



# **Rancho Springs Medical Center Project**

Preliminary Hydrology and Hydraulics Report

APN 912-010-032

25500 Medical Center Drive

Murrieta, CA 92562

## **Prepared for:**

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## **Prepared By:**

**Kimley»Horn**

Kimley-Horn and Associates, Inc.

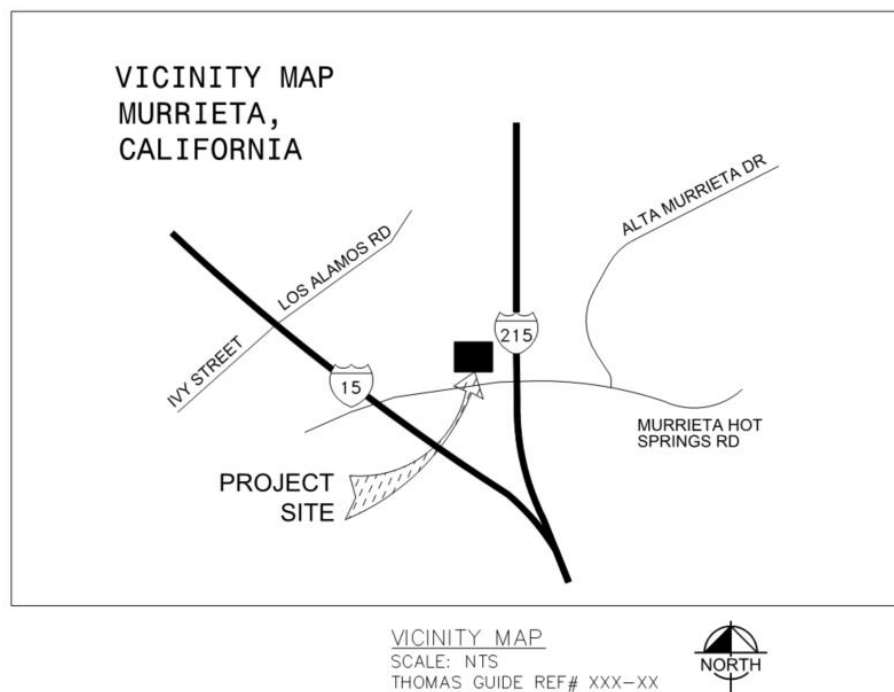
660 South Figueroa Street Suite 2050

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June 2020

## INTRODUCTION

The scope of the Project is to complete a preliminary hydrology and hydraulic analysis for the storm drain improvements associated with the proposed Rancho Springs Medical Center project in Murrieta, CA. The Project is located at 22500 Medical Center Drive on the northwest corner of the intersection of Interstate Freeway 215 and Murrieta Hot Springs Road. The Project consist of a 36,100 square foot hospital building expansion to be located centrally on the Rancho Springs Medical Center. Other project activities will also include utility improvements and parking areas and driveways redevelopment. The total project makes up approximately 5.23 acres.



**Figure 1: Rancho Springs Medical Center Location**

## HYDROLOGY

The preliminary hydrology and hydraulic analyses were completed in accordance with the Riverside County Hydrology Manual. A rational method analysis in accordance with the Manual was completed to calculate the peak discharges for existing conditions and project conditions. A review of the Geotechnical Investigation Report dated December 16, 2019 prepared by NOCA Services, Inc found that subsurface soils at the site consisted of silty and clayey sand and sandy silt fill material underlain by medium dense to very dense sandstone. Additionally, preliminary infiltration tests showed that the soils have low infiltration rates. Soil group C is defined as soils having slow infiltration rates (high runoff potential) and was used to calculate the soil loss rates.

Per the Riverside County Hydrology Manual, antecedent moisture condition (AMC) of 2 was used for the 100-year storm event. The land use for the project is commercial which has an impervious range percent between 80-100%. Storm depths from NOAA 14 were used for the analyses. The Advance Engineering Software (AES) Hydrosoft package was used to complete the rational method analysis.

Under existing conditions, the project discharges to multiple storm drain inlets located throughout the project. Runoff is routed through an existing onsite storm drain system that drains to a 60-inch storm drain lateral that ultimately discharges to the public storm drain system.

For proposed conditions, the project area was divided into three drainage areas (A-C). Each drainage area was then subdivided for the rational method calculations. Drainage area A consists of offsite runoff; therefore, it was rerouted to discharge directly into the existing 60-inch storm drain. Drainage area B consists of off-site areas and 0.31 acres from the project limits that cannot be captured in the proposed storm drain system due to grading constraints. Drainage area C consists of run-on areas and the remaining 4.92 acres from the proposed project which will be routed to a proposed detention basin via the proposed onsite storm drain system. The outlet from the detention basin will be limited to existing conditions flow rates or lower via a riser structure prior to discharging into the existing 60-inch storm drain.

Offsite areas from the north will be collected prior to entering the project area and rerouted to the existing 60-inch storm drain located beneath the project area. Offsite areas from the south and east perimeters will be collected in the project's proposed storm drain system and have been included in the proposed rational method and detention calculations. Hydrology maps and results for existing and proposed conditions are included in Appendix A.

## HYDRAULICS

### Storm Drain and Detention Basin Hydraulic Calculations

Hydraulic calculations for sizing storm drain were completed using Manning's equation. Each proposed storm drain lateral has been sized in AES will be able to convey the 100-year peak flow. Each storm drain line will discharge to a main lateral which will discharge to the onsite detention basin.

The unit hydrograph for the proposed project was completed using the AES software. The basin routing analysis was completed with Bentley PondPack, which uses the Modified-Puls method for flow-through basin analysis. Routing analysis results for the detention basin showed that the maximum water surface depth during the 100-year, 24-hour storm event was 3.75 feet, which would allow for more than 2 feet of freeboard. The total volume detained was 0.513 ac-ft. In addition, the peak outflow from the basin (4.42 cfs) was less than the existing conditions 100-year, 24-hour peak flow (5.07 cfs).

A 10-year, 1-hour storm analysis of the detention system was also calculations. Basin routing analysis for the 10-year, 1-hour storm showed a peak basin outflow discharge of 0.39 cfs, which is less than the unit hydrograph peak undeveloped discharge (0.45 cfs). The total volume detained was 0.865 ac-ft with a maximum water surface depth of 5.68 feet.

The detention basin system will outlet to the existing 60-inch storm drain lateral, matching the existing conditions. The outlet from the detention basin will discharge via a riser with an orifice and rectangular notch weir to limit the flows similar to existing conditions. The storm drain and basin routing calculations are included in Appendix B.

### **Catch Basin Calculations**

Catch basin capacity calculations were completed using Bentley's Flow Master software which uses HEC-22 Urban Drainage Design Manual (FHWA, 2009) methodology. The catch basins were designed for the 100-year 24-hour storm event and to limit the maximum ponding depth at the catch basins below 6 inches. The catch basin capacity calculations are included in Appendix C.

APPENDIX A: HYDROLOGY ANALYSIS



NOAA Atlas 14, Volume 6, Version 2  
Location name: Murrieta, California, USA\*  
Latitude: 33.5589°, Longitude: -117.1837°  
Elevation: 1144.08 ft\*\*  
\* source: ESRI Maps  
\*\* source: USGS



### POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Sarah Dietz, Sarah Heim, Lillian Hiner, Kazungu Maitaria, Deborah Martin, Sandra Pavlovic, Ishani Roy, Carl Trypaluk, Dale Unruh, Fenglin Yan, Michael Yekta, Tan Zhao, Geoffrey Bonnin, Daniel Brewer, Li-Chuan Chen, Tye Parzybok, John Yarchoan

NOAA, National Weather Service, Silver Spring, Maryland

[PF tabular](#) | [PF graphical](#) | [Maps & arials](#)

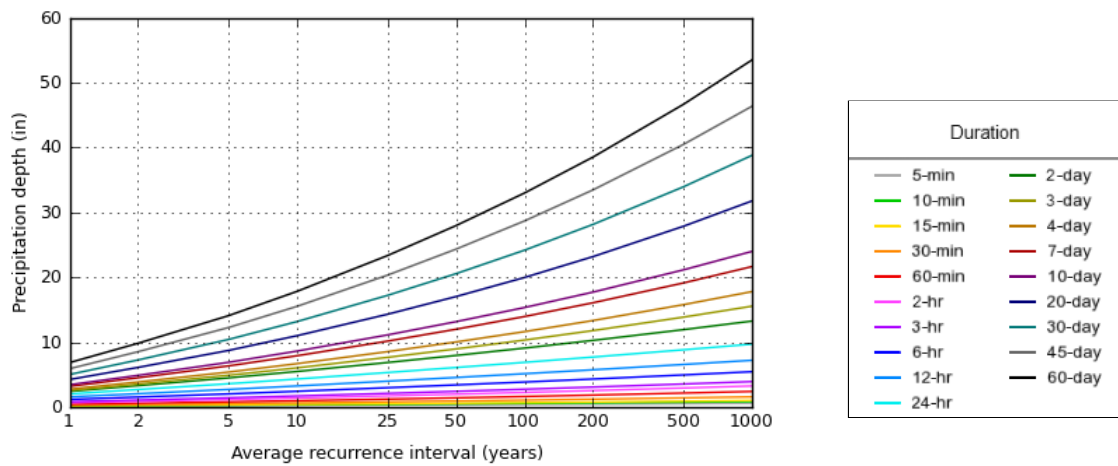
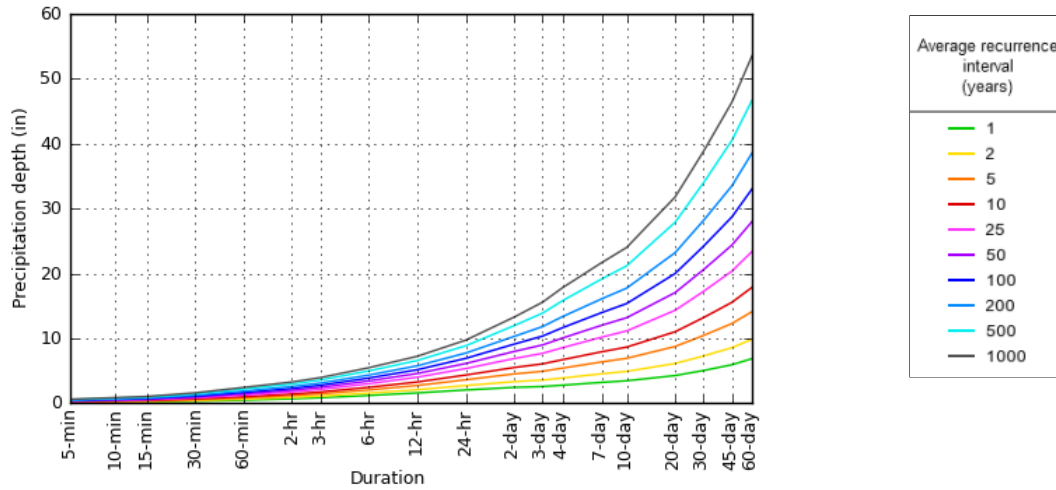
### PF tabular

PDS-based point precipitation frequency estimates with 90% confidence intervals (in inches) <sup>1</sup>										
Duration	Average recurrence interval (years)									
	1	2	5	10	25	50	100	200	500	1000
5-min	0.112 (0.094-0.135)	0.148 (0.124-0.179)	0.198 (0.166-0.240)	0.241 (0.199-0.293)	0.301 (0.240-0.380)	0.349 (0.273-0.450)	0.399 (0.304-0.529)	0.453 (0.335-0.618)	0.529 (0.374-0.754)	0.590 (0.402-0.873)
10-min	0.160 (0.135-0.193)	0.213 (0.178-0.256)	0.284 (0.238-0.344)	0.345 (0.286-0.421)	0.431 (0.345-0.544)	0.500 (0.391-0.645)	0.572 (0.436-0.758)	0.649 (0.480-0.886)	0.758 (0.536-1.08)	0.845 (0.577-1.25)
15-min	0.194 (0.163-0.234)	0.257 (0.216-0.310)	0.344 (0.287-0.416)	0.417 (0.346-0.509)	0.521 (0.417-0.658)	0.604 (0.472-0.780)	0.692 (0.527-0.917)	0.785 (0.581-1.07)	0.916 (0.649-1.31)	1.02 (0.698-1.51)
30-min	0.301 (0.253-0.362)	0.399 (0.335-0.481)	0.533 (0.446-0.645)	0.647 (0.536-0.789)	0.808 (0.646-1.02)	0.937 (0.733-1.21)	1.07 (0.818-1.42)	1.22 (0.901-1.66)	1.42 (1.01-2.03)	1.59 (1.08-2.35)
60-min	0.458 (0.384-0.551)	0.607 (0.509-0.732)	0.812 (0.678-0.981)	0.985 (0.816-1.20)	1.23 (0.983-1.55)	1.43 (1.12-1.84)	1.63 (1.24-2.17)	1.85 (1.37-2.53)	2.16 (1.53-3.09)	2.41 (1.65-3.57)
2-hr	0.669 (0.561-0.805)	0.878 (0.736-1.06)	1.16 (0.971-1.40)	1.40 (1.16-1.70)	1.73 (1.38-2.18)	1.99 (1.56-2.57)	2.26 (1.72-3.00)	2.55 (1.88-3.48)	2.94 (2.08-4.20)	3.26 (2.22-4.82)
3-hr	0.829 (0.696-0.997)	1.09 (0.910-1.31)	1.43 (1.20-1.73)	1.72 (1.42-2.09)	2.12 (1.69-2.67)	2.43 (1.90-3.14)	2.75 (2.10-3.65)	3.09 (2.29-4.22)	3.56 (2.52-5.08)	3.93 (2.68-5.81)
6-hr	1.18 (0.993-1.42)	1.55 (1.30-1.87)	2.03 (1.70-2.46)	2.44 (2.02-2.97)	2.99 (2.39-3.78)	3.42 (2.67-4.42)	3.86 (2.94-5.12)	4.32 (3.20-5.91)	4.96 (3.51-7.08)	5.46 (3.72-8.07)
12-hr	1.57 (1.32-1.89)	2.07 (1.73-2.49)	2.72 (2.28-3.29)	3.26 (2.70-3.97)	4.00 (3.19-5.05)	4.57 (3.57-5.90)	5.15 (3.92-6.82)	5.75 (4.25-7.85)	6.57 (4.65-9.38)	7.22 (4.92-10.7)
24-hr	2.03 (1.79-2.34)	2.71 (2.39-3.13)	3.60 (3.17-4.17)	4.33 (3.78-5.06)	5.33 (4.51-6.43)	6.10 (5.06-7.51)	6.90 (5.59-8.68)	7.71 (6.09-9.98)	8.83 (6.70-11.9)	9.71 (7.12-13.5)
2-day	2.42 (2.14-2.80)	3.31 (2.92-3.83)	4.50 (3.96-5.22)	5.49 (4.80-6.42)	6.87 (5.82-8.29)	7.96 (6.60-9.80)	9.09 (7.37-11.5)	10.3 (8.11-13.3)	11.9 (9.05-16.1)	13.3 (9.72-18.5)
3-day	2.56 (2.26-2.95)	3.55 (3.13-4.10)	4.91 (4.32-5.69)	6.05 (5.28-7.07)	7.67 (6.49-9.25)	8.97 (7.44-11.0)	10.3 (8.37-13.0)	11.8 (9.30-15.3)	13.9 (10.5-18.7)	15.6 (11.4-21.6)
4-day	2.76 (2.44-3.19)	3.87 (3.42-4.48)	5.40 (4.75-6.26)	6.70 (5.85-7.82)	8.55 (7.23-10.3)	10.0 (8.33-12.4)	11.6 (9.42-14.6)	13.3 (10.5-17.3)	15.8 (12.0-21.3)	17.8 (13.1-24.8)
7-day	3.20 (2.83-3.69)	4.52 (3.99-5.23)	6.35 (5.59-7.36)	7.92 (6.92-9.25)	10.2 (8.61-12.3)	12.0 (9.96-14.8)	14.0 (11.3-17.6)	16.1 (12.7-20.8)	19.1 (14.5-25.8)	21.7 (15.9-30.1)
10-day	3.44 (3.04-3.98)	4.89 (4.32-5.65)	6.90 (6.08-8.00)	8.63 (7.54-10.1)	11.1 (9.42-13.4)	13.2 (10.9-16.2)	15.4 (12.4-19.3)	17.7 (14.0-22.9)	21.2 (16.0-28.5)	24.0 (17.6-33.4)
20-day	4.25 (3.76-4.91)	6.11 (5.40-7.07)	8.73 (7.69-10.1)	11.0 (9.61-12.9)	14.3 (12.1-17.3)	17.0 (14.1-21.0)	20.0 (16.2-25.2)	23.2 (18.3-30.0)	27.9 (21.1-37.5)	31.8 (23.3-44.2)
30-day	5.03 (4.44-5.80)	7.26 (6.41-8.40)	10.4 (9.18-12.1)	13.2 (11.5-15.4)	17.2 (14.6-20.8)	20.6 (17.1-25.3)	24.2 (19.6-30.5)	28.2 (22.2-36.4)	34.0 (25.7-45.7)	38.8 (28.5-54.0)
45-day	5.91 (5.23-6.83)	8.54 (7.53-9.87)	12.3 (10.8-14.2)	15.5 (13.6-18.1)	20.3 (17.2-24.5)	24.3 (20.2-30.0)	28.7 (23.3-36.1)	33.5 (26.4-43.3)	40.5 (30.7-54.5)	46.4 (34.0-64.5)
60-day	6.85 (6.06-7.91)	9.84 (8.68-11.4)	14.1 (12.4-16.3)	17.8 (15.6-20.8)	23.4 (19.8-28.2)	28.0 (23.2-34.4)	33.0 (26.7-41.6)	38.5 (30.4-49.9)	46.7 (35.4-62.8)	53.5 (39.2-74.5)
<sup>1</sup> Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS). Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values. Please refer to NOAA Atlas 14 document for more information.										

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### PF graphical

PDS-based depth-duration-frequency (DDF) curves  
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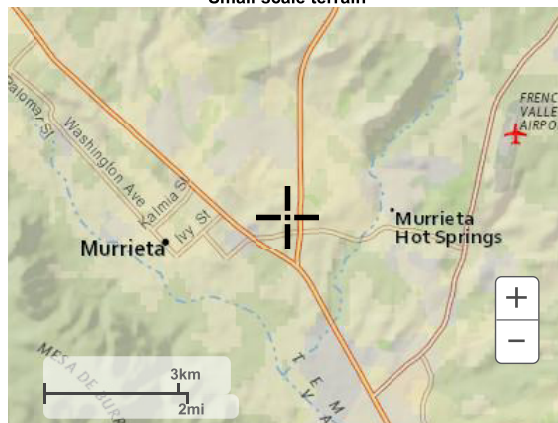
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## Maps & aerals

Small scale terrain



Large scale terrain



Large scale map



Large scale aerial



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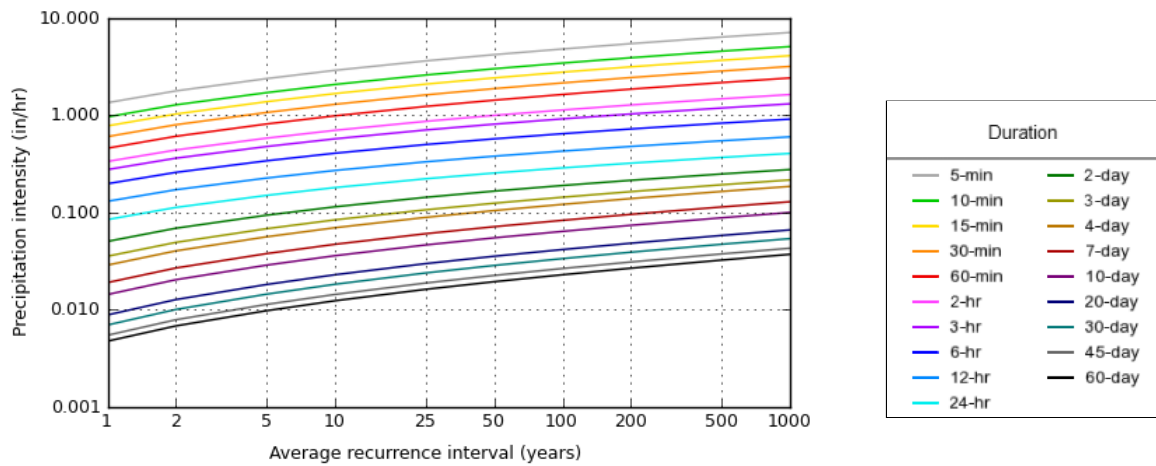
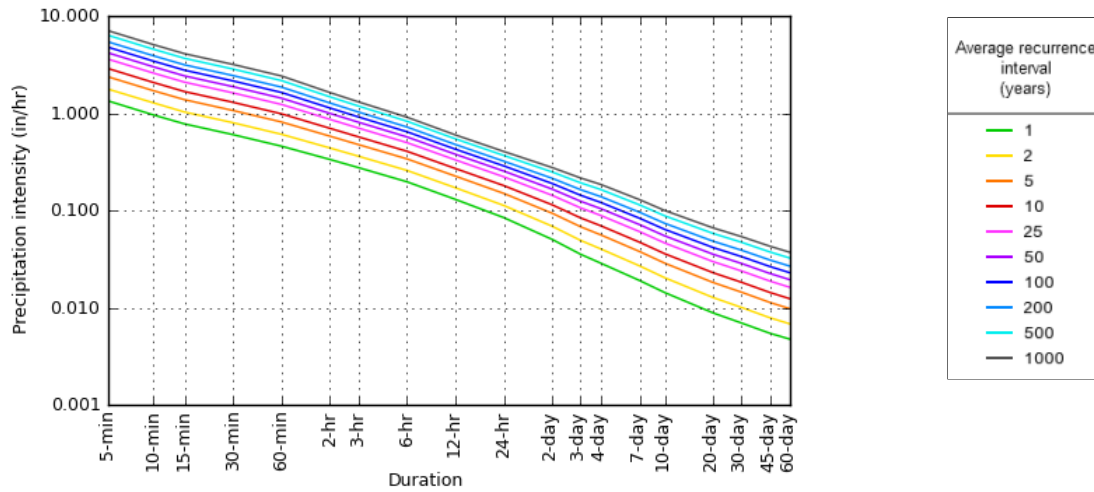
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Duration	Average recurrence interval (years)									
	1	2	5	10	25	50	100	200	500	1000
5-min	1.34 (1.13-1.62)	1.78 (1.49-2.15)	2.38 (1.99-2.88)	2.89 (2.39-3.52)	3.61 (2.88-4.56)	4.19 (3.28-5.40)	4.79 (3.65-6.35)	5.44 (4.02-7.42)	6.35 (4.49-9.05)	7.08 (4.82-10.5)
10-min	0.960 (0.810-1.16)	1.28 (1.07-1.54)	1.70 (1.43-2.06)	2.07 (1.72-2.53)	2.59 (2.07-3.26)	3.00 (2.35-3.87)	3.43 (2.62-4.55)	3.89 (2.88-5.32)	4.55 (3.22-6.49)	5.07 (3.46-7.51)
15-min	0.776 (0.652-0.936)	1.03 (0.864-1.24)	1.38 (1.15-1.66)	1.67 (1.38-2.04)	2.08 (1.67-2.63)	2.42 (1.89-3.12)	2.77 (2.11-3.67)	3.14 (2.32-4.29)	3.66 (2.60-5.23)	4.09 (2.79-6.05)
30-min	0.602 (0.506-0.724)	0.798 (0.670-0.962)	1.07 (0.892-1.29)	1.29 (1.07-1.58)	1.62 (1.29-2.04)	1.87 (1.47-2.42)	2.15 (1.64-2.85)	2.44 (1.80-3.33)	2.84 (2.01-4.06)	3.17 (2.16-4.69)
60-min	0.458 (0.384-0.551)	0.607 (0.509-0.732)	0.812 (0.678-0.981)	0.985 (0.816-1.20)	1.23 (0.983-1.55)	1.43 (1.12-1.84)	1.63 (1.24-2.17)	1.85 (1.37-2.53)	2.16 (1.53-3.09)	2.41 (1.65-3.57)
2-hr	0.334 (0.280-0.402)	0.439 (0.368-0.529)	0.580 (0.486-0.702)	0.699 (0.579-0.852)	0.864 (0.691-1.09)	0.995 (0.778-1.29)	1.13 (0.862-1.50)	1.27 (0.942-1.74)	1.47 (1.04-2.10)	1.63 (1.11-2.41)
3-hr	0.276 (0.232-0.332)	0.362 (0.303-0.436)	0.476 (0.398-0.575)	0.572 (0.474-0.697)	0.704 (0.563-0.889)	0.809 (0.632-1.04)	0.916 (0.698-1.21)	1.03 (0.761-1.41)	1.19 (0.839-1.69)	1.31 (0.893-1.94)
6-hr	0.198 (0.166-0.238)	0.259 (0.217-0.311)	0.340 (0.284-0.410)	0.407 (0.337-0.496)	0.499 (0.399-0.630)	0.571 (0.447-0.738)	0.645 (0.491-0.855)	0.722 (0.534-0.986)	0.828 (0.586-1.18)	0.911 (0.622-1.35)
12-hr	0.130 (0.109-0.157)	0.171 (0.144-0.207)	0.226 (0.189-0.273)	0.270 (0.224-0.330)	0.332 (0.265-0.419)	0.379 (0.296-0.489)	0.427 (0.326-0.566)	0.477 (0.353-0.652)	0.546 (0.386-0.779)	0.599 (0.409-0.886)
24-hr	0.085 (0.075-0.098)	0.113 (0.100-0.130)	0.150 (0.132-0.174)	0.180 (0.158-0.211)	0.222 (0.188-0.268)	0.254 (0.211-0.313)	0.287 (0.233-0.362)	0.321 (0.254-0.416)	0.368 (0.279-0.495)	0.404 (0.297-0.563)
2-day	0.050 (0.045-0.058)	0.069 (0.061-0.080)	0.094 (0.083-0.109)	0.114 (0.100-0.134)	0.143 (0.121-0.173)	0.166 (0.138-0.204)	0.189 (0.153-0.239)	0.214 (0.169-0.277)	0.249 (0.189-0.335)	0.276 (0.203-0.384)
3-day	0.036 (0.031-0.041)	0.049 (0.044-0.057)	0.068 (0.060-0.079)	0.084 (0.073-0.098)	0.106 (0.090-0.128)	0.125 (0.103-0.153)	0.144 (0.116-0.181)	0.164 (0.129-0.212)	0.193 (0.146-0.259)	0.216 (0.158-0.301)
4-day	0.029 (0.025-0.033)	0.040 (0.036-0.047)	0.056 (0.050-0.065)	0.070 (0.061-0.081)	0.089 (0.075-0.107)	0.105 (0.087-0.129)	0.121 (0.098-0.153)	0.139 (0.110-0.180)	0.165 (0.125-0.221)	0.185 (0.136-0.258)
7-day	0.019 (0.017-0.022)	0.027 (0.024-0.031)	0.038 (0.033-0.044)	0.047 (0.041-0.055)	0.061 (0.051-0.073)	0.071 (0.059-0.088)	0.083 (0.067-0.105)	0.096 (0.076-0.124)	0.114 (0.086-0.153)	0.129 (0.095-0.179)
10-day	0.014 (0.013-0.017)	0.020 (0.018-0.024)	0.029 (0.025-0.033)	0.036 (0.031-0.042)	0.046 (0.039-0.056)	0.055 (0.046-0.067)	0.064 (0.052-0.081)	0.074 (0.058-0.096)	0.088 (0.067-0.119)	0.100 (0.073-0.139)
20-day	0.009 (0.008-0.010)	0.013 (0.011-0.015)	0.018 (0.016-0.021)	0.023 (0.020-0.027)	0.030 (0.025-0.036)	0.035 (0.029-0.044)	0.042 (0.034-0.052)	0.048 (0.038-0.063)	0.058 (0.044-0.078)	0.066 (0.049-0.092)
30-day	0.007 (0.006-0.008)	0.010 (0.009-0.012)	0.014 (0.013-0.017)	0.018 (0.016-0.021)	0.024 (0.020-0.029)	0.029 (0.024-0.035)	0.034 (0.027-0.042)	0.039 (0.031-0.051)	0.047 (0.036-0.063)	0.054 (0.040-0.075)
45-day	0.005 (0.005-0.006)	0.008 (0.007-0.009)	0.011 (0.010-0.013)	0.014 (0.013-0.017)	0.019 (0.016-0.023)	0.023 (0.019-0.028)	0.027 (0.022-0.033)	0.031 (0.024-0.040)	0.037 (0.028-0.050)	0.043 (0.031-0.060)
60-day	0.005 (0.004-0.005)	0.007 (0.006-0.008)	0.010 (0.009-0.011)	0.012 (0.011-0.014)	0.016 (0.014-0.020)	0.019 (0.016-0.024)	0.023 (0.019-0.029)	0.027 (0.021-0.035)	0.032 (0.025-0.044)	0.037 (0.027-0.052)
<sup>1</sup> Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS). Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values. Please refer to NOAA Atlas 14 document for more information.										

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### PF graphical

PDS-based intensity-duration-frequency (IDF) curves  
Latitude: 33.5589°, Longitude: -117.1837°



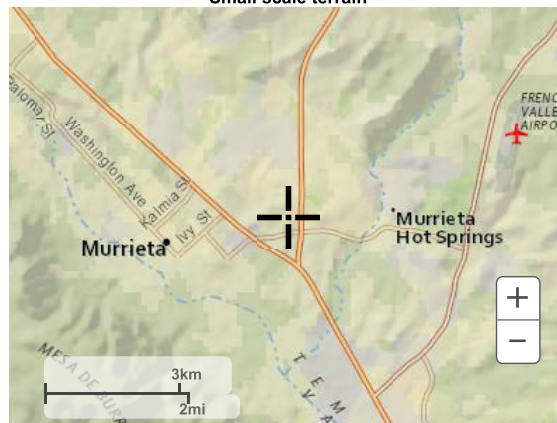
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## Maps & aerals

Small scale terrain



Large scale terrain



Large scale map



Large scale aerial

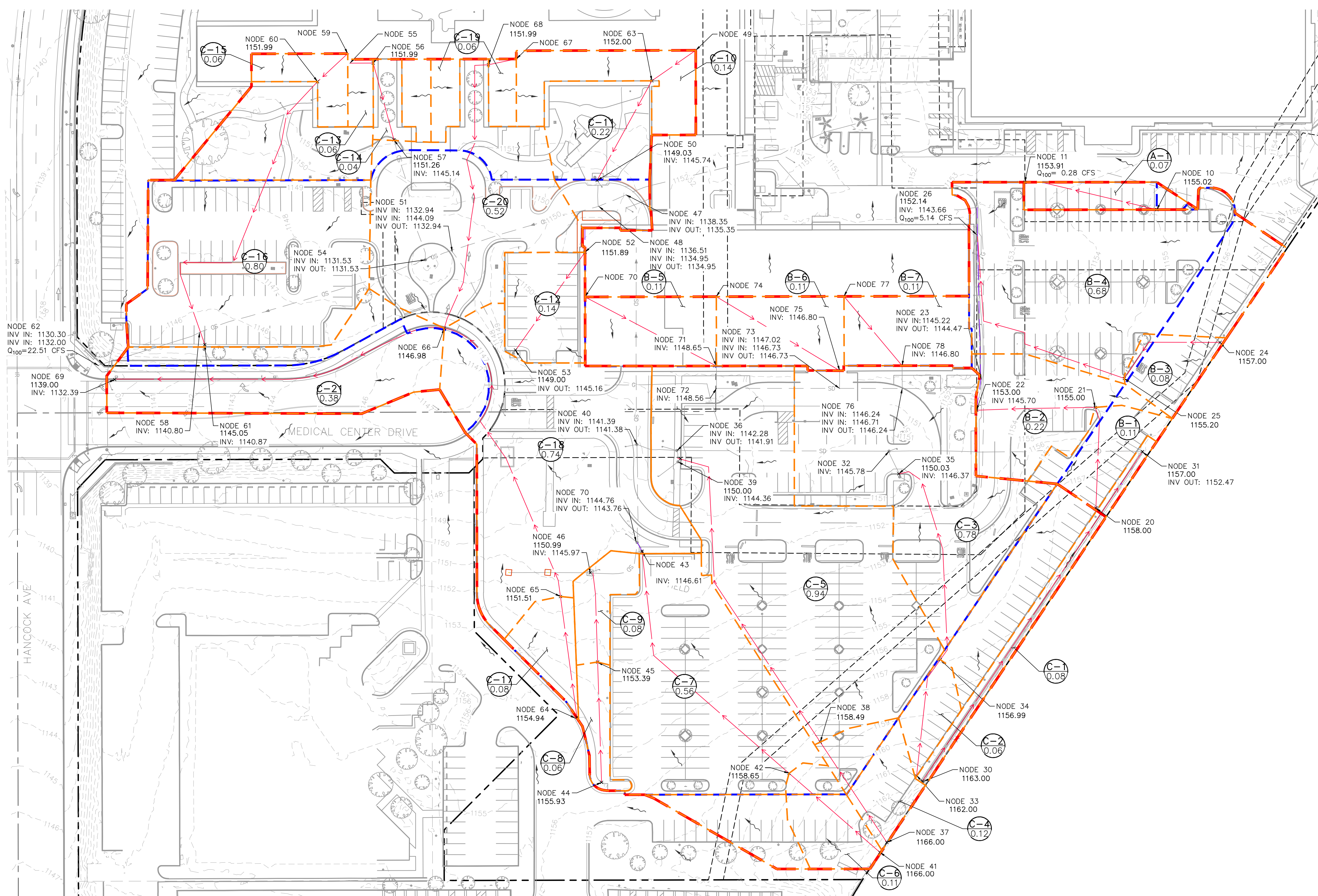


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[National Water Center](#)  
 1325 East West Highway  
 Silver Spring, MD 20910  
 Questions?: [HDSC.Questions@noaa.gov](mailto:HDSC.Questions@noaa.gov)

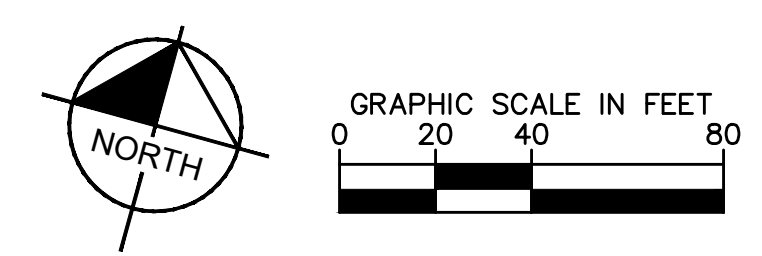
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**LEGEND**

- CENTER LINE
- PROPERTY LINE
- RIGHT-OF-WAY LINE / LEASE LINE
- EASEMENT LINE
- PROJECT LIMITS
- EXISTING STORM DRAIN LINE
- LONGEST FLOW PATH
- DENOTES DRAINAGE AREA BOUNDARY
- DENOTES SUB-DRAINAGE AREA BOUNDARY
- SUBAREA NAME  
AREA (AC)
- EXISTING SURFACE FLOW DIRECTION



RANCHO SPRINGS  
MEDICAL CENTER  
EXISTING CONDITIONS  
HYDROLOGY MAP  
JUNE 2020



\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM BASED ON  
 RIVERSIDE COUNTY FLOOD CONTROL & WATER CONSERVATION DISTRICT  
 (RCFC&WCD) 1978 HYDROLOGY MANUAL  
 (c) Copyright 1982-2011 Advanced Engineering Software (aes)  
 (Rational Tabling Version 18.0)  
 Release Date: 07/01/2011 License ID 1499

Analysis prepared by:

Kimley-Horn and Associates, Inc.  
 765 The City Drive  
 Suite 200  
 Orange, CA 92868

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*

\* UHS Rancho Springs \*  
 \* Existing Conditions \*  
 \* 10-year analysis \*  
 \*\*\*\*\*

FILE NAME: RS\_E.DAT  
 TIME/DATE OF STUDY: 21:12 05/17/2020

-----  
 USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
 -----

USER SPECIFIED STORM EVENT(YEAR) = 10.00  
 SPECIFIED MINIMUM PIPE SIZE(INCH) = 8.00  
 SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.95  
 10-YEAR STORM 10-MINUTE INTENSITY(INCH/HOUR) = 2.070  
 10-YEAR STORM 60-MINUTE INTENSITY(INCH/HOUR) = 0.985  
 100-YEAR STORM 10-MINUTE INTENSITY(INCH/HOUR) = 3.430  
 100-YEAR STORM 60-MINUTE INTENSITY(INCH/HOUR) = 1.630  
 SLOPE OF 10-YEAR INTENSITY-DURATION CURVE = 0.4144876  
 SLOPE OF 100-YEAR INTENSITY-DURATION CURVE = 0.4152232

COMPUTED RAINFALL INTENSITY DATA:

STORM EVENT = 10.00 1-HOUR INTENSITY(INCH/HOUR) = 0.995  
 SLOPE OF INTENSITY DURATION CURVE = 0.4145

RCFC&WCD HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD

NOTE: COMPUTE CONFLUENCE VALUES ACCORDING TO RCFC&WCD HYDROLOGY MANUAL

AND IGNORE OTHER CONFLUENCE COMBINATIONS FOR DOWNSTREAM ANALYSES

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

NO.	HALF- WIDTH (FT)	CROWN TO CROSSFALL (FT)	STREET-CROSSFALL: IN- / OUT- / PARK- SIDE / SIDE / WAY	CURB HEIGHT (FT)	GUTTER-GEOMETRIES: WIDTH (FT)	LIP (FT)	HIKE (FT)	MANNING FACTOR (n)
1	30.0	20.0	0.018/0.018/0.020	0.67	2.00	0.0313	0.167	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
 as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
 OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*

FLOW PROCESS FROM NODE 10.00 TO NODE 11.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

=====

ASSUMED INITIAL SUBAREA UNIFORM  
 DEVELOPMENT IS COMMERCIAL

```

TC = K*[(LENGTH**3)/(ELEVATION CHANGE)]**.2
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00
UPSTREAM ELEVATION(FEET) = 1155.02
DOWNSTREAM ELEVATION(FEET) = 1153.91
ELEVATION DIFFERENCE(FEET) = 1.11
TC = 0.303*[(100.00**3)/(1.11)]**.2 = 4.705
COMPUTED TIME OF CONCENTRATION INCREASED TO 5 MIN.
10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.787
COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8841
SOIL CLASSIFICATION IS "C"
SUBAREA RUNOFF(CFS) = 0.17
TOTAL AREA(ACRES) = 0.07 TOTAL RUNOFF(CFS) = 0.17

```

\*\*\*\*\*

```

FLOW PROCESS FROM NODE 20.00 TO NODE 21.00 IS CODE = 21

```

```

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

```

=====

```

ASSUMED INITIAL SUBAREA UNIFORM
DEVELOPMENT IS COMMERCIAL

```

```

TC = K*[(LENGTH**3)/(ELEVATION CHANGE)]**.2
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00
UPSTREAM ELEVATION(FEET) = 1158.00
DOWNSTREAM ELEVATION(FEET) = 1155.00
ELEVATION DIFFERENCE(FEET) = 3.00
TC = 0.303*[(100.00**3)/(3.00)]**.2 = 3.856
COMPUTED TIME OF CONCENTRATION INCREASED TO 5 MIN.
10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.787
COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8841
SOIL CLASSIFICATION IS "C"
SUBAREA RUNOFF(CFS) = 0.27
TOTAL AREA(ACRES) = 0.11 TOTAL RUNOFF(CFS) = 0.27

```

\*\*\*\*\*

```

FLOW PROCESS FROM NODE 21.00 TO NODE 22.00 IS CODE = 51

```

```

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<

```

```

>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<

```

=====

```

ELEVATION DATA: UPSTREAM(FEET) = 1155.00 DOWNSTREAM(FEET) = 1153.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 99.00 CHANNEL SLOPE = 0.0202
CHANNEL BASE(FEET) = 0.00 "Z" FACTOR = 99.000
MANNING'S FACTOR = 0.015 MAXIMUM DEPTH(FEET) = 1.00
10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.530
COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8828
SOIL CLASSIFICATION IS "C"
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.39
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 1.26
AVERAGE FLOW DEPTH(FEET) = 0.06 TRAVEL TIME(MIN.) = 1.31
Tc(MIN.) = 6.31
SUBAREA AREA(ACRES) = 0.11 SUBAREA RUNOFF(CFS) = 0.25
TOTAL AREA(ACRES) = 0.2 PEAK FLOW RATE(CFS) = 0.52

```

```

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

```

```

DEPTH(FEET) = 0.06 FLOW VELOCITY(FEET/SEC.) = 1.28
LONGEST FLOWPATH FROM NODE 20.00 TO NODE 22.00 = 199.00 FEET.

```

\*\*\*\*\*

```

FLOW PROCESS FROM NODE 22.00 TO NODE 22.00 IS CODE = 81

```

```

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<

```

=====

```

10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.530

```

COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8828  
 SOIL CLASSIFICATION IS "C"  
 SUBAREA AREA(ACRES) = 0.11 SUBAREA RUNOFF(CFS) = 0.25  
 TOTAL AREA(ACRES) = 0.3 TOTAL RUNOFF(CFS) = 0.76  
 TC(MIN.) = 6.31

\*\*\*\*\*

FLOW PROCESS FROM NODE 22.00 TO NODE 23.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<  
 >>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<

=====

ELEVATION DATA: UPSTREAM(Feet) = 1145.70 DOWNSTREAM(Feet) = 1144.47  
 FLOW LENGTH(Feet) = 26.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 21.0 INCH PIPE IS 2.2 INCHES  
 PIPE-FLOW VELOCITY(Feet/Sec.) = 5.75  
 GIVEN PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 0.76  
 PIPE TRAVEL TIME(MIN.) = 0.08 Tc(MIN.) = 6.39  
 LONGEST FLOWPATH FROM NODE 20.00 TO NODE 23.00 = 225.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 23.00 TO NODE 23.00 IS CODE = 10

>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<

\*\*\*\*\*

FLOW PROCESS FROM NODE 70.00 TO NODE 71.00 IS CODE = 22

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

=====

ASSUMED INITIAL SUBAREA UNIFORM  
 DEVELOPMENT IS COMMERCIAL  
 USER SPECIFIED Tc(MIN.) = 5.000  
 10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.787  
 COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8841  
 SOIL CLASSIFICATION IS "C"  
 SUBAREA RUNOFF(CFS) = 0.27  
 TOTAL AREA(ACRES) = 0.11 TOTAL RUNOFF(CFS) = 0.27

\*\*\*\*\*

FLOW PROCESS FROM NODE 71.00 TO NODE 72.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<  
 >>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<

=====

ELEVATION DATA: UPSTREAM(Feet) = 1148.65 DOWNSTREAM(Feet) = 1148.56  
 FLOW LENGTH(Feet) = 18.50 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 12.0 INCH PIPE IS 2.7 INCHES  
 PIPE-FLOW VELOCITY(Feet/Sec.) = 2.04  
 GIVEN PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 0.27  
 PIPE TRAVEL TIME(MIN.) = 0.15 Tc(MIN.) = 5.15  
 LONGEST FLOWPATH FROM NODE 70.00 TO NODE 72.00 = 10018.50 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 72.00 TO NODE 73.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<  
 >>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<

=====

ELEVATION DATA: UPSTREAM(Feet) = 1148.56 DOWNSTREAM(Feet) = 1147.02

```

                                RS_E_10.RES
FLOW LENGTH(FEET) = 102.00  MANNING'S N = 0.013
DEPTH OF FLOW IN 12.0 INCH PIPE IS 2.0 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 3.07
GIVEN PIPE DIAMETER(INCH) = 12.00  NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 0.27
PIPE TRAVEL TIME(MIN.) = 0.55  Tc(MIN.) = 5.71
LONGEST FLOWPATH FROM NODE 70.00 TO NODE 73.00 = 10120.50 FEET.

*****
FLOW PROCESS FROM NODE 73.00 TO NODE 73.00 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 5.71
RAINFALL INTENSITY(INCH/HR) = 2.64
TOTAL STREAM AREA(ACRES) = 0.11
PEAK FLOW RATE(CFS) AT CONFLUENCE = 0.27

*****
FLOW PROCESS FROM NODE 74.00 TO NODE 75.00 IS CODE = 22
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
=====
    ASSUMED INITIAL SUBAREA UNIFORM
    DEVELOPMENT IS COMMERCIAL
USER SPECIFIED Tc(MIN.) = 5.000
    10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.787
COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8841
SOIL CLASSIFICATION IS "C"
SUBAREA RUNOFF(CFS) = 0.27
TOTAL AREA(ACRES) = 0.11  TOTAL RUNOFF(CFS) = 0.27

*****
FLOW PROCESS FROM NODE 75.00 TO NODE 73.00 IS CODE = 41
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 1146.80  DOWNSTREAM(FEET) = 1146.73
FLOW LENGTH(FEET) = 14.70  MANNING'S N = 0.013
DEPTH OF FLOW IN 12.0 INCH PIPE IS 2.7 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 2.04
GIVEN PIPE DIAMETER(INCH) = 12.00  NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 0.27
PIPE TRAVEL TIME(MIN.) = 0.12  Tc(MIN.) = 5.12
LONGEST FLOWPATH FROM NODE 74.00 TO NODE 73.00 = 114.70 FEET.

*****
FLOW PROCESS FROM NODE 73.00 TO NODE 73.00 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 5.12
RAINFALL INTENSITY(INCH/HR) = 2.76
TOTAL STREAM AREA(ACRES) = 0.11
PEAK FLOW RATE(CFS) AT CONFLUENCE = 0.27

** CONFLUENCE DATA **

```



STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	0.27	5.71	2.638	0.11
2	0.27	5.12	2.759	0.11

\*\*\*\*\*WARNING\*\*\*\*\*

IN THIS COMPUTER PROGRAM, THE CONFLUENCE VALUE USED IS BASED  
ON THE RCFC&WCD FORMULA OF PLATE D-1 AS DEFAULT VALUE. THIS FORMULA  
WILL NOT NECESSARILY RESULT IN THE MAXIMUM VALUE OF PEAK FLOW.

\*\*\*\*\*

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	0.51	5.12	2.759
2	0.53	5.71	2.638

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 0.53 Tc(MIN.) = 5.71  
TOTAL AREA(ACRES) = 0.2  
LONGEST FLOWPATH FROM NODE 70.00 TO NODE 73.00 = 10120.50 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 73.00 TO NODE 76.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1146.73 DOWNSTREAM(FEET) = 1146.24  
FLOW LENGTH(FEET) = 52.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 12.0 INCH PIPE IS 3.2 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 3.13  
GIVEN PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 0.53  
PIPE TRAVEL TIME(MIN.) = 0.28 Tc(MIN.) = 5.98  
LONGEST FLOWPATH FROM NODE 70.00 TO NODE 76.00 = 10172.50 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 76.00 TO NODE 76.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 5.98  
RAINFALL INTENSITY(INCH/HR) = 2.59  
TOTAL STREAM AREA(ACRES) = 0.22  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 0.53

\*\*\*\*\*

FLOW PROCESS FROM NODE 77.00 TO NODE 78.00 IS CODE = 22

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

ASSUMED INITIAL SUBAREA UNIFORM  
DEVELOPMENT IS COMMERCIAL  
USER SPECIFIED Tc(MIN.) = 5.000  
10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.787  
COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8841  
SOIL CLASSIFICATION IS "C"

SUBAREA RUNOFF(CFS) = 0.27  
 TOTAL AREA(ACRES) = 0.11 TOTAL RUNOFF(CFS) = 0.27

\*\*\*\*\*

FLOW PROCESS FROM NODE 78.00 TO NODE 76.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<  
 >>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1146.80 DOWNSTREAM(FEET) = 1146.71  
 FLOW LENGTH(FEET) = 18.80 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 12.0 INCH PIPE IS 2.7 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 2.04  
 GIVEN PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 0.27  
 PIPE TRAVEL TIME(MIN.) = 0.15 Tc(MIN.) = 5.15  
 LONGEST FLOWPATH FROM NODE 77.00 TO NODE 76.00 = 10018.80 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 76.00 TO NODE 76.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 5.15  
 RAINFALL INTENSITY(INCH/HR) = 2.75  
 TOTAL STREAM AREA(ACRES) = 0.11  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 0.27

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	0.53	5.98	2.587	0.22
2	0.27	5.15	2.752	0.11

\*\*\*\*\*WARNING\*\*\*\*\*

IN THIS COMPUTER PROGRAM, THE CONFLUENCE VALUE USED IS BASED  
 ON THE RCFC&WCD FORMULA OF PLATE D-1 AS DEFAULT VALUE. THIS FORMULA  
 WILL NOT NECESSARILY RESULT IN THE MAXIMUM VALUE OF PEAK FLOW.

\*\*\*\*\*

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	0.73	5.15	2.752
2	0.78	5.98	2.587

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 0.78 Tc(MIN.) = 5.98  
 TOTAL AREA(ACRES) = 0.3  
 LONGEST FLOWPATH FROM NODE 70.00 TO NODE 76.00 = 10172.50 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 76.00 TO NODE 23.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<  
 >>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1146.24 DOWNSTREAM(FEET) = 1145.22  
 FLOW LENGTH(FEET) = 68.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 12.0 INCH PIPE IS 3.5 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 4.12  
 GIVEN PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 0.78  
 PIPE TRAVEL TIME(MIN.) = 0.28 Tc(MIN.) = 6.26  
 LONGEST FLOWPATH FROM NODE 70.00 TO NODE 23.00 = 10240.50 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 23.00 TO NODE 23.00 IS CODE = 11

>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<<

\*\* MAIN STREAM CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	0.78	6.26	2.539	0.33

LONGEST FLOWPATH FROM NODE 70.00 TO NODE 23.00 = 10240.50 FEET.

\*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	0.76	6.39	2.518	0.33

LONGEST FLOWPATH FROM NODE 20.00 TO NODE 23.00 = 225.00 FEET.

\*\*\*\*\*WARNING\*\*\*\*\*

IN THIS COMPUTER PROGRAM, THE CONFLUENCE VALUE USED IS BASED  
 ON THE RCFC&WCD FORMULA OF PLATE D-1 AS DEFAULT VALUE. THIS FORMULA  
 WILL NOT NECESSARILY RESULT IN THE MAXIMUM VALUE OF PEAK FLOW.

\*\*\*\*\*

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	1.53	6.26	2.539
2	1.54	6.39	2.518

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 1.53 Tc(MIN.) = 6.26  
 TOTAL AREA(ACRES) = 0.7

\*\*\*\*\*

FLOW PROCESS FROM NODE 23.00 TO NODE 23.00 IS CODE = 12

>>>>CLEAR MEMORY BANK # 1 <<<<<

\*\*\*\*\*

FLOW PROCESS FROM NODE 23.00 TO NODE 26.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1144.47 DOWNSTREAM(FEET) = 1143.66  
 FLOW LENGTH(FEET) = 120.60 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 21.0 INCH PIPE IS 4.9 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 3.55  
 GIVEN PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 1.53  
 PIPE TRAVEL TIME(MIN.) = 0.57 Tc(MIN.) = 6.82  
 LONGEST FLOWPATH FROM NODE 70.00 TO NODE 26.00 = 10361.10 FEET.

```

*****
FLOW PROCESS FROM NODE      26.00 TO NODE      26.00 IS CODE =   1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 6.82
RAINFALL INTENSITY(INCH/HR) = 2.45
TOTAL STREAM AREA(ACRES) = 0.66
PEAK FLOW RATE(CFS) AT CONFLUENCE = 1.53

*****
FLOW PROCESS FROM NODE      24.00 TO NODE      25.00 IS CODE =  21
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
=====
      ASSUMED INITIAL SUBAREA UNIFORM
      DEVELOPMENT IS COMMERCIAL
TC = K*[(LENGTH**3)/(ELEVATION CHANGE)]**.2
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00
UPSTREAM ELEVATION(FEET) = 1157.00
DOWNSTREAM ELEVATION(FEET) = 1155.20
ELEVATION DIFFERENCE(FEET) = 1.80
TC = 0.303*[( 100.00**3)/( 1.80)]**.2 = 4.271
COMPUTED TIME OF CONCENTRATION INCREASED TO 5 MIN.
  10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.787
COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8841
SOIL CLASSIFICATION IS "C"
SUBAREA RUNOFF(CFS) = 0.20
TOTAL AREA(ACRES) = 0.08 TOTAL RUNOFF(CFS) = 0.20

*****
FLOW PROCESS FROM NODE      25.00 TO NODE      26.00 IS CODE =  51
-----
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 1155.20 DOWNSTREAM(FEET) = 1152.14
CHANNEL LENGTH THRU SUBAREA(FEET) = 197.00 CHANNEL SLOPE = 0.0155
CHANNEL BASE(FEET) = 0.00 "Z" FACTOR = 99.000
MANNING'S FACTOR = 0.015 MAXIMUM DEPTH(FEET) = 1.00
  10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.346
COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8817
SOIL CLASSIFICATION IS "C"
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.55
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 1.27
AVERAGE FLOW DEPTH(FEET) = 0.07 TRAVEL TIME(MIN.) = 2.58
Tc(MIN.) = 7.58
SUBAREA AREA(ACRES) = 0.34 SUBAREA RUNOFF(CFS) = 0.70
TOTAL AREA(ACRES) = 0.4 PEAK FLOW RATE(CFS) = 0.90

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH(FEET) = 0.08 FLOW VELOCITY(FEET/SEC.) = 1.45
LONGEST FLOWPATH FROM NODE 24.00 TO NODE 26.00 = 297.00 FEET.

*****
FLOW PROCESS FROM NODE      26.00 TO NODE      26.00 IS CODE =  81
-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====
  10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.346

```

COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8817  
 SOIL CLASSIFICATION IS "C"  
 SUBAREA AREA(ACRES) = 0.34 SUBAREA RUNOFF(CFS) = 0.70  
 TOTAL AREA(ACRES) = 0.8 TOTAL RUNOFF(CFS) = 1.60  
 TC(MIN.) = 7.58

\*\*\*\*\*

FLOW PROCESS FROM NODE 26.00 TO NODE 26.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 7.58  
 RAINFALL INTENSITY(INCH/HR) = 2.35  
 TOTAL STREAM AREA(ACRES) = 0.76  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 1.60

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	1.53	6.82	2.450	0.66
2	1.60	7.58	2.346	0.76

\*\*\*\*\*WARNING\*\*\*\*\*

IN THIS COMPUTER PROGRAM, THE CONFLUENCE VALUE USED IS BASED  
 ON THE RCFC&WCD FORMULA OF PLATE D-1 AS DEFAULT VALUE. THIS FORMULA  
 WILL NOT NECESSARILY RESULT IN THE MAXIMUM VALUE OF PEAK FLOW.

\*\*\*\*\*

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	2.98	6.82	2.450
2	3.07	7.58	2.346

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 3.07 Tc(MIN.) = 7.58  
 TOTAL AREA(ACRES) = 1.4  
 LONGEST FLOWPATH FROM NODE 70.00 TO NODE 26.00 = 10361.10 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 30.00 TO NODE 31.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
 >>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1163.00 DOWNSTREAM(FEET) = 1157.00  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 329.00 CHANNEL SLOPE = 0.0182  
 CHANNEL BASE(FEET) = 1.60 "Z" FACTOR = 99.000  
 MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 0.50  
 10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 1.947  
 COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8788  
 SOIL CLASSIFICATION IS "C"  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.14  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 1.28  
 AVERAGE FLOW DEPTH(FEET) = 0.15 TRAVEL TIME(MIN.) = 4.30  
 Tc(MIN.) = 11.87  
 SUBAREA AREA(ACRES) = 0.08 SUBAREA RUNOFF(CFS) = 0.14

```

                                RS_E_10.RES
TOTAL AREA(ACRES) =          1.5          PEAK FLOW RATE(CFS) =          3.21

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH(FEET) = 0.16  FLOW VELOCITY(FEET/SEC.) = 1.21
LONGEST FLOWPATH FROM NODE      70.00 TO NODE      31.00 = 10690.10 FEET.

*****
FLOW PROCESS FROM NODE      31.00 TO NODE      32.00 IS CODE = 41
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 1152.57  DOWNSTREAM(FEET) = 1145.78
FLOW LENGTH(FEET) = 210.50  MANNING'S N = 0.013
DEPTH OF FLOW IN 12.0 INCH PIPE IS 6.1 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 7.99
GIVEN PIPE DIAMETER(INCH) = 12.00  NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 3.21
PIPE TRAVEL TIME(MIN.) = 0.44  Tc(MIN.) = 12.31
LONGEST FLOWPATH FROM NODE      70.00 TO NODE      32.00 = 10900.60 FEET.

*****
FLOW PROCESS FROM NODE      32.00 TO NODE      32.00 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 12.31
RAINFALL INTENSITY(INCH/HR) = 1.92
TOTAL STREAM AREA(ACRES) = 1.50
PEAK FLOW RATE(CFS) AT CONFLUENCE = 3.21

*****
FLOW PROCESS FROM NODE      33.00 TO NODE      34.00 IS CODE = 21
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
=====
    ASSUMED INITIAL SUBAREA UNIFORM
    DEVELOPMENT IS COMMERCIAL
    TC = K*[(LENGTH**3)/(ELEVATION CHANGE)]**.2
    INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00
    UPSTREAM ELEVATION(FEET) = 1162.00
    DOWNSTREAM ELEVATION(FEET) = 1156.99
    ELEVATION DIFFERENCE(FEET) = 5.01
    TC = 0.303*[( 100.00**3)/( 5.01)]**.2 = 3.480
    COMPUTED TIME OF CONCENTRATION INCREASED TO 5 MIN.
    10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.787
    COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8841
    SOIL CLASSIFICATION IS "C"
    SUBAREA RUNOFF(CFS) = 0.15
    TOTAL AREA(ACRES) = 0.06  TOTAL RUNOFF(CFS) = 0.15

*****
FLOW PROCESS FROM NODE      34.00 TO NODE      35.00 IS CODE = 51
-----
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 1156.99  DOWNSTREAM(FEET) = 1150.03
CHANNEL LENGTH THRU SUBAREA(FEET) = 175.00  CHANNEL SLOPE = 0.0398
CHANNEL BASE(FEET) = 0.00  "Z" FACTOR = 99.000
MANNING'S FACTOR = 0.015  MAXIMUM DEPTH(FEET) = 1.00

```

10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.486  
 COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8825  
 SOIL CLASSIFICATION IS "C"  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.58  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 1.84  
 AVERAGE FLOW DEPTH(FEET) = 0.06 TRAVEL TIME(MIN.) = 1.59  
 Tc(MIN.) = 6.59  
 SUBAREA AREA(ACRES) = 0.39 SUBAREA RUNOFF(CFS) = 0.86  
 TOTAL AREA(ACRES) = 0.4 PEAK FLOW RATE(CFS) = 1.00

## END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.07 FLOW VELOCITY(FEET/SEC.) = 1.98  
 LONGEST FLOWPATH FROM NODE 33.00 TO NODE 35.00 = 275.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 35.00 TO NODE 35.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<

=====

10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.486  
 COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8825  
 SOIL CLASSIFICATION IS "C"  
 SUBAREA AREA(ACRES) = 0.39 SUBAREA RUNOFF(CFS) = 0.86  
 TOTAL AREA(ACRES) = 0.8 TOTAL RUNOFF(CFS) = 1.86  
 TC(MIN.) = 6.59

\*\*\*\*\*

FLOW PROCESS FROM NODE 35.00 TO NODE 32.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<

>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1146.37 DOWNSTREAM(FEET) = 1145.76  
 FLOW LENGTH(FEET) = 23.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 4.1 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 6.23  
 GIVEN PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 1.86  
 PIPE TRAVEL TIME(MIN.) = 0.06 Tc(MIN.) = 6.65  
 LONGEST FLOWPATH FROM NODE 33.00 TO NODE 32.00 = 298.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 32.00 TO NODE 32.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 6.65  
 RAINFALL INTENSITY(INCH/HR) = 2.48  
 TOTAL STREAM AREA(ACRES) = 0.84  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 1.86

## \*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	3.21	12.31	1.918	1.50
2	1.86	6.65	2.476	0.84

\*\*\*\*\*WARNING\*\*\*\*\*

IN THIS COMPUTER PROGRAM, THE CONFLUENCE VALUE USED IS BASED  
 ON THE RCFC&WCD FORMULA OF PLATE D-1 AS DEFAULT VALUE. THIS FORMULA

WILL NOT NECESSARILY RESULT IN THE MAXIMUM VALUE OF PEAK FLOW.

\*\*\*\*\*

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	3.59	6.65	2.476
2	4.65	12.31	1.918

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 4.65 Tc(MIN.) = 12.31

TOTAL AREA(ACRES) = 2.3

LONGEST FLOWPATH FROM NODE 70.00 TO NODE 32.00 = 10900.60 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 32.00 TO NODE 36.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<

>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1145.75 DOWNSTREAM(FEET) = 1142.04

FLOW LENGTH(FEET) = 176.00 MANNING'S N = 0.013

DEPTH OF FLOW IN 24.0 INCH PIPE IS 6.2 INCHES

PIPE-FLOW VELOCITY(FEET/SEC.) = 7.26

GIVEN PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 4.65

PIPE TRAVEL TIME(MIN.) = 0.40 Tc(MIN.) = 12.72

LONGEST FLOWPATH FROM NODE 70.00 TO NODE 36.00 = 11076.60 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 36.00 TO NODE 36.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

TOTAL NUMBER OF STREAMS = 2

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:

TIME OF CONCENTRATION(MIN.) = 12.72

RAINFALL INTENSITY(INCH/HR) = 1.89

TOTAL STREAM AREA(ACRES) = 2.34

PEAK FLOW RATE(CFS) AT CONFLUENCE = 4.65

\*\*\*\*\*

FLOW PROCESS FROM NODE 37.00 TO NODE 38.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

ASSUMED INITIAL SUBAREA UNIFORM

DEVELOPMENT IS COMMERCIAL

TC = K\*[(LENGTH\*\*3)/(ELEVATION CHANGE)]\*\*.2

INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00

UPSTREAM ELEVATION(FEET) = 1166.00

DOWNSTREAM ELEVATION(FEET) = 1158.49

ELEVATION DIFFERENCE(FEET) = 7.51

TC = 0.303\*[(100.00\*\*3)/(7.51)]\*\*.2 = 3.210

COMPUTED TIME OF CONCENTRATION INCREASED TO 5 MIN.

10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.787

COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8841

SOIL CLASSIFICATION IS "C"

SUBAREA RUNOFF(CFS) = 0.30

TOTAL AREA(ACRES) = 0.12 TOTAL RUNOFF(CFS) = 0.30



\*\*\*\*\*

FLOW PROCESS FROM NODE 38.00 TO NODE 39.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<

>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1158.49 DOWNSTREAM(FEET) = 1150.00

CHANNEL LENGTH THRU SUBAREA(FEET) = 282.00 CHANNEL SLOPE = 0.0301

CHANNEL BASE(FEET) = 0.00 "Z" FACTOR = 99.000

MANNING'S FACTOR = 0.015 MAXIMUM DEPTH(FEET) = 1.00

10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.344

COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8817

SOIL CLASSIFICATION IS "C"

TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.78

TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 1.81

AVERAGE FLOW DEPTH(FEET) = 0.07 TRAVEL TIME(MIN.) = 2.59

Tc(MIN.) = 7.59

SUBAREA AREA(ACRES) = 0.47 SUBAREA RUNOFF(CFS) = 0.97

TOTAL AREA(ACRES) = 0.6 PEAK FLOW RATE(CFS) = 1.27

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.08 FLOW VELOCITY(FEET/SEC.) = 2.04

LONGEST FLOWPATH FROM NODE 37.00 TO NODE 39.00 = 382.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 39.00 TO NODE 39.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<

10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.344

COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8817

SOIL CLASSIFICATION IS "C"

SUBAREA AREA(ACRES) = 0.47 SUBAREA RUNOFF(CFS) = 0.97

TOTAL AREA(ACRES) = 1.1 TOTAL RUNOFF(CFS) = 2.24

TC(MIN.) = 7.59

\*\*\*\*\*

FLOW PROCESS FROM NODE 39.00 TO NODE 36.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<

>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1144.36 DOWNSTREAM(FEET) = 1142.28

FLOW LENGTH(FEET) = 9.50 MANNING'S N = 0.013

DEPTH OF FLOW IN 18.0 INCH PIPE IS 2.6 INCHES

PIPE-FLOW VELOCITY(FEET/SEC.) = 13.85

GIVEN PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 2.24

PIPE TRAVEL TIME(MIN.) = 0.01 Tc(MIN.) = 7.60

LONGEST FLOWPATH FROM NODE 37.00 TO NODE 36.00 = 391.50 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 36.00 TO NODE 36.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<

TOTAL NUMBER OF STREAMS = 2

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:

TIME OF CONCENTRATION(MIN.) = 7.60

RAINFALL INTENSITY(INCH/HR) = 2.34

TOTAL STREAM AREA(ACRES) = 1.06

RS\_E\_10.RES  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 2.24

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	4.65	12.72	1.893	2.34
2	2.24	7.60	2.342	1.06

\*\*\*\*\*WARNING\*\*\*\*\*  
IN THIS COMPUTER PROGRAM, THE CONFLUENCE VALUE USED IS BASED  
ON THE RCFC&WCD FORMULA OF PLATE D-1 AS DEFAULT VALUE. THIS FORMULA  
WILL NOT NECESSARILY RESULT IN THE MAXIMUM VALUE OF PEAK FLOW.  
\*\*\*\*\*

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	5.02	7.60	2.342
2	6.46	12.72	1.893

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 6.46 Tc(MIN.) = 12.72  
TOTAL AREA(ACRES) = 3.4  
LONGEST FLOWPATH FROM NODE 70.00 TO NODE 36.00 = 11076.60 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 36.00 TO NODE 40.00 IS CODE = 41  
-----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<  
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1141.91 DOWNSTREAM(FEET) = 1141.39  
FLOW LENGTH(FEET) = 33.70 MANNING'S N = 0.013  
DEPTH OF FLOW IN 24.0 INCH PIPE IS 7.9 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 7.13  
GIVEN PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 6.46  
PIPE TRAVEL TIME(MIN.) = 0.08 Tc(MIN.) = 12.79  
LONGEST FLOWPATH FROM NODE 70.00 TO NODE 40.00 = 11110.30 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 40.00 TO NODE 40.00 IS CODE = 10  
-----

>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<

\*\*\*\*\*  
FLOW PROCESS FROM NODE 41.00 TO NODE 42.00 IS CODE = 21  
-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

=====

ASSUMED INITIAL SUBAREA UNIFORM  
DEVELOPMENT IS COMMERCIAL  
TC =  $K * [(LENGTH ** 3) / (ELEVATION CHANGE)] ** .2$   
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
UPSTREAM ELEVATION(FEET) = 1166.00  
DOWNSTREAM ELEVATION(FEET) = 1158.65  
ELEVATION DIFFERENCE(FEET) = 7.35  
TC =  $0.303 * [(100.00 ** 3) / (7.35)] ** .2 = 3.224$   
COMPUTED TIME OF CONCENTRATION INCREASED TO 5 MIN.

```

                                RS_E_10.RES
    10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.787
    COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8841
    SOIL CLASSIFICATION IS "C"
    SUBAREA RUNOFF(CFS) = 0.27
    TOTAL AREA(ACRES) = 0.11 TOTAL RUNOFF(CFS) = 0.27

*****
FLOW PROCESS FROM NODE 42.00 TO NODE 43.00 IS CODE = 51
-----
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 1158.65 DOWNSTREAM(FEET) = 1151.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 236.00 CHANNEL SLOPE = 0.0324
CHANNEL BASE(FEET) = 0.00 "Z" FACTOR = 99.000
MANNING'S FACTOR = 0.015 MAXIMUM DEPTH(FEET) = 1.00
    10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.379
    COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8819
    SOIL CLASSIFICATION IS "C"
    TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.57
    TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 1.69
    AVERAGE FLOW DEPTH(FEET) = 0.06 TRAVEL TIME(MIN.) = 2.32
    Tc(MIN.) = 7.32
    SUBAREA AREA(ACRES) = 0.28 SUBAREA RUNOFF(CFS) = 0.59
    TOTAL AREA(ACRES) = 0.4 PEAK FLOW RATE(CFS) = 0.86

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH(FEET) = 0.07 FLOW VELOCITY(FEET/SEC.) = 2.00
LONGEST FLOWPATH FROM NODE 41.00 TO NODE 43.00 = 336.00 FEET.

*****
FLOW PROCESS FROM NODE 43.00 TO NODE 43.00 IS CODE = 81
-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====
    10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.379
    COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8819
    SOIL CLASSIFICATION IS "C"
    SUBAREA AREA(ACRES) = 0.29 SUBAREA RUNOFF(CFS) = 0.60
    TOTAL AREA(ACRES) = 0.7 TOTAL RUNOFF(CFS) = 1.46
    TC(MIN.) = 7.32

*****
FLOW PROCESS FROM NODE 43.00 TO NODE 80.00 IS CODE = 31
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 1146.61 DOWNSTREAM(FEET) = 1143.76
FLOW LENGTH(FEET) = 8.30 MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 8.000
DEPTH OF FLOW IN 8.0 INCH PIPE IS 2.5 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 15.66
ESTIMATED PIPE DIAMETER(INCH) = 8.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 1.46
PIPE TRAVEL TIME(MIN.) = 0.01 Tc(MIN.) = 7.33
LONGEST FLOWPATH FROM NODE 41.00 TO NODE 80.00 = 344.30 FEET.

*****
FLOW PROCESS FROM NODE 80.00 TO NODE 80.00 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
=====

```

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
 TIME OF CONCENTRATION(MIN.) = 7.33  
 RAINFALL INTENSITY(INCH/HR) = 2.38  
 TOTAL STREAM AREA(ACRES) = 0.68  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 1.46

\*\*\*\*\*

FLOW PROCESS FROM NODE 44.00 TO NODE 45.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

ASSUMED INITIAL SUBAREA UNIFORM

DEVELOPMENT IS COMMERCIAL

TC =  $K * [(LENGTH ** 3) / (ELEVATION \text{ CHANGE})] ** .2$

INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00

UPSTREAM ELEVATION(FEET) = 1155.93

DOWNSTREAM ELEVATION(FEET) = 1153.39

ELEVATION DIFFERENCE(FEET) = 2.54

TC =  $0.303 * [(100.00 ** 3) / (2.54)] ** .2 = 3.987$

COMPUTED TIME OF CONCENTRATION INCREASED TO 5 MIN.

