

Appendix H.1



Transportation Impact Report

Cheval Blanc Beverly Hills Specific Plan

Transportation Impact Report

Prepared for:

Eyestone Environmental

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FEHR PEERS

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1. Study Overview

This transportation impact report presents the results of the analysis conducted by Fehr & Peers for the proposed Cheval Blanc Beverly Hills Specific Plan and other requested approvals as set forth in the Draft Environmental Impact Report at section 27, "Required Approvals" (herein collectively referred to as the "proposed Project" or the "Project") in the City of Beverly Hills. The purpose of this study is to provide the transportation impact analysis required for the Environmental Impact Report being prepared for the proposed Project. Transportation conditions in the Project vicinity with the development of the proposed land use changes are compared to existing conditions. This chapter outlines the purpose of the study, the geographic scope, and the study scenarios.

1.1 Study Purpose

The purpose of this study is to analyze the potential for significant transportation impacts to occur with the development of the Project. The City of Beverly Hills has adopted new transportation impact thresholds and guidelines to adhere to CEQA requirements pertaining to Senate Bill 743 (SB 743). The primary purpose of SB 743 was eliminating level of service (LOS) as a measure of vehicular capacity and traffic congestion as a basis for determining significant transportation impacts under CEQA. Rather, SB 743 required lead agencies to shift the focus from evaluating traffic impacts based on metrics that only consider vehicle travel time and delay (i.e., impacts to drivers) to metrics that capture the state's goals of improved air quality, reduced greenhouse gas emissions, and improved public health (i.e., impacts of driving).

In response to SB 743, the Governor's Office of Planning and Research (OPR) selected vehicle miles travelled (VMT) as the new transportation impact metric for which lead agencies are required to define methodologies, thresholds, and mitigation consistent with their respective General Plan goals. It should be noted that while LOS no longer constitutes a CEQA impact, it can still be used to inform decision makers on the overall effects of a project. The deadline for agencies to implement SB 743 was July 1, 2020.

Given the new CEQA requirements, a separate traffic operations analysis has been completed and documented in the *Cheval Blanc Beverly Hills Specific Plan Local Transportation Assessment* (Fehr & Peers, September 2021). This traffic operations report analyzes changes to intersection LOS with development of the proposed Project and compares traffic operations with the proposed Project to both existing conditions and opening year conditions.

1.2 Project Study Area

The Project is located in the heart of the City of Beverly Hills. As shown in **Figure 1**, the Project site is bordered by South Santa Monica Boulevard on the north, North Beverly Drive on the east, North Rodeo Drive on the west, and existing developments on the south. The Project study area is generally bounded by North Santa Monica Boulevard to the north, North Cañon Drive to the east, North Rodeo Drive to the west, and Brighton Way to the south. **Figure 1** displays the study area and the locations of the study intersections in the immediate vicinity of the Project site.

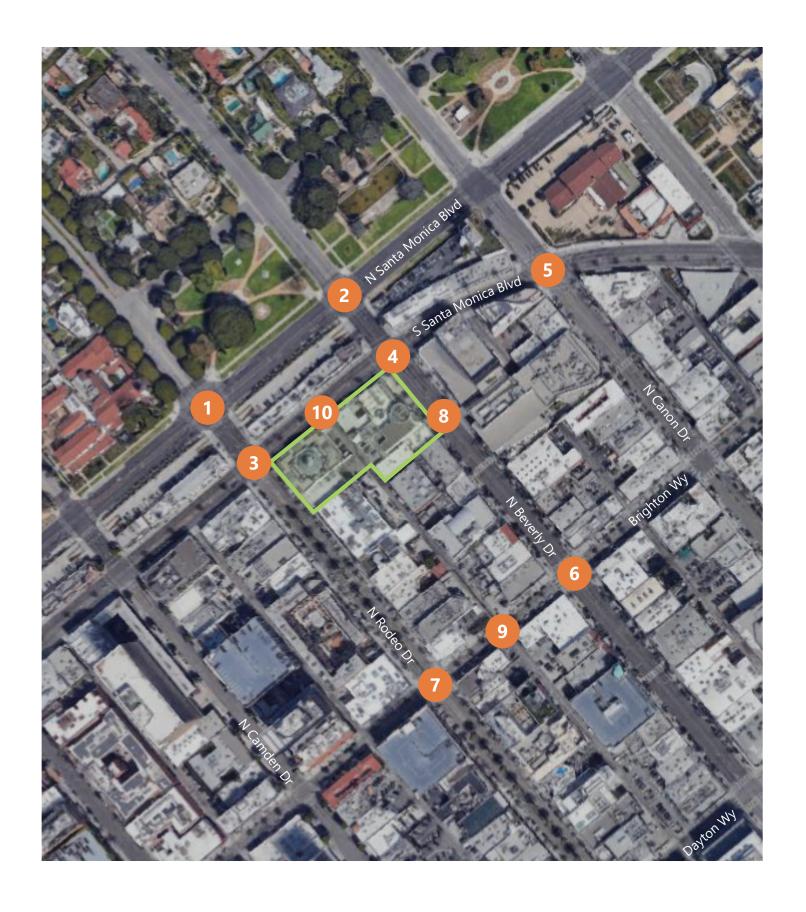




Figure 1
Project Location and Study Intersections

1.3 Analysis Scenarios

The following scenarios are considered in the analysis of transportation impacts:

- Existing (2019) Conditions Existing conditions is based on traffic volume estimates that reflect 2019 conditions.¹
- Existing (2019) plus Project Conditions This scenario reflects the changes to Project-generated travel demands under Existing (2019) conditions with the land use and site access changes proposed under the Project.
- **Cumulative (2026) Conditions** Future traffic projections were developed to reflect the year 2026. This scenario reflects future travel demands from regional growth and related projects in the vicinity of the Project site by the anticipated Project opening year of 2026.
- **Cumulative (2026) plus Project Conditions** This scenario reflects the changes to Project-generated travel demands in the year 2026 with the land use and site access changes proposed under the Project.

¹ Due to the statewide stay-at-home order and social distancing measures issued by the Governor of California and Los Angeles County Department of Health to slow the spread of COVID-19, data collection in 2020 or early 2021 would not reflect typical travel conditions in the study area. Therefore, traffic counts for the study intersections were compiled from available data collected at various times from before the COVID-19 pandemic to estimate travel demand under existing conditions. Historic counts were grown to reflect 2019 conditions using an average annual growth rate of 0.5% per year.

Existing & Planned Transportation Conditions

This chapter discusses the existing plans and policies related to transportation in the City of Beverly Hills and the transportation conditions in the Project study area. This discussion addresses the existing and planned roadway network, the bus transit network, and the bicycle and pedestrian facilities in the study area. In addition, in April 2021, the City adopted a citywide Complete Streets Plan that identifies goals and policies and potential improvements in the study area to enhance active transportation and transit service that are included in this chapter.

2.1 Existing Plans & Policies

This section summarizes state, regional, and local regulatory framework that serve as the foundation for evaluating transportation impacts under CEQA.

2.1.1.1 California Environmental Quality Act

CEQA generally requires state and local government agencies to inform decision makers and the public about the potential environmental impacts of proposed projects, and to reduce those environmental impacts to the extent feasible. CEQA Section 15064.3 describes specific considerations for determining a project's transportation impacts. Generally, vehicle miles traveled (VMT) is the most appropriate measure of transportation impacts. For the purposes of this section, "vehicle miles traveled" refers to the amount and distance of automobile travel attributable to a project. Other relevant considerations may include the effects of the project on transit and non-motorized travel (CEQA 2019).

2.1.1.2 California Senate Bill 743

Senate Bill 743 (SB 743) directed the Office of Planning and Research (OPR) to develop revisions to the CEQA Guidelines to establish new criteria for determining the significance of transportation impacts and define alternative metrics for traffic analysis. On September 27, 2013, California Governor Jerry Brown signed SB 743 into law and started a process that changed transportation impact analysis as part of CEQA compliance. These changes include elimination of auto delay, level of service (LOS), and other similar measures of vehicular capacity or traffic congestion as a basis for determining significant impacts for land use and transportation projects in California.

In 2016, OPR released the Revised Proposal on Updates to the CEQA Guidelines on Evaluating Transportation Impacts in CEQA. Of particular relevance was the updated text of the new Section 15064.3 that relates to the new transportation impact metric of VMT and describes the determination of the significance of transportations impacts and mitigation measures. To help lead agencies with SB 743 implementation, the Governor's Office of Planning and



Research (OPR) produced a *Technical Advisory*. More information on the determination of the significance of impacts is included in Chapter 4, Vehicle Miles Traveled.

2.1.1.3 California Assembly Bill 32 and Senate Bill 375

Assembly Bill 32 (AB 32), also known as the California Global Warming Solutions Act of 2006, is California's major initiative for reducing greenhouse gas (GHG) emissions. AB 32 requires California to reduce its GHG emissions to 1990 levels by 2020, a reduction of approximately 15% below emissions expected under a "business as usual" scenario.

As stated in AB 32, the California Air Resources Board (CARB) must adopt regulations to achieve the maximum technologically feasible and cost-effective GHG emission reductions. The full implementation of AB 32 will help mitigate risks associated with climate change, while improving energy efficiency, expanding the use of renewable energy resources, cleaner transportation, and reducing waste (CARB 2018).

Signed in 2008, Senate Bill 375 (SB 375) directs CARB to develop regional GHG emission reduction targets to be achieved by passenger vehicles by 2020 and 2035. SB 375 also directs each of California's major metropolitan planning organizations (MPOs) to prepare a sustainable communities strategy (SCS) that identifies a growth strategy to meet emissions targets, to be included in each MPOs regional transportation plan (RTP).

In 2010, CARB adopted regional targets for reducing GHG emissions by 2020 and 2035, using 2005 as a base year. The Southern California Association of Governments (SCAG) was assigned targets of an 8% reduction in GHGs from transportation sources by 2020 and a 13% reduction in GHGs from transportation sources by 2035.

On March 22, 2018, CARB adopted updated regional targets for reducing GHG emissions from 2005 levels by 2020 and 2035. The Southern California Association of Governments (SCAG) was assigned targets of an 8 percent reduction in per capita GHG emissions from passenger vehicles by 2020 and a 19 percent reduction in per capita GHG emissions from passenger vehicles by 2035. In the SCAG region, SB 375 also provides the option for the coordinated development of subregional plans by the subregional councils of governments and the county transportation commissions to meet SB 375 requirements. On September 3, 2020, the SCAG's Regional Council formally adopted the 2020-2045 RTP/SCS titled Connect SoCal, which meets the requirements of SB 375.

2.1.1.4 Southern California Association of Governments (SCAG) 2020-2045 Regional Transportation Plan and Sustainable Communities Strategy (RTP/SCS)

On September 3, 2020, the SCAG's Regional Council formally adopted the 2020-2045 RTP/SCS titled Connect SoCal. The 2020-2045 RTP/SCS builds upon the progress made through implementation of the 2016-2040 RTP/SCS and includes 10 goals focused on promoting economic prosperity, improving mobility, protecting the environment, and supporting healthy/complete communities. The SCS implementation strategies include focusing growth near destinations and mobility options, promoting diverse housing choices, leveraging technology innovations, and supporting implementation of sustainability policies. The SCS establishes a land use vision of center focused placemaking, concentrating growth in and near Priority Growth Areas, transferring of development rights, urban

² Governor's Office of Planning and Research, *Technical Advisory on Evaluating Transportation Impacts in CEQA*, 2018. Cheval Blanc Beverly Hills Specific Plan Transportation Impact Report

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greening, creating greenbelts and community separators, and implementing regional advance mitigation (SCAG 2020).

2.1.1.5 LA Metro First Last Mile Strategic Plan

The LA Metro First Last Mile Strategic Plan (Metro, SCAG 2014) outlines an approach for identifying barriers and planning for/implementing improvements for connecting transit services to nearby trip origins (e.g., an individual's home) and destinations (e.g., an individual's place of employment). Examples of first/last mile improvements include but are not limited to: pedestrian and bicycle infrastructure, signage and wayfinding, and shared use services (e.g., car share). The First Last Mile Plan developed what is known as "The Pathway," a proposed countywide transit access network designed to enhance transit accessibility. The Pathway is a series of active transportation improvements that connect to and from Metro Rail and BRT stations.

Within the study area, the City of Beverly Hills worked with Metro to develop the *Wilshire/Rodeo Station Pathway Plan* for the Wilshire/Rodeo Station. The Pathway Plan notes that Wilshire Boulevard would benefit from numerous first/last mile improvements, including bus stop enhancements, high-visibility crosswalks, street furniture, and street trees where needed. The Pathway Plan also identifies a series of bicycle improvements that will help facilitate station access, such as intersection treatments to create a bicycle-friendly environment.

2.1.1.6 City of Beverly Hills General Plan - Circulation Element

The City of Beverly Hills General Plan Circulation Element (City of Beverly Hills, 2010) has two overarching objectives: that the neighborhoods of Beverly Hills should be preserved and enhanced, including limiting negative effects caused by vehicles. Secondly, vehicles should move into, out of, or through Beverly Hills as expeditiously as possible. The Circulation Element identifies the following goals that are relevant to this study:

- **CIR 1 Circulation System**: Provide a safe and efficient roadway circulation system within the City.
- **CIR 2 Transit**: Development of a safe, comprehensive, and integrated transit system that serves as an essential component of a multi-modal mobility system within the City.
- **CIR 3 Neighborhood Traffic Management**: An improved community character and quality of life in City neighborhoods through the implementation of traffic management techniques.
- **CIR 6 Transportation Demand Management (TDM)**: A reduction in single-occupant motor vehicle travel in the City through Transportation Demand Management (TDM) that ensures efficiency of the existing transportation network and promotes the movement of people instead of personal automobiles.
- **CIR 7 Pedestrians**: A safe and comfortable pedestrian environment that results in walking as a desirable travel choice, particularly for short trips, within the City.
- CIR 8 Bikeways. An integrated, complete, and safe bicycle system to encourage bicycling within the City.

2.1.1.7 Complete Streets Planning in Beverly Hills

In April 2021, the City of Beverly Hills adopted a citywide Complete Streets Plan. The City of Beverly Hills Complete Streets Plan (City of Beverly Hills, 2021) creates a blueprint for transportation improvements that balance the

needs of all road users: bicyclists, pedestrians, transit riders, and motorists. The goal of the Complete Streets Plan is to provide more options for people to choose the mode that best works for their trip type, and a network of streets where individual modes will be prioritized.

The Complete Streets Plan identifies the following goals that are relevant to this study:

- Goal B1: Provide a Safe and Efficient Bicycle Circulation System Within the City
- Goal B2: Provide a Holistic and Connected Bicycle Network
- Goal B3: Expand Bike Parking
- Goal B4: Support and Encourage Bicycle Transportation
- Goal P1: Improve Pedestrian Safety
- Goal P2: Make Walking a Desirable Travel Choice
- Goal P3: Enhance Sidewalks as Public Spaces
- Goal T1: Provide First/Last Mile Connections
- Goal T2: Improve the Rider Experience
- Goal T3: Increase Transit Ridership
- Goal V1: Reduce Traffic Congestion
- Goal V2: Harness the Power of Data and Technology
- Goal V3: Support Safe, Complete, Livable, Sustainable, and Quality Neighborhoods

The Complete Streets Plan identifies a series of bicycle improvements that will help facilitate access to the Wilshire/Rodeo Station. The Complete Streets Plan also identifies pedestrian corridors to enhance the overall pedestrian experience. Potential improvements could include new and upgraded sidewalks, tightened curb radii to slow vehicle speeds, and mid-block crossings, among others.

The Complete Streets Plan identifies North Santa Monica Boulevard, Wilshire Boulevard, Burton Way, Olympic Boulevard, and Beverly Drive as the City's proposed Transit Enhanced Network. Bus stop enhancements, such as shelter, seating, lighting, trash/recycling bins, poles/signs with route information and schedules, a system map (or link to one), a paved boarding area, and ADA-compliant pedestrian connections, are identified along these corridors.

2.1.1.8 City of Beverly Hills Master Plan of Streets

The City of Beverly Hills Master Plan of Streets (Master Plan of Streets, City of Beverly Hills, 1973) defines the functional class of all City streets, highways, and alleys. The City Engineer may approve and allow variations from the requirements of the Master Plan of Streets as issues arise. Development of the proposed Project would require an amendment to the Master Plan of Streets to accommodate the alley relocation, and to reflect existing curb radii and overall roadway right of way width on South Santa Monica Boulevard.

2.2 Transportation Facilities

A comprehensive data collection effort was undertaken to identify existing transportation conditions in the vicinity of the proposed Project. The assessment of existing conditions relevant to this study includes an inventory of the street system and traffic volumes at the study intersections. Existing public transit service and bicycle and pedestrian facilities are also described.

2.2.1 Existing Street System

The Project is in the Beverly Hills Business Triangle and served by a grid system of streets. Major roadways within the study area are shown above in **Figure 1** and described below.

- **South Santa Monica Boulevard** or "Little Santa Monica Boulevard" parallels North Santa Monica Boulevard through the City of Beverly Hills and would provide the primary access to the Project site. The roadway begins east of Moreno Drive and becomes Burton Way at Rexford Drive. The roadway has two travel lanes in each direction. The roadway is classified as a Principal Arterial adjacent to the Project site.
- **Rodeo Drive** runs north-south through the City of Beverly Hills. The roadway begins at the intersection with Sunset Boulevard and terminates just south of the south City limit at the intersection with Beverwil Drive. Within the study area, the roadway has two travel lanes in each direction. The roadway is classified as a local street within the study area.
- **Beverly Drive** runs north-south through the City of Beverly Hills. The roadway begins in the Beverly Crest neighborhood of the City of Los Angeles and terminates just north of Interstate 10, also in the City of Los Angeles. Within the study area, the roadway has two travel lanes in each direction and is classified as a local street north of South Santa Monica Boulevard and a Minor Arterial from South Santa Monica Boulevard to the south City limit.
- North Santa Monica Boulevard is a major north-south roadway and is referred to as North Santa Monica Boulevard in the City of Beverly Hills. Within the study area, this roadway generally travels in a southwest to northeast direction. To the west, Santa Monica Boulevard continues outside of the study area through the City of Los Angeles where it connects to the Interstate 405 and extends into the City of Santa Monica, where it terminates. To the east, Santa Monica Boulevard continues into the City of West Hollywood and eventually terminates east of US Highway 101. Within the study area, the roadway has two travel lanes in each direction in the City of Beverly Hills and three travel lanes in each direction in the City of Los Angeles. The roadway is designated as a Principal Arterial in the City of Beverly Hills.
- **Cañon Drive** runs north-south through the City of Beverly Hills. The roadway begins at the intersection with Sunset Boulevard and terminates just north of the south City limit at the intersection with Beverly Drive. Due to construction of the Metro D Line, Cañon Drive is currently closed just north of the Wilshire Boulevard intersection. Within the study area, the roadway has two travel lanes in each direction and the roadway is classified as a local street.
- **Brighton Way** runs northeast-southwest through central Beverly Hills. It begins at Wilshire Boulevard in the west and terminates at Crescent Drive in the east. Brighton Way is one-way and flows in the southwest direction. Within the study area, the roadway provides two travel lanes and is classified as a local street.

2.2.2 Existing Intersection Volumes and Lane Configurations

Due to the statewide stay-at-home order and social distancing measures issued by the Governor of California and Los Angeles County Department of Health to slow the spread of COVID-19, data collection in 2020 or early 2021 would not reflect typical travel conditions in the study area. Therefore, traffic counts for the study intersections were compiled from available data collected at various times from before the COVID-19 pandemic to estimate travel demand under existing conditions. Historic counts were grown to reflect 2019 conditions using an average annual growth rate of 0.5% per year. Where traffic count data was not available, turning volumes were estimated based on balancing with adjacent intersections and observed traffic flows. Intersection turning movement counts were collected at the following times:

- Weekday morning peak period (7:00 to 9:00 AM)
- Weekday evening peak period (4:00 to 6:00 PM)

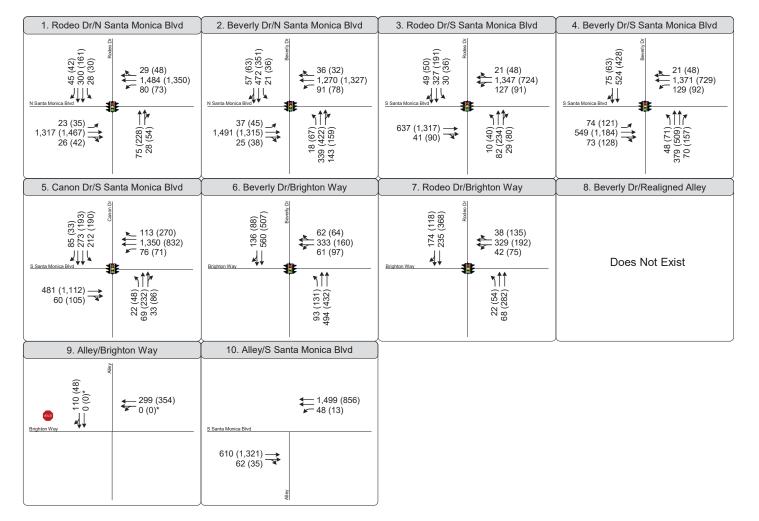
Existing lane configurations and signal controls were obtained through field observations. **Figure 2** presents the existing peak periods turning movement volumes, corresponding lane configurations, and traffic control devices.

2.2.3 Cumulative Traffic Volume Forecasts

Future traffic projections were developed to reflect cumulative conditions. The year 2026 was used to forecast cumulative conditions to reflect the expected opening year of the proposed Project. The growth in traffic in the study area reflects future travel demands from regional growth and related projects in the vicinity of the Project site. A variety of sources were consulted to develop the cumulative traffic forecasts. These sources include:

- Historic traffic counts, grown to reflect Existing (2019) conditions
- Traffic from approved and pending projects in the City of Beverly Hills, City of Los Angeles, and City of West Hollywood
- Ambient growth in existing traffic volumes to reflect growth in regional traffic (a growth rate of 0.5% per year was applied to the 2019 traffic volumes to reflect this ambient growth)

The list of related projects used to develop the cumulative traffic forecasts is provided in **Appendix A**. The related projects and their expected trip generation were obtained from the Cities of Beverly Hills, West Hollywood, and Los Angeles. Traffic volumes for cumulative (2026) conditions are shown in **Figure 3**.



* Data was not available for volumes on the alley south of Brighton Way, so these turning movements are shown 0. No changes to these volumes would occur as a result of the proposed project.

AM (PM) Peak Hour Traffic Volume



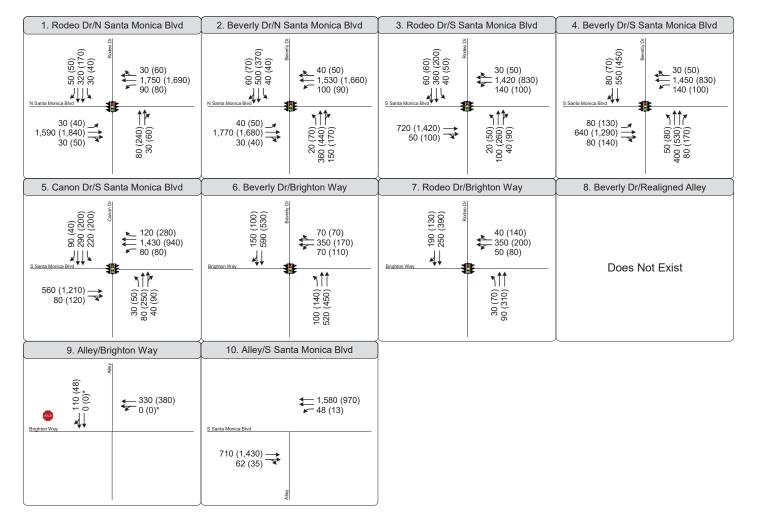
Lane Configuration



Signalized



Figure 2



* Data was not available for volumes on the alley south of Brighton Way, so these turning movements are shown 0. No changes to these volumes would occur as a result of the proposed project.

AM (PM) Peak Hour Traffic Volume



Stop Sign

Signalized



Figure 3

2.2.4 Existing Transit Service

Several transit lines operate within the study area with service provided by the Metropolitan Transportation Authority (Metro). Every six months, typically in June and December, Metro Operations undergoes a service change program where bus schedules are adjusted to accommodate ridership demands and improve connections between Metro Bus and Rail. Metro provides service on multiple bus lines with frequent service (at least every 15 minutes during weekday peak hours) in the study area. Due to the reduction in ridership caused by the COVID-19 pandemic and related lockdown orders, Metro reduced service on many routes in 2020. However, in response to increasing ridership demands later in the year, Metro implemented increased service beginning December 2020. In February 2021, Metro's Board adopted Motion 27.1,3 committing to restoring pre-pandemic-level 7 million annualized revenue service hours for bus lines by September 2021, and in its April 14, 20214 Budget Development Update designated funding to achieve this goal.

In addition to restoring transit service, Metro adopted the NextGen Bus Plan in 2020, a once-in-a-generation overhaul of bus routes and service design concepts intended to provide faster and more frequent bus service, including during off-peak periods, better reliability and accessibility to key destinations, better connectivity with municipal transit operators, and improved perception of safety onboard buses and at bus stops. Some of the bus routes in Beverly Hills were modified as a result of the NextGen Bus Plan. The NextGen Bus Plan recently went into operation in June 2021 discontinued Line 16 bus service west of San Vicente Boulevard (service continues east/west on Third Street between West Hollywood and downtown Los Angeles at six to 10-minute frequencies.) A total of 14 stops for Line 16 were eliminated in the City of Beverly Hills on Burton Way and North Santa Monica Boulevard. A new line, Line 617, provides service between the Expo Light Rail Station on Venice Boulevard and a new mini-transit hub located at Cedars Sinai Hospital, and then continues west through Beverly Hills along Burton Way and Beverly Drive. Line 617 operates every 45 minutes on weekdays and every 60 minutes on weekends. This new service on Burton Way replaces the service formerly provided by Line 16.

The service routes and frequencies that reflect these recent service changes, as well as service frequencies in 2019 and 2020 prior to the pandemic that Metro has committed to returning to by September 2021, are described below. For lines with stops within one half-mile of the proposed Project, walking distances are also provided.

Figure 4 depicts existing transit service in the City of Beverly Hills.

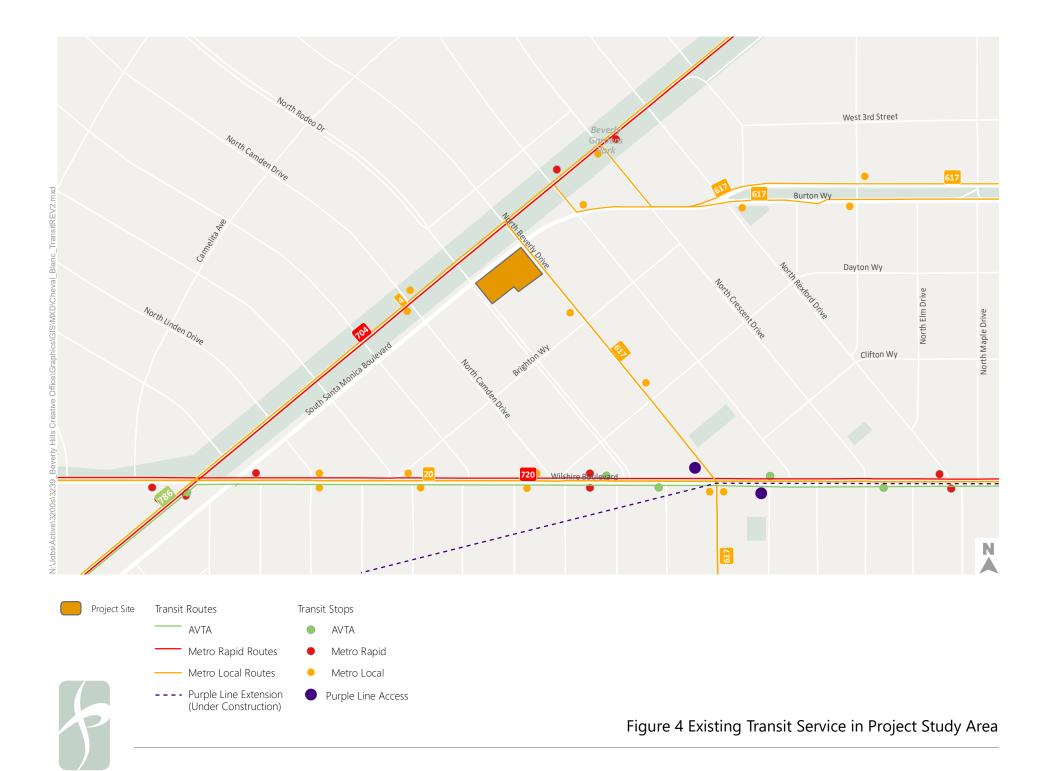
• Metro Rapid Line 704 – Metro Line 704 provides express bus service between Downtown Los Angeles and the City of Santa Monica with principal service along North Santa Monica Boulevard as part of Metro's Rapid network. The line travels along Sunset Boulevard and Santa Monica Boulevard connecting the communities of downtown Los Angeles, Echo Park, Silver Lake, West Hollywood, Beverly Hills, Century City, Westwood, West Los Angeles, and Santa Monica. As of the June service changes, buses operate along North Santa Monica Boulevard every 20 minutes during peak periods and every 20 to 30 minutes off-peak/weekends. The closest Line 704 bus stop to the proposed Project is located on the north side of North Santa Monica Boulevard at Crescent Drive (0.3 miles).

⁴ APRIL 14, 2021 BUDGET DEVELOPMENT UPDATE: https://media.metro.net/2021/6-Apr-21-FY22 budget-item.pdf



³ MOTION 27.1: http://media.metro.net/board/recap/2021/2021-0225-recap-rbm.pdf

- Metro Rapid Line 720 Line 720 provides an express service between Downtown Los Angeles and the City of Santa Monica with principal service along Wilshire Boulevard as part of Metro's Rapid network. The line travels along Wilshire Boulevard connecting the communities of Beverly Hills, Boyle Heights, Brentwood, Downtown Los Angeles, Hancock Park, Koreatown, Park La Brea, Santa Monica, and Westwood. As of the June service changes, buses operate every five minutes along Wilshire Boulevard during the peak periods and every seven to ten minutes off-peak/weekends. The closest Line 720 bus stop to the proposed Project is located on the northeast corner of the intersection of Wilshire Boulevard & South Santa Monica Boulevard (0.4 miles).
- Metro Line 4 Line 4 provides service between downtown Los Angeles and west Los Angeles with service along North Santa Monica Boulevard. It travels along Santa Monica Boulevard connecting the communities of Echo Park, Silver Lake, West Hollywood, Beverly Hills, Century City, and West Los Angeles. Bus service in the early morning and owl service travels further west into the City of Santa Monica. Line 4 is a local service bus and has frequent stops along Santa Monica Boulevard. Most stops are approximately one to two blocks apart. As of the June service changes, bus frequency is basically the same on both weekdays and weekends. Service is provided approximately every 12 minutes during daytime hours, including weekends. Evening service is reduced to every 15 to 20 minutes, owl service is every 25 to 30 minutes. The closest stops to the proposed Project site are located on both sides of North Santa Monica Boulevard at the intersection with Camden Drive (0.3 miles) and on the north side of the street (westbound) at Crescent Drive (0.3 miles).
- Metro Line 20 Line 20 provides service between downtown Los Angeles and Westwood with service along Wilshire Boulevard. It travels along Wilshire Boulevard connecting the communities of Beverly Hills, Los Angeles, Hancock Park, Park La Brea, UCLA, West Los Angeles, and Westwood. Early morning, late night and owl service is extended to Santa Monica along Wilshire Boulevard. Line 20 is a local service bus and follows the same route as Metro Rapid Line 720, but with more frequent stops. Most stops are approximately one to two blocks apart. As of the June service changes, service is provided every 10 to 12 minutes during peak hours on both weekdays and weekends. Off-peak headways are approximately 30 minutes to an hour. The closest Line 20 bus stop to the proposed Project is located on the south side of Wilshire Boulevard at Rodeo Drive (0.4 miles).
- **Metro Line 617** Line 617 provides services between Beverly Hills and Culver City. The line travels along Beverly Dr, Santa Monica Boulevard, Crescent Drive, Burton Way, 3rd Street, San Vicente, La Cienega and Robertson Boulevard. Line 617 connects the communities of Beverlywood, Beverly Hills, Pico—Robertson, La Cienega Heights, and Downtown Culver City. As of the June service changes, weekday service is approximately every 45 minutes during both peak and off-peak hours. Weekend service is every hour. Within the study area, the closest stop to the Project site is located on the west side of Beverly Drive just north of Brighton Way in the southbound direction (0.1 miles).



• Antelope Valley Transit Authority (AVTA) Line 786 – AVTA Line 786 provides commuter bus service from the Antelope Valley (Lancaster / Palmdale) to West Los Angeles and Hollywood along Santa Monica and Wilshire Boulevards. There are 5 daily roundtrips on weekdays – there is no weekend service. Morning trips in Beverly Hills arrive between the hours of 6 and 8 AM with 20-to-30 minute headways, evening service to the Antelope Valley depart between 3 and 5:15 PM with 20-to-40 minute headways. The closest Line 786 bus stop to the proposed Project is located on the north side of Wilshire Boulevard at Rodeo Drive (0.4 miles).

2.2.5 Planned Transit Service

The D Line Extension will extend the existing D Line (formerly, the Purple Line) subway from its current terminus at Wilshire/Western to a proposed new station in Westwood. Sections 1 and 2 of the D Line Extension are currently under construction. Section 1 is expected to begin operations in 2023 and includes one new station in Beverly Hills at Wilshire/La Cienega and two new stations in Los Angeles (Wilshire/La Brea and Wilshire/Fairfax). Section 2 is expected to begin operations in 2025 and includes one new station in Beverly Hills at Wilshire/Rodeo and one just west of the City at Century City/Constellation. Section 3 of the D Line Extension project is currently in preconstruction and is anticipated to open for operations in 2026 with two new stations (Wilshire/Westwood and Wilshire/VA Hospital). The station planned for Wilshire/Rodeo is closest to the proposed Project site. In November 2020, the City approved the construction of the North Portal which would provide an entrance/exit on the west side of North Beverly Drive, within the existing street right-of-way, north of Wilshire Boulevard. The walking distance between the Project site and North Portal is 0.4 miles.

The City of Beverly Hills Complete Streets Plan identifies North Santa Monica Boulevard and Beverly Drive as part of the City's proposed Transit Enhanced Network. Bus stop enhancements, such as shelter, seating, lighting, trash/recycling bins, poles/signs with route information and schedules, a system map (or link to one), a paved boarding area, and ADA-compliant pedestrian connections, are identified along North Santa Monica Boulevard, including the bus stops on Cañon Drive at both North Santa Monica Boulevard and South Santa Monica Boulevard, closest to the Project site.

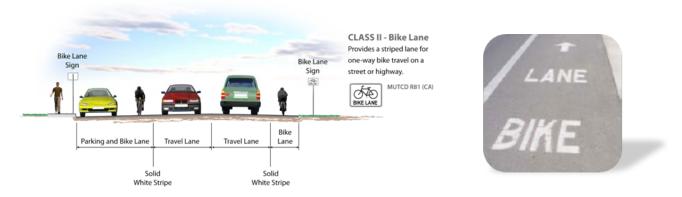
2.2.6 Existing Bicycle and Pedestrian Facilities

Bicycle facilities generally consist of four types of facilities, which are outlined below:

• <u>Bike or Shared Use Paths</u> provide a separate right-of-way and is designated for the exclusive use of bicycles and pedestrians with vehicle and pedestrian crossflow minimized. Generally, the recommended pavement width for a two-directional shared use path is ten feet.



• <u>Bike Lanes</u> provide a restricted right-of-way and are designated for the use of bicycles with a striped lane on a street or highway. Adjacent vehicle parking and vehicle/pedestrian crossflow is permitted.

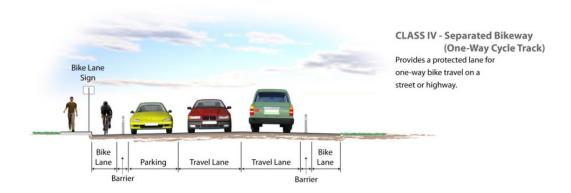


• <u>Bike Route or Signed Shared Roadways</u> provide for a right-of-way designated by signs or shared lane pavement markings, or "sharrows," for shared use with pedestrians or motor vehicles.





• <u>Separated Bikeways or Cycle Tracks</u> provide on-street bicycle facilities that are separated from vehicle travel by a vertical barrier to provide a protected bicycle lane. At intersections, the barrier is typically removed to allow vehicles to enter the bike lane to make a right-turn.



Within the study area, North Santa Monica Boulevard has Class II bicycle lanes that are enhanced through green paint in the City of Beverly Hills (from the western City limit just west of the Project site to the eastern City limit at Doheny Drive). The closest bikeshare station to the Project site is at the corner of South Santa Monica Boulevard & Camden Drive.

A majority of the roadways within the study area have sidewalks and crosswalks. There are sidewalks along the roadways that border the site including South Santa Monica Boulevard, North Beverly Drive, and North Rodeo Drive. The exception is the south side of North Santa Monica Boulevard, which lacks sidewalks. There are also crosswalks and pedestrian "walk/don't walk" indicators at the signalized intersections in the study area. East-west crosswalks across North Santa Monica Boulevard provide connectivity to the north-south sidewalks, despite the lack of sidewalks on the south side of North Santa Monica Boulevard itself. The signalized crossings for pedestrians, including mid-block crossings and intersections that operate with a pedestrian scramble (all-walk) signal phase in the Project area are shown in **Figure 5**.

A pedestrian pathway is also located through the Beverly Gardens Park located north of the Project site along North Santa Monica Boulevard. In 2018, as part of the North Santa Monica Boulevard Reconstruction Project, the City completed the implementation of eight raised crosswalks connecting the decomposed granite pedestrian path through Beverly Gardens Park across intersections.





LIII Existing Signalized Crossing

Figure 5

2.2.7 Planned Bicycle and Pedestrian Facilities

In April 2021, the City of Beverly Hills adopted a citywide Complete Streets Plan. The *City of Beverly Hills Complete Streets Plan* contains a vision for transportation improvements that balance the needs of all road users including bicyclists and pedestrians.

Within the study area, the Complete Streets Plan identifies a series of bicycle improvements that will improve facilities for bicyclists traveling in the City and help facilitate access to the Wilshire/Rodeo Station, including a new Class IV protected bicycle lane on Beverly Drive, a new Class II bicycle lane on Cañon Drive, and a new Class III bicycle boulevard on Brighton Way.

The Complete Streets Plan also identifies pedestrian corridors to enhance the overall pedestrian experience. Pedestrian corridor improvements are envisioned on South Santa Monica Boulevard. Potential improvements could include new and upgraded sidewalks, tightened curb radii to slow vehicle speeds, and mid-block crossings, among others.

3. Proposed Project Transportation Characteristics

This chapter presents the land uses and trip generation of the proposed Project and describes the total number of vehicle trips that would be generated by the proposed land uses in comparison to existing uses and historic uses on the Project site.

3.1 Project Overview

The Project is located in the heart of Beverly Hills. The 1.277-acre Project site is bordered by South Santa Monica Boulevard on the north, North Beverly Drive on the east, North Rodeo Drive on the west, and existing developments on the south. The proposed Project would provide a luxury hotel and multiple-use development, compatible with the scale and massing of the surrounding neighborhood and providing pedestrian-friendly amenities and uses along the street level. The Project consists of a single four- to nine-story structure including a luxury hotel, private membership club, appurtenant hotel uses including a day spa and wellness center, and uses open to the general public, including restaurant space and retail. The portion of the existing north-south alley that bisects the Project site is currently accessed from South Santa Monica Boulevard and would be relocated to the southern portion of the Project site. The new access point to the alley would be from the west side of North Beverly Drive.

3.1.1 Project Land Uses

The Project allows for a maximum allowable floor area of 220,949 square feet (sf) and a maximum of 115 hotel rooms. The Project also includes a private membership club with up to 500 members. Dedicated club facilities include a 36-seat screening room, a bar and lounge, and social spaces. Other Project features include appurtenant hotel uses include a day spa and wellness center, uses open to the general public including 25,094 sf of restaurant space (indoor and outdoor) and 24,976 sf of retail, and 178 parking spaces located in a subterranean garage. The Project opening year is expected to be 2026.

The proposed Project would replace 56,787 sf of existing commercial space in four structures located at:

- 456 North Rodeo Drive: 6,895 sf commercial with 9 surface parking spaces that is currently occupied.
- 468 North Rodeo Drive: 20,265 sf commercial with 6 surface parking spaces that is currently vacant.
- 449, 451, and 453 North Beverly Drive: 6,276 sf commercial that is currently vacant.
- 461-465 North Beverly Drive: 23,351 sf institutional with 5 surface and 45 underground spaces with driveway access on South Santa Monica Boulevard that is currently occupied.

A total of 33,436 sf of retail space is being removed, equal to a net reduction of 8,460 sf of retail on the site should the proposed Project be built.

3.1.2 Project Trip Generation

Trip generation for the Cheval Blanc Project uses were generally based on the most recent edition of the Institute of Transportation Engineers (ITE) *Trip Generation Manual* (10th Edition). Specific ITE Land Use codes for each use are provided in **Table 1**. ITE trip generation rates estimate the total number of trips to a given land use for all trip types, including trips made by employees, residents, or visitors to the site.

The only proposed use that was not estimated using ITE rates was the 500-member private membership club. The club provides access to a screening room, bar, lounge and social spaces, and access to the hotel's wellness center and spa. The club will have the ability to hold a limited number of members-only events per year based on the size of the event. Due to the unique nature of the programmed activities, there is not a comparable trip rate provided by ITE. A custom trip generation rate was developed for the private membership club for member trips based on the expected daily member visitation as identified in the *Parking Demand Analysis Study* (July 16, 2020) for the proposed Project. Based on the membership levels and site amenities, the membership club was estimated to generate 180 daily vehicle-trips and up to 40 vehicle-trips in a peak hour. This trip generation also assumes that members will drive alone to the Project site.

Table 1 provides the trip generation rates applied to the proposed Project.

Table 1: Trip Generation Rates

| Land Use | Trip Rates | | | | | |
|--------------------------------------|------------|------|------|--|--|--|
| | Daily | АМ | PM | | | |
| Hotel ¹ | 8.36 | 0.47 | 0.60 | | | |
| Private Membership Club ² | 0.36 | 0.04 | 0.08 | | | |
| Quality Restaurant ³ | 83.84 | 0.73 | 7.80 | | | |
| Retail ⁴ | 37.75 | 0.94 | 3.81 | | | |
| Day Spa ⁵ | 14.50 | 1.21 | 1.45 | | | |

Notes:

Vehicle trip generation estimates were adjusted based on a variety of factors applicable to the Project context. For one type of credit, a 20% internalization trip credit was applied to the restaurant, retail, and day spa uses. That is, it was assumed that 20% of patrons to these businesses will be hotel guests arriving by foot internally from within the hotel building, not requiring an additional vehicle trip. This rate is consistent with the internal capture rate assumed in the *Parking Demand Analysis Study*. The Mixed-Use (MXD) Trip Generation Model was also utilized to determine if this level of internalization was reasonable. The MXD Model was developed by Fehr & Peers and the

¹ Hotel trip rates based on ITE Land Use 310 – Hotel.

² Trip generation rates based on daily member visitation rates provided in the Cheval Blanc Initial Study.

³ Restaurant trip rates based on ITE Land Use 931 – Quality Restaurant.

⁴ Retail trip rates based on ITE Land Use 820 – Shopping Center.

⁵ Day Spa trip rates based on ITE Land Use 918 – Hair Salon.

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Environmental Protection Agency (EPA), and it accounts for the site context and other factors to estimate potential internalization and multimodal trip reductions. The MXD results confirmed that a 20% internal capture rate is appropriate for the mix of uses that make up the proposed Project.

A 30% pass-by credit was assumed for the retail use per the most recent edition of the ITE *Trip Generation Handbook* (3rd Edition). Pass-by trips are those vehicles already passing the proposed Project location, and therefore these are not new trips to the overall roadway network but are instead existing trips that are already in the Beverly Hills Business Triangle and will visit the proposed retail use.

An adjustment was also made based on trip generation estimates for the existing commercial uses that will be demolished to make way for the proposed Project. Because some of the existing uses are currently vacant, the trip credit has been applied only for existing, active uses to account for the vehicle trips already on the roadway network.

No additional credits have been applied to the Project trip generation. However, it should be noted that hotel and club employees who wish to travel by transit would be provided with free transit passes, and secure bicycle parking, charging facilities for e-bicycles, bicycle showers, and bicycle lockers would be provided to encourage bicycle commuting, both of which measures may reduce employee vehicle trips.

Table 2 provides the detailed trip generation estimates for the proposed Project. After making the appropriate adjustments, the maximum development proposed in the Project will generate approximately 2,360 daily vehicle trips and up to approximately 90 vehicle trips during the AM peak travel hour and approximately 220 vehicle trips during the PM peak travel hour.

These Project trips were then broken down into the following trip types: employees, visitors arriving by private vehicle and using the valet, and visitors arriving by shared mobility transportation network companies (TNC), such as Uber or Lyft. The proliferation of TNCs in recent years is important to consider in a project of this type and size. Pick-up and drop-off trips, such as those utilizing TNC services, do not utilize site parking but they still generate a vehicle trip to and from the Project site. In order to account for TNCs, it was assumed that TNCs will account for 50% of the vehicle trips generated by the restaurant, and 66.6% of the vehicle trips generated by the hotel, based on observed drive ratios provided in the *Parking Demand Analysis Study*. Since each inbound TNC trip also results in an outbound TNC trip, the demand for inbound and outbound TNC trips were estimated and the higher of the two calculations was assumed for both directions to account for TNCs that drop off a patron and leave the Project site without picking up a new passenger. The percentage of trips generated by employees traveling to the Project site was also estimated using the parking demand estimates from the *Parking Demand Analysis Study*. **Table 3** provides the distribution of Project trips by type.



Table 2: Trip Generation Estimates

| | | Trip Estimates | | | | | | |
|---------------------------|--------------------------------|----------------|------|------|-------|------|------|-------|
| Land Use | Quantity | D.:1 | | AM | | PM | | |
| | | Daily | In | Out | Total | ln | Out | Total |
| Hotel | 115 rooms | 961 | 32 | 22 | 54 | 35 | 34 | 69 |
| Private Membership Club | 500 members | 180 | 16 | 4 | 20 | 32 | 8 | 40 |
| Quality Restaurant | 25,094 sf | 2,104 | 9 | 9 | 18 | 131 | 65 | 196 |
| | Internal Capture ¹ | (421) | (2) | (2) | (4) | (26) | (13) | (39) |
| Retail | 24,976 sf | 943 | 14 | 9 | 23 | 46 | 49 | 95 |
| | Internal Capture ¹ | (189) | (3) | (2) | (5) | (9) | (10) | (19) |
| | Pass-by Reduction ² | (226) | (3) | (2) | (5) | (11) | (12) | (23) |
| D. C. | 12,936 sf | 188 | 8 | 8 | 16 | 3 | 16 | 19 |
| Day Spa | Internal Capture ¹ | (37) | (1) | (2) | (3) | (1) | (3) | (4) |
| Total Gross Vehicle Trips | | 3,503 | 70 | 44 | 114 | 200 | 134 | 334 |
| Existing, Active Uses | 30,246 sf | (1,142) | (18) | (10) | (28) | (55) | (60) | (115) |
| | TOTAL NET VEHICLE TRIPS | 2,361 | 52 | 34 | 86 | 145 | 74 | 219 |

Notes: Detailed trip generation calculation contained in **Appendix C**. $^{\rm 1}$ Internal capture rate assumed to be 20%.

² Pass-by reduction assumed to be 30% based on the ITE *Trip Generation Handbook* (3rd Edition).

Table 3: Project Trips by Type

| | Vehicle Trip Estimates | | | | | | | |
|--|------------------------|--------------|---------|---------|--------------|---------|-----------|--|
| Land Use | Daily | AM Peak Hour | | | PM Peak Hour | | | |
| | | In | Out | Total | In | Out | Total | |
| Total Gross Vehicle Trips | 3,503 | 70 | 44 | 114 | 200 | 134 | 334 | |
| Total Estimated Employee Trips | 521 | 10 | 6 | 16 | 30 | 20 | 50 | |
| Total Estimated Visitor Valet Trips | 1,501 | 35 | 19 | 54 | 95 | 65 | 160 | |
| Estimated Visitor TNC Trips ^{1,2} | 1,482 | 25 | (19) 25 | (44) 50 | 75 | (49) 75 | (124) 150 | |
| Adjusted Total Gross Vehicle Trips | 3,503 | 70 | 50 | 120 | 200 | 160 | 360 | |

Notes:

- (1) TNCs assumed to be 50% of the vehicle trips generated by the restaurant, and 66.6% of the vehicle trips generated by the hotel, based on observed drive ratios provided in the *Parking Demand Analysis Study* technical memorandum (July 16, 2020).
- (2) Where inbound and outbound trips were unequal, the higher of the two calculations was assumed for both directions to account for TNCs that drop off a patron and leave the Project site without picking up a new passenger.

While the transportation assessment only considers a trip credit for existing uses that are currently active, the trip generation of the historic uses were also estimated to illustrate the vehicle travel demand for the Project in comparison to full occupancy of the existing uses on the site. **Table 4** compares the proposed Project trip generation to the historic trip generation of the site (i.e., when all existing uses were in operation). As shown, the Project will result in a net increase of 1,359 daily trips, including 67 AM peak hour trips and 144 PM peak hour trips, as compared to the historic trip generation of the Project site.

Table 4: Project vs. Historical Site Trip Generation

| | | Vehicle Trip Estimates | | | | | | | |
|---|-------|------------------------|-----|-------|-----|-----|-------|--|--|
| Land Use | Daily | АМ | | | PM | | | | |
| | | ln | Out | Total | ln | Out | Total | | |
| Total Gross Project Vehicle Trips (Without credit) | 3,503 | 70 | 50 | 120 | 200 | 160 | 360 | | |
| Total Existing Uses Historic (Fully Occupied) Vehicle Trips | 2,144 | 34 | 19 | 53 | 104 | 112 | 216 | | |
| NET CHANGE IN SITE-GENERATED VEHICLE TRIPS | 1,359 | 36 | 31 | 67 | 96 | 48 | 144 | | |



3.1.3 Alley Realignment

An existing north-south public alley connects South Santa Monica Boulevard and Brighton Way, parallel with North Rodeo Drive and North Beverly Drive. The alley is currently accessed via South Santa Monica Boulevard, and bisects the Project site. The Project proposes to relocate that portion of the alley that bisects the Project site and relocate it, as a public alley, so that it connects North Beverly Drive to Brighton Way. Accordingly, existing trips into the alley from South Santa Monica Boulevard will reroute with implementation of the proposed Project to instead use the new alley entrance on North Beverly Drive.

The new alley access will be located approximately 120 feet north of the existing signalized mid-block crossing on North Beverly Drive. Access from northbound North Beverly Drive will be provided by a two-way left-turn lane which, immediately north of the proposed alley entrance, transitions to a northbound left-turn pocket for vehicles turning onto South Santa Monica Boulevard. Across from the proposed alley location are two adjacent driveways for parking garages on the east side of North Beverly Drive.

The relocation of the alley will require on-street parking to be relocated or removed, potentially affecting up to five (5) parking meter spaces on North Beverly Drive. At the time parking observations were collected in early 2021, a portion of on-street parking on the west side of North Beverly Drive had been converted to outside dining space and only four (4) short-term (20 minute) parking spaces were in operation.

The alley will remain one-way in the westbound/southbound direction, and the existing exit onto Brighton Way will remain as is. Three of the existing uses within the Project site have parking in the alley. The alley parking used by existing uses within the Project site will be eliminated. Parking and valet operations located in the alley for sites adjacent to the Project site will remain unchanged. The proposed alley relocation, including the turn geometry, has been designed in accordance with City standards to ensure emergency vehicle, utility, delivery, and other service truck access.

The existing alley travel demand was obtained from Appendix IS-9: Alley Study of the *Cheval Blanc Beverly Hills Specific Plan: Initial Study* (Eyestone Environmental, 2020) (Alley Study). The Alley Study collected weekday and weekend traffic counts at the South Santa Monica Boulevard alley entrance in April and May of 2019. The following average weekday counts were observed:

- 718 vehicles per day (485 from the west / 233 from the east)
 - o 91% automobile
 - o 8% single-unit delivery trucks
 - o 1% garbage trucks and motorcycles
- 110 vehicles in the AM peak hour (62 from the west / 48 from the east)
 - o 94% automobile

- 5% single-unit delivery trucks
- o 1% motorcycles
- No garbage trucks observed
- 48 vehicles in the PM peak hour (35 from the west / 13 from the east)
 - o 90% automobile
 - o 10% single-unit delivery trucks
 - No motorcycles or garbage trucks observed

The alley demand in the mid-day peak hour was observed to be similar to and slightly higher than the PM peak hour. Daily demand and AM peak hour demand on a Saturday were observed to be only slightly lower than on a typical weekday, while the mid-day demand and PM peak hour demand was approximately the same on a Saturday as on a weekday. The alley demand on a Sunday was observed to be substantially lower (approximately 40% of the typical weekday demand).

Based on the alley travel demands observed in 2019, these vehicles were rerouted to the realigned alley entrance on North Beverly Drive. Vehicles can enter the alley from northbound or southbound North Beverly Drive and will exit the alley onto Brighton Way.

Development of the proposed Project would require an amendment to the Master Plan of Streets to accommodate the alley relocation. The Master Plan of Streets (Sheets 31 and 32) would be updated to reflect the new alley alignment. In addition, the cross-section of South Santa Monica Boulevard would be updated in the Master Plan of Streets (Sheet 53) to reflect new curb radii at the intersections with North Rodeo Drive and North Beverly Drive and reflect the right-of-way width of 71.5 feet along the western two-thirds of the Project site and 82 feet on the eastern one-third of the Project site (compared to 75 feet in current Master Plan of Streets).



3.1.4 Project Access

Visitors to the Project traveling either by private vehicle or TNC are assumed to access the Project using the motor court located on South Santa Monica Boulevard. Those traveling by private vehicle will use the valet service, and valet employees will then drive arriving guests' vehicles eastbound on South Santa Monica Boulevard and southbound on North Beverly Drive to enter the reconfigured alley and access the Project's subterranean parking. For departing guests, valet employees will use the direct outbound access from the subterranean parking to the motor court. The Project site plan is provided in **Figure 6**.

Similar to the existing alley entrance, vehicles could enter the motor court from both eastbound and westbound South Santa Monica Boulevard. Left turns out of the motor court will be prohibited such that all departing vehicles must turn right onto South Santa Monica Boulevard.

Employees at the Project will self-park in the subterranean parking garage. Employees will exit the Project using the southbound alley onto Brighton Way. Service and utility vehicles will access the Project site via the relocated alley entrance on North Beverly Drive. Full-size utility and service vehicles will use the two loading bays provided at the south end of the Project site, while smaller van-sized utility and service vehicles will use two additional loading bays provided in the below-grade parking structure.

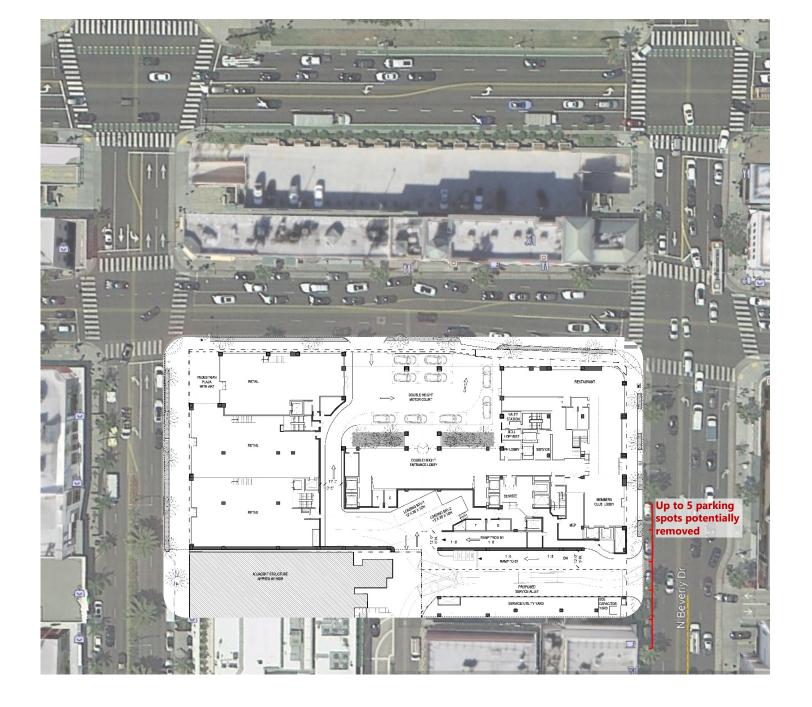




Figure 6

4. Vehicle Miles Traveled

This section documents the vehicle miles traveled (VMT) analysis of the Project. This VMT analysis is part of the environmental impact report being prepared for the proposed Project and follows the CEQA guidance for determining transportation impacts in accordance with SB 743.

4.1 Overview

On September 27, 2013, Governor Jerry Brown signed SB 743 into law, which initiated a process to change transportation impact analyses completed in support of CEQA documentation. SB 743 eliminates level of service (LOS) as a basis for determining significant transportation impacts under CEQA and provides a new performance metric, VMT. As a result, the State is shifting from measuring a project's impact to drivers (LOS) to measuring the impact of driving (VMT) as it relates to achieving State goals of reducing greenhouse gas (GHG) emissions, encouraging infill development, and improving public health through active transportation. To help lead agencies with SB 743 implementation, the Governor's Office of Planning and Research (OPR) produced a *Technical Advisory*. This VMT analysis follows OPR guidance and the City's adopted transportation impact thresholds. 6

4.2 CEQA Thresholds

SB 743 directed OPR to "prepare, develop, and transmit to the Secretary of the Natural Resources Agency for certification and adoption proposed revisions to the guidelines adopted pursuant to Section 21083 establishing criteria for determining the significance of transportation impacts of projects within transit priority areas... Upon certification of the guidelines by the Secretary of the Natural Resources Agency pursuant to this section, automobile delay, as described solely by LOS or similar measures of vehicular capacity or traffic congestion within a transit priority area, shall not support a finding of significance pursuant to this division...".

On January 20, 2016, OPR updated the CEQA Guidelines "Revised Proposal on Updates to the CEQA Guidelines on Evaluating Transportation Impacts in CEQA". In this update, the evaluation of VMT was recognized as "generally the most appropriate measure of transportation impacts." On November 2017, OPR proposed a new section, 15064.3, to help determine the significance of transportation impacts. The purpose of this section is to describe specific elements for considering the transportation impacts of a given project given the use of VMT as the primary measurement. This section was updated in July 2018 and finalized in December 2018 with criteria for analyzing transportation impacts.

⁵ Governor's Office of Planning and Research, Technical Advisory on Evaluating Transportation Impacts in CEQA, 2018.

⁶ City of Beverly Hills, Local California Environmental Quality Act Thresholds of Significance for Transportation Impacts and Local Transportation Assessment Guidelines, 2019, 10.

Per the guidance from OPR, "a lead agency may elect to be governed by the provisions of this section immediately. Beginning on July 1, 2020, the provisions of this section shall apply statewide." The City of Beverly Hills formally adopted the use of VMT for CEQA transportation impacts on October 10, 2019.

In accordance with Appendix G of the CEQA Guidelines, the proposed Project would have a significant impact related to transportation if it would:

- 1. **Conflict with a program, plan, ordinance, or policy** addressing the circulation system, including transit, roadways, bicycle, and pedestrian facilities.
- 2. Conflict or be inconsistent with CEQA Guidelines Section 15064.3, Subdivision (b) per the following criteria:
 - a. Land Use projects. Vehicle miles traveled exceeding an applicable threshold of significance may indicate a significant impact. Generally, projects within one-half mile of either an existing major transit stop or a stop along an existing high-quality transit corridor should be presumed to cause a less than significant transportation impact. projects that decrease vehicle miles traveled in the project area compared to existing conditions should be presumed to have a less than significant transportation impact.
 - b. Transportation projects. Transportation projects that reduce, or have no impact on, vehicle miles traveled should be presumed to cause a less than significant transportation impact. For roadway capacity projects, agencies have discretion to determine the appropriate measure of transportation impact consistent with CEQA and other applicable requirements. To the extent that such impacts have already been adequately addressed at a programmatic level, such as in a regional transportation plan EIR, a lead agency may tier from that analysis as provided in Section 15152.
 - c. Qualitative Analysis. If existing models or methods are not available to estimate the vehicle miles traveled for the particular project being considered, a lead agency may analyze the project's vehicle miles traveled qualitatively. Such a qualitative analysis would evaluate factors such as the availability of transit, proximity to other destinations, etc. For many projects, a qualitative analysis of construction traffic may be appropriate.
 - d. Methodology. A lead agency has discretion to choose the most appropriate methodology to evaluate a project's vehicle miles traveled, including whether to express the change in absolute terms, per capita, per household or in any other measure. A lead agency may use models to estimate a project's vehicle miles traveled and may revise those estimates to reflect professional judgment based on substantial evidence. Any assumptions used to estimate vehicle miles traveled and any revisions to model outputs should be documented and explained in the environmental document prepared for the project. The standard of adequacy in Section 15151 shall apply to the analysis described in this section.
- 3. **Substantially increase hazards due to a geometric design feature** (e.g., sharp curves or dangerous intersections) or incompatible uses (e.g., farm equipment).
- 4. Result in inadequate emergency access.

A summary of potential Project impacts regarding VMT under item 2 above is described below.



4.3 VMT Methodology

The VMT analysis begins with a review of the baseline VMT metrics and VMT impact thresholds developed in conjunction with the City of Beverly Hills and based on OPR guidance and the City's adopted transportation impact thresholds. The Project is then evaluated under four VMT analysis screening options to determine if it may have a VMT impact and require further evaluation. The analysis concludes by assessing if the Project may have an impact under cumulative conditions.

4.3.1 Baseline VMT

The Southern California Association of Governments (SCAG) 2016 Regional Transportation Plan/Sustainable Communities Strategy (RTP/SCS) trip-based model is a travel demand model with socioeconomic and transportation network inputs, such as population, employment, and the regional and local roadway network. The model outputs several travel behavior metrics, such as vehicle trips and trip lengths, that can be used to calculate VMT. The RTP/SCS model forecasts long-term transportation demands and identifies policies, actions, and funding sources to accommodate these demands. The RTP/SCS consists of the construction of new transportation facilities, transportation systems management strategies, transportation demand management and land use strategies. While SCAG recently adopted the 2020-2045 RTP/SCS Connect SoCal, the travel demand forecasting model used to evaluate the plan is not yet available for use. SCAG's new RTP/SCS model is expected to be available for use on land use and transportation planning projects in late 2021. Based on the planned growth and transportation improvements envisioned in the new RTP/SCS, the VMT trends reported from the 2016 RTP/SCS model are expected to be similar to those in the new 2020 model.

The SCAG RTP/SCS trip-based model was used to estimate the regional baseline VMT and the baseline VMT for the City. The current 2016 SCAG model has 2012 as the base year and 2040 as the forecast year. This baseline VMT methodology includes vehicle trips within the SCAG model to generate the following metrics:

- 1. Home-based VMT per Capita: Home-based vehicle trips are traced back to the residence of the trip-maker (non-home-based trips are excluded) and then divided by the residential population within the geographic area. This metric is used to estimate VMT for residential land uses.
- 2. Home-based Work VMT per Employee: Vehicle trips between home and work are counted, and then divided by the number of employees within the geographic area. This metric is used to estimate VMT for office, retail, and other commercial land uses.

The City's baseline VMT for each metric is shown in **Table 5**. These metrics estimate current VMT trends for residential and employment uses in the City of Beverly Hills for Year 2020 which is when the Notice of Preparation (NOP) was released for the Project.

Table 5: Baseline VMT for City of Beverly Hills

| VMT Metrics | | City Baseline VMT |
|---------------------|---|-------------------|
| VIVIT METRICS | | Year 2020 |
| Home-Based VMT | Baseline Home-Based VMT per Capita | 6.7 |
| Home-Based Work VMT | Baseline Home-Based Work VMT per Employee | 16.0 |

4.3.2 VMT Impact Thresholds

The City of Beverly Hills adopted a VMT impact threshold for land use projects on October 10, 2019, which states that a significant impact would occur if the Project generates VMT higher than 15% below the regional average.⁷ The regional average reflects that average amount of VMT generated within the SCAG region whereas the VMT data presented in the prior table reflects the average VMT generated within the City of Beverly Hills. The City's VMT impact thresholds based on the regional average are summarized in **Table 6**.

Table 6: City of Beverly Hills VMT Impact Thresholds

| | | Year 2020 | |
|---------------------|---|--------------------------|--------------------------|
| VMT Metrics | | Regional Baseline VMT | VMT Impact Threshold* |
| Home-Based VMT | Baseline Home-Based VMT per Capita | 14.5 | 12.3 |
| Home-Based Work VMT | Baseline Home-Based Work VMT per Employee | 17.7 | 15.0 |

^{*} The VMT Impact Threshold for each VMT metric is 15% below the respective Baseline VMT.

4.4 VMT Screening

The first step of a VMT analysis is to determine what type of analysis, if any, is needed. Based on the OPR *Technical Advisory*, the City of Beverly Hills adopted four screening criteria that the City may use to identify if a proposed project is expected to cause a less-than-significant impact without conducting a detailed study: project size, locally serving retail, project location in a low VMT area, and project accessibility to transit. The four screening criteria are detailed below and applied to all or, as applicable, various components of the Project to determine if the Project as a whole, or a particular component, has the potential to result in a VMT impact. Once the Project as a whole, or a Project component, qualifies under one of the screening criteria, the Project or the applicable component is screened out from further consideration.

⁷ City of Beverly Hills, Local California Environmental Quality Act Thresholds of Significance for Transportation Impacts and Local Transportation Assessment Guidelines, 2019, 10.



4.4.1 Screening Criteria 1: Project Size

Land use projects that generate less than 110 daily trips are presumed to have less than significant VMT impacts absent substantial evidence to the contrary. Therefore, these projects are screened out from completing a VMT analysis based on project size.

When compared to the existing land uses on the Project site, the Project would generate approximately 2,360 net new vehicle trips (as shown in **Table 2**). This daily trip generation exceeds the number of daily trips (up to 110 trips) that is applicable for project size screening. Therefore, the proposed Project does not meet this screening criteria.

4.4.2 Screening Criteria 2: Locally Serving Retail

Land use projects that have local-serving retail uses, defined as commercial projects with retail uses less than 50,000 sf, are presumed to have less than significant VMT impacts absent substantial evidence to the contrary. The commercial component of the Project would construct up to 25,000 sf of mercantile retail space. In comparison to the amount of existing retail uses located on the Project site, the Proposed Project would result in a net reduction in retail space of 8,460 sf. Nevertheless, the amount of new retail space would meet the screening criteria for locally serving retail uses and while the Project would reduce the total amount of retail uses, the screening criteria is met, which means that the retail component of the proposed Project is presumed to have a less than significant VMT impact and can be screened out from further VMT analysis.

4.4.3 Screening Criteria 3: Low VMT Area Screening

OPR guidance states that residential and office projects located within a low VMT generating area may be presumed to have a less than significant impact absent substantial evidence to the contrary. A low VMT generating area generally has higher density, a mix of land uses, and provides opportunities for people to walk to nearby uses instead of always driving. Since the Project contains neither residential nor office uses, the Project does not meet this screening criteria.

4.4.4 Screening Criteria 4: Transit Priority Areas (TPA) Screening

Projects located in a Transit Priority Area (TPA) may also be screened out from conducting a VMT analysis because they are presumed to have a less than significant impact absent substantial evidence to the contrary. TPAs are defined in the OPR *Technical Advisory* as a ½ mile radius around an existing or planned major transit stop or an existing stop along a high-quality transit corridor (HQTC). A HQTC is defined as a corridor with fixed route bus service frequency of 15 minutes (or less) during peak commute hours.

The City of Beverly Hills's adopted VMT thresholds allow screening for TPAs that are located within ½ mile of a Metro Rapid bus stop for commercial zones. The TPAs in the City of Beverly Hills are shown in **Figure 7**. The TPAs in the City are based on bus schedules and service frequencies that reflect typical conditions in 2019 and early 2020. Beginning in July 2020, Metro implemented temporary service changes in response to the impacts of COVID-19 which caused the majority of bus routes in the study area to operate on a Sunday service schedule with reduced frequencies compared to typical weekday operations. However, in response to recent increasing ridership demands, Metro implemented service changes beginning December 13, 2020. While the majority of the transit lines that

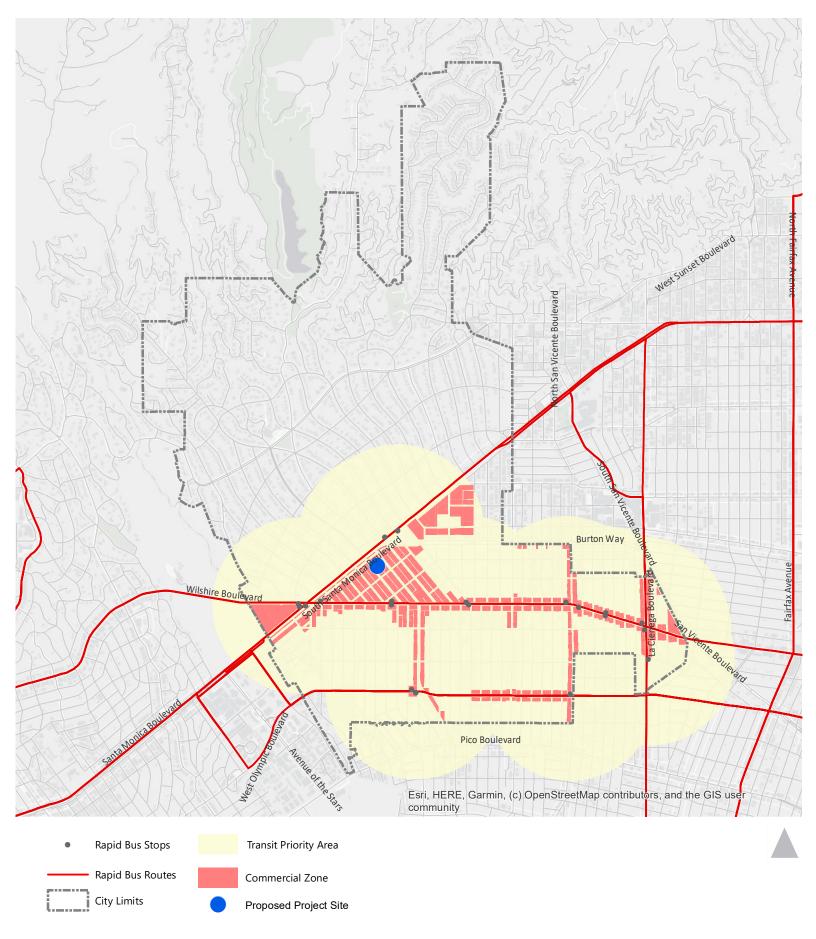




Figure 7

provide service in the vicinity of the Project site are still operating on reduced frequencies in comparison to service levels prior to the pandemic, these changes are anticipated to be temporary with service returning to typical weekday frequencies as travel and ridership demands increase.

The presumption that a project in a TPA will have a less than significant impact absent substantial evidence to the contrary may not be appropriate if the project:

- 1. Has a Floor Area Ratio (FAR) of less than 0.75;
- Includes more parking than is required by the City, unless additional parking is being provided for design feasibility, such as completing the floor of a subterranean or structured parking facility, or if additional parking is located within the project site to serve adjacent uses; or
- 3. Is inconsistent with the applicable Sustainable Communities Strategy (as determined by the City).

Based on existing transit service in Beverly Hills, the Project is located in a commercial zone within a TPA and is less than ½ mile from six Metro Rapid bus stops, including the Santa Monica/Crescent eastbound stop, the Santa Monica/Cañon westbound stop, and the Santa Monica/Wilshire bi-directional stop of Metro Rapid Line 704, as well as the Wilshire/Santa Monica bi-directional stop of Metro Rapid Line 720. In addition, the Project site will be 0.4 miles from the recently approved North Portal entrance to the Metro D Line Wilshire/Rodeo station. The proposed Project's FAR is 4.03 and meets the 0.75 minimum requirement. The Project is also providing less parking than required by the City's Municipal Code. The Project site is designated as Mixed Residential and Commercial in the SCAG RTP/SCS, and therefore, the proposed land uses are consistent with the RTP/SCS. Based on this information, the Project is presumed to have a less than significant VMT impact and can be screened out from further VMT analysis.

4.5 VMT Analysis for Cumulative Conditions

For cumulative conditions, OPR states that a project that is below the VMT impact thresholds and does not have a VMT impact under baseline conditions would also not have a cumulative impact as long as it is aligned with long-term State environmental goals, such as reducing GHG emissions, and relevant plans, such as the SCAG RTP/SCS.⁸ The City of Beverly Hills adopted the following cumulative threshold for VMT impacts:

- 1. A significant impact would occur if the project causes VMT within the City to be higher than the no project alternative under cumulative conditions.
- 2. A significant impact would occur if the project is determined to be inconsistent with the RTP/SCS.

Table 7 shows a comparison of socio-economic characteristics and VMT metrics of the Tier 2 Traffic Analysis Zone (TAZ) of the Project location between the baseline and future year. The TAZ area consists of the proposed Project site and adjacent commercial uses. Based on the expected increase in employment growth in Year 2040, the proposed Project site uses are accounted for in the SCAG model growth projections. The TAZs in the City of Beverly Hills and Project TAZ are shown in **Appendix C**.

 ⁸ Governor's Office of Planning and Research, Technical Advisory on Evaluating Transportation Impacts in CEQA, 2018, 12.
 Cheval Blanc Beverly Hills Specific Plan Transportation Impact Report

As shown in **Table 7**, the employment in the TAZ is anticipated to increase by approximately 1,250, while VMT per employee is anticipated to decline from 17.1 to 12.2 based on additional land use densities, increased transit service, and trip reduction strategies envisioned by SCAG in the RTP/SCS. In addition, the Project site is designated as Retail and Commercial and Services in the SCAG RTP/SCS. Therefore, the Project is consistent with the RTP/SCS.

For evaluating potential VMT impacts under cumulative conditions, the future horizon year forecasted in the SCAG RTP/SCS model is considered to be the no project condition. Since the growth included in the SCAG model already reflects the development that is proposed to occur with the Project, the Project would not increase VMT in comparison to cumulative no project conditions and would not have a cumulative VMT impact.

Table 7: SCAG Growth Assumptions for Project TAZ

| 2016 SCAG RTP/SCS | Base Year Data | Year 2040 Data |
|---------------------------------|----------------|----------------|
| Tier 2 TAZ | 20868200 | 20868200 |
| Household | - | - |
| Total Employment | 15,196 | 16,442 |
| Home-Based VMT per capita | - | - |
| Home-Base Work VMT per employee | 17.1 | 12.2 |

Source: 2016 SCAG RTP Travel Demand Model.

4.6 VMT Summary and Conclusions

The Project meets the following screening criteria adopted by the City of Beverly Hills:

Screening Criteria 2, Locally Serving Retail Screening, states that projects which provide local-serving retail uses, defined as commercial projects with retail uses less than 50,000 sf, are presumed to have a less than significant VMT impact absent substantial evidence to the contrary. The proposed Project includes 24,976 sf of retail space and meets the criteria for retail screening. This means that the retail component of the Project is presumed to have a less than significant VMT impact and can be screened from further VMT analysis.

Screening Criteria 4, TPA Screening, states that projects will not need to complete a VMT analysis if the project is located in the City's definition of TPA which accounts for commercial zones in proximity to Metro Rapid bus stops. The Project is located within the boundary of three existing TPAs and meets the additional design criteria outlined for TPA screening.

Based on the screening criteria, the Project is presumed to have a less than significant VMT impact and is screened out from further VMT analysis.



5. Site Access & Circulation

This chapter presents an overview of site access and on-site circulation for the Project.

5.1 Overview

A valet motor court on South Santa Monica Boulevard would be used for drop-off and pick-up for hotel guests, club members, and spa, retail, and restaurant patrons. Valet-driven vehicles would return from the subterranean parking garage to the motor court via ground-floor internal circulation.

The city block bounded by South Santa Monica Boulevard on the north, North Beverly Drive on the east, Brighton Way on the south, and North Rodeo Drive on the west is currently bifurcated by a north-south alley connecting South Santa Monica Boulevard with Brighton Way. The portion of the alley that bisects the Project site would be relocated to the southern portion of the Project site. The new access point to the alley would be located on the west side of North Beverly Drive.

The 178-space subterranean parking garage would also provide electric vehicle charging equipment, bicycle parking, and charging facilities for electric bicycles. Employees would self-park in the below-grade garage accessed via the relocated alley entrance on North Beverly Drive and exit the Project site by travelling south down the alley to Brighton Way. Large format delivery vehicles, emergency services, and utility trucks would enter via the relocated alley and use the two full-size loading areas located at-grade on the Project site, and then exit southbound via the alley to Brighton Way. Two small-format van loading spaces would also be provided below grade, accessed via North Beverly Boulevard; smaller format vans would also exit southbound via the alley to Brighton Way.

Primary pedestrian access to the Project would be provided through the hotel entrance along South Santa Monica Boulevard. A club member lobby at ground level would provide secondary pedestrian access from North Beverly Drive. Retail spaces along Rodeo Drive would have separate pedestrian access points from the sidewalk along the street. Hotel visitors would not be provided access to the hotel via the Rodeo Drive retail spaces. The main access to the ground floor restaurant would be through the hotel lobby, with an ancillary, pedestrian-only access point provided on South Santa Monica Boulevard and/or North Beverly Drive.

The site plan for the Project was previously shown in **Figure 6**. The Specific Plan contains several objectives related to site access and circulation as summarized below.

- Provide pedestrian friendly amenities and uses along the street level, including sidewalk widths and setbacks that are generally consistent with other development along South Santa Monica Boulevard, North Rodeo Drive, and North Beverly Drive.
- Accommodate vehicle flow on adjacent City streets and promote multiple transportation modes (walking, bicycling) by relocating the alley bisecting the Site, placing parking underground, limiting driveway access points, and enhancing the pedestrian environment on all of the adjoining streets.

5.2 Project Driveways

As shown in **Figure 6**, several driveways would provide access to the Project site, including separate ingress and egress driveways on South Santa Monica Boulevard to and from the motor court, and the subterranean parking garage driveway with access to and from the realigned alley. The access driveways are described in detail below.

Motor Court Ingress – This driveway provides ingress into the valet motor court from South Santa Monica Boulevard. Both right and left-turns into the Project site would be allowed, similar to the permitted turning movements at the existing alley entrance. This driveway would be utilized for drop-off by entering hotel guests, club members, and spa, retail, and restaurant patrons, whether they arrive in their own vehicles or via a shared-ride vehicle. Visitors arriving in their own vehicles would utilize valet service, and valet operators would park their vehicles in the subterranean garage, which would require exiting the motor court and entering the realigned alley from North Beverly Drive to access the parking garage.

Motor Court Egress – This driveway provides egress from the valet motor court to South Santa Monica Boulevard. Egress would be limited to right-turns only and would be controlled by a stop sign for departing vehicles. This driveway would be utilized by hotel guests, club members, and spa, retail, and restaurant patrons following pick up of their vehicles in the motor court. Visitors who arrived in their own vehicles and utilized valet parking would pick up their vehicles in the motor court. Valet operators would utilize an internal drive aisle that provides a direct connection from the subterranean parking garage to the motor court to exit the site via this driveway.

Alley Access – The alley entrance would be relocated to North Beverly Drive on the southern edge of the Project site. The alley entrance would provide ingress to the subterranean parking facility and the ground-level full-size loading docks. The existing north-south portion of the alley south of the Project site would remain as is and would allow truck deliveries to exit the site and employees to exit the subterranean parking garage. Valet operators would only utilize the new east-west portion of the alley to enter the parking garage.

5.3 Alley Operations

The proposed alley reconfiguration will require that vehicles using the alley make a 90-degree turn from the new east-west oriented portion of the alley (from Beverly Drive) to access the existing and unaffected north-south segment. Project-generated traffic in the existing portion of the north-south alley will be limited to employees, delivery trucks, emergency services, and utility trucks only. As part of the Alley Study, a vehicular turning movement evaluation for the reconfigured alley was conducted for each of the vehicle types directly observed or anticipated to utilize the alley, including typical single-unit delivery trucks (SU-30 and SU-40), a typical garbage truck, two types of single-body fire trucks (not large "hook and ladder" trucks)⁹, and a semi-trailer truck (WB-40) of the size typically used for deliveries in urban environments. The Alley Study indicated that each of these vehicle types would be able to make the required new turn with little or no difficulty (no multi-point turns or other such maneuvers). As a result, the proposed reconfiguration of the alley would not limit its use.

⁹ The Beverly Hills Fire Department specified the type of fire trucks to be tested. Single-body fire trucks impose more stringent turning requirements than hook-and-ladder trucks.

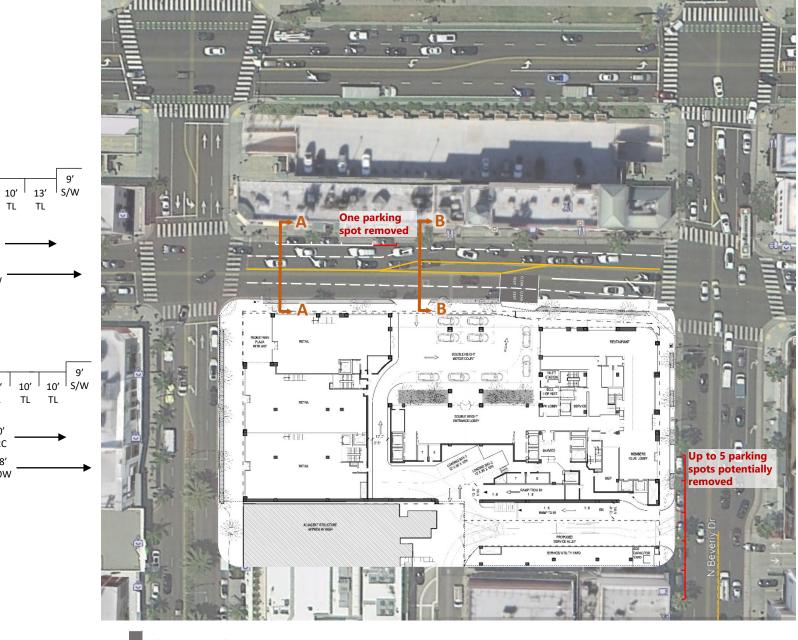


5.4 Access Recommendations

The Project's site access was reviewed in relation to the existing roadway network and permitted turning movements at Project driveways. For the primary Project access to the motor court from South Santa Monica Boulevard, the westbound left-turn from South Santa Monica Boulevard is projected to have a demand of approximately 30 vehicles in the AM peak hour and 90 vehicles in the PM peak hour. To minimize vehicle queueing on eastbound South Santa Monica Boulevard, a left-turn lane for vehicles entering the into the motor court could be implemented as follows:

Remove one parking spot from the north side of South Santa Monica Boulevard in order to extend the painted median to the Project motor court entrance, as illustrated on **Figure 8**. This would provide a separate storage lane for westbound left-turning vehicles such that westbound through traffic would not be impeded by vehicles waiting to turn. It is noted that the parking spot that would be removed under this alternative site access option was not in operation as of February 2021, when it was observed that a bag had been placed over the meter.

For the access driveway to the realigned alley, the northbound left-turn from North Beverly Drive is projected to have a demand of approximately 15 vehicles in the AM peak hour and 10 vehicles in the PM peak hour. These vehicles could utilize the existing center turn lane on North Beverly Drive to turn into the alley without blocking northbound through vehicles.





North

North

A-A

B-B

S/W

S/W

10′

10' | 10' | 10' | TL TL TL

68' ROW

10'

50′ C2C

68' ROW

TL

TL

"KEEP CLEAR" Pavement Striping

Site Access Recommendation

Figure 8

6. Active Transportation System

This chapter discusses the Project in relation to the surrounding active transportation system.

6.1 Overview

The transit, bicycle and pedestrian impacts of the proposed Project were compared to existing conditions in the study area. For the proposed Project, the active transportation system was considered to be impacted if the Project conflicted with existing facilities or adopted policies, plans, or programs supporting active transportation.

6.2 Disruptions to Existing Transit Service

No existing transit service is provided along the Project's frontage on South Santa Monica Boulevard. On North Beverly Drive, the closest transit stop to the Project site is on the west side of the street just north of Brighton Way. Therefore, the land use and site access changes under the Project, including the reconfiguration of the alley entrance onto North Beverly Drive, would not result in a disruption to existing transit service.

6.3 Interferes with Planned Transit Service

No transit projects are planned on South Santa Monica Boulevard or on North Rodeo Drive. On North Beverly Drive, the North Portal entrance/exit to the D Line Wilshire/Rodeo Line station will be constructed on the west side of the street just north of Wilshire Boulevard, approximately 0.4 miles from the Project site. On-street parking will be removed on the southern portion of North Beverly Drive to provide the right-of-way needed to construct the North Portal and additional parking may be removed to provide pick-up/drop-off loading zones for transit riders. Given that these changes would occur south of Dayton Way, two blocks south of the Project site, the Project would not interfere with the planned changes on North Beverly Drive. Therefore, the land use and site access changes under the Project would not result in a disruption to planned transit service.

6.4 Disruptions to Existing Bicycle Facilities

There are no existing bicycle facilities adjacent to the Project site. Therefore, the Project would not result in a disruption to existing bicycle facilities.

6.5 Interferes with Planned Bicycle Facilities

There are bicycle facilities envisioned in the *City of Beverly Hills Complete Streets Plan* for each of the roadways by which access to the proposed Project is provided. A Class IV protected bicycle lane is planned for Beverly Boulevard, a Class II bicycle lane is planned for South Santa Monica Boulevard, and a Class III Bicycle Boulevard is planned for Brighton Way. The Project site would not change the right-of-way available on the adjacent roadways, and therefore, the Project would not interfere with the implementation of these facilities. Therefore, the Project would not result in interference with planned bicycle facilities.

6.6 Disruptions to Existing Pedestrian Facilities

The Project site plan proposes to improve pedestrian facilities compared to existing conditions, providing pedestrian-friendly treatments along the public rights-of-way adjacent to the Project site. The ground level is designed with pedestrian amenities such as an approximately 670 sf pedestrian plaza area at the corner of South Santa Monica Boulevard & North Rodeo Drive, special paving for the public sidewalk right-of-way, dedication of additional surface right-of-way for public sidewalk uses along South Santa Monica Boulevard, and landscaping in parkways on the perimeter of the Project site. While the Project would add additional driveways along South Santa Monica Boulevard and North Beverly Drive, these driveways are not expected to result in a significant impact to pedestrians. Upon completion of the proposed Project, enhanced pedestrian connectivity and improvements to the pedestrian environment would be available via the pedestrian facilities just described. Additionally, by placing retail, restaurant, and hotel uses in close proximity to existing commercial and residential centers and high-quality public transit, as well as by enhancing the pedestrian environment with landscaping, the proposed Project would encourage pedestrian activity in the Project area. The pedestrian improvements provided by the proposed Project would be in accordance with General Plan Goal CIR 6 by enhancing multi-modal transportation options and CIR 7 by making walking a more desirable travel choice, as well as with Complete Streets Plan Goals P1 through P3 and V3 by enhancing the pedestrian and neighborhood environment in the Project area. Therefore, the Project would not result in disruptions to existing pedestrian facilities.

6.7 Interferes with Planned Pedestrian Facilities

The City of Beverly Hills Complete Streets Plan envisions pedestrian corridor improvements on South Santa Monica Boulevard throughout the study area, including new and upgraded sidewalks, tightened curb radii to slow vehicle speeds, and mid-block crossings, among others. The pedestrian improvements planned for the proposed Project will enhance and align with the improvements identified by the City and will further the City's efforts to improve the pedestrian experience. Therefore, the Project would not result in a disruption to planned pedestrian facilities.



7. Construction Conditions

This chapter reviews the potential construction impacts of the proposed Project. The construction evaluation for the proposed Project considered the temporary impacts due to lane closures, need for temporary traffic control, emergency vehicle access, traffic hazards to bicycles and/or pedestrians, damage to the roadbed, the potential for truck traffic on roadways not designated as truck routes, and other similar impediments to circulation.

7.1 Overview

The initial construction phase is expected to commence in 2022 and be completed in 2026. Most construction activity would occur from 8:00 AM to 4:00 PM with some nighttime work, principally excavation, material loading and hauling. The duration of the construction elements based on information provided by the Project applicant is as follows:

Phase 1 is expected to have a 7.5-month duration with a start date in 2022. Project elements slated for construction during Phase 1 include:

- Utilities relocation
 - Infrastructure
- Demolition of 449 and 461 Beverly Drive
- Excavation (6 weeks)
 - Excavation of 449 Beverly and partial excavation of 461 Beverly in preparation for garage construction under relocated alley; garage construction at driveway to grade with overhead shoring in place
- Parking garage construction, Phase 1

Phase 2 would overlap with Phase 1 for 1.5 months. The overall duration of Phase 2 construction is expected to last 32 months. Project elements slated for construction during Phase 2 include:

- Utilities relocation
 - New utility cutover
- Demolition of 456 Rodeo Drive and 468 Rodeo Drive
- Excavation (15 weeks)
- Parking garage construction, Phase 2
- Hotel Building
- Site Work

The overall duration of construction is expected to last 38 months.

There are four main construction traffic impacts associated with the Project:

- Trucks traveling to and from the site to remove debris, fill, and other items (haul trucks)
- Equipment and material delivery/staging
- Worker traffic
- Worker parking

7.1.1 Haul Truck Traffic

Hauling activity is expected to occur between the Project site and off-site staging and/or logistics areas still to be determined. Between the hours of 7:00 PM to 10:00 PM, the designated outbound (leaving the Project site) haul route is anticipated to be from the Project site to eastbound South Santa Monica Boulevard to Burton Way to San Vicente Boulevard to southbound La Cienega Boulevard to Interstate 10. The reverse of this route would be used for inbound truck traffic from 7:00 PM to 10:00 PM. Between the hours of 10:00 PM to 7:30 AM, the designated outbound haul route is anticipated to be from the Project site to southbound Beverly Drive to eastbound Wilshire Boulevard to southbound La Cienega Boulevard. Between the hours of 10:00 PM to 7:30 AM, the inbound haul route would be from Interstate 10 to northbound La Cienega Boulevard to westbound Wilshire Boulevard to northbound North Camden Drive to eastbound South Santa Monica Boulevard to the Project site.

The proposed Project would create a construction management plan that provides for truck staging and designates appropriate travel routes to access the site. However, trucks could impact the adjacent roadway network as follows:

- The roadways designated as the truck routes for the Project are already some of the most congested in the City of Beverly Hills and the City of Los Angeles.
- There is no guarantee that truck traffic would not deviate from the designated routes and impact other roadways when traveling to and from the site.
- The number of trucks required to access the site during the excavation process would be approximately 60 trucks per day for a 21-week period.

7.1.2 Delivery and Staging of Material and Equipment

Another source of construction traffic would derive from the transportation of materials and equipment to the site. One example would be concrete, of which substantial quantities would be required for the parking garage and the buildings on-site. Other materials could include plumbing supplies, electrical fixtures, and even items used in furnishing the hotel and other uses. These materials would have to be delivered to the site and stored on-site as well. These deliveries would occur through variously sized vehicles including small delivery trucks to cement mixer trucks, and possible 18-wheel trucks.

Additionally, heavy construction equipment would have to be delivered to the site. This equipment could include cranes, bulldozers, excavators, and other large items of machinery. Most of the heavy equipment would be transported to the site on large trucks such as 18-wheelers or other similar sized vehicles, and the heavy equipment would remain on-site until it's no longer needed.



The influx of this material and equipment could create impacts on the adjacent roadway network based on the following considerations:

- There may be intermittent periods when large numbers of material deliveries are required such as when concrete trucks would be needed for the parking garage and the buildings.
- Some of the materials and equipment could require the use of large trucks (18-wheelers), which can create additional congestion on the adjacent roadways.
- Delivery vehicles may need to park temporarily on adjacent roadways such as Santa Monica Boulevard, Beverly Drive, and Rodeo Drive as they deliver their items.

A City-approved construction traffic control plan and haul route would be implemented.

7.1.3 Worker Traffic

The maximum number of workers on the Project site would be 500 per day. The peak number of construction workers for each general construction phase is as follows.

Excavation/Foundations: 98 construction workers

Parking Garage: 137 construction workers

• Hotel Building: 477 construction workers

• Sitework: 25 construction workers

The number of vehicles associated with these workers could be estimated by applying the following process:

- Each worker would drive to and from the site daily at least once (two daily person trips per worker).
- A small percentage of the workers may carpool or travel together. This can be based on regional auto occupancy factors (1.25 persons per vehicle).
- Workers would travel to/from the site in the morning (7:00 to 9:00 AM) and afternoon peak hours (4:00 to 6:00 PM). They are not all likely to arrive at the construction site within the same hour nor would they leave the site at the same time. It was assumed that no more than half of the drivers would arrive during a single peak hour either in the morning or afternoon as many construction workers arrive at the site outside of the peak hours, arriving prior to 7:00 AM and leaving the site before 4:00 PM.

Using the maximum number of workers (500), the number of worker trips would be as follows:

- 800 daily trips
- 200 Peak hour trips (one hour in the morning and afternoon peak period)

7.1.4 Worker Parking

During the initial four years of construction, construction workers would utilize a mixture of public and private parking facilities in the close proximity to the Project site. Once construction of the on-site subterranean parking

structure is sufficiently progressed, construction employees would utilize on-site spaces as they become available, greatly reducing the off-site construction parking demand.

The need to park workers off-site could result in a specific traffic related impact because it could lead to worker parking spilling over into adjacent, and potentially residential areas. Workers may park in these areas because they find the off-site parking arrangement cumbersome and want to park at a location closer to the site.

7.1.5 Construction Summary & Mitigations

Several potential traffic-related impacts could result from construction of the proposed Project:

- Haul trucks traveling on congested roadways adjacent to the site could create additional congestion on the roadways.
- Truck traffic traveling to/from the site for material and equipment delivery could be very large trucks (18-wheelers), which could increase congestion on the adjacent roadways.
- The material and equipment delivery process could require vehicles to temporarily stop and unload on the adjacent streets. This loading/unloading process could involve temporary lane closures on the adjacent streets.
- Workers needing to park off-site while the parking garage is being constructed could forgo parking in designated off-site locations and instead park along adjacent streets. This parking spillover could impact the adjacent residential areas.

The construction impacts and recommended mitigation measures are described below.

Temporary Construction Impact 1: This impact derives from the haul truck traffic accessing the site and the delivery of materials/equipment. The Project applicant would prepare a Draft Construction Traffic Management Plan to address the issues above.

Mitigation Measure 1: Mitigating this impact would require the implementation of the following measures:

The developer shall update their Construction Traffic Management Plan to include plans to accomplish the following:

- Maintain existing access for land uses in proximity of the Project site during Project construction.
- Schedule deliveries and pick-ups of construction materials to non-peak travel periods, to the maximum extent feasible.
- Coordinate deliveries and pick-ups to reduce the potential of trucks waiting to load or unload for protracted periods of time.
- Minimize obstruction of through traffic lanes on Wilshire Boulevard and Santa Monica Boulevard.
- Construction equipment traffic from the contractors shall be controlled by flagman.



- Identify designated transport routes for heavy trucks (in addition to haul trucks) to be used over the duration of the proposed Project.
- Schedule vehicle movements to ensure that there are no vehicles waiting off-site and impeding public traffic flow on the surrounding streets.
- Establish requirements for loading/unloading and storage of materials on the Project site, where parking spaces would be encumbered, length of time traffic travel lanes can be encumbered, sidewalk closings or pedestrian diversions to ensure the safety of the pedestrian and access to local businesses.
- Coordinate with adjacent businesses and emergency service providers to ensure adequate access exists to the Project site and neighboring businesses.

Significance After Mitigation: Less than significant

Temporary Construction Impact 2: Construction workers could choose to park in areas adjacent to the Project site including residential streets. These workers might choose to park in these areas because on-site parking could be limited due to the construction activities or off-site parking areas might be considered to be too remote or inconvenient.

Mitigation Measure 2: The developer shall submit a Construction Workers' Parking Plan identifying parking locations for construction workers. To the maximum extent feasible, all worker parking shall be accommodated on the Project site. During phases when construction worker parking cannot be accommodated on the Project site, the Construction Worker's Parking Plan shall identify alternate parking locations for construction workers and the method of transportation to and from the Project site for approval by the City 30 days prior to commencement of construction. The Construction Workers Parking Plan must include appropriate measures to ensure that the parking location requirements for construction workers would be strictly enforced. These include but are not limited to the following measures:

- Provide all construction contractors with written information on where their workers and their subcontractors are permitted to park and provide clear consequences to violators for failure to follow these regulations. This information would clearly state that no parking is permitted on residential streets north of Wilshire or in public parking structures.
- No construction worker parking shall be permitted within 500 feet of the nearest point of the Project site
 except within designated areas. The contractor shall be responsible for informing subcontractors and
 construction workers of this requirement, and if necessary, for hiring a security guard to enforce these
 parking provisions. Contractor shall be responsible for all costs associated with enforcement of this
 mitigation measure.
- In lieu of the above, the Project developer/construction contractor has the option of phasing demolition and construction activities such that all construction worker parking can be accommodated on the Project site throughout the entire duration of demolition and construction activities.

Significance After Mitigation: Less than significant

7.1.6 Cumulative Construction Traffic Impacts

Additional construction impacts could occur as the result of simultaneous construction activities in the Project area, such as the on-going construction of the D Line Extension and the North Portal for the Wilshire/Rodeo station. Potential impacts include:

- Simultaneous arrival and departure of haul trucks The increased volume of haul truck traffic and number
 of trucks entering/exiting roadways surrounding the two Project sites could result in congestion on those
 roadways.
- Simultaneous arrival and departure of delivery trucks Equipment and supply delivery vehicles could
 impact adjacent roadways by creating additional congestion. There may also be temporary queuing of
 these delivery vehicles if large numbers of vehicles arrive or depart at once.

Temporary Construction Impact 3: Simultaneous construction activities in the Project area could result in significant, although temporary, traffic impacts resulting from haul truck traffic and the simultaneous delivery of materials/equipment. For this reason, construction associated with the proposed Project would have a cumulatively considerable, and therefore significant, contribution to cumulative traffic impacts.

Mitigation Measure 3: With implementation of the following mitigation measures, the proposed Project's contribution to cumulative traffic impacts would be reduced to less than significant.

The developer for the Project shall coordinate with the City of Beverly Hills regarding the following:

- All temporary roadway closures shall be coordinated to limit overlap of roadway closures.
- All major deliveries shall be coordinated to limit the occurrence of simultaneous deliveries. The Project
 applicant shall ensure that deliveries of items such as concrete and other high-volume items shall be
 reported to the City's major delivery schedule and reporting shall be incorporated as a requirement into
 the Construction Traffic Management Plan to ensure that simultaneous deliveries are avoided when
 feasible.
- The applicant shall coordinate regarding the loading and unloading of delivery vehicles. Any off-site staging areas for delivery vehicles shall be consolidated and shared where feasible.
- The applicant or its representative shall meet on a regular basis with the City during construction to address any outstanding issues related to construction traffic, deliveries, and worker parking.
- If construction on other major projects in the vicinity is occurring simultaneously with this Project, the City can require as part of the Construction Traffic Management Plan that the applicant meet with other applicants and the City to address construction traffic, deliveries, and worker parking.

Significance After Mitigation: Less than significant



Appendix A: Related Project List

Attachment C: Related Project List for Project Study Area

| No | Street | City | Existing Use | Proposed Use | ITE Code | Size | Unit | Daily | AM In | AM Out | AM Total | PM In | PM Out | PM Total |
|----|-------------------------------|---------------------|---|---|--|------|------------|-------|----------|--------|----------|-------|----------|----------|
| | y Hills Related Projects | | | | | | | | | | | | | |
| 1 | 100 N. Crescent Dr. | Beverly Hills CA | 2,550 SF Screening Room, 103,535 SF | Commercial Office: 4,330 SF of restaurant, 2,489 SF of screening room, | Office (N/A) | 51 | KSF | | 45 | 4 | 48 | 17 | 61 | 79 |
| | | G. t | Commercial Office | 154,336 SF of office; 465 parking spaces | 932 | 4 | KSF | | 26 | 21 | 47 | 26 | 17 | 43 |
| | | | - | | | ' | Total | | 71 | 25 | 96 | 43 | 78 | 121 |
| 2 | 250 N. Crescent Dr. | Beverly Hills CA | Vacant Lot | Multi-Family Residential: 7 Condo Units, 1 Affordable Rental Unit, 12,400 SF residential uses; 14 parking spaces | 230 | 8 | DU | | 1 | 3 | 4 | 3 | 1 | 4 |
| 3 | 154-168 N. La Peer Dr. | Beverly Hills CA | Multi-Family Residential (3 buildings) - 6 units | Multi-Family Residential: 16 Condo Units, 39,084 SF residential uses; 59 parking spaces | 230 | 16 | DU | | 5 | 2 | 7 | 6 | 2 | 8 |
| 4 | 140 S. Lasky Drive | Beverly Hills | _ | 4-story hotel - 36,760-SF with 66 rooms, | 310 | 22 | Rooms | | 9 | 7 | 16 | 8 | 8 | 16 |
| | · | CA | SF, 44 rooms (Occ.) | 1,845 SF restaurant (898 SF indoor, and 947 SF outdoor), and rooftop uses (roof deck and pool deck), and 3 levels of subterranean parking with 94 spaces. | 931 | 2 | TSF | | 7 | 2 | 9 | 10 | 6 | 16 |
| | | | | | | | Total | | 16 | 9 | 25 | 18 | 14 | 32 |
| 5 | 457 N. Oakhurst Dr. | Beverly Hills CA | 2-story, 2-unit | 6-unit, 5-story condominium building | 221 (Mid-rise) | 6 | unit | | 1 | 2 | 3 | 2 | 1 | 3 |
| | | CA | building (vacant) | | | | | | 0 | 0 | 0 | 0 | 0 | 0 |
| | | | | | | | Total | | 1 | 2 | 3 | 2 | 1 | 3 |
| 6 | 9212 Olympic Blvd. | | | Commercial Office with | 710 | 13 | TSF | | 18 | 2 | 20 | 4 | 16 | 20 |
| | | CA | associated with adjacent Auto Dealer | Retail/Restaurant: 6,900 SF of Retail/Restaurant (with a max. of 1,000 SF | 933 | 1 | TSF | | 35 | 28 | 63 | 27 | 25 | 52 |
| | | | (not a part) | of bar and dining area), 13,344 SF of Commercial Office; 58 parking spaces | 814 | 5 | TSF | | 15 | 17 | 32 | 14 | 10 | 24 |
| | | | ' | | | | Total | | 68 | 47 | 115 | 45 | 51 | 96 |
| 7 | 9120 Olympic Blvd. | Beverly Hills CA | 54,262 SF (educational facility) (occ.) | Total new floor area: 80,719 SF (net increase of 26,457 SF) | 534 (Private K-8) | 26 | TSF | | 169 | 138 | 307 | 85 | 88 | 173 |
| 8 | 9230 Olympic Blvd | Beverly Hills | 1 ' ' | 18,163 SF Commercial: 1,359 SF | 931 (Quality Restaurant) | 1 | TSF | | 5 | 2 | 7 | 7 | 5 | 12 |
| | | CA | Commercial (Office) | Restaurant and 16,804 SF of Office | 710 (Gen. Office Bldg.) | 17 | TSF | | 21 | 5 | 26 | 7 | 19 | 26 |
| | | | ' | | | | Total | | 26 | 7 | 33 | 14 | 24 | 38 |
| 9 | 425 N. Palm Dr. | Beverly Hills CA | Multi-Family Residential (3 buildings) - 18 Units | Multi-Family Residential: 20 Multi-Family Residential Units - Approx. 64,000 Total; 62 parking spaces | 230 | 20 | DU | | 2 | 7 | 9 | 7 | 4 | 11 |
| 10 | 340 S. Rexford | Beverly Hills | Vacant Lot | 3-Unit Condominium Building | 232 | 3 | DU | | 6 | 25 | 31 | 11 | 7 | 18 |
| 11 | 370 N. Rodeo Dr. | CA Beverly Hills | 9,587 SF Commercial | Commercial (Retail): 15,250 SF of Retail | 014 | | 1465 | | 10 | 24 | 40 | 1.0 | 42 | |
| | | CA | (Retail) | Use (net increase of 5,663 SF) | 814 | 6 | KSF | | 19 | 21 | 40 | 16 | 13 | 29 |
| 12 | 400-408 N. Rodeo Dr. | Beverly Hills CA | 28,128 SF Commercial (Retail) (12,864 SF at 400 Rodeo and 15,264 SF at 408 Rodeo) | 29,767 SF Commercial (Retail) | 876 (Apparel Store) | 2 | TSF | | 5 | 4 | 9 | 4 | 4 | 8 |
| | 9220 N. Santa Monica Blvd. | Beverly Hills CA | Vacant | 11 Office buildings totaling 114,202 SF, and an underground parking garage with 230,559 SF and 476 parking spaces | 714 (Corporate Headquarters Building) | 114 | TSF | | 190 | 6 | 196 | 40 | 171 | 211 |
| | 9900-9908 S. Santa | | | Mixed-Use Multi-Family and Commercial: | 230 | 27 | DU | | 4 | 8 | 12 | 10 | 4 | 14 |
| | Monica Blvd. | CA | Club) | 13,036 SF of Commercial, 25 Condo Units | 814 | 14 | KSF | | 45 | 49 | 94 | 39 | 30 | 69 |
| | | | | | | | Total | | 49 | 57 | 106 | 49 | 34 | 83 |
| 15 | 8600 Wilshire Blvd. | , | | Mixed-Use Multi-family and Commercial: | 230 | 21 | DU | | 1 | 8 | 9 | 7 | 4 | 11 |
| | | CA | Commercial Building | 6,355 SF Retail; 18 Units; 3,412 SF Public Use; 82 parking spaces* | 820E | 5 | TSF | | 15 | 10 | 25 | 41 | 44 | 84 |
| | | | | | 820R | 3 | TSF | | -2 | -1 | -3 | -5 | -5 | -9 |
| | | | | | | | Total | | 14 | 17 | 31 | 43 | 43 | 86 |
| 16 | 8633 Wilshire | Beverly Hills CA | Commercial building (restaurant) | 25,565 SF Commercial Office; 76 parking spaces | 710 (Gen. Office Bldg.) | 26 | TSF | | 32 | 6 | 38 | 8 | 32 | 40 |
| 17 | 9000 Wilshire Blvd. | Beverly Hills | | Commercial Office: 31,702 SF Commercial Office; 91 parking spaces | 710 | 32 | TSF | | 13 | 2 | 15 | 3 | 12 | 15 |
| 18 | 9111 Wilshire Blvd. | Beverly Hills | _ | No change to floor area. Change in use | Office Building (710) | 112 | TSF | | 146 | 20 | 166 | 29 | 131 | 160 |
| | | CA | | from Office Building (710) to Hotel (310) | Hotel | 154 | Room | | 45 | 39 | 84 | 55 | 40 | 95 |
| | | | | | | | Total | | 191 | 59 | 250 | 84 | 171 | 255 |
| 19 | 9145 Wilshire Blvd. | Beverly Hills CA | (Bank/Office - now vacant); 15 parking | 8,269 SF religious institution; 16 parking spaces | 560 | 8 | TSF | | 3 | 3 | 6 | 5 | 3 | 8 |
| 20 | 9200 Wilshire Blvd. | Beverly Hills | spaces Vacant Lot | Mixed-Use Multi-family and Commercial: | 230 | 53 | DU | | 4 | 20 | 23 | 19 | 9 | 28 |
| | | CA | | 54 Multi-Family Residential Units, 14,000 | 820E | 8 | TSF | | 22 | 14 | 35 | 59 | 63 | 122 |
| | | | | SF Commercial; 321 parking spaces | 931 | 6 | TSF | | 2 | 2 | 5 | 28 | 14 | 42 |
| | | | | | | | Total | | 28 | 36 | 64 | 106 | 86 | 192 |
| 21 | 9596 Wilshire Blvd. | | Surface Parking Lot | 48,374 SF Commercial building | 874 | 48 | KSF | | 53 | 51 | 104 | 61 | 75 | 136 |
| 22 | 9900 Wilshire Blvd. | CA Beverly Hills | Vacant (Former | Mixed-Use (Condominium and | | | | | | | | | | |
| | 5500 Wilstine DIVU. | CA CA | | Commercial): 193 Condo Units with 134 | 310 | 134 | Rooms | | 47 | 38 | 85 | 56 | 43 | 99 |
| | | | | Rooms, 16,057 SF of Restaurant/Retail, | 232 | 193 | DU | | 13 | 52 | 65 | 45 | 28 | 73 |
| | | | | 7,942 SF of Ballrooms/Conference Rooms, 18,826 SF of Ancillary Uses, 1,140 | 820R-1 932-1 | 18 | TSF TSF | | 11 65 | 7 | 18 79 | 33 | 36 48 | 128 |
| | | | | narking snaces | 322-1 | 14 | | | | | | 214 | | 128 |
| | | | | | | | Total | | 136 | 111 | 247 | 214 | 155 | 369 |

Attachment C: Related Project List for Project Study Area

| 20 20 20 20 20 20 20 20 | No | Street | City | Existing Use | Proposed Use | ITE Code | Size | Unit | Daily | AM In | AM Out | AM Total | PM In | PM Out | PM Total |
|--|--------|-----------------------------|-------------------|--|--|--------------------------|--------|-------------|-------|-------|--------|----------|-------|--------|----------|
| March 1980 | | | | 1 | | | | | | | | | | | |
| 100 | 23 | | | | | 310 | | | | | | | | | 27 |
| Companies Comp | | _ | | | | | | | | | | | | | 57 |
| MISS NINK PETALON Petal-His List 19 Scote Petal-His List 19 Scot | | | | | 15 | | | | | | | | | | 37 |
| Mathematical Content | | | | | Phase II [.] | 820 | 5 | | | _ | | | _ | | 209 |
| Michael Series Mich | 24 | 9850, 9876, 9900 and | Beverly Hills | 3,521 SF Service | Demolish 3,521 SF of service station and | | | Total | | 42 | 03 | 103 | 120 | 09 | 209 |
| Part | | 9988 Wilshire Boulevard. | CA | Station (9988 Wilshire); Vacant (9900 Wilshire); 786 hotel room Beverly Hilton Hotel (9876 Wilshire) and 170 hotel room Waldorf Astoria Beverly Hills Hotel (9850 Wilshire) – combined existing Hilton/WABH floor area of 724,649 SF. | 166,834 SF of Beverly Hilton floor area (including demolition of 217 existing hotel rooms). Add: new 162 residential unit, 499,806 SF residential building; new 141 residential unit, 424,266 SF residential building; New 213,966 SF 37 residential building; New 213,966 SF 37 residential unit, 42 hotel room hotel/residential building; new 127,324 SF structure containing amenities and support areas, including 30 accessory spaces that could be used for staff housing; replacement 37,562 SF Beverly Hilton Conference Center; new re[placement 72,697 SF Beverly Hilton addition containing restaurant, retail, 36 | NA | NA | NA | | 11 | 47 | 58 | 68 | 20 | 88 |
| Part | | | | | Mixed Use | Condominiums | 103 | Total Units | 1224 | | | 99 | | | 111 |
| Part | | and starts | _ | | | | | | | | | | | | 182 |
| Part | | | | | | | | | | | | | | | 229 |
| Part | | | | | | | | | | | | | | | 72 |
| Part | | | | | | | | | | | | | | | 76 |
| Part | | | | | | | | | | | | | | | 67 |
| Part | | | | | | | | | | | | | | | 631 |
| Part | | | | | | | | | | | | | | | -552 |
| March Marc | | | | | | | | | | | | | | | -128 |
| March Marc | | | | | | | | | | | | | | | -140 |
| Median CA Median Stage Content Con | | | | | | | | | | 21 | 20 | | 274 | 274 | 548 |
| Part | 26 | 10250 W Santa Monica | Los Angeles | Century City | Add 71,700 SF and renovate shopping | Retail | 71700 | SF | 1350 | | | 26 | | | 140 |
| 1959 S Ave of the Stars Los Angless Century City Century Milhard User Residential Office, Retail and Milhard User Retail Office, Retail of Retail of Retail Office, Retail Office, Retail of Retail Office, Retail of Retail Office, Retail of Retail Office, Retail of | | Blvd | CA | | center (total 831,891 SF) | Retail | 1308 | SF | | | | | | | 4 |
| CA Mobility Hub | | | | Center | | | | Total | 1350 | 16 | 10 | 26 | 69 | 75 | 144 |
| Main | 27 | 1950 S Ave of the Stars | _ | Century City Center | · · · · | Office | 725830 | SF | 4603 | 604 | 83 | 687 | 103 | 501 | 604 |
| 29 1036 W Santa Monica Lox Angeles 26 Apt 10 91 Apt or 116 Apt 30 30 30 30 30 30 30 3 | 28 | 888 S Devon Ave | Los Angeles | | Apartment building: 5 stories over 2 | Apartments | 32 | DU | 213 | 3 | 13 | 16 | 10 | 6 | 16 |
| Mode | | Blvd | CA | | 1 1 1 | Apartments | 116 | DU | 598 | 15 | 31 | 46 | 25 | 21 | 46 |
| | 30 | | _ | | , , | Apartments | 121 | DU | | 10 | 43 | 53 | 32 | 18 | 50 |
| 1 | West I | - | | 020) | parking(1-street & 2-basement) | | | | | | | | | | |
| Retail R | | | | | | | 30 | DII | 200 | 2 | 12 | 15 | 12 | 7 | 19 |
| Trip September Trip September Trip September Septemb | | | , , | | | | | | | | | | | | |
| Building (Office) 3 | | | CA | | | | | | | | | | | | 18 |
| Total 450 9 15 24 22 20 | | | | | | | 3 | KSF | 38 | 4 | 1 | 5 | 1 | 4 | 5 |
| Second Property Restaurant Second Propert | | | | | | Gallery | 1 | KSF | 1 | 0 | 0 | 0 | 0 | 0 | 0 |
| Hollywood CA | | | | | | | | | 450 | 9 | 15 | 24 | | 20 | 42 |
| September CA September | 32 | 8816 Beverly | | | | 931 - Quality Restaurant | | | | | 0 | 0 | | | 153 |
| Part | | | | | | | 25 | | | 3 | 1 | 4 | 2 | 5 | 7 |
| Total Final Property Final Property | | | | | | | | | | - | | | | | 260 |
| Development Pour | | | | | | - | 1 | KSF | 69 | 2 | 1 | 3 | 5 | 2 | 7 |
| No. No. | | | | | | | 9 | KSF | 82 | 3 | 1 | 4 | 2 | 1 | 3 |
| Hollywood CA | | | | | | ., | | Total | 4354 | 167 | 42 | 209 | 178 | 241 | 419 |
| Hollywood CA | 33 | 8899 Beverly | | | | | 12 | DU | 80 | 1 | 5 | 6 | 5 | 2 | 7 |
| 230 - Condominiums 13 DU 76 1 5 6 5 2 | | | | | | | | | | | | | | | 29 |
| 826 - Specialty Retail 20 KSF 881 0 0 0 24 30 931 - Quality Restaurant 4 KSF 395 0 0 0 0 22 11 710 - General Office Building (Office) 11 KSF 116 14 2 16 3 13 120 Larrabee West Hollywood CA | | | | | | | | | | | | | | | 7 |
| Part | | | | | | | | | | · · | | | | | 54 |
| T10 - General Office 11 KSF 116 14 2 16 3 13 | | | | | | | | | | | | | | | 33 |
| Second S | | | | | | 710 - General Office | | | | | | | | | 16 |
| 34 1120 Larrabee West Hollywood CA 220 - Multifamily Housing (Low-Rise) (Residential) 22 DU 161 2 8 10 8 4 Shapping Centers | | | | | | Building (Office) | 11 | | | | | | | | |
| Hollywood CA Hollywood CA 417 Robertson West Hollywood CA West B20 - Multifamily Housing (Low-Rise) (Residential) 22 DU 161 2 8 10 8 4 B20 - Shopping Center (Low-Rise) (Residential) | 2.4 | 1120 Larrahoo | West | | | | | Total | -129 | -69 | 21 | -48 | 17 | -54 | -37 |
| | 34 | 1120 Lattablee | Hollywood | | | | 22 | DU | 161 | 2 | 8 | 10 | 8 | 4 | 12 |
| Hollywood | 35 | 417 Robertson | West Hollywood | | | | 8 | KSF | 283 | 4 | 3 | 7 | 14 | 15 | 29 |

Attachment C: Related Project List for Project Study Area

| No | Street | City | Existing Use | Proposed Use | ITE Code | Size | Unit | Daily | AM In | AM Out | AM Total | PM In | PM Out | PM Total |
|-----|--------------------------|-------------------|--------------|---|--|----------|------------------|---------------|------------|-----------|-------------|------------|-------------|-------------|
| 36 | 645 Robertson | West | | | 826 - Specialty Retail | 18 | KSF | 803 | 14 | 10 | 24 | 22 | 27 | 49 |
| | | Hollywood CA | | | 931 - Quality Restaurant | 33 | KSF | 2995 | 22 | 5 | 27 | 167 | 82 | 249 |
| | | G. t | | | 310 - Hotel (Lodging) | 241 | RMS | 1969 | 75 | 53 | 128 | 74 | 71 | 145 |
| | | | | 890 - Design Showroom | 10 | KSF | 52 | 1 | 1 | 2 | 2 | 2 | 4 | |
| | | | | | 925 - Drinking Place (Services) | 4 | KSF | 515 | 0 | 0 | 0 | 28 | 15 | 43 |
| | | | - | | (00111000) | | Total | 3351 | 94 | 54 | 148 | 134 | 104 | 238 |
| 37 | 9001 Santa Monica | West | | | 820 - Shopping Center | 10 | KSF | 370 | 6 | 3 | 9 | 18 | 19 | 37 |
| | | Hollywood CA | | | (Retail) 932 - High-Turnover (Sit- | | | | | | | | | |
| | | | | | Down) Restaurant (Services) | 10 | KSF | 1099 | 53 | 44 | 97 | 60 | 36 | 96 |
| | | | | | (Services) | | Total | 1469 | 59 | 47 | 106 | 78 | 55 | 133 |
| 38A | 9040 Santa Monica | West | | Project 38A reflects the approved | 220 - Multifamily Housing | 76 | DU | 505 | 8 | 31 | 39 | 31 | 16 | 47 |
| | | Hollywood CA | | Melrose Triangle project site in West Hollywood. | (Low-Rise) (Residential) Specialty Retail | 45 | KSF | 1999 | 36 | 24 | 60 | 54 | 68 | 122 |
| | | | | , | 710 - General Office | 137 | KSF | | 212 | | | 39 | | |
| | | | | | Building (Office) | | | 1701 | | 29 | 241 | | 193 | 232 |
| | | | | | 890 - Furniture Store | 16 12 | KSF | 727 62 | 13 | 9 | 22 | 20 3 | 25 | 45 6 |
| | | | | | 931 - Quality Restaurant | 8 | KSF | 738 | 5 | 1 | 6 | 41 | 20 | 61 |
| | | | | | Existing Land Use | 0 | KSI | -2154 | -83 | -28 | -111 | -64 | -146 | -210 |
| | | | | | Existing Land 030 | | Total | 3578 | 192 | 67 | 259 | 124 | 179 | 303 |
| 38B | 9040 Santa Monica | West | | Project 38B reflects the current land use | 220 - Multifamily Housing | 41 | DU | 300 | 6 | 17 | 23 | 16 | 11 | 27 |
| | | Hollywood CA | | proposal for the Melrose Triangle site. Since the proposed land use generated | (Low-Rise) (Residential) | | KSF | | | | | | | |
| | | CA | | more vehicle-trips, Project 38B was | Specialty Retail 710 - General Office | 45 | | 1999 | 36 | 24 | 60 | 54 | 68 | 122 |
| | | | | applied to the cumulative conditions analysis. | Building (Office) | 245 | KSF | 2386 | 317 | 43 | 360 | 63 | 285 | 348 |
| | | | | unalysis. | 890 - Furniture Store | 12 | KSF | 62 | 1 | 1 | 2 | 3 | 3 | 6 |
| | | | | | 931 - Quality Restaurant | 8 | KSF | 738 | 5 | 1 | 6 | 41 | 20 | 61 |
| | | | | | Existing Land Use | | Total | -2154 3331 | -83 282 | -28 58 | -111 340 | -64 113 | -146 241 | -210 354 |
| 39 | 8920 Sunset | West | | | Specialty Retail | 10 | KSF | 457 | 7 | 5 | 12 | 12 | 16 | 28 |
| | | Hollywood | | | 932 - High-Turnover (Sit- | 10 | KSI | 437 | , | 3 | 12 | 12 | 10 | |
| | | CA | | | Down) Restaurant (Services) | 2 | KSF | 224 | 10 | 9 | 19 | 10 | 7 | 17 |
| | | | | | 710 - General Office Building (Office) | 46 | KSF | 506 | 63 | 9 | 72 | 12 | 56 | 68 |
| | | | | | 580 - Museum | 2 | KSF | 0 | 1 | 0 | 1 | 0 | 0 | 0 |
| | | | | | (Institutional) | | | | | | | | | |
| | | | | | Arts Club | 7 | MEMBERS Total | 1771 1961 | 55 103 | 15 19 | 70 122 | 69 68 | 56 91 | 125 159 |
| 40 | 8850 Sunset | West | | | 220 - Multifamily Housing | 41 | DU | 300 | | | | | | |
| | | Hollywood CA | | | (Residential) 932 - High-Turnover (Sit- | 41 | DU | 300 | 6 | 17 | 23 | 16 | 11 | 27 |
| | | CA | | | Down) Restaurant (Services) | 29 | KSF | 3231 | 230 | 174 | 404 | 260 | 241 | 501 |
| | | | | | 310 - Hotel (Lodging) | 115 | RMS | 961 | 33 | 29 | 62 | 41 | 29 | 70 |
| | | | | | 925 - Night Club (Drinking | 5 | KSF | 645 | 0 | 0 | 0 | 35 | 18 | 53 |
| | | | | | Place) | | Total | 5137 | 269 | 220 | 489 | 352 | 299 | 651 |
| 41 | 9034 Sunset | West | | | 220 - Multifamily Housing | 10 | | | | | | | | |
| | | Hollywood CA | | | (High-Rise) (Residential) 932 - High-Turnover (Sit- | 10 | DU | 45 | 1 | 2 | 3 | 2 | 2 | 4 |
| | | | | | Down) Restaurant (Services) | 11 | KSF | 921 | 4 | 4 | 8 | 57 | 27 | 84 |
| | | | | | 310 - Hotel (Lodging) | 237 | RMS | 1981 | 65 | 46 | 111 | 72 | 70 | 142 |
| | | | - | | , 5 5 | | Total | 2199 | 70 | 52 | 122 | 129 | 96 | 225 |
| 42 | 910 Wetherly | West | | | 220 - Multifamily Housing | | | | | | | | | |
| | | Hollywood CA | | | (Residential) | 93 | DU | 681 | 15 | 37 | 52 | 36 | 26 | 62 |
| 43 | 8650 Melrose | West Hollywood | | | 220 - Multifamily Housing (Residential) | 7 | DU | 51 | 1 | 3 | 4 | 3 | 2 | 5 |
| | | CA | | | 814 - Retail | 15 | KSF | 925 | 33 | 33 | 66 | 54 | 54 | 108 |
| | | | | | | | Total | 976 | 34 | 36 | 70 | 57 | 56 | 113 |
| 44 | 923 Palm | West Hollywood | | | 220 - Multifamily Housing | 49 | DU | 359 | 7 | 20 | 27 | 19 | 14 | 33 |
| 45 | 8555 Santa Monica | CA West | | | (Residential) 220 - Multifamily Housing | | | | | | | | | |
| 40 | מאווא ווואס הכנט Nionica | West Hollywood | | | (Residential) | 123 | DU | 900 | 19 | 50 | 69 | 48 | 34 | 82 |
| | | CA | | | 814 - Retail | 15 | KSF | 925 | 33 | 33 | 66 | 54 | 54 | 108 |
| | | | | | 932 - High-Turnover (Sit- Down) Restaurant | 4 | KSF | 438 | 31 | 24 | 55 | 35 | 33 | 68 |
| | | | | | (Services) | | | .50 | | | | | 33 | |
| | | | | | 710 - General Office Building (Office) | 7 | KSF | 65 | 9 | 1 | 10 | 2 | 8 | 10 |
| | | | | | 918 - Personal Services | 4 | KSF | NA | 3 | 1 | 4 | 3 | 4 | 7 |
| | | | | | | | Total | 2328 | 95 | 109 | 204 | 142 | 133 | 275 |
| 46 | 8430 Sunset | West Hollywood | | | 220 - Multifamily Housing (Residential) | 125 | DU | 915 | 20 | 50 | 70 | 49 | 35 | 84 |
| | | CA | | | (Residential) 850 - Retail | 35 | KSF | 3737 | 121 | 112 | 233 | 138 | 128 | 266 |
| | | | | | | | Total | 4652 | 141 | 162 | 303 | 187 | 163 | 350 |
| 47 | 8497 Sunset | West | | | 932 - High-Turnover (Sit- | | | | | | | | | |
| | | Hollywood CA | | | Down) Restaurant (Services) | 10 | KSF | 1096 | 78 | 59 | 137 | 88 | 82 | 170 |
| | | | | | 710 - General Office | 12 | KSF | 112 | 15 | 2 | 17 | 3 | 13 | 16 |
| | | | | | Building (Office) | | Total | | | | | | 95 | |
| | | | | | | | rotal | 1208 | 93 | 61 | 154 | 91 | 95 | 186 |

Appendix B: Detailed Trip Generation Rates

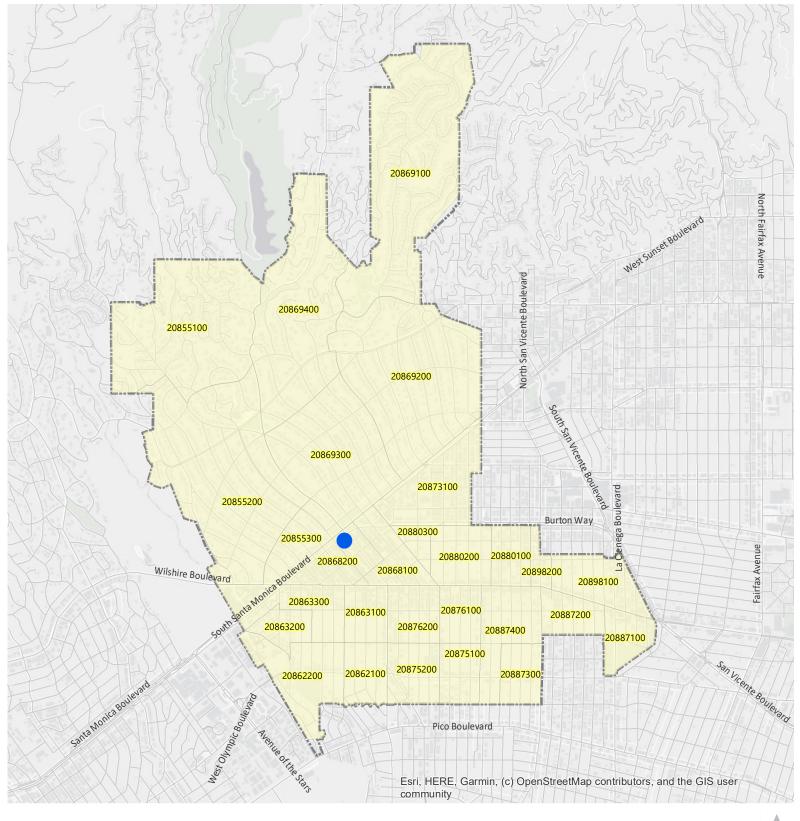
ATTACHMENT A CHEVAL BLANC HOTEL, CLUB & MIXED USE PROJECT PROPOSED PROJECT TRIP GENERATION ESTIMATES

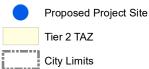
| | | | | | Trip (| Senerati | on Estin | nates | | | | | | | | | |
|--|------|-----------------------------|-----------|---------|--------|----------|-----------|----------|----------|--|---------------------|-----------------|--------------|------------------|------------|-------------------|----------------|
| | | | | | Tr | ip Gene | ration Ra | ites [a] | | | | Estima | ated Ti | ip Ger | eratio | n | |
| Land Use | ITE# | Size | Daily | AM | Peak F | lour | PN | 1 Peak H | our | Trip Rate | Weekday | AM | Peak | Hour | PM | Peak I | lour |
| Land Ose | IIE# | Size | Rate | Rate | % In | % Out | Rate | % In | % Out | Unit | Daily | In | Out | Total | ln | Out | Total |
| | | | | | | | | | | | | | | | | | |
| Proposed Project | | | | | | | | | | | | | | | | | |
| Hotel | 310 | 115 rooms | 8.36 | 0.47 | 59% | 41% | 0.60 | 51% | 49% | per room | 961 | 32 | 22 | 54 | 35 | 34 | 69 |
| TNC [e] | | | | | | | | | | | 640 | 21 | 15 | 36 | 23 | 23 | 46 |
| Employee | | | | | | | | | | | 125 | 4 | 3 | 7 | 5 | 4 | 9 |
| Valet | | | | | | | | | | | 196 | 7 | 4 | 11 | 7 | 7 | 14 |
| Total check | | | | | | | | | | | 961 | 32 | 22 | 54 | 35 | 34 | 69 |
| Private Membership Club | [c] | 500 members | 0.36 | 0.04 | 80% | 20% | 0.08 | 80% | 20% | member | 180 | 16 | 4 | 20 | 32 | 8 | 40 |
| TNC [e] | | | | | | | | | | | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Employee | | | | | | | | | | | 23 | 2 | 1 | 3 | 4 | 1 | 5 |
| Valet | | | | | | | | | | | 157 | 14 | 3 | 17 | 28 | 7 | 35 |
| Total check | | | | | | | | | | | 180 | 16 | 4 | 20 | 32 | 8 | 40 |
| Quality Restaurant | 931 | 25.094 ksf | 83.84 | 0.73 | 50% | 50% | 7.8 | 67% | 33% | per ksf | 2,104 | 9 | 9 | 18 | 131 | 65 | 196 |
| Less Internal Capture [b] | 331 | 23.034 K31 | 20% | 20% | 20% | 20% | 0% | 20% | 20% | per ksi | (421) | (2) | (2) | (4) | (26) | (13) | (39) |
| New Trips | | | 2070 | 2070 | 2070 | 2070 | 0,0 | 2070 | 2070 | | 1,683 | 7 | 7 | 14 | 105 | 52 | 157 |
| TNC [e] | | | | | | | | | | | 842 | 4 | 4 | 8 | 52 | 26 | 78 |
| Employee | | | | | | | | | | | 252 | 1 | 1 | 2 | 16 | 8 | 24 |
| Valet | | | | | | | | | | | 589 | 2 | 2 | 4 | 37 | 18 | 55 |
| Total check | | | | | | | | | | | 1,683 | 7 | 7 | 14 | 105 | 52 | 157 |
| | | | | | | | | | | | | | | | | | |
| Retail | 820 | 24.976 ksf | 37.75 | 0.94 | 62% | 38% | 3.81 | 48% | 52% | per ksf | 943 | 14 | 9 | 23 | 46 | 49 | 95 |
| Less Internal Capture [b] | | | 20% | 20% | 20% | | | 20% | 20% | | (189) | (3) | (2) | (5) | (9) | | (19) |
| Less Pass-By | | | 30% | 30% | 30% | 30% | 30% | 30% | 30% | | <i>(226)</i> 528 | <i>(3)</i> 8 | <i>(2)</i> 5 | <i>(5)</i> 13 | (11) 26 | <i>(12)</i> 27 | <i>(23)</i> 53 |
| New Trips TNC [e] | | | | | | | | | | | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Employee | | | | | | | | | | | 100 | 2 | 1 | 2 | 5 | 5 | 10 |
| Valet | | | | | | | | | | | 428 | 6 | 4 | 11 | 21 | 22 | 43 |
| Total check | | | | | | | | | | | 528 | 8 | 5 | 13 | 26 | 27 | 53 |
| | | | | | | | | | | | | | | | | | |
| Day Spa [d] | 918 | 12.936 ksf | 14.50 | 1.21 | 50% | 50% | 1.45 | 17% | 83% | per ksf | 188 | 8 | 8 | 16 | 3 | 16 | 19 |
| Less Internal Capture [b] | | | 20% | 20% | 20% | 20% | 0% | 20% | 20% | | <i>(37)</i> | (1) | (2) | (3) | (1) | (3) | (4) |
| New Trips | | | | | | | | | | | 151 | 7 | 6 | 13 | 2 | 13 | 15 |
| TNC [e] | | | | | | | | | | | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Employee | | | | | | | | | | | 20 | 1 | 1 | 2 | 0 | 2 | 2 |
| Valet | | | | | | | | | | | 131 | 6 | 5 | 11 | 2 | 11 | 13 |
| Total check | | | | | | | | | | | 151 | 7 | 6 | 13 | 2 | 13 | 15 |
| | 7 | <u> </u> ΓΟΤΑL ESTIMATED | PROJEC | T TRIPS | (NEW | TRIPS) | <u> </u> | | <u> </u> | <u> </u> | 3,503 | 70 | 44 | 114 | 200 | 134 | 334 |
| TOTAL ESTIMATED PROJECT TRIPS (EMPLOYEE TRIPS) | | | | | | | 521 | 10 | 6 | 16 | 30 | 20 | 50 | | | | |
| TOTAL ESTIMATED PROJECT TRIPS (VALET) | | | | | | | | 1,501 | 35 | 19 | 54 | 95 | 65 | 160 | | | |
| | | L ESTIMATED PROJ | | | | | - | | | | 1,482 | 25 | 19 | 44 | 75 | 49 | 124 |
| | TOT | TAL ESTIMATED PRO | | | JSTED | TNC TRII | PS) | | | | 1,482 | 25 | 25 | 50 | 75 | 75 | 150 |
| | | | VE USES | | TDIDO | 1 | | | | | -1,142 | -18 | -10 | -28 | -55 | -60 | -115 |
| | | TOTAL ADJ | US I ED P | KUJECT | IKIPS | 1 | | | | | 2,361 | 52 | 40 | 92 | 145 | 100 | 245 |

Notes:

- [a] Source: ITE Trip Generation Manual, 10th Edition, 2017, except where noted.
- [b] Internal capture represents the percentage of trips between land uses that occur within the site without requiring a vehicle trip. Internal capture rates are derived from "Parking Demand Analysis Study Cheval Blanc Hotel in the City of Beverly Hills, CA", Kimley Horn (2020).
- [c] Private membeship member trip rates derived from "Parking Demand Analysis Study Cheval Blanc Hotel in the City of Beverly Hills, CA", Kimley Horn (2020).
- [d] No daily trip rate is provided by ITE for Land Use 918 Hair Salon. Daily rate assumes that the PM peak hour trip rate is equal to 10% of the daily trip rate.
- [e] The proliferation of shared mobility transportation network companies (TNCs), such as Lyft and Uber, in recent years is important to consider in a project of this type and size. Pick-up and drop-off trips, such as those utilizing TNC services, do not utilize site parking and result in an additional trip generated compared to patrons who drive themselves and park their own cars at the site. In order to account for TNCs, it was assumed that TNCs would account for 50% of the vehicle trips generated by the restaurant, and 66.6% of the vehicle trips generated by the hotel, based on observed drive ratios provided in the Parking Demand Analysis Study technical memorandum (July 16, 2020). Where inbound and outbound trips were unequal, the higher of the two calculations was assumed for both directions to account for TNCs that drop off a patron and leave the project site without

Appendix C: SCAG Model Data for VMT Analysis





SCAG Regional Average calculated using SCAG model

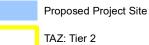




Appendix C-1

SCAG Tier 2 Traffic Analysis Zones in Beverly Hills







Appendix C-2

Appendix H.2



Local Transportation Assessment

Cheval Blanc Beverly Hills Specific Plan

Local Transportation Assessment

Prepared for:

Eyestone Environmental

September 2021

LA20-3243

FEHR PEERS

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1. Study Overview

This local transportation assessment presents the results of the traffic operations analysis conducted by Fehr & Peers for the proposed Cheval Blanc Beverly Hills Specific Plan and other requested approvals as set forth in the Draft Environmental Impact Report as section 27, "Required Approvals" (herein collectively referred to as the "proposed Project" or the "Project") in the City of Beverly Hills. The purpose of this study is to identify traffic operations in the Project vicinity with the development of the proposed Project. This chapter outlines the purpose of the study, the geographic scope of the local transportation assessment, and the study scenarios. This study relies on data contained in the Cheval Blanc Beverly Hills Specific Plan Transportation Impact Report (Fehr & Peers, September 2021) that was prepared as part of the Environmental Impact Report for the proposed Project.

1.1 Study Purpose

The purpose of this study is to analyze traffic operations with the new land uses that would occur with the development of the Project. In October 2019, the City of Beverly Hills Planning Commission adopted new transportation impact thresholds and guidelines to adhere to CEQA requirements pertaining to Senate Bill 743 (SB 743). The primary purpose of SB 743 was eliminating level of service (LOS) as a measure of vehicular capacity and traffic congestion as a basis for determining significant transportation impacts under CEQA. Rather, SB 743 required lead agencies to shift the focus from evaluating traffic impacts based on metrics that only consider vehicle travel time and delay (i.e., impacts to drivers) to a new metric that captures the state's goals of improved air quality, reduced greenhouse gas emissions, and improved public health (i.e., impacts of driving) known as vehicle miles travelled (VMT).

While LOS no longer constitutes a CEQA impact, it can still be used to inform decision makers on the overall effects of a project. Therefore, the City developed Local Transportation Assessment Guidelines at the time it adopted its new transportation thresholds in October 2019. The traffic operations analysis completed for this Local Transportation Assessment is based on the City's guidelines.

1.2 Project Study Area

The Project is located in the heart of the City of Beverly Hills. As shown in **Figure 1**, the Project site is bordered by South Santa Monica Boulevard on the north, North Beverly Drive on the east, North Rodeo Drive on the west, and existing developments on the south. The Project study area is generally bounded by North Santa Monica Boulevard to the north, North Cañon Drive to the east, Rodeo Drive to the west, and Brighton Way to the south. **Figure 1** displays the study area and the locations of the following study intersections:

- 1. North Rodeo Drive/North Santa Monica Boulevard (S)*
- 2. North Beverly Drive/North Santa Monica Boulevard (S)

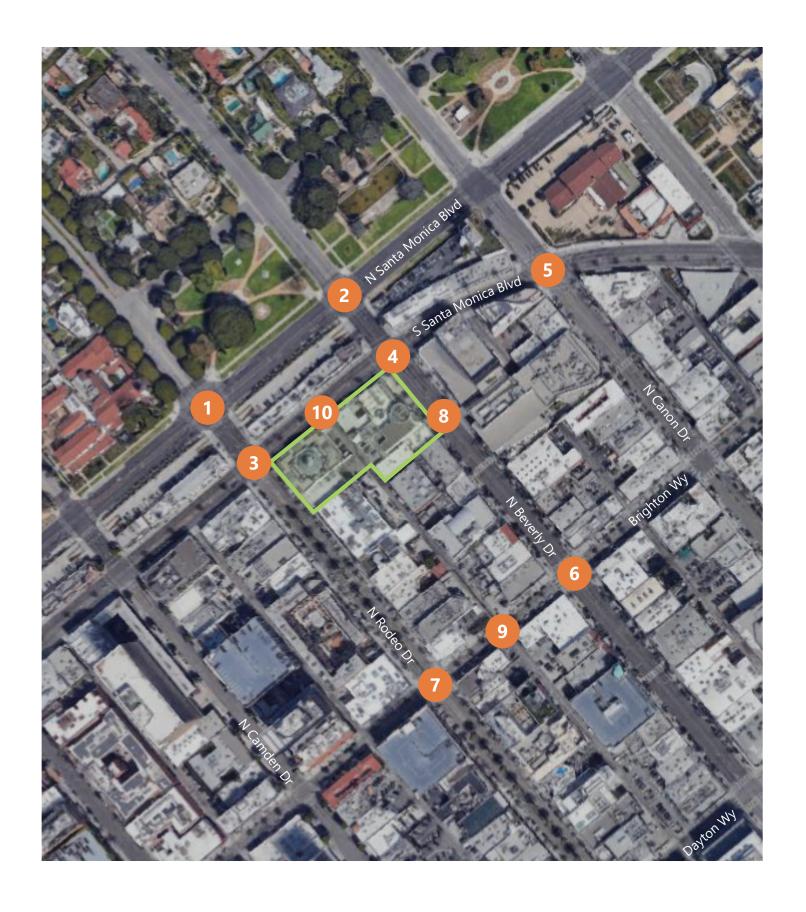




Figure 1 **Project Location and Study Intersections**

- 3. North Rodeo Drive/South Santa Monica Boulevard (S)
- 4. North Beverly Drive/South Santa Monica Boulevard (S)
- 5. North Cañon Drive/South Santa Monica Boulevard (S)
- 6. North Beverly Drive/Brighton Way (S)
- 7. North Rodeo Drive/Brighton Way (S)
- 8. North Beverly Drive/Realigned Alley (future intersection) (SSSC)**
- 9. Alley/Brighton Way (SSSC)
- 10. Alley (or future Project Driveway)/South Santa Monica Boulevard (SSSC)
- * (S) indicates signalized intersection
- ** (SSSC) indicates side-street stop-controlled intersection

1.3 Analysis Scenarios

The operations of the study intersection were analyzed during the weekday morning (AM) and evening (PM) peak hours for the following scenarios:

- Existing (2019) Conditions The analysis of existing traffic conditions was based on traffic volume estimates that reflect 2019 conditions. Traffic counts for the study intersections were compiled from available data collected at various times from before the COVID-19 pandemic. Historic counts were grown to reflect 2019 conditions using an average annual growth rate of 0.5% per year.
- Existing (2019) plus Project Conditions This traffic scenario provides an analysis of operating conditions with the changes to Project-generated traffic based on development of the Project. The existing plus Project conditions analysis accounts for both the land use and site access changes proposed under the Project, including the realignment of the alley. The changes to traffic operations were then compared to operations under existing conditions.
- **Future (2026) No Project Conditions** Future traffic projections were developed to reflect the year 2026. The objective of this analysis was to project future traffic growth and operating conditions that could be expected to result from regional growth and related projects in the vicinity of the Project site by the anticipated Project opening year.
- **Future (2026) plus Project Conditions** This traffic scenario provides projected traffic volumes and an analysis of operating conditions for the year 2026 and accounts for both the land use and site access changes proposed with the Project. The changes with the proposed Project on future traffic operating conditions were then identified.

In addition to the scenarios above, traffic operations in the study area were also analyzed assuming full occupancy of the existing uses that are located on the Project site but are currently vacant. The purpose of this additional scenario is to compare traffic operations with the Project to the historic trip generation of the existing uses on the Project site and assess the Project effects on traffic operations.

2. Analysis Methodology & Criteria

This chapter describes the analysis methodologies and criteria that are required by the City of Beverly Hills Local Transportation Assessment Guidelines. The purpose of analyzing traffic operations is to understand operational changes that are expected to occur as a result of the Project.

2.1 Traffic Analysis Methods

The analysis of roadway operations performed for this study is based on procedures presented in the *Highway Capacity Manual 6th Edition (HCM 6)*, published by the Transportation Research Board in 2016. The operations of roadway facilities are described with the term level of service (LOS). LOS is a qualitative description of traffic flow based on factors such as speed, travel time, delay, and freedom to maneuver. Six levels are defined from LOS A, with the least congested operating conditions, to LOS F, with the most congested operating conditions. LOS E represents "at-capacity" operations. Operations are designated as LOS F when volumes exceed capacity, resulting in stop-and-go conditions. The methodologies for signalized and unsignalized intersections are described in the subsections below.

2.1.1 Signalized Intersections

The method described in "Chapter 19: Signalized Intersections" of the HCM 6 was used to prepare the LOS calculations for the signalized study intersections. This LOS method analyzes a signalized intersection's operation based on average control delay per vehicle. Control delay alone is used to characterize LOS for the entire intersection or for an approach. Control delay includes the initial deceleration delay, queue move-up time, stopped delay, and final acceleration delay. The average control delay for signalized intersections is calculated using Synchro 10.0 analysis software and is correlated to a LOS designation, as shown in **Table 1**. Synchro 10.0 analysis accounts for delays associated with conflicting pedestrian crossings, buses stopping and blocking the through lane, and vehicles pulling into or out of adjacent onstreet parking. Other Synchro inputs including saturation flow rate, peak hour factor, and initial vehicle queues were estimated to reflect congested conditions that were observed in the study area before the COVID-19 pandemic.



Table 1: Level of Service Definitions for Signalized Intersections

| Level of Service | Description | Delay in Seconds |
|---------------------|---|------------------|
| A | Progression is extremely favorable, and most vehicles arrive during the green phase. Most vehicles do not stop at all. Short cycle lengths may also contribute to low delay. | ≤ 10.0 |
| В | Progression is good, cycle lengths are short, or both. More vehicles stop than with LOS A, causing higher levels of average delay. | > 10.0 to 20.0 |
| С | Higher congestion may result from fair progression, longer cycle lengths, or both. Individual cycle failures may begin to appear at this level, though many still pass through the intersection without stopping. | > 20.0 to 35.0 |
| D | The influence of congestion becomes more noticeable. Longer delays may result from some combination of unfavorable progression, long cycle lengths, or high V/C ratios. Many vehicles stop, and the proportion of vehicles not stopping declines. Individual cycle failures are noticeable. | > 35.0 to 55.0 |
| E | This level is considered by many agencies to be the limit of acceptable delay. These high-delay values generally indicate poor progression, long cycle lengths, and high V/C ratios. Individual cycle failures are frequent occurrences. | > 55.0 to 80.0 |
| F | This level is considered unacceptable with oversaturation, which is when arrival flow rates exceed the capacity of the intersection. This level may also occur at high V/C ratios below 1.0 with many individual cycle failures. Poor progression and long cycle lengths may also be contributing factors to such delay levels. | > 80.0 |

Source: *Highway Capacity Manual 6th Edition*, Transportation Research Board, 2016.

2.1.2 Unsignalized Intersections

The operations of the unsignalized intersections were evaluated using the method contained in "Chapter 20: Two-Way Stop-Controlled Intersections" of the *HCM* 6. LOS ratings for stop-sign-controlled intersections are based on the average control delay expressed in seconds per vehicle. At a two-way- or side-street-stop-controlled (SSSC) intersection, the average control delay is calculated for the minor-street stopped movement and the major-street left turns, not for the intersection as a whole. For approaches composed of a single lane, the control delay is computed as the average of all movements in that lane. For approaches with multiple lanes, the control delay is computed for each movement; the movement with the worst (i.e., longest) delay is presented for SSSC. As shown in **Table 2**, LOS F is assigned to the movement if the volume-to-capacity (V/C) ratio for the movement exceeds 1.0, regardless of control delay. The average control delay for unsignalized intersections is calculated using Synchro 10.0 analysis software and is correlated to a LOS designation, as shown in **Table 2**.

In the case of the future Project Driveway/South Santa Monica Boulevard intersection, the private driveway approach was not evaluated, and only operations on the public roadway approaches are reported.

Table 2: Unsignalized Intersection Level of Service Definitions

| Level of Service $(v/c \le 1.0)$ | Level of Service (v/c > 1.0) ¹ | Description | Average Control Delay Per Vehicle (Seconds) |
|----------------------------------|--|---|---|
| Α | F | Little or no delay. | ≤ 10.0 |
| В | F | Short traffic delay. | > 10.0 to 15.0 |
| С | F | Average traffic delays. | > 15.0 to 25.0 |
| D | F | Long traffic delays. | > 25.0 to 35.0 |
| E | F | Very long traffic delays. | > 35.0 to 50.0 |
| F | F | Extreme traffic delays with intersection capacity exceeded. | > 50.0 |

Source: *Highway Capacity Manual*, Transportation Research Board, 2016.

Notes

2.2 Analysis Criteria

The analysis compares existing or future baseline operations with "plus project" conditions to determine whether project implementation is expected to cause undesirable increases in delay on the surrounding roadways. Based on the most recent City of Beverly Hills guidelines, a signalized intersection should be identified if it has an increase in average total delay equal to or greater than 10.0 seconds for intersections operating at LOS D, and equal to or greater than 5.0 seconds for intersections operating at LOS E or F after the addition of project traffic. A change in LOS from LOS D to LOS E or LOS E to LOS F does not signify an undesirable effect unless the increase in average delay of 10.0 seconds (LOS D) or 5.0 seconds (LOS E or F) also occurs with the project. Intersections operating at LOS A, B, or C after the addition of the project traffic are not considered undesirable regardless of the increase in delay. **Table 3** below summarizes the criteria for a signalized intersection.

Table 3: Signalized Intersection Criteria

| LOS with Project | Average Total Delay (seconds per vehicle) | Project-Related Increase in Delay |
|------------------|---|---------------------------------------|
| D | >35.0 – 55.0 | Equal to or greater than 10.0 seconds |
| E or F | > 55.0 | Equal to or greater than 5.0 seconds |

Source: City of Beverly Hills Local Transportation Assessment Guidelines, October 2019.

An unsignalized, SSSC intersection operations may be considered undesirable if the location has an increase in total delay that results in operations degrading from LOS D to LOS E, LOS E to LOS F, or by more than 10.0 seconds of delay for locations already operating at LOS F after the addition of project



¹ For approach-based and intersection-wide assessments, such as that used for all-way stop controlled intersections, LOS is defined solely by control delay.

traffic. In addition to the delay thresholds, the unsignalized intersection should only be identified if it also meets the peak hour signal warrant. The signal warrants used for this evaluation are those described in Chapter 4C of the *California Manual of Uniform Control Devices* (CAMUTCD, 2014 Edition), published by the US Department of Transportation Federal Highways Administration (FHWA) then revised and adopted by Caltrans. Intersections operating at LOS A, B, or C after the addition of the project traffic are not considered undesirable regardless of the increase in total delay. **Table 4** summarizes the criteria for an unsignalized intersection.

Table 4: City of Beverly Hills Unsignalized Intersection (SSSC) Criteria

| LOS with Project | Average Total Delay for Side Street Approach (seconds per vehicle) | Project-Related Increase in LOS or Seconds of Average Total Delay |
|------------------|--|---|
| Е | > 35.0 and ≤ 50.0 | LOS D or better to LOS E or worse, and meets the peak hour warrant for a traffic signal |
| F | > 50.0 | LOS E to LOS F, or greater than 10.0 seconds for worst- case approach is already at LOS F, and meets the peak hour warrant for a traffic signal |

Source: City of Beverly Hills Local Transportation Assessment Guidelines, October 2019.

3. Existing Conditions

This chapter discusses the existing traffic operations in the study area. A complete description of the study area's roadway network, transit service, and active transportation facilities is provided in the *Cheval Blanc Beverly Hills Specific Plan Transportation Impact Report* (Fehr & Peers, September 2021).

3.1 Existing Traffic Volumes

Due to the statewide stay-at-home order and social distancing measures issued by the Governor of California and Los Angeles County Department of Health to slow the spread of COVID-19, data collection in 2020 would not reflect typical travel conditions in the study area. Therefore, traffic counts for the study intersections were compiled from available data collected at various times from before the COVID-19 pandemic to estimate travel demand under existing conditions. Historic counts were grown to reflect 2019 conditions using an average annual growth rate of 0.5% per year. Where traffic count data was not available (North Rodeo Drive/South Santa Monica Boulevard), turning volumes were estimated based on volume balancing with adjacent intersections and observed travel flows in the area.

Intersection turning movement counts are reported for the following times:

- Weekday morning peak period (7:00 to 9:00 AM)
- Weekday evening peak period (4:00 to 6:00 PM)

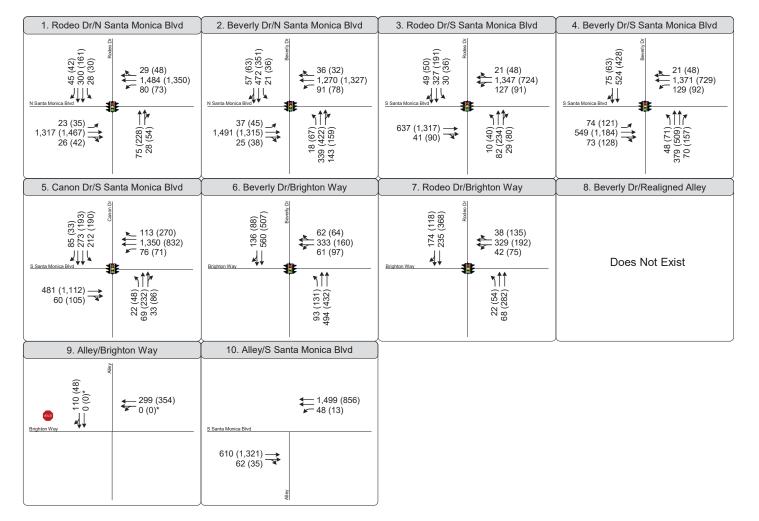
Existing lane configurations and signal controls were obtained through field observations. Signal timing data was provided by the City of Beverly Hills staff. **Figure 2** presents the existing peak hour turning movement volumes, corresponding lane configurations, and traffic control devices. **Appendix A** provides historic traffic count data sheets.

3.2 Existing Intersection Operations

Existing peak hour volumes and lane configurations were used to calculate the LOS for each of the study intersections. The results of the existing LOS analysis are presented in **Table 5** and the corresponding LOS calculation sheets are included in **Appendix B**.

As shown in **Table 5**, most study intersections operate at LOS D or better under existing conditions. The one exception is North Rodeo Drive/South Santa Monica Boulevard which is calculated to operate at undesirable levels of LOS E in the AM peak hour.





* Data was not available for volumes on the alley south of Brighton Way, so these turning movements are shown 0. No changes to these volumes would occur as a result of the proposed project.

AM (PM) Peak Hour Traffic Volume



Lane Configuration



Stop Sign



Signalized



Table 5: Existing (2019) Intersection Operations

| Internation | Cambual | Peak Hour | Existing Operations | | | |
|--|-------------|-----------|------------------------------|------------------|--|--|
| Intersection | Control | Peak Hour | Delay (sec/veh) ¹ | LOS ² | | |
| 1 N Padaa Dr/N Canta Manica Phyd | Cianalizad | AM | 23.7 | С | | |
| 1. N Rodeo Dr/N Santa Monica Blvd | Signalized | PM | 33.9 | С | | |
| 2 N Royarly Dr/N Santa Monica Plyd | Cianalizad | AM | <u>37.8</u> | <u>D</u> | | |
| 2. N Beverly Dr/N Santa Monica Blvd | Signalized | PM | 31.6 | С | | |
| 2 N. Dodgo Dr./C Conto Manico Dividi | Cianalizad | AM | 63.9 | <u>E</u> | | |
| 3. N Rodeo Dr/S Santa Monica Blvd ³ | Signalized | PM | 27.9 | С | | |
| 4 N. Bassarks Dar/C Conta Marrian Blood | Cianalia ad | AM | <u>35.9</u> | <u>D</u> | | |
| 4. N Beverly Dr/S Santa Monica Blvd | Signalized | PM | 41.0 | <u>D</u> | | |
| E. N. Cañan Du/C Canta Manias Blad | C: | AM | 29.4 | С | | |
| 5. N Cañon Dr/S Santa Monica Blvd | Signalized | PM | 19.7 | В | | |
| C N De de a Du/Brinkton W. | C: d | AM | 11.4 | В | | |
| 6. N Rodeo Dr/Brighton Wy | Signalized | PM | 11.9 | В | | |
| 7 N.D. ad. D./D. altra W. 3 | C' 1' 1 | AM | 25.9 | С | | |
| 7. N Beverly Dr/Brighton Wy ³ | Signalized | PM | 26.7 | С | | |
| O N. Daniel - Day Daniel - and Alle | 5556 | AM | DNE | N/A | | |
| 8. N Beverly Dr/Realigned Alley | SSSC | PM | DNE | N/A | | |
| O Brighton Mar/Alloy | cccc | AM | 10.2 | В | | |
| 9. Brighton Wy/Alley | SSSC | PM | | А | | |
| 10. Alley (or future Project Dwy)/S Santa | cccc | AM | 9.6 | Α | | |
| Monica Blvd | SSSC | PM | 14.5 | В | | |

Source: Fehr & Peers, 2021.

Notes:

SSSC indicates Side street stop-controlled intersection.

DNE indicates the intersection does not exist under this scenario.

<u>Underlined</u> text indicates a LOS of D, E, or F.



¹ Whole intersection weighted average stopped delay expressed in seconds per vehicle for signalized intersections. The vehicular delay for the worst movement is reported for the SSSC intersections.

² LOS calculations performed using the *Highway Capacity Manual* 6th Edition (*HCM* 6) method.

³ LOS calculations performed using the *Highway Capacity Manual* 5th Edition method due to signal phasing.

4. Proposed Project Transportation Characteristics

This chapter summarizes the land uses and trip generation of the proposed Project and describes the total number of vehicle trips that would be generated in comparison to existing conditions. In addition to the trip generation estimates, this chapter presents the Project trip distribution and assignment of Project trips to the surrounding roadway network.

4.1 Project Overview

The Project is located in the heart of Beverly Hills. The 1.277-acre Project site is bordered by South Santa Monica Boulevard on the north, North Beverly Drive on the east, North Rodeo Drive on the west, and existing developments on the south. The proposed Project would provide a luxury hotel and multiple-use development, compatible with the scale and massing of the surrounding neighborhood, and providing pedestrian-friendly amenities and uses along the street level. The Project consists of a single four- to nine-story structure including a luxury hotel, private membership club, appurtenant hotel uses including a day spa and wellness center, and uses open to the general public, including restaurant space and retail. The portion of the existing north-south alley that bisects the Project site and is currently accessed from South Santa Monica Boulevard would be relocated to the southern portion of the Project site. The new access point to the alley would be from the west side of North Beverly Drive.

4.1.1 Project Land Uses

The Project allows for a maximum allowable floor area of 220,949 square feet (sf) and a maximum of 115 hotel rooms. The Project also includes a private membership club with up to 500 members (dedicated club facilities include a 36-seat screening room and bar, lounge and social spaces) and appurtenant hotel uses including a day spa and wellness center, uses open to the general public including 25,094 sf of restaurant space and 24,976 sf of retail, and 178 parking spaces located in a subterranean garage. The Project opening year is expected to be 2026.

The proposed Project would replace 56,787 sf of existing commercial space in four structures located at:

- 456 North Rodeo Drive: 6,895 sf commercial with 9 surface parking spaces that is currently occupied
- 468 North Rodeo Drive: 20,265 sf commercial with 6 surface parking spaces that is currently vacant
- 449, 451, and 453 North Beverly Drive: 6,276 sf commercial that is currently vacant
- 461-465 North Beverly Drive: 23,351 sf institutional with 5 surface and 45 underground spaces with driveway access on South Santa Monica Boulevard that is currently occupied

4.1.2 Project Trip Generation

Trip generation for the Cheval Blanc Project uses were generally based on the most recent edition of the Institute of Transportation Engineers (ITE) *Trip Generation Manual* (10th Edition). Specific ITE Land Use codes for each use are provided in **Table 6**. ITE trip generation rates estimate the total number of trips to a given land use for all trip types, including trips made by employees, residents, or visitors to the site.

The only proposed use that was not estimated using ITE rates was the 500-member private membership club. The club provides access to a screening room, bar, lounge and socials spaces, and access to the hotel's wellness center and spa. The club will have the ability to hold a limited number of events for club members per year based on the size of the event. Due to the unique nature of the programmed activities, there is not a comparable trip rate provided by ITE. A custom trip generation rate was developed for the private membership club for member trips based on the expected daily member visitation as identified in the *Parking Demand Analysis Study* (July 16, 2020) for the proposed Project. Based on the membership levels and site amenities, the membership club was estimated to generate 180 daily vehicle-trips and up to 40 vehicle-trips in a peak hour. This trip generation also assumes that members will drive alone to the Project site.

Table 6 provides the trip generation rates applied to the proposed Project.

Table 6: Trip Generation Rates

| Land Has | Trip Rates | | | | | | |
|--------------------------------------|------------|------|------|--|--|--|--|
| Land Use | Daily | AM | PM | | | | |
| Hotel ¹ | 8.36 | 0.47 | 0.60 | | | | |
| Private Membership Club ² | 0.36 | 0.04 | 0.08 | | | | |
| Quality Restaurant ³ | 83.84 | 0.73 | 7.80 | | | | |
| Retail ⁴ | 37.75 | 0.94 | 3.81 | | | | |
| Day Spa ⁵ | 14.50 | 1.21 | 1.45 | | | | |

Notes:

Vehicle trip generation estimates were adjusted based on a variety of factors applicable to the Project context. For one type of credit, a 20% internalization trip credit was applied to the restaurant, retail, and day spa uses. That is, it was assumed that 20% of patrons to these businesses will be hotel guests arriving by foot internally from within the hotel building, not requiring an additional vehicle trip. This rate is consistent with the internal capture rate assumed in the *Parking Demand Analysis Study*. The Mixed-Use



¹ Hotel trip rates based on ITE Land Use 310 – Hotel.

² Trip generation rates based on daily member visitation rates provided in the Cheval Blanc Initial Study.

³ Restaurant trip rates based on ITE Land Use 931 – Quality Restaurant.

⁴ Retail trip rates based on ITE Land Use 820 – Shopping Center.

⁵ Day Spa trip rates based on ITE Land Use 918 – Hair Salon.

(MXD) Trip Generation Model was also utilized to determine if this level of internalization was reasonable. The MXD Model was developed by Fehr & Peers and the Environmental Protection Agency (EPA), and it accounts for the site context and other factors to estimate potential internalization and multimodal trip reductions. The MXD results confirmed that a 20% internal capture rate is appropriate for the mix of uses that make up the proposed Project.

A 30% pass-by credit was assumed for the retail use per the most recent edition of the ITE *Trip Generation Handbook* (3rd Edition). Pass-by trips are those vehicles already passing the proposed Project location, and therefore these are not new trips to the overall roadway network, but are instead existing trips that are already in the Beverly Hills Business Triangle and will visit the proposed retail use.

An adjustment was also made based on trip generation estimates for the existing commercial uses that will be demolished to make way for the proposed Project. Because some of the existing uses are currently vacant, the trip credit has been applied only for existing, active uses to account for the vehicle trips already on the roadway network.

No additional credits were applied to the Project trip generation. However, it should be noted that hotel and club employees who wish to travel by transit would be provided with free transit passes, and secure bicycle parking, showers, and lockers, and charging facilities for e-bicycles would be provided to encourage bicycle commuting, both of which measures may reduce employee vehicle trips.

Table 7 provides the detailed trip generation estimates for the proposed Project. After making the appropriate adjustments, the maximum development proposed in the Project will generate approximately 2,360 daily vehicle trips, of which up to approximately 90 vehicle trips are projected to be generated during the AM peak travel hour and up to approximately 220 vehicle trips are projected to be generated during the PM peak travel hour.

Table 7: Trip Generation Estimates

| | | | | Trip | | | | |
|------------------------------------|--------------------------------|---------|------|------|-------|------|------|-------|
| Land Use | Quantity | 5 " | | АМ | | | PM | |
| | | Daily | In | Out | Total | In | Out | Total |
| Hotel | 115 rooms | 961 | 32 | 22 | 54 | 35 | 34 | 69 |
| Private Membership Club | 500 members | 180 | 16 | 4 | 20 | 32 | 8 | 40 |
| Quality Restaurant | 25,094 sf | 2,104 | 9 | 9 | 18 | 131 | 65 | 196 |
| | Internal Capture ¹ | (421) | (2) | (2) | (4) | (26) | (13) | (39) |
| | 24,976 sf | 943 | 14 | 9 | 23 | 46 | 49 | 95 |
| Retail | Internal Capture ¹ | (189) | (3) | (2) | (5) | (9) | (10) | (19) |
| | Pass-by Reduction ² | (226) | (3) | (2) | (5) | (11) | (12) | (23) |
| D 6 | 12,936 sf | 188 | 8 | 8 | 16 | 3 | 16 | 19 |
| Day Spa | Internal Capture ¹ | (37) | (1) | (2) | (3) | (1) | (3) | (4) |
| | Total Gross Vehicle Trips | 3,503 | 70 | 44 | 114 | 200 | 134 | 334 |
| Existing, Active Uses ³ | 30,246 sf | (1,142) | (18) | (10) | (28) | (55) | (60) | (115) |
| | TOTAL NET VEHICLE TRIPS | 2,361 | 52 | 34 | 86 | 145 | 74 | 219 |

Notes: Detailed trip generation calculation contained in **Appendix C**.



¹ Internal capture rate assumed to be 20%.

² Pass-by reduction assumed to be 30% based on the ITE *Trip Generation Handbook* (3rd Edition).

³ Trip generation for existing, active uses was based on the ITE Trip Generation Rate for general retail; ITE Land Use 820 – Shopping Center rates are shown in Table 6.

These Project trips were then broken down into the following trip types: employees, visitors arriving by private vehicle and using the valet, and visitors arriving by shared mobility transportation network companies (TNC), such as Uber or Lyft. The proliferation of TNCs in recent years is important to consider in a project of this type and size. Pick-up and drop-off trips, such as those utilizing TNC services, do not utilize site parking but they still generate a vehicle trip to and from the Project site. In order to account for TNCs, it was assumed that TNCs will account for 50% of the vehicle trips generated by the restaurant, and 66.6% of the vehicle trips generated by the hotel, based on observed drive ratios provided in the *Parking Demand Analysis Study*. Since each inbound TNC trip also results in an outbound TNC trip, the demand for inbound and outbound TNC trips were estimated and the higher of the two calculations was assumed for both directions to account for TNCs that drop off a patron and leave the Project site without picking up a new passenger. The percentage of trips generated by employees traveling to the Project site was also estimated using the parking demand estimates from the *Parking Demand Analysis Study*. The reason that employment trip generation is estimated separately in the table below is because these vehicles would self-park whereas visitors to the site would utilize the motor court. **Table 8** provides the breakdown of Project trips by type.

Table 8: Project Trips by Type

| | Vehicle Trip Estimates | | | | | | | | |
|--|------------------------|----|-----------|---------|-----|-----------|-----------|--|--|
| Land Use | Delle | A | M Peak Ho | our | PI | M Peak Ho | our | | |
| | Daily | In | Out | Total | ln | Out | Total | | |
| Total Gross Vehicle Trips | 3,503 | 70 | 44 | 114 | 200 | 134 | 334 | | |
| Total Estimated Employee Trips | 521 | 10 | 6 | 16 | 30 | 20 | 50 | | |
| Total Estimated Visitor Valet Trips | 1,501 | 35 | 19 | 54 | 95 | 65 | 160 | | |
| Estimated Visitor TNC Trips ^{1,2} | 1,482 | 25 | (19) 25 | (44) 50 | 75 | (49) 75 | (124) 150 | | |
| Adjusted Total Gross Vehicle Trips | 3,503 | 70 | 50 | 120 | 200 | 160 | 360 | | |

Notes:

- (1) TNCs assumed to be 50% of the vehicle trips generated by the restaurant, and 66.6% of the vehicle trips generated by the hotel, based on observed drive ratios provided in the *Parking Demand Analysis Study* technical memorandum (July 16, 2020).
- (2) Where inbound and outbound trips were unequal, the higher of the two calculations was assumed for both directions to account for TNCs that drop off a patron and leave the Project site without picking up a new passenger.

While the transportation assessment only considers a trip credit for existing uses that are currently active, the trip generation of the historic uses were also estimated to illustrate the vehicle travel demand for the Project in comparison to full occupancy of the existing uses on the site. **Table 9** compares the proposed Project trip generation to the historic trip generation of the site (i.e., when all existing uses were in operation). As shown, the Project will result in a net increase of 1,359 daily trips, including 67 AM peak hour trips and 144 PM peak hour trips, as compared to the historic trip generation of the Project site.

