

ALLARD ENGINEERING

civil engineering land surveying land planning

TRACT 17841 APN 0434-063-02

At the corner of Navajo and Sandia Road, Apple Valley, CA

Drainage Report

November 10, 2020

Prepared By: Allard Engineering 16866 Seville Avenue Fontana, CA 92335 (909) 356-1815 Fax (909) 356-1795

Prepared under the supervision of:

Street PROFESSIONATION

Rayl l. allart

Raymond J Allard, P.E. RCE 36052 Exp. 06-30-22

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Discussion

Introduction

APN 0434-063-02 is a tract (Tract# 17841) proposed to be developed as a multifamily dwelling (Apartment) site in Apple Valley, California. The site is located at the northwest corner of Navajo Road and Sandia Road and lies within a sparsely but developing area. The site is located within the tributary of the proposed Master Plan Storm Drain System (S-01) prepared by the San Bernardino County Flood Control District in 1996. Upon build out of the master plan, there will be trapezoidal natural channel (80' base width, 10' depth, 3:1 side slope) running across the site which will drain to Navajo Road. The master plan facility (S-01) sized for an average Q100 of 6,702cfs across the site. The Town will ultimately improve the channel downstream

Purpose

The purpose of this Drainage Report is to assess the existing and future flows that affect the site and provide necessary flood protection. The criteria utilized for hydrologic analysis is the San Bernardino County Hydrology Manual. San Bernardino Master Drainage Plan and AES software was used to calculate the maximum water surface elevation for the estimated peak runoff from the offsite tributary area that runs through the proposed site. Also we have calculated the water surface depth in the same master storm plan Line S-01in developed condition of the proposed tract.

Criteria

Findings

The existing topography of this site slopes from southwest towards the northwest at approximately 0.4% slope. The site has the evidence of flows within the existing drainage swale crossing the site from southwest towards the northeast. This existing drainage swale carries the storm runoff as indicated in the Master Plan of Drainage.

In the proposed condition the site will be developed as multifamily dwelling (Apartment complex) and in ultimate condition the site will drain to the proposed earthen trapezoidal channel (at the footprint of the existing flowline) which will be built per the ultimate facility according to the Apple Valley Master Plan of Drainage as designated as Line S-01 [Base width (b): 80-ft, Channel Depth (h): 10-ft, Side Slope(z): 3:1 with a slope of 0.004] on Comprehensive Storm Drain Plan (See attached reference documents). This proposed channel (Line S-01) will convey runoff from upstream offsite areas and onsite area in a northeasterly direction at a slope of 0.4 and drain to Navajo Road per the Master Drainage Plan.

Per the Comprehensive Storm Drain Plan, the ultimate facility (Line S-01) will carry a total runoff of 6,702 cfs from offsite tributary areas and onsite area from a 100-year storm event and will drain to the northeast towards Navajo Road. For proposed site development we ran the Rational Method Hydrology calculation and estimated that a flow of 55.5 cfs will be generated. We add this runoff from onsite with ultimate flow (6,702-cfs) and ran the hydraulic calculation to estimate the water depth and top width of the proposed channel (See attached RM hydrology calc and the hydraulic calculations in Reference Material Section). Line S-01 of the Comprehensive Storm Drain has the capacity to handle the runoff and will only increase the flow depth by about 0.5 inch. Flow depth calculated for Line S-01 with undeveloped site condition is 7.41-ft where as it is 7.45-ft. Therefore, the proposed ultimate facility (Line S-01) will be able to transfer upstream offsite tributary area and the onsite runoff in safe manner.

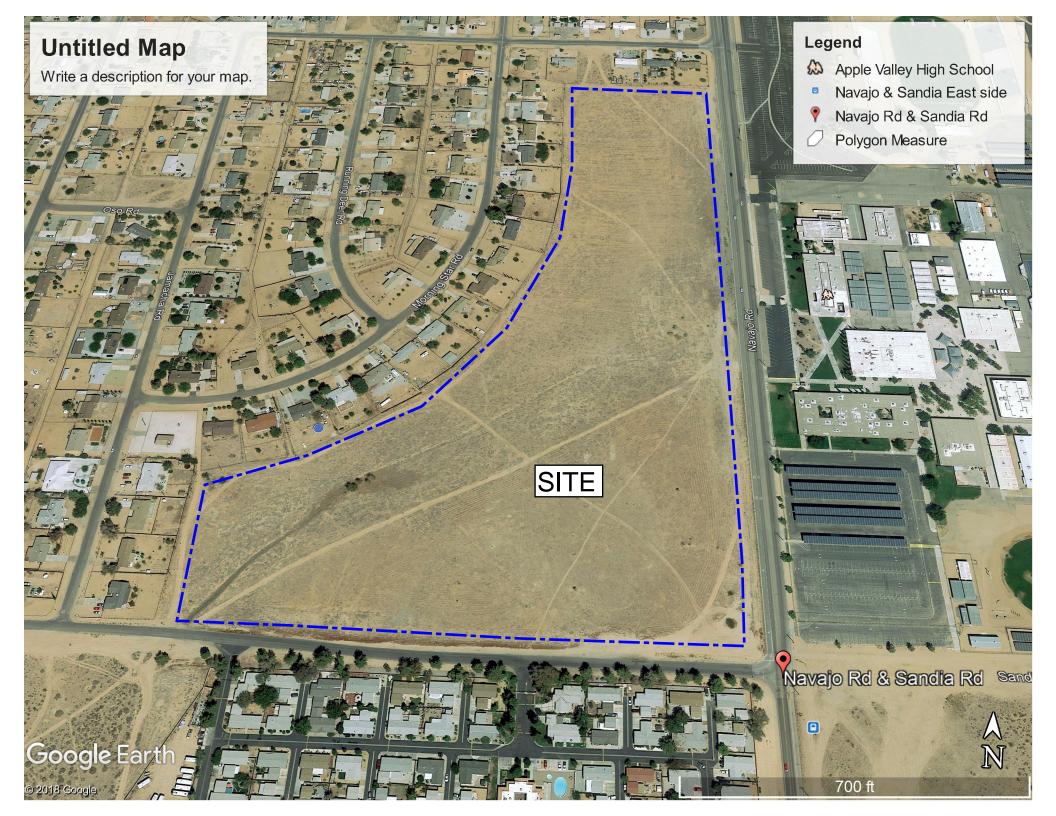
It is proposed a segment of the channel (Around 50-ft segment) approximately 20-ft upstream from Navajo Road to be built 2-ft deeper than the proposed depth (10-ft) to incorporate Water Quality Volume retention/infiltration purposes. The proposed channel will daylight at around 20-ft upstream from ROW of Navajo Road. Please refer to the Drainage Exhibit attached here on with the report.

