

Perris Truck Yard Noise Impact Analysis City of Perris

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12915-04 Noise Study



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LIST OF ABBREVIATED TERMS

(1) Reference

ADT Average Daily Traffic

ANSI American National Standards Institute

Calveno California Vehicle Noise

CEQA California Environmental Quality Act
CNEL Community Noise Equivalent Level

dBA A-weighted decibels

EPA Environmental Protection Agency
FHWA Federal Highway Administration
FTA Federal Transit Administration

INCE Institute of Noise Control Engineering

 $\begin{array}{lll} L_{eq} & & & \text{Equivalent continuous (average) sound level} \\ L_{max} & & \text{Maximum level measured over the time interval} \\ L_{min} & & \text{Minimum level measured over the time interval} \end{array}$

mph Miles per hour

OPR Office of Planning and Research

PPV Peak particle velocity
Project Perris Truck Yard

REMEL Reference Energy Mean Emission Level

RMS Root-mean-square VdB Vibration Decibels



EXECUTIVE SUMMARY

Urban Crossroads, Inc. has prepared this noise study to determine the potential noise impacts and the necessary noise mitigation measures, if any, for Perris Truck Yard development ("Project"). The Project is proposed to consist of a 250-parking stall truck yard on 9.52 acres. At the time this noise analysis was prepared, the future tenants of the proposed Project were unknown, and therefore, this noise study includes a conservative analysis of the proposed Project uses. This study has been prepared to satisfy applicable City of Perris standards and thresholds of significance based on guidance provided by Appendix G of the California Environmental Quality Act (CEQA) Guidelines. (1)

The results of this Perris Truck Yard Noise Impact Analysis are summarized below based on the significance criteria in Section 4 of this report. Table ES-1 shows the findings of significance for each potential noise and/or vibration impact under CEQA before and after any required mitigation measures.

TABLE ES-1: SUMMARY OF CEQA SIGNIFICANCE FINDINGS

Amahusia	Report	Significano	e Findings
Analysis	Section	Unmitigated	Mitigated
Operational Noise	7	Less Than Significant	-
Construction Noise		Less Than Significant	-
Construction Vibration	8	Less Than Significant	-



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1 INTRODUCTION

This noise analysis has been completed to determine the noise impacts associated with the development of Perris Truck Yard ("Project"). This noise study briefly describes the proposed Project, provides information regarding noise fundamentals, sets out the local regulatory setting, presents the study methods and procedures for transportation related CNEL traffic noise analysis, and evaluates the future exterior noise environment. In addition, this study includes an analysis of the potential Project-related long-term stationary-source operational noise and short-term construction noise and vibration impacts.

1.1 SITE LOCATION

The Perris Truck Yard Project is located north of Markham Street and east of Perris Boulevard, as shown on Exhibit 1-A. The Project is within the City of Perris' *Perris Valley Commerce Center Specific Plan* (PVCC SP). The Project is located adjacent to existing industrial and commercial land with noise sensitive single-residential homes located to the north, northeast and southwest of the Project site.

1.2 PROJECT DESCRIPTION

The Project is proposed to consist of a 250-parking stall truck yard on 9.52 acres, as shown on Exhibit 1-B. It is anticipated that the Project would be constructed in one phase by the year 2021. Access to the Project site will be provided by a single driveway on Markham Street.

The on-site Project-related noise sources are expected to include: truck terminal activity, entry gate & truck movements, roof-top air conditioning units, and trash enclosure activity. This noise analysis is intended to describe noise level impacts associated with the expected typical operational activities at the Project site. To present a conservative approach, this report assumes the Project will operate 24-hours daily for seven days per week.

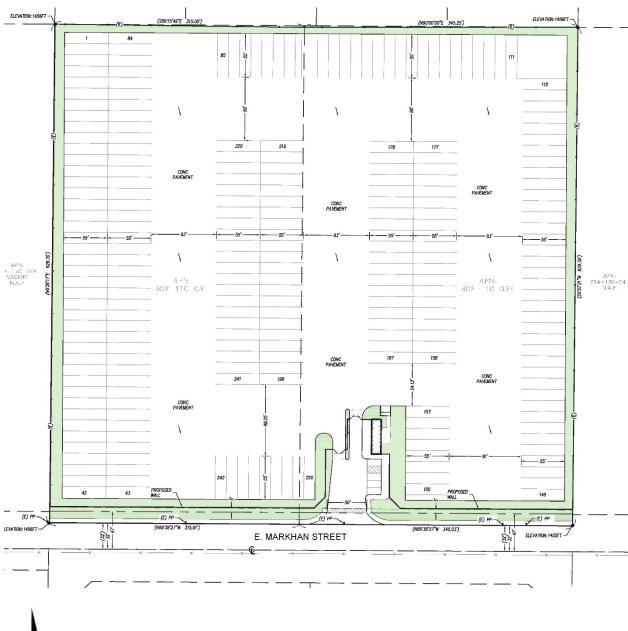


Oleander Ave_ Harley Knox Blvd Harley Knox Blvd E Nance St SITE W Markham St E Markham St W Perry St Sources: Esri, HERE, Garmin, Intermap, increment P Corp., GEBCO, USGS, FAO, NPS, NRCAN, GeoBase, IGN, Kadaster NL, Ordnar RamonaExpy Survey, Esti Japan, METI, Esri China (Hong Kong), (t) OpenStreetMap contributors, and the GIS **LEGEND:** Site Boundary

EXHIBIT 1-A: LOCATION MAP



EXHIBIT 1-B: SITE PLAN







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2 FUNDAMENTALS

Noise is simply defined as "unwanted sound." Sound becomes unwanted when it interferes with normal activities, when it causes actual physical harm or when it has adverse effects on health. Noise is measured on a logarithmic scale of sound pressure level known as a decibel (dB). Aweighted decibels (dBA) approximate the subjective response of the human ear to broad frequency noise source by discriminating against very low and very high frequencies of the audible spectrum. They are adjusted to reflect only those frequencies which are audible to the human ear. Exhibit 2-A presents a summary of the typical noise levels and their subjective loudness and effects that are described in more detail below.

EXHIBIT 2-A: TYPICAL NOISE LEVELS

COMMON OUTDOOR ACTIVITIES	COMMON INDOOR ACTIVITIES	A - WEIGHTED SOUND LEVEL dBA	SUBJECTIVE LOUDNESS	EFFECTS OF NOISE
THRESHOLD OF PAIN		140		
NEAR JET ENGINE		130	INTOLERABLE OR	
		120	DEAFENING	HEARING LOSS
JET FLY-OVER AT 300m (1000 ft)	ROCK BAND	110		
LOUD AUTO HORN		100		
GAS LAWN MOWER AT 1m (3 ft)		90	VERY NOISY	
DIESEL TRUCK AT 15m (50 ft), at 80 km/hr (50 mph)	FOOD BLENDER AT 1m (3 ft)	80	1	
NOISY URBAN AREA, DAYTIME	VACUUM CLEANER AT 3m (10 ft)	70	LOUD	SPEECH INTERFERENCE
HEAVY TRAFFIC AT 90m (300 ft)	NORMAL SPEECH AT 1m (3 ft)	60	2000	HATEIG ENERGE
QUIET URBAN DAYTIME	LARGE BUSINESS OFFICE	50	MODERATE	SLEEP
QUIET URBAN NIGHTTIME	THEATER, LARGE CONFERENCE ROOM (BACKGROUND)	40		DISTURBANCE
QUIET SUBURBAN NIGHTTIME	LIBRARY	30		
QUIET RURAL NIGHTTIME	BEDROOM AT NIGHT, CONCERT HALL (BACKGROUND)	20	FAINT	
	BROADCAST/RECORDING STUDIO	10	VERY FAINT	NO EFFECT
LOWEST THRESHOLD OF HUMAN HEARING	LOWEST THRESHOLD OF HUMAN HEARING	0	VERT FAIRT	

2.1 RANGE OF NOISE

Since the range of intensities that the human ear can detect is so large, the scale frequently used to measure intensity is a scale based on multiples of 10, the logarithmic scale. The scale for measuring intensity is the decibel scale. Each interval of 10 decibels indicates a sound energy ten times greater than before, which is perceived by the human ear as being roughly twice as loud. (2) The most common sounds vary between 40 dBA (very quiet) to 100 dBA (very loud). Normal conversation at three feet is roughly at 60 dBA, while loud jet engine noises equate to 110 dBA at approximately 100 feet, which can cause serious discomfort. (3) Another important aspect of noise is the duration of the sound and the way it is described and distributed in time.



2.2 Noise Descriptors

Environmental noise descriptors are generally based on averages, rather than instantaneous, noise levels. The most used figure is the equivalent level (L_{eq}). Equivalent sound levels are not measured directly but are calculated from sound pressure levels typically measured in Aweighted decibels (dBA). The equivalent sound level (L_{eq}) represents a steady state sound level containing the same total energy as a time varying signal over a given sample period (typically one hour) and is commonly used to describe the "average" noise levels within the environment.

Peak hour or average noise levels, while useful, do not completely describe a given noise environment. Noise levels lower than peak hour may be disturbing if they occur during times when quiet is most desirable, namely evening and nighttime (sleeping) hours. To account for this, the Community Noise Equivalent Level (CNEL), representing a composite 24-hour noise level is utilized. The CNEL is the weighted average of the intensity of a sound, with corrections for time of day, and averaged over 24 hours. The time of day corrections require the addition of 5 decibels to dBA Leq sound levels in the evening from 7:00 p.m. to 10:00 p.m., and the addition of 10 decibels to dBA Leq sound levels at night between 10:00 p.m. and 7:00 a.m. These additions are made to account for the noise sensitive time periods during the evening and night hours when sound appears louder. CNEL does not represent the actual sound level heard at any time, but rather represents the total sound exposure. The City of Perris relies on the 24-hour CNEL level to assess land use compatibility with transportation related noise sources.

2.3 SOUND PROPAGATION

When sound propagates over a distance, it changes in level and frequency content. The way noise reduces with distance depends on the following factors.

2.3.1 GEOMETRIC SPREADING

Sound from a localized source (i.e., a stationary point source) propagates uniformly outward in a spherical pattern. The sound level attenuates (or decreases) at a rate of 6 dB for each doubling of distance from a point source. Highways consist of several localized noise sources on a defined path and hence can be treated as a line source, which approximates the effect of several point sources. Noise from a line source propagates outward in a cylindrical pattern, often referred to as cylindrical spreading. Sound levels attenuate at a rate of 3 dB for each doubling of distance from a line source. (2)

2.3.2 GROUND ABSORPTION

The propagation path of noise from a highway to a receiver is usually very close to the ground. Noise attenuation from ground absorption and reflective wave canceling adds to the attenuation associated with geometric spreading. Traditionally, the excess attenuation has also been expressed in terms of attenuation per doubling of distance. This approximation is usually sufficiently accurate for distances of less than 200 ft. For acoustically hard sites (i.e., sites with a reflective surface between the source and the receiver, such as a parking lot or body of water), no excess ground attenuation is assumed. For acoustically absorptive or soft sites (i.e., those



sites with an absorptive ground surface between the source and the receiver such as soft dirt, grass, or scattered bushes and trees), an excess ground attenuation value of 1.5 dB per doubling of distance is normally assumed. When added to the cylindrical spreading, the excess ground attenuation results in an overall drop-off rate of 4.5 dB per doubling of distance from a line source. (4)

2.3.3 ATMOSPHERIC EFFECTS

Receivers located downwind from a source can be exposed to increased noise levels relative to calm conditions, whereas locations upwind can have lowered noise levels. Sound levels can be increased at large distances (e.g., more than 500 feet) due to atmospheric temperature inversion (i.e., increasing temperature with elevation). Other factors such as air temperature, humidity, and turbulence can also have significant effects. (2)

2.3.4 SHIELDING

A large object or barrier in the path between a noise source and a receiver can substantially attenuate noise levels at the receiver. The amount of attenuation provided by shielding depends on the size of the object and the frequency content of the noise source. Shielding by trees and other such vegetation typically only has an "out of sight, out of mind" effect. That is, the perception of noise impact tends to decrease when vegetation blocks the line-of-sight to nearest residents. However, for vegetation to provide a substantial, or even noticeable, noise reduction, the vegetation area must be at least 15 feet in height, 100 feet wide and dense enough to completely obstruct the line-of sight between the source and the receiver. This size of vegetation may provide up to 5 dBA of noise reduction. The Federal Highway Administration (FHWA) does not consider the planting of vegetation to be a noise abatement measure. (4)

2.3.5 REFLECTION

Field studies conducted by the FHWA have shown that the reflection from barriers and buildings does not substantially increase noise levels. (4) If all the noise striking a structure was reflected back to a given receiving point, the increase would be theoretically limited to 3 dBA. Further, not all the acoustical energy is reflected back to same point. Some of the energy would go over the structure, some is reflected to points other than the given receiving point, some is scattered by ground coverings (e.g., grass and other plants), and some is blocked by intervening structures and/or obstacles (e.g., the noise source itself). Additionally, some of the reflected energy is lost due to the longer path that the noise must travel. FHWA measurements made to quantify reflective increases in traffic noise have not shown an increase of greater than 1-2 dBA; an increase that is not perceptible to the average human ear.

2.4 Noise Control

Noise control is the process of obtaining an acceptable noise environment for an observation point or receiver by controlling the noise source, transmission path, receiver, or all three. This concept is known as the source-path-receiver concept. In general, noise control measures can be applied to these three elements.



2.5 Noise Barrier Attenuation

Effective noise barriers can reduce noise levels by up to 10 to 15 dBA, cutting the loudness of traffic noise in half. A noise barrier is most effective when placed close to the noise source or receiver. Noise barriers, however, do have limitations. For a noise barrier to work, it must be high enough and long enough to block the path of the noise source. (4)

2.6 LAND USE COMPATIBILITY WITH NOISE

Some land uses are more tolerant of noise than others. For example, schools, hospitals, churches, and residences are more sensitive to noise intrusion than are commercial or industrial developments and related activities. As ambient noise levels affect the perceived amenity or livability of a development, so too can the mismanagement of noise impacts impair the economic health and growth potential of a community by reducing the area's desirability as a place to live, shop and work. For this reason, land use compatibility with the noise environment is an important consideration in the planning and design process. The FHWA encourages State and Local government to regulate land development in such a way that noise-sensitive land uses are either prohibited from being located adjacent to a highway, or that the developments are planned, designed, and constructed in such a way that noise impacts are minimized. (5)

2.7 COMMUNITY RESPONSE TO NOISE

Community responses to noise may range from registering a complaint by telephone or letter, to initiating court action, depending upon everyone's susceptibility to noise and personal attitudes about noise. Several factors are related to the level of community annoyance including:

- Fear associated with noise producing activities;
- Socio-economic status and educational level;
- Perception that those affected are being unfairly treated;
- Attitudes regarding the usefulness of the noise-producing activity;
- Belief that the noise source can be controlled.

