PERCOLATION REPORT FOR PROPOSED STORM WATER BASINS



Prepared For Meta Housing Corporation

Proposed Two Retention Basins Southwest corner of Avenue Q-12 and 25th Street East Palmdale, Los Angeles County, California APN: 3018-027-036

BRUIN GEOTECHNICAL SERVICES, INC.

44732 Yucca Avenue Lancaster, California 93534

> Job No: 20-229 December 28, 2020



SOIL AND MATERIAL TESTING AND INSPECTIONS

December 28, 2020 Mr. Scott Nakaatari **Meta Housing Corporation** 11150 West Olympic Blvd., Ste. 620 Los Angeles, CA 90064 J.N. 20-229

Project: Proposed Retention Basins Vicinity of Avenue Q-12 and 25th Street East, Palmdale, Los Angeles County, California APN: 3018-027-036

Subject: Percolation Testing for Proposed Storm Water Basins

Dear Mr. Nakaatari:

Presented herewith are the results of the percolation testing performed as requested for the referenced project. The purpose of the percolation testing program was to determine soil percolation characteristics relative to the proposed storm drain water retention system. It is our understanding the subject site will be developed as Multi-Family Three Stories Apartment Buildings with Associated Parking Spaces and landscape areas. This report concludes the scope of work per our agreement.

Site Description

The subject site, herein after referred to as Site, is located at the southeast corner of Avenue Q-12 and 25th Street East in Palmdale, Los Angeles County, California. The rectangular-shaped parcel consists of approximately 8.39 acres. At the time of our investigation, the Site vegetation consisted of a light covering of annual weeds and shrubs and a moderate to dense covering of juniper bushes. Dirt trails traversed the Site in many directions. The aforementioned site description is intended to be illustrative and is specifically not intended for use as a legal description of the Site.

The Site is located in a semi-developed area of Palmdale, with single-family and multifamily developments in the vicinity of the subject site. The parcels immediately east were undeveloped, vacant land. The parcel to the north contains a multi-family complex, and the parcels south and west of the site are single-family residential subdivisions.

Access to the Site is from 25th Street East or Avenue Q-12, both of which are paved roads.

The Site topography is relatively flat and level with a general slope to the east with drainage by sheet flow at approximately one to two (1-2) percent across the Site. The approximate elevation of the Site is approximately 2,657 feet above mean sea level.

Proposed Storm Water Basins

At the time of writing this report, the proposed drainage for the project site is under development. It is our understanding the final plans will propose a drainage system that includes a combination of sheet flow across the parking lot and storm drain features (gutters, catch basins drains, etc.) at localized areas of the site to collect stormwater generated by impervious areas and ultimately draining into the proposed water retention basins. Each proposed retention basins have an anticipated invert elevation approximately 10 below ground surface (bgs).

Field Procedures

The field-testing program was performed on October 27, 2020 and consisted of drilling two (2) borings utilizing a CME 75 drill rig with eight (8)-inch hollow stem auger to a depth of thirty (30) feet below existing ground surface. The boring location plan is presented in Appendix A.

The soil was logged during drilling and classified in accordance with the Unified Soil Classification System. No groundwater was encountered during drilling. The soil consisted of silty sand (SM) and poorly graded sand (SP). The boring logs are presented in Appendix B.

The Geotechnical and Materials Engineering Division of Los Angeles County Department of Public Works provides the Low Impact Development Storm-water Infiltration (GS200.2) as a guideline for testing procedures, calculation for infiltration, and percolation rates for large projects. Test procedures are in general conformity with GS200.2 and approved by the City of Palmdale.

Subsequent to drilling the test holes, a 4-inch O.D. perforated plastic pipe was placed at the center of the boring holes. Then, the annular space between the pipe and the boring wall was backfilled with gravel to prevent caving when adding water to the pipe.