10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.787

COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8841

SOIL CLASSIFICATION IS "C"

SUBAREA RUNOFF(CFS) = 0.15

TOTAL AREA(ACRES) = 0.06 TOTAL RUNOFF(CFS) = 0.15

\*\*\*\*\*

FLOW PROCESS FROM NODE 45.00 TO NODE 46.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1153.39 DOWNSTREAM(FEET) = 1150.99

CHANNEL LENGTH THRU SUBAREA(FEET) = 74.30 CHANNEL SLOPE = 0.0323

CHANNEL BASE(FEET) = 0.00 "Z" FACTOR = 99.000

MANNING'S FACTOR = 0.015 MAXIMUM DEPTH(FEET) = 1.00

10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.572

COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8830

SOIL CLASSIFICATION IS "C"

TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.19

TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 1.16

AVERAGE FLOW DEPTH(FEET) = 0.04 TRAVEL TIME(MIN.) = 1.07

Tc(MIN.) = 6.07

SUBAREA AREA(ACRES) = 0.04 SUBAREA RUNOFF(CFS) = 0.09

TOTAL AREA(ACRES) = 0.1 PEAK FLOW RATE(CFS) = 0.24

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.04 FLOW VELOCITY(FEET/SEC.) = 1.31

LONGEST FLOWPATH FROM NODE 44.00 TO NODE 46.00 = 174.30 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 46.00 TO NODE 46.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.572

COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8830

SOIL CLASSIFICATION IS "C"

SUBAREA AREA(ACRES) = 0.04 SUBAREA RUNOFF(CFS) = 0.09

TOTAL AREA(ACRES) = 0.1 TOTAL RUNOFF(CFS) = 0.33

TC(MIN.) = 6.07

\*\*\*\*\*

FLOW PROCESS FROM NODE 46.00 TO NODE 80.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<  
 >>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1145.97 DOWNSTREAM(FEET) = 1144.76  
 FLOW LENGTH(FEET) = 57.10 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 12.0 INCH PIPE IS 2.1 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 3.63  
 GIVEN PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 0.33  
 PIPE TRAVEL TIME(MIN.) = 0.26 Tc(MIN.) = 6.33  
 LONGEST FLOWPATH FROM NODE 44.00 TO NODE 80.00 = 231.40 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 80.00 TO NODE 80.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 6.33  
 RAINFALL INTENSITY(INCH/HR) = 2.53  
 TOTAL STREAM AREA(ACRES) = 0.14  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 0.33

## \*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	1.46	7.33	2.378	0.68
2	0.33	6.33	2.527	0.14

\*\*\*\*\*WARNING\*\*\*\*\*

IN THIS COMPUTER PROGRAM, THE CONFLUENCE VALUE USED IS BASED  
 ON THE RCFC&WCD FORMULA OF PLATE D-1 AS DEFAULT VALUE. THIS FORMULA  
 WILL NOT NECESSARILY RESULT IN THE MAXIMUM VALUE OF PEAK FLOW.

\*\*\*\*\*

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

## \*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	1.59	6.33	2.527
2	1.77	7.33	2.378

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 1.77 Tc(MIN.) = 7.33  
 TOTAL AREA(ACRES) = 0.8  
 LONGEST FLOWPATH FROM NODE 41.00 TO NODE 80.00 = 344.30 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 80.00 TO NODE 40.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<  
 >>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1143.76 DOWNSTREAM(FEET) = 1141.39  
 FLOW LENGTH(FEET) = 81.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 24.0 INCH PIPE IS 3.5 INCHES

PIPE-FLOW VELOCITY(FEET/SEC.) = 6.15  
 GIVEN PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 1.77  
 PIPE TRAVEL TIME(MIN.) = 0.22 Tc(MIN.) = 7.55  
 LONGEST FLOWPATH FROM NODE 41.00 TO NODE 40.00 = 425.30 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 40.00 TO NODE 40.00 IS CODE = 11

>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<

=====

\*\* MAIN STREAM CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	1.77	7.55	2.349	0.82

LONGEST FLOWPATH FROM NODE 41.00 TO NODE 40.00 = 425.30 FEET.

\*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	6.46	12.79	1.888	3.40

LONGEST FLOWPATH FROM NODE 70.00 TO NODE 40.00 = 11110.30 FEET.

\*\*\*\*\*WARNING\*\*\*\*\*

IN THIS COMPUTER PROGRAM, THE CONFLUENCE VALUE USED IS BASED  
 ON THE RCFC&WCD FORMULA OF PLATE D-1 AS DEFAULT VALUE. THIS FORMULA  
 WILL NOT NECESSARILY RESULT IN THE MAXIMUM VALUE OF PEAK FLOW.

\*\*\*\*\*

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	5.58	7.55	2.349
2	7.88	12.79	1.888

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 7.88 Tc(MIN.) = 12.79  
 TOTAL AREA(ACRES) = 4.2

\*\*\*\*\*

FLOW PROCESS FROM NODE 40.00 TO NODE 40.00 IS CODE = 12

>>>>CLEAR MEMORY BANK # 1 <<<<

=====

\*\*\*\*\*

FLOW PROCESS FROM NODE 40.00 TO NODE 47.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<

>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1141.38 DOWNSTREAM(FEET) = 1138.35  
 FLOW LENGTH(FEET) = 210.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 24.0 INCH PIPE IS 9.0 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 7.35  
 GIVEN PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 7.88  
 PIPE TRAVEL TIME(MIN.) = 0.48 Tc(MIN.) = 13.27  
 LONGEST FLOWPATH FROM NODE 70.00 TO NODE 47.00 = 11320.30 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 47.00 TO NODE 48.00 IS CODE = 41

```

>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

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```

=====
ELEVATION DATA: UPSTREAM(FEET) = 1135.35 DOWNSTREAM(FEET) = 1134.95
FLOW LENGTH(FEET) = 25.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 60.0 INCH PIPE IS 6.5 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 6.89
GIVEN PIPE DIAMETER(INCH) = 60.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 7.88
PIPE TRAVEL TIME(MIN.) = 0.06 Tc(MIN.) = 13.33
LONGEST FLOWPATH FROM NODE 70.00 TO NODE 48.00 = 11345.30 FEET.

```

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*****

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FLOW PROCESS FROM NODE 48.00 TO NODE 48.00 IS CODE = 1

```

```

>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

```

```

=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 13.33
RAINFALL INTENSITY(INCH/HR) = 1.86
TOTAL STREAM AREA(ACRES) = 4.22
PEAK FLOW RATE(CFS) AT CONFLUENCE = 7.88

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*****

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```

FLOW PROCESS FROM NODE 49.00 TO NODE 63.00 IS CODE = 22

```

```

>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

```

```

=====
ASSUMED INITIAL SUBAREA UNIFORM
DEVELOPMENT IS COMMERCIAL
USER SPECIFIED Tc(MIN.) = 5.000
10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.787
COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8841
SOIL CLASSIFICATION IS "C"
SUBAREA RUNOFF(CFS) = 0.34
TOTAL AREA(ACRES) = 0.14 TOTAL RUNOFF(CFS) = 0.34

```

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*****

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FLOW PROCESS FROM NODE 63.00 TO NODE 50.00 IS CODE = 51

```

```

>>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
>>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

```

```

=====
ELEVATION DATA: UPSTREAM(FEET) = 1152.00 DOWNSTREAM(FEET) = 1149.03
CHANNEL LENGTH THRU SUBAREA(FEET) = 94.00 CHANNEL SLOPE = 0.0316
CHANNEL BASE(FEET) = 0.00 "Z" FACTOR = 99.000
MANNING'S FACTOR = 0.015 MAXIMUM DEPTH(FEET) = 1.00
10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.576
COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8830
SOIL CLASSIFICATION IS "C"
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.47
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 1.50
AVERAGE FLOW DEPTH(FEET) = 0.06 TRAVEL TIME(MIN.) = 1.04
Tc(MIN.) = 6.04
SUBAREA AREA(ACRES) = 0.11 SUBAREA RUNOFF(CFS) = 0.25
TOTAL AREA(ACRES) = 0.2 PEAK FLOW RATE(CFS) = 0.60

```

```

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH(FEET) = 0.06 FLOW VELOCITY(FEET/SEC.) = 1.78
LONGEST FLOWPATH FROM NODE 49.00 TO NODE 50.00 = 1000094.00 FEET.

```

\*\*\*\*\*

FLOW PROCESS FROM NODE 50.00 TO NODE 50.00 IS CODE = 81

&gt;&gt;&gt;&gt;ADDITION OF SUBAREA TO MAINLINE PEAK FLOW&lt;&lt;&lt;&lt;

=====

10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.576  
 COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8830  
 SOIL CLASSIFICATION IS "C"  
 SUBAREA AREA(ACRES) = 0.11 SUBAREA RUNOFF(CFS) = 0.25  
 TOTAL AREA(ACRES) = 0.4 TOTAL RUNOFF(CFS) = 0.85  
 TC(MIN.) = 6.04

\*\*\*\*\*

FLOW PROCESS FROM NODE 50.00 TO NODE 48.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<  
 >>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<

=====

ELEVATION DATA: UPSTREAM(Feet) = 1145.74 DOWNSTREAM(Feet) = 1136.51  
 FLOW LENGTH(Feet) = 24.30 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 1.5 INCHES  
 PIPE-FLOW VELOCITY(Feet/Sec.) = 12.53  
 GIVEN PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 0.85  
 PIPE TRAVEL TIME(MIN.) = 0.03 Tc(MIN.) = 6.08  
 LONGEST FLOWPATH FROM NODE 49.00 TO NODE 48.00 = 1000118.31 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 48.00 TO NODE 48.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 6.08  
 RAINFALL INTENSITY(INCH/HR) = 2.57  
 TOTAL STREAM AREA(ACRES) = 0.36  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 0.85

## \*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	7.88	13.33	1.856	4.22
2	0.85	6.08	2.570	0.36

\*\*\*\*\*WARNING\*\*\*\*\*

IN THIS COMPUTER PROGRAM, THE CONFLUENCE VALUE USED IS BASED  
 ON THE RCFC&WCD FORMULA OF PLATE D-1 AS DEFAULT VALUE. THIS FORMULA  
 WILL NOT NECESSARILY RESULT IN THE MAXIMUM VALUE OF PEAK FLOW.

\*\*\*\*\*

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

## \*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	4.44	6.08	2.570
2	8.49	13.33	1.856

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 8.49 Tc(MIN.) = 13.33



TOTAL AREA(ACRES) = 4.6  
 LONGEST FLOWPATH FROM NODE 49.00 TO NODE 48.00 = 1000118.31 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 48.00 TO NODE 51.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<  
 >>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1134.95 DOWNSTREAM(FEET) = 1132.94  
 FLOW LENGTH(FEET) = 126.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 60.0 INCH PIPE IS 6.7 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 7.04  
 GIVEN PIPE DIAMETER(INCH) = 60.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 8.49  
 PIPE TRAVEL TIME(MIN.) = 0.30 Tc(MIN.) = 13.63  
 LONGEST FLOWPATH FROM NODE 49.00 TO NODE 51.00 = 1000244.31 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 51.00 TO NODE 51.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
 TIME OF CONCENTRATION(MIN.) = 13.63  
 RAINFALL INTENSITY(INCH/HR) = 1.84  
 TOTAL STREAM AREA(ACRES) = 4.58  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 8.49

\*\*\*\*\*

FLOW PROCESS FROM NODE 51.00 TO NODE 53.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

=====

ASSUMED INITIAL SUBAREA UNIFORM  
 DEVELOPMENT IS COMMERCIAL  
 $TC = K * [(LENGTH ** 3) / (ELEVATION CHANGE)] ** .2$   
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
 UPSTREAM ELEVATION(FEET) = 1151.89  
 DOWNSTREAM ELEVATION(FEET) = 1149.00  
 ELEVATION DIFFERENCE(FEET) = 2.89  
 $TC = 0.303 * [(100.00 ** 3) / (2.89)] ** .2 = 3.885$   
 COMPUTED TIME OF CONCENTRATION INCREASED TO 5 MIN.  
 10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.787  
 COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8841  
 SOIL CLASSIFICATION IS "C"  
 SUBAREA RUNOFF(CFS) = 0.34  
 TOTAL AREA(ACRES) = 0.14 TOTAL RUNOFF(CFS) = 0.34

\*\*\*\*\*

FLOW PROCESS FROM NODE 53.00 TO NODE 51.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<  
 >>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1145.16 DOWNSTREAM(FEET) = 1144.09  
 FLOW LENGTH(FEET) = 76.70 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 12.0 INCH PIPE IS 2.4 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 3.15  
 GIVEN PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 0.34  
 PIPE TRAVEL TIME(MIN.) = 0.41 Tc(MIN.) = 5.41

```

                                RS_E_10.RES
LONGEST FLOWPATH FROM NODE      51.00 TO NODE      51.00 =      176.70 FEET.

*****
FLOW PROCESS FROM NODE      51.00 TO NODE      51.00 IS CODE =      1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<
=====
TOTAL NUMBER OF STREAMS =      2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM      2 ARE:
TIME OF CONCENTRATION(MIN.) =      5.41
RAINFALL INTENSITY(INCH/HR) =      2.70
TOTAL STREAM AREA(ACRES) =      0.14
PEAK FLOW RATE(CFS) AT CONFLUENCE =      0.34

** CONFLUENCE DATA **
STREAM      RUNOFF      Tc      INTENSITY      AREA
NUMBER      (CFS)      (MIN.)      (INCH/HR)      (ACRE)
      1      8.49      13.63      1.839      4.58
      2      0.34      5.41      2.698      0.14

*****WARNING*****
IN THIS COMPUTER PROGRAM, THE CONFLUENCE VALUE USED IS BASED
ON THE RCFC&WCD FORMULA OF PLATE D-1 AS DEFAULT VALUE. THIS FORMULA
WILL NOT NECESSARILY RESULT IN THE MAXIMUM VALUE OF PEAK FLOW.
*****

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR      2 STREAMS.

** PEAK FLOW RATE TABLE **
STREAM      RUNOFF      Tc      INTENSITY
NUMBER      (CFS)      (MIN.)      (INCH/HR)
      1      3.71      5.41      2.698
      2      8.73      13.63      1.839

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
PEAK FLOW RATE(CFS) =      8.73      Tc(MIN.) =      13.63
TOTAL AREA(ACRES) =      4.7
LONGEST FLOWPATH FROM NODE      49.00 TO NODE      51.00 = 1000244.31 FEET.

*****
FLOW PROCESS FROM NODE      51.00 TO NODE      54.00 IS CODE =      41
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<
=====
ELEVATION DATA: UPSTREAM(Feet) = 1132.94 DOWNSTREAM(Feet) = 1131.53
FLOW LENGTH(Feet) =      23.50 MANNING'S N = 0.013
DEPTH OF FLOW IN 60.0 INCH PIPE IS 5.0 INCHES
PIPE-FLOW VELOCITY(Feet/Sec.) = 11.27
GIVEN PIPE DIAMETER(INCH) = 60.00 NUMBER OF PIPES =      1
PIPE-FLOW(CFS) =      8.73
PIPE TRAVEL TIME(MIN.) = 0.03 Tc(MIN.) = 13.66
LONGEST FLOWPATH FROM NODE      49.00 TO NODE      54.00 = 1000267.81 FEET.

*****
FLOW PROCESS FROM NODE      54.00 TO NODE      54.00 IS CODE =      1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
=====
TOTAL NUMBER OF STREAMS =      2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM      1 ARE:

```

TIME OF CONCENTRATION(MIN.) = 13.66  
 RAINFALL INTENSITY(INCH/HR) = 1.84  
 TOTAL STREAM AREA(ACRES) = 4.72  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 8.73

\*\*\*\*\*

FLOW PROCESS FROM NODE 55.00 TO NODE 56.00 IS CODE = 22

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

=====

ASSUMED INITIAL SUBAREA UNIFORM  
 DEVELOPMENT IS COMMERCIAL  
 USER SPECIFIED Tc(MIN.) = 5.000  
 10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.787  
 COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8841  
 SOIL CLASSIFICATION IS "C"  
 SUBAREA RUNOFF(CFS) = 0.15  
 TOTAL AREA(ACRES) = 0.06 TOTAL RUNOFF(CFS) = 0.15

\*\*\*\*\*

FLOW PROCESS FROM NODE 56.00 TO NODE 57.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<  
 >>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1151.99 DOWNSTREAM(FEET) = 1151.26  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 60.00 CHANNEL SLOPE = 0.0122  
 CHANNEL BASE(FEET) = 0.00 "Z" FACTOR = 99.000  
 MANNING'S FACTOR = 0.015 MAXIMUM DEPTH(FEET) = 1.00  
 10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.571  
 COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8830  
 SOIL CLASSIFICATION IS "C"  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.17  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 0.94  
 AVERAGE FLOW DEPTH(FEET) = 0.04 TRAVEL TIME(MIN.) = 1.07  
 Tc(MIN.) = 6.07  
 SUBAREA AREA(ACRES) = 0.02 SUBAREA RUNOFF(CFS) = 0.05  
 TOTAL AREA(ACRES) = 0.1 PEAK FLOW RATE(CFS) = 0.19

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.05 FLOW VELOCITY(FEET/SEC.) = 0.83  
 LONGEST FLOWPATH FROM NODE 55.00 TO NODE 57.00 = \*\*\*\*\* FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 57.00 TO NODE 57.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<

=====

10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.571  
 COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8830  
 SOIL CLASSIFICATION IS "C"  
 SUBAREA AREA(ACRES) = 0.02 SUBAREA RUNOFF(CFS) = 0.05  
 TOTAL AREA(ACRES) = 0.1 TOTAL RUNOFF(CFS) = 0.24  
 TC(MIN.) = 6.07

\*\*\*\*\*

FLOW PROCESS FROM NODE 57.00 TO NODE 54.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<  
 >>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1145.14 DOWNSTREAM(FEET) = 1135.70  
 FLOW LENGTH(FEET) = 103.00 MANNING'S N = 0.013

DEPTH OF FLOW IN 10.0 INCH PIPE IS 1.3 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 5.62  
 GIVEN PIPE DIAMETER(INCH) = 10.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 0.24  
 PIPE TRAVEL TIME(MIN.) = 0.31 Tc(MIN.) = 6.37  
 LONGEST FLOWPATH FROM NODE 55.00 TO NODE 54.00 = \*\*\*\*\* FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 54.00 TO NODE 54.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 6.37  
 RAINFALL INTENSITY(INCH/HR) = 2.52  
 TOTAL STREAM AREA(ACRES) = 0.10  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 0.24

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	8.73	13.66	1.837	4.72
2	0.24	6.37	2.520	0.10

\*\*\*\*\*WARNING\*\*\*\*\*

IN THIS COMPUTER PROGRAM, THE CONFLUENCE VALUE USED IS BASED  
 ON THE RCFC&WCD FORMULA OF PLATE D-1 AS DEFAULT VALUE. THIS FORMULA  
 WILL NOT NECESSARILY RESULT IN THE MAXIMUM VALUE OF PEAK FLOW.

\*\*\*\*\*

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	4.31	6.37	2.520
2	8.90	13.66	1.837

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 8.90 Tc(MIN.) = 13.66  
 TOTAL AREA(ACRES) = 4.8  
 LONGEST FLOWPATH FROM NODE 55.00 TO NODE 54.00 = \*\*\*\*\* FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 54.00 TO NODE 58.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1131.53 DOWNSTREAM(FEET) = 1130.68  
 FLOW LENGTH(FEET) = 197.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 60.0 INCH PIPE IS 9.4 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 4.51  
 GIVEN PIPE DIAMETER(INCH) = 60.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 8.90  
 PIPE TRAVEL TIME(MIN.) = 0.73 Tc(MIN.) = 14.39  
 LONGEST FLOWPATH FROM NODE 55.00 TO NODE 58.00 = \*\*\*\*\* FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 58.00 TO NODE 58.00 IS CODE = 1

-----  
 >>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<  
 =====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
 TIME OF CONCENTRATION(MIN.) = 14.39  
 RAINFALL INTENSITY(INCH/HR) = 1.80  
 TOTAL STREAM AREA(ACRES) = 4.82  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 8.90

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 59.00 TO NODE 60.00 IS CODE = 22  
 -----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<  
 =====

ASSUMED INITIAL SUBAREA UNIFORM  
 DEVELOPMENT IS COMMERCIAL  
 USER SPECIFIED Tc(MIN.) = 5.000  
 10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.787  
 COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8841  
 SOIL CLASSIFICATION IS "C"  
 SUBAREA RUNOFF(CFS) = 0.15  
 TOTAL AREA(ACRES) = 0.06 TOTAL RUNOFF(CFS) = 0.15

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 60.00 TO NODE 61.00 IS CODE = 51  
 -----

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<  
 >>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<  
 =====

ELEVATION DATA: UPSTREAM(FEET) = 1151.99 DOWNSTREAM(FEET) = 1145.05  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 285.00 CHANNEL SLOPE = 0.0244  
 CHANNEL BASE(FEET) = 0.00 "Z" FACTOR = 99.000  
 MANNING'S FACTOR = 0.015 MAXIMUM DEPTH(FEET) = 1.00  
 10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.307  
 COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8815  
 SOIL CLASSIFICATION IS "C"  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.55  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 1.65  
 AVERAGE FLOW DEPTH(FEET) = 0.06 TRAVEL TIME(MIN.) = 2.88  
 Tc(MIN.) = 7.88  
 SUBAREA AREA(ACRES) = 0.40 SUBAREA RUNOFF(CFS) = 0.81  
 TOTAL AREA(ACRES) = 0.5 PEAK FLOW RATE(CFS) = 0.96

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.07 FLOW VELOCITY(FEET/SEC.) = 1.80  
 LONGEST FLOWPATH FROM NODE 59.00 TO NODE 61.00 = 319.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 61.00 TO NODE 61.00 IS CODE = 81  
 -----

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<  
 =====

10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.307  
 COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8815  
 SOIL CLASSIFICATION IS "C"  
 SUBAREA AREA(ACRES) = 0.40 SUBAREA RUNOFF(CFS) = 0.81  
 TOTAL AREA(ACRES) = 0.9 TOTAL RUNOFF(CFS) = 1.77  
 TC(MIN.) = 7.88

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 61.00 TO NODE 58.00 IS CODE = 31  
 -----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

```
=====
ELEVATION DATA: UPSTREAM(FEET) = 1140.87  DOWNSTREAM(FEET) = 1140.80
FLOW LENGTH(FEET) = 14.00  MANNING'S N = 0.013
DEPTH OF FLOW IN 12.0 INCH PIPE IS 7.6 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 3.40
ESTIMATED PIPE DIAMETER(INCH) = 12.00  NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 1.77
PIPE TRAVEL TIME(MIN.) = 0.07  Tc(MIN.) = 7.95
LONGEST FLOWPATH FROM NODE 59.00 TO NODE 58.00 = 333.00 FEET.
```

\*\*\*\*\*

FLOW PROCESS FROM NODE 58.00 TO NODE 58.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<

```
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 7.95
RAINFALL INTENSITY(INCH/HR) = 2.30
TOTAL STREAM AREA(ACRES) = 0.86
PEAK FLOW RATE(CFS) AT CONFLUENCE = 1.77
```

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	8.90	14.39	1.798	4.82
2	1.77	7.95	2.299	0.86

\*\*\*\*\*WARNING\*\*\*\*\*

IN THIS COMPUTER PROGRAM, THE CONFLUENCE VALUE USED IS BASED  
 ON THE RCFC&WCD FORMULA OF PLATE D-1 AS DEFAULT VALUE. THIS FORMULA  
 WILL NOT NECESSARILY RESULT IN THE MAXIMUM VALUE OF PEAK FLOW.

\*\*\*\*\*

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	6.69	7.95	2.299
2	10.29	14.39	1.798

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

```
PEAK FLOW RATE(CFS) = 10.29  Tc(MIN.) = 14.39
TOTAL AREA(ACRES) = 5.7
LONGEST FLOWPATH FROM NODE 55.00 TO NODE 58.00 = ***** FEET.
```

\*\*\*\*\*

FLOW PROCESS FROM NODE 58.00 TO NODE 62.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<  
 >>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<

```
=====
ELEVATION DATA: UPSTREAM(FEET) = 1130.68  DOWNSTREAM(FEET) = 1130.30
FLOW LENGTH(FEET) = 86.00  MANNING'S N = 0.013
DEPTH OF FLOW IN 60.0 INCH PIPE IS 10.0 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 4.75
GIVEN PIPE DIAMETER(INCH) = 60.00  NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 10.29
```

```

                                RS_E_10.RES
PIPE TRAVEL TIME(MIN.) =    0.30    Tc(MIN.) =    14.69
LONGEST FLOWPATH FROM NODE    55.00 TO NODE    62.00 = ***** FEET.

*****
FLOW PROCESS FROM NODE    62.00 TO NODE    62.00 IS CODE = 10
-----
>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<
=====
*****
FLOW PROCESS FROM NODE    64.00 TO NODE    65.00 IS CODE = 21
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
=====
    ASSUMED INITIAL SUBAREA UNIFORM
    DEVELOPMENT IS COMMERCIAL
    TC = K*[(LENGTH**3)/(ELEVATION CHANGE)]**.2
    INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00
    UPSTREAM ELEVATION(FEET) = 1154.94
    DOWNSTREAM ELEVATION(FEET) = 1151.51
    ELEVATION DIFFERENCE(FEET) = 3.43
    TC = 0.303*[( 100.00**3)/( 3.43)]**.2 = 3.754
    COMPUTED TIME OF CONCENTRATION INCREASED TO 5 MIN.
    10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.787
    COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8841
    SOIL CLASSIFICATION IS "C"
    SUBAREA RUNOFF(CFS) = 0.20
    TOTAL AREA(ACRES) = 0.08    TOTAL RUNOFF(CFS) = 0.20

*****
FLOW PROCESS FROM NODE    65.00 TO NODE    66.00 IS CODE = 51
-----
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 1151.51    DOWNSTREAM(FEET) = 1146.98
CHANNEL LENGTH THRU SUBAREA(FEET) = 260.00    CHANNEL SLOPE = 0.0174
CHANNEL BASE(FEET) = 0.00    "Z" FACTOR = 99.000
MANNING'S FACTOR = 0.015    MAXIMUM DEPTH(FEET) = 1.00
    10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.259
    COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8811
    SOIL CLASSIFICATION IS "C"
    TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.56
    TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 1.32
    AVERAGE FLOW DEPTH(FEET) = 0.07    TRAVEL TIME(MIN.) = 3.29
    Tc(MIN.) = 8.29
    SUBAREA AREA(ACRES) = 0.37    SUBAREA RUNOFF(CFS) = 0.74
    TOTAL AREA(ACRES) = 0.4    PEAK FLOW RATE(CFS) = 0.93

    END OF SUBAREA CHANNEL FLOW HYDRAULICS:
    DEPTH(FEET) = 0.08    FLOW VELOCITY(FEET/SEC.) = 1.51
    LONGEST FLOWPATH FROM NODE    64.00 TO NODE    66.00 = 360.00 FEET.

*****
FLOW PROCESS FROM NODE    66.00 TO NODE    66.00 IS CODE = 81
-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====
    10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.259
    COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8811
    SOIL CLASSIFICATION IS "C"
    SUBAREA AREA(ACRES) = 0.37    SUBAREA RUNOFF(CFS) = 0.74
    TOTAL AREA(ACRES) = 0.8    TOTAL RUNOFF(CFS) = 1.67

```

TC(MIN.) = 8.29

\*\*\*\*\*

FLOW PROCESS FROM NODE 66.00 TO NODE 66.00 IS CODE = 1

&gt;&gt;&gt;&gt;DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE&lt;&lt;&lt;&lt;&lt;

=====

TOTAL NUMBER OF STREAMS = 2

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:

TIME OF CONCENTRATION(MIN.) = 8.29

RAINFALL INTENSITY(INCH/HR) = 2.26

TOTAL STREAM AREA(ACRES) = 0.82

PEAK FLOW RATE(CFS) AT CONFLUENCE = 1.67

\*\*\*\*\*

FLOW PROCESS FROM NODE 67.00 TO NODE 68.00 IS CODE = 22

&gt;&gt;&gt;&gt;RATIONAL METHOD INITIAL SUBAREA ANALYSIS&lt;&lt;&lt;&lt;&lt;

=====

ASSUMED INITIAL SUBAREA UNIFORM

DEVELOPMENT IS COMMERCIAL

USER SPECIFIED Tc(MIN.) = 5.000

10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.787

COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8841

SOIL CLASSIFICATION IS "C"

SUBAREA RUNOFF(CFS) = 0.15

TOTAL AREA(ACRES) = 0.06 TOTAL RUNOFF(CFS) = 0.15

\*\*\*\*\*

FLOW PROCESS FROM NODE 68.00 TO NODE 66.00 IS CODE = 51

&gt;&gt;&gt;&gt;COMPUTE TRAPEZOIDAL CHANNEL FLOW&lt;&lt;&lt;&lt;&lt;

&gt;&gt;&gt;&gt;TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)&lt;&lt;&lt;&lt;&lt;

=====

ELEVATION DATA: UPSTREAM(FEET) = 1151.99 DOWNSTREAM(FEET) = 1146.98

CHANNEL LENGTH THRU SUBAREA(FEET) = 236.00 CHANNEL SLOPE = 0.0212

CHANNEL BASE(FEET) = 0.00 "Z" FACTOR = 99.000

MANNING'S FACTOR = 0.015 MAXIMUM DEPTH(FEET) = 1.00

10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.295

COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8814

SOIL CLASSIFICATION IS "C"

TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.41

TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 1.32

AVERAGE FLOW DEPTH(FEET) = 0.06 TRAVEL TIME(MIN.) = 2.98

Tc(MIN.) = 7.98

SUBAREA AREA(ACRES) = 0.26 SUBAREA RUNOFF(CFS) = 0.53

TOTAL AREA(ACRES) = 0.3 PEAK FLOW RATE(CFS) = 0.67

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.07 FLOW VELOCITY(FEET/SEC.) = 1.57

LONGEST FLOWPATH FROM NODE 67.00 TO NODE 66.00 = 3636.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 66.00 TO NODE 66.00 IS CODE = 81

&gt;&gt;&gt;&gt;ADDITION OF SUBAREA TO MAINLINE PEAK FLOW&lt;&lt;&lt;&lt;&lt;

=====

10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.295

COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8814

SOIL CLASSIFICATION IS "C"

SUBAREA AREA(ACRES) = 0.26 SUBAREA RUNOFF(CFS) = 0.53

TOTAL AREA(ACRES) = 0.6 TOTAL RUNOFF(CFS) = 1.20

TC(MIN.) = 7.98



\*\*\*\*\*

FLOW PROCESS FROM NODE 66.00 TO NODE 66.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 7.98  
RAINFALL INTENSITY(INCH/HR) = 2.30  
TOTAL STREAM AREA(ACRES) = 0.58  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 1.20

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	T <sub>c</sub> (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	1.67	8.29	2.259	0.82
2	1.20	7.98	2.295	0.58

\*\*\*\*\*WARNING\*\*\*\*\*

IN THIS COMPUTER PROGRAM, THE CONFLUENCE VALUE USED IS BASED  
ON THE RCFC&WCD FORMULA OF PLATE D-1 AS DEFAULT VALUE. THIS FORMULA  
WILL NOT NECESSARILY RESULT IN THE MAXIMUM VALUE OF PEAK FLOW.

\*\*\*\*\*

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	T <sub>c</sub> (MIN.)	INTENSITY (INCH/HOUR)
1	2.81	7.98	2.295
2	2.85	8.29	2.259

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 2.85 T<sub>c</sub>(MIN.) = 8.29  
TOTAL AREA(ACRES) = 1.4  
LONGEST FLOWPATH FROM NODE 67.00 TO NODE 66.00 = 3636.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 66.00 TO NODE 69.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<

=====

ELEVATION DATA: UPSTREAM(Feet) = 1146.98 DOWNSTREAM(Feet) = 1139.00  
CHANNEL LENGTH THRU SUBAREA(Feet) = 281.00 CHANNEL SLOPE = 0.0284  
CHANNEL BASE(Feet) = 0.00 "Z" FACTOR = 99.000  
MANNING'S FACTOR = 0.015 MAXIMUM DEPTH(Feet) = 1.00  
10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.073  
COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8798  
SOIL CLASSIFICATION IS "C"  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.02  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(Feet/Sec.) = 2.45  
AVERAGE FLOW DEPTH(Feet) = 0.11 TRAVEL TIME(MIN.) = 1.91  
T<sub>c</sub>(MIN.) = 10.20  
SUBAREA AREA(ACRES) = 0.19 SUBAREA RUNOFF(CFS) = 0.35  
TOTAL AREA(ACRES) = 1.6 PEAK FLOW RATE(CFS) = 3.20

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(Feet) = 0.11 FLOW VELOCITY(Feet/Sec.) = 2.59  
LONGEST FLOWPATH FROM NODE 67.00 TO NODE 69.00 = 3917.00 FEET.

```

*****
FLOW PROCESS FROM NODE      69.00 TO NODE      69.00 IS CODE =  81
-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====
  10 YEAR RAINFALL INTENSITY(INCH/HOUR) =  2.073
  COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8798
  SOIL CLASSIFICATION IS "C"
  SUBAREA AREA(ACRES) =    0.19   SUBAREA RUNOFF(CFS) =    0.35
  TOTAL AREA(ACRES) =    1.8   TOTAL RUNOFF(CFS) =    3.54
  TC(MIN.) =   10.20

*****
FLOW PROCESS FROM NODE      69.00 TO NODE      62.00 IS CODE =  41
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 1132.39  DOWNSTREAM(FEET) = 1132.00
FLOW LENGTH(FEET) =   11.40  MANNING'S N = 0.013
DEPTH OF FLOW IN  18.0 INCH PIPE IS  5.3 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) =  8.21
GIVEN PIPE DIAMETER(INCH) =  18.00  NUMBER OF PIPES =  1
PIPE-FLOW(CFS) =    3.54
PIPE TRAVEL TIME(MIN.) =  0.02  Tc(MIN.) =  10.22
LONGEST FLOWPATH FROM NODE      67.00 TO NODE      62.00 =    3928.40 FEET.

*****
FLOW PROCESS FROM NODE      62.00 TO NODE      62.00 IS CODE =  11
-----
>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<
=====

** MAIN STREAM CONFLUENCE DATA **
STREAM      RUNOFF      Tc      INTENSITY      AREA
NUMBER      (CFS)      (MIN.)  (INCH/HOUR)  (ACRE)
   1         3.54      10.22      2.072        1.78
LONGEST FLOWPATH FROM NODE      67.00 TO NODE      62.00 =    3928.40 FEET.

** MEMORY BANK # 1 CONFLUENCE DATA **
STREAM      RUNOFF      Tc      INTENSITY      AREA
NUMBER      (CFS)      (MIN.)  (INCH/HOUR)  (ACRE)
   1        10.29      14.69      1.782        5.68
LONGEST FLOWPATH FROM NODE      55.00 TO NODE      62.00 = ***** FEET.

*****WARNING*****
IN THIS COMPUTER PROGRAM, THE CONFLUENCE VALUE USED IS BASED
ON THE RCFC&WCD FORMULA OF PLATE D-1 AS DEFAULT VALUE. THIS FORMULA
WILL NOT NECESSARILY RESULT IN THE MAXIMUM VALUE OF PEAK FLOW.
*****

** PEAK FLOW RATE TABLE **
STREAM      RUNOFF      Tc      INTENSITY
NUMBER      (CFS)      (MIN.)  (INCH/HOUR)
   1        10.70      10.22      2.072
   2        13.34      14.69      1.782

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
PEAK FLOW RATE(CFS) =    13.34  Tc(MIN.) =  14.69
TOTAL AREA(ACRES) =    7.5

```

\*\*\*\*\*

FLOW PROCESS FROM NODE 62.00 TO NODE 62.00 IS CODE = 12

-----  
>>>>CLEAR MEMORY BANK # 1 <<<<  
=====

=====

END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 7.5 TC(MIN.) = 14.69

PEAK FLOW RATE(CFS) = 13.34  
=====

=====

END OF RATIONAL METHOD ANALYSIS



\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM BASED ON  
 RIVERSIDE COUNTY FLOOD CONTROL & WATER CONSERVATION DISTRICT  
 (RCFC&WCD) 1978 HYDROLOGY MANUAL  
 (c) Copyright 1982-2011 Advanced Engineering Software (aes)  
 (Rational Tabling Version 18.0)  
 Release Date: 07/01/2011 License ID 1499

Analysis prepared by:

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 Suite 200  
 Orange, CA 92868

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*

\* UHS Rancho Springs \*  
 \* Existing Conditions \*  
 \* 100-year analysis \*  
 \*\*\*\*\*

FILE NAME: RS\_E.DAT  
 TIME/DATE OF STUDY: 21:13 05/17/2020

-----  
 USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
 -----

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
 SPECIFIED MINIMUM PIPE SIZE(INCH) = 8.00  
 SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.95  
 10-YEAR STORM 10-MINUTE INTENSITY(INCH/HOUR) = 2.070  
 10-YEAR STORM 60-MINUTE INTENSITY(INCH/HOUR) = 0.985  
 100-YEAR STORM 10-MINUTE INTENSITY(INCH/HOUR) = 3.430  
 100-YEAR STORM 60-MINUTE INTENSITY(INCH/HOUR) = 1.630  
 SLOPE OF 10-YEAR INTENSITY-DURATION CURVE = 0.4144876  
 SLOPE OF 100-YEAR INTENSITY-DURATION CURVE = 0.4152232

COMPUTED RAINFALL INTENSITY DATA:

STORM EVENT = 100.00 1-HOUR INTENSITY(INCH/HOUR) = 1.630  
 SLOPE OF INTENSITY DURATION CURVE = 0.4152

RCFC&WCD HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD

NOTE: COMPUTE CONFLUENCE VALUES ACCORDING TO RCFC&WCD HYDROLOGY MANUAL

AND IGNORE OTHER CONFLUENCE COMBINATIONS FOR DOWNSTREAM ANALYSES

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

NO.	HALF- WIDTH (FT)	CROWN TO CROSSFALL (FT)	STREET-CROSSFALL: IN- / OUT- / PARK- SIDE / SIDE / WAY	CURB HEIGHT (FT)	GUTTER-GEOMETRIES: WIDTH (FT)	LIP (FT)	HIKE (FT)	MANNING FACTOR (n)
1	30.0	20.0	0.018/0.018/0.020	0.67	2.00	0.0313	0.167	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
 as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
 OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*

FLOW PROCESS FROM NODE 10.00 TO NODE 11.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

=====

ASSUMED INITIAL SUBAREA UNIFORM  
 DEVELOPMENT IS COMMERCIAL

```

TC = K*[(LENGTH**3)/(ELEVATION CHANGE)]**.2
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00
UPSTREAM ELEVATION(FEET) = 1155.02
DOWNSTREAM ELEVATION(FEET) = 1153.91
ELEVATION DIFFERENCE(FEET) = 1.11
TC = 0.303*[(100.00**3)/(1.11)]**.2 = 4.705
COMPUTED TIME OF CONCENTRATION INCREASED TO 5 MIN.
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.574
COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8896
SOIL CLASSIFICATION IS "C"
SUBAREA RUNOFF(CFS) = 0.28
TOTAL AREA(ACRES) = 0.07 TOTAL RUNOFF(CFS) = 0.28

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```

FLOW PROCESS FROM NODE 20.00 TO NODE 21.00 IS CODE = 21
-----

```

```

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
=====

```

```

    ASSUMED INITIAL SUBAREA UNIFORM
    DEVELOPMENT IS COMMERCIAL

```

```

TC = K*[(LENGTH**3)/(ELEVATION CHANGE)]**.2
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00
UPSTREAM ELEVATION(FEET) = 1158.00
DOWNSTREAM ELEVATION(FEET) = 1155.00
ELEVATION DIFFERENCE(FEET) = 3.00
TC = 0.303*[(100.00**3)/(3.00)]**.2 = 3.856
COMPUTED TIME OF CONCENTRATION INCREASED TO 5 MIN.
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.574
COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8896
SOIL CLASSIFICATION IS "C"
SUBAREA RUNOFF(CFS) = 0.45
TOTAL AREA(ACRES) = 0.11 TOTAL RUNOFF(CFS) = 0.45

```

\*\*\*\*\*

```

FLOW PROCESS FROM NODE 21.00 TO NODE 22.00 IS CODE = 51
-----

```

```

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<
=====

```

```

ELEVATION DATA: UPSTREAM(FEET) = 1155.00 DOWNSTREAM(FEET) = 1153.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 99.00 CHANNEL SLOPE = 0.0202
CHANNEL BASE(FEET) = 0.00 "Z" FACTOR = 99.000
MANNING'S FACTOR = 0.015 MAXIMUM DEPTH(FEET) = 1.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.217
COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8888
SOIL CLASSIFICATION IS "C"
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.65
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 1.53
AVERAGE FLOW DEPTH(FEET) = 0.07 TRAVEL TIME(MIN.) = 1.08
Tc(MIN.) = 6.08
SUBAREA AREA(ACRES) = 0.11 SUBAREA RUNOFF(CFS) = 0.41
TOTAL AREA(ACRES) = 0.2 PEAK FLOW RATE(CFS) = 0.86

```

```

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH(FEET) = 0.07 FLOW VELOCITY(FEET/SEC.) = 1.61
LONGEST FLOWPATH FROM NODE 20.00 TO NODE 22.00 = 199.00 FEET.

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\*\*\*\*\*

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FLOW PROCESS FROM NODE 22.00 TO NODE 22.00 IS CODE = 81
-----

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>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====

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100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.217

```

COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8888  
 SOIL CLASSIFICATION IS "C"  
 SUBAREA AREA(ACRES) = 0.11 SUBAREA RUNOFF(CFS) = 0.41  
 TOTAL AREA(ACRES) = 0.3 TOTAL RUNOFF(CFS) = 1.27  
 TC(MIN.) = 6.08

\*\*\*\*\*

FLOW PROCESS FROM NODE 22.00 TO NODE 23.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<  
 >>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<

=====

ELEVATION DATA: UPSTREAM(Feet) = 1145.70 DOWNSTREAM(Feet) = 1144.47  
 FLOW LENGTH(Feet) = 26.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 21.0 INCH PIPE IS 2.8 INCHES  
 PIPE-FLOW VELOCITY(Feet/Sec.) = 6.70  
 GIVEN PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 1.27  
 PIPE TRAVEL TIME(MIN.) = 0.06 Tc(MIN.) = 6.15  
 LONGEST FLOWPATH FROM NODE 20.00 TO NODE 23.00 = 225.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 23.00 TO NODE 23.00 IS CODE = 10

>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<

\*\*\*\*\*

FLOW PROCESS FROM NODE 70.00 TO NODE 71.00 IS CODE = 22

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

=====

ASSUMED INITIAL SUBAREA UNIFORM  
 DEVELOPMENT IS COMMERCIAL  
 USER SPECIFIED Tc(MIN.) = 5.000  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.574  
 COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8896  
 SOIL CLASSIFICATION IS "C"  
 SUBAREA RUNOFF(CFS) = 0.45  
 TOTAL AREA(ACRES) = 0.11 TOTAL RUNOFF(CFS) = 0.45

\*\*\*\*\*

FLOW PROCESS FROM NODE 71.00 TO NODE 72.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<  
 >>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<

=====

ELEVATION DATA: UPSTREAM(Feet) = 1148.65 DOWNSTREAM(Feet) = 1148.56  
 FLOW LENGTH(Feet) = 18.50 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 12.0 INCH PIPE IS 3.5 INCHES  
 PIPE-FLOW VELOCITY(Feet/Sec.) = 2.35  
 GIVEN PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 0.45  
 PIPE TRAVEL TIME(MIN.) = 0.13 Tc(MIN.) = 5.13  
 LONGEST FLOWPATH FROM NODE 70.00 TO NODE 72.00 = 10018.50 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 72.00 TO NODE 73.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<  
 >>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<

=====

ELEVATION DATA: UPSTREAM(Feet) = 1148.56 DOWNSTREAM(Feet) = 1147.02

```

                                RS_E_100.RES
FLOW LENGTH(FEET) = 102.00  MANNING'S N = 0.013
DEPTH OF FLOW IN 12.0 INCH PIPE IS 2.6 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 3.53
GIVEN PIPE DIAMETER(INCH) = 12.00  NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 0.45
PIPE TRAVEL TIME(MIN.) = 0.48  Tc(MIN.) = 5.61
LONGEST FLOWPATH FROM NODE 70.00 TO NODE 73.00 = 10120.50 FEET.

*****
FLOW PROCESS FROM NODE 73.00 TO NODE 73.00 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 5.61
RAINFALL INTENSITY(INCH/HR) = 4.36
TOTAL STREAM AREA(ACRES) = 0.11
PEAK FLOW RATE(CFS) AT CONFLUENCE = 0.45

*****
FLOW PROCESS FROM NODE 74.00 TO NODE 75.00 IS CODE = 22
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
=====
    ASSUMED INITIAL SUBAREA UNIFORM
    DEVELOPMENT IS COMMERCIAL
USER SPECIFIED Tc(MIN.) = 5.000
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.574
COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8896
SOIL CLASSIFICATION IS "C"
SUBAREA RUNOFF(CFS) = 0.45
TOTAL AREA(ACRES) = 0.11  TOTAL RUNOFF(CFS) = 0.45

*****
FLOW PROCESS FROM NODE 75.00 TO NODE 73.00 IS CODE = 41
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 1146.80  DOWNSTREAM(FEET) = 1146.73
FLOW LENGTH(FEET) = 14.70  MANNING'S N = 0.013
DEPTH OF FLOW IN 12.0 INCH PIPE IS 3.5 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 2.35
GIVEN PIPE DIAMETER(INCH) = 12.00  NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 0.45
PIPE TRAVEL TIME(MIN.) = 0.10  Tc(MIN.) = 5.10
LONGEST FLOWPATH FROM NODE 74.00 TO NODE 73.00 = 114.70 FEET.

*****
FLOW PROCESS FROM NODE 73.00 TO NODE 73.00 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 5.10
RAINFALL INTENSITY(INCH/HR) = 4.53
TOTAL STREAM AREA(ACRES) = 0.11
PEAK FLOW RATE(CFS) AT CONFLUENCE = 0.45

** CONFLUENCE DATA **

```

STREAM NUMBER	RUNOFF (CFS)	T <sub>c</sub> (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	0.45	5.61	4.359	0.11
2	0.45	5.10	4.535	0.11

\*\*\*\*\*WARNING\*\*\*\*\*

IN THIS COMPUTER PROGRAM, THE CONFLUENCE VALUE USED IS BASED  
ON THE RCFC&WCD FORMULA OF PLATE D-1 AS DEFAULT VALUE. THIS FORMULA  
WILL NOT NECESSARILY RESULT IN THE MAXIMUM VALUE OF PEAK FLOW.

\*\*\*\*\*

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	T <sub>c</sub> (MIN.)	INTENSITY (INCH/HOUR)
1	0.85	5.10	4.535
2	0.88	5.61	4.359

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 0.88 T<sub>c</sub>(MIN.) = 5.61

TOTAL AREA(ACRES) = 0.2

LONGEST FLOWPATH FROM NODE 70.00 TO NODE 73.00 = 10120.50 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 73.00 TO NODE 76.00 IS CODE = 41

-----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1146.73 DOWNSTREAM(FEET) = 1146.24  
FLOW LENGTH(FEET) = 52.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 12.0 INCH PIPE IS 4.2 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 3.62  
GIVEN PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 0.88  
PIPE TRAVEL TIME(MIN.) = 0.24 T<sub>c</sub>(MIN.) = 5.85  
LONGEST FLOWPATH FROM NODE 70.00 TO NODE 76.00 = 10172.50 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 76.00 TO NODE 76.00 IS CODE = 1

-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 5.85  
RAINFALL INTENSITY(INCH/HR) = 4.28  
TOTAL STREAM AREA(ACRES) = 0.22  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 0.88

\*\*\*\*\*

FLOW PROCESS FROM NODE 77.00 TO NODE 78.00 IS CODE = 22

-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

ASSUMED INITIAL SUBAREA UNIFORM  
DEVELOPMENT IS COMMERCIAL  
USER SPECIFIED T<sub>c</sub>(MIN.) = 5.000  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.574  
COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8896  
SOIL CLASSIFICATION IS "C"



SUBAREA RUNOFF(CFS) = 0.45  
 TOTAL AREA(ACRES) = 0.11 TOTAL RUNOFF(CFS) = 0.45

\*\*\*\*\*

FLOW PROCESS FROM NODE 78.00 TO NODE 76.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<  
 >>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1146.80 DOWNSTREAM(FEET) = 1146.71  
 FLOW LENGTH(FEET) = 18.80 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 12.0 INCH PIPE IS 3.5 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 2.35  
 GIVEN PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 0.45  
 PIPE TRAVEL TIME(MIN.) = 0.13 Tc(MIN.) = 5.13  
 LONGEST FLOWPATH FROM NODE 77.00 TO NODE 76.00 = 10018.80 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 76.00 TO NODE 76.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 5.13  
 RAINFALL INTENSITY(INCH/HR) = 4.52  
 TOTAL STREAM AREA(ACRES) = 0.11  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 0.45

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	0.88	5.85	4.284	0.22
2	0.45	5.13	4.524	0.11

\*\*\*\*\*WARNING\*\*\*\*\*

IN THIS COMPUTER PROGRAM, THE CONFLUENCE VALUE USED IS BASED  
 ON THE RCFC&WCD FORMULA OF PLATE D-1 AS DEFAULT VALUE. THIS FORMULA  
 WILL NOT NECESSARILY RESULT IN THE MAXIMUM VALUE OF PEAK FLOW.

\*\*\*\*\*

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	1.22	5.13	4.524
2	1.30	5.85	4.284

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 1.30 Tc(MIN.) = 5.85  
 TOTAL AREA(ACRES) = 0.3  
 LONGEST FLOWPATH FROM NODE 70.00 TO NODE 76.00 = 10172.50 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 76.00 TO NODE 23.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<  
 >>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1146.24 DOWNSTREAM(FEET) = 1145.22  
 FLOW LENGTH(FEET) = 68.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 12.0 INCH PIPE IS 4.6 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 4.77  
 GIVEN PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 1.30  
 PIPE TRAVEL TIME(MIN.) = 0.24 Tc(MIN.) = 6.09  
 LONGEST FLOWPATH FROM NODE 70.00 TO NODE 23.00 = 10240.50 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 23.00 TO NODE 23.00 IS CODE = 11

>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<<

\*\* MAIN STREAM CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	1.30	6.09	4.214	0.33

LONGEST FLOWPATH FROM NODE 70.00 TO NODE 23.00 = 10240.50 FEET.

\*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	1.27	6.15	4.198	0.33

LONGEST FLOWPATH FROM NODE 20.00 TO NODE 23.00 = 225.00 FEET.

\*\*\*\*\*WARNING\*\*\*\*\*

IN THIS COMPUTER PROGRAM, THE CONFLUENCE VALUE USED IS BASED  
 ON THE RCFC&WCD FORMULA OF PLATE D-1 AS DEFAULT VALUE. THIS FORMULA  
 WILL NOT NECESSARILY RESULT IN THE MAXIMUM VALUE OF PEAK FLOW.

\*\*\*\*\*

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	2.56	6.09	4.214
2	2.57	6.15	4.198

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 2.56 Tc(MIN.) = 6.09  
 TOTAL AREA(ACRES) = 0.7

\*\*\*\*\*

FLOW PROCESS FROM NODE 23.00 TO NODE 23.00 IS CODE = 12

>>>>CLEAR MEMORY BANK # 1 <<<<<

\*\*\*\*\*

FLOW PROCESS FROM NODE 23.00 TO NODE 26.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1144.47 DOWNSTREAM(FEET) = 1143.66  
 FLOW LENGTH(FEET) = 120.60 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 21.0 INCH PIPE IS 6.4 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 4.12  
 GIVEN PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 2.56  
 PIPE TRAVEL TIME(MIN.) = 0.49 Tc(MIN.) = 6.58  
 LONGEST FLOWPATH FROM NODE 70.00 TO NODE 26.00 = 10361.10 FEET.

```

*****
FLOW PROCESS FROM NODE      26.00 TO NODE      26.00 IS CODE =   1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) =   6.58
RAINFALL INTENSITY(INCH/HR) =   4.08
TOTAL STREAM AREA(ACRES) =    0.66
PEAK FLOW RATE(CFS) AT CONFLUENCE =    2.56

*****
FLOW PROCESS FROM NODE      24.00 TO NODE      25.00 IS CODE =  21
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
=====
      ASSUMED INITIAL SUBAREA UNIFORM
      DEVELOPMENT IS COMMERCIAL
TC = K*[(LENGTH**3)/(ELEVATION CHANGE)]**.2
INITIAL SUBAREA FLOW-LENGTH(FEET) =  100.00
UPSTREAM ELEVATION(FEET) =  1157.00
DOWNSTREAM ELEVATION(FEET) =  1155.20
ELEVATION DIFFERENCE(FEET) =    1.80
TC = 0.303*[( 100.00**3)/(    1.80)]**.2 =   4.271
COMPUTED TIME OF CONCENTRATION INCREASED TO 5 MIN.
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  4.574
COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8896
SOIL CLASSIFICATION IS "C"
SUBAREA RUNOFF(CFS) =    0.33
TOTAL AREA(ACRES) =    0.08  TOTAL RUNOFF(CFS) =    0.33

*****
FLOW PROCESS FROM NODE      25.00 TO NODE      26.00 IS CODE =  51
-----
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) =  1155.20  DOWNSTREAM(FEET) =  1152.14
CHANNEL LENGTH THRU SUBAREA(FEET) =  197.00  CHANNEL SLOPE =  0.0155
CHANNEL BASE(FEET) =   0.00  "Z" FACTOR =  99.000
MANNING'S FACTOR = 0.015  MAXIMUM DEPTH(FEET) =  1.00
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  3.905
COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8880
SOIL CLASSIFICATION IS "C"
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) =    0.92
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) =  1.42
AVERAGE FLOW DEPTH(FEET) =   0.08  TRAVEL TIME(MIN.) =  2.32
Tc(MIN.) =   7.32
SUBAREA AREA(ACRES) =    0.34  SUBAREA RUNOFF(CFS) =    1.18
TOTAL AREA(ACRES) =    0.4  PEAK FLOW RATE(CFS) =    1.50

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH(FEET) =  0.10  FLOW VELOCITY(FEET/SEC.) =  1.64
LONGEST FLOWPATH FROM NODE      24.00 TO NODE      26.00 =    297.00 FEET.

*****
FLOW PROCESS FROM NODE      26.00 TO NODE      26.00 IS CODE =  81
-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  3.905

```

COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8880  
 SOIL CLASSIFICATION IS "C"  
 SUBAREA AREA(ACRES) = 0.34 SUBAREA RUNOFF(CFS) = 1.18  
 TOTAL AREA(ACRES) = 0.8 TOTAL RUNOFF(CFS) = 2.68  
 TC(MIN.) = 7.32

\*\*\*\*\*

FLOW PROCESS FROM NODE 26.00 TO NODE 26.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 7.32  
 RAINFALL INTENSITY(INCH/HR) = 3.91  
 TOTAL STREAM AREA(ACRES) = 0.76  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 2.68

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	2.56	6.58	4.081	0.66
2	2.68	7.32	3.905	0.76

\*\*\*\*\*WARNING\*\*\*\*\*

IN THIS COMPUTER PROGRAM, THE CONFLUENCE VALUE USED IS BASED  
 ON THE RCFC&WCD FORMULA OF PLATE D-1 AS DEFAULT VALUE. THIS FORMULA  
 WILL NOT NECESSARILY RESULT IN THE MAXIMUM VALUE OF PEAK FLOW.

\*\*\*\*\*

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	4.98	6.58	4.081
2	5.14	7.32	3.905

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 5.14 Tc(MIN.) = 7.32  
 TOTAL AREA(ACRES) = 1.4  
 LONGEST FLOWPATH FROM NODE 70.00 TO NODE 26.00 = 10361.10 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 30.00 TO NODE 31.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
 >>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1163.00 DOWNSTREAM(FEET) = 1157.00  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 329.00 CHANNEL SLOPE = 0.0182  
 CHANNEL BASE(FEET) = 1.60 "Z" FACTOR = 99.000  
 MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 0.50  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.272  
 COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8861  
 SOIL CLASSIFICATION IS "C"  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 5.25  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 1.41  
 AVERAGE FLOW DEPTH(FEET) = 0.19 TRAVEL TIME(MIN.) = 3.89  
 Tc(MIN.) = 11.20  
 SUBAREA AREA(ACRES) = 0.08 SUBAREA RUNOFF(CFS) = 0.23

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                                RS_E_100.RES
TOTAL AREA(ACRES) =          1.5          PEAK FLOW RATE(CFS) =          5.37

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH(FEET) = 0.19   FLOW VELOCITY(FEET/SEC.) = 1.41
LONGEST FLOWPATH FROM NODE      70.00 TO NODE      31.00 = 10690.10 FEET.

*****
FLOW PROCESS FROM NODE      31.00 TO NODE      32.00 IS CODE = 41
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 1152.57 DOWNSTREAM(FEET) = 1145.78
FLOW LENGTH(FEET) = 210.50   MANNING'S N = 0.013
DEPTH OF FLOW IN 12.0 INCH PIPE IS 8.6 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 8.92
GIVEN PIPE DIAMETER(INCH) = 12.00   NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 5.37
PIPE TRAVEL TIME(MIN.) = 0.39   Tc(MIN.) = 11.59
LONGEST FLOWPATH FROM NODE      70.00 TO NODE      32.00 = 10900.60 FEET.

*****
FLOW PROCESS FROM NODE      32.00 TO NODE      32.00 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 11.59
RAINFALL INTENSITY(INCH/HR) = 3.23
TOTAL STREAM AREA(ACRES) = 1.50
PEAK FLOW RATE(CFS) AT CONFLUENCE = 5.37

*****
FLOW PROCESS FROM NODE      33.00 TO NODE      34.00 IS CODE = 21
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
=====
    ASSUMED INITIAL SUBAREA UNIFORM
    DEVELOPMENT IS COMMERCIAL
TC = K*[(LENGTH**3)/(ELEVATION CHANGE)]**.2
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00
UPSTREAM ELEVATION(FEET) = 1162.00
DOWNSTREAM ELEVATION(FEET) = 1156.99
ELEVATION DIFFERENCE(FEET) = 5.01
TC = 0.303*[( 100.00**3)/( 5.01)]**.2 = 3.480
COMPUTED TIME OF CONCENTRATION INCREASED TO 5 MIN.
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.574
COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8896
SOIL CLASSIFICATION IS "C"
SUBAREA RUNOFF(CFS) = 0.24
TOTAL AREA(ACRES) = 0.06   TOTAL RUNOFF(CFS) = 0.24

*****
FLOW PROCESS FROM NODE      34.00 TO NODE      35.00 IS CODE = 51
-----
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 1156.99 DOWNSTREAM(FEET) = 1150.03
CHANNEL LENGTH THRU SUBAREA(FEET) = 175.00   CHANNEL SLOPE = 0.0398
CHANNEL BASE(FEET) = 0.00   "Z" FACTOR = 99.000
MANNING'S FACTOR = 0.015   MAXIMUM DEPTH(FEET) = 1.00

```

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.154  
 COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8887  
 SOIL CLASSIFICATION IS "C"  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.96  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 2.24  
 AVERAGE FLOW DEPTH(FEET) = 0.07 TRAVEL TIME(MIN.) = 1.30  
 Tc(MIN.) = 6.30  
 SUBAREA AREA(ACRES) = 0.39 SUBAREA RUNOFF(CFS) = 1.44  
 TOTAL AREA(ACRES) = 0.4 PEAK FLOW RATE(CFS) = 1.68

## END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.09 FLOW VELOCITY(FEET/SEC.) = 2.26  
 LONGEST FLOWPATH FROM NODE 33.00 TO NODE 35.00 = 275.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 35.00 TO NODE 35.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.154  
 COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8887  
 SOIL CLASSIFICATION IS "C"  
 SUBAREA AREA(ACRES) = 0.39 SUBAREA RUNOFF(CFS) = 1.44  
 TOTAL AREA(ACRES) = 0.8 TOTAL RUNOFF(CFS) = 3.12  
 TC(MIN.) = 6.30

\*\*\*\*\*

FLOW PROCESS FROM NODE 35.00 TO NODE 32.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<

>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1146.37 DOWNSTREAM(FEET) = 1145.76  
 FLOW LENGTH(FEET) = 23.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 5.3 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 7.23  
 GIVEN PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 3.12  
 PIPE TRAVEL TIME(MIN.) = 0.05 Tc(MIN.) = 6.36  
 LONGEST FLOWPATH FROM NODE 33.00 TO NODE 32.00 = 298.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 32.00 TO NODE 32.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 6.36  
 RAINFALL INTENSITY(INCH/HR) = 4.14  
 TOTAL STREAM AREA(ACRES) = 0.84  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 3.12

## \*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	5.37	11.59	3.226	1.50
2	3.12	6.36	4.140	0.84

\*\*\*\*\*WARNING\*\*\*\*\*

IN THIS COMPUTER PROGRAM, THE CONFLUENCE VALUE USED IS BASED  
 ON THE RCFC&WCD FORMULA OF PLATE D-1 AS DEFAULT VALUE. THIS FORMULA

WILL NOT NECESSARILY RESULT IN THE MAXIMUM VALUE OF PEAK FLOW.

\*\*\*\*\*

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	6.07	6.36	4.140
2	7.80	11.59	3.226

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 7.80 Tc(MIN.) = 11.59

TOTAL AREA(ACRES) = 2.3

LONGEST FLOWPATH FROM NODE 70.00 TO NODE 32.00 = 10900.60 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 32.00 TO NODE 36.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<

>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1145.75 DOWNSTREAM(FEET) = 1142.04

FLOW LENGTH(FEET) = 176.00 MANNING'S N = 0.013

DEPTH OF FLOW IN 24.0 INCH PIPE IS 8.1 INCHES

PIPE-FLOW VELOCITY(FEET/SEC.) = 8.41

GIVEN PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 7.80

PIPE TRAVEL TIME(MIN.) = 0.35 Tc(MIN.) = 11.94

LONGEST FLOWPATH FROM NODE 70.00 TO NODE 36.00 = 11076.60 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 36.00 TO NODE 36.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

TOTAL NUMBER OF STREAMS = 2

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:

TIME OF CONCENTRATION(MIN.) = 11.94

RAINFALL INTENSITY(INCH/HR) = 3.19

TOTAL STREAM AREA(ACRES) = 2.34

PEAK FLOW RATE(CFS) AT CONFLUENCE = 7.80

\*\*\*\*\*

FLOW PROCESS FROM NODE 37.00 TO NODE 38.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

ASSUMED INITIAL SUBAREA UNIFORM

DEVELOPMENT IS COMMERCIAL

TC = K\*[(LENGTH\*\*3)/(ELEVATION CHANGE)]\*\*.2

INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00

UPSTREAM ELEVATION(FEET) = 1166.00

DOWNSTREAM ELEVATION(FEET) = 1158.49

ELEVATION DIFFERENCE(FEET) = 7.51

TC = 0.303\*[(100.00\*\*3)/(7.51)]\*\*.2 = 3.210

COMPUTED TIME OF CONCENTRATION INCREASED TO 5 MIN.

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.574

COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8896

SOIL CLASSIFICATION IS "C"

SUBAREA RUNOFF(CFS) = 0.49

TOTAL AREA(ACRES) = 0.12 TOTAL RUNOFF(CFS) = 0.49

\*\*\*\*\*

FLOW PROCESS FROM NODE 38.00 TO NODE 39.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1158.49 DOWNSTREAM(FEET) = 1150.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 282.00 CHANNEL SLOPE = 0.0301  
CHANNEL BASE(FEET) = 0.00 "Z" FACTOR = 99.000  
MANNING'S FACTOR = 0.015 MAXIMUM DEPTH(FEET) = 1.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.902  
COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8880  
SOIL CLASSIFICATION IS "C"  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.31  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 2.02  
AVERAGE FLOW DEPTH(FEET) = 0.08 TRAVEL TIME(MIN.) = 2.33  
Tc(MIN.) = 7.33  
SUBAREA AREA(ACRES) = 0.47 SUBAREA RUNOFF(CFS) = 1.63  
TOTAL AREA(ACRES) = 0.6 PEAK FLOW RATE(CFS) = 2.12

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
DEPTH(FEET) = 0.10 FLOW VELOCITY(FEET/SEC.) = 2.30  
LONGEST FLOWPATH FROM NODE 37.00 TO NODE 39.00 = 382.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 39.00 TO NODE 39.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.902  
COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8880  
SOIL CLASSIFICATION IS "C"  
SUBAREA AREA(ACRES) = 0.47 SUBAREA RUNOFF(CFS) = 1.63  
TOTAL AREA(ACRES) = 1.1 TOTAL RUNOFF(CFS) = 3.75  
TC(MIN.) = 7.33

\*\*\*\*\*

FLOW PROCESS FROM NODE 39.00 TO NODE 36.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<  
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1144.36 DOWNSTREAM(FEET) = 1142.28  
FLOW LENGTH(FEET) = 9.50 MANNING'S N = 0.013  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 3.4 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 16.12  
GIVEN PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 3.75  
PIPE TRAVEL TIME(MIN.) = 0.01 Tc(MIN.) = 7.34  
LONGEST FLOWPATH FROM NODE 37.00 TO NODE 36.00 = 391.50 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 36.00 TO NODE 36.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 7.34  
RAINFALL INTENSITY(INCH/HR) = 3.90  
TOTAL STREAM AREA(ACRES) = 1.06



PEAK FLOW RATE(CFS) AT CONFLUENCE = 3.75

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	7.80	11.94	3.186	2.34
2	3.75	7.34	3.900	1.06

\*\*\*\*\*WARNING\*\*\*\*\*

IN THIS COMPUTER PROGRAM, THE CONFLUENCE VALUE USED IS BASED  
ON THE RCFC&WCD FORMULA OF PLATE D-1 AS DEFAULT VALUE. THIS FORMULA  
WILL NOT NECESSARILY RESULT IN THE MAXIMUM VALUE OF PEAK FLOW.

\*\*\*\*\*

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	8.54	7.34	3.900
2	10.86	11.94	3.186

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 10.86 Tc(MIN.) = 11.94  
TOTAL AREA(ACRES) = 3.4  
LONGEST FLOWPATH FROM NODE 70.00 TO NODE 36.00 = 11076.60 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 36.00 TO NODE 40.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<  
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<

=====

ELEVATION DATA: UPSTREAM(Feet) = 1141.91 DOWNSTREAM(Feet) = 1141.39  
FLOW LENGTH(Feet) = 33.70 MANNING'S N = 0.013  
DEPTH OF FLOW IN 24.0 INCH PIPE IS 10.5 INCHES  
PIPE-FLOW VELOCITY(Feet/Sec.) = 8.21  
GIVEN PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 10.86  
PIPE TRAVEL TIME(MIN.) = 0.07 Tc(MIN.) = 12.01  
LONGEST FLOWPATH FROM NODE 70.00 TO NODE 40.00 = 11110.30 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 40.00 TO NODE 40.00 IS CODE = 10

>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<

\*\*\*\*\*

FLOW PROCESS FROM NODE 41.00 TO NODE 42.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

=====

ASSUMED INITIAL SUBAREA UNIFORM  
DEVELOPMENT IS COMMERCIAL  
TC = K\*[(LENGTH\*\*3)/(ELEVATION CHANGE)]\*\*.2  
INITIAL SUBAREA FLOW-LENGTH(Feet) = 100.00  
UPSTREAM ELEVATION(Feet) = 1166.00  
DOWNSTREAM ELEVATION(Feet) = 1158.65  
ELEVATION DIFFERENCE(Feet) = 7.35  
TC = 0.303\*[( 100.00\*\*3)/( 7.35)]\*\*.2 = 3.224  
COMPUTED TIME OF CONCENTRATION INCREASED TO 5 MIN.

```

                                RS_E_100.RES
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.574
COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8896
SOIL CLASSIFICATION IS "C"
SUBAREA RUNOFF(CFS) = 0.45
TOTAL AREA(ACRES) = 0.11 TOTAL RUNOFF(CFS) = 0.45

*****
FLOW PROCESS FROM NODE 42.00 TO NODE 43.00 IS CODE = 51
-----
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 1158.65 DOWNSTREAM(FEET) = 1151.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 236.00 CHANNEL SLOPE = 0.0324
CHANNEL BASE(FEET) = 0.00 "Z" FACTOR = 99.000
MANNING'S FACTOR = 0.015 MAXIMUM DEPTH(FEET) = 1.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.950
COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8881
SOIL CLASSIFICATION IS "C"
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.94
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 1.86
AVERAGE FLOW DEPTH(FEET) = 0.07 TRAVEL TIME(MIN.) = 2.12
Tc(MIN.) = 7.12
SUBAREA AREA(ACRES) = 0.28 SUBAREA RUNOFF(CFS) = 0.98
TOTAL AREA(ACRES) = 0.4 PEAK FLOW RATE(CFS) = 1.43

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH(FEET) = 0.08 FLOW VELOCITY(FEET/SEC.) = 2.20
LONGEST FLOWPATH FROM NODE 41.00 TO NODE 43.00 = 336.00 FEET.

*****
FLOW PROCESS FROM NODE 43.00 TO NODE 43.00 IS CODE = 81
-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.950
COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8881
SOIL CLASSIFICATION IS "C"
SUBAREA AREA(ACRES) = 0.29 SUBAREA RUNOFF(CFS) = 1.01
TOTAL AREA(ACRES) = 0.7 TOTAL RUNOFF(CFS) = 2.44
TC(MIN.) = 7.12

*****
FLOW PROCESS FROM NODE 43.00 TO NODE 80.00 IS CODE = 31
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 1146.61 DOWNSTREAM(FEET) = 1143.76
FLOW LENGTH(FEET) = 8.30 MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 8.000
DEPTH OF FLOW IN 8.0 INCH PIPE IS 3.3 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 18.08
ESTIMATED PIPE DIAMETER(INCH) = 8.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 2.44
PIPE TRAVEL TIME(MIN.) = 0.01 Tc(MIN.) = 7.13
LONGEST FLOWPATH FROM NODE 41.00 TO NODE 80.00 = 344.30 FEET.