Approximately ten percent of the population has a very low tolerance for noise and will object to any noise not of their making. Consequently, even in the quietest environment, some complaints will occur. Twenty-five percent of the population will not complain even in very severe noise environments. Thus, a variety of reactions can be expected from people exposed to any given noise environment. (6) Surveys have shown that about ten percent of the people exposed to traffic noise of 60 dBA will report being highly annoyed with the noise, and each increase of one dBA is associated with approximately two percent more people being highly annoyed. When traffic noise exceeds 60 dBA or aircraft noise exceeds 55 dBA, people may begin to complain. (6) Despite this variability in behavior on an individual level, the population can be expected to exhibit the following responses to changes in noise levels as shown on Exhibit 2-B. A change of 3 dBA are considered *barely perceptible*, and changes of 5 dBA are considered *readily perceptible*. (4)



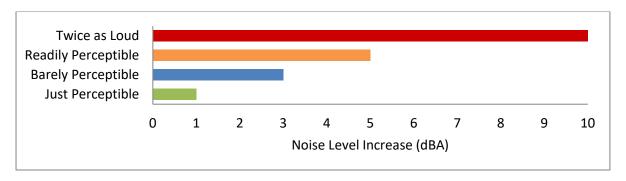


EXHIBIT 2-B: NOISE LEVEL INCREASE PERCEPTION

2.8 VIBRATION

Per the Federal Transit Administration (FTA) *Transit Noise and Vibration Impact Assessment Manual* (7), vibration is the periodic oscillation of a medium or object. The rumbling sound caused by the vibration of room surfaces is called structure-borne noise. Sources of ground-borne vibrations include natural phenomena (e.g., earthquakes, volcanic eruptions, sea waves, landslides) or human-made causes (e.g., explosions, machinery, traffic, trains, construction equipment). Vibration sources may be continuous, such as factory machinery, or transient, such as explosions. As is the case with airborne sound, ground-borne vibrations may be described by amplitude and frequency.

There are several different methods that are used to quantify vibration. The peak particle velocity (PPV) is defined as the maximum instantaneous peak of the vibration signal. The PPV is most frequently used to describe vibration impacts to buildings but is not always suitable for evaluating human response (annoyance) because it takes some time for the human body to respond to vibration signals. Instead, the human body responds to average vibration amplitude often described as the root mean square (RMS). The RMS amplitude is defined as the average of the squared amplitude of the signal and is most frequently used to describe the effect of vibration on the human body. Decibel notation (VdB) is commonly used to measure RMS. Decibel notation (VdB) serves to reduce the range of numbers used to describe human response to vibration. Typically, ground-borne vibration generated by man-made activities attenuates rapidly with distance from the source of the vibration. Sensitive receivers for vibration include structures (especially older masonry structures), people (especially residents, the elderly, and sick), and vibration-sensitive equipment and/or activities

The background vibration-velocity level in residential areas is generally 50 VdB. Ground-borne vibration is normally perceptible to humans at approximately 65 VdB. For most people, a vibration-velocity level of 75 VdB is the approximate dividing line between barely perceptible and distinctly perceptible levels. Typical outdoor sources of perceptible ground-borne vibration are construction equipment, steel-wheeled trains, and traffic on rough roads. If a roadway is smooth, the ground-borne vibration is rarely perceptible. The range of interest is from approximately 50 VdB, which is the typical background vibration-velocity level, to 100 VdB, which is the general threshold where minor damage can occur in fragile buildings. Exhibit 2-C illustrates common vibration sources and the human and structural response to ground-borne vibration.

Velocity Typical Sources Level* Human/Structural Response (50 ft from source) 100 Threshold, minor cosmetic damage Blasting from construction projects fragile buildings Bulldozers and other heavy tracked construction equipment Difficulty with tasks such as 90 reading a VDT screen Commuter rail, upper range 80 Residential annoyance, infrequent Rapid transit, upper range events (e.g. commuter rail) Commuter rail, typical Residential annoyance, frequent Bus or truck over bump events (e.g. rapid transit) Rapid transit, typical Limit for vibration sensitive equipment. Approx. threshold for Bus or truck, typical human perception of vibration 60 Typical background vibration 50

EXHIBIT 2-C: TYPICAL LEVELS OF GROUND-BORNE VIBRATION

* RMS Vibration Velocity Level in VdB relative to 10-6 inches/second

Source: Federal Transit Administration (FTA) Transit Noise and Vibration Impact Assessment Manual.



3 REGULATORY SETTING

To limit population exposure to physically and/or psychologically damaging as well as intrusive noise levels, the federal government, the State of California, various county governments, and most municipalities in the state have established standards and ordinances to control noise. In most areas, automobile and truck traffic is the major source of environmental noise. Traffic activity generally produces an average sound level that remains constant with time. Air and rail traffic, and commercial and industrial activities are also major sources of noise in some areas. Federal, state, and local agencies regulate different aspects of environmental noise. Federal and state agencies generally set noise standards for mobile sources such as aircraft and motor vehicles, while regulation of stationary sources is left to local agencies.

3.1 STATE OF CALIFORNIA NOISE REQUIREMENTS

The State of California regulates freeway noise, sets standards for sound transmission, provides occupational noise control criteria, identifies noise standards, and provides guidance for local land use compatibility. State law requires that each county and city adopt a General Plan that includes a Noise Element which is to be prepared per guidelines adopted by the Governor's Office of Planning and Research (OPR). (8) The purpose of the Noise Element is to *limit the exposure of the community to excessive noise levels*. In addition, the California Environmental Quality Act (CEQA) requires that all known environmental effects of a project be analyzed, including environmental noise impacts.

3.2 STATE OF CALIFORNIA GREEN BUILDING STANDARDS CODE

The State of California's Green Building Standards Code (CALGreen) contains mandatory measures for non-residential building construction in Section 5.507 on Environmental Comfort. (9) These noise standards are applied to new construction in California for controlling interior noise levels resulting from exterior noise sources. The regulations specify that acoustical studies must be prepared when non-residential structures are developed in areas where the exterior noise levels exceed 65 dBA CNEL, such as within a noise contour of an airport, freeway, railroad, and other areas where noise contours are not readily available. If the development falls within an airport or freeway 65 dBA CNEL noise contour, the combined sound transmission class (STC) rating of the wall and roof-ceiling assemblies shall be constructed to provide an interior noise environment attributable to exterior sources that does not exceed an hourly equivalent noise level of 50 dBA Leq in occupied areas during any hour of operation (Section 5.507.4.2).



3.3 CITY OF PERRIS GENERAL PLAN NOISE ELEMENT

The City of Perris has adopted a Noise Element of the General Plan (10) to control and abate environmental noise, and to protect the citizens of Perris from excessive exposure to noise. The Noise Element specifies the maximum allowable unmitigated exterior noise levels for new developments impacted by transportation noise sources such as arterial roads, freeways, airports, and railroads. In addition, the Noise Element identifies noise polices and implementation measures designed to protect, create, and maintain an environment free from noise that may jeopardize the health or welfare of sensitive receptors, or degrade quality of life.

The noise standards identified in the City of Perris General Plan are guidelines to evaluate the acceptability of the transportation related noise level impacts. These standards are based on the Governor's Office of Planning and Research (OPR) and are used to assess the long-term traffic noise impacts on land uses. According to the City's Land Use Compatibility for Community Noise Exposure (Exhibit N-1), noise-sensitive land uses such as single-family residences are normally acceptable with exterior noise levels below 60 dBA CNEL and conditionally acceptable with noise levels below 65 dBA CNEL. Industrial uses, such as the Project, are considered normally acceptable with exterior noise levels of up to 70 dBA CNEL, and conditionally acceptable with exterior noise levels between 70 to 80 dBA CNEL. (10)

3.4 OPERATIONAL STANDARDS

To analyze noise impacts originating from a designated fixed location or private property such as the Perris Truck Yard, operational noise such as the expected truck terminal activity, entry gate & truck movements, roof-top air conditioning units, and trash enclosure activity are typically evaluated against standards established under a City's Municipal Code.

The City of Perris Municipal Code, Chapter 7.34 *Noise Control*, Section 7.34.040, establishes the permissible noise level at any point on the property line of the affected residential receiver. Therefore, for residential properties, the exterior noise level shall not exceed a maximum noise level of 80 dBA L_{max} during daytime hours (7:01 a.m. to 10:00 p.m.) and shall not exceed a maximum noise level of 60 dBA L_{max} during the nighttime hours (10:01 p.m. to 7:00 a.m.), as shown on Table 3-1. (11) The City of Perris Municipal Code is included in Appendix 3.1.

Additional exterior noise level standards are identified in the City of Perris General Plan Noise Element Implementation Measure V.A.1 which requires that new industrial facilities within 160 feet of the property line of existing noise-sensitive land uses must demonstrate compliance with a 60 dBA CNEL exterior noise level standard. Table 3-1 shows the Municipal Code and General Plan standards used in this analysis to evaluate the potential operational noise levels from the Project.



TABLE 3-1: OPERATIONAL NOISE LEVEL STANDARDS

Jurisdiction	Land Use	Time Period	Noise Level Standard (dBA)
_	Decidential ¹	Daytime (7:01 a.m 10:00 p.m.)	80 dBA L _{max}
City of Perris	Residential ¹	Nighttime (10:01 p.m 7:00 a.m.)	60 dBA L _{max}
1 61113	Within 160 Feet of Property Line ²	24-Hours	60 dBA CNEL

¹ Source: City of Perris Municipal Code, Sections 7.34.040 & 7.34.050 (Appendix 3.1).

3.5 CONSTRUCTION NOISE STANDARDS

To analyze noise impacts originating from the construction of the Perris Truck Yard site, noise from construction activities are typically evaluated against standards established under a City's Municipal Code. The City of Perris Municipal Code, Section 7.34.060, identifies the City's construction noise standards and permitted hours of construction activity (refer to Table 3-2). Further, the City of Perris Municipal Code, Section 7.34.060, noise level standard of 80 dBA L_{max} at residential properties shall apply to the noise-sensitive receiver locations located in the City of Perris. (11)

TABLE 3-2: CONSRUCTION NOISE LEVEL STANDARDS

Jurisdiction	Permitted Hours of Construction Activity	Construction Noise Level Standard
City of Perris ¹	7:00 a.m. to 7:00 p.m. on any day except Sundays and legal holidays (except for Columbus Day and Washington's birthday).	80 dBA L _{max}

¹ Source: City of Perris Municipal Code, Section 7.34.060 (Appendix 3.1).

3.6 CONSTRUCTION VIBRATION STANDARDS

The City of Perris has not identified or adopted specific vibration level standards. However, the United States Department of Transportation Federal Transit Administration (FTA) *Transit Noise and Vibration Impact Assessment* methodology provides guidelines for maximum-acceptable vibration criteria for different types of land uses. These guidelines allow 90 VdB for industrial (workshop) use, 84 VdB for office use and 78 VdB for daytime residential uses. (7 p. 131)

Construction activities can result in varying degrees of ground-borne vibration, depending on the equipment and methods used, distance to the affected structures and soil type. Construction vibration is generally associated with pile driving and rock blasting. Other construction equipment such as air compressors, light trucks, hydraulic loaders, etc., generates little or no ground vibration. Large bulldozers and loaded trucks can cause perceptible vibration levels proximate receptors.



² Source: City of Perris General Plan Noise Element, Implementation Measure V.A.1.

Although Project construction noise and vibration impacts will be *less than significant*, the Project is required to comply with the following construction-related mitigation measures (MM) from the PVCC Specific Plan Environmental Impact Report:

- MM Noise 1 During all project site excavation and grading on site, the construction contractors shall equip all construction equipment, fixed or mobile, with properly operating and maintained mufflers consistent with manufacturer's standards. The construction contractor shall place all stationary construction equipment so that emitted noise is directed away from the noise sensitive receptors nearest the project site.
- **MM Noise 2** During construction, stationary construction equipment, stockpiling and vehicle staging areas would be placed a minimum of 446 feet away from the closest sensitive receptor.
- **MM Noise 3** No combustion-powered equipment, such as pumps or generators, shall be allowed to operate within 446 feet of any occupied residence unless the equipment is surrounded by a noise protection barrier.
- **MM Noise 4** Construction contractors of implementing development projects shall limit haul truck deliveries to the same hours specified for construction equipment. To the extent feasible, haul routes shall not pass sensitive land uses or residential dwellings.