Table 9: Project vs. Historical Site Trip Generation

| | Vehicle Trip Estimates | | | | | | | | | |
|--|------------------------|----|-----|-------|-----|-----|-------|--|--|--|
| Land Use | Daile | | AM | | PM | | | | | |
| | Daily | In | Out | Total | ln | Out | Total | | | |
| Total Gross Project Vehicle Trips (without credit) | 3,503 | 70 | 50 | 120 | 200 | 160 | 360 | | | |
| Total Existing Uses Historic (Fully Occupied) Vehicle Trips | 2,144 | 34 | 19 | 53 | 104 | 112 | 216 | | | |
| NET CHANGE IN SITE-GENERATED VEHICLE TRIPS | 1,359 | 36 | 31 | 67 | 96 | 48 | 144 | | | |

4.1.3 Alley Realignment

An existing north-south public alley connects South Santa Monica Boulevard and Brighton Way, parallel with North Rodeo Drive and North Beverly Drive. The alley is currently accessed via South Santa Monica Boulevard, and bisects the Project site. The Project proposes to relocate that portion of the alley that bisects the Project site and relocate it, as a public alley, so that it connects North Beverly Drive to Brighton Way. Accordingly, existing trips into the alley from South Santa Monica Boulevard will reroute with implementation of the proposed Project to instead use the new alley entrance on North Beverly Drive.

The new alley access will be located approximately 120 feet north of the existing signalized mid-block crossing on North Beverly Drive. Access from northbound North Beverly Drive will be provided by a two-way left-turn lane which immediately north of the proposed alley transitions to a northbound left-turn pocket for vehicles turning onto South Santa Monica Boulevard. Across from the proposed alley location are two adjacent driveways for parking garages on the east side of North Beverly Drive. The relocation of the alley will require on-street parking to be relocated or removed, potentially affecting up to five (5) parking stalls.

The alley will remain one-way in the westbound/southbound direction, and the existing exit onto Brighton Way will remain as is. All existing parking or valet operations located in the alley will remain unchanged for uses adjacent to the Project site. The proposed alley relocation, including the turn geometry, has been designed in accordance with City standards to ensure emergency vehicle, utility, delivery, and other service truck access.

The existing alley travel demand was obtained from Appendix IS-9: Hirsch Green Alley Study of the *Cheval Blanc Beverly Hills Specific Plan: Initial Study* (Eyestone Environmental, 2020) (Alley Study). The Alley Study collected weekday and weekend traffic counts at the South Santa Monica Boulevard alley entrance in April and May of 2019. The following average weekday counts were observed:



- 718 vehicles per day (485 from the west / 233 from the east)
- 110 vehicles in the AM peak hour (62 from the west / 48 from the east)
- 48 vehicles in the PM peak hour (35 from the west / 13 from the east)

Based on the alley travel demands observed in 2019, these vehicles were rerouted to the realigned alley entrance on North Beverly Drive. Vehicles can enter the alley from northbound or southbound North Beverly Drive and will exit the alley onto Brighton Way.

4.1.4 Project Access

Visitors to the Project traveling either by private vehicle or TNC are assumed to access the Project using the motor court located on South Santa Monica Boulevard. Those traveling by private vehicle will use the valet service, and valet employees will then drive arriving guests' vehicles eastbound on South Santa Monica Boulevard and southbound on North Beverly Drive to enter the reconfigured alley and access the Project's subterranean parking. For departing guests, valet employees will use the direct outbound access from the subterranean parking to the motor court. The Project site plan is provided in **Figure 3**.

Similar to the existing alley entrance, vehicles could enter the motor court from both eastbound and westbound South Santa Monica Boulevard. Left turns out of the motor court will be prohibited such that all departing vehicles must turn right onto South Santa Monica Boulevard.

Employees at the Project will self-park in the subterranean parking garage. Employees will exit the Project using the southbound alley onto Brighton Way. Service and utility vehicles will access the Project site via the relocated alley entrance on North Beverly Drive. Full-size utility and service vehicles will use the two loading bays provided at the south end of the Project site, while smaller van-sized utility sand service vehicles will use two additional loading bays provided in the below-grade parking structure. A complete description of the Project's access and circulation is provided in the *Cheval Blanc Beverly Hills Specific Plan Transportation Impact Report* (Fehr & Peers, September 2021).

4.2 Trip Distribution

The distribution of Project trips was estimated based on existing counts available for intersections adjacent or near the proposed Project site. Based on traffic flows in the area, it is expected that 10% of proposed Project generated trips will originate in the north, 30% will originate in the east, 30% will originate in the south, and 30% will originate in the west. The Project is composed of a mixture of uses (hotel, private membership club, restaurant, retail, and day spa) and it is expected that hotel guests will travel to and from a wide variety of locations for various purposes. Potential trip purposes could include shopping, recreation, and work trips for employees.

The Project trip distribution is shown in **Figure 4**, and the resulting Project trip assignment is provided in **Figure 5**. The directionality of the arrows in Figure 4 illustrate inbound travel flows to the Project site; however, outbound travel flows are expected to follow the same pattern.

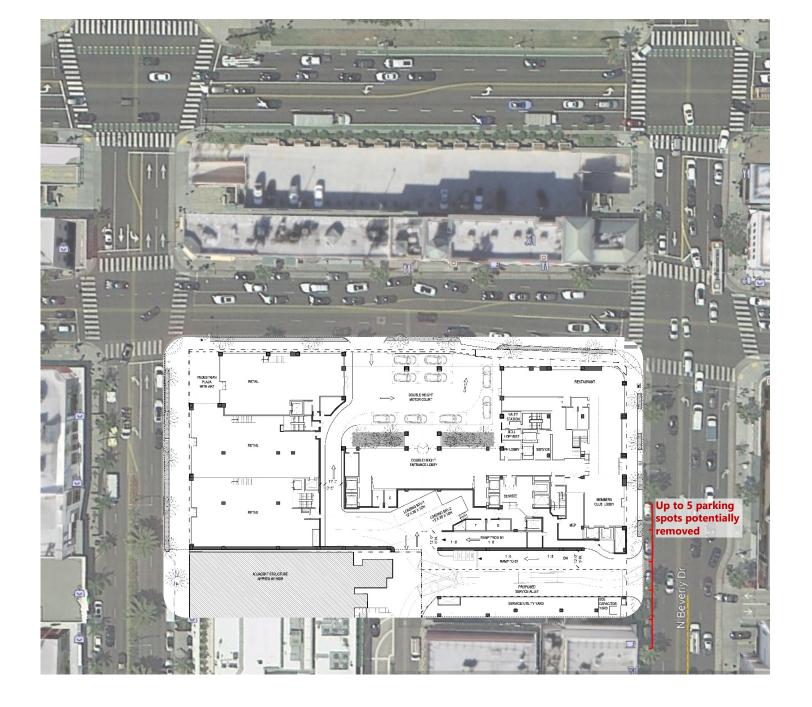




Figure 3

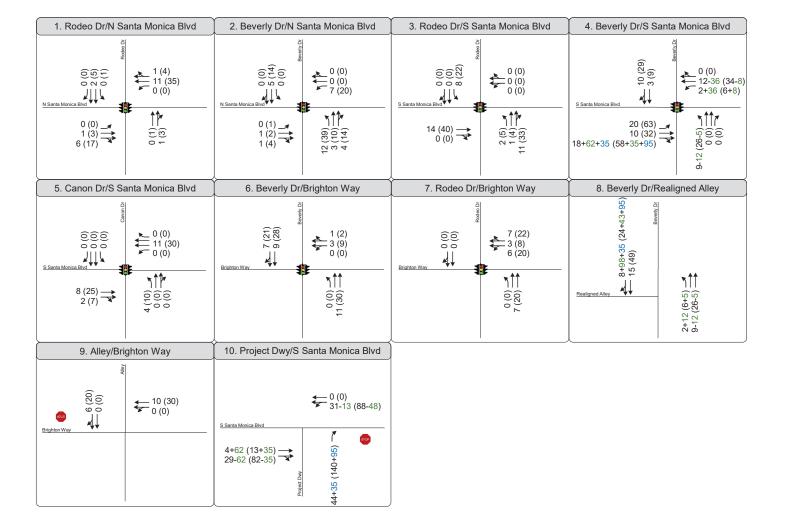




LegendProject Location

← Trip Distribution

Figure 4 **Project Trip Distribution**



AM (PM) Peak Hour Traffic Volume

Project trips, except valet-driven

Alley reassignment

Valet-driven trips



Lane Configuration



Stop Sign



Signalized



5. Existing Plus Project Conditions

This chapter presents the traffic operations analysis for Existing plus Project conditions with the proposed Project.

5.1 Existing Plus Project Traffic Volumes

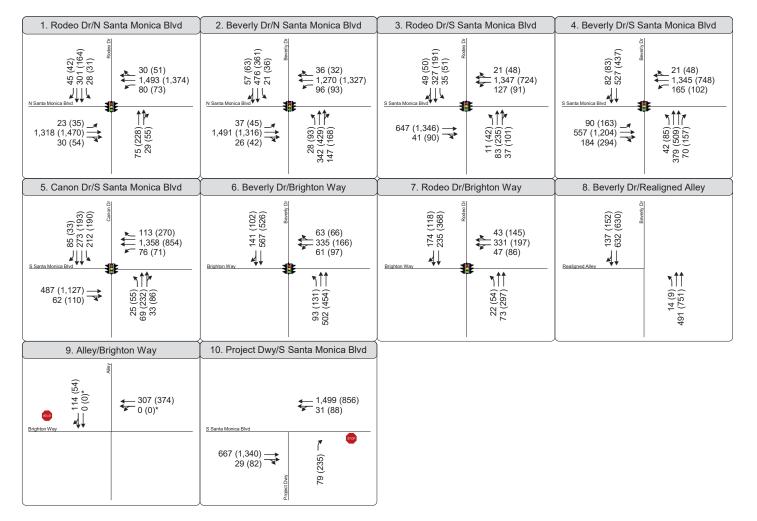
The traffic volumes for the proposed Project are comprised of the existing conditions traffic volumes with the proposed Project land uses in place and the rerouted alley trips. The trip generation and trip distribution presented in the above chapter were used to generate the Existing plus Project traffic volumes provided in **Figure 6**.

5.2 Existing Plus Project Intersection Operations

As shown in **Table 10**, when comparing Existing conditions to the Existing plus Project intersection operations, most of the study intersections experience an increase in average vehicle delay with the Project land use and site access changes in place. In some cases, an intersection may experience a decrease in average vehicle delay with the Project in place. This can occur when the Project adds traffic to a movement that has less delay than the overall average for the intersection, which results in a slight decrease in the weighted average delay. Despite the changes in delay, most study intersections are projected to operate at LOS D or better under Existing plus Project conditions. The following intersections are projected to operate at LOS E or LOS F levels with implementation of the Project under one or both peak hours:

- Although North Rodeo Drive/South Santa Monica Boulevard is projected to operate at LOS E
 under Existing plus Project conditions in the AM peak hour, the addition of Project traffic
 increases average vehicle delay by only one (1) second. Therefore, the increase in delay at this
 location does not exceed the City's criteria for signalized intersections.
- At the North Beverly Drive/South Santa Monica Boulevard intersection, operations are expected
 to degrade from LOS D to LOS E in the PM peak hour, and LOS D will be exacerbated in the AM
 peak hour, with increases in delay of more than 10 seconds. Therefore, the increase in delay at
 this location exceeds the City's criteria for signalized intersections.

The LOS calculation sheets are included in **Appendix B.**



* Data was not available for volumes on the alley south of Brighton Way, so these turning movements are shown 0. No changes to these volumes would occur as a result of the proposed project.

AM (PM) Peak Hour Traffic Volume



Stop Sign

Signalized



Figure 6

Table 10: Existing (2019) No Project and Existing Plus Project Intersection Operations

| | | Peak | Existing No Project | | Existing Plu | s Project | Change in | |
|---|-------------|------|---------------------------------|------------------|---------------------------------|------------------|---------------------------------|--|
| Intersection | Control | Hour | Delay (sec/veh) ¹ | LOS ² | Delay (sec/veh) ¹ | LOS ² | Delay (sec/veh) ³ | |
| 1. N Rodeo Dr/N Santa | Signalized | AM | 23.7 | С | 24.0 | С | 0.3 | |
| Monica Blvd | Signalized | PM | 33.9 | С | <u>35.6</u> | <u>D</u> | 1.7 | |
| 2. N Beverly Dr/N Santa | Signalized | AM | <u>37.8</u> | <u>D</u> | 40.7 | <u>D</u> | 2.9 | |
| Monica Blvd | Signalized | PM | 31.6 | С | <u>36.0</u> | <u>D</u> | 4.4 | |
| 3. N Rodeo Dr/S Santa Monica Blvd ⁴ | Cianalizad | AM | 63.9 | <u>E</u> | <u>64.9</u> | <u>E</u> | 1.0 | |
| | Signalized | PM | 27.9 | С | 30.9 | С | 3.0 | |
| 4. N Beverly Dr/S Santa Monica Blvd | Cianalizad | AM | 35.9 | <u>D</u> | <u>53.8</u> | <u>D</u> | 17.9 | |
| | Signalized | PM | <u>41.0</u> | <u>D</u> | <u>57.0</u> | <u>E</u> | 16.0 | |
| 5. N Cañon Dr/S Santa | Signalized | AM | 29.4 | С | 29.7 | С | 0.3 | |
| Monica Blvd | | PM | 19.7 | В | 18.3 | В | -1.4 | |
| C NI Dadaa Da/Daiahtaa W. | | AM | 11.4 | В | 12.5 | В | 1.1 | |
| 6. N Rodeo Dr/Brighton Wy | Signalized | PM | 11.9 | В | 12.5 | В | 0.6 | |
| 7. N. Davisuh i Du / Duisih taun N/. 4 | Ciamalina d | AM | 25.9 | С | 26.0 | С | 0.1 | |
| 7. N Beverly Dr/Brighton Wy ⁴ | Signalized | PM | 26.7 | С | 26.8 | С | 0.1 | |
| 8. N Beverly Dr/Realigned | CCCC | AM | DNE | N/A | 10.0 | А | N/A | |
| Alley | SSSC | PM | DNE | N/A | 15.8 | С | N/A | |
| O. Brighton Mar/Alloy | CCCC | AM | 10.2 | В | 10.3 | В | 0.1 | |
| 9. Brighton Wy/Alley | SSSC | PM | 9.7 | Α | 9.8 | А | 0.1 | |
| 10. Alley (or future Project | cccc | AM | 9.6 | Α | 9.4* | A* | -0.2 | |
| Dwy)/S Santa Monica Blvd | SSSC | PM | 14.5 | В | 18.0* | C* | 3.5 | |

Source: Fehr & Peers, 2021.

Notes:

SSSC indicates Side street stop-controlled intersection.

DNE indicates the intersection does not exist under this scenario.

Underlined text indicates a LOS of D, E, or F.

Bold text indicates that the delay or LOS exceeds the City's criteria as a result of the Project trips.

¹ Whole intersection weighted average stopped delay expressed in seconds per vehicle for signalized intersections. The vehicular delay for the worst movement is reported for the SSSC intersections.

² LOS calculations performed using the *Highway Capacity Manual* 6th Edition (*HCM* 6) method.

³ Unacceptable seconds of delay per vehicle and LOS or increases in seconds of delay per vehicle highlighted in **bold**.

⁴ LOS calculations performed using the *Highway Capacity Manual* 5th Edition method due to signal phasing.

^{*} Operations only on the public roadway approaches are reported.

5.3 Comparison of Intersection Operations with Existing Uses in Operation

The Project's effects on traffic operations reported above compares traffic operations with the Project to existing traffic conditions. As discussed in the land use section above, the proposed Project would replace 56,787 sf of existing commercial space in four structures located at:

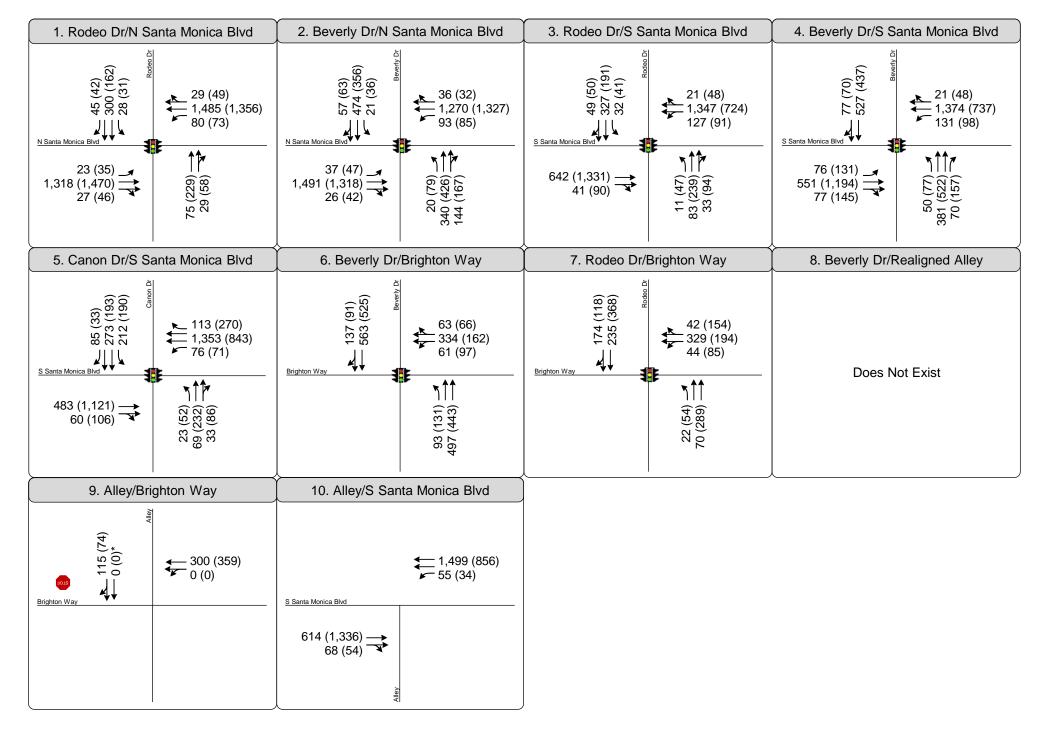
- 456 North Rodeo Drive: 6,895 sf commercial with 9 surface parking spaces that is currently occupied
- 468 North Rodeo Drive: 20,265 sf commercial with 6 surface parking spaces that is currently vacant
- 449, 451, and 453 North Beverly Drive: 6,276 sf commercial that is currently vacant
- 461-465 North Beverly Drive: 23,351 sf institutional with 5 surface and 45 underground spaces with driveway access on South Santa Monica Boulevard that is currently occupied

Given that some of the existing commercial spaces are vacant, a trip credit was not applied for these uses to the proposed Project. In addition, the vehicle-trips being generated by these vacant uses are not included in the Existing conditions analysis. Therefore, an additional traffic operations analysis was completed assuming full occupancy of the existing uses that are located on the Project site, referred to as the "Existing plus Existing Uses in Operation" scenario. The purpose of this additional scenario is to compare traffic operations with the Project to the historic trip generation of the existing uses on the Project site and determine if the Project would exceed the City's criteria for intersection operations.

As shown above in **Table 9**, full occupancy of the existing commercial spaces on the Project site would generate approximately 2,145 daily trips with approximately 55 trips occurring during the AM peak hour and 215 trips occurring in the PM peak hour. Since some of the existing uses are currently occupied, only the trips generated from unoccupied uses were added to existing traffic volumes. The trip assignment was based on the parking location for the existing unoccupied uses and the vehicle trips were routed through each of the study intersections. The traffic volumes for Existing plus Existing Uses in Operation are shown on **Figure 7**.

The results of the LOS analysis for Existing plus Existing Uses in Operation are presented in **Table 11** and the corresponding LOS calculation sheets are included in **Appendix B**. When comparing Existing plus Existing Uses in Operation to the Existing plus Project intersection operations, the increase in vehicle delay is lower at most of the study intersections than the results shown above comparing the Project to Existing conditions. However, one study intersection, North Beverly Drive/South Santa Monica Boulevard, would still have an increase in average vehicle delay of more than 10 seconds during the AM (LOS D) and PM (LOS E) peak hours, when comparing Existing plus Existing Uses in Operation to the Existing plus Project intersection operations, which exceeds the City's criteria for signalized intersections.





*Data was not available for volumes on the alley south of Brighton Way, so these turning movements are shown 0. No changes to these volumes would occur as a result of the proposed project.

AM (PM) Peak Hour Traffic Volume



Stop Sign

\$ Signalized



Figure 7

Peak Hour Traffic Volumes and Lane Configurations -Existing Plus Existing Uses in Operation

Table 11: Existing (2019) Plus Existing Uses in Operation and Existing Plus Project Intersection Operations

| Intersection | Control | Peak | Existing Plu Uses in Op | | Existing Plu | s Project | Change in Delay |
|--|------------|------|---------------------------------|------------------|---------------------------------|------------------|------------------------|
| | Control | Hour | Delay (sec/veh) ¹ | LOS ² | Delay (sec/veh) ¹ | LOS ² | (sec/veh) ³ |
| 1. N Rodeo Dr/N Santa | Signalized | AM | 23.7 | С | 24.0 | С | 0.3 |
| Monica Blvd | Signalized | PM | 34.7 | С | <u>35.6</u> | <u>D</u> | 0.9 |
| 2. N Beverly Dr/N Santa | Signalized | AM | <u>38.5</u> | <u>D</u> | 40.7 | <u>D</u> | 2.2 |
| Monica Blvd | Signalized | PM | 33.3 | С | 36.0 | <u>D</u> | 2.7 |
| 3. N Rodeo Dr/S Santa | Signalized | AM | <u>64.2</u> | <u>E</u> | 64.9 | <u>E</u> | 0.7 |
| Monica Blvd ⁴ | Signalized | PM | 29.6 | С | 30.9 | С | 1.3 |
| 4. N Beverly Dr/S Santa | Cianalizad | AM | <u>36.7</u> | <u>D</u> | <u>53.8</u> | <u>D</u> | 17.1 |
| Monica Blvd | Signalized | PM | 43.0 | <u>D</u> | <u>57.0</u> | <u>E</u> | 14.0 |
| 5. N Cañon Dr/S Santa | Signalized | AM | 29.5 | С | 29.7 | С | 0.2 |
| Monica Blvd | | PM | 16.5 | В | 18.3 | В | 1.8 |
| C. N. Dadaa Du/Duiahtau W. | C: l: l | AM | 11.4 | В | 12.5 | В | 1.1 |
| 6. N Rodeo Dr/Brighton Wy | Signalized | PM | 12.0 | В | 12.5 | В | 0.5 |
| 7 N. Bouarly Dr./Princhton W. 4 | Cianalizad | AM | 25.9 | С | 26.0 | С | 0.1 |
| 7. N Beverly Dr/Brighton Wy ⁴ | Signalized | PM | 26.7 | С | 26.8 | С | 0.1 |
| 8. N Beverly Dr/Realigned | ccc | AM | DNE | N/A | 10.0 | А | N/A |
| Alley | SSSC | PM | DNE | N/A | 15.8 | С | N/A |
| O Deighton Mar/Allon | ccc | AM | 10.2 | В | 10.3 | В | 0.1 |
| 9. Brighton Wy/Alley | SSSC | PM | 9.9 | Α | 9.8 | Α | -0.1 |
| 10. Alley (or future Project | ccc | AM | 9.7 | Α | 9.4* | A* | -0.3 |
| Dwy)/S Santa Monica Blvd | SSSC | PM | 15.4 | С | 18.0* | C* | 2.6 |

Source: Fehr & Peers, 2021.

Notes:

SSSC indicates Side street stop-controlled intersection.

DNE indicates the intersection does not exist under this scenario.

<u>Underlined</u> text indicates a LOS of D, E, or F.

Bold text indicates that the delay or LOS exceeds the City's criteria as a result of the Project trips



¹ Whole intersection weighted average stopped delay expressed in seconds per vehicle for signalized intersections. The vehicular delay for the worst movement is reported for the SSSC intersections.

² LOS calculations performed using the *Highway Capacity Manual* 6th Edition (*HCM* 6) method.

³ Unacceptable seconds of delay per vehicle and LOS or increases in seconds of delay per vehicle highlighted in **bold**.

⁴LOS calculations performed using the Highway Capacity Manual 5th Edition method due to signal phasing.

^{*}Operations only on the public roadway approaches are reported.

6. Future (2026) Conditions

This chapter addresses the traffic operations with the proposed Project under Future (2026) conditions, which represents conditions as they are expected to occur with the buildout of the Project.

6.1 Future Traffic Volume Forecasts

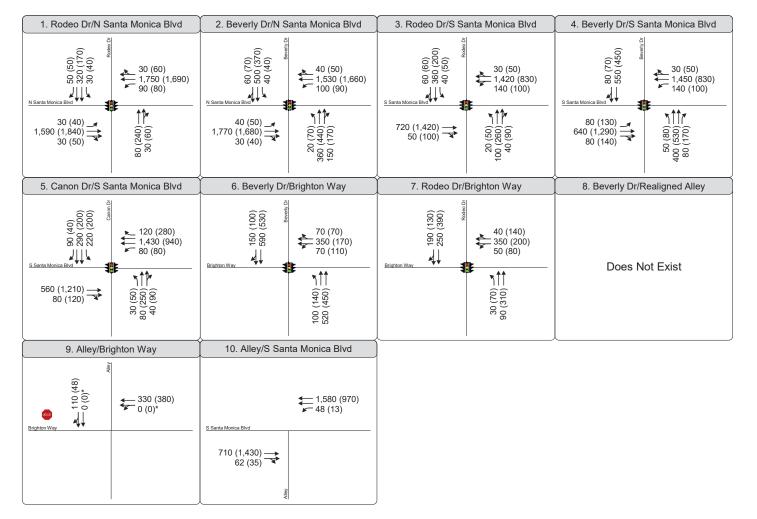
The year 2026 was used to forecast Future conditions to reflect the expected opening year of the proposed Project. The growth in traffic in the study area reflects future travel demands from regional growth and related projects in the vicinity of the Project site. A variety of sources were consulted to develop the cumulative traffic forecasts. These sources include:

- Historic traffic counts, grown to reflect Existing (2019) conditions
- Traffic from approved and pending projects in the City of Beverly Hills, City of Los Angeles, and City of West Hollywood
- Ambient growth in existing traffic volumes to reflect growth in regional traffic (a growth rate of 0.5% per year was applied to the 2019 traffic volumes to reflect this ambient growth)

The list of related projects used to develop the cumulative traffic forecasts is provided in the *Cheval Blanc Beverly Hills Specific Plan Transportation Impact Report* (Fehr & Peers, September 2021).

Traffic volumes for Future (2026) No Project conditions are shown on **Figure 8**.

The Project trip assignment was superimposed on Future (2026) No Project traffic volumes to yield Future (2026) plus Project volumes, shown on **Figure 9**.



* Data was not available for volumes on the alley south of Brighton Way, so these turning movements are shown 0. No changes to these volumes would occur as a result of the proposed project.

AM (PM) Peak Hour Traffic Volume



Lane Configuration



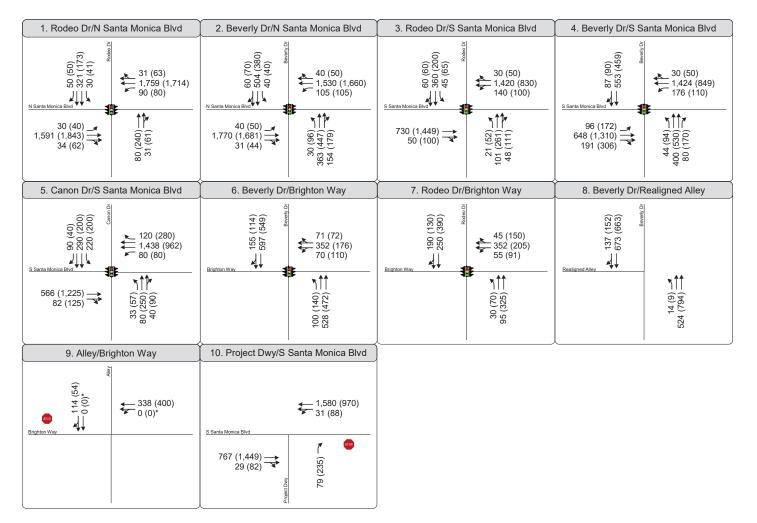
Stop Sign



Signalized



Figure 8



* Data was not available for volumes on the alley south of Brighton Way, so these turning movements are shown 0. No changes to these volumes would occur as a result of the proposed project.

AM (PM) Peak Hour Traffic Volume



Lane Configuration



Stop Sign



Signalized



6.2 Future Intersection Operations

The results of the LOS analysis for Future (2026) conditions with and without the Project are presented in **Table 12** and the corresponding LOS calculation sheets are included in **Appendix B**. Under Future No Project conditions, three of the study intersections operate at LOS F during one or both of the peak hours. With the Project in place, most of the study intersections experience an increase in average vehicle delay while some experience a decrease in delay. As noted in the Existing plus Project conditions analysis, a decrease in delay can occur when the Project adds traffic to a movement that has less delay than the overall average for the intersection, which results in a slight decrease in the weighted average delay. The following intersections are projected to operate at LOS E or LOS F levels with implementation of the Project under one or both peak hours:

- The North Rodeo Drive/North Santa Monica Boulevard intersection is projected to operate at LOS F under Future conditions both without and with the Project in the PM peak hour. The addition of Project traffic is estimated to increase average vehicle delay by 5.1 seconds during this time period, exceeding the delay criteria provided in the City's guidelines for signalized intersections. Although delays could be slightly reduced through signal timing modifications, this improvement is considered infeasible due to the coordination between traffic signals along the greater North Santa Monica Boulevard corridor.
- The North Beverly Drive/North Santa Monica Boulevard intersection is projected to operate at LOS F under Future conditions both without and with the Project in both peak hours. In the AM peak hour, the addition of Project traffic is estimated to increase average vehicle delay by 5.4 seconds, while in the PM peak hour the addition of Project traffic is estimated to increase delay by 4.8 seconds. Therefore, this location exceeds the delay criteria of the City's guidelines during the AM peak hour. Although operations could be slightly improved through signal timing modifications, this improvement is considered infeasible due to the coordination between traffic signals along the greater North Santa Monica Boulevard corridor.
- Although the North Rodeo Drive/South Santa Monica Boulevard intersection is projected to
 operate at LOS F under Future conditions both without and with the Project in the AM peak hour,
 the addition of Project traffic increases average vehicle delay by less than one (1) second.
 Therefore, this location does not exceed the delay criteria of the City's analysis guidelines.
- At the North Beverly Drive/South Santa Monica Boulevard intersection, operations are expected to degrade from LOS D to LOS E in both peak hours, with increases in delay of nearly 20 seconds. Therefore, this location exceeds the delay criteria of the City's guidelines during both peak periods. A potential option for improving operations would be to modify the Project site plan to widen the roadway and provide a separate eastbound right-turn lane pocket. However, this improvement would reduce average vehicle delay by less than five (5) seconds and the delay increase would still exceed the City's delay criteria. In addition, widening South Santa Monica Boulevard to provide a separate right-turn lane would increase crossing distances for pedestrians and preclude the sidewalk widening that is proposed as part of the Project. Given the vibrant pedestrian environment in the Project area, this would be an undesirable outcome.



Table 12: Future (2026) No Project and Future Plus Project Intersection Operations

| | | Peak | Future No | Project | Future Plus | Project | Change in | |
|---|------------|------|---------------------------------|------------------|---------------------------------|------------------|---------------------|--|
| Intersection | Control | Hour | Delay (sec/veh) ¹ | LOS ² | Delay (sec/veh) ¹ | LOS ² | Delay (sec/veh)³ | |
| 1. N Rodeo Dr/N Santa | Signalized | AM | 47.8 | <u>D</u> | 49.0 | <u>D</u> | 1.2 | |
| Monica Blvd | Signalized | PM | <u>103.4</u> | <u>E</u> | <u>108.5</u> | <u>E</u> | 5.1 | |
| 2. N Beverly Dr/N Santa | Signalized | AM | <u>87.0</u> | <u>E</u> | 92.4 | <u>E</u> | 5.4 | |
| Monica Blvd | Signalized | PM | 98.0 | <u>E</u> | 102.8 | <u>E</u> | 4.8 | |
| 3. N Rodeo Dr/S Santa Monica Blvd ⁴ | C: | AM | <u>98.4</u> | <u>E</u> | <u>99.3</u> | <u>E</u> | 0.9 | |
| | Signalized | PM | <u>41.9</u> | <u>D</u> | <u>45.3</u> | <u>D</u> | 3.4 | |
| 4. N Beverly Dr/S Santa Monica Blvd | C: | AM | <u>38.6</u> | D | <u>57.0</u> | <u>E</u> | 18.4 | |
| | Signalized | PM | <u>41.6</u> | <u>D</u> | 61.3 | <u>E</u> | 19.7 | |
| 5. N Cañon Dr/S Santa | Signalized | AM | 34.4 | С | <u>35.6</u> | D | 1.2 | |
| Monica Blvd | | PM | 23.9 | С | 22.1 | С | -1.8 | |
| C. N. Davida a Davida la cara M | | AM | 11.8 | В | 13.3 | В | 1.5 | |
| 6. N Rodeo Dr/Brighton Wy | Signalized | PM | 12.3 | В | 13.0 | В | 0.7 | |
| 7 N.D. ad. D./D.:hu.a. N/ 4 | C' I' I | AM | 29.1 | С | 29.2 | С | 0.1 | |
| 7. N Beverly Dr/Brighton Wy ⁴ | Signalized | PM | 29.4 | С | 29.4 | С | 0.0 | |
| 8. N Beverly Dr/Realigned | cccc | AM | DNE | N/A | 10.2 | В | N/A | |
| Alley | SSSC | PM | DNE | N/A | 16.2 | С | N/A | |
| O. Brighton Mar/Alloy | CCCC | AM | 10.4 | В | 10.5 | В | 0.1 | |
| 9. Brighton Wy/Alley | SSSC | PM | 9.8 | Α | 9.9 | Α | 0.1 | |
| 10. Alley (or future Project | CCCC | AM | 10.1 | В | 9.9* | A* | -0.2 | |
| Dwy)/S Santa Monica Blvd | SSSC | PM | 15.6 | С | 19.9* | C* | 4.3 | |

Source: Fehr & Peers, 2021.

Notes:

SSSC indicates Side street stop-controlled intersection.

DNE indicates the intersection does not exist under this scenario.

Underlined text indicates a LOS of D, E, or F.

Bold text indicates that the delay or LOS exceeds the City's criteria as a result of the Project trips.

¹ Whole intersection weighted average stopped delay expressed in seconds per vehicle for signalized intersections. The vehicular delay for the worst movement is reported for the SSSC intersections.

² LOS calculations performed using the *Highway Capacity Manual* 6th Edition (*HCM* 6) method.

³ Unacceptable seconds of delay per vehicle and LOS or increases in seconds of delay per vehicle highlighted in **bold**.

⁴ LOS calculations performed using the *Highway Capacity Manual* 5th Edition method due to signal phasing.

^{*} Operations only on the public roadway approaches are reported.

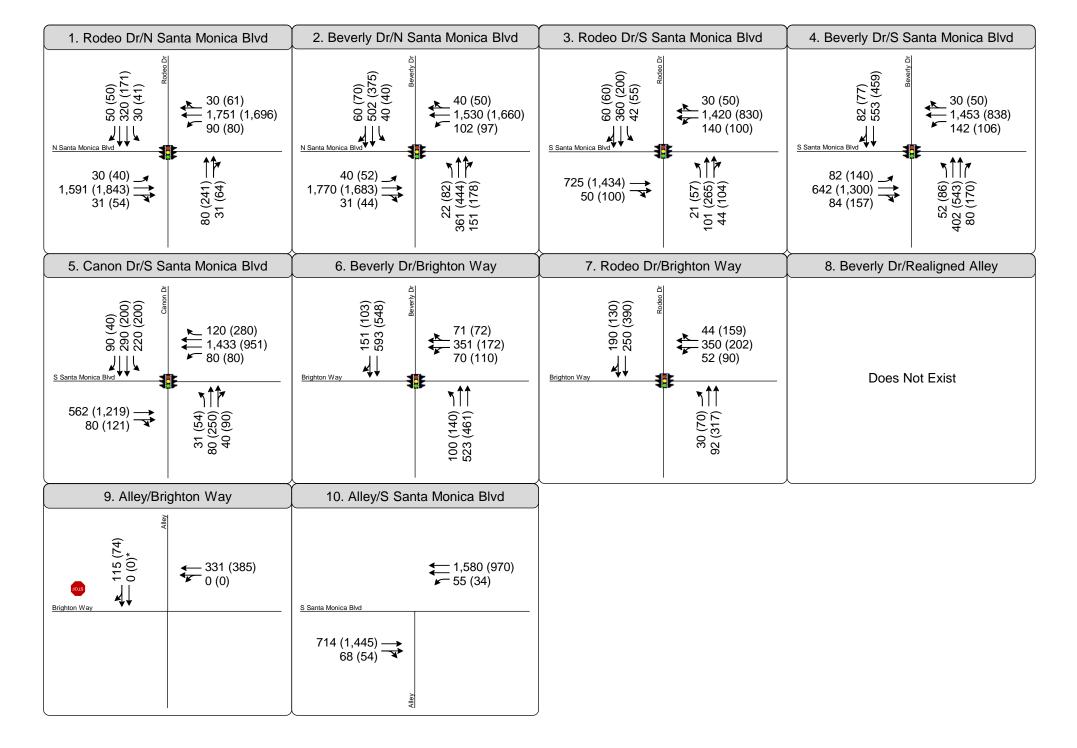
6.3 Comparison of Future Intersection Operations with Existing Uses in Operation

Similar to the comparison of Existing and Existing plus Project conditions described above, the Project's effects on traffic operations reported under Future (2026) conditions compares traffic operations with the Project to Future traffic conditions. The Future (2026) conditions analysis did not account for vehicle-trips being generated by commercial uses on the Project site that are currently vacant. Therefore, an additional traffic operations analysis was completed assuming full occupancy of the existing uses under Future (2026) conditions, referred to as the "Future plus Existing Uses in Operation" scenario. The purpose of this additional scenario is to compare traffic operations with the Cheval Blanc Specific Plan to the historic trip generation of the existing uses on the Project site in addition to planned development projects and ambient growth in the study area under Future (2026) conditions and determine if the Project would exceed the City's criteria for intersection operations.

The vehicle-trips generated from unoccupied uses were added to Future (2026) traffic volume forecasts. The trip assignment was based on the parking location for the existing unoccupied uses and the vehicle trips were routed through each of the study intersections. The traffic volumes for Future plus Existing Uses in Operation are shown on **Figure 10**.

The results of the LOS analysis for Future plus Existing Uses in Operation and Future plus Project conditions are presented in **Table 13** and the corresponding LOS calculation sheets are included in **Appendix B**. When comparing Future plus Existing Uses in Operation to the Future plus Project intersection operations, the increase in vehicle delay is lower at most of the study intersections than the results shown above comparing the Project to Future conditions. As discussed above, three intersections would exceed the City's criteria for signalized intersections when comparing Future plus Project to Future conditions. Under this additional scenario that accounts for full occupancy of the existing commercial uses on the Project site, only one intersection would exceed the City's criteria for signalized intersections, during both peak times. Similar to the results of the Existing plus Project analysis presented above, the intersection that would continue to experience an increase in delay that exceeds the City's criteria is North Beverly Drive/South Santa Monica Boulevard. This intersection would continue to have an increase in average vehicle delay of more than 10 seconds during the AM (LOS E) and PM (LOS E) peak hours, when comparing Future plus Existing Uses in Operation to the Future plus Project intersection operations.





^{*}Data was not available for volumes on the alley south of Brighton Way, so these turning movements are shown 0. No changes to these volumes would occur as a result of the proposed project.

AM (PM) Peak Hour Traffic Volume



Lane Configuration



Stop Sign



Signalized



Figure 10

Peak Hour Traffic Volumes and Lane Configurations -Future (2026) Plus Existing Uses in Operation

Table 13: Future (2026) Plus Existing Uses in Operation and Future Plus Project Intersection Operations

| Intersection | Control | Peak | Future Plus Uses in Op | | Future Plus | Change in Delay | | |
|--|------------|------|---------------------------------|------------------|---------------------------------|--------------------|------------------------|--|
| mersection | Control | Hour | Delay (sec/veh) ¹ | LOS ² | Delay (sec/veh) ¹ | LOS ² | (sec/veh) ³ | |
| 1. N Rodeo Dr/N Santa | Signalized | AM | <u>48.0</u> | <u>D</u> | 49.0 | <u>D</u> | 1.0 | |
| Monica Blvd | Signalized | PM | <u>105.0</u> | <u>E</u> | 108.5 | <u>E</u> | 3.5 | |
| 2. N Beverly Dr/N Santa | Signalized | AM | <u>88.3</u> | <u>F</u> | 92.4 | <u>F</u> | 4.1 | |
| Monica Blvd | Signalized | PM | <u>101.5</u> | <u>F</u> | 102.8 | <u>F</u> | 1.3 | |
| 3. N Rodeo Dr/S Santa | Signalized | AM | <u>98.4</u> | <u>F</u> | 99.3 | <u>F</u> | 0.9 | |
| Monica Blvd ⁴ | Signalized | PM | 43.4 | <u>D</u> | <u>45.3</u> | <u>D</u> | 1.9 | |
| 4. N Beverly Dr/S Santa | Signalized | AM | <u>39.5</u> | <u>D</u> | <u>57.0</u> | <u>E</u> | 17.5 | |
| Monica Blvd | | PM | 46.5 | <u>D</u> | <u>61.3</u> | <u>E</u> | 14.8 | |
| 5. N Cañon Dr/S Santa | Signalized | AM | <u>35.1</u> | <u>D</u> | <u>35.6</u> | <u>D</u> | 0.5 | |
| Monica Blvd | | PM | 23.9 | С | 22.1 | С | -1.8 | |
| C. N. Dadaa Dr/Brighton W. | C: l: d | AM | 11.8 | В | 13.3 | В | 1.5 | |
| 6. N Rodeo Dr/Brighton Wy | Signalized | PM | 12.4 | В | 13.0 | В | 0.6 | |
| 7. N Beverly Dr/Brighton Wy ⁴ | C: I: I | AM | 29.1 | С | 29.2 | С | 0.1 | |
| 7. N beverly DI/Brighton wy | Signalized | PM | 29.3 | С | 29.4 | С | 0.1 | |
| 8. N Beverly Dr/Realigned | ccc | AM | DNE | N/A | 10.2 | В | N/A | |
| Alley | SSSC | PM | DNE | N/A | 16.2 | С | N/A | |
| O. Princhton Mar/Alloy | CCCC | AM | 10.4 | В | 10.5 | В | 0.1 | |
| 9. Brighton Wy/Alley | SSSC | PM | 10 | А | 9.9 | А | -0.1 | |
| 10. Alley (or future Project | CCCC | AM | 10.2 | В | 9.9* | A* | -0.3 | |
| Dwy)/S Santa Monica Blvd | SSSC | PM | 16.6 | С | 19.9* | C* | 3.3 | |

Source: Fehr & Peers, 2021.

Notes:

SSSC indicates Side street stop-controlled intersection.

DNE indicates the intersection does not exist under this scenario.

<u>Underlined</u> text indicates a LOS of D, E, or F.

Bold text indicates that the delay or LOS exceeds the City's criteria as a result of the Project trips.



¹ Whole intersection weighted average stopped delay expressed in seconds per vehicle for signalized intersections. The vehicular delay for the worst movement is reported for the SSSC intersections.

² LOS calculations performed using the *Highway Capacity Manual* 6th Edition (*HCM* 6) method.

³ Unacceptable seconds of delay per vehicle and LOS or increases in seconds of delay per vehicle highlighted in **bold**.

⁴LOS calculations performed using the Highway Capacity Manual 5th Edition method due to signal phasing.

^{*}Operations only on the public roadway approaches are reported.

6.4 Site Access Operations

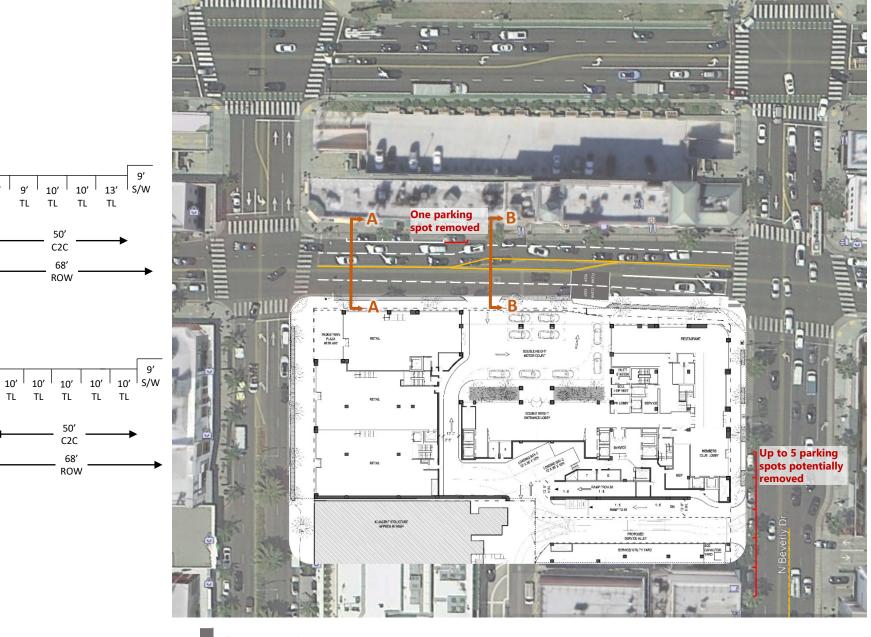
In addition to studying intersection LOS, an evaluation of queueing at the Project access points was also performed. Because static Synchro queue calculations did not appear sensitive to shared versus exclusive turn lanes, a SimTraffic analysis was performed.

For the primary Project access to the motorcourt from South Santa Monica Boulevard, the westbound left-turn from South Santa Monica Boulevard is projected to have a demand of 31 vehicles in the AM peak hour and 88 vehicles in the PM peak hour. Under Future plus Project conditions, the projected 95th percentile queue is approximately 4 vehicles in the AM peak hour and the upstream intersection is blocked 6% of the time. In the PM peak hour the projected 95th percentile queue is approximately 3 vehicles and the upstream intersection is blocked 11% of the time. These queues extend to the upstream intersection because the existing configuration of South Santa Monica Boulevard does not provide storage for westbound left turns into the Project site, and therefore, any queued vehicles would block westbound through traffic. To provide a turn lane into the motor court, the following could be implemented:

• Remove one parking spot from the north side of South Santa Monica Boulevard in order to extend the painted median to the Project motorcourt entrance, as illustrated on **Figure 11**. This would provide a separate storage lane for westbound left-turning vehicles such that westbound through traffic would not be impeded by vehicles waiting to turn. It is noted that the parking spot that would be removed under this alternative site access option was not in operation as of February 2021, when it was observed that a bag had been placed over the meter.

This improvement would result in 95th percentile queues of only approximately 1 vehicle, and the upstream intersection would be blocked 2% of the time during both peak hours. SimTraffic queue summaries are provided in **Appendix D**.

For the secondary Project access to the realigned alley, the northbound left-turn from North Beverly Drive is projected to have a demand of 14 vehicles in the AM peak hour and 9 vehicles in the PM peak hour. Under Future plus Project conditions, the projected 95th percentile queue is only 1 vehicle under both peak hours, indicating that the new alley location is not expected to cause operational issues along North Beverly Drive due to turning vehicles queueing.





North

North

A-A

B-B

S/W

S/W

TL

"KEEP CLEAR" Pavement Striping

Figure 11

Appendix A: Historic Traffic Counts

Table A-1: Historic Count Summary

| | Count Data | | |
|--------|--------------------|------------------------------|------------|
| Number | North/South Street | East/West Street | Count Date |
| 1 | Rodeo Drive | Santa Monica Boulevard North | 10/3/2013 |
| 2 | Beverly Drive | Santa Monica Boulevard North | 12/10/2019 |
| 3 | Rodeo Drive | Santa Monica Boulevard South | Estimated |
| 4 | Beverly Drive | Santa Monica Boulevard South | 9/21/2016 |
| 5 | Canon Drive | Santa Monica Boulevard South | 4/23/2019 |
| 6 | Beverly Drive | Brighton Way | 9/19/2017 |
| 7 | Rodeo Drive | Brighton Way | 8/15/2018 |
| 8 | Beverly Drive | Realligned Alley | Estimated |
| 9 | Existing Alley | Brighton Way | Estimated |
| 10 | Existing Alley | Santa Monica Boulevard South | 5/1/2019 |

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City of Beverly Hills N/S: N. Rodeo Drive

E/W: N. Santa Monica Boulevard

Weather: Sunny

File Name: BVHSMROAM Site Code: 04213393

Start Date : 10/3/2013 Page No : 1

Groups Printed- Total Volume

| | Groups Printed- Total Volume | | | | | | | | | | | | | | | | |
|-------------|--|-------|-------|------------|------|------|-------|------------|--------|---------|---------|------------|----------------|------|-------|------------|------------|
| | N. Santa Monica Boulevard N. Rodeo Drive | | | | | | | N. Sa | nta Mo | nica Bo | ulevard | | N. Rodeo Drive | | | | |
| | | South | bound | | | West | bound | | | North | nbound | | | | | | |
| Start Time | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | Int. Total |
| 07:00 AM | 7 | 394 | 1 | 402 | 0 | 7 | 5 | 12 | 7 | 181 | 1 | 189 | 2 | 38 | 13 | 53 | 656 |
| 07:15 AM | 12 | 470 | 2 | 484 | 0 | 8 | 4 | 12 | 8 | 193 | 2 | 203 | 1 | 37 | 7 | 45 | 744 |
| 07:30 AM | 10 | 471 | 4 | 485 | 0 | 5 | 3 | 8 | 10 | 252 | 8 | 270 | 2 | 46 | 11 | 59 | 822 |
| 07:45 AM | 18 | 437 | 4 | 459 | 0 | 20 | 3 | 23 | 5 | 294 | 1 | 300 | 3 | 78 | 10 | 91 | 873 |
| Total | 47 | 1772 | 11 | 1830 | 0 | 40 | 15 | 55 | 30 | 920 | 12 | 962 | 8 | 199 | 41 | 248 | 3095 |
| | | | | | | | | | | | | | | | | | |
| 08:00 AM | 15 | 386 | 7 | 408 | 0 | 15 | 6 | 21 | 6 | 299 | 4 | 309 | 5 | 53 | 7 | 65 | 803 |
| 08:15 AM | 14 | 351 | 8 | 373 | 0 | 11 | 4 | 15 | 3 | 315 | 6 | 324 | 4 | 67 | 11 | 82 | 794 |
| 08:30 AM | 20 | 363 | 5 | 388 | 0 | 22 | 6 | 28 | 9 | 313 | 6 | 328 | 3 | 81 | 7 | 91 | 835 |
| 08:45 AM | 29 | 340 | 8 | 377 | 0 | 25 | 11 | 36 | 4 | 351 | 9 | 364 | 15 | 90 | 19 | 124 | 901 |
| Total | 78 | 1440 | 28 | 1546 | 0 | 73 | 27 | 100 | 22 | 1278 | 25 | 1325 | 27 | 291 | 44 | 362 | 3333 |
| | | | | | | | | | | | | | | | | | |
| Grand Total | 125 | 3212 | 39 | 3376 | 0 | 113 | 42 | 155 | 52 | 2198 | 37 | 2287 | 35 | 490 | 85 | 610 | 6428 |
| Apprch % | 3.7 | 95.1 | 1.2 | | 0 | 72.9 | 27.1 | | 2.3 | 96.1 | 1.6 | | 5.7 | 80.3 | 13.9 | | |
| Total % | 1.9 | 50 | 0.6 | 52.5 | 0 | 1.8 | 0.7 | 2.4 | 8.0 | 34.2 | 0.6 | 35.6 | 0.5 | 7.6 | 1.3 | 9.5 | |

| | N. Santa Monica Boulevard | | | | | N. Rod | eo Driv | е | N. Santa Monica Boulevard | | | | | N. Rodeo Drive | | | | |
|--|---------------------------|---------|---------|------------|-----------|--------|---------|------------|---------------------------|-------|--------|------------|------|----------------|-------|------------|------------|--|
| | | South | nbound | | Westbound | | | | | North | nbound | | | | | | | |
| Start Time | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | Int. Total | |
| Peak Hour Analysis From 07:00 AM to 08:45 AM - Peak 1 of 1 | | | | | | | | | | | | | | | | | | |
| Peak Hour for E | Entire In | tersect | ion Beg | ins at 08: | MA 00 | | | | | | | | | | | | | |
| 08:00 AM | 15 | 386 | 7 | 408 | 0 | 15 | 6 | 21 | 6 | 299 | 4 | 309 | 5 | 53 | 7 | 65 | 803 | |
| 08:15 AM | 14 | 351 | 8 | 373 | 0 | 11 | 4 | 15 | 3 | 315 | 6 | 324 | 4 | 67 | 11 | 82 | 794 | |
| 08:30 AM | 20 | 363 | 5 | 388 | 0 | 22 | 6 | 28 | 9 | 313 | 6 | 328 | 3 | 81 | 7 | 91 | 835 | |
| 08:45 AM | 29 | 340 | 8 | 377 | 0 | 25 | 11 | 36 | 4 | 351 | 9 | 364 | 15 | 90 | 19 | 124 | 901 | |
| Total Volume | 78 | 1440 | 28 | 1546 | 0 | 73 | 27 | 100 | 22 | 1278 | 25 | 1325 | 27 | 291 | 44 | 362 | 3333 | |
| % App. Total | 5 | 93.1 | 1.8 | | 0 | 73 | 27 | | 1.7 | 96.5 | 1.9 | | 7.5 | 80.4 | 12.2 | | | |
| PHF | .672 | .933 | .875 | .947 | .000 | .730 | .614 | .694 | .611 | .910 | .694 | .910 | .450 | .808 | .579 | .730 | .925 | |

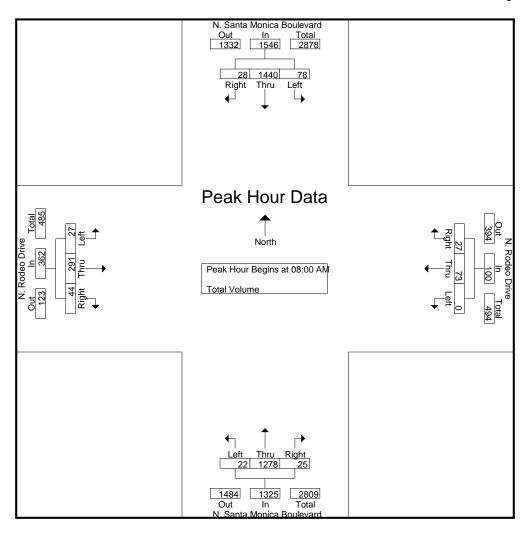
City of Beverly Hills N/S: N. Rodeo Drive

E/W: N. Santa Monica Boulevard

Weather: Sunny

File Name: BVHSMROAM Site Code : 04213393

Start Date : 10/3/2013 Page No : 2



Peak Hour Analysis From 07:00 AM to 08:45 AM - Peak 1 of 1

| Peak Hour for | <u>Each A</u> | pproact | n Begins | s at: | | | | | | | | | | | | |
|---------------|---------------|---------|----------|-------|----------|------|------|------|----------|------|------|------|----------|------|------|------|
| | 07:15 AM | 1 | | | 08:00 AM | 1 | | | 08:00 AN | 1 | | | 08:00 AM | 1 | | |
| +0 mins. | 12 | 470 | 2 | 484 | 0 | 15 | 6 | 21 | 6 | 299 | 4 | 309 | 5 | 53 | 7 | 65 |
| +15 mins. | 10 | 471 | 4 | 485 | 0 | 11 | 4 | 15 | 3 | 315 | 6 | 324 | 4 | 67 | 11 | 82 |
| +30 mins. | 18 | 437 | 4 | 459 | 0 | 22 | 6 | 28 | 9 | 313 | 6 | 328 | 3 | 81 | 7 | 91 |
| +45 mins. | 15 | 386 | 7 | 408 | 0 | 25 | 11 | 36 | 4 | 351 | 9 | 364 | 15 | 90 | 19 | 124 |
| Total Volume | 55 | 1764 | 17 | 1836 | 0 | 73 | 27 | 100 | 22 | 1278 | 25 | 1325 | 27 | 291 | 44 | 362 |
| % App. Total | 3 | 96.1 | 0.9 | | 0 | 73 | 27 | | 1.7 | 96.5 | 1.9 | | 7.5 | 80.4 | 12.2 | |
| PHF | .764 | .936 | .607 | .946 | .000 | .730 | .614 | .694 | .611 | .910 | .694 | .910 | .450 | .808 | .579 | .730 |

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City of Beverly Hills N/S: N. Rodeo Drive

E/W: N. Santa Monica Boulevard

Weather: Sunny

File Name : BVHSMROPM Site Code : 04213393

Start Date : 10/3/2013 Page No : 1

Groups Printed- Total Volume

| | Groups i finited- Total Volume | | | | | | | | | | | | | | | | |
|--------------------|--------------------------------|---------|---------|------------|------|--------|----------|------------|-------|--------|---------|------------|------|--------|----------|------------|------------|
| | N. Sa | nta Moi | nica Bo | ulevard | | N. Rod | leo Driv | 'e | N. Sa | nta Mo | nica Bo | ulevard | | N. Roc | leo Driv | е | |
| | | South | nbound | | | West | bound | | | North | bound | | | East | bound | | |
| Start Time | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | Int. Total |
| 04:00 PM | 31 | 321 | 19 | 371 | 3 | 48 | 16 | 67 | 6 | 340 | 13 | 359 | 7 | 46 | 17 | 70 | 867 |
| 04:15 PM | 20 | 340 | 12 | 372 | 0 | 42 | 11 | 53 | 11 | 349 | 13 | 373 | 9 | 34 | 11 | 54 | 852 |
| 04:30 PM | 18 | 312 | 13 | 343 | 0 | 44 | 14 | 58 | 13 | 370 | 12 | 395 | 7 | 37 | 15 | 59 | 855 |
| 04:45 PM | 15 | 280 | 9 | 304 | 0 | 56 | 16 | 72 | 10 | 325 | 16 | 351 | 4 | 31 | 8 | 43 | 770 |
| Total | 84 | 1253 | 53 | 1390 | 3 | 190 | 57 | 250 | 40 | 1384 | 54 | 1478 | 27 | 148 | 51 | 226 | 3344 |
| | | | | | | | | | | | | | | | | | |
| 05:00 PM | 19 | 297 | 16 | 332 | 2 | 61 | 12 | 75 | 8 | 381 | 9 | 398 | 5 | 48 | 9 | 62 | 867 |
| 05:15 PM | 19 | 323 | 8 | 350 | 0 | 57 | 17 | 74 | 10 | 340 | 15 | 365 | 8 | 41 | 13 | 62 | 851 |
| 05:30 PM | 18 | 332 | 12 | 362 | 0 | 62 | 15 | 77 | 11 | 345 | 7 | 363 | 10 | 36 | 13 | 59 | 861 |
| 05:45 PM | 15 | 358 | 11 | 384 | 1 | 41 | 8 | 50 | 5 | 358 | 10 | 373 | 6 | 31 | 6 | 43 | 850 |
| Total | 71 | 1310 | 47 | 1428 | 3 | 221 | 52 | 276 | 34 | 1424 | 41 | 1499 | 29 | 156 | 41 | 226 | 3429 |
| | | | | | | | | | | | | | | | | | |
| Grand Total | 155 | 2563 | 100 | 2818 | 6 | 411 | 109 | 526 | 74 | 2808 | 95 | 2977 | 56 | 304 | 92 | 452 | 6773 |
| Apprch % | 5.5 | 91 | 3.5 | | 1.1 | 78.1 | 20.7 | | 2.5 | 94.3 | 3.2 | | 12.4 | 67.3 | 20.4 | | |
| Total % | 2.3 | 37.8 | 1.5 | 41.6 | 0.1 | 6.1 | 1.6 | 7.8 | 1.1 | 41.5 | 1.4 | 44 | 0.8 | 4.5 | 1.4 | 6.7 | |

| | N. Sa | nta Moi | nica Boi | ulevard | | N. Rod | leo Driv | е | N. Sa | nta Mo | nica Bo | ulevard | | N. Roc | leo Driv | е | |
|-----------------|-----------|----------|----------|-------------|---------|----------|----------|------------|-------|--------|---------|------------|------|--------|----------|------------|------------|
| | | South | nbound | | | West | tbound | | | North | nbound | | | East | bound | | |
| Start Time | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | Int. Total |
| Peak Hour Ana | alysis Fr | om 04:0 | 00 PM to | o 05:45 P | M - Pea | k 1 of 1 | | | | | _ | | | | _ | | |
| Peak Hour for I | Entire Ir | ntersect | ion Beg | ins at 05:0 | 00 PM | | | | | | | | | | | | |
| 05:00 PM | 19 | 297 | 16 | 332 | 2 | 61 | 12 | 75 | 8 | 381 | 9 | 398 | 5 | 48 | 9 | 62 | 867 |
| 05:15 PM | 19 | 323 | 8 | 350 | 0 | 57 | 17 | 74 | 10 | 340 | 15 | 365 | 8 | 41 | 13 | 62 | 851 |
| 05:30 PM | 18 | 332 | 12 | 362 | 0 | 62 | 15 | 77 | 11 | 345 | 7 | 363 | 10 | 36 | 13 | 59 | 861 |
| 05:45 PM | 15 | 358 | 11 | 384 | 1 | 41 | 8 | 50 | 5 | 358 | 10 | 373 | 6 | 31 | 6 | 43 | 850_ |
| Total Volume | 71 | 1310 | 47 | 1428 | 3 | 221 | 52 | 276 | 34 | 1424 | 41 | 1499 | 29 | 156 | 41 | 226 | 3429 |
| % App. Total | 5 | 91.7 | 3.3 | | 1.1 | 80.1 | 18.8 | | 2.3 | 95 | 2.7 | | 12.8 | 69 | 18.1 | | |
| PHF | .934 | .915 | .734 | .930 | .375 | .891 | .765 | .896 | .773 | .934 | .683 | .942 | .725 | .813 | .788 | .911 | .989 |

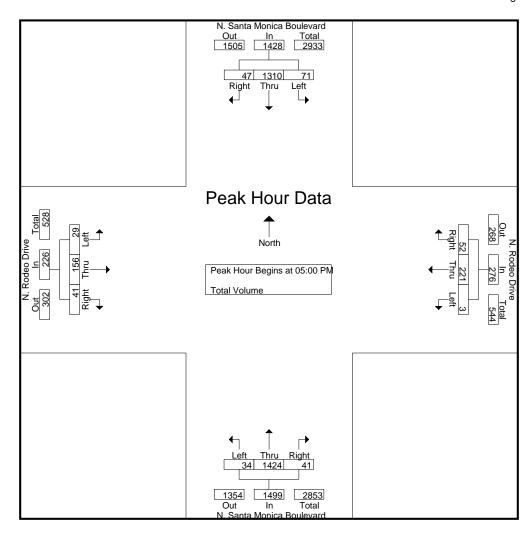
City of Beverly Hills N/S: N. Rodeo Drive

E/W: N. Santa Monica Boulevard

Weather: Sunny

File Name: BVHSMROPM Site Code: 04213393 Start Date: 10/3/2013

Page No : 2



Peak Hour Analysis From 04:00 PM to 05:45 PM - Peak 1 of 1

Peak Hour for Each Approach Begins at: 05:00 PM 04:45 PM 04:15 PM 04:00 PM +0 mins. +15 mins. +30 mins. +45 mins. Total Volume % App. Total 91.7 3.3 0.7 79.2 20.1 2.8 93.9 3.3 11.9 65.5 22.6 .930 .968 .953 .807 PHF .934 .915 .734 .250 .952 .882 .808 .935 .781 .750 .804 .750

Location: Beverly Hills

N/S: E/W: N. Santa Monica Boulevard

Rodeo Drive



Date: 10/3/2013 File: BVHSMRO

PEDESTRIANS

| | North Leg N. Santa Monica Boulevard | East Leg Rodeo Drive | South Leg N. Santa Monica Boulevard | West Leg Rodeo Drive | |
|----------------|--|-------------------------|--|-------------------------|-------|
| | Pedestrians | Pedestrians | Pedestrians | Pedestrians | TOTAL |
| 7:00 AM | 1 | 0 | 1 | 2 | 4 |
| 7:15 AM | 2 | 0 | 0 | 7 | 9 |
| 7:30 AM | 4 | 0 | 3 | 8 | 15 |
| 7:45 AM | 1 | 0 | 0 | 2 | 3 |
| 8:00 AM | 2 | 0 | 1 | 4 | 7 |
| 8:15 AM | 1 | 0 | 4 | 10 | 15 |
| 8:30 AM | 3 | 3 | 1 | 8 | 15 |
| 8:45 AM | 5 | 3 | 1 | 7 | 16 |
| TOTAL VOLUMES: | 19 | 6 | 11 | 48 | 84 |

| | North Leg N. Santa Monica Boulevard | East Leg Rodeo Drive | South Leg N. Santa Monica Boulevard | West Leg Rodeo Drive | |
|----------------|--|-------------------------|--|-------------------------|-------|
| | Pedestrians | Pedestrians | Pedestrians | Pedestrians | TOTAL |
| 4:00 PM | 14 | 1 | 10 | 4 | 29 |
| 4:15 PM | 25 | 12 | 14 | 5 | 56 |
| 4:30 PM | 15 | 7 | 9 | 9 | 40 |
| 4:45 PM | 26 | 7 | 8 | 7 | 48 |
| 5:00 PM | 14 | 4 | 6 | 6 | 30 |
| 5:15 PM | 18 | 8 | 7 | 10 | 43 |
| 5:30 PM | 15 | 9 | 2 | 4 | 30 |
| 5:45 PM | 26 | 1 | 6 | 10 | 43 |
| TOTAL VOLUMES: | 153 | 49 | 62 | 55 | 319 |

Location: Beverly Hills

N/S: E/W: N. Santa Monica Boulevard

Rodeo Drive



Date: 10/3/2013 File: BVHSMRO

BICYCLES

| | North Leg N. Santa Monica Boulevard | East Leg Rodeo Drive | South Leg N. Santa Monica Boulevard | West Leg Rodeo Drive | |
|----------------|--|-------------------------|--|-------------------------|-------|
| | Bicycles | Bicycles | Bicycles | Bicycles | TOTAL |
| 7:00 AM | 0 | 2 | 2 | 1 | 5 |
| 7:15 AM | 0 | 1 | 1 | 4 | 6 |
| 7:30 AM | 0 | 0 | 1 | 3 | 4 |
| 7:45 AM | 0 | 0 | 0 | 7 | 7 |
| 8:00 AM | 0 | 0 | 0 | 4 | 4 |
| 8:15 AM | 0 | 0 | 0 | 7 | 7 |
| 8:30 AM | 0 | 0 | 0 | 4 | 4 |
| 8:45 AM | 0 | 0 | 1 | 5 | 6 |
| TOTAL VOLUMES: | 0 | 3 | 5 | 35 | 43 |

| | North Leg N. Santa Monica Boulevard | East Leg Rodeo Drive | South Leg N. Santa Monica Boulevard | West Leg Rodeo Drive | |
|----------------|--|-------------------------|--|-------------------------|-------|
| | Bicycles | Bicycles | Bicycles | Bicycles | TOTAL |
| 4:00 PM | 0 | 1 | 0 | 1 | 2 |
| 4:15 PM | 0 | 1 | 0 | 1 | 2 |
| 4:30 PM | 1 | 1 | 0 | 0 | 2 |
| 4:45 PM | 1 | 4 | 0 | 2 | 7 |
| 5:00 PM | 2 | 1 | 0 | 1 | 4 |
| 5:15 PM | 0 | 0 | 0 | 0 | 0 |
| 5:30 PM | 0 | 4 | 0 | 2 | 6 |
| 5:45 PM | 1 | 3 | 0 | 3 | 7 |
| TOTAL VOLUMES: | 5 | 15 | 0 | 10 | 30 |

Turning Movement Count Report AM

Location ID: 1

North/South: N Beverly Dr Date: 12/10/19

East/West: N Santa Monica Blvd City: Beverly Hills, CA

| | 9 | Southbound | d | ı | Nestbound | 1 | / | Northbound | d | | Eastbound | | |
|----------------|------|------------|----|----|-----------|-----|-----|------------|----|----|-----------|----|---------|
| | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | Totals: |
| Movements: | R | Т | L | R | Т | L | R | Т | L | R | Т | L | Totals. |
| 7:00 | 24 | 75 | 3 | 6 | 379 | 12 | 23 | 47 | 1 | 0 | 195 | 7 | 772 |
| 7:15 | 18 | 82 | 4 | 2 | 374 | 32 | 19 | 58 | 2 | 5 | 265 | 8 | 869 |
| 7:30 | 15 | 83 | 8 | 7 | 368 | 19 | 25 | 52 | 3 | 3 | 277 | 8 | 868 |
| 7:45 | 9 | 85 | 5 | 6 | 354 | 20 | 28 | 80 | 5 | 5 | 351 | 14 | 962 |
| 8:00 | 13 | 100 | 4 | 6 | 258 | 23 | 37 | 77 | 3 | 5 | 379 | 11 | 916 |
| 8:15 | 15 | 121 | 3 | 10 | 345 | 20 | 31 | 76 | 6 | 8 | 367 | 10 | 1012 |
| 8:30 | 14 | 116 | 6 | 8 | 329 | 22 | 36 | 87 | 5 | 3 | 366 | 13 | 1005 |
| 8:45 | 15 | 135 | 8 | 12 | 338 | 26 | 39 | 99 | 4 | 9 | 379 | 3 | 1067 |
| | | | | | | | | | | | | | |
| Total Volume: | 123 | 797 | 41 | 57 | 2745 | 174 | 238 | 576 | 29 | 38 | 2579 | 74 | 7471 |
| Approach % | 13% | 83% | 4% | 2% | 92% | 6% | 28% | 68% | 3% | 1% | 96% | 3% | |
| | | • | | | | | | | | | | | |
| Peak Hr Begin: | 8:00 | | | | | | | | | | | | |
| PHV | 57 | 472 | 21 | 36 | 1270 | 91 | 143 | 339 | 18 | 25 | 1491 | 37 | 4000 |
| PHF | | 0.870 | | | 0.929 | | | 0.880 | | | 0.983 | | 0.937 |

Turning Movement Count Report PM

Location ID: 1

North/South: N Beverly Dr Date: 12/10/19

East/West: N Santa Monica Blvd City: Beverly Hills, CA

| | 9 | Southbound | d | | Westbound | 1 | 1 | Northbound | d | | Eastbound | 1 | |
|------------|----|------------|----|----|-----------|----|----|------------|----|----|-----------|----|---------|
| | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | Totals: |
| Movements: | R | T | L | R | Т | L | R | Т | L | R | T | L | Totals. |
| 16:00 | 22 | 86 | 9 | 4 | 302 | 23 | 42 | 91 | 22 | 9 | 330 | 6 | 946 |
| 16:15 | 12 | 99 | 12 | 13 | 311 | 16 | 45 | 88 | 15 | 9 | 322 | 6 | 948 |
| 16:30 | 16 | 97 | 9 | 9 | 321 | 23 | 51 | 88 | 12 | 6 | 286 | 3 | 921 |
| 16:45 | 12 | 84 | 5 | 8 | 286 | 27 | 41 | 77 | 12 | 8 | 338 | 5 | 903 |
| 17:00 | 17 | 88 | 8 | 9 | 326 | 19 | 41 | 112 | 17 | 11 | 348 | 13 | 1009 |
| 17:15 | 12 | 80 | 8 | 8 | 315 | 18 | 31 | 116 | 19 | 7 | 327 | 18 | 959 |
| 17:30 | 19 | 78 | 10 | 12 | 358 | 22 | 46 | 114 | 15 | 8 | 320 | 9 | 1011 |
| 17:45 | 15 | 105 | 10 | 3 | 328 | 19 | 41 | 80 | 16 | 12 | 320 | 5 | 954 |
| | | | | | | | | | | | | | |
| | | | | | | | | | | | | | |

| Total Volume: | 125 | 717 | 71 | 66 | 2547 | 167 | 338 | 766 | 128 | 70 | 2591 | 65 | 7651 |
|---------------|-----|-----|----|----|------|-----|-----|-----|-----|----|------|----|------|
| Approach % | 14% | 79% | 8% | 2% | 92% | 6% | 27% | 62% | 10% | 3% | 95% | 2% | |

| Peak Hr Begin: | 17:00 | | | | | | | | | | | | |
|----------------|-------|-------|----|----|-------|----|-----|-------|----|----|-------|----|-------|
| PHV | 63 | 351 | 36 | 32 | 1327 | 78 | 159 | 422 | 67 | 38 | 1315 | 45 | 3933 |
| PHF | | 0.865 | | | 0.916 | | | 0.926 | | | 0.940 | | 0.973 |

Pedestrian/Bicycle Count Report

Location ID: 1

North/South: N Beverly Dr Date: 12/10/19

East/West: N Santa Monica Blvd City: Beverly Hills, CA

| Leg: | No | rth | Ec | ast | So | uth | W | est |
|--------|------|---------|------|---------|------|---------|------|---------|
| Class: | Peds | Bicycle | Peds | Bicycle | Peds | Bicycle | Peds | Bicycle |
| 7:00 | 3 | 0 | 1 | 0 | 6 | 0 | 0 | 0 |
| 7:15 | 6 | 0 | 4 | 0 | 8 | 0 | 1 | 0 |
| 7:30 | 5 | 0 | 2 | 0 | 11 | 0 | 4 | 0 |
| 7:45 | 3 | 1 | 1 | 0 | 4 | 0 | 1 | 0 |
| 8:00 | 11 | 0 | 8 | 0 | 8 | 0 | 0 | 0 |
| 8:15 | 5 | 1 | 3 | 0 | 7 | 0 | 0 | 0 |
| 8:30 | 9 | 0 | 1 | 0 | 9 | 0 | 5 | 0 |
| 8:45 | 13 | 0 | 4 | 1 | 9 | 0 | 5 | 0 |
| 11:00 | 19 | 0 | 0 | 0 | 10 | 0 | 6 | 0 |
| 11:15 | 16 | 0 | 5 | 0 | 4 | 0 | 10 | 1 |
| 11:30 | 25 | 0 | 11 | 0 | 8 | 0 | 8 | 0 |
| 11:45 | 46 | 0 | 5 | 0 | 8 | 1 | 20 | 0 |
| 12:00 | 17 | 0 | 10 | 0 | 7 | 0 | 11 | 0 |
| 12:15 | 35 | 1 | 1 | 0 | 5 | 0 | 8 | 0 |
| 12:30 | 23 | 1 | 10 | 1 | 3 | 0 | 4 | 0 |
| 12:45 | 29 | 1 | 21 | 0 | 10 | 0 | 12 | 0 |
| 1:00 | 44 | 0 | 18 | 0 | 12 | 0 | 12 | 0 |
| 1:15 | 24 | 0 | 14 | 0 | 15 | 0 | 12 | 0 |
| 1:30 | 29 | 2 | 18 | 1 | 13 | 0 | 12 | 1 |
| 1:45 | 20 | 0 | 10 | 0 | 9 | 1 | 8 | 0 |
| 7:00 | 29 | 0 | 10 | 0 | 15 | 0 | 9 | 1 |
| 7:15 | 25 | 0 | 8 | 0 | 6 | 1 | 7 | 1 |
| 7:30 | 18 | 0 | 12 | 0 | 7 | 0 | 9 | 0 |
| 7:45 | 12 | 0 | 6 | 0 | 12 | 1 | 9 | 0 |
| 8:00 | 7 | 0 | 8 | 0 | 8 | 1 | 8 | 0 |
| 8:15 | 13 | 0 | 10 | 0 | 7 | 0 | 6 | 0 |
| 8:30 | 13 | 0 | 3 | 0 | 5 | 0 | 8 | 0 |
| 8:45 | 4 | 0 | 4 | 0 | 6 | 0 | 1 | 0 |

Intersection Turning Movement Prepared by:

National Data & Surveying Services

Day: Wednesday **Project ID:** 16-5573-003

City: Beverly Hills

Date: 9/21/2016

| | City. D | everiy riilis | | | | | AN | 1 | | | | Date. | 7/21/2010 | | | | | |
|---|---------------------|---------------|------------|-----------|---------|------------|-----------|---------|------------|---------|---------|------------|-----------|-------|----|-----|------|----|
| | NS/EW Streets: | Santa | Monica Blv | ∕d S | Santa | Monica Blv | d S | E | Beverly Dr | | ŀ | Beverly Dr | | | | | | |
| _ | | NO | ORTHBOUN | D | S | OUTHBOUN | D | E | ASTBOUND |) | V | VESTBOUND |) | | | UTU | JRNS | |
| | LANES: | NL 1 | NT 1.5 | NR 0.5 | SL 1 | ST 1.5 | SR 0.5 | EL 0 | ET 2 | ER 0 | WL 1 | WT | WR | TOTAL | NB | SB | EB | WB |
| | | | | | | | 0.5 | | | | | | | | | | | |
| | 7:00 AM | 5 | 61 | 17 | 21 | 196 | 2 | 0 | 66 | 15 | 10 | 49 | 6 | 448 | 0 | 0 | 0 | 0 |
| | 7:15 AM | 10 | 58 | 14 | 21 | 307 | 4 | 0 | 85 | 20 | 8 | 63 | 14 | 604 | 0 | 0 | 0 | 1 |
| | 7:30 AM | 11 | 89 | 17 | 34 | 350 | 12 | 0 | 95 | 24 | 6 | 65 | 17 | 720 | 0 | 0 | 0 | 0 |
| | 7:45 AM | 11 | 121 | 13 | 36 | 258 | 11 | 0 | 119 | 28 | 18 | 75 | 26 | 716 | 0 | 0 | 0 | 0 |
| | 8:00 AM | 25 | 153 | 13 | 32 | 313 | 4 | 0 | 111 | 11 | 13 | 94 | 18 | 787 | 0 | 0 | 0 | 0 |
| | 8:15 AM | 17 | 114 | 18 | 19 | 395 | 5 | 0 | 108 | 33 | 13 | 102 | 14 | 838 | 0 | 0 | 0 | 0 |
| | 8:30 AM | 18 | 129 | 21 | 32 | 327 | 4 | 0 | 138 | 15 | 11 | 72 | 13 | 780 | 0 | 0 | 0 | 0 |
| | 8:45 AM | 13 | 145 | 20 | 44 | 316 | 8 | 0 | 159 | 15 | 10 | 105 | 24 | 859 | 0 | 0 | 0 | 0 |
| | | NL | NT | NR | SL | ST | SR | EL | ET | ER | WL | WT | WR | TOTAL | NB | SB | EB | WB |
| | TOTAL VOLUMES: | 110 | 870 | 133 | 239 | 2462 | 50 | 0 | 881 | 161 | 89 | 625 | 132 | 5752 | 0 | 0 | 0 | 1 |
| | APPROACH %'s: | 9.88% | 78.17% | 11.95% | 8.69% | 89.49% | 1.82% | 0.00% | 84.55% | 15.45% | 10.52% | 73.88% | 15.60% | ļ | | Ī | Ī | |
| P | EAK HR START TIME : | 800 A | M | | | | | | | | | | | TOTAL | | | | |
| | PEAK HR VOL: | 73 | 541 | 72 | 127 | 1351 | 21 | 0 | 516 | 74 | 47 | 373 | 69 | 3264 | | | | |
| | PEAK HR FACTOR: | | 0.898 | | | 0.894 | | | 0.848 | | | 0.879 | | 0.950 | | | | |

CONTROL: Signalized

Intersection Turning Movement Prepared by:

National Data & Surveying Services

Day: Wednesday **Project ID:** 16-5573-003

PΜ

City: Beverly Hills

Date: 9/21/2016

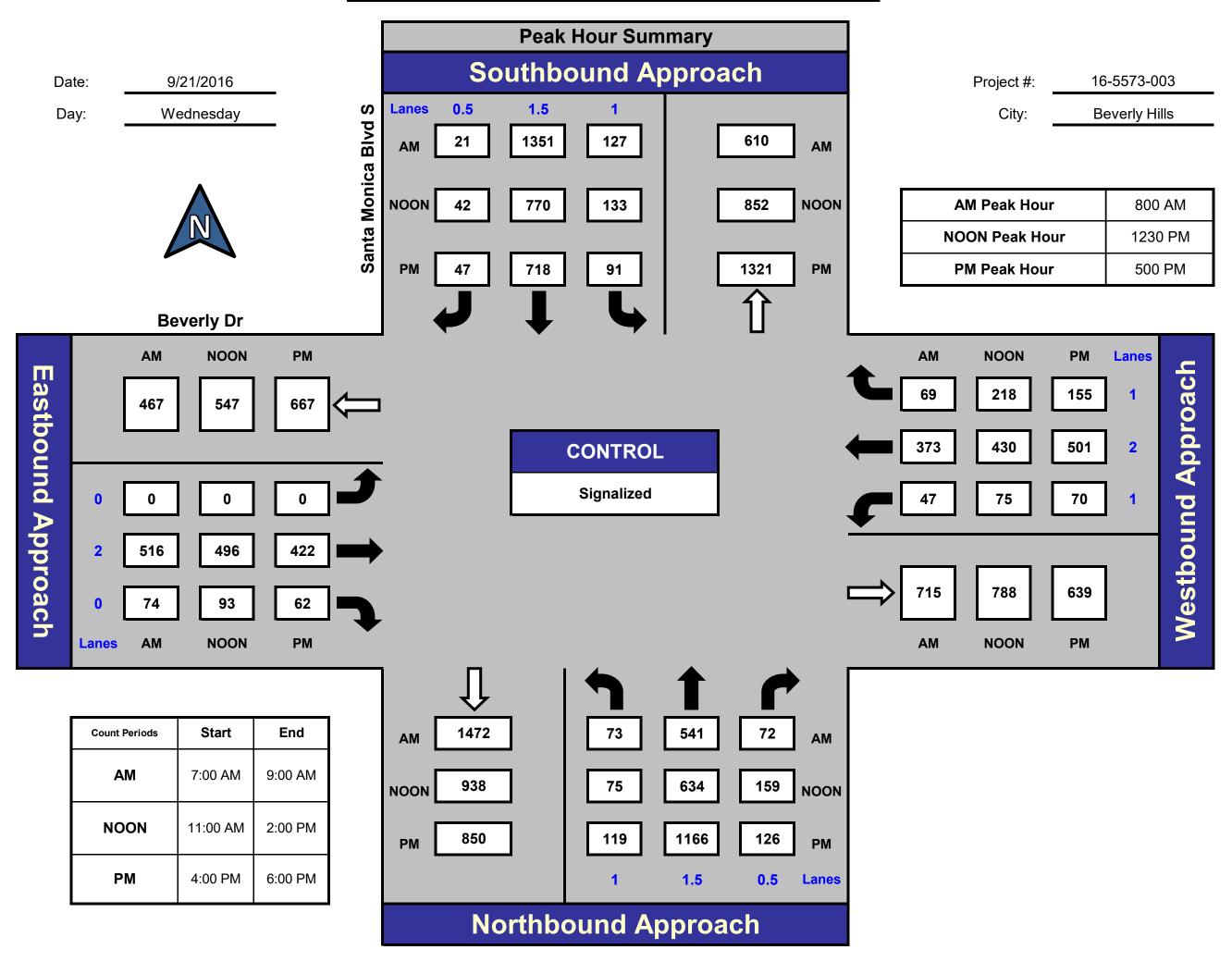
| NS/EW Streets: | Santa | Monica Blv | rd S | Santa | Monica Blv | d S | i | Beverly Dr | | | Beverly Dr | | | | | | |
|--|--|--|--|--|--|---|----------------------------|--|---|--|--|--|--|----------------------------|----------------------------|----------------------------|----------------------------|
| | N | ORTHBOUN | D | S | OUTHBOUND | D | E | ASTBOUND |) | V | VESTBOUND |) | | | UT | URNS | |
| LANES: | NL 1 | NT 1.5 | NR 0.5 | SL 1 | ST 1.5 | SR 0.5 | EL 0 | ET 2 | ER 0 | WL 1 | WT 2 | WR 1 | TOTAL | NB | SB | ЕВ | WB |
| 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:45 PM | 22 36 28 26 28 24 26 41 | 259 220 298 281 286 286 282 312 | 42 42 31 22 36 31 32 27 | 26 24 24 24 20 26 22 23 | 174 186 172 181 175 165 193 185 | 4 7 8 2 9 13 11 14 | 0 0 0 0 0 0 | 111 96 127 97 95 106 95 126 | 8 14 12 18 19 12 13 18 | 19 21 15 18 21 15 15 | 134 100 127 135 132 125 123 121 | 38 36 46 33 41 39 42 33 | 837 782 888 837 862 842 854 919 | 0 0 0 0 0 0 | 0 0 0 0 0 0 | 0 0 0 0 0 0 | 0 0 0 0 0 0 |
| TOTAL VOLUMES : APPROACH %'s : | NL 231 8.50% | NT 2224 81.82% | NR 263 9.68% | SL 189 11.20% | ST 1431 84.77% | SR 68 4.03% | EL 0 0.00% | ET 853 88.21% | ER 114 11.79% | WL 143 9.88% | WT 997 68.85% | WR 308 21.27% | TOTAL 6821 | NB 0 | SB 0 | EB 0 | WB 0 |
| PEAK HR START TIME : PEAK HR VOL : | 119 | PM 1166 | 126 | 91 | 718 | 47 | 0 | 422 | 62 | 70 | 501 | 155 | TOTAL 3477 | | | | |
| PEAK HR FACTOR : | | 0.928 | | | 0.947 | | | 0.840 | | | 0.936 | | 0.946 | | | | |

CONTROL: Signalized

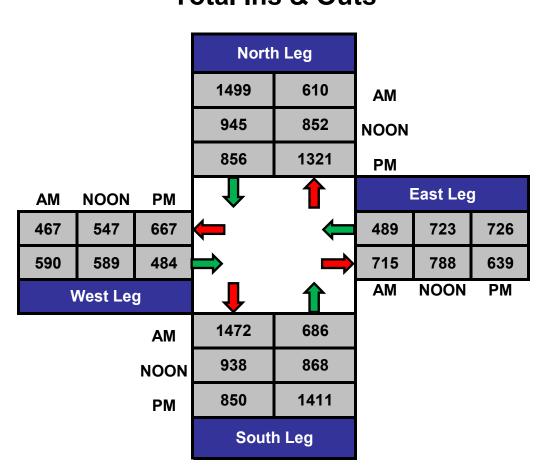
ITM Peak Hour Summary



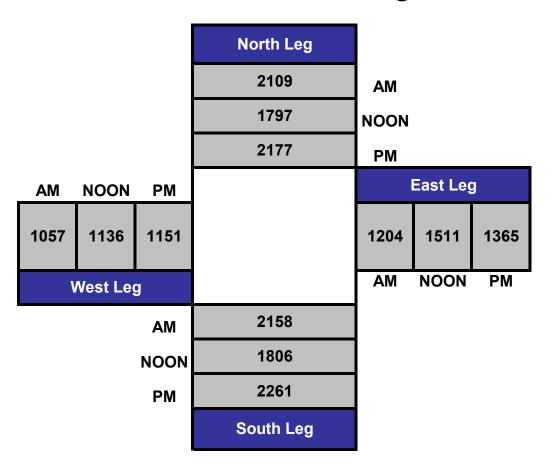
Santa Monica Blvd S and Beverly Dr , Beverly Hills



Total Ins & Outs



Total Volume Per Leg



Intersection Turning Movement Count Location: N Canon Dr & S Santa Monica Blvd City Paradictivity

6:15 PM

6:30 PM

6:45 PM

TOTAL VOLUMES:

APPROACH %'s:

PEAK HR VOL:

PEAK HR FACTOR :

PEAK HR:

50

NT

860

232

0.935

05:30 PM - 06:30 PM

0.882

12.82% 60.27%

183

48

0.857

28

NR

383

26.84%

86

0.741

NU

0.07%

1

0.250

City: Beverly Hills **Project ID:** Historical **Date:** 4/23/2019 **Control:** Signalized

| Control: S | Signalized | | | | | | | | | | | | | Date: 4 | 4/23/2019 | | |
|------------------|------------|---------------|-------------|---------|---------|---------------|-------------|----------------------|---------|---------------|-------------|---------|----------------------|----------------------|-------------|----------------------|-------|
| _ | | | | | | | | To | tal | | | | | | | | _ |
| NS/EW Streets: | | N Cand | on Dr | | | N Cano | on Dr | | | S Santa Mo | nica Blvd | | | S Santa Mo | nica Blvd | | |
| | | NORTH | BOUND | | | SOUTH | BOUND | | | EASTB | OUND | | | WESTE | BOUND | | |
| AM | 1 NL | 1.5 NT | 0.5 NR | 0 NU | 1 SL | 2 ST | 1 SR | <mark>0</mark> SU | 0 EL | 2 ET | 0 ER | 0 EU | <mark>1</mark> WL | <mark>2</mark> WT | 1 WR | <mark>0</mark> WU | TOTAL |
| 7:00 AM | 3 | 11 | 7 | 0 | 29 | 23 | 10 | 0 | 0 | 48 | 12 | 0 | 9 | 249 | 26 | 0 | 427 |
| 7:15 AM | 2 | 12 | 4 | 0 | 44 | 30 | 16 | 0 | 0 | 65 | 14 | 0 | 7 | 310 | 40 | 0 | 544 |
| 7:30 AM | 2 | 17 | 4 | 0 | 35 | 41 | 11 | 0 | 0 | 85 | 4 | 0 | 12 | 367 | 35 | 0 | 613 |
| 7:45 AM | 2 | 13 | 7 | 0 | 36 | 49 | 16 | 0 | 0 | 126 | 11 | 0 | 12 | 330 | 39 | 0 | 641 |
| 8:00 AM | 3 | 8 | 11 | 0 | 44 | 36 | 14 | 0 | 1 | 110 | 13 | 0 | 20 | 283 | 24 | 0 | 567 |
| 8:15 AM | 7 | 16 | 10 | 0 | 45 | 43 | 19 | 0 | 1 | 105 | 13 | 0 | 11 | 310 | 34 | 0 | 614 |
| 8:30 AM | 5 | 19 | 3 | 0 | 45 | 74 | 21 | 0 | 0 | 100 | 12 | 0 | 19 | 357 | 23 | 0 | 678 |
| 8:45 AM | 6 | 13 | 10 | 0 | 59 | <u>59</u> | 19 | 0 | 0 | 115 | 9 | 0 | 19 | 356 | 39 | 0 | 704 |
| 9:00 AM | 8 | 19 | 7 | 0 | 51 | 67 | 23 | 0 | 0 | 121 | 23 | 0 | 20 | 326 | 26 | 0 | 691 |
| 9:15 AM | 3 | 18 | 13 | 0 | 57 | 73 | 22 | 0 | 1 | 145 | 16 | 0 | 18 | 311 | 25 | 0 | 702 |
| 9:30 AM | 3 | 28 | 17 | 0 | 42 | 77 | 14 | 0 | 1 | 132 | 27 | 0 | 16 | 256 | 25 | 0 | 638 |
| 9:45 AM | 8 | 22 | 12 | 0 | 59 | 70 | 25 | 0 | 3 | 138 | 23 | 0 | 15 | 247 | 25 | 0 | 647 |
| | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| TOTAL VOLUMES : | 52 | 196 | 105 | 0 | 546 | 642 | 210 | 0 | 7 | 1290 | 177 | 0 | 178 | 3702 | 361 | 0 | 7466 |
| APPROACH %'s: | 14.73% | 55.52% | 29.75% | 0.00% | 39.06% | 45.92% | 15.02% | 0.00% | 0.47% | 87.52% | 12.01% | 0.00% | 4.20% | 87.29% | 8.51% | 0.00% | |
| PEAK HR : | | 08:30 AM - | | | | | | | | | | | | | | | TOTAL |
| PEAK HR VOL : | 22 | 69 | 33 | 0 | 212 | 273 | 85 | 0 | 1 | 481 | 60 | 0 | 76 | 1350 | 113 | 0 | 2775 |
| PEAK HR FACTOR : | 0.688 | 0.908 0.91 | 0.635 12 | 0.000 | 0.898 | 0.922 0.93 | 0.924 38 | 0.000 | 0.250 | 0.829 0.83 | 0.652 36 | 0.000 | 0.950 | 0.945 0.92 | 0.724 29 | 0.000 | 0.985 |
| " | | | | | | | | | | | | | | | | | |
| DNA | 4 | NORTH | | 0 | 4 | SOUTH | BOUND | 0 | 0 | EASTB | OUND | 0 | 4 | WESTE | BOUND | 0 | |
| PM | NL | 1.5 NT | 0.5 NR | 0 NU | SL | ST | SR | 0 SU | 0 EL | ET | ER | 0 EU | WL | WT | WR | WU | TOTAL |
| 3:00 PM | 11 | 58 | 34 | 0 | 52 | 50 | 11 | 0 | 1 | 228 | 27 | 0 | 25 | 204 | 40 | 0 | 741 |
| 3:15 PM | 13 | 50 | 19 | 0 | 59 | 54 | 7 | 0 | 0 | 257 | 36 | 0 | 15 | 215 | 48 | 0 | 773 |
| 3:30 PM | 6 | 49 | 19 | 0 | 45 | 43 | 11 | 0 | 2 | 253 | 20 | 0 | 17 | 206 | 47 | 0 | 718 |
| 3:45 PM | 9 | 34 | 19 | 0 | 52 | 45 | 8 | 0 | 2 | 234 | 22 | 0 | 25 | 224 | 38 | 0 | 712 |
| 4:00 PM | 11 | 55 | 36 | 0 | 53 | 47 | 12 | 0 | 1 | 258 | 30 | 0 | 14 | 205 | 46 | 0 | 768 |
| 4:15 PM | 9 | 52 | 15 | 0 | 57 | 48 | 9 | 0 | 0 | 233 | 29 | 0 | 13 | 207 | 53 | 0 | 725 |
| 4:30 PM | 13 | 50 | 29 | 0 | 50 | 50 | 13 | 0 | 0 | 255 | 19 | 0 | 17 | 181 | 55 | 0 | 732 |
| 4:45 PM | 17 | 65 | 24 | 0 | 48 | 56 | 12 | 0 | 2 | 268 | 32 | 0 | 14 | 202 | 62 | 0 | 802 |
| 5:00 PM | 9 | 63 | 24 | 0 | 40 | 36 | 6 | 0 | 0 | 280 | 20 | 0 | 16 | 199 | 52 | 0 | 745 |
| 5:15 PM | 10 | 49 | 29 | 0 | 47 | 52 | 6 | 0 | 1 | 286 | 18 | 0 | 11 | 223 | 65 | 0 | 797 |
| 5:30 PM | 9 | 62 | 24 | 0 | 48 | 41 | 10 | 0 | 0 | 260 | 23 | 0 | 15 | 227 | 76 | 0 | 795 |
| 5:45 PM | 11 | 57 | 12 | 1 | 48 | 56 | 7 | 0 | 0 | 268 | 23 | 0 | 22 | 195 | 51 | 0 | 751 |
| 6.00 DM | 1 / | <i>C</i> 1 | 20 | | FO | 16 | 7 | | | 202 | 20 | | 20 | 104 | 74 | | 006 |

0

SU

0

0

0.000

0.00%

EL

12

0

0.000

0.26%

SR

143

33

0.825

8.53%

ST

766

193

0.862

0.937

45.68%

SL

768

190

0.950

45.80%

283

ET

4216

1112

0.924

0.916

90.71%

28

ER

420

105

0.847

9.04%

0

EU

0

0

0.000

0.00%

14

WL

274

71

0.807

6.19%

167

WT

3269

832

0.916

0.922

73.91%

39

WR

880

270

0.888

19.90%

821

715

TOTAL

12175

TOTAL

3173

0.966

0

WU

0

0

0.000

0.00%

Intersection Turning Movement Count

Location: N Canon Dr & S Santa Monica Blvd

City: Beverly Hills **Control:** Signalized

APPROACH %'s:

PEAK HR VOL:

PEAK HR FACTOR :

PEAK HR:

0.00

12.50% 62.50% 25.00%

0.000

05:30 PM - 06:30 PM

0.000

Project ID: Historical **Date:** 4/23/2019

| | K I | _ | |
|--|----------|---|--|
| | — | _ | |

| PEAK HR: 08:30 AM - 09:30 AM | 0 | TO' 0 2 2 2 2 0 1 4 3 2 0 3 0 0 |
|---|---|---|
| AM 1 1.5 0.5 0 1 2 1 0 0 2 0 0 1 2 NL NT NR NU SL ST SR SU EL ET ER EU WL WT N 7:00 AM 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | 0 WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | 0 2 2 2 0 1 4 3 2 0 |
| NL | 0 0 0 0 0 0 0 0 0 | 0 2 2 2 0 1 4 3 2 0 |
| 7:15 AM | 0 0 0 0 0 0 0 0 | 2 2 2 0 1 4 3 2 0 |
| 7:30 AM | 0 0 0 0 0 0 0 | 2 2 0 1 4 3 2 0 |
| 7:45 AM | 0 0 0 0 0 0 | 2 0 1 4 3 2 0 |
| 8:00 AM | 0 0 0 0 0 0 | 3 2 0 3 |
| 8:15 AM 0 1 1 0 0 0 0 1 </th <th>0 0 0 0 0</th> <th>1 4 3 2 0 3</th> | 0 0 0 0 0 | 1 4 3 2 0 3 |
| 8:30 AM | 0 0 0 0 0 | 0 3 |
| 8:45 AM | 0 0 0 0 | 0 3 |
| 9:00 AM | 0 0 0 | 0 3 |
| 9:15 AM | 0 | 3 |
| 9:30 AM | | 3 |
| 9:45 AM 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | | |
| NL NT NR NU SL ST SR SU EL ET ER EU WL WT NT NPR NU | 0 | C |
| TOTAL VOLUMES: 0 1 0 0 0 0 2 0 0 8 0 0 2 5 APPROACH %'s: 0.00% 100.00% | | |
| TOTAL VOLUMES: 0 1 0 0 0 0 2 0 0 8 0 0 2 5 APPROACH %'s: 0.00% 100.00% | | |
| APPROACH %'s: 0.00% 100.00% 0.00% 0.00% 0.00% 0.00% 100.00% 0.00% 0.00% 100.00% | R WU | TO |
| PEAK HR: 08:30 AM - 09:30 AM | 0 | 1 |
| | 0.00% | 0% |
| | | TO |
| PEAK HR VOL : 0 0 0 0 0 0 2 0 0 3 0 0 2 2 | 0 | g |
| PEAK HR FACTOR: 0.000 0.000 0.000 0.000 0.000 0.000 0.500 0.000 0.000 0.750 0.000 0.000 0.500 0.500 0. | 0.000 | 0 0 - |
| 0.500 0.750 0.500 | | 0.5 |
| | | |
| NORTHBOUND SOUTHBOUND EASTBOUND WESTBOU |) | |
| PM 1 1.5 0.5 0 1 2 1 0 0 2 0 0 1 2 | 0 | |
| NL NT NR NU SL ST SR SU EL ET ER EU WL WT N | R WU | TO' |
| 3:00 PM 0 1 1 0 0 0 0 0 0 2 0 0 0 | 0 | 5 |
| 3:15 PM 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | 0 | C |
| 3:30 PM 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | 0 | C |
| 3:45 PM 0 1 0 0 1 0 0 0 1 5 0 0 2 | 0 | 1 |
| 4:00 PM 0 0 0 0 0 0 0 0 0 1 0 0 0 | 0 | 1 |
| 4:15 PM 0 0 0 0 1 1 0 0 0 0 0 0 0 | 0 | 2 |
| 4:30 PM 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | 0 | 2 |
| | 0 | |
| 4:45 PM 0 0 0 0 0 3 0 0 0 2 0 0 1 | 0 | 5 |
| 5:00 PM 0 3 0 0 0 0 0 0 0 0 1 0 0 1 | · II | |
| 5:00 PM 0 3 0 0 0 0 0 0 0 1 0 0 1 5:15 PM 0 0 0 0 0 0 0 0 0 0 0 1 | 0 | 3 |
| 5:00 PM 0 3 0 0 0 0 0 0 0 1 0 0 1 5:15 PM 0 0 0 0 0 0 0 0 0 0 0 0 0 1 5:30 PM 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | 0 | 1 |
| 5:00 PM 0 3 0 0 0 0 0 0 0 0 1 0 0 1 5:15 PM 0 0 0 0 0 0 0 0 0 0 0 0 0 1 5:30 PM 0 <th>0 0 0</th> <th>1 2</th> | 0 0 0 | 1 2 |
| 5:00 PM 0 3 0 0 0 0 0 0 0 1 0 0 1 5:15 PM 0 0 0 0 0 0 0 0 0 0 0 0 1 0 0 0 1 0 < | 0 0 0 0 | 1 2 1 |
| 5:00 PM 0 3 0 0 0 0 0 0 0 0 1 0 0 1 5:15 PM 0 0 0 0 0 0 0 0 0 0 0 1 5:30 PM 0 <th>0 0 0</th> <th>1 2 1 3</th> | 0 0 0 | 1 2 1 3 |
| 5:00 PM 0 3 0 0 0 0 0 0 1 0 0 1 5:15 PM 0 < | 0 0 0 | 1 2 1 3 1 |
| 5:00 PM 0 3 0 0 0 0 0 0 0 1 0 0 1 5:15 PM 0 0 0 0 0 0 0 0 0 0 0 1 5:30 PM 0 0 0 0 0 0 0 0 0 0 0 0 0 5:45 PM 0 | 0 0 0 | 1 2 1 3 1 4 |
| 5:00 PM 0 3 0 0 0 0 0 0 0 0 0 1 0 0 1 5:15 PM 0 < | 0 0 0 0 0 0 | 1 2 1 3 1 4 |
| 5:00 PM 0 3 0 0 0 0 0 0 1 0 0 1 5:15 PM 0 < | 0 0 0 0 0 0 | 1 2 1 3 1 4 7 7 7 7 7 |

33.33% 66.67%

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0.00%

0.000

0

0.000

0.00% 85.71% 14.29%

0.250 0.000

0.250

0.00%

0.000

TOTAL

7

0.583

0.00%

0.000

Intersection Turning Movement Count City: Beverly Hills City: Beverly Hills Date: 4/23/2019

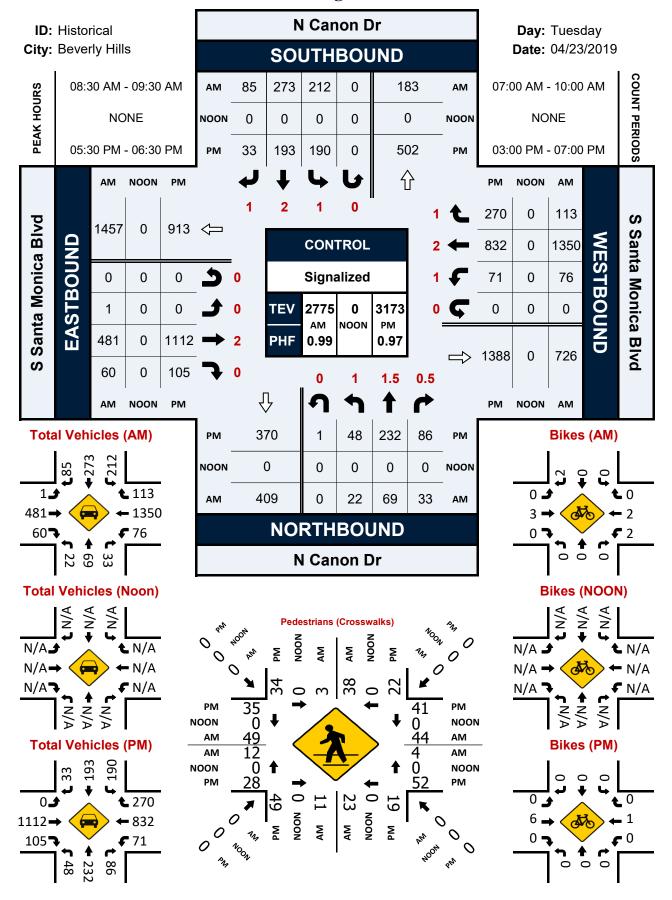
Pedestrians (Crosswalks)

| NS/EW Streets: | N Can | on Dr | N Car | on Dr | S Santa M | lonica Blvd | S Santa M | onica Blvd | |
|-----------------|----------|------------|--------|--------|-----------|-------------|------------------|------------|-------|
| ARA | NORT | H LEG | SOUT | H LEG | EAS | Γ LEG | WES ⁻ | Γ LEG | |
| AM | EB | WB | EB | WB | NB | SB | NB | SB | TOTAL |
| 7:00 AM | 0 | 2 | 0 | 2 | 2 | 9 | 1 | 2 | 18 |
| 7:15 AM | 1 | 3 | 0 | 1 | 2 | 2 | 4 | 4 | 17 |
| 7:30 AM | 1 | 3 | 7 | 2 | 1 | 4 | 0 | 5 | 23 |
| 7:45 AM | 1 | 5 | 3 | 2 | 0 | 3 | 2 | 7 | 23 |
| 8:00 AM | 3 | 7 | 1 | 3 | 1 | 3 | 0 | 6 | 24 |
| 8:15 AM | 2 | 5 | 4 | 3 | 2 | 0 | 2 | 7 | 25 |
| 8:30 AM | 1 | 7 | 4 | 8 | 0 | 11 | 2 | 9 | 42 |
| 8:45 AM | 1 | 14 | 1 | 8 | 0 | 10 | 4 | 19 | 57 |
| 9:00 AM | 0 | 4 | 3 | 5 | 4 | 11 | 5 | 8 | 40 |
| 9:15 AM | 1 | 13 | 3 | 2 | 0 | 12 | 1 | 13 | 45 |
| 9:30 AM | 1 | 6 | 6 | 7 | 2 | 5 | 4 | 7 | 38 |
| 9:45 AM | 1 | 9 | 5 | 4 | 0 | 0 | 5 | 7 | 31 |
| | | | | | | | | | |
| | EB | WB | EB | WB | NB | SB | NB | SB | TOTAL |
| TOTAL VOLUMES: | 13 | 78 | 37 | 47 | 14 | 70 | 30 | 94 | 383 |
| APPROACH %'s: | 14.29% | 85.71% | 44.05% | 55.95% | 16.67% | 83.33% | 24.19% | 75.81% | |
| PEAK HR: | 08:30 AM | - 09:30 AM | | | | | | | TOTAL |
| PEAK HR VOL: | 3 | 38 | 11 | 23 | 4 | 44 | 12 | 49 | 184 |
| PEAK HR FACTOR: | 0.750 | 0.679 | 0.688 | 0.719 | 0.250 | 0.917 | 0.600 | 0.645 | 0.007 |
| | 0.6 | 583 | 0.7 | 708 | 0.8 | 300 | 0.6 | 563 | 0.807 |

| DNA | NORT | H LEG | SOUT | H LEG | EAST | LEG | WEST | LEG | |
|-----------------------|----------|------------|--------|--------|--------|--------|--------|--------|-------|
| PM | EB | WB | EB | WB | NB | SB | NB | SB | TOTAL |
| 3:00 PM | 5 | 6 | 9 | 5 | 6 | 6 | 7 | 6 | 50 |
| 3:15 PM | 10 | 11 | 16 | 2 | 11 | 5 | 10 | 10 | 75 |
| 3:30 PM | 17 | 17 | 20 | 9 | 11 | 11 | 23 | 10 | 118 |
| 3:45 PM | 4 | 10 | 19 | 11 | 2 | 1 | 7 | 16 | 70 |
| 4:00 PM | 3 | 5 | 11 | 4 | 7 | 6 | 5 | 7 | 48 |
| 4:15 PM | 4 | 4 | 14 | 11 | 2 | 5 | 12 | 10 | 62 |
| 4:30 PM | 4 | 1 | 10 | 8 | 6 | 7 | 9 | 7 | 52 |
| 4:45 PM | 7 | 4 | 13 | 4 | 5 | 6 | 12 | 6 | 57 |
| 5:00 PM | 13 | 6 | 10 | 10 | 4 | 5 | 6 | 21 | 75 |
| 5:15 PM | 2 | 3 | 16 | 5 | 10 | 8 | 9 | 8 | 61 |
| 5:30 PM | 11 | 10 | 20 | 4 | 18 | 18 | 11 | 13 | 105 |
| 5:45 PM | 8 | 2 | 9 | 2 | 15 | 7 | 7 | 5 | 55 |
| 6:00 PM | 10 | 6 | 9 | 3 | 6 | 9 | 8 | 13 | 64 |
| 6:15 PM | 5 | 4 | 11 | 10 | 13 | 7 | 2 | 4 | 56 |
| 6:30 PM | 4 | 5 | 12 | 3 | 3 | 4 | 4 | 6 | 41 |
| 6:45 PM | 9 | 2 | 17 | 6 | 17 | 9 | 7 | 4 | 71 |
| | | | | | | | | | |
| | EB | WB | EB | WB | NB | SB | NB | SB | TOTAL |
| TOTAL VOLUMES: | 116 | 96 | 216 | 97 | 136 | 114 | 139 | 146 | 1060 |
| APPROACH %'s: | 54.72% | 45.28% | 69.01% | 30.99% | 54.40% | 45.60% | 48.77% | 51.23% | |
| PEAK HR : | 05:30 PM | - 06:30 PM | | | | | | | TOTAL |
| PEAK HR VOL : | 34 | 22 | 49 | 19 | 52 | 41 | 28 | 35 | 280 |
| PEAK HR FACTOR : | 0.773 | 0.550 | 0.613 | 0.475 | 0.722 | 0.569 | 0.636 | 0.673 | 0.667 |
| | 0.0 | 667 | 0.7 | 708 | 0.6 | 546 | 0.6 | 556 | 0.667 |

N Canon Dr & S Santa Monica Blvd

Peak Hour Turning Movement Count



Intersection Turning Movement Count

Location: N Beverly Dr & Brighton Way **City:** Beverly Hills

Control: Signalized

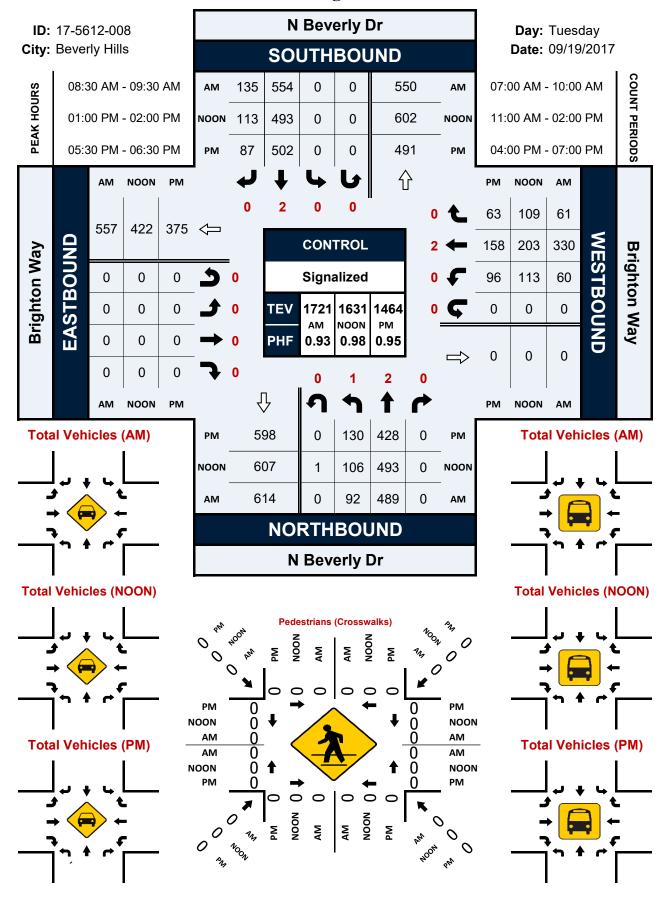
Project ID: 17-5612-008 **Date:** 9/19/2017

| | _ |
|---|---|
| _ | _ |
| | |

| NS/EW Streets: | | N Bever | rly Dr | | | N Beve | rly Dr | | | Brighto | on Way | | | Brighto | n Way | | |
|-----------------------------------|--------------|---------------|------------|------------|------------|---------------|---------------|------------|------------|------------|------------|----------------------|--------------|---------------|---------------|------------|---------------|
| | | NORTH | | | _ | SOUTH | | _ | _ | | BOUND | _ | _ | WESTE | | | |
| AM | 1 NL | 2 NT | 0 NR | 0 NU | 0 SL | 2 ST | 0 SR | 0 SU | 0 EL | 0 ET | 0 ER | 0 EU | 0 WL | 2 WT | 0 WR | 0 WU | TOTAL |
| 7:00 AM | NL 8 | 55 | 0 | 0 | 0 0 | 79 | 14 | 0 | EL | 0 | 0 0 | 0 | 5 | 11 | 9 | 0 | 181 |
| 7:15 AM | 4 | 89 | 0 | 0 | 0 | 96 | 15 | 0 | 0 | 0 | 0 | 0 | 4 | 16 | 12 | 0 | 236 |
| 7:30 AM | 10 | 73 | 0 | 0 | 0 | 88 | 23 | 0 | 0 | 0 | 0 | 0 | 9 | 34 | 15 | 0 | 252 |
| 7:45 AM | 26 | 120 | 0 | 0 | 0 | 105 | 42 | 0 | 0 | 0 | 0 | 0 | 11 | 70 | 11 | 0 | 385 |
| 8:00 AM 8:15 AM | 11 25 | 102 118 | 0 0 | 0 | 0 0 | 129 122 | 38 29 | 0 | 0 | 0 | 0 | 0 | 11 14 | 50 55 | 15 10 | 0 0 | 356 373 |
| 8:30 AM | 26 | 125 | 0 | 0 | 0 | 142 | 34 | 0 | 0 | 0 | 0 | 0 | 13 | 79 | 15 | 0 | 434 |
| 8:45 AM | 23 | 99 | 0 | 0 | 0 | 120 | 40 | 0 | 0 | 0 | 0 | 0 | 17 | 88 | 16 | 0 | 403 |
| 9:00 AM | 15 | 122 143 | 0 | 0 | 0 | 145 147 | 30 | 0 | 0 | 0 | 0 | 0 | 15 | 80 | 16 | 0 0 | 423 |
| 9:15 AM 9:30 AM | 28 30 | 143 | 0 0 | 0 | 0 0 | 147 | 31 26 | 0 | 0 | 0 | 0 | 0 0 | 15 17 | 83 71 | 14 17 | 0 | 461 409 |
| 9:45 AM | 20 | 112 | 0 | 0 | 0 | 144 | 33 | 0 | 0 | 0 | 0 | 0 | 20 | 56 | 20 | 0 | 405 |
| | | | | <u> </u> | | | | - | | | | | | | | | |
| TOTAL VOLUMES : | NL 226 | NT 1269 | NR 0 | NU 0 | SL 0 | ST 1454 | SR 355 | SU 0 | EL 0 | ET 0 | ER 0 | EU 0 | WL 151 | WT 693 | WR 170 | WU 0 | TOTAL 4318 |
| APPROACH %'s: | 15.12% | | 0.00% | 0.00% | • | 80.38% | 333 19.62% | 0.00% | U | U | U | U | 14.89% | 68.34% | 170 16.77% | 0.00% | |
| PEAK HR : | | | 09:30 AM | 0.0070 | 0.0070 | 0013070 | 13.02 70 | 0.0070 | | | | | 1110370 | 00.5 170 | 1017770 | 0.0070 | TOTAL |
| PEAK HR VOL : | 92 | 489 | 0 | 0 | 0 | 554 | 135 | 0 | 0 | 0 | 0 | 0 | 60 | 330 | 61 | 0 | 1721 |
| PEAK HR FACTOR : | 0.821 | 0.855 0.84 | 0.000 | 0.000 | 0.000 | 0.942 0.96 | 0.844 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.882 | 0.938 0.93 | 0.953 | 0.000 | 0.933 |
| | | 0.05 | 13 | | | 0.90 | 00 | | | | | | | 0.9. | 02 | | |
| | | NORTH | | | | SOUTH | BOUND | | | EAST | BOUND | | | WESTE | | | |
| NOON | 1 NL | 2 NT | 0 NR | 0 NU | 0 SL | 2 ST | 0 SR | 0 SU | 0 EL | 0 ET | 0 ER | <mark>0</mark> EU | 0 WL | 2 WT | 0 WR | 0 WU | TOTAL |
| 11:00 AM | | 111 | 0 | 0 | 0 | 139 | 26 | 0 | 0 | 0 | 0 | 0 | 29 | 49 | 26 | 0 | 402 |
| 11:15 AM | 18 | 123 | 0 | 0 | 0 | 142 | 29 | 1 | 0 | 0 | 0 | 0 | 21 | 30 | 30 | 0 | 394 |
| 11:30 AM | 22 | 139 | 0 | 0 | 0 | 145 | 25 | 0 | 0 | 0 | 0 | 0 | 25 | 10 | 18 | 0 | 384 |
| 11:45 AM 12:00 PM | 15 18 | 120 113 | 0 | 0 | 0 | 113 123 | 42 28 | 0 | 0 | 0 | 0 | 0 | 25 31 | 35 51 | 23 28 | 0 | 373 392 |
| 12:15 PM | 20 | 116 | 0 | 0 | 0 | 117 | 38 | 0 | 0 | 0 | 0 | 0 | 25 | 47 | 39 | 0 | 402 |
| 12:30 PM | 17 | 110 | 0 | 1 | 0 | 137 | 30 | 0 | 0 | 0 | 0 | 0 | 24 | 50 | 29 | 0 | 398 |
| 12:45 PM | 19 | 109 | 0 | 0 | 0 | 130 | 19 | 0 | 0 | 0 | 0 | 0 | 22 | 37 | 30 | 0 | 366 |
| 1:00 PM 1:15 PM | 21 25 | 125 131 | 0 0 | 0 | 0 0 | 121 121 | 27 32 | 0 | 0 | 0 | 0 | 0 | 26 24 | 55 43 | 30 24 | 0 | 406 400 |
| 1:30 PM | 30 | 111 | 0 | 0 | 0 | 134 | 30 | 0 | 0 | 0 | 0 | 0 | 23 | 56 | 27 | 0 | 411 |
| 1:45 PM | 30 | 126 | 0 | 0 | 0 | 117 | 24 | 0 | 0 | 0 | 0 | 0 | 40 | 49 | 28 | 0 | 414 |
| | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| TOTAL VOLUMES : | 257 | 1434 | 0 | 2 | 0 | 1539 | 350 | 1 | 0 | 0 | 0 | 0 | 315 | 512 | 332 | 0 | 4742 |
| APPROACH %'s: | 15.18% | | 0.00% | 0.12% | 0.00% | 81.43% | 18.52% | 0.05% | | | | | 27.18% | 44.18% | 28.65% | 0.00% | |
| PEAK HR: | | 01:00 PM - | | 4 | 0 | 402 | 110 | 0 | 0 | 0 | 0 | 0 | 440 | 202 | 100 | 0 | TOTAL |
| PEAK HR VOL : PEAK HR FACTOR : | 106 0.883 | 493 0.941 | 0 0.000 | 1 0.250 | 0 0.000 | 493 0.920 | 113 0.883 | 0 0.000 | 0 0.000 | 0 0.000 | 0 0.000 | 0 0.000 | 113 0.706 | 203 0.906 | 109 0.908 | 0 0.000 | 1631 |
| PLAKTIKT ACTOR: | 0.005 | 0.96 | | 0.230 | 0.000 | 0.92 | | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.700 | 0.90 | | 0.000 | 0.985 |
| | | NODELI | 2011112 | | | 0011711 | BOLIND | | | EACT | | | ı | MEGT | | | |
| PM | 1 | NORTHI | 0 BOUND | 0 | 0 | SOUTH | 0 BOUND | 0 | 0 | EAST 0 | BOUND 0 | 0 | 0 | WESTE | OUND 0 | 0 | |
| r IVI | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| 4:00 PM | 27 | 116 | 0 | 0 | 0 | 130 | 19 | 0 | 0 | 0 | 0 | 0 | 27 | 44 | 22 | 0 | 385 |
| 4:15 PM 4:30 PM | 27 29 | 85 97 | 0 0 | 0 | 0 0 | 133 118 | 19 19 | 0 | 0 | 0 | 0 | 0 | 20 30 | 46 39 | 27 20 | 0 | 357 352 |
| 4:45 PM | 26 | 92 | 0 | 0 | 0 | 132 | 15 | 0 | 0 | 0 | 0 | 0 | 30 | 32 | 17 | 0 | 344 |
| 5:00 PM | 30 | 93 | 0 | 0 | 0 | 126 | 24 | 0 | 0 | 0 | 0 | 0 | 41 | 33 | 16 | 0 | 363 |
| 5:15 PM | 25 | 111 | 0 | 0 | 0 | 123 | 12 | 0 | 0 | 0 | 0 | 0 | 23 | 38 | 11 | 0 | 343 |
| 5:30 PM 5:45 PM | 29 31 | 119 117 | 0 0 | 0 | 0 0 | 120 133 | 21 28 | 0 | 0 | 0 | 0 | 0 0 | 24 18 | 42 37 | 13 21 | 0 | 368 385 |
| 6:00 PM | 40 | 99 | 0 | 0 | 0 | 128 | 18 | 0 | 0 | 0 | 0 | 0 | 27 | 30 | 14 | 0 | 356 |
| 6:15 PM | 30 | 93 | 0 | 0 | 0 | 121 | 20 | 0 | 0 | 0 | 0 | 0 | 27 | 49 | 15 | 0 | 355 |
| 6:30 PM | 38 | 121 | 0 | 0 | 0 | 115 | 22 | 0 | 0 | 0 | 0 | 0 | 15 | 25 | 17 | 0 | 353 |
| 6:45 PM | 37 | 113 | 0 | 0 | 0 | 117 | 18 | 0 | 0 | 0 | 0 | 0 | 18 | 34 | 20 | 0 | 357 |
| | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| TOTAL VOLUMES : | 369 | 1256 | 0 | 0 | 0 | 1496 | 235 | 0 | 0 | 0 | 0 | 0 | 300 | 449 | 213 | 0 | 4318 |
| APPROACH %'s: | 22.71% | | 0.00% | 0.00% | 0.00% | 86.42% | 13.58% | 0.00% | | | | | 31.19% | 46.67% | 22.14% | 0.00% | |
| PEAK HR VOL | | 05:30 PM - | | 0 | 0 | E02 | 07 | 0 | 0 | 0 | 0 | 0 | 06 | 150 | 62 | 0 | TOTAL |
| PEAK HR VOL : PEAK HR FACTOR : | 130 0.813 | 428 0.899 | 0 0.000 | 0 0.000 | 0 0.000 | 502 0.944 | 87 0.777 | 0 0.000 | 0 0.000 | 0 0.000 | 0 0.000 | 0 0.000 | 96 0.889 | 158 0.806 | 63 0.750 | 0 0.000 | 1464 |
| - LAKTIK I ACTOR I | 0.013 | 0.099 | | 0.000 | J.000 | 0.91 | | 3.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.005 | 0.800 | | 3.300 | 0.951 |
| | | | | | | | | | | | | | | | | | |

N Beverly Dr & Brighton Way

Peak Hour Turning Movement Count



Intersection Turning Movement Count

Location: Rodeo Dr & Brighton Way
City: Beverly Hills
Control: Signalized

Project ID: 18-05534-010

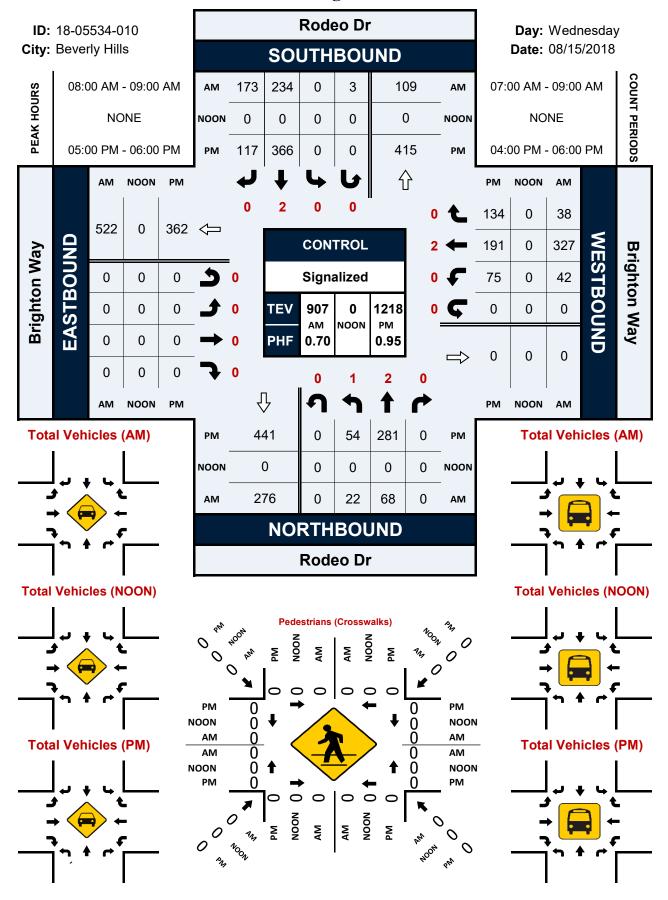
Date: 8

| Date: | 8/15/2018 |
|-------|-----------|

| 7:00 AM 7:15 AM 7:30 AM | 1 NL 0 | Rodeo NORTH 2 | o Dr | | | | | To | ובי | | | | | | | | |
|---|---------------------------------|--|-------------------------------------|------------------|------------|---------------|---------------|------------|---------|---------|---------|---------|---------------|---------------|---------------|------------|---|
| 7:00 AM 7:15 AM 7:30 AM | | NORTH 2 | Dr Dr | | | | | 10 | Lai | | | | | | | | |
| 7:00 AM 7:15 AM 7:30 AM | | 2 | | | | Rode | Dr Dr | | | Brighto | n Way | | | Brightor | า Way | | |
| 7:00 AM 7:15 AM 7:30 AM | | 2 | BOUND | | | SOUTH | BOUND | | | EAST | BOUND | | | WESTE | OUND | | |
| 7:00 AM 7:15 AM 7:30 AM | | | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | |
| 7:15 AM 7:30 AM | 0 | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| 7:30 AM | 1 | 6 | 0 | 0 | 0 | 20 | 21 | 0 | 0 | 0 | 0 | 0 | 0 | 22 | 9 | 0 | 78 |
| | _ | 13 | 0 | 0 | 0 | 31 | 17 | 0 | 0 | 0 | 0 | 0 | 5 | 41 | 2 | 0 | 110 |
| | 1 | 13 | 0 | 0 | 0 | 36 | 36 | 0 | 0 | 0 | 0 | 0 | 0 | 35 | 4 | 0 | 125 |
| 7:45 AM | 4 | 9 | 0 | 0 | 0 | 49 | 50 | 0 | 0 | 0 | 0 | 0 | 4 | 66 | 4 | 0 | 186 |
| 8:00 AM | 3 | 16 | 0 | 0 | 0 | 46 | 27 | 1 | 0 | 0 | 0 | 0 | 7 | 46 | 7 | 0 | 153 |
| 8:15 AM | 3 | 11 | 0 | 0 | 0 | 56 | 54 | 0 | 0 | 0 | 0 | 0 | 9 | 72 | 11 | 0 | 216 |
| 8:30 AM | 3 | 19 | 0 | 0 | 0 | 59 | 42 | 1 | 0 | 0 | 0 | 0 | 13 | 75 | 4 | 0 | 216 |
| 8:45 AM | 13 | 22 | 0 | 0 | 0 | 73 | 50 | 1 | 0 | 0 | 0 | 0 | 13 | 134 | 16 | 0 | 322 |
| | | | | | | | | | | | | | | | | | |
| | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| TOTAL VOLUMES : | 28 | 109 | 0 | 0 | 0 | 370 | 297 | 3 | 0 | 0 | 0 | 0 | 51 | 491 | 57 | 0 | 1406 |
| APPROACH %'s: | 20.44% | 79.56% | 0.00% | 0.00% | 0.00% | 55.22% | 44.33% | 0.45% | | | | | 8.51% | 81.97% | 9.52% | 0.00% | |
| PEAK HR : | | 8:00 AM - | | | | | | | | | | | | | | | TOTAL |
| PEAK HR VOL : | 22 | 68 | 0 | 0 | 0 | 234 | 173 | 3 | 0 | 0 | 0 | 0 | 42 | 327 | 38 | 0 | 907 |
| EAK HR FACTOR : | 0.423 | 0.773 | 0.000 | 0.000 | 0.000 | 0.801 | 0.801 | 0.750 | 0.000 | 0.000 | 0.000 | 0.000 | 0.808 | 0.610 | 0.594 | 0.000 | 0.704 |
| | | 0.64 | 13 | | | 0.82 | 27 | | | | | | | 0.62 | 24 | | |
| | | NORTH | BOUND | | | SOUTH | BOUND | | | FASTI | BOUND | | | WESTE | ROLIND | | |
| PM | 1 | 2 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | |
| 11111 | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| 4:00 PM | 16 | 67 | 0 | 0 | 0 | 87 | 31 | 0 | 0 | 0 | 0 | 0 | 13 | 66 | 28 | 0 | 308 |
| 4:15 PM | 18 | 56 | 0 | 0 | 0 | 100 | 35 | 0 | 0 | 0 | 0 | 0 | 19 | 61 | 21 | 0 | 310 |
| 4:30 PM | 13 | 69 | 0 | 1 | 0 | 79 | 34 | 1 | 0 | 0 | 0 | 0 | 14 | 45 | 30 | 0 | 286 |
| 4:45 PM | 15 | 75 | 0 | 0 | 0 | 75 | 30 | 1 | 0 | 0 | 0 | 0 | 12 | 44 | 26 | 0 | 278 |
| 5:00 PM | 13 | 67 | 0 | 0 | 0 | 90 | 34 | 0 | 0 | 0 | 0 | 0 | 17 | 52 | 31 | 0 | 304 |
| | 11 | 59 | 0 | 0 | 0 | 105 | 38 | 0 | 0 | 0 | 0 | 0 | 17 | 50 | 41 | 0 | 321 |
| 5:15 PM | 11 | 92 | 0 | 0 | 0 | 78 | 28 | 0 | 0 | 0 | 0 | 0 | 25 | 46 | 31 | 0 | 313 |
| 5:15 PM 5:30 PM | 13 | | ^ | 0 | 0 | 93 | 17 | 0 | 0 | 0 | 0 | 0 | 16 | 43 | 31 | 0 | 280 |
| 5:15 PM | | 63 | 0 | U | | | | (| | | | | 1 | | | | |
| 5:15 PM 5:30 PM | 13 17 | 63 | _ | | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| 5:15 PM 5:30 PM 5:45 PM | 13 17 NL | 63 NT | NR | NU 1 | SL 0 | ST 707 | SR 247 | SU 2 | EL 0 | ET 0 | ER 0 | EU 0 | WL 133 | WT 407 | WR 239 | WU 0 | |
| 5:15 PM 5:30 PM 5:45 PM | 13 17 NL 116 | 63 NT 548 | NR 0 | NU 1 | 0 | 707 | 247 | 2 | | ET 0 | ER 0 | | 133 | 407 | 239 | 0 | TOTAL 2400 |
| 5:15 PM 5:30 PM 5:45 PM TOTAL VOLUMES : APPROACH %'s : | 13 17 NL 116 17.44% | 63 NT 548 82.41% | NR 0 0.00% | | 0 | | | | | | ER 0 | | | | | | 2400 |
| 5:15 PM 5:30 PM 5:45 PM FOTAL VOLUMES : APPROACH %'s : PEAK HR : | 13 17 NL 116 17.44% | 63 NT 548 82.41% 05:00 PM - | NR 0 0.00% | NU 1 | 0 0.00% | 707 73.95% | 247 25.84% | 2 | | 0 | ER 0 | | 133 17.07% | 407 52.25% | 239 30.68% | 0 0.00% | 2400 TOTAL |
| 5:15 PM 5:30 PM 5:45 PM TOTAL VOLUMES : APPROACH %'s : | 13 17 NL 116 17.44% | 63 NT 548 82.41% | NR 0 0.00% 06:00 PM | NU 1 0.15% | 0 | 707 | 247 | 2 0.21% | 0 | | 0 | 0 | 133 | 407 | 239 | 0 | TOTAL 2400 TOTAL 1218 0.949 |

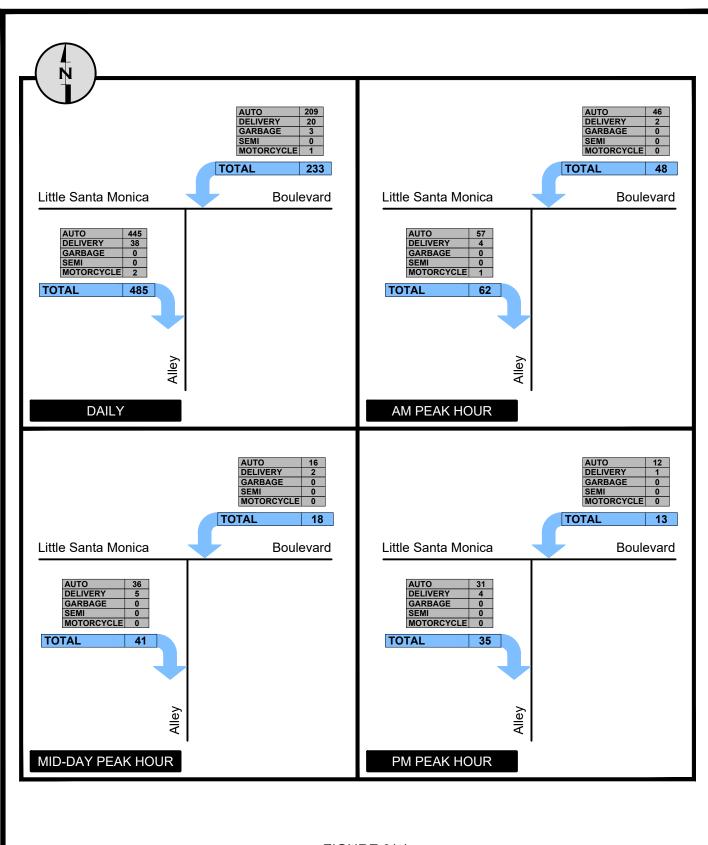
Rodeo Dr & Brighton Way

Peak Hour Turning Movement Count



CHEVAL BLANC HOTEL PROJECT SUMMARY OF CURRENT WEEKDAY ALLEY TRAFFIC ACTIVITY ONE-WAY SOUTHBOUND ALLEY BETWEEN SANTA MONICA BOULEVARD (S) AND BRIGHTON WAY

| DAYIDATE Tuesday, April 23, 2019 Daily | 483 61 37 36 369 57 25 24 440 65 35 30 380 53 29 28 505 51 27 | 30 1 4 8 39 3 8 4 44 5 7 0 35 7 5 1 | ND RIGHT-TI GARBAGE 1 0 0 0 0 0 0 0 0 0 0 0 1 1 0 0 | | | 516 62 41 45 409 61 33 28 488 72 42 30 417 61 34 29 | 208 45 17 10 164 41 9 8 226 50 17 16 187 36 14 8 | ## WESTBOUT DELIVERY 13 | 3 2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | | | 226 49 17 11 190 45 12 9 248 51 18 16 208 37 17 | 691 106 54 46 533 98 34 32 666 115 52 46 | ### DELIVERY 43 3 4 9 62 7 11 5 63 5 8 0 51 8 8 8 | ALLEY VOI GARBAGE 4 2 0 0 0 0 2 0 0 0 3 0 0 0 0 0 0 0 0 0 0 | | ## MC 4 0 0 1 1 1 1 0 0 0 5 3 3 0 0 0 4 1 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | 742 1111 58 56 599 106 45 37 736 123 60 46 |
|--|---|--|--|---|--|--|---|--|--|---|---|---|---|---|--|---------------------------------|---|---|
| Tuesday, April 23, 2019 Daily AM Peak Hour (8:45-9:45 AM) Mid-Day Peak Hour (12:00 N - 1:00 PM) Monday, May 13, 2019 Daily AM Peak Hour (8:45-9:45 AM) Mid-Day Peak Hour (12:00 N - 1:00 PM) PM Peak Hour (3:30 - 4:30 PM) Tuesday, May 14, 2019 Daily AM Peak Hour (8:45-9:45 AM) Mid-Day Peak Hour (1:00 - 2:00 PM) PM Peak Hour (8:45-9:45 AM) Mid-Day Peak Hour (1:00 - 2:00 PM) Monday, May 20, 2019 Daily AM Peak Hour (8:45-9:45 AM) Mid-Day Peak Hour (1:20 N - 1:00 PM) PM Peak Hour (1:20 N - 1:00 PM) Tuesday, May 21, 2019 Daily AM Peak Hour (1:25 - 5:15 PM) Tuesday, May 21, 2019 Daily AM Peak Hour (8:45 - 9:45 AM) Mid-Day Peak Hour (1:245 - 1:45 PM) Tuesday, May 21, 2019 Daily AM Peak Hour (8:45 - 9:45 AM) Mid-Day Peak Hour (1:25 - 1:45 PM) Wednesday, May 22, 2019 Daily AM Peak Hour (8:45 - 9:45 AM) Mid-Day Peak Hour (8:45 - 9:45 AM) Mid-Day Peak Hour | 483 61 37 36 369 57 25 24 440 65 35 30 380 53 29 28 505 51 27 | 30 1 4 8 39 3 8 4 44 5 7 0 35 7 5 1 | 1 0 0 0 0 0 0 0 0 0 0 0 | | 2 0 0 1 1 1 1 0 0 0 0 0 0 0 0 0 0 0 0 0 | 516 62 41 45 409 61 33 28 488 72 42 30 417 61 34 29 | 208 45 17 10 164 41 9 8 226 50 17 16 187 36 14 8 | 13 2 0 1 23 4 3 1 1 19 0 1 0 | 3 2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | | 2 0 0 0 0 0 0 0 0 0 0 | 226 49 17 11 190 45 12 9 248 51 18 16 | 691 106 54 46 533 98 34 32 666 115 52 46 | 43 3 4 9 62 7 11 5 63 5 8 0 51 8 | 4 2 0 0 0 3 0 0 0 0 0 0 | | 4 0 0 1 1 1 1 0 0 0 5 3 0 0 | 742 1111 58 56 599 106 45 37 736 123 60 46 |
| Daily AM Peak Hour (8:45 - 9:45 AM) Mid-Day Peak Hour (12:20 N - 1:30 PM) PM Peak Hour (3:30 - 4:30 PM) Monday, May 13, 2019 Daily AM Peak Hour (3:45 - 9:45 AM) Mid-Day Peak Hour (12:00 N - 1:30 PM) Tuesday, May 14, 2019 Daily AM Peak Hour (8:45 - 9:45 AM) Mid-Day Peak Hour (1:00 - 2:00 PM) PM Peak Hour (4:00 - 5:00 PM) Monday, May 20, 2019 Daily AM Peak Hour (1:00 - 2:00 PM) Mid-Day Peak Hour (1:00 - 1:00 PM) PM Peak Hour (1:00 - 1:00 PM) PM Peak Hour (1:00 - 1:00 PM) Tuesday, May 21, 2019 Daily AM Peak Hour (1:50 - 1:45 PM) Tuesday, May 21, 2019 Daily AM Peak Hour (8:45 - 9:45 AM) Mid-Day Peak Hour (1:245 - 1:45 PM) Tuesday, May 22, 2019 Daily AM Peak Hour (8:45 - 9:45 AM) Mid-Day Peak Hour (1:245 - 1:45 PM) Wednesday, May 22, 2019 Daily AM Peak Hour (8:45 - 9:45 AM) Mid-Day Peak Hour (1:45 - 1:45 PM) PM Peak Hour (8:45 - 9:45 AM) Mid-Day Peak Hour | 61 37 36 369 57 25 24 440 65 35 30 380 53 29 28 505 51 27 | 1 4 8 39 3 8 4 44 5 7 0 35 7 5 1 | 0 0 0 0 0 0 0 0 0 0 0 0 | 0 0 0 0 0 0 0 0 0 | 0 0 1 1 1 0 0 0 2 0 0 | 409 61 33 28 488 72 42 30 417 61 34 29 | 45 17 10 164 41 9 8 226 50 17 16 187 36 14 | 2 0 1 23 4 3 1 19 0 1 0 16 1 3 1 | 2 0 0 3 0 0 0 0 0 0 0 0 | | 0 0 0 0 0 0 0 0 0 | 49 17 11 190 45 12 9 248 51 18 16 208 37 | 106 54 46 533 98 34 32 666 115 52 46 567 89 | 3 4 9 62 7 11 5 63 5 8 0 | 2 0 0 0 3 0 0 0 0 0 0 0 | | 0 0 1 1 1 1 0 0 5 3 0 0 | 1111 58 56 599 106 45 37 736 123 60 46 |
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| Mid-Day Peak Hour (12:00 N - 1:00 PM) PM Peak Hour (3:30 - 4:30 PM) Monday, May 13, 2019 Daily AM Peak Hour (8:45 - 9:45 AM) Mid-Day Peak Hour (3:30 - 4:30 PM) Tuesday, May 14, 2019 Daily AM Peak Hour (8:45 - 9:45 AM) Mid-Day Peak Hour (1:00 - 2:00 PM) PM Peak Hour (4:00 - 5:00 PM) Monday, May 20, 2019 Daily AM Peak Hour (8:45 - 9:45 AM) Mid-Day Peak Hour (1:200 N - 1:00 PM) PM Peak Hour (8:45 - 9:45 AM) Mid-Day Peak Hour (1:200 N - 1:00 PM) Tuesday, May 21, 2019 Daily AM Peak Hour (8:45 - 9:45 AM) Mid-Day Peak Hour (1:245 - 1:45 PM) Tuesday, May 21, 2019 Daily AM Peak Hour (8:45 - 9:45 AM) Mid-Day Peak Hour (1:245 - 1:45 PM) PM Peak Hour (8:45 - 9:45 AM) Wid-Day Peak Hour (1:45 - 1:45 PM) Wednesday, May 22, 2019 Daily AM Peak Hour (8:45 - 9:45 AM) Mid-Day Peak Hour | 36 369 57 25 24 440 65 35 30 380 53 29 28 505 51 | 8 39 3 8 4 44 5 7 0 35 7 5 1 | 0 0 0 0 0 0 0 0 0 | 0 0 0 0 0 0 0 0 | 1 1 1 0 0 4 2 0 0 0 | 409 61 33 28 488 72 42 30 417 61 34 29 | 10 164 41 9 8 226 50 17 16 187 36 14 8 | 1 23 4 3 1 1 19 0 1 0 1 0 | 0 3 0 0 0 0 0 0 0 0 | 0 0 0 0 0 0 0 | 0 0 0 0 0 0 0 1 1 1 0 | 11 190 45 12 9 248 51 18 16 208 37 | 46 533 98 34 32 666 115 52 46 567 89 | 9 62 7 11 5 63 5 8 0 | 0 3 0 0 0 0 2 0 0 0 | 0 0 0 0 0 0 0 | 1 1 1 1 0 0 0 5 3 3 0 0 | 56 599 106 45 37 736 123 60 46 625 98 |
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| Monday, May 13, 2019 Daily AM Peak Hour (8:45-9:45 AM) Mid-Day Peak Hour (12:00 N - 1:00 PM) PM Peak Hour (8:45-9:45 AM) AM Peak Hour (8:45-9:45 AM) Mid-Day Peak Hour (1:00-2:00 PM) Monday, May 20, 2019 Daily AM Peak Hour (8:45-9:45 AM) Mid-Day Peak Hour (1:00-1:00 PM) Monday, May 20, 2019 Daily AM Peak Hour (8:45-9:45 AM) Mid-Day Peak Hour (1:2:00 N - 1:00 PM) PM Peak Hour (8:45-9:45 AM) Tuesday, May 21, 2019 Daily AM Peak Hour (8:45-9:45 PM) Mid-Day Peak Hour (12:45-1:45 PM) Wednesday, May 22, 2019 Daily AM Peak Hour (8:45-9:45 AM) Mid-Day Peak Hour (12:45-1:45 PM) Wednesday, May 22, 2019 Daily AM Peak Hour (8:45-9:45 AM) Mid-Day Peak Hour (8:45-9:45 AM) Mid-Day Peak Hour (8:45-9:45 AM) Mid-Day Peak Hour | 57 25 24 440 65 35 30 380 53 29 28 505 51 27 | 3 8 4 44 5 7 0 35 7 5 1 | 0 0 0 0 0 0 0 0 0 | 0 0 0 0 0 0 0 0 | 1 0 0 4 2 0 0 0 | 61 33 28 488 72 42 30 417 61 34 29 | 41 9 8 226 50 17 16 187 36 14 | 4 3 1 19 0 1 0 16 1 3 1 | 0 0 0 2 0 0 0 0 | 0 0 0 0 0 0 | 0 0 0 1 1 1 0 0 | 45 12 9 248 51 18 16 208 37 17 | 98 34 32 666 115 52 46 567 89 | 7 11 5 63 5 8 0 | 0 0 0 2 0 0 0 | 0 0 0 0 0 0 | 1 0 0 5 3 0 0 | 106 45 37 736 123 60 46 625 98 |
| Daily AM Peak Hour (8:45 - 9:45 AM) Mid-Day Peak Hour (12:200 N - 1:200 PM) PM Peak Hour (3:30 - 4:30 PM) Tuesday, May 14, 2019 Daily AM Peak Hour (8:45 - 9:45 AM) Mid-Day Peak Hour (1:00 - 2:00 PM) PM Peak Hour (8:45 - 9:45 AM) Mid-Day Peak Hour (1:200 N - 1:00 PM) PM Peak Hour (1:200 N - 1:00 PM) PM Peak Hour (1:50 S - 9:45 AM) Mid-Day Peak Hour (1:45 - 5:15 PM) Tuesday, May 21, 2019 Daily AM Peak Hour (8:45 - 9:45 AM) Mid-Day Peak Hour (1:245 - 1:45 PM) PM Peak Hour (1:245 - 1:45 PM) PM Peak Hour (1:45 S - 9:45 AM) Mid-Day Peak Hour (1:45 S - 9:45 AM) Wednesday, May 22, 2019 Daily AM Peak Hour (8:45 - 9:45 AM) Wid-Day Peak Hour (1:45 S - 9:45 AM) Mid-Day Peak Hour (1:45 S - 9:45 AM) Mid-Day Peak Hour (8:45 S - 9:45 AM) Mid-Day Peak Hour (1:40 S - 9:45 AM) Mid-Day Peak Hour | 57 25 24 440 65 35 30 380 53 29 28 505 51 27 | 3 8 4 44 5 7 0 35 7 5 1 | 0 0 0 0 0 0 0 0 0 | 0 0 0 0 0 0 0 0 | 1 0 0 4 2 0 0 0 | 61 33 28 488 72 42 30 417 61 34 29 | 41 9 8 226 50 17 16 187 36 14 | 4 3 1 19 0 1 0 16 1 3 1 | 0 0 0 2 0 0 0 0 | 0 0 0 0 0 0 | 0 0 0 1 1 1 0 0 | 45 12 9 248 51 18 16 208 37 17 | 98 34 32 666 115 52 46 567 89 | 7 11 5 63 5 8 0 | 0 0 0 2 0 0 0 | 0 0 0 0 0 0 | 1 0 0 5 3 0 0 | 106 45 37 736 123 60 46 625 98 |
| (8.45 - 9.45 AM) Mid-Day Peak Hour (12:00 N - 1:00 PM) PM Peak Hour (3:30 - 4:30 PM) Tuesday, May 14, 2019 Daily AM Peak Hour (8:45 - 9:45 AM) Mid-Day Peak Hour (1:00 - 2:00 PM) PM Peak Hour (8:45 - 9:45 AM) Mid-Day Peak Hour (1:200 N - 1:00 PM) PM Peak Hour (8:45 - 9:45 AM) Mid-Day Peak Hour (6:45 - 9:45 AM) Tuesday, May 21, 2019 Daily AM Peak Hour (8:45 - 9:45 AM) Mid-Day Peak Hour (1:245 - 1:45 PM) The Peak Hour (1:245 - 1:45 PM) PM Peak Hour (1:245 - 1:45 PM) Wednesday, May 22, 2019 Daily AM Peak Hour (1:45 - 9:45 AM) Wid-Day Peak Hour (1:45 - 9:45 AM) Wid-Day Peak Hour (8:45 - 9:45 AM) Mid-Day Peak Hour (1:00 - 2:00 PM) PM Peak Hour | 25 24 440 65 35 30 380 53 29 28 505 51 27 | 8 4 44 5 7 0 35 7 5 1 | 0 0 0 0 0 0 0 0 | 0 0 0 0 0 0 0 | 0 0 4 2 0 0 0 | 33 28 488 72 42 30 417 61 34 29 | 9 8 226 50 17 16 187 36 14 | 19 0 1 0 16 1 3 | 0 0 2 0 0 0 0 | 0 0 0 0 0 | 0 0 1 1 0 0 | 12 9 248 51 18 16 208 37 | 34 32 666 115 52 46 567 89 | 11 5 63 5 8 0 51 8 | 0 0 2 0 0 0 0 | 0 0 0 0 0 0 | 0 0 5 3 0 0 | 45 37 736 123 60 46 625 98 |
| Mid-Day Peak Hour (12-00 N - 1:00 PM) PM Peak Hour (3:30 - 4:30 PM) Tuesday, May 14, 2019 Daily AM Peak Hour (8:45 - 9:45 AM) Mid-Day Peak Hour (1:00 - 2:00 PM) Monday, May 20, 2019 Daily AM Peak Hour (8:45 - 9:45 AM) Mid-Day Peak Hour (12:00 N - 1:00 PM) PM Peak Hour (4:15 - 5:15 PM) Tuesday, May 21, 2019 Daily AM Peak Hour (8:45 - 9:45 AM) Mid-Day Peak Hour (12:45 - 1:45 PM) Tuesday, May 21, 2019 Daily AM Peak Hour (8:45 - 9:45 AM) Mid-Day Peak Hour (12:45 - 1:45 PM) PM Peak Hour (8:45 - 9:45 AM) Wednesday, May 22, 2019 Daily AM Peak Hour (8:45 - 9:45 AM) Mid-Day Peak Hour (10-2:00 PM) | 24 440 65 35 30 380 53 29 28 505 51 | 4 44 5 7 0 35 7 5 1 | 0 0 0 0 0 0 0 | 0 0 0 0 0 | 0 4 2 0 0 2 1 0 | 488 72 42 30 417 61 34 29 | 8 226 50 17 16 187 36 14 8 | 1 19 0 1 0 16 1 3 | 0 2 0 0 0 0 3 0 | 0 | 0 1 1 0 0 | 9 248 51 18 16 208 37 | 666 115 52 46 567 89 | 5 63 5 8 0 51 8 | 0 2 0 0 0 0 | 0 0 0 0 0 | 0 5 3 0 0 | 736 123 60 46 625 98 |
| PM Peak Hour (3:30-4:30 PM) Tuesday, May 14, 2019 Daily AM Peak Hour (8:45-9:45 AM) Mid-Day Peak Hour (1:00-2:00 PM) PM Peak Hour (8:45-9:45 AM) Mid-Day Peak Hour (1:200 N-1:00 PM) PM Peak Hour (8:45-9:45 AM) Mid-Day Peak Hour (8:45-9:45 AM) Tuesday, May 21, 2019 Daily AM Peak Hour (8:45-9:45 AM) Mid-Day Peak Hour (8:45-9:45 AM) Mid-Day Peak Hour (8:45-9:45 AM) Wednesday, May 22, 2019 Daily AM Peak Hour (8:45-9:45 AM) Wednesday, May 22, 2019 Daily AM Peak Hour (8:45-9:45 AM) Wid-Day Peak Hour (8:45-9:45 AM) Mid-Day Peak Hour (8:45-9:45 AM) Mid-Day Peak Hour (8:45-9:45 AM) Mid-Day Peak Hour | 440 65 35 30 380 53 29 28 505 51 27 | 44 5 7 0 35 7 5 1 | 0 0 0 0 0 0 0 | 0 0 0 0 0 0 0 | 4 2 0 0 0 0 1 1 0 0 0 0 0 0 0 0 0 0 0 0 0 | 488 72 42 30 417 61 34 29 | 226 50 17 16 187 36 14 | 19 0 1 0 16 1 3 | 2 0 0 0 0 | 0 0 0 0 | 1 1 0 0 | 248 51 18 16 208 37 | 666 115 52 46 567 89 | 63 5 8 0 51 8 | 2 0 0 0 0 | 0 0 0 0 | 5 3 0 0 | 736 123 60 46 625 98 |
| Tuesday, May 14, 2019 Daily AM Peak Hour (8:45 - 9:45 AM) Mid-Day Peak Hour (1:00 - 2:00 PM) PM Peak Hour (4:00 - 5:00 PM) Monday, May 20, 2019 Daily AM Peak Hour (1:200 N - 1:00 PM) PM Peak Hour (4:15 - 9:45 AM) Tuesday, May 21, 2019 Daily AM Peak Hour (8:45 - 9:45 AM) Mid-Day Peak Hour (12:45 - 1:45 PM) PM Peak Hour (3:00 - 4:00 PM) PM Peak Hour (8:45 - 9:45 AM) Wednesday, May 22, 2019 Daily AM Peak Hour (8:45 - 9:45 AM) Wednesday, May 22, 2019 Daily AM Peak Hour (8:45 - 9:45 AM) Mid-Day Peak Hour (1:00 - 2:00 PM) PM Peak Hour | 65 35 30 380 53 29 28 505 51 27 | 5 7 0 35 7 5 1 | 0 0 0 0 0 0 0 | 0 0 0 0 0 0 | 2 0 0 2 1 0 0 | 72 42 30 417 61 34 29 | 50 17 16 187 36 14 | 0 1 0 16 1 3 | 0 0 0 3 0 | 0 0 0 0 0 0 | 1 0 0 2 0 | 51 18 16 208 37 17 | 115 52 46 567 89 | 5 8 0 51 8 | 0 0 0 3 0 | 0 0 0 | 3 0 0 4 1 | 123 60 46 625 98 |
| Daily AM Peak Hour (8:45-9:45 AM) Mid-Day Peak Hour (1:00-2:00 PM) PM Peak Hour (4:00-5:00 PM) Monday, May 20, 2019 Daily AM Peak Hour (1:200 N-1:00 PM) PM Peak Hour (4:15-5:15 PM) Tuesday, May 21, 2019 Daily AM Peak Hour (8:45-9:45 AM) Mid-Day Peak Hour (12:45-1:45 PM) PM Peak Hour (12:45-1:45 PM) PM Peak Hour (8:45-9:45 AM) Mid-Day Peak Hour (8:45-9:45 AM) Wednesday, May 22, 2019 Daily AM Peak Hour (8:45-9:45 AM) Mid-Day Peak Hour (10:00-2:00 PM) PM Peak Hour | 65 35 30 380 53 29 28 505 51 27 | 5 7 0 35 7 5 1 | 0 0 0 0 0 0 0 | 0 0 0 0 0 0 | 2 0 0 2 1 0 0 | 72 42 30 417 61 34 29 | 50 17 16 187 36 14 | 0 1 0 16 1 3 | 0 0 0 3 0 | 0 0 0 0 0 0 | 1 0 0 2 0 | 51 18 16 208 37 17 | 115 52 46 567 89 | 5 8 0 51 8 | 0 0 0 3 0 | 0 0 0 | 3 0 0 4 1 | 123 60 46 625 98 |
| (845 - 9.45 AM) Mid-Day Peak Hour (1:00 - 2:00 PM) PM Peak Hour (4:00 - 5:00 PM) Monday, May 20, 2019 Daily AM Peak Hour (8:45 - 9.45 AM) Mid-Day Peak Hour (1:2:00 N - 1:00 PM) Tuesday, May 21, 2019 Daily AM Peak Hour (8:45 - 9.45 AM) Mid-Day Peak Hour (12:45 - 1.45 PM) PM Peak Hour (3:00 - 4:00 PM) Wednesday, May 22, 2019 Daily AM Peak Hour (8:45 - 9.45 AM) Wid-Day Peak Hour (1:45 - 1.45 PM) Wednesday, May 22, 2019 Daily AM Peak Hour (8:45 - 9.45 AM) Mid-Day Peak Hour (1:00 - 2:00 PM) PM Peak Hour | 35 30 380 53 29 28 505 51 27 | 7 0 35 7 5 1 | 0 0 0 0 0 | 0 0 0 0 0 | 0 0 2 1 0 | 42 30 417 61 34 29 | 17 16 187 36 14 8 | 1 0 16 1 3 | 0 0 3 0 | 0 0 0 0 | 0 0 2 0 | 18 16 208 37 17 | 52 46 567 89 | 8 0 51 8 8 | 0 0 3 0 | 0 0 0 0 | 0 0 4 1 | 60 46 625 98 |
| Mid-Day Peak Hour (1:00 - 2:00 PM) PM Peak Hour (4:00 - 5:00 PM) Monday, May 20, 2019 Daily AM Peak Hour (8:45 - 9:45 AM) Mid-Day Peak Hour (4:15 - 5:15 PM) Tuesday, May 21, 2019 Daily AM Peak Hour (8:45 - 9:45 AM) Mid-Day Peak Hour (8:45 - 9:45 AM) Mid-Day Peak Hour (8:45 - 9:45 AM) Mid-Day Peak Hour (8:25 - 9:45 AM) Wednesday, May 22, 2019 Daily AM Peak Hour (8:00 - 4:00 PM) Wednesday, May 22, 2019 Daily AM Peak Hour (8:45 - 9:45 AM) Mid-Day Peak Hour (8:45 - 9:45 AM) Mid-Day Peak Hour (1:00 - 2:00 PM) | 380 53 29 28 505 51 27 | 0 35 7 5 1 | 0 0 0 0 | 0 0 0 0 0 0 0 | 0 2 1 0 0 | 30 417 61 34 29 | 16 187 36 14 8 | 0 16 1 3 | 0 3 0 | 0 0 0 | 0 2 0 0 | 208 37 17 | 46 567 89 | 51 8 8 | 0 3 0 | 0 0 0 | 0 4 1 | 46 625 98 |
| PM Peak Hour (4:00 - 5:00 PM) Monday, May 20, 2019 Daily AM Peak Hour (8:45 - 9:45 AM) Mid-Day Peak Hour (1:2:00 N - 1:00 PM) PM Peak Hour (8:45 - 9:45 AM) Tuesday, May 21, 2019 Daily AM Peak Hour (8:45 - 9:45 AM) Mid-Day Peak Hour (1:2:45 - 1:45 PM) PM Peak Hour (3:00 - 4:00 PM) Wednesday, May 22, 2019 Daily AM Peak Hour (8:45 - 9:45 AM) Mid-Day Peak Hour (1:00 - 2:00 PM) PM Peak Hour | 380 53 29 28 505 51 27 | 35 7 5 1 | 0 0 0 0 1 1 | 0 0 0 0 0 0 | 2 1 0 0 | 417 61 34 29 | 187 36 14 8 | 16 1 3 | 3 0 | 0 0 | 2 0 | 208 37 17 | 567 89 | 51 8 8 | 3 0 | 0 0 | 4 | 625 98 |
| Monday, May 20, 2019 Daily AM Peak Hour (8.45-9.45 AM) Mid-Day Peak Hour (1200 N-1:00 PM) PM Peak Hour (4:15-5:15 PM) Tuesday, May 21, 2019 Daily AM Peak Hour (8.45-9.45 AM) Mid-Day Peak Hour (1245-1:45 PM) PM Peak Hour (3:00-4:00 PM) Wednesday, May 22, 2019 Daily AM Peak Hour (8:45-9.45 AM) Mid-Day Peak Hour (1:00-4:00 PM) Wednesday, May 22, 2019 Daily AM Peak Hour (8:45-9.45 AM) Mid-Day Peak Hour (1:00-2:00 PM) PM Peak Hour | 53 29 28 505 51 27 | 7 5 1 40 4 | 0 0 0 | 0 0 0 | 1 0 0 | 61 34 29 546 | 36 14 8 | 1 3 1 | 0 | 0 | 0 | 37 17 | 89 | 8 | 0 | 0 | 1 | 98 |
| Daily AM Peak Hour (8:45 - 9:45 AM) Mid-Day Peak Hour (1:200 N - 1:00 PM) PM Peak Hour (4:15 - 5:15 PM) Tuesday, May 21, 2019 Daily AM Peak Hour (8:45 - 9:45 AM) Mid-Day Peak Hour (1:245 - 1:45 PM) PM Peak Hour (3:00 - 4:00 PM) Wednesday, May 22, 2019 Daily AM Peak Hour (8:45 - 9:45 AM) Mid-Day Peak Hour (1:00 - 2:00 PM) | 53 29 28 505 51 27 | 7 5 1 40 4 | 0 0 0 | 0 0 0 | 1 0 0 | 61 34 29 546 | 36 14 8 | 1 3 1 | 0 | 0 | 0 | 37 17 | 89 | 8 | 0 | 0 | 1 | 98 |
| AM Peak Hour (845 - 9.45 AM) Mid-Day Peak Hour (12:00 N - 1:00 PM) PM Peak Hour (415 - 5:15 PM) Tuesday, May 21, 2019 Daily AM Peak Hour (845 - 9.45 AM) Mid-Day Peak Hour (12:45 - 1:45 PM) PM Peak Hour (3:00 - 4:00 PM) Wednesday, May 22, 2019 Daily AM Peak Hour (845 - 9.45 AM) Mid-Day Peak Hour (1:00 - 2:00 PM) PM Peak Hour | 53 29 28 505 51 27 | 7 5 1 40 4 | 0 0 0 | 0 0 0 | 1 0 0 | 61 34 29 546 | 36 14 8 | 1 3 1 | 0 | 0 | 0 | 37 17 | 89 | 8 | 0 | 0 | 1 | 98 |
| Mid-Day Peak Hour (12:00 N - 1:00 PM) PM Peak Hour (4:15 - 5:15 PM) Tuesday, May 21, 2019 Daily AM Peak Hour (6:45 - 9:45 AM) Mid-Day Peak Hour (12:45 - 1:45 PM) PM Peak Hour (3:00 - 4:00 PM) Wednesday, May 22, 2019 Daily AM Peak Hour (8:45 - 9:45 AM) Mid-Day Peak Hour (10:0 - 2:00 PM) Mid-Day Peak Hour | 28 505 51 27 | 40 4 | 0 1 1 | 0 0 0 | 0 | 29 546 | 8 | 1 | | | | | 43 | | | | 0 | 51 |
| PM Peak Hour (4:15 - 5:15 PM) Tuesday, May 21, 2019 Daily AM Peak Hour (8:45 - 9:45 AM) Mid-Day Peak Hour (12:45 - 1:45 PM) PM Peak Hour (3:00 - 4:00 PM) Wednesday, May 22, 2019 Daily AM Peak Hour (8:45 - 9:45 AM) Mid-Day Peak Hour (1:00 - 2:00 PM) PM Peak Hour | 505 51 27 | 40 | 1 | 0 | 0 | 546 | | | 0 | 0 | 0 | 9 | | | 0 | 0 | | |
| Tuesday, May 21, 2019 Daily AM Peak Hour (8:45 - 9:45 AM) Mid-Day Peak Hour (12:45 - 1:45 PM) PM Peak Hour (3:00 - 4:00 PM) Wednesday, May 22, 2019 Daily AM Peak Hour (8:45 - 9:45 AM) Mid-Day Peak Hour (1:00 - 2:00 PM) PM Peak Hour | 51 27 | 4 | 1 | 0 | | | 225 | 27 | | | | • | 36 | 2 | - | U | 0 | 38 |
| Daily AM Peak Hour (8.45 - 9.45 AM) Mid-Day Peak Hour (12.45 - 1.45 PM) PM Peak Hour (3.00 - 4.00 PM) Wednesday, May 22, 2019 Daily AM Peak Hour (8.45 - 9.45 AM) Mid-Day Peak Hour (100 - 2.00 PM) PM Peak Hour | 51 27 | 4 | 1 | 0 | | | 225 | 27 | | | | | | | | | | |
| (8.45 - 9.45 AM) Mid-Day Peak Hour (12.45 - 1.45 PM) PM Peak Hour (3.00 - 4.00 PM) Wednesday, May 22, 2019 Daily AM Peak Hour (8.45 - 9.45 AM) Mid-Day Peak Hour (100 - 2.00 PM) PM Peak Hour | 27 | | | | 0 | 56 | | 41 | 3 | 0 | 0 | 255 | 730 | 67 | 4 | 0 | 0 | 801 |
| Mid-Day Peak Hour (12-45 - 1-45 PM) PM Peak Hour (3:00 - 4:00 PM) Wednesday, May 22, 2019 Daily AM Peak Hour (8:45 - 9:45 AM) Mid-Day Peak Hour (1:00 - 2:00 PM) PM Peak Hour | | 5 | 0 | 0 | | | 53 | 3 | 0 | 0 | 0 | 56 | 104 | 7 | 1 | 0 | 0 | 112 |
| PM Peak Hour (3.00 - 4.00 PM) Wednesday, May 22, 2019 Daily AM Peak Hour (8.45 - 9.45 AM) Mid-Day Peak Hour (1:00 - 2:00 PM) PM Peak Hour | 30 | | | U | 0 | 32 | 18 | 3 | 0 | 0 | 0 | 21 | 45 | 8 | 0 | 0 | 0 | 53 |
| Wednesday, May 22, 2019 Daily AM Peak Hour (8:45-9:45 AM) Mid-Day Peak Hour (1:00-2:00 PM) PM Peak Hour | | 4 | 0 | 0 | 0 | 34 | 12 | 2 | 0 | 0 | 0 | 14 | 42 | 6 | 0 | 0 | 0 | 48 |
| Daily AM Peak Hour (8:45 - 9:45 AM) Mid-Day Peak Hour (1:00 - 2:00 PM) PM Peak Hour | | | | | | | | | | | | | | | | | | |
| (8:45 - 9:45 AM) Mid-Day Peak Hour (1:00 - 2:00 PM) PM Peak Hour | 435 | 49 | 1 | 1 | 1 | 487 | 211 | 23 | 2 | 0 | 0 | 236 | 646 | 72 | 3 | 1 | 1 | 723 |
| (1:00 - 2:00 PM) PM Peak Hour | 53 | 5 | 0 | 0 | 0 | 58 | 50 | 1 | 0 | 0 | 0 | 51 | 103 | 6 | 0 | 0 | 0 | 109 |
| | 36 | 2 | 0 | 0 | 1 | 39 | 18 | 2 | 0 | 0 | 0 | 20 | 54 | 4 | 0 | 0 | 1 | 59 |
| | 23 | 5 | 0 | 0 | 0 | 28 | 9 | 1 | 0 | 0 | 0 | 10 | 32 | 6 | 0 | 0 | 0 | 38 |
| Thursday, May 23, 2019 | | | | | | | | | | | | | | | | | | |
| Daily | 485 | 38 | 0 | 0 | 0 | 523 | 230 | 24 | 2 | 0 | 0 | 256 | 715 | 62 | 2 | 0 | 0 | 779 |
| AM Peak Hour (8:30 - 9:30 AM) | 61 | 3 | 0 | 0 | 0 | 64 | 39 | 1 | 0 | 0 | 0 | 40 | 100 | 4 | 0 | 0 | 0 | 104 |
| Mid-Day Peak Hour | 46 | 3 | 0 | 0 | 0 | 49 | 20 | 1 | 0 | 0 | 0 | 21 | 66 | 4 | 0 | 0 | 0 | 70 |
| PM Peak Hour | 35 | 3 | 0 | 0 | 0 | 38 | 11 | 3 | 0 | 0 | 0 | 14 | 46 | 6 | 0 | 0 | 0 | 52 |
| Friday, May 24, 2019 | | | | | | | | | | | | | | | | | | |
| Daily AM Peak Hour | 462 56 | 30 4 | 0 | 0 | 2 | 494 61 | 219 50 | 15 1 | 0 | 0 | 3 | 239 52 | 681 106 | 45 5 | 0 | 0 | 5 2 | 733 113 |
| (8:45 - 9:45 AM) | | | | | | | | | | | | | | | | | | |
| Mid-Day Peak Hour (12:15 - 1:15 PM) | 53 | 4 | 0 | 0 | 0 | 57 | 18 | 0 | 0 | 0 | 0 | 18 | 71 | 4 | 0 | 0 | 0 | 75 |
| PM Peak Hour (3:00 - 4:00 PM) | 39 | 3 | 0 | 0 | 0 | 42 | 20 | 1 | 0 | 0 | 0 | 21 | 59 | 4 | 0 | 0 | 0 | 63 |
| Weekday Average (8 Days) | | | | | | | | | | | | | | | | | | |
| Daily | 445 | 38 | 0 | 0 | 2 | 485 | 209 | 20 | 3 | 0 | 1 | 233 | 654 | 58 | 3 | 0 | 3 | 718 |
| AM Peak Hour | 57 | 4 | 0 | 0 | 1 | 62 | 46 | 2 | 0 | 0 | 0 | 48 | 103 | 6 | 0 | 0 | 1 | 110 |
| Mid-Day Peak Hour PM Peak Hour | 36 31 | 5 4 | 0 | 0 | 0 | 41 35 | 16 12 | 2 1 | 0 | 0 | 0 | 18 13 | 52 43 | 7 5 | 0 | 0 | 0 | 59 48 |
| | | | | | | | | | | | | | | | | | | |
| Maximums (by category) Daily | 505 | 49 | 1 | 1 | 4 | | 230 | 27 | 3 | 0 | 3 | | 730 | 72 | 4 | 1 | 5 | |
| AM Peak Hour | | 49 7 | 1 | 0 | 2 | | 53 | 4 | 2 | 0 | 3 1 | | 115 | 8 | 2 | 0 | 3 | |
| Mid-Day Peak Hour | 65 | | | | 1 | | 20 | 3 | 0 | 0 | 0 | | 71 | 11 | 0 | 0 | 1 | |
| PM Peak Hour | 65 53 | 8 | 0 | 0 | | | 20 | 3 | 0 | 0 | 0 | | 59 | 9 | 0 | 0 | 1 | |



IRSCH GREEN

Hirsch/Green Transportation Consulting, Inc.

