FOR REVIEW ONLY

First Harley Knox DPR 20-00014 City of Perris, Riverside County, California

Preliminary Drainage Study

Prepared for: First Industrial Realty Trust 898 N. Sepulveda Boulevard, Suite 175 El Segundo, CA 90245



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PERRIS VALLEY MDP LAT D-3A PLANS



SECTION 1 - SUMMARY

PURPOSE

The purpose of this report is to document the hydrologic and hydraulic analyses performed in support of the First Harley Knox logistics project located in the City of Perris, County of Riverside, California. The project site is located at the northwest corner of Harley Knox Boulevard and Redlands Ave. The project is bounded by Oleander Ave to the north, existing light industrial complex to the west, Harley Knox Boulevard to the south, and the Redlands Avenue to the east. The project proposes to build an industrial warehouse on approximately 9.5 acres. This report will summarize the hydrologic and hydraulic analyses that were conducted in order to determine the necessary drainage improvements required to provide flood protection for the proposed building and safely convey the runoff through the site.

The scope of this report will include the following:

- Determine the peak 100-year and 10-year flow rates for the developed condition using the Riverside County Flood Control and Water Conservation District (RCFC&WCD) Rational Method.
- Determine the required storm drain facilities, alignment, and sizes required to flood protect the project site.
- Determine the necessary underground storage area and volume required for water quality treatment and to mitigate for increases in runoff.
- Preparation of a preliminary report summarizing the hydrology and hydraulic results.

DESCRIPTION OF WATERSHED

The project is proposing an industrial warehouse (approximately 158,550square feet) on approximately 9.5 acres of vacant land. Existing elevations across the site vary from 1459 at the northwest corner to 1458 at the southeast corner (NAVD88 Datum). The site currently slopes down at approximately 0.3% to the southeast corner. The existing drainage pattern for the site and the general area is characterized by sheet flow that currently flows to Harley Knox Boulevard. Flows are captured by an existing catch basin located on the north side of Harley Knox Boulevard and then conveyed within the existing Lat D-3A-4 towards the Perris Valley Storm Drain Channel.

PROPOSED CONDITIONS

The project site is not impacted by off-site flows as there are existing streets around the perimeter of the project that convey any offsite flow away from the site. The balanced earthwork does not allow for conventional gravity storm drains due to lack of drop across the site from the south to the north. In order to convey on-site flows, the project will utilize subsurface storm drain to discharge into underground storage chambers. The chambers are located at the east side of the auto parking stalls along Redlands Avenue and they are sized to hold only the water quality design capture volume for the project. Large flows will be forced out of the chambers at an outlet above the chamber soffit and gravity flow to the existing 48" storm drain line (Lat D-3A) at Harley Knox Boulevard. Water quality runoff will be pumped from the chambers into a Contech Filterra unit.



METHODOLOGY

HYDROLOGY

Hydrologic calculations were performed in accordance with the RCFC&WCD Hydrology Manual, dated April 1978. The Rational Method was utilized in determining peak flow rates.

The hydrological parameters, including rainfall values and soil types were derived from the RCFC&WCD Hydrology Manual. The isohyetal maps and soil map have been included in Section 2.

Rational Method calculations were performed using a computer program developed by CivilDesign Corporation and Joseph E. Bonadiman and Associates Inc. The computer program is commonly referred to as CivilD which incorporates the hydrological parameters outlined in the RCFC&WCD Hydrology Manual.

The Rational Method was used to determine the peak flow rates to size and design the drainage facilities need to convey onsite flows through the site to the proposed basin. The flow rates were computed by generating a hydrologic "link-node" model in which the overall area is divided into separate drainage sub-areas, each tributary to a concentration point (node) determined by the proposed layout and grading.

The Unit Hydrograph Method was used to determine the peak flow rates and volumes associated with the 100-year storm events for the site. Calculations were performed for both the existing condition and developed condition to be used in the analysis of the proposed basin. See Section 2 for additional information and results regarding the hydrologic analyses performed for this project.

HYDRAULICS

Water quality basin calculations were performed using spreadsheets that were created by RCFC&WCD. preliminary calculations and additional details can be found in the preliminary-WQMP.

Basin routing calculations were performed using the CivilD computer program. The CivilD program utilizes the Modified-Puls methodology to routes unit hydrographs through a basin using the stage-storage and stage-discharge curves determined from the proposed basin design. See Section 3 for additional discussion and results.

Hydraulic calculations to determine the required pipe sizes of the proposed onsite storm drain facilities will be provided in the Final Drainage Study.



First Industrial Realty Trust

Preliminary Drainage Study – April, 2021

Section 1 First Industrial – Harley Knox

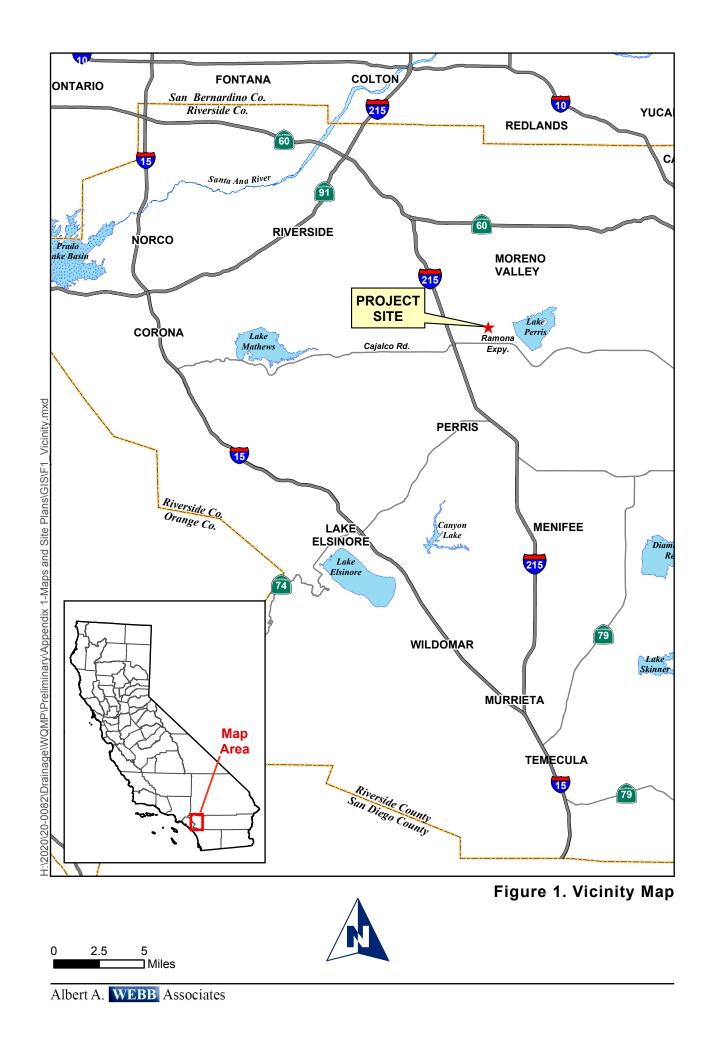
FIG. 1 VICINITY MAP

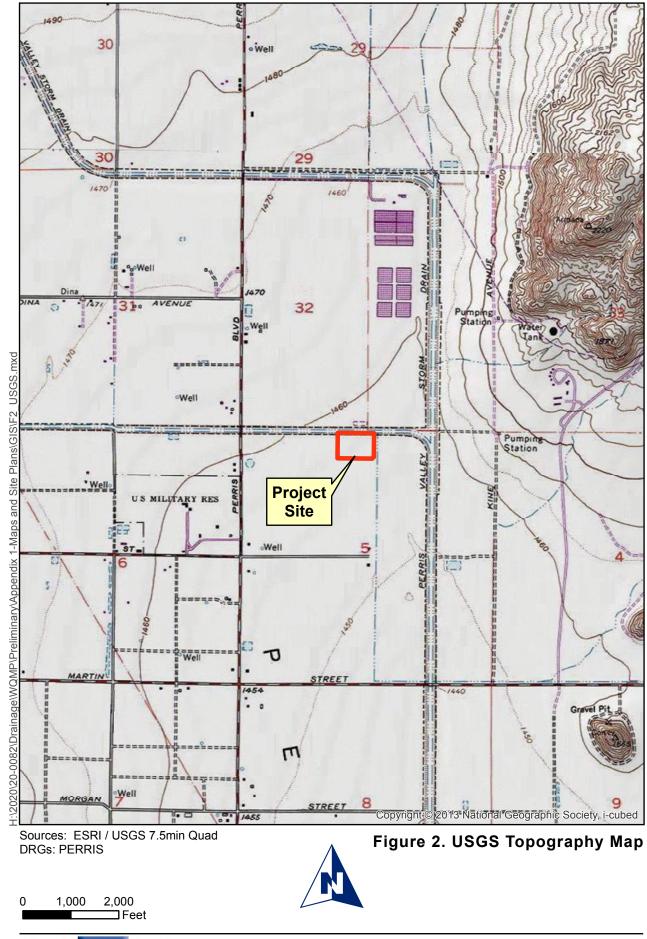
FIG. 2 USGS TOPOGRAPHY MAP

FIG. 3 AERIAL PHOTOGRAPH

FIG. 4 RECEIVING WATERBODIES

FIG. 5 SOILS MAP





Albert A. WEBB Associates

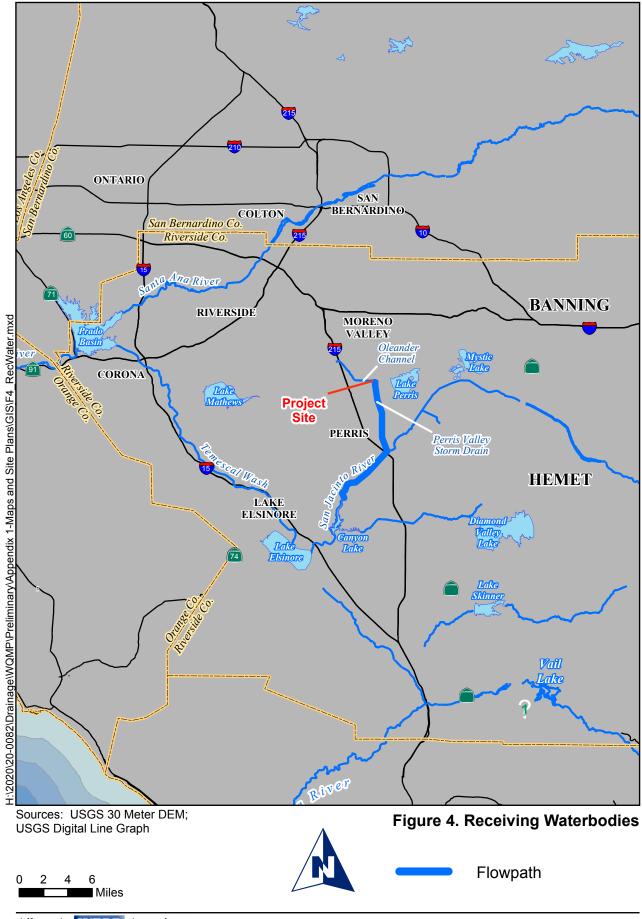




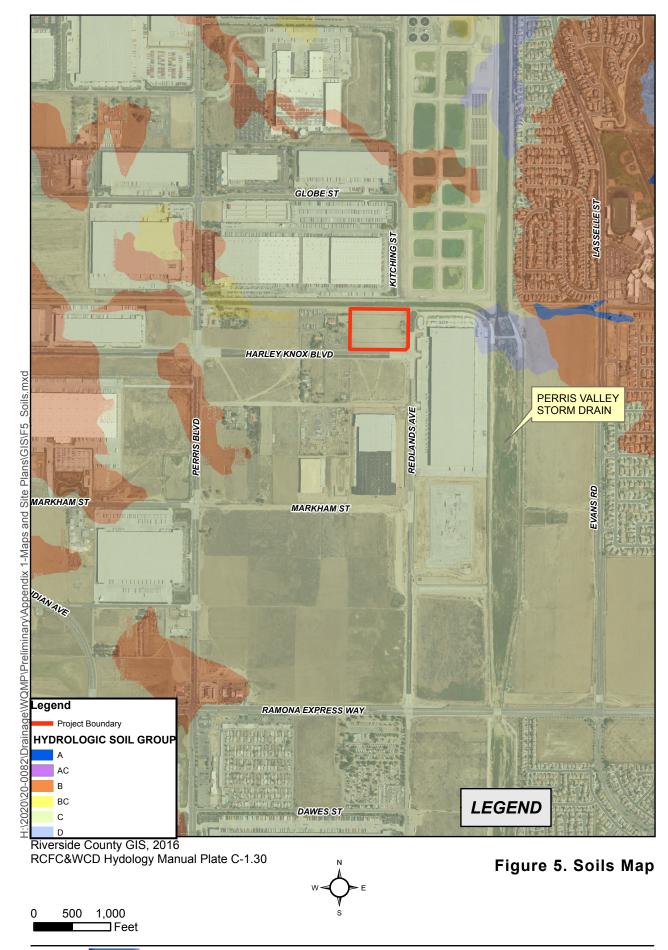
Figure 3. Aerial Photograph

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Albert A. WEBB Associates







Albert A. WEBB Associates

SECTION 2 - HYDROLOGY ANALYSIS

HYDROLOGY PARAMETERS

The RCFC&WCD Hydrology Manual was used to determine several of the hydrological parameters. The following rainfall depths were utilized in the hydrology analyses, which were obtained from the isohyetal maps provided in the RCFC&WCD Hydrology Manual:

	Duration	
Storm Event	1-Hour (inches)	
10-Year	0.78	
100-Year	1.12	

Table 1 –	Precipitation	Values
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The value for slope of intensity was determined to be 0.49. The isohyetal maps have been included in Appendix A.

Based on the Plate C-1.30 (Perris) in the RCFC&WCD Hydrology Manual, the project site is classified as soil type C. The soils map is included in Appendix A.

The residential\commercial landscaping cover type was used to represent the developed condition. Table 2 below summarizes the runoff index values and the recommended values for percentage of impervious cover for each category:

Cover Type	Soil Group A	Soil Group B	Soil Group C	Soil Group D	Percentage of Impervious Cover
Commercial Landscaping	32	56	69	75	90%

Fable 2 – (Cover	Гуре
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ON-SITE RATIONAL METHOD HYDROLOGY

The rational method was used to determine peak flow rates in order to adequately size the proposed subsurface storm drains and associated inlets used to convey on-site flows to the proposed underground storage chambers. The project site was separated into four subareas. Subarea 1 (5.6 acres) is essentially the northerly half of the site and is tributary to inlet 102. Subarea 2 (0.9 acres) is the northernly half of the eastern parking area and is tributary to inlet 202. Subarea 3 (0.3 acres) is the southernly half of the eastern parking area and is tributary to inlet 302. Subarea 4 (2.4 acres) is the southerly half of the site and is tributary to inlet 302. Subarea 4 (2.4 acres) is the southerly half of the site and is tributary to inlet 402. The project is comprised of approximately 15% pervious cover (landscaping). The project was modeled as commercial land use which assumes a 10% pervious cover which is slightly more conservative than what is proposed. As previously described, the underground storage chambers will utilize an outlet structure where high flow will gravity feed to the existing Lat D-3A line located in

Harley Knox Boulevard. Low flows from the underground storage chambers will discharge to a Contech Filterra unit for water quality treatment.

The rational method was used to determine peak flow rates in order to adequately size the proposed subsurface storm drains and associated inlets used to convey on-site flows through the site and into the existing Lat D-3A storm drain. The project site area was divided into 4 subareas.

Area-1 (approximately 5.6 acres) surface flows into a trench drain along the truck docking stalls. A 100-year peak flow of 14.3 cfs is generated by this subarea. The runoff will be conveyed around the building towards Area-2 using Line-A.

Area-2 (approximately 0.9 acres) surface flows into 1 low point on the east side of the project. A 100-year peak flow of 2.3 cfs is generated by this subarea. The runoff will be conveyed towards the underground storage chambers using Lat A-1.

Area-3 (approximately 0.3 acres) surface flows into 1 low point on the east side of the project. A 100-year peak flow of 1.0 cfs is generated by this subarea. The runoff will be conveyed towards the underground storage chambers using Lat A-2.

Area-4 (approximately 2.4 acres) surface flows into several low points on the south side of the project. A 100-year peak flow of 8.0 cfs is generated by this subarea. The runoff will be conveyed towards the underground storage chambers using Line-B.

A peak 100 year flow rate of 23.7 cfs is generated by the site, including the off-site areas and underground storage area. An emergency escape route will be provided capable of bypassing the peak 100 year flow rate.

The following table summarizes the rational method results at key points:

Point of Interest	10-Year Peak Flow Rate (cfs)	100-Year Peak Flow Rate (cfs)
Node 102 – Flow tributary to proposed inlet and Line A	9.9	14.3
Node 103 – Total Flow tributary to line A	16.4	23.7
Node 202 – Flow tributary to proposed inlet and Lat A-1	1.6	2.3
Node 203 – Total Flow tributary to Lat A-1	16.4	23.7
Node 302 – Flow tributary to proposed inlet and Lat A-2	0.7	1.0
Node 303 – Total Flow tributary to Lat A-2	16.4	23.7
Node 402 – Flow tributary to proposed inlet and Line B	5.8	8.0
Node 403 – Total Flow tributary to Line B	16.4	23.7

Table 3 - Rational Method Results

The rational method output files and hydrology map have been included in Appendix A.



SECTION 3 - HYDRAULIC ANALYSIS

ON-SITE STORM DRAIN FACILITIES

The project proposes minimal subsurface storm drain and will utilize curb and gutter and ribbon gutters to convey onsite high flows to the proposed underground storage chamber. The proposed underground storage chambers will receive the runoff generated by 9.5 acres of the site primarily on the easterly side of the site for water quality treatment.

The project proposes one subsurface storm drain system to convey on-site flows. The runoff will discharge into the underground storage chambers. The discharge from the underground storage chambers will be conveyed to a pump facility where it will outflow for water quality purposes. High flows discharged from the underground storage chambers will gravity flow to the existing Line D-3A located in Harley Knox Boulevard.

A brief summary of each system has been provided and the results of the hydraulic analyses are included at the end of the section. The peak flow rates determined during the 100-year rational method on-site hydrology analysis were utilized to evaluate the proposed storm drain systems.

Line-A (Onsite)

The north portion of the project site will surface flow to a trench drain along the truck docking stalls and be collected by Line A-1, a 24" HDPE pipe. Line-A proposes to convey the 100-year peak flow rate to the underground storage chamber. A hydraulic model for Line A-1 will be provided during final engineering to further assess the storm drain design.

Line-B (Onsite)

The south portion of the project site will surface flow to several low points in the south side landscaping area and be collected by Line B-1, a 24" HDPE pipe. Line-B proposes to convey the 100-year peak flow rate to the underground storage chamber. A hydraulic model for Line B-1 will be provided during final engineering to further assess the storm drain design.

OFF-SITE STORM DRAIN FACILITIES

As part of this project, the only offsite improvements proposed for Harley Knox Blvd include the construction of a driveway and sidewalk along the project frontage. There is an existing low point (Lat D-3A-4), within Harley Knox Boulevard. A 30" RCP offsite storm drain connection is proposed to convey all collected, onsite flows towards the existing 48" RCP lateral D-3A located along Harley Knox Boulevard. A peak flow rate of 21.1 cfs is expected per the rational method analysis (See Section 2 and Appendix A for more detail).



SECTION 4 - CONCLUSION

Based on the analyses and results of this report, the following conclusions were derived from the hydrology and hydraulic results:

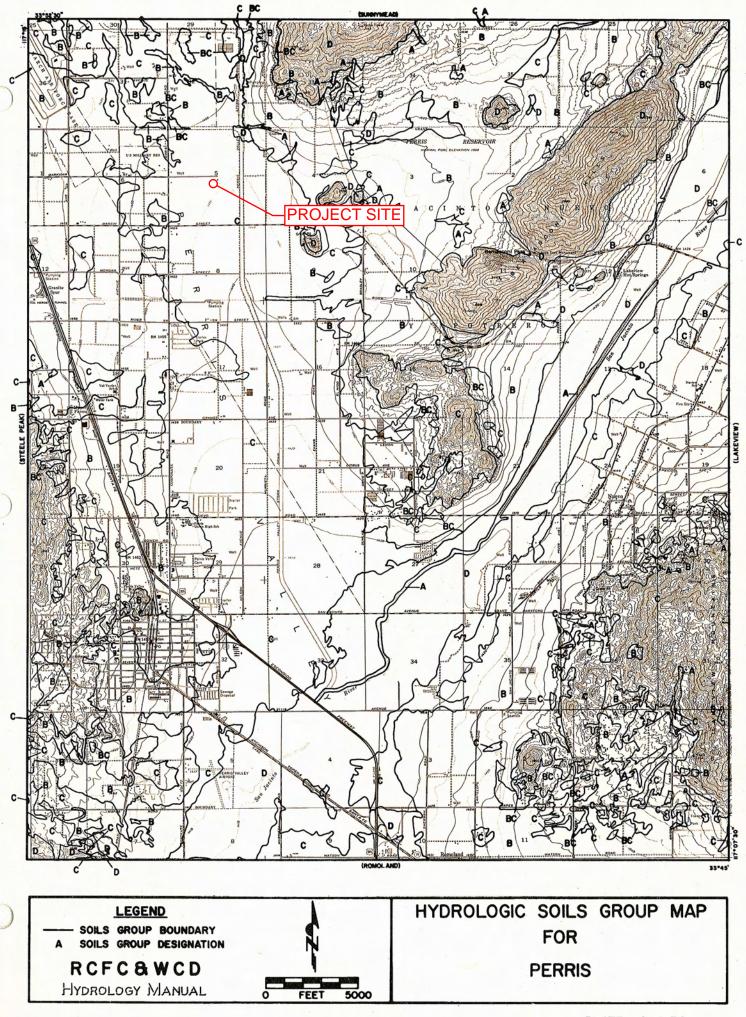
- The proposed drainage improvements will adequately convey flows to the underground storage chambers and provide flood protection for the 100-year storm event.
- The proposed Contech Filterra unit will provide adequate water quality treatment.
- The proposed project will not impact flooding condition to upstream or downstream properties.