3.7 MARCH AIR RESERVE BASE/INLAND PORT AIRPORT LAND USE COMPATIBILITY

The March Air Reserve Base/Inland Port Airport (MARB/IPA) is located approximately 1.3 miles northwest of the Project site boundary. The *March Air Reserve Base/Inland Port Airport Land Use Compatibility Plan* (MARB/IPA LUCP) includes the policies for determining the land use compatibility of the Project. (12) The MARB/IPA, Map MA-1, indicates that the Project site is located within Compatibility Zone D, and the Table MA-1 Compatibility Zone Factors indicates that this area is considered to have a *moderate to low* noise impact, and is mostly within or near the 55 dBA CNEL noise level contour boundaries. Consistent with the Basic Compatibility Criteria, listed in Table MA-2 of the MARB/IPA LUCP, noise sensitive outdoor uses are not permitted. The MARB/IPA LUCP does not identify industrial-use specific noise compatibility standards, and therefore, the Governor's Office of Planning and Research (OPR) Land Use Compatibility for Community Noise Exposure, previously discussed in Section 3.3, is used to assess potential aircraft-related noise levels at the Project site. The OPR guidelines indicate that industrial uses, such as the Project, are considered *normally acceptable* with exterior noise levels of up to 70 dBA CNEL. (8)

The noise contour boundaries of MARB/IPA are presented on Exhibit 3-A of this report and show that the Project is considered *normally acceptable* land use since it is located outside the 55 dBA CNEL noise level contour boundaries



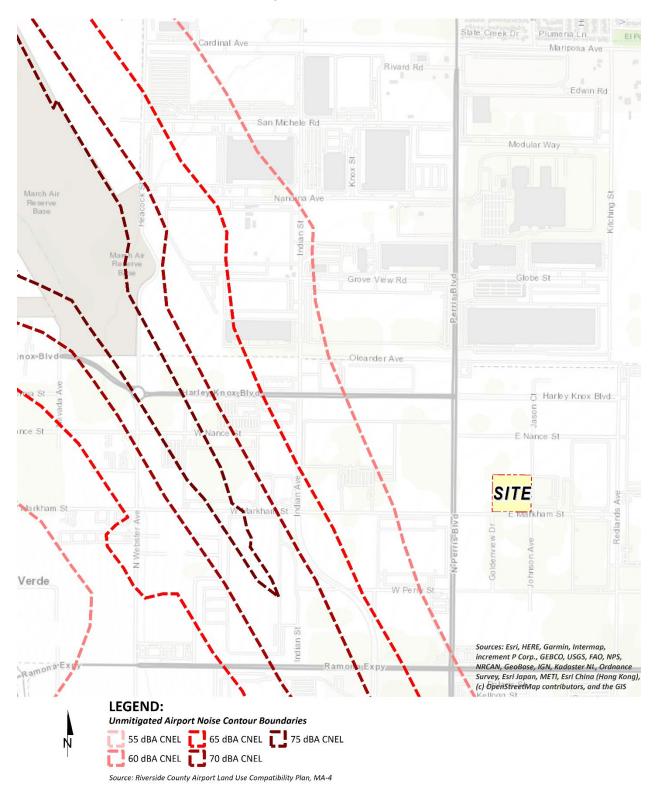


EXHIBIT 3-A: MARB/IPA FUTURE AIRPORT NOISE CONTOURS



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4 SIGNIFICANCE CRITERIA

The following significance criteria are based on currently adopted guidance provided by Appendix G of the California Environmental Quality Act (CEQA) Guidelines. (1) For the purposes of this report, impacts would be potentially significant if the Project results in or causes:

- A. Generation of a substantial temporary or permanent increase in ambient noise levels in the vicinity of the project in excess of standards established in the local general plan or noise ordinance, or applicable standards of other agencies?
- B. Generation of excessive ground-borne vibration or ground-borne noise levels?
- C. For a project located within the vicinity of a private airstrip or an airport land use plan or, where such a plan has not been adopted, within two miles of a public airport or public use airport, would the project expose people residing or working in the project area to excessive noise levels?

While the City of Perris General Plan Guidelines provide direction on noise compatibility and establish noise standards by land use type that are sufficient to assess the significance of noise impacts, they do not define the levels at which increases are considered substantial temporary or permanent for use under Guideline A. CEQA Appendix G Guideline C applies to the nearest public and private airports, if any, and the Project's land use compatibility.

4.1 CEQA GUIDELINES NOT FURTHER ANALYZED

The closest airport which would require additional noise analysis under CEQA Appendix G Guideline C is the MARB/IPA. As previously described in Section 3.7, the Project is located in Compatibility Zone D2, and the Table MA-1 Compatibility Zone Factors indicates that this area is considered to have a *moderate to low* noise impact. In addition, Table MA-2 indicates that the Project land use satisfies the basic compatibility criteria. Therefore, the potential impacts under CEQA Appendix G Guideline C, are *less than significant* and are not further analyzed in this noise study.

4.2 **PVCC SP EIR THRESHOLDS**

As identified in the PVCC SP EIR, sensitive receivers are areas where humans are participating in activities that may be subject to the stress of significant interference from noise and often include residential dwellings, mobile homes, hotels, motels, hospitals, nursing homes, educational facilities, and libraries. Other receivers include office and industrial buildings, which are not considered as sensitive as single-family homes, but are still protected by City of Perris land use compatibility standards, as discussed below.

Noise level increases at nearest receiver locations resulting from the Project are evaluated based on the PVCC SP EIR Thresholds described below at nearest sensitive receiver locations. Further, CEQA requires that consideration be given to the magnitude of the increase, the existing ambient noise levels, and the location of noise-sensitive receivers to determine if a noise increase represents a significant adverse environmental impact. This approach recognizes that there is no single noise increase that renders the noise impact significant. (13)



According to the PVCC SP EIR, there is no official "industry standard" of determining significance of noise impacts. However, typically, a jurisdiction will identify either 3 dBA or 5 dBA increase as being the threshold because these levels represent varying levels of perceived noise increases. The PVCC SP EIR indicates that a 5 dBA noise level increase is considered discernable to most people in an exterior environment when the resulting noise levels are below 60 dBA. Further, it identifies a 3 dBA increase threshold when the noise levels already exceed 60 dBA. In addition, according to the PVCC SP EIR, an increase of 5 dBA or more above without Project noise levels is considered a significant impact at all other sensitive land uses. (14)

4.3 SIGNIFICANCE CRITERIA SUMMARY

Noise impacts shall be considered significant if any of the following occur as a direct result of the proposed Project. Table 4-1 shows the significance criteria summary matrix.

TABLE 4-1: SIGNIFICANCE CRITERIA SUMMARY

Analysis	Receiving Land Use	Condition(s)	Significance Criteria		
	Land Use		Daytime	Nighttime	
		At residential land use ¹	80 dBA L _{max}	60 dBA L _{max}	
Operational	Noise- Sensitive	Within 160 Feet of residential use ²	60 dBA CNEL		
Operational		If resulting noise level is < 60 dBA L _{eq} ³	≥ 5 dBA L _{eq} Project increase		
		If resulting noise level is > 60 dBA L _{eq} ³	≥ 3 dBA L _{eq} Project increase		
	Noise-	Noise Level Threshold⁴	80 dBA L _{max}		
Constant	Sensitive	Vibration Level Threshold ⁵ 78 VdB		/dB	
Construction	Office	Vibration Level Threshold⁵	84 VdB		
	Industrial	Vibration Level Threshold⁵	90 VdB		

 $^{^{\}rm 1}\text{City}$ of Perris Municipal Code, Section 7.34.040 (Appendix 3.1).



² City of Perris General Plan Noise Element, Implementation Measure V.A.1.

³ PVCC SP EIR, Page 4.9-20.

⁴ City of Perris Municipal Code, Section 7.34.060 (Appendix 3.1).

⁵ Federal Transit Administration, Transit Noise and Vibration Impact Assessment Manual

[&]quot;Daytime" = 7:01 a.m. - 10:00 p.m.; "Nighttime" = 10:01 p.m. - 7:00 a.m.

5 EXISTING NOISE LEVEL MEASUREMENTS

To assess the existing noise level environment, 24-hour noise level measurements were taken at three locations in the Project study area. The receiver locations were selected to describe and document the existing noise environment within the Project study area. Exhibit 5-A provides the boundaries of the Project study area and the noise level measurement locations. To fully describe the existing noise conditions, noise level measurements were collected by Urban Crossroads, Inc. on Thursday, May 14th, 2020. Appendix 5.1 includes study area photos.

5.1 Measurement Procedure and Criteria

To describe the existing noise environment, the hourly noise levels were measured during typical weekday conditions over a 24-hour period. By collecting individual hourly noise level measurements, it is possible to describe the daytime and nighttime hourly noise levels and calculate the 24-hour CNEL. The long-term noise readings were recorded using Piccolo Type 2 integrating sound level meter and dataloggers. The Piccolo sound level meters were calibrated using a Larson-Davis calibrator, Model CAL 150. All noise meters were programmed in "slow" mode to record noise levels in "A" weighted form. The sound level meters and microphones were equipped with a windscreen during all measurements. All noise level measurement equipment satisfies the American National Standards Institute (ANSI) standard specifications for sound level meters ANSI S1.4-2014/IEC 61672-1:2013. (15)

5.2 Noise Measurement Locations

The long-term noise level measurements were positioned as close to the nearest sensitive receiver locations as possible to assess the existing ambient hourly noise levels surrounding the Project site. Both Caltrans and the FTA recognize that it is not reasonable to collect noise level measurements that can fully represent every part of a private yard, patio, deck, or balcony normally used for human activity when estimating impacts for new development projects. This is demonstrated in the Caltrans general site location guidelines which indicate that, sites must be free of noise contamination by sources other than sources of interest. Avoid sites located near sources such as barking dogs, lawnmowers, pool pumps, and air conditioners unless it is the express intent of the analyst to measure these sources. (2) Further, FTA guidance states, that it is not necessary nor recommended that existing noise exposure be determined by measuring at every noise-sensitive location in the project area. Rather, the recommended approach is to characterize the noise environment for clusters of sites based on measurements or estimates at representative locations in the community. (7)

Based on recommendations of Caltrans and the FTA, it is not necessary to collect measurements at each individual building or residence, because each receiver measurement represents a group of buildings that share acoustical equivalence. (7) In other words, the area represented by the receiver shares similar shielding, terrain, and geometric relationship to the reference noise source. Receivers represent a location of noise sensitive areas and are used to estimate the future noise level impacts. Collecting reference ambient noise level measurements at the nearby sensitive receiver locations allows for a comparison of the before and after Project noise levels



and is necessary to assess potential noise impacts due to the Project's contribution to the ambient noise levels.

5.3 Noise Measurement Results

The noise measurements presented below focus on the average or equivalent sound levels (L_{eq}). The equivalent sound level (L_{eq}) represents a steady state sound level containing the same total energy as a time varying signal over a given sample period. Table 5-1 identifies the hourly daytime (7:00 a.m. to 10:00 p.m.) and nighttime (10:00 p.m. to 7:00 a.m.) noise levels at each noise level measurement location. Appendix 5.2 provides a summary of the existing hourly ambient noise levels.

Table 5-1 provides the (energy average) noise levels used to describe the daytime and nighttime ambient conditions. These daytime and nighttime energy average noise levels represent the average of all hourly noise levels observed during these time periods expressed as a single number. The background ambient noise levels in the Project study area are dominated by the transportation-related noise associated with surface streets. This includes the auto and heavy truck activities on study area roadway segments near the noise level measurement locations. The 24-hour existing noise level measurement results are shown on Table 5-1.

TABLE 5-1: 24-HOUR AMBIENT NOISE LEVEL MEASUREMENTS

Location ¹	Description	Energy A Noise (dBA	CNEL	
		Daytime	Nighttime	
L1	Located northwest of the Project site on East Nance Street near existing single-family residential home at 75 East Nance Street.	60.9	60.5	67.1
L2	Located northeast of the Project site on Las Palmas near existing single-family residential home at 220 East Nance Street.	50.5	47.3	54.7
L3	Located southwest of the Project site on Perry street near existing single-family residential home at 77 Perry Street.	56.7	55.6	62.5

¹ See Exhibit 5-A for the noise level measurement locations.



² Energy (logarithmic) average levels. The long-term 24-hour measurement worksheets are included in Appendix 5.2.

[&]quot;Daytime" = 7:00 a.m. to 10:00 p.m.; "Nighttime" = 10:00 p.m. to 7:00 a.m.

ASON CT HARLEY KNOX BLVD NANCE ST SITE MARKHAM ST JOHNSON AVE PERRY ST

EXHIBIT 5-A: NOISE MEASUREMENT LOCATIONS





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6 SENSITIVE RECEIVER LOCATIONS

To assess the potential for long-term operational and short-term construction noise impacts, the following sensitive receiver locations, as shown on Exhibit 6-A, were identified as representative locations for analysis. Sensitive receivers are generally defined as locations where people reside or where the presence of unwanted sound could otherwise adversely affect the use of the land. Noise-sensitive land uses are generally considered to include schools, hospitals, single-family dwellings, mobile home parks, churches, libraries, and recreation areas. Moderately noise-sensitive land uses typically include multi-family dwellings, hotels, motels, dormitories, out-patient clinics, cemeteries, golf courses, country clubs, athletic/tennis clubs, and equestrian clubs. Land uses that are considered relatively insensitive to noise include business, commercial, and professional developments. Land uses that are typically not affected by noise include: industrial, manufacturing, utilities, agriculture, undeveloped land, parking lots, warehousing, liquid and solid waste facilities, salvage yards, and transit terminals.

To describe the potential off-site Project noise levels, three receiver locations in the vicinity of the Project site were identified. All distances are measured from the Project site boundary to the outdoor living areas (e.g., private backyards) or at the building façade, whichever is closer to the Project site. The selection of receiver locations is based on FHWA guidelines and is consistent with additional guidance provided by Caltrans and the FTA, as previously described in Section 5.2. Other sensitive land uses in the Project study area that are located at greater distances than those identified in this noise study will experience lower noise levels than those presented in this report due to the additional attenuation from distance and the shielding of intervening structures. Distance is measured in a straight line from the project boundary to each receiver location.

- R1: Location R1 represents the existing noise sensitive residence at 75 East Nance Street, approximately 389 feet north of the Project site. R1 is placed in the private outdoor living area (backyard) facing the Project site. A 24-hour noise measurement was taken near this location, L1, to describe the existing ambient noise environment.
- R2: Location R2 represents the existing noise sensitive residence at 220 East Nance Street, approximately 786 feet northeast of the Project site. Since there are no private outdoor living areas (backyards) facing the Project site, receiver R2 is placed at the residential building façade. A 24-hour noise measurement was taken near this location, L2, to describe the existing ambient noise environment.
- R3: Location R3 represents the existing noise sensitive residence at 77 Perry Street, approximately 1,854 feet southwest of the Project site. Since there are no private outdoor living areas (backyards) facing the Project site, receiver R3 is placed at the residential building façade. A 24-hour noise measurement near this location, L3, is used to describe the existing ambient noise environment.

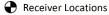


ASON CT HARLEY KNOX BLVD NANCE ST SITE MARKHAM ST PERRY ST

EXHIBIT 6-A: SENSITIVE RECEIVER LOCATIONS



LEGEND:



Distance from receiver to Project site boundary (in feet)



7 OPERATIONAL NOISE IMPACTS

This section analyzes the potential stationary-source operational noise impacts at the nearest receiver locations, identified in Section 6, resulting from the operation of the Perris Truck Yard Project. Exhibit 7-A identifies the representative noise source activities used to assess the operational noise levels.

7.1 OPERATIONAL NOISE SOURCES

This operational noise analysis is intended to describe noise level impacts associated with the typical daytime and nighttime activities at the Project site. To present the potential worst-case noise conditions, this analysis assumes the Project would be operational 24 hours per day, seven days per week. The on-site Project-related noise sources are expected to include: truck terminal activity, entry gate & truck movements, roof-top air conditioning units, and trash enclosure activity.

7.2 REFERENCE NOISE LEVELS

To estimate the Project operational noise impacts, reference noise level measurements were collected from similar types of activities to represent the noise levels expected with the development of the proposed Project. This section provides a detailed description of the reference noise level measurements shown on Table 7-1 used to estimate the Project operational noise impacts. It is important to note that the following projected noise levels assume the worst-case noise environment with the truck terminal activity, entry gate & truck movements, roof-top air conditioning units, and trash enclosure activity all operating continuously. These sources of noise activity will likely vary throughout the day.