CHEVAL BLANC HOTEL (BEVERLY HILLS) \ ALLEY VOLUMES (WEEKDAY)

FIGURE 3(a)

EXISTING ALLEY TRAFFIC VOLUMES WEEKDAY (8-DAY AVERAGE)

Appendix B: LOS Worksheets

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|--|-------------|-------------|-------------|-------------|-------------|--------------|---|-------------|-------------|-------------|-------------|-------------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ሻ | ∱ ⊅ | | ሻ | ∱ ∱ | | | ∱ ∱ | | 7 | ^ | 7 |
| Traffic Volume (veh/h) | 23 | 1317 | 26 | 80 | 1484 | 29 | 0 | 75 | 28 | 28 | 300 | 45 |
| Future Volume (veh/h) | 23 | 1317 | 26 | 80 | 1484 | 29 | 0 | 75 | 28 | 28 | 300 | 45 |
| Initial Q (Qb), veh | 0 | 10 | 0 | 0 | 15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | | 0.97 | 1.00 | | 0.99 | 1.00 | | 0.97 | 0.99 | | 0.98 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach | | No | | | No | | _ | No | | | No | |
| Adj Sat Flow, veh/h/ln | 1367 | 1367 | 1367 | 1367 | 1367 | 1367 | 0 | 1660 | 1660 | 1660 | 1660 | 1660 |
| Adj Flow Rate, veh/h | 26 | 1463 | 28 | 89 | 1649 | 31 | 0 | 83 | 8 | 31 | 333 | 26 |
| Peak Hour Factor | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Percent Heavy Veh, % | 3 | 3 | 3 | 3 | 3 | 3 | 0 | 3 | 3 | 3 | 3 | 3 |
| Cap, veh/h | 117 | 1916 | 35 | 72 | 1921 | 32 | 0 | 483 | 46 | 253 | 525 | 230 |
| Arrive On Green | 0.73 | 0.73 | 0.73 | 0.73 | 0.73 | 0.73 | 0.00 | 0.17 | 0.17 | 0.17 | 0.17 | 0.17 |
| Sat Flow, veh/h | 240 | 2606 | 50 | 288 | 2608 | 49 | 0 | 2987 | 276 | 1282 | 3154 | 1379 |
| Grp Volume(v), veh/h | 26 | 728 | 763 | 89 | 820 | 860 | 0 | 44 | 47 | 31 | 333 | 26 |
| Grp Sat Flow(s),veh/h/ln | 240 | 1299 | 1356 | 288 | 1299 | 1358 | 0 | 1577 | 1602 | 1282 | 1577 | 1379 |
| Q Serve(g_s), s | 8.8 | 33.9 | 34.1 | 27.1 | 45.4 | 45.9 | 0.0 | 2.4 | 2.5 | 2.1 | 9.8 | 1.6 |
| Cycle Q Clear(g_c), s | 54.7 | 33.9 | 34.1 | 61.1 | 45.4 | 45.9 | 0.0 | 2.4 | 2.5 | 4.6 | 9.8 | 1.6 |
| Prop In Lane | 1.00 | 054 | 0.04 | 1.00 | 054 | 0.04 | 0.00 | 000 | 0.17 | 1.00 | F0F | 1.00 |
| Lane Grp Cap(c), veh/h | 117 | 954 | 997 | 72 | 954 | 998 | 0 | 263 | 267 | 253 | 525 | 230 |
| V/C Ratio(X) | 0.22 | 0.76 | 0.76 | 1.24 | 0.86 | 0.86 | 0.00 | 0.17 | 0.17 | 0.12 381 | 0.63 | 0.11 |
| Avail Cap(c_a), veh/h | 138 1.00 | 954 1.00 | 996 1.00 | 186 1.00 | 954 1.00 | 997 | 1.00 | 420 1.00 | 426 1.00 | 1.00 | 839 1.00 | 367 1.00 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 0.41 | 0.41 | 1.00 0.41 | 0.00 | 0.99 | 0.99 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 36.0 | 8.5 | 8.5 | 50.0 | 10.4 | 10.4 | 0.00 | 35.7 | 35.8 | 37.8 | 38.8 | 35.4 |
| Uniform Delay (d), s/veh Incr Delay (d2), s/veh | 4.3 | 5.8 | 5.6 | 145.4 | 4.4 | 4.3 | 0.0 | 0.3 | 0.3 | 0.2 | 1.3 | 0.2 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.8 | 0.8 | 0.0 | 3.2 | 2.9 | 0.0 | 0.0 | 0.0 | 0.2 | 0.0 | 0.2 |
| %ile BackOfQ(50%),veh/ln | 0.7 | 9.6 | 9.9 | 4.7 | 12.8 | 13.3 | 0.0 | 1.0 | 1.0 | 0.0 | 3.9 | 0.6 |
| Unsig. Movement Delay, s/veh | | 3.0 | 9.9 | 7.1 | 12.0 | 10.0 | 0.0 | 1.0 | 1.0 | 0.1 | 0.0 | 0.0 |
| LnGrp Delay(d),s/veh | 40.4 | 15.1 | 14.8 | 195.4 | 18.0 | 17.6 | 0.0 | 36.0 | 36.1 | 38.0 | 40.1 | 35.6 |
| LnGrp LOS | D | В | В | F | В | В | A | D | D | D | D | D |
| Approach Vol, veh/h | | 1517 | | | 1769 | | <u>, , , , , , , , , , , , , , , , , , , </u> | 91 | | | 390 | |
| Approach Delay, s/veh | | 15.4 | | | 26.7 | | | 36.1 | | | 39.6 | |
| Approach LOS | | В | | | C | | | D | | | D | |
| | | | | | | | | | | | | |
| Timer - Assigned Phs | | 2 | | 4 | | 6 | | 8 | | | | |
| Phs Duration (G+Y+Rc), s | | 78.9 | | 21.1 | | 78.9 | | 21.1 | | | | |
| Change Period (Y+Rc), s | | 5.4 | | 4.5 | | 5.4 | | 4.5 | | | | |
| Max Green Setting (Gmax), s | | 63.5 | | 26.6 | | 63.5 | | 26.6 | | | | |
| Max Q Clear Time (g_c+l1), s | | 56.7 | | 11.8 | | 63.1 | | 4.5 | | | | |
| Green Ext Time (p_c), s | | 6.1 | | 2.1 | | 0.4 | | 0.4 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 6th Ctrl Delay | | | 23.7 | | | | | | | | | |
| HCM 6th LOS | | | С | | | | | | | | | |

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|---------------------------|------|-----------|------|----------|-----------|------|------|-----------|------|-------------|------------|------|--|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR | |
| Lane Configurations | ħ | ħβ | | ሻ | ħβ | | ሻ | ħβ | | ሻ | ∱ } | | |
| Traffic Volume (veh/h) | 37 | 1491 | 25 | 91 | 1270 | 36 | 18 | 339 | 143 | 21 | 472 | 57 | |
| Future Volume (veh/h) | 37 | 1491 | 25 | 91 | 1270 | 36 | 18 | 339 | 143 | 21 | 472 | 57 | |
| Initial Q (Qb), veh | 0 | 10 | 0 | 0 | 15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Ped-Bike Adj(A_pbT) | 1.00 | | 0.98 | 1.00 | | 0.97 | 0.99 | | 0.97 | 0.99 | | 0.98 | |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Work Zone On Approac | :h | No | | | No | | | No | | | No | | |
| Adj Sat Flow, veh/h/ln | 1367 | 1367 | 1367 | 1367 | 1367 | 1367 | 1660 | 1660 | 1660 | 1660 | 1660 | 1660 | |
| Adj Flow Rate, veh/h | 41 | 1657 | 27 | 101 | 1411 | 38 | 20 | 377 | 139 | 23 | 524 | 53 | |
| Peak Hour Factor | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | |
| Percent Heavy Veh, % | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | |
| Cap, veh/h | 109 | 1734 | 20 | 72 | 1708 | 41 | 123 | 523 | 190 | 154 | 673 | 68 | |
| Arrive On Green | 0.66 | 0.66 | 0.66 | 0.66 | 0.66 | 0.66 | 0.47 | 0.47 | 0.47 | 0.23 | 0.23 | 0.23 | |
| Sat Flow, veh/h | 300 | 2615 | 43 | 239 | 2582 | 69 | 825 | 2244 | 814 | 872 | 2887 | 291 | |
| Grp Volume(v), veh/h | 41 | 822 | 862 | 101 | 709 | 740 | 20 | 263 | 253 | 23 | 286 | 291 | |
| Grp Sat Flow(s),veh/h/lr | | 1299 | 1359 | 239 | 1299 | 1352 | 825 | 1577 | 1481 | 872 | 1577 | 1601 | |
| Q Serve(g_s), s | 11.9 | 58.7 | 59.3 | 6.6 | 41.0 | 41.2 | 2.2 | 13.4 | 13.9 | 2.5 | 17.0 | 17.1 | |
| Cycle Q Clear(g_c), s | 53.1 | 58.7 | 59.3 | 65.9 | 41.0 | 41.2 | 19.3 | 13.4 | 13.9 | 16.3 | 17.0 | 17.1 | |
| Prop In Lane | 1.00 | | 0.03 | 1.00 | | 0.05 | 1.00 | | 0.55 | 1.00 | | 0.18 | |
| Lane Grp Cap(c), veh/h | | 856 | 897 | 72 | 856 | 892 | 123 | 368 | 345 | 154 | 368 | 373 | |
| V/C Ratio(X) | 0.38 | 0.96 | 0.96 | 1.40 | 0.83 | 0.83 | 0.16 | 0.72 | 0.73 | 0.15 | 0.78 | 0.78 | |
| Avail Cap(c_a), veh/h | 146 | 856 | 895 | 88 | 856 | 891 | 151 | 420 | 394 | 183 | 420 | 426 | |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 2.00 | 2.00 | 2.00 | 1.00 | 1.00 | 1.00 | |
| Upstream Filter(I) | 0.34 | 0.34 | 0.34 | 1.00 | 1.00 | 1.00 | 0.83 | 0.83 | 0.83 | 1.00 | 1.00 | 1.00 | |
| Uniform Delay (d), s/vel | | 16.5 | 16.5 | 50.0 | 13.7 | 13.6 | 33.5 | 24.0 | 24.2 | 42.1 | 35.9 | 36.0 | |
| Incr Delay (d2), s/veh | 3.4 | 10.7 | 10.6 | 245.5 | 9.1 | 8.8 | 0.5 | 4.1 | 5.0 | 0.4 | 7.9 | 8.1 | |
| Initial Q Delay(d3),s/veh | | 6.1 | 5.8 | 0.0 | 3.2 | 3.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | |
| %ile BackOfQ(50%),vel | | 19.3 | 20.1 | 6.7 | 14.1 | 14.6 | 0.4 | 4.3 | 4.2 | 0.5 | 7.3 | 7.5 | |
| Unsig. Movement Delay | | | | 0.7 | | 11.0 | 0.1 | 1.0 | | 0.0 | 7.0 | 7.0 | |
| LnGrp Delay(d),s/veh | 44.9 | 33.4 | 32.9 | 295.5 | 26.0 | 25.4 | 34.0 | 28.2 | 29.2 | 42.5 | 43.8 | 44.0 | |
| LnGrp LOS | D | С | C | F | C | C | С | C | C | D | D | D | |
| Approach Vol, veh/h | | 1725 | | <u> </u> | 1550 | | | 536 | | | 600 | | |
| Approach Delay, s/veh | | 33.4 | | | 43.3 | | | 28.9 | | | 43.9 | | |
| Approach LOS | | 00.4 C | | | 43.3 D | | | 20.3 C | | | 43.3 D | | |
| | | U | | | U | | | U | | | U | | |
| Timer - Assigned Phs | | 2 | | 4 | | 6 | | 8 | | | | | |
| Phs Duration (G+Y+Rc) | | 71.3 | | 28.7 | | 71.3 | | 28.7 | | | | | |
| Change Period (Y+Rc), | | 5.4 | | 5.4 | | 5.4 | | 5.4 | | | | | |
| Max Green Setting (Gm | | 62.6 | | 26.6 | | 62.6 | | 26.6 | | | | | |
| Max Q Clear Time (g_c | | 61.3 | | 19.1 | | 67.9 | | 21.3 | | | | | |
| Green Ext Time (p_c), s | 5 | 1.3 | | 2.3 | | 0.0 | | 1.6 | | | | | |
| Intersection Summary | | | | | | | | | | | | | |
| HCM 6th Ctrl Delay | | | 37.8 | | | | | | | | | | |
| HCM 6th LOS | | | D | | | | | | | | | | |

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|-----------------------------------|---------|------------|--------|-------|------------|------------|---------|------------|----------|----------|------------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | ∱ } | | | €Î∌ | | ň | ∱ } | | ሻ | ↑ ↑ | |
| Traffic Volume (vph) | 0 | 637 | 41 | 127 | 1347 | 21 | 10 | 82 | 29 | 30 | 327 | 49 |
| Future Volume (vph) | 0 | 637 | 41 | 127 | 1347 | 21 | 10 | 82 | 29 | 30 | 327 | 49 |
| Ideal Flow (vphpl) | 1700 | 1700 | 1700 | 1400 | 1400 | 1400 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 |
| Total Lost time (s) | | 5.1 | | | 5.1 | | 4.5 | 4.5 | | 4.5 | 4.5 | |
| Lane Util. Factor | | 0.95 | | | 0.95 | | 1.00 | 0.95 | | 1.00 | 0.95 | |
| Frpb, ped/bikes | | 1.00 | | | 1.00 | | 1.00 | 0.99 | | 1.00 | 0.99 | |
| Flpb, ped/bikes | | 1.00 | | | 1.00 | | 0.98 | 1.00 | | 0.96 | 1.00 | |
| Frt | | 0.99 | | | 1.00 | | 1.00 | 0.96 | | 1.00 | 0.98 | |
| Flt Protected | | 1.00 | | | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | | 3098 | | | 2559 | | 1543 | 2760 | | 1511 | 3057 | |
| Flt Permitted | | 1.00 | | | 0.74 | | 0.39 | 1.00 | | 0.68 | 1.00 | |
| Satd. Flow (perm) | | 3098 | | | 1903 | | 640 | 2760 | | 1078 | 3057 | |
| Peak-hour factor, PHF | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Adj. Flow (vph) | 0 | 671 | 43 | 134 | 1418 | 22 | 11 | 86 | 31 | 32 | 344 | 52 |
| RTOR Reduction (vph) | 0 | 4 | 0 | 0 | 1 | 0 | 0 | 24 | 0 | 0 | 12 | 0 |
| Lane Group Flow (vph) | 0 | 710 | 0 | 0 | 1573 | 0 | 11 | 93 | 0 | 32 | 384 | 0 |
| Confl. Peds. (#/hr) | 100 | | 29 | 29 | | 100 | 24 | | 33 | 33 | | 24 |
| Confl. Bikes (#/hr) | | | 3 | | | 2 | | | 1 | | | 1 |
| Heavy Vehicles (%) | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% |
| Parking (#/hr) | | | | | | | | 8 | 8 | | | |
| Turn Type | | NA | | pm+pt | NA | | Perm | NA | | Perm | NA | |
| Protected Phases | | 2 | | 1 | 6 | | | 8 | | | 4 | |
| Permitted Phases | | | | 6 | | | 8 | | | 4 | | |
| Actuated Green, G (s) | | 59.5 | | | 67.2 | | 23.2 | 23.2 | | 23.2 | 23.2 | |
| Effective Green, g (s) | | 59.5 | | | 67.2 | | 23.2 | 23.2 | | 23.2 | 23.2 | |
| Actuated g/C Ratio | | 0.60 | | | 0.67 | | 0.23 | 0.23 | | 0.23 | 0.23 | |
| Clearance Time (s) | | 5.1 | | | 5.1 | | 4.5 | 4.5 | | 4.5 | 4.5 | |
| Vehicle Extension (s) | | 5.0 | | | 5.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | | 1843 | | | 1308 | | 148 | 640 | | 250 | 709 | |
| v/s Ratio Prot | | 0.23 | | | c0.05 | | | 0.03 | | | c0.13 | |
| v/s Ratio Perm | | | | | c0.75 | | 0.02 | | | 0.03 | | |
| v/c Ratio | | 0.38 | | | 1.20 | | 0.07 | 0.15 | | 0.13 | 0.54 | |
| Uniform Delay, d1 | | 10.6 | | | 16.4 | | 30.0 | 30.5 | | 30.4 | 33.7 | |
| Progression Factor | | 1.00 | | | 0.52 | | 1.00 | 1.00 | | 0.43 | 0.39 | |
| Incremental Delay, d2 | | 0.6 | | | 95.5 | | 0.2 | 0.1 | | 0.2 | 0.7 | |
| Delay (s) | | 11.2 | | | 104.0 | | 30.2 | 30.6 | | 13.2 | 13.9 | |
| Level of Service | | В | | | F | | С | С | | В | В | |
| Approach Delay (s) | | 11.2 | | | 104.0 | | | 30.6 | | | 13.9 | |
| Approach LOS | | В | | | F | | | С | | | В | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 63.9 | Н | CM 2000 | Level of S | Service | | E | | | |
| HCM 2000 Volume to Capacit | v ratio | | 1.07 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 100.0 | S | um of lost | time (s) | | | 12.8 | | | |
| Intersection Capacity Utilization | on | | 109.2% | | CU Level | | | | Н | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

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|---------------------------|---------|------------|---------------|-------|------|------|------|----------|------|------|------|------|--|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR | |
| Lane Configurations | ሻ | ∱ } | | ሻ | ħβ | | ሻ | ^ | 7 | | ħβ | | |
| Traffic Volume (veh/h) | 74 | 549 | 73 | 129 | 1371 | 21 | 48 | 379 | 70 | 0 | 524 | 75 | |
| Future Volume (veh/h) | 74 | 549 | 73 | 129 | 1371 | 21 | 48 | 379 | 70 | 0 | 524 | 75 | |
| Initial Q (Qb), veh | 0 | 10 | 0 | 0 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Ped-Bike Adj(A_pbT) | 1.00 | | 0.95 | 0.99 | | 0.96 | 0.98 | | 0.91 | 1.00 | | 0.91 | |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Work Zone On Approac | ch | No | | | No | | | No | | | No | | |
| Adj Sat Flow, veh/h/ln | 1660 | 1660 | 1660 | 1367 | 1367 | 1367 | 1660 | 1660 | 1660 | 0 | 1660 | 1660 | |
| Adj Flow Rate, veh/h | 78 | 578 | 66 | 136 | 1443 | 21 | 51 | 399 | 18 | 0 | 552 | 68 | |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | |
| Percent Heavy Veh, % | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 0 | 3 | 3 | |
| Cap, veh/h | 72 | 2203 | 246 | 72 | 2030 | 28 | 131 | 817 | 333 | 0 | 724 | 89 | |
| Arrive On Green | 0.77 | 0.77 | 0.77 | 1.00 | 1.00 | 1.00 | 0.26 | 0.26 | 0.26 | 0.00 | 0.26 | 0.26 | |
| Sat Flow, veh/h | 358 | 2838 | 323 | 636 | 2619 | 38 | 785 | 3154 | 1285 | 0 | 2878 | 343 | |
| Grp Volume(v), veh/h | 78 | 320 | 324 | 136 | 715 | 749 | 51 | 399 | 18 | 0 | 310 | 310 | |
| Grp Sat Flow(s), veh/h/lr | n 358 | 1577 | 1584 | 636 | 1299 | 1358 | 785 | 1577 | 1285 | 0 | 1577 | 1560 | |
| Q Serve(g_s), s | 6.4 | 5.8 | 5.8 | 2.4 | 0.0 | 0.0 | 6.4 | 10.7 | 1.1 | 0.0 | 18.2 | 18.3 | |
| Cycle Q Clear(g_c), s | 6.8 | 5.8 | 5.8 | 8.8 | 0.0 | 0.0 | 24.8 | 10.7 | 1.1 | 0.0 | 18.2 | 18.3 | |
| Prop In Lane | 1.00 | | 0.20 | 1.00 | | 0.03 | 1.00 | | 1.00 | 0.00 | | 0.22 | |
| Lane Grp Cap(c), veh/h | 72 | 1221 | 1228 | 72 | 1006 | 1052 | 131 | 817 | 333 | 0 | 408 | 404 | |
| V/C Ratio(X) | 1.08 | 0.26 | 0.26 | 1.89 | 0.71 | 0.71 | 0.39 | 0.49 | 0.05 | 0.00 | 0.76 | 0.77 | |
| Avail Cap(c_a), veh/h | 348 | 1221 | 1227 | 524 | 1006 | 1052 | 131 | 817 | 333 | 0 | 408 | 404 | |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 2.00 | 2.00 | 2.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 0.51 | 0.51 | 0.51 | 0.92 | 0.92 | 0.92 | 0.00 | 0.35 | 0.35 | |
| Uniform Delay (d), s/vel | h 50.0 | 3.4 | 3.4 | 38.7 | 0.0 | 0.0 | 45.7 | 31.4 | 27.8 | 0.0 | 34.2 | 34.2 | |
| Incr Delay (d2), s/veh | 129.8 | 0.5 | 0.5 | 423.9 | 2.2 | 2.1 | 1.7 | 0.4 | 0.1 | 0.0 | 3.0 | 3.1 | |
| Initial Q Delay(d3),s/veh | า 0.0 | 0.2 | 0.2 | 0.0 | 0.6 | 0.6 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | |
| %ile BackOfQ(50%),vel | h/lr4.4 | 2.1 | 2.1 | 10.2 | 0.8 | 8.0 | 1.3 | 4.1 | 0.3 | 0.0 | 7.3 | 7.3 | |
| Unsig. Movement Delay | , s/veh | | | | | | | | | | | | |
| LnGrp Delay(d),s/veh | 179.8 | 4.1 | 4.1 | 462.6 | 2.8 | 2.7 | 47.4 | 31.8 | 27.9 | 0.0 | 37.1 | 37.4 | |
| LnGrp LOS | F | Α | Α | F | Α | Α | D | С | С | Α | D | D | |
| Approach Vol, veh/h | | 722 | | | 1600 | | | 468 | | | 620 | | |
| Approach Delay, s/veh | | 23.0 | | | 41.8 | | | 33.4 | | | 37.3 | | |
| Approach LOS | | С | | | D | | | С | | | D | | |
| Timer - Assigned Phs | | 2 | | 4 | | 6 | | 8 | | | | | |
| Phs Duration (G+Y+Rc) |), s | 82.9 | | 31.0 | | 82.9 | | 31.0 | | | | | |
| Change Period (Y+Rc), | S | 5.1 | | * 5.1 | | 5.1 | | 5.1 | | | | | |
| Max Green Setting (Gm | nax), s | 64.3 | | * 26 | | 64.3 | | 25.5 | | | | | |
| Max Q Clear Time (g_c | +l1), s | 8.8 | | 26.8 | | 10.8 | | 20.3 | | | | | |
| Green Ext Time (p_c), s | 3 | 13.9 | | 0.0 | | 37.0 | | 1.8 | | | | | |
| Intersection Summary | | | | | | | | | | | | | |
| HCM 6th Ctrl Delay | | | 35.9 | | | | | | | | | | |
| HCM 6th LOS | | | D | | | | | | | | | | |
| Notes | | | | | | | | | | | | | |

^{*} HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

| • | - | \searrow | • | ← | • | 4 | † | / | > | ļ | 4 |
|-------------------------------|------------|------------|-------|----------|------|------|------------|------|-------------|----------|------|
| Movement EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ↑ ↑ | | ሻ | ^ | 7 | * | ↑ ↑ | | * | ^ | 7 |
| Traffic Volume (veh/h) 0 | 481 | 60 | 76 | 1350 | 113 | 22 | 69 | 33 | 212 | 273 | 85 |
| Future Volume (veh/h) 0 | 481 | 60 | 76 | 1350 | 113 | 22 | 69 | 33 | 212 | 273 | 85 |
| Initial Q (Qb), veh 0 | 10 | 0 | 0 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) 1.00 | 10 | 0.97 | 0.99 | 10 | 0.97 | 0.95 | U | 0.92 | 0.94 | U | 0.94 |
| Parking Bus, Adj 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach | No | 1.00 | 1.00 | No | 1.00 | 1.00 | No | 1.00 | 1.00 | No | 1.00 |
| Adj Sat Flow, veh/h/ln 0 | 1660 | 1660 | 1367 | 1367 | 1367 | 1660 | 1660 | 1660 | 1660 | 1660 | 1660 |
| Adj Flow Rate, veh/h 0 | 486 | 53 | 77 | 1364 | 89 | 22 | 70 | 33 | 214 | 276 | 67 |
| Peak Hour Factor 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 |
| Percent Heavy Veh, % 0 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 |
| Cap, veh/h 0 | 1662 | 175 | 72 | 1505 | 649 | 291 | 468 | 200 | 415 | 1018 | 428 |
| Arrive On Green 0.00 | 0.77 | 0.77 | 0.58 | 0.58 | 0.58 | 0.22 | 0.22 | 0.22 | 0.07 | 0.32 | 0.32 |
| | 2943 | 310 | 703 | 2598 | 1120 | 977 | 2089 | 894 | 1581 | 3154 | 1327 |
| · | | | | | | | | | | | |
| Grp Volume(v), veh/h 0 | 267 | 272 | 77 | 1364 | 89 | 22 | 51 | 52 | 214 | 276 | 67 |
| Grp Sat Flow(s),veh/h/ln 0 | 1577 | 1593 | 703 | 1299 | 1120 | 977 | 1577 | 1405 | 1581 | 1577 | 1327 |
| Q Serve(g_s), s 0.0 | 5.0 | 5.1 | 5.8 | 46.5 | 3.6 | 1.8 | 2.6 | 3.0 | 6.9 | 6.5 | 3.6 |
| Cycle Q Clear(g_c), s 0.0 | 5.0 | 5.1 | 10.9 | 46.5 | 3.6 | 1.8 | 2.6 | 3.0 | 6.9 | 6.5 | 3.6 |
| Prop In Lane 0.00 | | 0.19 | 1.00 | | 1.00 | 1.00 | | 0.64 | 1.00 | | 1.00 |
| Lane Grp Cap(c), veh/h 0 | 913 | 924 | 72 | 1505 | 649 | 291 | 353 | 315 | 415 | 1018 | 428 |
| V/C Ratio(X) 0.00 | 0.29 | 0.29 | 1.07 | 0.91 | 0.14 | 0.08 | 0.14 | 0.16 | 0.52 | 0.27 | 0.16 |
| Avail Cap(c_a), veh/h 0 | 913 | 923 | 444 | 1505 | 649 | 346 | 442 | 394 | 415 | 1196 | 503 |
| HCM Platoon Ratio 1.00 | 1.33 | 1.33 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) 0.00 | 0.96 | 0.96 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh 0.0 | 5.6 | 5.6 | 50.0 | 19.3 | 9.6 | 30.8 | 31.1 | 31.3 | 29.1 | 25.1 | 24.1 |
| Incr Delay (d2), s/veh 0.0 | 0.8 | 0.8 | 126.4 | 9.5 | 0.4 | 0.1 | 0.2 | 0.2 | 0.5 | 0.1 | 0.2 |
| Initial Q Delay(d3),s/veh 0.0 | 0.3 | 0.3 | 0.0 | 3.4 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/lr0.0 | 2.0 | 2.1 | 4.3 | 16.6 | 0.9 | 0.4 | 1.0 | 1.0 | 1.5 | 2.5 | 1.2 |
| Unsig. Movement Delay, s/veh | | | | | | | | | | | |
| LnGrp Delay(d),s/veh 0.0 | 6.7 | 6.7 | 176.4 | 32.2 | 10.1 | 30.9 | 31.3 | 31.5 | 29.6 | 25.3 | 24.3 |
| LnGrp LOS A | Α | Α | F | С | В | С | С | С | С | С | С |
| Approach Vol, veh/h | 539 | | | 1530 | | | 125 | | | 557 | |
| Approach Delay, s/veh | 6.7 | | | 38.2 | | | 31.3 | | | 26.8 | |
| Approach LOS | Α | | | D | | | С | | | С | |
| | | | 1 | | C | 7 | | | | | |
| Timer - Assigned Phs | 2 | | 4 | | 6 | 7 | 8 | | | | |
| Phs Duration (G+Y+Rc), s | 63.0 | | 37.0 | | 63.0 | 9.9 | 27.1 | | | | |
| Change Period (Y+Rc), s | 5.1 | | * 4.7 | | 5.1 | 3.0 | * 4.7 | | | | |
| Max Green Setting (Gmax), s | 52.3 | | * 38 | | 52.3 | 6.9 | * 28 | | | | |
| Max Q Clear Time (g_c+l1), s | 7.1 | | 8.5 | | 48.5 | 8.9 | 5.0 | | | | |
| Green Ext Time (p_c), s | 7.9 | | 2.2 | | 3.5 | 0.0 | 0.6 | | | | |
| Intersection Summary | | | | | | | | | | | |
| HCM 6th Ctrl Delay | | 29.4 | | | | | | | | | |
| HCM 6th LOS | | С | | | | | | | | | |
| Notes | | | | | | | | | | | |

^{*} HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

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|---------------------------|---------|----------|---------------|------|-----------|-------|----------|----------|------|------|------------|------|--|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR | |
| Lane Configurations | | | | | 474 | | ሻ | ^ | | | ∱ } | | |
| Traffic Volume (veh/h) | 0 | 0 | 0 | 61 | 333 | 62 | 93 | 494 | 0 | 0 | 560 | 136 | |
| Future Volume (veh/h) | 0 | 0 | 0 | 61 | 333 | 62 | 93 | 494 | 0 | 0 | 560 | 136 | |
| Initial Q (Qb), veh | | | | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Ped-Bike Adj(A_pbT) | | | | 1.00 | | 0.91 | 0.99 | | 1.00 | 1.00 | | 0.96 | |
| Parking Bus, Adj | | | | 0.85 | 1.00 | 0.85 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.81 | |
| Work Zone On Approach | 1 | | | | No | | | No | | | No | | |
| Adj Sat Flow, veh/h/ln | | | | 1660 | 1660 | 1660 | 1660 | 1660 | 0 | 0 | 1660 | 1660 | |
| Adj Flow Rate, veh/h | | | | 66 | 358 | 45 | 100 | 531 | 0 | 0 | 602 | 113 | |
| Peak Hour Factor | | | | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | |
| Percent Heavy Veh, % | | | | 3 | 3 | 3 | 3 | 3 | 0 | 0 | 3 | 3 | |
| Cap, veh/h | | | | 114 | 646 | 85 | 409 | 1739 | 0 | 0 | 1311 | 245 | |
| Arrive On Green | | | | 0.31 | 0.31 | 0.31 | 0.55 | 0.55 | 0.00 | 0.00 | 0.55 | 0.55 | |
| Sat Flow, veh/h | | | | 366 | 2070 | 271 | 726 | 3237 | 0 | 0 | 2460 | 445 | |
| Grp Volume(v), veh/h | | | | 249 | 0 | 220 | 100 | 531 | 0 | 0 | 399 | 316 | |
| Grp Sat Flow(s), veh/h/ln | | | | 1385 | 0 | 1324 | 726 | 1577 | 0 | 0 | 1577 | 1245 | |
| Q Serve(g_s), s | | | | 9.1 | 0.0 | 8.2 | 5.8 | 5.4 | 0.0 | 0.0 | 9.1 | 9.2 | |
| Cycle Q Clear(g_c), s | | | | 9.1 | 0.0 | 8.2 | 14.9 | 5.4 | 0.0 | 0.0 | 9.1 | 9.2 | |
| Prop In Lane | | | | 0.26 | 0.0 | 0.20 | 1.00 | 0.1 | 0.00 | 0.00 | 0.1 | 0.36 | |
| Lane Grp Cap(c), veh/h | | | | 432 | 0 | 413 | 409 | 1739 | 0.00 | 0.00 | 870 | 686 | |
| V/C Ratio(X) | | | | 0.58 | 0.00 | 0.53 | 0.24 | 0.31 | 0.00 | 0.00 | 0.46 | 0.46 | |
| Avail Cap(c_a), veh/h | | | | 595 | 0.00 | 569 | 409 | 1739 | 0.00 | 0.00 | 870 | 686 | |
| HCM Platoon Ratio | | | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Upstream Filter(I) | | | | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 0.00 | 0.00 | 0.55 | 0.55 | |
| Uniform Delay (d), s/veh | | | | 17.3 | 0.0 | 17.0 | 12.6 | 7.3 | 0.0 | 0.0 | 8.1 | 8.1 | |
| Incr Delay (d2), s/veh | | | | 1.2 | 0.0 | 1.1 | 1.4 | 0.5 | 0.0 | 0.0 | 1.0 | 1.2 | |
| Initial Q Delay(d3),s/veh | | | | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | |
| %ile BackOfQ(50%),veh | /ln | | | 2.8 | 0.0 | 2.4 | 1.0 | 1.7 | 0.0 | 0.0 | 2.8 | 2.3 | |
| Unsig. Movement Delay, | | | | 2.0 | 0.0 | ۷.٦ | 1.0 | 1.7 | 0.0 | 0.0 | 2.0 | 2.0 | |
| LnGrp Delay(d),s/veh | 0/ 10/1 | | | 18.6 | 0.0 | 18.1 | 14.0 | 7.7 | 0.0 | 0.0 | 9.0 | 9.3 | |
| LnGrp LOS | | | | В | Α | В | В | A | Α | A | Α | Α | |
| Approach Vol, veh/h | | | | | 469 | | | 631 | | | 715 | | |
| Approach Delay, s/veh | | | | | 18.3 | | | 8.7 | | | 9.2 | | |
| Approach LOS | | | | | 10.3 B | | | Α. | | | 9.2 A | | |
| Approach LOS | | | | | D | | | А | | | A | | |
| Timer - Assigned Phs | | 2 | | | | 6 | | 8 | | | | | |
| Phs Duration (G+Y+Rc), | | 37.3 | | | | 37.3 | | 22.7 | | | | | |
| Change Period (Y+Rc), s | | * 4.2 | | | | * 4.2 | | 4.0 | | | | | |
| Max Green Setting (Gma | | * 26 | | | | * 26 | | 25.8 | | | | | |
| Max Q Clear Time (g_c+ | ·I1), s | 16.9 | | | | 11.2 | | 11.1 | | | | | |
| Green Ext Time (p_c), s | | 4.4 | | | | 6.9 | | 2.6 | | | | | |
| Intersection Summary | | | | | | | | | | | | | |
| HCM 6th Ctrl Delay | | | 11.4 | | | | | | | | | | |
| HCM 6th LOS | | | В | | | | | | | | | | |
| Notes | | | | | | | | | | | | | |

^{*} HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

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|-----------------------------------|-------|----------|-------|---------|------------|------------|---------|----------|-------------|----------|------------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | | | | €Î}• | | 7 | ^ | | | ↑ ↑ | |
| Traffic Volume (vph) | 0 | 0 | 0 | 42 | 329 | 38 | 22 | 68 | 0 | 0 | 235 | 174 |
| Future Volume (vph) | 0 | 0 | 0 | 42 | 329 | 38 | 22 | 68 | 0 | 0 | 235 | 174 |
| Ideal Flow (vphpl) | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 |
| Total Lost time (s) | | | | | 3.0 | | 4.0 | 4.0 | | | 4.0 | |
| Lane Util. Factor | | | | | 0.95 | | 1.00 | 0.95 | | | 0.95 | |
| Frpb, ped/bikes | | | | | 1.00 | | 1.00 | 1.00 | | | 0.99 | |
| Flpb, ped/bikes | | | | | 1.00 | | 1.00 | 1.00 | | | 1.00 | |
| Frt | | | | | 0.99 | | 1.00 | 1.00 | | | 0.94 | |
| Flt Protected | | | | | 0.99 | | 0.95 | 1.00 | | | 1.00 | |
| Satd. Flow (prot) | | | | | 2873 | | 1568 | 2885 | | | 2693 | |
| Flt Permitted | | | | | 0.99 | | 0.25 | 1.00 | | | 1.00 | |
| Satd. Flow (perm) | | | | | 2873 | | 413 | 2885 | | | 2693 | |
| Peak-hour factor, PHF | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 |
| Adj. Flow (vph) | 0 | 0 | 0 | 60 | 470 | 54 | 31 | 97 | 0 | 0 | 336 | 249 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 11 | 0 | 0 | 0 | 0 | 0 | 191 | 0 |
| Lane Group Flow (vph) | 0 | 0 | 0 | 0 | 573 | 0 | 31 | 97 | 0 | 0 | 394 | 0 |
| Confl. Bikes (#/hr) | | | 1 | | | 1 | | | 1 | | | 1 |
| Heavy Vehicles (%) | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% |
| Parking (#/hr) | | | | 6 | 6 | 4 | | 12 | | | 11 | 11 |
| Turn Type | | | | Perm | NA | | Perm | NA | | | NA | |
| Protected Phases | | | | 1 01111 | 6 | | . 0 | 8 | | | 4 | |
| Permitted Phases | | | | 6 | | | 8 | | | | • | |
| Actuated Green, G (s) | | | | | 23.0 | | 16.0 | 16.0 | | | 16.0 | |
| Effective Green, g (s) | | | | | 23.0 | | 16.0 | 16.0 | | | 16.0 | |
| Actuated g/C Ratio | | | | | 0.33 | | 0.23 | 0.23 | | | 0.23 | |
| Clearance Time (s) | | | | | 3.0 | | 4.0 | 4.0 | | | 4.0 | |
| Vehicle Extension (s) | | | | | 2.0 | | 2.0 | 2.0 | | | 2.0 | |
| Lane Grp Cap (vph) | | | | | 943 | | 94 | 659 | | | 615 | |
| v/s Ratio Prot | | | | | 3-10 | | J-1 | 0.03 | | | c0.15 | |
| v/s Ratio Perm | | | | | 0.20 | | 0.08 | 0.00 | | | 00.10 | |
| v/c Ratio | | | | | 0.61 | | 0.33 | 0.15 | | | 0.64 | |
| Uniform Delay, d1 | | | | | 19.7 | | 22.5 | 21.6 | | | 24.4 | |
| Progression Factor | | | | | 1.00 | | 1.00 | 1.00 | | | 1.00 | |
| Incremental Delay, d2 | | | | | 2.9 | | 9.1 | 0.5 | | | 5.0 | |
| Delay (s) | | | | | 22.6 | | 31.7 | 22.0 | | | 29.4 | |
| Level of Service | | | | | C | | C | C | | | 23.4 C | |
| Approach Delay (s) | | 0.0 | | | 22.6 | | U | 24.4 | | | 29.4 | |
| Approach LOS | | Α | | | C | | | C | | | C | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 25.9 | Н | CM 2000 | Level of S | Service | | С | | | |
| HCM 2000 Volume to Capacity | ratio | | 0.41 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 70.0 | S | um of lost | t time (s) | | | 11.0 | | | |
| Intersection Capacity Utilization | ۱ | | 40.0% | | | of Service | | | Α | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

| Intersection | | | | | | | | | | | | |
|------------------------|------|------|------|----------|--------|------|------|-------|------|---------|------------|-------|
| Int Delay, s/veh | 2.7 | | | | | | | | | | | |
| | | | | | | | | | | | | |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | | | | 41 | | | | | | ∱ ⊅ | |
| Traffic Vol, veh/h | 0 | 0 | 0 | 0 | 299 | 0 | 0 | 0 | 0 | 0 | 0 | 110 |
| Future Vol, veh/h | 0 | 0 | 0 | 0 | 299 | 0 | 0 | 0 | 0 | 0 | 0 | 110 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 79 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | - | - | - | - | - | - | - | - | - | - |
| Veh in Median Storage, | ,# - | 2 | - | - | 0 | - | - | 16974 | - | - | 0 | - |
| Grade, % | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 82 | 82 | 82 | 82 | 82 | 82 | 82 | 82 | 82 | 82 | 82 | 82 |
| Heavy Vehicles, % | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 |
| Mvmt Flow | 0 | 0 | 0 | 0 | 365 | 0 | 0 | 0 | 0 | 0 | 0 | 134 |
| | | | | | | | | | | | | |
| Major/Minor | | | ı | Major2 | | | | | Λ | /linor2 | | |
| Conflicting Flow All | | | - | 79 | 0 | 0 | | | | - | 444 | 183 |
| Stage 1 | | | | - | - | - | | | | _ | 365 | 103 |
| Stage 2 | | | | _ | _ | _ | | | | _ | 79 | _ |
| Critical Hdwy | | | | 4.16 | _ | _ | | | | _ | 6.56 | 6.96 |
| Critical Hdwy Stg 1 | | | | 4.10 | _ | _ | | | | _ | 5.56 | 0.30 |
| Critical Hdwy Stg 2 | | | | _ | _ | _ | | | | _ | 5.50 | _ |
| Follow-up Hdwy | | | | 2.23 | _ | _ | | | | _ | 4.03 | 3.33 |
| Pot Cap-1 Maneuver | | | | 1510 | _ | 0 | | | | 0 | 505 | 825 |
| Stage 1 | | | | 1010 | _ | 0 | | | | 0 | 619 | - 025 |
| Stage 2 | | | | _ | _ | 0 | | | | 0 | - | _ |
| Platoon blocked, % | | | | | _ | U | | | | U | | |
| Mov Cap-1 Maneuver | | | | 1510 | _ | _ | | | | _ | 0 | 825 |
| Mov Cap-1 Maneuver | | | | 1010 | _ | _ | | | | _ | 0 | - 025 |
| Stage 1 | | | | _ | _ | _ | | | | _ | 0 | _ |
| Stage 2 | | | | _ | _ | _ | | | | _ | 0 | _ |
| Olaye Z | | | | | | _ | | | | | U | |
| | | | | | | | | | | | | |
| Approach | | | | WB | | | | | | SB | | |
| HCM Control Delay, s | | | | 0 | | | | | | 10.2 | | |
| HCM LOS | | | | | | | | | | В | | |
| | | | | | | | | | | | | |
| Minor Lane/Major Mvm | t | WBL | WRT | SBLn1 | SBI n2 | | | | | | | |
| Capacity (veh/h) | | 1510 | WDT | - JDLIII | | | | | | | | |
| HCM Lane V/C Ratio | | | - | | 0.163 | | | | | | | |
| HCM Control Delay (s) | | 0 | - | | | | | | | | | |
| HCM Lane LOS | | | - | 0 | | | | | | | | |
| | | A | - | Α | В | | | | | | | |
| HCM 95th %tile Q(veh) | | 0 | - | - | 0.6 | | | | | | | |

| Intersection | | | | | | |
|------------------------|----------|-------|---------|----------|----------|------|
| Int Delay, s/veh | 0.2 | | | | | |
| | | | | | | |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | ħβ | | ሻ | ^ | | 7 |
| Traffic Vol, veh/h | 610 | 62 | 48 | 1499 | 0 | 0 |
| Future Vol, veh/h | 610 | 62 | 48 | 1499 | 0 | 0 |
| Conflicting Peds, #/hr | 0 | 31 | 31 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | 25 | - | - | 0 |
| Veh in Median Storage, | # 0 | - | - | 0 | 0 | - |
| Grade, % | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 94 | 94 | 94 | 94 | 94 | 94 |
| Heavy Vehicles, % | 3 | 3 | 3 | 3 | 3 | 3 |
| Mymt Flow | 649 | 66 | 51 | 1595 | 0 | 0 |
| WWW.CT IOW | 0.10 | 00 | 01 | 1000 | • | • |
| | | | | | | |
| Major/Minor M | 1ajor1 | N | //ajor2 | - 1 | Minor1 | |
| Conflicting Flow All | 0 | 0 | 746 | 0 | - | 389 |
| Stage 1 | - | - | - | - | - | - |
| Stage 2 | _ | - | _ | _ | - | - |
| Critical Hdwy | _ | _ | 4.16 | - | - | 6.96 |
| Critical Hdwy Stg 1 | _ | _ | - | _ | _ | - |
| Critical Hdwy Stg 2 | _ | _ | _ | _ | _ | _ |
| Follow-up Hdwy | _ | _ | 2.23 | _ | _ | 3.33 |
| Pot Cap-1 Maneuver | _ | _ | 851 | _ | 0 | 607 |
| Stage 1 | <u>-</u> | _ | - | _ | 0 | - |
| Stage 2 | _ | _ | _ | _ | 0 | _ |
| | | | - | | U | - |
| Platoon blocked, % | - | - | 000 | - | | E00 |
| Mov Cap-1 Maneuver | - | - | 826 | - | - | 589 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - |
| Stage 1 | - | - | - | - | - | - |
| Stage 2 | - | - | - | - | - | - |
| | | | | | | |
| Approach | EB | | WB | | NB | |
| HCM Control Delay, s | 0 | | 0.3 | | 0 | |
| HCM LOS | U | | 0.5 | | | |
| HOW LOS | | | | | Α | |
| | | | | | | |
| Minor Lane/Major Mvmt | | NBLn1 | EBT | EBR | WBL | WBT |
| Capacity (veh/h) | | _ | _ | | 826 | _ |
| HCM Lane V/C Ratio | | _ | _ | _ | 0.062 | _ |
| HCM Control Delay (s) | | 0 | _ | _ | 9.6 | _ |
| HCM Lane LOS | | A | | _ | 9.0 A | _ |
| HCM 95th %tile Q(veh) | | | - | - | 0.2 | |
| HOW SOUT WITH Q(Ven) | | - | - | - | 0.2 | - |

| | ۶ | → | • | • | ← | • | • | † | <i>></i> | \ | ↓ | -√ |
|--|-------------|-------------|-------------|------------|-------------|-------------|------|-------------|--------------|-------------|-------------|-------------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ሻ | ∱ ⊅ | | ሻ | ∱ ∱ | | | ∱ ∱ | | 7 | ^ | 7 |
| Traffic Volume (veh/h) | 35 | 1467 | 42 | 73 | 1350 | 48 | 0 | 228 | 54 | 30 | 161 | 42 |
| Future Volume (veh/h) | 35 | 1467 | 42 | 73 | 1350 | 48 | 0 | 228 | 54 | 30 | 161 | 42 |
| Initial Q (Qb), veh | 0 | 15 | 0 | 0 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | | 0.97 | 1.00 | | 0.97 | 1.00 | | 0.97 | 0.98 | | 0.89 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach | | No | | | No | | _ | No | | | No | |
| Adj Sat Flow, veh/h/ln | 1367 | 1367 | 1367 | 1367 | 1367 | 1367 | 0 | 1660 | 1660 | 1660 | 1660 | 1660 |
| Adj Flow Rate, veh/h | 39 | 1630 | 45 | 81 | 1500 | 50 | 0 | 253 | 39 | 33 | 179 | 17 |
| Peak Hour Factor | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Percent Heavy Veh, % | 3 | 3 | 3 | 3 | 3 | 3 | 0 | 3 | 3 | 3 | 3 | 3 |
| Cap, veh/h | 102 | 1754 | 35 | 72 | 1732 | 52 | 0 | 623 | 95 | 229 | 719 | 286 |
| Arrive On Green | 0.67 | 0.67 | 0.67 | 0.67 | 0.67 | 0.67 | 0.00 | 0.23 | 0.23 | 0.23 | 0.23 | 0.23 |
| Sat Flow, veh/h | 272 | 2580 | 71 | 241 | 2563 | 85 | 0 | 2817 | 415 | 1062 | 3154 | 1254 |
| Grp Volume(v), veh/h | 39 | 818 | 857 | 81 | 759 | 791 | 0 | 144 | 148 | 33 | 179 | 17 |
| Grp Sat Flow(s),veh/h/ln | 272 | 1299 | 1352 | 241 | 1299 | 1349 | 0 | 1577 | 1572 | 1062 | 1577 | 1254 |
| Q Serve(g_s), s | 13.2 | 55.6 | 56.5 | 10.8 | 45.9 | 46.4 | 0.0 | 7.8 | 8.0 | 2.7 | 4.6 | 1.1 |
| Cycle Q Clear(g_c), s | 59.6 | 55.6 | 56.5 | 67.3 | 45.9 | 46.4 | 0.0 | 7.8 | 8.0 | 10.7 | 4.6 | 1.1 |
| Prop In Lane | 1.00 | 074 | 0.05 | 1.00 | 074 | 0.06 | 0.00 | 250 | 0.26 | 1.00 | 740 | 1.00 |
| Lane Grp Cap(c), veh/h | 102 | 874 | 913 | 72 | 874 | 909 | 0 | 359 | 358 | 229 | 719 | 286 |
| V/C Ratio(X) | 0.38 | 0.94 | 0.94 | 1.12 | 0.87 | 0.87 | 0.00 | 0.40 | 0.41 | 0.14 | 0.25 | 0.06 |
| Avail Cap(c_a), veh/h | 129 1.00 | 874 1.00 | 910 1.00 | 98 1.00 | 874 1.00 | 908 1.00 | 1.00 | 420 1.00 | 418 | 269 1.00 | 839 1.00 | 334 1.00 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 0.32 | 0.32 | 0.32 | 0.00 | 0.84 | 1.00 0.84 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 42.9 | 15.5 | 15.5 | 50.0 | 13.4 | 13.5 | 0.00 | 32.8 | 32.9 | 37.5 | 31.6 | 30.2 |
| Uniform Delay (d), s/veh Incr Delay (d2), s/veh | 10.6 | 18.4 | 18.1 | 97.7 | 4.0 | 4.0 | 0.0 | 0.6 | 0.6 | 0.3 | 0.2 | 0.1 |
| Initial Q Delay(d3),s/veh | 0.0 | 8.3 | 7.9 | 0.0 | 1.8 | 1.7 | 0.0 | 0.0 | 0.0 | 0.0 | 0.2 | 0.0 |
| %ile BackOfQ(50%),veh/ln | 1.2 | 21.1 | 22.0 | 3.7 | 13.2 | 13.7 | 0.0 | 3.0 | 3.1 | 0.0 | 1.8 | 0.0 |
| Unsig. Movement Delay, s/veh | | 21.1 | 22.0 | 3.1 | 13.2 | 13.7 | 0.0 | 3.0 | J. I | 0.7 | 1.0 | 0.5 |
| LnGrp Delay(d),s/veh | 53.5 | 42.1 | 41.5 | 147.7 | 19.3 | 19.1 | 0.0 | 33.4 | 33.5 | 37.8 | 31.8 | 30.3 |
| LnGrp LOS | D | 72.1 D | T1.5 | F | В | В | Α | C | 00.0 C | 57.0 D | C C | 00.5 C |
| Approach Vol, veh/h | | 1714 | | <u> </u> | 1631 | | | 292 | | | 229 | |
| Approach Delay, s/veh | | 42.0 | | | 25.6 | | | 33.5 | | | 32.5 | |
| Approach LOS | | 42.0 D | | | 23.0 C | | | 00.0 C | | | 02.5 C | |
| | | | | | U | | | | | | <u> </u> | |
| Timer - Assigned Phs | | 2 | | 4 | | 6 | | 8 | | | | |
| Phs Duration (G+Y+Rc), s | | 72.7 | | 27.3 | | 72.7 | | 27.3 | | | | |
| Change Period (Y+Rc), s | | 5.4 | | 4.5 | | 5.4 | | 4.5 | | | | |
| Max Green Setting (Gmax), s | | 63.5 | | 26.6 | | 63.5 | | 26.6 | | | | |
| Max Q Clear Time (g_c+l1), s | | 61.6 | | 12.7 | | 69.3 | | 10.0 | | | | |
| Green Ext Time (p_c), s | | 1.8 | | 1.1 | | 0.0 | | 1.6 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 6th Ctrl Delay | | | 33.9 | | | | | | | | | |
| HCM 6th LOS | | | С | | | | | | | | | |

| Lane Configurations 7 | | ۶ | - | • | • | ← | • | • | † | ~ | > | ļ | 4 | |
|--|---------------------------|---------|------|------|-------|----------|------|------|------------|------|-------------|------|------|--|
| Traffic Volume (veh/h) | Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR | |
| Future Volume (veh/h) 45 1315 38 78 1327 32 67 422 159 36 351 63 Initial Q (Qb), veh V | Lane Configurations | ሻ | ħβ | | ሻ | ħβ | | ሻ | ∱ ∱ | | ሻ | ħβ | | |
| Initial Q (Ob), weh | Traffic Volume (veh/h) | 45 | 1315 | 38 | 78 | 1327 | 32 | 67 | 422 | 159 | 36 | 351 | 63 | |
| Ped-Bike Adj(A_pbT) | Future Volume (veh/h) | 45 | 1315 | 38 | 78 | 1327 | 32 | 67 | 422 | 159 | 36 | 351 | 63 | |
| Parking Bus, Adj | Initial Q (Qb), veh | 0 | 15 | | | 10 | 0 | | 0 | | | 0 | | |
| Work Zone On Ápproach | Ped-Bike Adj(A_pbT) | | | | | | | | | | | | | |
| Adj Sat Flow, veh/h/n 1367 1367 1367 1367 1367 1367 1367 1367 | Parking Bus, Adj | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | |
| Adj Flow Rate, veh/h 50 1461 40 87 1474 34 74 469 145 40 390 54 Peak Hour Factor 0.90 0.90 0.90 0.90 0.90 0.90 0.90 0.9 | | | | | | | | | | | | | | |
| Peak Hour Factor 0,90 0,90 0,90 0,90 0,90 0,90 0,90 0,9 | Adj Sat Flow, veh/h/ln | 1367 | | | | | | | | | | | | |
| Percent Heavy Veh, % 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 | Adj Flow Rate, veh/h | | 1461 | | | | | | | | | | | |
| Cap, veh/h Arrive On Green 0.65 0.65 0.65 0.65 0.65 0.65 0.65 0.65 | Peak Hour Factor | | | | | | | | | | | | | |
| Arrive On Green | Percent Heavy Veh, % | | | | | | | | | | | | | |
| Sat Flow, veh/h 284 2580 71 286 2594 60 927 2358 723 795 2774 381 Grp Volume(v), veh/h 50 734 767 87 737 771 74 312 302 40 220 224 Grp Sat Flow(s), veh/h/ln 284 1299 1355 927 1577 1503 795 1577 1578 Q Serve(g.s.), s 17.6 46.1 46.5 18.1 46.5 46.8 7.2 16.6 17.0 4.9 12.2 12.4 Cycle Q Clear(g.c.), s 64.4 46.1 46.5 64.5 46.8 19.6 16.6 17.0 4.9 12.2 12.4 Prop In Lane 1.00 0.05 1.00 0.04 1.00 0.48 3.83 371 133 389 389 V/C Ratio(X) 0.49 0.88 0.88 1.21 0.83 0.88 0.40 0.80 0.81 1.00 0.00 <t< td=""><td>Cap, veh/h</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></t<> | Cap, veh/h | | | | | | | | | | | | | |
| Grp Volume(v), veh/h 50 734 767 87 737 771 74 312 302 40 220 224 Grp Sat Flow(s), veh/h/ln 284 1299 1352 286 1299 1355 927 1577 1503 795 1577 1578 Q Serve(g_s), s 17.6 46.1 46.5 18.1 46.5 46.5 46.5 17.0 4.9 12.2 12.4 Cycle Q Clear(g_c), s 64.4 46.1 46.5 64.5 46.5 46.5 46.8 19.6 16.6 17.0 21.9 12.2 12.4 Prop In Lane 1.00 0.05 1.00 0.04 1.00 0.48 1.00 0.24 Lane Grp Cap(c), veh/h 103 838 874 72 838 875 185 389 371 133 389 389 V/C Ratio(X) 0.49 0.88 0.88 1.21 0.88 0.88 0.40 0.80 0.81 0.30 0.57 0.57 Avail Cap(c_a), veh/h 122 838 872 124 838 874 203 420 400 149 420 420 HCM Platoon Ratio 1.00 1.00 1.00 1.00 1.00 1.00 1.00 2.00 2 | Arrive On Green | | | | | | | | | | | | | |
| Grp Sat Flow(s), veh/h/ln 284 1299 1352 286 1299 1355 927 1577 1503 795 1577 1578 Q Serve(g_s), s 17.6 46.1 46.5 18.1 46.5 46.8 7.2 16.6 17.0 4.9 12.2 12.4 Cycle Q Clear(g_c), s 64.4 46.1 46.5 18.1 46.5 46.8 7.2 16.6 17.0 21.9 12.2 12.4 Prop In Lane 1.00 0.05 1.00 0.04 1.00 0.48 1.00 0.24 Lane Grp Cap(c), veh/h 103 838 874 72 838 875 185 389 371 133 389 389 V/C Ratio(X) 0.49 0.88 0.88 1.21 0.88 0.88 0.40 0.80 0.81 0.30 0.57 0.57 Avail Cap(c_a), veh/h 122 838 872 124 838 874 203 420 400 149 420 420 HCM Platoon Ratio 1.00 1.00 1.00 1.00 1.00 1.00 2.00 2.00 | Sat Flow, veh/h | 284 | 2580 | 71 | 286 | 2594 | 60 | 927 | 2358 | 723 | 795 | 2774 | 381 | |
| Q Serve(g_s), s | Grp Volume(v), veh/h | | | | | | | | | | | | | |
| Cycle Q Clear(g_c), s 64.4 46.1 46.5 64.5 46.5 46.8 19.6 16.6 17.0 21.9 12.2 12.4 Prop In Lane 1.00 0.55 1.00 0.04 1.00 0.48 1.00 0.24 Lane Grp Cap(c), veh/h 103 838 874 72 838 875 185 389 371 133 389 389 V/C Ratio(X) 0.49 0.88 0.88 1.21 0.88 0.88 0.80 0.81 0.30 0.57 0.57 Avail Cap(c_a), veh/h 122 838 872 124 838 874 203 420 400 149 420 420 HCM Platoon Ratio 1.00 1.00 1.00 1.00 1.00 1.00 1.00 2.00 2 | Grp Sat Flow(s), veh/h/li | n 284 | 1299 | 1352 | 286 | 1299 | 1355 | 927 | 1577 | 1503 | 795 | 1577 | 1578 | |
| Prop In Lane | Q Serve(g_s), s | 17.6 | 46.1 | 46.5 | 18.1 | 46.5 | 46.8 | 7.2 | 16.6 | 17.0 | 4.9 | 12.2 | 12.4 | |
| Lane Grp Cap(c), veh/h 103 838 874 72 838 875 185 389 371 133 389 389 V/C Ratio(X) 0.49 0.88 0.88 1.21 0.88 0.88 0.40 0.80 0.81 0.30 0.57 0.57 Avail Cap(c_a), veh/h 122 838 872 124 838 874 203 420 400 149 420 420 HCM Platoon Ratio 1.00 1.00 1.00 1.00 1.00 2.00 2.00 2.00 | Cycle Q Clear(g_c), s | 64.4 | 46.1 | 46.5 | 64.5 | 46.5 | 46.8 | 19.6 | 16.6 | 17.0 | 21.9 | 12.2 | 12.4 | |
| V/C Ratio(X) | Prop In Lane | 1.00 | | 0.05 | 1.00 | | 0.04 | 1.00 | | 0.48 | 1.00 | | 0.24 | |
| Avail Cap(c_a), veh/h 122 838 872 124 838 874 203 420 400 149 420 420 HCM Platoon Ratio 1.00 1.00 1.00 1.00 1.00 1.00 1.00 2.00 2 | Lane Grp Cap(c), veh/h | 103 | 838 | 874 | 72 | 838 | 875 | 185 | 389 | 371 | 133 | 389 | 389 | |
| HCM Platoon Ratio | V/C Ratio(X) | 0.49 | 0.88 | 0.88 | 1.21 | 0.88 | 0.88 | 0.40 | 0.80 | 0.81 | 0.30 | 0.57 | 0.57 | |
| Upstream Filter(I) 0.09 0.09 0.09 1.00 1.00 1.00 0.66 0.66 0.66 1.00 1.00 | Avail Cap(c_a), veh/h | 122 | 838 | 872 | 124 | 838 | 874 | | 420 | 400 | 149 | 420 | 420 | |
| Uniform Delay (d), s/veh 44.6 15.4 15.4 50.0 15.2 15.2 29.6 23.3 23.4 44.9 33.0 33.1 Incr Delay (d2), s/veh 1.5 1.3 1.3 172.5 12.7 12.4 0.9 6.9 7.8 1.2 1.5 1.7 Initial Q Delay(d3),s/veh 0.0 4.7 4.3 0.0 2.1 2.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 %ile BackOfQ(50%),veh/lrl.3 14.1 14.6 5.2 15.8 16.4 1.4 5.3 5.2 1.0 4.8 4.9 Unsig. Movement Delay, s/veh LnGrp Delay(d),s/veh 46.0 21.4 21.0 222.5 30.0 29.5 30.6 30.2 31.2 46.1 34.5 34.7 LnGrp LOS D C F C C C C D C C D C C Approach Vol, veh/lrh 1551 1595 688 484 Approach Delay, s/veh 22.0 40.3 30.7 35.6 Approach LOS C D C D C D C D T C D T C D T C D T C D T C D C D | HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 2.00 | 2.00 | 2.00 | 1.00 | 1.00 | 1.00 | |
| Incr Delay (d2), s/veh | Upstream Filter(I) | 0.09 | 0.09 | 0.09 | 1.00 | 1.00 | 1.00 | 0.66 | 0.66 | 0.66 | 1.00 | 1.00 | 1.00 | |
| Initial Q Delay(d3),s/veh | Uniform Delay (d), s/vel | h 44.6 | | | | | | 29.6 | | | | | | |
| %ile BackOfQ(50%), yeh/lr1.3 14.1 14.6 5.2 15.8 16.4 1.4 5.3 5.2 1.0 4.8 4.9 Unsig. Movement Delay, s/veh LnGrp Delay(d), s/veh 46.0 21.4 21.0 222.5 30.0 29.5 30.6 30.2 31.2 46.1 34.5 34.7 LnGrp LOS D C C F C C C C D C Approach Vol, veh/h 1551 1595 688 484 Approach LOS C D C D C D Timer - Assigned Phs 2 4 6 8 Phs Duration (G+Y+Rc), s 69.9 30.1 69.9 30.1 Change Period (Y+Rc), s 5.4 5.4 5.4 5.4 Max Green Setting (Gmax), s 62.6 26.6 62.6 26.6 Max Q Clear Time (g_c+l1), s 66.4 23.9 66.5 21.6 Green Ext Time (p_c), s 0.0 0.8 0.0 1.9 Intersection Summary HCM 6th Ctrl Delay 31.6 <td>Incr Delay (d2), s/veh</td> <td>1.5</td> <td>1.3</td> <td>1.3</td> <td>172.5</td> <td>12.7</td> <td>12.4</td> <td>0.9</td> <td>6.9</td> <td>7.8</td> <td>1.2</td> <td>1.5</td> <td>1.7</td> <td></td> | Incr Delay (d2), s/veh | 1.5 | 1.3 | 1.3 | 172.5 | 12.7 | 12.4 | 0.9 | 6.9 | 7.8 | 1.2 | 1.5 | 1.7 | |
| Unsig. Movement Delay, s/veh LnGrp Delay(d),s/veh | Initial Q Delay(d3),s/veh | า 0.0 | | | | | | | | | | | | |
| LnGrp Delay(d),s/veh 46.0 21.4 21.0 222.5 30.0 29.5 30.6 30.2 31.2 46.1 34.5 34.7 LnGrp LOS D C C F C C C C D C C Approach Vol, veh/h 1551 1595 688 484 Approach Delay, s/veh 22.0 40.3 30.7 35.6 Approach LOS C D C D Timer - Assigned Phs 2 4 6 8 Phs Duration (G+Y+Rc), s 69.9 30.1 69.9 30.1 Change Period (Y+Rc), s 5.4 5.4 5.4 5.4 Max Green Setting (Gmax), s 62.6 26.6 26.6 26.6 Max Q Clear Time (g_c+I1), s 66.4 23.9 66.5 21.6 Green Ext Time (p_c), s 0.0 0.8 0.0 1.9 Intersection Summary HCM 6th Ctrl Delay 31.6 | %ile BackOfQ(50%),vel | h/ln1.3 | 14.1 | 14.6 | 5.2 | 15.8 | 16.4 | 1.4 | 5.3 | 5.2 | 1.0 | 4.8 | 4.9 | |
| LnGrp LOS D C C F C C C C D C Approach Vol, veh/h 1551 1595 688 484 Approach Delay, s/veh 22.0 40.3 30.7 35.6 Approach LOS C D C D Timer - Assigned Phs 2 4 6 8 Phs Duration (G+Y+Rc), s 69.9 30.1 69.9 30.1 Change Period (Y+Rc), s 5.4 5.4 5.4 Max Green Setting (Gmax), s 62.6 26.6 62.6 Max Q Clear Time (g_c+l1), s 66.4 23.9 66.5 21.6 Green Ext Time (p_c), s 0.0 0.8 0.0 1.9 Intersection Summary HCM 6th Ctrl Delay 31.6 | Unsig. Movement Delay | , s/veh | | | | | | | | | | | | |
| Approach Vol, veh/h Approach Delay, s/veh Approach Delay, s/veh Approach LOS C D C D C D Timer - Assigned Phs 2 4 6 8 Phs Duration (G+Y+Rc), s 69.9 30.1 Change Period (Y+Rc), s 5.4 Max Green Setting (Gmax), s 62.6 Max Q Clear Time (g_c+l1), s 66.4 Case | LnGrp Delay(d),s/veh | 46.0 | 21.4 | 21.0 | 222.5 | 30.0 | 29.5 | 30.6 | 30.2 | 31.2 | 46.1 | 34.5 | 34.7 | |
| Approach Delay, s/veh 22.0 40.3 30.7 35.6 Approach LOS C D C D Timer - Assigned Phs 2 4 6 8 Phs Duration (G+Y+Rc), s 69.9 30.1 69.9 30.1 Change Period (Y+Rc), s 5.4 5.4 5.4 Max Green Setting (Gmax), s 62.6 26.6 26.6 Max Q Clear Time (g_c+l1), s 66.4 23.9 66.5 21.6 Green Ext Time (p_c), s 0.0 0.8 0.0 1.9 Intersection Summary HCM 6th Ctrl Delay 31.6 | LnGrp LOS | D | С | С | F | С | С | С | С | С | D | С | С | |
| Approach LOS C D C D Timer - Assigned Phs 2 4 6 8 Phs Duration (G+Y+Rc), s 69.9 30.1 69.9 30.1 Change Period (Y+Rc), s 5.4 5.4 5.4 Max Green Setting (Gmax), s 62.6 26.6 62.6 26.6 Max Q Clear Time (g_c+l1), s 66.4 23.9 66.5 21.6 Green Ext Time (p_c), s 0.0 0.8 0.0 1.9 Intersection Summary HCM 6th Ctrl Delay 31.6 | Approach Vol, veh/h | | 1551 | | | 1595 | | | 688 | | | 484 | | |
| Timer - Assigned Phs 2 4 6 8 Phs Duration (G+Y+Rc), s 69.9 30.1 69.9 30.1 Change Period (Y+Rc), s 5.4 5.4 5.4 Max Green Setting (Gmax), s 62.6 26.6 26.6 Max Q Clear Time (g_c+l1), s 66.4 23.9 66.5 21.6 Green Ext Time (p_c), s 0.0 0.8 0.0 1.9 Intersection Summary HCM 6th Ctrl Delay 31.6 | Approach Delay, s/veh | | 22.0 | | | 40.3 | | | 30.7 | | | 35.6 | | |
| Timer - Assigned Phs 2 4 6 8 Phs Duration (G+Y+Rc), s 69.9 30.1 69.9 30.1 Change Period (Y+Rc), s 5.4 5.4 5.4 Max Green Setting (Gmax), s 62.6 26.6 26.6 Max Q Clear Time (g_c+l1), s 66.4 23.9 66.5 21.6 Green Ext Time (p_c), s 0.0 0.8 0.0 1.9 Intersection Summary HCM 6th Ctrl Delay 31.6 | Approach LOS | | С | | | D | | | С | | | D | | |
| Phs Duration (G+Y+Rc), s 69.9 30.1 69.9 30.1 Change Period (Y+Rc), s 5.4 5.4 5.4 Max Green Setting (Gmax), s 62.6 26.6 62.6 26.6 Max Q Clear Time (g_c+l1), s 66.4 23.9 66.5 21.6 Green Ext Time (p_c), s 0.0 0.8 0.0 1.9 Intersection Summary HCM 6th Ctrl Delay 31.6 | Timer - Assigned Phs | | 2 | | 4 | | 6 | | 8 | | | | | |
| Change Period (Y+Rc), s 5.4 5.4 5.4 5.4 5.4 Max Green Setting (Gmax), s 62.6 26.6 62.6 26.6 Max Q Clear Time (g_c+l1), s 66.4 23.9 66.5 21.6 Green Ext Time (p_c), s 0.0 0.8 0.0 1.9 Intersection Summary HCM 6th Ctrl Delay 31.6 | |). s | | | | | | | | | | | | |
| Max Green Setting (Gmax), s 62.6 26.6 26.6 Max Q Clear Time (g_c+l1), s 66.4 23.9 66.5 21.6 Green Ext Time (p_c), s 0.0 0.8 0.0 1.9 Intersection Summary HCM 6th Ctrl Delay 31.6 | , | | | | | | | | | | | | | |
| Max Q Clear Time (g_c+l1), s 66.4 23.9 66.5 21.6 Green Ext Time (p_c), s 0.0 0.8 0.0 1.9 Intersection Summary HCM 6th Ctrl Delay 31.6 | . , | | | | | | | | | | | | | |
| Green Ext Time (p_c), s 0.0 0.8 0.0 1.9 Intersection Summary HCM 6th Ctrl Delay 31.6 | | | | | | | | | | | | | | |
| HCM 6th Ctrl Delay 31.6 | | | | | | | | | | | | | | |
| HCM 6th Ctrl Delay 31.6 | Intersection Summary | | | | | | | | | | | | | |
| · | • | | | 31.6 | | | | | | | | | | |
| 110111 0411 200 | HCM 6th LOS | | | С | | | | | | | | | | |

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|---------------------------------|-----------|-------------|--------|-------|------------|----------|---------|------------|----------|----------|------------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | † 1> | | | €Î}• | | ň | ∱ } | | Ŋ | ∱ } | |
| Traffic Volume (vph) | 0 | 1317 | 90 | 91 | 724 | 48 | 40 | 234 | 80 | 36 | 191 | 50 |
| Future Volume (vph) | 0 | 1317 | 90 | 91 | 724 | 48 | 40 | 234 | 80 | 36 | 191 | 50 |
| Ideal Flow (vphpl) | 1400 | 1400 | 1400 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 |
| Total Lost time (s) | | 5.1 | | | 5.1 | | 4.5 | 4.5 | | 4.5 | 4.5 | |
| Lane Util. Factor | | 0.95 | | | 0.95 | | 1.00 | 0.95 | | 1.00 | 0.95 | |
| Frpb, ped/bikes | | 0.98 | | | 0.98 | | 1.00 | 0.93 | | 1.00 | 0.93 | |
| Flpb, ped/bikes | | 1.00 | | | 1.00 | | 0.79 | 1.00 | | 0.84 | 1.00 | |
| Frt | | 0.99 | | | 0.99 | | 1.00 | 0.96 | | 1.00 | 0.97 | |
| Flt Protected | | 1.00 | | | 0.99 | | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | | 2516 | | | 3030 | | 1235 | 2600 | | 1312 | 2835 | |
| Flt Permitted | | 1.00 | | | 0.58 | | 0.55 | 1.00 | | 0.46 | 1.00 | |
| Satd. Flow (perm) | | 2516 | | | 1754 | | 717 | 2600 | | 640 | 2835 | |
| Peak-hour factor, PHF | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Adj. Flow (vph) | 0 | 1386 | 95 | 96 | 762 | 51 | 42 | 246 | 84 | 38 | 201 | 53 |
| RTOR Reduction (vph) | 0 | 4 | 0 | 0 | 4 | 0 | 0 | 34 | 0 | 0 | 24 | 0 |
| Lane Group Flow (vph) | 0 | 1477 | 0 | 0 | 905 | 0 | 42 | 296 | 0 | 38 | 230 | 0 |
| Confl. Peds. (#/hr) | 423 | | 174 | 174 | | 423 | 282 | | 215 | 215 | | 282 |
| Confl. Bikes (#/hr) | | | 6 | | | 1 | | | 1 | | | 1 |
| Heavy Vehicles (%) | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% |
| Parking (#/hr) | | | | | | | | 8 | 8 | | | |
| Turn Type | | NA | | pm+pt | NA | | Perm | NA | | Perm | NA | |
| Protected Phases | | 2 | | 1 | 6 | | | 8 | | | 4 | |
| Permitted Phases | | | | 6 | | | 8 | | | 4 | | |
| Actuated Green, G (s) | | 59.7 | | | 67.4 | | 23.0 | 23.0 | | 23.0 | 23.0 | |
| Effective Green, g (s) | | 59.7 | | | 67.4 | | 23.0 | 23.0 | | 23.0 | 23.0 | |
| Actuated g/C Ratio | | 0.60 | | | 0.67 | | 0.23 | 0.23 | | 0.23 | 0.23 | |
| Clearance Time (s) | | 5.1 | | | 5.1 | | 4.5 | 4.5 | | 4.5 | 4.5 | |
| Vehicle Extension (s) | | 5.0 | | | 5.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | | 1502 | | | 1239 | | 164 | 598 | | 147 | 652 | |
| v/s Ratio Prot | | c0.59 | | | c0.03 | | | c0.11 | | | 0.08 | |
| v/s Ratio Perm | | | | | 0.46 | | 0.06 | | | 0.06 | | |
| v/c Ratio | | 0.98 | | | 0.73 | | 0.26 | 0.50 | | 0.26 | 0.35 | |
| Uniform Delay, d1 | | 19.7 | | | 10.5 | | 31.5 | 33.5 | | 31.5 | 32.3 | |
| Progression Factor | | 1.00 | | | 0.83 | | 1.00 | 1.00 | | 0.56 | 0.51 | |
| Incremental Delay, d2 | | 19.5 | | | 1.8 | | 0.8 | 0.6 | | 0.8 | 0.3 | |
| Delay (s) | | 39.2 | | | 10.5 | | 32.3 | 34.1 | | 18.5 | 16.8 | |
| Level of Service | | D | | | В | | С | C | | В | В | |
| Approach Delay (s) | | 39.2 | | | 10.5 | | | 33.9 | | | 17.0 | |
| Approach LOS | | D | | | В | | | С | | | В | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 27.9 | Н | CM 2000 | Level of | Service | | С | | | |
| HCM 2000 Volume to Capac | ity ratio | | 0.84 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 100.0 | S | um of lost | time (s) | | | 12.8 | | | |
| Intersection Capacity Utilizati | on | | 120.7% | | CU Level | | | | Н | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

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|---------------------------|------------|------------|---------------|------------|------------|------|------|----------|------|------|------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | * | ↑ ↑ | | ሻ | ∱ ∱ | | ሻ | ^ | 7 | | ħβ | |
| Traffic Volume (veh/h) | 121 | 1184 | 128 | 92 | 729 | 48 | 71 | 509 | 157 | 0 | 428 | 63 |
| Future Volume (veh/h) | 121 | 1184 | 128 | 92 | 729 | 48 | 71 | 509 | 157 | 0 | 428 | 63 |
| Initial Q (Qb), veh | 0 | 10 | 0 | 0 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 0.97 | | 0.89 | 1.00 | | 0.89 | 0.95 | | 0.82 | 1.00 | • | 0.83 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approac | | No | | | No | | | No | | | No | |
| | 1367 | 1367 | 1367 | 1660 | 1660 | 1660 | 1660 | 1660 | 1660 | 0 | 1660 | 1660 |
| Adj Flow Rate, veh/h | 127 | 1246 | 128 | 97 | 767 | 46 | 75 | 536 | 138 | 0 | 451 | 54 |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Percent Heavy Veh, % | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 0 | 3 | 3 |
| Cap, veh/h | 73 | 1625 | 156 | 72 | 2062 | 121 | 164 | 809 | 296 | 0 | 710 | 84 |
| Arrive On Green | 0.69 | 0.69 | 0.69 | 1.00 | 1.00 | 1.00 | 0.26 | 0.26 | 0.26 | 0.00 | 0.26 | 0.26 |
| Sat Flow, veh/h | 532 | 2349 | 240 | 392 | 3000 | 180 | 842 | 3154 | 1154 | 0 | 2853 | 328 |
| Grp Volume(v), veh/h | 127 | 686 | 688 | 97 | 403 | 410 | 75 | 536 | 138 | 0 | 255 | 250 |
| Grp Sat Flow(s), veh/h/lr | | 1299 | 1290 | 392 | 1577 | 1602 | 842 | 1577 | 1154 | 0 | 1577 | 1521 |
| Q Serve(g_s), s | 9.9 | 35.1 | 35.9 | 20.5 | 0.0 | 0.0 | 8.7 | 15.2 | 10.1 | 0.0 | 14.3 | 14.7 |
| Cycle Q Clear(g_c), s | 10.0 | 35.1 | 35.9 | 56.8 | 0.0 | 0.0 | 23.4 | 15.2 | 10.1 | 0.0 | 14.3 | 14.7 |
| Prop In Lane | 1.00 | 00.1 | 0.19 | 1.00 | 0.0 | 0.11 | 1.00 | 10.2 | 1.00 | 0.00 | 17.0 | 0.22 |
| Lane Grp Cap(c), veh/h | | 891 | 888 | 72 | 1082 | 1100 | 164 | 809 | 296 | 0.00 | 404 | 390 |
| V/C Ratio(X) | 1.73 | 0.77 | 0.77 | 1.35 | 0.37 | 0.37 | 0.46 | 0.66 | 0.47 | 0.00 | 0.63 | 0.64 |
| Avail Cap(c_a), veh/h | 436 | 891 | 885 | 198 | 1082 | 1100 | 167 | 817 | 299 | 0.00 | 404 | 390 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 2.00 | 2.00 | 2.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 0.90 | 0.90 | 0.90 | 0.95 | 0.95 | 0.95 | 0.00 | 0.72 | 0.72 |
| Uniform Delay (d), s/vel | | 11.0 | 11.0 | 34.3 | 0.0 | 0.0 | 43.5 | 33.3 | 31.4 | 0.0 | 33.0 | 33.1 |
| Incr Delay (d2), s/veh | | 6.4 | | 218.2 | 0.9 | 0.9 | 1.9 | 1.9 | 1.1 | 0.0 | 2.3 | 2.6 |
| Initial Q Delay(d3),s/veh | | 1.0 | 1.0 | 0.0 | 0.2 | 0.2 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),vel | | 11.4 | 11.6 | 6.1 | 0.2 | 0.2 | 1.9 | 6.0 | 2.9 | 0.0 | 5.7 | 5.7 |
| Unsig. Movement Delay | | | 11.0 | J. 1 | 3.0 | 3.0 | 1.0 | 3.0 | 2.0 | 0.0 | 0.1 | 0.1 |
| LnGrp Delay(d),s/veh | | 18.3 | 18.6 | 252.5 | 1.1 | 1.1 | 45.4 | 35.2 | 32.5 | 0.0 | 35.2 | 35.7 |
| LnGrp LOS | -51.0 F | В | В | 202.0 F | Α | A | D | D | C | Α | D | D |
| Approach Vol, veh/h | <u>'</u> | 1501 | | ' | 910 | , , | | 749 | | 71 | 505 | |
| Approach Delay, s/veh | | 53.3 | | | 27.9 | | | 35.7 | | | 35.4 | |
| Approach LOS | | D | | | C C | | | D | | | D | |
| • • | | | | | J | | | | | | - 0 | |
| Timer - Assigned Phs | | 2 | | 4 | | 6 | | 8 | | | | |
| Phs Duration (G+Y+Rc) | | 73.9 | | 30.7 | | 73.9 | | 30.7 | | | | |
| Change Period (Y+Rc), | | 5.1 | | * 5.1 | | 5.1 | | 5.1 | | | | |
| Max Green Setting (Gm | | 64.3 | | * 26 | | 64.3 | | 25.5 | | | | |
| Max Q Clear Time (g_c- | , . | 37.9 | | 25.4 | | 58.8 | | 16.7 | | | | |
| Green Ext Time (p_c), s | 3 | 20.8 | | 0.3 | | 3.9 | | 2.1 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 6th Ctrl Delay | | | 41.0 | | | | | | | | | |
| HCM 6th LOS | | | D | | | | | | | | | |
| Notes | | | | | | | | | | | | |

^{*} HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

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|---------------------------|------|------------|---------------|-------|----------|-----------|------|-----------|-----------|------|-----------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | ↑ ↑ | | ሻ | ^ | 7 | ሻ | † | | ሻ | ^ | 7 |
| Traffic Volume (veh/h) | 0 | 1112 | 105 | 71 | 832 | 270 | 48 | 232 | 86 | 190 | 193 | 33 |
| Future Volume (veh/h) | 0 | 1112 | 105 | 71 | 832 | 270 | 48 | 232 | 86 | 190 | 193 | 33 |
| Initial Q (Qb), veh | 0 | 10 | 0 | 0 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | | 0.95 | 0.99 | .0 | 0.95 | 0.92 | | 0.89 | 0.95 | | 0.92 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approac | | No | 1.00 | 1.00 | No | 1.00 | 1.00 | No | 1.00 | 1.00 | No | 1.00 |
| Adj Sat Flow, veh/h/ln | 0 | 1367 | 1367 | 1660 | 1660 | 1660 | 1660 | 1660 | 1660 | 1660 | 1660 | 1660 |
| Adj Flow Rate, veh/h | 0 | 1146 | 102 | 73 | 858 | 172 | 49 | 239 | 89 | 196 | 199 | 10 |
| Peak Hour Factor | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 |
| Percent Heavy Veh, % | 0 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 |
| Cap, veh/h | 0 | 1345 | 104 | 72 | 1741 | 739 | 340 | 553 | 196 | 335 | 1105 | 453 |
| Arrive On Green | 0.00 | 1.00 | 1.00 | 0.55 | 0.55 | 0.55 | 0.25 | 0.25 | 0.25 | 0.07 | 0.35 | 0.35 |
| Sat Flow, veh/h | 0 | 2469 | 213 | 439 | 3154 | 1339 | 1067 | 2202 | 780 | 1581 | 3154 | 1295 |
| Grp Volume(v), veh/h | 0 | 619 | 629 | 73 | 858 | 172 | 49 | 168 | 160 | 196 | 199 | 10 |
| Grp Sat Flow(s), veh/h/lr | | 1299 | 1315 | 439 | 1577 | 1339 | 1067 | 1577 | 1405 | 1581 | 1577 | 1295 |
| Q Serve(g_s), s | 0.0 | 0.0 | 0.0 | 8.9 | 16.7 | 6.6 | 3.6 | 8.9 | 9.6 | 6.9 | 4.4 | 0.5 |
| Cycle Q Clear(g_c), s | 0.0 | 0.0 | 0.0 | 8.9 | 16.7 | 6.6 | 3.6 | 8.9 | 9.6 | 6.9 | 4.4 | 0.5 |
| Prop In Lane | 0.00 | 0.0 | 0.16 | 1.00 | 10.7 | 1.00 | 1.00 | 0.5 | 0.56 | 1.00 | т.т | 1.00 |
| Lane Grp Cap(c), veh/h | | 717 | 729 | 72 | 1741 | 739 | 340 | 396 | 353 | 335 | 1105 | 453 |
| V/C Ratio(X) | 0.00 | 0.86 | 0.86 | 1.01 | 0.49 | 0.23 | 0.14 | 0.42 | 0.45 | 0.59 | 0.18 | 0.02 |
| Avail Cap(c_a), veh/h | 0.00 | 717 | 726 | 314 | 1741 | 739 | 371 | 442 | 393 | 335 | 1196 | 491 |
| HCM Platoon Ratio | 1.00 | 2.00 | 2.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 0.00 | 0.50 | 0.50 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/vel | | 0.0 | 0.0 | 50.0 | 14.2 | 11.5 | 29.4 | 31.4 | 31.6 | 28.3 | 22.5 | 21.3 |
| Incr Delay (d2), s/veh | 0.0 | 7.1 | 7.0 | 110.0 | 1.0 | 0.7 | 0.2 | 0.7 | 0.9 | 1.8 | 0.1 | 0.0 |
| Initial Q Delay(d3),s/veh | | 2.6 | 2.5 | 0.0 | 0.5 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),vel | | 1.9 | 1.9 | 4.0 | 6.7 | 2.1 | 0.0 | 3.5 | 3.4 | 1.5 | 1.6 | 0.0 |
| Unsig. Movement Delay | | | 1.5 | т.0 | 0.1 | 2.1 | 0.0 | 0.0 | 0.7 | 1.0 | 1.0 | U.Z |
| LnGrp Delay(d),s/veh | 0.0 | 9.7 | 9.4 | 160.0 | 15.7 | 12.3 | 29.6 | 32.1 | 32.6 | 30.1 | 22.6 | 21.3 |
| LnGrp LOS | Α | Α | Α. | F | В | 12.3 B | C | C | 02.0 C | C | C | C C |
| Approach Vol, veh/h | | 1248 | | ' | 1103 | <u> </u> | | 377 | | | 405 | |
| Approach Delay, s/veh | | 9.6 | | | 24.7 | | | 32.0 | | | 26.2 | |
| Approach LOS | | 9.0 A | | | C C | | | 02.0 C | | | 20.2 C | |
| •• | | | | | U | | | | | | U | |
| Timer - Assigned Phs | | 2 | | 4 | | 6 | 7 | 8 | | | | |
| Phs Duration (G+Y+Rc) | | 60.3 | | 39.7 | | 60.3 | 9.9 | 29.8 | | | | |
| Change Period (Y+Rc), | | 5.1 | | * 4.7 | | 5.1 | 3.0 | * 4.7 | | | | |
| Max Green Setting (Gm | | 52.3 | | * 38 | | 52.3 | 6.9 | * 28 | | | | |
| Max Q Clear Time (g_c- | , . | 2.0 | | 6.4 | | 18.7 | 8.9 | 11.6 | | | | |
| Green Ext Time (p_c), s | 3 | 26.0 | | 1.4 | | 17.6 | 0.0 | 2.1 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 6th Ctrl Delay | | | 19.7 | | | | | | | | | |
| HCM 6th LOS | | | В | | | | | | | | | |
| Notes | | | | | | | | | | | | |

^{*} HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

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|---------------------------|----------|----------|------------|------|----------|-------|------|----------|------|------|------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | | | | 414 | | ች | ^ | | | ħβ | |
| Traffic Volume (veh/h) | 0 | 0 | 0 | 97 | 160 | 64 | 131 | 432 | 0 | 0 | 507 | 88 |
| Future Volume (veh/h) | 0 | 0 | 0 | 97 | 160 | 64 | 131 | 432 | 0 | 0 | 507 | 88 |
| nitial Q (Qb), veh | | | | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | | | | 1.00 | | 0.79 | 0.94 | | 1.00 | 1.00 | | 0.77 |
| Parking Bus, Adj | | | | 0.85 | 1.00 | 0.85 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.81 |
| Nork Zone On Approach | า | | | | No | | | No | | | No | |
| Adj Sat Flow, veh/h/ln | | | | 1660 | 1660 | 1660 | 1660 | 1660 | 0 | 0 | 1660 | 1660 |
| Adj Flow Rate, veh/h | | | | 102 | 168 | 46 | 138 | 455 | 0 | 0 | 534 | 70 |
| Peak Hour Factor | | | | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Percent Heavy Veh, % | | | | 3 | 3 | 3 | 3 | 3 | 0 | 0 | 3 | 3 |
| Cap, veh/h | | | | 303 | 513 | 143 | 383 | 1549 | 0 | 0 | 1198 | 155 |
| Arrive On Green | | | | 0.37 | 0.37 | 0.37 | 0.49 | 0.49 | 0.00 | 0.00 | 0.49 | 0.49 |
| Sat Flow, veh/h | | | | 814 | 1377 | 384 | 758 | 3237 | 0 | 0 | 2522 | 316 |
| Grp Volume(v), veh/h | | | | 171 | 0 | 145 | 138 | 455 | 0 | 0 | 343 | 261 |
| Grp Sat Flow(s),veh/h/ln | | | | 1362 | 0 | 1213 | 758 | 1577 | 0 | 0 | 1577 | 1177 |
| Q Serve(g_s), s | | | | 5.4 | 0.0 | 5.1 | 8.7 | 5.1 | 0.0 | 0.0 | 8.5 | 8.7 |
| Cycle Q Clear(g_c), s | | | | 5.4 | 0.0 | 5.1 | 17.4 | 5.1 | 0.0 | 0.0 | 8.5 | 8.7 |
| Prop In Lane | | | | 0.60 | 0.0 | 0.32 | 1.00 | 0.1 | 0.00 | 0.00 | 0.0 | 0.27 |
| Lane Grp Cap(c), veh/h | | | | 507 | 0 | 452 | 383 | 1549 | 0 | 0 | 775 | 578 |
| V/C Ratio(X) | | | | 0.34 | 0.00 | 0.32 | 0.36 | 0.29 | 0.00 | 0.00 | 0.44 | 0.45 |
| Avail Cap(c_a), veh/h | | | | 586 | 0 | 522 | 383 | 1549 | 0.00 | 0.00 | 775 | 578 |
| HCM Platoon Ratio | | | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Jpstream Filter(I) | | | | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 0.00 | 0.00 | 0.61 | 0.61 |
| Uniform Delay (d), s/veh | | | | 13.5 | 0.0 | 13.4 | 15.7 | 9.1 | 0.0 | 0.0 | 9.9 | 10.0 |
| ncr Delay (d2), s/veh | | | | 0.4 | 0.0 | 0.4 | 2.6 | 0.5 | 0.0 | 0.0 | 1.1 | 1.6 |
| Initial Q Delay(d3),s/veh | | | | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh | | | | 1.6 | 0.0 | 1.3 | 1.7 | 1.7 | 0.0 | 0.0 | 2.8 | 2.2 |
| Unsig. Movement Delay, | | | | | | | | | | | | |
| LnGrp Delay(d),s/veh | , | | | 13.9 | 0.0 | 13.8 | 18.3 | 9.6 | 0.0 | 0.0 | 11.1 | 11.5 |
| _nGrp LOS | | | | В | Α | В | В | Α | Α | Α | В | В |
| Approach Vol, veh/h | | | | | 316 | | | 593 | | | 604 | |
| Approach Delay, s/veh | | | | | 13.9 | | | 11.6 | | | 11.3 | |
| Approach LOS | | | | | В | | | В | | | В | |
| Timer - Assigned Phs | | 2 | | | | 6 | | 8 | | | | |
| Phs Duration (G+Y+Rc), | 9 | 33.7 | | | | 33.7 | | 26.3 | | | | |
| Change Period (Y+Rc), | | * 4.2 | | | | * 4.2 | | 4.0 | | | | |
| Max Green Setting (Gma | | * 26 | | | | * 26 | | 25.8 | | | | |
| Max Q Clear Time (g_c+ | | 19.4 | | | | 10.7 | | 7.4 | | | | |
| Green Ext Time (p_c), s | | 3.2 | | | | 6.0 | | 1.9 | | | | |
| (1 –). | | J.Z | | | | 0.0 | | 1.3 | | | | |
| ntersection Summary | | | 44.0 | | | | | | | | | |
| HCM 6th Ctrl Delay | | | 11.9 | | | | | | | | | |
| HCM 6th LOS | | | В | | | | | | | | | |
| Notes | | | | | | | | | | | | |

^{*} HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

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|-----------------------------------|-------|-------------|---|---------|------------|------------|---|------------|---|----------|------------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | | | | 414 | | * | † † | | | ∱ } | |
| Traffic Volume (vph) | 0 | 0 | 0 | 75 | 192 | 135 | 54 | 282 | 0 | 0 | 368 | 118 |
| Future Volume (vph) | 0 | 0 | 0 | 75 | 192 | 135 | 54 | 282 | 0 | 0 | 368 | 118 |
| Ideal Flow (vphpl) | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 |
| Total Lost time (s) | | | | | 3.0 | | 4.0 | 4.0 | | | 4.0 | |
| Lane Util. Factor | | | | | 0.95 | | 1.00 | 0.95 | | | 0.95 | |
| Frpb, ped/bikes | | | | | 1.00 | | 1.00 | 1.00 | | | 1.00 | |
| Flpb, ped/bikes | | | | | 1.00 | | 1.00 | 1.00 | | | 1.00 | |
| Frt | | | | | 0.95 | | 1.00 | 1.00 | | | 0.96 | |
| Flt Protected | | | | | 0.99 | | 0.95 | 1.00 | | | 1.00 | |
| Satd. Flow (prot) | | | | | 2747 | | 1568 | 2885 | | | 2779 | |
| Flt Permitted | | | | | 0.99 | | 0.30 | 1.00 | | | 1.00 | |
| Satd. Flow (perm) | | | | | 2747 | | 503 | 2885 | | | 2779 | |
| Peak-hour factor, PHF | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Adj. Flow (vph) | 0 | 0 | 0 | 79 | 202 | 142 | 57 | 297 | 0 | 0 | 387 | 124 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 87 | 0 | 0 | 0 | 0 | 0 | 44 | 0 |
| Lane Group Flow (vph) | 0 | 0 | 0 | 0 | 336 | 0 | 57 | 297 | 0 | 0 | 467 | 0 |
| Confl. Bikes (#/hr) | | | 1 | | | 1 | <u> </u> | | 1 | • | | 1 |
| Heavy Vehicles (%) | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% |
| Parking (#/hr) | • 70 | 3 ,3 | • | 6 | 6 | 4 | • | 12 | • | • 70 | 11 | 11 |
| Turn Type | | | | Perm | NA | • | Perm | NA | | | NA | |
| Protected Phases | | | | 1 01111 | 6 | | 1 01111 | 8 | | | 4 | |
| Permitted Phases | | | | 6 | | | 8 | | | | • | |
| Actuated Green, G (s) | | | | | 23.0 | | 16.0 | 16.0 | | | 16.0 | |
| Effective Green, g (s) | | | | | 23.0 | | 16.0 | 16.0 | | | 16.0 | |
| Actuated g/C Ratio | | | | | 0.33 | | 0.23 | 0.23 | | | 0.23 | |
| Clearance Time (s) | | | | | 3.0 | | 4.0 | 4.0 | | | 4.0 | |
| Vehicle Extension (s) | | | | | 2.0 | | 2.0 | 2.0 | | | 2.0 | |
| Lane Grp Cap (vph) | | | | | 902 | | 114 | 659 | | | 635 | |
| v/s Ratio Prot | | | | | 302 | | 117 | 0.10 | | | c0.17 | |
| v/s Ratio Perm | | | | | 0.12 | | 0.11 | 0.10 | | | CO. 17 | |
| v/c Ratio | | | | | 0.12 | | 0.50 | 0.45 | | | 0.74 | |
| Uniform Delay, d1 | | | | | 18.0 | | 23.5 | 23.2 | | | 25.0 | |
| Progression Factor | | | | | 1.00 | | 1.00 | 1.00 | | | 1.00 | |
| Incremental Delay, d2 | | | | | 1.00 | | 14.8 | 2.2 | | | 7.4 | |
| Delay (s) | | | | | 19.2 | | 38.3 | 25.4 | | | 32.5 | |
| Level of Service | | | | | 19.2 B | | 30.3 D | 23.4 C | | | 32.3 C | |
| Approach Delay (s) | | 0.0 | | | 19.2 | | U | 27.5 | | | 32.5 | |
| Approach LOS | | Α | | | В | | | C C | | | 02.5 C | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 26.7 | H | CM 2000 | Level of | Service | | С | | | |
| HCM 2000 Volume to Capacity | ratio | | 0.34 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 70.0 | Sı | um of lost | time (s) | | | 11.0 | | | |
| Intersection Capacity Utilization | 1 | | 47.1% | | | of Service | | | Α | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

| Intersection | | | | | | | | | | | | |
|------------------------|------|------|------|--------|-------|------|------|-------|------|---------|------|--------|
| Int Delay, s/veh | 1.2 | | | | | | | | | | | |
| | | | | | | | | | | | | |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | | | | 4₽ | | | | | | Φ₽ | |
| Traffic Vol, veh/h | 0 | 0 | 0 | 0 | 354 | 0 | 0 | 0 | 0 | 0 | 0 | 48 |
| Future Vol, veh/h | 0 | 0 | 0 | 0 | 354 | 0 | 0 | 0 | 0 | 0 | 0 | 48 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 251 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | - | - | - | - | - | - | - | - | - | - |
| Veh in Median Storage, | # - | 2 | - | - | 0 | - | - | 16974 | - | - | 0 | - |
| Grade, % | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 |
| Heavy Vehicles, % | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 |
| Mvmt Flow | 0 | 0 | 0 | 0 | 373 | 0 | 0 | 0 | 0 | 0 | 0 | 51 |
| | | | | | | | | | | | | |
| Major/Minor | | | | Majora | | | | | | /linor2 | | |
| | | | | Major2 | ^ | 0 | | | | | 604 | 107 |
| Conflicting Flow All | | | | 251 | 0 | 0 | | | | - | 624 | 187 |
| Stage 1 | | | | - | - | - | | | | - | 373 | - |
| Stage 2 | | | | 4.40 | - | - | | | | - | 251 | - 0.00 |
| Critical Hdwy | | | | 4.16 | - | - | | | | - | 6.56 | 6.96 |
| Critical Hdwy Stg 1 | | | | - | - | - | | | | - | 5.56 | - |
| Critical Hdwy Stg 2 | | | | - | - | - | | | | - | - | - |
| Follow-up Hdwy | | | | 2.23 | - | - | | | | - | 4.03 | 3.33 |
| Pot Cap-1 Maneuver | | | | 1304 | - | 0 | | | | 0 | 398 | 820 |
| Stage 1 | | | | - | - | 0 | | | | 0 | 614 | - |
| Stage 2 | | | | - | - | 0 | | | | 0 | - | - |
| Platoon blocked, % | | | | | - | | | | | | | |
| Mov Cap-1 Maneuver | | | | 1304 | - | - | | | | - | 0 | 820 |
| Mov Cap-2 Maneuver | | | | - | - | - | | | | - | 0 | - |
| Stage 1 | | | | - | - | - | | | | - | 0 | - |
| Stage 2 | | | | - | - | - | | | | - | 0 | - |
| | | | | | | | | | | | | |
| Approach | | | | WB | | | | | | SB | | |
| HCM Control Delay, s | | | | 0 | | | | | | 9.7 | | |
| HCM LOS | | | | | | | | | | Α | | |
| TOW LOO | | | | | | | | | | | | |
| | | | | | | | | | | | | |
| Minor Lane/Major Mvmt | | WBL | WBT: | SBLn1 | | | | | | | | |
| Capacity (veh/h) | | 1304 | - | - | 820 | | | | | | | |
| HCM Lane V/C Ratio | | - | - | - | 0.062 | | | | | | | |
| HCM Control Delay (s) | | 0 | - | 0 | 9.7 | | | | | | | |
| HCM Lane LOS | | Α | - | Α | Α | | | | | | | |
| HCM 95th %tile Q(veh) | | 0 | - | - | 0.2 | | | | | | | |

| Intersection | | | | | | |
|------------------------|----------|-------|--------|----------|--------|------|
| Int Delay, s/veh | 0.1 | | | | | |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | † | LDIX | ሻ | ^ | NDL | 7 |
| Traffic Vol, veh/h | 1321 | 35 | 13 | 856 | 0 | 0 |
| Future Vol, veh/h | 1321 | 35 | 13 | 856 | 0 | 0 |
| Conflicting Peds, #/hr | 0 | 100 | 100 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | _ | - | 25 | - | _ | 0 |
| Veh in Median Storage | , # 0 | - | | 0 | 0 | - |
| Grade, % | 0 | _ | _ | 0 | 0 | _ |
| Peak Hour Factor | 96 | 96 | 96 | 96 | 96 | 96 |
| Heavy Vehicles, % | 3 | 3 | 3 | 3 | 3 | 3 |
| Mymt Flow | 1376 | 36 | 14 | 892 | 0 | 0 |
| | 1010 | | | 002 | • | • |
| | | | | - | | |
| | /lajor1 | | Major2 | | Minor1 | |
| Conflicting Flow All | 0 | 0 | 1512 | 0 | - | 806 |
| Stage 1 | - | - | - | - | - | - |
| Stage 2 | - | - | - | - | - | - |
| Critical Hdwy | - | - | 4.16 | - | - | 6.96 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - |
| Critical Hdwy Stg 2 | - | - | - | - | - | - |
| Follow-up Hdwy | - | - | 2.23 | - | - | 3.33 |
| Pot Cap-1 Maneuver | - | - | 433 | - | 0 | 323 |
| Stage 1 | - | - | - | - | 0 | - |
| Stage 2 | - | - | - | - | 0 | _ |
| Platoon blocked, % | - | - | | - | | |
| Mov Cap-1 Maneuver | - | - | 392 | - | - | 292 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - |
| Stage 1 | - | - | - | - | - | - |
| Stage 2 | - | - | - | - | - | - |
| Ü | | | | | | |
| Annroach | EB | | MD | | ND | |
| Approach | | | WB | | NB | |
| HCM Control Delay, s | 0 | | 0.2 | | 0 | |
| HCM LOS | | | | | Α | |
| | | | | | | |
| Minor Lane/Major Mvm | t 1 | NBLn1 | EBT | EBR | WBL | WBT |
| Capacity (veh/h) | | _ | _ | - | 392 | _ |
| HCM Lane V/C Ratio | | _ | _ | | 0.035 | _ |
| HCM Control Delay (s) | | 0 | _ | _ | 14.5 | - |
| HCM Lane LOS | | A | _ | _ | В | _ |
| HCM 95th %tile Q(veh) | | - | _ | _ | 0.1 | _ |
| TOW JOHN JUNE Q(VEII) | | | | | 0.1 | |

| | ۶ | → | • | • | ← | • | 1 | † | / | / | ↓ | -√ |
|-------------------------------|----------|--------------|---------|---------|------------|---------|------|------------|----------|----------|----------|----------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | Ŋ | ∱ ⊅ | | Ť | ∱ ⊅ | | | ∱ ⊅ | | 7 | ^ | 7 |
| Traffic Volume (veh/h) | 23 | 1318 | 30 | 80 | 1493 | 30 | 0 | 75 | 29 | 28 | 301 | 45 |
| Future Volume (veh/h) | 23 | 1318 | 30 | 80 | 1493 | 30 | 0 | 75 | 29 | 28 | 301 | 45 |
| Initial Q (Qb), veh | 0 | 10 | 0 | 0 | 15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | | 0.97 | 1.00 | | 0.99 | 1.00 | | 0.97 | 0.99 | | 0.98 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach | 1007 | No | 4007 | 4007 | No | 4007 | • | No | 1000 | 4000 | No | 4000 |
| Adj Sat Flow, veh/h/ln | 1367 | 1367 | 1367 | 1367 | 1367 | 1367 | 0 | 1660 | 1660 | 1660 | 1660 | 1660 |
| Adj Flow Rate, veh/h | 26 | 1464 | 32 | 89 | 1659 | 32 | 0 | 83 | 8 | 31 | 334 | 27 |
| Peak Hour Factor | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Percent Heavy Veh, % | 3 115 | 3 | 3 40 | 3 72 | 3 1919 | 3 32 | 0 | 3 484 | 3 46 | 3 254 | 3 526 | 230 |
| Cap, veh/h Arrive On Green | 0.73 | 1910 0.73 | 0.73 | 0.73 | 0.73 | 0.73 | 0.00 | 0.17 | 0.17 | 0.17 | 0.17 | 0.17 |
| Sat Flow, veh/h | 238 | 2597 | 57 | 287 | 2606 | 50 | 0.00 | 2987 | 276 | 1282 | 3154 | 1379 |
| Grp Volume(v), veh/h | 26 | 731 | 765 | 89 | 825 | 866 | 0 | 44 | 47 | 31 | 334 | 27 |
| Grp Sat Flow(s), veh/h/ln | 238 | 1299 | 1355 | 287 | 1299 | 1357 | 0 | 1577 | 1602 | 1282 | 1577 | 1379 |
| Q Serve(g_s), s | 9.0 | 34.2 | 34.4 | 27.4 | 46.3 | 46.8 | 0.0 | 2.4 | 2.5 | 2.1 | 9.9 | 1.7 |
| Cycle Q Clear(g_c), s | 55.8 | 34.2 | 34.4 | 61.9 | 46.3 | 46.8 | 0.0 | 2.4 | 2.5 | 4.6 | 9.9 | 1.7 |
| Prop In Lane | 1.00 | UT.Z | 0.04 | 1.00 | 70.0 | 0.04 | 0.00 | ۷.٦ | 0.17 | 1.00 | 3.3 | 1.00 |
| Lane Grp Cap(c), veh/h | 115 | 954 | 995 | 72 | 954 | 998 | 0.00 | 263 | 267 | 254 | 526 | 230 |
| V/C Ratio(X) | 0.23 | 0.77 | 0.77 | 1.24 | 0.87 | 0.87 | 0.00 | 0.17 | 0.17 | 0.12 | 0.64 | 0.12 |
| Avail Cap(c_a), veh/h | 135 | 954 | 995 | 184 | 954 | 997 | 0 | 420 | 426 | 381 | 839 | 367 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 0.41 | 0.41 | 0.41 | 0.00 | 0.99 | 0.99 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 36.7 | 8.5 | 8.5 | 50.0 | 10.5 | 10.5 | 0.0 | 35.7 | 35.8 | 37.7 | 38.8 | 35.4 |
| Incr Delay (d2), s/veh | 4.5 | 5.9 | 5.7 | 145.4 | 4.6 | 4.5 | 0.0 | 0.3 | 0.3 | 0.2 | 1.3 | 0.2 |
| Initial Q Delay(d3),s/veh | 0.0 | 8.0 | 0.8 | 0.0 | 3.3 | 3.1 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/ln | 0.7 | 9.7 | 10.0 | 4.7 | 13.1 | 13.6 | 0.0 | 1.0 | 1.0 | 0.7 | 3.9 | 0.6 |
| Unsig. Movement Delay, s/veh | | | | | | | | | | | | |
| LnGrp Delay(d),s/veh | 41.2 | 15.3 | 15.0 | 195.4 | 18.4 | 18.1 | 0.0 | 36.0 | 36.1 | 37.9 | 40.1 | 35.6 |
| LnGrp LOS | D | В | В | F | В | В | A | D | D | D | D | <u>D</u> |
| Approach Vol, veh/h | | 1522 | | | 1780 | | | 91 | | | 392 | |
| Approach Delay, s/veh | | 15.6 | | | 27.1 | | | 36.0 | | | 39.6 | |
| Approach LOS | | В | | | С | | | D | | | D | |
| Timer - Assigned Phs | | 2 | | 4 | | 6 | | 8 | | | | |
| Phs Duration (G+Y+Rc), s | | 78.8 | | 21.2 | | 78.8 | | 21.2 | | | | |
| Change Period (Y+Rc), s | | 5.4 | | 4.5 | | 5.4 | | 4.5 | | | | |
| Max Green Setting (Gmax), s | | 63.5 | | 26.6 | | 63.5 | | 26.6 | | | | |
| Max Q Clear Time (g_c+I1), s | | 57.8 | | 11.9 | | 63.9 | | 4.5 | | | | |
| Green Ext Time (p_c), s | | 5.2 | | 2.1 | | 0.0 | | 0.4 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 6th Ctrl Delay | | | 24.0 | | | | | | | | | |
| HCM 6th LOS | | | С | | | | | | | | | |

| Aane Configurations 7 ↑ ↑ ↑ ↑ ↑ ↑ ↑ ↑ ↑ ↑ ↑ ↑ ↑ ↑ ↑ ↑ ↑ ↑ | | ۶ | → | • | • | ← | • | 1 | † | / | / | ļ | 4 | |
|--|---------------------------|------|-------------|------|-------|----------|------|------|------|----------|------|------------|------|--|
| Traffic Volume (vehrh) 37 1491 26 96 1270 36 28 342 147 21 476 57 Truture Volume (vehrh) 37 1491 26 96 1270 36 28 342 147 21 476 57 Truture Volume (vehrh) 37 1491 26 96 1270 36 28 342 147 21 476 57 Truture Volume (vehrh) 37 1491 26 96 1270 36 28 342 147 21 476 57 Truture Volume (vehrh) 37 1491 26 96 1270 36 28 342 147 21 476 57 Truture Volume (vehrh) 37 1491 26 96 1270 36 28 342 147 21 476 57 Truture Volume (vehrh) 37 1491 26 96 1270 36 28 342 147 21 476 57 Truture Volume (vehrh) 100 10 10 0 100 100 1.00 1.00 1.00 1.0 | Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR | |
| Traffic Volume (vehrh) 37 1491 26 96 1270 36 28 342 147 21 476 57 Truture Volume (vehrh) 37 1491 26 96 1270 36 28 342 147 21 476 57 Truture Volume (vehrh) 37 1491 26 96 1270 36 28 342 147 21 476 57 Truture Volume (vehrh) 37 1491 26 96 1270 36 28 342 147 21 476 57 Truture Volume (vehrh) 37 1491 26 96 1270 36 28 342 147 21 476 57 Truture Volume (vehrh) 37 1491 26 96 1270 36 28 342 147 21 476 57 Truture Volume (vehrh) 37 1491 26 96 1270 36 28 342 147 21 476 57 Truture Volume (vehrh) 100 10 10 0 10 10 1.00 1.00 1.00 1.00 | Lane Configurations | * | † 1> | | | ΦÞ | | | | | | ↑ ↑ | | |
| Future Volume (veh/h) 37 1491 26 96 1270 36 28 342 147 21 476 57 minital Q (Qb), veh | | | | 26 | | | 36 | | | 147 | | | 57 | |
| Ped-Bike Adj(A_pbT) 1.00 | Future Volume (veh/h) | 37 | 1491 | 26 | 96 | 1270 | 36 | 28 | 342 | 147 | 21 | 476 | 57 | |
| Parking Bus, Adj | Initial Q (Qb), veh | 0 | 10 | 0 | 0 | 15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Nork Zone On Approach No No No No No No No N | Ped-Bike Adj(A_pbT) | 1.00 | | 0.98 | 1.00 | | 0.97 | 0.99 | | 0.97 | 0.99 | | 0.98 | |
| Adj Sat Flow, veh/h/ln 1367 1367 1367 1367 1367 1367 1367 1367 | Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Adj Flow Rate, veh/h | Work Zone On Approach | h | No | | | No | | | No | | | No | | |
| Peak Hour Factor 0.90 0.90 0.90 0.90 0.90 0.90 0.90 0.9 | Adj Sat Flow, veh/h/ln | 1367 | 1367 | 1367 | 1367 | 1367 | 1367 | 1660 | 1660 | 1660 | 1660 | 1660 | 1660 | |
| Percent Heavy Veh, % 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 | Adj Flow Rate, veh/h | 41 | 1657 | 28 | 107 | 1411 | 38 | 31 | 380 | 143 | 23 | 529 | 54 | |
| Cap, veh/h 100 1719 17 72 1691 40 128 535 198 160 692 70 Arrive On Green 0.65 0.65 0.65 0.65 0.65 0.65 0.65 0.65 | Peak Hour Factor | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | |
| Arrive On Green 0.65 0.65 0.65 0.65 0.65 0.65 0.65 0.65 | Percent Heavy Veh, % | 3 | 3 | | | | | 3 | | 3 | | | | |
| Sat Flow, veh/h 300 2613 44 239 2582 69 820 2231 826 866 2884 293 Sirp Volume(v), veh/h 41 822 863 107 709 740 31 267 256 23 289 294 Sirp Sat Flow(s), veh/h/h 300 1299 1358 239 1299 1352 820 1577 1479 866 1577 1600 2 Serve(g.s), s 12, 2 60.0 60.6 4.7 41.8 42.0 3.5 13.3 13.8 16.2 17.0 17.1 Sirp Cap(Cap(c), s 54.2 60.0 60.6 65.2 41.8 42.0 3.5 13.3 13.8 16.2 17.0 17.1 Sirp Cap(Cap(c), veh/h 100 847 888 72 847 883 128 378 355 160 378 384 72 847 883 128 378 355 160 378 384 72 847 848 128 378 378 378 378 378 378 378 378 378 37 | Cap, veh/h | | | | | 1691 | | | | | | | | |
| Samp Volume(v), veh/h | Arrive On Green | | | | | | | | | | | | | |
| Sarp Sat Flow(s), veh/h/ln 300 1299 1358 239 1299 1352 820 1577 1479 866 1577 1600 Discrey(g_s), s 12,2 60.0 60.6 4.7 41.8 42.0 3.5 13.3 13.8 2.4 17.0 17.1 Cycle Q Clear(g_c), s 54.2 60.0 60.6 65.2 41.8 42.0 20.7 13.3 13.8 16.2 17.0 17.1 Cycle Q Clear(g_c), s 54.2 60.0 60.6 65.2 41.8 42.0 20.7 13.3 13.8 16.2 17.0 17.1 Cycle Q Clear(g_c), s 54.2 60.0 60.6 65.2 41.8 42.0 20.7 13.3 13.8 16.2 17.0 17.1 Cycle Q Clear(g_c), s 54.2 60.0 60.6 65.2 41.8 42.0 20.7 13.3 13.8 16.2 17.0 17.1 Cycle Q Clear(g_c), s 54.2 60.0 60.6 65.2 41.8 42.0 20.7 13.3 13.8 16.2 17.0 17.1 Cycle Q Clear(g_c), s 54.2 60.0 60.6 65.2 41.8 42.0 20.7 13.3 13.8 16.2 17.0 17.1 Cycle Q Clear(g_c), s 64.2 60.0 60.6 66.6 65.2 41.8 42.0 20.7 13.3 13.8 16.2 17.0 17.1 Cycle Q Clear(g_c), s 64.1 10.0 10.0 0.05 10.0 0.56 10.0 0.56 10.0 0.60 0.7 Avail Cap(c_a), veh/h 142 847 886 83 847 882 150 420 393 183 420 426 ChCM Platon Ratio 1.00 1.00 1.00 1.00 1.00 2.00 2.00 2.00 1.00 1.00 1.00 Jpstream Filter(l) 0.33 0.33 0.33 1.00 1.00 1.00 0.82 0.82 0.82 0.82 1.00 1.00 1.00 Jniform Delay (d), s/veh 4.1 12.1 11.8 278.7 9.6 9.3 0.8 3.9 4.7 0.4 7.3 7.5 Jnsig. Movement Delay, s/veh 1.1 2.0 2.1 3.3 3.3 3.2 0.0 0.0 0.0 0.0 0.0 0.0 Wile BackOfO(50%), veh/h 1726 17.2 17.2 17.2 17.2 17.2 17.3 14.5 15.0 0.7 4.2 4.1 0.5 7.3 7.5 Jnsig. Movement Delay, s/veh 37.6 47.8 28.0 42.7 42.9 42.0 4 | Sat Flow, veh/h | 300 | 2613 | 44 | 239 | 2582 | 69 | 820 | 2231 | 826 | 866 | 2884 | 293 | |
| 2 Serve(g_s), s 12.2 60.0 60.6 4.7 41.8 42.0 3.5 13.3 13.8 2.4 17.0 17.1 Dycle Q Clear(g_c), s 54.2 60.0 60.6 65.2 41.8 42.0 20.7 13.3 13.8 16.2 17.0 17.1 Dycle Q Clear(g_c), s 54.2 60.0 60.6 65.2 41.8 42.0 20.7 13.3 13.8 16.2 17.0 17.1 Dycle Q Clear(g_c), s 54.2 60.0 60.6 65.2 41.8 42.0 20.7 13.3 13.8 16.2 17.0 17.1 Dycle Q Clear(g_c), s 54.2 60.0 60.6 65.2 41.8 42.0 20.7 13.3 13.8 16.2 17.0 17.1 Dycle Q Clear(g_c), s 54.2 60.0 60.6 65.2 41.8 42.0 20.7 13.3 13.8 16.2 17.0 17.1 Dycle Q Clear(g_c), s 54.2 60.0 60.6 65.2 41.8 42.0 20.7 13.3 13.8 16.2 17.0 17.1 Dycle Q Clear(g_c), s 54.2 60.0 60.6 65.2 41.8 42.0 20.7 13.3 13.8 16.2 17.0 17.1 Dycle Q Clear(g_c), s 54.2 60.0 60.6 65.2 41.8 42.0 20.7 13.3 13.8 16.2 17.0 17.1 Dycle Q Clear(g_c), s 54.2 60.0 60.6 65.2 41.8 42.0 20.7 13.3 13.8 16.2 17.0 17.1 Dycle Q Clear(g_c), s 54.2 60.0 60.6 65.2 41.8 42.0 20.7 13.3 13.8 16.2 17.0 17.1 Dycle Q Clear(g_c), s 64.2 60.0 0.0 0.0 0.0 0.0 0.0 0.7 0.7 0.7 0.7 | Grp Volume(v), veh/h | 41 | 822 | 863 | 107 | 709 | 740 | 31 | 267 | 256 | 23 | 289 | 294 | |
| Cycle Q Clear(g_c), s 54.2 60.0 60.6 65.2 41.8 42.0 20.7 13.3 13.8 16.2 17.0 17.1 CProp In Lane 1.00 0.33 1.00 0.05 1.00 0.56 1.00 0.18 clane Grp Cap(c), veh/h 100 847 888 72 847 883 128 378 355 160 378 384 (7/C Ratio(X) 0.41 0.97 0.97 1.49 0.84 0.84 0.24 0.71 0.72 0.14 0.76 0.77 avail Cap(c_a), veh/h 142 847 886 83 847 882 150 420 393 183 420 426 classed Filter(I) 0.33 0.33 0.33 1.00 1.00 1.00 1.00 1.00 | Grp Sat Flow(s), veh/h/ln | 300 | 1299 | 1358 | 239 | 1299 | 1352 | 820 | 1577 | 1479 | 866 | 1577 | 1600 | |
| Prop In Lane 1.00 0.03 1.00 0.05 1.00 0.56 1.00 0.18 Jane Grp Cap(c), veh/h 100 847 888 72 847 883 128 378 355 160 378 384 J/C Ratio(X) 0.41 0.97 0.97 1.49 0.84 0.84 0.24 0.71 0.72 0.14 0.76 0.77 Avail Cap(c_a), veh/h 142 847 886 83 847 882 150 420 393 183 420 426 HCM Platoon Ratio 1.00 1.00 1.00 1.00 1.00 1.00 0.00 2.00 2 | Q Serve(g_s), s | 12.2 | 60.0 | 60.6 | 4.7 | 41.8 | 42.0 | 3.5 | 13.3 | 13.8 | 2.4 | 17.0 | 17.1 | |
| Lane Grp Cap(c), veh/h 100 847 888 72 847 883 128 378 355 160 378 384 //C Ratio(X) | Cycle Q Clear(g_c), s | 54.2 | 60.0 | 60.6 | 65.2 | 41.8 | 42.0 | 20.7 | 13.3 | 13.8 | 16.2 | 17.0 | 17.1 | |
| //C Ratio(X) | Prop In Lane | 1.00 | | 0.03 | 1.00 | | 0.05 | 1.00 | | 0.56 | 1.00 | | 0.18 | |
| Avail Cap(c_a), veh/h 142 847 886 83 847 882 150 420 393 183 420 426 HCM Platoon Ratio 1.00 1.00 1.00 1.00 1.00 1.00 2.00 2.00 | Lane Grp Cap(c), veh/h | 100 | 847 | 888 | 72 | 847 | 883 | 128 | 378 | 355 | 160 | 378 | 384 | |
| HCM Platoon Ratio 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.0 | V/C Ratio(X) | 0.41 | 0.97 | 0.97 | 1.49 | 0.84 | 0.84 | 0.24 | 0.71 | 0.72 | 0.14 | 0.76 | 0.77 | |
| Destream Filter(I) | Avail Cap(c_a), veh/h | | 847 | 886 | 83 | 847 | 882 | 150 | 420 | | | 420 | | |
| Juliform Delay (d), s/veh 43.6 17.2 17.2 50.0 14.2 14.2 33.2 23.2 23.4 41.4 35.4 35.4 35.4 17.5 17 | HCM Platoon Ratio | | | | 1.00 | 1.00 | 1.00 | | | | | 1.00 | | |
| ncr Delay (d2), s/veh 4.1 12.1 11.8 278.7 9.6 9.3 0.8 3.9 4.7 0.4 7.3 7.5 nitial Q Delay(d3), s/veh 0.0 8.5 8.0 0.0 3.5 3.2 0.0 0.0 0.0 0.0 0.0 0.0 %ile BackOfQ(50%), veh/In1.1 20.6 21.3 7.3 14.5 15.0 0.7 4.2 4.1 0.5 7.3 7.5 Unsig. Movement Delay, s/veh LnGrp Delay(d), s/veh 47.7 37.8 37.0 328.7 27.3 26.7 34.0 27.1 28.1 41.8 42.7 42.9 LnGrp LOS D D D F C C C C D D D Approach Vol, veh/h 1726 1556 554 606 Approach Delay, s/veh 37.6 47.8 28.0 42.7 Approach LOS D D D C D Filmer - Assigned Phs 2 4 6 8 Phs Duration (G+Y+Rc), s 70.6 29.4 70.6 29.4 Change Period (Y+Rc), s 5.4 5.4 5.4 5.4 Max Green Setting (Gmax), s 62.6 26.6 62.6 26.6 Max Q Clear Time (g_c+11), s 62.6 19.1 67.2 22.7 Green Ext Time (p_c), s 0.0 2.3 0.0 1.3 Intersection Summary HCM 6th Ctrl Delay 40.7 | Upstream Filter(I) | | 0.33 | | 1.00 | 1.00 | 1.00 | | | | | | | |
| nitial Q Delay(d3),s/veh 0.0 8.5 8.0 0.0 3.5 3.2 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0 | | | | | | | | | | | | | | |
| Wile BackOfQ(50%),veh/Iril. | Incr Delay (d2), s/veh | 4.1 | | | | | | | | | | | | |
| Unsig. Movement Delay, s/veh UnGrp Delay(d),s/veh | Initial Q Delay(d3),s/veh | | | | | | | | | | | | | |
| Approach Vol, veh/h 1726 1556 554 606 Approach Delay, s/veh 37.6 47.8 28.0 42.7 Approach LOS D D D D D C D D D D D D D D D D D D D | , , | | | 21.3 | 7.3 | 14.5 | 15.0 | 0.7 | 4.2 | 4.1 | 0.5 | 7.3 | 7.5 | |
| Approach Vol, veh/h 1726 1556 554 606 Approach Delay, s/veh 37.6 47.8 28.0 42.7 Approach LOS D D C D Fimer - Assigned Phs 2 4 6 8 Phs Duration (G+Y+Rc), s 70.6 29.4 70.6 29.4 Change Period (Y+Rc), s 5.4 5.4 5.4 5.4 Max Green Setting (Gmax), s 62.6 26.6 62.6 26.6 Max Q Clear Time (g_c+I1), s 62.6 19.1 67.2 22.7 Green Ext Time (p_c), s 0.0 2.3 0.0 1.3 Intersection Summary HCM 6th Ctrl Delay 40.7 | | | | | | | | | | | | | | |
| Approach Vol, veh/h 1726 1556 554 606 Approach Delay, s/veh 37.6 47.8 28.0 42.7 Approach LOS D D C D Fimer - Assigned Phs 2 4 6 8 Phs Duration (G+Y+Rc), s 70.6 29.4 70.6 29.4 Change Period (Y+Rc), s 5.4 5.4 5.4 5.4 Max Green Setting (Gmax), s 62.6 26.6 62.6 26.6 Max Q Clear Time (g_c+I1), s 62.6 19.1 67.2 22.7 Green Ext Time (p_c), s 0.0 2.3 0.0 1.3 Intersection Summary HCM 6th Ctrl Delay 40.7 | | | | | 328.7 | | | | | | 41.8 | | | |
| Approach Delay, s/veh 37.6 47.8 28.0 42.7 Approach LOS D D C D Fimer - Assigned Phs 2 4 6 8 Phs Duration (G+Y+Rc), s 70.6 29.4 70.6 29.4 Change Period (Y+Rc), s 5.4 5.4 5.4 Max Green Setting (Gmax), s 62.6 26.6 62.6 26.6 Max Q Clear Time (g_c+I1), s 62.6 19.1 67.2 22.7 Green Ext Time (p_c), s 0.0 2.3 0.0 1.3 Intersection Summary HCM 6th Ctrl Delay 40.7 | LnGrp LOS | D | | D | F | С | С | С | | С | D | | D | |
| Approach LOS D D C D Fimer - Assigned Phs 2 4 6 8 Phs Duration (G+Y+Rc), s 70.6 29.4 70.6 29.4 Change Period (Y+Rc), s 5.4 5.4 5.4 Max Green Setting (Gmax), s 62.6 26.6 62.6 26.6 Max Q Clear Time (g_c+l1), s 62.6 19.1 67.2 22.7 Green Ext Time (p_c), s 0.0 2.3 0.0 1.3 Intersection Summary HCM 6th Ctrl Delay 40.7 | Approach Vol, veh/h | | | | | | | | | | | | | |
| Fimer - Assigned Phs 2 4 6 8 Phs Duration (G+Y+Rc), s 70.6 29.4 70.6 29.4 Change Period (Y+Rc), s 5.4 5.4 5.4 Max Green Setting (Gmax), s 62.6 26.6 62.6 26.6 Max Q Clear Time (g_c+l1), s 62.6 19.1 67.2 22.7 Green Ext Time (p_c), s 0.0 2.3 0.0 1.3 Intersection Summary HCM 6th Ctrl Delay 40.7 | Approach Delay, s/veh | | 37.6 | | | 47.8 | | | | | | 42.7 | | |
| Phs Duration (G+Y+Rc), s 70.6 29.4 70.6 29.4 Change Period (Y+Rc), s 5.4 5.4 5.4 5.4 Max Green Setting (Gmax), s 62.6 26.6 62.6 26.6 Max Q Clear Time (g_c+I1), s 62.6 19.1 67.2 22.7 Green Ext Time (p_c), s 0.0 2.3 0.0 1.3 Intersection Summary HCM 6th Ctrl Delay 40.7 | Approach LOS | | D | | | D | | | С | | | D | | |
| Change Period (Y+Rc), s 5.4 5.4 5.4 5.4 5.4 Max Green Setting (Gmax), s 62.6 26.6 62.6 26.6 Max Q Clear Time (g_c+l1), s 62.6 19.1 67.2 22.7 Green Ext Time (p_c), s 0.0 2.3 0.0 1.3 | Timer - Assigned Phs | | 2 | | 4 | | 6 | | 8 | | | | | |
| Change Period (Y+Rc), s 5.4 5.4 5.4 5.4 5.4 Max Green Setting (Gmax), s 62.6 26.6 62.6 26.6 Max Q Clear Time (g_c+l1), s 62.6 19.1 67.2 22.7 Green Ext Time (p_c), s 0.0 2.3 0.0 1.3 | | , S | 70.6 | | 29.4 | | 70.6 | | 29.4 | | | | | |
| Max Green Setting (Gmax), s 62.6 26.6 62.6 26.6 Max Q Clear Time (g_c+I1), s 62.6 19.1 67.2 22.7 Green Ext Time (p_c), s 0.0 2.3 0.0 1.3 Intersection Summary HCM 6th Ctrl Delay 40.7 | | | | | | | | | | | | | | |
| Max Q Clear Time (g_c+I1), s 62.6 19.1 67.2 22.7 Green Ext Time (p_c), s 0.0 2.3 0.0 1.3 Intersection Summary HCM 6th Ctrl Delay 40.7 | • , , , | | | | | | | | | | | | | |
| Green Ext Time (p_c), s 0.0 2.3 0.0 1.3 ntersection Summary 40.7 40.7 | | | | | | | | | | | | | | |
| ntersection Summary HCM 6th Ctrl Delay 40.7 | Green Ext Time (p_c), s | , . | | | | | | | | | | | | |
| HCM 6th Ctrl Delay 40.7 | Intersection Summary | | | | | | | | | | | | | |
| , | HCM 6th Ctrl Delay | | | 40.7 | | | | | | | | | | |
| TOTAL COLUMN TOTAL | HCM 6th LOS | | | D | | | | | | | | | | |

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|-----------------------------------|---------|------------|--------|-------|------------|------------|---------|------------|----------|----------|------------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | ∱ } | | | €Î∌ | | * | ∱ } | | ሻ | ∱ } | |
| Traffic Volume (vph) | 0 | 647 | 41 | 127 | 1347 | 21 | 11 | 83 | 37 | 35 | 327 | 49 |
| Future Volume (vph) | 0 | 647 | 41 | 127 | 1347 | 21 | 11 | 83 | 37 | 35 | 327 | 49 |
| Ideal Flow (vphpl) | 1700 | 1700 | 1700 | 1400 | 1400 | 1400 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 |
| Total Lost time (s) | | 5.1 | | | 5.1 | | 4.5 | 4.5 | | 4.5 | 4.5 | |
| Lane Util. Factor | | 0.95 | | | 0.95 | | 1.00 | 0.95 | | 1.00 | 0.95 | |
| Frpb, ped/bikes | | 1.00 | | | 1.00 | | 1.00 | 0.98 | | 1.00 | 0.99 | |
| Flpb, ped/bikes | | 1.00 | | | 1.00 | | 0.98 | 1.00 | | 0.96 | 1.00 | |
| Frt | | 0.99 | | | 1.00 | | 1.00 | 0.95 | | 1.00 | 0.98 | |
| Flt Protected | | 1.00 | | | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | | 3098 | | | 2559 | | 1543 | 2734 | | 1511 | 3057 | |
| Flt Permitted | | 1.00 | | | 0.74 | | 0.39 | 1.00 | | 0.67 | 1.00 | |
| Satd. Flow (perm) | | 3098 | | | 1895 | | 640 | 2734 | | 1069 | 3057 | |
| Peak-hour factor, PHF | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Adj. Flow (vph) | 0 | 681 | 43 | 134 | 1418 | 22 | 12 | 87 | 39 | 37 | 344 | 52 |
| RTOR Reduction (vph) | 0 | 4 | 0 | 0 | 1 | 0 | 0 | 30 | 0 | 0 | 12 | 0 |
| Lane Group Flow (vph) | 0 | 720 | 0 | 0 | 1573 | 0 | 12 | 96 | 0 | 37 | 384 | 0 |
| Confl. Peds. (#/hr) | 100 | | 29 | 29 | | 100 | 24 | | 33 | 33 | | 24 |
| Confl. Bikes (#/hr) | | | 3 | | | 2 | | | 1 | | | 1 |
| Heavy Vehicles (%) | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% |
| Parking (#/hr) | | | | | | | | 8 | 8 | | | |
| Turn Type | | NA | | pm+pt | NA | | Perm | NA | | Perm | NA | |
| Protected Phases | | 2 | | 1 | 6 | | | 8 | | | 4 | |
| Permitted Phases | | | | 6 | | | 8 | | | 4 | | |
| Actuated Green, G (s) | | 59.5 | | | 67.2 | | 23.2 | 23.2 | | 23.2 | 23.2 | |
| Effective Green, g (s) | | 59.5 | | | 67.2 | | 23.2 | 23.2 | | 23.2 | 23.2 | |
| Actuated g/C Ratio | | 0.60 | | | 0.67 | | 0.23 | 0.23 | | 0.23 | 0.23 | |
| Clearance Time (s) | | 5.1 | | | 5.1 | | 4.5 | 4.5 | | 4.5 | 4.5 | |
| Vehicle Extension (s) | | 5.0 | | | 5.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | | 1843 | | | 1303 | | 148 | 634 | | 248 | 709 | |
| v/s Ratio Prot | | 0.23 | | | c0.05 | | 1.0 | 0.04 | | 2.0 | c0.13 | |
| v/s Ratio Perm | | 0.20 | | | c0.76 | | 0.02 | 0.01 | | 0.03 | 00.10 | |
| v/c Ratio | | 0.39 | | | 1.21 | | 0.08 | 0.15 | | 0.15 | 0.54 | |
| Uniform Delay, d1 | | 10.7 | | | 16.4 | | 30.1 | 30.6 | | 30.5 | 33.7 | |
| Progression Factor | | 1.00 | | | 0.53 | | 1.00 | 1.00 | | 0.43 | 0.40 | |
| Incremental Delay, d2 | | 0.6 | | | 97.8 | | 0.2 | 0.1 | | 0.2 | 0.7 | |
| Delay (s) | | 11.3 | | | 106.5 | | 30.3 | 30.7 | | 13.3 | 14.1 | |
| Level of Service | | В | | | F | | C | С | | В | В | |
| Approach Delay (s) | | 11.3 | | | 106.5 | | | 30.6 | | | 14.0 | |
| Approach LOS | | В | | | F | | | C | | | В | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 64.9 | Н | CM 2000 | Level of | Service | | Е | | | |
| HCM 2000 Volume to Capacit | y ratio | | 1.07 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 100.0 | S | um of lost | t time (s) | | | 12.8 | | | |
| Intersection Capacity Utilization | n | | 109.5% | | U Level | | | | Н | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

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|---------------------------|------|------------|---------------|-------|----------|-------|------|----------|------|------|------------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | ↑ ↑ | | ሻ | † | | ሻ | ^ | 7 | 022 | ↑ ↑ | 02.1 |
| Traffic Volume (veh/h) | 90 | 557 | 184 | 165 | 1345 | 21 | 42 | 379 | 70 | 0 | 527 | 82 |
| Future Volume (veh/h) | 90 | 557 | 184 | 165 | 1345 | 21 | 42 | 379 | 70 | 0 | 527 | 82 |
| Initial Q (Qb), veh | 0 | 10 | 0 | 0 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | | 0.95 | 0.99 | | 0.95 | 0.98 | | 0.91 | 1.00 | • | 0.91 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approac | | No | | | No | ,,,,, | | No | | | No | |
| Adj Sat Flow, veh/h/ln | 1660 | 1660 | 1660 | 1367 | 1367 | 1367 | 1660 | 1660 | 1660 | 0 | 1660 | 1660 |
| Adj Flow Rate, veh/h | 95 | 586 | 183 | 174 | 1416 | 21 | 44 | 399 | 18 | 0 | 555 | 73 |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Percent Heavy Veh, % | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 0 | 3 | 3 |
| Cap, veh/h | 73 | 1813 | 550 | 72 | 2017 | 29 | 128 | 817 | 333 | 0 | 717 | 94 |
| Arrive On Green | 0.77 | 0.77 | 0.77 | 1.00 | 1.00 | 1.00 | 0.26 | 0.26 | 0.26 | 0.00 | 0.26 | 0.26 |
| Sat Flow, veh/h | 367 | 2338 | 728 | 568 | 2618 | 39 | 779 | 3154 | 1285 | 0 | 2852 | 363 |
| Grp Volume(v), veh/h | 95 | 395 | 374 | 174 | 702 | 735 | 44 | 399 | 18 | 0 | 315 | 313 |
| Grp Sat Flow(s), veh/h/li | | 1577 | 1488 | 568 | 1299 | 1358 | 779 | 1577 | 1285 | 0 | 1577 | 1554 |
| Q Serve(g_s), s | 8.2 | 7.7 | 7.7 | 5.6 | 0.0 | 0.0 | 5.6 | 10.7 | 1.1 | 0.0 | 18.5 | 18.7 |
| Cycle Q Clear(g_c), s | 8.6 | 7.7 | 7.7 | 14.0 | 0.0 | 0.0 | 24.2 | 10.7 | 1.1 | 0.0 | 18.5 | 18.7 |
| Prop In Lane | 1.00 | • • • | 0.49 | 1.00 | 0.0 | 0.03 | 1.00 | | 1.00 | 0.00 | | 0.23 |
| Lane Grp Cap(c), veh/h | | 1214 | 1148 | 72 | 1000 | 1046 | 128 | 817 | 333 | 0 | 408 | 403 |
| V/C Ratio(X) | 1.31 | 0.33 | 0.33 | 2.41 | 0.70 | 0.70 | 0.34 | 0.49 | 0.05 | 0.00 | 0.77 | 0.78 |
| Avail Cap(c_a), veh/h | 353 | 1214 | 1146 | 461 | 1000 | 1046 | 128 | 817 | 333 | 0 | 408 | 403 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 2.00 | 2.00 | 2.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 0.51 | 0.51 | 0.51 | 1.00 | 1.00 | 1.00 | 0.00 | 0.30 | 0.30 |
| Uniform Delay (d), s/vel | | 3.7 | 3.7 | 38.5 | 0.0 | 0.0 | 45.6 | 31.4 | 27.8 | 0.0 | 34.3 | 34.4 |
| Incr Delay (d2), s/veh | | 0.7 | 0.8 | | 2.1 | 2.0 | 1.6 | 0.5 | 0.1 | 0.0 | 2.8 | 3.0 |
| Initial Q Delay(d3),s/veh | | 0.2 | 0.2 | 0.0 | 0.6 | 0.6 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),vel | | 2.7 | 2.6 | 14.9 | 0.8 | 0.8 | 1.1 | 4.1 | 0.3 | 0.0 | 7.4 | 7.3 |
| Unsig. Movement Delay | | | | | | | | | | | | |
| LnGrp Delay(d),s/veh | | 4.6 | 4.7 | 695.3 | 2.7 | 2.6 | 47.2 | 31.9 | 27.9 | 0.0 | 37.1 | 37.3 |
| LnGrp LOS | F | A | Α | F | Α | A | D | С | C | Α | D | D |
| Approach Vol, veh/h | | 864 | | | 1611 | | | 461 | | | 628 | |
| Approach Delay, s/veh | | 32.6 | | | 77.5 | | | 33.2 | | | 37.2 | |
| Approach LOS | | С | | | E | | | С | | | D | |
| •• | | | | | | ^ | | | | | | |
| Timer - Assigned Phs | | 2 | | 4 | | 6 | | 8 | | | | |
| Phs Duration (G+Y+Rc) | | 82.5 | | 31.0 | | 82.5 | | 31.0 | | | | |
| Change Period (Y+Rc), | | 5.1 | | * 5.1 | | 5.1 | | 5.1 | | | | |
| Max Green Setting (Gm | | 64.3 | | * 26 | | 64.3 | | 25.5 | | | | |
| Max Q Clear Time (g_c | , . | 10.6 | | 26.2 | | 16.0 | | 20.7 | | | | |
| Green Ext Time (p_c), s | 5 | 17.9 | | 0.0 | | 35.0 | | 1.7 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 6th Ctrl Delay | | | 53.8 | | | | | | | | | |
| HCM 6th LOS | | | D | | | | | | | | | |
| Notes | | | | | | | | | | | | |

^{*} HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

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|---|------|----------|------|-------|----------|------|------|------------|------|-------------|----------|------|--|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR | |
| Lane Configurations | | ħβ | | * | ^ | 7 | * | ∱ ∱ | | ች | ^ | 7 | |
| Traffic Volume (veh/h) | 0 | 487 | 62 | 76 | 1358 | 113 | 25 | 69 | 33 | 212 | 273 | 85 | |
| Future Volume (veh/h) | 0 | 487 | 62 | 76 | 1358 | 113 | 25 | 69 | 33 | 212 | 273 | 85 | |
| Initial Q (Qb), veh | 0 | 10 | 0 | 0 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| | 1.00 | | 0.97 | 0.99 | | 0.97 | 0.95 | <u> </u> | 0.92 | 0.94 | | 0.94 | |
| , | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Work Zone On Approach | | No | | | No | | | No | | | No | | |
| Adj Sat Flow, veh/h/ln | 0 | 1660 | 1660 | 1367 | 1367 | 1367 | 1660 | 1660 | 1660 | 1660 | 1660 | 1660 | |
| Adj Flow Rate, veh/h | 0 | 492 | 55 | 77 | 1372 | 89 | 25 | 70 | 33 | 214 | 276 | 68 | |
| | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | |
| Percent Heavy Veh, % | 0 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | |
| Cap, veh/h | 0 | 1657 | 179 | 72 | 1505 | 649 | 291 | 468 | 200 | 415 | 1018 | 428 | |
| | 0.00 | 0.77 | 0.77 | 0.58 | 0.58 | 0.58 | 0.22 | 0.22 | 0.22 | 0.07 | 0.32 | 0.32 | |
| Sat Flow, veh/h | 0.00 | 2934 | 317 | 698 | 2598 | 1120 | 976 | 2089 | 894 | 1581 | 3154 | 1327 | |
| Grp Volume(v), veh/h | 0 | 271 | 276 | 77 | 1372 | 89 | 25 | 51 | 52 | 214 | 276 | 68 | |
| Grp Sat Flow(s), veh/h/ln | | 1577 | 1591 | 698 | 1299 | 1120 | 976 | 1577 | 1405 | 1581 | 1577 | 1327 | |
| | 0.0 | 5.1 | 5.2 | 5.9 | 47.1 | 3.6 | 2.0 | 2.6 | 3.0 | 6.9 | 6.5 | 3.7 | |
| Q Serve(g_s), s | 0.0 | 5.1 | 5.2 | 11.0 | 47.1 | 3.6 | 2.0 | 2.6 | 3.0 | 6.9 | 6.5 | 3.7 | |
| Cycle Q Clear(g_c), s | | ე. I | 0.20 | 1.00 | 47.1 | 1.00 | 1.00 | 2.0 | 0.64 | 1.00 | 0.5 | 1.00 | |
| | 0.00 | 012 | | | 1505 | | | 252 | 315 | | 1010 | | |
| Lane Grp Cap(c), veh/h | 0 | 913 | 923 | 72 | 1505 | 649 | 291 | 353 | | 415 | 1018 | 428 | |
| . , | 0.00 | 0.30 | 0.30 | 1.07 | 0.91 | 0.14 | 0.09 | 0.14 | 0.16 | 0.52 | 0.27 | 0.16 | |
| Avail Cap(c_a), veh/h | 0 | 913 | 922 | 440 | 1505 | 649 | 345 | 442 | 394 | 415 | 1196 | 503 | |
| | 1.00 | 1.33 | 1.33 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| • | 0.00 | 0.93 | 0.93 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Uniform Delay (d), s/veh | | 5.6 | 5.6 | 50.0 | 19.5 | 9.6 | 30.9 | 31.1 | 31.3 | 29.1 | 25.1 | 24.2 | |
| Incr Delay (d2), s/veh | 0.0 | 0.8 | 0.8 | 126.4 | 9.9 | 0.4 | 0.1 | 0.2 | 0.2 | 0.5 | 0.1 | 0.2 | |
| Initial Q Delay(d3),s/veh | | 0.3 | 0.3 | 0.0 | 3.6 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | |
| %ile BackOfQ(50%),veh/ | | 2.1 | 2.1 | 4.3 | 16.8 | 0.9 | 0.5 | 1.0 | 1.0 | 1.5 | 2.5 | 1.2 | |
| Unsig. Movement Delay, | | | | | | | | | | | | | |
| LnGrp Delay(d),s/veh | 0.0 | 6.7 | 6.7 | 176.4 | 33.0 | 10.1 | 31.0 | 31.3 | 31.5 | 29.6 | 25.3 | 24.3 | |
| LnGrp LOS | A | Α | A | F | С | В | С | С | С | С | С | С | |
| Approach Vol, veh/h | | 547 | | | 1538 | | | 128 | | | 558 | | |
| Approach Delay, s/veh | | 6.7 | | | 38.8 | | | 31.3 | | | 26.8 | | |
| Approach LOS | | Α | | | D | | | С | | | С | | |
| Timer - Assigned Phs | | 2 | | 4 | | 6 | 7 | 8 | | | | | |
| Phs Duration (G+Y+Rc), | S | 63.0 | | 37.0 | | 63.0 | 9.9 | 27.1 | | | | | |
| Change Period (Y+Rc), s | | 5.1 | | * 4.7 | | 5.1 | 3.0 | * 4.7 | | | | | |
| Max Green Setting (Gma | | 52.3 | | * 38 | | 52.3 | 6.9 | * 28 | | | | | |
| Max Q Clear Time (g_c+ | | 7.2 | | 8.5 | | 49.1 | 8.9 | 5.0 | | | | | |
| Green Ext Time (p_c), s | ,, 3 | 8.1 | | 2.2 | | 3.0 | 0.0 | 0.7 | | | | | |
| Intersection Summary | | J., | | | | 3.0 | 3.0 | J., | | | | | |
| | | | 29.7 | | | | | | | | | | |
| HCM 6th LCC | | | | | | | | | | | | | |
| HCM 6th LOS | | | С | | | | | | | | | | |
| Notes | | | | | | | | | | | | | |

^{*} HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

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|---------------------------|-----|-------|---------------|------|------|-------|------|----------|------|------|------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | | | | 414 | | ሻ | ^ | | | ħβ | |
| Traffic Volume (veh/h) | 0 | 0 | 0 | 61 | 335 | 63 | 93 | 502 | 0 | 0 | 567 | 141 |
| Future Volume (veh/h) | 0 | 0 | 0 | 61 | 335 | 63 | 93 | 502 | 0 | 0 | 567 | 141 |
| nitial Q (Qb), veh | | | | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | | | | 1.00 | | 0.92 | 0.99 | | 1.00 | 1.00 | | 0.96 |
| Parking Bus, Adj | | | | 0.85 | 1.00 | 0.85 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.83 |
| Nork Zone On Approach | h | | | | No | | | No | | | No | |
| Adj Sat Flow, veh/h/ln | | | | 1367 | 1367 | 1367 | 1660 | 1660 | 0 | 0 | 1660 | 1660 |
| Adj Flow Rate, veh/h | | | | 66 | 360 | 46 | 100 | 540 | 0 | 0 | 610 | 117 |
| Peak Hour Factor | | | | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 |
| Percent Heavy Veh, % | | | | 3 | 3 | 3 | 3 | 3 | 0 | 0 | 3 | 3 |
| Cap, veh/h | | | | 99 | 562 | 75 | 388 | 1683 | 0 | 0 | 1277 | 244 |
| Arrive On Green | | | | 0.33 | 0.33 | 0.33 | 0.53 | 0.53 | 0.00 | 0.00 | 0.53 | 0.53 |
| Sat Flow, veh/h | | | | 300 | 1704 | 227 | 718 | 3237 | 0 | 0 | 2477 | 458 |
| Grp Volume(v), veh/h | | | | 251 | 0 | 221 | 100 | 540 | 0 | 0 | 401 | 326 |
| Grp Sat Flow(s),veh/h/ln |) | | | 1140 | 0 | 1090 | 718 | 1577 | 0 | 0 | 1577 | 1274 |
| Q Serve(g_s), s | | | | 11.4 | 0.0 | 10.2 | 6.1 | 5.8 | 0.0 | 0.0 | 9.5 | 9.6 |
| Cycle Q Clear(g_c), s | | | | 11.4 | 0.0 | 10.2 | 15.7 | 5.8 | 0.0 | 0.0 | 9.5 | 9.6 |
| Prop In Lane | | | | 0.26 | | 0.21 | 1.00 | | 0.00 | 0.00 | | 0.36 |
| Lane Grp Cap(c), veh/h | | | | 376 | 0 | 359 | 388 | 1683 | 0 | 0 | 842 | 680 |
| V/C Ratio(X) | | | | 0.67 | 0.00 | 0.61 | 0.26 | 0.32 | 0.00 | 0.00 | 0.48 | 0.48 |
| Avail Cap(c_a), veh/h | | | | 490 | 0 | 469 | 388 | 1683 | 0 | 0 | 842 | 680 |
| HCM Platoon Ratio | | | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Jpstream Filter(I) | | | | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 0.00 | 0.00 | 1.00 | 1.00 |
| Jniform Delay (d), s/veh |) | | | 17.3 | 0.0 | 16.9 | 13.7 | 7.9 | 0.0 | 0.0 | 8.8 | 8.8 |
| ncr Delay (d2), s/veh | | | | 2.2 | 0.0 | 1.7 | 1.6 | 0.5 | 0.0 | 0.0 | 1.9 | 2.4 |
| Initial Q Delay(d3),s/veh | | | | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh | | | | 3.0 | 0.0 | 2.5 | 1.1 | 1.8 | 0.0 | 0.0 | 3.2 | 2.7 |
| Jnsig. Movement Delay | | | | | | | | | | | | |
| LnGrp Delay(d),s/veh | | | | 19.5 | 0.0 | 18.6 | 15.3 | 8.4 | 0.0 | 0.0 | 10.7 | 11.2 |
| _nGrp LOS | | | | В | Α | В | В | Α | Α | Α | В | В |
| Approach Vol, veh/h | | | | | 472 | | | 640 | | | 727 | |
| Approach Delay, s/veh | | | | | 19.1 | | | 9.5 | | | 10.9 | |
| Approach LOS | | | | | В | | | Α | | | В | |
| Timer - Assigned Phs | | 2 | | | | 6 | | 8 | | | | |
| Phs Duration (G+Y+Rc) | c | 36.2 | | | | 36.2 | | 23.8 | | | | |
| Change Period (Y+Rc), | | * 4.2 | | | | * 4.2 | | 4.0 | | | | |
| Max Green Setting (Gm | | * 26 | | | | * 26 | | 25.8 | | | | |
| Max Q Clear Time (g_c+ | | 17.7 | | | | 11.6 | | 13.4 | | | | |
| Green Ext Time (p_c), s | , . | 4.2 | | | | 6.8 | | 2.4 | | | | |
| | | 7.2 | | | | 0.0 | | ۷.٦ | | | | |
| ntersection Summary | | | 40.5 | | | | | | | | | |
| HCM 6th Ctrl Delay | | | 12.5 | | | | | | | | | |
| HCM 6th LOS | | | В | | | | | | | | | |
| Notes | | | | | | | | | | | | |

^{*} HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

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|-----------------------------------|-------|----------|-------|------|------------|------------|---------|------------|------|-------------|------------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | | | | 414 | | ¥ | † † | | | ∱ } | |
| Traffic Volume (vph) | 0 | 0 | 0 | 47 | 331 | 43 | 22 | 73 | 0 | 0 | 235 | 174 |
| Future Volume (vph) | 0 | 0 | 0 | 47 | 331 | 43 | 22 | 73 | 0 | 0 | 235 | 174 |
| Ideal Flow (vphpl) | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 |
| Total Lost time (s) | | | | | 3.0 | | 4.0 | 4.0 | | | 4.0 | |
| Lane Util. Factor | | | | | 0.95 | | 1.00 | 0.95 | | | 0.95 | |
| Frpb, ped/bikes | | | | | 1.00 | | 1.00 | 1.00 | | | 0.99 | |
| Flpb, ped/bikes | | | | | 1.00 | | 1.00 | 1.00 | | | 1.00 | |
| Frt | | | | | 0.98 | | 1.00 | 1.00 | | | 0.94 | |
| Flt Protected | | | | | 0.99 | | 0.95 | 1.00 | | | 1.00 | |
| Satd. Flow (prot) | | | | | 2868 | | 1568 | 2885 | | | 2693 | |
| Flt Permitted | | | | | 0.99 | | 0.25 | 1.00 | | | 1.00 | |
| Satd. Flow (perm) | | | | | 2868 | | 413 | 2885 | | | 2693 | |
| Peak-hour factor, PHF | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 |
| Adj. Flow (vph) | 0 | 0 | 0 | 67 | 473 | 61 | 31 | 104 | 0 | 0 | 336 | 249 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 12 | 0 | 0 | 0 | 0 | 0 | 191 | 0 |
| Lane Group Flow (vph) | 0 | 0 | 0 | 0 | 589 | 0 | 31 | 104 | 0 | 0 | 394 | 0 |
| Confl. Bikes (#/hr) | | | 1 | | | 1 | | | 1 | | | 1 |
| Heavy Vehicles (%) | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% |
| Parking (#/hr) | | | | 6 | 6 | 4 | | 12 | | | 11 | 11 |
| Turn Type | | | | Perm | NA | | Perm | NA | | | NA | |
| Protected Phases | | | | | 6 | | | 8 | | | 4 | |
| Permitted Phases | | | | 6 | | | 8 | | | | | |
| Actuated Green, G (s) | | | | | 23.0 | | 16.0 | 16.0 | | | 16.0 | |
| Effective Green, g (s) | | | | | 23.0 | | 16.0 | 16.0 | | | 16.0 | |
| Actuated g/C Ratio | | | | | 0.33 | | 0.23 | 0.23 | | | 0.23 | |
| Clearance Time (s) | | | | | 3.0 | | 4.0 | 4.0 | | | 4.0 | |
| Vehicle Extension (s) | | | | | 2.0 | | 2.0 | 2.0 | | | 2.0 | |
| Lane Grp Cap (vph) | | | | | 942 | | 94 | 659 | | | 615 | |
| v/s Ratio Prot | | | | | | | | 0.04 | | | c0.15 | |
| v/s Ratio Perm | | | | | 0.21 | | 0.08 | | | | | |
| v/c Ratio | | | | | 0.63 | | 0.33 | 0.16 | | | 0.64 | |
| Uniform Delay, d1 | | | | | 19.9 | | 22.5 | 21.6 | | | 24.4 | |
| Progression Factor | | | | | 1.00 | | 1.00 | 1.00 | | | 1.00 | |
| Incremental Delay, d2 | | | | | 3.1 | | 9.1 | 0.5 | | | 5.0 | |
| Delay (s) | | | | | 23.0 | | 31.7 | 22.1 | | | 29.4 | |
| Level of Service | | | | | С | | С | С | | | С | |
| Approach Delay (s) | | 0.0 | | | 23.0 | | | 24.3 | | | 29.4 | |
| Approach LOS | | Α | | | С | | | С | | | С | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 26.0 | Н | CM 2000 | Level of | Service | | С | | | |
| HCM 2000 Volume to Capacity | ratio | | 0.42 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 70.0 | Sı | um of lost | time (s) | | | 11.0 | | | |
| Intersection Capacity Utilization | | | 40.4% | | | of Service | | | A | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

| Intersection | | | | | | |
|------------------------|----------|------|---------|----------|------------|------|
| Int Delay, s/veh | 0.1 | | | | | |
| | | | | | | |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | | 7 | | ^ | ∱ ∱ | |
| Traffic Vol, veh/h | 0 | 0 | 14 | 491 | 632 | 137 |
| Future Vol, veh/h | 0 | 0 | 14 | 491 | 632 | 137 |
| Conflicting Peds, #/hr | 0 | 0 | 46 | 0 | 0 | 46 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | 0 | 25 | - | - | - |
| Veh in Median Storage, | # 0 | - | - | 0 | 0 | - |
| Grade, % | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 94 | 94 | 94 | 94 | 94 | 94 |
| Heavy Vehicles, % | 3 | 3 | 3 | 3 | 3 | 3 |
| Mvmt Flow | 0 | 0 | 15 | 522 | 672 | 146 |
| | • | | 10 | 022 | 0.2 | 1.0 |
| | | | | | | |
| | 1inor2 | | //ajor1 | | /lajor2 | |
| Conflicting Flow All | - | 455 | 864 | 0 | - | 0 |
| Stage 1 | - | - | - | - | - | - |
| Stage 2 | - | - | - | - | - | - |
| Critical Hdwy | - | 6.96 | 4.16 | - | - | - |
| Critical Hdwy Stg 1 | - | - | - | - | - | - |
| Critical Hdwy Stg 2 | - | - | - | - | - | - |
| Follow-up Hdwy | - | 3.33 | 2.23 | - | _ | - |
| Pot Cap-1 Maneuver | 0 | 550 | 768 | _ | - | - |
| Stage 1 | 0 | - | - | - | _ | _ |
| Stage 2 | 0 | _ | _ | _ | _ | _ |
| Platoon blocked, % | U | | | _ | <u>-</u> | _ |
| Mov Cap-1 Maneuver | _ | 526 | 734 | _ | _ | _ |
| Mov Cap-1 Maneuver | <u>-</u> | 520 | 7 34 | - | _ | _ |
| • | - | - | - | - | - | - |
| Stage 1 | | | | - | | |
| Stage 2 | - | - | - | - | - | - |
| | | | | | | |
| Approach | EB | | NB | | SB | |
| HCM Control Delay, s | 0 | | 0.3 | | 0 | |
| HCM LOS | A | | | | | |
| | | | | | | |
| | | NE | NET | -DI 4 | 007 | 000 |
| Minor Lane/Major Mvmt | | NBL | NBT | EBLn1 | SBT | SBR |
| Capacity (veh/h) | | 734 | - | - | - | - |
| HCM Lane V/C Ratio | | 0.02 | - | - | - | - |
| HCM Control Delay (s) | | 10 | - | 0 | - | - |
| HCM Lane LOS | | В | - | Α | - | - |
| HCM 95th %tile Q(veh) | | 0.1 | - | - | - | - |
| | | | | | | |

| Intersection | | | | | | | | | | | | |
|------------------------|-------|------|------|----------|--------|------|------|-------|------|---------|------|------|
| Int Delay, s/veh | 2.8 | | | | | | | | | | | |
| | | | | | | | | | | | | |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | | | | 4₽ | | | | | | ΦÞ | |
| Traffic Vol, veh/h | 0 | 0 | 0 | 0 | 307 | 0 | 0 | 0 | 0 | 0 | 0 | 114 |
| Future Vol, veh/h | 0 | 0 | 0 | 0 | 307 | 0 | 0 | 0 | 0 | 0 | 0 | 114 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 79 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | - | - | - | - | - | - | - | - | - | - |
| Veh in Median Storage, | , # - | 2 | - | - | 0 | - | - | 16974 | - | - | 0 | - |
| Grade, % | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 82 | 82 | 82 | 82 | 82 | 82 | 82 | 82 | 82 | 82 | 82 | 82 |
| Heavy Vehicles, % | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 |
| Mvmt Flow | 0 | 0 | 0 | 0 | 374 | 0 | 0 | 0 | 0 | 0 | 0 | 139 |
| | | | | | | | | | | | | |
| Major/Minor | | | | Major2 | | | | | | /linor2 | | |
| Major/Minor | | | | | ^ | ^ | | | | | 450 | 407 |
| Conflicting Flow All | | | | 79 | 0 | 0 | | | | - | 453 | 187 |
| Stage 1 | | | | - | - | - | | | | - | 374 | - |
| Stage 2 | | | | 4.40 | - | - | | | | - | 79 | - |
| Critical Hdwy | | | | 4.16 | - | - | | | | - | 6.56 | 6.96 |
| Critical Hdwy Stg 1 | | | | - | - | - | | | | - | 5.56 | - |
| Critical Hdwy Stg 2 | | | | - | - | - | | | | - | - | - |
| Follow-up Hdwy | | | | 2.23 | - | - | | | | - | 4.03 | 3.33 |
| Pot Cap-1 Maneuver | | | | 1510 | - | 0 | | | | 0 | 499 | 820 |
| Stage 1 | | | | - | - | 0 | | | | 0 | 614 | - |
| Stage 2 | | | | - | - | 0 | | | | 0 | - | - |
| Platoon blocked, % | | | | 4=:- | - | | | | | | | |
| Mov Cap-1 Maneuver | | | | 1510 | - | - | | | | - | 0 | 820 |
| Mov Cap-2 Maneuver | | | | - | - | - | | | | - | 0 | - |
| Stage 1 | | | | - | - | - | | | | - | 0 | - |
| Stage 2 | | | | - | - | - | | | | - | 0 | - |
| | | | | | | | | | | | | |
| Approach | | | | WB | | | | | | SB | | |
| HCM Control Delay, s | | | | 0 | | | | | | 10.3 | | |
| HCM LOS | | | | | | | | | | В | | |
| | | | | | | | | | | | | |
| Minor Long/Maior M | | WDI | WDT | CDL =4.0 | בי וחי | | | | | | | |
| Minor Lane/Major Mvm | | WBL | WBI | SBLn1 | | | | | | | | |
| Capacity (veh/h) | | 1510 | - | - | 820 | | | | | | | |
| HCM Lane V/C Ratio | | - | - | - | 0.17 | | | | | | | |
| HCM Control Delay (s) | | 0 | - | 0 | 10.3 | | | | | | | |
| HCM Lane LOS | | Α | - | Α | В | | | | | | | |
| HCM 95th %tile Q(veh) | | 0 | - | - | 0.6 | | | | | | | |

| Intersection | | | | | | |
|-------------------------|-------|----------|----------------|-------|--------|------|
| Int Delay, s/veh | 1.8 | | | | | |
| | | | | 11/5- | | |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | ħ₽ | | | 4₽ | | 7 |
| Traffic Vol, veh/h | 667 | 29 | 31 | 1499 | 0 | 79 |
| Future Vol, veh/h | 667 | 29 | 31 | 1499 | 0 | 79 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | - | 0 |
| Veh in Median Storage, | # 0 | _ | _ | 0 | 0 | - |
| Grade, % | 0 | _ | _ | 0 | 0 | _ |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 |
| Mymt Flow | 725 | 32 | 34 | 1629 | 0 | 86 |
| INIVIIIL I IOW | 123 | JZ | J 4 | 1023 | U | 00 |
| | | | | | | |
| Major/Minor Major/Minor | ajor1 | N | Major2 | N | Minor1 | |
| Conflicting Flow All | 0 | 0 | 757 | 0 | - | 379 |
| Stage 1 | _ | _ | _ | _ | _ | - |
| Stage 2 | _ | _ | _ | _ | _ | _ |
| Critical Hdwy | _ | _ | 4.14 | _ | _ | 6.94 |
| Critical Hdwy Stg 1 | _ | <u>-</u> | 7.17 | _ | _ | 0.04 |
| Critical Hdwy Stg 2 | _ | - | - | _ | _ | _ |
| | _ | _ | 2.22 | _ | | 3.32 |
| Follow-up Hdwy | | | | | - | |
| Pot Cap-1 Maneuver | - | - | 850 | - | 0 | 619 |
| Stage 1 | - | - | - | - | 0 | - |
| Stage 2 | - | - | - | - | 0 | - |
| Platoon blocked, % | - | - | | - | | |
| Mov Cap-1 Maneuver | - | - | 850 | - | - | 619 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - |
| Stage 1 | - | - | - | - | - | - |
| Stage 2 | - | - | - | - | - | - |
| | | | | | | |
| | | | 14/5 | | ND | |
| Approach | EB | | WB | | NB | |
| HCM Control Delay, s | 0 | | 2.1 | | 11.8 | |
| HCM LOS | | | | | В | |
| | | | | | | |
| Minor Lang/Major Munt | N | IDI 51 | EDT | EDD | \\/DI | WBT |
| Minor Lane/Major Mvmt | Γ | NBLn1 | EBT | EBR | WBL | |
| Capacity (veh/h) | | 619 | - | - | 850 | - |
| HCM Lane V/C Ratio | | 0.139 | - | - | 0.04 | - |
| HCM Control Delay (s) | | 11.8 | - | - | 9.4 | 1.9 |
| HCM Lane LOS | | В | - | - | Α | Α |
| HCM 95th %tile Q(veh) | | 0.5 | - | - | 0.1 | - |

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|---|-------------|-------------|-------------|------------|-------------|-------------|---|-------------|-------------|-------------|-------------|-------------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ሻ | ∱ ⊅ | | ሻ | ተኈ | | | ∱ ∱ | | ሻ | ^ | 7 |
| Traffic Volume (veh/h) | 35 | 1470 | 54 | 73 | 1374 | 51 | 0 | 228 | 55 | 31 | 164 | 42 |
| Future Volume (veh/h) | 35 | 1470 | 54 | 73 | 1374 | 51 | 0 | 228 | 55 | 31 | 164 | 42 |
| Initial Q (Qb), veh | 0 | 15 | 0 | 0 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | | 0.97 | 1.00 | | 0.97 | 1.00 | | 0.97 | 0.98 | | 0.89 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach | | No | | | No | | _ | No | | | No | |
| Adj Sat Flow, veh/h/ln | 1367 | 1367 | 1367 | 1367 | 1367 | 1367 | 0 | 1660 | 1660 | 1660 | 1660 | 1660 |
| Adj Flow Rate, veh/h | 39 | 1633 | 57 | 81 | 1527 | 54 | 0 | 253 | 40 | 34 | 182 | 18 |
| Peak Hour Factor | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Percent Heavy Veh, % | 3 | 3 | 3 | 3 | 3 | 3 | 0 | 3 | 3 | 3 | 3 | 3 |
| Cap, veh/h | 95 | 1746 | 41 | 72 | 1728 | 54 | 0 | 621 | 97 | 229 | 720 | 286 |
| Arrive On Green | 0.67 | 0.67 | 0.67 | 0.67 | 0.67 | 0.67 | 0.00 | 0.23 | 0.23 | 0.23 | 0.23 | 0.23 |
| Sat Flow, veh/h | 264 | 2558 | 89 | 238 | 2557 | 90 | 0 | 2806 | 424 | 1061 | 3154 | 1254 |
| Grp Volume(v), veh/h | 39 | 826 | 864 | 81 | 774 | 807 | 0 | 145 | 148 | 34 | 182 | 18 |
| Grp Sat Flow(s),veh/h/ln | 264 | 1299 | 1348 | 238 | 1299 | 1348 | 0 | 1577 | 1570 | 1061 | 1577 | 1254 |
| Q Serve(g_s), s | 14.1 | 57.2 | 58.4 | 8.9 | 48.2 | 48.9 | 0.0 | 7.8 | 8.0 | 2.8 | 4.7 | 1.1 |
| Cycle Q Clear(g_c), s | 63.0 | 57.2 | 58.4 | 67.3 | 48.2 | 48.9 | 0.0 | 7.8 | 8.0 | 10.9 | 4.7 | 1.1 |
| Prop In Lane | 1.00 | 074 | 0.07 | 1.00 | 074 | 0.07 | 0.00 | 200 | 0.27 | 1.00 | 700 | 1.00 |
| Lane Grp Cap(c), veh/h | 95 | 874 | 911 | 72 1.12 | 874 | 908 | 0.00 | 360 | 358 | 229 | 720 | 286 |
| V/C Ratio(X) | 0.41 121 | 0.95 874 | 0.95 907 | 93 | 0.89 874 | 0.89 907 | 0.00 | 0.40 420 | 0.41 418 | 0.15 269 | 0.25 839 | 0.06 334 |
| Avail Cap(c_a), veh/h HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 0.30 | 0.30 | 0.30 | 0.00 | 0.81 | 0.81 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 44.8 | 15.7 | 15.8 | 50.0 | 13.9 | 13.9 | 0.00 | 32.8 | 32.9 | 37.5 | 31.6 | 30.2 |
| Incr Delay (d2), s/veh | 12.5 | 19.7 | 19.6 | 95.9 | 4.4 | 4.4 | 0.0 | 0.6 | 0.6 | 0.3 | 0.2 | 0.1 |
| Initial Q Delay(d3),s/veh | 0.0 | 9.7 | 9.4 | 0.0 | 2.1 | 2.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.2 | 0.0 |
| %ile BackOfQ(50%),veh/ln | 1.3 | 22.3 | 23.2 | 3.7 | 13.9 | 14.5 | 0.0 | 3.1 | 3.1 | 0.8 | 1.8 | 0.3 |
| Unsig. Movement Delay, s/veh | | 22.0 | 20.2 | 0.1 | 10.5 | 14.0 | 0.0 | 0.1 | 0.1 | 0.0 | 1.0 | 0.0 |
| LnGrp Delay(d),s/veh | 57.3 | 45.2 | 44.8 | 145.9 | 20.3 | 20.2 | 0.0 | 33.4 | 33.5 | 37.8 | 31.8 | 30.3 |
| LnGrp LOS | E | D | D | F | C | C | A | C | C | D | C | C |
| Approach Vol, veh/h | | 1729 | | <u> </u> | 1662 | | , , <u>, , , , , , , , , , , , , , , , , </u> | 293 | | | 234 | |
| Approach Delay, s/veh | | 45.3 | | | 26.4 | | | 33.4 | | | 32.6 | |
| Approach LOS | | D | | | C | | | С | | | C | |
| Timer - Assigned Phs | | 2 | | 4 | | 6 | | 8 | | | | |
| Phs Duration (G+Y+Rc), s | | 72.7 | | 27.3 | | 72.7 | | 27.3 | | | | |
| Change Period (Y+Rc), s | | 5.4 | | 4.5 | | 5.4 | | 4.5 | | | | |
| Max Green Setting (Gmax), s | | 63.5 | | 26.6 | | 63.5 | | 26.6 | | | | |
| Max Q Clear Time (g_c+l1), s | | 65.0 | | 12.9 | | 69.3 | | 10.0 | | | | |
| Green Ext Time (p_c), s | | 0.0 | | 1.1 | | 0.0 | | 1.6 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 6th Ctrl Delay | | | 35.6 | | | | | | | | | |
| HCM 6th LOS | | | 55.0 D | | | | | | | | | |
| I IOW OUT LOO | | | D | | | | | | | | | |

