

**PRELIMINARY HYDROLOGY STUDY  
251-271 AND 341-351 W. IMPERIAL HWY  
LA HABRA, CA  
TTM No. 19143**

**Project Address:**

251-271 and 341-351 W. Imperial Hwy  
La Habra, CA 90631

**Prepared For:**

The Olson Company  
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**Prepared: March 2021  
Revised: May 2021**

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**Preliminary Hydrology Study  
For  
251-271 and 341-351 W. Imperial Hwy  
TR 19143, La Habra**

This Preliminary Hydrology Study was prepared by C&V Consulting, Inc. under the supervision of Ryan J. Bittner, P.E.



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Ryan J. Bittner, R.C.E. 68167  
Principal, C&V Consulting, Inc.



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5/17/21  
Date

## **1.0 SITE DESCRIPTION:**

The proposed site is located at 251-271 and 341-351 W. Imperial Highway, in the City of La Habra, County of Orange. It encompasses two parcels APN 019-041-21 and APN 019-042-24. The site is currently occupied by several commercial and industrial businesses including used car dealers, a wooden pallet manufacturer, and a gymnastics center. The site is bounded by single family homes to the north, commercial development to the east and west, and W. Imperial Highway to the south. Per the City of La Habra General Plan 2035, Land Use Plan Diagram the site is located within the Residential Multi-Family 1 category.

## **2.0 PURPOSE OF STUDY:**

The purpose of this report is to provide quantitative information to verify the design of the storm drain infrastructure and hydrologic methodology of the project site. The values and statements within confirm the subject site is designed and planned in accordance with the Orange County Hydrology Manual and the City of La Habra drainage requirements.

## **3.0 EXISTING CONDITIONS:**

The existing site consists of 6 industrial buildings and warehouses. A semi-subterranean truck loading dock is located at the central portion of the site. Vegetation on-site is sparse and located within planters adjacent to the buildings. The existing building coverage is approximately 65,031 square feet, the existing landscaping coverage is approximately 4,275 square feet, and the AC coverage is approximately 144,465 square feet.

The site generally sheet flows overland in the southwesterly direction toward W. Imperial Highway. There is approximately 7' of fall in the westerly direction across the northern property line. There is approximately 8' of fall in the westerly direction along Imperial Highway. There is approximately 10' of fall in the southerly direction along the west and east property lines.

Along the rear of the site there are significant down slopes in the private yards of the single-family homes above. The slopes range in height from approximately 13' to 25'. There are a combination of timber and other "random material" retaining devices in the slope or at the bottom of slope, all of which are in relatively poor condition. At the northwesterly corner of the site, this slope encroaches into the site up to 20' horizontally. Accordingly, the single-family home rear yards are draining onto the project site.

There does not appear to be any significant on-site storm drain facilities. There are a couple of small drop inlet catch basins that appear to outlet to W. Imperial Highway through parkway culverts. The site generally drains overland to W. Imperial Highway and those flows are carried westerly in the W. Imperial Highway curb and gutter to 3 catch basins that are owned and maintained by Caltrans. There is a grated inlet catch basin at the center of the project frontage which drains directly south across Imperial Highway via a 24" HDPE. There is a curb inlet catch basin located approx. 60' from the easterly property line which drains directly south across Imperial Highway via a 24" HDPE. There is a third catch basin approximately 30' west of the westerly property line which drains directly across W. Imperial Highway via a 24" ACP. There do not appear to be any storm drain facilities running east/west, parallel to the site frontage. All flows in the immediate project vicinity ultimately drain and/or connect directly to the Imperial Channel, which is an Orange County Flood Control facility, located on the south side of W. Imperial Highway behind a large screen wall. Runoff continues west in the Imperial Channel to the Coyote Creek Channel. The Coyote Creek Channel



confluences with the San Gabriel River before discharging into the Pacific Ocean just north of the Anaheim Bay.

Refer to the Existing Conditions Hydrology Map located within Appendix A of this report for additional information.

#### **4.0 PROPOSED CONDITIONS:**

The proposed development will consist of 21 buildings consisting of 2- story triplexes and 3 story townhomes for a total of 117 units. Both building types will have side-by-side or tandem garage parking. The proposed building coverage is approximately 120,779 square feet, the drive aisle and open parking coverage is approximately 58,682 square feet, and the open space (public and private) lot coverage is approximately 34,310 square feet. Based on the proposed land use of the residential lot, the imperviousness was assumed to be 85% per the Orange County Hydrology Manual, Figure C-4. Actual imperviousness will be calculated during final engineering, and hydrology calculations will be updated.

The project proposes onsite private drive aisles, parking areas, hardscape, and landscaped areas, and is accessed by one entrance along Imperial Highway. Drive aisles and parking areas will consist of asphalt concrete pavement and sidewalks comprised of Portland concrete cement (PCC). Decorative hardscape is proposed within the walkways, common areas and portions of the drive aisles. Landscaping will be incorporated in open space areas including vegetation and street trees. The site proposes 28 open parking spaces and 234 garage parking spaces. The open space areas will be maintained by the appointed Homeowners Association (HOA).

The proposed residential development will be divided into fourteen (14) Drainage Areas which will be graded to match the existing drainage condition. The storm water will be collected and conveyed by a series of area drains and street surface flow, towards curb opening catch basins & bio-filtration devices. These devices will be sized to treat the required water quality stormwater runoff flow rate and have been designed conservatively. The bio-filtration chambers will contain a d-vert by-pass system and overflow pipe to allow the conveyance of larger storm events. At catch basin #3 in sub-area P4 and at catch basin #7 in sub-area P12, runoff will be conveyed into the proposed catch basin which will direct low flows into the biofiltration vaults. When the storm event exceeds the biofiltration treatment capacity, runoff will overflow in the proposed catch basin and be conveyed offsite via proposed parkway culverts that outlet to W. Imperial Highway. In subareas P6 and P8 (catch basins #4 and #5 accordingly) runoff will be conveyed into the proposed catch basin which will direct low flows into the biofiltration vaults. When the storm event exceeds the biofiltration vault treatment capacity, flows will be diverted into the proposed junction structure and then through a proposed parkway culvert that will discharge onto W. Imperial Highway. In sub-area P10, Catch Basin #6, runoff will be conveyed into the proposed catch basin. Low flows will be routed into the biofiltration vaults. When the treatment capacity of the biofiltration vaults is exceeded, runoff will be directed into a proposed stormwater sump pump system where it will be pumped into W. Imperial Highway via a proposed parkway culvert. Runoff that enters W. Imperial Highway will drain into the Coyote Creek Channel and eventually the Pacific Ocean.

Along the northern property line of the site there are significant down slopes in the private yards of the single-family homes to the north of the site. The slopes range in height from approximately 13' to 25'. There are a combination of timber and other "random material" retaining devices in the slope or at the bottom of slope, all of which are in relatively poor condition.

At the northwesterly corner of the site, this slope encroaches into the site up to 20' horizontally. Accordingly, the single-family home rear yards are draining onto the project site. A proposed catch basin and concrete drainage swale along the northern property line have been incorporated into the design in order to collect and convey offsite run-on from the slope to the northwesterly corner of the site. These flows will be conveyed through the site in a separate underground storm drain system. The existing slope will not be altered in the proposed condition. The offsite drainage has been quantified in the existing and proposed condition as drainage area X1. This drainage area consists of 0.11 ac of the proposed site area and 1.29 ac of offsite area. Near the northeast corner of the site, there is additional offsite run-on from an existing alley which is quantified in the existing and proposed condition as drainage area X2. This drainage area consists of 0.17 ac of offsite area. Another proposed catch basin will collect this run-on and will convey the flows through the site in a separate underground storm drain pipe. All offsite run-on flows will not co-mingle with any onsite flows.

Refer to the Proposed Conditions Hydrology Map located within Appendix A of the report.

## **5.0 METHODOLOGY:**

The existing/proposed subarea was analyzed for acreage, land-use, soil type, peak flow rate, and time of concentration according to the Rational Method.

A perviousness value was calculated for the existing subarea based on site topography, and the proposed condition was assumed an 85% imperviousness based on residential land use.

## **6.0 RESULTS:**

| <b>Existing Conditions</b>                 |                         |                         |                          |                          |                            |
|--|-------------------------|-------------------------|--------------------------|--------------------------|----------------------------|
| <b>Drainage Area</b>                       | <b>Area (ac)</b>        | <b>Q10 (cfs)</b>        | <b>Q25 (cfs)</b>         | <b>Q100 (cfs)</b>        | <b>T<sub>c</sub> (min)</b> |
| X1 (offsite)                               | 1.40                    | 4.96                    | 5.93                     | 7.64                     | 5.00                       |
| X2 (offsite)                               | 0.17                    | 0.46                    | 0.55                     | 0.71                     | 7.86                       |
| X3   | 0.30                    | 1.09                    | 1.30                     | 1.67                     | 5.00                       |
| X4   | 1.33                    | 3.71                    | 4.55                     | 6.0                      | 10.20                      |
| X5   | 0.15                    | 0.48                    | 0.57                     | 0.73                     | 6.32                       |
| X6   | 1.67                    | 3.44                    | 4.22                     | 5.58                     | 14.02                      |
| X7   | 0.11                    | 0.40                    | 0.48                     | 0.61                     | 5.00                       |
| X8   | 1.24                    | 2.65                    | 3.27                     | 4.33                     | 13.22                      |
| <b>Total<br/>(Including offsite runon)</b> | <b>4.80<br/>(6.36*)</b> | <b>9.80<br/>(15.22)</b> | <b>12.04<br/>(18.52)</b> | <b>15.91<br/>(24.25)</b> |                            |

| <b>Proposed Conditions</b>   |                         |                        |                        |                         |                            |
|--|-------------------------|------------------------|------------------------|-------------------------|----------------------------|
| <b>Drainage Area</b>   | <b>Area (ac)</b>        | <b>Q10 (cfs)</b>       | <b>Q25 (cfs)</b>       | <b>Q100 (cfs)</b>       | <b>T<sub>c</sub> (min)</b> |
| X1 (offsite)   | 1.40                    | 4.96                   | 5.93                   | 7.64                    | 5.00                       |
| P3   | 0.06                    | 0.22                   | 0.26                   | 0.33                    | 5.00                       |
| P4   | 1.50                    | 2.39                   | 2.98                   | 3.99                    | 17.75                      |
| <b>Total at Catch Basin #3/<br/>Parkway Culvert #1<br/>(Including offsite runon)</b> | <b>1.56<br/>(2.96*)</b> | <b>2.49<br/>(7.45)</b> | <b>3.10<br/>(9.03)</b> | <b>4.15<br/>(11.79)</b> | <b>17.75</b>               |
| P5   | 0.03                    | 0.11                   | 0.13                   | 0.17                    | 5.00                       |

|   |                               |                              |                              |                              |              |
|---|-------------------------------|------------------------------|------------------------------|------------------------------|--------------|
| P6  | 0.64                          | 1.21                         | 1.48                         | 1.97                         | 13.79        |
| <b>Total at Catch Basin #4</b>  | <b>0.67</b>                   | <b>1.27</b>                  | <b>1.55</b>                  | <b>2.06</b>                  | <b>13.79</b> |
| P7  | 0.11                          | 0.40                         | 0.47                         | 0.61                         | 5.00         |
| P8  | 0.95                          | 1.61                         | 2.01                         | 2.68                         | 16.03        |
| <b>Total at Catch Basin #5</b>  | <b>1.06</b>                   | <b>1.80</b>                  | <b>2.24</b>                  | <b>2.99</b>                  | <b>16.03</b> |
| <b>Total at Proposed JS/<br/>Parkway Culvert #2</b>                                   | <b>1.73</b>                   | <b>2.93</b>                  | <b>3.65</b>                  | <b>4.88</b>                  | <b>16.32</b> |
| P9  | 0.05                          | 0.18                         | 0.22                         | 0.28                         | 5.00         |
| P10   | 0.55                          | 1.32                         | 1.58                         | 2.02                         | 10.14        |
| <b>Total at Catch Basin #6/<br/>Parkway Culvert #3</b>                                | <b>0.60</b>                   | <b>1.44</b>                  | <b>1.72</b>                  | <b>2.21</b>                  | <b>10.14</b> |
| P11   | 0.22                          | 0.79                         | 0.94                         | 1.21                         | 5.06         |
| P12   | 0.68                          | 1.40                         | 1.72                         | 2.28                         | 11.86        |
| <b>Total at Catch Basin #7/<br/>Parkway Culvert #4<br/>(Including offsite runoff)</b> | <b>0.90</b><br><b>(1.07)</b>  | <b>1.85</b><br><b>(2.31)</b> | <b>2.28</b><br><b>(2.83)</b> | <b>3.01</b><br><b>(3.74)</b> | <b>11.86</b> |
| <b>Total</b>  | <b>4.80</b><br><b>(6.36*)</b> | <b>14.13</b>                 | <b>17.23</b>                 | <b>22.62</b>                 | <b>--</b>    |

Note: All time of concentrations indicated above refer to the 100-year storm event.

\*Area includes offsite drainage areas

#### Catch Basin Sizing

Catch basin Sizing was analyzed for the 100-year storm event peak flow. Refer to Appendix C for Catch Basin Sizing.

#### Pipe Sizing

Onsite underground storm drain pipe will be analyzed for the 100-year storm event peak flow rate utilizing WSPG software and provided during final engineering.

#### Parkway Culvert Sizing

Parkway Culvert Sizing was analyzed for the 100-year storm event peak flow, including offsite runoff areas. Refer to Appendix C for Parkway Culvert Sizing.

#### Wall Knockout Sizing

Wall knockouts will provide an emergency overland escape route during larger storm events. Calculations for one half block (8" x 8") knockout are provided in Appendix C.

| <b>Drainage Area</b> | <b>Q100 (cfs)</b> | <b>Knockout Size</b> |
|----------------------|-------------------|----------------------|
| P4                   | 4.15              | 3 Blocks             |
| P6                   | 2.06              | 2 Blocks             |
| P8                   | 2.98              | 3 Blocks             |
| P12                  | 3.03              | 3 Blocks             |

#### 100-Year Water Surface Ponding Exhibit/ Calculations

Water surface elevations for the 100-year storm event peak flow rates will verify that the proposed finish floor elevations are set at least 1 foot above the water surface elevation. A ponding exhibit has

been prepared based on the 100-year water surface elevation tributary to each subarea. Refer to Appendix C.

## **7.0 CONCLUSION:**

The results from this hydrology study demonstrate that the proposed condition of the site will generate a lower peak runoff flowrate than the existing condition of the site. This is a result of the increase in pervious area in the proposed condition. Since the peak flows are decreased in the proposed condition, no onsite detention is required. Existing historic drainage patterns and discharge location will be preserved and has been incorporated into the proposed drainage design.

## **8.0 DESIGN PARAMETERS:**

1. The onsite drainage area was analyzed for a 10, 25, 100-Year storm event using Rational Method Analysis per the County of Orange Hydrology Manual.
2. The drainage area is located in Soil Groups D per the Orange County Public Works Technical Guidance Document (TGD).
3. The infiltration rate for the pervious area as a function of soil group,  $F_p$ , is 0.20 inches/hour, according to page C-13 of the Hydrology Manual.
4. Onsite overflow structures have been designed for a 100-Year storm event.
5. An estimated 85% impervious coverage was assigned to the proposed condition of the project site. Existing impervious coverage was calculated to be approximately 98% utilizing field survey topography.
6. Time of concentration  $T_c$  were calculated by using the County of Orange Hydrology Manual to calculate flow rates and volume amounts.
7. There is offsite run-on tributary to the site.

## **9.0 REFERENCES:**

1. Orange County Hydrology Manual dated October 1986
2. Hydraflow Express Extension for Autodesk AutoCAD Civil 3D
3. Existing Storm Drain As-Built Plans
4. Orange County Technical Guidance Document Figure XVI-2a, NRCS Hydrologic Soils Groups

# **APPENDIX A**

## **HYDROLOGY MAPS**

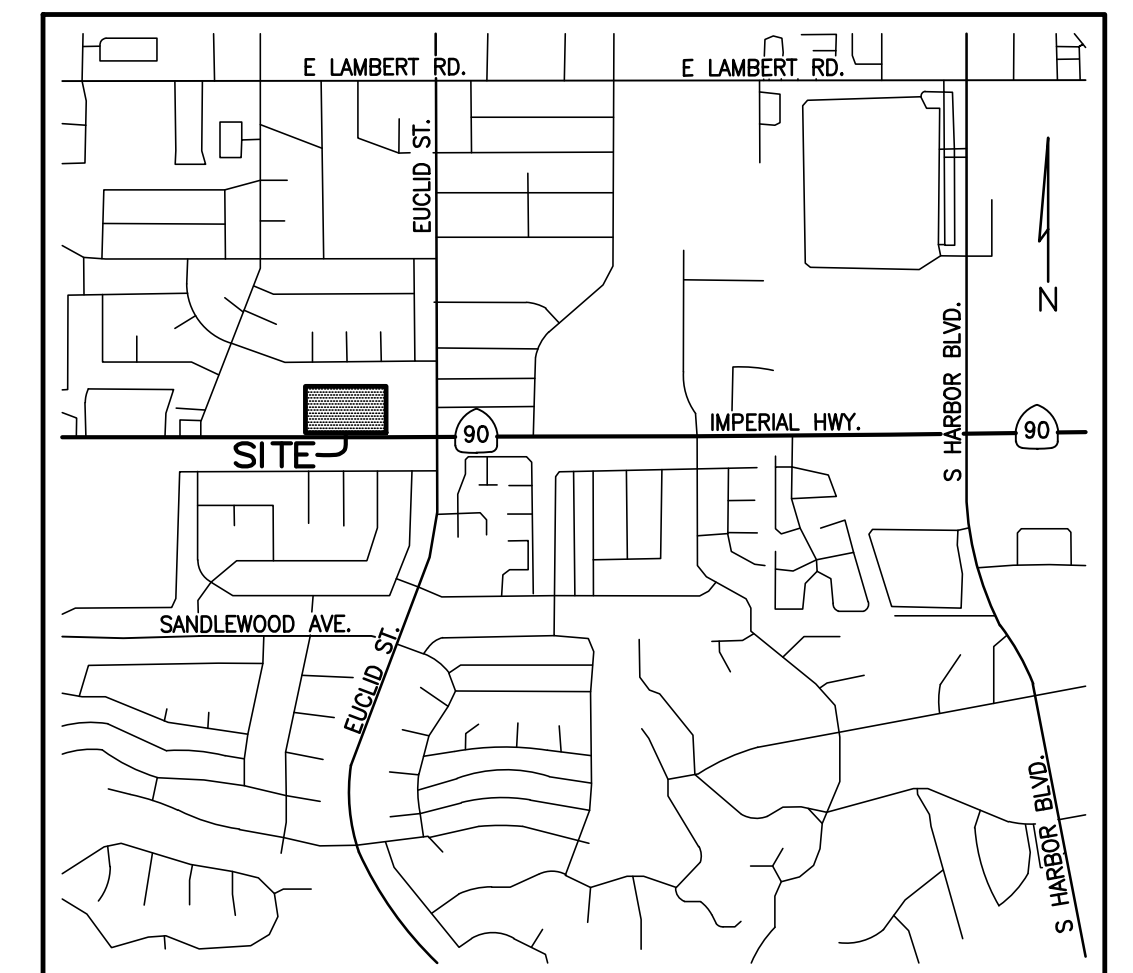
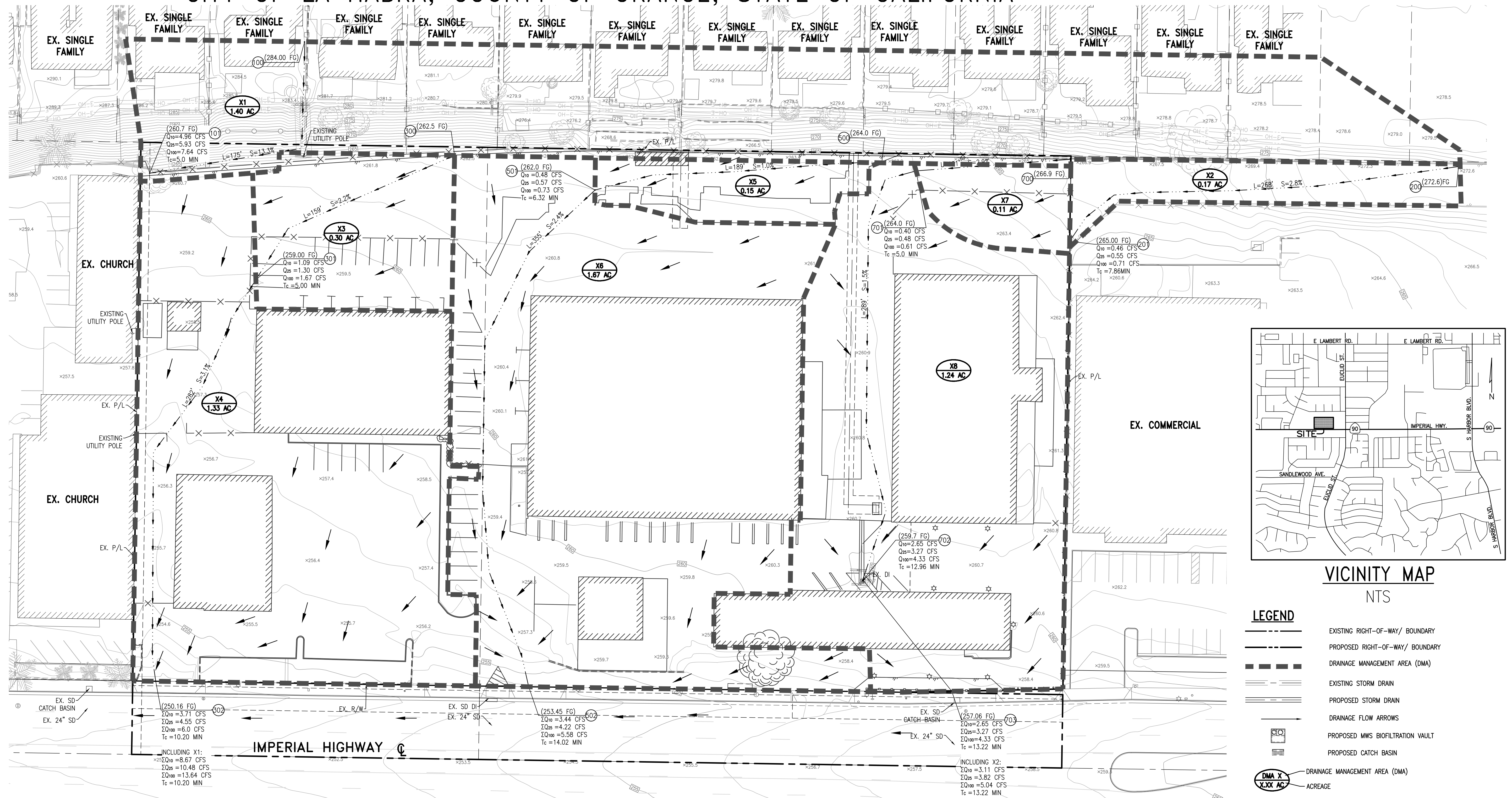
# **Existing Conditions Hydrology Map**

# EXISTING CONDITIONS HYDROLOGY MAP

TR 19143

## 251-271 AND 341-351 IMPERIAL HIGHWAY

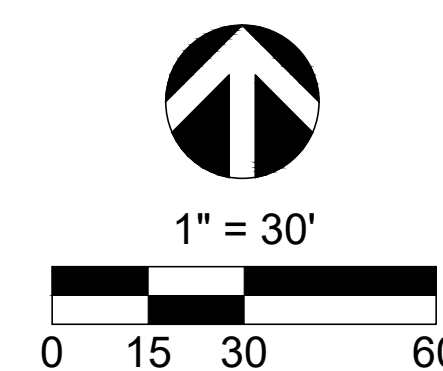
CITY OF LA HABRA, COUNTY OF ORANGE, STATE OF CALIFORNIA



VICINITY MAP  
NTS

### LEGEND

- EXISTING RIGHT-OF-WAY/ BOUNDARY
- PROPOSED RIGHT-OF-WAY/ BOUNDARY
- DRAINAGE MANAGEMENT AREA (DMA)
- EXISTING STORM DRAIN
- PROPOSED STORM DRAIN
- DRAINAGE FLOW ARROWS
- PROPOSED MWS BIOFILTRATION VAULT
- PROPOSED CATCH BASIN
- DMA X  
X.XX AC
- ACREAGE



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TENTATIVE TRACT NO. 19143  
EXISTING CONDITIONS  
HYDROLOGY MAP

SCALE: AS SHOWN

DRAWN BY: SP

DATE: 3/1/2021

SHEET 1 OF 1

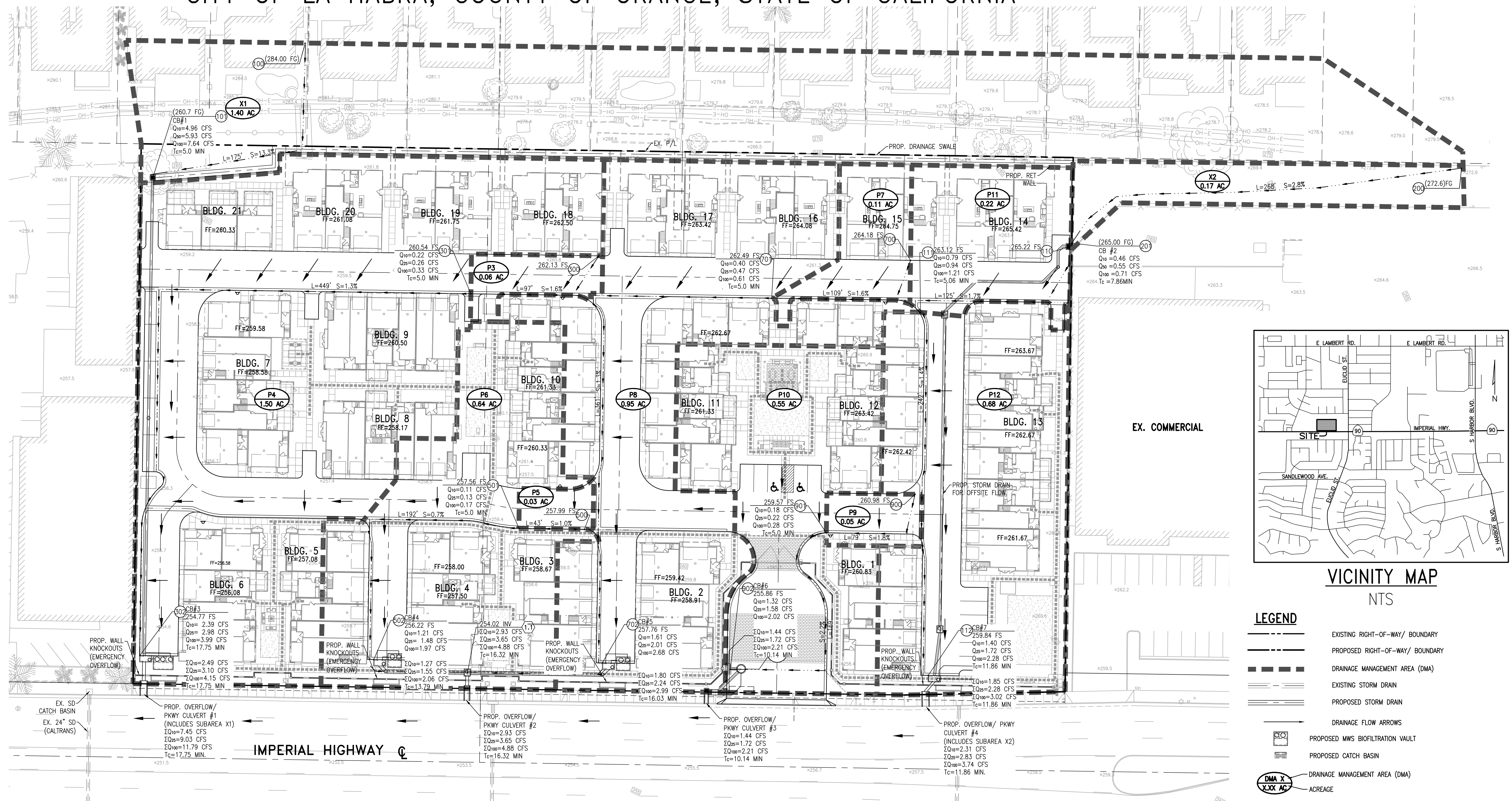
CHECKED BY: JH

CITY OF LA HABRA

# **Proposed Conditions Hydrology Map**












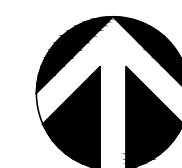
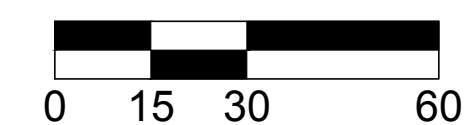
PROPOSED CONDITIONS HYDROLOGY MAP  
TR 19143  
251-271 AND 341-351 IMPERIAL HIGHWAY  
CITY OF LA HABRA, COUNTY OF ORANGE, STATE OF CALIFORNIA



## VICINITY MAP

**LEGEND**

- |   |   |
|---|---|
|  | EXISTING RIGHT-OF-WAY/ BOUNDARY           |
|  | PROPOSED RIGHT-OF-WAY/ BOUNDARY           |
|  | DRAINAGE MANAGEMENT AREA (DMA)            |
|  | EXISTING STORM DRAIN                      |
|  | PROPOSED STORM DRAIN                      |
|  | DRAINAGE FLOW ARROWS                      |
|  | PROPOSED MWS BIOFILTRATION VAULT          |
|  | PROPOSED CATCH BASIN                      |
|  | DRAINAGE MANAGEMENT AREA (DMA)<br>ACREAGE |


$$1'' = 30'$$


PREPARED BY :



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# TENTATIVE TRACT NO. 19143 PROPOSED CONDITIONS HYDROLOGY MAP

DATE: 5/17/2021

SHEET 1 OF 1

SCALE: AS SHOWN

DRAWN BY: SP

CHECKED BY: JH

CITY OF LA HABRA

# **APPENDIX B**

## **HYDROLOGY CALCULATIONS**

# **Existing Conditions Hydrology Calculations (10, 25, 100-year Storm Event)**

\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
(Reference: 1986 ORANGE COUNTY HYDROLOGY CRITERION)  
(c) Copyright 1983-2014 Advanced Engineering Software (aes)  
Ver. 21.0 Release Date: 06/01/2014 License ID 1580

Analysis prepared by:

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*

\* OLS0109 \*  
\* PRELIM \*  
\* EXISTING Q10 \*  
\*\*\*\*\*

FILE NAME: OL109X10.DAT  
TIME/DATE OF STUDY: 07:04 03/01/2021

=====

USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:

=====

--\*TIME-OF-CONCENTRATION MODEL\*--

USER SPECIFIED STORM EVENT(YEAR) = 10.00  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.95  
\*DATA BANK RAINFALL USED\*  
\*ANTECEDENT MOISTURE CONDITION (AMC) I ASSUMED FOR RATIONAL METHOD\*

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

| NO. | HALF-<br>WIDTH<br>(FT) | CROWN TO<br>CROSSFALL<br>(FT) | STREET-CROSSFALL:<br>IN- / OUT- / PARK-<br>SIDE / SIDE / WAY | CURB<br>HEIGHT<br>(FT) | GUTTER-GEOMETRIES:<br>WIDTH LIP HIKE<br>(FT) (FT) (FT) | MANNING<br>FACTOR<br>(n) |
|-----|------------------------|-------------------------------|--|------------------------|--|--------------------------|
| 1   | 30.0                   | 20.0                          | 0.018/0.018/0.020  | 0.67                   | 2.00 0.0313 0.167                                      | 0.0150                   |

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

\*\*\*\*\*

FLOW PROCESS FROM NODE 100.00 TO NODE 101.00 IS CODE = 21

-----  
>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 175.00  
ELEVATION DATA: UPSTREAM(FEET) = 284.00 DOWNSTREAM(FEET) = 260.70