7.2.1 MEASUREMENT PROCEDURES

The reference noise level measurements presented in this section were collected using a Larson Davis LxT Type 1 precisions sound level meter (serial number 01146). The LxT sound level meter was calibrated using a Larson-Davis calibrator, Model CAL 200, was programmed in "slow" mode to record noise levels in "A" weighted form and was located at approximately five feet above the ground elevation for each measurement. The sound level meters and microphones were equipped with a windscreen during all measurements. All noise level measurement equipment satisfies the American National Standards Institute (ANSI) standard specifications for sound level meters ANSI S1.4-2014/IEC 61672-1:2013. (15)



EXHIBIT 7-A: OPERATIONAL NOISE SOURCE LOCATIONS

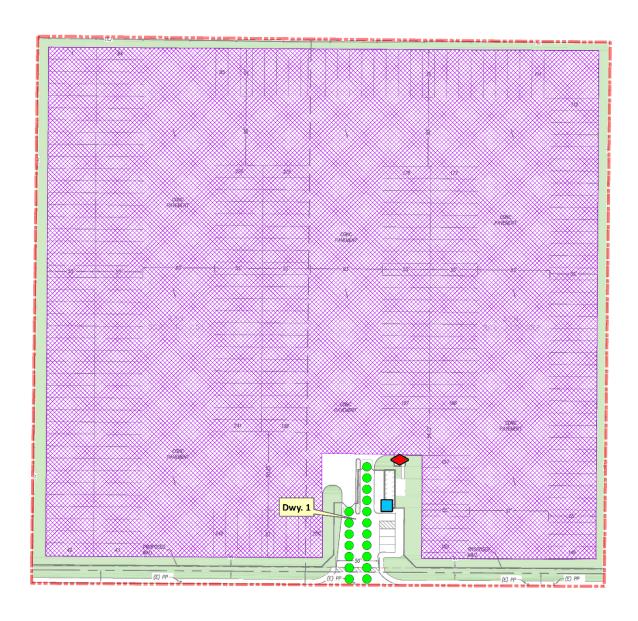






TABLE 7-1: REFERENCE NOISE LEVEL MEASUREMENTS

	Noise Source	Min./	Hour ²	Reference	Reference Noise Level @ 50' (dBA L _{max})	
Noise Source ¹	Height (Feet)	Day	Night	Noise Level @ 50' (dBA L _{eq})		
Truck Terminal Activity	8'	60	60	62.8	71.2	
Entry Gate & Truck Movements	8'	_3	_3	58.0	73.1	
Roof-Top Air Conditioning Units	5'	39	28	57.2	57.7	
Trash Enclosure Activity	5'	10	10	56.8	71.1	

¹ As measured by Urban Crossroads, Inc.

7.2.2 TRUCK TERMINAL ACTIVITY

To evaluate the noise levels associated with truck idling, backup alarms, trailer movements and storage activities, Urban Crossroads collected a reference noise level measurement at an existing parcel hub facility to describe the potential operational noise levels associated with Project operational activities. The measured reference noise level at 50 feet from activity was measured at 62.8 dBA L_{eq}. The reference noise level measurement includes a semi-truck with trailer pass-by event, background switcher cab trailer towing, drop-off, idling, and backup alarm events. Noise associated with trailer storage activity is expected to operate for the entire hour (60 minutes).

7.2.3 ENTRY GATE & TRUCK MOVEMENTS

An entry gate and truck movements reference noise level measurement were taken at the southern entry gate of the Motivational Fulfillment & Logistics Services distribution facility located at 6810 Bickmore Avenue in the City of Chino over a 15-minute period and represents multiple noise sources producing a reference noise level of 58.0 dBA L_{eq} at 50 feet. The noise sources included at this measurement location account for the rattling and squeaking during normal opening and closing operations, the gate closure equipment, truck engines idling outside the entry gate, truck movements through the entry gate, and background truck court activities and forklift backup alarm noise. Consistent with Perris Truck Yard Trip Generation & Scoping Memorandum, the Project is expected to generate a total of approximately 376 trip-ends per day (actual vehicles) and includes 199 truck trip-ends per day. (16) This noise study relies on the actual Project trips (as opposed to the passenger car equivalents) to accurately account for the effect of individual truck trips on the study area roadway network. Using the estimated number of truck trips in combination with time of day vehicle splits, the number of entry gate and truck movements by driveway location were calculated. As shown on Table 7-2, this information is then used to calculate the entry gate and truck movements operational noise source activity based on the number of events by time of day.



² Anticipated duration (minutes within the hour) of noise activity during typical hourly conditions expected at the Project site.

[&]quot;Daytime" = 7:00 a.m. to 10:00 p.m.; "Nighttime" = 10:00 p.m. to 7:00 a.m.

³ Entry Gate & Truck Movements are calculate based on the number of events by time of day (See Table 7-2).

TABLE 7-2: ENTRY GATE & TRUCK MOVEMENTS BY LOCATION

Entry Gate	Total	Trip	Dist. ³		Time of	Day Vehicl	e Splits ⁵	Truc	ck Moveme	ents ⁶
& Truck Movement Location ¹	Project Truck Trips ²	In	Out	Truck Trips by Location ⁴	Day	Evening	Night	Day	Evening	Night
Dwy. 1	199	100%	100%	199	86.50%	2.70%	10.80%	172	5	21

¹ Driveway location as shown on Exhibit 7-A.

7.2.4 ROOF-TOP AIR CONDITIONING UNITS

To assess the noise levels created by the roof-top air conditioning units, reference noise level measurements were collected from a Lennox SCA120 series 10-ton model packaged air conditioning unit. At the uniform reference distance of 50 feet, the reference noise levels are 57.2 dBA L_{eq}. Based on the typical operating conditions observed over a four-day measurement period, the roof-top air conditioning units are estimated to operate for an average of 39 minutes per hour during the daytime hours, and 28 minutes per hour during the nighttime hours. For this noise analysis, the air conditioning units are expected to be located on the roof of the proposed building. This reference noise level describes the expected roof-top air conditioning units located 5 feet above the roof for the planned air conditioning units at the Project site.

7.2.5 Trash Enclosure Activity

To describe the noise levels associated with a trash enclosure activity, Urban Crossroads collected a reference noise level measurement at an existing trash enclosure containing two dumpster bins. The trash enclosure noise levels describe metal gates opening and closing, metal scraping against concrete floor sounds, dumpster movement on metal wheels, and trash dropping into the metal dumpster. The reference noise levels describe trash enclosure noise activities when trash is dropped into an empty metal dumpster, as would occur at the Project site. The measured reference noise level at the uniform 50-foot reference distance is 56.8 dBA L_{eq} for the trash enclosure activity. The reference noise level describes the expected noise source activities associated with the trash enclosures for the Project's proposed building. Typical trash enclosure activities are estimated to occur for 5 minutes per hour.

7.3 CADNAA NOISE PREDICTION MODEL

To fully describe the exterior operational noise levels from the Project, Urban Crossroads, Inc. developed a noise prediction model using the CadnaA (Computer Aided Noise Abatement) computer program. CadnaA can analyze multiple types of noise sources using the spatially accurate Project site plan, georeferenced Nearmap aerial imagery, topography, buildings, and barriers in its calculations to predict outdoor noise levels.



² Total Project truck trips according to Table 3 Perris Truck Yard Trip Generation & Scoping Memorandum, Urban Crossroads, Inc.

³ Project truck trip distribution according to the Perris Truck Yard Trip Generation & Scoping Memorandum, Urban Crossroads, Inc.

⁴ Calculated trip trucks per location represents the product of the total (inbound and outbound) project truck trips and the trip distribution.

⁵ Heavy truck time of day vehicle splits (typical Southern California vehicle mix).

[&]quot;Daytime" = 7:00 a.m. to 7:00 p.m.; "Evening" = 7:00 p.m. to 10:00 p.m.; "Nighttime" = 10:00 p.m. to 7:00 a.m.

⁶ Calculated time of day entry gate and truck movements by location.

Using the ISO 9613 protocol, CadnaA will calculate the distance from each noise source to the noise receiver locations, using the ground absorption, distance, and barrier/building attenuation inputs to provide a summary of noise level at each receiver and the partial noise level contributions by noise source. Consistent with the ISO 9613 protocol, the CadnaA noise prediction model relies on the reference sound power level (PWL) to describe individual noise sources. While sound pressure levels (e.g. Leq) quantify in decibels the intensity of given sound sources at a reference distance, sound power levels (PWL) are connected to the sound source and are independent of distance. Sound pressure levels vary substantially with distance from the source and diminish from intervening obstacles and barriers, air absorption, wind, and other factors. Sound power is the acoustical energy emitted by the sound source and is an absolute value that is not affected by the environment.

The operational noise level calculations provided in this noise study account for the distance attenuation provided due to geometric spreading, when sound from a localized stationary source (i.e., a point source) propagates uniformly outward in a spherical pattern. A default ground attenuation factor of 0.5 was used in the noise analysis to account for mixed ground representing a combination of hard and soft surfaces. Appendix 7.1 includes the detailed noise model inputs.

7.4 Project Operational Noise Levels

Using the reference noise levels to represent the proposed Project operations that include truck terminal activity, entry gate & truck movements, roof-top air conditioning units, and trash enclosure activity, Urban Crossroads, Inc. calculated the operational source noise levels that are expected to be generated at the Project site and the Project-related noise level increases that would be experienced at each of the sensitive receiver locations. Table 7-3 shows the Project operational noise levels during the daytime hours of 7:00 a.m. to 10:00 p.m. The daytime hourly noise levels at the off-site receiver locations are expected to range from 49.0 to 59.8 dBA L_{max}.

Table 7-4 shows the Project operational noise levels during the nighttime hours of 10:00 p.m. to 7:00 a.m. The nighttime hourly noise levels at the off-site receiver locations are expected to range from 49.0 to 59.8 dBA L_{max} . The differences between the daytime and nighttime noise levels is largely related to the duration of noise activity (Table 7-1) and the number of Entry Gate & Truck Movements (Table 7-2).

TABLE 7-3: DAYTIME PROJECT OPERATIONAL NOISE LEVELS

Noise Source ¹	Operational Noise Levels by Receiver Location (dBA L _{max})					
Noise Source	R1	R2	R3			
Truck Terminal Activity	59.8	55.8	49.0			
Entry Gate & Truck Movements	30.4	26.7	23.5			
Roof-Top Air Conditioning Units	22.2	19.6	14.8			
Trash Enclosure Activity	33.0	30.2	21.2			
Total (All Noise Sources)	59.8	55.8	49.0			

¹ See Exhibit 7-A for the noise source locations. CadnaA noise model calculations are included in Appendix 7.1.



TABLE 7-4: NIGHTTIME PROJECT OPERATIONAL NOISE LEVELS

Noise Source ¹	Operational Noise Levels by Receiver Location (dBA L _{max})					
Noise Source	R1	R2	R3			
Truck Terminal Activity	59.8	55.8	49.0			
Entry Gate & Truck Movements	21.3	17.6	14.3			
Roof-Top Air Conditioning Units	19.8	17.2	12.4			
Trash Enclosure Activity	32.0	29.2	20.2			
Total (All Noise Sources)	59.8	55.8	49.0			

¹ See Exhibit 7-A for the noise source locations. CadnaA noise model calculations are included in Appendix 7.1.

7.5 Project Operational Noise Level Compliance

To demonstrate compliance with local noise regulations, the Project-only operational noise levels are evaluated against exterior noise level thresholds based on the City of Perris exterior noise level standards at nearest noise-sensitive receiver locations. Table 7-5 shows the operational noise levels associated with Perris Truck Yard Project will satisfy the City of Perris exterior noise level standards at all nearby receiver locations. Therefore, the operational noise impacts are considered *less than significant* at the nearest noise-sensitive receiver locations.

TABLE 7-5: OPERATIONAL NOISE LEVEL COMPLIANCE

Receiver Location ¹	Project Operational Noise Levels (dBA L _{max}) ²			l Standards L _{max}) ³	Noise Level Standards Exceeded? ⁴		
Location	Daytime	Nighttime	Daytime	Nighttime	Daytime	Nighttime	
R1	59.8	59.8	80.0	60.0	No	No	
R2	55.8	55.8	80.0	60.0	No	No	
R3	49.0	49.0	80.0	60.0	No	No	

 $^{^{\}mbox{\tiny 1}}$ See Exhibit 6-A for the receiver locations.

Consistent with the City of Perris General Plan Noise Element, Implementation Measure V.A.1, Project operational noise levels at nearest sensitive receiver locations cannot exceed 60 dBA CNEL. The CNEL metric is typically used to describe 24-hour transportation-related noise levels. Table 7-6 includes the evening and nighttime adjustments made to the operational noise levels during the applicable hours to convert the worst-case hourly operational noise levels (Leq) to 24-hour CNELs.

Table 7-6 indicates that the 24-hour noise levels associated with the Perris Truck Yard at the nearest sensitive receiver locations are expected to range from 47.4 to 58.2 dBA CNEL. The Project-related operational noise levels shown on Table 7-6 will satisfy the City of Perris 60 dBA CNEL exterior noise level standards at the nearest sensitive receiver locations.



² Proposed Project operational noise levels as shown on Tables 7-3 and 7-4.

³ Exterior noise level standards per the City of Perris Municipal Code, sections 7.34.040 (Appendix 3.1).

⁴ Do the estimated Project operational noise source activities exceed the noise level standards?

[&]quot;Daytime" = 7:00 a.m. to 10:00 p.m.; "Nighttime" = 10:00 p.m. to 7:00 a.m.

TABLE 7-6: OPERATIONAL NOISE LEVEL COMPLIANCE (CNEL)

	Project	Operational Noise	Exterior Noise	Noise Level		
Receiver Location ¹	Daytime (dBA L _{eq})	Nighttime (dBA L _{eq})	24-Hour (CNEL)	Level Standards (CNEL) ³	Standards Exceeded? ⁴	
R1	51.5	51.5	58.2	60	No	
R2	47.5	47.4	54.1	60	No	
R3	40.8	40.7	47.4	60	No	

¹ See Exhibit 6-A for the receiver locations.

