |  |
| Freeway Maximum Capacity, $\mathrm{c}_{\mathrm{IFL}}$ | 2,400 | pchpl |
| Density-Based Capacity, $\mathrm{c}_{\mathrm{IWL}}$ | 9,340 | pchpl |
| Demand Flow-Based Capacity, $\mathrm{c}_{\mathrm{IW}}$ | 16,292 | pch |
| Weaving Segment Capacity, $\mathrm{c}_{\mathrm{w}}$ | 16,292 | vph |
| Adjusted Weaving Area Capacity, $\mathrm{c}_{\mathrm{wa}}$ | 16,292 | vph |
| Volume-to-Capacity Ratio, $\mathrm{v} / \mathrm{c}$ | 0.30 |  |


| Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |
| Minimum Lane Change Rate, $\mathrm{LC}_{\mathrm{MIN}}$ | 711 | $\mathrm{Ic} / \mathrm{h}$ |  |  |  |
| Weaving Lane Change Rate, $\mathrm{LC}_{\mathrm{W}}$ | 730 | $\mathrm{Ic} / \mathrm{h}$ |  |  |  |
| Non-weaving Vehicle Index, $\mathrm{I}_{\mathrm{NW}}$ | 187 |  |  |  |  |
| Non-weaving Lane Change Rate, $\mathrm{LC}_{\mathrm{NW}}$ | 427 | $\mathrm{Ic} / \mathrm{h}$ |  |  |  |
| Total Lane Change Rate, $\mathrm{LC}_{\mathrm{ALL}}$ | 1,157 | $\mathrm{Ic} / \mathrm{h}$ |  |  |  |
| Weaving Intensity Factor, W | 0.438 |  |  |  |  |
| Average Weaving Speed, $\mathrm{S}_{\mathrm{W}}$ | 53.3 | mph |  |  |  |
| Average Non-Weaving Speed, $\mathrm{S}_{\mathrm{NW}}$ | 58.7 | mph |  |  |  |
| Average Speed, S | 57.9 | mph |  |  |  |
| Density, D | 22.5 | pcpmpl |  |  |  |
| Level of Service, LOS | C |  |  |  |  |
|  |  |  |  |  |  |

## Capacity Checks

|  | Flow | Capacity |  | $\underline{\text { V/C Ratio }}$ |
| :--- | :---: | :---: | :---: | :---: |
| Entering General Purpose Lanes | 4,572 | 7,200 | pcph | 0.64 |
| Exiting General Purpose Lanes | 5,105 | 7,200 | pcph | 0.71 |
| On Ramp | 622 | 1,900 | pcph | 0.33 |
| Off Ramp | 89 | 1,900 | pcph | 0.05 |

## Leisch Method for Weaving Analysis

## Data Input

Number of Entering Mainline Lanes
Number of Lanes in Weaving Section Length of Weaving Section (feet)

| $\mathrm{N}_{\mathrm{b}}$ | 3 |
| :---: | :---: |
| N | 4 |
| L | 500 |

Mainline to Off-ramp ( $\mathrm{W}_{2}$ )

| 452 | Volume (vph)* |
| :---: | :--- |
| $1.8 \%$ | Truck Percentage |
| 2.0 | PCE for Trucks |
| 460 | Volume (pcph) |

Volume (pcph)


The LOS in the chart above refers to the capacity of weaving traffic only; through and ramp to ramp traffic is not included.

* Note: Do not adjust by a Peak Hour Factor (PHF). The methodology incorporates the PHF in the Service Volume tables.

Sources: Completion of Procedures for Analysis and Design of Traffic Weaving Sections, Jack E. Leisch \& Associates, September 1983 and Highway Design Manual , California Department of Transportation, 2014

|  | Freeway Basic Report |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Westbound I-80 |
| Segment | Richards Blvd SB Off to On |
| Alternative | Existing Conditions |
| Time Period | PM Peak Hour |


|  | General |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
|  | Purpose Lanes - Geometric Data |  |  |  |  |  |
| General Purpose Lanes, N | 3 | ln | Terrain Type | Level |  |  |
| Segment Length, L | 210 | ft | Percent Grade | - |  |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |  |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 1.83 | $\mathrm{ramps} / \mathrm{mi}$ |  |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 70.0 | mph |  |


| General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


|  | General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | ---: | :---: |
| Volume, V | 4,536 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |  |
| Peak Hour Factor, PHF | 0.99 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,665 | pcphpl |  |
| Total Trucks | $9.0 \%$ |  | Capacity, c | 2,400 | pcphpl |  |
| Single Unit/Tractor-Trailer Mix | - | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |  |  |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.69 |  |  |


| General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 70.0 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 67.5 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 24.7 | pcpmpl |
| Total Ramp Density Adjustment | 5.4 | mph | Level of Service, LOS | C |  |

$\qquad$


| Entering General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :--- | :---: | :--- | :--- | :--- | :--- |
| Volume, V | 4,536 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.99 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,665 | pcphpl |
| Total Trucks | $9.0 \%$ |  | Capacity, c | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |  |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.69 |  |


| Entering General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 70.4 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 67.8 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 24.6 | pcpmpl |
| Total Ramp Density Adjustment | 5.0 | mph | Level of Service, LOS | C |  |


| Segment General Purpose Lanes - Capacity, Speed, and Density |  |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
| General Purpose Lanes, N | 4 | $\ln$ | Average Speed, S | 70.2 | mph |  |
| Adjusted Capacity, cadj | 2,400 | pcphpl | Density, D | 18.8 | pcphpl |  |
| Flow Rate, vp | 1,321 | pcphpl | Level of Service, LOS | C |  |  |
| Volume-to-Capacity Ratio, v/c | 0.55 |  |  |  |  |  |

## Freeway Diverge Report

|  | Freeway Diverg |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Westbound I-80 |
| Segment | Lane Add to Old Davis Off |
| Alternative | Existing Conditions |
| Time Period | PM Peak Hour |


|  |  |  |  |
| :--- | :---: | :---: | :---: |
|  | Geometric Data |  |  |
|  |  |  |  |
| Number of Lanes, N | Freeway | Off Ramp |  |
| Free-Flow Speed, FFS | 4 | 1 |  |
| Segment Length, L Deceleration Length, LD | 70.0 | 45 | mph |
| Terrain Type | 1,190 | 150 | ft |
| Percent Grade | Level | Level |  |
| Grade Length | - | - | - |
| Segment Type / Ramp Type | - | Right | ft |

## Adjustment Factors

|  | $\frac{\text { Freeway }}{}$ | $\frac{\text { Off Ramp }}{}$ |
| :--- | :---: | :---: |
| Driver Population | Familiar | Familiar |
| Weather Type | Non-severe | Non-severe |
| Incident Type | No incident | No incident |
| Capacity Adjustment Factor, CAF | 1.00 | 1.00 |
| Demand Adjustment Factor, DAF | 1.00 | 1.00 |


|  | Volume Data |  |  |  |
| :--- | :---: | :---: | :---: | :---: |
|  |  |  |  |  |
| Junction Components | $\underline{\text { Freeway }}$ | $\underline{\text { Off Ramp }}$ |  |  |
| Volume, V | 4,798 | 155 | vph |  |
| Peak Hour Factor, PHF | 0.99 | 0.90 |  |  |
| Total Trucks | $9.0 \%$ | $1.9 \%$ |  |  |
| Single Unit/Tractor-Trailer Mix | - | - |  |  |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 | 2.0 |  |  |
| Heavy Vehicle Adjustment, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 | 0.981 |  |  |
| Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 5,283 | 175 | pcph |  |

Adjacent Ramp Meeting Criteria
Upstream Downstream

Type of Adjacent Ramp
Distance to Adjacent Ramp ft
Volume on Adjacent Ramp
pcph

## Freeway Diverge Report



|  | Freeway Basic Report |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Westbound I-80 |
| Segment | West of Old Davis Rd |
| Alternative | Existing Conditions |
| Time Period | PM Peak Hour |


|  | General |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
|  | Purpose Lanes - Geometric Data |  |  |  |  |  |
| General Purpose Lanes, N | 5 | ln | Terrain Type | Level |  |  |
| Segment Length, L | 1,350 | ft | Percent Grade | - |  |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |  |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 1.83 | $\mathrm{ramps} / \mathrm{mi}$ |  |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 70.0 | mph |  |


| General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


| General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Volume, V | 4,643 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.99 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,022 | pcphpl |
| Total Trucks | 9.0\% |  | Capacity, c | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - |  | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.43 |  |


| General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 70.0 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 70.0 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 14.6 | pcpmpl |
| Total Ramp Density Adjustment | 5.4 | mph | Level of Service, LOS | B |  |

$\qquad$

| Output Summary |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| General Information |  |  |  |  |  |  |  |  |
| Project description: Analyst: | I-80/Richards Blvd Interchange - Existing Conditions |  |  |  |  |  |  |  |
|  | DS | Date: | 1/20/2018 |  | Area type: |  | Urban |  |
| First year of analysis: | 2016 |  |  |  |  |  |  |  |
| Last year of analysis: | 2016 |  |  |  |  |  |  |  |
| Crash Data Description |  |  |  |  |  |  |  |  |
| Freeway segments | Segment crash data available? |  |  | No | First year of crash data: |  |  |  |
|  | Project-level crash data available? |  |  | No | Last year of crash data: |  |  |  |
| Ramp segments | Segment crash data available? |  |  | Yes | First year of crash data: |  |  | 2012 |
|  | Project-level crash data available? |  |  | No | Last year of crash data: |  |  | 2014 |
| Ramp terminals | Segment crash data available? |  |  | No | First year of crash data: |  |  |  |
|  | Project-level crash data available? |  |  | No | Last year of crash data: |  |  |  |
| Estimated Crash Statistics |  |  |  |  |  |  |  |  |
| Crashes for Entire Facility |  |  | Total | K | A | B | C | PDO |
| Estimated number of crashes during Study Period, crashes: |  |  | 4.0 | 0.0 | 0.1 | 0.6 | 0.8 | 2.4 |
| Estimated average crash freq. during Study Period, crashes/yr: |  |  | 4.0 | 0.0 | 0.1 | 0.6 | 0.8 | 2.4 |
| Crashes by Facility Component |  | Nbr. Sites | Total | K | A | B | C | PDO |
| Freeway segments, crashes: |  | 0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Ramp segments, crashes: |  | 5 | 4.0 | 0.0 | 0.1 | 0.6 | 0.8 | 2.4 |
|  |  | 0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Crashes for Entire Facility by Year |  | Year | Total | K | A | B | C | PDO |
| Estimated number of crashes during the Study Period, crashes: |  | 2016 | 4.0 | 0.0 | 0.1 | 0.6 | 0.8 | 2.4 |
|  |  | 2017 |  |  |  |  |  |  |
|  |  | 2018 |  |  |  |  |  |  |
|  |  | 2019 |  |  |  |  |  |  |
|  |  | 2020 |  |  |  |  |  |  |
|  |  | 2021 |  |  |  |  |  |  |
|  |  | 2022 |  |  |  |  |  |  |
|  |  | 2023 |  |  |  |  |  |  |
|  |  | 2024 |  |  |  |  |  |  |
|  |  | 2025 |  |  |  |  |  |  |
|  |  | 2026 |  |  |  |  |  |  |
|  |  | 2027 |  |  |  |  |  |  |
|  |  | 2028 |  |  |  |  |  |  |
|  |  | 2029 |  |  |  |  |  |  |
|  |  | 2030 |  |  |  |  |  |  |
|  |  | 2031 |  |  |  |  |  |  |
|  |  | 2032 |  |  |  |  |  |  |
|  |  | 2033 |  |  |  |  |  |  |
|  |  | 2034 |  |  |  |  |  |  |
|  |  | 2035 |  |  |  |  |  |  |
|  |  | 2036 |  |  |  |  |  |  |
|  |  | 2037 |  |  |  |  |  |  |
|  |  | 2038 |  |  |  |  |  |  |
|  |  | 2039 |  |  |  |  |  |  |
| Distribution of Crashes for Entire Facility |  |  |  |  |  |  |  |  |
| Crash Type | Crash Type Category |  | Estimated Number of Crashes During the Study Period |  |  |  |  |  |
|  |  |  | Total | K | A | B | C | PDO |
| Multiple vehicle | Head-on crashes: |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
|  | Right-angle crashes: |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
|  | Rear-end crashes: |  | 0.2 | 0.0 | 0.0 | 0.0 | 0.1 | 0.1 |
|  | Sideswipe crashes: |  | 0.1 | 0.0 | 0.0 | 0.0 | 0.0 | 0.1 |
|  | Other multiple-vehicle crashes: |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
|  | Total multiple-vehicle crashes: |  | 0.3 | 0.0 | 0.0 | 0.1 | 0.1 | 0.2 |
| Single vehicle | Crashes with animal: |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
|  | Crashes with fixed object: |  | 2.9 | 0.0 | 0.1 | 0.4 | 0.5 | 1.9 |
|  | Crashes with other object: |  | 0.1 | 0.0 | 0.0 | 0.0 | 0.0 | 0.1 |
|  | Crashes with parked vehicle: |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
|  | Other single-vehicle crashes |  | 0.6 | 0.0 | 0.0 | 0.1 | 0.2 | 0.3 |
|  | Total single-vehicle crashes: |  | 3.7 | 0.0 | 0.1 | 0.6 | 0.7 | 2.3 |
| Total crashes: |  |  | 4.0 | 0.0 | 0.1 | 0.6 | 0.8 | 2.4 |


|  |  | ance M | Conditions |
| :---: | :---: | :---: | :---: |
| Speed Bin |  |  | Vehicle Miles of Travel (VMT) |
| 1 | $>0$ | <=5 | 2,431 |
| 2 | >5 | <=10 | 40,862 |
| 3 | $>10$ | <=15 | 40,752 |
| 4 | $>15$ | <=20 | 74,656 |
| 5 | $>20$ | <=25 | 284,651 |
| 6 | $>25$ | <=30 | 152,480 |
| 7 | >30 | <=35 | 181,912 |
| 8 | $>35$ | < $=40$ | 71,359 |
| 9 | >40 | <=45 | 922,020 |
| 10 | $>45$ | <=50 | 435,359 |
| 11 | $>50$ | <=55 | 8,716 |
| 12 | $>55$ | < $=60$ | 145,630 |
| 13 | $>60$ | <=65 | 0 |
| 14 | $>65$ | < $=70$ | 0 |
| 15 | $>70$ | <=75 | 0 |
| 16 | $>75$ |  | 0 |
| Total |  |  | 2,360,828 |


| Speed Bin | Davis Model Wide Performance Measures-Cumulative No Build Conditions |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Congested Speed |  | Vehicle Miles of Travel (VMT) |  |  |  |  |
|  | $>0$ | $<=5$ | 21,666 |  |  |  |  |
| 2 | $>5$ | $<=10$ | 88,051 |  |  |  |  |
| 3 | $>10$ | $<=15$ | 75,900 |  |  |  |  |
| 4 | $>15$ | $<=20$ | 79,555 |  |  |  |  |
| 5 | $>20$ | $<=25$ | 419,018 |  |  |  |  |
| 6 | $>25$ | $<=30$ | 173,661 |  |  |  |  |
| 7 | $>30$ | $<=35$ | 157,139 |  |  |  |  |
| 8 | $>35$ | $<=40$ | 991,544 |  |  |  |  |
| 9 | $>40$ | $<=45$ | 330,834 |  |  |  |  |
| 10 | $>45$ | $<=50$ | 460,922 |  |  |  |  |
| 11 | $>50$ | $<=55$ | 11,078 |  |  |  |  |
| 12 | $>55$ | $<=60$ | 170,851 |  |  |  |  |
| 13 | $>60$ | $<=65$ | 0 |  |  |  |  |
| 14 | $>65$ | $<=70$ | 0 |  |  |  |  |
| 15 | $>70$ | $<=75$ | 0 |  |  |  |  |
| 16 | Total |  |  |  |  |  | 0 |
|  |  |  | $\mathbf{2 , 9 8 0 , 2 1 9}$ |  |  |  |  |


|  |  | Measu | uild Conditions |
| :---: | :---: | :---: | :---: |
| Speed Bin |  |  | Vehicle Miles of Travel (VMT) |
| 1 | >0 | <=5 | 17,036 |
| 2 | $>5$ | <=10 | 86,330 |
| 3 | $>10$ | <=15 | 77,488 |
| 4 | >15 | <=20 | 87,251 |
| 5 | $>20$ | < $=25$ | 408,957 |
| 6 | $>25$ | <=30 | 189,145 |
| 7 | >30 | <=35 | 156,430 |
| 8 | $>35$ | < $=40$ | 991,490 |
| 9 | >40 | <=45 | 312,856 |
| 10 | >45 | <=50 | 478,222 |
| 11 | $>50$ | < $=55$ | 11,179 |
| 12 | $>55$ | <=60 | 171,314 |
| 13 | >60 | <=65 | 0 |
| 14 | $>65$ | < $=70$ | 0 |
| 15 | $>70$ | <=75 | 0 |
| 16 | >75 |  | 0 |
| Total |  |  | 2,987,698 |

Vissim Post-Processor
I-80 / Richards Blvd Interchange
Average Results from 10 Runs Construction Year No Build Conditions
Volume and Delay by Movement
AM Peak Hour

Intersection 1
D St/First St
Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) |  | Total Delay (sec/veh) |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 10 | 10 | 98.0\% | 30.0 | 23.5 | C |
|  | Through | 20 | 17 | 85.5\% | 50.9 | 13.1 | D |
|  | Right Turn | 30 | 31 | 102.0\% | 7.0 | 3.3 | A |
|  | Subtotal | 60 | 58 | 95.8\% | 25.8 | 6.8 | C |
| SB | Left Turn | 40 | 39 | 98.5\% | 55.4 | 15.4 | E |
|  | Through | 30 | 27 | 91.3\% | 57.8 | 12.1 | E |
|  | Right Turn | 40 | 41 | 103.0\% | 17.6 | 6.3 | B |
|  | Subtotal | 110 | 108 | 98.2\% | 40.9 | 9.4 | D |
| EB | Left Turn | 10 | 8 | 81.0\% | 58.7 | 28.4 | E |
|  | Through | 260 | 273 | 104.8\% | 12.2 | 2.0 | B |
|  | Right Turn | 30 | 27 | 89.0\% | 9.8 | 6.1 | A |
|  | Subtotal | 300 | 307 | 102.5\% | 13.3 | 2.3 | B |
| WB | Left Turn | 30 | 26 | 86.3\% | 54.5 | 7.3 | D |
|  | Through | 470 | 463 | 98.4\% | 7.0 | 2.1 | A |
|  | Right Turn | 50 | 48 | 95.0\% | 5.3 | 5.1 | A |
|  | Subtotal | 550 | 536 | 97.5\% | 9.8 | 2.5 | A |
| Total |  | 1,020 | 1,009 | 98.9\% | 15.8 | 2.2 | B |

## Intersection 2 E St-Richards Blvd/First St Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) |  | Total Delay (sec/veh) |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 520 | 505 | 97.2\% | 22.7 | 3.3 | C |
|  | Through | 90 | 83 | 92.6\% | 26.0 | 5.1 | C |
|  | Right Turn | 250 | 238 | 95.1\% | 11.6 | 1.6 | B |
|  | Subtotal | 860 | 826 | 96.1\% | 19.6 | 2.5 | B |
| SB | Left Turn | 10 | 9 | 87.0\% | 68.1 | 31.4 | E |
|  | Through | 110 | 110 | 100.0\% | 48.6 | 10.4 | D |
|  | Right Turn | 10 | 10 | 95.0\% | 18.8 | 23.2 | B |
|  | Subtotal | 130 | 128 | 98.6\% | 47.2 | 8.7 | D |
| EB | Left Turn | 10 | 11 | 105.0\% | 59.7 | 33.6 | E |
|  | Through | 30 | 29 | 97.7\% | 56.1 | 18.3 | E |
|  | Right Turn | 290 | 302 | 104.0\% | 12.7 | 2.6 | B |
|  | Subtotal | 330 | 341 | 103.4\% | 18.8 | 3.8 | B |
| WB | Left Turn | 150 | 146 | 97.1\% | 80.6 | 15.2 | F |
|  | Through | 20 | 20 | 101.5\% | 64.4 | 21.1 | E |
|  | Right Turn | 10 | 11 | 114.0\% | 38.6 | 28.2 | D |
|  | Subtotal | 180 | 177 | 98.5\% | 76.9 | 13.7 | E |
| Total |  | 1,500 | 1,473 | 98.2\% | 29.5 | 3.1 | C |

Vissim Post-Processor
I-80 / Richards Blvd Interchange
Average Results from 10 Runs Construction Year No Build Conditions
Volume and Delay by Movement
AM Peak Hour

Intersection 3
Richards Blvd/Olive Dr
Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) |  | Total Delay (sec/veh) |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 160 | 154 | 96.5\% | 206.6 | 87.1 | F |
|  | Through | 650 | 628 | 96.6\% | 170.8 | 89.8 | F |
|  | Right Turn | 40 | 39 | 96.5\% | 133.8 | 87.4 | F |
|  | Subtotal | 850 | 821 | 96.6\% | 176.2 | 88.8 | F |
| SB | Left Turn | 30 | 29 | 97.7\% | 62.3 | 9.7 | E |
|  | Through | 480 | 483 | 100.6\% | 18.3 | 2.7 | B |
|  | Right Turn | 40 | 41 | 103.3\% | 16.4 | 5.6 | B |
|  | Subtotal | 550 | 554 | 100.7\% | 20.2 | 2.6 | C |
| EB | Left Turn | 40 | 38 | 94.8\% | 47.9 | 17.5 | D |
|  | Through | 10 | 10 | 104.0\% | 44.8 | 16.5 | D |
|  | Right Turn | 100 | 99 | 98.6\% | 28.4 | 9.7 | C |
|  | Subtotal | 150 | 147 | 97.9\% | 36.2 | 7.9 | D |
| WB | Left Turn | 120 | 121 | 100.8\% | 58.9 | 20.9 | E |
|  | Through | 40 | 40 | 100.8\% | 76.0 | 25.7 | E |
|  | Right Turn | 170 | 162 | 95.2\% | 70.4 | 22.2 | E |
|  | Subtotal | 330 | 323 | 97.9\% | 66.6 | 18.8 | E |
| Total |  | 1,880 | 1,845 | 98.1\% | 97.8 | 37.0 | F |


| Intersection 4 |  | I-80 WB Ramps/Richards Blvd |  |  | Uncontrolled |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Direction | Movement | Demand Volume (vph) | Served Volume (vph) |  | Total Delay (sec/veh) |  |  |
|  |  |  | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 60 | 57 | 95.2\% | 113.4 | 90.2 | F |
|  | Through | 400 | 400 | 99.9\% | 131.2 | 86.8 | F |
|  | Right Turn | 390 | 376 | 96.4\% | 13.2 | 23.7 | B |
|  | Subtotal | 850 | 833 | 97.9\% | 79.7 | 60.2 | F |
| SB | Left Turn |  |  |  |  |  |  |
|  | Through | 520 | 521 | 100.1\% | 1.5 | 0.2 | A |
|  | Right Turn | 190 | 189 | 99.3\% | 5.2 | 0.9 | A |
|  | Subtotal | 710 | 709 | 99.9\% | 2.5 | 0.3 | A |
| EB | Left Turn |  |  |  |  |  |  |
|  | Through |  |  |  |  |  |  |
|  | Right Turn | 200 | 197 | 98.4\% | 1.0 | 0.2 | A |
|  | Subtotal | 200 | 197 | 98.4\% | 1.0 | 0.2 | A |
| WB | Left Turn |  |  |  |  |  |  |
|  | Through |  |  |  |  |  |  |
|  | Right Turn | 450 | 426 | 94.6\% | 162.3 | 87.4 | F |
|  | Subtotal | 450 | 426 | 94.6\% | 162.3 | 87.4 | F |
| Total |  | 2,210 | 2,164 | 97.9\% | 62.0 | 33.3 | F |

Vissim Post-Processor
I-80 / Richards Blvd Interchange
Average Results from 10 Runs
Construction Year No Build Conditions
Volume and Delay by Movement
AM Peak Hour

Intersection 5
Richards Blvd/I-80 EB Ramps
Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) |  | Total Delay (sec/veh) |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn |  |  |  |  |  |  |
|  | Through | 640 | 638 | 99.7\% | 25.4 | 4.0 | C |
|  | Right Turn | 120 | 115 | 95.8\% | 20.4 | 4.6 | C |
|  | Subtotal | 760 | 753 | 99.1\% | 24.7 | 3.9 | C |
| SB | Left Turn | 260 | 259 | 99.5\% | 59.7 | 7.0 | E |
|  | Through | 460 | 458 | 99.6\% | 32.0 | 8.6 | C |
|  | Right Turn |  |  |  |  |  |  |
|  | Subtotal | 720 | 717 | 99.6\% | 42.0 | 6.4 | D |
| EB | Left Turn |  |  |  |  |  |  |
|  | Through |  |  |  |  |  |  |
|  | Right Turn |  |  |  |  |  |  |
|  | Subtotal |  |  |  |  |  |  |
| WB | Left Turn | 510 | 508 | 99.6\% | 63.8 | 26.8 | E |
|  | Through |  |  |  |  |  |  |
|  | Right Turn | 210 | 206 | 97.9\% | 33.5 | 20.0 | C |
|  | Subtotal | 720 | 714 | 99.1\% | 55.0 | 25.3 | D |
| Total |  | 2,200 | 2,183 | 99.2\% | 39.8 | 10.5 | D |


| Intersection 6 |  | Research Park Dr/Richards Blvd-Cowell Blvd |  |  |  |  | Signal |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Direction | Movement | Demand Volume (vph) | Served Volume (vph) |  | Total Delay (sec/veh) |  |  |
|  |  |  | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 70 | 68 | 97.3\% | 55.3 | 7.3 | E |
|  | Through | 10 | 10 | 100.0\% | 35.3 | 22.8 | D |
|  | Right Turn | 30 | 30 | 99.3\% | 11.2 | 9.7 | B |
|  | Subtotal | 110 | 108 | 98.1\% | 42.1 | 7.3 | D |
| SB | Left Turn | 20 | 24 | 120.5\% | 49.6 | 15.6 | D |
|  | Through | 20 | 19 | 94.0\% | 43.2 | 12.9 | D |
|  | Right Turn | 90 | 86 | 95.6\% | 13.8 | 5.0 | B |
|  | Subtotal | 130 | 129 | 99.2\% | 25.1 | 6.1 | C |
| EB | Left Turn | 250 | 252 | 100.7\% | 53.4 | 10.3 | D |
|  | Through | 580 | 572 | 98.6\% | 40.3 | 7.8 | D |
|  | Right Turn | 140 | 142 | 101.1\% | 29.6 | 7.1 | C |
|  | Subtotal | 970 | 965 | 99.5\% | 42.2 | 6.0 | D |
| WB | Left Turn | 30 | 31 | 103.3\% | 78.4 | 14.0 | E |
|  | Through | 580 | 586 | 101.1\% | 53.0 | 16.3 | D |
|  | Right Turn | 20 | 21 | 103.5\% | 26.4 | 18.4 | C |
|  | Subtotal | 630 | 638 | 101.3\% | 53.4 | 15.8 | D |
| Total |  | 1,840 | 1,840 | 100.0\% | 44.8 | 8.5 | D |

Vissim Post-Processor
I-80 / Richards Blvd Interchange
Average Results from 10 Runs Construction Year No Build Conditions
Volume and Delay by Movement
PM Peak Hour

Intersection 1
D St/First St
Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) |  | Total Delay (sec/veh) |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 30 | 30 | 100.7\% | 47.2 | 15.5 | D |
|  | Through | 40 | 40 | 99.5\% | 58.9 | 14.0 | E |
|  | Right Turn | 50 | 50 | 100.0\% | 16.3 | 4.3 | B |
|  | Subtotal | 120 | 120 | 100.0\% | 39.5 | 7.9 | D |
| SB | Left Turn | 70 | 69 | 98.1\% | 61.9 | 13.2 | E |
|  | Through | 40 | 40 | 100.5\% | 56.0 | 13.5 | E |
|  | Right Turn | 20 | 20 | 98.0\% | 12.9 | 5.1 | B |
|  | Subtotal | 130 | 129 | 98.8\% | 53.0 | 8.4 | D |
| EB | Left Turn | 10 | 10 | 95.0\% | 88.4 | 24.3 | F |
|  | Through | 360 | 369 | 102.5\% | 33.4 | 6.2 | C |
|  | Right Turn | 60 | 56 | 92.7\% | 29.3 | 7.8 | C |
|  | Subtotal | 430 | 434 | 101.0\% | 34.3 | 6.1 | C |
| WB | Left Turn | 70 | 68 | 97.0\% | 58.3 | 5.6 | E |
|  | Through | 310 | 316 | 101.9\% | 7.5 | 1.4 | A |
|  | Right Turn | 50 | 50 | 100.2\% | 2.7 | 1.6 | A |
|  | Subtotal | 430 | 434 | 100.9\% | 14.9 | 2.5 | B |
| Total |  | 1,110 | 1,117 | 100.6\% | 29.4 | 2.7 | C |

## Intersection 2 E St-Richards Blvd/First St Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) |  | Total Delay (sec/veh) |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 360 | 363 | 100.9\% | 14.1 | 4.8 | B |
|  | Through | 140 | 131 | 93.7\% | 18.6 | 6.8 | B |
|  | Right Turn | 320 | 305 | 95.4\% | 8.1 | 2.5 | A |
|  | Subtotal | 820 | 800 | 97.5\% | 12.5 | 3.8 | B |
| SB | Left Turn | 10 | 8 | 80.0\% | 36.7 | 35.5 | D |
|  | Through | 160 | 158 | 98.9\% | 52.6 | 6.2 | D |
|  | Right Turn | 20 | 21 | 103.0\% | 21.3 | 10.5 | C |
|  | Subtotal | 190 | 187 | 98.3\% | 48.2 | 5.5 | D |
| EB | Left Turn | 10 | 10 | 95.0\% | 58.7 | 44.6 | E |
|  | Through | 50 | 55 | 110.2\% | 73.0 | 15.5 | E |
|  | Right Turn | 420 | 425 | 101.1\% | 12.5 | 3.6 | B |
|  | Subtotal | 480 | 489 | 101.9\% | 19.9 | 6.3 | B |
| WB | Left Turn | 200 | 197 | 98.7\% | 109.7 | 37.6 | F |
|  | Through | 50 | 50 | 100.0\% | 70.0 | 23.4 | E |
|  | Right Turn | 10 | 10 | 100.0\% | 36.2 | 32.1 | D |
|  | Subtotal | 260 | 257 | 99.0\% | 99.6 | 35.9 | F |
| Total |  | 1,750 | 1,733 | 99.0\% | 31.8 | 6.3 | C |

Vissim Post-Processor
Average Results from 10 Runs
I-80 / Richards Blvd Interchange

Volume and Delay by Movement

## Construction Year No Build Conditions

Intersection 3
Richards Blvd/Olive Dr
Signal

| Direction | Movement | Demand <br> Volume (vph) | Served Volume (vph) |  | Total Delay (sec/veh) |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 100 | 96 | 95.6\% | 92.5 | 26.0 | F |
|  | Through | 630 | 616 | 97.8\% | 38.6 | 16.8 | D |
|  | Right Turn | 80 | 77 | 95.9\% | 19.1 | 13.7 | B |
|  | Subtotal | 810 | 788 | 97.3\% | 43.4 | 17.8 | D |
| SB | Left Turn | 90 | 90 | 100.1\% | 53.1 | 10.9 | D |
|  | Through | 640 | 642 | 100.3\% | 23.3 | 5.8 | C |
|  | Right Turn | 50 | 48 | 96.2\% | 22.5 | 6.4 | C |
|  | Subtotal | 780 | 780 | 100.1\% | 26.9 | 6.5 | C |
| EB | Left Turn | 50 | 49 | 97.8\% | 305.7 | 132.6 | F |
|  | Through | 20 | 21 | 103.0\% | 304.6 | 131.6 | F |
|  | Right Turn | 170 | 171 | 100.6\% | 291.0 | 136.6 | F |
|  | Subtotal | 240 | 241 | 100.3\% | 294.9 | 135.2 | F |
| WB | Left Turn | 140 | 139 | 99.1\% | 96.6 | 59.4 | F |
|  | Through | 30 | 30 | 98.7\% | 46.8 | 17.7 | D |
|  | Right Turn | 140 | 137 | 97.9\% | 32.4 | 19.0 | C |
|  | Subtotal | 310 | 305 | 98.5\% | 65.7 | 44.7 | E |
| Total |  | 2,140 | 2,115 | 98.8\% | 68.3 | 18.8 | E |


| Intersection 4 <br> Direction | 4 Movement | I-80 WB Ramps/Richards Blvd |  |  | Uncontrolled |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Demand | Served V | me (vph) |  | elay (sec/v |  |
|  |  | Volume (vph) | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 30 | 30 | 98.3\% | 9.6 | 9.6 | A |
|  | Through | 570 | 552 | 96.8\% | 12.8 | 11.0 | B |
|  | Right Turn | 560 | 555 | 99.1\% | 3.5 | 0.7 | A |
|  | Subtotal | 1,160 | 1,136 | 97.9\% | 8.3 | 5.5 | A |
| SB | Left Turn |  |  |  |  |  |  |
|  | Through | 660 | 658 | 99.7\% | 1.8 | 0.3 | A |
|  | Right Turn | 310 | 313 | 101.0\% | 4.7 | 0.8 | A |
|  | Subtotal | 970 | 971 | 100.1\% | 2.7 | 0.4 | A |
| EB | Left Turn |  |  |  |  |  |  |
|  | Through |  |  |  |  |  |  |
|  | Right Turn | 100 | 98 | 97.8\% | 0.9 | 0.3 | A |
|  | Subtotal | 100 | 98 | 97.8\% | 0.9 | 0.3 | A |
| WB | Left Turn |  |  |  |  |  |  |
|  | Through |  |  |  |  |  |  |
|  | Right Turn | 240 | 241 | 100.5\% | 2.5 | 2.8 | A |
|  | Subtotal | 240 | 241 | 100.5\% | 2.5 | 2.8 | A |
| Total |  | 2,470 | 2,446 | 99.0\% | 5.1 | 2.7 | A |

Vissim Post-Processor
I-80 / Richards Blvd Interchange
Average Results from 10 Runs
Construction Year No Build Conditions
Volume and Delay by Movement
PM Peak Hour

Intersection 5
Richards Blvd/I-80 EB Ramps
Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) |  | Total Delay (sec/veh) |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn |  |  |  |  |  |  |
|  | Through | 930 | 932 | 100.2\% | 16.5 | 3.0 | B |
|  | Right Turn | 120 | 118 | 98.0\% | 10.6 | 2.9 | B |
|  | Subtotal | 1,050 | 1,050 | 100.0\% | 15.8 | 2.8 | B |
| SB | Left Turn | 210 | 219 | 104.2\% | 50.6 | 3.4 | D |
|  | Through | 550 | 536 | 97.5\% | 21.8 | 3.3 | C |
|  | Right Turn |  |  |  |  |  |  |
|  | Subtotal | 760 | 755 | 99.3\% | 29.8 | 2.1 | C |
| EB | Left Turn |  |  |  |  |  |  |
|  | Through |  |  |  |  |  |  |
|  | Right Turn |  |  |  |  |  |  |
|  | Subtotal |  |  |  |  |  |  |
| WB | Left Turn | 570 | 522 | 91.5\% | 327.7 | 52.1 | F |
|  | Through |  |  |  |  |  |  |
|  | Right Turn | 230 | 206 | 89.7\% | 291.6 | 46.7 | F |
|  | Subtotal | 800 | 728 | 91.0\% | 317.6 | 50.1 | F |
| Total |  | 2,610 | 2,533 | 97.0\% | 106.2 | 12.2 | F |



Vissim Post-Processor
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Average Results from 10 Runs
Construction Year Build Conditions
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AM Peak Hour

| Intersection |  | D St/First St |  |  |  |  | Signal |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Demand | Served V | me (vph) |  | elay (sec/v |  |
| Direction | Movement | Volume (vph) | Average | Percent | Average | Std. Dev. | LOS |
|  | Left Turn | 10 | 9 | 94.0\% | 34.0 | 29.1 | C |
| NB | Through | 20 | 19 | 96.0\% | 45.9 | 20.3 | D |
| NB | Right Turn | 30 | 29 | 96.7\% | 5.2 | 1.8 | A |
|  | Subtotal | 60 | 58 | 96.0\% | 27.7 | 10.2 | C |
|  | Left Turn | 40 | 41 | 101.5\% | 60.3 | 9.0 | E |
| SB | Through | 30 | 28 | 94.7\% | 55.8 | 13.8 | E |
| SB | Right Turn | 40 | 38 | 93.8\% | 18.3 | 10.0 | B |
|  | Subtotal | 110 | 107 | 96.8\% | 43.3 | 7.2 | D |
|  | Left Turn | 10 | 10 | 96.0\% | 50.2 | 29.7 | D |
| EB | Through | 260 | 266 | 102.2\% | 12.2 | 2.3 | B |
| EB | Right Turn | 30 | 30 | 99.0\% | 7.7 | 3.6 | A |
|  | Subtotal | 300 | 305 | 101.6\% | 13.3 | 2.4 | B |
|  | Left Turn | 30 | 27 | 89.3\% | 71.4 | 6.7 | E |
| WB | Through | 470 | 482 | 102.6\% | 1.2 | 0.4 | A |
|  | Right Turn | 50 | 50 | 99.0\% | 1.5 | 0.8 | A |
|  | Subtotal | 550 | 559 | 101.6\% | 5.5 | 2.1 | A |
|  | Total | 1,020 | 1,028 | 100.8\% | 12.8 | 1.8 | B |

Intersection 2 E St-Richards Blvd/First St Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) |  | Total Delay (sec/veh) |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 520 | 527 | 101.4\% | 9.6 | 2.1 | A |
|  | Through | 90 | 92 | 102.2\% | 12.7 | 7.1 | B |
|  | Right Turn | 250 | 254 | 101.8\% | 3.0 | 1.0 | A |
|  | Subtotal | 860 | 874 | 101.6\% | 8.0 | 2.1 | A |
| SB | Left Turn | 10 | 9 | 89.0\% | 56.6 | 17.5 | E |
|  | Through | 110 | 108 | 97.7\% | 46.5 | 8.1 | D |
|  | Right Turn | 10 | 12 | 119.0\% | 26.2 | 25.2 | C |
|  | Subtotal | 130 | 128 | 98.7\% | 45.2 | 7.6 | D |
| EB | Left Turn | 10 | 9 | 88.0\% | 63.6 | 34.4 | E |
|  | Through | 30 | 30 | 98.3\% | 67.5 | 14.3 | E |
|  | Right Turn | 290 | 296 | 102.0\% | 11.0 | 1.6 | B |
|  | Subtotal | 330 | 334 | 101.2\% | 18.6 | 2.4 | B |
| WB | Left Turn | 150 | 148 | 98.5\% | 51.0 | 6.8 | D |
|  | Through | 20 | 20 | 100.5\% | 55.5 | 12.9 | E |
|  | Right Turn | 10 | 9 | 90.0\% | 18.7 | 16.6 | B |
|  | Subtotal | 180 | 177 | 98.3\% | 49.7 | 7.5 | D |
| Total |  | 1,500 | 1,513 | 100.8\% | 18.3 | 2.2 | B |

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Construction Year Build Conditions
Volume and Delay by Movement
AM Peak Hour

| Intersection 3 |  | Richards Blvd/Olive Dr |  |  |  |  | Signal |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Direction | Movement | Demand Volume (vph) | Served Volume (vph) |  | Total Delay (sec/veh) |  |  |
|  |  |  | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 280 | 280 | 99.8\% | 78.1 | 11.0 | E |
|  | Through | 760 | 765 | 100.7\% | 25.4 | 3.0 | C |
|  | Right Turn | 110 | 97 | 87.9\% | 6.1 | 2.2 | A |
|  | Subtotal | 1,150 | 1,142 | 99.3\% | 36.4 | 4.5 | D |
| SB | Left Turn | 30 | 29 | 97.3\% | 69.2 | 17.8 | E |
|  | Through | 480 | 481 | 100.2\% | 35.1 | 6.2 | D |
|  | Right Turn | 40 | 38 | 95.5\% | 32.4 | 7.9 | C |
|  | Subtotal | 550 | 549 | 99.7\% | 36.5 | 6.1 | D |
| EB | Left Turn | 40 | 41 | 102.3\% | 52.0 | 9.7 | D |
|  | Through | 10 | 9 | 91.0\% | 41.4 | 28.9 | D |
|  | Right Turn | 100 | 97 | 97.4\% | 12.6 | 3.8 | B |
|  | Subtotal | 150 | 147 | 98.3\% | 26.7 | 5.5 | C |
| WB | Left Turn | 120 | 117 | 97.8\% | 48.0 | 7.5 | D |
|  | Through | 30 | 25 | 84.0\% | 78.6 | 21.5 | E |
|  | Right Turn | 60 | 67 | 111.0\% | 72.9 | 19.8 | E |
|  | Subtotal | 210 | 209 | 99.6\% | 59.1 | 11.6 | E |
| Total |  | 2,060 | 2,047 | 99.3\% | 38.3 | 3.9 | D |


| Intersection 4 |  | Richards Blvd/I-80 WB Ramps |  |  |  |  | Signal |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Direction | Movement | Demand Volume (vph) | Served Volume (vph) |  | Total Delay (sec/veh) |  |  |
|  |  |  | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 390 | 393 | 100.6\% | 50.7 | 2.7 | D |
|  | Through Right Turn | 460 | 463 | 100.6\% | 36.3 | 3.5 | D |
|  | Subtotal | 850 | 855 | 100.6\% | 42.8 | 2.9 | D |
| SB | Left Turn |  |  |  |  |  |  |
|  | Through | 520 | 516 | 99.2\% | 12.8 | 3.2 | B |
|  | Right Turn | 190 | 188 | 98.7\% | 6.8 | 1.8 | A |
|  | Subtotal | 710 | 704 | 99.1\% | 11.2 | 2.4 | B |
| EB | Left Turn <br> Through <br> Right Turn |  |  |  |  |  |  |
|  | Subtotal |  |  |  |  |  |  |
| WB | Left Turn <br> Through | 200 | 199 | 99.5\% | 51.6 | 6.9 | D |
|  | Right Turn | 690 | 685 | 99.3\% | 42.6 | 15.1 | D |
|  | Subtotal | 890 | 884 | 99.3\% | 44.9 | 11.8 | D |
| Total |  | 2,450 | 2,443 | 99.7\% | 34.9 | 3.8 | C |

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Vissim Post-Processor
I-80 / Richards Blvd Interchange
Average Results from 10 Runs
Construction Year Build Conditions
Volume and Delay by Movement
PM Peak Hour

| Intersection 1 |  | D St/First St |  |  |  |  | Signal |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Movement | Demand Volume (vph) | Served Volume (vph) |  | Total Delay (sec/veh) |  |  |
| Direction |  |  | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 30 | 30 | 100.7\% | 54.0 | 14.3 | D |
|  | Through | 40 | 38 | 95.3\% | 56.7 | 18.1 | E |
|  | Right Turn | 50 | 49 | 98.8\% | 21.1 | 5.2 | C |
|  | Subtotal | 120 | 118 | 98.1\% | 42.5 | 10.1 | D |
| SB | Left Turn | 70 | 68 | 97.3\% | 72.0 | 19.0 | E |
|  | Through | 40 | 42 | 105.0\% | 65.4 | 13.4 | E |
|  | Right Turn | 20 | 19 | 95.0\% | 25.0 | 10.9 | C |
|  | Subtotal | 130 | 129 | 99.3\% | 63.1 | 16.3 | E |
| EB | Left Turn | 10 | 11 | 109.0\% | 67.1 | 24.0 | E |
|  | Through | 360 | 368 | 102.1\% | 48.2 | 28.5 | D |
|  | Right Turn | 60 | 57 | 94.5\% | 40.2 | 24.5 | D |
|  | Subtotal | 430 | 435 | 101.2\% | 47.5 | 27.1 | D |
| WB | Left Turn | 70 | 71 | 101.1\% | 54.9 | 4.7 | D |
|  | Through | 310 | 316 | 101.8\% | 6.9 | 0.8 | A |
|  | Right Turn | 50 | 48 | 95.2\% | 3.2 | 1.7 | A |
|  | Subtotal | 430 | 434 | 100.9\% | 15.1 | 1.9 | B |
| Total |  | 1,110 | 1,116 | 100.5\% | 36.2 | 11.3 | D |

Intersection 2 E St-Richards Blvd/First St Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) |  | Total Delay (sec/veh) |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 360 | 361 | 100.3\% | 9.3 | 2.8 | A |
|  | Through | 140 | 135 | 96.7\% | 7.9 | 3.5 | A |
|  | Right Turn | 320 | 313 | 97.7\% | 3.5 | 0.8 | A |
|  | Subtotal | 820 | 809 | 98.7\% | 6.7 | 1.9 | A |
| SB | Left Turn | 10 | 10 | 102.0\% | 65.0 | 29.7 | E |
|  | Through | 160 | 156 | 97.8\% | 57.1 | 15.7 | E |
|  | Right Turn | 20 | 20 | 98.0\% | 40.1 | 14.3 | D |
|  | Subtotal | 190 | 186 | 98.0\% | 56.4 | 15.5 | E |
| EB | Left Turn | 10 | 10 | 100.0\% | 80.7 | 22.0 | F |
|  | Through | 50 | 54 | 107.6\% | 79.9 | 16.9 | E |
|  | Right Turn | 420 | 421 | 100.3\% | 21.2 | 8.9 | C |
|  | Subtotal | 480 | 485 | 101.0\% | 29.1 | 8.0 | C |
| WB | Left Turn | 200 | 194 | 97.0\% | 53.0 | 6.3 | D |
|  | Through | 50 | 53 | 106.8\% | 46.3 | 10.1 | D |
|  | Right Turn | 10 | 9 | 92.0\% | 23.1 | 15.1 | C |
|  | Subtotal | 260 | 257 | 98.7\% | 50.5 | 4.4 | D |
| Total |  | 1,750 | 1,737 | 99.2\% | 25.6 | 3.7 | C |

Vissim Post-Processor
I-80 / Richards Blvd Interchange
Average Results from 10 Runs
Construction Year Build Conditions
Volume and Delay by Movement
PM Peak Hour

| Intersection 3 |  | Richards Blvd/Olive Dr |  |  |  |  | Signal |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Direction | Movement | Demand | Served V | me (vph) |  | elay (sec/v |  |
|  |  | Volume (vph) | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 130 | 183 | 140.7\% | 77.5 | 6.4 | E |
|  | Through | 630 | 621 | 98.5\% | 25.6 | 3.0 | C |
|  | Right Turn | 210 | 207 | 98.6\% | 5.2 | 0.9 | A |
|  | Subtotal | 970 | 1,011 | 104.2\% | 30.2 | 2.8 | C |
| SB | Left Turn | 90 | 91 | 101.6\% | 70.0 | 10.4 | E |
|  | Through | 640 | 634 | 99.0\% | 39.5 | 12.9 | D |
|  | Right Turn | 50 | 48 | 96.2\% | 43.3 | 13.1 | D |
|  | Subtotal | 780 | 773 | 99.1\% | 43.8 | 12.2 | D |
| EB | Left Turn | 50 | 49 | 97.2\% | 66.5 | 17.0 | E |
|  | Through | 20 | 20 | 102.0\% | 66.7 | 28.4 | E |
|  | Right Turn | 170 | 170 | 99.7\% | 34.3 | 8.2 | C |
|  | Subtotal | 240 | 239 | 99.4\% | 42.6 | 10.9 | D |
| WB | Left Turn | 140 | 137 | 97.9\% | 97.2 | 60.5 | F |
|  | Through | 30 | 28 | 92.7\% | 168.5 | 84.6 | F |
|  | Right Turn | 140 | 141 | 100.5\% | 161.0 | 81.3 | F |
|  | Subtotal | 310 | 306 | 98.5\% | 133.7 | 70.5 | F |
| Total |  | 2,300 | 2,328 | 101.2\% | 52.2 | 14.7 | D |

Intersection 4 Richards Blvd/I-80 WB Ramps Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) |  | Total Delay (sec/veh) |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 560 | 521 | 93.1\% | 60.3 | 3.1 | E |
|  | Through Right Turn | 600 | 643 | 107.1\% | 5.7 | 1.8 | A |
|  | Subtotal | 1,160 | 1,164 | 100.3\% | 31.8 | 1.7 | C |
| SB | Left Turn |  |  |  |  |  |  |
|  | Through | 660 | 664 | 100.5\% | 9.5 | 1.6 | A |
|  | Right Turn | 310 | 294 | 94.7\% | 7.4 | 1.2 | A |
|  | Subtotal | 970 | 957 | 98.7\% | 8.9 | 1.3 | A |
| EB | Left Turn |  |  |  |  |  |  |
|  | Through |  |  |  |  |  |  |
|  | Right Turn |  |  |  |  |  |  |
|  | Subtotal |  |  |  |  |  |  |
| WB | Left Turn | 100 | 99 | 98.7\% | 47.7 | 7.5 | D |
|  | Through |  |  |  |  |  |  |
|  | Right Turn | 370 | 368 | 99.5\% | 20.9 | 4.5 | C |
|  | Subtotal | 470 | 467 | 99.3\% | 26.9 | 3.8 | C |
| Total |  | 2,600 | 2,588 | 99.5\% | 22.5 | 1.0 | C |