$T_c = K * [(LENGTH^{**} 3.00) / (ELEVATION\ CHANGE)]^{**0.20}$

SUBAREA ANALYSIS USED MINIMUM  $T_c$ (MIN.) = 5.000

\* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 4.060

SUBAREA  $T_c$  AND LOSS RATE DATA(AMC I):

| DEVELOPMENT TYPE/<br>LAND USE | SCS SOIL<br>GROUP | AREA<br>(ACRES) | Fp<br>(INCH/HR) | Ap<br>(DECIMAL) | SCS<br>CN | $T_c$<br>(MIN.) |
|-------------------------------|-------------------|-----------------|-----------------|-----------------|-----------|-----------------|
|-------------------------------|-------------------|-----------------|-----------------|-----------------|-----------|-----------------|

RESIDENTIAL

|                      |   |      |      |       |    |      |
|----------------------|---|------|------|-------|----|------|
| "3-4 DWELLINGS/ACRE" | D | 1.40 | 0.20 | 0.600 | 57 | 5.00 |
|----------------------|---|------|------|-------|----|------|

SUBAREA AVERAGE PERVIOUS LOSS RATE,  $F_p$ (INCH/HR) = 0.20

SUBAREA AVERAGE PERVIOUS AREA FRACTION,  $A_p$  = 0.600

SUBAREA RUNOFF(CFS) = 4.96

TOTAL AREA(ACRES) = 1.40 PEAK FLOW RATE(CFS) = 4.96

\*\*\*\*\*

FLOW PROCESS FROM NODE 200.00 TO NODE 201.00 IS CODE = 21

-----  
>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 268.00  
ELEVATION DATA: UPSTREAM(FEET) = 272.60 DOWNSTREAM(FEET) = 265.00

$T_c = K * [(LENGTH^{**} 3.00) / (ELEVATION\ CHANGE)]^{**0.20}$

SUBAREA ANALYSIS USED MINIMUM  $T_c$ (MIN.) = 7.863

\* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.132

SUBAREA  $T_c$  AND LOSS RATE DATA(AMC I):

| DEVELOPMENT TYPE/<br>LAND USE | SCS SOIL<br>GROUP | AREA<br>(ACRES) | Fp<br>(INCH/HR) | Ap<br>(DECIMAL) | SCS<br>CN | $T_c$<br>(MIN.) |
|-------------------------------|-------------------|-----------------|-----------------|-----------------|-----------|-----------------|
|-------------------------------|-------------------|-----------------|-----------------|-----------------|-----------|-----------------|

RESIDENTIAL

|                      |   |      |      |       |    |      |
|----------------------|---|------|------|-------|----|------|
| "3-4 DWELLINGS/ACRE" | D | 0.17 | 0.20 | 0.600 | 57 | 7.86 |
|----------------------|---|------|------|-------|----|------|

SUBAREA AVERAGE PERVIOUS LOSS RATE,  $F_p$ (INCH/HR) = 0.20

SUBAREA AVERAGE PERVIOUS AREA FRACTION,  $A_p$  = 0.600

SUBAREA RUNOFF(CFS) = 0.46

TOTAL AREA(ACRES) = 0.17 PEAK FLOW RATE(CFS) = 0.46

\*\*\*\*\*

FLOW PROCESS FROM NODE 300.00 TO NODE 301.00 IS CODE = 21

-----  
>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 159.00  
ELEVATION DATA: UPSTREAM(FEET) = 262.50 DOWNSTREAM(FEET) = 259.00

$T_c = K * [(LENGTH^{**} 3.00) / (ELEVATION\ CHANGE)]^{**} 0.20$   
 SUBAREA ANALYSIS USED MINIMUM  $T_c(MIN.) = 5.000$   
 \* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 4.060  
 SUBAREA  $T_c$  AND LOSS RATE DATA(AMC I):  

| DEVELOPMENT TYPE/<br>LAND USE | SCS SOIL<br>GROUP | AREA<br>(ACRES) | Fp<br>(INCH/HR) | Ap<br>(DECIMAL) | SCS<br>CN | Tc<br>(MIN.) |
|-------------------------------|-------------------|-----------------|-----------------|-----------------|-----------|--------------|
| COMMERCIAL                    | D                 | 0.30            | 0.20            | 0.100           | 57        | 5.00         |

 SUBAREA AVERAGE PERVIOUS LOSS RATE,  $F_p(INCH/HR) = 0.20$   
 SUBAREA AVERAGE PERVIOUS AREA FRACTION,  $A_p = 0.100$   
 SUBAREA RUNOFF(CFS) = 1.09  
 TOTAL AREA(ACRES) = 0.30 PEAK FLOW RATE(CFS) = 1.09

\*\*\*\*\*

FLOW PROCESS FROM NODE 301.00 TO NODE 302.00 IS CODE = 61

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>(STANDARD CURB SECTION USED)<<<<<

UPSTREAM ELEVATION(FEET) = 259.00 DOWNSTREAM ELEVATION(FEET) = 250.16  
 STREET LENGTH(FEET) = 282.00 CURB HEIGHT(INCHES) = 6.0  
 STREET HALFWIDTH(FEET) = 12.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 6.00  
 INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
 OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
 STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
 Manning's FRICTION FACTOR for Streetflow Section(curb-to-curb) = 0.0950  
 Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.66

\*\*\*STREET FLOWING FULL\*\*\*

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.38

HALFSTREET FLOOD WIDTH(FEET) = 12.00

AVERAGE FLOW VELOCITY(FEET/SEC.) = 0.75

PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.29

STREET FLOW TRAVEL TIME(MIN.) = 6.25  $T_c(MIN.) = 11.25$

\* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.550

SUBAREA LOSS RATE DATA(AMC I):

| DEVELOPMENT TYPE/<br>LAND USE | SCS SOIL<br>GROUP | AREA<br>(ACRES) | Fp<br>(INCH/HR) | Ap<br>(DECIMAL) | SCS<br>CN |
|-------------------------------|-------------------|-----------------|-----------------|-----------------|-----------|
| COMMERCIAL                    | D                 | 1.33            | 0.20            | 0.100           | 57        |

SUBAREA AVERAGE PERVIOUS LOSS RATE,  $F_p(INCH/HR) = 0.20$

SUBAREA AVERAGE PERVIOUS AREA FRACTION,  $A_p = 0.100$

SUBAREA AREA(ACRES) = 1.33 SUBAREA RUNOFF(CFS) = 3.03

EFFECTIVE AREA(ACRES) = 1.63 AREA-AVERAGED  $F_m(INCH/HR) = 0.02$

AREA-AVERAGED  $F_p(INCH/HR) = 0.20$  AREA-AVERAGED  $A_p = 0.10$

TOTAL AREA(ACRES) = 1.6 PEAK FLOW RATE(CFS) = 3.71

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.42 HALFSTREET FLOOD WIDTH(FEET) = 12.00

FLOW VELOCITY(FEET/SEC.) = 0.86 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.36

LONGEST FLOWPATH FROM NODE 300.00 TO NODE 302.00 = 441.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 500.00 TO NODE 501.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 198.00

ELEVATION DATA: UPSTREAM(FEET) = 264.00 DOWNSTREAM(FEET) = 262.00

$T_c = K * [(LENGTH^{**} 3.00) / (ELEVATION\ CHANGE)]^{**0.20}$

SUBAREA ANALYSIS USED MINIMUM  $T_c$ (MIN.) = 6.319

\* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.550

SUBAREA  $T_c$  AND LOSS RATE DATA(AMC I ):

| DEVELOPMENT TYPE/<br>LAND USE | SCS SOIL<br>GROUP | AREA<br>(ACRES) | $F_p$<br>(INCH/HR) | $A_p$<br>(DECIMAL) | SCS<br>CN | $T_c$<br>(MIN.) |
|-------------------------------|-------------------|-----------------|--------------------|--------------------|-----------|-----------------|
| COMMERCIAL                    | D                 | 0.15            | 0.20               | 0.100              | 57        | 6.32            |

SUBAREA AVERAGE PERVIOUS LOSS RATE,  $F_p$ (INCH/HR) = 0.20

SUBAREA AVERAGE PERVIOUS AREA FRACTION,  $A_p$  = 0.100

SUBAREA RUNOFF(CFS) = 0.48

TOTAL AREA(ACRES) = 0.15 PEAK FLOW RATE(CFS) = 0.48

\*\*\*\*\*

FLOW PROCESS FROM NODE 501.00 TO NODE 502.00 IS CODE = 61

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STANDARD CURB SECTION USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 262.00 DOWNSTREAM ELEVATION(FEET) = 253.45

STREET LENGTH(FEET) = 355.00 CURB HEIGHT(INCHES) = 6.0

STREET HALFWIDTH(FEET) = 12.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 6.00

INSIDE STREET CROSSFALL(DECIMAL) = 0.020

OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2

STREET PARKWAY CROSSFALL(DECIMAL) = 0.020

Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0950

Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.13

\*\*\*STREET FLOWING FULL\*\*\*

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.38  
 HALFSTREET FLOOD WIDTH(FEET) = 12.00  
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 0.64  
 PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.24  
 STREET FLOW TRAVEL TIME(MIN.) = 9.25 Tc(MIN.) = 15.57  
 \* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.117  
 SUBAREA LOSS RATE DATA(AMC I):  

| DEVELOPMENT TYPE/<br>LAND USE | SCS SOIL<br>GROUP | AREA<br>(ACRES) | Fp<br>(INCH/HR) | Ap<br>(DECIMAL) | SCS<br>CN |
|-------------------------------|-------------------|-----------------|-----------------|-----------------|-----------|
| COMMERCIAL                    | D                 | 1.67            | 0.20            | 0.100           | 57        |

 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100  
 SUBAREA AREA(ACRES) = 1.67 SUBAREA RUNOFF(CFS) = 3.15  
 EFFECTIVE AREA(ACRES) = 1.82 AREA-AVERAGED Fm(INCH/HR) = 0.02  
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.10  
 TOTAL AREA(ACRES) = 1.8 PEAK FLOW RATE(CFS) = 3.44

END OF SUBAREA STREET FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.42 HALFSTREET FLOOD WIDTH(FEET) = 12.00  
 FLOW VELOCITY(FEET/SEC.) = 0.77 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.33  
 LONGEST FLOWPATH FROM NODE 500.00 TO NODE 502.00 = 553.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 700.00 TO NODE 701.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
 >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

INITIAL SUBAREA FLOW-LENGTH(FEET) = 101.00  
 ELEVATION DATA: UPSTREAM(FEET) = 266.90 DOWNSTREAM(FEET) = 264.00

Tc = K\*[(LENGTH\*\* 3.00)/(ELEVATION CHANGE)]\*\*0.20  
 SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 5.000  
 \* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 4.060  
 SUBAREA Tc AND LOSS RATE DATA(AMC I):  

| DEVELOPMENT TYPE/<br>LAND USE | SCS SOIL<br>GROUP | AREA<br>(ACRES) | Fp<br>(INCH/HR) | Ap<br>(DECIMAL) | SCS<br>CN | Tc<br>(MIN.) |
|-------------------------------|-------------------|-----------------|-----------------|-----------------|-----------|--------------|
| COMMERCIAL                    | D                 | 0.11            | 0.20            | 0.100           | 57        | 5.00         |

 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100  
 SUBAREA RUNOFF(CFS) = 0.40  
 TOTAL AREA(ACRES) = 0.11 PEAK FLOW RATE(CFS) = 0.40

\*\*\*\*\*

FLOW PROCESS FROM NODE 701.00 TO NODE 702.00 IS CODE = 61

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>(STANDARD CURB SECTION USED)<<<<<

UPSTREAM ELEVATION(FEET) = 264.00 DOWNSTREAM ELEVATION(FEET) = 259.70



STREET LENGTH(FEET) = 289.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 12.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 6.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0950  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.70

\*\*\*STREET FLOWING FULL\*\*\*

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.38

HALFSTREET FLOOD WIDTH(FEET) = 12.00

AVERAGE FLOW VELOCITY(FEET/SEC.) = 0.50

PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.19

STREET FLOW TRAVEL TIME(MIN.) = 9.55 Tc(MIN.) = 14.55

\* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.201

SUBAREA LOSS RATE DATA(AMC I):

| DEVELOPMENT TYPE/<br>LAND USE | SCS SOIL<br>GROUP | AREA<br>(ACRES) | Fp<br>(INCH/HR) | Ap<br>(DECIMAL) | SCS<br>CN |
|-------------------------------|-------------------|-----------------|-----------------|-----------------|-----------|
| COMMERCIAL                    | D                 | 1.24            | 0.20            | 0.100           | 57        |

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20

SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100

SUBAREA AREA(ACRES) = 1.24 SUBAREA RUNOFF(CFS) = 2.43

EFFECTIVE AREA(ACRES) = 1.35 AREA-AVERAGED Fm(INCH/HR) = 0.02

AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.10

TOTAL AREA(ACRES) = 1.4 PEAK FLOW RATE(CFS) = 2.65

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.42 HALFSTREET FLOOD WIDTH(FEET) = 12.00

FLOW VELOCITY(FEET/SEC.) = 0.60 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.25

LONGEST FLOWPATH FROM NODE 700.00 TO NODE 702.00 = 390.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 702.00 TO NODE 703.00 IS CODE = 31

>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 256.70 DOWNSTREAM(FEET) = 255.78

FLOW LENGTH(FEET) = 92.50 MANNING'S N = 0.012

ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000

DEPTH OF FLOW IN 18.0 INCH PIPE IS 6.0 INCHES

PIPE-FLOW VELOCITY(FEET/SEC.) = 5.14

ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 2.65

PIPE TRAVEL TIME(MIN.) = 0.30 Tc(MIN.) = 14.85  
LONGEST FLOWPATH FROM NODE 700.00 TO NODE 703.00 = 482.50 FEET.

=====

END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 1.4 TC(MIN.) = 14.85  
EFFECTIVE AREA(ACRES) = 1.35 AREA-AVERAGED Fm(INCH/HR)= 0.02  
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.100  
PEAK FLOW RATE(CFS) = 2.65

=====

=====

END OF RATIONAL METHOD ANALYSIS



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RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
(Reference: 1986 ORANGE COUNTY HYDROLOGY CRITERION)  
(c) Copyright 1983-2014 Advanced Engineering Software (aes)  
Ver. 21.0 Release Date: 06/01/2014 License ID 1580

Analysis prepared by:

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*

\* OLS0109 \*  
\* PRELIM \*  
\* EXISTING Q25 \*  
\*\*\*\*\*

FILE NAME: OL109X25.DAT  
TIME/DATE OF STUDY: 07:06 03/01/2021

=====

USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:

=====

--\*TIME-OF-CONCENTRATION MODEL\*--

USER SPECIFIED STORM EVENT(YEAR) = 25.00  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.95  
\*DATA BANK RAINFALL USED\*  
\*ANTECEDENT MOISTURE CONDITION (AMC) I ASSUMED FOR RATIONAL METHOD\*

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

| NO. | HALF-<br>WIDTH<br>(FT) | CROWN TO<br>CROSSFALL<br>(FT) | STREET-CROSSFALL:<br>IN- / OUT- / PARK-<br>SIDE / SIDE / WAY | CURB<br>HEIGHT<br>(FT) | GUTTER-GEOMETRIES:<br>WIDTH LIP HIKE<br>(FT) (FT) (FT) | MANNING<br>FACTOR<br>(n) |
|-----|------------------------|-------------------------------|--|------------------------|--|--------------------------|
| 1   | 30.0                   | 20.0                          | 0.018/0.018/0.020  | 0.67                   | 2.00 0.0312 0.167                                      | 0.0150                   |

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

\*\*\*\*\*

FLOW PROCESS FROM NODE 100.00 TO NODE 101.00 IS CODE = 21

-----  
>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 175.00

ELEVATION DATA: UPSTREAM(FEET) = 284.00 DOWNSTREAM(FEET) = 260.70

$T_c = K * [(LENGTH^{**} 3.00) / (ELEVATION\ CHANGE)]^{**0.20}$

SUBAREA ANALYSIS USED MINIMUM  $T_c$ (MIN.) = 5.000

\* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 4.824

SUBAREA  $T_c$  AND LOSS RATE DATA(AMC I):

| DEVELOPMENT TYPE/<br>LAND USE | SCS SOIL<br>GROUP | AREA<br>(ACRES) | Fp<br>(INCH/HR) | Ap<br>(DECIMAL) | SCS<br>CN | $T_c$<br>(MIN.) |
|-------------------------------|-------------------|-----------------|-----------------|-----------------|-----------|-----------------|
|-------------------------------|-------------------|-----------------|-----------------|-----------------|-----------|-----------------|

RESIDENTIAL

"3-4 DWELLINGS/ACRE" D 1.40 0.20 0.600 57 5.00

SUBAREA AVERAGE PERVIOUS LOSS RATE,  $F_p$ (INCH/HR) = 0.20

SUBAREA AVERAGE PERVIOUS AREA FRACTION,  $A_p$  = 0.600

SUBAREA RUNOFF(CFS) = 5.93

TOTAL AREA(ACRES) = 1.40 PEAK FLOW RATE(CFS) = 5.93

\*\*\*\*\*

FLOW PROCESS FROM NODE 200.00 TO NODE 201.00 IS CODE = 21

-----  
>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 268.00

ELEVATION DATA: UPSTREAM(FEET) = 272.60 DOWNSTREAM(FEET) = 265.00

$T_c = K * [(LENGTH^{**} 3.00) / (ELEVATION\ CHANGE)]^{**0.20}$

SUBAREA ANALYSIS USED MINIMUM  $T_c$ (MIN.) = 7.863

\* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 3.733

SUBAREA  $T_c$  AND LOSS RATE DATA(AMC I):

| DEVELOPMENT TYPE/<br>LAND USE | SCS SOIL<br>GROUP | AREA<br>(ACRES) | Fp<br>(INCH/HR) | Ap<br>(DECIMAL) | SCS<br>CN | $T_c$<br>(MIN.) |
|-------------------------------|-------------------|-----------------|-----------------|-----------------|-----------|-----------------|
|-------------------------------|-------------------|-----------------|-----------------|-----------------|-----------|-----------------|

RESIDENTIAL

"3-4 DWELLINGS/ACRE" D 0.17 0.20 0.600 57 7.86

SUBAREA AVERAGE PERVIOUS LOSS RATE,  $F_p$ (INCH/HR) = 0.20

SUBAREA AVERAGE PERVIOUS AREA FRACTION,  $A_p$  = 0.600

SUBAREA RUNOFF(CFS) = 0.55

TOTAL AREA(ACRES) = 0.17 PEAK FLOW RATE(CFS) = 0.55

\*\*\*\*\*

FLOW PROCESS FROM NODE 300.00 TO NODE 301.00 IS CODE = 21

-----  
>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 159.00

ELEVATION DATA: UPSTREAM(FEET) = 262.50 DOWNSTREAM(FEET) = 259.00

$T_c = K * [(LENGTH^{**} 3.00) / (ELEVATION\ CHANGE)]^{**} 0.20$   
 SUBAREA ANALYSIS USED MINIMUM  $T_c(MIN.) = 5.000$   
 \* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 4.824  
 SUBAREA  $T_c$  AND LOSS RATE DATA(AMC I):  

| DEVELOPMENT TYPE/<br>LAND USE | SCS SOIL<br>GROUP | AREA<br>(ACRES) | Fp<br>(INCH/HR) | Ap<br>(DECIMAL) | SCS<br>CN | Tc<br>(MIN.) |
|-------------------------------|-------------------|-----------------|-----------------|-----------------|-----------|--------------|
| COMMERCIAL                    | D                 | 0.30            | 0.20            | 0.100           | 57        | 5.00         |

 SUBAREA AVERAGE PERVIOUS LOSS RATE,  $F_p(INCH/HR) = 0.20$   
 SUBAREA AVERAGE PERVIOUS AREA FRACTION,  $A_p = 0.100$   
 SUBAREA RUNOFF(CFS) = 1.30  
 TOTAL AREA(ACRES) = 0.30 PEAK FLOW RATE(CFS) = 1.30

\*\*\*\*\*

FLOW PROCESS FROM NODE 301.00 TO NODE 302.00 IS CODE = 61

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>(STANDARD CURB SECTION USED)<<<<<

UPSTREAM ELEVATION(FEET) = 259.00 DOWNSTREAM ELEVATION(FEET) = 250.16  
 STREET LENGTH(FEET) = 282.00 CURB HEIGHT(INCHES) = 6.0  
 STREET HALFWIDTH(FEET) = 12.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 6.00  
 INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
 OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
 STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
 Manning's FRICTION FACTOR for Streetflow Section(curb-to-curb) = 0.0950  
 Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.21

\*\*\*STREET FLOWING FULL\*\*\*

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.40

HALFSTREET FLOOD WIDTH(FEET) = 12.00

AVERAGE FLOW VELOCITY(FEET/SEC.) = 0.81

PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.33

STREET FLOW TRAVEL TIME(MIN.) = 5.78  $T_c(MIN.) = 10.78$

\* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 3.123

SUBAREA LOSS RATE DATA(AMC I):

| DEVELOPMENT TYPE/<br>LAND USE | SCS SOIL<br>GROUP | AREA<br>(ACRES) | Fp<br>(INCH/HR) | Ap<br>(DECIMAL) | SCS<br>CN |
|-------------------------------|-------------------|-----------------|-----------------|-----------------|-----------|
| COMMERCIAL                    | D                 | 1.33            | 0.20            | 0.100           | 57        |

SUBAREA AVERAGE PERVIOUS LOSS RATE,  $F_p(INCH/HR) = 0.20$

SUBAREA AVERAGE PERVIOUS AREA FRACTION,  $A_p = 0.100$

SUBAREA AREA(ACRES) = 1.33 SUBAREA RUNOFF(CFS) = 3.71

EFFECTIVE AREA(ACRES) = 1.63 AREA-AVERAGED  $F_m(INCH/HR) = 0.02$

AREA-AVERAGED  $F_p(INCH/HR) = 0.20$  AREA-AVERAGED  $A_p = 0.10$

TOTAL AREA(ACRES) = 1.6 PEAK FLOW RATE(CFS) = 4.55

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.44 HALFSTREET FLOOD WIDTH(FEET) = 12.00

FLOW VELOCITY(FEET/SEC.) = 0.93 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.41

LONGEST FLOWPATH FROM NODE 300.00 TO NODE 302.00 = 441.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 500.00 TO NODE 501.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 198.00

ELEVATION DATA: UPSTREAM(FEET) = 264.00 DOWNSTREAM(FEET) = 262.00

$T_c = K * [(LENGTH^{**} 3.00) / (ELEVATION\ CHANGE)]^{**0.20}$

SUBAREA ANALYSIS USED MINIMUM  $T_c$ (MIN.) = 6.319

\* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 4.225

SUBAREA  $T_c$  AND LOSS RATE DATA(AMC I):

| DEVELOPMENT TYPE/<br>LAND USE | SCS SOIL<br>GROUP | AREA<br>(ACRES) | $F_p$<br>(INCH/HR) | $A_p$<br>(DECIMAL) | SCS<br>CN | $T_c$<br>(MIN.) |
|-------------------------------|-------------------|-----------------|--------------------|--------------------|-----------|-----------------|
| COMMERCIAL                    | D                 | 0.15            | 0.20               | 0.100              | 57        | 6.32            |

SUBAREA AVERAGE PERVIOUS LOSS RATE,  $F_p$ (INCH/HR) = 0.20

SUBAREA AVERAGE PERVIOUS AREA FRACTION,  $A_p$  = 0.100

SUBAREA RUNOFF(CFS) = 0.57

TOTAL AREA(ACRES) = 0.15 PEAK FLOW RATE(CFS) = 0.57

\*\*\*\*\*

FLOW PROCESS FROM NODE 501.00 TO NODE 502.00 IS CODE = 61

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STANDARD CURB SECTION USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 262.00 DOWNSTREAM ELEVATION(FEET) = 253.45

STREET LENGTH(FEET) = 355.00 CURB HEIGHT(INCHES) = 6.0

STREET HALFWIDTH(FEET) = 12.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 6.00

INSIDE STREET CROSSFALL(DECIMAL) = 0.020

OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2

STREET PARKWAY CROSSFALL(DECIMAL) = 0.020

Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0950

Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.60

\*\*\*STREET FLOWING FULL\*\*\*

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.39  
 HALFSTREET FLOOD WIDTH(FEET) = 12.00  
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 0.69  
 PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.27  
 STREET FLOW TRAVEL TIME(MIN.) = 8.60 Tc(MIN.) = 14.92  
 \* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 2.598  
 SUBAREA LOSS RATE DATA(AMC I):  

| DEVELOPMENT TYPE/<br>LAND USE | SCS SOIL<br>GROUP | AREA<br>(ACRES) | Fp<br>(INCH/HR) | Ap<br>(DECIMAL) | SCS<br>CN |
|-------------------------------|-------------------|-----------------|-----------------|-----------------|-----------|
| COMMERCIAL                    | D                 | 1.67            | 0.20            | 0.100           | 57        |

 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100  
 SUBAREA AREA(ACRES) = 1.67 SUBAREA RUNOFF(CFS) = 3.87  
 EFFECTIVE AREA(ACRES) = 1.82 AREA-AVERAGED Fm(INCH/HR) = 0.02  
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.10  
 TOTAL AREA(ACRES) = 1.8 PEAK FLOW RATE(CFS) = 4.22

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.45 HALFSTREET FLOOD WIDTH(FEET) = 12.00  
 FLOW VELOCITY(FEET/SEC.) = 0.84 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.37  
 LONGEST FLOWPATH FROM NODE 500.00 TO NODE 502.00 = 553.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 700.00 TO NODE 701.00 IS CODE = 21

>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
 >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

INITIAL SUBAREA FLOW-LENGTH(FEET) = 101.00  
 ELEVATION DATA: UPSTREAM(FEET) = 266.90 DOWNSTREAM(FEET) = 264.00

Tc = K\*[(LENGTH\*\* 3.00)/(ELEVATION CHANGE)]\*\*0.20  
 SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 5.000  
 \* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 4.824  
 SUBAREA Tc AND LOSS RATE DATA(AMC I):  

| DEVELOPMENT TYPE/<br>LAND USE | SCS SOIL<br>GROUP | AREA<br>(ACRES) | Fp<br>(INCH/HR) | Ap<br>(DECIMAL) | SCS<br>CN | Tc<br>(MIN.) |
|-------------------------------|-------------------|-----------------|-----------------|-----------------|-----------|--------------|
| COMMERCIAL                    | D                 | 0.11            | 0.20            | 0.100           | 57        | 5.00         |

 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100  
 SUBAREA RUNOFF(CFS) = 0.48  
 TOTAL AREA(ACRES) = 0.11 PEAK FLOW RATE(CFS) = 0.48

\*\*\*\*\*

FLOW PROCESS FROM NODE 701.00 TO NODE 702.00 IS CODE = 61

>>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>>(STANDARD CURB SECTION USED)<<<<<

UPSTREAM ELEVATION(FEET) = 264.00 DOWNSTREAM ELEVATION(FEET) = 259.70

STREET LENGTH(FEET) = 289.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 12.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 6.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curb-to-curb) = 0.0950  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.07

\*\*\*STREET FLOWING FULL\*\*\*

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.39

HALFSTREET FLOOD WIDTH(FEET) = 12.00

AVERAGE FLOW VELOCITY(FEET/SEC.) = 0.54

PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.21

STREET FLOW TRAVEL TIME(MIN.) = 8.85 Tc(MIN.) = 13.85

\* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 2.709

SUBAREA LOSS RATE DATA(AMC I):

| DEVELOPMENT TYPE/<br>LAND USE | SCS SOIL<br>GROUP | AREA<br>(ACRES) | Fp<br>(INCH/HR) | Ap<br>(DECIMAL) | SCS<br>CN |
|-------------------------------|-------------------|-----------------|-----------------|-----------------|-----------|
| COMMERCIAL                    | D                 | 1.24            | 0.20            | 0.100           | 57        |

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20

SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100

SUBAREA AREA(ACRES) = 1.24 SUBAREA RUNOFF(CFS) = 3.00

EFFECTIVE AREA(ACRES) = 1.35 AREA-AVERAGED Fm(INCH/HR) = 0.02

AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.10

TOTAL AREA(ACRES) = 1.4 PEAK FLOW RATE(CFS) = 3.27

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.44 HALFSTREET FLOOD WIDTH(FEET) = 12.00

FLOW VELOCITY(FEET/SEC.) = 0.65 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.29

LONGEST FLOWPATH FROM NODE 700.00 TO NODE 702.00 = 390.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 702.00 TO NODE 703.00 IS CODE = 31

>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 256.70 DOWNSTREAM(FEET) = 255.78

FLOW LENGTH(FEET) = 92.50 MANNING'S N = 0.012

ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000

DEPTH OF FLOW IN 18.0 INCH PIPE IS 6.7 INCHES

PIPE-FLOW VELOCITY(FEET/SEC.) = 5.45

ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 3.27



PIPE TRAVEL TIME(MIN.) = 0.28      Tc(MIN.) = 14.14  
LONGEST FLOWPATH FROM NODE 700.00 TO NODE 703.00 = 482.50 FEET.

