



Drainage Analysis – Lands of McLaughlin & Konolige

Prepared July 9, 2020

Site:

5575 Lovall Valley Road Napa, California APN: 050-361-013-000

HLS Project # 3567

Analysis Prepared by: Hogan Land Services, Inc. 1702 4th Street Santa Rosa, CA 95404 Jim Conklin, EIT jconklin@hoganls.com 707-544-2104 Owners: Janet Mclaughlin & Kurt Konolige 865 College Ave Menlo Park, CA 94025 (650) 796-1228





PREPARED: May 21, 2020

SUBJECT: 10-Year event hydrology calculations and reasoning for drainage network sizing capacity and

velocity

PROJECT: Drainage Analysis – Lands of McLaughlin & Konolige

ADDRESS: 5575 Lovall Valley Road, Napa California

APN: 050-361-013-000

REFERENCES:

1. Napa County Road & Street Standards, by Napa County, Revised February 4, 2020.

PROJECT DESCRIPTION:

The subject parcel is located at 5575 Lovall Valley Road in Napa California. Existing onsite infrastructure consists of, gravel driveway, gravel parking area, barn, shed, and existing dirt road. The development under B19-00701 include existing common drive improvements, main residence, and a residential gravel driveway. The proposed development project under this permit includes a residential fire safe AC driveway to replace the existing dirt road. This road will serve as residential access to the future residential development on the Sonoma county side under separate future development. Topography of the area consists of moderate to steep slopes (10-50%) with most of the lot vegetated with native trees and grasses. This drainage analysis evaluates the potential drainage impacts of the proposed development under this permit.

EXISTING AND PROPOSED DRAINAGE PATTERN:

Runoff from the site sheet flows north-east across the subject parcel before converging at the existing unnamed blue line creek onsite (See attached watershed exhibit). Flow within the unnamed blue line creek eventually discharges to Huichica Creek. The proposed development includes rock lined swales along the proposed driveway and retaining walls and a culvert to discharge to the bioretention facility for treatment and retention. The discharge will then return to sheet flow towards the unnamed blue line creek onsite. The overall drainage pattern will remain unchanged from pre to post conditions with all runoff from the site converging at the unnamed blue line creek onsite and eventually converge with Huichica Creek.

DESIGN REQUIREMENTS:

The parcel lies within Napa County and is subject to BASMAA requirements (See associated Stormwater Control Plan). This analysis focuses strictly on the 10-year event sizing of the proposed improvements. BASMAA requirements are addressed within the Stormwater Control Plan.

EXISTING ON-SITE AND OFF-SITE CONDITIONS & IMPACTS OF DEVELOPMENT:

The drainage pattern at a regional scale remains unchanged from pre to post development conditions. The proposed bioretention facility will mitigate storm water level increases and pollutant increases projected for the development. (See Stormwater Control Plan)

DESIGN CRITERIA & ASSUMPTIONS:

This evaluation is based on the policies and procedures detailed in Napa County Road & Street Standards, Revised September 2017, issued by Napa County. The hydraulic design of the individual drainage improvements is based on the rational formula $(Q = C \mid A)$ and is based on the 10-year, 10-minute initial time of concentration



storm. A mean annual precipitation of 35 was used resulting in a 60-min rainfall of 1.10 inches. Volume capture and treatment requirements are addressed within associated Stormwater Control Plan. Minor landscape area drains were evaluated only for the worst case run within network. The worst-case pipe sizing and slope is then conservatively used throughout the network.

METHODOLOGIES USED:

Rational Formula calculations for the 10-year storm are included based on the composite runoff coefficients for each tributary for sizing of the individual drainage improvements. The calculation spreadsheets are attached with this submittal.