APPENDIX A – HYDROLOGY



HYDROLOGIC SOILS GROUP MAP (PLATE C-1.30)





ISOHYETAL MAPS



RCF Hydro	MIRA LONA	MURRIETA - TEMECULA & Rancho California	NORCO	PALM SPRINGS	PERRIS VALLEY
RCFC 8	DURATION FREQUENCY MINUTES 10 100 YEAR YEAR	DURATION FREQUENCY MINUTES 10 100 YEAR YEAR	DURATION FREQUENCY MINUTES 10 100 YEAR YEAR	DURATION FREQUENCY MINUTES 10 100 YEAR YEAR	DURATION FREQUENCY MINUTES 10 100 YEAR YEAR
MA,	5 2.84 4.48 6 2.58 4.07 7 2.37 3.75 8 2.21 3.49 9 2.08 3.28	5 3.45 5.10 6 3.12 4.61 7 2.87 4.24 8 2.67 3.94 9 2.50 3.69	5 2.77 4.16 6 2.53 3.79 7 2.34 3.51 8 2.19 3.29 9 2.07 3.10	5 4.23 6.76 6 3.80 6.08 7 3.48 5.56 8 3.22 5.15 9 3.01 4.81	5 2.64 3.78 6 2.41 3.46 7 2.24 3.21 8 2.09 3.01 9 1.98 2.84
NUAL	10 1.96 3.10 11 1.87 2.95 12 1.78 2.82 13 1.71 2.70 14 1.64 2.60	10 2.36 3.48 11 2.24 3.30 12 2.13 3.15 13 2.04 3.01 14 1.96 2.89	10 1.96 2.94 11 1.87 2.80 12 1.79 2.68 13 1.72 2.58 14 1.66 2.48	10 2.83 4.52 11 2.67 4.28 12 2.54 4.07 13 2.43 3.88 14 2.33 3.72	10 1.88 2.69 11 1.79 2.57 12 1.72 2.46 13 1.65 2.37 14 1.59 2.29
	15 1.58 2.50 16 1.53 2.42 17 1.48 2.34 18 1.44 2.27 19 1.40 2.21	15 1.89 2.79 16 1.82 2.69 17 1.76 2.60 18 1.71 2.52 19 1.66 2.45	15 1.60 2.40 16 1.55 2.32 17 1.50 2.25 18 1.46 2.19 19 1.42 2.13	15 2.23 3.58 16 2.15 3.44 17 2.08 3.32 18 2.01 3.22 19 1.95 3.12	15 1.54 2.21 16 1.49 2.14 17 1.45 2.08 18 1.41 2.02 19 1.37 1.97
	20 1.36 2.15 22 1.29 2.04 24 1.24 1.95 26 1.18 1.87 28 1.14 1.80	20 1.61 2.38 22 1.53 2.26 24 1.46 2.15 26 1.39 2.06 28 1.34 1.98	20 1.39 2.08 22 1.32 1.98 24 1.26 1.90 26 1.22 1.82 28 1.17 1.76	20 1.89 3.03 22 1.79 2.86 24 1.70 2.72 26 1.62 2.60 28 1.56 2.49	20 1.34 1.92 22 1.28 1.83 24 1.22 1.75 26 1.18 1.69 28 1.13 1.63
	30 1.10 1.73 32 1.06 1.67 34 1.03 1.62 36 1.00 1.57 38 .97 1.53	30 1.29 1.90 32 1.24 1.84 34 1.20 1.78 36 1.17 1.72 38 1.13 1.67	30 1.13 1.70 32 1.10 1.64 34 1.06 1.59 36 1.03 1.55 38 1.01 1.51	30 1.49 2.39 32 1.44 2.30 34 1.39 2.22 36 1.34 2.15 38 1.30 2.09	30 1.10 1.57 32 1.06 1.52 34 1.03 1.48 36 1.00 1.44 38 .98 1.40
STANDARD INTENSITY - DUR CURVES DA	40 .94 1.49 45 .89 1.40 50 .84 1.32 55 .80 1.26 60 .76 1.20	40 1.10 1.62 45 1.03 1.52 50 .97 1.44 55 .92 1.36 60 .88 1.30	40 .98 1.47 45 .92 1.39 50 .88 1.31 55 .84 1.25 60 .80 1.20	40 1.27 2.02 45 1.18 1.89 50 1.11 1.78 55 1.05 1.68 60 1.00 1.60	40 .95 1.37 45 .90 1.29 50 .85 1.22 55 .81 1.17 60 .78 1.12
DARD - DURATION DATA	65 .73 1.15 70 .70 1.11 75 .68 1.07 80 .65 1.03 85 .63 1.00	65 .84 1.24 70 .81 1.19 75 .78 1.15 80 .75 1.11 85 .73 1.07	65 .77 1.15 70 .74 1.11 75 .72 1.07 80 .69 1.04 85 .67 1.01	65 .95 1.53 70 .91 1.46 75 .88 1.41 80 .85 1.35 85 .82 1.31	65 .75 1.08 70 .72 1.04 75 .70 1.00 80 .68 .97 85 .66 .94
ION	SLOPE ≭ . 530	SLOPE = .550	SLOPE = .500	SLOPE = .580	SLOPE = •490

PLATE D-4.1 (4 of 6)

10-YEAR ONSITE HYDROLOGY (RATIONAL METHOD)



Riverside County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software, (c) 1989 - 2004 Version 7.0 Rational Hydrology Study Date: 08/12/21 File:prop10.out 20-0082 - FIR HK ONSITE RATIONAL METHOD HYDROLOGY 10 YEAR STORM EVENT FN: PROP10.OUT RC _____ ******* Hydrology Study Control Information ********* English (in-lb) Units used in input data file Program License Serial Number 4010 _____ Rational Method Hydrology Program based on Riverside County Flood Control & Water Conservation District 1978 hydrology manual Storm event (year) = 10.00 Antecedent Moisture Condition = 2 Standard intensity-duration curves data (Plate D-4.1) For the [Perris Valley] area used. 10 year storm 10 minute intensity = 1.880(In/Hr) 10 year storm 60 minute intensity = 0.780(In/Hr)100 year storm 10 minute intensity = 2.690(In/Hr) 100 year storm 60 minute intensity = 1.120(In/Hr) Storm event year = 10.0Calculated rainfall intensity data: 1 hour intensity = 0.780(In/Hr)Slope of intensity duration curve = 0.4900 Process from Point/Station 101.000 to Point/Station 102.000 **** INITIAL AREA EVALUATION **** Initial area flow distance = 363.000(Ft.) Top (of initial area) elevation = 1459.100(Ft.) Bottom (of initial area) elevation = 1456.800(Ft.)

```
Difference in elevation = 2.300(Ft.)
Slope = 0.00634 s(percent)=
                                0.63
TC = k(0.300)*[(length^3)/(elevation change)]^{0.2}
Initial area time of concentration = 8.724 min.
Rainfall intensity =
                      2.006(In/Hr) for a 10.0 year storm
COMMERCIAL subarea type
Runoff Coefficient = 0.879
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2) = 69.00
Pervious area fraction = 0.100; Impervious fraction = 0.900
                        9.880(CFS)
Initial subarea runoff =
Total initial stream area =
                              5.600(Ac.)
Pervious area fraction = 0.100
Process from Point/Station
                           102.000 to Point/Station
                                                     103.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
Upstream point/station elevation = 1451.900(Ft.)
Downstream point/station elevation = 1450.300(Ft.)
Pipe length = 512.00(Ft.) Manning's N = 0.012
No. of pipes = 1 Required pipe flow = 9.880(CFS)
Nearest computed pipe diameter = 21.00(In.)
Calculated individual pipe flow = 9.880(CFS)
Normal flow depth in pipe = 17.81(In.)
Flow top width inside pipe = 15.07(In.)
Critical Depth = 14.04(In.)
Pipe flow velocity = 4.54(Ft/s)
Travel time through pipe = 1.88 min.
Time of concentration (TC) = 10.60 min.
Process from Point/Station 102.000 to Point/Station
                                                     103.000
**** CONFLUENCE OF MINOR STREAMS ****
Along Main Stream number: 1 in normal stream number 1
Stream flow area = 5.600(Ac.)
Runoff from this stream =
                          9.880(CFS)
Time of concentration = 10.60 min.
Rainfall intensity = 1.823(In/Hr)
Process from Point/Station
                           201.000 to Point/Station
                                                     202.000
**** INITIAL AREA EVALUATION ****
```

```
Initial area flow distance =
                            395.000(Ft.)
Top (of initial area) elevation = 1460.100(Ft.)
Bottom (of initial area) elevation = 1457.400(Ft.)
Difference in elevation =
                           2.700(Ft.)
Slope =
         0.00684 s(percent)=
                                  0.68
TC = k(0.300)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =
                                    8.888 min.
Rainfall intensity =
                       1.988(In/Hr) for a
                                           10.0 year storm
COMMERCIAL subarea type
Runoff Coefficient = 0.879
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2) = 69.00
Pervious area fraction = 0.100; Impervious fraction = 0.900
Initial subarea runoff =
                           1.573(CFS)
Total initial stream area =
                               0.900(Ac.)
Pervious area fraction = 0.100
Process from Point/Station
                             202.000 to Point/Station
                                                        203.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
Upstream point/station elevation = 1451.800(Ft.)
Downstream point/station elevation = 1451.500(Ft.)
Pipe length =
                29.00(Ft.)
                            Manning's N = 0.012
No. of pipes = 1 Required pipe flow =
                                        1.573(CFS)
Nearest computed pipe diameter =
                                   9.00(In.)
Calculated individual pipe flow =
                                   1.573(CFS)
Normal flow depth in pipe =
                            6.45(In.)
Flow top width inside pipe =
                             8.11(In.)
Critical Depth = 6.93(In.)
Pipe flow velocity =
                       4.64(Ft/s)
Travel time through pipe = 0.10 min.
Time of concentration (TC) =
                            8.99 min.
Process from Point/Station
                             202.000 to Point/Station
                                                        203.000
**** CONFLUENCE OF MINOR STREAMS ****
Along Main Stream number: 1 in normal stream number 2
Stream flow area =
                     0.900(Ac.)
Runoff from this stream =
                            1.573(CFS)
Time of concentration =
                        8.99 min.
Rainfall intensity = 1.977(In/Hr)
```

```
Initial area flow distance = 120.000(Ft.)
Top (of initial area) elevation = 1461.000(Ft.)
Bottom (of initial area) elevation = 1458.600(Ft.)
Difference in elevation =
                           2.400(Ft.)
          0.02000 s(percent)=
                                   2.00
Slope =
TC = k(0.300)*[(length^3)/(elevation change)]^{0.2}
Warning: TC computed to be less than 5 min.; program is assuming the
time of concentration is 5 minutes.
Initial area time of concentration =
                                    5.000 min.
Rainfall intensity =
                        2.636(In/Hr) for a 10.0 year storm
COMMERCIAL subarea type
Runoff Coefficient = 0.883
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2) = 69.00
Pervious area fraction = 0.100; Impervious fraction = 0.900
Initial subarea runoff =
                           0.698(CFS)
Total initial stream area =
                                0.300(Ac.)
Pervious area fraction = 0.100
Process from Point/Station 302.000 to Point/Station
                                                         303.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
Upstream point/station elevation = 1451.800(Ft.)
```

```
Downstream point/station elevation = 1451.500(Ft.)
Pipe length = 41.00(Ft.) Manning's N = 0.012
No. of pipes = 1 Required pipe flow = 0.698(CFS)
Nearest computed pipe diameter =
                                  9.00(In.)
Calculated individual pipe flow =
                                    0.698(CFS)
Normal flow depth in pipe =
                            4.27(In.)
Flow top width inside pipe =
                             8.99(In.)
Critical Depth = 4.56(In.)
Pipe flow velocity =
                        3.39(Ft/s)
Travel time through pipe = 0.20 min.
Time of concentration (TC) = 5.20 min.
```

```
Along Main Stream number: 1 in normal stream number 3
Stream flow area =
                     0.300(Ac.)
Runoff from this stream =
                            0.698(CFS)
Time of concentration =
                        5.20 min.
Rainfall intensity = 2.585(In/Hr)
Process from Point/Station
                            401.000 to Point/Station
                                                        402.000
**** INITIAL AREA EVALUATION ****
Initial area flow distance = 171.000(Ft.)
Top (of initial area) elevation = 1462.100(Ft.)
Bottom (of initial area) elevation = 1458.300(Ft.)
                           3.800(Ft.)
Difference in elevation =
         0.02222 s(percent)=
Slope =
                                  2.22
TC = k(0.300)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration = 5.023 min.
Rainfall intensity =
                       2.630(In/Hr) for a 10.0 year storm
COMMERCIAL subarea type
Runoff Coefficient = 0.883
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2) = 69.00
Pervious area fraction = 0.100; Impervious fraction = 0.900
Initial subarea runoff =
                           5.575(CFS)
Total initial stream area =
                               2.400(Ac.)
Pervious area fraction = 0.100
Process from Point/Station
                            402.000 to Point/Station
                                                        403.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
Upstream point/station elevation = 1454.200(Ft.)
Downstream point/station elevation = 1451.300(Ft.)
Pipe length = 597.00(Ft.)
                           Manning's N = 0.012
No. of pipes = 1 Required pipe flow =
                                        5.575(CFS)
Nearest computed pipe diameter =
                                  18.00(In.)
Calculated individual pipe flow =
                                 5.575(CFS)
                         11.13(In.)
Normal flow depth in pipe =
Flow top width inside pipe =
                            17.49(In.)
Critical Depth = 10.93(In.)
Pipe flow velocity =
                       4.86(Ft/s)
Travel time through pipe = 2.05 min.
Time of concentration (TC) =
                          7.07 min.
```

Process from Point/Station 402.000 to Point/Station 403.000 **** CONFLUENCE OF MINOR STREAMS **** Along Main Stream number: 1 in normal stream number 4 Stream flow area = 2.400(Ac.) 5.575(CFS) Runoff from this stream = Time of concentration = 7.07 min. Rainfall intensity = 2.224(In/Hr) Summary of stream data: Stream Flow rate TC Rainfall Intensity No. (CFS) (min) (In/Hr) 9.880 1 10.60 1.823 2 1.573 8.99 1.977 3 0.698 5.20 2.585 5.575 4 7.07 2.224 Largest stream flow has longer time of concentration 9.880 + sum of Qp = 0b Ia/Ib 1.573 * 0.922 = 1.451 Qb Ia/Ib 0.698 * 0.705 = 0.493 0b Ia/Ib 5.575 * 0.820 =4.571 0p = 16.394 Total of 4 streams to confluence: Flow rates before confluence point: 9.880 1.573 5.575 0.698 Area of streams before confluence: 5.600 0.900 0.300 2.400 Results of confluence: Total flow rate = 16.394(CFS) Time of concentration = 10.604 min. Effective stream area after confluence = 9.200(Ac.) End of computations, total study area = 9.20 (Ac.) The following figures may be used for a unit hydrograph study of the same area. Area averaged pervious area fraction(Ap) = 0.100 Area averaged RI index number = 69.0

100-YEAR ONSITE HYDROLOGY (RATIONAL METHOD)



Riverside County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software, (c) 1989 - 2004 Version 7.0 Rational Hydrology Study Date: 08/12/21 File:prop100.out 20-0082 - FIR HK ONSITE RATIONAL METHOD HYDROLOGY 100 YEAR STORM EVENT FN: PROP100.OUT RC _____ ******** Hydrology Study Control Information ********* English (in-lb) Units used in input data file _____ Program License Serial Number 4010 _____ Rational Method Hydrology Program based on Riverside County Flood Control & Water Conservation District 1978 hydrology manual Storm event (year) = 100.00 Antecedent Moisture Condition = 2 Standard intensity-duration curves data (Plate D-4.1) For the [Perris Valley] area used. 10 year storm 10 minute intensity = 1.880(In/Hr) 10 year storm 60 minute intensity = 0.780(In/Hr)100 year storm 10 minute intensity = 2.690(In/Hr) 100 year storm 60 minute intensity = 1.120(In/Hr) Storm event year = 100.0Calculated rainfall intensity data: 1 hour intensity = 1.120(In/Hr)Slope of intensity duration curve = 0.4900 Process from Point/Station 101.000 to Point/Station 102.000 **** INITIAL AREA EVALUATION **** Initial area flow distance = 363.000(Ft.) Top (of initial area) elevation = 1459.100(Ft.) Bottom (of initial area) elevation = 1456.800(Ft.)

```
Difference in elevation = 2.300(Ft.)
Slope = 0.00634 s(percent)=
                                 0.63
TC = k(0.300)*[(length^3)/(elevation change)]^{0.2}
Initial area time of concentration = 8.724 min.
Rainfall intensity =
                      2.881(In/Hr) for a 100.0 year storm
COMMERCIAL subarea type
Runoff Coefficient = 0.885
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2) = 69.00
Pervious area fraction = 0.100; Impervious fraction = 0.900
Initial subarea runoff = 14.271(CFS)
Total initial stream area =
                              5.600(Ac.)
Pervious area fraction = 0.100
Process from Point/Station
                            102.000 to Point/Station
                                                      103.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
Upstream point/station elevation = 1451.900(Ft.)
Downstream point/station elevation = 1450.300(Ft.)
Pipe length = 512.00(Ft.) Manning's N = 0.012
No. of pipes = 1 Required pipe flow = 14.271(CFS)
Nearest computed pipe diameter = 24.00(In.)
Calculated individual pipe flow = 14.271(CFS)
Normal flow depth in pipe = 20.72(In.)
Flow top width inside pipe = 16.49(In.)
Critical Depth = 16.33(In.)
Pipe flow velocity = 4.95(Ft/s)
Travel time through pipe = 1.72 min.
Time of concentration (TC) = 10.45 min.
Process from Point/Station 102.000 to Point/Station
                                                      103.000
**** CONFLUENCE OF MINOR STREAMS ****
Along Main Stream number: 1 in normal stream number 1
Stream flow area = 5.600(Ac.)
Runoff from this stream =
                          14.271(CFS)
Time of concentration = 10.45 min.
Rainfall intensity = 2.637(In/Hr)
Process from Point/Station
                           201.000 to Point/Station
                                                      202.000
**** INITIAL AREA EVALUATION ****
```

```
Initial area flow distance =
                            395.000(Ft.)
Top (of initial area) elevation = 1460.100(Ft.)
Bottom (of initial area) elevation = 1457.400(Ft.)
Difference in elevation =
                           2.700(Ft.)
Slope =
         0.00684 s(percent)=
                                  0.68
TC = k(0.300)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =
                                    8.888 min.
Rainfall intensity =
                       2.855(In/Hr) for a 100.0 year storm
COMMERCIAL subarea type
Runoff Coefficient = 0.884
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2) = 69.00
Pervious area fraction = 0.100; Impervious fraction = 0.900
Initial subarea runoff =
                           2.272(CFS)
Total initial stream area =
                               0.900(Ac.)
Pervious area fraction = 0.100
Process from Point/Station
                             202.000 to Point/Station
                                                        203.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
Upstream point/station elevation = 1451.800(Ft.)
Downstream point/station elevation = 1451.500(Ft.)
                            Manning's N = 0.012
Pipe length =
                29.00(Ft.)
No. of pipes = 1 Required pipe flow =
                                        2.272(CFS)
Nearest computed pipe diameter =
                                  12.00(In.)
Calculated individual pipe flow =
                                  2.272(CFS)
Normal flow depth in pipe =
                            6.55(In.)
Flow top width inside pipe =
                            11.95(In.)
Critical Depth = 7.73(In.)
Pipe flow velocity =
                       5.18(Ft/s)
Travel time through pipe = 0.09 min.
Time of concentration (TC) =
                            8.98 min.
Process from Point/Station
                             202.000 to Point/Station
                                                        203.000
**** CONFLUENCE OF MINOR STREAMS ****
Along Main Stream number: 1 in normal stream number 2
Stream flow area =
                     0.900(Ac.)
Runoff from this stream =
                            2.272(CFS)
Time of concentration =
                        8.98 min.
Rainfall intensity = 2.840(In/Hr)
```

```
Initial area flow distance = 120.000(Ft.)
Top (of initial area) elevation = 1461.000(Ft.)
Bottom (of initial area) elevation = 1458.600(Ft.)
Difference in elevation =
                           2.400(Ft.)
          0.02000 s(percent)=
                                   2.00
Slope =
TC = k(0.300)*[(length^3)/(elevation change)]^{0.2}
Warning: TC computed to be less than 5 min.; program is assuming the
time of concentration is 5 minutes.
Initial area time of concentration =
                                     5.000 min.
Rainfall intensity =
                        3.785(In/Hr) for a 100.0 year storm
COMMERCIAL subarea type
Runoff Coefficient = 0.888
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2) = 69.00
Pervious area fraction = 0.100; Impervious fraction = 0.900
Initial subarea runoff =
                           1.008(CFS)
Total initial stream area =
                                0.300(Ac.)
Pervious area fraction = 0.100
Process from Point/Station 302.000 to Point/Station
                                                         303.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
Upstream point/station elevation = 1451.800(Ft.)
```

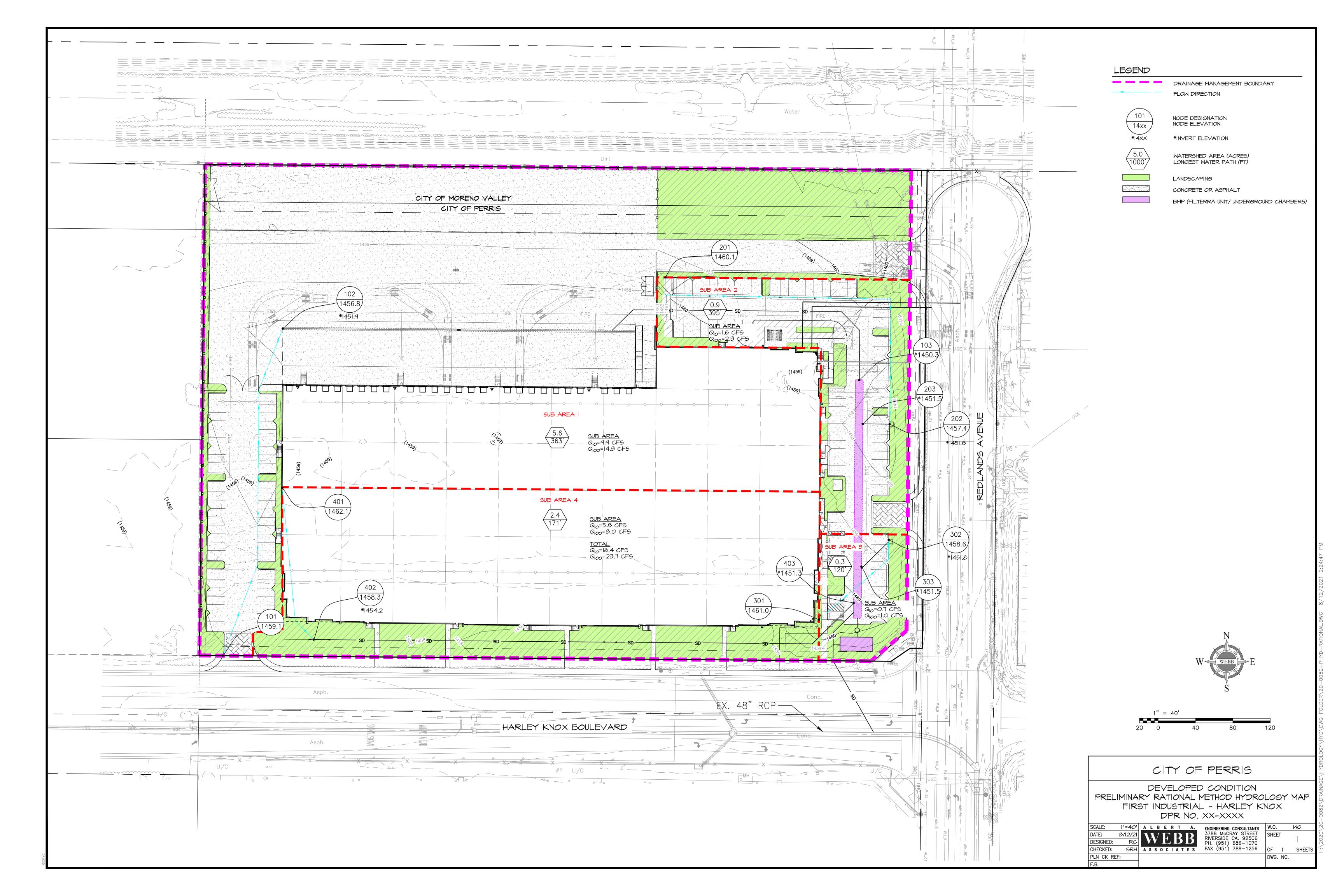
```
Downstream point/station elevation = 1451.500(Ft.)
Pipe length = 41.00(Ft.) Manning's N = 0.012
No. of pipes = 1 Required pipe flow =
                                        1.008(CFS)
Nearest computed pipe diameter =
                                  9.00(In.)
Calculated individual pipe flow =
                                    1.008(CFS)
Normal flow depth in pipe =
                            5.33(In.)
Flow top width inside pipe =
                             8.85(In.)
Critical Depth = 5.53(In.)
Pipe flow velocity =
                        3.70(Ft/s)
Travel time through pipe = 0.18 min.
Time of concentration (TC) = 5.18 min.
```

```
Along Main Stream number: 1 in normal stream number 3
Stream flow area =
                     0.300(Ac.)
Runoff from this stream =
                            1.008(CFS)
Time of concentration =
                        5.18 min.
Rainfall intensity = 3.718(In/Hr)
Process from Point/Station
                             401.000 to Point/Station
                                                        402.000
**** INITIAL AREA EVALUATION ****
Initial area flow distance = 171.000(Ft.)
Top (of initial area) elevation = 1462.100(Ft.)
Bottom (of initial area) elevation = 1458.300(Ft.)
                           3.800(Ft.)
Difference in elevation =
         0.02222 s(percent)=
Slope =
                                  2.22
TC = k(0.300)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =
                                   5.023 min.
Rainfall intensity =
                       3.776(In/Hr) for a 100.0 year storm
COMMERCIAL subarea type
Runoff Coefficient = 0.888
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2) = 69.00
Pervious area fraction = 0.100; Impervious fraction = 0.900
Initial subarea runoff =
                           8.045(CFS)
Total initial stream area =
                               2.400(Ac.)
Pervious area fraction = 0.100
Process from Point/Station
                             402.000 to Point/Station
                                                        403.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
Upstream point/station elevation = 1454.200(Ft.)
Downstream point/station elevation = 1451.300(Ft.)
Pipe length = 597.00(Ft.)
                            Manning's N = 0.012
No. of pipes = 1 Required pipe flow =
                                        8.045(CFS)
Nearest computed pipe diameter =
                                  18.00(In.)
Calculated individual pipe flow =
                                   8.045(CFS)
                         15.00(In.)
Normal flow depth in pipe =
Flow top width inside pipe =
                            13.42(In.)
Critical Depth = 13.18(In.)
Pipe flow velocity =
                       5.11(Ft/s)
Travel time through pipe = 1.95 min.
Time of concentration (TC) = 6.97 min.
```