Vissim Post-Processor
I-80 / Richards Blvd Interchange
Average Results from 10 Runs
Construction Year Build Conditions
Volume and Delay by Movement
PM Peak Hour

Intersection 6 Research Park Dr/Richards Blvd-Cowell Blvd Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) |  | Total Delay (sec/veh) |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 130 | 128 | 98.2\% | 51.2 | 5.7 | D |
|  | Through | 40 | 40 | 101.0\% | 37.0 | 13.8 | D |
|  | Right Turn | 60 | 59 | 98.8\% | 13.1 | 7.2 | B |
|  | Subtotal | 230 | 227 | 98.8\% | 39.1 | 4.3 | D |
| SB | Left Turn | 40 | 44 | 109.8\% | 54.0 | 11.8 | D |
|  | Through | 10 | 11 | 108.0\% | 38.7 | 20.9 | D |
|  | Right Turn | 190 | 186 | 98.1\% | 13.8 | 4.7 | B |
|  | Subtotal | 240 | 241 | 100.5\% | 22.2 | 4.9 | C |
| EB | Left Turn | 320 | 302 | 94.5\% | 54.2 | 5.3 | D |
|  | Through | 740 | 749 | 101.2\% | 11.0 | 4.0 | B |
|  | Right Turn | 60 | 58 | 96.3\% | 6.0 | 3.8 | A |
|  | Subtotal | 1,120 | 1,109 | 99.0\% | 22.7 | 2.8 | C |
| WB | Left Turn | 20 | 18 | 90.0\% | 59.2 | 8.3 | E |
|  | Through | 680 | 692 | 101.8\% | 40.4 | 5.9 | D |
|  | Right Turn | 40 | 34 | 85.8\% | 22.3 | 12.2 | C |
|  | Subtotal | 740 | 744 | 100.6\% | 40.1 | 5.7 | D |
| Total |  | 2,330 | 2,322 | 99.6\% | 29.9 | 1.8 | C |

Vissim Post-Processor
Average Results from 10 Runs
Queue Length

I-80 / Richards Blvd Interchange
Construction Year Build Conditions
AM Peak Hour

Signal

D St/First St

| Direction | Movement | Storage <br> (ft) | Average Queue (ft) |  |  |  | Maximum Queue (ft) |  |  |  | Exceeds <br> Storage? |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Average | Std. Dev. | Minimum | Maximum | Average | Std. Dev. | Minimum | Maximum |  |
| NB | U Turn |  |  |  |  |  |  |  |  |  |  |
|  | Second Left |  |  |  |  |  |  |  |  |  |  |
|  | Left Turn | 100 | 8 | 2 | 5 | 12 | 48 | 9 | 41 | 71 | No |
|  | Through | 100 | 8 | 2 | 5 | 12 | 48 | 9 | 41 | 71 | NO |
|  | Right Turn | 400 | 1 | 0 | 0 | 1 | 32 | 6 | 24 | 42 | NO |
|  | Second Right |  |  |  |  |  |  |  |  |  |  |
| SB | U Turn |  |  |  |  |  |  |  |  |  |  |
|  | Second Left |  |  |  |  |  |  |  |  |  |  |
|  | Left Turn | 400 | 22 | 3 | 18 | 28 | 129 | 23 | 101 | 179 | NO |
|  | Through | 400 | 22 | 3 | 18 | 28 | 129 | 23 | 101 | 179 | NO |
|  | Right Turn | 400 | 2 | 1 | 1 | 5 | 92 | 32 | 57 | 159 | NO |
|  | Second Right |  |  |  |  |  |  |  |  |  |  |
| EB | U Turn |  |  |  |  |  |  |  |  |  |  |
|  | Second Left |  |  |  |  |  |  |  |  |  |  |
|  | Left Turn | 75 | 3 | 1 | 1 | 5 | 24 | 6 | 15 | 34 | NO |
|  | Through | 250 | 8 | 2 | 6 | 12 | 127 | 19 | 100 | 163 | NO |
|  | Right Turn | 250 | 9 | 2 | 6 | 13 | 130 | 19 | 103 | 166 | NO |
|  | Second Right |  |  |  |  |  |  |  |  |  |  |
| WB | U Turn |  |  |  |  |  |  |  |  |  |  |
|  | Second Left |  |  |  |  |  |  |  |  |  |  |
|  | Left Turn | 100 | 0 | 0 | 0 | 0 | 4 | 5 | 0 | 14 | NO |
|  | Through | 225 | 0 | 0 | 0 | 0 | 4 | 5 | 0 | 14 | NO |
|  | Right Turn | 225 | 0 | 0 | 0 | 0 | 4 | 5 | 0 | 14 | NO |
|  | Second Right |  |  |  |  |  |  |  |  |  |  |

Vissim Post-Processor
Average Results from 10 Runs
Queue Length
I-80 / Richards Blvd Interchange
Construction Year Build Conditions
AM Peak Hour

Intersection 2
E St-Richards Blvd/First St
Signal

| Direction | Movement | Storage | Average Queue (ft) |  |  |  | Maximum Queue (ft) |  |  |  | Exceeds Storage? |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | (ft) | Average | Std. Dev. | Minimum | Maximum | Average | Std. Dev. | Minimum | Maximum |  |
| NB | U Turn |  |  |  |  |  |  |  |  |  |  |
|  | Second Left |  |  |  |  |  |  |  |  |  |  |
|  | Left Turn | 625 | 34 | 7 | 20 | 42 | 411 | 116 | 181 | 539 | NO |
|  | Through | 625 | 34 | 7 | 20 | 42 | 411 | 116 | 181 | 539 | NO |
|  | Right Turn | 180 | 0 | 0 | 0 | 0 | 12 | 11 | 0 | 31 | NO |
|  | Second Right |  |  |  |  |  |  |  |  |  |  |
| SB | U Turn |  |  |  |  |  |  |  |  |  |  |
|  | Second Left |  |  |  |  |  |  |  |  |  |  |
|  | Left Turn | 400 | 31 | 4 | 26 | 40 | 142 | 20 | 118 | 173 | NO |
|  | Through | 400 | 31 | 4 | 26 | 40 | 142 | 20 | 118 | 173 | NO |
|  | Right Turn | 400 | 5 | 2 | 1 | 8 | 85 | 31 | 41 | 141 | NO |
|  | Second Right |  |  |  |  |  |  |  |  |  |  |
| EB | U Turn |  |  |  |  |  |  |  |  |  |  |
|  | Second Left |  |  |  |  |  |  |  |  |  |  |
|  | Left Turn | 100 | 16 | 3 | 12 | 22 | 73 | 11 | 58 | 93 | NO |
|  | Through | 225 | 16 | 3 | 12 | 22 | 73 | 11 | 58 | 93 | NO |
|  | Right Turn | 225 | 21 | 3 | 16 | 28 | 193 | 29 | 140 | 235 | NO |
|  | Second Right |  |  |  |  |  |  |  |  |  |  |
| WB | U Turn |  |  |  |  |  |  |  |  |  |  |
|  | Second Left |  |  |  |  |  |  |  |  |  |  |
|  | Left Turn | 225 | 40 | 4 | 33 | 47 | 172 | 18 | 146 | 205 | NO |
|  |  |  |  |  |  |  |  |  |  |  |  |
|  | Through | 225 | 40 | 4 | 33 | 47 | 172 | 18 | 146 | 205 | NO |
|  | Right Turn | 225 | 40 | 4 | 33 | 47 | 172 | 18 | 146 | 205 | NO |
|  | Second Right |  |  |  |  |  |  |  |  |  |  |

Vissim Post-Processor
Average Results from 10 Runs
Queue Length

I-80 / Richards Blvd Interchange
Construction Year Build Conditions
AM Peak Hour

## Intersection 3 Richards Blvd/Olive Dr

Signal

| Direction | Movement | Storage <br> (ft) | Average Queue (ft) |  |  |  | Maximum Queue (ft) |  |  |  | Exceeds <br> Storage? |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Average | Std. Dev. | Minimum | Maximum | Average | Std. Dev. | Minimum | Maximum |  |
| NB | U Turn |  |  |  |  |  |  |  |  |  |  |
|  | Second Left |  |  |  |  |  |  |  |  |  |  |
|  | Left Turn | 175 | 125 | 10 | 113 | 143 | 524 | 48 | 408 | 580 | MAX |
|  | Through | 600 | 116 | 11 | 96 | 137 | 541 | 35 | 464 | 578 | NO |
|  | Right Turn | 275 | 0 | 0 | 0 | 0 | 20 | 9 | 7 | 39 | NO |
|  | Second Right |  |  |  |  |  |  |  |  |  |  |
| SB | U Turn |  |  |  |  |  |  |  |  |  |  |
|  | Second Left |  |  |  |  |  |  |  |  |  |  |
|  | Left Turn | 625 | 9 | 2 | 5 | 12 | 56 | 10 | 46 | 81 | NO |
|  | Through | 625 | 81 | 14 | 66 | 112 | 475 | 44 | 419 | 546 | NO |
|  | Right Turn | 625 | 78 | 14 | 63 | 110 | 473 | 44 | 417 | 545 | NO |
|  | Second Right |  |  |  |  |  |  |  |  |  |  |
| EB | U Turn |  |  |  |  |  |  |  |  |  |  |
|  | Second Left |  |  |  |  |  |  |  |  |  |  |
|  | Left Turn | 250 | 15 | 3 | 11 | 21 | 119 | 25 | 75 | 159 | NO |
|  | Through | 600 | 15 | 3 | 11 | 21 | 119 | 25 | 75 | 159 | NO |
|  | Right Turn | 250 | 5 | 2 | 2 | 9 | 99 | 31 | 50 | 149 | NO |
|  | Second Right |  |  |  |  |  |  |  |  |  |  |
| WB | U Turn |  |  |  |  |  |  |  |  |  |  |
|  | Second Left |  |  |  |  |  |  |  |  |  |  |
|  | Left Turn | 200 | 1 | 1 | 0 | 2 | 36 | 19 | 6 | 69 | NO |
|  | Through | 1,500 | 1 | 1 | 0 | 2 | 36 | 19 | 6 | 69 | NO |
|  | Right Turn | 1,500 | 1 | 1 | 0 | 2 | 36 | 19 | 6 | 69 | NO |
|  | Second Right |  |  |  |  |  |  |  |  |  |  |

Vissim Post-Processor
Average Results from 10 Runs
Queue Length

Richards Blvd/I-80 WB Ramps
Stor

Intersection 4

| $\begin{array}{c}\text { Storage } \\ (\mathrm{ft})\end{array}$ | Average |
| :---: | :---: |

Average Queue (ft)

|  |  | Maximum Queue (ft) |  |
| :--- | :--- | :--- | :---: |
| Maximum | Average $\quad$ Std. Dev. $\quad$ Minimu |  |  |



Exceeds

Vissim Post-Processor
Average Results from 10 Runs
Queue Length

I-80 / Richards Blvd Interchange
Construction Year Build Conditions
AM Peak Hour

Signal

| Direction | Movement | Storage <br> (ft) | Average Queue (ft) |  |  |  | Maximum Queue (ft) |  |  |  | Exceeds <br> Storage? |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Average | Std. Dev. | Minimum | Maximum | Average | Std. Dev. | Minimum | Maximum |  |
| NB | U Turn |  |  |  |  |  |  |  |  |  |  |
|  | Second Left |  |  |  |  |  |  |  |  |  |  |
|  | Left Turn |  |  |  |  |  |  |  |  |  |  |
|  | Through | 450 | 22 | 5 | 17 | 30 | 270 | 39 | 228 | 350 | NO |
|  | Right Turn | 450 | 16 | 4 | 12 | 23 | 246 | 39 | 203 | 325 | NO |
|  | Second Right |  |  |  |  |  |  |  |  |  |  |
| SB | U Turn |  |  |  |  |  |  |  |  |  |  |
|  | Second Left |  |  |  |  |  |  |  |  |  |  |
|  | Left Turn | 350 | 67 | 6 | 57 | 73 | 152 | 20 | 129 | 185 | NO |
|  | Through | 600 | 16 | 2 | 15 | 20 | 139 | 11 | 127 | 162 | NO |
|  | Right Turn |  |  |  |  |  |  |  |  |  |  |
|  | Second Right |  |  |  |  |  |  |  |  |  |  |
| EB | U Turn |  |  |  |  |  |  |  |  |  |  |
|  | Second Left |  |  |  |  |  |  |  |  |  |  |
|  | Left Turn |  |  |  |  |  |  |  |  |  |  |
|  | Through |  |  |  |  |  |  |  |  |  |  |
|  | Right Turn |  |  |  |  |  |  |  |  |  |  |
|  | Second Right |  |  |  |  |  |  |  |  |  |  |
| WB | U Turn |  |  |  |  |  |  |  |  |  |  |
|  | Second Left |  |  |  |  |  |  |  |  |  |  |
|  | Left Turn | 175 | 61 | 3 | 58 | 66 | 245 | 18 | 209 | 273 | MAX |
|  | Through |  |  |  |  |  |  |  |  |  |  |
|  | Right Turn | 1,625 | 9 | 1 | 8 | 12 | 99 | 18 | 75 | 135 | NO |
|  | Second Right |  |  |  |  |  |  |  |  |  |  |

Vissim Post-Processor
Average Results from 10 Runs
Queue Length

I-80 / Richards Blvd Interchange
Construction Year Build Conditions
AM Peak Hour

Signal

## Intersection 6 <br> Research Park Dr/Richards Blvd-Cowell Blvd

| Direction | Movement | Storage (ft) | Average Queue (ft) |  |  |  | Maximum Queue (ft) |  |  |  | Exceeds <br> Storage? |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Average | Std. Dev. | Minimum | Maximum | Average | Std. Dev. | Minimum | Maximum |  |
| NB | U Turn | $\begin{aligned} & 100 \\ & 625 \end{aligned}$ | 172 | 21 | $\begin{gathered} 15 \\ 1 \end{gathered}$ | $\begin{gathered} 20 \\ 3 \end{gathered}$ | $\begin{aligned} & 74 \\ & 39 \end{aligned}$ | $\begin{aligned} & 10 \\ & 12 \end{aligned}$ | $\begin{aligned} & 65 \\ & 22 \end{aligned}$ | $\begin{aligned} & 98 \\ & 60 \end{aligned}$ | $\begin{aligned} & \text { NO } \\ & \text { NO } \end{aligned}$ |
|  | Second Left |  |  |  |  |  |  |  |  |  |  |
|  | Left Turn |  |  |  |  |  |  |  |  |  |  |
|  | Through |  |  |  |  |  |  |  |  |  |  |
|  | Right Turn |  |  |  |  |  |  |  |  |  |  |
|  | Second Right |  |  |  |  |  |  |  |  |  |  |
| SB | U Turn | $\begin{gathered} 125 \\ 1,500 \end{gathered}$ | 48 | 1 | 34 | $\begin{gathered} 5 \\ 13 \end{gathered}$ | 4091 | $\begin{gathered} 6 \\ 21 \end{gathered}$ | $\begin{aligned} & 30 \\ & 68 \end{aligned}$ | $\begin{gathered} 47 \\ 131 \end{gathered}$ | $\begin{aligned} & \text { NO } \\ & \text { NO } \end{aligned}$ |
|  | Second Left |  |  |  |  |  |  |  |  |  |  |
|  | Left Turn |  |  |  |  |  |  |  |  |  |  |
|  | Through |  |  |  |  |  |  |  |  |  |  |
|  | Right Turn |  |  |  |  |  |  |  |  |  |  |
|  | Second Right |  |  |  |  |  |  |  |  |  |  |
| EB | U Turn | 450 | 82 | 8 | 67 | 99 | 310 | 72 | 228 | 436 | NO |
|  | Second Left |  |  |  |  |  |  |  |  |  |  |
|  | Left Turn | 450 | 82 | 8 | 67 | 99 | 310 | 72 | 228 | 436 | NO |
|  | Through | 450 | 40 | 4 | 35 | 47 | 269 | 19 | 239 | 296 | NO |
|  | Right Turn |  |  |  |  |  |  |  |  |  |  |
|  | Second Right |  |  |  |  |  |  |  |  |  |  |
| WB | U Turn |  | 0 | 0 |  | 1 | 2330 | 2322 | 00 | 7377 | NONO |
|  | Second Left |  |  |  |  |  |  |  |  |  |  |
|  | Left Turn |  |  |  |  |  |  |  |  |  |  |
|  | Through |  |  |  |  |  |  |  |  |  |  |
|  | Right Turn |  |  |  |  |  |  |  |  |  |  |
|  | Second Right |  |  |  |  |  |  |  |  |  |  |

Vissim Post-Processor
Average Results from 10 Runs
Queue Length
I-80 / Richards Blvd Interchange
Construction Year Build Conditions
PM Peak Hour

Intersection 1 D St/First St Signal

| Direction | Movement | Storage <br> (ft) | Average Queue (ft) |  |  |  | Maximum Queue (ft) |  |  |  | Exceeds <br> Storage? |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Average | Std. Dev. | Minimum | Maximum | Average | Std. Dev. | Minimum | Maximum |  |
| NB | U Turn |  |  |  |  |  |  |  |  |  |  |
|  | Second Left |  |  |  |  |  |  |  |  |  |  |
|  | Left Turn | 100 | 21 | 4 | 17 | 28 | 119 | 32 | 84 | 175 | MAX |
|  | Through | 100 | 21 | 4 | 17 | 28 | 119 | 32 | 84 | 175 | MAX |
|  | Right Turn | 400 | 2 | 0 | 1 | 2 | 47 | 12 | 25 | 62 | NO |
|  | Second Right |  |  |  |  |  |  |  |  |  |  |
| SB | U Turn |  |  |  |  |  |  |  |  |  |  |
|  | Second Left |  |  |  |  |  |  |  |  |  |  |
|  | Left Turn | 400 | 36 | 5 | 29 | 47 | 157 | 17 | 126 | 190 | NO |
|  | Through | 400 | 36 | 5 | 29 | 47 | 157 | 17 | 126 | 190 | NO |
|  | Right Turn | 400 | 5 | 3 | 2 | 10 | 124 | 29 | 82 | 162 | NO |
|  | Second Right |  |  |  |  |  |  |  |  |  |  |
| EB | U Turn |  |  |  |  |  |  |  |  |  |  |
|  | Second Left |  |  |  |  |  |  |  |  |  |  |
|  | Left Turn | 75 | 4 | 2 | 2 | 8 | 45 | 42 | 23 | 162 | NO |
|  | Through | 250 | 82 | 47 | 44 | 207 | 381 | 62 | 297 | 498 | MAX |
|  | Right Turn | 250 | 83 | 48 | 45 | 209 | 384 | 62 | 300 | 501 | MAX |
|  | Second Right |  |  |  |  |  |  |  |  |  |  |
| WB | U Turn |  |  |  |  |  |  |  |  |  |  |
|  | Second Left |  |  |  |  |  |  |  |  |  |  |
|  | Left Turn | 100 | 2 | 3 | 0 | 8 | 26 | 31 | 0 | 109 | NO |
|  | Through | 225 | 2 | 3 | 0 | 8 | 26 | 31 | 0 | 109 | NO |
|  | Right Turn | 225 | 2 | 3 | 0 | 8 | 26 | 31 | 0 | 109 | NO |
|  | Second Right |  |  |  |  |  |  |  |  |  |  |

Vissim Post-Processor
Average Results from 10 Runs
Queue Length
I-80 / Richards Blvd Interchange
Construction Year Build Conditions
PM Peak Hour

Intersection 2 E St-Richards Blvd/First St
Signal


Vissim Post-Processor

## Average Results from 10 Runs

Queue Length
I-80 / Richards Blvd Interchange
Construction Year Build Conditions
PM Peak Hour

Intersection 3 Richards Blvd/Olive Dr
Signal

| Direction | Movement | Storage <br> (ft) | Average Queue (ft) |  |  |  | Maximum Queue (ft) |  |  |  | Exceeds Storage? |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Average | Std. Dev. | Minimum | Maximum | Average | Std. Dev. | Minimum | Maximum |  |
| NB | U Turn |  |  |  |  |  |  |  |  |  |  |
|  | Second Left |  |  |  |  |  |  |  |  |  |  |
|  | Left Turn | 175 | 84 | 9 | 75 | 102 | 270 | 54 | 210 | 353 | MAX |
|  | Through | 600 | 93 | 7 | 85 | 108 | 469 | 14 | 449 | 493 | NO |
|  | Right Turn | 275 | 1 | 0 | 1 | 2 | 51 | 11 | 43 | 76 | NO |
|  | Second Right |  |  |  |  |  |  |  |  |  |  |
| SB | U Turn |  |  |  |  |  |  |  |  |  |  |
|  | Second Left |  |  |  |  |  |  |  |  |  |  |
|  | Left Turn | 625 | 43 | 21 | 21 | 78 | 300 | 130 | 134 | 534 | NO |
|  | Through | 625 | 194 | 39 | 135 | 257 | 684 | 32 | 639 | 752 | MAX |
|  | Right Turn | 625 | 192 | 39 | 133 | 255 | 683 | 32 | 638 | 751 | MAX |
|  | Second Right |  |  |  |  |  |  |  |  |  |  |
| EB | U Turn |  |  |  |  |  |  |  |  |  |  |
|  | Second Left |  |  |  |  |  |  |  |  |  |  |
|  | Left Turn | 250 | 40 | 7 | 24 | 50 | 248 | 37 | 193 | 295 | NO |
|  | Through | 600 | 40 | 7 | 24 | 50 | 248 | 37 | 193 | 295 | NO |
|  | Right Turn | 250 | 25 | 8 | 15 | 36 | 249 | 43 | 182 | 297 | NO |
|  | Second Right |  |  |  |  |  |  |  |  |  |  |
| WB | U Turn |  |  |  |  |  |  |  |  |  |  |
|  | Second Left |  |  |  |  |  |  |  |  |  |  |
|  | Left Turn | 200 | 64 | 65 | 3 | 169 | 260 | 136 | 89 | 457 | MAX |
|  | Through | 1,500 | 64 | 65 | 3 | 169 | 260 | 136 | 89 | 457 | NO |
|  | Right Turn | 1,500 | 64 | 65 | 3 | 169 | 260 | 136 | 89 | 457 | NO |
|  | Second Right |  |  |  |  |  |  |  |  |  |  |

Vissim Post-Processor
Average Results from 10 Runs
Queue Length
I-80 / Richards Blvd Interchange
Construction Year Build Conditions
PM Peak Hour

Intersection 4 Richards Blvd/I-80 WB Ramps
Signal

| Direction | Movement | Storage <br> (ft) | Average Queue (ft) |  |  |  | Maximum Queue (ft) |  |  |  | Exceeds <br> Storage? |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Average | Std. Dev. | Minimum | Maximum | Average | Std. Dev. | Minimum | Maximum |  |
| NB |  |  |  |  |  |  |  |  |  |  |  |
|  | Second Left |  |  |  |  |  |  |  |  |  |  |
|  | Left Turn | 475 | 92 | 7 | 80 | 102 | 278 | 31 | 248 | 348 | NO |
|  | Through | 825 | 8 | 2 | 5 | 11 | 174 | 34 | 117 | 214 | NO |
|  | Right Turn |  |  |  |  |  |  |  |  |  |  |
|  | Second Right |  |  |  |  |  |  |  |  |  |  |
| SB | U Turn |  |  |  |  |  |  |  |  |  |  |
|  | Second Left |  |  |  |  |  |  |  |  |  |  |
|  | Left Turn |  |  |  |  |  |  |  |  |  |  |
|  | Through | 600 | 23 | 2 | 20 | 26 | 137 | 20 | 100 | 162 | NO |
|  | Right Turn | 225 | 1 | 0 | 0 | 1 | 41 | 16 | 15 | 67 | NO |
|  | Second Right |  |  |  |  |  |  |  |  |  |  |
| EB | U Turn |  |  |  |  |  |  |  |  |  |  |
|  | Second Left |  |  |  |  |  |  |  |  |  |  |
|  | Left Turn |  |  |  |  |  |  |  |  |  |  |
|  | Through |  |  |  |  |  |  |  |  |  |  |
|  | Right Turn |  |  |  |  |  |  |  |  |  |  |
|  | Second Right |  |  |  |  |  |  |  |  |  |  |
| WB | U Turn |  |  |  |  |  |  |  |  |  |  |
|  | Second Left |  |  |  |  |  |  |  |  |  |  |
|  | Left Turn | 450 | 28 | 2 | 24 | 32 | 140 | 23 | 112 | 198 | NO |
|  | Through |  |  |  |  |  |  |  |  |  |  |
|  | Right Turn | 1,225 | 46 | 7 | 39 | 60 | 256 | 40 | 190 | 318 | NO |
|  | Second Right |  |  |  |  |  |  |  |  |  |  |

Vissim Post-Processor
Average Results from 10 Runs
Queue Length
I-80 / Richards Blvd Interchange
Construction Year Build Conditions
PM Peak Hour

Intersection 5 I-80 EB Ramps/Richards Blvd
Signal


Vissim Post-Processor
Average Results from 10 Runs
Queue Length
I-80 / Richards Blvd Interchange
Construction Year Build Conditions
PM Peak Hour

Intersection 6 Research Park Dr/Richards Blvd-Cowell Blvd
Signal

| Direction | Movement | Storage <br> (ft) | Average Queue ( ft ) |  |  |  | Maximum Queue (ft) |  |  |  | Exceeds Storage? |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Average | Std. Dev. | Minimum | Maximum | Average | Std. Dev. | Minimum | Maximum |  |
| NB | U Turn | $\begin{aligned} & 100 \\ & 625 \end{aligned}$ | 2912 | 3 | $\begin{gathered} 23 \\ 8 \end{gathered}$ | $\begin{aligned} & 34 \\ & 16 \end{aligned}$ | $\begin{aligned} & 100 \\ & 108 \end{aligned}$ | $\begin{aligned} & 11 \\ & 25 \end{aligned}$ | $\begin{aligned} & 81 \\ & 81 \end{aligned}$ | $\begin{aligned} & 119 \\ & 158 \end{aligned}$ | $\begin{aligned} & \text { NO } \\ & \text { NO } \end{aligned}$ |
|  | Second Left |  |  |  |  |  |  |  |  |  |  |
|  | Left Turn |  |  |  |  |  |  |  |  |  |  |
|  | Through |  |  |  |  |  |  |  |  |  |  |
|  | Right Turn |  |  |  |  |  |  |  |  |  |  |
|  | Second Right |  |  |  |  |  |  |  |  |  |  |
| SB | U Turn | $\begin{gathered} 125 \\ 1,500 \end{gathered}$ | 139 | 32 | 87 | $\begin{aligned} & 19 \\ & 13 \end{aligned}$ | $\begin{gathered} 71 \\ 129 \end{gathered}$ | $\begin{aligned} & 10 \\ & 31 \end{aligned}$ | $\begin{aligned} & 54 \\ & 95 \end{aligned}$ | $\begin{gathered} 91 \\ 193 \end{gathered}$ | $\begin{aligned} & \text { NO } \\ & \text { NO } \end{aligned}$ |
|  | Second Left |  |  |  |  |  |  |  |  |  |  |
|  | Left Turn |  |  |  |  |  |  |  |  |  |  |
|  | Through |  |  |  |  |  |  |  |  |  |  |
|  | Right Turn |  |  |  |  |  |  |  |  |  |  |
|  | Second Right |  |  |  |  |  |  |  |  |  |  |
| EB | U Turn | 450 | 103 | 12 | 91 | 127 | 351 | 60 | 287 | 472 | NO |
|  | Second Left |  |  |  |  |  |  |  |  |  |  |
|  | Left Turn | 450 | 103 | 12 | 91 | 127 | 351 | 60 | 287 | 472 | NO |
|  | Through | 450 | 29 | 8 | 18 | 44 | 222 | 28 | 173 | 262 | NO |
|  | Right Turn |  |  |  |  |  |  |  |  |  |  |
|  | Second Right |  |  |  |  |  |  |  |  |  |  |
| WB | U Turn | 751,125 | 1 | 1 | 00 | 33 | 4346 | 2930 | 1315 | $\begin{gathered} 95 \\ 101 \end{gathered}$ | NONO |
|  | Second Left |  |  |  |  |  |  |  |  |  |  |
|  | Left Turn |  |  |  |  |  |  |  |  |  |  |
|  | Through |  |  |  |  |  |  |  |  |  |  |
|  | Right Turn |  |  |  |  |  |  |  |  |  |  |
|  | Second Right |  |  |  |  |  |  |  |  |  |  |


|  | Freeway Basic Report |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Eastbound I-80 |
| Segment | West of Old Davis Rd |
| Alternative | Construction Year |
| Time Period | AM Peak Hour |


|  | General |  |  |  |  |  | Purpose Lanes - Geometric Data |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| General Purpose Lanes, N | 5 | In | Terrain Type | Level |  |  |  |  |  |
| Segment Length, L | 1,500 | ft | Percent Grade | - |  |  |  |  |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |  |  |  |  |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 1.67 | $\mathrm{ramps} / \mathrm{mi}$ |  |  |  |  |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 70.5 | mph |  |  |  |  |


| General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


| General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | ---: |
| Volume, V | 4,740 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.95 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,088 | pcphpl |
| Total Trucks | $9.0 \%$ |  | Capacity, c | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |  |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.45 |  |


| General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS ${ }_{\text {adj }}$ | 70.5 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 70.5 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 15.4 | pcpmpl |
| Total Ramp Density Adjustment | 4.9 | mph | Level of Service, LOS | B |  |

$\qquad$


| Entering General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Volume, V | 4,740 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.95 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,088 | pcphpl |
| Total Trucks | 9.0\% |  | Capacity, c | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - |  | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.45 |  |


| Entering General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 70.5 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 70.5 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 15.4 | pcpmpl |
| Total Ramp Density Adjustment | 4.9 | mph | Level of Service, LOS | B |  |


| Segment General Purpose Lanes - Capacity, Speed, and Density |  |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
| General Purpose Lanes, N | 6 | $\ln$ | Average Speed, S | 70.5 | mph |  |
| Adjusted Capacity, cadj | 2,400 | pcphpl | Density, D | 13.0 | pcphpl |  |
| Flow Rate, vp | 916 | pcphpl | Level of Service, LOS | B |  |  |
| Volume-to-Capacity Ratio, v/c | 0.38 |  |  |  |  |  |

## Freeway Merge Report



## Freeway Merge Report



| Ramp Influence Area Density and Level of Service |  |  |
| :--- | :--- | :---: |
|  |  |  |
| Density in Ramp Influence Area, $D_{R}$ | pcpmpl |  |
| Level of Service, LOS |  |  |

## Segment Speed, Flow, and Density

Speed Adjustment Factor, SAF
Speed Index, $\mathrm{M}_{\mathrm{S}}$ or $\mathrm{D}_{\mathrm{S}}$
Average Speed in Ramp Influence Area, $\mathrm{S}_{\mathrm{R}} \mathrm{mph}$

Average Flow in Outer Lanes, $\mathrm{v}_{\mathrm{OA}}$
pcphpl
mph
Average Speed in Outer Lanes, $\mathrm{S}_{0}$
mph
Density across All Lanes, D
pcpmpl

|  | Freeway Basic Repor |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Eastbound I-80 |
| Segment | Old Davis Rd to Lane Drop 1 |
| Alternative | Construction Year |
| Time Period | AM Peak Hour |


|  | General |  |  |  |  |  |  | Purpose Lanes - Geometric Data |  |  |
| :--- | :---: | :---: | :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| General Purpose Lanes, N | 5 | ln | Terrain Type | Level |  |  |  |  |  |  |
| Segment Length, L | 820 | ft | Percent Grade | - |  |  |  |  |  |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |  |  |  |  |  |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 1.67 | $\mathrm{ramps} / \mathrm{mi}$ |  |  |  |  |  |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 70.5 | mph |  |  |  |  |  |


| General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


| General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Volume, V | 4,790 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.95 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,099 | pcphpl |
| Total Trucks | 9.0\% |  | Capacity, c | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - |  | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.46 |  |


| General Purpose Lanes - Speed and Density |  |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 70.5 | mph |  |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 70.5 | mph |  |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 15.6 | pcpmpl |  |
| Total Ramp Density Adjustment | 4.9 | mph | Level of Service, LOS | B |  |  |

$\qquad$

|  | Freeway Basic Report |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Eastbound I-80 |
| Segment | Lane Drop 1 to Lane Drop 2 |
| Alternative | Construction Year |
| Time Period | AM Peak Hour |


|  | General |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
|  | Purpose Lanes - Geometric Data |  |  |  |  |  |
| General Purpose Lanes, N | 4 | ln | Terrain Type | Level |  |  |
| Segment Length, L | 1,480 | ft | Percent Grade | - |  |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |  |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 1.50 | $\mathrm{ramps} / \mathrm{mi}$ |  |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 70.9 | mph |  |


| General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


| General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Volume, V | 4,790 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.95 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,374 | pcphpl |
| Total Trucks | 9.0\% |  | Capacity, c | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - |  | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.57 |  |


| General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 70.9 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 70.4 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 19.5 | pcpmpl |
| Total Ramp Density Adjustment | 4.5 | mph | Level of Service, LOS | C |  |

$\qquad$

## Freeway Diverge Report

| Freeway Diverge Report |  |  |  |
| :---: | :---: | :---: | :---: |
| Project I-80/Richards B <br> Freeway Eastbound I-80 <br> Segment Richards Blvd O <br> Alternative Construction Ye <br> Time Period AM Peak Hour |  |  |  |
| Geometric Data |  |  |  |
|  | Freeway | Off Ramp |  |
| Number of Lanes, N | 3 | 1 |  |
| Free-Flow Speed, FFS | 70.9 | 25 | mph |
| Segment Length, L / Deceleration Length, LD | 1,240 | 150 | ft |
| Terrain Type | Level | Level |  |
| Percent Grade | - | - |  |
| Grade Length | - | - | ft |
| Segment Type / Ramp Type | Freeway | Right |  |
| Adjustment Factors |  |  |  |
|  | Freeway | Off Ramp |  |
| Driver Population | Familiar | Familiar |  |
| Weather Type | Non-severe | Non-severe |  |
| Incident Type | No incident | No incident |  |
| Capacity Adjustment Factor, CAF | 1.00 | 1.00 |  |
| Demand Adjustment Factor, DAF | 1.00 | 1.00 |  |
| Volume Data |  |  |  |
| Junction Components | Freeway | Off Ramp |  |
| Volume, V | 4,790 | 590 | vph |
| Peak Hour Factor, PHF | 0.95 | 0.88 |  |
| Total Trucks | 9.0\% | 3.3\% |  |
| Single Unit/Tractor-Trailer Mix | - | - |  |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 | 2.0 |  |
| Heavy Vehicle Adjustment, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 | 0.968 |  |
| Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 5,496 | 693 | pcph |

## Adjacent Ramp Data

Adjacent Ramp Meeting Criteria
Type of Adjacent Ramp
Distance to Adjacent Ramp
Volume on Adjacent Ramp

| Upstream | Downstream |
| :---: | :---: |
| No | Yes |
|  | On |
|  | 2,740 |
|  | 381 |

## Freeway Diverge Report



|  | Freeway Basic Report |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Eastbound I-80 |
| Segment | Richards Blvd Off to On |
| Alternative | Construction Year |
| Time Period | AM Peak Hour |


|  | General |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
|  | Purpose Lanes - Geometric Data |  |  |  |  |  |
| General Purpose Lanes, N | 3 | ln | Terrain Type | Level |  |  |
| Segment Length, L | 1,500 | ft | Percent Grade | - |  |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |  |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 1.67 | $\mathrm{ramps} / \mathrm{mi}$ |  |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 70.5 | mph |  |


| General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


| General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Volume, V | 4,200 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.95 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,606 | pcphpl |
| Total Trucks | 9.0\% |  | Capacity, c | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - |  | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.67 |  |


| General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 70.5 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 68.4 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 23.5 | pcpmpl |
| Total Ramp Density Adjustment | 4.9 | mph | Level of Service, LOS | C |  |


| Freeway Merge Report |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Project I-80/Richards <br> Freeway Eastbound I-80 <br> Segment Richards Blvd On <br> Alternative Construction Y <br> Time Period AM Peak Hour |  |  |  |  |
| Geometric Data |  |  |  |  |
|  | Freeway | On Ramp |  |  |
| Number of Lanes, N | 3 | 1 |  |  |
| Free-Flow Speed, FFS | 70.5 | 45 |  | mph |
| Segment Length, L / Acceleration Length, LA | 1,500 | 500 |  | ft |
| Terrain Type | Level | Level |  |  |
| Percent Grade | - | - |  |  |
| Grade Length | - | - |  | ft |
| Segment Type / Ramp Type | Freeway | Right |  |  |
| Adjustment Factors |  |  |  |  |
|  | Freeway | On Ramp |  |  |
| Driver Population | Familiar | Familiar |  |  |
| Weather Type | Non-severe | Non-severe |  |  |
| Incident Type | No incident | No incident |  |  |
| Capacity Adjustment Factor, CAF | 1.00 | 1.00 |  |  |
| Demand Adjustment Factor, DAF | 1.00 | 1.00 |  |  |
| Volume Data |  |  |  |  |
| Junction Components | Freeway | On Ramp |  |  |
| Volume, V | 4,200 | 330 |  | vph |
| Peak Hour Factor, PHF | 0.95 | 0.88 |  |  |
| Total Trucks | 9.0\% | 1.7\% |  |  |
| Single Unit/Tractor-Trailer Mix | - | - |  |  |
| Passenger Car Equivalent, $\mathrm{E}_{T}$ | 2.0 | 2.0 |  |  |
| Heavy Vehicle Adjustment, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 | 0.983 |  |  |
| Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 4,819 | 381 |  | pcph |
| Adjacent Ramp Data |  |  |  |  |
|  |  | Upstream | Downstream |  |
| Adjacent Ramp Meeting Criteria |  | Yes | No |  |
| Type of Adjacent Ramp |  | Off |  |  |
| Distance to Adjacent Ramp |  | 2,740 |  | ft |
| Volume on Adjacent Ramp |  | 693 |  | pcph |


| Freeway Merge Report |  |  |
| :---: | :---: | :---: |
| Project I-80/Richards Blvd Interchange <br> Freeway Eastbound I-80 <br> Segment Richards Blvd On Ramp <br> Alternative Construction Year <br> Time Period AM Peak Hour |  |  |
| Estimation of Volume in Ramp Influence Area |  |  |
| Adjacent Upstream On-ramp Equilibrium Distance, $\mathrm{L}_{\mathrm{EQ}}$ <br> Adjacent Downstream On-ramp Equilibrium Distance, $\mathrm{L}_{\mathrm{EQ}}$ <br> Proportion of Freeway Vehicles in Lanes 1 and 2, $\mathrm{P}_{\mathrm{FM}}$ or $\mathrm{P}_{\mathrm{FD}}$ <br> Flow Rate in Lanes 1 and 2, $\mathrm{v}_{12}$ | $\begin{aligned} & 1,286 \\ & 0.592 \\ & 2,850 \end{aligned}$ | ft <br> ft pcph |
| Capacity Checks |  |  |
| Flow Capacity |  | V/C Ratio |
| Entering General Purpose Lanes 4,819 7,200 | pcph | 0.67 |
| $\begin{array}{lll}\text { Exiting General Purpose Lanes } & \text { 5,200 } & \text { 7,200 }\end{array}$ | pcph | 0.72 |
| $\begin{array}{llll}\text { On Ramp } & 381 & \text { 2,100 }\end{array}$ | pcph | 0.18 |
| Ramp Influence Area 3 3,232 4,600 | pcph | 0.70 |
| Ramp Influence Area Density and Level of Service |  |  |
| Density in Ramp Influence Area, $D_{R}$ Level of Service, LOS | $\begin{gathered} 27.4 \\ \text { C } \end{gathered}$ | pcpmpl |
| Segment Speed, Flow, and Density |  |  |
| Speed Adjustment Factor, SAF | 1.00 |  |
| Speed Index, $\mathrm{M}_{\mathrm{S}}$ or $\mathrm{D}_{\mathrm{S}}$ | 0.375 |  |
| Average Speed in Ramp Influence Area, $\mathrm{S}_{\mathrm{R}}$ | 59.8 | mph |
| Average Flow in Outer Lanes, $\mathrm{v}_{\mathrm{OA}}$ | 1,969 | pcphpl |
| Average Speed in Outer Lanes, $\mathrm{S}_{0}$ | 65.2 | mph |
| Average Speed for Segment, S | 61.7 | mph |
| Density across All Lanes, D | 29.0 | pcpmpl |


|  | Freeway Basic Report |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Eastbound I-80 |
| Segment | Richards Blvd to Chiles Rd |
| Alternative | Construction Year |
| Time Period | AM Peak Hour |


|  | General |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
|  | Purpose Lanes - Geometric Data |  |  |  |  |  |
| General Purpose Lanes, N | 3 | ln | Terrain Type | Level |  |  |
| Segment Length, L | 5,710 | ft | Percent Grade | - |  |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |  |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 1.50 | $\mathrm{ramps} / \mathrm{mi}$ |  |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 70.9 | mph |  |


| General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


| General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Volume, V | 4,530 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.95 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,733 | pcphpl |
| Total Trucks | 9.0\% |  | Capacity, c | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - |  | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.72 |  |


| General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 70.9 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 67.2 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 25.8 | pcpmpl |
| Total Ramp Density Adjustment | 4.5 | mph | Level of Service, LOS | C |  |

## Freeway Diverge Report

| Freeway Diverge Report |  |  |  |
| :---: | :---: | :---: | :---: |
| Project I-80/Richards B <br> Freeway Eastbound I-80 <br> Segment Chiles Rd Off Ra <br> Alternative Construction Ye <br> Time Period AM Peak Hour |  |  |  |
| Geometric Data |  |  |  |
|  | Freeway | Off Ramp |  |
| Number of Lanes, N | 3 | 2 |  |
| Free-Flow Speed, FFS | 70.9 | 25 | mph |
| Segment Length, L / Deceleration Length, LD | 1,500 | 1,500 | ft |
| Terrain Type | Level | Level |  |
| Percent Grade | - | - |  |
| Grade Length | - |  | ft |
| Segment Type / Ramp Type | Freeway | Right |  |
| Adjustment Factors |  |  |  |
|  | Freeway | Off Ramp |  |
| Driver Population | Familiar | Familiar |  |
| Weather Type | Non-severe | Non-severe |  |
| Incident Type | No incident | No incident |  |
| Capacity Adjustment Factor, CAF | 1.00 | 1.00 |  |
| Demand Adjustment Factor, DAF | 1.00 | 1.00 |  |
| Volume Data |  |  |  |
| Junction Components | Freeway | Off Ramp |  |
| Volume, V | 4,530 | 380 | vph |
| Peak Hour Factor, PHF | 0.95 | 0.78 |  |
| Total Trucks | 9.0\% | 3.0\% |  |
| Single Unit/Tractor-Trailer Mix | - | - |  |
| Passenger Car Equivalent, $\mathrm{E}_{T}$ | 2.0 | 2.0 |  |
| Heavy Vehicle Adjustment, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 | 0.971 |  |
| Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 5,198 | 502 | pcph |

## Adjacent Ramp Data

Adjacent Ramp Meeting Criteria
Upstream Downstream

Type of Adjacent Ramp
Distance to Adjacent Ramp
Volume on Adjacent Ramp

## Freeway Diverge Report



|  | Freeway Basic Repor |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Eastbound I-80 |
| Segment | Chiles Rd Off to Mace Rd On |
| Alternative | Construction Year |
| Time Period | AM Peak Hour |


|  | General |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
|  | Purpose Lanes - Geometric Data |  |  |  |  |  |
| General Purpose Lanes, N | 3 | ln | Terrain Type | Level |  |  |
| Segment Length, L | 1,000 | ft | Percent Grade | - |  |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |  |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 1.50 | $\mathrm{ramps} / \mathrm{mi}$ |  |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 70.9 | mph |  |


| General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


| General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Volume, V | 4,150 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.95 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,587 | pcphpl |
| Total Trucks | 9.0\% |  | Capacity, c | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - |  | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.66 |  |


| General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 70.9 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 68.8 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 23.1 | pcpmpl |
| Total Ramp Density Adjustment | 4.5 | mph | Level of Service, LOS | C |  |


|  | Freeway Basic Report |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Eastbound I-80 |
| Segment | West of Old Davis Rd |
| Alternative | Construction Year |
| Time Period | PM Peak Hour |


|  | General |  |  |  |  |  | Purpose Lanes - Geometric Data |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| General Purpose Lanes, N | 5 | ln | Terrain Type | Level |  |  |  |  |  |
| Segment Length, L | 1,500 | ft | Percent Grade | - |  |  |  |  |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |  |  |  |  |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 1.67 | $\mathrm{ramps} / \mathrm{mi}$ |  |  |  |  |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 70.5 | mph |  |  |  |  |


| General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


|  | General Purpose Lanes - Demand and Capacity |  |  |  |  |
| :--- | :---: | :--- | :--- | :--- | :--- |
| Volume, V | 4,930 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.99 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,086 | pcphpl |
| Total Trucks | $9.0 \%$ |  | Capacity, c | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |  |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.45 |  |


| General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 70.5 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 70.5 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 15.4 | pcpmpl |
| Total Ramp Density Adjustment | 4.9 | mph | Level of Service, LOS | B |  |

$\qquad$


| Entering General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :--- | :---: | :--- | :--- | :--- | :--- |
| Volume, V | 4,930 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.99 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,086 | pcphpl |
| Total Trucks | $9.0 \%$ |  | Capacity, c | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |  |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.45 |  |


| Entering General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 70.5 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 70.5 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 15.4 | pcpmpl |
| Total Ramp Density Adjustment | 4.9 | mph | Level of Service, LOS | B |  |


| Segment General Purpose Lanes - Capacity, Speed, and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| General Purpose Lanes, N | 6 | $\ln$ | Average Speed, S | 70.5 | mph |
| Adjusted Capacity, cadj | 2,400 | pcphpl | Density, D | 13.6 | pcphpl |
| Flow Rate, vp | 961 | pcphpl | Level of Service, LOS | B |  |
| Volume-to-Capacity Ratio, v/c | 0.40 |  |  |  |  |

## Freeway Merge Report

| Freeway Merge Report |  |  |  |
| :---: | :---: | :---: | :---: |
| Project I-80/Richards B <br> Freeway Eastbound I-80 <br> Segment Old Davis Rd O <br> Alternative Construction Y <br> Time Period PM Peak Hour |  |  |  |
| Geometric Data |  |  |  |
|  | Freeway | On Ramp |  |
| Number of Lanes, N | 5 | 2 |  |
| Free-Flow Speed, FFS | 70.5 | 45 | mph |
| Segment Length, L / Acceleration Length, LA | 1,500 | 0 | ft |
| Terrain Type | Level | Level |  |
| Percent Grade | - | - |  |
| Grade Length | - |  | ft |
| Segment Type / Ramp Type | Freeway | Right |  |
| Adjustment Factors |  |  |  |
|  | Freeway | On Ramp |  |
| Driver Population | Familiar | Familiar |  |
| Weather Type | Non-severe | Non-severe |  |
| Incident Type | No incident | No incident |  |
| Capacity Adjustment Factor, CAF | 1.00 | 1.00 |  |
| Demand Adjustment Factor, DAF | 1.00 | 1.00 |  |
| Volume Data |  |  |  |
| Junction Components | Freeway | On Ramp |  |
| Volume, V | 4,930 | 260 | vph |
| Peak Hour Factor, PHF | 0.99 | 0.77 |  |
| Total Trucks | 9.0\% | 0.5\% |  |
| Single Unit/Tractor-Trailer Mix | - | - |  |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 | 2.0 |  |
| Heavy Vehicle Adjustment, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 | 0.995 |  |
| Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 5,428 | 339 | pcph |

## Adjacent Ramp Data

Adjacent Ramp Meeting Criteria
Upstream Downstream

Type of Adjacent Ramp
Distance to Adjacent Ramp
Volume on Adjacent Ramp

## Freeway Merge Report



| Ramp Influence Area Density and Level of Service |  |  |
| :--- | :--- | :---: |
|  | pcpmpl |  |
| Density in Ramp Influence Area, $D_{R}$ |  |  |

## Segment Speed, Flow, and Density

Speed Adjustment Factor, SAF
Speed Index, $\mathrm{M}_{\mathrm{S}}$ or $\mathrm{D}_{\mathrm{S}}$
Average Speed in Ramp Influence Area, $\mathrm{S}_{\mathrm{R}} \mathrm{mph}$