100 YEAR STORM IMPACT AND FLOODING CONCERNS:

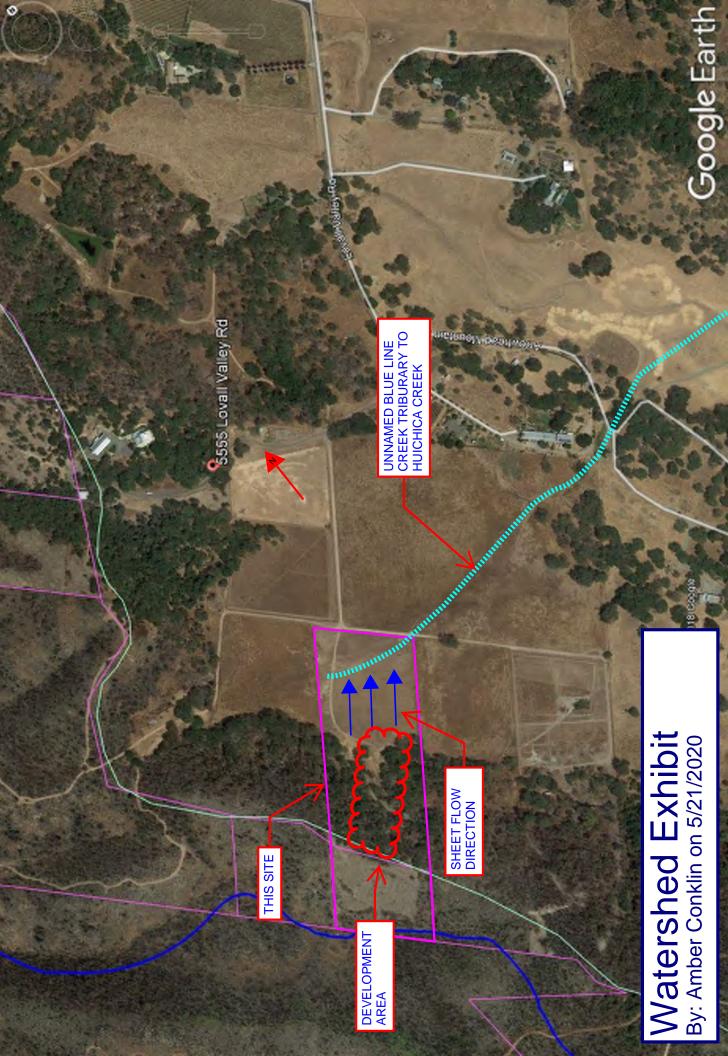
The parcel lies outside of the 100-year flood zone therefore flooding is not expected. A 100-year storm event would likely result in overflow of the culverts and swales and runoff returns to sheet flow downhill.

CONCLUSION:

The calculations and analysis provided herein is based upon the Napa County Road & Street Standards and generally accepted engineering principals. The proposed drainage improvements for the development have been sized to accommodate the 10-year storm event. Drainage network calculations are based on free flow and should be routinely inspected by the property owner.

ATTACHMENTS:

- Rational Method Spreadsheet with Composite Runoff Coefficient Calculations
- Swale and Pipe Hydraulic Calculations
- 10-Yr Post-Development Watershed Map



			2.60 Total Flow CFS				1.01 Total Flow CFS				0.06 Total Flow CFS
	Flow	Q (cfs)	2.60		Flow	Q (cfs)	1.01		Flow	Q (cfs)	0.00
		ΣΔΑС	1.00			ΣΔΑС	0.39			ΣΔΑС	0.02
		AAC	1.00			ΔAC	0.39			AAC	0.02
	Total Area	Ą	1.67		Total Area	٨	0.65		Total Area	Ą	90.0
		ΔΑ	1.67			ΔΑ	0.65			ΔΑ	90.0
	Runnoff Coefficient	C_comp	09:0		Runnoff Coefficient	C_comp	09.0		Runnoff Coefficient	C_comp	0.40
	Intensity	1	2.60		Intensity	1	2.60		Intensity	1	2.60
	centration	Total Time	10		centration	Total Time	10		centration	Total Time	10
	Time of Concentration	Travel Time (sec.)	INITIAL		Time of Concentration	Travel Time (sec.)	INITIAL		Time of Concentration	Travel Time (sec.)	INITIAL
35		Velocity fps		35		Velocity fps		35		Velocity fps	
ipitation		Length		ipitation		Length		ipitation		Length	
Mean Precipitation	ributary 1	Avg. Slope %		Mean Precipitation	ributary 2	Avg. Slope %		Mean Precipitation	ributary 3	Avg. Slope %	
10	Post-Development - Tributary 1	Area (ac.)	1.67	10	Post-Development - Tributary 2	Area (ac.)	0.65	10	Post-Development - Tributary 3	Area (ac.)	0.06
dnency	Post-1	Point of Conc.	POC 1	dnency	Post-1	Point of Conc.	POC 2	dnency	Post-	Point of Conc.	POC 3
Storm Frequency		Tributary	1	Storm Frequency		Tributary	2	Storm Frequency		Tributary	3