*****
FLOW PROCESS FROM NODE 80.00 TO NODE 80.00 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
=====

```

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
 TIME OF CONCENTRATION(MIN.) = 7.13  
 RAINFALL INTENSITY(INCH/HR) = 3.95  
 TOTAL STREAM AREA(ACRES) = 0.68  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 2.44

\*\*\*\*\*

FLOW PROCESS FROM NODE 44.00 TO NODE 45.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

ASSUMED INITIAL SUBAREA UNIFORM

DEVELOPMENT IS COMMERCIAL

TC =  $K * [(LENGTH ** 3) / (ELEVATION \text{ CHANGE})] ** .2$   
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
 UPSTREAM ELEVATION(FEET) = 1155.93  
 DOWNSTREAM ELEVATION(FEET) = 1153.39  
 ELEVATION DIFFERENCE(FEET) = 2.54  
 $TC = 0.303 * [(100.00 ** 3) / (2.54)] ** .2 = 3.987$   
 COMPUTED TIME OF CONCENTRATION INCREASED TO 5 MIN.  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.574  
 COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8896  
 SOIL CLASSIFICATION IS "C"  
 SUBAREA RUNOFF(CFS) = 0.24  
 TOTAL AREA(ACRES) = 0.06 TOTAL RUNOFF(CFS) = 0.24

\*\*\*\*\*

FLOW PROCESS FROM NODE 45.00 TO NODE 46.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1153.39 DOWNSTREAM(FEET) = 1150.99  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 74.30 CHANNEL SLOPE = 0.0323  
 CHANNEL BASE(FEET) = 0.00 "Z" FACTOR = 99.000  
 MANNING'S FACTOR = 0.015 MAXIMUM DEPTH(FEET) = 1.00  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.268  
 COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8889  
 SOIL CLASSIFICATION IS "C"  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.32  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 1.37  
 AVERAGE FLOW DEPTH(FEET) = 0.05 TRAVEL TIME(MIN.) = 0.91  
 $T_c(MIN.) = 5.91$   
 SUBAREA AREA(ACRES) = 0.04 SUBAREA RUNOFF(CFS) = 0.15  
 TOTAL AREA(ACRES) = 0.1 PEAK FLOW RATE(CFS) = 0.40

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.05 FLOW VELOCITY(FEET/SEC.) = 1.57  
 LONGEST FLOWPATH FROM NODE 44.00 TO NODE 46.00 = 174.30 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 46.00 TO NODE 46.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.268  
 COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8889  
 SOIL CLASSIFICATION IS "C"  
 SUBAREA AREA(ACRES) = 0.04 SUBAREA RUNOFF(CFS) = 0.15  
 TOTAL AREA(ACRES) = 0.1 TOTAL RUNOFF(CFS) = 0.55  
 $TC(MIN.) = 5.91$

\*\*\*\*\*

FLOW PROCESS FROM NODE 46.00 TO NODE 80.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<  
 >>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1145.97 DOWNSTREAM(FEET) = 1144.76  
 FLOW LENGTH(FEET) = 57.10 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 12.0 INCH PIPE IS 2.7 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 4.21  
 GIVEN PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 0.55  
 PIPE TRAVEL TIME(MIN.) = 0.23 Tc(MIN.) = 6.13  
 LONGEST FLOWPATH FROM NODE 44.00 TO NODE 80.00 = 231.40 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 80.00 TO NODE 80.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 6.13  
 RAINFALL INTENSITY(INCH/HR) = 4.20  
 TOTAL STREAM AREA(ACRES) = 0.14  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 0.55

## \*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	2.44	7.13	3.948	0.68
2	0.55	6.13	4.202	0.14

\*\*\*\*\*WARNING\*\*\*\*\*

IN THIS COMPUTER PROGRAM, THE CONFLUENCE VALUE USED IS BASED  
 ON THE RCFC&WCD FORMULA OF PLATE D-1 AS DEFAULT VALUE. THIS FORMULA  
 WILL NOT NECESSARILY RESULT IN THE MAXIMUM VALUE OF PEAK FLOW.

\*\*\*\*\*

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

## \*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	2.65	6.13	4.202
2	2.95	7.13	3.948

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 2.95 Tc(MIN.) = 7.13  
 TOTAL AREA(ACRES) = 0.8  
 LONGEST FLOWPATH FROM NODE 41.00 TO NODE 80.00 = 344.30 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 80.00 TO NODE 40.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<  
 >>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1143.76 DOWNSTREAM(FEET) = 1141.39  
 FLOW LENGTH(FEET) = 81.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 24.0 INCH PIPE IS 4.5 INCHES

PIPE-FLOW VELOCITY(FEET/SEC.) = 7.15  
 GIVEN PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 2.95  
 PIPE TRAVEL TIME(MIN.) = 0.19 Tc(MIN.) = 7.32  
 LONGEST FLOWPATH FROM NODE 41.00 TO NODE 40.00 = 425.30 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 40.00 TO NODE 40.00 IS CODE = 11

>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<

=====

\*\* MAIN STREAM CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	2.95	7.32	3.905	0.82

LONGEST FLOWPATH FROM NODE 41.00 TO NODE 40.00 = 425.30 FEET.

\*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	10.86	12.01	3.179	3.40

LONGEST FLOWPATH FROM NODE 70.00 TO NODE 40.00 = 11110.30 FEET.

\*\*\*\*\*WARNING\*\*\*\*\*

IN THIS COMPUTER PROGRAM, THE CONFLUENCE VALUE USED IS BASED  
 ON THE RCFC&WCD FORMULA OF PLATE D-1 AS DEFAULT VALUE. THIS FORMULA  
 WILL NOT NECESSARILY RESULT IN THE MAXIMUM VALUE OF PEAK FLOW.

\*\*\*\*\*

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	9.57	7.32	3.905
2	13.27	12.01	3.179

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 13.27 Tc(MIN.) = 12.01  
 TOTAL AREA(ACRES) = 4.2

\*\*\*\*\*

FLOW PROCESS FROM NODE 40.00 TO NODE 40.00 IS CODE = 12

>>>>CLEAR MEMORY BANK # 1 <<<<

=====

\*\*\*\*\*

FLOW PROCESS FROM NODE 40.00 TO NODE 47.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<

>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1141.38 DOWNSTREAM(FEET) = 1138.35  
 FLOW LENGTH(FEET) = 210.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 24.0 INCH PIPE IS 12.0 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 8.44  
 GIVEN PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 13.27  
 PIPE TRAVEL TIME(MIN.) = 0.41 Tc(MIN.) = 12.43  
 LONGEST FLOWPATH FROM NODE 70.00 TO NODE 47.00 = 11320.30 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 47.00 TO NODE 48.00 IS CODE = 41

```

>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

```

```

=====
ELEVATION DATA: UPSTREAM(FEET) = 1135.35 DOWNSTREAM(FEET) = 1134.95
FLOW LENGTH(FEET) = 25.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 60.0 INCH PIPE IS 8.3 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 8.05
GIVEN PIPE DIAMETER(INCH) = 60.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 13.27
PIPE TRAVEL TIME(MIN.) = 0.05 Tc(MIN.) = 12.48
LONGEST FLOWPATH FROM NODE 70.00 TO NODE 48.00 = 11345.30 FEET.

```

```

*****
FLOW PROCESS FROM NODE 48.00 TO NODE 48.00 IS CODE = 1

```

```

>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

```

```

=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 12.48
RAINFALL INTENSITY(INCH/HR) = 3.13
TOTAL STREAM AREA(ACRES) = 4.22
PEAK FLOW RATE(CFS) AT CONFLUENCE = 13.27

```

```

*****
FLOW PROCESS FROM NODE 49.00 TO NODE 63.00 IS CODE = 22

```

```

>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

```

```

=====
ASSUMED INITIAL SUBAREA UNIFORM
DEVELOPMENT IS COMMERCIAL
USER SPECIFIED Tc(MIN.) = 5.000
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.574
COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8896
SOIL CLASSIFICATION IS "C"
SUBAREA RUNOFF(CFS) = 0.57
TOTAL AREA(ACRES) = 0.14 TOTAL RUNOFF(CFS) = 0.57

```

```

*****
FLOW PROCESS FROM NODE 63.00 TO NODE 50.00 IS CODE = 51

```

```

>>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
>>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

```

```

=====
ELEVATION DATA: UPSTREAM(FEET) = 1152.00 DOWNSTREAM(FEET) = 1149.03
CHANNEL LENGTH THRU SUBAREA(FEET) = 94.00 CHANNEL SLOPE = 0.0316
CHANNEL BASE(FEET) = 0.00 "Z" FACTOR = 99.000
MANNING'S FACTOR = 0.015 MAXIMUM DEPTH(FEET) = 1.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.282
COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8890
SOIL CLASSIFICATION IS "C"
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.78
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 1.82
AVERAGE FLOW DEPTH(FEET) = 0.07 TRAVEL TIME(MIN.) = 0.86
Tc(MIN.) = 5.86
SUBAREA AREA(ACRES) = 0.11 SUBAREA RUNOFF(CFS) = 0.42
TOTAL AREA(ACRES) = 0.2 PEAK FLOW RATE(CFS) = 0.99

```

```

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH(FEET) = 0.07 FLOW VELOCITY(FEET/SEC.) = 1.95
LONGEST FLOWPATH FROM NODE 49.00 TO NODE 50.00 = 1000094.00 FEET.

```

\*\*\*\*\*

FLOW PROCESS FROM NODE 50.00 TO NODE 50.00 IS CODE = 81

&gt;&gt;&gt;&gt;ADDITION OF SUBAREA TO MAINLINE PEAK FLOW&lt;&lt;&lt;&lt;

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.282  
 COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8890  
 SOIL CLASSIFICATION IS "C"  
 SUBAREA AREA(ACRES) = 0.11 SUBAREA RUNOFF(CFS) = 0.42  
 TOTAL AREA(ACRES) = 0.4 TOTAL RUNOFF(CFS) = 1.41  
 TC(MIN.) = 5.86

\*\*\*\*\*

FLOW PROCESS FROM NODE 50.00 TO NODE 48.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<  
 >>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1145.74 DOWNSTREAM(FEET) = 1136.51  
 FLOW LENGTH(FEET) = 24.30 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 1.9 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 14.58  
 GIVEN PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 1.41  
 PIPE TRAVEL TIME(MIN.) = 0.03 Tc(MIN.) = 5.89  
 LONGEST FLOWPATH FROM NODE 49.00 TO NODE 48.00 = 1000118.31 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 48.00 TO NODE 48.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 5.89  
 RAINFALL INTENSITY(INCH/HR) = 4.27  
 TOTAL STREAM AREA(ACRES) = 0.36  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 1.41

## \*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	13.27	12.48	3.129	4.22
2	1.41	5.89	4.273	0.36

\*\*\*\*\*WARNING\*\*\*\*\*

IN THIS COMPUTER PROGRAM, THE CONFLUENCE VALUE USED IS BASED  
 ON THE RCFC&WCD FORMULA OF PLATE D-1 AS DEFAULT VALUE. THIS FORMULA  
 WILL NOT NECESSARILY RESULT IN THE MAXIMUM VALUE OF PEAK FLOW.

\*\*\*\*\*

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

## \*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	7.67	5.89	4.273
2	14.30	12.48	3.129

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 14.30 Tc(MIN.) = 12.48

TOTAL AREA(ACRES) = 4.6  
 LONGEST FLOWPATH FROM NODE 49.00 TO NODE 48.00 = 1000118.31 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 48.00 TO NODE 51.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<  
 >>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1134.95 DOWNSTREAM(FEET) = 1132.94  
 FLOW LENGTH(FEET) = 126.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 60.0 INCH PIPE IS 8.6 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 8.22  
 GIVEN PIPE DIAMETER(INCH) = 60.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 14.30  
 PIPE TRAVEL TIME(MIN.) = 0.26 Tc(MIN.) = 12.73  
 LONGEST FLOWPATH FROM NODE 49.00 TO NODE 51.00 = 1000244.31 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 51.00 TO NODE 51.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
 TIME OF CONCENTRATION(MIN.) = 12.73  
 RAINFALL INTENSITY(INCH/HR) = 3.10  
 TOTAL STREAM AREA(ACRES) = 4.58  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 14.30

\*\*\*\*\*

FLOW PROCESS FROM NODE 51.00 TO NODE 53.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

=====

ASSUMED INITIAL SUBAREA UNIFORM  
 DEVELOPMENT IS COMMERCIAL  
 $TC = K * [(LENGTH ** 3) / (ELEVATION CHANGE)] ** .2$   
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
 UPSTREAM ELEVATION(FEET) = 1151.89  
 DOWNSTREAM ELEVATION(FEET) = 1149.00  
 ELEVATION DIFFERENCE(FEET) = 2.89  
 $TC = 0.303 * [(100.00 ** 3) / (2.89)] ** .2 = 3.885$   
 COMPUTED TIME OF CONCENTRATION INCREASED TO 5 MIN.  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.574  
 COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8896  
 SOIL CLASSIFICATION IS "C"  
 SUBAREA RUNOFF(CFS) = 0.57  
 TOTAL AREA(ACRES) = 0.14 TOTAL RUNOFF(CFS) = 0.57

\*\*\*\*\*

FLOW PROCESS FROM NODE 53.00 TO NODE 51.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<  
 >>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1145.16 DOWNSTREAM(FEET) = 1144.09  
 FLOW LENGTH(FEET) = 76.70 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 12.0 INCH PIPE IS 3.0 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 3.66  
 GIVEN PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 0.57  
 PIPE TRAVEL TIME(MIN.) = 0.35 Tc(MIN.) = 5.35



LONGEST FLOWPATH FROM NODE 51.00 TO NODE 51.00 = 176.70 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 51.00 TO NODE 51.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 5.35  
RAINFALL INTENSITY(INCH/HR) = 4.45  
TOTAL STREAM AREA(ACRES) = 0.14  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 0.57

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	T <sub>c</sub> (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	14.30	12.73	3.103	4.58
2	0.57	5.35	4.448	0.14

\*\*\*\*\*WARNING\*\*\*\*\*

IN THIS COMPUTER PROGRAM, THE CONFLUENCE VALUE USED IS BASED  
ON THE RCFC&WCD FORMULA OF PLATE D-1 AS DEFAULT VALUE. THIS FORMULA  
WILL NOT NECESSARILY RESULT IN THE MAXIMUM VALUE OF PEAK FLOW.

\*\*\*\*\*

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	T <sub>c</sub> (MIN.)	INTENSITY (INCH/HOUR)
1	6.58	5.35	4.448
2	14.69	12.73	3.103

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 14.69 T<sub>c</sub>(MIN.) = 12.73

TOTAL AREA(ACRES) = 4.7

LONGEST FLOWPATH FROM NODE 49.00 TO NODE 51.00 = 1000244.31 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 51.00 TO NODE 54.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<  
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1132.94 DOWNSTREAM(FEET) = 1131.53  
FLOW LENGTH(FEET) = 23.50 MANNING'S N = 0.013  
DEPTH OF FLOW IN 60.0 INCH PIPE IS 6.4 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 13.19  
GIVEN PIPE DIAMETER(INCH) = 60.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 14.69  
PIPE TRAVEL TIME(MIN.) = 0.03 T<sub>c</sub>(MIN.) = 12.76  
LONGEST FLOWPATH FROM NODE 49.00 TO NODE 54.00 = 1000267.81 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 54.00 TO NODE 54.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:

TIME OF CONCENTRATION(MIN.) = 12.76  
 RAINFALL INTENSITY(INCH/HR) = 3.10  
 TOTAL STREAM AREA(ACRES) = 4.72  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 14.69

\*\*\*\*\*

FLOW PROCESS FROM NODE 55.00 TO NODE 56.00 IS CODE = 22

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

=====

ASSUMED INITIAL SUBAREA UNIFORM

DEVELOPMENT IS COMMERCIAL

USER SPECIFIED Tc(MIN.) = 5.000

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.574

COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8896

SOIL CLASSIFICATION IS "C"

SUBAREA RUNOFF(CFS) = 0.24

TOTAL AREA(ACRES) = 0.06 TOTAL RUNOFF(CFS) = 0.24

\*\*\*\*\*

FLOW PROCESS FROM NODE 56.00 TO NODE 57.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<

>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1151.99 DOWNSTREAM(FEET) = 1151.26

CHANNEL LENGTH THRU SUBAREA(FEET) = 60.00 CHANNEL SLOPE = 0.0122

CHANNEL BASE(FEET) = 0.00 "Z" FACTOR = 99.000

MANNING'S FACTOR = 0.015 MAXIMUM DEPTH(FEET) = 1.00

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.208

COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8888

SOIL CLASSIFICATION IS "C"

TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.28

TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 0.90

AVERAGE FLOW DEPTH(FEET) = 0.06 TRAVEL TIME(MIN.) = 1.11

Tc(MIN.) = 6.11

SUBAREA AREA(ACRES) = 0.02 SUBAREA RUNOFF(CFS) = 0.07

TOTAL AREA(ACRES) = 0.1 PEAK FLOW RATE(CFS) = 0.32

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.06 FLOW VELOCITY(FEET/SEC.) = 1.02

LONGEST FLOWPATH FROM NODE 55.00 TO NODE 57.00 = \*\*\*\*\* FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 57.00 TO NODE 57.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.208

COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8888

SOIL CLASSIFICATION IS "C"

SUBAREA AREA(ACRES) = 0.02 SUBAREA RUNOFF(CFS) = 0.07

TOTAL AREA(ACRES) = 0.1 TOTAL RUNOFF(CFS) = 0.39

TC(MIN.) = 6.11

\*\*\*\*\*

FLOW PROCESS FROM NODE 57.00 TO NODE 54.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<

>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1145.14 DOWNSTREAM(FEET) = 1135.70

FLOW LENGTH(FEET) = 103.00 MANNING'S N = 0.013

DEPTH OF FLOW IN 10.0 INCH PIPE IS 1.7 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 6.61  
 GIVEN PIPE DIAMETER(INCH) = 10.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 0.39  
 PIPE TRAVEL TIME(MIN.) = 0.26 Tc(MIN.) = 6.37  
 LONGEST FLOWPATH FROM NODE 55.00 TO NODE 54.00 = \*\*\*\*\* FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 54.00 TO NODE 54.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 6.37  
 RAINFALL INTENSITY(INCH/HR) = 4.14  
 TOTAL STREAM AREA(ACRES) = 0.10  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 0.39

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	14.69	12.76	3.100	4.72
2	0.39	6.37	4.136	0.10

\*\*\*\*\*WARNING\*\*\*\*\*

IN THIS COMPUTER PROGRAM, THE CONFLUENCE VALUE USED IS BASED  
 ON THE RCFC&WCD FORMULA OF PLATE D-1 AS DEFAULT VALUE. THIS FORMULA  
 WILL NOT NECESSARILY RESULT IN THE MAXIMUM VALUE OF PEAK FLOW.

\*\*\*\*\*

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	7.73	6.37	4.136
2	14.99	12.76	3.100

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 14.99 Tc(MIN.) = 12.76  
 TOTAL AREA(ACRES) = 4.8  
 LONGEST FLOWPATH FROM NODE 55.00 TO NODE 54.00 = \*\*\*\*\* FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 54.00 TO NODE 58.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1131.53 DOWNSTREAM(FEET) = 1130.68  
 FLOW LENGTH(FEET) = 197.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 60.0 INCH PIPE IS 12.2 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 5.26  
 GIVEN PIPE DIAMETER(INCH) = 60.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 14.99  
 PIPE TRAVEL TIME(MIN.) = 0.62 Tc(MIN.) = 13.39  
 LONGEST FLOWPATH FROM NODE 55.00 TO NODE 58.00 = \*\*\*\*\* FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 58.00 TO NODE 58.00 IS CODE = 1

-----  
 >>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<  
 =====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
 TIME OF CONCENTRATION(MIN.) = 13.39  
 RAINFALL INTENSITY(INCH/HR) = 3.04  
 TOTAL STREAM AREA(ACRES) = 4.82  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 14.99

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 59.00 TO NODE 60.00 IS CODE = 22  
 -----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<  
 =====

ASSUMED INITIAL SUBAREA UNIFORM  
 DEVELOPMENT IS COMMERCIAL  
 USER SPECIFIED Tc(MIN.) = 5.000  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.574  
 COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8896  
 SOIL CLASSIFICATION IS "C"  
 SUBAREA RUNOFF(CFS) = 0.24  
 TOTAL AREA(ACRES) = 0.06 TOTAL RUNOFF(CFS) = 0.24

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 60.00 TO NODE 61.00 IS CODE = 51  
 -----

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<  
 >>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<  
 =====

ELEVATION DATA: UPSTREAM(FEET) = 1151.99 DOWNSTREAM(FEET) = 1145.05  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 285.00 CHANNEL SLOPE = 0.0244  
 CHANNEL BASE(FEET) = 0.00 "Z" FACTOR = 99.000  
 MANNING'S FACTOR = 0.015 MAXIMUM DEPTH(FEET) = 1.00  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.812  
 COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8878  
 SOIL CLASSIFICATION IS "C"  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.92  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 1.72  
 AVERAGE FLOW DEPTH(FEET) = 0.07 TRAVEL TIME(MIN.) = 2.76  
 Tc(MIN.) = 7.76  
 SUBAREA AREA(ACRES) = 0.40 SUBAREA RUNOFF(CFS) = 1.35  
 TOTAL AREA(ACRES) = 0.5 PEAK FLOW RATE(CFS) = 1.60

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.09 FLOW VELOCITY(FEET/SEC.) = 2.05  
 LONGEST FLOWPATH FROM NODE 59.00 TO NODE 61.00 = 319.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 61.00 TO NODE 61.00 IS CODE = 81  
 -----

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<  
 =====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.812  
 COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8878  
 SOIL CLASSIFICATION IS "C"  
 SUBAREA AREA(ACRES) = 0.40 SUBAREA RUNOFF(CFS) = 1.35  
 TOTAL AREA(ACRES) = 0.9 TOTAL RUNOFF(CFS) = 2.95  
 TC(MIN.) = 7.76

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 61.00 TO NODE 58.00 IS CODE = 31  
 -----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

```
=====
ELEVATION DATA: UPSTREAM(FEET) = 1140.87  DOWNSTREAM(FEET) = 1140.80
FLOW LENGTH(FEET) = 14.00  MANNING'S N = 0.013
DEPTH OF FLOW IN 15.0 INCH PIPE IS 8.9 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 3.88
ESTIMATED PIPE DIAMETER(INCH) = 15.00  NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 2.95
PIPE TRAVEL TIME(MIN.) = 0.06  Tc(MIN.) = 7.82
LONGEST FLOWPATH FROM NODE 59.00 TO NODE 58.00 = 333.00 FEET.
```

\*\*\*\*\*

```
FLOW PROCESS FROM NODE 58.00 TO NODE 58.00 IS CODE = 1
```

```
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<
```

```
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 7.82
RAINFALL INTENSITY(INCH/HR) = 3.80
TOTAL STREAM AREA(ACRES) = 0.86
PEAK FLOW RATE(CFS) AT CONFLUENCE = 2.95
```

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	14.99	13.39	3.039	4.82
2	2.95	7.82	3.799	0.86

\*\*\*\*\*WARNING\*\*\*\*\*

IN THIS COMPUTER PROGRAM, THE CONFLUENCE VALUE USED IS BASED  
 ON THE RCFC&WCD FORMULA OF PLATE D-1 AS DEFAULT VALUE. THIS FORMULA  
 WILL NOT NECESSARILY RESULT IN THE MAXIMUM VALUE OF PEAK FLOW.

\*\*\*\*\*

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	11.70	7.82	3.799
2	17.35	13.39	3.039

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

```
PEAK FLOW RATE(CFS) = 17.35  Tc(MIN.) = 13.39
TOTAL AREA(ACRES) = 5.7
LONGEST FLOWPATH FROM NODE 55.00 TO NODE 58.00 = ***** FEET.
```

\*\*\*\*\*

```
FLOW PROCESS FROM NODE 58.00 TO NODE 62.00 IS CODE = 41
```

```
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<
```

```
=====
ELEVATION DATA: UPSTREAM(FEET) = 1130.68  DOWNSTREAM(FEET) = 1130.30
FLOW LENGTH(FEET) = 86.00  MANNING'S N = 0.013
DEPTH OF FLOW IN 60.0 INCH PIPE IS 13.0 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 5.54
GIVEN PIPE DIAMETER(INCH) = 60.00  NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 17.35
```

```

                                RS_E_100.RES
PIPE TRAVEL TIME(MIN.) =    0.26    Tc(MIN.) =    13.65
LONGEST FLOWPATH FROM NODE    55.00 TO NODE    62.00 = ***** FEET.

*****
FLOW PROCESS FROM NODE    62.00 TO NODE    62.00 IS CODE = 10
-----
>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<
=====
*****
FLOW PROCESS FROM NODE    64.00 TO NODE    65.00 IS CODE = 21
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
=====
    ASSUMED INITIAL SUBAREA UNIFORM
    DEVELOPMENT IS COMMERCIAL
    TC = K*[(LENGTH**3)/(ELEVATION CHANGE)]**.2
    INITIAL SUBAREA FLOW-LENGTH(FEET) =    100.00
    UPSTREAM ELEVATION(FEET) =    1154.94
    DOWNSTREAM ELEVATION(FEET) =    1151.51
    ELEVATION DIFFERENCE(FEET) =        3.43
    TC = 0.303*[( 100.00**3)/(    3.43)]**.2 =    3.754
    COMPUTED TIME OF CONCENTRATION INCREASED TO 5 MIN.
    100 YEAR RAINFALL INTENSITY(INCH/HOUR) =    4.574
    COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8896
    SOIL CLASSIFICATION IS "C"
    SUBAREA RUNOFF(CFS) =        0.33
    TOTAL AREA(ACRES) =        0.08    TOTAL RUNOFF(CFS) =        0.33

*****
FLOW PROCESS FROM NODE    65.00 TO NODE    66.00 IS CODE = 51
-----
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<
=====
    ELEVATION DATA: UPSTREAM(FEET) =    1151.51    DOWNSTREAM(FEET) =    1146.98
    CHANNEL LENGTH THRU SUBAREA(FEET) =    260.00    CHANNEL SLOPE =    0.0174
    CHANNEL BASE(FEET) =        0.00    "Z" FACTOR =    99.000
    MANNING'S FACTOR =    0.015    MAXIMUM DEPTH(FEET) =    1.00
    100 YEAR RAINFALL INTENSITY(INCH/HOUR) =    3.801
    COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8877
    SOIL CLASSIFICATION IS "C"
    TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) =        0.96
    TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) =    1.54
    AVERAGE FLOW DEPTH(FEET) =    0.08    TRAVEL TIME(MIN.) =    2.81
    Tc(MIN.) =        7.81
    SUBAREA AREA(ACRES) =        0.37    SUBAREA RUNOFF(CFS) =    1.25
    TOTAL AREA(ACRES) =        0.4    PEAK FLOW RATE(CFS) =        1.57

    END OF SUBAREA CHANNEL FLOW HYDRAULICS:
    DEPTH(FEET) =    0.10    FLOW VELOCITY(FEET/SEC.) =    1.71
    LONGEST FLOWPATH FROM NODE    64.00 TO NODE    66.00 =    360.00 FEET.

*****
FLOW PROCESS FROM NODE    66.00 TO NODE    66.00 IS CODE = 81
-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====
    100 YEAR RAINFALL INTENSITY(INCH/HOUR) =    3.801
    COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8877
    SOIL CLASSIFICATION IS "C"
    SUBAREA AREA(ACRES) =        0.37    SUBAREA RUNOFF(CFS) =    1.25
    TOTAL AREA(ACRES) =        0.8    TOTAL RUNOFF(CFS) =    2.82

```

TC(MIN.) = 7.81

\*\*\*\*\*

FLOW PROCESS FROM NODE 66.00 TO NODE 66.00 IS CODE = 1

&gt;&gt;&gt;&gt;DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE&lt;&lt;&lt;&lt;&lt;

TOTAL NUMBER OF STREAMS = 2

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:

TIME OF CONCENTRATION(MIN.) = 7.81

RAINFALL INTENSITY(INCH/HR) = 3.80

TOTAL STREAM AREA(ACRES) = 0.82

PEAK FLOW RATE(CFS) AT CONFLUENCE = 2.82

\*\*\*\*\*

FLOW PROCESS FROM NODE 67.00 TO NODE 68.00 IS CODE = 22

&gt;&gt;&gt;&gt;RATIONAL METHOD INITIAL SUBAREA ANALYSIS&lt;&lt;&lt;&lt;&lt;

ASSUMED INITIAL SUBAREA UNIFORM

DEVELOPMENT IS COMMERCIAL

USER SPECIFIED Tc(MIN.) = 5.000

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.574

COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8896

SOIL CLASSIFICATION IS "C"

SUBAREA RUNOFF(CFS) = 0.24

TOTAL AREA(ACRES) = 0.06 TOTAL RUNOFF(CFS) = 0.24

\*\*\*\*\*

FLOW PROCESS FROM NODE 68.00 TO NODE 66.00 IS CODE = 51

&gt;&gt;&gt;&gt;COMPUTE TRAPEZOIDAL CHANNEL FLOW&lt;&lt;&lt;&lt;&lt;

&gt;&gt;&gt;&gt;TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)&lt;&lt;&lt;&lt;&lt;

ELEVATION DATA: UPSTREAM(FEET) = 1151.99 DOWNSTREAM(FEET) = 1146.98

CHANNEL LENGTH THRU SUBAREA(FEET) = 236.00 CHANNEL SLOPE = 0.0212

CHANNEL BASE(FEET) = 0.00 "Z" FACTOR = 99.000

MANNING'S FACTOR = 0.015 MAXIMUM DEPTH(FEET) = 1.00

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.876

COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8880

SOIL CLASSIFICATION IS "C"

TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.69

TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 1.61

AVERAGE FLOW DEPTH(FEET) = 0.07 TRAVEL TIME(MIN.) = 2.45

Tc(MIN.) = 7.45

SUBAREA AREA(ACRES) = 0.26 SUBAREA RUNOFF(CFS) = 0.89

TOTAL AREA(ACRES) = 0.3 PEAK FLOW RATE(CFS) = 1.14

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.08 FLOW VELOCITY(FEET/SEC.) = 1.75

LONGEST FLOWPATH FROM NODE 67.00 TO NODE 66.00 = 3636.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 66.00 TO NODE 66.00 IS CODE = 81

&gt;&gt;&gt;&gt;ADDITION OF SUBAREA TO MAINLINE PEAK FLOW&lt;&lt;&lt;&lt;&lt;

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.876

COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8880

SOIL CLASSIFICATION IS "C"

SUBAREA AREA(ACRES) = 0.26 SUBAREA RUNOFF(CFS) = 0.89

TOTAL AREA(ACRES) = 0.6 TOTAL RUNOFF(CFS) = 2.03

TC(MIN.) = 7.45

\*\*\*\*\*

FLOW PROCESS FROM NODE 66.00 TO NODE 66.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 7.45  
RAINFALL INTENSITY(INCH/HR) = 3.88  
TOTAL STREAM AREA(ACRES) = 0.58  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 2.03

## \*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	T <sub>c</sub> (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	2.82	7.81	3.801	0.82
2	2.03	7.45	3.876	0.58

\*\*\*\*\*WARNING\*\*\*\*\*

IN THIS COMPUTER PROGRAM, THE CONFLUENCE VALUE USED IS BASED  
ON THE RCFC&WCD FORMULA OF PLATE D-1 AS DEFAULT VALUE. THIS FORMULA  
WILL NOT NECESSARILY RESULT IN THE MAXIMUM VALUE OF PEAK FLOW.

\*\*\*\*\*

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

## \*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	T <sub>c</sub> (MIN.)	INTENSITY (INCH/HOUR)
1	4.73	7.45	3.876
2	4.82	7.81	3.801

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 4.82 T<sub>c</sub>(MIN.) = 7.81  
TOTAL AREA(ACRES) = 1.4  
LONGEST FLOWPATH FROM NODE 67.00 TO NODE 66.00 = 3636.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 66.00 TO NODE 69.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1146.98 DOWNSTREAM(FEET) = 1139.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 281.00 CHANNEL SLOPE = 0.0284  
CHANNEL BASE(FEET) = 0.00 "Z" FACTOR = 99.000  
MANNING'S FACTOR = 0.015 MAXIMUM DEPTH(FEET) = 1.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.511  
COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8869  
SOIL CLASSIFICATION IS "C"  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 5.11  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 2.86  
AVERAGE FLOW DEPTH(FEET) = 0.13 TRAVEL TIME(MIN.) = 1.64  
T<sub>c</sub>(MIN.) = 9.45  
SUBAREA AREA(ACRES) = 0.19 SUBAREA RUNOFF(CFS) = 0.59  
TOTAL AREA(ACRES) = 1.6 PEAK FLOW RATE(CFS) = 5.41

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.14 FLOW VELOCITY(FEET/SEC.) = 2.78  
LONGEST FLOWPATH FROM NODE 67.00 TO NODE 69.00 = 3917.00 FEET.



\*\*\*\*\*

FLOW PROCESS FROM NODE 69.00 TO NODE 69.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) =	3.511
COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT =	.8869
SOIL CLASSIFICATION IS	"C"
SUBAREA AREA(ACRES) =	0.19
SUBAREA RUNOFF(CFS) =	0.59
TOTAL AREA(ACRES) =	1.8
TOTAL RUNOFF(CFS) =	6.00
TC(MIN.) =	9.45

\*\*\*\*\*

FLOW PROCESS FROM NODE 69.00 TO NODE 62.00 IS CODE = 41

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<  
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) =	1132.39	DOWNSTREAM(FEET) =	1132.00
FLOW LENGTH(FEET) =	11.40	MANNING'S N =	0.013
DEPTH OF FLOW IN 18.0 INCH PIPE IS	7.0 INCHES		
PIPE-FLOW VELOCITY(FEET/SEC.) =	9.51		
GIVEN PIPE DIAMETER(INCH) =	18.00	NUMBER OF PIPES =	1
PIPE-FLOW(CFS) =	6.00		
PIPE TRAVEL TIME(MIN.) =	0.02	Tc(MIN.) =	9.47
LONGEST FLOWPATH FROM NODE	67.00 TO NODE	62.00 =	3928.40 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 62.00 TO NODE 62.00 IS CODE = 11

-----  
>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<

\*\*\*\*\*

\*\* MAIN STREAM CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	6.00	9.47	3.508	1.78
LONGEST FLOWPATH FROM NODE 67.00 TO NODE 62.00 = 3928.40 FEET.				

\*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	17.35	13.65	3.015	5.68
LONGEST FLOWPATH FROM NODE 55.00 TO NODE 62.00 = ***** FEET.				

\*\*\*\*\*WARNING\*\*\*\*\*

IN THIS COMPUTER PROGRAM, THE CONFLUENCE VALUE USED IS BASED  
ON THE RCFC&WCD FORMULA OF PLATE D-1 AS DEFAULT VALUE. THIS FORMULA  
WILL NOT NECESSARILY RESULT IN THE MAXIMUM VALUE OF PEAK FLOW.

\*\*\*\*\*

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	18.04	9.47	3.508
2	22.51	13.65	3.015

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) =	22.51	Tc(MIN.) =	13.65
TOTAL AREA(ACRES) =	7.5		

\*\*\*\*\*

FLOW PROCESS FROM NODE 62.00 TO NODE 62.00 IS CODE = 12

-----  
>>>>>CLEAR MEMORY BANK # 1 <<<<<  
=====

=====

END OF STUDY SUMMARY:

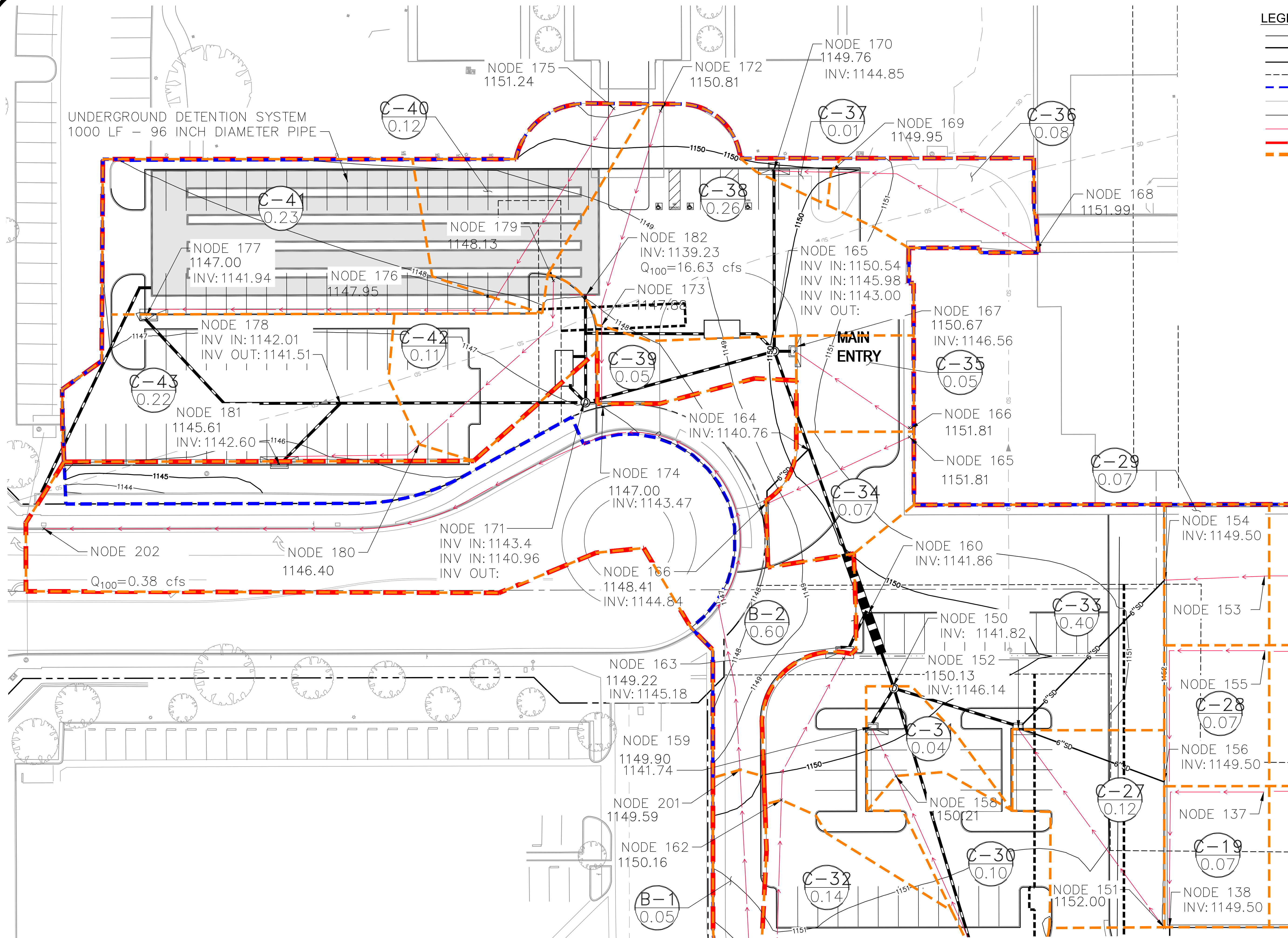
TOTAL AREA(ACRES) = 7.5 TC(MIN.) = 13.65

PEAK FLOW RATE(CFS) = 22.51  
=====

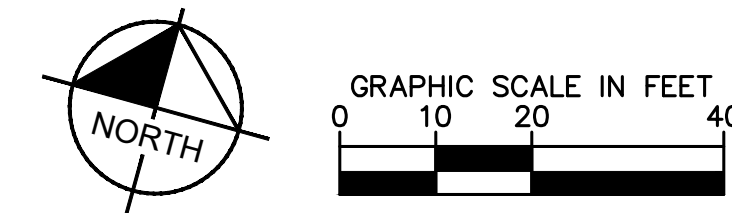
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END OF RATIONAL METHOD ANALYSIS



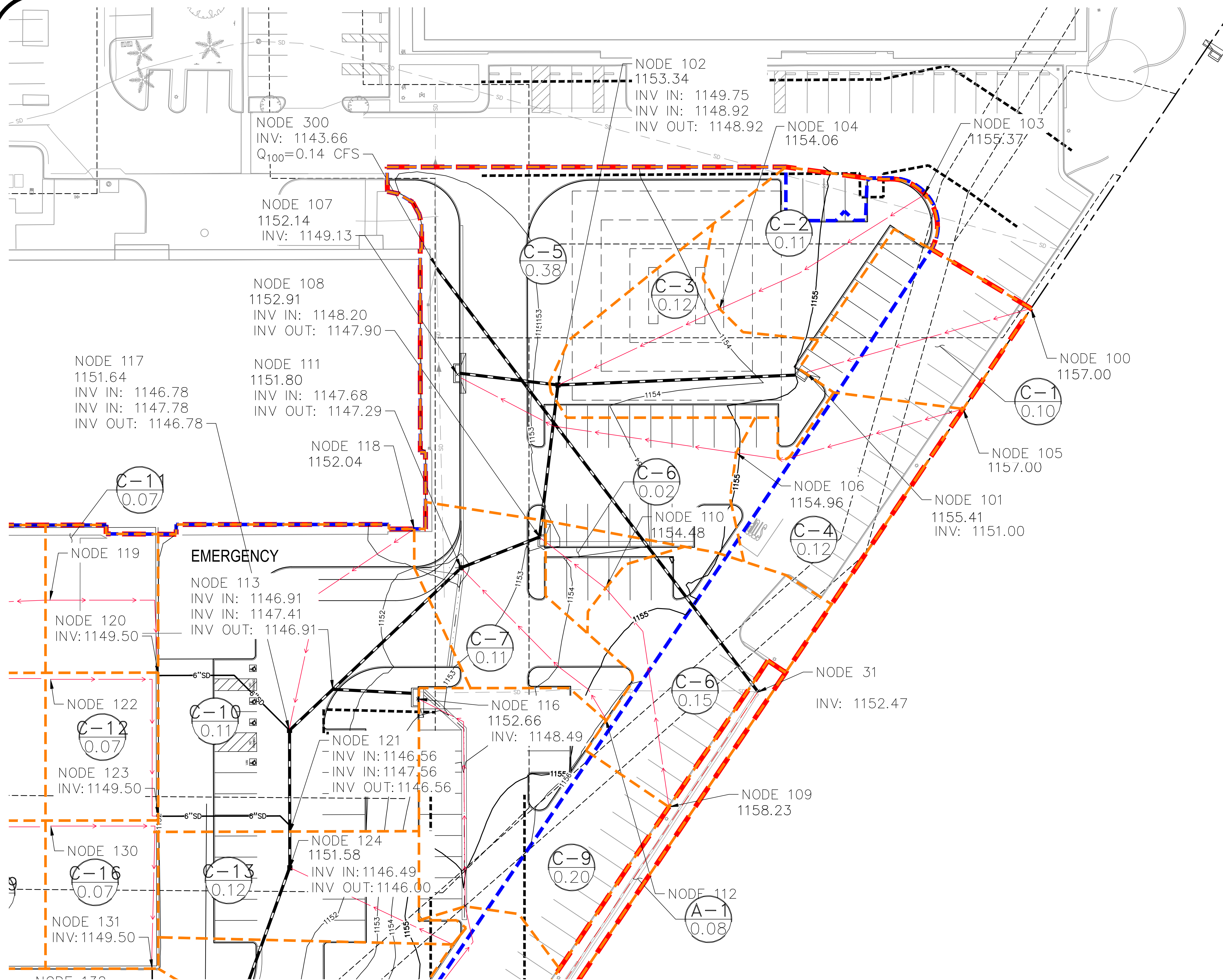


LEGEND	
	CENTER LINE
	PROPERTY LINE
	RIGHT-OF-WAY LINE / LEASE LINE
	EASEMENT LINE
	PROJECT LIMITS
	EXISTING STORM DRAIN LINE
	PROPOSED STORM DRAIN LINE
	LONGEST FLOW PATH
	DENOTES DRAINAGE AREA BOUNDARY
	DENOTES SUB-DRAINAGE AREA BOUNDARY
	SUBAREA NAME AREA (AC)
	EXISTING SURFACE FLOW DIRECTION



RANCHO SPRINGS  
MEDICAL CENTER  
EXISTING CONDITIONS  
HYDROLOGY MAP  
SHEET 1 OF 3  
JUNE 2020





# LEGEND

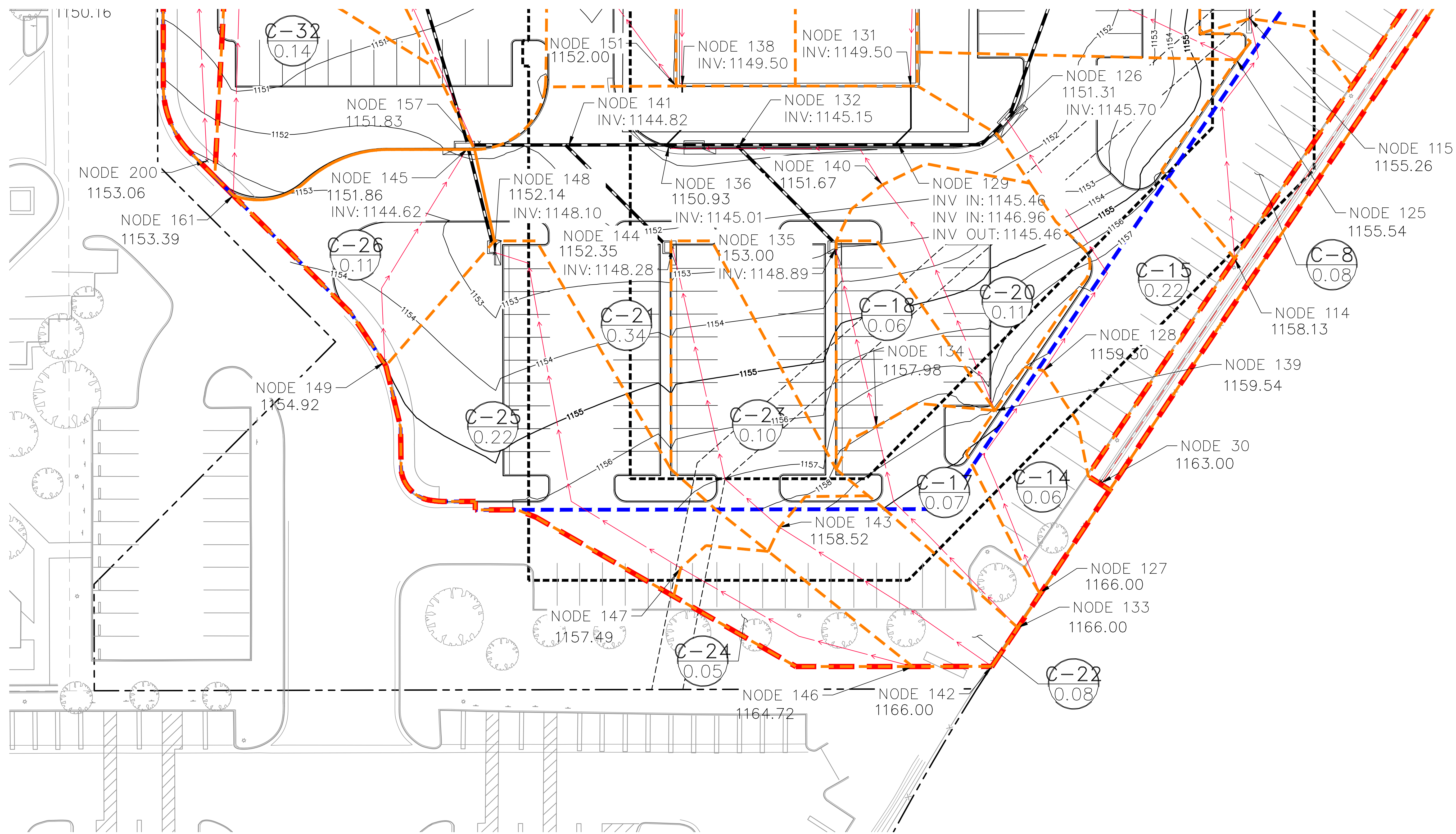
- CENTER LINE
- PROPERTY LINE
- RIGHT-OF-WAY LINE / LEASE LINE
- EASEMENT LINE
- PROJECT LIMITS
- EXISTING STORM DRAIN LINE
- PROPOSED STORM DRAIN LINE
- LONGEST FLOW PATH
- DENOTES DRAINAGE AREA BOUNDARY
- DENOTES SUB-DRAINAGE AREA BOUNDARY
- SUBAREA NAME  
AREA (AC)
- EXISTING SURFACE FLOW DIRECTION

RANCHO SPRINGS  
MEDICAL CENTER  
EXISTING CONDITIONS  
HYDROLOGY MAP  
SHEET 2 OF 3  
JUNE 2020

**Kimley»Horn**

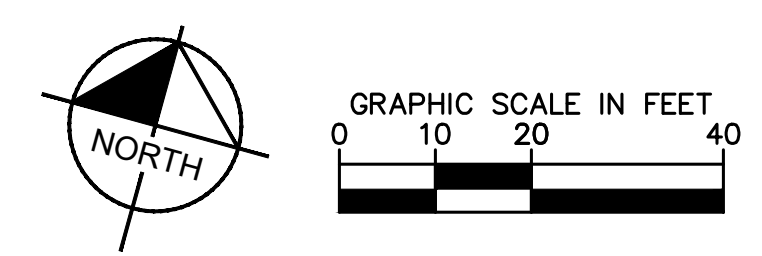
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660 S. FIGUEROA ST., SUITE 2050, LOS ANGELES, CA 90017  
PHONE: 213-261-4040





**LEGEND**

	CENTER LINE
	PROPERTY LINE
	RIGHT-OF-WAY LINE / LEASE LINE
	EASEMENT LINE
	PROJECT LIMITS
	EXISTING STORM DRAIN LINE
	PROPOSED STORM DRAIN LINE
	LONGEST FLOW PATH
	DENOTES DRAINAGE AREA BOUNDARY
	DENOTES SUB-DRAINAGE AREA BOUNDARY
	SUBAREA NAME AREA (AC)
	EXISTING SURFACE FLOW DIRECTION



RANCHO SPRINGS  
MEDICAL CENTER  
EXISTING CONDITIONS  
HYDROLOGY MAP  
SHEET 3 OF 3  
JUNE 2020

\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM BASED ON  
 RIVERSIDE COUNTY FLOOD CONTROL & WATER CONSERVATION DISTRICT  
 (RCFC&WCD) 1978 HYDROLOGY MANUAL  
 (c) Copyright 1982-2011 Advanced Engineering Software (aes)  
 (Rational Tabling Version 18.0)  
 Release Date: 07/01/2011 License ID 1499

Analysis prepared by:

Kimley-Horn and Associates, Inc.  
 765 The City Drive  
 Suite 200  
 Orange, CA 92868

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*

\* Rancho Springs Medical Center \*  
 \* Proposed Conditions \*  
 \* 10-year analysis \*

\*\*\*\*\*

FILE NAME: RS\_P.DAT

TIME/DATE OF STUDY: 07:27 05/18/2020

-----  
 USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
 -----

USER SPECIFIED STORM EVENT(YEAR) = 10.00  
 SPECIFIED MINIMUM PIPE SIZE(INCH) = 12.00  
 SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.95  
 10-YEAR STORM 10-MINUTE INTENSITY(INCH/HOUR) = 2.070  
 10-YEAR STORM 60-MINUTE INTENSITY(INCH/HOUR) = 0.985  
 100-YEAR STORM 10-MINUTE INTENSITY(INCH/HOUR) = 3.430  
 100-YEAR STORM 60-MINUTE INTENSITY(INCH/HOUR) = 1.630  
 SLOPE OF 10-YEAR INTENSITY-DURATION CURVE = 0.4144876  
 SLOPE OF 100-YEAR INTENSITY-DURATION CURVE = 0.4152232

COMPUTED RAINFALL INTENSITY DATA:

STORM EVENT = 10.00 1-HOUR INTENSITY(INCH/HOUR) = 0.995  
 SLOPE OF INTENSITY DURATION CURVE = 0.4145

RCFC&WCD HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD

NOTE: COMPUTE CONFLUENCE VALUES ACCORDING TO RCFC&WCD HYDROLOGY MANUAL

AND IGNORE OTHER CONFLUENCE COMBINATIONS FOR DOWNSTREAM ANALYSES

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

NO.	HALF- WIDTH (FT)	CROWN TO CROSSFALL (FT)	STREET-CROSSFALL: IN- / OUT- / PARK- SIDE / SIDE / WAY	CURB HEIGHT (FT)	GUTTER-GEOMETRIES: WIDTH (FT)	LIP (FT)	HIKE (FT)	MANNING FACTOR (n)
1	30.0	20.0	0.018/0.018/0.020	0.67	2.00	0.0313	0.167	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
 as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
 OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*

FLOW PROCESS FROM NODE 30.00 TO NODE 31.00 IS CODE = 7

>>>>USER SPECIFIED HYDROLOGY INFORMATION AT NODE<<<<

=====

USER-SPECIFIED VALUES ARE AS FOLLOWS:

TC(MIN) = 5.00 RAIN INTENSITY(INCH/HOUR) = 2.79

```

                                RS_P_10.RES
TOTAL AREA(ACRES) =      0.08   TOTAL RUNOFF(CFS) =      0.14

*****
FLOW PROCESS FROM NODE      31.00 TO NODE      300.00 IS CODE =  41
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 1152.47 DOWNSTREAM(FEET) = 1143.66
FLOW LENGTH(FEET) =  226.00  MANNING'S N =  0.013
DEPTH OF FLOW IN 12.0 INCH PIPE IS  1.2 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) =  3.53
GIVEN PIPE DIAMETER(INCH) = 12.00  NUMBER OF PIPES =  1
PIPE-FLOW(CFS) =      0.14
PIPE TRAVEL TIME(MIN.) =  1.07  Tc(MIN.) =  6.07
LONGEST FLOWPATH FROM NODE      0.00 TO NODE      300.00 =      226.00 FEET.

*****
FLOW PROCESS FROM NODE      100.00 TO NODE      101.00 IS CODE =  21
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
=====
    ASSUMED INITIAL SUBAREA UNIFORM
    DEVELOPMENT IS COMMERCIAL
TC = K*[(LENGTH**3)/(ELEVATION CHANGE)]**.2
INITIAL SUBAREA FLOW-LENGTH(FEET) =  102.00
UPSTREAM ELEVATION(FEET) =  1157.00
DOWNSTREAM ELEVATION(FEET) =  1155.41
ELEVATION DIFFERENCE(FEET) =  1.59
TC = 0.303*[( 102.00**3)/( 1.59)]**.2 =  4.431
COMPUTED TIME OF CONCENTRATION INCREASED TO 5 MIN.
  10 YEAR RAINFALL INTENSITY(INCH/HOUR) =  2.787
COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8841
SOIL CLASSIFICATION IS "C"
SUBAREA RUNOFF(CFS) =      0.25
TOTAL AREA(ACRES) =      0.10  TOTAL RUNOFF(CFS) =      0.25

*****
FLOW PROCESS FROM NODE      101.00 TO NODE      102.00 IS CODE =  41
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 1151.00 DOWNSTREAM(FEET) = 1149.75
FLOW LENGTH(FEET) =  104.00  MANNING'S N =  0.013
DEPTH OF FLOW IN 12.0 INCH PIPE IS  2.1 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) =  2.71
GIVEN PIPE DIAMETER(INCH) = 12.00  NUMBER OF PIPES =  1
PIPE-FLOW(CFS) =      0.25
PIPE TRAVEL TIME(MIN.) =  0.64  Tc(MIN.) =  5.64
LONGEST FLOWPATH FROM NODE      100.00 TO NODE      102.00 =      206.00 FEET.

*****
FLOW PROCESS FROM NODE      102.00 TO NODE      102.00 IS CODE =  1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
=====
TOTAL NUMBER OF STREAMS =  3
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM  1 ARE:
TIME OF CONCENTRATION(MIN.) =  5.64
RAINFALL INTENSITY(INCH/HR) =  2.65
TOTAL STREAM AREA(ACRES) =  0.10
PEAK FLOW RATE(CFS) AT CONFLUENCE =      0.25

```

\*\*\*\*\*

FLOW PROCESS FROM NODE 103.00 TO NODE 104.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

=====

ASSUMED INITIAL SUBAREA UNIFORM

DEVELOPMENT IS COMMERCIAL

TC =  $K * [(LENGTH ** 3) / (ELEVATION CHANGE)] ** .2$

INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00

UPSTREAM ELEVATION(FEET) = 1155.37

DOWNSTREAM ELEVATION(FEET) = 1154.06

ELEVATION DIFFERENCE(FEET) = 1.31

TC =  $0.303 * [(100.00 ** 3) / (1.31)] ** .2 = 4.551$

COMPUTED TIME OF CONCENTRATION INCREASED TO 5 MIN.

10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.787

COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8841

SOIL CLASSIFICATION IS "C"

SUBAREA RUNOFF(CFS) = 0.27

TOTAL AREA(ACRES) = 0.11 TOTAL RUNOFF(CFS) = 0.27

\*\*\*\*\*

FLOW PROCESS FROM NODE 104.00 TO NODE 102.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<

>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1154.06 DOWNSTREAM(FEET) = 1153.34

CHANNEL LENGTH THRU SUBAREA(FEET) = 76.00 CHANNEL SLOPE = 0.0095

CHANNEL BASE(FEET) = 0.00 "Z" FACTOR = 99.000

MANNING'S FACTOR = 0.015 MAXIMUM DEPTH(FEET) = 1.00

10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.540

COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8828

SOIL CLASSIFICATION IS "C"

TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.34

TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 1.01

AVERAGE FLOW DEPTH(FEET) = 0.06 TRAVEL TIME(MIN.) = 1.25

Tc(MIN.) = 6.25

SUBAREA AREA(ACRES) = 0.06 SUBAREA RUNOFF(CFS) = 0.13

TOTAL AREA(ACRES) = 0.2 PEAK FLOW RATE(CFS) = 0.41

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.06 FLOW VELOCITY(FEET/SEC.) = 1.00

LONGEST FLOWPATH FROM NODE 103.00 TO NODE 102.00 = 176.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 102.00 TO NODE 102.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<

=====

10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.540

COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8828

SOIL CLASSIFICATION IS "C"

SUBAREA AREA(ACRES) = 0.06 SUBAREA RUNOFF(CFS) = 0.13

TOTAL AREA(ACRES) = 0.2 TOTAL RUNOFF(CFS) = 0.54

TC(MIN.) = 6.25

\*\*\*\*\*

FLOW PROCESS FROM NODE 102.00 TO NODE 102.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

=====

TOTAL NUMBER OF STREAMS = 3



CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:

TIME OF CONCENTRATION(MIN.) = 6.25  
 RAINFALL INTENSITY(INCH/HR) = 2.54  
 TOTAL STREAM AREA(ACRES) = 0.23  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 0.54

\*\*\*\*\*

FLOW PROCESS FROM NODE 105.00 TO NODE 106.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

ASSUMED INITIAL SUBAREA UNIFORM  
 DEVELOPMENT IS COMMERCIAL

TC =  $K * [(LENGTH ** 3) / (ELEVATION \text{ CHANGE})] ** .2$   
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
 UPSTREAM ELEVATION(FEET) = 1157.00  
 DOWNSTREAM ELEVATION(FEET) = 1154.96  
 ELEVATION DIFFERENCE(FEET) = 2.04  
 TC =  $0.303 * [(100.00 ** 3) / (2.04)] ** .2 = 4.165$   
 COMPUTED TIME OF CONCENTRATION INCREASED TO 5 MIN.  
 10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.787  
 COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8841  
 SOIL CLASSIFICATION IS "C"  
 SUBAREA RUNOFF(CFS) = 0.30  
 TOTAL AREA(ACRES) = 0.12 TOTAL RUNOFF(CFS) = 0.30

\*\*\*\*\*

FLOW PROCESS FROM NODE 106.00 TO NODE 107.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1154.96 DOWNSTREAM(FEET) = 1152.14  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 123.00 CHANNEL SLOPE = 0.0229  
 CHANNEL BASE(FEET) = 0.00 "Z" FACTOR = 99.000  
 MANNING'S FACTOR = 0.015 MAXIMUM DEPTH(FEET) = 1.00  
 10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.523  
 COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8827  
 SOIL CLASSIFICATION IS "C"  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.51  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 1.52  
 AVERAGE FLOW DEPTH(FEET) = 0.06 TRAVEL TIME(MIN.) = 1.35  
 Tc(MIN.) = 6.35  
 SUBAREA AREA(ACRES) = 0.19 SUBAREA RUNOFF(CFS) = 0.42  
 TOTAL AREA(ACRES) = 0.3 PEAK FLOW RATE(CFS) = 0.72

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.07 FLOW VELOCITY(FEET/SEC.) = 1.68  
 LONGEST FLOWPATH FROM NODE 105.00 TO NODE 107.00 = 223.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 107.00 TO NODE 107.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.523  
 COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8827  
 SOIL CLASSIFICATION IS "C"  
 SUBAREA AREA(ACRES) = 0.19 SUBAREA RUNOFF(CFS) = 0.42  
 TOTAL AREA(ACRES) = 0.5 TOTAL RUNOFF(CFS) = 1.14  
 TC(MIN.) = 6.35

\*\*\*\*\*

```

                                RS_P_10.RES
FLOW PROCESS FROM NODE      107.00 TO NODE      102.00 IS CODE =  31
-----
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 1149.13  DOWNSTREAM(FEET) = 1148.92
FLOW LENGTH(FEET) =  43.00  MANNING'S N = 0.013
DEPTH OF FLOW IN 12.0 INCH PIPE IS  5.8 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) =  3.05
ESTIMATED PIPE DIAMETER(INCH) = 12.00  NUMBER OF PIPES =  1
PIPE-FLOW(CFS) =  1.14
PIPE TRAVEL TIME(MIN.) =  0.24  Tc(MIN.) =  6.59
LONGEST FLOWPATH FROM NODE  105.00 TO NODE  102.00 =  266.00 FEET.

*****
FLOW PROCESS FROM NODE      102.00 TO NODE      102.00 IS CODE =  1
-----
>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<
=====
TOTAL NUMBER OF STREAMS =  3
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM  3 ARE:
TIME OF CONCENTRATION(MIN.) =  6.59
RAINFALL INTENSITY(INCH/HR) =  2.49
TOTAL STREAM AREA(ACRES) =  0.50
PEAK FLOW RATE(CFS) AT CONFLUENCE =  1.14

** CONFLUENCE DATA **
STREAM      RUNOFF      Tc      INTENSITY      AREA
NUMBER      (CFS)      (MIN.)  (INCH/ HOUR)  (ACRE)
   1         0.25       5.64       2.651       0.10
   2         0.54       6.25       2.540       0.23
   3         1.14       6.59       2.486       0.50

*****WARNING*****
IN THIS COMPUTER PROGRAM, THE CONFLUENCE VALUE USED IS BASED
ON THE RCFC&WCD FORMULA OF PLATE D-1 AS DEFAULT VALUE. THIS FORMULA
WILL NOT NECESSARILY RESULT IN THE MAXIMUM VALUE OF PEAK FLOW.
*****

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR  3 STREAMS.

** PEAK FLOW RATE TABLE **
STREAM      RUNOFF      Tc      INTENSITY
NUMBER      (CFS)      (MIN.)  (INCH/ HOUR)
   1         1.71       5.64       2.651
   2         1.86       6.25       2.540
   3         1.90       6.59       2.486

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
PEAK FLOW RATE(CFS) =  1.90  Tc(MIN.) =  6.59
TOTAL AREA(ACRES) =  0.8
LONGEST FLOWPATH FROM NODE  105.00 TO NODE  102.00 =  266.00 FEET.

*****
FLOW PROCESS FROM NODE      102.00 TO NODE      108.00 IS CODE =  31
-----
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 1148.92  DOWNSTREAM(FEET) = 1148.20
FLOW LENGTH(FEET) =  65.00  MANNING'S N = 0.013

```

```

                                RS_P_10.RES
DEPTH OF FLOW IN 12.0 INCH PIPE IS 6.1 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 4.70
ESTIMATED PIPE DIAMETER(INCH) = 12.00    NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 1.90
PIPE TRAVEL TIME(MIN.) = 0.23    Tc(MIN.) = 6.82
LONGEST FLOWPATH FROM NODE 105.00 TO NODE 108.00 = 331.00 FEET.

*****
FLOW PROCESS FROM NODE 108.00 TO NODE 108.00 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 6.82
RAINFALL INTENSITY(INCH/HR) = 2.45
TOTAL STREAM AREA(ACRES) = 0.83
PEAK FLOW RATE(CFS) AT CONFLUENCE = 1.90

*****
FLOW PROCESS FROM NODE 109.00 TO NODE 110.00 IS CODE = 21
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
=====
    ASSUMED INITIAL SUBAREA UNIFORM
    DEVELOPMENT IS COMMERCIAL
TC = K*[(LENGTH**3)/(ELEVATION CHANGE)]**.2
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00
UPSTREAM ELEVATION(FEET) = 1158.23
DOWNSTREAM ELEVATION(FEET) = 1154.48
ELEVATION DIFFERENCE(FEET) = 3.75
TC = 0.303*[(100.00**3)/(3.75)]**.2 = 3.688
COMPUTED TIME OF CONCENTRATION INCREASED TO 5 MIN.
10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.787
COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8841
SOIL CLASSIFICATION IS "C"
SUBAREA RUNOFF(CFS) = 0.37
TOTAL AREA(ACRES) = 0.15    TOTAL RUNOFF(CFS) = 0.37

*****
FLOW PROCESS FROM NODE 110.00 TO NODE 108.00 IS CODE = 51
-----
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 1154.48    DOWNSTREAM(FEET) = 1152.91
CHANNEL LENGTH THRU SUBAREA(FEET) = 35.00    CHANNEL SLOPE = 0.0449
CHANNEL BASE(FEET) = 0.00    "Z" FACTOR = 99.000
MANNING'S FACTOR = 0.015    MAXIMUM DEPTH(FEET) = 1.00
10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.708
COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8837
SOIL CLASSIFICATION IS "C"
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.38
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 1.63
AVERAGE FLOW DEPTH(FEET) = 0.05    TRAVEL TIME(MIN.) = 0.36
Tc(MIN.) = 5.36
SUBAREA AREA(ACRES) = 0.01    SUBAREA RUNOFF(CFS) = 0.02
TOTAL AREA(ACRES) = 0.2    PEAK FLOW RATE(CFS) = 0.39

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH(FEET) = 0.05    FLOW VELOCITY(FEET/SEC.) = 1.68
LONGEST FLOWPATH FROM NODE 109.00 TO NODE 108.00 = 135.00 FEET.

```

\*\*\*\*\*

FLOW PROCESS FROM NODE 108.00 TO NODE 108.00 IS CODE = 81

&gt;&gt;&gt;&gt;ADDITION OF SUBAREA TO MAINLINE PEAK FLOW&lt;&lt;&lt;&lt;

10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.708

COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8837

SOIL CLASSIFICATION IS "C"

SUBAREA AREA(ACRES) = 0.01 SUBAREA RUNOFF(CFS) = 0.02

TOTAL AREA(ACRES) = 0.2 TOTAL RUNOFF(CFS) = 0.42

TC(MIN.) = 5.36

\*\*\*\*\*

FLOW PROCESS FROM NODE 108.00 TO NODE 108.00 IS CODE = 1

&gt;&gt;&gt;&gt;DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE&lt;&lt;&lt;&lt;

&gt;&gt;&gt;&gt;AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES&lt;&lt;&lt;&lt;

TOTAL NUMBER OF STREAMS = 2

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:

TIME OF CONCENTRATION(MIN.) = 5.36

RAINFALL INTENSITY(INCH/HR) = 2.71

TOTAL STREAM AREA(ACRES) = 0.17

PEAK FLOW RATE(CFS) AT CONFLUENCE = 0.42

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	1.90	6.82	2.450	0.83
2	0.42	5.36	2.708	0.17

\*\*\*\*\*WARNING\*\*\*\*\*

IN THIS COMPUTER PROGRAM, THE CONFLUENCE VALUE USED IS BASED  
ON THE RCFC&WCD FORMULA OF PLATE D-1 AS DEFAULT VALUE. THIS FORMULA  
WILL NOT NECESSARILY RESULT IN THE MAXIMUM VALUE OF PEAK FLOW.

\*\*\*\*\*

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	1.91	5.36	2.708
2	2.28	6.82	2.450

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 2.28 Tc(MIN.) = 6.82

TOTAL AREA(ACRES) = 1.0

LONGEST FLOWPATH FROM NODE 105.00 TO NODE 108.00 = 331.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 108.00 TO NODE 111.00 IS CODE = 31

&gt;&gt;&gt;&gt;COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA&lt;&lt;&lt;&lt;

&gt;&gt;&gt;&gt;USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)&lt;&lt;&lt;&lt;

ELEVATION DATA: UPSTREAM(FEET) = 1147.90 DOWNSTREAM(FEET) = 1147.68

FLOW LENGTH(FEET) = 36.00 MANNING'S N = 0.013

DEPTH OF FLOW IN 12.0 INCH PIPE IS 8.4 INCHES

PIPE-FLOW VELOCITY(FEET/SEC.) = 3.87

ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 2.28

```

                                RS_P_10.RES
PIPE TRAVEL TIME(MIN.) =    0.15    Tc(MIN.) =    6.97
LONGEST FLOWPATH FROM NODE    105.00 TO NODE    111.00 =    367.00 FEET.