On October 28, 2020, the total depth of the holes was measured and documented. The test holes were then filled with water to 10 feet below existing grade, the proposed approximate invert elevation of the retention system ("initial water level"), utilizing a 1.5-inch hose.

The test holes were again filled with water to the initial water level. The total volume of water required to fill the hole was documented. After 15 minutes, the water depth was measured and documented, and the holes were again filled to the initial water level. The total depth of the test holes was measured and documented. The water level drop did not exceed ten (10) feet below the initial water level. The time intervals between readings was set to 30 minutes. The testing was performed a minimum of six (6) hours and until at least 1 hour after flow rate into boring had stabilized (the percolation rate stabilized for three (3) consecutive readings).

The procedures on the GS200.2 requires a graph showing the cumulative volume (gal) vs. time (hr.) which is used to find the slope of the line for each boring test hole. After generating the graph and analyzing the tabulated data obtained in the field (shown in Appendix C) the cumulative volume of water used at times 4.5 and 6.5 hours were used to calculate the stabilized flowrate for each test boring. To account for the reduction of the diameter size of the boring during testing, the volume of water absorbed by the eight (8) inch diameter hole was adjusted to a larger volume based on the ratio of the sidewall surface areas, and the surface area of percolation was increased to eighteen (18) inch diameter hole in order to calculate the raw infiltration rate. Refer to Appendix D.

The raw infiltration rate calculations and reduction factors as outlined in GS200.2 have been incorporated into the Design Infiltration Rate, as shown in Appendix D. This percolation test method is in general accordance with low impact development standards for infiltration testing in Southern California, and general conformance with Los Angeles County GS200.2

GS200.2 require the application of safety factors related to the type of test method, site variability, number of tests performed and maintenance/siltation conditions.

<u>Results</u>

Coefficient of Permeability

Reduction factors must be applied to the measured percolation rates, per requirements of GS200.2, to determine the design values that will represent the long-term performance of the proposed infiltration BMP's. The calculations are presented below.

Infiltration design calculations

Under the section named "reduction factors" of GS200.2, there is a table showing the range of values that may be used for each factor applicable to the project for the calculation of the reduction factor. The raw infiltration rates were reduced depending on the factors selected from the "reduction factors" table from GS 200.2, based on our overall understanding of the project, and applied as shown below:

- Test-specific reduction factor (Boring Percolation Test), RFT = 2
- Site variability, number of tests performed, thoroughness of subsurface investigation, $FR_V = 1$
- Long-term siltation, plugging and maintenance, RFs = 1

Total Reduction Factor, RF = RF⁺*RF⁺*RFs = 2*1*1 = 2

The calculated reduction factor (RF) was applied to the raw infiltration rates obtaining the design infiltration rate of the retention basin. Furthermore, they are compared to the minimum infiltration rate suggested by GS200.2 guidelines to show their compliance, as indicated in Appendix D.

For the proposed infiltration basin, the design infiltration rates obtained from boring holes 1 and 2 are calculated to be 2.88 and 3.11 inches per hour respectively, which meet the minimum percolation design infiltration rate of 0.3 in/hr.

Conclusions

Based on the infiltration testing performed as indicated in this report, it is our professional opinion that the proposed retention basin is feasible from a geotechnical standpoint. The slowest infiltration rate of 2.88 in/hr. may be utilized for the proposed retention basin design.

Limitations

This report presents the results of the percolation test performed at the referenced location only to aid in design of the proposed basin. Appropriate safety factors shall be incorporated into the design. Based on Bruin GSI's current knowledge, no known barriers to groundwater flow (i.e. bedrock etc.) or problems associated with "mounding" are known to exist in the site vicinity. The opinions provided in this report are based on data from the field-testing program and our professional experience. Hydro-geologic conditions will vary with subsurface conditions, precipitation, geologic setting, and site topography.

This office should be notified if the proposed development changes and is other than indicated in this report.