Ī			0.06 Total Flow CFS
	Flow	Q (cfs)	90.06
		ΣΔΑС	0.05
		ΔAC	0.05
	Total Area	А	90.0
		ΔΑ	90.0
	Runnoff Coefficient	C_comp	0.40
	Intensity	1	2.60
	centration	Total Time	10
	Time of Concentration	Travel Time (sec.)	INITIAL
35		Avg. Slope Length Velocity fps 7	
ipitation	Post-Development - Tributary 4	Length	
Mean Precipitation		Avg. Slope %	
10		Area (ac.)	90.0
equency	Post-L	Point of Conc.	POC 4
Storm Frequency		Tributary	4

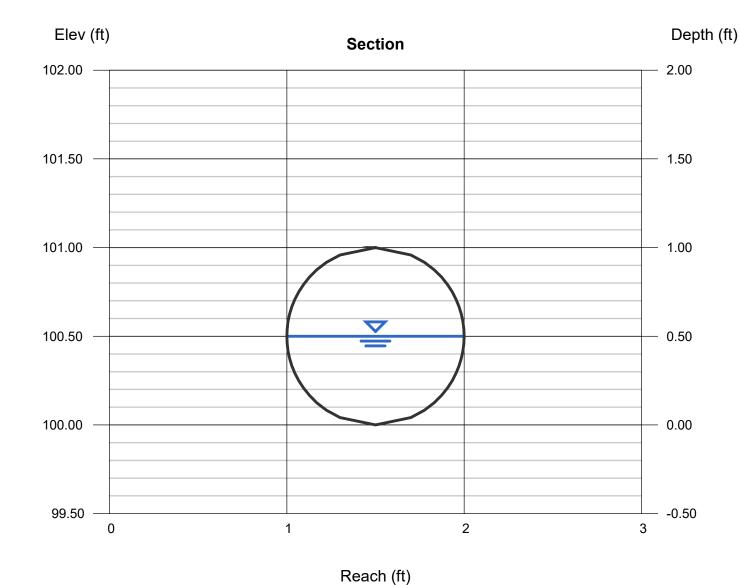
POC/	POC / Design	Tributaries Receiving	Total Q (cfs)
	6" SWALE	183	2.66
POC 1	9" SWALE	183	2.66
	12" PIPE	183	2.66
POC 2	6" SWALE	2	10.1
POC 3	6" SWALE	ဗ	90'0
1000	6" SWALE	1, 3, & 4	2.72
1	Hald "A	1384	62.6

Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

Thursday, May 28 2020

POC 1 - (P) 12 INCH PIPE

Circular		Highlighted	
Diameter (ft)	= 1.00	Depth (ft)	= 0.50
. ,		Q (cfs)	= 2.660
		Area (sqft)	= 0.39
Invert Elev (ft)	= 100.00	Velocity (ft/s)	= 6.74
Slope (%)	= 2.00	Wetted Perim (ft)	= 1.57
N-Value	= 0.012	Crit Depth, Yc (ft)	= 0.70
		Top Width (ft)	= 1.00
Calculations		EGL (ft)	= 1.21
Compute by:	Known Q		
Known Q (cfs)	= 2.66		