7.6 Project Operational Noise Level Increases

To describe the Project operational noise level increases, the Project operational noise levels are combined with the existing ambient noise levels measurements for the nearest receiver locations potentially impacted by Project operational noise sources. Since the units used to measure noise, decibels (dB), are logarithmic units, the Project-operational and existing ambient noise levels cannot be combined using standard arithmetic equations. (2) Instead, they must be logarithmically added using the following base equation:

$$\mathsf{SPL}_{\mathsf{Total}} = \mathsf{10log}_{\mathsf{10}} [\mathsf{10}^{\mathsf{SPL1/10}} + \mathsf{10}^{\mathsf{SPL2/10}} + ... \ \mathsf{10}^{\mathsf{SPLn/10}}]$$

Where "SPL1," "SPL2," etc. are equal to the sound pressure levels being combined, or in this case, the Project-operational and existing ambient noise levels. The difference between the combined Project and ambient noise levels describe the Project noise level increases to the existing ambient noise environment. As indicated on Tables 7-7 and 7-8, the Project will generate daytime and nighttime operational noise level increases ranging from 0.1 to 3.1 dBA L_{eq} at the nearest receiver locations. Project-related operational noise level increases will satisfy the operational noise level increase significance criteria presented on Table 4-1. Therefore, the incremental Project operational noise level increase is considered *less than significant* at all receiver locations.



² Proposed Project operational noise level calculations are included in Appendix 7.2.

³ City of Perris General Plan Noise Element Implementation Measure V.A.1

⁴ Do the estimated Project operational noise source activities exceed the noise level standards?

[&]quot;Daytime" = 7:01 a.m. to 10:00 p.m.; "Nighttime" = 10:01 p.m. to 7:00 a.m.

TABLE 7-7: DAYTIME PROJECT OPERATIONAL NOISE LEVEL INCREASES

Receiver Location ¹	Total Project Operational Noise Level ²	Measurement Location ³	Reference Ambient Noise Levels ⁴	Combined Project and Ambient ⁵	Project Increase ⁶	Noise Sensitive Land Use?	Increase Criteria ⁷	Increase Criteria Exceeded? ⁷
R1	51.5	L1	60.9	61.4	0.5	Yes	3	No
R2	47.5	L2	50.5	52.3	1.8	Yes	5	No
R3	40.8	L3	56.7	56.8	0.1	Yes	5	No

¹ See Exhibit 6-A for the receiver locations.

TABLE 7-8: NIGHTTIME OPERATIONAL NOISE LEVEL INCREASES

Receiver Location ¹	Total Project Operational Noise Level ²	Measurement Location ³	Reference Ambient Noise Levels ⁴	Combined Project and Ambient ⁵	Project Increase ⁶	Noise Sensitive Land Use?	Increase Criteria ⁷	Increase Criteria Exceeded? ⁷
R1	51.5	L1	60.5	61.0	0.5	Yes	3	No
R2	47.5	L2	47.3	50.4	3.1	Yes	5	No
R3	40.8	L3	55.6	55.7	0.1	Yes	5	No

¹ See Exhibit 6-A for the receiver locations.



² Total Project daytime operational noise levels as shown on Table 7-6.

³ Reference noise level measurement locations as shown on Exhibit 5-A.

⁴ Observed daytime ambient noise levels as shown on Table 5-1.

⁵ Represents the combined ambient conditions plus the Project activities.

⁶ The noise level increase expected with the addition of the proposed Project activities.

⁷ Significance increase criteria as shown on Table 4-1.

² Total Project nighttime operational noise levels as shown on Table 7-6.

³ Reference noise level measurement locations as shown on Exhibit 5-A.

⁴ Observed nighttime ambient noise levels as shown on Table 5-1.

⁵ Represents the combined ambient conditions plus the Project activities.

⁶ The noise level increase expected with the addition of the proposed Project activities.

⁷ Significance increase criteria as shown on Table 4-1.

8 CONSTRUCTION IMPACTS

This section analyzes potential impacts resulting from the short-term construction activities associated with the development of the Project. Exhibit 8-A shows the construction noise source locations in relation to the nearest sensitive receiver locations previously described in Section 8.

8.1 Construction Noise Levels

Noise generated by the Project construction equipment will include a combination of trucks, power tools, concrete mixers, and portable generators operating simultaneously that when combined can reach high levels. The number and mix of construction equipment are expected to occur in the following stages:

- Site Preparation
- Grading
- Building Construction
- Paving
- Architectural Coating

8.2 Typical Construction Reference Noise Levels

This construction noise analysis was prepared using reference construction equipment noise levels from the Federal Highway Administration (FHWA) published the Roadway Construction Noise Model (RCNM), which includes a national database of construction equipment reference noise emission levels. (17) The RCNM equipment database, provides a comprehensive list of the noise generating characteristics for specific types of construction equipment including reference L_{max} noise levels measured at 50 feet.

Noise levels generated by heavy construction equipment can range from approximately 68 dBA to more than 85 dBA L_{max} when measured at 50 feet. However, these noise levels diminish with distance from the construction site at a rate of 6 dBA per doubling of distance. For example, a noise level of 85 dBA L_{max} measured at 50 feet from the noise source to the receiver would be reduced to 79 dBA L_{max} at 100 feet from the source to the receiver, and would be further reduced to 73 dBA L_{max} at 200 feet from the source to the receiver. Table 8-1 provides a summary of the construction reference noise levels expected with the Project construction activities.



ASON CT HARLEY KNOX BLVD NANCE ST ⊕R1 MARKHAM ST JOHNSON AVE PERRY ST ribiotica

EXHIBIT 8-A: Typical Construction Noise Source Locations





Construction Activity



Receiver Locations

Distance from receiver to Project site boundary (in feet)



TABLE 8-1: TYPICAL CONSTRUCTION REFERENCE NOISE LEVELS

Construction Stage	Construction Activity	Reference Noise Level @ 50 Feet (dBA L _{max}) ¹	Highest Reference Noise Level (dBA L _{max})	
Site	Crawler Tractors	82	82	
Preparation	Rubber Tired Dozers	79	02	
	Crawler Tractors	82		
	Excavators	81		
Grading	Graders	85	85	
	Rubber Tired Dozers	79		
	Graders	85		
	Cranes	81		
	Crawler Tractors	82		
Building Construction	Rubber Tired Dozers	79	82	
Construction	Generator Sets	73		
	Welders	74		
	Pavers	77		
Paving	Hauling Trucks	76	80	
	Rollers	80		
Arch. Coating	Air Compressors	78	78	

¹ FHWA's Roadway Construction Noise Model, January 2006.

8.3 Typical Construction Noise Analysis

Using the reference RCNM L_{max} construction equipment noise levels and the CadnaA noise prediction model, calculations of the Project construction noise level impacts with multiple pieces of equipment operating simultaneously at the nearest receiver locations were completed. To assess the worst-case construction noise levels, the Project construction noise analysis relies on the highest noise level impacts when the equipment with the highest reference noise level is operating at the closest point from the edge of primary construction activity (Project site boundary) to each receiver location.

As shown on Table 8-2, the construction noise levels are expected to range from 54.6 to 72.1 dBA L_{max} , and the highest construction levels are expected to range from 61.6 to 72.1 dBA L_{max} at the nearby receiver locations. Appendix 8.1 includes the detailed CadnaA construction noise model inputs.



TABLE 8-2: TYPICAL CONSTRUCTION EQUIPMENT NOISE LEVEL SUMMARY

	Construction Noise Levels (dBA L _{max})							
Receiver Location ¹	Site Preparation	Grading	Building Construction	Paving	Arch. Coating	Highest Levels ²		
R1	69.1	72.1	69.1	67.1	65.1	72.1		
R2	65.1	68.1	65.1	63.1	61.1	68.1		
R3	58.6	61.6	58.6	56.6	54.6	61.6		

¹ Noise receiver locations are shown on Exhibit 8-A.

8.4 Typical Construction Noise Level Compliance

To evaluate whether the Project will generate potentially significant short-term noise levels at nearest noise sensitive receiver locations, a construction-related daytime noise level threshold of 80 dBA L_{max} is used as a reasonable threshold to assess the daytime construction noise level impacts. The construction noise analysis shows that the nearest receiver locations will satisfy the daytime 80 dBA L_{max} significance threshold during Project construction activities as shown on Table 8-3. Therefore, the noise impacts due to Project construction noise is considered *less than significant* at all receiver locations.

TABLE 8-3: TYPICAL CONSTRUCTION NOISE LEVEL COMPLIANCE

		Construction Noise Levels (dBA L _{max})					
Receiver Location ¹	Land Use	Highest Construction Noise Levels ² Threshold ³		Threshold Exceeded? ⁴			
R1	Residential	72.1	80	No			
R2	Residential	68.1 80		No			
R3	Residential	61.6	80	No			

¹ Noise receiver locations are shown on Exhibit 8-A.

8.6 Typical Construction Vibration Impacts

Construction activity can result in varying degrees of ground vibration, depending on the equipment and methods used, distance to the affected structures and soil type. It is expected that ground-borne vibration from Project construction activities would cause only intermittent, localized intrusion. Ground-borne vibration levels resulting from typical construction activities occurring within the Project site were estimated by data published by the Federal Transit Administration (FTA). (7) However, while vehicular traffic is rarely perceptible, construction has the potential to result in varying degrees of temporary ground vibration, depending on the specific construction activities and equipment used. Ground vibration levels associated with



² Construction noise level calculations based on distance from the project site boundaries (construction activity area) to nearby receiver locations. CadnaA construction noise model inputs are included in Appendix 8.1.

² Highest construction noise level calculations based on distance from the construction noise source activity to nearby receiver locations as shown on Table 8-2.

³ Construction noise level thresholds are limited to the noise sensitive receiver locations (Section 3.5).

⁴ Do the estimated Project construction noise levels exceed the construction noise level threshold?

various types of construction equipment are summarized on Table 8-4. Based on the representative vibration levels presented for various construction equipment types, it is possible to estimate the potential Project construction vibration levels using the following vibration assessment methods defined by the FTA. To describe the human response (annoyance) associated with vibration impacts the FTA provides the following equation: $L_{VdB}(D) = L_{VdB}(25 \text{ ft}) - 30\log(D/25)$

TABLE 8-4: VIBRATION SOURCE LEVELS FOR CONSTRUCTION EQUIPMENT

Equipment	Vibration Decibels (VdB) at 25 feet
Small bulldozer	58
Jackhammer	79
Loaded Trucks	86
Large bulldozer	87

Source: Federal Transit Administration, Transit Noise and Vibration Impact Assessment Manual.

Table 8-5 presents the expected typical construction equipment vibration levels at the nearby receiver locations. At distances ranging from 389 feet to 1,854 feet from typical Project construction activities (at the Project site boundary), construction vibration levels are estimated to range from 30.9 to 51.2 VdB and will satisfy the FTA *Transit Noise and Vibration Impact Assessment* vibration criteria at all receiver locations. Therefore, the vibration impacts due to Project construction is considered *less than significant* at all receiver locations.

Further, vibration levels at the site of the closest sensitive receiver are unlikely to be sustained during the entire construction period but will occur rather only during the times that heavy construction equipment is operating simultaneously adjacent to the Project site perimeter.

TABLE 8-5: TYPICAL CONSTRUCTION EQUIPMENT VIBRATION LEVELS

		Distance to	Receiver Vibration Levels (VdB) ²						
Receiver Location ¹	Land Use	Construction Activity (Feet)	Small Bulldozer	Jack- hammer	Loaded Trucks	Large Bulldozer	Highest Vibration Levels	Threshold VdB ³	Threshold Exceeded? ⁴
R1	Residential	389'	22.2	43.2	50.2	51.2	51.2	78	No
R2	Residential	786'	13.1	34.1	41.1	42.1	42.1	78	No
R3	Residential	1,854'	1.9	22.9	29.9	30.9	30.9	78	No

¹ Noise receiver locations are shown on Exhibit 8-A.



² Based on the Vibration Source Levels of Construction Equipment included on Table 8-4.

³ FTA Transit Noise and Vibration Impact Assessment Manual maximum acceptable vibration criteria as shown on Table 4-1.

⁴ Does the vibration level exceed the maximum acceptable vibration threshold?



9 REFERENCES

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- 3. Environmental Protection Agency Office of Noise Abatement and Control. Information on Levels of Environmental Noise Requisite to Protect Public Health and Welfare with an Adequate Margin of Safety. March 1974. EPA/ONAC 550/9/74-004.
- 4. U.S. Department of Transportation, Federal Highway Administration, Office of Environment and Planning, Noise and Air Quality Branch. Highway Traffic Noise Analysis and Abatement Policy and Guidance. December 2011.
- 5. **U.S. Department of Transportation, Federal Highway Administration.** *Highway Traffic Noise in the United States, Problem and Response.* April 2000. p. 3.
- 6. **U.S. Environmental Protection Agency Office of Noise Abatement and Control.** *Noise Effects Handbook-A Desk Reference to Health and Welfare Effects of Noise.* October 1979 (revised July 1981). EPA 550/9/82/106.
- 7. **U.S. Department of Transportation, Federal Transit Administration.** *Transit Noise and Vibration Impact Assessment Manual.* September 2018.
- 8. Office of Planning and Research. State of California General Plan Guidelines. 2019.
- 9. State of California. 2016 California Green Building Standards Code. August 2019 Supplement.
- 10. City of Perris. General Plan Noise Element. August 2005.
- 11. . Municipal Code, Chapter 7.34 Noise Control.
- 12. **Riverside County Airport Land Use Commission.** *March Air Reserve Base/Inland Port Airport Land Use Compatibility Plan.* November 2014.
- 13. California Court of Appeal. *Gray v. County of Madera, F053661.* 167 Cal.App.4th 1099; Cal.Rptr.3d, October 2008.
- 14. City of Perris. Perris Valley Commerce Center Specific Plan Environmental Impact Report. July 2011.
- 15. American National Standards Institute (ANSI). Specification for Sound Level Meters ANSI S1.4-2014/IEC 61672-1:2013.
- 16. **Urban Crossroads, Inc.** Perris Truck Yard Trip Generation & Scoping Memorandum. July 2020.
- 17. U.S. Department of Transportation, Federal Highway Administration, Office of Environment and Planning. FHWA Roadway Construction Noise Model. January, 2006.





10 CERTIFICATION

The contents of this noise study report represent an accurate depiction of the noise environment and impacts associated with the proposed Perris Truck Yard Project. The information contained in this noise study report is based on the best available data at the time of preparation. If you have any questions, please contact me directly at (949) 336-5979.