=====

END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 1.4      TC(MIN.) = 14.14  
EFFECTIVE AREA(ACRES) = 1.35      AREA-AVERAGED Fm(INCH/HR)= 0.02  
AREA-AVERAGED Fp(INCH/HR) = 0.20      AREA-AVERAGED Ap = 0.100  
PEAK FLOW RATE(CFS) = 3.27

=====

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END OF RATIONAL METHOD ANALYSIS



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RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
(Reference: 1986 ORANGE COUNTY HYDROLOGY CRITERION)  
(c) Copyright 1983-2014 Advanced Engineering Software (aes)  
Ver. 21.0 Release Date: 06/01/2014 License ID 1580

Analysis prepared by:

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*  
\* OLS0109 \*  
\* PRELIM \*  
\* EXISTING Q100 \*  
\*\*\*\*\*

FILE NAME: 0109X100.DAT  
TIME/DATE OF STUDY: 07:08 03/01/2021

=====

USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:

=====

--\*TIME-OF-CONCENTRATION MODEL\*--

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.95  
\*DATA BANK RAINFALL USED\*  
\*ANTECEDENT MOISTURE CONDITION (AMC) I ASSUMED FOR RATIONAL METHOD\*

| *USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL* |                |                       |   |                        |  |                          |       |        |
|--|----------------|-----------------------|---|------------------------|--|--------------------------|-------|--------|
|  | HALF-<br>WIDTH | CROWN TO<br>CROSSFALL | STREET-CROSSFALL:<br>IN- / OUT-/PARK-<br>SIDE / SIDE/ WAY | CURB<br>HEIGHT<br>(FT) | GUTTER-GEOMETRIES:<br>WIDTH LIP HIKE<br>(FT) (FT) (FT) | MANNING<br>FACTOR<br>(n) |       |        |
| NO.  | (FT)           | (FT)                  |   |                        |  |                          |       |        |
| ===  | =====          | =====                 | =====   | =====                  | =====  | =====                    | ===== | =====  |
| 1  | 30.0           | 20.0                  | 0.018/0.018/0.020   | 0.67                   | 2.00   | 0.0312                   | 0.167 | 0.0150 |

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

\*\*\*\*\*

FLOW PROCESS FROM NODE 100.00 TO NODE 101.00 IS CODE = 21

-----  
>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 175.00

ELEVATION DATA: UPSTREAM(FEET) = 284.00 DOWNSTREAM(FEET) = 260.70

$T_c = K * [(LENGTH^{**} 3.00) / (ELEVATION\ CHANGE)]^{**0.20}$

SUBAREA ANALYSIS USED MINIMUM  $T_c$ (MIN.) = 5.000

\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 6.187

SUBAREA  $T_c$  AND LOSS RATE DATA(AMC I):

| DEVELOPMENT TYPE/<br>LAND USE | SCS SOIL<br>GROUP | AREA<br>(ACRES) | Fp<br>(INCH/HR) | Ap<br>(DECIMAL) | SCS<br>CN | $T_c$<br>(MIN.) |
|-------------------------------|-------------------|-----------------|-----------------|-----------------|-----------|-----------------|
|-------------------------------|-------------------|-----------------|-----------------|-----------------|-----------|-----------------|

RESIDENTIAL

|                      |   |      |      |       |    |      |
|----------------------|---|------|------|-------|----|------|
| "3-4 DWELLINGS/ACRE" | D | 1.40 | 0.20 | 0.600 | 57 | 5.00 |
|----------------------|---|------|------|-------|----|------|

SUBAREA AVERAGE PERVIOUS LOSS RATE,  $F_p$ (INCH/HR) = 0.20

SUBAREA AVERAGE PERVIOUS AREA FRACTION,  $A_p$  = 0.600

SUBAREA RUNOFF(CFS) = 7.64

TOTAL AREA(ACRES) = 1.40 PEAK FLOW RATE(CFS) = 7.64

\*\*\*\*\*

FLOW PROCESS FROM NODE 200.00 TO NODE 201.00 IS CODE = 21

-----  
>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 268.00

ELEVATION DATA: UPSTREAM(FEET) = 272.60 DOWNSTREAM(FEET) = 265.00

$T_c = K * [(LENGTH^{**} 3.00) / (ELEVATION\ CHANGE)]^{**0.20}$

SUBAREA ANALYSIS USED MINIMUM  $T_c$ (MIN.) = 7.863

\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 4.773

SUBAREA  $T_c$  AND LOSS RATE DATA(AMC I):

| DEVELOPMENT TYPE/<br>LAND USE | SCS SOIL<br>GROUP | AREA<br>(ACRES) | Fp<br>(INCH/HR) | Ap<br>(DECIMAL) | SCS<br>CN | $T_c$<br>(MIN.) |
|-------------------------------|-------------------|-----------------|-----------------|-----------------|-----------|-----------------|
|-------------------------------|-------------------|-----------------|-----------------|-----------------|-----------|-----------------|

RESIDENTIAL

|                      |   |      |      |       |    |      |
|----------------------|---|------|------|-------|----|------|
| "3-4 DWELLINGS/ACRE" | D | 0.17 | 0.20 | 0.600 | 57 | 7.86 |
|----------------------|---|------|------|-------|----|------|

SUBAREA AVERAGE PERVIOUS LOSS RATE,  $F_p$ (INCH/HR) = 0.20

SUBAREA AVERAGE PERVIOUS AREA FRACTION,  $A_p$  = 0.600

SUBAREA RUNOFF(CFS) = 0.71

TOTAL AREA(ACRES) = 0.17 PEAK FLOW RATE(CFS) = 0.71

\*\*\*\*\*

FLOW PROCESS FROM NODE 300.00 TO NODE 301.00 IS CODE = 21

-----  
>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 159.00

ELEVATION DATA: UPSTREAM(FEET) = 262.50 DOWNSTREAM(FEET) = 259.00

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$   
 SUBAREA ANALYSIS USED MINIMUM  $T_c(MIN.) = 5.000$   
 \* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 6.187  
 SUBAREA  $T_c$  AND LOSS RATE DATA(AMC I):  

| DEVELOPMENT TYPE/<br>LAND USE | SCS SOIL<br>GROUP | AREA<br>(ACRES) | $F_p$<br>(INCH/HR) | $A_p$<br>(DECIMAL) | SCS<br>CN | $T_c$<br>(MIN.) |
|-------------------------------|-------------------|-----------------|--------------------|--------------------|-----------|-----------------|
| COMMERCIAL                    | D                 | 0.30            | 0.20               | 0.100              | 57        | 5.00            |

 SUBAREA AVERAGE PERVIOUS LOSS RATE,  $F_p(INCH/HR) = 0.20$   
 SUBAREA AVERAGE PERVIOUS AREA FRACTION,  $A_p = 0.100$   
 SUBAREA RUNOFF(CFS) = 1.67  
 TOTAL AREA(ACRES) = 0.30 PEAK FLOW RATE(CFS) = 1.67

\*\*\*\*\*

FLOW PROCESS FROM NODE 301.00 TO NODE 302.00 IS CODE = 61

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>(STANDARD CURB SECTION USED)<<<<<

UPSTREAM ELEVATION(FEET) = 259.00 DOWNSTREAM ELEVATION(FEET) = 250.16  
 STREET LENGTH(FEET) = 282.00 CURB HEIGHT(INCHES) = 6.0  
 STREET HALFWIDTH(FEET) = 12.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 6.00  
 INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
 OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
 STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
 Manning's FRICTION FACTOR for Streetflow Section(curb-to-curb) = 0.0950  
 Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 4.18

\*\*\*STREET FLOWING FULL\*\*\*

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
 STREET FLOW DEPTH(FEET) = 0.43  
 HALFSTREET FLOOD WIDTH(FEET) = 12.00  
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 0.90  
 PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.39  
 STREET FLOW TRAVEL TIME(MIN.) = 5.20  $T_c(MIN.) = 10.20$   
 \* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 4.113

SUBAREA LOSS RATE DATA(AMC I):

| DEVELOPMENT TYPE/<br>LAND USE | SCS SOIL<br>GROUP | AREA<br>(ACRES) | $F_p$<br>(INCH/HR) | $A_p$<br>(DECIMAL) | SCS<br>CN |
|-------------------------------|-------------------|-----------------|--------------------|--------------------|-----------|
| COMMERCIAL                    | D                 | 1.33            | 0.20               | 0.100              | 57        |

SUBAREA AVERAGE PERVIOUS LOSS RATE,  $F_p(INCH/HR) = 0.20$

SUBAREA AVERAGE PERVIOUS AREA FRACTION,  $A_p = 0.100$

SUBAREA AREA(ACRES) = 1.33 SUBAREA RUNOFF(CFS) = 4.90

EFFECTIVE AREA(ACRES) = 1.63 AREA-AVERAGED  $F_m(INCH/HR) = 0.02$

AREA-AVERAGED  $F_p(INCH/HR) = 0.20$  AREA-AVERAGED  $A_p = 0.10$

TOTAL AREA(ACRES) = 1.6 PEAK FLOW RATE(CFS) = 6.00

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.48 HALFSTREET FLOOD WIDTH(FEET) = 12.00

FLOW VELOCITY(FEET/SEC.) = 1.04 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.50

LONGEST FLOWPATH FROM NODE 300.00 TO NODE 302.00 = 441.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 500.00 TO NODE 501.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 198.00

ELEVATION DATA: UPSTREAM(FEET) = 264.00 DOWNSTREAM(FEET) = 262.00

$T_c = K * [(LENGTH^{**} 3.00) / (ELEVATION\ CHANGE)]^{**0.20}$

SUBAREA ANALYSIS USED MINIMUM  $T_c$ (MIN.) = 6.319

\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 5.410

SUBAREA  $T_c$  AND LOSS RATE DATA(AMC I ):

| DEVELOPMENT TYPE/<br>LAND USE | SCS SOIL<br>GROUP | AREA<br>(ACRES) | $F_p$<br>(INCH/HR) | $A_p$<br>(DECIMAL) | SCS<br>CN | $T_c$<br>(MIN.) |
|-------------------------------|-------------------|-----------------|--------------------|--------------------|-----------|-----------------|
| COMMERCIAL                    | D                 | 0.15            | 0.20               | 0.100              | 57        | 6.32            |

SUBAREA AVERAGE PERVIOUS LOSS RATE,  $F_p$ (INCH/HR) = 0.20

SUBAREA AVERAGE PERVIOUS AREA FRACTION,  $A_p$  = 0.100

SUBAREA RUNOFF(CFS) = 0.73

TOTAL AREA(ACRES) = 0.15 PEAK FLOW RATE(CFS) = 0.73

\*\*\*\*\*

FLOW PROCESS FROM NODE 501.00 TO NODE 502.00 IS CODE = 61

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STANDARD CURB SECTION USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 262.00 DOWNSTREAM ELEVATION(FEET) = 253.45

STREET LENGTH(FEET) = 355.00 CURB HEIGHT(INCHES) = 6.0

STREET HALFWIDTH(FEET) = 12.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 6.00

INSIDE STREET CROSSFALL(DECIMAL) = 0.020

OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2

STREET PARKWAY CROSSFALL(DECIMAL) = 0.020

Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0950

Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.39

\*\*\*STREET FLOWING FULL\*\*\*

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.42  
 HALFSTREET FLOOD WIDTH(FEET) = 12.00  
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 0.77  
 PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.32  
 STREET FLOW TRAVEL TIME(MIN.) = 7.70 Tc(MIN.) = 14.02  
 \* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 3.427  
 SUBAREA LOSS RATE DATA(AMC I):  

| DEVELOPMENT TYPE/<br>LAND USE | SCS SOIL<br>GROUP | AREA<br>(ACRES) | Fp<br>(INCH/HR) | Ap<br>(DECIMAL) | SCS<br>CN |
|-------------------------------|-------------------|-----------------|-----------------|-----------------|-----------|
| COMMERCIAL                    | D                 | 1.67            | 0.20            | 0.100           | 57        |

 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100  
 SUBAREA AREA(ACRES) = 1.67 SUBAREA RUNOFF(CFS) = 5.12  
 EFFECTIVE AREA(ACRES) = 1.82 AREA-AVERAGED Fm(INCH/HR) = 0.02  
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.10  
 TOTAL AREA(ACRES) = 1.8 PEAK FLOW RATE(CFS) = 5.58

END OF SUBAREA STREET FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.49 HALFSTREET FLOOD WIDTH(FEET) = 12.00  
 FLOW VELOCITY(FEET/SEC.) = 0.93 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.45  
 LONGEST FLOWPATH FROM NODE 500.00 TO NODE 502.00 = 553.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 700.00 TO NODE 701.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
 >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

INITIAL SUBAREA FLOW-LENGTH(FEET) = 101.00  
 ELEVATION DATA: UPSTREAM(FEET) = 266.90 DOWNSTREAM(FEET) = 264.00

Tc = K\*[(LENGTH\*\* 3.00)/(ELEVATION CHANGE)]\*\*0.20  
 SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 5.000  
 \* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 6.187  
 SUBAREA Tc AND LOSS RATE DATA(AMC I):  

| DEVELOPMENT TYPE/<br>LAND USE | SCS SOIL<br>GROUP | AREA<br>(ACRES) | Fp<br>(INCH/HR) | Ap<br>(DECIMAL) | SCS<br>CN | Tc<br>(MIN.) |
|-------------------------------|-------------------|-----------------|-----------------|-----------------|-----------|--------------|
| COMMERCIAL                    | D                 | 0.11            | 0.20            | 0.100           | 57        | 5.00         |

 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100  
 SUBAREA RUNOFF(CFS) = 0.61  
 TOTAL AREA(ACRES) = 0.11 PEAK FLOW RATE(CFS) = 0.61

\*\*\*\*\*

FLOW PROCESS FROM NODE 701.00 TO NODE 702.00 IS CODE = 61

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>(STANDARD CURB SECTION USED)<<<<<

UPSTREAM ELEVATION(FEET) = 264.00 DOWNSTREAM ELEVATION(FEET) = 259.70

STREET LENGTH(FEET) = 289.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 12.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 6.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0950  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.71

\*\*\*STREET FLOWING FULL\*\*\*

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.42

HALFSTREET FLOOD WIDTH(FEET) = 12.00

AVERAGE FLOW VELOCITY(FEET/SEC.) = 0.61

PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.26

STREET FLOW TRAVEL TIME(MIN.) = 7.96 Tc(MIN.) = 12.96

\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 3.586

SUBAREA LOSS RATE DATA(AMC I):

| DEVELOPMENT TYPE/<br>LAND USE | SCS SOIL<br>GROUP | AREA<br>(ACRES) | Fp<br>(INCH/HR) | Ap<br>(DECIMAL) | SCS<br>CN |
|-------------------------------|-------------------|-----------------|-----------------|-----------------|-----------|
| COMMERCIAL                    | D                 | 1.24            | 0.20            | 0.100           | 57        |

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20

SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100

SUBAREA AREA(ACRES) = 1.24 SUBAREA RUNOFF(CFS) = 3.98

EFFECTIVE AREA(ACRES) = 1.35 AREA-AVERAGED Fm(INCH/HR) = 0.02

AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.10

TOTAL AREA(ACRES) = 1.4 PEAK FLOW RATE(CFS) = 4.33

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.48 HALFSTREET FLOOD WIDTH(FEET) = 12.00

FLOW VELOCITY(FEET/SEC.) = 0.73 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.35

LONGEST FLOWPATH FROM NODE 700.00 TO NODE 702.00 = 390.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 702.00 TO NODE 703.00 IS CODE = 31

>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 256.70 DOWNSTREAM(FEET) = 255.78

FLOW LENGTH(FEET) = 92.50 MANNING'S N = 0.012

ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000

DEPTH OF FLOW IN 18.0 INCH PIPE IS 7.8 INCHES

PIPE-FLOW VELOCITY(FEET/SEC.) = 5.88

ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 4.33

PIPE TRAVEL TIME(MIN.) = 0.26 Tc(MIN.) = 13.22  
LONGEST FLOWPATH FROM NODE 700.00 TO NODE 703.00 = 482.50 FEET.

=====

END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 1.4 TC(MIN.) = 13.22  
EFFECTIVE AREA(ACRES) = 1.35 AREA-AVERAGED Fm(INCH/HR)= 0.02  
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.100  
PEAK FLOW RATE(CFS) = 4.33

=====

=====

END OF RATIONAL METHOD ANALYSIS





# **Proposed Conditions Hydrology Calculations (10, 25, 100-year Storm Event)**

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RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
(Reference: 1986 ORANGE COUNTY HYDROLOGY CRITERION)  
(c) Copyright 1983-2014 Advanced Engineering Software (aes)  
Ver. 21.0 Release Date: 06/01/2014 License ID 1580

Analysis prepared by:

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*  
\* OLS0109 \*  
\* PRELIM \*  
\* PROPOSED Q10 \*  
\*\*\*\*\*

FILE NAME: 0109P10.DAT  
TIME/DATE OF STUDY: 14:35 03/09/2021

=====

USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:

=====

--\*TIME-OF-CONCENTRATION MODEL\*--

USER SPECIFIED STORM EVENT(YEAR) = 10.00  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.95  
\*DATA BANK RAINFALL USED\*  
\*ANTECEDENT MOISTURE CONDITION (AMC) I ASSUMED FOR RATIONAL METHOD\*

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

| NO. | HALF-<br>WIDTH<br>(FT) | CROWN TO<br>CROSSFALL<br>(FT) | STREET-CROSSFALL:<br>IN- / OUT- / PARK-<br>SIDE / SIDE / WAY | CURB<br>HEIGHT<br>(FT) | GUTTER-GEOMETRIES:<br>WIDTH LIP HIKE<br>(FT) (FT) (FT) | MANNING<br>FACTOR<br>(n) |
|-----|------------------------|-------------------------------|--|------------------------|--|--------------------------|
| 1   | 30.0                   | 20.0                          | 0.018/0.018/0.020  | 0.67                   | 2.00 0.0313 0.167                                      | 0.0150                   |

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

\*\*\*\*\*

FLOW PROCESS FROM NODE 100.00 TO NODE 101.00 IS CODE = 21

-----  
>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 175.00

ELEVATION DATA: UPSTREAM(FEET) = 284.00 DOWNSTREAM(FEET) = 260.70

$T_c = K * [(LENGTH^{**} 3.00) / (ELEVATION\ CHANGE)]^{**0.20}$

SUBAREA ANALYSIS USED MINIMUM  $T_c$ (MIN.) = 5.000

\* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 4.060

SUBAREA  $T_c$  AND LOSS RATE DATA(AMC I):

| DEVELOPMENT TYPE/<br>LAND USE | SCS SOIL<br>GROUP | AREA<br>(ACRES) | Fp<br>(INCH/HR) | Ap<br>(DECIMAL) | SCS<br>CN | $T_c$<br>(MIN.) |
|-------------------------------|-------------------|-----------------|-----------------|-----------------|-----------|-----------------|
|-------------------------------|-------------------|-----------------|-----------------|-----------------|-----------|-----------------|

RESIDENTIAL

|                      |   |      |      |       |    |      |
|----------------------|---|------|------|-------|----|------|
| "3-4 DWELLINGS/ACRE" | D | 1.40 | 0.20 | 0.600 | 57 | 5.00 |
|----------------------|---|------|------|-------|----|------|

SUBAREA AVERAGE PERVIOUS LOSS RATE,  $F_p$ (INCH/HR) = 0.20

SUBAREA AVERAGE PERVIOUS AREA FRACTION,  $A_p$  = 0.600

SUBAREA RUNOFF(CFS) = 4.96

TOTAL AREA(ACRES) = 1.40 PEAK FLOW RATE(CFS) = 4.96

\*\*\*\*\*

FLOW PROCESS FROM NODE 200.00 TO NODE 201.00 IS CODE = 21

-----  
>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 268.00

ELEVATION DATA: UPSTREAM(FEET) = 272.60 DOWNSTREAM(FEET) = 265.00

$T_c = K * [(LENGTH^{**} 3.00) / (ELEVATION\ CHANGE)]^{**0.20}$

SUBAREA ANALYSIS USED MINIMUM  $T_c$ (MIN.) = 7.863

\* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.132

SUBAREA  $T_c$  AND LOSS RATE DATA(AMC I):

| DEVELOPMENT TYPE/<br>LAND USE | SCS SOIL<br>GROUP | AREA<br>(ACRES) | Fp<br>(INCH/HR) | Ap<br>(DECIMAL) | SCS<br>CN | $T_c$<br>(MIN.) |
|-------------------------------|-------------------|-----------------|-----------------|-----------------|-----------|-----------------|
|-------------------------------|-------------------|-----------------|-----------------|-----------------|-----------|-----------------|

RESIDENTIAL

|                      |   |      |      |       |    |      |
|----------------------|---|------|------|-------|----|------|
| "3-4 DWELLINGS/ACRE" | D | 0.17 | 0.20 | 0.600 | 57 | 7.86 |
|----------------------|---|------|------|-------|----|------|

SUBAREA AVERAGE PERVIOUS LOSS RATE,  $F_p$ (INCH/HR) = 0.20

SUBAREA AVERAGE PERVIOUS AREA FRACTION,  $A_p$  = 0.600

SUBAREA RUNOFF(CFS) = 0.46

TOTAL AREA(ACRES) = 0.17 PEAK FLOW RATE(CFS) = 0.46

\*\*\*\*\*

FLOW PROCESS FROM NODE 300.00 TO NODE 301.00 IS CODE = 21

-----  
>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 97.00

ELEVATION DATA: UPSTREAM(FEET) = 262.13 DOWNSTREAM(FEET) = 260.54

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION\ CHANGE)] ** 0.20$   
 SUBAREA ANALYSIS USED MINIMUM  $T_c(MIN.) = 5.000$   
 \* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 4.060  
 SUBAREA  $T_c$  AND LOSS RATE DATA(AMC I):  

| DEVELOPMENT TYPE/<br>LAND USE | SCS SOIL<br>GROUP | AREA<br>(ACRES) | Fp<br>(INCH/HR) | Ap<br>(DECIMAL) | SCS<br>CN | $T_c$<br>(MIN.) |
|-------------------------------|-------------------|-----------------|-----------------|-----------------|-----------|-----------------|
| RESIDENTIAL                   |                   |                 |                 |                 |           |                 |
| "11+ DWELLINGS/ACRE"          | D                 | 0.06            | 0.20            | 0.200           | 57        | 5.00            |

 SUBAREA AVERAGE PERVIOUS LOSS RATE,  $F_p(INCH/HR) = 0.20$   
 SUBAREA AVERAGE PERVIOUS AREA FRACTION,  $A_p = 0.200$   
 SUBAREA RUNOFF(CFS) = 0.22  
 TOTAL AREA(ACRES) = 0.06 PEAK FLOW RATE(CFS) = 0.22

\*\*\*\*\*

FLOW PROCESS FROM NODE 301.00 TO NODE 302.00 IS CODE = 61

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>(STANDARD CURB SECTION USED)<<<<<

UPSTREAM ELEVATION(FEET) = 260.54 DOWNSTREAM ELEVATION(FEET) = 254.77  
 STREET LENGTH(FEET) = 447.00 CURB HEIGHT(INCHES) = 6.0  
 STREET HALFWIDTH(FEET) = 11.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 5.50  
 INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
 OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
 STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
 Manning's FRICTION FACTOR for Streetflow Section(curb-to-curb) = 0.0950  
 Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.55  
 \*\*\*STREET FLOWING FULL\*\*\*

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
 STREET FLOW DEPTH(FEET) = 0.37  
 HALFSTREET FLOOD WIDTH(FEET) = 11.00  
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 0.48  
 PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.18  
 STREET FLOW TRAVEL TIME(MIN.) = 15.44  $T_c(MIN.) = 20.44$   
 \* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 1.812

SUBAREA LOSS RATE DATA(AMC I):  

| DEVELOPMENT TYPE/<br>LAND USE | SCS SOIL<br>GROUP | AREA<br>(ACRES) | Fp<br>(INCH/HR) | Ap<br>(DECIMAL) | SCS<br>CN |
|-------------------------------|-------------------|-----------------|-----------------|-----------------|-----------|
| RESIDENTIAL                   |                   |                 |                 |                 |           |
| "11+ DWELLINGS/ACRE"          | D                 | 1.50            | 0.20            | 0.200           | 57        |

 SUBAREA AVERAGE PERVIOUS LOSS RATE,  $F_p(INCH/HR) = 0.20$   
 SUBAREA AVERAGE PERVIOUS AREA FRACTION,  $A_p = 0.200$   
 SUBAREA AREA(ACRES) = 1.50 SUBAREA RUNOFF(CFS) = 2.39

EFFECTIVE AREA(ACRES) = 1.56 AREA-AVERAGED Fm(INCH/HR) = 0.04  
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.20  
TOTAL AREA(ACRES) = 1.6 PEAK FLOW RATE(CFS) = 2.49

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.42 HALFSTREET FLOOD WIDTH(FEET) = 11.00  
FLOW VELOCITY(FEET/SEC.) = 0.58 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.24  
LONGEST FLOWPATH FROM NODE 300.00 TO NODE 302.00 = 544.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 110.00 TO NODE 111.00 IS CODE = 21

>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 125.00

ELEVATION DATA: UPSTREAM(FEET) = 265.22 DOWNSTREAM(FEET) = 263.12

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$

SUBAREA ANALYSIS USED MINIMUM  $T_c$ (MIN.) = 5.061

\* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 4.031

SUBAREA  $T_c$  AND LOSS RATE DATA(AMC I):

| DEVELOPMENT TYPE/<br>LAND USE | SCS SOIL<br>GROUP | AREA<br>(ACRES) | Fp<br>(INCH/HR) | Ap<br>(DECIMAL) | SCS<br>CN | $T_c$<br>(MIN.) |
|-------------------------------|-------------------|-----------------|-----------------|-----------------|-----------|-----------------|
|-------------------------------|-------------------|-----------------|-----------------|-----------------|-----------|-----------------|

|                      |   |      |      |       |    |      |
|----------------------|---|------|------|-------|----|------|
| RESIDENTIAL          |   |      |      |       |    |      |
| "11+ DWELLINGS/ACRE" | D | 0.22 | 0.20 | 0.200 | 57 | 5.06 |

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20

SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.200

SUBAREA RUNOFF(CFS) = 0.79

TOTAL AREA(ACRES) = 0.22 PEAK FLOW RATE(CFS) = 0.79

\*\*\*\*\*

FLOW PROCESS FROM NODE 111.00 TO NODE 112.00 IS CODE = 61

>>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>>(STANDARD CURB SECTION USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 263.12 DOWNSTREAM ELEVATION(FEET) = 259.84

STREET LENGTH(FEET) = 238.00 CURB HEIGHT(INCHES) = 6.0

STREET HALFWIDTH(FEET) = 11.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 5.50

INSIDE STREET CROSSFALL(DECIMAL) = 0.020

OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1

STREET PARKWAY CROSSFALL(DECIMAL) = 0.020

Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0950

Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.52

\*\*\*STREET FLOWING FULL\*\*\*

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.37

HALFSTREET FLOOD WIDTH(FEET) = 11.00

AVERAGE FLOW VELOCITY(FEET/SEC.) = 0.49

PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.18

STREET FLOW TRAVEL TIME(MIN.) = 8.17 Tc(MIN.) = 13.23

\* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.325

SUBAREA LOSS RATE DATA(AMC I):

| DEVELOPMENT TYPE/<br>LAND USE | SCS SOIL<br>GROUP | AREA<br>(ACRES) | Fp<br>(INCH/HR) | Ap<br>(DECIMAL) | SCS<br>CN |
|-------------------------------|-------------------|-----------------|-----------------|-----------------|-----------|
|-------------------------------|-------------------|-----------------|-----------------|-----------------|-----------|

RESIDENTIAL

|                      |   |      |      |       |    |
|----------------------|---|------|------|-------|----|
| "11+ DWELLINGS/ACRE" | D | 0.68 | 0.20 | 0.200 | 57 |
|----------------------|---|------|------|-------|----|

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20

SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.200

SUBAREA AREA(ACRES) = 0.68 SUBAREA RUNOFF(CFS) = 1.40

EFFECTIVE AREA(ACRES) = 0.90 AREA-AVERAGED Fm(INCH/HR) = 0.04

AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.20

TOTAL AREA(ACRES) = 0.9 PEAK FLOW RATE(CFS) = 1.85

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.38 HALFSTREET FLOOD WIDTH(FEET) = 11.00

FLOW VELOCITY(FEET/SEC.) = 0.53 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.20

LONGEST FLOWPATH FROM NODE 110.00 TO NODE 112.00 = 363.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 900.00 TO NODE 901.00 IS CODE = 21

>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 79.00

ELEVATION DATA: UPSTREAM(FEET) = 260.98 DOWNSTREAM(FEET) = 259.57

Tc = K\*[(LENGTH\*\* 3.00)/(ELEVATION CHANGE)]\*\*0.20

SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 5.000

\* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 4.060

SUBAREA Tc AND LOSS RATE DATA(AMC I):

| DEVELOPMENT TYPE/<br>LAND USE | SCS SOIL<br>GROUP | AREA<br>(ACRES) | Fp<br>(INCH/HR) | Ap<br>(DECIMAL) | SCS<br>CN | Tc<br>(MIN.) |
|-------------------------------|-------------------|-----------------|-----------------|-----------------|-----------|--------------|
|-------------------------------|-------------------|-----------------|-----------------|-----------------|-----------|--------------|

RESIDENTIAL

|                      |   |      |      |       |    |      |
|----------------------|---|------|------|-------|----|------|
| "11+ DWELLINGS/ACRE" | D | 0.05 | 0.20 | 0.200 | 57 | 5.00 |
|----------------------|---|------|------|-------|----|------|

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20

SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.200

SUBAREA RUNOFF(CFS) = 0.18

TOTAL AREA(ACRES) = 0.05 PEAK FLOW RATE(CFS) = 0.18

\*\*\*\*\*

FLOW PROCESS FROM NODE 901.00 TO NODE 902.00 IS CODE = 61

-----  
>>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>>(STANDARD CURB SECTION USED)<<<<<  
=====

UPSTREAM ELEVATION(FEET) = 259.57 DOWNSTREAM ELEVATION(FEET) = 255.86  
STREET LENGTH(FEET) = 170.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 11.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 5.50  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curb-to-curb) = 0.0950  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.84

\*\*\*STREET FLOW SPLITS OVER STREET-CROWN\*\*\*

FULL DEPTH(FEET) = 0.35 FLOOD WIDTH(FEET) = 11.00  
FULL HALF-STREET VELOCITY(FEET/SEC.) = 0.55  
SPLIT DEPTH(FEET) = 0.21 SPLIT FLOOD WIDTH(FEET) = 4.09  
SPLIT FLOW(CFS) = 0.11 SPLIT VELOCITY(FEET/SEC.) = 0.38

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.35  
HALFSTREET FLOOD WIDTH(FEET) = 11.00  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 0.55  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.19  
STREET FLOW TRAVEL TIME(MIN.) = 5.14 Tc(MIN.) = 10.14  
\* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.708

SUBAREA LOSS RATE DATA(AMC I):

| DEVELOPMENT TYPE/<br>LAND USE                                 | SCS SOIL<br>GROUP | AREA<br>(ACRES) | Fp<br>(INCH/HR) | Ap<br>(DECIMAL) | SCS<br>CN |
|---|-------------------|-----------------|-----------------|-----------------|-----------|
| RESIDENTIAL   |                   |                 |                 |                 |           |
| "11+ DWELLINGS/ACRE"  | D                 | 0.55            | 0.20            | 0.200           | 57        |
| SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20        |                   |                 |                 |                 |           |
| SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.200            |                   |                 |                 |                 |           |
| SUBAREA AREA(ACRES) = 0.55 SUBAREA RUNOFF(CFS) = 1.32         |                   |                 |                 |                 |           |
| EFFECTIVE AREA(ACRES) = 0.60 AREA-AVERAGED Fm(INCH/HR) = 0.04 |                   |                 |                 |                 |           |
| AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.20      |                   |                 |                 |                 |           |
| TOTAL AREA(ACRES) = 0.6 PEAK FLOW RATE(CFS) = 1.44            |                   |                 |                 |                 |           |

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.35 HALFSTREET FLOOD WIDTH(FEET) = 11.00  
FLOW VELOCITY(FEET/SEC.) = 0.55 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.19  
LONGEST FLOWPATH FROM NODE 900.00 TO NODE 902.00 = 249.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 700.00 TO NODE 701.00 IS CODE = 21  
-----

>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 109.00  
ELEVATION DATA: UPSTREAM(FEET) = 264.18 DOWNSTREAM(FEET) = 262.49

$T_c = K * [(LENGTH^{**} 3.00) / (ELEVATION\ CHANGE)]^{**} 0.20$   
SUBAREA ANALYSIS USED MINIMUM  $T_c$ (MIN.) = 5.000  
\* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 4.060  
SUBAREA  $T_c$  AND LOSS RATE DATA(AMC I):

| DEVELOPMENT TYPE/<br>LAND USE | SCS SOIL<br>GROUP | AREA<br>(ACRES) | Fp<br>(INCH/HR) | Ap<br>(DECIMAL) | SCS<br>CN | $T_c$<br>(MIN.) |
|-------------------------------|-------------------|-----------------|-----------------|-----------------|-----------|-----------------|
| RESIDENTIAL                   |                   |                 |                 |                 |           |                 |
| "11+ DWELLINGS/ACRE"          | D                 | 0.11            | 0.20            | 0.200           | 57        | 5.00            |

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20  
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.200  
SUBAREA RUNOFF(CFS) = 0.40  
TOTAL AREA(ACRES) = 0.11 PEAK FLOW RATE(CFS) = 0.40

\*\*\*\*\*

FLOW PROCESS FROM NODE 701.00 TO NODE 702.00 IS CODE = 61

-----

>>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>>(STANDARD CURB SECTION USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 262.49 DOWNSTREAM ELEVATION(FEET) = 257.76  
STREET LENGTH(FEET) = 359.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 11.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 5.50  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0950  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.28  
\*\*\*STREET FLOWING FULL\*\*\*  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.36  
HALFSTREET FLOOD WIDTH(FEET) = 11.00  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 0.45  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.16  
STREET FLOW TRAVEL TIME(MIN.) = 13.40  $T_c$ (MIN.) = 18.40  
\* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 1.924

SUBAREA LOSS RATE DATA(AMC I):

| DEVELOPMENT TYPE/<br>LAND USE | SCS SOIL<br>GROUP | AREA<br>(ACRES) | Fp<br>(INCH/HR) | Ap<br>(DECIMAL) | SCS<br>CN |
|-------------------------------|-------------------|-----------------|-----------------|-----------------|-----------|
|-------------------------------|-------------------|-----------------|-----------------|-----------------|-----------|



# RESIDENTIAL

"11+ DWELLINGS/ACRE"            D            0.95            0.20            0.200            57  
 SUBAREA AVERAGE PERVIOUS LOSS RATE,  $F_p$ (INCH/HR) = 0.20  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION,  $A_p$  = 0.200  
 SUBAREA AREA(ACRES) = 0.95            SUBAREA RUNOFF(CFS) = 1.61  
 EFFECTIVE AREA(ACRES) = 1.06            AREA-AVERAGED  $F_m$ (INCH/HR) = 0.04  
 AREA-AVERAGED  $F_p$ (INCH/HR) = 0.20    AREA-AVERAGED  $A_p$  = 0.20  
 TOTAL AREA(ACRES) = 1.1            PEAK FLOW RATE(CFS) = 1.80

## END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.38    HALFSTREET FLOOD WIDTH(FEET) = 11.00  
 FLOW VELOCITY(FEET/SEC.) = 0.51    DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.20  
 LONGEST FLOWPATH FROM NODE 700.00 TO NODE 702.00 = 468.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 702.00 TO NODE 1.10 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 254.75    DOWNSTREAM(FEET) = 254.02  
 FLOW LENGTH(FEET) = 87.47    MANNING'S N = 0.012  
 ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 5.1 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 4.33  
 ESTIMATED PIPE DIAMETER(INCH) = 18.00    NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 1.80  
 PIPE TRAVEL TIME(MIN.) = 0.34     $T_c$ (MIN.) = 18.74  
 LONGEST FLOWPATH FROM NODE 700.00 TO NODE 1.10 = 555.47 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1.10 TO NODE 1.10 IS CODE = 10