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Friday, May 29 2020

POC 1 - (P) 9 INCH ROCK LINED SWALE

Triangular
Side Slopes (z:1) = 2.00, 2.00
Total Depth (ft) = 0.75

Invert Elev (ft) = 100.00 Slope (%) = 5.00 N-Value = 0.035

Calculations

Compute by: Known Q Known Q (cfs) = 2.66

 Highlighted

 Depth (ft)
 = 0.59

 Q (cfs)
 = 2.660

 Area (sqft)
 = 0.70

 Velocity (ft/s)
 = 3.82

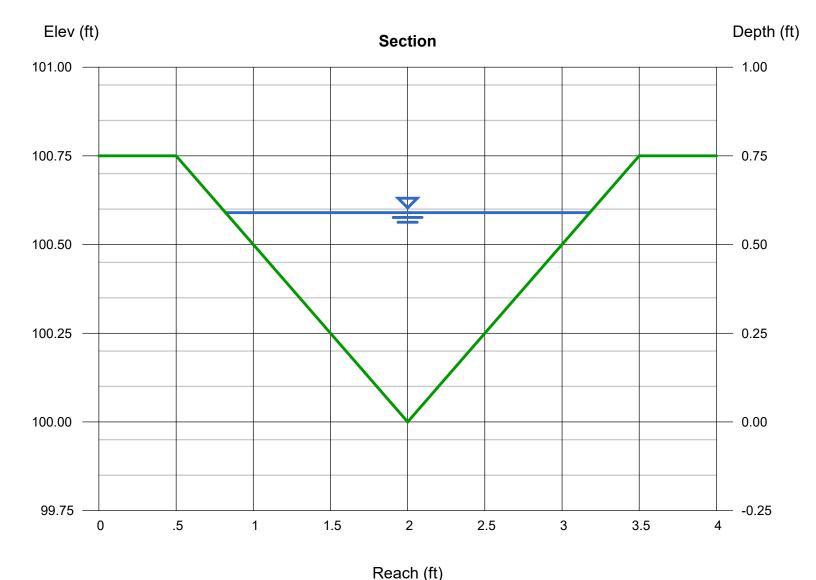
Velocity (ft/s) = 3.82

Wetted Perim (ft) = 2.64

Crit Depth, Yc (ft) = 0.65

Top Width (ft) = 2.36

EGL (ft) = 0.82



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= 0.035

Thursday, May 28 2020

POC 1 - (P) 6 INCH ROCK LINED SWALE

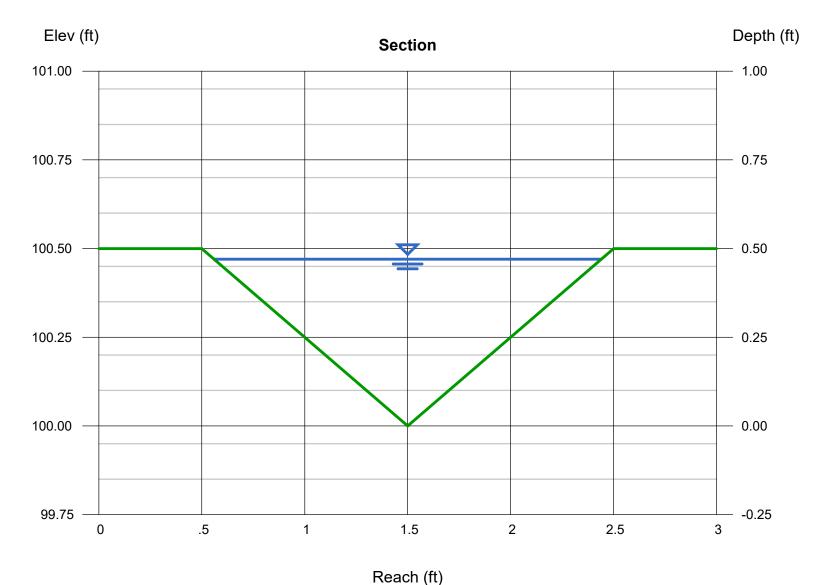
Side Slopes (z:1) Total Depth (ft)	= 2.00, 2.00 = 0.50
Invert Elev (ft)	= 100.00
Slope (%)	= 18.00

Calculations

N-Value

Compute by: Known Q Known Q (cfs) = 2.66

Highlighted		
Depth (ft)	=	0.47
Q (cfs)	=	2.660
Area (sqft)	=	0.44
Velocity (ft/s)	=	6.02
Wetted Perim (ft)	=	2.10
Crit Depth, Yc (ft)	=	0.50
Top Width (ft)	=	1.88
EGL (ft)	=	1.03



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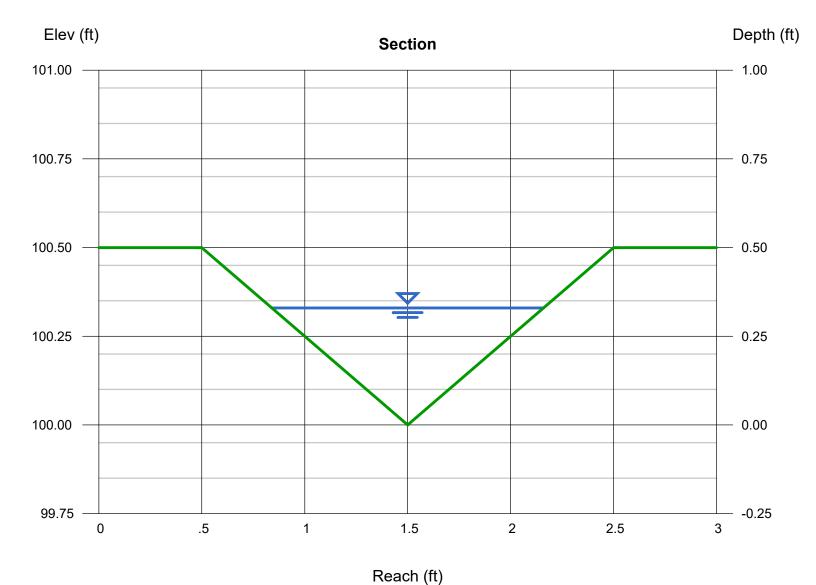
Wednesday, Jul 8 2020