*****
FLOW PROCESS FROM NODE    111.00 TO NODE    111.00 IS CODE =    1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) =    6.97
RAINFALL INTENSITY(INCH/HR) =    2.43
TOTAL STREAM AREA(ACRES) =    1.00
PEAK FLOW RATE(CFS) AT CONFLUENCE =    2.28

*****
FLOW PROCESS FROM NODE    112.00 TO NODE    111.00 IS CODE =   21
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
=====
    ASSUMED INITIAL SUBAREA UNIFORM
    DEVELOPMENT IS COMMERCIAL
TC = K*[(LENGTH**3)/(ELEVATION CHANGE)]**.2
INITIAL SUBAREA FLOW-LENGTH(FEET) =    89.00
UPSTREAM ELEVATION(FEET) =    1156.08
DOWNSTREAM ELEVATION(FEET) =    1151.80
ELEVATION DIFFERENCE(FEET) =    4.28
TC = 0.303*[(    89.00**3)/(    4.28)]**.2 =    3.349
COMPUTED TIME OF CONCENTRATION INCREASED TO 5 MIN.
    10 YEAR RAINFALL INTENSITY(INCH/HOUR) =    2.787
COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8841
SOIL CLASSIFICATION IS "C"
SUBAREA RUNOFF(CFS) =    0.27
TOTAL AREA(ACRES) =    0.11    TOTAL RUNOFF(CFS) =    0.27

*****
FLOW PROCESS FROM NODE    111.00 TO NODE    111.00 IS CODE =    1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) =    5.00
RAINFALL INTENSITY(INCH/HR) =    2.79
TOTAL STREAM AREA(ACRES) =    0.11
PEAK FLOW RATE(CFS) AT CONFLUENCE =    0.27

** CONFLUENCE DATA **
STREAM      RUNOFF      Tc      INTENSITY      AREA
NUMBER      (CFS)      (MIN.)  (INCH/HOUR)  (ACRE)
    1         2.28        6.97        2.428        1.00
    2         0.27        5.00        2.787        0.11

*****WARNING*****
IN THIS COMPUTER PROGRAM, THE CONFLUENCE VALUE USED IS BASED
ON THE RCFC&WCD FORMULA OF PLATE D-1 AS DEFAULT VALUE. THIS FORMULA
WILL NOT NECESSARILY RESULT IN THE MAXIMUM VALUE OF PEAK FLOW.
*****

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

```

## \*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	1.91	5.00	2.787
2	2.52	6.97	2.428

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 2.52 Tc(MIN.) = 6.97

TOTAL AREA(ACRES) = 1.1

LONGEST FLOWPATH FROM NODE 105.00 TO NODE 111.00 = 367.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 111.00 TO NODE 113.00 IS CODE = 31

&gt;&gt;&gt;&gt;COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA&lt;&lt;&lt;&lt;

&gt;&gt;&gt;&gt;USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)&lt;&lt;&lt;&lt;

=====

ELEVATION DATA: UPSTREAM(FEET) = 1147.29 DOWNSTREAM(FEET) = 1146.91

FLOW LENGTH(FEET) = 75.00 MANNING'S N = 0.013

DEPTH OF FLOW IN 15.0 INCH PIPE IS 8.0 INCHES

PIPE-FLOW VELOCITY(FEET/SEC.) = 3.75

ESTIMATED PIPE DIAMETER(INCH) = 15.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 2.52

PIPE TRAVEL TIME(MIN.) = 0.33 Tc(MIN.) = 7.31

LONGEST FLOWPATH FROM NODE 105.00 TO NODE 113.00 = 442.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 113.00 TO NODE 113.00 IS CODE = 1

&gt;&gt;&gt;&gt;DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE&lt;&lt;&lt;&lt;

=====

TOTAL NUMBER OF STREAMS = 2

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:

TIME OF CONCENTRATION(MIN.) = 7.31

RAINFALL INTENSITY(INCH/HR) = 2.38

TOTAL STREAM AREA(ACRES) = 1.11

PEAK FLOW RATE(CFS) AT CONFLUENCE = 2.52

\*\*\*\*\*

FLOW PROCESS FROM NODE 114.00 TO NODE 115.00 IS CODE = 21

&gt;&gt;&gt;&gt;RATIONAL METHOD INITIAL SUBAREA ANALYSIS&lt;&lt;&lt;&lt;

=====

ASSUMED INITIAL SUBAREA UNIFORM

DEVELOPMENT IS COMMERCIAL

TC = K\*[(LENGTH\*\*3)/(ELEVATION CHANGE)]\*\*.2

INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00

UPSTREAM ELEVATION(FEET) = 1158.13

DOWNSTREAM ELEVATION(FEET) = 1155.26

ELEVATION DIFFERENCE(FEET) = 2.87

TC = 0.303\*[(100.00\*\*3)/(2.87)]\*\*.2 = 3.891

COMPUTED TIME OF CONCENTRATION INCREASED TO 5 MIN.

10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.787

COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8841

SOIL CLASSIFICATION IS "C"

SUBAREA RUNOFF(CFS) = 0.20

TOTAL AREA(ACRES) = 0.08 TOTAL RUNOFF(CFS) = 0.20

\*\*\*\*\*

FLOW PROCESS FROM NODE 115.00 TO NODE 116.00 IS CODE = 51

&gt;&gt;&gt;&gt;COMPUTE TRAPEZOIDAL CHANNEL FLOW&lt;&lt;&lt;&lt;

&gt;&gt;&gt;&gt;TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)&lt;&lt;&lt;&lt;

```

=====
ELEVATION DATA: UPSTREAM(FEET) = 1155.26 DOWNSTREAM(FEET) = 1152.66
CHANNEL LENGTH THRU SUBAREA(FEET) = 100.00 CHANNEL SLOPE = 0.0260
CHANNEL BASE(FEET) = 0.00 "Z" FACTOR = 99.000
MANNING'S FACTOR = 0.015 MAXIMUM DEPTH(FEET) = 1.00
10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.538
COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8828
SOIL CLASSIFICATION IS "C"
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.31
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 1.32
AVERAGE FLOW DEPTH(FEET) = 0.05 TRAVEL TIME(MIN.) = 1.26
Tc(MIN.) = 6.26
SUBAREA AREA(ACRES) = 0.10 SUBAREA RUNOFF(CFS) = 0.22
TOTAL AREA(ACRES) = 0.2 PEAK FLOW RATE(CFS) = 0.42

```

```

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH(FEET) = 0.06 FLOW VELOCITY(FEET/SEC.) = 1.34
LONGEST FLOWPATH FROM NODE 114.00 TO NODE 116.00 = 200.00 FEET.

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*****

```

```

FLOW PROCESS FROM NODE 116.00 TO NODE 116.00 IS CODE = 81

```

```

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<

```

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=====
10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.538
COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8828
SOIL CLASSIFICATION IS "C"
SUBAREA AREA(ACRES) = 0.10 SUBAREA RUNOFF(CFS) = 0.22
TOTAL AREA(ACRES) = 0.3 TOTAL RUNOFF(CFS) = 0.65
TC(MIN.) = 6.26

```

```

*****

```

```

FLOW PROCESS FROM NODE 116.00 TO NODE 113.00 IS CODE = 31

```

```

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

```

```

=====
ELEVATION DATA: UPSTREAM(FEET) = 1148.49 DOWNSTREAM(FEET) = 1147.41
FLOW LENGTH(FEET) = 35.00 MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 12.000
DEPTH OF FLOW IN 12.0 INCH PIPE IS 2.6 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 5.02
ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 0.65
PIPE TRAVEL TIME(MIN.) = 0.12 Tc(MIN.) = 6.38
LONGEST FLOWPATH FROM NODE 114.00 TO NODE 113.00 = 235.00 FEET.

```

```

*****

```

```

FLOW PROCESS FROM NODE 113.00 TO NODE 113.00 IS CODE = 1

```

```

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<

```

```

=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 6.38
RAINFALL INTENSITY(INCH/HR) = 2.52
TOTAL STREAM AREA(ACRES) = 0.28
PEAK FLOW RATE(CFS) AT CONFLUENCE = 0.65

```

```

** CONFLUENCE DATA **

```

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
------------------	-----------------	--------------	--------------------------	----------------

1	2.52	7.31	2.381	1.11
2	0.65	6.38	2.519	0.28

\*\*\*\*\*WARNING\*\*\*\*\*

IN THIS COMPUTER PROGRAM, THE CONFLUENCE VALUE USED IS BASED  
ON THE RCFC&WCD FORMULA OF PLATE D-1 AS DEFAULT VALUE. THIS FORMULA  
WILL NOT NECESSARILY RESULT IN THE MAXIMUM VALUE OF PEAK FLOW.

\*\*\*\*\*

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	T <sub>c</sub> (MIN.)	INTENSITY (INCH/HOUR)
1	2.84	6.38	2.519
2	3.13	7.31	2.381

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 3.13 T<sub>c</sub>(MIN.) = 7.31  
TOTAL AREA(ACRES) = 1.4  
LONGEST FLOWPATH FROM NODE 105.00 TO NODE 113.00 = 442.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 113.00 TO NODE 117.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1146.91 DOWNSTREAM(FEET) = 1146.78  
FLOW LENGTH(FEET) = 25.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 15.0 INCH PIPE IS 9.1 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 3.99  
ESTIMATED PIPE DIAMETER(INCH) = 15.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 3.13  
PIPE TRAVEL TIME(MIN.) = 0.10 T<sub>c</sub>(MIN.) = 7.41  
LONGEST FLOWPATH FROM NODE 105.00 TO NODE 117.00 = 467.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 117.00 TO NODE 117.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 3  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 7.41  
RAINFALL INTENSITY(INCH/HR) = 2.37  
TOTAL STREAM AREA(ACRES) = 1.39  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 3.13

\*\*\*\*\*

FLOW PROCESS FROM NODE 118.00 TO NODE 117.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

ASSUMED INITIAL SUBAREA UNIFORM  
DEVELOPMENT IS COMMERCIAL  
TC = K\*[(LENGTH\*\*3)/(ELEVATION CHANGE)]\*\*.2  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
UPSTREAM ELEVATION(FEET) = 1152.04  
DOWNSTREAM ELEVATION(FEET) = 1151.64  
ELEVATION DIFFERENCE(FEET) = 0.40  
TC = 0.303\*[(100.00\*\*3)/(0.40)]\*\*.2 = 5.770



```

                                RS_P_10.RES
10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.626
COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8833
SOIL CLASSIFICATION IS "C"
SUBAREA RUNOFF(CFS) = 0.79
TOTAL AREA(ACRES) = 0.34 TOTAL RUNOFF(CFS) = 0.79

*****
FLOW PROCESS FROM NODE 117.00 TO NODE 117.00 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
=====
TOTAL NUMBER OF STREAMS = 3
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 5.77
RAINFALL INTENSITY(INCH/HR) = 2.63
TOTAL STREAM AREA(ACRES) = 0.34
PEAK FLOW RATE(CFS) AT CONFLUENCE = 0.79

*****
FLOW PROCESS FROM NODE 119.00 TO NODE 120.00 IS CODE = 22
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
=====
ASSUMED INITIAL SUBAREA UNIFORM
DEVELOPMENT IS COMMERCIAL
USER SPECIFIED Tc(MIN.) = 5.000
10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.787
COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8841
SOIL CLASSIFICATION IS "C"
SUBAREA RUNOFF(CFS) = 0.17
TOTAL AREA(ACRES) = 0.07 TOTAL RUNOFF(CFS) = 0.17

*****
FLOW PROCESS FROM NODE 120.00 TO NODE 117.00 IS CODE = 31
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 1149.50 DOWNSTREAM(FEET) = 1147.78
FLOW LENGTH(FEET) = 66.00 MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 12.000
DEPTH OF FLOW IN 12.0 INCH PIPE IS 1.4 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 3.23
ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 0.17
PIPE TRAVEL TIME(MIN.) = 0.34 Tc(MIN.) = 5.34
LONGEST FLOWPATH FROM NODE 119.00 TO NODE 117.00 = 166.00 FEET.

*****
FLOW PROCESS FROM NODE 117.00 TO NODE 117.00 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<
=====
TOTAL NUMBER OF STREAMS = 3
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 3 ARE:
TIME OF CONCENTRATION(MIN.) = 5.34
RAINFALL INTENSITY(INCH/HR) = 2.71
TOTAL STREAM AREA(ACRES) = 0.07
PEAK FLOW RATE(CFS) AT CONFLUENCE = 0.17

```

\*\* CONFLUENCE DATA \*\*

STREAM	RUNOFF	Tc	INTENSITY	AREA
--------	--------	----	-----------	------

NUMBER	(CFS)	(MIN.)	(INCH/HOUR)	(ACRE)
1	3.13	7.41	2.367	1.39
2	0.79	5.77	2.626	0.34
3	0.17	5.34	2.711	0.07

\*\*\*\*\*WARNING\*\*\*\*\*

IN THIS COMPUTER PROGRAM, THE CONFLUENCE VALUE USED IS BASED  
ON THE RCFC&WCD FORMULA OF PLATE D-1 AS DEFAULT VALUE. THIS FORMULA  
WILL NOT NECESSARILY RESULT IN THE MAXIMUM VALUE OF PEAK FLOW.

\*\*\*\*\*

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 3 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	T <sub>c</sub> (MIN.)	INTENSITY (INCH/HOUR)
1	3.16	5.34	2.711
2	3.39	5.77	2.626
3	3.99	7.41	2.367

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 3.99 T<sub>c</sub>(MIN.) = 7.41  
TOTAL AREA(ACRES) = 1.8  
LONGEST FLOWPATH FROM NODE 105.00 TO NODE 117.00 = 467.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 117.00 TO NODE 121.00 IS CODE = 31

-----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(Feet) = 1146.78 DOWNSTREAM(Feet) = 1146.56  
FLOW LENGTH(Feet) = 44.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 15.0 INCH PIPE IS 11.1 INCHES  
PIPE-FLOW VELOCITY(Feet/Sec.) = 4.10  
ESTIMATED PIPE DIAMETER(INCH) = 15.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 3.99  
PIPE TRAVEL TIME(MIN.) = 0.18 T<sub>c</sub>(MIN.) = 7.59  
LONGEST FLOWPATH FROM NODE 105.00 TO NODE 121.00 = 511.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 121.00 TO NODE 121.00 IS CODE = 1

-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 7.59  
RAINFALL INTENSITY(INCH/HR) = 2.34  
TOTAL STREAM AREA(ACRES) = 1.80  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 3.99

\*\*\*\*\*

FLOW PROCESS FROM NODE 122.00 TO NODE 123.00 IS CODE = 22

-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

ASSUMED INITIAL SUBAREA UNIFORM  
DEVELOPMENT IS COMMERCIAL  
USER SPECIFIED T<sub>c</sub>(MIN.) = 5.000  
10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.787  
COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8841

SOIL CLASSIFICATION IS "C"

SUBAREA RUNOFF(CFS) = 0.17

TOTAL AREA(ACRES) = 0.07 TOTAL RUNOFF(CFS) = 0.17

\*\*\*\*\*

FLOW PROCESS FROM NODE 123.00 TO NODE 121.00 IS CODE = 31

&gt;&gt;&gt;&gt;COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA&lt;&lt;&lt;&lt;

&gt;&gt;&gt;&gt;USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)&lt;&lt;&lt;&lt;

=====

ELEVATION DATA: UPSTREAM(FEET) = 1149.50 DOWNSTREAM(FEET) = 1147.56

FLOW LENGTH(FEET) = 59.00 MANNING'S N = 0.013

ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 12.000

DEPTH OF FLOW IN 12.0 INCH PIPE IS 1.4 INCHES

PIPE-FLOW VELOCITY(FEET/SEC.) = 3.47

ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 0.17

PIPE TRAVEL TIME(MIN.) = 0.28 Tc(MIN.) = 5.28

LONGEST FLOWPATH FROM NODE 122.00 TO NODE 121.00 = 103.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 121.00 TO NODE 121.00 IS CODE = 1

&gt;&gt;&gt;&gt;DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE&lt;&lt;&lt;&lt;

&gt;&gt;&gt;&gt;AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES&lt;&lt;&lt;&lt;

=====

TOTAL NUMBER OF STREAMS = 2

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:

TIME OF CONCENTRATION(MIN.) = 5.28

RAINFALL INTENSITY(INCH/HR) = 2.72

TOTAL STREAM AREA(ACRES) = 0.07

PEAK FLOW RATE(CFS) AT CONFLUENCE = 0.17

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	3.99	7.59	2.344	1.80
2	0.17	5.28	2.724	0.07

\*\*\*\*\*WARNING\*\*\*\*\*

IN THIS COMPUTER PROGRAM, THE CONFLUENCE VALUE USED IS BASED  
ON THE RCFC&WCD FORMULA OF PLATE D-1 AS DEFAULT VALUE. THIS FORMULA  
WILL NOT NECESSARILY RESULT IN THE MAXIMUM VALUE OF PEAK FLOW.

\*\*\*\*\*

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	2.95	5.28	2.724
2	4.14	7.59	2.344

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 4.14 Tc(MIN.) = 7.59

TOTAL AREA(ACRES) = 1.9

LONGEST FLOWPATH FROM NODE 105.00 TO NODE 121.00 = 511.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 121.00 TO NODE 124.00 IS CODE = 31

&gt;&gt;&gt;&gt;COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA&lt;&lt;&lt;&lt;

&gt;&gt;&gt;&gt;USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)&lt;&lt;&lt;&lt;

```

=====
ELEVATION DATA: UPSTREAM(FEET) = 1146.56 DOWNSTREAM(FEET) = 1146.49
FLOW LENGTH(FEET) = 15.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 15.0 INCH PIPE IS 11.8 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 4.00
ESTIMATED PIPE DIAMETER(INCH) = 15.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 4.14
PIPE TRAVEL TIME(MIN.) = 0.06 Tc(MIN.) = 7.65
LONGEST FLOWPATH FROM NODE 105.00 TO NODE 124.00 = 526.00 FEET.

```

\*\*\*\*\*

```

FLOW PROCESS FROM NODE 124.00 TO NODE 124.00 IS CODE = 1
-----

```

&gt;&gt;&gt;&gt;DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE&lt;&lt;&lt;&lt;

```

=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 7.65
RAINFALL INTENSITY(INCH/HR) = 2.34
TOTAL STREAM AREA(ACRES) = 1.87
PEAK FLOW RATE(CFS) AT CONFLUENCE = 4.14

```

\*\*\*\*\*

```

FLOW PROCESS FROM NODE 125.00 TO NODE 124.00 IS CODE = 21
-----

```

&gt;&gt;&gt;&gt;RATIONAL METHOD INITIAL SUBAREA ANALYSIS&lt;&lt;&lt;&lt;

```

=====
ASSUMED INITIAL SUBAREA UNIFORM
DEVELOPMENT IS COMMERCIAL
TC = K*[(LENGTH**3)/(ELEVATION CHANGE)]**.2
INITIAL SUBAREA FLOW-LENGTH(FEET) = 76.00
UPSTREAM ELEVATION(FEET) = 1155.54
DOWNSTREAM ELEVATION(FEET) = 1151.58
ELEVATION DIFFERENCE(FEET) = 3.96
TC = 0.303*[( 76.00**3)/( 3.96)]**.2 = 3.094
COMPUTED TIME OF CONCENTRATION INCREASED TO 5 MIN.
10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.787
COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8841
SOIL CLASSIFICATION IS "C"
SUBAREA RUNOFF(CFS) = 0.30
TOTAL AREA(ACRES) = 0.12 TOTAL RUNOFF(CFS) = 0.30

```

\*\*\*\*\*

```

FLOW PROCESS FROM NODE 124.00 TO NODE 124.00 IS CODE = 1
-----

```

```

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<

```

```

=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 5.00
RAINFALL INTENSITY(INCH/HR) = 2.79
TOTAL STREAM AREA(ACRES) = 0.12
PEAK FLOW RATE(CFS) AT CONFLUENCE = 0.30

```

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	4.14	7.65	2.336	1.87
2	0.30	5.00	2.787	0.12

\*\*\*\*\*WARNING\*\*\*\*\*

IN THIS COMPUTER PROGRAM, THE CONFLUENCE VALUE USED IS BASED  
ON THE RCFC&WCD FORMULA OF PLATE D-1 AS DEFAULT VALUE. THIS FORMULA  
WILL NOT NECESSARILY RESULT IN THE MAXIMUM VALUE OF PEAK FLOW.

\*\*\*\*\*

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	3.00	5.00	2.787
2	4.38	7.65	2.336

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 4.38 Tc(MIN.) = 7.65  
TOTAL AREA(ACRES) = 2.0  
LONGEST FLOWPATH FROM NODE 105.00 TO NODE 124.00 = 526.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 124.00 TO NODE 126.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1146.00 DOWNSTREAM(FEET) = 1145.70  
FLOW LENGTH(FEET) = 60.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 15.0 INCH PIPE IS 12.1 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 4.14  
ESTIMATED PIPE DIAMETER(INCH) = 15.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 4.38  
PIPE TRAVEL TIME(MIN.) = 0.24 Tc(MIN.) = 7.89  
LONGEST FLOWPATH FROM NODE 105.00 TO NODE 126.00 = 586.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 126.00 TO NODE 126.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 7.89  
RAINFALL INTENSITY(INCH/HR) = 2.31  
TOTAL STREAM AREA(ACRES) = 1.99  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 4.38

\*\*\*\*\*

FLOW PROCESS FROM NODE 127.00 TO NODE 128.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

ASSUMED INITIAL SUBAREA UNIFORM  
DEVELOPMENT IS COMMERCIAL  
TC = K\*[(LENGTH\*\*3)/(ELEVATION CHANGE)]\*\*.2  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
UPSTREAM ELEVATION(FEET) = 1166.00  
DOWNSTREAM ELEVATION(FEET) = 1159.30  
ELEVATION DIFFERENCE(FEET) = 6.70  
TC = 0.303\*[(100.00\*\*3)/(6.70)]\*\*.2 = 3.284  
COMPUTED TIME OF CONCENTRATION INCREASED TO 5 MIN.  
10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.787  
COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8841  
SOIL CLASSIFICATION IS "C"

SUBAREA RUNOFF(CFS) = 0.15  
 TOTAL AREA(ACRES) = 0.06 TOTAL RUNOFF(CFS) = 0.15

\*\*\*\*\*

FLOW PROCESS FROM NODE 128.00 TO NODE 126.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<

>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1159.30 DOWNSTREAM(FEET) = 1151.31  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 118.00 CHANNEL SLOPE = 0.0677  
 CHANNEL BASE(FEET) = 0.00 "Z" FACTOR = 99.000  
 MANNING'S FACTOR = 0.015 MAXIMUM DEPTH(FEET) = 1.00  
 10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.548  
 COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8829  
 SOIL CLASSIFICATION IS "C"  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.27  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 1.63  
 AVERAGE FLOW DEPTH(FEET) = 0.04 TRAVEL TIME(MIN.) = 1.20  
 Tc(MIN.) = 6.20  
 SUBAREA AREA(ACRES) = 0.11 SUBAREA RUNOFF(CFS) = 0.25  
 TOTAL AREA(ACRES) = 0.2 PEAK FLOW RATE(CFS) = 0.40

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.04 FLOW VELOCITY(FEET/SEC.) = 2.17  
 LONGEST FLOWPATH FROM NODE 127.00 TO NODE 126.00 = 218.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 126.00 TO NODE 126.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<

=====

10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.548  
 COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8829  
 SOIL CLASSIFICATION IS "C"  
 SUBAREA AREA(ACRES) = 0.11 SUBAREA RUNOFF(CFS) = 0.25  
 TOTAL AREA(ACRES) = 0.3 TOTAL RUNOFF(CFS) = 0.64  
 TC(MIN.) = 6.20

\*\*\*\*\*

FLOW PROCESS FROM NODE 126.00 TO NODE 126.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 6.20  
 RAINFALL INTENSITY(INCH/HR) = 2.55  
 TOTAL STREAM AREA(ACRES) = 0.28  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 0.64

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	4.38	7.89	2.306	1.99
2	0.64	6.20	2.548	0.28

\*\*\*\*\*WARNING\*\*\*\*\*

IN THIS COMPUTER PROGRAM, THE CONFLUENCE VALUE USED IS BASED  
 ON THE RCFC&WCD FORMULA OF PLATE D-1 AS DEFAULT VALUE. THIS FORMULA  
 WILL NOT NECESSARILY RESULT IN THE MAXIMUM VALUE OF PEAK FLOW.

\*\*\*\*\*

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	4.09	6.20	2.548
2	4.96	7.89	2.306

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 4.96 Tc(MIN.) = 7.89

TOTAL AREA(ACRES) = 2.3

LONGEST FLOWPATH FROM NODE 105.00 TO NODE 126.00 = 586.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 126.00 TO NODE 129.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1145.70 DOWNSTREAM(FEET) = 1145.46

FLOW LENGTH(FEET) = 48.00 MANNING'S N = 0.013

DEPTH OF FLOW IN 18.0 INCH PIPE IS 10.9 INCHES

PIPE-FLOW VELOCITY(FEET/SEC.) = 4.41

ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 4.96

PIPE TRAVEL TIME(MIN.) = 0.18 Tc(MIN.) = 8.07

LONGEST FLOWPATH FROM NODE 105.00 TO NODE 129.00 = 634.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 129.00 TO NODE 129.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

TOTAL NUMBER OF STREAMS = 2

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:

TIME OF CONCENTRATION(MIN.) = 8.07

RAINFALL INTENSITY(INCH/HR) = 2.28

TOTAL STREAM AREA(ACRES) = 2.27

PEAK FLOW RATE(CFS) AT CONFLUENCE = 4.96

\*\*\*\*\*

FLOW PROCESS FROM NODE 130.00 TO NODE 131.00 IS CODE = 22

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

ASSUMED INITIAL SUBAREA UNIFORM

DEVELOPMENT IS COMMERCIAL

USER SPECIFIED Tc(MIN.) = 5.000

10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.787

COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8841

SOIL CLASSIFICATION IS "C"

SUBAREA RUNOFF(CFS) = 0.17

TOTAL AREA(ACRES) = 0.07 TOTAL RUNOFF(CFS) = 0.17

\*\*\*\*\*

FLOW PROCESS FROM NODE 131.00 TO NODE 129.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1149.50 DOWNSTREAM(FEET) = 1146.96

FLOW LENGTH(FEET) = 26.00 MANNING'S N = 0.013  
 ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 12.000  
 DEPTH OF FLOW IN 12.0 INCH PIPE IS 1.1 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 5.11  
 ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 0.17  
 PIPE TRAVEL TIME(MIN.) = 0.08 Tc(MIN.) = 5.08  
 LONGEST FLOWPATH FROM NODE 130.00 TO NODE 129.00 = 74.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 129.00 TO NODE 129.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====  
 TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 5.08  
 RAINFALL INTENSITY(INCH/HR) = 2.77  
 TOTAL STREAM AREA(ACRES) = 0.07  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 0.17

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	4.96	8.07	2.285	2.27
2	0.17	5.08	2.767	0.07

\*\*\*\*\*WARNING\*\*\*\*\*

IN THIS COMPUTER PROGRAM, THE CONFLUENCE VALUE USED IS BASED  
 ON THE RCFC&WCD FORMULA OF PLATE D-1 AS DEFAULT VALUE. THIS FORMULA  
 WILL NOT NECESSARILY RESULT IN THE MAXIMUM VALUE OF PEAK FLOW.

\*\*\*\*\*

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	3.30	5.08	2.767
2	5.11	8.07	2.285

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 5.11 Tc(MIN.) = 8.07  
 TOTAL AREA(ACRES) = 2.3  
 LONGEST FLOWPATH FROM NODE 105.00 TO NODE 129.00 = 634.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 129.00 TO NODE 132.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====  
 ELEVATION DATA: UPSTREAM(FEET) = 1145.46 DOWNSTREAM(FEET) = 1145.15  
 FLOW LENGTH(FEET) = 63.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 11.2 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 4.41  
 ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 5.11  
 PIPE TRAVEL TIME(MIN.) = 0.24 Tc(MIN.) = 8.31  
 LONGEST FLOWPATH FROM NODE 105.00 TO NODE 132.00 = 697.00 FEET.



\*\*\*\*\*

FLOW PROCESS FROM NODE 132.00 TO NODE 132.00 IS CODE = 1

&gt;&gt;&gt;&gt;DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE&lt;&lt;&lt;&lt;

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
 TIME OF CONCENTRATION(MIN.) = 8.31  
 RAINFALL INTENSITY(INCH/HR) = 2.26  
 TOTAL STREAM AREA(ACRES) = 2.34  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 5.11

\*\*\*\*\*

FLOW PROCESS FROM NODE 133.00 TO NODE 134.00 IS CODE = 21

&gt;&gt;&gt;&gt;RATIONAL METHOD INITIAL SUBAREA ANALYSIS&lt;&lt;&lt;&lt;

=====

ASSUMED INITIAL SUBAREA UNIFORM  
 DEVELOPMENT IS COMMERCIAL  
 $TC = K * [(LENGTH ** 3) / (ELEVATION \text{ CHANGE})] ** .2$   
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
 UPSTREAM ELEVATION(FEET) = 1166.00  
 DOWNSTREAM ELEVATION(FEET) = 1157.98  
 ELEVATION DIFFERENCE(FEET) = 8.02  
 $TC = 0.303 * [(100.00 ** 3) / (8.02)] ** .2 = 3.168$   
 COMPUTED TIME OF CONCENTRATION INCREASED TO 5 MIN.  
 10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.787  
 COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8841  
 SOIL CLASSIFICATION IS "C"  
 SUBAREA RUNOFF(CFS) = 0.17  
 TOTAL AREA(ACRES) = 0.07 TOTAL RUNOFF(CFS) = 0.17

\*\*\*\*\*

FLOW PROCESS FROM NODE 134.00 TO NODE 135.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<  
 >>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1157.98 DOWNSTREAM(FEET) = 1153.00  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 72.00 CHANNEL SLOPE = 0.0692  
 CHANNEL BASE(FEET) = 0.00 "Z" FACTOR = 99.000  
 MANNING'S FACTOR = 0.015 MAXIMUM DEPTH(FEET) = 1.00  
 10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.637  
 COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8833  
 SOIL CLASSIFICATION IS "C"  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.21  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FT/SEC.) = 1.68  
 AVERAGE FLOW DEPTH(FT) = 0.04 TRAVEL TIME(MIN.) = 0.71  
 $T_c(MIN.) = 5.71$   
 SUBAREA AREA(ACRES) = 0.03 SUBAREA RUNOFF(CFS) = 0.07  
 TOTAL AREA(ACRES) = 0.1 PEAK FLOW RATE(CFS) = 0.24

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
 DEPTH(FT) = 0.04 FLOW VELOCITY(FT/SEC.) = 1.97  
 LONGEST FLOWPATH FROM NODE 133.00 TO NODE 135.00 = 172.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 135.00 TO NODE 135.00 IS CODE = 81

&gt;&gt;&gt;&gt;ADDITION OF SUBAREA TO MAINLINE PEAK FLOW&lt;&lt;&lt;&lt;

=====

10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.637  
 COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8833

SOIL CLASSIFICATION IS "C"

SUBAREA AREA(ACRES) = 0.03 SUBAREA RUNOFF(CFS) = 0.07  
 TOTAL AREA(ACRES) = 0.1 TOTAL RUNOFF(CFS) = 0.31  
 TC(MIN.) = 5.71

\*\*\*\*\*

FLOW PROCESS FROM NODE 135.00 TO NODE 132.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1148.89 DOWNSTREAM(FEET) = 1146.15  
 FLOW LENGTH(FEET) = 55.00 MANNING'S N = 0.013  
 ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 12.000  
 DEPTH OF FLOW IN 12.0 INCH PIPE IS 1.7 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 4.78  
 ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 0.31  
 PIPE TRAVEL TIME(MIN.) = 0.19 Tc(MIN.) = 5.91  
 LONGEST FLOWPATH FROM NODE 133.00 TO NODE 132.00 = 227.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 132.00 TO NODE 132.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 5.91  
 RAINFALL INTENSITY(INCH/HR) = 2.60  
 TOTAL STREAM AREA(ACRES) = 0.13  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 0.31

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	5.11	8.31	2.257	2.34
2	0.31	5.91	2.601	0.13

\*\*\*\*\*WARNING\*\*\*\*\*

IN THIS COMPUTER PROGRAM, THE CONFLUENCE VALUE USED IS BASED  
 ON THE RCFC&WCD FORMULA OF PLATE D-1 AS DEFAULT VALUE. THIS FORMULA  
 WILL NOT NECESSARILY RESULT IN THE MAXIMUM VALUE OF PEAK FLOW.

\*\*\*\*\*

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	3.94	5.91	2.601
2	5.38	8.31	2.257

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 5.38 Tc(MIN.) = 8.31  
 TOTAL AREA(ACRES) = 2.5  
 LONGEST FLOWPATH FROM NODE 105.00 TO NODE 132.00 = 697.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 132.00 TO NODE 136.00 IS CODE = 31

-----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

```
=====
ELEVATION DATA: UPSTREAM(FEET) = 1145.15  DOWNSTREAM(FEET) = 1145.01
FLOW LENGTH(FEET) = 28.00  MANNING'S N = 0.013
DEPTH OF FLOW IN 18.0 INCH PIPE IS 11.6 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 4.49
ESTIMATED PIPE DIAMETER(INCH) = 18.00  NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 5.38
PIPE TRAVEL TIME(MIN.) = 0.10  Tc(MIN.) = 8.42
LONGEST FLOWPATH FROM NODE 105.00 TO NODE 136.00 = 725.00 FEET.
```

\*\*\*\*\*

FLOW PROCESS FROM NODE 136.00 TO NODE 136.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

```
=====
TOTAL NUMBER OF STREAMS = 3
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 8.42
RAINFALL INTENSITY(INCH/HR) = 2.25
TOTAL STREAM AREA(ACRES) = 2.47
PEAK FLOW RATE(CFS) AT CONFLUENCE = 5.38
```

\*\*\*\*\*

FLOW PROCESS FROM NODE 137.00 TO NODE 138.00 IS CODE = 22

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

```
=====
ASSUMED INITIAL SUBAREA UNIFORM
DEVELOPMENT IS COMMERCIAL
USER SPECIFIED Tc(MIN.) = 5.000
10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.787
COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8841
SOIL CLASSIFICATION IS "C"
SUBAREA RUNOFF(CFS) = 0.17
TOTAL AREA(ACRES) = 0.07  TOTAL RUNOFF(CFS) = 0.17
```

\*\*\*\*\*

FLOW PROCESS FROM NODE 138.00 TO NODE 136.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

```
=====
ELEVATION DATA: UPSTREAM(FEET) = 1149.50  DOWNSTREAM(FEET) = 1147.26
FLOW LENGTH(FEET) = 26.00  MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 12.000
DEPTH OF FLOW IN 12.0 INCH PIPE IS 1.1 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 4.90
ESTIMATED PIPE DIAMETER(INCH) = 12.00  NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 0.17
PIPE TRAVEL TIME(MIN.) = 0.09  Tc(MIN.) = 5.09
LONGEST FLOWPATH FROM NODE 137.00 TO NODE 136.00 = 54.00 FEET.
```

\*\*\*\*\*

FLOW PROCESS FROM NODE 136.00 TO NODE 136.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

```
=====
TOTAL NUMBER OF STREAMS = 3
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 5.09
RAINFALL INTENSITY(INCH/HR) = 2.77
```

TOTAL STREAM AREA(ACRES) = 0.07  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 0.17

\*\*\*\*\*

FLOW PROCESS FROM NODE 139.00 TO NODE 140.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

=====

ASSUMED INITIAL SUBAREA UNIFORM  
 DEVELOPMENT IS COMMERCIAL  
 TC =  $K * [(LENGTH ** 3) / (ELEVATION\ CHANGE)] ** .2$   
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
 UPSTREAM ELEVATION(FEET) = 1159.54  
 DOWNSTREAM ELEVATION(FEET) = 1151.67  
 ELEVATION DIFFERENCE(FEET) = 7.87  
 TC =  $0.303 * [(100.00 ** 3) / (7.87)] ** .2 = 3.180$   
 COMPUTED TIME OF CONCENTRATION INCREASED TO 5 MIN.  
 10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.787  
 COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8841  
 SOIL CLASSIFICATION IS "C"  
 SUBAREA RUNOFF(CFS) = 0.27  
 TOTAL AREA(ACRES) = 0.11 TOTAL RUNOFF(CFS) = 0.27

\*\*\*\*\*

FLOW PROCESS FROM NODE 140.00 TO NODE 136.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<  
 >>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1151.67 DOWNSTREAM(FEET) = 1150.93  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 91.00 CHANNEL SLOPE = 0.0081  
 CHANNEL BASE(FEET) = 0.00 "Z" FACTOR = 99.000  
 MANNING'S FACTOR = 0.015 MAXIMUM DEPTH(FEET) = 1.00  
 10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.471  
 COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8824  
 SOIL CLASSIFICATION IS "C"  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.46  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 0.90  
 AVERAGE FLOW DEPTH(FEET) = 0.07 TRAVEL TIME(MIN.) = 1.68  
 Tc(MIN.) = 6.68  
 SUBAREA AREA(ACRES) = 0.17 SUBAREA RUNOFF(CFS) = 0.37  
 TOTAL AREA(ACRES) = 0.3 PEAK FLOW RATE(CFS) = 0.64

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.08 FLOW VELOCITY(FEET/SEC.) = 1.03  
 LONGEST FLOWPATH FROM NODE 139.00 TO NODE 136.00 = 191.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 136.00 TO NODE 136.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<

=====

10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.471  
 COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8824  
 SOIL CLASSIFICATION IS "C"  
 SUBAREA AREA(ACRES) = 0.17 SUBAREA RUNOFF(CFS) = 0.37  
 TOTAL AREA(ACRES) = 0.4 TOTAL RUNOFF(CFS) = 1.01  
 TC(MIN.) = 6.68

\*\*\*\*\*

FLOW PROCESS FROM NODE 136.00 TO NODE 136.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

&gt;&gt;&gt;&gt;&gt;AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES&lt;&lt;&lt;&lt;&lt;

```
=====
TOTAL NUMBER OF STREAMS = 3
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 3 ARE:
TIME OF CONCENTRATION(MIN.) = 6.68
RAINFALL INTENSITY(INCH/HR) = 2.47
TOTAL STREAM AREA(ACRES) = 0.45
PEAK FLOW RATE(CFS) AT CONFLUENCE = 1.01
```

## \*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	5.38	8.42	2.246	2.47
2	0.17	5.09	2.766	0.07
3	1.01	6.68	2.471	0.45

## \*\*\*\*\*WARNING\*\*\*\*\*

IN THIS COMPUTER PROGRAM, THE CONFLUENCE VALUE USED IS BASED  
ON THE RCFC&WCD FORMULA OF PLATE D-1 AS DEFAULT VALUE. THIS FORMULA  
WILL NOT NECESSARILY RESULT IN THE MAXIMUM VALUE OF PEAK FLOW.

## \*\*\*\*\*

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 3 STREAMS.

## \*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	4.20	5.09	2.766
2	5.43	6.68	2.471
3	6.44	8.42	2.246

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 6.44 Tc(MIN.) = 8.42  
TOTAL AREA(ACRES) = 3.0  
LONGEST FLOWPATH FROM NODE 105.00 TO NODE 136.00 = 725.00 FEET.

## \*\*\*\*\*

FLOW PROCESS FROM NODE 136.00 TO NODE 141.00 IS CODE = 31

&gt;&gt;&gt;&gt;&gt;COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA&lt;&lt;&lt;&lt;&lt;

&gt;&gt;&gt;&gt;&gt;USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)&lt;&lt;&lt;&lt;&lt;

```
=====
ELEVATION DATA: UPSTREAM(Feet) = 1145.01 DOWNSTREAM(Feet) = 1144.82
FLOW LENGTH(Feet) = 40.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 18.0 INCH PIPE IS 13.5 INCHES
PIPE-FLOW VELOCITY(Feet/Sec.) = 4.53
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 6.44
PIPE TRAVEL TIME(MIN.) = 0.15 Tc(MIN.) = 8.56
LONGEST FLOWPATH FROM NODE 105.00 TO NODE 141.00 = 765.00 FEET.
```

## \*\*\*\*\*

FLOW PROCESS FROM NODE 141.00 TO NODE 141.00 IS CODE = 1

&gt;&gt;&gt;&gt;&gt;DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE&lt;&lt;&lt;&lt;&lt;

```
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 8.56
RAINFALL INTENSITY(INCH/HR) = 2.23
TOTAL STREAM AREA(ACRES) = 2.99
PEAK FLOW RATE(CFS) AT CONFLUENCE = 6.44
```

\*\*\*\*\*

FLOW PROCESS FROM NODE 142.00 TO NODE 143.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

=====

ASSUMED INITIAL SUBAREA UNIFORM

DEVELOPMENT IS COMMERCIAL

$TC = K * [(LENGTH ** 3) / (ELEVATION CHANGE)] ** .2$

INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00

UPSTREAM ELEVATION(FEET) = 1166.00

DOWNSTREAM ELEVATION(FEET) = 1158.52

ELEVATION DIFFERENCE(FEET) = 7.48

$TC = 0.303 * [(100.00 ** 3) / (7.48)] ** .2 = 3.212$

COMPUTED TIME OF CONCENTRATION INCREASED TO 5 MIN.

10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.787

COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8841

SOIL CLASSIFICATION IS "C"

SUBAREA RUNOFF(CFS) = 0.20

TOTAL AREA(ACRES) = 0.08 TOTAL RUNOFF(CFS) = 0.20

\*\*\*\*\*

FLOW PROCESS FROM NODE 143.00 TO NODE 144.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<

>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1158.52 DOWNSTREAM(FEET) = 1152.35

CHANNEL LENGTH THRU SUBAREA(FEET) = 122.00 CHANNEL SLOPE = 0.0506

CHANNEL BASE(FEET) = 0.00 "Z" FACTOR = 99.000

MANNING'S FACTOR = 0.015 MAXIMUM DEPTH(FEET) = 1.00

10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.526

COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8827

SOIL CLASSIFICATION IS "C"

TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.25

TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 1.52

AVERAGE FLOW DEPTH(FEET) = 0.04 TRAVEL TIME(MIN.) = 1.34

Tc(MIN.) = 6.34

SUBAREA AREA(ACRES) = 0.05 SUBAREA RUNOFF(CFS) = 0.11

TOTAL AREA(ACRES) = 0.1 PEAK FLOW RATE(CFS) = 0.31

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.04 FLOW VELOCITY(FEET/SEC.) = 1.69

LONGEST FLOWPATH FROM NODE 142.00 TO NODE 144.00 = 222.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 144.00 TO NODE 144.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<

=====

10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.526

COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8827

SOIL CLASSIFICATION IS "C"

SUBAREA AREA(ACRES) = 0.05 SUBAREA RUNOFF(CFS) = 0.11

TOTAL AREA(ACRES) = 0.2 TOTAL RUNOFF(CFS) = 0.42

TC(MIN.) = 6.34

\*\*\*\*\*

FLOW PROCESS FROM NODE 144.00 TO NODE 141.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1148.28 DOWNSTREAM(FEET) = 1145.82  
 FLOW LENGTH(FEET) = 56.00 MANNING'S N = 0.013  
 ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 12.000  
 DEPTH OF FLOW IN 12.0 INCH PIPE IS 2.0 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 5.04  
 ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 0.42  
 PIPE TRAVEL TIME(MIN.) = 0.19 Tc(MIN.) = 6.52  
 LONGEST FLOWPATH FROM NODE 142.00 TO NODE 141.00 = 278.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 141.00 TO NODE 141.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 6.52  
 RAINFALL INTENSITY(INCH/HR) = 2.50  
 TOTAL STREAM AREA(ACRES) = 0.18  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 0.42

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	6.44	8.56	2.229	2.99
2	0.42	6.52	2.496	0.18

\*\*\*\*\*WARNING\*\*\*\*\*

IN THIS COMPUTER PROGRAM, THE CONFLUENCE VALUE USED IS BASED  
 ON THE RCFC&WCD FORMULA OF PLATE D-1 AS DEFAULT VALUE. THIS FORMULA  
 WILL NOT NECESSARILY RESULT IN THE MAXIMUM VALUE OF PEAK FLOW.

\*\*\*\*\*

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	5.32	6.52	2.496
2	6.81	8.56	2.229

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 6.81 Tc(MIN.) = 8.56  
 TOTAL AREA(ACRES) = 3.2  
 LONGEST FLOWPATH FROM NODE 105.00 TO NODE 141.00 = 765.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 141.00 TO NODE 145.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1144.82 DOWNSTREAM(FEET) = 1144.62  
 FLOW LENGTH(FEET) = 39.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 13.7 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 4.71  
 ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 6.81  
 PIPE TRAVEL TIME(MIN.) = 0.14 Tc(MIN.) = 8.70  
 LONGEST FLOWPATH FROM NODE 105.00 TO NODE 145.00 = 804.00 FEET.

```

*****
FLOW PROCESS FROM NODE    145.00 TO NODE    145.00 IS CODE =    1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
=====
TOTAL NUMBER OF STREAMS = 3
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) =    8.70
RAINFALL INTENSITY(INCH/HR) =    2.21
TOTAL STREAM AREA(ACRES) =    3.17
PEAK FLOW RATE(CFS) AT CONFLUENCE =    6.81

*****
FLOW PROCESS FROM NODE    146.00 TO NODE    147.00 IS CODE =   21
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
=====
    ASSUMED INITIAL SUBAREA UNIFORM
    DEVELOPMENT IS COMMERCIAL
TC = K*[(LENGTH**3)/(ELEVATION CHANGE)]**.2
INITIAL SUBAREA FLOW-LENGTH(FEET) =   100.00
UPSTREAM ELEVATION(FEET) =   1164.72
DOWNSTREAM ELEVATION(FEET) =   1157.49
ELEVATION DIFFERENCE(FEET) =     7.23
TC = 0.303*[( 100.00**3)/(    7.23)]**.2 =    3.234
COMPUTED TIME OF CONCENTRATION INCREASED TO 5 MIN.
    10 YEAR RAINFALL INTENSITY(INCH/HOUR) =    2.787
COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8841
SOIL CLASSIFICATION IS "C"
SUBAREA RUNOFF(CFS) =     0.12
TOTAL AREA(ACRES) =     0.05    TOTAL RUNOFF(CFS) =     0.12

*****
FLOW PROCESS FROM NODE    147.00 TO NODE    148.00 IS CODE =   51
-----
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) =   1157.49 DOWNSTREAM(FEET) =   1152.14
CHANNEL LENGTH THRU SUBAREA(FEET) =   160.00 CHANNEL SLOPE =   0.0334
CHANNEL BASE(FEET) =    0.00 "Z" FACTOR =  99.000
MANNING'S FACTOR = 0.015 MAXIMUM DEPTH(FEET) =    1.00
    10 YEAR RAINFALL INTENSITY(INCH/HOUR) =    2.422
COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8822
SOIL CLASSIFICATION IS "C"
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) =     0.24
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) =    1.33
AVERAGE FLOW DEPTH(FEET) =    0.04 TRAVEL TIME(MIN.) =    2.01
Tc(MIN.) =    7.01
SUBAREA AREA(ACRES) =     0.11    SUBAREA RUNOFF(CFS) =     0.24
TOTAL AREA(ACRES) =     0.2    PEAK FLOW RATE(CFS) =     0.36

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH(FEET) =    0.05 FLOW VELOCITY(FEET/SEC.) =    1.53
LONGEST FLOWPATH FROM NODE    146.00 TO NODE    148.00 =    260.00 FEET.

*****
FLOW PROCESS FROM NODE    148.00 TO NODE    148.00 IS CODE =   81
-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====
    10 YEAR RAINFALL INTENSITY(INCH/HOUR) =    2.422

```



COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8822  
 SOIL CLASSIFICATION IS "C"  
 SUBAREA AREA(ACRES) = 0.11 SUBAREA RUNOFF(CFS) = 0.24  
 TOTAL AREA(ACRES) = 0.3 TOTAL RUNOFF(CFS) = 0.59  
 TC(MIN.) = 7.01

\*\*\*\*\*

FLOW PROCESS FROM NODE 148.00 TO NODE 145.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1148.10 DOWNSTREAM(FEET) = 1145.62  
 FLOW LENGTH(FEET) = 41.00 MANNING'S N = 0.013  
 ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 12.000  
 DEPTH OF FLOW IN 12.0 INCH PIPE IS 2.1 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 6.27  
 ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 0.59  
 PIPE TRAVEL TIME(MIN.) = 0.11 Tc(MIN.) = 7.12  
 LONGEST FLOWPATH FROM NODE 146.00 TO NODE 145.00 = 301.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 145.00 TO NODE 145.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

=====

TOTAL NUMBER OF STREAMS = 3  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 7.12  
 RAINFALL INTENSITY(INCH/HR) = 2.41  
 TOTAL STREAM AREA(ACRES) = 0.27  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 0.59

\*\*\*\*\*

FLOW PROCESS FROM NODE 149.00 TO NODE 145.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

=====

ASSUMED INITIAL SUBAREA UNIFORM  
 DEVELOPMENT IS COMMERCIAL  
 $TC = K * [(LENGTH ** 3) / (ELEVATION CHANGE)] ** .2$   
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 94.00  
 UPSTREAM ELEVATION(FEET) = 1154.92  
 DOWNSTREAM ELEVATION(FEET) = 1151.86  
 ELEVATION DIFFERENCE(FEET) = 3.06  
 $TC = 0.303 * [(94.00 ** 3) / (3.06)] ** .2 = 3.701$   
 COMPUTED TIME OF CONCENTRATION INCREASED TO 5 MIN.  
 10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.787  
 COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8841  
 SOIL CLASSIFICATION IS "C"  
 SUBAREA RUNOFF(CFS) = 0.27  
 TOTAL AREA(ACRES) = 0.11 TOTAL RUNOFF(CFS) = 0.27

\*\*\*\*\*

FLOW PROCESS FROM NODE 145.00 TO NODE 145.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<

=====

TOTAL NUMBER OF STREAMS = 3  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 3 ARE:  
 TIME OF CONCENTRATION(MIN.) = 5.00

RAINFALL INTENSITY(INCH/HR) = 2.79  
 TOTAL STREAM AREA(ACRES) = 0.11  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 0.27

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	6.81	8.70	2.215	3.17
2	0.59	7.12	2.407	0.27
3	0.27	5.00	2.787	0.11

\*\*\*\*\*WARNING\*\*\*\*\*  
 IN THIS COMPUTER PROGRAM, THE CONFLUENCE VALUE USED IS BASED  
 ON THE RCFC&WCD FORMULA OF PLATE D-1 AS DEFAULT VALUE. THIS FORMULA  
 WILL NOT NECESSARILY RESULT IN THE MAXIMUM VALUE OF PEAK FLOW.  
 \*\*\*\*\*

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 3 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	4.60	5.00	2.787
2	6.40	7.12	2.407
3	7.57	8.70	2.215

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 7.57 Tc(MIN.) = 8.70  
 TOTAL AREA(ACRES) = 3.6  
 LONGEST FLOWPATH FROM NODE 105.00 TO NODE 145.00 = 804.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 145.00 TO NODE 150.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1144.62 DOWNSTREAM(FEET) = 1141.82  
 FLOW LENGTH(FEET) = 136.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 15.0 INCH PIPE IS 10.5 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 8.25  
 ESTIMATED PIPE DIAMETER(INCH) = 15.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 7.57  
 PIPE TRAVEL TIME(MIN.) = 0.27 Tc(MIN.) = 8.98  
 LONGEST FLOWPATH FROM NODE 105.00 TO NODE 150.00 = 940.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 150.00 TO NODE 150.00 IS CODE = 10

>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<

\*\*\*\*\*

FLOW PROCESS FROM NODE 151.00 TO NODE 152.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

=====

ASSUMED INITIAL SUBAREA UNIFORM  
 DEVELOPMENT IS COMMERCIAL  
 TC = K\*[(LENGTH\*\*3)/(ELEVATION CHANGE)]\*\*.2  
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
 UPSTREAM ELEVATION(FEET) = 1152.00

DOWNSTREAM ELEVATION(FEET) = 1150.13  
 ELEVATION DIFFERENCE(FEET) = 1.87  
 $TC = 0.303 * [(100.00 ** 3) / (1.87)] ** .2 = 4.239$   
 COMPUTED TIME OF CONCENTRATION INCREASED TO 5 MIN.  
 10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.787  
 COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8841  
 SOIL CLASSIFICATION IS "C"  
 SUBAREA RUNOFF(CFS) = 0.30  
 TOTAL AREA(ACRES) = 0.12 TOTAL RUNOFF(CFS) = 0.30

\*\*\*\*\*

FLOW PROCESS FROM NODE 152.00 TO NODE 152.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====  
 TOTAL NUMBER OF STREAMS = 3  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
 TIME OF CONCENTRATION(MIN.) = 5.00  
 RAINFALL INTENSITY(INCH/HR) = 2.79  
 TOTAL STREAM AREA(ACRES) = 0.12  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 0.30

\*\*\*\*\*

FLOW PROCESS FROM NODE 153.00 TO NODE 154.00 IS CODE = 22

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====  
 ASSUMED INITIAL SUBAREA UNIFORM  
 DEVELOPMENT IS COMMERCIAL  
 USER SPECIFIED Tc(MIN.) = 5.000  
 10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.787  
 COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8841  
 SOIL CLASSIFICATION IS "C"  
 SUBAREA RUNOFF(CFS) = 0.17  
 TOTAL AREA(ACRES) = 0.07 TOTAL RUNOFF(CFS) = 0.17

\*\*\*\*\*

FLOW PROCESS FROM NODE 154.00 TO NODE 152.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====  
 ELEVATION DATA: UPSTREAM(FEET) = 1149.50 DOWNSTREAM(FEET) = 1146.64  
 FLOW LENGTH(FEET) = 93.00 MANNING'S N = 0.013  
 ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 12.000  
 DEPTH OF FLOW IN 12.0 INCH PIPE IS 1.4 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 3.47  
 ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 0.17  
 PIPE TRAVEL TIME(MIN.) = 0.45 Tc(MIN.) = 5.45  
 LONGEST FLOWPATH FROM NODE 153.00 TO NODE 152.00 = 193.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 152.00 TO NODE 152.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====  
 TOTAL NUMBER OF STREAMS = 3  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 5.45  
 RAINFALL INTENSITY(INCH/HR) = 2.69  
 TOTAL STREAM AREA(ACRES) = 0.07  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 0.17

\*\*\*\*\*

FLOW PROCESS FROM NODE 155.00 TO NODE 156.00 IS CODE = 22

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

=====

ASSUMED INITIAL SUBAREA UNIFORM  
DEVELOPMENT IS COMMERCIAL  
USER SPECIFIED Tc(MIN.) = 5.000  
10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.787  
COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8841  
SOIL CLASSIFICATION IS "C"  
SUBAREA RUNOFF(CFS) = 0.17  
TOTAL AREA(ACRES) = 0.07 TOTAL RUNOFF(CFS) = 0.17

\*\*\*\*\*

FLOW PROCESS FROM NODE 156.00 TO NODE 152.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1149.50 DOWNSTREAM(FEET) = 1146.64  
FLOW LENGTH(FEET) = 70.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 12.000  
DEPTH OF FLOW IN 12.0 INCH PIPE IS 1.3 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 3.73  
ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 0.17  
PIPE TRAVEL TIME(MIN.) = 0.31 Tc(MIN.) = 5.31  
LONGEST FLOWPATH FROM NODE 155.00 TO NODE 152.00 = 163.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 152.00 TO NODE 152.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<

=====

TOTAL NUMBER OF STREAMS = 3  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 3 ARE:  
TIME OF CONCENTRATION(MIN.) = 5.31  
RAINFALL INTENSITY(INCH/HR) = 2.72  
TOTAL STREAM AREA(ACRES) = 0.07  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 0.17

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	0.30	5.00	2.787	0.12
2	0.17	5.45	2.689	0.07
3	0.17	5.31	2.717	0.07

\*\*\*\*\*WARNING\*\*\*\*\*

IN THIS COMPUTER PROGRAM, THE CONFLUENCE VALUE USED IS BASED  
ON THE RCFC&WCD FORMULA OF PLATE D-1 AS DEFAULT VALUE. THIS FORMULA  
WILL NOT NECESSARILY RESULT IN THE MAXIMUM VALUE OF PEAK FLOW.

\*\*\*\*\*

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 3 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
------------------	-----------------	--------------	--------------------------

1	0.62	5.00	2.787
2	0.63	5.31	2.717
3	0.63	5.45	2.689

## COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 0.62 Tc(MIN.) = 5.00

TOTAL AREA(ACRES) = 0.3

LONGEST FLOWPATH FROM NODE 153.00 TO NODE 152.00 = 193.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 152.00 TO NODE 150.00 IS CODE = 31

&gt;&gt;&gt;&gt;COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA&lt;&lt;&lt;&lt;&lt;

&gt;&gt;&gt;&gt;USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)&lt;&lt;&lt;&lt;&lt;

=====

ELEVATION DATA: UPSTREAM(FEET) = 1146.14 DOWNSTREAM(FEET) = 1142.83

FLOW LENGTH(FEET) = 58.00 MANNING'S N = 0.013

ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 12.000

DEPTH OF FLOW IN 12.0 INCH PIPE IS 2.2 INCHES

PIPE-FLOW VELOCITY(FEET/SEC.) = 6.17

ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 0.62

PIPE TRAVEL TIME(MIN.) = 0.16 Tc(MIN.) = 5.16

LONGEST FLOWPATH FROM NODE 153.00 TO NODE 150.00 = 251.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 150.00 TO NODE 150.00 IS CODE = 14.0

&gt;&gt;&gt;&gt;MEMORY BANK # 1 COPIED ONTO MAIN-STREAM MEMORY&lt;&lt;&lt;&lt;&lt;

=====

## MAIN-STREAM MEMORY DEFINED AS FOLLOWS:

STREAM RUNOFF Tc

NUMBER (CFS) (MIN.)

1 7.57 8.98

TOTAL AREA = 3.6

\*\*\*\*\*

FLOW PROCESS FROM NODE 150.00 TO NODE 150.00 IS CODE = 1

&gt;&gt;&gt;&gt;DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE&lt;&lt;&lt;&lt;&lt;

=====

TOTAL NUMBER OF STREAMS = 2

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:

TIME OF CONCENTRATION(MIN.) = 8.98

RAINFALL INTENSITY(INCH/HR) = 2.19

TOTAL STREAM AREA(ACRES) = 3.55

PEAK FLOW RATE(CFS) AT CONFLUENCE = 7.57

\*\*\*\*\*

FLOW PROCESS FROM NODE 157.00 TO NODE 158.00 IS CODE = 21

&gt;&gt;&gt;&gt;RATIONAL METHOD INITIAL SUBAREA ANALYSIS&lt;&lt;&lt;&lt;&lt;

=====

ASSUMED INITIAL SUBAREA UNIFORM

DEVELOPMENT IS COMMERCIAL

TC = K\*[(LENGTH\*\*3)/(ELEVATION CHANGE)]\*\*.2

INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00

UPSTREAM ELEVATION(FEET) = 1151.83

DOWNSTREAM ELEVATION(FEET) = 1150.21

ELEVATION DIFFERENCE(FEET) = 1.62

TC = 0.303\*[(100.00\*\*3)/(1.62)]\*\*.2 = 4.362

COMPUTED TIME OF CONCENTRATION INCREASED TO 5 MIN.

```

                                RS_P_10.RES
    10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.787
    COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8841
    SOIL CLASSIFICATION IS "C"
    SUBAREA RUNOFF(CFS) = 0.25
    TOTAL AREA(ACRES) = 0.10 TOTAL RUNOFF(CFS) = 0.25

*****
FLOW PROCESS FROM NODE 158.00 TO NODE 159.00 IS CODE = 51
-----
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 1150.21 DOWNSTREAM(FEET) = 1149.90
CHANNEL LENGTH THRU SUBAREA(FEET) = 23.00 CHANNEL SLOPE = 0.0135
CHANNEL BASE(FEET) = 0.00 "Z" FACTOR = 99.000
MANNING'S FACTOR = 0.015 MAXIMUM DEPTH(FEET) = 1.00
    10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.708
    COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8837
    SOIL CLASSIFICATION IS "C"
    TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.27
    TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 1.07
    AVERAGE FLOW DEPTH(FEET) = 0.05 TRAVEL TIME(MIN.) = 0.36
    Tc(MIN.) = 5.36
    SUBAREA AREA(ACRES) = 0.02 SUBAREA RUNOFF(CFS) = 0.05
    TOTAL AREA(ACRES) = 0.1 PEAK FLOW RATE(CFS) = 0.29

    END OF SUBAREA CHANNEL FLOW HYDRAULICS:
    DEPTH(FEET) = 0.06 FLOW VELOCITY(FEET/SEC.) = 0.94
    LONGEST FLOWPATH FROM NODE 157.00 TO NODE 159.00 = 123.00 FEET.

*****
FLOW PROCESS FROM NODE 159.00 TO NODE 159.00 IS CODE = 81
-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====
    10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.708
    COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8837
    SOIL CLASSIFICATION IS "C"
    SUBAREA AREA(ACRES) = 0.02 SUBAREA RUNOFF(CFS) = 0.05
    TOTAL AREA(ACRES) = 0.1 TOTAL RUNOFF(CFS) = 0.34
    TC(MIN.) = 5.36

*****
FLOW PROCESS FROM NODE 159.00 TO NODE 150.00 IS CODE = 31
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 1141.90 DOWNSTREAM(FEET) = 1141.82
FLOW LENGTH(FEET) = 20.00 MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 12.000
DEPTH OF FLOW IN 12.0 INCH PIPE IS 3.2 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 2.02
ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 0.34
PIPE TRAVEL TIME(MIN.) = 0.16 Tc(MIN.) = 5.52
LONGEST FLOWPATH FROM NODE 157.00 TO NODE 150.00 = 143.00 FEET.

*****
FLOW PROCESS FROM NODE 150.00 TO NODE 150.00 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<

```

```

=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 5.52
RAINFALL INTENSITY(INCH/HR) = 2.67
TOTAL STREAM AREA(ACRES) = 0.14
PEAK FLOW RATE(CFS) AT CONFLUENCE = 0.34

```

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	7.57	8.98	2.186	3.55
2	0.34	5.52	2.674	0.14

\*\*\*\*\*WARNING\*\*\*\*\*

IN THIS COMPUTER PROGRAM, THE CONFLUENCE VALUE USED IS BASED  
ON THE RCFC&WCD FORMULA OF PLATE D-1 AS DEFAULT VALUE. THIS FORMULA  
WILL NOT NECESSARILY RESULT IN THE MAXIMUM VALUE OF PEAK FLOW.

\*\*\*\*\*

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	5.00	5.52	2.674
2	7.85	8.98	2.186

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 7.85 Tc(MIN.) = 8.98  
TOTAL AREA(ACRES) = 3.7  
LONGEST FLOWPATH FROM NODE 105.00 TO NODE 150.00 = 940.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 150.00 TO NODE 160.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

```

=====
ELEVATION DATA: UPSTREAM(FEET) = 1141.82 DOWNSTREAM(FEET) = 1141.64
FLOW LENGTH(FEET) = 35.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 21.0 INCH PIPE IS 13.1 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 4.99
ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 7.85
PIPE TRAVEL TIME(MIN.) = 0.12 Tc(MIN.) = 9.09
LONGEST FLOWPATH FROM NODE 105.00 TO NODE 160.00 = 975.00 FEET.

```

\*\*\*\*\*

FLOW PROCESS FROM NODE 160.00 TO NODE 160.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

```

=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 9.09
RAINFALL INTENSITY(INCH/HR) = 2.17
TOTAL STREAM AREA(ACRES) = 3.69
PEAK FLOW RATE(CFS) AT CONFLUENCE = 7.85

```

\*\*\*\*\*

FLOW PROCESS FROM NODE 161.00 TO NODE 162.00 IS CODE = 21

-----  
 >>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<  
 =====

ASSUMED INITIAL SUBAREA UNIFORM  
 DEVELOPMENT IS COMMERCIAL

TC =  $K * [(LENGTH ** 3) / (ELEVATION CHANGE)] ** .2$   
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
 UPSTREAM ELEVATION(FEET) = 1153.39  
 DOWNSTREAM ELEVATION(FEET) = 1150.16  
 ELEVATION DIFFERENCE(FEET) = 3.23  
 TC =  $0.303 * [(100.00 ** 3) / (3.23)] ** .2 = 3.800$   
 COMPUTED TIME OF CONCENTRATION INCREASED TO 5 MIN.  
 10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.787  
 COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8841  
 SOIL CLASSIFICATION IS "C"  
 SUBAREA RUNOFF(CFS) = 0.34  
 TOTAL AREA(ACRES) = 0.14 TOTAL RUNOFF(CFS) = 0.34

\*\*\*\*\*

FLOW PROCESS FROM NODE 162.00 TO NODE 163.00 IS CODE = 51  
 -----

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<  
 >>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<  
 =====

ELEVATION DATA: UPSTREAM(FEET) = 1150.16 DOWNSTREAM(FEET) = 1149.22  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 72.00 CHANNEL SLOPE = 0.0131  
 CHANNEL BASE(FEET) = 0.00 "Z" FACTOR = 99.000  
 MANNING'S FACTOR = 0.015 MAXIMUM DEPTH(FEET) = 1.00  
 10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.573  
 COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8830  
 SOIL CLASSIFICATION IS "C"  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.57  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 1.13  
 AVERAGE FLOW DEPTH(FEET) = 0.07 TRAVEL TIME(MIN.) = 1.06  
 Tc(MIN.) = 6.06  
 SUBAREA AREA(ACRES) = 0.20 SUBAREA RUNOFF(CFS) = 0.45  
 TOTAL AREA(ACRES) = 0.3 PEAK FLOW RATE(CFS) = 0.80

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.08 FLOW VELOCITY(FEET/SEC.) = 1.29  
 LONGEST FLOWPATH FROM NODE 161.00 TO NODE 163.00 = 172.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 163.00 TO NODE 163.00 IS CODE = 81  
 -----

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<  
 =====

10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.573  
 COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8830  
 SOIL CLASSIFICATION IS "C"  
 SUBAREA AREA(ACRES) = 0.20 SUBAREA RUNOFF(CFS) = 0.45  
 TOTAL AREA(ACRES) = 0.5 TOTAL RUNOFF(CFS) = 1.25  
 TC(MIN.) = 6.06

\*\*\*\*\*

FLOW PROCESS FROM NODE 163.00 TO NODE 160.00 IS CODE = 31  
 -----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<  
 =====

ELEVATION DATA: UPSTREAM(FEET) = 1145.18 DOWNSTREAM(FEET) = 1141.94  
 FLOW LENGTH(FEET) = 17.00 MANNING'S N = 0.013  
 ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 12.000



DEPTH OF FLOW IN 12.0 INCH PIPE IS 2.3 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 11.67  
 ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 1.25  
 PIPE TRAVEL TIME(MIN.) = 0.02 Tc(MIN.) = 6.09  
 LONGEST FLOWPATH FROM NODE 161.00 TO NODE 160.00 = 189.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 160.00 TO NODE 160.00 IS CODE = 1

-----  
 >>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 6.09  
 RAINFALL INTENSITY(INCH/HR) = 2.57  
 TOTAL STREAM AREA(ACRES) = 0.54  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 1.25

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	7.85	9.09	2.175	3.69
2	1.25	6.09	2.569	0.54

\*\*\*\*\*WARNING\*\*\*\*\*

IN THIS COMPUTER PROGRAM, THE CONFLUENCE VALUE USED IS BASED  
 ON THE RCFC&WCD FORMULA OF PLATE D-1 AS DEFAULT VALUE. THIS FORMULA  
 WILL NOT NECESSARILY RESULT IN THE MAXIMUM VALUE OF PEAK FLOW.

\*\*\*\*\*

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	6.51	6.09	2.569
2	8.92	9.09	2.175

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 8.92 Tc(MIN.) = 9.09  
 TOTAL AREA(ACRES) = 4.2  
 LONGEST FLOWPATH FROM NODE 105.00 TO NODE 160.00 = 975.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 160.00 TO NODE 164.00 IS CODE = 31

-----  
 >>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1141.78 DOWNSTREAM(FEET) = 1140.76  
 FLOW LENGTH(FEET) = 78.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 11.8 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 7.29  
 ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 8.92  
 PIPE TRAVEL TIME(MIN.) = 0.18 Tc(MIN.) = 9.27  
 LONGEST FLOWPATH FROM NODE 105.00 TO NODE 164.00 = 1053.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 164.00 TO NODE 164.00 IS CODE = 1

-----  
 >>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 =====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
 TIME OF CONCENTRATION(MIN.) = 9.27  
 RAINFALL INTENSITY(INCH/HR) = 2.16  
 TOTAL STREAM AREA(ACRES) = 4.23  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 8.92

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 165.00 TO NODE 166.00 IS CODE = 21  
 -----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
 =====

ASSUMED INITIAL SUBAREA UNIFORM  
 DEVELOPMENT IS COMMERCIAL  
 $TC = K * [(LENGTH ** 3) / (ELEVATION \text{ CHANGE})] ** .2$   
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 70.00  
 UPSTREAM ELEVATION(FEET) = 1151.81  
 DOWNSTREAM ELEVATION(FEET) = 1148.41  
 ELEVATION DIFFERENCE(FEET) = 3.40  
 $TC = 0.303 * [(70.00 ** 3) / (3.40)] ** .2 = 3.036$   
 COMPUTED TIME OF CONCENTRATION INCREASED TO 5 MIN.  
 10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.787  
 COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8841  
 SOIL CLASSIFICATION IS "C"  
 SUBAREA RUNOFF(CFS) = 0.17  
 TOTAL AREA(ACRES) = 0.07 TOTAL RUNOFF(CFS) = 0.17

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 166.00 TO NODE 164.00 IS CODE = 31  
 -----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<  
 =====

ELEVATION DATA: UPSTREAM(FEET) = 1144.84 DOWNSTREAM(FEET) = 1142.76  
 FLOW LENGTH(FEET) = 31.00 MANNING'S N = 0.013  
 ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 12.000  
 DEPTH OF FLOW IN 12.0 INCH PIPE IS 1.1 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 4.52  
 ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 0.17  
 PIPE TRAVEL TIME(MIN.) = 0.11  $T_c$ (MIN.) = 5.11  
 LONGEST FLOWPATH FROM NODE 165.00 TO NODE 164.00 = 101.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 164.00 TO NODE 164.00 IS CODE = 1  
 -----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<  
 =====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 5.11  
 RAINFALL INTENSITY(INCH/HR) = 2.76  
 TOTAL STREAM AREA(ACRES) = 0.07  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 0.17

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	$T_c$ (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	8.92	9.27	2.157	4.23

2      0.17      5.11      2.761

0.07

\*\*\*\*\*WARNING\*\*\*\*\*

IN THIS COMPUTER PROGRAM, THE CONFLUENCE VALUE USED IS BASED  
ON THE RCFC&WCD FORMULA OF PLATE D-1 AS DEFAULT VALUE. THIS FORMULA  
WILL NOT NECESSARILY RESULT IN THE MAXIMUM VALUE OF PEAK FLOW.