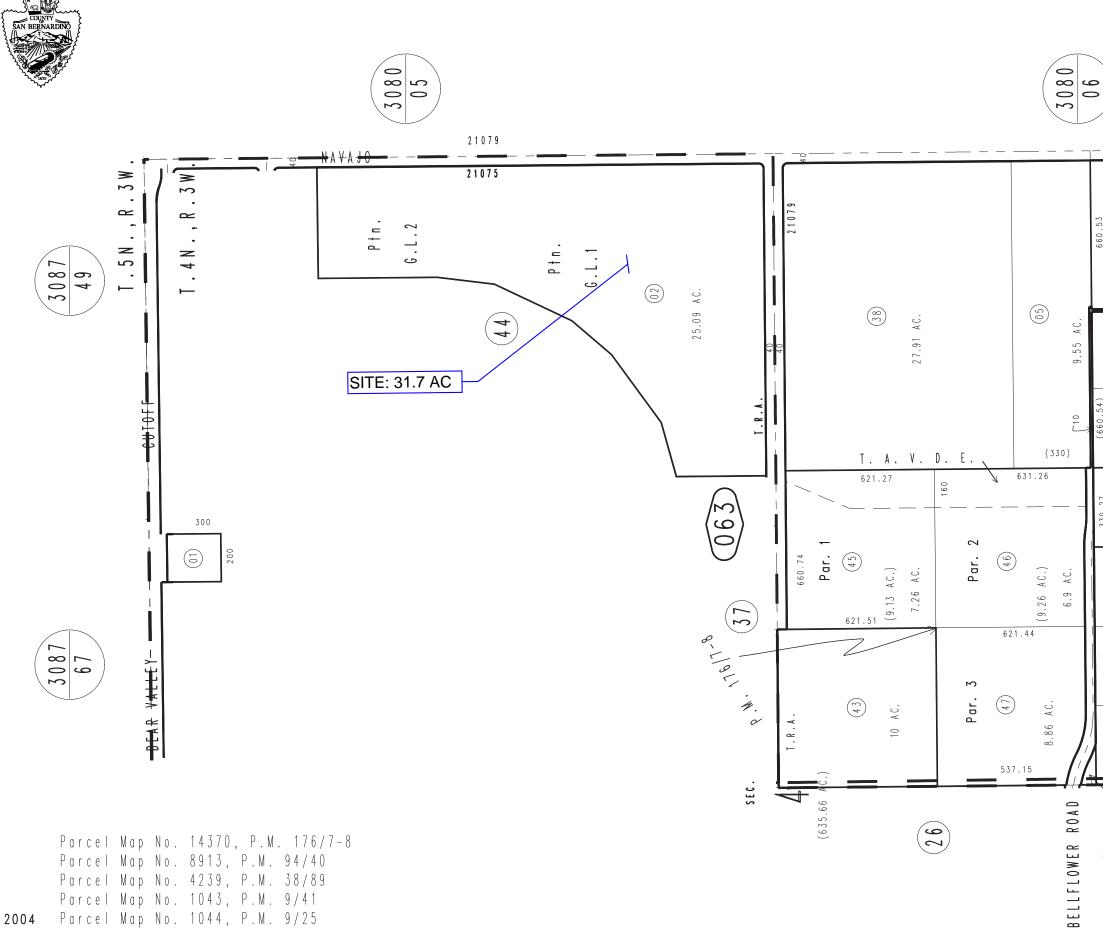
Since there is no downstream outlet at this time due to the High School not being required to construct the channel, the system ends at Navajo Road. If an event occurs that would cause ponding to a depth that would over flow the channel, the water would enter Navajo Road like it does today. This is highly unlikely due to the watershed not being nearly fully developed. The Town assures that there will be no increased runoff with their detention basin policy. The channel is fenced like all flood control facilities and gates can be locked during a storm event.

A small pilot channel will be constructed in the channel to contain low flow and nuisance flows, This will allow for some passive recreational use to occur in the main channel.

Calculations and exhibits are attached to support these findings.

