

Hydrology Report to Determine Area of Influence for Cultivation Irrigation Wells

for

Nina Star Farms

APN: 014-006-16

23180 Shady Grove Road Middletown, CA 95461

September 6, 2021



Prepared for:

Lake County Community Development Department 255 North Forbes Street Lakeport, CA 95453



INTRODUCTION

The purpose of this study is to determine the area of influence on an existing well that will continue to be used for residential domestic supply and irrigation for proposed commercial cannabis. The "Project" is currently proposing 37,446 sf of commercial cannabis canopy area.

The parcels on which the Project is located is owned by Nina Star LLC and will be managed by Nina Bogdonava.

This report estimates the amount of water available and recharge rate during a drought year from the existing wells. In addition, this report estimates the zone of influence to the surrounding and to estimate the cumulative impacts where interference is with existing wells.

STUDY LIMITATIONS

The yield of wells cannot be estimated with precision because of all the uncertainty with the aquifer and the amount of rain percentage of rainfall that percolates through the ground. Therefore, conservative estimates and assumptions are used in this report.

This study is based on the following information and assumptions.

- Cooper Jacob well equation
- Well Completion Reports obtained from Lake Co EHD, and CA State database.
- Well Yield Test and Drillers Reports by Jim's Pumps
- Rainfall for a drought year is 20% of annual precipitation
- Aquifer is uniform throughout the area of well influence

WELL

There is only one (1) well that is proposed to be used for this project that is analyzed in this report. And two residential neighboring wells are analyzed as well. (See Surrounding Well Map in Appendix C). These wells are identified as follows:

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WELL #1

- APN: 014-006-16, Nina Star Primary well for 2BR dwelling and proposed cultivation (37,446 sf canopy).
- Total drill depth of +43 feet below the surface.
- The capacity of the well is at least 16 gpm. (See Appendix A)
- Pump depth: 43 feet
- Unconfined aquifer with thickness of 33feet (10m) (no driller's log available assumed from characteristics of Well #3 below)

WELL #2

- APN: 115-004-05. Owned by Kevin and Barbra Valllauri
- The total drill depth of 125 feet, screen at 30-70 depth(Appendix A 8/4//1999)
- The capacity is only 1.5 gpm.
- Use: 3 BR dwelling unit
- Unconfined aquifer with thickness of 40 feet (12.2m)

WELL #3

- APN: 014-006-14 Owned HiCann LLC
- Total drill depth of 26 feet (Appendix A 8/3/81)
- Capacity of at <u>10 gphr</u> per well driller's report
- Use: 3BR Dwelling
- Unconfined aquifer with thickness of 11 feet (3.35m)
- Note: this property is proposing several acres of +/- 78 acres commercial cannabis canopy. However, the well proposed for cultivation is off site (Well#4) on apn 013-027-08. (Appendix C)

WELL #4

- APN: 013-027-08 Owned HiCann LLC
- Well depth of 716 feet (Appendix A 9/21/2020)
- Capacity of at 10 gpm per well driller's report
- Use: Irrigation Well
- Confined aquifer with thickness of 280 feet (85m)

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WELL RADIUS OF INFLUENCE

The well radius of influence (cumulative impact) is estimated by the Cooper-Jacob equation:

$$R_{(well)} = \sqrt{\frac{2.24584Tt}{S}}$$

Where,

 $R_{(well)} = Radius of Influence (m)$ t = time (seconds) T = transmissivity (m² / day) S = water storage capacity (%) unitless

T = K * b

Where,

K = 2.0 E-4 m/s for Basalt porosity b = aquifer thickness, m t = 1 day = 86,400 seconds S = 0.15,

Therefore;

 $\begin{array}{l} R_{\scriptscriptstyle(1)} => 51\,m = 167 \; feet \\ R_{\scriptscriptstyle(2)} => 56 \; m = 184 \; feet \\ R_{\scriptscriptstyle(3)} => 29 \; m = 97 \; feet \\ R_{\scriptscriptstyle(4)} => 148 \; m = 486 \; feet \end{array}$

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Based on the locations and the calculated Radius of Influences the project Well, Well#1 does not intersect with the wells in the area.