Process from Point/Station 402.000 to Point/Station 403.000 **** CONFLUENCE OF MINOR STREAMS **** Along Main Stream number: 1 in normal stream number 4 Stream flow area = 2.400(Ac.) Runoff from this stream = 8.045(CFS) Time of concentration = 6.97 min. Rainfall intensity = 3.216(In/Hr) Summary of stream data: Stream Flow rate TC Rainfall Intensity No. (CFS) (min) (In/Hr) 1 14.271 10.45 2.637 2 8.98 2.272 2.840 3 1.008 5.18 3.718 6.97 4 8.045 3.216 Largest stream flow has longer time of concentration Qp = 14.271 + sum of 0b Ia/Ib 2.272 * 0.929 = 2.110 Qb Ia/Ib 1.008 * 0.709 = 0.715 0b Ia/Ib 8.045 * 0.820 =6.597 0p = 23.693 Total of 4 streams to confluence: Flow rates before confluence point: 14.271 2.272 8.045 1.008 Area of streams before confluence: 5.600 0.900 0.300 2.400 Results of confluence: Total flow rate = 23.693(CFS) Time of concentration = 10.448 min. Effective stream area after confluence = 9.200(Ac.) End of computations, total study area = 9.20 (Ac.) The following figures may be used for a unit hydrograph study of the same area. Area averaged pervious area fraction(Ap) = 0.100 Area averaged RI index number = 69.0

HYDROLOGY MAPS





APPENDIX B – HYDRAULICS



HYDRAULIC CALCULATIONS

Hydraulic calculations to be provided in Final Engineering.

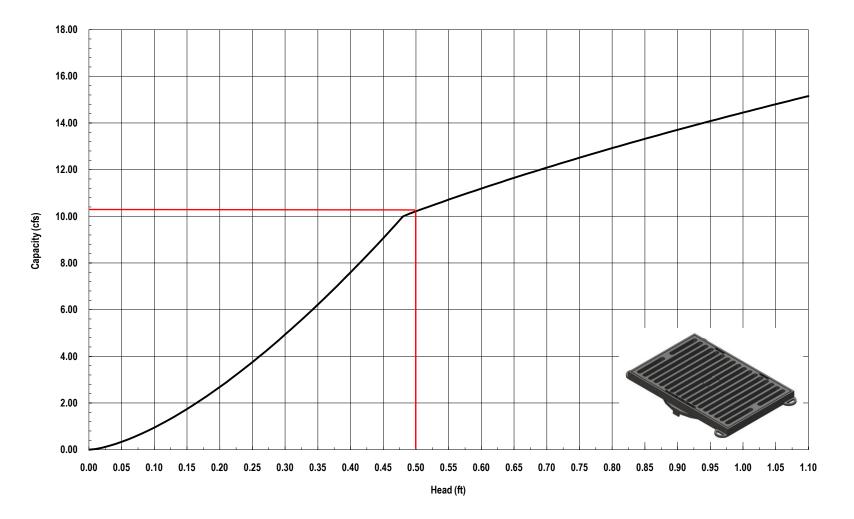


First Industrial – Harley Knox

INLET AND CATCH BASIN CALCULATIONS



Nyloplast 2' x 3' Road & Highway Grate Inlet Capacity Chart





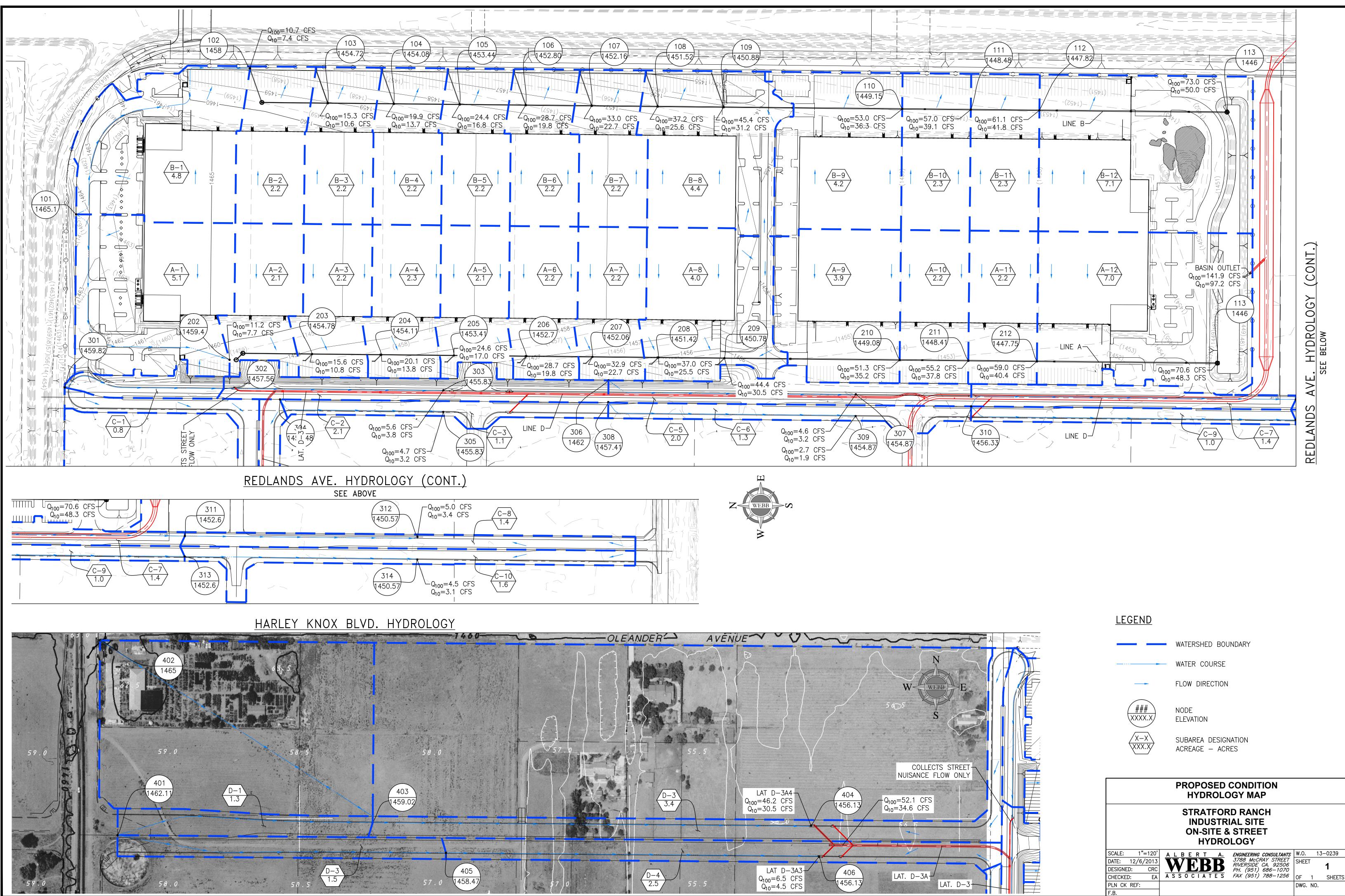
3130 Verona Avenue • Buford, GA 30518 (866) 888-8479 / (770) 932-2443 • Fax: (770) 932-2490 © Nyloplast Inlet Capacity Charts June 2012

APPENDIX C – REFERENCES



PERRIS VALLEY MDP LAT D-3A PLANS





GENERAL NOTES

- IT SHALL BE THE RESPONSIBILITY OF THE DEVELOPER/OWNER CONTRACTOR TO APPLY TO THE CITY OF PERRIS ENGINEERING DEPARTMENT, PERMIT SÉCTION, FOR AN ENCROACHMENT PERMIT FOR ALL WORK PERFORMED WITHIN PUBLIC RIGHT-OF-WAY, DEDICATED AND ACCEPTED FOR PUBLIC USE; AND TO BE RESPONSIBLE FOR SATISFACTORY COMPLIANCE FOR ALL CURRENT ENVIRONMENTAL REGULATIONS DURING THE LIFE OF CONSTRUCTION ACTIVITIES FOR THIS PROJECT, ADDITIONAL STUDIES AND/OR PERMITS MAY BE REQUIRED.
- THE CONTRACTOR/DEVELOPER SHALL BE RESPONSIBLE FOR THE CLEARING OF THE WORK AREA, AND RELOCATION COSTS OF ALL EXISTING UTILITIES. THIS INCLUDES UNDERGROUNDING OF EXISTING OVERHEAD LINES ALONG THE PROJECT FRONTAGE AS REQUIRED BY THE CONDITIONS OF APPROVAL. PERMITEE MUST INFORM CITY OF CONSTRUCTION SCHEDULE AT LEAST 48 HOURS PRIOR TO BEGINNING OF CONSTRUCTION. PHONE: (951) 943-6504.
- THE DEVELOPER WILL INSTALL STREET NAME SIGNS CONFORMING TO COUNTY STANDARD NO. 816 OR AS APPROVED BY THE CITY ENGINEER.
- ALL WORK SHALL CONFORM TO THE REQUIREMENTS OF THE RIVERSIDE COUNTY TRANSPORTATION DEPARTMENT IMPROVEMENT STANDARDS AND SPECIFICATIONS, LATEST EDITION, COUNTY ORDINANCE NO. 461 AND SUBSEQUENT AMENDMENTS.
- 5. IT SHALL BE THE RESPONSIBILITY OF THE DEVELOPER TO NOTIFY THE ENGINEER TO INSTALL STREET CENTERLINE MONUMENTS AS REQUIRED BY RIVERSIDE COUNTY ORDINANCE NO. 461 (TRACTS AND PARCEL MAPS ONLY). ALL EXISTING SURVEY MONUMENTS SHALL BE PROTECTED IN PLACE OR RELOCATED BY A LICENSED PROFESSIONAL PRIOR TO CONSTRUCTION.
- ALL UNDERGROUND FACILITIES, WITH LATERALS, SHALL BE IN PLACE PRIOR TO PAVING THE STREET, INCLUDING, BUT NOT LIMITED TO, THE FOLLOWING: SEWER, WATER, ELECTRIC, GAS, STORM DRAINS.
- CURB DEPRESSIONS AND DRIVEWAY APPROACHES WILL BE INSTALLED AND CONSTRUCTED ACCORDING TO COUNTY STANDARD NO. 207A, AS DIRECTED IN THE FIELD AND AS APPROVED BY THE CITY ENGINEER.
- 8. IT SHALL BE THE RESPONSIBILITY OF THE DEVELOPER OR CONTRACTOR TO INSTALL AND MAINTAIN ALL CONSTRUCTION. REGULATORY. GUIDE AND WARNING SIGNS WITHIN THE PROJECT LIMITS AND ITS SURROUNDINGS TO PROVIDE SAFE PASSAGE FOR THE TRAVELING PUBLIC AND WORKERS UNTIL THE FINAL COMPLETION AND ACCEPTANCE OF THE PROJECT BY THE CITY. A TRAFFIC CONTROL PLAN MUST BE SUBMITTED FOR REVIEW TO THE PERMITS SECTION OR INSPECTION SECTION PRIOR TO OBTAINING AN ENCROACHMENT PERMIT.
- ALL STREET SECTIONS ARE MINIMUM REQUIREMENTS. ADDITIONAL SOIL TESTS SHALL BE TAKEN AFTER ROUGH GRADING TO DETERMINE THE RECOMMENDED STREET SECTION REQUIREMENTS. USE COUNTY STD. NO. 401 IF EXPANSIVE SOILS ARE ENCOUNTERED.
- 10. ASPHALTIC EMULSION (FOG SEAL) SHALL BE APPLIED NOT LESS THAN FOURTEEN DAYS FOLLOWING PLACEMENT OF THE ASPHALT SURFACING. FOG SEAL AND PAINT BINDER SHALL BE APPLIED AT A RATE OF 0.05 AND 0.03 GALLON PER SQUARE YARD RESPECTIVELY. ASPHALTIC EMULSION SHALL CONFORM TO SECTION 37, 39 AND 94 OF THE STATE STANDARD SPECIFICATIONS.
- INSTALL STREET TREES IN ACCORDANCE WITH ORDINANCE NO. 461 AND THE COMPREHENSIVE LANDSCAPING 11. GUIDELINES.
- 12. STREET LIGHTS SHALL BE INSTALLED PER RIVERSIDE COUNTY STANDRADS AND IN ACCORDANCE WITH THE APPROVED STREET LIGHTING PLAN.
- 13. AS DETERMINED BY THE CITY ENGINEER, THE DEVELOPER IS RESPONSIBLE AT A MINIMUM FOR ROAD IMPROVEMENTS TO CENTERLINE, AND MAY BE REQUIRED TO RECONSTRUCT EXISTING PAVEMENT, INCLUDING BASE, AND MATCHING OVERLAY REQUIRED TO MEET THE STRUCTURAL STANDARDS FOR THE CURRENT ASSIGNED TRAFFIC INDEX PER ENGINEERING CONDITION OF APPROVAL.
- ANY PRIVATE DRAINAGE FACILITIES SHOWN ON THESE PLANS ARE FOR INFORMATION ONLY. BY SIGNING THESE IMPROVEMENT PLANS, NO REVIEW OR APPROVAL OF THOSE PRIVATE FACILITIES IS IMPLIED OR INTENDED BY THE CITY OF PERRIS ENGINEERING DEPARTMENT.
- 15. CONSTRUCTION PROJECTS MUST OBTAIN A NATIONAL POLLUTANT DISCHARGE ELIMINATION SYSTEM (NPDES) PERMIT. OWNERS/DEVELOPERS ARE REQUIRED TO FILE A NOTICE OF INTENT (NOI) WITH THE STATE WATER RESOURCES CONTROL BOARD (SWRCB), PREPARE A STORM WATER POLLUTION PREVENTION PLAN (SWPPP) AND MONITORING PLAN FOR THE SITE.

PRIOR TO ANY CONSTRUCTION, THE DEVELOPER SHALL PROVIDE THE CITY A COPY OF THE NOI WITH A VALID WDID NUMBER.

- 16. THE DEVELOPER SHALL BE RESPONSIBLE FOR THE INSTALLATION OF ADDITIONAL SIGNS AND MARKINGS NOT INCLUDED IN THE SIGNING AND STRIPING PLAN WITHIN THE PROJECT AREAS, OR ON ROADWAYS ADJACENT TO THE PROJECT BOUNDARIES. UPON THE REQUEST OF THE CITY ENGINEER OR HIS DESIGNEE TO IMPROVE TRAFFIC SAFETY ON THE ROADS UNDER THE JURISDICTION OF THE DEVELOPER.
- 17. EXISTING STORM DRAIN PIPES / CULVERTS (WHETHER TO BE CONNECTED TO, EXTENDED, ADJUSTED, DRAINED TO, OR JUST IN THE PROJECT VICINITY) MUST BE REPAIRED, AND/OR CLEANED TO MAKE THEM FUNCTIONAL AND ACCEPTABLE APPROVED BY THE CITY ENGINEER
- 18. FOR ALL DRIVEWAY RECONSTRUCTION BEYOND RIGHT-OF-WAY, PROOF OF DRIVEWAY OWNER NOTIFICATION IS REQUIRED PRIOR TO CONSTRUCTION.
- 19. IN THE EVENT OF ANY DAMAGE TO ADJACENT STREETS CAUSED BY THE CONSTRUCTION, CONTRACTOR SHALL REMOVE AND REPLACE DAMAGES AS DIRECTED BY CITY ENGINEER.

NOTICE TO CONTRACTORS

CONTRACTOR AGREES THAT HE SHALL ASSUME COMPLETE AND SOLE RESPONSIBILITY FOR JOB SITE CONDITIONS DURING THE COURSE OF CONSTRUCTION, INCLUDING SAFETY OF ALL PERSONS AND PROPERTY; THAT THIS REQUIREMENT SHALL CONTINUOUSLY AND NOT BE LIMITED TO NORMAL WORKING HOURS; AND THAT THE CONTRACTOR SHALL DEFEND, INDEMNIFY AND HOLD THE OWNER AND ENGINEER HARMLESS FROM ANY AND ALL LIABILITY, REAL OR ALLEGED, IN CONNECTION WITH THE PERFORMANCE OF WORK ON THIS PROJECT, EXCEPTING FROM LIABILITY ARISING FROM THE SOLE NEGLIGENCE OF THE OWNER OR ENGINEER.

UNDERGROUND STRUCTURES

ALL UNDERGROUND STRUCTURES OR UTILITIES REPORTED BY THE OWNER OR OTHERS AND THOSE SHOWN ON THE RECORDS EXAMINED ARE INDICATED WITH THEIR APPROXIMATE LOCATION AND EXTENT.

THE OWNER, BY ACCEPTING THESE PLANS OR PROCEEDING WITH THE IMPROVEMENTS PURSUANT THERETO AGREES TO ASSUME LIABILITY AND TO HOLD THE UNDERSIGNED HARMLESS FOR ANY DAMAGES RESULTING FROM THE EXISTENCE OF UNDERGROUND UTILITIES OR STRUCTURES NOT REPORTED TO THE UNDERSIGNED, NOT INDICATED ON THE PUBLIC RECORDS EXAMINED, OR LOCATED AT VARIANCE WITH THAT REPORTED OR SHOWN ON THE RECORDS EXAMINED.

THE CONTRACTOR IS REQUIRED TO TAKE DUE PRECAUTIONARY MEASURES TO PROTECT THE UTILITIES OR STRUCTURES SHOWN AND ANY OTHER UTILITIES OR STRUCTURES FOUND AT THE SITE. IT SHALL BE THE CONTRACTOR'S RESPONSIBILITY TO NOTIFY THE OWNERS OF THE UTILITIES OR STRUCTURES CONCERNED BEFORE STARTING WORK.

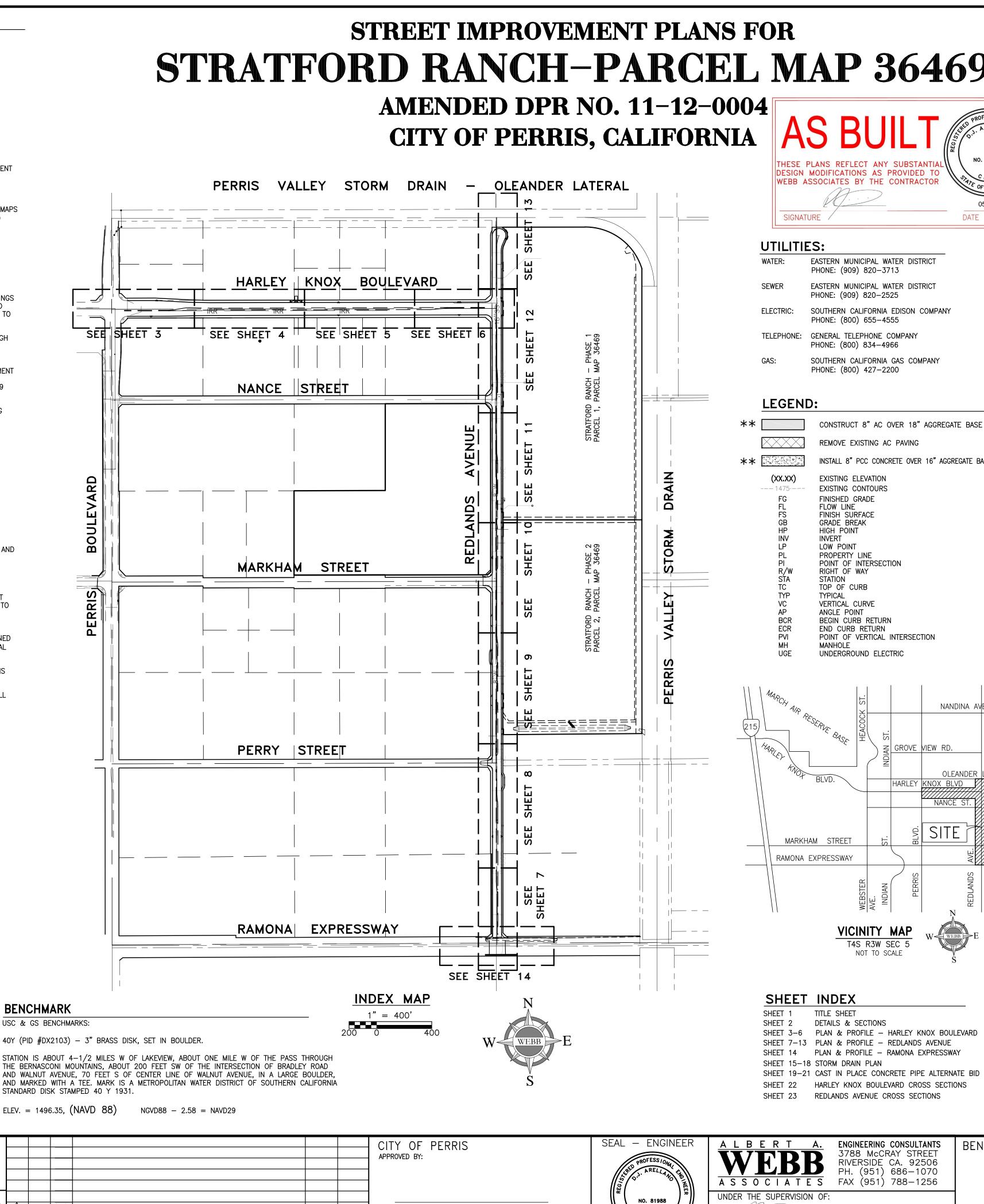
BASIS OF BEARINGS

THE BASIS OF BEARINGS FOR THIS SURVEY IS THE CALIFORNIA COORDINATE SYSTEM ZONE 6, NAD 83, 1991.35 EPOCH AS DETERMINED LOCALLY BY A LINE BETWEEN 40 Y (PID DX2103) AND SANTA FE (PID DX3719) BEING NORTH 80°43'18" WEST AS DERIVED FROM GEODETIC VALUES PUBLISHED BY NATIONAL GEODETIC SURVEY(NGS)

DISTANCES SHOWN HEREON ARE GROUND DISTANCES UNLESS OTHERWISE NOTED. TO OBTAIN GRID DISTANCES MULTIPLY GROUND DISTANCES BY 0.99999207.