REFERENCE MATERIALS

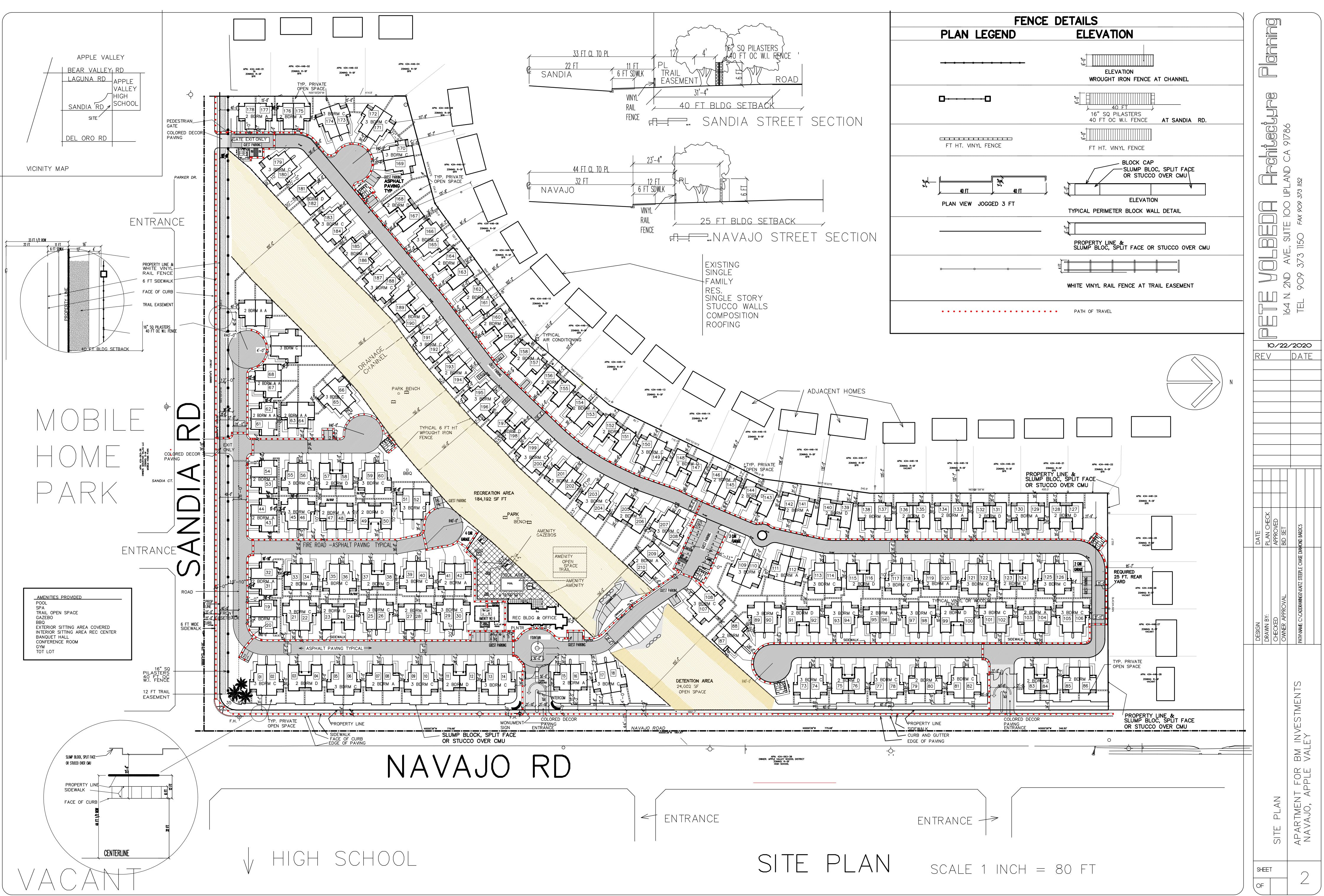


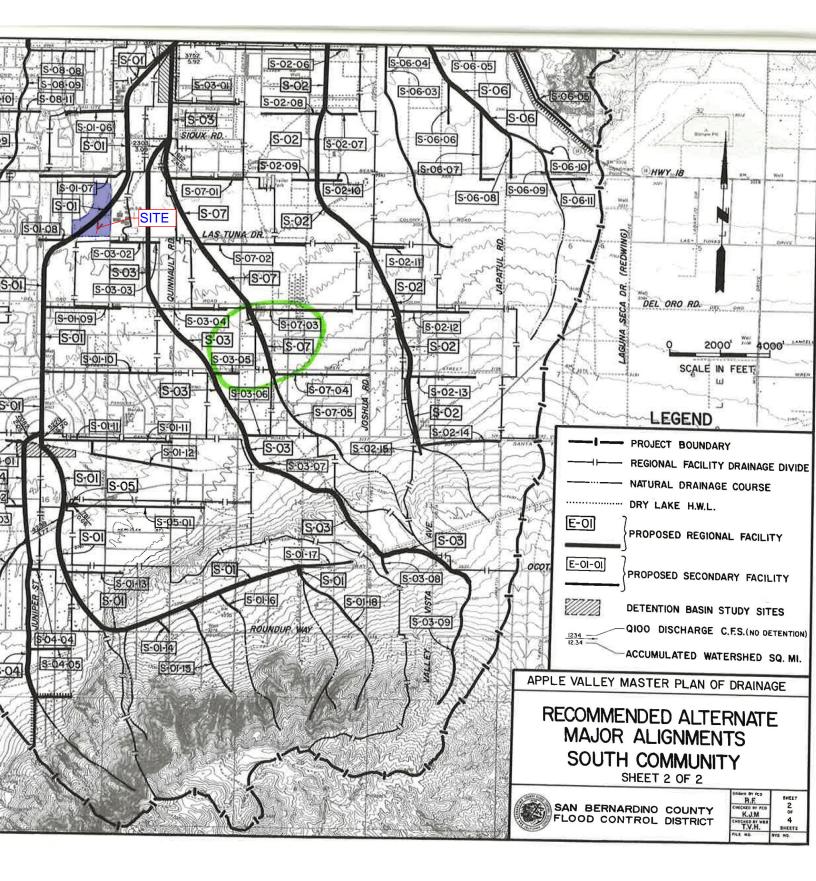