WATER USAGE

The proposed project has water usage for proposed canopy of 0.86 acres (37,446sf) and 2BR Dwelling Unit. For the purposes of this analysis, in an abundance of caution, we have assumed a canopy of 1.0 acres and water usage for 4 employees.

WATER USAGE FROM WELLS #1

The total water usage of the canopy area is estimated by the square footage of the canopy multiplied by the in/year needed for a singe cannabis plant. The in/yr is estimated to be similar to a tomato plant, which is 20in/year.

 $W_{Irrigation} = A * (ft/yr)$

 $W_{Irrigation} = (1.0 \text{ acres}) * (43,560 \text{ sf/acres}) * (1.66 \text{ ft/year}) * (7.48 \text{ gal/cf})$ = 540,875 gal/year

W_{Domestic} = [(4 employees) * (15 gals/employee/day) * (0.7 days/week used)] + (2BR) * (1.5 person/BR) * 75gal/person/day)] * 365 days/year = 97,455 gal/year

Total Water Usage = $W_{Irrigation} + W_{Domesic}$ = 638,330 gal/year

AQUIFER RECHARGE

The proposed project has an estimated total annual water usage of 638,330 gallons per year.

Calculation of Aquifer Recharge is based on the tributary area to the radius of influence of the well. Because of the location of the wells near St. Helena Creek,

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Wm. VanDerWall, R.C.E. 62560 3745 E. Main Street • Kelseyville, CA 95451 • (707) 279-4887 www.vdwengr.com • contact@vdwengr.com

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the aquifer recharge is in two areas. Per map shown in Appendix D, the total recharge area is 277,989 sf.

Given: Annual Precipitation, P = 40 inches per year, assume a drought year is 20% of the annual precipitation, yields 8" (0.66ft) of rainfall. (Note: Rainfall of 2021 for lake county was 9" per NOAA)

Volume of water for recharge = Area x Drought Precipitation x Coefficient of Seepage.

 $V = (277,989 \text{ sf}) \times (0.66 \text{ ft/yr}) \times (7.48 \text{ gal/cf}) \times (0.7)$

V = 960,663 gal/year

960,663 > 638,330 therefore the well is adequate to handle the 1.0 acres of cultivation in a drought year.

CONCLUSION

Per our calculations and assumptions, the project does have an adequate water supply for the proposed irrigation use. However, the project must be limited to 1 acre of canopy and irrigated with dripline only. Canopy size exceeding 1 acre will require the development of a new well(s).

Through our calculations, review of available Well Completion Reports and Pump Yield Tests, the proposed use of the well onsite does not interfere with surrounding wells.

The well on the property (apn: 14-006-17) will not be impacted by the Nina Star Farm because the well's radius of influence do not intersect. The distance between the well radius of the project well, and the neighboring well is approximately 186' based on our theoretical calculations noted in this report. The neighboring well has pump yield test of 1.5 gpm which is very poor. Per conversations with the owner, the well is near dry and water is delivered to the site during drought years (currently).

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Well Completion & Test Results (A) Well Area of Influence Map (B) Surrounding Aerial Map (C) Well Recharge Area (D)

Α





Hole to Home

WELL PERFORMANCE TEST REPORT

Client Name: NinaStar LLC Property Location: 23180 Shady Grove, Middletown, CA Parcel Number: 014-006-16 Number of Wells Evaluated: One Well Performance Test Completion Date: March 12, 2020 Water Samples Collected: No Pump Technician: Jim Jackson

Location Description: 38.718582, -122.613146 (WGS84) Total Depth: 43-feet below top of casing Depth to Static Water Level: 10.33-feet below the top of casing Diameter of well: 10-inches Casing type: Steel Test Duration: 2-hours Test Type: Pump Pumping Rate: 16-Gallons Per Minute (GPM)

Observations: JAK Drilling & Pump (JAK) performed a visual inspection of the well on March 12, 2020. The well is located on the northwest side of the access road that runs along the eastern edge of the property (see Well Location Map attached). There is an existing and operational ½-horse 230volt submersible pump, of unknown production specifications, installed in the well that is supplied power via connection to PG&E power supply.