>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<<

\*\*\*\*\*

FLOW PROCESS FROM NODE 500.00 TO NODE 501.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
 >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 43.00  
 ELEVATION DATA: UPSTREAM(FEET) = 257.99    DOWNSTREAM(FEET) = 257.56

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$

SUBAREA ANALYSIS USED MINIMUM  $T_c$ (MIN.) = 5.000

\* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 4.060

SUBAREA  $T_c$  AND LOSS RATE DATA(AMC I ):

| DEVELOPMENT TYPE/ | SCS SOIL | AREA | $F_p$ | $A_p$ | SCS | $T_c$ |
|-------------------|----------|------|-------|-------|-----|-------|
|-------------------|----------|------|-------|-------|-----|-------|

| LAND USE             | GROUP | (ACRES) | (INCH/HR) | (DECIMAL) | CN | (MIN.) |
|----------------------|-------|---------|-----------|-----------|----|--------|
| RESIDENTIAL          |       |         |           |           |    |        |
| "11+ DWELLINGS/ACRE" | D     | 0.03    | 0.20      | 0.200     | 57 | 5.00   |

SUBAREA AVERAGE PERVIOUS LOSS RATE,  $F_p$ (INCH/HR) = 0.20  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION,  $A_p$  = 0.200  
 SUBAREA RUNOFF(CFS) = 0.11  
 TOTAL AREA(ACRES) = 0.03 PEAK FLOW RATE(CFS) = 0.11

\*\*\*\*\*

FLOW PROCESS FROM NODE 501.00 TO NODE 502.00 IS CODE = 61

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STANDARD CURB SECTION USED)<<<<<

UPSTREAM ELEVATION(FEET) = 257.56 DOWNSTREAM ELEVATION(FEET) = 256.22  
 STREET LENGTH(FEET) = 192.00 CURB HEIGHT(INCHES) = 6.0  
 STREET HALFWIDTH(FEET) = 11.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 5.50  
 INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
 OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
 STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
 Manning's FRICTION FACTOR for Streetflow Section(curb-to-curb) = 0.0950  
 Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.75

\*\*\*STREET FLOW SPLITS OVER STREET-CROWN\*\*\*

FULL DEPTH(FEET) = 0.35 FLOOD WIDTH(FEET) = 11.00  
 FULL HALF-STREET VELOCITY(FEET/SEC.) = 0.31  
 SPLIT DEPTH(FEET) = 0.33 SPLIT FLOOD WIDTH(FEET) = 10.10  
 SPLIT FLOW(CFS) = 0.34 SPLIT VELOCITY(FEET/SEC.) = 0.30

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.35  
 HALFSTREET FLOOD WIDTH(FEET) = 11.00  
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 0.31  
 PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.11

STREET FLOW TRAVEL TIME(MIN.) = 10.26  $T_c$ (MIN.) = 15.26

\* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.142

SUBAREA LOSS RATE DATA(AMC I):

| DEVELOPMENT TYPE/<br>LAND USE | SCS SOIL<br>GROUP | AREA<br>(ACRES) | $F_p$<br>(INCH/HR) | $A_p$<br>(DECIMAL) | SCS<br>CN |
|-------------------------------|-------------------|-----------------|--------------------|--------------------|-----------|
| RESIDENTIAL                   |                   |                 |                    |                    |           |

|                      |   |      |      |       |    |
|----------------------|---|------|------|-------|----|
| "11+ DWELLINGS/ACRE" | D | 0.64 | 0.20 | 0.200 | 57 |
|----------------------|---|------|------|-------|----|

SUBAREA AVERAGE PERVIOUS LOSS RATE,  $F_p$ (INCH/HR) = 0.20

SUBAREA AVERAGE PERVIOUS AREA FRACTION,  $A_p$  = 0.200

SUBAREA AREA(ACRES) = 0.64 SUBAREA RUNOFF(CFS) = 1.21

EFFECTIVE AREA(ACRES) = 0.67 AREA-AVERAGED  $F_m$ (INCH/HR) = 0.04

AREA-AVERAGED  $F_p$ (INCH/HR) = 0.20 AREA-AVERAGED  $A_p$  = 0.20

TOTAL AREA(ACRES) = 0.7 PEAK FLOW RATE(CFS) = 1.27

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.38 HALFSTREET FLOOD WIDTH(FEET) = 11.00  
FLOW VELOCITY(FEET/SEC.) = 0.37 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.14  
LONGEST FLOWPATH FROM NODE 500.00 TO NODE 502.00 = 235.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 502.00 TO NODE 1.10 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 254.84 DOWNSTREAM(FEET) = 254.02  
FLOW LENGTH(FEET) = 62.59 MANNING'S N = 0.012  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 3.8 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 4.60  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 1.27  
PIPE TRAVEL TIME(MIN.) = 0.23 Tc(MIN.) = 15.48  
LONGEST FLOWPATH FROM NODE 500.00 TO NODE 1.10 = 297.59 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1.10 TO NODE 1.10 IS CODE = 11

>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<<

=====

\*\* MAIN STREAM CONFLUENCE DATA \*\*

| STREAM<br>NUMBER | Q<br>(CFS) | Tc<br>(MIN.) | Intensity<br>(INCH/HR) | Fp(Fm)<br>(INCH/HR) | Ap   | Ae<br>(ACRES) | HEADWATER<br>NODE |
|------------------|------------|--------------|------------------------|---------------------|------|---------------|-------------------|
| 1                | 1.27       | 15.48        | 2.124                  | 0.20( 0.04)         | 0.20 | 0.7           | 500.00            |

LONGEST FLOWPATH FROM NODE 500.00 TO NODE 1.10 = 297.59 FEET.

\*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

| STREAM<br>NUMBER | Q<br>(CFS) | Tc<br>(MIN.) | Intensity<br>(INCH/HR) | Fp(Fm)<br>(INCH/HR) | Ap   | Ae<br>(ACRES) | HEADWATER<br>NODE |
|------------------|------------|--------------|------------------------|---------------------|------|---------------|-------------------|
| 1                | 1.80       | 18.74        | 1.904                  | 0.20( 0.04)         | 0.20 | 1.1           | 700.00            |

LONGEST FLOWPATH FROM NODE 700.00 TO NODE 1.10 = 555.47 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM<br>NUMBER | Q<br>(CFS) | Tc<br>(MIN.) | Intensity<br>(INCH/HR) | Fp(Fm)<br>(INCH/HR) | Ap   | Ae<br>(ACRES) | HEADWATER<br>NODE |
|------------------|------------|--------------|------------------------|---------------------|------|---------------|-------------------|
| 1                | 2.93       | 15.48        | 2.124                  | 0.20( 0.04)         | 0.20 | 1.5           | 500.00            |
| 2                | 2.93       | 18.74        | 1.904                  | 0.20( 0.04)         | 0.20 | 1.7           | 700.00            |

TOTAL AREA(ACRES) = 1.7

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 2.93 Tc(MIN.) = 18.742

EFFECTIVE AREA(ACRES) = 1.73 AREA-AVERAGED Fm(INCH/HR) = 0.04  
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.20  
 TOTAL AREA(ACRES) = 1.7  
 LONGEST FLOWPATH FROM NODE 700.00 TO NODE 1.10 = 555.47 FEET.

=====

END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 1.7 TC(MIN.) = 18.74  
 EFFECTIVE AREA(ACRES) = 1.73 AREA-AVERAGED Fm(INCH/HR)= 0.04  
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.200  
 PEAK FLOW RATE(CFS) = 2.93

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM<br>NUMBER | Q<br>(CFS) | Tc<br>(MIN.) | Intensity<br>(INCH/HR) | Fp(Fm)<br>(INCH/HR) | Ap   | Ae<br>(ACRES) | HEADWATER<br>NODE |
|------------------|------------|--------------|------------------------|---------------------|------|---------------|-------------------|
| 1                | 2.93       | 15.48        | 2.124                  | 0.20( 0.04)         | 0.20 | 1.5           | 500.00            |
| 2                | 2.93       | 18.74        | 1.904                  | 0.20( 0.04)         | 0.20 | 1.7           | 700.00            |

=====

END OF RATIONAL METHOD ANALYSIS



\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
(Reference: 1986 ORANGE COUNTY HYDROLOGY CRITERION)  
(c) Copyright 1983-2014 Advanced Engineering Software (aes)  
Ver. 21.0 Release Date: 06/01/2014 License ID 1580

Analysis prepared by:

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*  
\* OLS0109 \*  
\* LA HABRA \*  
\* PROPOSED Q25 \*  
\*\*\*\*\*

FILE NAME: 0109P25.DAT  
TIME/DATE OF STUDY: 14:37 03/09/2021

=====

USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:

=====

--\*TIME-OF-CONCENTRATION MODEL\*--

USER SPECIFIED STORM EVENT(YEAR) = 25.00  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.95  
\*DATA BANK RAINFALL USED\*  
\*ANTECEDENT MOISTURE CONDITION (AMC) I ASSUMED FOR RATIONAL METHOD\*

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

| NO. | HALF-<br>WIDTH<br>(FT) | CROWN TO<br>CROSSFALL<br>(FT) | STREET-CROSSFALL:<br>IN- / OUT- / PARK-<br>SIDE / SIDE / WAY | CURB<br>HEIGHT<br>(FT) | GUTTER-GEOMETRIES:<br>WIDTH LIP HIKE<br>(FT) (FT) (FT) | MANNING<br>FACTOR<br>(n) |
|-----|------------------------|-------------------------------|--|------------------------|--|--------------------------|
| 1   | 30.0                   | 20.0                          | 0.018/0.018/0.020  | 0.67                   | 2.00 0.0312 0.167                                      | 0.0150                   |

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

\*\*\*\*\*

FLOW PROCESS FROM NODE 100.00 TO NODE 101.00 IS CODE = 21

-----  
>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 175.00  
ELEVATION DATA: UPSTREAM(FEET) = 284.00 DOWNSTREAM(FEET) = 260.70

$T_c = K * [(LENGTH^{**} 3.00) / (ELEVATION\ CHANGE)]^{**0.20}$

SUBAREA ANALYSIS USED MINIMUM  $T_c$ (MIN.) = 5.000

\* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 4.824

SUBAREA  $T_c$  AND LOSS RATE DATA(AMC I):

| DEVELOPMENT TYPE/<br>LAND USE | SCS SOIL<br>GROUP | AREA<br>(ACRES) | Fp<br>(INCH/HR) | Ap<br>(DECIMAL) | SCS<br>CN | $T_c$<br>(MIN.) |
|-------------------------------|-------------------|-----------------|-----------------|-----------------|-----------|-----------------|
| RESIDENTIAL                   |                   |                 |                 |                 |           |                 |

|                      |   |      |      |       |    |      |
|----------------------|---|------|------|-------|----|------|
| "3-4 DWELLINGS/ACRE" | D | 1.40 | 0.20 | 0.600 | 57 | 5.00 |
|----------------------|---|------|------|-------|----|------|

SUBAREA AVERAGE PERVIOUS LOSS RATE,  $F_p$ (INCH/HR) = 0.20

SUBAREA AVERAGE PERVIOUS AREA FRACTION,  $A_p$  = 0.600

SUBAREA RUNOFF(CFS) = 5.93

TOTAL AREA(ACRES) = 1.40 PEAK FLOW RATE(CFS) = 5.93

\*\*\*\*\*

FLOW PROCESS FROM NODE 200.00 TO NODE 201.00 IS CODE = 21

-----  
>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 268.00  
ELEVATION DATA: UPSTREAM(FEET) = 272.60 DOWNSTREAM(FEET) = 265.00

$T_c = K * [(LENGTH^{**} 3.00) / (ELEVATION\ CHANGE)]^{**0.20}$

SUBAREA ANALYSIS USED MINIMUM  $T_c$ (MIN.) = 7.863

\* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 3.733

SUBAREA  $T_c$  AND LOSS RATE DATA(AMC I):

| DEVELOPMENT TYPE/<br>LAND USE | SCS SOIL<br>GROUP | AREA<br>(ACRES) | Fp<br>(INCH/HR) | Ap<br>(DECIMAL) | SCS<br>CN | $T_c$<br>(MIN.) |
|-------------------------------|-------------------|-----------------|-----------------|-----------------|-----------|-----------------|
| RESIDENTIAL                   |                   |                 |                 |                 |           |                 |

|                      |   |      |      |       |    |      |
|----------------------|---|------|------|-------|----|------|
| "3-4 DWELLINGS/ACRE" | D | 0.17 | 0.20 | 0.600 | 57 | 7.86 |
|----------------------|---|------|------|-------|----|------|

SUBAREA AVERAGE PERVIOUS LOSS RATE,  $F_p$ (INCH/HR) = 0.20

SUBAREA AVERAGE PERVIOUS AREA FRACTION,  $A_p$  = 0.600

SUBAREA RUNOFF(CFS) = 0.55

TOTAL AREA(ACRES) = 0.17 PEAK FLOW RATE(CFS) = 0.55

\*\*\*\*\*

FLOW PROCESS FROM NODE 300.00 TO NODE 301.00 IS CODE = 21

-----  
>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 97.00  
ELEVATION DATA: UPSTREAM(FEET) = 262.13 DOWNSTREAM(FEET) = 260.54

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION\ CHANGE)] ** 0.20$   
 SUBAREA ANALYSIS USED MINIMUM  $T_c(MIN.) = 5.000$   
 \* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 4.824  
 SUBAREA  $T_c$  AND LOSS RATE DATA(AMC I):  

| DEVELOPMENT TYPE/<br>LAND USE | SCS SOIL<br>GROUP | AREA<br>(ACRES) | Fp<br>(INCH/HR) | Ap<br>(DECIMAL) | SCS<br>CN | $T_c$<br>(MIN.) |
|-------------------------------|-------------------|-----------------|-----------------|-----------------|-----------|-----------------|
| RESIDENTIAL                   |                   |                 |                 |                 |           |                 |
| "11+ DWELLINGS/ACRE"          | D                 | 0.06            | 0.20            | 0.200           | 57        | 5.00            |

 SUBAREA AVERAGE PERVIOUS LOSS RATE,  $F_p(INCH/HR) = 0.20$   
 SUBAREA AVERAGE PERVIOUS AREA FRACTION,  $A_p = 0.200$   
 SUBAREA RUNOFF(CFS) = 0.26  
 TOTAL AREA(ACRES) = 0.06 PEAK FLOW RATE(CFS) = 0.26

\*\*\*\*\*

FLOW PROCESS FROM NODE 301.00 TO NODE 302.00 IS CODE = 61

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>(STANDARD CURB SECTION USED)<<<<<

UPSTREAM ELEVATION(FEET) = 260.54 DOWNSTREAM ELEVATION(FEET) = 254.77  
 STREET LENGTH(FEET) = 447.00 CURB HEIGHT(INCHES) = 6.0  
 STREET HALFWIDTH(FEET) = 11.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 5.50  
 INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
 OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
 STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
 Manning's FRICTION FACTOR for Streetflow Section(curb-to-curb) = 0.0950  
 Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.90  
 \*\*\*STREET FLOWING FULL\*\*\*

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
 STREET FLOW DEPTH(FEET) = 0.39  
 HALFSTREET FLOOD WIDTH(FEET) = 11.00  
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 0.52  
 PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.20  
 STREET FLOW TRAVEL TIME(MIN.) = 14.22  $T_c(MIN.) = 19.22$   
 \* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 2.251

SUBAREA LOSS RATE DATA(AMC I):  

| DEVELOPMENT TYPE/<br>LAND USE | SCS SOIL<br>GROUP | AREA<br>(ACRES) | Fp<br>(INCH/HR) | Ap<br>(DECIMAL) | SCS<br>CN |
|-------------------------------|-------------------|-----------------|-----------------|-----------------|-----------|
| RESIDENTIAL                   |                   |                 |                 |                 |           |
| "11+ DWELLINGS/ACRE"          | D                 | 1.50            | 0.20            | 0.200           | 57        |

 SUBAREA AVERAGE PERVIOUS LOSS RATE,  $F_p(INCH/HR) = 0.20$   
 SUBAREA AVERAGE PERVIOUS AREA FRACTION,  $A_p = 0.200$   
 SUBAREA AREA(ACRES) = 1.50 SUBAREA RUNOFF(CFS) = 2.98

EFFECTIVE AREA(ACRES) = 1.56 AREA-AVERAGED Fm(INCH/HR) = 0.04  
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.20  
TOTAL AREA(ACRES) = 1.6 PEAK FLOW RATE(CFS) = 3.10

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.45 HALFSTREET FLOOD WIDTH(FEET) = 11.00  
FLOW VELOCITY(FEET/SEC.) = 0.63 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.28  
LONGEST FLOWPATH FROM NODE 300.00 TO NODE 302.00 = 544.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 110.00 TO NODE 111.00 IS CODE = 21

>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 125.00

ELEVATION DATA: UPSTREAM(FEET) = 265.22 DOWNSTREAM(FEET) = 263.12

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$

SUBAREA ANALYSIS USED MINIMUM  $T_c$ (MIN.) = 5.061

\* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 4.791

SUBAREA  $T_c$  AND LOSS RATE DATA(AMC I):

| DEVELOPMENT TYPE/<br>LAND USE | SCS SOIL<br>GROUP | AREA<br>(ACRES) | Fp<br>(INCH/HR) | Ap<br>(DECIMAL) | SCS<br>CN | $T_c$<br>(MIN.) |
|-------------------------------|-------------------|-----------------|-----------------|-----------------|-----------|-----------------|
|-------------------------------|-------------------|-----------------|-----------------|-----------------|-----------|-----------------|

|                      |   |      |      |       |    |      |
|----------------------|---|------|------|-------|----|------|
| RESIDENTIAL          |   |      |      |       |    |      |
| "11+ DWELLINGS/ACRE" | D | 0.22 | 0.20 | 0.200 | 57 | 5.06 |

SUBAREA AVERAGE PERVIOUS LOSS RATE,  $F_p$ (INCH/HR) = 0.20

SUBAREA AVERAGE PERVIOUS AREA FRACTION,  $A_p$  = 0.200

SUBAREA RUNOFF(CFS) = 0.94

TOTAL AREA(ACRES) = 0.22 PEAK FLOW RATE(CFS) = 0.94

\*\*\*\*\*

FLOW PROCESS FROM NODE 111.00 TO NODE 112.00 IS CODE = 61

>>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>>(STANDARD CURB SECTION USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 263.12 DOWNSTREAM ELEVATION(FEET) = 259.84

STREET LENGTH(FEET) = 238.00 CURB HEIGHT(INCHES) = 6.0

STREET HALFWIDTH(FEET) = 11.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 5.50

INSIDE STREET CROSSFALL(DECIMAL) = 0.020

OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1

STREET PARKWAY CROSSFALL(DECIMAL) = 0.020

Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0950

Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200



\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.83

\*\*\*STREET FLOWING FULL\*\*\*

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.38

HALFSTREET FLOOD WIDTH(FEET) = 11.00

AVERAGE FLOW VELOCITY(FEET/SEC.) = 0.52

PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.20

STREET FLOW TRAVEL TIME(MIN.) = 7.57 Tc(MIN.) = 12.63

\* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 2.854

SUBAREA LOSS RATE DATA(AMC I):

| DEVELOPMENT TYPE/<br>LAND USE | SCS SOIL<br>GROUP | AREA<br>(ACRES) | Fp<br>(INCH/HR) | Ap<br>(DECIMAL) | SCS<br>CN |
|-------------------------------|-------------------|-----------------|-----------------|-----------------|-----------|
|-------------------------------|-------------------|-----------------|-----------------|-----------------|-----------|

RESIDENTIAL

|                      |   |      |      |       |    |
|----------------------|---|------|------|-------|----|
| "11+ DWELLINGS/ACRE" | D | 0.68 | 0.20 | 0.200 | 57 |
|----------------------|---|------|------|-------|----|

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20

SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.200

SUBAREA AREA(ACRES) = 0.68 SUBAREA RUNOFF(CFS) = 1.72

EFFECTIVE AREA(ACRES) = 0.90 AREA-AVERAGED Fm(INCH/HR) = 0.04

AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.20

TOTAL AREA(ACRES) = 0.9 PEAK FLOW RATE(CFS) = 2.28

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.41 HALFSTREET FLOOD WIDTH(FEET) = 11.00

FLOW VELOCITY(FEET/SEC.) = 0.57 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.23

LONGEST FLOWPATH FROM NODE 110.00 TO NODE 112.00 = 363.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 900.00 TO NODE 901.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 79.00

ELEVATION DATA: UPSTREAM(FEET) = 260.98 DOWNSTREAM(FEET) = 259.57

Tc = K\*[(LENGTH\*\* 3.00)/(ELEVATION CHANGE)]\*\*0.20

SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 5.000

\* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 4.824

SUBAREA Tc AND LOSS RATE DATA(AMC I):

| DEVELOPMENT TYPE/<br>LAND USE | SCS SOIL<br>GROUP | AREA<br>(ACRES) | Fp<br>(INCH/HR) | Ap<br>(DECIMAL) | SCS<br>CN | Tc<br>(MIN.) |
|-------------------------------|-------------------|-----------------|-----------------|-----------------|-----------|--------------|
|-------------------------------|-------------------|-----------------|-----------------|-----------------|-----------|--------------|

RESIDENTIAL

|                      |   |      |      |       |    |      |
|----------------------|---|------|------|-------|----|------|
| "11+ DWELLINGS/ACRE" | D | 0.05 | 0.20 | 0.200 | 57 | 5.00 |
|----------------------|---|------|------|-------|----|------|

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20

SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.200

SUBAREA RUNOFF(CFS) = 0.22

TOTAL AREA(ACRES) = 0.05 PEAK FLOW RATE(CFS) = 0.22

\*\*\*\*\*

FLOW PROCESS FROM NODE 901.00 TO NODE 902.00 IS CODE = 61

-----  
>>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>>(STANDARD CURB SECTION USED)<<<<<  
=====

UPSTREAM ELEVATION(FEET) = 259.57 DOWNSTREAM ELEVATION(FEET) = 255.86  
STREET LENGTH(FEET) = 170.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 11.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 5.50  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curb-to-curb) = 0.0950  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.01

\*\*\*STREET FLOW SPLITS OVER STREET-CROWN\*\*\*

FULL DEPTH(FEET) = 0.35 FLOOD WIDTH(FEET) = 11.00  
FULL HALF-STREET VELOCITY(FEET/SEC.) = 0.55  
SPLIT DEPTH(FEET) = 0.27 SPLIT FLOOD WIDTH(FEET) = 7.09  
SPLIT FLOW(CFS) = 0.27 SPLIT VELOCITY(FEET/SEC.) = 0.44

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.35  
HALFSTREET FLOOD WIDTH(FEET) = 11.00  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 0.55  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.19  
STREET FLOW TRAVEL TIME(MIN.) = 5.14 Tc(MIN.) = 10.14  
\* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 3.234

SUBAREA LOSS RATE DATA(AMC I):

| DEVELOPMENT TYPE/<br>LAND USE                          | SCS SOIL<br>GROUP | AREA<br>(ACRES)                  | Fp<br>(INCH/HR) | Ap<br>(DECIMAL) | SCS<br>CN |
|--|-------------------|----------------------------------|-----------------|-----------------|-----------|
| RESIDENTIAL  |                   |                                  |                 |                 |           |
| "11+ DWELLINGS/ACRE"                                   | D                 | 0.55                             | 0.20            | 0.200           | 57        |
| SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20 |                   |                                  |                 |                 |           |
| SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.200     |                   |                                  |                 |                 |           |
| SUBAREA AREA(ACRES) = 0.55                             |                   | SUBAREA RUNOFF(CFS) = 1.58       |                 |                 |           |
| EFFECTIVE AREA(ACRES) = 0.60                           |                   | AREA-AVERAGED Fm(INCH/HR) = 0.04 |                 |                 |           |
| AREA-AVERAGED Fp(INCH/HR) = 0.20                       |                   | AREA-AVERAGED Ap = 0.20          |                 |                 |           |
| TOTAL AREA(ACRES) = 0.6                                |                   | PEAK FLOW RATE(CFS) = 1.72       |                 |                 |           |

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.36 HALFSTREET FLOOD WIDTH(FEET) = 11.00  
FLOW VELOCITY(FEET/SEC.) = 0.59 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.21  
LONGEST FLOWPATH FROM NODE 900.00 TO NODE 902.00 = 249.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 700.00 TO NODE 701.00 IS CODE = 21  
-----

>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 109.00  
ELEVATION DATA: UPSTREAM(FEET) = 264.18 DOWNSTREAM(FEET) = 262.49

$T_c = K * [(LENGTH^{**} 3.00) / (ELEVATION\ CHANGE)]^{**} 0.20$   
SUBAREA ANALYSIS USED MINIMUM  $T_c$ (MIN.) = 5.000  
\* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 4.824  
SUBAREA  $T_c$  AND LOSS RATE DATA(AMC I):

| DEVELOPMENT TYPE/<br>LAND USE | SCS SOIL<br>GROUP | AREA<br>(ACRES) | Fp<br>(INCH/HR) | Ap<br>(DECIMAL) | SCS<br>CN | $T_c$<br>(MIN.) |
|-------------------------------|-------------------|-----------------|-----------------|-----------------|-----------|-----------------|
| RESIDENTIAL                   |                   |                 |                 |                 |           |                 |
| "11+ DWELLINGS/ACRE"          | D                 | 0.11            | 0.20            | 0.200           | 57        | 5.00            |

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20  
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.200  
SUBAREA RUNOFF(CFS) = 0.47  
TOTAL AREA(ACRES) = 0.11 PEAK FLOW RATE(CFS) = 0.47

\*\*\*\*\*

FLOW PROCESS FROM NODE 701.00 TO NODE 702.00 IS CODE = 61

-----

>>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>>(STANDARD CURB SECTION USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 262.49 DOWNSTREAM ELEVATION(FEET) = 257.76  
STREET LENGTH(FEET) = 359.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 11.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 5.50  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0950  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.56  
\*\*\*STREET FLOWING FULL\*\*\*  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.37  
HALFSTREET FLOOD WIDTH(FEET) = 11.00  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 0.49  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.18  
STREET FLOW TRAVEL TIME(MIN.) = 12.33  $T_c$ (MIN.) = 17.33  
\* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 2.387

SUBAREA LOSS RATE DATA(AMC I):

| DEVELOPMENT TYPE/<br>LAND USE | SCS SOIL<br>GROUP | AREA<br>(ACRES) | Fp<br>(INCH/HR) | Ap<br>(DECIMAL) | SCS<br>CN |
|-------------------------------|-------------------|-----------------|-----------------|-----------------|-----------|
|-------------------------------|-------------------|-----------------|-----------------|-----------------|-----------|

# RESIDENTIAL

"11+ DWELLINGS/ACRE"            D            0.95            0.20            0.200            57  
 SUBAREA AVERAGE PERVIOUS LOSS RATE,  $F_p$ (INCH/HR) = 0.20  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION,  $A_p$  = 0.200  
 SUBAREA AREA(ACRES) = 0.95            SUBAREA RUNOFF(CFS) = 2.01  
 EFFECTIVE AREA(ACRES) = 1.06            AREA-AVERAGED  $F_m$ (INCH/HR) = 0.04  
 AREA-AVERAGED  $F_p$ (INCH/HR) = 0.20            AREA-AVERAGED  $A_p$  = 0.20  
 TOTAL AREA(ACRES) = 1.1            PEAK FLOW RATE(CFS) = 2.24

## END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.41    HALFSTREET FLOOD WIDTH(FEET) = 11.00  
 FLOW VELOCITY(FEET/SEC.) = 0.56    DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.23  
 LONGEST FLOWPATH FROM NODE 700.00 TO NODE 702.00 = 468.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 702.00 TO NODE 1.10 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 254.75    DOWNSTREAM(FEET) = 254.02  
 FLOW LENGTH(FEET) = 87.47    MANNING'S N = 0.012  
 ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 5.7 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 4.61  
 ESTIMATED PIPE DIAMETER(INCH) = 18.00    NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 2.24  
 PIPE TRAVEL TIME(MIN.) = 0.32     $T_c$ (MIN.) = 17.64  
 LONGEST FLOWPATH FROM NODE 700.00 TO NODE 1.10 = 555.47 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1.10 TO NODE 1.10 IS CODE = 10

>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<<

\*\*\*\*\*

FLOW PROCESS FROM NODE 500.00 TO NODE 501.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
 >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 43.00  
 ELEVATION DATA: UPSTREAM(FEET) = 257.99    DOWNSTREAM(FEET) = 257.56

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$

SUBAREA ANALYSIS USED MINIMUM  $T_c$ (MIN.) = 5.000

\* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 4.824

SUBAREA  $T_c$  AND LOSS RATE DATA(AMC I ):

| DEVELOPMENT TYPE/ | SCS SOIL | AREA | $F_p$ | $A_p$ | SCS | $T_c$ |
|-------------------|----------|------|-------|-------|-----|-------|
|-------------------|----------|------|-------|-------|-----|-------|

| LAND USE             | GROUP | (ACRES) | (INCH/HR) | (DECIMAL) | CN | (MIN.) |
|----------------------|-------|---------|-----------|-----------|----|--------|
| RESIDENTIAL          |       |         |           |           |    |        |
| "11+ DWELLINGS/ACRE" | D     | 0.03    | 0.20      | 0.200     | 57 | 5.00   |

SUBAREA AVERAGE PERVIOUS LOSS RATE,  $F_p$ (INCH/HR) = 0.20  
SUBAREA AVERAGE PERVIOUS AREA FRACTION,  $A_p$  = 0.200  
SUBAREA RUNOFF(CFS) = 0.13  
TOTAL AREA(ACRES) = 0.03 PEAK FLOW RATE(CFS) = 0.13

\*\*\*\*\*

FLOW PROCESS FROM NODE 501.00 TO NODE 502.00 IS CODE = 61

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STANDARD CURB SECTION USED)<<<<<

UPSTREAM ELEVATION(FEET) = 257.56 DOWNSTREAM ELEVATION(FEET) = 256.22  
STREET LENGTH(FEET) = 192.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 11.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 5.50  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0950  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.92

\*\*\*STREET FLOWING FULL\*\*\*

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.35

HALFSTREET FLOOD WIDTH(FEET) = 11.00

AVERAGE FLOW VELOCITY(FEET/SEC.) = 0.33

PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.12

STREET FLOW TRAVEL TIME(MIN.) = 9.80  $T_c$ (MIN.) = 14.80

\* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 2.610

SUBAREA LOSS RATE DATA(AMC I):

| DEVELOPMENT TYPE/<br>LAND USE | SCS SOIL<br>GROUP | AREA<br>(ACRES) | $F_p$<br>(INCH/HR) | $A_p$<br>(DECIMAL) | SCS<br>CN |
|-------------------------------|-------------------|-----------------|--------------------|--------------------|-----------|
|-------------------------------|-------------------|-----------------|--------------------|--------------------|-----------|

RESIDENTIAL

|                      |   |      |      |       |    |
|----------------------|---|------|------|-------|----|
| "11+ DWELLINGS/ACRE" | D | 0.64 | 0.20 | 0.200 | 57 |
|----------------------|---|------|------|-------|----|

SUBAREA AVERAGE PERVIOUS LOSS RATE,  $F_p$ (INCH/HR) = 0.20

SUBAREA AVERAGE PERVIOUS AREA FRACTION,  $A_p$  = 0.200

SUBAREA AREA(ACRES) = 0.64 SUBAREA RUNOFF(CFS) = 1.48

EFFECTIVE AREA(ACRES) = 0.67 AREA-AVERAGED  $F_m$ (INCH/HR) = 0.04

AREA-AVERAGED  $F_p$ (INCH/HR) = 0.20 AREA-AVERAGED  $A_p$  = 0.20

TOTAL AREA(ACRES) = 0.7 PEAK FLOW RATE(CFS) = 1.55

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.40 HALFSTREET FLOOD WIDTH(FEET) = 11.00

FLOW VELOCITY(FEET/SEC.) = 0.40 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.16  
LONGEST FLOWPATH FROM NODE 500.00 TO NODE 502.00 = 235.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 502.00 TO NODE 1.10 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 254.84 DOWNSTREAM(FEET) = 254.02  
FLOW LENGTH(FEET) = 62.59 MANNING'S N = 0.012  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 4.2 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 4.89  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 1.55  
PIPE TRAVEL TIME(MIN.) = 0.21 Tc(MIN.) = 15.01  
LONGEST FLOWPATH FROM NODE 500.00 TO NODE 1.10 = 297.59 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1.10 TO NODE 1.10 IS CODE = 11

-----  
>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<

=====

\*\* MAIN STREAM CONFLUENCE DATA \*\*

| STREAM<br>NUMBER | Q<br>(CFS) | Tc<br>(MIN.) | Intensity<br>(INCH/HR) | Fp(Fm)<br>(INCH/HR) | Ap   | Ae<br>(ACRES) | HEADWATER<br>NODE |
|------------------|------------|--------------|------------------------|---------------------|------|---------------|-------------------|
| 1                | 1.55       | 15.01        | 2.589                  | 0.20( 0.04)         | 0.20 | 0.7           | 500.00            |

LONGEST FLOWPATH FROM NODE 500.00 TO NODE 1.10 = 297.59 FEET.