This report has been prepared for the exclusive use of our client in conformance with generally accepted engineering practices. No reproduction or use of the report other than as indicated herein shall be allowed.

This report does not guarantee the issuance of building or grading permits.

<u>Closure</u>

We trust this report provides the information required at this time. Please direct any questions to this office. We appreciate the opportunity to provide our services.

Respectfully Submitted, Bruin Geotechnical Services Inc.

Ryan D. Duke P.E.

RDD/mes



PLOT MAP

APPENDIX A



BORING LOG SOIL CLASSIFICATION KEY

APPENDIX B

		Date(s) dnlled	10/27/2020	LOG OF	BORIN	G 1	
		Drilling Contractor	GP Drilling	Page 1 of 1			
	\sim	Dnilling Method Hollow Stem Auger					
BRU	Logged By DM						
GEOTICSI SLAVICIS For SP		Drill Bit Size/Type	8"	Checked By. MS			
	/	Sampling Method(s)	N/A	Total Depth of Borehole 30' be	gs		
Client: Meta Housi	ng Corporation	Groundwater	None Encountered	Boring Location: See F	igure 2		
Project Number:	20-229	Borehoie Backfill	Native/ Cuttings	Notes:			
Project Location:	Palmdale	Hammer Data	140#, 30" drop				
Depth Sample USCS	Graphic Log	N	laterial Description		Penetralion Resistance (Blows/6")	Dry Unit Weight pcf	Water Content %
5' SM 5' SM 10' SM/SP 10' SM/SP 20' SM/SP 20' SP 30' SP	Cemented Yellowish brown fi	Very dense, m wm slightly silty Dense, slightly wm slightly silty Medium dense	fine to coarse send w/#4 grave moist fine to medium send w/occ. co , slightly moist and w/coarse send & occ. 3/8 moist	el & occ. 3/6" gravel arse sand	31-43 17-31 18-24 30-36		
30'	Boring to			d No coulog			
	Boring termin	ated at 30'bgs.	No groundwater encountere	d. No caving.	<u> </u>		

	Date(s) drilled 10/27/2020	LOG OF BORING 2
A S	Contractor GP Drilling	Page 1 of 1
	Drilling Method Hollow Stem Auger	
BRUIN	Drill Rig Type CME 75	Logged By DM
	Dnill Bit Size/Type 8"	Checked By: MS
	Sampling N/A Method(s)	Total Depth of Borehole 30' bgs
Client: Meta Housing Corporation		Boring Location: See Figure 2
Project Number: 20-229	Borehole Native/ Cuttings	Notes:
Project Location: Palmdale	Hammer Data 140#, 30" drop]
Depth USCS Graphic Log	Material Description	Penetration Penetration (Blows/8°) Dry Unit Weight por
	Dense, moist e in gravel (1/2" gravel) Dense, moist wm, slightly silty fine to coarse sand w/ #4 - 3/8" g Dense, slightly moist	ravel

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Soils Key

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44732 Yucca Avenue

Sheet 1 of 2

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	SOIL CLASSIFICATION KEY						
	I	Major Divisior	Typical Names				
	Gravels	Clean gravels with little or no	GW		Well graded gravels, gravel-sand mixtures		
eve	More than half	fines	GP		Poorly graded gravels, gravel-sand mixtures		
oils #200 sie	coarse-fraction is larger than No. 4 sieve size	Gravel with	GM		Silty gravels, poorly graded gravel-sand-silt mixtures		
ained S er than		over 12% fines	GC		Clayey gravels, poorly graded gravel-sand-clay mixtures		
Coarse Grained Soils more larger than #20	Sam da	Clean sands	SW		Well graded sands, gravelly sands		
Cc Sor m	More than half coarse-fraction is larger than No. 4 sieve size Sands More than half coarse-fraction is smaller than No. 4 sieve size	with little or no fines	SP		Poorly graded sands, gravelly sands		
50			SM		Silty sands, poorly graded sand-silt mixtures		
			SC		Clayey sands, poorly graded sand-clay mixtures		
ve	0.14	1.01	ML		Inorganic silts, rock flour, clayey silts		
e Grained Soils smaller than #200 sieve	Silts an Liquid limit l	nd Clays ess than 50	CL		Inorganic clays of low to medium plasticity, sandy clays, silty clays		
Fine Grained Soils ore smaller than #			OL		Organic clays and organic silty clays of low plasticity		
le Grain smalle			MH		Inorganic silts, micaceous or diatomaceous fine sandy/silty soils, elastic silts		
Fine 50% or more	Silts ar Liquid limit gre	n d Clays eater than 50	СН		Inorganic clays with high plasticity, fat clays		
20%			ОН		Organic clays of medium to high plasticity, organic silts		
	Highly Orga	anic Soils	Pt		Peat and other highly organic soils		