CALCULATIONS FROM GRID TO GROUND VALUES AND CONVERGANCE ANGLE FOR THIS SURVEY WERE MADE AT POINT #653 WITH COORDINATES OF N-2,252,331.06, E-6,265,288.22, USING AN ELEVATION OF 1454.22(NAVD88)

	NOTE:				
	WORK CONTAINED WITHIN THESE PLANS SHALL NOT				
	COMMENCE UNTIL AN ENCROACHMENT PERMIT				
	AND/OR A GRADING PERMIT HAS BEEN ISSUED.				
BEFORE DIAL DAYS BEFORE	THE PRIVATE ENGINEER SIGNING THESE PLANS IS RESPONSIBLE FOR				
YOU DIG	ASSURING THE ACCURACY AND ACCEPTABILITY OF THE DESIGN HEREON.	\triangle	DJ	5/29/15	CATCH BASIN REVISED PER FIELD CONDITIONS
TOLL FREE 1-800-227-2600	IN THE EVENT OF DISCREPANCIES ARISING AFTER CITY APPROVAL OR DURING CONSTRUCTION, THE PRIVATE ENGINEER SHALL BE	Λ	DJ	3/5/15	ADDED CONSTRUCTION NOTE
A PUBLIC SERVICE BY	RESPONSIBLE FOR DETERMINING AN ACCEPTABLE SOLUTION AND	MARK	BY	DATE	REVISIONS
UNDERGROUND SERVICE ALERT	REVISING THE PLANS FOR APPROVAL BY THE CITY.	E	NGINEE	R	NEVISIONS



CITY ENGINEER

DATE

APPR. DATE

CITY

BENCHMARK

USC & GS BENCHMARKS:

40Y (PID #DX2103) - 3" BRASS DISK, SET IN BOULDER.

STANDARD DISK STAMPED 40 Y 1931.

ELEV. = 1496.35, (NAVD 88)

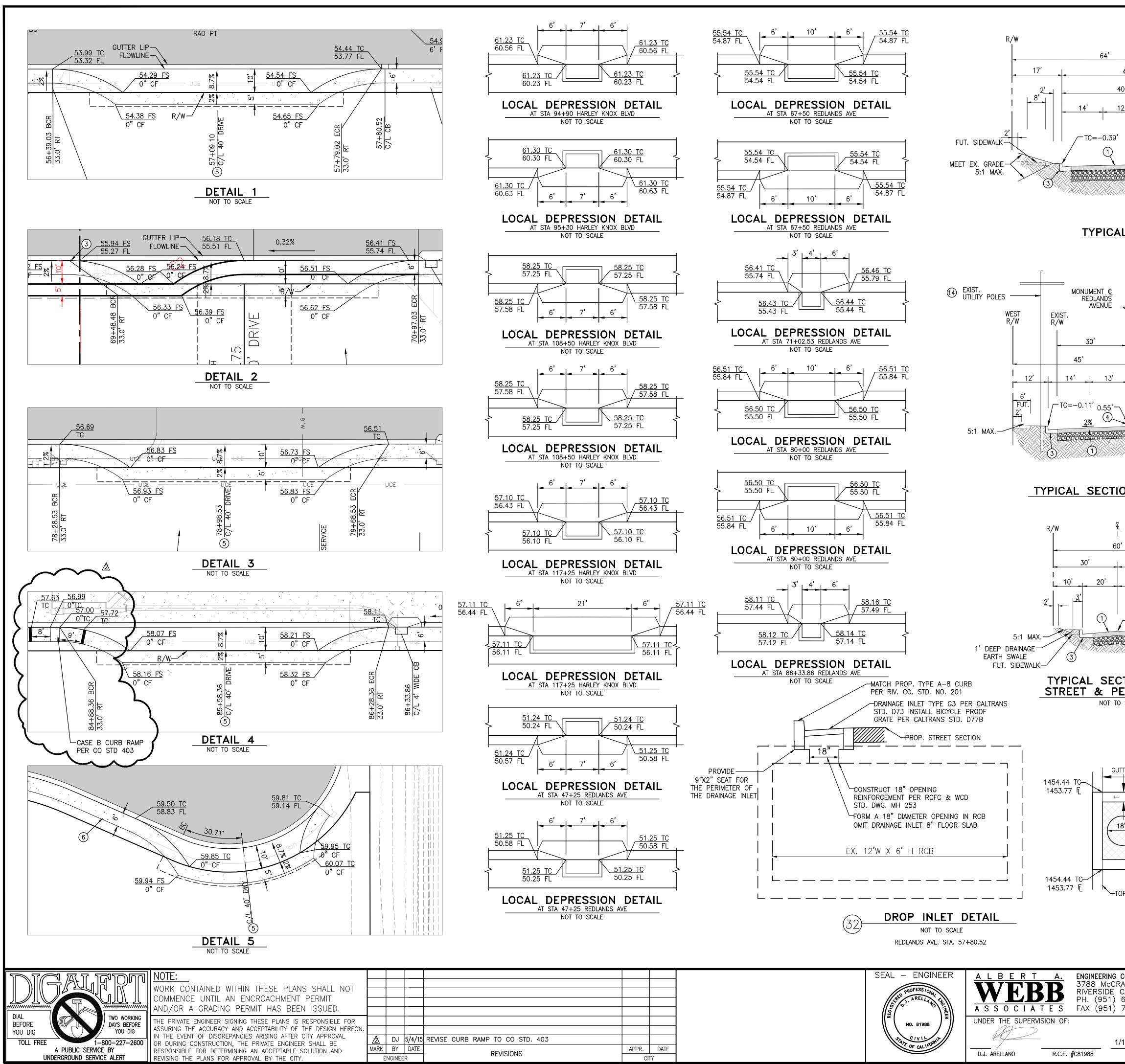
	1	CONSTRUCT MINIMUM 8" AC OVER 18" AB CLASS II (401,625 SF) 19,370 TC 22,310 C	
6469 **	2	CONSTRUCT MIN. 8" (4,000 PSI) PCC OVER 16" CLASS II AB (C.J. @ 20' O.C.) 122,134 SF 3,020 CY 6,020 CY	CONC
	3	CONSTRUCT TYPE "A-8" CURB & GUTTER PER RIV. CO. STD. NO. 201 15,120	Lf
ED PROFESSIONAL	4	CONSTRUCT 6" TYPE "D" CURB PER RIV. CO. STD. NO. 204 13,325	SI
PROFESSIONAL STREET	5	CONSTRUCT COMMERCIAL DRIVE PER RIV. CO. STD. NO. 207A 4,550	Lf
「日本語』 「日本語』 NO. 81988	6	CONSTRUCT 6' WIDE SIDEWALK PER RIV. CO. STD. 401 30,700	Lf
	$\overline{\mathcal{T}}$	CONSTRUCT CURB RAMP PER RIV. CO. STD. NO. 403, CASE A 18	EA
TRACTOR	8	COORD UNDERGROUNDING/RELOCATION OF PP 5 & GUY WIRE – BY UTILITY COMPANY 5	EA
05/19/2016 DATE	9	RELOCATE EX. UTILITY RISER – BY UTILITY COMPANY 16	EA
UAIL	10	REMOVE AC PAVEMENT AND DISPOSE OF LEGALLY 1,150	SI
	(11)	SAWCUT & JOIN EX. A.C. PAVEMENT PER DETAIL ON SHEET 2 700	Lf
DISTRICT	(12)	RELOCATE 4	EA
DISTRICT	(13)	ADJUST TO GRADE 19	EA
SON COMPANY	(14)	PROTECT IN PLACE –	
	(15)	INSTALL 3" AC OVER 95% COMPACTED NATIVE 1,455	SI
PANY	16	REMOVE EX. FENCE 1,900	Lf
S COMPANY	(17)	CONSTRUCT CROSS GUTTER PER RIV. CO. STD. NO. 209 1,425	SI
-	(18)	CONSTRUCT 6" TYPE "D-1" CURB PER RIV. CO. STD. NO. 203 -	Lf
	(19)	0.15' GRIND AND OVERLAY 3,550	SI
R 18" AGGREGATE BASE	20	INSTALL 48" RCP (D–LOAD PER PLAN) 280	Lf
AVING	21	INSTALL 36" RCP (D-LOAD PER PLAN) 860	Lf
OVER 16" AGGREGATE BASE	22	INSTALL 24" RCP (D-LOAD PER PLAN) 2,110	Lf
Ī	(23)	INSTALL 18" RCP (D–LOAD PER PLAN) 560	Lf
-	(24)	CONSTRUCT JUNCTION STRUCTURE NO 2 PER RCFC&WCD STD. JS227 6	E
-	(25)	CONSTRUCT JUNCTION STRUCTURE NO 3 PER RCFC&WCD STD. JS228 1	EA
-	(26)	CONSTRUCT JUNCTION STRUCTURE NO 4 PER RCFC&WCD STD. JS229 1	E/
-	(27)	CONSTRUCT CURB INLET CATCH BASIN PER RIV. CO. STD. NO. 300 17	E/
-	(28)	CONSTRUCT LOCAL DEPRESSION PER RIV. CO. STD. NO. 311 17	 E/
-	(29)	CONSTRUCT MANHOLE NO.1 PER RFC&WCD STD. MH251 5	
-	$\overline{)}$		
ERSECTION	(30)		E4
;	(31)	CONSTRUCT MANHOLE NO.4 PER RFC&WCD STD. MH254 4 CONSTRUCT DRAINAGE INLET TYPE G3 PER CALTRANS PLAN D73, 1	E4
-	(32)	AND DETAIL ON SHEET 2	EA
	$\overline{}$	REMOVE CONCRETE BULKHEAD 1	EA
NANDINA AVE.	$\overline{\bigcirc}$	INSTALL 12" DIA. HDPE N-12 STORM DRAIN PIPE ("ADS" OR APPROVED EQUAL) 190	D Lf
	(35)	INSTALL 18" DRAIN BASIN ("NYLOPLAST" OR EQUAL) WITH DOME GRATE 6	E/
ROVE VIEW RD.	(36)	REMOVE BACKFLOW AND SERVICE. COORDINATE WITH EMWD 1	E/
OLEANDER LATERAL	(37)	CONSTRUCT 8" THICK CONCRETE CLASS 560-C-3250; "B" AGGREGATE GRADATION 4	EA
RLEY KNOX BLVD	38	CONSTRUCT BUS TURNOUT PER RIV. CO. STD. NO. 814 2	EA
NANCE ST.	39	INSTALL 48" CIPCD PER MANUFACTURES SPECS 280	Lf
SITE	(40)	INSTALL 36" CIPCD PER MANUFACTURES SPECS 860	Lf
	(41)	INSTALL 24" CIPCD PER MANUFACTURES SPECS 1,300	Lf
	(42)	INSTALL 6" SLURRY BACKFILL (2 SACK) 395	Lf
PERRIS	43	INSTALL CONCRETE COLLAR PER RFC&WCD STD. M803 1	E/
	(44)	INSTALL 24" CMP HEL-COR PIPE ("CONTECH" OR APPROVED EQUAL) 100	LF
	(45)	INSTALL 24" FLARED END SECTION ("CONTECH" OR APPROVED EQUAL) 2	E/
5	(46)	CONSTRUCT CONCRETE BULKHEAD	E/
	(47)	CONSTRUCT MODIFIED GRATING CATCH BASIN PER SPPWC STD 303-3	
∫ ⊦	$\overline{}$	AND DETAIL ON SHEET 16	
۲ <u>۲</u>	(48)	CONSTRUCT LOCAL DEPRESSION PER SSPWC STD 313-3 CASE C 1	E/

D.J. ARELLANO

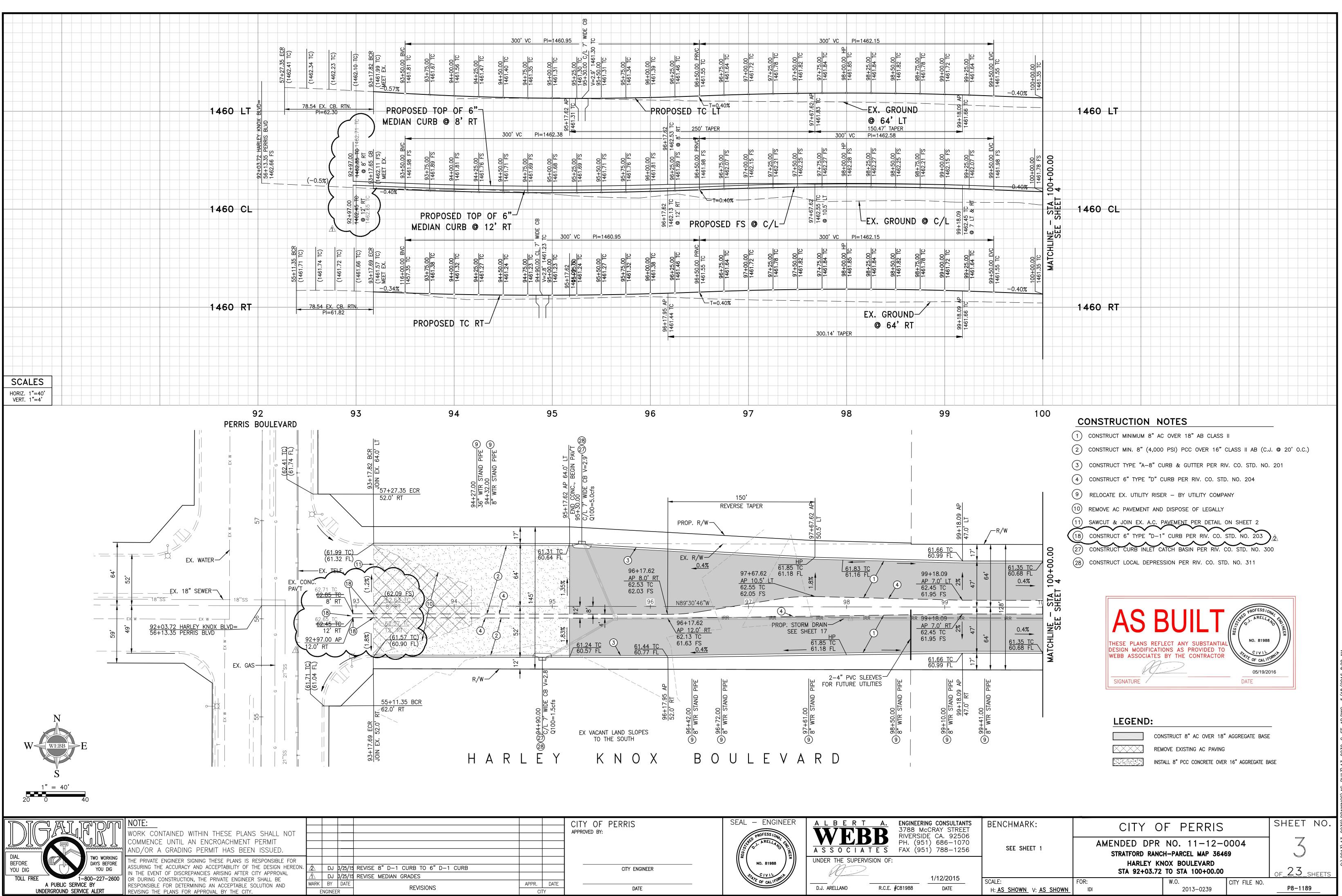
R.C.E. #C81988

THE QUANTITY ESTIMATE SHOWN HEREON IS FOR THE USE OF GOVERNING AGENCIES IN DETERMINING BOND AMOUNT AND/OR FEES AND IS NOT TO BE USED FOR BID PURPOSES. ** SEE GENERAL NOTE NO. 9

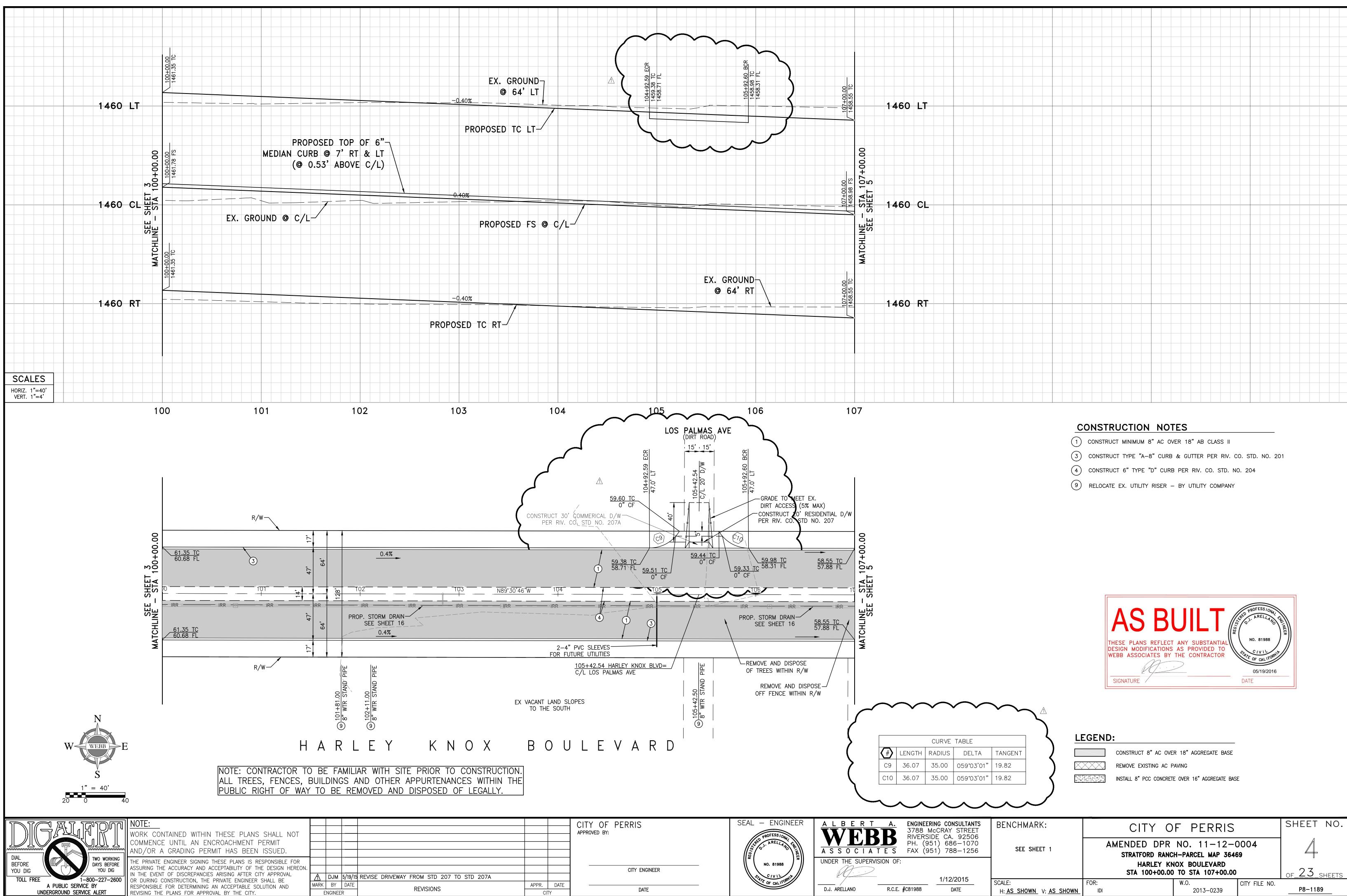
SHEET NO. **BENCHMARK:** CITY OF PERRIS AMENDED DPR NO. 11-12-0004 SEE HEREON STRATFORD RANCH-PARCEL MAP 36469 STREET IMPROVEMENT PLAN - 23 SHEETS TITLE SHEET 1/12/2015 SCALE: FOR: W.O. CITY FILE NO. P8-1189 DATE 2013-0239 H: <u>AS SHOWN</u> ∨: <u>AS SHOWN</u> IDI