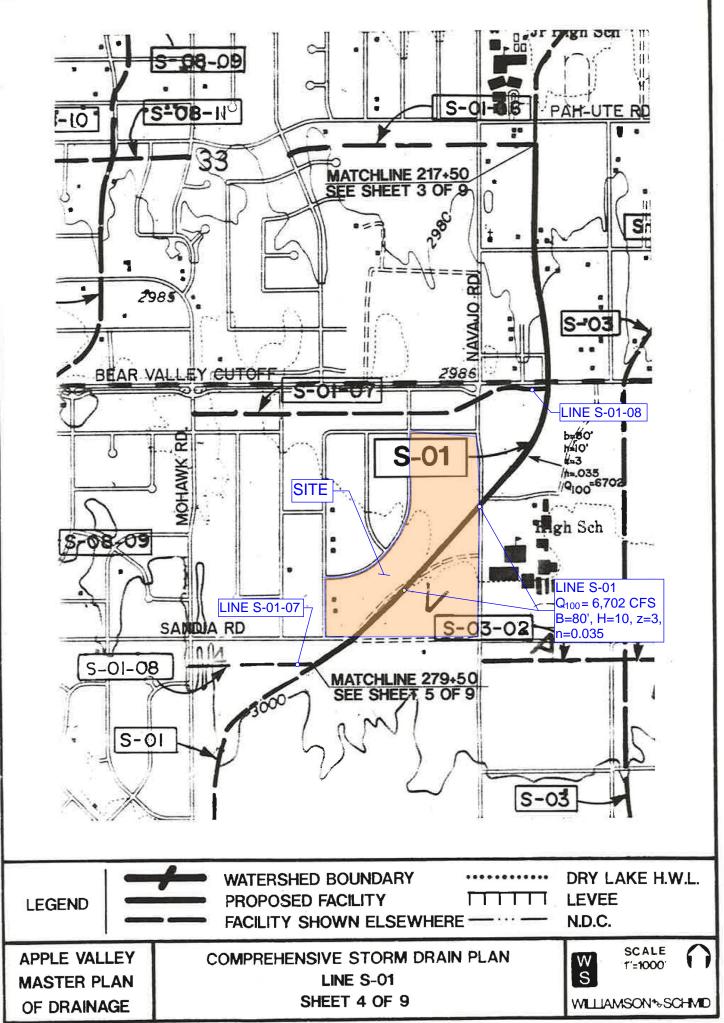
April 2004 Parcel Map No. 1044, P.M. 9/25