Average Flow in Outer Lanes, $\mathrm{v}_{\mathrm{OA}}$
pcphpl
mph
Average Speed in Outer Lanes, $\mathrm{S}_{0}$
Average Speed for Segment, S
mph
Density across All Lanes, D
pcpmpl

|  | Freeway Basic Report |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Eastbound I-80 |
| Segment | Old Davis Rd to Lane Drop 1 |
| Alternative | Construction Year |
| Time Period | PM Peak Hour |


|  | General |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
|  | Purpose Lanes - Geometric Data |  |  |  |  |  |
| General Purpose Lanes, N | 5 | ln | Terrain Type | Level |  |  |
| Segment Length, L | 820 | ft | Percent Grade | - |  |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |  |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 1.67 | $\mathrm{ramps} / \mathrm{mi}$ |  |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 70.5 | mph |  |


| General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


|  | General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :--- | :--- | :--- |
| Volume, V | 5,190 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{Hv}}$ | 0.917 |  |  |
| Peak Hour Factor, PHF | 0.99 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,143 | pcphpl |  |
| Total Trucks | $9.0 \%$ |  | Capacity, c | 2,400 | pcphpl |  |
| Single Unit/Tractor-Trailer Mix | - | Adjusted Capacity, $\mathrm{c}_{\mathrm{adj}}$ | 2,400 | pcphpl |  |  |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 | Volume-to-Capacity Ratio, v/c | 0.48 |  |  |  |


| General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 70.5 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 70.5 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 16.2 | pcpmpl |
| Total Ramp Density Adjustment | 4.9 | mph | Level of Service, LOS | B |  |

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|  | Freeway Basic Report |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Eastbound I-80 |
| Segment | Lane Drop 1 to Lane Drop 2 |
| Alternative | Construction Year |
| Time Period | PM Peak Hour |


|  | General |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
|  | Purpose Lanes - Geometric Data |  |  |  |  |  |
| General Purpose Lanes, N | 4 | ln | Terrain Type | Level |  |  |
| Segment Length, L | 1,480 | ft | Percent Grade | - |  |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |  |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 1.50 | $\mathrm{ramps} / \mathrm{mi}$ |  |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 70.9 | mph |  |


| General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


|  | General Purpose Lanes - Demand and Capacity |  |  |  |  |
| :--- | :---: | :--- | :--- | :--- | :--- |
| Volume, V | 5,190 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.99 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,429 | pcphpl |
| Total Trucks | $9.0 \%$ |  | Capacity, c | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |  |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.60 |  |


| General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 70.9 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 70.1 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 20.4 | pcpmpl |
| Total Ramp Density Adjustment | 4.5 | mph | Level of Service, LOS | C |  |

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## Freeway Diverge Report

| Freeway Diverge Report |  |  |  |
| :---: | :---: | :---: | :---: |
| Project I-80/Richards B <br> Freeway Eastbound I-80 <br> Segment Richards Blvd O <br> Alternative Construction Ye <br> Time Period PM Peak Hour |  |  |  |
| Geometric Data |  |  |  |
|  | Freeway | Off Ramp |  |
| Number of Lanes, N | 3 | 1 |  |
| Free-Flow Speed, FFS | 70.9 | 25 | mph |
| Segment Length, L / Deceleration Length, LD | 1,240 | 150 | ft |
| Terrain Type | Level | Level |  |
| Percent Grade | - | - |  |
| Grade Length | - |  | ft |
| Segment Type / Ramp Type | Freeway | Right |  |
| Adjustment Factors |  |  |  |
|  | Freeway | Off Ramp |  |
| Driver Population | Familiar | Familiar |  |
| Weather Type | Non-severe | Non-severe |  |
| Incident Type | No incident | No incident |  |
| Capacity Adjustment Factor, CAF | 1.00 | 1.00 |  |
| Demand Adjustment Factor, DAF | 1.00 | 1.00 |  |
| Volume Data |  |  |  |
| Junction Components | Freeway | Off Ramp |  |
| Volume, V | 5,190 | 660 | vph |
| Peak Hour Factor, PHF | 0.99 | 0.86 |  |
| Total Trucks | 9.0\% | 2.4\% |  |
| Single Unit/Tractor-Trailer Mix | - | - |  |
| Passenger Car Equivalent, $\mathrm{E}_{T}$ | 2.0 | 2.0 |  |
| Heavy Vehicle Adjustment, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 | 0.977 |  |
| Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 5,714 | 786 | pcph |

## Adjacent Ramp Data

Adjacent Ramp Meeting Criteria
Type of Adjacent Ramp
Distance to Adjacent Ramp
Volume on Adjacent Ramp

| Upstream | Downstream |
| :---: | :---: |
| No | Yes |
|  | On |
|  | 2,740 |
|  | 414 |

## Freeway Diverge Report



|  | Freeway Basic Report |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Eastbound I-80 |
| Segment | Richards Blvd Off to On |
| Alternative | Construction Year |
| Time Period | PM Peak Hour |


|  | General |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
|  | Purpose Lanes - Geometric Data |  |  |  |  |  |
| General Purpose Lanes, N | 3 | ln | Terrain Type | Level |  |  |
| Segment Length, L | 1,500 | ft | Percent Grade | - |  |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |  |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 1.67 | $\mathrm{ramps} / \mathrm{mi}$ |  |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 70.5 | mph |  |


| General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


| General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Volume, V | 4,530 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.99 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,663 | pcphpl |
| Total Trucks | 9.0\% |  | Capacity, c | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - |  | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.69 |  |


| General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 70.5 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 67.8 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 24.5 | pcpmpl |
| Total Ramp Density Adjustment | 4.9 | mph | Level of Service, LOS | C |  |


| Freeway Merge Report |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Project I-80/Richards B <br> Freeway Eastbound I-80 <br> Segment Richards Blvd O <br> Alternative Construction Ye <br> Time Period PM Peak Hour |  |  |  |  |
| Geometric Data |  |  |  |  |
|  | Freeway | On Ramp |  |  |
| Number of Lanes, N | 3 | 1 |  |  |
| Free-Flow Speed, FFS | 70.5 | 45 |  | mph |
| Segment Length, L / Acceleration Length, LA | 1,500 | 500 |  | ft |
| Terrain Type | Level | Level |  |  |
| Percent Grade | - | - |  |  |
| Grade Length | - | - |  | ft |
| Segment Type / Ramp Type | Freeway | Right |  |  |
| Adjustment Factors |  |  |  |  |
|  | Freeway | On Ramp |  |  |
| Driver Population | Familiar | Familiar |  |  |
| Weather Type | Non-severe | Non-severe |  |  |
| Incident Type | No incident | No incident |  |  |
| Capacity Adjustment Factor, CAF | 1.00 | 1.00 |  |  |
| Demand Adjustment Factor, DAF | 1.00 | 1.00 |  |  |
| Volume Data |  |  |  |  |
| Junction Components | Freeway | On Ramp |  |  |
| Volume, V | 4,530 | 340 |  | vph |
| Peak Hour Factor, PHF | 0.99 | 0.84 |  |  |
| Total Trucks | 9.0\% | 2.2\% |  |  |
| Single Unit/Tractor-Trailer Mix | - | - |  |  |
| Passenger Car Equivalent, $\mathrm{E}_{T}$ | 2.0 | 2.0 |  |  |
| Heavy Vehicle Adjustment, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 | 0.978 |  |  |
| Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 4,988 | 414 |  | pcph |
| Adjacent Ramp Data |  |  |  |  |
|  |  | Upstream | Downstream |  |
| Adjacent Ramp Meeting Criteria |  | Yes | No |  |
| Type of Adjacent Ramp |  | Off |  |  |
| Distance to Adjacent Ramp |  | 2,740 |  | ft |
| Volume on Adjacent Ramp |  | 786 |  | pcph |


| Freeway Merge Report |  |  |
| :---: | :---: | :---: |
| Project I-80/Richards Blvd Interchange <br> Freeway Eastbound I-80 <br> Segment Richards Blvd On Ramp <br> Alternative Construction Year <br> Time Period PM Peak Hour |  |  |
| Estimation of Volume in Ramp Influence Area |  |  |
| Adjacent Upstream On-ramp Equilibrium Distance, $\mathrm{L}_{\mathrm{EQ}}$ <br> Adjacent Downstream On-ramp Equilibrium Distance, $\mathrm{L}_{\mathrm{EQ}}$ <br> Proportion of Freeway Vehicles in Lanes 1 and 2, $\mathrm{P}_{\mathrm{FM}}$ or $\mathrm{P}_{\mathrm{FD}}$ <br> Flow Rate in Lanes 1 and 2, $\mathrm{v}_{12}$ | 1,329 0.592 2,950 | ft <br> ft pcph |
| Capacity Checks |  |  |
| Flow Capacity |  | V/C Ratio |
| Entering General Purpose Lanes 4 4,988 7,200 | pcph | 0.69 |
| Exiting General Purpose Lanes $\quad$ 5,401 7,200 | pcph | 0.75 |
| On Ramp 414 | pcph | 0.20 |
| $\begin{array}{lll}\text { Ramp Influence Area } & \text { 3,364 } & 4,600\end{array}$ | pcph | 0.73 |
| Ramp Influence Area Density and Level of Service |  |  |
| Density in Ramp Influence Area, $D_{R}$ Level of Service, LOS | $\begin{gathered} 28.5 \\ D \end{gathered}$ | pcpmpl |
| Segment Speed, Flow, and Density |  |  |
| Speed Adjustment Factor, SAF | 1.00 |  |
| Speed Index, $\mathrm{M}_{\mathrm{S}}$ or $\mathrm{D}_{\mathrm{S}}$ | 0.389 |  |
| Average Speed in Ramp Influence Area, $\mathrm{S}_{\mathrm{R}}$ | 59.4 | mph |
| Average Flow in Outer Lanes, $\mathrm{v}_{\mathrm{OA}}$ | 2,037 | pcphpl |
| Average Speed in Outer Lanes, $\mathrm{S}_{0}$ | 64.9 | mph |
| Average Speed for Segment, S | 61.4 | mph |
| Density across All Lanes, D | 30.3 | pcpmpl |


|  | Freeway Basic Report |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Eastbound I-80 |
| Segment | Richards Blvd to Chiles Rd |
| Alternative | Construction Year |
| Time Period | PM Peak Hour |


|  | General |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
|  | Purpose Lanes - Geometric Data |  |  |  |  |  |
| General Purpose Lanes, N | 3 | ln | Terrain Type | Level |  |  |
| Segment Length, L | 5,710 | ft | Percent Grade | - |  |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |  |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 1.50 | $\mathrm{ramps} / \mathrm{mi}$ |  |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 70.9 | mph |  |


| General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


| General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :--- | :---: | :--- | :--- | :--- | :---: |
| Volume, V | 4,870 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.99 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,787 |  |
| Total Trucks | $9.0 \%$ | Capacity, | pcphpl |  |  |
| Single Unit/Tractor-Trailer Mix | - | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |  |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 | Volume-to-Capacity Ratio, v/c | 2,400 | pcphpl |  |


| General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 70.9 | mph |
| Lane Width Adjustment, f LW | 0.0 | mph | Average Speed, S | 66.4 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 26.9 | pcpmpl |
| Total Ramp Density Adjustment | 4.5 | mph | Level of Service, LOS | D |  |

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## Freeway Diverge Report



## Adjacent Ramp Data

Adjacent Ramp Meeting Criteria
Upstream Downstream

Type of Adjacent Ramp
Distance to Adjacent Ramp
Volume on Adjacent Ramp

## Freeway Diverge Report



|  | Freeway Basic Report |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Eastbound I-80 |
| Segment | Chiles Rd Off to Mace Rd On |
| Alternative | Construction Year |
| Time Period | PM Peak Hour |


|  | General |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
|  | Purpose Lanes - Geometric Data |  |  |  |  |  |
| General Purpose Lanes, N | 3 | ln | Terrain Type | Level |  |  |
| Segment Length, L | 1,000 | ft | Percent Grade | - |  |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |  |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 1.50 | $\mathrm{ramps} / \mathrm{mi}$ |  |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 70.9 | mph |  |


| General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


| General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Volume, V | 4,440 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.99 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,629 | pcphpl |
| Total Trucks | 9.0\% |  | Capacity, c | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - |  | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.68 |  |


| General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 70.9 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 68.4 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 23.8 | pcpmpl |
| Total Ramp Density Adjustment | 4.5 | mph | Level of Service, LOS | C |  |

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|  | Freeway Basic Report |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Westbound I-80 |
| Segment | East of Mace Blvd |
| Alternative | Construction Year No Build |
| Time Period | AM Peak Hour |


|  | General |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
|  | Purpose Lanes - Geometric Data |  |  |  |  |  |
| General Purpose Lanes, N | 3 | ln | Terrain Type | Level |  |  |
| Segment Length, L | 2,590 | ft | Percent Grade | - |  |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |  |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 1.50 | $\mathrm{ramps} / \mathrm{mi}$ |  |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 70.9 | mph |  |


| General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


| General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Volume, V | 4,550 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.98 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,687 | pcphpl |
| Total Trucks | 9.0\% |  | Capacity, c | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - |  | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.70 |  |


| General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 70.9 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 67.7 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 24.9 | pcpmpl |
| Total Ramp Density Adjustment | 4.5 | mph | Level of Service, LOS | C |  |



| Entering General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :--- | :---: | :--- | :--- | :--- | :--- |
| Volume, V | 4,550 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.98 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,687 | pcphpl |
| Total Trucks | $9.0 \%$ |  | Capacity, c | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |  |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.70 |  |


| Entering General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 71.3 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 68.0 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 24.8 | pcpmpl |
| Total Ramp Density Adjustment | 4.1 | mph | Level of Service, LOS | C |  |


| Segment General Purpose Lanes - Capacity, Speed, and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| General Purpose Lanes, N | 4 | $\ln$ | Average Speed, S | 70.5 | mph |
| Adjusted Capacity, cadj | 2,400 | pcphpl | Density, D | 20.1 | pcphpl |
| Flow Rate, vp | 1,419 | pcphpl | Level of Service, LOS | C |  |
| Volume-to-Capacity Ratio, v/c | 0.59 |  |  |  |  |

## Freeway Merge Report

| Freeway Merge Report |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Project I-80/Richards B <br> Freeway Westbound I-80 <br> Segment Mace Blvd to La <br> Alternative Construction Ye <br> Time Period AM Peak Hour |  |  |  |  |
| Geometric Data |  |  |  |  |
|  | Freeway | On Ramp |  |  |
| Number of Lanes, N | 3 | 2 |  |  |
| Free-Flow Speed, FFS | 71.3 | 45 |  | mph |
| Segment Length, L / Acceleration Length, LA | 1,850 | 0 |  | ft |
| Terrain Type | Level | Level |  |  |
| Percent Grade | - | - |  |  |
| Grade Length | - | - |  | ft |
| Segment Type / Ramp Type | Freeway | Right |  |  |
| Adjustment Factors |  |  |  |  |
|  | Freeway | On Ramp |  |  |
| Driver Population | Familiar | Familiar |  |  |
| Weather Type | Non-severe | Non-severe |  |  |
| Incident Type | No incident | No incident |  |  |
| Capacity Adjustment Factor, CAF | 1.00 | 1.00 |  |  |
| Demand Adjustment Factor, DAF | 1.00 | 1.00 |  |  |
| Volume Data |  |  |  |  |
| Junction Components | Freeway | On Ramp |  |  |
| Volume, V | 4,550 | 550 |  | vph |
| Peak Hour Factor, PHF | 0.98 | 0.92 |  |  |
| Total Trucks | 9.0\% | 3.0\% |  |  |
| Single Unit/Tractor-Trailer Mix | - | - |  |  |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 | 2.0 |  |  |
| Heavy Vehicle Adjustment, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 | 0.971 |  |  |
| Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 5,061 | 616 |  | pcph |
| Adjacent Ramp Data |  |  |  |  |
|  |  | Upstream | Downstream |  |
| Adjacent Ramp Meeting Criteria |  | No | No |  |
| Type of Adjacent Ramp |  |  |  |  |
| Distance to Adjacent Ramp |  |  |  | ft |
| Volume on Adjacent Ramp |  |  |  | pcph |

## Freeway Merge Report



| Ramp Influence Area Density and Level of Service |  |  |
| :--- | :--- | :---: |
|  | pcpmpl |  |
| Density in Ramp Influence Area, $D_{R}$ |  |  |

## Segment Speed, Flow, and Density

Speed Adjustment Factor, SAF
Speed Index, $\mathrm{M}_{\mathrm{S}}$ or $\mathrm{D}_{\mathrm{S}}$
Average Speed in Ramp Influence Area, $\mathrm{S}_{\mathrm{R}} \mathrm{mph}$

Average Flow in Outer Lanes, $\mathrm{v}_{\mathrm{OA}}$
pcphpl
mph
Average Speed in Outer Lanes, $\mathrm{S}_{0}$
mph
Density across All Lanes, D
pcpmpl

|  | Freeway Basic Report |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Westbound I-80 |
| Segment | Lane Drop to Olive Dr |
| Alternative | Construction Year No Build |
| Time Period | AM Peak Hour |


|  | General |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
|  | Purpose Lanes - Geometric Data |  |  |  |  |  |
| General Purpose Lanes, N | 3 | ln | Terrain Type | Level |  |  |
| Segment Length, L | 4,780 | ft | Percent Grade | - |  |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |  |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 1.33 | $\mathrm{ramps} / \mathrm{mi}$ |  |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 71.3 | mph |  |


| General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


|  | General Purpose Lanes - Demand and Capacity |  |  |  |  |
| :--- | :---: | :--- | :--- | :--- | :--- |
| Volume, V | 5,100 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.98 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,891 | pcphpl |
| Total Trucks | $9.0 \%$ |  | Capacity, c | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |  |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.79 |  |


| General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 71.3 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 65.0 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 29.1 | pcpmpl |
| Total Ramp Density Adjustment | 4.1 | mph | Level of Service, LOS | D |  |

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## Freeway Diverge Report

|  | Freeway Diverg |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Westbound I-80 |
| Segment | Olive Dr Off |
| Alternative | Construction Year No Build |
| Time Period | AM Peak Hour |


| Geometric Data |  |  |  |
| :---: | :---: | :---: | :---: |
|  | Freeway | Off Ramp |  |
| Number of Lanes, N | 3 | 1 |  |
| Free-Flow Speed, FFS | 71.3 | 35 | mph |
| Segment Length, L / Deceleration Length, LD | 1,500 | 150 | ft |
| Terrain Type | Level | Level |  |
| Percent Grade | - | - |  |
| Grade Length | - | - | ft |
| Segment Type / Ramp Type | Freeway | Right |  |
| Adjustment Factors |  |  |  |
|  | Freeway | Off Ramp |  |
| Driver Population | Familiar | Familiar |  |
| Weather Type | Non-severe | Non-severe |  |
| Incident Type | No incident | No incident |  |
| Capacity Adjustment Factor, CAF | 1.00 | 1.00 |  |
| Demand Adjustment Factor, DAF | 1.00 | 1.00 |  |


|  | Volume Data |  |  |  |
| :--- | :---: | :---: | :---: | :---: |
|  |  |  |  |  |
| Junction Components | $\underline{\text { Freeway }}$ | $\underline{\text { Off Ramp }}$ |  |  |
| Volume, V | 5,100 | 230 | vph |  |
| Peak Hour Factor, PHF | 0.98 | 0.92 |  |  |
| Total Trucks | $9.0 \%$ | $3.0 \%$ |  |  |
| Single Unit/Tractor-Trailer Mix | - | - |  |  |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 | 2.0 |  |  |
| Heavy Vehicle Adjustment, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 | 0.971 |  |  |
| Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 5,672 | 258 | pcph |  |

Adjacent Ramp Meeting Criteria

| Upstream | Downstream |
| :---: | :---: |
| No | Yes |
|  | Off |
|  | 2,390 |
|  | 403 |

## Freeway Diverge Report



|  | Freeway Basic Report |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Westbound I-80 |
| Segment | Olive Dr to Richards Blvd |
| Alternative | Construction Year No Build |
| Time Period | AM Peak Hour |


|  | General |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
|  | Purpose Lanes - Geometric Data |  |  |  |  |  |
| General Purpose Lanes, N | 3 | ln | Terrain Type | Level |  |  |
| Segment Length, L | 890 | ft | Percent Grade | - |  |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |  |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 1.83 | $\mathrm{ramps} / \mathrm{mi}$ |  |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 70.0 | mph |  |


| General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


|  | General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :--- | :--- | :--- |
| Volume, V | 4,870 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{Hv}}$ | 0.917 |  |  |
| Peak Hour Factor, PHF | 0.98 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,806 | pcphpl |  |
| Total Trucks | $9.0 \%$ |  | Capacity, c | 2,400 | pcphpl |  |
| Single Unit/Tractor-Trailer Mix | - | Adjusted Capacity, $\mathrm{c}_{\mathrm{adj}}$ | 2,400 | pcphpl |  |  |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 | Volume-to-Capacity Ratio, v/c | 0.75 |  |  |  |


| General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 70.0 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 65.8 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 27.5 | pcpmpl |
| Total Ramp Density Adjustment | 5.4 | mph | Level of Service, LOS | D |  |

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## Freeway Diverge Report

| Freeway Diverge Report |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Project I-80/Richards Blv <br> Freeway Westbound I-80 <br> Segment Richards Blvd NB <br> Alternative Construction Yea <br> Time Period AM Peak Hour |  |  |  |  |
| Geometric Data |  |  |  |  |
|  | Freeway |  | Off Ramp |  |
| Number of Lanes, N | 3 |  | 1 |  |
| Free-Flow Speed, FFS | 70.0 |  | 45 | mph |
| Segment Length, L / Deceleration Length, LD | 1,500 |  | 150 | ft |
| Terrain Type | Level |  | Level |  |
| Percent Grade | - |  | - |  |
| Grade Length | - |  | - | ft |
| Segment Type / Ramp Type | Freeway |  | Right |  |
| Adjustment Factors |  |  |  |  |
|  | Freeway |  | Off Ramp |  |
| Driver Population | Familiar |  | Familiar |  |
| Weather Type | Non-severe |  | Non-severe |  |
| Incident Type | No incident |  | No incident |  |
| Capacity Adjustment Factor, CAF | 1.00 |  | 1.00 |  |
| Demand Adjustment Factor, DAF | 1.00 |  | 1.00 |  |
| Volume Data |  |  |  |  |
| Junction Components | Freeway |  | Off Ramp |  |
| Volume, V | 4,870 |  | 360 | vph |
| Peak Hour Factor, PHF | 0.98 |  | 0.92 |  |
| Total Trucks | 9.0\% |  | 3.0\% |  |
| Single Unit/Tractor-Trailer Mix | - |  | - |  |
| Passenger Car Equivalent, $\mathrm{E}_{T}$ | 2.0 |  | 2.0 |  |
| Heavy Vehicle Adjustment, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  | 0.971 |  |
| Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 5,417 |  | 403 | pcph |
| Adjacent Ramp Data |  |  |  |  |
|  |  | Upstream | Downstream |  |
| Adjacent Ramp Meeting Criteria |  | Yes | No |  |
| Type of Adjacent Ramp |  | Off |  |  |
| Distance to Adjacent Ramp |  | 2,390 |  | ft |
| Volume on Adjacent Ramp |  | 258 |  | pcph |

## Freeway Diverge Report



|  | Freeway Basic Report |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Westbound I-80 |
| Segment | Richards Blvd NB Off to On |
| Alternative | Construction Year No Build |
| Time Period | AM Peak Hour |


|  | General |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
|  | Purpose Lanes - Geometric Data |  |  |  |  |  |
| General Purpose Lanes, N | 3 | ln | Terrain Type | Level |  |  |
| Segment Length, L | 430 | ft | Percent Grade | - |  |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |  |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 1.83 | $\mathrm{ramps} / \mathrm{mi}$ |  |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 70.0 | mph |  |


| General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


|  | General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :--- | :--- | :--- |
| Volume, V | 4,510 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{Hv}}$ | 0.917 |  |  |
| Peak Hour Factor, PHF | 0.98 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,672 | pcphpl |  |
| Total Trucks | $9.0 \%$ |  | Capacity, c | 2,400 | pcphpl |  |
| Single Unit/Tractor-Trailer Mix | - | Adjusted Capacity, $\mathrm{c}_{\mathrm{adj}}$ | 2,400 | pcphpl |  |  |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 | Volume-to-Capacity Ratio, v/c | 0.70 |  |  |  |


| General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 70.0 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 67.4 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 24.8 | pcpmpl |
| Total Ramp Density Adjustment | 5.4 | mph | Level of Service, LOS | C |  |

## Freeway Weave Report

| Project | I-80/Richards Blvd Interchange |
| :--- | :--- |
| Freeway | Westbound I-80 |
| Segment | Richards Blvd NB On to SB Off |
| Alternative | Construction Year No Build |
| Time period | AM Peak Hour |

## Geometric Data

Segment Type
Weaving Configuration
Number of Lanes, N
Weaving Segment Length, $L_{S}$
Interchange Density, ID
Number of Manuever Lanes, $\mathrm{N}_{\mathrm{WL}}$
On Ramp to Freeway Lane Changes, $\mathrm{LC}_{\mathrm{RF}}$
Freeway to Off Ramp Lane Changes, $\mathrm{LC}_{\mathrm{FR}}$
On Ramp to Off Ramp Lane Changes, $\mathrm{LC}_{\text {RR }}$

Freeway
One-sided

| 4 | $\ln$ |
| :---: | :---: |
| 500 | ft |
| 0.8 | $\mathrm{int} / \mathrm{mi}$ |
| 2.0 | $\ln$ |

2.0

In
1
1
0

## Adjustment Factors

| Driver Population | Familiar |
| :--- | :---: |
| Weather Type | Non-severe |
| Incident Type | No incident |
| Capacity Adjustment Factor, CAF |  |
| Demand Adjustment Factor, DAF |  |

Volume Data

Volume, V
Peak-hour factor, PHF
Total Trucks
Terrain Type
Grade
Length
SUT/TT Mix
Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$
Heavy Vehicle Adjustment, $\mathrm{f}_{\mathrm{HV}}$
Demand Adjustment Factor, DAF
Flow Rate, $\mathrm{v}_{\mathrm{p}}$


Weaving Flow Rate, vW
Non-Weaving Flow Rate, vNW
829 Total Flow Rate,
5,623
4,794 Volume Ratio, VR 0.148

## Freeway Weave Report

| Project | I-80/Richards Blvd Interchange |
| :--- | :--- |
| Freeway | Westbound I-80 |
| Segment | Richards Blvd NB On to SB Off |
| Alternative | Construction Year No Build |
| Time period | AM Peak Hour |


|  | Capacity |  |  |
| :--- | :---: | :---: | :---: |
|  |  |  |  |
| Maximum Weaving Length, $\mathrm{L}_{\mathrm{MAX}}$ | 4,007 | ft |  |
| Weaving Length Check | OK |  |  |
| Freeway Maximum Capacity, $\mathrm{c}_{\mathrm{IFL}}$ | 2,400 | pchpl |  |
| Density-Based Capacity, $\mathrm{c}_{\mathrm{IWL}}$ | 9,332 | pchpl |  |
| Demand Flow-Based Capacity, $\mathrm{c}_{\mathrm{IW}}$ | 15,087 | pch |  |
| Weaving Segment Capacity, $\mathrm{c}_{\mathrm{w}}$ | 15,087 | vph |  |
| Adjusted Weaving Area Capacity, $\mathrm{c}_{\mathrm{wa}}$ | 15,087 | vph |  |
| Volume-to-Capacity Ratio, $\mathrm{v} / \mathrm{c}$ | 0.35 |  |  |


| Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: |
|  |  | 829 |  |  |  |
| Minimum Lane Change Rate, $\mathrm{LC}_{\mathrm{MIN}}$ | 849 | $\mathrm{Ic} / \mathrm{h}$ |  |  |  |
| Weaving Lane Change Rate, $\mathrm{LC}_{\mathrm{W}}$ | 200 |  |  |  |  |
| Non-weaving Vehicle Index, $\mathrm{I}_{\mathrm{NW}}$ | 488 | $\mathrm{Ic} / \mathrm{h}$ |  |  |  |
| Non-weaving Lane Change Rate, $\mathrm{LC}_{\mathrm{NW}}$ | 1,337 | $\mathrm{Ic} / \mathrm{h}$ |  |  |  |
| Total Lane Change Rate, $\mathrm{LC}_{\mathrm{ALL}}$ | 0.491 |  |  |  |  |
| Weaving Intensity Factor, W | 51.9 | mph |  |  |  |
| Average Weaving Speed, $\mathrm{S}_{\mathrm{W}}$ | 57.3 | mph |  |  |  |
| Average Non-Weaving Speed, $\mathrm{S}_{\mathrm{NW}}$ | 56.5 | mph |  |  |  |
| Average Speed, S | 24.9 | pcpmpl |  |  |  |
| Density, D | C |  |  |  |  |
| Level of Service, LOS |  |  |  |  |  |

## Capacity Checks

|  | $\underline{\text { Flow }}$ | Capacity |  | V/C Ratio |
| :--- | :---: | :---: | :---: | :---: |
| Entering General Purpose Lanes | 5,016 | 7,200 | pcph | 0.70 |
| Exiting General Purpose Lanes | 5,263 | 7,200 | pcph | 0.73 |
| On Ramp | 470 | 1,900 | pcph | 0.25 |
| Off Ramp | 224 | 1,900 | pcph | 0.12 |

## Leisch Method for Weaving Analysis

## Data Input

Number of Entering Mainline Lanes
Number of Lanes in Weaving Section Length of Weaving Section (feet)

| $N_{b}$ | 3 |
| :---: | :---: |
| $N$ | 4 |
|  | 500 |

On-ramp to Mainline ( $\mathrm{W}_{1}$ )

| 420 |
| :---: |
| $2.2 \%$ |
| 2.0 |
| 429 |

Volume (vph)*
Truck Percentage
PCE for Trucks
Volume (pcph)


The LOS in the chart above refers to the capacity of weaving traffic only; through and ramp to ramp traffic is not included

* Note: Do not adjust by a Peak Hour Factor (PHF). The methodology incorporates the PHF in the Service Volume tables.

Sources: Completion of Procedures for Analysis and Design of Traffic Weaving Sections, Jack E. Leisch \& Associates, September 1983 and
Highway Design Manual , California Department of Transportation, 2014

|  | Freeway Basic Report |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Westbound I-80 |
| Segment | Richards Blvd SB Off to On |
| Alternative | Construction Year No Build |
| Time Period | AM Peak Hour |


|  | General |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
|  | Purpose Lanes - Geometric Data |  |  |  |  |  |
| General Purpose Lanes, N | 3 | ln | Terrain Type | Level |  |  |
| Segment Length, L | 210 | ft | Percent Grade | - |  |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |  |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 1.83 | $\mathrm{ramps} / \mathrm{mi}$ |  |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 70.0 | mph |  |


| General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


| General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Volume, V | 4,730 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.98 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,754 | pcphpl |
| Total Trucks | 9.0\% |  | Capacity, c | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - |  | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.73 |  |


| General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 70.0 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 66.5 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 26.4 | pcpmpl |
| Total Ramp Density Adjustment | 5.4 | mph | Level of Service, LOS | D |  |

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| Freeway Basic Report |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Project <br> Freeway <br> Segment <br> Alternative <br> Time Period | I-80/Richards Blvd Interchange <br> Westbound I-80 <br> Richards Blvd to Lane Add <br> Construction Year No Build <br> AM Peak Hour |  |  |  |
| Entering General Purpose Lanes - Geometric Data |  |  |  |  |
| General Purpose Lanes, N Segment Length, L <br> Base Free Flow Speed, BFFS <br> Lane Width <br> Right Side Lateral Clearance | 4 ln <br> 3,770 ft <br> 75.4 mph <br> 12.0 ft <br> 6.0 ft | Terrain Type <br> Percent Grade <br> Grade Length <br> Total Ramp Density, TRD <br> Free Flow Speed, FFS | Level $1.67$ $70.4$ | mi $\mathrm{ramps} / \mathrm{mi}$ mph |
| Entering General Purpose Lanes - Adjustment Factors |  |  |  |  |
| Driver Population Weather Type Incident Type | Familiar <br> Non-severe <br> No incident | Speed Adjustment Factor, SAF <br> Capacity Adjustment Factor, CAF <br> Demand Adjustment Factor, DAF | $\begin{aligned} & 1.00 \\ & 1.00 \\ & 1.00 \end{aligned}$ |  |


| Entering General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :--- | :---: | :--- | :--- | :--- | :--- |
| Volume, V | 4,730 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.98 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,315 | pcphpl |
| Total Trucks | $9.0 \%$ |  | Capacity, c | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |  |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.55 |  |


| Entering General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 70.4 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 70.2 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 18.7 | pcpmpl |
| Total Ramp Density Adjustment | 5.0 | mph | Level of Service, LOS | C |  |

## Segment General Purpose Lanes - Capacity, Speed, and Density

| General Purpose Lanes, N | 4 | $\ln$ | Average Speed, S | 70.1 | mph |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Adjusted Capacity, cadj | 2,400 | pcphpl | Density, D | 19.3 | pcphpl |
| Flow Rate, vp | 1,352 | pcphpl | Level of Service, LOS | C |  |
| Volume-to-Capacity Ratio, v/c | 0.56 |  |  |  |  |


| Freeway Merge Report |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Project I-80/Richards B <br> Freeway Westbound I-80 <br> Segment Richards Blvd to <br> Alternative Construction Ye <br> Time Period AM Peak Hour |  |  |  |  |
| Geometric Data |  |  |  |  |
|  | Freeway | On Ramp |  |  |
| Number of Lanes, N | 4 | 1 |  |  |
| Free-Flow Speed, FFS | 70.4 | 45 |  | mph |
| Segment Length, L / Acceleration Length, LA | 3,770 | 0 |  | ft |
| Terrain Type | Level | Level |  |  |
| Percent Grade | - | - |  |  |
| Grade Length | - | - |  | ft |
| Segment Type / Ramp Type | Freeway | Right |  |  |
| Adjustment Factors |  |  |  |  |
|  | Freeway | On Ramp |  |  |
| Driver Population | Familiar | Familiar |  |  |
| Weather Type | Non-severe | Non-severe |  |  |
| Incident Type | No incident | No incident |  |  |
| Capacity Adjustment Factor, CAF | 1.00 | 1.00 |  |  |
| Demand Adjustment Factor, DAF | 1.00 | 1.00 |  |  |
| Volume Data |  |  |  |  |
| Junction Components | Freeway | On Ramp |  |  |
| Volume, V | 4,730 | 130 |  | vph |
| Peak Hour Factor, PHF | 0.98 | 0.92 |  |  |
| Total Trucks | 9.0\% | 3.0\% |  |  |
| Single Unit/Tractor-Trailer Mix | - | - |  |  |
| Passenger Car Equivalent, $\mathrm{E}_{T}$ | 2.0 | 2.0 |  |  |
| Heavy Vehicle Adjustment, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 | 0.971 |  |  |
| Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 5,261 | 146 |  | pcph |
| Adjacent Ramp Data |  |  |  |  |
|  |  | Upstream | Downstream |  |
| Adjacent Ramp Meeting Criteria |  | No | No |  |
| Type of Adjacent Ramp |  |  |  |  |
| Distance to Adjacent Ramp |  |  |  | ft |
| Volume on Adjacent Ramp |  |  |  | pcph |

## Freeway Merge Report



| Ramp Influence Area Density and Level of Service |  |  |  |
| :--- | :--- | :---: | :---: |
| Density in Ramp Influence Area, $D_{R}$ | pcpmpl |  |  |
| Level of Service, LOS |  |  |  |

## Segment Speed, Flow, and Density

Speed Adjustment Factor, SAF
Speed Index, $\mathrm{M}_{\mathrm{S}}$ or $\mathrm{D}_{\mathrm{S}}$
Average Speed in Ramp Influence Area, $\mathrm{S}_{\mathrm{R}} \mathrm{mph}$

Average Flow in Outer Lanes, $\mathrm{v}_{\mathrm{OA}}$
pcphpl
mph
Average Speed in Outer Lanes, $\mathrm{S}_{0}$
mph
Density across All Lanes, D
pcpmpl

## Freeway Diverge Report

|  | Freeway Diverg |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Westbound I-80 |
| Segment | Lane Add to Old Davis Off |
| Alternative | Construction Year No Build |
| Time Period | AM Peak Hour |


| Geometric Data |  |  |  |
| :---: | :---: | :---: | :---: |
|  | Freeway | Off Ramp |  |
| Number of Lanes, N | 5 | 1 |  |
| Free-Flow Speed, FFS | 70.0 | 45 | mph |
| Segment Length, L / Deceleration Length, LD | 1,190 | 150 | ft |
| Terrain Type | Level | Level |  |
| Percent Grade | - | - |  |
| Grade Length | - | - | ft |
| Segment Type / Ramp Type | Freeway | Right |  |
| Adjustment Factors |  |  |  |
|  | Freeway | Off Ramp |  |
| Driver Population | Familiar | Familiar |  |
| Weather Type | Non-severe | Non-severe |  |
| Incident Type | No incident | No incident |  |
| Capacity Adjustment Factor, CAF | 1.00 | 1.00 |  |
| Demand Adjustment Factor, DAF | 1.00 | 1.00 |  |
| Volume Data |  |  |  |
| Junction Components | Freeway | Off Ramp |  |
| Volume, V | 4,860 | 490 | vph |
| Peak Hour Factor, PHF | 0.98 | 0.92 |  |
| Total Trucks | 9.0\% | 3.0\% |  |
| Single Unit/Tractor-Trailer Mix | - | - |  |
| Passenger Car Equivalent, $\mathrm{E}_{T}$ | 2.0 | 2.0 |  |
| Heavy Vehicle Adjustment, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 | 0.971 |  |
| Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 5,406 | 549 | pcph |

Adjacent Ramp Meeting Criteria
Upstream Downstream

Type of Adjacent Ramp
Distance to Adjacent Ramp
Volume on Adjacent Ramp
pcph

## Freeway Diverge Report



|  | Freeway Basic Report |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Westbound I-80 |
| Segment | West of Old Davis Rd |
| Alternative | Construction Year No Build |
| Time Period | AM Peak Hour |


|  | General |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
|  | Purpose Lanes - Geometric Data |  |  |  |  |  |
| General Purpose Lanes, N | 5 | ln | Terrain Type | Level |  |  |
| Segment Length, L | 1,350 | ft | Percent Grade | - |  |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |  |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 1.83 | $\mathrm{ramps} / \mathrm{mi}$ |  |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 70.0 | mph |  |


| General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


| General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Volume, V | 4,370 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.98 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 972 | pcphpl |
| Total Trucks | 9.0\% |  | Capacity, c | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - |  | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.41 |  |


| General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 70.0 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 70.0 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 13.9 | pcpmpl |
| Total Ramp Density Adjustment | 5.4 | mph | Level of Service, LOS | B |  |

$\qquad$

|  | Freeway Basic Report |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Westbound I-80 |
| Segment | East of Mace Blvd |
| Alternative | Construction Year No Build |
| Time Period | PM Peak Hour |


|  | General |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
|  | Purpose Lanes - Geometric Data |  |  |  |  |  |
| General Purpose Lanes, N | 3 | ln | Terrain Type | Level |  |  |
| Segment Length, L | 2,590 | ft | Percent Grade | - |  |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |  |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 1.50 | $\mathrm{ramps} / \mathrm{mi}$ |  |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 70.9 | mph |  |


| General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


| General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Volume, V | 4,290 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.99 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,574 | pcphpl |
| Total Trucks | 9.0\% |  | Capacity, c | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - |  | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.66 |  |


| General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 70.9 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 68.9 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 22.8 | pcpmpl |
| Total Ramp Density Adjustment | 4.5 | mph | Level of Service, LOS | C |  |


| Freeway Basic Report |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Project <br> Freeway <br> Segment <br> Alternative <br> Time Period | I-80/Richards Blvd Interchange <br> Westbound I-80 <br> Mace Blvd to Lane Drop <br> Construction Year No Build <br> PM Peak Hour |  |  |  |
| Entering General Purpose Lanes - Geometric Data |  |  |  |  |
| General Purpose Lanes, N Segment Length, L <br> Base Free Flow Speed, BFFS <br> Lane Width <br> Right Side Lateral Clearance | 3 ln <br> 1,850 ft <br> 75.4 mph <br> 12.0 ft <br> 6.0 ft | Terrain Type <br> Percent Grade <br> Grade Length <br> Total Ramp Density, TRD <br> Free Flow Speed, FFS | Level $1.33$ <br> 71.3 | mi $\mathrm{ramps} / \mathrm{mi}$ mph |
| Entering General Purpose Lanes - Adjustment Factors |  |  |  |  |
| Driver Population Weather Type Incident Type | Familiar <br> Non-severe <br> No incident | Speed Adjustment Factor, SAF <br> Capacity Adjustment Factor, CAF <br> Demand Adjustment Factor, DAF | $\begin{aligned} & 1.00 \\ & 1.00 \\ & 1.00 \end{aligned}$ |  |


| Entering General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :--- | :---: | :--- | :--- | :--- | :--- |
| Volume, V | 4,290 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.99 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,574 | pcphpl |
| Total Trucks | $9.0 \%$ |  | Capacity, c | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |  |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.66 |  |


| Entering General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS ${ }_{\text {adj }}$ | 71.3 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{Lw}}$ | 0.0 | mph | Average Speed, S | 69.2 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 22.7 | pcpmpl |
| Total Ramp Density Adjustment | 4.1 | mph | Level of Service, LOS | C |  |


| Segment General Purpose Lanes - Capacity, Speed, and Density |  |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
| General Purpose Lanes, N | 4 | $\ln$ | Average Speed, S | 70.9 | mph |  |
| Adjusted Capacity, cadj | 2,400 | pcphpl | Density, D | 18.7 | pcphpl |  |
| Flow Rate, vp | 1,324 | pcphpl | Level of Service, LOS | C |  |  |
| Volume-to-Capacity Ratio, v/c | 0.55 |  |  |  |  |  |

## Freeway Merge Report

| Freeway Merge Report |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Project I-80/Richards B <br> Freeway Westbound I-80 <br> Segment Mace Blvd to La <br> Alternative Construction Ye <br> Time Period PM Peak Hour |  |  |  |  |
| Geometric Data |  |  |  |  |
|  | Freeway | On Ramp |  |  |
| Number of Lanes, N | 3 | 2 |  |  |
| Free-Flow Speed, FFS | 71.3 | 45 |  | mph |
| Segment Length, L / Acceleration Length, LA | 1,850 | 0 |  | ft |
| Terrain Type | Level | Level |  |  |
| Percent Grade | - | - |  |  |
| Grade Length | - | - |  | ft |
| Segment Type / Ramp Type | Freeway | Right |  |  |
| Adjustment Factors |  |  |  |  |
|  | Freeway | On Ramp |  |  |
| Driver Population | Familiar | Familiar |  |  |
| Weather Type | Non-severe | Non-severe |  |  |
| Incident Type | No incident | No incident |  |  |
| Capacity Adjustment Factor, CAF | 1.00 | 1.00 |  |  |
| Demand Adjustment Factor, DAF | 1.00 | 1.00 |  |  |
| Volume Data |  |  |  |  |
| Junction Components | Freeway | On Ramp |  |  |
| Volume, V | 4,290 | 510 |  | vph |
| Peak Hour Factor, PHF | 0.99 | 0.92 |  |  |
| Total Trucks | 9.0\% | 3.0\% |  |  |
| Single Unit/Tractor-Trailer Mix | - | - |  |  |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 | 2.0 |  |  |
| Heavy Vehicle Adjustment, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 | 0.971 |  |  |
| Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 4,723 | 571 |  | pcph |
| Adjacent Ramp Data |  |  |  |  |
|  |  | Upstream | Downstream |  |
| Adjacent Ramp Meeting Criteria |  | No | No |  |
| Type of Adjacent Ramp |  |  |  |  |
| Distance to Adjacent Ramp |  |  |  | ft |
| Volume on Adjacent Ramp |  |  |  | pcph |

## Freeway Merge Report



| Ramp Influence Area Density and Level of Service |  |  |
| :--- | :--- | :---: |
|  | pcpmpl |  |
| Density in Ramp Influence Area, $D_{R}$ |  |  |

## Segment Speed, Flow, and Density

Speed Adjustment Factor, SAF
Speed Index, $\mathrm{M}_{\mathrm{S}}$ or $\mathrm{D}_{\mathrm{S}}$
Average Speed in Ramp Influence Area, $\mathrm{S}_{\mathrm{R}} \mathrm{mph}$

Average Flow in Outer Lanes, $\mathrm{v}_{\mathrm{OA}}$
pcphpl
mph
Average Speed in Outer Lanes, $\mathrm{S}_{0}$
mph
Density across All Lanes, D
pcpmpl

|  | Freeway Basic Report |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Westbound I-80 |
| Segment | Lane Drop to Olive Dr |
| Alternative | Construction Year No Build |
| Time Period | PM Peak Hour |


|  | General |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
|  | Purpose Lanes - Geometric Data |  |  |  |  |  |
| General Purpose Lanes, N | 3 | ln | Terrain Type | Level |  |  |
| Segment Length, L | 4,780 | ft | Percent Grade | - |  |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |  |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 1.33 | $\mathrm{ramps} / \mathrm{mi}$ |  |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 71.3 | mph |  |


| General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


| General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Volume, V | 4,800 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.99 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,762 | pcphpl |
| Total Trucks | 9.0\% |  | Capacity, c | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - |  | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.73 |  |


| General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 71.3 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 67.0 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 26.3 | pcpmpl |
| Total Ramp Density Adjustment | 4.1 | mph | Level of Service, LOS | D |  |

$\qquad$

## Freeway Diverge Report

|  | Freeway Diverg |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Westbound I-80 |
| Segment | Olive Dr Off |
| Alternative | Construction Year No Build |
| Time Period | PM Peak Hour |


| Geometric Data |  |  |  |
| :---: | :---: | :---: | :---: |
|  | Freeway | Off Ramp |  |
| Number of Lanes, N | 3 | 1 |  |
| Free-Flow Speed, FFS | 71.3 | 35 | mph |
| Segment Length, L / Deceleration Length, LD | 1,500 | 150 | ft |
| Terrain Type | Level | Level |  |
| Percent Grade | - | - |  |
| Grade Length | - | - | ft |
| Segment Type / Ramp Type | Freeway | Right |  |
| Adjustment Factors |  |  |  |
|  | Freeway | Off Ramp |  |
| Driver Population | Familiar | Familiar |  |
| Weather Type | Non-severe | Non-severe |  |
| Incident Type | No incident | No incident |  |
| Capacity Adjustment Factor, CAF | 1.00 | 1.00 |  |
| Demand Adjustment Factor, DAF | 1.00 | 1.00 |  |
| Volume Data |  |  |  |
| Junction Components | Freeway | Off Ramp |  |
| Volume, V | 4,800 | 130 | vph |
| Peak Hour Factor, PHF | 0.99 | 0.92 |  |
| Total Trucks | 9.0\% | 3.0\% |  |
| Single Unit/Tractor-Trailer Mix | - | - |  |
| Passenger Car Equivalent, $\mathrm{E}_{T}$ | 2.0 | 2.0 |  |
| Heavy Vehicle Adjustment, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 | 0.971 |  |
| Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 5,285 | 146 | pcph |

Adjacent Ramp Meeting Criteria
Type of Adjacent Ramp
Distance to Adjacent Ramp

| Upstream |  |  |  |
| :---: | :---: | :---: | :---: |
| No |  |  |  |
|  | Yewnstream |  |  |
|  | Off |  |  |
|  | 2,390 | ft |  |
|  | 246 | pcph |  |

## Freeway Diverge Report



|  | Freeway Basic Report |
| :--- | :--- |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Westbound I-80 |
| Segment | Olive Dr to Richards Blvd |
| Alternative | Construction Year No Build |
| Time Period | PM Peak Hour |


|  | General |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
|  | Purpose Lanes - Geometric Data |  |  |  |  |  |
| General Purpose Lanes, N | 3 | ln | Terrain Type | Level |  |  |
| Segment Length, L | 890 | ft | Percent Grade | - |  |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |  |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 1.83 | $\mathrm{ramps} / \mathrm{mi}$ |  |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 70.0 | mph |  |


| General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


| General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Volume, V | 4,670 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.99 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,714 | pcphpl |
| Total Trucks | 9.0\% |  | Capacity, c | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - |  | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.71 |  |


| General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 70.0 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 67.0 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 25.6 | pcpmpl |
| Total Ramp Density Adjustment | 5.4 | mph | Level of Service, LOS | C |  |