Well Performance Pump Test: The four-hour pump test was conducted using the existing submersible pump and in accordance with industry standards. The static water level within the well was measured prior to the start of the test. Once the performance test began, the depth-to-water or pumping level was measured manually with a Powers Water Meter in the well every five minutes during the first half hour of the test and then every 10-minutes for the next hour of the test. The measurement interval was then increased to every 30-minutes for the remainder of the four-hour test. The pumping rate was measured by timing the flow into a volume verified 5-gallon bucket. The pumping rate was measured at the same intervals as the pumping level. Both the depth-to-water/pumping level and pumping rate measurements are summarized in the attached table.

The static water level was measured at 10.33-feet below the top of casing at the start of the performance test. The maximum drawdown of 1.5-feet at 11.83-feet below the top of casing was observed immediately after the start of the test. The pumping level remained constant at 11.83-feet below the top of casing for the duration of the test. The pumping rate, measured by timing



the flow into a volume verified 5-gallon bucket, remained a constant 16.0-GPM for the duration of the test. The performance test was concluded after the production rate and the pumping level remained constant for at least 2-hours.

After 2-hours of pumping, the well pump was shut off and the well was then allowed to rest and recharge. The depth-to-water was measured in the well after 10-minutes at 11.0-feet and then again after 30-minutes at 10.33-feet below the top of casing. The resulting recharge rate of 100% indicates the well has a strong recovery.

Disclaimer:

Observations made of the well(s) are strictly limited to the date and time that the test(s) was conducted and are in no way a guarantee of future conditions, including but not limited to the quantity and/or quality of the water produced by this well.

Please feel free to contact our office if there are any questions regarding the well test and/or well test report.

Sincerely,

Jessica Moreno JAK Drilling & Pump

Attachments: Well Location Map Table 1: Well Performance Test Data





WELL LOCATION MAP 23180 Shady Grove

Middletown, CA





TABLE 1 WELL PERFORMANCE TEST DATA 23180 Shady Grove Rd, Middletown, CA March 12, 2020

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13:00	Static	10.33				
13:05	16.00	11.83				
13:10	16.00	11.83				
13:15	16.00	11.83				
13:20	16.00	11.83				
13:25	16.00	11.83				
13:30	16.00	11.83				
13:40	16.00	11.83				
13:50	16.00	11.83				
14:00	16.00	11.83				
14:10	16.00	11.83				
14:20	16.00	11.83				
14:30	16.00	11.83				
15:00	16.00	11.83				
15:10	RECHARGE	11.00				
15:30	RECHARGE	10.33				

Flow rate measured by timing flow into a volume confirmed 5-gallon bucket.

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WELL #4

WELL PRODUCTION REPORT

Client: HiCann LLC Well Location: 22999 South State Highway 29, Middletown, CA APN: 013-027-08 Location Description: 38.72181, -122.60500 Total Depth: 716-feet below ground surface (bgs) Diameter of well: 5 inches Casing type: PVC Production Rate: 100-gallons per minute Test Duration: 8-hours Test Type: Airlifting % Recharge: 100

Observations: JAK was retained by the client for the purpose of drilling and installing a new water well. The well has been drilled to a depth of 716-feet below ground surface using a mud-rotary style method of drilling. The well was cased to 716-feet using 5-inch PVC well casing with the annular space gravel packed and sealed per industry standards. As part of the well completion process, JAK airlifted the well for approximately 8-hours on November 28, 2020. Airlifting allows the driller to remove additional fines and sediments from the well that could potentially foul a submersible pump while also evaluating the production rate for the new well. Typically, when a pump test is completed, the pumping level (or water level) is measured in the well at set intervals for the duration of the test. However, due to the dynamic nature of airlifting it is impossible to measure the pumping level during the test therefore only the static water level and the recovery or recharge water level was measured. The water produced via airlifting was directed into a 5-inch discharge pipe temporarily connected to the well with the volume measured by timing the flow through a discharge weir.