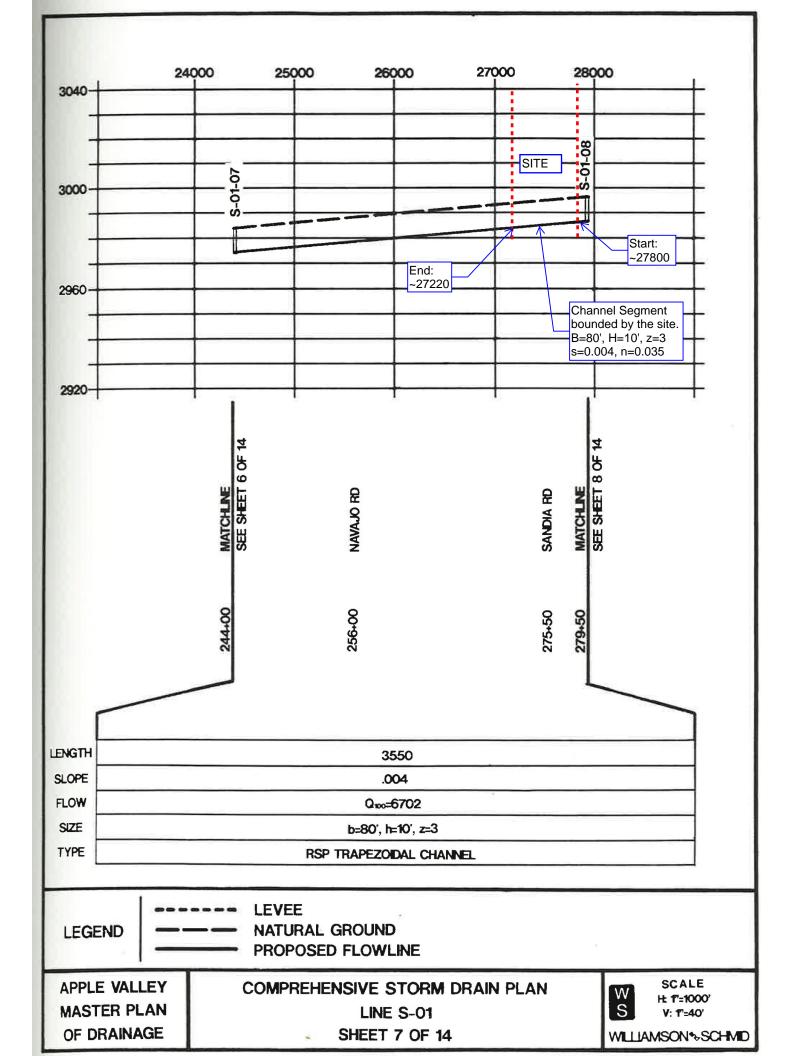
Parcel Map No. 1043, P.M. 9/41

Town of Apple Valley 0434—06 Tax Rate Area 21075 21079 Ш⁰⁰ -ROAD660.88 660.87 660.53 Par. 2 80 Par. $\begin{pmatrix} L \\ 0 \end{pmatrix}$ AC. AC. 9.9 9.9 Par 661.06 (661.07) 1 d ar. 3 8 | 89 33 С 10 (N) 36 Ē 4 Par 35 44) 2 d $\begin{pmatrix} 5\\ 0 \end{pmatrix}$ (660. $\binom{5}{2}$ $\binom{2}{4}$ 660 (J4) Par 1 \leftarrow (661.26) 45 330.63 330.63 4 330.25 Par. 2 Par. 1 Par. (13) (Ξ) 330. 0 Par. 330. 14/6 330.67 330.68 330.68 $\begin{pmatrix} 4\\2 \end{pmatrix}$ 4. 66 $\begin{pmatrix} 4\\ 0 \end{pmatrix}$ (7 Par.4 AC. Par.1 $\begin{pmatrix} - \\ - \\ - \\ - \end{pmatrix}$ ഹ 01 46.4.0 Par.3-Par.2 $\begin{pmatrix} 5 \\ 0 \end{pmatrix}$ (0) $\begin{pmatrix} 5 \\ 5 \end{pmatrix}$ 2.5AC. 2.5AC. AC. (=) $\begin{pmatrix} 7 \\ 7 \end{pmatrix}$ 6 2.5AC. .5AC. 0 ∢ 30 33 (*) Par. REVISED 10/30/10 KC Assessor's Map Book 0434 Page 06 San Bernardino County









ONSITE HYDROLOGY CALCULATION Rational Method Hydrology

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE (Reference: 1986 SAN BERNARDINO CO. HYDROLOGY CRITERION) (c) Copyright 1983-2006 Advanced Engineering Software (aes) Ver. 13.0 Release Date: 06/01/2006 License ID 1400 Analysis prepared by: Allard Engineering 16866 Seville Avenue Fontana Ca. 92335 Tel. 909-356-18185, Fax. 909-356-1795 * NAVAJO TRACT, APPLE VALLY * * ONSITE-DEVELOPED CONDITION * 100-YR STORM EVENT FILE NAME: NAVAJO.DAT TIME/DATE OF STUDY: 16:00 10/16/2019 _____ USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION: --*TIME-OF-CONCENTRATION MODEL*--USER SPECIFIED STORM EVENT(YEAR) = 100.00 SPECIFIED MINIMUM PIPE SIZE(INCH) = 60.00 SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90 *USER-DEFINED LOGARITHMIC INTERPOLATION USED FOR RAINFALL* SLOPE OF INTENSITY DURATION CURVE(LOG(I; IN/HR) vs. LOG(Tc; MIN)) = 0.6000 USER SPECIFIED 1-HOUR INTENSITY(INCH/HOUR) = 1.0200 *ANTECEDENT MOISTURE CONDITION (AMC) III ASSUMED FOR RATIONAL METHOD* *USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL* HALF- CROWN TO STREET-CROSSFALL: CURB GUTTER-GEOMETRIES: MANNING WIDTH CROSSFALL IN- / OUT-/PARK- HEIGHT WIDTH LIP HIKE FACTOR (FT) SIDE / SIDE/ WAY (FT) (FT) (FT) (FT) (FT) NO (n) --- ---- ----- ------ ----- ----- -----1 30.0 20.0 0.018/0.018/0.020 0.67 2.00 0.0313 0.167 0.0150 GLOBAL STREET FLOW-DEPTH CONSTRAINTS: 1. Relative Flow-Depth = 0.00 FEET as (Maximum Allowable Street Flow Depth) - (Top-of-Curb) 2. (Depth)*(Velocity) Constraint = 6.0 (FT*FT/S) *SIZE PIPE WITH A FLOW CAPACITY GREATER THAN OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.* *USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED FLOW PROCESS FROM NODE 10.00 TO NODE 20.00 IS CODE = 21 _____ >>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<< >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<< ______ INITIAL SUBAREA FLOW-LENGTH(FEET) = 1540.00 ELEVATION DATA: UPSTREAM(FEET) = 3003.00 DOWNSTREAM(FEET) = 2996.00 Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20 SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 17.949

* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 2.104 SUBAREA TC AND LOSS RATE DATA(AMC III): DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS Tc GROUP (ACRES) (INCH/HR) (DECIMAL) CN (MIN.) LAND USE APARTMENTS 31.70 0.80 0.200 52 17.95 A SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.80 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.200 SUBAREA RUNOFF(CFS) =55.49TOTAL AREA(ACRES) =31.70PEAK FLOW RATE(CFS) = 55.49 _____ END OF STUDY SUMMARY: TOTAL AREA(ACRES)=31.70TC(MIN.)=17.95EFFECTIVE AREA(ACRES)=31.70AREA-AVERAGED Fm(INCH/HR)=0.16 AREA-AVERAGED Fp(INCH/HR) = 0.80 AREA-AVERAGED Ap = 0.200 PEAK FLOW RATE(CFS) = 55.49 _____ _____ END OF RATIONAL METHOD ANALYSIS



NOAA Atlas 14, Volume 6, Version 2 Location name: Apple Valley, California, USA* Latitude: 34.4655°, Longitude: -117.192° Elevation: 2993.55 ft** * source: ESRI Maps ** source: USGS



POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Sarah Dietz, Sarah Heim, Lillian Hiner, Kazungu Maitaria, Deborah Martin, Sandra Pavlovic, Ishani Roy, Carl Trypaluk, Dale Unruh, Fenglin Yan, Michael Yekta, Tan Zhao, Geoffrey Bonnin, Daniel Brewer, Li-Chuan Chen, Tye Parzybok, John Yarchoan