\*\*\*\*\*

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	5.09	5.11	2.761
2	9.05	9.27	2.157

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 9.05 Tc(MIN.) = 9.27

TOTAL AREA(ACRES) = 4.3

LONGEST FLOWPATH FROM NODE 105.00 TO NODE 164.00 = 1053.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 164.00 TO NODE 165.00 IS CODE = 31

&gt;&gt;&gt;&gt;COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA&lt;&lt;&lt;&lt;

&gt;&gt;&gt;&gt;USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)&lt;&lt;&lt;&lt;

ELEVATION DATA: UPSTREAM(FEET) = 1140.76 DOWNSTREAM(FEET) = 1140.53

FLOW LENGTH(FEET) = 47.00 MANNING'S N = 0.013

DEPTH OF FLOW IN 21.0 INCH PIPE IS 14.7 INCHES

PIPE-FLOW VELOCITY(FEET/SEC.) = 5.03

ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 9.05

PIPE TRAVEL TIME(MIN.) = 0.16 Tc(MIN.) = 9.43

LONGEST FLOWPATH FROM NODE 105.00 TO NODE 165.00 = 1100.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 165.00 TO NODE 165.00 IS CODE = 1

&gt;&gt;&gt;&gt;DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE&lt;&lt;&lt;&lt;

TOTAL NUMBER OF STREAMS = 3

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:

TIME OF CONCENTRATION(MIN.) = 9.43

RAINFALL INTENSITY(INCH/HR) = 2.14

TOTAL STREAM AREA(ACRES) = 4.30

PEAK FLOW RATE(CFS) AT CONFLUENCE = 9.05

\*\*\*\*\*

FLOW PROCESS FROM NODE 166.00 TO NODE 167.00 IS CODE = 21

&gt;&gt;&gt;&gt;RATIONAL METHOD INITIAL SUBAREA ANALYSIS&lt;&lt;&lt;&lt;

ASSUMED INITIAL SUBAREA UNIFORM

DEVELOPMENT IS COMMERCIAL

TC = K\*[(LENGTH\*\*3)/(ELEVATION CHANGE)]\*\*.2

INITIAL SUBAREA FLOW-LENGTH(FEET) = 61.00

UPSTREAM ELEVATION(FEET) = 1151.81

DOWNSTREAM ELEVATION(FEET) = 1150.67

ELEVATION DIFFERENCE(FEET) = 1.14

TC = 0.303\*[( 61.00\*\*3)/( 1.14)]\*\*.2 = 3.479

COMPUTED TIME OF CONCENTRATION INCREASED TO 5 MIN.

```

                                RS_P_10.RES
10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.787
COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8841
SOIL CLASSIFICATION IS "C"
SUBAREA RUNOFF(CFS) = 0.12
TOTAL AREA(ACRES) = 0.05 TOTAL RUNOFF(CFS) = 0.12

*****
FLOW PROCESS FROM NODE 167.00 TO NODE 165.00 IS CODE = 31
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 1146.56 DOWNSTREAM(FEET) = 1145.98
FLOW LENGTH(FEET) = 8.00 MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 12.000
DEPTH OF FLOW IN 12.0 INCH PIPE IS 1.0 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 4.15
ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 0.12
PIPE TRAVEL TIME(MIN.) = 0.03 Tc(MIN.) = 5.03
LONGEST FLOWPATH FROM NODE 166.00 TO NODE 165.00 = 69.00 FEET.

*****
FLOW PROCESS FROM NODE 165.00 TO NODE 165.00 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
=====
TOTAL NUMBER OF STREAMS = 3
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 5.03
RAINFALL INTENSITY(INCH/HR) = 2.78
TOTAL STREAM AREA(ACRES) = 0.05
PEAK FLOW RATE(CFS) AT CONFLUENCE = 0.12

*****
FLOW PROCESS FROM NODE 168.00 TO NODE 169.00 IS CODE = 21
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
=====
ASSUMED INITIAL SUBAREA UNIFORM
DEVELOPMENT IS COMMERCIAL
TC = K*[(LENGTH**3)/(ELEVATION CHANGE)]**.2
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00
UPSTREAM ELEVATION(FEET) = 1151.99
DOWNSTREAM ELEVATION(FEET) = 1149.95
ELEVATION DIFFERENCE(FEET) = 2.04
TC = 0.303*[(100.00**3)/(2.04)]**.2 = 4.165
COMPUTED TIME OF CONCENTRATION INCREASED TO 5 MIN.
10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.787
COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8841
SOIL CLASSIFICATION IS "C"
SUBAREA RUNOFF(CFS) = 0.20
TOTAL AREA(ACRES) = 0.08 TOTAL RUNOFF(CFS) = 0.20

*****
FLOW PROCESS FROM NODE 169.00 TO NODE 170.00 IS CODE = 51
-----
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 1149.95 DOWNSTREAM(FEET) = 1149.76
CHANNEL LENGTH THRU SUBAREA(FEET) = 25.00 CHANNEL SLOPE = 0.0076
CHANNEL BASE(FEET) = 0.00 "Z" FACTOR = 99.000

```

RS\_P\_10.RES

MANNING'S FACTOR = 0.015    MAXIMUM DEPTH(Feet) = 1.00  
 10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.675  
 COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8835  
 SOIL CLASSIFICATION IS "C"  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.20  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(Feet/Sec.) = 0.81  
 AVERAGE FLOW DEPTH(Feet) = 0.05    TRAVEL TIME(Min.) = 0.52  
 Tc(Min.) = 5.52  
 SUBAREA AREA(ACRES) = 0.01    SUBAREA RUNOFF(CFS) = 0.01  
 TOTAL AREA(ACRES) = 0.1    PEAK FLOW RATE(CFS) = 0.21

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
 DEPTH(Feet) = 0.05    FLOW VELOCITY(Feet/Sec.) = 0.83  
 LONGEST FLOWPATH FROM NODE 168.00 TO NODE 170.00 = 125.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 170.00 TO NODE 170.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<

10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.675  
 COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8835  
 SOIL CLASSIFICATION IS "C"  
 SUBAREA AREA(ACRES) = 0.01    SUBAREA RUNOFF(CFS) = 0.01  
 TOTAL AREA(ACRES) = 0.1    TOTAL RUNOFF(CFS) = 0.22  
 TC(Min.) = 5.52

\*\*\*\*\*

FLOW PROCESS FROM NODE 170.00 TO NODE 165.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

ELEVATION DATA: UPSTREAM(Feet) = 1144.85    DOWNSTREAM(Feet) = 1143.00  
 FLOW LENGTH(Feet) = 83.00    MANNING'S N = 0.013  
 ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 12.000  
 DEPTH OF FLOW IN 12.0 INCH PIPE IS 1.7 INCHES  
 PIPE-FLOW VELOCITY(Feet/Sec.) = 3.31  
 ESTIMATED PIPE DIAMETER(INCH) = 12.00    NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 0.22  
 PIPE TRAVEL TIME(Min.) = 0.42    Tc(Min.) = 5.93  
 LONGEST FLOWPATH FROM NODE 168.00 TO NODE 165.00 = 208.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 165.00 TO NODE 165.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<

TOTAL NUMBER OF STREAMS = 3  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 3 ARE:  
 TIME OF CONCENTRATION(Min.) = 5.93  
 RAINFALL INTENSITY(INCH/HR) = 2.60  
 TOTAL STREAM AREA(ACRES) = 0.09  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 0.22

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (Min.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	9.05	9.43	2.142	4.30
2	0.12	5.03	2.779	0.05
3	0.22	5.93	2.595	0.09

\*\*\*\*\*WARNING\*\*\*\*\*

IN THIS COMPUTER PROGRAM, THE CONFLUENCE VALUE USED IS BASED  
ON THE RCFC&WCD FORMULA OF PLATE D-1 AS DEFAULT VALUE. THIS FORMULA  
WILL NOT NECESSARILY RESULT IN THE MAXIMUM VALUE OF PEAK FLOW.

\*\*\*\*\*

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 3 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	5.14	5.03	2.779
2	6.04	5.93	2.595
3	9.33	9.43	2.142

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 9.33 Tc(MIN.) = 9.43  
TOTAL AREA(ACRES) = 4.4  
LONGEST FLOWPATH FROM NODE 105.00 TO NODE 165.00 = 1100.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 165.00 TO NODE 171.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1140.52 DOWNSTREAM(FEET) = 1140.09  
FLOW LENGTH(FEET) = 87.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 21.0 INCH PIPE IS 15.0 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 5.08  
ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 9.33  
PIPE TRAVEL TIME(MIN.) = 0.29 Tc(MIN.) = 9.71  
LONGEST FLOWPATH FROM NODE 105.00 TO NODE 171.00 = 1187.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 171.00 TO NODE 171.00 IS CODE = 10

>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 2 <<<<

\*\*\*\*\*

FLOW PROCESS FROM NODE 172.00 TO NODE 173.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

=====

ASSUMED INITIAL SUBAREA UNIFORM  
DEVELOPMENT IS COMMERCIAL  
TC =  $K * [(LENGTH ** 3) / (ELEVATION CHANGE)] ** .2$   
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
UPSTREAM ELEVATION(FEET) = 1150.81  
DOWNSTREAM ELEVATION(FEET) = 1147.88  
ELEVATION DIFFERENCE(FEET) = 2.93  
TC =  $0.303 * [(100.00 ** 3) / (2.93)] ** .2 = 3.874$   
COMPUTED TIME OF CONCENTRATION INCREASED TO 5 MIN.  
10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.787  
COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8841  
SOIL CLASSIFICATION IS "C"  
SUBAREA RUNOFF(CFS) = 0.64  
TOTAL AREA(ACRES) = 0.26 TOTAL RUNOFF(CFS) = 0.64

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                                RS_P_10.RES
FLOW PROCESS FROM NODE    173.00 TO NODE    174.00 IS CODE =   51
-----
>>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
>>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) =   1147.88  DOWNSTREAM(FEET) =   1147.00
CHANNEL LENGTH THRU SUBAREA(FEET) =    35.00  CHANNEL SLOPE =   0.0251
CHANNEL BASE(FEET) =     0.00  "Z" FACTOR =  99.000
MANNING'S FACTOR = 0.015  MAXIMUM DEPTH(FEET) =    1.00
  10 YEAR RAINFALL INTENSITY(INCH/HOUR) =   2.705
COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8837
SOIL CLASSIFICATION IS "C"
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) =      0.68
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) =   1.58
AVERAGE FLOW DEPTH(FEET) =    0.07  TRAVEL TIME(MIN.) =   0.37
Tc(MIN.) =    5.37
SUBAREA AREA(ACRES) =      0.03      SUBAREA RUNOFF(CFS) =    0.07
TOTAL AREA(ACRES) =      0.3      PEAK FLOW RATE(CFS) =      0.71

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH(FEET) = 0.07  FLOW VELOCITY(FEET/SEC.) =   1.66
LONGEST FLOWPATH FROM NODE    172.00 TO NODE    174.00 =    135.00 FEET.

*****
FLOW PROCESS FROM NODE    174.00 TO NODE    174.00 IS CODE =   81
-----
>>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
=====
  10 YEAR RAINFALL INTENSITY(INCH/HOUR) =   2.705
COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8837
SOIL CLASSIFICATION IS "C"
SUBAREA AREA(ACRES) =      0.03  SUBAREA RUNOFF(CFS) =    0.07
TOTAL AREA(ACRES) =      0.3  TOTAL RUNOFF(CFS) =    0.78
TC(MIN.) =    5.37

*****
FLOW PROCESS FROM NODE    174.00 TO NODE    171.00 IS CODE =   31
-----
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) =   1143.47  DOWNSTREAM(FEET) =   1143.30
FLOW LENGTH(FEET) =     5.00  MANNING'S N =   0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 12.000
DEPTH OF FLOW IN 12.0 INCH PIPE IS   2.8 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) =   5.53
ESTIMATED PIPE DIAMETER(INCH) =  12.00  NUMBER OF PIPES =    1
PIPE-FLOW(CFS) =      0.78
PIPE TRAVEL TIME(MIN.) =   0.02  Tc(MIN.) =    5.38
LONGEST FLOWPATH FROM NODE    172.00 TO NODE    171.00 =    140.00 FEET.

*****
FLOW PROCESS FROM NODE    171.00 TO NODE    171.00 IS CODE =   10
-----
>>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 3 <<<<<
=====

*****
FLOW PROCESS FROM NODE    175.00 TO NODE    176.00 IS CODE =   21
-----
>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
=====
ASSUMED INITIAL SUBAREA UNIFORM

```

DEVELOPMENT IS COMMERCIAL

TC =  $K * [(LENGTH ** 3) / (ELEVATION\ CHANGE)] ** .2$ 

INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00

UPSTREAM ELEVATION(FEET) = 1151.24

DOWNSTREAM ELEVATION(FEET) = 1147.95

ELEVATION DIFFERENCE(FEET) = 3.29

TC =  $0.303 * [(100.00 ** 3) / (3.29)] ** .2 = 3.786$ 

COMPUTED TIME OF CONCENTRATION INCREASED TO 5 MIN.

10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.787

COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8841

SOIL CLASSIFICATION IS "C"

SUBAREA RUNOFF(CFS) = 0.30

TOTAL AREA(ACRES) = 0.12 TOTAL RUNOFF(CFS) = 0.30

\*\*\*\*\*

FLOW PROCESS FROM NODE 176.00 TO NODE 177.00 IS CODE = 51

&gt;&gt;&gt;&gt;COMPUTE TRAPEZOIDAL CHANNEL FLOW&lt;&lt;&lt;&lt;&lt;

&gt;&gt;&gt;&gt;TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)&lt;&lt;&lt;&lt;&lt;

ELEVATION DATA: UPSTREAM(FEET) = 1147.95 DOWNSTREAM(FEET) = 1147.00

CHANNEL LENGTH THRU SUBAREA(FEET) = 158.00 CHANNEL SLOPE = 0.0060

CHANNEL BASE(FEET) = 0.00 "Z" FACTOR = 99.000

MANNING'S FACTOR = 0.015 MAXIMUM DEPTH(FEET) = 1.00

10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.269

COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8812

SOIL CLASSIFICATION IS "C"

TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.42

TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 0.82

AVERAGE FLOW DEPTH(FEET) = 0.07 TRAVEL TIME(MIN.) = 3.21

Tc(MIN.) = 8.21

SUBAREA AREA(ACRES) = 0.12 SUBAREA RUNOFF(CFS) = 0.24

TOTAL AREA(ACRES) = 0.2 PEAK FLOW RATE(CFS) = 0.54

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.08 FLOW VELOCITY(FEET/SEC.) = 0.86

LONGEST FLOWPATH FROM NODE 175.00 TO NODE 177.00 = 258.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 177.00 TO NODE 177.00 IS CODE = 81

&gt;&gt;&gt;&gt;ADDITION OF SUBAREA TO MAINLINE PEAK FLOW&lt;&lt;&lt;&lt;&lt;

10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.269

COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8812

SOIL CLASSIFICATION IS "C"

SUBAREA AREA(ACRES) = 0.12 SUBAREA RUNOFF(CFS) = 0.24

TOTAL AREA(ACRES) = 0.4 TOTAL RUNOFF(CFS) = 0.78

TC(MIN.) = 8.21

\*\*\*\*\*

FLOW PROCESS FROM NODE 177.00 TO NODE 178.00 IS CODE = 31

&gt;&gt;&gt;&gt;COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA&lt;&lt;&lt;&lt;&lt;

&gt;&gt;&gt;&gt;USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)&lt;&lt;&lt;&lt;&lt;

ELEVATION DATA: UPSTREAM(FEET) = 1141.94 DOWNSTREAM(FEET) = 1141.01

FLOW LENGTH(FEET) = 105.00 MANNING'S N = 0.013

ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 12.000

DEPTH OF FLOW IN 12.0 INCH PIPE IS 4.0 INCHES

PIPE-FLOW VELOCITY(FEET/SEC.) = 3.39

ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 0.78



```

                                RS_P_10.RES
PIPE TRAVEL TIME(MIN.) =    0.52    Tc(MIN.) =    8.72
LONGEST FLOWPATH FROM NODE    175.00 TO NODE    178.00 =    363.00 FEET.

*****
FLOW PROCESS FROM NODE    178.00 TO NODE    178.00 IS CODE =    1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
=====
TOTAL NUMBER OF STREAMS =    2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM    1 ARE:
TIME OF CONCENTRATION(MIN.) =    8.72
RAINFALL INTENSITY(INCH/HR) =    2.21
TOTAL STREAM AREA(ACRES) =    0.36
PEAK FLOW RATE(CFS) AT CONFLUENCE =    0.78

*****
FLOW PROCESS FROM NODE    179.00 TO NODE    180.00 IS CODE =    21
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
=====
    ASSUMED INITIAL SUBAREA UNIFORM
    DEVELOPMENT IS COMMERCIAL
TC = K*[(LENGTH**3)/(ELEVATION CHANGE)]**.2
INITIAL SUBAREA FLOW-LENGTH(FEET) =    100.00
UPSTREAM ELEVATION(FEET) =    1148.13
DOWNSTREAM ELEVATION(FEET) =    1146.40
ELEVATION DIFFERENCE(FEET) =    1.73
TC = 0.303*[(    100.00**3)/(    1.73)]**.2 =    4.305
COMPUTED TIME OF CONCENTRATION INCREASED TO 5 MIN.
    10 YEAR RAINFALL INTENSITY(INCH/HOUR) =    2.787
COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8841
SOIL CLASSIFICATION IS "C"
SUBAREA RUNOFF(CFS) =    0.26
TOTAL AREA(ACRES) =    0.11    TOTAL RUNOFF(CFS) =    0.26

*****
FLOW PROCESS FROM NODE    180.00 TO NODE    181.00 IS CODE =    51
-----
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) =    1146.40    DOWNSTREAM(FEET) =    1145.61
CHANNEL LENGTH THRU SUBAREA(FEET) =    62.00    CHANNEL SLOPE =    0.0127
CHANNEL BASE(FEET) =    0.00    "Z" FACTOR =    99.000
MANNING'S FACTOR = 0.015    MAXIMUM DEPTH(FEET) =    1.00
    10 YEAR RAINFALL INTENSITY(INCH/HOUR) =    2.603
COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8832
SOIL CLASSIFICATION IS "C"
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) =    0.39
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) =    1.16
AVERAGE FLOW DEPTH(FEET) =    0.06    TRAVEL TIME(MIN.) =    0.89
Tc(MIN.) =    5.89
SUBAREA AREA(ACRES) =    0.11    SUBAREA RUNOFF(CFS) =    0.25
TOTAL AREA(ACRES) =    0.2    PEAK FLOW RATE(CFS) =    0.51

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH(FEET) =    0.07    FLOW VELOCITY(FEET/SEC.) =    1.20
LONGEST FLOWPATH FROM NODE    179.00 TO NODE    181.00 =    162.00 FEET.

*****
FLOW PROCESS FROM NODE    181.00 TO NODE    181.00 IS CODE =    81
-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<

```

```
=====
10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.603
COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8832
SOIL CLASSIFICATION IS "C"
SUBAREA AREA(ACRES) = 0.11 SUBAREA RUNOFF(CFS) = 0.25
TOTAL AREA(ACRES) = 0.3 TOTAL RUNOFF(CFS) = 0.77
TC(MIN.) = 5.89
```

```
*****
FLOW PROCESS FROM NODE 181.00 TO NODE 178.00 IS CODE = 31
-----
```

```
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
```

```
=====
ELEVATION DATA: UPSTREAM(FEET) = 1142.60 DOWNSTREAM(FEET) = 1142.01
FLOW LENGTH(FEET) = 39.00 MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 12.000
DEPTH OF FLOW IN 12.0 INCH PIPE IS 3.5 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 4.10
ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 0.77
PIPE TRAVEL TIME(MIN.) = 0.16 Tc(MIN.) = 6.05
LONGEST FLOWPATH FROM NODE 179.00 TO NODE 178.00 = 201.00 FEET.
```

```
*****
FLOW PROCESS FROM NODE 178.00 TO NODE 178.00 IS CODE = 1
-----
```

```
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<
```

```
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 6.05
RAINFALL INTENSITY(INCH/HR) = 2.57
TOTAL STREAM AREA(ACRES) = 0.33
PEAK FLOW RATE(CFS) AT CONFLUENCE = 0.77
```

**\*\* CONFLUENCE DATA \*\***

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	0.78	8.72	2.212	0.36
2	0.77	6.05	2.575	0.33

\*\*\*\*\*WARNING\*\*\*\*\*

IN THIS COMPUTER PROGRAM, THE CONFLUENCE VALUE USED IS BASED  
ON THE RCFC&WCD FORMULA OF PLATE D-1 AS DEFAULT VALUE. THIS FORMULA  
WILL NOT NECESSARILY RESULT IN THE MAXIMUM VALUE OF PEAK FLOW.

\*\*\*\*\*

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

**\*\* PEAK FLOW RATE TABLE \*\***

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	1.30	6.05	2.575
2	1.43	8.72	2.212

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

```
PEAK FLOW RATE(CFS) = 1.43 Tc(MIN.) = 8.72
TOTAL AREA(ACRES) = 0.7
LONGEST FLOWPATH FROM NODE 175.00 TO NODE 178.00 = 363.00 FEET.
```

\*\*\*\*\*

FLOW PROCESS FROM NODE 178.00 TO NODE 171.00 IS CODE = 31

&gt;&gt;&gt;&gt;COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA&lt;&lt;&lt;&lt;

&gt;&gt;&gt;&gt;USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)&lt;&lt;&lt;&lt;

ELEVATION DATA: UPSTREAM(FEET) = 1141.01 DOWNSTREAM(FEET) = 1140.96

FLOW LENGTH(FEET) = 110.00 MANNING'S N = 0.013

DEPTH OF FLOW IN 18.0 INCH PIPE IS 10.7 INCHES

PIPE-FLOW VELOCITY(FEET/SEC.) = 1.32

ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 1.43

PIPE TRAVEL TIME(MIN.) = 1.39 Tc(MIN.) = 10.12

LONGEST FLOWPATH FROM NODE 175.00 TO NODE 171.00 = 473.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 171.00 TO NODE 171.00 IS CODE = 14.0

&gt;&gt;&gt;&gt;MEMORY BANK # 2 COPIED ONTO MAIN-STREAM MEMORY&lt;&lt;&lt;&lt;

MAIN-STREAM MEMORY DEFINED AS FOLLOWS:

STREAM RUNOFF Tc

NUMBER (CFS) (MIN.)

1 9.33 9.71

TOTAL AREA = 4.4

\*\*\*\*\*

FLOW PROCESS FROM NODE 171.00 TO NODE 171.00 IS CODE = 11

&gt;&gt;&gt;&gt;CONFLUENCE MEMORY BANK # 3 WITH THE MAIN-STREAM MEMORY&lt;&lt;&lt;&lt;

\*\* MAIN STREAM CONFLUENCE DATA \*\*

STREAM RUNOFF Tc INTENSITY AREA

NUMBER (CFS) (MIN.) (INCH/HOUR) (ACRE)

1 9.33 9.71 2.116 4.44

LONGEST FLOWPATH FROM NODE 105.00 TO NODE 171.00 = 1187.00 FEET.

\*\* MEMORY BANK # 3 CONFLUENCE DATA \*\*

STREAM RUNOFF Tc INTENSITY AREA

NUMBER (CFS) (MIN.) (INCH/HOUR) (ACRE)

1 0.78 5.38 2.702 0.32

LONGEST FLOWPATH FROM NODE 172.00 TO NODE 171.00 = 140.00 FEET.

\*\*\*\*\*WARNING\*\*\*\*\*

IN THIS COMPUTER PROGRAM, THE CONFLUENCE VALUE USED IS BASED  
ON THE RCFC&WCD FORMULA OF PLATE D-1 AS DEFAULT VALUE. THIS FORMULA  
WILL NOT NECESSARILY RESULT IN THE MAXIMUM VALUE OF PEAK FLOW.

\*\*\*\*\*

\*\* PEAK FLOW RATE TABLE \*\*

STREAM RUNOFF Tc INTENSITY

NUMBER (CFS) (MIN.) (INCH/HOUR)

1 5.96 5.38 2.702

2 9.94 9.71 2.116

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 9.94 Tc(MIN.) = 9.71

TOTAL AREA(ACRES) = 4.8

\*\*\*\*\*

FLOW PROCESS FROM NODE 171.00 TO NODE 182.00 IS CODE = 31

```

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

```

```

=====
ELEVATION DATA: UPSTREAM(FEET) = 1140.09 DOWNSTREAM(FEET) = 1139.23
FLOW LENGTH(FEET) = 48.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 18.0 INCH PIPE IS 11.4 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 8.45
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 9.94
PIPE TRAVEL TIME(MIN.) = 0.09 Tc(MIN.) = 9.81
LONGEST FLOWPATH FROM NODE 105.00 TO NODE 182.00 = 1235.00 FEET.

```

```

*****

```

```

FLOW PROCESS FROM NODE 200.00 TO NODE 201.00 IS CODE = 21

```

```

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

```

```

=====
ASSUMED INITIAL SUBAREA UNIFORM
DEVELOPMENT IS COMMERCIAL
TC = K*[(LENGTH**3)/(ELEVATION CHANGE)]**.2
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00
UPSTREAM ELEVATION(FEET) = 1153.06
DOWNSTREAM ELEVATION(FEET) = 1149.59
ELEVATION DIFFERENCE(FEET) = 3.47
TC = 0.303*[( 100.00**3)/( 3.47)]**.2 = 3.746
COMPUTED TIME OF CONCENTRATION INCREASED TO 5 MIN.
10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.787
COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8841
SOIL CLASSIFICATION IS "C"
SUBAREA RUNOFF(CFS) = 0.12
TOTAL AREA(ACRES) = 0.05 TOTAL RUNOFF(CFS) = 0.12

```

```

*****

```

```

FLOW PROCESS FROM NODE 201.00 TO NODE 202.00 IS CODE = 51

```

```

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<

```

```

=====
ELEVATION DATA: UPSTREAM(FEET) = 1149.59 DOWNSTREAM(FEET) = 1139.16
CHANNEL LENGTH THRU SUBAREA(FEET) = 454.00 CHANNEL SLOPE = 0.0230
CHANNEL BASE(FEET) = 0.00 "Z" FACTOR = 99.000
MANNING'S FACTOR = 0.015 MAXIMUM DEPTH(FEET) = 1.00
10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 1.987
COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8792
SOIL CLASSIFICATION IS "C"
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.15
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 1.20
AVERAGE FLOW DEPTH(FEET) = 0.04 TRAVEL TIME(MIN.) = 6.30
Tc(MIN.) = 11.30
SUBAREA AREA(ACRES) = 0.03 SUBAREA RUNOFF(CFS) = 0.05
TOTAL AREA(ACRES) = 0.1 PEAK FLOW RATE(CFS) = 0.18

```

```

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH(FEET) = 0.04 FLOW VELOCITY(FEET/SEC.) = 1.05
LONGEST FLOWPATH FROM NODE 200.00 TO NODE 202.00 = 554.00 FEET.

```

```

*****

```

```

FLOW PROCESS FROM NODE 202.00 TO NODE 202.00 IS CODE = 81

```

```

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<

```

```

=====
10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 1.987

```

COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8792

SOIL CLASSIFICATION IS "C"

SUBAREA AREA(ACRES) =	0.03	SUBAREA RUNOFF(CFS) =	0.05
TOTAL AREA(ACRES) =	0.1	TOTAL RUNOFF(CFS) =	0.23
TC(MIN.) =	11.30		

=====

END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 0.1 TC(MIN.) = 11.30

PEAK FLOW RATE(CFS) = 0.23

=====

END OF RATIONAL METHOD ANALYSIS



\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM BASED ON  
 RIVERSIDE COUNTY FLOOD CONTROL & WATER CONSERVATION DISTRICT  
 (RCFC&WCD) 1978 HYDROLOGY MANUAL  
 (c) Copyright 1982-2011 Advanced Engineering Software (aes)  
 (Rational Tabling Version 18.0)  
 Release Date: 07/01/2011 License ID 1499

Analysis prepared by:

Kimley-Horn and Associates, Inc.  
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 Suite 200  
 Orange, CA 92868

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*

\* Rancho Springs Medical Center \*  
 \* Proposed Conditions \*  
 \* 100-year analysis \*  
 \*\*\*\*\*

FILE NAME: RS\_P.DAT  
 TIME/DATE OF STUDY: 07:28 05/18/2020

-----  
 USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
 -----

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
 SPECIFIED MINIMUM PIPE SIZE(INCH) = 12.00  
 SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.95  
 10-YEAR STORM 10-MINUTE INTENSITY(INCH/HOUR) = 2.070  
 10-YEAR STORM 60-MINUTE INTENSITY(INCH/HOUR) = 0.985  
 100-YEAR STORM 10-MINUTE INTENSITY(INCH/HOUR) = 3.430  
 100-YEAR STORM 60-MINUTE INTENSITY(INCH/HOUR) = 1.630  
 SLOPE OF 10-YEAR INTENSITY-DURATION CURVE = 0.4144876  
 SLOPE OF 100-YEAR INTENSITY-DURATION CURVE = 0.4152232  
 COMPUTED RAINFALL INTENSITY DATA:

STORM EVENT = 100.00 1-HOUR INTENSITY(INCH/HOUR) = 1.630  
 SLOPE OF INTENSITY DURATION CURVE = 0.4152

RCFC&WCD HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD  
 NOTE: COMPUTE CONFLUENCE VALUES ACCORDING TO RCFC&WCD HYDROLOGY MANUAL  
 AND IGNORE OTHER CONFLUENCE COMBINATIONS FOR DOWNSTREAM ANALYSES

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

NO.	HALF- WIDTH (FT)	CROWN TO CROSSFALL (FT)	STREET-CROSSFALL: IN- / OUT- / PARK- SIDE / SIDE / WAY	CURB HEIGHT (FT)	GUTTER-GEOMETRIES: WIDTH LIP HIKE (FT) (FT) (FT)	MANNING FACTOR (n)
1	30.0	20.0	0.018/0.018/0.020	0.67	2.00 0.0313 0.167	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
 as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
  2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)
- \*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
 OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*

FLOW PROCESS FROM NODE 30.00 TO NODE 31.00 IS CODE = 7

>>>>USER SPECIFIED HYDROLOGY INFORMATION AT NODE<<<<

=====

USER-SPECIFIED VALUES ARE AS FOLLOWS:

TC(MIN) = 5.00 RAIN INTENSITY(INCH/HOUR) = 4.57

```

                                RS_P_100.RES
TOTAL AREA(ACRES) =      0.08   TOTAL RUNOFF(CFS) =      0.14

*****
FLOW PROCESS FROM NODE      31.00 TO NODE      300.00 IS CODE =  41
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 1152.47  DOWNSTREAM(FEET) = 1143.66
FLOW LENGTH(FEET) =  226.00  MANNING'S N =  0.013
DEPTH OF FLOW IN 12.0 INCH PIPE IS  1.2 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) =  3.53
GIVEN PIPE DIAMETER(INCH) = 12.00  NUMBER OF PIPES =  1
PIPE-FLOW(CFS) =      0.14
PIPE TRAVEL TIME(MIN.) =  1.07  Tc(MIN.) =  6.07
LONGEST FLOWPATH FROM NODE      0.00 TO NODE      300.00 =      226.00 FEET.

*****
FLOW PROCESS FROM NODE      100.00 TO NODE      101.00 IS CODE =  21
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
=====
    ASSUMED INITIAL SUBAREA UNIFORM
    DEVELOPMENT IS COMMERCIAL
TC = K*[(LENGTH**3)/(ELEVATION CHANGE)]**.2
INITIAL SUBAREA FLOW-LENGTH(FEET) =  102.00
UPSTREAM ELEVATION(FEET) =  1157.00
DOWNSTREAM ELEVATION(FEET) =  1155.41
ELEVATION DIFFERENCE(FEET) =  1.59
TC = 0.303*[( 102.00**3)/( 1.59)]**.2 =  4.431
COMPUTED TIME OF CONCENTRATION INCREASED TO 5 MIN.
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  4.574
COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8896
SOIL CLASSIFICATION IS "C"
SUBAREA RUNOFF(CFS) =      0.41
TOTAL AREA(ACRES) =      0.10  TOTAL RUNOFF(CFS) =      0.41

*****
FLOW PROCESS FROM NODE      101.00 TO NODE      102.00 IS CODE =  41
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 1151.00  DOWNSTREAM(FEET) = 1149.75
FLOW LENGTH(FEET) =  104.00  MANNING'S N =  0.013
DEPTH OF FLOW IN 12.0 INCH PIPE IS  2.6 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) =  3.17
GIVEN PIPE DIAMETER(INCH) = 12.00  NUMBER OF PIPES =  1
PIPE-FLOW(CFS) =      0.41
PIPE TRAVEL TIME(MIN.) =  0.55  Tc(MIN.) =  5.55
LONGEST FLOWPATH FROM NODE      100.00 TO NODE      102.00 =      206.00 FEET.

*****
FLOW PROCESS FROM NODE      102.00 TO NODE      102.00 IS CODE =  1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
=====
TOTAL NUMBER OF STREAMS =  3
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM  1 ARE:
TIME OF CONCENTRATION(MIN.) =  5.55
RAINFALL INTENSITY(INCH/HR) =  4.38
TOTAL STREAM AREA(ACRES) =  0.10
PEAK FLOW RATE(CFS) AT CONFLUENCE =      0.41

```

```

*****
FLOW PROCESS FROM NODE    103.00 TO NODE    104.00 IS CODE =  21
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
=====
      ASSUMED INITIAL SUBAREA UNIFORM
      DEVELOPMENT IS COMMERCIAL
TC = K*[(LENGTH**3)/(ELEVATION CHANGE)]**.2
INITIAL SUBAREA FLOW-LENGTH(FEET) =  100.00
UPSTREAM ELEVATION(FEET) =  1155.37
DOWNSTREAM ELEVATION(FEET) =  1154.06
ELEVATION DIFFERENCE(FEET) =    1.31
TC = 0.303*[( 100.00**3)/(    1.31)]**.2 =   4.551
COMPUTED TIME OF CONCENTRATION INCREASED TO 5 MIN.
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  4.574
COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8896
SOIL CLASSIFICATION IS "C"
SUBAREA RUNOFF(CFS) =    0.45
TOTAL AREA(ACRES) =    0.11  TOTAL RUNOFF(CFS) =    0.45

*****
FLOW PROCESS FROM NODE    104.00 TO NODE    102.00 IS CODE =  51
-----
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) =  1154.06  DOWNSTREAM(FEET) =  1153.34
CHANNEL LENGTH THRU SUBAREA(FEET) =   76.00  CHANNEL SLOPE =  0.0095
CHANNEL BASE(FEET) =   0.00  "Z" FACTOR =  99.000
MANNING'S FACTOR = 0.015  MAXIMUM DEPTH(FEET) =   1.00
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  4.181
COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8887
SOIL CLASSIFICATION IS "C"
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) =    0.56
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) =   1.05
AVERAGE FLOW DEPTH(FEET) =   0.07  TRAVEL TIME(MIN.) =   1.21
Tc(MIN.) =   6.21
SUBAREA AREA(ACRES) =    0.06  SUBAREA RUNOFF(CFS) =    0.22
TOTAL AREA(ACRES) =    0.2    PEAK FLOW RATE(CFS) =    0.67

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH(FEET) =  0.08  FLOW VELOCITY(FEET/SEC.) =   1.08
LONGEST FLOWPATH FROM NODE    103.00 TO NODE    102.00 =   176.00 FEET.

*****
FLOW PROCESS FROM NODE    102.00 TO NODE    102.00 IS CODE =  81
-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  4.181
COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8887
SOIL CLASSIFICATION IS "C"
SUBAREA AREA(ACRES) =    0.06  SUBAREA RUNOFF(CFS) =    0.22
TOTAL AREA(ACRES) =    0.2    TOTAL RUNOFF(CFS) =    0.89
TC(MIN.) =   6.21

*****
FLOW PROCESS FROM NODE    102.00 TO NODE    102.00 IS CODE =   1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
=====
TOTAL NUMBER OF STREAMS =  3

```



CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:

TIME OF CONCENTRATION(MIN.) = 6.21  
 RAINFALL INTENSITY(INCH/HR) = 4.18  
 TOTAL STREAM AREA(ACRES) = 0.23  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 0.89

\*\*\*\*\*

FLOW PROCESS FROM NODE 105.00 TO NODE 106.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

ASSUMED INITIAL SUBAREA UNIFORM  
 DEVELOPMENT IS COMMERCIAL

TC =  $K * [(LENGTH ** 3) / (ELEVATION \text{ CHANGE})] ** .2$   
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
 UPSTREAM ELEVATION(FEET) = 1157.00  
 DOWNSTREAM ELEVATION(FEET) = 1154.96  
 ELEVATION DIFFERENCE(FEET) = 2.04  
 $TC = 0.303 * [(100.00 ** 3) / (2.04)] ** .2 = 4.165$   
 COMPUTED TIME OF CONCENTRATION INCREASED TO 5 MIN.  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.574  
 COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8896  
 SOIL CLASSIFICATION IS "C"  
 SUBAREA RUNOFF(CFS) = 0.49  
 TOTAL AREA(ACRES) = 0.12 TOTAL RUNOFF(CFS) = 0.49

\*\*\*\*\*

FLOW PROCESS FROM NODE 106.00 TO NODE 107.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1154.96 DOWNSTREAM(FEET) = 1152.14  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 123.00 CHANNEL SLOPE = 0.0229  
 CHANNEL BASE(FEET) = 0.00 "Z" FACTOR = 99.000  
 MANNING'S FACTOR = 0.015 MAXIMUM DEPTH(FEET) = 1.00  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.173  
 COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8887  
 SOIL CLASSIFICATION IS "C"  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.84  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 1.66  
 AVERAGE FLOW DEPTH(FEET) = 0.07 TRAVEL TIME(MIN.) = 1.24  
 $T_c(MIN.) = 6.24$   
 SUBAREA AREA(ACRES) = 0.19 SUBAREA RUNOFF(CFS) = 0.70  
 TOTAL AREA(ACRES) = 0.3 PEAK FLOW RATE(CFS) = 1.19

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.08 FLOW VELOCITY(FEET/SEC.) = 1.83  
 LONGEST FLOWPATH FROM NODE 105.00 TO NODE 107.00 = 223.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 107.00 TO NODE 107.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.173  
 COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8887  
 SOIL CLASSIFICATION IS "C"  
 SUBAREA AREA(ACRES) = 0.19 SUBAREA RUNOFF(CFS) = 0.70  
 TOTAL AREA(ACRES) = 0.5 TOTAL RUNOFF(CFS) = 1.90  
 $TC(MIN.) = 6.24$

\*\*\*\*\*

FLOW PROCESS FROM NODE 107.00 TO NODE 102.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1149.13 DOWNSTREAM(FEET) = 1148.92  
FLOW LENGTH(FEET) = 43.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 12.0 INCH PIPE IS 8.0 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 3.41  
ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 1.90  
PIPE TRAVEL TIME(MIN.) = 0.21 Tc(MIN.) = 6.45  
LONGEST FLOWPATH FROM NODE 105.00 TO NODE 102.00 = 266.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 102.00 TO NODE 102.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<

TOTAL NUMBER OF STREAMS = 3  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 3 ARE:  
TIME OF CONCENTRATION(MIN.) = 6.45  
RAINFALL INTENSITY(INCH/HR) = 4.12  
TOTAL STREAM AREA(ACRES) = 0.50  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 1.90

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	0.41	5.55	4.381	0.10
2	0.89	6.21	4.181	0.23
3	1.90	6.45	4.116	0.50

\*\*\*\*\*WARNING\*\*\*\*\*

IN THIS COMPUTER PROGRAM, THE CONFLUENCE VALUE USED IS BASED  
ON THE RCFC&WCD FORMULA OF PLATE D-1 AS DEFAULT VALUE. THIS FORMULA  
WILL NOT NECESSARILY RESULT IN THE MAXIMUM VALUE OF PEAK FLOW.

\*\*\*\*\*

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 3 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	2.84	5.55	4.381
2	3.11	6.21	4.181
3	3.16	6.45	4.116

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 3.16 Tc(MIN.) = 6.45  
TOTAL AREA(ACRES) = 0.8  
LONGEST FLOWPATH FROM NODE 105.00 TO NODE 102.00 = 266.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 102.00 TO NODE 108.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1148.92 DOWNSTREAM(FEET) = 1148.20  
FLOW LENGTH(FEET) = 65.00 MANNING'S N = 0.013

```

                                RS_P_100.RES
DEPTH OF FLOW IN 12.0 INCH PIPE IS 8.6 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 5.24
ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 3.16
PIPE TRAVEL TIME(MIN.) = 0.21 Tc(MIN.) = 6.65
LONGEST FLOWPATH FROM NODE 105.00 TO NODE 108.00 = 331.00 FEET.

*****
FLOW PROCESS FROM NODE 108.00 TO NODE 108.00 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 6.65
RAINFALL INTENSITY(INCH/HR) = 4.06
TOTAL STREAM AREA(ACRES) = 0.83
PEAK FLOW RATE(CFS) AT CONFLUENCE = 3.16

*****
FLOW PROCESS FROM NODE 109.00 TO NODE 110.00 IS CODE = 21
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
=====
ASSUMED INITIAL SUBAREA UNIFORM
DEVELOPMENT IS COMMERCIAL
TC = K*[(LENGTH**3)/(ELEVATION CHANGE)]**.2
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00
UPSTREAM ELEVATION(FEET) = 1158.23
DOWNSTREAM ELEVATION(FEET) = 1154.48
ELEVATION DIFFERENCE(FEET) = 3.75
TC = 0.303*[(100.00**3)/(3.75)]**.2 = 3.688
COMPUTED TIME OF CONCENTRATION INCREASED TO 5 MIN.
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.574
COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8896
SOIL CLASSIFICATION IS "C"
SUBAREA RUNOFF(CFS) = 0.61
TOTAL AREA(ACRES) = 0.15 TOTAL RUNOFF(CFS) = 0.61

*****
FLOW PROCESS FROM NODE 110.00 TO NODE 108.00 IS CODE = 51
-----
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 1154.48 DOWNSTREAM(FEET) = 1152.91
CHANNEL LENGTH THRU SUBAREA(FEET) = 35.00 CHANNEL SLOPE = 0.0449
CHANNEL BASE(FEET) = 0.00 "Z" FACTOR = 99.000
MANNING'S FACTOR = 0.015 MAXIMUM DEPTH(FEET) = 1.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.468
COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8894
SOIL CLASSIFICATION IS "C"
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.63
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 2.01
AVERAGE FLOW DEPTH(FEET) = 0.06 TRAVEL TIME(MIN.) = 0.29
Tc(MIN.) = 5.29
SUBAREA AREA(ACRES) = 0.01 SUBAREA RUNOFF(CFS) = 0.04
TOTAL AREA(ACRES) = 0.2 PEAK FLOW RATE(CFS) = 0.65

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH(FEET) = 0.06 FLOW VELOCITY(FEET/SEC.) = 1.94
LONGEST FLOWPATH FROM NODE 109.00 TO NODE 108.00 = 135.00 FEET.

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\*\*\*\*\*

FLOW PROCESS FROM NODE 108.00 TO NODE 108.00 IS CODE = 81

&gt;&gt;&gt;&gt;ADDITION OF SUBAREA TO MAINLINE PEAK FLOW&lt;&lt;&lt;&lt;

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.468  
 COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8894  
 SOIL CLASSIFICATION IS "C"  
 SUBAREA AREA(ACRES) = 0.01 SUBAREA RUNOFF(CFS) = 0.04  
 TOTAL AREA(ACRES) = 0.2 TOTAL RUNOFF(CFS) = 0.69  
 TC(MIN.) = 5.29

\*\*\*\*\*

FLOW PROCESS FROM NODE 108.00 TO NODE 108.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 5.29  
 RAINFALL INTENSITY(INCH/HR) = 4.47  
 TOTAL STREAM AREA(ACRES) = 0.17  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 0.69

## \*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	3.16	6.65	4.062	0.83
2	0.69	5.29	4.468	0.17

\*\*\*\*\*WARNING\*\*\*\*\*

IN THIS COMPUTER PROGRAM, THE CONFLUENCE VALUE USED IS BASED  
 ON THE RCFC&WCD FORMULA OF PLATE D-1 AS DEFAULT VALUE. THIS FORMULA  
 WILL NOT NECESSARILY RESULT IN THE MAXIMUM VALUE OF PEAK FLOW.

\*\*\*\*\*

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

## \*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	3.20	5.29	4.468
2	3.79	6.65	4.062

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 3.79 Tc(MIN.) = 6.65  
 TOTAL AREA(ACRES) = 1.0  
 LONGEST FLOWPATH FROM NODE 105.00 TO NODE 108.00 = 331.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 108.00 TO NODE 111.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1147.90 DOWNSTREAM(FEET) = 1147.68  
 FLOW LENGTH(FEET) = 36.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 15.0 INCH PIPE IS 9.9 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 4.42  
 ESTIMATED PIPE DIAMETER(INCH) = 15.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 3.79

```

                                RS_P_100.RES
PIPE TRAVEL TIME(MIN.) =    0.14    Tc(MIN.) =    6.79
LONGEST FLOWPATH FROM NODE    105.00 TO NODE    111.00 =    367.00 FEET.

*****
FLOW PROCESS FROM NODE    111.00 TO NODE    111.00 IS CODE =    1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
=====
TOTAL NUMBER OF STREAMS =    2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM    1 ARE:
TIME OF CONCENTRATION(MIN.) =    6.79
RAINFALL INTENSITY(INCH/HR) =    4.03
TOTAL STREAM AREA(ACRES) =    1.00
PEAK FLOW RATE(CFS) AT CONFLUENCE =    3.79

*****
FLOW PROCESS FROM NODE    112.00 TO NODE    111.00 IS CODE =    21
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
=====
    ASSUMED INITIAL SUBAREA UNIFORM
    DEVELOPMENT IS COMMERCIAL
TC = K*[(LENGTH**3)/(ELEVATION CHANGE)]**.2
INITIAL SUBAREA FLOW-LENGTH(FEET) =    89.00
UPSTREAM ELEVATION(FEET) =    1156.08
DOWNSTREAM ELEVATION(FEET) =    1151.80
ELEVATION DIFFERENCE(FEET) =    4.28
TC = 0.303*[(    89.00**3)/(    4.28)]**.2 =    3.349
COMPUTED TIME OF CONCENTRATION INCREASED TO 5 MIN.
    100 YEAR RAINFALL INTENSITY(INCH/HOUR) =    4.574
COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8896
SOIL CLASSIFICATION IS "C"
SUBAREA RUNOFF(CFS) =    0.45
TOTAL AREA(ACRES) =    0.11    TOTAL RUNOFF(CFS) =    0.45

*****
FLOW PROCESS FROM NODE    111.00 TO NODE    111.00 IS CODE =    1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<
=====
TOTAL NUMBER OF STREAMS =    2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM    2 ARE:
TIME OF CONCENTRATION(MIN.) =    5.00
RAINFALL INTENSITY(INCH/HR) =    4.57
TOTAL STREAM AREA(ACRES) =    0.11
PEAK FLOW RATE(CFS) AT CONFLUENCE =    0.45

** CONFLUENCE DATA **
STREAM    RUNOFF    Tc    INTENSITY    AREA
NUMBER    (CFS)    (MIN.)    (INCH/HOUR)    (ACRE)
    1        3.79    6.79        4.029        1.00
    2        0.45    5.00        4.574        0.11

*****WARNING*****
IN THIS COMPUTER PROGRAM, THE CONFLUENCE VALUE USED IS BASED
ON THE RCFC&WCD FORMULA OF PLATE D-1 AS DEFAULT VALUE. THIS FORMULA
WILL NOT NECESSARILY RESULT IN THE MAXIMUM VALUE OF PEAK FLOW.
*****

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR    2 STREAMS.

```

## \*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	3.24	5.00	4.574
2	4.18	6.79	4.029

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 4.18 Tc(MIN.) = 6.79

TOTAL AREA(ACRES) = 1.1

LONGEST FLOWPATH FROM NODE 105.00 TO NODE 111.00 = 367.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 111.00 TO NODE 113.00 IS CODE = 31

&gt;&gt;&gt;&gt;COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA&lt;&lt;&lt;&lt;

&gt;&gt;&gt;&gt;USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)&lt;&lt;&lt;&lt;

=====

ELEVATION DATA: UPSTREAM(FEET) = 1147.29 DOWNSTREAM(FEET) = 1146.91

FLOW LENGTH(FEET) = 75.00 MANNING'S N = 0.013

DEPTH OF FLOW IN 15.0 INCH PIPE IS 11.5 INCHES

PIPE-FLOW VELOCITY(FEET/SEC.) = 4.15

ESTIMATED PIPE DIAMETER(INCH) = 15.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 4.18

PIPE TRAVEL TIME(MIN.) = 0.30 Tc(MIN.) = 7.09

LONGEST FLOWPATH FROM NODE 105.00 TO NODE 113.00 = 442.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 113.00 TO NODE 113.00 IS CODE = 1

&gt;&gt;&gt;&gt;DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE&lt;&lt;&lt;&lt;

=====

TOTAL NUMBER OF STREAMS = 2

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:

TIME OF CONCENTRATION(MIN.) = 7.09

RAINFALL INTENSITY(INCH/HR) = 3.96

TOTAL STREAM AREA(ACRES) = 1.11

PEAK FLOW RATE(CFS) AT CONFLUENCE = 4.18

\*\*\*\*\*

FLOW PROCESS FROM NODE 114.00 TO NODE 115.00 IS CODE = 21

&gt;&gt;&gt;&gt;RATIONAL METHOD INITIAL SUBAREA ANALYSIS&lt;&lt;&lt;&lt;

=====

ASSUMED INITIAL SUBAREA UNIFORM

DEVELOPMENT IS COMMERCIAL

TC = K\*[(LENGTH\*\*3)/(ELEVATION CHANGE)]\*\*.2

INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00

UPSTREAM ELEVATION(FEET) = 1158.13

DOWNSTREAM ELEVATION(FEET) = 1155.26

ELEVATION DIFFERENCE(FEET) = 2.87

TC = 0.303\*[( 100.00\*\*3)/( 2.87)]\*\*.2 = 3.891

COMPUTED TIME OF CONCENTRATION INCREASED TO 5 MIN.

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.574

COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8896

SOIL CLASSIFICATION IS "C"

SUBAREA RUNOFF(CFS) = 0.33

TOTAL AREA(ACRES) = 0.08 TOTAL RUNOFF(CFS) = 0.33

\*\*\*\*\*

FLOW PROCESS FROM NODE 115.00 TO NODE 116.00 IS CODE = 51

&gt;&gt;&gt;&gt;COMPUTE TRAPEZOIDAL CHANNEL FLOW&lt;&lt;&lt;&lt;

&gt;&gt;&gt;&gt;TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)&lt;&lt;&lt;&lt;

```

=====
ELEVATION DATA: UPSTREAM(FEET) = 1155.26 DOWNSTREAM(FEET) = 1152.66
CHANNEL LENGTH THRU SUBAREA(FEET) = 100.00 CHANNEL SLOPE = 0.0260
CHANNEL BASE(FEET) = 0.00 "Z" FACTOR = 99.000
MANNING'S FACTOR = 0.015 MAXIMUM DEPTH(FEET) = 1.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.215
COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8888
SOIL CLASSIFICATION IS "C"
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.51
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 1.53
AVERAGE FLOW DEPTH(FEET) = 0.06 TRAVEL TIME(MIN.) = 1.09
Tc(MIN.) = 6.09
SUBAREA AREA(ACRES) = 0.10 SUBAREA RUNOFF(CFS) = 0.37
TOTAL AREA(ACRES) = 0.2 PEAK FLOW RATE(CFS) = 0.70

```

```

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH(FEET) = 0.07 FLOW VELOCITY(FEET/SEC.) = 1.63
LONGEST FLOWPATH FROM NODE 114.00 TO NODE 116.00 = 200.00 FEET.

```

```

*****
FLOW PROCESS FROM NODE 116.00 TO NODE 116.00 IS CODE = 81
-----

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>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<

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```

=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.215
COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8888
SOIL CLASSIFICATION IS "C"
SUBAREA AREA(ACRES) = 0.10 SUBAREA RUNOFF(CFS) = 0.37
TOTAL AREA(ACRES) = 0.3 TOTAL RUNOFF(CFS) = 1.07
TC(MIN.) = 6.09

```

```

*****
FLOW PROCESS FROM NODE 116.00 TO NODE 113.00 IS CODE = 31
-----

```

```

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

```

```

=====
ELEVATION DATA: UPSTREAM(FEET) = 1148.49 DOWNSTREAM(FEET) = 1147.41
FLOW LENGTH(FEET) = 35.00 MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 12.000
DEPTH OF FLOW IN 12.0 INCH PIPE IS 3.4 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 5.86
ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 1.07
PIPE TRAVEL TIME(MIN.) = 0.10 Tc(MIN.) = 6.19
LONGEST FLOWPATH FROM NODE 114.00 TO NODE 113.00 = 235.00 FEET.

```

```

*****
FLOW PROCESS FROM NODE 113.00 TO NODE 113.00 IS CODE = 1
-----

```

```

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<

```

```

=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 6.19
RAINFALL INTENSITY(INCH/HR) = 4.19
TOTAL STREAM AREA(ACRES) = 0.28
PEAK FLOW RATE(CFS) AT CONFLUENCE = 1.07

```

```

** CONFLUENCE DATA **

```

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
------------------	-----------------	--------------	--------------------------	----------------

1	4.18	7.09	3.957	1.11
2	1.07	6.19	4.187	0.28

\*\*\*\*\*WARNING\*\*\*\*\*

IN THIS COMPUTER PROGRAM, THE CONFLUENCE VALUE USED IS BASED  
ON THE RCFC&WCD FORMULA OF PLATE D-1 AS DEFAULT VALUE. THIS FORMULA  
WILL NOT NECESSARILY RESULT IN THE MAXIMUM VALUE OF PEAK FLOW.

\*\*\*\*\*

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	4.72	6.19	4.187
2	5.20	7.09	3.957

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 5.20 Tc(MIN.) = 7.09

TOTAL AREA(ACRES) = 1.4

LONGEST FLOWPATH FROM NODE 105.00 TO NODE 113.00 = 442.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 113.00 TO NODE 117.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1146.91 DOWNSTREAM(FEET) = 1146.78

FLOW LENGTH(FEET) = 25.00 MANNING'S N = 0.013

DEPTH OF FLOW IN 18.0 INCH PIPE IS 11.1 INCHES

PIPE-FLOW VELOCITY(FEET/SEC.) = 4.52

ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 5.20

PIPE TRAVEL TIME(MIN.) = 0.09 Tc(MIN.) = 7.18

LONGEST FLOWPATH FROM NODE 105.00 TO NODE 117.00 = 467.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 117.00 TO NODE 117.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

TOTAL NUMBER OF STREAMS = 3

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:

TIME OF CONCENTRATION(MIN.) = 7.18

RAINFALL INTENSITY(INCH/HR) = 3.94

TOTAL STREAM AREA(ACRES) = 1.39

PEAK FLOW RATE(CFS) AT CONFLUENCE = 5.20

\*\*\*\*\*

FLOW PROCESS FROM NODE 118.00 TO NODE 117.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

ASSUMED INITIAL SUBAREA UNIFORM

DEVELOPMENT IS COMMERCIAL

TC =  $K * [(LENGTH ** 3) / (ELEVATION CHANGE)] ** .2$

INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00

UPSTREAM ELEVATION(FEET) = 1152.04

DOWNSTREAM ELEVATION(FEET) = 1151.64

ELEVATION DIFFERENCE(FEET) = 0.40

TC =  $0.303 * [(100.00 ** 3) / (0.40)] ** .2 = 5.770$



```

                                RS_P_100.RES
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.310
COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8890
SOIL CLASSIFICATION IS "C"
SUBAREA RUNOFF(CFS) = 1.30
TOTAL AREA(ACRES) = 0.34 TOTAL RUNOFF(CFS) = 1.30

*****
FLOW PROCESS FROM NODE 117.00 TO NODE 117.00 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
=====
TOTAL NUMBER OF STREAMS = 3
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 5.77
RAINFALL INTENSITY(INCH/HR) = 4.31
TOTAL STREAM AREA(ACRES) = 0.34
PEAK FLOW RATE(CFS) AT CONFLUENCE = 1.30

*****
FLOW PROCESS FROM NODE 119.00 TO NODE 120.00 IS CODE = 22
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
=====
ASSUMED INITIAL SUBAREA UNIFORM
DEVELOPMENT IS COMMERCIAL
USER SPECIFIED Tc(MIN.) = 5.000
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.574
COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8896
SOIL CLASSIFICATION IS "C"
SUBAREA RUNOFF(CFS) = 0.28
TOTAL AREA(ACRES) = 0.07 TOTAL RUNOFF(CFS) = 0.28

*****
FLOW PROCESS FROM NODE 120.00 TO NODE 117.00 IS CODE = 31
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 1149.50 DOWNSTREAM(FEET) = 1147.78
FLOW LENGTH(FEET) = 66.00 MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 12.000
DEPTH OF FLOW IN 12.0 INCH PIPE IS 1.8 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 3.73
ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 0.28
PIPE TRAVEL TIME(MIN.) = 0.29 Tc(MIN.) = 5.29
LONGEST FLOWPATH FROM NODE 119.00 TO NODE 117.00 = 166.00 FEET.

*****
FLOW PROCESS FROM NODE 117.00 TO NODE 117.00 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<
=====
TOTAL NUMBER OF STREAMS = 3
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 3 ARE:
TIME OF CONCENTRATION(MIN.) = 5.29
RAINFALL INTENSITY(INCH/HR) = 4.47
TOTAL STREAM AREA(ACRES) = 0.07
PEAK FLOW RATE(CFS) AT CONFLUENCE = 0.28

** CONFLUENCE DATA **
STREAM RUNOFF Tc INTENSITY AREA

```

NUMBER	(CFS)	(MIN.)	(INCH/HOUR)	(ACRE)
1	5.20	7.18	3.935	1.39
2	1.30	5.77	4.310	0.34
3	0.28	5.29	4.466	0.07

\*\*\*\*\*WARNING\*\*\*\*\*

IN THIS COMPUTER PROGRAM, THE CONFLUENCE VALUE USED IS BASED  
ON THE RCFC&WCD FORMULA OF PLATE D-1 AS DEFAULT VALUE. THIS FORMULA  
WILL NOT NECESSARILY RESULT IN THE MAXIMUM VALUE OF PEAK FLOW.

\*\*\*\*\*

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 3 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	5.31	5.29	4.466
2	5.75	5.77	4.310
3	6.64	7.18	3.935

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 6.64 Tc(MIN.) = 7.18

TOTAL AREA(ACRES) = 1.8

LONGEST FLOWPATH FROM NODE 105.00 TO NODE 117.00 = 467.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 117.00 TO NODE 121.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

ELEVATION DATA: UPSTREAM(Feet) = 1146.78 DOWNSTREAM(Feet) = 1146.56

FLOW LENGTH(Feet) = 44.00 MANNING'S N = 0.013

DEPTH OF FLOW IN 18.0 INCH PIPE IS 13.6 INCHES

PIPE-FLOW VELOCITY(Feet/Sec.) = 4.65

ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 6.64

PIPE TRAVEL TIME(MIN.) = 0.16 Tc(MIN.) = 7.34

LONGEST FLOWPATH FROM NODE 105.00 TO NODE 121.00 = 511.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 121.00 TO NODE 121.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

TOTAL NUMBER OF STREAMS = 2

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:

TIME OF CONCENTRATION(MIN.) = 7.34

RAINFALL INTENSITY(INCH/HR) = 3.90

TOTAL STREAM AREA(ACRES) = 1.80

PEAK FLOW RATE(CFS) AT CONFLUENCE = 6.64

\*\*\*\*\*

FLOW PROCESS FROM NODE 122.00 TO NODE 123.00 IS CODE = 22

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

ASSUMED INITIAL SUBAREA UNIFORM

DEVELOPMENT IS COMMERCIAL

USER SPECIFIED Tc(MIN.) = 5.000

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.574

COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8896

SOIL CLASSIFICATION IS "C"

SUBAREA RUNOFF(CFS) = 0.28

TOTAL AREA(ACRES) = 0.07 TOTAL RUNOFF(CFS) = 0.28

\*\*\*\*\*

FLOW PROCESS FROM NODE 123.00 TO NODE 121.00 IS CODE = 31

&gt;&gt;&gt;&gt;COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA&lt;&lt;&lt;&lt;

&gt;&gt;&gt;&gt;USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)&lt;&lt;&lt;&lt;

=====

ELEVATION DATA: UPSTREAM(FEET) = 1149.50 DOWNSTREAM(FEET) = 1147.56

FLOW LENGTH(FEET) = 59.00 MANNING'S N = 0.013

ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 12.000

DEPTH OF FLOW IN 12.0 INCH PIPE IS 1.7 INCHES

PIPE-FLOW VELOCITY(FEET/SEC.) = 4.09

ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 0.28

PIPE TRAVEL TIME(MIN.) = 0.24 Tc(MIN.) = 5.24

LONGEST FLOWPATH FROM NODE 122.00 TO NODE 121.00 = 103.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 121.00 TO NODE 121.00 IS CODE = 1

&gt;&gt;&gt;&gt;DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE&lt;&lt;&lt;&lt;

&gt;&gt;&gt;&gt;AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES&lt;&lt;&lt;&lt;

=====

TOTAL NUMBER OF STREAMS = 2

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:

TIME OF CONCENTRATION(MIN.) = 5.24

RAINFALL INTENSITY(INCH/HR) = 4.49

TOTAL STREAM AREA(ACRES) = 0.07

PEAK FLOW RATE(CFS) AT CONFLUENCE = 0.28

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	6.64	7.34	3.900	1.80
2	0.28	5.24	4.486	0.07

\*\*\*\*\*WARNING\*\*\*\*\*

IN THIS COMPUTER PROGRAM, THE CONFLUENCE VALUE USED IS BASED  
ON THE RCFC&WCD FORMULA OF PLATE D-1 AS DEFAULT VALUE. THIS FORMULA  
WILL NOT NECESSARILY RESULT IN THE MAXIMUM VALUE OF PEAK FLOW.

\*\*\*\*\*

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	5.02	5.24	4.486
2	6.88	7.34	3.900

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 6.88 Tc(MIN.) = 7.34

TOTAL AREA(ACRES) = 1.9

LONGEST FLOWPATH FROM NODE 105.00 TO NODE 121.00 = 511.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 121.00 TO NODE 124.00 IS CODE = 31

&gt;&gt;&gt;&gt;COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA&lt;&lt;&lt;&lt;

&gt;&gt;&gt;&gt;USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)&lt;&lt;&lt;&lt;

```

=====
ELEVATION DATA: UPSTREAM(FEET) = 1146.56  DOWNSTREAM(FEET) = 1146.49
FLOW LENGTH(FEET) = 15.00  MANNING'S N = 0.013
DEPTH OF FLOW IN 18.0 INCH PIPE IS 14.5 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 4.51
ESTIMATED PIPE DIAMETER(INCH) = 18.00  NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 6.88
PIPE TRAVEL TIME(MIN.) = 0.06  Tc(MIN.) = 7.40
LONGEST FLOWPATH FROM NODE 105.00 TO NODE 124.00 = 526.00 FEET.

```

\*\*\*\*\*

```

FLOW PROCESS FROM NODE 124.00 TO NODE 124.00 IS CODE = 1
-----

```

&gt;&gt;&gt;&gt;DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE&lt;&lt;&lt;&lt;

```

=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 7.40
RAINFALL INTENSITY(INCH/HR) = 3.89
TOTAL STREAM AREA(ACRES) = 1.87
PEAK FLOW RATE(CFS) AT CONFLUENCE = 6.88

```

\*\*\*\*\*

```

FLOW PROCESS FROM NODE 125.00 TO NODE 124.00 IS CODE = 21
-----

```

&gt;&gt;&gt;&gt;RATIONAL METHOD INITIAL SUBAREA ANALYSIS&lt;&lt;&lt;&lt;

```

=====
ASSUMED INITIAL SUBAREA UNIFORM
DEVELOPMENT IS COMMERCIAL
TC = K*[(LENGTH**3)/(ELEVATION CHANGE)]**.2
INITIAL SUBAREA FLOW-LENGTH(FEET) = 76.00
UPSTREAM ELEVATION(FEET) = 1155.54
DOWNSTREAM ELEVATION(FEET) = 1151.58
ELEVATION DIFFERENCE(FEET) = 3.96
TC = 0.303*[( 76.00**3)/( 3.96)]**.2 = 3.094
COMPUTED TIME OF CONCENTRATION INCREASED TO 5 MIN.
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.574
COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8896
SOIL CLASSIFICATION IS "C"
SUBAREA RUNOFF(CFS) = 0.49
TOTAL AREA(ACRES) = 0.12  TOTAL RUNOFF(CFS) = 0.49

```

\*\*\*\*\*

```

FLOW PROCESS FROM NODE 124.00 TO NODE 124.00 IS CODE = 1
-----

```

```

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<

```

```

=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 5.00
RAINFALL INTENSITY(INCH/HR) = 4.57
TOTAL STREAM AREA(ACRES) = 0.12
PEAK FLOW RATE(CFS) AT CONFLUENCE = 0.49

```

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	6.88	7.40	3.888	1.87
2	0.49	5.00	4.574	0.12

\*\*\*\*\*WARNING\*\*\*\*\*

IN THIS COMPUTER PROGRAM, THE CONFLUENCE VALUE USED IS BASED  
ON THE RCFC&WCD FORMULA OF PLATE D-1 AS DEFAULT VALUE. THIS FORMULA  
WILL NOT NECESSARILY RESULT IN THE MAXIMUM VALUE OF PEAK FLOW.

\*\*\*\*\*

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	5.14	5.00	4.574
2	7.30	7.40	3.888

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 7.30 Tc(MIN.) = 7.40  
TOTAL AREA(ACRES) = 2.0  
LONGEST FLOWPATH FROM NODE 105.00 TO NODE 124.00 = 526.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 124.00 TO NODE 126.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1146.00 DOWNSTREAM(FEET) = 1145.70  
FLOW LENGTH(FEET) = 60.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 21.0 INCH PIPE IS 12.6 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 4.86  
ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 7.30  
PIPE TRAVEL TIME(MIN.) = 0.21 Tc(MIN.) = 7.60  
LONGEST FLOWPATH FROM NODE 105.00 TO NODE 126.00 = 586.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 126.00 TO NODE 126.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 7.60  
RAINFALL INTENSITY(INCH/HR) = 3.84  
TOTAL STREAM AREA(ACRES) = 1.99  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 7.30

\*\*\*\*\*

FLOW PROCESS FROM NODE 127.00 TO NODE 128.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

ASSUMED INITIAL SUBAREA UNIFORM  
DEVELOPMENT IS COMMERCIAL  
TC =  $K * [(LENGTH ** 3) / (ELEVATION CHANGE)] ** .2$   
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
UPSTREAM ELEVATION(FEET) = 1166.00  
DOWNSTREAM ELEVATION(FEET) = 1159.30  
ELEVATION DIFFERENCE(FEET) = 6.70  
TC =  $0.303 * [(100.00 ** 3) / (6.70)] ** .2 = 3.284$   
COMPUTED TIME OF CONCENTRATION INCREASED TO 5 MIN.  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.574  
COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8896  
SOIL CLASSIFICATION IS "C"

SUBAREA RUNOFF(CFS) = 0.24  
 TOTAL AREA(ACRES) = 0.06 TOTAL RUNOFF(CFS) = 0.24

\*\*\*\*\*

FLOW PROCESS FROM NODE 128.00 TO NODE 126.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<

>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1159.30 DOWNSTREAM(FEET) = 1151.31  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 118.00 CHANNEL SLOPE = 0.0677  
 CHANNEL BASE(FEET) = 0.00 "Z" FACTOR = 99.000  
 MANNING'S FACTOR = 0.015 MAXIMUM DEPTH(FEET) = 1.00  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.235  
 COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8888  
 SOIL CLASSIFICATION IS "C"  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.45  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 1.93  
 AVERAGE FLOW DEPTH(FEET) = 0.05 TRAVEL TIME(MIN.) = 1.02  
 Tc(MIN.) = 6.02  
 SUBAREA AREA(ACRES) = 0.11 SUBAREA RUNOFF(CFS) = 0.41  
 TOTAL AREA(ACRES) = 0.2 PEAK FLOW RATE(CFS) = 0.66

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.06 FLOW VELOCITY(FEET/SEC.) = 2.10  
 LONGEST FLOWPATH FROM NODE 127.00 TO NODE 126.00 = 218.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 126.00 TO NODE 126.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.235  
 COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8888  
 SOIL CLASSIFICATION IS "C"  
 SUBAREA AREA(ACRES) = 0.11 SUBAREA RUNOFF(CFS) = 0.41  
 TOTAL AREA(ACRES) = 0.3 TOTAL RUNOFF(CFS) = 1.07  
 TC(MIN.) = 6.02

\*\*\*\*\*

FLOW PROCESS FROM NODE 126.00 TO NODE 126.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 6.02  
 RAINFALL INTENSITY(INCH/HR) = 4.23  
 TOTAL STREAM AREA(ACRES) = 0.28  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 1.07

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	7.30	7.60	3.844	1.99
2	1.07	6.02	4.235	0.28

\*\*\*\*\*WARNING\*\*\*\*\*

IN THIS COMPUTER PROGRAM, THE CONFLUENCE VALUE USED IS BASED  
 ON THE RCFC&WCD FORMULA OF PLATE D-1 AS DEFAULT VALUE. THIS FORMULA  
 WILL NOT NECESSARILY RESULT IN THE MAXIMUM VALUE OF PEAK FLOW.

\*\*\*\*\*

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	6.85	6.02	4.235
2	8.27	7.60	3.844

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 8.27 Tc(MIN.) = 7.60

TOTAL AREA(ACRES) = 2.3

LONGEST FLOWPATH FROM NODE 105.00 TO NODE 126.00 = 586.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 126.00 TO NODE 129.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1145.70 DOWNSTREAM(FEET) = 1145.46

FLOW LENGTH(FEET) = 48.00 MANNING'S N = 0.013

DEPTH OF FLOW IN 21.0 INCH PIPE IS 13.7 INCHES

PIPE-FLOW VELOCITY(FEET/SEC.) = 4.99

ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 8.27

PIPE TRAVEL TIME(MIN.) = 0.16 Tc(MIN.) = 7.76

LONGEST FLOWPATH FROM NODE 105.00 TO NODE 129.00 = 634.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 129.00 TO NODE 129.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

TOTAL NUMBER OF STREAMS = 2

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:

TIME OF CONCENTRATION(MIN.) = 7.76

RAINFALL INTENSITY(INCH/HR) = 3.81

TOTAL STREAM AREA(ACRES) = 2.27

PEAK FLOW RATE(CFS) AT CONFLUENCE = 8.27

\*\*\*\*\*

FLOW PROCESS FROM NODE 130.00 TO NODE 131.00 IS CODE = 22

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

ASSUMED INITIAL SUBAREA UNIFORM

DEVELOPMENT IS COMMERCIAL

USER SPECIFIED Tc(MIN.) = 5.000

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.574

COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8896

SOIL CLASSIFICATION IS "C"

SUBAREA RUNOFF(CFS) = 0.28

TOTAL AREA(ACRES) = 0.07 TOTAL RUNOFF(CFS) = 0.28

\*\*\*\*\*

FLOW PROCESS FROM NODE 131.00 TO NODE 129.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1149.50 DOWNSTREAM(FEET) = 1146.96

FLOW LENGTH(FEET) = 26.00 MANNING'S N = 0.013  
 ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 12.000  
 DEPTH OF FLOW IN 12.0 INCH PIPE IS 1.3 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 5.94  
 ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 0.28  
 PIPE TRAVEL TIME(MIN.) = 0.07 Tc(MIN.) = 5.07  
 LONGEST FLOWPATH FROM NODE 130.00 TO NODE 129.00 = 74.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 129.00 TO NODE 129.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====  
 TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 5.07  
 RAINFALL INTENSITY(INCH/HR) = 4.55  
 TOTAL STREAM AREA(ACRES) = 0.07  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 0.28

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	8.27	7.76	3.811	2.27
2	0.28	5.07	4.546	0.07

\*\*\*\*\*WARNING\*\*\*\*\*

IN THIS COMPUTER PROGRAM, THE CONFLUENCE VALUE USED IS BASED  
 ON THE RCFC&WCD FORMULA OF PLATE D-1 AS DEFAULT VALUE. THIS FORMULA  
 WILL NOT NECESSARILY RESULT IN THE MAXIMUM VALUE OF PEAK FLOW.