POC 2 - (P) 6 INCH ROCK LINED SWALE

Triangular Side Slopes (z:1) Total Depth (ft)	= 2.00, 2.00 = 0.50
Invert Elev (ft)	= 100.00
Slope (%)	= 18.00
N-Value	= 0.035

Calculations	
Compute by:	Known Q
Known Q (cfs)	= 1.01

Highlighted	
Depth (ft)	= 0.33
Q (cfs)	= 1.010
Area (sqft)	= 0.22
Velocity (ft/s)	= 4.64
Wetted Perim (ft)	= 1.48
Crit Depth, Yc (ft)	= 0.44
Top Width (ft)	= 1.32
EGL (ft)	= 0.66



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Thursday, May 28 2020

POC 3 - (P) 6 INCH ROCK LINED SWALE

 Triangular

 Side Slopes (z:1)
 = 2.00, 2.00

 Total Depth (ft)
 = 0.50

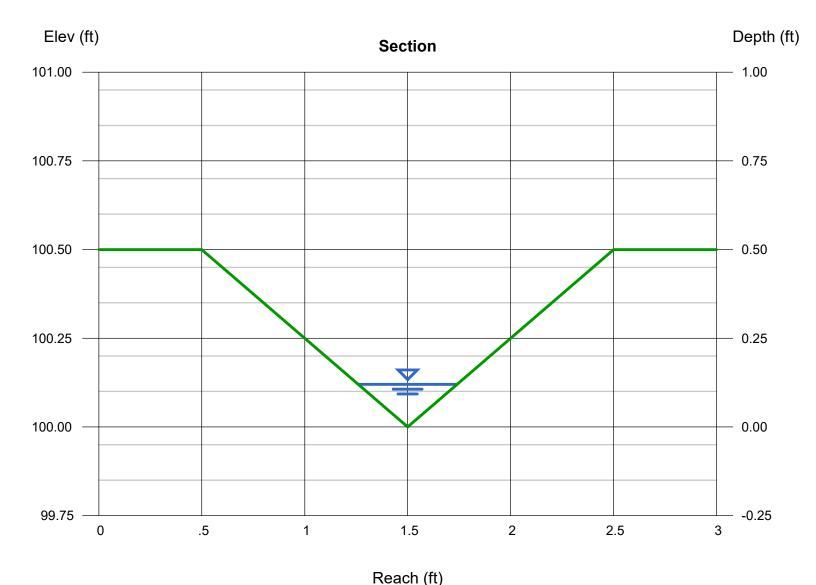
 Invert Elev (ft)
 = 100.00

Slope (%) = 100.00 N-Value = 0.035

Calculations

Compute by: Known Q Known Q (cfs) = 0.06

Highlighted = 0.12Depth (ft) Q (cfs) = 0.060Area (sqft) = 0.03Velocity (ft/s) = 2.08Wetted Perim (ft) = 0.54Crit Depth, Yc (ft) = 0.15Top Width (ft) = 0.48EGL (ft) = 0.19



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Wednesday, Jul 8 2020

POC 4 - (P) 6 INCH PIPE

Diameter (ft) $= 0.5$	0

Invert Elev (ft)	=	100.00
Slope (%)	=	5.00
N-Value	=	0.012

Calculations

Circular

Compute by: Known Q Known Q (cfs) = 1.15

Total flow: 2.72 cfs

Inlet will handle: 1.63 cfs Pipe will handle: 1.15 cfs Remaining flow: 1.57 cfs See next calculation