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## Freeway Diverge Report

|  | Freeway Diverg |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Westbound I-80 |
| Segment | Richards Blvd NB Off |
| Alternative | Construction Year No Build |
| Time Period | PM Peak Hour |


|  |  |  |  |
| :--- | :---: | :---: | :---: |
|  | Geometric Data |  |  |
|  |  |  |  |
| Number of Lanes, N | Freeway | Off Ramp |  |
| Free-Flow Speed, FFS | 3 | 1 |  |
| Segment Length, L Deceleration Length, LD | 70.0 | 45 | mph |
| Terrain Type | 1,500 | 150 | ft |
| Percent Grade | Level | Level |  |
| Grade Length | - | - | - |
| Segment Type / Ramp Type | - | Right | ft |

## Adjustment Factors

|  | $\frac{\text { Freeway }}{}$ | $\frac{\text { Off Ramp }}{}$ |
| :--- | :---: | :---: |
| Driver Population | Familiar | Familiar |
| Weather Type | Non-severe | Non-severe |
| Incident Type | No incident | No incident |
| Capacity Adjustment Factor, CAF | 1.00 | 1.00 |
| Demand Adjustment Factor, DAF | 1.00 | 1.00 |


|  | Volume Data |  |  |  |
| :--- | :---: | :---: | :---: | :---: |
|  |  |  |  |  |
| Junction Components | $\underline{\text { Freeway }}$ | $\underline{\text { Off Ramp }}$ |  |  |
| Volume, V | 4,670 | 220 | vph |  |
| Peak Hour Factor, PHF | 0.99 | 0.92 |  |  |
| Total Trucks | $9.0 \%$ | $3.0 \%$ |  |  |
| Single Unit/Tractor-Trailer Mix | - | - |  |  |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 | 2.0 |  |  |
| Heavy Vehicle Adjustment, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 | 0.971 |  |  |
| Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 5,142 | 246 | pcph |  |


| Upstream | Downstream |
| :---: | :---: |
| Yes | No |
| Off |  |
| 2,390 |  |
| 146 |  |

## Freeway Diverge Report



|  | Freeway Basic Report |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Westbound I-80 |
| Segment | Richards Blvd NB Off to On |
| Alternative | Construction Year No Build |
| Time Period | PM Peak Hour |


|  | General |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
|  | Purpose Lanes - Geometric Data |  |  |  |  |  |
| General Purpose Lanes, N | 3 | ln | Terrain Type | Level |  |  |
| Segment Length, L | 430 | ft | Percent Grade | - |  |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |  |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 1.83 | $\mathrm{ramps} / \mathrm{mi}$ |  |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 70.0 | mph |  |


| General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


| General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :--- | :---: | :--- | :--- | :--- | :--- |
| Volume, V | 4,450 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.99 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,633 | pcphpl |
| Total Trucks | $9.0 \%$ |  | Capacity, | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |  |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.68 |  |


| General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 70.0 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 67.9 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 24.1 | pcpmpl |
| Total Ramp Density Adjustment | 5.4 | mph | Level of Service, LOS | C |  |

## Freeway Weave Report

| Project | I-80/Richards Blvd Interchange |
| :--- | :--- |
| Freeway | Westbound I-80 |
| Segment | Richards Blvd NB On to SB Off |
| Alternative | Construction Year No Build |
| Time period | PM Peak Hour |

## Geometric Data

Segment Type
Weaving Configuration
Number of Lanes, N
Weaving Segment Length, $L_{S}$
Interchange Density, ID
Number of Manuever Lanes, $\mathrm{N}_{\mathrm{WL}}$
On Ramp to Freeway Lane Changes, $\mathrm{LC}_{\mathrm{RF}}$
Freeway to Off Ramp Lane Changes, $\mathrm{LC}_{\mathrm{FR}}$
On Ramp to Off Ramp Lane Changes, $\mathrm{LC}_{\text {RR }}$

Freeway
One-sided

| 4 | $\ln$ |
| :---: | :---: |
| 500 | ft |
| 0.8 | $\mathrm{int} / \mathrm{mi}$ |
| 2.0 | ln |

In

1
1
0

## Adjustment Factors

| Driver Population | Familiar |
| :--- | :---: |
| Weather Type | Non-severe |
| Incident Type | No incident |
| Capacity Adjustment Factor, CAF |  |
| Demand Adjustment Factor, DAF |  |

Volume Data

Volume, V
Peak-hour factor, PHF
Total Trucks
Terrain Type
Grade
Length
SUT/TT Mix
Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$
Heavy Vehicle Adjustment, $\mathrm{f}_{\mathrm{HV}}$
Demand Adjustment Factor, DAF
Flow Rate, $\mathrm{v}_{\mathrm{p}}$

Weaving Flow Rate, vW
Non-Weaving Flow Rate, vNW


## Freeway Weave Report

| Project | I-80/Richards Blvd Interchange |
| :--- | :--- |
| Freeway | Westbound I-80 |
| Segment | Richards Blvd NB On to SB Off |
| Alternative | Construction Year No Build |
| Time period | PM Peak Hour |


|  | Capacity |  |  |
| :--- | :---: | :---: | :---: |
|  |  |  |  |
| Maximum Weaving Length, $\mathrm{L}_{\mathrm{MAX}}$ | 4,028 | ft |  |
| Weaving Length Check | OK |  |  |
| Freeway Maximum Capacity, $\mathrm{c}_{\mathrm{IFL}}$ | 2,400 | pchpl |  |
| Density-Based Capacity, $\mathrm{c}_{\mathrm{IWL}}$ | 9,330 | pchpl |  |
| Demand Flow-Based Capacity, $\mathrm{c}_{\mathrm{IW}}$ | 14,869 | pch |  |
| Weaving Segment Capacity, $\mathrm{c}_{\mathrm{w}}$ | 14,869 | vph |  |
| Adjusted Weaving Area Capacity, $\mathrm{c}_{\text {wa }}$ | 14,869 | vph |  |
| Volume-to-Capacity Ratio, v/c | 0.35 |  |  |


|  | Speed and Density |  |
| :--- | :---: | :---: |
|  |  |  |
| Minimum Lane Change Rate, $\mathrm{LC}_{\mathrm{MIN}}$ | 845 | $\mathrm{Ic} / \mathrm{h}$ |
| Weaving Lane Change Rate, $\mathrm{LC}_{\mathrm{W}}$ | 865 | $\mathrm{Ic} / \mathrm{h}$ |
| Non-weaving Vehicle Index, $\mathrm{I}_{\mathrm{NW}}$ | 200 |  |
| Non-weaving Lane Change Rate, $\mathrm{LC}_{\mathrm{NW}}$ | 489 | $\mathrm{Ic} / \mathrm{h}$ |
| Total Lane Change Rate, $\mathrm{LC}_{\mathrm{ALL}}$ | 1,354 | $\mathrm{Ic} / \mathrm{h}$ |
| Weaving Intensity Factor, W | 0.496 |  |
| Average Weaving Speed, $\mathrm{S}_{\mathrm{W}}$ | 51.8 | mph |
| Average Non-Weaving Speed, $\mathrm{S}_{\mathrm{NW}}$ | 57.2 | mph |
| Average Speed, S | 56.3 | mph |
| Density, D | 25.1 | pcpmpl |
| Level of Service, LOS | C |  |

## Capacity Checks

Entering General Purpose Lanes
Exiting General Purpose Lanes
On Ramp
Off Ramp

| Flow |  | Capacity |  | V/C Ratio |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 4,899 |  | 7,200 |  | pcph | 0.68 |
| 5,392 |  | 7,200 |  | pcph | 0.75 |
| 593 |  | 1,900 |  | pcph | 0.31 |
| 101 |  | 1,900 |  | pcph | 0.05 |

## Leisch Method for Weaving Analysis

## Data Input

Number of Entering Mainline Lanes
Number of Lanes in Weaving Section Length of Weaving Section (feet)

| Total Weaving Section (V) |  |
| :--- | :---: |
| Volume (vph)* | 4,980 |
| Truck Percentage | $8.1 \%$ |
| PCE for Trucks | 2.0 |
| Volume (pcph) | 5,382 |

Mainline to Off-ramp (W2)

| 530 | Volume (vph)* |
| :---: | :--- |
| $1.8 \%$ | Truck Percentage |
| 2.0 | PCE for Trucks |
| 540 | Volume (pcph) |



The LOS in the chart above refers to the capacity of weaving traffic only; through and ramp to ramp traffic is not included.

* Note: Do not adjust by a Peak Hour Factor (PHF). The methodology incorporates the PHF in the Service Volume tables.

Sources: Completion of Procedures for Analysis and Design of Traffic Weaving Sections, Jack E. Leisch \& Associates, September 1983 and
Highway Design Manual , California Department of Transportation, 2014

|  | Freeway Basic Report |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Westbound I-80 |
| Segment | Richards Blvd SB Off to On |
| Alternative | Construction Year No Build |
| Time Period | PM Peak Hour |


|  | General |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
|  | Purpose Lanes - Geometric Data |  |  |  |  |  |
| General Purpose Lanes, N | 3 | ln | Terrain Type | Level |  |  |
| Segment Length, L | 210 | ft | Percent Grade | - |  |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |  |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 1.83 | $\mathrm{ramps} / \mathrm{mi}$ |  |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 70.0 | mph |  |


| General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


| General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Volume, V | 4,890 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.99 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,795 | pcphpl |
| Total Trucks | 9.0\% |  | Capacity, c | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - |  | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.75 |  |


| General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 70.0 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 65.9 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 27.2 | pcpmpl |
| Total Ramp Density Adjustment | 5.4 | mph | Level of Service, LOS | D |  |

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| Freeway Basic Report |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Project <br> Freeway <br> Segment <br> Alternative <br> Time Period | I-80/Richards Blvd Interchange <br> Westbound I-80 <br> Richards Blvd to Lane Add <br> Construction Year No Build <br> PM Peak Hour |  |  |  |
| Entering General Purpose Lanes - Geometric Data |  |  |  |  |
| General Purpose Lanes, N Segment Length, L <br> Base Free Flow Speed, BFFS <br> Lane Width <br> Right Side Lateral Clearance | 3 ln <br> 3,770 ft <br> 75.4 mph <br> 12.0 ft <br> 6.0 ft | Terrain Type <br> Percent Grade <br> Grade Length <br> Total Ramp Density, TRD <br> Free Flow Speed, FFS | Level $1.67$ $70.4$ | mi $\mathrm{ramps} / \mathrm{mi}$ mph |
| Entering General Purpose Lanes - Adjustment Factors |  |  |  |  |
| Driver Population Weather Type Incident Type | Familiar <br> Non-severe <br> No incident | Speed Adjustment Factor, SAF <br> Capacity Adjustment Factor, CAF <br> Demand Adjustment Factor, DAF | $\begin{aligned} & 1.00 \\ & 1.00 \\ & 1.00 \end{aligned}$ |  |


| Entering General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Volume, V | 4,890 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.99 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,795 | pcphpl |
| Total Trucks | 9.0\% |  | Capacity, c | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - |  | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |
| Passenger Car Equivalent, $\mathrm{E}_{T}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.75 |  |


| Entering General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 70.4 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 66.1 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 27.1 | pcpmpl |
| Total Ramp Density Adjustment | 5.0 | mph | Level of Service, LOS | D |  |

## Segment General Purpose Lanes - Capacity, Speed, and Density

| Segment General |  |  |  |  |  |  | Purpose Lanes - Capacity, Speed, and Density |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: | :---: |
| General Purpose Lanes, N | 4 | In | Average Speed, S | 69.8 | mph |  |  |
| Adjusted Capacity, cadj | 2,400 | pcphpl | Density, D | 20.5 | pcphpl |  |  |
| Flow Rate, vp | 1,427 | pcphpl | Level of Service, LOS | C |  |  |  |
| Volume-to-Capacity Ratio, v/c | 0.59 |  |  |  |  |  |  |


| Freeway Merge Report |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Project I-80/Richards B <br> Freeway Westbound I-80 <br> Segment Richards Blvd to <br> Alternative Construction Ye <br> Time Period PM Peak Hour |  |  |  |  |
| Geometric Data |  |  |  |  |
|  | Freeway | On Ramp |  |  |
| Number of Lanes, N | 3 | 1 |  |  |
| Free-Flow Speed, FFS | 70.4 | 45 |  | mph |
| Segment Length, L / Acceleration Length, LA | 3,770 | 0 |  | ft |
| Terrain Type | Level | Level |  |  |
| Percent Grade | - | - |  |  |
| Grade Length | - | - |  | ft |
| Segment Type / Ramp Type | Freeway | Right |  |  |
| Adjustment Factors |  |  |  |  |
|  | Freeway | On Ramp |  |  |
| Driver Population | Familiar | Familiar |  |  |
| Weather Type | Non-severe | Non-severe |  |  |
| Incident Type | No incident | No incident |  |  |
| Capacity Adjustment Factor, CAF | 1.00 | 1.00 |  |  |
| Demand Adjustment Factor, DAF | 1.00 | 1.00 |  |  |
| Volume Data |  |  |  |  |
| Junction Components | Freeway | On Ramp |  |  |
| Volume, V | 4,890 | 290 |  | vph |
| Peak Hour Factor, PHF | 0.99 | 0.92 |  |  |
| Total Trucks | 9.0\% | 3.0\% |  |  |
| Single Unit/Tractor-Trailer Mix | - | - |  |  |
| Passenger Car Equivalent, $\mathrm{E}_{T}$ | 2.0 | 2.0 |  |  |
| Heavy Vehicle Adjustment, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 | 0.971 |  |  |
| Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 5,384 | 325 |  | pcph |
| Adjacent Ramp Data |  |  |  |  |
|  |  | Upstream | Downstream |  |
| Adjacent Ramp Meeting Criteria |  | No | No |  |
| Type of Adjacent Ramp |  |  |  |  |
| Distance to Adjacent Ramp |  |  |  | ft |
| Volume on Adjacent Ramp |  |  |  | pcph |

## Freeway Merge Report



| Ramp Influence Area Density and Level of Service |  |  |
| :--- | :--- | :---: |
|  | pcpmpl |  |
| Density in Ramp Influence Area, $D_{R}$ |  |  |

## Segment Speed, Flow, and Density

Speed Adjustment Factor, SAF
Speed Index, $\mathrm{M}_{\mathrm{S}}$ or $\mathrm{D}_{\mathrm{S}}$
Average Speed in Ramp Influence Area, $\mathrm{S}_{\mathrm{R}} \mathrm{mph}$

Average Flow in Outer Lanes, $\mathrm{v}_{\mathrm{OA}}$
pcphpl
mph
Average Speed in Outer Lanes, $\mathrm{S}_{0}$
mph
Density across All Lanes, D
pcpmpl

## Freeway Diverge Report

|  | Freeway Diverg |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Westbound I-80 |
| Segment | Lane Add to Old Davis Off |
| Alternative | Construction Year No Build |
| Time Period | PM Peak Hour |


| Geometric Data |  |  |  |
| :---: | :---: | :---: | :---: |
|  | Freeway | Off Ramp |  |
| Number of Lanes, N | 4 | 1 |  |
| Free-Flow Speed, FFS | 70.0 | 45 | mph |
| Segment Length, L / Deceleration Length, LD | 1,190 | 150 | ft |
| Terrain Type | Level | Level |  |
| Percent Grade | - | - |  |
| Grade Length | - | - | ft |
| Segment Type / Ramp Type | Freeway | Right |  |
| Adjustment Factors |  |  |  |
|  | Freeway | Off Ramp |  |
| Driver Population | Familiar | Familiar |  |
| Weather Type | Non-severe | Non-severe |  |
| Incident Type | No incident | No incident |  |
| Capacity Adjustment Factor, CAF | 1.00 | 1.00 |  |
| Demand Adjustment Factor, DAF | 1.00 | 1.00 |  |
| Volume Data |  |  |  |
| Junction Components | Freeway | Off Ramp |  |
| Volume, V | 5,180 | 210 | vph |
| Peak Hour Factor, PHF | 0.99 | 0.92 |  |
| Total Trucks | 9.0\% | 3.0\% |  |
| Single Unit/Tractor-Trailer Mix | - | - |  |
| Passenger Car Equivalent, $\mathrm{E}_{T}$ | 2.0 | 2.0 |  |
| Heavy Vehicle Adjustment, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 | 0.971 |  |
| Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 5,703 | 235 | pcph |

Adjacent Ramp Meeting Criteria
Upstream Downstream

Type of Adjacent Ramp
Distance to Adjacent Ramp
Volume on Adjacent Ramp
pcph

## Freeway Diverge Report



|  | Freeway Basic Report |
| :--- | :--- |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Westbound I-80 |
| Segment | West of Old Davis Rd |
| Alternative | Construction Year No Build |
| Time Period | PM Peak Hour |


|  | General |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
|  | Purpose Lanes - Geometric Data |  |  |  |  |  |
| General Purpose Lanes, N | 5 | ln | Terrain Type | Level |  |  |
| Segment Length, L | 1,350 | ft | Percent Grade | - |  |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |  |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 1.83 | $\mathrm{ramps} / \mathrm{mi}$ |  |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 70.0 | mph |  |


| General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


| General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Volume, V | 4,970 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.99 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,094 | pcphpl |
| Total Trucks | 9.0\% |  | Capacity, c | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - |  | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |
| Passenger Car Equivalent, $\mathrm{E}_{T}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.46 |  |


| General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 70.0 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 70.0 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 15.6 | pcpmpl |
| Total Ramp Density Adjustment | 5.4 | mph | Level of Service, LOS | B |  |

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|  | Freeway Basic Report |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Westbound I-80 |
| Segment | East of Mace Blvd |
| Alternative | Construction Year Build |
| Time Period | AM Peak Period |


|  | General |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
|  | Purpose Lanes - Geometric Data |  |  |  |  |  |
| General Purpose Lanes, N | 3 | ln | Terrain Type | Level |  |  |
| Segment Length, L | 2,590 | ft | Percent Grade | - |  |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |  |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 1.00 | $\mathrm{ramps} / \mathrm{mi}$ |  |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 72.2 | mph |  |


| General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


| General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Volume, V | 4,550 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.98 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,687 | pcphpl |
| Total Trucks | 9.0\% |  | Capacity, c | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - |  | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.70 |  |


| General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 72.2 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 68.4 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 24.7 | pcpmpl |
| Total Ramp Density Adjustment | 3.2 | mph | Level of Service, LOS | C |  |

$\qquad$

|  | Freeway Basic Report |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Westbound I-80 |
| Segment | Mace Blvd to Lane Drop |
| Alternative | Construction Year Build |
| Time Period | AM Peak Period |


|  |  |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
|  | Entering General Purpose Lanes - Geometric Data |  |  |  |  |  |
| General Purpose Lanes, N | 3 | ln | Terrain Type | Level |  |  |
| Segment Length, L | 1,850 | ft | Percent Grade | - |  |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |  |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 0.83 | $\mathrm{ramps} / \mathrm{mi}$ |  |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 72.6 | mph |  |


| Entering General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


| Entering General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :--- | :---: | :--- | :--- | :--- | :--- |
| Volume, V | 4,550 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.98 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,687 | pcphpl |
| Total Trucks | $9.0 \%$ |  | Capacity, c | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - | Adjusted Capacity, $\mathrm{c}_{\mathrm{adj}}$ | 2,400 | pcphpl |  |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.70 |  |


| Entering General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 72.6 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 68.7 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 24.6 | pcpmpl |
| Total Ramp Density Adjustment | 2.8 | mph | Level of Service, LOS | C |  |

## Segment General Purpose Lanes - Capacity, Speed, and Density

| Segment General Purpose Lanes - Capacity, Speed, and Density |  |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
| General Purpose Lanes, N | 4 | In | Average Speed, S | 71.5 | mph |  |
| Adjusted Capacity, cadj | 2,400 | pcphpl | Density, D | 19.9 | pcphpl |  |
| Flow Rate, vp | 1,419 | pcphpl | Level of Service, LOS | C |  |  |
| Volume-to-Capacity Ratio, v/c | 0.59 |  |  |  |  |  |

## Freeway Merge Report

| Freeway Merge Report |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Project I-80/Richards BI <br> Freeway Westbound I-80 <br> Segment Mace Blvd to La <br> Alternative Construction Ye <br> Time Period AM Peak Period |  |  |  |  |
| Geometric Data |  |  |  |  |
|  | Freeway | On Ramp |  |  |
| Number of Lanes, N | 3 | 2 |  |  |
| Free-Flow Speed, FFS | 72.6 | 45 |  | mph |
| Segment Length, L / Acceleration Length, LA | 1,850 | 0 |  | ft |
| Terrain Type | Level | Level |  |  |
| Percent Grade | - | - |  |  |
| Grade Length | - | - |  | ft |
| Segment Type / Ramp Type | Freeway | Right |  |  |
| Adjustment Factors |  |  |  |  |
|  | Freeway | On Ramp |  |  |
| Driver Population | Familiar | Familiar |  |  |
| Weather Type | Non-severe | Non-severe |  |  |
| Incident Type | No incident | No incident |  |  |
| Capacity Adjustment Factor, CAF | 1.00 | 1.00 |  |  |
| Demand Adjustment Factor, DAF | 1.00 | 1.00 |  |  |
| Volume Data |  |  |  |  |
| Junction Components | Freeway | On Ramp |  |  |
| Volume, V | 4,550 | 550 |  | vph |
| Peak Hour Factor, PHF | 0.98 | 0.92 |  |  |
| Total Trucks | 9.0\% | 3.0\% |  |  |
| Single Unit/Tractor-Trailer Mix | - | - |  |  |
| Passenger Car Equivalent, $\mathrm{E}_{T}$ | 2.0 | 2.0 |  |  |
| Heavy Vehicle Adjustment, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 | 0.971 |  |  |
| Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 5,061 | 616 |  | pcph |
| Adjacent Ramp Data |  |  |  |  |
|  |  | Upstream | Downstream |  |
| Adjacent Ramp Meeting Criteria |  | No | No |  |
| Type of Adjacent Ramp |  |  |  |  |
| Distance to Adjacent Ramp |  |  |  | ft |
| Volume on Adjacent Ramp |  |  |  | pcph |

## Freeway Merge Report



| Ramp Influence Area Density and Level of Service |  |  |
| :--- | :--- | :---: |
|  | pcpmpl |  |
| Density in Ramp Influence Area, $D_{R}$ |  |  |

## Segment Speed, Flow, and Density

Speed Adjustment Factor, SAF
Speed Index, $\mathrm{M}_{\mathrm{S}}$ or $\mathrm{D}_{\mathrm{S}}$
Average Speed in Ramp Influence Area, $\mathrm{S}_{\mathrm{R}} \mathrm{mph}$

Average Flow in Outer Lanes, $\mathrm{v}_{\mathrm{OA}}$
pcphpl
mph
Average Speed in Outer Lanes, $\mathrm{S}_{0}$
mph
Density across All Lanes, D
pcpmpl

|  | Freeway Basic Report |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Westbound I-80 |
| Segment | Lane Drop to Richards Blvd |
| Alternative | Construction Year Build |
| Time Period | AM Peak Period |


|  | General |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
|  | Purpose Lanes - Geometric Data |  |  |  |  |  |
| General Purpose Lanes, N | 3 | ln | Terrain Type | Level |  |  |
| Segment Length, L | 7,170 | ft | Percent Grade | - |  |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |  |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 0.83 | $\mathrm{ramps} / \mathrm{mi}$ |  |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 72.6 | mph |  |


| General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


|  | General Purpose Lanes - Demand and Capacity |  |  |  |  |
| :--- | :---: | :--- | :--- | :--- | :--- |
| Volume, V | 5,100 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.98 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,891 | pcphpl |
| Total Trucks | $9.0 \%$ |  | Capacity, c | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |  |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.79 |  |


| General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 72.6 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 65.5 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 28.9 | pcpmpl |
| Total Ramp Density Adjustment | 2.8 | mph | Level of Service, LOS | D |  |

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## Freeway Diverge Report

|  | Freeway Diverg |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Westbound I-80 |
| Segment | Richards Blvd Off Ramp |
| Alternative | Construction Year Build |
| Time Period | AM Peak Period |


| Geometric Data |  |  |  |
| :---: | :---: | :---: | :---: |
|  | Freeway | Off Ramp |  |
| Number of Lanes, N | 3 | 1 |  |
| Free-Flow Speed, FFS | 72.6 | 45 | mph |
| Segment Length, L / Deceleration Length, LD | 1,500 | 150 | ft |
| Terrain Type | Level | Level |  |
| Percent Grade | - | - |  |
| Grade Length | - | - | ft |
| Segment Type / Ramp Type | Freeway | Right |  |
| Adjustment Factors |  |  |  |
|  | Freeway | Off Ramp |  |
| Driver Population | Familiar | Familiar |  |
| Weather Type | Non-severe | Non-severe |  |
| Incident Type | No incident | No incident |  |
| Capacity Adjustment Factor, CAF | 1.00 | 1.00 |  |
| Demand Adjustment Factor, DAF | 1.00 | 1.00 |  |
| Volume Data |  |  |  |
| Junction Components | Freeway | Off Ramp |  |
| Volume, V | 5,100 | 430 | vph |
| Peak Hour Factor, PHF | 0.98 | 0.92 |  |
| Total Trucks | 9.0\% | 3.0\% |  |
| Single Unit/Tractor-Trailer Mix | - | - |  |
| Passenger Car Equivalent, $\mathrm{E}_{T}$ | 2.0 | 2.0 |  |
| Heavy Vehicle Adjustment, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 | 0.971 |  |
| Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 5,672 | 481 | pcph |

Adjacent Ramp Meeting Criteria
Upstream Downstream

Type of Adjacent Ramp
Distance to Adjacent Ramp
Volume on Adjacent Ramp
pcph

## Freeway Diverge Report



|  | Freeway Basic Report |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Westbound I-80 |
| Segment | Richards Blvd Off to On |
| Alternative | Construction Year Build |
| Time Period | AM Peak Period |


|  | General |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
|  | Purpose Lanes - Geometric Data |  |  |  |  |  |
| General Purpose Lanes, N | 3 | ln | Terrain Type | Level |  |  |
| Segment Length, L | 2,140 | ft | Percent Grade | - |  |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |  |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 1.33 | $\mathrm{ramps} / \mathrm{mi}$ |  |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 71.3 | mph |  |


| General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


|  | General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :--- | :--- | :--- |
| Volume, V | 4,670 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{Hv}}$ | 0.917 |  |  |
| Peak Hour Factor, PHF | 0.98 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,731 | pcphpl |  |
| Total Trucks | $9.0 \%$ |  | Capacity, c | 2,400 | pcphpl |  |
| Single Unit/Tractor-Trailer Mix | - | Adjusted Capacity, $\mathrm{c}_{\mathrm{adj}}$ | 2,400 | pcphpl |  |  |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 | Volume-to-Capacity Ratio, v/c | 0.72 |  |  |  |


| General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 71.3 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 67.4 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 25.7 | pcpmpl |
| Total Ramp Density Adjustment | 4.1 | mph | Level of Service, LOS | C |  |

$\qquad$


| Entering General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :--- | :---: | :--- | :--- | :--- | :--- |
| Volume, V | 4,670 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.98 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,299 | pcphpl |
| Total Trucks | $9.0 \%$ |  | Capacity, c | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |  |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 | Volume-to-Capacity Ratio, v/c | 0.54 |  |  |


| Entering General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 71.3 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 71.0 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 18.3 | pcpmpl |
| Total Ramp Density Adjustment | 4.1 | mph | Level of Service, LOS | C |  |


| Segment General Purpose Lanes - Capacity, Speed, and Density |  |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
| General Purpose Lanes, N | 4 | $\ln$ | Average Speed, S | 70.2 | mph |  |
| Adjusted Capacity, cadj | 2,400 | pcphpl | Density, D | 20.7 | pcphpl |  |
| Flow Rate, vp | 1,452 | pcphpl | Level of Service, LOS | C |  |  |
| Volume-to-Capacity Ratio, v/c | 0.61 |  |  |  |  |  |


| Freeway Merge Report |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Project I-80/Richards B <br> Freeway Westbound I-80 <br> Segment Richards Blvd O <br> Alternative Construction Ye <br> Time Period AM Peak Period |  |  |  |  |
| Geometric Data |  |  |  |  |
|  | Freeway | On Ramp |  |  |
| Number of Lanes, N | 4 | 1 |  |  |
| Free-Flow Speed, FFS | 71.3 | 45 |  | mph |
| Segment Length, L / Acceleration Length, LA | 3,770 | 0 |  | ft |
| Terrain Type | Level | Level |  |  |
| Percent Grade | - | - |  |  |
| Grade Length | - | - |  | ft |
| Segment Type / Ramp Type | Freeway | Right |  |  |
| Adjustment Factors |  |  |  |  |
|  | Freeway | On Ramp |  |  |
| Driver Population | Familiar | Familiar |  |  |
| Weather Type | Non-severe | Non-severe |  |  |
| Incident Type | No incident | No incident |  |  |
| Capacity Adjustment Factor, CAF | 1.00 | 1.00 |  |  |
| Demand Adjustment Factor, DAF | 1.00 | 1.00 |  |  |
| Volume Data |  |  |  |  |
| Junction Components | Freeway | On Ramp |  |  |
| Volume, V | 4,670 | 550 |  | vph |
| Peak Hour Factor, PHF | 0.98 | 0.92 |  |  |
| Total Trucks | 9.0\% | 3.0\% |  |  |
| Single Unit/Tractor-Trailer Mix | - | - |  |  |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 | 2.0 |  |  |
| Heavy Vehicle Adjustment, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 | 0.971 |  |  |
| Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 5,194 | 616 |  | pcph |
| Adjacent Ramp Data |  |  |  |  |
|  |  | Upstream | Downstream |  |
| Adjacent Ramp Meeting Criteria |  | No | No |  |
| Type of Adjacent Ramp |  |  |  |  |
| Distance to Adjacent Ramp |  |  |  | ft |
| Volume on Adjacent Ramp |  |  |  | pcph |

## Freeway Merge Report



| Ramp Influence Area Density and Level of Service |  |  |
| :--- | :--- | :---: |
|  |  |  |
| Density in Ramp Influence Area, $D_{R}$ | pcpmpl |  |
| Level of Service, LOS |  |  |

## Segment Speed, Flow, and Density

Speed Adjustment Factor, SAF
Speed Index, $\mathrm{M}_{\mathrm{S}}$ or $\mathrm{D}_{\mathrm{S}}$
Average Speed in Ramp Influence Area, $\mathrm{S}_{\mathrm{R}} \mathrm{mph}$

Average Flow in Outer Lanes, $\mathrm{v}_{\mathrm{OA}}$
pcphpl
mph
Average Speed in Outer Lanes, $\mathrm{S}_{0}$
mph
Density across All Lanes, D
pcpmpl

## Freeway Diverge Report

|  | Freeway Diverg |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Westbound I-80 |
| Segment | Lane Add to Davis Off |
| Alternative | Construction Year Build |
| Time Period | AM Peak Period |


| Geometric Data |  |  |  |
| :---: | :---: | :---: | :---: |
|  | Freeway | Off Ramp |  |
| Number of Lanes, N | 5 | 1 |  |
| Free-Flow Speed, FFS | 71.3 | 45 | mph |
| Segment Length, L / Deceleration Length, LD | 1,190 | 150 | ft |
| Terrain Type | Level | Level |  |
| Percent Grade | - | - |  |
| Grade Length | - | - | ft |
| Segment Type / Ramp Type | Freeway | Right |  |
| Adjustment Factors |  |  |  |
|  | Freeway | Off Ramp |  |
| Driver Population | Familiar | Familiar |  |
| Weather Type | Non-severe | Non-severe |  |
| Incident Type | No incident | No incident |  |
| Capacity Adjustment Factor, CAF | 1.00 | 1.00 |  |
| Demand Adjustment Factor, DAF | 1.00 | 1.00 |  |
| Volume Data |  |  |  |
| Junction Components | Freeway | Off Ramp |  |
| Volume, V | 5,220 | 481 | vph |
| Peak Hour Factor, PHF | 0.98 | 0.92 |  |
| Total Trucks | 9.0\% | 3.0\% |  |
| Single Unit/Tractor-Trailer Mix | - | - |  |
| Passenger Car Equivalent, $\mathrm{E}_{T}$ | 2.0 | 2.0 |  |
| Heavy Vehicle Adjustment, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 | 0.971 |  |
| Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 5,806 | 539 | pcph |

Adjacent Ramp Meeting Criteria
Upstream Downstream

Type of Adjacent Ramp
Distance to Adjacent Ramp
Volume on Adjacent Ramp
pcph

## Freeway Diverge Report



|  | Freeway Basic Report |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Westbound I-80 |
| Segment | West of Old Davis Rd |
| Alternative | Construction Year Build |
| Time Period | AM Peak Period |


|  | General |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :--- | :---: | :---: |
|  | Purpose Lanes - Geometric Data |  |  |  |  |  |
| General Purpose Lanes, N | 5 | ln | Terrain Type | Level |  |  |
| Segment Length, L | 1,350 | ft | Percent Grade | - |  |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |  |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 1.33 | $\mathrm{ramps} / \mathrm{mi}$ |  |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 71.3 | mph |  |


| General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


| General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Volume, V | 4,739 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.98 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,054 | pcphpl |
| Total Trucks | 9.0\% |  | Capacity, c | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - |  | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.44 |  |


| General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 71.3 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 71.3 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 14.8 | pcpmpl |
| Total Ramp Density Adjustment | 4.1 | mph | Level of Service, LOS | B |  |

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|  | Freeway Basic Report |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Westbound I-80 |
| Segment | East of Mace Blvd |
| Alternative | Construction Year Build |
| Time Period | PM Peak Period |


|  | General |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
|  | Purpose Lanes - Geometric Data |  |  |  |  |  |
| General Purpose Lanes, N | 3 | ln | Terrain Type | Level |  |  |
| Segment Length, L | 2,590 | ft | Percent Grade | - |  |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |  |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 1.00 | $\mathrm{ramps} / \mathrm{mi}$ |  |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 72.2 | mph |  |


| General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


| General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Volume, V | 4,290 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.99 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,574 | pcphpl |
| Total Trucks | 9.0\% |  | Capacity, c | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - |  | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.66 |  |


| General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 72.2 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 69.8 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 22.6 | pcpmpl |
| Total Ramp Density Adjustment | 3.2 | mph | Level of Service, LOS | C |  |

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| Entering General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :--- | :---: | :--- | :--- | :--- | :--- |
| Volume, V | 4,290 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.99 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,574 | pcphpl |
| Total Trucks | $9.0 \%$ |  | Capacity, c | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |  |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.66 |  |


| Entering General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 72.6 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 70.0 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 22.5 | pcpmpl |
| Total Ramp Density Adjustment | 2.8 | mph | Level of Service, LOS | C |  |

## Segment General Purpose Lanes - Capacity, Speed, and Density

| Segment General Purpose Lanes - Capacity, Speed, and Density |  |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
| General Purpose Lanes, N | 4 | In | Average Speed, S | 72.1 | mph |  |
| Adjusted Capacity, cadj | 2,400 | pcphpl | Density, D | 18.4 | pcphpl |  |
| Flow Rate, vp | 1,324 | pcphpl | Level of Service, LOS | C |  |  |
| Volume-to-Capacity Ratio, v/c | 0.55 |  |  |  |  |  |

## Freeway Merge Report

| Freeway Merge Report |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Project I-80/Richards BI <br> Freeway Westbound I-80 <br> Segment Mace Blvd to La <br> Alternative Construction Ye <br> Time Period PM Peak Period |  |  |  |  |
| Geometric Data |  |  |  |  |
|  | Freeway | On Ramp |  |  |
| Number of Lanes, N | 3 | 2 |  |  |
| Free-Flow Speed, FFS | 72.6 | 45 |  | mph |
| Segment Length, L / Acceleration Length, LA | 1,850 | 0 |  | ft |
| Terrain Type | Level | Level |  |  |
| Percent Grade | - | - |  |  |
| Grade Length | - | - |  | ft |
| Segment Type / Ramp Type | Freeway | Right |  |  |
| Adjustment Factors |  |  |  |  |
|  | Freeway | On Ramp |  |  |
| Driver Population | Familiar | Familiar |  |  |
| Weather Type | Non-severe | Non-severe |  |  |
| Incident Type | No incident | No incident |  |  |
| Capacity Adjustment Factor, CAF | 1.00 | 1.00 |  |  |
| Demand Adjustment Factor, DAF | 1.00 | 1.00 |  |  |
| Volume Data |  |  |  |  |
| Junction Components | Freeway | On Ramp |  |  |
| Volume, V | 4,290 | 510 |  | vph |
| Peak Hour Factor, PHF | 0.99 | 0.92 |  |  |
| Total Trucks | 9.0\% | 3.0\% |  |  |
| Single Unit/Tractor-Trailer Mix | - | - |  |  |
| Passenger Car Equivalent, $\mathrm{E}_{T}$ | 2.0 | 2.0 |  |  |
| Heavy Vehicle Adjustment, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 | 0.971 |  |  |
| Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 4,723 | 571 |  | pcph |
| Adjacent Ramp Data |  |  |  |  |
|  |  | Upstream | Downstream |  |
| Adjacent Ramp Meeting Criteria |  | No | No |  |
| Type of Adjacent Ramp |  |  |  |  |
| Distance to Adjacent Ramp |  |  |  | ft |
| Volume on Adjacent Ramp |  |  |  | pcph |

## Freeway Merge Report



| Ramp Influence Area Density and Level of Service |  |  |
| :--- | :--- | :---: |
|  | pcpmpl |  |
| Density in Ramp Influence Area, $D_{R}$ |  |  |

## Segment Speed, Flow, and Density

Speed Adjustment Factor, SAF
Speed Index, $\mathrm{M}_{\mathrm{S}}$ or $\mathrm{D}_{\mathrm{S}}$
Average Speed in Ramp Influence Area, $\mathrm{S}_{\mathrm{R}} \mathrm{mph}$

Average Flow in Outer Lanes, $\mathrm{v}_{\mathrm{OA}}$
pcphpl
mph
Average Speed in Outer Lanes, $\mathrm{S}_{0}$
mph
Density across All Lanes, D
pcpmpl

|  | Freeway Basic Report |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Westbound I-80 |
| Segment | Lane Drop to Richards Blvd |
| Alternative | Construction Year Build |
| Time Period | PM Peak Period |


|  | General |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
|  | Purpose Lanes - Geometric Data |  |  |  |  |  |
| General Purpose Lanes, N | 3 | ln | Terrain Type | Level |  |  |
| Segment Length, L | 7,170 | ft | Percent Grade | - |  |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |  |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 0.83 | $\mathrm{ramps} / \mathrm{mi}$ |  |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 72.6 | mph |  |


| General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


| General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Volume, V | 4,800 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.99 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,762 | pcphpl |
| Total Trucks | 9.0\% |  | Capacity, c | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - |  | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.73 |  |


| General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 72.6 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 67.6 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 26.1 | pcpmpl |
| Total Ramp Density Adjustment | 2.8 | mph | Level of Service, LOS | D |  |

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## Freeway Diverge Report

| Freeway Diverge Report |  |  |  |
| :---: | :---: | :---: | :---: |
| Project I-80/Richards Blvd <br> Freeway Westbound I-80 <br> Segment Richards Blvd Of <br> Alternative Construction Yea <br> Time Period PM Peak Period |  |  |  |
| Geometric Data |  |  |  |
|  | Freeway | Off Ramp |  |
| Number of Lanes, N | 3 | 1 |  |
| Free-Flow Speed, FFS | 72.6 | 45 | mph |
| Segment Length, L / Deceleration Length, LD | 1,500 | 150 | ft |
| Terrain Type | Level | Level |  |
| Percent Grade | - | - |  |
| Grade Length | - | - | ft |
| Segment Type / Ramp Type | Freeway | Right |  |
| Adjustment Factors |  |  |  |
|  | Freeway | Off Ramp |  |
| Driver Population | Familiar | Familiar |  |
| Weather Type | Non-severe | Non-severe |  |
| Incident Type | No incident | No incident |  |
| Capacity Adjustment Factor, CAF | 1.00 | 1.00 |  |
| Demand Adjustment Factor, DAF | 1.00 | 1.00 |  |
| Volume Data |  |  |  |
| Junction Components | Freeway | Off Ramp |  |
| Volume, V | 4,800 | 440 | vph |
| Peak Hour Factor, PHF | 0.99 | 0.92 |  |
| Total Trucks | 9.0\% | 3.0\% |  |
| Single Unit/Tractor-Trailer Mix | - | - |  |
| Passenger Car Equivalent, $\mathrm{E}_{T}$ | 2.0 | 2.0 |  |
| Heavy Vehicle Adjustment, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 | 0.971 |  |
| Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 5,285 | 493 | pcph |

## Adjacent Ramp Data

Adjacent Ramp Meeting Criteria
Upstream Downstream

Type of Adjacent Ramp
Distance to Adjacent Ramp
Volume on Adjacent Ramp

## Freeway Diverge Report



|  | Freeway Basic Report |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Westbound I-80 |
| Segment | Richards Blvd Off to On |
| Alternative | Construction Year Build |
| Time Period | PM Peak Period |


|  | General |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
|  | Purpose Lanes - Geometric Data |  |  |  |  |  |
| General Purpose Lanes, N | 3 | ln | Terrain Type | Level |  |  |
| Segment Length, L | 2,140 | ft | Percent Grade | - |  |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |  |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 1.33 | $\mathrm{ramps} / \mathrm{mi}$ |  |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 71.3 | mph |  |


| General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


| General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Volume, V | 4,360 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.99 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,600 | pcphpl |
| Total Trucks | 9.0\% |  | Capacity, c | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - |  | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.67 |  |


| General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 71.3 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 69.0 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 23.2 | pcpmpl |
| Total Ramp Density Adjustment | 4.1 | mph | Level of Service, LOS | C |  |

$\qquad$


| Entering General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :--- | :---: | :--- | :--- | :--- | :--- |
| Volume, V | 4,360 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.99 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,200 | pcphpl |
| Total Trucks | $9.0 \%$ |  | Capacity, c | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |  |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 | Volume-to-Capacity Ratio, v/c | 0.50 |  |  |


| Entering General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 71.3 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 71.3 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 16.8 | pcpmpl |
| Total Ramp Density Adjustment | 4.1 | mph | Level of Service, LOS | B |  |

Segment General Purpose Lanes - Capacity, Speed, and Density

| General Purpose Lanes, N | 3 | $\ln$ | Average Speed, S | 64.7 | mph |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Adjusted Capacity, cadj | 2,400 | pcphpl | Density, D | 29.5 | pcphpl |
| Flow Rate, vp | 1,906 | pcphpl | Level of Service, LOS | D |  |
| Volume-to-Capacity Ratio, v/c | 0.79 |  |  |  |  |


| Freeway Merge Report |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Project I-80/Richards B <br> Freeway Westbound I-80 <br> Segment Richards Blvd O <br> Alternative Construction Ye <br> Time Period PM Peak Period |  |  |  |  |
| Geometric Data |  |  |  |  |
|  | Freeway | On Ramp |  |  |
| Number of Lanes, N | 4 | 1 |  |  |
| Free-Flow Speed, FFS | 71.3 | 45 |  | mph |
| Segment Length, L / Acceleration Length, LA | 3,770 | 0 |  | ft |
| Terrain Type | Level | Level |  |  |
| Percent Grade | - | - |  |  |
| Grade Length | - | - |  | ft |
| Segment Type / Ramp Type | Freeway | Right |  |  |
| Adjustment Factors |  |  |  |  |
|  | Freeway | On Ramp |  |  |
| Driver Population | Familiar | Familiar |  |  |
| Weather Type | Non-severe | Non-severe |  |  |
| Incident Type | No incident | No incident |  |  |
| Capacity Adjustment Factor, CAF | 1.00 | 1.00 |  |  |
| Demand Adjustment Factor, DAF | 1.00 | 1.00 |  |  |
| Volume Data |  |  |  |  |
| Junction Components | Freeway | On Ramp |  |  |
| Volume, V | 4,360 | 820 |  | vph |
| Peak Hour Factor, PHF | 0.99 | 0.92 |  |  |
| Total Trucks | 9.0\% | 3.0\% |  |  |
| Single Unit/Tractor-Trailer Mix | - | - |  |  |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 | 2.0 |  |  |
| Heavy Vehicle Adjustment, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 | 0.971 |  |  |
| Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 4,800 | 918 |  | pcph |
| Adjacent Ramp Data |  |  |  |  |
| Adjacent Ramp Meeting Criteria |  | Upstream | Downstream |  |
|  |  | No | No |  |
| Type of Adjacent Ramp |  |  |  |  |
| Distance to Adjacent Ramp |  |  |  | ft |
| Volume on Adjacent Ramp |  |  |  | pcph |

## Freeway Merge Report



| Ramp Influence Area Density and Level of Service |  |  |  |
| :--- | :--- | :---: | :---: |
| Density in Ramp Influence Area, $D_{R}$ | pcpmpl |  |  |
| Level of Service, LOS |  |  |  |

## Segment Speed, Flow, and Density

Speed Adjustment Factor, SAF
Speed Index, $\mathrm{M}_{\mathrm{S}}$ or $\mathrm{D}_{\mathrm{S}}$
Average Speed in Ramp Influence Area, $\mathrm{S}_{\mathrm{R}} \mathrm{mph}$
Average Flow in Outer Lanes, $\mathrm{v}_{\mathrm{OA}}$
pcphpl
Average Speed in Outer Lanes, $\mathrm{S}_{\mathrm{O}}$
mph
Average Speed for Segment, S
mph
Density across All Lanes, D pcpmpl

## Freeway Diverge Report

| Freeway Diverge Report |  |  |  |
| :---: | :---: | :---: | :---: |
| Project I-80/Richards Blvd <br> Freeway Westbound I-80 <br> Segment Lane Add to Davis <br> Alternative Construction Yea <br> Time Period PM Peak Period |  |  |  |
| Geometric Data |  |  |  |
|  | Freeway | Off Ramp |  |
| Number of Lanes, N | 5 | 1 |  |
| Free-Flow Speed, FFS | 71.3 | 45 | mph |
| Segment Length, L / Deceleration Length, LD | 1,190 | 150 | ft |
| Terrain Type | Level | Level |  |
| Percent Grade | - | - |  |
| Grade Length | - | - | ft |
| Segment Type / Ramp Type | Freeway | Right |  |
| Adjustment Factors |  |  |  |
|  | Freeway | Off Ramp |  |
| Driver Population | Familiar | Familiar |  |
| Weather Type | Non-severe | Non-severe |  |
| Incident Type | No incident | No incident |  |
| Capacity Adjustment Factor, CAF | 1.00 | 1.00 |  |
| Demand Adjustment Factor, DAF | 1.00 | 1.00 |  |
| Volume Data |  |  |  |
| Junction Components | Freeway | Off Ramp |  |
| Volume, V | 5,180 | 210 | vph |
| Peak Hour Factor, PHF | 0.99 | 0.92 |  |
| Total Trucks | 9.0\% | 3.0\% |  |
| Single Unit/Tractor-Trailer Mix | - | - |  |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 | 2.0 |  |
| Heavy Vehicle Adjustment, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 | 0.971 |  |
| Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 5,703 | 235 | pcph |

## Adjacent Ramp Data

Adjacent Ramp Meeting Criteria
Upstream Downstream

Type of Adjacent Ramp
Distance to Adjacent Ramp
Volume on Adjacent Ramp

## Freeway Diverge Report



|  | Freeway Basic Report |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Westbound I-80 |
| Segment | West of Old Davis Rd |
| Alternative | Construction Year Build |
| Time Period | PM Peak Period |


|  | General |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
|  | Purpose Lanes - Geometric Data |  |  |  |  |  |
| General Purpose Lanes, N | 5 | ln | Terrain Type | Level |  |  |
| Segment Length, L | 1,350 | ft | Percent Grade | - |  |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |  |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 1.33 | $\mathrm{ramps} / \mathrm{mi}$ |  |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 71.3 | mph |  |


| General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


| General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | ---: |
| Volume, V | 4,970 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.99 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,094 | pcphpl |
| Total Trucks | $9.0 \%$ |  | Capacity, c | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |  |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.46 |  |


| General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 71.3 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 71.3 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 15.3 | pcpmpl |
| Total Ramp Density Adjustment | 4.1 | mph | Level of Service, LOS | B |  |