\*\*\*\*\*

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	5.69	5.07	4.546
2	8.51	7.76	3.811

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 8.51 Tc(MIN.) = 7.76  
 TOTAL AREA(ACRES) = 2.3  
 LONGEST FLOWPATH FROM NODE 105.00 TO NODE 129.00 = 634.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 129.00 TO NODE 132.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====  
 ELEVATION DATA: UPSTREAM(FEET) = 1145.46 DOWNSTREAM(FEET) = 1145.15  
 FLOW LENGTH(FEET) = 63.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 21.0 INCH PIPE IS 14.0 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 4.99  
 ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 8.51  
 PIPE TRAVEL TIME(MIN.) = 0.21 Tc(MIN.) = 7.97  
 LONGEST FLOWPATH FROM NODE 105.00 TO NODE 132.00 = 697.00 FEET.



\*\*\*\*\*

FLOW PROCESS FROM NODE 132.00 TO NODE 132.00 IS CODE = 1

&gt;&gt;&gt;&gt;DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE&lt;&lt;&lt;&lt;

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
 TIME OF CONCENTRATION(MIN.) = 7.97  
 RAINFALL INTENSITY(INCH/HR) = 3.77  
 TOTAL STREAM AREA(ACRES) = 2.34  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 8.51

\*\*\*\*\*

FLOW PROCESS FROM NODE 133.00 TO NODE 134.00 IS CODE = 21

&gt;&gt;&gt;&gt;RATIONAL METHOD INITIAL SUBAREA ANALYSIS&lt;&lt;&lt;&lt;

=====

ASSUMED INITIAL SUBAREA UNIFORM  
 DEVELOPMENT IS COMMERCIAL  
 $TC = K * [(LENGTH ** 3) / (ELEVATION CHANGE)] ** .2$   
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
 UPSTREAM ELEVATION(FEET) = 1166.00  
 DOWNSTREAM ELEVATION(FEET) = 1157.98  
 ELEVATION DIFFERENCE(FEET) = 8.02  
 $TC = 0.303 * [(100.00 ** 3) / (8.02)] ** .2 = 3.168$   
 COMPUTED TIME OF CONCENTRATION INCREASED TO 5 MIN.  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.574  
 COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8896  
 SOIL CLASSIFICATION IS "C"  
 SUBAREA RUNOFF(CFS) = 0.28  
 TOTAL AREA(ACRES) = 0.07 TOTAL RUNOFF(CFS) = 0.28

\*\*\*\*\*

FLOW PROCESS FROM NODE 134.00 TO NODE 135.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<  
 >>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1157.98 DOWNSTREAM(FEET) = 1153.00  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 72.00 CHANNEL SLOPE = 0.0692  
 CHANNEL BASE(FEET) = 0.00 "Z" FACTOR = 99.000  
 MANNING'S FACTOR = 0.015 MAXIMUM DEPTH(FEET) = 1.00  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.369  
 COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8891  
 SOIL CLASSIFICATION IS "C"  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.34  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 2.06  
 AVERAGE FLOW DEPTH(FEET) = 0.04 TRAVEL TIME(MIN.) = 0.58  
 $T_c(MIN.) = 5.58$   
 SUBAREA AREA(ACRES) = 0.03 SUBAREA RUNOFF(CFS) = 0.12  
 TOTAL AREA(ACRES) = 0.1 PEAK FLOW RATE(CFS) = 0.40

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.04 FLOW VELOCITY(FEET/SEC.) = 2.20  
 LONGEST FLOWPATH FROM NODE 133.00 TO NODE 135.00 = 172.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 135.00 TO NODE 135.00 IS CODE = 81

&gt;&gt;&gt;&gt;ADDITION OF SUBAREA TO MAINLINE PEAK FLOW&lt;&lt;&lt;&lt;

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.369  
 COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8891

SOIL CLASSIFICATION IS "C"

SUBAREA AREA(ACRES) = 0.03 SUBAREA RUNOFF(CFS) = 0.12  
 TOTAL AREA(ACRES) = 0.1 TOTAL RUNOFF(CFS) = 0.52  
 TC(MIN.) = 5.58

\*\*\*\*\*

FLOW PROCESS FROM NODE 135.00 TO NODE 132.00 IS CODE = 31

-----

&gt;&gt;&gt;&gt;COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA&lt;&lt;&lt;&lt;

&gt;&gt;&gt;&gt;USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)&lt;&lt;&lt;&lt;

=====

ELEVATION DATA: UPSTREAM(FEET) = 1148.89 DOWNSTREAM(FEET) = 1146.15  
 FLOW LENGTH(FEET) = 55.00 MANNING'S N = 0.013  
 ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 12.000  
 DEPTH OF FLOW IN 12.0 INCH PIPE IS 2.1 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 5.62  
 ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 0.52  
 PIPE TRAVEL TIME(MIN.) = 0.16 Tc(MIN.) = 5.75  
 LONGEST FLOWPATH FROM NODE 133.00 TO NODE 132.00 = 227.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 132.00 TO NODE 132.00 IS CODE = 1

-----

&gt;&gt;&gt;&gt;DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE&lt;&lt;&lt;&lt;

&gt;&gt;&gt;&gt;AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES&lt;&lt;&lt;&lt;

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 5.75  
 RAINFALL INTENSITY(INCH/HR) = 4.32  
 TOTAL STREAM AREA(ACRES) = 0.13  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 0.52

## \*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	8.51	7.97	3.769	2.34
2	0.52	5.75	4.317	0.13

\*\*\*\*\*WARNING\*\*\*\*\*

IN THIS COMPUTER PROGRAM, THE CONFLUENCE VALUE USED IS BASED  
 ON THE RCFC&WCD FORMULA OF PLATE D-1 AS DEFAULT VALUE. THIS FORMULA  
 WILL NOT NECESSARILY RESULT IN THE MAXIMUM VALUE OF PEAK FLOW.

\*\*\*\*\*

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

## \*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	6.65	5.75	4.317
2	8.96	7.97	3.769

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 8.96 Tc(MIN.) = 7.97  
 TOTAL AREA(ACRES) = 2.5  
 LONGEST FLOWPATH FROM NODE 105.00 TO NODE 132.00 = 697.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 132.00 TO NODE 136.00 IS CODE = 31

-----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

```
=====
ELEVATION DATA: UPSTREAM(FEET) = 1145.15  DOWNSTREAM(FEET) = 1145.01
FLOW LENGTH(FEET) = 28.00  MANNING'S N = 0.013
DEPTH OF FLOW IN 21.0 INCH PIPE IS 14.5 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 5.07
ESTIMATED PIPE DIAMETER(INCH) = 21.00  NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 8.96
PIPE TRAVEL TIME(MIN.) = 0.09  Tc(MIN.) = 8.06
LONGEST FLOWPATH FROM NODE 105.00 TO NODE 136.00 = 725.00 FEET.
```

\*\*\*\*\*

```
FLOW PROCESS FROM NODE 136.00 TO NODE 136.00 IS CODE = 1
```

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

```
=====
TOTAL NUMBER OF STREAMS = 3
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 8.06
RAINFALL INTENSITY(INCH/HR) = 3.75
TOTAL STREAM AREA(ACRES) = 2.47
PEAK FLOW RATE(CFS) AT CONFLUENCE = 8.96
```

\*\*\*\*\*

```
FLOW PROCESS FROM NODE 137.00 TO NODE 138.00 IS CODE = 22
```

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

```
=====
ASSUMED INITIAL SUBAREA UNIFORM
DEVELOPMENT IS COMMERCIAL
USER SPECIFIED Tc(MIN.) = 5.000
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.574
COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8896
SOIL CLASSIFICATION IS "C"
SUBAREA RUNOFF(CFS) = 0.28
TOTAL AREA(ACRES) = 0.07  TOTAL RUNOFF(CFS) = 0.28
```

\*\*\*\*\*

```
FLOW PROCESS FROM NODE 138.00 TO NODE 136.00 IS CODE = 31
```

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

```
=====
ELEVATION DATA: UPSTREAM(FEET) = 1149.50  DOWNSTREAM(FEET) = 1147.26
FLOW LENGTH(FEET) = 26.00  MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 12.000
DEPTH OF FLOW IN 12.0 INCH PIPE IS 1.4 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 5.72
ESTIMATED PIPE DIAMETER(INCH) = 12.00  NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 0.28
PIPE TRAVEL TIME(MIN.) = 0.08  Tc(MIN.) = 5.08
LONGEST FLOWPATH FROM NODE 137.00 TO NODE 136.00 = 54.00 FEET.
```

\*\*\*\*\*

```
FLOW PROCESS FROM NODE 136.00 TO NODE 136.00 IS CODE = 1
```

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

```
=====
TOTAL NUMBER OF STREAMS = 3
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 5.08
RAINFALL INTENSITY(INCH/HR) = 4.55
```

TOTAL STREAM AREA(ACRES) = 0.07  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 0.28

\*\*\*\*\*

FLOW PROCESS FROM NODE 139.00 TO NODE 140.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

=====

ASSUMED INITIAL SUBAREA UNIFORM  
 DEVELOPMENT IS COMMERCIAL

TC =  $K * [(LENGTH * 3) / (ELEVATION\ CHANGE)]^{** .2}$   
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
 UPSTREAM ELEVATION(FEET) = 1159.54  
 DOWNSTREAM ELEVATION(FEET) = 1151.67  
 ELEVATION DIFFERENCE(FEET) = 7.87  
 $TC = 0.303 * [(100.00 * 3) / (7.87)]^{** .2} = 3.180$   
 COMPUTED TIME OF CONCENTRATION INCREASED TO 5 MIN.  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.574  
 COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8896  
 SOIL CLASSIFICATION IS "C"  
 SUBAREA RUNOFF(CFS) = 0.45  
 TOTAL AREA(ACRES) = 0.11 TOTAL RUNOFF(CFS) = 0.45

\*\*\*\*\*

FLOW PROCESS FROM NODE 140.00 TO NODE 136.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<  
 >>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1151.67 DOWNSTREAM(FEET) = 1150.93  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 91.00 CHANNEL SLOPE = 0.0081  
 CHANNEL BASE(FEET) = 0.00 "Z" FACTOR = 99.000  
 MANNING'S FACTOR = 0.015 MAXIMUM DEPTH(FEET) = 1.00  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.104  
 COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8885  
 SOIL CLASSIFICATION IS "C"  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.76  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 1.02  
 AVERAGE FLOW DEPTH(FEET) = 0.09 TRAVEL TIME(MIN.) = 1.49  
 Tc(MIN.) = 6.49  
 SUBAREA AREA(ACRES) = 0.17 SUBAREA RUNOFF(CFS) = 0.62  
 TOTAL AREA(ACRES) = 0.3 PEAK FLOW RATE(CFS) = 1.07

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.10 FLOW VELOCITY(FEET/SEC.) = 1.16  
 LONGEST FLOWPATH FROM NODE 139.00 TO NODE 136.00 = 191.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 136.00 TO NODE 136.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.104  
 COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8885  
 SOIL CLASSIFICATION IS "C"  
 SUBAREA AREA(ACRES) = 0.17 SUBAREA RUNOFF(CFS) = 0.62  
 TOTAL AREA(ACRES) = 0.4 TOTAL RUNOFF(CFS) = 1.69  
 TC(MIN.) = 6.49

\*\*\*\*\*

FLOW PROCESS FROM NODE 136.00 TO NODE 136.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

&gt;&gt;&gt;&gt;&gt;AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES&lt;&lt;&lt;&lt;&lt;

```

=====
TOTAL NUMBER OF STREAMS = 3
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 3 ARE:
TIME OF CONCENTRATION(MIN.) = 6.49
RAINFALL INTENSITY(INCH/HR) = 4.10
TOTAL STREAM AREA(ACRES) = 0.45
PEAK FLOW RATE(CFS) AT CONFLUENCE = 1.69

```

## \*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	8.96	8.06	3.751	2.47
2	0.28	5.08	4.545	0.07
3	1.69	6.49	4.104	0.45

## \*\*\*\*\*WARNING\*\*\*\*\*

IN THIS COMPUTER PROGRAM, THE CONFLUENCE VALUE USED IS BASED  
ON THE RCFC&WCD FORMULA OF PLATE D-1 AS DEFAULT VALUE. THIS FORMULA  
WILL NOT NECESSARILY RESULT IN THE MAXIMUM VALUE OF PEAK FLOW.

## \*\*\*\*\*

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 3 STREAMS.

## \*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	7.25	5.08	4.545
2	9.16	6.49	4.104
3	10.74	8.06	3.751

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 10.74 Tc(MIN.) = 8.06  
TOTAL AREA(ACRES) = 3.0  
LONGEST FLOWPATH FROM NODE 105.00 TO NODE 136.00 = 725.00 FEET.

## \*\*\*\*\*

FLOW PROCESS FROM NODE 136.00 TO NODE 141.00 IS CODE = 31

&gt;&gt;&gt;&gt;&gt;COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA&lt;&lt;&lt;&lt;&lt;

&gt;&gt;&gt;&gt;&gt;USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)&lt;&lt;&lt;&lt;&lt;

```

=====
ELEVATION DATA: UPSTREAM(Feet) = 1145.01 DOWNSTREAM(Feet) = 1144.82
FLOW LENGTH(Feet) = 40.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 24.0 INCH PIPE IS 14.9 INCHES
PIPE-FLOW VELOCITY(Feet/Sec.) = 5.24
ESTIMATED PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 10.74
PIPE TRAVEL TIME(MIN.) = 0.13 Tc(MIN.) = 8.19
LONGEST FLOWPATH FROM NODE 105.00 TO NODE 141.00 = 765.00 FEET.

```

## \*\*\*\*\*

FLOW PROCESS FROM NODE 141.00 TO NODE 141.00 IS CODE = 1

&gt;&gt;&gt;&gt;&gt;DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE&lt;&lt;&lt;&lt;&lt;

```

=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 8.19
RAINFALL INTENSITY(INCH/HR) = 3.73
TOTAL STREAM AREA(ACRES) = 2.99
PEAK FLOW RATE(CFS) AT CONFLUENCE = 10.74

```

```

*****
FLOW PROCESS FROM NODE    142.00 TO NODE    143.00 IS CODE =  21
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
=====
      ASSUMED INITIAL SUBAREA UNIFORM
      DEVELOPMENT IS COMMERCIAL
TC = K*[(LENGTH**3)/(ELEVATION CHANGE)]**.2
INITIAL SUBAREA FLOW-LENGTH(FEET) =  100.00
UPSTREAM ELEVATION(FEET) =  1166.00
DOWNSTREAM ELEVATION(FEET) =  1158.52
ELEVATION DIFFERENCE(FEET) =    7.48
TC = 0.303*[( 100.00**3)/(    7.48)]**.2 =    3.212
COMPUTED TIME OF CONCENTRATION INCREASED TO 5 MIN.
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  4.574
COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8896
SOIL CLASSIFICATION IS "C"
SUBAREA RUNOFF(CFS) =    0.33
TOTAL AREA(ACRES) =    0.08  TOTAL RUNOFF(CFS) =    0.33

*****
FLOW PROCESS FROM NODE    143.00 TO NODE    144.00 IS CODE =  51
-----
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) =  1158.52  DOWNSTREAM(FEET) =  1152.35
CHANNEL LENGTH THRU SUBAREA(FEET) =  122.00  CHANNEL SLOPE =  0.0506
CHANNEL BASE(FEET) =    0.00  "Z" FACTOR =  99.000
MANNING'S FACTOR = 0.015  MAXIMUM DEPTH(FEET) =  1.00
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  4.201
COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8888
SOIL CLASSIFICATION IS "C"
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) =    0.42
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) =  1.79
AVERAGE FLOW DEPTH(FEET) =  0.05  TRAVEL TIME(MIN.) =  1.14
Tc(MIN.) =  6.14
SUBAREA AREA(ACRES) =    0.05  SUBAREA RUNOFF(CFS) =    0.19
TOTAL AREA(ACRES) =    0.1    PEAK FLOW RATE(CFS) =    0.51

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH(FEET) =  0.05  FLOW VELOCITY(FEET/SEC.) =  2.03
LONGEST FLOWPATH FROM NODE    142.00 TO NODE    144.00 =    222.00 FEET.

*****
FLOW PROCESS FROM NODE    144.00 TO NODE    144.00 IS CODE =  81
-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  4.201
COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8888
SOIL CLASSIFICATION IS "C"
SUBAREA AREA(ACRES) =    0.05  SUBAREA RUNOFF(CFS) =    0.19
TOTAL AREA(ACRES) =    0.2    TOTAL RUNOFF(CFS) =    0.70
TC(MIN.) =  6.14

*****
FLOW PROCESS FROM NODE    144.00 TO NODE    141.00 IS CODE =  31
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
=====

```

ELEVATION DATA: UPSTREAM(FEET) = 1148.28 DOWNSTREAM(FEET) = 1145.82  
 FLOW LENGTH(FEET) = 56.00 MANNING'S N = 0.013  
 ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 12.000  
 DEPTH OF FLOW IN 12.0 INCH PIPE IS 2.5 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 5.85  
 ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 0.70  
 PIPE TRAVEL TIME(MIN.) = 0.16 Tc(MIN.) = 6.30  
 LONGEST FLOWPATH FROM NODE 142.00 TO NODE 141.00 = 278.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 141.00 TO NODE 141.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 6.30  
 RAINFALL INTENSITY(INCH/HR) = 4.16  
 TOTAL STREAM AREA(ACRES) = 0.18  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 0.70

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	10.74	8.19	3.726	2.99
2	0.70	6.30	4.156	0.18

\*\*\*\*\*WARNING\*\*\*\*\*

IN THIS COMPUTER PROGRAM, THE CONFLUENCE VALUE USED IS BASED  
 ON THE RCFC&WCD FORMULA OF PLATE D-1 AS DEFAULT VALUE. THIS FORMULA  
 WILL NOT NECESSARILY RESULT IN THE MAXIMUM VALUE OF PEAK FLOW.

\*\*\*\*\*

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	8.96	6.30	4.156
2	11.37	8.19	3.726

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 11.37 Tc(MIN.) = 8.19  
 TOTAL AREA(ACRES) = 3.2  
 LONGEST FLOWPATH FROM NODE 105.00 TO NODE 141.00 = 765.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 141.00 TO NODE 145.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1144.82 DOWNSTREAM(FEET) = 1144.62  
 FLOW LENGTH(FEET) = 39.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 24.0 INCH PIPE IS 15.1 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 5.47  
 ESTIMATED PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 11.37  
 PIPE TRAVEL TIME(MIN.) = 0.12 Tc(MIN.) = 8.31  
 LONGEST FLOWPATH FROM NODE 105.00 TO NODE 145.00 = 804.00 FEET.

```

*****
FLOW PROCESS FROM NODE    145.00 TO NODE    145.00 IS CODE =    1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
=====
TOTAL NUMBER OF STREAMS = 3
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) =    8.31
RAINFALL INTENSITY(INCH/HR) =    3.70
TOTAL STREAM AREA(ACRES) =    3.17
PEAK FLOW RATE(CFS) AT CONFLUENCE =    11.37

*****
FLOW PROCESS FROM NODE    146.00 TO NODE    147.00 IS CODE =   21
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
=====
    ASSUMED INITIAL SUBAREA UNIFORM
    DEVELOPMENT IS COMMERCIAL
TC = K*[(LENGTH**3)/(ELEVATION CHANGE)]**.2
INITIAL SUBAREA FLOW-LENGTH(FEET) =   100.00
UPSTREAM ELEVATION(FEET) =   1164.72
DOWNSTREAM ELEVATION(FEET) =   1157.49
ELEVATION DIFFERENCE(FEET) =     7.23
TC = 0.303*[( 100.00**3)/(    7.23)]**.2 =    3.234
COMPUTED TIME OF CONCENTRATION INCREASED TO 5 MIN.
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  4.574
COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8896
SOIL CLASSIFICATION IS "C"
SUBAREA RUNOFF(CFS) =     0.20
TOTAL AREA(ACRES) =     0.05  TOTAL RUNOFF(CFS) =     0.20

*****
FLOW PROCESS FROM NODE    147.00 TO NODE    148.00 IS CODE =   51
-----
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) =   1157.49  DOWNSTREAM(FEET) =   1152.14
CHANNEL LENGTH THRU SUBAREA(FEET) =   160.00  CHANNEL SLOPE =   0.0334
CHANNEL BASE(FEET) =    0.00  "Z" FACTOR =  99.000
MANNING'S FACTOR = 0.015  MAXIMUM DEPTH(FEET) =    1.00
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  4.057
COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8884
SOIL CLASSIFICATION IS "C"
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) =     0.40
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) =    1.59
AVERAGE FLOW DEPTH(FEET) =    0.05  TRAVEL TIME(MIN.) =    1.67
Tc(MIN.) =    6.67
SUBAREA AREA(ACRES) =     0.11  SUBAREA RUNOFF(CFS) =     0.40
TOTAL AREA(ACRES) =     0.2  PEAK FLOW RATE(CFS) =     0.60

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH(FEET) =  0.06  FLOW VELOCITY(FEET/SEC.) =    1.79
LONGEST FLOWPATH FROM NODE    146.00 TO NODE    148.00 =    260.00 FEET.

*****
FLOW PROCESS FROM NODE    148.00 TO NODE    148.00 IS CODE =   81
-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  4.057

```



COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8884  
 SOIL CLASSIFICATION IS "C"  
 SUBAREA AREA(ACRES) = 0.11 SUBAREA RUNOFF(CFS) = 0.40  
 TOTAL AREA(ACRES) = 0.3 TOTAL RUNOFF(CFS) = 1.00  
 TC(MIN.) = 6.67

\*\*\*\*\*

FLOW PROCESS FROM NODE 148.00 TO NODE 145.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1148.10 DOWNSTREAM(FEET) = 1145.62  
 FLOW LENGTH(FEET) = 41.00 MANNING'S N = 0.013  
 ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 12.000  
 DEPTH OF FLOW IN 12.0 INCH PIPE IS 2.8 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 7.28  
 ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 1.00  
 PIPE TRAVEL TIME(MIN.) = 0.09 Tc(MIN.) = 6.77  
 LONGEST FLOWPATH FROM NODE 146.00 TO NODE 145.00 = 301.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 145.00 TO NODE 145.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

=====

TOTAL NUMBER OF STREAMS = 3  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 6.77  
 RAINFALL INTENSITY(INCH/HR) = 4.03  
 TOTAL STREAM AREA(ACRES) = 0.27  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 1.00

\*\*\*\*\*

FLOW PROCESS FROM NODE 149.00 TO NODE 145.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

=====

ASSUMED INITIAL SUBAREA UNIFORM  
 DEVELOPMENT IS COMMERCIAL  
 $TC = K * [(LENGTH ** 3) / (ELEVATION CHANGE)] ** .2$   
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 94.00  
 UPSTREAM ELEVATION(FEET) = 1154.92  
 DOWNSTREAM ELEVATION(FEET) = 1151.86  
 ELEVATION DIFFERENCE(FEET) = 3.06  
 $TC = 0.303 * [(94.00 ** 3) / (3.06)] ** .2 = 3.701$   
 COMPUTED TIME OF CONCENTRATION INCREASED TO 5 MIN.  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.574  
 COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8896  
 SOIL CLASSIFICATION IS "C"  
 SUBAREA RUNOFF(CFS) = 0.45  
 TOTAL AREA(ACRES) = 0.11 TOTAL RUNOFF(CFS) = 0.45

\*\*\*\*\*

FLOW PROCESS FROM NODE 145.00 TO NODE 145.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<

=====

TOTAL NUMBER OF STREAMS = 3  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 3 ARE:  
 TIME OF CONCENTRATION(MIN.) = 5.00

RAINFALL INTENSITY(INCH/HR) = 4.57  
 TOTAL STREAM AREA(ACRES) = 0.11  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 0.45

## \*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	11.37	8.31	3.704	3.17
2	1.00	6.77	4.034	0.27
3	0.45	5.00	4.574	0.11

\*\*\*\*\*WARNING\*\*\*\*\*  
 IN THIS COMPUTER PROGRAM, THE CONFLUENCE VALUE USED IS BASED  
 ON THE RCFC&WCD FORMULA OF PLATE D-1 AS DEFAULT VALUE. THIS FORMULA  
 WILL NOT NECESSARILY RESULT IN THE MAXIMUM VALUE OF PEAK FLOW.  
 \*\*\*\*\*

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 3 STREAMS.

## \*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	8.02	5.00	4.574
2	10.65	6.77	4.034
3	12.64	8.31	3.704

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 12.64 Tc(MIN.) = 8.31  
 TOTAL AREA(ACRES) = 3.6  
 LONGEST FLOWPATH FROM NODE 105.00 TO NODE 145.00 = 804.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 145.00 TO NODE 150.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1144.62 DOWNSTREAM(FEET) = 1141.82  
 FLOW LENGTH(FEET) = 136.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 12.9 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 9.35  
 ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 12.64  
 PIPE TRAVEL TIME(MIN.) = 0.24 Tc(MIN.) = 8.55  
 LONGEST FLOWPATH FROM NODE 105.00 TO NODE 150.00 = 940.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 150.00 TO NODE 150.00 IS CODE = 10

>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<

\*\*\*\*\*

FLOW PROCESS FROM NODE 151.00 TO NODE 152.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

=====

ASSUMED INITIAL SUBAREA UNIFORM  
 DEVELOPMENT IS COMMERCIAL  
 $TC = K * [(LENGTH ** 3) / (ELEVATION CHANGE)] ** .2$   
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
 UPSTREAM ELEVATION(FEET) = 1152.00

DOWNSTREAM ELEVATION(FEET) = 1150.13  
 ELEVATION DIFFERENCE(FEET) = 1.87  
 $TC = 0.303 * [(100.00^{**3}) / (1.87)]^{**0.2} = 4.239$   
 COMPUTED TIME OF CONCENTRATION INCREASED TO 5 MIN.  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.574  
 COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8896  
 SOIL CLASSIFICATION IS "C"  
 SUBAREA RUNOFF(CFS) = 0.49  
 TOTAL AREA(ACRES) = 0.12 TOTAL RUNOFF(CFS) = 0.49

\*\*\*\*\*

FLOW PROCESS FROM NODE 152.00 TO NODE 152.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====  
 TOTAL NUMBER OF STREAMS = 3  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
 TIME OF CONCENTRATION(MIN.) = 5.00  
 RAINFALL INTENSITY(INCH/HR) = 4.57  
 TOTAL STREAM AREA(ACRES) = 0.12  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 0.49

\*\*\*\*\*

FLOW PROCESS FROM NODE 153.00 TO NODE 154.00 IS CODE = 22

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====  
 ASSUMED INITIAL SUBAREA UNIFORM  
 DEVELOPMENT IS COMMERCIAL  
 USER SPECIFIED Tc(MIN.) = 5.000  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.574  
 COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8896  
 SOIL CLASSIFICATION IS "C"  
 SUBAREA RUNOFF(CFS) = 0.28  
 TOTAL AREA(ACRES) = 0.07 TOTAL RUNOFF(CFS) = 0.28

\*\*\*\*\*

FLOW PROCESS FROM NODE 154.00 TO NODE 152.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====  
 ELEVATION DATA: UPSTREAM(FEET) = 1149.50 DOWNSTREAM(FEET) = 1146.64  
 FLOW LENGTH(FEET) = 93.00 MANNING'S N = 0.013  
 ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 12.000  
 DEPTH OF FLOW IN 12.0 INCH PIPE IS 1.8 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 3.97  
 ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 0.28  
 PIPE TRAVEL TIME(MIN.) = 0.39 Tc(MIN.) = 5.39  
 LONGEST FLOWPATH FROM NODE 153.00 TO NODE 152.00 = 193.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 152.00 TO NODE 152.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====  
 TOTAL NUMBER OF STREAMS = 3  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 5.39  
 RAINFALL INTENSITY(INCH/HR) = 4.43  
 TOTAL STREAM AREA(ACRES) = 0.07  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 0.28

\*\*\*\*\*

FLOW PROCESS FROM NODE 155.00 TO NODE 156.00 IS CODE = 22

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

=====

ASSUMED INITIAL SUBAREA UNIFORM  
DEVELOPMENT IS COMMERCIAL  
USER SPECIFIED Tc(MIN.) = 5.000  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.574  
COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8896  
SOIL CLASSIFICATION IS "C"  
SUBAREA RUNOFF(CFS) = 0.28  
TOTAL AREA(ACRES) = 0.07 TOTAL RUNOFF(CFS) = 0.28

\*\*\*\*\*

FLOW PROCESS FROM NODE 156.00 TO NODE 152.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1149.50 DOWNSTREAM(FEET) = 1146.64  
FLOW LENGTH(FEET) = 70.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 12.000  
DEPTH OF FLOW IN 12.0 INCH PIPE IS 1.7 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 4.36  
ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 0.28  
PIPE TRAVEL TIME(MIN.) = 0.27 Tc(MIN.) = 5.27  
LONGEST FLOWPATH FROM NODE 155.00 TO NODE 152.00 = 163.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 152.00 TO NODE 152.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<

=====

TOTAL NUMBER OF STREAMS = 3  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 3 ARE:  
TIME OF CONCENTRATION(MIN.) = 5.27  
RAINFALL INTENSITY(INCH/HR) = 4.48  
TOTAL STREAM AREA(ACRES) = 0.07  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 0.28

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	0.49	5.00	4.574	0.12
2	0.28	5.39	4.433	0.07
3	0.28	5.27	4.476	0.07

\*\*\*\*\*WARNING\*\*\*\*\*

IN THIS COMPUTER PROGRAM, THE CONFLUENCE VALUE USED IS BASED  
ON THE RCFC&WCD FORMULA OF PLATE D-1 AS DEFAULT VALUE. THIS FORMULA  
WILL NOT NECESSARILY RESULT IN THE MAXIMUM VALUE OF PEAK FLOW.

\*\*\*\*\*

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 3 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
------------------	-----------------	--------------	--------------------------

1	1.02	5.00	4.574
2	1.04	5.27	4.476
3	1.04	5.39	4.433

## COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 1.02 Tc(MIN.) = 5.00

TOTAL AREA(ACRES) = 0.3

LONGEST FLOWPATH FROM NODE 153.00 TO NODE 152.00 = 193.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 152.00 TO NODE 150.00 IS CODE = 31

&gt;&gt;&gt;&gt;COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA&lt;&lt;&lt;&lt;

&gt;&gt;&gt;&gt;USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)&lt;&lt;&lt;&lt;

=====

ELEVATION DATA: UPSTREAM(FEET) = 1146.14 DOWNSTREAM(FEET) = 1142.83

FLOW LENGTH(FEET) = 58.00 MANNING'S N = 0.013

ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 12.000

DEPTH OF FLOW IN 12.0 INCH PIPE IS 2.8 INCHES

PIPE-FLOW VELOCITY(FEET/SEC.) = 7.18

ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 1.02

PIPE TRAVEL TIME(MIN.) = 0.13 Tc(MIN.) = 5.13

LONGEST FLOWPATH FROM NODE 153.00 TO NODE 150.00 = 251.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 150.00 TO NODE 150.00 IS CODE = 14.0

&gt;&gt;&gt;&gt;MEMORY BANK # 1 COPIED ONTO MAIN-STREAM MEMORY&lt;&lt;&lt;&lt;

=====

## MAIN-STREAM MEMORY DEFINED AS FOLLOWS:

STREAM RUNOFF Tc

NUMBER (CFS) (MIN.)

1 12.64 8.55

TOTAL AREA = 3.6

\*\*\*\*\*

FLOW PROCESS FROM NODE 150.00 TO NODE 150.00 IS CODE = 1

&gt;&gt;&gt;&gt;DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE&lt;&lt;&lt;&lt;

=====

TOTAL NUMBER OF STREAMS = 2

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:

TIME OF CONCENTRATION(MIN.) = 8.55

RAINFALL INTENSITY(INCH/HR) = 3.66

TOTAL STREAM AREA(ACRES) = 3.55

PEAK FLOW RATE(CFS) AT CONFLUENCE = 12.64

\*\*\*\*\*

FLOW PROCESS FROM NODE 157.00 TO NODE 158.00 IS CODE = 21

&gt;&gt;&gt;&gt;RATIONAL METHOD INITIAL SUBAREA ANALYSIS&lt;&lt;&lt;&lt;

=====

ASSUMED INITIAL SUBAREA UNIFORM

DEVELOPMENT IS COMMERCIAL

TC = K\*[(LENGTH\*\*3)/(ELEVATION CHANGE)]\*\*.2

INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00

UPSTREAM ELEVATION(FEET) = 1151.83

DOWNSTREAM ELEVATION(FEET) = 1150.21

ELEVATION DIFFERENCE(FEET) = 1.62

TC = 0.303\*[(100.00\*\*3)/(1.62)]\*\*.2 = 4.362

COMPUTED TIME OF CONCENTRATION INCREASED TO 5 MIN.

```

                                RS_P_100.RES
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.574
COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8896
SOIL CLASSIFICATION IS "C"
SUBAREA RUNOFF(CFS) = 0.41
TOTAL AREA(ACRES) = 0.10 TOTAL RUNOFF(CFS) = 0.41

*****
FLOW PROCESS FROM NODE 158.00 TO NODE 159.00 IS CODE = 51
-----
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 1150.21 DOWNSTREAM(FEET) = 1149.90
CHANNEL LENGTH THRU SUBAREA(FEET) = 23.00 CHANNEL SLOPE = 0.0135
CHANNEL BASE(FEET) = 0.00 "Z" FACTOR = 99.000
MANNING'S FACTOR = 0.015 MAXIMUM DEPTH(FEET) = 1.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.448
COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8893
SOIL CLASSIFICATION IS "C"
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.45
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 1.10
AVERAGE FLOW DEPTH(FEET) = 0.06 TRAVEL TIME(MIN.) = 0.35
Tc(MIN.) = 5.35
SUBAREA AREA(ACRES) = 0.02 SUBAREA RUNOFF(CFS) = 0.08
TOTAL AREA(ACRES) = 0.1 PEAK FLOW RATE(CFS) = 0.49

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH(FEET) = 0.06 FLOW VELOCITY(FEET/SEC.) = 1.20
LONGEST FLOWPATH FROM NODE 157.00 TO NODE 159.00 = 123.00 FEET.

*****
FLOW PROCESS FROM NODE 159.00 TO NODE 159.00 IS CODE = 81
-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.448
COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8893
SOIL CLASSIFICATION IS "C"
SUBAREA AREA(ACRES) = 0.02 SUBAREA RUNOFF(CFS) = 0.08
TOTAL AREA(ACRES) = 0.1 TOTAL RUNOFF(CFS) = 0.57
TC(MIN.) = 5.35

*****
FLOW PROCESS FROM NODE 159.00 TO NODE 150.00 IS CODE = 31
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 1141.90 DOWNSTREAM(FEET) = 1141.82
FLOW LENGTH(FEET) = 20.00 MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 12.000
DEPTH OF FLOW IN 12.0 INCH PIPE IS 4.1 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 2.35
ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 0.57
PIPE TRAVEL TIME(MIN.) = 0.14 Tc(MIN.) = 5.49
LONGEST FLOWPATH FROM NODE 157.00 TO NODE 150.00 = 143.00 FEET.

*****
FLOW PROCESS FROM NODE 150.00 TO NODE 150.00 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<

```

```

=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 5.49
RAINFALL INTENSITY(INCH/HR) = 4.40
TOTAL STREAM AREA(ACRES) = 0.14
PEAK FLOW RATE(CFS) AT CONFLUENCE = 0.57

```

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	12.64	8.55	3.660	3.55
2	0.57	5.49	4.400	0.14

\*\*\*\*\*WARNING\*\*\*\*\*

IN THIS COMPUTER PROGRAM, THE CONFLUENCE VALUE USED IS BASED  
ON THE RCFC&WCD FORMULA OF PLATE D-1 AS DEFAULT VALUE. THIS FORMULA  
WILL NOT NECESSARILY RESULT IN THE MAXIMUM VALUE OF PEAK FLOW.

\*\*\*\*\*

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	8.68	5.49	4.400
2	13.11	8.55	3.660

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 13.11 Tc(MIN.) = 8.55  
TOTAL AREA(ACRES) = 3.7  
LONGEST FLOWPATH FROM NODE 105.00 TO NODE 150.00 = 940.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 150.00 TO NODE 160.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1141.82 DOWNSTREAM(FEET) = 1141.64  
FLOW LENGTH(FEET) = 35.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 24.0 INCH PIPE IS 16.7 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 5.63  
ESTIMATED PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 13.11  
PIPE TRAVEL TIME(MIN.) = 0.10 Tc(MIN.) = 8.66  
LONGEST FLOWPATH FROM NODE 105.00 TO NODE 160.00 = 975.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 160.00 TO NODE 160.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 8.66  
RAINFALL INTENSITY(INCH/HR) = 3.64  
TOTAL STREAM AREA(ACRES) = 3.69  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 13.11

\*\*\*\*\*

FLOW PROCESS FROM NODE 161.00 TO NODE 162.00 IS CODE = 21

-----  
 >>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<  
 =====

ASSUMED INITIAL SUBAREA UNIFORM  
 DEVELOPMENT IS COMMERCIAL

TC = K\*[(LENGTH\*\*3)/(ELEVATION CHANGE)]\*\*.2  
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
 UPSTREAM ELEVATION(FEET) = 1153.39  
 DOWNSTREAM ELEVATION(FEET) = 1150.16  
 ELEVATION DIFFERENCE(FEET) = 3.23  
 TC = 0.303\*[( 100.00\*\*3)/( 3.23)]\*\*.2 = 3.800  
 COMPUTED TIME OF CONCENTRATION INCREASED TO 5 MIN.  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.574  
 COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8896  
 SOIL CLASSIFICATION IS "C"  
 SUBAREA RUNOFF(CFS) = 0.57  
 TOTAL AREA(ACRES) = 0.14 TOTAL RUNOFF(CFS) = 0.57

\*\*\*\*\*

FLOW PROCESS FROM NODE 162.00 TO NODE 163.00 IS CODE = 51

-----  
 >>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<  
 >>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<  
 =====

ELEVATION DATA: UPSTREAM(FEET) = 1150.16 DOWNSTREAM(FEET) = 1149.22  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 72.00 CHANNEL SLOPE = 0.0131  
 CHANNEL BASE(FEET) = 0.00 "Z" FACTOR = 99.000  
 MANNING'S FACTOR = 0.015 MAXIMUM DEPTH(FEET) = 1.00  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.294  
 COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8890  
 SOIL CLASSIFICATION IS "C"  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.95  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 1.46  
 AVERAGE FLOW DEPTH(FEET) = 0.08 TRAVEL TIME(MIN.) = 0.82  
 Tc(MIN.) = 5.82  
 SUBAREA AREA(ACRES) = 0.20 SUBAREA RUNOFF(CFS) = 0.76  
 TOTAL AREA(ACRES) = 0.3 PEAK FLOW RATE(CFS) = 1.33

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.09 FLOW VELOCITY(FEET/SEC.) = 1.51  
 LONGEST FLOWPATH FROM NODE 161.00 TO NODE 163.00 = 172.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 163.00 TO NODE 163.00 IS CODE = 81

-----  
 >>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<  
 =====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.294  
 COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8890  
 SOIL CLASSIFICATION IS "C"  
 SUBAREA AREA(ACRES) = 0.20 SUBAREA RUNOFF(CFS) = 0.76  
 TOTAL AREA(ACRES) = 0.5 TOTAL RUNOFF(CFS) = 2.10  
 TC(MIN.) = 5.82

\*\*\*\*\*

FLOW PROCESS FROM NODE 163.00 TO NODE 160.00 IS CODE = 31

-----  
 >>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<  
 =====

ELEVATION DATA: UPSTREAM(FEET) = 1145.18 DOWNSTREAM(FEET) = 1141.94  
 FLOW LENGTH(FEET) = 17.00 MANNING'S N = 0.013  
 ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 12.000



DEPTH OF FLOW IN 12.0 INCH PIPE IS 3.0 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 13.55  
 ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 2.10  
 PIPE TRAVEL TIME(MIN.) = 0.02 Tc(MIN.) = 5.84  
 LONGEST FLOWPATH FROM NODE 161.00 TO NODE 160.00 = 189.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 160.00 TO NODE 160.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 5.84  
 RAINFALL INTENSITY(INCH/HR) = 4.29  
 TOTAL STREAM AREA(ACRES) = 0.54  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 2.10

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	13.11	8.66	3.642	3.69
2	2.10	5.84	4.287	0.54

\*\*\*\*\*WARNING\*\*\*\*\*

IN THIS COMPUTER PROGRAM, THE CONFLUENCE VALUE USED IS BASED  
 ON THE RCFC&WCD FORMULA OF PLATE D-1 AS DEFAULT VALUE. THIS FORMULA  
 WILL NOT NECESSARILY RESULT IN THE MAXIMUM VALUE OF PEAK FLOW.

\*\*\*\*\*

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	10.95	5.84	4.287
2	14.90	8.66	3.642

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 14.90 Tc(MIN.) = 8.66  
 TOTAL AREA(ACRES) = 4.2  
 LONGEST FLOWPATH FROM NODE 105.00 TO NODE 160.00 = 975.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 160.00 TO NODE 164.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1141.78 DOWNSTREAM(FEET) = 1140.76  
 FLOW LENGTH(FEET) = 78.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 21.0 INCH PIPE IS 14.8 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 8.23  
 ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 14.90  
 PIPE TRAVEL TIME(MIN.) = 0.16 Tc(MIN.) = 8.81  
 LONGEST FLOWPATH FROM NODE 105.00 TO NODE 164.00 = 1053.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 164.00 TO NODE 164.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
 TIME OF CONCENTRATION(MIN.) = 8.81  
 RAINFALL INTENSITY(INCH/HR) = 3.61  
 TOTAL STREAM AREA(ACRES) = 4.23  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 14.90

\*\*\*\*\*

FLOW PROCESS FROM NODE 165.00 TO NODE 166.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

ASSUMED INITIAL SUBAREA UNIFORM  
 DEVELOPMENT IS COMMERCIAL  
 $TC = K * [(LENGTH ** 3) / (ELEVATION \text{ CHANGE})] ** .2$   
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 70.00  
 UPSTREAM ELEVATION(FEET) = 1151.81  
 DOWNSTREAM ELEVATION(FEET) = 1148.41  
 ELEVATION DIFFERENCE(FEET) = 3.40  
 $TC = 0.303 * [(70.00 ** 3) / (3.40)] ** .2 = 3.036$   
 COMPUTED TIME OF CONCENTRATION INCREASED TO 5 MIN.  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.574  
 COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8896  
 SOIL CLASSIFICATION IS "C"  
 SUBAREA RUNOFF(CFS) = 0.28  
 TOTAL AREA(ACRES) = 0.07 TOTAL RUNOFF(CFS) = 0.28

\*\*\*\*\*

FLOW PROCESS FROM NODE 166.00 TO NODE 164.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1144.84 DOWNSTREAM(FEET) = 1142.76  
 FLOW LENGTH(FEET) = 31.00 MANNING'S N = 0.013  
 ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 12.000  
 DEPTH OF FLOW IN 12.0 INCH PIPE IS 1.5 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 5.15  
 ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 0.28  
 PIPE TRAVEL TIME(MIN.) = 0.10  $T_c$ (MIN.) = 5.10  
 LONGEST FLOWPATH FROM NODE 165.00 TO NODE 164.00 = 101.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 164.00 TO NODE 164.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 5.10  
 RAINFALL INTENSITY(INCH/HR) = 4.54  
 TOTAL STREAM AREA(ACRES) = 0.07  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 0.28

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	$T_c$ (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	14.90	8.81	3.615	4.23

2            0.28            5.10            4.536            0.07

\*\*\*\*\*WARNING\*\*\*\*\*  
 IN THIS COMPUTER PROGRAM, THE CONFLUENCE VALUE USED IS BASED  
 ON THE RCFC&WCD FORMULA OF PLATE D-1 AS DEFAULT VALUE. THIS FORMULA  
 WILL NOT NECESSARILY RESULT IN THE MAXIMUM VALUE OF PEAK FLOW.  
 \*\*\*\*\*

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	8.90	5.10	4.536
2	15.12	8.81	3.615

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 15.12 Tc(MIN.) = 8.81  
 TOTAL AREA(ACRES) = 4.3  
 LONGEST FLOWPATH FROM NODE 105.00 TO NODE 164.00 = 1053.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 164.00 TO NODE 165.00 IS CODE = 31  
 -----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1140.76 DOWNSTREAM(FEET) = 1140.53  
 FLOW LENGTH(FEET) = 47.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 24.0 INCH PIPE IS 19.3 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 5.60  
 ESTIMATED PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 15.12  
 PIPE TRAVEL TIME(MIN.) = 0.14 Tc(MIN.) = 8.95  
 LONGEST FLOWPATH FROM NODE 105.00 TO NODE 165.00 = 1100.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 165.00 TO NODE 165.00 IS CODE = 1  
 -----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

=====

TOTAL NUMBER OF STREAMS = 3  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
 TIME OF CONCENTRATION(MIN.) = 8.95  
 RAINFALL INTENSITY(INCH/HR) = 3.59  
 TOTAL STREAM AREA(ACRES) = 4.30  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 15.12

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 166.00 TO NODE 167.00 IS CODE = 21  
 -----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

=====

ASSUMED INITIAL SUBAREA UNIFORM  
 DEVELOPMENT IS COMMERCIAL  
 $TC = K * [(LENGTH ** 3) / (ELEVATION CHANGE)] ** .2$   
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 61.00  
 UPSTREAM ELEVATION(FEET) = 1151.81  
 DOWNSTREAM ELEVATION(FEET) = 1150.67  
 ELEVATION DIFFERENCE(FEET) = 1.14  
 $TC = 0.303 * [(61.00 ** 3) / (1.14)] ** .2 = 3.479$   
 COMPUTED TIME OF CONCENTRATION INCREASED TO 5 MIN.

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.574  
 COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8896  
 SOIL CLASSIFICATION IS "C"  
 SUBAREA RUNOFF(CFS) = 0.20  
 TOTAL AREA(ACRES) = 0.05 TOTAL RUNOFF(CFS) = 0.20

\*\*\*\*\*

FLOW PROCESS FROM NODE 167.00 TO NODE 165.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1146.56 DOWNSTREAM(FEET) = 1145.98  
 FLOW LENGTH(FEET) = 8.00 MANNING'S N = 0.013  
 ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 12.000  
 DEPTH OF FLOW IN 12.0 INCH PIPE IS 1.2 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 4.83  
 ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 0.20  
 PIPE TRAVEL TIME(MIN.) = 0.03 Tc(MIN.) = 5.03  
 LONGEST FLOWPATH FROM NODE 166.00 TO NODE 165.00 = 69.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 165.00 TO NODE 165.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

=====

TOTAL NUMBER OF STREAMS = 3  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 5.03  
 RAINFALL INTENSITY(INCH/HR) = 4.56  
 TOTAL STREAM AREA(ACRES) = 0.05  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 0.20

\*\*\*\*\*

FLOW PROCESS FROM NODE 168.00 TO NODE 169.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

=====

ASSUMED INITIAL SUBAREA UNIFORM  
 DEVELOPMENT IS COMMERCIAL  
 $TC = K * [(LENGTH ** 3) / (ELEVATION CHANGE)] ** .2$   
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
 UPSTREAM ELEVATION(FEET) = 1151.99  
 DOWNSTREAM ELEVATION(FEET) = 1149.95  
 ELEVATION DIFFERENCE(FEET) = 2.04  
 $TC = 0.303 * [(100.00 ** 3) / (2.04)] ** .2 = 4.165$   
 COMPUTED TIME OF CONCENTRATION INCREASED TO 5 MIN.  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.574  
 COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8896  
 SOIL CLASSIFICATION IS "C"  
 SUBAREA RUNOFF(CFS) = 0.33  
 TOTAL AREA(ACRES) = 0.08 TOTAL RUNOFF(CFS) = 0.33

\*\*\*\*\*

FLOW PROCESS FROM NODE 169.00 TO NODE 170.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<  
 >>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1149.95 DOWNSTREAM(FEET) = 1149.76  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 25.00 CHANNEL SLOPE = 0.0076  
 CHANNEL BASE(FEET) = 0.00 "Z" FACTOR = 99.000

MANNING'S FACTOR = 0.015    MAXIMUM DEPTH(Feet) = 1.00  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.396  
 COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8892  
 SOIL CLASSIFICATION IS "C"  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.34  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(Feet/Sec.) = 0.83  
 AVERAGE FLOW DEPTH(Feet) = 0.06    TRAVEL TIME(Min.) = 0.50  
 Tc(Min.) = 5.50  
 SUBAREA AREA(ACRES) = 0.01    SUBAREA RUNOFF(CFS) = 0.02  
 TOTAL AREA(ACRES) = 0.1    PEAK FLOW RATE(CFS) = 0.35

## END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(Feet) = 0.06    FLOW VELOCITY(Feet/Sec.) = 0.86  
 LONGEST FLOWPATH FROM NODE 168.00 TO NODE 170.00 = 125.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 170.00 TO NODE 170.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.396  
 COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8892  
 SOIL CLASSIFICATION IS "C"  
 SUBAREA AREA(ACRES) = 0.01    SUBAREA RUNOFF(CFS) = 0.02  
 TOTAL AREA(ACRES) = 0.1    TOTAL RUNOFF(CFS) = 0.37  
 TC(Min.) = 5.50

\*\*\*\*\*

FLOW PROCESS FROM NODE 170.00 TO NODE 165.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

ELEVATION DATA: UPSTREAM(Feet) = 1144.85    DOWNSTREAM(Feet) = 1143.00  
 FLOW LENGTH(Feet) = 83.00    MANNING'S N = 0.013  
 ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 12.000  
 DEPTH OF FLOW IN 12.0 INCH PIPE IS 2.2 INCHES  
 PIPE-FLOW VELOCITY(Feet/Sec.) = 3.85  
 ESTIMATED PIPE DIAMETER(INCH) = 12.00    NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 0.37  
 PIPE TRAVEL TIME(Min.) = 0.36    Tc(Min.) = 5.86  
 LONGEST FLOWPATH FROM NODE 168.00 TO NODE 165.00 = 208.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 165.00 TO NODE 165.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<

TOTAL NUMBER OF STREAMS = 3  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 3 ARE:  
 TIME OF CONCENTRATION(Min.) = 5.86  
 RAINFALL INTENSITY(INCH/HR) = 4.28  
 TOTAL STREAM AREA(ACRES) = 0.09  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 0.37

## \*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (Min.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	15.12	8.95	3.591	4.30
2	0.20	5.03	4.563	0.05
3	0.37	5.86	4.282	0.09

\*\*\*\*\*WARNING\*\*\*\*\*

IN THIS COMPUTER PROGRAM, THE CONFLUENCE VALUE USED IS BASED  
ON THE RCFC&WCD FORMULA OF PLATE D-1 AS DEFAULT VALUE. THIS FORMULA  
WILL NOT NECESSARILY RESULT IN THE MAXIMUM VALUE OF PEAK FLOW.

\*\*\*\*\*

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 3 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	9.01	5.03	4.563
2	10.46	5.86	4.282
3	15.59	8.95	3.591

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 15.59 Tc(MIN.) = 8.95

TOTAL AREA(ACRES) = 4.4

LONGEST FLOWPATH FROM NODE 105.00 TO NODE 165.00 = 1100.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 165.00 TO NODE 171.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1140.52 DOWNSTREAM(FEET) = 1140.09

FLOW LENGTH(FEET) = 87.00 MANNING'S N = 0.013

DEPTH OF FLOW IN 27.0 INCH PIPE IS 17.2 INCHES

PIPE-FLOW VELOCITY(FEET/SEC.) = 5.83

ESTIMATED PIPE DIAMETER(INCH) = 27.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 15.59

PIPE TRAVEL TIME(MIN.) = 0.25 Tc(MIN.) = 9.20

LONGEST FLOWPATH FROM NODE 105.00 TO NODE 171.00 = 1187.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 171.00 TO NODE 171.00 IS CODE = 10

>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 2 <<<<

\*\*\*\*\*

FLOW PROCESS FROM NODE 172.00 TO NODE 173.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

ASSUMED INITIAL SUBAREA UNIFORM

DEVELOPMENT IS COMMERCIAL

TC = K\*[(LENGTH\*\*3)/(ELEVATION CHANGE)]\*\*.2

INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00

UPSTREAM ELEVATION(FEET) = 1150.81

DOWNSTREAM ELEVATION(FEET) = 1147.88

ELEVATION DIFFERENCE(FEET) = 2.93

TC = 0.303\*[(100.00\*\*3)/(2.93)]\*\*.2 = 3.874

COMPUTED TIME OF CONCENTRATION INCREASED TO 5 MIN.

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.574

COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8896

SOIL CLASSIFICATION IS "C"

SUBAREA RUNOFF(CFS) = 1.06

TOTAL AREA(ACRES) = 0.26 TOTAL RUNOFF(CFS) = 1.06

\*\*\*\*\*

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                                RS_P_100.RES
FLOW PROCESS FROM NODE      173.00 TO NODE      174.00 IS CODE =   51
-----
>>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
>>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) =  1147.88  DOWNSTREAM(FEET) =  1147.00
CHANNEL LENGTH THRU SUBAREA(FEET) =   35.00  CHANNEL SLOPE =  0.0251
CHANNEL BASE(FEET) =    0.00  "Z" FACTOR =  99.000
MANNING'S FACTOR = 0.015  MAXIMUM DEPTH(FEET) =   1.00
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  4.456
COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8893
SOIL CLASSIFICATION IS "C"
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) =       1.12
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) =   1.80
AVERAGE FLOW DEPTH(FEET) =   0.08  TRAVEL TIME(MIN.) =   0.32
Tc(MIN.) =    5.32
SUBAREA AREA(ACRES) =    0.03      SUBAREA RUNOFF(CFS) =    0.12
TOTAL AREA(ACRES) =    0.3        PEAK FLOW RATE(CFS) =    1.18

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH(FEET) =  0.08  FLOW VELOCITY(FEET/SEC.) =   1.81
LONGEST FLOWPATH FROM NODE      172.00 TO NODE      174.00 =    135.00 FEET.

*****
FLOW PROCESS FROM NODE      174.00 TO NODE      174.00 IS CODE =   81
-----
>>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
=====
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  4.456
COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8893
SOIL CLASSIFICATION IS "C"
SUBAREA AREA(ACRES) =    0.03  SUBAREA RUNOFF(CFS) =    0.12
TOTAL AREA(ACRES) =    0.3    TOTAL RUNOFF(CFS) =    1.30
TC(MIN.) =    5.32

*****
FLOW PROCESS FROM NODE      174.00 TO NODE      171.00 IS CODE =   31
-----
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) =  1143.47  DOWNSTREAM(FEET) =  1143.30
FLOW LENGTH(FEET) =    5.00  MANNING'S N =  0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 12.000
DEPTH OF FLOW IN  12.0 INCH PIPE IS   3.7 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) =   6.40
ESTIMATED PIPE DIAMETER(INCH) =  12.00  NUMBER OF PIPES =   1
PIPE-FLOW(CFS) =    1.30
PIPE TRAVEL TIME(MIN.) =   0.01  Tc(MIN.) =   5.34
LONGEST FLOWPATH FROM NODE      172.00 TO NODE      171.00 =    140.00 FEET.

*****
FLOW PROCESS FROM NODE      171.00 TO NODE      171.00 IS CODE =   10
-----
>>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 3 <<<<<
=====

*****
FLOW PROCESS FROM NODE      175.00 TO NODE      176.00 IS CODE =   21
-----
>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
=====
ASSUMED INITIAL SUBAREA UNIFORM

```

## DEVELOPMENT IS COMMERCIAL

$TC = K * [(LENGTH ** 3) / (ELEVATION\ CHANGE)] ** .2$   
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
 UPSTREAM ELEVATION(FEET) = 1151.24  
 DOWNSTREAM ELEVATION(FEET) = 1147.95  
 ELEVATION DIFFERENCE(FEET) = 3.29  
 $TC = 0.303 * [(100.00 ** 3) / (3.29)] ** .2 = 3.786$   
 COMPUTED TIME OF CONCENTRATION INCREASED TO 5 MIN.  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.574  
 COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8896  
 SOIL CLASSIFICATION IS "C"  
 SUBAREA RUNOFF(CFS) = 0.49  
 TOTAL AREA(ACRES) = 0.12 TOTAL RUNOFF(CFS) = 0.49

\*\*\*\*\*

FLOW PROCESS FROM NODE 176.00 TO NODE 177.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
 >>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1147.95 DOWNSTREAM(FEET) = 1147.00  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 158.00 CHANNEL SLOPE = 0.0060  
 CHANNEL BASE(FEET) = 0.00 "Z" FACTOR = 99.000  
 MANNING'S FACTOR = 0.015 MAXIMUM DEPTH(FEET) = 1.00  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.794  
 COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8877  
 SOIL CLASSIFICATION IS "C"  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.69  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 0.93  
 AVERAGE FLOW DEPTH(FEET) = 0.09 TRAVEL TIME(MIN.) = 2.84  
 $T_c(MIN.) = 7.84$   
 SUBAREA AREA(ACRES) = 0.12 SUBAREA RUNOFF(CFS) = 0.40  
 TOTAL AREA(ACRES) = 0.2 PEAK FLOW RATE(CFS) = 0.89

## END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.09 FLOW VELOCITY(FEET/SEC.) = 1.01  
 LONGEST FLOWPATH FROM NODE 175.00 TO NODE 177.00 = 258.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 177.00 TO NODE 177.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.794  
 COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8877  
 SOIL CLASSIFICATION IS "C"  
 SUBAREA AREA(ACRES) = 0.12 SUBAREA RUNOFF(CFS) = 0.40  
 TOTAL AREA(ACRES) = 0.4 TOTAL RUNOFF(CFS) = 1.30  
 $TC(MIN.) = 7.84$

\*\*\*\*\*

FLOW PROCESS FROM NODE 177.00 TO NODE 178.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1141.94 DOWNSTREAM(FEET) = 1141.01  
 FLOW LENGTH(FEET) = 105.00 MANNING'S N = 0.013  
 ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 12.000  
 DEPTH OF FLOW IN 12.0 INCH PIPE IS 5.3 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 3.92  
 ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 1.30



```

                                RS_P_100.RES
PIPE TRAVEL TIME(MIN.) =    0.45    Tc(MIN.) =    8.29
LONGEST FLOWPATH FROM NODE    175.00 TO NODE    178.00 =    363.00 FEET.

*****
FLOW PROCESS FROM NODE    178.00 TO NODE    178.00 IS CODE =    1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
=====
TOTAL NUMBER OF STREAMS =    2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM    1 ARE:
TIME OF CONCENTRATION(MIN.) =    8.29
RAINFALL INTENSITY(INCH/HR) =    3.71
TOTAL STREAM AREA(ACRES) =    0.36
PEAK FLOW RATE(CFS) AT CONFLUENCE =    1.30

*****
FLOW PROCESS FROM NODE    179.00 TO NODE    180.00 IS CODE =    21
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
=====
    ASSUMED INITIAL SUBAREA UNIFORM
    DEVELOPMENT IS COMMERCIAL
TC = K*[(LENGTH**3)/(ELEVATION CHANGE)]**.2
INITIAL SUBAREA FLOW-LENGTH(FEET) =    100.00
UPSTREAM ELEVATION(FEET) =    1148.13
DOWNSTREAM ELEVATION(FEET) =    1146.40
ELEVATION DIFFERENCE(FEET) =    1.73
TC = 0.303*[(    100.00**3)/(    1.73)]**.2 =    4.305
COMPUTED TIME OF CONCENTRATION INCREASED TO 5 MIN.
    100 YEAR RAINFALL INTENSITY(INCH/HOUR) =    4.574
COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8896
SOIL CLASSIFICATION IS "C"
SUBAREA RUNOFF(CFS) =    0.43
TOTAL AREA(ACRES) =    0.11    TOTAL RUNOFF(CFS) =    0.43

*****
FLOW PROCESS FROM NODE    180.00 TO NODE    181.00 IS CODE =    51
-----
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) =    1146.40    DOWNSTREAM(FEET) =    1145.61
CHANNEL LENGTH THRU SUBAREA(FEET) =    62.00    CHANNEL SLOPE =    0.0127
CHANNEL BASE(FEET) =    0.00    "Z" FACTOR =    99.000
MANNING'S FACTOR = 0.015    MAXIMUM DEPTH(FEET) =    1.00
    100 YEAR RAINFALL INTENSITY(INCH/HOUR) =    4.282
COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8890
SOIL CLASSIFICATION IS "C"
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) =    0.64
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) =    1.20
AVERAGE FLOW DEPTH(FEET) =    0.07    TRAVEL TIME(MIN.) =    0.86
Tc(MIN.) =    5.86
SUBAREA AREA(ACRES) =    0.11    SUBAREA RUNOFF(CFS) =    0.42
TOTAL AREA(ACRES) =    0.2    PEAK FLOW RATE(CFS) =    0.85

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH(FEET) =    0.08    FLOW VELOCITY(FEET/SEC.) =    1.31
LONGEST FLOWPATH FROM NODE    179.00 TO NODE    181.00 =    162.00 FEET.