Depth (ft)	= 0.36
Q (cfs)	= 1.15
Area (sqft)	= 0.15

Highlighted

0 Velocity (ft/s) = 7.58Wetted Perim (ft) = 1.02Crit Depth, Yc (ft)
Top Width (ft) = 0.49= 0.45EGL (ft) = 1.25

Elev (ft) Section 101.00 — 100.75 — 100.50 -100.25 — 100.00 — 99.75 0 1

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Wednesday, Jul 8 2020

POC 4 - (P) 6 INCH ROCK LINED SWALE

 Triangular

 Side Slopes (z:1)
 = 2.00, 2.00

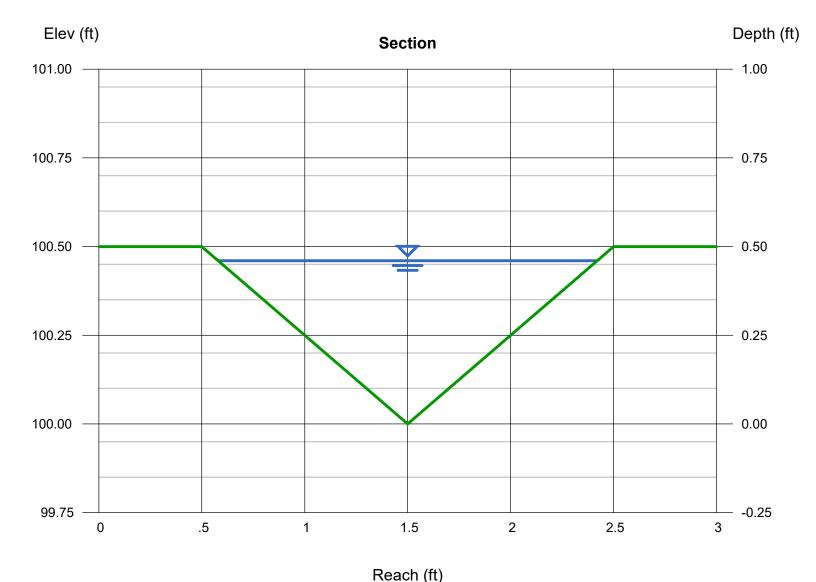
 Total Depth (ft)
 = 0.50

 Invert Elev (ft)
 = 100.00

Invert Elev (ft) = 100.00 Slope (%) = 7.00 N-Value = 0.035

Calculations

Compute by: Known Q Known Q (cfs) = 1.57 Highlighted Depth (ft) = 0.46Q (cfs) = 1.570Area (sqft) = 0.42Velocity (ft/s) = 3.71Wetted Perim (ft) = 2.06Crit Depth, Yc (ft) = 0.50Top Width (ft) = 1.84EGL (ft) = 0.67





18" CATCH BASIN

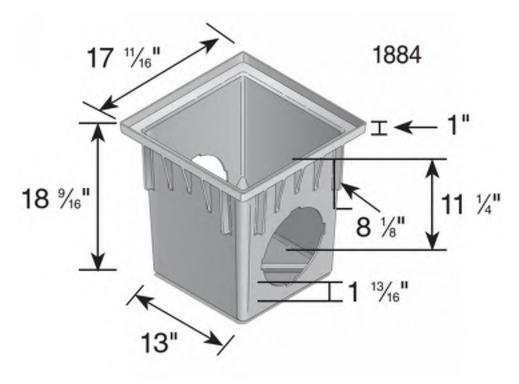
Part #: 1882, 1884

18" Catch Basin

Grate Number(s)	Description	Flow Rate with ½" Head
1810, 1811, 1812	18" x 18" Square Grate	264.03 GPM
1813	18" x 18" Cast Iron Square Grate	338.65 GPM
(181 5)	18" Square Galvanized Steel Grate	731.13 GPM
1881, 1891	18" x 18" Atrium Grate	273.49 GPM

OUTLET FLOW CAPACITIES

Part #	Flow Rate per Outlet	
1242, 1243	102.50 GPM	
(with reducer ring)		
1245	Top: 97.53 GPM	
(with reducer ring)	Middle: 103.88 GPM	
	Bottom: 107.24 GPM	
1266	349.48 GPM	
(with reducer ring)		
1888	439.80 GPM	
1889	336.87 GPM	