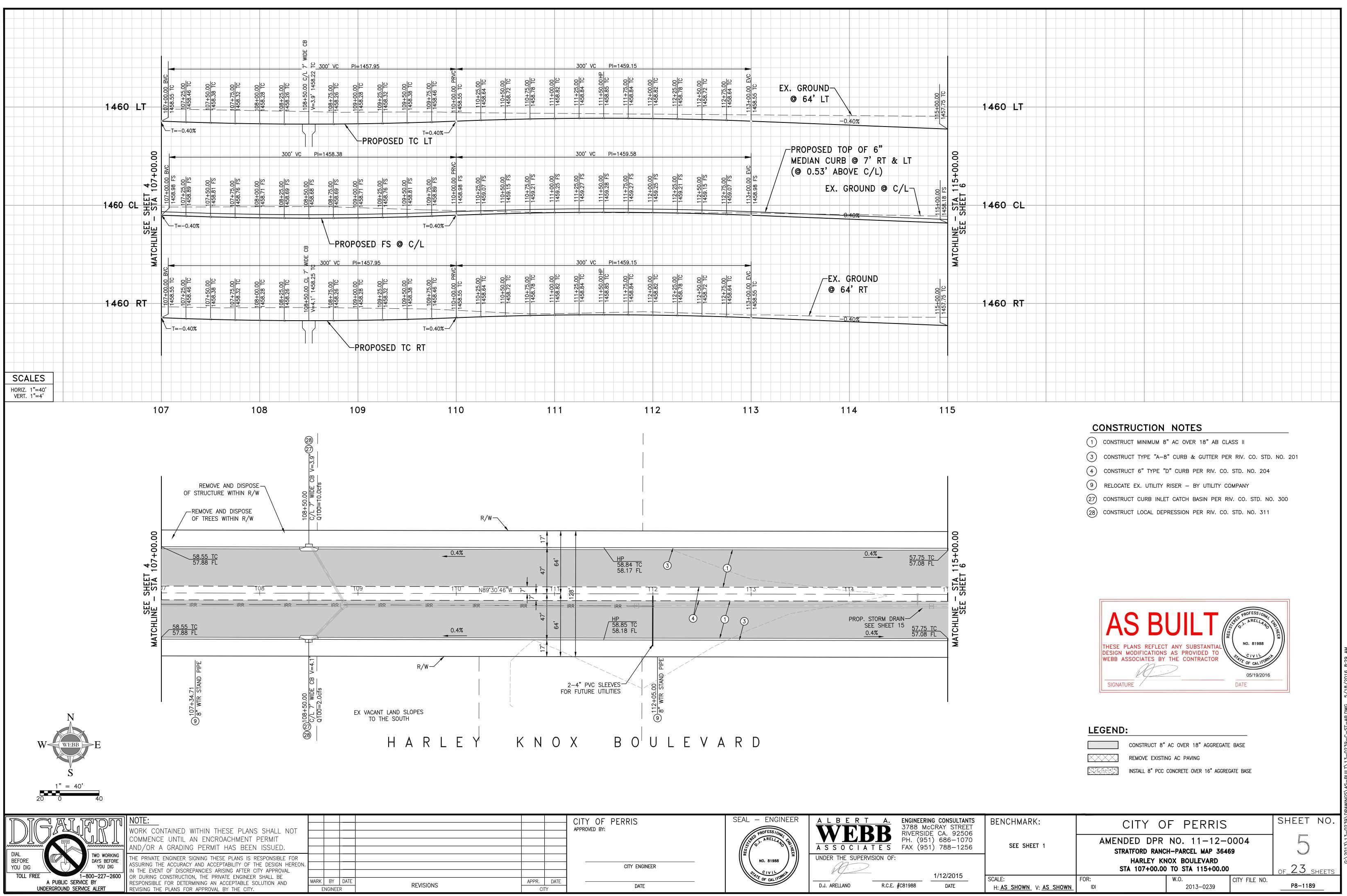
	C/L 47' 7' $7'$ $40'14'$ $12'14'$ $2%RAISEDION-LANDSCAPEDMEDIAN$	R/W 64' 17' 12' 14' TC=-0.39' 1 3	2 <u>'</u> FUT. SIDEWALK -MEET EX. GRADE 5:1 MAX.			
CONSTREDIA	N HARLEY KNOX E NOT TO SCALE T.I. = 11 TRUCTION Q NDS AVENUE 43' 13' $14'$ $10'AISED LANDSCAPED 6'TC=-0.1$	THESE PLANS DESIGN MODIF WEBB ASSOCIA SIGNATURE 25.0' SLOPED LANDSCAPE	BUIL REFLECT ANY SUBSTA ACATIONS AS PROVIDE ATES BY THE CONTRACT ACATON SAS PROVIDE ATES BY THE CONTRACT ACATON SAS PROVIDE ATES BY THE CONTRACT ATES	D TO CTOR	5/19/2016	
60' 	TC=0.16' 	PROPOSED 6"-CURB ONLY CURB ONLY 2% 2% 2% LEFT TURN P	VARIES 1%	STREET		
	6" FOR TYPE G3 DRAINAGE ET PER CALTRANS STD. D73 CE 2" X 2" GALVANIZED E MESH OVER INLET BOTTOM	19' SAWCUT 2 1 SAWCUT 1	19	EX. STRIPING (PROTECT IN PL EX. AC PAVEM		G:\2013\13-0239\DRAWINGS\AS-BUILT\13-0239-C-ST-AB.DWG 5/18/2016 8:29 AM
IG CONSULTANTS CRAY STREET	BENCHMARK:	CITY O	F PERRIS		SHEET NO.	0239\DRA
E CA. 92506) 686-1070) 788-1256	SEE SHEET 1	AMENDED DPR STRATFORD RANC	NO. 11-12-0 H-PARCEL MAP 3640		2	2013\13-
1/12/2015	SCALE:	FOR:	AND DETAILS W.O.	CITY FILE NO.	OF_23_SHEETS	:) ;;
DATE	H: <u>AS SHOWN</u> V: <u>AS SHOWN</u>	IDI	2013–0239		P8_1189	



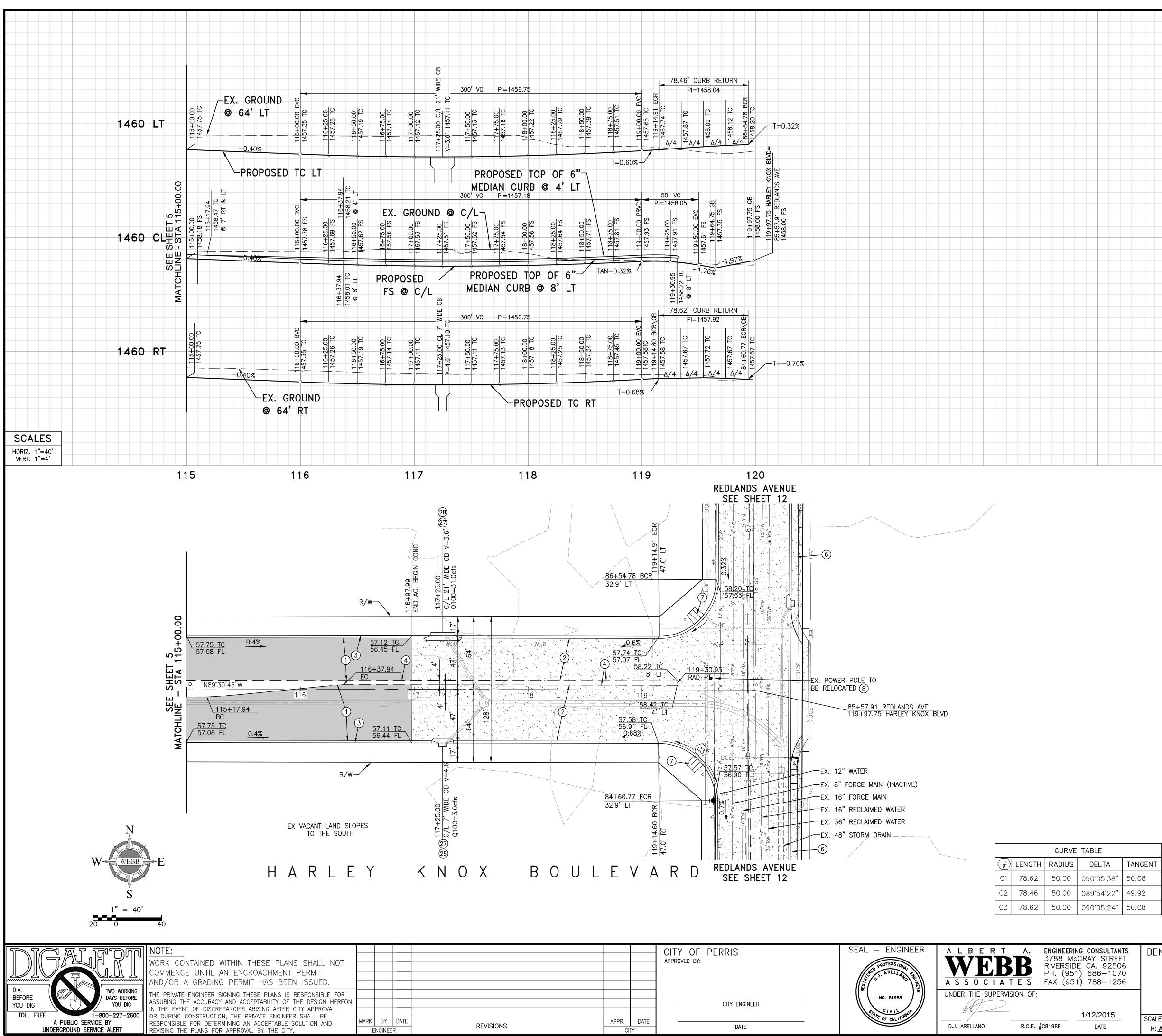
			CITY OF PERRIS APPROVED BY:	SEAL - ENGINEER	A L B E R T A. WEBB A S S O C I A T E S	ENGINEERING 3788 McCR RIVERSIDE PH. (951) FAX (951)
1 CURB			CITY ENGINEER	NO. 81988	UNDER THE SUPERVISION OF:	: 1/
	APPR. Cl	DATE TY	DATE	OF CAL IFON	D.J. ARELLANO R.C.E.	#C81988







		CITY OF PERRIS APPROVED BY:	SEAL – ENGINEER	A L B E R T A.	ENGINEERING CONSULTANTS 3788 McCRAY STREET	BENCHMARK:	CITY O	F PERRIS		SHEET NO.
 			LAND J. ARELLAND	A S S O C I A T E S	RIVERSIDE CA. 92506 PH. (951) 686—1070 FAX (951) 788—1256	SEE SHEET 1	AMENDED DPR	NO. $11 - 12 - 0$		5
		CITY ENGINEER	NO. 81988	UNDER THE SUPERVISION OF			HARLEY K	NOX BOULEVARD TO STA 115+00.00		of 23 sheets
APPR.	DATE Y	DATE	STE OF CALIFORNIE	D.J. ARELLANO R.C.E.	1/12/2015 #C81988 DATE	SCALE: H: <u>AS_SHOWN</u> V: <u>AS_SHOWN</u>	FOR: IDI	W.O. 2013-0239	CITY FILE NO.	



		CITY OF PERRIS APPROVED BY:	SEAL – ENGINEER		N 3788 M	RING CONSULTANTS	BENCHMARK:	CITY C	F PERRIS		SHEET NO.
			AND DAY I THE	A S S O C I A T E	PH. (95	DE CA. 92506 51) 686—1070 51) 788—1256	SEE SHEET 1		NO. 11-12-C CH-PARCEL MAP 3646		6
		CITY ENGINEER	NO. 81988	UNDER THE SUPERVISION	OF:	4/40/2045			NOX BOULEVARD 0 TO STA 119+93.75		of_23_sheets
APPR. DATI	ATE	DATE	TE OF CALIFORN	D.J. ARELLANO R	.C.E. #C81988	1/12/2015 DATE	SCALE: H: <u>AS_SHOWN_</u> V: <u>AS_SHOWN</u>	FOR: IDI	W.O. 2013-0239	CITY FILE NO.	P8-1189

CONSTRUCTION NOTES

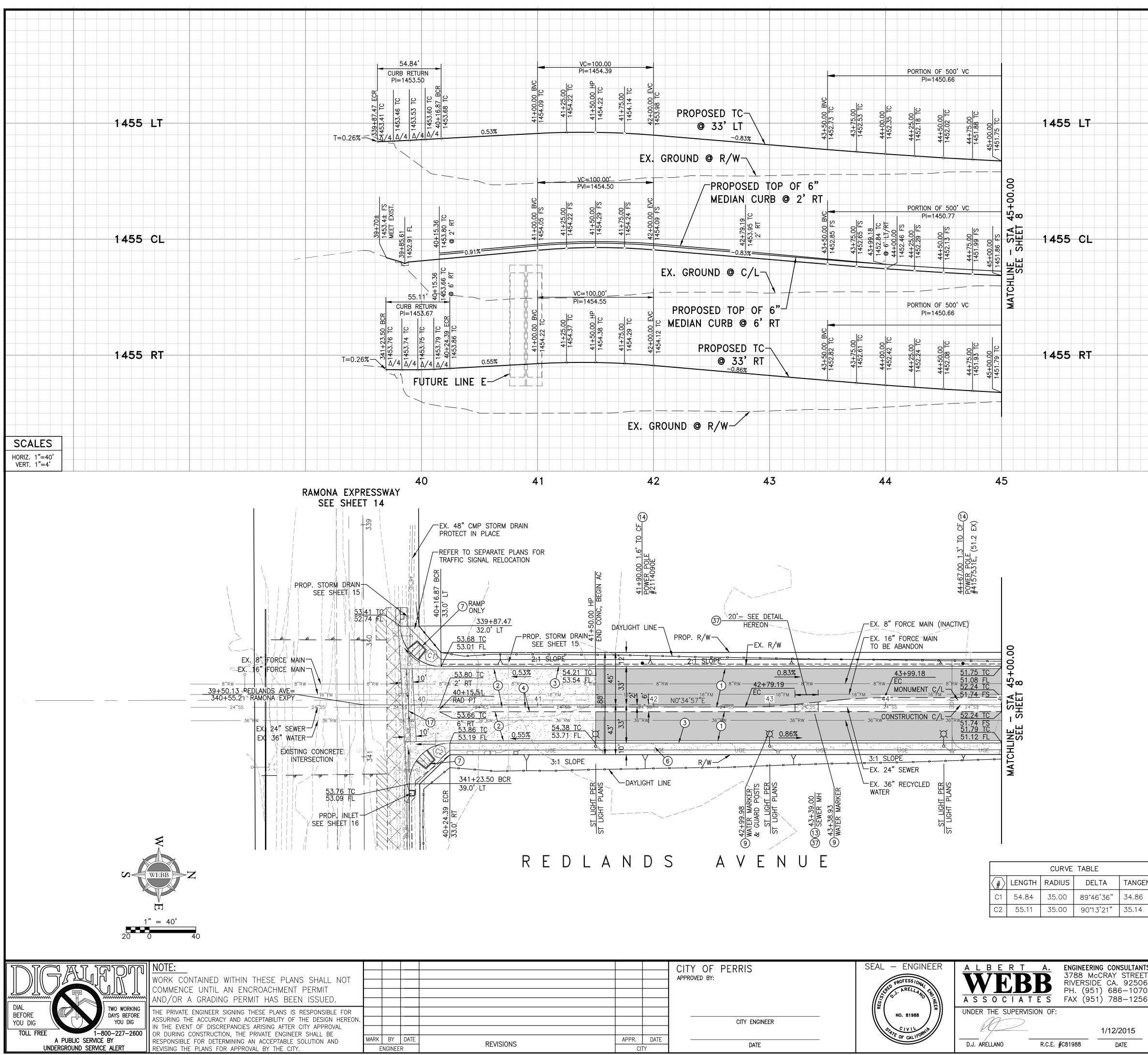
- (1) CONSTRUCT MINIMUM 8" AC OVER 18" AB CLASS II
- (2) CONSTRUCT MIN. 8" (4,000 PSI) PCC OVER 16" CLASS II AB (C.J. @ 20' O.C.)
- 3 CONSTRUCT TYPE "A-8" CURB & GUTTER PER RIV. CO. STD. NO. 201
- (4) CONSTRUCT 6" TYPE "D" CURB PER RIV. CO. STD. NO. 204
- (6) CONSTRUCT 6' WIDE SIDEWALK PER RIV. CO. STD. 401
- (7) CONSTRUCT CURB RAMP PER RIV. CO. STD. NO. 403, CASE A
- 8 COORD UNDERGROUNDING/RELOCATION OF PP & GUY WIRE BY UTILITY COMPANY
- (27) CONSTRUCT CURB INLET CATCH BASIN PER RIV. CO. STD. NO. 300
- (28) CONSTRUCT LOCAL DEPRESSION PER RIV. CO. STD. NO. 311



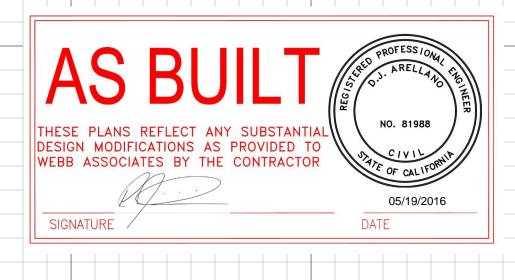
LEGEND:

CONSTRUCT 8" AC OVER 18" AGGREGATE BASE REMOVE EXISTING AC PAVING

 $\langle X X \rangle$ INSTALL 8" PCC CONCRETE OVER 16" AGGREGATE BASE



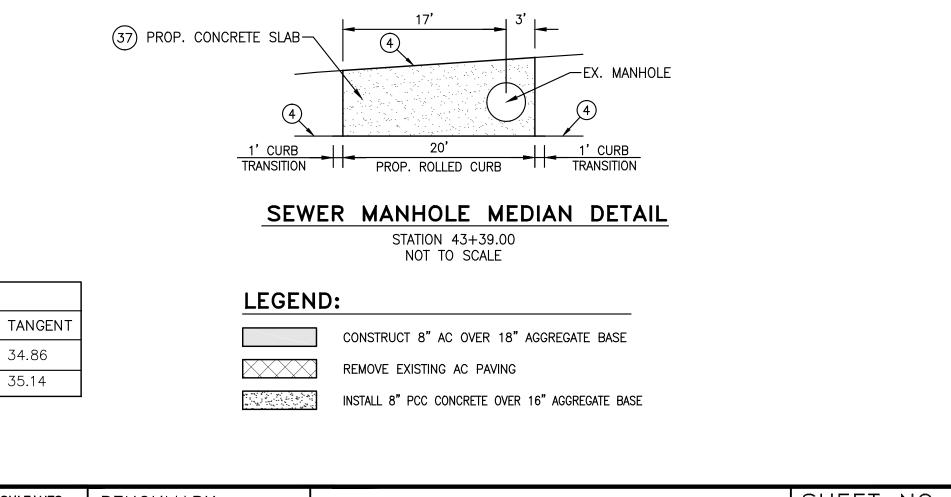
			SEAL – ENGINEER	ALBERTA. WERR	ENGINEERING CONSULTANTS 3788 McCRAY STREET	BENCHMARK:	CITY OF PERRIS	SHEET NO.
			RELLAND IN ARELLAND	A S S O C I A T E S	RIVERSIDE CA. 92506 PH. (951) 686—1070 FAX (951) 788—1256	SEE SHEET 1	AMENDED DPR NO. 11-12-000 STRATFORD RANCH-PARCEL MAP 36469	04
		CITY ENGINEER		UNDER THE SUPERVISION OF:			REDLANDS AVENUE STA 39+50.13 TO STA 45+00.00	OF_23_SHEETS
AF	APPR. D. CITY	E DATE	UP CIVIL	D.J. ARELLANO R.C.E.	#C81988 DATE	SCALE: H: <u>AS SHOWN</u> V: <u>AS SHOWN</u>	FOR: W.O. CIT IDI 2013–0239	Y FILE NO