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|---------------------------|---------|----------|------|-------|----------|------|------|------|-------------|----------|------------|------|--|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR | |
| Lane Configurations | ň | ħβ | | ሻ | ħβ | | ሻ | ħβ | | ሻ | ∱ } | | |
| Traffic Volume (veh/h) | 45 | 1316 | 42 | 93 | 1327 | 32 | 93 | 429 | 168 | 36 | 361 | 63 | |
| Future Volume (veh/h) | 45 | 1316 | 42 | 93 | 1327 | 32 | 93 | 429 | 168 | 36 | 361 | 63 | |
| Initial Q (Qb), veh | 0 | 15 | 0 | 0 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Ped-Bike Adj(A_pbT) | 1.00 | | 0.97 | 1.00 | | 0.98 | 0.99 | | 0.97 | 0.99 | | 0.97 | |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Work Zone On Approac | h | No | | | No | | | No | | | No | | |
| Adj Sat Flow, veh/h/ln | 1367 | 1367 | 1367 | 1367 | 1367 | 1367 | 1660 | 1660 | 1660 | 1660 | 1660 | 1660 | |
| Adj Flow Rate, veh/h | 50 | 1462 | 45 | 103 | 1474 | 34 | 103 | 477 | 156 | 40 | 401 | 56 | |
| Peak Hour Factor | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | |
| Percent Heavy Veh, % | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | |
| Cap, veh/h | 96 | 1639 | 40 | 72 | 1648 | 33 | 194 | 602 | 195 | 142 | 718 | 100 | |
| Arrive On Green | 0.63 | 0.63 | 0.63 | 0.63 | 0.63 | 0.63 | 0.52 | 0.52 | 0.52 | 0.26 | 0.26 | 0.26 | |
| Sat Flow, veh/h | 284 | 2570 | 79 | 284 | 2594 | 60 | 917 | 2322 | 753 | 783 | 2771 | 384 | |
| Grp Volume(v), veh/h | 50 | 737 | 770 | 103 | 737 | 771 | 103 | 323 | 310 | 40 | 227 | 230 | |
| Grp Sat Flow(s),veh/h/lr | ո 284 | 1299 | 1350 | 284 | 1299 | 1355 | 917 | 1577 | 1498 | 783 | 1577 | 1578 | |
| Q Serve(g_s), s | 14.8 | 48.2 | 48.7 | 14.6 | 48.2 | 48.5 | 10.6 | 16.7 | 17.0 | 4.9 | 12.4 | 12.7 | |
| Cycle Q Clear(g_c), s | 63.3 | 48.2 | 48.7 | 63.3 | 48.2 | 48.5 | 23.3 | 16.7 | 17.0 | 21.9 | 12.4 | 12.7 | |
| Prop In Lane | 1.00 | | 0.06 | 1.00 | | 0.04 | 1.00 | | 0.50 | 1.00 | | 0.24 | |
| Lane Grp Cap(c), veh/h | 96 | 822 | 856 | 72 | 822 | 858 | 194 | 409 | 388 | 142 | 409 | 409 | |
| V/C Ratio(X) | 0.52 | 0.90 | 0.90 | 1.43 | 0.90 | 0.90 | 0.53 | 0.79 | 0.80 | 0.28 | 0.55 | 0.56 | |
| Avail Cap(c_a), veh/h | 114 | 822 | 854 | 113 | 822 | 858 | 200 | 420 | 399 | 147 | 420 | 420 | |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 2.00 | 2.00 | 2.00 | 1.00 | 1.00 | 1.00 | |
| Upstream Filter(I) | 0.09 | 0.09 | 0.09 | 1.00 | 1.00 | 1.00 | 0.64 | 0.64 | 0.64 | 1.00 | 1.00 | 1.00 | |
| Uniform Delay (d), s/vel | ո 46.4 | 16.6 | 16.6 | 50.0 | 16.2 | 16.2 | 29.4 | 21.8 | 21.9 | 43.7 | 32.0 | 32.1 | |
| Incr Delay (d2), s/veh | 1.8 | 1.7 | 1.6 | 256.5 | 14.5 | 14.1 | 1.6 | 6.3 | 7.1 | 1.1 | 1.5 | 1.6 | |
| Initial Q Delay(d3),s/veh | 0.0 | 5.8 | 5.4 | 0.0 | 2.6 | 2.4 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | |
| %ile BackOfQ(50%),vel | n/ln1.3 | 15.2 | 15.7 | 6.9 | 16.9 | 17.5 | 2.1 | 5.1 | 5.0 | 1.0 | 4.9 | 5.0 | |
| Unsig. Movement Delay | , s/veh | | | | | | | | | | | | |
| LnGrp Delay(d),s/veh | 48.3 | 24.1 | 23.6 | 306.5 | 33.3 | 32.8 | 31.0 | 28.2 | 29.1 | 44.8 | 33.6 | 33.8 | |
| LnGrp LOS | D | С | С | F | С | С | С | С | С | D | С | С | |
| Approach Vol, veh/h | | 1557 | | | 1611 | | | 736 | | | 497 | | |
| Approach Delay, s/veh | | 24.6 | | | 50.5 | | | 28.9 | | | 34.6 | | |
| Approach LOS | | С | | | D | | | С | | | С | | |
| Timer - Assigned Phs | | 2 | | 4 | | 6 | | 8 | | | | | |
| Phs Duration (G+Y+Rc) | . S | 68.7 | | 31.3 | | 68.7 | | 31.3 | | | | | |
| Change Period (Y+Rc), | | 5.4 | | 5.4 | | 5.4 | | 5.4 | | | | | |
| Max Green Setting (Gm | | 62.6 | | 26.6 | | 62.6 | | 26.6 | | | | | |
| Max Q Clear Time (g_c | | 65.3 | | 23.9 | | 65.3 | | 25.3 | | | | | |
| Green Ext Time (p_c), s | , . | 0.0 | | 0.8 | | 0.0 | | 0.6 | | | | | |
| Intersection Summary | | 3.0 | | 5.5 | | 3.0 | | 3.0 | | | | | |
| HCM 6th Ctrl Delay | | | 36.0 | | | | | | | | | | |
| • | | | | | | | | | | | | | |
| HCM 6th LOS | | | D | | | | | | | | | | |

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|-----------------------------------|------|------------|--------|-------|------------|----------|---------|-------------|----------|----------|------------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | ↑ ↑ | | | €Î}• | | * | ∱ 1≽ | | ň | ∱ } | |
| Traffic Volume (vph) | 0 | 1346 | 90 | 91 | 724 | 48 | 42 | 235 | 101 | 51 | 191 | 50 |
| Future Volume (vph) | 0 | 1346 | 90 | 91 | 724 | 48 | 42 | 235 | 101 | 51 | 191 | 50 |
| Ideal Flow (vphpl) | 1400 | 1400 | 1400 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 |
| Total Lost time (s) | | 5.1 | | | 5.1 | | 4.5 | 4.5 | | 4.5 | 4.5 | |
| Lane Util. Factor | | 0.95 | | | 0.95 | | 1.00 | 0.95 | | 1.00 | 0.95 | |
| Frpb, ped/bikes | | 0.98 | | | 0.98 | | 1.00 | 0.91 | | 1.00 | 0.93 | |
| Flpb, ped/bikes | | 1.00 | | | 1.00 | | 0.79 | 1.00 | | 0.84 | 1.00 | |
| Frt | | 0.99 | | | 0.99 | | 1.00 | 0.95 | | 1.00 | 0.97 | |
| Flt Protected | | 1.00 | | | 0.99 | | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | | 2517 | | | 3030 | | 1235 | 2545 | | 1324 | 2835 | |
| Flt Permitted | | 1.00 | | | 0.57 | | 0.55 | 1.00 | | 0.44 | 1.00 | |
| Satd. Flow (perm) | | 2517 | | | 1736 | | 717 | 2545 | | 612 | 2835 | |
| Peak-hour factor, PHF | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Adj. Flow (vph) | 0 | 1417 | 95 | 96 | 762 | 51 | 44 | 247 | 106 | 54 | 201 | 53 |
| RTOR Reduction (vph) | 0 | 4 | 0 | 0 | 4 | 0 | 0 | 48 | 0 | 0 | 24 | 0 |
| Lane Group Flow (vph) | 0 | 1508 | 0 | 0 | 905 | 0 | 44 | 305 | 0 | 54 | 230 | 0 |
| Confl. Peds. (#/hr) | 423 | | 174 | 174 | | 423 | 282 | | 215 | 215 | | 282 |
| Confl. Bikes (#/hr) | | | 6 | | | 1 | | | 1 | | | 1 |
| Heavy Vehicles (%) | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% |
| Parking (#/hr) | | | | | | | | 8 | 8 | | | |
| Turn Type | | NA | | pm+pt | NA | | Perm | NA | | Perm | NA | |
| Protected Phases | | 2 | | 1 | 6 | | | 8 | | | 4 | |
| Permitted Phases | | | | 6 | | | 8 | | | 4 | | |
| Actuated Green, G (s) | | 59.5 | | | 67.2 | | 23.2 | 23.2 | | 23.2 | 23.2 | |
| Effective Green, g (s) | | 59.5 | | | 67.2 | | 23.2 | 23.2 | | 23.2 | 23.2 | |
| Actuated g/C Ratio | | 0.60 | | | 0.67 | | 0.23 | 0.23 | | 0.23 | 0.23 | |
| Clearance Time (s) | | 5.1 | | | 5.1 | | 4.5 | 4.5 | | 4.5 | 4.5 | |
| Vehicle Extension (s) | | 5.0 | | | 5.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | | 1497 | | | 1224 | | 166 | 590 | | 141 | 657 | |
| v/s Ratio Prot | | c0.60 | | | c0.03 | | | c0.12 | | | 0.08 | |
| v/s Ratio Perm | | | | | 0.46 | | 0.06 | | | 0.09 | | |
| v/c Ratio | | 1.01 | | | 0.74 | | 0.27 | 0.52 | | 0.38 | 0.35 | |
| Uniform Delay, d1 | | 20.2 | | | 10.7 | | 31.4 | 33.5 | | 32.4 | 32.1 | |
| Progression Factor | | 1.00 | | | 0.76 | | 1.00 | 1.00 | | 0.59 | 0.53 | |
| Incremental Delay, d2 | | 25.0 | | | 1.9 | | 0.9 | 0.8 | | 1.4 | 0.3 | |
| Delay (s) | | 45.2 | | | 10.0 | | 32.3 | 34.3 | | 20.5 | 17.4 | |
| Level of Service | | D | | | Α | | С | С | | С | В | |
| Approach Delay (s) | | 45.2 | | | 10.0 | | | 34.0 | | | 17.9 | |
| Approach LOS | | D | | | Α | | | С | | | В | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 30.9 | Н | CM 2000 | Level of | Service | | С | | | |
| HCM 2000 Volume to Capacity r | atio | | 0.87 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 100.0 | S | um of lost | time (s) | | | 12.8 | | | |
| Intersection Capacity Utilization | | | 121.7% | | U Level | | | | Н | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

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|---------------------------|------|------|---------------|-------|------------|------|------|----------|------|------|-------------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ሻ | ħβ | | ሻ | ∱ } | | | ^ | 7 | | † 1> | |
| Traffic Volume (veh/h) | 163 | 1204 | 294 | 102 | 748 | 48 | 85 | 509 | 157 | 0 | 437 | 83 |
| Future Volume (veh/h) | 163 | 1204 | 294 | 102 | 748 | 48 | 85 | 509 | 157 | 0 | 437 | 83 |
| Initial Q (Qb), veh | 0 | 10 | 0 | 0 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 0.97 | 10 | 0.90 | 1.00 | 10 | 0.90 | 0.95 | | 0.82 | 1.00 | • | 0.83 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approac | | No | 1.00 | 1.00 | No | 1.00 | 1.00 | No | 1.00 | 1.00 | No | 1.00 |
| Adj Sat Flow, veh/h/ln | 1367 | 1367 | 1367 | 1660 | 1660 | 1660 | 1660 | 1660 | 1660 | 0 | 1660 | 1660 |
| Adj Flow Rate, veh/h | 172 | 1267 | 302 | 107 | 787 | 47 | 89 | 536 | 140 | 0 | 460 | 71 |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Percent Heavy Veh, % | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 0.55 | 3 | 3 |
| Cap, veh/h | 72 | 1611 | 350 | 72 | 2331 | 136 | 156 | 817 | 299 | 0 | 689 | 105 |
| Arrive On Green | 0.77 | 0.77 | 0.77 | 1.00 | 1.00 | 1.00 | 0.26 | 0.26 | 0.26 | 0.00 | 0.26 | 0.26 |
| Sat Flow, veh/h | 524 | 2045 | 475 | 325 | 3003 | 179 | 826 | 3154 | 1156 | 0.00 | 2744 | 405 |
| | | | | | | | | | | | | |
| Grp Volume(v), veh/h | 172 | 793 | 776 | 107 | 413 | 421 | 89 | 536 | 140 | 0 | 270 | 261 |
| Grp Sat Flow(s),veh/h/li | | 1299 | 1221 | 325 | 1577 | 1605 | 826 | 1577 | 1156 | 0 | 1577 | 1489 |
| Q Serve(g_s), s | 11.2 | 35.2 | 39.3 | 30.4 | 0.0 | 0.0 | 10.2 | 15.2 | 10.2 | 0.0 | 15.3 | 15.7 |
| Cycle Q Clear(g_c), s | 11.6 | 35.2 | 39.3 | 71.5 | 0.0 | 0.0 | 25.9 | 15.2 | 10.2 | 0.0 | 15.3 | 15.7 |
| Prop In Lane | 1.00 | 4007 | 0.39 | 1.00 | 4000 | 0.11 | 1.00 | 047 | 1.00 | 0.00 | 400 | 0.27 |
| Lane Grp Cap(c), veh/h | | 1007 | 952 | 72 | 1222 | 1245 | 156 | 817 | 299 | 0 | 408 | 386 |
| V/C Ratio(X) | 2.38 | 0.79 | 0.82 | 1.48 | 0.34 | 0.34 | 0.57 | 0.66 | 0.47 | 0.00 | 0.66 | 0.68 |
| Avail Cap(c_a), veh/h | 476 | 1007 | 947 | 190 | 1222 | 1244 | 156 | 817 | 299 | 0 | 408 | 386 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 2.00 | 2.00 | 2.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 0.89 | 0.89 | 0.89 | 1.00 | 1.00 | 1.00 | 0.00 | 0.66 | 0.66 |
| Uniform Delay (d), s/vel | | 6.9 | 7.3 | 38.7 | 0.0 | 0.0 | 45.2 | 33.1 | 31.2 | 0.0 | 33.1 | 33.3 |
| Incr Delay (d2), s/veh | | 6.2 | 7.6 | 272.1 | 0.7 | 0.7 | 4.9 | 1.9 | 1.1 | 0.0 | 2.6 | 3.1 |
| Initial Q Delay(d3),s/vel | | 0.8 | 1.1 | 0.0 | 0.2 | 0.2 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),vel | | 10.1 | 10.7 | 7.2 | 0.3 | 0.3 | 2.4 | 6.0 | 2.9 | 0.0 | 6.1 | 6.0 |
| Unsig. Movement Delay | | | | | | | | | | | | |
| LnGrp Delay(d),s/veh | | 14.0 | | 310.8 | 0.8 | 0.8 | 50.1 | 35.0 | 32.4 | 0.0 | 35.8 | 36.4 |
| LnGrp LOS | F | В | В | F | A | A | D | С | С | A | D | D |
| Approach Vol, veh/h | | 1741 | | | 941 | | | 765 | | | 531 | |
| Approach Delay, s/veh | | 83.8 | | | 36.1 | | | 36.3 | | | 36.1 | |
| Approach LOS | | F | | | D | | | D | | | D | |
| Timer - Assigned Phs | | 2 | | 4 | | 6 | | 8 | | | | |
| Phs Duration (G+Y+Rc) |). s | 83.0 | | 31.0 | | 83.0 | | 31.0 | | | | |
| Change Period (Y+Rc), | | 5.1 | | * 5.1 | | 5.1 | | 5.1 | | | | |
| Max Green Setting (Gm | | 64.3 | | * 26 | | 64.3 | | 25.5 | | | | |
| Max Q Clear Time (g_c | , , | 41.3 | | 27.9 | | 73.5 | | 17.7 | | | | |
| Green Ext Time (p_c), s | | 20.4 | | 0.0 | | 0.0 | | 2.1 | | | | |
| " | | 20.7 | | 0.0 | | 0.0 | | ۷. ۱ | | | | |
| Intersection Summary | | | E7.0 | | | | | | | | | |
| HCM 6th Ctrl Delay | | | 57.0 | | | | | | | | | |
| HCM 6th LOS | | | E | | | | | | | | | |
| Notes | | | | | | | | | | | | |

^{*} HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

| • | - | \rightarrow | • | ← | • | 4 | † | 1 | \ | ļ | 4 |
|---|------------|---------------|-------|----------|------|------|------------|------|----------|----------|------|
| Movement EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ↑ ↑ | | ሻ | ^ | 7 | ሻ | ↑ ⊅ | | * | ^ | 7 |
| Traffic Volume (veh/h) 0 | 1127 | 110 | 71 | 854 | 270 | 55 | 232 | 86 | 190 | 193 | 33 |
| Future Volume (veh/h) 0 | 1127 | 110 | 71 | 854 | 270 | 55 | 232 | 86 | 190 | 193 | 33 |
| Initial Q (Qb), veh 0 | 10 | 0 | 0 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) 1.00 | | 0.95 | 0.99 | 10 | 0.95 | 0.92 | • | 0.89 | 0.95 | • | 0.92 |
| Parking Bus, Adj 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach | No | 1.00 | 1.00 | No | 1.00 | 1.00 | No | 1.00 | 1.00 | No | 1.00 |
| Adj Sat Flow, veh/h/ln 0 | 1367 | 1367 | 1660 | 1660 | 1660 | 1660 | 1660 | 1660 | 1660 | 1660 | 1660 |
| Adj Flow Rate, veh/h 0 | 1162 | 107 | 73 | 880 | 175 | 57 | 239 | 89 | 196 | 199 | 10 |
| Peak Hour Factor 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 |
| Percent Heavy Veh, % 0 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 |
| Cap, veh/h 0 | 1343 | 106 | 73 | 1741 | 739 | 340 | 553 | 196 | 335 | 1105 | 453 |
| Arrive On Green 0.00 | 1.00 | 1.00 | 0.55 | 0.55 | 0.55 | 0.25 | 0.25 | 0.25 | 0.07 | 0.35 | 0.35 |
| Sat Flow, veh/h 0 | 2461 | 220 | 430 | 3154 | 1339 | 1067 | 2202 | 780 | 1581 | 3154 | 1295 |
| | 630 | 639 | 73 | 880 | 175 | 57 | 168 | 160 | 196 | 199 | 10 |
| Grp Volume(v), veh/h 0 Grp Sat Flow(s),veh/h/ln 0 | 1299 | 1314 | 430 | 1577 | 1339 | 1067 | 1577 | 1405 | 1581 | 1577 | 1295 |
| 1 (); | 0.0 | 0.0 | 9.2 | 17.3 | 6.7 | 4.2 | 8.9 | 9.6 | 6.9 | 4.4 | 0.5 |
| (0-) | | 0.0 | 9.2 | | 6.7 | 4.2 | 8.9 | 9.6 | 6.9 | 4.4 | 0.5 |
| , (O—); | 0.0 | | | 17.3 | | | 0.9 | | 1.00 | 4.4 | 1.00 |
| Prop In Lane 0.00 | 717 | 0.17 | 1.00 | 1711 | 1.00 | 1.00 | 200 | 0.56 | | 1105 | |
| Lane Grp Cap(c), veh/h 0 | 717 | 729 | 73 | 1741 | 739 | 340 | 396 | 353 | 335 | 1105 | 453 |
| V/C Ratio(X) 0.00 | 0.88 | 0.88 | 1.00 | 0.51 | 0.24 | 0.17 | 0.42 | 0.45 | 0.59 | 0.18 | 0.02 |
| Avail Cap(c_a), veh/h 0 | 717 | 725 | 309 | 1741 | 739 | 371 | 442 | 393 | 335 | 1196 | 491 |
| HCM Platoon Ratio 1.00 | 2.00 | 2.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) 0.00 | 0.20 | 0.20 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh 0.0 | 0.0 | 0.0 | 50.0 | 14.3 | 11.6 | 29.6 | 31.4 | 31.6 | 28.3 | 22.5 | 21.3 |
| Incr Delay (d2), s/veh 0.0 | 3.4 | 3.3 | 105.3 | 1.1 | 8.0 | 0.2 | 0.7 | 0.9 | 1.8 | 0.1 | 0.0 |
| Initial Q Delay(d3),s/veh 0.0 | 2.9 | 2.8 | 0.0 | 0.5 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/lr0.0 | 1.3 | 1.2 | 4.0 | 7.0 | 2.1 | 1.1 | 3.5 | 3.4 | 1.5 | 1.6 | 0.2 |
| Unsig. Movement Delay, s/vel | | | 4== 4 | 4= 0 | 46.5 | 00.0 | 00.4 | 00.0 | 00.4 | 00.0 | 010 |
| LnGrp Delay(d),s/veh 0.0 | 6.3 | 6.1 | 155.3 | 15.9 | 12.3 | 29.8 | 32.1 | 32.6 | 30.1 | 22.6 | 21.3 |
| LnGrp LOS A | Α | Α | F | В | В | С | С | С | С | С | С |
| Approach Vol, veh/h | 1269 | | | 1128 | | | 385 | | | 405 | |
| Approach Delay, s/veh | 6.2 | | | 24.3 | | | 32.0 | | | 26.2 | |
| Approach LOS | Α | | | С | | | С | | | С | |
| Timer - Assigned Phs | 2 | | 4 | | 6 | 7 | 8 | | | | |
| Phs Duration (G+Y+Rc), s | 60.3 | | 39.7 | | 60.3 | 9.9 | 29.8 | | | | |
| Change Period (Y+Rc), s | 5.1 | | * 4.7 | | 5.1 | 3.0 | * 4.7 | | | | |
| Max Green Setting (Gmax), s | 52.3 | | * 38 | | 52.3 | 6.9 | * 28 | | | | |
| Max Q Clear Time (g_c+l1), s | 2.0 | | 6.4 | | 19.3 | 8.9 | 11.6 | | | | |
| Green Ext Time (p_c), s | 26.7 | | 1.4 | | 17.9 | 0.0 | 2.1 | | | | |
| " ' | 20.1 | | 1.4 | | 17.3 | 0.0 | Ζ. Ι | | | | |
| Intersection Summary | | 10.2 | | | | | | | | | |
| HCM 6th Ctrl Delay | | 18.3 | | | | | | | | | |
| HCM 6th LOS | | В | | | | | | | | | |
| Notes | | | | | | | | | | | |

^{*} HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

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|---------------------------|---------|----------|---------------|-----------|------|-----------|------|----------|----------|----------|-----------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | | | | 414 | | ሻ | ^ | | | ħβ | |
| Traffic Volume (veh/h) | 0 | 0 | 0 | 97 | 166 | 66 | 131 | 454 | 0 | 0 | 526 | 102 |
| Future Volume (veh/h) | 0 | 0 | 0 | 97 | 166 | 66 | 131 | 454 | 0 | 0 | 526 | 102 |
| nitial Q (Qb), veh | | | | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | | | | 1.00 | | 0.79 | 0.94 | | 1.00 | 1.00 | | 0.77 |
| Parking Bus, Adj | | | | 0.85 | 1.00 | 0.85 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.83 |
| Work Zone On Approac | h | | | | No | | | No | | | No | |
| Adj Sat Flow, veh/h/ln | | | | 1660 | 1660 | 1660 | 1660 | 1660 | 0 | 0 | 1660 | 1660 |
| Adj Flow Rate, veh/h | | | | 102 | 175 | 49 | 138 | 478 | 0 | 0 | 554 | 82 |
| Peak Hour Factor | | | | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Percent Heavy Veh, % | | | | 3 | 3 | 3 | 3 | 3 | 0 | 0 | 3 | 3 |
| Cap, veh/h | | | | 293 | 516 | 147 | 370 | 1549 | 0 | 0 | 1186 | 174 |
| Arrive On Green | | | | 0.37 | 0.37 | 0.37 | 0.49 | 0.49 | 0.00 | 0.00 | 0.49 | 0.49 |
| Sat Flow, veh/h | | | | 788 | 1387 | 395 | 740 | 3237 | 0.00 | 0.00 | 2497 | 354 |
| Grp Volume(v), veh/h | | | | 176 | 0 | 150 | 138 | 478 | 0 | 0 | 360 | 276 |
| Grp Sat Flow(s),veh/h/lr | 1 | | | 1363 | 0 | 1207 | 740 | 1577 | 0 | 0 | 1577 | 1191 |
| Q Serve(g_s), s | • | | | 5.6 | 0.0 | 5.3 | 9.1 | 5.5 | 0.0 | 0.0 | 9.0 | 9.2 |
| Cycle Q Clear(g_c), s | | | | 5.6 | 0.0 | 5.3 | 18.3 | 5.5 | 0.0 | 0.0 | 9.0 | 9.2 |
| Prop In Lane | | | | 0.58 | 0.0 | 0.33 | 1.00 | 0.0 | 0.00 | 0.00 | 3.0 | 0.30 |
| Lane Grp Cap(c), veh/h | | | | 508 | 0 | 449 | 370 | 1549 | 0.00 | 0.00 | 774 | 585 |
| V/C Ratio(X) | | | | 0.35 | 0.00 | 0.33 | 0.37 | 0.31 | 0.00 | 0.00 | 0.46 | 0.47 |
| Avail Cap(c_a), veh/h | | | | 586 | 0.00 | 519 | 370 | 1549 | 0.00 | 0.00 | 774 | 585 |
| HCM Platoon Ratio | | | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Jpstream Filter(I) | | | | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 0.00 | 0.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | , | | | 13.6 | 0.00 | 13.5 | 16.2 | 9.2 | 0.00 | 0.00 | 10.1 | 10.1 |
| ncr Delay (d2), s/veh | I | | | 0.4 | 0.0 | 0.4 | 2.9 | 0.5 | 0.0 | 0.0 | 2.0 | 2.7 |
| | | | | 0.4 | 0.0 | 0.4 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Initial Q Delay(d3),s/veh | | | | 1.6 | 0.0 | 1.4 | 1.7 | 1.8 | 0.0 | 0.0 | 3.1 | 2.5 |
| %ile BackOfQ(50%),veh | | | | 1.0 | 0.0 | 1.4 | 1.7 | 1.0 | 0.0 | 0.0 | J. I | 2.5 |
| Unsig. Movement Delay | , s/ven | | | 14.0 | 0.0 | 13.9 | 19.1 | 9.7 | 0.0 | 0.0 | 12.1 | 12.8 |
| LnGrp Delay(d),s/veh | | | | 14.0 B | | 13.9 B | | | | | 12.1 B | |
| LnGrp LOS | | | | D | A | D | В | A 646 | <u>A</u> | <u>A</u> | | В |
| Approach Vol, veh/h | | | | | 326 | | | 616 | | | 636 | |
| Approach Delay, s/veh | | | | | 14.0 | | | 11.8 | | | 12.4 | |
| Approach LOS | | | | | В | | | В | | | В | |
| Timer - Assigned Phs | | 2 | | | | 6 | | 8 | | | | |
| Phs Duration (G+Y+Rc) | , S | 33.7 | | | | 33.7 | | 26.3 | | | | |
| Change Period (Y+Rc), | | * 4.2 | | | | * 4.2 | | 4.0 | | | | |
| Max Green Setting (Gm | | * 26 | | | | * 26 | | 25.8 | | | | |
| Max Q Clear Time (g_c- | | 20.3 | | | | 11.2 | | 7.6 | | | | |
| Green Ext Time (p_c), s | | 3.0 | | | | 6.2 | | 1.9 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| · | | | 12.5 | | | | | | | | | |
| HCM 6th Ctrl Delay | | | | | | | | | | | | |
| HCM 6th LOS | | | В | | | | | | | | | |
| Votes | | | | | | | | | | | | |

^{*} HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

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|-----------------------------------|-------|------|-------|------|------------|------------|---------|------------|------|-------------|-------------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | | | | 413- | | ሻ | † † | | | ∱ 1≽ | |
| Traffic Volume (vph) | 0 | 0 | 0 | 86 | 197 | 145 | 54 | 297 | 0 | 0 | 368 | 118 |
| Future Volume (vph) | 0 | 0 | 0 | 86 | 197 | 145 | 54 | 297 | 0 | 0 | 368 | 118 |
| Ideal Flow (vphpl) | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 |
| Total Lost time (s) | | | | | 3.0 | | 4.0 | 4.0 | | | 4.0 | |
| Lane Util. Factor | | | | | 0.95 | | 1.00 | 0.95 | | | 0.95 | |
| Frpb, ped/bikes | | | | | 1.00 | | 1.00 | 1.00 | | | 1.00 | |
| Flpb, ped/bikes | | | | | 1.00 | | 1.00 | 1.00 | | | 1.00 | |
| Frt | | | | | 0.95 | | 1.00 | 1.00 | | | 0.96 | |
| Flt Protected | | | | | 0.99 | | 0.95 | 1.00 | | | 1.00 | |
| Satd. Flow (prot) | | | | | 2743 | | 1568 | 2885 | | | 2779 | |
| Flt Permitted | | | | | 0.99 | | 0.30 | 1.00 | | | 1.00 | |
| Satd. Flow (perm) | | | | | 2743 | | 503 | 2885 | | | 2779 | |
| Peak-hour factor, PHF | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Adj. Flow (vph) | 0 | 0 | 0 | 91 | 207 | 153 | 57 | 313 | 0 | 0 | 387 | 124 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 90 | 0 | 0 | 0 | 0 | 0 | 44 | 0 |
| Lane Group Flow (vph) | 0 | 0 | 0 | 0 | 361 | 0 | 57 | 313 | 0 | 0 | 467 | 0 |
| Confl. Bikes (#/hr) | | | 1 | | | 1 | | | 1 | | | 1 |
| Heavy Vehicles (%) | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% |
| Parking (#/hr) | | | | 6 | 6 | 4 | | 12 | | | 11 | 11 |
| Turn Type | | | | Perm | NA | | Perm | NA | | | NA | |
| Protected Phases | | | | | 6 | | | 8 | | | 4 | |
| Permitted Phases | | | | 6 | | | 8 | | | | | |
| Actuated Green, G (s) | | | | | 23.0 | | 16.0 | 16.0 | | | 16.0 | |
| Effective Green, g (s) | | | | | 23.0 | | 16.0 | 16.0 | | | 16.0 | |
| Actuated g/C Ratio | | | | | 0.33 | | 0.23 | 0.23 | | | 0.23 | |
| Clearance Time (s) | | | | | 3.0 | | 4.0 | 4.0 | | | 4.0 | |
| Vehicle Extension (s) | | | | | 2.0 | | 2.0 | 2.0 | | | 2.0 | |
| Lane Grp Cap (vph) | | | | | 901 | | 114 | 659 | | | 635 | |
| v/s Ratio Prot | | | | | | | | 0.11 | | | c0.17 | |
| v/s Ratio Perm | | | | | 0.13 | | 0.11 | | | | | |
| v/c Ratio | | | | | 0.40 | | 0.50 | 0.47 | | | 0.74 | |
| Uniform Delay, d1 | | | | | 18.2 | | 23.5 | 23.4 | | | 25.0 | |
| Progression Factor | | | | | 1.00 | | 1.00 | 1.00 | | | 1.00 | |
| Incremental Delay, d2 | | | | | 1.3 | | 14.8 | 2.4 | | | 7.4 | |
| Delay (s) | | | | | 19.5 | | 38.3 | 25.8 | | | 32.5 | |
| Level of Service | | | | | В | | D | С | | | С | |
| Approach Delay (s) | | 0.0 | | | 19.5 | | | 27.7 | | | 32.5 | |
| Approach LOS | | Α | | | В | | | С | | | С | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 26.8 | Н | CM 2000 | Level of | Service | | С | | | |
| HCM 2000 Volume to Capacity | ratio | | 0.36 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 70.0 | S | um of lost | time (s) | | | 11.0 | | | |
| Intersection Capacity Utilization | | | 48.0% | IC | U Level | of Service | | | Α | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

| Intersection | | | | | | |
|------------------------|-------|----------|---------|----------|------------|------|
| Int Delay, s/veh | 0.1 | | | | | |
| | | EDD | NDI | NDT | CDT | CDD |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | | 7 | Ť | ^ | ∱ } | |
| Traffic Vol, veh/h | 0 | 0 | 9 | 751 | 630 | 152 |
| Future Vol, veh/h | 0 | 0 | 9 | 751 | 630 | 152 |
| Conflicting Peds, #/hr | 0 | 0 | 406 | 0 | 0 | 406 |
| | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | 0 | 25 | - | - | - |
| Veh in Median Storage, | # 0 | - | - | 0 | 0 | - |
| Grade, % | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 95 | 95 | 95 | 95 | 95 | 95 |
| Heavy Vehicles, % | 3 | 3 | 3 | 3 | 3 | 3 |
| Mvmt Flow | 0 | 0 | 9 | 791 | 663 | 160 |
| WWW.CTIOW | | • | U | 701 | 000 | 100 |
| | | | | | | |
| Major/Minor M | inor2 | N | //ajor1 | Λ | /lajor2 | |
| Conflicting Flow All | - | 818 | 1229 | 0 | - | 0 |
| Stage 1 | - | - | - | - | - | - |
| Stage 2 | - | - | - | - | - | - |
| Critical Hdwy | _ | 6.96 | 4.16 | - | _ | - |
| Critical Hdwy Stg 1 | _ | - | - | _ | _ | _ |
| Critical Hdwy Stg 2 | _ | _ | _ | _ | _ | _ |
| Follow-up Hdwy | _ | 3.33 | 2.23 | _ | _ | _ |
| Pot Cap-1 Maneuver | 0 | 317 | 557 | _ | _ | _ |
| Stage 1 | 0 | - | - 551 | | _ | _ |
| | 0 | <u>-</u> | - | <u>-</u> | <u>-</u> | - |
| Stage 2 | U | - | _ | - | - | - |
| Platoon blocked, % | | 101 | 0.40 | - | - | - |
| Mov Cap-1 Maneuver | - | 194 | 342 | - | - | - |
| Mov Cap-2 Maneuver | - | - | - | - | - | - |
| Stage 1 | - | - | - | - | - | - |
| Stage 2 | - | - | - | | - | - |
| | | | | | | |
| Approach | EB | | NB | | SB | |
| | | | | | | |
| HCM Control Delay, s | 0 | | 0.2 | | 0 | |
| HCM LOS | Α | | | | | |
| | | | | | | |
| Minor Lane/Major Mvmt | | NBL | NBT | EBLn1 | SBT | SBR |
| Capacity (veh/h) | | 342 | | | | |
| HCM Lane V/C Ratio | | 0.028 | - | _ | _ | - |
| | | | - | 0 | - | - |
| HCM Control Delay (s) | | 15.8 | - | | - | - |
| HCM Lane LOS | | C | - | Α | - | - |
| HCM 95th %tile Q(veh) | | 0.1 | - | - | - | - |

| Intersection | | | | | | | | | | | | |
|------------------------|------|------|------|--------|-------|------|------|-------|------|--------|------------|------|
| Int Delay, s/veh | 1.2 | | | | | | | | | | | |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| | EDL | EBI | EBK | WAR | | WBK | INDL | INDI | NDK | OBL | | SBK |
| Lane Configurations | ^ | ٥ | ٥ | 0 | 41 | ^ | ٥ | ٥ | 0 | ۸ | ↑ ↑ | T 4 |
| Traffic Vol, veh/h | 0 | 0 | 0 | 0 | 374 | 0 | 0 | 0 | 0 | 0 | 0 | 54 |
| Future Vol, veh/h | 0 | 0 | 0 | 0 | 374 | 0 | 0 | 0 | 0 | 0 | 0 | 54 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 251 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | | - | - | None |
| Storage Length | - | - | - | - | - | - | - | 40074 | - | - | - | - |
| Veh in Median Storage, | # - | 2 | - | - | 0 | - | | 16974 | - | - | 0 | - |
| Grade, % | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 |
| Heavy Vehicles, % | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 |
| Mvmt Flow | 0 | 0 | 0 | 0 | 394 | 0 | 0 | 0 | 0 | 0 | 0 | 57 |
| | | | | | | | | | | | | |
| Major/Minor | | | | Major2 | | | | | N | Minor2 | | |
| Conflicting Flow All | | | | 251 | 0 | 0 | | | | - | 645 | 197 |
| Stage 1 | | | | - | - | - | | | | - | 394 | - |
| Stage 2 | | | | - | - | - | | | | - | 251 | _ |
| Critical Hdwy | | | | 4.16 | - | - | | | | - | 6.56 | 6.96 |
| Critical Hdwy Stg 1 | | | | - | _ | _ | | | | _ | 5.56 | - |
| Critical Hdwy Stg 2 | | | | _ | _ | _ | | | | - | - | _ |
| Follow-up Hdwy | | | | 2.23 | _ | _ | | | | _ | 4.03 | 3.33 |
| Pot Cap-1 Maneuver | | | | 1304 | _ | 0 | | | | 0 | 387 | 808 |
| Stage 1 | | | | - | _ | 0 | | | | 0 | 601 | - |
| Stage 2 | | | | _ | _ | 0 | | | | 0 | - | _ |
| Platoon blocked, % | | | | | _ | | | | | | | |
| Mov Cap-1 Maneuver | | | | 1304 | _ | _ | | | | - | 0 | 808 |
| Mov Cap-2 Maneuver | | | | - | _ | _ | | | | _ | 0 | - |
| Stage 1 | | | | _ | _ | _ | | | | - | 0 | _ |
| Stage 2 | | | | - | _ | _ | | | | _ | 0 | _ |
| | | | | | | | | | | | | |
| Approach | | | | WB | | | | | | SB | | |
| HCM Control Delay, s | | | | 0 | | | | | | 9.8 | | |
| HCM LOS | | | | | | | | | | A | | |
| | | | | | | | | | | , , | | |
| Minor Lane/Major Mvmt | | WBL | WBT: | SBLn1 | SBLn2 | | | | | | | |
| Capacity (veh/h) | | 1304 | - | - | 808 | | | | | | | |
| HCM Lane V/C Ratio | | - | _ | - | 0.07 | | | | | | | |
| HCM Control Delay (s) | | 0 | _ | 0 | 9.8 | | | | | | | |
| HCM Lane LOS | | Ā | _ | A | A | | | | | | | |
| HCM 95th %tile Q(veh) | | 0 | _ | - | 0.2 | | | | | | | |
| | | _ | | | 7.2 | | | | | | | |

| Intersection | | | | | | |
|------------------------|--------------------|-----------|----------|------|---------|-------------|
| Int Delay, s/veh | 8 | | | | | |
| | | EDD. | MDI | MPT | ND | NDD |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | † | 00 | 00 | 41 | • | 7 |
| , | 1340 | 82 | 88 | 856 | 0 | 235 |
| | 1340 | 82 | 88 | 856 | 0 | 235 |
| Conflicting Peds, #/hr | _ 0 | 100 | 100 | _ 0 | 0 | 0 |
| 0 | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | - | 0 |
| Veh in Median Storage, | | - | - | 0 | 0 | - |
| Grade, % | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 96 | 96 | 96 | 96 | 96 | 96 |
| Heavy Vehicles, % | 3 | 3 | 3 | 3 | 3 | 3 |
| Mvmt Flow | 1396 | 85 | 92 | 892 | 0 | 245 |
| | | | | | | |
| Major/Minor M | ajor1 | N | Major2 | N | /linor1 | |
| | <u>ajui i</u> 0 | | 1581 | 0 | | 841 |
| Conflicting Flow All | | 0 | 1001 | | - | 04 1 |
| Stage 1 | - | - | - | - | - | - |
| Stage 2 | - | - | 4.40 | - | - | - |
| Critical Hdwy | - | - | 4.16 | - | - | 6.96 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - |
| Critical Hdwy Stg 2 | - | - | - | - | - | - |
| Follow-up Hdwy | - | - | 2.23 | - | - | 3.33 |
| Pot Cap-1 Maneuver | - | - | 407 | - | 0 | 306 |
| Stage 1 | - | - | - | - | 0 | - |
| Stage 2 | - | - | - | - | 0 | - |
| Platoon blocked, % | - | - | | - | | |
| Mov Cap-1 Maneuver | - | - | 368 | - | - | 277 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - |
| Stage 1 | - | - | - | - | - | - |
| Stage 2 | - | - | - | - | - | - |
| , | | | | | | |
| A | ED | | WD | | ND | |
| Approach | EB | | WB | | NB | |
| HCM Control Delay, s | 0 | | 5 | | 68.3 | |
| HCM LOS | | | | | F | |
| | | | | | | |
| Minor Lane/Major Mvmt | 1 | NBLn1 | EBT | EBR | WBL | WBT |
| Capacity (veh/h) | | 277 | | - | | - |
| HCM Lane V/C Ratio | | 0.884 | <u>-</u> | | 0.249 | - |
| HCM Control Delay (s) | | 68.3 | <u>-</u> | _ | 18 | 3.7 |
| HCM Lane LOS | | 00.3 F | - | - | C | 3. <i>1</i> |
| HCM 95th %tile Q(veh) | | 7.8 | | - | 1 | - - |
| now your wille Q(ven) | | 7.0 | - | - | l | - |

| | ۶ | → | • | € | ← | • | • | † | <i>></i> | > | ↓ | -√ |
|--|------------|-------------|-------------|-----------------|-------------|-------------|------|-------------|-------------|-------------|-------------|-------------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | ∱ ⊅ | | ሻ | ∱ ∱ | | | ∱ ∱ | | 7 | ^ | 7 |
| Traffic Volume (veh/h) | 30 | 1590 | 30 | 90 | 1750 | 30 | 0 | 80 | 30 | 30 | 320 | 50 |
| Future Volume (veh/h) | 30 | 1590 | 30 | 90 | 1750 | 30 | 0 | 80 | 30 | 30 | 320 | 50 |
| Initial Q (Qb), veh | 0 | 10 | 0 | 0 | 15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | | 0.97 | 1.00 | | 0.99 | 1.00 | | 0.97 | 0.99 | | 0.98 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach | | No | | | No | | _ | No | | | No | |
| Adj Sat Flow, veh/h/ln | 1367 | 1367 | 1367 | 1367 | 1367 | 1367 | 0 | 1660 | 1660 | 1660 | 1660 | 1660 |
| Adj Flow Rate, veh/h | 33 | 1767 | 32 | 100 | 1944 | 32 | 0 | 89 | 17 | 33 | 356 | 37 |
| Peak Hour Factor | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Percent Heavy Veh, % | 3 | 3 | 3 | 3 | 3 | 3 | 0 | 3 | 3 | 3 | 3 | 3 |
| Cap, veh/h | 72 | 1906 | 29 | 72 | 1921 | 17 | 0 | 457 | 85 | 253 | 545 | 239 |
| Arrive On Green | 0.73 | 0.73 | 0.73 | 0.73 | 0.73 | 0.73 | 0.00 | 0.17 | 0.17 | 0.17 | 0.17 | 0.17 |
| Sat Flow, veh/h | 180 | 2609 | 47 | 214 | 2615 | 43 | 0 | 2727 | 490 | 1265 | 3154 | 1380 |
| Grp Volume(v), veh/h | 33 | 877 | 922 | 100 | 963 | 1013 | 0 | 52 | 54 | 33 | 356 | 37 |
| Grp Sat Flow(s), veh/h/ln | 180 | 1299 | 1357 | 214 | 1299 | 1359 | 0 | 1577 | 1557 | 1265 | 1577 | 1380 |
| Q Serve(g_s), s | 0.0 | 56.6 | 57.6 | 15.3 | 72.8 | 72.8 | 0.0 | 2.8 | 3.0 | 2.3 | 10.5 | 2.3 |
| Cycle Q Clear(g_c), s | 72.8 | 56.6 | 57.6 | 72.8 | 72.8 | 72.8 | 0.0 | 2.8 | 3.0 | 5.3 | 10.5 | 2.3 |
| Prop In Lane | 1.00 | 0.40 | 0.03 | 1.00 | 0.40 | 0.03 | 0.00 | 070 | 0.31 | 1.00 | 545 | 1.00 |
| Lane Grp Cap(c), veh/h | 72 | 946 | 989 | 72 | 946 | 992 | 0 | 273 | 269 | 253 | 545 | 239 |
| V/C Ratio(X) | 0.46 | 0.93 | 0.93 | 1.39 | 1.02 | 1.02 | 0.00 | 0.19 | 0.20 | 0.13 | 0.65 | 0.16 |
| Avail Cap(c_a), veh/h | 72 1.00 | 946 1.00 | 988 1.00 | 105 1.00 | 946 1.00 | 989 1.00 | 1.00 | 420 1.00 | 414 1.00 | 371 1.00 | 839 1.00 | 367 1.00 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 0.09 | 0.09 | 0.09 | 0.00 | 0.98 | 0.98 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 50.0 | 12.0 | 12.1 | 50.0 | 13.6 | 13.6 | 0.00 | 35.4 | 35.4 | 37.7 | 38.6 | 35.1 |
| Uniform Delay (d), s/veh Incr Delay (d2), s/veh | 19.6 | 16.3 | 16.2 | 182.7 | 13.8 | 14.7 | 0.0 | 0.3 | 0.4 | 0.2 | 1.3 | 0.3 |
| Initial Q Delay(d3),s/veh | 0.0 | 2.8 | 2.7 | 0.0 | 28.6 | 27.2 | 0.0 | 0.0 | 0.4 | 0.2 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/ln | 1.2 | 18.0 | 18.9 | 5.4 | 26.6 | 27.8 | 0.0 | 1.1 | 1.2 | 0.7 | 4.2 | 0.8 |
| Unsig. Movement Delay, s/veh | | 10.0 | 10.5 | J. T | 20.0 | 21.0 | 0.0 | 1.1 | 1.2 | 0.1 | 7.2 | 0.0 |
| LnGrp Delay(d),s/veh | 69.6 | 31.1 | 31.1 | 232.7 | 55.9 | 55.5 | 0.0 | 35.7 | 35.8 | 37.9 | 39.9 | 35.4 |
| LnGrp LOS | 65.6 E | C | C | F | 55.5 F | 55.5 F | Α | D | D | D | D | D |
| Approach Vol, veh/h | | 1832 | | <u>'</u> | 2076 | <u>'</u> | | 106 | | | 426 | |
| Approach Delay, s/veh | | 31.8 | | | 64.2 | | | 35.7 | | | 39.3 | |
| Approach LOS | | C C | | | E | | | D | | | D | |
| | | | | | | | | | | | | |
| Timer - Assigned Phs | | 2 | | 4 | | 6 | | 8 | | | | |
| Phs Duration (G+Y+Rc), s | | 78.2 | | 21.8 | | 78.2 | | 21.8 | | | | |
| Change Period (Y+Rc), s | | 5.4 | | 4.5 | | 5.4 | | 4.5 | | | | |
| Max Green Setting (Gmax), s | | 63.5 | | 26.6 | | 63.5 | | 26.6 | | | | |
| Max Q Clear Time (g_c+l1), s | | 74.8 | | 12.5 | | 74.8 | | 5.0 | | | | |
| Green Ext Time (p_c), s | | 0.0 | | 2.2 | | 0.0 | | 0.5 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 6th Ctrl Delay | | | 47.8 | | | | | | | | | |
| HCM 6th LOS | | | D | | | | | | | | | |

| ane Configurations 1 | | ۶ | → | • | • | ← | • | 1 | † | <i>></i> | \ | ļ | ✓ | |
|--|---------------------------|------|------------|------|-------|----------|------|------|----------|-------------|----------|------|------|--|
| raffic Volume (veh/h) | Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR | |
| raffic Volume (veh/h) | Lane Configurations | ሻ | ∱ Ъ | | * | ħβ | | ሻ | ħβ | | * | ħβ | | |
| uture Volume (vehvlh) 40 1770 30 100 1530 40 20 360 150 40 500 60 ed-Bike Adji(A, pbr) 1.00 0 0 10 0 15 0 0 0 0 0 0 ed-Bike Adji(A, pbr) 1.00 1.0 | Traffic Volume (veh/h) | 40 | | 30 | 100 | | 40 | | | 150 | 40 | | 60 | |
| red-Bike Adj(A_pbT) 1.00 | Future Volume (veh/h) | 40 | 1770 | 30 | 100 | 1530 | 40 | 20 | 360 | 150 | 40 | 500 | 60 | |
| Parking Bus, Adj | Initial Q (Qb), veh | 0 | 10 | 0 | 0 | 15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Nork Zone On Approach | Ped-Bike Adj(A_pbT) | 1.00 | | 0.98 | 1.00 | | 0.97 | 0.99 | | 0.97 | 0.99 | | 0.98 | |
| dj Sat Flow, veh/hi/n 1367 1367 1367 1367 1367 1367 1367 1367 | Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| dj Flow Rate, veh/h 44 1967 32 111 1700 42 22 240 157 44 556 57 eak Hour Factor 0.90 | Work Zone On Approacl | h | No | | | No | | | No | | | No | | |
| Server Company Compa | Adj Sat Flow, veh/h/ln | 1367 | 1367 | | 1367 | 1367 | 1367 | 1660 | 1660 | 1660 | 1660 | 1660 | 1660 | |
| Percent Heavy Veh, % 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 | Adj Flow Rate, veh/h | | | | 111 | 1700 | 42 | | | | | | | |
| Rap, veh/h 72 1717 15 72 1711 20 119 530 205 147 695 71 Arrive On Green 0.65 0.65 0.65 0.65 0.65 0.65 0.65 0.65 | Peak Hour Factor | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | |
| Arrive On Green 0.65 0.65 0.65 0.65 0.65 0.65 0.65 0.65 | Percent Heavy Veh, % | | | | | | | 3 | | 3 | | | | |
| tat Flow, veh/h | Cap, veh/h | | | | | | | | | | | | | |
| Gry Volume(v), veh/h 44 974 1025 111 850 892 22 285 272 44 304 309 Grp Sat Flow(s), veh/h/ln 226 1299 1359 176 1299 1353 798 1577 1473 840 1577 1600 Very Cle Q Clear(g_c), s 0.0 65.1 | Arrive On Green | | | | | | | | | | | | | |
| Strip Sat Flow(s), veh/h/ln 226 1299 1359 176 1299 1353 798 1577 1473 840 1577 1600 2 Serve(g_s), s | Sat Flow, veh/h | | | | | 2589 | | | | | | | | |
| R Serve(g_s), s | Grp Volume(v), veh/h | | | | 111 | | 892 | | | | | | | |
| Sycle Q Clear(g_c), s 65.1 65.1 65.1 65.1 65.1 65.1 65.1 20.8 14.7 15.1 20.2 18.1 18.2 chrop In Lane 1.00 0.03 1.00 0.05 1.00 0.58 1.00 0.18 ane Grp Cap(c), veh/h 72 845 887 72 845 886 119 380 355 147 380 386 Wail Cap(c_a), veh/h 72 845 884 72 845 881 139 420 392 168 420 426 ICM Platon Ratio 1.00 1.00 1.00 1.00 1.00 1.00 1.00 2.00 2 | | | | | | | | | | | | | | |
| Trop In Lane 1.00 0.03 1.00 0.05 1.00 0.58 1.00 0.18 and Grp Cap(c), veh/h 72 845 887 72 845 886 119 380 355 147 380 386 7/C Ratio(X) 0.61 1.15 1.16 1.54 1.01 1.01 0.18 0.75 0.77 0.30 0.80 0.80 vail Cap(c_a), veh/h 72 845 884 72 845 881 139 420 392 168 420 426 (ICM Platoon Ratio 1.00 1.00 1.00 1.00 1.00 1.00 2.00 2.00 | Q Serve(g_s), s | 0.0 | 65.1 | 65.1 | 0.0 | 65.1 | 65.1 | 2.6 | 14.7 | 15.1 | 5.0 | 18.1 | 18.2 | |
| ane Grp Cap(c), veh/h 72 845 887 72 845 886 119 380 355 147 380 386 //C Ratio(X) | Cycle Q Clear(g_c), s | 65.1 | 65.1 | 65.1 | 65.1 | 65.1 | 65.1 | 20.8 | 14.7 | 15.1 | 20.2 | 18.1 | 18.2 | |
| ### CRatio(X) | Prop In Lane | 1.00 | | 0.03 | 1.00 | | 0.05 | 1.00 | | 0.58 | 1.00 | | 0.18 | |
| Avail Cap(c_a), veh/h 72 845 884 72 845 881 139 420 392 168 420 426 11 100 1.00 1.00 1.00 1.00 1.00 1.00 1 | Lane Grp Cap(c), veh/h | 72 | 845 | 887 | 72 | 845 | 886 | 119 | 380 | 355 | 147 | 380 | 386 | |
| CM Platoon Ratio 1.00 1.00 1.00 1.00 1.00 1.00 1.00 2.00 2.00 2.00 1. | V/C Ratio(X) | 0.61 | 1.15 | 1.16 | 1.54 | 1.01 | 1.01 | 0.18 | 0.75 | 0.77 | 0.30 | 0.80 | 0.80 | |
| Postream Filter(I) | Avail Cap(c_a), veh/h | | | | | 845 | 881 | 139 | 420 | 392 | 168 | 420 | | |
| Iniform Delay (d), s/veh 50.0 17.5 17.5 50.0 17.5 17.5 33.5 23.4 23.6 43.7 35.7 35.7 ncr Delay (d2), s/veh 3.5 69.8 71.5 301.3 32.4 31.9 0.6 5.3 6.4 1.1 9.6 9.8 nitial Q Delay(d3),s/veh 0.0 21.3 20.3 0.0 31.9 30.5 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 | HCM Platoon Ratio | 1.00 | | | 1.00 | 1.00 | 1.00 | 2.00 | 2.00 | 2.00 | | 1.00 | | |
| ncr Delay (d2), s/veh 3.5 69.8 71.5 301.3 32.4 31.9 0.6 5.3 6.4 1.1 9.6 9.8 nitial Q Delay(d3), s/veh 0.0 21.3 20.3 0.0 31.9 30.5 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 | Upstream Filter(I) | 0.09 | 0.09 | | | 1.00 | 1.00 | | | | | | | |
| nitial Q Delay(d3),s/veh 0.0 21.3 20.3 0.0 31.9 30.5 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 | Uniform Delay (d), s/veh | 50.0 | | | 50.0 | 17.5 | 17.5 | 33.5 | | | | | 35.7 | |
| 6ile BackOfQ(50%),yeh/lrl.2 37.4 39.4 7.8 31.1 32.1 0.5 4.6 4.5 1.1 7.9 8.1 Insig. Movement Delay, s/veh nGrp Delay(d),s/veh 53.5 108.5 109.2 351.3 81.8 79.9 34.1 28.8 30.0 44.8 45.2 45.5 nGrp LOS D F F F F C C C D D D approach Vol, veh/h 2043 1853 579 657 <td>Incr Delay (d2), s/veh</td> <td></td> | Incr Delay (d2), s/veh | | | | | | | | | | | | | |
| Unsig. Movement Delay, s/veh InGrp Delay(d),s/veh 53.5 108.5 109.2 351.3 81.8 79.9 34.1 28.8 30.0 44.8 45.2 45.5 InGrp LOS D F F F F F F C C C D D D Improach Vol, veh/h 2043 1853 579 657 Improach Delay, s/veh 107.7 97.0 29.5 45.3 Improach LOS F F F C C D D Improach LOS F F F F C C D Improach LOS F F F F C C D Improach LOS F F C C C D Improach LOS F C D Improach LOS F F F F F F F F F F F F F F F F F F F | Initial Q Delay(d3),s/veh | | | | | | | | | | | | | |
| nGrp Delay(d),s/veh 53.5 108.5 109.2 351.3 81.8 79.9 34.1 28.8 30.0 44.8 45.2 45.5 nGrp LOS | | | | 39.4 | 7.8 | 31.1 | 32.1 | 0.5 | 4.6 | 4.5 | 1.1 | 7.9 | 8.1 | |
| nGrp LOS D F F F F F C C C D D D Approach Vol, veh/h 2043 1853 579 657 Approach Delay, s/veh 107.7 97.0 29.5 45.3 Approach LOS F F C C D Timer - Assigned Phs 2 4 6 8 Phs Duration (G+Y+Rc), s 70.5 29.5 70.5 29.5 Change Period (Y+Rc), s 5.4 5.4 5.4 5.4 Max Green Setting (Gmax), s 62.6 26.6 62.6 26.6 Max Q Clear Time (g_c+11), s 67.1 22.2 67.1 22.8 Green Ext Time (p_c), s 0.0 1.7 0.0 1.3 Intersection Summary ICM 6th Ctrl Delay 87.0 | | | | | | | | | | | | | | |
| Approach Vol, veh/h 2043 1853 579 657 Approach Delay, s/veh 107.7 97.0 29.5 45.3 Approach LOS F F F C D Timer - Assigned Phs 2 4 6 8 Phs Duration (G+Y+Rc), s 70.5 29.5 70.5 29.5 Change Period (Y+Rc), s 5.4 5.4 5.4 5.4 Max Green Setting (Gmax), s 62.6 26.6 62.6 26.6 Max Q Clear Time (g_c+I1), s 67.1 22.2 67.1 22.8 Approach Vol, veh/h 2043 45.3 The Standard Phs C D The S | LnGrp Delay(d),s/veh | | | | 351.3 | | 79.9 | 34.1 | | | 44.8 | | | |
| pproach Delay, s/veh 107.7 97.0 29.5 45.3 pproach LOS F F C D Timer - Assigned Phs 2 4 6 8 Phs Duration (G+Y+Rc), s 70.5 29.5 70.5 29.5 Phange Period (Y+Rc), s 5.4 5.4 5.4 5.4 Max Green Setting (Gmax), s 62.6 26.6 62.6 26.6 Max Q Clear Time (g_c+I1), s 67.1 22.2 67.1 22.8 Pereen Ext Time (p_c), s 0.0 1.7 0.0 1.3 Phtersection Summary ICM 6th Ctrl Delay 87.0 | LnGrp LOS | D | | F | F | F | F | С | С | С | D | D | D | |
| F | Approach Vol, veh/h | | 2043 | | | | | | | | | 657 | | |
| Timer - Assigned Phs 2 4 6 8 Phs Duration (G+Y+Rc), s 70.5 29.5 70.5 29.5 Change Period (Y+Rc), s 5.4 5.4 5.4 Max Green Setting (Gmax), s 62.6 26.6 62.6 26.6 Max Q Clear Time (g_c+l1), s 67.1 22.2 67.1 22.8 Green Ext Time (p_c), s 0.0 1.7 0.0 1.3 Intersection Summary ICM 6th Ctrl Delay 87.0 | Approach Delay, s/veh | | 107.7 | | | 97.0 | | | | | | 45.3 | | |
| Phs Duration (G+Y+Rc), s 70.5 29.5 70.5 29.5 Change Period (Y+Rc), s 5.4 5.4 5.4 Max Green Setting (Gmax), s 62.6 26.6 62.6 26.6 Max Q Clear Time (g_c+I1), s 67.1 22.2 67.1 22.8 Green Ext Time (p_c), s 0.0 1.7 0.0 1.3 Intersection Summary MCM 6th Ctrl Delay 87.0 | Approach LOS | | F | | | F | | | С | | | D | | |
| Phs Duration (G+Y+Rc), s 70.5 29.5 70.5 29.5 Change Period (Y+Rc), s 5.4 5.4 5.4 Max Green Setting (Gmax), s 62.6 26.6 62.6 26.6 Max Q Clear Time (g_c+I1), s 67.1 22.2 67.1 22.8 Green Ext Time (p_c), s 0.0 1.7 0.0 1.3 Intersection Summary 87.0 | Timer - Assigned Phs | | 2 | | 4 | | 6 | | 8 | | | | | |
| Change Period (Y+Rc), s 5.4 5.4 5.4 5.4 Max Green Setting (Gmax), s 62.6 26.6 62.6 26.6 Max Q Clear Time (g_c+l1), s 67.1 22.2 67.1 22.8 Green Ext Time (p_c), s 0.0 1.7 0.0 1.3 Intersection Summary ICM 6th Ctrl Delay 87.0 | | , S | 70.5 | | 29.5 | | 70.5 | | 29.5 | | | | | |
| Max Green Setting (Gmax), s 62.6 26.6 62.6 26.6 Max Q Clear Time (g_c+I1), s 67.1 22.2 67.1 22.8 Green Ext Time (p_c), s 0.0 1.7 0.0 1.3 Intersection Summary ICM 6th Ctrl Delay 87.0 | | | | | | | | | | | | | | |
| Max Q Clear Time (g_c+l1), s 67.1 22.2 67.1 22.8 Green Ext Time (p_c), s 0.0 1.7 0.0 1.3 Intersection Summary ICM 6th Ctrl Delay 87.0 | , , | | | | | | | | | | | | | |
| Green Ext Time (p_c), s 0.0 1.7 0.0 1.3 Intersection Summary ICM 6th Ctrl Delay 87.0 | | | | | | | | | | | | | | |
| ntersection Summary ICM 6th Ctrl Delay 87.0 | Green Ext Time (p_c), s | , . | | | | | | | | | | | | |
| ICM 6th Ctrl Delay 87.0 | Intersection Summary | | | | | | | | | | | | | |
| • | | | | 87.0 | | | | | | | | | | |
| | HCM 6th LOS | | | F | | | | | | | | | | |

| | ٠ | → | • | • | ← | • | • | † | / | / | ļ | 4 |
|-----------------------------------|-------|------------|--------|-------|------------|----------|---------|------------|----------|----------|------------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | ∱ } | | | €Î}• | | * | ∱ } | | ሻ | ↑ ↑ | |
| Traffic Volume (vph) | 0 | 720 | 50 | 140 | 1420 | 30 | 20 | 100 | 40 | 40 | 360 | 60 |
| Future Volume (vph) | 0 | 720 | 50 | 140 | 1420 | 30 | 20 | 100 | 40 | 40 | 360 | 60 |
| Ideal Flow (vphpl) | 1700 | 1700 | 1700 | 1400 | 1400 | 1400 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 |
| Total Lost time (s) | | 5.1 | | | 5.1 | | 4.5 | 4.5 | | 4.5 | 4.5 | |
| Lane Util. Factor | | 0.95 | | | 0.95 | | 1.00 | 0.95 | | 1.00 | 0.95 | |
| Frpb, ped/bikes | | 1.00 | | | 1.00 | | 1.00 | 0.98 | | 1.00 | 0.99 | |
| Flpb, ped/bikes | | 1.00 | | | 1.00 | | 0.99 | 1.00 | | 0.96 | 1.00 | |
| Frt | | 0.99 | | | 1.00 | | 1.00 | 0.96 | | 1.00 | 0.98 | |
| Flt Protected | | 1.00 | | | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | | 3094 | | | 2555 | | 1545 | 2747 | | 1513 | 3050 | |
| Flt Permitted | | 1.00 | | | 0.69 | | 0.35 | 1.00 | | 0.66 | 1.00 | |
| Satd. Flow (perm) | | 3094 | | | 1783 | | 567 | 2747 | | 1049 | 3050 | |
| Peak-hour factor, PHF | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Adj. Flow (vph) | 0 | 758 | 53 | 147 | 1495 | 32 | 21 | 105 | 42 | 42 | 379 | 63 |
| RTOR Reduction (vph) | 0 | 5 | 0 | 0 | 1 | 0 | 0 | 32 | 0 | 0 | 14 | 0 |
| Lane Group Flow (vph) | 0 | 806 | 0 | 0 | 1673 | 0 | 21 | 115 | 0 | 42 | 428 | 0 |
| Confl. Peds. (#/hr) | 100 | | 29 | 29 | | 100 | 24 | | 33 | 33 | | 24 |
| Confl. Bikes (#/hr) | | | 3 | | | 2 | | | 1 | | | 1 |
| Heavy Vehicles (%) | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% |
| Parking (#/hr) | | | | | | | | 8 | 8 | | | |
| Turn Type | | NA | | pm+pt | NA | | Perm | NA | | Perm | NA | |
| Protected Phases | | 2 | | 1 | 6 | | | 8 | | | 4 | |
| Permitted Phases | | | | 6 | | | 8 | | | 4 | | |
| Actuated Green, G (s) | | 59.5 | | | 67.2 | | 23.2 | 23.2 | | 23.2 | 23.2 | |
| Effective Green, g (s) | | 59.5 | | | 67.2 | | 23.2 | 23.2 | | 23.2 | 23.2 | |
| Actuated g/C Ratio | | 0.60 | | | 0.67 | | 0.23 | 0.23 | | 0.23 | 0.23 | |
| Clearance Time (s) | | 5.1 | | | 5.1 | | 4.5 | 4.5 | | 4.5 | 4.5 | |
| Vehicle Extension (s) | | 5.0 | | | 5.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | | 1840 | | | 1232 | | 131 | 637 | | 243 | 707 | |
| v/s Ratio Prot | | 0.26 | | | c0.06 | | | 0.04 | | | c0.14 | |
| v/s Ratio Perm | | | | | c0.85 | | 0.04 | | | 0.04 | | |
| v/c Ratio | | 0.44 | | | 1.36 | | 0.16 | 0.18 | | 0.17 | 0.61 | |
| Uniform Delay, d1 | | 11.1 | | | 16.4 | | 30.6 | 30.8 | | 30.7 | 34.3 | |
| Progression Factor | | 1.00 | | | 0.49 | | 1.00 | 1.00 | | 0.43 | 0.39 | |
| Incremental Delay, d2 | | 8.0 | | | 163.4 | | 0.6 | 0.1 | | 0.2 | 0.9 | |
| Delay (s) | | 11.9 | | | 171.4 | | 31.2 | 30.9 | | 13.4 | 14.1 | |
| Level of Service | | В | | | F | | С | С | | В | В | |
| Approach Delay (s) | | 11.9 | | | 171.4 | | | 31.0 | | | 14.1 | |
| Approach LOS | | В | | | F | | | С | | | В | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 98.4 | Н | CM 2000 | Level of | Service | | F | | | |
| HCM 2000 Volume to Capacity | ratio | | 1.20 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 100.0 | S | um of lost | time (s) | | | 12.8 | | | |
| Intersection Capacity Utilization | n | | 123.7% | | CU Level | | ! | | Н | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

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|--|------|------------|---------------|------------|-------------|-------------|-----------|----------|------|------|-------------|-------------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | * | ↑ ↑ | | ሻ | † 1> | | | ^ | 7 | | ∱ } | |
| Traffic Volume (veh/h) | 80 | 640 | 80 | 140 | 1450 | 30 | 50 | 400 | 80 | 0 | 550 | 80 |
| Future Volume (veh/h) | 80 | 640 | 80 | 140 | 1450 | 30 | 50 | 400 | 80 | 0 | 550 | 80 |
| Initial Q (Qb), veh | 0 | 10 | 0 | 0 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | 10 | 0.95 | 0.99 | 10 | 0.96 | 0.99 | U | 0.91 | 1.00 | U | 0.91 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approac | | No | 1.00 | 1.00 | No | 1.00 | 1.00 | No | 1.00 | 1.00 | No | 1.00 |
| Adj Sat Flow, veh/h/ln | 1660 | 1660 | 1660 | 1367 | 1367 | 1367 | 1660 | 1660 | 1660 | 0 | 1660 | 1660 |
| Adj Flow Rate, veh/h | 84 | 674 | 75 | 147 | 1526 | 31 | 53 | 421 | 21 | 0 | 579 | 73 |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Percent Heavy Veh, % | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 0.55 | 3 | 3 |
| Cap, veh/h | 72 | 2212 | 241 | 72 | 2018 | 39 | 121 | 817 | 333 | 0 | 721 | 91 |
| Arrive On Green | 0.77 | 0.77 | 0.77 | 1.00 | 1.00 | 1.00 | 0.26 | 0.26 | 0.26 | 0.00 | 0.26 | 0.26 |
| Sat Flow, veh/h | 327 | 2847 | 316 | 578 | 2601 | 53 | 763 | 3154 | 1285 | 0.00 | 2868 | 350 |
| | 84 | 373 | | | | | | 421 | 21 | 0 | | 325 |
| Grp Volume(v), veh/h Grp Sat Flow(s), veh/h/lr | | | 376 1586 | 147 578 | 761 1299 | 796 1355 | 53 763 | 1577 | 1285 | 0 | 327 1577 | 325 1558 |
| . , | | 1577 | | | | | | | | | | |
| Q Serve(g_s), s | 7.9 | 7.0 | 7.0 | 3.7 | 0.0 | 0.0 | 6.4 | 11.4 | 1.2 | 0.0 | 19.4 | 19.5 |
| Cycle Q Clear(g_c), s | 8.3 | 7.0 | 7.0 | 11.4 | 0.0 | 0.0 | 25.9 | 11.4 | 1.2 | 0.0 | 19.4 | 19.5 |
| Prop In Lane | 1.00 | 4000 | 0.20 | 1.00 | 4007 | 0.04 | 1.00 | 047 | 1.00 | 0.00 | 400 | 0.22 |
| Lane Grp Cap(c), veh/h | | 1222 | 1230 | 72 | 1007 | 1050 | 121 | 817 | 333 | 0 | 408 | 404 |
| V/C Ratio(X) | 1.16 | 0.31 | 0.31 | 2.04 | 0.76 | 0.76 | 0.44 | 0.52 | 0.06 | 0.00 | 0.80 | 0.81 |
| Avail Cap(c_a), veh/h | 324 | 1222 | 1229 | 476 | 1007 | 1050 | 121 | 817 | 333 | 0 | 408 | 404 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 2.00 | 2.00 | 2.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 0.40 | 0.40 | 0.40 | 0.91 | 0.91 | 0.91 | 0.00 | 0.09 | 0.09 |
| Uniform Delay (d), s/vel | | 3.5 | 3.5 | 38.7 | 0.0 | 0.0 | 47.1 | 31.7 | 27.9 | 0.0 | 34.6 | 34.7 |
| Incr Delay (d2), s/veh | | 0.6 | 0.6 | | 2.2 | 2.1 | 2.3 | 0.5 | 0.1 | 0.0 | 1.1 | 1.1 |
| Initial Q Delay(d3),s/veh | | 0.2 | 0.2 | 0.0 | 0.7 | 0.7 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),vel | | 2.5 | 2.5 | 11.5 | 8.0 | 0.8 | 1.4 | 4.4 | 0.4 | 0.0 | 7.5 | 7.5 |
| Unsig. Movement Delay | | | | | | | | | | | | |
| LnGrp Delay(d),s/veh | | 4.3 | 4.3 | 524.7 | 2.9 | 2.8 | 49.4 | 32.2 | 28.0 | 0.0 | 35.7 | 35.8 |
| LnGrp LOS | F | A | Α | F | A | A | D | С | С | Α | D | D |
| Approach Vol, veh/h | | 833 | | | 1704 | | | 495 | | | 652 | |
| Approach Delay, s/veh | | 24.8 | | | 47.9 | | | 33.9 | | | 35.8 | |
| Approach LOS | | С | | | D | | | С | | | D | |
| Timer - Assigned Phs | | 2 | | 4 | | 6 | | 8 | | | | |
| Phs Duration (G+Y+Rc) |) s | 83.0 | | 31.0 | | 83.0 | | 31.0 | | | | |
| Change Period (Y+Rc), | | 5.1 | | * 5.1 | | 5.1 | | 5.1 | | | | |
| Max Green Setting (Gm | | 64.3 | | * 26 | | 64.3 | | 25.5 | | | | |
| Max Q Clear Time (g_c | | 10.3 | | 27.9 | | 13.4 | | 21.5 | | | | |
| Green Ext Time (p_c), s | , . | 17.1 | | 0.0 | | 38.7 | | 1.5 | | | | |
| | • | 17.1 | | 0.0 | | 30.1 | | 1.0 | | | | |
| Intersection Summary | | | 00.5 | | | | | | | | | |
| HCM 6th Ctrl Delay | | | 38.6 | | | | | | | | | |
| HCM 6th LOS | | | D | | | | | | | | | |
| Notes | | | | | | | | | | | | |

^{*} HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

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|---------------------------|------|------------|---------------|-------|----------|------|------|------------|------|------|----------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | ↑ ↑ | | ሻ | ^ | 7 | ሻ | ↑ ↑ | | ሻ | ^ | 7 |
| Traffic Volume (veh/h) | 0 | 560 | 80 | 80 | 1430 | 120 | 30 | 80 | 40 | 220 | 290 | 90 |
| Future Volume (veh/h) | 0 | 560 | 80 | 80 | 1430 | 120 | 30 | 80 | 40 | 220 | 290 | 90 |
| Initial Q (Qb), veh | 0 | 10 | 0 | 0 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | | 0.97 | 0.99 | | 0.97 | 0.95 | | 0.92 | 0.94 | • | 0.94 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approacl | | No | | | No | | | No | | | No | |
| Adj Sat Flow, veh/h/ln | 0 | 1660 | 1660 | 1367 | 1367 | 1367 | 1660 | 1660 | 1660 | 1660 | 1660 | 1660 |
| Adj Flow Rate, veh/h | 0 | 566 | 72 | 81 | 1444 | 95 | 30 | 81 | 40 | 222 | 293 | 75 |
| Peak Hour Factor | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 |
| Percent Heavy Veh, % | 0 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 |
| Cap, veh/h | 0 | 1628 | 200 | 72 | 1501 | 647 | 287 | 463 | 207 | 407 | 1022 | 430 |
| Arrive On Green | 0.00 | 1.00 | 1.00 | 0.58 | 0.58 | 0.58 | 0.23 | 0.23 | 0.23 | 0.07 | 0.32 | 0.32 |
| Sat Flow, veh/h | 0 | 2888 | 356 | 641 | 2598 | 1120 | 957 | 2055 | 921 | 1581 | 3154 | 1328 |
| Grp Volume(v), veh/h | 0 | 318 | 320 | 81 | 1444 | 95 | 30 | 60 | 61 | 222 | 293 | 75 |
| Grp Sat Flow(s), veh/h/ln | | 1577 | 1583 | 641 | 1299 | 1120 | 957 | 1577 | 1398 | 1581 | 1577 | 1328 |
| Q Serve(g_s), s | 0.0 | 0.0 | 0.0 | 6.1 | 52.8 | 3.9 | 2.5 | 3.1 | 3.5 | 6.9 | 6.9 | 4.0 |
| Cycle Q Clear(g_c), s | 0.0 | 0.0 | 0.0 | 6.1 | 52.8 | 3.9 | 2.5 | 3.1 | 3.5 | 6.9 | 6.9 | 4.0 |
| Prop In Lane | 0.00 | 0.0 | 0.22 | 1.00 | 02.0 | 1.00 | 1.00 | • | 0.66 | 1.00 | 0.0 | 1.00 |
| Lane Grp Cap(c), veh/h | | 912 | 916 | 72 | 1501 | 647 | 287 | 355 | 315 | 407 | 1022 | 430 |
| V/C Ratio(X) | 0.00 | 0.35 | 0.35 | 1.12 | 0.96 | 0.15 | 0.10 | 0.17 | 0.19 | 0.55 | 0.29 | 0.17 |
| Avail Cap(c_a), veh/h | 0 | 912 | 915 | 442 | 1501 | 647 | 340 | 442 | 392 | 407 | 1196 | 503 |
| HCM Platoon Ratio | 1.00 | 2.00 | 2.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 0.00 | 0.94 | 0.94 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | | 0.0 | 0.0 | 50.0 | 20.8 | 9.7 | 31.0 | 31.2 | 31.4 | 29.6 | 25.2 | 24.2 |
| Incr Delay (d2), s/veh | 0.0 | 1.0 | 1.0 | 144.1 | 15.8 | 0.5 | 0.2 | 0.2 | 0.3 | 0.9 | 0.2 | 0.2 |
| Initial Q Delay(d3),s/veh | | 0.3 | 0.3 | 0.0 | 8.4 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh | | 0.3 | 0.3 | 4.7 | 20.8 | 1.0 | 0.6 | 1.2 | 1.2 | 1.8 | 2.6 | 1.3 |
| Unsig. Movement Delay | | | | | | | | | | | | |
| LnGrp Delay(d),s/veh | 0.0 | 1.3 | 1.3 | 194.1 | 44.9 | 10.2 | 31.2 | 31.4 | 31.7 | 30.4 | 25.3 | 24.4 |
| LnGrp LOS | Α | A | A | F | D | В | С | С | С | С | С | С |
| Approach Vol, veh/h | | 638 | | | 1620 | | | 151 | | | 590 | |
| Approach Delay, s/veh | | 1.3 | | | 50.3 | | | 31.5 | | | 27.1 | |
| Approach LOS | | Α | | | D | | | С | | | С | |
| •• | | | | 4 | | ^ | 7 | | | | | |
| Timer - Assigned Phs | | 2 | | 4 | | 6 | 7 | 8 | | | | |
| Phs Duration (G+Y+Rc) | | 62.9 | | 37.1 | | 62.9 | 9.9 | 27.2 | | | | |
| Change Period (Y+Rc), | | 5.1 | | * 4.7 | | 5.1 | 3.0 | * 4.7 | | | | |
| Max Green Setting (Gm | | 52.3 | | * 38 | | 52.3 | 6.9 | * 28 | | | | |
| Max Q Clear Time (g_c+ | , . | 2.0 | | 8.9 | | 54.8 | 8.9 | 5.5 | | | | |
| Green Ext Time (p_c), s | | 10.0 | | 2.4 | | 0.0 | 0.0 | 0.8 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 6th Ctrl Delay | | | 34.4 | | | | | | | | | |
| HCM 6th LOS | | | С | | | | | | | | | |
| Notes | | | | | | | | | | | | |

^{*} HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

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|---------------------------|------|----------|---------------|------|------|-------|------|----------|------|------|------------|------|--|
| Movement El | BL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR | |
| Lane Configurations | | | | | 474 | | * | ^ | | | ∱ } | | |
| Traffic Volume (veh/h) | 0 | 0 | 0 | 70 | 350 | 70 | 100 | 520 | 0 | 0 | 590 | 150 | |
| uture Volume (veh/h) | 0 | 0 | 0 | 70 | 350 | 70 | 100 | 520 | 0 | 0 | 590 | 150 | |
| nitial Q (Qb), veh | | | | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Ped-Bike Adj(A_pbT) | | | | 1.00 | | 0.91 | 0.99 | | 1.00 | 1.00 | | 0.96 | |
| Parking Bus, Adj | | | | 0.85 | 1.00 | 0.85 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.81 | |
| Nork Zone On Approach | | | | | No | | | No | | | No | | |
| Adj Sat Flow, veh/h/ln | | | | 1660 | 1660 | 1660 | 1660 | 1660 | 0 | 0 | 1660 | 1660 | |
| Adj Flow Rate, veh/h | | | | 75 | 376 | 52 | 108 | 559 | 0 | 0 | 634 | 126 | |
| Peak Hour Factor | | | | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | |
| Percent Heavy Veh, % | | | | 3 | 3 | 3 | 3 | 3 | 0 | 0 | 3 | 3 | |
| Cap, veh/h | | | | 124 | 646 | 93 | 381 | 1715 | 0 | 0 | 1278 | 253 | |
| Arrive On Green | | | | 0.32 | 0.32 | 0.32 | 0.54 | 0.54 | 0.00 | 0.00 | 0.54 | 0.54 | |
| Sat Flow, veh/h | | | | 387 | 2023 | 292 | 696 | 3237 | 0.00 | 0.00 | 2434 | 466 | |
| Grp Volume(v), veh/h | | | | 268 | 0 | 235 | 108 | 559 | 0 | 0 | 425 | 335 | |
| Grp Sat Flow(s), veh/h/ln | | | | 1384 | 0 | 1318 | 696 | 1577 | 0 | 0 | 1577 | 1240 | |
| . , | | | | 9.8 | 0.0 | 8.9 | 6.9 | 5.9 | 0.0 | 0.0 | 10.1 | 10.1 | |
| Q Serve(g_s), s | | | | 9.8 | 0.0 | | | | | | | | |
| Cycle Q Clear(g_c), s | | | | | 0.0 | 8.9 | 17.0 | 5.9 | 0.0 | 0.0 | 10.1 | 10.1 | |
| Prop In Lane | | | | 0.28 | ٥ | 0.22 | 1.00 | 4745 | 0.00 | 0.00 | 050 | 0.38 | |
| ane Grp Cap(c), veh/h | | | | 442 | 0 | 421 | 381 | 1715 | 0 | 0 | 858 | 674 | |
| //C Ratio(X) | | | | 0.61 | 0.00 | 0.56 | 0.28 | 0.33 | 0.00 | 0.00 | 0.50 | 0.50 | |
| Avail Cap(c_a), veh/h | | | | 595 | 0 | 567 | 381 | 1715 | 0 | 0 | 858 | 674 | |
| HCM Platoon Ratio | | | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Jpstream Filter(I) | | | | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 0.00 | 0.00 | 0.49 | 0.49 | |
| Jniform Delay (d), s/veh | | | | 17.2 | 0.0 | 16.9 | 13.9 | 7.6 | 0.0 | 0.0 | 8.5 | 8.6 | |
| ncr Delay (d2), s/veh | | | | 1.3 | 0.0 | 1.2 | 1.9 | 0.5 | 0.0 | 0.0 | 1.0 | 1.3 | |
| nitial Q Delay(d3),s/veh | | | | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | |
| %ile BackOfQ(50%),veh/In | | | | 3.1 | 0.0 | 2.6 | 1.2 | 1.8 | 0.0 | 0.0 | 3.1 | 2.5 | |
| Jnsig. Movement Delay, s | /veh | | | | | | | | | | | | |
| _nGrp Delay(d),s/veh | | | | 18.6 | 0.0 | 18.1 | 15.7 | 8.1 | 0.0 | 0.0 | 9.5 | 9.8 | |
| ∟nGrp LOS | | | | В | Α | В | В | Α | Α | Α | Α | Α | |
| Approach Vol, veh/h | | | | | 503 | | | 667 | | | 760 | | |
| Approach Delay, s/veh | | | | | 18.3 | | | 9.3 | | | 9.7 | | |
| Approach LOS | | | | | В | | | Α | | | Α | | |
| imer - Assigned Phs | | 2 | | | | 6 | | 8 | | | | | |
| Phs Duration (G+Y+Rc), s | | 36.8 | | | | 36.8 | | 23.2 | | | | | |
| Change Period (Y+Rc), s | | * 4.2 | | | | * 4.2 | | 4.0 | | | | | |
| Max Green Setting (Gmax) | | * 26 | | | | * 26 | | 25.8 | | | | | |
| Max Q Clear Time (g_c+l1 | | 19.0 | | | | 12.1 | | 11.8 | | | | | |
| Green Ext Time (p_c), s | ,, J | 3.8 | | | | 7.0 | | 2.7 | | | | | |
| ntersection Summary | | | | | | | | | | | | | |
| HCM 6th Ctrl Delay | | | 11.8 | | | | | | | | | | |
| HCM 6th LOS | | | | | | | | | | | | | |
| | | | В | | | | | | | | | | |
| Notes | | | | | | | | | | | | | |

^{*} HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

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|-----------------------------------|-------|----------|-------|------|------------|------------|----------|----------|-------------|------|------------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | | | | 414 | | Ť | ^ | | | ∱ Ъ | |
| Traffic Volume (vph) | 0 | 0 | 0 | 50 | 350 | 40 | 30 | 90 | 0 | 10 | 250 | 190 |
| Future Volume (vph) | 0 | 0 | 0 | 50 | 350 | 40 | 30 | 90 | 0 | 10 | 250 | 190 |
| Ideal Flow (vphpl) | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 |
| Total Lost time (s) | | | | | 3.0 | | 4.0 | 4.0 | | | 4.0 | |
| Lane Util. Factor | | | | | 0.95 | | 1.00 | 0.95 | | | 0.95 | |
| Frpb, ped/bikes | | | | | 1.00 | | 1.00 | 1.00 | | | 0.99 | |
| Flpb, ped/bikes | | | | | 1.00 | | 1.00 | 1.00 | | | 1.00 | |
| Frt | | | | | 0.99 | | 1.00 | 1.00 | | | 0.94 | |
| Flt Protected | | | | | 0.99 | | 0.95 | 1.00 | | | 1.00 | |
| Satd. Flow (prot) | | | | | 2873 | | 1568 | 2885 | | | 2692 | |
| Flt Permitted | | | | | 0.99 | | 0.25 | 1.00 | | | 0.95 | |
| Satd. Flow (perm) | | | | | 2873 | | 413 | 2885 | | | 2556 | |
| Peak-hour factor, PHF | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 |
| Adj. Flow (vph) | 0 | 0 | 0 | 71 | 500 | 57 | 43 | 129 | 0 | 14 | 357 | 271 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 10 | 0 | 0 | 0 | 0 | 0 | 188 | 0 |
| Lane Group Flow (vph) | 0 | 0 | 0 | 0 | 618 | 0 | 43 | 129 | 0 | 0 | 454 | 0 |
| Confl. Bikes (#/hr) | | | 1 | | | 1 | | | 1 | | | 1 |
| Heavy Vehicles (%) | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% |
| Parking (#/hr) | | | | 6 | 6 | 4 | | 12 | | | 11 | 11 |
| Turn Type | | | | Perm | NA | | Perm | NA | | Perm | NA | |
| Protected Phases | | | | | 6 | | | 8 | | | 4 | |
| Permitted Phases | | | | 6 | | | 8 | | | 4 | | |
| Actuated Green, G (s) | | | | | 23.0 | | 16.0 | 16.0 | | | 16.0 | |
| Effective Green, g (s) | | | | | 23.0 | | 16.0 | 16.0 | | | 16.0 | |
| Actuated g/C Ratio | | | | | 0.33 | | 0.23 | 0.23 | | | 0.23 | |
| Clearance Time (s) | | | | | 3.0 | | 4.0 | 4.0 | | | 4.0 | |
| Vehicle Extension (s) | | | | | 2.0 | | 2.0 | 2.0 | | | 2.0 | |
| Lane Grp Cap (vph) | | | | | 943 | | 94 | 659 | | | 584 | |
| v/s Ratio Prot | | | | | | | <u> </u> | 0.04 | | | | |
| v/s Ratio Perm | | | | | 0.22 | | 0.10 | 0.0 | | | c0.18 | |
| v/c Ratio | | | | | 0.66 | | 0.46 | 0.20 | | | 0.78 | |
| Uniform Delay, d1 | | | | | 20.1 | | 23.3 | 21.8 | | | 25.3 | |
| Progression Factor | | | | | 1.00 | | 1.00 | 1.00 | | | 1.00 | |
| Incremental Delay, d2 | | | | | 3.5 | | 15.2 | 0.7 | | | 9.8 | |
| Delay (s) | | | | | 23.7 | | 38.5 | 22.5 | | | 35.1 | |
| Level of Service | | | | | C | | D | C | | | D | |
| Approach Delay (s) | | 0.0 | | | 23.7 | | | 26.5 | | | 35.1 | |
| Approach LOS | | A | | | C | | | C | | | D | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 29.1 | Н | CM 2000 | Level of | Service | | С | | | |
| HCM 2000 Volume to Capacity | ratio | | 0.47 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 70.0 | S | um of lost | t time (s) | | | 11.0 | | | |
| Intersection Capacity Utilization |) | | 47.1% | | | of Service | <u> </u> | | Α | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

| Interception | | | | | | | | | | | | |
|--------------------------|-----|------|-------|--------|-------|------|------|-------|------|---------|------------|------|
| Intersection | 2.6 | | | | | | | | | | | |
| Int Delay, s/veh | ∠.0 | | | | | | | | | | | |
| Movement E | BL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | | | | 41 | | | | | | ∱ ∱ | |
| Traffic Vol, veh/h | 0 | 0 | 0 | 0 | 330 | 0 | 0 | 0 | 0 | 0 | 0 | 110 |
| Future Vol, veh/h | 0 | 0 | 0 | 0 | 330 | 0 | 0 | 0 | 0 | 0 | 0 | 110 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 79 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control F | ree | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | - | - | - | - | - | - | - | - | - | - |
| Veh in Median Storage, # | - | 2 | - | - | 0 | - | - | 16974 | - | - | 0 | - |
| Grade, % | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 82 | 82 | 82 | 82 | 82 | 82 | 82 | 82 | 82 | 82 | 82 | 82 |
| Heavy Vehicles, % | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 |
| Mvmt Flow | 0 | 0 | 0 | 0 | 402 | 0 | 0 | 0 | 0 | 0 | 0 | 134 |
| | | | | | | | | | | | | |
| Major/Minor | | | ı | Major2 | | | | | N | /linor2 | | |
| Conflicting Flow All | | | | 79 | 0 | 0 | | | | - | 481 | 201 |
| Stage 1 | | | | - | - | - | | | | _ | 402 | - |
| Stage 2 | | | | _ | _ | _ | | | | _ | 79 | _ |
| Critical Hdwy | | | | 4.16 | _ | _ | | | | _ | 6.56 | 6.96 |
| Critical Hdwy Stg 1 | | | | - - | _ | _ | | | | _ | 5.56 | - |
| Critical Hdwy Stg 2 | | | | _ | _ | _ | | | | - | - | _ |
| Follow-up Hdwy | | | | 2.23 | - | - | | | | - | 4.03 | 3.33 |
| Pot Cap-1 Maneuver | | | | 1510 | - | 0 | | | | 0 | 481 | 803 |
| Stage 1 | | | | - | _ | 0 | | | | 0 | 596 | - |
| Stage 2 | | | | - | _ | 0 | | | | 0 | - | - |
| Platoon blocked, % | | | | | _ | | | | | | | |
| Mov Cap-1 Maneuver | | | | 1510 | - | - | | | | - | 0 | 803 |
| Mov Cap-2 Maneuver | | | | - | - | - | | | | - | 0 | - |
| Stage 1 | | | | - | - | - | | | | - | 0 | - |
| Stage 2 | | | | - | - | - | | | | - | 0 | - |
| | | | | | | | | | | | | |
| Approach | | | | WB | | | | | | SB | | |
| HCM Control Delay, s | | | | 0 | | | | | | 10.4 | | |
| HCM LOS | | | | - 0 | | | | | | В | | |
| TIOWI LOO | | | | | | | | | | U | | |
| Minor Lane/Major Mvmt | | WBL | WBT S | SBLn1 | SBLn2 | | | | | | | |
| Capacity (veh/h) | | 1510 | | - | 803 | | | | | | | |
| HCM Lane V/C Ratio | | - | _ | | 0.167 | | | | | | | |
| HCM Control Delay (s) | | 0 | _ | 0 | 10.4 | | | | | | | |
| HCM Lane LOS | | A | _ | A | В | | | | | | | |
| HCM 95th %tile Q(veh) | | 0 | _ | - | 0.6 | | | | | | | |
| 110111 00th 70th Q(1011) | | , | | | 0.0 | | | | | | | |

| Intersection | | | | | | |
|------------------------|-------|-------|---------|----------|--------|------|
| Int Delay, s/veh | 0.2 | | | | | |
| | | | | | | |
| | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | ተኈ | | ሻ | ^ | | 7 |
| Traffic Vol, veh/h | 710 | 62 | 48 | 1580 | 0 | 0 |
| Future Vol, veh/h | 710 | 62 | 48 | 1580 | 0 | 0 |
| Conflicting Peds, #/hr | 0 | 31 | 31 | 0 | 0 | 0 |
| <u> </u> | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | 25 | - | - | 0 |
| Veh in Median Storage, | # 0 | - | - | 0 | 0 | - |
| Grade, % | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 94 | 94 | 94 | 94 | 94 | 94 |
| Heavy Vehicles, % | 3 | 3 | 3 | 3 | 3 | 3 |
| Mvmt Flow | 755 | 66 | 51 | 1681 | 0 | 0 |
| mining i ion | | 00 | • | 1001 | • | |
| | | | | | | |
| Major/Minor Ma | ajor1 | N | /lajor2 | 1 | Minor1 | |
| Conflicting Flow All | 0 | 0 | 852 | 0 | - | 442 |
| Stage 1 | - | - | - | - | - | - |
| Stage 2 | - | - | - | - | - | - |
| Critical Hdwy | - | - | 4.16 | - | - | 6.96 |
| Critical Hdwy Stg 1 | _ | _ | - | _ | _ | - |
| Critical Hdwy Stg 2 | _ | _ | _ | _ | _ | _ |
| Follow-up Hdwy | _ | _ | 2.23 | _ | - | 3.33 |
| Pot Cap-1 Maneuver | _ | _ | 776 | _ | 0 | 560 |
| Stage 1 | _ | _ | - | _ | 0 | - |
| Stage 2 | _ | _ | _ | _ | 0 | _ |
| Platoon blocked, % | _ | _ | | _ | U | |
| Mov Cap-1 Maneuver | _ | _ | 753 | | _ | 543 |
| | | | | - | | |
| Mov Cap-2 Maneuver | - | - | - | - | - | - |
| Stage 1 | - | - | - | - | - | - |
| Stage 2 | - | - | - | - | - | - |
| | | | | | | |
| Approach | EB | | WB | | NB | |
| HCM Control Delay, s | 0 | | 0.3 | | 0 | |
| HCM LOS | U | | 0.5 | | A | |
| TICIVI LOG | | | | | | |
| | | | | | | |
| Minor Lane/Major Mvmt | 1 | NBLn1 | EBT | EBR | WBL | WBT |
| Capacity (veh/h) | | - | - | - | 753 | _ |
| HCM Lane V/C Ratio | | _ | _ | _ | 0.068 | - |
| HCM Control Delay (s) | | 0 | _ | _ | 10.1 | _ |
| HCM Lane LOS | | A | - | _ | В | _ |
| HCM 95th %tile Q(veh) | | - | _ | _ | 0.2 | _ |
| HOW JOHN JOHN Q(VOII) | | _ | | | U.Z | _ |

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|------------------------------|------|------------|-------|-------|------------|------|------|------|----------|-------------|----------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | ∱ ∱ | | 7 | ∱ ∱ | | | ħβ | | * | ^ | 7 |
| Traffic Volume (veh/h) | 40 | 1840 | 50 | 80 | 1690 | 60 | 0 | 240 | 60 | 40 | 170 | 50 |
| Future Volume (veh/h) | 40 | 1840 | 50 | 80 | 1690 | 60 | 0 | 240 | 60 | 40 | 170 | 50 |
| Initial Q (Qb), veh | 0 | 15 | 0 | 0 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | | 0.97 | 1.00 | | 0.97 | 1.00 | | 0.97 | 0.99 | | 0.89 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach | | No | | | No | | | No | | | No | |
| Adj Sat Flow, veh/h/ln | 1367 | 1367 | 1367 | 1367 | 1367 | 1367 | 0 | 1660 | 1660 | 1660 | 1660 | 1660 |
| Adj Flow Rate, veh/h | 44 | 2044 | 54 | 89 | 1878 | 64 | 0 | 267 | 58 | 44 | 189 | 37 |
| Peak Hour Factor | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Percent Heavy Veh, % | 3 | 3 | 3 | 3 | 3 | 3 | 0 | 3 | 3 | 3 | 3 | 3 |
| Cap, veh/h | 72 | 1747 | 26 | 72 | 1742 | 31 | 0 | 601 | 128 | 220 | 737 | 294 |
| Arrive On Green | 0.67 | 0.67 | 0.67 | 0.67 | 0.67 | 0.67 | 0.00 | 0.23 | 0.23 | 0.23 | 0.23 | 0.23 |
| Sat Flow, veh/h | 186 | 2584 | 68 | 160 | 2561 | 87 | 0 | 2656 | 548 | 1032 | 3154 | 1257 |
| Grp Volume(v), veh/h | 44 | 1022 | 1076 | 89 | 946 | 996 | 0 | 162 | 163 | 44 | 189 | 37 |
| Grp Sat Flow(s),veh/h/ln | 186 | 1299 | 1353 | 160 | 1299 | 1349 | 0 | 1577 | 1544 | 1032 | 1577 | 1257 |
| Q Serve(g_s), s | 0.0 | 66.7 | 66.7 | 0.0 | 66.7 | 66.7 | 0.0 | 8.8 | 9.1 | 3.8 | 4.9 | 2.3 |
| Cycle Q Clear(g_c), s | 66.7 | 66.7 | 66.7 | 66.7 | 66.7 | 66.7 | 0.0 | 8.8 | 9.1 | 12.9 | 4.9 | 2.3 |
| Prop In Lane | 1.00 | | 0.05 | 1.00 | | 0.06 | 0.00 | | 0.36 | 1.00 | | 1.00 |
| Lane Grp Cap(c), veh/h | 72 | 867 | 907 | 72 | 867 | 906 | 0 | 369 | 361 | 220 | 737 | 294 |
| V/C Ratio(X) | 0.61 | 1.18 | 1.19 | 1.24 | 1.09 | 1.10 | 0.00 | 0.44 | 0.45 | 0.20 | 0.26 | 0.13 |
| Avail Cap(c_a), veh/h | 72 | 867 | 903 | 72 | 867 | 900 | 0 | 420 | 411 | 253 | 839 | 334 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 0.09 | 0.09 | 0.09 | 0.00 | 0.80 | 0.80 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 50.0 | 16.6 | 16.6 | 50.0 | 16.6 | 16.6 | 0.0 | 32.7 | 32.8 | 38.4 | 31.2 | 30.3 |
| Incr Delay (d2), s/veh | 33.0 | 92.6 | 95.1 | 117.0 | 43.3 | 46.6 | 0.0 | 0.7 | 0.7 | 0.4 | 0.2 | 0.2 |
| Initial Q Delay(d3),s/veh | 0.0 | 31.2 | 29.8 | 0.0 | 20.8 | 19.9 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/ln | 1.7 | 45.8 | 48.2 | 4.1 | 31.4 | 33.4 | 0.0 | 3.4 | 3.5 | 1.0 | 1.9 | 0.7 |
| Unsig. Movement Delay, s/veh | | | | | | | | | | | | |
| LnGrp Delay(d),s/veh | 83.0 | 140.4 | 141.5 | 167.0 | 80.8 | 83.2 | 0.0 | 33.4 | 33.5 | 38.8 | 31.4 | 30.4 |
| LnGrp LOS | F | F | F | F | F | F | Α | С | С | D | С | С |
| Approach Vol, veh/h | | 2142 | | | 2031 | | | 325 | | | 270 | |
| Approach Delay, s/veh | | 139.7 | | | 85.7 | | | 33.5 | | | 32.5 | |
| Approach LOS | | F | | | F | | | С | | | С | |
| Timer - Assigned Phs | | 2 | | 4 | | 6 | | 8 | | | | |
| Phs Duration (G+Y+Rc), s | | 72.1 | | 27.9 | | 72.1 | | 27.9 | | | | |
| Change Period (Y+Rc), s | | 5.4 | | 4.5 | | 5.4 | | 4.5 | | | | |
| Max Green Setting (Gmax), s | | 63.5 | | 26.6 | | 63.5 | | 26.6 | | | | |
| Max Q Clear Time (g_c+l1), s | | 68.7 | | 14.9 | | 68.7 | | 11.1 | | | | |
| Green Ext Time (p_c), s | | 0.0 | | 1.2 | | 0.0 | | 1.7 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 6th Ctrl Delay | | | 103.4 | | | | | | | | | |
| HCM 6th LOS | | | F | | | | | | | | | |

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|--------------------------|------|----------|-------|-------|------------|-------|------|-------------|-------------|------|-----------|------|--|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR | |
| Lane Configurations | ሻ | ħβ | | * | ተ ኈ | | ሻ | ∱ } | | ሻ | ħβ | | |
| Traffic Volume (veh/h) | 50 | 1680 | 40 | 90 | 1660 | 50 | 70 | 440 | 170 | 40 | 370 | 70 | |
| Future Volume (veh/h) | 50 | 1680 | 40 | 90 | 1660 | 50 | 70 | 440 | 170 | 40 | 370 | 70 | |
| Initial Q (Qb), veh | 0 | 15 | 0 | 0 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Ped-Bike Adj(A_pbT) | 1.00 | | 0.97 | 1.00 | | 0.98 | 0.99 | | 0.97 | 0.99 | | 0.97 | |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Work Zone On Approac | h | No | | | No | | | No | | | No | | |
| Adj Sat Flow, veh/h/ln | 1367 | 1367 | 1367 | 1367 | 1367 | 1367 | 1660 | 1660 | 1660 | 1660 | 1660 | 1660 | |
| Adj Flow Rate, veh/h | 56 | 1867 | 43 | 100 | 1844 | 54 | 78 | 489 | 176 | 44 | 411 | 65 | |
| Peak Hour Factor | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | |
| Percent Heavy Veh, % | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | |
| Cap, veh/h | 72 | 1654 | 20 | 72 | 1649 | 25 | 189 | 593 | 212 | 132 | 714 | 112 | |
| Arrive On Green | 0.63 | 0.63 | 0.63 | 0.63 | 0.63 | 0.63 | 0.52 | 0.52 | 0.52 | 0.26 | 0.26 | 0.26 | |
| Sat Flow, veh/h | 194 | 2594 | 59 | 192 | 2576 | 75 | 902 | 2258 | 807 | 761 | 2719 | 426 | |
| Grp Volume(v), veh/h | 56 | 931 | 979 | 100 | 925 | 973 | 78 | 341 | 324 | 44 | 237 | 239 | |
| Grp Sat Flow(s),veh/h/lr | | 1299 | 1354 | 192 | 1299 | 1352 | 902 | 1577 | 1487 | 761 | 1577 | 1569 | |
| Q Serve(g_s), s | 0.0 | 63.0 | 63.0 | 0.0 | 63.0 | 63.0 | 7.7 | 18.1 | 18.4 | 5.7 | 13.0 | 13.3 | |
| Cycle Q Clear(g_c), s | 63.0 | 63.0 | 63.0 | 63.0 | 63.0 | 63.0 | 21.0 | 18.1 | 18.4 | 24.0 | 13.0 | 13.3 | |
| Prop In Lane | 1.00 | | 0.04 | 1.00 | | 0.06 | 1.00 | | 0.54 | 1.00 | | 0.27 | |
| Lane Grp Cap(c), veh/h | 72 | 818 | 856 | 72 | 818 | 856 | 189 | 414 | 390 | 132 | 414 | 412 | |
| V/C Ratio(X) | 0.78 | 1.14 | 1.14 | 1.39 | 1.13 | 1.14 | 0.41 | 0.82 | 0.83 | 0.33 | 0.57 | 0.58 | |
| Avail Cap(c_a), veh/h | 72 | 818 | 853 | 72 | 818 | 851 | 192 | 420 | 396 | 134 | 420 | 417 | |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 2.00 | 2.00 | 2.00 | 1.00 | 1.00 | 1.00 | |
| Upstream Filter(I) | 0.09 | 0.09 | 0.09 | 1.00 | 1.00 | 1.00 | 0.62 | 0.62 | 0.62 | 1.00 | 1.00 | 1.00 | |
| Uniform Delay (d), s/veh | | 18.5 | 18.5 | 50.0 | 18.5 | 18.5 | 28.4 | 21.8 | 21.9 | 45.1 | 32.0 | 32.1 | |
| Incr Delay (d2), s/veh | 7.3 | 63.9 | 65.9 | 240.1 | 74.2 | 75.8 | 0.9 | 8.0 | 9.0 | 1.5 | 1.8 | 2.0 | |
| nitial Q Delay(d3),s/veh | | 33.0 | 31.5 | 0.0 | 22.0 | 21.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | |
| %ile BackOfQ(50%),veh | | 37.9 | 39.8 | 6.6 | 37.7 | 39.6 | 1.5 | 5.6 | 5.5 | 1.1 | 5.2 | 5.3 | |
| Unsig. Movement Delay | | | | | | | | J. . | | | | 3.0 | |
| LnGrp Delay(d),s/veh | 57.3 | 115.4 | 116.0 | 290.1 | 114.8 | 115.3 | 29.3 | 29.8 | 30.9 | 46.5 | 33.8 | 34.1 | |
| LnGrp LOS | E | F | F | F | F | F | C | C | C | D | C | С | |
| Approach Vol, veh/h | _ | 1966 | | • | 1998 | | | 743 | | _ | 520 | | |
| Approach Delay, s/veh | | 114.0 | | | 123.8 | | | 30.3 | | | 35.0 | | |
| Approach LOS | | F | | | 120.0 | | | C | | | 00.0 D | | |
| | | , | | | | | | | | | | | |
| Timer - Assigned Phs | | 2 | | 4 | | 6 | | 8 | | | | | |
| Phs Duration (G+Y+Rc) | | 68.4 | | 31.6 | | 68.4 | | 31.6 | | | | | |
| Change Period (Y+Rc), | | 5.4 | | 5.4 | | 5.4 | | 5.4 | | | | | |
| Max Green Setting (Gm | | 62.6 | | 26.6 | | 62.6 | | 26.6 | | | | | |
| Max Q Clear Time (g_c- | , . | | | 26.0 | | 65.0 | | 23.0 | | | | | |
| Green Ext Time (p_c), s | | 0.0 | | 0.2 | | 0.0 | | 1.6 | | | | | |
| Intersection Summary | | | | | | | | | | | | | |
| HCM 6th Ctrl Delay | | | 98.0 | | | | | | | | | | |
| HCM 6th LOS | | | F | | | | | | | | | | |

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|----------------------------------|-----------|------------|--------|-------|------------|------------|---------|------------|----------|----------|-------------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | ∱ ∱ | | | 413- | | ሻ | ↑ ↑ | | ሻ | † 1> | |
| Traffic Volume (vph) | 0 | 1420 | 100 | 100 | 830 | 50 | 50 | 250 | 90 | 50 | 200 | 60 |
| Future Volume (vph) | 0 | 1420 | 100 | 100 | 830 | 50 | 50 | 250 | 90 | 50 | 200 | 60 |
| Ideal Flow (vphpl) | 1400 | 1400 | 1400 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 |
| Total Lost time (s) | | 5.1 | | | 5.1 | | 4.5 | 4.5 | | 4.5 | 4.5 | |
| Lane Util. Factor | | 0.95 | | | 0.95 | | 1.00 | 0.95 | | 1.00 | 0.95 | |
| Frpb, ped/bikes | | 0.98 | | | 0.98 | | 1.00 | 0.92 | | 1.00 | 0.93 | |
| Flpb, ped/bikes | | 1.00 | | | 1.00 | | 0.80 | 1.00 | | 0.85 | 1.00 | |
| Frt | | 0.99 | | | 0.99 | | 1.00 | 0.96 | | 1.00 | 0.97 | |
| Flt Protected | | 1.00 | | | 0.99 | | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | | 2514 | | | 3038 | | 1248 | 2587 | | 1327 | 2805 | |
| Flt Permitted | | 1.00 | | | 0.55 | | 0.53 | 1.00 | | 0.43 | 1.00 | |
| Satd. Flow (perm) | | 2514 | | | 1664 | | 694 | 2587 | | 606 | 2805 | |
| Peak-hour factor, PHF | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Adj. Flow (vph) | 0 | 1495 | 105 | 105 | 874 | 53 | 53 | 263 | 95 | 53 | 211 | 63 |
| RTOR Reduction (vph) | 0 | 5 | 0 | 0 | 4 | 0 | 0 | 37 | 0 | 0 | 26 | 0 |
| Lane Group Flow (vph) | 0 | 1595 | 0 | 0 | 1028 | 0 | 53 | 321 | 0 | 53 | 248 | 0 |
| Confl. Peds. (#/hr) | 423 | | 174 | 174 | | 423 | 282 | | 215 | 215 | | 282 |
| Confl. Bikes (#/hr) | | | 6 | | | 1 | | | 1 | | | 1 |
| Heavy Vehicles (%) | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% |
| Parking (#/hr) | | | | | | | | 8 | 8 | | | |
| Turn Type | | NA | | pm+pt | NA | | Perm | NA | | Perm | NA | |
| Protected Phases | | 2 | | 1 | 6 | | | 8 | | | 4 | |
| Permitted Phases | | | | 6 | | | 8 | | | 4 | | |
| Actuated Green, G (s) | | 59.5 | | | 67.2 | | 23.2 | 23.2 | | 23.2 | 23.2 | |
| Effective Green, g (s) | | 59.5 | | | 67.2 | | 23.2 | 23.2 | | 23.2 | 23.2 | |
| Actuated g/C Ratio | | 0.60 | | | 0.67 | | 0.23 | 0.23 | | 0.23 | 0.23 | |
| Clearance Time (s) | | 5.1 | | | 5.1 | | 4.5 | 4.5 | | 4.5 | 4.5 | |
| Vehicle Extension (s) | | 5.0 | | | 5.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | | 1495 | | | 1180 | | 161 | 600 | | 140 | 650 | |
| v/s Ratio Prot | | c0.63 | | | c0.04 | | | c0.12 | | | 0.09 | |
| v/s Ratio Perm | | | | | 0.55 | | 0.08 | | | 0.09 | | |
| v/c Ratio | | 1.07 | | | 0.87 | | 0.33 | 0.54 | | 0.38 | 0.38 | |
| Uniform Delay, d1 | | 20.2 | | | 13.0 | | 31.9 | 33.7 | | 32.3 | 32.4 | |
| Progression Factor | | 1.00 | | | 0.96 | | 1.00 | 1.00 | | 0.58 | 0.52 | |
| Incremental Delay, d2 | | 43.4 | | | 6.3 | | 1.2 | 0.9 | | 1.0 | 0.2 | |
| Delay (s) | | 63.7 | | | 18.8 | | 33.1 | 34.6 | | 19.9 | 16.9 | |
| Level of Service | | Е | | | В | | С | С | | В | В | |
| Approach Delay (s) | | 63.7 | | | 18.8 | | | 34.4 | | | 17.4 | |
| Approach LOS | | E | | | В | | | С | | | В | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 41.9 | Н | CM 2000 | Level of S | Service | | D | | | |
| HCM 2000 Volume to Capacity | v ratio | | 0.92 | | | | | | | | | |
| Actuated Cycle Length (s) | , | | 100.0 | S | um of lost | time (s) | | | 12.8 | | | |
| Intersection Capacity Utilizatio | n | | 128.6% | | | of Service | | | H | | | |
| Analysis Period (min) | | | 15 | | 2 23.51 | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

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|--|------------|------------|---------------|------------|-------------|----------|-----------|-----------|-----------|----------|------------|-----------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | ↑ ↑ | | ሻ | † 1> | | | ^ | 7 | | ∱ } | |
| Traffic Volume (veh/h) | 130 | 1290 | 140 | 100 | 830 | 50 | 80 | 530 | 170 | 0 | 450 | 70 |
| Future Volume (veh/h) | 130 | 1290 | 140 | 100 | 830 | 50 | 80 | 530 | 170 | 0 | 450 | 70 |
| Initial Q (Qb), veh | 0 | 10 | 0 | 0 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 0.98 | 10 | 0.90 | 1.00 | 10 | 0.90 | 0.95 | J | 0.82 | 1.00 | | 0.83 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach | | No | 1.00 | 1.00 | No | 1.00 | 1.00 | No | 1.00 | 1.00 | No | 1.00 |
| | 1367 | 1367 | 1367 | 1660 | 1660 | 1660 | 1660 | 1660 | 1660 | 0 | 1660 | 1660 |
| Adj Flow Rate, veh/h | 137 | 1358 | 140 | 105 | 874 | 49 | 84 | 558 | 158 | 0 | 474 | 61 |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Percent Heavy Veh, % | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 0.50 | 3 | 3 |
| Cap, veh/h | 73 | 1834 | 178 | 72 | 2341 | 129 | 156 | 817 | 299 | 0 | 710 | 90 |
| Arrive On Green | 0.77 | 0.77 | 0.77 | 1.00 | 1.00 | 1.00 | 0.26 | 0.26 | 0.26 | 0.00 | 0.26 | 0.26 |
| Sat Flow, veh/h | 483 | 2352 | 240 | 348 | 3017 | 169 | 824 | 3154 | 1156 | 0.00 | 2824 | 349 |
| Grp Volume(v), veh/h | 137 | 745 | 753 | 105 | 457 | 466 | 84 | 558 | 158 | 0 | 271 | 264 |
| Grp Sat Flow(s), veh/h/ln | | 1299 | 1293 | 348 | 1577 | 1609 | 824 | 1577 | 1156 | 0 | 1577 | 1513 |
| Q Serve(g_s), s | 9.1 | 30.2 | 31.4 | 21.0 | 0.0 | 0.0 | 10.2 | 15.9 | 11.7 | 0.0 | 15.3 | 15.7 |
| Cycle Q Clear(g_c), s | 9.5 | 30.2 | 31.4 | 53.9 | 0.0 | 0.0 | 25.9 | 15.9 | 11.7 | 0.0 | 15.3 | 15.7 |
| Prop In Lane | 1.00 | 30.2 | 0.19 | 1.00 | 0.0 | 0.11 | 1.00 | 15.5 | 1.00 | 0.00 | 10.0 | 0.23 |
| Lane Grp Cap(c), veh/h | | 1007 | 1005 | 72 | 1222 | 1247 | 156 | 817 | 299 | 0.00 | 408 | 392 |
| V/C Ratio(X) | 1.89 | 0.74 | 0.75 | 1.46 | 0.37 | 0.37 | 0.54 | 0.68 | 0.53 | 0.00 | 0.66 | 0.67 |
| Avail Cap(c_a), veh/h | 445 | 1007 | 1002 | 227 | 1222 | 1247 | 156 | 817 | 299 | 0.00 | 408 | 392 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 2.00 | 2.00 | 2.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 0.86 | 0.86 | 0.86 | 0.94 | 0.94 | 0.94 | 0.00 | 0.46 | 0.46 |
| | | 6.3 | 6.4 | 38.7 | 0.0 | 0.0 | 44.9 | 33.4 | 31.8 | 0.00 | 33.1 | 33.3 |
| Uniform Delay (d), s/veh | | 4.9 | 5.1 | 259.1 | 0.0 | 0.0 | 3.4 | 2.2 | 1.6 | 0.0 | 1.9 | 2.1 |
| Incr Delay (d2), s/veh Initial Q Delay(d3),s/veh | | 0.7 | 0.7 | 0.0 | 0.8 | 0.7 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | | 8.6 | 8.9 | 6.9 | 0.2 | 0.2 | 2.2 | 6.3 | 3.4 | 0.0 | 6.1 | 6.0 |
| %ile BackOfQ(50%),veh Unsig. Movement Delay | | | 0.9 | 0.9 | 0.3 | 0.5 | ۷.۷ | 0.5 | 3.4 | 0.0 | 0.1 | 0.0 |
| LnGrp Delay(d),s/veh | | 11.9 | 12.3 | 297.9 | 0.9 | 0.9 | 48.3 | 35.6 | 33.4 | 0.0 | 35.0 | 35.4 |
| • | 495.6 F | 11.9 B | 12.3 B | 297.9 F | 0.9 A | 0.9 A | 46.3 D | 35.6 D | 33.4 C | 0.0 A | 35.0 C | 35.4 D |
| LnGrp LOS | Г | | D | Г | | A | U | | U | A | | U |
| Approach Vol, veh/h | | 1635 | | | 1028 | | | 800 | | | 535 | |
| Approach Delay, s/veh | | 52.6 | | | 31.3 | | | 36.5 | | | 35.2 | |
| Approach LOS | | D | | | С | | | D | | | D | |
| Timer - Assigned Phs | | 2 | | 4 | | 6 | | 8 | | | | |
| Phs Duration (G+Y+Rc) | , S | 83.0 | | 31.0 | | 83.0 | | 31.0 | | | | |
| Change Period (Y+Rc), | | 5.1 | | * 5.1 | | 5.1 | | 5.1 | | | | |
| Max Green Setting (Gm | | 64.3 | | * 26 | | 64.3 | | 25.5 | | | | |
| Max Q Clear Time (g_c+ | , . | 33.4 | | 27.9 | | 55.9 | | 17.7 | | | | |
| Green Ext Time (p_c), s | | 25.4 | | 0.0 | | 6.3 | | 2.1 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 6th Ctrl Delay | | | 41.6 | | | | | | | | | |
| HCM 6th LOS | | | 41.0 D | | | | | | | | | |
| Notes | | | | | | | | | | | | |

^{*} HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

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|---------------------------------------|------|-------------|------------|-------|----------|------|------|------------|------|-------------|----------|------|
| Movement EE | BL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | † 1> | | ሻ | ^ | 7 | | ∱ ∱ | | * | ^ | 7 |
| Traffic Volume (veh/h) | 0 | 1210 | 120 | 80 | 940 | 280 | 50 | 250 | 90 | 200 | 200 | 40 |
| Future Volume (veh/h) | 0 | 1210 | 120 | 80 | 940 | 280 | 50 | 250 | 90 | 200 | 200 | 40 |
| Initial Q (Qb), veh | 0 | 10 | 0 | 0 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) 1.0 | | 10 | 0.95 | 0.99 | 10 | 0.95 | 0.92 | U | 0.89 | 0.95 | U | 0.92 |
| ,, <u> </u> | 00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach | 00 | No | 1.00 | 1.00 | No | 1.00 | 1.00 | No | 1.00 | 1.00 | No | 1.00 |
| Adj Sat Flow, veh/h/ln | 0 | 1367 | 1367 | 1660 | 1660 | 1660 | 1660 | 1660 | 1660 | 1660 | 1660 | 1660 |
| Adj Flow Rate, veh/h | 0 | 1247 | 117 | 82 | 969 | 191 | 52 | 258 | 93 | 206 | 206 | 13 |
| Peak Hour Factor 0.9 | | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 |
| Percent Heavy Veh, % | 0 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 |
| Cap, veh/h | 0 | 1365 | 95 | 72 | 1739 | 738 | 339 | 559 | 193 | 326 | 1107 | 454 |
| Arrive On Green 0.0 | | 1.00 | 1.00 | 0.55 | 0.55 | 0.55 | 0.25 | 0.25 | 0.25 | 0.07 | 0.35 | 0.35 |
| Sat Flow, veh/h | 0 | 2457 | 223 | 393 | 3154 | 1339 | 1059 | 2221 | 766 | 1581 | 3154 | 1295 |
| Grp Volume(v), veh/h | 0 | 676 | 688 | 82 | 969 | 191 | 52 | 180 | 171 | 206 | 206 | 13 |
| | 0 | 1299 | 1313 | 393 | 1577 | 1339 | 1059 | 1577 | 1410 | 1581 | 1577 | 1295 |
| Grp Sat Flow(s), veh/h/ln | 0.0 | 0.0 | 0.0 | 11.8 | 19.9 | 7.5 | 3.9 | 9.6 | 10.3 | 6.9 | 4.5 | 0.7 |
| |).0 | 0.0 | 0.0 | 11.8 | 19.9 | 7.5 | 3.9 | 9.6 | 10.3 | 6.9 | 4.5 | 0.7 |
| (0-) | 00 | 0.0 | | 1.00 | 19.9 | 1.00 | | 9.0 | 0.54 | 1.00 | 4.5 | 1.00 |
| | | 716 | 0.17 | 72 | 1720 | | 1.00 | 207 | 355 | | 1107 | 454 |
| Lane Grp Cap(c), veh/h | 0 | 716 | 731 | | 1739 | 738 | 339 | 397 | | 326 0.63 | 1107 | 0.03 |
| V/C Ratio(X) 0.0 | | 0.94 | 0.94 | 1.14 | 0.56 | 0.26 | 0.15 | 0.45 | 0.48 | | 0.19 | |
| Avail Cap(c_a), veh/h | 0 | 716 | 724 | 289 | 1739 | 738 | 368 | 442 | 395 | 326 | 1196 | 491 |
| | 00 | 2.00 | 2.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) 0.0 | | 0.36 | 0.36 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh 0 | | 0.0 | 0.0 | 50.0 | 14.9 | 11.7 | 29.4 | 31.6 | 31.9 | 29.3 | 22.5 | 21.3 |
| 3 \ /' | 0.0 | 10.7 | 10.3 | 148.7 | 1.3 | 0.8 | 0.2 | 0.8 | 1.0 | 3.0 | 0.1 | 0.0 |
| , , , , , , , , , , , , , , , , , , , | 0.0 | 6.3 | 5.8 | 0.0 | 0.5 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/ln0 | | 3.4 | 3.3 | 4.8 | 7.9 | 2.4 | 1.0 | 3.8 | 3.6 | 1.9 | 1.7 | 0.2 |
| Unsig. Movement Delay, s/ | | | 16.0 | 100.7 | 10.0 | 10.0 | 20.0 | 20.4 | 20.0 | 20.2 | 20.6 | 24.2 |
| | 0.0 | 17.1 | 16.0 | 198.7 | 16.8 | 12.6 | 29.6 | 32.4 | 32.9 | 32.3 | 22.6 | 21.3 |
| LnGrp LOS | Α | B | В | F | B | В | С | C 400 | С | С | C 405 | С |
| Approach Vol, veh/h | | 1364 | | | 1242 | | | 403 | | | 425 | |
| Approach Delay, s/veh | | 16.5 | | | 28.1 | | | 32.2 | | | 27.3 | |
| Approach LOS | | В | | | С | | | С | | | С | |
| Timer - Assigned Phs | | 2 | | 4 | | 6 | 7 | 8 | | | | |
| Phs Duration (G+Y+Rc), s | | 60.2 | | 39.8 | | 60.2 | 9.9 | 29.9 | | | | |
| Change Period (Y+Rc), s | | 5.1 | | * 4.7 | | 5.1 | 3.0 | * 4.7 | | | | |
| Max Green Setting (Gmax) |). S | 52.3 | | * 38 | | 52.3 | 6.9 | * 28 | | | | |
| Max Q Clear Time (g_c+l1) | | 2.0 | | 6.5 | | 21.9 | 8.9 | 12.3 | | | | |
| Green Ext Time (p_c), s | ,, . | 29.6 | | 1.5 | | 19.0 | 0.0 | 2.2 | | | | |
| Intersection Summary | | _0.0 | | | | .0.0 | 0.0 | | | | | |
| | | | 23.9 | | | | | | | | | |
| HCM 6th Ctrl Delay | | | | | | | | | | | | |
| HCM 6th LOS | | | С | | | | | | | | | |
| Notes | | | | | | | | | | | | |

^{*} HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

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|---------------------------|----------------|----------|---------------|------|------|-------|------|----------|------|------|----------|------|--|
| Movement E | BL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR | |
| Lane Configurations | | | | | 414 | | ሻ | ^ | | | ħβ | | |
| Traffic Volume (veh/h) | 0 | 0 | 0 | 110 | 170 | 70 | 140 | 450 | 0 | 0 | 530 | 100 | |
| Future Volume (veh/h) | 0 | 0 | 0 | 110 | 170 | 70 | 140 | 450 | 0 | 0 | 530 | 100 | |
| Initial Q (Qb), veh | | | | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Ped-Bike Adj(A_pbT) | | | | 1.00 | | 0.79 | 0.94 | | 1.00 | 1.00 | | 0.77 | |
| Parking Bus, Adj | | | | 0.85 | 1.00 | 0.85 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.81 | |
| Work Zone On Approach | | | | | No | | | No | | | No | | |
| Adj Sat Flow, veh/h/ln | | | | 1660 | 1660 | 1660 | 1660 | 1660 | 0 | 0 | 1660 | 1660 | |
| Adj Flow Rate, veh/h | | | | 116 | 179 | 54 | 147 | 474 | 0 | 0 | 558 | 80 | |
| Peak Hour Factor | | | | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | |
| Percent Heavy Veh, % | | | | 3 | 3 | 3 | 3 | 3 | 0 | 0 | 3 | 3 | |
| Cap, veh/h | | | | 311 | 493 | 151 | 367 | 1548 | 0 | 0 | 1178 | 167 | |
| Arrive On Green | | | | 0.37 | 0.37 | 0.37 | 0.49 | 0.49 | 0.00 | 0.00 | 0.49 | 0.49 | |
| Sat Flow, veh/h | | | | 834 | 1323 | 406 | 739 | 3237 | 0.00 | 0.00 | 2484 | 341 | |
| Grp Volume(v), veh/h | | | | 189 | 0 | 160 | 147 | 474 | 0 | 0 | 365 | 273 | |
| | | | | | | 1202 | 739 | 1577 | 0 | 0 | 1577 | 1164 | |
| Grp Sat Flow(s),veh/h/ln | | | | 1361 | 0 | | | | | | | | |
| Q Serve(g_s), s | | | | 6.1 | 0.0 | 5.8 | 9.9 | 5.4 | 0.0 | 0.0 | 9.2 | 9.4 | |
| Cycle Q Clear(g_c), s | | | | 6.1 | 0.0 | 5.8 | 19.3 | 5.4 | 0.0 | 0.0 | 9.2 | 9.4 | |
| Prop In Lane | | | | 0.61 | • | 0.34 | 1.00 | 4540 | 0.00 | 0.00 | 774 | 0.29 | |
| Lane Grp Cap(c), veh/h | | | | 507 | 0 | 448 | 367 | 1548 | 0 | 0 | 774 | 571 | |
| V/C Ratio(X) | | | | 0.37 | 0.00 | 0.36 | 0.40 | 0.31 | 0.00 | 0.00 | 0.47 | 0.48 | |
| Avail Cap(c_a), veh/h | | | | 585 | 0 | 517 | 367 | 1548 | 0 | 0 | 774 | 571 | |
| HCM Platoon Ratio | | | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Upstream Filter(I) | | | | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 0.00 | 0.00 | 0.53 | 0.53 | |
| Uniform Delay (d), s/veh | | | | 13.7 | 0.0 | 13.6 | 16.6 | 9.2 | 0.0 | 0.0 | 10.1 | 10.2 | |
| Incr Delay (d2), s/veh | | | | 0.5 | 0.0 | 0.5 | 3.2 | 0.5 | 0.0 | 0.0 | 1.1 | 1.5 | |
| Initial Q Delay(d3),s/veh | | | | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | |
| %ile BackOfQ(50%),veh/lr | า | | | 1.8 | 0.0 | 1.5 | 1.9 | 1.7 | 0.0 | 0.0 | 3.0 | 2.3 | |
| Unsig. Movement Delay, s | s/veh | | | | | | | | | | | | |
| LnGrp Delay(d),s/veh | | | | 14.2 | 0.0 | 14.1 | 19.8 | 9.7 | 0.0 | 0.0 | 11.2 | 11.7 | |
| LnGrp LOS | | | | В | Α | В | В | Α | Α | Α | В | В | |
| Approach Vol, veh/h | | | | | 349 | | | 621 | | | 638 | | |
| Approach Delay, s/veh | | | | | 14.1 | | | 12.1 | | | 11.4 | | |
| Approach LOS | | | | | В | | | В | | | В | | |
| Timer - Assigned Phs | | 2 | | | | 6 | | 8 | | | | | |
| Phs Duration (G+Y+Rc), s | | 33.6 | | | | 33.6 | | 26.4 | | | | | |
| Change Period (Y+Rc), s | | * 4.2 | | | | * 4.2 | | 4.0 | | | | | |
| Max Green Setting (Gmax | 2 (2 | * 26 | | | | * 26 | | 25.8 | | | | | |
| Max Q Clear Time (g_c+l1 | | 21.3 | | | | 11.4 | | 8.1 | | | | | |
| Green Ext Time (p_c), s | ı <i>j</i> , ə | 2.5 | | | | 6.1 | | 2.1 | | | | | |
| (1 – 7) | | | | | | J., | | | | | | | |
| Intersection Summary | | | 40.0 | | | | | | | | | | |
| HCM 6th Ctrl Delay | | | 12.3 | | | | | | | | | | |
| HCM 6th LOS | | | В | | | | | | | | | | |
| Notes | | | | | | | | | | | | | |

^{*} HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

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|-----------------------------------|-------|----------|-------|------|-------------|------------|---------|---|-------------|----------|------------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | | | | € 1₽ | | ¥ | ^ | | | ∱ ⊅ | |
| Traffic Volume (vph) | 0 | 0 | 0 | 80 | 200 | 140 | 70 | 310 | 0 | 0 | 390 | 130 |
| Future Volume (vph) | 0 | 0 | 0 | 80 | 200 | 140 | 70 | 310 | 0 | 0 | 390 | 130 |
| Ideal Flow (vphpl) | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 |
| Total Lost time (s) | | | | | 3.0 | | 4.0 | 4.0 | | | 4.0 | |
| Lane Util. Factor | | | | | 0.95 | | 1.00 | 0.95 | | | 0.95 | |
| Frpb, ped/bikes | | | | | 1.00 | | 1.00 | 1.00 | | | 1.00 | |
| Flpb, ped/bikes | | | | | 1.00 | | 1.00 | 1.00 | | | 1.00 | |
| Frt | | | | | 0.95 | | 1.00 | 1.00 | | | 0.96 | |
| Flt Protected | | | | | 0.99 | | 0.95 | 1.00 | | | 1.00 | |
| Satd. Flow (prot) | | | | | 2748 | | 1568 | 2885 | | | 2775 | |
| Flt Permitted | | | | | 0.99 | | 0.27 | 1.00 | | | 1.00 | |
| Satd. Flow (perm) | | | | | 2748 | | 447 | 2885 | | | 2775 | |
| Peak-hour factor, PHF | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Adj. Flow (vph) | 0 | 0 | 0 | 84 | 211 | 147 | 74 | 326 | 0 | 0 | 411 | 137 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 85 | 0 | 0 | 0 | 0 | 0 | 46 | 0 |
| Lane Group Flow (vph) | 0 | 0 | 0 | 0 | 357 | 0 | 74 | 326 | 0 | 0 | 502 | 0 |
| Confl. Bikes (#/hr) | | | 1 | | | 1 | | | 1 | | | 1 |
| Heavy Vehicles (%) | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% |
| Parking (#/hr) | | | | 6 | 6 | 4 | | 12 | | | 11 | 11 |
| Turn Type | | | | Perm | NA | | Perm | NA | | | NA | |
| Protected Phases | | | | | 6 | | | 8 | | | 4 | |
| Permitted Phases | | | | 6 | | | 8 | | | | | |
| Actuated Green, G (s) | | | | | 23.0 | | 16.0 | 16.0 | | | 16.0 | |
| Effective Green, g (s) | | | | | 23.0 | | 16.0 | 16.0 | | | 16.0 | |
| Actuated g/C Ratio | | | | | 0.33 | | 0.23 | 0.23 | | | 0.23 | |
| Clearance Time (s) | | | | | 3.0 | | 4.0 | 4.0 | | | 4.0 | |
| Vehicle Extension (s) | | | | | 2.0 | | 2.0 | 2.0 | | | 2.0 | |
| Lane Grp Cap (vph) | | | | | 902 | | 102 | 659 | | | 634 | |
| v/s Ratio Prot | | | | | | | | 0.11 | | | c0.18 | |
| v/s Ratio Perm | | | | | 0.13 | | 0.17 | • | | | | |
| v/c Ratio | | | | | 0.40 | | 0.73 | 0.49 | | | 0.79 | |
| Uniform Delay, d1 | | | | | 18.1 | | 25.0 | 23.5 | | | 25.4 | |
| Progression Factor | | | | | 1.00 | | 1.00 | 1.00 | | | 1.00 | |
| Incremental Delay, d2 | | | | | 1.3 | | 36.1 | 2.6 | | | 9.8 | |
| Delay (s) | | | | | 19.4 | | 61.1 | 26.1 | | | 35.2 | |
| Level of Service | | | | | В | | E | C | | | D | |
| Approach Delay (s) | | 0.0 | | | 19.4 | | | 32.6 | | | 35.2 | |
| Approach LOS | | A | | | В | | | C | | | D | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 29.4 | Н | CM 2000 | Level of | Service | | С | | | |
| HCM 2000 Volume to Capacity | ratio | | 0.37 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 70.0 | S | um of lost | time (s) | | | 11.0 | | | |
| Intersection Capacity Utilization | 1 | | 48.8% | | | of Service | | | A | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | . • | | | | | | | | | |

| Intersection | | | | | | | | | | | | |
|------------------------|------|------|-------|----------|-------|------|------|-------|------|---------|------|------|
| Int Delay, s/veh | 1.1 | | | | | | | | | | | |
| | | | | | | | | | | | | |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | | | | 41 | | | | | | ħβ | |
| Traffic Vol, veh/h | 0 | 0 | 0 | 0 | 380 | 0 | 0 | 0 | 0 | 0 | 0 | 48 |
| Future Vol, veh/h | 0 | 0 | 0 | 0 | 380 | 0 | 0 | 0 | 0 | 0 | 0 | 48 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 251 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | - | - | - | - | - | - | - | - | - | - |
| Veh in Median Storage | ,# - | 2 | - | - | 0 | - | - | 16974 | - | - | 0 | - |
| Grade, % | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 |
| Heavy Vehicles, % | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 |
| Mvmt Flow | 0 | 0 | 0 | 0 | 400 | 0 | 0 | 0 | 0 | 0 | 0 | 51 |
| | | | | | | | | | | | | |
| Major/Minor | | | ı | Major2 | | | | | N | /linor2 | | |
| Conflicting Flow All | | | | 251 | 0 | 0 | | | 11 | - | 651 | 200 |
| Stage 1 | | | | 201 | | | | | | _ | 400 | |
| | | | | - | - | - | | | | _ | 251 | - |
| Stage 2 | | | | 4.16 | - | _ | | | | _ | 6.56 | 6.96 |
| Critical Hdwy | | | | 4.10 | _ | - | | | | _ | 5.56 | |
| Critical Hdwy Stg 1 | | | | - | - | _ | | | | _ | | - |
| Critical Hdwy Stg 2 | | | | 2.23 | | - | | | | - | 4 02 | 2 22 |
| Follow-up Hdwy | | | | | - | - | | | | - | 4.03 | 3.33 |
| Pot Cap-1 Maneuver | | | | 1304 | - | 0 | | | | 0 | 384 | 804 |
| Stage 1 | | | | - | - | 0 | | | | 0 | 597 | - |
| Stage 2 | | | | - | - | 0 | | | | 0 | - | - |
| Platoon blocked, % | | | | 1204 | - | | | | | | 0 | 004 |
| Mov Cap-1 Maneuver | | | | 1304 | - | - | | | | - | 0 | 804 |
| Mov Cap-2 Maneuver | | | | - | - | - | | | | - | 0 | - |
| Stage 1 | | | | - | - | - | | | | - | 0 | - |
| Stage 2 | | | | - | - | - | | | | - | 0 | - |
| | | | | | | | | | | | | |
| Approach | | | | WB | | | | | | SB | | |
| HCM Control Delay, s | | | | 0 | | | | | | 9.8 | | |
| HCM LOS | | | | | | | | | | A | | |
| | | | | | | | | | | | | |
| | | 14/5 | 14/5- | . | 001 6 | | | | | | | |
| Minor Lane/Major Mvm | t | WBL | WBT | SBLn1 | | | | | | | | |
| Capacity (veh/h) | | 1304 | - | - | ••• | | | | | | | |
| HCM Lane V/C Ratio | | - | - | | 0.063 | | | | | | | |
| HCM Control Delay (s) | | 0 | - | 0 | 9.8 | | | | | | | |
| HCM Lane LOS | | Α | - | Α | Α | | | | | | | |
| HCM 95th %tile Q(veh) | | 0 | - | - | 0.2 | | | | | | | |

| Intersection | | | | | | |
|------------------------|----------|----------|---------|----------|--------|------|
| Int Delay, s/veh | 0.1 | | | | | |
| | | | | | | |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | ħβ | | ሻ | ^ | | 7 |
| Traffic Vol, veh/h | 1430 | 35 | 13 | 970 | 0 | 0 |
| Future Vol, veh/h | 1430 | 35 | 13 | 970 | 0 | 0 |
| Conflicting Peds, #/hr | 0 | 100 | 100 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | 25 | - | - | 0 |
| Veh in Median Storage, | # 0 | - | - | 0 | 0 | - |
| Grade, % | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 96 | 96 | 96 | 96 | 96 | 96 |
| Heavy Vehicles, % | 3 | 3 | 3 | 3 | 3 | 3 |
| Mvmt Flow | 1490 | 36 | 14 | 1010 | 0 | 0 |
| | 1100 | 00 | | 1010 | • | |
| | | | | | | |
| | 1ajor1 | | //ajor2 | 1 | Minor1 | |
| Conflicting Flow All | 0 | 0 | 1626 | 0 | - | 863 |
| Stage 1 | - | - | - | - | - | - |
| Stage 2 | - | - | - | - | - | - |
| Critical Hdwy | - | - | 4.16 | - | - | 6.96 |
| Critical Hdwy Stg 1 | _ | - | - | _ | _ | - |
| Critical Hdwy Stg 2 | _ | _ | _ | _ | _ | _ |
| Follow-up Hdwy | _ | _ | 2.23 | _ | _ | 3.33 |
| Pot Cap-1 Maneuver | _ | _ | 391 | _ | 0 | 296 |
| Stage 1 | <u>-</u> | <u>-</u> | - | _ | 0 | - |
| Stage 2 | _ | _ | _ | _ | 0 | _ |
| Platoon blocked, % | | _ | _ | _ | U | _ |
| | | | 354 | | | 260 |
| Mov Cap-1 Maneuver | - | - | | - | - | 268 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - |
| Stage 1 | - | - | - | - | - | - |
| Stage 2 | - | - | - | - | - | - |
| | | | | | | |
| Approach | EB | | WB | | NB | |
| HCM Control Delay, s | 0 | | 0.2 | | 0 | |
| HCM LOS | U | | 0.2 | | A | |
| TIOW LOO | | | | | | |
| | | | | | | |
| Minor Lane/Major Mvmt | t 1 | NBLn1 | EBT | EBR | WBL | WBT |
| Capacity (veh/h) | | _ | _ | - | 354 | _ |
| HCM Lane V/C Ratio | | _ | _ | _ | 0.038 | - |
| HCM Control Delay (s) | | 0 | _ | _ | 15.6 | _ |
| HCM Lane LOS | | A | - | _ | C | _ |
| HCM 95th %tile Q(veh) | | - | _ | _ | 0.1 | _ |
| How Jour Joure Q(Ver) | | _ | | _ | 0.1 | _ |

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|------------------------------|------|------------|------|-------|------------|------|------|------|----------|----------|----------|----------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ሻ | ∱ ⊅ | | ሻ | ∱ ⊅ | | | ħβ | | 7 | ^ | 7 |
| Traffic Volume (veh/h) | 30 | 1591 | 34 | 90 | 1759 | 31 | 0 | 80 | 31 | 30 | 321 | 50 |
| Future Volume (veh/h) | 30 | 1591 | 34 | 90 | 1759 | 31 | 0 | 80 | 31 | 30 | 321 | 50 |
| Initial Q (Qb), veh | 0 | 10 | 0 | 0 | 15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | | 0.97 | 1.00 | | 0.99 | 1.00 | | 0.97 | 0.99 | | 0.98 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach | | No | | | No | | | No | | | No | |
| Adj Sat Flow, veh/h/ln | 1367 | 1367 | 1367 | 1367 | 1367 | 1367 | 0 | 1660 | 1660 | 1660 | 1660 | 1660 |
| Adj Flow Rate, veh/h | 33 | 1768 | 37 | 100 | 1954 | 33 | 0 | 89 | 18 | 33 | 357 | 37 |
| Peak Hour Factor | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Percent Heavy Veh, % | 3 | 3 | 3 | 3 | 3 | 3 | 0 | 3 | 3 | 3 | 3 | 3 |
| Cap, veh/h | 72 | 1900 | 33 | 72 | 1919 | 18 | 0 | 453 | 89 | 253 | 546 | 239 |
| Arrive On Green | 0.73 | 0.73 | 0.73 | 0.73 | 0.73 | 0.73 | 0.00 | 0.17 | 0.17 | 0.17 | 0.17 | 0.17 |
| Sat Flow, veh/h | 178 | 2600 | 54 | 213 | 2614 | 44 | 0 | 2700 | 513 | 1264 | 3154 | 1380 |
| Grp Volume(v), veh/h | 33 | 880 | 925 | 100 | 968 | 1019 | 0 | 53 | 54 | 33 | 357 | 37 |
| Grp Sat Flow(s),veh/h/ln | 178 | 1299 | 1356 | 213 | 1299 | 1359 | 0 | 1577 | 1552 | 1264 | 1577 | 1380 |
| Q Serve(g_s), s | 0.0 | 57.3 | 58.4 | 14.4 | 72.8 | 72.8 | 0.0 | 2.8 | 3.0 | 2.3 | 10.6 | 2.3 |
| Cycle Q Clear(g_c), s | 72.8 | 57.3 | 58.4 | 72.8 | 72.8 | 72.8 | 0.0 | 2.8 | 3.0 | 5.3 | 10.6 | 2.3 |
| Prop In Lane | 1.00 | | 0.04 | 1.00 | | 0.03 | 0.00 | | 0.33 | 1.00 | | 1.00 |
| Lane Grp Cap(c), veh/h | 72 | 945 | 988 | 72 | 945 | 992 | 0 | 273 | 269 | 253 | 546 | 239 |
| V/C Ratio(X) | 0.46 | 0.93 | 0.94 | 1.39 | 1.02 | 1.03 | 0.00 | 0.19 | 0.20 | 0.13 | 0.65 | 0.15 |
| Avail Cap(c_a), veh/h | 72 | 945 | 987 | 103 | 945 | 989 | 0 | 420 | 413 | 370 | 839 | 367 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 0.09 | 0.09 | 0.09 | 0.00 | 0.98 | 0.98 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 50.0 | 12.1 | 12.2 | 50.0 | 13.6 | 13.6 | 0.0 | 35.4 | 35.4 | 37.7 | 38.5 | 35.1 |
| Incr Delay (d2), s/veh | 19.6 | 16.7 | 16.8 | 182.7 | 15.8 | 16.9 | 0.0 | 0.3 | 0.4 | 0.2 | 1.3 | 0.3 |
| Initial Q Delay(d3),s/veh | 0.0 | 2.9 | 2.9 | 0.0 | 28.6 | 27.2 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/ln | 1.2 | 18.4 | 19.4 | 5.4 | 27.2 | 28.4 | 0.0 | 1.1 | 1.2 | 0.7 | 4.2 | 0.8 |
| Unsig. Movement Delay, s/veh | | | | | | | | | | | | |
| LnGrp Delay(d),s/veh | 69.6 | 31.8 | 31.9 | 232.7 | 58.0 | 57.7 | 0.0 | 35.7 | 35.8 | 37.9 | 39.9 | 35.4 |
| LnGrp LOS | Е | С | С | F | F | F | Α | D | D | D | D | <u>D</u> |
| Approach Vol, veh/h | | 1838 | | | 2087 | | | 107 | | | 427 | |
| Approach Delay, s/veh | | 32.6 | | | 66.2 | | | 35.7 | | | 39.3 | |
| Approach LOS | | С | | | Е | | | D | | | D | |
| Timer - Assigned Phs | | 2 | | 4 | | 6 | | 8 | | | | |
| Phs Duration (G+Y+Rc), s | | 78.2 | | 21.8 | | 78.2 | | 21.8 | | | | |
| Change Period (Y+Rc), s | | 5.4 | | 4.5 | | 5.4 | | 4.5 | | | | |
| Max Green Setting (Gmax), s | | 63.5 | | 26.6 | | 63.5 | | 26.6 | | | | |
| Max Q Clear Time (g_c+l1), s | | 74.8 | | 12.6 | | 74.8 | | 5.0 | | | | |
| Green Ext Time (p_c), s | | 0.0 | | 2.2 | | 0.0 | | 0.5 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 6th Ctrl Delay | | | 49.0 | | | | | | | | | |
| HCM 6th LOS | | | D | | | | | | | | | |

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|--------------------------|-------|------------|-------|-------|-------|------|------|----------|----------|----------|----------|------|--|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR | |
| Lane Configurations | ķ | ∱ } | | ¥ | ħβ | | ķ | † | | ķ | † | | |
| Traffic Volume (veh/h) | 40 | 1770 | 31 | 105 | 1530 | 40 | 30 | 363 | 154 | 40 | 504 | 60 | |
| Future Volume (veh/h) | 40 | 1770 | 31 | 105 | 1530 | 40 | 30 | 363 | 154 | 40 | 504 | 60 | |
| Initial Q (Qb), veh | 0 | 10 | 0 | 0 | 15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Ped-Bike Adj(A_pbT) | 1.00 | | 0.98 | 1.00 | | 0.97 | 1.00 | | 0.97 | 0.99 | | 0.98 | |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Work Zone On Approac | | No | | | No | | | No | | | No | | |
| Adj Sat Flow, veh/h/ln | 1367 | 1367 | 1367 | 1367 | 1367 | 1367 | 1660 | 1660 | 1660 | 1660 | 1660 | 1660 | |
| Adj Flow Rate, veh/h | 44 | 1967 | 33 | 117 | 1700 | 42 | 33 | 403 | 161 | 44 | 560 | 58 | |
| Peak Hour Factor | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | |
| Percent Heavy Veh, % | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | |
| Cap, veh/h | 72 | 1692 | 15 | 72 | 1687 | 20 | 127 | 548 | 216 | 157 | 721 | 74 | |
| Arrive On Green | 0.64 | 0.64 | 0.64 | 0.64 | 0.64 | 0.64 | 0.50 | 0.50 | 0.50 | 0.25 | 0.25 | 0.25 | |
| Sat Flow, veh/h | 226 | 2614 | 44 | 176 | 2589 | 64 | 795 | 2188 | 861 | 835 | 2880 | 297 | |
| Grp Volume(v), veh/h | 44 | 974 | 1026 | 117 | 850 | 892 | 33 | 289 | 275 | 44 | 306 | 312 | |
| Grp Sat Flow(s),veh/h/lr | 226 | 1299 | 1358 | 176 | 1299 | 1353 | 795 | 1577 | 1472 | 835 | 1577 | 1600 | |
| Q Serve(g_s), s | 0.0 | 64.2 | 64.2 | 0.0 | 64.2 | 64.2 | 3.9 | 14.4 | 14.9 | 5.0 | 18.0 | 18.2 | |
| Cycle Q Clear(g_c), s | 64.2 | 64.2 | 64.2 | 64.2 | 64.2 | 64.2 | 22.1 | 14.4 | 14.9 | 19.9 | 18.0 | 18.2 | |
| Prop In Lane | 1.00 | | 0.03 | 1.00 | | 0.05 | 1.00 | | 0.59 | 1.00 | | 0.19 | |
| _ane Grp Cap(c), veh/h | 72 | 833 | 874 | 72 | 833 | 873 | 127 | 395 | 368 | 157 | 395 | 400 | |
| V/C Ratio(X) | 0.61 | 1.17 | 1.17 | 1.62 | 1.02 | 1.02 | 0.26 | 0.73 | 0.75 | 0.28 | 0.78 | 0.78 | |
| Avail Cap(c_a), veh/h | 72 | 833 | 872 | 72 | 833 | 868 | 139 | 420 | 392 | 170 | 420 | 426 | |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 2.00 | 2.00 | 2.00 | 1.00 | 1.00 | 1.00 | |
| Upstream Filter(I) | 0.09 | 0.09 | 0.09 | 1.00 | 1.00 | 1.00 | 0.77 | 0.77 | 0.77 | 1.00 | 1.00 | 1.00 | |
| Jniform Delay (d), s/veh | 150.0 | 17.9 | 17.9 | 50.0 | 17.9 | 17.9 | 32.8 | 22.3 | 22.4 | 42.6 | 34.9 | 34.9 | |
| Incr Delay (d2), s/veh | 3.5 | 77.4 | 79.2 | 335.7 | 36.4 | 35.9 | 0.8 | 4.7 | 5.6 | 1.0 | 8.4 | 8.5 | |
| nitial Q Delay(d3),s/veh | 0.0 | 21.6 | 20.6 | 0.0 | 32.4 | 30.9 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | |
| %ile BackOfQ(50%),vel | | 38.9 | 41.0 | 8.5 | 31.9 | 32.9 | 0.7 | 4.5 | 4.4 | 1.1 | 7.8 | 8.0 | |
| Jnsig. Movement Delay | | 1 | | | | | | | | | | | |
| LnGrp Delay(d),s/veh | 53.5 | 116.9 | 117.7 | 385.7 | 86.7 | 84.8 | 33.6 | 27.0 | 28.1 | 43.6 | 43.2 | 43.4 | |
| _nGrp LOS | D | F | F | F | F | F | С | С | С | D | D | D | |
| Approach Vol, veh/h | | 2044 | | | 1859 | | | 597 | | | 662 | | |
| Approach Delay, s/veh | | 115.9 | | | 104.6 | | | 27.9 | | | 43.3 | | |
| Approach LOS | | F | | | F | | | С | | | D | | |
| Fimer - Assigned Phs | | 2 | | 4 | | 6 | | 8 | | | | | |
| Phs Duration (G+Y+Rc) | c | 69.6 | | 30.4 | | 69.6 | | 30.4 | | | | | |
| Change Period (Y+Rc), | | 5.4 | | 5.4 | | 5.4 | | 5.4 | | | | | |
| Max Green Setting (Gm | | 62.6 | | 26.6 | | 62.6 | | 26.6 | | | | | |
| Max Q Clear Time (g_c- | | | | 21.9 | | 66.2 | | 24.1 | | | | | |
| Green Ext Time (p_c), s | | 0.0 | | 1.8 | | 0.0 | | 1.0 | | | | | |
| u = 7; | | 0.0 | | 1.0 | | 0.0 | | 1.0 | | | | | |
| ntersection Summary | | | | | | | | | | | | | |
| HCM 6th Ctrl Delay | | | 92.4 | | | | | | | | | | |
| HCM 6th LOS | | | F | | | | | | | | | | |

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|-----------------------------------|----------|------------|--------|-------|------------|------------|---------|-------------|----------|----------|-------------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | ∱ ⊅ | | | 413- | | ሻ | † 1> | | ሻ | † 1> | |
| Traffic Volume (vph) | 0 | 730 | 50 | 140 | 1420 | 30 | 21 | 101 | 48 | 45 | 360 | 60 |
| Future Volume (vph) | 0 | 730 | 50 | 140 | 1420 | 30 | 21 | 101 | 48 | 45 | 360 | 60 |
| Ideal Flow (vphpl) | 1700 | 1700 | 1700 | 1400 | 1400 | 1400 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 |
| Total Lost time (s) | | 5.1 | | | 5.1 | | 4.5 | 4.5 | | 4.5 | 4.5 | |
| Lane Util. Factor | | 0.95 | | | 0.95 | | 1.00 | 0.95 | | 1.00 | 0.95 | |
| Frpb, ped/bikes | | 1.00 | | | 1.00 | | 1.00 | 0.98 | | 1.00 | 0.99 | |
| Flpb, ped/bikes | | 1.00 | | | 1.00 | | 0.99 | 1.00 | | 0.97 | 1.00 | |
| Frt | | 0.99 | | | 1.00 | | 1.00 | 0.95 | | 1.00 | 0.98 | |
| Flt Protected | | 1.00 | | | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | | 3095 | | | 2555 | | 1545 | 2725 | | 1514 | 3050 | |
| Flt Permitted | | 1.00 | | | 0.69 | | 0.35 | 1.00 | | 0.65 | 1.00 | |
| Satd. Flow (perm) | | 3095 | | | 1775 | | 567 | 2725 | | 1040 | 3050 | |
| Peak-hour factor, PHF | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Adj. Flow (vph) | 0 | 768 | 53 | 147 | 1495 | 32 | 22 | 106 | 51 | 47 | 379 | 63 |
| RTOR Reduction (vph) | 0 | 4 | 0 | 0 | 1 | 0 | 0 | 39 | 0 | 0 | 14 | 0 |
| Lane Group Flow (vph) | 0 | 817 | 0 | 0 | 1673 | 0 | 22 | 118 | 0 | 47 | 428 | 0 |
| Confl. Peds. (#/hr) | 100 | | 29 | 29 | | 100 | 24 | | 33 | 33 | | 24 |
| Confl. Bikes (#/hr) | | | 3 | | | 2 | | | 1 | | | 1 |
| Heavy Vehicles (%) | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% |
| Parking (#/hr) | | | | | | | | 8 | 8 | | | |
| Turn Type | | NA | | pm+pt | NA | | Perm | NA | | Perm | NA | |
| Protected Phases | | 2 | | 1 | 6 | | | 8 | | | 4 | |
| Permitted Phases | | | | 6 | | | 8 | | | 4 | | |
| Actuated Green, G (s) | | 59.5 | | | 67.2 | | 23.2 | 23.2 | | 23.2 | 23.2 | |
| Effective Green, g (s) | | 59.5 | | | 67.2 | | 23.2 | 23.2 | | 23.2 | 23.2 | |
| Actuated g/C Ratio | | 0.60 | | | 0.67 | | 0.23 | 0.23 | | 0.23 | 0.23 | |
| Clearance Time (s) | | 5.1 | | | 5.1 | | 4.5 | 4.5 | | 4.5 | 4.5 | |
| Vehicle Extension (s) | | 5.0 | | | 5.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | | 1841 | | | 1227 | | 131 | 632 | | 241 | 707 | |
| v/s Ratio Prot | | 0.26 | | | c0.06 | | | 0.04 | | | c0.14 | |
| v/s Ratio Perm | | | | | c0.85 | | 0.04 | | | 0.05 | | |
| v/c Ratio | | 0.44 | | | 1.36 | | 0.17 | 0.19 | | 0.20 | 0.61 | |
| Uniform Delay, d1 | | 11.1 | | | 16.4 | | 30.7 | 30.8 | | 30.9 | 34.3 | |
| Progression Factor | | 1.00 | | | 0.50 | | 1.00 | 1.00 | | 0.43 | 0.39 | |
| Incremental Delay, d2 | | 8.0 | | | 166.2 | | 0.6 | 0.1 | | 0.2 | 0.9 | |
| Delay (s) | | 11.9 | | | 174.4 | | 31.3 | 31.0 | | 13.5 | 14.3 | |
| Level of Service | | В | | | F | | С | С | | В | В | |
| Approach Delay (s) | | 11.9 | | | 174.4 | | | 31.0 | | | 14.3 | |
| Approach LOS | | В | | | F | | | С | | | В | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 99.3 | Н | CM 2000 | Level of S | Service | | F | | | |
| HCM 2000 Volume to Capacit | ty ratio | | 1.21 | | | | | | | | | |
| Actuated Cycle Length (s) | · | | 100.0 | S | um of lost | t time (s) | | | 12.8 | | | |
| Intersection Capacity Utilization | on | | 124.0% | | | of Service | | | Н | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

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|---------------------------|------------|-----------|------------|------------|------------|----------|-----------|-----------|-----------|------|-----------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ሻ | ħβ | | ች | ∱ ∱ | | ሻ | ^ | 7 | | ħβ | |
| Traffic Volume (veh/h) | 96 | 648 | 191 | 176 | 1424 | 30 | 44 | 400 | 80 | 0 | 553 | 87 |
| Future Volume (veh/h) | 96 | 648 | 191 | 176 | 1424 | 30 | 44 | 400 | 80 | 0 | 553 | 87 |
| Initial Q (Qb), veh | 0 | 10 | 0 | 0 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | .0 | 0.95 | 0.99 | | 0.96 | 0.99 | | 0.91 | 1.00 | | 0.91 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approac | | No | 1.00 | 1.00 | No | 1.00 | 1.00 | No | 1.00 | 1.00 | No | 1.00 |
| Adj Sat Flow, veh/h/ln | 1660 | 1660 | 1660 | 1367 | 1367 | 1367 | 1660 | 1660 | 1660 | 0 | 1660 | 1660 |
| Adj Flow Rate, veh/h | 101 | 682 | 192 | 185 | 1499 | 31 | 46 | 421 | 21 | 0 | 582 | 79 |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Percent Heavy Veh, % | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 0 | 3 | 3 |
| Cap, veh/h | 72 | 1875 | 514 | 72 | 2017 | 40 | 117 | 817 | 333 | 0 | 714 | 97 |
| Arrive On Green | 0.77 | 0.77 | 0.77 | 1.00 | 1.00 | 1.00 | 0.26 | 0.26 | 0.26 | 0.00 | 0.26 | 0.26 |
| Sat Flow, veh/h | 336 | 2402 | 676 | 515 | 2600 | 54 | 758 | 3154 | 1285 | 0.00 | 2839 | 373 |
| Grp Volume(v), veh/h | 101 | 448 | 426 | 185 | 748 | 782 | 46 | 421 | 21 | 0 | 332 | 329 |
| Grp Sat Flow(s), veh/h/li | | 1577 | 1501 | 515 | 1299 | 1355 | 758 | 1577 | 1285 | 0 | 1577 | 1551 |
| Q Serve(g_s), s | 9.8 | 8.9 | 8.9 | 8.3 | 0.0 | 0.0 | 6.0 | 11.4 | 1.2 | 0.0 | 19.8 | 19.9 |
| Cycle Q Clear(g_c), s | 10.2 | 8.9 | 8.9 | 18.0 | 0.0 | 0.0 | 25.9 | 11.4 | 1.2 | 0.0 | 19.8 | 19.9 |
| Prop In Lane | 1.00 | 0.5 | 0.45 | 1.00 | 0.0 | 0.04 | 1.00 | 11.7 | 1.00 | 0.00 | 13.0 | 0.24 |
| Lane Grp Cap(c), veh/h | | 1222 | 1165 | 72 | 1007 | 1050 | 117 | 817 | 333 | 0.00 | 408 | 402 |
| V/C Ratio(X) | 1.40 | 0.37 | 0.37 | 2.57 | 0.74 | 0.74 | 0.39 | 0.52 | 0.06 | 0.00 | 0.81 | 0.82 |
| Avail Cap(c_a), veh/h | 331 | 1222 | 1163 | 422 | 1007 | 1050 | 117 | 817 | 333 | 0.00 | 408 | 402 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 2.00 | 2.00 | 2.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 0.40 | 0.40 | 0.40 | 1.00 | 1.00 | 1.00 | 0.00 | 0.09 | 0.09 |
| Uniform Delay (d), s/vel | | 3.7 | 3.7 | 38.7 | 0.0 | 0.0 | 47.1 | 31.7 | 27.9 | 0.0 | 34.8 | 34.8 |
| Incr Delay (d2), s/veh | | 0.8 | 0.9 | 720.4 | 2.0 | 2.0 | 2.1 | 0.6 | 0.1 | 0.0 | 1.2 | 1.3 |
| Initial Q Delay(d3),s/ver | | 0.8 | 0.9 | 0.0 | 0.7 | 0.6 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),vel | | 3.1 | 2.9 | 16.2 | 0.7 | 0.8 | 1.2 | 4.4 | 0.0 | 0.0 | 7.7 | 7.6 |
| Unsig. Movement Delay | | | 2.3 | 10.2 | 0.0 | 0.0 | 1.2 | 7.7 | 0.4 | 0.0 | 1.1 | 7.0 |
| LnGrp Delay(d),s/veh | | 4.8 | 4.8 | 759.2 | 2.7 | 2.6 | 49.2 | 32.2 | 28.0 | 0.0 | 36.0 | 36.1 |
| LnGrp LOS | 294.1 F | 4.0 A | 4.0 A | 739.Z F | 2.7 A | 2.0 A | 49.2 D | 32.2 C | 20.0 C | Α | 30.0 D | D |
| Approach Vol, veh/h | 1 | 975 | | <u> </u> | 1715 | | U | 488 | <u> </u> | | 661 | U |
| Approach Delay, s/veh | | 34.8 | | | 84.3 | | | 33.7 | | | 36.0 | |
| Approach LOS | | 34.0 C | | | 04.3 F | | | 33.7 C | | | 30.0 D | |
| ., | | | | | Г | | | | | | U | |
| Timer - Assigned Phs | | 2 | | 4 | | 6 | | 8 | | | | |
| Phs Duration (G+Y+Rc) |), s | 83.0 | | 31.0 | | 83.0 | | 31.0 | | | | |
| Change Period (Y+Rc), | S | 5.1 | | * 5.1 | | 5.1 | | 5.1 | | | | |
| Max Green Setting (Gm | nax), s | 64.3 | | * 26 | | 64.3 | | 25.5 | | | | |
| Max Q Clear Time (g_c | +I1), s | 12.2 | | 27.9 | | 20.0 | | 21.9 | | | | |
| Green Ext Time (p_c), s | 3 | 21.2 | | 0.0 | | 35.2 | | 1.4 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 6th Ctrl Delay | | | 57.0 | | | | | | | | | |
| HCM 6th LOS | | | Е | | | | | | | | | |
| Notes | | | | | | | | | | | | |

^{*} HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

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|---------------------------|---------|------------|------------|-------|----------|------|------|------------|------|------|----------|------|--|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR | |
| Lane Configurations | | ∱ ∱ | | ች | ^ | 7 | ሻ | ↑ ↑ | | * | ^ | 7 | |
| Traffic Volume (veh/h) | 0 | 566 | 82 | 80 | 1438 | 120 | 33 | 80 | 40 | 220 | 290 | 90 | |
| Future Volume (veh/h) | 0 | 566 | 82 | 80 | 1438 | 120 | 33 | 80 | 40 | 220 | 290 | 90 | |
| Initial Q (Qb), veh | 0 | 10 | 0 | 0 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Ped-Bike Adj(A_pbT) | 1.00 | | 0.97 | 0.99 | | 0.97 | 0.95 | | 0.92 | 0.94 | | 0.94 | |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Work Zone On Approac | | No | 1.00 | 1.00 | No | 1.00 | 1.00 | No | 1.00 | 1.00 | No | 1.00 | |
| Adj Sat Flow, veh/h/ln | 0 | 1660 | 1660 | 1367 | 1367 | 1367 | 1660 | 1660 | 1660 | 1660 | 1660 | 1660 | |
| Adj Flow Rate, veh/h | 0 | 572 | 74 | 81 | 1453 | 95 | 33 | 81 | 40 | 222 | 293 | 75 | |
| Peak Hour Factor | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | |
| Percent Heavy Veh, % | 0.55 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | |
| Cap, veh/h | 0 | 1624 | 203 | 72 | 1501 | 647 | 287 | 463 | 207 | 407 | 1022 | 430 | |
| Arrive On Green | 0.00 | 1.00 | 1.00 | 0.58 | 0.58 | 0.58 | 0.23 | 0.23 | 0.23 | 0.07 | 0.32 | 0.32 | |
| Sat Flow, veh/h | 0.00 | 2881 | 361 | 636 | 2598 | 1120 | 957 | 2055 | 921 | 1581 | 3154 | 1328 | |
| | 0 | 322 | 324 | 81 | 1453 | 95 | 33 | 60 | 61 | 222 | 293 | 75 | |
| Grp Volume(v), veh/h | | | | | | | | | 1398 | 1581 | | 1328 | |
| Grp Sat Flow(s), veh/h/lr | | 1577 | 1582 | 636 | 1299 | 1120 | 957 | 1577 | | | 1577 | | |
| Q Serve(g_s), s | 0.0 | 0.0 | 0.0 | 6.2 | 53.6 | 3.9 | 2.8 | 3.1 | 3.5 | 6.9 | 6.9 | 4.0 | |
| Cycle Q Clear(g_c), s | 0.0 | 0.0 | 0.0 | 6.2 | 53.6 | 3.9 | 2.8 | 3.1 | 3.5 | 6.9 | 6.9 | 4.0 | |
| Prop In Lane | 0.00 | 044 | 0.23 | 1.00 | 4504 | 1.00 | 1.00 | 055 | 0.66 | 1.00 | 4000 | 1.00 | |
| Lane Grp Cap(c), veh/h | | 911 | 915 | 72 | 1501 | 647 | 287 | 355 | 315 | 407 | 1022 | 430 | |
| V/C Ratio(X) | 0.00 | 0.35 | 0.35 | 1.12 | 0.97 | 0.15 | 0.11 | 0.17 | 0.19 | 0.55 | 0.29 | 0.17 | |
| Avail Cap(c_a), veh/h | 0 | 911 | 914 | 440 | 1501 | 647 | 340 | 442 | 392 | 407 | 1196 | 503 | |
| HCM Platoon Ratio | 1.00 | 2.00 | 2.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Upstream Filter(I) | 0.00 | 0.90 | 0.90 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Uniform Delay (d), s/vel | | 0.0 | 0.0 | 50.0 | 21.0 | 9.7 | 31.1 | 31.2 | 31.4 | 29.6 | 25.2 | 24.2 | |
| Incr Delay (d2), s/veh | 0.0 | 1.0 | 1.0 | 144.1 | 16.7 | 0.5 | 0.2 | 0.2 | 0.3 | 0.9 | 0.2 | 0.2 | |
| Initial Q Delay(d3),s/veh | | 0.3 | 0.3 | 0.0 | 9.9 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | |
| %ile BackOfQ(50%),vel | | 0.3 | 0.3 | 4.7 | 21.5 | 1.0 | 0.7 | 1.2 | 1.2 | 1.8 | 2.6 | 1.3 | |
| Unsig. Movement Delay | , s/veh | | | | | | | | | | | | |
| LnGrp Delay(d),s/veh | 0.0 | 1.3 | 1.3 | 194.1 | 47.6 | 10.2 | 31.3 | 31.4 | 31.7 | 30.4 | 25.3 | 24.4 | |
| LnGrp LOS | Α | Α | Α | F | D | В | С | С | С | С | С | С | |
| Approach Vol, veh/h | | 646 | | | 1629 | | | 154 | | | 590 | | |
| Approach Delay, s/veh | | 1.3 | | | 52.7 | | | 31.5 | | | 27.1 | | |
| Approach LOS | | Α | | | D | | | С | | | С | | |
| Timer - Assigned Phs | | 2 | | 4 | | 6 | 7 | 8 | | | | | |
| Phs Duration (G+Y+Rc) | . S | 62.9 | | 37.1 | | 62.9 | 9.9 | 27.2 | | | | | |
| Change Period (Y+Rc), | | 5.1 | | * 4.7 | | 5.1 | 3.0 | * 4.7 | | | | | |
| Max Green Setting (Gm | | 52.3 | | * 38 | | 52.3 | 6.9 | * 28 | | | | | |
| Max Q Clear Time (g_c- | | 2.0 | | 8.9 | | 55.6 | 8.9 | 5.5 | | | | | |
| Green Ext Time (p_c), s | | 10.2 | | 2.4 | | 0.0 | 0.0 | 0.8 | | | | | |
| Intersection Summary | | 10.2 | | 2.7 | | 0.0 | 0.0 | 0.0 | | | | | |
| | | | 35.6 | | | | | | | | | | |
| HCM 6th Ctrl Delay | | | | | | | | | | | | | |
| HCM 6th LOS | | | D | | | | | | | | | | |
| Notes | | | | | | | | | | | | | |

^{*} HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

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|---------------------------|----------|-------|------------|------|------|-------|------|----------|------|------|-------------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | | | | 414 | | | ^ | | | † 1> | |
| Traffic Volume (veh/h) | 0 | 0 | 0 | 70 | 352 | 71 | 100 | 528 | 0 | 0 | 597 | 155 |
| Future Volume (veh/h) | 0 | 0 | 0 | 70 | 352 | 71 | 100 | 528 | 0 | 0 | 597 | 155 |
| Initial Q (Qb), veh | | | · | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | | | | 1.00 | v | 0.92 | 0.99 | | 1.00 | 1.00 | | 0.96 |
| Parking Bus, Adj | | | | 0.85 | 1.00 | 0.85 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.83 |
| Work Zone On Approac | h | | | 0.00 | No | 0.00 | 1.00 | No | 1.00 | 1.00 | No | 0.00 |
| Adj Sat Flow, veh/h/ln | /I I | | | 1367 | 1367 | 1367 | 1660 | 1660 | 0 | 0 | 1660 | 1660 |
| Adj Flow Rate, veh/h | | | | 75 | 378 | 52 | 108 | 568 | 0 | 0 | 642 | 130 |
| Peak Hour Factor | | | | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 |
| Percent Heavy Veh, % | | | | 3 | 3 | 3 | 3 | 3 | 0.55 | 0.55 | 3 | 3 |
| Cap, veh/h | | | | 107 | 565 | 81 | 360 | 1656 | 0 | 0 | 1243 | 251 |
| Arrive On Green | | | | 0.34 | 0.34 | 0.34 | 0.53 | 0.53 | 0.00 | 0.00 | 0.53 | 0.53 |
| Sat Flow, veh/h | | | | 318 | 1669 | 240 | 689 | 3237 | 0.00 | 0.00 | 2451 | 478 |
| | | | | | | | | | | | | |
| Grp Volume(v), veh/h | | | | 269 | 0 | 236 | 108 | 568 | 0 | 0 | 427 | 345 |
| Grp Sat Flow(s),veh/h/lr | n | | | 1139 | 0 | 1087 | 689 | 1577 | 0 | 0 | 1577 | 1269 |
| Q Serve(g_s), s | | | | 12.3 | 0.0 | 11.0 | 7.3 | 6.3 | 0.0 | 0.0 | 10.6 | 10.6 |
| Cycle Q Clear(g_c), s | | | | 12.3 | 0.0 | 11.0 | 17.9 | 6.3 | 0.0 | 0.0 | 10.6 | 10.6 |
| Prop In Lane | | | | 0.28 | • | 0.22 | 1.00 | 1050 | 0.00 | 0.00 | 000 | 0.38 |
| Lane Grp Cap(c), veh/h | | | | 385 | 0 | 368 | 360 | 1656 | 0 | 0 | 828 | 666 |
| V/C Ratio(X) | | | | 0.70 | 0.00 | 0.64 | 0.30 | 0.34 | 0.00 | 0.00 | 0.52 | 0.52 |
| Avail Cap(c_a), veh/h | | | | 490 | 0 | 468 | 360 | 1656 | 0 | 0 | 828 | 666 |
| HCM Platoon Ratio | | | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | | | | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 0.00 | 0.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/vel | h | | | 17.2 | 0.0 | 16.8 | 15.1 | 8.3 | 0.0 | 0.0 | 9.3 | 9.3 |
| Incr Delay (d2), s/veh | | | | 3.1 | 0.0 | 1.9 | 2.1 | 0.6 | 0.0 | 0.0 | 2.3 | 2.9 |
| Initial Q Delay(d3),s/veh | | | | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),vel | | | | 3.3 | 0.0 | 2.7 | 1.3 | 1.9 | 0.0 | 0.0 | 3.6 | 3.0 |
| Unsig. Movement Delay | /, s/veh | | | | | | | | | | | |
| LnGrp Delay(d),s/veh | | | | 20.3 | 0.0 | 18.7 | 17.3 | 8.8 | 0.0 | 0.0 | 11.6 | 12.2 |
| LnGrp LOS | | | | С | Α | В | В | Α | Α | Α | В | В |
| Approach Vol, veh/h | | | | | 505 | | | 676 | | | 772 | |
| Approach Delay, s/veh | | | | | 19.5 | | | 10.2 | | | 11.8 | |
| Approach LOS | | | | | В | | | В | | | В | |
| Timer - Assigned Phs | | 2 | | | | 6 | | 8 | | | | |
| Phs Duration (G+Y+Rc) |) s | 35.7 | | | | 35.7 | | 24.3 | | | | |
| Change Period (Y+Rc), | | * 4.2 | | | | * 4.2 | | 4.0 | | | | |
| Max Green Setting (Gm | | * 26 | | | | * 26 | | 25.8 | | | | |
| Max Q Clear Time (g_c | | 19.9 | | | | 12.6 | | 14.3 | | | | |
| Green Ext Time (p_c), s | | 3.4 | | | | 6.9 | | 2.5 | | | | |
| · | • | 3.4 | | | | 0.9 | | 2.0 | | | | |
| ntersection Summary | | | 40.0 | | | | | | | | | |
| HCM 6th Ctrl Delay | | | 13.3 | | | | | | | | | |
| HCM 6th LOS | | | В | | | | | | | | | |
| Notes | | | | | | | | | | | | |