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| Output Summary |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| General Information |  |  |  |  |  |  |  |  |
| Project description: Analyst: | I-80/Richards Blvd Interchange - Construction Year Conditions No Build Alternative |  |  |  |  |  |  |  |
|  | DS | Date: | 1/20/2018 |  | Area type: |  | Urban |  |
| First year of analysis: | 2022 |  |  |  |  |  |  |  |
| Last year of analysis: | 2022 |  |  |  |  |  |  |  |
| Crash Data Description |  |  |  |  |  |  |  |  |
| Freeway segments | Segment crash data available? |  |  | No | First year of crash data: |  |  |  |
|  | Project-level crash data available? |  |  | No | Last year of crash data: |  |  |  |
| Ramp segments | Segment crash data available? |  |  | Yes | First year of crash data: |  |  | 2012 |
|  | Project-level crash data available? |  |  | No | Last year of | ash data |  | 2014 |
| Ramp terminals | Segment crash data available? |  |  | No | First year of crash data: |  |  |  |
|  | Project-level crash data available? |  |  | No | Last year o | ash data |  |  |
| Estimated Crash Statistics |  |  |  |  |  |  |  |  |
| Crashes for Entire Facility |  |  | Total | K | A | B | C | PDO |
| Estimated number of crashes during Study Period, crashes: |  |  | 4.3 | 0.0 | 0.1 | 0.7 | 0.8 | 2.6 |
| Estimated average crash freq. during Study Period, crashes/yr: |  |  | 4.3 | 0.0 | 0.1 | 0.7 | 0.8 | 2.6 |
| Crashes by Facility Component |  | Nbr. Sites | Total | K | A | B | C | PDO |
| Freeway segments, crashes: |  | 0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Ramp segments, crashes: |  | 5 | 4.3 | 0.0 | 0.1 | 0.7 | 0.8 | 2.6 |
| Crossroad ramp terminals, crashes: |  | 0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Crashes for Entire Facility by Year |  | Year | Total | K | A | B | C | PDO |
| Estimated number of crashes during the Study Period, crashes: |  | 2022 | 4.3 | 0.0 | 0.1 | 0.7 | 0.8 | 2.6 |
|  |  | 2023 |  |  |  |  |  |  |
|  |  | 2024 |  |  |  |  |  |  |
|  |  | 2025 |  |  |  |  |  |  |
|  |  | 2026 |  |  |  |  |  |  |
|  |  | 2027 |  |  |  |  |  |  |
|  |  | 2028 |  |  |  |  |  |  |
|  |  | 2029 |  |  |  |  |  |  |
|  |  | 2030 |  |  |  |  |  |  |
|  |  | 2031 |  |  |  |  |  |  |
|  |  | 2032 |  |  |  |  |  |  |
|  |  | 2033 |  |  |  |  |  |  |
|  |  | 2034 |  |  |  |  |  |  |
|  |  | 2035 |  |  |  |  |  |  |
|  |  | 2036 |  |  |  |  |  |  |
|  |  | 2037 |  |  |  |  |  |  |
|  |  | 2038 |  |  |  |  |  |  |
|  |  | 2039 |  |  |  |  |  |  |
|  |  | 2040 |  |  |  |  |  |  |
|  |  | 2041 |  |  |  |  |  |  |
|  |  | 2042 |  |  |  |  |  |  |
|  |  | 2043 |  |  |  |  |  |  |
|  |  | 2044 |  |  |  |  |  |  |
|  |  | 2045 |  |  |  |  |  |  |
| Distribution of Crashes for Entire Facility |  |  |  |  |  |  |  |  |
| Crash Type | Crash Type Category |  | Estimated Number of Crashes During the Study Period |  |  |  |  |  |
|  |  |  | Total | K | A | B | C | PDO |
| Multiple vehicle | Head-on crashes: |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
|  | Right-angle crashes: |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
|  | Rear-end crashes: |  | 0.2 | 0.0 | 0.0 | 0.0 | 0.1 | 0.1 |
|  | Sideswipe crashes: |  | 0.1 | 0.0 | 0.0 | 0.0 | 0.0 | 0.1 |
|  | Other multiple-vehicle crashes: |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
|  | Total multiple-vehicle crashes: |  | 0.3 | 0.0 | 0.0 | 0.1 | 0.1 | 0.2 |
| Single vehicle | Crashes with animal: |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
|  | Crashes with fixed object: |  | 3.2 | 0.0 | 0.1 | 0.4 | 0.5 | 2.1 |
|  | Crashes with other object: |  | 0.1 | 0.0 | 0.0 | 0.0 | 0.0 | 0.1 |
|  | Crashes with parked vehicle: |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
|  | Other single-vehicle crashes |  | 0.7 | 0.0 | 0.0 | 0.2 | 0.2 | 0.3 |
|  | Total single-vehicle crashes: |  | 4.0 | 0.0 | 0.1 | 0.6 | 0.8 | 2.5 |
| Total crashes: |  |  | 4.3 | 0.0 | 0.1 | 0.7 | 0.8 | 2.6 |



Vissim Post-Processor
I-80 / Richards Blvd Interchange
Design Year No Build Conditions
AM Peak Hour
Volume and Delay by Movement

Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) |  | Total Delay (sec/veh) |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 20 | 14 | 68.0\% | 335.9 | 372.5 | F |
|  | Through | 30 | 25 | 84.3\% | 357.6 | 370.8 | F |
|  | Right Turn | 30 | 21 | 70.0\% | 1012.4 | 406.9 | F |
|  | Subtotal | 80 | 60 | 74.9\% | 694.7 | 472.2 | F |
| SB | Left Turn | 90 | 8 | 9.1\% | 2155.4 | 1615.7 | F |
|  | Through | 50 | 5 | 10.8\% | 1886.2 | 1738.5 | F |
|  | Right Turn | 140 | 16 | 11.5\% | 2059.8 | 1587.3 | F |
|  | Subtotal | 280 | 30 | 10.6\% | 2126.1 | 1610.9 | F |
| EB | Left Turn | 50 | 34 | 68.0\% | 327.2 | 41.9 | F |
|  | Through | 260 | 175 | 67.4\% | 413.6 | 87.9 | F |
|  | Right Turn | 30 | 19 | 64.3\% | 339.5 | 69.4 | F |
|  | Subtotal | 340 | 229 | 67.2\% | 395.6 | 83.0 | F |
| WB | Left Turn | 30 | 25 | 84.3\% | 76.8 | 9.8 | E |
|  | Through | 570 | 521 | 91.4\% | 1.9 | 0.9 | A |
|  | Right Turn | 50 | 41 | 82.8\% | 1.2 | 0.4 | A |
|  | Subtotal | 650 | 588 | 90.4\% | 5.4 | 1.7 | A |
| Total |  | 1,350 | 906 | 67.1\% | 234.3 | 136.8 | F |

Intersection 2
E St-Richards Blvd/First St
Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) |  | Total Delay (sec/veh) |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 580 | 517 | 89.2\% | 20.4 | 3.7 | C |
|  | Through | 90 | 72 | 79.6\% | 25.7 | 5.8 | C |
|  | Right Turn | 290 | 250 | 86.2\% | 8.3 | 2.9 | A |
|  | Subtotal | 960 | 839 | 87.4\% | 17.4 | 3.7 | B |
| SB | Left Turn | 10 | 8 | 80.0\% | 440.4 | 255.8 | F |
|  | Through | 200 | 178 | 89.1\% | 562.5 | 103.4 | F |
|  | Right Turn | 20 | 18 | 90.5\% | 443.6 | 182.4 | F |
|  | Subtotal | 230 | 204 | 88.8\% | 556.9 | 102.7 | F |
| EB | Left Turn | 10 | 7 | 67.0\% | 78.9 | 53.6 | E |
|  | Through | 60 | 42 | 70.3\% | 100.1 | 25.4 | F |
|  | Right Turn | 310 | 156 | 50.2\% | 157.5 | 24.9 | F |
|  | Subtotal | 380 | 205 | 53.8\% | 143.7 | 16.9 | F |
| WB | Left Turn | 190 | 185 | 97.4\% | 145.4 | 29.1 | F |
|  | Through | 50 | 52 | 103.4\% | 95.3 | 16.8 | F |
|  | Right Turn | 10 | 11 | 108.0\% | 82.5 | 35.0 | F |
|  | Subtotal | 250 | 248 | 99.0\% | 133.1 | 23.9 | F |
| Total |  | 1,820 | 1,495 | 82.2\% | 125.1 | 12.6 | F |

Vissim Post-Processor
I-80 / Richards Blvd Interchange
Design Year No Build Conditions
AM Peak Hour
Volume and Delay by Movement

Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) |  | Total Delay (sec/veh) |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 380 | 331 | 87.1\% | 85.8 | 15.5 | F |
|  | Through | 690 | 613 | 88.9\% | 68.9 | 12.1 | E |
|  | Right Turn | 50 | 37 | 73.2\% | 46.9 | 13.1 | D |
|  | Subtotal | 1,120 | 981 | 87.6\% | 74.1 | 12.9 | E |
| SB | Left Turn | 40 | 26 | 66.0\% | 110.3 | 18.2 | F |
|  | Through | 600 | 452 | 75.4\% | 88.7 | 3.3 | F |
|  | Right Turn | 60 | 41 | 68.0\% | 82.6 | 7.5 | F |
|  | Subtotal | 700 | 520 | 74.2\% | 89.4 | 3.7 | F |
| EB | Left Turn | 60 | 59 | 98.3\% | 57.9 | 13.0 | E |
|  | Through | 30 | 30 | 100.3\% | 56.4 | 16.3 | E |
|  | Right Turn | 210 | 206 | 98.1\% | 21.0 | 5.7 | C |
|  | Subtotal | 300 | 295 | 98.4\% | 30.8 | 6.9 | C |
| WB | Left Turn | 150 | 118 | 78.6\% | 484.4 | 37.7 | F |
|  | Through | 100 | 81 | 80.7\% | 566.4 | 53.3 | F |
|  | Right Turn | 210 | 166 | 79.1\% | 544.0 | 49.7 | F |
|  | Subtotal | 460 | 365 | 79.3\% | 530.2 | 45.9 | F |
| Total |  | 2,580 | 2,161 | 83.7\% | 141.6 | 9.1 | F |

Intersection 4
I-80 WB Ramps/Richards Blvd
Uncontrolled


Vissim Post-Processor
I-80 / Richards Blvd Interchange
Average Results from 10 Runs
Volume and Delay by Movement
AM Peak Hour

Intersection 5 Richards Blvd/I-80 EB Ramps Signal


Intersection 6 Research Park Dr/Richards Blvd-Cowell Blvd Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) |  | Total Delay (sec/veh) |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 80 | 81 | 100.6\% | 50.0 | 8.3 | D |
|  | Through | 20 | 18 | 89.5\% | 38.1 | 15.5 | D |
|  | Right Turn | 40 | 42 | 105.3\% | 13.3 | 8.2 | B |
|  | Subtotal | 140 | 141 | 100.4\% | 37.6 | 5.1 | D |
| SB | Left Turn | 20 | 18 | 88.5\% | 57.1 | 17.9 | E |
|  | Through | 40 | 40 | 100.3\% | 39.4 | 10.7 | D |
|  | Right Turn | 110 | 112 | 101.6\% | 19.6 | 4.4 | B |
|  | Subtotal | 170 | 170 | 99.8\% | 28.3 | 2.9 | C |
| EB | Left Turn | 420 | 341 | 81.1\% | 90.8 | 11.6 | F |
|  | Through | 980 | 791 | 80.7\% | 50.5 | 5.4 | D |
|  | Right Turn | 160 | 136 | 85.0\% | 46.3 | 8.7 | D |
|  | Subtotal | 1,560 | 1,267 | 81.2\% | 60.8 | 5.0 | E |
| WB | Left Turn | 30 | 24 | 81.3\% | 337.0 | 27.4 | F |
|  | Through | 800 | 613 | 76.6\% | 295.9 | 17.9 | F |
|  | Right Turn | 20 | 15 | 72.5\% | 227.7 | 82.4 | F |
|  | Subtotal | 850 | 651 | 76.6\% | 296.1 | 17.7 | F |
| Total |  | 2,720 | 2,229 | 81.9\% | 122.7 | 5.3 | F |

Vissim Post-Processor
I-80 / Richards Blvd Interchange
Average Results from 10 Runs
Volume and Delay by Movement

Design Year No Build Conditions
PM Peak Hour

Intersection 1 D St/First St Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) |  | Total Delay (sec/veh) |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 40 | 40 | 98.8\% | 49.8 | 10.4 | D |
|  | Through | 60 | 58 | 96.3\% | 50.7 | 13.1 | D |
|  | Right Turn | 60 | 61 | 102.0\% | 26.4 | 15.3 | C |
|  | Subtotal | 160 | 159 | 99.1\% | 39.6 | 9.7 | D |
| SB | Left Turn | 90 | 87 | 96.8\% | 120.4 | 69.2 | F |
|  | Through | 60 | 59 | 97.8\% | 117.4 | 73.7 | F |
|  | Right Turn | 40 | 41 | 102.5\% | 69.9 | 61.3 | E |
|  | Subtotal | 190 | 187 | 98.3\% | 110.1 | 69.0 | F |
| EB | Left Turn | 30 | 32 | 106.0\% | 89.3 | 16.4 | F |
|  | Through | 250 | 257 | 102.9\% | 41.2 | 18.7 | D |
|  | Right Turn | 60 | 56 | 92.7\% | 36.3 | 13.4 | D |
|  | Subtotal | 340 | 345 | 101.4\% | 44.6 | 16.5 | D |
| WB | Left Turn | 80 | 70 | 86.9\% | 72.2 | 6.6 | E |
|  | Through | 420 | 389 | 92.6\% | 3.7 | 1.7 | A |
|  | Right Turn | 50 | 41 | 81.6\% | 2.3 | 1.5 | A |
|  | Subtotal | 550 | 499 | 90.8\% | 13.0 | 2.3 | B |
| Total |  | 1,240 | 1,189 | 95.9\% | 41.3 | 14.4 | D |

Intersection 2
E St-Richards Blvd/First St
Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) |  | Total Delay (sec/veh) |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 400 | 353 | 88.2\% | 13.1 | 3.0 | B |
|  | Through | 220 | 180 | 81.6\% | 13.1 | 3.0 | B |
|  | Right Turn | 480 | 394 | 82.1\% | 5.3 | 1.0 | A |
|  | Subtotal | 1,100 | 926 | 84.2\% | 9.8 | 1.9 | A |
| SB | Left Turn | 10 | 10 | 102.0\% | 59.4 | 33.3 | E |
|  | Through | 180 | 176 | 98.0\% | 63.5 | 9.2 | E |
|  | Right Turn | 40 | 39 | 96.3\% | 34.0 | 9.5 | C |
|  | Subtotal | 230 | 225 | 97.9\% | 59.4 | 9.0 | E |
| EB | Left Turn | 10 | 10 | 103.0\% | 46.5 | 33.2 | D |
|  | Through | 50 | 53 | 105.2\% | 58.7 | 9.2 | E |
|  | Right Turn | 340 | 342 | 100.7\% | 20.2 | 7.4 | C |
|  | Subtotal | 400 | 405 | 101.3\% | 25.9 | 6.6 | C |
| WB | Left Turn | 180 | 180 | 100.2\% | 95.2 | 34.1 | F |
|  | Through | 110 | 108 | 98.1\% | 67.8 | 16.8 | E |
|  | Right Turn | 20 | 21 | 106.5\% | 67.0 | 22.4 | E |
|  | Subtotal | 310 | 310 | 99.9\% | 84.4 | 27.5 | F |
| Total |  | 2,040 | 1,866 | 91.5\% | 31.8 | 5.1 | C |

Vissim Post-Processor
I-80 / Richards Blvd Interchange
Average Results from 10 Runs
Volume and Delay by Movement

## Design Year No Build Conditions

PM Peak Hour

Intersection 3 Richards Blvd/Olive Dr Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) |  | Total Delay (sec/veh) |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 230 | 187 | 81.1\% | 75.2 | 14.5 | E |
|  | Through | 850 | 697 | 81.9\% | 44.6 | 13.0 | D |
|  | Right Turn | 100 | 65 | 65.4\% | 25.9 | 12.1 | C |
|  | Subtotal | 1,180 | 948 | 80.4\% | 49.6 | 12.7 | D |
| SB | Left Turn | 90 | 94 | 104.4\% | 71.3 | 8.6 | E |
|  | Through | 510 | 498 | 97.6\% | 48.8 | 7.3 | D |
|  | Right Turn | 100 | 105 | 105.2\% | 51.9 | 5.2 | D |
|  | Subtotal | 700 | 697 | 99.5\% | 52.9 | 6.7 | D |
| EB | Left Turn | 80 | 71 | 88.4\% | 417.0 | 20.6 | F |
|  | Through | 60 | 55 | 92.2\% | 423.1 | 25.9 | F |
|  | Right Turn | 440 | 369 | 83.9\% | 492.4 | 24.7 | F |
|  | Subtotal | 580 | 495 | 85.4\% | 472.9 | 21.3 | F |
| WB | Left Turn | 190 | 175 | 91.8\% | 399.4 | 176.6 | F |
|  | Through | 50 | 44 | 88.2\% | 327.4 | 133.5 | F |
|  | Right Turn | 170 | 158 | 93.2\% | 318.3 | 141.5 | F |
|  | Subtotal | 410 | 377 | 92.0\% | 358.8 | 155.3 | F |
| Total |  | 2,870 | 2,517 | 87.7\% | 182.7 | 20.6 | F |

Intersection 4
I-80 WB Ramps/Richards Blvd
Uncontrolled

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) |  | Total Delay (sec/veh) |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 30 | 21 | 69.3\% | 24.1 | 26.4 | C |
|  | Through | 910 | 672 | 73.9\% | 31.2 | 25.3 | D |
|  | Right Turn | 810 | 621 | 76.7\% | 4.5 | 0.8 | A |
|  | Subtotal | 1,750 | 1,314 | 75.1\% | 18.6 | 13.9 | C |
| SB | Left Turn <br> Through | 760 | 687 | 90.4\% | 0.8 | 0.2 | A |
|  | Right Turn | 420 | 394 | 93.8\% | 2.1 | 0.3 | A |
|  | Subtotal | 1,180 | 1,081 | 91.6\% | 1.3 | 0.2 | A |
| EB | Left Turn |  |  |  |  |  |  |
|  | Through |  |  |  |  |  |  |
|  | Right Turn | 180 | 179 | 99.4\% | 0.9 | 0.2 | A |
|  | Subtotal | 180 | 179 | 99.4\% | 0.9 | 0.2 | A |
| WB | Left Turn |  |  |  |  |  |  |
|  | Through |  |  |  |  |  |  |
|  | Right Turn | 280 | 277 | 99.0\% | 3.4 | 2.3 | A |
|  | Subtotal | 280 | 277 | 99.0\% | 3.4 | 2.3 | A |
| Total |  | 3,390 | 2,851 | 84.1\% | 9.6 | 6.5 | A |

Vissim Post-Processor
I-80 / Richards Blvd Interchange
Average Results from 10 Runs
Design Year No Build Conditions
Volume and Delay by Movement
PM Peak Hour

| Intersection 5 |  | Richards Blvd/I-80 EB Ramps |  |  |  |  | Signal |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Direction | Movement | Demand Volume (vph) | Served Volume (vph) |  | Total Delay (sec/veh) |  |  |
|  |  |  | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn |  |  |  |  |  |  |
|  | Through | 1,500 | 1,177 | 78.5\% | 32.7 | 11.5 | C |
|  | Right Turn | 180 | 129 | 71.8\% | 16.3 | 3.5 | B |
|  | Subtotal | 1,680 | 1,306 | 77.8\% | 31.1 | 10.5 | C |
| SB | Left Turn | 250 | 224 | 89.4\% | 65.5 | 4.0 | E |
|  | Through | 690 | 647 | 93.8\% | 25.3 | 3.9 | C |
|  | Right Turn |  |  |  |  |  |  |
|  | Subtotal | 940 | 871 | 92.6\% | 35.5 | 3.6 | D |
| EB | Left Turn |  |  |  |  |  |  |
|  | Through |  |  |  |  |  |  |
|  | Right Turn |  |  |  |  |  |  |
|  | Subtotal |  |  |  |  |  |  |
| WB | Left Turn | 780 | 442 | 56.6\% | 500.6 | 62.2 | F |
|  | Through |  |  |  |  |  |  |
|  | Right Turn | 250 | 141 | 56.2\% | 443.8 | 50.8 | F |
|  | Subtotal | 1,030 | 582 | 56.5\% | 487.2 | 59.9 | F |
| Total |  | 3,650 | 2,759 | 75.6\% | 131.2 | 9.1 | F |

Intersection 6 Research Park Dr/Richards Blvd-Cowell Blvd Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) |  | Total Delay (sec/veh) |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 150 | 148 | 98.7\% | 64.2 | 7.2 | E |
|  | Through | 40 | 40 | 99.0\% | 41.4 | 14.3 | D |
|  | Right Turn | 70 | 64 | 91.6\% | 16.5 | 5.8 | B |
|  | Subtotal | 260 | 252 | 96.8\% | 50.3 | 5.9 | D |
| SB | Left Turn | 40 | 42 | 104.0\% | 99.2 | 43.1 | F |
|  | Through | 30 | 32 | 105.0\% | 85.6 | 55.2 | F |
|  | Right Turn | 330 | 323 | 97.8\% | 62.6 | 58.4 | E |
|  | Subtotal | 400 | 396 | 99.0\% | 69.1 | 56.2 | E |
| EB | Left Turn | 290 | 221 | 76.1\% | 76.0 | 12.0 | E |
|  | Through | 1,100 | 812 | 73.8\% | 26.5 | 6.2 | C |
|  | Right Turn | 80 | 62 | 77.3\% | 18.3 | 8.1 | B |
|  | Subtotal | 1,470 | 1,094 | 74.4\% | 35.4 | 7.9 | D |
| WB | Left Turn | 30 | 19 | 63.7\% | 261.7 | 15.4 | F |
|  | Through | 1,110 | 766 | 69.0\% | 212.0 | 15.6 | F |
|  | Right Turn | 40 | 28 | 69.0\% | 182.2 | 20.9 | F |
|  | Subtotal | 1,180 | 813 | 68.9\% | 212.4 | 15.2 | F |
| Total |  | 3,310 | 2,554 | 77.2\% | 101.3 | 10.2 | F |

Vissim Post-Processor
I-80 / Richards Blvd Interchange
Average Results from 10 Runs
Design Year Build Conditions
Volume and Delay by Movement
AM Peak Hour

| Intersection 1 |  | D St/First St |  |  |  |  | Signal |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Direction | Movement | Demand | Served V | me (vph) |  | elay (sec/v |  |
|  |  | Volume (vph) | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 20 | 19 | 94.0\% | 48.3 | 22.1 | D |
|  | Through | 30 | 27 | 91.3\% | 37.8 | 13.5 | D |
|  | Right Turn | 30 | 31 | 102.0\% | 8.2 | 2.6 | A |
|  | Subtotal | 80 | 77 | 96.0\% | 31.2 | 5.7 | C |
| SB | Left Turn | 90 | 87 | 97.1\% | 88.2 | 24.2 | F |
|  | Through | 50 | 49 | 97.4\% | 77.9 | 26.1 | E |
|  | Right Turn | 140 | 138 | 98.4\% | 64.8 | 18.5 | E |
|  | Subtotal | 280 | 274 | 97.8\% | 75.0 | 22.2 | E |
| EB | Left Turn | 50 | 48 | 95.8\% | 66.5 | 11.7 | E |
|  | Through | 260 | 263 | 101.3\% | 17.1 | 4.5 | B |
|  | Right Turn | 30 | 31 | 102.0\% | 15.0 | 5.3 | B |
|  | Subtotal | 340 | 342 | 100.6\% | 24.3 | 4.4 | C |
| WB | Left Turn | 30 | 24 | 79.7\% | 77.9 | 5.2 | E |
|  | Through | 570 | 570 | 100.0\% | 2.0 | 0.5 | A |
|  | Right Turn | 50 | 52 | 103.6\% | 1.2 | 0.4 | A |
|  | Subtotal | 650 | 646 | 99.3\% | 5.3 | 1.5 | A |
| Total |  | 1,350 | 1,338 | 99.1\% | 26.3 | 6.1 | C |

Intersection 2 E St-Richards Blvd/First St Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) |  | Total Delay (sec/veh) |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 580 | 575 | 99.1\% | 14.3 | 3.3 | B |
|  | Through | 90 | 87 | 96.4\% | 15.9 | 5.7 | B |
|  | Right Turn | 290 | 288 | 99.3\% | 2.9 | 1.1 | A |
|  | Subtotal | 960 | 949 | 98.9\% | 11.1 | 2.7 | B |
| SB | Left Turn | 10 | 8 | 80.0\% | 37.8 | 24.3 | D |
|  | Through | 200 | 200 | 100.2\% | 52.5 | 6.7 | D |
|  | Right Turn | 20 | 19 | 92.5\% | 29.3 | 24.9 | C |
|  | Subtotal | 230 | 227 | 98.6\% | 50.6 | 6.6 | D |
| EB | Left Turn | 10 | 10 | 100.0\% | 100.6 | 38.9 | F |
|  | Through | 60 | 63 | 104.5\% | 106.0 | 20.4 | F |
|  | Right Turn | 310 | 307 | 99.2\% | 11.9 | 3.2 | B |
|  | Subtotal | 380 | 380 | 100.0\% | 29.6 | 5.5 | C |
| WB | Left Turn | 190 | 185 | 97.5\% | 76.0 | 24.1 | E |
|  | Through | 50 | 53 | 105.0\% | 51.8 | 11.7 | D |
|  | Right Turn | 10 | 10 | 100.0\% | 37.9 | 59.3 | D |
|  | Subtotal | 250 | 248 | 99.1\% | 69.3 | 21.1 | E |
| Total |  | 1,820 | 1,804 | 99.1\% | 28.0 | 2.9 | C |

Vissim Post-Processor
Average Results from 10 Runs
Volume and Delay by Movement

I-80 / Richards Blvd Interchange
Design Year Build Conditions
AM Peak Hour

## Intersection 3

Richards Blvd/Olive Dr
Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) |  | Total Delay (sec/veh) |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 530 | 531 | 100.2\% | 50.9 | 3.3 | D |
|  | Through | 820 | 811 | 98.9\% | 34.7 | 5.3 | C |
|  | Right Turn | 120 | 120 | 100.2\% | 11.0 | 2.6 | B |
|  | Subtotal | 1,470 | 1,462 | 99.5\% | 39.1 | 3.2 | D |
| SB | Left Turn | 40 | 38 | 94.8\% | 84.0 | 16.5 | F |
|  | Through | 600 | 596 | 99.3\% | 54.2 | 11.5 | D |
|  | Right Turn | 60 | 59 | 97.7\% | 49.6 | 8.7 | D |
|  | Subtotal | 700 | 692 | 98.9\% | 55.3 | 11.1 | E |
| EB | Left Turn | 60 | 59 | 98.2\% | 54.8 | 10.5 | D |
|  | Through | 30 | 31 | 104.7\% | 40.3 | 11.1 | D |
|  | Right Turn | 210 | 205 | 97.8\% | 13.2 | 1.5 | B |
|  | Subtotal | 300 | 296 | 98.5\% | 24.4 | 3.9 | C |
| WB | Left Turn | 150 | 148 | 98.7\% | 86.1 | 26.4 | F |
|  | Through | 20 | 19 | 96.0\% | 44.5 | 17.2 | D |
|  | Right Turn | 80 | 77 | 96.6\% | 49.5 | 11.9 | D |
|  | Subtotal | 250 | 245 | 97.8\% | 72.1 | 17.8 | E |
| Total |  | 2,720 | 2,695 | 99.1\% | 44.8 | 4.2 | D |


| Intersection 4 |  | Richards Blvd/I-80 WB Ramps |  |  |  |  | Signal |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Direction | Movement | Demand Volume (vph) | Served Volume (vph) |  | Total Delay (sec/veh) |  |  |
|  |  |  | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 510 | 523 | 102.5\% | 61.3 | 1.4 | E |
|  | Through Right Turn | 580 | 586 | 101.0\% | 47.0 | 5.1 | D |
|  | Subtotal | 1,090 | 1,109 | 101.7\% | 53.7 | 2.6 | D |
| SB | Left Turn |  |  |  |  |  |  |
|  | Through | 780 | 770 | 98.7\% | 12.8 | 1.7 | B |
|  | Right Turn | 190 | 187 | 98.3\% | 5.6 | 0.8 | A |
|  | Subtotal | 970 | 957 | 98.6\% | 11.4 | 1.4 | B |
| EB | Left Turn |  |  |  |  |  |  |
|  | Through |  |  |  |  |  |  |
|  | Right Turn |  |  |  |  |  |  |
|  | Subtotal |  |  |  |  |  |  |
| WB | Left Turn | 280 | 282 | 100.8\% | 48.2 | 4.0 | D |
|  | Through |  |  |  |  |  |  |
|  | Right Turn | 890 | 883 | 99.2\% | 44.2 | 16.6 | D |
|  | Subtotal | 1,170 | 1,165 | 99.6\% | 45.2 | 13.1 | D |
| Total |  | 3,230 | 3,230 | 100.0\% | 38.3 | 4.7 | D |

Vissim Post-Processor
Average Results from 10 Runs
Volume and Delay by Movement

I-80 / Richards Blvd Interchange
Design Year Build Conditions
AM Peak Hour

| Intersection 5 |  | I-80 EB Ramps/Richards Blvd |  |  | Total Delay (sec/veh) |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Direction | Movement | Demand Volume (vph) | Served Volume (vph) |  |  |  |  |
|  |  |  | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn |  |  |  |  |  |  |
|  | Through | 820 | 837 | 102.1\% | 31.6 | 6.9 | C |
|  | Right Turn | 210 | 209 | 99.4\% | 28.3 | 6.6 | C |
|  | Subtotal | 1,030 | 1,046 | 101.6\% | 30.9 | 6.6 | C |
| SB | Left Turn | 290 | 286 | 98.8\% | 18.7 | 2.6 | B |
|  | Through <br> Right Turn | 770 | 764 | 99.2\% | 16.1 | 1.6 | B |
|  | Subtotal | 1,060 | 1,050 | 99.0\% | 16.8 | 1.2 | B |
| EB | Left Turn <br> Through Right Turn |  |  |  |  |  |  |
|  | Subtotal |  |  |  |  |  |  |
| WB | Left Turn | 790 | 789 | 99.8\% | 48.5 | 10.0 | D |
|  | Through |  |  |  |  |  |  |
|  |  | 270 | 266 | 98.6\% | 20.9 | 13.0 | C |
|  | Subtotal | 1,060 | 1,055 | 99.5\% | 41.5 | 10.8 | D |
| Total |  | 3,150 | 3,151 | 100.0\% | 29.9 | 3.4 | C |


| Intersection <br> Direction | 6 Research Park Dr/Richards Blvd-Cowell Blvd |  |  |  |  |  | SignalLOS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Movement | Demand Volume (vph) | Served Volume (vph) |  | Total Delay (sec/veh) |  |  |
|  |  |  | Average | Percent | Average | Std. Dev. |  |
| NB | Left Turn | 80 | 84 | 104.9\% | 49.9 | 7.2 | D |
|  | Through | 20 | 20 | 100.5\% | 31.1 | 17.7 | C |
|  | Right Turn | 40 | 36 | 91.0\% | 8.5 | 4.8 | A |
|  | Subtotal | 140 | 140 | 100.3\% | 36.4 | 3.4 | D |
| SB | Left Turn | 20 | 21 | 107.0\% | 45.8 | 19.1 | D |
|  | Through | 40 | 42 | 104.0\% | 39.2 | 8.1 | D |
|  | Right Turn | 110 | 108 | 98.4\% | 25.5 | 5.1 | C |
|  | Subtotal | 170 | 171 | 100.7\% | 32.1 | 3.8 | C |
| EB | Left Turn | 420 | 415 | 98.7\% | 41.0 | 10.6 | D |
|  | Through | 980 | 976 | 99.6\% | 29.1 | 7.1 | C |
|  | Right Turn | 160 | 162 | 101.3\% | 18.4 | 5.4 | B |
|  | Subtotal | 1,560 | 1,553 | 99.6\% | 31.4 | 7.2 | C |
| WB | Left Turn | 30 | 29 | 95.3\% | 95.7 | 21.8 | F |
|  | Through | 800 | 812 | 101.5\% | 77.6 | 19.8 | E |
|  | Right Turn |  | 18 | 88.0\% | 71.1 | 39.1 | E |
|  | Subtotal | 850 | 858 | 101.0\% | 78.3 | 19.8 | E |
| Total |  | 2,720 | 2,723 | 100.1\% | 47.2 | 9.0 | D |

Vissim Post-Processor
I-80 / Richards Blvd Interchange
Average Results from 10 Runs
Design Year Build Conditions
Volume and Delay by Movement
PM Peak Hour

| Intersection 1 |  | D St/First St |  |  |  |  | Signal |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Direction | Movement | Demand | Served V | me (vph) |  | elay (sec/v |  |
|  |  | Volume (vph) | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 40 | 40 | 100.0\% | 61.9 | 16.2 | E |
|  | Through | 60 | 60 | 100.2\% | 62.5 | 11.3 | E |
|  | Right Turn | 60 | 59 | 98.3\% | 22.9 | 5.3 | C |
|  | Subtotal | 160 | 159 | 99.4\% | 47.5 | 9.8 | D |
| SB | Left Turn | 90 | 88 | 98.1\% | 81.2 | 33.2 | F |
|  | Through | 60 | 59 | 99.0\% | 70.8 | 25.4 | E |
|  | Right Turn | 40 | 39 | 98.5\% | 42.4 | 26.2 | D |
|  | Subtotal | 190 | 187 | 98.5\% | 71.4 | 28.2 | E |
| EB | Left Turn | 30 | 31 | 102.7\% | 76.9 | 31.4 | E |
|  | Through | 250 | 257 | 102.9\% | 39.6 | 19.0 | D |
|  | Right Turn | 60 | 57 | 94.8\% | 32.5 | 14.7 | C |
|  | Subtotal | 340 | 345 | 101.5\% | 41.9 | 19.0 | D |
| WB | Left Turn | 80 | 76 | 95.0\% | 71.8 | 8.0 | E |
|  | Through | 420 | 403 | 96.0\% | 4.4 | 1.4 | A |
|  | Right Turn | 50 | 45 | 89.8\% | 1.9 | 1.0 | A |
|  | Subtotal | 550 | 524 | 95.3\% | 13.8 | 3.4 | B |
| Total |  | 1,240 | 1,216 | 98.0\% | 35.9 | 9.9 | D |

Intersection 2 E St-Richards Blvd/First St Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) |  | Total Delay (sec/veh) |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 400 | 378 | 94.6\% | 11.7 | 1.3 | B |
|  | Through | 220 | 207 | 93.9\% | 11.4 | 2.4 | B |
|  | Right Turn | 480 | 464 | 96.7\% | 3.1 | 0.5 | A |
|  | Subtotal | 1,100 | 1,049 | 95.4\% | 7.8 | 0.9 | A |
| SB | Left Turn | 10 | 10 | 95.0\% | 50.9 | 28.1 | D |
|  | Through | 180 | 178 | 99.1\% | 62.0 | 12.7 | E |
|  | Right Turn | 40 | 36 | 90.0\% | 44.9 | 18.6 | D |
|  | Subtotal | 230 | 224 | 97.3\% | 59.4 | 12.4 | E |
| EB | Left Turn | 10 | 9 | 87.0\% | 93.1 | 55.0 | F |
|  | Through | 50 | 49 | 97.4\% | 88.0 | 22.3 | F |
|  | Right Turn | 340 | 347 | 102.1\% | 15.0 | 4.9 | B |
|  | Subtotal | 400 | 404 | 101.1\% | 26.0 | 4.9 | C |
| WB | Left Turn | 180 | 179 | 99.4\% | 70.4 | 17.3 | E |
|  | Through | 110 | 109 | 99.4\% | 54.3 | 8.5 | D |
|  | Right Turn | 20 | 21 | 106.5\% | 39.8 | 12.8 | D |
|  | Subtotal | 310 | 310 | 99.8\% | 63.1 | 12.0 | E |
| Total |  | 2,040 | 1,987 | 97.4\% | 27.0 | 3.6 | C |

Vissim Post-Processor
Average Results from 10 Runs
Volume and Delay by Movement

I-80 / Richards Blvd Interchange
Design Year Build Conditions
PM Peak Hour

## Intersection 3

Richards Blvd/Olive Dr
Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) |  | Total Delay (sec/veh) |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 260 | 248 | 95.3\% | 50.8 | 3.5 | D |
|  | Through | 850 | 808 | 95.0\% | 40.4 | 8.2 | D |
|  | Right Turn | 240 | 238 | 99.1\% | 13.2 | 4.6 | B |
|  | Subtotal | 1,350 | 1,293 | 95.8\% | 37.4 | 5.7 | D |
| SB | Left Turn | 90 | 90 | 99.6\% | 79.8 | 21.2 | E |
|  | Through | 510 | 507 | 99.3\% | 43.7 | 8.9 | D |
|  | Right Turn | 100 | 107 | 106.5\% | 48.1 | 10.4 | D |
|  | Subtotal | 700 | 703 | 100.4\% | 49.4 | 11.0 | D |
| EB | Left Turn | 80 | 78 | 97.5\% | 57.5 | 5.3 | E |
|  | Through | 60 | 59 | 98.3\% | 53.7 | 10.4 | D |
|  | Right Turn | 440 | 438 | 99.6\% | 18.2 | 2.7 | B |
|  | Subtotal | 580 | 575 | 99.2\% | 27.7 | 2.1 | C |
| WB | Left Turn | 190 | 190 | 100.2\% | 86.6 | 36.5 | F |
|  | Through | 50 | 48 | 95.8\% | 67.4 | 24.9 | E |
|  | Right Turn | 170 | 164 | 96.5\% | 71.4 | 27.0 | E |
|  | Subtotal | 410 | 402 | 98.1\% | 79.4 | 28.1 | E |
| Total |  | 3,040 | 2,974 | 97.8\% | 44.4 | 5.1 | D |



Vissim Post-Processor
Average Results from 10 Runs
Volume and Delay by Movement

I-80 / Richards Blvd Interchange
Design Year Build Conditions
PM Peak Hour

| Intersection 5 |  | Richards Blvd/l-80 EB Ramps |  |  | Total Delay (sec/veh) |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Movement | Demand Volume (vph) | Served Volume (vph) |  |  |  |  |
| Direction |  |  | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn |  |  |  |  |  |  |
|  | Through | 1,500 | 1,431 | 95.4\% | 19.8 | 6.9 | B |
|  | Right Turn | 180 | 170 | 94.4\% | 15.4 | 7.5 | B |
|  | Subtotal | 1,680 | 1,601 | 95.3\% | 19.4 | 6.9 | B |
| SB | Left Turn | 250 | 242 | 96.8\% | 49.1 | 8.7 | D |
|  | Through <br> Right Turn | 690 | 685 | 99.2\% | 17.0 | 1.8 | B |
|  | Subtotal | 940 | 927 | 98.6\% | 24.6 | 2.7 | C |
| EB | Left Turn <br> Through Right Turn |  |  |  |  |  |  |
|  | Subtotal |  |  |  |  |  |  |
| WB | Left Turn | 780 | 739 | 94.8\% | 149.9 | 94.4 | F |
|  | Through Right Turn | 250 | 242 | 96.7\% | 115.7 | 76.3 | F |
|  | Subtotal | 1,030 | 981 | 95.2\% | 141.8 | 90.3 | F |
| Total |  | 3,650 | 3,508 | 96.1\% | 52.9 | 20.7 | D |


| Intersection 6 |  | Research Park Dr/Richards Blvd-Cowell Blvd |  |  |  |  | Signal |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Direction | Movement | Demand | Served | me (vph) |  | elay (sec/v |  |
|  |  | Volume (vph) | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 150 | 145 | 96.7\% | 53.6 | 5.3 | D |
|  | Through | 40 | 41 | 103.5\% | 28.6 | 10.6 | C |
|  | Right Turn | 70 | 71 | 100.9\% | 13.3 | 6.4 | B |
|  | Subtotal | 260 | 257 | 98.8\% | 36.9 | 8.1 | D |
| SB | Left Turn | 40 | 37 | 92.0\% | 131.5 | 102.3 | F |
|  | Through | 30 | 28 | 94.7\% | 121.2 | 106.7 | F |
|  | Right Turn | 330 | 329 | 99.7\% | 112.7 | 95.1 | F |
|  | Subtotal | 400 | 394 | 98.5\% | 115.0 | 96.5 | F |
| EB | Left Turn | 290 | 274 | 94.6\% | 106.4 | 22.2 | F |
|  | Through | 1,050 | 1,068 | 101.7\% | 22.5 | 3.6 | C |
|  | Right Turn | 80 | 76 | 95.3\% | 18.4 | 7.3 | B |
|  | Subtotal | 1,420 | 1,418 | 99.9\% | 38.7 | 5.5 | D |
| WB | Left Turn | 30 | 28 | 93.3\% | 158.2 | 16.2 | F |
|  | Through | 1,110 | 1,048 | 94.4\% | 124.5 | 7.6 | F |
|  | Right Turn | 40 | 39 | 96.3\% | 113.4 | 14.0 | F |
|  | Subtotal | 1,180 | 1,115 | 94.5\% | 125.1 | 7.4 | F |
| Total |  | 3,260 | 3,184 | 97.7\% | 77.7 | 11.6 | E |

D St/First St
Signal


E St-Richards Blvd/First St
Signal

| Direction | Movement | Storage | Average Queue (ft) |  |  |  | Maximum Queue (ft) |  |  |  | Exceeds <br> Storage? |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | (ft) | Average | Std. Dev. | Minimum | Maximum | Average | Std. Dev. | Minimum | Maximum |  |
| NB | U Turn |  |  |  |  |  |  |  |  |  |  |
|  | Second Left |  |  |  |  |  |  |  |  |  |  |
|  | Left Turn | 625 | 56 | 15 | 31 | 75 | 397 | 133 | 168 | 552 | NO |
|  | Through | 625 | 56 | 15 | 31 | 75 | 397 | 133 | 168 | 552 | NO |
|  | Right Turn | 180 | 0 | 0 | 0 | 0 | 23 | 10 | 11 | 42 | NO |
|  | Second Right |  |  |  |  |  |  |  |  |  |  |
| SB | U Turn |  |  |  |  |  |  |  |  |  |  |
|  | Second Left |  |  |  |  |  |  |  |  |  |  |
|  | Left Turn | 400 | 64 | 4 | 58 | 69 | 258 | 25 | 211 | 296 | NO |
|  | Through | 400 | 64 | 4 | 58 | 69 | 258 | 25 | 211 | 296 | NO |
|  | Right Turn | 400 | 12 | 7 | 4 | 23 | 169 | 48 | 80 | 232 | NO |
|  | Second Right |  |  |  |  |  |  |  |  |  |  |
| EB | U Turn |  |  |  |  |  |  |  |  |  |  |
|  | Second Left |  |  |  |  |  |  |  |  |  |  |
|  | Left Turn | 100 | 49 | 6 | 39 | 58 | 263 | 39 | 195 | 346 | MAX |
|  | Through | 225 | 49 | 6 | 39 | 58 | 263 | 39 | 195 | 346 | MAX |
|  | Right Turn | 225 | 23 | 2 | 20 | 26 | 203 | 19 | 167 | 231 | NO |
|  | Second Right |  |  |  |  |  |  |  |  |  |  |
| WB | U Turn |  |  |  |  |  |  |  |  |  |  |
|  | Second Left |  |  |  |  |  |  |  |  |  |  |
|  | Left Turn | 225 | 74 | 17 | 50 | 98 | 242 | 56 | 186 | 338 | MAX |
|  |  |  |  |  |  |  |  |  |  |  |  |
|  | Through | 225 | 74 | 17 | 50 | 98 | 242 | 56 | 186 | 338 | MAX |
|  | Right Turn | 225 | 74 | 17 | 50 | 98 | 242 | 56 | 186 | 338 | MAX |
|  | Second Right |  |  |  |  |  |  |  |  |  |  |

Richards Blvd/Olive Dr
Signal

| Direction | Movement | Storage | Average Queue (ft) |  |  |  | Maximum Queue (ft) |  |  |  | Exceeds Storage? |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | (ft) | Average | Std. Dev. | Minimum | Maximum | Average | Std. Dev. | Minimum | Maximum |  |
| NB | U Turn |  |  |  |  |  |  |  |  |  |  |
|  | Second Left |  |  |  |  |  |  |  |  |  |  |
|  | Left Turn | 175 | 144 | 9 | 125 | 160 | 580 | 7 | 569 | 591 | MAX |
|  | Through | 600 | 176 | 13 | 160 | 199 | 580 | 10 | 570 | 604 | NO |
|  | Right Turn | 275 | 0 | 0 | 0 | 0 | 25 | 7 | 15 | 40 | NO |
|  | Second Right |  |  |  |  |  |  |  |  |  |  |
| SB | U Turn |  |  |  |  |  |  |  |  |  |  |
|  | Second Left |  |  |  |  |  |  |  |  |  |  |
|  | Left Turn | 625 | 13 | 4 | 8 | 19 | 119 | 77 | 54 | 250 | NO |
|  | Through | 625 | 188 | 25 | 157 | 218 | 675 | 51 | 598 | 749 | MAX |
|  | Right Turn | 625 | 186 | 25 | 155 | 216 | 674 | 51 | 598 | 748 | MAX |
|  | Second Right |  |  |  |  |  |  |  |  |  |  |
| EB | U Turn |  |  |  |  |  |  |  |  |  |  |
|  | Second Left |  |  |  |  |  |  |  |  |  |  |
|  | Left Turn | 250 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | NO |
|  | Through | 600 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | NO |
|  | Right Turn | 250 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | NO |
|  | Second Right |  |  |  |  |  |  |  |  |  |  |
| WB | U Turn |  |  |  |  |  |  |  |  |  |  |
|  | Second Left |  |  |  |  |  |  |  |  |  |  |
|  | Left Turn | 200 | 5 | 6 | 0 | 14 | 77 | 61 | 25 | 215 | NO |
|  | Through | 1,500 | 5 | 6 | 0 | 14 | 77 | 61 | 25 | 215 | NO |
|  | Right Turn |  | 5 | 6 | 0 | 14 | 77 | 61 | 25 | 215 | NO |
|  | Second Right |  |  |  |  |  |  |  |  |  |  |

Intersection 4
Richards Blvd/I-80 WB Ramps
Signal

| Direction | Movement | Storage <br> (ft) | Average Queue ( ft ) |  |  |  | Maximum Queue (ft) |  |  |  | Exceeds <br> Storage? |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Average | Std. Dev. | Minimum | Maximum | Average | Std. Dev. | Minimum | Maximum |  |
| NB | U Turn | $\begin{aligned} & 475 \\ & 825 \end{aligned}$ | $\begin{aligned} & 102 \\ & 181 \end{aligned}$ | $\begin{gathered} 5 \\ 14 \end{gathered}$ | $\begin{gathered} 94 \\ 166 \end{gathered}$ | $\begin{aligned} & 113 \\ & 215 \end{aligned}$ | $\begin{aligned} & 301 \\ & 575 \end{aligned}$ | $\begin{aligned} & 17 \\ & 39 \end{aligned}$ | $\begin{aligned} & 268 \\ & 494 \end{aligned}$ | $\begin{aligned} & 319 \\ & 644 \end{aligned}$ | $\begin{aligned} & \text { NO } \\ & \text { NO } \end{aligned}$ |
|  | Second Left |  |  |  |  |  |  |  |  |  |  |
|  | Left Turn |  |  |  |  |  |  |  |  |  |  |
|  | Through |  |  |  |  |  |  |  |  |  |  |
|  | Right Turn |  |  |  |  |  |  |  |  |  |  |
|  | Second Right |  |  |  |  |  |  |  |  |  |  |
| SB | U Turn | $\begin{aligned} & 600 \\ & 225 \end{aligned}$ | 34 | 40 | $\begin{gathered} 29 \\ 0 \end{gathered}$ | $\begin{gathered} 40 \\ 1 \end{gathered}$ | $\begin{gathered} 279 \\ 63 \end{gathered}$ | $\begin{aligned} & 29 \\ & 27 \end{aligned}$ | $\begin{gathered} 255 \\ 25 \end{gathered}$ | $\begin{aligned} & 339 \\ & 111 \end{aligned}$ | $\begin{aligned} & \text { NO } \\ & \text { NO } \end{aligned}$ |
|  | Second Left |  |  |  |  |  |  |  |  |  |  |
|  | Left Turn |  |  |  |  |  |  |  |  |  |  |
|  | Through |  |  |  |  |  |  |  |  |  |  |
|  | Right Turn |  |  |  |  |  |  |  |  |  |  |
|  | Second Right |  |  |  |  |  |  |  |  |  |  |
| EB | U Turn |  |  |  |  |  |  |  |  |  |  |
|  | Second Left |  |  |  |  |  |  |  |  |  |  |
|  | Left Turn |  |  |  |  |  |  |  |  |  |  |
|  | Through |  |  |  |  |  |  |  |  |  |  |
|  | Right Turn |  |  |  |  |  |  |  |  |  |  |
|  | Second Right |  |  |  |  |  |  |  |  |  |  |
| WB | U Turn | 450 | 83 | 6 | 69 | 88 | 315 | 36 | 250 | 363 | NO |
|  | Second Left |  |  |  |  |  |  |  |  |  |  |
|  | Left Turn |  |  |  |  |  |  |  |  |  |  |
|  | Through |  |  |  |  |  |  |  |  |  |  |
|  | Right Turn | 1,225 | 167 | 56 | 74 | 240 | 577 | 191 | 341 | 824 | NO |
|  | Second Right |  |  |  |  |  |  |  |  |  |  |