Prior to airlifting, the static water level was measured at 46-feet below ground surface. The well was then airlifted for 8-hours and as expected, the volume of water produced from the well increased with the removal of the fine sediments. Initially the production rate of the well measured at 30-gallons per minute then as the clarity of the water improved the production rate increased to 100-gallons per minute. After 8-hours of airlifting the well was then allowed to rest and recharge. Following 30-minutes of inactivity the water level in the well was measured and at 44-feet below ground surface indicating that the well had fully recharged.

Disclaimer: Observations made of the well(s) are strictly limited to the date and time that the test(s) was conducted and are in no way a guarantee of future conditions, including but not limited to the quantity and/or quality of the water produced by this well.

Please feel free to contact our office if there are any questions regarding the well test and/or well test report.

Sincerely,

Jessica Moreno Operations Manager JAK Drilling & Pump

Attachments: Well Location Map



State of California Well Completion Report Form DWR 188 Submitted 12/18/2020 WCR2020-017295

WELL #4

Owner's Well Nur	mber 1				Date Work	Begar	n 09/21	/2020		C	ate Wor	k Ended	11/29/	2020	
Local Permit Age	ncy Lake C	County Health	Services	Departme	nt - Enviror	nmenta	al Health D	ivision							
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500	540	quartz with iron
540	560	blue shale, with iron, quartz = possible water
560	580	quartz with iron and some basalt
580	610	quartz and basalt - possible water
610	620	brown clay, basalt and quartz
620	660	iron, quartz, basalt
660	680	iron, quartz, shale, basalt - Possible Water
680	700	basalt, sandstone - possible water
700	716	basalt

					Casing	s					
Casing #		m Surface o Feet	Casing Typ	oe Material	Casings Specificatons	Wall Thickness (inches)	s Outside Diameter (inches)	Screen Type	Slot Size if any (inches)	Description	
1	0	80	Blank	PVC	N/A	0.214	4.5			Well Casing	
1	80	100	Screen	PVC	N/A	0.214	4.5	Milled Slots	0.032	Screen	
1	100	120	Blank	PVC	N/A	0.214	4.5			SOLID	
1	120	140	Screen	PVC	N/A	0.214	4.5	Milled Slots	0.032	screen	
1	140	160	Blank	PVC	N/A	0.214	4.5			Well casing	
1	160	180	Screen	PVC	N/A	0.214	4.5	Milled Slots	0.032	Well Casing	
1	180	200	Blank	PVC	N/A	0.214	4.5			Well Casing	
1	200	220	Screen	PVC	N/A	0.214	4.5	Milled Slots	0.032	well casing	
1	220	240	Blank	PVC	N/A	0.214	4.5			well casing	
1	240	260	Screen	PVC	N/A	0.214	4.5	Milled Slots	0.032	well casing	
1	260	280	Blank	PVC	N/A	0.214	4.5			well casing	
1	280	300	Screen	PVC	N/A	0.214	4.5	Milled Slots	0.032	Well Casing	
1	300	320	Blank	PVC	N/A	0.214	4.5			Well Casing	
1	320	340	Screen	PVC	N/A	0.214	4.5	Milled Slots	0.032	Well Casing	
1	340	360	Blank	PVC	N/A	0.214	4.5			Well Casing	
1	360	380	Screen	PVC	N/A	0.214	4.5	Milled Slots	0.032	Well Casing	
1	380	400	Blank	PVC	N/A	0.214	4.5			Well Casing	
1	400	420	Screen	PVC	N/A	0.214	4.5	Milled Slots	0.032	Well Casing	
1	420	480	Blank	PVC	N/A	0.214	4.5			Well Casing	
1	480	500	Screen	PVC	N/A	0.214	4.5	Milled Slots	0.032	Well Casing	
1	500	520	Blank	PVC	N/A	0.214	4.5			Well Casing	
1	520	540	Screen	PVC	N/A	0.214	4.5	Milled Slots	0.032	Well Casing	
1	540	560	Blank	PVC	N/A	0.214	4.5			well casing	
1	560	580	Screen	PVC	N/A	0.214	4.5	Milled Slots	0.032	well casing	
1	580	600	Blank	PVC	N/A	0.214	4.5			WELL CASING	
1	600	620	Screen	PVC	N/A	0.214	4.5	Milled Slots	0.032	well casing	
1	620	640	Blank	PVC	N/A	0.214	4.5				
1	640	660	Screen	PVC	N/A	0.214	4.5	Milled Slots	0.032	well casing	
1	660	680	Blank	PVC	N/A	0.214	4.5			well casing	
1	680	700	Screen	PVC	N/A	0.214	4.5	Milled Slots	0.032	well casing	
1	700	716	Blank	PVC	N/A	0.214	4.5			cellar	
					Annular Ma	terial					
Śur	f rom face to Feet	Fill		Fill Type Details				Size	Description		
25	716	Filter F	Pack Othe	er Gravel Pack		F	ea Gravel		double wa	ashed pea gravel	
0	25	Bento	nite Othe	er Bentonite					hydrated	bentonite sanitary seal	