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EDUCATION

Master of Science in Civil and Environmental Engineering California Polytechnic State University, San Luis Obispo • December, 1993

Bachelor of Science in City and Regional Planning California Polytechnic State University, San Luis Obispo • June, 1992

PROFESSIONAL REGISTRATIONS

PE – Registered Professional Traffic Engineer – TR 2537 • January, 2009

AICP – American Institute of Certified Planners – 013011 • June, 1997–January 1, 2012

PTP – Professional Transportation Planner • May, 2007 – May, 2013

INCE – Institute of Noise Control Engineering • March, 2004

PROFESSIONAL AFFILIATIONS

ASA – Acoustical Society of America ITE – Institute of Transportation Engineers

PROFESSIONAL CERTIFICATIONS

Certified Acoustical Consultant – County of Orange • February, 2011 FHWA-NHI-142051 Highway Traffic Noise Certificate of Training • February, 2013





APPENDIX 3.1:

CITY OF PERRIS MUNICIPAL CODE





Sec. 7.34.010. - Declaration of policy.

Excessive noise levels are detrimental to the health and safety of individuals. Noise is considered a public nuisance, and the city discourages unnecessary, excessive or annoying noises from all sources. Creating, maintaining, causing, or allowing to be created, caused or maintained, any noise or vibration in a manner prohibited by the provisions of the ordinance codified in this chapter is a public nuisance and shall be punishable as a misdemeanor.

(Code 1972, § 7.34.010; Ord. No. 1082, § 2(part), 2000)

Sec. 7.34.020. - Definitions.

(a) *General.* The following words, terms and phrases, when used in this chapter, shall have the meanings ascribed to them in this section, except where the context clearly indicates a different meaning:

Ambient noise means the all-encompassing noise associated with a given environment usually being composed of sounds from many sources near and far. For the purpose of this chapter, ambient noise level is the level obtained when the noise level is averaged over a period of five minutes without inclusion of noise from isolated identifiable sources at the location and time of day near that at which a comparison is to be made.

Decibel (dB) means an intensity unit which denotes the ratio between two quantities which are proportional to power; the number of decibels corresponding to the ratio is ten times the common logarithm of this ratio.

Sound amplifying equipment means any machine or device for the amplification of the human voice, music or any other sound. The term "sound amplifying equipment" does not include standard vehicle radios when used and heard only by the occupants of the vehicle in which the vehicle radio is installed. The term "sound amplifying equipment," as used in this chapter, does not include warning devices on any vehicle used only for traffic safety purposes and shall not include communications equipment used by public or private utilities when restoring utility service following a public emergency or when doing work required to protect person or property from an imminent exposure to danger.

Sound level (noise level) in decibels is the value of a sound measurement using the "A" weighting network of a sound level meter. Slow response of the sound level meter needle shall be used except where the sound is impulsive or rapidly varying in nature, in which case, fast response shall be used.

Sound level meter means an instrument, including a microphone, an amplifier, an output meter and frequency weighting networks, for the measurement of sound levels, which satisfies the pertinent requirements in American National Standards Institute's specification S1.4-1971 or the most recent revision for type S-2A general purpose sound level meters.

(b) Supplementary definitions of technical terms. Definitions of technical terms not defined in this section shall be obtained from the American National Standards Institute's Acoustical Terminology S1-1971 or the most recent revision thereof.

(Code 1972, § 7.34.020; Ord. No. 1082, § 2(part), 2000)

Sec. 7.34.030. - Measurement methods.

- (a) Sound shall be measured with a sound level meter as defined in section 7.34.020.
- (b) Unless otherwise provided, outdoor measurements shall be taken with the microphone located at any point

- on the property line of the noise source but no closer than five feet from any wall or vertical obstruction and three to five feet above ground level whenever possible.
- (c) Unless otherwise provided, indoor measurements shall be taken inside the structure with the microphone located at any point as follows:
 - (1) No less than three feet above floor level;
 - (2) No less than five feet from any wall or vertical obstruction; and
 - (3) Not under common possession and control with the building or portion of the building from which the sound is emanating.

(Code 1972, § 7.34.030; Ord. No. 1082, § 2(part), 2000)

Sec. 7.34.040. - Sound amplification.

No person shall amplify sound using sound amplifying equipment contrary to any of the following:

- (1) The only amplified sound permitted shall be either music or the human voice, or both.
- (2) The volume of amplified sound shall not exceed the noise levels set forth in this subsection when measured outdoors at or beyond the property line of the property from which the sound emanates.

Time Period	Maximum Noise Level
10:01 p.m.—7:00 a.m.	60 dBA
7:01 a.m.—10:00 p.m.	80 dBA

(Code 1972, § 7.34.040; Ord. No. 1082, § 2(part), 2000)

Sec. 7.34.050. - General prohibition.

- (a) It unlawful for any person to willfully make, cause or suffer, or permit to be made or caused, any loud excessive or offensive noises or sounds which unreasonably disturb the peace and quiet of any residential neighborhood or which are physically annoying to persons of ordinary sensitivity or which are so harsh, prolonged or unnatural or unusual in their use, time or place as to occasion physical discomfort to the inhabitants of the city, or any section thereof. The standards for dBA noise level in section 7.34.040 shall apply to this section. To the extent that the noise created causes the noise level at the property line to exceed the ambient noise level by more than 1.0 decibels, it shall be presumed that the noise being created also is in violation of this section.
- (b) The characteristics and conditions which should be considered in determining whether a violation of the provisions of this section exists should include, but not be limited to, the following:
 - (1) The level of the noise;
 - (2) Whether the nature of the noise is usual or unusual;
 - (3) Whether the origin of the noise is natural or unnatural;
 - (4) The level of the ambient noise;
 - (5) The proximity of the noise to sleeping facilities;

- (6) The nature and zoning of the area from which the noise emanates and the area where it is received;
- (7) The time of day or night the noise occurs;
- (8) The duration of the noise; and
- (9) Whether the noise is recurrent, intermittent or constant.

(Code 1972, § 7.34.050; Ord. No. 1082, § 2(part), 2000)

Sec. 7.34.060. - Construction noise.

It is unlawful for any person between the hours of 7:00 p.m. of any day and 7:00 a.m. of the following day, or on a legal holiday, with the exception of Columbus Day and Washington's birthday, or on Sundays to erect, construct, demolish, excavate, alter or repair any building or structure in such a manner as to create disturbing, excessive or offensive noise. Construction activity shall not exceed 80 dBA in residential zones in the city.

(Code 1972, § 7.34.060; Ord. No. 1082, § 2(part), 2000)

Sec. 7.34.070. - Refuse vehicles and parking lot sweepers.

No person shall operate or permit to be operated a refuse compacting, processing or collection vehicle or parking lot sweeper between the hours of 7:00 p.m. to 7:00 a.m. in any residential area unless a permit has been applied for and granted by the city.

(Code 1972, § 7.34.070; Ord. No. 1082, § 2(part), 2000)

Sec. 7.34.080. - Disturbing, excessive, offensive noises; declaration of certain acts constituting.

The following activities, among others, are declared to cause loud, disturbing, excessive or offensive noises in violation of this section and are unlawful, namely:

- (1) *Horns, signaling devices, etc.* Unnecessary use or operation of horns, signaling devices or other similar devices on automobiles, motorcycles or any other vehicle.
- (2) Radios, television sets, phonographs, loud speaking amplifiers and similar devices. The use or operation of any sound production or reproduction device, radio receiving set, musical instrument, drums, phonograph, television set, loudspeakers, sound amplifier, or other similar machine or device for the producing or reproducing of sound, in such a manner as to disturb the peace, quiet or comfort of any reasonable person of normal sensitivity in any area of the city is prohibited. This provision shall not apply to any participant in a licensed parade or to any person who has been otherwise duly authorized by the city to engage in such conduct.

(3) Animals.

- a. The keeping or maintenance, or the permitting to be kept or maintained, upon any premises owned, occupied or controlled by any person of any animal or animals which by any frequent or long-continued noise shall cause annoyance or discomfort to a reasonable person of normal sensitiveness in the vicinity.
- b. The noise from any such animal or animals that disturbs two or more residents residing in separate residences adjacent to any part of the property on which the subject animal or animals are kept or maintained, or three or more residents residing in separate residences in close proximity to the

property on which the subject animal or animals are kept or maintained, shall be prima facie evidence of a violation of this section.

- (4) Hospitals, schools, libraries, rest homes, long-term medical or mental care facilities. To make loud, disturbing, excessive noises adjacent to a hospital, school, library, rest home or long-term medical or mental care facility, which noise unreasonably interferes with the workings of such institutions or which disturbs or unduly annoys occupants in said institutions.
- (5) Playing of radios on buses and trolleys. The operation of any radio, phonograph or tape player on an urban transit bus or trolley so as to emit noise that is audible to any other person in the vehicle is prohibited.
- (6) Playing of radios, phonographs and other sound production or reproduction devices in public parks and public parking lots and streets adjacent thereto. The operation of any radio, phonograph, television set or any other sound production or reproduction device in any public park or any public parking lot, or street adjacent to such park or beach, without the prior written approval of the city manager or the administrator, in such a manner that such radio, phonograph, television set or sound production or reproduction device emits a sound level exceeding those found in the table in section 7.34.040.

(7) Leaf blowers.

- a. The term "leaf blower" means any portable, hand-held or backpack, engine-powered device with a nozzle that creates a directable airstream which is capable of and intended for moving leaves and light materials.
- b. No person shall operate a leaf blower in any residential zoned area between the hours of 7:00 p.m. and 8:00 a.m. on weekdays and 5:00 p.m. and 9:00 a.m. on weekends or on legal holidays.
- c. No person may operate any leaf blower at a sound level in excess of 80 decibels measured at a distance of 50 feet or greater from the point of noise origin.
- d. Leaf blowers shall be equipped with functional mufflers and an approved sound limiting device required to ensure that the leaf blower is not capable of generating a sound level exceeding any limit prescribed in this section.

(Code 1972, § 7.34.080; Ord. No. 1082, § 2(part), 2000)

Sec. 7.34.090. - Burglar alarms.

- (a) Audible burglar alarms for structures or motor vehicles are prohibited unless the operation of such burglar alarm can be terminated within 20 minutes of being activated.
- (b) Notwithstanding the requirements of this provision, any member of the county sheriff's department, Perris Division, shall have the right to take such steps as may be reasonable and necessary to disconnect any such alarm installed in any building, dwelling or motor vehicle at any time during the period of its activation. On or after 30 days from the effective date of the ordinance codified in this chapter, any building, dwelling or motor vehicle upon which a burglar alarm has been installed shall prominently display the telephone number at which communication may be made with the owner of such building, dwelling or motor vehicle.

(Code 1972, § 7.34.090; Ord. No. 1082, § 2(part), 2000)

Sec. 7.34.100. - Motor vehicles.

- (a) Off-highway.
 - (1) Except as otherwise provided for in this chapter, it shall be unlawful to operate any motor vehicle of any

type on any site, other than on a public street or highway as defined in the California Vehicle Code, in any manner so as to cause noise in excess of those noise levels permitted for on-highway motor vehicles as specified in the table for "45-mile-per-hour or less speed limits" contained in section 23130 of the California Vehicle Code and as corrected for distances set forth in subsection (a)(2) of this section.

(2) The maximum noise level as the on-highway vehicle passes may be measured at a distance of other than 50 feet from the centerline of travel, provided the measurement is further adjusted by adding algebraically the application correction as follows:

Distance (feet)	Correction (decibels)
25	-6
28	-5
32	-4
35	-3
40	-2
45	-1
50 (preferred distance)	0
56	+1
63	+2
70	+3
80	+4
90	+5
100	+6

(Code 1972, § 7.34.100; Ord. No. 1082, § 2(part), 2000)

⁽b) Nothing in this section shall apply to authorized emergency vehicles when being used in emergency situations including the blowing of sirens and/or horns.



APPENDIX 5.1:

STUDY AREA PHOTOS





JN: 12915 Study Area Photos



L1_E 33, 51' 19.580000", 117, 13' 31.260000"



L1_N 33, 51' 19.580000", 117, 13' 31.260000"



L1_S 33, 51' 19.590000", 117, 13' 31.260000"



L1_W 33, 51' 19.590000", 117, 13' 31.230000"



L2_E 33, 51' 22.450000", 117, 13' 18.290000"



L2_N 33, 51' 24.230000", 117, 13' 18.100000"

JN: 12915 Study Area Photos



L2_S 33, 51' 22.450000", 117, 13' 18.290000"



L2_W 33, 51' 22.570000", 117, 13' 18.180000"



L3_E 33, 50' 52.510000", 117, 13' 36.970000"



L3_N



_3_S ,



L3_W 33, 50' 54.020000", 117, 13' 38.890000"

APPENDIX 5.2:

NOISE LEVEL MEASUREMENT WORKSHEETS





24-Hour Noise Level Measurement Summary

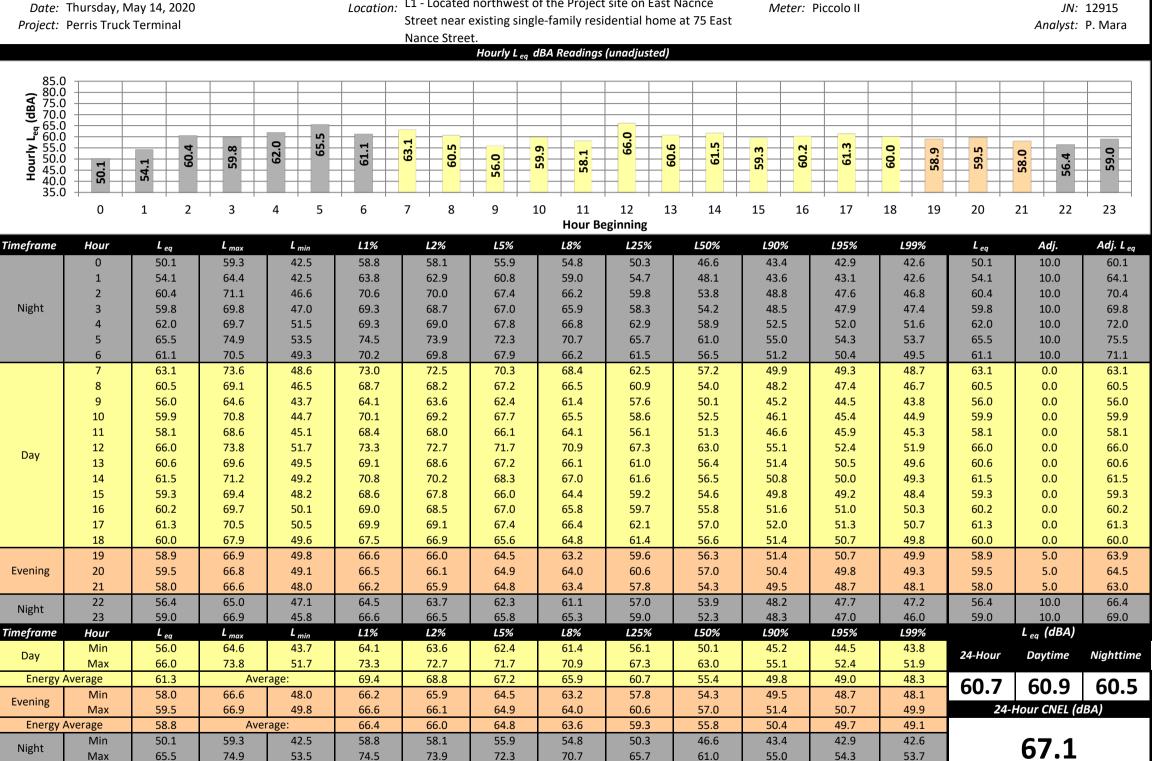
L1 - Located northwest of the Project site on East Nacnce Location: Date: Thursday, May 14, 2020