^{*} HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

| Movement EBL EBT EBR WBL WBT WBR NBL NBT NBR SBL | | * |
|--|------------|------|
| | SBT | SBR |
| Lane Configurations 45 1 | ↑ ↑ | 02 |
| Traffic Volume (vph) 0 0 0 55 352 45 30 95 0 10 | 250 | 190 |
| Future Volume (vph) 0 0 0 55 352 45 30 95 0 10 | 250 | 190 |
| Ideal Flow (vphpl) 1700 1700 1700 1700 1700 1700 1700 170 | 1700 | 1700 |
| Total Lost time (s) 3.0 4.0 4.0 | 4.0 | |
| Lane Util. Factor 0.95 1.00 0.95 | 0.95 | |
| Frpb, ped/bikes 1.00 1.00 1.00 | 0.99 | |
| Flpb, ped/bikes 1.00 1.00 1.00 | 1.00 | |
| Frt 0.99 1.00 1.00 | 0.94 | |
| Fit Protected 0.99 0.95 1.00 | 1.00 | |
| Satd. Flow (prot) 2867 1568 2885 | 2692 | |
| Flt Permitted 0.99 0.25 1.00 | 0.95 | |
| Satd. Flow (perm) 2867 413 2885 | 2555 | |
| Peak-hour factor, PHF 0.70 0.70 0.70 0.70 0.70 0.70 0.70 0.7 | 0.70 | 0.70 |
| Adj. Flow (vph) 0 0 0 79 503 64 43 136 0 14 | 357 | 271 |
| RTOR Reduction (vph) 0 0 0 0 11 0 0 0 0 | 188 | 0 |
| Lane Group Flow (vph) 0 0 0 0 635 0 43 136 0 0 | 454 | 0 |
| Confl. Bikes (#/hr) 1 1 1 | | 1 |
| Heavy Vehicles (%) 3% 3% 3% 3% 3% 3% 3% 3% 3% 3% 3% | 3% | 3% |
| Parking (#/hr) 6 6 4 12 | 11 | 11 |
| Turn Type Perm NA Perm NA Perm | NA | |
| Protected Phases 6 8 | 4 | |
| Permitted Phases 6 8 4 | • | |
| Actuated Green, G (s) 23.0 16.0 16.0 | 16.0 | |
| Effective Green, g (s) 23.0 16.0 | 16.0 | |
| Actuated g/C Ratio 0.33 0.23 0.23 | 0.23 | |
| Clearance Time (s) 3.0 4.0 4.0 | 4.0 | |
| Vehicle Extension (s) 2.0 2.0 2.0 | 2.0 | |
| Lane Grp Cap (vph) 942 94 659 | 584 | |
| v/s Ratio Prot 0.05 | 00. | |
| v/s Ratio Perm 0.22 0.10 | c0.18 | |
| v/c Ratio 0.67 0.46 0.21 | 0.78 | |
| Uniform Delay, d1 20.3 23.3 21.9 | 25.3 | |
| Progression Factor 1.00 1.00 1.00 | 1.00 | |
| Incremental Delay, d2 3.8 15.2 0.7 | 9.8 | |
| Delay (s) 24.1 38.5 22.6 | 35.1 | |
| Level of Service C D C | D | |
| Approach Delay (s) 0.0 24.1 26.4 | 35.1 | |
| Approach LOS A C C | D | |
| Intersection Summary | | |
| HCM 2000 Control Delay 29.2 HCM 2000 Level of Service C | | |
| HCM 2000 Volume to Capacity ratio 0.47 | | |
| Actuated Cycle Length (s) 70.0 Sum of lost time (s) 11.0 | | |
| Intersection Capacity Utilization 47.5% ICU Level of Service A | | |
| Analysis Period (min) 15 | | |
| c Critical Lane Group | | |

| Intersection | | | | | | |
|-------------------------------------|------------|-------|---------|-------------|-------------|-------------|
| Int Delay, s/veh | 0.1 | | | | | |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | LUL | | NDL | <u>₩</u> | ↑ ↑ | ODIX |
| Traffic Vol. veh/h | 0 | 0 | 14 | 524 | 673 | 137 |
| Future Vol, veh/h | 0 | 0 | 14 | 524 | 673 | 137 |
| Conflicting Peds, #/hr | 0 | 0 | 46 | 0 | 0/3 | 46 |
| | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | olop - | None | - | None | - | None |
| Storage Length | _ | 0 | 25 | - | - | NONE |
| Veh in Median Storage, # | | - | 25 | 0 | 0 | _ |
| Grade, % | <i>+</i> 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 94 | 94 | 94 | 94 | 94 | 94 |
| | | 3 | 3 | 3 | 3 | 3 |
| Heavy Vehicles, % | 3 | | | | | |
| Mvmt Flow | 0 | 0 | 15 | 557 | 716 | 146 |
| | | | | | | |
| Major/Minor Mir | nor2 | N | //ajor1 | N | /lajor2 | |
| Conflicting Flow All | _ | 477 | 908 | 0 | | 0 |
| Stage 1 | _ | _ | _ | _ | _ | _ |
| Stage 2 | _ | _ | _ | _ | _ | _ |
| Critical Hdwy | _ | 6.96 | 4.16 | _ | _ | _ |
| Critical Hdwy Stg 1 | _ | - | - | _ | _ | _ |
| Critical Hdwy Stg 2 | _ | _ | _ | - | _ | _ |
| Follow-up Hdwy | _ | 3.33 | 2.23 | _ | _ | _ |
| Pot Cap-1 Maneuver | 0 | 532 | 739 | _ | _ | _ |
| Stage 1 | 0 | - 502 | 100 | _ | <u>-</u> | _ |
| Stage 2 | 0 | _ | | | _ | |
| Platoon blocked, % | U | _ | _ | _ | _ | _ |
| Mov Cap-1 Maneuver | | 509 | 707 | - | - | - |
| | - | 509 | | | | - |
| Mov Cap-2 Maneuver | - | - | - | - | - | - |
| Stage 1 | - | - | - | - | - | - |
| Stage 2 | - | - | - | - | - | - |
| | | | | | | |
| Approach | EB | | NB | | SB | |
| HCM Control Delay, s | 0 | | 0.3 | | 0 | |
| HCM LOS | A | | 0.0 | | • | |
| 110M 200 | ,, | | | | | |
| | | | | | | |
| | | NBL | NBT | EBLn1 | SBT | SBR |
| Minor Lane/Major Mvmt | | | | | | |
| Capacity (veh/h) | | 707 | - | - | - | - |
| | | 0.021 | - | - | - | - |
| Capacity (veh/h) | | | | - - 0 | - - - | - - - |
| Capacity (veh/h) HCM Lane V/C Ratio | | 0.021 | - | | | |

| Intersection | | | | | | | | | | | | |
|------------------------|-------|------|------|---------|-------|------|------|-------|------|---------|------|--------|
| Int Delay, s/veh | 2.6 | | | | | | | | | | | |
| | | | | | | | | | | | | |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | | | | 41 | | | | | | ΦÞ | |
| Traffic Vol, veh/h | 0 | 0 | 0 | 0 | 338 | 0 | 0 | 0 | 0 | 0 | 0 | 114 |
| Future Vol, veh/h | 0 | 0 | 0 | 0 | 338 | 0 | 0 | 0 | 0 | 0 | 0 | 114 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 79 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | - | - | - | - | - | - | - | - | - | - |
| Veh in Median Storage, | , # - | 2 | - | - | 0 | - | - | 16974 | - | - | 0 | - |
| Grade, % | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 82 | 82 | 82 | 82 | 82 | 82 | 82 | 82 | 82 | 82 | 82 | 82 |
| Heavy Vehicles, % | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 |
| Mvmt Flow | 0 | 0 | 0 | 0 | 412 | 0 | 0 | 0 | 0 | 0 | 0 | 139 |
| | | | | | | | | | | | | |
| Major/Minor | | | | Major2 | | | | | | /linor2 | | |
| Major/Minor | | | | | ^ | ^ | | | | | 404 | 2000 |
| Conflicting Flow All | | | | 79 | 0 | 0 | | | | - | 491 | 206 |
| Stage 1 | | | | - | - | - | | | | - | 412 | - |
| Stage 2 | | | | 4.40 | - | - | | | | - | 79 | - 0.00 |
| Critical Hdwy | | | | 4.16 | - | - | | | | - | 6.56 | 6.96 |
| Critical Hdwy Stg 1 | | | | - | - | - | | | | - | 5.56 | - |
| Critical Hdwy Stg 2 | | | | - | - | - | | | | - | - | - |
| Follow-up Hdwy | | | | 2.23 | - | - | | | | - | 4.03 | 3.33 |
| Pot Cap-1 Maneuver | | | | 1510 | - | 0 | | | | 0 | 475 | 797 |
| Stage 1 | | | | - | - | 0 | | | | 0 | 590 | - |
| Stage 2 | | | | - | - | 0 | | | | 0 | - | - |
| Platoon blocked, % | | | | 4=:- | - | | | | | | | |
| Mov Cap-1 Maneuver | | | | 1510 | - | - | | | | - | 0 | 797 |
| Mov Cap-2 Maneuver | | | | - | - | - | | | | - | 0 | - |
| Stage 1 | | | | - | - | - | | | | - | 0 | - |
| Stage 2 | | | | - | - | - | | | | - | 0 | - |
| | | | | | | | | | | | | |
| Approach | | | | WB | | | | | | SB | | |
| HCM Control Delay, s | | | | 0 | | | | | | 10.5 | | |
| HCM LOS | | | | | | | | | | В | | |
| | | | | | | | | | | | | |
| Minor Long/Maior M | | WDI | WDT | CDL 4 (| CDL O | | | | | | | |
| Minor Lane/Major Mvm | l e | WBL | WBI | SBLn1 | | | | | | | | |
| Capacity (veh/h) | | 1510 | - | - | 797 | | | | | | | |
| HCM Lane V/C Ratio | | - | - | | 0.174 | | | | | | | |
| HCM Control Delay (s) | | 0 | - | 0 | 10.5 | | | | | | | |
| HCM Lane LOS | | Α | - | Α | В | | | | | | | |
| HCM 95th %tile Q(veh) | | 0 | - | - | 0.6 | | | | | | | |

| Intersection | | | | | | |
|---------------------------------------|----------|-------|--------|-------|--------|--------|
| Int Delay, s/veh | 3.4 | | | | | |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | † | בטוע | TTDL | 41 | TIDE | TVDIX |
| Traffic Vol, veh/h | 767 | 29 | 31 | 1580 | 0 | 79 |
| Future Vol, veh/h | 767 | 29 | 31 | 1580 | 0 | 79 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | | - | None |
| Storage Length | _ | - | _ | - | _ | 0 |
| Veh in Median Storage, | # 0 | _ | _ | 0 | 0 | - |
| Grade, % | 0 | _ | _ | 0 | 0 | _ |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 |
| Mymt Flow | 834 | 32 | 34 | 1717 | 0 | 86 |
| WWW.CT IOW | 001 | 02 | 01 | ., ., | | - 00 |
| | | | | | | |
| | /lajor1 | | Major2 | | Minor1 | |
| Conflicting Flow All | 0 | 0 | 866 | 0 | - | 433 |
| Stage 1 | - | - | - | - | - | - |
| Stage 2 | - | - | - | - | - | - |
| Critical Hdwy | - | - | 4.14 | - | - | 6.94 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - |
| Critical Hdwy Stg 2 | - | - | - | - | - | - |
| Follow-up Hdwy | - | - | 2.22 | - | - | 3.32 |
| Pot Cap-1 Maneuver | - | - | 773 | - | 0 | 571 |
| Stage 1 | - | - | - | - | 0 | - |
| Stage 2 | - | - | - | - | 0 | - |
| Platoon blocked, % | - | - | | - | | |
| Mov Cap-1 Maneuver | - | - | 773 | - | - | 571 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - |
| Stage 1 | - | - | - | - | - | - |
| Stage 2 | - | - | - | - | - | - |
| J. H. G. | | | | | | |
| A | ED | | WD | | ND | |
| Approach | EB | | WB | | NB | |
| HCM Control Delay, s | 0 | | 4.6 | | 12.4 | |
| HCM LOS | | | | | В | |
| | | | | | | |
| Minor Lane/Major Mvmt | t 1 | NBLn1 | EBT | EBR | WBL | WBT |
| Capacity (veh/h) | | 571 | _ | _ | 773 | _ |
| HCM Lane V/C Ratio | | 0.15 | _ | | 0.044 | _ |
| HCM Control Delay (s) | | 12.4 | _ | _ | 9.9 | 4.5 |
| | | | | | | Α. |
| HCM Lane LOS | | В | - | - | А | A |
| HCM Lane LOS HCM 95th %tile Q(veh) | | 0.5 | - | - | 0.1 | - - |

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|------------------------------|------|------------|-------|-------|------------|------|------|------------|----------|----------|----------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | Ŋ | ∱ ⊅ | | Ť | ∱ ∱ | | | ∱ ∱ | | 7 | ^ | 7 |
| Traffic Volume (veh/h) | 40 | 1843 | 62 | 80 | 1714 | 63 | 0 | 240 | 61 | 41 | 173 | 50 |
| Future Volume (veh/h) | 40 | 1843 | 62 | 80 | 1714 | 63 | 0 | 240 | 61 | 41 | 173 | 50 |
| Initial Q (Qb), veh | 0 | 15 | 0 | 0 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | | 0.97 | 1.00 | | 0.97 | 1.00 | | 0.97 | 0.99 | | 0.89 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach | | No | | | No | | | No | | | No | |
| Adj Sat Flow, veh/h/ln | 1367 | 1367 | 1367 | 1367 | 1367 | 1367 | 0 | 1660 | 1660 | 1660 | 1660 | 1660 |
| Adj Flow Rate, veh/h | 44 | 2048 | 66 | 89 | 1904 | 67 | 0 | 267 | 60 | 46 | 192 | 37 |
| Peak Hour Factor | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Percent Heavy Veh, % | 3 | 3 | 3 | 3 | 3 | 3 | 0 | 3 | 3 | 3 | 3 | 3 |
| Cap, veh/h | 72 | 1739 | 32 | 72 | 1738 | 32 | 0 | 599 | 132 | 219 | 739 | 295 |
| Arrive On Green | 0.67 | 0.67 | 0.67 | 0.67 | 0.67 | 0.67 | 0.00 | 0.23 | 0.23 | 0.23 | 0.23 | 0.23 |
| Sat Flow, veh/h | 181 | 2566 | 82 | 157 | 2558 | 89 | 0 | 2638 | 563 | 1030 | 3154 | 1258 |
| Grp Volume(v), veh/h | 44 | 1030 | 1084 | 89 | 960 | 1011 | 0 | 163 | 164 | 46 | 192 | 37 |
| Grp Sat Flow(s),veh/h/ln | 181 | 1299 | 1350 | 157 | 1299 | 1348 | 0 | 1577 | 1541 | 1030 | 1577 | 1258 |
| Q Serve(g_s), s | 0.0 | 66.7 | 66.7 | 0.0 | 66.7 | 66.7 | 0.0 | 8.8 | 9.1 | 4.0 | 5.0 | 2.3 |
| Cycle Q Clear(g_c), s | 66.7 | 66.7 | 66.7 | 66.7 | 66.7 | 66.7 | 0.0 | 8.8 | 9.1 | 13.1 | 5.0 | 2.3 |
| Prop In Lane | 1.00 | | 0.06 | 1.00 | | 0.07 | 0.00 | | 0.37 | 1.00 | | 1.00 |
| Lane Grp Cap(c), veh/h | 72 | 866 | 905 | 72 | 866 | 905 | 0 | 370 | 361 | 219 | 739 | 295 |
| V/C Ratio(X) | 0.61 | 1.19 | 1.20 | 1.24 | 1.11 | 1.12 | 0.00 | 0.44 | 0.45 | 0.21 | 0.26 | 0.13 |
| Avail Cap(c_a), veh/h | 72 | 866 | 900 | 72 | 866 | 899 | 0 | 420 | 410 | 252 | 839 | 335 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 0.09 | 0.09 | 0.09 | 0.00 | 0.77 | 0.77 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 50.0 | 16.7 | 16.7 | 50.0 | 16.7 | 16.7 | 0.0 | 32.7 | 32.8 | 38.4 | 31.2 | 30.2 |
| Incr Delay (d2), s/veh | 33.0 | 96.8 | 100.0 | 117.0 | 50.9 | 54.5 | 0.0 | 0.6 | 0.7 | 0.5 | 0.2 | 0.2 |
| Initial Q Delay(d3),s/veh | 0.0 | 31.2 | 29.8 | 0.0 | 20.8 | 19.9 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/ln | 1.7 | 46.8 | 49.3 | 4.1 | 33.2 | 35.4 | 0.0 | 3.4 | 3.5 | 1.0 | 1.9 | 0.7 |
| Unsig. Movement Delay, s/veh | | | | | | | | | | | | |
| LnGrp Delay(d),s/veh | 83.0 | 144.6 | 146.5 | 167.0 | 88.4 | 91.1 | 0.0 | 33.3 | 33.5 | 38.9 | 31.4 | 30.4 |
| LnGrp LOS | F | F | F | F | F | F | Α | С | С | D | С | С |
| Approach Vol, veh/h | | 2158 | | | 2060 | | | 327 | | | 275 | |
| Approach Delay, s/veh | | 144.3 | | | 93.1 | | | 33.4 | | | 32.5 | |
| Approach LOS | | F | | | F | | | С | | | С | |
| Timer - Assigned Phs | | 2 | | 4 | | 6 | | 8 | | | | |
| Phs Duration (G+Y+Rc), s | | 72.1 | | 27.9 | | 72.1 | | 27.9 | | | | |
| Change Period (Y+Rc), s | | 5.4 | | 4.5 | | 5.4 | | 4.5 | | | | |
| Max Green Setting (Gmax), s | | 63.5 | | 26.6 | | 63.5 | | 26.6 | | | | |
| Max Q Clear Time (g_c+l1), s | | 68.7 | | 15.1 | | 68.7 | | 11.1 | | | | |
| Green Ext Time (p_c), s | | 0.0 | | 1.2 | | 0.0 | | 1.7 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 6th Ctrl Delay | | | 108.5 | | | | | | | | | |
| HCM 6th LOS | | | F | | | | | | | | | |

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|---------------------------|------|----------|-------|-------|------------|----------|------|------------|----------|----------|-------------|------|--|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR | |
| Lane Configurations | ķ | ħβ | | ¥ | ∱ } | | ¥ | ↑ ↑ | | ķ | ↑ 1> | | |
| Traffic Volume (veh/h) | 50 | 1681 | 44 | 105 | 1660 | 50 | 96 | 447 | 179 | 40 | 380 | 70 | |
| Future Volume (veh/h) | 50 | 1681 | 44 | 105 | 1660 | 50 | 96 | 447 | 179 | 40 | 380 | 70 | |
| Initial Q (Qb), veh | 0 | 15 | 0 | 0 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Ped-Bike Adj(A_pbT) | 1.00 | | 0.97 | 1.00 | | 0.98 | 0.99 | | 0.97 | 1.00 | | 0.97 | |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Work Zone On Approac | | No | | | No | | | No | | | No | | |
| • | 1367 | 1367 | 1367 | 1367 | 1367 | 1367 | 1660 | 1660 | 1660 | 1660 | 1660 | 1660 | |
| Adj Flow Rate, veh/h | 56 | 1868 | 47 | 117 | 1844 | 54 | 107 | 497 | 186 | 44 | 422 | 65 | |
| Peak Hour Factor | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | |
| Percent Heavy Veh, % | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | |
| Cap, veh/h | 72 | 1643 | 21 | 72 | 1640 | 25 | 189 | 593 | 221 | 129 | 726 | 111 | |
| Arrive On Green | 0.63 | 0.63 | 0.63 | 0.63 | 0.63 | 0.63 | 0.53 | 0.53 | 0.53 | 0.27 | 0.27 | 0.27 | |
| Sat Flow, veh/h | 194 | 2587 | 65 | 191 | 2576 | 75 | 893 | 2231 | 829 | 748 | 2731 | 417 | |
| Grp Volume(v), veh/h | 56 | 933 | 982 | 117 | 925 | 973 | 107 | 350 | 333 | 44 | 242 | 245 | |
| Grp Sat Flow(s), veh/h/lr | | 1299 | 1353 | 191 | 1299 | 1352 | 893 | 1577 | 1483 | 748 | 1577 | 1571 | |
| Q Serve(g_s), s | 0.0 | 62.6 | 62.6 | 0.0 | 62.6 | 62.6 | 11.6 | 18.7 | 19.0 | 5.8 | 13.3 | 13.5 | |
| Cycle Q Clear(g_c), s | 62.6 | 62.6 | 62.6 | 62.6 | 62.6 | 62.6 | 25.2 | 18.7 | 19.0 | 24.8 | 13.3 | 13.5 | |
| Prop In Lane | 1.00 | | 0.05 | 1.00 | | 0.06 | 1.00 | | 0.56 | 1.00 | | 0.27 | |
| Lane Grp Cap(c), veh/h | 72 | 813 | 851 | 72 | 813 | 851 | 189 | 420 | 394 | 129 | 420 | 418 | |
| V/C Ratio(X) | 0.78 | 1.15 | 1.15 | 1.62 | 1.14 | 1.14 | 0.57 | 0.84 | 0.84 | 0.34 | 0.58 | 0.59 | |
| Avail Cap(c_a), veh/h | 72 | 813 | 847 | 72 | 813 | 846 | 189 | 420 | 394 | 129 | 420 | 418 | |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 2.00 | 2.00 | 2.00 | 1.00 | 1.00 | 1.00 | |
| Upstream Filter(I) | 0.09 | 0.09 | 0.09 | 1.00 | 1.00 | 1.00 | 0.61 | 0.61 | 0.61 | 1.00 | 1.00 | 1.00 | |
| Uniform Delay (d), s/veh | | 18.7 | 18.7 | 50.0 | 18.7 | 18.7 | 29.6 | 21.6 | 21.6 | 45.4 | 31.8 | 31.9 | |
| Incr Delay (d2), s/veh | 7.3 | 68.0 | 70.4 | 335.7 | 76.8 | 78.3 | 2.4 | 8.8 | 9.9 | 1.6 | 2.0 | 2.1 | |
| Initial Q Delay(d3),s/veh | | 33.2 | 31.7 | 0.0 | 22.1 | 21.2 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | |
| %ile BackOfQ(50%),veh | | 38.7 | 40.7 | 8.5 | 38.2 | 40.1 | 2.3 | 5.9 | 5.7 | 1.1 | 5.3 | 5.4 | |
| Unsig. Movement Delay | | | | | | | | | | | | | |
| LnGrp Delay(d),s/veh | 57.3 | 119.9 | 120.8 | 385.7 | 117.6 | 118.2 | 32.1 | 30.4 | 31.5 | 47.0 | 33.8 | 34.0 | |
| LnGrp LOS | E | F | F | F | F | <u> </u> | С | С | С | D | С | С | |
| Approach Vol, veh/h | | 1971 | | | 2015 | | | 790 | | | 531 | | |
| Approach Delay, s/veh | | 118.6 | | | 133.5 | | | 31.1 | | | 35.0 | | |
| Approach LOS | | F | | | F | | | С | | | С | | |
| Timer - Assigned Phs | | 2 | | 4 | | 6 | | 8 | | | | | |
| Phs Duration (G+Y+Rc) | , S | 68.0 | | 32.0 | | 68.0 | | 32.0 | | | | | |
| Change Period (Y+Rc), | | 5.4 | | 5.4 | | 5.4 | | 5.4 | | | | | |
| Max Green Setting (Gm | | 62.6 | | 26.6 | | 62.6 | | 26.6 | | | | | |
| Max Q Clear Time (g_c- | | | | 26.8 | | 64.6 | | 27.2 | | | | | |
| Green Ext Time (p_c), s | | 0.0 | | 0.0 | | 0.0 | | 0.0 | | | | | |
| Intersection Summary | | | | | | | | | | | | | |
| HCM 6th Ctrl Delay | | | 102.8 | | | | | | | | | | |
| HCM 6th LOS | | | F | | | | | | | | | | |

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|-----------------------------------|--------|------------|--------|-----------|------------|------------|---------|-------------|-------------|----------|-------------|----------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | ↑ Ъ | | | 414 | | ሻ | ↑ 1> | | * | ↑ 1> | |
| Traffic Volume (vph) | 0 | 1449 | 100 | 100 | 830 | 50 | 52 | 251 | 111 | 65 | 200 | 60 |
| Future Volume (vph) | 0 | 1449 | 100 | 100 | 830 | 50 | 52 | 251 | 111 | 65 | 200 | 60 |
| Ideal Flow (vphpl) | 1400 | 1400 | 1400 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 |
| Total Lost time (s) | | 5.1 | | | 5.1 | | 4.5 | 4.5 | | 4.5 | 4.5 | |
| Lane Util. Factor | | 0.95 | | | 0.95 | | 1.00 | 0.95 | | 1.00 | 0.95 | |
| Frpb, ped/bikes | | 0.98 | | | 0.98 | | 1.00 | 0.91 | | 1.00 | 0.93 | |
| Flpb, ped/bikes | | 1.00 | | | 1.00 | | 0.80 | 1.00 | | 0.85 | 1.00 | |
| Frt | | 0.99 | | | 0.99 | | 1.00 | 0.95 | | 1.00 | 0.97 | |
| Flt Protected | | 1.00 | | | 0.99 | | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | | 2515 | | | 3038 | | 1248 | 2537 | | 1338 | 2805 | |
| Flt Permitted | | 1.00 | | | 0.54 | | 0.53 | 1.00 | | 0.41 | 1.00 | |
| Satd. Flow (perm) | | 2515 | | | 1651 | | 694 | 2537 | | 577 | 2805 | |
| Peak-hour factor, PHF | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Adj. Flow (vph) | 0.93 | 1525 | 105 | 105 | 874 | 53 | 55 | 264 | 117 | 68 | 211 | 63 |
| RTOR Reduction (vph) | 0 | 4 | 0 | 0 | 4 | 0 | 0 | 51 | 0 | 00 | 26 | 0 |
| Lane Group Flow (vph) | 0 | 1626 | 0 | 0 | 1028 | 0 | 55 | 330 | 0 | 68 | 248 | 0 |
| Confl. Peds. (#/hr) | 423 | 1020 | 174 | 174 | 1020 | 423 | 282 | 330 | 215 | 215 | 240 | 282 |
| | 423 | | 6 | 1/4 | | | 202 | | | 213 | | 202 |
| Confl. Bikes (#/hr) | 3% | 3% | 3% | 3% | 3% | 1 3% | 3% | 3% | 1 3% | 3% | 3% | 3% |
| Heavy Vehicles (%) | 3% | 3% | 3% | 370 | 3% | 3% | 3% | 3% 8 | 3% 8 | 3% | 3% | 3% |
| Parking (#/hr) | | N 1 A | | | NIA. | | | | 0 | _ | N.1.A | |
| Turn Type | | NA | | pm+pt | NA | | Perm | NA | | Perm | NA | |
| Protected Phases | | 2 | | 1 | 6 | | • | 8 | | | 4 | |
| Permitted Phases | | 50.5 | | 6 | 07.0 | | 8 | 00.0 | | 4 | 00.0 | |
| Actuated Green, G (s) | | 59.5 | | | 67.2 | | 23.2 | 23.2 | | 23.2 | 23.2 | |
| Effective Green, g (s) | | 59.5 | | | 67.2 | | 23.2 | 23.2 | | 23.2 | 23.2 | |
| Actuated g/C Ratio | | 0.60 | | | 0.67 | | 0.23 | 0.23 | | 0.23 | 0.23 | |
| Clearance Time (s) | | 5.1 | | | 5.1 | | 4.5 | 4.5 | | 4.5 | 4.5 | |
| Vehicle Extension (s) | | 5.0 | | | 5.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | | 1496 | | | 1171 | | 161 | 588 | | 133 | 650 | |
| v/s Ratio Prot | | c0.65 | | | c0.04 | | | c0.13 | | | 0.09 | |
| v/s Ratio Perm | | | | | 0.55 | | 0.08 | | | 0.12 | | |
| v/c Ratio | | 1.09 | | | 0.92dl | | 0.34 | 0.56 | | 0.51 | 0.38 | |
| Uniform Delay, d1 | | 20.2 | | | 13.1 | | 32.0 | 33.9 | | 33.5 | 32.4 | |
| Progression Factor | | 1.00 | | | 0.88 | | 1.00 | 1.00 | | 0.62 | 0.53 | |
| Incremental Delay, d2 | | 50.6 | | | 6.5 | | 1.3 | 1.2 | | 1.9 | 0.2 | |
| Delay (s) | | 70.8 | | | 18.1 | | 33.3 | 35.1 | | 22.6 | 17.5 | |
| Level of Service | | Е | | | В | | С | D | | С | В | |
| Approach Delay (s) | | 70.8 | | | 18.1 | | | 34.9 | | | 18.5 | |
| Approach LOS | | Е | | | В | | | С | | | В | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 45.3 | Н | CM 2000 | Level of | Service | | D | | | |
| HCM 2000 Volume to Capacity | ratio | | 0.94 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 100.0 | S | um of lost | t time (s) | | | 12.8 | | | |
| Intersection Capacity Utilization | | | 129.6% | | CU Level | | ! | | Н | | | |
| Analysis Period (min) | | | 15 | | 2 = 3.51 | | | | | | | |
| dl Defacto Left Lane. Recode | with 1 | though la | | eft lane. | | | | | | | | |
| c Critical Lane Group | | | 2.5 3 | | | | | | | | | |
| 5 Sillious Lario Oroup | | | | | | | | | | | | |

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|---------------------------|-------|------------|---------------|-------|----------|------|------|----------|------|----------|------------|--------------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ሻ | † ‡ | | ሻ | † | | ሻ | ^ | 7 | <u> </u> | ↑ ↑ | 02. (|
| Traffic Volume (veh/h) | 172 | 1310 | 306 | 110 | 849 | 50 | 94 | 530 | 170 | 0 | 459 | 90 |
| Future Volume (veh/h) | 172 | 1310 | 306 | 110 | 849 | 50 | 94 | 530 | 170 | 0 | 459 | 90 |
| Initial Q (Qb), veh | 0 | 10 | 0 | 0 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 0.98 | 10 | 0.90 | 1.00 | 10 | 0.90 | 0.96 | U | 0.82 | 1.00 | U | 0.83 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approac | | No | 1.00 | 1.00 | No | 1.00 | 1.00 | No | 1.00 | 1.00 | No | 1.00 |
| Adj Sat Flow, veh/h/ln | 1367 | 1367 | 1367 | 1660 | 1660 | 1660 | 1660 | 1660 | 1660 | 0 | 1660 | 1660 |
| Adj Flow Rate, veh/h | 181 | 1379 | 315 | 116 | 894 | 49 | 99 | 558 | 160 | 0 | 483 | 78 |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Percent Heavy Veh, % | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 0.93 | 3 | 3 |
| Cap, veh/h | 73 | 1636 | 330 | 72 | 2345 | 126 | 145 | 817 | 299 | 0 | 683 | 109 |
| | | | | | | | | | | | 0.26 | |
| Arrive On Green | 0.77 | 0.77 | 0.77 | 1.00 | 1.00 | 1.00 | 0.26 | 0.26 | 0.26 | 0.00 | | 0.26 |
| Sat Flow, veh/h | 475 | 2070 | 456 | 288 | 3021 | 166 | 808 | 3154 | 1156 | 0 | 2721 | 421 |
| Grp Volume(v), veh/h | 181 | 847 | 847 | 116 | 467 | 476 | 99 | 558 | 160 | 0 | 286 | 275 |
| Grp Sat Flow(s),veh/h/li | | 1299 | 1227 | 288 | 1577 | 1610 | 808 | 1577 | 1156 | 0 | 1577 | 1482 |
| Q Serve(g_s), s | 14.1 | 42.1 | 50.2 | 25.0 | 0.0 | 0.0 | 9.1 | 15.9 | 11.9 | 0.0 | 16.4 | 16.8 |
| Cycle Q Clear(g_c), s | 14.5 | 42.1 | 50.2 | 77.5 | 0.0 | 0.0 | 25.9 | 15.9 | 11.9 | 0.0 | 16.4 | 16.8 |
| Prop In Lane | 1.00 | | 0.37 | 1.00 | | 0.10 | 1.00 | | 1.00 | 0.00 | | 0.28 |
| Lane Grp Cap(c), veh/h | | 1007 | 958 | 72 | 1222 | 1248 | 145 | 817 | 299 | 0 | 408 | 384 |
| V/C Ratio(X) | 2.49 | 0.84 | 0.88 | 1.61 | 0.38 | 0.38 | 0.68 | 0.68 | 0.53 | 0.00 | 0.70 | 0.72 |
| Avail Cap(c_a), veh/h | 438 | 1007 | 951 | 144 | 1222 | 1247 | 145 | 817 | 299 | 0 | 408 | 384 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 2.00 | 2.00 | 2.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 0.85 | 0.85 | 0.85 | 1.00 | 1.00 | 1.00 | 0.00 | 0.28 | 0.28 |
| Uniform Delay (d), s/ve | | 7.8 | 8.6 | 38.7 | 0.0 | 0.0 | 46.7 | 33.4 | 31.9 | 0.0 | 33.5 | 33.7 |
| Incr Delay (d2), s/veh | 710.3 | 8.5 | 11.7 | 321.5 | 8.0 | 0.8 | 12.3 | 2.3 | 1.8 | 0.0 | 1.5 | 1.8 |
| Initial Q Delay(d3),s/vel | h 0.0 | 1.1 | 1.7 | 0.0 | 0.2 | 0.2 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),vel | | 12.4 | 14.2 | 8.2 | 0.3 | 0.3 | 3.0 | 6.3 | 3.5 | 0.0 | 6.4 | 6.2 |
| Unsig. Movement Delay | | | | | | | | | | | | |
| LnGrp Delay(d),s/veh | | 17.3 | 22.0 | 360.3 | 1.0 | 0.9 | 58.9 | 35.7 | 33.7 | 0.0 | 35.1 | 35.5 |
| LnGrp LOS | F | В | С | F | Α | Α | Е | D | С | Α | D | D |
| Approach Vol, veh/h | | 1875 | | | 1059 | | | 817 | | | 561 | |
| Approach Delay, s/veh | | 91.1 | | | 40.3 | | | 38.1 | | | 35.3 | |
| Approach LOS | | F | | | D | | | D | | | D | |
| •• | | | | 1 | | C | | | | | | |
| Timer - Assigned Phs | \ - | 2 | | 4 | | 6 | | 8 | | | | |
| Phs Duration (G+Y+Rc) | | 83.0 | | 31.0 | | 83.0 | | 31.0 | | | | |
| Change Period (Y+Rc), | | 5.1 | | * 5.1 | | 5.1 | | 5.1 | | | | |
| Max Green Setting (Gm | | 64.3 | | * 26 | | 64.3 | | 25.5 | | | | |
| Max Q Clear Time (g_c | , . | 52.2 | | 27.9 | | 79.5 | | 18.8 | | | | |
| Green Ext Time (p_c), s | S | 11.5 | | 0.0 | | 0.0 | | 2.0 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 6th Ctrl Delay | | | 61.3 | | | | | | | | | |
| HCM 6th LOS | | | Е | | | | | | | | | |
| Notes | | | | | | | | | | | | |

^{*} HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

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|---------------------------|---------|-----------|------------|-------|----------|------|------|----------|------|----------|----------|------|--|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR | |
| Lane Configurations | | ħβ | | ች | ^ | 7 | ሻ | ħβ | | ች | ^ | 1 | |
| Traffic Volume (veh/h) | 0 | 1225 | 125 | 80 | 962 | 280 | 57 | 250 | 90 | 200 | 200 | 40 | |
| Future Volume (veh/h) | 0 | 1225 | 125 | 80 | 962 | 280 | 57 | 250 | 90 | 200 | 200 | 40 | |
| Initial Q (Qb), veh | 0 | 10 | 0 | 0 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Ped-Bike Adj(A_pbT) | 1.00 | | 0.95 | 0.99 | | 0.95 | 0.92 | • | 0.89 | 0.95 | | 0.92 | |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Work Zone On Approac | | No | 1.00 | 1.00 | No | 1.00 | 1.00 | No | 1.00 | 1.00 | No | 1.00 | |
| Adj Sat Flow, veh/h/ln | 0 | 1367 | 1367 | 1660 | 1660 | 1660 | 1660 | 1660 | 1660 | 1660 | 1660 | 1660 | |
| Adj Flow Rate, veh/h | 0 | 1263 | 122 | 82 | 992 | 194 | 59 | 258 | 93 | 206 | 206 | 13 | |
| Peak Hour Factor | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | |
| Percent Heavy Veh, % | 0.57 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | |
| Cap, veh/h | 0 | 1379 | 90 | 72 | 1739 | 738 | 339 | 559 | 193 | 326 | 1107 | 454 | |
| Arrive On Green | 0.00 | 1.00 | 1.00 | 0.55 | 0.55 | 0.55 | 0.25 | 0.25 | 0.25 | 0.07 | 0.35 | 0.35 | |
| Sat Flow, veh/h | 0.00 | 2450 | 229 | 386 | 3154 | 1339 | 1059 | 2221 | 766 | 1581 | 3154 | 1295 | |
| | | | | | | | | | | | | | |
| Grp Volume(v), veh/h | 0 | 687 | 698 | 82 | 992 | 194 | 59 | 180 | 171 | 206 | 206 | 13 | |
| Grp Sat Flow(s),veh/h/lr | | 1299 | 1312 | 386 | 1577 | 1339 | 1059 | 1577 | 1410 | 1581 | 1577 | 1295 | |
| Q Serve(g_s), s | 0.0 | 0.0 | 0.0 | 12.1 | 20.6 | 7.6 | 4.4 | 9.6 | 10.3 | 6.9 | 4.5 | 0.7 | |
| Cycle Q Clear(g_c), s | 0.0 | 0.0 | 0.0 | 12.1 | 20.6 | 7.6 | 4.4 | 9.6 | 10.3 | 6.9 | 4.5 | 0.7 | |
| Prop In Lane | 0.00 | = 10 | 0.17 | 1.00 | 4=00 | 1.00 | 1.00 | | 0.54 | 1.00 | 440= | 1.00 | |
| Lane Grp Cap(c), veh/h | | 716 | 732 | 72 | 1739 | 738 | 339 | 397 | 355 | 326 | 1107 | 454 | |
| V/C Ratio(X) | 0.00 | 0.96 | 0.95 | 1.14 | 0.57 | 0.26 | 0.17 | 0.45 | 0.48 | 0.63 | 0.19 | 0.03 | |
| Avail Cap(c_a), veh/h | 0 | 716 | 723 | 285 | 1739 | 738 | 368 | 442 | 395 | 326 | 1196 | 491 | |
| HCM Platoon Ratio | 1.00 | 2.00 | 2.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Upstream Filter(I) | 0.00 | 0.09 | 0.09 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Uniform Delay (d), s/veł | n 0.0 | 0.0 | 0.0 | 50.0 | 15.1 | 11.8 | 29.6 | 31.6 | 31.9 | 29.3 | 22.5 | 21.3 | |
| Incr Delay (d2), s/veh | 0.0 | 4.3 | 3.9 | 148.7 | 1.4 | 0.9 | 0.2 | 0.8 | 1.0 | 3.0 | 0.1 | 0.0 | |
| Initial Q Delay(d3),s/veh | า 0.0 | 8.6 | 7.4 | 0.0 | 0.6 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | |
| %ile BackOfQ(50%),vel | n/ln0.0 | 2.6 | 2.3 | 4.8 | 8.2 | 2.4 | 1.2 | 3.8 | 3.6 | 1.9 | 1.7 | 0.2 | |
| Unsig. Movement Delay | , s/veh | 1 | | | | | | | | | | | |
| LnGrp Delay(d),s/veh | 0.0 | 12.9 | 11.3 | 198.7 | 17.0 | 12.6 | 29.9 | 32.4 | 32.9 | 32.3 | 22.6 | 21.3 | |
| LnGrp LOS | Α | В | В | F | В | В | С | С | С | С | С | C | |
| Approach Vol, veh/h | | 1385 | | | 1268 | | | 410 | | | 425 | | |
| Approach Delay, s/veh | | 12.1 | | | 28.1 | | | 32.2 | | | 27.3 | | |
| Approach LOS | | 12.1 B | | | 20.1 | | | C | | | 27.0 | | |
| | | | | | U | | | | | | U | | |
| Timer - Assigned Phs | | 2 | | 4 | | 6 | 7 | 8 | | | | | |
| Phs Duration (G+Y+Rc) | | 60.2 | | 39.8 | | 60.2 | 9.9 | 29.9 | | | | | |
| Change Period (Y+Rc), | S | 5.1 | | * 4.7 | | 5.1 | 3.0 | * 4.7 | | | | | |
| Max Green Setting (Gm | ax), s | 52.3 | | * 38 | | 52.3 | 6.9 | * 28 | | | | | |
| Max Q Clear Time (g_c- | | 2.0 | | 6.5 | | 22.6 | 8.9 | 12.3 | | | | | |
| Green Ext Time (p_c), s | | 30.2 | | 1.5 | | 19.1 | 0.0 | 2.2 | | | | | |
| Intersection Summary | | | | | | | | | | | | | |
| HCM 6th Ctrl Delay | | | 22.1 | | | | | | | | | | |
| HCM 6th LOS | | | C | | | | | | | | | | |
| | | | 3 | | | | | | | | | | |
| Notes | | | | | | | | | | | | | |

^{*} HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

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|--|---------|----------|---------------|------|------|-------|------|----------|------|------|----------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | | | | 414 | | ሻ | ^ | | | ħβ | |
| Traffic Volume (veh/h) | 0 | 0 | 0 | 110 | 176 | 72 | 140 | 472 | 0 | 0 | 549 | 114 |
| Future Volume (veh/h) | 0 | 0 | 0 | 110 | 176 | 72 | 140 | 472 | 0 | 0 | 549 | 114 |
| Initial Q (Qb), veh | | | | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | | | | 1.00 | | 0.79 | 0.95 | | 1.00 | 1.00 | | 0.77 |
| Parking Bus, Adj | | | | 0.85 | 1.00 | 0.85 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.83 |
| Work Zone On Approach | h | | | | No | | | No | | | No | |
| Adj Sat Flow, veh/h/ln | | | | 1660 | 1660 | 1660 | 1660 | 1660 | 0 | 0 | 1660 | 1660 |
| Adj Flow Rate, veh/h | | | | 116 | 185 | 57 | 147 | 497 | 0 | 0 | 578 | 93 |
| Peak Hour Factor | | | | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Percent Heavy Veh, % | | | | 3 | 3 | 3 | 3 | 3 | 0 | 0.00 | 3 | 3 |
| Cap, veh/h | | | | 303 | 496 | 156 | 354 | 1546 | 0 | 0 | 1165 | 186 |
| Arrive On Green | | | | 0.37 | 0.37 | 0.37 | 0.49 | 0.49 | 0.00 | 0.00 | 0.49 | 0.49 |
| Sat Flow, veh/h | | | | 812 | 1329 | 418 | 720 | 3237 | 0.00 | 0.00 | 2459 | 379 |
| Grp Volume(v), veh/h | | | | 195 | 0 | 163 | 147 | 497 | 0 | 0 | 382 | 289 |
| Grp Volume(v), ven/n Grp Sat Flow(s),veh/h/ln | | | | 1362 | 0 | 1197 | 720 | 1577 | 0 | 0 | 1577 | 1177 |
| 1 / | | | | 6.3 | 0.0 | | 10.4 | | 0.0 | 0.0 | 9.8 | 10.0 |
| Q Serve(g_s), s | | | | 6.3 | 0.0 | 5.9 | | 5.7 | | | 9.8 | |
| Cycle Q Clear(g_c), s | | | | | 0.0 | 5.9 | 20.4 | 5.7 | 0.0 | 0.0 | 9.0 | 10.0 |
| Prop In Lane | | | | 0.60 | ٥ | 0.35 | 1.00 | 1510 | 0.00 | 0.00 | 770 | 0.32 |
| Lane Grp Cap(c), veh/h | | | | 508 | 0 | 446 | 354 | 1546 | 0 | 0 | 773 | 577 |
| V/C Ratio(X) | | | | 0.38 | 0.00 | 0.37 | 0.42 | 0.32 | 0.00 | 0.00 | 0.49 | 0.50 |
| Avail Cap(c_a), veh/h | | | | 586 | 0 | 515 | 354 | 1546 | 0 | 0 | 773 | 577 |
| HCM Platoon Ratio | | | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | | | | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 0.00 | 0.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | | | | 13.8 | 0.0 | 13.7 | 17.2 | 9.3 | 0.0 | 0.0 | 10.3 | 10.3 |
| Incr Delay (d2), s/veh | | | | 0.5 | 0.0 | 0.5 | 3.6 | 0.6 | 0.0 | 0.0 | 2.2 | 3.1 |
| Initial Q Delay(d3),s/veh | | | | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh | | | | 1.8 | 0.0 | 1.5 | 1.9 | 1.8 | 0.0 | 0.0 | 3.4 | 2.7 |
| Unsig. Movement Delay | , s/veh | | | | | | | | | | | |
| _nGrp Delay(d),s/veh | | | | 14.2 | 0.0 | 14.2 | 20.8 | 9.8 | 0.0 | 0.0 | 12.5 | 13.4 |
| _nGrp LOS | | | | В | Α | В | С | Α | Α | Α | В | В |
| Approach Vol, veh/h | | | | | 358 | | | 644 | | | 671 | |
| Approach Delay, s/veh | | | | | 14.2 | | | 12.3 | | | 12.9 | |
| Approach LOS | | | | | В | | | В | | | В | |
| Timer - Assigned Phs | | 2 | | | | 6 | | 8 | | | | |
| Phs Duration (G+Y+Rc), | c | 33.6 | | | | 33.6 | | 26.4 | | | | |
| Change Period (Y+Rc), | | * 4.2 | | | | * 4.2 | | 4.0 | | | | |
| Max Green Setting (Gma | | * 26 | | | | * 26 | | 25.8 | | | | |
| Max Green Setting (Gma Max Q Clear Time (g_c+ | | 22.4 | | | | 12.0 | | 8.3 | | | | |
| | , . | 22.4 | | | | | | | | | | |
| Green Ext Time (p_c), s | | Z. I | | | | 6.3 | | 2.1 | | | | |
| ntersection Summary | | | | | | | | | | | | |
| HCM 6th Ctrl Delay | | | 13.0 | | | | | | | | | |
| HCM 6th LOS | | | В | | | | | | | | | |
| Notes | | | | | | | | | | | | |

^{*} HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

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|-----------------------------------|-------|----------|-------|------|-------------|------------|---------|----------|-------------|----------|------------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | | | | €1 } | | ¥ | ^ | | | ∱ ⊅ | |
| Traffic Volume (vph) | 0 | 0 | 0 | 91 | 205 | 150 | 70 | 325 | 0 | 0 | 390 | 130 |
| Future Volume (vph) | 0 | 0 | 0 | 91 | 205 | 150 | 70 | 325 | 0 | 0 | 390 | 130 |
| Ideal Flow (vphpl) | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 |
| Total Lost time (s) | | | | | 3.0 | | 4.0 | 4.0 | | | 4.0 | |
| Lane Util. Factor | | | | | 0.95 | | 1.00 | 0.95 | | | 0.95 | |
| Frpb, ped/bikes | | | | | 1.00 | | 1.00 | 1.00 | | | 1.00 | |
| Flpb, ped/bikes | | | | | 1.00 | | 1.00 | 1.00 | | | 1.00 | |
| Frt | | | | | 0.95 | | 1.00 | 1.00 | | | 0.96 | |
| Flt Protected | | | | | 0.99 | | 0.95 | 1.00 | | | 1.00 | |
| Satd. Flow (prot) | | | | | 2744 | | 1568 | 2885 | | | 2775 | |
| Flt Permitted | | | | | 0.99 | | 0.27 | 1.00 | | | 1.00 | |
| Satd. Flow (perm) | | | | | 2744 | | 447 | 2885 | | | 2775 | |
| Peak-hour factor, PHF | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Adj. Flow (vph) | 0 | 0 | 0 | 96 | 216 | 158 | 74 | 342 | 0 | 0 | 411 | 137 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 87 | 0 | 0 | 0 | 0 | 0 | 46 | 0 |
| Lane Group Flow (vph) | 0 | 0 | 0 | 0 | 383 | 0 | 74 | 342 | 0 | 0 | 502 | 0 |
| Confl. Bikes (#/hr) | | | 1 | | | 1 | | | 1 | | | 1 |
| Heavy Vehicles (%) | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% |
| Parking (#/hr) | | | | 6 | 6 | 4 | | 12 | | | 11 | 11 |
| Turn Type | | | | Perm | NA | | Perm | NA | | | NA | |
| Protected Phases | | | | | 6 | | | 8 | | | 4 | |
| Permitted Phases | | | | 6 | | | 8 | | | | | |
| Actuated Green, G (s) | | | | | 23.0 | | 16.0 | 16.0 | | | 16.0 | |
| Effective Green, g (s) | | | | | 23.0 | | 16.0 | 16.0 | | | 16.0 | |
| Actuated g/C Ratio | | | | | 0.33 | | 0.23 | 0.23 | | | 0.23 | |
| Clearance Time (s) | | | | | 3.0 | | 4.0 | 4.0 | | | 4.0 | |
| Vehicle Extension (s) | | | | | 2.0 | | 2.0 | 2.0 | | | 2.0 | |
| Lane Grp Cap (vph) | | | | | 901 | | 102 | 659 | | | 634 | |
| v/s Ratio Prot | | | | | | | | 0.12 | | | c0.18 | |
| v/s Ratio Perm | | | | | 0.14 | | 0.17 | V | | | | |
| v/c Ratio | | | | | 0.42 | | 0.73 | 0.52 | | | 0.79 | |
| Uniform Delay, d1 | | | | | 18.3 | | 25.0 | 23.6 | | | 25.4 | |
| Progression Factor | | | | | 1.00 | | 1.00 | 1.00 | | | 1.00 | |
| Incremental Delay, d2 | | | | | 1.5 | | 36.1 | 2.9 | | | 9.8 | |
| Delay (s) | | | | | 19.8 | | 61.1 | 26.5 | | | 35.2 | |
| Level of Service | | | | | В | | E | C | | | D | |
| Approach Delay (s) | | 0.0 | | | 19.8 | | _ | 32.7 | | | 35.2 | |
| Approach LOS | | A | | | В | | | C | | | D | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 29.4 | Н | CM 2000 | Level of | Service | | С | | | |
| HCM 2000 Volume to Capacity | ratio | | 0.38 | | _,,, | | | | | | | |
| Actuated Cycle Length (s) | | | 70.0 | S | um of lost | time (s) | | | 11.0 | | | |
| Intersection Capacity Utilization | 1 | | 49.7% | | | of Service | | | A | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | . • | | | | | | | | | |

| Intersection | | | | | | |
|------------------------|--------|-----------|---------|----------|------------|----------|
| Int Delay, s/veh | 0.1 | | | | | |
| | | EDD | NDI | NET | ODT | ODD |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | | 7 | ሻ | ^ | ↑ ↑ | |
| Traffic Vol, veh/h | 0 | 0 | 9 | 794 | 663 | 152 |
| Future Vol, veh/h | 0 | 0 | 9 | 794 | 663 | 152 |
| Conflicting Peds, #/hr | 0 | 0 | 406 | 0 | 0 | 406 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | 0 | 25 | - | - | - |
| Veh in Median Storage, | # 0 | - | - | 0 | 0 | - |
| Grade, % | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 95 | 95 | 95 | 95 | 95 | 95 |
| Heavy Vehicles, % | 3 | 3 | 3 | 3 | 3 | 3 |
| Mvmt Flow | 0 | 0 | 9 | 836 | 698 | 160 |
| | | - | | | | |
| | | | | | | |
| | 1inor2 | | //ajor1 | | Major2 | |
| Conflicting Flow All | - | 835 | 1264 | 0 | - | 0 |
| Stage 1 | - | - | - | - | - | - |
| Stage 2 | - | - | - | - | - | - |
| Critical Hdwy | - | 6.96 | 4.16 | - | - | - |
| Critical Hdwy Stg 1 | _ | _ | - | - | _ | _ |
| Critical Hdwy Stg 2 | _ | _ | _ | _ | _ | _ |
| Follow-up Hdwy | _ | 3.33 | 2.23 | _ | _ | _ |
| Pot Cap-1 Maneuver | 0 | 309 | 540 | _ | _ | _ |
| Stage 1 | 0 | - | | _ | _ | _ |
| Stage 2 | 0 | _ | _ | | _ | |
| Platoon blocked, % | U | _ | | _ | _ | _ |
| | | 100 | 224 | - | | - |
| Mov Cap-1 Maneuver | - | 190 | 331 | - | - | - |
| Mov Cap-2 Maneuver | - | - | - | - | - | - |
| Stage 1 | - | - | - | - | - | - |
| Stage 2 | - | - | - | - | - | - |
| | | | | | | |
| Approach | EB | | NB | | SB | |
| HCM Control Delay, s | 0 | | 0.2 | | 0 | |
| HCM LOS | A | | 0.2 | | U | |
| HOW LOS | А | | | | | |
| | | | | | | |
| Minor Lane/Major Mvmt | | NBL | NBT | EBLn1 | SBT | SBR |
| Capacity (veh/h) | | 331 | | _ | _ | _ |
| HCM Lane V/C Ratio | | 0.029 | _ | _ | _ | <u>-</u> |
| HCM Control Delay (s) | | 16.2 | _ | 0 | _ | |
| HCM Lane LOS | | 10.2 C | | A | _ | _ |
| HCM 95th %tile Q(veh) | | 0.1 | _ | - - | - | _ |
| | | 117 | | | | |

| Intersection | | | | | | | | | | | | |
|------------------------|------|-------|---------|--------|-------|------|------|-------|------|---------|------------|-------------|
| Int Delay, s/veh | 1.2 | | | | | | | | | | | |
| | | - FDT | EDD | MPI | MOT | MPP | ND | NET | NDD | ODI | ODT | ODD |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | | | _ | 41 | _ | _ | _ | | | ∱ } | |
| Traffic Vol, veh/h | 0 | 0 | 0 | 0 | 400 | 0 | 0 | 0 | 0 | 0 | 0 | 54 |
| Future Vol, veh/h | 0 | 0 | 0 | 0 | 400 | 0 | 0 | 0 | 0 | 0 | 0 | 54 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 251 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | - | - | - | - | - | - | - | - | - | - |
| Veh in Median Storage, | ,# - | 2 | - | - | 0 | - | - | 16974 | - | - | 0 | - |
| Grade, % | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 |
| Heavy Vehicles, % | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 |
| Mvmt Flow | 0 | 0 | 0 | 0 | 421 | 0 | 0 | 0 | 0 | 0 | 0 | 57 |
| | | | | | | | | | | | | |
| Major/Minor | | | | Major2 | | | | | _ N | /linor2 | | |
| Conflicting Flow All | | | | 251 | 0 | 0 | | | | - | 672 | 211 |
| Stage 1 | | | | ZJ I | - | - | | | | - | 421 | Z I I |
| Stage 2 | | | | _ | _ | _ | | | | | 251 | _ |
| Critical Hdwy | | | | 4.16 | | _ | | | | _ | 6.56 | 6.96 |
| Critical Hdwy Stg 1 | | | | 4.10 | _ | _ | | | | _ | 5.56 | 0.90 |
| Critical Hdwy Stg 2 | | | | - | - | - | | | | - | 5.56 | - |
| Follow-up Hdwy | | | | 2.23 | - | - | | | | - | 4.03 | 3.33 |
| Pot Cap-1 Maneuver | | | | 1304 | - | 0 | | | | 0 | 374 | 3.33 791 |
| | | | | | | 0 | | | | | 585 | |
| Stage 1 | | | | - | - | | | | | 0 | ებე | - |
| Stage 2 | | | | - | - | 0 | | | | U | - | - |
| Platoon blocked, % | | | | 1201 | - | | | | | | ^ | 704 |
| Mov Cap-1 Maneuver | | | | 1304 | - | - | | | | - | 0 | 791 |
| Mov Cap-2 Maneuver | | | | - | - | - | | | | - | 0 | - |
| Stage 1 | | | | - | - | - | | | | - | 0 | - |
| Stage 2 | | | | - | - | - | | | | - | 0 | - |
| | | | | | | | | | | | | |
| Approach | | | | WB | | | | | | SB | | |
| HCM Control Delay, s | | | | 0 | | | | | | 9.9 | | |
| HCM LOS | | | | | | | | | | Α | | |
| | | | | | | | | | | | | |
| Minor Lane/Major Mvmt | | WBL | \M/DT (| SBLn1 | SBLb2 | | | | | | | |
| | | | VVDI | | | | | | | | | |
| Capacity (veh/h) | | 1304 | - | - | | | | | | | | |
| HCM Cartral Dalay (2) | | - | - | | 0.072 | | | | | | | |
| HCM Control Delay (s) | | 0 | - | 0 | 9.9 | | | | | | | |
| HCM Lane LOS | | A | - | Α | A | | | | | | | |
| HCM 95th %tile Q(veh) | | 0 | - | - | 0.2 | | | | | | | |

| Intersection | | | | | | |
|------------------------|----------|-------|--------|------|--------|------|
| Int Delay, s/veh | 9.9 | | | | | |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | † | רטוע | TTDL | 41 | TIDL | 7 |
| Traffic Vol, veh/h | 1449 | 82 | 88 | 970 | 0 | 235 |
| Future Vol, veh/h | 1449 | 82 | 88 | 970 | 0 | 235 |
| Conflicting Peds, #/hr | 0 | 100 | 100 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | | - | None |
| Storage Length | _ | - | _ | - | _ | 0 |
| Veh in Median Storage | ,# 0 | - | _ | 0 | 0 | - |
| Grade, % | 0 | _ | _ | 0 | 0 | _ |
| Peak Hour Factor | 96 | 96 | 96 | 96 | 96 | 96 |
| Heavy Vehicles, % | 3 | 3 | 3 | 3 | 3 | 3 |
| Mvmt Flow | 1509 | 85 | 92 | 1010 | 0 | 245 |
| WWWIICTIOW | 1000 | 00 | JZ. | 1010 | U | 2-10 |
| | | | | | | |
| | /lajor1 | | Major2 | | Minor1 | |
| Conflicting Flow All | 0 | 0 | 1694 | 0 | - | 897 |
| Stage 1 | - | - | - | - | - | - |
| Stage 2 | - | - | - | - | - | - |
| Critical Hdwy | - | - | 4.16 | - | - | 6.96 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - |
| Critical Hdwy Stg 2 | - | - | - | - | - | - |
| Follow-up Hdwy | - | - | 2.23 | - | - | 3.33 |
| Pot Cap-1 Maneuver | - | - | 368 | - | 0 | 281 |
| Stage 1 | - | - | - | - | 0 | - |
| Stage 2 | - | - | - | - | 0 | - |
| Platoon blocked, % | - | - | | - | | |
| Mov Cap-1 Maneuver | - | - | 333 | - | - | 254 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - |
| Stage 1 | - | - | - | - | - | - |
| Stage 2 | - | - | - | - | - | - |
| | | | | | | |
| Annanah | ED | | \A/D | | ND | |
| Approach | EB | | WB | | NB | |
| HCM Control Delay, s | 0 | | 6.5 | | 89.8 | |
| HCM LOS | | | | | F | |
| | | | | | | |
| Minor Lane/Major Mvm | t l | NBLn1 | EBT | EBR | WBL | WBT |
| Capacity (veh/h) | | 254 | - | - | | - |
| HCM Lane V/C Ratio | | 0.964 | _ | _ | 0.275 | - |
| HCM Control Delay (s) | | 89.8 | - | - | | 5.3 |
| HCM Lane LOS | | F | _ | _ | С | A |
| HCM 95th %tile Q(veh) | | 9 | _ | _ | 1.1 | - |
| . Tom com /one w(ven) | | J | | | 1.1 | |

| Intersection | | | | | | |
|------------------------|----------|-------|---------|----------|--------|------|
| Int Delay, s/veh | 0.5 | | | | | |
| | | EDD | MD | WET | ND | NDD |
| | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | † | | 7 | ^ | | 7 |
| Traffic Vol, veh/h | 767 | 29 | 31 | 1580 | 0 | 79 |
| Future Vol, veh/h | 767 | 29 | 31 | 1580 | 0 | 79 |
| Conflicting Peds, #/hr | _ 0 | 0 | _ 0 | _ 0 | 0 | 0 |
| 0 | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | | None |
| Storage Length | - | - | 25 | - | - | 0 |
| Veh in Median Storage, | | - | - | 0 | 0 | - |
| Grade, % | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 834 | 32 | 34 | 1717 | 0 | 86 |
| | | | | | | |
| Major/Minor Ma | aior1 | N | /aior? | | Minor1 | |
| | ajor1 | | //ajor2 | | | 400 |
| Conflicting Flow All | 0 | 0 | 866 | 0 | - | 433 |
| Stage 1 | - | - | - | - | - | - |
| Stage 2 | - | - | - | - | - | - |
| Critical Hdwy | - | - | 4.14 | - | - | 6.94 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - |
| Critical Hdwy Stg 2 | - | - | - | - | - | - |
| Follow-up Hdwy | - | - | 2.22 | - | - | 3.32 |
| Pot Cap-1 Maneuver | - | - | 773 | - | 0 | 571 |
| Stage 1 | - | - | - | - | 0 | - |
| Stage 2 | - | - | - | - | 0 | - |
| Platoon blocked, % | - | - | | - | | |
| Mov Cap-1 Maneuver | - | - | 773 | - | - | 571 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - |
| Stage 1 | - | - | - | - | - | - |
| Stage 2 | _ | _ | _ | _ | _ | _ |
| 5.66g0 <u>2</u> | | | | | | |
| | | | | | | |
| Approach | EB | | WB | | NB | |
| HCM Control Delay, s | 0 | | 0.2 | | 12.4 | |
| HCM LOS | | | | | В | |
| | | | | | | |
| Minor Lane/Major Mvmt | N | NBLn1 | EBT | EBR | WBL | WBT |
| | ľ | | | | | |
| Capacity (veh/h) | | 571 | - | - | 773 | - |
| HCM Lane V/C Ratio | | 0.15 | - | | 0.044 | - |
| HCM Control Delay (s) | | 12.4 | - | - | 9.9 | - |
| HCM Lane LOS | | В | - | - | A | - |
| HCM 95th %tile Q(veh) | | 0.5 | - | - | 0.1 | - |

| Intersection | | | | | | |
|---|----------|----------|-----------|----------|-----------|-----------|
| Int Delay, s/veh | 8.1 | | | | | |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | † | LUI | VVDL آ | <u>₩</u> | NDL | NDIX * |
| | 1449 | 82 | 88 | 970 | 0 | 235 |
| | 1449 | 82 | 88 | 970 | | |
| | | | | | 0 | 235 |
| Conflicting Peds, #/hr | 0 | 100 | 100 | 0 | 0 | 0 |
| | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | 25 | - | - | 0 |
| Veh in Median Storage, | # 0 | - | - | 0 | 0 | - |
| Grade, % | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 96 | 96 | 96 | 96 | 96 | 96 |
| Heavy Vehicles, % | 3 | 3 | 3 | 3 | 3 | 3 |
| | 1509 | 85 | 92 | 1010 | 0 | 245 |
| | 1000 | 00 | 02 | 1010 | Ū | 2.0 |
| | | | | | | |
| Major/Minor Major/Minor | ajor1 | N | Major2 | 1 | Minor1 | |
| Conflicting Flow All | 0 | 0 | 1694 | 0 | - | 897 |
| Stage 1 | - | - | - | - | - | - |
| Stage 2 | _ | _ | _ | _ | _ | _ |
| Critical Hdwy | _ | _ | 4.16 | _ | _ | 6.96 |
| Critical Hdwy Stg 1 | _ | <u>-</u> | 4.10 | _ | _ | 0.30 |
| | _ | _ | _ | _ | _ | |
| Critical Hdwy Stg 2 | - | - | | | | |
| Follow-up Hdwy | - | - | 2.23 | - | - | 3.33 |
| Pot Cap-1 Maneuver | - | - | 368 | - | 0 | 281 |
| Stage 1 | - | - | - | - | 0 | - |
| Stage 2 | - | - | - | - | 0 | - |
| Platoon blocked, % | - | - | | - | | |
| Mov Cap-1 Maneuver | - | - | 333 | - | - | 254 |
| Mov Cap-2 Maneuver | _ | _ | - | _ | - | _ |
| Stage 1 | _ | _ | _ | _ | _ | _ |
| Stage 2 | <u>-</u> | _ | _ | <u>-</u> | _ | _ |
| Slaye 2 | - | - | - | - | - | - |
| | | | | | | |
| Approach | EB | | WB | | NB | |
| HCM Control Delay, s | 0 | | 1.7 | | 89.8 | |
| HCM LOS | - 0 | | 1.7 | | 03.0 F | |
| I IOWI LOG | | | | | r r | |
| | | | | | | |
| Minor Lane/Major Mvmt | 1 | NBLn1 | EBT | EBR | WBL | WBT |
| Capacity (veh/h) | | 254 | - | | 333 | _ |
| HCM Lane V/C Ratio | | 0.964 | _ | | 0.275 | _ |
| HCM Control Delay (s) | | 89.8 | | _ | 19.9 | - |
| | | | - | - | | |
| HCM Lane LOS HCM 95th %tile Q(veh) | | F | - | - | C | - |
| LIC'N/I (16+b) U/ +ilo (\/\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\ | | 9 | - | - | 1.1 | - |

| | ۶ | → | • | • | ← | • | 4 | † | / | > | ţ | 4 |
|------------------------------|-------|----------|-----------|-------|------------|------|------|----------|----------|-------------|------------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ¥ | ^ | 7 | Ť | ∱ ∱ | | ř | ^ | 7 | | ∱ ⊅ | |
| Traffic Volume (veh/h) | 96 | 648 | 191 | 176 | 1424 | 30 | 44 | 400 | 80 | 0 | 553 | 87 |
| Future Volume (veh/h) | 96 | 648 | 191 | 176 | 1424 | 30 | 44 | 400 | 80 | 0 | 553 | 87 |
| Initial Q (Qb), veh | 0 | 10 | 0 | 0 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | | 0.95 | 0.99 | | 0.96 | 0.99 | | 0.91 | 1.00 | | 0.91 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach | | No | | | No | | | No | | | No | |
| Adj Sat Flow, veh/h/ln | 1660 | 1660 | 1660 | 1367 | 1367 | 1367 | 1660 | 1660 | 1660 | 0 | 1660 | 1660 |
| Adj Flow Rate, veh/h | 101 | 682 | 192 | 185 | 1499 | 31 | 46 | 421 | 21 | 0 | 582 | 79 |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Percent Heavy Veh, % | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 0 | 3 | 3 |
| Cap, veh/h | 72 | 2445 | 1041 | 72 | 2017 | 40 | 117 | 817 | 333 | 0 | 714 | 97 |
| Arrive On Green | 0.77 | 0.77 | 0.77 | 1.00 | 1.00 | 1.00 | 0.26 | 0.26 | 0.26 | 0.00 | 0.26 | 0.26 |
| Sat Flow, veh/h | 336 | 3154 | 1344 | 515 | 2600 | 54 | 758 | 3154 | 1285 | 0 | 2839 | 373 |
| Grp Volume(v), veh/h | 101 | 682 | 192 | 185 | 748 | 782 | 46 | 421 | 21 | 0 | 332 | 329 |
| Grp Sat Flow(s), veh/h/ln | 336 | 1577 | 1344 | 515 | 1299 | 1355 | 758 | 1577 | 1285 | 0 | 1577 | 1551 |
| Q Serve(g_s), s | 9.8 | 6.2 | 3.8 | 5.9 | 0.0 | 0.0 | 6.0 | 11.4 | 1.2 | 0.0 | 19.8 | 19.9 |
| Cycle Q Clear(g_c), s | 10.2 | 6.2 | 3.8 | 12.7 | 0.0 | 0.0 | 25.9 | 11.4 | 1.2 | 0.0 | 19.8 | 19.9 |
| Prop In Lane | 1.00 | 0.2 | 1.00 | 1.00 | 0.0 | 0.04 | 1.00 | 11.4 | 1.00 | 0.00 | 19.0 | 0.24 |
| | 72 | 2445 | 1041 | 72 | 1007 | 1050 | | 817 | 333 | | 400 | |
| Lane Grp Cap(c), veh/h | | 2445 | | | 1007 | | 117 | | | 0 | 408 | 402 |
| V/C Ratio(X) | 1.40 | 0.28 | 0.18 | 2.57 | 0.74 | 0.74 | 0.39 | 0.52 | 0.06 | 0.00 | 0.81 | 0.82 |
| Avail Cap(c_a), veh/h | 331 | 2445 | 1041 | 436 | 1007 | 1050 | 117 | 817 | 333 | 0 | 408 | 402 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 2.00 | 2.00 | 2.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 0.40 | 0.40 | 0.40 | 1.00 | 1.00 | 1.00 | 0.00 | 0.09 | 0.09 |
| Uniform Delay (d), s/veh | 50.0 | 3.4 | 3.0 | 38.7 | 0.0 | 0.0 | 47.1 | 31.7 | 27.9 | 0.0 | 34.8 | 34.8 |
| Incr Delay (d2), s/veh | 244.1 | 0.3 | 0.4 | 720.4 | 2.0 | 2.0 | 2.1 | 0.6 | 0.1 | 0.0 | 1.2 | 1.3 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.2 | 0.0 | 0.0 | 0.7 | 0.6 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/ln | 6.7 | 2.1 | 0.9 | 16.2 | 8.0 | 0.8 | 1.2 | 4.4 | 0.4 | 0.0 | 7.7 | 7.6 |
| Unsig. Movement Delay, s/vel | | | | | | | | | | | | |
| LnGrp Delay(d),s/veh | 294.1 | 3.9 | 3.3 | 759.2 | 2.7 | 2.6 | 49.2 | 32.2 | 28.0 | 0.0 | 36.0 | 36.1 |
| LnGrp LOS | F | Α | Α | F | Α | Α | D | С | С | Α | D | D |
| Approach Vol, veh/h | | 975 | | | 1715 | | | 488 | | | 661 | |
| Approach Delay, s/veh | | 33.8 | | | 84.3 | | | 33.7 | | | 36.0 | |
| Approach LOS | | С | | | F | | | С | | | D | |
| Timer - Assigned Phs | | 2 | | 4 | | 6 | | 8 | | | | |
| Phs Duration (G+Y+Rc), s | | 83.0 | | 31.0 | | 83.0 | | 31.0 | | | | |
| Change Period (Y+Rc), s | | 5.1 | | * 5.1 | | 5.1 | | 5.1 | | | | |
| Max Green Setting (Gmax), s | | 64.3 | | * 26 | | 64.3 | | 25.5 | | | | |
| Max Q Clear Time (g_c+l1), s | | 12.2 | | 27.9 | | 14.7 | | 21.9 | | | | |
| Green Ext Time (p_c), s | | 19.8 | | 0.0 | | 38.4 | | 1.4 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 6th Ctrl Delay | | | 56.7 | | | | | | | | | |
| HCM 6th LOS | | | 50.7 E | | | | | | | | | |
| Notes | | | | | | | | | | | | |

^{*} HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

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|-----------------------------------|------------|----------|----------|------------|------------|----------|-----------|-----------|-------------|-------------|------------|-----------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ň | ^ | 7 | Ť | ∱ ∱ | | ř | ^ | 7 | | ∱ ⊅ | |
| Traffic Volume (veh/h) | 172 | 1310 | 306 | 110 | 849 | 50 | 94 | 530 | 170 | 0 | 459 | 90 |
| Future Volume (veh/h) | 172 | 1310 | 306 | 110 | 849 | 50 | 94 | 530 | 170 | 0 | 459 | 90 |
| Initial Q (Qb), veh | 0 | 10 | 0 | 0 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 0.98 | | 0.90 | 1.00 | | 0.90 | 0.96 | | 0.82 | 1.00 | | 0.83 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach | | No | | | No | | | No | | | No | |
| Adj Sat Flow, veh/h/ln | 1367 | 1367 | 1367 | 1660 | 1660 | 1660 | 1660 | 1660 | 1660 | 0 | 1660 | 1660 |
| Adj Flow Rate, veh/h | 181 | 1379 | 314 | 116 | 894 | 49 | 99 | 558 | 160 | 0 | 483 | 78 |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Percent Heavy Veh, % | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 0 | 3 | 3 |
| Cap, veh/h | 73 | 2013 | 811 | 72 | 2345 | 126 | 145 | 817 | 299 | 0 | 683 | 109 |
| Arrive On Green | 0.77 | 0.77 | 0.77 | 1.00 | 1.00 | 1.00 | 0.26 | 0.26 | 0.26 | 0.00 | 0.26 | 0.26 |
| Sat Flow, veh/h | 475 | 2598 | 1046 | 288 | 3021 | 166 | 808 | 3154 | 1156 | 0 | 2721 | 421 |
| Grp Volume(v), veh/h | 181 | 1379 | 314 | 116 | 467 | 476 | 99 | 558 | 160 | 0 | 286 | 275 |
| Grp Sat Flow(s), veh/h/ln | 475 | 1299 | 1046 | 288 | 1577 | 1610 | 808 | 1577 | 1156 | 0 | 1577 | 1482 |
| Q Serve(g_s), s | 14.1 | 25.5 | 9.7 | 28.9 | 0.0 | 0.0 | 9.1 | 15.9 | 11.9 | 0.0 | 16.4 | 16.8 |
| Cycle Q Clear(g_c), s | 14.5 | 25.5 | 9.7 | 55.7 | 0.0 | 0.0 | 25.9 | 15.9 | 11.9 | 0.0 | 16.4 | 16.8 |
| Prop In Lane | 1.00 | 20.0 | 1.00 | 1.00 | 0.0 | 0.10 | 1.00 | 10.5 | 1.00 | 0.00 | 10.4 | 0.28 |
| Lane Grp Cap(c), veh/h | 73 | 2013 | 811 | 72 | 1222 | 1248 | 145 | 817 | 299 | 0.00 | 408 | 384 |
| V/C Ratio(X) | 2.49 | 0.68 | 0.39 | 1.61 | 0.38 | 0.38 | 0.68 | 0.68 | 0.53 | 0.00 | 0.70 | 0.72 |
| Avail Cap(c_a), veh/h | 438 | 2013 | 811 | 218 | 1222 | 1247 | 145 | 817 | 299 | 0.00 | 408 | 384 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 2.00 | 2.00 | 2.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 0.85 | 0.85 | 0.85 | 1.00 | 1.00 | 1.00 | 0.00 | 0.28 | 0.28 |
| Uniform Delay (d), s/veh | 50.0 | 5.8 | 3.6 | 38.7 | 0.03 | 0.0 | 46.7 | 33.4 | 31.9 | 0.0 | 33.5 | 33.7 |
| Incr Delay (d2), s/veh | 710.3 | 1.9 | 1.4 | 321.5 | 0.8 | 0.8 | 12.3 | 2.3 | 1.8 | 0.0 | 1.5 | 1.8 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.6 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/ln | 16.2 | 6.7 | 1.9 | 8.2 | 0.2 | 0.2 | 3.0 | 6.3 | 3.5 | 0.0 | 6.4 | 6.2 |
| Unsig. Movement Delay, s/ver | | 0.7 | 1.9 | 0.2 | 0.5 | 0.5 | 3.0 | 0.5 | 3.5 | 0.0 | 0.4 | 0.2 |
| • | 760.3 | 8.2 | 5.0 | 360.3 | 1.0 | 0.9 | 58.9 | 35.7 | 33.7 | 0.0 | 35.1 | 35.5 |
| LnGrp Delay(d),s/veh LnGrp LOS | 700.5 F | 0.2 A | 3.0 A | 300.3 F | 1.0 A | 0.9 A | 56.9 E | 33.7 D | 33.7 C | 0.0 A | 33.1 D | 33.5 D |
| | Г | | A | Г | | A | | | U | A | | |
| Approach Vol, veh/h | | 1874 | | | 1059 | | | 817 | | | 561 | |
| Approach Delay, s/veh | | 80.3 | | | 40.3 | | | 38.1 | | | 35.3 | |
| Approach LOS | | F | | | D | | | D | | | D | |
| Timer - Assigned Phs | | 2 | | 4 | | 6 | | 8 | | | | |
| Phs Duration (G+Y+Rc), s | | 83.0 | | 31.0 | | 83.0 | | 31.0 | | | | |
| Change Period (Y+Rc), s | | 5.1 | | * 5.1 | | 5.1 | | 5.1 | | | | |
| Max Green Setting (Gmax), s | | 64.3 | | * 26 | | 64.3 | | 25.5 | | | | |
| Max Q Clear Time (g_c+l1), s | | 27.5 | | 27.9 | | 57.7 | | 18.8 | | | | |
| Green Ext Time (p_c), s | | 30.9 | | 0.0 | | 5.3 | | 2.0 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 6th Ctrl Delay | | | 56.6 | | | | | | | | | |
| HCM 6th LOS | | | E | | | | | | | | | |
| Notes | | | _ | | | | | | | | | |

^{*} HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

Appendix B (continued): Existing Uses Scenario

| | ۶ | → | * | • | — | • | 1 | † | / | / | + | ✓ |
|--|-------------|--------------|------------|---------------|-------------|-------------|----------|------------|-----------|-----------|-------------|-----------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ሻ | ∱ ∱ | | ሻ | ∱ ∱ | | | ∱ ∱ | | ሻ | ^↑ | 7 |
| Traffic Volume (veh/h) | 23 | 1318 | 27 | 80 | 1485 | 29 | 0 | 75 | 28 | 28 | 300 | 45 |
| Future Volume (veh/h) | 23 | 1318 | 27 | 80 | 1485 | 29 | 0 | 75 | 28 | 28 | 300 | 45 |
| Initial Q (Qb), veh | 0 | 10 | 0 | 0 | 15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | | 0.97 | 1.00 | | 0.99 | 1.00 | | 0.97 | 0.99 | | 0.98 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach | | No | | | No | | _ | No | | | No | |
| Adj Sat Flow, veh/h/ln | 1367 | 1367 | 1367 | 1367 | 1367 | 1367 | 0 | 1660 | 1660 | 1660 | 1660 | 1660 |
| Adj Flow Rate, veh/h | 26 | 1464 | 29 | 89 | 1650 | 31 | 0 | 83 | 8 | 31 | 333 | 26 |
| Peak Hour Factor | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Percent Heavy Veh, % | 3 | 3 | 3 | 3 | 3 | 3 | 0 | 3 | 3 | 3 | 3 | 3 |
| Cap, veh/h | 117 | 1915 | 36 | 72 | 1921 | 32 | 0 | 483 | 46 | 253 | 525 | 230 |
| Arrive On Green | 0.73 | 0.73 | 0.73 | 0.73 | 0.73 | 0.73 | 0.00 | 0.17 | 0.17 | 0.17 | 0.17 | 0.17 |
| Sat Flow, veh/h | 240 | 2603 | 52 | 288 | 2608 | 49 | 0 | 2987 | 276 | 1282 | 3154 | 1379 |
| Grp Volume(v), veh/h | 26 | 730 | 763 | 89 | 820 | 861 | 0 | 44 | 47 | 31 | 333 | 26 |
| Grp Sat Flow(s),veh/h/ln | 240 | 1299 | 1356 | 288 | 1299 | 1358 | 0 | 1577 | 1602 | 1282 | 1577 | 1379 |
| Q Serve(g_s), s | 8.8 | 34.0 | 34.2 | 27.2 | 45.5 | 46.0 | 0.0 | 2.4 | 2.5 | 2.1 | 9.8 | 1.6 |
| Cycle Q Clear(g_c), s | 54.8 | 34.0 | 34.2 | 61.4 | 45.5 | 46.0 | 0.0 | 2.4 | 2.5 | 4.6 | 9.8 | 1.6 |
| Prop In Lane | 1.00 | 054 | 0.04 | 1.00 | 054 | 0.04 | 0.00 | 200 | 0.17 | 1.00 | 505 | 1.00 |
| Lane Grp Cap(c), veh/h | 117 | 954 | 997 | 72 | 954 | 998 | 0 | 263 | 267 | 253 | 525 | 230 |
| V/C Ratio(X) | 0.22 | 0.76 | 0.77 | 1.24 | 0.86 | 0.86 | 0.00 | 0.17 | 0.17 | 0.12 | 0.63 | 0.11 |
| Avail Cap(c_a), veh/h | 138 | 954 | 996 | 185 | 954 | 997 | 0 | 420 | 426 | 381 | 839 | 367 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 0.40 | 0.40 | 0.40 | 0.00 | 0.99 | 0.99 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 36.1 4.4 | 8.5 | 8.5 | 50.0 | 10.4 4.3 | 10.4 4.2 | 0.0 | 35.7 | 35.8 | 37.8 | 38.8 1.3 | 35.4 |
| Incr Delay (d2), s/veh | 0.0 | 5.8 0.8 | 5.6 0.8 | 144.7 | | 3.0 | 0.0 | 0.3 | 0.3 | 0.2 | 0.0 | 0.2 |
| Initial Q Delay(d3),s/veh | 0.0 | 9.6 | 10.0 | 0.0 4.7 | 3.2 12.8 | 13.3 | 0.0 | 1.0 | 1.0 | 0.0 | 3.9 | 0.0 |
| %ile BackOfQ(50%),veh/ln Unsig. Movement Delay, s/veh | | 9.0 | 10.0 | 4.7 | 12.0 | 13.3 | 0.0 | 1.0 | 1.0 | 0.7 | 3.9 | 0.0 |
| LnGrp Delay(d),s/veh | 40.5 | 15.2 | 14.9 | 194.7 | 17.9 | 17.6 | 0.0 | 36.0 | 36.1 | 38.0 | 40.1 | 35.6 |
| LnGrp LOS | 40.5 D | 15.2 B | 14.9 B | 194. <i>1</i> | 17.9 B | 17.0 B | 0.0 A | 30.0 D | 30.1 D | 36.0 D | 40.1 D | 35.0 D |
| | U | | Ь | <u> </u> | 1770 | ь | ^ | 91 | <u> </u> | <u> </u> | 390 | |
| Approach Vol, veh/h | | 1519 15.5 | | | 26.6 | | | 36.1 | | | 39.6 | |
| Approach LOS | | _ | | | | | | _ | | | _ | |
| Approach LOS | | В | | | С | | | D | | | D | |
| Timer - Assigned Phs | | 2 | | 4 | | 6 | | 8 | | | | |
| Phs Duration (G+Y+Rc), s | | 78.9 | | 21.1 | | 78.9 | | 21.1 | | | | |
| Change Period (Y+Rc), s | | 5.4 | | 4.5 | | 5.4 | | 4.5 | | | | |
| Max Green Setting (Gmax), s | | 63.5 | | 26.6 | | 63.5 | | 26.6 | | | | |
| Max Q Clear Time (g_c+l1), s | | 56.8 | | 11.8 | | 63.4 | | 4.5 | | | | |
| Green Ext Time (p_c), s | | 6.0 | | 2.1 | | 0.1 | | 0.4 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 6th Ctrl Delay | | | 23.7 | | | | | | | | | |
| HCM 6th LOS | | | С | | | | | | | | | |

| • | | → | • | • | ← | • | • | † | <i>></i> | \ | Ţ | √ |
|-------------------------------|-----|------------|------|-------|------------|------|------|------|-------------|----------|------|----------|
| Movement EB | L | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ነ | † } | | ሻ | ↑ ↑ | | ሻ | ħβ | | ሻ | ħβ | |
| Traffic Volume (veh/h) 3 | • | 1491 | 26 | 93 | 1270 | 36 | 20 | 339 | 144 | 21 | 473 | 57 |
| Future Volume (veh/h) 3 | | 1491 | 26 | 93 | 1270 | 36 | 20 | 339 | 144 | 21 | 473 | 57 |
| \ / |) | 10 | 0 | 0 | 15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) 1.0 |) | | 0.98 | 1.00 | | 0.97 | 0.99 | | 0.97 | 0.99 | | 0.98 |
| Parking Bus, Adj 1.0 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach | | No | | | No | | | No | | | No | |
| Adj Sat Flow, veh/h/ln 136 | 7 1 | 1367 | 1367 | 1367 | 1367 | 1367 | 1660 | 1660 | 1660 | 1660 | 1660 | 1660 |
| Adj Flow Rate, veh/h 4 | | 1657 | 28 | 103 | 1411 | 38 | 22 | 377 | 140 | 23 | 526 | 53 |
| Peak Hour Factor 0.9 | | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 |
| Cap, veh/h 10 | | 1730 | 20 | 72 | 1705 | 40 | 124 | 525 | 192 | 156 | 677 | 68 |
| Arrive On Green 0.6 | | 0.66 | 0.66 | 0.66 | 0.66 | 0.66 | 0.47 | 0.47 | 0.47 | 0.23 | 0.23 | 0.23 |
| Sat Flow, veh/h 30 | | 2613 | 44 | 239 | 2582 | 69 | 823 | 2240 | 818 | 871 | 2888 | 290 |
| Grp Volume(v), veh/h 4 | | 822 | 863 | 103 | 709 | 740 | 22 | 264 | 253 | 23 | 286 | 293 |
| Grp Sat Flow(s), veh/h/ln 30 | | 1299 | 1358 | 239 | 1299 | 1352 | 823 | 1577 | 1480 | 871 | 1577 | 1601 |
| Q Serve(g_s), s 12. | | 59.1 | 59.6 | 6.1 | 41.2 | 41.4 | 2.5 | 13.3 | 13.8 | 2.5 | 17.0 | 17.1 |
| Cycle Q Clear(g_c), s 53.4 | | 59.1 | 59.6 | 65.8 | 41.2 | 41.4 | 19.6 | 13.3 | 13.8 | 16.3 | 17.0 | 17.1 |
| Prop In Lane 1.0 | | | 0.03 | 1.00 | | 0.05 | 1.00 | | 0.55 | 1.00 | • | 0.18 |
| Lane Grp Cap(c), veh/h 10 | | 854 | 895 | 72 | 854 | 890 | 124 | 370 | 347 | 156 | 370 | 375 |
| V/C Ratio(X) 0.38 | | 0.96 | 0.96 | 1.43 | 0.83 | 0.83 | 0.18 | 0.71 | 0.73 | 0.15 | 0.77 | 0.78 |
| Avail Cap(c_a), veh/h 14 | | 854 | 893 | 87 | 854 | 889 | 150 | 420 | 394 | 183 | 420 | 426 |
| HCM Platoon Ratio 1.0 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 2.00 | 2.00 | 2.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) 0.3 | | 0.34 | 0.34 | 1.00 | 1.00 | 1.00 | 0.83 | 0.83 | 0.83 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh 42. | | 16.7 | 16.7 | 50.0 | 13.8 | 13.8 | 33.4 | 23.9 | 24.0 | 42.0 | 35.8 | 35.9 |
| Incr Delay (d2), s/veh 3.5 | | 11.1 | 10.9 | 256.5 | 9.2 | 8.9 | 0.6 | 4.1 | 4.9 | 0.4 | 7.8 | 8.0 |
| Initial Q Delay(d3),s/veh 0.0 | | 6.6 | 6.2 | 0.0 | 3.3 | 3.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/lnl. | | 19.6 | 20.4 | 6.9 | 14.2 | 14.6 | 0.5 | 4.3 | 4.2 | 0.5 | 7.3 | 7.5 |
| Unsig. Movement Delay, s/v | | | | | | | | | | | | |
| LnGrp Delay(d),s/veh 45. | | 34.4 | 33.9 | 306.5 | 26.2 | 25.7 | 34.0 | 27.9 | 28.9 | 42.4 | 43.6 | 43.8 |
| LnGrp LOS [| | С | С | F | С | С | С | С | С | D | D | D |
| Approach Vol, veh/h | , | 1726 | | | 1552 | | | 539 | | | 602 | |
| Approach Delay, s/veh | | 34.4 | | | 44.6 | | | 28.7 | | | 43.7 | |
| Approach LOS | | С | | | D | | | C | | | D | |
| Timer - Assigned Phs | | 2 | | 4 | | 6 | | 8 | | | | |
| Phs Duration (G+Y+Rc), s | | 71.2 | | 28.8 | | 71.2 | | 28.8 | | | | |
| Change Period (Y+Rc), s | | 5.4 | | 5.4 | | 5.4 | | 5.4 | | | | |
| Max Green Setting (Gmax), | c | 62.6 | | 26.6 | | 62.6 | | 26.6 | | | | |
| Max Q Clear Time (g_c+l1), | | 61.6 | | 19.1 | | 67.8 | | 21.6 | | | | |
| Green Ext Time (p_c), s | J | 0.9 | | 2.3 | | 0.0 | | 1.5 | | | | |
| " , | | 0.0 | | 2.0 | | 0.0 | | 1.0 | | | | |
| Intersection Summary | | | 20.5 | | | | | | | | | |
| HCM 6th Ctrl Delay | | | 38.5 | | | | | | | | | |
| HCM 6th LOS | | | D | | | | | | | | | |

AM Peak Hour

| | • | - | • | • | ← | • | 4 | † | / | > | ļ | 1 |
|----------------------------------|---------|------------|--------|-------|------------|------------|---------|------------|------|-------------|-------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | ∱ } | | | 413- | | ሻ | ∱ } | | ሻ | ħβ | |
| Traffic Volume (vph) | 0 | 641 | 41 | 127 | 1347 | 21 | 11 | 82 | 32 | 31 | 327 | 49 |
| Future Volume (vph) | 0 | 641 | 41 | 127 | 1347 | 21 | 11 | 82 | 32 | 31 | 327 | 49 |
| Ideal Flow (vphpl) | 1700 | 1700 | 1700 | 1400 | 1400 | 1400 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 |
| Total Lost time (s) | | 5.1 | | | 5.1 | | 4.5 | 4.5 | | 4.5 | 4.5 | |
| Lane Util. Factor | | 0.95 | | | 0.95 | | 1.00 | 0.95 | | 1.00 | 0.95 | |
| Frpb, ped/bikes | | 1.00 | | | 1.00 | | 1.00 | 0.98 | | 1.00 | 0.99 | |
| Flpb, ped/bikes | | 1.00 | | | 1.00 | | 0.98 | 1.00 | | 0.96 | 1.00 | |
| Frt | | 0.99 | | | 1.00 | | 1.00 | 0.96 | | 1.00 | 0.98 | |
| Flt Protected | | 1.00 | | | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | | 3098 | | | 2559 | | 1543 | 2749 | | 1511 | 3057 | |
| Flt Permitted | | 1.00 | | | 0.74 | | 0.39 | 1.00 | | 0.68 | 1.00 | |
| Satd. Flow (perm) | | 3098 | | | 1900 | | 640 | 2749 | | 1075 | 3057 | |
| Peak-hour factor, PHF | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Adj. Flow (vph) | 0 | 675 | 43 | 134 | 1418 | 22 | 12 | 86 | 34 | 33 | 344 | 52 |
| RTOR Reduction (vph) | 0 | 4 | 0 | 0 | 1 | 0 | 0 | 26 | 0 | 0 | 12 | 0 |
| Lane Group Flow (vph) | 0 | 714 | 0 | 0 | 1573 | 0 | 12 | 94 | 0 | 33 | 384 | 0 |
| Confl. Peds. (#/hr) | 100 | | 29 | 29 | | 100 | 24 | | 33 | 33 | | 24 |
| Confl. Bikes (#/hr) | | | 3 | | | 2 | | | 1 | | | 1 |
| Heavy Vehicles (%) | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% |
| Parking (#/hr) | | | | | | | | 8 | 8 | | | |
| Turn Type | | NA | | pm+pt | NA | | Perm | NA | | Perm | NA | |
| Protected Phases | | 2 | | 1 | 6 | | | 8 | | | 4 | |
| Permitted Phases | | | | 6 | | | 8 | | | 4 | | |
| Actuated Green, G (s) | | 59.5 | | | 67.2 | | 23.2 | 23.2 | | 23.2 | 23.2 | |
| Effective Green, g (s) | | 59.5 | | | 67.2 | | 23.2 | 23.2 | | 23.2 | 23.2 | |
| Actuated g/C Ratio | | 0.60 | | | 0.67 | | 0.23 | 0.23 | | 0.23 | 0.23 | |
| Clearance Time (s) | | 5.1 | | | 5.1 | | 4.5 | 4.5 | | 4.5 | 4.5 | |
| Vehicle Extension (s) | | 5.0 | | | 5.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | | 1843 | | | 1306 | | 148 | 637 | | 249 | 709 | |
| v/s Ratio Prot | | 0.23 | | | c0.05 | | | 0.03 | | | c0.13 | |
| v/s Ratio Perm | | 0.00 | | | c0.75 | | 0.02 | 0.45 | | 0.03 | 0.54 | |
| v/c Ratio | | 0.39 | | | 1.20 | | 0.08 | 0.15 | | 0.13 | 0.54 | |
| Uniform Delay, d1 | | 10.7 | | | 16.4 | | 30.1 | 30.5 | | 30.4 | 33.7 | |
| Progression Factor | | 1.00 | | | 0.52 | | 1.00 | 1.00 | | 0.43 | 0.39 | |
| Incremental Delay, d2 | | 0.6 | | | 96.2 | | 0.2 | 0.1 | | 0.2 | 0.7 | |
| Delay (s) | | 11.3 | | | 104.8 | | 30.3 | 30.6 | | 13.2 | 14.0 | |
| Level of Service | | B | | | F | | С | C | | В | 12.0 | |
| Approach LOC | | 11.3 | | | 104.8 F | | | 30.6 | | | 13.9 | |
| Approach LOS | | В | | | Г | | | С | | | В | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 64.2 | Н | CM 2000 | Level of | Service | | Е | | | |
| HCM 2000 Volume to Capacity | y ratio | | 1.07 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 100.0 | | um of lost | | | | 12.8 | | | |
| Intersection Capacity Utilizatio | n | | 109.4% | IC | CU Level | of Service | ! | | Н | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

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|--------------------------|-------|----------|-----------|-------|------------|------|------|----------|------|----------|----------|------|--|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR | |
| Lane Configurations | ች | ħβ | | ች | ∱ } | | ች | ^ | 7 | | ΦÞ | | |
| Traffic Volume (veh/h) | 75 | 550 | 77 | 131 | 1373 | 21 | 49 | 381 | 70 | 0 | 527 | 77 | |
| Future Volume (veh/h) | | 550 | 77 | 131 | 1373 | 21 | 49 | 381 | 70 | 0 | 527 | 77 | |
| Initial Q (Qb), veh | 0 | 10 | 0 | 0 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Ped-Bike Adj(A_pbT) | 1.00 | | 0.95 | 0.99 | | 0.96 | 0.98 | • | 0.91 | 1.00 | | 0.91 | |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Work Zone On Approa | | No | 1.00 | 1.00 | No | 1.00 | 1.00 | No | 1.00 | 1.00 | No | 1.00 | |
| Adj Sat Flow, veh/h/ln | 1660 | 1660 | 1660 | 1367 | 1367 | 1367 | 1660 | 1660 | 1660 | 0 | 1660 | 1660 | |
| Adj Flow Rate, veh/h | 79 | 579 | 70 | 138 | 1445 | 21 | 52 | 401 | 18 | 0 | 555 | 70 | |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | |
| Percent Heavy Veh, % | | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 0.50 | 3 | 3 | |
| Cap, veh/h | 72 | 2190 | 259 | 72 | 2031 | 28 | 130 | 817 | 333 | 0 | 721 | 91 | |
| Arrive On Green | 0.77 | 0.77 | 0.77 | 1.00 | 1.00 | 1.00 | 0.26 | 0.26 | 0.26 | 0.00 | 0.26 | 0.26 | |
| Sat Flow, veh/h | 357 | 2818 | 340 | 633 | 2619 | 38 | 781 | 3154 | 1285 | 0.00 | 2869 | 350 | |
| | 79 | 323 | 326 | | 716 | | 52 | 401 | 18 | 0 | 313 | 312 | |
| Grp Volume(v), veh/h | | | | 138 | | 750 | | | | | | | |
| Grp Sat Flow(s), veh/h/ | | 1577 | 1580 | 633 | 1299 | 1358 | 781 | 1577 | 1285 | 0 | 1577 | 1558 | |
| Q Serve(g_s), s | 6.5 | 5.8 | 5.8 | 2.5 | 0.0 | 0.0 | 6.6 | 10.8 | 1.1 | 0.0 | 18.4 | 18.5 | |
| Cycle Q Clear(g_c), s | 6.9 | 5.8 | 5.8 | 9.0 | 0.0 | 0.0 | 25.1 | 10.8 | 1.1 | 0.0 | 18.4 | 18.5 | |
| Prop In Lane | 1.00 | 4000 | 0.21 | 1.00 | 4007 | 0.03 | 1.00 | 0.47 | 1.00 | 0.00 | 400 | 0.22 | |
| Lane Grp Cap(c), veh/h | | 1222 | 1226 | 72 | 1007 | 1053 | 130 | 817 | 333 | 0 | 408 | 404 | |
| V/C Ratio(X) | 1.09 | 0.26 | 0.27 | 1.91 | 0.71 | 0.71 | 0.40 | 0.49 | 0.05 | 0.00 | 0.77 | 0.77 | |
| Avail Cap(c_a), veh/h | 347 | 1222 | 1225 | 522 | 1007 | 1053 | 130 | 817 | 333 | 0 | 408 | 404 | |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 2.00 | 2.00 | 2.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 0.51 | 0.51 | 0.51 | 0.92 | 0.92 | 0.92 | 0.00 | 0.33 | 0.33 | |
| Uniform Delay (d), s/ve | | 3.4 | 3.4 | 38.7 | 0.0 | 0.0 | 46.0 | 31.5 | 27.8 | 0.0 | 34.3 | 34.3 | |
| Incr Delay (d2), s/veh | | 0.5 | 0.5 | 436.1 | 2.2 | 2.1 | 1.8 | 0.4 | 0.1 | 0.0 | 2.9 | 3.1 | |
| Initial Q Delay(d3),s/ve | | 0.2 | 0.2 | 0.0 | 0.6 | 0.6 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | |
| %ile BackOfQ(50%),ve | | 2.1 | 2.1 | 10.5 | 0.8 | 0.8 | 1.4 | 4.2 | 0.3 | 0.0 | 7.3 | 7.3 | |
| Unsig. Movement Dela | • | | | | | | | | | | | | |
| LnGrp Delay(d),s/veh | 184.2 | 4.1 | 4.1 | 474.8 | 2.8 | 2.7 | 47.8 | 31.9 | 27.9 | 0.0 | 37.2 | 37.4 | |
| LnGrp LOS | F | Α | Α | F | Α | Α | D | С | С | Α | D | D | |
| Approach Vol, veh/h | | 728 | | | 1604 | | | 471 | | | 625 | | |
| Approach Delay, s/veh | | 23.6 | | | 43.4 | | | 33.5 | | | 37.3 | | |
| Approach LOS | | С | | | D | | | С | | | D | | |
| Timer - Assigned Phs | | 2 | | 4 | | 6 | | 8 | | | | | |
| Phs Duration (G+Y+Ro | c), s | 83.0 | | 31.0 | | 83.0 | | 31.0 | | | | | |
| Change Period (Y+Rc) | , . | 5.1 | | * 5.1 | | 5.1 | | 5.1 | | | | | |
| Max Green Setting (Gr | | 64.3 | | * 26 | | 64.3 | | 25.5 | | | | | |
| Max Q Clear Time (g_c | | 8.9 | | 27.1 | | 11.0 | | 20.5 | | | | | |
| Green Ext Time (p_c), | | 14.1 | | 0.0 | | 37.1 | | 1.8 | | | | | |
| Intersection Summary | | | | | | | | | | | | | |
| HCM 6th Ctrl Delay | | | 36.7 | | | | | | | | | | |
| HCM 6th LOS | | | 30.7 D | | | | | | | | | | |
| | | | U | | | | | | | | | | |
| Notes | | | | | | | | | | | | | |

^{*} HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

| • | → | • | • | • | • | • | † | / | / | ↓ | 4 | |
|-------------------------------|----------|------|-------|----------|------|------|----------|-------|------|----------|------|--|
| Movement EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR | |
| Lane Configurations | † | LDIT | ሻ | ^ | 7 | ሻ | † | TIDIT | ሻ | ^ | 7 | |
| Traffic Volume (veh/h) 1 | 482 | 60 | 76 | 1353 | 113 | 23 | 69 | 33 | 212 | 273 | 85 | |
| Future Volume (veh/h) 1 | 482 | 60 | 76 | 1353 | 113 | 23 | 69 | 33 | 212 | 273 | 85 | |
| Initial Q (Qb), veh 0 | 10 | 0 | 0 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Ped-Bike Adj(A_pbT) 1.00 | 10 | 0.97 | 0.99 | 10 | 0.97 | 0.95 | U | 0.92 | 0.94 | U | 0.94 | |
| Parking Bus, Adj 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Work Zone On Approach | No | 1.00 | 1.00 | No | 1.00 | 1.00 | No | 1.00 | 1.00 | No | 1.00 | |
| Adj Sat Flow, veh/h/ln 1660 | 1660 | 1660 | 1367 | 1367 | 1367 | 1660 | 1660 | 1660 | 1660 | 1660 | 1660 | |
| Adj Flow Rate, veh/h | 487 | 53 | 77 | 1367 | 89 | 23 | 70 | 33 | 214 | 276 | 67 | |
| Peak Hour Factor 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | |
| | 3 | 3 | 3 | 0.99 | | | 3 | 3 | 3 | | 3 | |
| Percent Heavy Veh, % 3 | | | | | 3 | 3 | | | | 3 | | |
| Cap, veh/h 36 | 1651 | 170 | 72 | 1505 | 649 | 291 | 468 | 200 | 415 | 1018 | 428 | |
| Arrive On Green 0.77 | 0.77 | 0.77 | 0.58 | 0.58 | 0.58 | 0.22 | 0.22 | 0.22 | 0.07 | 0.32 | 0.32 | |
| Sat Flow, veh/h 1 | 2799 | 303 | 702 | 2598 | 1120 | 977 | 2089 | 894 | 1581 | 3154 | 1327 | |
| Grp Volume(v), veh/h 288 | 0 | 253 | 77 | 1367 | 89 | 23 | 51 | 52 | 214 | 276 | 67 | |
| Grp Sat Flow(s), veh/h/ln1658 | 0 | 1444 | 702 | 1299 | 1120 | 977 | 1577 | 1405 | 1581 | 1577 | 1327 | |
| Q Serve(g_s), s 0.0 | 0.0 | 5.2 | 5.8 | 46.7 | 3.6 | 1.9 | 2.6 | 3.0 | 6.9 | 6.5 | 3.6 | |
| Cycle Q Clear(g_c), s 5.2 | 0.0 | 5.2 | 11.1 | 46.7 | 3.6 | 1.9 | 2.6 | 3.0 | 6.9 | 6.5 | 3.6 | |
| Prop In Lane 0.00 | | 0.21 | 1.00 | | 1.00 | 1.00 | | 0.64 | 1.00 | | 1.00 | |
| Lane Grp Cap(c), veh/h 993 | 0 | 837 | 72 | 1505 | 649 | 291 | 353 | 315 | 415 | 1018 | 428 | |
| V/C Ratio(X) 0.29 | 0.00 | 0.30 | 1.07 | 0.91 | 0.14 | 0.08 | 0.14 | 0.16 | 0.52 | 0.27 | 0.16 | |
| Avail Cap(c_a), veh/h 997 | 0 | 836 | 442 | 1505 | 649 | 346 | 442 | 394 | 415 | 1196 | 503 | |
| HCM Platoon Ratio 1.33 | 1.33 | 1.33 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Upstream Filter(I) 0.96 | 0.00 | 0.96 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Uniform Delay (d), s/veh 5.7 | 0.0 | 5.6 | 50.0 | 19.4 | 9.6 | 30.8 | 31.1 | 31.3 | 29.1 | 25.1 | 24.1 | |
| Incr Delay (d2), s/veh 0.7 | 0.0 | 0.9 | 126.4 | 9.6 | 0.4 | 0.1 | 0.2 | 0.2 | 0.5 | 0.1 | 0.2 | |
| Initial Q Delay(d3),s/veh 0.3 | 0.0 | 0.4 | 0.0 | 3.5 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | |
| %ile BackOfQ(50%),veh/lr2.2 | 0.0 | 2.0 | 4.3 | 16.7 | 0.9 | 0.5 | 1.0 | 1.0 | 1.5 | 2.5 | 1.2 | |
| Unsig. Movement Delay, s/veh | | | | | | | | | | | | |
| LnGrp Delay(d),s/veh 6.7 | 0.0 | 6.9 | 176.4 | 32.5 | 10.1 | 31.0 | 31.3 | 31.5 | 29.6 | 25.3 | 24.3 | |
| LnGrp LOS A | Α | Α | F | С | В | С | С | С | С | С | С | |
| Approach Vol, veh/h | 541 | | · · | 1533 | | | 126 | | | 557 | | |
| Approach Delay, s/veh | 6.8 | | | 38.4 | | | 31.3 | | | 26.8 | | |
| Approach LOS | A | | | D | | | C | | | C | | |
| | | | | | | | | | | | | |
| Timer - Assigned Phs | 2 | | 4 | | 6 | 7 | 8 | | | | | |
| Phs Duration (G+Y+Rc), s | 63.0 | | 37.0 | | 63.0 | 9.9 | 27.1 | | | | | |
| Change Period (Y+Rc), s | 5.1 | | * 4.7 | | 5.1 | 3.0 | * 4.7 | | | | | |
| Max Green Setting (Gmax), s | 52.3 | | * 38 | | 52.3 | 6.9 | * 28 | | | | | |
| Max Q Clear Time (g_c+l1), s | 7.2 | | 8.5 | | 48.7 | 8.9 | 5.0 | | | | | |
| Green Ext Time (p_c), s | 8.0 | | 2.2 | | 3.3 | 0.0 | 0.7 | | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 6th Ctrl Delay | | 29.5 | | | | | | | | | | |
| HCM 6th LOS | | C | | | | | | | | | | |
| Notes | | J | | | | | | | | | | |

^{*} HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

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|--|-------------|----------|-------|------|------|-------|------|----------|------|-------------|----------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | | LDIT | 1100 | 414 | 11511 | ሻ | ^ | ITEL | 052 | † | OBIT |
| raffic Volume (veh/h) | 0 | 0 | 0 | 61 | 333 | 62 | 93 | 497 | 0 | 0 | 563 | 136 |
| uture Volume (veh/h) | 0 | 0 | 0 | 61 | 333 | 62 | 93 | 497 | 0 | 0 | 563 | 136 |
| nitial Q (Qb), veh | | J | , , | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | | | | 1.00 | U | 0.91 | 0.99 | U | 1.00 | 1.00 | U | 0.96 |
| arking Bus, Adj | | | | 0.85 | 1.00 | 0.85 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.81 |
| Vork Zone On Approac | ·h | | | 0.00 | No | 0.00 | 1.00 | No | 1.00 | 1.00 | No | 0.01 |
| dj Sat Flow, veh/h/ln | <i>,</i> 11 | | | 1660 | 1660 | 1660 | 1660 | 1660 | 0 | 0 | 1660 | 1660 |
| dj Flow Rate, veh/h | | | | 66 | 358 | 45 | 100 | 534 | 0 | 0 | 605 | 113 |
| Peak Hour Factor | | | | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 |
| Percent Heavy Veh, % | | | | 3 | 3 | 3 | 3 | 3 | 0.93 | 0.93 | 3 | 3 |
| Cap, veh/h | | | | 114 | 646 | 85 | 408 | 1739 | 0 | 0 | 1312 | 244 |
| Arrive On Green | | | | 0.31 | 0.31 | 0.31 | 0.55 | 0.55 | 0.00 | 0.00 | 0.55 | 0.55 |
| | | | | 366 | 2070 | 271 | 724 | 3237 | 0.00 | 0.00 | 2462 | 443 |
| Sat Flow, veh/h | | | | | | | | | | | | 318 |
| Grp Volume(v), veh/h | | | | 249 | 0 | 220 | 100 | 534 | 0 | 0 | 400 | |
| Grp Sat Flow(s),veh/h/li | n | | | 1385 | 0 | 1324 | 724 | 1577 | 0 | 0 | 1577 | 1245 |
| Q Serve(g_s), s | | | | 9.1 | 0.0 | 8.2 | 5.8 | 5.5 | 0.0 | 0.0 | 9.2 | 9.2 |
| Cycle Q Clear(g_c), s | | | | 9.1 | 0.0 | 8.2 | 15.0 | 5.5 | 0.0 | 0.0 | 9.2 | 9.2 |
| Prop In Lane | | | | 0.26 | • | 0.20 | 1.00 | 4700 | 0.00 | 0.00 | 070 | 0.36 |
| ane Grp Cap(c), veh/h | | | | 432 | 0 | 413 | 408 | 1739 | 0 | 0 | 870 | 687 |
| //C Ratio(X) | | | | 0.58 | 0.00 | 0.53 | 0.25 | 0.31 | 0.00 | 0.00 | 0.46 | 0.46 |
| vail Cap(c_a), veh/h | | | | 595 | 0 | 569 | 408 | 1739 | 0 | 0 | 870 | 687 |
| CM Platoon Ratio | | | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| pstream Filter(I) | | | | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 0.00 | 0.00 | 0.54 | 0.54 |
| niform Delay (d), s/vel | h | | | 17.3 | 0.0 | 17.0 | 12.6 | 7.3 | 0.0 | 0.0 | 8.1 | 8.1 |
| ncr Delay (d2), s/veh | | | | 1.2 | 0.0 | 1.1 | 1.4 | 0.5 | 0.0 | 0.0 | 0.9 | 1.2 |
| nitial Q Delay(d3),s/veh | | | | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),vel | | | | 2.8 | 0.0 | 2.4 | 1.0 | 1.7 | 0.0 | 0.0 | 2.8 | 2.3 |
| Insig. Movement Delay | /, s/veh | | | | | | | | | | | |
| nGrp Delay(d),s/veh | | | | 18.6 | 0.0 | 18.1 | 14.0 | 7.7 | 0.0 | 0.0 | 9.0 | 9.3 |
| nGrp LOS | | | | В | A | В | В | A | Α | A | A | A |
| Approach Vol, veh/h | | | | | 469 | | | 634 | | | 718 | |
| pproach Delay, s/veh | | | | | 18.3 | | | 8.7 | | | 9.2 | |
| pproach LOS | | | | | В | | | Α | | | Α | |
| imer - Assigned Phs | | 2 | | | | 6 | | 8 | | | | |
| Phs Duration (G+Y+Rc) | ۱ ۹ | 37.3 | | | | 37.3 | | 22.7 | | | | |
| Change Period (Y+Rc), | | * 4.2 | | | | * 4.2 | | 4.0 | | | | |
| Max Green Setting (Gm | | * 26 | | | | * 26 | | 25.8 | | | | |
| nax Green Setting (Gir Nax Q Clear Time (g_c | | 17.0 | | | | 11.2 | | 11.1 | | | | |
| iax Q Clear Time (g_c ireen Ext Time (p_c), s | | 4.4 | | | | 6.9 | | 2.6 | | | | |
| (i — /- |) | 4.4 | | | | 0.9 | | 2.0 | | | | |
| tersection Summary | | | 4.1.1 | | | | | | | | | |
| HCM 6th Ctrl Delay | | | 11.4 | | | | | | | | | |
| HCM 6th LOS | | | В | | | | | | | | | |
| Notes | | | | | | | | | | | | |

^{*} HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

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|-----------------------------------|---------|----------|-------|------|-------------|----------|---------|----------|-------------|----------|------------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | | | | €1 } | | ሻ | ^ | | | ∱ ∱ | |
| Traffic Volume (vph) | 0 | 0 | 0 | 43 | 329 | 41 | 22 | 70 | 0 | 0 | 235 | 174 |
| Future Volume (vph) | 0 | 0 | 0 | 43 | 329 | 41 | 22 | 70 | 0 | 0 | 235 | 174 |
| Ideal Flow (vphpl) | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 |
| Total Lost time (s) | | | | | 3.0 | | 4.0 | 4.0 | | | 4.0 | |
| Lane Util. Factor | | | | | 0.95 | | 1.00 | 0.95 | | | 0.95 | |
| Frpb, ped/bikes | | | | | 1.00 | | 1.00 | 1.00 | | | 0.99 | |
| Flpb, ped/bikes | | | | | 1.00 | | 1.00 | 1.00 | | | 1.00 | |
| Frt | | | | | 0.98 | | 1.00 | 1.00 | | | 0.94 | |
| Flt Protected | | | | | 0.99 | | 0.95 | 1.00 | | | 1.00 | |
| Satd. Flow (prot) | | | | | 2870 | | 1568 | 2885 | | | 2693 | |
| Flt Permitted | | | | | 0.99 | | 0.25 | 1.00 | | | 1.00 | |
| Satd. Flow (perm) | | | | | 2870 | | 413 | 2885 | | | 2693 | |
| Peak-hour factor, PHF | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 |
| Adj. Flow (vph) | 0 | 0 | 0 | 61 | 470 | 59 | 31 | 100 | 0 | 0 | 336 | 249 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 11 | 0 | 0 | 0 | 0 | 0 | 191 | 0 |
| Lane Group Flow (vph) | 0 | 0 | 0 | 0 | 579 | 0 | 31 | 100 | 0 | 0 | 394 | 0 |
| Confl. Bikes (#/hr) | | | 1 | | | 1 | | | 1 | | | 1 |
| Heavy Vehicles (%) | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% |
| Parking (#/hr) | | | | 6 | 6 | 4 | | 12 | | | 11 | 11 |
| Turn Type | | | | Perm | NA | | Perm | NA | | | NA | |
| Protected Phases | | | | | 6 | | | 8 | | | 4 | |
| Permitted Phases | | | | 6 | | | 8 | | | | | |
| Actuated Green, G (s) | | | | | 23.0 | | 16.0 | 16.0 | | | 16.0 | |
| Effective Green, g (s) | | | | | 23.0 | | 16.0 | 16.0 | | | 16.0 | |
| Actuated g/C Ratio | | | | | 0.33 | | 0.23 | 0.23 | | | 0.23 | |
| Clearance Time (s) | | | | | 3.0 | | 4.0 | 4.0 | | | 4.0 | |
| Vehicle Extension (s) | | | | | 2.0 | | 2.0 | 2.0 | | | 2.0 | |
| Lane Grp Cap (vph) | | | | | 943 | | 94 | 659 | | | 615 | |
| v/s Ratio Prot | | | | | | | | 0.03 | | | c0.15 | |
| v/s Ratio Perm | | | | | 0.20 | | 0.08 | | | | | |
| v/c Ratio | | | | | 0.61 | | 0.33 | 0.15 | | | 0.64 | |
| Uniform Delay, d1 | | | | | 19.8 | | 22.5 | 21.6 | | | 24.4 | |
| Progression Factor | | | | | 1.00 | | 1.00 | 1.00 | | | 1.00 | |
| Incremental Delay, d2 | | | | | 3.0 | | 9.1 | 0.5 | | | 5.0 | |
| Delay (s) | | | | | 22.7 | | 31.7 | 22.1 | | | 29.4 | |
| Level of Service | | | | | С | | С | С | | | С | |
| Approach Delay (s) | | 0.0 | | | 22.7 | | | 24.3 | | | 29.4 | |
| Approach LOS | | Α | | | С | | | С | | | С | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 25.9 | H | CM 2000 | Level of | Service | | С | | | |
| HCM 2000 Volume to Capacity | y ratio | | 0.41 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 70.0 | Sı | um of lost | time (s) | | | 11.0 | | | |
| Intersection Capacity Utilization | n | | 40.1% | | U Level | | ! | | Α | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

| Intersection | | | | | | | | | | | | |
|------------------------|------|------|----------|--------|-------|------|------|------|------|---------|------|------|
| Int Delay, s/veh | 2.8 | | | | | | | | | | | |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | | | | 4₽ | | | | | | ħβ | |
| Traffic Vol, veh/h | 0 | 0 | 0 | 0 | 300 | 0 | 0 | 0 | 0 | 0 | 0 | 114 |
| Future Vol, veh/h | 0 | 0 | 0 | 0 | 300 | 0 | 0 | 0 | 0 | 0 | 0 | 114 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 79 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | _ | - | - | - | - | - | - | - | - | - |
| Veh in Median Storage, | ,# - | 2 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, % | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 82 | 82 | 82 | 82 | 82 | 82 | 82 | 82 | 82 | 82 | 82 | 82 |
| Heavy Vehicles, % | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 |
| Mvmt Flow | 0 | 0 | 0 | 0 | 366 | 0 | 0 | 0 | 0 | 0 | 0 | 139 |
| | | | | | | | | | | | | |
| Major/Minor | | | <u> </u> | Major2 | | | | | N | /linor2 | | |
| Conflicting Flow All | | | | 79 | 0 | 0 | | | | - | 445 | 183 |
| Stage 1 | | | | - | - | - | | | | - | 366 | - |
| Stage 2 | | | | - | - | - | | | | - | 79 | - |
| Critical Hdwy | | | | 4.16 | - | - | | | | - | 6.56 | 6.96 |
| Critical Hdwy Stg 1 | | | | - | - | - | | | | - | 5.56 | - |
| Critical Hdwy Stg 2 | | | | - | - | - | | | | - | - | - |
| Follow-up Hdwy | | | | 2.23 | - | - | | | | - | 4.03 | 3.33 |
| Pot Cap-1 Maneuver | | | | 1510 | - | 0 | | | | 0 | 504 | 825 |
| Stage 1 | | | | - | - | 0 | | | | 0 | 619 | - |
| Stage 2 | | | | - | - | 0 | | | | 0 | - | - |
| Platoon blocked, % | | | | | - | | | | | | | |
| Mov Cap-1 Maneuver | | | | 1510 | - | - | | | | - | 0 | 825 |
| Mov Cap-2 Maneuver | | | | - | - | - | | | | - | 0 | - |
| Stage 1 | | | | - | - | - | | | | - | 0 | - |
| Stage 2 | | | | - | - | - | | | | - | 0 | - |
| | | | | | | | | | | | | |
| Approach | | | | WB | | | | | | SB | | |
| HCM Control Delay, s | | | | 0 | | | | | | 10.2 | | |
| HCM LOS | | | | | | | | | | В | | |
| | | | | | | | | | | | | |
| Minor Lane/Major Mvm | t | WBL | WBT S | SBLn1 | SBLn2 | | | | | | | |
| Capacity (veh/h) | | 1510 | - | - | 825 | | | | | | | |
| HCM Lane V/C Ratio | | - | - | - | 0.169 | | | | | | | |
| HCM Control Delay (s) | | 0 | - | 0 | 10.2 | | | | | | | |
| HCM Lane LOS | | Α | - | Α | В | | | | | | | |
| HCM 95th %tile Q(veh) | | 0 | - | - | 0.6 | | | | | | | |
| | | | | | | | | | | | | |

| Intersection | | | | | | |
|------------------------|----------|-------|---------|----------|----------|------|
| Int Delay, s/veh | 0.2 | | | | | |
| | | EDD | \A/D1 | MOT | ND: | NDD |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | ΦÞ | | - ሽ | ^ | | 7 |
| Traffic Vol, veh/h | 613 | 68 | 54 | 1499 | 0 | 0 |
| Future Vol, veh/h | 613 | 68 | 54 | 1499 | 0 | 0 |
| Conflicting Peds, #/hr | 0 | 31 | 31 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | 25 | - | - | 0 |
| Veh in Median Storage | , # 0 | - | - | 0 | 0 | - |
| Grade, % | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 94 | 94 | 94 | 94 | 94 | 94 |
| Heavy Vehicles, % | 3 | 3 | 3 | 3 | 3 | 3 |
| Mymt Flow | 652 | 72 | 57 | 1595 | 0 | 0 |
| WWITH TOW | 002 | 12 | O1 | 1000 | U | U |
| | | | | | | |
| Major/Minor N | /lajor1 | N | //ajor2 | N | /linor1 | |
| Conflicting Flow All | 0 | 0 | 755 | 0 | - | 393 |
| Stage 1 | - | - | - | - | - | - |
| Stage 2 | _ | - | _ | - | - | - |
| Critical Hdwy | - | _ | 4.16 | _ | _ | 6.96 |
| Critical Hdwy Stg 1 | _ | _ | - | _ | _ | - |
| Critical Hdwy Stg 2 | _ | _ | _ | _ | _ | _ |
| Follow-up Hdwy | <u>-</u> | _ | 2.23 | _ | - | 3.33 |
| Pot Cap-1 Maneuver | _ | _ | 845 | _ | 0 | 603 |
| Stage 1 | | _ | - | _ | 0 | - |
| Stage 2 | _ | | _ | | 0 | _ |
| | _ | _ | _ | _ | U | _ |
| Platoon blocked, % | - | - | 000 | - | | F0F |
| Mov Cap-1 Maneuver | - | - | 820 | - | - | 585 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - |
| Stage 1 | - | - | - | - | - | - |
| Stage 2 | - | - | - | - | - | - |
| | | | | | | |
| Approach | EB | | WB | | NB | |
| HCM Control Delay, s | 0 | | 0.3 | | 0 | |
| HCM LOS | U | | 0.3 | | | |
| LOS TOUR | | | | | Α | |
| | | | | | | |
| Minor Lane/Major Mvm | t 1 | NBLn1 | EBT | EBR | WBL | WBT |
| Capacity (veh/h) | | _ | _ | | 820 | |
| HCM Lane V/C Ratio | | _ | _ | _ | 0.07 | _ |
| HCM Control Delay (s) | | 0 | | _ | 9.7 | |
| HCM Lane LOS | | | | | 9.7 A | |
| | | Α | - | - | | - |
| HCM 95th %tile Q(veh) | | - | - | - | 0.2 | - |

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|---------------------------------------|------------|------------|------------|-------|------------|------|------|------------|------|------------|----------|----------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 7 | ∱ ⊅ | | ሻ | ∱ ∱ | | | ∱ ⊅ | | 7 | ^ | 7 |
| Traffic Volume (veh/h) | 35 | 1470 | 46 | 73 | 1355 | 48 | 0 | 228 | 58 | 30 | 162 | 42 |
| Future Volume (veh/h) | 35 | 1470 | 46 | 73 | 1355 | 48 | 0 | 228 | 58 | 30 | 162 | 42 |
| Initial Q (Qb), veh | 0 | 15 | 0 | 0 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | 4.00 | 0.97 | 1.00 | 4.00 | 0.97 | 1.00 | 4.00 | 0.97 | 0.98 | 4.00 | 0.89 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach | 4007 | No | 4007 | 4007 | No | 4007 | ^ | No | 4000 | 4000 | No | 4000 |
| Adj Sat Flow, veh/h/ln | 1367 | 1367 | 1367 | 1367 | 1367 | 1367 | 0 | 1660 | 1660 | 1660 | 1660 | 1660 |
| Adj Flow Rate, veh/h | 39 0.90 | 1633 | 49 0.90 | 81 | 1506 | 50 | 0 | 253 | 43 | 33 0.90 | 180 | 17 |
| Peak Hour Factor Percent Heavy Veh, % | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Cap, veh/h | 100 | 1750 | 36 | 72 | 1731 | 52 | 0 | 614 | 103 | 227 | 720 | 286 |
| Arrive On Green | 0.67 | 0.67 | 0.67 | 0.67 | 0.67 | 0.67 | 0.00 | 0.23 | 0.23 | 0.23 | 0.23 | 0.23 |
| Sat Flow, veh/h | 271 | 2573 | 77 | 240 | 2563 | 85 | 0.00 | 2774 | 450 | 1058 | 3154 | 1254 |
| Grp Volume(v), veh/h | 39 | 822 | 860 | 81 | 761 | 795 | 0 | 147 | 149 | 33 | 180 | 17 |
| Grp Sat Flow(s), veh/h/ln | 271 | 1299 | 1351 | 240 | 1299 | 1349 | 0 | 1577 | 1564 | 1058 | 1577 | 1254 |
| Q Serve(g_s), s | 13.4 | 56.4 | 57.4 | 9.9 | 46.4 | 46.9 | 0.0 | 7.9 | 8.2 | 2.7 | 4.7 | 1.1 |
| Cycle Q Clear(g_c), s | 60.3 | 56.4 | 57.4 | 67.3 | 46.4 | 46.9 | 0.0 | 7.9 | 8.2 | 10.9 | 4.7 | 1.1 |
| Prop In Lane | 1.00 | 00.1 | 0.06 | 1.00 | 10.1 | 0.06 | 0.00 | 1.0 | 0.29 | 1.00 | ••• | 1.00 |
| Lane Grp Cap(c), veh/h | 100 | 874 | 912 | 72 | 874 | 909 | 0 | 360 | 357 | 227 | 720 | 286 |
| V/C Ratio(X) | 0.39 | 0.94 | 0.94 | 1.12 | 0.87 | 0.87 | 0.00 | 0.41 | 0.42 | 0.15 | 0.25 | 0.06 |
| Avail Cap(c_a), veh/h | 127 | 874 | 909 | 96 | 874 | 908 | 0 | 420 | 416 | 267 | 839 | 334 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 0.32 | 0.32 | 0.32 | 0.00 | 0.81 | 0.81 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 43.4 | 15.6 | 15.6 | 50.0 | 13.5 | 13.6 | 0.0 | 32.8 | 32.9 | 37.6 | 31.6 | 30.2 |
| Incr Delay (d2), s/veh | 11.1 | 19.0 | 18.8 | 97.7 | 4.2 | 4.1 | 0.0 | 0.6 | 0.6 | 0.3 | 0.2 | 0.1 |
| Initial Q Delay(d3),s/veh | 0.0 | 8.9 | 8.6 | 0.0 | 1.8 | 1.7 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/ln | 1.2 | 21.7 | 22.6 | 3.7 | 13.4 | 13.9 | 0.0 | 3.1 | 3.2 | 0.7 | 1.8 | 0.3 |
| Unsig. Movement Delay, s/veh | | | | | | | | | | | | |
| LnGrp Delay(d),s/veh | 54.5 | 43.5 | 43.0 | 147.7 | 19.5 | 19.4 | 0.0 | 33.4 | 33.6 | 37.9 | 31.8 | 30.3 |
| LnGrp LOS | D | D | D | F | В | В | A | С | С | D | С | <u>C</u> |
| Approach Vol, veh/h | | 1721 | | | 1637 | | | 296 | | | 230 | |
| Approach Delay, s/veh | | 43.5 | | | 25.8 | | | 33.5 | | | 32.5 | |
| Approach LOS | | D | | | С | | | С | | | С | |
| Timer - Assigned Phs | | 2 | | 4 | | 6 | | 8 | | | | |
| Phs Duration (G+Y+Rc), s | | 72.7 | | 27.3 | | 72.7 | | 27.3 | | | | |
| Change Period (Y+Rc), s | | 5.4 | | 4.5 | | 5.4 | | 4.5 | | | | |
| Max Green Setting (Gmax), s | | 63.5 | | 26.6 | | 63.5 | | 26.6 | | | | |
| Max Q Clear Time (g_c+l1), s | | 62.3 | | 12.9 | | 69.3 | | 10.2 | | | | |
| Green Ext Time (p_c), s | | 1.2 | | 1.1 | | 0.0 | | 1.6 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 6th Ctrl Delay | | | 34.7 | | | | | | | | | |
| HCM 6th LOS | | | С | | | | | | | | | |

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|---------------------------------------|----------|-----------|-----------|------------|----------|-----------|-----------|-----------|-----------|------|-------|-----------|--|
| Movement EE | 3L | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR | |
| Lane Configurations | ķ | ħβ | | × | ħβ | | Ť | ħβ | | ň | ħβ | | |
| Traffic Volume (veh/h) 4 | 46 | 1317 | 42 | 85 | 1327 | 32 | 78 | 426 | 166 | 36 | 355 | 63 | |
| | 46 | 1317 | 42 | 85 | 1327 | 32 | 78 | 426 | 166 | 36 | 355 | 63 | |
| , , , , , , , , , , , , , , , , , , , | 0 | 15 | 0 | 0 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Ped-Bike Adj(A_pbT) 1.0 | | | 0.97 | 1.00 | | 0.98 | 0.99 | | 0.97 | 0.99 | | 0.97 | |
| Parking Bus, Adj 1.0 | 00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Work Zone On Approach | | No | | | No | | | No | | | No | | |
| Adj Sat Flow, veh/h/ln 136 | | 1367 | 1367 | 1367 | 1367 | 1367 | 1660 | 1660 | 1660 | 1660 | 1660 | 1660 | |
| | 51 | 1463 | 45 | 94 | 1474 | 34 | 87 | 473 | 152 | 40 | 394 | 54 | |
| Peak Hour Factor 0.9 | | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | |
| Percent Heavy Veh, % | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | |
| Cap, veh/h | | 1662 | 42 | 72 | 1672 | 34 | 187 | 583 | 186 | 132 | 694 | 94 | |
| Arrive On Green 0.6 | | 0.64 | 0.64 | 0.64 | 0.64 | 0.64 | 0.50 | 0.50 | 0.50 | 0.25 | 0.25 | 0.25 | |
| · | 84 | 2570 | 79 | 284 | 2594 | 60 | 924 | 2333 | 743 | 788 | 2778 | 378 | |
| | 51 | 738 | 770 | 94 | 737 | 771 | 87 | 318 | 307 | 40 | 222 | 226 | |
| Grp Sat Flow(s), veh/h/ln 28 | | 1299 | 1350 | 284 | 1299 | 1355 | 924 | 1577 | 1499 | 788 | 1577 | 1578 | |
| Q Serve(g_s), s 17 | | 47.1 | 47.5 | 16.8 | 46.9 | 47.2 | 8.7 | 17.0 | 17.3 | 4.9 | 12.3 | 12.5 | |
| Cycle Q Clear(g_c), s 64 | | 47.1 | 47.5 | 64.2 | 46.9 | 47.2 | 21.2 | 17.0 | 17.3 | 22.3 | 12.3 | 12.5 | |
| Prop In Lane 1.0 | | | 0.06 | 1.00 | | 0.04 | 1.00 | | 0.50 | 1.00 | | 0.24 | |
| Lane Grp Cap(c), veh/h 10 | | 834 | 869 | 72 | 834 | 871 | 187 | 394 | 374 | 132 | 394 | 394 | |
| V/C Ratio(X) 0.5 | | 0.88 | 0.89 | 1.31 | 0.88 | 0.88 | 0.47 | 0.81 | 0.82 | 0.30 | 0.56 | 0.57 | |
| – , | 20 | 834 | 867 | 120 | 834 | 870 | 202 | 420 | 399 | 145 | 420 | 420 | |
| HCM Platoon Ratio 1.0 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 2.00 | 2.00 | 2.00 | 1.00 | 1.00 | 1.00 | |
| Upstream Filter(I) 0.0 | | 0.09 | 0.09 | 1.00 | 1.00 | 1.00 | 0.65 | 0.65 | 0.65 | 1.00 | 1.00 | 1.00 | |
| Uniform Delay (d), s/veh 45 | | 15.8 | 15.8 | 50.0 | 15.4 | 15.4 | 29.9 | 23.0 | 23.1 | 44.9 | 32.8 | 32.8 | |
| 3 (), | .6 | 1.4 | 1.4 | 208.1 | 13.1 | 12.7 | 1.2 | 7.2 | 8.2 | 1.3 | 1.5 | 1.7 | |
| , , , , , , , , , , , , , , , , , , , | 0.0 | 5.0 | 4.7 | 0.0 | 2.2 | 2.1 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | |
| %ile BackOfQ(50%),veh/lnl | | 14.5 | 15.0 | 5.9 | 16.1 | 16.7 | 1.7 | 5.4 | 5.3 | 1.0 | 4.9 | 5.0 | |
| Unsig. Movement Delay, s/v | | 00.0 | 24.0 | 050.4 | 20.7 | 20.0 | 24.4 | 20.0 | 24.2 | 46.0 | 242 | 24 5 | |
| LnGrp Delay(d),s/veh 46 | 0.0 D | 22.3 C | 21.9 C | 258.1 F | 30.7 | 30.2 C | 31.1 C | 30.2 C | 31.3 C | 46.2 | 34.3 | 34.5 C | |
| | ט | | U | | C 4000 | U | U | | U | D | C 400 | U | |
| Approach Vol, veh/h | | 1559 | | | 1602 | | | 712 | | | 488 | | |
| Approach LOS | | 22.9 | | | 43.8 | | | 30.8 | | | 35.4 | | |
| Approach LOS | | С | | | D | | | С | | | D | | |
| Timer - Assigned Phs | | 2 | | 4 | | 6 | | 8 | | | | | |
| Phs Duration (G+Y+Rc), s | | 69.6 | | 30.4 | | 69.6 | | 30.4 | | | | | |
| Change Period (Y+Rc), s | | 5.4 | | 5.4 | | 5.4 | | 5.4 | | | | | |
| Max Green Setting (Gmax), | | 62.6 | | 26.6 | | 62.6 | | 26.6 | | | | | |
| Max Q Clear Time (g_c+l1) |), S | 66.2 | | 24.3 | | 66.2 | | 23.2 | | | | | |
| Green Ext Time (p_c), s | | 0.0 | | 0.7 | | 0.0 | | 1.5 | | | | | |
| Intersection Summary | | | | | | | | | | | | | |
| HCM 6th Ctrl Delay | | | 33.3 | | | | | | | | | | |
| HCM 6th LOS | | | С | | | | | | | | | | |

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|----------------------------------|---------|------------|--------|-------|------------|------------|---------|------------|------|----------|------------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | ∱ ∱ | | | 413- | | 7 | ∱ } | | ሻ | ↑ ↑ | |
| Traffic Volume (vph) | 0 | 1331 | 90 | 91 | 724 | 48 | 46 | 239 | 94 | 41 | 191 | 50 |
| Future Volume (vph) | 0 | 1331 | 90 | 91 | 724 | 48 | 46 | 239 | 94 | 41 | 191 | 50 |
| Ideal Flow (vphpl) | 1400 | 1400 | 1400 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 |
| Total Lost time (s) | | 5.1 | | | 5.1 | | 4.5 | 4.5 | | 4.5 | 4.5 | |
| Lane Util. Factor | | 0.95 | | | 0.95 | | 1.00 | 0.95 | | 1.00 | 0.95 | |
| Frpb, ped/bikes | | 0.98 | | | 0.98 | | 1.00 | 0.92 | | 1.00 | 0.93 | |
| Flpb, ped/bikes | | 1.00 | | | 1.00 | | 0.79 | 1.00 | | 0.84 | 1.00 | |
| Frt | | 0.99 | | | 0.99 | | 1.00 | 0.96 | | 1.00 | 0.97 | |
| Flt Protected | | 1.00 | | | 0.99 | | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | | 2516 | | | 3030 | | 1235 | 2567 | | 1323 | 2835 | |
| FIt Permitted | | 1.00 | | | 0.57 | | 0.55 | 1.00 | | 0.44 | 1.00 | |
| Satd. Flow (perm) | | 2516 | | | 1744 | | 717 | 2567 | | 615 | 2835 | |
| Peak-hour factor, PHF | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Adj. Flow (vph) | 0 | 1401 | 95 | 96 | 762 | 51 | 48 | 252 | 99 | 43 | 201 | 53 |
| RTOR Reduction (vph) | 0 | 4 | 0 | 0 | 4 | 0 | 0 | 41 | 0 | 0 | 24 | 0 |
| Lane Group Flow (vph) | 0 | 1492 | 0 | 0 | 905 | 0 | 48 | 310 | 0 | 43 | 230 | 0 |
| Confl. Peds. (#/hr) | 423 | | 174 | 174 | | 423 | 282 | | 215 | 215 | | 282 |
| Confl. Bikes (#/hr) | | | 6 | | | 1 | | | 1 | | | 1 |
| Heavy Vehicles (%) | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% |
| Parking (#/hr) | | | | | | | | 8 | 8 | | | |
| Turn Type | | NA | | pm+pt | NA | | Perm | NA | | Perm | NA | |
| Protected Phases | | 2 | | 1 | 6 | | | 8 | | | 4 | |
| Permitted Phases | | | | 6 | | | 8 | | | 4 | | |
| Actuated Green, G (s) | | 59.5 | | | 67.2 | | 23.2 | 23.2 | | 23.2 | 23.2 | |
| Effective Green, g (s) | | 59.5 | | | 67.2 | | 23.2 | 23.2 | | 23.2 | 23.2 | |
| Actuated g/C Ratio | | 0.60 | | | 0.67 | | 0.23 | 0.23 | | 0.23 | 0.23 | |
| Clearance Time (s) | | 5.1 | | | 5.1 | | 4.5 | 4.5 | | 4.5 | 4.5 | |
| Vehicle Extension (s) | | 5.0 | | | 5.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | | 1497 | | | 1229 | | 166 | 595 | | 142 | 657 | |
| v/s Ratio Prot | | c0.59 | | | c0.03 | | | c0.12 | | | 0.08 | |
| v/s Ratio Perm | | | | | 0.46 | | 0.07 | | | 0.07 | | |
| v/c Ratio | | 1.00 | | | 0.74 | | 0.29 | 0.52 | | 0.30 | 0.35 | |
| Uniform Delay, d1 | | 20.1 | | | 10.6 | | 31.6 | 33.5 | | 31.7 | 32.1 | |
| Progression Factor | | 1.00 | | | 0.80 | | 1.00 | 1.00 | | 0.57 | 0.52 | |
| Incremental Delay, d2 | | 22.4 | | | 1.8 | | 1.0 | 0.8 | | 1.0 | 0.3 | |
| Delay (s) | | 42.6 | | | 10.3 | | 32.6 | 34.4 | | 19.1 | 16.9 | |
| Level of Service | | D | | | В | | С | С | | В | В | |
| Approach Delay (s) | | 42.6 | | | 10.3 | | | 34.1 | | | 17.3 | |
| Approach LOS | | D | | | В | | | С | | | В | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 29.6 | Н | CM 2000 | Level of | Service | | С | | | |
| HCM 2000 Volume to Capacit | v ratio | | 0.86 | | | | | | | | | |
| Actuated Cycle Length (s) | , | | 100.0 | S | um of lost | t time (s) | | | 12.8 | | | |
| Intersection Capacity Utilizatio | n | | 121.2% | | CU Level | | ! | | Н | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

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|--|----------|------------|-----------|-------|-----------|------|------|-----------|------|----------|-----------|------|--|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR | |
| Lane Configurations | ች | ∱ } | | ች | † | | ች | ^ | 7 | | ħβ | | |
| Traffic Volume (veh/h) | 131 | 1193 | 145 | 98 | 737 | 48 | 77 | 522 | 157 | 0 | 437 | 69 | |
| Future Volume (veh/h) | | 1193 | 145 | 98 | 737 | 48 | 77 | 522 | 157 | 0 | 437 | 69 | |
| Initial Q (Qb), veh | 0 | 10 | 0 | 0 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Ped-Bike Adj(A_pbT) | 0.97 | 10 | 0.90 | 1.00 | 10 | 0.90 | 0.95 | | 0.82 | 1.00 | Ū | 0.83 | |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Work Zone On Approa | | No | 1.00 | 1.00 | No | 1.00 | 1.00 | No | 1.00 | 1.00 | No | 1.00 | |
| Adj Sat Flow, veh/h/ln | 1367 | 1367 | 1367 | 1660 | 1660 | 1660 | 1660 | 1660 | 1660 | 0 | 1660 | 1660 | |
| Adj Flow Rate, veh/h | 138 | 1256 | 146 | 103 | 776 | 46 | 81 | 549 | 138 | 0 | 460 | 61 | |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | |
| Percent Heavy Veh, % | | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 0.93 | 3 | 3 | |
| | 72 | 1806 | 200 | 72 | 2332 | 136 | 161 | 817 | 299 | 0 | 707 | 93 | |
| Cap, veh/h Arrive On Green | | | | | | | | 0.26 | 0.26 | 0.00 | 0.26 | 0.26 | |
| | 0.77 | 0.77 | 0.77 | 1.00 | 1.00 | 1.00 | 0.26 | | | | | | |
| Sat Flow, veh/h | 529 | 2316 | 268 | 381 | 3005 | 178 | 833 | 3154 | 1156 | 0 | 2812 | 358 | |
| Grp Volume(v), veh/h | 138 | 701 | 701 | 103 | 407 | 415 | 81 | 549 | 138 | 0 | 264 | 257 | |
| Grp Sat Flow(s),veh/h/ | | 1299 | 1285 | 381 | 1577 | 1606 | 833 | 1577 | 1156 | 0 | 1577 | 1509 | |
| Q Serve(g_s), s | 8.1 | 26.4 | 27.0 | 15.2 | 0.0 | 0.0 | 9.6 | 15.6 | 10.0 | 0.0 | 14.9 | 15.2 | |
| Cycle Q Clear(g_c), s | 8.5 | 26.4 | 27.0 | 43.6 | 0.0 | 0.0 | 24.9 | 15.6 | 10.0 | 0.0 | 14.9 | 15.2 | |
| Prop In Lane | 1.00 | | 0.21 | 1.00 | | 0.11 | 1.00 | | 1.00 | 0.00 | | 0.24 | |
| Lane Grp Cap(c), veh/l | | 1007 | 998 | 72 | 1222 | 1245 | 161 | 817 | 299 | 0 | 408 | 391 | |
| V/C Ratio(X) | 1.91 | 0.70 | 0.70 | 1.43 | 0.33 | 0.33 | 0.50 | 0.67 | 0.46 | 0.00 | 0.65 | 0.66 | |
| Avail Cap(c_a), veh/h | 480 | 1007 | 996 | 259 | 1222 | 1244 | 161 | 817 | 299 | 0 | 408 | 391 | |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 2.00 | 2.00 | 2.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 0.90 | 0.90 | 0.90 | 0.94 | 0.94 | 0.94 | 0.00 | 0.70 | 0.70 | |
| Uniform Delay (d), s/ve | eh 50.0 | 5.9 | 5.9 | 38.7 | 0.0 | 0.0 | 44.2 | 33.2 | 31.2 | 0.0 | 33.0 | 33.1 | |
| Incr Delay (d2), s/veh | 456.2 | 4.0 | 4.1 | 250.1 | 0.7 | 0.6 | 2.3 | 2.0 | 1.0 | 0.0 | 2.5 | 2.8 | |
| Initial Q Delay(d3),s/ve | | 0.6 | 0.6 | 0.0 | 0.2 | 0.2 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | |
| %ile BackOfQ(50%),ve | | 7.5 | 7.5 | 6.8 | 0.3 | 0.3 | 2.1 | 6.2 | 2.9 | 0.0 | 5.9 | 5.9 | |
| Jnsig. Movement Dela | | | | | | | | | | | | | |
| LnGrp Delay(d),s/veh | • | 10.4 | 10.7 | 288.9 | 0.8 | 0.8 | 46.5 | 35.3 | 32.2 | 0.0 | 35.4 | 35.9 | |
| LnGrp LOS | F | В | В | F | A | A | D | D | C | A | D | D | |
| Approach Vol, veh/h | | 1540 | | | 925 | | | 768 | | | 521 | | |
| Approach Vol, veli/li Approach Delay, s/veh | <u> </u> | 55.0 | | | 32.9 | | | 35.9 | | | 35.7 | | |
| Approach LOS | ! | 55.0 D | | | 32.9 C | | | 33.9 D | | | 33.7 D | | |
| | | U | | | U | | | U | | | U | | |
| Timer - Assigned Phs | | 2 | | 4 | | 6 | | 8 | | | | | |
| Phs Duration (G+Y+Ro | c), s | 83.0 | | 31.0 | | 83.0 | | 31.0 | | | | | |
| Change Period (Y+Rc) |), S | 5.1 | | * 5.1 | | 5.1 | | 5.1 | | | | | |
| Max Green Setting (Gr | | 64.3 | | * 26 | | 64.3 | | 25.5 | | | | | |
| Max Q Clear Time (g_c | | | | 26.9 | | 45.6 | | 17.2 | | | | | |
| Green Ext Time (p_c), | | 26.7 | | 0.0 | | 11.0 | | 2.1 | | | | | |
| ntersection Summary | | | | | | | | | | | | | |
| HCM 6th Ctrl Delay | | | 43.0 | | | | | | | | | | |
| HCM 6th LOS | | | 43.0 D | | | | | | | | | | |
| | | | U | | | | | | | | | | |
| Notes | | | | | | | | | | | | | |

^{*} HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

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|---------------------------|--------|----------|------|-------|----------|------|------|----------|-------|-------------|----------|------|--|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR | |
| Lane Configurations | | † | LDIT | ሻ | ^ | 7 | ሻ | † | TIDIT | ኘ | ^ | 7 | |
| Traffic Volume (veh/h) | 0 | 1120 | 106 | 71 | 842 | 270 | 51 | 232 | 86 | 190 | 193 | 33 | |
| Future Volume (veh/h) | 0 | 1120 | 106 | 71 | 842 | 270 | 51 | 232 | 86 | 190 | 193 | 33 | |
| Initial Q (Qb), veh | 0 | 10 | 0 | 0 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| | 1.00 | | 0.95 | 0.99 | | 0.95 | 0.92 | • | 0.89 | 0.95 | | 0.92 | |
| , —, , | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Work Zone On Approach | | No | | | No | | | No | | | No | | |
| Adj Sat Flow, veh/h/ln | 0 | 1367 | 1367 | 1660 | 1660 | 1660 | 1660 | 1660 | 1660 | 1660 | 1660 | 1660 | |
| Adj Flow Rate, veh/h | 0 | 1155 | 103 | 73 | 868 | 172 | 53 | 239 | 89 | 196 | 199 | 10 | |
| | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | |
| Percent Heavy Veh, % | 0 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | |
| Cap, veh/h | 0 | 1345 | 104 | 277 | 1741 | 739 | 340 | 553 | 196 | 335 | 1105 | 453 | |
| | 0.00 | 1.00 | 1.00 | 0.55 | 0.55 | 0.55 | 0.25 | 0.25 | 0.25 | 0.07 | 0.35 | 0.35 | |
| Sat Flow, veh/h | 0 | 2469 | 214 | 435 | 3154 | 1339 | 1067 | 2202 | 780 | 1581 | 3154 | 1295 | |
| Grp Volume(v), veh/h | 0 | 624 | 634 | 73 | 868 | 172 | 53 | 168 | 160 | 196 | 199 | 10 | |
| Grp Sat Flow(s), veh/h/ln | | 1299 | 1315 | 435 | 1577 | 1339 | 1067 | 1577 | 1405 | 1581 | 1577 | 1295 | |
| Q Serve(g_s), s | 0.0 | 0.0 | 0.0 | 9.0 | 17.0 | 6.6 | 3.9 | 8.9 | 9.6 | 6.9 | 4.4 | 0.5 | |
| Cycle Q Clear(g_c), s | 0.0 | 0.0 | 0.0 | 9.0 | 17.0 | 6.6 | 3.9 | 8.9 | 9.6 | 6.9 | 4.4 | 0.5 | |
| | 0.00 | 0.0 | 0.16 | 1.00 | | 1.00 | 1.00 | 0.0 | 0.56 | 1.00 | | 1.00 | |
| Lane Grp Cap(c), veh/h | 0 | 717 | 729 | 277 | 1741 | 739 | 340 | 396 | 353 | 335 | 1105 | 453 | |
| | 0.00 | 0.87 | 0.87 | 0.26 | 0.50 | 0.23 | 0.16 | 0.42 | 0.45 | 0.59 | 0.18 | 0.02 | |
| Avail Cap(c_a), veh/h | 0 | 717 | 726 | 312 | 1741 | 739 | 371 | 442 | 393 | 335 | 1196 | 491 | |
| | 1.00 | 2.00 | 2.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| | 0.00 | 0.46 | 0.46 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Uniform Delay (d), s/veh | | 0.0 | 0.0 | 17.7 | 14.2 | 11.5 | 29.5 | 31.4 | 31.6 | 28.3 | 22.5 | 21.3 | |
| Incr Delay (d2), s/veh | 0.0 | 6.9 | 6.8 | 2.3 | 1.0 | 0.7 | 0.2 | 0.7 | 0.9 | 1.8 | 0.1 | 0.0 | |
| Initial Q Delay(d3),s/veh | 0.0 | 2.7 | 2.6 | 0.0 | 0.5 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | |
| %ile BackOfQ(50%),veh/ | | 1.9 | 1.9 | 1.2 | 6.8 | 2.1 | 1.0 | 3.5 | 3.4 | 1.5 | 1.6 | 0.2 | |
| Unsig. Movement Delay, | | | | | | | | | | | | | |
| LnGrp Delay(d),s/veh | 0.0 | 9.7 | 9.4 | 20.0 | 15.7 | 12.3 | 29.7 | 32.1 | 32.6 | 30.1 | 22.6 | 21.3 | |
| LnGrp LOS | Α | Α | Α | В | В | В | С | С | С | С | С | С | |
| Approach Vol, veh/h | | 1258 | | | 1113 | | | 381 | | | 405 | | |
| Approach Delay, s/veh | | 9.5 | | | 15.5 | | | 32.0 | | | 26.2 | | |
| Approach LOS | | Α | | | В | | | С | | | С | | |
| | | 2 | | 4 | | 6 | 7 | 8 | | | | | |
| Timer - Assigned Phs | _ | | | | | 60.3 | 7 | | | | | | |
| Phs Duration (G+Y+Rc), | | 60.3 | | 39.7 | | 60.3 | 9.9 | 29.8 | | | | | |
| Change Period (Y+Rc), s | | 5.1 | | * 4.7 | | 5.1 | 3.0 | * 4.7 | | | | | |
| Max Green Setting (Gma | | 52.3 | | * 38 | | 52.3 | 6.9 | * 28 | | | | | |
| Max Q Clear Time (g_c+ | 11), S | 2.0 | | 6.4 | | 19.0 | 8.9 | 11.6 | | | | | |
| Green Ext Time (p_c), s | | 26.4 | | 1.4 | | 17.8 | 0.0 | 2.1 | | | | | |
| Intersection Summary | | | | | | | | | | | | | |
| HCM 6th Ctrl Delay | | | 16.5 | | | | | | | | | | |
| HCM 6th LOS | | | В | | | | | | | | | | |
| Notes | | | | | | | | | | | | | |

^{*} HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

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|---------------------------|-----|----------|---------------|------|-------------|-------|------|----------|------|-------------|------------|------|--|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR | |
| Lane Configurations | | | | | € 1} | | ች | ^ | | | † } | | |
| Traffic Volume (veh/h) | 0 | 0 | 0 | 97 | 162 | 65 | 131 | 442 | 0 | 0 | 524 | 91 | |
| Future Volume (veh/h) | 0 | 0 | 0 | 97 | 162 | 65 | 131 | 442 | 0 | 0 | 524 | 91 | |
| Initial Q (Qb), veh | | | · | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Ped-Bike Adj(A_pbT) | | | | 1.00 | | 0.79 | 0.94 | | 1.00 | 1.00 | • | 0.77 | |
| Parking Bus, Adj | | | | 0.85 | 1.00 | 0.85 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.81 | |
| Work Zone On Approach | h | | | 0.00 | No | 0.00 | 1.00 | No | 1.00 | 1.00 | No | 0.01 | |
| Adj Sat Flow, veh/h/ln | 11 | | | 1660 | 1660 | 1660 | 1660 | 1660 | 0 | 0 | 1660 | 1660 | |
| Adj Flow Rate, veh/h | | | | 102 | 171 | 47 | 138 | 465 | 0 | 0 | 552 | 73 | |
| Peak Hour Factor | | | | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | |
| Percent Heavy Veh, % | | | | 3 | 3 | 3 | 3 | 3 | 0.93 | 0.93 | 3 | 3 | |
| | | | | 299 | 515 | 144 | 374 | 1549 | | | 1196 | 156 | |
| Cap, veh/h | | | | 0.37 | | | | | 0 | 0.00 | 0.49 | | |
| Arrive On Green | | | | | 0.37 | 0.37 | 0.49 | 0.49 | 0.00 | | | 0.49 | |
| Sat Flow, veh/h | | | | 804 | 1383 | 387 | 746 | 3237 | 0 | 0 | 2518 | 319 | |
| Grp Volume(v), veh/h | | | | 173 | 0 | 147 | 138 | 465 | 0 | 0 | 356 | 269 | |
| Grp Sat Flow(s), veh/h/ln | 1 | | | 1363 | 0 | 1211 | 746 | 1577 | 0 | 0 | 1577 | 1176 | |
| Q Serve(g_s), s | | | | 5.5 | 0.0 | 5.2 | 9.0 | 5.3 | 0.0 | 0.0 | 8.9 | 9.1 | |
| Cycle Q Clear(g_c), s | | | | 5.5 | 0.0 | 5.2 | 18.1 | 5.3 | 0.0 | 0.0 | 8.9 | 9.1 | |
| Prop In Lane | | | | 0.59 | | 0.32 | 1.00 | | 0.00 | 0.00 | | 0.27 | |
| Lane Grp Cap(c), veh/h | | | | 507 | 0 | 451 | 374 | 1549 | 0 | 0 | 775 | 578 | |
| V/C Ratio(X) | | | | 0.34 | 0.00 | 0.33 | 0.37 | 0.30 | 0.00 | 0.00 | 0.46 | 0.47 | |
| Avail Cap(c_a), veh/h | | | | 586 | 0 | 521 | 374 | 1549 | 0 | 0 | 775 | 578 | |
| HCM Platoon Ratio | | | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Upstream Filter(I) | | | | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 0.00 | 0.00 | 0.58 | 0.58 | |
| Uniform Delay (d), s/veh |) | | | 13.5 | 0.0 | 13.5 | 16.0 | 9.1 | 0.0 | 0.0 | 10.0 | 10.1 | |
| Incr Delay (d2), s/veh | | | | 0.4 | 0.0 | 0.4 | 2.8 | 0.5 | 0.0 | 0.0 | 1.1 | 1.6 | |
| Initial Q Delay(d3),s/veh | | | | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | |
| %ile BackOfQ(50%),veh | | | | 1.6 | 0.0 | 1.4 | 1.7 | 1.7 | 0.0 | 0.0 | 2.9 | 2.3 | |
| Unsig. Movement Delay | | | | | | | | | | | | | |
| LnGrp Delay(d),s/veh | , | | | 13.9 | 0.0 | 13.9 | 18.8 | 9.6 | 0.0 | 0.0 | 11.2 | 11.7 | |
| LnGrp LOS | | | | В | A | В | В | A | A | A | В | В | |
| Approach Vol, veh/h | | | | | 320 | | | 603 | | - ' | 625 | _ | |
| Approach Delay, s/veh | | | | | 13.9 | | | 11.7 | | | 11.4 | | |
| Approach LOS | | | | | В | | | В | | | В | | |
| | | | | | ט | | | U | | | U | | |
| Timer - Assigned Phs | | 2 | | | | 6 | | 8 | | | | | |
| Phs Duration (G+Y+Rc), | , s | 33.7 | | | | 33.7 | | 26.3 | | | | | |
| Change Period (Y+Rc), | | * 4.2 | | | | * 4.2 | | 4.0 | | | | | |
| Max Green Setting (Gma | | * 26 | | | | * 26 | | 25.8 | | | | | |
| Max Q Clear Time (g_c+ | | 20.1 | | | | 11.1 | | 7.5 | | | | | |
| Green Ext Time (p_c), s | | 3.0 | | | | 6.1 | | 1.9 | | | | | |
| Intersection Summary | | | | | | | | | | | | | |
| HCM 6th Ctrl Delay | | | 12.0 | | | | | | | | | | |
| HCM 6th LOS | | | 12.0 B | | | | | | | | | | |
| | | | D | | | | | | | | | | |
| Notes | | | | | | | | | | | | | |

^{*} HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

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|----------------------------------|---------|----------|-------|------|-----------|-------------|----------|-----------|-------------|----------|------------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | | | | र्सी | | 7 | ^ | | | ∱ ∱ | |
| Traffic Volume (vph) | 0 | 0 | 0 | 85 | 194 | 153 | 54 | 289 | 0 | 0 | 368 | 118 |
| Future Volume (vph) | 0 | 0 | 0 | 85 | 194 | 153 | 54 | 289 | 0 | 0 | 368 | 118 |
| Ideal Flow (vphpl) | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 |
| Total Lost time (s) | | | | | 3.0 | | 4.0 | 4.0 | | | 4.0 | |
| Lane Util. Factor | | | | | 0.95 | | 1.00 | 0.95 | | | 0.95 | |
| Frpb, ped/bikes | | | | | 1.00 | | 1.00 | 1.00 | | | 1.00 | |
| Flpb, ped/bikes | | | | | 1.00 | | 1.00 | 1.00 | | | 1.00 | |
| Frt | | | | | 0.95 | | 1.00 | 1.00 | | | 0.96 | |
| Flt Protected | | | | | 0.99 | | 0.95 | 1.00 | | | 1.00 | |
| Satd. Flow (prot) | | | | | 2737 | | 1568 | 2885 | | | 2779 | |
| Flt Permitted | | | | | 0.99 | | 0.30 | 1.00 | | | 1.00 | |
| Satd. Flow (perm) | | | | | 2737 | | 503 | 2885 | | | 2779 | |
| Peak-hour factor, PHF | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Adj. Flow (vph) | 0 | 0 | 0 | 89 | 204 | 161 | 57 | 304 | 0 | 0 | 387 | 124 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 102 | 0 | 0 | 0 | 0 | 0 | 44 | 0 |
| Lane Group Flow (vph) | 0 | 0 | 0 | 0 | 352 | 0 | 57 | 304 | 0 | 0 | 467 | 0 |
| Confl. Bikes (#/hr) | | | 1 | | | 1 | | | 1 | | | 1 |
| Heavy Vehicles (%) | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% |
| Parking (#/hr) | | | | 6 | 6 | 4 | | 12 | | | 11 | 11 |
| Turn Type | | | | Perm | NA | | Perm | NA | | | NA | |
| Protected Phases | | | | . 0 | 6 | | . 0 | 8 | | | 4 | |
| Permitted Phases | | | | 6 | | | 8 | Ū | | | • | |
| Actuated Green, G (s) | | | | | 23.0 | | 16.0 | 16.0 | | | 16.0 | |
| Effective Green, g (s) | | | | | 23.0 | | 16.0 | 16.0 | | | 16.0 | |
| Actuated g/C Ratio | | | | | 0.33 | | 0.23 | 0.23 | | | 0.23 | |
| Clearance Time (s) | | | | | 3.0 | | 4.0 | 4.0 | | | 4.0 | |
| Vehicle Extension (s) | | | | | 2.0 | | 2.0 | 2.0 | | | 2.0 | |
| Lane Grp Cap (vph) | | | | | 899 | | 114 | 659 | | | 635 | |
| v/s Ratio Prot | | | | | 000 | | 117 | 0.11 | | | c0.17 | |
| v/s Ratio Perm | | | | | 0.13 | | 0.11 | 0.11 | | | 00.17 | |
| v/c Ratio | | | | | 0.39 | | 0.50 | 0.46 | | | 0.74 | |
| Uniform Delay, d1 | | | | | 18.1 | | 23.5 | 23.3 | | | 25.0 | |
| Progression Factor | | | | | 1.00 | | 1.00 | 1.00 | | | 1.00 | |
| Incremental Delay, d2 | | | | | 1.3 | | 14.8 | 2.3 | | | 7.4 | |
| Delay (s) | | | | | 19.4 | | 38.3 | 25.6 | | | 32.5 | |
| Level of Service | | | | | В | | D | 23.0 C | | | 02.5 C | |
| Approach Delay (s) | | 0.0 | | | 19.4 | | | 27.6 | | | 32.5 | |
| Approach LOS | | Α | | | В | | | C | | | 02.0 C | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 26.7 | Н | CM 2000 | Level of | Service | | С | | | |
| HCM 2000 Volume to Capacity | v ratio | | 0.35 | | OIVI 2000 | LOVOIOI | JCI VICC | | U | | | |
| Actuated Cycle Length (s) | Tallo | | 70.0 | S | um of los | time (s) | | | 11.0 | | | |
| Intersection Capacity Utilizatio | n | | 48.2% | | | of Service | | | Α | | | |
| Analysis Period (min) | | | 15 | i. | O LGVOI (| JI OCI VICE | | | | | | |
| c Critical Lane Group | | | 10 | | | | | | | | | |
| C Official Latte Group | | | | | | | | | | | | |

| Intersection | | | | | | | | | | | | |
|------------------------|------|------|----------|--------|--------|------|------|------|------|---------|------------|------|
| Int Delay, s/veh | 1.7 | | | | | | | | | | | |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | | | | 414 | | | | | | ∱ } | |
| Traffic Vol, veh/h | 0 | 0 | 0 | 0 | 359 | 0 | 0 | 0 | 0 | 0 | 0 | 74 |
| Future Vol, veh/h | 0 | 0 | 0 | 0 | 359 | 0 | 0 | 0 | 0 | 0 | 0 | 74 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 251 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | - | - | - | - | - | - | - | - | - | - |
| Veh in Median Storage, | ,# - | 2 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, % | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 |
| Heavy Vehicles, % | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 |
| Mvmt Flow | 0 | 0 | 0 | 0 | 378 | 0 | 0 | 0 | 0 | 0 | 0 | 78 |
| | | | | | | | | | | | | |
| Major/Minor | | | ľ | Major2 | | | | | N | /linor2 | | |
| Conflicting Flow All | | | | 251 | 0 | 0 | | | | - | 629 | 189 |
| Stage 1 | | | | - | - | - | | | | - | 378 | - |
| Stage 2 | | | | - | - | - | | | | - | 251 | - |
| Critical Hdwy | | | | 4.16 | - | - | | | | - | 6.56 | 6.96 |
| Critical Hdwy Stg 1 | | | | - | - | - | | | | - | 5.56 | - |
| Critical Hdwy Stg 2 | | | | - | - | - | | | | - | - | - |
| Follow-up Hdwy | | | | 2.23 | - | - | | | | - | 4.03 | 3.33 |
| Pot Cap-1 Maneuver | | | | 1304 | - | 0 | | | | 0 | 396 | 818 |
| Stage 1 | | | | - | - | 0 | | | | 0 | 611 | - |
| Stage 2 | | | | - | - | 0 | | | | 0 | - | - |
| Platoon blocked, % | | | | | - | | | | | | | |
| Mov Cap-1 Maneuver | | | | 1304 | - | - | | | | - | 0 | 818 |
| Mov Cap-2 Maneuver | | | | - | - | - | | | | - | 0 | - |
| Stage 1 | | | | - | - | - | | | | - | 0 | - |
| Stage 2 | | | | - | - | - | | | | - | 0 | - |
| | | | | | | | | | | | | |
| Approach | | | | WB | | | | | | SB | | |
| HCM Control Delay, s | | | | 0 | | | | | | 9.9 | | |
| HCM LOS | | | | | | | | | | A | | |
| | | | | | | | | | | - 1 | | |
| Minor Lane/Major Mvmt | 1 | WBL | WRT | SBLn1 | SBI n2 | | | | | | | |
| Capacity (veh/h) | | 1304 | - | - | 818 | | | | | | | |
| HCM Lane V/C Ratio | | - | _ | | 0.095 | | | | | | | |
| HCM Control Delay (s) | | 0 | _ | 0 | 9.9 | | | | | | | |
| HCM Lane LOS | | A | <u>-</u> | A | J.5 | | | | | | | |
| HCM 95th %tile Q(veh) | | 0 | _ | - | 0.3 | | | | | | | |
| | | - 0 | | | 3.0 | | | | | | | |

| Intersection | | | | | | |
|------------------------|----------|-------|--------|----------|---------|------|
| Int Delay, s/veh | 0.2 | | | | | |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | † | LDIX | ሻ | ^ | IIDL | 7 |
| | 1335 | 54 | 33 | 856 | 0 | 0 |
| | 1335 | 54 | 33 | 856 | 0 | 0 |
| | | | | | | |
| Conflicting Peds, #/hr | _ 0 | 100 | 100 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | 25 | - | - | 0 |
| Veh in Median Storage, | # 0 | - | - | 0 | 0 | - |
| Grade, % | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 96 | 96 | 96 | 96 | 96 | 96 |
| Heavy Vehicles, % | 3 | 3 | 3 | 3 | 3 | 3 |
| | 1391 | 56 | 34 | 892 | 0 | 0 |
| WWW.CT IOW | 1001 | 00 | 01 | 002 | • | • |
| | | | | | | |
| Major/Minor M | ajor1 | N | Major2 | N | /linor1 | |
| Conflicting Flow All | 0 | 0 | 1547 | 0 | - | 824 |
| Stage 1 | - | - | - | - | - | - |
| Stage 2 | _ | _ | _ | _ | _ | _ |
| Critical Hdwy | _ | _ | 4.16 | _ | _ | 6.96 |
| Critical Hdwy Stg 1 | _ | _ | - | _ | _ | - |
| Critical Hdwy Stg 2 | | | | | _ | _ |
| | _ | _ | 2.23 | - | | |
| Follow-up Hdwy | - | - | | - | - | 3.33 |
| Pot Cap-1 Maneuver | - | - | 420 | - | 0 | 314 |
| Stage 1 | - | - | - | - | 0 | - |
| Stage 2 | - | - | - | - | 0 | - |
| Platoon blocked, % | - | - | | - | | |
| Mov Cap-1 Maneuver | - | - | 380 | - | - | 284 |
| Mov Cap-2 Maneuver | _ | - | - | - | - | - |
| Stage 1 | _ | _ | _ | _ | _ | _ |
| Stage 2 | _ | _ | _ | _ | _ | _ |
| Olage 2 | | | | | | |
| | | | | | | |
| Approach | EB | | WB | | NB | |
| HCM Control Delay, s | 0 | | 0.6 | | 0 | |
| HCM LOS | | | | | Α | |
| | | | | | | |
| | | | | | | |
| Minor Lane/Major Mvmt | 1 | NBLn1 | EBT | EBR | WBL | WBT |
| Capacity (veh/h) | | - | - | - | 380 | - |
| HCM Lane V/C Ratio | | - | - | - | 0.09 | - |
| HCM Control Delay (s) | | 0 | - | - | 15.4 | - |
| HCM Lane LOS | | A | _ | _ | С | _ |
| HCM 95th %tile Q(veh) | | - | _ | _ | 0.3 | _ |
| HOW Jour Joure Q(Veri) | | | | | 0.5 | |