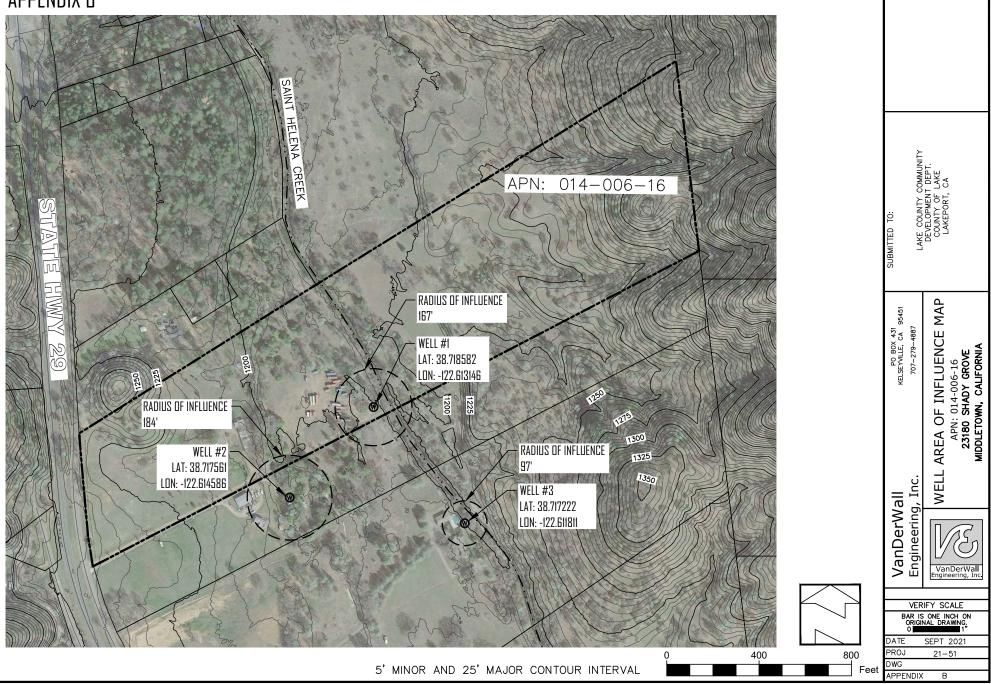
Other Observations:

Initially began drilling boring using air hammer, hole started falling a part around 280-feet and had to switch to mud-rotary style of drilling. Cleared hole and continued drilling to terminal depth of 716-feet below ground surface.