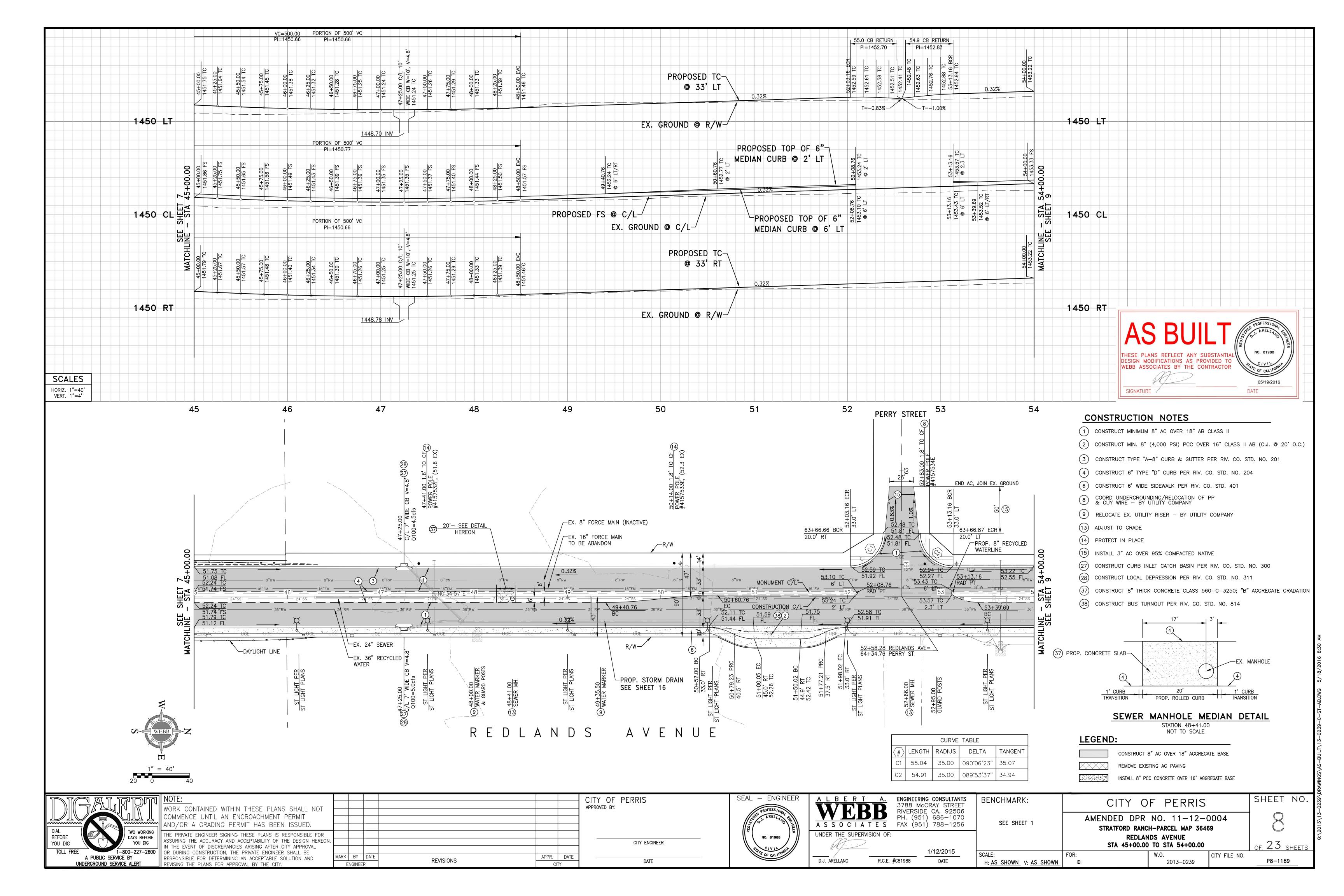


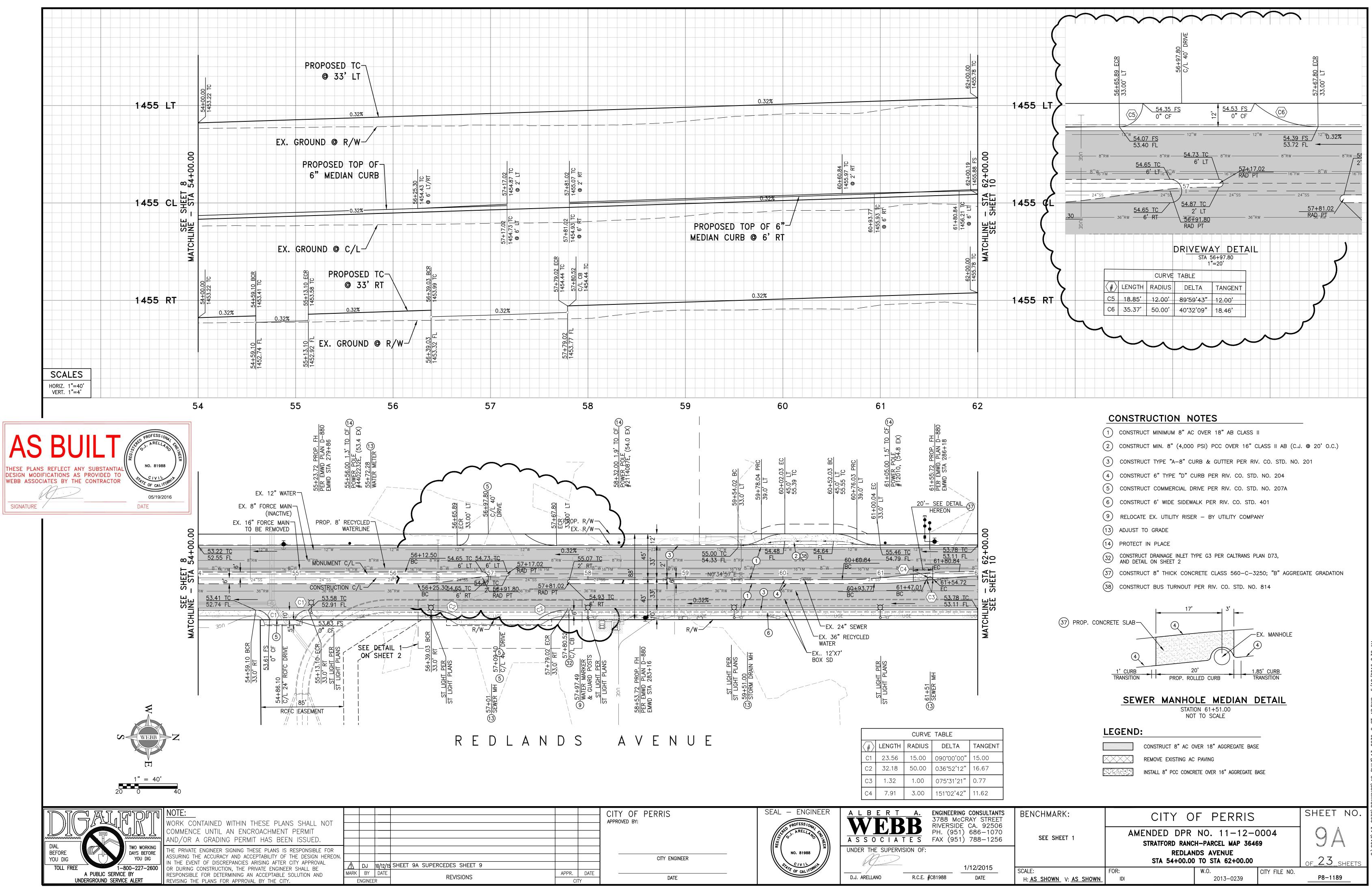
CONSTRUCTION NOTES

(1) CONSTRUCT MINIMUM 8" AC OVER 18" AB CLASS II

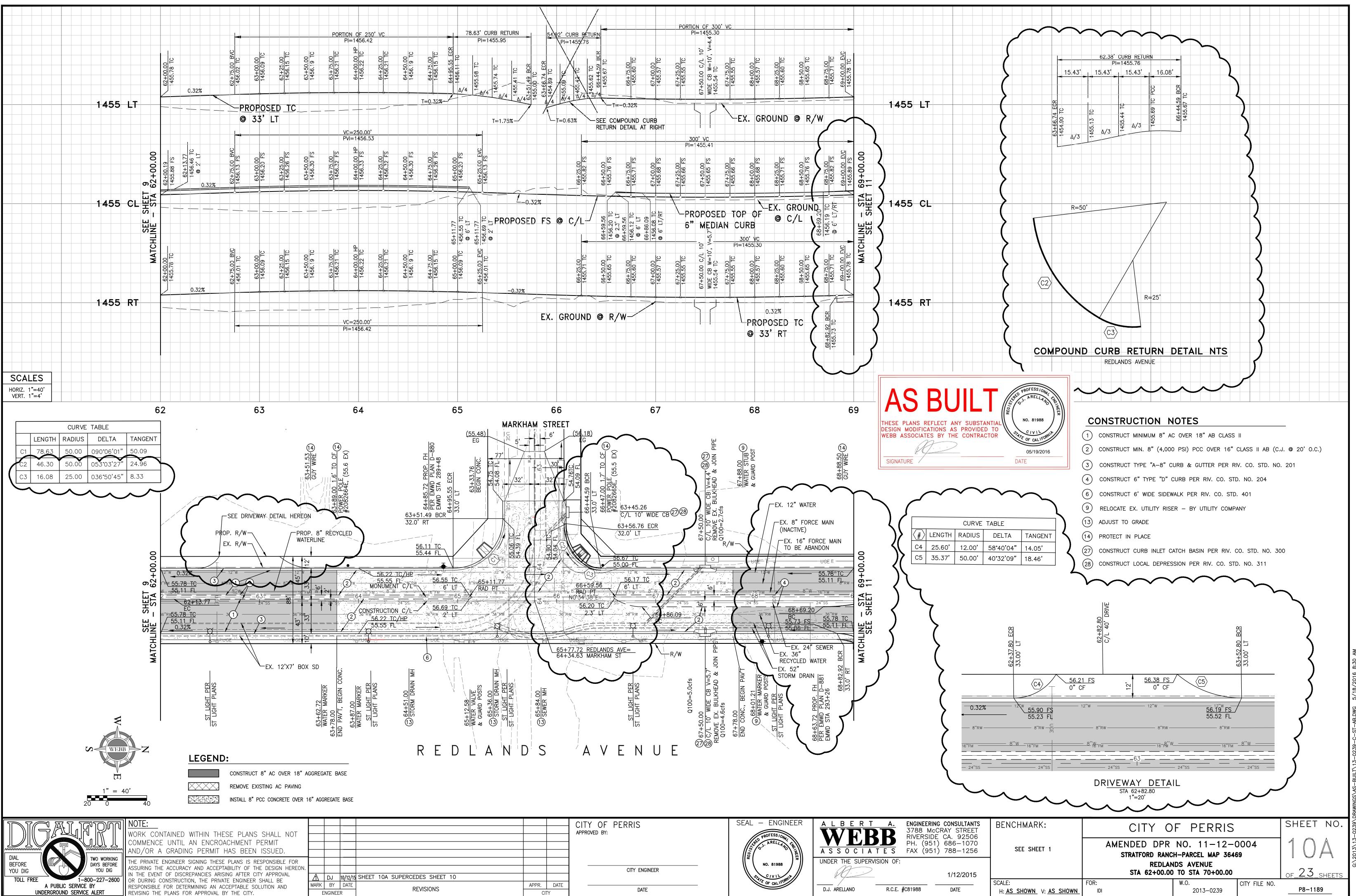
- (2) CONSTRUCT MIN. 8" (4,000 PSI) PCC OVER 16" CLASS II AB (C.J. @ 20' O.C.)
- (3) CONSTRUCT TYPE "A-8" CURB & GUTTER PER RIV. CO. STD. NO. 201
- (4) CONSTRUCT 6" TYPE "D" CURB PER RIV. CO. STD. NO. 204
- (6) CONSTRUCT 6' WIDE SIDEWALK PER RIV. CO. STD. 401
- (7) CONSTRUCT CURB RAMP PER RIV. CO. STD. NO. 403, CASE A
- (9) RELOCATE EX. UTILITY RISER BY UTILITY COMPANY
- (11) SAWCUT & JOIN EX. A.C. PAVEMENT PER DETAIL ON SHEET 2
- (13) ADJUST TO GRADE
- (14) PROTECT IN PLACE
- (17) CONSTRUCT CROSS GUTTER PER RIV. CO. STD. NO. 209
- (37) CONSTRUCT 8" THICK CONCRETE CLASS 560-C-3250; "B" AGGREGATE GRADATION



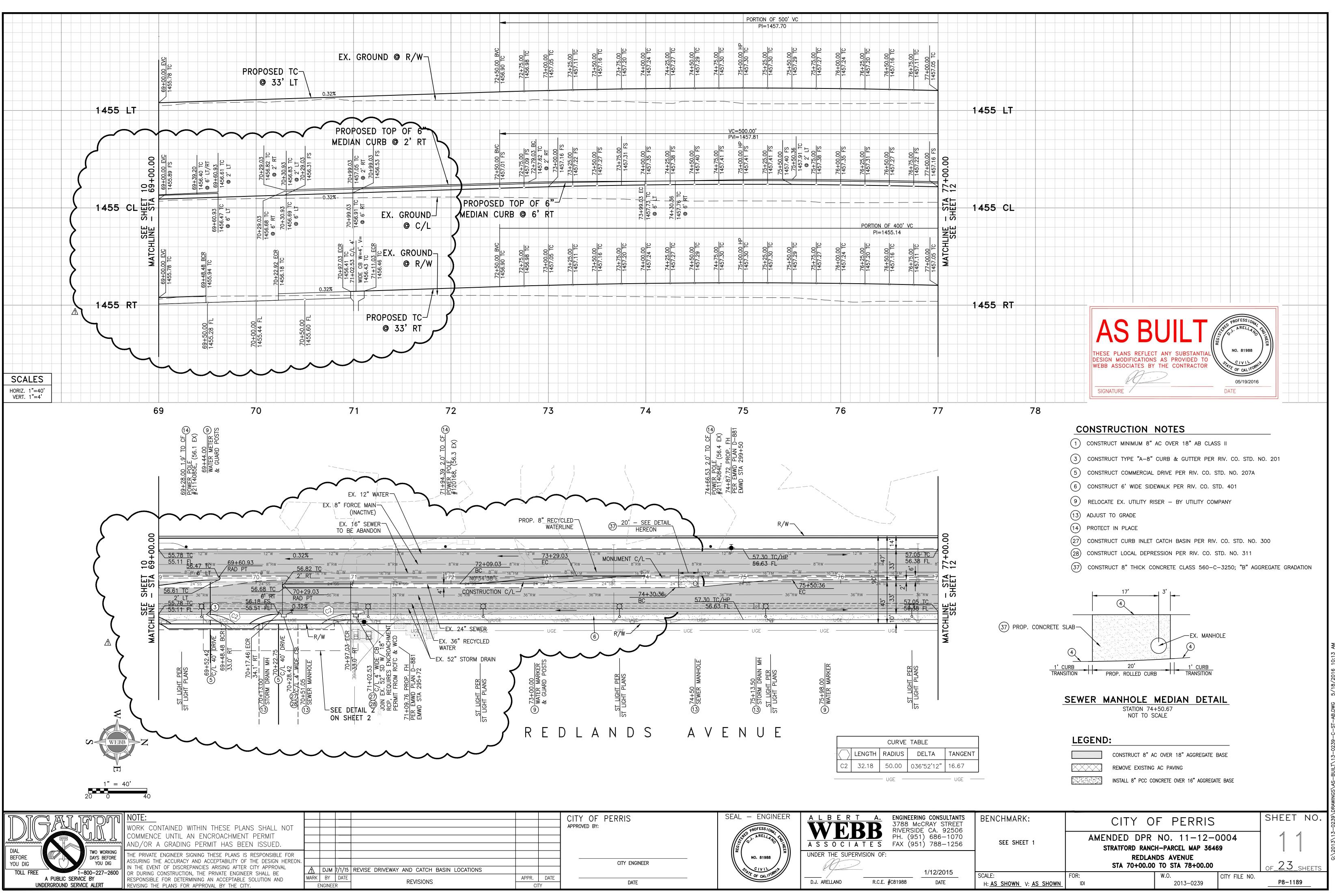




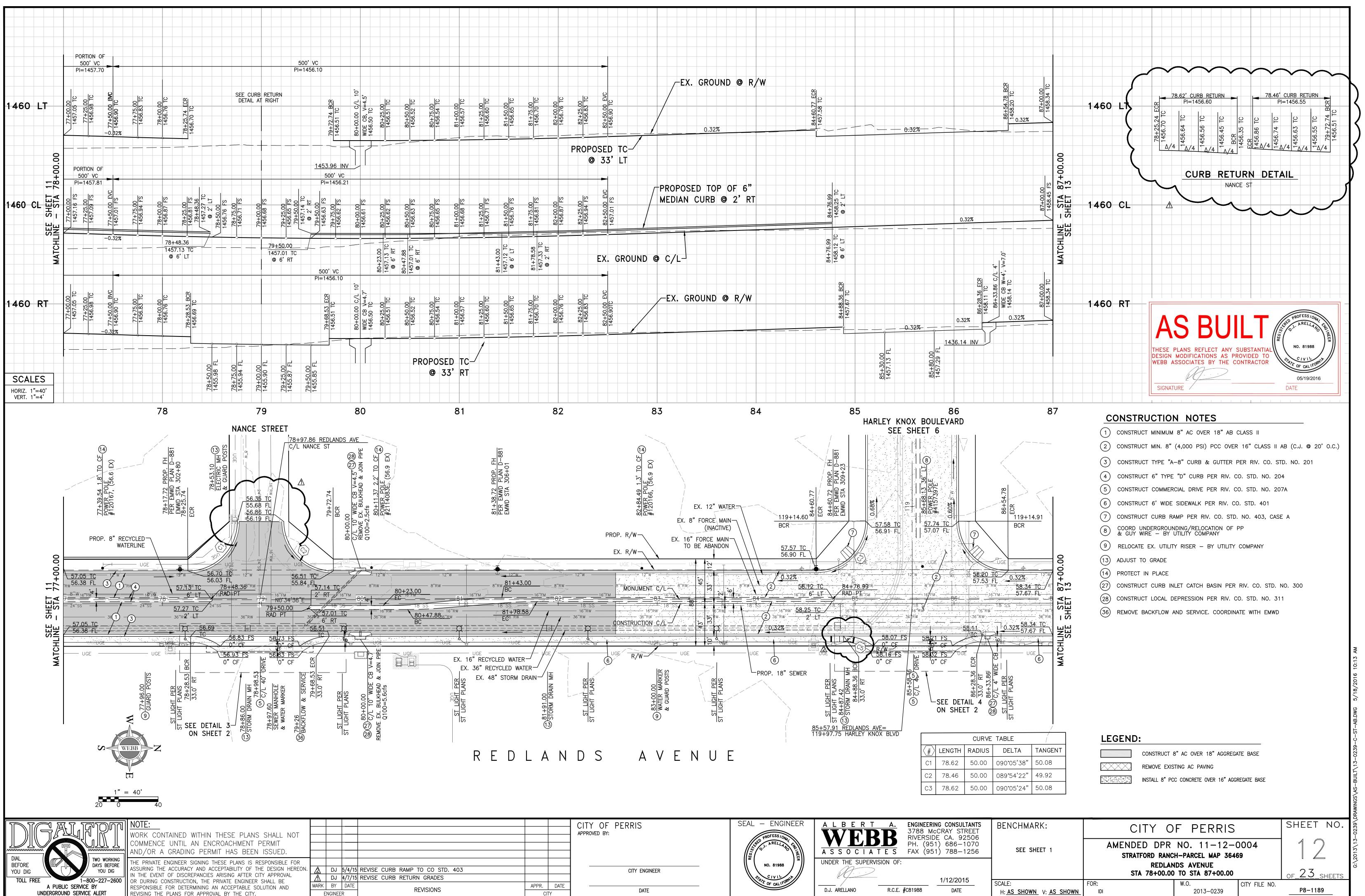
5\13-0239\DRAWINGS\AS-BUILT\13-0239-C-ST-AB.DWG 5/18/2



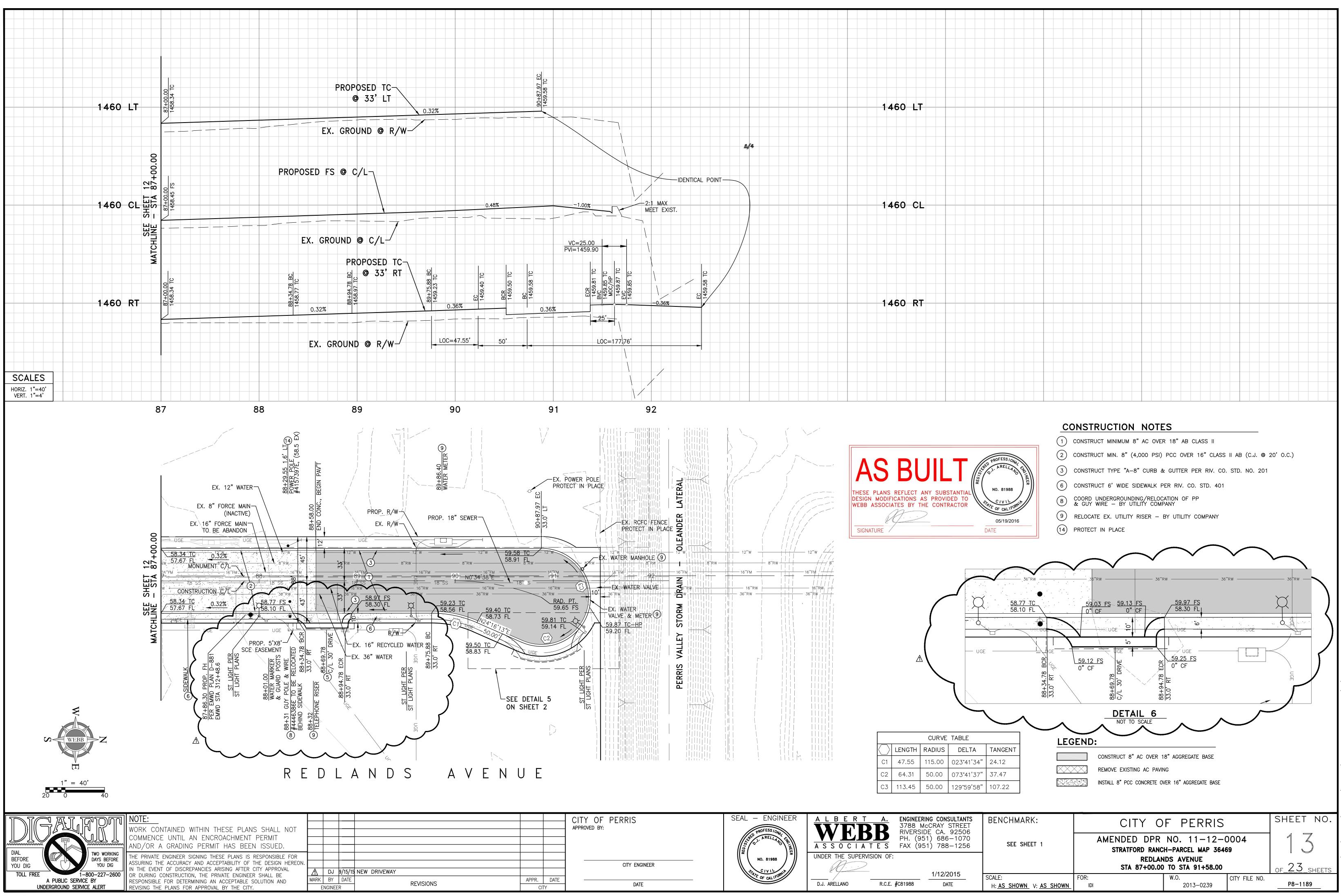
		CITY OF PERRIS	SEAL – ENGINEER	ALBERTA. ENGINEE	ERING CON
		APPROVED BY:			McCRAY
			PROFESS IONA		SIDE CA.
			Set S. ARELLAN, CH		951) 686
				ASSOCIATES FAX (9	951) 788
				UNDER THE SUPERVISION OF:	
		CITY ENGINEER	NO. 81988	M	
			1 CIVIL MIR	V.C.	1/1
APPR.	DATE		THE OF CALIFORT	/	
CIT		DATE		D.J. ARELLANO R.C.E. #C81988	DA

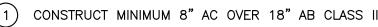


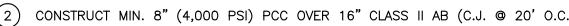
					CIATES FAX (951
				NO. 81988	SUPERVISION OF:
			CITY ENGINEER		
SIN LOCATIONS				ST CIVIL RENIA	
	APPR.	DATE	DATE	D.J. ARELLANO	R.C.E. #C81988
			DATE	D.J. ARELLANU	



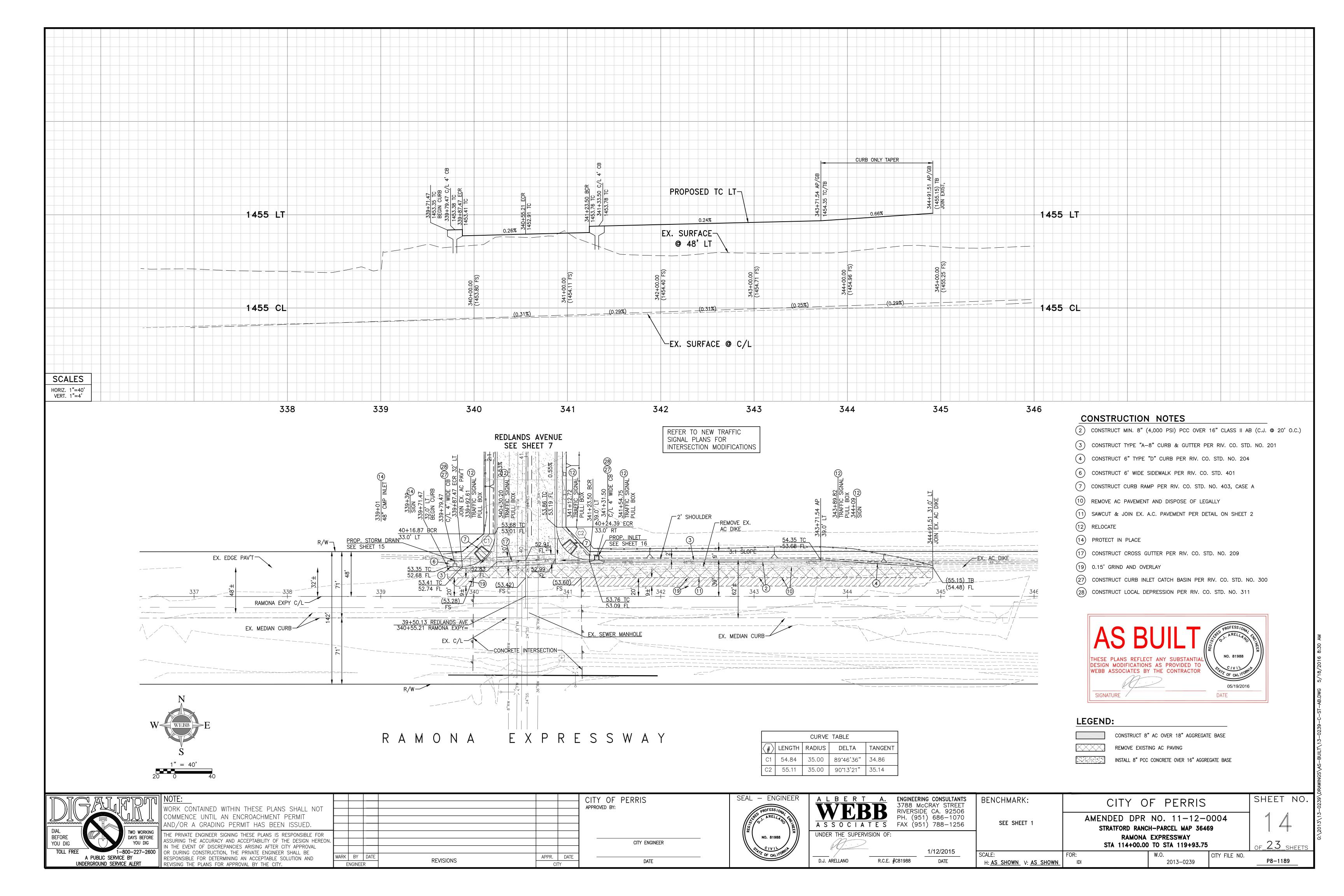
			CITY OF PERRIS APPROVED BY:	SEAL - ENGINEER	A L B E R T A.	ENGINEERING C 3788 McCRA RIVERSIDE C PH. (951) 6
403			CITY ENGINEER	NO. 81988	ASSOCIATES UNDER THE SUPERVISION OF:	FAX (951) 7
	APPR. Cl	DATE TY	DATE	THE OF CALIFORN	D.J. ARELLANO R.C.E.	#C81988