67.5

66.9

65.2

Meter: Piccolo II





64.0

58.8

53.9

48.8

48.1

47.5

Average:

60.5

Energy Average

24-Hour Noise Level Measurement Summary

L2 - Located northeast of the Project site on Las Palmas near Location: Date: Thursday, May 14, 2020

51.7

51.3

50.1

Meter: Piccolo II

JN: 12915 existing single-family residential home at 220 East Nance Project: Perris Truck Terminal Analyst: P. Mara Street. Hourly L_{ea} dBA Readings (unadjusted) 80.0 75.0 80.0 75.0 70.0 65.0 60.0 Hourly 155.0 55.0 45.0 45.0 40.0 0 47.0 20. 50. 40.0 35.0 3 5 7 8 10 13 20 23 0 1 2 Δ 6 9 11 12 15 17 18 19 21 22 14 16 **Hour Beginning Timeframe** L1% L2% L5% L8% L25% L50% L90% L95% L99% Adj. Adj. L ea Hour L_{eq} L max L min L_{eq} 46.0 45.7 44.8 0 43.1 46.3 41.2 45.2 43.6 42.8 41.7 41.5 41.3 43.1 10.0 53.1 1 43.2 47.4 41.1 47.0 46.6 45.8 45.2 43.6 42.6 41.6 41.4 41.2 43.2 10.0 53.2 2 43.6 48.5 40.4 48.1 47.8 47.2 46.5 44.4 42.7 40.9 40.7 40.5 43.6 10.0 53.6 Night 3 52.8 42.1 52.1 49.5 55.9 45.9 51.6 50.4 46.5 44.1 42.7 42.4 42.2 45.9 10.0 4 47.8 52.7 45.1 52.4 51.9 50.8 50.2 48.2 47.0 45.7 45.5 45.2 47.8 10.0 57.8 5 50.3 55.4 47.4 54.8 54.3 52.6 60.3 53.1 51.3 49.4 48.0 47.7 47.5 50.3 10.0 6 51.0 62.0 45.1 61.2 60.7 58.0 55.6 48.5 46.7 45.6 45.4 45.2 51.0 10.0 61.0 49.4 57.9 43.6 57.1 56.4 54.9 53.7 49.5 46.9 44.2 43.9 43.7 49.4 0.0 49.4 8 60.0 50.2 60.5 41.9 59.5 57.2 55.2 49.1 45.8 42.8 42.5 42.1 50.2 0.0 50.2 9 45.5 51.9 41.0 51.4 50.8 49.9 49.1 46.7 43.8 41.5 41.3 41.1 45.5 0.0 45.5 10 47.7 56.8 41.8 56.2 55.1 52.8 51.9 48.0 44.8 42.5 42.3 41.9 47.7 0.0 47.7 11 48.1 56.5 43.5 55.6 54.7 52.8 51.7 48.5 46.2 44.2 43.9 43.6 48.1 0.0 48.1 12 71.5 47.5 68.4 49.8 71.0 69.9 69.1 65.4 61.0 51.7 50.1 48.0 49.8 0.0 49.8 Day 13 55.0 63.0 47.2 62.6 62.0 59.9 59.0 55.8 52.8 49.3 48.5 47.4 55.0 0.0 55.0 14 53.0 61.8 45.4 60.4 59.3 58.2 49.2 53.0 61.1 53.4 46.3 46.0 45.5 53.0 0.0 15 54.9 48.4 55.3 44.3 54.2 52.5 51.2 48.7 47.3 45.2 44.8 44.5 48.4 0.0 48.4 16 60.1 46.5 59.4 58.5 50.5 54.3 52.8 50.2 49.0 47.3 47.0 46.6 50.5 0.0 50.5 50.8 17 50.8 56.4 47.2 55.9 55.3 54.3 53.7 51.4 49.9 48.0 47.7 47.3 0.0 50.8 18 50.4 55.9 45.8 55.7 55.2 54.4 53.7 50.9 49.4 46.7 46.3 45.9 50.4 0.0 50.4 19 55.3 46.1 54.6 47.0 5.0 55.1 50.1 55.0 53.5 52.9 51.0 49.2 46.7 46.3 50.1 **Evening** 20 50.6 57.3 45.6 57.0 56.7 45.7 55.6 55.3 54.3 51.5 48.7 46.3 46.0 50.6 5.0 21 48.7 55.9 43.5 54.7 53.6 52.6 49.4 46.7 43.6 48.7 5.0 53.7 55.3 44.2 43.9 22 50.2 42.7 10.0 45.3 49.8 49.3 48.4 47.7 45.8 44.5 43.2 43.0 42.8 45.3 55.3 Night 23 47.0 54.5 41.8 53.9 53.2 51.9 51.1 48.3 44.0 42.3 42.1 41.9 47.0 10.0 57.0 L_{eq} (dBA) L2% L25% L50% L90% L95% L99% **Timeframe** Hour L1% L5% L8% 45.5 51.9 51.4 50.8 49.9 49.1 46.7 43.8 41.5 41.3 41.1 Min 41.0 24-Hour Daytime **Nighttime** Max 55.0 71.5 47.5 71.0 69.9 69.1 68.4 65.4 61.0 51.7 50.1 48.0 50.6 58.4 57.7 55.9 54.9 51.5 48.8 45.8 45.4 44.8 **Energy Average** Average 49.5 50.5 47.3 48.7 55.0 43.9 43.6 54.6 53.5 52.6 49.4 46.7 44.2 Min 55.3 43.5 **Evening** 24-Hour CNEL (dBA) Max 50.6 57.3 46.1 57.0 56.7 55.3 54.3 51.5 49.2 47.0 46.7 46.3 55.4 54.2 53.3 50.7 49.9 Average: 55.8 48.2 45.8 45.5 45.2 **Energy Average** 43.1 46.3 40.4 46.0 45.7 45.2 44.8 43.6 42.6 40.9 40.7 40.5 Min 54.7 Night 51.0 62.0 47.4 61.2 60.7 58.0 55.6 49.4 48.0 47.7 47.5 Max 51.3



49.3

46.7

44.9

43.5

43.3

43.1

Average:

47.3

Energy Average

24-Hour Noise Level Measurement Summary

L3 - Located southwest of the Project site on Perry street Location: Date: Thursday, May 14, 2020

62.9

62.3

60.4

Meter: Piccolo II

JN: 12915 near existing single-family residential home at 77 Perry Project: Perris Truck Terminal Analyst: P. Mara Street. Hourly L_{ea} dBA Readings (unadjusted) 80.0 75.0 80.0 75.0 70.0 65.0 60.0 Hourly 155.0 55.0 45.0 45.0 40.0 6 6 9 8 ∞ 4 56. 26 22. 54. 55 53. 35.0 3 4 5 6 7 8 9 10 13 18 20 21 22 23 0 1 2 11 12 14 15 17 19 16 **Hour Beginning Timeframe** L1% L2% L5% L8% L25% L50% L90% L95% L99% Adj. Adj. L ea Hour L_{eq} L max L min L_{eq} 57.1 53.7 0 49.9 58.2 44.9 57.8 55.1 50.0 47.7 45.6 45.3 45.0 49.9 10.0 59.9 1 55.8 61.5 50.4 61.2 60.8 59.8 59.1 57.3 54.7 51.4 50.9 50.6 55.8 10.0 65.8 2 54.5 63.9 49.6 63.3 62.7 60.2 58.4 53.9 52.1 50.5 50.2 49.6 54.5 10.0 64.5 Night 3 55.1 61.6 51.5 61.3 60.9 59.3 58.2 65.1 55.3 53.8 52.2 51.9 51.6 55.1 10.0 4 56.6 66.3 50.3 65.8 65.0 62.7 60.6 55.9 53.8 51.2 50.8 50.4 56.6 10.0 66.6 5 57.6 65.2 52.0 64.7 58.1 64.1 62.1 61.1 56.0 53.2 52.7 52.2 57.6 10.0 67.6 6 57.1 64.8 50.6 64.5 64.1 62.8 61.7 57.2 54.8 51.9 51.3 50.8 57.1 10.0 67.1 60.6 69.7 49.9 69.2 68.9 66.9 65.1 61.6 55.7 52.3 51.6 50.1 60.6 0.0 60.6 8 56.9 66.7 49.3 66.2 65.5 63.0 61.1 56.4 54.0 50.7 50.1 49.5 56.9 0.0 56.9 9 54.7 61.9 48.7 61.6 61.3 60.1 58.8 52.7 49.7 49.3 48.9 0.0 54.7 55.4 54.7 10 58.0 68.3 46.1 67.6 67.0 65.6 63.3 57.5 51.9 47.6 47.0 46.3 58.0 0.0 58.0 11 53.8 62.1 46.1 61.7 61.1 59.5 58.6 54.5 50.2 47.2 46.7 46.3 53.8 0.0 53.8 12 75.0 72.7 72.0 51.0 76.4 46.7 75.5 68.8 66.2 47.8 47.3 46.8 51.0 0.0 51.0 Day 13 56.9 66.8 47.0 66.2 65.7 63.7 61.9 56.6 52.5 48.0 47.6 47.1 56.9 0.0 56.9 14 60.4 69.6 47.9 68.9 68.4 67.4 66.2 60.1 54.3 49.3 48.6 48.0 60.4 60.4 0.0 15 55.5 66.2 45.4 65.7 65.2 62.9 60.3 54.8 50.2 46.5 46.0 45.5 55.5 0.0 55.5 16 54.7 66.6 46.6 65.8 64.9 61.9 58.2 52.6 50.2 47.5 47.1 46.7 54.7 0.0 54.7 17 55.3 66.2 47.5 65.6 64.7 62.0 60.3 53.7 50.8 48.4 48.0 47.6 55.3 0.0 55.3 18 54.6 63.6 45.9 62.9 61.2 59.9 54.1 50.7 46.9 46.5 46.0 54.6 0.0 54.6 63.3 19 55.2 45.1 52.5 45.2 55.2 5.0 65.4 65.2 64.8 63.2 61.2 49.2 46.0 45.6 60.2 **Evening** 20 55.2 62.9 48.7 62.5 62.0 60.2 59.3 49.5 49.1 60.2 55.7 53.2 48.8 55.2 5.0 21 57.8 68.0 49.9 67.6 67.0 62.4 50.8 50.4 50.0 5.0 62.8 64.7 57.2 53.3 57.8 22 10.0 56.6 66.6 49.8 66.0 65.1 63.2 60.6 55.8 53.4 50.6 50.2 49.9 56.6 66.6 Night 23 53.4 61.9 48.4 61.6 60.9 58.9 57.0 53.2 51.3 49.3 48.9 48.5 53.4 10.0 63.4 L_{eq} (dBA) L2% L25% L50% L90% L95% L99% **Timeframe** Hour L1% L5% L8% 51.0 61.9 61.6 61.1 59.5 58.2 52.6 50.2 46.5 46.0 45.5 Min 45.4 24-Hour Daytime **Nighttime** Max 60.6 76.4 49.9 75.5 75.0 72.7 72.0 68.8 66.2 52.3 51.6 50.1 56.8 66.5 65.9 63.9 62.2 57.2 53.3 48.5 48.0 47.4 **Energy Average** Average 56.4 56.7 55.6 55.2 59.3 45.2 62.5 62.0 60.2 52.5 49.2 46.0 45.6 Min 62.9 45.1 **Evening** 24-Hour CNEL (dBA) Max 57.8 68.0 49.9 67.6 67.0 64.7 62.4 57.2 53.3 50.8 50.4 50.0 62.7 55.1 51.9 56.3 Average: 65.1 64.6 61.0 48.8 48.4 48.0 **Energy Average** 49.9 58.2 44.9 57.8 57.1 55.1 53.7 50.0 47.7 45.6 45.3 45.0 Min **62.5** Night 57.6 66.6 52.0 66.0 65.1 63.2 58.1 56.0 52.7 52.2 Max 61.7 53.2



58.9

55.2

53.1

50.7

50.3

49.9

Average:

55.6

Energy Average



APPENDIX 7.1:

CADNAA OPERATIONAL NOISE MODEL INPUTS





12915 - Perris Truck Yard

CadnaA Noise Prediction Model: 12915-04 Lmax.cna

Date: 15.09.20 Analyst: S. Shami

Calculation Configuration

Calculation Configurat	
Parameter	Value
General	
Country	(user defined)
Max. Error (dB)	0.00
Max. Search Radius (#(Unit,LEN))	2000.01
Min. Dist Src to Rcvr	0.00
Partition	
Raster Factor	0.50
Max. Length of Section (#(Unit,LEN))	999.99
Min. Length of Section (#(Unit,LEN))	1.01
Min. Length of Section (%)	0.00
Proj. Line Sources	On
Proj. Area Sources	On
Ref. Time	
Reference Time Day (min)	960.00
Reference Time Night (min)	480.00
Daytime Penalty (dB)	0.00
Recr. Time Penalty (dB)	5.00
Night-time Penalty (dB)	10.00
DTM	
Standard Height (m)	0.00
Model of Terrain	Triangulation
Reflection	. 0
max. Order of Reflection	2
Search Radius Src	100.00
Search Radius Rcvr	100.00
Max. Distance Source - Rcvr	1000.00 1000.00
Min. Distance Rvcr - Reflector	1.00 1.00
Min. Distance Source - Reflector	0.10
Industrial (ISO 9613)	
Lateral Diffraction	some Obj
Obst. within Area Src do not shield	On
Screening	Incl. Ground Att. over Barrier
	Dz with limit (20/25)
Barrier Coefficients C1,2,3	3.0 20.0 0.0
Temperature (#(Unit,TEMP))	10
rel. Humidity (%)	70
Ground Absorption G	0.50
Wind Speed for Dir. (#(Unit,SPEED))	3.0
Roads (RLS-90)	
Strictly acc. to RLS-90	
Railways (FTA/FRA)	
Aircraft (???)	
Strictly acc. to AzB	
Julicity acc. to ALD	1