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|--|-----------|--------------|-----------|------------|--------------|-----------|----------|-------------------|-------------|-----------|-----------|-----------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 7 | ∱ ∱ | | ሻ | ∱ ∱ | | | ∱ ∱ | | ሻ | ^↑ | 7 |
| Traffic Volume (veh/h) | 30 | 1591 | 31 | 90 | 1751 | 30 | 0 | 80 | 30 | 30 | 320 | 50 |
| Future Volume (veh/h) | 30 | 1591 | 31 | 90 | 1751 | 30 | 0 | 80 | 30 | 30 | 320 | 50 |
| Initial Q (Qb), veh | 0 | 10 | 0 | 0 | 15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | | 0.97 | 1.00 | | 0.99 | 1.00 | | 0.97 | 0.99 | | 0.98 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach | | No | | | No | | _ | No | | | No | |
| Adj Sat Flow, veh/h/ln | 1367 | 1367 | 1367 | 1367 | 1367 | 1367 | 0 | 1660 | 1660 | 1660 | 1660 | 1660 |
| Adj Flow Rate, veh/h | 33 | 1768 | 33 | 100 | 1946 | 32 | 0 | 89 | 17 | 33 | 356 | 37 |
| Peak Hour Factor | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Percent Heavy Veh, % | 3 | 3 | 3 | 3 | 3 | 3 | 0 | 3 | 3 | 3 | 3 | 3 |
| Cap, veh/h | 72 | 1905 | 30 | 72 | 1921 | 17 | 0 | 457 | 85 | 253 | 545 | 239 |
| Arrive On Green | 0.73 | 0.73 | 0.73 | 0.73 | 0.73 | 0.73 | 0.00 | 0.17 | 0.17 | 0.17 | 0.17 | 0.17 |
| Sat Flow, veh/h | 180 | 2607 | 49 | 214 | 2615 | 43 | 0 | 2727 | 490 | 1265 | 3154 | 1380 |
| Grp Volume(v), veh/h | 33 | 878 | 923 | 100 | 964 | 1014 | 0 | 52 | 54 | 33 | 356 | 37 |
| Grp Sat Flow(s),veh/h/ln | 180 | 1299 | 1357 | 214 | 1299 | 1359 | 0 | 1577 | 1557 | 1265 | 1577 | 1380 |
| Q Serve(g_s), s | 0.0 | 56.8 | 57.8 | 15.0 | 72.8 | 72.8 | 0.0 | 2.8 | 3.0 | 2.3 | 10.5 | 2.3 |
| Cycle Q Clear(g_c), s | 72.8 | 56.8 | 57.8 | 72.8 | 72.8 | 72.8 | 0.0 | 2.8 | 3.0 | 5.3 | 10.5 | 2.3 |
| Prop In Lane | 1.00 | 0.10 | 0.04 | 1.00 | 0.10 | 0.03 | 0.00 | | 0.31 | 1.00 | | 1.00 |
| Lane Grp Cap(c), veh/h | 72 | 946 | 989 | 72 | 946 | 992 | 0 | 273 | 269 | 253 | 545 | 239 |
| V/C Ratio(X) | 0.46 | 0.93 | 0.93 | 1.39 | 1.02 | 1.02 | 0.00 | 0.19 | 0.20 | 0.13 | 0.65 | 0.16 |
| Avail Cap(c_a), veh/h | 72 | 946 | 988 | 104 | 946 | 989 | 0 | 420 | 414 | 371 | 839 | 367 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 0.09 | 0.09 | 0.09 | 0.00 | 0.98 | 0.98 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 50.0 | 12.1 | 12.1 | 50.0 | 13.6 | 13.6 | 0.0 | 35.4 | 35.4 | 37.7 | 38.6 | 35.1 |
| Incr Delay (d2), s/veh | 19.6 | 16.4 | 16.4 | 182.7 | 14.1 | 15.1 | 0.0 | 0.3 | 0.4 | 0.2 | 1.3 | 0.3 |
| Initial Q Delay(d3),s/veh | 0.0 | 2.8 | 2.7 | 0.0 | 28.6 | 27.2 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/ln Unsig. Movement Delay, s/veh | 1.2 | 18.1 | 19.1 | 5.4 | 26.7 | 27.9 | 0.0 | 1.1 | 1.2 | 0.7 | 4.2 | 8.0 |
| | | 31.3 | 31.3 | 232.7 | 56.3 | 55.9 | 0.0 | 35.7 | 35.8 | 37.9 | 39.9 | 35.4 |
| LnGrp Delay(d),s/veh LnGrp LOS | 69.6 E | 31.3 C | 31.3 C | 232.1 F | 50.5 F | 55.9 F | 0.0 A | აა. <i>1</i> D | ან. D | 37.9 D | აყ.ყ D | 35.4 D |
| | | | | Г | | Г | A | 106 | U | U | 426 | |
| Approach Vol, veh/h | | 1834 32.0 | | | 2078 64.6 | | | 35.7 | | | 39.3 | |
| Approach LOS | | | | | _ | | | _ | | | _ | |
| Approach LOS | | С | | | E | | | D | | | D | |
| Timer - Assigned Phs | | 2 | | 4 | | 6 | | 8 | | | | |
| Phs Duration (G+Y+Rc), s | | 78.2 | | 21.8 | | 78.2 | | 21.8 | | | | |
| Change Period (Y+Rc), s | | 5.4 | | 4.5 | | 5.4 | | 4.5 | | | | |
| Max Green Setting (Gmax), s | | 63.5 | | 26.6 | | 63.5 | | 26.6 | | | | |
| Max Q Clear Time (g_c+l1), s | | 74.8 | | 12.5 | | 74.8 | | 5.0 | | | | |
| Green Ext Time (p_c), s | | 0.0 | | 2.2 | | 0.0 | | 0.5 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 6th Ctrl Delay | | | 48.0 | | | | | | | | | |
| HCM 6th LOS | | | D | | | | | | | | | |

| _ | ۶ | → | • | • | ← | • | • | † | / | > | ţ | ✓ | |
|----------------------------|-------|--------------|-------|---------------|--------------|--------------|-------------|-------------|----------|-------------|-------------|-------------|--|
| Movement E | BL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR | |
| Lane Configurations | ٦ | ∱ } | | ሻ | ↑ } | | ሻ | ħβ | | ሻ | ∱ } | | |
| Traffic Volume (veh/h) | 40 | 1770 | 31 | 102 | 1530 | 40 | 22 | 360 | 151 | 40 | 501 | 60 | |
| Future Volume (veh/h) | 40 | 1770 | 31 | 102 | 1530 | 40 | 22 | 360 | 151 | 40 | 501 | 60 | |
| Initial Q (Qb), veh | 0 | 10 | 0 | 0 | 15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| ,, –, , | .00 | | 0.98 | 1.00 | | 0.97 | 0.99 | | 0.97 | 0.99 | | 0.98 | |
| • | .00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Work Zone On Approach | | No | | | No | | | No | | | No | | |
| • | 367 | 1367 | 1367 | 1367 | 1367 | 1367 | 1660 | 1660 | 1660 | 1660 | 1660 | 1660 | |
| Adj Flow Rate, veh/h | 44 | 1967 | 33 | 113 | 1700 | 42 | 24 | 400 | 158 | 44 | 557 | 57 | |
| | .90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | |
| Percent Heavy Veh, % | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | |
| Cap, veh/h | 72 | 1712 | 16 | 72 | 1707 | 20 | 121 | 533 | 207 | 149 | 700 | 71 | |
| | .65 | 0.65 | 0.65 | 0.65 | 0.65 | 0.65 | 0.49 | 0.49 | 0.49 | 0.24 | 0.24 | 0.24 | |
| | 226 | 2614 | 44 | 176 | 2589 | 64 | 798 | 2196 | 854 | 839 | 2883 | 294 | |
| Grp Volume(v), veh/h | 44 | 974 | 1026 | 113 | 850 | 892 | 24 | 286 | 272 | 44 | 304 | 310 | |
| | 226 | 1299 | 1358 | 176 | 1299 | 1353 | 798 | 1577 | 1473 | 839 | 1577 | 1600 | |
| (0- /- | 0.0 | 64.9 | 64.9 | 0.0 | 64.9 | 64.9 | 2.8 | 14.6 | 15.1 | 5.0 | 18.1 | 18.2 | |
| (6=) | 4.9 | 64.9 | 64.9 | 64.9 | 64.9 | 64.9 | 21.0 | 14.6 | 15.1 | 20.1 | 18.1 | 18.2 | |
| | .00 | 0.40 | 0.03 | 1.00 | 0.40 | 0.05 | 1.00 | 000 | 0.58 | 1.00 | 000 | 0.18 | |
| Lane Grp Cap(c), veh/h | 72 | 843 | 884 | 72 | 843 | 883 | 121 | 383 | 358 | 149 | 383 | 389 | |
| , | .61 | 1.16 | 1.16 | 1.57 | 1.01 | 1.01 | 0.20 | 0.75 | 0.76 | 0.30 | 0.79 | 0.80 | |
| Avail Cap(c_a), veh/h | 72 | 843 | 882 | 72 | 843 | 879 | 139 | 420 | 392 | 169 | 420 | 426 | |
| | .00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 2.00 | 2.00 | 2.00 | 1.00 | 1.00 | 1.00 | |
| | .09 | 0.09 | 0.09 | 1.00 | 1.00 | 1.00 | 0.79 | 0.79 | 0.79 | 1.00 | 1.00 | 1.00 | |
| Uniform Delay (d), s/veh 5 | 3.5 | 17.5 71.4 | 17.5 | 50.0 312.7 | 17.5 33.1 | 17.5 32.6 | 33.4 0.6 | 23.2 5.2 | 23.4 | 43.5 1.1 | 35.5 9.3 | 35.6 9.5 | |
| , , , , | 0.0 | 21.3 | 20.4 | 0.0 | 32.0 | 30.6 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | |
| %ile BackOfQ(50%),veh/lr | | 37.7 | 39.7 | 8.0 | 31.2 | 32.2 | 0.0 | 4.6 | 4.5 | 1.1 | 7.9 | 8.1 | |
| Unsig. Movement Delay, s | | | 55.1 | 0.0 | J1.Z | JZ.Z | 0.5 | 4.0 | 4.5 | 1.1 | 1.3 | 0.1 | |
| | | | 111.0 | 362.7 | 82.6 | 80.7 | 34.0 | 28.4 | 29.6 | 44.6 | 44.9 | 45.0 | |
| LnGrp LOS | D.5 | F | F | F | 62.0 F | F | C | C | C | D | TT.5 | 75.0 D | |
| Approach Vol, veh/h | | 2044 | | ' | 1855 | ' | | 582 | | | 658 | | |
| Approach Delay, s/veh | | 109.4 | | | 98.8 | | | 29.2 | | | 44.9 | | |
| Approach LOS | | 103.4 F | | | 90.0 F | | | 29.2 C | | | 44.9 D | | |
| | | | | | | | | | | | U | | |
| Timer - Assigned Phs | | 2 | | 4 | | 6 | | 8 | | | | | |
| Phs Duration (G+Y+Rc), s | 3 | 70.3 | | 29.7 | | 70.3 | | 29.7 | | | | | |
| Change Period (Y+Rc), s | | 5.4 | | 5.4 | | 5.4 | | 5.4 | | | | | |
| Max Green Setting (Gmax | | 62.6 | | 26.6 | | 62.6 | | 26.6 | | | | | |
| Max Q Clear Time (g_c+l1 | 1), s | 66.9 | | 22.1 | | 66.9 | | 23.0 | | | | | |
| Green Ext Time (p_c), s | | 0.0 | | 1.7 | | 0.0 | | 1.3 | | | | | |
| Intersection Summary | | | | | | | | | | | | | |
| HCM 6th Ctrl Delay | | | 88.3 | | | | | | | | | | |
| HCM 6th LOS | | | F | | | | | | | | | | |

| | ۶ | → | • | • | + | • | 1 | † | / | / | + | 4 |
|----------------------------------|---------|------------|--------|-------|------------|------------|---------|------------|------|----------|----------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | ∱ } | | | 4T> | | ሻ | ∱ } | | ሻ | ħβ | |
| Traffic Volume (vph) | 0 | 724 | 50 | 140 | 1420 | 30 | 21 | 100 | 43 | 41 | 360 | 60 |
| Future Volume (vph) | 0 | 724 | 50 | 140 | 1420 | 30 | 21 | 100 | 43 | 41 | 360 | 60 |
| Ideal Flow (vphpl) | 1700 | 1700 | 1700 | 1400 | 1400 | 1400 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 |
| Total Lost time (s) | | 5.1 | | | 5.1 | | 4.5 | 4.5 | | 4.5 | 4.5 | |
| Lane Util. Factor | | 0.95 | | | 0.95 | | 1.00 | 0.95 | | 1.00 | 0.95 | |
| Frpb, ped/bikes | | 1.00 | | | 1.00 | | 1.00 | 0.98 | | 1.00 | 0.99 | |
| Flpb, ped/bikes | | 1.00 | | | 1.00 | | 0.99 | 1.00 | | 0.97 | 1.00 | |
| Frt | | 0.99 | | | 1.00 | | 1.00 | 0.95 | | 1.00 | 0.98 | |
| Flt Protected | | 1.00 | | | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | | 3094 | | | 2555 | | 1545 | 2739 | | 1513 | 3050 | |
| FIt Permitted | | 1.00 | | | 0.69 | | 0.35 | 1.00 | | 0.66 | 1.00 | |
| Satd. Flow (perm) | | 3094 | | | 1780 | | 567 | 2739 | | 1046 | 3050 | |
| Peak-hour factor, PHF | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Adj. Flow (vph) | 0 | 762 | 53 | 147 | 1495 | 32 | 22 | 105 | 45 | 43 | 379 | 63 |
| RTOR Reduction (vph) | 0 | 4 | 0 | 0 | 1 | 0 | 0 | 35 | 0 | 0 | 14 | 0 |
| Lane Group Flow (vph) | 0 | 811 | 0 | 0 | 1673 | 0 | 22 | 115 | 0 | 43 | 428 | 0 |
| Confl. Peds. (#/hr) | 100 | | 29 | 29 | | 100 | 24 | | 33 | 33 | | 24 |
| Confl. Bikes (#/hr) | | | 3 | | | 2 | | | 1 | | | 1 |
| Heavy Vehicles (%) | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% |
| Parking (#/hr) | | | | | | | | 8 | 8 | | | |
| Turn Type | | NA | | pm+pt | NA | | Perm | NA | | Perm | NA | |
| Protected Phases | | 2 | | 1 | 6 | | | 8 | | | 4 | |
| Permitted Phases | | | | 6 | | | 8 | | | 4 | | |
| Actuated Green, G (s) | | 59.5 | | | 67.2 | | 23.2 | 23.2 | | 23.2 | 23.2 | |
| Effective Green, g (s) | | 59.5 | | | 67.2 | | 23.2 | 23.2 | | 23.2 | 23.2 | |
| Actuated g/C Ratio | | 0.60 | | | 0.67 | | 0.23 | 0.23 | | 0.23 | 0.23 | |
| Clearance Time (s) | | 5.1 | | | 5.1 | | 4.5 | 4.5 | | 4.5 | 4.5 | |
| Vehicle Extension (s) | | 5.0 | | | 5.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | | 1840 | | | 1231 | | 131 | 635 | | 242 | 707 | |
| v/s Ratio Prot | | 0.26 | | | c0.06 | | | 0.04 | | | c0.14 | |
| v/s Ratio Perm | | | | | c0.85 | | 0.04 | | | 0.04 | | |
| v/c Ratio | | 0.44 | | | 1.36 | | 0.17 | 0.18 | | 0.18 | 0.61 | |
| Uniform Delay, d1 | | 11.1 | | | 16.4 | | 30.7 | 30.8 | | 30.8 | 34.3 | |
| Progression Factor | | 1.00 | | | 0.49 | | 1.00 | 1.00 | | 0.43 | 0.39 | |
| Incremental Delay, d2 | | 0.8 | | | 163.9 | | 0.6 | 0.1 | | 0.2 | 0.9 | |
| Delay (s) | | 11.9 | | | 171.9 | | 31.3 | 30.9 | | 13.4 | 14.2 | |
| Level of Service | | В | | | F | | С | С | | В | В | |
| Approach Delay (s) | | 11.9 | | | 171.9 | | | 31.0 | | | 14.1 | |
| Approach LOS | | В | | | F | | | С | | | В | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 98.4 | Н | CM 2000 | Level of | Service | | F | | | |
| HCM 2000 Volume to Capacit | y ratio | | 1.20 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 100.0 | S | um of lost | t time (s) | | | 12.8 | | | |
| Intersection Capacity Utilizatio | n | | 123.8% | | CU Level | \ / | | | Н | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

| | ᄼ | → | \searrow | • | • | • | 4 | † | / | > | ↓ | ✓ | |
|--------------------------|-------|----------|------------|-------|------------|------|-----------|----------|------|-------------|----------|------|--|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR | |
| Lane Configurations | * | ħβ | | ች | ∱ } | | ች | ^ | 7 | | ΦÞ | | |
| Traffic Volume (veh/h) | 81 | 641 | 84 | 142 | 1452 | 30 | 51 | 402 | 80 | 0 | 553 | 82 | |
| Future Volume (veh/h) | 81 | 641 | 84 | 142 | 1452 | 30 | 51 | 402 | 80 | 0 | 553 | 82 | |
| Initial Q (Qb), veh | 0 | 10 | 0 | 0 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Ped-Bike Adj(A_pbT) | 1.00 | | 0.95 | 0.99 | | 0.96 | 0.99 | <u> </u> | 0.91 | 1.00 | | 0.91 | |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Work Zone On Approac | | No | | | No | | | No | | | No | | |
| Adj Sat Flow, veh/h/ln | 1660 | 1660 | 1660 | 1367 | 1367 | 1367 | 1660 | 1660 | 1660 | 0 | 1660 | 1660 | |
| Adj Flow Rate, veh/h | 85 | 675 | 79 | 149 | 1528 | 31 | 54 | 423 | 21 | 0 | 582 | 75 | |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | |
| Percent Heavy Veh, % | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 0.50 | 3 | 3 | |
| Cap, veh/h | 72 | 2198 | 252 | 72 | 2018 | 39 | 119 | 817 | 333 | 0 | 719 | 92 | |
| Arrive On Green | 0.77 | 0.77 | 0.77 | 1.00 | 1.00 | 1.00 | 0.26 | 0.26 | 0.26 | 0.00 | 0.26 | 0.26 | |
| Sat Flow, veh/h | 327 | 2829 | 331 | 575 | 2601 | 53 | 760 | 3154 | 1285 | 0.00 | 2860 | 357 | |
| | | | | | | | | | | | | 327 | |
| Grp Volume(v), veh/h | 85 | 376 | 378 | 149 | 762 | 797 | 54 760 | 423 | 21 | 0 | 330 | | |
| Grp Sat Flow(s), veh/h/l | | 1577 | 1582 | 575 | 1299 | 1355 | 760 | 1577 | 1285 | 0 | 1577 | 1556 | |
| Q Serve(g_s), s | 8.1 | 7.0 | 7.1 | 3.9 | 0.0 | 0.0 | 6.2 | 11.5 | 1.2 | 0.0 | 19.6 | 19.7 | |
| Cycle Q Clear(g_c), s | 8.5 | 7.0 | 7.1 | 11.6 | 0.0 | 0.0 | 25.9 | 11.5 | 1.2 | 0.0 | 19.6 | 19.7 | |
| Prop In Lane | 1.00 | 4000 | 0.21 | 1.00 | 4007 | 0.04 | 1.00 | 0.47 | 1.00 | 0.00 | 400 | 0.23 | |
| Lane Grp Cap(c), veh/h | | 1222 | 1227 | 72 | 1007 | 1050 | 119 | 817 | 333 | 0 | 408 | 403 | |
| V/C Ratio(X) | 1.18 | 0.31 | 0.31 | 2.07 | 0.76 | 0.76 | 0.45 | 0.52 | 0.06 | 0.00 | 0.81 | 0.81 | |
| Avail Cap(c_a), veh/h | 324 | 1222 | 1226 | 474 | 1007 | 1050 | 119 | 817 | 333 | 0 | 408 | 403 | |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 2.00 | 2.00 | 2.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 0.40 | 0.40 | 0.40 | 0.90 | 0.90 | 0.90 | 0.00 | 0.09 | 0.09 | |
| Uniform Delay (d), s/ve | | 3.5 | 3.5 | 38.7 | 0.0 | 0.0 | 47.3 | 31.7 | 27.9 | 0.0 | 34.7 | 34.8 | |
| Incr Delay (d2), s/veh | | 0.7 | 0.7 | 498.2 | 2.2 | 2.1 | 2.4 | 0.5 | 0.1 | 0.0 | 1.1 | 1.2 | |
| Initial Q Delay(d3),s/ve | | 0.2 | 0.2 | 0.0 | 0.7 | 0.7 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | |
| %ile BackOfQ(50%),ve | | 2.5 | 2.5 | 11.7 | 0.8 | 0.8 | 1.4 | 4.4 | 0.4 | 0.0 | 7.6 | 7.6 | |
| Unsig. Movement Dela | • | | | | | | | | | | | | |
| LnGrp Delay(d),s/veh | 211.8 | 4.3 | 4.3 | 537.0 | 2.9 | 2.8 | 49.8 | 32.2 | 28.0 | 0.0 | 35.8 | 36.0 | |
| LnGrp LOS | F | Α | Α | F | Α | Α | D | С | С | Α | D | D | |
| Approach Vol, veh/h | | 839 | | | 1708 | | | 498 | | | 657 | | |
| Approach Delay, s/veh | | 25.3 | | | 49.4 | | | 33.9 | | | 35.9 | | |
| Approach LOS | | С | | | D | | | С | | | D | | |
| Timer - Assigned Phs | | 2 | | 4 | | 6 | | 8 | | | | | |
| Phs Duration (G+Y+Ro | s), s | 83.0 | | 31.0 | | 83.0 | | 31.0 | | | | | |
| Change Period (Y+Rc) | | 5.1 | | * 5.1 | | 5.1 | | 5.1 | | | | | |
| Max Green Setting (Gn | | 64.3 | | * 26 | | 64.3 | | 25.5 | | | | | |
| Max Q Clear Time (g_c | | 10.5 | | 27.9 | | 13.6 | | 21.7 | | | | | |
| Green Ext Time (p_c), | | 17.3 | | 0.0 | | 38.6 | | 1.5 | | | | | |
| Intersection Summary | | | | 3.0 | | | | | | | | | |
| HCM 6th Ctrl Delay | | | 39.5 | | | | | | | | | | |
| HCM 6th LOS | | | 39.5 D | | | | | | | | | | |
| | | | U | | | | | | | | | | |
| Notes | | | | | | | | | | | | | |

^{*} HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

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|---------------------------|---------|------------|---------------|-------|----------|------|------|------------|------|-------------|----------|------|--|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR | |
| Lane Configurations | | ∱ } | | * | ^ | 7 | * | ↑ ⊅ | | ች | ^ | 7 | |
| Traffic Volume (veh/h) | 10 | 561 | 80 | 80 | 1433 | 120 | 31 | 80 | 40 | 220 | 290 | 90 | |
| Future Volume (veh/h) | 10 | 561 | 80 | 80 | 1433 | 120 | 31 | 80 | 40 | 220 | 290 | 90 | |
| Initial Q (Qb), veh | 0 | 10 | 0 | 0 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Ped-Bike Adj(A_pbT) | 1.00 | 10 | 0.97 | 0.99 | 10 | 0.97 | 0.95 | | 0.92 | 0.94 | J | 0.94 | |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Work Zone On Approac | | No | 1.00 | 1.00 | No | 1.00 | 1.00 | No | 1.00 | 1.00 | No | 1.00 | |
| | 1660 | 1660 | 1660 | 1367 | 1367 | 1367 | 1660 | 1660 | 1660 | 1660 | 1660 | 1660 | |
| Adj Flow Rate, veh/h | 10 | 567 | 72 | 81 | 1447 | 95 | 31 | 81 | 40 | 222 | 293 | 75 | |
| Peak Hour Factor | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | |
| Percent Heavy Veh, % | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | |
| Cap, veh/h | 39 | 1402 | 186 | 74 | 1501 | 647 | 287 | 463 | 207 | 407 | 1022 | 430 | |
| Arrive On Green | 1.00 | 1.00 | 1.00 | 0.58 | 0.58 | 0.58 | 0.23 | 0.23 | 0.23 | 0.07 | 0.32 | 0.32 | |
| | 1.00 | | | | | 1120 | | 2055 | 921 | | 3154 | 1328 | |
| Sat Flow, veh/h | | 2315 | 332 | 640 | 2598 | | 957 | | | 1581 | | | |
| Grp Volume(v), veh/h | 337 | 0 | 312 | 81 | 1447 | 95 | 31 | 60 | 61 | 222 | 293 | 75 | |
| Grp Sat Flow(s), veh/h/lr | | 0 | 1437 | 640 | 1299 | 1120 | 957 | 1577 | 1398 | 1581 | 1577 | 1328 | |
| Q Serve(g_s), s | 4.7 | 0.0 | 0.0 | 6.1 | 53.1 | 3.9 | 2.6 | 3.1 | 3.5 | 6.9 | 6.9 | 4.0 | |
| Cycle Q Clear(g_c), s | 57.8 | 0.0 | 0.0 | 6.1 | 53.1 | 3.9 | 2.6 | 3.1 | 3.5 | 6.9 | 6.9 | 4.0 | |
| Prop In Lane | 0.03 | | 0.23 | 1.00 | | 1.00 | 1.00 | | 0.66 | 1.00 | | 1.00 | |
| Lane Grp Cap(c), veh/h | | 0 | 832 | 74 | 1501 | 647 | 287 | 355 | 315 | 407 | 1022 | 430 | |
| V/C Ratio(X) | 0.46 | 0.00 | 0.37 | 1.09 | 0.96 | 0.15 | 0.11 | 0.17 | 0.19 | 0.55 | 0.29 | 0.17 | |
| Avail Cap(c_a), veh/h | 739 | 0 | 831 | 442 | 1501 | 647 | 340 | 442 | 392 | 407 | 1196 | 503 | |
| HCM Platoon Ratio | 2.00 | 2.00 | 2.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Upstream Filter(I) | 0.94 | 0.00 | 0.94 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Uniform Delay (d), s/veh | ո 4.8 | 0.0 | 0.0 | 49.9 | 20.8 | 9.7 | 31.0 | 31.2 | 31.4 | 29.6 | 25.2 | 24.2 | |
| Incr Delay (d2), s/veh | 1.9 | 0.0 | 1.2 | 131.8 | 16.1 | 0.5 | 0.2 | 0.2 | 0.3 | 0.9 | 0.2 | 0.2 | |
| Initial Q Delay(d3),s/veh | 0.6 | 0.0 | 0.4 | 0.0 | 8.8 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | |
| %ile BackOfQ(50%),veh | n/ln2.3 | 0.0 | 0.4 | 4.6 | 21.0 | 1.0 | 0.6 | 1.2 | 1.2 | 1.8 | 2.6 | 1.3 | |
| Unsig. Movement Delay | , s/veh | ı | | | | | | | | | | | |
| LnGrp Delay(d),s/veh | 7.4 | 0.0 | 1.6 | 181.7 | 45.7 | 10.2 | 31.2 | 31.4 | 31.7 | 30.4 | 25.3 | 24.4 | |
| LnGrp LOS | Α | Α | Α | F | D | В | С | С | С | С | С | С | |
| Approach Vol, veh/h | | 649 | | | 1623 | | | 152 | | | 590 | | |
| Approach Delay, s/veh | | 4.6 | | | 50.5 | | | 31.5 | | | 27.1 | | |
| Approach LOS | | Α | | | D | | | C | | | C | | |
| Timer - Assigned Phs | | 2 | | 4 | | 6 | 7 | 8 | | | | | |
| Phs Duration (G+Y+Rc) | , S | 62.9 | | 37.1 | | 62.9 | 9.9 | 27.2 | | | | | |
| Change Period (Y+Rc), | • | 5.1 | | * 4.7 | | 5.1 | 3.0 | * 4.7 | | | | | |
| Max Green Setting (Gm | | 52.3 | | * 38 | | 52.3 | 6.9 | * 28 | | | | | |
| Max Q Clear Time (g_c- | | 59.8 | | 8.9 | | 55.1 | 8.9 | 5.5 | | | | | |
| Green Ext Time (p_c), s | , . | 0.0 | | 2.4 | | 0.0 | 0.0 | 0.8 | | | | | |
| Intersection Summary | | | | | | | | | | | | | |
| HCM 6th Ctrl Delay | | | 35.1 | | | | | | | | | | |
| HCM 6th LOS | | | D | | | | | | | | | | |
| Notes | | | | | | | | | | | | | |

^{*} HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

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|--------------------------|-----|-------|---------------|------|------|-------|------|----------|------|-------------|------------|------|--|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR | |
| Lane Configurations | | | | | 414 | | ች | ^ | | | ↑ ⊅ | | |
| Traffic Volume (veh/h) | 0 | 0 | 0 | 70 | 350 | 70 | 100 | 523 | 0 | 0 | 593 | 150 | |
| Future Volume (veh/h) | 0 | 0 | 0 | 70 | 350 | 70 | 100 | 523 | 0 | 0 | 593 | 150 | |
| Initial Q (Qb), veh | | | · | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Ped-Bike Adj(A_pbT) | | | | 1.00 | U | 0.91 | 1.00 | U | 1.00 | 1.00 | U | 0.96 | |
| Parking Bus, Adj | | | | 0.85 | 1.00 | 0.85 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.81 | |
| Work Zone On Approacl | h | | | 0.00 | No | 0.00 | 1.00 | No | 1.00 | 1.00 | No | 0.01 | |
| Adj Sat Flow, veh/h/ln | 11 | | | 1660 | 1660 | 1660 | 1660 | 1660 | 0 | 0 | 1660 | 1660 | |
| Adj Flow Rate, veh/h | | | | 75 | 376 | 52 | 1000 | 562 | 0 | 0 | 638 | 126 | |
| Peak Hour Factor | | | | 0.93 | | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | |
| | | | | | 0.93 | | | | | | | | |
| Percent Heavy Veh, % | | | | 3 | 3 | 3 | 3 | 3 | 0 | 0 | 3 | 3 | |
| Cap, veh/h | | | | 124 | 646 | 93 | 379 | 1715 | 0 | 0 | 1280 | 252 | |
| Arrive On Green | | | | 0.32 | 0.32 | 0.32 | 0.54 | 0.54 | 0.00 | 0.00 | 0.54 | 0.54 | |
| Sat Flow, veh/h | | | | 387 | 2023 | 292 | 694 | 3237 | 0 | 0 | 2437 | 464 | |
| Grp Volume(v), veh/h | | | | 268 | 0 | 235 | 108 | 562 | 0 | 0 | 427 | 337 | |
| Grp Sat Flow(s),veh/h/ln | 1 | | | 1384 | 0 | 1318 | 694 | 1577 | 0 | 0 | 1577 | 1240 | |
| Q Serve(g_s), s | | | | 9.8 | 0.0 | 8.9 | 6.9 | 5.9 | 0.0 | 0.0 | 10.2 | 10.2 | |
| Cycle Q Clear(g_c), s | | | | 9.8 | 0.0 | 8.9 | 17.1 | 5.9 | 0.0 | 0.0 | 10.2 | 10.2 | |
| Prop In Lane | | | | 0.28 | | 0.22 | 1.00 | | 0.00 | 0.00 | | 0.37 | |
| ane Grp Cap(c), veh/h | | | | 442 | 0 | 421 | 379 | 1715 | 0 | 0 | 858 | 674 | |
| //C Ratio(X) | | | | 0.61 | 0.00 | 0.56 | 0.28 | 0.33 | 0.00 | 0.00 | 0.50 | 0.50 | |
| Avail Cap(c_a), veh/h | | | | 595 | 0 | 567 | 379 | 1715 | 0 | 0 | 858 | 674 | |
| HCM Platoon Ratio | | | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Jpstream Filter(I) | | | | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 0.00 | 0.00 | 0.48 | 0.48 | |
| Jniform Delay (d), s/veh | 1 | | | 17.2 | 0.0 | 16.9 | 13.9 | 7.6 | 0.0 | 0.0 | 8.6 | 8.6 | |
| ncr Delay (d2), s/veh | | | | 1.3 | 0.0 | 1.2 | 1.9 | 0.5 | 0.0 | 0.0 | 1.0 | 1.3 | |
| nitial Q Delay(d3),s/veh |) | | | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | |
| %ile BackOfQ(50%),veh | | | | 3.1 | 0.0 | 2.6 | 1.2 | 1.8 | 0.0 | 0.0 | 3.1 | 2.5 | |
| Jnsig. Movement Delay | | | | | | | | | | | | | |
| _nGrp Delay(d),s/veh | | | | 18.6 | 0.0 | 18.1 | 15.8 | 8.1 | 0.0 | 0.0 | 9.6 | 9.8 | |
| _nGrp LOS | | | | В | A | В | В | A | A | A | A | A | |
| Approach Vol, veh/h | | | | | 503 | | | 670 | | | 764 | | |
| Approach Delay, s/veh | | | | | 18.3 | | | 9.3 | | | 9.7 | | |
| Approach LOS | | | | | В | | | 3.5 A | | | Α. | | |
| | | | | | U | | | | | | - 7 | | |
| Timer - Assigned Phs | | 2 | | | | 6 | | 8 | | | | | |
| Phs Duration (G+Y+Rc) | , S | 36.8 | | | | 36.8 | | 23.2 | | | | | |
| Change Period (Y+Rc), | | * 4.2 | | | | * 4.2 | | 4.0 | | | | | |
| Max Green Setting (Gm | | * 26 | | | | * 26 | | 25.8 | | | | | |
| //ax Q Clear Time (g_c- | | 19.1 | | | | 12.2 | | 11.8 | | | | | |
| Green Ext Time (p_c), s | | 3.8 | | | | 7.0 | | 2.7 | | | | | |
| ntersection Summary | | | | | | | | | | | | | |
| HCM 6th Ctrl Delay | | | 11.8 | | | | | | | | | | |
| HCM 6th LOS | | | 11.0 B | | | | | | | | | | |
| | | | D | | | | | | | | | | |
| Notes | | | | | | | | | | | | | |

^{*} HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

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|----------------------------------|---------|----------|-------|------|------------|------------|---------|----------|------|----------|------------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | | | | €ि | | ሻ | ^ | | | ∱ ∱ | |
| Traffic Volume (vph) | 0 | 0 | 0 | 51 | 350 | 43 | 30 | 92 | 0 | 10 | 250 | 190 |
| Future Volume (vph) | 0 | 0 | 0 | 51 | 350 | 43 | 30 | 92 | 0 | 10 | 250 | 190 |
| Ideal Flow (vphpl) | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 |
| Total Lost time (s) | | | | | 3.0 | | 4.0 | 4.0 | | | 4.0 | |
| Lane Util. Factor | | | | | 0.95 | | 1.00 | 0.95 | | | 0.95 | |
| Frpb, ped/bikes | | | | | 1.00 | | 1.00 | 1.00 | | | 0.99 | |
| Flpb, ped/bikes | | | | | 1.00 | | 1.00 | 1.00 | | | 1.00 | |
| Frt | | | | | 0.99 | | 1.00 | 1.00 | | | 0.94 | |
| Flt Protected | | | | | 0.99 | | 0.95 | 1.00 | | | 1.00 | |
| Satd. Flow (prot) | | | | | 2870 | | 1568 | 2885 | | | 2692 | |
| Flt Permitted | | | | | 0.99 | | 0.25 | 1.00 | | | 0.95 | |
| Satd. Flow (perm) | | | | | 2870 | | 413 | 2885 | | | 2556 | |
| Peak-hour factor, PHF | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 |
| Adj. Flow (vph) | 0 | 0 | 0 | 73 | 500 | 61 | 43 | 131 | 0 | 14 | 357 | 271 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 11 | 0 | 0 | 0 | 0 | 0 | 188 | 0 |
| Lane Group Flow (vph) | 0 | 0 | 0 | 0 | 623 | 0 | 43 | 131 | 0 | 0 | 454 | 0 |
| Confl. Bikes (#/hr) | | | 1 | | | 1 | | | 1 | | | 1 |
| Heavy Vehicles (%) | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% |
| Parking (#/hr) | | | | 6 | 6 | 4 | | 12 | | | 11 | 11 |
| Turn Type | | | | Perm | NA | | Perm | NA | | Perm | NA | |
| Protected Phases | | | | | 6 | | | 8 | | | 4 | |
| Permitted Phases | | | | 6 | | | 8 | | | 4 | | |
| Actuated Green, G (s) | | | | | 23.0 | | 16.0 | 16.0 | | | 16.0 | |
| Effective Green, g (s) | | | | | 23.0 | | 16.0 | 16.0 | | | 16.0 | |
| Actuated g/C Ratio | | | | | 0.33 | | 0.23 | 0.23 | | | 0.23 | |
| Clearance Time (s) | | | | | 3.0 | | 4.0 | 4.0 | | | 4.0 | |
| Vehicle Extension (s) | | | | | 2.0 | | 2.0 | 2.0 | | | 2.0 | |
| Lane Grp Cap (vph) | | | | | 943 | | 94 | 659 | | | 584 | |
| v/s Ratio Prot | | | | | | | | 0.05 | | | | |
| v/s Ratio Perm | | | | | 0.22 | | 0.10 | | | | c0.18 | |
| v/c Ratio | | | | | 0.66 | | 0.46 | 0.20 | | | 0.78 | |
| Uniform Delay, d1 | | | | | 20.2 | | 23.3 | 21.8 | | | 25.3 | |
| Progression Factor | | | | | 1.00 | | 1.00 | 1.00 | | | 1.00 | |
| Incremental Delay, d2 | | | | | 3.6 | | 15.2 | 0.7 | | | 9.8 | |
| Delay (s) | | | | | 23.8 | | 38.5 | 22.5 | | | 35.1 | |
| Level of Service | | | | | С | | D | С | | | D | |
| Approach Delay (s) | | 0.0 | | | 23.8 | | | 26.4 | | | 35.1 | |
| Approach LOS | | Α | | | С | | | С | | | D | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 29.1 | Н | CM 2000 | Level of | Service | | С | | | |
| HCM 2000 Volume to Capacity | v ratio | | 0.47 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 70.0 | S | um of lost | time (s) | | | 11.0 | | | |
| Intersection Capacity Utilizatio | n | | 47.2% | | | of Service | ! | | Α | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

| Intersection | | | | | | | | | | | | | |
|------------------------|------|------|------|--------|--------|------|------|------|------|---------|------------|------|--|
| Int Delay, s/veh | 2.7 | | | | | | | | | | | | |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR | |
| Lane Configurations | | | | | 41 | | | | | | ∱ } | | |
| Traffic Vol, veh/h | 0 | 0 | 0 | 0 | 331 | 0 | 0 | 0 | 0 | 0 | 0 | 114 | |
| Future Vol, veh/h | 0 | 0 | 0 | 0 | 331 | 0 | 0 | 0 | 0 | 0 | 0 | 114 | |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 79 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop | |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None | |
| Storage Length | - | - | - | - | - | - | - | - | - | - | - | - | |
| Veh in Median Storage, | # - | 2 | - | - | 0 | - | - | 0 | - | - | 0 | - | |
| Grade, % | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - | |
| Peak Hour Factor | 82 | 82 | 82 | 82 | 82 | 82 | 82 | 82 | 82 | 82 | 82 | 82 | |
| Heavy Vehicles, % | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | |
| Mvmt Flow | 0 | 0 | 0 | 0 | 404 | 0 | 0 | 0 | 0 | 0 | 0 | 139 | |
| | | | | | | | | | | | | | |
| Major/Minor | | | _ N | Major2 | | | | | N | /linor2 | | | |
| Conflicting Flow All | | | | 79 | 0 | 0 | | | | - | 483 | 202 | |
| Stage 1 | | | | - | - | - | | | | - | 404 | - | |
| Stage 2 | | | | - | - | - | | | | - | 79 | - | |
| Critical Hdwy | | | | 4.16 | - | - | | | | - | 6.56 | 6.96 | |
| Critical Hdwy Stg 1 | | | | - | - | - | | | | - | 5.56 | - | |
| Critical Hdwy Stg 2 | | | | - | - | - | | | | - | - | - | |
| Follow-up Hdwy | | | | 2.23 | - | - | | | | - | 4.03 | 3.33 | |
| Pot Cap-1 Maneuver | | | | 1510 | - | 0 | | | | 0 | 480 | 802 | |
| Stage 1 | | | | - | - | 0 | | | | 0 | 595 | - | |
| Stage 2 | | | | - | - | 0 | | | | 0 | - | - | |
| Platoon blocked, % | | | | | - | | | | | | | | |
| Mov Cap-1 Maneuver | | | | 1510 | - | - | | | | - | 0 | 802 | |
| Mov Cap-2 Maneuver | | | | - | - | - | | | | - | 0 | - | |
| Stage 1 | | | | - | - | - | | | | - | 0 | - | |
| Stage 2 | | | | - | - | - | | | | - | 0 | - | |
| | | | | | | | | | | | | | |
| Approach | | | | WB | | | | | | SB | | | |
| HCM Control Delay, s | | | | 0 | | | | | | 10.4 | | | |
| HCM LOS | | | | | | | | | | В | | | |
| | | | | | | | | | | | | | |
| Minor Lane/Major Mvmt | | WBL | WRT | SBLn1 | SBI n2 | | | | | | | | |
| Capacity (veh/h) | | 1510 | - | - | 802 | | | | | | | | |
| HCM Lane V/C Ratio | | 1310 | _ | _ | 0.173 | | | | | | | | |
| HCM Control Delay (s) | | 0 | _ | 0 | 10.4 | | | | | | | | |
| HCM Lane LOS | | A | _ | A | В | | | | | | | | |
| HCM 95th %tile Q(veh) | | 0 | _ | - | 0.6 | | | | | | | | |
| TOM OUT TOUIS QUESTI | | | | | 3.0 | | | | | | | | |

| Intersection | | | | | | |
|------------------------|----------|-------|----------|----------|--------|------|
| Int Delay, s/veh | 0.2 | | | | | |
| | | EDD | WDI | WDT | NDI | NDD |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | † | | <u>ነ</u> | ^ | | 7 |
| Traffic Vol, veh/h | 713 | 68 | 54 | 1580 | 0 | 0 |
| Future Vol, veh/h | 713 | 68 | 54 | 1580 | 0 | 0 |
| Conflicting Peds, #/hr | 0 | 31 | 31 | 0 | 0 | 0 |
| | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | 25 | - | - | 0 |
| Veh in Median Storage, | # 0 | - | - | 0 | 0 | - |
| Grade, % | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 94 | 94 | 94 | 94 | 94 | 94 |
| Heavy Vehicles, % | 3 | 3 | 3 | 3 | 3 | 3 |
| Mvmt Flow | 759 | 72 | 57 | 1681 | 0 | 0 |
| WWW | 100 | 12 | O1 | 1001 | • | • |
| | | | | | | |
| | ajor1 | N | //ajor2 | 1 | Minor1 | |
| Conflicting Flow All | 0 | 0 | 862 | 0 | - | 447 |
| Stage 1 | - | - | - | - | - | - |
| Stage 2 | - | - | - | - | - | - |
| Critical Hdwy | - | - | 4.16 | - | - | 6.96 |
| Critical Hdwy Stg 1 | _ | _ | - | _ | _ | _ |
| Critical Hdwy Stg 2 | _ | - | _ | _ | _ | _ |
| Follow-up Hdwy | _ | _ | 2.23 | _ | _ | 3.33 |
| Pot Cap-1 Maneuver | _ | _ | 769 | _ | 0 | 556 |
| Stage 1 | _ | _ | - | _ | 0 | - |
| Stage 2 | _ | _ | _ | _ | 0 | _ |
| Platoon blocked, % | _ | _ | _ | _ | U | _ |
| | - | - | 746 | _ | | E40 |
| Mov Cap-1 Maneuver | - | _ | | - | - | 540 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - |
| Stage 1 | - | - | - | - | - | - |
| Stage 2 | - | - | - | - | - | - |
| | | | | | | |
| Approach | EB | | WB | | NB | |
| HCM Control Delay, s | 0 | | 0.3 | | 0 | |
| HCM LOS | U | | 0.5 | | A | |
| I IOIVI LOG | | | | | ٨ | |
| | | | | | | |
| Minor Lane/Major Mvmt | 1 | NBLn1 | EBT | EBR | WBL | WBT |
| Capacity (veh/h) | | - | - | - | 746 | - |
| HCM Lane V/C Ratio | | _ | _ | | 0.077 | _ |
| HCM Control Delay (s) | | 0 | _ | _ | | _ |
| HCM Lane LOS | | A | _ | _ | В | _ |
| HCM 95th %tile Q(veh) | | | | _ | 0.2 | - |
| HOW SOUL WILLE (Ven) | | - | - | - | 0.2 | - |

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|------------------------------------|-----------|--------------|--------------|------------|--------------|--------------|------|--------------|-------------|-------------|-------------|-------------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | ∱ ∱ | | ሻ | ∱ ∱ | | | ∱ ⊅ | | * | ^ | 7 |
| Traffic Volume (veh/h) | 40 | 1843 | 54 | 80 | 1695 | 60 | 0 | 240 | 64 | 40 | 171 | 50 |
| Future Volume (veh/h) | 40 | 1843 | 54 | 80 | 1695 | 60 | 0 | 240 | 64 | 40 | 171 | 50 |
| Initial Q (Qb), veh | 0 | 15 | 0 | 0 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | 4.00 | 0.97 | 1.00 | 4.00 | 0.97 | 1.00 | 4.00 | 0.97 | 0.99 | 4.00 | 0.89 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach | 4007 | No | 4007 | 4007 | No | 4007 | ^ | No | 4000 | 4000 | No | 4000 |
| Adj Sat Flow, veh/h/ln | 1367 | 1367 | 1367 | 1367 | 1367 | 1367 | 0 | 1660 | 1660 | 1660 | 1660 | 1660 |
| Adj Flow Rate, veh/h | 44 | 2048 | 58 | 89 | 1883 | 64 | 0 | 267 | 62 | 44 | 190 | 37 |
| Peak Hour Factor | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Percent Heavy Veh, % | 3 72 | 3 | 3 28 | 3 | 3 | 3 31 | 0 | 3 | 3 | 3 | 3 | 3 |
| Cap, veh/h Arrive On Green | 0.67 | 1744 0.67 | 0.67 | 72 0.67 | 1741 0.67 | 0.67 | 0.00 | 594 | 135 0.23 | 218 0.23 | 739 0.23 | 294 0.23 |
| | 185 | 2578 | 73 | 158 | 2561 | 86 | 0.00 | 0.23 2620 | 577 | 1028 | 3154 | 1258 |
| Sat Flow, veh/h | | | | | | | | | | | | |
| Grp Volume(v), veh/h | 44 185 | 1026 | 1080 | 89 | 949 | 998 | 0 | 164 1577 | 165 | 44 1028 | 190 | 37 |
| Grp Sat Flow(s),veh/h/ln | 0.0 | 1299 66.7 | 1352 66.7 | 158 0.0 | 1299 66.7 | 1349 66.7 | 0.0 | 8.9 | 1537 9.2 | 3.8 | 1577 4.9 | 1258 2.3 |
| Q Serve(g_s), s | 66.7 | 66.7 | 66.7 | 66.7 | 66.7 | 66.7 | 0.0 | 8.9 | 9.2 | 13.0 | 4.9 | 2.3 |
| Cycle Q Clear(g_c), s Prop In Lane | 1.00 | 00.7 | 0.05 | 1.00 | 00.7 | 0.06 | 0.00 | 0.9 | 0.38 | 1.00 | 4.9 | 1.00 |
| Lane Grp Cap(c), veh/h | 72 | 866 | 906 | 72 | 866 | 905 | 0.00 | 369 | 360 | 218 | 739 | 294 |
| V/C Ratio(X) | 0.61 | 1.18 | 1.19 | 1.24 | 1.10 | 1.10 | 0.00 | 0.44 | 0.46 | 0.20 | 0.26 | 0.13 |
| Avail Cap(c_a), veh/h | 72 | 866 | 901 | 72 | 866 | 899 | 0.00 | 420 | 409 | 251 | 839 | 335 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 0.09 | 0.09 | 0.09 | 0.00 | 0.76 | 0.76 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 50.0 | 16.7 | 16.7 | 50.0 | 16.7 | 16.7 | 0.0 | 32.7 | 32.9 | 38.5 | 31.2 | 30.2 |
| Incr Delay (d2), s/veh | 33.0 | 94.7 | 97.5 | 117.0 | 44.8 | 48.2 | 0.0 | 0.6 | 0.7 | 0.5 | 0.2 | 0.2 |
| Initial Q Delay(d3),s/veh | 0.0 | 31.2 | 29.8 | 0.0 | 20.8 | 19.9 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/ln | 1.7 | 46.3 | 48.8 | 4.1 | 31.8 | 33.9 | 0.0 | 3.5 | 3.5 | 1.0 | 1.9 | 0.7 |
| Unsig. Movement Delay, s/veh | | | | | | | | | | | | |
| LnGrp Delay(d),s/veh | 83.0 | 142.6 | 143.9 | 167.0 | 82.3 | 84.8 | 0.0 | 33.4 | 33.6 | 38.9 | 31.4 | 30.4 |
| LnGrp LOS | F | F | F | F | F | F | Α | С | С | D | С | С |
| Approach Vol, veh/h | | 2150 | | | 2036 | | | 329 | | | 271 | |
| Approach Delay, s/veh | | 142.0 | | | 87.2 | | | 33.5 | | | 32.5 | |
| Approach LOS | | F | | | F | | | С | | | С | |
| Timer - Assigned Phs | | 2 | | 4 | | 6 | | 8 | | | | |
| Phs Duration (G+Y+Rc), s | | 72.1 | | 27.9 | | 72.1 | | 27.9 | | | | |
| Change Period (Y+Rc), s | | 5.4 | | 4.5 | | 5.4 | | 4.5 | | | | |
| Max Green Setting (Gmax), s | | 63.5 | | 26.6 | | 63.5 | | 26.6 | | | | |
| Max Q Clear Time (g_c+I1), s | | 68.7 | | 15.0 | | 68.7 | | 11.2 | | | | |
| Green Ext Time (p_c), s | | 0.0 | | 1.2 | | 0.0 | | 1.8 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 6th Ctrl Delay | | | 105.0 | | | | | | | | | |
| HCM 6th LOS | | | F | | | | | | | | | |

| | • | → | • | • | ← | • | 4 | † | / | / | ţ | 4 | |
|---|-----------|--------------|--------------|---------------|--------------|--------------|-----------|------------|-------------|-------------|------------|------|--|
| | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR | |
| Lane Configurations | ሻ | ħβ | | ነ | ħβ | | 7 | ∱ ∱ | | ነ | ∱ ∱ | | |
| Traffic Volume (veh/h) | 51 | 1682 | 44 | 97 | 1660 | 50 | 81 | 444 | 177 | 40 | 374 | 70 | |
| Future Volume (veh/h) | 51 | 1682 | 44 | 97 | 1660 | 50 | 81 | 444 | 177 | 40 | 374 | 70 | |
| Initial Q (Qb), veh | 0 | 15 | 0 | 0 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| , _, , | 1.00 | | 0.97 | 1.00 | | 0.98 | 0.99 | | 0.97 | 1.00 | | 0.97 | |
| • , | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Work Zone On Approach | | No | | | No | | | No | | | No | | |
| • | 1367 | 1367 | 1367 | 1367 | 1367 | 1367 | 1660 | 1660 | 1660 | 1660 | 1660 | 1660 | |
| Adj Flow Rate, veh/h | 57 | 1869 | 48 | 108 | 1844 | 54 | 90 | 493 | 184 | 44 | 416 | 65 | |
| | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | |
| Percent Heavy Veh, % | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | |
| Cap, veh/h | 72 | 1644 | 22 | 72 | 1641 | 25 | 190 | 593 | 220 | 130 | 723 | 112 | |
| | 0.63 | 0.63 | 0.63 | 0.63 | 0.63 | 0.63 | 0.53 | 0.53 | 0.53 | 0.27 | 0.27 | 0.27 | |
| Sat Flow, veh/h | 194 | 2586 | 66 | 191 | 2576 | 75 | 898 | 2233 | 827 | 752 | 2725 | 422 | |
| Grp Volume(v), veh/h | 57 | 934 | 983 | 108 | 925 | 973 | 90 | 347 | 330 | 44 | 239 | 242 | |
| Grp Sat Flow(s),veh/h/ln | | 1299 | 1353 | 191 | 1299 | 1352 | 898 | 1577 | 1483 | 752 | 1577 | 1570 | |
| Q Serve(g_s), s | 0.0 | 62.7 | 62.7 | 0.0 | 62.7 | 62.7 | 9.2 | 18.5 | 18.8 | 5.7 | 13.1 | 13.4 | |
| (6-): | 62.7 | 62.7 | 62.7 | 62.7 | 62.7 | 62.7 | 22.6 | 18.5 | 18.8 | 24.5 | 13.1 | 13.4 | |
| | 1.00 | | 0.05 | 1.00 | | 0.06 | 1.00 | | 0.56 | 1.00 | | 0.27 | |
| Lane Grp Cap(c), veh/h | 72 | 814 | 852 | 72 | 814 | 852 | 190 | 419 | 394 | 130 | 419 | 417 | |
| . , | 0.79 | 1.15 | 1.15 | 1.50 | 1.14 | 1.14 | 0.47 | 0.83 | 0.84 | 0.34 | 0.57 | 0.58 | |
| Avail Cap(c_a), veh/h | 72 | 814 | 848 | 72 | 814 | 847 | 191 | 420 | 394 | 131 | 420 | 418 | |
| | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 2.00 | 2.00 | 2.00 | 1.00 | 1.00 | 1.00 | |
| 1 (/ | 0.09 | 0.09 | 0.09 | 1.00 | 1.00 | 1.00 | 0.61 | 0.61 | 0.61 | 1.00 | 1.00 | 1.00 | |
| Uniform Delay (d), s/veh | | 18.7 | 18.7 70.5 | 50.0 284.3 | 18.7 76.4 | 18.7 | 28.7 | 21.6 | 21.6 9.5 | 45.2 1.5 | 31.8 | 31.9 | |
| Incr Delay (d2), s/veh Initial Q Delay(d3),s/veh | 7.9 | 68.1 33.2 | 31.7 | 0.0 | 22.1 | 77.9 21.1 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | |
| %ile BackOfQ(50%),veh/ | | 38.7 | 40.8 | 7.5 | 38.1 | 40.0 | 1.8 | 5.8 | 5.6 | 1.1 | 5.2 | 5.3 | |
| Unsig. Movement Delay, | | | 40.0 | 1.5 | 30.1 | 40.0 | 1.0 | 5.0 | 5.0 | 1.1 | 0.2 | 5.5 | |
| , | | 119.9 | 120.9 | 334.3 | 117.2 | 117.7 | 29.8 | 29.9 | 31.1 | 46.7 | 33.7 | 33.9 | |
| LnGrp LOS | 57.5 E | F | 120.5 F | 554.5 F | F | F | 23.0 C | 23.3 C | C | D | 00.7 C | C | |
| Approach Vol, veh/h | | 1974 | | | 2006 | ı | | 767 | | <u> </u> | 525 | | |
| Approach Delay, s/veh | | 118.6 | | | 129.2 | | | 30.4 | | | 34.9 | | |
| Approach LOS | | F | | | 129.2 F | | | 30.4 C | | | 04.9 C | | |
| | | | | | | | | | | | U | | |
| Timer - Assigned Phs | | 2 | | 4 | | 6 | | 8 | | | | | |
| Phs Duration (G+Y+Rc), | | 68.1 | | 31.9 | | 68.1 | | 31.9 | | | | | |
| Change Period (Y+Rc), s | | 5.4 | | 5.4 | | 5.4 | | 5.4 | | | | | |
| Max Green Setting (Gma | ,, | 62.6 | | 26.6 | | 62.6 | | 26.6 | | | | | |
| Max Q Clear Time (g_c+ | l1), s | 64.7 | | 26.5 | | 64.7 | | 24.6 | | | | | |
| Green Ext Time (p_c), s | | 0.0 | | 0.0 | | 0.0 | | 1.0 | | | | | |
| Intersection Summary | | | | | | | | | | | | | |
| HCM 6th Ctrl Delay | | | 101.5 | | | | | | | | | | |
| HCM 6th LOS | | | F | | | | | | | | | | |

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|-----------------------------------|---------|------------|--------|-------|------------|------------|---------|------------|------|----------|------------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | ∱ ⊅ | | | €î₽ | | * | ∱ β | | ሻ | ∱ β | |
| Traffic Volume (vph) | 0 | 1434 | 100 | 100 | 830 | 50 | 56 | 265 | 104 | 55 | 200 | 60 |
| Future Volume (vph) | 0 | 1434 | 100 | 100 | 830 | 50 | 56 | 265 | 104 | 55 | 200 | 60 |
| Ideal Flow (vphpl) | 1400 | 1400 | 1400 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 |
| Total Lost time (s) | | 5.1 | | | 5.1 | | 4.5 | 4.5 | | 4.5 | 4.5 | |
| Lane Util. Factor | | 0.95 | | | 0.95 | | 1.00 | 0.95 | | 1.00 | 0.95 | |
| Frpb, ped/bikes | | 0.98 | | | 0.98 | | 1.00 | 0.92 | | 1.00 | 0.93 | |
| Flpb, ped/bikes | | 1.00 | | | 1.00 | | 0.80 | 1.00 | | 0.86 | 1.00 | |
| Frt | | 0.99 | | | 0.99 | | 1.00 | 0.96 | | 1.00 | 0.97 | |
| Flt Protected | | 1.00 | | | 0.99 | | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | | 2515 | | | 3038 | | 1248 | 2568 | | 1341 | 2805 | |
| Flt Permitted | | 1.00 | | | 0.54 | | 0.53 | 1.00 | | 0.40 | 1.00 | |
| Satd. Flow (perm) | | 2515 | | | 1658 | | 694 | 2568 | | 568 | 2805 | |
| Peak-hour factor, PHF | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Adj. Flow (vph) | 0 | 1509 | 105 | 105 | 874 | 53 | 59 | 279 | 109 | 58 | 211 | 63 |
| RTOR Reduction (vph) | 0 | 4 | 0 | 0 | 4 | 0 | 0 | 41 | 0 | 0 | 26 | 0 |
| Lane Group Flow (vph) | 0 | 1610 | 0 | 0 | 1028 | 0 | 59 | 347 | 0 | 58 | 248 | 0 |
| Confl. Peds. (#/hr) | 423 | | 174 | 174 | | 423 | 282 | | 215 | 215 | | 282 |
| Confl. Bikes (#/hr) | | | 6 | | | 1 | | | 1 | | | 1 |
| Heavy Vehicles (%) | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% |
| Parking (#/hr) | | | | | | | | 8 | 8 | | | |
| Turn Type | | NA | | pm+pt | NA | | Perm | NA | | Perm | NA | |
| Protected Phases | | 2 | | 1 | 6 | | | 8 | | | 4 | |
| Permitted Phases | | | | 6 | | | 8 | | | 4 | | |
| Actuated Green, G (s) | | 59.5 | | | 67.2 | | 23.2 | 23.2 | | 23.2 | 23.2 | |
| Effective Green, g (s) | | 59.5 | | | 67.2 | | 23.2 | 23.2 | | 23.2 | 23.2 | |
| Actuated g/C Ratio | | 0.60 | | | 0.67 | | 0.23 | 0.23 | | 0.23 | 0.23 | |
| Clearance Time (s) | | 5.1 | | | 5.1 | | 4.5 | 4.5 | | 4.5 | 4.5 | |
| Vehicle Extension (s) | | 5.0 | | | 5.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | | 1496 | | | 1176 | | 161 | 595 | | 131 | 650 | |
| v/s Ratio Prot | | c0.64 | | | c0.04 | | | c0.13 | | | 0.09 | |
| v/s Ratio Perm | | | | | 0.55 | | 0.09 | | | 0.10 | | |
| v/c Ratio | | 1.08 | | | 0.87 | | 0.37 | 0.58 | | 0.44 | 0.38 | |
| Uniform Delay, d1 | | 20.2 | | | 13.0 | | 32.2 | 34.1 | | 32.9 | 32.4 | |
| Progression Factor | | 1.00 | | | 0.93 | | 1.00 | 1.00 | | 0.60 | 0.52 | |
| Incremental Delay, d2 | | 46.6 | | | 6.4 | | 1.4 | 1.5 | | 1.4 | 0.2 | |
| Delay (s) | | 66.9 | | | 18.5 | | 33.6 | 35.6 | | 21.1 | 17.1 | |
| Level of Service | | Е | | | В | | С | D | | С | В | |
| Approach Delay (s) | | 66.9 | | | 18.5 | | | 35.3 | | | 17.8 | |
| Approach LOS | | Е | | | В | | | D | | | В | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 43.4 | Н | CM 2000 | Level of | Service | | D | | | |
| HCM 2000 Volume to Capacit | y ratio | | 0.94 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 100.0 | | um of lost | | | | 12.8 | | | |
| Intersection Capacity Utilization | n | | 129.1% | IC | CU Level | of Service | ! | | Н | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

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|--|--------|--------------|------|-------|----------|-------------|------|----------|------|-------------|-----------|------|--|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR | |
| Lane Configurations | * | ∱ } | | ች | ħβ | | ች | ^ | 7 | | ΦÞ | | |
| Traffic Volume (veh/h) | 140 | 1299 | 157 | 106 | 838 | 50 | 86 | 543 | 170 | 0 | 459 | 76 | |
| Future Volume (veh/h) | 140 | 1299 | 157 | 106 | 838 | 50 | 86 | 543 | 170 | 0 | 459 | 76 | |
| Initial Q (Qb), veh | 0 | 10 | 0 | 0 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Ped-Bike Adj(A_pbT) | 0.98 | 10 | 0.90 | 1.00 | 10 | 0.90 | 0.96 | | 0.82 | 1.00 | J | 0.83 | |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Work Zone On Approac | | No | 1.00 | 1.00 | No | 1.00 | 1.00 | No | 1.00 | 1.00 | No | 1.00 | |
| Adj Sat Flow, veh/h/ln | 1367 | 1367 | 1367 | 1660 | 1660 | 1660 | 1660 | 1660 | 1660 | 0 | 1660 | 1660 | |
| Adj Flow Rate, veh/h | 147 | 1367 | 158 | 112 | 882 | 49 | 91 | 572 | 158 | 0 | 483 | 67 | |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | |
| Percent Heavy Veh, % | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 0.93 | 3 | 3 | |
| | 73 | 1810 | 197 | 72 | 2343 | 128 | 150 | 817 | 299 | 0 | 702 | 96 | |
| Cap, veh/h | | | | | | | | | | | | | |
| Arrive On Green | 0.77 | 0.77 | 0.77 | 1.00 | 1.00 | 1.00 | 0.26 | 0.26 | 0.26 | 0.00 | 0.26 | 0.26 | |
| Sat Flow, veh/h | 480 | 2319 | 265 | 339 | 3019 | 168 | 814 | 3154 | 1156 | 0 | 2792 | 372 | |
| Grp Volume(v), veh/h | 147 | 759 | 766 | 112 | 461 | 470 | 91 | 572 | 158 | 0 | 279 | 271 | |
| Grp Sat Flow(s),veh/h/l | | 1299 | 1286 | 339 | 1577 | 1609 | 814 | 1577 | 1156 | 0 | 1577 | 1503 | |
| Q Serve(g_s), s | 10.1 | 31.6 | 33.2 | 25.8 | 0.0 | 0.0 | 9.6 | 16.4 | 11.7 | 0.0 | 15.9 | 16.3 | |
| Cycle Q Clear(g_c), s | 10.5 | 31.6 | 33.2 | 60.6 | 0.0 | 0.0 | 25.9 | 16.4 | 11.7 | 0.0 | 15.9 | 16.3 | |
| Prop In Lane | 1.00 | | 0.21 | 1.00 | | 0.10 | 1.00 | | 1.00 | 0.00 | | 0.25 | |
| Lane Grp Cap(c), veh/h | n 73 | 1007 | 999 | 72 | 1222 | 1248 | 150 | 817 | 299 | 0 | 408 | 389 | |
| V/C Ratio(X) | 2.02 | 0.75 | 0.77 | 1.55 | 0.38 | 0.38 | 0.61 | 0.70 | 0.53 | 0.00 | 0.68 | 0.70 | |
| Avail Cap(c_a), veh/h | 442 | 1007 | 996 | 217 | 1222 | 1247 | 150 | 817 | 299 | 0 | 408 | 389 | |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 2.00 | 2.00 | 2.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 0.86 | 0.86 | 0.86 | 0.94 | 0.94 | 0.94 | 0.00 | 0.38 | 0.38 | |
| Uniform Delay (d), s/ve | h 50.0 | 6.5 | 6.6 | 38.7 | 0.0 | 0.0 | 45.9 | 33.5 | 31.8 | 0.0 | 33.4 | 33.5 | |
| Incr Delay (d2), s/veh | 505.2 | 5.2 | 5.6 | 298.8 | 0.8 | 0.7 | 6.4 | 2.5 | 1.6 | 0.0 | 1.8 | 2.1 | |
| Initial Q Delay(d3),s/vel | | 0.7 | 0.8 | 0.0 | 0.2 | 0.2 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | |
| %ile BackOfQ(50%),ve | | 9.0 | 9.3 | 7.7 | 0.3 | 0.3 | 2.5 | 6.5 | 3.4 | 0.0 | 6.3 | 6.1 | |
| Unsig. Movement Delay | | | | | | | | | | | | | |
| LnGrp Delay(d),s/veh | • | 12.5 | 13.0 | 337.5 | 1.0 | 0.9 | 52.2 | 36.1 | 33.4 | 0.0 | 35.2 | 35.6 | |
| LnGrp LOS | F | В | В | F | Α | Α | D | D | С | Α | D | D | |
| Approach Vol, veh/h | | 1672 | | • | 1043 | | _ | 821 | | | 550 | | |
| Approach Delay, s/veh | | 60.4 | | | 37.1 | | | 37.3 | | | 35.4 | | |
| Approach LOS | | 00.4 E | | | D | | | 37.3 | | | 55.4 D | | |
| Timer - Assigned Phs | | 2 | | 4 | | 6 | | 8 | | | | | |
| Phs Duration (G+Y+Rc |) c | 83.0 | | 31.0 | | 83.0 | | 31.0 | | | | | |
| Change Period (Y+Rc), | , . | 5.1 | | * 5.1 | | 5.1 | | 5.1 | | | | | |
| | | | | * 26 | | | | | | | | | |
| Max Green Setting (Gr | | 64.3 | | | | 64.3 | | 25.5 | | | | | |
| Max Q Clear Time (g_c Green Ext Time (p_c), | | 35.2 24.5 | | 27.9 | | 62.6 1.4 | | 18.3 | | | | | |
| * | 3 | 24.0 | | 0.0 | | 1.4 | | ۷.۱ | | | | | |
| Intersection Summary | | | 40 = | | | | | | | | | | |
| HCM 6th Ctrl Delay | | | 46.5 | | | | | | | | | | |
| HCM 6th LOS | | | D | | | | | | | | | | |
| Notes | | | | | | | | | | | | | |

^{*} HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

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|-------------------------------|----------|------|-------|----------|------|------|------------|------|-------------|----------|------|--|
| Movement EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR | |
| Lane Configurations | † | | * | ^ | 7 | ች | † } | | ች | ^ | 7 | |
| Traffic Volume (veh/h) 0 | 1218 | 121 | 80 | 950 | 280 | 53 | 250 | 90 | 200 | 200 | 40 | |
| Future Volume (veh/h) 0 | 1218 | 121 | 80 | 950 | 280 | 53 | 250 | 90 | 200 | 200 | 40 | |
| Initial Q (Qb), veh 0 | 10 | 0 | 0 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Ped-Bike Adj(A_pbT) 1.00 | 10 | 0.95 | 0.99 | 10 | 0.95 | 0.92 | · · | 0.89 | 0.95 | J | 0.92 | |
| Parking Bus, Adj 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Work Zone On Approach | No | 1.00 | 1.00 | No | 1.00 | 1.00 | No | 1.00 | 1.00 | No | 1.00 | |
| Adj Sat Flow, veh/h/ln 0 | 1367 | 1367 | 1660 | 1660 | 1660 | 1660 | 1660 | 1660 | 1660 | 1660 | 1660 | |
| Adj Flow Rate, veh/h 0 | 1256 | 118 | 82 | 979 | 191 | 55 | 258 | 93 | 206 | 206 | 13 | |
| Peak Hour Factor 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | |
| Percent Heavy Veh, % 0 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | |
| Cap, veh/h 0 | 1371 | 92 | 72 | 1739 | 738 | 339 | 559 | 193 | 326 | 1107 | 454 | |
| Arrive On Green 0.00 | 1.00 | 1.00 | 0.55 | 0.55 | 0.55 | 0.25 | 0.25 | 0.25 | 0.07 | 0.35 | 0.35 | |
| Sat Flow, veh/h 0.00 | 2457 | 224 | 390 | 3154 | 1339 | 1059 | 2221 | 766 | 1581 | 3154 | 1295 | |
| | | | | | | | | | | | | |
| Grp Volume(v), veh/h 0 | 681 | 693 | 82 | 979 | 191 | 55 | 180 | 171 | 206 | 206 | 13 | |
| Grp Sat Flow(s), veh/h/ln 0 | 1299 | 1313 | 390 | 1577 | 1339 | 1059 | 1577 | 1410 | 1581 | 1577 | 1295 | |
| Q Serve(g_s), s 0.0 | 0.0 | 0.0 | 12.0 | 20.2 | 7.5 | 4.1 | 9.6 | 10.3 | 6.9 | 4.5 | 0.7 | |
| Cycle Q Clear(g_c), s 0.0 | 0.0 | 0.0 | 12.0 | 20.2 | 7.5 | 4.1 | 9.6 | 10.3 | 6.9 | 4.5 | 0.7 | |
| Prop In Lane 0.00 | | 0.17 | 1.00 | | 1.00 | 1.00 | | 0.54 | 1.00 | | 1.00 | |
| Lane Grp Cap(c), veh/h 0 | 716 | 731 | 72 | 1739 | 738 | 339 | 397 | 355 | 326 | 1107 | 454 | |
| V/C Ratio(X) 0.00 | 0.95 | 0.95 | 1.14 | 0.56 | 0.26 | 0.16 | 0.45 | 0.48 | 0.63 | 0.19 | 0.03 | |
| Avail Cap(c_a), veh/h 0 | 716 | 724 | 287 | 1739 | 738 | 368 | 442 | 395 | 326 | 1196 | 491 | |
| HCM Platoon Ratio 1.00 | 2.00 | 2.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Upstream Filter(I) 0.00 | 0.30 | 0.30 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Uniform Delay (d), s/veh 0.0 | 0.0 | 0.0 | 50.0 | 15.0 | 11.7 | 29.5 | 31.6 | 31.9 | 29.3 | 22.5 | 21.3 | |
| Incr Delay (d2), s/veh 0.0 | 10.1 | 9.5 | 148.7 | 1.3 | 0.9 | 0.2 | 0.8 | 1.0 | 3.0 | 0.1 | 0.0 | |
| Initial Q Delay(d3),s/veh 0.0 | 7.2 | 6.4 | 0.0 | 0.5 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | |
| %ile BackOfQ(50%),veh/lr0.0 | 3.4 | 3.2 | 4.8 | 8.0 | 2.4 | 1.1 | 3.8 | 3.6 | 1.9 | 1.7 | 0.2 | |
| Unsig. Movement Delay, s/veh | | | | | | | | | | | | |
| LnGrp Delay(d),s/veh 0.0 | 17.3 | 16.0 | 198.7 | 16.9 | 12.6 | 29.7 | 32.4 | 32.9 | 32.3 | 22.6 | 21.3 | |
| LnGrp LOS A | В | В | F | В | В | С | С | С | С | С | С | |
| Approach Vol, veh/h | 1374 | | | 1252 | | | 406 | | | 425 | | |
| Approach Delay, s/veh | 16.6 | | | 28.1 | | | 32.2 | | | 27.3 | | |
| Approach LOS | В | | | C | | | C | | | C | | |
| Timer - Assigned Phs | 2 | | 4 | | 6 | 7 | 8 | | | | | |
| Phs Duration (G+Y+Rc), s | 60.2 | | 39.8 | | 60.2 | 9.9 | 29.9 | | | | | |
| Change Period (Y+Rc), s | 5.1 | | * 4.7 | | 5.1 | 3.0 | * 4.7 | | | | | |
| Max Green Setting (Gmax), s | 52.3 | | * 38 | | 52.3 | 6.9 | * 28 | | | | | |
| Max Q Clear Time (g_c+l1), s | 2.0 | | 6.5 | | 22.2 | 8.9 | 12.3 | | | | | |
| Green Ext Time (p_c), s | 29.9 | | 1.5 | | 19.1 | 0.0 | 2.2 | | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 6th Ctrl Delay | | 23.9 | | | | | | | | | | |
| HCM 6th LOS | | С | | | | | | | | | | |
| Notes | | | | | | | | | | | | |

^{*} HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

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|---------------------------|---------|----------|------|------|----------|-------|------|----------|------|----------|------|------|--|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR | |
| Lane Configurations | | | | | 414 | | | ^ | | | ħβ | | |
| Traffic Volume (veh/h) | 0 | 0 | 0 | 110 | 172 | 71 | 140 | 460 | 0 | 0 | 547 | 103 | |
| Future Volume (veh/h) | 0 | 0 | 0 | 110 | 172 | 71 | 140 | 460 | 0 | 0 | 547 | 103 | |
| Initial Q (Qb), veh | | | | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Ped-Bike Adj(A_pbT) | | | | 1.00 | * | 0.79 | 0.95 | • | 1.00 | 1.00 | • | 0.77 | |
| Parking Bus, Adj | | | | 0.85 | 1.00 | 0.85 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.81 | |
| Work Zone On Approach | h | | | 0.00 | No | 0.00 | | No | | | No | 0.0. | |
| Adj Sat Flow, veh/h/ln | | | | 1660 | 1660 | 1660 | 1660 | 1660 | 0 | 0 | 1660 | 1660 | |
| Adj Flow Rate, veh/h | | | | 116 | 181 | 55 | 147 | 484 | 0 | 0 | 576 | 83 | |
| Peak Hour Factor | | | | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | |
| Percent Heavy Veh, % | | | | 3 | 3 | 3 | 3 | 3 | 0.00 | 0.00 | 3 | 3 | |
| Cap, veh/h | | | | 308 | 494 | 153 | 358 | 1547 | 0 | 0 | 1176 | 168 | |
| Arrive On Green | | | | 0.37 | 0.37 | 0.37 | 0.49 | 0.49 | 0.00 | 0.00 | 0.49 | 0.49 | |
| Sat Flow, veh/h | | | | 827 | 1325 | 410 | 727 | 3237 | 0.00 | 0.00 | 2481 | 342 | |
| Grp Volume(v), veh/h | | | | 191 | 0 | 161 | 147 | 484 | 0 | 0 | 377 | 282 | |
| | | | | 1362 | 0 | 1200 | 727 | 1577 | | 0 | 1577 | 1163 | |
| Grp Sat Flow(s), veh/h/ln | | | | | | | | | 0 | | | | |
| Q Serve(g_s), s | | | | 6.1 | 0.0 | 5.8 | 10.2 | 5.5 | 0.0 | 0.0 | 9.6 | 9.8 | |
| Cycle Q Clear(g_c), s | | | | 6.1 | 0.0 | 5.8 | 20.0 | 5.5 | 0.0 | 0.0 | 9.6 | 9.8 | |
| Prop In Lane | | | | 0.61 | ^ | 0.34 | 1.00 | 4547 | 0.00 | 0.00 | 774 | 0.29 | |
| Lane Grp Cap(c), veh/h | | | | 508 | 0 | 447 | 358 | 1547 | 0 | 0 | 774 | 571 | |
| V/C Ratio(X) | | | | 0.38 | 0.00 | 0.36 | 0.41 | 0.31 | 0.00 | 0.00 | 0.49 | 0.49 | |
| Avail Cap(c_a), veh/h | | | | 585 | 0 | 516 | 358 | 1547 | 0 | 0 | 774 | 571 | |
| HCM Platoon Ratio | | | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Upstream Filter(I) | | | | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 0.00 | 0.00 | 0.50 | 0.50 | |
| Uniform Delay (d), s/veh | 1 | | | 13.7 | 0.0 | 13.6 | 17.0 | 9.2 | 0.0 | 0.0 | 10.2 | 10.3 | |
| Incr Delay (d2), s/veh | | | | 0.5 | 0.0 | 0.5 | 3.5 | 0.5 | 0.0 | 0.0 | 1.1 | 1.5 | |
| Initial Q Delay(d3),s/veh | | | | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | |
| %ile BackOfQ(50%),veh | | | | 1.8 | 0.0 | 1.5 | 1.9 | 1.8 | 0.0 | 0.0 | 3.1 | 2.4 | |
| Unsig. Movement Delay | , s/veh | | | | | | | | | | | | |
| LnGrp Delay(d),s/veh | | | | 14.2 | 0.0 | 14.1 | 20.5 | 9.7 | 0.0 | 0.0 | 11.3 | 11.8 | |
| LnGrp LOS | | | | В | Α | В | С | Α | Α | Α | В | В | |
| Approach Vol, veh/h | | | | | 352 | | | 631 | | | 659 | | |
| Approach Delay, s/veh | | | | | 14.2 | | | 12.2 | | | 11.5 | | |
| Approach LOS | | | | | В | | | В | | | В | | |
| Timer - Assigned Phs | | 2 | | | | 6 | | 8 | | | | | |
| Phs Duration (G+Y+Rc) | S | 33.6 | | | | 33.6 | | 26.4 | | | | | |
| Change Period (Y+Rc), | | * 4.2 | | | | * 4.2 | | 4.0 | | | | | |
| Max Green Setting (Gm | | * 26 | | | | * 26 | | 25.8 | | | | | |
| Max Q Clear Time (g_c+ | | 22.0 | | | | 11.8 | | 8.1 | | | | | |
| Green Ext Time (p_c), s | | 2.2 | | | | 6.2 | | 2.1 | | | | | |
| Intersection Summary | | | | | | | | | | | | | |
| HCM 6th Ctrl Delay | | | 12.4 | | | | | | | | | | |
| | | | | | | | | | | | | | |
| HCM 6th LOS | | | В | | | | | | | | | | |
| Notes | | | | | | | | | | | | | |

^{*} HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

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|----------------------------------|---------|----------|-------|------|-------------|------------|---------|----------|----------|----------|------------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | | | | € 1} | | ň | ^ | | | ∱ } | |
| Traffic Volume (vph) | 0 | 0 | 0 | 90 | 202 | 158 | 70 | 317 | 0 | 0 | 390 | 130 |
| Future Volume (vph) | 0 | 0 | 0 | 90 | 202 | 158 | 70 | 317 | 0 | 0 | 390 | 130 |
| Ideal Flow (vphpl) | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 |
| Total Lost time (s) | | | | | 3.0 | | 4.0 | 4.0 | | | 4.0 | |
| Lane Util. Factor | | | | | 0.95 | | 1.00 | 0.95 | | | 0.95 | |
| Frpb, ped/bikes | | | | | 1.00 | | 1.00 | 1.00 | | | 1.00 | |
| Flpb, ped/bikes | | | | | 1.00 | | 1.00 | 1.00 | | | 1.00 | |
| Frt | | | | | 0.95 | | 1.00 | 1.00 | | | 0.96 | |
| Flt Protected | | | | | 0.99 | | 0.95 | 1.00 | | | 1.00 | |
| Satd. Flow (prot) | | | | | 2738 | | 1568 | 2885 | | | 2775 | |
| Flt Permitted | | | | | 0.99 | | 0.27 | 1.00 | | | 1.00 | |
| Satd. Flow (perm) | | | | | 2738 | | 447 | 2885 | | | 2775 | |
| Peak-hour factor, PHF | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Adj. Flow (vph) | 0 | 0 | 0 | 95 | 213 | 166 | 74 | 334 | 0 | 0 | 411 | 137 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 99 | 0 | 0 | 0 | 0 | 0 | 46 | 0 |
| Lane Group Flow (vph) | 0 | 0 | 0 | 0 | 375 | 0 | 74 | 334 | 0 | 0 | 502 | 0 |
| Confl. Bikes (#/hr) | | | 1 | | | 1 | | | 1 | | | 1 |
| Heavy Vehicles (%) | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% |
| Parking (#/hr) | | | | 6 | 6 | 4 | | 12 | | | 11 | 11 |
| Turn Type | | | | Perm | NA | | Perm | NA | | | NA | |
| Protected Phases | | | | | 6 | | | 8 | | | 4 | |
| Permitted Phases | | | | 6 | | | 8 | | | | | |
| Actuated Green, G (s) | | | | | 23.0 | | 16.0 | 16.0 | | | 16.0 | |
| Effective Green, g (s) | | | | | 23.0 | | 16.0 | 16.0 | | | 16.0 | |
| Actuated g/C Ratio | | | | | 0.33 | | 0.23 | 0.23 | | | 0.23 | |
| Clearance Time (s) | | | | | 3.0 | | 4.0 | 4.0 | | | 4.0 | |
| Vehicle Extension (s) | | | | | 2.0 | | 2.0 | 2.0 | | | 2.0 | |
| Lane Grp Cap (vph) | | | | | 899 | | 102 | 659 | | | 634 | |
| v/s Ratio Prot | | | | | 000 | | 102 | 0.12 | | | c0.18 | |
| v/s Ratio Perm | | | | | 0.14 | | 0.17 | V | | | 001.10 | |
| v/c Ratio | | | | | 0.42 | | 0.73 | 0.51 | | | 0.79 | |
| Uniform Delay, d1 | | | | | 18.3 | | 25.0 | 23.6 | | | 25.4 | |
| Progression Factor | | | | | 1.00 | | 1.00 | 1.00 | | | 1.00 | |
| Incremental Delay, d2 | | | | | 1.4 | | 36.1 | 2.8 | | | 9.8 | |
| Delay (s) | | | | | 19.7 | | 61.1 | 26.3 | | | 35.2 | |
| Level of Service | | | | | В | | E | C | | | D | |
| Approach Delay (s) | | 0.0 | | | 19.7 | | | 32.6 | | | 35.2 | |
| Approach LOS | | A | | | В | | | С | | | D | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 29.3 | H | CM 2000 | Level of | Service | | С | | | |
| HCM 2000 Volume to Capacity | y ratio | | 0.38 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 70.0 | Sı | um of lost | time (s) | | | 11.0 | | | |
| Intersection Capacity Utilizatio | n | | 49.8% | | | of Service | ! | | Α | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

| Intersection | | | | | | | | | | | | |
|------------------------|------|------|------|--------|-------|------|------|------|------|--------|------------|------|
| Int Delay, s/veh | 1.6 | | | | | | | | | | | |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | | | | 414 | | | | | | † ‡ | |
| Traffic Vol, veh/h | 0 | 0 | 0 | 0 | 385 | 0 | 0 | 0 | 0 | 0 | 0 | 74 |
| Future Vol, veh/h | 0 | 0 | 0 | 0 | 385 | 0 | 0 | 0 | 0 | 0 | 0 | 74 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 251 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | _ | - | None | - | - | None | - | - | | - | - | None |
| Storage Length | _ | _ | - | - | _ | - | - | - | _ | - | - | - |
| Veh in Median Storage, | # - | 2 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, % | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 |
| Heavy Vehicles, % | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 |
| Mvmt Flow | 0 | 0 | 0 | 0 | 405 | 0 | 0 | 0 | 0 | 0 | 0 | 78 |
| | | | | | | | | | | | | |
| Major/Minor | | | | Major2 | | | | | N | Minor2 | | |
| Conflicting Flow All | | | | 251 | 0 | 0 | | | | - | 656 | 203 |
| Stage 1 | | | | - | - | - | | | | - | 405 | |
| Stage 2 | | | | - | _ | - | | | | - | 251 | - |
| Critical Hdwy | | | | 4.16 | - | - | | | | - | 6.56 | 6.96 |
| Critical Hdwy Stg 1 | | | | - | - | - | | | | - | 5.56 | - |
| Critical Hdwy Stg 2 | | | | - | - | - | | | | - | - | - |
| Follow-up Hdwy | | | | 2.23 | - | - | | | | - | 4.03 | 3.33 |
| Pot Cap-1 Maneuver | | | | 1304 | - | 0 | | | | 0 | 382 | 801 |
| Stage 1 | | | | - | - | 0 | | | | 0 | 594 | - |
| Stage 2 | | | | - | - | 0 | | | | 0 | - | - |
| Platoon blocked, % | | | | | - | | | | | | | |
| Mov Cap-1 Maneuver | | | | 1304 | - | - | | | | - | 0 | 801 |
| Mov Cap-2 Maneuver | | | | - | - | - | | | | - | 0 | - |
| Stage 1 | | | | - | - | - | | | | - | 0 | - |
| Stage 2 | | | | - | - | - | | | | - | 0 | - |
| | | | | | | | | | | | | |
| Approach | | | | WB | | | | | | SB | | |
| HCM Control Delay, s | | | | 0 | | | | | | 10 | | |
| HCM LOS | | | | | | | | | | В | | |
| | | | | | | | | | | | | |
| Minor Lane/Major Mvm | t | WBL | WBT | SBLn1 | SBLn2 | | | | | | | |
| Capacity (veh/h) | | 1304 | - | - | 801 | | | | | | | |
| HCM Lane V/C Ratio | | - | - | - | 0.097 | | | | | | | |
| HCM Control Delay (s) | | 0 | - | 0 | 10 | | | | | | | |
| HCM Lane LOS | | A | - | A | В | | | | | | | |
| HCM 95th %tile Q(veh) | | 0 | - | - | 0.3 | | | | | | | |
| | | | | | | | | | | | | |

| Intersection | | | | | | |
|--------------------------|----------|-------|----------|----------|---------|------|
| Int Delay, s/veh | 0.2 | | | | | |
| | | EDD | WDI | WDT | NDI | NDD |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | † | - 1 | \ | ^ | | 7 |
| Traffic Vol, veh/h | 1444 | 54 | 33 | 970 | 0 | 0 |
| Future Vol, veh/h | 1444 | 54 | 33 | 970 | 0 | 0 |
| Conflicting Peds, #/hr | _ 0 | 100 | 100 | _ 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | 25 | - | - | 0 |
| Veh in Median Storage | e, # 0 | - | - | 0 | 0 | - |
| Grade, % | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 96 | 96 | 96 | 96 | 96 | 96 |
| Heavy Vehicles, % | 3 | 3 | 3 | 3 | 3 | 3 |
| Mvmt Flow | 1504 | 56 | 34 | 1010 | 0 | 0 |
| | | | | | | |
| | | - | | - | | |
| | Major1 | | Major2 | | /linor1 | |
| Conflicting Flow All | 0 | 0 | 1660 | 0 | - | 880 |
| Stage 1 | - | - | - | - | - | - |
| Stage 2 | - | - | - | - | - | - |
| Critical Hdwy | - | - | 4.16 | - | - | 6.96 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - |
| Critical Hdwy Stg 2 | - | _ | - | - | - | - |
| Follow-up Hdwy | _ | - | 2.23 | - | - | 3.33 |
| Pot Cap-1 Maneuver | _ | _ | 380 | _ | 0 | 288 |
| Stage 1 | _ | _ | - | _ | 0 | - |
| Stage 2 | _ | _ | _ | _ | 0 | _ |
| Platoon blocked, % | _ | _ | | _ | V | |
| Mov Cap-1 Maneuver | _ | | 344 | | _ | 261 |
| Mov Cap-1 Maneuver | <u> </u> | _ | J44 - | _ | _ | 201 |
| | - | - | - | - | - | - |
| Stage 1 | - | - | _ | - | - | - |
| Stage 2 | - | - | - | - | - | - |
| | | | | | | |
| Approach | EB | | WB | | NB | |
| HCM Control Delay, s | 0 | | 0.5 | | 0 | |
| HCM LOS | | | 3.0 | | A | |
| 1 JOHN LOO | | | | | | |
| | | | | | | |
| Minor Lane/Major Mvm | nt l | NBLn1 | EBT | EBR | WBL | WBT |
| Capacity (veh/h) | | - | _ | - | 344 | - |
| HCM Lane V/C Ratio | | - | - | - | 0.1 | - |
| HCM Control Delay (s) | | 0 | - | - | | - |
| HCM Lane LOS | | A | - | _ | С | - |
| HCM 95th %tile Q(veh |) | - | _ | - | 0.3 | - |
| TION JOHN JOHN WINE WINE | , | | | | 0.0 | |

Appendix C: Detailed Project Trip Generation

APPENDIX C CHEVAL BLANC HOTEL, CLUB & MIXED USE PROJECT PROPOSED PROJECT TRIP GENERATION ESTIMATES

| | | | | | Trip (| Senerati | on Estin | nates | | | | | | | | | | | |
|---------------------------|------|-----------------------|-----------|----------|---------|-----------|----------|----------|----------|--|---------|--------|---------|---------|---------|--------------|-------|--|--|
| | | | | | Tr | ip Genei | ation Ra | ites [a] | | | | Estima | ated Ti | rip Geı | neratio | n | | | |
| 1411 | ITE# | C : | Daily | AM | Peak F | lour | PN | 1 Peak H | lour | Trip Rate | Weekday | AM | Peak | Hour | PM | PM Peak Hour | | | |
| Land Use | ITE# | Size | Rate | Rate | % In | % Out | Rate | % In | % Out | Unit | Daily | ln | Out | Total | In | Out | Total | | |
| | | | | | | | | | | | | | | | | | | | |
| Proposed Project | | | | | | | | | | | | | | | | | | | |
| Hotel | 310 | 115 rooms | 8.36 | 0.47 | 59% | 41% | 0.60 | 51% | 49% | per room | 961 | 32 | 22 | 54 | 35 | 34 | 69 | | |
| TNC [e] | | | | | | | | | | | 640 | 21 | 15 | 36 | 23 | 23 | 46 | | |
| Employee | | | | | | | | | | | 125 | 4 | 3 | 7 | 5 | 4 | 9 | | |
| Valet | | | | | | | | | | | 196 | 7 | 4 | 11 | 7 | 7 | 14 | | |
| Total check | | | | | | | | | | | 961 | 32 | 22 | 54 | 35 | 34 | 69 | | |
| Private Membership Club | [c] | 500 members | 0.36 | 0.04 | 80% | 20% | 0.08 | 80% | 20% | member | 180 | 16 | 4 | 20 | 32 | 8 | 40 | | |
| TNC [e] | | | | | | | | | | | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | |
| Employee | | | | | | | | | | | 23 | 2 | 1 | 3 | 4 | 1 | 5 | | |
| Valet | | | | | | | | | | | 157 | 14 | 3 | 17 | 28 | 7 | 35 | | |
| Total check | | | | | | | | | | | 180 | 16 | 4 | 20 | 32 | 8 | 40 | | |
| Quality Restaurant | 931 | 25.094 ksf | 83.84 | 0.73 | 50% | 50% | 7.8 | 67% | 33% | per ksf | 2,104 | 9 | 9 | 18 | 131 | 65 | 196 | | |
| Less Internal Capture [b] | | | 20% | 20% | 20% | 20% | 0% | 20% | 20% | | (421) | (2) | (2) | (4) | (26) | (13) | (39) | | |
| New Trips | | | | | | | | | | | 1,683 | 7 | 7 | 14 | 105 | 52 | 157 | | |
| TNC [e] | | | | | | | | | | | 842 | 4 | 4 | 8 | 52 | 26 | 78 | | |
| Employee | | | | | | | | | | | 252 | 1 | 1 | 2 | 16 | 8 | 24 | | |
| Valet | | | | | | | | | | | 589 | 2 | 2 | 4 | 37 | 18 | 55 | | |
| Total check | | | | | | | | | | | 1,683 | 7 | 7 | 14 | 105 | 52 | 157 | | |
| Retail | 820 | 24.976 ksf | 37.75 | 0.94 | 62% | 38% | 3.81 | 48% | 52% | per ksf | 943 | 14 | 9 | 23 | 46 | 49 | 95 | | |
| Less Internal Capture [b] | | | 20% | 20% | 20% | 20% | 20% | 20% | 20% | | (189) | (3) | (2) | (5) | (9) | (10) | (19) | | |
| Less Pass-By | | | 30% | 30% | 30% | 30% | 30% | 30% | 30% | | (226) | (3) | (2) | (5) | (11) | (12) | (23) | | |
| New Trips | | | | | | | | | | | 528 | 8 | 5 | 13 | 26 | 27 | 53 | | |
| TNC [e] | | | | | | | | | | | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | |
| Employee | | | | | | | | | | | 100 | 2 | 1 | 2 | 5 | 5 | 10 | | |
| Valet | | | | | | | | | | | 428 | 6 | 4 | 11 | 21 | 22 | 43 | | |
| Total check | | | | | | | | | | | 528 | 8 | 5 | 13 | 26 | 27 | 53 | | |
| Day Spa [d] | 918 | 12.936 ksf | 14.50 | 1.21 | 50% | 50% | 1.45 | 17% | 83% | per ksf | 188 | 8 | 8 | 16 | 3 | 16 | 19 | | |
| Less Internal Capture [b] | | | 20% | 20% | 20% | 20% | 0% | 20% | 20% | | (37) | (1) | (2) | (3) | (1) | (3) | (4) | | |
| New Trips | | | | | | | | | | | 151 | 7 | 6 | 13 | 2 | 13 | 15 | | |
| TNC [e] | | | | | | | | | | | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | |
| Employee | | | | | | | | | | | 20 | 1 | 1 | 2 | 0 | 2 | 2 | | |
| Valet | | | | | | | | | | | 131 | 6 | 5 | 11 | 2 | 11 | 13 | | |
| Total check | | | | | | | | | | | 151 | 7 | 6 | 13 | 2 | 13 | 15 | | |
| | 1 | TOTAL ESTIMATED | PROJEC | T TRIPS | (NEW | TRIPS) | | <u> </u> | <u> </u> | <u> </u> | 3,503 | 70 | 44 | 114 | 200 | 134 | 334 | | |
| | T | OTAL ESTIMATED P | ROJECT T | RIPS (EN | /PLOYI | EE TRIPS) | | | | | 521 | 10 | 6 | 16 | 30 | 20 | 50 | | |
| | | TOTAL ESTIMAT | TED PROJ | ECT TRIF | PS (VAL | ET) | | | | | 1,501 | 35 | 19 | 54 | 95 | 65 | 160 | | |
| | TOTA | L ESTIMATED PROJI | ECT TRIPS | S (UNAD | JUSTE | TNC TF | RIPS) | | | | 1,482 | 25 | 19 | 44 | 75 | 49 | 124 | | |
| | TOT | AL ESTIMATED PRO | | | JSTED | TNC TRII | PS) | | | | 1,482 | 25 | 25 | 50 | 75 | 75 | 150 | | |
| | | | VE USES | | | | | | | | -1,142 | -18 | -10 | -28 | -55 | -60 | -115 | | |
| | | TOTAL ADJ | USTED P | ROJECT | TRIPS | 1 | | | | | 2,361 | 52 | 40 | 92 | 145 | 100 | 245 | | |

Notes:

- $\hbox{\small [a] Source: ITE Trip Generation Manual, 10th Edition, 2017, except where noted.}\\$
- [b] Internal capture represents the percentage of trips between land uses that occur within the site without requiring a vehicle trip. Internal capture rates are derived from "Parking Demand Analysis Study Cheval Blanc Hotel in the City of Beverly Hills, CA", Kimley Horn (2020).
- [c] Private membeship member trip rates derived from "Parking Demand Analysis Study Cheval Blanc Hotel in the City of Beverly Hills, CA", Kimley Horn (2020).
- [d] No daily trip rate is provided by ITE for Land Use 918 Hair Salon. Daily rate assumes that the PM peak hour trip rate is equal to 10% of the daily trip rate.
- [e] The proliferation of shared mobility transportation network companies (TNCs), such as Lyft and Uber, in recent years is important to consider in a project of this type and size. Pick-up and drop-off trips, such as those utilizing TNC services, do not utilize site parking and result in an additional trip generated compared to patrons who drive themselves and park their own cars at the site. In order to account for TNCs, it was assumed that TNCs would account for 50% of the vehicle trips generated by the restaurant, and 66.6% of the vehicle trips generated by the hotel, based on observed drive ratios provided in the Parking Demand Analysis Study technical memorandum (July 16, 2020). Where inbound and outbound trips were unequal, the higher of the two calculations was assumed for both directions to account for TNCs that drop off a patron and leave the project site without



Parking Demand Analysis Study

Page 1

TECHNICAL MEMORANDUM

| Gruen Associates |
|------------------|
| (|

From: Matt Stewart, P.E.

Kimley-Horn and Associates, Inc.

Date: January 6, 2022

Subject: Parking Demand Analysis Study - Cheval Blanc Hotel in the City of Beverly Hills, CA

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Appendix B – City Code Shared Parking Time-Of-Day Parking Demand

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Appendix F – ULI Shared Parking Time-Of-Day Parking Demand

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I. INTRODUCTION

Kimley-Horn and Associates, Inc. ("Kimley-Horn") was contracted by Gruen Associates to prepare a parking demand analysis for the Cheval Blanc Hotel located at 468 North Rodeo Drive, Beverly Hills, CA.

The proposed project includes a 115-room hotel, three retail spaces totaling 24,976 SF, four indoor restaurant spaces totaling 20,334 SF¹, two outdoor restaurant spaces totaling 4,760 SF², and an 8,198 SF member's club. Additional appurtenant uses that are considered to be part of the hotel include the hotel lobbies, a spa, a fitness center, a pool, a central kitchen, employee facilities, and hallways.

Projected parking demand for the project was calculated using the following two methodologies:

- City Code Parking Requirement Number of parking spaces required by the Beverly Hills
 City Code. The number of spaces required is calculated with no parking credits, with parking
 credits allowed by the City Code, and with time-of-day demand as recommended by Urban
 Land Institute's Shared Parking, 3rd Edition.
- 2. **Urban Land Institute Shared Parking Demand** An analysis of the number of spaces required by the project overall, accounting for a single shared parking supply that would accommodate all portions of the project and their unique time-of-day parking demands.

II. PARKING REQUIRED BY CITY CODE

The number of parking spaces required for the proposed elements of the Cheval Blanc Hotel project was calculated by referencing the Beverly Hills City Code. Section 10-3-2730 describes parking requirements for all developments in Beverly Hills while Section 10-3-2866 describe parking requirements for developments that include hotels. The Code sections below apply to portions of the Cheval Blanc Hotel project:

- 10-3-2730B
 - "The aggregate amount of required parking space for each type of use shall not be less than the following:"
 - "1. Hotels 1 space per rentable room or unit"3
 - "8. Open air dining on private property Parking shall be provided as required for indoor dining pursuant to this section except that the planning commission may establish parking requirements for open air dining areas that are different than those set forth in this section if the planning commission determines that the open air dining area will generate a need for parking different than the amount of parking required by this section or the planning commission determines that parking demand will be met by means other than those means specified in this section"

_

¹ Four indoor restaurant spaces are comprised of: GF (5,666 SF), L2 (2,419 SF), L6 (6,716 SF), and L7 (5,533 SF).

² Two outdoor restaurant spaces are comprised of: L6 (2,500 SF) and L7 (2,260 SF).

³ Hotel appurtenant uses such as lobbies, wellness (fitness center), spa, swimming pool and deck, central kitchen, employment facilities, office, corridors, and back of house are included in the hotel room ratio.



- "9. Eating and bar facilities not governed by subsections B5 through B7 of this section 1 space per 45 square feet of dining and bar floor area for the first 9,000 square feet of such area and 1 space per 65 square feet of dining and bar floor area in excess of 9,000 square feet. However, 25 percent of the spaces required to be provided for a building or structure by subsections B1 and B10 of this section may also be applied toward the requirements of this subsection"
 - Note that per Ordinance 19-O-2296, parking for larger restaurants and bars has been reduced to the same as for smaller restaurants (1 space per 350 square feet)
- "10. Commercial uses not otherwise specified in this section 1 space per 350 square feet of floor area"
- 10-3-2866A
 - "On-site parking space for hotel guestrooms as required by subsection 10-3-2730B1 of this chapter;"
- 10-3-2866B
 - "On-site parking for hotel restaurant and bar uses that are open to the public shall be provided as required by subsection 10-3-2730B9 of this chapter, except that the twenty five percent (25%) credit for parking set forth in that subsection shall not apply to a hotel restaurant or bar that is open to the public"

The City Code does not define a parking requirement for a member's club. To calculate the required parking for the member's club, the restaurant ratio was used for all member's club floor area, including back of house. **Table 1** below shows the parking requirement for the project with base parking requirement ratios.

| fode Parking Required (without parking credits |
|--|
| ode Parking Required (without parking credits |

| Use | Unit | Ratio | Spaces Required (City Code) |
|-----------------------------------|-----------|-----------------------------|-----------------------------|
| Hotel | 115 rooms | 1 space / rentable room | 115.0 |
| Hotel Restaurant/Bar ¹ | 16,928 SF | 1 space / 350 SF floor area | 48.4 |
| Restaurant/Bar ² | 8,166 SF | 1 space / 350 SF floor area | 23.3 |
| Retail | 24,976 SF | 1 space / 350 SF floor area | 71.4 |
| Member's Club | 8,198 SF | 1 space / 350 SF floor area | 23.4 |
| Total | | | 281.5 |

¹ - Hotel restaurant/Bar Includes 14,668 SF of restaurant/bar on 2nd, 6th, and 7th floors and 2,260 SF of private outdoor dining on L7. Compared to the Ground Floor restaurant, the 2nd Floor restaurant may be used more for hotel guests.

As shown in **Table 2**, the maximum number of parking spaces for the project required by City Code is 282.

² - Restaurant/Bar includes 5,666 SF of restaurant/bar on Ground Floor and 2,500 SF of private outdoor dining on L6.



Parking Credits

The Beverly Hills City Code includes the following credits that may be applied to parking requirements:

Retail and Hotel Combination

Section 10-3-2866 of the Beverly Hills City Code notes that a portion of the parking furnished for the hotel use may be credited to the parking required for the retail use:

10-3-2866D

- "On-site parking for retail and other commercial uses as required by section 10-3-2730 of this chapter; provided, further:
 - Fifty percent (50%) of the parking furnished under subsection A (hotel rooms at 1 space/rentable room) of this section may be credited to the parking requirements under this subsection;
 - The parking requirements specified in this article include parking for any floor area used as an integral part of the designated use, and subsection 10-3-2730B10 of this chapter shall not be applicable to such areas;"

The number of parking spaces required for retail (71.4) would be reduced by half of the number of spaces required for the hotel (115). The retail parking requirement is credited by 57.5 spaces. Therefore, a total of total of 13.9 parking spaces are required for the retail use.

Proximity to Transit and Shopping

Section 10-3-2866 of the Beverly Hills City Code notes that the number of parking spaces required may be reduced due to proximity to transit and a concentration of shopping around the site:

10-3-28661

"The number of parking spaces required by this section may be reduced by not more than fifteen percent (15%) where a finding is made in approval of the conditional use permit that; because of the location of the hotel; availability of public transportation; or proximity and concentration of shopping to the hotel site, the hotel use will not generate a need for the number of parking spaces designated by this section. The provisions of section 10-3-2730 of this chapter relative to the joint use of parking facilities where one use is primarily a daytime use and the other use is primarily a nighttime use shall not be applicable to the parking required by this article. (Ord. 84-O-1937, eff. 11-1-1984; amd. Ord. 87-0-2005, eff. 10-15-1987; Ord. 96-0-2256, eff. 4-5-1996; Ord. 98-O-2304, eff. 8-7-1998; Ord. 98-O-2306, eff. 9-11-1998)"

The Cheval Blanc Hotel will be located in an area with significant availability of public transportation. Existing and future transit lines are noted below:

- Metro Rapid 704 (15-minute weekday headways and stops along Santa Monica Boulevard 600-800' from hotel)
- Metro Lines 4, 14, 16, and 316
- Metro D Line (Heavy Rail Line with station less than half mile from hotel. Under construction and to be complete prior to hotel opening)



Furthermore, the hotel will be located in an area with a significant concentration of shopping. The Beverly Hills Business Triangle has a significant number of internally captured trips. A 15% proximity to transit credit is applied to the hotel, hotel restaurant/bar, restaurant/bar, and retail land uses.

Table 2 shows the number of parking spaces required for the project with the parking credits included.

Table 2 – City Code Parking Required (with parking credits)

| Use | Unit | Ratio | Spaces Required (City Code) |
|-----------------------------------|------------------------|-------------------------|-----------------------------|
| Hotel | 115 rooms | 1 space / rentable room | 115.0 |
| Hotel Restaurant/Bar ¹ | 16,928 SF | 1 space / 350 SF | 48.4 |
| Restaurant/Bar ² | 8,166 SF | 1 space / 350 SF | 23.3 |
| Retail | 24,976 SF | 1 space / 350 SF | 71.4 |
| Member's Club | 8,198 SF | 1 space / 350 SF | 23.4 |
| Subtotal | | | 281.5 |
| Retail/Hotel Credit (50% or | f required hotel space | es) | -57.5 |
| Proximity to Transit Credit | (15%) ³ | | -30.1 |
| Subtotal of Parking Cred | its | | -97.6 |
| Total | | | 193.9 |

¹ - Hotel restaurant/Bar Includes 14,668 SF of restaurant/bar on 2nd, 6th, and 7th floors and 2,260 SF of private outdoor dining on L7. Compared to the Ground Floor restaurant, the 2nd Floor restaurant may be used more for hotel guests.

As shown in **Table 2**, the maximum parking required by the City code if all parts of the Cheval Blanc experienced peak demand concurrently would be 194 parking spaces.

Provisions for Hotel Employees

The Beverly Hills City Code specifies that a portion of required parking spaces must be reserved for hotel employees:

10-3-2866E

- "One-third (1/3) of the parking spaces required by subsection A of this section shall be used exclusively for hotel employee parking, and such spaces shall be subject to the following provisions:
 - Such parking shall be furnished without charge to the employees;

Therefore, one third of the 115 parking spaces required for the hotel, or 39 parking spaces total, would be required to be reserved for hotel employees. An estimate of the number of hotel and hotel restaurant parking spaces that would be used by visitors and employees is included in **Table 3**. The ratios for visitors to employees were developed by referencing the Urban Land Institute's *Shared Parking*, 3rd Edition. *Shared Parking* notes the following relative demands:

 Hotel (Leisure) – 1 visitor parking space for every 0.15 employee parking spaces (weekday and weekend)

² - Restaurant/Bar includes 5,666 SF of restaurant/bar on Ground Floor and 2,500 SF of private outdoor dining on L6.

³ – Transit credit applied to hotel, hotel restaurant/bar, restaurant/bar, and retail land uses.



- Hotel Restaurant 6.67 visitor parking spaces for every 1 employee parking space (weekday)
- Hotel Restaurant 7.67 visitor parking spaces for every 1.33 employee parking spaces (weekend)

Shared Parking

The Cheval Blanc Hotel project contains a mixture of uses that would be expected to generate peak parking demands at different times of the day. The proposed project parking garage will contain 39 reserved parking spaces for hotel employees, but the remaining parking spaces would be shared among the hotel guests, restaurant guests and employees, retail guests and employees, and Club members.

A Shared Parking Analysis was conducted by using the time-of-day demand rates listed in Urban Land Institute's *Shared Parking*, 3rd Edition, on the Beverly Hills City Code parking requirements.

Shared Parking provides hourly demand percentages for visitors and employees for the project land uses. The weekday and weekend hourly demand percentages are included in **Appendix A**. The following land uses were used for the time-of-day analysis.

- Retail (over 2,000 SF) Visitor and Employee
- Restaurant (Fine/Casual Dining) Visitor and Employee
- Hotel (Leisure) Visitor and Employee
- Hotel Restaurant Visitor and Employee

Shared Parking does not provide hourly parking demand data for member's clubs. For this analysis, the time-of-day parking demand for the member's Club was estimated based on data provided by Cheval Blanc.

Hourly parking demand was calculated for the project for typical weekday and weekend days using the ULI time-of-day parking demand rates. The time-of-day analysis shows that the peak parking demand would occur on weekend days and weekdays at 8 PM. A secondary peak would occur at 12 PM on weekend days and weekdays. The time-of-day parking demand for weekdays and weekends is included in **Appendix B**. **Table 3** on the following page shows the peak parking demand at peak daytime (6 AM to 6 PM) and evening (6 PM to 12 AM) weekday and weekend periods.



Table 3 – City Code Parking Required (with parking credits and shared parking)

| Use | Unit | Spaces Required | | eekday nand | 7.7 | eekend nand |
|---------------------------------|--------------|------------------------|--------------------|-------------------|--------------------|-------------------|
| use | Unit | (with credits applied) | Daytime (12 PM) | Evening (8 PM) | Daytime (12 PM) | Evening (8 PM) |
| Hotel | 115 | 97.8 | | | | |
| Visitor ³ | 115 rooms | 85.0 | 55.3 | 76.5 | 55.3 | 76.5 |
| Employee ³ | 1001118 | 12.8 | 12.8 | 2.6 | 12.8 | 2.6 |
| Hotel Restaurant/Bar1 | | 41.1 | | | | |
| Visitor ⁴ | 16,928 SF | 34.8 | 34.8 | 24.4 | 35.0 | 24.5 |
| Employee ⁴ | J JF | 6.3 | 6.3 | 2.5 | 6.1 | 6.1 |
| Restaurant/Bar ² | | 19.8 | | | | |
| Visitor | 8,166 SF | 17.0 | 12.7 | 17.0 | 8.5 | 17.0 |
| Employee | 1 | 2.9 | 2.6 | 2.9 | 2.1 | 2.8 |
| Retail | 04.070 | 11.8 | | | | |
| Visitor | 24,976 SF | 9.5 | 9.5 | 6.2 | 9.0 | 6.1 |
| Employee | 01 | 2.3 | 2.3 | 2.1 | 2.4 | 1.8 |
| Member's Club | 8,198 SF | 23.4 | 7.0 | 21.1 | 7.0 | 21.1 |
| Unreserved Parking Space | es | | | | | |
| Unreserved Supply | | 146.0 | 146.0 | 185.0 | 146.0 | 185.0 |
| Unreserved Demand | | 174.9 | 124.2 | 155.1 | 119.2 | 158.5 |
| Reserved Parking Spaces | | | | | | |
| Reserved Supply | | 39.0 | 39.0 | - | 39.0 | - |
| Reserved Demand | | 19.0 | 19.0 | - | 18.8 | - |
| Total Parking Spaces | | | | | | |
| Total Supply | | 185.0 | 185.0 | 185.0 | 185.0 | 185.0 |
| Total Demand | | 193.9 | 143.2 | 155.1 | 138.1 | 158.5 |

¹ - Hotel restaurant/Bar Includes 14,668 SF of restaurant/bar on 2nd, 6th, and 7th floors and 2,260 SF of private outdoor dining on L7. Compared to the Ground Floor restaurant, the 2nd Floor restaurant may be used more for hotel guests.

Table 3 shows that from 6 AM to 6 PM on weekdays and weekends, the peak demand for reserved and unreserved spaces would be accommodated by the proposed supply of parking spaces (39 reserved spaces and 146 unreserved spaces). The peak parking demand during the weekday before 6 PM is 19.0 for the reserved hotel employee parking spaces and 124.2 for all other unreserved parking spaces. The peak parking demand during the weekend before 6 PM is 18.8 for the reserved hotel employee parking spaces and 119.2 for all other unreserved parking spaces.

The ULI Shared Parking model shows that parking demand for hotel employees typically decreases after 6 PM. The time-of-day model shows that employees would be expected to use a maximum of 8.6 of the 39 reserved parking spaces after 6 PM on weekdays and weekends. Therefore, it is recommended that a portion of the 39 reserved parking spaces be opened to other users after 6 PM.

² - Restaurant/Bar includes 5,666 SF of restaurant/bar on Ground Floor and 2,500 SF of private outdoor dining on L6

³ - Per ULI rates, the average hotel parking demand rate is 87% visitors and 13% employees

⁴ - Per ULI rates, the average hotel restaurant parking demand rate is 85% visitors and 15% employees



This analysis shows that the proposed supply of 185 parking spaces will meet the projected peak demand for the project.

III. PARKING DEMAND ANALYSIS

The second method for calculating parking demand for the Cheval Blanc focuses entirely on the shared parking principles described in *Shared Parking*. *Shared Parking* provides base parking demand rates for a variety of land uses. The manual provides guidance for adjusting the drive ratio and capture rates for each land use, along with time-of-day distributions.

Base Parking Demand Rates

Base parking demand rates are provided by *Shared Parking*. The base parking demand rates are generated based on surveys of stand-alone sites where nearly 100% of visitors and employees drive to the site. Base parking demand rates for the following components of the Cheval Blanc are supplied by *Shared Parking*:

- Hotel
 - Weekday 1 (visitor) and 0.15 (employee)
 - Weekend 1 (visitor) and 0.15 (employee)
- Hotel Restaurant
 - Weekday 6.67 (visitor) and 1.2 (employee)
 - Weekend 7.67 (visitor) and 1.33 (employee)
- Restaurant
 - Weekday 13.25 (visitor) and 2.25 (employee)
 - Weekend 15.25 (visitor) and 2.50 (employee)
- Retail (over 2,000 ksf)
 - Weekday 2.9 (visitor) and 0.7 (employee)
 - Weekend 3.2 (visitor) and 0.8 (employee)

Drive Ratio Adjustment

Shared Parking notes that the drive ratio should be determined based on a survey of local conditions. The following drive rates are estimated for each portion of the Cheval Blanc:

- Hotel-Leisure 33.4%
 - Based off a study of drive rates for luxury hotels in Beverly Hills between 2017 and 2019. Data included in **Appendix C.**
- Hotel Restaurant 47% (weekday) and 40% (weekend)
 - ULI Shared Parking recommend drive rates of 47% on weekdays and 40% on weekends for hotel restaurants in downtown locations with paid and/or valet parking.
- Restaurant 50%
 - Drive-rate of 29.7% observed between 2017 and 2019 at three luxury stand-alone restaurants with no self-parking option in Beverly Hills and similar communities. To be conservative, the drive-rate was increased from 29.7% to 50% to account for potential that some visitors may self-park at off-site parking facilities. However, research shows that a negligible number of visitors to luxury restaurants self-park off-site. Data included in Appendix D.
- Retail 75%



Drive-rate of 84.1% for retail uses observed in 2016 at the Beverly Hills Cartier store⁴. Data was collected on Saturday, May 16, Tuesday, May 17, and Saturday, May 21. The Cartier store is similar to the types of retail stores that will be included with the Project. The drive-rate for the Project is estimated to be marginally more than 10% lower than the drive-rate observed in 2016 due to the increase in rideshare popularity and the increase in high quality transit near the Project site that has been built and will continue to be built prior to the Project opening. A drive-rate of 75% is proposed for the Project.

• **Employees** – 50%

Orive-in rate for employees was estimated based on American Community Survey (ACS) data. The ACS data shows that 70% of service employees in Beverly Hills drive alone to work. Due to the project's location near two high-density transit corridors (Santa Monica Boulevard and Wilshire Boulevard), it is likely that the drive rate for service employees for jobs near the Cheval Blanc would be lower than 70%. The Cheval Blanc will provide transit passes for all employees. Provision of transit passes to employees has been shown to reduce vehicle miles traveled (VMT) by employees by up to 20% (Source: Los Angeles Department of Transportation Vehicle Miles Traveled Calculator). The reduction of VMT is assumed to match a similar reduction in parking space demand. Therefore, the assumed drive-in rate for employees is 50%.

Captive Ratio Adjustments

For mixed-use developments, a portion of the trips generated by one land use would be "captured" by other land uses that are also part of the development. For Cheval Blanc, internal capture of trips is expected to occur between the hotel and the restaurant and retail. No additional parking demand would be generated by internal trips between the hotel and restaurant and retail land uses. A 20% captive rate is assumed for restaurant and retail. The 20% captive ratio is justified by the ITE internal capture estimator tool. ITE Internal Capture worksheets are included in **Appendix E**.

Member's Club

Parking demand for the member's Club was estimated using two scenarios – A) using data from Cheval Blanc about how the Club is expected to be utilized; and B) using data from a similar membership club approved by the City of West Hollywood.

Scenario A

Parking demand for the membership club was estimated in consultation with Cheval Blanc about how the Club is expected to operate. The Member's Club consists of three areas on the 3rd Floor that will be dedicated for exclusive member's use (the Club Lounge, Club Meeting Room, and Club Screening Room). Member's will also have access to parts of the Cheval Blanc that are shared with hotel guests, including the Wellness Center and restaurants on the 6th and 7th floors. Per Cheval Blanc, the Member's Club will be limited to a maximum of 500 individual Club memberships. A parking demand rate of 0.06 parking spaces per member was developed based on forecast operations provided by Cheval Blanc. Parking demand for the Member's Club for uses that are analyzed separately (like the 6th and 7th floor

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⁴ 370 North Rodeo Drive Project Trip Generation Analysis, RK Engineering Group, July 23, 2018



restaurants) are assumed to be in addition to the typical parking demand for those uses, in order to be conservative. Furthermore, a drive-rate of 100% and average vehicle occupancy of 1 person per vehicle are assumed as a conservative analysis.

Scenario B

To verify projected Club parking demands, parking demand for a similar proposed membership club in West Hollywood was reviewed. The Arts Club West Hollywood Project was approved by the City of West Hollywood in 2018. It includes restaurants, lounges, private dining, guestrooms, a fitness/spa, and an outdoor pool and deck. A transportation study for the West Hollywood Arts Club was prepared in September 2017. The study relied on parking demand data gathered at an existing Arts Club site in London. The parking demand rate for the Arts Club West Hollywood employees was increased based on local parking demand in the West Hollywood area. The study forecast the following parking demand rates:

- Member demand: 0.019 spaces per member (weekday)
- Member demand: 0.032 spaces per member (weekend)
- Employee Demand: 0.023 spaces per member (weekday and weekend)

The parking demand for Cheval Blanc Club is anticipated to be similar to the West Hollywood Arts Club because they contain similar uses. Although the Cheval Blanc Club proposes to use hotel employees as staff for the Club, using the Arts Club parking demand rate calculates demand for members, their guests and employees based on the Arts Club and is thus a conservative estimate of Club parking demand.

Time of Day Shared Parking

Shared Parking principles indicate that the various portions of the Cheval Blanc would experience peak parking demand at different times of day. In general, retail tends to experience peak parking demands earlier in the day, while restaurant and hotel tends to experience peak parking demand later in the day. Based on the shared time-of-day distribution of parking demand, the peak demand is projected to be between 184 (Scenario A) and 185 (Scenario B) vehicles, depending on which parking demand rate and time-of-day distribution is used to estimate the parking demand for the private membership Club. The parking demand for the Cheval Blanc for all times of day for Scenarios A and B is shown in Appendix F.

The Cheval Blanc proposes to include 185 parking spaces. Based on the forecast peak parking demand, the projected demand would be accommodated by the proposed supply.



IV. PARKING DEMAND FOR EVENTS

The Cheval Blanc proposes to hold events that would generate different parking demands compared to typical conditions. Three types of events are analyzed in this parking demand analysis.

Event Type A

The Cheval Blanc will hold events in the 6th and/or 7th floor restaurants up to 6 times per year. These events would be open exclusively to Club members, hotel patrons and their respective guests, with total attendance capped at 150. During these events, the 6th and/or 7th floor restaurant would not be available for normal use and would therefore not generate its typical parking demand.

Event Type B

 The Cheval Blanc will hold events in the Penthouse up to 6 times per year with attendance capped at 75. During these events, all other parts of the Cheval Blanc would be available for typical use.

Event Type C

The Cheval Blanc will hold weekly events for Club members and their guests in the 3rd floor Club Lounge and Screening Room, with attendance capped at 50.

Event Parking Demand

Cheval Blanc event parking demand was calculated for a scenario where Event Types A, B, and C are held concurrently. In this scenario, the 6th and 7th floor indoor and outdoor restaurant spaces would not be open to non-event attendees and would not generate additional parking demand. Similarly, the 3rd Floor members Club spaces would not be open to members not attending the special event.

For event parking demand, a drive-in rate of 100% and an average vehicle occupancy (AVO) of 2 people per car is assumed. Data from National Household Travel Survey and Federal Highway Administration (FHWA) *Managing Travel for Planned Special Events* show that AVO for events typically range from 2.1 to 3.1.

To be conservative, event parking demand is analyzed for an event occurring when parking demand for other parts of the Cheval Blanc are at a peak. Event parking demand is analyzed with a consistent parking demand throughout the day. The parking demand for event attendees would be 138 vehicles (75 for Event Type A, 38 for Event Type B, and 25 for Event Type C).

Peak parking demand is projected to occur at 1 PM on weekdays and at 1 PM on weekend days. The peak parking demand would be 252 parking spaces. Parking demand for the Cheval Blanc during events is shown in **Appendix G**.

To accommodate the additional parking demand which may occur during events, the Cheval Blanc would implement a valet service plan. The Valet Service Plan Memorandum shows that the Cheval Blanc could accommodate up to 252 parking spaces. Therefore, the projected parking demand during events could be accommodated by on-site parking.



Appendix A – Shared Parking Time-Of-Day Parking Demand Percentages

| | | W | eel | kda | y - T | ime | -of- | Day | Pa | rkin | g D | ema | and | | | | | | | |
|---------------------------------|-----------|---------|---------|---------|---------|----------|----------|----------|---------|---------|---------|---------|---------|---------|---------|---------|---------|----------|----------|----------|
| Land Use | Туре | 6:00 AM | 7:00 AM | 8:00 AM | 9:00 AM | 10:00 AM | 11:00 AM | 12:00 PM | 1:00 PM | 2:00 PM | 3:00 PM | 4:00 PM | 5:00 PM | 6:00 PM | 7:00 PM | 8:00 PM | 9:00 PM | 10:00 PM | 11:00 PM | 12:00 AM |
| Hotel - Leisure | Visitors | 95% | 95% | 90% | 80% | 70% | 70% | 65% | 65% | 70% | 70% | 75% | 80% | 85% | 85% | 90% | 95% | 95% | 100% | 100% |
| | Employees | 10% | 30% | 100% | 100% | 100% | 100% | 100% | 100% | 100% | 100% | 70% | 70% | 40% | 20% | 20% | 20% | 20% | 10% | 5% |
| Hotel Restaurant ¹ | Visitor | 0% | 10% | 30% | 10% | 10% | 5% | 100% | 100% | 33% | 10% | 10% | 30% | 55% | 60% | 70% | 67% | 60% | 40% | 30% |
| | Employee | 10% | 10% | 60% | 100% | 100% | 100% | 100% | 100% | 100% | 100% | 100% | 100% | 60% | 40% | 40% | 20% | 0% | 0% | 0% |
| Fine/Casual Dining ² | Visitors | 0% | 0% | 0% | 0% | 15% | 40% | 75% | 75% | 65% | 40% | 50% | 75% | 95% | 100% | 100% | 100% | 95% | 75% | 25% |
| | Employees | 0% | 20% | 50% | 75% | 90% | 90% | 90% | 90% | 90% | 75% | 75% | 100% | 100% | 100% | 100% | 100% | 100% | 85% | 35% |
| Retail | Visitors | 1% | 5% | 15% | 35% | 60% | 75% | 100% | 100% | 95% | 85% | 85% | 85% | 90% | 80% | 65% | 45% | 15% | 5% | 0% |
| | Employees | 10% | 15% | 25% | 45% | 75% | 95% | 100% | 100% | 100% | 100% | 100% | 100% | 100% | 100% | 90% | 60% | 40% | 20% | 0% |
| Members Club ³ | Visitors | 10% | 27% | 40% | 100% | 67% | 40% | 30% | 20% | 30% | 10% | 10% | 0% | 60% | 70% | 90% | 60% | 40% | 10% | 10% |

¹ - Hotel restaurant/Bar Includes 14,668 SF of restaurant/bar on 2nd, 6th, and 7th floors and 2,260 SF of private outdoor dining on L7

³ - Members Club time-of-day percentages based on anticipated operations provided by Cheval Blanc

| | | W | eel | kend | T - b | ime | -of- | Day | / Pa | rkin | g D | ema | and | | | | | | | |
|---------------------------------|-----------|---------|---------|---------|---------|----------|----------|----------|---------|---------|---------|---------|---------|---------|---------|---------|---------|----------|----------|----------|
| Land Use | Туре | 6:00 AM | 7:00 AM | 8:00 AM | 9:00 AM | 10:00 AM | 11:00 AM | 12:00 PM | 1:00 PM | 2:00 PM | 3:00 PM | 4:00 PM | 5:00 PM | 6:00 PM | 7:00 PM | 8:00 PM | 9:00 PM | 10:00 PM | 11:00 PM | 12:00 AM |
| Hotel - Leisure | Visitors | 95% | 95% | 90% | 80% | 70% | 70% | 65% | 65% | 70% | 70% | 75% | 80% | 85% | 85% | 90% | 95% | 95% | 100% | 100% |
| | Employees | 10% | 30% | 100% | 100% | 100% | 100% | 100% | 100% | 100% | 100% | 70% | 70% | 40% | 20% | 20% | 20% | 20% | 10% | 5% |
| Hotel Restaurant ¹ | Visitor | 0% | 10% | 30% | 10% | 10% | 5% | 100% | 100% | 33% | 10% | 10% | 30% | 55% | 60% | 70% | 67% | 60% | 40% | 30% |
| | Employee | 10% | 10% | 60% | 100% | 100% | 100% | 100% | 100% | 100% | 100% | 100% | 100% | 100% | 100% | 100% | 100% | 60% | 10% | 10% |
| Fine/Casual Dining ² | Visitors | 0% | 0% | 0% | 0% | 0% | 15% | 50% | 55% | 45% | 45% | 45% | 60% | 90% | 95% | 100% | 90% | 90% | 90% | 50% |
| | Employees | 0% | 20% | 30% | 60% | 75% | 75% | 75% | 75% | 75% | 75% | 75% | 100% | 100% | 100% | 100% | 100% | 100% | 85% | 50% |
| Retail | Visitors | 1% | 5% | 30% | 50% | 70% | 90% | 95% | 100% | 100% | 95% | 90% | 80% | 75% | 70% | 65% | 50% | 30% | 10% | 0% |
| | Employees | 10% | 15% | 40% | 75% | 85% | 95% | 100% | 100% | 100% | 100% | 100% | 95% | 85% | 80% | 75% | 65% | 45% | 15% | 0% |
| Members Club ³ | Visitors | 10% | 27% | 40% | 100% | 67% | 40% | 30% | 20% | 30% | 10% | 10% | 0% | 60% | 70% | 90% | 60% | 40% | 10% | 10% |

^{1 -} Hotel restaurant/Bar Includes 14,668 SF of restaurant/bar on 2nd, 6th, and 7th floors and 2,260 SF of private outdoor dining on L7

² - Restaurant/Bar includes 5,666 SF of restaurant/bar on Ground Floor and 2,500 SF of private outdoor dining on L6

² - Restaurant/Bar includes 5,666 SF of restaurant/bar on Ground Floor and 2,500 SF of private outdoor dining on L6

 $^{^{\}rm 3}$ - Members Club time-of-day percentages based on anticipated operations by Cheval Blanc



Appendix B - City Code Shared Parking Time-Of-Day Parking Demand

| | | | | | | Sh | ared Parkir | ng De | man | d (W | eekda | ay) | | | | | | | | | | | | | | |
|-----------------------------|-----------|-----------------------------|-----------------|-----------------------|-----------------|------------------|----------------------|---------------|---------------|----------------|----------------|----------------|----------------|----------------|----------------|----------------|----------------|-------|----------------|-------|-------|-------|----------------|----------------|-------|----------------|
| | | | Spaces Required | Credit A | Spaces Required | Credit B | Spaces Required | AM | АМ | АМ | AM | AM | AM | PM | PM | PM | PM | PM | PM | PM | PM | PM | PM | PM | PM | AM |
| Use | Unit | Ratio | (no credits) | (Hotel/Retail credit) | (with Credit A) | (Transit Credit) | (with Credits A & B) | 00:9 | 7:00 | 8:00 | 9:00 | 10:00 | 11:00 | 12:00 PM | 1:00 | 2:00 | 3:00 | 4:00 | 5:00 | 00:9 | 7:00 | 8:00 | 9:00 | 10:00 | 11:00 | 12:00 |
| Hotel | | | 115.0 | 0.0 | 115.0 | -17.3 | 97.8 | | | | | | | | | | | | | | | | | | | |
| Visitor ³ | 115 rooms | 1 space / rentable room | 100.0 | 0.0 | 100.0 | -15.0 | 85.0 | 80.8 | 80.8 | 76.5 | 68.0 | 59.5 | 59.5 | 55.3 | 55.3 | 59.5 | 59.5 | 63.8 | 68.0 | 72.3 | 72.3 | 76.5 | 80.8 | 80.8 | 85.0 | 85.0 |
| Employee ³ | | | 15.0 | 0.0 | 15.0 | -2.3 | 12.8 | 1.3 | 3.8 | 12.8 | 12.8 | 12.8 | 12.8 | 12.8 | 12.8 | 12.8 | 12.8 | 8.9 | 8.9 | 5.1 | 2.6 | 2.6 | 2.6 | 2.6 | 1.3 | 0.6 |
| Hotel Restaurant/Bar 1 | | | 48.4 | 0.0 | 48.4 | -7.3 | 41.1 | | | | | | | | | | | | | | | | | | | |
| Visitor ⁴ | 16,928 SF | 1 space / 350 SF floor area | 41.0 | 0.0 | 41.0 | -6.1 | 34.8 | 0.0 | 3.5 | 10.5 | 3.5 | 3.5 | 1.7 | 34.8 | 34.8 | 11.5 | 3.5 | 3.5 | 10.5 | 19.2 | 20.9 | 24.4 | 23.3 | 20.9 | 13.9 | 10.5 |
| Employee ⁴ | | | 7.4 | 0.0 | 7.4 | -1.1 | 6.3 | 0.6 | 0.6 | 3.8 | 6.3 | 6.3 | 6.3 | 6.3 | 6.3 | 6.3 | 6.3 | 6.3 | 6.3 | 3.8 | 2.5 | 2.5 | 1.3 | 0.0 | 0.0 | 0.0 |
| Restaurant/Bar ² | | | 23.3 | 0.0 | 23.3 | -3.5 | 19.8 | | | | | | | | | U U | | • | | | • | u u | · · | | | |
| Visitor | 8,166 SF | 1 space / 350 SF floor area | 19.9 | 0.0 | 19.9 | -3.0 | 17.0 | 0.0 | 0.0 | 0.0 | 0.0 | 2.5 | 6.8 | 12.7 | 12.7 | 11.0 | 6.8 | 8.5 | 12.7 | 16.1 | 17.0 | 17.0 | 17.0 | 16.1 | 12.7 | 4.2 |
| Employee | | | 3.4 | 0.0 | 3.4 | -0.5 | 2.9 | 0.0 | 0.6 | 1.4 | 2.2 | 2.6 | 2.6 | 2.6 | 2.6 | 2.6 | 2.2 | 2.2 | 2.9 | 2.9 | 2.9 | 2.9 | 2.9 | 2.9 | 2.4 | 1.0 |
| Retail | | | 71.4 | -57.5 | 13.9 | -2.1 | 11.8 | | | | | | | | | | | | | | | | | | | |
| Visitor | 24,976 SF | 1 space / 350 SF floor area | 57.5 | -46.3 | 11.2 | -1.7 | 9.5 | 0.1 | 0.5 | 1.4 | 3.3 | 5.7 | 7.1 | 9.5 | 9.5 | 9.0 | 8.1 | 8.1 | 8.1 | 8.5 | 7.6 | 6.2 | 4.3 | 1.4 | 0.5 | 0.0 |
| Employee | | | 13.9 | -11.2 | 2.7 | -0.4 | 2.3 | 0.2 | 0.3 | 0.6 | 1.0 | 1.7 | 2.2 | 2.3 | 2.3 | 2.3 | 2.3 | 2.3 | 2.3 | 2.3 | 2.3 | 2.1 | 1.4 | 0.9 | 0.5 | 0.0 |
| Member's Club | 8,198 SF | 1 space / 350 SF floor area | 23.4 | 0.0 | 23.4 | 0.0 | 23.4 | 2.3 | 6.2 | 9.4 | 23.4 | 15.6 | 9.4 | 7.0 | 4.7 | 7.0 | 2.3 | 2.3 | 0.0 | 14.1 | 16.4 | 21.1 | 14.1 | 9.4 | 2.3 | 2.3 |
| | | | | | | | Unrese | erved Pa | | | 1 | | 1 | , | | | | 1 | 1 | 1 | 1 | | | | 1 | |
| Unreserved Supply | | | | | | | | 146.0 | | | 146.0 | 146.0 | 146.0 | 146.0 | 146.0 | | 146.0 | 146.0 | | | 185.0 | | 185.0 | 185.0 | 185.0 | 185.0 |
| Unreserved Demand | | | | | | | | 83.4 | 91.9 | 99.8 | 101.4 | 91.1 | 89.3 | 124.2 | 121.9 | 102.9 | 84.6 | 90.6 | 104.4 | 144.1 | 144.3 | 155.1 | 147.4 | 134.9 | 118.6 | 103.7 |
| D 10 1 | | | | | | | Reser | ved Parl | | | | | | | 00.0 | | 00.0 | | | T | ı | | | | l | |
| Reserved Supply | | | | | | | | 39.0 | 39.0 | 39.0 | 39.0 | 39.0 | 39.0 | 39.0 | 39.0 | 39.0 | 39.0 | 39.0 | 39.0 | - | - | - | - | - | - | - |
| Reserved Demand | | | | | | | Tot | 1.9 | 4.5 | 16.5 | 19.0 | 19.0 | 19.0 | 19.0 | 19.0 | 19.0 | 19.0 | 15.2 | 15.2 | - | - | - | - | - | - | _ |
| Total Cumply | | | | | | | lot | al Parkin | <u> </u> | | 405.0 | 405.0 | 405.0 | 405.0 | 405.0 | 105.0 | 105.0 | 105.0 | 405.0 | 105.0 | 405.0 | 405.0 | 105.0 | 405.0 | 185.0 | 405.0 |
| Total Supply Total Demand | | | | | | | | 185.0 85.3 | 185.0 96.3 | 185.0 116.3 | 185.0 120.4 | 185.0 110.2 | 185.0 108.3 | 185.0 143.2 | 185.0 140.9 | 185.0 122.0 | 185.0 103.6 | 185.0 | 185.0 119.6 | 185.0 | 185.0 | 185.0 | 185.0 147.4 | 185.0 134.9 | | 185.0 103.7 |

¹ - Hotel restaurant/Bar Includes 14,668 SF of restaurant/bar on 2nd, 6th, and 7th floors and 2,260 SF of private outdoor dining on L7

⁴ - Per ULI rates, the average hotel restaurant parking demand rate is 85% visitors and 15% employees

| | | | | | | Sh | ared Parkin | g De | man | d (We | eeker | nd) | | | | | | | | | | | | | | |
|-----------------------------------|-----------|-----------------------------|-----------------|-----------------------|-----------------|-----------------|----------------------|-------|----------|-------|-------|-------|-------|----------|---------|---------|---------|---------|---------|-------|-------|-------|---------|-------|----------|-------|
| | | | Spaces Required | Credit A | Spaces Required | Credit B | Spaces Required | АМ | AM | АМ | AM | AM | AM | PM | PM | PM | PM | PM | PM | PM | PM | PM | PM | PM | PM | AM |
| Use | Unit | Ratio | (no credits) | (Hotel/Retail credit) | (with Credit A) | (Transit Credit | (with Credits A & B) | 9:00 | 7:00 | 8:00 | 9:00 | 10:00 | 11:00 | 12:00 PM | 1:00 PM | 2:00 PM | 3:00 PM | 4:00 PM | 5:00 PM | 9:00 | 7:00 | 8:00 | 9:00 PM | 10:00 | 11:00 PM | 12:00 |
| Hotel | | | 115.0 | 0.0 | 115.0 | -17.3 | 97.8 | | | | | | | | | | | | | | | | | | | |
| Visitor ³ | 115 rooms | 1 space / rentable room | 100.0 | 0.0 | 100.0 | -15.0 | 85.0 | 80.8 | 80.8 | 76.5 | 68.0 | 59.5 | 59.5 | 55.3 | 55.3 | 59.5 | 59.5 | 63.8 | 68.0 | 72.3 | 72.3 | 76.5 | 80.8 | 80.8 | 85.0 | 85 |
| Employee ³ | | | 15.0 | 0.0 | 15.0 | -2.3 | 12.8 | 1.3 | 3.8 | 12.8 | 12.8 | 12.8 | 12.8 | 12.8 | 12.8 | 12.8 | 12.8 | 8.9 | 8.9 | 5.1 | 2.6 | 2.6 | 2.6 | 2.6 | 1.3 | 1 |
| Hotel Restaurant/Bar ¹ | | | 48.4 | 0.0 | 48.4 | -7.3 | 41.1 | | | | | | | | | | | | | | | | | | | |
| Visitor ⁴ | 16,928 SF | 1 space / 350 SF floor area | 41.0 | 0.0 | 41.0 | -6.1 | 34.8 | 0.0 | 3.5 | 10.5 | 3.5 | 3.5 | 1.8 | 35.0 | 35.0 | 11.6 | 3.5 | 3.5 | 10.5 | 19.3 | 21.0 | 24.5 | 23.5 | 21.0 | 14.0 | 11 |
| Employee ⁴ | | | 7.4 | 0.0 | 7.4 | -1.1 | 6.3 | 0.6 | 0.6 | 3.6 | 6.1 | 6.1 | 6.1 | 6.1 | 6.1 | 6.1 | 6.1 | 6.1 | 6.1 | 6.1 | 6.1 | 6.1 | 6.1 | 3.6 | 0.6 | 1 |
| Restaurant/Bar ² | | | 23.3 | 0.0 | 23.3 | -3.5 | 19.8 | | | l. | | | l | l | | | | | L | | | L | L | | | |
| Visitor | 8,166 SF | 1 space / 350 SF floor area | 20.0 | 0.0 | 20.0 | -3.0 | 17.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 2.6 | 8.5 | 9.4 | 7.7 | 7.7 | 7.7 | 10.2 | 15.3 | 16.2 | 17.0 | 15.3 | 15.3 | 15.3 | 9 |
| Employee | | | 3.3 | 0.0 | 3.3 | -0.5 | 2.8 | 0.0 | 0.6 | 0.8 | 1.7 | 2.1 | 2.1 | 2.1 | 2.1 | 2.1 | 2.1 | 2.1 | 2.8 | 2.8 | 2.8 | 2.8 | 2.8 | 2.8 | 2.4 | 1 |
| Retail | | | 71.4 | -57.5 | 13.9 | -2.1 | 11.8 | | | | | | | | | | | | | | | | | | | |
| Visitor | 24,976 SF | 1 space / 350 SF floor area | 57.1 | -46.0 | 11.1 | -1.7 | 9.4 | 0.1 | 0.5 | 2.8 | 4.7 | 6.6 | 8.5 | 9.0 | 9.4 | 9.4 | 9.0 | 8.5 | 7.5 | 7.1 | 6.6 | 6.1 | 4.7 | 2.8 | 0.9 | 0 |
| Employee | | | 14.3 | -11.5 | 2.8 | -0.4 | 2.4 | 0.2 | 0.4 | 0.9 | 1.8 | 2.0 | 2.2 | 2.4 | 2.4 | 2.4 | 2.4 | 2.4 | 2.2 | 2.0 | 1.9 | 1.8 | 1.5 | 1.1 | 0.4 | 0 |
| Member's Club | 8,198 SF | 1 space / 350 SF floor area | 23.4 | 0.0 | 23.4 | 0.0 | 23.4 | 2.3 | 6.2 | 9.4 | 23.4 | 15.6 | 9.4 | 7.0 | 4.7 | 7.0 | 2.3 | 2.3 | 0.0 | 14.1 | 16.4 | 21.1 | 14.1 | 9.4 | 2.3 | 2.3 |
| | | | | | | | Unrese | | king Spa | | | | • | • | | | | | | | | | | | | |
| Unreserved Supply | | | | | | | | 146.0 | 146.0 | 146.0 | 146.0 | 146.0 | 146.0 | 146.0 | 146.0 | 146.0 | 146.0 | 146.0 | 146.0 | 185.0 | 185.0 | 185.0 | 185.0 | 185.0 | 185.0 | 185.0 |
| Unreserved Demand | | | | | | | _ | 83.4 | 91.9 | 101.0 | 103.1 | 89.3 | 86.0 | 119.2 | 118.2 | 99.6 | 86.4 | 90.2 | 101.3 | 143.9 | 145.8 | 158.5 | 151.3 | 139.4 | 122.2 | 109.0 |
| | | | | | | | Reser | | ing Spac | | | | | | | | | | | | | 1 | 1 | | | |
| Reserved Supply | | | | | | | | 39.0 | 39.0 | 39.0 | 39.0 | 39.0 | 39.0 | 39.0 | 39.0 | 39.0 | 39.0 | 39.0 | 39.0 | - | - | - | - | - | - | |
| Reserved Demand | | | | | | | | 1.9 | 4.4 | 16.4 | 18.8 | 18.8 | 18.8 | 18.8 | 18.8 | 18.8 | 18.8 | 15.0 | 15.0 | | | - | - | | | - |
| Total Cumply | | | | | | | Tota | | g Spaces | | 405.0 | 405.0 | 405.0 | 405.0 | 405.0 | 405.0 | 405.0 | 405.0 | 405.0 | 405.0 | 405.0 | 405.0 | 405.0 | 405.0 | 405.0 | 405.0 |
| Total Supply | | | | | | | | 185.0 | 185.0 | 185.0 | 185.0 | 185.0 | 185.0 | 185.0 | 185.0 | | 185.0 | 185.0 | 185.0 | 185.0 | 185.0 | 185.0 | 185.0 | 185.0 | 185.0 | 185.0 |
| Total Demand | | | | | | | | 85.3 | 96.3 | 117.4 | 121.9 | 108.1 | 104.8 | 138.1 | 137.0 | 118.5 | 105.2 | 105.2 | 116.3 | 143.9 | 145.8 | 158.5 | 151.3 | 139.4 | 122.2 | 109.0 |

^{-1 -} Hotel restaurant/Bar Includes 14,668 SF of restaurant/bar on 2nd, 6th, and 7th floors and 2,260 SF of private outdoor dining on L7

² - Restaurant/Bar includes 5,666 SF of restaurant/bar on Ground Floor and 2,500 SF of private outdoor dining on L6 ³ - Per ULI rates, the average hotel parking demand rate is 87% visitors and 13% employees

² - Restaurant/Bar includes 5,666 SF of restaurant/bar on Ground Floor and 2,500 SF of private outdoor dining on L6

 $^{^{\}rm 3}$ - Per ULI rates, the average hotel parking demand rate is 87% visitors and 13% employees

⁴ - Per ULI rates, the average hotel restaurant parking demand rate is 85% visitors and 15% employees



Appendix C - Hotel Drive-Rate Data

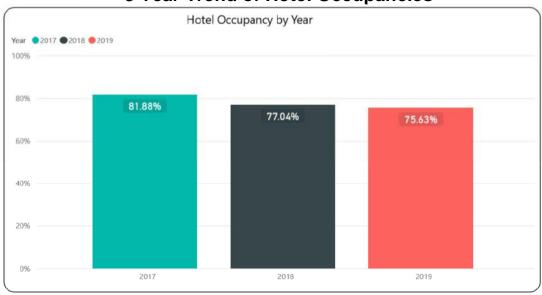
Cheval Blanc Beverly Hills Luxury Hotel Parking Analysis (March 10, 2020)

LAZ Parking, founded in 1981, operates hundreds of thousands of parking spaces from offices across the county and maintains data to manage its valet operations. LAZ Parking has developed tools to capture and analyze data on parked cars, hotel occupancies, and drive-in rates as follows:

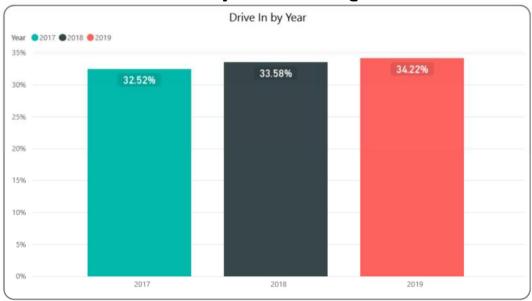
Empirical Data for Beverly Hills and Vicinity

The 3-year trend of hotel occupancies at Beverly Hills Luxury hotels from 2017 -2019 is 82%, 77%, and 76% respectively.





3 Year Trend of Luxury Hotel Overnight Drive-In Rates



The 3-year trend of overnight drive in rates is 32.5%, 33.6% and 34.2%

Hotel overnight drive in rates are derived by calculating the number of occupied rooms based on hotel occupancy and comparing that with the number of overnight cars parked based on market data from LAZ Parking.

For example, a 100-room hotel at 100% occupancy results in 100 rooms nights. Based on the market data over the past 3 years the average drive in rate on overnight cars is 33.4%. 100 room nights at 33.4% drive in rate would result in 33 cars on average per night. Required guest parking can then be calculated using the following formula:

33.4% x number of guest rooms = required Hotel Guest Parking

Cheval Blanc at 115 rooms and 100% occupancy would exhibit a parking demand of approximately 38.4 guest parking spaces.

Total Overnight Cars vs. Transient Cars Beverly Hills Luxury Hotels '18 and '19

LAZ Parking data indicates that transient visitor cars make up 75% of cars parked. Transient visitor cars are considered any other cars parked besides an overnight hotel guest (restaurant, banquet, event, meeting space, spa, etc.).



*Includes Banquet & Public Use Space Cars

Using the required number of guest parking spaces, the total number of required hotel visitor parking spaces can be determined. Transient Visitor Parking (including public assembly visitors) can be calculated using the following formula:

Hotel Guest Parking / 25% = Total Visitor Parking required

Total Visitor Parking Required x 75% = Transient Visitor Parking

For the 115-room Cheval Blanc project, the total breakdown of Transient Visitor Cars parked would be as follows:

38.4 Hotel Guest Cars / 25% = 153 Total Visitor Cars

Total Visitor Cars x 75% = 115 Transient Visitor Cars (including public assembly visitors)

Since the Cheval Blanc does not contain public assembly spaces, this number should be further reduced.

spaces in its motor court as proposed for Cheval Blanc.



Appendix D – Restaurant Drive-Rate Data

| | | Drive- | in Rates for | Luxury Resta | urants in Be | verly Hills and Simila | ar Commun | ties ¹ | | | | |
|------------|--|-----------------|----------------------------|------------------|---------------------|---------------------------|-----------|-------------------|---------|---------|--|--|
| Restaurant | Luxury | Stand- alone | Valet/ Self- Parking | Lunch/ Dinner | Capacity (Seats) | | 2017 | 2018 | 2019 | Average | | |
| | | | | | | Cover Counts | 94,977 | 109,983 | 104,094 | | | |
| Α | X | X | Valet Only | | | Cars Parked | 33,046 | 29,474 | 26,469 | | | |
| | | | | | | Drive in Rate | 35% | 27% | 25% | | | |
| | | | | | | Cover Counts ² | | 91,250 | | | | |
| В | X | X | Valet Only | Dinner Only | 250 | Cars Parked | 24,720 | 23,728 | 22,600 | | | |
| | | | | | | Drive in Rate | 27% | 26% | 25% | | | |
| | | | | | | Cover Counts ³ | | 150,800 | | | | |
| С | X | X | Valet Only | Dinner Only | 400 | Cars Parked | 47,580 | 47,377 | 46,867 | | | |
| | | | | | | Drive in Rate | 32% | 31% | 31% | | | |
| | Average Drive-in Rate 31.3% 28.6% 27.7% 29.2 | | | | | | | | | | | |

¹ Valet car parking and cover count data provided by LAZ Parking for three luxury stand-alone restaurants in Beverly Hills and similar communities. Data is proprietary and restaurants cannot be named

² Annual cover count estimated based on an average of 250 covers per night (provided by LAZ Parking)

³ Annual cover count estimated based on an average of 700-800 covers on Friday nights, 1,000 covers on Saturday nights, 0 covers on Sunday nights, and 300-450 covers on Monday-Thursday nights. Cover counts at the lower end of each range were assumed in order to be conservative (provided by LAZ Parking)



Appendix E – ITE Internal Capture Worksheets

| | NCHRP 684 Internal Trip C | ар | ture Estimation Tool | |
|-----------------------|----------------------------|----|----------------------|----------------------------------|
| Project Name: | Beverly Hills Cheval Blanc | | Organization: | Kimley-Horn and Associates, Inc. |
| Project Location: | Beverly Hills | | Performed By: | |
| Scenario Description: | | | Date: | |
| Analysis Year: | | | Checked By: | |
| Analysis Period: | AM Street Peak Hour | | Date: | |

| Land Use | Developme | ent Data (For Inf | formation Only) | | Estimated Vehicle-Trips ³ | |
|----------------------------------|-----------|-------------------|------------------|-------|--------------------------------------|---------|
| Land Ose | ITE LUCs1 | Quantity | Units | Total | Entering | Exiting |
| Office | | = | 1,000 Sq Ft | 0 | 0 | 0 |
| Retail | | 25 | 1,000 Sq Ft | 23 | 14 | 9 |
| Restaurant | | 25 | 1,000 Sq Ft | 18 | 14 | 4 |
| Cinema/Entertainment | | - | Screen(s) | 0 | 0 | 0 |
| Residential | | - | Dwelling Unit(s) | 0 | 0 | 0 |
| Hotel | | 115 | Room(s) | 54 | 32 | 22 |
| All Other Land Uses ² | | = | 0 | 0 | 0 | 0 |
| | | | - | 95 | 60 | 35 |

| | Table 2-A: Mode Split and Vehicle Occupancy Estimates | | | | | | | | | | | | | |
|----------------------------------|---|---------------|-----------------|---------------|------------|-----------|-----------------|--|--|--|--|--|--|--|
| Land Use | | Entering Trip | OS | Exiting Trips | | | | | | | | | | |
| Land Ose | Veh. Occ.4 | % Transit | % Non-Motorized | | Veh. Occ.4 | % Transit | % Non-Motorized | | | | | | | |
| Office | 1.00 | 0% | 0% | | 1.00 | 0% | 0% | | | | | | | |
| Retail | 1.00 | 0% | 0% | | 1.00 | 0% | 0% | | | | | | | |
| Restaurant | 1.00 | 0% | 0% | | 1.00 | 0% | 0% | | | | | | | |
| Cinema/Entertainment | 1.00 | 0% | 0% | | 1.00 | 0% | 0% | | | | | | | |
| Residential | 1.00 | 0% | 0% | | 1.00 | 0% | 0% | | | | | | | |
| Hotel | 1.00 | 0% | 0% | | 1.00 | 0% | 0% | | | | | | | |
| All Other Land Uses ² | 1.00 | 0% | 0% | | 1.00 | 0% | 0% | | | | | | | |

| | Table 3-A: Average Land Use Interchange Distances (Feet Walking Distance) | | | | | | | | | | |
|----------------------|---|--------|------------|----------------------|-------------|-------|--|--|--|--|--|
| Origin (Franc) | | | | Destination (To) | | | | | | | |
| Origin (From) | Office | Retail | Restaurant | Cinema/Entertainment | Residential | Hotel | | | | | |
| Office | | | | | | | | | | | |
| Retail | | | | | | | | | | | |
| Restaurant | | | | | | | | | | | |
| Cinema/Entertainment | | | | | | | | | | | |
| Residential | | | | | | | | | | | |
| Hotel | | | | | | | | | | | |

| Table 4-A: Internal Person-Trip Origin-Destination Matrix* | | | | | | | | | | | |
|--|--------|--------|------------|----------------------|-------------|-------|--|--|--|--|--|
| Origin (From) | | | | Destination (To) | | | | | | | |
| Origin (From) | Office | Retail | Restaurant | Cinema/Entertainment | Residential | Hotel | | | | | |
| Office | | 0 | 0 | 0 | 0 | 0 | | | | | |
| Retail | 0 | | 1 | 0 | 0 | 0 | | | | | |
| Restaurant | 0 | 1 | | 0 | 0 | 0 | | | | | |
| Cinema/Entertainment | 0 | 0 | 0 | | 0 | 0 | | | | | |
| Residential | 0 | 0 | 0 | 0 | | 0 | | | | | |
| Hotel | 0 | 1 | 1 | 0 | 0 | | | | | | |

| Table 5-A: Computations Summary | | | | | | | | | | | |
|---|----|----|-----|--|--|--|--|--|--|--|--|
| Total Entering Exiting | | | | | | | | | | | |
| All Person-Trips | 95 | 60 | 35 | | | | | | | | |
| Internal Capture Percentage | 8% | 7% | 11% | | | | | | | | |
| | | | | | | | | | | | |
| External Vehicle-Trips ⁵ | 87 | 56 | 31 | | | | | | | | |
| External Transit-Trips ⁶ | 0 | 0 | 0 | | | | | | | | |
| External Non-Motorized Trips ⁶ | 0 | 0 | 0 | | | | | | | | |

| Table 6-A: Interna | Table 6-A: Internal Trip Capture Percentages by Land Use | | | | | | | | | |
|----------------------|--|---------------|--|--|--|--|--|--|--|--|
| Land Use | Entering Trips | Exiting Trips | | | | | | | | |
| Office | N/A | N/A | | | | | | | | |
| Retail | 14% | 11% | | | | | | | | |
| Restaurant | 14% | 25% | | | | | | | | |
| Cinema/Entertainment | N/A | N/A | | | | | | | | |
| Residential | N/A | N/A | | | | | | | | |
| Hotel | 0% | 9% | | | | | | | | |

¹Land Use Codes (LUCs) from *Trip Generation Manual*, published by the Institute of Transportation Engineers.

⁶Person-Trips

*Indicates computation that has been rounded to the nearest whole number.

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²Total estimate for all other land uses at mixed-use development site is not subject to internal trip capture computations in this estimator.

³Enter trips assuming no transit or non-motorized trips (as assumed in ITE *Trip Generation Manual*).

⁴Enter vehicle occupancy assumed in Table 1-A vehicle trips. If vehicle occupancy changes for proposed mixed-use project, manual adjustments must be made to Tables 5-A, 9-A (O and D). Enter transit, non-motorized percentages that will result with proposed mixed-use project complete.

⁵Vehicle-trips computed using the mode split and vehicle occupancy values provided in Table 2-A.

| Project Name: | Beverly Hills Cheval Blanc |
|------------------|----------------------------|
| Analysis Period: | AM Street Peak Hour |

| | Table 7-A: Conversion of Vehicle-Trip Ends to Person-Trip Ends | | | | | | | | | | | |
|----------------------|--|-------------------|---------------|--|-----------|------------------------------|---------------|--|--|--|--|--|
| 1 111 | Tab | le 7-A (D): Enter | ing Trips | | | Table 7-A (O): Exiting Trips | 3 | | | | | |
| Land Use | Veh. Occ. | Vehicle-Trips | Person-Trips* | | Veh. Occ. | Vehicle-Trips | Person-Trips* | | | | | |
| Office | 1.00 | 0 | 0 | | 1.00 | 0 | 0 | | | | | |
| Retail | 1.00 | 14 | 14 | | 1.00 | 9 | 9 | | | | | |
| Restaurant | 1.00 | 14 | 14 | | 1.00 | 4 | 4 | | | | | |
| Cinema/Entertainment | 1.00 | 0 | 0 | | 1.00 | 0 | 0 | | | | | |
| Residential | 1.00 | 0 | 0 | | 1.00 | 0 | 0 | | | | | |
| Hotel | 1.00 | 32 | 32 | | 1.00 | 22 | 22 | | | | | |

| | Table 8-A (O): Internal Person-Trip Origin-Destination Matrix (Computed at Origin) | | | | | | | | | | |
|----------------------|--|------------------|------------|----------------------|-------------|-------|--|--|--|--|--|
| Origin (From) | | Destination (To) | | | | | | | | | |
| Origin (From) | Office | Retail | Restaurant | Cinema/Entertainment | Residential | Hotel | | | | | |
| Office | | 0 | 0 | 0 | 0 | 0 | | | | | |
| Retail | 3 | | 1 | 0 | 1 | 0 | | | | | |
| Restaurant | 1 | 1 | | 0 | 0 | 0 | | | | | |
| Cinema/Entertainment | 0 | 0 | 0 | | 0 | 0 | | | | | |
| Residential | 0 | 0 | 0 | 0 | | 0 | | | | | |
| Hotel | 17 | 3 | 2 | 0 | 0 | | | | | | |

| Table 8-A (D): Internal Person-Trip Origin-Destination Matrix (Computed at Destination) | | | | | | | | | | | |
|---|--------|------------------|------------|----------------------|-------------|-------|--|--|--|--|--|
| Origin (From) | | Destination (To) | | | | | | | | | |
| Origin (From) | Office | Retail | Restaurant | Cinema/Entertainment | Residential | Hotel | | | | | |
| Office | | 4 | 3 | 0 | 0 | 0 | | | | | |
| Retail | 0 | | 7 | 0 | 0 | 0 | | | | | |
| Restaurant | 0 | 1 | | 0 | 0 | 1 | | | | | |
| Cinema/Entertainment | 0 | 0 | 0 | | 0 | 0 | | | | | |
| Residential | 0 | 2 | 3 | 0 | | 0 | | | | | |
| Hotel | 0 | 1 | 1 | 0 | 0 | | | | | | |

| | Table 9-A (D): Internal and External Trips Summary (Entering Trips) | | | | | | | | | | | |
|----------------------------------|---|------------------|-------|-----|-------------------------|----------------------|----------------------------|--|--|--|--|--|
| Destination Land Lies | 1 | Person-Trip Esti | mates | | External Trips by Mode* | | | | | | | |
| Destination Land Use | Internal | External | Total | | Vehicles ¹ | Transit ² | Non-Motorized ² | | | | | |
| Office | 0 | 0 | 0 | 1 [| 0 | 0 | 0 | | | | | |
| Retail | 2 | 12 | 14 | | 12 | 0 | 0 | | | | | |
| Restaurant | 2 | 12 | 14 | 1 [| 12 | 0 | 0 | | | | | |
| Cinema/Entertainment | 0 | 0 | 0 | 7 I | 0 | 0 | 0 | | | | | |
| Residential | 0 | 0 | 0 | 1 [| 0 | 0 | 0 | | | | | |
| Hotel | 0 | 32 | 32 | | 32 | 0 | 0 | | | | | |
| All Other Land Uses ³ | 0 | 0 | 0 | | 0 | 0 | 0 | | | | | |

| | Table 9-A (O): Internal and External Trips Summary (Exiting Trips) | | | | | | | | | | | |
|----------------------------------|--|----------|-------|--|-------------------------|----------------------|----------------------------|--|--|--|--|--|
| Origin Land Han | Person-Trip Estimates | | | | External Trips by Mode* | | | | | | | |
| Origin Land Use | Internal | External | Total | | Vehicles ¹ | Transit ² | Non-Motorized ² | | | | | |
| Office | 0 | 0 | 0 | | 0 | 0 | 0 | | | | | |
| Retail | 1 | 8 | 9 | | 8 | 0 | 0 | | | | | |
| Restaurant | 1 | 3 | 4 | | 3 | 0 | 0 | | | | | |
| Cinema/Entertainment | 0 | 0 | 0 | | 0 | 0 | 0 | | | | | |
| Residential | 0 | 0 | 0 | | 0 | 0 | 0 | | | | | |
| Hotel | 2 | 20 | 22 | | 20 | 0 | 0 | | | | | |
| All Other Land Uses ³ | 0 | 0 | 0 | | 0 | 0 | 0 | | | | | |

¹Vehicle-trips computed using the mode split and vehicle occupancy values provided in Table 2-A

²Person-Trips

³Total estimate for all other land uses at mixed-use development site is not subject to internal trip capture computations in this estimator *Indicates computation that has been rounded to the nearest whole number.

| | NCHRP 684 Internal Trip Capture Estimation Tool | | | | | | | | | |
|-----------------------|---|---------------|----------------------------------|--|--|--|--|--|--|--|
| Project Name: | | Organization: | Kimley-Horn and Associates, Inc. | | | | | | | |
| Project Location: | | | Performed By: | | | | | | | |
| Scenario Description: | | | Date: | | | | | | | |
| Analysis Year: | | | Checked By: | | | | | | | |
| Analysis Period: | PM Street Peak Hour | | Date: | | | | | | | |

| | Table 1-P: Base Vehicle-Trip Generation Estimates (Single-Use Site Estimate) | | | | | | | | | | |
|----------------------------------|--|-------------------|------------------|-----|--------------------------------------|----------|---------|--|--|--|--|
| Land Use | Developme | ent Data (For Int | formation Only) | | Estimated Vehicle-Trips ³ | | | | | | |
| Land USE | ITE LUCs1 | Quantity | Units |] [| Total | Entering | Exiting | | | | |
| Office | | - | 1,000 Sq Ft | l I | 0 | 0 | 0 | | | | |
| Retail | | 25 | 1,000 Sq Ft | l I | 95 | 46 | 49 | | | | |
| Restaurant | | 25 | 1,000 Sq Ft | l I | 196 | 131 | 65 | | | | |
| Cinema/Entertainment | | - | Screen(s) | l I | 0 | 0 | 0 | | | | |
| Residential | | - | Dwelling Unit(s) | l I | 0 | 0 | 0 | | | | |
| Hotel | | 115 | Room(s) | l l | 69 | 35 | 34 | | | | |
| All Other Land Uses ² | | 0 | 0 | | 0 | 0 | 0 | | | | |
| | | | | | 360 | 212 | 148 | | | | |

| | Table 2-P: Mode Split and Vehicle Occupancy Estimates | | | | | | | | | | | | |
|----------------------------------|---|--------------|-----------------|--|---------------|-----------------------------|----|--|--|--|--|--|--|
| Land Use | | Entering Tri | ps | | Exiting Trips | | | | | | | | |
| Land Ose | Veh. Occ.4 | % Transit | % Non-Motorized | | Veh. Occ.4 | Veh. Occ. 4 % Transit % Nor | | | | | | | |
| Office | 1.00 | 0% | 0% | | 1.00 | 0% | 0% | | | | | | |
| Retail | 1.00 | 0% | 0% | | 1.00 | 0% | 0% | | | | | | |
| Restaurant | 1.00 | 0% | 0% | | 1.00 | 0% | 0% | | | | | | |
| Cinema/Entertainment | 1.00 | 0% | 0% | | 1.00 | 0% | 0% | | | | | | |
| Residential | 1.00 | 0% | 0% | | 1.00 | 0% | 0% | | | | | | |
| Hotel | 1.00 | 0% | 0% | | 1.00 | 0% | 0% | | | | | | |
| All Other Land Uses ² | 1.00 | 0% | 0% | | 1.00 | 0% | 0% | | | | | | |

| | Table 3-P: Average Land Use Interchange Distances (Feet Walking Distance) | | | | | | | | | | | | | |
|----------------------|---|------------------|------------|----------------------|-------------|-------|--|--|--|--|--|--|--|--|
| Origin (From) | | Destination (To) | | | | | | | | | | | | |
| | Office | Retail | Restaurant | Cinema/Entertainment | Residential | Hotel | | | | | | | | |
| Office | | | | | | | | | | | | | | |
| Retail | | | | | | | | | | | | | | |
| Restaurant | | | | | | | | | | | | | | |
| Cinema/Entertainment | | | | | | | | | | | | | | |
| Residential | | | | | | | | | | | | | | |
| Hotel | | | | | | | | | | | | | | |

| Table 4-P: Internal Person-Trip Origin-Destination Matrix* | | | | | | | | | | | | | | |
|--|--------|------------------|------------|----------------------|-------------|-------|--|--|--|--|--|--|--|--|
| Origin (From) | | Destination (To) | | | | | | | | | | | | |
| Origin (From) | Office | Retail | Restaurant | Cinema/Entertainment | Residential | Hotel | | | | | | | | |
| Office | | 0 | 0 | 0 | 0 | 0 | | | | | | | | |
| Retail | 0 | | 14 | 0 | 0 | 2 | | | | | | | | |
| Restaurant | 0 | 23 | | 0 | 0 | 5 | | | | | | | | |
| Cinema/Entertainment | 0 | 0 | 0 | | 0 | 0 | | | | | | | | |
| Residential | 0 | 0 | 0 | 0 | | 0 | | | | | | | | |
| Hotel | 0 | 1 | 7 | 0 | 0 | | | | | | | | | |

| Table 5-F | : Computatio | ns Summary | | |
|---|--------------|------------|-----|--|
| | Total | Exiting | | |
| All Person-Trips | 360 | 212 | 148 | |
| Internal Capture Percentage | 29% | 25% | 35% | |
| | | | | |
| External Vehicle-Trips ⁵ | 256 | 160 | 96 | |
| External Transit-Trips ⁶ | 0 | 0 | 0 | |
| External Non-Motorized Trips ⁶ | 0 | 0 | 0 | |

| Table 6-P: Interna | al Trip Capture Percentaç | ges by Land Use | | | | |
|----------------------|---------------------------|-----------------|--|--|--|--|
| Land Use | Entering Trips | Exiting Trips | | | | |
| Office | N/A | N/A | | | | |
| Retail | 52% | 33% | | | | |
| Restaurant | 16% | 43% | | | | |
| Cinema/Entertainment | N/A | N/A | | | | |
| Residential | N/A | N/A | | | | |
| Hotel | 20% | 24% | | | | |

¹Land Use Codes (LUCs) from *Trip Generation Manual*, published by the Institute of Transportation Engineers.

²Total estimate for all other land uses at mixed-use development site is not subject to internal trip capture computations in this estimator.

³Enter trips assuming no transit or non-motorized trips (as assumed in ITE *Trip Generation Manual*).

⁴Enter vehicle occupancy assumed in Table 1-P vehicle trips. If vehicle occupancy changes for proposed mixed-use project, manual adjustments must be ⁵Vehicle-trips computed using the mode split and vehicle occupancy values provided in Table 2-P.

⁶Person-Trips

*Indicates computation that has been rounded to the nearest whole number.

Estimation Tool Developed by the Texas A&M Transportation Institute - Version 2013.1

| Project Name: | 0 |
|------------------|---------------------|
| Analysis Period: | PM Street Peak Hour |

| Table 7-P: Conversion of Vehicle-Trip Ends to Person-Trip Ends | | | | | | | | | | | | |
|--|-----------|-------------------|---------------|---|-----------|------------------------------|---------------|--|--|--|--|--|
| Land Use | Table | 7-P (D): Entering | g Trips | | | Table 7-P (O): Exiting Trips | i | | | | | |
| Land Ose | Veh. Occ. | Vehicle-Trips | Person-Trips* | 1 | Veh. Occ. | Vehicle-Trips | Person-Trips* | | | | | |
| Office | 1.00 | 0 | 0 | | 1.00 | 0 | 0 | | | | | |
| Retail | 1.00 | 46 | 46 | | 1.00 | 49 | 49 | | | | | |
| Restaurant | 1.00 | 131 | 131 | | 1.00 | 65 | 65 | | | | | |
| Cinema/Entertainment | 1.00 | 0 | 0 | | 1.00 | 0 | 0 | | | | | |
| Residential | 1.00 | 0 | 0 | | 1.00 | 0 | 0 | | | | | |
| Hotel | 1.00 | 35 | 35 | | 1.00 | 34 | 34 | | | | | |

| Table 8-P (O): Internal Person-Trip Origin-Destination Matrix (Computed at Origin) | | | | | | | | | | | | | |
|--|------------------|--------|------------|----------------------|-------------|-------|--|--|--|--|--|--|--|
| Origin (From) | Destination (To) | | | | | | | | | | | | |
| Oligili (Floili) | Office | Retail | Restaurant | Cinema/Entertainment | Residential | Hotel | | | | | | | |
| Office | | 0 | 0 | 0 | 0 | 0 | | | | | | | |
| Retail | 1 | | 14 | 2 | 13 | 2 | | | | | | | |
| Restaurant | 2 | 27 | | 5 | 12 | 5 | | | | | | | |
| Cinema/Entertainment | 0 | 0 | 0 | | 0 | 0 | | | | | | | |
| Residential | 0 | 0 | 0 | 0 | | 0 | | | | | | | |
| Hotel | 0 | 5 | 23 | 0 | 1 | | | | | | | | |

| Table 8-P (D): Internal Person-Trip Origin-Destination Matrix (Computed at Destination) | | | | | | | | | | | | | |
|---|------------------|--------|------------|----------------------|-------------|-------|--|--|--|--|--|--|--|
| Origin (Franc) | Destination (To) | | | | | | | | | | | | |
| Origin (From) | Office | Retail | Restaurant | Cinema/Entertainment | Residential | Hotel | | | | | | | |
| Office | | 4 | 3 | 0 | 0 | 0 | | | | | | | |
| Retail | 0 | | 38 | 0 | 0 | 6 | | | | | | | |
| Restaurant | 0 | 23 | | 0 | 0 | 25 | | | | | | | |
| Cinema/Entertainment | 0 | 2 | 4 | | 0 | 0 | | | | | | | |
| Residential | 0 | 5 | 18 | 0 | | 4 | | | | | | | |
| Hotel | 0 | 1 | 7 | 0 | 0 | | | | | | | | |

| | Tal | ole 9-P (D): Inter | nal and External T | rips | Summary (Entering Tr | ips) | | | | | |
|----------------------------------|----------|--------------------|--------------------|------|-------------------------|----------------------|----------------------------|--|--|--|--|
| Destination Land Use | Р | erson-Trip Estima | ites | | External Trips by Mode* | | | | | | |
| Destination Land Use | Internal | External | Total | Ī | Vehicles ¹ | Transit ² | Non-Motorized ² | | | | |
| Office | 0 | 0 | 0 | | 0 | 0 | 0 | | | | |
| Retail | 24 | 22 | 46 | Ī | 22 | 0 | 0 | | | | |
| Restaurant | 21 | 110 | 131 | Ī | 110 | 0 | 0 | | | | |
| Cinema/Entertainment | 0 | 0 | 0 | Ī | 0 | 0 | 0 | | | | |
| Residential | 0 | 0 | 0 | Ī | 0 | 0 | 0 | | | | |
| Hotel | 7 | 28 | 35 | Ī | 28 | 0 | 0 | | | | |
| All Other Land Uses ³ | 0 | 0 | 0 | | 0 | 0 | 0 | | | | |

| | Та | ble 9-P (O): Inter | nal and External 1 | Γrip | s Summary (Exiting Tri | os) | | | | |
|----------------------------------|----------|--------------------|--------------------|------|--|-----|----------------------------|--|--|--|
| Origin Land Llos | Pe | erson-Trip Estima | ites | | External Trips by Mode* | | | | | |
| Origin Land Use | Internal | External | Total | Ī | Vehicles ¹ Transit ² | | Non-Motorized ² | | | |
| Office | 0 | 0 | 0 | | 0 | 0 | 0 | | | |
| Retail | 16 | 33 | 49 | | 33 | 0 | 0 | | | |
| Restaurant | 28 | 37 | 65 | | 37 | 0 | 0 | | | |
| Cinema/Entertainment | 0 | 0 | 0 | | 0 | 0 | 0 | | | |
| Residential | 0 | 0 | 0 | | 0 | 0 | 0 | | | |
| Hotel | 8 | 26 | 34 | | 26 | 0 | 0 | | | |
| All Other Land Uses ³ | 0 | 0 | 0 | | 0 | 0 | 0 | | | |

¹Vehicle-trips computed using the mode split and vehicle occupancy values provided in Table 2-P

²Person-Trips

³Total estimate for all other land uses at mixed-use development site is not subject to internal trip capture computations in this estimator

That has been rounded to the nearest whole number.