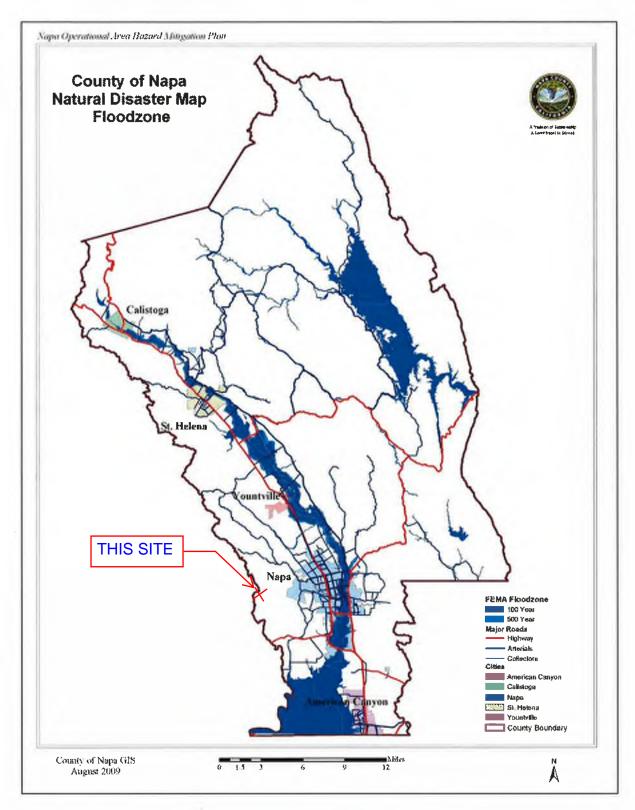
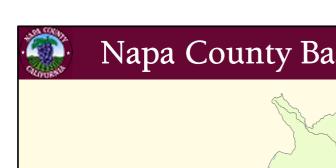
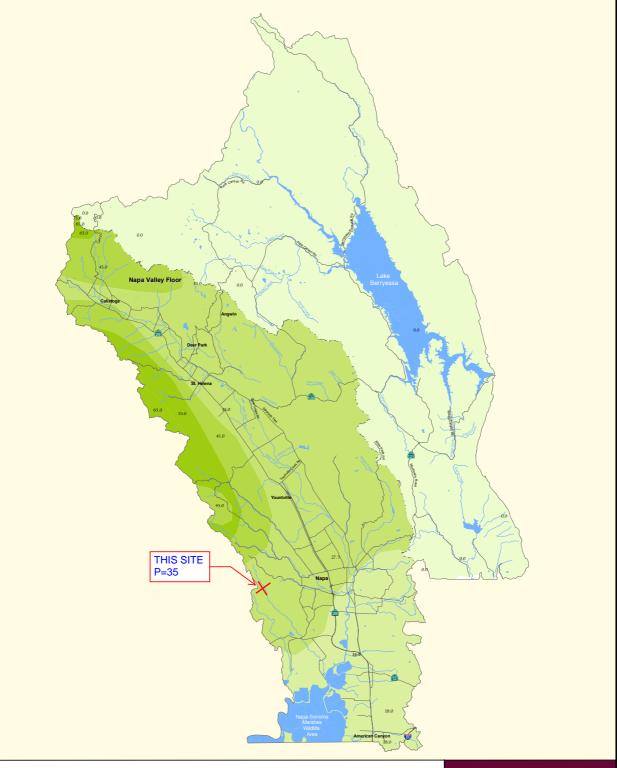
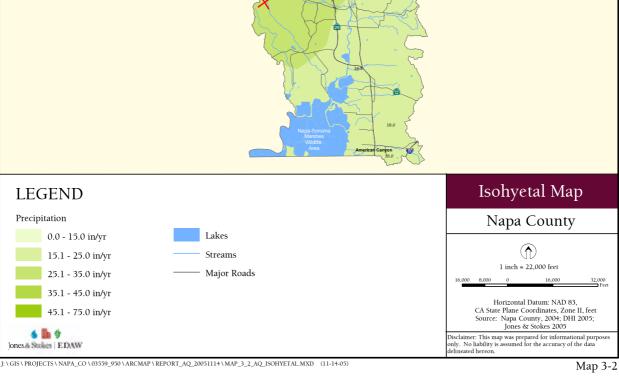