\*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

| STREAM<br>NUMBER | Q<br>(CFS) | Tc<br>(MIN.) | Intensity<br>(INCH/HR) | Fp(Fm)<br>(INCH/HR) | Ap   | Ae<br>(ACRES) | HEADWATER<br>NODE |
|------------------|------------|--------------|------------------------|---------------------|------|---------------|-------------------|
| 1                | 2.24       | 17.64        | 2.363                  | 0.20( 0.04)         | 0.20 | 1.1           | 700.00            |

LONGEST FLOWPATH FROM NODE 700.00 TO NODE 1.10 = 555.47 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM<br>NUMBER | Q<br>(CFS) | Tc<br>(MIN.) | Intensity<br>(INCH/HR) | Fp(Fm)<br>(INCH/HR) | Ap   | Ae<br>(ACRES) | HEADWATER<br>NODE |
|------------------|------------|--------------|------------------------|---------------------|------|---------------|-------------------|
| 1                | 3.64       | 15.01        | 2.589                  | 0.20( 0.04)         | 0.20 | 1.6           | 500.00            |
| 2                | 3.65       | 17.64        | 2.363                  | 0.20( 0.04)         | 0.20 | 1.7           | 700.00            |

TOTAL AREA(ACRES) = 1.7

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 3.65 Tc(MIN.) = 17.641  
EFFECTIVE AREA(ACRES) = 1.73 AREA-AVERAGED Fm(INCH/HR) = 0.04  
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.20  
TOTAL AREA(ACRES) = 1.7  
LONGEST FLOWPATH FROM NODE 700.00 TO NODE 1.10 = 555.47 FEET.

=====

END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 1.7 TC(MIN.) = 17.64  
 EFFECTIVE AREA(ACRES) = 1.73 AREA-AVERAGED Fm(INCH/HR)= 0.04  
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.200  
 PEAK FLOW RATE(CFS) = 3.65

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM<br>NUMBER | Q<br>(CFS) | Tc<br>(MIN.) | Intensity<br>(INCH/HR) | Fp(Fm)<br>(INCH/HR) | Ap   | Ae<br>(ACRES) | HEADWATER<br>NODE |
|------------------|------------|--------------|------------------------|---------------------|------|---------------|-------------------|
| 1                | 3.64       | 15.01        | 2.589                  | 0.20( 0.04)         | 0.20 | 1.6           | 500.00            |
| 2                | 3.65       | 17.64        | 2.363                  | 0.20( 0.04)         | 0.20 | 1.7           | 700.00            |

=====

=====

END OF RATIONAL METHOD ANALYSIS



\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
(Reference: 1986 ORANGE COUNTY HYDROLOGY CRITERION)  
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Ver. 21.0 Release Date: 06/01/2014 License ID 1580

Analysis prepared by:

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*

\* OLS0109 \*  
\* LA HABRA \*  
\* PROPOSED Q100 \*  
\*\*\*\*\*

FILE NAME: 0109P100.DAT  
TIME/DATE OF STUDY: 14:38 03/09/2021

=====

USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:

=====

--\*TIME-OF-CONCENTRATION MODEL\*--

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.95  
\*DATA BANK RAINFALL USED\*  
\*ANTECEDENT MOISTURE CONDITION (AMC) I ASSUMED FOR RATIONAL METHOD\*

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

| NO. | HALF-<br>WIDTH<br>(FT) | CROWN TO<br>CROSSFALL<br>(FT) | STREET-CROSSFALL:<br>IN- / OUT- / PARK-<br>SIDE / SIDE / WAY | CURB<br>HEIGHT<br>(FT) | GUTTER-GEOMETRIES:<br>WIDTH LIP HIKE<br>(FT) (FT) (FT) | MANNING<br>FACTOR<br>(n) |
|-----|------------------------|-------------------------------|--|------------------------|--|--------------------------|
| 1   | 30.0                   | 20.0                          | 0.018/0.018/0.020  | 0.67                   | 2.00 0.0312 0.167                                      | 0.0150                   |

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

\*\*\*\*\*

FLOW PROCESS FROM NODE 100.00 TO NODE 101.00 IS CODE = 21



-----  
>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 175.00  
ELEVATION DATA: UPSTREAM(FEET) = 284.00 DOWNSTREAM(FEET) = 260.70

$T_c = K * [(LENGTH^{**} 3.00) / (ELEVATION\ CHANGE)]^{**0.20}$   
SUBAREA ANALYSIS USED MINIMUM  $T_c$ (MIN.) = 5.000  
\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 6.187  
SUBAREA  $T_c$  AND LOSS RATE DATA(AMC I):

| DEVELOPMENT TYPE/<br>LAND USE | SCS SOIL<br>GROUP | AREA<br>(ACRES) | Fp<br>(INCH/HR) | Ap<br>(DECIMAL) | SCS<br>CN | $T_c$<br>(MIN.) |
|-------------------------------|-------------------|-----------------|-----------------|-----------------|-----------|-----------------|
| RESIDENTIAL                   |                   |                 |                 |                 |           |                 |
| "3-4 DWELLINGS/ACRE"          | D                 | 1.40            | 0.20            | 0.600           | 57        | 5.00            |

SUBAREA AVERAGE PERVIOUS LOSS RATE,  $F_p$ (INCH/HR) = 0.20  
SUBAREA AVERAGE PERVIOUS AREA FRACTION,  $A_p$  = 0.600  
SUBAREA RUNOFF(CFS) = 7.64  
TOTAL AREA(ACRES) = 1.40 PEAK FLOW RATE(CFS) = 7.64

\*\*\*\*\*

FLOW PROCESS FROM NODE 200.00 TO NODE 201.00 IS CODE = 21

-----

>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 268.00  
ELEVATION DATA: UPSTREAM(FEET) = 272.60 DOWNSTREAM(FEET) = 265.00

$T_c = K * [(LENGTH^{**} 3.00) / (ELEVATION\ CHANGE)]^{**0.20}$   
SUBAREA ANALYSIS USED MINIMUM  $T_c$ (MIN.) = 7.863  
\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 4.773  
SUBAREA  $T_c$  AND LOSS RATE DATA(AMC I):

| DEVELOPMENT TYPE/<br>LAND USE | SCS SOIL<br>GROUP | AREA<br>(ACRES) | Fp<br>(INCH/HR) | Ap<br>(DECIMAL) | SCS<br>CN | $T_c$<br>(MIN.) |
|-------------------------------|-------------------|-----------------|-----------------|-----------------|-----------|-----------------|
| RESIDENTIAL                   |                   |                 |                 |                 |           |                 |
| "3-4 DWELLINGS/ACRE"          | D                 | 0.17            | 0.20            | 0.600           | 57        | 7.86            |

SUBAREA AVERAGE PERVIOUS LOSS RATE,  $F_p$ (INCH/HR) = 0.20  
SUBAREA AVERAGE PERVIOUS AREA FRACTION,  $A_p$  = 0.600  
SUBAREA RUNOFF(CFS) = 0.71  
TOTAL AREA(ACRES) = 0.17 PEAK FLOW RATE(CFS) = 0.71

\*\*\*\*\*

FLOW PROCESS FROM NODE 300.00 TO NODE 301.00 IS CODE = 21

-----

>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 97.00  
ELEVATION DATA: UPSTREAM(FEET) = 262.13 DOWNSTREAM(FEET) = 260.54

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION\ CHANGE)] ** 0.20$   
 SUBAREA ANALYSIS USED MINIMUM  $T_c(MIN.) = 5.000$   
 \* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 6.187  
 SUBAREA  $T_c$  AND LOSS RATE DATA(AMC I):  

| DEVELOPMENT TYPE/<br>LAND USE | SCS SOIL<br>GROUP | AREA<br>(ACRES) | Fp<br>(INCH/HR) | Ap<br>(DECIMAL) | SCS<br>CN | $T_c$<br>(MIN.) |
|-------------------------------|-------------------|-----------------|-----------------|-----------------|-----------|-----------------|
| RESIDENTIAL                   |                   |                 |                 |                 |           |                 |
| "11+ DWELLINGS/ACRE"          | D                 | 0.06            | 0.20            | 0.200           | 57        | 5.00            |

 SUBAREA AVERAGE PERVIOUS LOSS RATE,  $F_p(INCH/HR) = 0.20$   
 SUBAREA AVERAGE PERVIOUS AREA FRACTION,  $A_p = 0.200$   
 SUBAREA RUNOFF(CFS) = 0.33  
 TOTAL AREA(ACRES) = 0.06 PEAK FLOW RATE(CFS) = 0.33

\*\*\*\*\*

FLOW PROCESS FROM NODE 301.00 TO NODE 302.00 IS CODE = 61

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>(STANDARD CURB SECTION USED)<<<<<

UPSTREAM ELEVATION(FEET) = 260.54 DOWNSTREAM ELEVATION(FEET) = 254.77  
 STREET LENGTH(FEET) = 447.00 CURB HEIGHT(INCHES) = 6.0  
 STREET HALFWIDTH(FEET) = 11.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 5.50  
 INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
 OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
 STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
 Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0950  
 Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.52  
 \*\*\*STREET FLOWING FULL\*\*\*

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
 STREET FLOW DEPTH(FEET) = 0.42  
 HALFSTREET FLOOD WIDTH(FEET) = 11.00  
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 0.58  
 PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.25  
 STREET FLOW TRAVEL TIME(MIN.) = 12.75  $T_c(MIN.) = 17.75$   
 \* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 2.994

SUBAREA LOSS RATE DATA(AMC I):  

| DEVELOPMENT TYPE/<br>LAND USE | SCS SOIL<br>GROUP | AREA<br>(ACRES) | Fp<br>(INCH/HR) | Ap<br>(DECIMAL) | SCS<br>CN |
|-------------------------------|-------------------|-----------------|-----------------|-----------------|-----------|
| RESIDENTIAL                   |                   |                 |                 |                 |           |
| "11+ DWELLINGS/ACRE"          | D                 | 1.50            | 0.20            | 0.200           | 57        |

 SUBAREA AVERAGE PERVIOUS LOSS RATE,  $F_p(INCH/HR) = 0.20$   
 SUBAREA AVERAGE PERVIOUS AREA FRACTION,  $A_p = 0.200$   
 SUBAREA AREA(ACRES) = 1.50 SUBAREA RUNOFF(CFS) = 3.99

EFFECTIVE AREA(ACRES) = 1.56 AREA-AVERAGED Fm(INCH/HR) = 0.04  
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.20  
TOTAL AREA(ACRES) = 1.6 PEAK FLOW RATE(CFS) = 4.15

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.49 HALFSTREET FLOOD WIDTH(FEET) = 11.00  
FLOW VELOCITY(FEET/SEC.) = 0.71 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.35  
LONGEST FLOWPATH FROM NODE 300.00 TO NODE 302.00 = 544.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 110.00 TO NODE 111.00 IS CODE = 21

>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 125.00

ELEVATION DATA: UPSTREAM(FEET) = 265.22 DOWNSTREAM(FEET) = 263.12

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$

SUBAREA ANALYSIS USED MINIMUM  $T_c$ (MIN.) = 5.061

\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 6.144

SUBAREA  $T_c$  AND LOSS RATE DATA(AMC I):

| DEVELOPMENT TYPE/<br>LAND USE | SCS SOIL<br>GROUP | AREA<br>(ACRES) | Fp<br>(INCH/HR) | Ap<br>(DECIMAL) | SCS<br>CN | $T_c$<br>(MIN.) |
|-------------------------------|-------------------|-----------------|-----------------|-----------------|-----------|-----------------|
|-------------------------------|-------------------|-----------------|-----------------|-----------------|-----------|-----------------|

|                      |   |      |      |       |    |      |
|----------------------|---|------|------|-------|----|------|
| RESIDENTIAL          |   |      |      |       |    |      |
| "11+ DWELLINGS/ACRE" | D | 0.22 | 0.20 | 0.200 | 57 | 5.06 |

SUBAREA AVERAGE PERVIOUS LOSS RATE,  $F_p$ (INCH/HR) = 0.20

SUBAREA AVERAGE PERVIOUS AREA FRACTION,  $A_p$  = 0.200

SUBAREA RUNOFF(CFS) = 1.21

TOTAL AREA(ACRES) = 0.22 PEAK FLOW RATE(CFS) = 1.21

\*\*\*\*\*

FLOW PROCESS FROM NODE 111.00 TO NODE 112.00 IS CODE = 61

>>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>>(STANDARD CURB SECTION USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 263.12 DOWNSTREAM ELEVATION(FEET) = 259.84

STREET LENGTH(FEET) = 238.00 CURB HEIGHT(INCHES) = 6.0

STREET HALFWIDTH(FEET) = 11.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 5.50

INSIDE STREET CROSSFALL(DECIMAL) = 0.020

OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1

STREET PARKWAY CROSSFALL(DECIMAL) = 0.020

Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0950

Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.39

\*\*\*STREET FLOWING FULL\*\*\*

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.41

HALFSTREET FLOOD WIDTH(FEET) = 11.00

AVERAGE FLOW VELOCITY(FEET/SEC.) = 0.58

PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.24

STREET FLOW TRAVEL TIME(MIN.) = 6.80 Tc(MIN.) = 11.86

\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 3.772

SUBAREA LOSS RATE DATA(AMC I):

| DEVELOPMENT TYPE/<br>LAND USE | SCS SOIL<br>GROUP | AREA<br>(ACRES) | Fp<br>(INCH/HR) | Ap<br>(DECIMAL) | SCS<br>CN |
|-------------------------------|-------------------|-----------------|-----------------|-----------------|-----------|
|-------------------------------|-------------------|-----------------|-----------------|-----------------|-----------|

RESIDENTIAL

|                      |   |      |      |       |    |
|----------------------|---|------|------|-------|----|
| "11+ DWELLINGS/ACRE" | D | 0.68 | 0.20 | 0.200 | 57 |
|----------------------|---|------|------|-------|----|

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20

SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.200

SUBAREA AREA(ACRES) = 0.68 SUBAREA RUNOFF(CFS) = 2.28

EFFECTIVE AREA(ACRES) = 0.90 AREA-AVERAGED Fm(INCH/HR) = 0.04

AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.20

TOTAL AREA(ACRES) = 0.9 PEAK FLOW RATE(CFS) = 3.02

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.44 HALFSTREET FLOOD WIDTH(FEET) = 11.00

FLOW VELOCITY(FEET/SEC.) = 0.64 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.28

LONGEST FLOWPATH FROM NODE 110.00 TO NODE 112.00 = 363.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 900.00 TO NODE 901.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 79.00

ELEVATION DATA: UPSTREAM(FEET) = 260.98 DOWNSTREAM(FEET) = 259.57

Tc = K\*[(LENGTH\*\* 3.00)/(ELEVATION CHANGE)]\*\*0.20

SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 5.000

\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 6.187

SUBAREA Tc AND LOSS RATE DATA(AMC I):

| DEVELOPMENT TYPE/<br>LAND USE | SCS SOIL<br>GROUP | AREA<br>(ACRES) | Fp<br>(INCH/HR) | Ap<br>(DECIMAL) | SCS<br>CN | Tc<br>(MIN.) |
|-------------------------------|-------------------|-----------------|-----------------|-----------------|-----------|--------------|
|-------------------------------|-------------------|-----------------|-----------------|-----------------|-----------|--------------|

RESIDENTIAL

|                      |   |      |      |       |    |      |
|----------------------|---|------|------|-------|----|------|
| "11+ DWELLINGS/ACRE" | D | 0.05 | 0.20 | 0.200 | 57 | 5.00 |
|----------------------|---|------|------|-------|----|------|

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20

SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.200

SUBAREA RUNOFF(CFS) = 0.28

TOTAL AREA(ACRES) = 0.05 PEAK FLOW RATE(CFS) = 0.28

\*\*\*\*\*

FLOW PROCESS FROM NODE 901.00 TO NODE 902.00 IS CODE = 61

-----  
>>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>>(STANDARD CURB SECTION USED)<<<<<  
=====

UPSTREAM ELEVATION(FEET) = 259.57 DOWNSTREAM ELEVATION(FEET) = 255.86  
STREET LENGTH(FEET) = 170.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 11.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 5.50  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curb-to-curb) = 0.0950  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.31

\*\*\*STREET FLOW SPLITS OVER STREET-CROWN\*\*\*

FULL DEPTH(FEET) = 0.35 FLOOD WIDTH(FEET) = 11.00  
FULL HALF-STREET VELOCITY(FEET/SEC.) = 0.55  
SPLIT DEPTH(FEET) = 0.32 SPLIT FLOOD WIDTH(FEET) = 9.93  
SPLIT FLOW(CFS) = 0.58 SPLIT VELOCITY(FEET/SEC.) = 0.53

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.35  
HALFSTREET FLOOD WIDTH(FEET) = 11.00  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 0.55  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.19  
STREET FLOW TRAVEL TIME(MIN.) = 5.14 Tc(MIN.) = 10.14  
\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 4.127

SUBAREA LOSS RATE DATA(AMC I):

| DEVELOPMENT TYPE/<br>LAND USE                          | SCS SOIL<br>GROUP | AREA<br>(ACRES)                  | Fp<br>(INCH/HR) | Ap<br>(DECIMAL) | SCS<br>CN |
|--|-------------------|----------------------------------|-----------------|-----------------|-----------|
| RESIDENTIAL  |                   |                                  |                 |                 |           |
| "11+ DWELLINGS/ACRE"                                   | D                 | 0.55                             | 0.20            | 0.200           | 57        |
| SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20 |                   |                                  |                 |                 |           |
| SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.200     |                   |                                  |                 |                 |           |
| SUBAREA AREA(ACRES) = 0.55                             |                   | SUBAREA RUNOFF(CFS) = 2.02       |                 |                 |           |
| EFFECTIVE AREA(ACRES) = 0.60                           |                   | AREA-AVERAGED Fm(INCH/HR) = 0.04 |                 |                 |           |
| AREA-AVERAGED Fp(INCH/HR) = 0.20                       |                   | AREA-AVERAGED Ap = 0.20          |                 |                 |           |
| TOTAL AREA(ACRES) = 0.6                                |                   | PEAK FLOW RATE(CFS) = 2.21       |                 |                 |           |

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.38 HALFSTREET FLOOD WIDTH(FEET) = 11.00  
FLOW VELOCITY(FEET/SEC.) = 0.65 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.25  
LONGEST FLOWPATH FROM NODE 900.00 TO NODE 902.00 = 249.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 700.00 TO NODE 701.00 IS CODE = 21  
-----

>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 109.00  
ELEVATION DATA: UPSTREAM(FEET) = 264.18 DOWNSTREAM(FEET) = 262.49

$T_c = K * [(LENGTH^{**} 3.00) / (ELEVATION\ CHANGE)]^{**} 0.20$   
SUBAREA ANALYSIS USED MINIMUM  $T_c$ (MIN.) = 5.000  
\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 6.187  
SUBAREA  $T_c$  AND LOSS RATE DATA(AMC I):

| DEVELOPMENT TYPE/<br>LAND USE | SCS SOIL<br>GROUP | AREA<br>(ACRES) | Fp<br>(INCH/HR) | Ap<br>(DECIMAL) | SCS<br>CN | $T_c$<br>(MIN.) |
|-------------------------------|-------------------|-----------------|-----------------|-----------------|-----------|-----------------|
| RESIDENTIAL                   |                   |                 |                 |                 |           |                 |
| "11+ DWELLINGS/ACRE"          | D                 | 0.11            | 0.20            | 0.200           | 57        | 5.00            |

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20  
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.200  
SUBAREA RUNOFF(CFS) = 0.61  
TOTAL AREA(ACRES) = 0.11 PEAK FLOW RATE(CFS) = 0.61

\*\*\*\*\*

FLOW PROCESS FROM NODE 701.00 TO NODE 702.00 IS CODE = 61

-----

>>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>>(STANDARD CURB SECTION USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 262.49 DOWNSTREAM ELEVATION(FEET) = 257.76  
STREET LENGTH(FEET) = 359.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 11.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 5.50  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0950  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.05  
\*\*\*STREET FLOWING FULL\*\*\*  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.40  
HALFSTREET FLOOD WIDTH(FEET) = 11.00  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 0.54  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.22  
STREET FLOW TRAVEL TIME(MIN.) = 11.03  $T_c$ (MIN.) = 16.03  
\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 3.174

SUBAREA LOSS RATE DATA(AMC I):

| DEVELOPMENT TYPE/<br>LAND USE | SCS SOIL<br>GROUP | AREA<br>(ACRES) | Fp<br>(INCH/HR) | Ap<br>(DECIMAL) | SCS<br>CN |
|-------------------------------|-------------------|-----------------|-----------------|-----------------|-----------|
|-------------------------------|-------------------|-----------------|-----------------|-----------------|-----------|

# RESIDENTIAL

"11+ DWELLINGS/ACRE"            D            0.95            0.20            0.200            57  
 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.200  
 SUBAREA AREA(ACRES) = 0.95            SUBAREA RUNOFF(CFS) = 2.68  
 EFFECTIVE AREA(ACRES) = 1.06            AREA-AVERAGED Fm(INCH/HR) = 0.04  
 AREA-AVERAGED Fp(INCH/HR) = 0.20            AREA-AVERAGED Ap = 0.20  
 TOTAL AREA(ACRES) = 1.1            PEAK FLOW RATE(CFS) = 2.99

## END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.44    HALFSTREET FLOOD WIDTH(FEET) = 11.00  
 FLOW VELOCITY(FEET/SEC.) = 0.63    DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.28  
 LONGEST FLOWPATH FROM NODE 700.00 TO NODE 702.00 = 468.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 702.00 TO NODE 1.10 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 254.75    DOWNSTREAM(FEET) = 254.02  
 FLOW LENGTH(FEET) = 87.47    MANNING'S N = 0.012  
 ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 6.7 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 4.99  
 ESTIMATED PIPE DIAMETER(INCH) = 18.00    NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 2.99  
 PIPE TRAVEL TIME(MIN.) = 0.29    Tc(MIN.) = 16.32  
 LONGEST FLOWPATH FROM NODE 700.00 TO NODE 1.10 = 555.47 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1.10 TO NODE 1.10 IS CODE = 10

>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<<

\*\*\*\*\*

FLOW PROCESS FROM NODE 500.00 TO NODE 501.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
 >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 43.00  
 ELEVATION DATA: UPSTREAM(FEET) = 257.99    DOWNSTREAM(FEET) = 257.56

Tc = K\*[(LENGTH\*\* 3.00)/(ELEVATION CHANGE)]\*\*0.20  
 SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 5.000  
 \* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 6.187

SUBAREA Tc AND LOSS RATE DATA(AMC I ):

| DEVELOPMENT TYPE/ | SCS SOIL | AREA | Fp | Ap | SCS | Tc |
|-------------------|----------|------|----|----|-----|----|
|-------------------|----------|------|----|----|-----|----|

| LAND USE             | GROUP | (ACRES) | (INCH/HR) | (DECIMAL) | CN | (MIN.) |
|----------------------|-------|---------|-----------|-----------|----|--------|
| RESIDENTIAL          |       |         |           |           |    |        |
| "11+ DWELLINGS/ACRE" | D     | 0.03    | 0.20      | 0.200     | 57 | 5.00   |

SUBAREA AVERAGE PERVIOUS LOSS RATE,  $F_p$ (INCH/HR) = 0.20  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION,  $A_p$  = 0.200  
 SUBAREA RUNOFF(CFS) = 0.17  
 TOTAL AREA(ACRES) = 0.03 PEAK FLOW RATE(CFS) = 0.17

\*\*\*\*\*

FLOW PROCESS FROM NODE 501.00 TO NODE 502.00 IS CODE = 61

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STANDARD CURB SECTION USED)<<<<<

UPSTREAM ELEVATION(FEET) = 257.56 DOWNSTREAM ELEVATION(FEET) = 256.22  
 STREET LENGTH(FEET) = 192.00 CURB HEIGHT(INCHES) = 6.0  
 STREET HALFWIDTH(FEET) = 11.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 5.50  
 INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
 OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
 STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
 Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0950  
 Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.22

\*\*\*STREET FLOWING FULL\*\*\*

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.38

HALFSTREET FLOOD WIDTH(FEET) = 11.00

AVERAGE FLOW VELOCITY(FEET/SEC.) = 0.36

PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.14

STREET FLOW TRAVEL TIME(MIN.) = 8.79  $T_c$ (MIN.) = 13.79

\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 3.460

SUBAREA LOSS RATE DATA(AMC I):

| DEVELOPMENT TYPE/<br>LAND USE | SCS SOIL<br>GROUP | AREA<br>(ACRES) | $F_p$<br>(INCH/HR) | $A_p$<br>(DECIMAL) | SCS<br>CN |
|-------------------------------|-------------------|-----------------|--------------------|--------------------|-----------|
|-------------------------------|-------------------|-----------------|--------------------|--------------------|-----------|

RESIDENTIAL

|                      |   |      |      |       |    |
|----------------------|---|------|------|-------|----|
| "11+ DWELLINGS/ACRE" | D | 0.64 | 0.20 | 0.200 | 57 |
|----------------------|---|------|------|-------|----|

SUBAREA AVERAGE PERVIOUS LOSS RATE,  $F_p$ (INCH/HR) = 0.20

SUBAREA AVERAGE PERVIOUS AREA FRACTION,  $A_p$  = 0.200

SUBAREA AREA(ACRES) = 0.64 SUBAREA RUNOFF(CFS) = 1.97

EFFECTIVE AREA(ACRES) = 0.67 AREA-AVERAGED  $F_m$ (INCH/HR) = 0.04

AREA-AVERAGED  $F_p$ (INCH/HR) = 0.20 AREA-AVERAGED  $A_p$  = 0.20

TOTAL AREA(ACRES) = 0.7 PEAK FLOW RATE(CFS) = 2.06

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.43 HALFSTREET FLOOD WIDTH(FEET) = 11.00



FLOW VELOCITY(FEET/SEC.) = 0.45 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.19  
 LONGEST FLOWPATH FROM NODE 500.00 TO NODE 502.00 = 235.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 502.00 TO NODE 1.10 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 254.84 DOWNSTREAM(FEET) = 254.02  
 FLOW LENGTH(FEET) = 62.59 MANNING'S N = 0.012  
 ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 4.9 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 5.29  
 ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 2.06  
 PIPE TRAVEL TIME(MIN.) = 0.20 Tc(MIN.) = 13.99  
 LONGEST FLOWPATH FROM NODE 500.00 TO NODE 1.10 = 297.59 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1.10 TO NODE 1.10 IS CODE = 11

>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<

\*\* MAIN STREAM CONFLUENCE DATA \*\*

| STREAM<br>NUMBER | Q<br>(CFS) | Tc<br>(MIN.) | Intensity<br>(INCH/HR) | Fp(Fm)<br>(INCH/HR) | Ap   | Ae<br>(ACRES) | HEADWATER<br>NODE |
|------------------|------------|--------------|------------------------|---------------------|------|---------------|-------------------|
| 1                | 2.06       | 13.99        | 3.432                  | 0.20( 0.04)         | 0.20 | 0.7           | 500.00            |

LONGEST FLOWPATH FROM NODE 500.00 TO NODE 1.10 = 297.59 FEET.

\*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

| STREAM<br>NUMBER | Q<br>(CFS) | Tc<br>(MIN.) | Intensity<br>(INCH/HR) | Fp(Fm)<br>(INCH/HR) | Ap   | Ae<br>(ACRES) | HEADWATER<br>NODE |
|------------------|------------|--------------|------------------------|---------------------|------|---------------|-------------------|
| 1                | 2.99       | 16.32        | 3.141                  | 0.20( 0.04)         | 0.20 | 1.1           | 700.00            |

LONGEST FLOWPATH FROM NODE 700.00 TO NODE 1.10 = 555.47 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM<br>NUMBER    | Q<br>(CFS) | Tc<br>(MIN.) | Intensity<br>(INCH/HR) | Fp(Fm)<br>(INCH/HR) | Ap   | Ae<br>(ACRES) | HEADWATER<br>NODE |
|---------------------|------------|--------------|------------------------|---------------------|------|---------------|-------------------|
| 1                   | 4.86       | 13.99        | 3.432                  | 0.20( 0.04)         | 0.20 | 1.6           | 500.00            |
| 2                   | 4.88       | 16.32        | 3.141                  | 0.20( 0.04)         | 0.20 | 1.7           | 700.00            |
| TOTAL AREA(ACRES) = |            |              |                        |                     |      |               | 1.7               |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 4.88 Tc(MIN.) = 16.322  
 EFFECTIVE AREA(ACRES) = 1.73 AREA-AVERAGED Fm(INCH/HR) = 0.04  
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.20  
 TOTAL AREA(ACRES) = 1.7  
 LONGEST FLOWPATH FROM NODE 700.00 TO NODE 1.10 = 555.47 FEET.

=====

END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 1.7 TC(MIN.) = 16.32  
 EFFECTIVE AREA(ACRES) = 1.73 AREA-AVERAGED Fm(INCH/HR)= 0.04  
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.200  
 PEAK FLOW RATE(CFS) = 4.88

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM<br>NUMBER | Q<br>(CFS) | Tc<br>(MIN.) | Intensity<br>(INCH/HR) | Fp(Fm)<br>(INCH/HR) | Ap   | Ae<br>(ACRES) | HEADWATER<br>NODE |
|------------------|------------|--------------|------------------------|---------------------|------|---------------|-------------------|
| 1                | 4.86       | 13.99        | 3.432                  | 0.20( 0.04)         | 0.20 | 1.6           | 500.00            |
| 2                | 4.88       | 16.32        | 3.141                  | 0.20( 0.04)         | 0.20 | 1.7           | 700.00            |

=====

END OF RATIONAL METHOD ANALYSIS



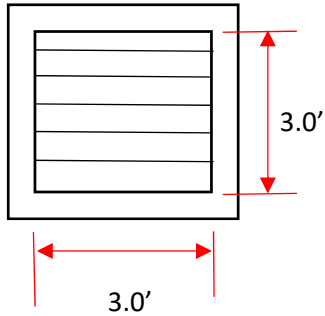
# **APPENDIX C**

## **HYDRAULIC CALCULATIONS**

# **100-Year Catch Basin Sizing**

**GRATE INLET CAPACITY CALCULATIONS**

CB #1 & 3 – Refer to Proposed Conditions Hydrology Map for Catch Basin locations.