Appendix F - ULI Shared Parking Time-Of-Day Parking Demand

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Project: Cheval Blanc Hotel, Beverly Hills

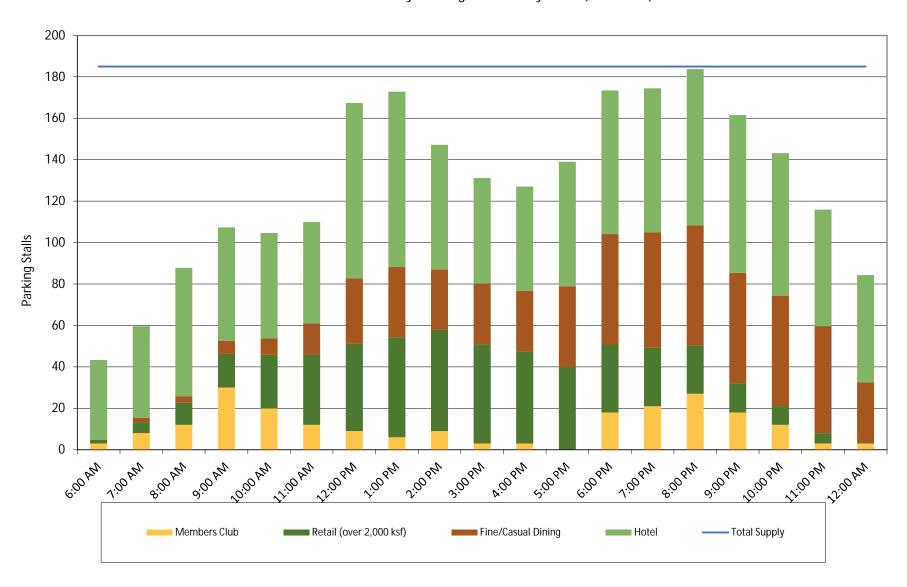
Description: Scenario A

| | | | | | | Sharo | ed Parking [| om and Si | ımmarv | | | | | | | | | |
|------------------------------|----------|---------------|----------------|---------|------------------|-------------------|--------------|----------------|----------|------------------|---------|----------|---------|------------|-----------|---------|-------------|-----------|
| | | | | | Peak M | | EMBER | | | WEEKEND | | | | | | | | |
| | | | | | Weekday | | | | | Weekend | | | | Weekday | | | Weekend | |
| Lond Hon | Proje | ct Data | Dana | Deluies | Non- | Daniant | Hait Fan | Base | Datistan | Non- | Desiret | Unit For | Peak Hr | Peak Mo | Estimated | Peak Hr | Peak Mo | Estimated |
| Land Use | | Base Ratio | Driving Adj | Captive | Project Ratio | Unit For Ratio | Ratio | Driving Adj | Captive | Project Ratio | Ratio | Adj | Adj | Parking | Adj | Adj | Parking | |
| | Quantity | Unit | Ratio | Auj | Ratio | Ratio | Katio | Katio | Auj | Ratio | Ratio | Ratio | 8 PM | December | Demand | 8 PM | ite Decemb | Demand |
| | Retail | | | | | | | | | | | | | | | | | |
| Retail (over 2,000 ksf) | 24,976 | sf GLA | 2.90 | 75% | 80% | 1.74 | ksf GLA | 3.20 | 75% | 80% | 1.92 | ksf GLA | 85% | 100% | 37 | 55% | 85% | 20 |
| Employee | | | 0.70 | 50% | 100% | 0.35 | | 0.80 | 50% | 100% | 0.40 | | 90% | 100% | 8 | 30% | 95% | 3 |
| | | | | | | | Food and | Beverage | ! | | | | | | | | | |
| Fine/Casual Dining | 8,166 | sf GLA | 13.25 | 50% | 80% | 5.30 | ksf GLA | 15.25 | 50% | 80% | 6.10 | ksf GLA | 100% | 100% | 44 | 100% | 95% | 48 |
| Employee | | | 2.25 | 50% | 100% | 1.13 | | 2.50 | 50% | 100% | 1.25 | | 100% | 100% | 10 | 100% | 100% | 11 |
| | | | | | | | Hotel and | Residentia | al | | | | | | | | | |
| Hotel-Business | | keys | 1.00 | 59% | 100% | 0.59 | key | 1.00 | 69% | 100% | 0.69 | key | 80% | 60% | - | 80% | 55% | - |
| Hotel-Leisure | 115 | keys | 1.00 | 33% | 100% | 0.33 | key | 1.00 | 33% | 100% | 0.33 | key | 90% | 50% | 17 | 90% | 100% | 35 |
| Hotel Employees | 115 | keys | 0.15 | 50% | 100% | 0.08 | key | 0.15 | 50% | 100% | 0.08 | key | 20% | 50% | 1 | 20% | 100% | 2 |
| Restaurant/Lounge | 16,928 | sf GLA | 6.67 | 47% | 80% | 2.51 | ksf GLA | 7.67 | 40% | 80% | 2.45 | ksf GLA | 70% | 100% | 30 | 70% | 95% | 28 |
| Restaurant/Meeting Employees | 16,928 | sf GLA | 1.20 | 50% | 100% | 0.60 | ksf GLA | 1.33 | 50% | 100% | 0.67 | ksf GLA | 40% | 100% | 4 | 100% | 100% | 12 |
| | | | | | | | Additiona | I Land Use | S | | | | | | | | | |
| Members Club | 500 | Members | 0.06 | 100% | 100% | 0.06 | Members | 0.06 | 100% | 100% | 0.06 | Members | 90% | 100% | 27 | 90% | 100% | 27 |
| Employee | | | 0.00 | 100% | 100% | 0.00 | | 0.00 | 100% | 100% | 0.00 | | 100% | 100% | - | 100% | 100% | - |
| | | | | | | | | | | | | | Custom | er/Visitor | 155 | Cus | tomer | 157 |
| | | | | | | | | | | | | | Employe | e/Resident | 23 | Employe | ee/Resident | 27 |
| | | | | | | | | | | | | | T | otal | 178 | T | otal | 184 |

Peak Month Daily Parking Demand by Hour (Weekday)



Peak Month Daily Parking Demand by Hour (Weekend)



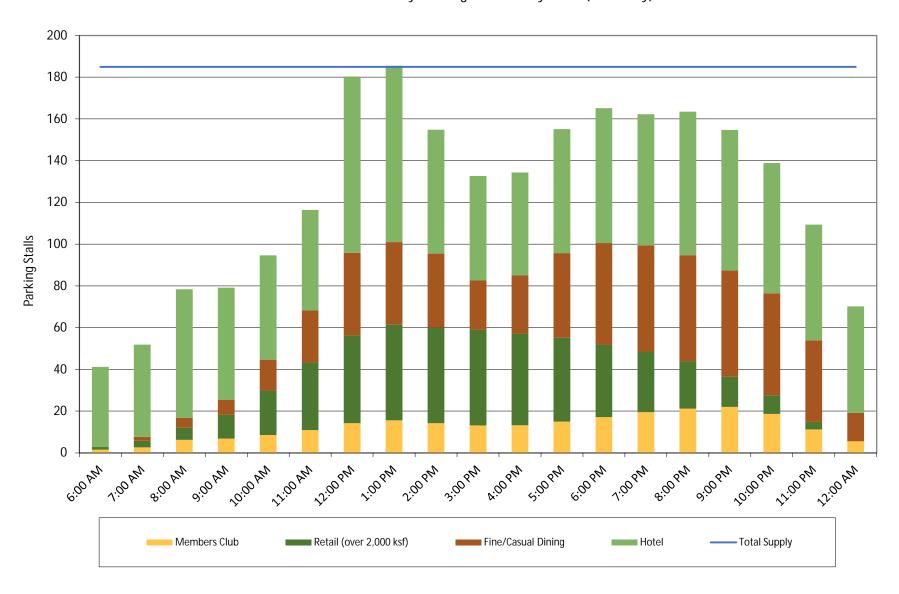
Copyright © 2020 All rights reserved. The Urban Land Institute, International Council of Shopping Centers, and National Parking Association.

Project: Cheval Blanc Hotel, Beverly Hills

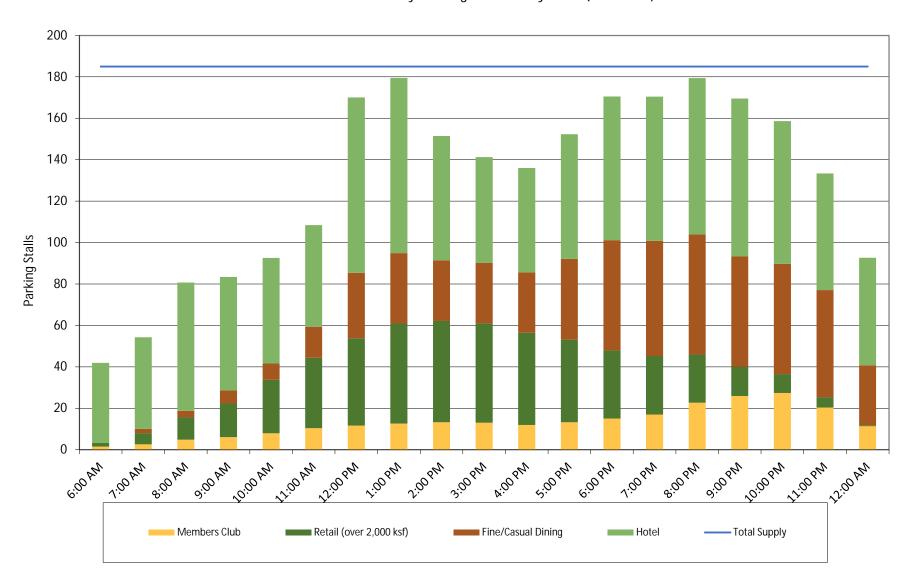
Description: Scenario B

| | | | | | | Share | ed Parking [| Demand Si | ummary | | | | | | | | | |
|--|-----------------------|---------|---------|---------|------------------|---------|--------------|------------|---------|------|---------|-----------|----------------------|-----------|-----------|-------------------|------------|-----------|
| Peak Month: LATE DECEMBER Peak Period: 1 PM, WEEKDAY | | | | | | | | | | | | | | | | | | |
| Land Use | Project Data | | Weekday | | | | | Weekend | | | | | Weekday | | | Weekend | | |
| | | | Base | Driving | Non- | Project | Unit For | Base | Driving | Non- | Project | Unit For | Peak Hr | Peak Mo | Estimated | Peak Hr | Peak Mo | Estimated |
| | | | Ratio | Adj | Captive Ratio | Ratio | Ratio | Ratio | Adj | | Ratio | Ratio - | Adj | Adj | Parking | Adj | Adj | Parking |
| | Quantity | Unit | | | | | | | Auj | | Ratio | | 1 PM | te Decemb | Demand | 1 PM | ite Decemb | Demand |
| Retail | | | | | | | | | | | | | | | | | | |
| Retail (over 2,000 ksf) | 24,976 | sf GLA | 2.90 | 75% | 80% | 1.74 | ksf GLA | 3.20 | 75% | 80% | 1.92 | ksf GLA | 100% | 85% | 37 | 95% | 85% | 39 |
| Employee | | | 0.70 | 50% | 100% | 0.35 | | 0.80 | 50% | 100% | 0.40 | | 100% | 95% | 9 | 100% | 95% | 10 |
| Food and Beverage | | | | | | | | | | | | | | | | | | |
| Fine/Casual Dining | 8,166 | sf GLA | 13.25 | 50% | 80% | 5.30 | ksf GLA | 15.25 | 50% | 80% | 6.10 | ksf GLA | 75% | 95% | 31 | 55% | 95% | 26 |
| Employee | | | 2.25 | 50% | 100% | 1.13 | | 2.50 | 50% | 100% | 1.25 | | 90% | 100% | 9 | 75% | 100% | 8 |
| | Hotel and Residential | | | | | | | | | | | | | | | | | |
| Hotel-Business | | keys | 1.00 | 59% | 100% | 0.59 | key | 1.00 | 69% | 100% | 0.69 | key | 55% | 55% | - | 55% | 55% | - |
| Hotel-Leisure | 115 | keys | 1.00 | 33% | 100% | 0.33 | key | 1.00 | 33% | 100% | 0.33 | key | 65% | 100% | 25 | 65% | 100% | 25 |
| Hotel Employees | 115 | keys | 0.15 | 50% | 100% | 0.08 | key | 0.15 | 50% | 100% | 0.08 | key | 100% | 100% | 9 | 100% | 100% | 9 |
| Restaurant/Lounge | 16,928 | sf GLA | 6.67 | 47% | 80% | 2.51 | ksf GLA | 7.67 | 40% | 80% | 2.45 | ksf GLA | 100% | 95% | 40 | 100% | 95% | 40 |
| Restaurant/Meeting Employees | 16,928 | sf GLA | 1.20 | 50% | 100% | 0.60 | ksf GLA | 1.33 | 50% | 100% | 0.67 | ksf GLA | 100% | 100% | 11 | 100% | 100% | 12 |
| | | | | | | | Additiona | I Land Use | S | | | | | | | | | |
| Members Club | 500 | Members | 0.02 | 100% | 100% | 0.02 | Members | 0.03 | 100% | 100% | 0.03 | Members | 60% | 100% | 6 | 19% | 100% | 3 |
| Employee | | | 0.02 | 100% | 100% | 0.02 | | 0.02 | 100% | 100% | 0.02 | | 80% | 100% | 10 | 80% | 100% | 10 |
| | | | | | | | | | | | | | Customer/Visitor 140 | | | Customer | | 132 |
| | | | | | | | | | | | | | Employee/Resident 46 | | 46 | Employee/Resident | | 47 |
| | | | | | | | | | | | | Total 185 | | | Total | | 180 | |

Peak Month Daily Parking Demand by Hour (Weekday)



Peak Month Daily Parking Demand by Hour (Weekend)





Appendix G – ULI Shared Parking Time-Of-Day Parking Demand for Events

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Project: Cheval Blanc Hotel, Beverly Hills

Description:

| | | | | | | Share | d Parking D | emand Si | ummary | | | | | | | | | |
|--|---------------------------------|----------|---------|----------------|-----------------|---------|-------------------|---------------|--------|-----------------------|-------|----------|----------------------|------------|-----------|----------|------------|-----------|
| Peak Month: LATE DECEMBER Peak Period: 1 PM, WEEKDAY | | | | | | | | | | | | | | | | | | |
| | Project Data Base Quantity Unit | | Weekday | | | | | Weekend | | | | | Weekday | | | Weekend | | |
| Land Use | | | Dana | Driving Adj | Non- Captive | Project | Unit For Ratio | Base Ratio | | Non- Captive Proje | D | | Peak Hr | Peak Mo | Estimated | Peak Hr | Peak Mo | Estimated |
| | | | | | | | | | | | Ratio | | Adj | Adj | Parking | Adj | Adj | Parking |
| | | | Katio | Auj | Ratio | | | | Auj | Ratio | Ratio | | 1 PM | te Decemb | Demand | 1 PM | ite Decemb | Demand |
| Retail | | | | | | | | | | | | | | | | | | |
| Retail (over 2,000 ksf) | 24,976 | sf GLA | 2.90 | 75% | 80% | 1.74 | ksf GLA | 3.20 | 75% | 80% | 1.92 | ksf GLA | 100% | 85% | 37 | 95% | 85% | 39 |
| Employee | | | 0.70 | 50% | 100% | 0.35 | | 0.80 | 50% | 100% | 0.40 | | 100% | 95% | 9 | 100% | 95% | 10 |
| Food and Beverage | | | | | | | | | | | | | | | | | | |
| Fine/Casual Dining | 5,666 | sf GLA | 13.25 | 50% | 80% | 5.30 | ksf GLA | 15.25 | 50% | 80% | 6.10 | ksf GLA | 75% | 95% | 22 | 55% | 95% | 18 |
| Employee | | | 2.25 | 50% | 100% | 1.13 | | 2.50 | 50% | 100% | 1.25 | | 90% | 100% | 6 | 75% | 100% | 6 |
| Hotel and Residential | | | | | | | | | | | | | | | | | | |
| Hotel-Leisure | 115 | keys | 1.00 | 33% | 100% | 0.33 | key | 1.00 | 33% | 100% | 0.33 | key | 65% | 100% | 25 | 65% | 100% | 25 |
| Hotel Employees | 115 | keys | 0.15 | 50% | 100% | 0.08 | key | 0.15 | 50% | 100% | 0.08 | key | 100% | 100% | 9 | 100% | 100% | 9 |
| Restaurant/Lounge | 2,419 | sf GLA | 6.67 | 47% | 80% | 2.51 | ksf GLA | 7.67 | 40% | 80% | 2.45 | ksf GLA | 100% | 95% | 6 | 100% | 95% | 6 |
| Restaurant/Meeting Employees | 2,419 | sf GLA | 1.20 | 50% | 100% | 0.60 | ksf GLA | 1.33 | 50% | 100% | 0.67 | ksf GLA | 100% | 100% | 2 | 100% | 100% | 2 |
| Additional Land Uses | | | | | | | | | | | | | | | | | | |
| Member's Club (Wellness Center Only) | 12 | visitors | 1.00 | 100% | 100% | 1.00 | visitors | 1.00 | 100% | 100% | 1.00 | visitors | 0% | 100% | | 0% | 100% | |
| Event Type A | 150 | visitors | 0.50 | 100% | 100% | 0.50 | visitors | 0.50 | 100% | 100% | 0.50 | visitors | 100% | 100% | 75 | 100% | 100% | 75 |
| Event Type B | 75 | visitors | 0.50 | 100% | 100% | 0.50 | visitors | 0.50 | 100% | 100% | 0.50 | visitors | 100% | 100% | 38 | 100% | 100% | 38 |
| Event Type C | 50 | visitors | 0.50 | 100% | 100% | 0.50 | visitors | 0.50 | 100% | 100% | 0.50 | visitors | 100% | 100% | 25 | 100% | 100% | 25 |
| | | | | | | | | | | | | | Customer/Visitor 228 | | | Customer | | 226 |
| | | | | | | | | | | | | | Employe | e/Resident | 25 | Employe | e/Resident | 26 |
| | | | | | | | | | | | | | T | otal | 252 | T | otal | 251 |





January 18, 2022

Mr. Masa Alkire, AICP Principal Planner Department of Community Development, Planning Division City of Beverly Hills 455 North Rexford Drive Beverly Hills, California 90210

RE: Updated Responses to April 10, 2020 Beverly Hills Department of Community Planning Initial Review Comment Letter on Cheval Blanc Hotel Specific Plan Project (PL2000138)

Dear Mr. Alkire,

This letter provides updated responses to the traffic and/or access-related comments contained in the City of Beverly Hills April 10, 2020 Department of Community Planning initial review letter regarding the proposed Cheval Blanc Hotel Specific Plan Project at 468 North Rodeo Drive; a copy of the Department's letter (including applicable supporting comments from Fehr & Peers, the City's contract traffic engineering consultant) is provided in the attachments. Specifically, this document addresses comments noted under the "Planning and Zoning Comments" heading ("Project Description Attachments" subheading, page 6) of the City's letter, including a request to study the traffic conditions in the north-south alley currently bisecting the project site (proposed to be modified by the project), as well as the effects of the project's access and construction activities on the alley operations. The following discussions also incorporate revisions to the project itself in response to comments received on the City's Draft Environmental Impact Report ("DEIR").

Alley Study

The subject alley is an approximately 20-foot wide, one-way southbound facility located mid-block between Rodeo Drive and Beverly Drive that connects South Santa Monica Boulevard on the north with Wilshire Boulevard on the south, as shown in Figure 1. Within the immediate vicinity of the proposed project, the alley provides access to loading and employee/customer parking areas for a variety of commercial and retail businesses fronting along both Rodeo Drive and Beverly Drive between South Santa Monica Boulevard and Brighton Way, along with an exit-only driveway for a private/public parking garage at 421 North Beverly Drive. The subject project proposes to vacate the portion of the alley adjacent to its currently individual parcels (in order to merge the separate project sites) and relocate the alley entrance to Beverly Drive, as indicated in Figure 2. As part of the City's initial review comments on the proposed project, Fehr & Peers noted that a study of the current (and anticipated future) operations of the alley should be provided to identify whether the proposed alley reconfiguration would impact other businesses using the alley.





FIGURE 1

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PROJECT SITE AND EXISTING ALLEY LOCATION





FIGURE 2

PROJECT SITE LAYOUT AND ALLEY ACCESS RECONFIGURATION

IRSCH © REEN

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Letter to Mr. Masa Alkire January 18, 2022 Page 4 of 12

Alley Traffic Volumes

The amount of traffic currently using the alley was identified through a series of 24-hour counts conducted at the alley's South Santa Monica Boulevard entrance in April and May of 2019, including a total of eight weekdays, two Saturdays, and two Sundays (a total of 12 survey days). These counts represent typical weekday and weekend conditions during weeks with no holidays or other notable special events, with area schools and businesses exhibiting normal operations, and seasonal weather conditions (temperatures, rainfall, etc.) throughout the count period.

The results of the counts indicate that on weekdays, the alley exhibited an eight-day average of approximately 718 total vehicles per day, including a maximum of about 801 vehicles per day. The majority (about 67 percent) of these vehicles entered the alley via an eastbound right turn from South Santa Monica Boulevard, with the remainder entering from the westbound direction via a left turn move. Further, most of the observed alley traffic consisted of typical automobiles (654 vehicles per day, or about 91 percent) and single-unit (SU-30 or SU-40) delivery trucks (58 vehicles per day, or about eight percent), with garbage trucks and motorcycles making up the rest of the traffic (each averaging three vehicles per day, or about 0.5 percent of the total).

These daily averages are generally maintained during each of the three weekday "peak periods" (morning, mid-day, and afternoon/evening) examined for the purposes of this study. Specifically, during the AM peak hour (which typically occurred within the period from 8:30 AM to 9:45 AM), the alley accommodated an average of 110 total vehicles (with a maximum of 123 vehicles), including 103 automobiles (approximately 94 percent), six delivery trucks (roughly five percent), and one motorcycle. During the mid-day peak hour (which varied widely for each individual day, but with all occurring between 12:00 noon and 2:00 PM), an average of about 59 total vehicles (maximum of 75 vehicles) accessed the alley, including 52 automobiles (about 88 percent) and seven delivery trucks (about 12 percent), while during the weekday afternoon/evening peak hour (which also varied by day, although all occurred during the period between 3:00 PM and 5:15 PM), an average of about 48 total vehicles (including a maximum of 63 vehicles) entered the alley, including 43 automobiles (about 90 percent) and five delivery trucks (about 10 percent). As with the overall daily conditions, most of the peak hour alley traffic (between about 56 and 73 percent) entered via a right turn from South Santa Monica Boulevard.

Overall traffic in the alley on weekends was substantially lower than during the weekdays, with two-day averages of about 597 total vehicles per day (maximum of 610 total vehicles per day) on Saturdays, and of about 279 total vehicles per day (maximum of 283 vehicles per day) on Sundays. Again, most of this traffic (around 70 percent for each day) entered the alley via a right turn from South Santa Monica Boulevard, and was comprised primarily of typical automobiles, including about 570 vehicles per day (about 95 percent) on Saturdays, and about 274 vehicles per day (about 98 percent) on Sundays. The remaining average daily Saturday traffic consisted primarily

Letter to Mr. Masa Alkire January 18, 2022 Page 5 of 12

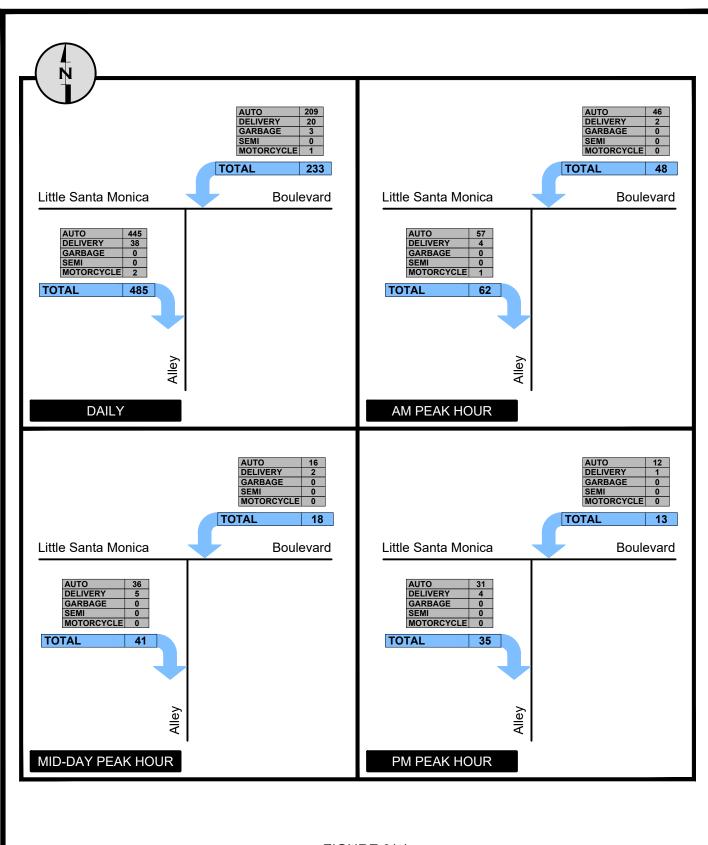
of single-unit delivery trucks (23 vehicles, or approximately four percent of the total), although three garbage trucks and one semi-trailer truck were also observed. However, while the averages suggest that a semi-trailer truck could be expected to access the alley on any typical Saturday, it is of note that only one semi-trailer truck used the alley during the 12-day observation period, on Saturday May 11, 2019 at 11:30 AM. On Sundays, in addition to the 274 daily automobiles, an average of five single-unit delivery trucks per day were observed (about two percent of the total daily traffic for that day); no other types of vehicles utilized the subject alley on Sundays.

During the AM peak hour on Saturday (from 8:45 AM to 9:45 AM for both count days), the alley exhibited an average total traffic demand of about 98 vehicles (and a maximum of 100 vehicles), including 96 automobiles (approximately 98 percent), and two delivery trucks (about two percent), while during the mid-day peak hour (between 12:00 noon and 1:00 PM for both observed days), an average (and maximum) of about 61 total vehicles utilized the alley, including 58 automobiles (about 95 percent) and three single-unit delivery trucks (about five percent). During the Saturday afternoon/evening peak hour (which occurred from 3:00 PM to 4:00 PM on both of the count days), an average of approximately 53 total vehicles (with a maximum of 59 vehicles) used the alley, including 50 automobiles (about 94 percent) and three delivery trucks (about six percent). Again, the majority of the Saturday peak hour traffic (between about 58 and 74 percent) entered the alley via an eastbound right turn from South Santa Monica Boulevard.

Finally, on Sunday, during the AM peak hour (occurring generally between 8:00 AM and 9:30 AM), an average of approximately 14 total vehicles (maximum of 16 total vehicles) utilized the alley, including 13 automobiles (about 93 percent), and one delivery truck (about seven percent). During the Sunday mid-day peak hour (generally between 12:00 noon and 1:15 PM), an average (and maximum) of approximately 25 total vehicles, including 24 automobiles (about 96 percent) and one delivery truck (about four percent) used the alley, along with an average (and maximum) of about 38 total vehicles (all automobiles) during the Sunday afternoon/evening peak hour (which occurred during the overall time period between 3:15 PM to 4:45 PM). As with both the weekday and Saturday conditions described previously, most of the Sunday peak hour traffic (about 64 to 72 percent) entered the alley via a right turn from South Santa Monica Boulevard.

The average alley traffic volumes for the weekday daily (24-hour) and various peak hour periods are shown in Figure 3(a), while the average alley volumes during these same periods are shown for Saturday and Sunday conditions in Figures 3(b) and 3(c), respectively. The alley traffic counts for each of the individual surveyed days are provided in the attachments to this document.

As identified previously in Figure 2, the project's proposed relocation of the alley entrance from its existing location to Beverly Drive will require that vehicles currently making the right turn into the alley instead continue eastward on South Santa Monica Boulevard to Beverly Drive, where they would then turn right onto Beverly Drive in order to access the new alley entrance. However,



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CHEVAL BLANC HOTEL (BEVERLY HILLS) \ ALLEY VOLUMES (WEEKDAY)

FIGURE 3(a)

EXISTING ALLEY TRAFFIC VOLUMES WEEKDAY (8-DAY AVERAGE)

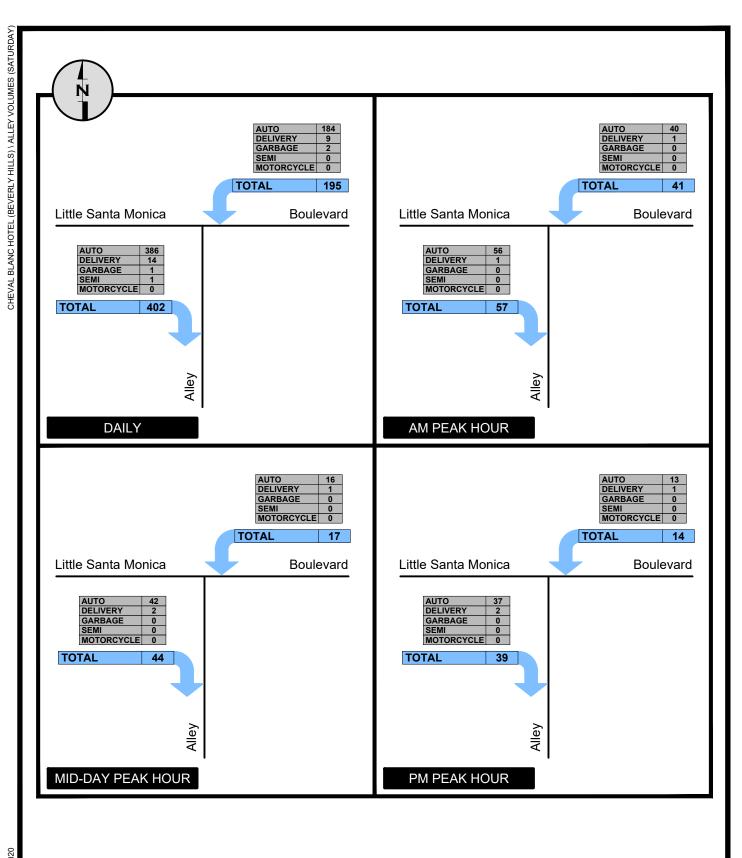
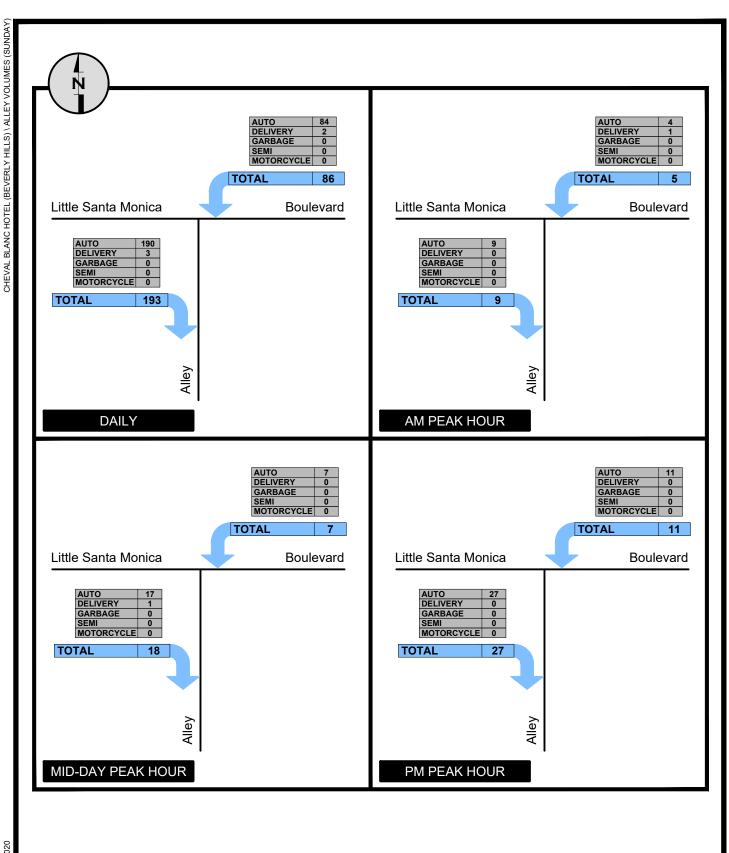


FIGURE 3(b)

EXISTING ALLEY TRAFFIC VOLUMES SATURDAY (2-DAY AVERAGE)

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Hirsch/Green Transportation Consulting, Inc.

FIGURE 3(c)

EXISTING ALLEY TRAFFIC VOLUMES SUNDAY (2-DAY AVERAGE)

Letter to Mr. Masa Alkire January 18, 2022 Page 9 of 12

while this "redistribution" of the eastbound traffic entering the alley would likely increase the number of vehicles travelling through the intersection of South Santa Monica Boulevard and Beverly Drive, as described earlier, any such additional traffic would be relatively nominal, with a maximum of about 72 vehicles per hour during any of the typical weekday "peak hour" periods (AM, Mid-day, PM), and a maximum of approximately 65 vehicles per hour during any of these time periods on typical weekends (specifically, on Saturdays). This potential increase in traffic at the subject intersection would equate to only about one or two new vehicles per signal cycle, assuming that none of the existing eastbound alley traffic diverts to other travel routes following the relocation of the alley entrance, and further, would be right turns, some of which could occur as a "right-turn on red" move when eastbound South Santa Monica Boulevard traffic is stopped.

The number of vehicles passing through this intersection along the other approaches would be essentially unchanged, although they would exhibit somewhat different travel patterns (changing from southbound right turns to southbound through movements, from westbound through moves to westbound left turns, and eliminating the northbound left turn move). Therefore, the impacts of the proposed relocation of the alley entrance alone on the operations of the intersection of South Santa Monica Boulevard and Beverly Drive are expected to be minimal. Additionally, under the current configuration, large trucks (including both single-unit and semi-trailer trucks) entering the alley from the curb lane of eastbound South Santa Monica Boulevard must typically "swing wide" into the inboard eastbound lane (and potentially, into the westbound inboard lane and oncoming traffic) to make the turn without impacting the buildings on either side of the alley. As detailed later in this document, due to the wider curb lane (including on-street parking) on southbound Beverly Drive, such large trucks will be able to access the relocated alley entrance without encroaching into the adjacent (or oncoming) lane.

Alley Access and Operations

In addition to the relocation of the alley entrance, the proposed alley reconfiguration will require that vehicles using the alley make a 90-degree turn from the new east-west oriented portion of the alley (from Beverly Drive) in order to access the existing and unaffected north-south segment. As a result, additional evaluations were performed to assure that all of the various vehicle types observed accessing the alley could make this maneuver. As described earlier, the majority of the vehicles using the alley are typical automobiles (including light trucks, such as pickups and vans), although a number of larger single-unit delivery trucks and garbage trucks were also identified, along with one semi-trailer truck. Further, although not observed during the alley traffic counts, the reconfigured alley must also accommodate certain emergency vehicles, such as fire trucks.

Therefore, the turning movement evaluations were conducted for each type of vehicle that was either directly observed during the alley traffic counts or are anticipated to use the alley, including typical single-unit delivery trucks (SU-30 and SU-40), a semi-trailer truck (WB-40) of the size

Letter to Mr. Masa Alkire January 18, 2022 Page 10 of 12

typically used for urban area deliveries, a typical garbage truck, two types of fire/rescue trucks similar to or larger than are used by the City¹, and an "articulated" ladder truck per specifications provided by the Beverly Hills Fire Department. The results of these evaluations, which are based on the project's current ground floor plan (dated "December 9, 2021"), are shown graphically in the attachments, indicate that all of these vehicle types will be able to make the left turn from the relocated portion of the alley to the remaining segment with little or no difficulty. Therefore, the proposed reconfiguration of the alley would not limit its use by any of the observed vehicle types, and since the portions of the alley south of the project site will be unaffected by its development, no significant impact to the existing operations of the alley for its other users are anticipated.

Additionally, vehicular access to the alley will be provided at all times during construction of the proposed project, so that no disruption in alley service for the existing businesses to the south of the project site will occur. As detailed in the proposed project's construction management plan (submitted under separate cover), the construction of the project will occur in multiple phases, with the first phase(s) involving the demolition of the eastern half of the project site, currently occupied by the Paley Center for Media building and adjacent 449 Beverly Drive building, and the subsequent excavation of that area in order to construct the project's subterranean levels. Vehicular access to the alley from its existing access location on South Santa Monica Boulevard will be maintained throughout this portion of the project's construction activities. This phase will also include the construction of the new segment of the alley, between Beverly Drive and the existing alley, atop the subterranean levels. Once the new alley segment has been completed, it will be connected to the remaining north-south portion of the alley, and the existing entrance from South Santa Monica Boulevard (along with the portions of the alley north of the new segment) will be closed and ultimately removed during subsequent phases of the project's construction. Note that the connection of the new alley segment with the remainder of the existing alley may require a temporary and short-duration closure of all access to the alley, although it is expected that this procedure can be accomplished during late weekday or weekend evening hours (with permission from the City) when alley activity is nominal to minimize impacts to alley operations.

As a result, based on these evaluations, the proposed alley reconfiguration will not affect access for any of the vehicle types observed to use that facility, up to and including semi-trailer trucks. Therefore, since neither the physical configuration nor the operational conditions of the portions of the alley south of the project site will be affected, the proposed relocation of the alley entrance is not anticipated to result in any significant impacts to other (non-project) users of the alley.

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¹ The City of Beverly Hills Fire Department provided specifications for a Caterpillar C12 Urban Search and Rescue Vehicle ("USRV") [e-mail from Dept. Fire Chief J. Matsch, August 6, 2019]. The AutoTurn software used for evaluating turn movements does not include this vehicle. Therefore, turning movements are provided for the Zahnen Rescue Unit, which is two inches shorter in overall length, but with a 24" longer wheelbase, than the Caterpillar C12 USRV. In addition, turning movements are also provided for the Smeal Aerial RM 55-foot vehicle, which is 24" longer overall than the Caterpillar C12 USRV.

Letter to Mr. Masa Alkire January 18, 2022 Page 11 of 12

Alley Access to Proposed Project Loading Docks and Subterranean Parking

As also shown earlier in Figure 2, vehicular access to the proposed project's on-site loading bays will be provided from the relocated portion of the alley. Delivery vehicles using the loading bays will enter the project site from the (relocated) alley, and then back into either of the two bays; once the loading/unloading activity is completed, the trucks will then exit the site into the alley to continue southward through the remaining north-south portion of the alley toward Brighton Way. New studies of the operations of the updated configuration of the project's loading bay area indicated that a typical SU-30 (single-unit) delivery truck, which is the type and size of vehicle anticipated to serve the proposed project, can accomplish the maneuvers necessary to access either of the two loading bays entirely within the project site, although it is also anticipated that multiple vehicle moves (all of which will be accommodated wholly within the project site, as shown in the attached graphics) will be required in order to exit from "loading bay 1" (the interior of the two loading bays) when another vehicle is occupying the adjacent (outermost) "loading bay 2".

Additionally, while larger trucks are not anticipated to utilize the proposed project's loading bays, a supplemental evaluation of the potential use of an SU-40 (single-unit) truck was conducted. As detailed in the earlier alley study prepared by our firm (dated "April 20, 2020"), that evaluation identified that an SU-40 truck could also enter and exit both of the loading bays, although such vehicles could encounter difficulty (due to their additional length and larger turning radii) when attempting to enter "loading bay 2" or exit from "loading bay 1", particularly when another vehicle is occupying the adjacent loading bay. These moves would require that the SU-40 truck encroach into the alley (backing up into the alley to provide the correct orientation). Due to these issues, the project will prohibit the use of "loading bay 1" by SU-40 trucks, although the loading bays have been redesigned to allow for the use of "loading bay 2" by SU-40 trucks without requiring multiple vehicle movements or encroachment into the alley. Graphics illustrating the entry and exit maneuvers of an SU-30 truck for both loading bays, and an SU-40 truck for "loading bay 2", both for when the adjacent bay is being used, are provided in the attachments.

However, it is of note that the loading bays are located in an area that will be used by vehicles returning from the proposed project's subterranean parking levels to the on-site porte cochere. Therefore, while adequate vehicular access to the project's on-site loading bays will be provided, in order to avoid conflicts with both "internal" (on-site) project-related vehicular circulation and general (non-project) alley operations, it is recommended that all deliveries to the project site that require the use of the loading bays be scheduled during the "off-peak" periods of the day, when traffic activity at the project site and/or in the alley are expected to be reduced. Further, during the delivery truck loading dock "entering" and "exiting" maneuvers, attendants should be provided to direct and/or control project and alley traffic, to further ensure that potential conflicts do not occur, and that acceptable vehicular circulation in the alley on the project site is maintained.

Letter to Mr. Masa Alkire January 18, 2022 Page 12 of 12

Summary and Conclusions

The evaluations of the Cheval Blanc Hotel Specific Plan Project's proposed relocation of the alley entry from its current location on South Santa Monica Boulevard to Beverly Drive indicate that no significant impacts to vehicular access or to the operations of the alley are expected. Further, the location and operations of the project's loading bays will be acceptable, and will not significantly impact the alley, although it is recommended that the project schedule deliveries for off-peak times, and provide attendants to assure that conflicts with alley traffic do not occur.

Please review the preceding and attached information and analyses, and feel free to contact me if you have any questions or comments.

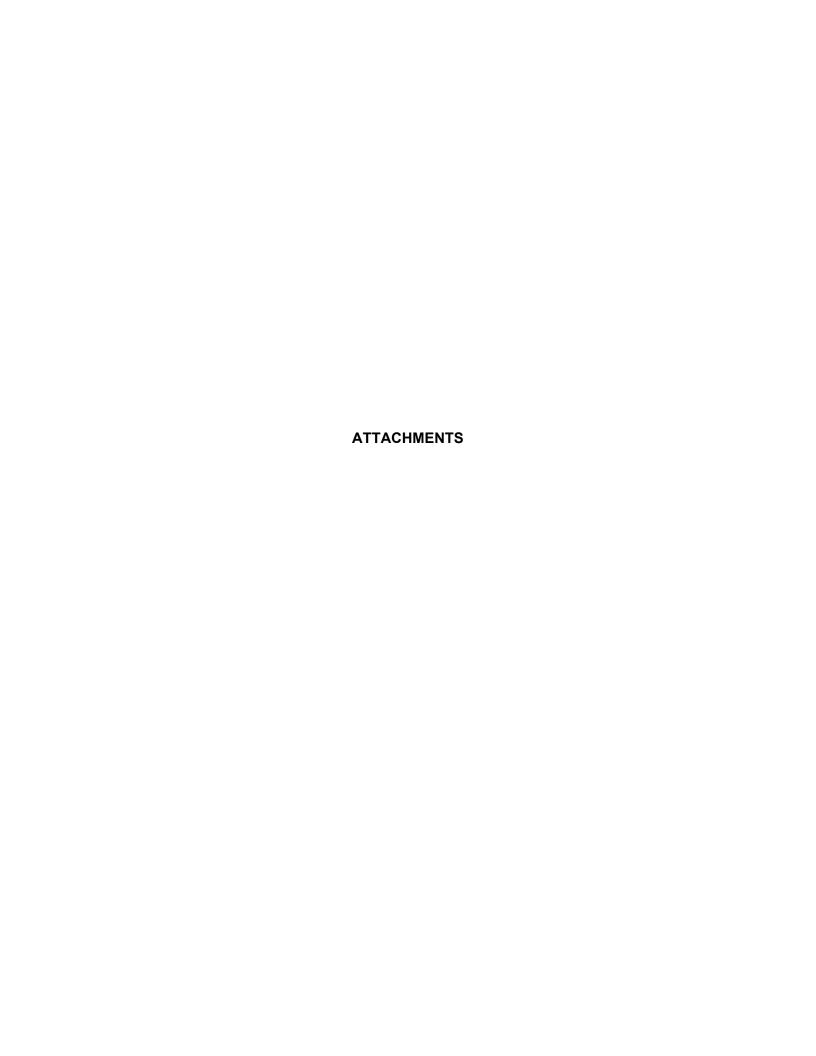
Sincerely,

Ron Hirsch, P.E.

Principal

Cc: Ms. Deborah Quick, Perkins Coie

Attachments



CITY OF BEVERLY HILLS DEPARTMENT OF COMMUNITY PLANNING
INITIAL REVIEW COMMENT LETTER (APRIL 10, 2020)
CHEVAL BLANC HOTEL SPECIFIC PLAN PROJECT (PL2000138)



April 10, 2020

Deborah E. Quick Morgan, Lewis & Bockius, LLP One Market, Spear Street Tower San Francisco, CA, 94105

RE: Initial Review of submitted application for the proposed Cheval Blanc Hotel Specific Plan Project (Specific Plan, Zoning Map and Zone Text Amendment, General Plan Amendment, Vesting Tentative Parcel Map, Encroachment Agreement, and Development Agreement) located at 468 North Rodeo Drive (PL2000138).

Dear Ms. Quick:

Staff has conducted a review of the above application, which was submitted to the City on March 12, 2020. At this time, the submitted application and plans have been deemed incomplete. Please note that due to the need for certain City staff to focus on providing essential City services during the on-going covid-19 pandemic, complete comments are not available from all City departments at this time. Responses to the following information requests and provided comments are required to continue evaluation of your application:

PLANNING AND ZONING COMMENTS

Project Plans

- 1) G001 PARCEL, NUMBERS AND SITE AREA: Also identify the total parcel size of 55,606 SF as an additional line item as this is the size of the project site if the parcel map is approved.
- 2) G001 FLOOR AREA AND FLOOR AREA RATIO: Add additional row "Gross Site Area – 55,606 SF". In the ON PLANS column provide the actual PROPOSED MAX. FAR TOTAL SITE calculation (4.06?), move the 4.2 FAR calculation to the SPECIFIC PLAN MAX. column. Also move the 3.9 PROPOSED MAX. FAR ABOVE GRADE figure to the SPECIFIC PLAN MAX. column, provide the actual FAR (3.78?) in the ON PLANS column.
- 3) G001- Add a table that provides floor area by use type: "Hotel" (breakdown by subcategory, such as "Member Club", "Public Restaurant", "Hotel Restaurant", "Spa/Wellness Center"), "Retail", "Exempt Space" and "Total". This table will be

- used as a reference in the future regulation amendments proposed in the Draft Specific Plan.
- 4) G001- BUILDING HEIGHT ZONING: delete ZONING from title. Retitle the text at the beginning of this section as "Current C-3 Height Requirement". Modify the table REQUESTED HEIGHT/STORIES into ON PLANS column and SPECIFIC PLAN MAX. column. Create rows in this table to clearly identify the maximum height allowed for the various portions of the building. See comments in the height section of the attached Specific Plan markup for further information.
- 5) G001- BUILDING HEIGHT: The "calculation of the height of the building" paragraph needs to be substantially rewritten, as the proposed height measurement for this Project does not match the cited BHMC section. See the comments on the Draft Specific Plan, and update this section. The list of allowable height exemptions can reference the appropriate section of Cheval Blanc Specific Plan instead of being listed in their entirety on the cover sheet.
- 6) G001- CODE PARKING ANALYSIS: Retitle text at beginning of this section as "Current Requirements". Retitle the table "Requested Parking Requirements". Rename columns "Provided Spaces On Plans" and "Specific Plan Required Spaces" and fill the table in with applicable information. Rename "Ratio" column "Required Ratio". Add rows to document parking credits the Project will utilize (in lieu parking, 50% hotel parking for retail credit, 15% project reduction credit). See comments in Draft Specific Plan regarding the 15% reduction credit. The credit rows should be filled in with negative numbers. The required and provided columns will then both have totals based on the sum of all rows included in the table.
- 7) G001- COMMERCIAL LOADING: Rename text at beginning of section "Current Requirements". Change end of section to "Requested Loading Requirements". Provide a table that includes columns: "Required Loading Space Type", "Required Loading Space Size", "Specific Plan Loading Space Requirement", and "Provided Loading Spaces".
- 8) G003- PLOT PLAN: Label location of height datum point. Provide elevation of height datum point. Label Pedestrian Plaza.
- 9) G003- PLOT PLAN: Clarify "Zero Lot Line No Setback" label. Is this a Specific Plan regulation, if so, include a setback regulation in the specific plan, and include a setback table on sheet G001 that identifies required and provided building setbacks. Identify the actual building distance from the lot line on the plot plan. There appears to be space between the lot line and the proposed building at both locations labeled "Zero Lot Line, No Setback".
- 10)G004- SITE CROSS SECTION: On each section, provide depth measurements from the ground surface to the top of the underground encroachments. The depth

- of these encroachments must meet or exceed the depth requirement proposed in the Draft Specific Plan (10 feet).
- 11)G004- SITE CROSS SECTION: Indicate the height datum elevation as a line across each elevation. Building height measurement should originate from this line. Provide a building height envelope line that visually represents the requested maximum building heights that are included in the Draft Specific Plan.
- 12)A101 to A103- BASEMENT LEVELS: Provide directional indicators for one way and two way drive aisles; provide dimension for drive aisle widths (one way and two way); on each sheet provide measurements for typical stall sizes for standard spaces, tandem spaces, compact spaces, and loading bays; provide measurements indicating additional required clearances from obstructions, such as building columns; label each tandem stall; provide ramp slope information for both transition slopes and main slopes.
- 13)A101 to A103- BASEMENT LEVELS: Revise the PARKING SUMMARY table on each sheet to identify tandem spaces on a per stall basis. This will double the number of spaces. This will allow the table to sum correctly and better mesh with the regulations requested in the draft Specific Plan.
- 14)A101 to A103- BASEMENT LEVELS: Provide electric vehicle charging information on applicable levels. The Green Building Code requires that a certain number of vehicle charging stations be provided. In addition vehicle charging was identified as a project feature in Section 4.9 of the draft Specific Plan.
- 15)A103- B1: Identify location of bicycle parking and bicycle amenities compliant with the Green Building Code and Sections 4.4.D and 4.9 of the draft Specific Plan.
- 16)A103- B1: The back-up area for Loading Bay 1 does not appear to be compliant with the loading space access requirements of 4.4.C. There appears to be a conflict with the most eastern parallel space.
- 17)A111- A192 All floor plans: Provide setback distances of the structure from property lines. At the ground level it appears that the building is setback from the southern interior property lines. Upper levels of the building are stepped back from the property line, provide information on those step back distances.
- 18)A111- GROUND LEVEL: Include directional information on vehicle drive aisles and ramps, provide width of drive vehicle drive aisles. Provide slope information for ramps.
- 19)A111- GROUND LEVEL: The configuration of the two truck loading bays appears to conflict with the draft Specific Plan's minimum drive aisle requirement for one way traffic.

- 20) CIRCULATION COMMENT: Provide a separate exhibit that provides turning radius information (AutoTURN) for vehicles that could access the site, such as identified delivery vehicle types, emergency vehicles and standard passenger vehicles.
- 21)A111- GROUND LEVEL: Label taxi/ride share spaces. Provide dimensions for all loading/drop-off and valet vehicle spaces in the motor court.
- 22)A121- SECOND LEVEL: Provide more detailed information regarding the dimensions and configuration of the Porte Cochere, as this sheet is referenced in draft Specific Plan Section 4.3 as the control on the size and attachment of this feature.
- 23) A151- 5th LEVEL: Provide height of glass guardrail and landscaped planter box located on guestroom balconies, provide height of operable awning.
- 24)A161- 6th LEVEL: Provide height for the following features: cabana shade structures, main shade structure, acoustic barrier, and exterior rooftop bar.
- 25)A171- 7th LEVEL: Provide building step back measurements; provide height of acoustic barrier, glass guardrail, and operable awnings on guestroom balconies.
- 26)A181- 8th LEVEL: Provide building step back measurements: provide height of acoustic barrier, glass guardrail, and operable awnings on guestroom balconies.
- 27) A191- 9th LEVEL: Provide building step back measurements: provide height of acoustic barrier, glass guardrail, planters for landscaping, trellis, shade structure, and operable awnings on guestroom balcony.
- 28)A192- LOW ROOF PLAN: Provide distance of mechanical enclosure from property lines. Provide height of screen wall.
- 29)A193- HIGH ROOF PLAN: Provide height of rooftop features.
- 30)ALL FLOOR AREA DIAGRAMS: Provide a floor area total for each of the use types that are color coded on each diagram sheet. Add an additional sheet that provides a table that tallies the floor area identified on each level. This new sheet should match the information in the new table requested on G001 (see Comment 3 above). Create a separate Outdoor Areas category, do not combine it with exempt space (MEP, Cores, shafts). Provide separate calculations for outdoor dining areas and other outdoor space. On each sheet provide the area of each elevator lobby exclusion.
- 31)ALL ELEVATIONS AND SECTIONS: Add the height datum as a line across the elevation. Provide a building height envelope that indicates the maximum allowable heights of the building. Include rooftop features on all elevations and indicate the height of the rooftop features. Include measurement on sections

identifying the depth of the portions of Level B2 that project beyond the property line.

Project Description

- 1) Provide more information on the Private Club use. This Project Description discussion should inform the regulations that you add to the draft Specific Plan that are applicable to the Private Club. The operation of the club within the hotel facilities, hours of operation, membership and guest policy should all be addressed. Questions include: the maximum number of members, the maximum occupancy of the club, the number of allowable guests per member, how will events be held at the club, and how does the lobby entrance on Beverly drive operate for pedestrians and vehicles? The operation of the Private Club could inform parking demand and should be directly addressed in the parking demand analysis.
- 2) Add information to the construction phasing discussion that address when the alley realignment will occur. This information will be an important consideration when construction related traffic impacts are analyzed. Also see the Public Works Engineering comments in this letter.
- 3) The appropriate recommended export hauling route will need to be discussed with the City's Traffic Engineer.
- 4) Provide specific in lieu parking information, including a copy of the covenant recorded against the property.
- 5) P.1 and P.5- Update to include proposed parcel size (1.275 acres), identify the 1.2 acres is exclusive of the alley area.
- 6) P.3- According to the plans the Private Club entrance is from Beverly Drive, not the alley.
- 7) P.8- Allowable construction hours in Beverly Hills start at 8 AM: BHMC 5-1-205. update Phase 1 information to reflect this requirement.
- 8) P.9- Provide a basis for the use of a 25% bulking/fluff factor.
- 9) P.11- Provide verification information that the cited privately owned sites have surplus parking available above the required parking for those sites, that can be used to provide construction employee parking for this Project.
- 10)P.11- Table 4: Why are operational hours identified as extended hours? That is a specific permit type in the BHMC that this Project does not require.

11) P.12- Application types: The application includes a submittal for a Vesting Tentative Parcel Map, not a Tract Map. Add Specific Plan to the list of requested entitlements.

Project Description Attachments

Exhibit 1 – Parking Demand Analysis

- 1) Please review the City's Traffic Engineer comments below and review the comments of the City's traffic peer reviewer (Attachment 2) regarding Parking Demand and the Motor Court.
- 2) Table 3 Parking Tabulation: identify in lieu parking as a row in the table and include the number of in lieu spaces as a negative number. Include a row in the table for the 15% reduction and include a negative number of spaces to account for the reduction. The 170 space total identified in this table does not match the project plans.

Exhibit 2- Valet Parking Management Plan

- 3) Please review the comments of the City's traffic peer reviewer (Attachment 2) regarding the valet parking plan.
- 4) Please provide more information as to when drive aisle stacked parking will be used. Is this intended for occasional use, such as during events or other functions of the Private Club?

Additional Traffic Peer Review Comments

5) Submit an Alley Study. Please review the City's traffic peer reviewer comments regarding submittal of an alley study for the Project.

Exhibit 3- Loading and Deliveries Narrative

- 6) The 12' by 35' spaces located on the ground level appear to conflict with the required drive aisle for vehicles exiting the ramp from B1, please clarify whether there is a conflict.
- 7) Provide information to describe an SU-30 truck and proof that this would be the largest delivery vehicle that would visit the site. Provide information whether the provided spaces are large enough for an SU-30 truck.
- 8) Provide a weekly or monthly estimated delivery schedule that includes both retail and hotel deliveries. It should include delivery type, size of vehicle used, and number of deliveries per week/month.

9) Please clarify the statement "if the City of Beverly Hills is hosting a large event". What does the statement refer to?

Exhibits 4 through 7

Thank you for providing two Historic Resource Assessments and building permit records for two of the sites. This information will be peer reviewed as part of the CEQA environmental review process.

10) Preliminary comment: The two assessments should analyze the National and California register criteria separately, and specifically with respect to the criteria relating to the significance of buildings that are less than 50 years old.

Exhibits 8 though 12

Thank you for providing the five geotechnical and seismic reports. These will be reviewed as part of the CEQA environmental review of the Project.

Draft Specific Plan

1) Please review the comments included in the attached marked-up Draft Specific Plan (Attachment 1) and resubmit a revised version of this document.

Draft Specific Plan Figures

- 1) Figure 3- EXISTING SITE CONDITIONS: Provide the boundaries of the existing parcels on the exhibit.
- Figure 5- MODIFIED ZONING AND LAND USE: The zoning and general plan maps will need to be updated to also include the M-PD-5 zoning and land use designation.
- 3) Figure 6- SPECIFIC PLAN LAND USE CONCEPTS: The east elevation identifies retail at the corner of North Beverly Drive and South Santa Monica Boulevard. This appears to be inaccurate.
- 4) Figure 7- BUILDING PLACEMENT: This figure is cited on page 7 of the Draft Specific Plan as controlling the size and configuration of the pedestrian plaza. If the figure is used for this purpose additional information needs to be included regarding the plaza, including: plaza dimensions, art location, as well as distances from obstructions for the art piece location, and ADA paths of travel in plaza.
- 5) Figure 8-SURROUNDING CIRCULATION: Provide the City's street classifications of the streets included in this exhibit.
- 6) Figure 9- SITE CIRCULATION: Provide directional information for alleys, on-site drive aisles and ramps.

- 7) Figures 10 to 12- PARKING PLANS: Update based on comments provided for the parking levels on the Plans.
- 8) Figure 13 to 18- UTILITY PLANS: These will need to be updated as more information becomes available.
- 9) Figure 29- AT-GRADE LOADING SPACES: Provide a separate exhibit to provide more detailed information regarding the utility yard and SCE capacitor yard. This exhibit should include screening information, access information, and provide information on the appearance from North Beverly Drive.
- 10) Figure 30- BUILDING HIEGHT: Identify 266' elevation as the height datum point for the project. Identify that all heights in exhibit are measured from the datum point. Label each height with the building feature that is measured (i.e. Rodeo Drive adjacent commercial, pool deck area, penthouse pool deck, etc.). Provide a table on this sheet that lists the height limitations of the Specific Plan.
- 11) Figure 31- OUTDOOR DINING GROUND FLOOR: Provide overall dimensions and area of outdoor dining area. Provide dimensions and area of outdoor dining on the public right of way and the outdoor dining on private property. Provide unobstructed width for adjacent sidewalk. Provide distance measurement between outdoor dining area and obstructions (i.e. tree well to the east)
- 12) Figure 32- OUTDOOR DINING LEVEL 6 & 7: Provide the area of each identified outdoor dining area, add a table that totals outdoor dining areas of the Project.
- 13) Figures 35 and 36- ELEVATIONS: Add a line that indicates project height datum. Provide height measurements to different features on each elevation. Identify the maximum height envelope. Show rooftop structures.
- 14) Figures 39 and 40- OUTDOOR LIVE ENTERTAINMENT: Identify height of acoustic barriers.

Vesting Tentative Parcel Map

- 1) Increase the differentiation between the lines used for "Existing Lot Line" and "Proposed Easement".
- 2) The area delineated by "Proposed Underground Building Limits" do not appear to match the configuration of underground parking as shown in the project plans.

Encroachment Permit (Subsurface Encroachment)

1) Add a request letter to the application requesting the encroachment and articulating why the encroachment is proposed.

- 2) Submit the encroachment fee (\$8490).
- 3) Submit the legal description and plat for the encroachment area for review.

Application

1) Attachment #4: Update to add Specific Plan and modify Vesting Tentative Tract Map to Vesting Tentative Parcel Map. Modify Encroachment Permit request to identify subsurface parking structure and remove above surface awnings.

Traffic Engineer Comments

- 1. Include an additional 1-FT width for parking spaces adjacent to obstructions/walls.
- 2. Include 26- foot-back up space for standard, compact, and tandem spaces.
- 3. Include "entrance" and "internal" ramp slopes.
- 4. Stack spaces shall meet the City's parallel parking standard guideline.
- 5. Check with Community Development/ Public Works regarding statement: "[t]en (10) feet below grade, parking spaces and aisles may extend under the public sidewalk up to the existing cub."
- 6. Reduce compacted parking limitation from 25% to 10%.
- **7.** Provide more information regarding "In Lieu Parking" to ensure those spaces are allocated to the uses permitted by BHMC Title 10, Article 33.

Public Works Department Comments

1) Please review the attached April 2, 2020 Memorandum from the Civil Engineering Division of the Public Works Department (Attachment 3).

<u>**Urban Designer Comments**</u>

<u>Historic Preservation and Preliminary Architectural Review Comments</u> <u>General Comments – Technical Reports</u>

- 1. At this time, materials related to the historic nature of the subject properties that has been provided by the applicant include:
 - a. Historic Resource Assessment Report for 461 North Beverly Drive (Paley Center)
 - b. Historic Resource Assessment Report for 468 North Rodeo Drive (formerly Brooks Brothers)
 - c. Overview building permit history

- In the environmental document that will be prepared for the proposed project (whether an EIR or other), a comprehensive overview of <u>all</u> of the subject properties' architectural descriptions and histories should be provided.
 - a. Please explain the decision to provide Historic Assessment Reports on two properties only. An analysis should be provided initially studying each property and explaining why further historic analysis was not required.
 - b. Permit history documentation has been provided loosely by the applicant. This information should be reviewed and synthesized by the applicant's historic consultant and included in the comprehensive overview.
 - c. Additional background on 461 North Beverly Drive (Paley Center) should also be provided to conclude the evaluation of the Master Architect's work with an understanding of any publications in which the structure had appeared and/or any design awards received (See Section 6, etc.).
- 3. Based on the scope of the project and the historic assessment reports provided, a peer review will be required, to be conducted by the City's historic consultant, Ostashay & Associates Consulting, for which a deposit is required to be remitted. Additional peer review will be required of the environmental document when it is prepared (i.e. EIR or other).

Architectural Comments – Preview – Drawing Set

 Consider closely vehicular circulation that extends beyond the building footprint and onto City streets, etc. A careful review of this component of the project, in conjunction with a traffic analysis, should be undertaken to ensure vehicular circulation does not negatively impact pedestrian circulation and busy existing traffic patterns at the site (south Santa Monica Boulevard and North Beverly Drive).

General Plan: CIR 1.4a Strive to maintain vehicle flow on City roadways and intersections. Congestion may be accepted, provided that provisions are made to improve the overall system and/or promote non-motorized transportation, such as bicycling and walking, as part of a development or City-initiated project. (Imp. 3.7)

General Plan: CIR 6.7 Multi-Modal Design. Require proposed development projects to implement site designs and on-site amenities that support alternative modes of transportation, and consider TDM programs with achievable trip reduction goals as partial mitigation for project traffic impacts. (Imp. 3.7)

General Plan: LU 2.8 Pedestrian-Active Streets. Require that buildings in business districts be oriented to, and actively engage the street through design features such as build-to lines, articulated and modulated façades, ground floor transparency such as large windows, and the limitation of parking entries directly on the street. Parking ingress and egress should be accessed from alleys where feasible. (Imp. 2.1)

General Plan: LU 11.4 Parking in Pedestrian-Oriented Districts. Require that driveways be minimized in pedestrian oriented commercial districts to avoid interruptions in the continuity of the pedestrian shopping experience, prioritizing driveway locations to side streets and alleys wherever feasible. (Imp. 2.1, 2.2)

2. In the current iteration of the design, the hotel lobby is sequestered within the massing at the ground level and accessible only through the vehicular circulation area off of South Santa Monica Boulevard. A pedestrian presence for the hotel may be considered off of the major City arterials, e.g., North Rodeo Drive to complement the proposed retail district and to afford general public access. Further consideration of a pedestrian friendly public entrance for the main programming of the project would also create a visual presence on the main street-facing elevation(s) and better inform the architecture as it addresses the public way.

General Plan: LU 11.3 Retail Street Frontages. Require that development and street frontages in districts containing retail uses be designed and developed to promote pedestrian activity including: (a) location and orientation of the building to the sidewalk; (b) transparency of and direct access to the ground floor elevation from the sidewalk; (c) articulation of street-facing elevations to promote interest and sense of quality; (d) inclusion of uses and public spaces that extend interior functions to the sidewalk such as cafes and plazas; and (e) use of pedestrian oriented signage and lighting. (Imp. 2.1, 2.2)

 Further consideration may also be given to creating a more uniquely contemporary architectural expression in design and materiality that responds to our own time, while imbuing the sense of timeless elegance suggested in the current design iteration.

General Plan: LU 2.4 Architectural and Site Design. Require that new construction and renovation of existing buildings and properties exhibit a high level of excellence in site planning, architectural design, building materials, use of sustainable design and construction practices, landscaping, and amenities that contribute to the City's distinctive image and complement existing development. (Imp. 2.2, 2.3)

General Plan: LU 11.2 Site Planning and Architectural Design. Require that commercial and office properties and buildings are planned and designed to exhibit a high level of site and architectural design quality and excellence. (Imp. 2.1, 2.2)

Plan Review Engineer (Building Safety) Comments

The purpose of this review is for a high-level preliminary conceptual review only. This is not a comprehensive plan review and or concept review. Other corrections may follow, after complete plans are submitted that are suitable for a thorough review.

Additional comments will follow when complete and fully dimensioned plans are submitted for thorough plan review.

- 1. Since the proposed project is a high-rise building, it shall comply with all the applicable requirements of Section 403 of 2019 CBC including but not limited to:
 - 403.3.3 Secondary water supply
 - 403.5.1 Remoteness of interior exit stairways
 - 403.5.2 Additional interior exit stairway
 - 403.6 Elevators (including enclosed elevator lobbies)
- 2. Please clarify whether nonseparated occupancies are used per Section 508.3 of 2019 CBC.
- 3. The building elements shall have a fire-resistance rating not less than that specified in Table 601 and exterior walls shall have a fire-resistance rating not less than that specified in Table 602. Where required to have a fire-resistance rating by Table 601, building elements shall comply with the applicable provisions of Section 703.2. The protection of openings, ducts and air transfer openings in building elements shall not be required unless required by other provisions of this code.
- 4. The maximum area of unprotected and protected openings permitted in an exterior wall in any story of a building shall not exceed the percentages specified in Table 705.8. Please provide required calculation to verify the maximum area of openings on the south and west (facing alley) sides of the building.
- 5. Please provide complete egress analyses for each space, story and entire building and show compliance with the corresponding sections in CH 10 of CBC:
 - Occupant Load (Section 1004)
 - Means of egress sizing (Section 1005)
 - Number of exits and exit access doorways (Section 1006); Egress from each space (1006.2) and egress from stories or occupied roof (1006.3)
 - Separation between required exits (1007.1)
 - Accessible means of egress (Section 1009)
 - Exit access travel distance (Section 1017) and common path of egress travel distance (Table 1006.2.1)
 - Exit discharge (Section 1028)
- 6. Exits shall discharge directly to the exterior of the building. The exit discharge shall be at grade or shall provide a direct path of egress travel to grade. The exit discharge shall not reenter a building. The combined use of Exceptions 1 and 2 shall not exceed 50 percent of the number and minimum width or required capacity of the required exits. (Section 1028)
 - The exits discharge the occupants to a location where it is still under the building. Please clarify.

- 7. Provide required number of exits in the Members Club area at third level, Spa in 4th and 5th levels and the restaurant in 6th floor.
- 8. Guest rooms shall comply with the accessibility requirements of CH. 11B and minimum number of guest rooms with mobility features and with communication features shall comply with Tables 11B-224.2 and 11B-224.4, respectively.
- 9. A complete and detailed construction means and method is required to elaborate all construction phases in detail including but not limited to shoring, excavation, haul route, tower crane installation, traffic control plan, etc.
- 10. Please clarify and elaborate fire department access to all sides of the building specially in the south, west and south west sides from the alley.
- 11. Please show a complete accessible path of travel from public way <u>AND</u> accessible parking spaces to all floors.
- 12. Please delineate long-term and short-term bicycle parking spaces with the minimum required vs provided bicycle parking stalls.
- 13. Please clarify and show the location and number of EVCS and accessible EVCS spaces on plans.

Should you have any questions regarding the above comments, please feel free to contact me at (310) 285-1135, or by email at malkire@beverlyhills.org.

| Sincerely, | |
|--------------------------------------|--|
| Masa Alkine | |
| Masa Alkire, AICP, Principal Planner | |

Attachments:

Attachment 1: Draft Specific Plan Mark-up Attachment 2: City Traffic Peer Reviewer Memo Attachment 3: Public Works Engineering Memo



CHEVAL BLANC INITIAL REVIEW OF SITE PLAN, SITE ACCESS AND PARKING

Specific Plan (March 12, 2020)

No transportation comments on Specific Plan; noted items below that relate to the other studies submitted to ensure consistency and clarity on project description.

Luxury hotel with private club, restaurant, lounge, bar and other appurtenant uses, ground floor and second floor retail:

- Up to 115 hotel rooms
- Member's club 7 KSF
- Restaurant 20 KSF
- Retail 24 KSF
- Parking 172 spaces
- Motor Court 9 pick-up/drop-off spaces (including 2 ridesharing spaces) + Truck loading may be used for pick-up/drop-off during peak event times
- Loading Two truck loading spaces (35-feet)

Existing uses consist of approximately 57 KSF retail and 65 parking spaces:

- Brooks Brothers 20,265 square feet and six surface parking spaces
- Celine 6,895 square feet and nine surface parking spaces
- Formerly the Paley Center for Media 23,351 square feet, five surface parking spaces and 45 underground parking spaces
- Three small retail shops (a beauty supply store, a jewelry store, and a pop-up shop) and a storage facility 6,276 square feet

Parking Analysis Study (March 10, 2020)

Parking Demand

- Empirical Data for Beverly Hills and Vicinity: Confirm that 3 Year Trend of Luxury Hotel
 Overnight Drive-In Rates (page 6) reflects Hotels in Beverly Hills
- The method for estimating hotel overnight demand and guest demand is reasonable (page 7):
 - o 38 overnight guest parking spaces (25% of demand)



- o 115 transient visitor parking spaces (74% of demand)
- o 153 total parking spaces
- Comments on Table 2 Parking Demand for the Cheval Blanc Project:
 - o Total visitor parking demand of 153 spaces is reasonable based on data provided
 - The reduction of 94 parking spaces due to lack of banquet facilities may be unreasonable due to the following:
 - The study is assuming that 94 of the 264 parking spaces at the Peninsula are devoted to public assembly (36% of parking) for a 2,630 square foot banquet facility and reducing the demand at the Cheval Blanc by 94 spaces since it doesn't have banquet facilities.
 - The transient parking demand of 75% of total guest parking accounts for some banquet use but the extent of banquets/special events is unclear. Since this is based on average daily demand, the extent of banquet/special event parking may be low when averaged throughout the week, and therefore subtracting 94 spaces from this demand may not be reasonable.
 - The amount of public assembly parking required per BHMC (1 space per 28 SF) for each of the hotels may be misleading; in comparing the BHMC code requirements to the total amount of parking provided at the hotels, the percentage of parking demand being assigned to the assembly space is 36% at the Peninsula (94 of 264 total spaces) and 83% at the Waldorf Astoria (261 of 314 total spaces).
 - The proposed hotel has a 7,000 square foot private club. The parking demand for the club is not factored into the parking demand and could be similar to, or potentially higher, than the 2,630 square feet of public assembly space at the Peninsula Hotel.
 - o It is unclear how the retail demand of 69 spaces is calculated.
 - Does the demand include retail and restaurant space?
 - Does the demand include the 50% credit for retail uses associated with hotels as noted in Table 1?
 - Does the demand factor in the in-lieu parking credits for existing retail uses?
 - No data is provided on how the employee parking demand of 30% of 120 employees per shift was developed.
- Comments on Table 3 Parking Tabulations from Cheval Blanc Specific Plan



- It appears that the only difference in parking demand between Table 1 and Table 3 is the 23 additional parking spaces required for BOH in Table 1. It is unclear why the BOH operations were not included in Table 3.
- General Comment on Parking Demand: It appears that if the BHMC requirements were applied to the project as shown in Table 1 and the study clearly accounted for the in-lieu parking credits of 49 spaces noted in Table 3, then the project would be able to show that it is meeting it's required parking demand through a combination of on-site supply and off-site in-lieu parking.

Motor Court

- Total demand is estimated at 11 spaces; project is proposing 9 spaces
- Total demand does not account for 7,000 sf private club
- In comparison to other hotels, the motor court appears to be sufficient to accommodate expected demand
- Point of clarification Does motor court provide vehicle egress from underground parking onto South Santa Monica Boulevard? If so, vehicle queuing capacity in the motor court for vehicles exiting onto South Santa Monica Boulevard should also be shown on the site plan.

Valet Parking Management Plan

- The overall assumptions and conclusions of the valet management plan are reasonable
- The valet study includes additional detail on the number of standard and tandem spaces that would be helpful to incorporate into the overall parking study; more clarification on who is using the standard vs. tandem spaces in comparison to their anticipated parking demand should be incorporated into the parking study.
- In addition, the valet study shows how additional parking demand can be met, if needed, through stacked parking in the drive aisles. Stacked parking would provide 64 additional parking spaces. Given that the project is not meeting BHMC parking requirements, it would be helpful for the parking study to note that demand during peak periods or special events associated with the private club could be accommodated through this additional stacked parking.



Additional Comments

- Request Alley Study An alley study should be prepared in consideration of the other existing uses that may be impacted by the realignment of the alley. The alley study should contain the following:
 - Existing daily traffic volumes entering alley from S. Santa Monica Boulevard and exiting alley onto Brighton Way (including AM and PM peak hour turning movement volumes so that directionality of travel to/from the alley is known)
 - o Number and type/size of trucks utilizing existing alley
 - Diagrams showing how trucks and emergency access vehicles will access realigned alley and turning movement radius for east/west to north/south alley transition
 - O Summary of any impacts to adjacent business resulting from alley realignment
 - Maintaining alley access during construction

CHEVAL BLANC HOTEL TRAFFIC VOLUME COUNTS ONE-WAY (SOUTHBOUND) ALLEY BETWEEN RODEO DRIVE AND BEVERLY DRIVE SOUTH SANTA MONICA BOULEVARD ENTRANCE



CHEVAL BLANC HOTEL PROJECT SUMMARY OF CURRENT WEEKDAY ALLEY TRAFFIC ACTIVITY ONE-WAY SOUTHBOUND ALLEY BETWEEN SANTA MONICA BOULEVARD (S) AND BRIGHTON WAY

| DAY/DATE Tuesday, April 23, 2019 Daily AM Peak Hour (8-45 - 9-45 AM) Mid-Day Peak Hour (12:00N - 1:00 PM) PM Peak Hour (3-30 - 4:30 PM) Monday, May 13, 2019 Daily AM Peak Hour (12:00N - 1:00 PM) PM Peak Hour (3-30 - 4:30 PM) Tuesday, May 14, 2019 Daily AM Peak Hour (3-30 - 4:30 PM) Tuesday, May 14, 2019 Daily AM Peak Hour (8-45 - 9-45 AM) Mid-Day Peak Hour (1:00 - 2:00 PM) Mid-Day Peak Hour (1:00 - 2:00 PM) | 483 61 37 36 369 57 25 24 440 65 | 30 1 4 8 39 3 8 4 44 5 | 0 0 0 0 0 | | | 516 62 41 45 409 61 33 | 208 45 17 10 164 41 9 | 13 2 0 1 1 23 4 | GARBAGE 3 2 0 | | | 226 49 17 | 691 106 54 | 43 3 4 | ALLEY VO GARBAGE 4 2 0 | | 4 0 0 | 742 111 58 |
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| Daily AM Peak Hour (8-45 - 8-45 AM) Mid-Day Peak Hour (12:00 N - 1:00 PM) PM Peak Hour (3-30 - 4-30 PM) Monday, May 13, 2019 Daily AM Peak Hour (12:00 N - 1:00 PM) PM Peak Hour (12:00 N - 1:00 PM) PM Peak Hour (3-30 - 4-30 PM) Tuesday, May 14, 2019 Daily AM Peak Hour (8-45 - 8-45 AM) Mid-Day Peak Hour (8-45 - 8-45 AM) Mid-Day Peak Hour (8-45 - 8-45 AM) Mid-Day Peak Hour (1:00 - 2-20 PM) PM Peak Hour | 61 37 36 369 57 25 24 440 65 35 | 1 4 8 39 3 8 4 | 0 0 0 0 0 0 | 0 0 0 | 0 0 1 1 1 1 | 62 41 45 409 61 | 45 17 10 164 41 | 2 0 1 | 2 0 | 0 | 0 | 49 17 | 106 | 3 | 0 | 0 | 0 | 111 |
| (8:45 - 9:45 AM) Mid-Day Peak Hour (12:00 N - 1:00 PM) PM Peak Hour (3:30 - 4:30 PM) Monday, May 13, 2019 Daily AM Peak Hour (8:45 - 9:45 AM) Mid-Day Peak Hour (12:00 N - 1:00 PM) PM Peak Hour (3:30 - 4:30 PM) Tuesday, May 14, 2019 Daily AM Peak Hour (8:45 - 9:45 AM) Mid-Day Peak Hour (1:00 - 2:00 PM) | 37 36 369 57 25 24 440 65 35 | 4 8 39 3 8 4 | 0 0 0 0 0 | 0 0 0 0 | 0 1 1 1 0 | 41 45 409 61 | 17 10 164 41 | 0 1 23 | 0 | 0 | 0 | 17 | | 4 | 0 | 0 | 0 | |
| Mid-Day Peak Hour (12:00 N - 1:00 PM) PM Peak Hour (3:30 - 4:30 PM) Monday, May 13, 2019 Daily AM Peak Hour (8:45 - 9:45 AM) Mid-Day Peak Hour (12:00 N - 1:00 PM) PM Peak Hour (3:30 - 4:30 PM) Tuesday, May 14, 2019 Daily AM Peak Hour (8:45 - 9:45 AM) Mid-Day Peak Hour (10:00 - 2:00 PM) | 369 57 25 24 440 65 | 39 3 8 4 | 0 0 0 0 0 | 0 0 0 | 1 1 1 0 | 45 409 61 | 10 164 41 | 23 | | | | | 54 | | | | | 59 |
| PM Peak Hour (3:30 - 4:30 PM) Monday, May 13, 2019 Daily AM Peak Hour (8:45 - 9:45 AM) Mid-Day Peak Hour (12:00 N - 1:00 PM) PM Peak Hour (3:30 - 4:30 PM) Tuesday, May 14, 2019 Daily AM Peak Hour (8:45 - 9:45 AM) Mid-Day Peak Hour (1:00 - 2:00 PM) PM Peak Hour | 369 57 25 24 440 65 35 | 39 3 8 4 | 0 0 0 0 | 0 0 | 1 1 0 | 409 61 | 164 41 | 23 | 0 | 0 | 0 | 11 | | | 0 | 0 | | 30 |
| Monday, May 13, 2019 Daily AM Peak Hour (8:45 - 9:45 AM) Mid-Day Peak Hour (12:00 N - 1:00 PM) PM Peak Hour (3:30 - 4:30 PM) Tuesday, May 14, 2019 Daily AM Peak Hour (8:45 - 9:45 AM) Mid-Day Peak Hour (1:00 - 2:00 PM) PM Peak Hour | 57 25 24 440 65 35 | 3 8 4 | 0 0 0 | 0 | 1 | 61 | 41 | | | | | 1.1 | 46 | 9 | 0 | - | 1 | 56 |
| Daily AM Peak Hour (8:45 - 9:45 AM) Mid-Day Peak Hour (12:00 N - 1:00 PM) PM Peak Hour (3:30 - 4:30 PM) Tuesday, May 14, 2019 Daily AM Peak Hour (8:45 - 9:45 AM) Mid-Day Peak Hour (1:00 - 2:00 PM) PM Peak Hour | 57 25 24 440 65 35 | 3 8 4 | 0 0 0 | 0 | 1 | 61 | 41 | | | | | | | | | | | |
| (8:45 - 9:45 AM) Mid-Day Peak Hour (12:00 N - 1:00 PM) PM Peak Hour (3:30 - 4:30 PM) Tuesday, May 14, 2019 Daily AM Peak Hour (8:45 - 9:45 AM) Mid-Day Peak Hour (1:00 - 2:00 PM) PM Peak Hour | 25 24 440 65 35 | 8 4 44 | 0 0 | 0 | 0 | | | 4 | 3 | 0 | 0 | 190 | 533 | 62 | 3 | 0 | 1 | 599 |
| Mid-Day Peak Hour (12:00 N - 1:00 PM) PM Peak Hour (3:30 - 4:30 PM) Tuesday, May 14, 2019 Daily AM Peak Hour (8:45 - 8:45 AM) Mid-Day Peak Hour (1:00 - 2:00 PM) PM Peak Hour | 24 440 65 35 | 4 | 0 | | | 33 | 9 | | 0 | 0 | 0 | 45 | 98 | 7 | 0 | 0 | 1 | 106 |
| PM Peak Hour (3:30 - 4:30 PM) Tuesday, May 14, 2019 Daily AM Peak Hour (8:45 - 9:45 AM) Mid-Day Peak Hour (1:00 - 2:00 PM) PM Peak Hour | 440 65 35 | 44 | 0 | 0 | 0 | | | 3 | 0 | 0 | 0 | 12 | 34 | 11 | 0 | 0 | 0 | 45 |
| Tuesday, May 14, 2019 Daily AM Peak Hour (8:45-9:45 AM) Mid-Day Peak Hour (1:00-200 PM) PM Peak Hour | 65 35 | | | | | 28 | 8 | 1 | 0 | 0 | 0 | 9 | 32 | 5 | 0 | 0 | 0 | 37 |
| Daily AM Peak Hour (8:45 - 9:45 AM) Mid-Day Peak Hour (1:00 - 2:00 PM) PM Peak Hour | 65 35 | | | | | | | | | | | | | | | | | |
| AM Peak Hour (8-45 - 9-45 AM) Mid-Day Peak Hour (1:00 - 2:00 PM) PM Peak Hour | 65 35 | | | 0 | 4 | 488 | 226 | 19 | 2 | 0 | 1 | 248 | 666 | 63 | 2 | 0 | 5 | 736 |
| Mid-Day Peak Hour (1:00 - 2:00 PM) PM Peak Hour | | | 0 | 0 | 2 | 72 | 50 | 0 | 0 | 0 | 1 | 51 | 115 | 5 | 0 | 0 | 3 | 123 |
| PM Peak Hour | 00 | 7 | 0 | 0 | 0 | 42 | 17 | 1 | 0 | 0 | 0 | 18 | 52 | 8 | 0 | 0 | 0 | 60 |
| (4:00 - 5:00 PM) | 30 | 0 | 0 | 0 | 0 | 30 | 16 | 0 | 0 | 0 | 0 | 16 | 46 | 0 | 0 | 0 | 0 | 46 |
| Manday Mar. 00 0010 | | | | | | | | | | | | | | | | | | |
| Monday, May 20, 2019 Daily | 380 | 35 | 0 | 0 | 2 | 417 | 187 | 16 | 3 | 0 | 2 | 208 | 567 | 51 | 3 | 0 | 4 | 625 |
| AM Peak Hour | 53 | 7 | 0 | 0 | 1 | 61 | 36 | 1 | 0 | 0 | 0 | 37 | 89 | 8 | 0 | 0 | 1 | 98 |
| (8:45 - 9:45 AM) Mid-Day Peak Hour | 29 | 5 | 0 | 0 | 0 | 34 | 14 | 3 | 0 | 0 | 0 | 17 | 43 | 8 | 0 | 0 | 0 | 51 |
| (12:00 N - 1:00 PM) PM Peak Hour | 28 | 1 | 0 | 0 | 0 | 29 | 8 | 1 | 0 | 0 | 0 | 9 | 36 | 2 | 0 | 0 | 0 | 38 |
| (4:15 - 5:15 PM) Tuesday, May 21, 2019 | | | | | | | | | | | | | | | | | | |
| Daily | 505 | 40 | 1 | 0 | 0 | 546 | 225 | 27 | 3 | 0 | 0 | 255 | 730 | 67 | 4 | 0 | 0 | 801 |
| AM Peak Hour (8:45 - 9:45 AM) | 51 | 4 | 1 | 0 | 0 | 56 | 53 | 3 | 0 | 0 | 0 | 56 | 104 | 7 | 1 | 0 | 0 | 112 |
| Mid-Day Peak Hour | 27 | 5 | 0 | 0 | 0 | 32 | 18 | 3 | 0 | 0 | 0 | 21 | 45 | 8 | 0 | 0 | 0 | 53 |
| PM Peak Hour (3:00 - 4:00 PM) | 30 | 4 | 0 | 0 | 0 | 34 | 12 | 2 | 0 | 0 | 0 | 14 | 42 | 6 | 0 | 0 | 0 | 48 |
| Wednesday, May 22, 2019 | | | | | | | | | | | | | | | | | | |
| Daily | 435 | 49 | 1 | 1 | 1 | 487 | 211 | 23 | 2 | 0 | 0 | 236 | 646 | 72 | 3 | 1 | 1 | 723 |
| AM Peak Hour (8:45 - 9:45 AM) | 53 | 5 | 0 | 0 | 0 | 58 | 50 | 1 | 0 | 0 | 0 | 51 | 103 | 6 | 0 | 0 | 0 | 109 |
| Mid-Day Peak Hour | 36 | 2 | 0 | 0 | 1 | 39 | 18 | 2 | 0 | 0 | 0 | 20 | 54 | 4 | 0 | 0 | 1 | 59 |
| PM Peak Hour (3:15 - 4:15 PM) | 23 | 5 | 0 | 0 | 0 | 28 | 9 | 1 | 0 | 0 | 0 | 10 | 32 | 6 | 0 | 0 | 0 | 38 |
| Thursday, May 23, 2019 | | | | | | | | | | | | | | | | | | |
| Daily | 485 | 38 | 0 | 0 | 0 | 523 | 230 | 24 | 2 | 0 | 0 | 256 | 715 | 62 | 2 | 0 | 0 | 779 |
| AM Peak Hour (8:30 - 9:30 AM) | 61 | 3 | 0 | 0 | 0 | 64 | 39 | 1 | 0 | 0 | 0 | 40 | 100 | 4 | 0 | 0 | 0 | 104 |
| Mid-Day Peak Hour | 46 | 3 | 0 | 0 | 0 | 49 | 20 | 1 | 0 | 0 | 0 | 21 | 66 | 4 | 0 | 0 | 0 | 70 |
| PM Peak Hour (3:00 - 4:00 PM) | 35 | 3 | 0 | 0 | 0 | 38 | 11 | 3 | 0 | 0 | 0 | 14 | 46 | 6 | 0 | 0 | 0 | 52 |
| Friday, May 24, 2019 | | | | | | | | | | | | | | | | | | |
| Daily AM Peak Hour | 462 56 | 30 4 | 0 | 0 | 2 | 494 61 | 219 50 | 15 1 | 0 | 0 | 3 | 239 52 | 681 106 | 45 5 | 0 | 0 | 5 2 | 733 113 |
| (8:45 - 9:45 AM) | 53 | 4 | 0 | 0 | 0 | 57 | | 0 | 0 | | 0 | 18 | | | | 0 | 0 | |
| Mid-Day Peak Hour (12:15 - 1:15 PM) | | | | | | | 18 | | | 0 | | | 71 | 4 | 0 | | | 75 |
| PM Peak Hour (3:00 - 4:00 PM) | 39 | 3 | 0 | 0 | 0 | 42 | 20 | 1 | 0 | 0 | 0 | 21 | 59 | 4 | 0 | 0 | 0 | 63 |
| Weekday Average (8 Days) | | | | | | | | | | | | | | | | | | |
| Daily | 445 | 38 | 0 | 0 | 2 | 485 | 209 | 20 | 3 | 0 | 1 | 233 | 654 | 58 | 3 | 0 | 3 | 718 |
| AM Peak Hour | 57 | 4 | 0 | 0 | 1 | 62 | 46 | 2 | 0 | 0 | 0 | 48 | 103 | 6 | 0 | 0 | 1 | 110 |
| Mid-Day Peak Hour PM Peak Hour | 36 31 | 5 4 | 0 | 0 | 0 | 41 35 | 16 12 | 2 1 | 0 | 0 | 0 | 18 13 | 52 43 | 7 5 | 0 | 0 | 0 | 59 48 |
| | | | | | | | | | | | | | | | | | | |
| Maximums (by category) Daily | 505 | 49 | 1 | 1 | 4 | | 230 | 27 | 3 | 0 | 3 | | 730 | 72 | 4 | 1 | 5 | |
| AM Peak Hour | 65 | 49 7 | 1 | 0 | 2 | | 53 | 4 | 2 | 0 | 3 1 | | 115 | 8 | 2 | 0 | 3 | |
| Mid-Day Peak Hour | 53 | 8 | 0 | 0 | 1 | | 20 | 3 | 0 | 0 | 0 | | 71 | 11 | 0 | 0 | 1 | |
| PM Peak Hour | 39 | 8 | 0 | 0 | 1 | | 20 | 3 | 0 | 0 | 0 | | 59 | 9 | 0 | 0 | 1 | |

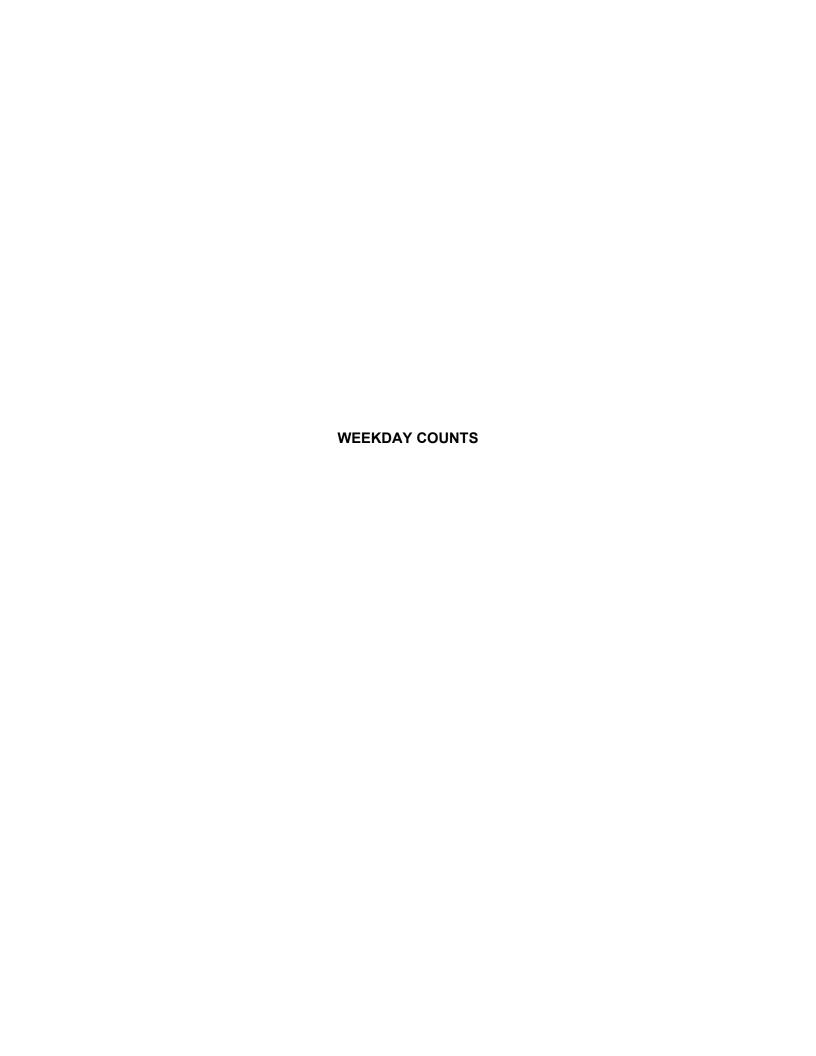
CHEVAL BLANC HOTEL PROJECT SUMMARY OF CURRENT SATURDAY ALLEY TRAFFIC ACTIVITY ONE-WAY SOUTHBOUND ALLEY BETWEEN SANTA MONICA BOULEVARD (S) AND BRIGHTON WAY

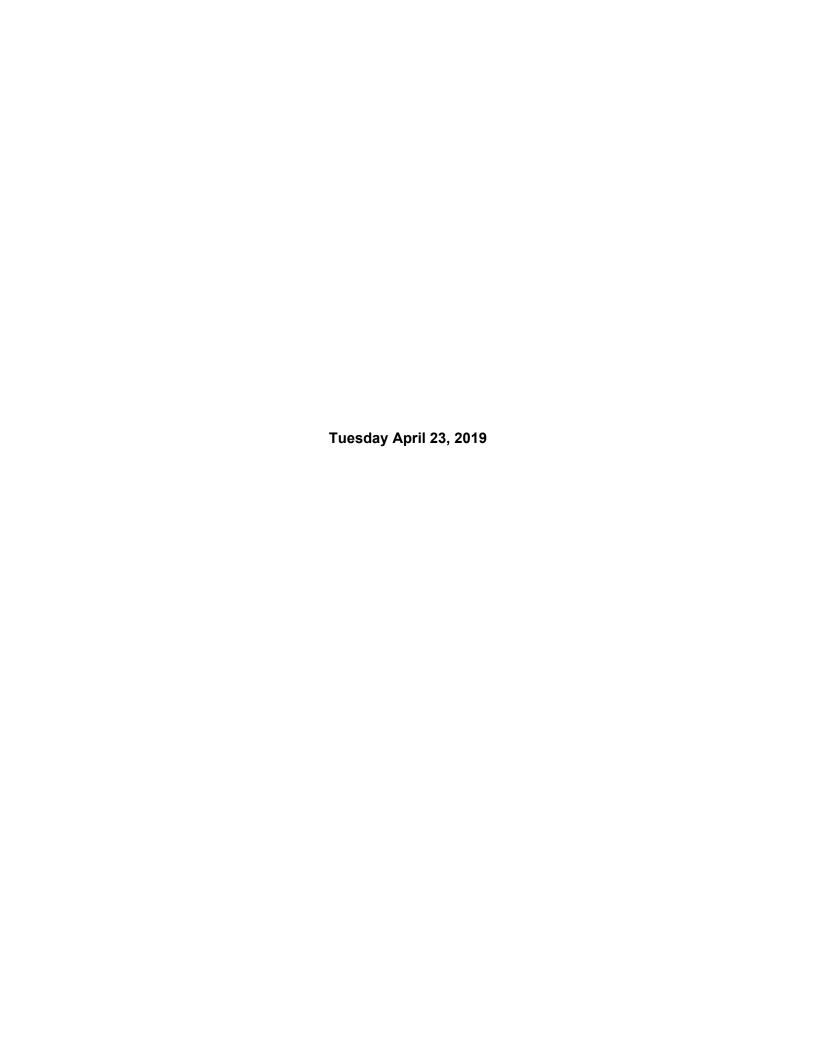
| | | EASTBOUN | ID RIGHT-TU | RN EN | TRY | | | WESTBOU | ND LEFT-TU | RN ENT | RY | | TOTAL ALLEY VOLUMES | | | | | | |
|--|-------|----------|-------------|-------|-----|-------|-------|----------|------------|--------|----|-------|---------------------|----------|---------|------|----|-------|--|
| DAY/DATE | AUTOS | DELIVERY | GARBAGE | SEMI | MC | TOTAL | AUTOS | DELIVERY | GARBAGE | SEMI | MC | TOTAL | AUTOS | DELIVERY | GARBAGE | SEMI | MC | TOTAL | |
| Saturday, May 11, 2019 | | | | | | | | | | | | | | | | | | | |
| Daily | 384 | 11 | 1 | 1 | 0 | 397 | 201 | 10 | 2 | 0 | 0 | 213 | 585 | 21 | 3 | 1 | 0 | 610 | |
| AM Peak Hour (8:45 - 9:45 AM) | 49 | 0 | 0 | 0 | 0 | 49 | 50 | 1 | 0 | 0 | 0 | 51 | 99 | 1 | 0 | 0 | 0 | 100 | |
| Mid-Day Peak Hour (12:00 N - 1:00 PM) | 42 | 1 | 0 | 0 | 0 | 43 | 14 | 1 | 0 | 0 | 0 | 15 | 56 | 2 | 0 | 0 | 0 | 58 | |
| PM Peak Hour (3:00 - 4:00 PM) | 43 | 2 | 0 | 0 | 0 | 45 | 13 | 1 | 0 | 0 | 0 | 14 | 56 | 3 | 0 | 0 | 0 | 59 | |
| Saturday, May 18, 2019 | | | | | | | | | | | | | | | | | | | |
| Daily | 387 | 16 | 1 | 0 | 0 | 404 | 166 | 8 | 2 | 0 | 0 | 176 | 553 | 24 | 3 | 0 | 0 | 580 | |
| AM Peak Hour (8:45 - 9:45 AM) | 63 | 2 | 0 | 0 | 0 | 65 | 29 | 1 | 0 | 0 | 0 | 30 | 92 | 3 | 0 | 0 | 0 | 95 | |
| Mid-Day Peak Hour (12:00 N - 1:00 PM) | 41 | 2 | 0 | 0 | 0 | 43 | 17 | 0 | 0 | 0 | 0 | 17 | 58 | 2 | 0 | 0 | 0 | 60 | |
| PM Peak Hour (3:00 - 4:00 PM) | 30 | 2 | 0 | 0 | 0 | 32 | 13 | 0 | 0 | 0 | 0 | 13 | 43 | 2 | 0 | 0 | 0 | 45 | |
| Saturday Average (2 Days) | | | | | | | | | | | | | | | | | | | |
| Daily | 386 | 14 | 1 | 1 | 0 | 402 | 184 | 9 | 2 | 0 | 0 | 195 | 570 | 23 | 3 | 1 | 0 | 597 | |
| AM Peak Hour | 56 | 1 | 0 | 0 | 0 | 57 | 40 | 1 | 0 | 0 | 0 | 41 | 96 | 2 | 0 | 0 | 0 | 98 | |
| Mid-Day Peak Hour | 42 | 2 | 0 | 0 | 0 | 44 | 16 | 1 | 0 | 0 | 0 | 17 | 58 | 3 | 0 | 0 | 0 | 61 | |
| PM Peak Hour | 37 | 2 | 0 | 0 | 0 | 39 | 13 | 1 | 0 | 0 | 0 | 14 | 50 | 3 | 0 | 0 | 0 | 53 | |
| Maximums (by category) | | | | | | | | | | | | | | | | | | | |
| Daily | 387 | 16 | 1 | 1 | 0 | | 201 | 10 | 2 | 0 | 0 | | 585 | 24 | 3 | 1 | 0 | | |
| AM Peak Hour | 63 | 2 | 0 | 0 | 0 | | 50 | 1 | 0 | 0 | 0 | | 99 | 3 | 0 | 0 | 0 | | |
| Mid-Day Peak Hour | 42 | 2 | 0 | 0 | 0 | | 17 | 1 | 0 | 0 | 0 | | 58 | 2 | 0 | 0 | 0 | | |
| PM Peak Hour | 43 | 2 | 0 | 0 | 0 | | 13 | 1 | 0 | 0 | 0 | | 56 | 3 | 0 | 0 | 0 | | |

CHEVAL BLANC HOTEL PROJECT SUMMARY OF CURRENT SUNDAY ALLEY TRAFFIC ACTIVITY ONE-WAY SOUTHBOUND ALLEY BETWEEN SANTA MONICA BOULEVARD (S) AND BRIGHTON WAY

| | | EASTBOUN | ID RIGHT-TU | RN EN | ΓRY | | | WESTBOL | IND LEFT-TU | TOTAL ALLEY VOLUMES | | | | | | | | |
|--|-------|----------|-------------|-------|-----|-------|-------|----------|-------------|---------------------|----|-------|-------|----------|---------|------|----|-------|
| DAY/DATE | AUTOS | DELIVERY | GARBAGE | SEMI | MC | TOTAL | AUTOS | DELIVERY | GARBAGE | SEMI | MC | TOTAL | AUTOS | DELIVERY | GARBAGE | SEMI | MC | TOTAL |
| Sunday, May 12, 2019 | | | | | | | | · | | | | | | | | | | |
| Daily | 179 | 1 | 0 | 0 | 0 | 180 | 91 | 1 | 0 | 0 | 0 | 92 | 270 | 2 | 0 | 0 | 0 | 272 |
| AM Peak Hour (8:00 - 9:00 AM) | 8 | 0 | 0 | 0 | 0 | 8 | 3 | 0 | 0 | 0 | 0 | 3 | 11 | 0 | 0 | 0 | 0 | 11 |
| Mid-Day Peak Hour (12:00 N - 1:00 PM) | 16 | 1 | 0 | 0 | 0 | 17 | 7 | 0 | 0 | 0 | 0 | 7 | 23 | 1 | 0 | 0 | 0 | 24 |
| PM Peak Hour (3:45 - 4:45 PM) | 26 | 0 | 0 | 0 | 0 | 26 | 10 | 0 | 0 | 0 | 0 | 10 | 36 | 0 | 0 | 0 | 0 | 36 |
| Sunday, May 19, 2019 | | | | | | | | | | | | | | | | | | |
| Daily | 201 | 4 | 0 | 0 | 0 | 205 | 76 | 2 | 0 | 0 | 0 | 78 | 277 | 6 | 0 | 0 | 0 | 283 |
| AM Peak Hour (8:30 - 9:30 AM) | 10 | 0 | 0 | 0 | 0 | 10 | 5 | 1 | 0 | 0 | 0 | 6 | 15 | 1 | 0 | 0 | 0 | 16 |
| Mid-Day Peak Hour (12:15 - 1:15 PM) | 18 | 0 | 0 | 0 | 0 | 18 | 6 | 0 | 0 | 0 | 0 | 6 | 24 | 0 | 0 | 0 | 0 | 24 |
| PM Peak Hour (3:15 - 4:15 PM) | 27 | 0 | 0 | 0 | 0 | 27 | 11 | 0 | 0 | 0 | 0 | 11 | 38 | 0 | 0 | 0 | 0 | 38 |
| Sunday Average (2 Days) | | | | | | | | | | | | | | | | | | |
| Daily | 190 | 3 | 0 | 0 | 0 | 193 | 84 | 2 | 0 | 0 | 0 | 86 | 274 | 5 | 0 | 0 | 0 | 279 |
| AM Peak Hour | 9 | 0 | 0 | 0 | 0 | 9 | 4 | 1 | 0 | 0 | 0 | 5 | 13 | 1 | 0 | 0 | 0 | 14 |
| Mid-Day Peak Hour | 17 | 1 | 0 | 0 | 0 | 18 | 7 | 0 | 0 | 0 | 0 | 7 | 24 | 1 | 0 | 0 | 0 | 25 |
| PM Peak Hour | 27 | 0 | 0 | 0 | 0 | 27 | 11 | 0 | 0 | 0 | 0 | 11 | 38 | 0 | 0 | 0 | 0 | 38 |
| Maximums (by category) | | | | | | | | | | | | | | | | | | |
| Daily | 201 | 4 | 0 | 0 | 0 | | 91 | 2 | 0 | 0 | 0 | | 277 | 6 | 0 | 0 | 0 | |
| AM Peak Hour | 10 | 0 | 0 | 0 | 0 | | 5 | 1 | 0 | 0 | 0 | | 15 | 1 | 0 | 0 | 0 | |
| Mid-Day Peak Hour | 18 | 1 | 0 | 0 | 0 | | 7 | 0 | 0 | 0 | 0 | | 24 | 1 | 0 | 0 | 0 | |
| PM Peak Hour | 27 | 0 | 0 | 0 | 0 | | 11 | 0 | 0 | 0 | 0 | | 38 | 0 | 0 | 0 | 0 | |

| INDIVIDUAL ALLEY ACCESS VEHICLE COUNT DATA SHEETS | |
|---|--|
| | |
| | |
| | |





CLIENT: HIRSCH/GREEN TRANSPORTATION CONSULTING, INC.

PROJECT: CHEVAL BLANC HOTEL - BEVERLY HILLS

DATE: TUESDAY, APRIL 23, 2019

PERIOD: 24-HOUR

INTERSECTION: N/S ALLEY (ONE-WAY SB)

| 15 MINUTE | | EASTRO | UND RIGHT | TUDNI EN | ITDV | | | WEST | BOUND LEFT | TUDNI EN | ITDV | | | | TOTAL EN | TDV | | |
|--------------|-------|----------|-----------|----------|------|-------|-------|------|------------|----------|------|-------|-------|----------|----------|------|----|-------|
| (START TIME) | AUTOS | DELIVERY | GARBAGE | SEMI | MC | TOTAL | AUTOS | | | SEMI | MC | TOTAL | AUTOS | DELIVERY | | SEMI | MC | TOTAL |
| | | | | | | | | | | | | | | | | | | |
| 12:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 12:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 12:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 12:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 1 |
| 1:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 1 |
| 2:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 1 |
| 3:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 3:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 3:30 AM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 3:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:15 AM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 4:30 AM | 2 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 1 | 0 | 0 | 3 | 4 | 0 | 1 | 0 | 0 | 5 |
| 4:45 AM | 2 | 0 | 0 | 0 | 0 | 2 | 1 | 0 | 0 | 0 | 0 | 1 | 3 | 0 | 0 | 0 | 0 | 3 |
| 5:00 AM | 3 | 0 | 0 | 0 | 0 | 3 | 1 | 0 | 0 | 0 | 0 | 1 | 4 | 0 | 0 | 0 | 0 | 4 |
| 5:15 AM | 1 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 2 |
| 5:30 AM | 1 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 2 |
| 5:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 1 |
| 6:00 AM | 2 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 0 | 0 | 0 | 2 | 4 | 0 | 0 | 0 | 0 | 4 |
| 6:15 AM | 3 | 0 | 1 | 0 | 0 | 4 | 1 | 0 | 0 | 0 | 0 | 1 | 4 | 0 | 1 | 0 | 0 | 5 |
| 6:30 AM | 6 | 0 | 0 | 0 | 0 | 6 | 2 | 0 | 0 | 0 | 0 | 2 | 8 | 0 | 0 | 0 | 0 | 8 |
| 6:45 AM | 6 | 0 | 0 | 0 | 0 | 6 | 1 | 0 | 0 | 0 | 0 | 1 | 7 | 0 | 0 | 0 | 0 | 7 |
| 7:00 AM | 4 | 0 | 0 | 0 | 0 | 4 | 2 | 0 | 0 | 0 | 0 | 2 | 6 | 0 | 0 | 0 | 0 | 6 |
| 7:15 AM | 6 | 0 | 0 | 0 | 0 | 6 | 4 | 0 | 0 | 0 | 0 | 4 | 10 | 0 | 0 | 0 | 0 | 10 |
| 7:30 AM | 4 | 0 | 0 | 0 | 0 | 4 | 3 | 0 | 0 | 0 | 0 | 3 | 7 | 0 | 0 | 0 | 0 | 7 |
| 7:45 AM | 6 | 0 | 0 | 0 | 0 | 6 | 7 | 0 | 0 | 0 | 0 | 7 | 13 | 0 | 0 | 0 | 0 | 13 |
| 8:00 AM | 7 | 0 | 0 | 0 | 0 | 7 | 2 | 0 | 0 | 0 | 0 | 2 | 9 | 0 | 0 | 0 | 0 | 9 |
| 8:15 AM | 7 | 0 | 0 | 0 | 0 | 7 | 3 | 0 | 0 | 0 | 0 | 3 | 10 | 0 | 0 | 0 | 0 | 10 |
| 8:30 AM | 8 | 0 | 0 | 0 | 0 | 8 | 5 | 0 | 0 | 0 | 0 | 5 | 13 | 0 | 0 | 0 | 0 | 13 |
| 8:45 AM | 13 | 1 | 0 | 0 | 0 | 14 | 10 | 1 | 1 | 0 | 0 | 12 | 23 | 2 | 1 | 0 | 0 | 26 |
| 9:00 AM | 22 | 0 | 0 | 0 | 0 | 22 | 7 | 0 | 0 | 0 | 0 | 7 | 29 | 0 | 0 | 0 | 0 | 29 |
| 9:15 AM | 14 | 0 | 0 | 0 | 0 | 14 | 17 | 1 | 0 | 0 | 0 | 18 | 31 | 1 | 0 | 0 | 0 | 32 |
| 9:30 AM | 12 | 0 | 0 | 0 | 0 | 12 | 11 | 0 | 1 | 0 | 0 | 12 | 23 | 0 | 1 | 0 | 0 | 24 |
| 9:45 AM | 13 | 1 | 00 | 0 | 0 | 14 | 6 | 0 | 0 | 0 | 0 | 6 | 19 | 1_ | 0 | 00 | 0 | 20 |
| 10:00 AM | 15 | 0 | 0 | 0 | 0 | 15 | 4 | 2 | 0 | 0 | 0 | 6 | 19 | 2 | 0 | 0 | 0 | 21 |
| 10:15 AM | 9 | 1 | 0 | 0 | 0 | 10 | 8 | 0 | 0 | 0 | 0 | 8 | 17 | 1 | 0 | 0 | 0 | 18 |
| 10:30 AM | 12 | 1 | 0 | 0 | 0 | 13 | 5 | 0 | 0 | 0 | 0 | 5 | 17 | 1 | 0 | 0 | 0 | 18 |
| 10:45 AM | 12 | 2 | 0 | 0 | 0 | 14 | 2 | 0 | 0 | 0 | 0 | 2 | 14 | 2 | 0 | 0 | 0 | 16 |
| 11:00 AM | 10 | 2 | 0 | 0 | 0 | 12 | 1 | 0 | 0 | 0 | 0 | 1 | 11 | 2 | 0 | 0 | 0 | 13 |
| 11:15 AM | 11 | 0 | 0 | 0 | 0 | 11 | 4 | 1 | 0 | 0 | 0 | 5 | 15 | 1 | 0 | 0 | 0 | 16 |
| 11:30 AM | 5 | 1 | 0 | 0 | 1 | 7 | 0 | 1 | 0 | 0 | 0 | 1 | 5 | 2 | 0 | 0 | 1 | 8 |
| 11:45 AM | 7 | 0 | 0 | 0 | 0 | 7 | 3 | 0 | 0 | 0 | 0 | 3 | 10 | 0 | 0 | 0 | 0 | 10 |
| 12:00 PM | 9 | 1 | 0 | 0 | 0 | 10 | 6 | 0 | 0 | 0 | 0 | 6 | 15 | 1 | 0 | 0 | 0 | 16 |
| 12:15 PM | 9 | 1 | 0 | 0 | 0 | 10 | 7 | 0 | 0 | 0 | 0 | 7 | 16 | 1 | 0 | 0 | 0 | 17 |
| 12:30 PM | 11 | 2 | 0 | 0 | 0 | 13 | 2 | 0 | 0 | 0 | 0 | 2 | 13 | 2 | 0 | 0 | 0 | 15 |
| 12:45 PM | 8 | 0 | 0 | 0 | 0 | 8 | 2 | 0 | 0 | 0 | 0 | 2 | 10 | 0 | 0 | 0 | 0 | 10 |
| 1:00 PM | 6 | 0 | 0 | 0 | 0 | 6 | 2 | 0 | 0 | 0 | 0 | 2 | 8 | 0 | 0 | 0 | 0 | 8 |
| 1:15 PM | 12 | 2 | 0 | 0 | 0 | 14 | 3 | 2 | 0 | 0 | 0 | 5 | 15 | 4 | 0 | 0 | 0 | 19 |
| 1:30 PM | 12 | 0 | 0 | 0 | 0 | 12 | 3 | 0 | 0 | 0 | 0 | 3 | 15 | 0 | 0 | 0 | 0 | 15 |
| 1:45 PM | 8 | 0 | 0 | 0 | 0 | 8 | 3 | 0 | 0 | 0 | 0 | 3 | 11 | 0 | 0 | 0 | 0 | 11 |

EASTBOUND RIGHT TURN ENTRY

CLIENT: HIRSCH/GREEN TRANSPORTATION CONSULTING, INC.

PROJECT: CHEVAL BLANC HOTEL - BEVERLY HILLS DATE: TUESDAY, APRIL 23, 2019

PERIOD: 24-HOUR

15 MINUTE

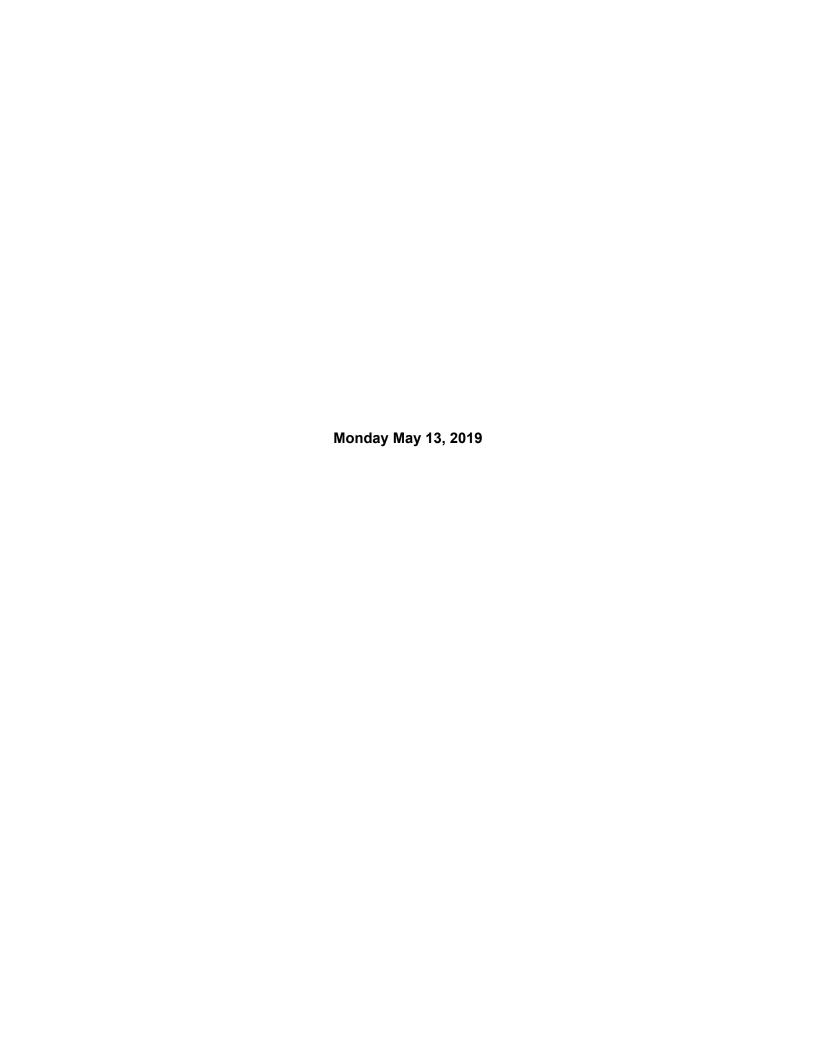
INTERSECTION: N/S ALLEY (ONE-WAY SB)

E/W SANTA MONICA BOULEVARD (S)

| | (START TIME) | AUTOS | DELIVERY | GARBAGE | SEMI | MC | TOTAL | AUTOS | DELIVERY | GARBAGE | SEMI | MC | TOTAL | AUTOS | DELIVERY | GARBAGE | SEMI | MC | TOTAL |
|---|--------------------|--------|----------|-----------|---------|------|--------|-------|----------|-----------|---------|------|--------|-------|----------|-----------|------|----|-------|
| | 2:00 PM | 9 | 1 | 0 | 0 | 0 | 10 | 3 | 0 | 0 | 0 | 1 | 4 | 12 | 1 | 0 | 0 | 1 | 14 |
| | 2:15 PM | 5 | 2 | 0 | 0 | 0 | 7 | 4 | 0 | 0 | 0 | 0 | 4 | 9 | 2 | 0 | 0 | 0 | 11 |
| | 2:30 PM | 5 | 0 | 0 | 0 | 0 | 5 | 2 | 1 | 0 | 0 | 0 | 3 | 7 | 1 | 0 | 0 | 0 | 8 |
| | 2:45 PM | 6 | 0 | 0 | 0 | 0 | 6 | 4 | 0 | 0 | 0 | 1 | 5 | 10 | 0 | 0 | 0 | 1 | 11 |
| | 3:00 PM | 13 | 1 | 0 | 0 | 0 | 14 | 1 | 0 | 0 | 0 | 0 | 1 | 14 | 1 | 0 | 0 | 0 | 15 |
| | 3:15 PM | 8 | 1 | 0 | 0 | 0 | 9 | 1 | 0 | 0 | 0 | 0 | 1 | 9 | 1 | 0 | 0 | 0 | 10 |
| | 3:30 PM | 11 | 5 | 0 | 0 | 0 | 16 | 1 | 0 | 0 | 0 | 0 | 1 | 12 | 5 | 0 | 0 | 0 | 17 |
| | 3:45 PM | 7 | 1 | 0 | 0 | 0 | 8 | 3 | 0 | 0 | 0 | 0 | 3 | 10 | 1 | 0 | 0 | 0 | 11 |
| | 4:00 PM | 10 | 2 | 0 | 0 | 0 | 12 | 2 | 1 | 0 | 0 | 0 | 3 | 12 | 3 | 0 | 0 | 0 | 15 |
| | 4:15 PM | 8 | 0 | 0 | 0 | 1 | 9 | 4 | 0 | 0 | 0 | 0 | 4 | 12 | 0 | 0 | 0 | 1 | 13 |
| | 4:30 PM | 6 | 0 | 0 | 0 | 0 | 6 | 3 | 0 | 0 | 0 | 0 | 3 | 9 | 0 | 0 | 0 | 0 | 9 |
| | 4:45 PM | 7 | 0 | 0 | 0 | 0 | 7 | 4 | 0 | 0 | 0 | 0 | 4 | 11 | 0 | 0 | 0 | 0 | 11 |
| | 5:00 PM | 8 | 0 | 0 | 0 | 0 | 8 | 3 | 0 | 0 | 0 | 0 | 3 | 11 | 0 | 0 | 0 | 0 | 11 |
| | 5:15 PM | 10 | 0 | 0 | 0 | 0 | 10 | 5 | 0 | 0 | 0 | 0 | 5 | 15 | 0 | 0 | 0 | 0 | 15 |
| | 5:30 PM | 8 | 0 | 0 | 0 | 0 | 8 | 1 | 0 | 0 | 0 | 0 | 1 | 9 | 0 | 0 | 0 | 0 | 9 |
| | 5:45 PM | 7 | 1 | 0 | 0 | 0 | 8 | 2 | 0 | 0 | 0 | 0 | 2 | 9 | 1 | 0 | 0 | 0 | 10 |
| | 6:00 PM | 7 | 0 | 0 | 0 | 0 | 7 | 2 | 0 | 0 | 0 | 0 | 2 | 9 | 0 | 0 | 0 | 0 | 9 |
| | 6:15 PM | 9 | 0 | 0 | 0 | 0 | 9 | 1 | 0 | 0 | 0 | 0 | 1 | 10 | 0 | 0 | 0 | 0 | 10 |
| | 6:30 PM | 7 | 0 | 0 | 0 | 0 | 7 | 4 | 0 | 0 | 0 | 0 | 4 | 11 | 0 | 0 | 0 | 0 | 11 |
| | 6:45 PM | 6 | 0 | 0 | 0 | 0 | 6 | 2 | 1 | 0 | 0 | 0 | 3 | 8 | 1 | 0 | 0 | 0 | 9 |
| | 7:00 PM | 5 | 0 | 0 | 0 | 0 | 5 | 3 | 0 | 0 | 0 | 0 | 3 | 8 | 0 | 0 | 0 | 0 | 8 |
| | 7:15 PM | 5 | 0 | 0 | 0 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 0 | 0 | 0 | 5 |
| | 7:30 PM | 3 | 0 | 0 | 0 | 0 | 3 0 | 1 | 0 | 0 | 0 | 0 | 1 0 | 4 | 0 | 0 | 0 | 0 | 4 |
| | 7:45 PM | 0 | 0 | 0 | | | | 0 | 0 | | 0 | 0 | | | • | | 0 | 0 | 0 |
| | 8:00 PM 8:15 PM | 2 1 | 0 1 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 1 | 2 | 0 1 | 0 | 0 | 0 | 2 |
| | 8:30 PM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| | 8:45 PM | 1 | 0 | 0 | 0 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 2 | 3 | 0 | 0 | 0 | 0 | 3 |
| | 9:00 PM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| | 9:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | 9:30 PM | 2 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 2 |
| | 9:45 PM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| | 10:00 PM | 1 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 2 |
| | 10:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | 10:30 PM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| | 10:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 1 |
| | 11:00 PM | 2 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 2 |
| | 11:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 1 |
| | 11:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | 11:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| i | | | | | | | | | | | | | | | | | | | |
| | | | EASTRO | UND RIGHT | TURN FN | ITRY | | | WESTR | OUND LEFT | TURN FN | ITRY | | | | TOTAL ENT | RY | | |
| | TOTALS | AUTOS | DELIVERY | GARBAGE | SEMI | MC | TOTAL | AUTOS | DELIVERY | GARBAGE | SEMI | MC | TOTAL | AUTOS | DELIVERY | GARBAGE | SEMI | MC | TOTAL |
| Ī | АМ | 144 | 2 | 1 | 0 | 0 | 147 | 92 | 3 | 3 | 0 | 0 | 98 | 236 | 5 | 4 | 0 | 0 | 245 |
| | MIDDAY | 156 | 13 | 0 | 0 | 1 | 170 | 55 | 6 | 0 | 0 | 0 | 61 | 211 | 19 | 0 | 0 | 1 | 231 |
| | PM | | | | | | | | | 0 | 0 | | | 244 | | 0 | | | |
| _ | | 183 | 15 | 0 | 0 | 1 | 199 | 61 | 4 | | | 2 | 67 | | 19 | | 0 | 3 | 266 |
| | DAILY | 483 | 30 | 1 | 0 | 2 | 516 | 208 | 13 | 3 | 0 | 2 | 226 | 691 | 43 | 4 | 0 | 4 | 742 |

WESTBOUND LEFT TURN ENTRY

TOTAL ENTRY



CLIENT: HIRSCH/GREEN TRANSPORTATION CONSULTING, INC.

PROJECT: CHEVAL BLANC HOTEL - BEVERLY HILLS

DATE: MONDAY, MAY 13, 2019

PERIOD: 24-HOUR

INTERSECTION: N/S ALLEY (ONE-WAY SB)

| 45 MINUTE | | EAGTEG | NIND DIGUT | TUDALES | ITDY | | | MEGTO | OLIND LEET | TUDN 5. | TDV | | | | TOTAL EN | TDV . | | |
|---------------------------|---------|----------|------------|---------|--------|--------|--------|--------|----------------------|---------|-----|---------|----------|----------|----------|--------|----|----------|
| 15 MINUTE (START TIME) | AUTOS | DELIVERY | GARBAGE | SEMI | MC | TOTAL | AUTOS | | OUND LEFT GARBAGE | SEMI | MC | TOTAL | AUTOS | DELIVERY | TOTAL EN | SEMI | MC | TOTAL |
| , | - | | | | | | | | | | | | | | | | | |
| 12:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 12:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 12:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 1 |
| 12:45 AM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 1:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1:15 AM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 1:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 1 | 0 | 0 | 0 | 0 | 0 |
| 2:00 AM | 0 | 0 | 0 | 0 | 0 | 0 1 | 1 0 | 0 | 0 | 0 | 0 | 1 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 2:15 AM | 1 | 0 | 0 | 0 | 0 | | | 0 | 0 | 0 | 0 | | | 0 | 0 | 0 | 0 | 1 |
| 2:30 AM | 1 | | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 0 | 0 | 0 | 0 | 0 | 1 |
| 2:45 AM | 0 1 | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 3 | 4 | 0 | 0 | 0 | 0 | 0 |
| 3:00 AM 3:15 AM | 0 | 0 0 | 0 | 0 | 0 | 1 0 | 3 1 | 0 1 | 0 | 0 | 0 | 2 | 1 | | 0 0 | 0 | 0 | 4 2 |
| | | | | | 0 | | | | | 0 | | | | 1 | | | | |
| 3:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 3:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:00 AM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 1 | 1 | 1 | 0 | 0 | 0 | 2 |
| 4:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 |
| 4:30 AM | 0 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 2 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:45 AM | | | 0 | | 0 | 2 | 1 | 0 | - | 0 | 0 | | 4 | | 0 | 0 | 0 | 4 |
| 5:00 AM | 5 | 0 | 0 | 0 | 0 | 5 | | 0 | 0 | 0 | 0 | 1 | 6 | 0 | 0 | 0 | 0 | 6 |
| 5:15 AM | 2 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 0 | 0 | 0 | 2 | 4 | 0 | 0 | 0 | 0 | 4 |
| 5:30 AM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 1 | 0 | 1 | 0 | 0 | 2 |
| 5:45 AM | 3 | 0 | 0 | 0 | 0 | 3 | 2 | 0 | 0 | 0 | 0 | 2 | 5 | 0 | 0 | 0 | 0 | 5 |
| 6:00 AM | 2 | 0 | 0 | 0 | 0 | 2 | 1 | 1 | 0 | 0 | 0 | 2 | 3 | 1 | 0 | 0 | 0 | 4 |
| 6:15 AM | 1 | 0 | 0 | 0 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 2 | 3 | 0 | 0 | 0 | 0 | 3 |
| 6:30 AM | 1 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 2 |
| 6:45 AM | 2 | 1 | 0 | 0 | 0 | 3 | 1 | 1 | 1 | 0 | 0 | 3 | 3 | 2 | 1 | 0 | 0 | 6 |
| 7:00 AM | 7 | 0 | 0 | 0 | 0 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 7 | 0 | 0 | 0 | 0 | 7 |
| 7:15 AM | 4 | 0 | 0 | 0 | 0 | 4 | 2 | 0 | 0 | 0 | 0 | 2 | 6 | 0 | 0 | 0 | 0 | 6 |
| 7:30 AM | 4 | 0 | 0 | 0 | 0 | 4 | 4 | 0 | 0 | 0 | 0 | 4 | 8 | 0 | 0 | 0 | 0 | 8 |
| 7:45 AM | 7 | 0 | 0 | 0 | 0 | 7 | 5 | 0 | 0 | 0 | 0 | 5 | 12 | 0 | 0 | 0 | 0 | 12 |
| 8:00 AM | 6 | 0 | 0 | 0 | 0 | 6 | 2 | 0 | 0 | 0 | 0 | 2 | 8 | 0 | 0 | 0 | 0 | 8 |
| 8:15 AM | 7 | 2 | 0 | 0 | 0 | 9 | 1 | 0 | 0 | 0 | 0 | 1 | 8 | 2 | 0 | 0 | 0 | 10 |
| 8:30 AM | 7 | 0 | 0 | 0 | 0 | 7 | 7 | 0 | 0 | 0 | 0 | 7 | 14 | 0 | 0 | 0 | 0 | 14 |
| 8:45 AM | 18 | 0 | 0 | 0 | 1 | 19 | 8 | 0 | 0 | 0 | 0 | 8 | 26 | 0 | 0 | 0 | 1 | 27 |
| 9:00 AM | 12 | 1 | 0 | 0 | 0 | 13 | 16 | 0 | 0 | 0 | 0 | 16 | 28 | 1 | 0 | 0 | 0 | 29 |
| 9:15 AM | 19 | 2 | 0 | 0 | 0 | 21 | 12 | 2 | 0 | 0 | 0 | 14 | 31 | 4 | 0 | 0 | 0 | 35 |
| 9:30 AM | 8 | 0 1 | 0 | 0 | 0 0 | 8 7 | 5 9 | 2 1 | 0 | 0 | 0 | 7 10 | 13 15 | 2 2 | 0 0 | 0 0 | 0 | 15 17 |
| 9:45 AM | 66 | | | | | | | | | | | | 15 | | | | | 17 |
| 10:00 AM | 6 11 | 1 | 0 | 0 | 0 | 7 | 0 | 1 | 0 | 0 | 0 | 1 9 | 6 | 2 | 0 | 0 | 0 | 8 |
| 10:15 AM | 11 | 2 | 0 | 0 | 0 | 13 | 8 | 1 | 0 | 0 | 0 | | 19 | 3 | 0 | 0 | 0 | 22 |
| 10:30 AM | 3 17 | 4 | 0 | 0 | 0 | 7 | 3 | 0 | 0 | 0 | 0 | 3 | 6 | 4 | 0 | 0 | 0 | 10 |
| 10:45 AM | 17 | 1 | 0 | 0 | 0 | 18 | 1 | 0 | 0 | 0 | 0 | 1 | 18 | 1 | 0 | 0 | 0 | 19 7 |
| 11:00 AM | 5 | 0 | 0 | 0 | 0 | 5 | 2 | 0 | 0 | 0 | 0 | 2 | 7 | 0 | 0 | 0 | 0 | 7 7 |
| 11:15 AM | 6 | 0 | 0 | 0 | 0 | 6 | 1 | 0 | | 0 | 0 | | 7 | 0 | 0 | 0 | 0 | |
| 11:30 AM | 11 | 1 | 0 | 0 | 0 | 12 | 5 | 1 | 0 | 0 | 0 | 6 | 16 | 2 | 0 | 0 | 0 | 18 |
| 11:45 AM | 9 | 0 | 0 | 0 | 0 | 9 | 0 | 1 | 0 | 0 | 0 | 1 | 9 | 1 | 0 | 0 | 0 | 10 |
| 12:00 PM | 7 | 1 | 0 | 0 | 0 | 8 | 5 | 0 | 0 | 0 | 0 | 5 | 12 | 1 | 0 | 0 | 0 | 13 |
| 12:15 PM | 8 | 5 | 0 | 0 | 0 | 13 | 2 | 0 | 0 | 0 | 0 | 2 | 10 | 5 | 0 | 0 | 0 | 15 |
| 12:30 PM | 6 | 2 | 0 | 0 | 0 | 8 | 1 | 1 | 0 | 0 | 0 | 2 | 7 | 3 | 0 | 0 | 0 | 10 |
| 12:45 PM | 4 | 0 | 0 | 0 | 0 | 4 | 1 | 2 | 0 | 0 | 0 | 3 | 5 | 2 | 0 | 0 | 0 | 7 |
| 1:00 PM | 6 | 0 | 0 | 0 | 0 | 6 | 3 | 1 | 0 | 0 | 0 | 4 | 9 | 1 | 0 | 0 | 0 | 10 |
| 1:15 PM | 2 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 0 | 0 | 0 | 2 | 4 | 0 | 0 | 0 | 0 | 4 |
| 1:30 PM | 9 | 1 | 0 | 0 | 0 | 10 | 2 | 0 | 0 | 0 | 0 | 2 | 11 | 1 | 0 | 0 | 0 | 12 |
| 1:45 PM | 3 | 1 | 0 | 0 | 0 | 4 | 4 | 0 | 0 | 0 | 0 | 4 | 7 | <u> </u> | 0 | 0 | 0 | 8 |

CLIENT: HIRSCH/GREEN TRANSPORTATION CONSULTING, INC.

PROJECT: CHEVAL BLANC HOTEL - BEVERLY HILLS

DATE: MONDAY, MAY 13, 2019 PERIOD:

24-HOUR INTERSECTION: N/S ALLEY (ONE-WAY SB)

| 45 MINUITS | | EAGTE | NIND DIOLET | TUDN C1 | ITDV | | | MEGTO | OUND LEET | CUDN EN | TDV | | | | TOTAL CLI | -DV | | |
|--------------------|--------|----------|-------------|---------|------|-------|-------|----------|-----------|---------|-----|--------|--------|---------------|-----------|------|-----|-------|
| 15 MINUTE | AUTOO | | OUND RIGHT | | | TOTAL | AUTOO | | OUND LEFT | | | TOTAL | ALITOO | DEL II (ED) (| TOTAL ENT | | 110 | TOTAL |
| (START TIME) | | DELIVERY | GARBAGE | SEMI | MC | TOTAL | | DELIVERY | GARBAGE | SEMI | MC | TOTAL | AUTOS | DELIVERY | GARBAGE | SEMI | MC | TOTAL |
| 2:00 PM | 8 | 1 | 0 | 0 | 0 | 9 | 3 | 0 | 0 | 0 | 0 | 3 | 11 | 1 | 0 | 0 | 0 | 12 |
| 2:15 PM | 7 | 4 | 0 | 0 | 0 | 11 | 3 | 1 | 0 | 0 | 0 | 4 | 10 | 5 | 0 | 0 | 0 | 15 |
| 2:30 PM | 10 | 1 | 0 | 0 | 0 | 11 | 4 | 1 | 0 | 0 | 0 | 5 | 14 | 2 | 0 | 0 | 0 | 16 |
| 2:45 PM | 6 | 1 | 0 | 0 | 0 | 7 | 1 | 0 | 0 | 0 | 0 | 1 | 7 | 1 | 0 | 0 | 0 | 8 |
| 3:00 PM | 6 | 0 | 0 | 0 | 0 | 6 | 0 | 1 | 0 | 0 | 0 | 1 | 6 | 1 | 0 | 0 | 0 | 7 |
| 3:15 PM | 7 | 0 | 0 | 0 | 0 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 7 | 0 | 0 | 0 | 0 | 7 |
| 3:30 PM | 9 | 1 | 0 | 0 | 0 | 10 | 4 | 1 | 0 | 0 | 0 | 5 | 13 | 2 | 0 | 0 | 0 | 15 |
| 3:45 PM | 2 | 2 | 0 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 0 | 0 | 4 |
| 4:00 PM | 6 | 0 | 0 | 0 | 0 | 6 | 1 | 0 | 0 | 0 | 0 | 1 | 7 | 0 | 0 | 0 | 0 | 7 |
| 4:15 PM | 7 | 1 | 0 | 0 | 0 | 8 | 3 | 0 | 0 | 0 | 0 | 3 | 10 | 1 | 0 | 0 | 0 | 11 |
| 4:30 PM | 7 | 1 | 0 | 0 | 0 | 8 | 1 | 0 | 0 | 0 | 0 | 1 | 8 | 1 | 0 | 0 | 0 | 9 |
| 4:45 PM | 3 | 0 | 0 | 0 | 0 | 3 | 2 | 0 | 0 | 0 | 0 | 2 | 5 | 0 | 0 | 0 | 0 | 5 |
| 5:00 PM | 4 | 0 | 0 | 0 | 0 | 4 | 3 | 0 | 0 | 0 | 0 | 3 | 7 | 0 | 0 | 0 | 0 | 7 |
| 5:15 PM | 3 | 0 | 0 | 0 | 0 | 3 | 1 | 0 | 0 | 0 | 0 | 1 | 4 | 0 | 0 | 0 | 0 | 4 |
| 5:30 PM | 6 | 0 | 0 | 0 | 0 | 6 | 1 | 0 | 0 | 0 | 0 | 1 | 7 | 0 | 0 | 0 | 0 | 7 |
| 5:45 PM | 10 | 0 | 0 | 0 | 0 | 10 | 3 | 0 | 0 | 0 | 0 | 3 | 13 | 0 | 0 | 0 | 0 | 13 |
| 6:00 PM | 2 | 0 | 0 | 0 | 0 | 2 | 1 | 0 | 0 | 0 | 0 | 1 | 3 | 0 | 0 | 0 | 0 | 3 |
| 6:15 PM | 3 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 3 |
| 6:30 PM | 3 | 1 | 0 | 0 | 0 | 4 | 3 | 0 | 0 | 0 | 0 | 3 | 6 | 1 | 0 | 0 | 0 | 7 |
| 6:45 PM | 3 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 1 | 3 | 0 | 0 | 0 | 0 | 3 |
| 7:00 PM | 0 | 0 | | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | | 1 | 0 | 0 | 0 | | 1 |
| 7:15 PM 7:30 PM | 1 3 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 1 0 | 2 | 0 | 0 | 0 | 0 | 2 |
| 7:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:00 PM | 2 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 2 |
| 8:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:30 PM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 8:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 9:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 9:15 PM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 9:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 9:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 10:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 10:15 PM | 2 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 2 |
| 10:30 PM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 10:45 PM | 2 | 0 | 0 | 0 | 0 | 2 | 0 | 1 | 0 | 0 | 0 | 1 | 2 | 1 | 0 | 0 | 0 | 3 |
| 11:00 PM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 11:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 11:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 11:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | | | | | | | | | | | | | | | | | | |
| | | EASTBO | OUND RIGHT | TURN EN | ITRY | | | WESTB | OUND LEFT | TURN EN | TRY | | | | TOTAL ENT | RY | | |
| TOTALS | AUTOS | DELIVERY | GARBAGE | SEMI | MC | TOTAL | AUTOS | DELIVERY | GARBAGE | SEMI | MC | TOTAL | AUTOS | DELIVERY | GARBAGE | SEMI | MC | TOTAL |
| AM | 130 | 7 | 0 | 0 | 1 | 138 | 88 | 10 | 3 | 0 | 0 | 101 | 218 | 17 | 3 | 0 | 1 | 239 |
| MIDDAY | 113 | 19 | 0 | 0 | 0 | 132 | 40 | 8 | 0 | 0 | 0 | 48 | 153 | 27 | 0 | 0 | 0 | 180 |
| PM | 126 | 13 | 0 | 0 | 0 | 139 | 36 | 5 | 0 | 0 | 0 | 41 | 162 | 18 | 0 | 0 | 0 | 180 |
| DAILY | 369 | 39 | 0 | 0 | 1 | 409 | 164 | 23 | 3 | 0 | 0 | 190 | 533 | 62 | 3 | 0 | 1 | 599 |



CLIENT: HIRSCH/GREEN TRANSPORTATION CONSULTING, INC.

PROJECT: CHEVAL BLANC HOTEL - BEVERLY HILLS

DATE: TUESDAY, MAY 14, 2019

PERIOD: 24-HOUR

INTERSECTION: N/S ALLEY (ONE-WAY SB)

| 15 MINUTE | | EASTRO | UND RIGHT | TUDNI EN | ITDV | | | WEST | BOUND LEFT | TUDNI EN | ITDV | | | | TOTAL EN | TDV | | |
|----------------------|--------|----------|-----------|----------|------|--------|-------|--------|------------|----------|------|-------|-------|----------|----------|------|-----|--------|
| (START TIME) | ALITOS | DELIVERY | GARBAGE | SEMI | MC | TOTAL | AUTOS | | | SEMI | MC | TOTAL | AUTOS | DELIVERY | | SEMI | MC | TOTAL |
| ` ' | | | | | | | | | | | | | | | | | | |
| 12:00 AM 12:15 AM | 1 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 1 |
| 12:15 AM 12:30 AM | 0 | 0 0 | 0 | 0 | 0 | 1 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 |
| | 0 | | 0 | 0 | | | 0 | 0 | 0 | | | 0 | 0 | 0 | 0 | 0 | | |
| 12:45 AM | 1 | 0 | | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 1 |
| 1:00 AM | | | 0 | | | 1 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | | | 0 | |
| 1:15 AM | 1 | 0 | | 0 | 0 | | | 0 | | 0 | 0 | | | - | 0 | 0 | 0 | 1 |
| 1:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2:15 AM | 1 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 2 |
| 2:30 AM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 2:45 AM | 2 | 0 | 0 | 0 | 0 | 2 | 1 | 0 | 0 | 0 | 0 | 1 | 3 | 0 | 0 | 0 | 0 | 3 |
| 3:00 AM | 1 | 1 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 2 |
| 3:15 AM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 3:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 1 |
| 3:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 1 |
| 4:00 AM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 4:15 AM | 1 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 2 |
| 4:30 AM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 1 | 0 | 1 | 0 | 0 | 2 |
| 4:45 AM | 4 | 0 | 0 | 0 | 0 | 4 | 1 | 0 | 0 | 0 | 0 | 1 | 5 | 0 | 0 | 0 | 0 | 5 |
| 5:00 AM | 3 | 0 | 0 | 0 | 1 | 4 | 4 | 0 | 0 | 0 | 0 | 4 | 7 | 0 | 0 | 0 | 1 | 8 |
| 5:15 AM | 3 | 1 | 0 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 1 | 0 | 0 | 0 | 4 |
| 5:30 AM | 4 | 0 | 0 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 4 |
| 5:45 AM | 2 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 0 | 0 | 0 | 2 | 4 | 0 | 0 | 0 | 0 | 4 |
| 6:00 AM | 2 | 0 | 0 | 0 | 0 | 2 | 1 | 0 | 0 | 0 | 0 | 1 | 3 | 0 | 0 | 0 | 0 | 3 |
| 6:15 AM | 2 | 0 | 0 | 0 | 0 | 2 | 0 | 1 | 0 | 0 | 0 | 1 | 2 | 1 | 0 | 0 | 0 | 3 |
| 6:30 AM | 4 | 0 | 0 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 4 |
| 6:45 AM | 2 | 0 | 0 | 0 | 0 | 2 | 4 | 0 | 0 | 0 | 0 | 4 | 6 | 0 | 0 | 0 | 0 | 6 |
| 7:00 AM | 4 | 0 | 0 | 0 | 0 | 4 | 2 | 0 | 0 | 0 | 0 | 2 | 6 | 0 | 0 | 0 | 0 | 6 |
| 7:15 AM | 4 | 0 | 0 | 0 | 0 | 4 | 2 | 0 | 1 | 0 | 0 | 3 | 6 | 0 | 1 | 0 | 0 | 7 |
| 7:30 AM | 10 | 0 | 0 | 0 | 0 | 10 | 8 | 0 | 0 | 0 | 0 | 8 | 18 | 0 | 0 | 0 | 0 | 18 |
| 7:45 AM | 1 | 1 | 0 | 0 | 0 | 2 | 8 | 1 | 0 | 0 | 0 | 9 | 9 | 2 | 0 | 0 | 0 | 11 |
| 8:00 AM | 5 | 1 | 0 | 0 | 0 | 6 | 4 | 1 | 0 | 0 | 0 | 5 | 9 | 2 | 0 | 0 | 0 | 11 |
| 8:15 AM | 9 | 1 | 0 | 0 | 0 | 10 | 6 | 0 | 0 | 0 | 0 | 6 | 15 | 1 | 0 | 0 | 0 | 16 |
| 8:30 AM | 12 | 0 | 0 | 0 | 0 | 12 | 5 | 0 | 0 | 0 | 0 | 5 | 17 | 0 | 0 | 0 | 0 | 17 |
| 8:45 AM | 18 | 1 | 0 | 0 | 1 | 20 | 10 | 0 | 0 | 0 | 1 | 11 | 28 | 1 | 0 | 0 | 2 | 31 |
| 9:00 AM | 22 | 2 | 0 | 0 | 0 | 24 | 18 | 0 | 0 | 0 | 0 | 18 | 40 | 2 | 0 | 0 | 0 | 42 |
| 9:15 AM | 14 | 2 | 0 | 0 | 1 | 17 | 13 | 0 | 0 | 0 | 0 | 13 | 27 | 2 | 0 | 0 | 1 | 30 |
| 9:30 AM | 11 | 0 | 0 | 0 | 0 | 11 | 9 | 0 | 0 | 0 | 0 | 9 | 20 | 0 | 0 | 0 | 0 | 20 |
| 9:45 AM | 12 | 2 | 00 | 0 | _1_ | 15 | 8 | 1 | 0 | 0 | 0 | 9 | 20 | 3 | 0 | 0 | _1_ | 24 |
| 10:00 AM | 8 | 1 | 0 | 0 | 0 | 9 | 10 | 1 | 0 | 0 | 0 | 11 | 18 | 2 | 0 | 0 | 0 | 20 |
| 10:15 AM | 14 | 1 | 0 | 0 | 0 | 15 | 3 | 0 | 0 | 0 | 0 | 3 | 17 | 1 | 0 | 0 | 0 | 18 |
| 10:30 AM | 4 | 1 | 0 | 0 | 0 | 5 | 4 | 1 | 0 | 0 | 0 | 5 | 8 | 2 | 0 | 0 | 0 | 10 |
| 10:45 AM | 7 | 1 | 0 | 0 | 0 | 8 | 4 | 0 | 0 | 0 | 0 | 4 | 11 | 1 | 0 | 0 | 0 | 12 |
| 11:00 AM | 10 | 0 | 0 | 0 | 0 | 10 | 5 | 0 | 0 | 0 | 0 | 5 | 15 | 0 | 0 | 0 | 0 | 15 |
| 11:15 AM | 9 | 2 | 0 | 0 | 0 | 11 | 2 | 2 | 0 | 0 | 0 | 4 | 11 | 4 | 0 | 0 | 0 | 15 |
| 11:30 AM | 9 | 2 | 0 | 0 | 0 | 11 | 2 | 0 | 0 | 0 | 0 | 2 | 11 | 2 | 0 | 0 | 0 | 13 |
| 11:45 AM | 6 | 1 | 0 | 0 | 0 | 7 | 7 | 2 | 0 | 0 | 0 | 9 | 13 | 3 | 0 | 0 | 0 | 16 |
| 12:00 PM | 5 | 1 | 0 | 0 | 0 | 6 | 5 | 0 | 0 | 0 | 0 | 5 | 10 | 1 | 0 | 0 | 0 | 11 |
| 12:15 PM | 11 | 0 | 0 | 0 | 0 | 11 | 0 | 0 | 0 | 0 | 0 | 0 | 11 | 0 | 0 | 0 | 0 | 11 |
| 12:30 PM | 7 | 2 | 0 | 0 | 0 | 9 | 3 | 0 | 0 | 0 | 0 | 3 | 10 | 2 | 0 | 0 | 0 | 12 |
| 12:45 PM | 6 | 0 | 0 | 0 | 0 | 6 | 5 | 0 | 0 | 0 | 0 | 5 | 11 | 0 | 0 | 0 | 0 | 11 |
| 1:00 PM | 10 | 0 | 0 | 0 | 0 | 10 | 2 | 1 | 0 | 0 | 0 | 3 | 12 | 1 | 0 | 0 | 0 | 13 |
| 1:15 PM | 10 | 2 | 0 | 0 | 0 | 12 | 3 | 0 | 0 | 0 | 0 | 3 | 13 | 2 | 0 | 0 | 0 | 15 |
| 1:30 PM | 8 | 3 | 0 | 0 | 0 | 11 | 8 | 0 | 0 | 0 | 0 | 8 | 16 | 3 | 0 | 0 | 0 | 19 |
| 1:45 PM | 7 | 2 | 0 | 0 | 0 | 9 | 4 | 0 | 0 | 0 | 0 | 4 | 11 | 2 | 0 | 0 | 0 | 13 |

CLIENT: HIRSCH/GREEN TRANSPORTATION CONSULTING, INC.

PROJECT: CHEVAL BLANC HOTEL - BEVERLY HILLS

DATE: TUESDAY, MAY 14, 2019

PERIOD: 24-HOUR

INTERSECTION: N/S ALLEY (ONE-WAY SB)

| | | | | | | | | | | | | | | | = | | | |
|----------------------|--------|----------|------------|------|----|--------|--------|----------|--------------|------|----|--------|--------|---------------|-----------|------|-----|--------|
| 15 MINUTE | | | OUND RIGHT | | | | | | BOUND LEFT 1 | | | | | | TOTAL ENT | | | |
| (START TIME) | AUTOS | DELIVERY | GARBAGE | SEMI | MC | TOTAL | AUTOS | DELIVERY | GARBAGE | SEMI | MC | TOTAL | AUTOS | DELIVERY | GARBAGE | SEMI | MC | TOTAL |
| 2:00 PM | 6 | 3 | 0 | 0 | 0 | 9 | 3 | 1 | 0 | 0 | 0 | 4 | 9 | 4 | 0 | 0 | 0 | 13 |
| 2:15 PM | 11 | 3 | 0 | 0 | 0 | 14 | 3 | 2 | 0 | 0 | 0 | 5 | 14 | 5 | 0 | 0 | 0 | 19 |
| 2:30 PM | 7 | 0 | 0 | 0 | 0 | 7 | 6 | 1 | 0 | 0 | 0 | 7 | 13 | 1 | 0 | 0 | 0 | 14 |
| 2:45 PM | 7 | 0 | 0 | 0 | 0 | 7 | 3 | 0 | 0 | 0 | 0 | 3 | 10 | 0 | 0 | 0 | 0 | 10 |
| 3:00 PM | 5 | 1 | 0 | 0 | 0 | 6 | 5 | 0 | 0 | 0 | 0 | 5 | 10 | 1 | 0 | 0 | 0 | 11 |
| 3:15 PM | 7 | 1 | 0 | 0 | 0 | 8 | 4 | 1 | 0 | 0 | 0 | 5 | 11 | 2 | 0 | 0 | 0 | 13 |
| 3:30 PM | 2 | 1 | 0 | 0 | 0 | 3 | 3 | 0 | 0 | 0 | 0 | 3 | 5 | 1 | 0 | 0 | 0 | 6 |
| 3:45 PM | 2 | 0 | 0 | 0 | 0 | 2 | 1 | 0 | 0 | 0 | 0 | 1 | 3 | 0 | 0 | 0 | 0 | 3 |
| 4:00 PM | 8 | 0 | 0 | 0 | 0 | 8 | 5 | 0 | 0 | 0 | 0 | 5 | 13 | 0 | 0 | 0 | 0 | 13 |
| 4:15 PM | 9 | 0 | 0 | 0 | 0 | 9 | 2 | 0 | 0 | 0 | 0 | 2 | 11 | 0 | 0 | 0 | 0 | 11 |
| 4:30 PM | 9 | 0 | 0 | 0 | 0 | 9 | 7 | 0 | 0 | 0 | 0 | 7 | 16 | 0 | 0 | 0 | 0 | 16 |
| 4:45 PM | 4 | 0 | 0 | 0 | 0 | 4 | 2 | 0 | 0 | 0 | 0 | 2 | 6 | 0 | 0 | 0 | 0 | 6 |
| 5:00 PM | 7 | 0 | 0 | 0 | 0 | 7 | 1 | 0 | 0 | 0 | 0 | 1 | 8 | 0 | 0 | 0 | 0 | 8 |
| 5:15 PM | 7 | 2 | 0 | 0 | 0 | 9 | 0 | 0 | 0 | 0 | 0 | 0 | 7 | 2 | 0 | 0 | 0 | 9 |
| 5:30 PM | 6 | 1 | 0 | 0 | 0 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 6 | 1 | 0 | 0 | 0 | 7 |
| 5:45 PM | 9 | 0 | 0 | 0 | 0 | 9 | 1 | 0 | 0 | 0 | 0 | 1 | 10 | 0 | 0 | 0 | 0 | 10 |
| 6:00 PM | 5 | 0 | 0 | 0 | 0 | 5 | 1 | 0 | 0 | 0 | 0 | 1 | 6 | 0 | 0 | 0 | 0 | 6 |
| 6:15 PM | 5 | 1 | 0 | 0 | 0 | 6 | 1 | 0 | 0 | 0 | 0 | 1 | 6 | 1 | 0 | 0 | 0 | 7 |
| 6:30 PM | 3 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 3 |
| 6:45 PM | 4 | 0 | 0 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 4 |
| 7:00 PM | 2 | 0 | 0 | 0 | 0 | 2 | 1 | 0 | 0 | 0 | 0 | 1 | 3 | 0 | 0 | 0 | 0 | 3 |
| 7:15 PM | 5 | 0 | 0 | 0 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 0 | 0 | 0 | 5 |
| 7:30 PM | 2 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 2 |
| 7:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:00 PM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 8:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:45 PM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 9:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 9:15 PM | 3 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 3 |
| 9:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 9:45 PM | 1 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 2 |
| 10:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 10:15 PM | 2 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 2 |
| 10:30 PM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 10:45 PM | 1 1 | 0 | 0 | 0 | 0 | 1 | 0 | 1 0 | 0 | 0 | 0 | 1 0 | 1 | 1 0 | 0 | 0 | 0 | 2 |
| 11:00 PM 11:15 PM | 1 2 | 0 | 0 | 0 | 0 | 1 2 | 0 | 0 | 0 | 0 | 0 | 0 | 1 2 | 0 | 0 | 0 | 0 | 1 2 |
| 11:30 PM | 2 | 0 | 0 | 0 | 0 | 2 | 0 | 1 | 0 | 0 | 0 | 1 | 2 | 1 | 0 | 0 | 0 | 3 |
| 11:30 PM 11:45 PM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 3 1 |
| 11.45 FIVI | | U | U | U | U | , | U | J | J | J | U | J | ' | U | J | J | J | 1 |
| | | | | | | | | | | | | | | | | | | |
| TOT-1:0 | ALITOC | | OADBAGE | | | TOTAL | ALITOS | | OUND LEFT 1 | | | TOTAL | ALITOS | DEL IV (ED) (| TOTAL ENT | | 1/0 | TOTAL |
| TOTALS | AUTOS | DELIVERY | GARBAGE | SEMI | MC | TOTAL | | DELIVERY | GARBAGE | SEMI | MC | TOTAL | | DELIVERY | GARBAGE | SEMI | MC | TOTAL |
| AM | 161 | 12 | 0 | 0 | 4 | 177 | 109 | 5 | 2 | 0 | 1 | 117 | 270 | 17 | 2 | 0 | 5 | 294 |
| MIDDAY | 131 | 19 | 0 | 0 | 0 | 150 | 67 | 7 | 0 | 0 | 0 | 74 | 198 | 26 | 0 | 0 | 0 | 224 |
| PM | 148 | 13 | 0 | 0 | 0 | 161 | 50 | 7 | 0 | 0 | 0 | 57 | 198 | 20 | 0 | 0 | 0 | 218 |
| DAILY | 440 | 44 | 0 | 0 | 4 | 488 | 226 | 19 | 2 | 0 | 1 | 248 | 666 | 63 | 2 | 0 | 5 | 736 |



CLIENT: HIRSCH/GREEN TRANSPORTATION CONSULTING, INC.

PROJECT: CHEVAL BLANC HOTEL - BEVERLY HILLS

DATE: MONDAY, MAY 20, 2019

PERIOD: 24-HOUR

INTERSECTION: N/S ALLEY (ONE-WAY SB)

| 15 MINUTE | | EACTE/ | OUND RIGHT | TUDN EN | ITDV | | | WEST | BOUND LEFT | TUDN EN | ITDV | | | | TOTAL EN | TDV | | |
|--------------|-------|----------|------------|---------|------|-------|-------|----------|------------|---------|------|-------|-------|----------|----------|-----|----|-------|
| (START TIME) | AUTOS | DELIVERY | GARBAGE | SEMI | MC | TOTAL | AUTOS | DELIVERY | | SEMI | MC | TOTAL | AUTOS | DELIVERY | | 1 | MC | TOTAL |
| | | | | | | | | | | | | | | | | | | |
| 12:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 12:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 1 |
| 12:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 12:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1:00 AM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 1:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 1 |
| 2:15 AM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 2:30 AM | 4 | 0 | 0 | 0 | 0 | 4 | 2 | 0 | 0 | 0 | 0 | 2 | 6 | 0 | 0 | 0 | 0 | 6 |
| 2:45 AM | 2 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 2 |
| 3:00 AM | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 |
| 3:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 3:30 AM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 3:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:15 AM | 6 | 0 | 0 | 0 | 0 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 6 | 0 | 0 | 0 | 0 | 6 |
| 4:30 AM | 2 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 0 | 0 | 0 | 2 | 4 | 0 | 0 | 0 | 0 | 4 |
| 4:45 AM | 5 | 0 | 0 | 0 | 0 | 5 | 0 | 0 | 1 | 0 | 0 | 1 | 5 | 0 | 1 | 0 | 0 | 6 |
| 5:00 AM | 4 | 0 | 0 | 0 | 0 | 4 | 1 | 1 | 0 | 0 | 0 | 2 | 5 | 1 | 0 | 0 | 0 | 6 |
| 5:15 AM | 2 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 2 |
| 5:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:45 AM | 1 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 2 |
| 6:00 AM | 5 | 1 | 0 | 0 | 0 | 6 | 2 | 1 | 0 | 0 | 0 | 3 | 7 | 2 | 0 | 0 | 0 | 9 |
| 6:15 AM | 2 | 0 | 0 | 0 | 0 | 2 | 1 | 0 | 0 | 0 | 0 | 1 | 3 | 0 | 0 | 0 | 0 | 3 |
| 6:30 AM | 0 | 1 | 0 | 0 | 0 | 1 | 1 | 0 | 2 | 0 | 0 | 3 | 1 | 1 | 2 | 0 | 0 | 4 |
| 6:45 AM | 5 | 0 | 0 | 0 | 0 | 5 | 1 | 0 | 0 | 0 | 0 | 1 | 6 | 0 | 0 | 0 | 0 | 6 |
| 7:00 AM | 3 | 0 | 0 | 0 | 0 | 3 | 1 | 0 | 0 | 0 | 0 | 1 | 4 | 0 | 0 | 0 | 0 | 4 |
| 7:15 AM | 5 | 0 | 0 | 0 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 0 | 0 | 0 | 5 |
| 7:30 AM | 3 | 0 | 0 | 0 | 0 | 3 | 5 | 0 | 0 | 0 | 0 | 5 | 8 | 0 | 0 | 0 | 0 | 8 |
| 7:45 AM | 9 | 0 | 0 | 0 | 0 | 9 | 5 | 0 | 0 | 0 | 0 | 5 | 14 | 0 | 0 | 0 | 0 | 14 |
| 8:00 AM | 8 | 0 | 0 | 0 | 0 | 8 | 5 | 0 | 0 | 0 | 0 | 5 | 13 | 0 | 0 | 0 | 0 | 13 |
| 8:15 AM | 7 | 2 | 0 | 0 | 0 | 9 | 5 | 0 | 0 | 0 | 0 | 5 | 12 | 2 | 0 | 0 | 0 | 14 |
| 8:30 AM | 4 | 0 | 0 | 0 | 0 | 4 | 6 | 0 | 0 | 0 | 0 | 6 | 10 | 0 | 0 | 0 | 0 | 10 |
| 8:45 AM | 13 | 1 | 0 | 0 | 1 | 15 | 12 | 0 | 0 | 0 | 0 | 12 | 25 | 1 | 0 | 0 | 1 | 27 |
| 9:00 AM | 13 | 3 | 0 | 0 | 0 | 16 | 5 | 0 | 0 | 0 | 0 | 5 | 18 | 3 | 0 | 0 | 0 | 21 |
| 9:15 AM | 16 | 3 | 0 | 0 | 0 | 19 | 12 | 1 | 0 | 0 | 0 | 13 | 28 | 4 | 0 | 0 | 0 | 32 |
| 9:30 AM | 11 | 0 | 0 | 0 | 0 | 11 | 7 | 0 | 0 | 0 | 0 | 7 | 18 | 0 | 0 | 0 | 0 | 18 |
| 9:45 AM | 10 | 00 | 0 | 0 | 0 | 10 | 5 | 0 | 0 | 0 | 0 | 5 | 15 | 0 | 0 | 0 | 0 | 15 |
| 10:00 AM | 9 | 0 | 0 | 0 | 0 | 9 | 3 | 1 | 0 | 0 | 0 | 4 | 12 | 1 | 0 | 0 | 0 | 13 |
| 10:15 AM | 9 | 1 | 0 | 0 | 0 | 10 | 9 | 1 | 0 | 0 | 0 | 10 | 18 | 2 | 0 | 0 | 0 | 20 |
| 10:30 AM | 3 | 3 | 0 | 0 | 0 | 6 | 5 | 0 | 0 | 0 | 0 | 5 | 8 | 3 | 0 | 0 | 0 | 11 |
| 10:45 AM | 6 | 0 | 0 | 0 | 0 | 6 | 2 | 0 | 0 | 0 | 0 | 2 | 8 | 0 | 0 | 0 | 0 | 8 |
| 11:00 AM | 5 | 2 | 0 | 0 | 0 | 7 | 1 | 0 | 0 | 0 | 0 | 1 | 6 | 2 | 0 | 0 | 0 | 8 |
| 11:15 AM | 6 | 0 | 0 | 0 | 0 | 6 | 3 | 0 | 0 | 0 | 0 | 3 | 9 | 0 | 0 | 0 | 0 | 9 |
| 11:30 AM | 6 | 1 | 0 | 0 | 0 | 7 | 1 | 0 | 0 | 0 | 0 | 1 | 7 | 1 | 0 | 0 | 0 | 8 |
| 11:45 AM | 17 | 0 | 0 | 0 | 0 | 17 | 3 | 1 | 0 | 0 | 0 | 4 | 20 | 1 | 0 | 0 | 0 | 21 |
| 12:00 PM | 9 | 2 | 0 | 0 | 0 | 11 | 5 | 1 | 0 | 0 | 0 | 6 | 14 | 3 | 0 | 0 | 0 | 17 |
| 12:15 PM | 5 | 1 | 0 | 0 | 0 | 6 | 3 | 2 | 0 | 0 | 0 | 5 | 8 | 3 | 0 | 0 | 0 | 11 |
| 12:30 PM | 10 | 2 | 0 | 0 | 0 | 12 | 3 | 0 | 0 | 0 | 0 | 3 | 13 | 2 | 0 | 0 | 0 | 15 |
| 12:45 PM | 5 | 0 | 0 | 0 | 0 | 5 | 3 | 0 | 0 | 0 | 0 | 3 | 8 | 0 | 0 | 0 | 0 | 8 |
| 1:00 PM | 4 | 0 | 0 | 0 | 0 | 4 | 7 | 0 | 0 | 0 | 1 | 8 | 11 | 0 | 0 | 0 | 1 | 12 |
| 1:15 PM | 4 | 0 | 0 | 0 | 0 | 4 | 3 | 0 | 0 | 0 | 0 | 3 | 7 | 0 | 0 | 0 | 0 | 7 |
| 1:30 PM | 7 | 0 | 0 | 0 | 0 | 7 | 4 | 1 | 0 | 0 | 1 | 6 | 11 | 1 | 0 | 0 | 1 | 13 |
| 1:45 PM | 9 | 3 | 0 | 0 | 0 | 12 | 2 | 0 | 0 | 0 | 0 | 2 | 11 | 3 | 0 | 0 | 0 | 14 |

CLIENT: HIRSCH/GREEN TRANSPORTATION CONSULTING, INC.

PROJECT: CHEVAL BLANC HOTEL - BEVERLY HILLS

DATE: MONDAY, MAY 20, 2019

PERIOD: 24-HOUR

INTERSECTION: N/S ALLEY (ONE-WAY SB)

| 15 MINUTE | | | OUND RIGHT | TURN EN | ITRY | | | | OUND LEFT | TURN EN | TRY | | | | TOTAL ENT | | | |
|----------------------|--------|----------|------------|---------|------|--------|--------|----------|-----------|---------|-----|-------|--------|----------|-----------|------|----|--------|
| (START TIME) | AUTOS | DELIVERY | GARBAGE | SEMI | MC | TOTAL | AUTOS | DELIVERY | GARBAGE | SEMI | MC | TOTAL | AUTOS | DELIVERY | GARBAGE | SEMI | MC | TOTAL |
| 2:00 PM | 11 | 0 | 0 | 0 | 0 | 11 | 5 | 0 | 0 | 0 | 0 | 5 | 16 | 0 | 0 | 0 | 0 | 16 |
| 2:15 PM | 10 | 0 | 0 | 0 | 0 | 10 | 1 | 1 | 0 | 0 | 0 | 2 | 11 | 1 | 0 | 0 | 0 | 12 |
| 2:30 PM | 6 | 1 | 0 | 0 | 0 | 7 | 3 | 1 | 0 | 0 | 0 | 4 | 9 | 2 | 0 | 0 | 0 | 11 |
| 2:45 PM | 5 | 1 | 0 | 0 | 0 | 6 | 3 | 0 | 0 | 0 | 0 | 3 | 8 | 1 | 0 | 0 | 0 | 9 |
| 3:00 PM | 4 | 0 | 0 | 0 | 1 | 5 | 1 | 1 | 0 | 0 | 0 | 2 | 5 | 1 | 0 | 0 | 1 | 7 |
| 3:15 PM | 2 | 2 | 0 | 0 | 0 | 4 | 1 | 0 | 0 | 0 | 0 | 1 | 3 | 2 | 0 | 0 | 0 | 5 |
| 3:30 PM | 3 | 0 | 0 | 0 | 0 | 3 | 2 | 1 | 0 | 0 | 0 | 3 | 5 | 1 | 0 | 0 | 0 | 6 |
| 3:45 PM | 2 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 0 | 0 | 0 | 2 | 4 | 0 | 0 | 0 | 0 | 4 |
| 4:00 PM | 4 | 2 | 0 | 0 | 0 | 6 | 2 | 0 | 0 | 0 | 0 | 2 | 6 | 2 | 0 | 0 | 0 | 8 |
| 4:15 PM | 9 | 0 | 0 | 0 | 0 | 9 | 2 | 0 | 0 | 0 | 0 | 2 | 11 | 0 | 0 | 0 | 0 | 11 |
| 4:30 PM | 8 | 0 | 0 | 0 | 0 | 8 | 3 | 1 | 0 | 0 | 0 | 4 | 11 | 1 | 0 | 0 | 0 | 12 |
| 4:45 PM | 4 | 1 | 0 | 0 | 0 | 5 | 1 | 0 | 0 | 0 | 0 | 1 | 5 | 1 | 0 | 0 | 0 | 6 |
| 5:00 PM | 7 | 0 | 0 | 0 | 0 | 7 | 2 | 0 | 0 | 0 | 0 | 2 | 9 | 0 | 0 | 0 | 0 | 9 |
| 5:15 PM | 4 | 0 | 0 | 0 | 0 | 4 | 3 | 0 | 0 | 0 | 0 | 3 | 7 | 0 | 0 | 0 | 0 | 7 |
| 5:30 PM | 11 | 1 | 0 | 0 | 0 | 12 | 1 | 0 | 0 | 0 | 0 | 1 | 12 | 1 | 0 | 0 | 0 | 13 |
| 5:45 PM | 5 | 0 | 0 | 0 | 0 | 5 | 2 | 0 | 0 | 0 | 0 | 2 | 7 | 0 | 0 | 0 | 0 | 7 |
| 6:00 PM | 1 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 2 |
| 6:15 PM | 3 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 3 |
| 6:30 PM | 5 | 0 | 0 | 0 | 0 | 5 | 3 | 0 | 0 | 0 | 0 | 3 | 8 | 0 | 0 | 0 | 0 | 8 |
| 6:45 PM | 2 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 2 |
| 7:00 PM | 2 | 0 | 0 | 0 | 0 | 2 | 1 | 0 | 0 | 0 | 0 | 1 | 3 | 0 | 0 | 0 | 0 | 3 |
| 7:15 PM | 1 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 2 |
| 7:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 3 | 3 | 0 | 0 | 0 | 0 | 3 |
| 7:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:00 PM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 8:15 PM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 8:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 1 |
| 9:00 PM | 1 | 0 | 0 | 0 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 2 | 3 | 0 | 0 | 0 | 0 | 3 |
| 9:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 9:30 PM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 9:45 PM | 1 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 2 |
| 10:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 1 |
| 10:15 PM | 0 3 | - | ~ | 0 | 0 | 0 | - | 0 | - | - | - | 0 | - | 0 | 0 | 0 | 0 | 0 |
| 10:30 PM | | 0 | 0 | 0 | 0 | 3 1 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 3 |
| 10:45 PM | 1 | 0 | 0 | 0 | 0 | 1 4 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 0 | 0 | 0 | 0 | 1 |
| 11:00 PM 11:15 PM | 4 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 4 1 |
| 11:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 11:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 0 | 0 | 0 | 2 |
| 11.40 FW | U | U | J | U | J | U | 2 | J | U | U | U | 2 | 2 | U | J | J | U | 2 |
| | | | | | | | | | | | | | | | | | | |
| TOTALC | ALITOO | | OUND RIGHT | | | TOTAL | ALITOO | | CARRACE | | | TOTAL | ALITOO | DELIVERY | TOTAL ENT | | MC | TOTAL |
| TOTALS | AUTOS | | GARBAGE | SEMI | MC | TOTAL | | DELIVERY | GARBAGE | SEMI | MC | TOTAL | AUTOS | DELIVERY | GARBAGE | SEMI | MC | TOTAL |
| AM | 143 | 12 | 0 | 0 | 1 | 156 | 80 | 4 | 3 | 0 | 0 | 87 | 223 | 16 | 3 | 0 | 1 | 243 |
| MIDDAY | 114 | 15 | 0 | 0 | 0 | 129 | 57 | 7 | 0 | 0 | 2 | 66 | 171 | 22 | 0 | 0 | 2 | 195 |
| PM | 123 | 8 | 0 | 0 | 1 | 132 | 50 | 5 | 0 | 0 | 0 | 55 | 173 | 13 | 0 | 0 | 1 | 187 |
| DAILY | 380 | 35 | 0 | 0 | 2 | 417 | 187 | 16 | 3 | 0 | 2 | 208 | 567 | 51 | 3 | 0 | 4 | 625 |



CLIENT: HIRSCH/GREEN TRANSPORTATION CONSULTING, INC.