CLASSIFICATION SYSTEM BASED ON UNIFIED SOIL CLASSIFICATION SYSTEM

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Key to Excavation Log

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Sheet 2 of 2

			(/							
Depth	Sample USCS	Graphic Log	Material Description			Dry Unit Weight pcf	Water Content %			
1	2 3	4	-	5	6	7	8			
COLU	COLUMN DESCRIPTIONS									
2 Sar 3 US0 4 Gra mat 5 Mat enc cold	1Depth: depth in feet below the ground surface.2Sample: type of sample taken at depth incurred3USCS: USCS symbol of the subsurface material.									
DIST=	Disturbed			CHEM= Chemical tests to assess co	orrosivity					
N/A= N	lot Analyzed									
	Californi Standaro	-	poon ration Test							
	Bulk San	nple								
	Grab Sar	nple								

GENERAL NOTES

1. Soil classifications are based on the Unified Soil Classification System. Descriptions and stratum lines are interpretive, and actual lithologic changes may be gradual. Field descriptions may have been modified to reflect results of lab tests.

2. Descriptions on these logs apply only at the specific boring locations and at the time the borings were advanced. They are not warranted to be representative of subsurface conditions at other locations or times.

PERCOLATION TEST RESULTS

APPENDIX C

BORING PERCOLATION TEST CALCULATIONS (GS200.2)

DATA CALCULATIONS:

DODING	STABILIZED	SUR	RAW				
BORING No.	[GAL/HR] **	[CF/HR]	DIA., [FT]	RADIUS, [FT]	HEIGHT, [FT]	S.A., [SF]	INFILTRATION RATE [FT/HR]
1	344.3	46.0	1.50	0.75	20	96.0	0.48
2	372.1	49.7	1.50	0.75	20	96.0	0.52

** Increased volume to account for reduction of boring diameter during testing.

REDUCTION FACTORS:

REDUCTION	DE			
RFt	RFv	RFs		
2	1	1	2	

DESIGN INFILTRATION RATE :

CALCULATED INFILTRATIO		GS200.2 MIN. DESIGN INFILT. RATE	CRITERIA MET?
[FT/HR]	[IN/HR]	[IN/HR]	
0.240	2.88	0.3	YES
0.259	3.11	0.3	YES

PERCOLATION TEST CALCULATIONS

APPENDIX D

BORING PERCOLATION FIELD LOG PER GS200.2

PROJECT NAME:	METAHOUSING	JOB No.: 20-229
TESTED BY:	MF	
LIQUID DESCRIPTION:	CLEAN TAP WATER	LOCATION: PALMDALE, CA
MEASUREMENT METHOD:	WATER SOUNDER	
DATE:	11/5/2020	

TIME INTERVAL STANDARD START TIME FOR STANDARD:

9:27 AM

1

0.67

30

10

10

YES

30 MIN.

OVER 100'