Intersection 5
I-80 EB Ramps/Richards Blvd
Signal


Research Park Dr/Richards Blvd-Cowell Blvd
Signal

| Direction | Movement | Storage (ft) | Average Queue (ft) |  |  |  | Maximum Queue (ft) |  |  |  | Exceeds Storage? |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Average | Std. Dev. | Minimum | Maximum | Average | Std. Dev. | Minimum | Maximum |  |
| NB | U Turn | $\begin{aligned} & 100 \\ & 625 \end{aligned}$ | 214 | 21 | $\begin{gathered} 19 \\ 2 \end{gathered}$ | $\begin{gathered} 25 \\ 6 \end{gathered}$ | $\begin{aligned} & 82 \\ & 53 \end{aligned}$ | $\begin{aligned} & 11 \\ & 16 \end{aligned}$ | $\begin{aligned} & 61 \\ & 23 \end{aligned}$ | $\begin{aligned} & 99 \\ & 75 \end{aligned}$ | $\begin{aligned} & \text { NO } \\ & \text { NO } \end{aligned}$ |
|  | Second Left |  |  |  |  |  |  |  |  |  |  |
|  | Left Turn |  |  |  |  |  |  |  |  |  |  |
|  | Through |  |  |  |  |  |  |  |  |  |  |
|  | Right Turn |  |  |  |  |  |  |  |  |  |  |
|  | Second Right |  |  |  |  |  |  |  |  |  |  |
| SB | U Turn | $\begin{gathered} 125 \\ 1,500 \end{gathered}$ | 618 | 23 | $\begin{gathered} 4 \\ 12 \end{gathered}$ | $\begin{gathered} 9 \\ 21 \end{gathered}$ | 48146 | $\begin{aligned} & 10 \\ & 22 \end{aligned}$ | $\begin{gathered} 30 \\ 118 \end{gathered}$ | $\begin{gathered} 65 \\ 174 \end{gathered}$ | $\begin{aligned} & \text { NO } \\ & \text { NO } \end{aligned}$ |
|  | Second Left |  |  |  |  |  |  |  |  |  |  |
|  | Left Turn |  |  |  |  |  |  |  |  |  |  |
|  | Through |  |  |  |  |  |  |  |  |  |  |
|  | Right Turn |  |  |  |  |  |  |  |  |  |  |
|  | Second Right |  |  |  |  |  |  |  |  |  |  |
| EB | U Turn | 450 | 113 | 19 | 86 | 151 | 453 | 39 | 392 | 513 | MAX |
|  | Second Left |  |  |  |  |  |  |  |  |  |  |
|  | Left Turn | 450 | 113 | 19 | 86 | 151 | 453 | 39 | 392 | 513 | MAX |
|  | Through | 450 | 112 | 10 | 95 | 130 | 453 | 27 | 395 | 480 | MAX |
|  | Right Turn |  |  |  |  |  |  |  |  |  |  |
|  | Second Right |  |  |  |  |  |  |  |  |  |  |
| WB | U Turn | $\begin{gathered} 75 \\ 1,125 \end{gathered}$ | 6767 | $\begin{aligned} & 72 \\ & 72 \end{aligned}$ | 8 | $\begin{aligned} & 245 \\ & 246 \end{aligned}$ | $\begin{aligned} & 520 \\ & 525 \end{aligned}$ | 220220 | 209215 | 874880 | $\begin{gathered} \text { MAX } \\ \text { NO } \end{gathered}$ |
|  | Second Left |  |  |  |  |  |  |  |  |  |  |
|  | Left Turn |  |  |  |  |  |  |  |  |  |  |
|  | Through |  |  |  |  |  |  |  |  |  |  |
|  | Right Turn |  |  |  |  |  |  |  |  |  |  |
|  | Second Right |  |  |  |  |  |  |  |  |  |  |

D St/First St
Signal


E St-Richards Blvd/First S
Signal


Richards Blvd/Olive Dr
Signal


Intersection 4
Richards Blvd/I-80 WB Ramps
Signal


## Intersection 5 Richards Blvd/I-80 EB Ramps

Signal


Signa

| Direction | Movement | Storage (ft) | Average Queue (ft) |  |  |  | Maximum Queue (ft) |  |  |  | Exceeds Storage? |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Average | Std. Dev. | Minimum | Maximum | Average | Std. Dev. | Minimum | Maximum |  |
| NB | U Turn | $\begin{aligned} & 100 \\ & 625 \end{aligned}$ | 3310 | 21 | $\begin{gathered} 29 \\ 8 \end{gathered}$ | $\begin{aligned} & 37 \\ & 12 \end{aligned}$ | $\begin{gathered} 107 \\ 93 \end{gathered}$ | $\begin{aligned} & 12 \\ & 15 \end{aligned}$ | $\begin{aligned} & 96 \\ & 76 \end{aligned}$ | $\begin{aligned} & 136 \\ & 123 \end{aligned}$ | $\begin{gathered} \text { MAX } \\ \text { NO } \end{gathered}$ |
|  | Second Left |  |  |  |  |  |  |  |  |  |  |
|  | Left Turn |  |  |  |  |  |  |  |  |  |  |
|  | Through |  |  |  |  |  |  |  |  |  |  |
|  | Right Turn |  |  |  |  |  |  |  |  |  |  |
|  | Second Right |  |  |  |  |  |  |  |  |  |  |
| SB | U Turn | $\begin{gathered} 125 \\ 1,500 \end{gathered}$ | $\begin{gathered} 14 \\ 204 \end{gathered}$ | $\begin{gathered} 4 \\ 125 \end{gathered}$ | $\begin{gathered} 6 \\ 104 \end{gathered}$ | $\begin{gathered} 21 \\ 521 \end{gathered}$ | 84498 | $\begin{gathered} 32 \\ 198 \end{gathered}$ | $\begin{gathered} 45 \\ 323 \end{gathered}$ | $\begin{aligned} & 131 \\ & 966 \end{aligned}$ | $\begin{aligned} & \text { NO } \\ & \text { NO } \end{aligned}$ |
|  | Second Left |  |  |  |  |  |  |  |  |  |  |
|  | Left Turn |  |  |  |  |  |  |  |  |  |  |
|  | Through |  |  |  |  |  |  |  |  |  |  |
|  | Right Turn |  |  |  |  |  |  |  |  |  |  |
|  | Second Right |  |  |  |  |  |  |  |  |  |  |
| EB | U Turn | 450 | 174 | 28 | 142 | 227 | 436 | 54 | 300 | 486 | NO |
|  | Second Left |  |  |  |  |  |  |  |  |  |  |
|  | Left Turn | 450 | 174 | 28 | 142 | 227 | 436 | 54 | 300 | 486 | NO |
|  | Through | 450 | 59 | 5 | 50 | 67 | 337 | 51 | 267 | 422 | NO |
|  | Right Turn |  |  |  |  |  |  |  |  |  |  |
|  | Second Right |  |  |  |  |  |  |  |  |  |  |
| WB | U Turn |  | $\begin{aligned} & 687 \\ & 689 \end{aligned}$ | $\begin{aligned} & 94 \\ & 95 \end{aligned}$ |  | 838840 | $\begin{aligned} & 1,462 \\ & 1,467 \end{aligned}$ | 117117 | $\begin{aligned} & 1,267 \\ & 1,273 \end{aligned}$ | 1,5811,587 | AVGMAX |
|  | Second Left |  |  |  |  |  |  |  |  |  |  |
|  | Left Turn |  |  |  |  |  |  |  |  |  |  |
|  | Through |  |  |  |  |  |  |  |  |  |  |
|  | Right Turn |  |  |  |  |  |  |  |  |  |  |
|  | Second Right |  |  |  |  |  |  |  |  |  |  |


|  | Freeway Basic Report |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Eastbound I-80 |
| Segment | West of Old Davis Rd |
| Alternative | Design Year |
| Time Period | AM Peak Hour |


|  | General |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
|  | Purpose Lanes - Geometric Data |  |  |  |  |  |
| General Purpose Lanes, N | 4 | ln | Terrain Type | Level |  |  |
| Segment Length, L | 1,500 | ft | Percent Grade | - |  |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |  |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 1.67 | $\mathrm{ramps} / \mathrm{mi}$ |  |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 70.5 | mph |  |


| General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


| General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Volume, V | 5,203 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.95 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,492 | pcphpl |
| Total Trucks | 9.0\% |  | Capacity, c | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - |  | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.62 |  |


| General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 70.5 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 69.3 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 21.5 | pcpmpl |
| Total Ramp Density Adjustment | 4.9 | mph | Level of Service, LOS | C |  |



| Entering General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :--- | :---: | :--- | :--- | :--- | :--- |
| Volume, V | 5,203 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.95 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,492 | pcphpl |
| Total Trucks | $9.0 \%$ |  | Capacity, c | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |  |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.62 |  |


| Entering General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 70.5 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 69.3 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 21.5 | pcpmpl |
| Total Ramp Density Adjustment | 4.9 | mph | Level of Service, LOS | C |  |


| Segment General Purpose Lanes - Capacity, Speed, and Density |  |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
| General Purpose Lanes, N | 5 | $\ln$ | Average Speed, S | 70.4 | mph |  |
| Adjusted Capacity, cadj | 2,400 | pcphpl | Density, D | 17.3 | pcphpl |  |
| Flow Rate, vp | 1,216 | pcphpl | Level of Service, LOS | B |  |  |
| Volume-to-Capacity Ratio, v/c | 0.51 |  |  |  |  |  |

## Freeway Merge Report

| Freeway Merge Report |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Project I-80/Richards B <br> Freeway Eastbound I-80 <br> Segment Old Davis Rd O <br> Alternative Design Year <br> Time Period AM Peak Hour |  |  |  |  |
| Geometric Data |  |  |  |  |
|  | Freeway | On Ramp |  |  |
| Number of Lanes, N | 4 | 2 |  |  |
| Free-Flow Speed, FFS | 70.5 | 45 |  | mph |
| Segment Length, L / Acceleration Length, LA | 1,500 | 0 |  | ft |
| Terrain Type | Level | Level |  |  |
| Percent Grade | - | - |  |  |
| Grade Length | - |  |  | ft |
| Segment Type / Ramp Type | Freeway | Right |  |  |
| Adjustment Factors |  |  |  |  |
|  | Freeway | On Ramp |  |  |
| Driver Population | Familiar | Familiar |  |  |
| Weather Type | Non-severe | Non-severe |  |  |
| Incident Type | No incident | No incident |  |  |
| Capacity Adjustment Factor, CAF | 1.00 | 1.00 |  |  |
| Demand Adjustment Factor, DAF | 1.00 | 1.00 |  |  |
| Volume Data |  |  |  |  |
| Junction Components | Freeway | On Ramp |  |  |
| Volume, V | 5,203 | 100 |  | vph |
| Peak Hour Factor, PHF | 0.95 | 0.92 |  |  |
| Total Trucks | 9.0\% | 3.0\% |  |  |
| Single Unit/Tractor-Trailer Mix | - | - |  |  |
| Passenger Car Equivalent, $\mathrm{E}_{T}$ | 2.0 | 2.0 |  |  |
| Heavy Vehicle Adjustment, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 | 0.971 |  |  |
| Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 5,970 | 112 |  | pcph |
| Adjacent Ramp Data |  |  |  |  |
|  |  | Upstream | Downstream |  |
| Adjacent Ramp Meeting Criteria |  | No | No |  |
| Type of Adjacent Ramp |  |  |  |  |
| Distance to Adjacent Ramp |  |  |  | ft |
| Volume on Adjacent Ramp |  |  |  | pcph |

## Freeway Merge Report



| Ramp Influence Area Density and Level of Service |  |  |
| :--- | :--- | :---: |
|  |  |  |
| Density in Ramp Influence Area, $D_{R}$ | pcpmpl |  |
| Level of Service, LOS |  |  |

## Segment Speed, Flow, and Density

Speed Adjustment Factor, SAF
Speed Index, $\mathrm{M}_{\mathrm{S}}$ or $\mathrm{D}_{\mathrm{S}}$
Average Speed in Ramp Influence Area, $S_{R} \mathrm{mph}$

Average Flow in Outer Lanes, $\mathrm{v}_{\mathrm{OA}}$
pcphpl
mph
Average Speed in Outer Lanes, $\mathrm{S}_{0}$
mph
Density across All Lanes, D
pcpmpl

|  | Freeway Basic Report |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Eastbound I-80 |
| Segment | Old Davis Rd to Lane Drop |
| Alternative | Design Year |
| Time Period | AM Peak Hour |


|  | General |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
|  | Purpose Lanes - Geometric Data |  |  |  |  |  |
| General Purpose Lanes, N | 4 | ln | Terrain Type | Level |  |  |
| Segment Length, L | 820 | ft | Percent Grade | - |  |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |  |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 1.67 | $\mathrm{ramps} / \mathrm{mi}$ |  |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 70.5 | mph |  |


| General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


|  | General Purpose Lanes - Demand and Capacity |  |  |  |  |
| :--- | :---: | :--- | :--- | :--- | :--- |
| Volume, V | 5,289 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.95 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,517 | pcphpl |
| Total Trucks | $9.0 \%$ |  | Capacity, c | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |  |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.63 |  |


| General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 70.5 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 69.2 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 21.9 | pcpmpl |
| Total Ramp Density Adjustment | 4.9 | mph | Level of Service, LOS | C |  |


|  | Freeway Basic Report |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Eastbound I-80 |
| Segment | Lane Drop to Richards Blvd |
| Alternative | Design Year |
| Time Period | AM Peak Hour |


|  | General |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
|  | Purpose Lanes - Geometric Data |  |  |  |  |  |
| General Purpose Lanes, N | 3 | ln | Terrain Type | Level |  |  |
| Segment Length, L | 1,220 | ft | Percent Grade | - |  |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |  |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 1.67 | $\mathrm{ramps} / \mathrm{mi}$ |  |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 70.5 | mph |  |


| General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


|  | General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :--- | :---: | :--- | :--- | :--- | :--- | :---: |
| Volume, V | 5,289 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |  |
| Peak Hour Factor, PHF | 0.95 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 2,023 | pcphpl |  |
| Total Trucks | $9.0 \%$ |  | Capacity, c | 2,400 | pcphpl |  |
| Single Unit/Tractor-Trailer Mix | - | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |  |  |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.84 |  |  |


| General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 70.5 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 62.3 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 32.5 | pcpmpl |
| Total Ramp Density Adjustment | 4.9 | mph | Level of Service, LOS | D |  |

$\qquad$

## Freeway Diverge Report

| Freeway Diverge Report |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Project I-80/Richards B <br> Freeway Eastbound I-80 <br> Segment Richards Blvd O <br> Alternative Design Year <br> Time Period AM Peak Hour |  |  |  |  |
| Geometric Data |  |  |  |  |
|  | Freeway |  | Off Ramp |  |
| Number of Lanes, N | 3 |  | 1 |  |
| Free-Flow Speed, FFS | 70.5 |  | 25 | mph |
| Segment Length, L / Deceleration Length, LD | 1,500 |  | 150 | ft |
| Terrain Type | Level |  | Level |  |
| Percent Grade | - |  | - |  |
| Grade Length | - |  | - | ft |
| Segment Type / Ramp Type | Freeway |  | Right |  |
| Adjustment Factors |  |  |  |  |
|  | Freeway |  | Off Ramp |  |
| Driver Population | Familiar |  | Familiar |  |
| Weather Type | Non-severe |  | Non-severe |  |
| Incident Type | No incident |  | No incident |  |
| Capacity Adjustment Factor, CAF | 1.00 |  | 1.00 |  |
| Demand Adjustment Factor, DAF | 1.00 |  | 1.00 |  |
| Volume Data |  |  |  |  |
| Junction Components | Freeway |  | Off Ramp |  |
| Volume, V | 5,289 |  | 940 | vph |
| Peak Hour Factor, PHF | 0.95 |  | 0.92 |  |
| Total Trucks | 9.0\% |  | 3.3\% |  |
| Single Unit/Tractor-Trailer Mix | - |  | - |  |
| Passenger Car Equivalent, $\mathrm{E}_{T}$ | 2.0 |  | 2.0 |  |
| Heavy Vehicle Adjustment, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  | 0.968 |  |
| Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 6,068 |  | 1,055 | pcph |
| Adjacent Ramp Data |  |  |  |  |
|  |  | Upstream | Downstream |  |
| Adjacent Ramp Meeting Criteria |  | No | Yes |  |
| Type of Adjacent Ramp |  |  | On |  |
| Distance to Adjacent Ramp |  |  | 1,780 | ft |
| Volume on Adjacent Ramp |  |  | 537 | pcph |

## Freeway Diverge Report



|  | Freeway Basic Report |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Eastbound I-80 |
| Segment | Richards Blvd Off to On |
| Alternative | Design Year |
| Time Period | AM Peak Hour |


|  | General |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
|  | Purpose Lanes - Geometric Data |  |  |  |  |  |
| General Purpose Lanes, N | 3 | ln | Terrain Type | Level |  |  |
| Segment Length, L | 1,500 | ft | Percent Grade | - |  |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |  |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 1.67 | $\mathrm{ramps} / \mathrm{mi}$ |  |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 70.5 | mph |  |


| General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


|  | General Purpose Lanes - Demand and Capacity |  |  |  |  |
| :--- | :---: | :--- | :--- | :--- | :--- |
| Volume, V | 4,481 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.95 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,714 | pcphpl |
| Total Trucks | $9.0 \%$ |  | Capacity, c | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |  |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.71 |  |


| General Purpose Lanes - Speed and Density |  |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 70.5 | mph |  |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 67.2 | mph |  |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 25.5 | pcpmpl |  |
| Total Ramp Density Adjustment | 4.9 | mph | Level of Service, LOS | C |  |  |


| Freeway Merge Report |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Project I-80/Richards B <br> Freeway Eastbound I-80 <br> Segment Richards Blvd O <br> Alternative Design Year <br> Time Period AM Peak Hour |  |  |  |  |
| Geometric Data |  |  |  |  |
|  | Freeway | On Ramp |  |  |
| Number of Lanes, N | 3 | 1 |  |  |
| Free-Flow Speed, FFS | 70.5 | 45 |  | mph |
| Segment Length, L / Acceleration Length, LA | 1,500 | 500 |  | ft |
| Terrain Type | Level | Level |  |  |
| Percent Grade | - | - |  |  |
| Grade Length | - | - |  | ft |
| Segment Type / Ramp Type | Freeway | Right |  |  |
| Adjustment Factors |  |  |  |  |
|  | Freeway | On Ramp |  |  |
| Driver Population | Familiar | Familiar |  |  |
| Weather Type | Non-severe | Non-severe |  |  |
| Incident Type | No incident | No incident |  |  |
| Capacity Adjustment Factor, CAF | 1.00 | 1.00 |  |  |
| Demand Adjustment Factor, DAF | 1.00 | 1.00 |  |  |
| Volume Data |  |  |  |  |
| Junction Components | Freeway | On Ramp |  |  |
| Volume, V | 4,481 | 480 |  | vph |
| Peak Hour Factor, PHF | 0.95 | 0.92 |  |  |
| Total Trucks | 9.0\% | 3.0\% |  |  |
| Single Unit/Tractor-Trailer Mix | - | - |  |  |
| Passenger Car Equivalent, $\mathrm{E}_{T}$ | 2.0 | 2.0 |  |  |
| Heavy Vehicle Adjustment, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 | 0.971 |  |  |
| Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 5,141 | 537 |  | pcph |
| Adjacent Ramp Data |  |  |  |  |
|  |  | Upstream | Downstream |  |
| Adjacent Ramp Meeting Criteria |  | Yes | No |  |
| Type of Adjacent Ramp |  | Off |  |  |
| Distance to Adjacent Ramp |  | 1,780 |  | ft |
| Volume on Adjacent Ramp |  | 1,055 |  | pcph |



|  | Freeway Basic Report |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Eastbound I-80 |
| Segment | Richards Blvd to Chiles Rd |
| Alternative | Design Year |
| Time Period | AM Peak Hour |


|  | General |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
|  | Purpose Lanes - Geometric Data |  |  |  |  |  |
| General Purpose Lanes, N | 3 | ln | Terrain Type | Level |  |  |
| Segment Length, L | 5,710 | ft | Percent Grade | - |  |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |  |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 1.50 | $\mathrm{ramps} / \mathrm{mi}$ |  |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 70.9 | mph |  |


| General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


|  | General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :--- | :--- | :--- |
| Volume, V | 4,893 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{Hv}}$ | 0.917 |  |  |
| Peak Hour Factor, PHF | 0.95 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,872 | pcphpl |  |
| Total Trucks | $9.0 \%$ |  | Capacity, c | 2,400 | pcphpl |  |
| Single Unit/Tractor-Trailer Mix | - | Adjusted Capacity, $\mathrm{c}_{\mathrm{adj}}$ | 2,400 | pcphpl |  |  |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 | Volume-to-Capacity Ratio, v/c | 0.78 |  |  |  |


| General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 70.9 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 65.1 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 28.7 | pcpmpl |
| Total Ramp Density Adjustment | 4.5 | mph | Level of Service, LOS | D |  |

$\qquad$

## Freeway Diverge Report

| Freeway Diverge Report |  |  |  |
| :---: | :---: | :---: | :---: |
| Project I-80/Richards B <br> Freeway Eastbound I-80 <br> Segment Chiles Rd Off Ra <br> Alternative Design Year <br> Time Period AM Peak Hour |  |  |  |
| Geometric Data |  |  |  |
|  | Freeway | Off Ramp |  |
| Number of Lanes, N | 3 | 2 |  |
| Free-Flow Speed, FFS | 70.9 | 25 | mph |
| Segment Length, L / Deceleration Length, LD | 1,500 | 1,500 | ft |
| Terrain Type | Level | Level |  |
| Percent Grade | - | - |  |
| Grade Length | - |  | ft |
| Segment Type / Ramp Type | Freeway | Right |  |
| Adjustment Factors |  |  |  |
|  | Freeway | Off Ramp |  |
| Driver Population | Familiar | Familiar |  |
| Weather Type | Non-severe | Non-severe |  |
| Incident Type | No incident | No incident |  |
| Capacity Adjustment Factor, CAF | 1.00 | 1.00 |  |
| Demand Adjustment Factor, DAF | 1.00 | 1.00 |  |
| Volume Data |  |  |  |
| Junction Components | Freeway | Off Ramp |  |
| Volume, V | 4,893 | 730 | vph |
| Peak Hour Factor, PHF | 0.95 | 0.92 |  |
| Total Trucks | 9.0\% | 3.0\% |  |
| Single Unit/Tractor-Trailer Mix | - | - |  |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 | 2.0 |  |
| Heavy Vehicle Adjustment, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 | 0.971 |  |
| Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 5,615 | 817 | pcph |

## Adjacent Ramp Data

Adjacent Ramp Meeting Criteria
Upstream Downstream

Type of Adjacent Ramp
Distance to Adjacent Ramp
ft
Volume on Adjacent Ramp
pcph

## Freeway Diverge Report



|  | Freeway Basic Report |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Eastbound I-80 |
| Segment | Chiles Rd Off to Mace Rd On |
| Alternative | Design Year |
| Time Period | AM Peak Hour |


|  | General |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
|  | Purpose Lanes - Geometric Data |  |  |  |  |  |
| General Purpose Lanes, N | 3 | ln | Terrain Type | Level |  |  |
| Segment Length, L | 1,000 | ft | Percent Grade | - |  |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |  |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 1.50 | $\mathrm{ramps} / \mathrm{mi}$ |  |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 70.9 | mph |  |


| General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


| General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Volume, V | 4,266 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.95 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,631 | pcphpl |
| Total Trucks | 9.0\% |  | Capacity, c | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - |  | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.68 |  |


| General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 70.9 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 68.4 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 23.9 | pcpmpl |
| Total Ramp Density Adjustment | 4.5 | mph | Level of Service, LOS | C |  |


|  | Freeway Basic Report |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Eastbound I-80 |
| Segment | West of Old Davis Rd |
| Alternative | Design Year |
| Time Period | PM Peak Hour |


|  | General |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
|  | Purpose Lanes - Geometric Data |  |  |  |  |  |
| General Purpose Lanes, N | 4 | ln | Terrain Type | Level |  |  |
| Segment Length, L | 1,500 | ft | Percent Grade | - |  |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |  |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 1.67 | $\mathrm{ramps} / \mathrm{mi}$ |  |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 70.5 | mph |  |


| General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


|  | General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :--- | :--- | :--- |
| Volume, V | 5,306 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{Hv}}$ | 0.917 |  |  |
| Peak Hour Factor, PHF | 0.99 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,461 | pcphpl |  |
| Total Trucks | $9.0 \%$ |  | Capacity, c | 2,400 | pcphpl |  |
| Single Unit/Tractor-Trailer Mix | - | Adjusted Capacity, $\mathrm{c}_{\mathrm{adj}}$ | 2,400 | pcphpl |  |  |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 | Volume-to-Capacity Ratio, v/c | 0.61 |  |  |  |


| General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 70.5 | mph |
| Lane Width Adjustment, f LW | 0.0 | mph | Average Speed, S | 69.6 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 21.0 | pcpmpl |
| Total Ramp Density Adjustment | 4.9 | mph | Level of Service, LOS | C |  |



| Entering General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :--- | :---: | :--- | :--- | :--- | :--- |
| Volume, V | 5,306 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.99 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,461 | pcphpl |
| Total Trucks | $9.0 \%$ |  | Capacity, c | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |  |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.61 |  |


| Entering General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 70.5 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 69.6 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 21.0 | pcpmpl |
| Total Ramp Density Adjustment | 4.9 | mph | Level of Service, LOS | C |  |


| Segment General Purpose Lanes - Capacity, Speed, and Density |  |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
| General Purpose Lanes, N | 5 | $\ln$ | Average Speed, S | 70.4 | mph |  |
| Adjusted Capacity, cadj | 2,400 | pcphpl | Density, D | 17.4 | pcphpl |  |
| Flow Rate, vp | 1,227 | pcphpl | Level of Service, LOS | B |  |  |
| Volume-to-Capacity Ratio, v/c | 0.51 |  |  |  |  |  |

## Freeway Merge Report

| Freeway Merge Report |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Project I-80/Richards Bl <br> Freeway Eastbound I-80 <br> Segment Old Davis Rd On <br> Alternative Design Year <br> Time Period PM Peak Hour |  |  |  |  |
| Geometric Data |  |  |  |  |
|  | Freeway | On Ramp |  |  |
| Number of Lanes, N | 4 | 2 |  |  |
| Free-Flow Speed, FFS | 70.5 | 45 |  | mph |
| Segment Length, L / Acceleration Length, LA | 1,500 | 0 |  | ft |
| Terrain Type | Level | Level |  |  |
| Percent Grade | - | - |  |  |
| Grade Length | - |  |  | ft |
| Segment Type / Ramp Type | Freeway | Right |  |  |
| Adjustment Factors |  |  |  |  |
|  | Freeway | On Ramp |  |  |
| Driver Population | Familiar | Familiar |  |  |
| Weather Type | Non-severe | Non-severe |  |  |
| Incident Type | No incident | No incident |  |  |
| Capacity Adjustment Factor, CAF | 1.00 | 1.00 |  |  |
| Demand Adjustment Factor, DAF | 1.00 | 1.00 |  |  |
| Volume Data |  |  |  |  |
| Junction Components | Freeway | On Ramp |  |  |
| Volume, V | 5,306 | 260 |  | vph |
| Peak Hour Factor, PHF | 0.99 | 0.92 |  |  |
| Total Trucks | 9.0\% | 3.0\% |  |  |
| Single Unit/Tractor-Trailer Mix | - | - |  |  |
| Passenger Car Equivalent, $\mathrm{E}_{T}$ | 2.0 | 2.0 |  |  |
| Heavy Vehicle Adjustment, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 | 0.971 |  |  |
| Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 5,842 | 291 |  | pcph |
| Adjacent Ramp Data |  |  |  |  |
|  |  | Upstream | Downstream |  |
| Adjacent Ramp Meeting Criteria |  | No | No |  |
| Type of Adjacent Ramp |  |  |  |  |
| Distance to Adjacent Ramp |  |  |  | ft |
| Volume on Adjacent Ramp |  |  |  | pcph |

## Freeway Merge Report



| Ramp Influence Area Density and Level of Service |  |  |
| :--- | :--- | :---: |
|  | pcpmpl |  |
| Density in Ramp Influence Area, $D_{R}$ |  |  |

## Segment Speed, Flow, and Density

Speed Adjustment Factor, SAF
Speed Index, $\mathrm{M}_{\mathrm{S}}$ or $\mathrm{D}_{\mathrm{S}}$
Average Speed in Ramp Influence Area, $S_{R} \mathrm{mph}$

Average Flow in Outer Lanes, $\mathrm{v}_{\mathrm{OA}}$
pcphpl
mph
Average Speed in Outer Lanes, $\mathrm{S}_{0}$
Average Speed for Segment, S
mph
Density across All Lanes, D
pcpmpl

|  | Freeway Basic Report |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Eastbound I-80 |
| Segment | Old Davis Rd to Lane Drop |
| Alternative | Design Year |
| Time Period | PM Peak Hour |


|  | General |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
|  | Purpose Lanes - Geometric Data |  |  |  |  |  |
| General Purpose Lanes, N | 4 | ln | Terrain Type | Level |  |  |
| Segment Length, L | 820 | ft | Percent Grade | - |  |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |  |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 1.67 | $\mathrm{ramps} / \mathrm{mi}$ |  |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 70.5 | mph |  |


| General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


|  | General Purpose Lanes - Demand and Capacity |  |  |  |  |
| :--- | :---: | :--- | :--- | :--- | :--- |
| Volume, V | 5,530 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.99 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,522 | pcphpl |
| Total Trucks | $9.0 \%$ |  | Capacity, c | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |  |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.63 |  |


| General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 70.5 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 69.1 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 22.0 | pcpmpl |
| Total Ramp Density Adjustment | 4.9 | mph | Level of Service, LOS | C |  |


|  | Freeway Basic Report |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Eastbound I-80 |
| Segment | Lane Drop to Richards Blvd |
| Alternative | Design Year |
| Time Period | PM Peak Hour |


|  | General |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
|  | Purpose Lanes - Geometric Data |  |  |  |  |  |
| General Purpose Lanes, N | 3 | ln | Terrain Type | Level |  |  |
| Segment Length, L | 1,220 | ft | Percent Grade | - |  |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |  |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 1.67 | $\mathrm{ramps} / \mathrm{mi}$ |  |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 70.5 | mph |  |


| General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


|  | General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :--- | :--- | :--- |
| Volume, V | 5,530 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{Hv}}$ | 0.917 |  |  |
| Peak Hour Factor, PHF | 0.99 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 2,029 | pcphpl |  |
| Total Trucks | $9.0 \%$ |  | Capacity, c | 2,400 | pcphpl |  |
| Single Unit/Tractor-Trailer Mix | - | Adjusted Capacity, $\mathrm{c}_{\mathrm{adj}}$ | 2,400 | pcphpl |  |  |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 | Volume-to-Capacity Ratio, v/c | 0.85 |  |  |  |


| General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 70.5 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 62.2 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 32.6 | pcpmpl |
| Total Ramp Density Adjustment | 4.9 | mph | Level of Service, LOS | D |  |

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## Freeway Diverge Report

| Freeway Diverge Report |  |  |  |
| :---: | :---: | :---: | :---: |
| Project I-80/Richards B <br> Freeway Eastbound I-80 <br> Segment Richards Blvd O <br> Alternative Design Year <br> Time Period PM Peak Hour |  |  |  |
| Geometric Data |  |  |  |
|  | Freeway | Off Ramp |  |
| Number of Lanes, N | 3 | 1 |  |
| Free-Flow Speed, FFS | 70.5 | 25 | mph |
| Segment Length, L / Deceleration Length, LD | 1,500 | 150 | ft |
| Terrain Type | Level | Level |  |
| Percent Grade | - | - |  |
| Grade Length | - | - | ft |
| Segment Type / Ramp Type | Freeway | Right |  |
| Adjustment Factors |  |  |  |
|  | Freeway | Off Ramp |  |
| Driver Population | Familiar | Familiar |  |
| Weather Type | Non-severe | Non-severe |  |
| Incident Type | No incident | No incident |  |
| Capacity Adjustment Factor, CAF | 1.00 | 1.00 |  |
| Demand Adjustment Factor, DAF | 1.00 | 1.00 |  |
| Volume Data |  |  |  |
| Junction Components | Freeway | Off Ramp |  |
| Volume, V | 5,530 | 890 | vph |
| Peak Hour Factor, PHF | 0.99 | 0.92 |  |
| Total Trucks | 9.0\% | 3.0\% |  |
| Single Unit/Tractor-Trailer Mix | - | - |  |
| Passenger Car Equivalent, $\mathrm{E}_{T}$ | 2.0 | 2.0 |  |
| Heavy Vehicle Adjustment, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 | 0.971 |  |
| Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 6,088 | 996 | pcph |

## Adjacent Ramp Data

Adjacent Ramp Meeting Criteria

| Upstream | Downstream |
| :---: | :---: |
| No | Yes |
|  | On |
|  | 1,780 |
|  | 526 |

Type of Adjacent Ramp
Distance to Adjacent Ramp
Volume on Adjacent Ramp

## Freeway Diverge Report



|  | Freeway Basic Report |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Eastbound I-80 |
| Segment | Richards Blvd Off to On |
| Alternative | Design Year |
| Time Period | PM Peak Hour |


|  | General |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
|  | Purpose Lanes - Geometric Data |  |  |  |  |  |
| General Purpose Lanes, N | 3 | ln | Terrain Type | Level |  |  |
| Segment Length, L | 1,500 | ft | Percent Grade | - |  |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |  |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 1.67 | $\mathrm{ramps} / \mathrm{mi}$ |  |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 70.5 | mph |  |


| General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


|  | General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :--- | :--- | :--- |
| Volume, V | 4,764 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{Hv}}$ | 0.917 |  |  |
| Peak Hour Factor, PHF | 0.99 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,749 | pcphpl |  |
| Total Trucks | $9.0 \%$ |  | Capacity, c | 2,400 | pcphpl |  |
| Single Unit/Tractor-Trailer Mix | - | Adjusted Capacity, $\mathrm{c}_{\mathrm{adj}}$ | 2,400 | pcphpl |  |  |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 | Volume-to-Capacity Ratio, v/c | 0.73 |  |  |  |


| General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 70.5 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 66.7 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 26.2 | pcpmpl |
| Total Ramp Density Adjustment | 4.9 | mph | Level of Service, LOS | D |  |

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| Freeway Merge Report |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Project I-80/Richards B <br> Freeway Eastbound I-80 <br> Segment Richards Blvd O <br> Alternative Design Year <br> Time Period PM Peak Hour |  |  |  |  |
| Geometric Data |  |  |  |  |
|  | Freeway | On Ramp |  |  |
| Number of Lanes, N | 3 | 1 |  |  |
| Free-Flow Speed, FFS | 70.5 | 45 |  | mph |
| Segment Length, L / Acceleration Length, LA | 1,500 | 500 |  | ft |
| Terrain Type | Level | Level |  |  |
| Percent Grade | - | - |  |  |
| Grade Length | - | - |  | ft |
| Segment Type / Ramp Type | Freeway | Right |  |  |
| Adjustment Factors |  |  |  |  |
|  | Freeway | On Ramp |  |  |
| Driver Population | Familiar | Familiar |  |  |
| Weather Type | Non-severe | Non-severe |  |  |
| Incident Type | No incident | No incident |  |  |
| Capacity Adjustment Factor, CAF | 1.00 | 1.00 |  |  |
| Demand Adjustment Factor, DAF | 1.00 | 1.00 |  |  |
| Volume Data |  |  |  |  |
| Junction Components | Freeway | On Ramp |  |  |
| Volume, V | 4,764 | 470 |  | vph |
| Peak Hour Factor, PHF | 0.99 | 0.92 |  |  |
| Total Trucks | 9.0\% | 3.0\% |  |  |
| Single Unit/Tractor-Trailer Mix | - | - |  |  |
| Passenger Car Equivalent, $\mathrm{E}_{T}$ | 2.0 | 2.0 |  |  |
| Heavy Vehicle Adjustment, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 | 0.971 |  |  |
| Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 5,246 | 526 |  | pcph |
| Adjacent Ramp Data |  |  |  |  |
|  |  | Upstream | Downstream |  |
| Adjacent Ramp Meeting Criteria |  | Yes | No |  |
| Type of Adjacent Ramp |  | Off |  |  |
| Distance to Adjacent Ramp |  | 1,780 |  | ft |
| Volume on Adjacent Ramp |  | 996 |  | pcph |

## Freeway Merge Report



|  | Freeway Basic Report |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Eastbound I-80 |
| Segment | Richards Blvd to Chiles Rd |
| Alternative | Design Year |
| Time Period | PM Peak Hour |


|  | General |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
|  | Purpose Lanes - Geometric Data |  |  |  |  |  |
| General Purpose Lanes, N | 3 | ln | Terrain Type | Level |  |  |
| Segment Length, L | 5,710 | ft | Percent Grade | - |  |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |  |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 1.50 | $\mathrm{ramps} / \mathrm{mi}$ |  |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 70.9 | mph |  |


| General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


| General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Volume, V | 5,169 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.99 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,897 | pcphpl |
| Total Trucks | 9.0\% |  | Capacity, c | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - |  | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |
| Passenger Car Equivalent, $\mathrm{E}_{T}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.79 |  |


| General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 70.9 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 64.7 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 29.3 | pcpmpl |
| Total Ramp Density Adjustment | 4.5 | mph | Level of Service, LOS | D |  |

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## Freeway Diverge Report

| Freeway Diverge Report |  |  |  |
| :---: | :---: | :---: | :---: |
| Project I-80/Richards B <br> Freeway Eastbound I-80 <br> Segment Chiles Rd Off Ra <br> Alternative Design Year <br> Time Period PM Peak Hour |  |  |  |
| Geometric Data |  |  |  |
|  | Freeway | Off Ramp |  |
| Number of Lanes, N | 3 | 2 |  |
| Free-Flow Speed, FFS | 70.9 | 25 | mph |
| Segment Length, L / Deceleration Length, LD | 1,500 | 1,500 | ft |
| Terrain Type | Level | Level |  |
| Percent Grade | - | - |  |
| Grade Length | - |  | ft |
| Segment Type / Ramp Type | Freeway | Right |  |
| Adjustment Factors |  |  |  |
|  | Freeway | Off Ramp |  |
| Driver Population | Familiar | Familiar |  |
| Weather Type | Non-severe | Non-severe |  |
| Incident Type | No incident | No incident |  |
| Capacity Adjustment Factor, CAF | 1.00 | 1.00 |  |
| Demand Adjustment Factor, DAF | 1.00 | 1.00 |  |
| Volume Data |  |  |  |
| Junction Components | Freeway | Off Ramp |  |
| Volume, V | 5,169 | 560 | vph |
| Peak Hour Factor, PHF | 0.99 | 0.92 |  |
| Total Trucks | 9.0\% | 3.0\% |  |
| Single Unit/Tractor-Trailer Mix | - | - |  |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 | 2.0 |  |
| Heavy Vehicle Adjustment, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 | 0.971 |  |
| Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 5,691 | 627 | pcph |

## Adjacent Ramp Data

Adjacent Ramp Meeting Criteria
Upstream Downstream

Type of Adjacent Ramp
Distance to Adjacent Ramp
Volume on Adjacent Ramp
pcph

## Freeway Diverge Report



|  | Freeway Basic Report |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Eastbound I-80 |
| Segment | Chiles Rd Off to Mace Rd On |
| Alternative | Design Year |
| Time Period | PM Peak Hour |


|  | General |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
|  | Purpose Lanes - Geometric Data |  |  |  |  |  |
| General Purpose Lanes, N | 3 | ln | Terrain Type | Level |  |  |
| Segment Length, L | 1,000 | ft | Percent Grade | - |  |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |  |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 1.50 | $\mathrm{ramps} / \mathrm{mi}$ |  |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 70.9 | mph |  |


| General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


| General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Volume, V | 4,687 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.99 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,720 | pcphpl |
| Total Trucks | 9.0\% |  | Capacity, c | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - |  | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.72 |  |


| General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 70.9 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 67.3 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 25.5 | pcpmpl |
| Total Ramp Density Adjustment | 4.5 | mph | Level of Service, LOS | C |  |


|  | Freeway Basic Report |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Westbound I-80 |
| Segment | East of Mace Blvd |
| Alternative | Design Year No Build |
| Time Period | AM Peak Hour |


|  | General |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
|  | Purpose Lanes - Geometric Data |  |  |  |  |  |
| General Purpose Lanes, N | 3 | ln | Terrain Type | Level |  |  |
| Segment Length, L | 2,590 | ft | Percent Grade | - |  |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |  |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 1.50 | $\mathrm{ramps} / \mathrm{mi}$ |  |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 70.9 | mph |  |


| General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


| General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Volume, V | 4,928 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.98 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,827 | pcphpl |
| Total Trucks | 9.0\% |  | Capacity, c | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - |  | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.76 |  |


| General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS ${ }_{\text {adj }}$ | 70.9 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 65.8 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 27.8 | pcpmpl |
| Total Ramp Density Adjustment | 4.5 | mph | Level of Service, LOS | D |  |

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| Entering General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :--- | :---: | :--- | :--- | :--- | :--- |
| Volume, V | 4,928 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.98 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,827 | pcphpl |
| Total Trucks | $9.0 \%$ |  | Capacity, c | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |  |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.76 |  |


| Entering General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 71.3 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 66.0 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 27.7 | pcpmpl |
| Total Ramp Density Adjustment | 4.1 | mph | Level of Service, LOS | D |  |

## Segment General Purpose Lanes - Capacity, Speed, and Density

| Segment General |  |  |  |  |  |  | Purpose Lanes - Capacity, Speed, and Density |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| General Purpose Lanes, N | 4 | In | Average Speed, S | 69.7 | mph |  |  |
| Adjusted Capacity, cadj | 2,400 | pcphpl | Density, D | 21.9 | pcphpl |  |  |
| Flow Rate, vp | 1,524 | pcphpl | Level of Service, LOS | C |  |  |  |
| Volume-to-Capacity Ratio, v/c | 0.64 |  |  |  |  |  |  |

## Freeway Merge Report

| Freeway Merge Report |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Project I-80/Richards B <br> Freeway Westbound I-8 <br> Segment Mace Blvd to L <br> Alternative Design Year No <br> Time Period AM Peak Hour |  |  |  |  |
| Geometric Data |  |  |  |  |
|  | Freeway | On Ramp |  |  |
| Number of Lanes, N | 3 | 2 |  |  |
| Free-Flow Speed, FFS | 71.3 | 45 |  | mph |
| Segment Length, L / Acceleration Length, LA | 1,850 | 0 |  | ft |
| Terrain Type | Level | Level |  |  |
| Percent Grade | - | - |  |  |
| Grade Length | - | - |  | ft |
| Segment Type / Ramp Type | Freeway | Right |  |  |
| Adjustment Factors |  |  |  |  |
|  | Freeway | On Ramp |  |  |
| Driver Population | Familiar | Familiar |  |  |
| Weather Type | Non-severe | Non-severe |  |  |
| Incident Type | No incident | No incident |  |  |
| Capacity Adjustment Factor, CAF | 1.00 | 1.00 |  |  |
| Demand Adjustment Factor, DAF | 1.00 | 1.00 |  |  |
| Volume Data |  |  |  |  |
| Junction Components | Freeway | On Ramp |  |  |
| Volume, V | 4,928 | 550 |  | vph |
| Peak Hour Factor, PHF | 0.98 | 0.92 |  |  |
| Total Trucks | 9.0\% | 3.0\% |  |  |
| Single Unit/Tractor-Trailer Mix | - | - |  |  |
| Passenger Car Equivalent, $\mathrm{E}_{T}$ | 2.0 | 2.0 |  |  |
| Heavy Vehicle Adjustment, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 | 0.971 |  |  |
| Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 5,481 | 616 |  | pcph |
| Adjacent Ramp Data |  |  |  |  |
|  |  | Upstream | Downstream |  |
| Adjacent Ramp Meeting Criteria |  | No | No |  |
| Type of Adjacent Ramp |  |  |  |  |
| Distance to Adjacent Ramp |  |  |  | ft |
| Volume on Adjacent Ramp |  |  |  | pcph |

## Freeway Merge Report



| Ramp Influence Area Density and Level of Service |  |  |  |
| :--- | :--- | :---: | :---: |
| Density in Ramp Influence Area, $D_{R}$ | pcpmpl |  |  |
| Level of Service, LOS |  |  |  |

## Segment Speed, Flow, and Density

Speed Adjustment Factor, SAF
Speed Index, $\mathrm{M}_{\mathrm{S}}$ or $\mathrm{D}_{\mathrm{S}}$
Average Speed in Ramp Influence Area, $\mathrm{S}_{\mathrm{R}} \mathrm{mph}$

Average Flow in Outer Lanes, $\mathrm{v}_{\mathrm{OA}}$
pcphpl
mph
Average Speed in Outer Lanes, $\mathrm{S}_{0}$
mph
Density across All Lanes, D
pcpmpl

|  | Freeway Basic Report |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Westbound I-80 |
| Segment | Lane Drop to Olive Dr |
| Alternative | Design Year No Build |
| Time Period | AM Peak Hour |


|  | General |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
|  | Purpose Lanes - Geometric Data |  |  |  |  |  |
| General Purpose Lanes, N | 3 | ln | Terrain Type | Level |  |  |
| Segment Length, L | 4,780 | ft | Percent Grade | - |  |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |  |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 1.33 | $\mathrm{ramps} / \mathrm{mi}$ |  |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 71.3 | mph |  |


| General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


|  | General Purpose Lanes - Demand and Capacity |  |  |  |  |
| :--- | :---: | :--- | :--- | :--- | :--- |
| Volume, V | 5,401 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.98 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 2,002 | pcphpl |
| Total Trucks | $9.0 \%$ |  | Capacity, c | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |  |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.83 |  |


| General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 71.3 | mph |
| Lane Width Adjustment, f LW | 0.0 | mph | Average Speed, S | 62.9 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 31.8 | pcpmpl |
| Total Ramp Density Adjustment | 4.1 | mph | Level of Service, LOS | D |  |

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## Freeway Diverge Report

|  | Freeway Diverg |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Westbound I-80 |
| Segment | Olive Dr Off |
| Alternative | Design Year No Build |
| Time Period | AM Peak Hour |


|  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: |
|  | Geometric Data |  |  |  |
|  |  |  |  |  |
| Number of Lanes, N | Freeway | Off Ramp |  |  |
| Free-Flow Speed, FFS | 3 | 1 |  |  |
| Segment Length, L / Deceleration Length, LD | 71.3 | 35 | mph |  |
| Terrain Type | 1,500 | 150 | ft |  |
| Percent Grade | Level | Level |  |  |
| Grade Length | - | - | - | ft |
| Segment Type / Ramp Type | - | Right |  |  |

## Adjustment Factors

|  | $\frac{\text { Freeway }}{}$ | $\frac{\text { Off Ramp }}{}$ |
| :--- | :---: | :---: |
| Driver Population | Familiar | Familiar |
| Weather Type | Non-severe | Non-severe |
| Incident Type | No incident | No incident |
| Capacity Adjustment Factor, CAF | 1.00 | 1.00 |
| Demand Adjustment Factor, DAF | 1.00 | 1.00 |


|  | Volume Data |  |  |  |
| :--- | :---: | :---: | :---: | :---: |
|  |  |  |  |  |
| Junction Components | $\underline{\text { Freeway }}$ | $\underline{\text { Off Ramp }}$ |  |  |
| Volume, V | 5,401 | 280 | vph |  |
| Peak Hour Factor, PHF | 0.98 | 0.92 |  |  |
| Total Trucks | $9.0 \%$ | $3.0 \%$ |  |  |
| Single Unit/Tractor-Trailer Mix | - | - |  |  |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 | 2.0 |  |  |
| Heavy Vehicle Adjustment, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 | 0.971 |  |  |
| Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 6,007 | 313 | pcph |  |

Adjacent Ramp Meeting Criteria

| Upstream | Downstream |
| :---: | :---: |
| No | Yes |
|  | Off |
|  | 2,390 |
|  | 672 |

## Freeway Diverge Report



|  | Freeway Basic Report |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Westbound I-80 |
| Segment | Olive Dr to Richards Blvd |
| Alternative | Design Year No Build |
| Time Period | AM Peak Hour |


|  | General |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
|  | Purpose Lanes - Geometric Data |  |  |  |  |  |
| General Purpose Lanes, N | 3 | ln | Terrain Type | Level |  |  |
| Segment Length, L | 890 | ft | Percent Grade | - |  |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |  |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 1.83 | $\mathrm{ramps} / \mathrm{mi}$ |  |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 70.0 | mph |  |


| General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


|  | General Purpose Lanes - Demand and Capacity |  |  |  |  |
| :--- | :---: | :--- | :--- | :--- | :--- |
| Volume, V | 5,160 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.98 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,913 | pcphpl |
| Total Trucks | $9.0 \%$ |  | Capacity, c | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |  |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.80 |  |


| General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 70.0 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 64.1 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 29.8 | pcpmpl |
| Total Ramp Density Adjustment | 5.4 | mph | Level of Service, LOS | D |  |

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## Freeway Diverge Report



## Adjacent Ramp Data

Adjacent Ramp Meeting Criteria

| Upstream | Downstream |
| :---: | :---: |
| Yes | No |
| Off |  |
| 2,390 |  |
| 313 |  |

## Freeway Diverge Report



|  | Freeway Basic Report |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Westbound I-80 |
| Segment | Richards Blvd NB Off to On |
| Alternative | Design Year No Build |
| Time Period | AM Peak Hour |


|  | General |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
|  | Purpose Lanes - Geometric Data |  |  |  |  |  |
| General Purpose Lanes, N | 3 | ln | Terrain Type | Level |  |  |
| Segment Length, L | 430 | ft | Percent Grade | - |  |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |  |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 1.83 | $\mathrm{ramps} / \mathrm{mi}$ |  |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 70.0 | mph |  |


| General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


|  | General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :--- | :--- | :--- |
| Volume, V | 4,644 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{Hv}}$ | 0.917 |  |  |
| Peak Hour Factor, PHF | 0.98 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,722 | pcphpl |  |
| Total Trucks | $9.0 \%$ |  | Capacity, c | 2,400 | pcphpl |  |
| Single Unit/Tractor-Trailer Mix | - | Adjusted Capacity, $\mathrm{c}_{\mathrm{adj}}$ | 2,400 | pcphpl |  |  |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 | Volume-to-Capacity Ratio, v/c | 0.72 |  |  |  |


| General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 70.0 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 66.9 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 25.7 | pcpmpl |
| Total Ramp Density Adjustment | 5.4 | mph | Level of Service, LOS | C |  |

$\qquad$

## Leisch Method for Weaving Analysis

## Data Input

Number of Entering Mainline Lanes
Number of Lanes in Weaving Section Length of Weaving Section (feet)

| $N_{b}$ | 3 |
| :---: | :---: |
| $N$ | 4 |
|  | 500 |

Volume (vph)*
Truck Percentage
PCE for Trucks
Volume (pcph)

| 510 |
| :---: |
| $3.0 \%$ |
| 2.0 |
| 525 |

Volume (vph)
Truck Percentage
PCE for Trucks
Volume (pcph)


The LOS in the chart above refers to the capacity of weaving traffic only; through and ramp to ramp traffic is not included.