NOAA, National Weather Service, Silver Spring, Maryland

PF tabular | PF graphical | Maps & aerials

PF tabular

PDS-based point precipitation frequency estimates with 90% confidence intervals (in inches) ¹									es) ¹		
Duration	Average recurrence interval (years)										
	1	2	5	10	25	50	100	200	500	1000	
5-min	0.078 (0.064-0.095)	0.110 (0.091–0.135)	0.155 (0.128–0.190)	0.194 (0.158–0.240)	0.250 (0.197-0.319)	0.295 (0.228-0.386)	0.344 (0.260-0.461)	0.397 (0.292–0.547)	0.473 (0.333-0.678)	0.535 (0.364-0.793	
10-min	0.112 (0.092-0.137)	0.158 (0.130-0.193)	0.222 (0.183-0.273)	0.278 (0.227-0.344)	0.358 (0.283-0.458)	0.423 (0.327-0.553)	0.494 (0.372-0.661)	0.569 (0.418-0.783)	0.678 (0.477-0.972)	0.766 (0.522-1.14)	
15-min	0.135 (0.112-0.165)	0.191 (0.157–0.234)	0.269 (0.221–0.330)	0.336 (0.274–0.416)	0.433 (0.342-0.554)	0.512 (0.396-0.669)	0.597 (0.450-0.799)	0.688 (0.505-0.947)	0.820 (0.577-1.18)	0.927 (0.631–1.38)	
30-min	0.185 (0.153-0.227)	0.261 (0.216-0.320)	0.368 (0.303-0.452)	0.460 (0.375-0.569)	0.593 (0.468-0.758)	0.701 (0.542–0.916)	0.817 (0.617–1.09)	0.943 (0.692–1.30)	1.12 (0.791–1.61)	1.27 (0.864–1.88)	
60-min	0.232 (0.192-0.284)	0.328 (0.270-0.401)	0.461 (0.379–0.566)	0.576 (0.470-0.713)	0.743 (0.586-0.950)	0.879 (0.679–1.15)	1.02 (0.773–1.37)	1.18 (0.867–1.63)	1.41 (0.991–2.02)	1.59 (1.08–2.36)	
2-hr	0.332 (0.274-0.406)	0.449 (0.370-0.550)	0.610 (0.502–0.749)	0.749 (0.611–0.927)	0.947 (0.748-1.21)	1.11 (0.857-1.45)	1.28 (0.965-1.71)	1.46 (1.07-2.01)	1.72 (1.21–2.47)	1.93 (1.31–2.87)	
3-hr	0.407 (0.336-0.497)	0.541 (0.446-0.662)	0.726 (0.597–0.891)	0.884 (0.721-1.09)	1.11 (0.876–1.42)	1.29 (0.999-1.69)	1.48 (1.12-1.99)	1.69 (1.24-2.33)	1.98 (1.39–2.84)	2.21 (1.51–3.28)	
6-hr	0.561 (0.464-0.686)	0.737 (0.608–0.902)	0.976 (0.803-1.20)	1.18 (0.962–1.46)	1.47 (1.16–1.88)	1.70 (1.31–2.22)	1.94 (1.46-2.59)	2.19 (1.61-3.02)	2.55 (1.80-3.66)	2.83 (1.93-4.21)	
12-hr	0.730 (0.603–0.893)	0.963 (0.794–1.18)	1.28 (1.05–1.57)	1.54 (1.26–1.91)	1.91 (1.51–2.45)	2.20 (1.70–2.88)	2.51 (1.89–3.35)	2.82 (2.07–3.89)	3.26 (2.30-4.68)	3.61 (2.46–5.36)	
24-hr	0.966 (0.856-1.11)	1.29 (1.15–1.49)	1.73 (1.53–2.00)	2.09 (1.83-2.44)	2.59 (2.20-3.12)	2.99 (2.48-3.67)	3.39 (2.74-4.27)	3.81 (3.00-4.93)	4.39 (3.32–5.92)	4.84 (3.54-6.76)	
2-day	1.16 (1.03–1.34)	1.58 (1.40-1.82)	2.14 (1.89–2.48)	2.60 (2.28-3.03)	3.23 (2.74–3.89)	3.72 (3.09–4.57)	4.22 (3.42–5.31)	4.73 (3.73–6.13)	5.44 (4.11-7.34)	5.98 (4.37-8.36)	
3-day	1.26 (1.12–1.46)	1.75 (1.55–2.01)	2.38 (2.10-2.75)	2.90 (2.54–3.38)	3.61 (3.06-4.34)	4.15 (3.45–5.11)	4.71 (3.82–5.93)	5.29 (4.17-6.85)	6.07 (4.59-8.20)	6.69 (4.89–9.34)	
4-day	1.34 (1.19–1.54)	1.86 (1.64–2.14)	2.54 (2.25–2.94)	3.10 (2.72–3.61)	3.86 (3.27-4.65)	4.45 (3.69-5.47)	5.05 (4.09-6.36)	5.67 (4.47-7.34)	6.51 (4.93-8.79)	7.17 (5.24–10.0)	
7-day	1.45 (1.29–1.67)	2.01 (1.78–2.31)	2.75 (2.43–3.17)	3.36 (2.94–3.91)	4.20 (3.56–5.06)	4.85 (4.03–5.96)	5.52 (4.47–6.95)	6.21 (4.89-8.04)	7.16 (5.42–9.67)	7.90 (5.77–11.0)	
10-day	1.54 (1.36–1.77)	2.11 (1.87–2.43)	2.89 (2.56-3.34)	3.54 (3.10-4.13)	4.45 (3.77-5.35)	5.15 (4.27–6.33)	5.87 (4.76-7.40)	6.63 (5.22-8.58)	7.67 (5.80-10.4)	8.49 (6.20–11.9)	
20-day	1.74 (1.54–2.00)	2.41 (2.13–2.77)	3.32 (2.93–3.84)	4.09 (3.59–4.77)	5.18 (4.39-6.24)	6.04 (5.01-7.42)	6.93 (5.61-8.73)	7.86 (6.20-10.2)	9.15 (6.92–12.3)	10.2 (7.43–14.2)	
30-day	1.96 (1.74–2.25)	2.72 (2.40–3.13)	3.77 (3.33–4.35)	4.66 (4.08–5.43)	5.93 (5.02-7.13)	6.93 (5.75-8.52)	7.98 (6.46-10.0)	9.07 (7.15-11.7)	10.6 (8.01–14.3)	11.8 (8.61–16.5)	
45-day	2.33 (2.07–2.68)	3.23 (2.86–3.72)	4.49 (3.96–5.19)	5.56 (4.87-6.48)	7.10 (6.02-8.55)	8.34 (6.92–10.3)	9.63 (7.80–12.1)	11.0 (8.65–14.2)	12.9 (9.73–17.4)	14.3 (10.5–20.0)	
60-day	2.54 (2.25–2.92)	3.50 (3.10-4.04)	4.87 (4.30–5.62)	6.04 (5.29–7.04)	7.73 (6.55–9.30)	9.09 (7.55-11.2)	10.5 (8.53–13.3)	12.0 (9.48–15.6)	14.1 (10.7–19.1)	15.8 (11.5–22.0)	