	В	orehole Specifications	Certification Statement								
Depth from Borehole Diameter (inches) Feet to Feet Feet to Feet			I, the undersigned, certify that this report is complete and accurate to the best of my knowledge and belief Name JAK DRILLING AND PUMP, Kharom Hellwege Person, Firm or Corporation								
0 25	25 716	10.875 7.875]	Person, Pri PO Box Addre	(250	Middletown City	CA State	95461 Zip			
			Signed		<i>signature</i> ed Water Wel	12/18/2020 Date Signed		13957 ense Number			
		Attachments			D	WR Use	e Only				
Well Produ	Well Production Report 11.30.2020.pdf - Other			State We	ell Number		Site Code	Local W	ell Number		
			La TRS:	titude De	g/Min/Seo	N	Longitude	e Deg/Mi	n/Sec		
			APN:								

В

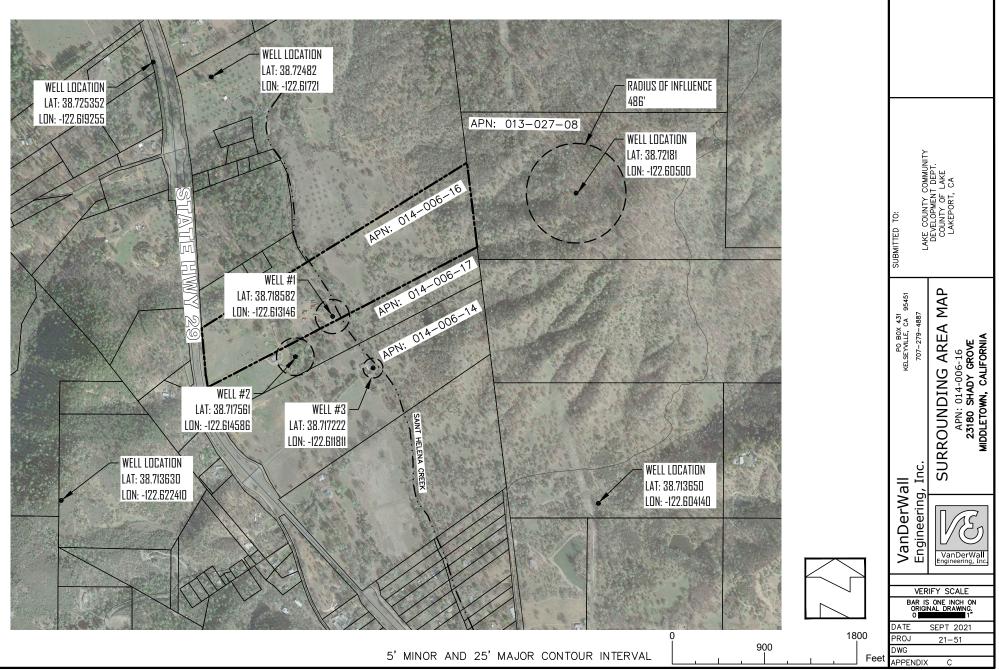
Well Area of Influence Map APPENDIX B



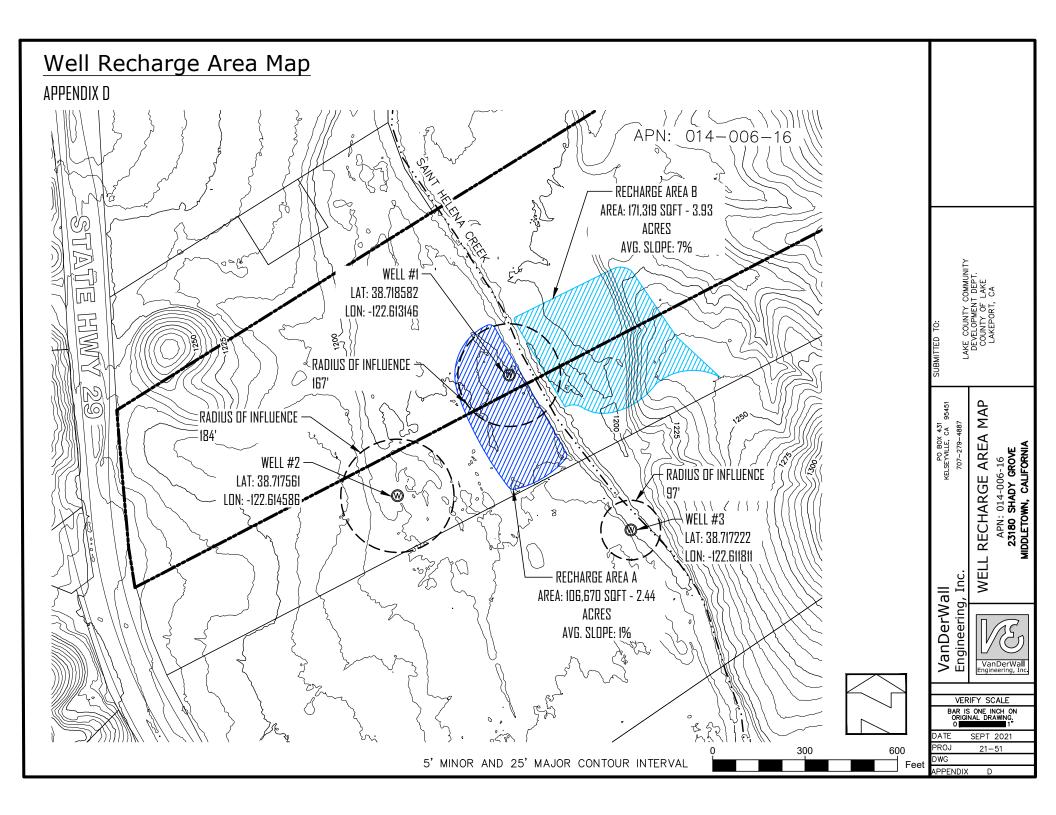
С

Surrounding Area Map

APPENDIX C



D



Drought Management Plan

<u>Purpose</u>

This Drought Management Plan has been prepared to fulfil the requirement for the Board of Supervisors Ordinance NO. 3106, adopted on July 27th, 2021. This plan is designed to conserve Lake County's water resources given the current emergency drought conditions. This plan has been created in combination with the previously submitted & reviewed Water Use Management Plan which outlined the proposed projects water use practices. The proposed methods aim to reduce water use by providing the most efficient delivery system and having as many preventative measures as possible in place to reduce to wasted water.

Methods to conserving water

The proposed projects most important aspect to reducing the amount of water used for irrigation is by utilizing drip irrigation directly into the root system of each plant. According to the USDA Natural Resources Conservation Service Irrigation Guide ("Irrigation Guide." USDA, Sept 1997, https://www.nrcs.usda.gov/Internet/FSE_DOCUMENTS/nrcs144p2_033068.pdf) drip