Receiver Noise Levels

Name	M.	ID	Leve	el Lr	Limit.	Value	Land Use			Height		Coordinates				
			Day	Night	Day	Night	Туре	Auto	Noise Type			Х	Υ	Z		
			(dBA)	(dBA)	(dBA)	(dBA)	A)			(ft)		(ft)	(ft)	(ft)		
RECEIVERS		R1	59.9	59.8	80.0	60.0				5.00	а	6266055.29	2256019.59	5.00		
RECEIVERS		R2	55.8	55.8	80.0	60.0				5.00	а	6266747.03	2256384.17	5.00		
RECEIVERS		R3	49.0	49.0	80.0	60.0				5.00 a		6264790.14	2253583.29	5.00		

Point Source(s)

Name	M.	ID	R	esult. PW	'L		Lw/L	i	Оре	Operating Time		K0	Height		C		
			Day	Evening	Night	Туре	ype Value norm.		Day	Special	Night				Х	Υ	Z
			(dBA)	(dBA)	(dBA)			dB(A)	(min)	(min)	(min)	(dB)	(ft)		(ft)	(ft)	(ft)
POINTSOURCE		TRASH01	102.8	102.8	102.8	Lw	102.8		150.00	0.00	90.00	0.0	5.00	а	6266401.15	2255142.31	5.00
POINTSOURCE		AC01	89.4	89.4	89.4	Lw	89.4		585.00	0.00	252.00	0.0	0.00	g	6266386.43	2255089.28	8.00

Line Source(s)

		-1-,																	
Name	M.	ID	R	Result. PW	/L	R	Result. PWL'			Lw / Li		Op	erating Ti	me		Moving	Pt. Src		Height
			Day	Evening	Night	Day	Evening	Night	Туре	Value	norm.	Day	Special	Night		Number		Speed	
			(dBA)	(dBA)	(dBA)	(dBA)	(dBA)	(dBA)			dB(A)	(min)	(min)	(min)	Day	Evening	Night	(mph)	(ft)
LINESOURCE		DWY01	90.0	74.6	80.8	73.8	58.4	64.6	PWL-Pt	91.4					172.0	5.0	21.0	6.2	8
LINESOURCE		DWY02	88.2	72.8	79.0	73.8	58.4	64.6	PWL-Pt	91.4					172.0	5.0	21.0	6.2	8

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Name	ŀ	lei	ght			Coordinat	es	
	Begin		End		х	у	Z	Ground
	(ft)		(ft)		(ft)	(ft)	(ft)	(ft)
LINESOURCE	8.00	0 a		6266363.39	2255134.93	8.00	0.00	
					6266363.37	2254997.48	8.00	0.00
LINESOURCE	8.00	.00 a		6266342.55	2255088.05	8.00	0.00	
					6266342.99	2254997.59	8.00	0.00

Area Source(s)

	-	- 1 - /													
Name	M.	ID	R	esult. PW	′L	Result. PWL"				Lw/L	i	Op	ime	Height	
			Day	Evening	Night	Day	Evening	Night	Туре	Value	norm.	Day	Special	Night	(ft)
			(dBA)	(dBA)	(dBA)	(dBA)	(dBA)	(dBA)			dB(A)	(min)	(min)	(min)	
AREASOURCE		TERMINAL01	118.5	118.5	118.5	73.3	73.3	73.3	Lw	118.5					8

Name	H	lei	ght			Coordinat	es	
	Begin		End (ft)		х	у	Z	Ground
	(ft)		(ft)		(ft)	(ft)	(ft)	(ft)
AREASOURCE	8.00	а			6266427.19	2255147.95	8.00	0.00
					6266311.30	2255149.68	8.00	0.00
					6266311.74	2255029.46	8.00	0.00
					6265992.29	2255030.76	8.00	0.00
					6265995.33	2255618.87	8.00	0.00
					6266631.18	2255615.40	8.00	0.00
					6266627.71	2255027.72	8.00	0.00
				6266426.75	2255028.59	8.00	0.00	

Building(s)

	٠0١	-,												
Name	M.	ID	RB	Residents	Absorption	Height	:	Coordinates						
						Begin		х	у	Z	Ground			
						(ft)		(ft)	(ft)	(ft)	(ft)			
BUILDING		BUILDING00001	х	0		8.00	а	6266382.91	2255131.47	8.00	0.00			
								6266396.84	2255131.34	8.00	0.00			
								6266396.58	2255085.24	8.00	0.00			
								6266382.26	2255085.24	8.00	0.00			

Urban Crossroads, Inc.

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APPENDIX 7.2:

CADNAA OPERATIONAL NOISE MODEL INPUTS





12915 - Perris Truck Yard

CadnaA Noise Prediction Model: 12915-04 Leq_CNEL.cna

Date: 15.09.20 Analyst: S. Shami

Calculation Configuration

Configurat	ion
Parameter	Value
General	
Country	(user defined)
Max. Error (dB)	0.00
Max. Search Radius (#(Unit,LEN))	2000.01
Min. Dist Src to Rcvr	0.00
Partition	
Raster Factor	0.50
Max. Length of Section (#(Unit,LEN))	999.99
Min. Length of Section (#(Unit,LEN))	1.01
Min. Length of Section (%)	0.00
Proj. Line Sources	On
Proj. Area Sources	On
Ref. Time	
Reference Time Day (min)	960.00
Reference Time Night (min)	480.00
Daytime Penalty (dB)	0.00
Recr. Time Penalty (dB)	5.00
Night-time Penalty (dB)	10.00
DTM	
Standard Height (m)	0.00
Model of Terrain	Triangulation
Reflection	
max. Order of Reflection	2
Search Radius Src	100.00
Search Radius Rcvr	100.00
Max. Distance Source - Rcvr	1000.00 1000.00
Min. Distance Rvcr - Reflector	1.00 1.00
Min. Distance Source - Reflector	0.10
Industrial (ISO 9613)	
Lateral Diffraction	some Obj
Obst. within Area Src do not shield	On
Screening	Incl. Ground Att. over Barrier
	Dz with limit (20/25)
Barrier Coefficients C1,2,3	3.0 20.0 0.0
Temperature (#(Unit,TEMP))	10
rel. Humidity (%)	70
Ground Absorption G	0.50
Wind Speed for Dir. (#(Unit,SPEED))	3.0
Roads (RLS-90)	
Strictly acc. to RLS-90	
Railways (FTA/FRA)	
Aircraft (???)	
Strictly acc. to AzB	

Receiver Noise Levels

Name	M.	ID		Level Lr		Lir	ue		Land	l Use	Height	:	Coordinates			
			Day	Night	CNEL	Day	.,			Auto	Noise Type			Х	Υ	Z
			(dBA)	(dBA)	(dBA)	(dBA)	(dBA)	(dBA)				(ft)		(ft)	(ft)	(ft)
RECEIVERS		R1	51.5	51.4	58.1	80.0	60.0	60.0				5.00	а	6266055.29	2256019.59	5.00
RECEIVERS		R2	47.4	47.4	54.1	80.0	60.0	60.0				5.00	а	6266747.03	2256384.17	5.00
RECEIVERS		R3	40.7	40.7	47.4	80.0	60.0	60.0				5.00	a	6264790.14	2253583.29	5.00

Point Source(s)

Name	M.	ID	R	esult. PW	'L	Lw / Li			Operating Time			K0	Height	С	oordinates	
			Day	Evening	Night	Туре	Value	norm.	Day	Special	Night			Х	Υ	Z
			(dBA)	(dBA)	(dBA)			dB(A)	(min)	(min)	(min)	(dB)	(ft)	(ft)	(ft)	(ft)
POINTSOURCE		TRASH01	88.5	88.5	88.5	Lw	88.5		150.00	0.00	90.00	0.0	5.00	a 6266401.15	2255142.31	5.00
POINTSOURCE		AC01	88.9	88.9	88.9	Lw	88.9		585.00	0.00	252.00	0.0	5.00	g 6266386.43	2255089.28	5.00

Line Source(s)

Name	M.	ID	R	esult. PW	/L	Result. PWL'				Lw / Li			Operating Time			Moving Pt. Src			
			Day	Evening	Night	Day	Evening	Night	Туре	Value	norm.	Day	Special	Night		Number		Speed	
			(dBA)	(dBA)	(dBA)	(dBA)	(dBA)	(dBA)			dB(A)	(min)	(min)	(min)	Day	Evening	Night	(mph)	(ft)
LINESOURCE		DWY01	88.3	72.9	79.1	72.1	56.7	62.9	PWL-Pt	89.7					172.0	5.0	21.0	6.2	8
LINESOURCE		DWY02	86.5	71.1	77.3	72.1	56.7	62.9	PWL-Pt	89.7					172.0	5.0	21.0	6.2	8

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Name	H	lei	ght		Coordinates								
	Begin		End (ft)		х	у	z	Ground					
	(ft)		(ft)		(ft)	(ft)	(ft)	(ft)					
LINESOURCE	8.00	а			6266363.39	2255134.93	8.00	0.00					
					6266363.37	2254997.48	8.00	0.00					
LINESOURCE	8.00	а			6266342.55	2255088.05	8.00	0.00					
					6266342.99	2254997.59	8.00	0.00					

Area Source(s)

	_	- 1 - /													
Name	М.	ID	R	esult. PW	'L	Result. PWL"			Lw / Li			Ope	Height		
			Day	Evening	Night	Day	Evening	Night	Туре	Value	norm.	Day	Special	Night	(ft)
			(dBA)	(dBA)	(dBA)	(dBA)	(dBA)	(dBA)			dB(A)	(min)	(min)	(min)	
AREASOURCE		TERMINAL01	110.1	110.1	110.1	64.9	64.9	64.9	Lw	110.1					8

Name	ŀ	lei	ght	Coordinates										
	Begin End		х	у	Z	Ground								
	(ft)		(ft)	(ft)	(ft)	(ft)	(ft)							
AREASOURCE	8.00	а		6266427.19	2255147.95	8.00	0.00							
				6266311.30	2255149.68	8.00	0.00							
				6266311.74	2255029.46	8.00	0.00							
				6265992.29	2255030.76	8.00	0.00							
				6265995.33	2255618.87	8.00	0.00							
				6266631.18	2255615.40	8.00	0.00							
				6266627.71	2255027.72	8.00	0.00							
				6266426.75	2255028.59	8.00	0.00							

Building(s)

	٠0١	-,									
Name	M.	ID	RB	Residents	Absorption	Height			Coordinat	es	
						Begin		х	у	Z	Ground
						(ft)		(ft)	(ft)	(ft)	(ft)
BUILDING		BUILDING00001	х	0		0.00	а	6266382.91	2255131.47	0.00	0.00
								6266396.84	2255131.34	0.00	0.00
								6266396.58	2255085.24	0.00	0.00
								6266382.26	2255085.24	0.00	0.00

Urban Crossroads, Inc.

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APPENDIX 8.1:

CADNAA CONSTRUCTION NOISE MODEL INPUTS





12915 - Perris Truck Yard

CadnaA Noise Prediction Model: 12915-04 Lmax - Construction.cna

Date: 15.09.20 Analyst: S. Shami

Calculation Configuration

Configurat	ion
Parameter	Value
General	
Country	(user defined)
Max. Error (dB)	0.00
Max. Search Radius (#(Unit,LEN))	2000.01
Min. Dist Src to Rcvr	0.00
Partition	
Raster Factor	0.50
Max. Length of Section (#(Unit,LEN))	999.99
Min. Length of Section (#(Unit,LEN))	1.01
Min. Length of Section (%)	0.00
Proj. Line Sources	On
Proj. Area Sources	On
Ref. Time	
Reference Time Day (min)	960.00
Reference Time Night (min)	480.00
Daytime Penalty (dB)	0.00
Recr. Time Penalty (dB)	5.00
Night-time Penalty (dB)	10.00
DTM	
Standard Height (m)	0.00
Model of Terrain	Triangulation
Reflection	
max. Order of Reflection	2
Search Radius Src	100.00
Search Radius Rcvr	100.00
Max. Distance Source - Rcvr	1000.00 1000.00
Min. Distance Rvcr - Reflector	1.00 1.00
Min. Distance Source - Reflector	0.10
Industrial (ISO 9613)	
Lateral Diffraction	some Obj
Obst. within Area Src do not shield	On
Screening	Incl. Ground Att. over Barrier
	Dz with limit (20/25)
Barrier Coefficients C1,2,3	3.0 20.0 0.0
Temperature (#(Unit,TEMP))	10
rel. Humidity (%)	70
Ground Absorption G	0.50
Wind Speed for Dir. (#(Unit,SPEED))	3.0
Roads (RLS-90)	
Strictly acc. to RLS-90	
Railways (FTA/FRA)	
Aircraft (???)	

Receiver Noise Levels

Name	M.	ID	Leve	el Lr	Limit.	Value		Lanc	Use	Height		Coordinates				
			Day	Night	Day	Night	Туре	Auto	Noise Type			Х	Υ	Z		
			(dBA)	(dBA)	(dBA)	(dBA)				(ft)		(ft)	(ft)	(ft)		
RECEIVERS		R1	72.1	72.1	80.0	60.0				5.00	а	6266055.29	2256019.59	5.00		
RECEIVERS		R2	68.1	68.1	80.0	60.0				5.00	а	6266747.03	2256384.17	5.00		
RECEIVERS		R3	61.6	61.6	80.0	60.0				5.00	а	6264790.14	2253583.29	5.00		

Area Source(s)

Name	M.	ID	Result. PWL			Result. PWL"			Lw / Li			Ор	Height		
			Day	Evening	Night	Day	Evening	Night	Туре	Value	norm.	Day	Special	Night	(ft)
			(dBA)	(dBA)	(dBA)	(dBA)	(dBA)	(dBA)			dB(A)	(min)	(min)	(min)	
SITEBOUNDARY		CONSTRUCTION	130.9	130.9	130.9	85.0	85.0	85.0	Lw"	85					8

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Name	ŀ	lei	ght		Coordinates									
	Begin		End		х	У	z	Ground						
	(ft)		(ft)		(ft)	(ft)	(ft)	(ft)						
SITEBOUNDARY	8.00 a				6265982.97	2255631.87	8.00	0.00						
					6266644.43	2255624.92	8.00	0.00						
					6266637.49	2254996.05	8.00	0.00						
					6265975.68	2254999.52	8.00	0.00						