~REFER TO THE URBAN DRAINAGE DESIGN MANUAL,  
UNITED STATES DEPARTMENT OF TRANSPORTATION

Ponding Depth,  $H = 0.25$  (3")

Perimeter,  $P = 12'$  (flows enter all sides)

$$Q/P = 3.0 H^{3/2}$$

$$Q = 3.0 H^{3/2} P$$

$$Q = 3.0(0.25)^{3/2}(12.0)$$

$$Q = 4.50 \text{ cfs}$$

$$50\% \text{ Clogging Factor} = 0.5(4.50) = \underline{2.25 \text{ cfs}}$$

$$\text{CB \#1} - Q_{25} = 0.83 \text{ cfs} < 2.25 \text{ cfs} \checkmark$$

$$\text{CB \#3} - Q_{25} = 1.33 \text{ cfs} < 2.25 \text{ cfs} \checkmark$$

# Inlet Report

## CB #3 Sizing Q100

### Curb Inlet

|                    |        |
|--------------------|--------|
| Location           | = Sag  |
| Curb Length (ft)   | = 7.00 |
| Throat Height (in) | = 6.00 |
| Grate Area (sqft)  | = -0-  |
| Grate Width (ft)   | = 3.00 |
| Grate Length (ft)  | = 3.00 |

### Gutter

|                   |         |
|-------------------|---------|
| Slope, Sw (ft/ft) | = 0.010 |
| Slope, Sx (ft/ft) | = 0.020 |
| Local Depr (in)   | = 2.00  |
| Gutter Width (ft) | = 1.50  |
| Gutter Slope (%)  | = -0-   |
| Gutter n-value    | = -0-   |

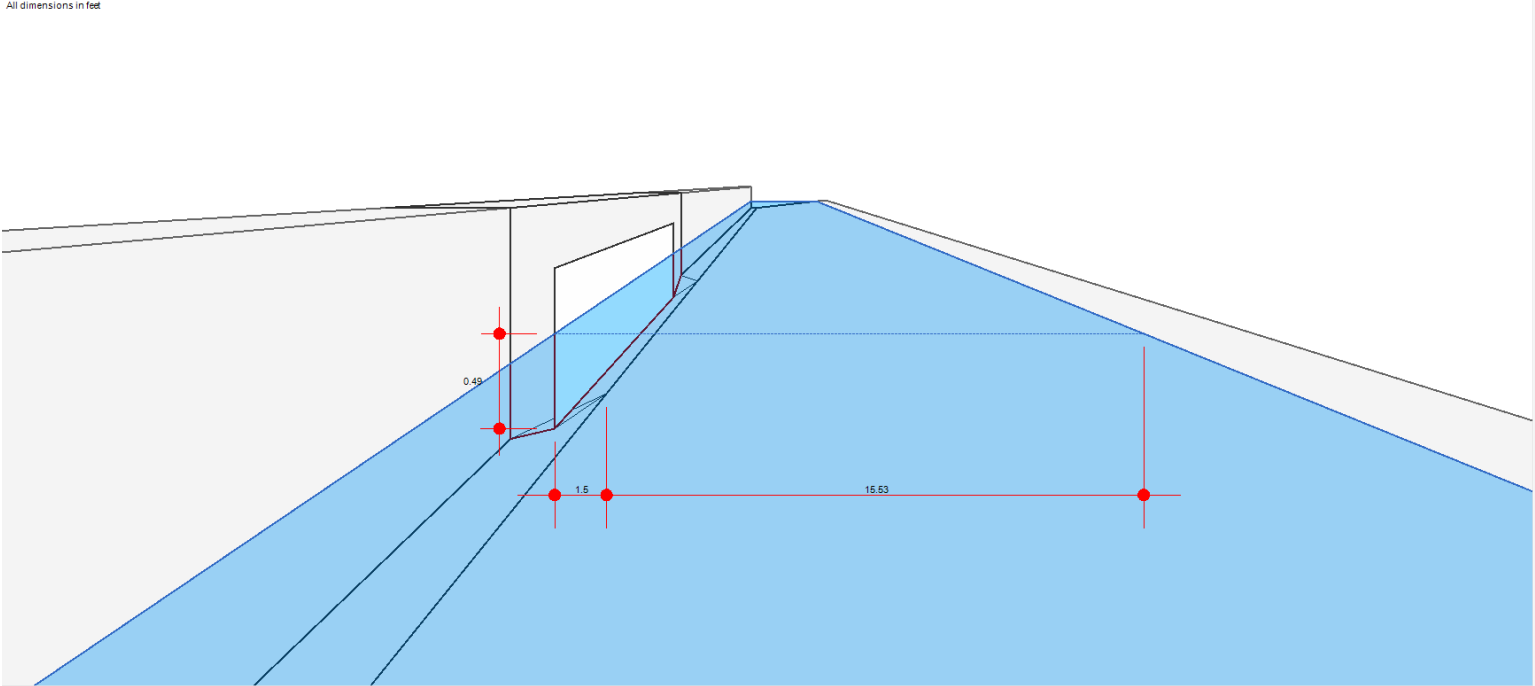
### Calculations

|             |         |
|-------------|---------|
| Compute by: | Known Q |
| Q (cfs)     | = 4.15  |

### Highlighted

|                     |         |
|---------------------|---------|
| Q Total (cfs)       | = 4.15  |
| Q Capt (cfs)        | = 4.15  |
| Q Bypass (cfs)      | = -0-   |
| Depth at Inlet (in) | = 5.91  |
| Efficiency (%)      | = 100   |
| Gutter Spread (ft)  | = 17.03 |
| Gutter Vel (ft/s)   | = -0-   |
| Bypass Spread (ft)  | = -0-   |
| Bypass Depth (in)   | = -0-   |

All dimensions in feet



# Inlet Report

## CB #4 Sizing Q100

### Curb Inlet

|                    |        |
|--------------------|--------|
| Location           | = Sag  |
| Curb Length (ft)   | = 7.00 |
| Throat Height (in) | = 6.00 |
| Grate Area (sqft)  | = -0-  |
| Grate Width (ft)   | = -0-  |
| Grate Length (ft)  | = -0-  |

### Gutter

|                   |         |
|-------------------|---------|
| Slope, Sw (ft/ft) | = 0.010 |
| Slope, Sx (ft/ft) | = 0.020 |
| Local Depr (in)   | = 2.00  |
| Gutter Width (ft) | = 1.50  |
| Gutter Slope (%)  | = -0-   |
| Gutter n-value    | = -0-   |

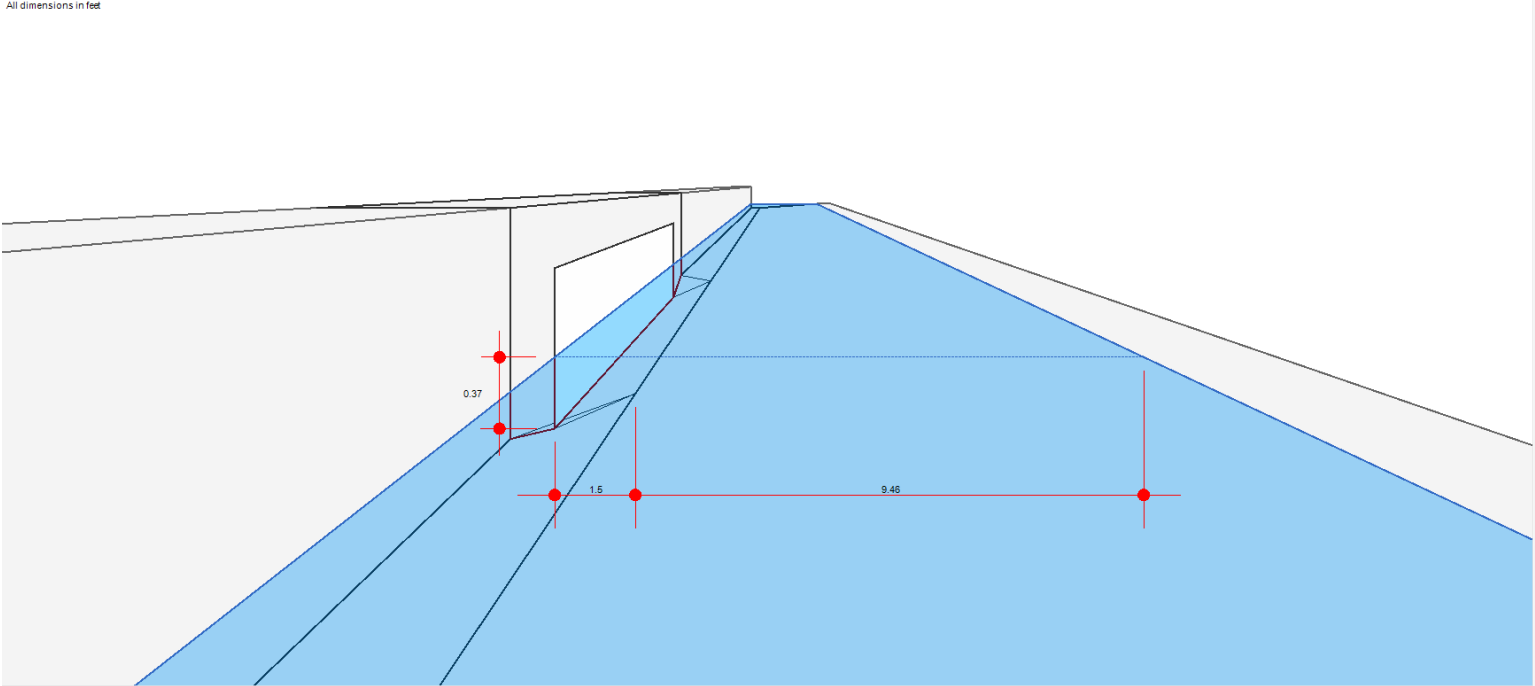
### Calculations

|             |         |
|-------------|---------|
| Compute by: | Known Q |
| Q (cfs)     | = 2.06  |

### Highlighted

|                     |         |
|---------------------|---------|
| Q Total (cfs)       | = 2.06  |
| Q Capt (cfs)        | = 2.06  |
| Q Bypass (cfs)      | = -0-   |
| Depth at Inlet (in) | = 4.45  |
| Efficiency (%)      | = 100   |
| Gutter Spread (ft)  | = 10.96 |
| Gutter Vel (ft/s)   | = -0-   |
| Bypass Spread (ft)  | = -0-   |
| Bypass Depth (in)   | = -0-   |

All dimensions in feet



# Inlet Report

## CB #5 Sizing Q100

### Curb Inlet

|                    |        |
|--------------------|--------|
| Location           | = Sag  |
| Curb Length (ft)   | = 7.00 |
| Throat Height (in) | = 6.00 |
| Grate Area (sqft)  | = -0-  |
| Grate Width (ft)   | = -0-  |
| Grate Length (ft)  | = -0-  |

### Gutter

|                   |         |
|-------------------|---------|
| Slope, Sw (ft/ft) | = 0.010 |
| Slope, Sx (ft/ft) | = 0.020 |
| Local Depr (in)   | = 2.00  |
| Gutter Width (ft) | = 1.50  |
| Gutter Slope (%)  | = -0-   |
| Gutter n-value    | = -0-   |

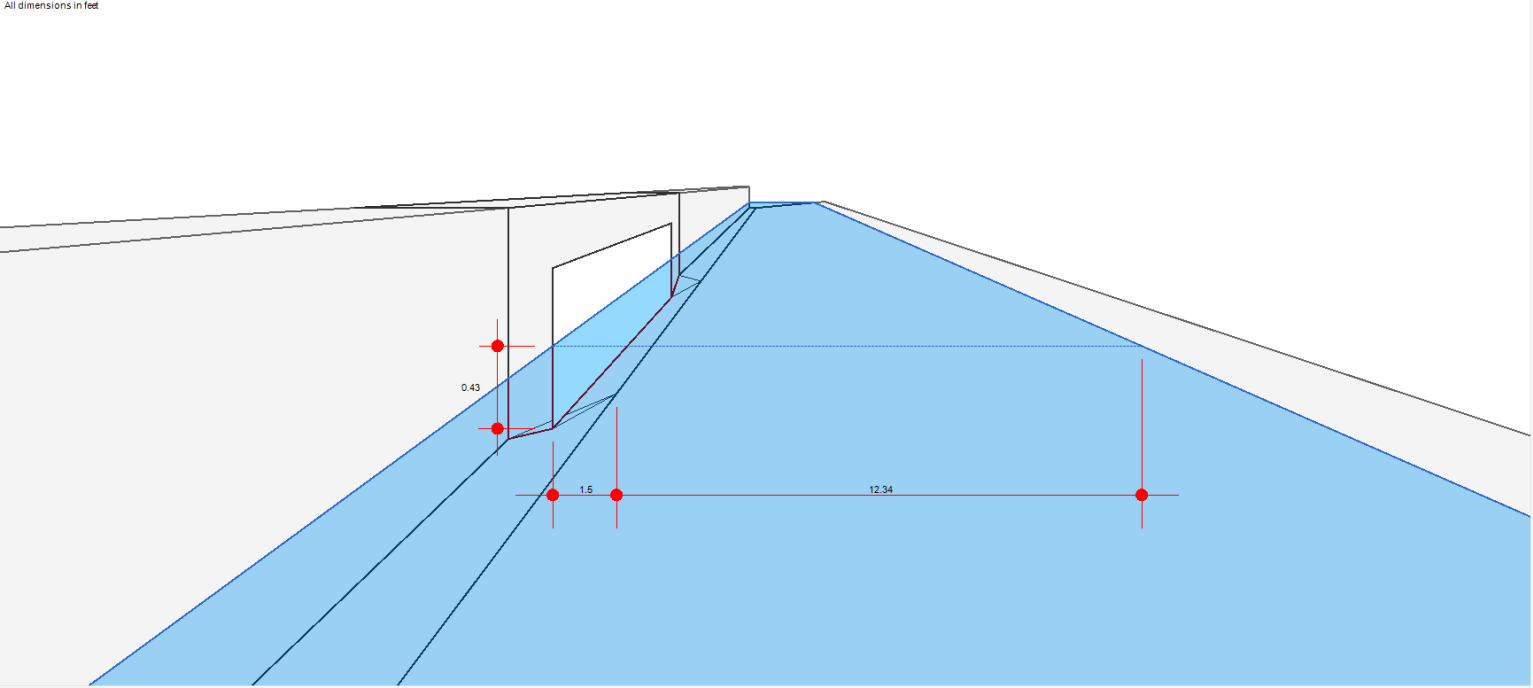
### Calculations

|             |         |
|-------------|---------|
| Compute by: | Known Q |
| Q (cfs)     | = 2.99  |

### Highlighted

|                     |         |
|---------------------|---------|
| Q Total (cfs)       | = 2.99  |
| Q Capt (cfs)        | = 2.99  |
| Q Bypass (cfs)      | = -0-   |
| Depth at Inlet (in) | = 5.14  |
| Efficiency (%)      | = 100   |
| Gutter Spread (ft)  | = 13.84 |
| Gutter Vel (ft/s)   | = -0-   |
| Bypass Spread (ft)  | = -0-   |
| Bypass Depth (in)   | = -0-   |

All dimensions in feet





# Inlet Report

## CB #6 Sizing Q100

### Curb Inlet

|                    |        |
|--------------------|--------|
| Location           | = Sag  |
| Curb Length (ft)   | = 7.00 |
| Throat Height (in) | = 6.00 |
| Grate Area (sqft)  | = -0-  |
| Grate Width (ft)   | = -0-  |
| Grate Length (ft)  | = -0-  |

### Gutter

|                   |         |
|-------------------|---------|
| Slope, Sw (ft/ft) | = 0.010 |
| Slope, Sx (ft/ft) | = 0.020 |
| Local Depr (in)   | = 2.00  |
| Gutter Width (ft) | = 1.50  |
| Gutter Slope (%)  | = -0-   |
| Gutter n-value    | = -0-   |

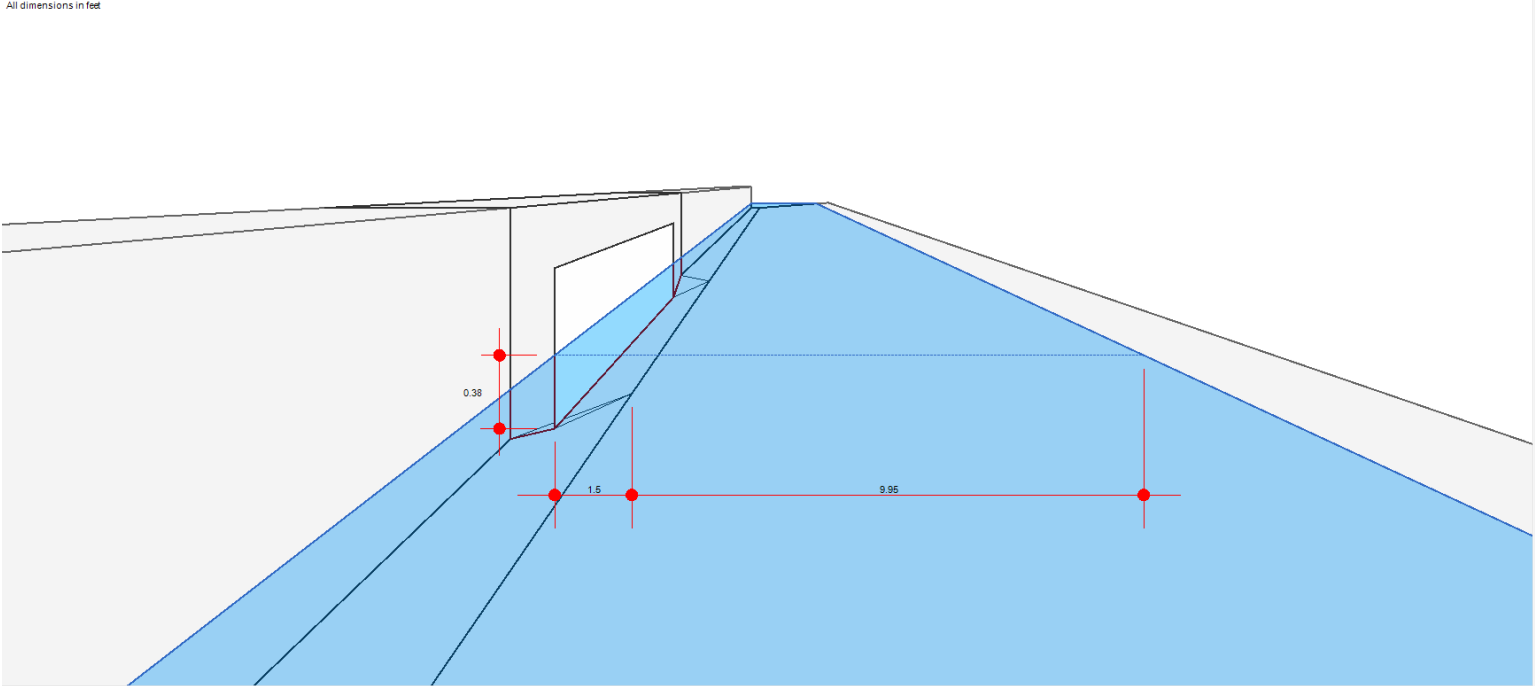
### Calculations

|             |         |
|-------------|---------|
| Compute by: | Known Q |
| Q (cfs)     | = 2.21  |

### Highlighted

|                     |         |
|---------------------|---------|
| Q Total (cfs)       | = 2.21  |
| Q Capt (cfs)        | = 2.21  |
| Q Bypass (cfs)      | = -0-   |
| Depth at Inlet (in) | = 4.57  |
| Efficiency (%)      | = 100   |
| Gutter Spread (ft)  | = 11.45 |
| Gutter Vel (ft/s)   | = -0-   |
| Bypass Spread (ft)  | = -0-   |
| Bypass Depth (in)   | = -0-   |

All dimensions in feet



# Inlet Report

## CB #7 Sizing Q100

### Curb Inlet

|                    |        |
|--------------------|--------|
| Location           | = Sag  |
| Curb Length (ft)   | = 7.00 |
| Throat Height (in) | = 6.00 |
| Grate Area (sqft)  | = -0-  |
| Grate Width (ft)   | = -0-  |
| Grate Length (ft)  | = -0-  |

### Gutter

|                   |         |
|-------------------|---------|
| Slope, Sw (ft/ft) | = 0.010 |
| Slope, Sx (ft/ft) | = 0.020 |
| Local Depr (in)   | = 2.00  |
| Gutter Width (ft) | = 1.50  |
| Gutter Slope (%)  | = -0-   |
| Gutter n-value    | = -0-   |

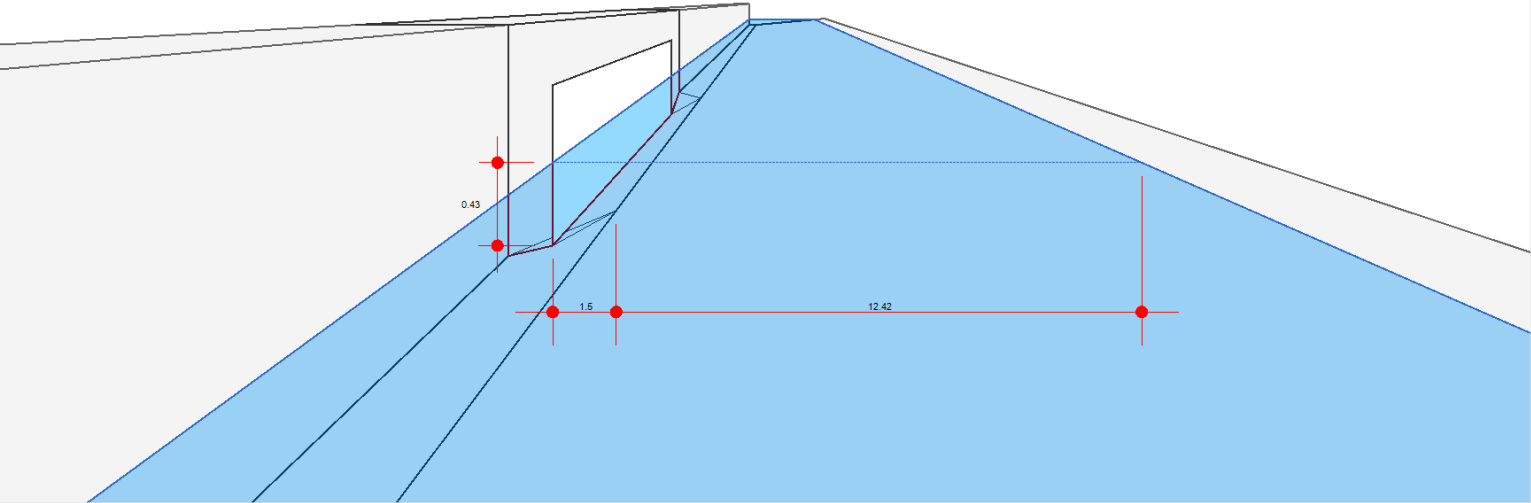
### Calculations

|             |         |
|-------------|---------|
| Compute by: | Known Q |
| Q (cfs)     | = 3.02  |

### Highlighted

|                     |         |
|---------------------|---------|
| Q Total (cfs)       | = 3.02  |
| Q Capt (cfs)        | = 3.02  |
| Q Bypass (cfs)      | = -0-   |
| Depth at Inlet (in) | = 5.16  |
| Efficiency (%)      | = 100   |
| Gutter Spread (ft)  | = 13.92 |
| Gutter Vel (ft/s)   | = -0-   |
| Bypass Spread (ft)  | = -0-   |
| Bypass Depth (in)   | = -0-   |

All dimensions in feet



# **Pipe Sizing**

*(To be provided during Final Engineering)*

# **Parkway Culvert Sizing**

# Channel Report

Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

Monday, May 17 2021

## Parkway Culvert #1\_Q100

### Rectangular

Bottom Width (ft) = 5.50

Total Depth (ft) = 0.33

Invert Elev (ft) = 100.00

Slope (%) = 2.00

N-Value = 0.013

### Calculations

Compute by: Known Q

Known Q (cfs) = 11.79

### Highlighted

Depth (ft) = 0.32

Q (cfs) = 11.79

Area (sqft) = 1.76

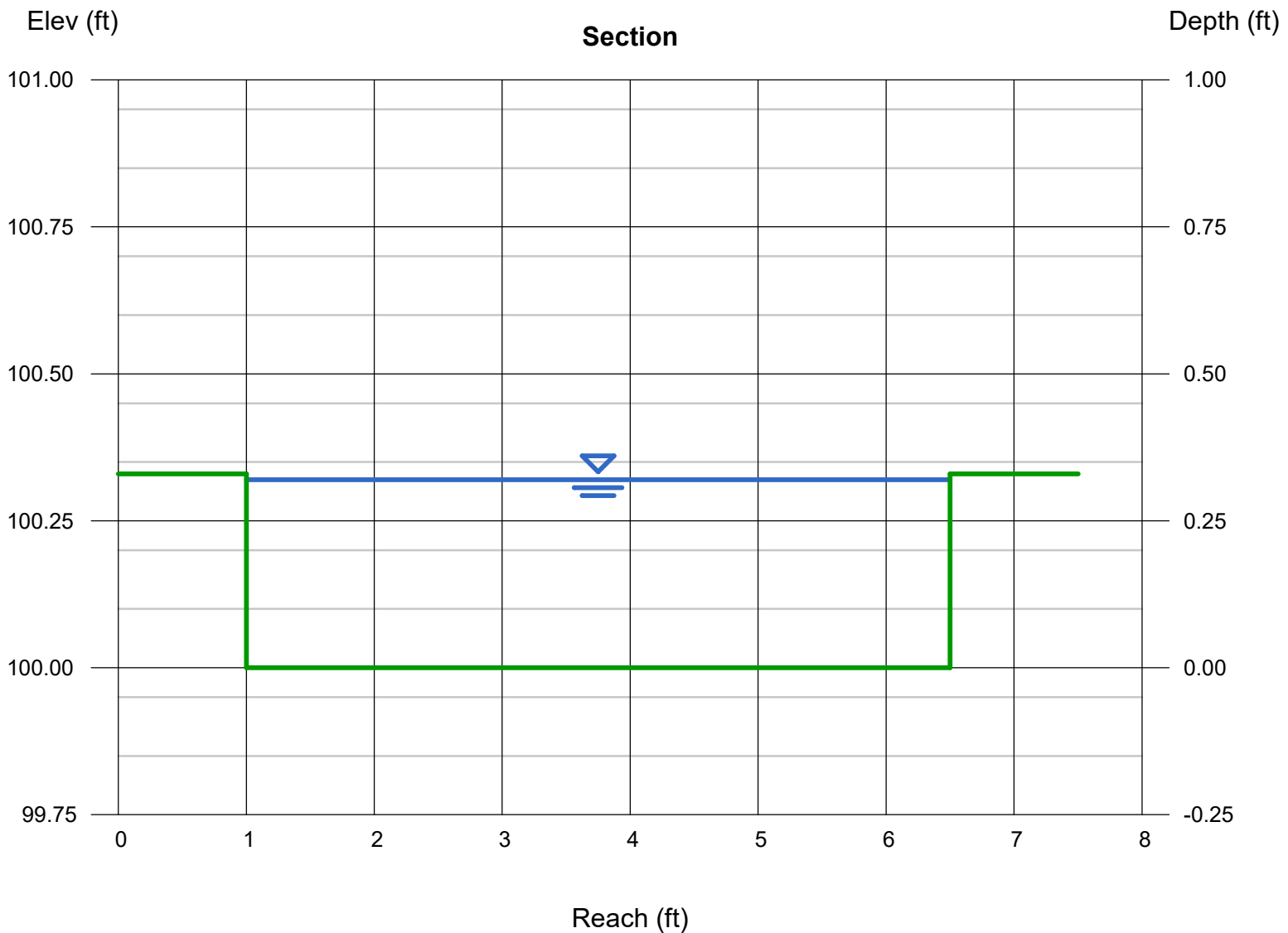
Velocity (ft/s) = 6.70

Wetted Perim (ft) = 6.14

Crit Depth, Yc (ft) = 0.33

Top Width (ft) = 5.50

EGL (ft) = 1.02



# Channel Report

## Parkway Culvert #2\_Q100

### Rectangular

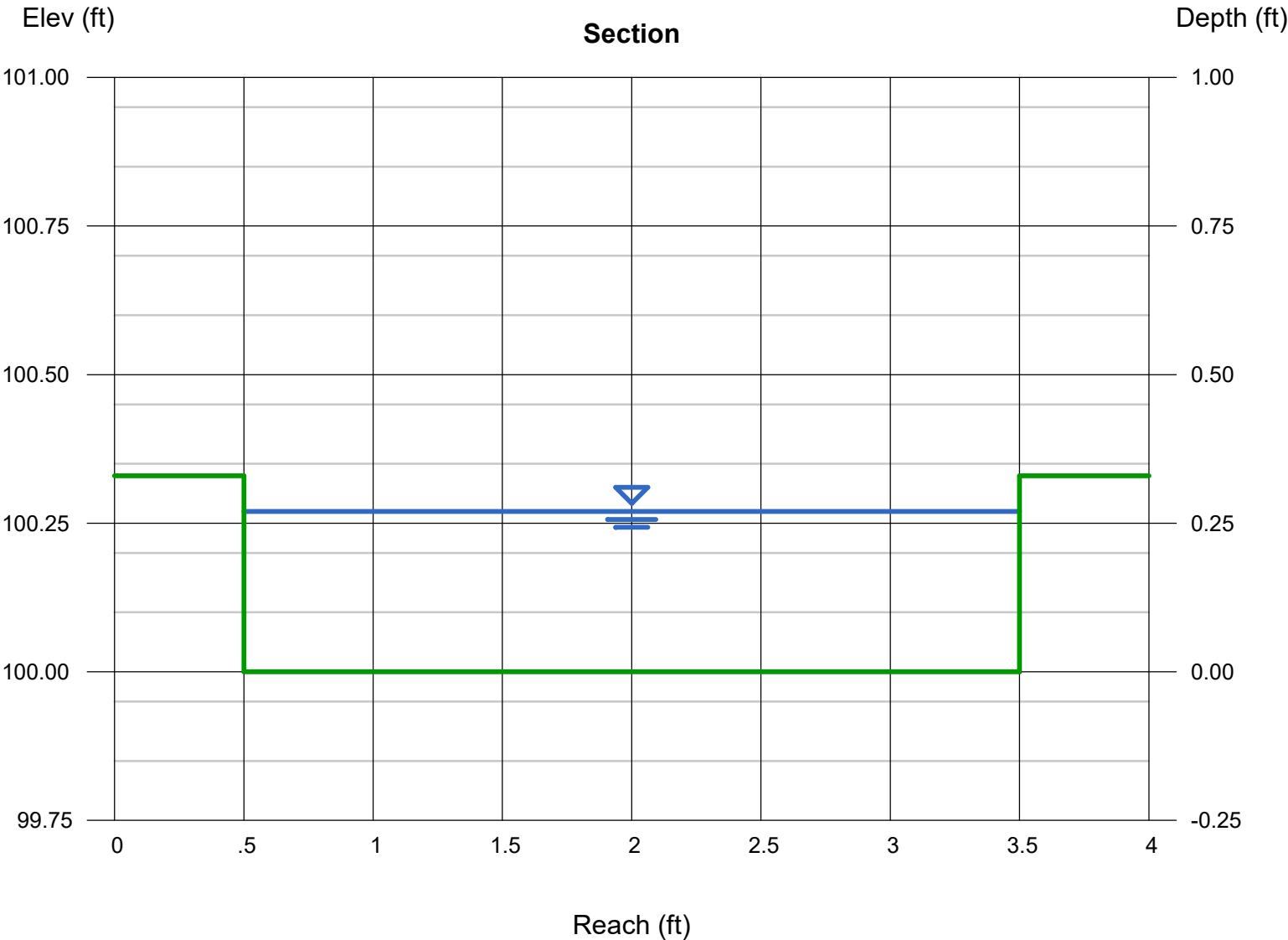
Bottom Width (ft) = 3.00  
Total Depth (ft) = 0.33  
  
Invert Elev (ft) = 100.00  
Slope (%) = 2.00  
N-Value = 0.013

### Calculations

Compute by: Known Q  
Known Q (cfs) = 4.88

### Highlighted

Depth (ft) = 0.27  
Q (cfs) = 4.880  
Area (sqft) = 0.81  
Velocity (ft/s) = 6.02  
Wetted Perim (ft) = 3.54  
Crit Depth, Yc (ft) = 0.33  
Top Width (ft) = 3.00  
EGL (ft) = 0.83