*****
FLOW PROCESS FROM NODE    181.00 TO NODE    181.00 IS CODE =    81
-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<

```

```
=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.282
COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8890
SOIL CLASSIFICATION IS "C"
SUBAREA AREA(ACRES) = 0.11 SUBAREA RUNOFF(CFS) = 0.42
TOTAL AREA(ACRES) = 0.3 TOTAL RUNOFF(CFS) = 1.27
TC(MIN.) = 5.86
```

```
*****
FLOW PROCESS FROM NODE 181.00 TO NODE 178.00 IS CODE = 31
-----
```

```
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
```

```
=====
ELEVATION DATA: UPSTREAM(Feet) = 1142.60 DOWNSTREAM(Feet) = 1142.01
FLOW LENGTH(Feet) = 39.00 MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 12.000
DEPTH OF FLOW IN 12.0 INCH PIPE IS 4.5 INCHES
PIPE-FLOW VELOCITY(Feet/Sec.) = 4.74
ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 1.27
PIPE TRAVEL TIME(MIN.) = 0.14 Tc(MIN.) = 6.00
LONGEST FLOWPATH FROM NODE 179.00 TO NODE 178.00 = 201.00 FEET.
```

```
*****
FLOW PROCESS FROM NODE 178.00 TO NODE 178.00 IS CODE = 1
-----
```

```
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<
```

```
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 6.00
RAINFALL INTENSITY(INCH/HR) = 4.24
TOTAL STREAM AREA(ACRES) = 0.33
PEAK FLOW RATE(CFS) AT CONFLUENCE = 1.27
```

**\*\* CONFLUENCE DATA \*\***

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	1.30	8.29	3.708	0.36
2	1.27	6.00	4.241	0.33

**\*\*\*\*\*WARNING\*\*\*\*\***

IN THIS COMPUTER PROGRAM, THE CONFLUENCE VALUE USED IS BASED  
ON THE RCFC&WCD FORMULA OF PLATE D-1 AS DEFAULT VALUE. THIS FORMULA  
WILL NOT NECESSARILY RESULT IN THE MAXIMUM VALUE OF PEAK FLOW.

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

**\*\* PEAK FLOW RATE TABLE \*\***

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	2.21	6.00	4.241
2	2.41	8.29	3.708

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

```
PEAK FLOW RATE(CFS) = 2.41 Tc(MIN.) = 8.29
TOTAL AREA(ACRES) = 0.7
LONGEST FLOWPATH FROM NODE 175.00 TO NODE 178.00 = 363.00 FEET.
```

\*\*\*\*\*

FLOW PROCESS FROM NODE 178.00 TO NODE 171.00 IS CODE = 31

&gt;&gt;&gt;&gt;COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA&lt;&lt;&lt;&lt;

&gt;&gt;&gt;&gt;USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)&lt;&lt;&lt;&lt;

```

=====
ELEVATION DATA: UPSTREAM(FEET) = 1141.01 DOWNSTREAM(FEET) = 1140.96
FLOW LENGTH(FEET) = 110.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 21.0 INCH PIPE IS 13.3 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 1.49
ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 2.41
PIPE TRAVEL TIME(MIN.) = 1.23 Tc(MIN.) = 9.52
LONGEST FLOWPATH FROM NODE 175.00 TO NODE 171.00 = 473.00 FEET.
=====

```

\*\*\*\*\*

FLOW PROCESS FROM NODE 171.00 TO NODE 171.00 IS CODE = 14.0

&gt;&gt;&gt;&gt;MEMORY BANK # 2 COPIED ONTO MAIN-STREAM MEMORY&lt;&lt;&lt;&lt;

MAIN-STREAM MEMORY DEFINED AS FOLLOWS:

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)
1	15.59	9.20
TOTAL AREA = 4.4		

\*\*\*\*\*

FLOW PROCESS FROM NODE 171.00 TO NODE 171.00 IS CODE = 11

&gt;&gt;&gt;&gt;CONFLUENCE MEMORY BANK # 3 WITH THE MAIN-STREAM MEMORY&lt;&lt;&lt;&lt;

\*\* MAIN STREAM CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	15.59	9.20	3.550	4.44
LONGEST FLOWPATH FROM NODE 105.00 TO NODE 171.00 = 1187.00 FEET.				

\*\* MEMORY BANK # 3 CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	1.30	5.34	4.452	0.32
LONGEST FLOWPATH FROM NODE 172.00 TO NODE 171.00 = 140.00 FEET.				

\*\*\*\*\*WARNING\*\*\*\*\*

IN THIS COMPUTER PROGRAM, THE CONFLUENCE VALUE USED IS BASED  
ON THE RCFC&WCD FORMULA OF PLATE D-1 AS DEFAULT VALUE. THIS FORMULA  
WILL NOT NECESSARILY RESULT IN THE MAXIMUM VALUE OF PEAK FLOW.

\*\*\*\*\*

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	10.34	5.34	4.452
2	16.63	9.20	3.550

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 16.63 Tc(MIN.) = 9.20  
TOTAL AREA(ACRES) = 4.8

\*\*\*\*\*

FLOW PROCESS FROM NODE 171.00 TO NODE 182.00 IS CODE = 31

```

>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

```

```

=====
ELEVATION DATA: UPSTREAM(FEET) = 1140.09 DOWNSTREAM(FEET) = 1139.23
FLOW LENGTH(FEET) = 48.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 21.0 INCH PIPE IS 14.3 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 9.56
ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 16.63
PIPE TRAVEL TIME(MIN.) = 0.08 Tc(MIN.) = 9.29
LONGEST FLOWPATH FROM NODE 105.00 TO NODE 182.00 = 1235.00 FEET.

```

```

*****

```

```

FLOW PROCESS FROM NODE 200.00 TO NODE 201.00 IS CODE = 21

```

```

>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

```

```

=====
ASSUMED INITIAL SUBAREA UNIFORM
DEVELOPMENT IS COMMERCIAL
TC = K*[(LENGTH**3)/(ELEVATION CHANGE)]**.2
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00
UPSTREAM ELEVATION(FEET) = 1153.06
DOWNSTREAM ELEVATION(FEET) = 1149.59
ELEVATION DIFFERENCE(FEET) = 3.47
TC = 0.303*[( 100.00**3)/( 3.47)]**.2 = 3.746
COMPUTED TIME OF CONCENTRATION INCREASED TO 5 MIN.
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.574
COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8896
SOIL CLASSIFICATION IS "C"
SUBAREA RUNOFF(CFS) = 0.20
TOTAL AREA(ACRES) = 0.05 TOTAL RUNOFF(CFS) = 0.20

```

```

*****

```

```

FLOW PROCESS FROM NODE 201.00 TO NODE 202.00 IS CODE = 51

```

```

>>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
>>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

```

```

=====
ELEVATION DATA: UPSTREAM(FEET) = 1149.59 DOWNSTREAM(FEET) = 1139.16
CHANNEL LENGTH THRU SUBAREA(FEET) = 454.00 CHANNEL SLOPE = 0.0230
CHANNEL BASE(FEET) = 0.00 "Z" FACTOR = 99.000
MANNING'S FACTOR = 0.015 MAXIMUM DEPTH(FEET) = 1.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.347
COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8863
SOIL CLASSIFICATION IS "C"
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.25
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 1.35
AVERAGE FLOW DEPTH(FEET) = 0.04 TRAVEL TIME(MIN.) = 5.61
Tc(MIN.) = 10.61
SUBAREA AREA(ACRES) = 0.03 SUBAREA RUNOFF(CFS) = 0.09
TOTAL AREA(ACRES) = 0.1 PEAK FLOW RATE(CFS) = 0.29

```

```

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH(FEET) = 0.05 FLOW VELOCITY(FEET/SEC.) = 1.25
LONGEST FLOWPATH FROM NODE 200.00 TO NODE 202.00 = 554.00 FEET.

```