* Note: Do not adjust by a Peak Hour Factor (PHF). The methodology incorporates the PHF in the Service Volume tables.

Sources: Completion of Procedures for Analysis and Design of Traffic Weaving Sections, Jack E. Leisch \& Associates, September 1983 and
Highway Design Manual , California Department of Transportation, 2014

| Project I-80/Richards B <br> Freeway Westbound I-80 <br> Segment Richards Blvd NB <br> Alternative Design Year No <br> Time Period AM Peak Hour |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Geometric Data |  |  |  |  |
|  | Freeway | On Ramp | Off Ramp |  |
| Number of Lanes, N | 3 | 1 | 1 |  |
| Free-Flow Speed, FFS | 70.0 | 25 | 25 | mph |
| Segment Length, L / Deceleration Length, LD | 1,500 | 0 | 0 | ft |
| Terrain Type | Level | Level | Level |  |
| Percent Grade | - | - | - |  |
| Grade Length | - | - | - | ft |
| Segment Type / Ramp Type | Freeway | Right | Right |  |
| Adjustment Factors |  |  |  |  |
|  | Freeway | On Ramp | Off Ramp |  |
| Driver Population | Familiar | Familiar | Familiar |  |
| Weather Type | Non-severe | Non-severe | Non-severe |  |
| Incident Type | No incident | No incident | No incident |  |
| Capacity Adjustment Factor, CAF | 1.00 | 1.00 | 1.00 |  |
| Demand Adjustment Factor, DAF | 1.00 | 1.00 | 1.00 |  |
| Volume Data |  |  |  |  |
| Junction Components | Freeway | On Ramp | Off Ramp |  |
| Volume, V | 4,644 | 510 | 290 | vph |
| Peak Hour Factor, PHF | 0.98 | 0.92 | 0.92 |  |
| Total Trucks | 9.0\% | 3.0\% | 3.0\% |  |
| Single Unit/Tractor-Trailer Mix | - | - | - |  |
| Passenger Car Equivalent, $\mathrm{E}_{T}$ | 2.0 | 2.0 | 2.0 |  |
| Heavy Vehicle Adjustment, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 | 0.971 | 0.971 |  |
| Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 5,165 | 571 | 325 | pcph |
| Adjacent Ramp Data |  |  |  |  |
|  |  | Upstream | Downstream |  |
| Adjacent Ramp Meeting Criteria |  |  |  |  |
| Type of Adjacent Ramp |  |  |  |  |
| Distance to Adjacent Ramp |  |  |  | ft |
| Volume on Adjacent Ramp |  |  |  | pcph |


|  |  |
| :--- | :--- |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Westbound I-80 |
| Segment | Richards Blvd NB On to SB Off |
| Alternative | Design Year No Build |
| Time Period | AM Peak Hour |


|  |  |  |  |
| :--- | :--- | :--- | :--- |


| Ramp Influence Area Density and Level of Service |  |  |  |
| :--- | :--- | :---: | :---: |
| Density in Ramp Influence Area, $D_{R}$ | pcpmpl |  |  |
| Level of Service, LOS |  |  |  |

## Segment Speed, Flow, and Density

Speed Adjustment Factor, SAF
Speed Index, $\mathrm{M}_{\mathrm{S}}$ or $\mathrm{D}_{\mathrm{S}}$
Average Speed in Ramp Influence Area, $\mathrm{S}_{\mathrm{R}} \mathrm{mph}$

Average Flow in Outer Lanes, $\mathrm{v}_{\mathrm{OA}}$
pcphpl
mph
Average Speed in Outer Lanes, $\mathrm{S}_{0}$
Average Speed for Segment, S
mph
Density across All Lanes, D
pcpmpl

## Freeway Weave Report

|  | Freeway Weave Report |  |  |
| :--- | :--- | :--- | :---: |
|  |  |  |  |
| Project | I-80/Richards Blvd Interchange |  |  |
| Freeway | Westbound I-80 |  |  |
| Segment | Richards Blvd NB On to SB Off |  |  |
| Alternative | Design Year No Build |  |  |
| Time period | AM Peak Hour |  |  |
|  |  |  |  |
|  |  |  |  |

## Adjustment Factors

| Driver Population | Familiar |
| :--- | :---: |
| Weather Type | Non-severe |
| Incident Type | No incident |
| Capacity Adjustment Factor, CAF | 1.00 |
| Demand Adjustment Factor, DAF | 1.00 |


| Volume Data |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Frwy to Frwy | On to Frwy | Frwy to Off | Frwy to Off | vph |
| Volume, V | 4,354 | 510 | 290 | 0 |  |
| Peak-hour factor, PHF | 0.98 | 0.92 | 0.92 | 0.95 |  |
| Total Trucks | 9.0\% | 3.0\% | 3.0\% | 3.0\% |  |
| Terrain Type | Level | Level | Level | Level |  |
| Grade |  |  |  |  |  |
| Length |  |  |  |  | mi |
| SUT/TT Mix |  |  |  |  |  |
| Passenger Car Equivalent, $\mathrm{E}_{T}$ | 2.0 | 2.0 | 2.0 | 2.0 |  |
| Heavy Vehicle Adjustment, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 | 0.971 | 0.971 | 0.971 |  |
| Demand Adjustment Factor, DAF | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 4,843 | 571 | 325 | 0 | pcph |
| Weaving Flow Rate, vW | 896 | Total Flow Ra |  |  | 5,738 |
| Non-Weaving Flow Rate, vNW | 4,843 | Volume Ratio |  |  | 0.156 |

## Freeway Weave Report

| Project | I-80/Richards Blvd Interchange |
| :--- | :--- |
| Freeway | Westbound I-80 |
| Segment | Richards Blvd NB On to SB Off |
| Alternative | Design Year No Build |
| Time period | AM Peak Hour |


|  | Capacity |  |  |
| :--- | :---: | :---: | :---: |
|  |  |  |  |
| Maximum Weaving Length, $\mathrm{L}_{\mathrm{MAX}}$ | 4,092 | ft |  |
| Weaving Length Check | OK |  |  |
| Freeway Maximum Capacity, $\mathrm{c}_{\mathrm{IFL}}$ | 2,400 | pchpl |  |
| Density-Based Capacity, $\mathrm{c}_{\mathrm{IWL}}$ | 9,325 | pchpl |  |
| Demand Flow-Based Capacity, $\mathrm{c}_{\mathrm{IW}}$ | 14,235 | pch |  |
| Weaving Segment Capacity, $\mathrm{c}_{\mathrm{w}}$ | 14,235 | vph |  |
| Adjusted Weaving Area Capacity, $\mathrm{c}_{\mathrm{wa}}$ | 14,235 | vph |  |
| Volume-to-Capacity Ratio, $\mathrm{v} / \mathrm{c}$ | 0.37 |  |  |


| Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |
| Minimum Lane Change Rate, $\mathrm{LC}_{\mathrm{MIN}}$ | 896 | $\mathrm{Ic} / \mathrm{h}$ |  |  |  |
| Weaving Lane Change Rate, $\mathrm{LC}_{\mathrm{W}}$ | 915 | $\mathrm{Ic} / \mathrm{h}$ |  |  |  |
| Non-weaving Vehicle Index, $\mathrm{I}_{\mathrm{NW}}$ | 202 |  |  |  |  |
| Non-weaving Lane Change Rate, $\mathrm{LC}_{\mathrm{NW}}$ | 498 | $\mathrm{Ic} / \mathrm{h}$ |  |  |  |
| Total Lane Change Rate, $\mathrm{LC}_{\mathrm{ALL}}$ | 1,413 | $\mathrm{Ic} / \mathrm{h}$ |  |  |  |
| Weaving Intensity Factor, W | 0.513 |  |  |  |  |
| Average Weaving Speed, $\mathrm{S}_{\mathrm{W}}$ | 51.4 | mph |  |  |  |
| Average Non-Weaving Speed, $\mathrm{S}_{\mathrm{NW}}$ | 56.7 | mph |  |  |  |
| Average Speed, S | 55.8 | mph |  |  |  |
| Density, D | 25.7 | pcpmpl |  |  |  |
| Level of Service, LOS | C |  |  |  |  |

## Capacity Checks

|  | Flow | Capacity |  | V/C Ratio |
| :---: | :---: | :---: | :---: | :---: |
| Entering General Purpose Lanes | 5,165 | 7,200 | pcph | 0.72 |
| Exiting General Purpose Lanes | 5,412 | 7,200 | pcph | 0.75 |
| On Ramp | 571 | 1,900 | pcph | 0.30 |
| Off Ramp | 325 | 1,900 | pcph | 0.17 |


|  | Freeway Basic Report |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Westbound I-80 |
| Segment | Richards Blvd SB Off to On |
| Alternative | Design Year No Build |
| Time Period | AM Peak Hour |


|  | General |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
|  | Purpose Lanes - Geometric Data |  |  |  |  |  |
| General Purpose Lanes, N | 3 | ln | Terrain Type | Level |  |  |
| Segment Length, L | 210 | ft | Percent Grade | - |  |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |  |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 1.83 | $\mathrm{ramps} / \mathrm{mi}$ |  |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 70.0 | mph |  |


| General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


|  | General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :--- | :--- | :--- |
| Volume, V | 4,833 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{Hv}}$ | 0.917 |  |  |
| Peak Hour Factor, PHF | 0.98 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,792 | pcphpl |  |
| Total Trucks | $9.0 \%$ |  | Capacity, c | 2,400 | pcphpl |  |
| Single Unit/Tractor-Trailer Mix | - | Adjusted Capacity, $\mathrm{c}_{\mathrm{adj}}$ | 2,400 | pcphpl |  |  |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 | Volume-to-Capacity Ratio, v/c | 0.75 |  |  |  |


| General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 70.0 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 66.0 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 27.2 | pcpmpl |
| Total Ramp Density Adjustment | 5.4 | mph | Level of Service, LOS | D |  |

$\qquad$

| Freeway Merge Report |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Project I-80/Richards B <br> Freeway Westbound I-80 <br> Segment Richards Blvd SB <br> Alternative Design Year No <br> Time Period AM Peak Hour |  |  |  |  |
| Geometric Data |  |  |  |  |
|  | Freeway | On Ramp |  |  |
| Number of Lanes, N | 3 | 1 |  |  |
| Free-Flow Speed, FFS | 70.4 | 45 |  | mph |
| Segment Length, L / Acceleration Length, LA | 1,500 | 400 |  | ft |
| Terrain Type | Level | Level |  |  |
| Percent Grade | - | - |  |  |
| Grade Length | - | - |  | ft |
| Segment Type / Ramp Type | Freeway | Right |  |  |
| Adjustment Factors |  |  |  |  |
|  | Freeway | On Ramp |  |  |
| Driver Population | Familiar | Familiar |  |  |
| Weather Type | Non-severe | Non-severe |  |  |
| Incident Type | No incident | No incident |  |  |
| Capacity Adjustment Factor, CAF | 1.00 | 1.00 |  |  |
| Demand Adjustment Factor, DAF | 1.00 | 1.00 |  |  |
| Volume Data |  |  |  |  |
| Junction Components | Freeway | On Ramp |  |  |
| Volume, V | 4,833 | 130 |  | vph |
| Peak Hour Factor, PHF | 0.98 | 0.92 |  |  |
| Total Trucks | 9.0\% | 3.0\% |  |  |
| Single Unit/Tractor-Trailer Mix | - | - |  |  |
| Passenger Car Equivalent, $\mathrm{E}_{T}$ | 2.0 | 2.0 |  |  |
| Heavy Vehicle Adjustment, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 | 0.971 |  |  |
| Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 5,376 | 146 |  | pcph |
| Adjacent Ramp Data |  |  |  |  |
|  |  | Upstream | Downstream |  |
|  |  | No | No |  |
| Type of Adjacent Ramp |  |  |  |  |
| Distance to Adjacent Ramp |  |  |  | ft |
| Volume on Adjacent Ramp |  |  |  | pcph |

## Freeway Merge Report



|  | Freeway Basic Report |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Westbound I-80 |
| Segment | Richards Blvd to Lane Add |
| Alternative | Design Year No Build |
| Time Period | AM Peak Hour |


|  | General |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
|  | Purpose Lanes - Geometric Data |  |  |  |  |  |
| General Purpose Lanes, N | 3 | ln | Terrain Type | Level |  |  |
| Segment Length, L | 2,270 | ft | Percent Grade | - |  |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |  |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 1.67 | $\mathrm{ramps} / \mathrm{mi}$ |  |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 70.4 | mph |  |


| General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


|  | General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :--- | :--- | :--- |
| Volume, V | 4,945 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{Hv}}$ | 0.917 |  |  |
| Peak Hour Factor, PHF | 0.98 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,833 | pcphpl |  |
| Total Trucks | $9.0 \%$ |  | Capacity, c | 2,400 | pcphpl |  |
| Single Unit/Tractor-Trailer Mix | - | Adjusted Capacity, $\mathrm{c}_{\mathrm{adj}}$ | 2,400 | pcphpl |  |  |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 | Volume-to-Capacity Ratio, v/c | 0.76 |  |  |  |


| General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 70.4 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 65.6 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 28.0 | pcpmpl |
| Total Ramp Density Adjustment | 5.0 | mph | Level of Service, LOS | D |  |

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## Freeway Diverge Report

|  | Freeway Diverg |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Westbound I-80 |
| Segment | Lane Add to Old Davis Off |
| Alternative | Design Year No Build |
| Time Period | AM Peak Hour |


|  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: |
|  | Geometric Data |  |  |  |
|  |  |  |  |  |
|  | Freeway | Off Ramp |  |  |
| Number of Lanes, N | 3 | 1 |  |  |
| Free-Flow Speed, FFS | 70.0 | 45 | mph |  |
| Segment Length, L / Deceleration Length, LD | 1,190 | 150 | ft |  |
| Terrain Type | Level | Level |  |  |
| Percent Grade | - | - | - | ft |
| Grade Length | - | Right |  |  |
| Segment Type / Ramp Type | Freeway |  |  |  |

## Adjustment Factors

|  | $\frac{\text { Freeway }}{}$ | $\frac{\text { Off Ramp }}{}$ |
| :--- | :---: | :---: |
| Driver Population | Familiar | Familiar |
| Weather Type | Non-severe | Non-severe |
| Incident Type | No incident | No incident |
| Capacity Adjustment Factor, CAF | 1.00 | 1.00 |
| Demand Adjustment Factor, DAF | 1.00 | 1.00 |


|  | Volume Data |  |  |  |
| :--- | :---: | :---: | :---: | :---: |
|  |  |  |  |  |
| Junction Components | $\underline{\text { Freeway }}$ | $\underline{\text { Off Ramp }}$ |  |  |
| Volume, V | 4,945 | 500 | vph |  |
| Peak Hour Factor, PHF | 0.98 | 0.92 |  |  |
| Total Trucks | $9.0 \%$ | $3.0 \%$ |  |  |
| Single Unit/Tractor-Trailer Mix | - | - |  |  |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 | 2.0 |  |  |
| Heavy Vehicle Adjustment, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 | 0.971 |  |  |
| Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 5,500 | 560 | pcph |  |

Adjacent Ramp Meeting Criteria
Upstream Downstream

Type of Adjacent Ramp
Distance to Adjacent Ramp
ft
pcph

## Freeway Diverge Report



|  | Freeway Basic Report |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Westbound I-80 |
| Segment | West of Old Davis Rd |
| Alternative | Design Year No Build |
| Time Period | AM Peak Hour |


|  | General |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
|  | Purpose Lanes - Geometric Data |  |  |  |  |  |
| General Purpose Lanes, N | 4 | ln | Terrain Type | Level |  |  |
| Segment Length, L | 1,350 | ft | Percent Grade | - |  |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |  |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 1.83 | $\mathrm{ramps} / \mathrm{mi}$ |  |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 70.0 | mph |  |


| General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


| General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Volume, V | 4,515 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.98 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,255 | pcphpl |
| Total Trucks | 9.0\% |  | Capacity, c | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - |  | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.52 |  |


| General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 70.0 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 70.0 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 17.9 | pcpmpl |
| Total Ramp Density Adjustment | 5.4 | mph | Level of Service, LOS | B |  |

$\qquad$

|  | Freeway Basic Report |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Westbound I-80 |
| Segment | East of Mace Blvd |
| Alternative | Design Year No Build |
| Time Period | PM Peak Hour |


|  | General |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
|  | Purpose Lanes - Geometric Data |  |  |  |  |  |
| General Purpose Lanes, N | 3 | ln | Terrain Type | Level |  |  |
| Segment Length, L | 2,590 | ft | Percent Grade | - |  |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |  |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 1.50 | $\mathrm{ramps} / \mathrm{mi}$ |  |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 70.9 | mph |  |


| General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


| General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Volume, V | 4,352 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.99 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,597 | pcphpl |
| Total Trucks | 9.0\% |  | Capacity, c | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - |  | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |
| Passenger Car Equivalent, $\mathrm{E}_{T}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.67 |  |


| General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 70.9 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 68.7 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 23.2 | pcpmpl |
| Total Ramp Density Adjustment | 4.5 | mph | Level of Service, LOS | C |  |


|  | Freeway Basic Report |
| :--- | :--- |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Westbound I-80 |
| Segment | Mace Blvd On Ramp |
| Alternative | Design Year No Build |
| Time Period | PM Peak Hour |


|  |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
|  | Entering General Purpose Lanes - Geometric Data |  |  |  |  |
| General Purpose Lanes, N | 3 | ln | Terrain Type | Level |  |
| Segment Length, L | 1,850 | ft | Percent Grade | - |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 1.33 | $\mathrm{ramps} / \mathrm{mi}$ |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 71.3 | mph |


| Entering General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


| Entering General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :--- | :---: | :--- | :--- | :--- | :--- |
| Volume, V | 4,352 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.99 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,597 | pcphpl |
| Total Trucks | $9.0 \%$ |  | Capacity, c | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - | Adjusted Capacity, $\mathrm{c}_{\mathrm{adj}}$ | 2,400 | pcphpl |  |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.67 |  |


| Entering General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 71.3 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 69.0 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 23.1 | pcpmpl |
| Total Ramp Density Adjustment | 4.1 | mph | Level of Service, LOS | C |  |


| Segment General Purpose Lanes - Capacity, Speed, and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| General Purpose Lanes, N | 4 | ln | Average Speed, S | 70.2 | mph |
| Adjusted Capacity, cadj | 2,400 | pcphpl | Density, D | 20.8 | pcphpl |
| Flow Rate, vp | 1,458 | pcphpl | Level of Service, LOS | C |  |
| Volume-to-Capacity Ratio, v/c | 0.61 |  |  |  |  |

## Freeway Merge Report



## Freeway Merge Report



| Ramp Influence Area Density and Level of Service |  |  |  |
| :--- | :--- | :---: | :---: |
| Density in Ramp Influence Area, $D_{R}$ | pcpmpl |  |  |
| Level of Service, LOS |  |  |  |

## Segment Speed, Flow, and Density

Speed Adjustment Factor, SAF
Speed Index, $\mathrm{M}_{\mathrm{S}}$ or $\mathrm{D}_{\mathrm{S}}$
Average Speed in Ramp Influence Area, $\mathrm{S}_{\mathrm{R}} \mathrm{mph}$

Average Flow in Outer Lanes, $\mathrm{v}_{\mathrm{OA}}$
pcphpl
mph
Average Speed in Outer Lanes, $\mathrm{S}_{0}$
mph
Density across All Lanes, D
pcpmpl

|  | Freeway Basic Report |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Westbound I-80 |
| Segment | Lane Drop to Olive Dr |
| Alternative | Design Year No Build |
| Time Period | PM Peak Hour |


|  | General |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
|  | Purpose Lanes - Geometric Data |  |  |  |  |  |
| General Purpose Lanes, N | 3 | ln | Terrain Type | Level |  |  |
| Segment Length, L | 4,780 | ft | Percent Grade | - |  |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |  |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 1.33 | $\mathrm{ramps} / \mathrm{mi}$ |  |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 71.3 | mph |  |


| General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


| General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Volume, V | 5,151 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.99 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,891 | pcphpl |
| Total Trucks | 9.0\% |  | Capacity, c | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - |  | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |
| Passenger Car Equivalent, $\mathrm{E}_{T}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.79 |  |


| General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 71.3 | mph |
| Lane Width Adjustment, f LW | 0.0 | mph | Average Speed, S | 65.0 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 29.1 | pcpmpl |
| Total Ramp Density Adjustment | 4.1 | mph | Level of Service, LOS | D |  |

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## Freeway Diverge Report

|  | Freeway Diverg |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Westbound I-80 |
| Segment | Olive Dr Off |
| Alternative | Design Year No Build |
| Time Period | PM Peak Hour |


|  |  |  |  |
| :--- | :---: | :---: | :---: |
|  | Geometric Data |  |  |
|  |  |  |  |
|  | Freeway |  |  |
| Number of Lanes, N | 3 | 1 |  |
| Free-Flow Speed, FFS | 71.3 | 35 | mph |
| Segment Length, L / Deceleration Length, LD | 1,500 | 150 | ft |
| Terrain Type | Level | Level |  |
| Percent Grade | - | - |  |
| Grade Length | - | - | ft |
| Segment Type / Ramp Type | Freeway | Right |  |


| Adjustment Factors |  |  |
| :--- | :---: | :---: |
|  |  | Freeway |
| Familiar | Off Ramp |  |
| Driver Population | Non-severe | Non-severe |
| Weather Type | No incident | No incident |
| Incident Type | 1.00 | 1.00 |
| Capacity Adjustment Factor, CAF | 1.00 | 1.00 |
| Demand Adjustment Factor, DAF |  |  |


|  | Volume Data |  |  |  |
| :--- | :---: | :---: | :---: | :---: |
|  |  |  |  |  |
| Junction Components | $\underline{\text { Freeway }}$ | $\underline{\text { Off Ramp }}$ |  |  |
| Volume, V | 5,151 | 140 | vph |  |
| Peak Hour Factor, PHF | 0.99 | 0.92 |  |  |
| Total Trucks | $9.0 \%$ | $3.0 \%$ |  |  |
| Single Unit/Tractor-Trailer Mix | - | - |  |  |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 | 2.0 |  |  |
| Heavy Vehicle Adjustment, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 | 0.971 |  |  |
| Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 5,672 | 157 | pcph |  |

Upstream Downstream

Type of Adjacent Ramp
Distance to Adjacent Ramp
No Yes

Volume on Adjacent Ramp
2,390
ft
336
pcph

## Freeway Diverge Report



|  | Freeway Basic Report |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Westbound I-80 |
| Segment | Olive Dr to Richards Blvd |
| Alternative | Design Year No Build |
| Time Period | PM Peak Hour |


|  | General |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
|  | Purpose Lanes - Geometric Data |  |  |  |  |  |
| General Purpose Lanes, N | 3 | ln | Terrain Type | Level |  |  |
| Segment Length, L | 890 | ft | Percent Grade | - |  |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |  |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 1.83 | $\mathrm{ramps} / \mathrm{mi}$ |  |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 70.0 | mph |  |


| General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


| General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Volume, V | 5,031 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.99 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,846 | pcphpl |
| Total Trucks | 9.0\% |  | Capacity, c | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - |  | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.77 |  |


| General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 70.0 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 65.2 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 28.3 | pcpmpl |
| Total Ramp Density Adjustment | 5.4 | mph | Level of Service, LOS | D |  |

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## Freeway Diverge Report

| Freeway Diverge Report |  |  |  |
| :---: | :---: | :---: | :---: |
| Project I-80/Richards B <br> Freeway Westbound I-80 <br> Segment Richards Blvd N <br> Alternative Design Year No <br> Time Period PM Peak Hour |  |  |  |
| Geometric Data |  |  |  |
|  | Freeway | Off Ramp |  |
| Number of Lanes, N | 3 | 1 |  |
| Free-Flow Speed, FFS | 70.0 | 45 | mph |
| Segment Length, L / Deceleration Length, LD | 1,500 | 150 | ft |
| Terrain Type | Level | Level |  |
| Percent Grade | - | - |  |
| Grade Length | - | - | ft |
| Segment Type / Ramp Type | Freeway | Right |  |
| Adjustment Factors |  |  |  |
|  | Freeway | Off Ramp |  |
| Driver Population | Familiar | Familiar |  |
| Weather Type | Non-severe | Non-severe |  |
| Incident Type | No incident | No incident |  |
| Capacity Adjustment Factor, CAF | 1.00 | 1.00 |  |
| Demand Adjustment Factor, DAF | 1.00 | 1.00 |  |
| Volume Data |  |  |  |
| Junction Components | Freeway | Off Ramp |  |
| Volume, V | 5,031 | 300 | vph |
| Peak Hour Factor, PHF | 0.99 | 0.92 |  |
| Total Trucks | 9.0\% | 3.0\% |  |
| Single Unit/Tractor-Trailer Mix | - | - |  |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 | 2.0 |  |
| Heavy Vehicle Adjustment, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 | 0.971 |  |
| Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 5,539 | 336 | pcph |

## Adjacent Ramp Data

Adjacent Ramp Meeting Criteria

| Upstream | Downstream |
| :---: | :---: |
| Yes | No |
| Off |  |
| 2,390 |  |
| 157 |  |

## Freeway Diverge Report



|  | Freeway Basic Report |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Westbound I-80 |
| Segment | Richards Blvd NB Off to On |
| Alternative | Design Year No Build |
| Time Period | PM Peak Hour |


|  | General |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
|  | Purpose Lanes - Geometric Data |  |  |  |  |  |
| General Purpose Lanes, N | 3 | ln | Terrain Type | Level |  |  |
| Segment Length, L | 430 | ft | Percent Grade | - |  |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |  |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 1.83 | $\mathrm{ramps} / \mathrm{mi}$ |  |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 70.0 | mph |  |


| General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


| General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Volume, V | 4,773 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.99 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,752 | pcphpl |
| Total Trucks | 9.0\% |  | Capacity, c | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - |  | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.73 |  |


| General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 70.0 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 66.5 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 26.3 | pcpmpl |
| Total Ramp Density Adjustment | 5.4 | mph | Level of Service, LOS | D |  |

$\qquad$

## Leisch Method for Weaving Analysis

## Data Input

Number of Entering Mainline Lanes
Number of Lanes in Weaving Section Length of Weaving Section (feet)

| $N_{b}$ | 3 |
| :---: | :---: |
| $N$ | 4 |
|  | 500 |

Volume (vph)*
Truck Percentage
PCE for Trucks
PCE for Trucks
Volume (pcph)


The LOS in the chart above refers to the capacity of weaving traffic only; through and ramp to ramp traffic is not included.

* Note: Do not adjust by a Peak Hour Factor (PHF). The methodology incorporates the PHF in the Service Volume tables.

Sources: Completion of Procedures for Analysis and Design of Traffic Weaving Sections, Jack E. Leisch \& Associates, September 1983 and
Highway Design Manual , California Department of Transportation, 2014


|  |  |
| :--- | :--- |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Westbound I-80 |
| Segment | Richards Blvd NB On to SB Off |
| Alternative | Design Year No Build |
| Time Period | PM Peak Hour |


|  |  |  |  |
| :--- | :--- | :--- | :--- |


| Ramp Influence Area Density and Level of Service |  |  |  |
| :--- | :--- | :---: | :---: |
| Density in Ramp Influence Area, $D_{R}$ | pcpmpl |  |  |
| Level of Service, LOS |  |  |  |

## Segment Speed, Flow, and Density

Speed Adjustment Factor, SAF
Speed Index, $\mathrm{M}_{\mathrm{S}}$ or $\mathrm{D}_{\mathrm{S}}$
Average Speed in Ramp Influence Area, $\mathrm{S}_{\mathrm{R}} \mathrm{mph}$

Average Flow in Outer Lanes, $\mathrm{v}_{\mathrm{OA}}$
pcphpl
mph
Average Speed in Outer Lanes, $\mathrm{S}_{0}$
Average Speed for Segment, S
mph
Density across All Lanes, D
pcpmpl

## Freeway Weave Report

| Project | I-80/Richards Blvd Interchange |
| :--- | :--- |
| Freeway | Westbound I-80 |
| Segment | Richards Blvd NB On to SB Off |
| Alternative | Design Year No Build |
| Time period | PM Peak Hour |

## Geometric Data

Segment Type
Weaving Configuration
Number of Lanes, N
Weaving Segment Length, $L_{S}$
Interchange Density, ID
Number of Manuever Lanes, $\mathrm{N}_{\mathrm{WL}}$
On Ramp to Freeway Lane Changes, $\mathrm{LC}_{\mathrm{RF}}$
Freeway to Off Ramp Lane Changes, $\mathrm{LC}_{\mathrm{FR}}$
On Ramp to Off Ramp Lane Changes, $\mathrm{LC}_{\text {RR }}$

Freeway
One-sided

| 4 | $\ln$ |
| :---: | :---: |
| 500 | ft |
| 0.8 | $\mathrm{int} / \mathrm{mi}$ |
| 2.0 | ln |

In

1
1
0

## Adjustment Factors

Driver Population
Familiar
Weather Type
Non-severe
Incident Type
Capacity Adjustment Factor, CAF
No incident
1.00

Demand Adjustment Factor, DAF
1.00

Volume Data

Volume, V
Peak-hour factor, PHF
Total Trucks
Terrain Type
Grade
Length
SUT/TT Mix
Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$
Heavy Vehicle Adjustment, $\mathrm{f}_{\mathrm{HV}}$
Demand Adjustment Factor, DAF
Flow Rate, $\mathrm{v}_{\mathrm{p}}$

Weaving Flow Rate, vW
Non-Weaving Flow Rate, vNW

| Frwy to Frwy | On to Frwy | Frwy to Off | Frwy to Off |
| :---: | :---: | :---: | :---: |
| 4,603 | 700 | 170 | 0 |
| 0.99 | 0.92 | 0.92 | 0.95 |
| 9.0\% | 3.0\% | 3.0\% | 3.0\% |
| Level | Level | Level | Level |
| 2.0 | 2.0 | 2.0 | 2.0 |
| 0.917 | 0.971 | 0.971 | 0.971 |
| 1.00 | 1.00 | 1.00 | 1.00 |
| 5,068 | 784 | 190 | 0 |

## Freeway Weave Report

| Project | I-80/Richards Blvd Interchange |
| :--- | :--- |
| Freeway | Westbound I-80 |
| Segment | Richards Blvd NB On to SB Off |
| Alternative | Design Year No Build |
| Time period | PM Peak Hour |


|  | Capacity |  |
| :--- | :---: | :---: |
|  |  |  |
|  |  |  |
| Maximum Weaving Length, $\mathrm{L}_{\mathrm{MAX}}$ | 4,143 | ft |
| Weaving Length Check | OK |  |
| Freeway Maximum Capacity, $\mathrm{c}_{\mathrm{IFL}}$ | 2,400 | pchpl |
| Density-Based Capacity, $\mathrm{c}_{\mathrm{IWL}}$ | 6,921 | pchpl |
| Demand Flow-Based Capacity, $\mathrm{c}_{\mathrm{IW}}$ | 13,787 | pch |
| Weaving Segment Capacity, $\mathrm{c}_{\mathrm{w}}$ | 13,787 | vph |
| Adjusted Weaving Area Capacity, $\mathrm{c}_{\mathrm{wa}}$ | 13,787 | vph |
| Volume-to-Capacity Ratio, $\mathrm{v} / \mathrm{c}$ | 0.41 |  |


| Speed and Density |  |  |
| :---: | :---: | :---: |
| Minimum Lane Change Rate, $\mathrm{LC}_{\text {MIN }}$ | 974 | $\mathrm{lc} / \mathrm{h}$ |
| Weaving Lane Change Rate, $\mathrm{LC}_{\mathrm{w}}$ | 993 | $\mathrm{lc} / \mathrm{h}$ |
| Non-weaving Vehicle Index, $\mathrm{I}_{\text {NW }}$ | 211 |  |
| Non-weaving Lane Change Rate, $\mathrm{LC}_{\mathrm{NW}}$ | 545 | Ic/h |
| Total Lane Change Rate, $\mathrm{LC}_{\text {ALL }}$ | 1,538 | $\mathrm{lc} / \mathrm{h}$ |
| Weaving Intensity Factor, W | 0.548 |  |
| Average Weaving Speed, $\mathrm{S}_{\mathrm{w}}$ | 50.5 | mph |
| Average Non-Weaving Speed, $\mathrm{S}_{\mathrm{NW}}$ | 55.8 | mph |
| Average Speed, S | 54.9 | mph |
| Density, D | 27.5 | pcpmpl |
| Level of Service, LOS | C |  |

## Capacity Checks

|  | Flow | Capacity |  | V/C Ratio |
| :---: | :---: | :---: | :---: | :---: |
| Entering General Purpose Lanes | 5,255 | 7,200 | pcph | 0.73 |
| Exiting General Purpose Lanes | 5,848 | 7,200 | pcph | 0.81 |
| On Ramp | 784 | 1,900 | pcph | 0.41 |
| Off Ramp | 190 | 1,900 | pcph | 0.10 |


|  | Freeway Basic Report |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Westbound I-80 |
| Segment | Richards Blvd SB Off to On |
| Alternative | Design Year No Build |
| Time Period | PM Peak Hour |


|  | General |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
|  | Purpose Lanes - Geometric Data |  |  |  |  |  |
| General Purpose Lanes, N | 3 | ln | Terrain Type | Level |  |  |
| Segment Length, L | 210 | ft | Percent Grade | - |  |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |  |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 1.83 | $\mathrm{ramps} / \mathrm{mi}$ |  |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 70.0 | mph |  |


| General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


|  | General Purpose Lanes - Demand and Capacity |  |  |  |  |
| :--- | :---: | :--- | :--- | :--- | :--- |
| Volume, V | 5,229 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.99 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,919 | pcphpl |
| Total Trucks | $9.0 \%$ |  | Capacity, c | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |  |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.80 |  |


| General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 70.0 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 64.0 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 30.0 | pcpmpl |
| Total Ramp Density Adjustment | 5.4 | mph | Level of Service, LOS | D |  |

$\qquad$


## Freeway Merge Report



|  | Freeway Basic Report |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Westbound I-80 |
| Segment | Richards Blvd SB On to Lane Add |
| Alternative | Design Year No Build |
| Time Period | PM Peak Hour |


| General Purpose Lanes - Geometric Data |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| General Purpose Lanes, N | 3 | In | Terrain Type | Level |  |
| Segment Length, L | 2,270 | ft | Percent Grade | - |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 1.67 | ramps/mi |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 70.4 | mph |


| General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


|  | General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :--- | :--- | :--- |
| Volume, V | 5,556 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{Hv}}$ | 0.917 |  |  |
| Peak Hour Factor, PHF | 0.99 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 2,039 | pcphpl |  |
| Total Trucks | $9.0 \%$ |  | Capacity, c | 2,400 | pcphpl |  |
| Single Unit/Tractor-Trailer Mix | - | Adjusted Capacity, $\mathrm{c}_{\mathrm{adj}}$ | 2,400 | pcphpl |  |  |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 | Volume-to-Capacity Ratio, v/c | 0.85 |  |  |  |


| General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 70.4 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 62.0 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 32.9 | pcpmpl |
| Total Ramp Density Adjustment | 5.0 | mph | Level of Service, LOS | D |  |

$\qquad$

## Freeway Diverge Report

|  | Freeway Diverg |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Westbound I-80 |
| Segment | Lane Add to Old Davis Off |
| Alternative | Design Year No Build |
| Time Period | PM Peak Hour |


|  |  |  |
| :--- | :---: | :---: |
|  | Geometric Data |  |
|  |  |  |


|  | Volume Data |  |  |  |
| :--- | :---: | :---: | :---: | :---: |
|  |  |  |  |  |
| Junction Components | $\underline{\text { Freeway }}$ | $\underline{\text { Off Ramp }}$ |  |  |
| Volume, V | 5,556 | 380 | vph |  |
| Peak Hour Factor, PHF | 0.99 | 0.92 |  |  |
| Total Trucks | $9.0 \%$ | $3.0 \%$ |  |  |
| Single Unit/Tractor-Trailer Mix | - | - |  |  |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 | 2.0 |  |  |
| Heavy Vehicle Adjustment, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 | 0.971 |  |  |
| Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 6,117 | 425 | pcph |  |

Adjacent Ramp Meeting Criteria
$\left.\begin{array}{cc}\text { Upstream } & \\ \text { No } & \\ & \\ & \\ & \\ & \\ & \\ & \\ & \\ & \\ & \\ & \end{array}\right)$

## Freeway Diverge Report



|  | Freeway Basic Report |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Westbound I-80 |
| Segment | West of Old Davis Rd |
| Alternative | Design Year No Build |
| Time Period | PM Peak Hour |


|  | General |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
|  | Purpose Lanes - Geometric Data |  |  |  |  |  |
| General Purpose Lanes, N | 4 | ln | Terrain Type | Level |  |  |
| Segment Length, L | 1,350 | ft | Percent Grade | - |  |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |  |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 1.83 | $\mathrm{ramps} / \mathrm{mi}$ |  |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 70.0 | mph |  |


| General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


|  | General Purpose Lanes - Demand and Capacity |  |  |  |  |
| :--- | :---: | :--- | :--- | :--- | :--- |
| Volume, V | 5,229 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.99 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,439 | pcphpl |
| Total Trucks | $9.0 \%$ |  | Capacity, c | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |  |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.60 |  |


| General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 70.0 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 69.4 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 20.7 | pcpmpl |
| Total Ramp Density Adjustment | 5.4 | mph | Level of Service, LOS | C |  |

$\qquad$

|  | Freeway Basic Report |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Westbound I-80 |
| Segment | East of Mace Blvd |
| Alternative | Design Year Build |
| Time Period | AM Peak Hour |


|  | General |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
|  | Purpose Lanes - Geometric Data |  |  |  |  |  |
| General Purpose Lanes, N | 3 | ln | Terrain Type | Level |  |  |
| Segment Length, L | 2,590 | ft | Percent Grade | - |  |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |  |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 1.00 | $\mathrm{ramps} / \mathrm{mi}$ |  |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 72.2 | mph |  |


| General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


|  | General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :--- | :--- | :--- |
| Volume, V | 4,928 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{Hv}}$ | 0.917 |  |  |
| Peak Hour Factor, PHF | 0.98 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,827 | pcphpl |  |
| Total Trucks | $9.0 \%$ |  | Capacity, c | 2,400 | pcphpl |  |
| Single Unit/Tractor-Trailer Mix | - | Adjusted Capacity, $\mathrm{c}_{\mathrm{adj}}$ | 2,400 | pcphpl |  |  |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 | Volume-to-Capacity Ratio, v/c | 0.76 |  |  |  |


| General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 72.2 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 66.4 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 27.5 | pcpmpl |
| Total Ramp Density Adjustment | 3.2 | mph | Level of Service, LOS | D |  |

$\qquad$


| Entering General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :--- | :---: | :--- | :--- | :--- | :--- |
| Volume, V | 4,928 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.98 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,827 | pcphpl |
| Total Trucks | $9.0 \%$ |  | Capacity, c | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |  |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 | Volume-to-Capacity Ratio, v/c | 0.76 |  |  |


| Entering General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 72.6 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 66.6 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 27.4 | pcpmpl |
| Total Ramp Density Adjustment | 2.8 | mph | Level of Service, LOS | D |  |


| Segment General Purpose Lanes - Capacity, Speed, and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| General Purpose Lanes, N | 4 | ln | Average Speed, S | 70.6 | mph |
| Adjusted Capacity, cadj | 2,400 | pcphpl | Density, D | 21.6 | pcphpl |
| Flow Rate, vp | 1,524 | pcphpl | Level of Service, LOS | C |  |
| Volume-to-Capacity Ratio, v/c | 0.64 |  |  |  |  |

## Freeway Merge Report



## Freeway Merge Report



| Ramp Influence Area Density and Level of Service |  |  |  |
| :--- | :--- | :---: | :---: |
| Density in Ramp Influence Area, $D_{R}$ | pcpmpl |  |  |
| Level of Service, LOS |  |  |  |

## Segment Speed, Flow, and Density

Speed Adjustment Factor, SAF
Speed Index, $\mathrm{M}_{\mathrm{S}}$ or $\mathrm{D}_{\mathrm{S}}$
Average Speed in Ramp Influence Area, $\mathrm{S}_{\mathrm{R}} \mathrm{mph}$

Average Flow in Outer Lanes, $\mathrm{v}_{\mathrm{OA}}$
pcphpl
mph
Average Speed in Outer Lanes, $\mathrm{S}_{0}$
mph
Density across All Lanes, D
pcpmpl

|  | Freeway Basic Report |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Westbound I-80 |
| Segment | Lane Drop to Richards Blvd |
| Alternative | Design Year Build |
| Time Period | AM Peak Hour |


|  | General |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
|  | Purpose Lanes - Geometric Data |  |  |  |  |  |
| General Purpose Lanes, N | 3 | ln | Terrain Type | Level |  |  |
| Segment Length, L | 7,170 | ft | Percent Grade | - |  |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |  |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 0.83 | $\mathrm{ramps} / \mathrm{mi}$ |  |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 72.6 | mph |  |


| General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


|  | General Purpose Lanes - Demand and Capacity |  |  |  |  |
| :--- | :---: | :--- | :--- | :--- | :--- |
| Volume, V | 5,401 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.98 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 2,002 | pcphpl |
| Total Trucks | $9.0 \%$ |  | Capacity, c | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |  |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.83 |  |


| General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 72.6 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 63.3 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 31.6 | pcpmpl |
| Total Ramp Density Adjustment | 2.8 | mph | Level of Service, LOS | D |  |

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## Freeway Diverge Report

| Freeway Diverge Report |  |  |  |
| :---: | :---: | :---: | :---: |
| Project I-80/Richards B <br> Freeway Westbound I-80 <br> Segment Richards Blvd O <br> Alternative Design Year Build <br> Time Period AM Peak Hour |  |  |  |
| Geometric Data |  |  |  |
|  | Freeway | Off Ramp |  |
| Number of Lanes, N | 3 | 1 |  |
| Free-Flow Speed, FFS | 72.6 | 45 | mph |
| Segment Length, L / Deceleration Length, LD | 1,500 | 150 | ft |
| Terrain Type | Level | Level |  |
| Percent Grade | - | - |  |
| Grade Length | - | - | ft |
| Segment Type / Ramp Type | Freeway | Right |  |
| Adjustment Factors |  |  |  |
|  | Freeway | Off Ramp |  |
| Driver Population | Familiar | Familiar |  |
| Weather Type | Non-severe | Non-severe |  |
| Incident Type | No incident | No incident |  |
| Capacity Adjustment Factor, CAF | 1.00 | 1.00 |  |
| Demand Adjustment Factor, DAF | 1.00 | 1.00 |  |
| Volume Data |  |  |  |
| Junction Components | Freeway | Off Ramp |  |
| Volume, V | 5,401 | 1,170 | vph |
| Peak Hour Factor, PHF | 0.98 | 0.92 |  |
| Total Trucks | 9.0\% | 3.0\% |  |
| Single Unit/Tractor-Trailer Mix | - | - |  |
| Passenger Car Equivalent, $\mathrm{E}_{T}$ | 2.0 | 2.0 |  |
| Heavy Vehicle Adjustment, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 | 0.971 |  |
| Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 6,007 | 1,310 | pcph |

## Adjacent Ramp Data

Adjacent Ramp Meeting Criteria
Type of Adjacent Ramp
Distance to Adjacent Ramp
Volume on Adjacent Ramp

| Upstream | Downstream |
| :---: | :---: |
| No | Yes |
|  | On |
|  | 3,640 |
|  | 717 |

## Freeway Diverge Report



|  | Freeway Basic Report |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Westbound I-80 |
| Segment | Richards Blvd Off to On |
| Alternative | Design Year Build |
| Time Period | AM Peak Hour |


|  | General |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
|  | Purpose Lanes - Geometric Data |  |  |  |  |  |
| General Purpose Lanes, N | 3 | ln | Terrain Type | Level |  |  |
| Segment Length, L | 2,140 | ft | Percent Grade | - |  |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |  |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 1.33 | $\mathrm{ramps} / \mathrm{mi}$ |  |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 71.3 | mph |  |


| General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


| General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Volume, V | 4,395 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.98 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,629 | pcphpl |
| Total Trucks | 9.0\% |  | Capacity, c | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - |  | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.68 |  |


| General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 71.3 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 68.6 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 23.7 | pcpmpl |
| Total Ramp Density Adjustment | 4.1 | mph | Level of Service, LOS | C |  |

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| Freeway Merge Report |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Project I-80/Richards B <br> Freeway Westbound I-80 <br> Segment Richards Blvd O <br> Alternative Design Year Build <br> Time Period AM Peak Hour |  |  |  |  |
| Geometric Data |  |  |  |  |
|  | Freeway | On Ramp |  |  |
| Number of Lanes, N | 3 | 1 |  |  |
| Free-Flow Speed, FFS | 71.3 | 45 |  | mph |
| Segment Length, L / Acceleration Length, LA | 1,500 | 400 |  | ft |
| Terrain Type | Level | Level |  |  |
| Percent Grade | - | - |  |  |
| Grade Length | - | - |  | ft |
| Segment Type / Ramp Type | Freeway | Right |  |  |
| Adjustment Factors |  |  |  |  |
|  | Freeway | On Ramp |  |  |
| Driver Population | Familiar | Familiar |  |  |
| Weather Type | Non-severe | Non-severe |  |  |
| Incident Type | No incident | No incident |  |  |
| Capacity Adjustment Factor, CAF | 1.00 | 1.00 |  |  |
| Demand Adjustment Factor, DAF | 1.00 | 1.00 |  |  |
| Volume Data |  |  |  |  |
| Junction Components | Freeway | On Ramp |  |  |
| Volume, V | 4,395 | 640 |  | vph |
| Peak Hour Factor, PHF | 0.98 | 0.92 |  |  |
| Total Trucks | 9.0\% | 3.0\% |  |  |
| Single Unit/Tractor-Trailer Mix | - | - |  |  |
| Passenger Car Equivalent, $\mathrm{E}_{T}$ | 2.0 | 2.0 |  |  |
| Heavy Vehicle Adjustment, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 | 0.971 |  |  |
| Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 4,888 | 717 |  | pcph |
| Adjacent Ramp Data |  |  |  |  |
|  |  | Upstream | Downstream |  |
| Adjacent Ramp Meeting Criteria |  | Yes | No |  |
| Type of Adjacent Ramp |  | Off |  |  |
| Distance to Adjacent Ramp |  | 3,640 |  | ft |
| Volume on Adjacent Ramp |  | 1,310 |  | pcph |



|  | Freeway Basic Report |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Westbound I-80 |
| Segment | Richards Blvd to Lane Add |
| Alternative | Design Year Build |
| Time Period | AM Peak Hour |


|  | General |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
|  | Purpose Lanes - Geometric Data |  |  |  |  |  |
| General Purpose Lanes, N | 3 | ln | Terrain Type | Level |  |  |
| Segment Length, L | 2,270 | ft | Percent Grade | - |  |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |  |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 1.33 | $\mathrm{ramps} / \mathrm{mi}$ |  |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 71.3 | mph |  |


| General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


|  | General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :--- | :--- | :--- |
| Volume, V | 4,945 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{Hv}}$ | 0.917 |  |  |
| Peak Hour Factor, PHF | 0.98 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,833 | pcphpl |  |
| Total Trucks | $9.0 \%$ |  | Capacity, c | 2,400 | pcphpl |  |
| Single Unit/Tractor-Trailer Mix | - | Adjusted Capacity, $\mathrm{c}_{\mathrm{adj}}$ | 2,400 | pcphpl |  |  |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 | Volume-to-Capacity Ratio, v/c | 0.76 |  |  |  |


| General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS ${ }_{\text {adj }}$ | 71.3 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 65.9 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 27.8 | pcpmpl |
| Total Ramp Density Adjustment | 4.1 | mph | Level of Service, LOS | D |  |