¹ Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values.

Please refer to NOAA Atlas 14 document for more information.

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ACTUAL IMPERVIOUS COVER								
Land Use (1)	Range-Percent	Recommended Value For Average Conditions-Percent (2)						
Natural or Agriculture	0 - 0	0						
Public Park	10 - 25	15						
School	30 - 50	40						
Single Family Residential: (3)								
2.5 acre lots 1 acre lots 2 dwellings/acre 3-4 dwellings/acre 5-7 dwellings/acre 8-10 dwellings/acre More than 10 dwellings/acre Multiple Family Residential:	5 - 15 $10 - 25$ $20 - 40$ $30 - 50$ $35 - 55$ $50 - 70$ $65 - 90$	10 20 30 40 50 60 80						
Condominiums	45 - 70	65						
Apartments	65 - 90	80						
Mobile Home Park	60 - 85	75						
Commercial, Downtown Business or Industrial	80 - 100	90						

Notes:

- 1. Land use should be based on ultimate development of the watershed. Long range master plans for the County and incorporated cities should be reviewed to insure reasonable land use assumptions.
- 2. Recommended values are based on average conditions which may not apply to a particular study area. The percentage impervious may vary greatly even on comparable sized lots due to differences in dwelling size, improvements, etc. Landscape practices should also be considered as it is common in some areas to use ornamental gravels underlain by impervious plastic materials in place of lawns and shrubs. A field investigation of a study area shall always be made, and a review of aerial photos, where available, may assist in estimating the percentage of impervious cover in developed areas.
- 3. For typical equestrian subdivisions increase impervious area 5 percent over the values recommended in the table above.