```

*****

```

```

FLOW PROCESS FROM NODE 202.00 TO NODE 202.00 IS CODE = 81

```

```

>>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

```

```

=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.347

```

COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8863

SOIL CLASSIFICATION IS "C"

SUBAREA AREA(ACRES) = 0.03 SUBAREA RUNOFF(CFS) = 0.09  
TOTAL AREA(ACRES) = 0.1 TOTAL RUNOFF(CFS) = 0.38  
TC(MIN.) = 10.61

=====

END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 0.1 TC(MIN.) = 10.61  
PEAK FLOW RATE(CFS) = 0.38

=====

=====

END OF RATIONAL METHOD ANALYSIS



APPENDIX B: STORM DRAIN HYDRAULIC ANALYSIS

UHS Rancho Springs Medical Center  
Synthetic Unit Hydrograph Method  
Loss Rate Estimates  
May-20

10-year and 100-year, AMC 2  
Existing Conditions

Soil Group	Cover Type	Curve (RI) Number	Pervious Area Infiltration Rate (in/hr)	Land Use	Decimal Percent of Impervious Area	Adj Infiltration Rate (in/hr)	Subarea (acres)	Total Area (acres)	Subarea/Total Area	Avg Adjusted Infiltration Rate (in/hr)*	Min Loss Rate (inch/hr)
C	Commercial Landscaping	69	0.11	Commercial	0.74	0.04	7.5	7.5	1	0.04	0.02

Low Loss Developed Condition = 0.9 - (0.8 x % Impervious) = 0.31 (Minimum value in AES is 0.5; therefore, 0.5 was used for the current study)

10-year and 100-year, AMC 2  
Project Conditions

Soil Group	Cover Type	Curve (RI) Number	Pervious Area Infiltration Rate (in/hr)	Land Use	Decimal Percent of Impervious Area	Adj Infiltration Rate (in/hr)	Subarea (acres)	Total Area (acres)	Subarea/Total Area	Avg Adjusted Infiltration Rate (in/hr)*	Min Loss Rate (inch/hr)
C	Commercial Landscaping	69	0.11	Commercial	0.85	0.03	5.9	5.9	1	0.03	0.01

Low Loss Developed Condition = 0.9 - (0.8 x % Impervious) = 0.22 (Minimum value in AES is 0.5; therefore, 0.5 was used for the current study)

Lag Time Calculations

	Tc (Min)	Tc (Hour)	Lag (Hour)
Existing DA C (100-year)	14	0.23	0.18
Existing DA C (10-year)	15	0.25	0.20
Project (100-year)	5	0.08	0.07
Project (10-year)	5	0.08	0.07

- 1. Lag time taken as 0.8(Tc), where Tc is time of concentration from rational method results.
  - 2. Tc from rational method results was used for existing conditions while a Tc of 5 was conservatively selected for the proposed conditions.
  - 3. Minimum lag time of 0.1 hr was used for analysis of proposed conditions.
- \*Minimum value in AES is 0.05; therefore, 0.05 was used for the study.

\*\*\*\*\*

## F L O O D     R O U T I N G     A N A L Y S I S

ACCORDING TO RIVERSIDE COUNTY FLOOD CONTROL AND WATER CONSERVATION DISTRICT  
(RCFC&WCD) 1978 HYDROLOGY MANUAL

(c) Copyright 1989-2011 Advanced Engineering Software (aes)

(Synthetic Unit Hydrograph Version 18.0)

Release Date: 05/01/2011 License ID 1499

Analysis prepared by:

Kimley-Horn and Associates, Inc.  
765 The City Drive  
Suite 200  
Orange, CA 92868

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*

\* UHS Rancho Springs Unit Hydrograph \*  
\* Proposed Conditions, 10-yr, 1-hr \*  
\* \*  
\*\*\*\*\*

FILE NAME: RS\_UNIT.DAT

TIME/DATE OF STUDY: 13:31 05/12/2020

\*\*\*\*\*

FLOW PROCESS FROM NODE 100.00 TO NODE 101.00 IS CODE = 1

-----

>>>>SUBAREA RUNOFF (UNIT-HYDROGRAPH ANALYSIS)<<<<

=====

(UNIT-HYDROGRAPH ADDED TO STREAM #1)

WATERSHED AREA = 5.900 ACRES

BASEFLOW = 0.000 CFS/SQUARE-MILE

Warning: Watershed Area is less than 10 acres

\*USER ENTERED "LAG" TIME = 0.100 HOURS

CAUTION: LAG TIME IS LESS THAN 0.50 HOURS.

THE 5-MINUTE PERIOD UH MODEL (USED IN THIS COMPUTER PROGRAM)

MAY BE TOO LARGE FOR PEAK FLOW ESTIMATES.

VALLEY S-GRAPH SELECTED

UNIFORM MEAN SOIL-LOSS(INCH/HOUR) = 0.050

LOW SOIL-LOSS RATE PERCENT(DECIMAL) = 0.500

USER-ENTERED RAINFALL = 0.99 INCHES

RCFC&WCD 1-Hour Storm (5-Minute period) SELECTED

(SLOPE OF INTENSITY-DURATION CURVE = 0.41)

RCFC&WCD DEPTH-AREA ADJUSTMENT FACTOR(PLATE E-5.8) = 1.0000

UNIT HYDROGRAPH TIME UNIT = 5.000 MINUTES

UNIT INTERVAL PERCENTAGE OF LAG-TIME = 83.333

=====

UNIT HYDROGRAPH DETERMINATION

-----

INTERVAL NUMBER	"S" GRAPH MEAN VALUES	UNIT HYDROGRAPH ORDINATES(CFS)
--------------------	--------------------------	-----------------------------------



1	13.994	9.985
2	59.664	32.587
3	78.792	13.649
4	86.766	5.689
5	91.428	3.326
6	94.514	2.202
7	96.650	1.524
8	98.044	0.995
9	98.699	0.467
10	99.289	0.421
11	99.716	0.304
12	99.929	0.152
13	100.000	0.051

↑

\*\*\*\*\*

UNIT PERIOD (NUMBER)	UNIT RAINFALL (INCHES)	UNIT SOIL-LOSS (INCHES)	EFFECTIVE RAINFALL (INCHES)
----------------------------	------------------------------	-------------------------------	-----------------------------------

1	0.0493	0.0042	0.0452
2	0.0517	0.0042	0.0475
3	0.0545	0.0042	0.0503
4	0.0593	0.0042	0.0551
5	0.0621	0.0042	0.0579
6	0.0694	0.0042	0.0652
7	0.0796	0.0042	0.0754
8	0.0864	0.0042	0.0822
9	0.1227	0.0042	0.1185
10	0.2220	0.0042	0.2178
11	0.0743	0.0042	0.0702
12	0.0537	0.0042	0.0495

TOTAL STORM RAINFALL(INCHES) = 0.99

TOTAL SOIL-LOSS(INCHES) = 0.05

TOTAL EFFECTIVE RAINFALL(INCHES) = 0.94

TOTAL SOIL-LOSS VOLUME(ACRE-FEET) =	0.0246
TOTAL STORM RUNOFF VOLUME(ACRE-FEET) =	0.4595

↑

# 1 - H O U R   S T O R M R U N O F F   H Y D R O G R A P H

HYDROGRAPH IN FIVE-MINUTE UNIT INTERVALS(CFS)  
(Note: Time indicated is at END of Each Unit Intervals)

TIME(HRS)	VOLUME(AF)	Q(CFS)	0.	5.0	10.0	15.0	20.0
0.083	0.0031	0.45	Q	.	.	.	.
0.167	0.0165	1.95	.V Q	.	.	.	.
0.250	0.0349	2.67	. V Q	.	.	.	.
0.333	0.0562	3.10	. V Q	.	.	.	.
0.417	0.0802	3.48	. Q	.	.	.	.
0.500	0.1066	3.83	. Q V.	.	.	.	.
0.583	0.1364	4.32	. Q .V	.	.	.	.
0.667	0.1702	4.91	. Q. V	.	.	.	.

RS_U_10.RES				
0.750	0.2096	5.72	.	.Q
0.833	0.2654	8.11	.	.
0.917	0.3376	10.48	.	.
1.000	0.3865	7.09	.	.
1.083	0.4184	4.64	.	.
1.167	0.4346	2.34	.	.
1.250	0.4439	1.35	.	.
1.333	0.4499	0.87	.	.
1.417	0.4537	0.56	.	.
1.500	0.4560	0.34	.	.
1.583	0.4576	0.23	.	.
1.667	0.4586	0.14	.	.
1.750	0.4591	0.08	.	.
1.833	0.4594	0.04	.	.
1.917	0.4595	0.01	.	.
2.000	0.4595	0.00	.	.

-----

TIME DURATION(minutes) OF PERCENTILES OF ESTIMATED PEAK FLOW RATE:  
 (Note: 100% of Peak Flow Rate estimate assumed to have  
 an instantaneous time duration)

Percentile of Estimated Peak Flow Rate	Duration (minutes)
=====	=====
0%	120.0
10%	70.0
20%	60.0
30%	45.0
40%	35.0
50%	20.0
60%	15.0
70%	10.0
80%	5.0
90%	5.0

=====

END OF FLOODSCx ROUTING ANALYSIS

## UHS Rancho Springs 10-yr, 1 hr Detention Analysis

---

### Project Summary

---

Title	UHS Rancho Springs_10 yr, 1 hr
Engineer	Nikki Kerry, P.E.
Company	Kimley-Horn and Associates, Inc.
Date	5/12/2020

---

---

### Notes

1. Inflow hydrograph (10-year, 1 hr) calculated based on Synthetic Unit Hydrograph Method from Riverside County Flood Control and Water Conservation District Hydrology Manual (April 1978) using AES software.
  2. Flow-through basin analysis completed using modified Pul's (storage indication routing).
-

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## UHS Rancho Springs 10-yr, 1 hr Detention Analysis

Subsection: User Notifications

### User Notifications

Message Id	17
Scenario	Base
Element Type	Composite Outlet Structure
Element Id	21
Label	Composite Outlet Structure - 1
Time	(N/A)
Message	Riser orifice equation controls at one or more headwater elevations for outlet structure.
Source	Information
Message Id	48
Scenario	Base
Element Type	Pond
Element Id	16
Label	Onsite Detention Basin
Time	(N/A)
Message	Outflow hydrograph never crested (last ordinate = max outflow).
Source	Warning

## UHS Rancho Springs 10-yr, 1 hr Detention Analysis

Subsection: Master Network Summary

### Catchments Summary

Label	Scenario	Return Event (years)	Hydrograph Volume (ac-ft)	Time to Peak (min)	Peak Flow (ft <sup>3</sup> /s)
Unit Hydrograph (Onsite Runoff)	Base	0	0.459	50.000	10.48

### Node Summary

Label	Scenario	Return Event (years)	Hydrograph Volume (ac-ft)	Time to Peak (min)	Peak Flow (ft <sup>3</sup> /s)
Outfall (POC)	Base	0	0.367	1,440.000	0.39

### Pond Summary

Label	Scenario	Return Event (years)	Hydrograph Volume (ac-ft)	Time to Peak (min)	Peak Flow (ft <sup>3</sup> /s)	Maximum Water Surface Elevation (ft)	Maximum Pond Storage (ac-ft)
Onsite Detention Basin (IN)	Base	0	1.226	51.000	9.80	(N/A)	(N/A)
Onsite Detention Basin (OUT)	Base	0	0.367	1,440.000	0.39	5.68	0.860

## UHS Rancho Springs 10-yr, 1 hr Detention Analysis

Subsection: Read Hydrograph

Label: Unit Hydrograph (Onsite Runoff)

Peak Discharge	10.48 ft <sup>3</sup> /s
Time to Peak	50.000 min
Hydrograph Volume	0.459 ac-ft

### HYDROGRAPH ORDINATES (ft<sup>3</sup>/s)

Output Time Increment = 5.000 min

Time on left represents time for first value in each row.

Time (min)	Flow (ft <sup>3</sup> /s)	Flow (ft <sup>3</sup> /s)	Flow (ft <sup>3</sup> /s)	Flow (ft <sup>3</sup> /s)	Flow (ft <sup>3</sup> /s)
0.000	0.45	1.95	2.67	3.10	3.48
25.000	3.83	4.32	4.91	5.72	8.11
50.000	10.48	7.09	4.64	2.34	1.35
75.000	0.87	0.56	0.34	0.23	0.14
100.000	0.08	0.04	0.01	0.00	0.42

## UHS Rancho Springs 10-yr, 1 hr Detention Analysis

Subsection: Addition Summary

Label: Outfall (POC)

### Summary for Hydrograph Addition at 'Outfall (POC)'

Upstream Link	Upstream Node
Outlet-1	Onsite Detention Basin

### Node Inflows

Inflow Type	Element	Volume (ac-ft)	Time to Peak (min)	Flow (Peak) (ft <sup>3</sup> /s)
Flow (From)	Outlet-1	0.367	1,440.000	0.39
Flow (In)	Outfall (POC)	0.367	1,440.000	0.39



## UHS Rancho Springs 10-yr, 1 hr Detention Analysis

Subsection: Time vs. Elevation

Label: Onsite Detention Basin (OUT)

### Time vs. Elevation (ft)

Output Time increment = 3.000 min

Time on left represents time for first value in each row.

Time (min)	Elevation (ft)	Elevation (ft)	Elevation (ft)	Elevation (ft)	Elevation (ft)
0.000	0.00	0.08	0.24	0.45	0.59
15.000	0.71	0.84	0.98	1.10	1.23
30.000	1.36	1.50	1.63	1.78	1.94
45.000	2.13	2.36	2.59	2.80	2.96
60.000	3.08	3.17	3.23	3.27	3.30
75.000	3.32	3.33	3.34	3.35	3.35
90.000	3.36	3.36	3.36	3.36	3.36
105.000	3.35	3.35	3.35	3.35	3.34
120.000	3.35	3.35	3.36	3.37	3.37
135.000	3.38	3.39	3.39	3.40	3.40
150.000	3.41	3.42	3.42	3.43	3.44
165.000	3.44	3.45	3.46	3.46	3.47
180.000	3.47	3.48	3.49	3.49	3.50
195.000	3.51	3.51	3.52	3.52	3.53
210.000	3.54	3.54	3.55	3.55	3.56
225.000	3.57	3.57	3.58	3.59	3.59
240.000	3.60	3.60	3.61	3.62	3.62
255.000	3.63	3.63	3.64	3.65	3.65
270.000	3.66	3.67	3.67	3.68	3.68
285.000	3.69	3.70	3.70	3.71	3.71
300.000	3.72	3.73	3.73	3.74	3.74
315.000	3.75	3.76	3.76	3.77	3.77
330.000	3.78	3.79	3.79	3.80	3.80
345.000	3.81	3.82	3.82	3.83	3.83
360.000	3.84	3.85	3.85	3.86	3.86
375.000	3.87	3.88	3.88	3.89	3.89
390.000	3.90	3.91	3.91	3.92	3.92
405.000	3.93	3.94	3.94	3.95	3.95
420.000	3.96	3.97	3.97	3.98	3.98
435.000	3.99	4.00	4.00	4.01	4.01
450.000	4.02	4.03	4.03	4.04	4.04
465.000	4.05	4.06	4.06	4.07	4.07
480.000	4.08	4.08	4.09	4.10	4.10
495.000	4.11	4.11	4.12	4.13	4.13
510.000	4.14	4.14	4.15	4.16	4.16
525.000	4.17	4.17	4.18	4.18	4.19
540.000	4.20	4.20	4.21	4.21	4.22
555.000	4.23	4.23	4.24	4.24	4.25
570.000	4.25	4.26	4.27	4.27	4.28
585.000	4.28	4.29	4.29	4.30	4.31
600.000	4.31	4.32	4.32	4.33	4.34

## UHS Rancho Springs 10-yr, 1 hr Detention Analysis

Subsection: Time vs. Elevation

Label: Onsite Detention Basin (OUT)

### Time vs. Elevation (ft)

Output Time increment = 3.000 min

Time on left represents time for first value in each row.

Time (min)	Elevation (ft)	Elevation (ft)	Elevation (ft)	Elevation (ft)	Elevation (ft)
615.000	4.34	4.35	4.35	4.36	4.36
630.000	4.37	4.38	4.38	4.39	4.39
645.000	4.40	4.40	4.41	4.42	4.42
660.000	4.43	4.43	4.44	4.44	4.45
675.000	4.46	4.46	4.47	4.47	4.48
690.000	4.48	4.49	4.50	4.50	4.51
705.000	4.51	4.52	4.52	4.53	4.54
720.000	4.54	4.55	4.55	4.56	4.56
735.000	4.57	4.58	4.58	4.59	4.59
750.000	4.60	4.61	4.61	4.62	4.62
765.000	4.63	4.63	4.64	4.65	4.65
780.000	4.66	4.66	4.67	4.67	4.68
795.000	4.69	4.69	4.70	4.70	4.71
810.000	4.71	4.72	4.72	4.73	4.74
825.000	4.74	4.75	4.75	4.76	4.76
840.000	4.77	4.78	4.78	4.79	4.79
855.000	4.80	4.80	4.81	4.82	4.82
870.000	4.83	4.83	4.84	4.84	4.85
885.000	4.85	4.86	4.87	4.87	4.88
900.000	4.88	4.89	4.89	4.90	4.91
915.000	4.91	4.92	4.92	4.93	4.93
930.000	4.94	4.94	4.95	4.96	4.96
945.000	4.97	4.97	4.98	4.98	4.99
960.000	4.99	5.00	5.01	5.01	5.02
975.000	5.02	5.03	5.03	5.04	5.05
990.000	5.05	5.06	5.06	5.07	5.07
1,005.000	5.08	5.09	5.09	5.10	5.10
1,020.000	5.11	5.11	5.12	5.13	5.13
1,035.000	5.14	5.14	5.15	5.15	5.16
1,050.000	5.17	5.17	5.18	5.18	5.19
1,065.000	5.19	5.20	5.20	5.21	5.22
1,080.000	5.22	5.23	5.23	5.24	5.24
1,095.000	5.25	5.26	5.26	5.27	5.27
1,110.000	5.28	5.28	5.29	5.29	5.30
1,125.000	5.31	5.31	5.32	5.32	5.33
1,140.000	5.33	5.34	5.35	5.35	5.36
1,155.000	5.36	5.37	5.37	5.38	5.38
1,170.000	5.39	5.40	5.40	5.41	5.41
1,185.000	5.42	5.42	5.43	5.43	5.44
1,200.000	5.45	5.45	5.46	5.46	5.47
1,215.000	5.47	5.48	5.48	5.49	5.50

## UHS Rancho Springs 10-yr, 1 hr Detention Analysis

Subsection: Time vs. Elevation

Label: Onsite Detention Basin (OUT)

### Time vs. Elevation (ft)

Output Time increment = 3.000 min

Time on left represents time for first value in each row.

Time (min)	Elevation (ft)	Elevation (ft)	Elevation (ft)	Elevation (ft)	Elevation (ft)
1,230.000	5.50	5.51	5.51	5.52	5.52
1,245.000	5.53	5.53	5.54	5.54	5.55
1,260.000	5.55	5.56	5.56	5.56	5.57
1,275.000	5.57	5.58	5.58	5.58	5.59
1,290.000	5.59	5.59	5.60	5.60	5.60
1,305.000	5.61	5.61	5.61	5.61	5.62
1,320.000	5.62	5.62	5.63	5.63	5.63
1,335.000	5.63	5.63	5.64	5.64	5.64
1,350.000	5.64	5.64	5.65	5.65	5.65
1,365.000	5.65	5.65	5.66	5.66	5.66
1,380.000	5.66	5.66	5.66	5.66	5.67
1,395.000	5.67	5.67	5.67	5.67	5.67
1,410.000	5.67	5.68	5.68	5.68	5.68
1,425.000	5.68	5.68	5.68	5.68	5.68
1,440.000	5.68	(N/A)	(N/A)	(N/A)	(N/A)

## UHS Rancho Springs 10-yr, 1 hr Detention Analysis

Subsection: Time vs. Volume

Label: Onsite Detention Basin

### Time vs. Volume (ac-ft)

Output Time increment = 3.000 min

Time on left represents time for first value in each row.

Time (min)	Volume (ac-ft)	Volume (ac-ft)	Volume (ac-ft)	Volume (ac-ft)	Volume (ac-ft)
0.000	0.000	0.001	0.005	0.019	0.029
15.000	0.041	0.054	0.070	0.084	0.099
30.000	0.116	0.136	0.154	0.176	0.201
45.000	0.231	0.267	0.307	0.342	0.371
60.000	0.393	0.408	0.419	0.426	0.431
75.000	0.434	0.437	0.439	0.440	0.441
90.000	0.441	0.442	0.442	0.442	0.441
105.000	0.441	0.440	0.440	0.439	0.439
120.000	0.440	0.441	0.442	0.443	0.444
135.000	0.445	0.446	0.448	0.449	0.450
150.000	0.451	0.452	0.453	0.455	0.456
165.000	0.457	0.458	0.459	0.460	0.461
180.000	0.463	0.464	0.465	0.466	0.467
195.000	0.468	0.469	0.471	0.472	0.473
210.000	0.474	0.475	0.476	0.477	0.478
225.000	0.479	0.481	0.482	0.483	0.484
240.000	0.485	0.486	0.487	0.488	0.489
255.000	0.491	0.492	0.493	0.494	0.495
270.000	0.496	0.497	0.498	0.500	0.501
285.000	0.502	0.503	0.504	0.505	0.506
300.000	0.507	0.508	0.510	0.511	0.512
315.000	0.513	0.514	0.515	0.516	0.517
330.000	0.518	0.519	0.521	0.522	0.523
345.000	0.524	0.525	0.526	0.527	0.528
360.000	0.529	0.531	0.532	0.533	0.534
375.000	0.535	0.536	0.537	0.538	0.539
390.000	0.540	0.542	0.543	0.544	0.545
405.000	0.546	0.547	0.548	0.549	0.550
420.000	0.551	0.552	0.554	0.555	0.556
435.000	0.557	0.558	0.559	0.560	0.561
450.000	0.562	0.563	0.564	0.566	0.567
465.000	0.568	0.569	0.570	0.571	0.572
480.000	0.573	0.574	0.575	0.576	0.577
495.000	0.578	0.580	0.581	0.582	0.583
510.000	0.584	0.585	0.586	0.587	0.588
525.000	0.589	0.590	0.591	0.592	0.594
540.000	0.595	0.596	0.597	0.598	0.599
555.000	0.600	0.601	0.602	0.603	0.604
570.000	0.605	0.606	0.607	0.608	0.610
585.000	0.611	0.612	0.613	0.614	0.615
600.000	0.616	0.617	0.618	0.619	0.620

## UHS Rancho Springs 10-yr, 1 hr Detention Analysis

Subsection: Time vs. Volume

Label: Onsite Detention Basin

### Time vs. Volume (ac-ft)

Output Time increment = 3.000 min

Time on left represents time for first value in each row.

Time (min)	Volume (ac-ft)	Volume (ac-ft)	Volume (ac-ft)	Volume (ac-ft)	Volume (ac-ft)
615.000	0.621	0.622	0.623	0.624	0.625
630.000	0.626	0.628	0.629	0.630	0.631
645.000	0.632	0.633	0.634	0.635	0.636
660.000	0.637	0.638	0.639	0.640	0.641
675.000	0.642	0.643	0.644	0.645	0.646
690.000	0.647	0.649	0.650	0.651	0.652
705.000	0.653	0.654	0.655	0.656	0.657
720.000	0.658	0.659	0.660	0.661	0.662
735.000	0.663	0.664	0.665	0.666	0.667
750.000	0.668	0.669	0.671	0.672	0.673
765.000	0.674	0.675	0.676	0.677	0.678
780.000	0.679	0.680	0.681	0.682	0.683
795.000	0.684	0.685	0.686	0.687	0.688
810.000	0.689	0.690	0.691	0.692	0.693
825.000	0.694	0.695	0.696	0.697	0.698
840.000	0.699	0.700	0.701	0.703	0.704
855.000	0.705	0.706	0.707	0.708	0.709
870.000	0.710	0.711	0.712	0.713	0.714
885.000	0.715	0.716	0.717	0.718	0.719
900.000	0.720	0.721	0.722	0.723	0.724
915.000	0.725	0.726	0.727	0.728	0.729
930.000	0.730	0.731	0.732	0.733	0.734
945.000	0.735	0.736	0.737	0.738	0.739
960.000	0.740	0.741	0.742	0.743	0.744
975.000	0.745	0.746	0.747	0.748	0.749
990.000	0.750	0.751	0.752	0.753	0.754
1,005.000	0.755	0.756	0.757	0.758	0.759
1,020.000	0.760	0.761	0.762	0.763	0.764
1,035.000	0.765	0.766	0.767	0.768	0.769
1,050.000	0.770	0.771	0.772	0.773	0.774
1,065.000	0.775	0.776	0.777	0.778	0.779
1,080.000	0.780	0.781	0.782	0.783	0.784
1,095.000	0.785	0.786	0.787	0.788	0.789
1,110.000	0.790	0.791	0.792	0.793	0.794
1,125.000	0.795	0.796	0.797	0.798	0.799
1,140.000	0.800	0.801	0.802	0.803	0.804
1,155.000	0.805	0.806	0.807	0.808	0.809
1,170.000	0.810	0.811	0.812	0.813	0.813
1,185.000	0.814	0.815	0.816	0.817	0.818
1,200.000	0.819	0.820	0.821	0.822	0.823
1,215.000	0.824	0.825	0.826	0.827	0.828

## UHS Rancho Springs 10-yr, 1 hr Detention Analysis

Subsection: Time vs. Volume

Label: Onsite Detention Basin

### Time vs. Volume (ac-ft)

Output Time increment = 3.000 min

Time on left represents time for first value in each row.

Time (min)	Volume (ac-ft)	Volume (ac-ft)	Volume (ac-ft)	Volume (ac-ft)	Volume (ac-ft)
1,230.000	0.829	0.830	0.831	0.832	0.833
1,245.000	0.833	0.834	0.835	0.836	0.837
1,260.000	0.837	0.838	0.839	0.840	0.840
1,275.000	0.841	0.842	0.842	0.843	0.844
1,290.000	0.844	0.845	0.845	0.846	0.846
1,305.000	0.847	0.847	0.848	0.848	0.849
1,320.000	0.849	0.850	0.850	0.850	0.851
1,335.000	0.851	0.852	0.852	0.852	0.853
1,350.000	0.853	0.853	0.854	0.854	0.854
1,365.000	0.855	0.855	0.855	0.855	0.856
1,380.000	0.856	0.856	0.856	0.857	0.857
1,395.000	0.857	0.857	0.858	0.858	0.858
1,410.000	0.858	0.858	0.859	0.859	0.859
1,425.000	0.859	0.859	0.860	0.860	0.860
1,440.000	0.860	(N/A)	(N/A)	(N/A)	(N/A)

## UHS Rancho Springs 10-yr, 1 hr Detention Analysis

Subsection: Pipe Volume

Label: Onsite Detention Basin

### Volume Results (Pipe)

Pipe Storage Upstream Invert	0.20 ft
Pipe Storage Downstream Invert	0.00 ft
Pipe Storage Length	200.00 ft
Pipe Storage Diameter	96.0 in
Pipe Storage Number of Barrels	5
Pipe Storage Slice Width	1.00 ft
Pipe Storage Vertical Increment	0.20 ft

Elevation (ft)	Perpendicular Downstream Depth (ft)	Perpendicular Downstream Area (ft²)	Wetted Length (ft)	Filled Length (ft)	Perpendicular Upstream Depth (ft)	Perpendicular Upstream Area (ft²)	Total Volume (ac-ft)
0.00	0.00	0.0	0.00	0.00	0.00	0.0	0.000
0.20	0.20	0.3	200.00	0.00	0.00	0.0	0.003
0.40	0.40	0.9	200.00	0.00	0.20	0.3	0.014
0.60	0.60	1.7	200.00	0.00	0.40	0.9	0.030
0.80	0.80	2.6	200.00	0.00	0.60	1.7	0.049
1.00	1.00	3.6	200.00	0.00	0.80	2.6	0.071
1.20	1.20	4.7	200.00	0.00	1.00	3.6	0.096
1.40	1.40	5.9	200.00	0.00	1.20	4.7	0.122
1.60	1.60	7.2	200.00	0.00	1.40	5.9	0.150
1.80	1.80	8.5	200.00	0.00	1.60	7.2	0.179
2.00	2.00	9.8	200.00	0.00	1.80	8.5	0.210
2.20	2.20	11.2	200.00	0.00	2.00	9.8	0.242
2.40	2.40	12.7	200.00	0.00	2.20	11.2	0.274
2.60	2.60	14.2	200.00	0.00	2.40	12.7	0.308
2.80	2.80	15.7	200.00	0.00	2.60	14.2	0.343
3.00	3.00	17.2	200.00	0.00	2.80	15.7	0.378
3.20	3.20	18.8	200.00	0.00	3.00	17.2	0.413
3.40	3.40	20.3	200.00	0.00	3.20	18.8	0.449
3.60	3.60	21.9	200.00	0.00	3.40	20.4	0.485
3.80	3.80	23.5	200.00	0.00	3.60	21.9	0.522
4.00	4.00	25.1	200.00	0.00	3.80	23.5	0.559
4.20	4.20	26.7	200.00	0.00	4.00	25.1	0.595
4.40	4.40	28.3	200.00	0.00	4.20	26.7	0.632
4.60	4.60	29.9	200.00	0.00	4.40	28.3	0.669
4.80	4.80	31.5	200.00	0.00	4.60	29.9	0.705
5.00	5.00	33.0	200.00	0.00	4.80	31.5	0.741
5.20	5.20	34.6	200.00	0.00	5.00	33.0	0.776
5.40	5.40	36.1	200.00	0.00	5.20	34.6	0.811
5.60	5.60	37.6	200.00	0.00	5.40	36.1	0.846
5.80	5.80	39.0	200.00	0.00	5.60	37.6	0.879
6.00	6.00	40.4	200.00	0.00	5.80	39.0	0.912

## UHS Rancho Springs 10-yr, 1 hr Detention Analysis

Subsection: Pipe Volume

Label: Onsite Detention Basin

Elevation (ft)	Perpendicular Downstream Depth (ft)	Perpendicular Downstream Area (ft <sup>2</sup> )	Wetted Length (ft)	Filled Length (ft)	Perpendicular Upstream Depth (ft)	Perpendicular Upstream Area (ft <sup>2</sup> )	Total Volume (ac-ft)
6.20	6.20	41.8	200.00	0.00	6.00	40.4	0.944
6.40	6.40	43.1	200.00	0.00	6.20	41.8	0.975
6.60	6.60	44.4	200.00	0.00	6.40	43.1	1.004
6.80	6.80	45.5	200.00	0.00	6.60	44.4	1.032
7.00	7.00	46.6	200.00	0.00	6.80	45.5	1.058
7.20	7.20	47.6	200.00	0.00	7.00	46.6	1.082
7.40	7.40	48.5	200.00	0.00	7.20	47.6	1.104
7.60	7.60	49.3	200.00	0.00	7.40	48.6	1.124
7.80	7.80	49.9	200.00	0.00	7.60	49.3	1.140
8.00	8.00	50.3	200.00	0.00	7.80	49.9	1.151
8.20	8.00	50.3	200.00	200.00	8.00	50.3	1.154



## UHS Rancho Springs 10-yr, 1 hr Detention Analysis

Subsection: Outlet Input Data

Label: Composite Outlet Structure - 1

Requested Pond Water Surface Elevations	
Minimum (Headwater)	0.00 ft
Increment (Headwater)	0.50 ft
Maximum (Headwater)	8.20 ft

### Outlet Connectivity

Structure Type	Outlet ID	Direction	Outfall	E1 (ft)	E2 (ft)
Stand Pipe	Riser - 1	Forward	TW	7.00	8.20
Orifice-Circular	Orifice - 1	Forward	TW	0.00	8.20
Rectangular Weir	Notch Weir	Forward	TW	5.50	8.20
Tailwater Settings	Tailwater			(N/A)	(N/A)

## UHS Rancho Springs 10-yr, 1 hr Detention Analysis

Subsection: Outlet Input Data

Label: Composite Outlet Structure - 1

Structure ID: Orifice - 1	
Structure Type: Orifice-Circular	
Number of Openings	1
Elevation	0.00 ft
Orifice Diameter	1.8 in
Orifice Coefficient	0.600
Structure ID: Notch Weir	
Structure Type: Rectangular Weir	
Number of Openings	1
Elevation	5.50 ft
Weir Length	0.50 ft
Weir Coefficient	3.00 (ft <sup>0.5</sup> )/s
Structure ID: Riser - 1	
Structure Type: Stand Pipe	
Number of Openings	1
Elevation	0.00 ft
Diameter	54.0 in
Orifice Area	15.9 ft <sup>2</sup>
Orifice Coefficient	0.600
Weir Length	14.14 ft
Weir Coefficient	3.00 (ft <sup>0.5</sup> )/s
K Reverse	1.000
Manning's n	0.000
Kev, Charged Riser	0.000
Weir Submergence	False
Orifice H to crest	True
Structure ID: TW	
Structure Type: TW Setup, DS Channel	
Tailwater Type	Free Outfall
Convergence Tolerances	
Maximum Iterations	30
Tailwater Tolerance (Minimum)	0.01 ft
Tailwater Tolerance (Maximum)	0.50 ft
Headwater Tolerance (Minimum)	0.01 ft
Headwater Tolerance (Maximum)	0.50 ft

## **UHS Rancho Springs 10-yr, 1 hr Detention Analysis**

Subsection: Outlet Input Data

Label: Composite Outlet Structure - 1

Convergence Tolerances	
Flow Tolerance (Minimum)	0.001 ft <sup>3</sup> /s
Flow Tolerance (Maximum)	10.000 ft <sup>3</sup> /s

## UHS Rancho Springs 10-yr, 1 hr Detention Analysis

Subsection: Individual Outlet Curves

Label: Composite Outlet Structure - 1

### RATING TABLE FOR ONE OUTLET TYPE

Structure ID = ()

-----

Upstream ID =

Downstream ID =

Water Surface Elevation (ft)	Flow (ft <sup>3</sup> /s)	Tailwater Elevation (ft)	Convergence Error (ft)
Contributing Structures			

## UHS Rancho Springs 10-yr, 1 hr Detention Analysis

Subsection: Individual Outlet Curves

Label: Composite Outlet Structure - 1

### RATING TABLE FOR ONE OUTLET TYPE

Structure ID = ()

-----

Upstream ID =

Downstream ID =

Water Surface Elevation (ft)	Flow (ft <sup>3</sup> /s)	Tailwater Elevation (ft)	Convergence Error (ft)
Contributing Structures			

## UHS Rancho Springs 10-yr, 1 hr Detention Analysis

Subsection: Individual Outlet Curves

Label: Composite Outlet Structure - 1

### RATING TABLE FOR ONE OUTLET TYPE

Structure ID = ()

-----

Upstream ID =

Downstream ID =

Water Surface Elevation (ft)	Flow (ft <sup>3</sup> /s)	Tailwater Elevation (ft)	Convergence Error (ft)
Contributing Structures			

## UHS Rancho Springs 10-yr, 1 hr Detention Analysis

Subsection: Composite Rating Curve

Label: Composite Outlet Structure - 1

### Composite Outflow Summary

Water Surface Elevation (ft)	Flow (ft <sup>3</sup> /s)	Tailwater Elevation (ft)	Convergence Error (ft)
0.00	0.00	(N/A)	0.00
0.50	0.05	(N/A)	0.00
1.00	0.08	(N/A)	0.00
1.50	0.10	(N/A)	0.00
2.00	0.11	(N/A)	0.00
2.50	0.13	(N/A)	0.00
3.00	0.14	(N/A)	0.00
3.50	0.15	(N/A)	0.00
4.00	0.16	(N/A)	0.00
4.50	0.17	(N/A)	0.00
5.00	0.18	(N/A)	0.00
5.50	0.19	(N/A)	0.00
6.00	0.73	(N/A)	0.00
6.50	1.70	(N/A)	0.00
7.00	205.49	(N/A)	0.00
7.50	214.10	(N/A)	0.00
8.00	222.67	(N/A)	0.00
8.20	226.08	(N/A)	0.00

### Contributing Structures

None Contributing

Orifice - 1

Orifice - 1

Orifice - 1

Orifice - 1

Orifice - 1

Orifice - 1

Orifice - 1

Orifice - 1

Orifice - 1

Orifice - 1

Orifice - 1 + Notch Weir

Orifice - 1 + Notch Weir

Orifice - 1 + Notch Weir

Riser - 1 + Orifice - 1 +  
Notch Weir

Riser - 1 + Orifice - 1 +  
Notch Weir

Riser - 1 + Orifice - 1 +  
Notch Weir

Riser - 1 + Orifice - 1 +  
Notch Weir

## UHS Rancho Springs 10-yr, 1 hr Detention Analysis

Subsection: Elevation-Volume-Flow Table (Pond)

Label: Onsite Detention Basin

Infiltration	
Infiltration Method (Computed)	No Infiltration
Initial Conditions	
Elevation (Water Surface, Initial)	0.00 ft
Volume (Initial)	0.000 ac-ft
Flow (Initial Outlet)	0.00 ft <sup>3</sup> /s
Flow (Initial Infiltration)	0.00 ft <sup>3</sup> /s
Flow (Initial, Total)	0.00 ft <sup>3</sup> /s
Time Increment	3.000 min

Elevation (ft)	Outflow (ft <sup>3</sup> /s)	Storage (ac-ft)	Area (ft <sup>2</sup> )	Infiltration (ft <sup>3</sup> /s)	Flow (Total) (ft <sup>3</sup> /s)	2S/t + O (ft <sup>3</sup> /s)
0.00	0.00	0.000	0	0.00	0.00	0.00
0.50	0.05	0.022	0	0.00	0.05	10.80
1.00	0.08	0.071	0	0.00	0.08	34.67
1.50	0.10	0.136	0	0.00	0.10	65.87
2.00	0.11	0.210	0	0.00	0.11	101.69
2.50	0.13	0.291	0	0.00	0.13	141.11
3.00	0.14	0.378	0	0.00	0.14	182.87
3.50	0.15	0.467	0	0.00	0.15	226.29
4.00	0.16	0.559	0	0.00	0.16	270.53
4.50	0.17	0.650	0	0.00	0.17	314.90
5.00	0.18	0.741	0	0.00	0.18	358.74
5.50	0.19	0.829	0	0.00	0.19	401.24
6.00	0.73	0.912	0	0.00	0.73	442.26
6.50	1.70	0.989	0	0.00	1.70	480.58
7.00	205.49	1.058	0	0.00	205.49	717.66
7.50	214.10	1.114	0	0.00	214.10	753.33
8.00	222.67	1.151	0	0.00	222.67	779.68
8.20	226.08	1.154	0	0.00	226.08	784.58



## UHS Rancho Springs 10-yr, 1 hr Detention Analysis

Subsection: Level Pool Pond Routing Summary

Label: Onsite Detention Basin (IN)

Infiltration			
Infiltration Method (Computed)		No Infiltration	
Initial Conditions			
Elevation (Water Surface, Initial)		0.00 ft	
Volume (Initial)		0.000 ac-ft	
Flow (Initial Outlet)		0.00 ft³/s	
Flow (Initial Infiltration)		0.00 ft³/s	
Flow (Initial, Total)		0.00 ft³/s	
Time Increment		3.000 min	
Inflow/Outflow Hydrograph Summary			
Flow (Peak In)		9.80 ft³/s	Time to Peak (Flow, In)
Flow (Peak Outlet)		0.39 ft³/s	Time to Peak (Flow, Outlet)
			51.000 min
			1,440.000 min
Peak Conditions			
Elevation (Water Surface, Peak)		5.68 ft	
Volume (Peak)		0.860 ac-ft	
Mass Balance (ac-ft)			
Volume (Initial)		0.000 ac-ft	
Volume (Total Inflow)		1.226 ac-ft	
Volume (Total Infiltration)		0.000 ac-ft	
Volume (Total Outlet Outflow)		0.367 ac-ft	
Volume (Retained)		0.858 ac-ft	
Volume (Unrouted)		-0.001 ac-ft	
Error (Mass Balance)		0.1 %	

## UHS Rancho Springs 10-yr, 1 hr Detention Analysis

Subsection: Pond Routed Hydrograph (total out)

Label: Onsite Detention Basin (OUT)

Peak Discharge	0.39 ft <sup>3</sup> /s
Time to Peak	1,440.000 min
Hydrograph Volume	0.367 ac-ft

### HYDROGRAPH ORDINATES (ft<sup>3</sup>/s)

Output Time Increment = 3.000 min

Time on left represents time for first value in each row.

Time (min)	Flow (ft <sup>3</sup> /s)	Flow (ft <sup>3</sup> /s)	Flow (ft <sup>3</sup> /s)	Flow (ft <sup>3</sup> /s)	Flow (ft <sup>3</sup> /s)
0.000	0.00	0.01	0.03	0.05	0.06
15.000	0.06	0.07	0.08	0.08	0.09
30.000	0.09	0.10	0.10	0.10	0.11
45.000	0.12	0.12	0.13	0.13	0.14
60.000	0.14	0.14	0.14	0.14	0.14
75.000	0.14	0.15	0.15	0.15	0.15
90.000	0.15	0.15	0.15	0.15	0.15
105.000	0.15	0.15	0.15	0.15	0.15
120.000	0.15	0.15	0.15	0.15	0.15
135.000	0.15	0.15	0.15	0.15	0.15
150.000	0.15	0.15	0.15	0.15	0.15
165.000	0.15	0.15	0.15	0.15	0.15
180.000	0.15	0.15	0.15	0.15	0.15
195.000	0.15	0.15	0.15	0.15	0.15
210.000	0.15	0.15	0.15	0.15	0.15
225.000	0.15	0.15	0.15	0.15	0.15
240.000	0.15	0.15	0.15	0.15	0.15
255.000	0.15	0.15	0.15	0.15	0.15
270.000	0.15	0.15	0.15	0.15	0.15
285.000	0.15	0.15	0.15	0.15	0.15
300.000	0.15	0.15	0.15	0.15	0.15
315.000	0.15	0.15	0.15	0.15	0.15
330.000	0.15	0.15	0.15	0.16	0.16
345.000	0.16	0.16	0.16	0.16	0.16
360.000	0.16	0.16	0.16	0.16	0.16
375.000	0.16	0.16	0.16	0.16	0.16
390.000	0.16	0.16	0.16	0.16	0.16
405.000	0.16	0.16	0.16	0.16	0.16
420.000	0.16	0.16	0.16	0.16	0.16
435.000	0.16	0.16	0.16	0.16	0.16
450.000	0.16	0.16	0.16	0.16	0.16
465.000	0.16	0.16	0.16	0.16	0.16
480.000	0.16	0.16	0.16	0.16	0.16
495.000	0.16	0.16	0.16	0.16	0.16
510.000	0.16	0.16	0.16	0.16	0.16
525.000	0.16	0.16	0.16	0.16	0.16
540.000	0.16	0.16	0.16	0.16	0.16

## UHS Rancho Springs 10-yr, 1 hr Detention Analysis

Subsection: Pond Routed Hydrograph (total out)

Label: Onsite Detention Basin (OUT)

### HYDROGRAPH ORDINATES (ft<sup>3</sup>/s)

Output Time Increment = 3.000 min

Time on left represents time for first value in each row.

Time (min)	Flow (ft <sup>3</sup> /s)	Flow (ft <sup>3</sup> /s)	Flow (ft <sup>3</sup> /s)	Flow (ft <sup>3</sup> /s)	Flow (ft <sup>3</sup> /s)
555.000	0.16	0.16	0.16	0.16	0.16
570.000	0.16	0.16	0.16	0.16	0.16
585.000	0.16	0.17	0.17	0.17	0.17
600.000	0.17	0.17	0.17	0.17	0.17
615.000	0.17	0.17	0.17	0.17	0.17
630.000	0.17	0.17	0.17	0.17	0.17
645.000	0.17	0.17	0.17	0.17	0.17
660.000	0.17	0.17	0.17	0.17	0.17
675.000	0.17	0.17	0.17	0.17	0.17
690.000	0.17	0.17	0.17	0.17	0.17
705.000	0.17	0.17	0.17	0.17	0.17
720.000	0.17	0.17	0.17	0.17	0.17
735.000	0.17	0.17	0.17	0.17	0.17
750.000	0.17	0.17	0.17	0.17	0.17
765.000	0.17	0.17	0.17	0.17	0.17
780.000	0.17	0.17	0.17	0.17	0.17
795.000	0.17	0.17	0.17	0.17	0.17
810.000	0.17	0.17	0.17	0.17	0.17
825.000	0.17	0.17	0.17	0.17	0.17
840.000	0.17	0.17	0.17	0.17	0.17
855.000	0.17	0.17	0.17	0.18	0.18
870.000	0.18	0.18	0.18	0.18	0.18
885.000	0.18	0.18	0.18	0.18	0.18
900.000	0.18	0.18	0.18	0.18	0.18
915.000	0.18	0.18	0.18	0.18	0.18
930.000	0.18	0.18	0.18	0.18	0.18
945.000	0.18	0.18	0.18	0.18	0.18
960.000	0.18	0.18	0.18	0.18	0.18
975.000	0.18	0.18	0.18	0.18	0.18
990.000	0.18	0.18	0.18	0.18	0.18
1,005.000	0.18	0.18	0.18	0.18	0.18
1,020.000	0.18	0.18	0.18	0.18	0.18
1,035.000	0.18	0.18	0.18	0.18	0.18
1,050.000	0.18	0.18	0.18	0.18	0.18
1,065.000	0.18	0.18	0.18	0.18	0.18
1,080.000	0.18	0.18	0.18	0.18	0.18
1,095.000	0.18	0.18	0.18	0.18	0.18
1,110.000	0.18	0.18	0.18	0.18	0.18
1,125.000	0.18	0.18	0.18	0.18	0.18
1,140.000	0.18	0.18	0.18	0.18	0.18
1,155.000	0.18	0.18	0.19	0.19	0.19
1,170.000	0.19	0.19	0.19	0.19	0.19

## UHS Rancho Springs 10-yr, 1 hr Detention Analysis

Subsection: Pond Routed Hydrograph (total out)

Label: Onsite Detention Basin (OUT)

### HYDROGRAPH ORDINATES (ft<sup>3</sup>/s)

Output Time Increment = 3.000 min

Time on left represents time for first value in each row.

Time (min)	Flow (ft <sup>3</sup> /s)	Flow (ft <sup>3</sup> /s)	Flow (ft <sup>3</sup> /s)	Flow (ft <sup>3</sup> /s)	Flow (ft <sup>3</sup> /s)
1,185.000	0.19	0.19	0.19	0.19	0.19
1,200.000	0.19	0.19	0.19	0.19	0.19
1,215.000	0.19	0.19	0.19	0.19	0.19
1,230.000	0.19	0.19	0.20	0.21	0.21
1,245.000	0.22	0.22	0.23	0.23	0.24
1,260.000	0.24	0.25	0.25	0.26	0.26
1,275.000	0.27	0.27	0.27	0.28	0.28
1,290.000	0.28	0.29	0.29	0.30	0.30
1,305.000	0.30	0.30	0.31	0.31	0.31
1,320.000	0.32	0.32	0.32	0.32	0.33
1,335.000	0.33	0.33	0.33	0.34	0.34
1,350.000	0.34	0.34	0.35	0.35	0.35
1,365.000	0.35	0.35	0.36	0.36	0.36
1,380.000	0.36	0.36	0.36	0.36	0.37
1,395.000	0.37	0.37	0.37	0.37	0.37
1,410.000	0.37	0.38	0.38	0.38	0.38
1,425.000	0.38	0.38	0.38	0.38	0.38
1,440.000	0.39	(N/A)	(N/A)	(N/A)	(N/A)

## UHS Rancho Springs 10-yr, 1 hr Detention Analysis

Subsection: Pond Inflow Summary

Label: Onsite Detention Basin (IN)

### Summary for Hydrograph Addition at 'Onsite Detention Basin'

Upstream Link	Upstream Node
<Catchment to Outflow Node>	Unit Hydrograph (Onsite Runoff)

### Node Inflows

Inflow Type	Element	Volume (ac-ft)	Time to Peak (min)	Flow (Peak) (ft <sup>3</sup> /s)
Flow (From)	Unit Hydrograph (Onsite Runoff)	0.459	50.000	10.48
Flow (In)	Onsite Detention Basin	1.226	51.000	9.80

## UHS Rancho Springs 10-yr, 1 hr Detention Analysis

Subsection: Diverted Hydrograph

Label: Outlet-1

Peak Discharge	0.39 ft <sup>3</sup> /s
Time to Peak	1,440.000 min
Hydrograph Volume	0.367 ac-ft

### HYDROGRAPH ORDINATES (ft<sup>3</sup>/s)

Output Time Increment = 3.000 min

Time on left represents time for first value in each row.

Time (min)	Flow (ft <sup>3</sup> /s)	Flow (ft <sup>3</sup> /s)	Flow (ft <sup>3</sup> /s)	Flow (ft <sup>3</sup> /s)	Flow (ft <sup>3</sup> /s)
0.000	0.00	0.01	0.03	0.05	0.06
15.000	0.06	0.07	0.08	0.08	0.09
30.000	0.09	0.10	0.10	0.10	0.11
45.000	0.12	0.12	0.13	0.13	0.14
60.000	0.14	0.14	0.14	0.14	0.14
75.000	0.14	0.15	0.15	0.15	0.15
90.000	0.15	0.15	0.15	0.15	0.15
105.000	0.15	0.15	0.15	0.15	0.15
120.000	0.15	0.15	0.15	0.15	0.15
135.000	0.15	0.15	0.15	0.15	0.15
150.000	0.15	0.15	0.15	0.15	0.15
165.000	0.15	0.15	0.15	0.15	0.15
180.000	0.15	0.15	0.15	0.15	0.15
195.000	0.15	0.15	0.15	0.15	0.15
210.000	0.15	0.15	0.15	0.15	0.15
225.000	0.15	0.15	0.15	0.15	0.15
240.000	0.15	0.15	0.15	0.15	0.15
255.000	0.15	0.15	0.15	0.15	0.15
270.000	0.15	0.15	0.15	0.15	0.15
285.000	0.15	0.15	0.15	0.15	0.15
300.000	0.15	0.15	0.15	0.15	0.15
315.000	0.15	0.15	0.15	0.15	0.15
330.000	0.15	0.15	0.15	0.16	0.16
345.000	0.16	0.16	0.16	0.16	0.16
360.000	0.16	0.16	0.16	0.16	0.16
375.000	0.16	0.16	0.16	0.16	0.16
390.000	0.16	0.16	0.16	0.16	0.16
405.000	0.16	0.16	0.16	0.16	0.16
420.000	0.16	0.16	0.16	0.16	0.16
435.000	0.16	0.16	0.16	0.16	0.16
450.000	0.16	0.16	0.16	0.16	0.16
465.000	0.16	0.16	0.16	0.16	0.16
480.000	0.16	0.16	0.16	0.16	0.16
495.000	0.16	0.16	0.16	0.16	0.16
510.000	0.16	0.16	0.16	0.16	0.16
525.000	0.16	0.16	0.16	0.16	0.16
540.000	0.16	0.16	0.16	0.16	0.16

## UHS Rancho Springs 10-yr, 1 hr Detention Analysis

Subsection: Diverted Hydrograph

Label: Outlet-1

### HYDROGRAPH ORDINATES (ft<sup>3</sup>/s)

Output Time Increment = 3.000 min

Time on left represents time for first value in each row.

Time (min)	Flow (ft <sup>3</sup> /s)	Flow (ft <sup>3</sup> /s)	Flow (ft <sup>3</sup> /s)	Flow (ft <sup>3</sup> /s)	Flow (ft <sup>3</sup> /s)
555.000	0.16	0.16	0.16	0.16	0.16
570.000	0.16	0.16	0.16	0.16	0.16
585.000	0.16	0.17	0.17	0.17	0.17
600.000	0.17	0.17	0.17	0.17	0.17
615.000	0.17	0.17	0.17	0.17	0.17
630.000	0.17	0.17	0.17	0.17	0.17
645.000	0.17	0.17	0.17	0.17	0.17
660.000	0.17	0.17	0.17	0.17	0.17
675.000	0.17	0.17	0.17	0.17	0.17
690.000	0.17	0.17	0.17	0.17	0.17
705.000	0.17	0.17	0.17	0.17	0.17
720.000	0.17	0.17	0.17	0.17	0.17
735.000	0.17	0.17	0.17	0.17	0.17
750.000	0.17	0.17	0.17	0.17	0.17
765.000	0.17	0.17	0.17	0.17	0.17
780.000	0.17	0.17	0.17	0.17	0.17
795.000	0.17	0.17	0.17	0.17	0.17
810.000	0.17	0.17	0.17	0.17	0.17
825.000	0.17	0.17	0.17	0.17	0.17
840.000	0.17	0.17	0.17	0.17	0.17
855.000	0.17	0.17	0.17	0.18	0.18
870.000	0.18	0.18	0.18	0.18	0.18
885.000	0.18	0.18	0.18	0.18	0.18
900.000	0.18	0.18	0.18	0.18	0.18
915.000	0.18	0.18	0.18	0.18	0.18
930.000	0.18	0.18	0.18	0.18	0.18
945.000	0.18	0.18	0.18	0.18	0.18
960.000	0.18	0.18	0.18	0.18	0.18
975.000	0.18	0.18	0.18	0.18	0.18
990.000	0.18	0.18	0.18	0.18	0.18
1,005.000	0.18	0.18	0.18	0.18	0.18
1,020.000	0.18	0.18	0.18	0.18	0.18
1,035.000	0.18	0.18	0.18	0.18	0.18
1,050.000	0.18	0.18	0.18	0.18	0.18
1,065.000	0.18	0.18	0.18	0.18	0.18
1,080.000	0.18	0.18	0.18	0.18	0.18
1,095.000	0.18	0.18	0.18	0.18	0.18
1,110.000	0.18	0.18	0.18	0.18	0.18
1,125.000	0.18	0.18	0.18	0.18	0.18
1,140.000	0.18	0.18	0.18	0.18	0.18
1,155.000	0.18	0.18	0.19	0.19	0.19
1,170.000	0.19	0.19	0.19	0.19	0.19

## UHS Rancho Springs 10-yr, 1 hr Detention Analysis

Subsection: Diverted Hydrograph

Label: Outlet-1

### HYDROGRAPH ORDINATES (ft<sup>3</sup>/s)

Output Time Increment = 3.000 min

Time on left represents time for first value in each row.

Time (min)	Flow (ft <sup>3</sup> /s)	Flow (ft <sup>3</sup> /s)	Flow (ft <sup>3</sup> /s)	Flow (ft <sup>3</sup> /s)	Flow (ft <sup>3</sup> /s)
1,185.000	0.19	0.19	0.19	0.19	0.19
1,200.000	0.19	0.19	0.19	0.19	0.19
1,215.000	0.19	0.19	0.19	0.19	0.19
1,230.000	0.19	0.19	0.20	0.21	0.21
1,245.000	0.22	0.22	0.23	0.23	0.24
1,260.000	0.24	0.25	0.25	0.26	0.26
1,275.000	0.27	0.27	0.27	0.28	0.28
1,290.000	0.28	0.29	0.29	0.30	0.30
1,305.000	0.30	0.30	0.31	0.31	0.31
1,320.000	0.32	0.32	0.32	0.32	0.33
1,335.000	0.33	0.33	0.33	0.34	0.34
1,350.000	0.34	0.34	0.35	0.35	0.35
1,365.000	0.35	0.35	0.36	0.36	0.36
1,380.000	0.36	0.36	0.36	0.36	0.37
1,395.000	0.37	0.37	0.37	0.37	0.37
1,410.000	0.37	0.38	0.38	0.38	0.38
1,425.000	0.38	0.38	0.38	0.38	0.38
1,440.000	0.39	(N/A)	(N/A)	(N/A)	(N/A)



# **UHS Rancho Springs 10-yr, 1 hr Detention Analysis**

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\*\*\*\*\*

## F L O O D     R O U T I N G     A N A L Y S I S

ACCORDING TO RIVERSIDE COUNTY FLOOD CONTROL AND WATER CONSERVATION DISTRICT  
 (RCFC&WCD) 1978 HYDROLOGY MANUAL  
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 (Synthetic Unit Hydrograph Version 18.0)  
 Release Date: 05/01/2011 License ID 1499

Analysis prepared by:

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## \*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*

\* UHS Rancho Springs Unit Hydrograph \*  
 \* Proposed Conditions, 100-yr, 24-hr \*  
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FILE NAME: RS\_UNIT.DAT  
 TIME/DATE OF STUDY: 12:57 05/12/2020

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FLOW PROCESS FROM NODE 100.00 TO NODE 101.00 IS CODE = 1

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>>>>SUBAREA RUNOFF (UNIT-HYDROGRAPH ANALYSIS)<<<<

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(UNIT-HYDROGRAPH ADDED TO STREAM #1)

WATERSHED AREA = 5.900 ACRES

BASEFLOW = 0.000 CFS/SQUARE-MILE

Warning: Watershed Area is less than 10 acres

\*USER ENTERED "LAG" TIME = 0.100 HOURS

CAUTION: LAG TIME IS LESS THAN 0.50 HOURS.

THE 5-MINUTE PERIOD UH MODEL (USED IN THIS COMPUTER PROGRAM)

MAY BE TOO LARGE FOR PEAK FLOW ESTIMATES.

VALLEY S-GRAPH SELECTED

UNIFORM MEAN SOIL-LOSS(INCH/HOUR) = 0.050

LOW SOIL-LOSS RATE PERCENT(DECIMAL) = 0.500

MINIMUM SOIL-LOSS RATE(INCH/HOUR) = 0.010

USER-ENTERED RAINFALL = 6.90 INCHES

RCFC&WCD 24-Hour Storm (15-Minute period) SELECTED

\*USER SPECIFIED PRECIPITATION DEPTH-AREA ADJUSTMENT FACTOR = 0.9990

UNIT HYDROGRAPH TIME UNIT = 15.000 MINUTES

UNIT INTERVAL PERCENTAGE OF LAG-TIME = 250.000

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## UNIT HYDROGRAPH DETERMINATION

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INTERVAL NUMBER	"S" GRAPH MEAN VALUES	UNIT HYDROGRAPH ORDINATES(CFS)
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1	50.817	12.086
2	90.903	9.534
3	97.798	1.640
4	99.444	0.392
5	99.778	0.079
6	99.944	0.040
7	100.000	0.013

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UNIT PERIOD (NUMBER)	UNIT RAINFALL (INCHES)	UNIT SOIL-LOSS (INCHES)	EFFECTIVE RAINFALL (INCHES)
1	0.0138	0.0069	0.0069
2	0.0207	0.0103	0.0103
3	0.0207	0.0103	0.0103
4	0.0276	0.0138	0.0138
5	0.0207	0.0103	0.0103
6	0.0207	0.0103	0.0103
7	0.0207	0.0103	0.0103
8	0.0276	0.0138	0.0138
9	0.0276	0.0138	0.0138
10	0.0276	0.0138	0.0138
11	0.0345	0.0172	0.0172
12	0.0345	0.0172	0.0172
13	0.0345	0.0172	0.0172
14	0.0345	0.0172	0.0172
15	0.0345	0.0172	0.0172
16	0.0414	0.0207	0.0207
17	0.0414	0.0207	0.0207
18	0.0483	0.0212	0.0271
19	0.0483	0.0208	0.0274
20	0.0551	0.0205	0.0347
21	0.0414	0.0201	0.0213
22	0.0483	0.0197	0.0285
23	0.0551	0.0194	0.0358
24	0.0551	0.0190	0.0361
25	0.0620	0.0187	0.0434
26	0.0620	0.0183	0.0437
27	0.0689	0.0180	0.0510
28	0.0689	0.0176	0.0513
29	0.0689	0.0173	0.0516
30	0.0758	0.0169	0.0589
31	0.0827	0.0166	0.0661
32	0.0896	0.0163	0.0733
33	0.1034	0.0159	0.0874
34	0.1034	0.0156	0.0878
35	0.1103	0.0153	0.0950
36	0.1172	0.0150	0.1022
37	0.1310	0.0147	0.1163
38	0.1379	0.0143	0.1235
39	0.1448	0.0140	0.1307
40	0.1516	0.0137	0.1379
41	0.1034	0.0134	0.0900
42	0.1034	0.0131	0.0903
43	0.1379	0.0128	0.1250
44	0.1379	0.0125	0.1253
45	0.1310	0.0122	0.1187
46	0.1310	0.0119	0.1190
47	0.1172	0.0116	0.1055

48	0.1241	0.0114	0.1127
49	0.1723	0.0111	0.1613
50	0.1792	0.0108	0.1684
51	0.1930	0.0105	0.1825
52	0.1999	0.0103	0.1896
53	0.2344	0.0100	0.2244
54	0.2344	0.0097	0.2246
55	0.1585	0.0095	0.1491
56	0.1585	0.0092	0.1493
57	0.1861	0.0089	0.1772
58	0.1792	0.0087	0.1705
59	0.1792	0.0084	0.1708
60	0.1723	0.0082	0.1641
61	0.1654	0.0080	0.1575
62	0.1585	0.0077	0.1508
63	0.1310	0.0075	0.1235
64	0.1310	0.0073	0.1237
65	0.0276	0.0070	0.0205
66	0.0276	0.0068	0.0208
67	0.0207	0.0066	0.0141
68	0.0207	0.0064	0.0143
69	0.0345	0.0062	0.0283
70	0.0345	0.0060	0.0285
71	0.0345	0.0058	0.0287
72	0.0276	0.0056	0.0220
73	0.0276	0.0054	0.0222
74	0.0276	0.0052	0.0224
75	0.0207	0.0050	0.0157
76	0.0138	0.0048	0.0090
77	0.0207	0.0047	0.0160
78	0.0276	0.0045	0.0231
79	0.0207	0.0043	0.0164
80	0.0138	0.0042	0.0096
81	0.0207	0.0040	0.0167
82	0.0207	0.0039	0.0168
83	0.0207	0.0037	0.0170
84	0.0138	0.0036	0.0102
85	0.0207	0.0035	0.0172
86	0.0138	0.0033	0.0105
87	0.0207	0.0032	0.0175
88	0.0138	0.0031	0.0107
89	0.0207	0.0030	0.0177
90	0.0138	0.0029	0.0109
91	0.0138	0.0028	0.0110
92	0.0138	0.0027	0.0111
93	0.0138	0.0027	0.0111
94	0.0138	0.0026	0.0112
95	0.0138	0.0025	0.0112
96	0.0138	0.0025	0.0113

TOTAL STORM RAINFALL(INCHES) = 6.89

TOTAL SOIL-LOSS(INCHES) = 1.02

TOTAL EFFECTIVE RAINFALL(INCHES) = 5.87

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TOTAL SOIL-LOSS VOLUME(ACRE-FEET) =	0.5031
TOTAL STORM RUNOFF VOLUME(ACRE-FEET) =	2.8845

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2 4 - H O U R   S T O R M  
R U N O F F   H Y D R O G R A P H

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HYDROGRAPH IN FIVE-MINUTE UNIT INTERVALS(CFS)

(Note: Time indicated is at END of Each Unit Intervals)

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TIME(HRS)	VOLUME(AF)	Q(CFS)	0.	2.5	5.0	7.5	10.0
0.083	0.0006	0.08	Q	.	.	.	.
0.167	0.0011	0.08	Q	.	.	.	.
0.250	0.0017	0.08	Q	.	.	.	.
0.333	0.0030	0.19	Q	.	.	.	.
0.417	0.0043	0.19	Q	.	.	.	.
0.500	0.0057	0.19	Q	.	.	.	.
0.583	0.0073	0.23	Q	.	.	.	.
0.667	0.0089	0.23	Q	.	.	.	.
0.750	0.0105	0.23	Q	.	.	.	.
0.833	0.0125	0.28	VQ	.	.	.	.
0.917	0.0144	0.28	VQ	.	.	.	.
1.000	0.0164	0.28	VQ	.	.	.	.
1.083	0.0183	0.28	VQ	.	.	.	.
1.167	0.0202	0.28	VQ	.	.	.	.
1.250	0.0221	0.28	VQ	.	.	.	.
1.333	0.0239	0.25	VQ	.	.	.	.
1.417	0.0256	0.25	VQ	.	.	.	.
1.500	0.0273	0.25	VQ	.	.	.	.
1.583	0.0290	0.25	Q	.	.	.	.
1.667	0.0307	0.25	Q	.	.	.	.
1.750	0.0324	0.25	Q	.	.	.	.
1.833	0.0344	0.29	VQ	.	.	.	.
1.917	0.0364	0.29	VQ	.	.	.	.
2.000	0.0384	0.29	VQ	.	.	.	.
2.083	0.0406	0.32	VQ	.	.	.	.
2.167	0.0428	0.32	VQ	.	.	.	.
2.250	0.0450	0.32	VQ	.	.	.	.
2.333	0.0473	0.33	VQ	.	.	.	.
2.417	0.0495	0.33	VQ	.	.	.	.
2.500	0.0518	0.33	VQ	.	.	.	.
2.583	0.0543	0.37	VQ	.	.	.	.
2.667	0.0568	0.37	VQ	.	.	.	.
2.750	0.0594	0.37	VQ	.	.	.	.
2.833	0.0621	0.40	VQ	.	.	.	.
2.917	0.0649	0.40	VQ	.	.	.	.
3.000	0.0677	0.40	VQ	.	.	.	.
3.083	0.0705	0.41	VQ	.	.	.	.
3.167	0.0733	0.41	Q	.	.	.	.
3.250	0.0761	0.41	Q	.	.	.	.
3.333	0.0789	0.41	.Q	.	.	.	.
3.417	0.0818	0.41	.Q	.	.	.	.
3.500	0.0846	0.41	.Q	.	.	.	.
3.583	0.0874	0.41	.Q	.	.	.	.
3.667	0.0902	0.41	.Q	.	.	.	.
3.750	0.0930	0.41	.Q	.	.	.	.
3.833	0.0962	0.45	.Q	.	.	.	.
3.917	0.0993	0.45	.Q	.	.	.	.
4.000	0.1024	0.45	.Q	.	.	.	.
4.083	0.1057	0.48	.Q	.	.	.	.
4.167	0.1090	0.48	.Q	.	.	.	.
4.250	0.1124	0.48	.Q	.	.	.	.
4.333	0.1163	0.57	.VQ	.	.	.	.
4.417	0.1202	0.57	.VQ	.	.	.	.
4.500	0.1241	0.57	.VQ	.	.	.	.
4.583	0.1285	0.63	.VQ	.	.	.	.
4.667	0.1328	0.63	.VQ	.	.	.	.

4.750	0.1372	0.63	.VQ	.	.	.	.
4.833	0.1423	0.74	.VQ	.	.	.	.
4.917	0.1473	0.74	. Q	.	.	.	.
5.000	0.1524	0.74	. Q	.	.	.	.
5.083	0.1569	0.65	. Q	.	.	.	.
5.167	0.1613	0.65	. Q	.	.	.	.
5.250	0.1658	0.65	. Q	.	.	.	.
5.333	0.1700	0.62	. Q	.	.	.	.
5.417	0.1743	0.62	. Q	.	.	.	.
5.500	0.1785	0.62	. Q	.	.	.	.
5.583	0.1837	0.76	. VQ	.	.	.	.
5.667	0.1889	0.76	. VQ	.	.	.	.
5.750	0.1942	0.76	. VQ	.	.	.	.
5.833	0.1999	0.84	. VQ	.	.	.	.
5.917	0.2057	0.84	. VQ	.	.	.	.
6.000	0.2114	0.84	. VQ	.	.	.	.
6.083	0.2179	0.94	. Q	.	.	.	.
6.167	0.2244	0.94	. Q	.	.	.	.
6.250	0.2309	0.94	. Q	.	.	.	.
6.333	0.2379	1.02	. VQ	.	.	.	.
6.417	0.2449	1.02	. VQ	.	.	.	.
6.500	0.2520	1.02	. VQ	.	.	.	.
6.583	0.2597	1.12	. VQ	.	.	.	.
6.667	0.2674	1.12	. VQ	.	.	.	.
6.750	0.2751	1.12	. VQ	.	.	.	.
6.833	0.2834	1.20	. VQ	.	.	.	.
6.917	0.2917	1.20	. Q	.	.	.	.
7.000	0.2999	1.20	. Q	.	.	.	.
7.083	0.3083	1.22	. Q	.	.	.	.
7.167	0.3167	1.22	. Q	.	.	.	.
7.250	0.3251	1.22	. Q	.	.	.	.
7.333	0.3342	1.31	. VQ	.	.	.	.
7.417	0.3432	1.31	. VQ	.	.	.	.
7.500	0.3523	1.31	. VQ	.	.	.	.
7.583	0.3624	1.47	. Q	.	.	.	.
7.667	0.3725	1.47	. Q	.	.	.	.
7.750	0.3827	1.47	. Q	.	.	.	.
7.833	0.3940	1.64	. VQ	.	.	.	.
7.917	0.4053	1.64	. VQ	.	.	.	.
8.000	0.4166	1.64	. VQ	.	.	.	.
8.083	0.4296	1.89	. V Q	.	.	.	.
8.167	0.4426	1.89	. VQ	.	.	.	.
8.250	0.4557	1.89	. VQ	.	.	.	.
8.333	0.4698	2.05	. V Q	.	.	.	.
8.417	0.4839	2.05	. V Q	.	.	.	.
8.500	0.4980	2.05	. V Q	.	.	.	.
8.583	0.5129	2.17	. VQ	.	.	.	.
8.667	0.5278	2.17	. VQ	.	.	.	.
8.750	0.5427	2.17	. VQ	.	.	.	.
8.833	0.5588	2.33	. V Q.	.	.	.	.
8.917	0.5748	2.33	. V Q.	.	.	.	.
9.000	0.5909	2.33	. VQ.	.	.	.	.
9.083	0.6086	2.58	. V Q	.	.	.	.
9.167	0.6264	2.58	. V Q	.	.	.	.
9.250	0.6442	2.58	. V Q	.	.	.	.
9.333	0.6636	2.82	. V.Q	.	.	.	.
9.417	0.6830	2.82	. V.Q	.	.	.	.
9.500	0.7024	2.82	. V.Q	.	.	.	.
9.583	0.7231	3.00	. V Q	.	.	.	.
9.667	0.7437	3.00	. V Q	.	.	.	.
9.750	0.7644	3.00	. V Q	.	.	.	.
9.833	0.7863	3.17	. V Q	.	.	.	.
9.917	0.8081	3.17	. VQ	.	.	.	.

10.000	0.8300	3.17	.	VQ	.	.	.
10.083	0.8484	2.68	.	QV	.	.	.
10.167	0.8669	2.68	.	Q V	.	.	.
10.250	0.8854	2.68	.	Q V	.	.	.
10.333	0.9008	2.24	.	Q . V	.	.	.
10.417	0.9162	2.24	.	Q . V	.	.	.
10.500	0.9317	2.24	.	Q . V	.	.	.
10.583	0.9495	2.59	.	Q V	.	.	.
10.667	0.9674	2.59	.	Q V	.	.	.
10.750	0.9852	2.59	.	Q V	.	.	.
10.833	1.0052	2.91	.	.Q V	.	.	.
10.917	1.0253	2.91	.	.Q V	.	.	.
11.000	1.0453	2.91	.	.Q V	.	.	.
11.083	1.0652	2.89	.	.Q V	.	.	.
11.167	1.0850	2.89	.	.Q V	.	.	.
11.250	1.1049	2.89	.	.Q V	.	.	.
11.333	1.1245	2.84	.	.Q V	.	.	.
11.417	1.1440	2.84	.	.Q V	.	.	.
11.500	1.1635	2.84	.	.Q V	.	.	.
11.583	1.1819	2.67	.	Q V	.	.	.
11.667	1.2003	2.67	.	Q V	.	.	.
11.750	1.2187	2.67	.	Q V	.	.	.
11.833	1.2368	2.63	.	Q V	.	.	.
11.917	1.2549	2.63	.	Q V	.	.	.
12.000	1.2730	2.63	.	Q V	.	.	.
12.083	1.2954	3.26	.	. Q V	.	.	.
12.167	1.3178	3.26	.	. Q V	.	.	.
12.250	1.3403	3.26	.	. Q V	.	.	.
12.333	1.3666	3.82	.	. Q V	.	.	.
12.417	1.3928	3.82	.	. Q V	.	.	.
12.500	1.4191	3.82	.	. Q V	.	.	.
12.583	1.4476	4.13	.	. Q V	.	.	.
12.667	1.4761	4.13	.	. Q V	.	.	.
12.750	1.5045	4.13	.	. Q V	.	.	.
12.833	1.5348	4.39	.	. Q .V	.	.	.
12.917	1.5650	4.39	.	. Q .V	.	.	.
13.000	1.5952	4.39	.	. Q . V	.	.	.
13.083	1.6289	4.90	.	. Q. V	.	.	.
13.167	1.6627	4.90	.	. Q. V	.	.	.
13.250	1.6965	4.90	.	. Q. V	.	.	.
13.333	1.7327	5.26	.	.Q V	.	.	.
13.417	1.7689	5.26	.	.Q V	.	.	.
13.500	1.8051	5.26	.	.Q V	.	.	.
13.583	1.8355	4.41	.	. Q V	.	.	.
13.667	1.8659	4.41	.	. Q V	.	.	.
13.750	1.8962	4.41	.	. Q V	.	.	.
13.833	1.9218	3.71	.	. Q V	.	.	.
13.917	1.9473	3.71	.	. Q V	.	.	.
14.000	1.9728	3.71	.	. Q V	.	.	.
14.083	1.9999	3.93	.	. Q V	.	.	.
14.167	2.0269	3.93	.	. Q V	.	.	.
14.250	2.0539	3.93	.	. Q V	.	.	.
14.333	2.0820	4.08	.	. Q V	.	.	.
14.417	2.1102	4.08	.	. Q V	.	.	.
14.500	2.1383	4.08	.	. Q V	.	.	.
14.583	2.1663	4.06	.	. Q V	.	.	.
14.667	2.1942	4.06	.	. Q V	.	.	.
14.750	2.2222	4.06	.	. Q V	.	.	.
14.833	2.2496	3.98	.	. Q .V	.	.	.
14.917	2.2771	3.98	.	. Q .V	.	.	.
15.000	2.3045	3.98	.	. Q .V	.	.	.
15.083	2.3309	3.84	.	. Q . V	.	.	.
15.167	2.3573	3.84	.	. Q . V	.	.	.

15.250	2.3838	3.84	.	.	Q	.	.	V	.
15.333	2.4091	3.68	.	.	Q	.	.	V	.
15.417	2.4345	3.68	.	.	Q	.	.	V	.
15.500	2.4599	3.68	.	.	Q	.	.	V	.
15.583	2.4824	3.28	.	.	Q	.	.	V	.
15.667	2.5050	3.28	.	.	Q	.	.	V	.
15.750	2.5275	3.28	.	.	Q	.	.	V	.
15.833	2.5482	3.00	.	.	Q	.	.	V	.
15.917	2.5689	3.00	.	.	Q	.	.	V	.
16.000	2.5896	3.00	.	.	Q	.	.	V	.
16.083	2.6014	1.71	.	Q	.	.	.	V	.
16.167	2.6131	1.71	.	Q	.	.	.	V	.
16.250	2.6249	1.71	.	Q	.	.	.	V	.
16.333	2.6299	0.72	.	Q	.	.	.	V	.
16.417	2.6348	0.72	.	Q	.	.	.	V	.
16.500	2.6398	0.72	.	Q	.	.	.	V	.
16.583	2.6430	0.47	.	Q	.	.	.	V	.
16.667	2.6462	0.47	.	Q	.	.	.	V	.
16.750	2.6494	0.47	.	Q	.	.	.	V	.
16.833	2.6520	0.37	.	Q	.	.	.	V	.
16.917	2.6545	0.37	.	Q	.	.	.	V	.
17.000	2.6570	0.37	.	Q	.	.	.	V	.
17.083	2.6606	0.52	.	Q	.	.	.	V	.
17.167	2.6641	0.52	.	Q	.	.	.	V	.
17.250	2.6677	0.52	.	Q	.	.	.	V	.
17.333	2.6721	0.65	.	Q	.	.	.	V	.
17.417	2.6766	0.65	.	Q	.	.	.	V	.
17.500	2.6811	0.65	.	Q	.	.	.	V	.
17.583	2.6857	0.67	.	Q	.	.	.	V	.
17.667	2.6903	0.67	.	Q	.	.	.	V	.
17.750	2.6950	0.67	.	Q	.	.	.	V	.
17.833	2.6991	0.60	.	Q	.	.	.	V	.
17.917	2.7032	0.60	.	Q	.	.	.	V	.
18.000	2.7073	0.60	.	Q	.	.	.	V	.
18.083	2.7110	0.54	.	Q	.	.	.	V	.
18.167	2.7148	0.54	.	Q	.	.	.	V	.
18.250	2.7185	0.54	.	Q	.	.	.	V	.
18.333	2.7221	0.53	.	Q	.	.	.	V	.
18.417	2.7258	0.53	.	Q	.	.	.	V	.
18.500	2.7295	0.53	.	Q	.	.	.	V	.
18.583	2.7326	0.45	.	Q	.	.	.	V	.
18.667	2.7357	0.45	.	Q	.	.	.	V	.
18.750	2.7388	0.45	.	Q	.	.	.	V	.
18.833	2.7409	0.31	.	Q	.	.	.	V	.
18.917	2.7430	0.31	.	Q	.	.	.	V	.
19.000	2.7451	0.31	.	Q	.	.	.	V	.
19.083	2.7473	0.32	.	Q	.	.	.	V	.
19.167	2.7495	0.32	.	Q	.	.	.	V	.
19.250	2.7517	0.32	.	Q	.	.	.	V	.
19.333	2.7548	0.46	.	Q	.	.	.	V	.
19.417	2.7580	0.46	.	Q	.	.	.	V	.
19.500	2.7611	0.46	.	Q	.	.	.	V	.
19.583	2.7642	0.45	.	Q	.	.	.	V	.
19.667	2.7673	0.45	.	Q	.	.	.	V	.
19.750	2.7704	0.45	.	Q	.	.	.	V	.
19.833	2.7726	0.32	.	Q	.	.	.	V	.
19.917	2.7748	0.32	.	Q	.	.	.	V	.
20.000	2.7770	0.32	.	Q	.	.	.	V	.
20.083	2.7792	0.33	.	Q	.	.	.	V	.
20.167	2.7815	0.33	.	Q	.	.	.	V	.
20.250	2.7838	0.33	.	Q	.	.	.	V	.
20.333	2.7865	0.39	.	Q	.	.	.	V	.
20.417	2.7891	0.39	.	Q	.	.	.	V	.



20.500	2.7918	0.39	.Q	.	.	.	V .
20.583	2.7945	0.40	.Q	.	.	.	V .
20.667	2.7973	0.40	.Q	.	.	.	V .
20.750	2.8000	0.40	.Q	.	.	.	V .
20.833	2.8022	0.32	.Q	.	.	.	V .
20.917	2.8045	0.32	.Q	.	.	.	V .
21.000	2.8067	0.32	.Q	.	.	.	V .
21.083	2.8090	0.34	.Q	.	.	.	V .
21.167	2.8114	0.34	.Q	.	.	.	V .
21.250	2.8137	0.34	.Q	.	.	.	V .
21.333	2.8159	0.32	.Q	.	.	.	V .
21.417	2.8181	0.32	.Q	.	.	.	V .
21.500	2.8203	0.32	.Q	.	.	.	V .
21.583	2.8226	0.35	.Q	.	.	.	V .
21.667	2.8250	0.35	.Q	.	.	.	V .
21.750	2.8274	0.35	.Q	.	.	.	V .
21.833	2.8296	0.32	.Q	.	.	.	V .
21.917	2.8318	0.32	.Q	.	.	.	V .
22.000	2.8340	0.32	.Q	.	.	.	V .
22.083	2.8364	0.35	.Q	.	.	.	V .
22.167	2.8389	0.35	.Q	.	.	.	V .
22.250	2.8413	0.35	.Q	.	.	.	V .
22.333	2.8435	0.33	.Q	.	.	.	V .
22.417	2.8458	0.33	.Q	.	.	.	V .
22.500	2.8480	0.33	.Q	.	.	.	V .
22.583	2.8499	0.27	.Q	.	.	.	V .
22.667	2.8518	0.27	.Q	.	.	.	V .
22.750	2.8536	0.27	.Q	.	.	.	V .
22.833	2.8555	0.26	.Q	.	.	.	V .
22.917	2.8573	0.26	.Q	.	.	.	V .
23.000	2.8591	0.26	.Q	.	.	.	V .
23.083	2.8609	0.26	.Q	.	.	.	V .
23.166	2.8627	0.26	.Q	.	.	.	V .
23.250	2.8646	0.26	.Q	.	.	.	V .
23.333	2.8664	0.27	.Q	.	.	.	V .
23.416	2.8682	0.27	.Q	.	.	.	V .
23.500	2.8701	0.27	.Q	.	.	.	V .
23.583	2.8719	0.27	.Q	.	.	.	V .
23.666	2.8737	0.27	.Q	.	.	.	V .
23.750	2.8756	0.27	.Q	.	.	.	V .
23.833	2.8774	0.27	.Q	.	.	.	V .
23.916	2.8793	0.27	.Q	.	.	.	V .
24.000	2.8811	0.27	.Q	.	.	.	V .
24.083	2.8820	0.13	Q	.	.	.	V .
24.166	2.8829	0.13	Q	.	.	.	V .
24.250	2.8838	0.13	Q	.	.	.	V .
24.333	2.8840	0.02	Q	.	.	.	V .
24.416	2.8842	0.02	Q	.	.	.	V .
24.500	2.8843	0.02	Q	.	.	.	V .
24.583	2.8844	0.01	Q	.	.	.	V .
24.666	2.8844	0.01	Q	.	.	.	V .
24.750	2.8844	0.01	Q	.	.	.	V .

-----

TIME DURATION(minutes) OF PERCENTILES OF ESTIMATED PEAK FLOW RATE:  
 (Note: 100% of Peak Flow Rate estimate assumed to have  
 an instantaneous time duration)

Percentile of Estimated Peak Flow Rate	Duration (minutes)
=====	=====
0%	1485.0
10%	810.0
20%	585.0

	RS_U_100.RES
30%	510.0
40%	450.0
50%	360.0
60%	240.0
70%	195.0
80%	60.0
90%	30.0

=====

END OF FLOODSCx ROUTING ANALYSIS

## UHS Rancho Springs 100-yr, 24 hr Detention Analysis

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### Project Summary

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Title	UHS Rancho Springs_100 yr, 24 hr
Engineer	Nikki Kerry, P.E.
Company	Kimley-Horn and Associates, Inc.
Date	5/12/2020

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### Notes

1. Inflow hydrograph (100-year, 24 hr) calculated based on Synthetic Unit Hydrograph Method from Riverside County Flood Control and Water Conservation District Hydrology Manual (April 1978) using AES software.
  2. Flow-through basin analysis completed using modified Pul's (storage indication routing).
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## UHS Rancho Springs 100-yr, 24 hr Detention Analysis

Subsection: User Notifications

### User Notifications

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Message Id	17
Scenario	Base
Element Type	Composite Outlet Structure
Element Id	21
Label	Composite Outlet Structure - 1
Time	(N/A)
Message	Riser orifice equation controls at one or more headwater elevations for outlet structure.
Source	Information

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## UHS Rancho Springs 100-yr, 24 hr Detention Analysis

Subsection: Master Network Summary

### Catchments Summary

Label	Scenario	Return Event (years)	Hydrograph Volume (ac-ft)	Time to Peak (min)	Peak Flow (ft <sup>3</sup> /s)
Unit Hydrograph (Onsite Runoff)	Base	0	2.888	795.000	5.26

### Node Summary

Label	Scenario	Return Event (years)	Hydrograph Volume (ac-ft)	Time to Peak (min)	Peak Flow (ft <sup>3</sup> /s)
Outfall (POC)	Base	0	2.676	810.000	4.42

### Pond Summary

Label	Scenario	Return Event (years)	Hydrograph Volume (ac-ft)	Time to Peak (min)	Peak Flow (ft <sup>3</sup> /s)	Maximum Water Surface Elevation (ft)	Maximum Pond Storage (ac-ft)
Onsite Detention Basin (IN)	Base	0	2.885	795.000	5.26	(N/A)	(N/A)
Onsite Detention Basin (OUT)	Base	0	2.676	810.000	4.42	3.75	0.513

## UHS Rancho Springs 100-yr, 24 hr Detention Analysis

Subsection: Read Hydrograph

Label: Unit Hydrograph (Onsite Runoff)

Peak Discharge	5.26 ft <sup>3</sup> /s
Time to Peak	800.000 min
Hydrograph Volume	2.888 ac-ft

### HYDROGRAPH ORDINATES (ft<sup>3</sup>/s)

Output Time Increment = 5.000 min

Time on left represents time for first value in each row.

Time (min)	Flow (ft <sup>3</sup> /s)	Flow (ft <sup>3</sup> /s)	Flow (ft <sup>3</sup> /s)	Flow (ft <sup>3</sup> /s)	Flow (ft <sup>3</sup> /s)
0.000	0.08	0.08	0.08	0.19	0.19
25.000	0.19	0.24	0.24	0.24	0.29
50.000	0.29	0.29	0.28	0.28	0.28
75.000	0.25	0.25	0.25	0.25	0.25
100.000	0.25	0.29	0.29	0.29	0.32
125.000	0.32	0.32	0.33	0.33	0.33
150.000	0.37	0.37	0.37	0.40	0.40
175.000	0.40	0.41	0.41	0.41	0.41
200.000	0.41	0.41	0.41	0.41	0.41
225.000	0.45	0.45	0.45	0.48	0.48
250.000	0.48	0.57	0.57	0.57	0.64
275.000	0.64	0.64	0.74	0.74	0.74
300.000	0.65	0.65	0.65	0.62	0.62
325.000	0.62	0.76	0.76	0.76	0.84
350.000	0.84	0.84	0.94	0.94	0.94
375.000	1.02	1.02	1.02	1.12	1.12
400.000	1.12	1.20	1.20	1.20	1.22
425.000	1.22	1.22	1.32	1.32	1.32
450.000	1.47	1.47	1.47	1.64	1.64
475.000	1.64	1.90	1.90	1.90	2.05
500.000	2.05	2.05	2.17	2.17	2.17
525.000	2.33	2.33	2.33	2.58	2.58
550.000	2.58	2.82	2.82	2.82	3.00
575.000	3.00	3.00	3.18	3.18	3.18
600.000	2.68	2.68	2.68	2.24	2.24
625.000	2.24	2.59	2.59	2.59	2.91
650.000	2.91	2.91	2.89	2.89	2.89
675.000	2.84	2.84	2.84	2.67	2.67
700.000	2.67	2.63	2.63	2.63	3.26
725.000	3.26	3.26	3.82	3.82	3.82
750.000	4.14	4.14	4.14	4.39	4.39
775.000	4.39	4.91	4.91	4.91	5.26
800.000	5.26	5.26	4.41	4.41	4.41
825.000	3.71	3.71	3.71	3.93	3.93
850.000	3.93	4.09	4.09	4.09	4.07
875.000	4.07	4.07	3.99	3.99	3.99
900.000	3.84	3.84	3.84	3.69	3.69

## UHS Rancho Springs 100-yr, 24 hr Detention Analysis

Subsection: Read Hydrograph

Label: Unit Hydrograph (Onsite Runoff)

### HYDROGRAPH ORDINATES (ft<sup>3</sup>/s)

Output Time Increment = 5.000 min

Time on left represents time for first value in each row.

Time (min)	Flow (ft <sup>3</sup> /s)	Flow (ft <sup>3</sup> /s)	Flow (ft <sup>3</sup> /s)	Flow (ft <sup>3</sup> /s)	Flow (ft <sup>3</sup> /s)
925.000	3.69	3.28	3.28	3.28	3.01
950.000	3.01	3.01	1.71	1.71	1.71
975.000	0.72	0.72	0.72	0.47	0.47
1,000.000	0.47	0.37	0.37	0.37	0.52
1,025.000	0.52	0.52	0.65	0.65	0.65
1,050.000	0.67	0.67	0.67	0.60	0.60
1,075.000	0.60	0.54	0.54	0.54	0.53
1,100.000	0.53	0.53	0.45	0.45	0.45
1,125.000	0.31	0.31	0.31	0.32	0.32
1,150.000	0.32	0.46	0.46	0.46	0.45
1,175.000	0.45	0.45	0.32	0.32	0.32
1,200.000	0.33	0.33	0.33	0.39	0.39
1,225.000	0.39	0.40	0.40	0.40	0.32
1,250.000	0.32	0.32	0.34	0.34	0.34
1,275.000	0.32	0.32	0.32	0.35	0.35
1,300.000	0.35	0.32	0.32	0.32	0.35
1,325.000	0.35	0.35	0.33	0.33	0.33
1,350.000	0.27	0.27	0.27	0.27	0.27
1,375.000	0.27	0.26	0.26	0.26	0.27
1,400.000	0.27	0.27	0.27	0.27	0.27
1,425.000	0.27	0.27	0.27	0.13	0.13
1,450.000	0.13	0.02	0.02	0.02	0.01
1,475.000	0.01	0.01	0.00	(N/A)	(N/A)



## UHS Rancho Springs 100-yr, 24 hr Detention Analysis

Subsection: Addition Summary

Label: Outfall (POC)

### Summary for Hydrograph Addition at 'Outfall (POC)'

Upstream Link	Upstream Node
Outlet-1	Onsite Detention Basin

### Node Inflows

Inflow Type	Element	Volume (ac-ft)	Time to Peak (min)	Flow (Peak) (ft <sup>3</sup> /s)
Flow (From)	Outlet-1	2.676	810.000	4.42
Flow (In)	Outfall (POC)	2.676	810.000	4.42

## UHS Rancho Springs 100-yr, 24 hr Detention Analysis

Subsection: Time vs. Elevation

Label: Onsite Detention Basin (OUT)

### Time vs. Elevation (ft)

Output Time increment = 3.000 min

Time on left represents time for first value in each row.

Time (min)	Elevation (ft)	Elevation (ft)	Elevation (ft)	Elevation (ft)	Elevation (ft)
0.000	0.00	0.01	0.01	0.02	0.03
15.000	0.05	0.06	0.08	0.10	0.11
30.000	0.13	0.15	0.18	0.20	0.22
45.000	0.24	0.26	0.29	0.31	0.34
60.000	0.36	0.38	0.40	0.43	0.45
75.000	0.47	0.49	0.50	0.51	0.52
90.000	0.53	0.53	0.54	0.55	0.56
105.000	0.57	0.58	0.59	0.60	0.61
120.000	0.62	0.63	0.64	0.65	0.66
135.000	0.67	0.69	0.70	0.71	0.72
150.000	0.73	0.74	0.76	0.77	0.78
165.000	0.80	0.81	0.82	0.84	0.85
180.000	0.87	0.88	0.89	0.91	0.92
195.000	0.94	0.95	0.97	0.98	0.99
210.000	1.01	1.02	1.03	1.04	1.05
225.000	1.06	1.07	1.08	1.10	1.11
240.000	1.12	1.13	1.15	1.16	1.17
255.000	1.19	1.20	1.22	1.23	1.25
270.000	1.27	1.28	1.30	1.32	1.34
285.000	1.36	1.38	1.40	1.42	1.44
300.000	1.46	1.48	1.49	1.51	1.53
315.000	1.54	1.56	1.57	1.59	1.60
330.000	1.62	1.64	1.66	1.68	1.70
345.000	1.72	1.74	1.76	1.78	1.80
360.000	1.82	1.84	1.86	1.88	1.90
375.000	1.92	1.94	1.96	1.98	2.00
390.000	2.02	2.04	2.06	2.08	2.10
405.000	2.11	2.13	2.15	2.17	2.18
420.000	2.20	2.21	2.23	2.24	2.25
435.000	2.27	2.28	2.30	2.31	2.33
450.000	2.34	2.36	2.37	2.39	2.40
465.000	2.42	2.43	2.45	2.46	2.48
480.000	2.50	2.52	2.54	2.55	2.57
495.000	2.59	2.60	2.62	2.64	2.65
510.000	2.67	2.68	2.70	2.71	2.73
525.000	2.74	2.76	2.77	2.79	2.80
540.000	2.82	2.84	2.85	2.87	2.89
555.000	2.90	2.92	2.94	2.96	2.97
570.000	2.99	3.01	3.03	3.04	3.06
585.000	3.07	3.09	3.11	3.12	3.13
600.000	3.14	3.14	3.14	3.14	3.14

## UHS Rancho Springs 100-yr, 24 hr Detention Analysis

Subsection: Time vs. Elevation

Label: Onsite Detention Basin (OUT)

### Time vs. Elevation (ft)

Output Time increment = 3.000 min

Time on left represents time for first value in each row.

Time (min)	Elevation (ft)	Elevation (ft)	Elevation (ft)	Elevation (ft)	Elevation (ft)
615.000	3.13	3.13	3.12	3.11	3.11
630.000	3.11	3.11	3.11	3.11	3.11
645.000	3.12	3.13	3.13	3.14	3.15
660.000	3.15	3.16	3.16	3.17	3.17
675.000	3.17	3.18	3.18	3.18	3.18
690.000	3.18	3.18	3.18	3.18	3.18
705.000	3.18	3.17	3.17	3.17	3.17
720.000	3.18	3.19	3.20	3.21	3.22
735.000	3.24	3.26	3.28	3.30	3.32
750.000	3.34	3.36	3.38	3.40	3.42
765.000	3.44	3.46	3.48	3.50	3.52
780.000	3.54	3.57	3.59	3.61	3.63
795.000	3.66	3.68	3.71	3.73	3.74
810.000	3.75	3.75	3.75	3.75	3.74
825.000	3.73	3.72	3.71	3.69	3.68
840.000	3.68	3.67	3.67	3.66	3.66
855.000	3.65	3.65	3.65	3.65	3.65
870.000	3.65	3.65	3.65	3.65	3.65
885.000	3.65	3.64	3.64	3.64	3.64
900.000	3.63	3.63	3.63	3.62	3.62
915.000	3.61	3.61	3.60	3.59	3.59
930.000	3.58	3.56	3.55	3.54	3.53
945.000	3.52	3.50	3.49	3.47	3.46
960.000	3.43	3.39	3.35	3.32	3.28
975.000	3.24	3.19	3.14	3.10	3.06
990.000	3.02	2.98	2.94	2.90	2.86
1,005.000	2.83	2.79	2.76	2.73	2.70
1,020.000	2.68	2.65	2.63	2.61	2.59
1,035.000	2.58	2.56	2.55	2.53	2.52
1,050.000	2.51	2.50	2.49	2.48	2.47
1,065.000	2.46	2.45	2.44	2.43	2.42
1,080.000	2.41	2.40	2.39	2.38	2.37
1,095.000	2.36	2.35	2.34	2.34	2.33
1,110.000	2.32	2.31	2.30	2.29	2.28
1,125.000	2.27	2.26	2.25	2.24	2.23
1,140.000	2.23	2.22	2.21	2.20	2.19
1,155.000	2.19	2.19	2.18	2.18	2.18
1,170.000	2.17	2.17	2.17	2.16	2.16
1,185.000	2.16	2.15	2.14	2.14	2.13
1,200.000	2.13	2.13	2.12	2.12	2.11
1,215.000	2.11	2.11	2.11	2.10	2.10

## UHS Rancho Springs 100-yr, 24 hr Detention Analysis

Subsection: Time vs. Elevation

Label: Onsite Detention Basin (OUT)

### Time vs. Elevation (ft)

Output Time increment = 3.000 min

Time on left represents time for first value in each row.

Time (min)	Elevation (ft)	Elevation (ft)	Elevation (ft)	Elevation (ft)	Elevation (ft)
1,230.000	2.10	2.10	2.10	2.10	2.09
1,245.000	2.09	2.09	2.09	2.08	2.08
1,260.000	2.08	2.08	2.07	2.07	2.07
1,275.000	2.07	2.07	2.06	2.06	2.06
1,290.000	2.06	2.06	2.06	2.06	2.05
1,305.000	2.05	2.05	2.05	2.05	2.05
1,320.000	2.05	2.05	2.05	2.04	2.04
1,335.000	2.04	2.04	2.04	2.04	2.04
1,350.000	2.04	2.04	2.03	2.03	2.03
1,365.000	2.03	2.03	2.02	2.02	2.02
1,380.000	2.02	2.02	2.02	2.01	2.01
1,395.000	2.01	2.01	2.01	2.01	2.01
1,410.000	2.01	2.00	2.00	2.00	2.00
1,425.000	2.00	2.00	2.00	2.00	2.00
1,440.000	1.99	(N/A)	(N/A)	(N/A)	(N/A)

## UHS Rancho Springs 100-yr, 24 hr Detention Analysis

Subsection: Time vs. Volume

Label: Onsite Detention Basin

### Time vs. Volume (ac-ft)

Output Time increment = 3.000 min

Time on left represents time for first value in each row.

Time (min)	Volume (ac-ft)	Volume (ac-ft)	Volume (ac-ft)	Volume (ac-ft)	Volume (ac-ft)
0.000	0.000	0.000	0.000	0.000	0.000
15.000	0.001	0.001	0.001	0.001	0.002
30.000	0.002	0.002	0.003	0.003	0.004
45.000	0.005	0.007	0.008	0.009	0.011
60.000	0.012	0.013	0.015	0.016	0.018
75.000	0.020	0.021	0.022	0.023	0.024
90.000	0.024	0.025	0.026	0.026	0.027
105.000	0.028	0.028	0.029	0.030	0.031
120.000	0.032	0.033	0.034	0.035	0.036
135.000	0.037	0.038	0.039	0.041	0.042
150.000	0.043	0.044	0.045	0.047	0.048
165.000	0.049	0.051	0.052	0.054	0.055
180.000	0.057	0.058	0.060	0.061	0.063
195.000	0.065	0.066	0.068	0.069	0.071
210.000	0.072	0.073	0.075	0.076	0.077
225.000	0.079	0.080	0.082	0.083	0.085
240.000	0.086	0.088	0.089	0.091	0.092
255.000	0.094	0.096	0.098	0.100	0.102
270.000	0.104	0.107	0.109	0.111	0.114
285.000	0.116	0.119	0.122	0.125	0.127
300.000	0.130	0.133	0.135	0.137	0.140
315.000	0.142	0.144	0.146	0.148	0.150
330.000	0.153	0.156	0.158	0.161	0.164
345.000	0.167	0.170	0.173	0.176	0.179
360.000	0.182	0.185	0.188	0.191	0.195
375.000	0.198	0.201	0.204	0.207	0.210
390.000	0.213	0.217	0.220	0.222	0.225
405.000	0.228	0.231	0.234	0.236	0.239
420.000	0.241	0.244	0.246	0.248	0.251
435.000	0.253	0.255	0.258	0.260	0.262
450.000	0.265	0.267	0.270	0.272	0.274
465.000	0.277	0.280	0.283	0.285	0.288
480.000	0.291	0.294	0.297	0.300	0.303
495.000	0.306	0.309	0.312	0.314	0.317
510.000	0.320	0.323	0.325	0.328	0.330
525.000	0.333	0.336	0.338	0.341	0.343
540.000	0.346	0.349	0.352	0.355	0.358
555.000	0.361	0.364	0.367	0.370	0.373
570.000	0.376	0.379	0.382	0.385	0.388
585.000	0.391	0.394	0.396	0.399	0.401
600.000	0.402	0.402	0.402	0.403	0.402

## UHS Rancho Springs 100-yr, 24 hr Detention Analysis

Subsection: Time vs. Volume

Label: Onsite Detention Basin

### Time vs. Volume (ac-ft)

Output Time increment = 3.000 min

Time on left represents time for first value in each row.

Time (min)	Volume (ac-ft)	Volume (ac-ft)	Volume (ac-ft)	Volume (ac-ft)	Volume (ac-ft)
615.000	0.401	0.400	0.399	0.397	0.396
630.000	0.396	0.397	0.397	0.397	0.397
645.000	0.399	0.400	0.401	0.402	0.404
660.000	0.405	0.405	0.406	0.407	0.408
675.000	0.408	0.409	0.409	0.410	0.410
690.000	0.410	0.410	0.410	0.409	0.409
705.000	0.409	0.408	0.408	0.408	0.408
720.000	0.409	0.411	0.413	0.415	0.417
735.000	0.421	0.424	0.428	0.431	0.434
750.000	0.438	0.442	0.446	0.449	0.452
765.000	0.456	0.460	0.463	0.467	0.470
780.000	0.475	0.479	0.483	0.487	0.491
795.000	0.496	0.500	0.505	0.509	0.511
810.000	0.513	0.513	0.512	0.512	0.512
825.000	0.510	0.507	0.505	0.503	0.501
840.000	0.499	0.498	0.497	0.496	0.496
855.000	0.495	0.495	0.495	0.495	0.495
870.000	0.495	0.495	0.495	0.494	0.494
885.000	0.494	0.494	0.493	0.493	0.492
900.000	0.492	0.491	0.490	0.489	0.488
915.000	0.487	0.486	0.485	0.484	0.483
930.000	0.481	0.479	0.477	0.475	0.472
945.000	0.470	0.467	0.465	0.463	0.459
960.000	0.454	0.447	0.440	0.434	0.428
975.000	0.420	0.411	0.403	0.395	0.388
990.000	0.381	0.373	0.367	0.360	0.354
1,005.000	0.347	0.341	0.336	0.330	0.326
1,020.000	0.321	0.317	0.314	0.310	0.307
1,035.000	0.304	0.302	0.299	0.297	0.295
1,050.000	0.293	0.291	0.290	0.288	0.286
1,065.000	0.284	0.283	0.281	0.279	0.277
1,080.000	0.276	0.274	0.272	0.271	0.269
1,095.000	0.268	0.267	0.265	0.264	0.263
1,110.000	0.261	0.260	0.258	0.257	0.255
1,125.000	0.254	0.252	0.250	0.249	0.247
1,140.000	0.246	0.244	0.243	0.242	0.241
1,155.000	0.240	0.239	0.239	0.238	0.238
1,170.000	0.237	0.237	0.236	0.236	0.235
1,185.000	0.235	0.234	0.233	0.232	0.231
1,200.000	0.230	0.230	0.229	0.228	0.228
1,215.000	0.227	0.227	0.227	0.226	0.226

## UHS Rancho Springs 100-yr, 24 hr Detention Analysis

Subsection: Time vs. Volume

Label: Onsite Detention Basin

### Time vs. Volume (ac-ft)

Output Time increment = 3.000 min

Time on left represents time for first value in each row.

Time (min)	Volume (ac-ft)	Volume (ac-ft)	Volume (ac-ft)	Volume (ac-ft)	Volume (ac-ft)
1,230.000	0.226	0.226	0.225	0.225	0.225
1,245.000	0.225	0.224	0.224	0.223	0.223
1,260.000	0.222	0.222	0.222	0.221	0.221
1,275.000	0.221	0.220	0.220	0.220	0.219
1,290.000	0.219	0.219	0.219	0.219	0.219
1,305.000	0.218	0.218	0.218	0.218	0.217
1,320.000	0.217	0.217	0.217	0.217	0.217
1,335.000	0.217	0.217	0.216	0.216	0.216
1,350.000	0.216	0.215	0.215	0.215	0.215
1,365.000	0.214	0.214	0.214	0.213	0.213
1,380.000	0.213	0.213	0.212	0.212	0.212
1,395.000	0.212	0.211	0.211	0.211	0.211
1,410.000	0.211	0.211	0.210	0.210	0.210
1,425.000	0.210	0.210	0.210	0.210	0.209
1,440.000	0.209	(N/A)	(N/A)	(N/A)	(N/A)

## UHS Rancho Springs 100-yr, 24 hr Detention Analysis

Subsection: Pipe Volume

Label: Onsite Detention Basin

### Volume Results (Pipe)

Pipe Storage Upstream Invert	0.20 ft
Pipe Storage Downstream Invert	0.00 ft
Pipe Storage Length	200.00 ft
Pipe Storage Diameter	96.0 in
Pipe Storage Number of Barrels	5
Pipe Storage Slice Width	1.00 ft
Pipe Storage Vertical Increment	0.20 ft

Elevation (ft)	Perpendicular Downstream Depth (ft)	Perpendicular Downstream Area (ft²)	Wetted Length (ft)	Filled Length (ft)	Perpendicular Upstream Depth (ft)	Perpendicular Upstream Area (ft²)	Total Volume (ac-ft)
0.00	0.00	0.0	0.00	0.00	0.00	0.0	0.000
0.20	0.20	0.3	200.00	0.00	0.00	0.0	0.003
0.40	0.40	0.9	200.00	0.00	0.20	0.3	0.014
0.60	0.60	1.7	200.00	0.00	0.40	0.9	0.030
0.80	0.80	2.6	200.00	0.00	0.60	1.7	0.049
1.00	1.00	3.6	200.00	0.00	0.80	2.6	0.071
1.20	1.20	4.7	200.00	0.00	1.00	3.6	0.096
1.40	1.40	5.9	200.00	0.00	1.20	4.7	0.122
1.60	1.60	7.2	200.00	0.00	1.40	5.9	0.150
1.80	1.80	8.5	200.00	0.00	1.60	7.2	0.179
2.00	2.00	9.8	200.00	0.00	1.80	8.5	0.210
2.20	2.20	11.2	200.00	0.00	2.00	9.8	0.242
2.40	2.40	12.7	200.00	0.00	2.20	11.2	0.274
2.60	2.60	14.2	200.00	0.00	2.40	12.7	0.308
2.80	2.80	15.7	200.00	0.00	2.60	14.2	0.343
3.00	3.00	17.2	200.00	0.00	2.80	15.7	0.378
3.20	3.20	18.8	200.00	0.00	3.00	17.2	0.413
3.40	3.40	20.3	200.00	0.00	3.20	18.8	0.449
3.60	3.60	21.9	200.00	0.00	3.40	20.4	0.485
3.80	3.80	23.5	200.00	0.00	3.60	21.9	0.522
4.00	4.00	25.1	200.00	0.00	3.80	23.5	0.559
4.20	4.20	26.7	200.00	0.00	4.00	25.1	0.595
4.40	4.40	28.3	200.00	0.00	4.20	26.7	0.632
4.60	4.60	29.9	200.00	0.00	4.40	28.3	0.669
4.80	4.80	31.5	200.00	0.00	4.60	29.9	0.705
5.00	5.00	33.0	200.00	0.00	4.80	31.5	0.741
5.20	5.20	34.6	200.00	0.00	5.00	33.0	0.776
5.40	5.40	36.1	200.00	0.00	5.20	34.6	0.811
5.60	5.60	37.6	200.00	0.00	5.40	36.1	0.846
5.80	5.80	39.0	200.00	0.00	5.60	37.6	0.879
6.00	6.00	40.4	200.00	0.00	5.80	39.0	0.912



## UHS Rancho Springs 100-yr, 24 hr Detention Analysis

Subsection: Pipe Volume

Label: Onsite Detention Basin

Elevation (ft)	Perpendicular Downstream Depth (ft)	Perpendicular Downstream Area (ft <sup>2</sup> )	Wetted Length (ft)	Filled Length (ft)	Perpendicular Upstream Depth (ft)	Perpendicular Upstream Area (ft <sup>2</sup> )	Total Volume (ac-ft)
6.20	6.20	41.8	200.00	0.00	6.00	40.4	0.944
6.40	6.40	43.1	200.00	0.00	6.20	41.8	0.975
6.60	6.60	44.4	200.00	0.00	6.40	43.1	1.004
6.80	6.80	45.5	200.00	0.00	6.60	44.4	1.032
7.00	7.00	46.6	200.00	0.00	6.80	45.5	1.058
7.20	7.20	47.6	200.00	0.00	7.00	46.6	1.082
7.40	7.40	48.5	200.00	0.00	7.20	47.6	1.104
7.60	7.60	49.3	200.00	0.00	7.40	48.6	1.124
7.80	7.80	49.9	200.00	0.00	7.60	49.3	1.140
8.00	8.00	50.3	200.00	0.00	7.80	49.9	1.151
8.20	8.00	50.3	200.00	200.00	8.00	50.3	1.154

## UHS Rancho Springs 100-yr, 24 hr Detention Analysis

Subsection: Outlet Input Data

Label: Composite Outlet Structure - 1

### Requested Pond Water Surface Elevations

Minimum (Headwater)	0.00 ft
Increment (Headwater)	0.50 ft
Maximum (Headwater)	8.21 ft

### Outlet Connectivity

Structure Type	Outlet ID	Direction	Outfall	E1 (ft)	E2 (ft)
Stand Pipe	Riser - 1	Forward	TW	7.00	8.20
Orifice-Circular	Orifice - 1	Forward	TW	0.00	8.20
Rectangular Weir	Notch Weir	Forward	TW	1.75	8.20
Tailwater Settings	Tailwater			(N/A)	(N/A)

## UHS Rancho Springs 100-yr, 24 hr Detention Analysis

Subsection: Outlet Input Data

Label: Composite Outlet Structure - 1

Structure ID: Orifice - 1	
Structure Type: Orifice-Circular	
Number of Openings	1
Elevation	0.00 ft
Orifice Diameter	1.8 in
Orifice Coefficient	0.600
Structure ID: Notch Weir	
Structure Type: Rectangular Weir	
Number of Openings	1
Elevation	1.75 ft
Weir Length	0.50 ft
Weir Coefficient	3.00 (ft <sup>0.5</sup> )/s
Structure ID: Riser - 1	
Structure Type: Stand Pipe	
Number of Openings	1
Elevation	0.00 ft
Diameter	54.0 in
Orifice Area	15.9 ft <sup>2</sup>
Orifice Coefficient	0.600
Weir Length	14.14 ft
Weir Coefficient	3.00 (ft <sup>0.5</sup> )/s
K Reverse	1.000
Manning's n	0.000
Kev, Charged Riser	0.000
Weir Submergence	False
Orifice H to crest	True
Structure ID: TW	
Structure Type: TW Setup, DS Channel	
Tailwater Type	Free Outfall
Convergence Tolerances	
Maximum Iterations	30
Tailwater Tolerance (Minimum)	0.01 ft
Tailwater Tolerance (Maximum)	0.50 ft
Headwater Tolerance (Minimum)	0.01 ft
Headwater Tolerance (Maximum)	0.50 ft

## UHS Rancho Springs 100-yr, 24 hr Detention Analysis

Subsection: Outlet Input Data

Label: Composite Outlet Structure - 1

Convergence Tolerances	
Flow Tolerance (Minimum)	0.001 ft <sup>3</sup> /s
Flow Tolerance (Maximum)	10.000 ft <sup>3</sup> /s

## UHS Rancho Springs 100-yr, 24 hr Detention Analysis

Subsection: Individual Outlet Curves

Label: Composite Outlet Structure - 1

### RATING TABLE FOR ONE OUTLET TYPE

Structure ID = Orifice - 1 (Orifice-Circular)

Upstream ID = (Pond Water Surface)

Downstream ID = Tailwater (Pond Outfall)

Water Surface Elevation (ft)	Flow (ft <sup>3</sup> /s)	Tailwater Elevation (ft)	Convergence Error (ft)
0.00	0.00	(N/A)	0.00
0.50	0.05	(N/A)	0.00
1.00	0.08	(N/A)	0.00
1.50	0.10	(N/A)	0.00
1.75	0.10	(N/A)	0.00
2.00	0.11	(N/A)	0.00
2.50	0.13	(N/A)	0.00
3.00	0.14	(N/A)	0.00
3.50	0.15	(N/A)	0.00
4.00	0.16	(N/A)	0.00
4.50	0.17	(N/A)	0.00
5.00	0.18	(N/A)	0.00
5.50	0.19	(N/A)	0.00
6.00	0.20	(N/A)	0.00
6.50	0.20	(N/A)	0.00
7.00	0.21	(N/A)	0.00
7.50	0.22	(N/A)	0.00
8.00	0.23	(N/A)	0.00
8.20	0.23	(N/A)	0.00

#### Computation Messages

Upstream HW &  
DNstream TW < Inv.El

H =.43

H =.93

H =1.43

H =1.68

H =1.93

H =2.43

H =2.93

H =3.43

H =3.93

H =4.43

H =4.93

H =5.43

H =5.93

H =6.43

H =6.93

**UHS Rancho Springs 100-yr, 24 hr Detention Analysis**

Subsection: Individual Outlet Curves  
Label: Composite Outlet Structure - 1

RATING TABLE FOR ONE OUTLET TYPE  
Structure ID = Orifice - 1 (Orifice-Circular)  
-----  
Upstream ID = (Pond Water Surface)  
Downstream ID = Tailwater (Pond Outfall)

Computation Messages
H =7.43
H =7.93
H =8.13

## UHS Rancho Springs 100-yr, 24 hr Detention Analysis

Subsection: Individual Outlet Curves

Label: Composite Outlet Structure - 1

### RATING TABLE FOR ONE OUTLET TYPE

Structure ID = Notch Weir (Rectangular Weir)

Upstream ID = (Pond Water Surface)

Downstream ID = Tailwater (Pond Outfall)

Water Surface Elevation (ft)	Flow (ft <sup>3</sup> /s)	Tailwater Elevation (ft)	Convergence Error (ft)
0.00	0.00	(N/A)	0.00
0.50	0.00	(N/A)	0.00
1.00	0.00	(N/A)	0.00
1.50	0.00	(N/A)	0.00
1.75	0.00	(N/A)	0.00
2.00	0.19	(N/A)	0.00
2.50	0.97	(N/A)	0.00
3.00	2.10	(N/A)	0.00
3.50	3.47	(N/A)	0.00
4.00	5.06	(N/A)	0.00
4.50	6.84	(N/A)	0.00
5.00	8.79	(N/A)	0.00
5.50	10.89	(N/A)	0.00
6.00	13.14	(N/A)	0.00
6.50	15.53	(N/A)	0.00
7.00	18.04	(N/A)	0.00
7.50	20.68	(N/A)	0.00
8.00	23.44	(N/A)	0.00
8.20	24.57	(N/A)	0.00

#### Computation Messages

HW & TW below  
Inv.El.=1.750  
HW & TW below  
Inv.El.=1.750  
HW & TW below  
Inv.El.=1.750  
HW & TW below  
Inv.El.=1.750  
H=.00; Htw=.00;  
Qfree=.00;  
H=.25; Htw=.00;  
Qfree=.19;  
H=.75; Htw=.00;  
Qfree=.97;  
H=1.25; Htw=.00;  
Qfree=2.10;  
H=1.75; Htw=.00;  
Qfree=3.47;

## UHS Rancho Springs 100-yr, 24 hr Detention Analysis

Subsection: Individual Outlet Curves

Label: Composite Outlet Structure - 1

### RATING TABLE FOR ONE OUTLET TYPE

Structure ID = Notch Weir (Rectangular Weir)

Upstream ID = (Pond Water Surface)

Downstream ID = Tailwater (Pond Outfall)

#### Computation Messages

H=2.25; Htw=.00; Qfree=5.06; H=2.75; Htw=.00; Qfree=6.84; H=3.25; Htw=.00; Qfree=8.79; H=3.75; Htw=.00; Qfree=10.89; H=4.25; Htw=.00; Qfree=13.14; H=4.75; Htw=.00; Qfree=15.53; H=5.25; Htw=.00; Qfree=18.04; H=5.75; Htw=.00; Qfree=20.68; H=6.25; Htw=.00; Qfree=23.44; H=6.45; Htw=.00; Qfree=24.57;
---



## UHS Rancho Springs 100-yr, 24 hr Detention Analysis

Subsection: Individual Outlet Curves

Label: Composite Outlet Structure - 1

### RATING TABLE FOR ONE OUTLET TYPE

Structure ID = Riser - 1 (Stand Pipe)

Upstream ID = (Pond Water Surface)

Downstream ID = Tailwater (Pond Outfall)

Water Surface Elevation (ft)	Flow (ft <sup>3</sup> /s)	Tailwater Elevation (ft)	Convergence Error (ft)
0.00	0.00	(N/A)	0.00
0.50	0.00	(N/A)	0.00
1.00	0.00	(N/A)	0.00
1.50	0.00	(N/A)	0.00
1.75	0.00	(N/A)	0.00
2.00	0.00	(N/A)	0.00
2.50	0.00	(N/A)	0.00
3.00	0.00	(N/A)	0.00
3.50	0.00	(N/A)	0.00
4.00	0.00	(N/A)	0.00
4.50	0.00	(N/A)	0.00
5.00	0.00	(N/A)	0.00
5.50	0.00	(N/A)	0.00
6.00	0.00	(N/A)	0.00
6.50	0.00	(N/A)	0.00
7.00	202.53	(N/A)	0.00
7.50	209.64	(N/A)	0.00
8.00	216.51	(N/A)	0.00
8.20	219.20	(N/A)	0.00

#### Computation Messages

E < E1= 7.000
E < E1= 7.000
E < E1= 7.000
E < E1= 7.000
E < E1= 7.000
E < E1= 7.000
E < E1= 7.000
E < E1= 7.000
E < E1= 7.000
E < E1= 7.000
E < E1= 7.000
E < E1= 7.000
E < E1= 7.000
E < E1= 7.000
E < E1= 7.000
E < E1= 7.000
E < E1= 7.000
E < E1= 7.000

## UHS Rancho Springs 100-yr, 24 hr Detention Analysis

Subsection: Individual Outlet Curves

Label: Composite Outlet Structure - 1

### RATING TABLE FOR ONE OUTLET TYPE

Structure ID = Riser - 1 (Stand Pipe)

Upstream ID = (Pond Water Surface)

Downstream ID = Tailwater (Pond Outfall)

#### Computation Messages

Orifice: H =7.00; Riser  
orifice equation  
controlling.

Orifice: H =7.50; Riser  
orifice equation  
controlling.

Orifice: H =8.00; Riser  
orifice equation  
controlling.

Orifice: H =8.20; Riser  
orifice equation  
controlling.

## UHS Rancho Springs 100-yr, 24 hr Detention Analysis

Subsection: Composite Rating Curve

Label: Composite Outlet Structure - 1

### Composite Outflow Summary

Water Surface Elevation (ft)	Flow (ft <sup>3</sup> /s)	Tailwater Elevation (ft)	Convergence Error (ft)
0.00	0.00	(N/A)	0.00
0.50	0.05	(N/A)	0.00
1.00	0.08	(N/A)	0.00
1.50	0.10	(N/A)	0.00
1.75	0.10	(N/A)	0.00
2.00	0.30	(N/A)	0.00
2.50	1.10	(N/A)	0.00
3.00	2.23	(N/A)	0.00
3.50	3.62	(N/A)	0.00
4.00	5.22	(N/A)	0.00
4.50	7.01	(N/A)	0.00
5.00	8.97	(N/A)	0.00
5.50	11.08	(N/A)	0.00
6.00	13.34	(N/A)	0.00
6.50	15.73	(N/A)	0.00
7.00	220.78	(N/A)	0.00
7.50	230.54	(N/A)	0.00
8.00	240.17	(N/A)	0.00
8.20	244.00	(N/A)	0.00

### Contributing Structures

None Contributing

Orifice - 1

Orifice - 1

Orifice - 1

Orifice - 1 + Notch Weir

Orifice - 1 + Notch Weir

Orifice - 1 + Notch Weir

Orifice - 1 + Notch Weir

Orifice - 1 + Notch Weir

Orifice - 1 + Notch Weir

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Orifice - 1 + Notch Weir

Riser - 1 + Orifice - 1 +

Notch Weir

Riser - 1 + Orifice - 1 +

Notch Weir

Riser - 1 + Orifice - 1 +

Notch Weir

Riser - 1 + Orifice - 1 +

Notch Weir

## UHS Rancho Springs 100-yr, 24 hr Detention Analysis

Subsection: Elevation-Volume-Flow Table (Pond)

Label: Onsite Detention Basin

Infiltration	
Infiltration Method (Computed)	No Infiltration
Initial Conditions	
Elevation (Water Surface, Initial)	0.00 ft
Volume (Initial)	0.000 ac-ft
Flow (Initial Outlet)	0.00 ft <sup>3</sup> /s
Flow (Initial Infiltration)	0.00 ft <sup>3</sup> /s
Flow (Initial, Total)	0.00 ft <sup>3</sup> /s
Time Increment	3.000 min

Elevation (ft)	Outflow (ft <sup>3</sup> /s)	Storage (ac-ft)	Area (ft <sup>2</sup> )	Infiltration (ft <sup>3</sup> /s)	Flow (Total) (ft <sup>3</sup> /s)	2S/t + O (ft <sup>3</sup> /s)
0.00	0.00	0.000	0	0.00	0.00	0.00
0.50	0.05	0.022	0	0.00	0.05	10.80
1.00	0.08	0.071	0	0.00	0.08	34.67
1.50	0.10	0.136	0	0.00	0.10	65.87
1.75	0.10	0.172	0	0.00	0.10	83.29
2.00	0.30	0.210	0	0.00	0.30	101.88
2.50	1.10	0.291	0	0.00	1.10	142.08
3.00	2.23	0.378	0	0.00	2.23	184.97
3.50	3.62	0.467	0	0.00	3.62	229.76
4.00	5.22	0.559	0	0.00	5.22	275.59
4.50	7.01	0.650	0	0.00	7.01	321.74
5.00	8.97	0.741	0	0.00	8.97	367.53
5.50	11.08	0.829	0	0.00	11.08	412.13
6.00	13.34	0.912	0	0.00	13.34	454.87
6.50	15.73	0.989	0	0.00	15.73	494.61
7.00	220.78	1.058	0	0.00	220.78	732.95
7.50	230.54	1.114	0	0.00	230.54	769.77
8.00	240.17	1.151	0	0.00	240.17	797.19
8.20	244.00	1.154	0	0.00	244.00	802.50

## UHS Rancho Springs 100-yr, 24 hr Detention Analysis

Subsection: Level Pool Pond Routing Summary

Label: Onsite Detention Basin (IN)

Infiltration			
Infiltration Method (Computed)		No Infiltration	
Initial Conditions			
Elevation (Water Surface, Initial)		0.00 ft	
Volume (Initial)		0.000 ac-ft	
Flow (Initial Outlet)		0.00 ft³/s	
Flow (Initial Infiltration)		0.00 ft³/s	
Flow (Initial, Total)		0.00 ft³/s	
Time Increment		3.000 min	
Inflow/Outflow Hydrograph Summary			
Flow (Peak In)		5.26 ft³/s	Time to Peak (Flow, In)
Flow (Peak Outlet)		4.42 ft³/s	Time to Peak (Flow, Outlet)
			795.000 min
			810.000 min
Peak Conditions			
Elevation (Water Surface, Peak)		3.75 ft	
Volume (Peak)		0.513 ac-ft	
Mass Balance (ac-ft)			
Volume (Initial)		0.000 ac-ft	
Volume (Total Inflow)		2.885 ac-ft	
Volume (Total Infiltration)		0.000 ac-ft	
Volume (Total Outlet Outflow)		2.676 ac-ft	
Volume (Retained)		0.208 ac-ft	
Volume (Unrouted)		-0.001 ac-ft	
Error (Mass Balance)		0.0 %	

## UHS Rancho Springs 100-yr, 24 hr Detention Analysis

Subsection: Pond Routed Hydrograph (total out)

Label: Onsite Detention Basin (OUT)

Peak Discharge	4.42 ft <sup>3</sup> /s
Time to Peak	810.000 min
Hydrograph Volume	2.676 ac-ft

### HYDROGRAPH ORDINATES (ft<sup>3</sup>/s)

Output Time Increment = 3.000 min

Time on left represents time for first value in each row.

Time (min)	Flow (ft <sup>3</sup> /s)	Flow (ft <sup>3</sup> /s)	Flow (ft <sup>3</sup> /s)	Flow (ft <sup>3</sup> /s)	Flow (ft <sup>3</sup> /s)
3.000	0.00	0.00	0.00	0.00	0.00
18.000	0.01	0.01	0.01	0.01	0.01
33.000	0.02	0.02	0.02	0.02	0.03
48.000	0.03	0.03	0.03	0.04	0.04
63.000	0.04	0.04	0.04	0.05	0.05
78.000	0.05	0.05	0.05	0.05	0.05
93.000	0.05	0.05	0.06	0.06	0.06
108.000	0.06	0.06	0.06	0.06	0.06
123.000	0.06	0.06	0.06	0.06	0.06
138.000	0.06	0.06	0.06	0.06	0.06
153.000	0.06	0.07	0.07	0.07	0.07
168.000	0.07	0.07	0.07	0.07	0.07
183.000	0.07	0.07	0.07	0.07	0.07
198.000	0.07	0.08	0.08	0.08	0.08
213.000	0.08	0.08	0.08	0.08	0.08
228.000	0.08	0.08	0.08	0.08	0.08
243.000	0.08	0.08	0.08	0.08	0.08
258.000	0.08	0.09	0.09	0.09	0.09
273.000	0.09	0.09	0.09	0.09	0.09
288.000	0.09	0.09	0.09	0.09	0.09
303.000	0.10	0.10	0.10	0.10	0.10
318.000	0.10	0.10	0.10	0.10	0.10
333.000	0.10	0.10	0.10	0.10	0.10
348.000	0.10	0.11	0.13	0.14	0.16
363.000	0.17	0.19	0.21	0.22	0.24
378.000	0.25	0.27	0.29	0.30	0.34
393.000	0.37	0.40	0.43	0.45	0.48
408.000	0.51	0.54	0.56	0.59	0.61
423.000	0.64	0.66	0.68	0.71	0.73
438.000	0.75	0.78	0.80	0.82	0.84
453.000	0.87	0.89	0.92	0.94	0.96
468.000	0.99	1.02	1.04	1.07	1.10
483.000	1.14	1.18	1.22	1.26	1.30
498.000	1.34	1.37	1.41	1.44	1.48
513.000	1.52	1.55	1.58	1.62	1.65
528.000	1.69	1.72	1.75	1.79	1.83
543.000	1.87	1.90	1.94	1.98	2.02

## UHS Rancho Springs 100-yr, 24 hr Detention Analysis

Subsection: Pond Routed Hydrograph (total out)

Label: Onsite Detention Basin (OUT)

### HYDROGRAPH ORDINATES (ft<sup>3</sup>/s)

Output Time Increment = 3.000 min

Time on left represents time for first value in each row.

Time (min)	Flow (ft <sup>3</sup> /s)	Flow (ft <sup>3</sup> /s)	Flow (ft <sup>3</sup> /s)	Flow (ft <sup>3</sup> /s)	Flow (ft <sup>3</sup> /s)
558.000	2.06	2.10	2.14	2.18	2.22
573.000	2.26	2.31	2.35	2.39	2.44
588.000	2.48	2.53	2.57	2.60	2.61
603.000	2.62	2.62	2.63	2.62	2.61
618.000	2.58	2.56	2.54	2.53	2.53
633.000	2.53	2.53	2.54	2.54	2.56
648.000	2.58	2.60	2.62	2.64	2.66
663.000	2.67	2.68	2.70	2.71	2.72
678.000	2.72	2.73	2.74	2.74	2.74
693.000	2.74	2.73	2.73	2.72	2.72
708.000	2.71	2.71	2.70	2.71	2.73
723.000	2.76	2.79	2.82	2.86	2.91
738.000	2.96	3.02	3.07	3.12	3.17
753.000	3.23	3.29	3.34	3.39	3.45
768.000	3.51	3.56	3.62	3.68	3.75
783.000	3.83	3.91	3.98	4.05	4.12
798.000	4.20	4.28	4.35	4.40	4.42
813.000	4.42	4.42	4.42	4.41	4.37
828.000	4.33	4.28	4.24	4.21	4.18
843.000	4.17	4.15	4.13	4.12	4.12
858.000	4.12	4.11	4.11	4.11	4.11
873.000	4.10	4.10	4.10	4.10	4.09
888.000	4.08	4.08	4.07	4.06	4.05
903.000	4.04	4.02	4.01	4.00	3.98
918.000	3.96	3.94	3.92	3.90	3.86
933.000	3.82	3.79	3.75	3.71	3.67
948.000	3.62	3.59	3.55	3.50	3.41
963.000	3.31	3.21	3.12	3.02	2.89
978.000	2.76	2.63	2.51	2.40	2.28
993.000	2.18	2.09	2.01	1.92	1.84
1,008.000	1.76	1.69	1.62	1.56	1.50
1,023.000	1.45	1.40	1.35	1.31	1.27
1,038.000	1.24	1.21	1.18	1.15	1.12
1,053.000	1.10	1.08	1.07	1.05	1.03
1,068.000	1.02	1.00	0.98	0.97	0.95
1,083.000	0.94	0.92	0.90	0.89	0.88
1,098.000	0.86	0.85	0.84	0.82	0.81
1,113.000	0.79	0.78	0.77	0.75	0.74
1,128.000	0.72	0.70	0.69	0.67	0.66
1,143.000	0.65	0.63	0.62	0.61	0.60
1,158.000	0.60	0.59	0.59	0.58	0.58
1,173.000	0.57	0.57	0.56	0.56	0.55

## UHS Rancho Springs 100-yr, 24 hr Detention Analysis

Subsection: Pond Routed Hydrograph (total out)

Label: Onsite Detention Basin (OUT)

### HYDROGRAPH ORDINATES (ft<sup>3</sup>/s)

Output Time Increment = 3.000 min

Time on left represents time for first value in each row.

Time (min)	Flow (ft <sup>3</sup> /s)	Flow (ft <sup>3</sup> /s)	Flow (ft <sup>3</sup> /s)	Flow (ft <sup>3</sup> /s)	Flow (ft <sup>3</sup> /s)
1,188.000	0.54	0.53	0.52	0.51	0.51
1,203.000	0.50	0.49	0.49	0.48	0.48
1,218.000	0.47	0.47	0.47	0.46	0.46
1,233.000	0.46	0.46	0.45	0.45	0.45
1,248.000	0.44	0.44	0.43	0.43	0.42
1,263.000	0.42	0.42	0.41	0.41	0.41
1,278.000	0.40	0.40	0.40	0.39	0.39
1,293.000	0.39	0.39	0.39	0.39	0.38
1,308.000	0.38	0.38	0.38	0.37	0.37
1,323.000	0.37	0.37	0.37	0.37	0.37
1,338.000	0.37	0.37	0.36	0.36	0.36
1,353.000	0.36	0.35	0.35	0.35	0.34
1,368.000	0.34	0.34	0.33	0.33	0.33
1,383.000	0.33	0.32	0.32	0.32	0.32
1,398.000	0.31	0.31	0.31	0.31	0.31
1,413.000	0.31	0.31	0.30	0.30	0.30
1,428.000	0.30	0.30	0.30	0.30	0.29



## UHS Rancho Springs 100-yr, 24 hr Detention Analysis

Subsection: Pond Inflow Summary

Label: Onsite Detention Basin (IN)

### Summary for Hydrograph Addition at 'Onsite Detention Basin'

Upstream Link	Upstream Node
<Catchment to Outflow Node>	Unit Hydrograph (Onsite Runoff)

### Node Inflows

Inflow Type	Element	Volume (ac-ft)	Time to Peak (min)	Flow (Peak) (ft <sup>3</sup> /s)
Flow (From)	Unit Hydrograph (Onsite Runoff)	2.888	795.000	5.26
Flow (In)	Onsite Detention Basin	2.885	795.000	5.26

## UHS Rancho Springs 100-yr, 24 hr Detention Analysis

Subsection: Diverted Hydrograph

Label: Outlet-1

Peak Discharge	4.42 ft <sup>3</sup> /s
Time to Peak	810.000 min
Hydrograph Volume	2.676 ac-ft

### HYDROGRAPH ORDINATES (ft<sup>3</sup>/s)

Output Time Increment = 3.000 min

Time on left represents time for first value in each row.

Time (min)	Flow (ft <sup>3</sup> /s)	Flow (ft <sup>3</sup> /s)	Flow (ft <sup>3</sup> /s)	Flow (ft <sup>3</sup> /s)	Flow (ft <sup>3</sup> /s)
3.000	0.00	0.00	0.00	0.00	0.00
18.000	0.01	0.01	0.01	0.01	0.01
33.000	0.02	0.02	0.02	0.02	0.03
48.000	0.03	0.03	0.03	0.04	0.04
63.000	0.04	0.04	0.04	0.05	0.05
78.000	0.05	0.05	0.05	0.05	0.05
93.000	0.05	0.05	0.06	0.06	0.06
108.000	0.06	0.06	0.06	0.06	0.06
123.000	0.06	0.06	0.06	0.06	0.06
138.000	0.06	0.06	0.06	0.06	0.06
153.000	0.06	0.07	0.07	0.07	0.07
168.000	0.07	0.07	0.07	0.07	0.07
183.000	0.07	0.07	0.07	0.07	0.07
198.000	0.07	0.08	0.08	0.08	0.08
213.000	0.08	0.08	0.08	0.08	0.08
228.000	0.08	0.08	0.08	0.08	0.08
243.000	0.08	0.08	0.08	0.08	0.08
258.000	0.08	0.09	0.09	0.09	0.09
273.000	0.09	0.09	0.09	0.09	0.09
288.000	0.09	0.09	0.09	0.09	0.09
303.000	0.10	0.10	0.10	0.10	0.10
318.000	0.10	0.10	0.10	0.10	0.10
333.000	0.10	0.10	0.10	0.10	0.10
348.000	0.10	0.11	0.13	0.14	0.16
363.000	0.17	0.19	0.21	0.22	0.24
378.000	0.25	0.27	0.29	0.30	0.34
393.000	0.37	0.40	0.43	0.45	0.48
408.000	0.51	0.54	0.56	0.59	0.61
423.000	0.64	0.66	0.68	0.71	0.73
438.000	0.75	0.78	0.80	0.82	0.84
453.000	0.87	0.89	0.92	0.94	0.96
468.000	0.99	1.02	1.04	1.07	1.10
483.000	1.14	1.18	1.22	1.26	1.30
498.000	1.34	1.37	1.41	1.44	1.48
513.000	1.52	1.55	1.58	1.62	1.65
528.000	1.69	1.72	1.75	1.79	1.83
543.000	1.87	1.90	1.94	1.98	2.02

## UHS Rancho Springs 100-yr, 24 hr Detention Analysis

Subsection: Diverted Hydrograph

Label: Outlet-1

### HYDROGRAPH ORDINATES (ft<sup>3</sup>/s)

Output Time Increment = 3.000 min

Time on left represents time for first value in each row.

Time (min)	Flow (ft <sup>3</sup> /s)	Flow (ft <sup>3</sup> /s)	Flow (ft <sup>3</sup> /s)	Flow (ft <sup>3</sup> /s)	Flow (ft <sup>3</sup> /s)
558.000	2.06	2.10	2.14	2.18	2.22
573.000	2.26	2.31	2.35	2.39	2.44
588.000	2.48	2.53	2.57	2.60	2.61
603.000	2.62	2.62	2.63	2.62	2.61
618.000	2.58	2.56	2.54	2.53	2.53
633.000	2.53	2.53	2.54	2.54	2.56
648.000	2.58	2.60	2.62	2.64	2.66
663.000	2.67	2.68	2.70	2.71	2.72
678.000	2.72	2.73	2.74	2.74	2.74
693.000	2.74	2.73	2.73	2.72	2.72
708.000	2.71	2.71	2.70	2.71	2.73
723.000	2.76	2.79	2.82	2.86	2.91
738.000	2.96	3.02	3.07	3.12	3.17
753.000	3.23	3.29	3.34	3.39	3.45
768.000	3.51	3.56	3.62	3.68	3.75
783.000	3.83	3.91	3.98	4.05	4.12
798.000	4.20	4.28	4.35	4.40	4.42
813.000	4.42	4.42	4.42	4.41	4.37
828.000	4.33	4.28	4.24	4.21	4.18
843.000	4.17	4.15	4.13	4.12	4.12
858.000	4.12	4.11	4.11	4.11	4.11
873.000	4.10	4.10	4.10	4.10	4.09
888.000	4.08	4.08	4.07	4.06	4.05
903.000	4.04	4.02	4.01	4.00	3.98
918.000	3.96	3.94	3.92	3.90	3.86
933.000	3.82	3.79	3.75	3.71	3.67
948.000	3.62	3.59	3.55	3.50	3.41
963.000	3.31	3.21	3.12	3.02	2.89
978.000	2.76	2.63	2.51	2.40	2.28
993.000	2.18	2.09	2.01	1.92	1.84
1,008.000	1.76	1.69	1.62	1.56	1.50
1,023.000	1.45	1.40	1.35	1.31	1.27
1,038.000	1.24	1.21	1.18	1.15	1.12
1,053.000	1.10	1.08	1.07	1.05	1.03
1,068.000	1.02	1.00	0.98	0.97	0.95
1,083.000	0.94	0.92	0.90	0.89	0.88
1,098.000	0.86	0.85	0.84	0.82	0.81
1,113.000	0.79	0.78	0.77	0.75	0.74
1,128.000	0.72	0.70	0.69	0.67	0.66
1,143.000	0.65	0.63	0.62	0.61	0.60
1,158.000	0.60	0.59	0.59	0.58	0.58
1,173.000	0.57	0.57	0.56	0.56	0.55

## UHS Rancho Springs 100-yr, 24 hr Detention Analysis

Subsection: Diverted Hydrograph

Label: Outlet-1

### HYDROGRAPH ORDINATES (ft<sup>3</sup>/s)

Output Time Increment = 3.000 min

Time on left represents time for first value in each row.

Time (min)	Flow (ft <sup>3</sup> /s)	Flow (ft <sup>3</sup> /s)	Flow (ft <sup>3</sup> /s)	Flow (ft <sup>3</sup> /s)	Flow (ft <sup>3</sup> /s)
1,188.000	0.54	0.53	0.52	0.51	0.51
1,203.000	0.50	0.49	0.49	0.48	0.48
1,218.000	0.47	0.47	0.47	0.46	0.46
1,233.000	0.46	0.46	0.45	0.45	0.45
1,248.000	0.44	0.44	0.43	0.43	0.42
1,263.000	0.42	0.42	0.41	0.41	0.41
1,278.000	0.40	0.40	0.40	0.39	0.39
1,293.000	0.39	0.39	0.39	0.39	0.38
1,308.000	0.38	0.38	0.38	0.37	0.37
1,323.000	0.37	0.37	0.37	0.37	0.37
1,338.000	0.37	0.37	0.36	0.36	0.36
1,353.000	0.36	0.35	0.35	0.35	0.34
1,368.000	0.34	0.34	0.33	0.33	0.33
1,383.000	0.33	0.32	0.32	0.32	0.32
1,398.000	0.31	0.31	0.31	0.31	0.31
1,413.000	0.31	0.31	0.30	0.30	0.30
1,428.000	0.30	0.30	0.30	0.30	0.29

## **UHS Rancho Springs 100-yr, 24 hr Detention Analysis**

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Unit Hydrograph (Onsite Runoff) (Read Hydrograph)...4, 5

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APPENDIX C: INLET CAPACITY CALCULATIONS

## Worksheet for 2'x2' Grate Inlet in Sag (Largest runoff)

Project Description	
Solve For	Spread
Input Data	
Discharge	1.30 cfs
Gutter Width	0.00 ft
Gutter Cross Slope	0.000 ft/ft
Road Cross Slope	0.020 ft/ft
Grate Width	2.00 ft
Grate Length	2.0 ft
Local Depression	0.0 in
Local Depression Width	0.0 in
Grate Type	P-50 mm (P-1 -7/8")
Clogging	50.0 %
Results	
Spread	12.9 ft
Depth	3.1 in
Gutter Depression	0.0 in
Total Depression	0.0 in
Open Grate Area	1.8 ft <sup>2</sup>
Active Grate Weir Length	4.0 ft

## Worksheet for 2'x2' Grate Inlet On Grade (Largest runoff)

Project Description	
Solve For	Efficiency
Input Data	
Discharge	1.30 cfs
Slope	0.020 ft/ft
Gutter Width	0.00 ft
Gutter Cross Slope	0.000 ft/ft
Road Cross Slope	0.020 ft/ft
Roughness Coefficient	0.015
Grate Width	2.00 ft
Grate Length	2.0 ft
Grate Type	P-50 mm (P-1 -7/8")
Clogging	50.0 %
Options	
Grate Flow Option	Exclude None
Results	
Efficiency	61.24 %
Intercepted Flow	0.80 cfs
Bypass Flow	0.50 cfs
Spread	6.8 ft
Depth	1.6 in
Flow Area	0.5 ft <sup>2</sup>
Gutter Depression	0.0 in
Total Depression	0.0 in
Velocity	2.80 ft/s
Splash Over Velocity	5.66 ft/s
Frontal Flow Factor	1.000
Side Flow Factor	0.021
Grate Flow Ratio	0.604
Active Grate Length	1.0 ft



## Worksheet for 3' Curb Inlet (Largest runoff)

Project Description	
Solve For	Spread
Input Data	
Discharge	1.00 cfs
Gutter Width	0.00 ft
Gutter Cross Slope	0.000 ft/ft
Road Cross Slope	0.020 ft/ft
Curb Opening Length	3.0 ft
Opening Height	0.8 ft
Curb Throat Type	Horizontal
Local Depression	0.0 in
Local Depression Width	0.0 in
Throat Incline Angle	90.00 degrees
Results	
Spread	11.6 ft
Depth	2.8 in
Gutter Depression	0.0 in
Total Depression	0.0 in

## Worksheet for 7' Curb Inlet (Largest runoff)

Project Description	
Solve For	Spread
Input Data	
Discharge	2.10 cfs
Gutter Width	0.00 ft
Gutter Cross Slope	0.000 ft/ft
Road Cross Slope	0.020 ft/ft
Curb Opening Length	7.0 ft
Opening Height	0.8 ft
Curb Throat Type	Horizontal
Local Depression	0.0 in
Local Depression Width	0.0 in
Throat Incline Angle	90.00 degrees
Results	
Spread	10.8 ft
Depth	2.6 in
Gutter Depression	0.0 in
Total Depression	0.0 in