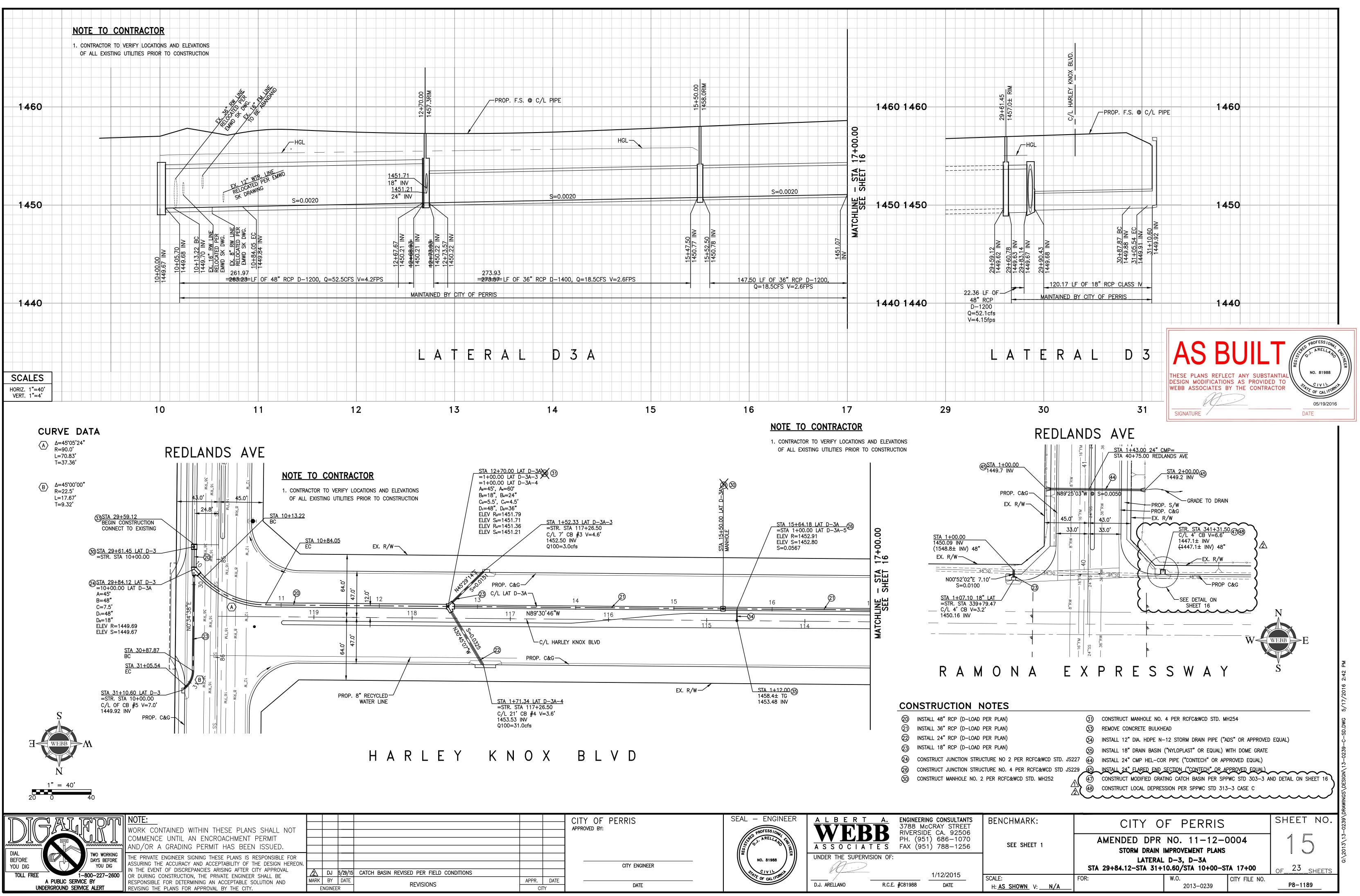






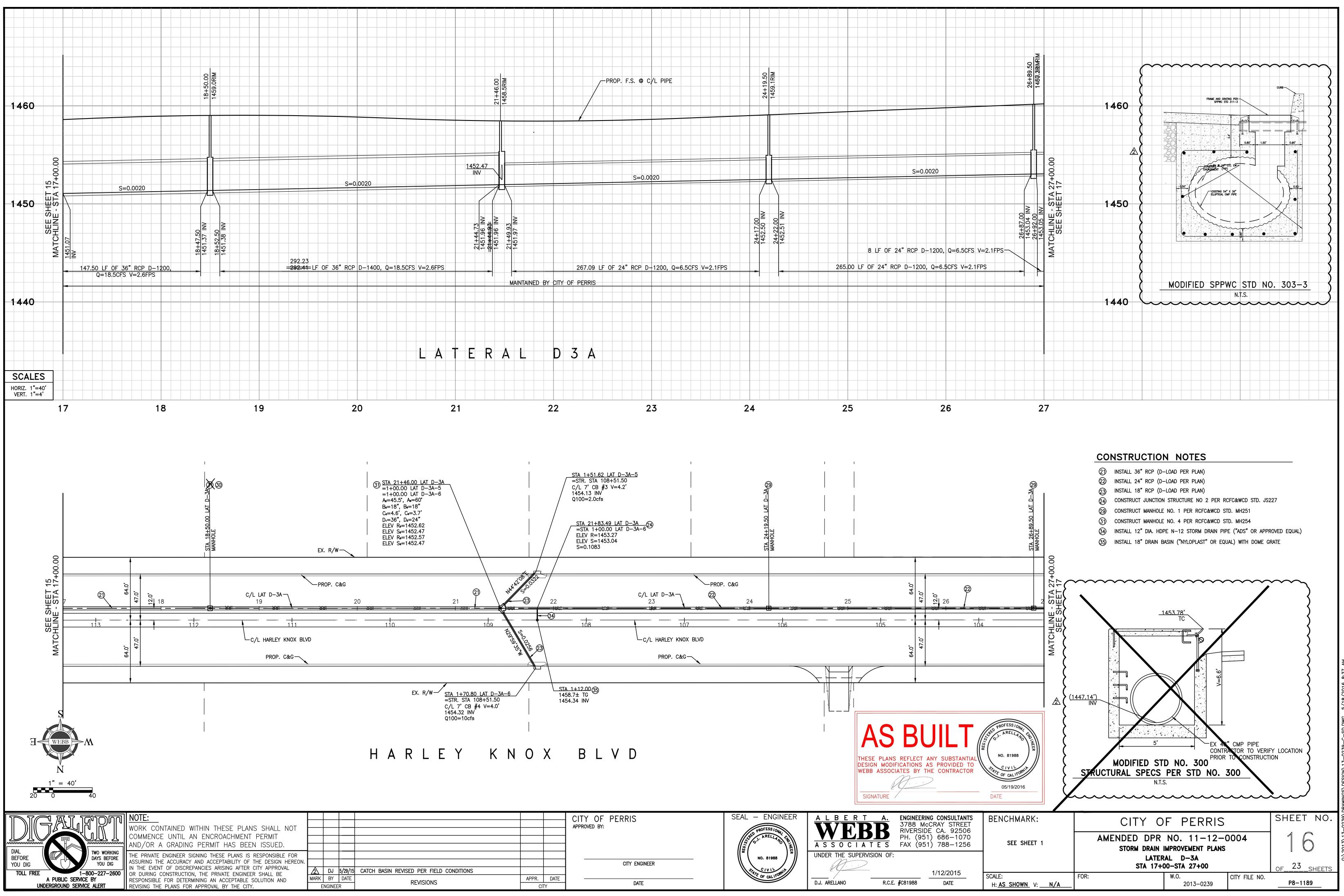
CONSULTANTS RAY STREET CA. 92506	BENCHMARK:	CITY O	F PERRIS		SHEET NO.
686–1070 788–1256	SEE SHEET 1	AMENDED DPR STRATFORD RANC	NO. 11-12-0 H-PARCEL MAP 3640		13
4/40/0045		REDLAN STA 87+00.00	of_23_sheets		
1/12/2015 DATE	SCALE: H: <u>AS_SHOWN_</u> V: <u>AS_SHOWN</u>	FOR: IDI	W.O. 2013-0239	CITY FILE NO.	P8-1189

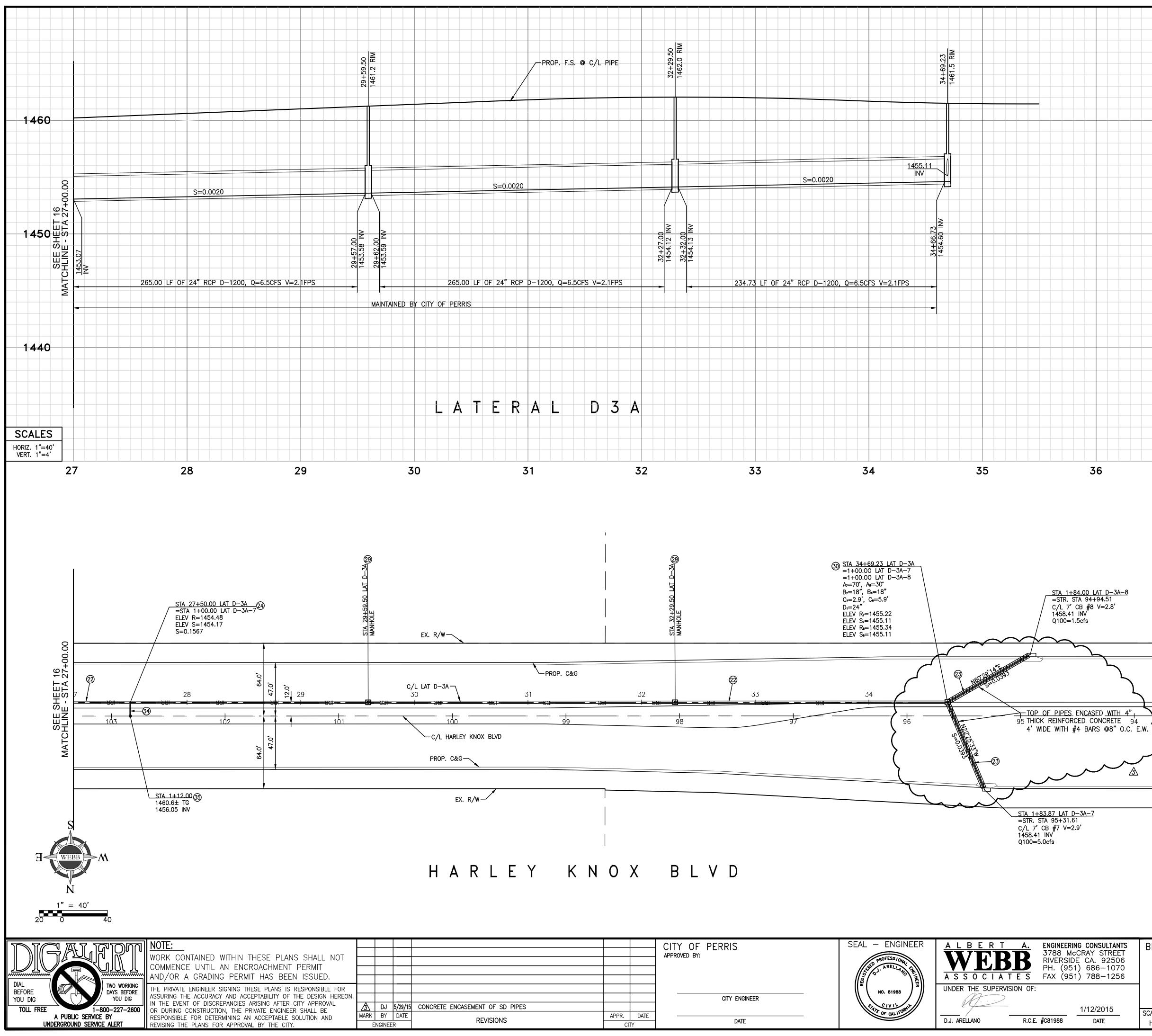




			APPROVED BY:			3788 McC
			AFFROVED DI.	D PROFESSIONAL		RIVERSIDE
				ARELLAND THE		PH. (951)
				REG	ASSOCIATES	FAX (951)
				⁻ NO. 81988 [∞]	UNDER THE SUPERVISION OF:	
			CITY ENGINEER			
CONDITIONS				OF CIVIL	E /	
	APPR.	DATE	DATE	OF CALIFOU	D.J. ARELLANO R.C.E	
	Cľ	TY	DAIL			. που 1300

	LATERAL D-3, D-3A STA 29+84.12-STA 31+10.60/STA 10+00-STA			
 SCALE:	FOR:	W.O.	CITY	
H: <u>AS_SHOWN_</u> V: <u>N/A</u>		2013–0239		



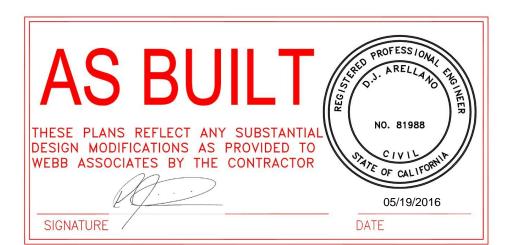


			CITY OF PERRIS	SEAL – ENGINEER	ALBERT A.	ENGINEERING
			APPROVED BY:			3788 McCR
				ED PROFESSIONAL		RIVERSIDE
				Lev S. ARELLAN CHE		PH. (951)
					ASSOCIATES	FAX (951)
				() ((²² () NO. 81988) ³⁷))	UNDER THE SUPERVISION OF:	
			CITY ENGINEER		M	
PES				ST CIVIL	P.J	1/
	APPR.	DATE		THE OF CALIFOR	D.J. ARELLANO R.C.E. #	#C81988
	Cľ	ΤY	DATE		D.J. ARELLANO R.C.E. $\frac{1}{7}$	#C01900

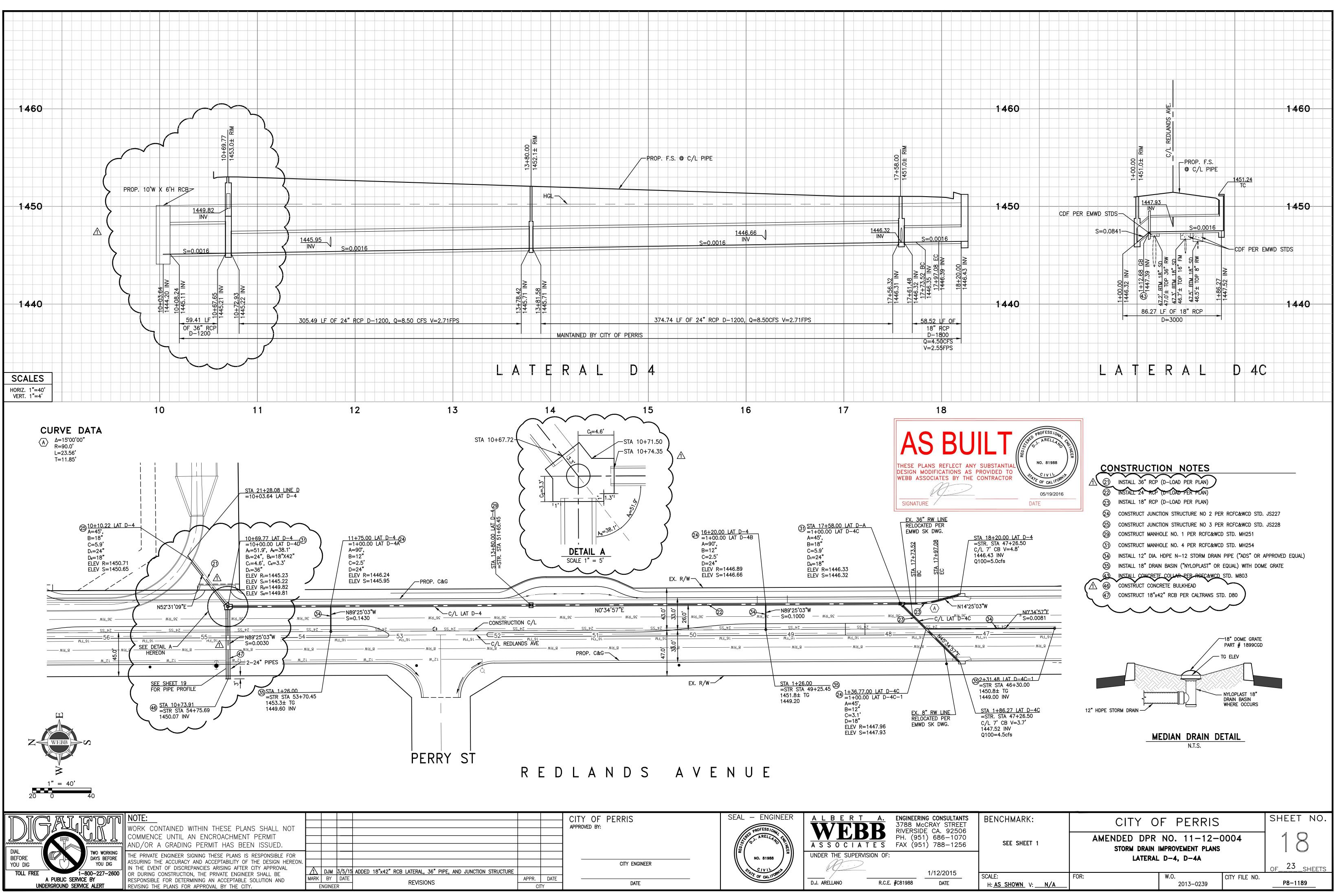
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CONSTRUCTION NOTES

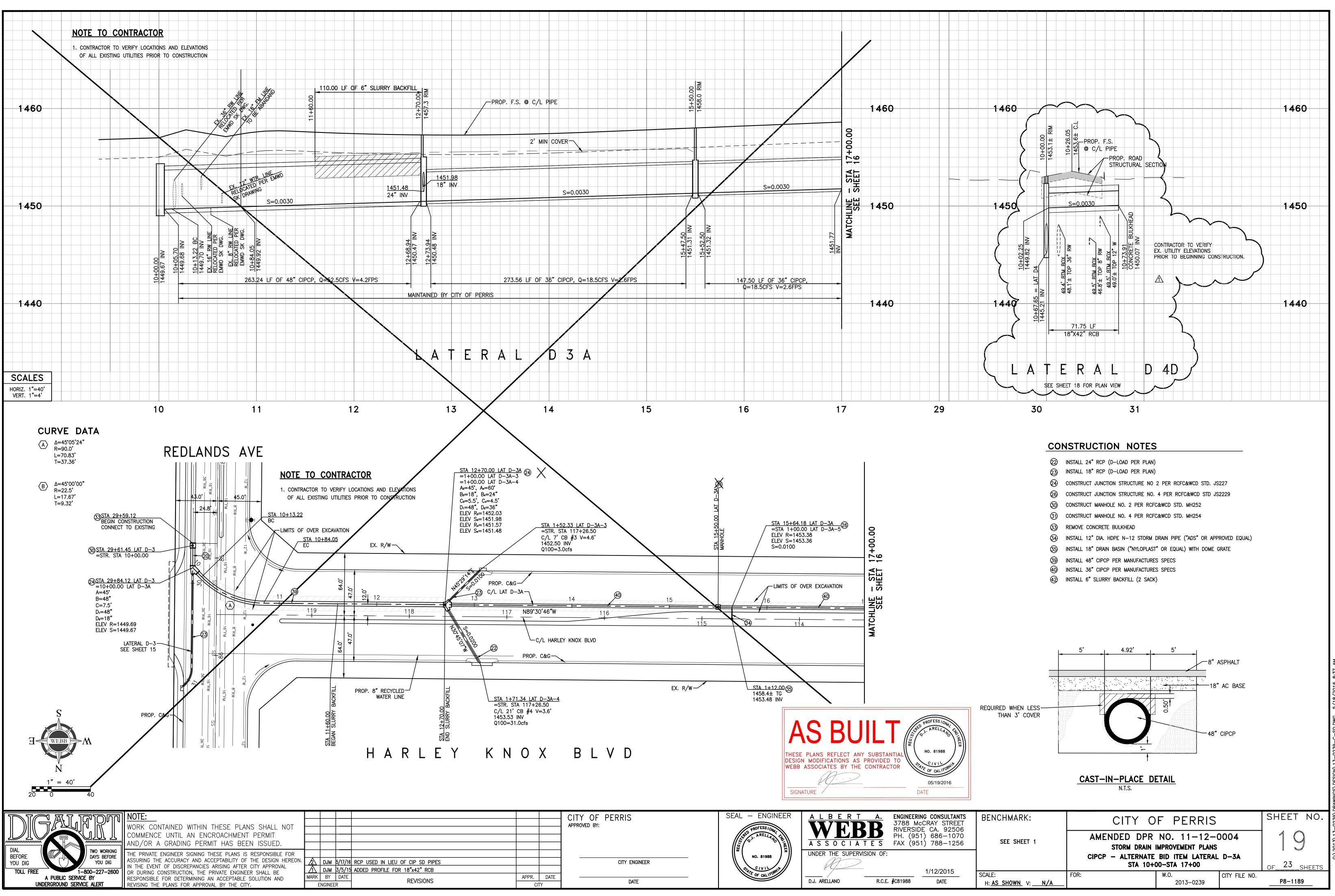
- 2 INSTALL 24" RCP (D-LOAD PER PLAN)
- (23) INSTALL 18" RCP (D-LOAD PER PLAN)
- (24) CONSTRUCT JUNCTION STRUCTURE NO 2 PER RCFC&WCD STD. JS227
- (29) CONSTRUCT MANHOLE NO. 1 PER RCFC&WCD STD. MH251 (3) CONSTRUCT MANHOLE NO. 4 PER RCFC&WCD STD. MH254
- 34) INSTALL 12" DIA. HDPE N-12 STORM DRAIN PIPE ("ADS" OR APPROVED EQUAL)
- 35 INSTALL 18" DRAIN BASIN ("NYLOPLAST" OR EQUAL) WITH DOME GRATE