BORING #

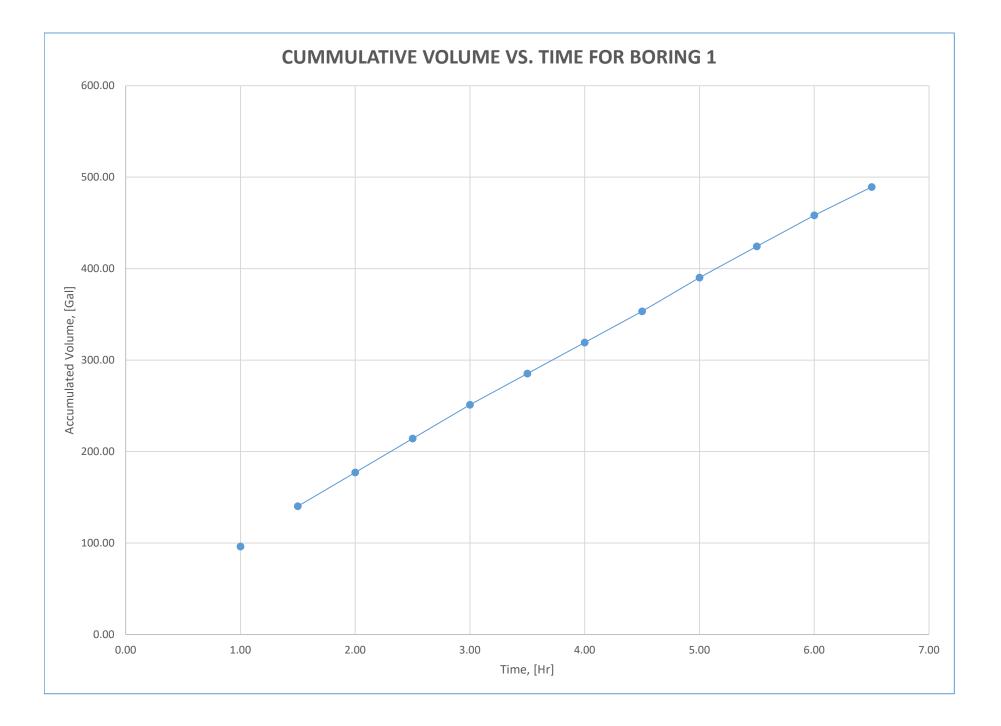
DIAMETER OF BORING, FT: DEPTH OF EXCAVATION, FT: DEPTH OF INVERT OF BMP, FT: DEPTH OF WATER TABLE: DEPTH TO INI. WATER DEPTH: WATER REMAINING IN EXCAV.? STD. TIME BETWEEN READINGS:

	DIA. P. PIPE, IN.: <u>4</u>	
FT		

TOTAL BORING V = 52 GAL.

							VOLUME [GAL	VS. TIME [HR]	
READING NO.	TIME START/END (HH:MM)	ELAPSED TIME (MIN)	WATER METER READINGS (START/END)	V, [GAL] ADDED	WATER SURFACE ELEVATION (FT)	WATER SURFACE ELEVATION DROP, Δ (FT)	CUMMULATIVE TIME, HR.	CUMULATIVE VOLUME, GAL.	
Presoak	8:55	30	3007497	52	10	17	0.50	52.22	
FTESOak	9:25	50	3007549	52	27	17	0.50	52.22	
1	9:27	30	3007549	44	10	17	1.00	96.22	
-	9:57	50	3007593	44	27	17	1.00	50.22	
2	9:59	30	3007593	44	10	14	1.50	140.22	
2	10:29	50	3007637	44	24	14	1.50	140.22	
3	10:30	30	3007637	37	10	14	2.00	177.22	
5	11:00	50	3007674	57	24	14			
4	11:03	30	3007674	37	10	14	2.50	214.22	
-	11:33	50	3007711	57	24	14			
5	11:36	30	3007711	37	10	13	3.00	251.22	
5	1:20	50	3007748	57	23	15	5.00	231.22	
6	12:09	30	3007748	34	10	13	3.50	285.22	
	12:39	55	3007782	5.	23	10	5.50	205.22	
7	12:42	30	3007782	34	10	13	4.00	319.22	
,	1:12	50	3007816	54	23	15	4.00	319.22	
8	1:15	30	3007816	34	10	14	4.50	353.22	
0	1:45	50	3007850	34	24	14	4.50	333.22	
9	1:48	30	3007850	37	10	13	5.00	390.22	
5	2:18	50	3007887	57	23	15	5.00	350.22	
10	2:18	30	3007887	34	10	13	5.50	424.22	
10	2:48	55	3007921	5.	23	10	5.50		
11	2:50	30	3007921	34	10	12	6.00	458.22	
	3:20	50	3007955		22		0.00	430.22	
12	3:22	30	3007955	31	10	12	6.50 48	489.22	
	3:52	50	3007986	51	22		0.50	405.22	