# Channel Report

Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

Monday, May 17 2021

## Parkway Culvert #3\_Q100

### Rectangular

Bottom Width (ft) = 2.00

Total Depth (ft) = 0.33

Invert Elev (ft) = 100.00

Slope (%) = 2.00

N-Value = 0.013

### Calculations

Compute by: Known Q

Known Q (cfs) = 2.21

### Highlighted

Depth (ft) = 0.22

Q (cfs) = 2.210

Area (sqft) = 0.44

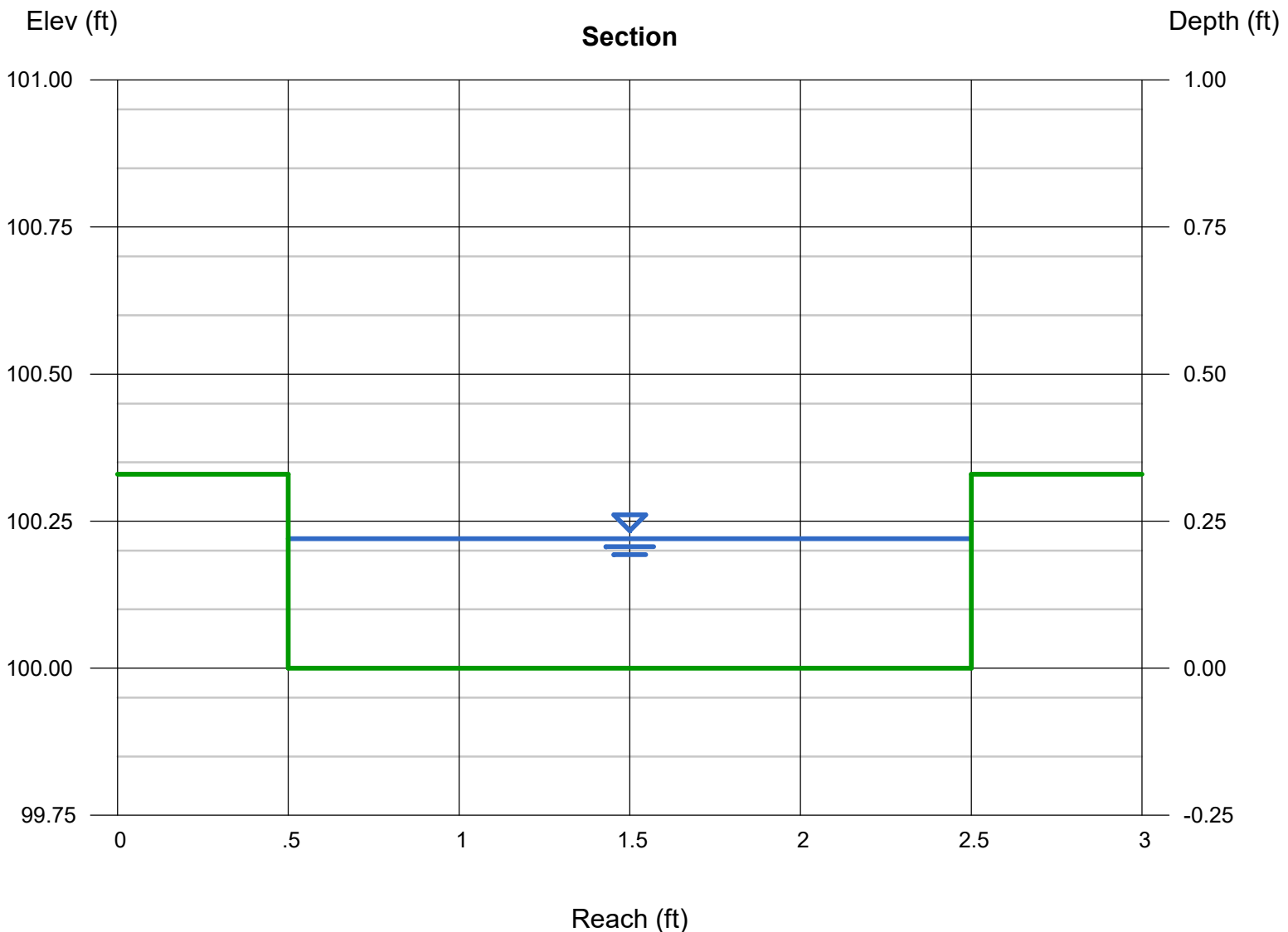
Velocity (ft/s) = 5.02

Wetted Perim (ft) = 2.44

Crit Depth, Yc (ft) = 0.33

Top Width (ft) = 2.00

EGL (ft) = 0.61



# Channel Report

Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

Monday, May 17 2021

## Parkway Culvert #4\_Q100

### Rectangular

Bottom Width (ft) = 2.50

Total Depth (ft) = 0.33

Invert Elev (ft) = 100.00

Slope (%) = 2.00

N-Value = 0.013

### Calculations

Compute by: Known Q

Known Q (cfs) = 3.74

### Highlighted

Depth (ft) = 0.26

Q (cfs) = 3.740

Area (sqft) = 0.65

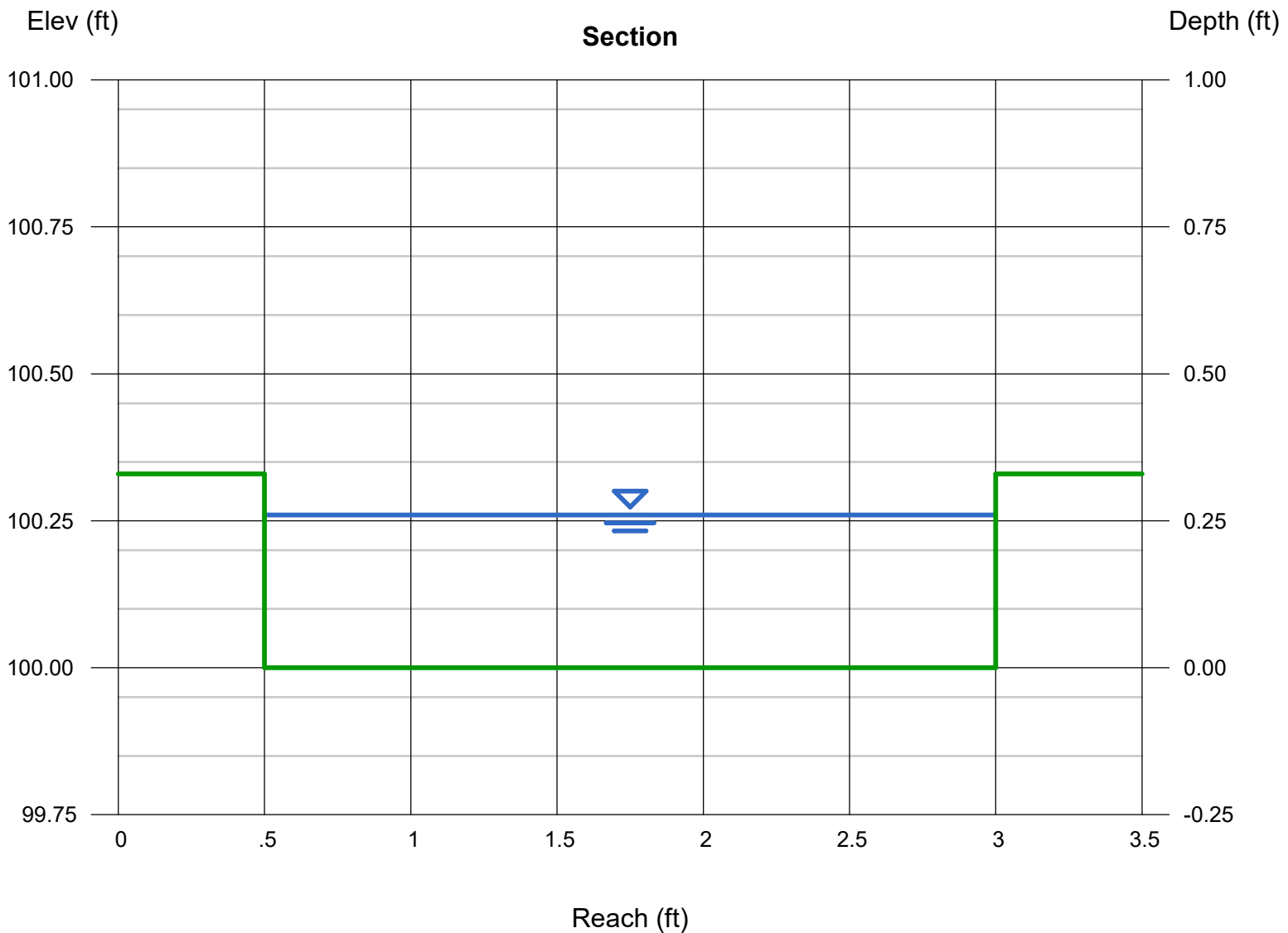
Velocity (ft/s) = 5.75

Wetted Perim (ft) = 3.02

Crit Depth, Yc (ft) = 0.33

Top Width (ft) = 2.50

EGL (ft) = 0.77





# Wall Knockout Sizing

# Weir Report

## Wall Knockout

### Rectangular Weir

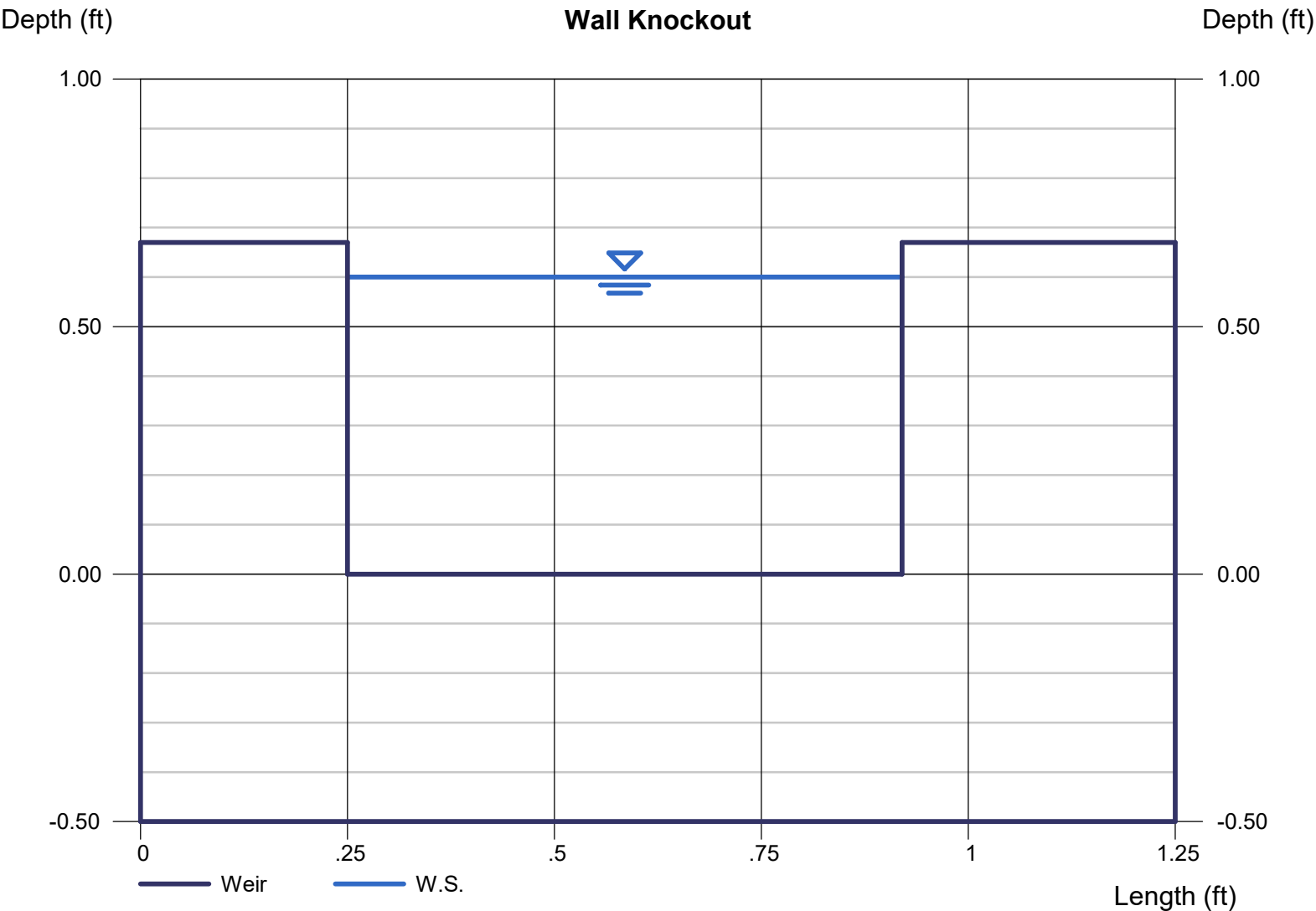
Crest = Sharp  
Bottom Length (ft) = 0.67  
Total Depth (ft) = 0.67

### Calculations

Weir Coeff. Cw = 3.33  
Compute by: Known Depth  
Known Depth (ft) = 0.60

### Highlighted

Depth (ft) = 0.60  
Q (cfs) = 1.037  
Area (sqft) = 0.40  
Velocity (ft/s) = 2.58  
Top Width (ft) = 0.67



# **100-Year Water Surface Ponding Calculations**

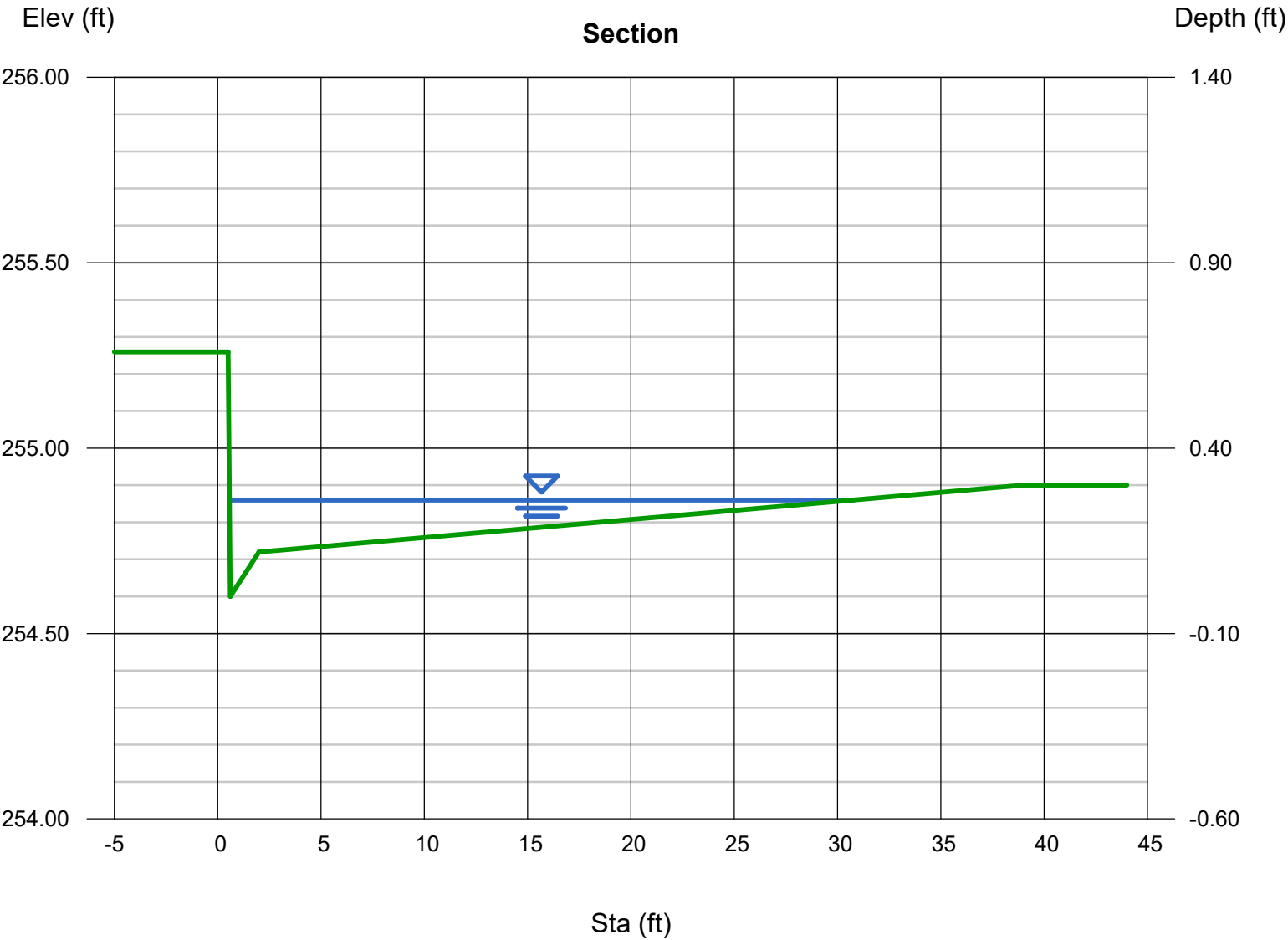
# Channel Report

## Q100\_CB # 3 Depth of Flow

| User-defined     |          | Highlighted         |         |
|------------------|----------|---------------------|---------|
| Invert Elev (ft) | = 254.60 | Depth (ft)          | = 0.26  |
| Slope (%)        | = 0.80   | Q (cfs)             | = 4.150 |
| N-Value          | = 0.013  | Area (sqft)         | = 2.30  |
|                  |          | Velocity (ft/s)     | = 1.81  |
|                  |          | Wetted Perim (ft)   | = 30.44 |
|                  |          | Crit Depth, Yc (ft) | = 0.27  |
|                  |          | Top Width (ft)      | = 30.21 |
|                  |          | EGL (ft)            | = 0.31  |

**Calculations**  
Compute by: Known Q  
Known Q (cfs) = 4.15

**(Sta, El, n)-(Sta, El, n)...**  
( 0.00, 255.26)-(0.50, 255.26, 0.013)-(0.61, 254.60, 0.013)-(2.00, 254.72, 0.013)-(39.00, 254.90, 0.013)



# Channel Report

Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

Monday, Mar 1 2021

## Q100\_CB # 4 Depth of Flow

### User-defined

Invert Elev (ft) = 256.05  
Slope (%) = 0.80  
N-Value = 0.013

### Calculations

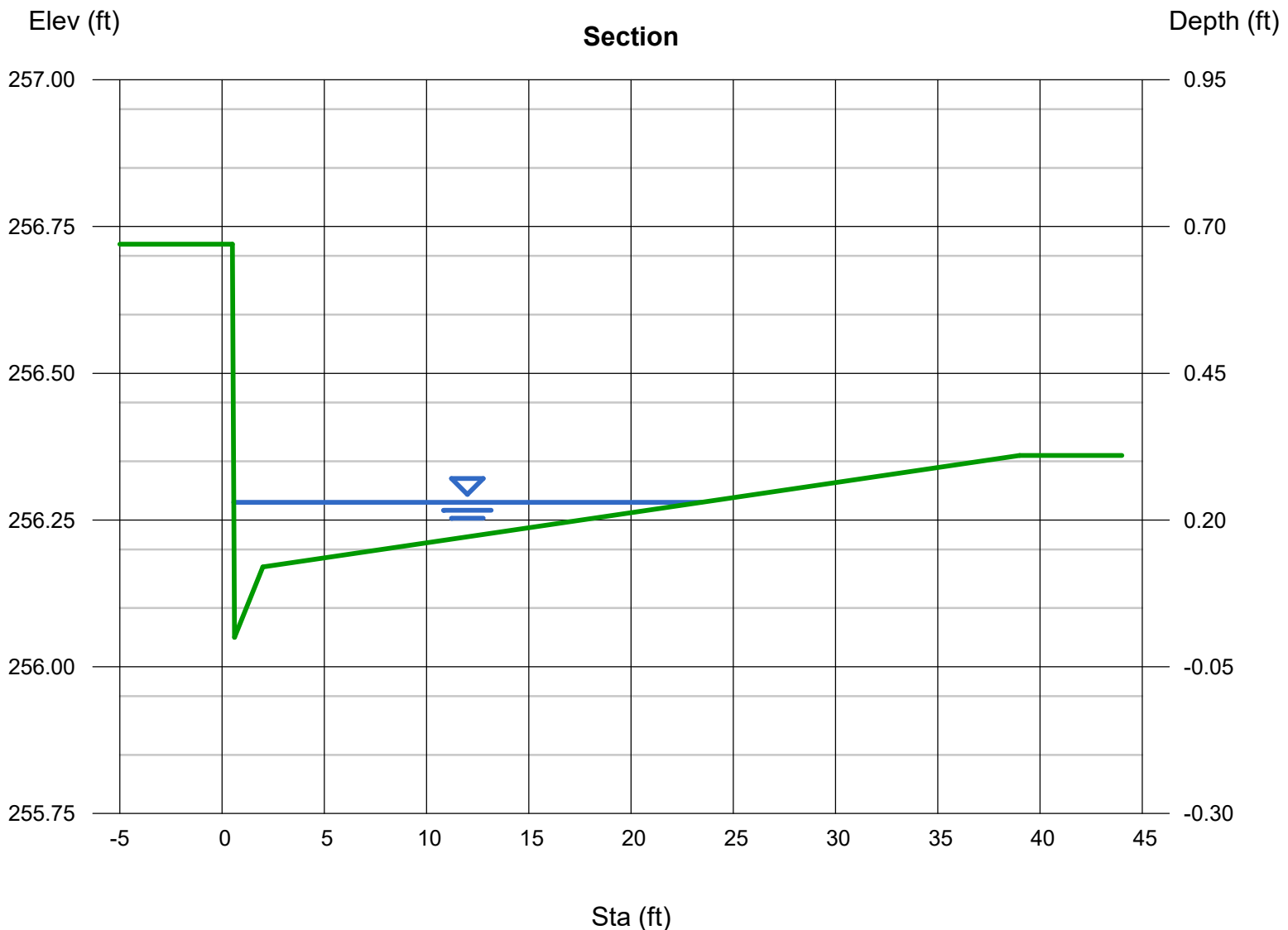
Compute by: Known Q  
Known Q (cfs) = 2.06

### Highlighted

Depth (ft) = 0.23  
Q (cfs) = 2.060  
Area (sqft) = 1.42  
Velocity (ft/s) = 1.45  
Wetted Perim (ft) = 23.05  
Crit Depth, Yc (ft) = 0.24  
Top Width (ft) = 22.85  
EGL (ft) = 0.26

(Sta, El, n)-(Sta, El, n)...

(0.00, 256.72)-(0.50, 256.72, 0.013)-(0.61, 256.05, 0.013)-(2.00, 256.17, 0.013)-(39.00, 256.36, 0.013)



# Channel Report

Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

Tuesday, Mar 9 2021

## Q100\_CB #5 Depth of Flow

### User-defined

Invert Elev (ft) = 257.59  
Slope (%) = 0.80  
N-Value = 0.013

### Calculations

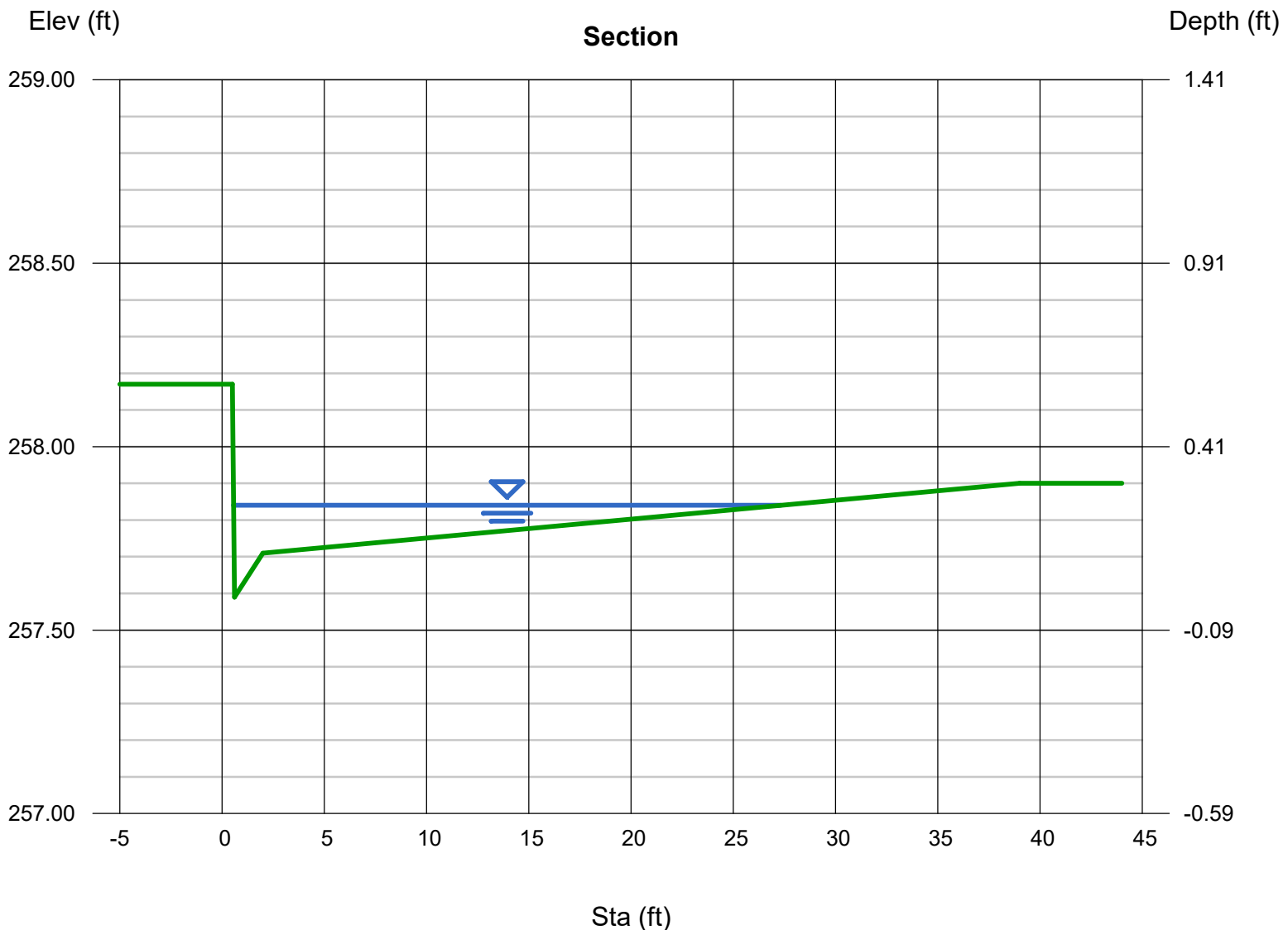
Compute by: Known Q  
Known Q (cfs) = 2.99

### Highlighted

Depth (ft) = 0.25  
Q (cfs) = 2.990  
Area (sqft) = 1.92  
Velocity (ft/s) = 1.56  
Wetted Perim (ft) = 26.97  
Crit Depth, Yc (ft) = 0.26  
Top Width (ft) = 26.75  
EGL (ft) = 0.29

### (Sta, El, n)-(Sta, El, n)...

(0.00, 258.17)-(0.50, 258.17, 0.013)-(0.61, 257.59, 0.013)-(2.00, 257.71, 0.013)-(39.00, 257.90, 0.013)



# Channel Report

Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

Monday, Mar 1 2021

## CB #6 Depth of Flow

### User-defined

Invert Elev (ft) = 255.71  
Slope (%) = 0.80  
N-Value = 0.013

### Calculations

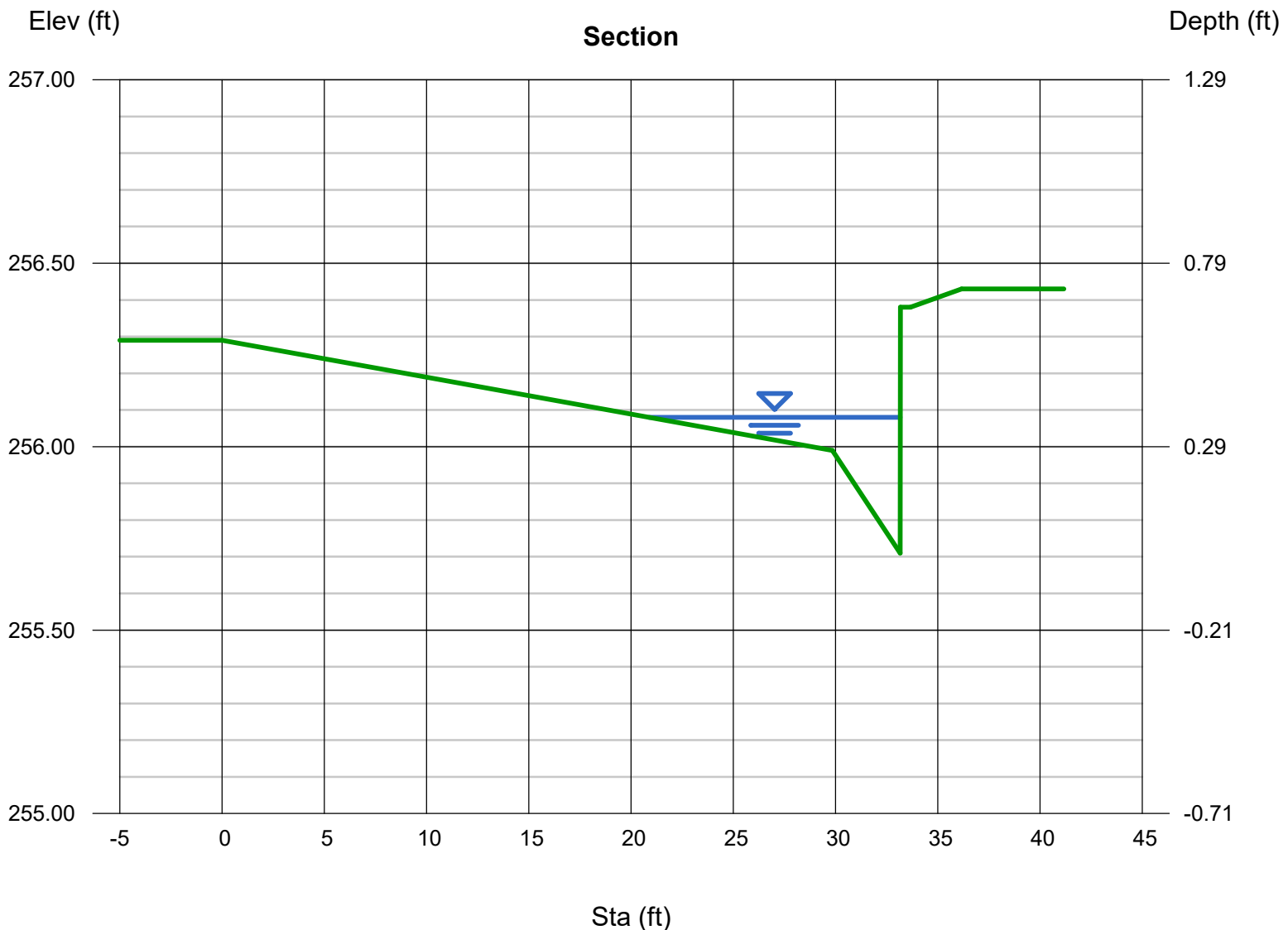
Compute by: Known Q  
Known Q (cfs) = 2.21

### Highlighted

Depth (ft) = 0.37  
Q (cfs) = 2.210  
Area (sqft) = 1.17  
Velocity (ft/s) = 1.89  
Wetted Perim (ft) = 12.66  
Crit Depth, Yc (ft) = 0.38  
Top Width (ft) = 12.28  
EGL (ft) = 0.43

### (Sta, El, n)-(Sta, El, n)...

(0.00, 256.29)-(29.84, 255.99, 0.013)-(33.16, 255.71, 0.013)-(33.17, 256.38, 0.013)-(33.67, 256.38, 0.013)-(36.17, 256.43, 0.013)



# Channel Report

Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

Tuesday, Mar 9 2021

## Q100\_CB #7 Depth of Flow

### User-defined

Invert Elev (ft) = 259.67  
Slope (%) = 0.80  
N-Value = 0.013

### Calculations

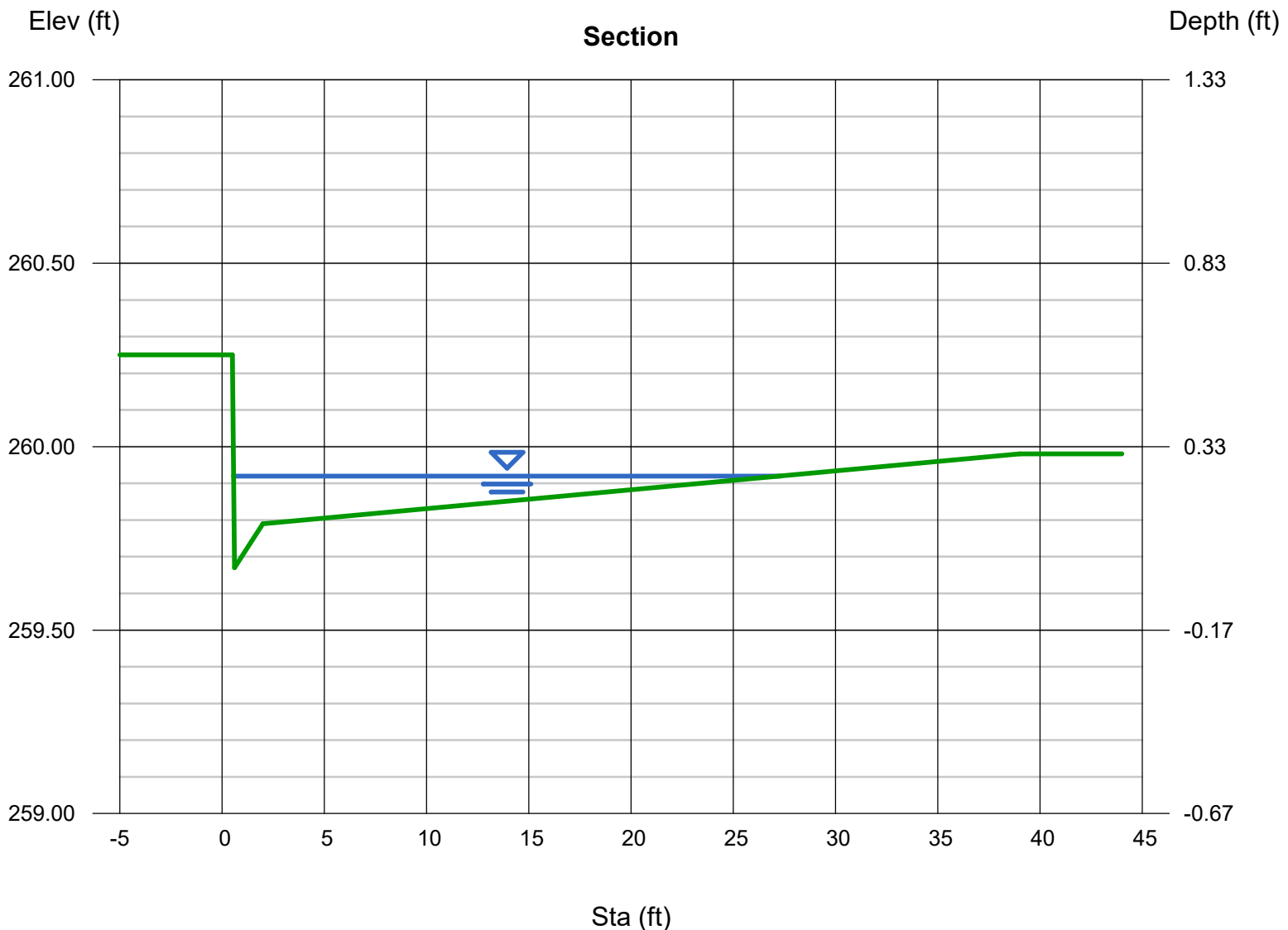
Compute by: Known Q  
Known Q (cfs) = 3.02

### Highlighted

Depth (ft) = 0.25  
Q (cfs) = 3.020  
Area (sqft) = 1.92  
Velocity (ft/s) = 1.58  
Wetted Perim (ft) = 26.97  
Crit Depth, Yc (ft) = 0.26  
Top Width (ft) = 26.75  
EGL (ft) = 0.29

(Sta, El, n)-(Sta, El, n)...