SAN BERNARDINO COUNTY

ACTUAL IMPERVIOUS COVER FOR DEVELOPED AREAS

HYDROLOGY MANUAL

25

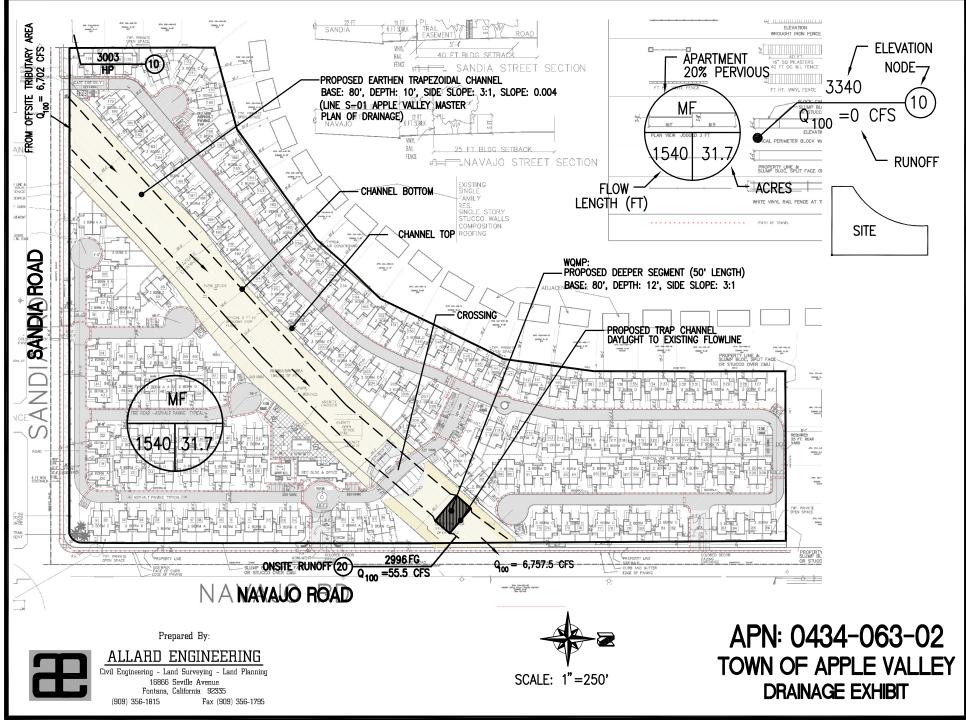
HYDRAULIC CALCULATIOM

CHANNEL SIZING CALC - ONSITE EXISTING CONDITION

HYDRAULIC ELEMENTS - I PROGRAM PACKAGE (C) Copyright 1982-2006 Advanced Engineering Software (aes) Ver. 13.0 Release Date: 06/01/2006 License ID 1400 Analysis prepared by: Allard Engineering 16866 Seville Avenue Fontana Ca. 92335 Tel. 909-356-18185, Fax. 909-356-1795 -----TIME/DATE OF STUDY: 15:04 10/16/2019 _____ Problem Descriptions: LINE S-01 DEPTH OF FLOW CALC FOR 100-YR STORM EXISTING CONDITION ***** >>>>CHANNEL INPUT INFORMATION<<<< _____ _____ CHANNEL Z1(HORIZONTAL/VERTICAL) = 3.00 Z2(HORIZONTAL/VERTICAL) = 3.00 BASEWIDTH(FEET) = 80.00 CONSTANT CHANNEL SLOPE(FEET/FEET) = 0.004000 UNIFORM FLOW(CFS) = 6702.00MANNINGS FRICTION FACTOR = 0.0350 _____ NORMAL-DEPTH FLOW INFORMATION: >>>> NORMAL DEPTH(FEET) = 7.41 -FLOW TOP-WIDTH(FEET) = 7.41 FLOW AREA(SQUARE FEET) = 124.48 HYDRAULIC DEPTH(FEET) = 758.01 HYDRAULIC DEPTH(FEET) = 6.09 FLOW AVERAGE VELOCITY(FEET/SEC.) = 8.84 UNIFORM FROUDE NUMBER = 0.631 PRESSURE + MOMENTUM(POUNDS) = 277454.59 AVERAGED VELOCITY HEAD(FEET) = 1.214 SPECIFIC ENERGY(FEET) = 8.628 CRITICAL-DEPTH FLOW INFORMATION: _____ CRITICAL FLOW TOP-WIDTH(FEET) = 113.55 CRITICAL FLOW AREA(SQUARE FEET) = 541 CRITICAL FLOW AREA(SQUARE FEET) = 541.18 CRITICAL FLOW HYDRAULIC DEPTH(FEET) = 4.77 CRITICAL FLOW AVERAGE VELOCITY(FEET/SEC.) = 12.38 CRITICAL DEPTH(FEET) = 5.59 CRITICAL FLOW PRESSURE + MOMENTUM(POUNDS) = 249805.83 AVERAGED CRITICAL FLOW VELOCITY HEAD(FEET) = 2.381 CRITICAL FLOW SPECIFIC ENERGY(FEET) = 7.974 _____

CHANNEL SIZING CALC - ONSITE DEVELOPED CONDITION

HYDRAULIC ELEMENTS - I PROGRAM PACKAGE (C) Copyright 1982-2006 Advanced Engineering Software (aes) Ver. 13.0 Release Date: 06/01/2006 License ID 1400 Analysis prepared by: Allard Engineering 16866 Seville Avenue Fontana Ca. 92335 Tel. 909-356-18185, Fax. 909-356-1795 _____ TIME/DATE OF STUDY: 16:09 10/16/2019 _____ Problem Descriptions: LINE S-01 DEPTH OF FLOW CALC FOR 100-YR STORM WITH ONSITE DEVELOPED CONDITION ***** >>>>CHANNEL INPUT INFORMATION< _____ CHANNEL Z1(HORIZONTAL/VERTICAL) = 3.00 Z2(HORIZONTAL/VERTICAL) = 3.00BASEWIDTH(FEET) = 80.00 CONSTANT CHANNEL SLOPE(FEET/FEET) = 0.004000 UNIFORM FLOW(CFS) = 6757.50MANNINGS FRICTION FACTOR = 0.0350 _____ NORMAL-DEPTH FLOW INFORMATION: >>>> NORMAL DEPTH(FEET) = 7.45 FLOW AREA(SQUARE FEET) = 762.23 HYDRAULIC DEPTH(FEET) = 6.11 762.28 FLOW AVERAGE VELOCITY(FEET/SEC.) = 8.86 UNIFORM FROUDE NUMBER = 0.632 PRESSURE + MOMENTUM(POUNDS) = 280337.78 AVERAGED VELOCITY HEAD(FEET) = 1.220 SPECIFIC ENERGY(FEET) = 8.668 CRITICAL-DEPTH FLOW INFORMATION: _____ CRITICAL FLOW TOP-WIDTH(FEET) = 113.72 CRITICAL FLOW AREA(SQUARE FEET) = 544.43 CRITICAL FLOW HYDRAULIC DEPTH(FEET) = 4.79 CRITICAL FLOW ANDROLL = 4.79 CRITICAL FLOW AREA(SQUARE FEET) = CRITICAL FLOW AVERAGE VELOCITY(FEET/SEC.) = 12.41 CRITICAL DEPTH(FEET) = 5.62 CRITICAL FLOW PRESSURE + MOMENTUM(POUNDS) = 252473.33 AVERAGED CRITICAL FLOW VELOCITY HEAD(FEET) = 2.392 CRITICAL FLOW SPECIFIC ENERGY(FEET) = 8.013 _____ ONSITE DRAINAGE EXHIBIT



Filename: I:\Barbara Monroy\Apple Valley\PROJECT ADMIN\REPORTS\DRAINAGE UPDATE\Drainage Site Exhibit.dwg