Figure 2-15: Napa County Flood Zone Map

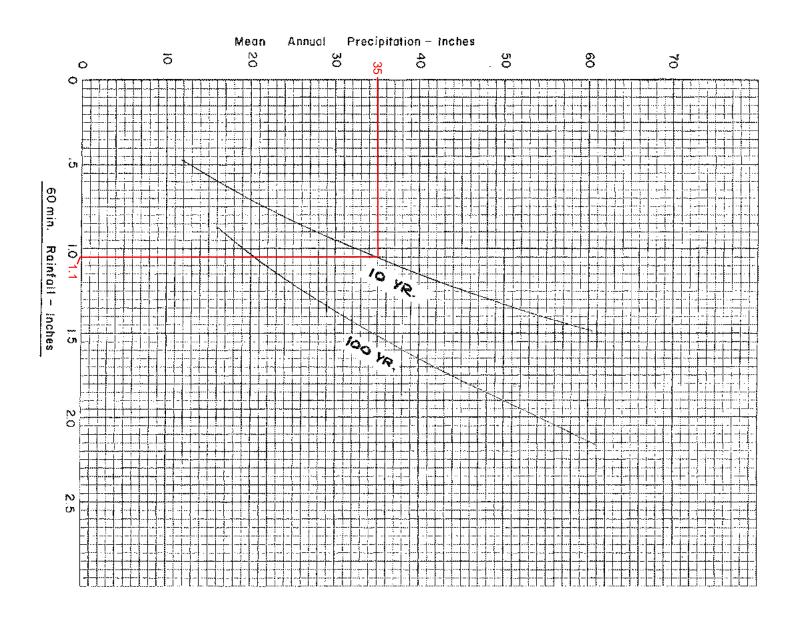


Napa County Baseline Data Report

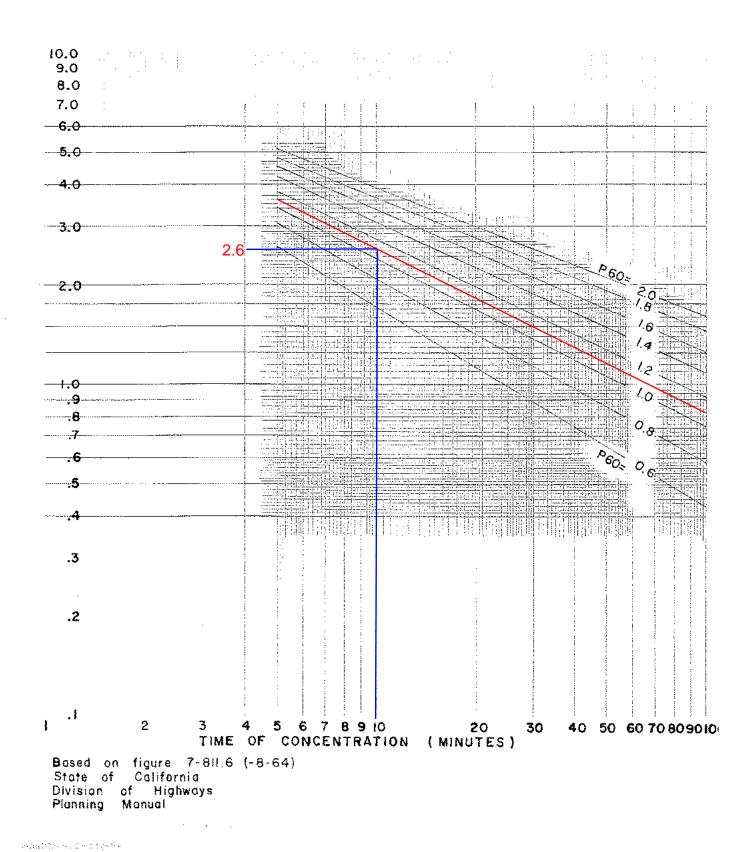




MEAN ANNUAL PRECIPITATION VS. 60 MINUTE RAINFALL



INTENSITY – DURATION CHART



RUNOFF COEFFICIENT FOR DEVELOPED AREAS

Type of Davidonment	Coefficient	
Type of Development	Mild Slope	Steep Slope
Low Density Residential 1-3 Units/Acre	0.40	0.60
Medium Density Residential 4-9 Units/Acre	0.45	0.65
High Density Residential 10 or more Units/Acre	0.60	0.75
Limited Industrial	0.60	0.80
Industrial	0.75	0.90
Commercial	0.80	0.90
Schools	0.45	0.65
Parks	0.25	0.50

FIGURE 3.1

UNLINED CHANNEL VELOCITY

Recommended Permissible Velocities for Unlined Channels

Types of Material in Everyation Costion	Permissible Velocity (FT/Sec)			
Types of Material in Excavation Section	Intermittent Flow	Sustained Flow		
Fine Sand (Noncolloidal)	2.5	2.5		
Sandy Loam (Noncolloidal)	2.5	2.5		
Silt Loam (Noncolloidal)	3.0	3.0		
Fin Loam	3.5	3.5		
Volcanic Ash	4.0	3.5		
Fine Gravel	5.0	4.0		
Stiff Clay (Colloidal)	6.0	4.5		
Graded Material (Noncolloidal)				
Loam to Gravel	6.5	5.0		
Silt to Gravel	7.0	5.5		
Gravel	7.5	6.0		
Coarse Gravel	8.0	6.5		
Gravel to Cobbles (Under 6 inches)	9.0	7.0		
Gravel to Cobbles (Under 8 inches)	10.0	8.0		

FIGURE 5