(0.00, 260.25)-(0.50, 260.25, 0.013)-(0.61, 259.67, 0.013)-(2.00, 259.79, 0.013)-(39.00, 259.98, 0.013)





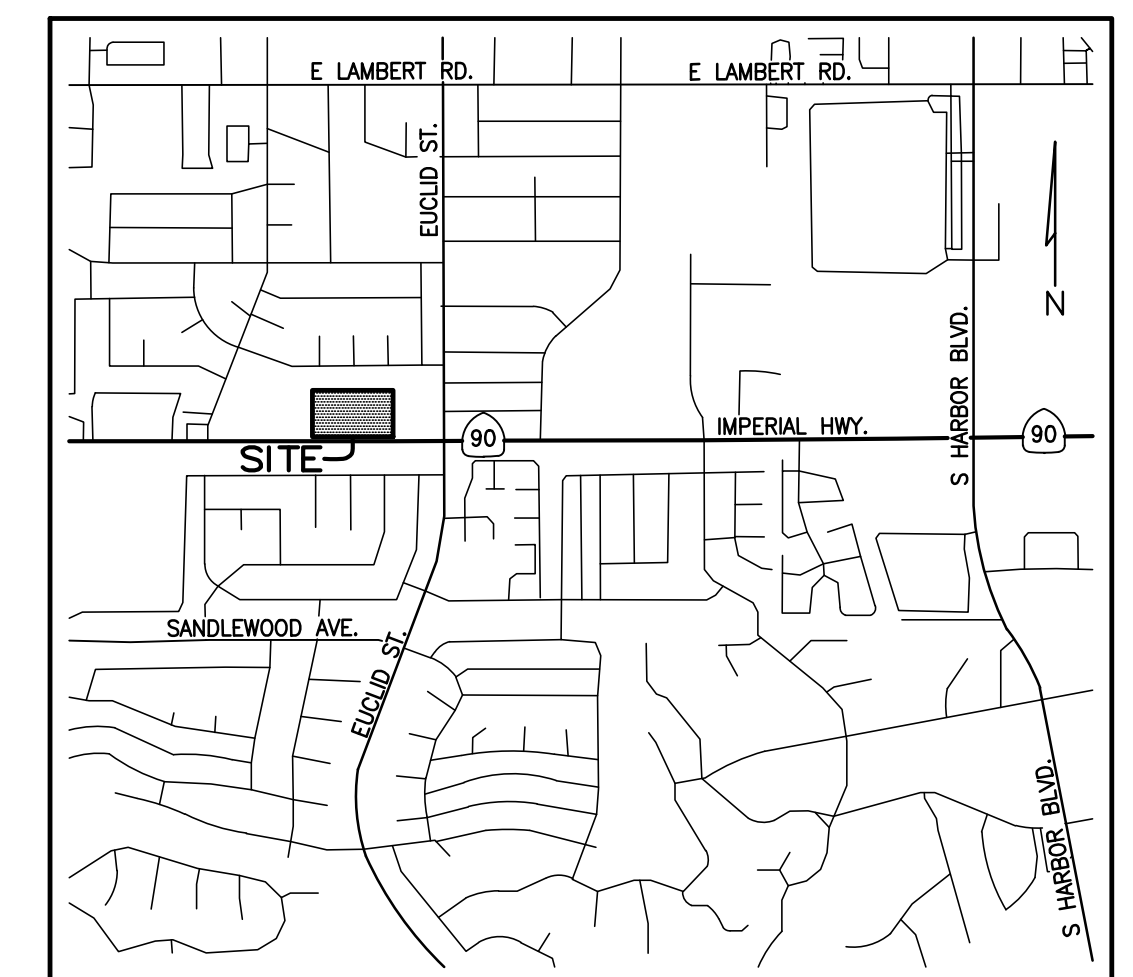
**Site Plan Details:**

- Buildings:** BLDG. 1 through BLDG. 21. Each building is labeled with its footprint (FF) and area (AC). For example, BLDG. 1 has FF=260.83 and BLDG. 21 has FF=260.33.
- Drainage Management Areas (DMA):** P1 through P12. Each DMA is labeled with its area (AC). For example, P1 has 0.05 AC and P12 has 0.68 AC.
- Storm Drains:** Labeled with elevations and flow directions. For example, Q100 ELEVATION 256.08 and Q100 ELEVATION 259.92.
- Catch Basins:** Labeled with elevations and flow directions. For example, PROP. CB #3 with 255.26 TC and 254.60 FL.
- Other Features:** EX. SD CATCH BASIN, EX. 24" SD, IMPERIAL HIGHWAY, SADDLEWOOD AVE, EX. COMMERCIAL, EX. P/L, PROP. DRAINAGE SWALE, PROP. RET. WALL.

**VICINITY MAP**  
NTS



**LEGEND**

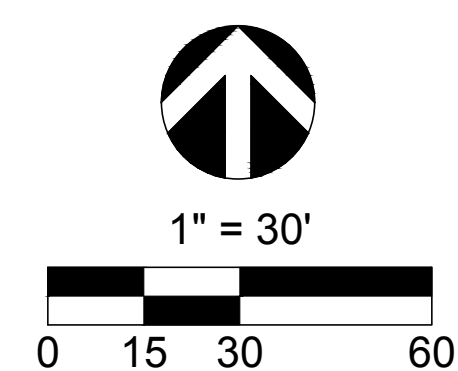
- EXISTING RIGHT-OF-WAY/ BOUNDARY
- DRAINAGE MANAGEMENT AREA (DMA)
- EXISTING STORM DRAIN
- PROPOSED STORM DRAIN
- DRAINAGE FLOW ARROWS
- PROPOSED MWS BIOFILTRATION VAULT
- PROPOSED CATCH BASIN
- DRAINAGE MANAGEMENT AREA (DMA)
- ACREAGE



VICINITY MAP  
NTS

**LEGEND**

- 
- --- --- --- ---  
 EXISTING RIGHT-OF-WAY/ BOUNDARY  
 ■ ■ ■ ■ ■  
 DRAINAGE MANAGEMENT AREA (DMA)  
 ===  
 EXISTING STORM DRAIN  
 ===  
 PROPOSED STORM DRAIN  
 →  
 DRAINAGE FLOW ARROWS  
  
 PROPOSED MWS BIOFILTRATION VAULT  
  
 PROPOSED CATCH BASIN



PREPARED BY :



**CONSULTING, INC.**  
CIVIL ENGINEERING  
LAND PLANNING & SURVEYING

(949) 916-3800  
INFO@CVC-INC.NET  
WWW.CVC-INC.NET



|  |   |
|--|---|
| TENTATIVE TRACT NO. 19143<br>PONDING EXHIBIT | D |
|--|---|

DATE: 5/17/2021

SHEET 1 OF 1

SCALE: AS SHOWN

DRAWN BY: SP

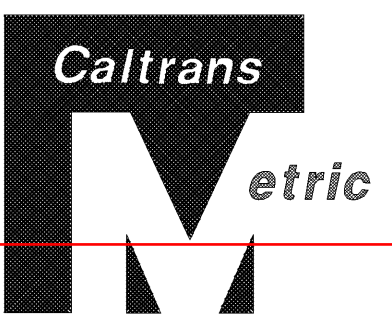
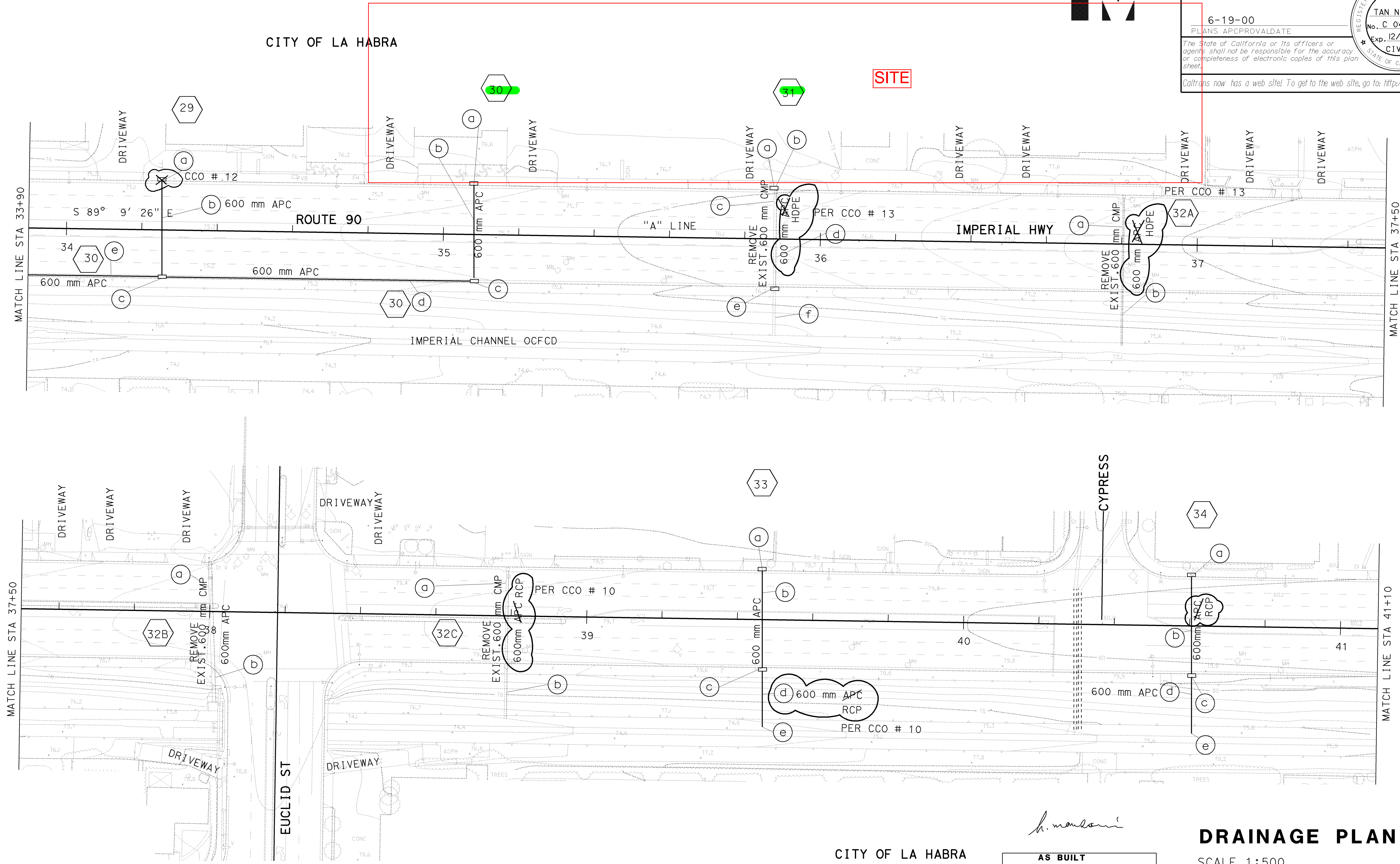
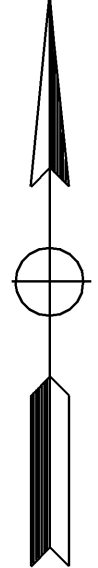
CHECKED BY: JH

CITY OF LA HABRA

# **APPENDIX D**

## **REFERENCE MATERIALS**





|      |        |       |                              |          |              |
|------|--------|-------|------------------------------|----------|--------------|
| DIST | COUNTY | ROUTE | KILOMETER POST TOTAL PROJECT | SHEET No | TOTAL SHEETS |
| 12   | Ora    | 90    | 0.8/4.1, 8.1/13.0            | 25       | 134          |

12/15/99

REGISTERED CIVIL ENGINEER

6-19-00

PLANS APPROVAL DATE

THE STATE OF CALIFORNIA OR ITS OFFICERS OR AGENTS SHALL NOT BE RESPONSIBLE FOR THE ACCURACY OR COMPLETENESS OF ELECTRONIC COPIES OF THIS PLAN SHEET.

Caltrans now has a web site! To get to the web site, go to: <http://www.dot.ca.gov>

REGISTERED PROFESSIONAL ENGINEER

TAN NGUYEN

No. C 047660

Exp. 12/31/99

CIVIL

STATE OF CALIFORNIA

AS BUILT

CONTRACT NUMBER 12-0296A4

CORRECTIONS BY MIKE GROTKE

COMPLETION DATE FEB. 14, 2003

DRAINAGE PLAN

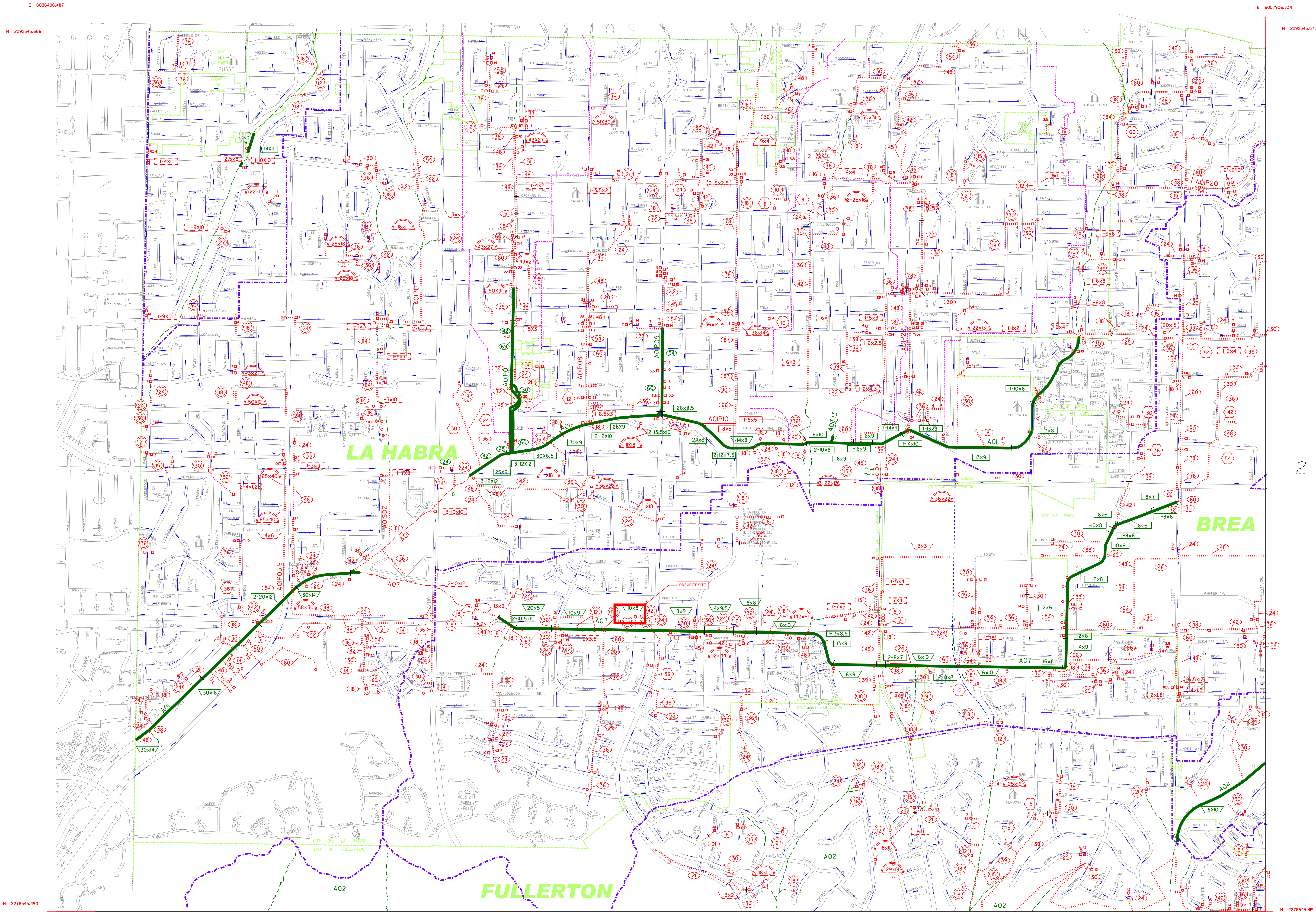
SCALE 1:500

D-4









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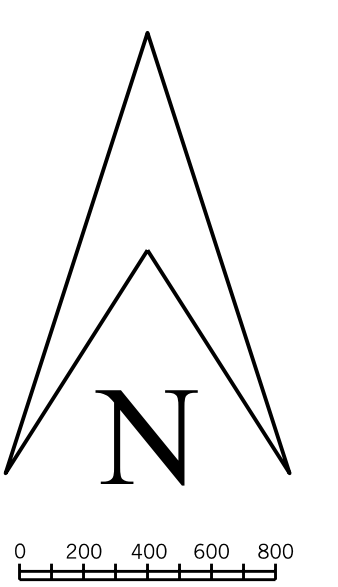
ORANGE COUNTY FLOOD CONTROL DISTRICT

#### BASE MAP OF DRAINAGE FACILITIES IN ORANGE COUNTY

REVISION: S. GUTIERREZ DATE: JAN 3, 2021 SHEET NO: 1 DRAWING NO: MAPS-113-3

|   |                                       | EXISTING FACILITIES |   |
|---|---------------------------------------|---------------------|---|
|   |                                       | O.C.F.C.D.          | LOCAL   |
|   | Channel Drainage Area Boundary        |                     | Earth Trapezoidal Channel (base width by height in feet)                              |
|   | Major Sub-Area Drainage Boundary      |                     | Reinforced Concrete Trapezoidal Channel (base width by height in feet)                |
|   | Minor Sub-Area Drainage Boundary      |                     | Reinforced Concrete Rectangular Channel (base width by height in feet)                |
|   | Existing O.C.F.C.D. Facility          |                     | Reinforced Concrete Box (RCB) (number of barrels-span by height in feet)              |
|   | Existing Local Facility               |                     | Reinforced Concrete Pipe (RCP) (diameter in inches)                                   |
|   | Existing Retarding Basin or Reservoir |                     | Metal Sheet Channel (MSC) (Base width by pile height in feet/Sheet pile total length) |
|   | Natural Watercourse                   |                     | Corrugated Metal Pipe (CMP) (diameter in inches)                                      |
|   | City Limits                           |                     | Concrete Pipe (diameter in inches)  |
|   | Greenbelt                             |                     | Concrete Oval Pipe (width by height in inches)  |
|   | Pump Station                          |                     | Steel Pipe (diameter in inches)   |
|   | Catch Basin (length in feet)          |                     | Reinforced Concrete Arch (base span by height in inches)                              |
|   | Drop Inlet or Other Entry             |                     | Corrugated Metal Arch (base span by height in inches)                                 |
|   | OCFCD Basins or Reservoirs            |                     |   |
| Ownership: (If other than City or County): Private = <b>P</b> State = <b>S</b> Federal = <b>F</b> |                                       |                     |   |





O.C.F.C.D. maintains Coyote Creek (AO1) from North Fork to the beginning of O.C.F.C.D. R/W 5200' south of the center line of Imperial Hwy per Agreement No. B02 (566-U) with L.A.C.F.C.D.

Coyote Creek from the ocean to North Fork is owned and maintained by L.A.C.F.C.D.


























NOTICE

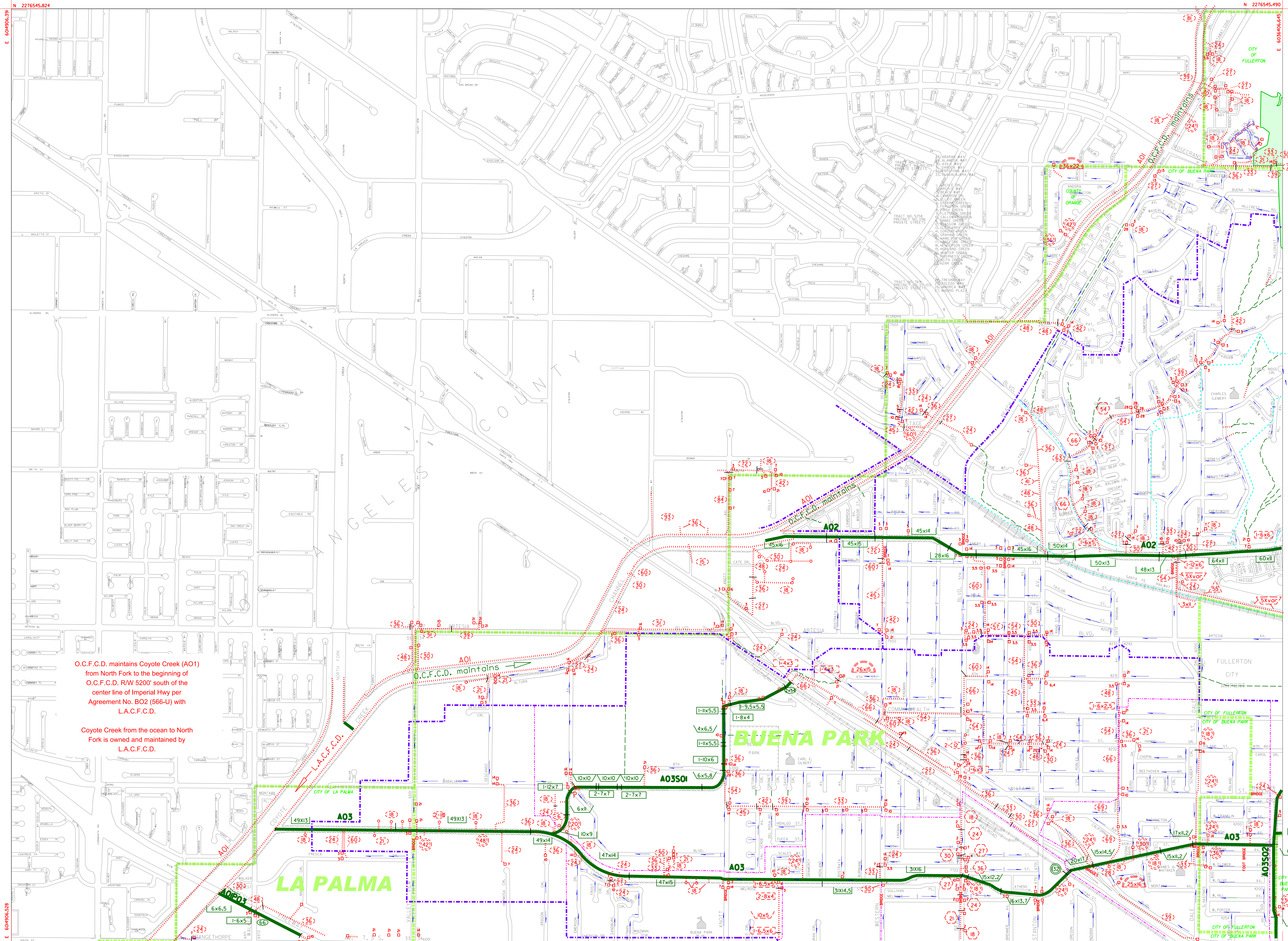
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| ORANGE COUNTY FLOOD CONTROL DISTRICT             |              |           |            |
|--|--------------|-----------|------------|
| BASE MAP OF DRAINAGE FACILITIES IN ORANGE COUNTY |              |           |            |
| REVISION   | DATE         | SHEET NO. | DWG. NO.   |
| S. GUTIERREZ                                     | MAR. 12, 200 | 5         | MAPS-113-5 |

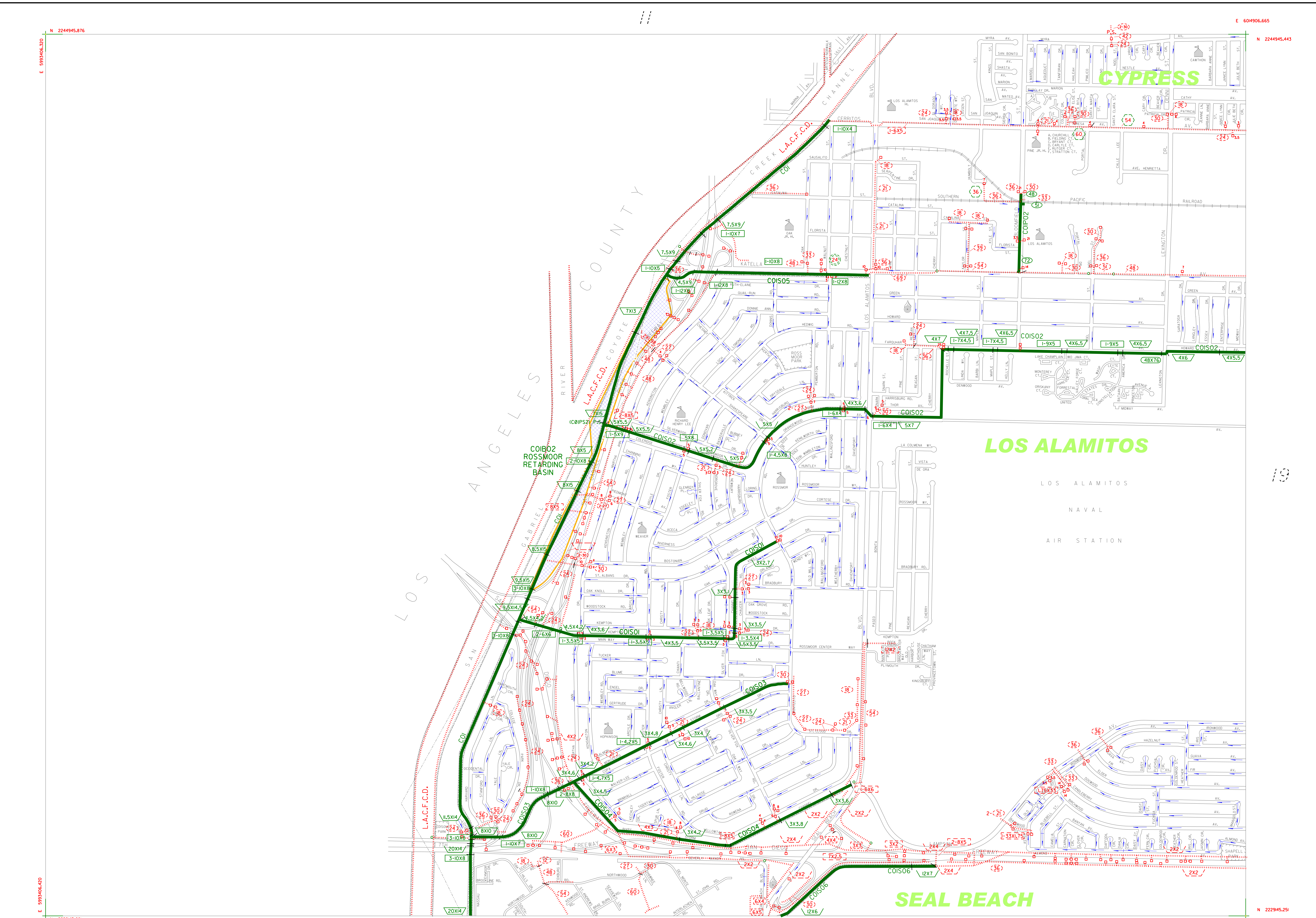
|   |                                       | EXISTING FACILITIES   |   |   |
|---|---------------------------------------|---|---|---|
|   |                                       | O.C.F.C.D.  | LOCAL   |   |
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|  | City Limits                           |   |   | Concrete Pipe (diameter in inches)  |
|  | Greenbelt                             |   |   | Concrete Oval Pipe (width by height in inches)  |
|  | Pump Station                          |   |   | Steel Pipe (diameter in inches)   |
|  | Catch Basin (length in feet)          |   |   | Reinforced Concrete Arch (base span by height in inches)                              |
|  | Drop Inlet or Other Entry             |   |   | Corrugated Metal Arch (base span by height in inches)                                 |
|  | OCFCD Basins or Reservoirs            |   |   |   |
| Ownership (If other than City or County): Private = P State = S Federal = F           |                                       |   |   |   |



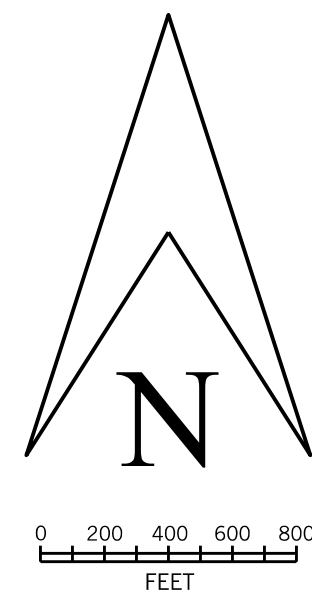








18



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#### BASE MAP OF DRAINAGE FACILITIES IN ORANGE COUNTY

| REVISION     | DATE       | SHEET NO. | DWG. NO.   |
|--------------|------------|-----------|------------|
| S. GUTIERREZ | JUN 9 2008 | 18        | MAPS-113-3 |

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- Major Sub-Area Drainage Boundary
- Minor Sub-Area Drainage Boundary
- Existing O.C.F.C.D. Facility
- Existing Local Facility
- Existing Retarding Basin or Reservoir
- Natural Watercourse
- City Limits
- Greenbelt
- Pump Station
- Catch Basin (length in feet)
- Drop Inlet or Other Entry
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