* CUMULATIVE VOLUME USED TO DETERMINE RAW INFILTRATION RATE



BORING PERCOLATION FIELD LOG PER GS200.2

PROJECT NAME:	METAHOUSING	JOB No.: 20-229
TESTED BY:	MF	
LIQUID DESCRIPTION:	CLEAN TAP WATER	LOCATION: PALMDALE, CA
MEASUREMENT METHOD:	WATER SOUNDER	
DATE:	11/5/2020	
TIME INTERVAL STANDARD		
START TIME FOR STANDARD:	9:32 AM	TOTAL BORING V = 52 GAL.

2

10

30 MIN.

BORING #

DIAMETER OF BORING, FT: DEPTH OF EXCAVATION, FT: DEPTH OF INVERT OF BMP, FT: DEPTH OF WATER TABLE: DEPTH TO INI. WATER DEPTH: WATER REMAINING IN EXCAV.? STD. TIME BETWEEN READINGS:

2	_		
0.67			DIA. P. PIPE, IN.: 4
30	_		
10			
OVER 100'			
10	FT		
YES			
30 MIN			

							VOLUME [GAL] VS. TIME [HR]
READING NO.	TIME START/END (HH:MM)	ELAPSED TIME (MIN)	WATER METER READINGS (START/END)	V, [GAL] ADDED	WATER SURFACE ELEVATION (FT)	WATER SURFACE ELEVATION DROP, Δ (FT)	CUMMULATIVE TIME, HR.	CUMULATIVE VOLUME, GAL.
Presoak	9:00	30	3007986	52	10.00	18	0.50	52.22
	9:30		3008038		28.00			
1	9:32	30	3008038	47	10.00	18	1.00	99.22
	10:02		3008085		28.00			
2	10:04	30	3008085	47	10.00	15	1.50	146.22
	10:34		3008132		25.00			
3	10:37	30	3008132	39	10.00	15	2.00	185.22
	11:07		3008171		25.00			
4	11:08	30	3008171	39	10.00	15	2.50	224.22
	11:38		3008210		25.00			
5	11:40	30	3008210	- 39	10.00	14	3.00	263.22
	12:10		3008249		24.00			
6	12:40	30	3008249	37	10.00	14	3.50	300.22
	1:10		3008286		24.00			
7	1:12	30	3008286	37	10.00	14	4.00	337.22
	1:42		3008323		24.00			
8	2:08	30	3008323	37	10.00	15	4.50	374.22
	2:38		3008360		25.00			
9	2:40	30	3008360	- 39	10.00	14	5.00	413.22
	3:10		3008399		24.00			
10	3:12	30	3008399	37	10.00	- 14	5.50	450.22
	3:42		3008436		24.00			
11	3:44	30	3008436	37	10.00	13	6.00	487.22
	4:14		3008473		23.00			
12	4:16	30	3008473	34	10.00	13	6.50	521.22
	4:46		3008507		23.00			

* CUMULATIVE VOLUME USED TO DETERMINE RAW INFILTRATION RATE