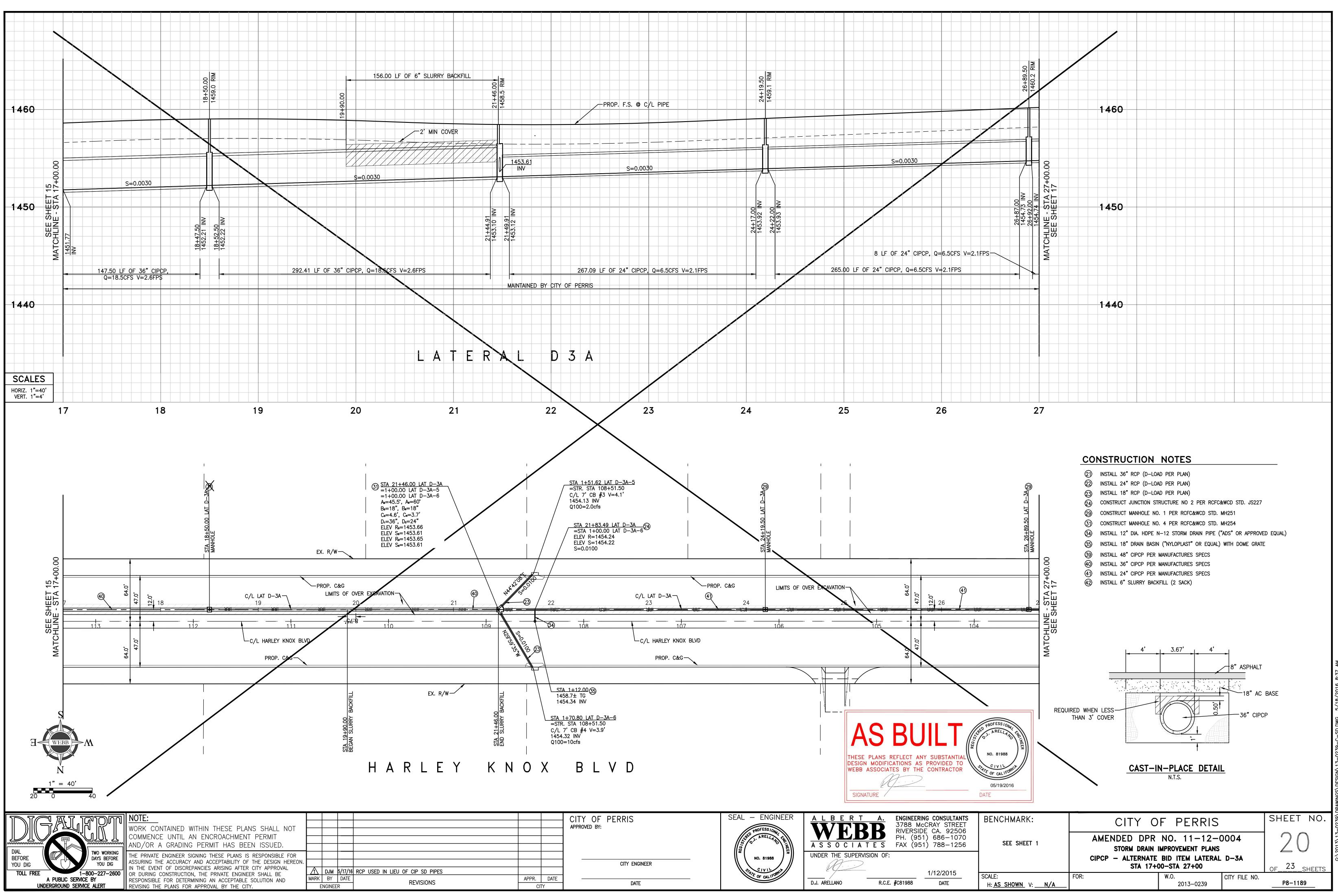


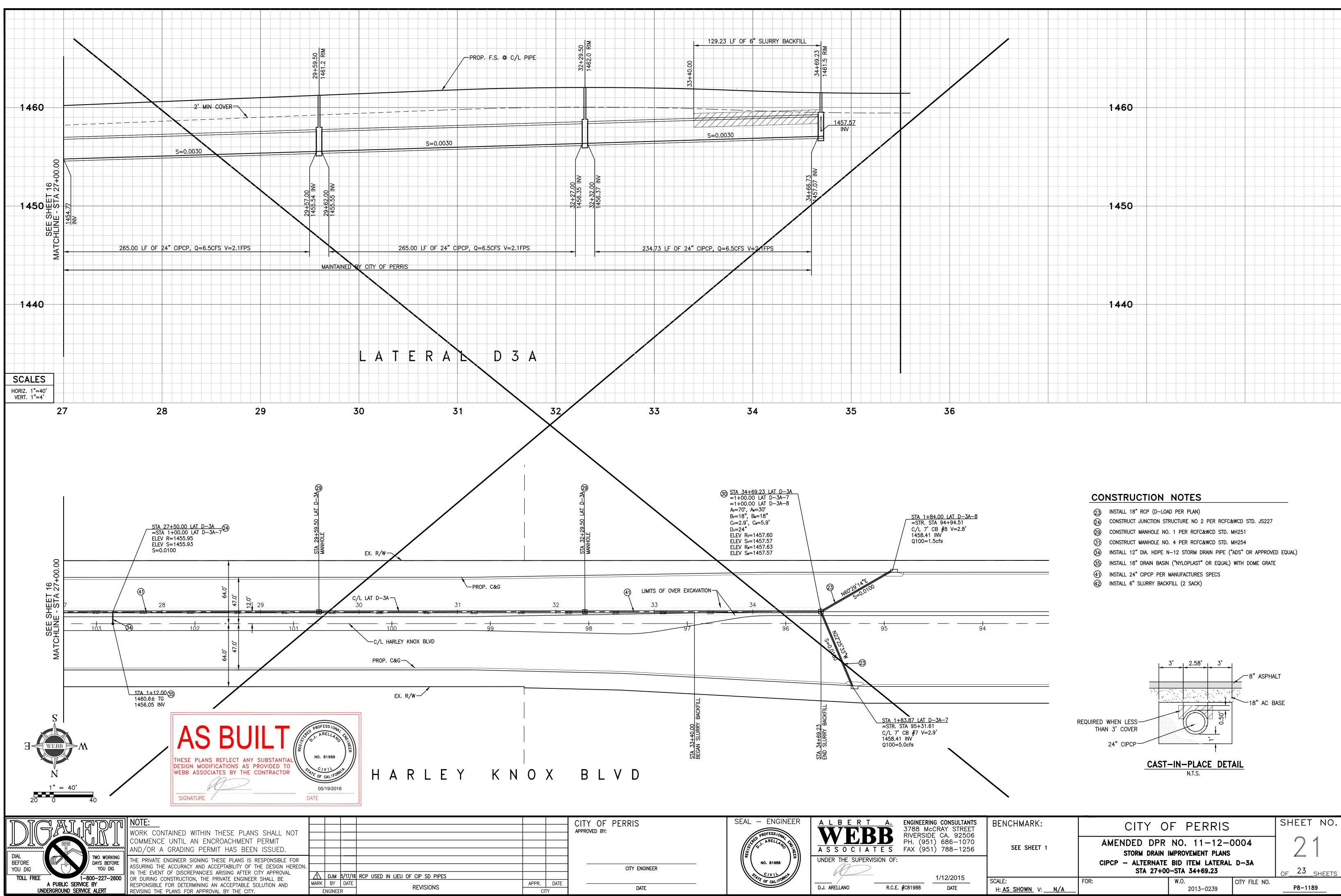
CONSULTANTS CAY STREET CA. 92506	BENCHMARK:	CITY O	F PERRIS		SHEET NO.
686–1070 788–1256	SEE SHEET 1	12-0004 Plans 17			
140/0045			RAL D-3A)-STA 34+69.23		of 23 sheets
/12/2015 DATE	SCALE: H: <u>AS SHOWN</u> V: <u>N/A</u>	FOR:	W.O. 2013-0239	CITY FILE NO.	P8-1189



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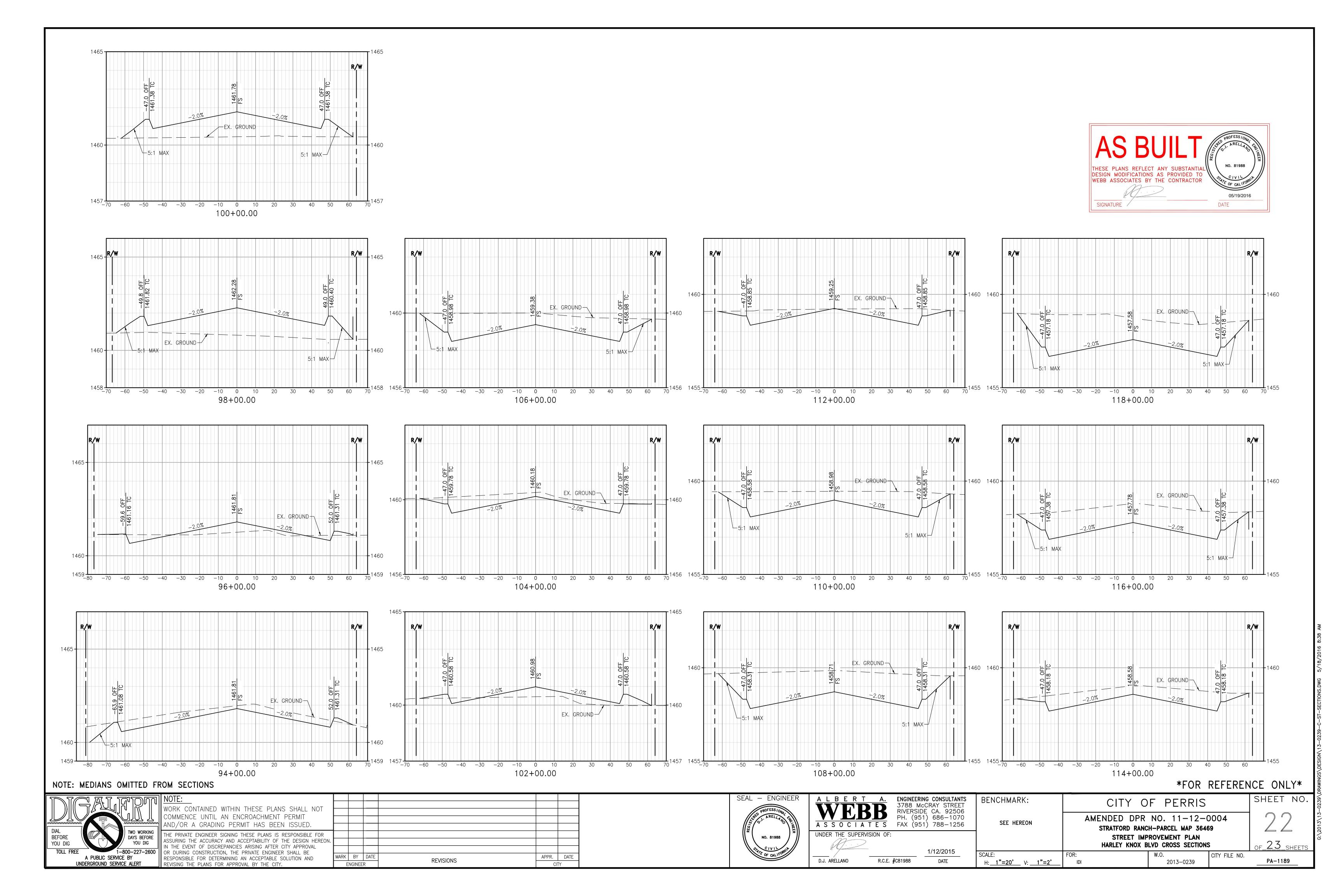


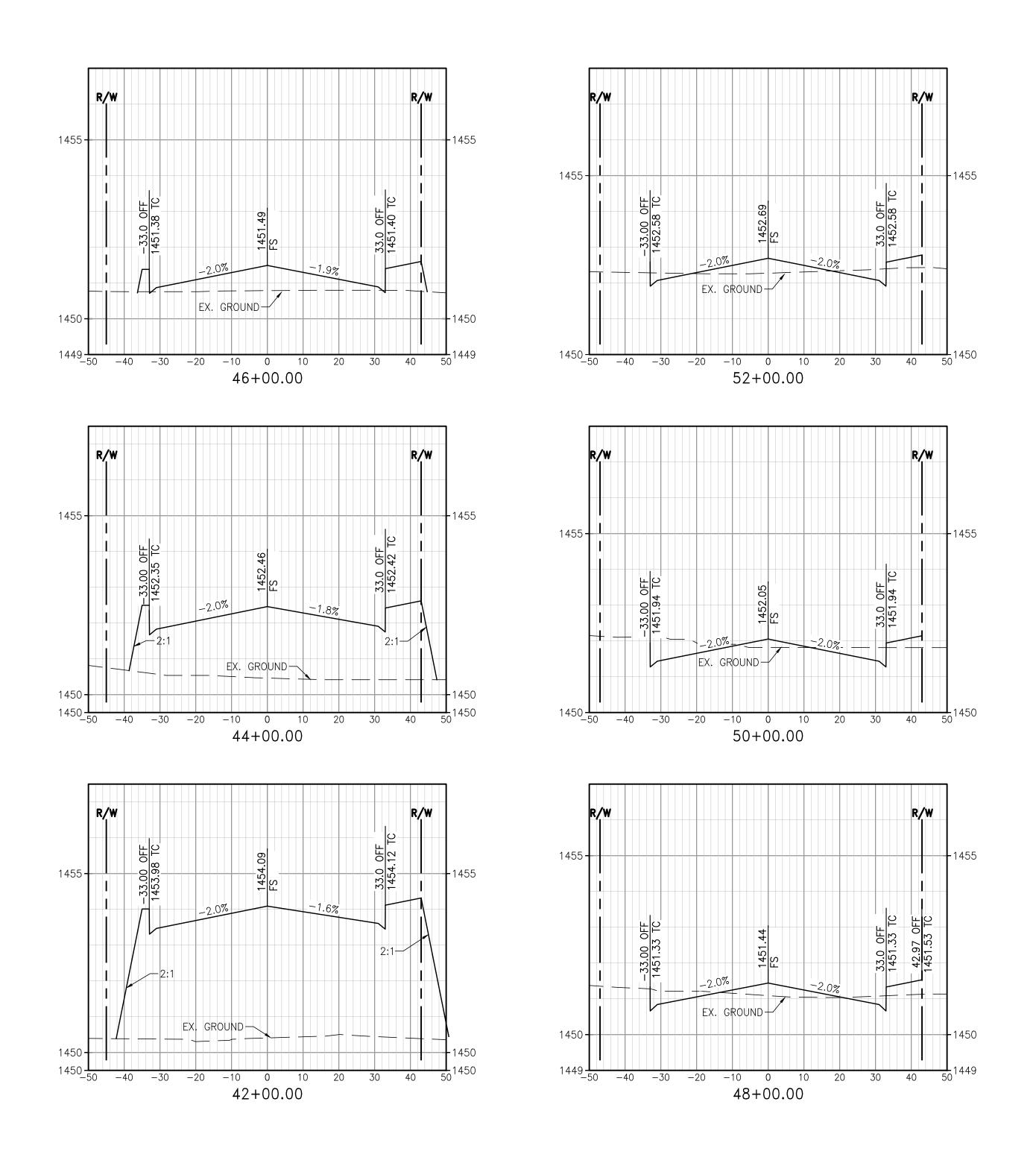


			Level Arella		RIVERSIDE PH. (951) FAX (951)
		CITY ENGINEER	NO. 81988		
			VI CIVIL	E	1
APPR.	DATE		OF CALIFO	D.J. ARELLANO R.C.E. #	
CL	TY	DATE		D.J. AKELLANO K.C.E. $\frac{1}{2}$	¥C81988

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	1450						
	1440						
36							

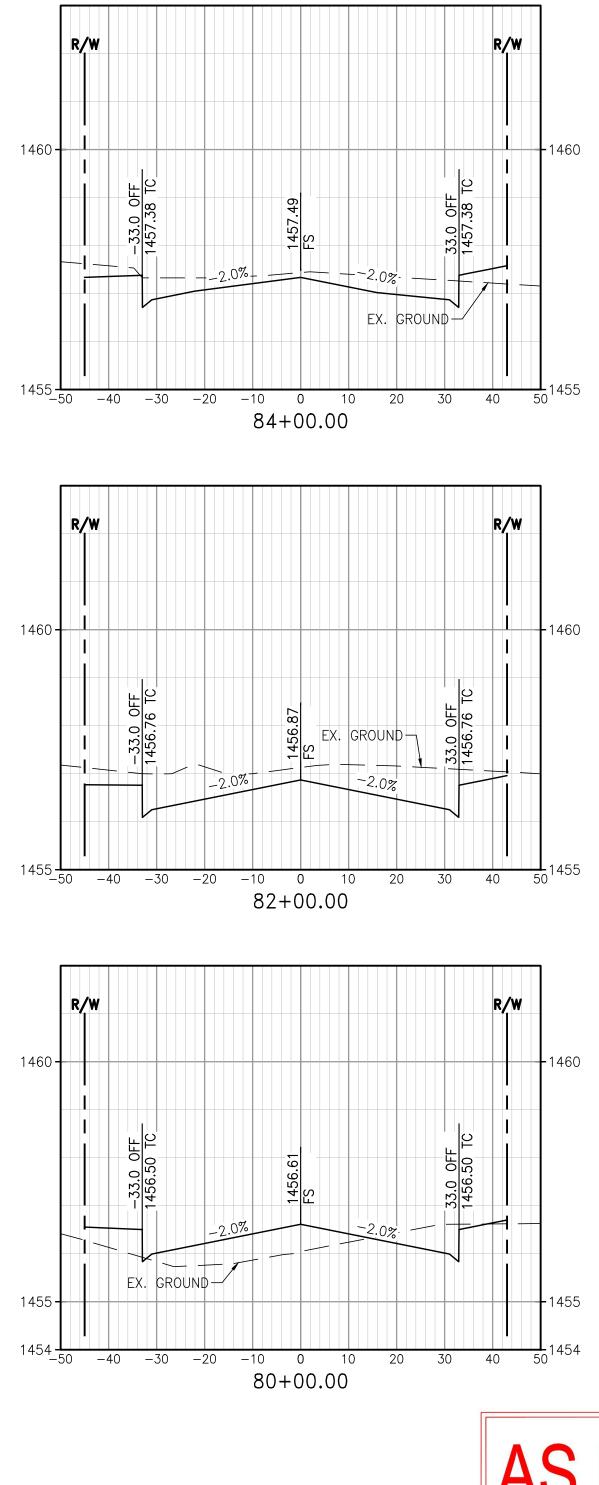






NOTE: MEDIANS OMITTED FROM SECTIONS

DIAL BEFORE YOU DIGTWO WORKING DAYS BEFORE YOU DIGNOTE:DIAL BEFORE YOU DIGTwo working Days Before YOU DIGWORK CONTAINED WITHIN THESE PLANS SHALL I COMMENCE UNTIL AN ENCROACHMENT PERMIT AND/OR A GRADING PERMIT HAS BEEN ISSUED.TOLL FREE A PUBLIC SERVICE BY UNDERGROUND SERVICE ALERTTHE PRIVATE ENGINEER SIGNING THESE PLANS IS RESPONSIBLE A CONSTRUCTION, THE PRIVATE ENGINEER SHALL BE RESPONSIBLE FOR DETERMINING AN ACCEPTABLE SOLUTION AND REVISING THE PLANS FOR APPROVAL BY THE CITY.	FOR IEREON.	Image: Constraint of the second se	SEAL - ENGINEER	A L B E T A. WEBBB A S S O C A S S C CA T CA S S C CA S S C CA C CA S S C I <thi< th=""> I I I <t< th=""></t<></thi<>
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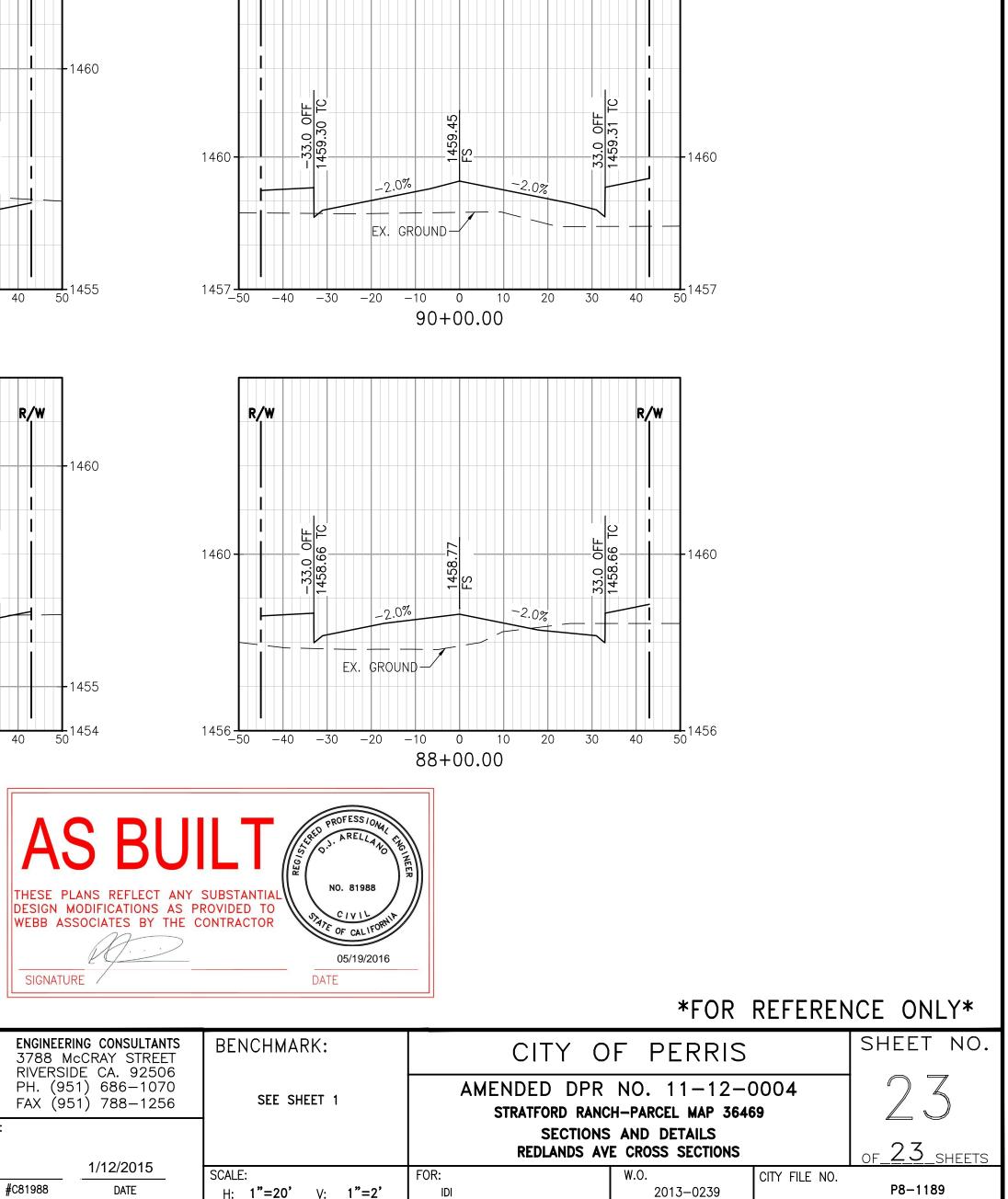




H:<u>1"=20'</u> V: <u>1"=2'</u>

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R/W

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2013-0239