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## Freeway Diverge Report

|  | Freeway Diverg |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Westbound I-80 |
| Segment | Lane Add to Old Davis Off |
| Alternative | Design Year Build |
| Time Period | AM Peak Hour |


| Geometric Data |  |  |  |
| :---: | :---: | :---: | :---: |
|  | Freeway | Off Ramp |  |
| Number of Lanes, N | 3 | 1 |  |
| Free-Flow Speed, FFS | 71.3 | 45 | mph |
| Segment Length, L / Deceleration Length, LD | 1,190 | 150 | ft |
| Terrain Type | Level | Level |  |
| Percent Grade | - | - |  |
| Grade Length | - | - | ft |
| Segment Type / Ramp Type | Freeway | Right |  |
| Adjustment Factors |  |  |  |
|  | Freeway | Off Ramp |  |
| Driver Population | Familiar | Familiar |  |
| Weather Type | Non-severe | Non-severe |  |
| Incident Type | No incident | No incident |  |
| Capacity Adjustment Factor, CAF | 1.00 | 1.00 |  |
| Demand Adjustment Factor, DAF | 1.00 | 1.00 |  |
| Volume Data |  |  |  |
| Junction Components | Freeway | Off Ramp |  |
| Volume, V | 4,945 | 500 | vph |
| Peak Hour Factor, PHF | 0.98 | 0.92 |  |
| Total Trucks | 9.0\% | 3.0\% |  |
| Single Unit/Tractor-Trailer Mix | - | - |  |
| Passenger Car Equivalent, $\mathrm{E}_{T}$ | 2.0 | 2.0 |  |
| Heavy Vehicle Adjustment, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 | 0.971 |  |
| Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 5,500 | 560 | pcph |

Adjacent Ramp Meeting Criteria
Upstream Downstream

Type of Adjacent Ramp
Distance to Adjacent Ramp
Volume on Adjacent Ramp
pcph

## Freeway Diverge Report



|  | Freeway Basic Report |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Westbound I-80 |
| Segment | West of Old Davis Rd |
| Alternative | Design Year Build |
| Time Period | AM Peak Hour |


|  | General |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
|  | Purpose Lanes - Geometric Data |  |  |  |  |  |
| General Purpose Lanes, N | 4 | ln | Terrain Type | Level |  |  |
| Segment Length, L | 1,350 | ft | Percent Grade | - |  |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |  |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 1.33 | $\mathrm{ramps} / \mathrm{mi}$ |  |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 71.3 | mph |  |


| General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


| General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Volume, V | 4,515 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.98 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,255 | pcphpl |
| Total Trucks | 9.0\% |  | Capacity, c | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - |  | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.52 |  |


| General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 71.3 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 71.2 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 17.6 | pcpmpl |
| Total Ramp Density Adjustment | 4.1 | mph | Level of Service, LOS | B |  |

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|  | Freeway Basic Report |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Westbound I-80 |
| Segment | East of Mace Blvd |
| Alternative | Design Year Build |
| Time Period | PM Peak Hour |


|  | General Purpose Lanes - Geometric Data |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :--- | :---: | :---: |
|  | 3 | ln | Terrain Type |  |  |  |
| General Purpose Lanes, N | 2,590 | ft | Percent Grade | - |  |  |
| Segment Length, L | 75.4 | mph | Grade Length | - | mi |  |
| Base Free Flow Speed, BFFS | 12.0 | ft | Total Ramp Density, TRD | 1.00 | $\mathrm{ramps} / \mathrm{mi}$ |  |
| Lane Width | 6.0 | ft | Free Flow Speed, FFS | 72.2 | mph |  |


| General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


| General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Volume, V | 4,352 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.99 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,597 | pcphpl |
| Total Trucks | 9.0\% |  | Capacity, c | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - |  | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |
| Passenger Car Equivalent, $\mathrm{E}_{T}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.67 |  |


| General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 72.2 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 69.5 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 23.0 | pcpmpl |
| Total Ramp Density Adjustment | 3.2 | mph | Level of Service, LOS | C |  |


|  | Freeway Basic Report |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Westbound I-80 |
| Segment | Mace Blvd to Lane Drop |
| Alternative | Design Year Build |
| Time Period | PM Peak Hour |


|  |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
|  | Entering General Purpose Lanes - Geometric Data |  |  |  |  |
| General Purpose Lanes, N | 3 | ln | Terrain Type | Level |  |
| Segment Length, L | 1,850 | ft | Percent Grade | - |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 0.83 | $\mathrm{ramps} / \mathrm{mi}$ |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 72.6 | mph |


| Entering General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


| Entering General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :--- | :---: | :--- | :--- | :--- | :--- |
| Volume, V | 4,352 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.99 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,597 | pcphpl |
| Total Trucks | $9.0 \%$ |  | Capacity, c | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - | Adjusted Capacity, $\mathrm{c}_{\mathrm{adj}}$ | 2,400 | pcphpl |  |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.67 |  |


| Entering General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS ${ }_{\text {adj }}$ | 72.6 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{Lw}}$ | 0.0 | mph | Average Speed, S | 69.8 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 22.9 | pcpmpl |
| Total Ramp Density Adjustment | 2.8 | mph | Level of Service, LOS | C |  |

## Segment General Purpose Lanes - Capacity, Speed, and Density

| Segment General |  |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
| General Purpose Lanes - Capacity, Speed, and Density |  |  |  |  |  |  |
| Adjusted Capacity, cadj | 4 | In | Average Speed, S | 71.1 | mph |  |
| Flow Rate, vp | 2,400 | pcphpl | Density, D | 20.5 | pcphpl |  |
| Volume-to-Capacity Ratio, v/c | 1,458 | pcphpl | Level of Service, LOS | C |  |  |

## Freeway Merge Report



## Freeway Merge Report



| Ramp Influence Area Density and Level of Service |  |  |  |
| :--- | :--- | :---: | :---: |
| Density in Ramp Influence Area, $D_{R}$ | pcpmpl |  |  |
| Level of Service, LOS |  |  |  |

## Segment Speed, Flow, and Density

Speed Adjustment Factor, SAF
Speed Index, $\mathrm{M}_{\mathrm{S}}$ or $\mathrm{D}_{\mathrm{S}}$
Average Speed in Ramp Influence Area, $\mathrm{S}_{\mathrm{R}} \mathrm{mph}$

Average Flow in Outer Lanes, $\mathrm{v}_{\mathrm{OA}}$
pcphpl
mph
Average Speed in Outer Lanes, $\mathrm{S}_{0}$
mph
Density across All Lanes, D
pcpmpl

|  | Freeway Basic Report |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Westbound I-80 |
| Segment | Lane Drop to Richards Blvd |
| Alternative | Design Year Build |
| Time Period | PM Peak Hour |


|  | General |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
|  | Purpose Lanes - Geometric Data |  |  |  |  |  |
| General Purpose Lanes, N | 3 | ln | Terrain Type | Level |  |  |
| Segment Length, L | 7,170 | ft | Percent Grade | - |  |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |  |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 0.83 | $\mathrm{ramps} / \mathrm{mi}$ |  |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 72.6 | mph |  |


| General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


|  | General Purpose Lanes - Demand and Capacity |  |  |  |  |
| :--- | :---: | :--- | :--- | :--- | :--- |
| Volume, V | 5,151 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.99 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,891 | pcphpl |
| Total Trucks | $9.0 \%$ |  | Capacity, c | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |  |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.79 |  |


| General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 72.6 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 65.5 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 28.9 | pcpmpl |
| Total Ramp Density Adjustment | 2.8 | mph | Level of Service, LOS | D |  |

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## Freeway Diverge Report

| Freeway Diverge Report |  |  |  |
| :---: | :---: | :---: | :---: |
| Project I-80/Richards B <br> Freeway Westbound I-80 <br> Segment Richards Blvd O <br> Alternative Design Year Build <br> Time Period PM Peak Hour |  |  |  |
| Geometric Data |  |  |  |
|  | Freeway | Off Ramp |  |
| Number of Lanes, N | 3 | 1 |  |
| Free-Flow Speed, FFS | 72.6 | 45 | mph |
| Segment Length, L / Deceleration Length, LD | 1,500 | 150 | ft |
| Terrain Type | Level | Level |  |
| Percent Grade | - | - |  |
| Grade Length | - | - | ft |
| Segment Type / Ramp Type | Freeway | Right |  |
| Adjustment Factors |  |  |  |
|  | Freeway | Off Ramp |  |
| Driver Population | Familiar | Familiar |  |
| Weather Type | Non-severe | Non-severe |  |
| Incident Type | No incident | No incident |  |
| Capacity Adjustment Factor, CAF | 1.00 | 1.00 |  |
| Demand Adjustment Factor, DAF | 1.00 | 1.00 |  |
| Volume Data |  |  |  |
| Junction Components | Freeway | Off Ramp |  |
| Volume, V | 5,151 | 610 | vph |
| Peak Hour Factor, PHF | 0.99 | 0.92 |  |
| Total Trucks | 9.0\% | 3.0\% |  |
| Single Unit/Tractor-Trailer Mix | - | - |  |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 | 2.0 |  |
| Heavy Vehicle Adjustment, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 | 0.971 |  |
| Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 5,672 | 683 | pcph |

## Adjacent Ramp Data

Adjacent Ramp Meeting Criteria

| Upstream | Downstream |
| :---: | :---: |
| No | Yes |
|  | On |
|  | 3,700 |
|  | 1,209 |

Type of Adjacent Ramp
Distance to Adjacent Ramp
Volume on Adjacent Ramp

## Freeway Diverge Report



|  | Freeway Basic Report |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Westbound I-80 |
| Segment | Richards Blvd Off to On |
| Alternative | Design Year Build |
| Time Period | PM Peak Hour |


|  | General |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
|  | Purpose Lanes - Geometric Data |  |  |  |  |  |
| General Purpose Lanes, N | 3 | ln | Terrain Type | Level |  |  |
| Segment Length, L | 2,200 | ft | Percent Grade | - |  |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |  |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 0.83 | $\mathrm{ramps} / \mathrm{mi}$ |  |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 72.6 | mph |  |


| General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


|  | General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :--- | :---: | :--- | :--- | :--- | :--- | :---: |
| Volume, V | 4,627 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |  |
| Peak Hour Factor, PHF | 0.99 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,698 | pcphpl |  |
| Total Trucks | $9.0 \%$ |  | Capacity, c | 2,400 | pcphpl |  |
| Single Unit/Tractor-Trailer Mix | - | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |  |  |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.71 |  |  |


| General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 72.6 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 68.5 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 24.8 | pcpmpl |
| Total Ramp Density Adjustment | 2.8 | mph | Level of Service, LOS | C |  |

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| Freeway Merge Report |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Project I-80/Richards B <br> Freeway Westbound I-8 <br> Segment Richards Blvd On <br> Alternative Design Year Bu <br> Time Period PM Peak Hour |  |  |  |  |
| Geometric Data |  |  |  |  |
|  | Freeway | On Ramp |  |  |
| Number of Lanes, N | 3 | 1 |  |  |
| Free-Flow Speed, FFS | 71.3 | 45 |  | mph |
| Segment Length, L / Acceleration Length, LA | 1,500 | 400 |  | ft |
| Terrain Type | Level | Level |  |  |
| Percent Grade | - | - |  |  |
| Grade Length | - |  |  | ft |
| Segment Type / Ramp Type | Freeway | Right |  |  |
| Adjustment Factors |  |  |  |  |
|  | Freeway | On Ramp |  |  |
| Driver Population | Familiar | Familiar |  |  |
| Weather Type | Non-severe | Non-severe |  |  |
| Incident Type | No incident | No incident |  |  |
| Capacity Adjustment Factor, CAF | 1.00 | 1.00 |  |  |
| Demand Adjustment Factor, DAF | 1.00 | 1.00 |  |  |
| Volume Data |  |  |  |  |
| Junction Components | Freeway | On Ramp |  |  |
| Volume, V | 4,627 | 1,080 |  | vph |
| Peak Hour Factor, PHF | 0.99 | 0.92 |  |  |
| Total Trucks | 9.0\% | 3.0\% |  |  |
| Single Unit/Tractor-Trailer Mix | - | - |  |  |
| Passenger Car Equivalent, $\mathrm{E}_{T}$ | 2.0 | 2.0 |  |  |
| Heavy Vehicle Adjustment, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 | 0.971 |  |  |
| Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 5,094 | 1,209 |  | pcph |
| Adjacent Ramp Data |  |  |  |  |
|  |  | Upstream | Downstream |  |
| Adjacent Ramp Meeting Criteria |  | Yes | No |  |
| Type of Adjacent Ramp |  | Off |  |  |
| Distance to Adjacent Ramp |  | 3,700 |  | ft |
| Volume on Adjacent Ramp |  | 683 |  | pcph |



|  | Freeway Basic Report |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Westbound I-80 |
| Segment | Richards Blvd to Lane Add |
| Alternative | Design Year Build |
| Time Period | PM Peak Hour |


|  | General |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
|  | Purpose Lanes - Geometric Data |  |  |  |  |  |
| General Purpose Lanes, N | 3 | ln | Terrain Type | Level |  |  |
| Segment Length, L | 2,270 | ft | Percent Grade | - |  |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |  |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 1.33 | $\mathrm{ramps} / \mathrm{mi}$ |  |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 71.3 | mph |  |


| General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


|  | General Purpose Lanes - Demand and Capacity |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :--- | :--- | :--- |
| Volume, V | 5,556 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{Hv}}$ | 0.917 |  |  |
| Peak Hour Factor, PHF | 0.99 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 2,039 | pcphpl |  |
| Total Trucks | $9.0 \%$ |  | Capacity, c | 2,400 | pcphpl |  |
| Single Unit/Tractor-Trailer Mix | - | Adjusted Capacity, $\mathrm{c}_{\mathrm{adj}}$ | 2,400 | pcphpl |  |  |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 | Volume-to-Capacity Ratio, v/c | 0.85 |  |  |  |


| General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 71.3 | mph |
| Lane Width Adjustment, f LW | 0.0 | mph | Average Speed, S | 62.2 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 32.8 | pcpmpl |
| Total Ramp Density Adjustment | 4.1 | mph | Level of Service, LOS | D |  |

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## Freeway Diverge Report

|  | Freeway Diverg |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Westbound I-80 |
| Segment | Lane Add to Old Davis Off |
| Alternative | Design Year Build |
| Time Period | PM Peak Hour |


| Geometric Data |  |  |  |
| :---: | :---: | :---: | :---: |
|  | Freeway | Off Ramp |  |
| Number of Lanes, N | 4 | 1 |  |
| Free-Flow Speed, FFS | 71.3 | 45 | mph |
| Segment Length, L / Deceleration Length, LD | 1,190 | 150 | ft |
| Terrain Type | Level | Level |  |
| Percent Grade | - | - |  |
| Grade Length | - | - | ft |
| Segment Type / Ramp Type | Freeway | Right |  |
| Adjustment Factors |  |  |  |
|  | Freeway | Off Ramp |  |
| Driver Population | Familiar | Familiar |  |
| Weather Type | Non-severe | Non-severe |  |
| Incident Type | No incident | No incident |  |
| Capacity Adjustment Factor, CAF | 1.00 | 1.00 |  |
| Demand Adjustment Factor, DAF | 1.00 | 1.00 |  |
| Volume Data |  |  |  |
| Junction Components | Freeway | Off Ramp |  |
| Volume, V | 5,556 | 380 | vph |
| Peak Hour Factor, PHF | 0.99 | 0.92 |  |
| Total Trucks | 9.0\% | 3.0\% |  |
| Single Unit/Tractor-Trailer Mix | - | - |  |
| Passenger Car Equivalent, $\mathrm{E}_{T}$ | 2.0 | 2.0 |  |
| Heavy Vehicle Adjustment, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 | 0.971 |  |
| Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 6,117 | 425 | pcph |

Adjacent Ramp Meeting Criteria
Upstream Downstream

Type of Adjacent Ramp
Distance to Adjacent Ramp
Volume on Adjacent Ramp
pcph

## Freeway Diverge Report



|  | Freeway Basic Report |
| :--- | :--- |
|  |  |
| Project | I-80/Richards Blvd Interchange |
| Freeway | Westbound I-80 |
| Segment | West of Old Davis Rd |
| Alternative | Design Year Build |
| Time Period | PM Peak Hour |


|  | General |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: |
|  | Purpose Lanes - Geometric Data |  |  |  |  |  |
| General Purpose Lanes, N | 4 | ln | Terrain Type | Level |  |  |
| Segment Length, L | 1,350 | ft | Percent Grade | - |  |  |
| Base Free Flow Speed, BFFS | 75.4 | mph | Grade Length | - | mi |  |
| Lane Width | 12.0 | ft | Total Ramp Density, TRD | 1.33 | $\mathrm{ramps} / \mathrm{mi}$ |  |
| Right Side Lateral Clearance | 6.0 | ft | Free Flow Speed, FFS | 71.3 | mph |  |


| General Purpose Lanes - Adjustment Factors |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: |
| Driver Population | Familiar | Speed Adjustment Factor, SAF | 1.00 |  |
| Weather Type | Non-severe | Capacity Adjustment Factor, CAF | 1.00 |  |
| Incident Type | No incident | Demand Adjustment Factor, DAF | 1.00 |  |


|  | General Purpose Lanes - Demand and Capacity |  |  |  |  |
| :--- | :---: | :--- | :--- | :--- | :--- |
| Volume, V | 5,229 | vph | Heavy Vehicle Adjustment Factor, $\mathrm{f}_{\mathrm{HV}}$ | 0.917 |  |
| Peak Hour Factor, PHF | 0.99 |  | Flow Rate, $\mathrm{v}_{\mathrm{p}}$ | 1,439 | pcphpl |
| Total Trucks | $9.0 \%$ |  | Capacity, c | 2,400 | pcphpl |
| Single Unit/Tractor-Trailer Mix | - | Adjusted Capacity, $\mathrm{c}_{\text {adj }}$ | 2,400 | pcphpl |  |
| Passenger Car Equivalent, $\mathrm{E}_{\mathrm{T}}$ | 2.0 |  | Volume-to-Capacity Ratio, v/c | 0.60 |  |


| General Purpose Lanes - Speed and Density |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :---: | :---: |
| Measured or Base FFS | Base |  | Adjusted Free Flow Speed, FFS adj | 71.3 | mph |
| Lane Width Adjustment, $\mathrm{f}_{\mathrm{LW}}$ | 0.0 | mph | Average Speed, S | 70.3 | mph |
| Right Lateral Clearance Adjustment, $\mathrm{f}_{\text {RLC }}$ | 0.0 | mph | Density, D | 20.5 | pcpmpl |
| Total Ramp Density Adjustment | 4.1 | mph | Level of Service, LOS | C |  |


| Output Summary |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| General Information |  |  |  |  |  |  |  |  |
| Project description: Analyst: | I-80/Richards Blvd Interchange - Design Year Conditions No Build Alternative |  |  |  |  |  |  |  |
|  | DS | Date: | 1/20/2018 |  | Area type: |  | Urban |  |
| First year of analysis: | 2035 |  |  |  |  |  |  |  |
| Last year of analysis: | 2035 |  |  |  |  |  |  |  |
| Crash Data Description |  |  |  |  |  |  |  |  |
| Freeway segments | Segment crash data available? |  |  | No | First year of crash data: |  |  |  |
|  | Project-level crash data available? |  |  | No | Last year of crash data: |  |  |  |
| Ramp segments | Segment crash data available? |  |  | Yes | First year of crash data: |  |  | 2012 |
|  | Project-level crash data available? |  |  | No | Last year of crash data: |  |  | 2014 |
| Ramp terminals | Segment crash data available? |  |  | No | First year of crash data: |  |  |  |
|  | Project-level crash data available? |  |  | No | Last year of crash data: |  |  |  |
| Estimated Crash Statistics |  |  |  |  |  |  |  |  |
| Crashes for Entire Facility |  |  | Total | K | A | B | C | PDO |
| Estimated number of crashes during Study Period, crashes: |  |  | 5.7 | 0.1 | 0.2 | 0.9 | 1.1 | 3.5 |
| Estimated average crash freq. during Study Period, crashes/yr: |  |  | 5.7 | 0.1 | 0.2 | 0.9 | 1.1 | 3.5 |
| Crashes by Facility Component |  | Nbr. Sites | Total | K | A | B | C | PDO |
| Freeway segments, crashes: |  | 0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Ramp segments, crashes: |  | 5 | 5.7 | 0.1 | 0.2 | 0.9 | 1.1 | 3.5 |
|  |  | 0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Crashes for Entire Facility by Year |  | Year | Total | K | A | B | C | PDO |
| Estimated number of crashes during the Study Period, crashes: |  | 2035 | 5.7 | 0.1 | 0.2 | 0.9 | 1.1 | 3.5 |
|  |  | 2036 |  |  |  |  |  |  |
|  |  | 2037 |  |  |  |  |  |  |
|  |  | 2038 |  |  |  |  |  |  |
|  |  | 2039 |  |  |  |  |  |  |
|  |  | 2040 |  |  |  |  |  |  |
|  |  | 2041 |  |  |  |  |  |  |
|  |  | 2042 |  |  |  |  |  |  |
|  |  | 2043 |  |  |  |  |  |  |
|  |  | 2044 |  |  |  |  |  |  |
|  |  | 2045 |  |  |  |  |  |  |
|  |  | 2046 |  |  |  |  |  |  |
|  |  | 2047 |  |  |  |  |  |  |
|  |  | 2048 |  |  |  |  |  |  |
|  |  | 2049 |  |  |  |  |  |  |
|  |  | 2050 |  |  |  |  |  |  |
|  |  | 2051 |  |  |  |  |  |  |
|  |  | 2052 |  |  |  |  |  |  |
|  |  | 2053 |  |  |  |  |  |  |
|  |  | 2054 |  |  |  |  |  |  |
|  |  | 2055 |  |  |  |  |  |  |
|  |  | 2056 |  |  |  |  |  |  |
|  |  | 2057 |  |  |  |  |  |  |
|  |  | 2058 |  |  |  |  |  |  |
| Distribution of Crashes for Entire Facility |  |  |  |  |  |  |  |  |
| Crash Type | Crash Type Category |  | Estimated Number of Crashes During the Study Period |  |  |  |  |  |
|  |  |  | Total | K | A | B | C | PDO |
| Multiple vehicle | Head-on crashes: |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
|  | Right-angle crashes: |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
|  | Rear-end crashes: |  | 0.3 | 0.0 | 0.0 | 0.1 | 0.1 | 0.2 |
|  | Sideswipe crashes: |  | 0.1 | 0.0 | 0.0 | 0.0 | 0.0 | 0.1 |
|  | Other multiple-vehicle crashes: |  | 0.1 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
|  | Total multiple-vehicle crashes: |  | 0.5 | 0.0 | 0.0 | 0.1 | 0.1 | 0.3 |
| Single vehicle | Crashes with animal: |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
|  | Crashes with fixed object: |  | 4.1 | 0.0 | 0.1 | 0.6 | 0.7 | 2.7 |
|  | Crashes with other object: |  | 0.1 | 0.0 | 0.0 | 0.0 | 0.0 | 0.1 |
|  | Crashes with parked vehicle: |  | 0.1 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
|  | Other single-vehicle crashes |  | 0.9 | 0.0 | 0.0 | 0.2 | 0.2 | 0.4 |
|  | Total single-vehicle crashes: |  | 5.2 | 0.1 | 0.2 | 0.8 | 1.0 | 3.2 |
| Total crashes: |  |  | 5.7 | 0.1 | 0.2 | 0.9 | 1.1 | 3.5 |


| Output Summary |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| General Information |  |  |  |  |  |  |  |  |
| Project description: Analyst: | \|1-80/Richards Blvd Interchange - Design Year Conditions Build Alternative |  |  |  |  |  |  |  |
|  | DS | Date: | 1/20/2018 |  | Area type: |  | Urban |  |
| First year of analysis: | 2035 |  |  |  |  |  |  |  |
| Last year of analysis: | 2035 |  |  |  |  |  |  |  |
| Crash Data Description |  |  |  |  |  |  |  |  |
| Freeway segments | Segment crash data available? |  |  | No | First year of crash data: |  |  |  |
|  | Project-level crash data available? |  |  | No | Last year of crash data: |  |  |  |
| Ramp segments | Segment crash data available? |  |  | No | First year of crash data: |  |  |  |
|  | Project-level crash data available? |  |  | No | Last year of crash data: |  |  |  |
| Ramp terminals | Segment crash data available? |  |  | No | First year of crash data: |  |  |  |
|  | Project-level crash data available? |  |  | No | Last year of crash data: |  |  |  |
| Estimated Crash Statistics |  |  |  |  |  |  |  |  |
| Crashes for Entire Facility |  |  | Total | K | A | B | C | PDO |
| Estimated number of crashes during Study Period, crashes: |  |  | 2.1 | 0.0 | 0.1 | 0.4 | 0.5 | 1.1 |
| Estimated average crash freq. during Study Period, crashes/yr: |  |  | 2.1 | 0.0 | 0.1 | 0.4 | 0.5 | 1.1 |
| Crashes by Facility Component |  | Nbr. Sites | Total | K | A | B | C | PDO |
| Freeway segments, crashes: |  | 0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Ramp segments, crashes: |  | 2 | 2.1 | 0.0 | 0.1 | 0.4 | 0.5 | 1.1 |
| Crossroad ramp terminals, crashes: |  | 0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Crashes for Entire Facility by Year |  | Year | Total | K | A | B | C | PDO |
| Estimated number of crashes during the Study Period, crashes: |  | 2035 | 2.1 | 0.0 | 0.1 | 0.4 | 0.5 | 1.1 |
|  |  | 2036 |  |  |  |  |  |  |
|  |  | 2037 |  |  |  |  |  |  |
|  |  | 2038 |  |  |  |  |  |  |
|  |  | 2039 |  |  |  |  |  |  |
|  |  | 2040 |  |  |  |  |  |  |
|  |  | 2041 |  |  |  |  |  |  |
|  |  | 2042 |  |  |  |  |  |  |
|  |  | 2043 |  |  |  |  |  |  |
|  |  | 2044 |  |  |  |  |  |  |
|  |  | 2045 |  |  |  |  |  |  |
|  |  | 2046 |  |  |  |  |  |  |
|  |  | 2047 |  |  |  |  |  |  |
|  |  | 2048 |  |  |  |  |  |  |
|  |  | 2049 |  |  |  |  |  |  |
|  |  | 2050 |  |  |  |  |  |  |
|  |  | 2051 |  |  |  |  |  |  |
|  |  | 2052 |  |  |  |  |  |  |
|  |  | 2053 |  |  |  |  |  |  |
|  |  | 2054 |  |  |  |  |  |  |
|  |  | 2055 |  |  |  |  |  |  |
|  |  | 2056 |  |  |  |  |  |  |
|  |  | 2057 |  |  |  |  |  |  |
|  |  | 2058 |  |  |  |  |  |  |
| Distribution of Crashes for Entire Facility |  |  |  |  |  |  |  |  |
| Crash Type | Crash Type Category |  | Estimated Number of Crashes During the Study Period |  |  |  |  |  |
|  |  |  | Total | K | A | B | C | PDO |
| Multiple vehicle | Head-on crashes: |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
|  | Right-angle crashes: |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
|  | Rear-end crashes: |  | 0.2 | 0.0 | 0.0 | 0.0 | 0.1 | 0.1 |
|  | Sideswipe crashes: |  | 0.1 | 0.0 | 0.0 | 0.0 | 0.0 | 0.1 |
|  | Other multiple-vehicle crashes: |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
|  | Total multiple-vehicle crashes: |  | 0.4 | 0.0 | 0.0 | 0.1 | 0.1 | 0.2 |
| Single vehicle | Crashes with animal: |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
|  | Crashes with fixed object: |  | 1.3 | 0.0 | 0.0 | 0.2 | 0.3 | 0.7 |
|  | Crashes with other object: |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
|  | Crashes with parked vehicle: |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
|  | Other single-vehicle crashes |  | 0.3 | 0.0 | 0.0 | 0.1 | 0.1 | 0.1 |
|  | Total single-vehicle crashes: |  | 1.7 | 0.0 | 0.1 | 0.3 | 0.4 | 0.8 |
| Total crashes: |  |  | 2.1 | 0.0 | 0.1 | 0.4 | 0.5 | 1.1 |

## RAMP METERING ANALYSIS

Project: I-80/Richards Blvd Interchange
Ramp: Westbound I-80 On-ramp
Scenario: Build Alternative Design Year Conditions

Configuration: 1 metered + 1 HOV
Peak Hour Volume: 640
Peak Period Volume: 1,250

| HOV Bypass (\%) | $15 \%$ |
| ---: | :---: |
| Metered Volume $(\mathrm{veh} / \mathrm{hr})$ | 544 |
| Metering Rate $(\mathrm{veh} / \mathrm{hr})$ | 575 |
| Discharge Rate $(\mathrm{veh} / 15 \mathrm{~min})$ | 144 |


| Storage Length (ft) | 630 |
| ---: | :---: |
| Storage Lanes | 1 |
| Maximum Storage (veh) | 21 |


| Time <br> Interval | Hourly <br> Arrival <br> Distribution | Estimated <br> 15-Minute <br> Volumes | Metered <br> 15-Minute <br> min flows | Excess <br> Demand | Accum- <br> ulated <br> Vehicles | Total <br> Delay <br> (veh-hr) | Vehicles <br> Delayed | Total <br> Hourly <br> Volume | Metered <br> Hourly <br> Volume |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $7: 00-7: 15$ | $18 \%$ | 115 | 98 | 0 | 0 | 0.00 | 0 |  |  |
| 7:15-7:30 | $22 \%$ | 141 | 120 | 0 | 0 | 0.00 | 0 |  |  |
| $7: 30-7: 45$ | $26 \%$ | 168 | 143 | 0 | 0 | 0.00 | 0 |  |  |
| $7: 45-8: 00$ | $30 \%$ | 189 | 161 | 17 | 17 | 4.23 | 161 | 613 | 521 |
| $8: 00-8: 15$ | $19 \%$ | 124 | 105 | 0 | 0 | 0.00 | 0 | 622 | 529 |
| $8: 15-8: 30$ | $24 \%$ | 153 | 130 | 0 | 0 | 0.00 | 0 | 634 | 539 |
| $8: 30-8: 45$ | $30 \%$ | 190 | 162 | 18 | 18 | 4.44 | 162 | 656 | 558 |
| $8: 45-9: 00$ | $27 \%$ | 172 | 146 | 2 | 20 | 5.05 | 146 | 639 | 543 |


| Total Delay (veh-hr) | 14 |
| ---: | :---: |
| Total Vehicles Delayed (veh) | 468 |
| Average Delay (hr) | 0.03 |
| Average Delay (min) | 1.76 |


| Maximum Queue (veh) | 20 |
| ---: | :---: |
| Maximum Queue (ft) | 606 |

Project: I-80/Richards Blvd Interchange
Ramp: Westbound I-80 On-ramp
Scenario: Build Alternative Design Year Conditions

Configuration: 1 metered + 1 HOV Peak Hour Volume: 1,080
Peak Period Volume: 2,150

| HOV Bypass $(\%)$ | $15 \%$ |
| ---: | :---: |
| Metered Volume $(\mathrm{veh} / \mathrm{hr})$ | 918 |
| Metering Rate $(\mathrm{veh} / \mathrm{hr})$ | 900 |
| Discharge Rate $(\mathrm{veh} / 15 \mathrm{~min})$ | 225 |


| Storage Length (ft) | 630 |
| ---: | :---: |
| Storage Lanes | 1 |
| Maximum Storage (veh) | 21 |


| Time <br> Interval | Hourly <br> Arrival <br> Distribution | Estimated <br> 15-Minute <br> Volumes | Metered <br> 15-Minute <br> min flows | Excess <br> Demand | Accum- <br> ulated <br> Vehicles | Total <br> Delay <br> (veh-hr) | Vehicles <br> Delayed | Total <br> Hourly <br> Volume | Metered <br> Hourly <br> Volume |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $4: 00-4: 15$ | $23 \%$ | 245 | 208 | 0 | 0 | 0.00 | 0 |  |  |
| $4: 15-4: 30$ | $24 \%$ | 262 | 223 | 0 | 0 | 0.00 | 0 |  |  |
| $4: 30-4: 45$ | $22 \%$ | 233 | 198 | 0 | 0 | 0.00 | 0 |  |  |
| $4: 45-5: 00$ | $24 \%$ | 254 | 216 | 0 | 0 | 0.00 | 0 | 994 | 845 |
| $5: 00-5: 15$ | $31 \%$ | 331 | 281 | 56 | 56 | 14.09 | 281 | 1080 | 918 |
| $5: 15-5: 30$ | $27 \%$ | 292 | 248 | 23 | 80 | 19.89 | 248 | 1110 | 944 |
| $5: 30-5: 45$ | $28 \%$ | 299 | 254 | 29 | 109 | 27.18 | 254 | 1176 | 1000 |
| $5: 45-3: 00$ | $21 \%$ | 230 | 196 | 0 | 79 | 19.80 | 196 | 1152 | 979 |


| Total Delay (veh-hr) | 81 |
| ---: | :---: |
| Total Vehicles Delayed $(\mathrm{veh})$ | 979 |
| Average Delay $(\mathrm{hr})$ | 0.08 |
| Average Delay $(\mathrm{min})$ | 4.96 |


| Maximum Queue (veh) | 109 |
| ---: | :---: |
| Maximum Queue (ft) | 3,261 |

## RAMP METERING ANALYSIS

Project: I-80/Richards Blvd Interchange
Ramp: Westbound I-80 On-ramp
Scenario: Build Alternative Design Year Conditions

Configuration: 1 metered + 1 HOV
Peak Hour Volume: 640
Peak Period Volume: $\mathbf{1 , 2 5 0}$

| HOV Bypass (\%) | $15 \%$ |
| ---: | :---: |
| Metered Volume $(\mathrm{veh} / \mathrm{hr})$ | 544 |
| Metering Rate $(\mathrm{veh} / \mathrm{hr})$ | 540 |
| Discharge Rate $(\mathrm{veh} / 15 \mathrm{~min})$ | 135 |


| Storage Length (ft) | 630 |
| ---: | :---: |
| Storage Lanes | 2 |
| Maximum Storage (veh) | 42 |


| Time <br> Interval | Hourly <br> Arrival <br> Distribution | Estimated <br> 15-Minute <br> Volumes | Metered <br> 15-Minute <br> min flows | Excess <br> Demand | Accum- <br> ulated <br> Vehicles | Total <br> Delay <br> (veh-hr) | Vehicles <br> Delayed | Total <br> Hourly <br> Volume | Metered <br> Hourly <br> Volume |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $7: 00-7: 15$ | $18 \%$ | 115 | 98 | 0 | 0 | 0.00 | 0 |  |  |
| 7:15-7:30 | $22 \%$ | 141 | 120 | 0 | 0 | 0.00 | 0 |  |  |
| $7: 30-7: 45$ | $26 \%$ | 168 | 143 | 8 | 8 | 1.95 | 143 |  |  |
| $7: 45-8: 00$ | $30 \%$ | 189 | 161 | 26 | 33 | 8.36 | 161 | 613 | 521 |
| $8: 00-8: 15$ | $19 \%$ | 124 | 105 | 0 | 4 | 0.96 | 105 | 622 | 529 |
| $8: 15-8: 30$ | $24 \%$ | 153 | 130 | 0 | 0 | 0.00 | 0 | 634 | 539 |
| $8: 30-8: 45$ | $30 \%$ | 190 | 162 | 27 | 27 | 6.63 | 162 | 656 | 558 |
| $8: 45-9: 00$ | $27 \%$ | 172 | 146 | 11 | 38 | 9.43 | 146 | 639 | 543 |


| Total Delay (veh-hr) | 27 |
| ---: | :---: |
| Total Vehicles Delayed (veh) | 717 |
| Average Delay (hr) | 0.04 |
| Average Delay $(\mathrm{min})$ | 2.29 |


| Maximum Queue (veh) | 38 |
| ---: | :---: |
| Maximum Queue (ft) | 566 |

Project: I-80/Richards Blvd Interchange
Ramp: Westbound I-80 On-ramp
Scenario: Build Alternative Design Year Conditions

Configuration: 1 metered + 1 HOV Peak Hour Volume: 1,080
Peak Period Volume: 2,150

| HOV Bypass $(\%)$ | $15 \%$ |
| ---: | :---: |
| Metered Volume $(\mathrm{veh} / \mathrm{hr})$ | 918 |
| Metering Rate $(\mathrm{veh} / \mathrm{hr})$ | 990 |
| Discharge Rate $(\mathrm{veh} / 15 \mathrm{~min})$ | 248 |


| Storage Length (ft) | 630 |
| ---: | :---: |
| Storage Lanes | 2 |
| Maximum Storage (veh) |  |
| 42 |  |


| Time <br> Interval | Hourly <br> Arrival <br> Distribution | Estimated <br> 15-Minute <br> Volumes | Metered <br> 15-Minute <br> min flows | Excess <br> Demand | Accum- <br> ulated <br> Vehicles | Total <br> Delay <br> (veh-hr) | Vehicles <br> Delayed | Total <br> Hourly <br> Volume | Metered <br> Hourly <br> Volume |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $4: 00-4: 15$ | $23 \%$ | 245 | 208 | 0 | 0 | 0.00 | 0 |  |  |
| $4: 15-4: 30$ | $24 \%$ | 262 | 223 | 0 | 0 | 0.00 | 0 |  |  |
| $4: 30-4: 45$ | $22 \%$ | 233 | 198 | 0 | 0 | 0.00 | 0 |  |  |
| $4: 45-5: 00$ | $24 \%$ | 254 | 216 | 0 | 0 | 0.00 | 0 | 994 | 845 |
| $5: 00-5: 15$ | $31 \%$ | 331 | 281 | 34 | 34 | 8.46 | 281 | 1080 | 918 |
| $5: 15-5: 30$ | $27 \%$ | 292 | 248 | 1 | 35 | 8.64 | 248 | 1110 | 944 |
| $5: 30-5: 45$ | $28 \%$ | 299 | 254 | 7 | 41 | 10.30 | 254 | 1176 | 1000 |
| $5: 45-3: 00$ | $21 \%$ | 230 | 196 | 0 | 0 | 0.00 | 0 | 1152 | 979 |


| Total Delay (veh-hr) | 27 |
| ---: | :---: |
| Total Vehicles Delayed $(\mathrm{veh})$ | 784 |
| Average Delay $(\mathrm{hr})$ | 0.03 |
| Average Delay $(\mathrm{min})$ | 2.10 |


| Maximum Queue (veh) | 41 |
| ---: | :---: |
| Maximum Queue (ft) | 618 |

## Traffic Index for Pavement Design



[^9]
## Traffic Index for Pavement Design

| Roadway: I-80 <br> Limits: East of Olive Drive <br> Facility type: Freeway or Expressway |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Lanes in one direction |  |  |  |  |
| Design life in years | 20 |  |  |  |
| 1. Baseline one-way daily traffic volume |  | 2022 Forecast |  |  |
| Forecasted one-way daily traffic volume | 90,090 | 2042 Forecast |  |  |
| 2. Baseline truck percentage | 9.0\% | Caltrans truck volumes, 2015 |  |  |
| Baseline one-way daily truck traffic volume | 6,496 |  |  |  |
| 3. Forecasted truck percentage | 9.0\% | Caltrans truck volumes, 2015 |  |  |
| Forecasted one-way daily truck traffic volume | 8,108 |  |  |  |
| 4. Expanded average daily truck traffic | 7,302 |  |  |  |
| 5. Distribution of truck traffic by axles | Caltrans truck volumes, 2015 |  |  |  |
|  |  |  | Outside Lanes | Inside Lanes |
|  | Vehicle Type | Percentage | Daily Trucks | Daily Trucks |
|  | 2 Axle | 28.5\% | 1,666 | 417 |
|  | 3 Axle | 7.6\% | 442 | 111 |
|  | 4 Axle | 3.4\% | 201 | 50 |
|  | 5+ Axle | 60.5\% | 3,532 | 883 |
| 6. Calculation of total ESAL (Equivalent Single-Axle Loads) |  |  |  |  |
|  |  | Constants for | Outside Lanes | Inside Lanes |
|  | Vehicle Type | $\underline{20-Y e a r ~ E S A L ~}$ | 20-Year ESAL | 20-Year ESAL |
|  | 2 Axle | 1,380 | 2,299,632 | 574,908 |
|  | 3 Axle | 3,680 | 1,628,032 | 407,008 |
|  | 4 Axle | 5,880 | 1,180,704 | 295,176 |
|  | 5+ Axle | 13,780 | 48,670,960 | 12,167,740 |
|  | TOTAL |  | 53,779,328 | 13,444,832 |
| 7. Calculation of Traffic Index |  |  |  |  |
|  |  | Outside Lanes | Inside Lanes |  |
|  | Raw Value | 14.5 | 12.3 |  |
|  | Final Value | 14.5 | 12.5 |  |

[^10]
## Traffic Index for Pavement Design

| Roadway: Richards Boulevard <br> Limits: I-80 Overcrossing <br> Facility type: Conventional Highway |  |  |  |
| :---: | :---: | :---: | :---: |
| Design life in years: $10$ | $\begin{gathered} 2 \\ 10 \end{gathered}$ |  |  |
| 1. Baseline one-way daily traffic volume Forecasted one-way daily traffic volume | $\begin{aligned} & 13,960 \\ & 20,580 \end{aligned}$ | 2025 Forecast |  |
| 2. Baseline truck percentage | 2.0\% | May 2016 peak hour traffic counts |  |
| Baseline one-way daily truck traffic volume | 279 |  |  |
| 3. Forecasted truck percentage | 2.0\% | May 2016 peak hour traffic counts |  |
| Forecasted one-way daily truck traffic volume | 412 |  |  |
| 4. Expanded average daily truck traffic | 345 |  |  |
| 5. Distribution of truck traffic by axles | Estimated |  |  |
|  | Vehicle Type | Percentage | Daily Trucks |
|  | 2 Axle | 60.0\% | 207 |
|  | 3 Axle | 10.0\% | 35 |
|  | 4 Axle | 10.0\% | 35 |
|  | 5+Axle | 20.0\% | 69 |
| 6. Calculation of total ESAL (Equivalent Single-Axle Loads) |  |  |  |
|  | Constants for |  |  |
|  | Vehicle Type | 10-Year ESAL | 10-Year ESAL |
|  | 2 Axle | 690 | 142,830 |
|  | 3 Axle | 1,840 | 64,400 |
|  | 4 Axle | 2,940 | 102,900 |
|  | $\underline{5+\text { Axle }}$ | 6,890 | 475,410 |
|  | TOTAL |  | 785,540 |
| 7. Calculation of Traffic Index |  |  |  |
| Raw Value 8.7 |  |  |  |
| Final Value 10.0 |  |  |  |

## Traffic Index for Pavement Design

| Roadway: Richards Boulevard <br> Limits: I-80 Overcrossing <br> Facility type: Conventional Highway |  |  |  |
| :---: | :---: | :---: | :---: |
| Lanes in one direction Design life in years | $\begin{gathered} 2 \\ 20 \end{gathered}$ |  |  |
| 1. Baseline one-way daily traffic volume Forecasted one-way daily traffic volume | $\begin{aligned} & 13,960 \\ & 20,580 \end{aligned}$ | 2025 Forecast <br> 2045 Forecast |  |
| 2. Baseline truck percentage | 2.0\% | May 2016 peak hour traffic counts |  |
| Baseline one-way daily truck traffic volume | 279 |  |  |
| 3. Forecasted truck percentage | 2.0\% | May 2016 peak hour traffic counts |  |
| Forecasted one-way daily truck traffic volume | 412 |  |  |
| 4. Expanded average daily truck traffic | 345 |  |  |
| 5. Distribution of truck traffic by axles | Estimated |  |  |
|  | Vehicle Type | Percentage | Daily Trucks |
|  | 2 Axle | 60.0\% | 207 |
|  | 3 Axle | 10.0\% | 35 |
|  | 4 Axle | 10.0\% | 35 |
|  | 5+Axle | 20.0\% | 69 |
| 6. Calculation of total ESAL (Equivalent Single-Axle Loads) |  |  |  |
|  |  | Constants for |  |
|  | Vehicle Type | $\underline{20-Y e a r ~ E S A L ~}$ | 20-Year ESAL |
|  | 2 Axle | 1,380 | 285,660 |
|  | 3 Axle | 3,680 | 128,800 |
|  | 4 Axle | 5,880 | 205,800 |
|  | $\underline{5+\text { Axle }}$ | 13,780 | 950,820 |
|  | TOTAL |  | 1,571,080 |
| 7. Calculation of Traffic Index |  |  |  |
|  | Raw Value | 9.5 |  |
|  | Final Value | 10.0 |  |


[^0]:    1 Occupancy of burrowing owl habitat during preconstruction surveys is confirmed at a site when at least one burrowing owl or sign (fresh whitewash, fresh pellets, feathers, or nest ornamentation) is observed at or near a burrow entrance.

[^1]:    2 The Conservancy will maintain a checklist of passive relocation techniques. CDFW will approve the initial list, and the Conservancy will update as needed in coordination with CDFW.

[^2]:    3 See Table 2.14 in IPCC Fourth Assessment Report: Climate Change 2007 (AR4): The Physical Science Basis. Contribution of Working Group I to the Fourth Assessment Report of the Intergovernmental Panel on Climate Change [Solomon, S., D. Qin, M. Manning, Z. Chen, M. Marquis, K.B. Averyt, M. Tignor and H.L. Miller (eds.)]. Cambridge University Press, Cambridge, United Kingdom, and New York, NY, USA. http://www.ipcc.ch/pdf/assessment-report/ar4/wg1/ar4-wg1-chapter2.pdf.
    4 See http://www.airquality.org/Businesses/CEQA-Land-Use-Planning/CEQA-Guidance-Tools.

[^3]:    5 The term recognized environmental condition (REC) means the presence or likely presence of any hazardous substances or petroleum products on a property under conditions that indicate an existing release, a past release, or a material threat of a release of any hazardous substances or petroleum products into structures on the property or into the ground, ground water, or surface water of the property. The term includes hazardous substances or petroleum products even under conditions in compliance with laws. The term is not intended to include de minimis conditions that generally do not present a threat to human health or the environment and that generally would not be the subject of an enforcement action if brought to the attention of appropriate governmental agencies. Conditions determined to be de minimis are not recognized environmental conditions.

[^4]:    6 A sound's loudness is measured in decibels (dB). Normal conversation is about 60 dB , a lawn mower is about 90 dB , and a loud rock concert is about 120 dB .

[^5]:    7 A-weighted decibels, abbreviated dBA , or dBa , or $\mathrm{dB}(\mathrm{a})$, are an expression of the relative loudness of sounds in air as perceived by the human ear. In the A-weighted system, the decibel values of sounds at low frequencies are reduced, compared with unweighted decibels, in which no correction is made for audio frequency.

[^6]:    8 Lmax is the maximum sound level during a measurement period or a noise event.

[^7]:    ${ }^{1}$ RMSE is a statistical measure for how close the estimated value is to the observed data, regardless of positive or negative direction.
    ${ }^{2}$ Correlation coefficient is a variable that determines the degree to which two variables are associated. The value varies between $-1(-100 \%)$ and 1 (100\%). A value closer to 1 suggests, in general, the model estimates are in line with observed data.

[^8]:    Note: Values are in collisions per year.
    Source: Caltrans TASAS Table B, January 2012 to December 2014, and Fehr \& Peers, 2018

[^9]:    Source: Highway Design Manual, Chapter 610 (Caltrans, 2012)

[^10]:    Source: Highway Design Manual, Chapter 610 (Caltrans, 2012)