irrigation with proper water management, can be in the range of 80 to 90 percent effective for the area irrigated. Drip irrigation maximizes the efficiency by reducing the amount of water that is lost to evaporation as well as runoff. The greenhouses are fully enclosed so there is no potential for runoff, which allows for immediate recapturing of excess water underneath the cultivation beds to further maximize water use efficiency. Additionally, due to the greenhouses being fully enclosed they are capable of optimizing the internal environment. This means controlling the humidity and light level which reduces the amount of water needed to irrigate each plant.

The proposed project plans to supplement the soil with compost from the vegetative waste produced by the plants. The composted soils, elevated in nutrients will be mixed in the cultivation medium to further improve the soil health and ultimately increase its water-holding capacity. Mulch not only insulates and protects the lower soil levels from drying up, but also increases the rate of water absorption.

Water will only be delivered to the plants through the holding tanks and not directly from the well. The water storage tanks will be equipped with float valves to prevent overflow and runoff of irrigation water when full. Additionally, safety valves will be equipped to supply lines in case the flow of water needs to be stopped in an emergency situation.

Hydrology Report

The hydrology report was prepared by VanDerWall Engineering on September 6, 2021. Outlined below are key take away from the report, however for the full results please see the submitted hydrology report:

- The project does have an adequate water supply for the proposed irrigation use. However, the project must be limited to 1 acre of canopy and irrigated by dripline only.
- The proposed use of the well onsite does not interfere with surrounding wells.