PROJECT: CHEVAL BLANC HOTEL - BEVERLY HILLS

DATE: TUESDAY, MAY 21, 2019

PERIOD: 24-HOUR

INTERSECTION: N/S ALLEY (ONE-WAY SB)

| 45 MINUITE | | FACTRO | LIND DICUT | TUDN EN | ITDV | | | WEST | DOLIND LEET | TUDNI EN | ITDV | | | | TOTAL EN | TDV | | |
|---------------------------|-------|----------|------------|---------|------|-------|-------|------|-------------|----------|------|-------|-------|----------|----------|------|----|-------|
| 15 MINUTE (START TIME) | AUTOS | DELIVERY | UND RIGHT | SEMI | MC | TOTAL | AUTOS | | GARBAGE | SEMI | MC | TOTAL | AUTOS | DELIVERY | GARBAGE | SEMI | MC | TOTAL |
| , | | | | | | | | | | | | | | | | | | |
| 12:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 12:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 12:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 12:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1:45 AM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 2:00 AM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 2:15 AM | 2 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | | 0 | 0 | | 2 | 0 | 0 | 0 | 0 | 2 |
| 2:30 AM | 6 | 0 | 0 | 0 | 0 | 6 | 1 | 0 | 0 | 0 | 0 | 1 | 7 | 0 | 0 | 0 | 0 | 7 |
| 2:45 AM | 3 | 0 | 0 | 0 | 0 | 3 | 1 | 0 | 0 | 0 | 0 | 1 | 4 | 0 | 0 | 0 | 0 | 4 |
| 3:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 1 |
| 3:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 3:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 1 |
| 3:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 1 |
| 4:15 AM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 4:30 AM | 2 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 1 | 0 | 0 | 1 | 2 | 0 | 1 | 0 | 0 | 3 |
| 4:45 AM | 10 | 1 | 0 | 0 | 0 | 11 | 1 | 0 | 0 | 0 | 0 | 1 | 11 | 1 | 0 | 0 | 0 | 12 |
| 5:00 AM | 5 | 0 | 0 | 0 | 0 | 5 | 1 | 0 | 0 | 0 | 0 | 1 | 6 | 0 | 0 | 0 | 0 | 6 |
| 5:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 1 |
| 5:30 AM | 6 | 0 | 0 | 0 | 0 | 6 | 1 | 2 | 0 | 0 | 0 | 3 | 7 | 2 | 0 | 0 | 0 | 9 |
| 5:45 AM | 3 | 0 | 0 | 0 | 0 | 3 | 0 | 2 | 0 | 0 | 0 | 2 | 3 | 2 | 0 | 0 | 0 | 5 |
| 6:00 AM | 6 | 0 | 0 | 0 | 0 | 6 | 2 | 1 | 0 | 0 | 0 | 3 | 8 | 1 | 0 | 0 | 0 | 9 |
| 6:15 AM | 2 | 1 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 1 | 0 | 0 | 0 | 3 |
| 6:30 AM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 6:45 AM | 6 | 1 | 0 | 0 | 0 | 7 | 2 | 0 | 0 | 0 | 0 | 2 | 8 | 1 | 0 | 0 | 0 | 9 |
| 7:00 AM | 4 | 0 | 0 | 0 | 0 | 4 | 2 | 1 | 0 | 0 | 0 | 3 | 6 | 1 | 0 | 0 | 0 | 7 |
| 7:15 AM | 6 | 1 | 0 | 0 | 0 | 7 | 2 | 0 | 1 | 0 | 0 | 3 | 8 | 1 | 1 | 0 | 0 | 10 |
| 7:30 AM | 5 | 0 | 0 | 0 | 0 | 5 | 11 | 0 | 0 | 0 | 0 | 11 | 16 | 0 | 0 | 0 | 0 | 16 |
| 7:45 AM | 8 | 1 | 0 | 0 | 0 | 9 | 9 | 1 | 0 | 0 | 0 | 10 | 17 | 2 | 0 | 0 | 0 | 19 |
| 8:00 AM | 6 | 0 | 0 | 0 | 0 | 6 | 4 | 0 | 0 | 0 | 0 | 4 | 10 | 0 | 0 | 0 | 0 | 10 |
| 8:15 AM | 9 | 1 | 0 | 0 | 0 | 10 | 3 | 0 | 0 | 0 | 0 | 3 | 12 | 1 | 0 | 0 | 0 | 13 |
| 8:30 AM | 12 | 0 | 0 | 0 | 0 | 12 | 3 | 0 | 1 | 0 | 0 | 4 | 15 | 0 | 1 | 0 | 0 | 16 |
| 8:45 AM | 14 | 0 | 1 | 0 | 0 | 15 | 12 | 1 | 0 | 0 | 0 | 13 | 26 | 1 | 1 | 0 | 0 | 28 |
| 9:00 AM | 16 | 2 | 0 | 0 | 0 | 18 | 10 | 0 | 0 | 0 | 0 | 10 | 26 | 2 | 0 | 0 | 0 | 28 |
| 9:15 AM | 10 | 0 | 0 | 0 | 0 | 10 | 20 | 2 | 0 | 0 | 0 | 22 | 30 | 2 | 0 | 0 | 0 | 32 |
| 9:30 AM | 11 | 2 | 0 | 0 | 0 | 13 | 11 | 0 | 0 | 0 | 0 | 11 | 22 | 2 | 0 | 0 | 0 | 24 |
| 9:45 AM | 16 | 2 | 00 | 0 | 0 | 18 | 6 | 0 | 0 | 0 | 0 | 6 | 22 | 2 | 0 | 00 | 0 | 24 |
| 10:00 AM | 12 | 1 | 0 | 0 | 0 | 13 | 4 | 1 | 0 | 0 | 0 | 5 | 16 | 2 | 0 | 0 | 0 | 18 |
| 10:15 AM | 14 | 1 | 0 | 0 | 0 | 15 | 9 | 0 | 0 | 0 | 0 | 9 | 23 | 1 | 0 | 0 | 0 | 24 |
| 10:30 AM | 7 | 0 | 0 | 0 | 0 | 7 | 3 | 0 | 0 | 0 | 0 | 3 | 10 | 0 | 0 | 0 | 0 | 10 |
| 10:45 AM | 11 | 3 | 0 | 0 | 0 | 14 | 7 | 0 | 0 | 0 | 0 | 7 | 18 | 3 | 0 | 0 | 0 | 21 |
| 11:00 AM | 9 | 1 | 0 | 0 | 0 | 10 | 5 | 1 | 0 | 0 | 0 | 6 | 14 | 2 | 0 | 0 | 0 | 16 |
| 11:15 AM | 10 | 2 | 0 | 0 | 0 | 12 | 2 | 0 | 0 | 0 | 0 | 2 | 12 | 2 | 0 | 0 | 0 | 14 |
| 11:30 AM | 7 | 0 | 0 | 0 | 0 | 7 | 3 | 1 | 0 | 0 | 0 | 4 | 10 | 1 | 0 | 0 | 0 | 11 |
| 11:45 AM | 17 | 0 | 0 | 0 | 0 | 17 | 2 | 1 | 0 | 0 | 0 | 3 | 19 | 1 | 0 | 0 | 0 | 20 |
| 12:00 PM | 11 | 2 | 0 | 0 | 0 | 13 | 1 | 0 | 0 | 0 | 0 | 1 | 12 | 2 | 0 | 0 | 0 | 14 |
| 12:15 PM | 8 | 3 | 0 | 0 | 0 | 11 | 3 | 1 | 0 | 0 | 0 | 4 | 11 | 4 | 0 | 0 | 0 | 15 |
| 12:30 PM | 6 | 0 | 0 | 0 | 0 | 6 | 4 | 0 | 0 | 0 | 0 | 4 | 10 | 0 | 0 | 0 | 0 | 10 |
| 12:45 PM | 7 | 0 | 0 | 0 | 0 | 7 | 4 | 0 | 0 | 0 | 0 | 4 | 11 | 0 | 0 | 0 | 0 | 11 |
| 1:00 PM | 5 | 2 | 0 | 0 | 0 | 7 | 2 | 2 | 0 | 0 | 0 | 4 | 7 | 4 | 0 | 0 | 0 | 11 |
| 1:15 PM | 5 | 2 | 0 | 0 | 0 | 7 | 9 | 0 | 0 | 0 | 0 | 9 | 14 | 2 | 0 | 0 | 0 | 16 |
| 1:30 PM | 10 | 1 | 0 | 0 | 0 | 11 | 3 | 1 | 0 | 0 | 0 | 4 | 13 | 2 | 0 | 0 | 0 | 15 |
| 1:45 PM | 3 | 1 | 0 | 0 | 0 | 4 | 4 | 1 | 0 | 0 | 0 | 5 | 7 | 2 | 0 | 0 | 0 | 9 |

CLIENT: HIRSCH/GREEN TRANSPORTATION CONSULTING, INC.

PROJECT: CHEVAL BLANC HOTEL - BEVERLY HILLS

DATE: TUESDAY, MAY 21, 2019 24-HOUR PERIOD:

INTERSECTION: N/S ALLEY (ONE-WAY SB)

| 15 MINUTE | | | OUND RIGHT | | | | | | BOUND LEFT | | | | | | TOTAL ENT | | | |
|--------------|-------|----------|------------|------|----|-------|-------|----------|------------|------|----|-------|-------|----------|-----------|------|----|-------|
| (START TIME) | AUTOS | DELIVERY | GARBAGE | SEMI | MC | TOTAL | AUTOS | DELIVERY | GARBAGE | SEMI | MC | TOTAL | AUTOS | DELIVERY | GARBAGE | SEMI | MC | TOTAL |
| 2:00 PM | 11 | 0 | 0 | 0 | 0 | 11 | 3 | 0 | 0 | 0 | 0 | 3 | 14 | 0 | 0 | 0 | 0 | 14 |
| 2:15 PM | 16 | 1 | 0 | 0 | 0 | 17 | 1 | 1 | 0 | 0 | 0 | 2 | 17 | 2 | 0 | 0 | 0 | 19 |
| 2:30 PM | 7 | 0 | 0 | 0 | 0 | 7 | 2 | 0 | 0 | 0 | 0 | 2 | 9 | 0 | 0 | 0 | 0 | 9 |
| 2:45 PM | 10 | 1 | 0 | 0 | 0 | 11 | 7 | 0 | 0 | 0 | 0 | 7 | 17 | 1 | 0 | 0 | 0 | 18 |
| 3:00 PM | 7 | 1 | 0 | 0 | 0 | 8 | 1 | 0 | 0 | 0 | 0 | 1 | 8 | 1 | 0 | 0 | 0 | 9 |
| 3:15 PM | 9 | 1 | 0 | 0 | 0 | 10 | 2 | 0 | 0 | 0 | 0 | 2 | 11 | 1 | 0 | 0 | 0 | 12 |
| 3:30 PM | 6 | 0 | 0 | 0 | 0 | 6 | 4 | 2 | 0 | 0 | 0 | 6 | 10 | 2 | 0 | 0 | 0 | 12 |
| 3:45 PM | 8 | 2 | 0 | 0 | 0 | 10 | 5 | 0 | 0 | 0 | 0 | 5 | 13 | 2 | 0 | 0 | 0 | 15 |
| 4:00 PM | 7 | 0 | 0 | 0 | 0 | 7 | 1 | 0 | 0 | 0 | 0 | 1 | 8 | 0 | 0 | 0 | 0 | 8 |
| 4:15 PM | 9 | 0 | 0 | 0 | 0 | 9 | 1 | 1 | 0 | 0 | 0 | 2 | 10 | 1 | 0 | 0 | 0 | 11 |
| 4:30 PM | 9 | 1 | 0 | 0 | 0 | 10 | 2 | 0 | 0 | 0 | 0 | 2 | 11 | 1 | 0 | 0 | 0 | 12 |
| 4:45 PM | 6 | 0 | 0 | 0 | 0 | 6 | 5 | 1 | 0 | 0 | 0 | 6 | 11 | 1 | 0 | 0 | 0 | 12 |
| 5:00 PM | 8 | 0 | 0 | 0 | 0 | 8 | 1 | 0 | 0 | 0 | 0 | 1 | 9 | 0 | 0 | 0 | 0 | 9 |
| 5:15 PM | 8 | 0 | 0 | 0 | 0 | 8 | 3 | 0 | 0 | 0 | 0 | 3 | 11 | 0 | 0 | 0 | 0 | 11 |
| 5:30 PM | 6 | 0 | 0 | 0 | 0 | 6 | 2 | 0 | 0 | 0 | 0 | 2 | 8 | 0 | 0 | 0 | 0 | 8 |
| 5:45 PM | 8 | 0 | 0 | 0 | 0 | 8 | 3 | 0 | 0 | 0 | 0 | 3 | 11 | 0 | 0 | 0 | 0 | 11 |
| 6:00 PM | 2 | 1 | 0 | 0 | 0 | 3 | 1 | 0 | 0 | 0 | 0 | 1 | 3 | 1 | 0 | 0 | 0 | 4 |
| 6:15 PM | 5 | 0 | 0 | 0 | 0 | 5 | 3 | 0 | 0 | 0 | 0 | 3 | 8 | 0 | 0 | 0 | 0 | 8 |
| 6:30 PM | 10 | 0 | 0 | 0 | 0 | 10 | 3 | 0 | 0 | 0 | 0 | 3 | 13 | 0 | 0 | 0 | 0 | 13 |
| 6:45 PM | 13 | 0 | 0 | 0 | 0 | 13 | 1 | 0 | 0 | 0 | 0 | 1 | 14 | 0 | 0 | 0 | 0 | 14 |
| 7:00 PM | 3 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 3 |
| 7:15 PM | 1 | 0 | 0 | 0 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 2 | 3 | 0 | 0 | 0 | 0 | 3 |
| 7:30 PM | 1 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 2 |
| 7:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:00 PM | 3 | 0 | 0 | 0 | 0 | 3 | 1 | 0 | 0 | 0 | 0 | 1 | 4 | 0 | 0 | 0 | 0 | 4 |
| 8:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 1 |
| 8:30 PM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 8:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 9:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 9:15 PM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 9:30 PM | 3 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 3 |
| 9:45 PM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 10:00 PM | 2 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 2 |
| 10:15 PM | 3 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 3 |
| 10:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 10:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 11:00 PM | 2 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 2 |
| 11:15 PM | 3 | 0 | 0 | 0 | 0 | 3 | 0 | 1 | 0 | 0 | 0 | 1 | 3 | 1 | 0 | 0 | 0 | 4 |
| 11:30 PM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 11:45 PM | 1 | 1 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 2 |
| | | | | | | | | | | | | | | | | | | |
| | | 1 | OUND RIGHT | | | | | | BOUND LEFT | | | | | | TOTAL ENT | | | |
| TOTALS | AUTOS | DELIVERY | GARBAGE | SEMI | MC | TOTAL | AUTOS | DELIVERY | GARBAGE | SEMI | MC | TOTAL | AUTOS | DELIVERY | GARBAGE | SEMI | MC | TOTAL |
| AM | 172 | 12 | 1 | 0 | 0 | 185 | 104 | 12 | 3 | 0 | 0 | 119 | 276 | 24 | 4 | 0 | 0 | 304 |
| MIDDAY | 142 | 19 | 0 | 0 | 0 | 161 | 65 | 9 | 0 | 0 | 0 | 74 | 207 | 28 | 0 | 0 | 0 | 235 |
| PM | 191 | 9 | 0 | 0 | 0 | 200 | 56 | 6 | 0 | 0 | 0 | 62 | 247 | 15 | 0 | 0 | 0 | 262 |
| DAILY | 505 | 40 | 1 | 0 | 0 | 546 | 225 | 27 | 3 | 0 | 0 | 255 | 730 | 67 | 4 | 0 | 0 | 801 |



CLIENT: HIRSCH/GREEN TRANSPORTATION CONSULTING, INC.

PROJECT: CHEVAL BLANC HOTEL - BEVERLY HILLS DATE: WEDNESDAY, MAY 22, 2019

PERIOD: 24-HOUR

INTERSECTION: N/S ALLEY (ONE-WAY SB)

| 15 MINUTE | | EASTRO | UND RIGHT | TUDNI EN | ITDV | | | WEST | BOUND LEFT | TUDNI EN | ITDV | | | | TOTAL EN | TDV | | |
|--------------------|--------|----------|-----------|----------------|------|--------|--------|----------------|------------|----------|--------|--------|--------|----------|---------------|------|----|--------|
| (START TIME) | AUTOS | DELIVERY | GARBAGE | SEMI | MC | TOTAL | AUTOS | | | SEMI | MC | TOTAL | AUTOS | DELIVERY | | SEMI | MC | TOTAL |
| ` ' | - | | | | | | | | | | | | | | | | | |
| 12:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 12:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 12:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 12:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 1 |
| 1:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 |
| 1:30 AM | 0 | 0 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1:45 AM | 0 3 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 1 | 0 4 | 1 0 | | 0 | 0 | 1 |
| 2:00 AM | 3 1 | 0 | 0 | | 0 | 3 | 1 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 4 1 |
| 2:15 AM 2:30 AM | 0 | 0 | 0 | 0 | | 1 0 | 2 | 0 | 0 | | | 2 | 2 | 0 | 0 | 0 | | 2 |
| | 1 | | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 1 | 2 | 0 | | 0 | 0 | |
| 2:45 AM 3:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 0 | 0 | | 2 0 |
| | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 3:15 AM | 1 | 0 | | 1 | | | 0 | | 0 | | | 0 | 1 | 0 | 0 | 1 | | |
| 3:30 AM | • | | 0 | | 0 | 2 | | 0 | 0 | 0 | 0 | | | _ | | | 0 | 2 |
| 3:45 AM 4:00 AM | 0 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 0 | 0 | 0 | 0 | 0 0 | 0 | 0 | 0 |
| | | | | | | | | | 1 | | | 1 | | 0 | 1 | | | 0 |
| 4:15 AM 4:30 AM | 3 3 | 0 | 0 | 0 | 0 | 3 3 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 4 3 |
| | | 0 | 0 | | 0 | | 0 | 0 | 0 | 0 | | 0 | 6 | _ | 0 | 0 | 0 | |
| 4:45 AM | 6 4 | 0 | 0 | 0 | 0 | 6 4 | 2 | 0 | 0 | 0 | 0 | 2 | 6 | 0 | 0 | 0 | 0 | 6 6 |
| 5:00 AM | | | | | | | | | 0 | | | 0 | | - | | | | |
| 5:15 AM | 2 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 0 | 0 | 0 | 2 |
| 5:30 AM 5:45 AM | 1 3 | 0 | 0 | 0 | 0 | 1 3 | 1 | 0 | 0 | 0 | 0 0 | 1 | 1 4 | 0 | 0 | 0 | 0 | 1 |
| | | | | | | | | | | | | • | | - | | | | 4 |
| 6:00 AM | 6 | 2 1 | 0 | 0 | 0 | 8 | 0 | 2 0 | 0 | 0 | 0 | 2 1 | 6 3 | 4 1 | 0 1 | 0 | 0 | 10 |
| 6:15 AM | 3 2 | 1 | 1 | 0 | 0 | 4 4 | 0 | 0 | 1 0 | 0 | 0 0 | 0 | 2 | 1 | 1 | 0 | 0 | 5 4 |
| 6:30 AM 6:45 AM | 1 | 0 | 0 | 0 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 2 | 3 | 0 | 0 | 0 | 0 | 3 |
| 7:00 AM | 4 | 0 | 0 | 0 | 0 | 4 | 2 | 0 | 0 | 0 | 0 | 2 | 6 | 0 | 0 | 0 | 0 | 6 |
| 7:15 AM | 2 | 1 | 0 | 0 | 0 | 3 | 0 | 1 | 0 | 0 | 0 | 1 | 2 | 2 | 0 | 0 | 0 | 4 |
| 7:30 AM | 2 | 1 | 0 | 0 | 0 | 3 | 7 | 1 | 0 | 0 | 0 | 8 | 9 | 2 | 0 | 0 | 0 | 11 |
| 7:45 AM | 8 | 0 | 0 | 0 | 0 | 8 | 8 | 0 | 0 | 0 | 0 | 8 | 16 | 0 | 0 | 0 | 0 | 16 |
| 8:00 AM | 4 | 0 | 0 | 0 | 0 | 4 | 4 | 0 | 0 | 0 | 0 | 4 | 8 | 0 | 0 | 0 | 0 | 8 |
| 8:15 AM | 16 | 1 | 0 | 0 | 0 | 17 | 4 | 0 | 0 | 0 | 0 | 4 | 20 | 1 | 0 | 0 | 0 | 21 |
| 8:30 AM | 6 | 0 | 0 | 0 | 0 | 6 | 3 | 0 | 0 | 0 | 0 | 3 | 9 | 0 | 0 | 0 | 0 | 9 |
| 8:45 AM | 14 | 1 | 0 | 0 | 0 | 15 | 10 | 1 | 0 | 0 | 0 | 11 | 24 | 2 | 0 | 0 | 0 | 26 |
| 9:00 AM | 19 | 1 | 0 | 0 | 0 | 20 | 14 | 0 | 0 | 0 | 0 | 14 | 33 | 1 | 0 | 0 | 0 | 34 |
| 9:00 AM 9:15 AM | 11 | 1 | 0 | 0 | 0 | 12 | 14 | 0 | 0 | 0 | 0 | 14 | 25 | 1 | 0 | 0 | 0 | 26 |
| 9:30 AM | 9 | 2 | 0 | 0 | 0 | 11 | 12 | 0 | 0 | 0 | 0 | 12 | 23 | 2 | 0 | 0 | 0 | 23 |
| 9:45 AM | 10 | 2 | 0 | 0 | 0 | 12 | 6 | 0 | 0 | 0 | 0 | 6 | 16 | 2 | 0 | 0 | 0 | 18 |
| 10:00 AM | 13 | 2 | | $-\frac{1}{0}$ | 0 | 15 | | $-\frac{3}{2}$ | | <u> </u> | 0 | 4 | 15 | 4 | - | | 0 | 19 |
| 10:15 AM | 15 | 1 | 0 | 0 | 0 | 16 | 6 | 3 | 0 | 0 | 0 | 9 | 21 | 4 | 0 | 0 | 0 | 25 |
| 10:30 AM | 15 | 0 | 0 | 0 | 0 | 15 | 1 | 0 | 0 | 0 | 0 | 1 | 16 | 0 | 0 | 0 | 0 | 16 |
| 10:45 AM | 5 | 3 | 0 | 0 | 0 | 8 | 2 | 0 | 0 | 0 | 0 | 2 | 7 | 3 | 0 | 0 | 0 | 10 |
| 11:00 AM | 9 | 1 | 0 | 0 | 0 | 10 | 3 | 0 | 0 | 0 | 0 | 3 | 12 | 1 | 0 | 0 | 0 | 13 |
| 11:15 AM | 16 | 0 | 0 | 0 | 0 | 16 | 5 | 1 | 0 | 0 | 0 | 6 | 21 | 1 | 0 | 0 | 0 | 22 |
| 11:30 AM | 14 | 0 | 0 | 0 | 0 | 14 | 5 | 2 | 0 | 0 | 0 | 7 | 19 | 2 | 0 | 0 | 0 | 21 |
| 11:45 AM | 8 | 1 | 0 | 0 | 0 | 9 | 6 | 0 | 0 | 0 | 0 | 6 | 14 | 1 | 0 | 0 | 0 | 15 |
| 12:00 PM | 13 | 4 | 0 | 0 | 0 | 17 | 2 | 1 | 0 | 0 | 0 | 3 | 15 | 5 | 0 | 0 | 0 | 20 |
| 12:15 PM | 2 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 0 | 0 | 0 | 2 | 4 | 0 | 0 | 0 | 0 | 4 |
| 12:30 PM | 5 | 0 | 0 | 0 | 0 | 5 | 4 | 1 | 0 | 0 | 0 | 5 | 9 | 1 | 0 | 0 | 0 | 10 |
| 12:45 PM | 6 | 1 | 0 | 0 | 0 | 7 | 5 | 0 | 0 | 0 | 0 | 5 | 11 | 1 | 0 | 0 | 0 | 12 |
| 1:00 PM | 12 | 1 | 0 | 0 | 1 | 14 | 4 | 0 | 0 | 0 | 0 | 4 | 16 | 1 | 0 | 0 | 1 | 18 |
| 1:15 PM | 7 | 1 | 0 | 0 | 0 | 8 | 3 | 0 | 0 | 0 | 0 | 3 | 10 | 1 | 0 | 0 | 0 | 11 |
| 1:30 PM | 10 | 0 | 0 | 0 | 0 | 10 | 7 | 0 | 0 | 0 | 0 | 7 | 17 | 0 | 0 | 0 | 0 | 17 |
| 1:45 PM | 7 | 0 | 0 | 0 | 0 | 7 | 4 | 2 | 0 | 0 | 0 | 6 | 11 | 2 | 0 | 0 | 0 | 13 |
| 1.43 FIVI | ′ | | | | | ′ | | | | | | | | | | | | 13 |

CLIENT: HIRSCH/GREEN TRANSPORTATION CONSULTING, INC.

PROJECT: CHEVAL BLANC HOTEL - BEVERLY HILLS DATE: WEDNESDAY, MAY 22, 2019

24-HOUR PERIOD:

INTERSECTION: N/S ALLEY (ONE-WAY SB)

| 15 MINUTE | | | OUND RIGHT | TURN EN | NTRY | | | | OUND LEFT | TURN EN | ITRY | | | | TOTAL ENT | | | |
|----------------------|--------|----------|------------|---------|------|--------|--------|----------|-----------|---------|------|-------|--------|----------|-----------|------|----|-------|
| (START TIME) | AUTOS | DELIVERY | GARBAGE | SEMI | MC | TOTAL | AUTOS | DELIVERY | GARBAGE | SEMI | MC | TOTAL | AUTOS | DELIVERY | GARBAGE | SEMI | MC | TOTAL |
| 2:00 PM | 4 | 4 | 0 | 0 | 0 | 8 | 2 | 0 | 0 | 0 | 0 | 2 | 6 | 4 | 0 | 0 | 0 | 10 |
| 2:15 PM | 4 | 0 | 0 | 0 | 0 | 4 | 3 | 0 | 0 | 0 | 0 | 3 | 7 | 0 | 0 | 0 | 0 | 7 |
| 2:30 PM | 12 | 1 | 0 | 0 | 0 | 13 | 4 | 1 | 0 | 0 | 0 | 5 | 16 | 2 | 0 | 0 | 0 | 18 |
| 2:45 PM | 8 | 0 | 0 | 0 | 0 | 8 | 8 | 0 | 0 | 0 | 0 | 8 | 16 | 0 | 0 | 0 | 0 | 16 |
| 3:00 PM | 3 | 1 | 0 | 0 | 0 | 4 | 3 | 0 | 0 | 0 | 0 | 3 | 6 | 1 | 0 | 0 | 0 | 7 |
| 3:15 PM | 4 | 1 | 0 | 0 | 0 | 5 | 2 | 1 | 0 | 0 | 0 | 3 | 6 | 2 | 0 | 0 | 0 | 8 |
| 3:30 PM | 5 | 1 | 0 | 0 | 0 | 6 | 3 | 0 | 0 | 0 | 0 | 3 | 8 | 1 | 0 | 0 | 0 | 9 |
| 3:45 PM | 7 | 1 | 0 | 0 | 0 | 8 | 3 | 0 | 0 | 0 | 0 | 3 | 10 | 1 | 0 | 0 | 0 | 11 |
| 4:00 PM | 7 | 2 | 0 | 0 | 0 | 9 | 1 | 0 | 0 | 0 | 0 | 1 | 8 | 2 | 0 | 0 | 0 | 10 |
| 4:15 PM | 2 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 0 | 0 | 0 | 2 | 4 | 0 | 0 | 0 | 0 | 4 |
| 4:30 PM | 3 | 2 | 0 | 0 | 0 | 5 | 1 | 1 | 0 | 0 | 0 | 2 | 4 | 3 | 0 | 0 | 0 | 7 |
| 4:45 PM | 6 | 2 | 0 | 0 | 0 | 8 | 3 | 0 | 0 | 0 | 0 | 3 | 9 | 2 | 0 | 0 | 0 | 11 |
| 5:00 PM | 5 | 0 | 0 | 0 | 0 | 5 | 1 | 0 | 0 | 0 | 0 | 1 | 6 | 0 | 0 | 0 | 0 | 6 |
| 5:15 PM | 2 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 0 | 0 | 0 | 2 | 4 | 0 | 0 | 0 | 0 | 4 |
| 5:30 PM | 3 | 0 | 0 | 0 | 0 | 3 | 2 | 0 | 0 | 0 | 0 | 2 | 5 | 0 | 0 | 0 | 0 | 5 |
| 5:45 PM | 7 | 0 | 0 | 0 | 0 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 7 | 0 | 0 | 0 | 0 | 7 |
| 6:00 PM | 5 | 1 | 0 | 0 | 0 | 6 | 1 | 0 | 0 | 0 | 0 | 1 | 6 | 1 | 0 | 0 | 0 | 7 |
| 6:15 PM | 5 | 0 | 0 | 0 | 0 | 5 | 1 | 0 | 0 | 0 | 0 | 1 | 6 | 0 | 0 | 0 | 0 | 6 |
| 6:30 PM | 9 | 0 | 0 | 0 | 0 | 9 | 1 | 0 | 0 | 0 | 0 | 1 | 10 | 0 | 0 | 0 | 0 | 10 |
| 6:45 PM | 8 | 0 | 0 | 0 | 0 | 8 | 2 | 0 | 0 | 0 | 0 | 2 | 10 | 0 | 0 | 0 | 0 | 10 |
| 7:00 PM | 2 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 0 | 0 | 0 | 2 | 4 | 0 | 0 | 0 | 0 | 4 |
| 7:15 PM | 2 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 2 |
| 7:30 PM | 1 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 2 |
| 7:45 PM | 2 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 0 | 0 | 0 | 2 | 4 | 0 | 0 | 0 | 0 | 4 |
| 8:00 PM | 2 | 2 | 0 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 0 | 0 | 4 |
| 8:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:30 PM | 0 | 1 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 0 | 0 | 0 | 2 |
| 8:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 0 | 0 | 0 | 2 |
| 9:00 PM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 1 | 1 | 1 | 0 | 0 | 0 | 2 |
| 9:15 PM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 9:30 PM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 9:45 PM | 2 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 2 |
| 10:00 PM | 1 2 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 10:15 PM | 2 | • | · | 0 | 0 | 2 2 | - | 0 | - | - | _ | 0 | 2 | 0 | 0 | 0 | 0 | 2 |
| 10:30 PM 10:45 PM | 2 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 3 |
| | | | 0 | 0 | | 1 | 1 | 0 | 0 | 0 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 2 |
| 11:00 PM 11:15 PM | 1 1 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 2 |
| 11:30 PM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 11:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 2 | 1 | 1 | 0 | 0 | 0 | 2 |
| 11.45 F W | U | U | U | U | U | U | ' | ' | U | U | U | 2 | ' | ' | U | U | U | 2 |
| | | | | | | | | | | | | | | | | | | |
| TOTALC | ALITOO | | OUND RIGHT | | | TOTAL | ALITOO | | OUND LEFT | | | TOTAL | ALITOO | DELIVERY | TOTAL ENT | | MC | TOTAL |
| TOTALS | AUTOS | | GARBAGE . | SEMI | MC | TOTAL | | DELIVERY | GARBAGE | SEMI | MC | TOTAL | AUTOS | DELIVERY | GARBAGE | SEMI | MC | TOTAL |
| AM | 145 | 15 | 1 | 1 | 0 | 162 | 93 | 6 | 2 | 0 | 0 | 101 | 238 | 21 | 3 | 1 | 0 | 263 |
| MIDDAY | 157 | 15 | 0 | 0 | 1 | 173 | 61 | 12 | 0 | 0 | 0 | 73 | 218 | 27 | 0 | 0 | 1 | 246 |
| PM | 133 | 19 | 0 | 0 | 0 | 152 | 57 | 5 | 0 | 0 | 0 | 62 | 190 | 24 | 0 | 0 | 0 | 214 |
| DAILY | 435 | 49 | 1 | 1 | 1 | 487 | 211 | 23 | 2 | 0 | 0 | 236 | 646 | 72 | 3 | 1 | 1 | 723 |



CLIENT: HIRSCH/GREEN TRANSPORTATION CONSULTING, INC.

PROJECT: CHEVAL BLANC HOTEL - BEVERLY HILLS DATE: THURSDAY, MAY 23, 2019

PERIOD: 24-HOUR

INTERSECTION: N/S ALLEY (ONE-WAY SB)

| 45 MINUITE | | EACTD/ | NIND DICLIT | TUDN EN | ITDV | | | WEST | DOLIND LEET | | ITDV | | | | TOTAL EN | TDV | | |
|--------------|-------|----------|-------------|---------|------|-------|-------|------|--------------------|------|------|-------|-------|----------|----------|------|----|-------|
| 15 MINUTE | AUTOS | DELIVERY | GARBAGE | SEMI | MC | TOTAL | AUTOS | | BOUND LEFT GARBAGE | | MC | TOTAL | AUTOS | DELIVERY | TOTAL EN | SEMI | MC | TOTAL |
| (START TIME) | | | | | | | | | - | SEMI | | | | | | | | TOTAL |
| 12:00 AM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 12:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 12:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 1 |
| 12:45 AM | 2 | 1 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 1 | 0 | 0 | 0 | 3 |
| 1:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1:30 AM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 1:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2:00 AM | 0 | 1 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 0 | 0 | 0 | 2 |
| 2:15 AM | 1 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 2 |
| 2:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 1 |
| 2:45 AM | 1 | 0 | 0 | 0 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 2 | 3 | 0 | 0 | 0 | 0 | 3 |
| 3:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 3:15 AM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 3:30 AM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 1 | 1 | 1 | 0 | 0 | 0 | 2 |
| 3:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:00 AM | 1 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 2 |
| 4:15 AM | 6 | 0 | 0 | 0 | 0 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 6 | 0 | 0 | 0 | 0 | 6 |
| 4:30 AM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 1 | 0 | 1 | 0 | 0 | 2 |
| 4:45 AM | 5 | 0 | 0 | 0 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 0 | 0 | 0 | 5 |
| 5:00 AM | 2 | 0 | 0 | 0 | 0 | 2 | 1 | 1 | 0 | 0 | 0 | 2 | 3 | 1 | 0 | 0 | 0 | 4 |
| 5:15 AM | 1 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 0 | 0 | 0 | 2 | 2 | 1 | 0 | 0 | 0 | 3 |
| 5:30 AM | 4 | 0 | 0 | 0 | 0 | 4 | 1 | 0 | 0 | 0 | 0 | 1 | 5 | 0 | 0 | 0 | 0 | 5 |
| 5:45 AM | 2 | 1 | 0 | 0 | 0 | 3 | 2 | 0 | 0 | 0 | 0 | 2 | 4 | 1 | 0 | 0 | 0 | 5 |
| 6:00 AM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 1 | 1 | 1 | 0 | 0 | 0 | 2 |
| 6:15 AM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 6:30 AM | 4 | 0 | 0 | 0 | 0 | 4 | 2 | 0 | 0 | 0 | 0 | 2 | 6 | 0 | 0 | 0 | 0 | 6 |
| 6:45 AM | 1 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 1 | 0 | 0 | 2 | 2 | 0 | 1 | 0 | 0 | 3 |
| 7:00 AM | 7 | 0 | 0 | 0 | 0 | 7 | 1 | 0 | 0 | 0 | 0 | 1 | 8 | 0 | 0 | 0 | 0 | 8 |
| 7:15 AM | 4 | 0 | 0 | 0 | 0 | 4 | 1 | 1 | 0 | 0 | 0 | 2 | 5 | 1 | 0 | 0 | 0 | 6 |
| 7:30 AM | 3 | 0 | 0 | 0 | 0 | 3 | 9 | 0 | 0 | 0 | 0 | 9 | 12 | 0 | 0 | 0 | 0 | 12 |
| 7:45 AM | 5 | 0 | 0 | 0 | 0 | 5 | 6 | 1 | 0 | 0 | 0 | 7 | 11 | 1 | 0 | 0 | 0 | 12 |
| 8:00 AM | 6 | 0 | 0 | 0 | 0 | 6 | 4 | 0 | 0 | 0 | 0 | 4 | 10 | 0 | 0 | 0 | 0 | 10 |
| 8:15 AM | 9 | 1 | 0 | 0 | 0 | 10 | 5 | 0 | 0 | 0 | 0 | 5 | 14 | 1 | 0 | 0 | 0 | 15 |
| 8:30 AM | 15 | 0 | 0 | 0 | 0 | 15 | 4 | 0 | 0 | 0 | 0 | 4 | 19 | 0 | 0 | 0 | 0 | 19 |
| 8:45 AM | 18 | 2 | 0 | 0 | 0 | 20 | 7 | 0 | 0 | 0 | 0 | 7 | 25 | 2 | 0 | 0 | 0 | 27 |
| 9:00 AM | 17 | 0 | 0 | 0 | 0 | 17 | 13 | 0 | 0 | 0 | 0 | 13 | 30 | 0 | 0 | 0 | 0 | 30 |
| 9:15 AM | 11 | 1 | 0 | 0 | 0 | 12 | 15 | 1 | 0 | 0 | 0 | 16 | 26 | 2 | 0 | 0 | 0 | 28 |
| 9:30 AM | 10 | 0 | 0 | 0 | 0 | 10 | 8 | 0 | 0 | 0 | 0 | 8 | 18 | 0 | 0 | 0 | 0 | 18 |
| 9:45 AM | 6 | 11 | 0 | 0 | 0 | 7 | 6 | 0 | 0 | 0 | 0 | 6 | 12 | 1 | 0 | 0 | 0 | 13 |
| 10:00 AM | 11 | 2 | 0 | 0 | 0 | 13 | 6 | 2 | 0 | 0 | 0 | 8 | 17 | 4 | 0 | 0 | 0 | 21 |
| 10:15 AM | 10 | 1 | 0 | 0 | 0 | 11 | 9 | 1 | 0 | 0 | 0 | 10 | 19 | 2 | 0 | 0 | 0 | 21 |
| 10:30 AM | 10 | 3 | 0 | 0 | 0 | 13 | 6 | 0 | 0 | 0 | 0 | 6 | 16 | 3 | 0 | 0 | 0 | 19 |
| 10:45 AM | 14 | 0 | 0 | 0 | 0 | 14 | 7 | 0 | 0 | 0 | 0 | 7 | 21 | 0 | 0 | 0 | 0 | 21 |
| 11:00 AM | 11 | 1 | 0 | 0 | 0 | 12 | 5 | 3 | 0 | 0 | 0 | 8 | 16 | 4 | 0 | 0 | 0 | 20 |
| 11:15 AM | 13 | 2 | 0 | 0 | 0 | 15 | 3 | 1 | 0 | 0 | 0 | 4 | 16 | 3 | 0 | 0 | 0 | 19 |
| 11:30 AM | 12 | 0 | 0 | 0 | 0 | 12 | 7 | 1 | 0 | 0 | 0 | 8 | 19 | 1 | 0 | 0 | 0 | 20 |
| 11:45 AM | 9 | 2 | 0 | 0 | 0 | 11 | 8 | 1 | 0 | 0 | 0 | 9 | 17 | 3 | 0 | 0 | 0 | 20 |
| 12:00 PM | 16 | 2 | 0 | 0 | 0 | 18 | 2 | 0 | 0 | 0 | 0 | 2 | 18 | 2 | 0 | 0 | 0 | 20 |
| 12:15 PM | 4 | 0 | 0 | 0 | 0 | 4 | 5 | 1 | 0 | 0 | 0 | 6 | 9 | 1 | 0 | 0 | 0 | 10 |
| 12:30 PM | 7 | 2 | 0 | 0 | 0 | 9 | 2 | 0 | 0 | 0 | 0 | 2 | 9 | 2 | 0 | 0 | 0 | 11 |
| 12:45 PM | 8 | 0 | 0 | 0 | 0 | 8 | 7 | 1 | 0 | 0 | 0 | 8 | 15 | 1 | 0 | 0 | 0 | 16 |
| 1:00 PM | 12 | 1 | 0 | 0 | 0 | 13 | 2 | 0 | 0 | 0 | 0 | 2 | 14 | 1 | 0 | 0 | 0 | 15 |
| 1:15 PM | 13 | 1 | 0 | 0 | 0 | 14 | 5 | 0 | 0 | 0 | 0 | 5 | 18 | 1 | 0 | 0 | 0 | 19 |
| 1:30 PM | 13 | 1 | 0 | 0 | 0 | 14 | 6 | 0 | 0 | 0 | 0 | 6 | 19 | 1 | 0 | 0 | 0 | 20 |
| 1:45 PM | 10 | 2 | 0 | 0 | 0 | 12 | 11 | 0 | 0 | 0 | 0 | 11 | 11 | 2 | 0 | 0 | 0 | 13 |

CLIENT: HIRSCH/GREEN TRANSPORTATION CONSULTING, INC.

PROJECT: CHEVAL BLANC HOTEL - BEVERLY HILLS

DATE: THURSDAY, MAY 23, 2019 24-HOUR PERIOD:

INTERSECTION: N/S ALLEY (ONE-WAY SB)

| 15 MINUTE | | | OUND RIGHT | TURN EN | ITRY | | | | OUND LEFT | TURN EN | ITRY | | | | TOTAL ENT | | | |
|----------------------|--------|----------|------------|---------|------|--------|--------|----------|------------|---------|------|-------|--------|----------|-----------|------|----|--------|
| (START TIME) | AUTOS | DELIVERY | GARBAGE | SEMI | MC | TOTAL | AUTOS | DELIVERY | GARBAGE | SEMI | MC | TOTAL | AUTOS | DELIVERY | GARBAGE | SEMI | MC | TOTAL |
| 2:00 PM | 13 | 0 | 0 | 0 | 0 | 13 | 4 | 0 | 0 | 0 | 0 | 4 | 17 | 0 | 0 | 0 | 0 | 17 |
| 2:15 PM | 5 | 1 | 0 | 0 | 0 | 6 | 1 | 1 | 0 | 0 | 0 | 2 | 6 | 2 | 0 | 0 | 0 | 8 |
| 2:30 PM | 6 | 0 | 0 | 0 | 0 | 6 | 1 | 0 | 0 | 0 | 0 | 1 | 7 | 0 | 0 | 0 | 0 | 7 |
| 2:45 PM | 12 | 1 | 0 | 0 | 0 | 13 | 7 | 0 | 0 | 0 | 0 | 7 | 19 | 1 | 0 | 0 | 0 | 20 |
| 3:00 PM | 8 | 1 | 0 | 0 | 0 | 9 | 3 | 1 | 0 | 0 | 0 | 4 | 11 | 2 | 0 | 0 | 0 | 13 |
| 3:15 PM | 10 | 1 | 0 | 0 | 0 | 11 | 2 | 1 | 0 | 0 | 0 | 3 | 12 | 2 | 0 | 0 | 0 | 14 |
| 3:30 PM | 11 | 1 | 0 | 0 | 0 | 12 | 3 | 1 | 0 | 0 | 0 | 4 | 14 | 2 | 0 | 0 | 0 | 16 |
| 3:45 PM | 6 | 0 | 0 | 0 | 0 | 6 | 3 | 0 | 0 | 0 | 0 | 3 | 9 | 0 | 0 | 0 | 0 | 9 |
| 4:00 PM | 9 | 0 | 0 | 0 | 0 | 9 | 1 | 0 | 0 | 0 | 0 | 1 | 10 | 0 | 0 | 0 | 0 | 10 |
| 4:15 PM | 7 | 1 | 0 | 0 | 0 | 8 | 1 | 0 | 0 | 0 | 0 | 1 | 8 | 1 | 0 | 0 | 0 | 9 |
| 4:30 PM | 6 | 0 | 0 | 0 | 0 | 6 | 1 | 0 | 0 | 0 | 0 | 1 | 7 | 0 | 0 | 0 | 0 | 7 |
| 4:45 PM | 5 | 0 | 0 | 0 | 0 | 5 | 2 | 0 | 0 | 0 | 0 | 2 | 7 | 0 | 0 | 0 | 0 | 7 |
| 5:00 PM | 7 | 0 | 0 | 0 | 0 | 7 | 3 | 0 | 0 | 0 | 0 | 3 | 10 | 0 | 0 | 0 | 0 | 10 |
| 5:15 PM | 8 | 1 | 0 | 0 | 0 | 9 | 1 | 0 | 0 | 0 | 0 | 1 | 9 | 1 | 0 | 0 | 0 | 10 |
| 5:30 PM | 4 | 0 | 0 | 0 | 0 | 4 | 3 | 0 | 0 | 0 | 0 | 3 | 7 | 0 | 0 | 0 | 0 | 7 |
| 5:45 PM | 10 | 2 | 0 | 0 | 0 | 12 | 5 | 0 | 0 | 0 | 0 | 5 | 15 | 2 | 0 | 0 | 0 | 17 |
| 6:00 PM | 3 | 0 | 0 | 0 | 0 | 3 | 2 | 0 | 0 | 0 | 0 | 2 | 5 | 0 | 0 | 0 | 0 | 5 |
| 6:15 PM | 4 | 0 | 0 | 0 | 0 | 4 | 1 | 0 | 0 | 0 | 0 | 1 | 5 | 0 | 0 | 0 | 0 | 5 |
| 6:30 PM | 4 | 0 | 0 | 0 | 0 | 4 | 2 | 0 | 0 | 0 | 0 | 2 | 6 | 0 | 0 | 0 | 0 | 6 |
| 6:45 PM | 15 | 0 | 0 | 0 | 0 | 15 | 4 | 0 | 0 | 0 | 0 | 4 | 19 | 0 | 0 | 0 | 0 | 19 |
| 7:00 PM | 3 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 3 |
| 7:15 PM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 7:30 PM | 1 | 1 | 0 | 0 | 0 | 2 | 1 | 0 | 0 | 0 | 0 | 1 | 2 | 1 | 0 | 0 | 0 | 3 |
| 7:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:00 PM | 1 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 2 |
| 8:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 0 | 0 | 0 | 2 |
| 9:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 9:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 2 | 1 | 1 | 0 | 0 | 0 | 2 |
| 9:30 PM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 9:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 10:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 10:15 PM | 3 | 0 | 0 | 0 | 0 | 3 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 3 |
| 10:30 PM | 0 | | 0 | 0 | 0 | 1 | 0 | 0 | 0 | | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 |
| 10:45 PM | 1 | 0 | 0 | 0 | 0 | • | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 0 | 0 | 0 | 0 | 1 0 |
| 11:00 PM 11:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 11:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 11:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 1 |
| 11.43 FIVI | U | U | J | U | J | J | | J | U | J | U | | | U | J | J | U | ' |
| | | | | | | | | | | | | | | | | | | |
| TOTALS | ALITOO | | OUND RIGHT | | | TOTAL | ALITOO | | SOUND LEFT | | | TOTAL | ALITOO | DELIVERY | TOTAL ENT | | MC | TOTAL |
| TOTALS | AUTOS | | GARBAGE | SEMI | МС | TOTAL | | DELIVERY | GARBAGE | SEMI | MC | TOTAL | | DELIVERY | GARBAGE | SEMI | MC | TOTAL |
| AM | 148 | 8 | 0 | 0 | 0 | 156 | 93 | 8 | 2 | 0 | 0 | 103 | 241 | 16 | 2 | 0 | 0 | 259 |
| MIDDAY | 173 | 20 | 0 | 0 | 0 | 193 | 81 | 11 | 0 | 0 | 0 | 92 | 254 | 31 | 0 | 0 | 0 | 285 |
| PM | 164 | 10 | 0 | 0 | 0 | 174 | 56 | 5 | 0 | 0 | 0 | 61 | 220 | 15 | 0 | 0 | 0 | 235 |
| DAILY | 485 | 38 | 0 | 0 | 0 | 523 | 230 | 24 | 2 | 0 | 0 | 256 | 715 | 62 | 2 | 0 | 0 | 779 |



CLIENT: HIRSCH/GREEN TRANSPORTATION CONSULTING, INC.

PROJECT: CHEVAL BLANC HOTEL - BEVERLY HILLS

DATE: FRIDAY, MAY 24, 2019

PERIOD: 24-HOUR

INTERSECTION: N/S ALLEY (ONE-WAY SB)

| 15 MINUTE | | EASTRO | UND RIGHT | TUDNI EN | ITDV | | | WEST | BOUND LEFT | TUDNI EN | ITDV | | | | TOTAL EN | TDV | | |
|----------------------|--------|----------|-----------|----------|------|--------|-------|--------|------------|----------|------|-------|-------|----------|----------|------|----|--------|
| (START TIME) | ALITOS | DELIVERY | GARBAGE | SEMI | MC | TOTAL | AUTOS | | 1 | SEMI | MC | TOTAL | AUTOS | DELIVERY | | SEMI | MC | TOTAL |
| | | | | | | | | | | | | | | | | | | |
| 12:00 AM 12:15 AM | 1 0 | 0 1 | 0 | 0 | 0 | 1 | 0 | 0 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 1 |
| 12:30 AM | 0 | 0 | 0 | 0 | 0 | 1 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 0 | 0 | 0 | 0 | 0 |
| | 1 | | 0 | 0 | | | 0 | 0 | 0 | | | 0 | - | | | 0 | | 1 |
| 12:45 AM | 1 | 0 0 | | 0 | 0 | 1 | 0 | | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | |
| 1:00 AM | | | 0 | | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | | 0 | | | 0 | 1 |
| 1:15 AM | 0 | 0 | | 0 | 0 | 0 | | 0 | | 0 | 0 | | 0 | - | 0 | 0 | 0 | 0 |
| 1:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 1 |
| 2:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 1 |
| 2:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 1 |
| 2:45 AM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 3:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 1 |
| 3:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 3:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 1 |
| 3:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:00 AM | 1 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 2 |
| 4:15 AM | 1 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 2 |
| 4:30 AM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 1 | 0 | 1 | 0 | 0 | 2 |
| 4:45 AM | 2 | 0 | 0 | 0 | 0 | 2 | 1 | 0 | 0 | 0 | 0 | 1 | 3 | 0 | 0 | 0 | 0 | 3 |
| 5:00 AM | 7 | 0 | 0 | 0 | 0 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 7 | 0 | 0 | 0 | 0 | 7 |
| 5:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 1 |
| 5:30 AM | 2 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 2 |
| 5:45 AM | 1 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 2 |
| 6:00 AM | 3 | 1 | 0 | 0 | 0 | 4 | 4 | 0 | 0 | 0 | 0 | 4 | 7 | 1 | 0 | 0 | 0 | 8 |
| 6:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 1 | 0 | 0 | 6 | 5 | 0 | 1 | 0 | 0 | 6 |
| 6:30 AM | 3 | 0 | 0 | 0 | 0 | 3 | 1 | 1 | 0 | 0 | 0 | 2 | 4 | 1 | 0 | 0 | 0 | 5 |
| 6:45 AM | 2 | 0 | 0 | 0 | 0 | 2 | 1 | 0 | 0 | 0 | 0 | 1 | 3 | 0 | 0 | 0 | 0 | 3 |
| 7:00 AM | 3 | 0 | 0 | 0 | 0 | 3 | 2 | 0 | 0 | 0 | 0 | 2 | 5 | 0 | 0 | 0 | 0 | 5 |
| 7:15 AM | 5 | 0 | 0 | 0 | 0 | 5 | 1 | 0 | 0 | 0 | 0 | 1 | 6 | 0 | 0 | 0 | 0 | 6 |
| 7:30 AM | 6 | 0 | 0 | 0 | 0 | 6 | 5 | 0 | 0 | 0 | 0 | 5 | 11 | 0 | 0 | 0 | 0 | 11 |
| 7:45 AM | 15 | 0 | 0 | 0 | 0 | 15 | 3 | 0 | 0 | 0 | 0 | 3 | 18 | 0 | 0 | 0 | 0 | 18 |
| 8:00 AM | 6 | 0 | 0 | 0 | 0 | 6 | 4 | 1 | 0 | 0 | 0 | 5 | 10 | 1 | 0 | 0 | 0 | 11 |
| 8:15 AM | 13 | 1 | 0 | 0 | 0 | 14 | 3 | 0 | 0 | 0 | 0 | 3 | 16 | 1 | 0 | 0 | 0 | 17 |
| 8:30 AM | 9 | 0 | 0 | 0 | 1 | 10 | 6 | 0 | 0 | 0 | 0 | 6 | 15 | 0 | 0 | 0 | 1 | 16 |
| 8:45 AM | 17 | 2 | 0 | 0 | 1 | 20 | 9 | 0 | 0 | 0 | 0 | 9 | 26 | 2 | 0 | 0 | 1 | 29 |
| 9:00 AM | 17 | 0 | 0 | 0 | 0 | 17 | 19 | 0 | 0 | 0 | 1 | 20 | 36 | 0 | 0 | 0 | 1 | 37 |
| 9:15 AM | 13 | 1 | 0 | 0 | 0 | 14 | 11 | 0 | 0 | 0 | 0 | 11 | 24 | 1 | 0 | 0 | 0 | 25 |
| 9:30 AM | 9 | 1 | 0 | 0 | 0 | 10 | 11 | 1 | 0 | 0 | 0 | 12 | 20 | 2 | 0 | 0 | 0 | 22 |
| 9:45 AM | 8 | 0 | 00 | 0 | 0 | 8 | 8 | 1_ | 0 | 0 | 0 | 9 | 16 | 11 | 0 | 0 | 0 | 17 |
| 10:00 AM | 12 | 0 | 0 | 0 | 0 | 12 | 3 | 0 | 0 | 0 | 0 | 3 | 15 | 0 | 0 | 0 | 0 | 15 |
| 10:15 AM | 8 | 2 | 0 | 0 | 0 | 10 | 2 | 2 | 0 | 0 | 0 | 4 | 10 | 4 | 0 | 0 | 0 | 14 |
| 10:30 AM | 9 | 2 | 0 | 0 | 0 | 11 | 6 | 0 | 0 | 0 | 0 | 6 | 15 | 2 | 0 | 0 | 0 | 17 |
| 10:45 AM | 10 | 1 | 0 | 0 | 0 | 11 | 2 | 2 | 0 | 0 | 1 | 5 | 12 | 3 | 0 | 0 | 1 | 16 |
| 11:00 AM | 9 | 1 | 0 | 0 | 0 | 10 | 2 | 0 | 0 | 0 | 0 | 2 | 11 | 1 | 0 | 0 | 0 | 12 |
| 11:15 AM | 11 | 1 | 0 | 0 | 0 | 12 | 3 | 0 | 0 | 0 | 0 | 3 | 14 | 1 | 0 | 0 | 0 | 15 |
| 11:30 AM | 9 | 0 | 0 | 0 | 0 | 9 | 8 | 0 | 0 | 0 | 0 | 8 | 17 | 0 | 0 | 0 | 0 | 17 |
| 11:45 AM | 9 | 2 | 0 | 0 | 0 | 11 | 5 | 1 | 0 | 0 | 0 | 6 | 14 | 3 | 0 | 0 | 0 | 17 |
| 12:00 PM | 9 | 1 | 0 | 0 | 0 | 10 | 1 | 2 | 0 | 0 | 0 | 3 | 10 | 3 | 0 | 0 | 0 | 13 |
| 12:15 PM | 7 | 0 | 0 | 0 | 0 | 7 | 9 | 0 | 0 | 0 | 0 | 9 | 16 | 0 | 0 | 0 | 0 | 16 |
| 12:30 PM | 14 | 1 | 0 | 0 | 0 | 15 | 3 | 0 | 0 | 0 | 0 | 3 | 17 | 1 | 0 | 0 | 0 | 18 |
| 12:45 PM | 7 | 1 | 0 | 0 | 0 | 8 | 3 | 0 | 0 | 0 | 0 | 3 | 10 | 1 | 0 | 0 | 0 | 11 |
| 1:00 PM | 25 | 2 | 0 | 0 | 0 | 27 | 3 | 0 | 0 | 0 | 0 | 3 | 28 | 2 | 0 | 0 | 0 | 30 |
| 1:15 PM | 6 | 0 | 0 | 0 | 0 | 6 | 3 | 0 | 0 | 0 | 0 | 3 | 9 | 0 | 0 | 0 | 0 | 9 |
| 1:30 PM | 16 | 0 | 0 | 0 | 0 | 16 | 5 | 0 | 0 | 0 | 0 | 5 | 21 | 0 | 0 | 0 | 0 | 21 |
| 1:45 PM | 6 | 0 | 0 | 0 | 0 | 6 | 9 | 0 | 0 | 0 | 0 | 9 | 15 | 0 | 0 | 0 | 0 | 15 |

CLIENT: HIRSCH/GREEN TRANSPORTATION CONSULTING, INC.

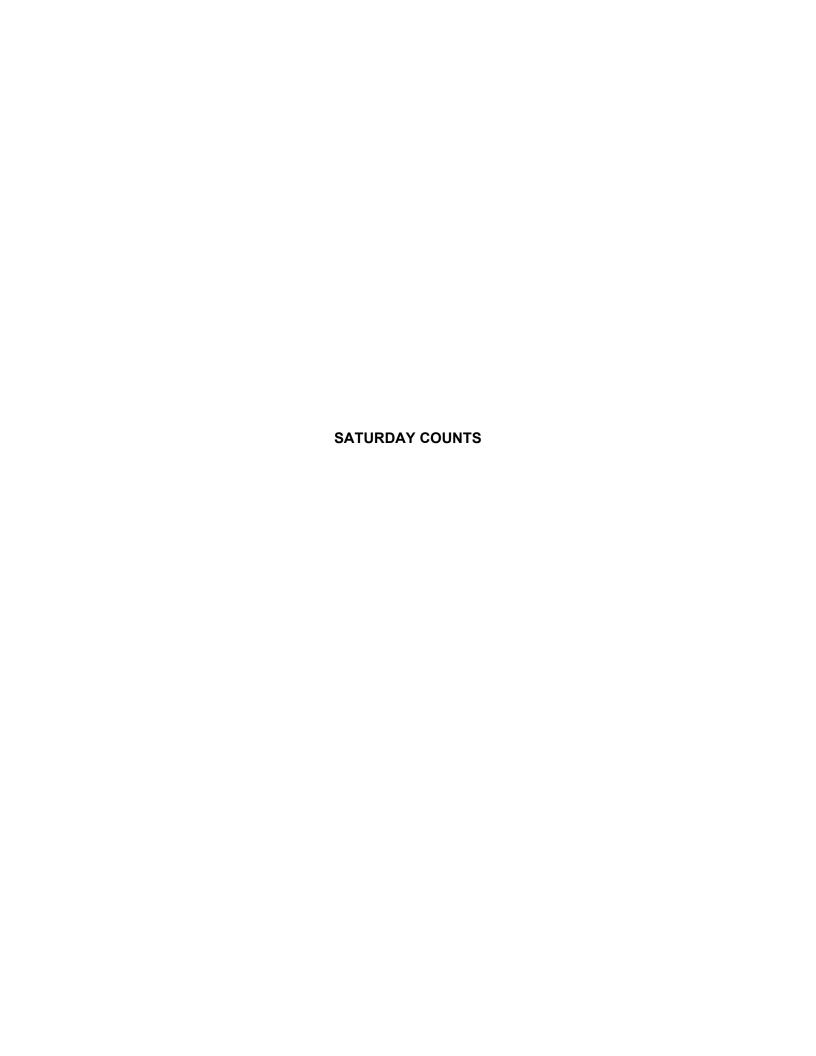
PROJECT: CHEVAL BLANC HOTEL - BEVERLY HILLS

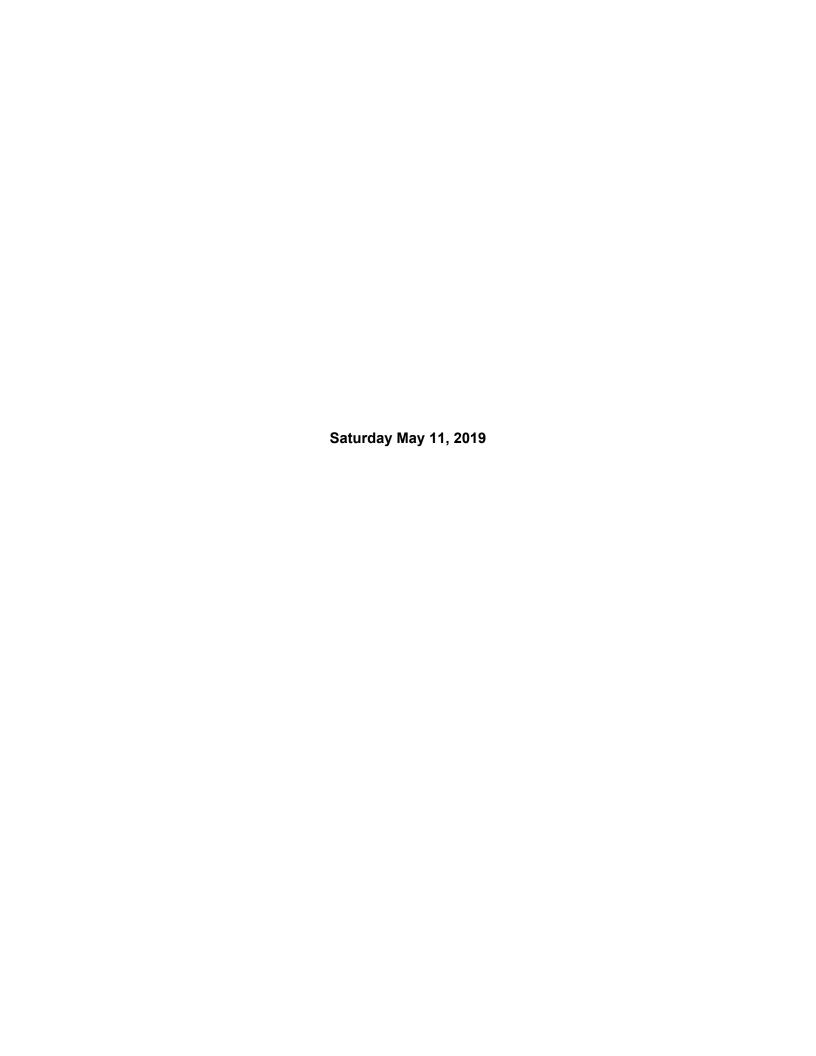
DATE: FRIDAY, MAY 24, 2019

PERIOD: 24-HOUR

INTERSECTION: N/S ALLEY (ONE-WAY SB)

| | | OANTA MON | | | | | | | | | | | | | | | | |
|---------------------|--------|-----------|------------|---------|------|--------|-------|----------|-----------|----------|-----|-------|--------|----------|-----------|------|----|--------|
| 15 MINUTE | | | OUND RIGHT | | ITRY | | | | OUND LEFT | | TRY | | | | TOTAL ENT | | | |
| (START TIME) | AUTOS | DELIVERY | GARBAGE | SEMI | MC | TOTAL | AUTOS | DELIVERY | GARBAGE | SEMI | MC | TOTAL | AUTOS | DELIVERY | GARBAGE | SEMI | MC | TOTAL |
| 2:00 PM | 8 | 4 | 0 | 0 | 0 | 12 | 1 | 0 | 0 | 0 | 0 | 1 | 9 | 4 | 0 | 0 | 0 | 13 |
| 2:15 PM | 9 | 0 | 0 | 0 | 0 | 9 | 1 | 0 | 0 | 0 | 0 | 1 | 10 | 0 | 0 | 0 | 0 | 10 |
| 2:30 PM | 11 | 0 | 0 | 0 | 0 | 11 | 3 | 0 | 0 | 0 | 0 | 3 | 14 | 0 | 0 | 0 | 0 | 14 |
| 2:45 PM | 5 | 0 | 0 | 0 | 0 | 5 | 3 | 0 | 0 | 0 | 0 | 3 | 8 | 0 | 0 | 0 | 0 | 8 |
| 3:00 PM | 10 | 2 | 0 | 0 | 0 | 12 | 7 | 0 | 0 | 0 | 0 | 7 | 17 | 2 | 0 | 0 | 0 | 19 |
| 3:15 PM | 10 | 0 | 0 | 0 | 0 | 10 | 3 | 0 | 0 | 0 | 0 | 3 | 13 | 0 | 0 | 0 | 0 | 13 |
| 3:30 PM | 12 | 1 | 0 | 0 | 0 | 13 | 3 | 1 | 0 | 0 | 0 | 4 | 15 | 2 | 0 | 0 | 0 | 17 |
| 3:45 PM | 7 | 0 | 0 | 0 | 0 | 7 | 7 | 0 | 0 | 0 | 0 | 7 | 14 | 0 | 0 | 0 | 0 | 14 |
| 4:00 PM | 6 | 1 | 0 | 0 | 0 | 7 | 3 | 0 | 0 | 0 | 0 | 3 | 9 | 1 | 0 | 0 | 0 | 10 |
| 4:15 PM | 6 | 0 | 0 | 0 | 0 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 6 | 0 | 0 | 0 | 0 | 6 |
| 4:30 PM | 5 | 0 | 0 | 0 | 0 | 5 | 1 | 0 | 0 | 0 | 0 | 1 | 6 | 0 | 0 | 0 | 0 | 6 |
| 4:45 PM | 4 | 0 | 0 | 0 | 0 | 4 | 3 | 0 | 0 | 0 | 1 | 4 | 7 | 0 | 0 | 0 | 1 | 8 |
| 5:00 PM | 6 | 0 | 0 | 0 | 0 | 6 | 3 | 1 | 0 | 0 | 0 | 4 | 9 | 1 | 0 | 0 | 0 | 10 |
| 5:15 PM | 5 | 1 | 0 | 0 | 0 | 6 | 1 | 0 | 0 | 0 | 0 | 1 | 6 | 1 | 0 | 0 | 0 | 7 |
| 5:30 PM | 7 | 0 | 0 | 0 | 0 | 7 | 1 | 0 | 0 | 0 | 0 | 1 | 8 | 0 | 0 | 0 | 0 | 8 |
| 5:45 PM | 8 | 0 | 0 | 0 | 0 | 8 | 1 | 0 | 0 | 0 | 0 | 1 | 9 | 0 | 0 | 0 | 0 | 9 |
| 6:00 PM | 5 | 0 | 0 | 0 | 0 | 5 | 2 | 0 | 0 | 0 | 0 | 2 | 7 | 0 | 0 | 0 | 0 | 7 |
| 6:15 PM | 6 | 0 | 0 | 0 | 0 | 6 | 1 | 0 | 0 | 0 | 0 | 1 | 7 | 0 | 0 | 0 | 0 | 7 |
| 6:30 PM | 2 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 0 | 0 | 0 | 2 | 4 | 0 | 0 | 0 | 0 | 4 |
| 6:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 1 |
| 7:00 PM | 2 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 2 |
| 7:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 0 | 0 | 0 | 2 |
| 7:30 PM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 7:45 PM | 1 | 0 | 0 | 0 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 2 | 3 | 0 | 0 | 0 | 0 | 3 |
| 8:00 PM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 8:15 PM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 8:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 9:00 PM | 2 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 2 |
| 9:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 9:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | 0 | - | | | 0 | | 0 | 0 | 0 | 0 |
| 9:45 PM 10:00 PM | 1 0 | 0 | 0 | 0 | 0 | 1 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 0 | 0 | 0 | 0 | 0 | 1 0 |
| 10:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 10:30 PM | 3 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 3 |
| 10:45 PM | 3 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 3 |
| 11:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 11:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 11:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 11:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | | | • | | | - | | | • | | | • | | | | - | | |
| | | EASTRO | OUND RIGHT | TUDNIEN | ITDV | | | WEST | OUND LEFT | TUDNI EN | TDV | | | | TOTAL ENT | TDV | | |
| TOTALS | AUTOS | | GARBAGE | SEMI | MC | TOTAL | AUTOS | DELIVERY | GARBAGE | SEMI | MC | TOTAL | AUTOS | DELIVERY | GARBAGE | SEMI | MC | TOTAL |
| AM | 148 | 7 | 0 | 0 | 2 | 157 | 101 | 6 | 2 | 0 | 1 | 110 | 249 | 13 | 2 | 0 | 3 | 267 |
| MIDDAY | 167 | 14 | 0 | 0 | 0 | 181 | 67 | 7 | 0 | 0 | 1 | 75 | 234 | 21 | 0 | 0 | 1 | 256 |
| PM | 147 | 9 | 0 | 0 | 0 | 156 | 51 | 2 | 0 | 0 | 1 | 54 | 198 | 11 | 0 | 0 | 1 | 210 |
| DAILY | 462 | 30 | 0 | 0 | 2 | 494 | 219 | 15 | 2 | 0 | 3 | 239 | 681 | 45 | 2 | 0 | 5 | 733 |
| DAILT | 402 | 30 | U | U | 2 | 494 | 219 | 10 | 2 | U | 3 | 239 | 001 | 40 | 2 | U | 5 | 133 |





CLIENT: HIRSCH/GREEN TRANSPORTATION CONSULTING, INC.

PROJECT: CHEVAL BLANC HOTEL - BEVERLY HILLS

DATE: SATURDAY, MAY 11, 2019

PERIOD: 24-HOUR

INTERSECTION: N/S ALLEY (ONE-WAY SB)

| 45 MINUITE | | FACTR | NIND DICUT | TUDN EN | ITDV | | | WEST | BOUND LEET | TUDN E | UTDV | | | | TOTAL EN | ITDV | | |
|---------------------------|---------|----------|------------|---------|------|---------|--------|----------|------------|--------|------|--------|----------|-----------|----------|--------|----|----------|
| 15 MINUTE (START TIME) | AUTOS | DELIVERY | GARBAGE | SEMI | MC | TOTAL | AUTOS | DELIVERY | GARBAGE | SEMI | MC | TOTAL | AUTOS | DELIVERY | TOTAL EN | 1 | MC | TOTAL |
| , | - | | | | | | | | | | | | | | • | | | |
| 12:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 12:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 12:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 12:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 3:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 3:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 3:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 3:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:15 AM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 4:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 0 | 0 | 0 | 2 |
| 4:45 AM | 4 | 0 | 0 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 4 |
| 5:00 AM | 1 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 2 |
| 5:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 1 |
| 5:30 AM | 2 | 1 | 0 | 0 | 0 | 3 | 0 | 0 | 1 | 0 | 0 | 1 | 2 | 1 | 1 | 0 | 0 | 4 |
| 5:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 2 | 1 | 0 | 1 | 0 | 0 | 2 |
| 6:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 6:15 AM | 2 | 0 | 0 | 0 | 0 | 2 | 1 | 0 | 0 | 0 | 0 | 1 | 3 | 0 | 0 | 0 | 0 | 3 |
| 6:30 AM | 2 | 0 | 0 | 0 | 0 | 2 | 1 | 0 | 0 | 0 | 0 | 1 | 3 | 0 | 0 | 0 | 0 | 3 |
| 6:45 AM | 2 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 2 |
| 7:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 0 | 0 | 0 | 2 |
| 7:15 AM | 1 | 0 | 1 | 0 | 0 | 2 | 2 | 0 | 0 | 0 | 0 | 2 | 3 | 0 | 1 | 0 | 0 | 4 |
| 7:30 AM | 5 | 0 | 0 | 0 | 0 | 5 | 3 | 0 | 0 | 0 | 0 | 3 | 8 | 0 | 0 | 0 | 0 | 8 |
| 7:45 AM | 3 | 0 | 0 | 0 | 0 | 3 | 4 | 0 | 0 | 0 | 0 | 4 | 7 | 0 | 0 | 0 | 0 | 7 |
| 8:00 AM | 5 | 0 | 0 | 0 | 0 | 5 | 1 | 1 | 0 | 0 | 0 | 2 | 6 | 1 | 0 | 0 | 0 | 7 |
| 8:15 AM | 4 | 0 | 0 | 0 | 0 | 4 | 3 | 0 | 0 | 0 | 0 | 3 | 7 | 0 | 0 | 0 | 0 | 7 |
| 8:30 AM | 6 | 0 | 0 | 0 | 0 | 6 | 6 | 0 | 0 | 0 | 0 | 6 | 12 | 0 | 0 | 0 | 0 | 12 |
| 8:45 AM | 9 | 0 | 0 | 0 | 0 | 9 | 15 | 0 | 0 | 0 | 0 | 15 | 24 | 0 | 0 | 0 | 0 | 24 |
| 9:00 AM | 19 | 0 | 0 | 0 | 0 | 19 | 11 | 0 | 0 | 0 | 0 | 11 | 30 | 0 | 0 | 0 | 0 | 30 |
| 9:15 AM | 9 | 0 | 0 | 0 | 0 | 9 | 15 | 1 | 0 | 0 | 0 | 16 | 24 | 1 | 0 | 0 | 0 | 25 |
| 9:30 AM | 12 | 0 | 0 | 0 | 0 | 12 | 9 | 0 | 0 | 0 | 0 | 9 | 21 | 0 | 0 | 0 | 0 | 21 |
| 9:45 AM | | 0 | | 0 | 0 | | 5 | <u> </u> | 0 | 0 | 00 | 5 | 13 | | 0 | 0 | 0 | 13 |
| 10:00 AM | 7 | 0 | 0 | 0 | 0 | 7 | 3 | 0 | 0 | 0 | 0 | 3 | 10 | 0 1 | 0 | 0 | 0 | 10 |
| 10:15 AM | 6 | 1 | | | | 7 | 5 | | | 0 | 0 | 5 | 11 | | | | 0 | 12 |
| 10:30 AM 10:45 AM | 2 | 3 0 | 0 | 0 | 0 | 5 5 | 8 7 | 0 | 0 | 0 | 0 | 8 7 | 10 12 | 3 0 | 0 | 0 | 0 | 13 12 |
| 11:00 AM | 5 | | 0 | 0 | 0 | 5 7 | | | 0 | | | | | 1 | 0 | 0 | 0 | |
| 11:15 AM | 6 8 | 1 0 | 0 | 0 | 0 | 8 | 2 5 | 0 | 0 | 0 | 0 | 2 5 | 8 13 | 0 | 0 | 0 | 0 | 9 13 |
| | | | | | 0 | | | | | | | | | | | | | |
| 11:30 AM 11:45 AM | 11 8 | 0 | 0 | 1 0 | 0 | 12 8 | 5 3 | 0 1 | 0 | 0 | 0 | 5 4 | 16 11 | 0 1 | 0 | 1 0 | 0 | 17 12 |
| 11:45 AM 12:00 PM | | 0 | 0 | | 0 | | | 0 | 0 | 0 | 0 | 4 | 11 | 0 | 0 | 0 | 0 | 12 |
| | 14 | | | 0 | | 14 | 4 | | | | | | | | | | | |
| 12:15 PM 12:30 PM | 9 | 0 | 0 | 0 | 0 | 9 15 | 5 | 1 0 | 0 | 0 | 0 | 6 3 | 14 17 | 1 1 | 0 | 0 | 0 | 15 |
| 12:30 PM 12:45 PM | 14 5 | 1 0 | 0 | 0 | 0 | 15 5 | 3 2 | 0 | 0 | 0 | 0 | 2 | 17 7 | 0 | 0 | 0 | 0 | 18 7 |
| 1:00 PM | 9 | 0 | 0 | 0 | 0 | 9 | 2 | 0 | 0 | 0 | 0 | 2 | 11 | 0 | 0 | 0 | 0 | 11 |
| 1:00 PM 1:15 PM | 9 | 0 | 0 | 0 | 0 | 9 | 6 | 0 | 0 | 0 | 0 | 6 | 15 | 0 | 0 | 0 | 0 | 15 |
| 1:30 PM | 6 | 0 | 0 | 0 | 0 | 6 | 2 | 0 | 0 | 0 | 0 | 2 | 8 | 0 | 0 | 0 | 0 | 8 |
| 1:45 PM | 5 | 0 | 0 | 0 | 0 | 5 | 4 | 1 | 0 | 0 | 0 | 5 | 9 | 1 | 0 | 0 | 0 | 10 |
| 1.+3 F IVI | | | | | | | | | | | | | | . | | | | 10 |

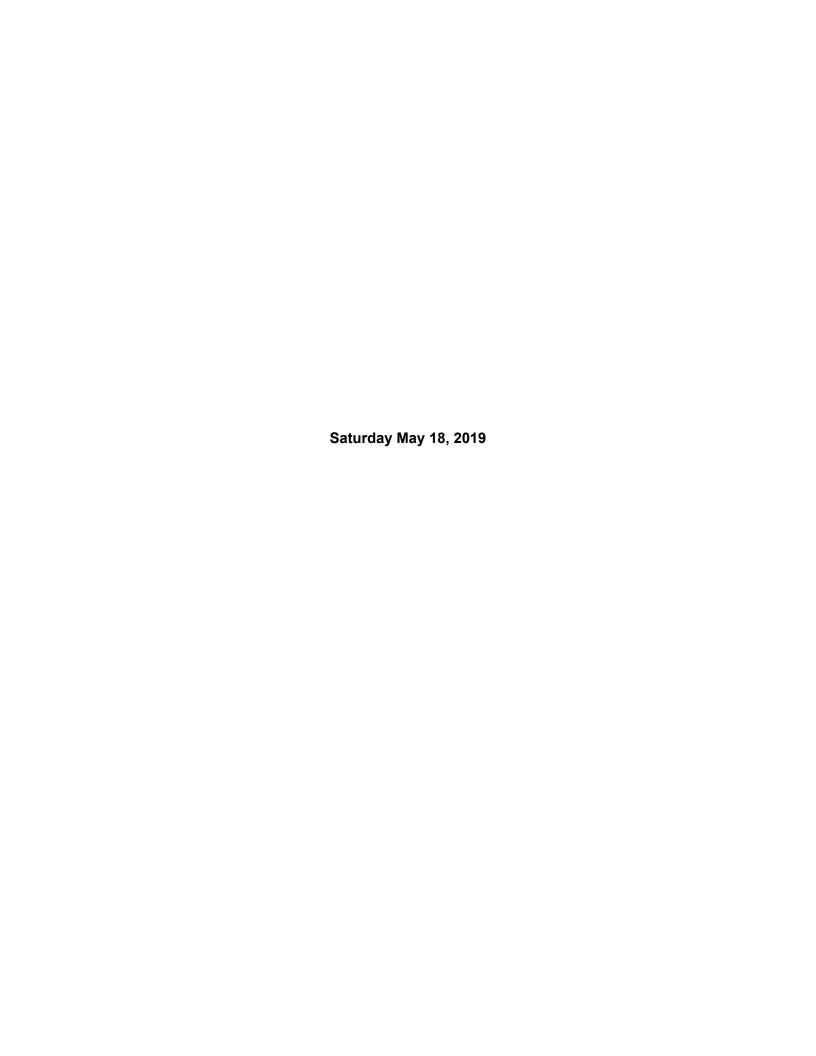
CLIENT: HIRSCH/GREEN TRANSPORTATION CONSULTING, INC.

PROJECT: CHEVAL BLANC HOTEL - BEVERLY HILLS

DATE: SATURDAY, MAY 11, 2019 **PERIOD:** 24-HOUR

INTERSECTION: N/S ALLEY (ONE-WAY SB)

| 15 MINUTE | | | OUND RIGHT | TURN EN | ITRY | | | WESTE | OUND LEFT | TURN EN | ITRY | | | | TOTAL ENT | RY | | |
|--------------|-------|----------|------------|---------|------|-------|-------|----------|------------|---------|------|-------|-------|----------|-----------|------|----|-------|
| (START TIME) | AUTOS | DELIVERY | GARBAGE | SEMI | MC | TOTAL | AUTOS | DELIVERY | GARBAGE | SEMI | MC | TOTAL | AUTOS | DELIVERY | GARBAGE | SEMI | MC | TOTAL |
| 2:00 PM | 8 | 0 | 0 | 0 | 0 | 8 | 3 | 0 | 0 | 0 | 0 | 3 | 11 | 0 | 0 | 0 | 0 | 11 |
| 2:15 PM | 5 | 0 | 0 | 0 | 0 | 5 | 3 | 0 | 0 | 0 | 0 | 3 | 8 | 0 | 0 | 0 | 0 | 8 |
| 2:30 PM | 13 | 0 | 0 | 0 | 0 | 13 | 4 | 1 | 0 | 0 | 0 | 5 | 17 | 1 | 0 | 0 | 0 | 18 |
| 2:45 PM | 12 | 0 | 0 | 0 | 0 | 12 | 2 | 0 | 0 | 0 | 0 | 2 | 14 | 0 | 0 | 0 | 0 | 14 |
| 3:00 PM | 9 | 0 | 0 | 0 | 0 | 9 | 4 | 0 | 0 | 0 | 0 | 4 | 13 | 0 | 0 | 0 | 0 | 13 |
| 3:15 PM | 7 | 1 | 0 | 0 | 0 | 8 | 2 | 1 | 0 | 0 | 0 | 3 | 9 | 2 | 0 | 0 | 0 | 11 |
| 3:30 PM | 9 | 1 | 0 | 0 | 0 | 10 | 5 | 0 | 0 | 0 | 0 | 5 | 14 | 1 | 0 | 0 | 0 | 15 |
| 3:45 PM | 18 | 0 | 0 | 0 | 0 | 18 | 2 | 0 | 0 | 0 | 0 | 2 | 20 | 0 | 0 | 0 | 0 | 20 |
| 4:00 PM | 6 | 0 | 0 | 0 | 0 | 6 | 0 | 1 | 0 | 0 | 0 | 1 | 6 | 1 | 0 | 0 | 0 | 7 |
| 4:15 PM | 5 | 0 | 0 | 0 | 0 | 5 | 3 | 0 | 0 | 0 | 0 | 3 | 8 | 0 | 0 | 0 | 0 | 8 |
| 4:30 PM | 12 | 0 | 0 | 0 | 0 | 12 | 2 | 0 | 0 | 0 | 0 | 2 | 14 | 0 | 0 | 0 | 0 | 14 |
| 4:45 PM | 12 | 0 | 0 | 0 | 0 | 12 | 0 | 0 | 0 | 0 | 0 | 0 | 12 | 0 | 0 | 0 | 0 | 12 |
| 5:00 PM | 11 | 0 | 0 | 0 | 0 | 11 | 1 | 0 | 0 | 0 | 0 | 1 | 12 | 0 | 0 | 0 | 0 | 12 |
| 5:15 PM | 9 | 0 | 0 | 0 | 0 | 9 | 5 | 0 | 0 | 0 | 0 | 5 | 14 | 0 | 0 | 0 | 0 | 14 |
| 5:30 PM | 6 | 0 | 0 | 0 | 0 | 6 | 4 | 0 | 0 | 0 | 0 | 4 | 10 | 0 | 0 | 0 | 0 | 10 |
| 5:45 PM | 3 | 0 | 0 | 0 | 0 | 3 | 4 | 0 | 0 | 0 | 0 | 4 | 7 | 0 | 0 | 0 | 0 | 7 |
| 6:00 PM | 1 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 2 |
| 6:15 PM | 4 | 0 | 0 | 0 | 0 | 4 | 1 | 0 | 0 | 0 | 0 | 1 | 5 | 0 | 0 | 0 | 0 | 5 |
| 6:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 0 | 0 | 0 | 2 |
| 6:45 PM | 2 | 0 | 0 | 0 | 0 | 2 | 1 | 0 | 0 | 0 | 0 | 1 | 3 | 0 | 0 | 0 | 0 | 3 |
| 7:00 PM | 2 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 0 | 0 | 0 | 2 | 4 | 0 | 0 | 0 | 0 | 4 |
| 7:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:30 PM | 3 | 0 | 0 | 0 | 0 | 3 | 1 | 0 | 0 | 0 | 0 | 1 | 4 | 0 | 0 | 0 | 0 | 4 |
| 7:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:00 PM | 1 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 2 |
| 8:15 PM | 2 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 2 |
| 8:30 PM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 8:45 PM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 9:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 9:15 PM | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 |
| 9:30 PM | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 |
| 9:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 10:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 10:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 10:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 10:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 11:00 PM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 11:15 PM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 11:30 PM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 11:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 1 |
| | | | | | | | | | | | | | | | | | | |
| | | FASTRO | OUND RIGHT | TURN FN | ITRY | | | WESTE | BOUND LEFT | TURN FA | ITRY | | | | TOTAL ENT | RY | | |
| TOTALS | AUTOS | | GARBAGE | SEMI | MC | TOTAL | AUTOS | DELIVERY | GARBAGE | SEMI | MC | TOTAL | AUTOS | DELIVERY | GARBAGE | SEMI | MC | TOTAL |
| AM | 95 | 1 | 1 | 0 | 0 | 97 | 82 | 3 | 2 | 0 | 0 | 87 | 177 | 4 | 3 | 0 | 0 | 184 |
| MIDDAY | 124 | 6 | 0 | 1 | 0 | 131 | 66 | 3 | 0 | 0 | 0 | 69 | 190 | 9 | 0 | 1 | 0 | 200 |
| | | | | • | | | | | | | | | | | | • | | |
| PM | 165 | 4 | 0 | 0 | 0 | 169 | 53 | 4 | 0 | 0 | 0 | 57 | 218 | 8 | 0 | 0 | 0 | 226 |
| DAILY | 384 | 11 | 1 | 1 | 0 | 397 | 201 | 10 | 2 | 0 | 0 | 213 | 585 | 21 | 3 | 1 | 0 | 610 |



CLIENT: HIRSCH/GREEN TRANSPORTATION CONSULTING, INC.

PROJECT: CHEVAL BLANC HOTEL - BEVERLY HILLS

DATE: SATURDAY, MAY 18, 2019

PERIOD: 24-HOUR

INTERSECTION: N/S ALLEY (ONE-WAY SB)

| 15 MINUTE | | EASTBC | OUND RIGHT | TURN EN | ITRY | | | WESTE | BOUND LEFT | TURN EN | NTRY | | | | TOTAL EN | TRY | | |
|--------------|-------|----------|------------|---------|------|-------|-------|-------|------------|---------|------|-------|-------|----------|----------|------|----|-------|
| (START TIME) | AUTOS | DELIVERY | GARBAGE | SEMI | MC | TOTAL | AUTOS | | | SEMI | МС | TOTAL | AUTOS | DELIVERY | GARBAGE | SEMI | MC | TOTAL |
| 12:00 AM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 12:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 12:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 1 |
| 12:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2:15 AM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 2:30 AM | 2 | 0 | 0 | 0 | 0 | 2 | 1 | 0 | 0 | 0 | 0 | 1 | 3 | 0 | 0 | 0 | 0 | 3 |
| 2:45 AM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 3:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 3:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | | | | | | | 1 | | 0 | | | | 1 | | | | | |
| 3:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | | 0 | • | 0 | 0 | 1 | | 0 | 0 | 0 | 0 | 1 |
| 3:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 1 |
| 4:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:15 AM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 4:30 AM | 2 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 1 | 0 | 0 | 3 | 4 | 0 | 1 | 0 | 0 | 5 |
| 4:45 AM | 4 | 0 | 0 | 0 | 0 | 4 | 0 | 1 | 0 | 0 | 0 | 1 | 4 | 1 | 0 | 0 | 0 | 5 |
| 5:00 AM | 3 | 0 | 0 | 0 | 0 | 3 | 2 | 0 | 0 | 0 | 0 | 2 | 5 | 0 | 0 | 0 | 0 | 5 |
| 5:15 AM | 3 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 3 |
| 5:30 AM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 5:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 |
| 6:00 AM | 2 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 0 | 0 | 0 | 2 | 4 | 0 | 0 | 0 | 0 | 4 |
| 6:15 AM | 2 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 2 |
| 6:30 AM | 2 | 0 | 0 | 0 | 0 | 2 | 1 | 0 | 0 | 0 | 0 | 1 | 3 | 0 | 0 | 0 | 0 | 3 |
| 6:45 AM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 7:00 AM | 1 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 0 | 0 | 0 | 2 | 2 | 1 | 0 | 0 | 0 | 3 |
| 7:15 AM | 2 | 1 | 0 | 0 | 0 | 3 | 1 | 0 | 0 | 0 | 0 | 1 | 3 | 1 | 0 | 0 | 0 | 4 |
| 7:30 AM | 4 | 0 | 0 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 4 |
| 7:45 AM | 1 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 2 |
| 8:00 AM | 4 | 0 | 1 | 0 | 0 | 5 | 1 | 0 | 0 | 0 | 0 | 1 | 5 | 0 | 1 | 0 | 0 | 6 |
| 8:15 AM | 7 | 0 | 0 | 0 | 0 | 7 | 1 | 0 | 0 | 0 | 0 | 1 | 8 | 0 | 0 | 0 | 0 | 8 |
| 8:30 AM | 9 | 0 | 0 | 0 | 0 | 9 | 5 | 0 | 0 | 0 | 0 | 5 | 14 | 0 | 0 | 0 | 0 | 14 |
| 8:45 AM | 12 | 1 | 0 | 0 | 0 | 13 | 12 | 0 | 0 | 0 | 0 | 12 | 24 | 1 | 0 | 0 | 0 | 25 |
| 9:00 AM | 19 | 0 | 0 | 0 | 0 | 19 | 8 | 0 | 0 | 0 | 0 | 8 | 27 | 0 | 0 | 0 | 0 | 27 |
| 9:15 AM | 18 | 1 | 0 | 0 | 0 | 19 | 3 | 0 | 0 | 0 | 0 | 3 | 21 | 1 | 0 | 0 | 0 | 22 |
| 9:30 AM | 14 | 0 | 0 | 0 | 0 | 14 | 6 | 1 | 0 | 0 | 0 | 7 | 20 | 1 | 0 | 0 | 0 | 21 |
| 9:45 AM | 3 | 0 | 0 | 0 | 0 | 3 | 2 | 0 | 0 | 0 | 0 | 2 | 5 | 0 | 0 | 0 | 0 | 5 |
| 10:00 AM | 7 | 0 | 0 | 0 | 0 | 7 | 5 | 0 | 0 | 0 | 0 | 5 | 12 | 0 | 0 | 0 | 0 | 12 |
| 10:15 AM | 9 | 2 | 0 | 0 | 0 | 11 | 3 | 0 | 0 | 0 | 0 | 3 | 12 | 2 | 0 | 0 | 0 | 14 |
| 10:30 AM | 7 | 0 | 0 | 0 | 0 | 7 | 5 | 0 | 0 | 0 | 0 | 5 | 12 | 0 | 0 | 0 | 0 | 12 |
| 10:45 AM | 10 | 1 | 0 | 0 | 0 | 11 | 4 | 0 | 0 | 0 | 0 | 4 | 14 | 1 | 0 | 0 | 0 | 15 |
| 11:00 AM | 9 | 0 | 0 | 0 | 0 | 9 | 3 | 0 | 0 | 0 | 0 | 3 | 12 | 0 | 0 | 0 | 0 | 12 |
| 11:15 AM | 8 | 0 | 0 | 0 | 0 | 8 | 2 | 0 | 0 | 0 | 0 | 2 | 10 | 0 | 0 | 0 | 0 | 10 |
| 11:30 AM | 10 | 0 | 0 | 0 | 0 | 10 | 2 | 0 | 0 | 0 | 0 | 2 | 12 | 0 | 0 | 0 | 0 | 12 |
| 11:45 AM | 5 | 2 | 0 | 0 | 0 | 7 | 2 | 0 | 0 | 0 | 0 | 2 | 7 | 2 | 0 | 0 | 0 | 9 |
| 12:00 PM | 8 | 0 | 0 | 0 | 0 | 8 | 3 | 0 | 0 | 0 | 0 | 3 | 11 | 0 | 0 | 0 | 0 | 11 |
| 12:15 PM | 14 | 0 | 0 | 0 | 0 | 14 | 2 | 0 | 0 | 0 | 0 | 2 | 16 | 0 | 0 | 0 | 0 | 16 |
| 12:30 PM | 6 | 0 | 0 | 0 | 0 | 6 | 4 | 0 | 0 | 0 | 0 | 4 | 10 | 0 | 0 | 0 | 0 | 10 |
| 12:45 PM | 13 | 2 | 0 | 0 | 0 | 15 | 8 | 0 | 0 | 0 | 0 | 8 | 21 | 2 | 0 | 0 | 0 | 23 |
| 1:00 PM | 5 | 0 | 0 | 0 | 0 | 5 | 5 | 0 | 0 | 0 | 0 | 5 | 10 | 0 | 0 | 0 | 0 | 10 |
| 1:15 PM | 5 | 1 | 0 | 0 | 0 | 6 | 2 | 0 | 0 | 0 | 0 | 2 | 7 | 1 | 0 | 0 | 0 | 8 |
| 1:30 PM | 8 | 0 | 0 | 0 | 0 | 8 | 10 | 0 | 0 | 0 | 0 | 10 | 18 | 0 | 0 | 0 | 0 | 18 |
| 1:45 PM | 10 | 1 | 0 | 0 | 0 | 11 | 6 | 0 | 0 | 0 | 0 | 6 | 16 | 1 | 0 | 0 | 0 | 17 |

CLIENT: HIRSCH/GREEN TRANSPORTATION CONSULTING, INC.

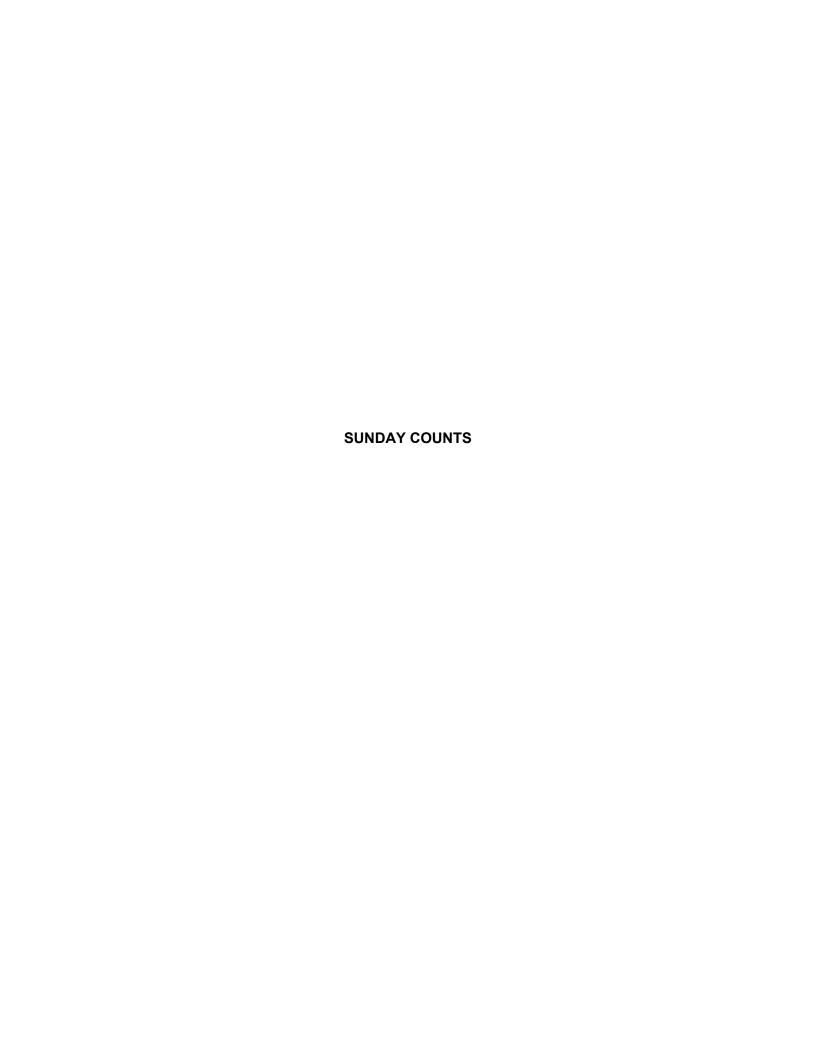
PROJECT: CHEVAL BLANC HOTEL - BEVERLY HILLS

DATE: SATURDAY, MAY 18, 2019

PERIOD: 24-HOUR

INTERSECTION: N/S ALLEY (ONE-WAY SB)

| | | =.0== | | | | | | | | | | | | | ======================================= | | | |
|--------------|-------|----------|-----------|------|----|-------|-------|----------|-------------|------|----|-------|-------|----------|---|------|----|-------|
| 15 MINUTE | ==== | | UND RIGHT | | | | | | OUND LEFT 1 | | | | | | TOTAL ENT | | | |
| (START TIME) | AUTOS | DELIVERY | GARBAGE | SEMI | MC | TOTAL | AUTOS | DELIVERY | GARBAGE | SEMI | MC | TOTAL | AUTOS | DELIVERY | GARBAGE | SEMI | MC | TOTAL |
| 2:00 PM | 11 | 0 | 0 | 0 | 0 | 11 | 6 | 0 | 0 | 0 | 0 | 6 | 17 | 0 | 0 | 0 | 0 | 17 |
| 2:15 PM | 13 | 0 | 0 | 0 | 0 | 13 | 2 | 1 | 0 | 0 | 0 | 3 | 15 | 1 | 0 | 0 | 0 | 16 |
| 2:30 PM | 7 | 0 | 0 | 0 | 0 | 7 | 3 | 1 | 0 | 0 | 0 | 4 | 10 | 1 | 0 | 0 | 0 | 11 |
| 2:45 PM | 7 | 0 | 0 | 0 | 0 | 7 | 6 | 0 | 0 | 0 | 0 | 6 | 13 | 0 | 0 | 0 | 0 | 13 |
| 3:00 PM | 11 | 1 | 0 | 0 | 0 | 12 | 5 | 0 | 0 | 0 | 0 | 5 | 16 | 1 | 0 | 0 | 0 | 17 |
| 3:15 PM | 8 | 0 | 0 | 0 | 0 | 8 | 2 | 0 | 0 | 0 | 0 | 2 | 10 | 0 | 0 | 0 | 0 | 10 |
| 3:30 PM | 6 | 1 | 0 | 0 | 0 | 7 | 3 | 0 | 0 | 0 | 0 | 3 | 9 | 1 | 0 | 0 | 0 | 10 |
| 3:45 PM | 5 | 0 | 0 | 0 | 0 | 5 | 3 | 0 | 0 | 0 | 0 | 3 | 8 | 0 | 0 | 0 | 0 | 8 |
| 4:00 PM | 5 | 0 | 0 | 0 | 0 | 5 | 1 | 0 | 0 | 0 | 0 | 1 | 6 | 0 | 0 | 0 | 0 | 6 |
| 4:15 PM | 8 | 0 | 0 | 0 | 0 | 8 | 3 | 0 | 0 | 0 | 0 | 3 | 11 | 0 | 0 | 0 | 0 | 11 |
| 4:30 PM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 4:45 PM | 6 | 1 | 0 | 0 | 0 | 7 | 2 | 0 | 0 | 0 | 0 | 2 | 8 | 1 | 0 | 0 | 0 | 9 |
| 5:00 PM | 5 | 0 | 0 | 0 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 0 | 0 | 0 | 5 |
| 5:15 PM | 3 | 0 | 0 | 0 | 0 | 3 | 3 | 0 | 0 | 0 | 0 | 3 | 6 | 0 | 0 | 0 | 0 | 6 |
| 5:30 PM | 6 | 0 | 0 | 0 | 0 | 6 | 1 | 0 | 0 | 0 | 0 | 1 | 7 | 0 | 0 | 0 | 0 | 7 |
| 5:45 PM | 7 | 0 | 0 | 0 | 0 | 7 | 1 | 0 | 0 | 0 | 0 | 1 | 8 | 0 | 0 | 0 | 0 | 8 |
| 6:00 PM | 6 | 0 | 0 | 0 | 0 | 6 | 2 | 0 | 0 | 0 | 0 | 2 | 8 | 0 | 0 | 0 | 0 | 8 |
| 6:15 PM | 4 | 1 | 0 | 0 | 0 | 5 | 1 | 0 | 0 | 0 | 0 | 1 | 5 | 1 | 0 | 0 | 0 | 6 |
| 6:30 PM | 3 | 0 | 0 | 0 | 0 | 3 | 1 | 0 | 0 | 0 | 0 | 1 | 4 | 0 | 0 | 0 | 0 | 4 |
| 6:45 PM | 1 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 2 |
| 7:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:15 PM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 7:30 PM | 1 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 2 |
| 7:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:00 PM | 1 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 2 |
| 8:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:30 PM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 8:45 PM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 9:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 9:15 PM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 9:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 9:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 10:00 PM | 2 | 0 | 0 | 0 | 0 | 2 | 0 | 1 | 0 | 0 | 0 | 1 | 2 | 1 | 0 | 0 | 0 | 3 |
| 10:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 10:30 PM | 2 | 0 | 0 | 0 | 0 | 2 | 0 | 1 | 0 | 0 | 0 | 1 | 2 | 1 | 0 | 0 | 0 | 3 |
| 10:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 11:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 11:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 11:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 11:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 1 |
| | | | | | | | | | | | | | | | | | | |
| | | | UND RIGHT | | | | | | OUND LEFT 1 | | | | | | TOTAL ENT | | | |
| TOTALS | AUTOS | DELIVERY | GARBAGE | SEMI | MC | TOTAL | AUTOS | DELIVERY | GARBAGE | SEMI | MC | TOTAL | AUTOS | DELIVERY | GARBAGE | SEMI | MC | TOTAL |
| AM | 120 | 3 | 1 | 0 | 0 | 124 | 51 | 4 | 2 | 0 | 0 | 57 | 171 | 7 | 3 | 0 | 0 | 181 |
| MIDDAY | 134 | 9 | 0 | 0 | 0 | 143 | 66 | 0 | 0 | 0 | 0 | 66 | 200 | 9 | 0 | 0 | 0 | 209 |
| PM | 133 | 4 | 0 | 0 | 0 | 137 | 49 | 4 | 0 | 0 | 0 | 53 | 182 | 8 | 0 | 0 | 0 | 190 |
| DAILY | 387 | 16 | 1 | 0 | 0 | 404 | 166 | 8 | 2 | 0 | 0 | 176 | 553 | 24 | 3 | 0 | 0 | 580 |





CLIENT: HIRSCH/GREEN TRANSPORTATION CONSULTING, INC.

PROJECT: CHEVAL BLANC HOTEL - BEVERLY HILLS

DATE: SUNDAY, MAY 12, 2019

PERIOD: 24-HOUR

INTERSECTION: N/S ALLEY (ONE-WAY SB)

| 15 MINUTE | | EASTRO | UND RIGHT | TUDNI EN | ITDV | | | WEST | BOUND LEFT | TUDNI EN | ITDV | | | | TOTAL EN | TDV | | |
|--------------------|--------|----------|-----------|----------|------|-------|-------|------|------------|----------|--------|-------|-------|----------|----------|-----|----|--------|
| (START TIME) | AUTOS | DELIVERY | GARBAGE | SEMI | MC | TOTAL | AUTOS | | | SEMI | MC | TOTAL | AUTOS | DELIVERY | | 1 1 | MC | TOTAL |
| , | | | | | | | | | | | | | | | | | | |
| 12:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 12:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 12:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 12:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | 0 | 0 | 0 |
| 2:00 AM 2:15 AM | 0 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 0 | 0 | 1 | 0 | 0 0 | 0 | 0 | 0 1 |
| 2:30 AM | 0 | | 0 | | 0 | 1 | 0 | 0 | 0 | | | 0 | 0 | 0 | 0 | 0 | | |
| 2:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 0 | 0 | 0 | 0 | | 0 | 0 | 0 |
| 3:00 AM | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 0 | 0 | 0 | 0 |
| | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 3:15 AM | | | | | | | | | | | | | | | | | | |
| 3:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 3:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:45 AM | 1 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 2 |
| 5:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 1 |
| 5:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 1 |
| 6:00 AM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 6:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 6:30 AM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 6:45 AM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 7:00 AM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 7:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 1 |
| 7:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:00 AM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 8:15 AM | 2 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 2 |
| 8:30 AM | 2 | 0 | 0 | 0 | 0 | 2 | 1 | 0 | 0 | 0 | 0 | 1 | 3 | 0 | 0 | 0 | 0 | 3 |
| 8:45 AM | 3 | 0 | 0 | 0 | 0 | 3 | 2 | 0 | 0 | 0 | 0 | 2 | 5 | 0 | 0 | 0 | 0 | 5 |
| 9:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 9:15 AM | 1 | 0 | 0 | 0 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 2 | 3 | 0 | 0 | 0 | 0 | 3 |
| 9:30 AM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 9:45 AM | 2 | 0 | 0 | 0 | 0 | 2 | 1 | 0 | 0 | 0 | 0 | 1 | 3 | 0 | 0 | 0 | 0 | 3 |
| 10:00 AM | 3 | 0 | 0 | 0 | 0 | 3 | 2 | 0 | 0 | 0 | 0 | 2 | 5 | 0 | 0 | 0 | 0 | 5 |
| 10:15 AM | 3 | 0 | 0 | 0 | 0 | 3 | 1 | 0 | 0 | 0 | 0 | 1 | 4 | 0 | 0 | 0 | 0 | 4 |
| 10:30 AM | 5 | 0 | 0 | 0 | 0 | 5 | 2 | 0 | 0 | 0 | 0 | 2 | 7 | 0 | 0 | 0 | 0 | 7 |
| 10:45 AM | 3 | 0 | 0 | 0 | 0 | 3 | 9 | 0 | 0 | 0 | 0 | 9 | 12 | 0 | 0 | 0 | 0 | 12 |
| 11:00 AM | 3 | 0 | 0 | 0 | 0 | 3 | 5 | 0 | 0 | 0 | 0 | 5 | 8 | 0 | 0 | 0 | 0 | 8 |
| 11:15 AM | 4 | 0 | 0 | 0 | 0 | 4 | 9 | 0 | 0 | 0 | 0 | 9 | 13 | 0 | 0 | 0 | 0 | 13 |
| 11:30 AM | 7 | 0 | 0 | 0 | 0 | 7 | 4 | 0 | 0 | 0 | 0 | 4 | 11 | 0 | 0 | 0 | 0 | 11 |
| 11:45 AM | 7 | 0 | 0 | 0 | 0 | 7 | 3 | 0 | 0 | 0 | 0 | 3 | 10 | 0 | 0 | 0 | 0 | 10 |
| 12:00 PM | 4 | 1 | 0 | 0 | 0 | 5 | 2 | 0 | 0 | 0 | 0 | 2 | 6 | 1 | 0 | 0 | 0 | 7 |
| 12:15 PM | 4 | 0 | 0 | 0 | 0 | 4 | 2 | 0 | 0 | 0 | 0 | 2 | 6 | 0 | 0 | 0 | 0 | 6 |
| 12:30 PM | 5 | 0 | 0 | 0 | 0 | 5 | 1 | 0 | 0 | 0 | 0 | 1 | 6 | 0 | 0 | 0 | 0 | 6 |
| 12:45 PM | 3 | 0 | 0 | 0 | 0 | 3 | 2 | 0 | 0 | 0 | 0 | 2 | 5 | 0 | 0 | 0 | 0 | 5 |
| 1:00 PM | 5 | 0 | 0 | 0 | 0 | 5 | 1 | 0 | 0 | 0 | 0 | 1 | 6 | 0 | 0 | 0 | 0 | 6 |
| 1:15 PM | 3 | 0 | 0 | 0 | 0 | 3 | 1 | 0 | 0 | 0 | 0 | 1 | 4 | 0 | 0 | 0 | 0 | 4 |
| 1:30 PM | 2 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 0 | 0 | 0 | 2 | 4 | 0 | 0 | 0 | 0 | 4 |
| 1:45 PM | 2 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 00 | 0 | 0 | 2 | 4 | 0 | 0 | 0 | 0 | 4 |

CLIENT: HIRSCH/GREEN TRANSPORTATION CONSULTING, INC.

PROJECT: CHEVAL BLANC HOTEL - BEVERLY HILLS DATE: SUNDAY, MAY 12, 2019

24-HOUR PERIOD:

INTERSECTION: N/S ALLEY (ONE-WAY SB)

| 15 MINUTE | | | OUND RIGHT | TURN EN | ITRY | | | | OUND LEFT | TURN EN | TRY | | | | TOTAL EN | | | |
|----------------------|--------|----------|------------|---------|------|--------|--------|----------|------------|---------|-----|-------|--------|-------------|-----------|------|-----|--------|
| (START TIME) | AUTOS | DELIVERY | GARBAGE | SEMI | MC | TOTAL | AUTOS | DELIVERY | GARBAGE | SEMI | MC | TOTAL | AUTOS | DELIVERY | GARBAGE | SEMI | MC | TOTAL |
| 2:00 PM | 5 | 0 | 0 | 0 | 0 | 5 | 2 | 0 | 0 | 0 | 0 | 2 | 7 | 0 | 0 | 0 | 0 | 7 |
| 2:15 PM | 11 | 0 | 0 | 0 | 0 | 11 | 3 | 0 | 0 | 0 | 0 | 3 | 14 | 0 | 0 | 0 | 0 | 14 |
| 2:30 PM | 8 | 0 | 0 | 0 | 0 | 8 | 3 | 0 | 0 | 0 | 0 | 3 | 11 | 0 | 0 | 0 | 0 | 11 |
| 2:45 PM | 5 | 0 | 0 | 0 | 0 | 5 | 2 | 0 | 0 | 0 | 0 | 2 | 7 | 0 | 0 | 0 | 0 | 7 |
| 3:00 PM | 2 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 0 | 0 | 0 | 2 | 4 | 0 | 0 | 0 | 0 | 4 |
| 3:15 PM | 5 | 0 | 0 | 0 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 0 | 0 | 0 | 5 |
| 3:30 PM | 5 | 0 | 0 | 0 | 0 | 5 | 1 | 0 | 0 | 0 | 0 | 1 | 6 | 0 | 0 | 0 | 0 | 6 |
| 3:45 PM | 6 | 0 | 0 | 0 | 0 | 6 | 2 | 0 | 0 | 0 | 0 | 2 | 8 | 0 | 0 | 0 | 0 | 8 |
| 4:00 PM | 9 | 0 | 0 | 0 | 0 | 9 | 4 | 0 | 0 | 0 | 0 | 4 | 13 | 0 | 0 | 0 | 0 | 13 |
| 4:15 PM | 6 | 0 | 0 | 0 | 0 | 6 | 1 | 0 | 0 | 0 | 0 | 1 | 7 | 0 | 0 | 0 | 0 | 7 |
| 4:30 PM | 5 | 0 | 0 | 0 | 0 | 5 | 3 | 0 | 0 | 0 | 0 | 3 | 8 | 0 | 0 | 0 | 0 | 8 |
| 4:45 PM | 5 | 0 | 0 | 0 | 0 | 5 | 1 | 0 | 0 | 0 | 0 | 1 | 6 | 0 | 0 | 0 | 0 | 6 |
| 5:00 PM | 3 | 0 | 0 | 0 | 0 | 3 | 1 | 0 | 0 | 0 | 0 | 1 | 4 | 0 | 0 | 0 | 0 | 4 |
| 5:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 1 |
| 5:30 PM | 2 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 2 |
| 5:45 PM | 4 | 0 | 0 | 0 | 0 | 4 | 3 | 0 | 0 | 0 | 0 | 3 | 7 | 0 | 0 | 0 | 0 | 7 |
| 6:00 PM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 6:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 6:30 PM | 2 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 2 |
| 6:45 PM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 7:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:15 PM | 2 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 2 |
| 7:30 PM | 2 | 0 | 0 | 0 | 0 | 2 | 1 | 0 | 0 | 0 | 0 | 1 | 3 | 0 | 0 | 0 | 0 | 3 |
| 7:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 1 |
| 8:15 PM | 2 | 0 | 0 | 0 | 0 | 2 | 1 | 0 | 0 | 0 | 0 | 1 | 3 | 0 | 0 | 0 | 0 | 3 |
| 8:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:45 PM | 1 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 2 |
| 9:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 9:15 PM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 9:30 PM | 2 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 2 |
| 9:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 10:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 10:15 PM | 2 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 2 |
| 10:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 10:45 PM | 0 1 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 1 |
| 11:00 PM 11:15 PM | 0 | 0 | 0 | 0 | 0 | 1 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 0 |
| 11:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | | | 0 | 0 | 0 | | | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | 0 |
| 11:45 PM | 0 | 0 | U | U | U | 0 | 0 | U | U | U | U | 0 | U | U | U | U | U | U |
| | | | | | | | | | | | | | | | | | | |
| TOT:: 0 | ALITOS | | OARRAGE | | | TOTAL | ALITOS | | BOUND LEFT | | | TOTAL | ALITOC | DELIN (ED.) | TOTAL ENT | | 1/0 | TOTAL |
| TOTALS | AUTOS | | GARBAGE | SEMI | MC | TOTAL | | DELIVERY | GARBAGE | SEMI | MC | TOTAL | | DELIVERY | GARBAGE | SEMI | MC | TOTAL |
| AM | 18 | 0 | 0 | 0 | 0 | 18 | 9 | 1 | 0 | 0 | 0 | 10 | 27 | 1 | 0 | 0 | 0 | 28 |
| MIDDAY | 63 | 1 | 0 | 0 | 0 | 64 | 48 | 0 | 0 | 0 | 0 | 48 | 111 | 1 | 0 | 0 | 0 | 112 |
| PM | 98 | 0 | 0 | 0 | 0 | 98 | 34 | 0 | 0 | 0 | 0 | 34 | 132 | 0 | 0 | 0 | 0 | 132 |
| DAILY | 179 | 1 | 0 | 0 | 0 | 180 | 91 | 1 | 0 | 0 | 0 | 92 | 270 | 2 | 0 | 0 | 0 | 272 |



INTERSECTION TURNING MOVEMENT COUNT SUMMARY

CLIENT: HIRSCH/GREEN TRANSPORTATION CONSULTING, INC.

PROJECT: CHEVAL BLANC HOTEL - BEVERLY HILLS

DATE: SUNDAY, MAY 19, 2019

PERIOD: 24-HOUR

INTERSECTION: N/S ALLEY (ONE-WAY SB)

E/W SANTA MONICA BOULEVARD (S)

| 15 MINUTE | | EASTRO | UND RIGHT | TUDNI EN | ITDV | | | WEST | BOUND LEFT | TUDNI EN | ITDV | | | | TOTAL EN | TDV | | |
|--------------|--------|----------|-----------|----------|------|-------|-------|------|------------|----------|------|-------|-------|----------|----------|-----|----|-------|
| (START TIME) | ALITOS | DELIVERY | GARBAGE | SEMI | MC | TOTAL | AUTOS | | | SEMI | MC | TOTAL | AUTOS | DELIVERY | | | MC | TOTAL |
| | | | | | | | | | | | | | | | | | | |
| 12:00 AM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 12:15 AM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 12:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 |
| 12:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 3:00 AM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 3:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 3:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 3:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 0 | 0 | 0 | 2 |
| 4:45 AM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 5:00 AM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 5:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 6:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 1 |
| 6:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 6:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 6:45 AM | 2 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 2 |
| 7:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:15 AM | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 |
| 7:30 AM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 7:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:15 AM | 1 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 2 |
| 8:30 AM | 4 | 0 | 0 | 0 | 0 | 4 | 1 | 0 | 0 | 0 | 0 | 1 | 5 | 0 | 0 | 0 | 0 | 5 |
| 8:45 AM | 3 | 0 | 0 | 0 | 0 | 3 | 2 | 0 | 0 | 0 | 0 | 2 | 5 | 0 | 0 | 0 | 0 | 5 |
| 9:00 AM | 2 | 0 | 0 | 0 | 0 | 2 | 0 | 1 | 0 | 0 | 0 | 1 | 2 | 1 | 0 | 0 | 0 | 3 |
| 9:15 AM | 1 | 0 | 0 | 0 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 2 | 3 | 0 | 0 | 0 | 0 | 3 |
| 9:30 AM | 1 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 2 |
| 9:45 AM | 4 | 0 | 0 | 0 | 0 | 44 | 2 | 0 | 0 | 0 | 0 | 2 | 6 | 0 | 0 | 00 | 0 | 6 |
| 10:00 AM | 1 | 0 | 0 | 0 | 0 | 1 | 5 | 0 | 0 | 0 | 0 | 5 | 6 | 0 | 0 | 0 | 0 | 6 |
| 10:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 1 |
| 10:30 AM | 6 | 0 | 0 | 0 | 0 | 6 | 2 | 0 | 0 | 0 | 0 | 2 | 8 | 0 | 0 | 0 | 0 | 8 |
| 10:45 AM | 7 | 0 | 0 | 0 | 0 | 7 | 3 | 0 | 0 | 0 | 0 | 3 | 10 | 0 | 0 | 0 | 0 | 10 |
| 11:00 AM | 5 | 0 | 0 | 0 | 0 | 5 | 5 | 0 | 0 | 0 | 0 | 5 | 10 | 0 | 0 | 0 | 0 | 10 |
| 11:15 AM | 9 | 0 | 0 | 0 | 0 | 9 | 4 | 0 | 0 | 0 | 0 | 4 | 13 | 0 | 0 | 0 | 0 | 13 |
| 11:30 AM | 4 | 0 | 0 | 0 | 0 | 4 | 2 | 0 | 0 | 0 | 0 | 2 | 6 | 0 | 0 | 0 | 0 | 6 |
| 11:45 AM | 9 | 0 | 0 | 0 | 0 | 9 | 4 | 0 | 0 | 0 | 0 | 4 | 13 | 0 | 0 | 0 | 0 | 13 |
| 12:00 PM | 4 | 0 | 0 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 4 |
| 12:15 PM | 3 | 0 | 0 | 0 | 0 | 3 | 2 | 0 | 0 | 0 | 0 | 2 | 5 | 0 | 0 | 0 | 0 | 5 |
| 12:30 PM | 7 | 0 | 0 | 0 | 0 | 7 | 3 | 0 | 0 | 0 | 0 | 3 | 10 | 0 | 0 | 0 | 0 | 10 |
| 12:45 PM | 4 | 0 | 0 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 4 |
| 1:00 PM | 4 | 0 | 0 | 0 | 0 | 4 | 1 | 0 | 0 | 0 | 0 | 1 | 5 | 0 | 0 | 0 | 0 | 5 |
| 1:15 PM | 3 | 0 | 0 | 0 | 0 | 3 | 1 | 0 | 0 | 0 | 0 | 1 | 4 | 0 | 0 | 0 | 0 | 4 |
| 1:30 PM | 1 | 0 | 0 | 0 | 0 | 1 | 3 | 0 | 0 | 0 | 0 | 3 | 4 | 0 | 0 | 0 | 0 | 4 |
| 1:45 PM | 5 | 0 | 0 | 0 | 0 | 5 | 2 | 0 | 0 | 0 | 0 | 2 | 7 | 0 | 0 | 0 | 0 | 7 |

INTERSECTION TURNING MOVEMENT COUNT SUMMARY

CLIENT: HIRSCH/GREEN TRANSPORTATION CONSULTING, INC.

PROJECT: CHEVAL BLANC HOTEL - BEVERLY HILLS DATE: SUNDAY, MAY 19, 2019

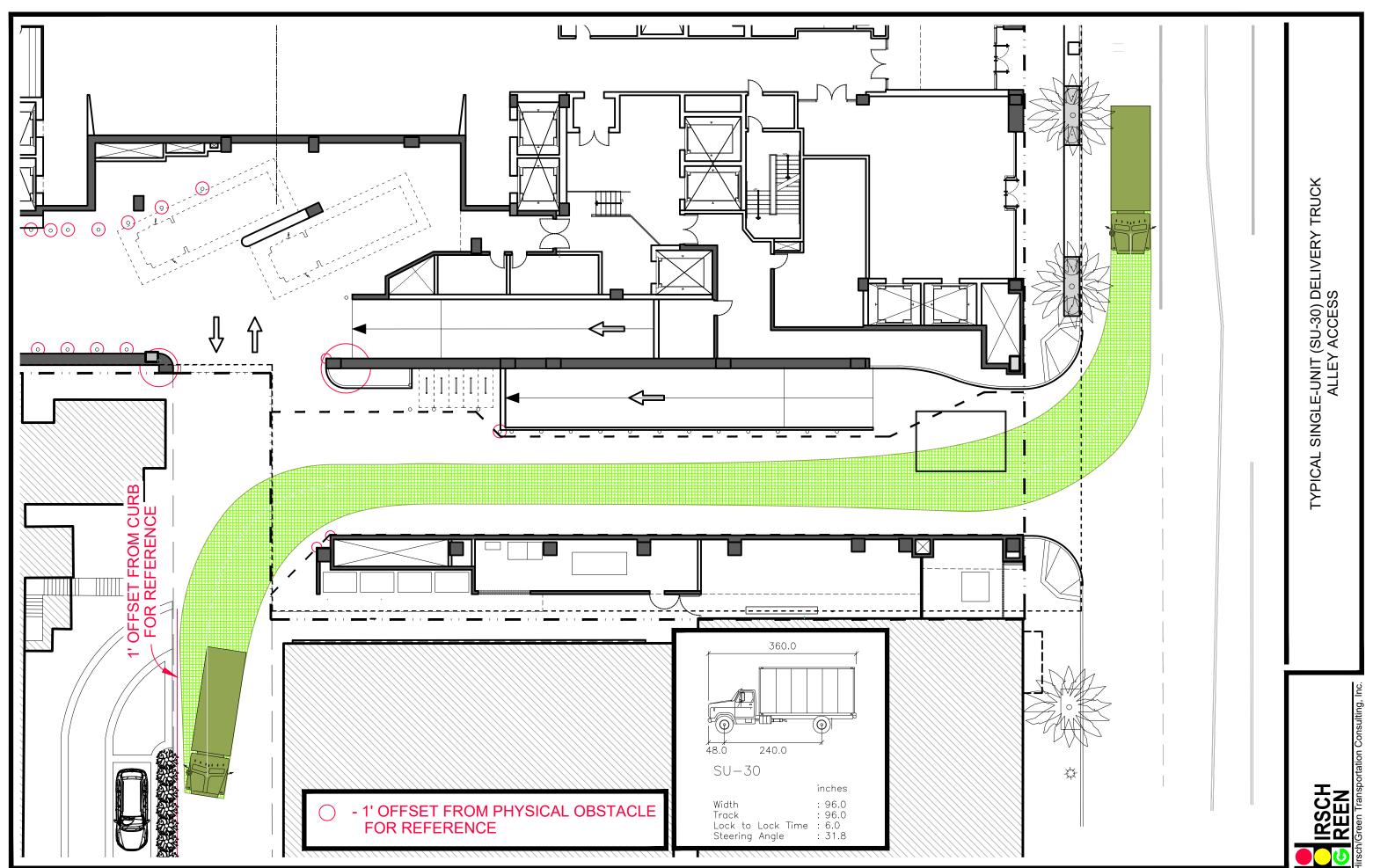
PERIOD: 24-HOUR

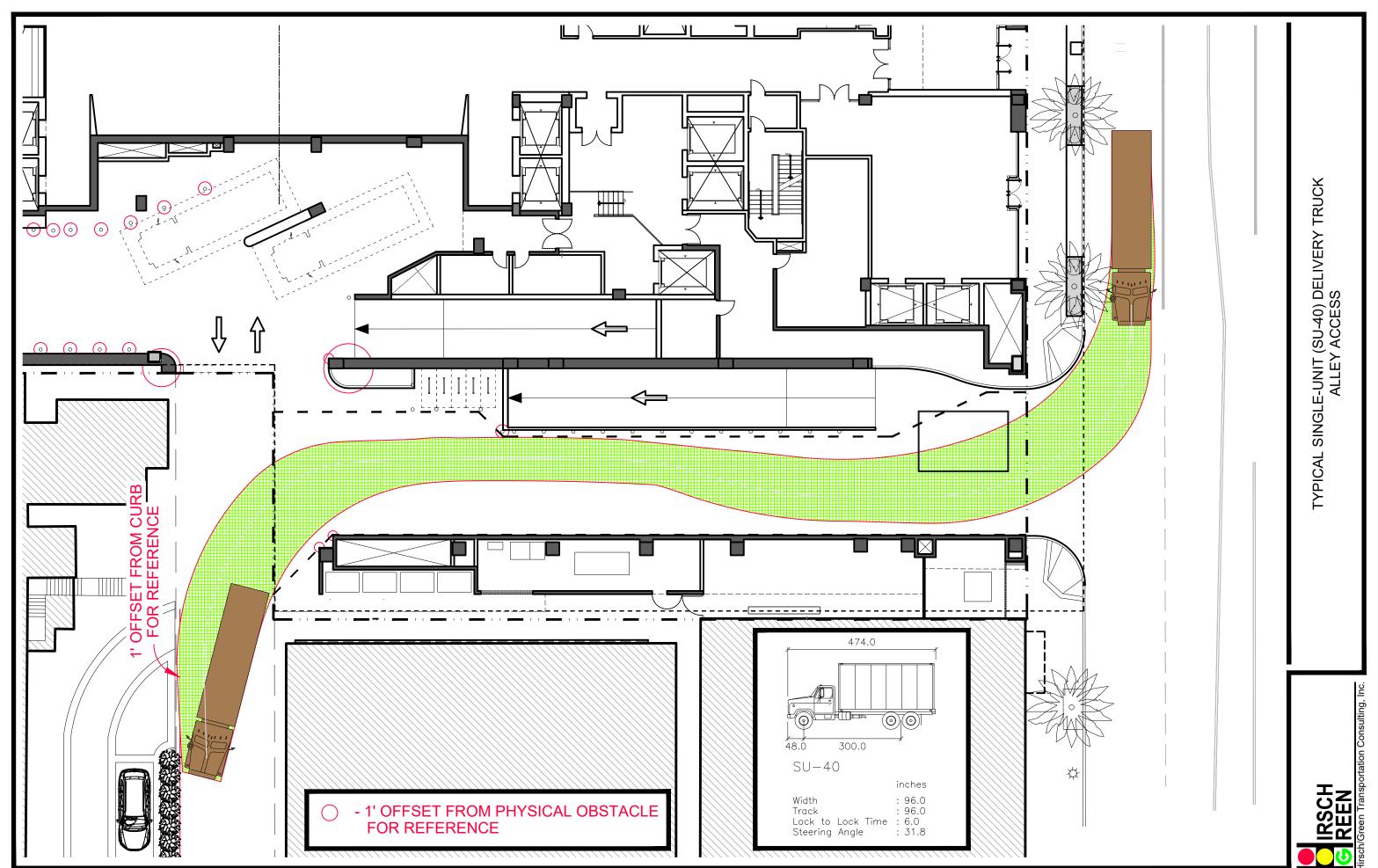
INTERSECTION: N/S ALLEY (ONE-WAY SB)

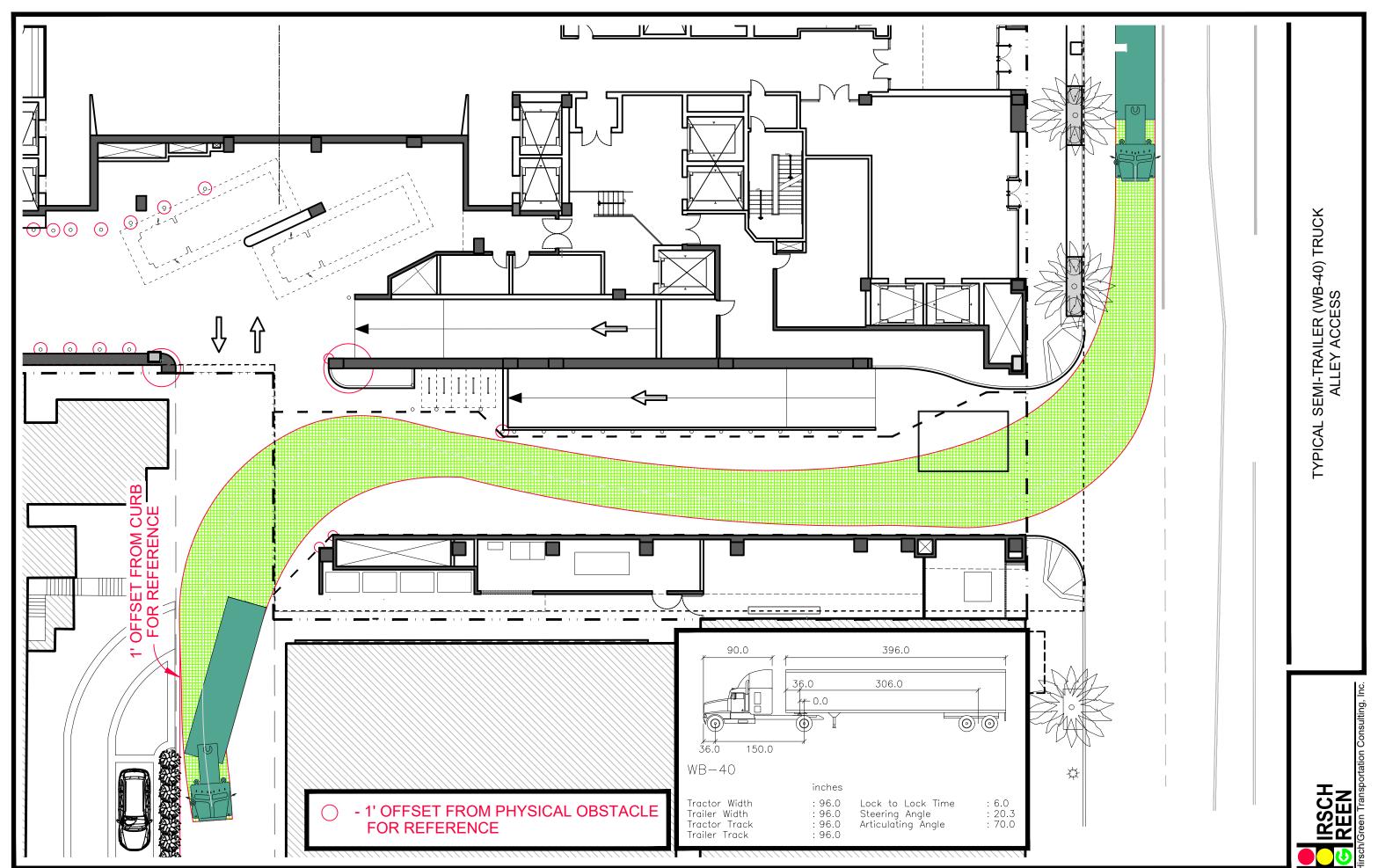
E/W SANTA MONICA BOULEVARD (S)

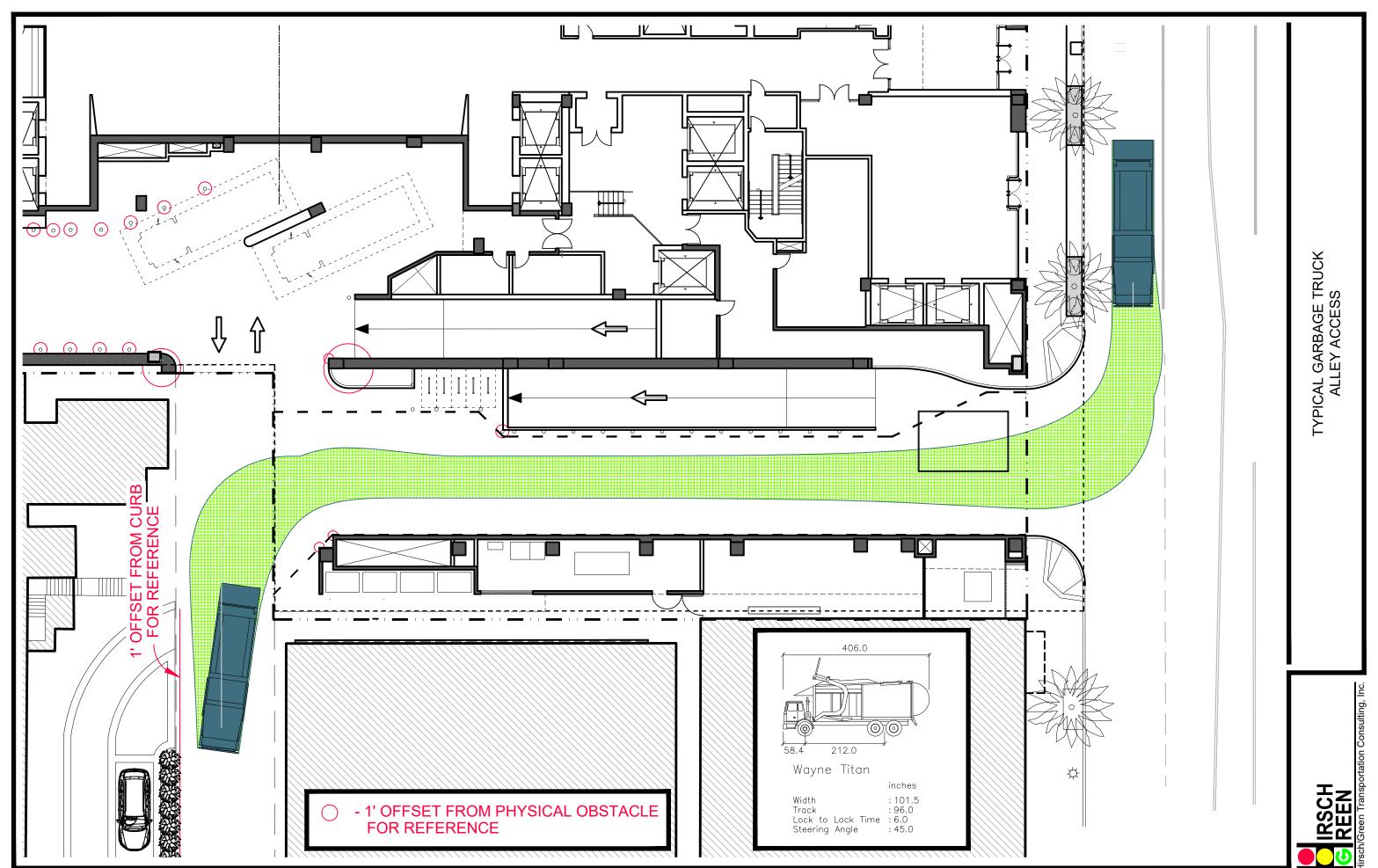
| 15 MINUTE | | EASTBO | OUND RIGHT | TURN EN | ITRY | | WESTBOUND LEFT TURN ENTRY | | | | | TOTAL ENTRY | | | | | | |
|----------------------|--------|----------|------------|----------|------|--------|---------------------------|---------------------------|---------|------|----|-------------|--------|----------|-----------|------|----|--------|
| (START TIME) | AUTOS | DELIVERY | GARBAGE | SEMI | MC | TOTAL | AUTOS | DELIVERY | GARBAGE | SEMI | MC | TOTAL | AUTOS | DELIVERY | GARBAGE | SEMI | MC | TOTAL |
| 2:00 PM | 6 | 0 | 0 | 0 | 0 | 6 | 0 | 1 | 0 | 0 | 0 | 1 | 6 | 1 | 0 | 0 | 0 | 7 |
| 2:15 PM | 5 | 1 | 0 | 0 | 0 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 1 | 0 | 0 | 0 | 6 |
| 2:30 PM | 5 | 0 | 0 | 0 | 0 | 5 | 1 | 0 | 0 | 0 | 0 | 1 | 6 | 0 | 0 | 0 | 0 | 6 |
| 2:45 PM | 9 | 0 | 0 | 0 | 0 | 9 | 1 | 0 | 0 | 0 | 0 | 1 | 10 | 0 | 0 | 0 | 0 | 10 |
| 3:00 PM | 3 | 1 | 0 | 0 | 0 | 4 | 1 | 0 | 0 | 0 | 0 | 1 | 4 | 1 | 0 | 0 | 0 | 5 |
| 3:15 PM | 6 | 0 | 0 | 0 | 0 | 6 | 3 | 0 | 0 | 0 | 0 | 3 | 9 | 0 | 0 | 0 | 0 | 9 |
| 3:30 PM | 9 | 0 | 0 | 0 | 0 | 9 | 3 | 0 | 0 | 0 | 0 | 3 | 12 | 0 | 0 | 0 | 0 | 12 |
| 3:45 PM | 6 | 0 | 0 | 0 | 0 | 6 | 2 | 0 | 0 | 0 | 0 | 2 | 8 | 0 | 0 | 0 | 0 | 8 |
| 4:00 PM | 6 | 0 | 0 | 0 | 0 | 6 | 3 | 0 | 0 | 0 | 0 | 3 | 9 | 0 | 0 | 0 | 0 | 9 |
| 4:15 PM | 2 | 0 | 0 | 0 | 0 | 2 | 1 | 0 | 0 | 0 | 0 | 1 | 3 | 0 | 0 | 0 | 0 | 3 |
| 4:30 PM | 3 | 0 | 0 | 0 | 0 | 3 | 3 | 0 | 0 | 0 | 0 | 3 | 6 | 0 | 0 | 0 | 0 | 6 |
| 4:45 PM | 3 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 3 |
| 5:00 PM | 6 | 0 | 0 | 0 | 0 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 6 | 0 | 0 | 0 | 0 | 6 |
| 5:15 PM | 2 | 0 | 0 | 0 | 0 | 2 | 1 | 0 | 0 | 0 | 0 | 1 | 3 | 0 | 0 | 0 | 0 | 3 |
| 5:30 PM | 5 | 0 | 0 | 0 | 0 | 5 | 1 | 0 | 0 | 0 | 0 | 1 | 6 | 0 | 0 | 0 | 0 | 6 |
| 5:45 PM | 2 | 0 | 0 | 0 | 0 | 2 | 1 | 0 | 0 | 0 | 0 | 1 | 3 | 0 | 0 | 0 | 0 | 3 |
| 6:00 PM | 4 | 0 | 0 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 4 |
| 6:15 PM | 1 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 2 |
| 6:30 PM | 1 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 2 |
| 6:45 PM | 2 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 0 | 0 | 0 | 2 | 4 | 0 | 0 | 0 | 0 | 4 |
| 7:00 PM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 7:15 PM | 4 | 0 | 0 | 0 | 0 | 4 | 1 | 0 | 0 | 0 | 0 | 1 | 5 | 0 | 0 | 0 | 0 | 5 |
| 7:30 PM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 7:45 PM | 2 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 2 |
| 8:00 PM | 2 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 2 |
| 8:15 PM | 1 | 1 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 2 |
| 8:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 9:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 9:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 9:30 PM | 0 | 0 | - | 0 | 0 | | 0 | 0 | - | - | 0 | | 0 | 0 | - | - | 0 | 0 |
| 9:45 PM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 10:00 PM 10:15 PM | 0 2 | 0 | 0 | 0 | 0 | 0 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 2 | 0 | 0 | 0 | 0 | 0 2 |
| 10:15 PM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 10:30 PM 10:45 PM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 11:00 PM | 2 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 2 |
| 11:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 11:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 11:45 PM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| | | • | • | | | | | | • | | | | | | • | | | |
| | | FACTO | NIND DICUT | TUDNI EN | ITDV | | | WESTBOUND LEFT TURN ENTRY | | | | | | | TOTAL ENT | 'DV | | |
| TOTALS | AUTOS | | GARBAGE | SEMI | MC | TOTAL | AUTOS | DELIVERY | GARBAGE | SEMI | MC | TOTAL | AUTOS | DELIVERY | GARBAGE | SEMI | MC | TOTAL |
| AM | 24 | 1 | 0 | 0 | 0 | 25 | 12 | 1 | 0 | 0 | 0 | 13 | 36 | 2 | 0 | 0 | 0 | 38 |
| MIDDAY | 72 | 0 | 0 | 0 | 0 | 72 | 38 | 0 | 0 | 0 | 0 | 38 | 110 | 0 | 0 | 0 | 0 | 110 |
| PM | 105 | 3 | 0 | 0 | 0 | 108 | 26 | 1 | 0 | 0 | 0 | 30 27 | 131 | 4 | 0 | 0 | 0 | 135 |
| DAILY | | 4 | 0 | 0 | | | 76 | 2 | 0 | 0 | 0 | 78 | | 6 | 0 | 0 | 0 | 283 |
| DAILY | 201 | 4 | U | U | 0 | 205 | 76 | 2 | U | U | U | 78 | 277 | б | U | U | U | ∠83 |

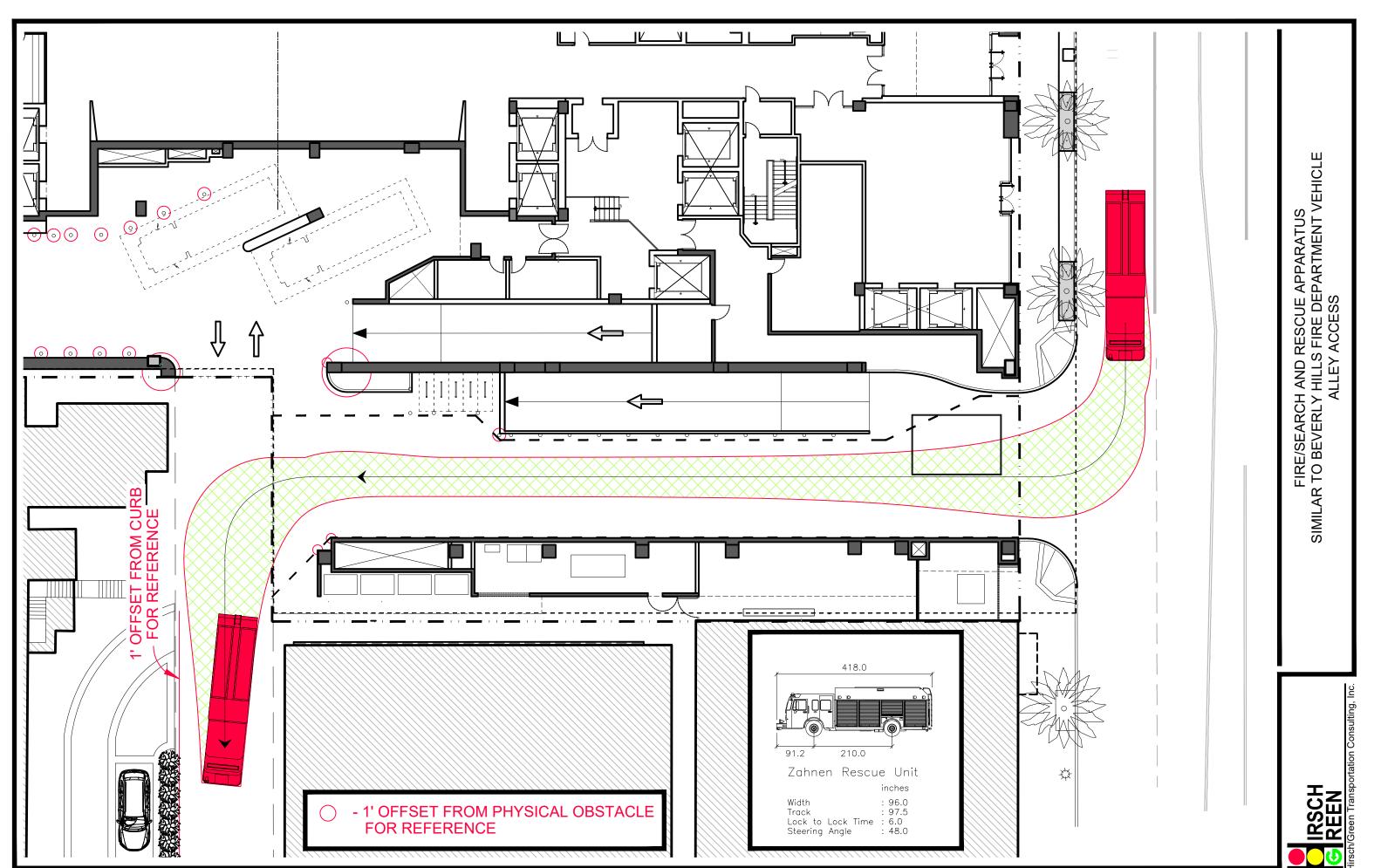
| RELOCATED ALLEY VEHICULAR ACCESS TURNING MOVEMENT DIAGRAMS |
|--|
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| |

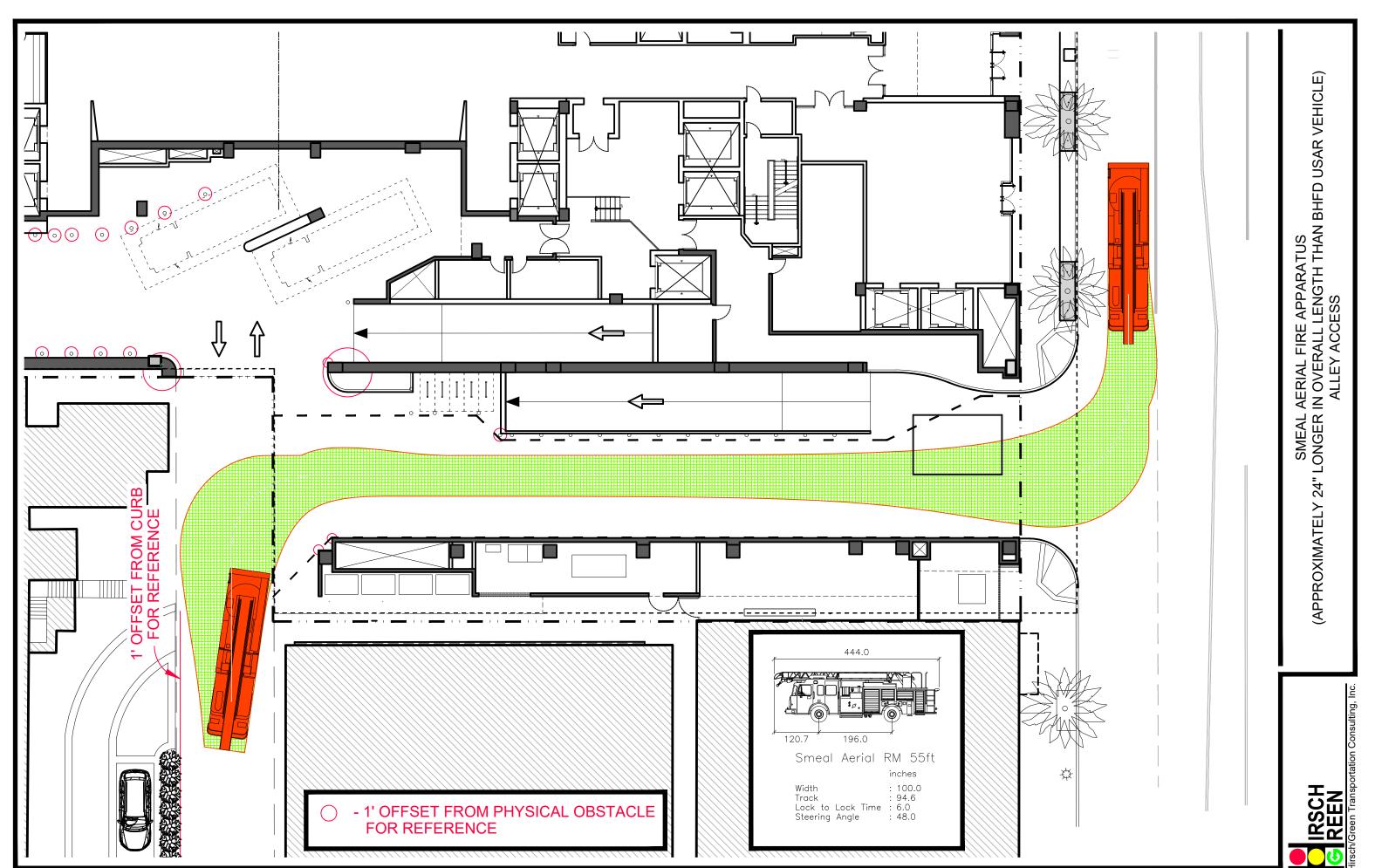


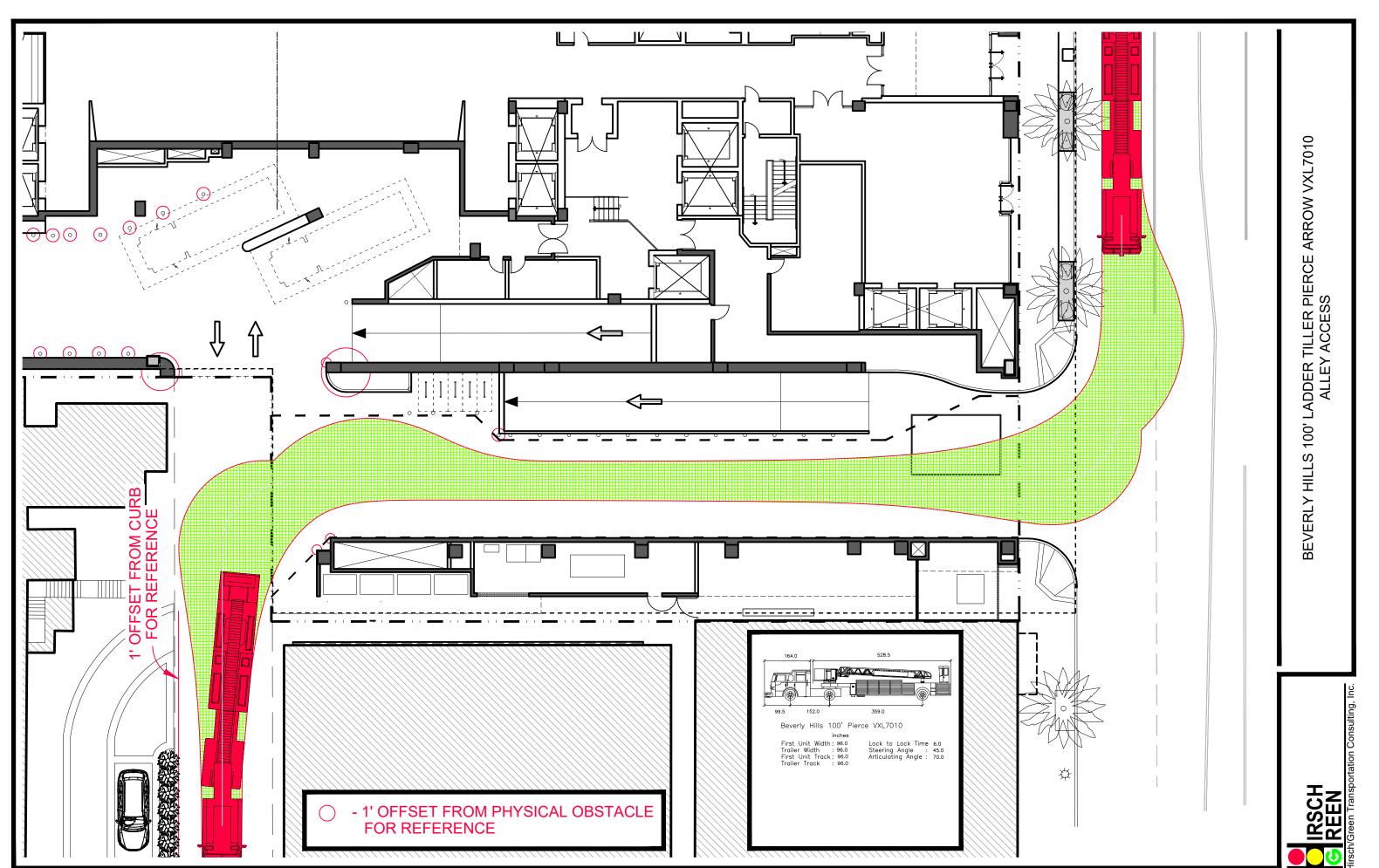




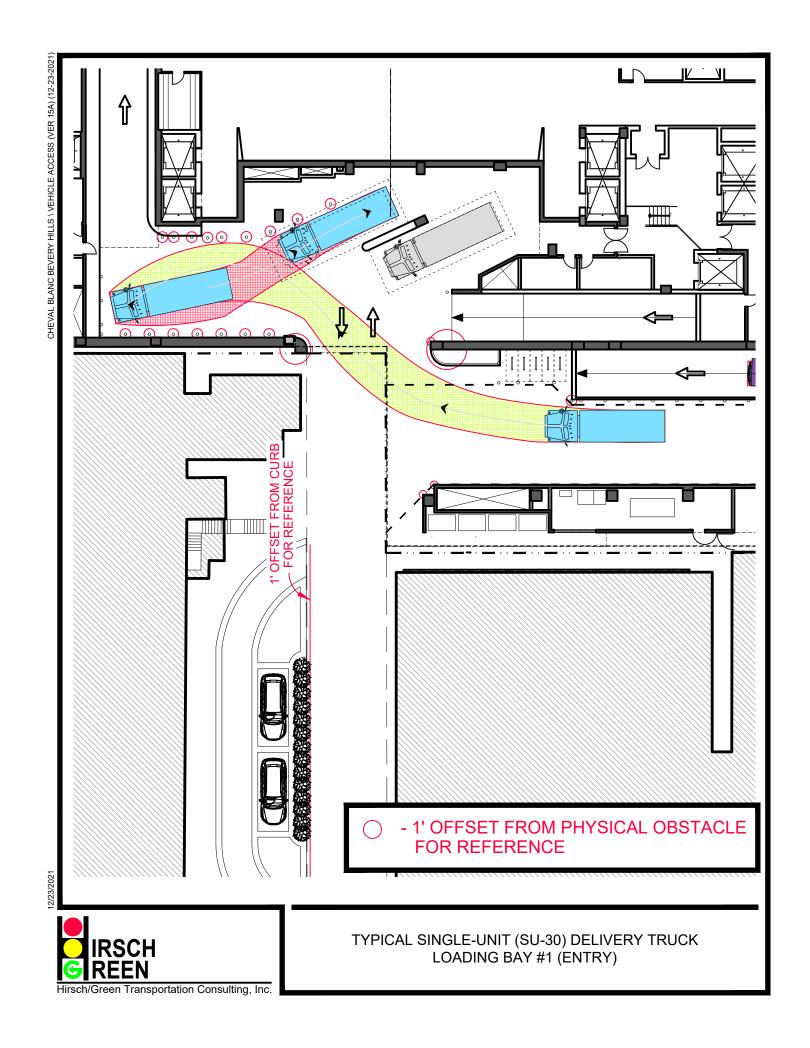


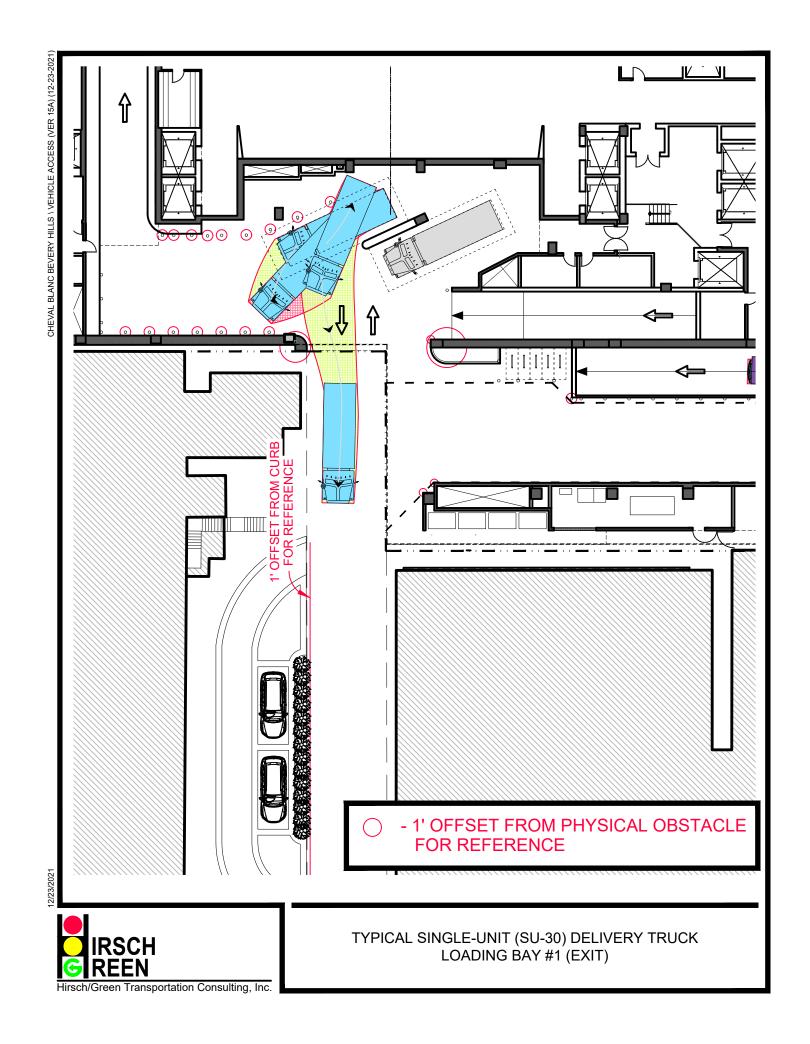


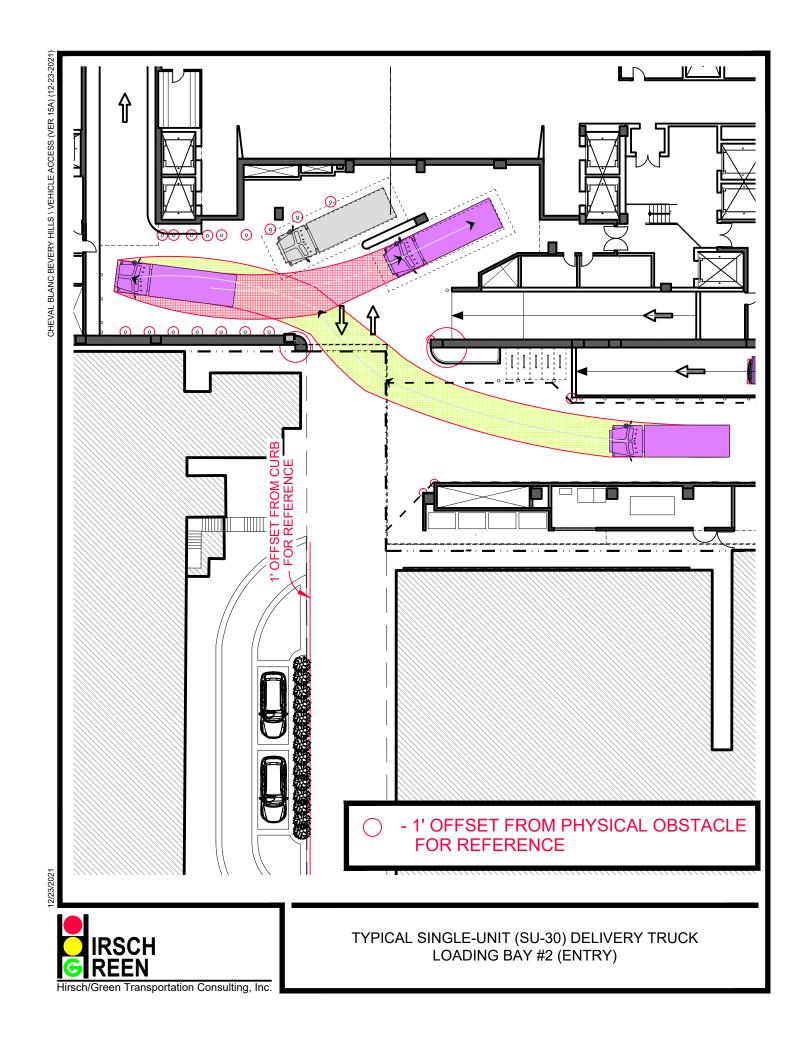


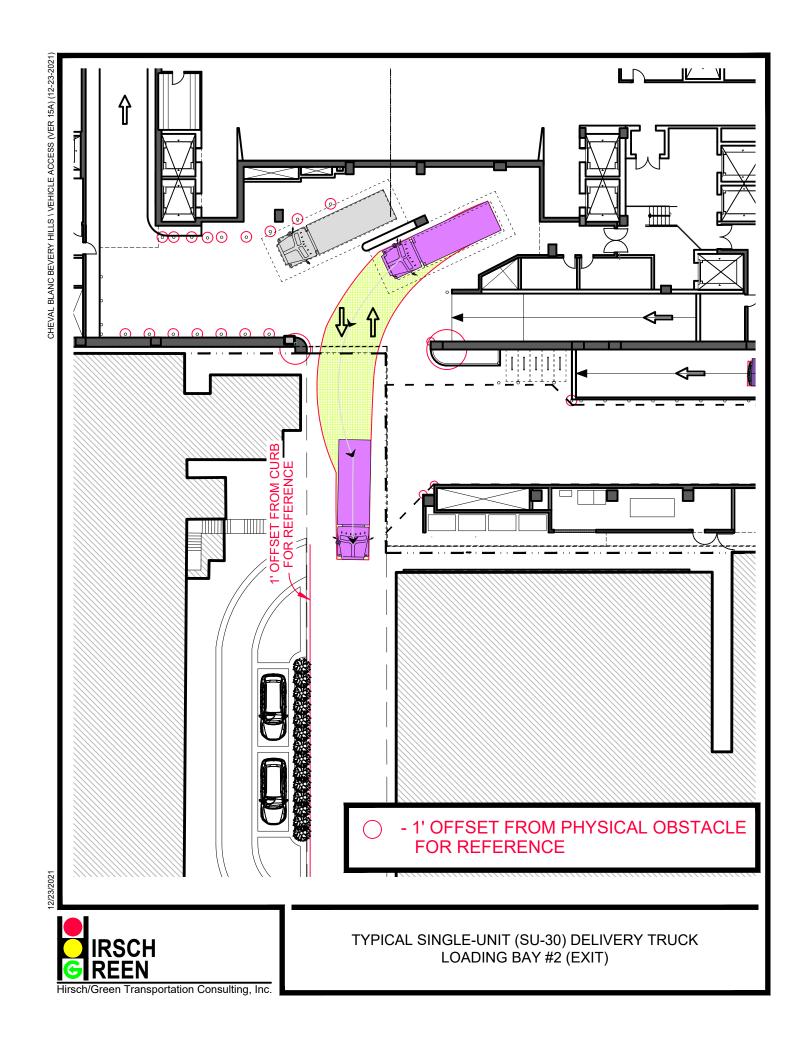


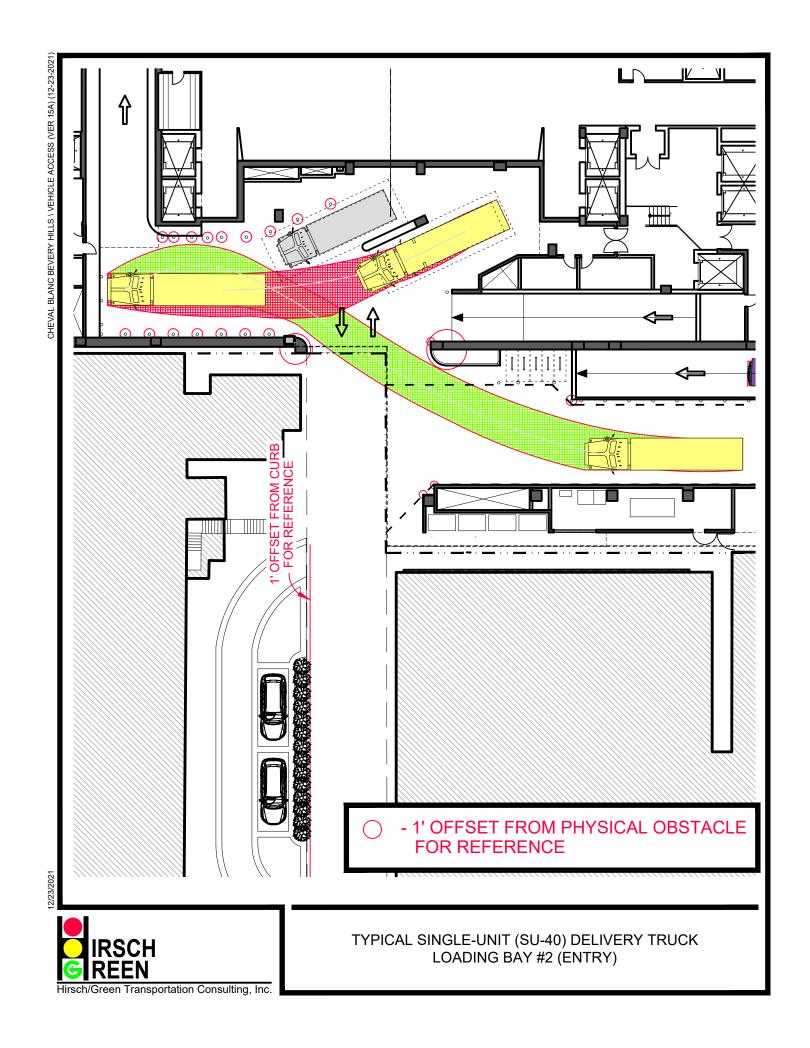
| PROPOSED P | ROJECT LOADING BA | AY VEHICULAR A | ACCESS DIAGRAM | IS |
|------------|-------------------|----------------|----------------|----|
| | | | | |
| | | | | |
| | | | | |
| | | | | |
| | | | | |

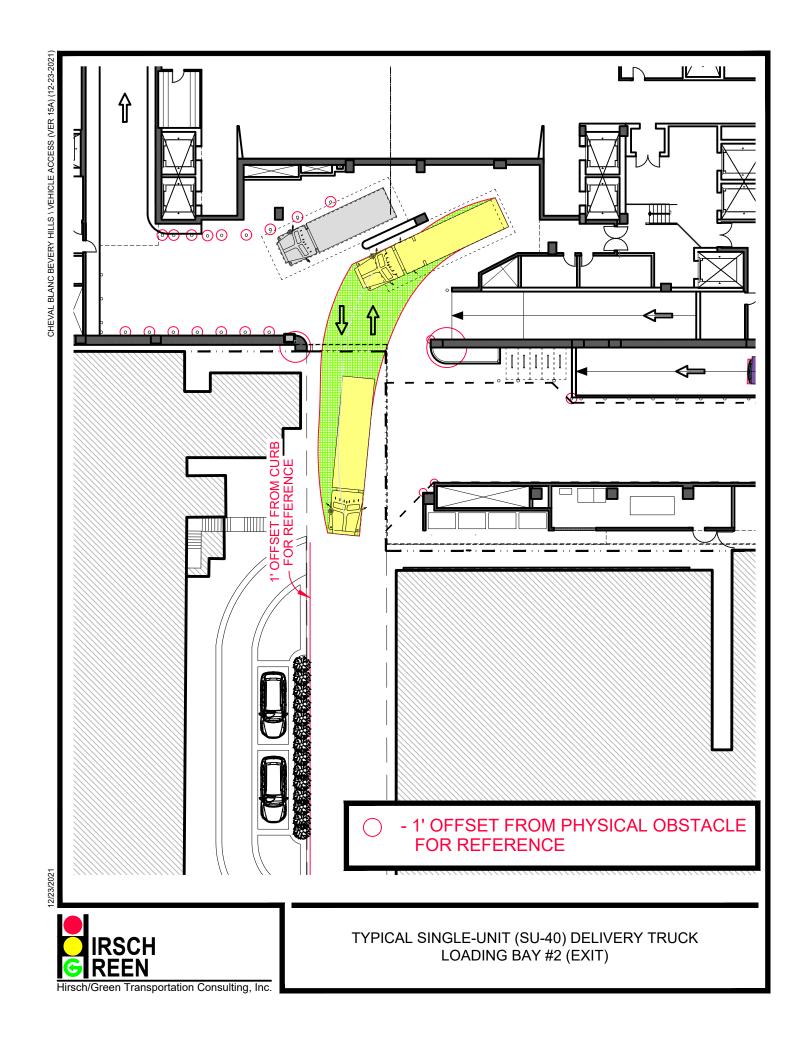


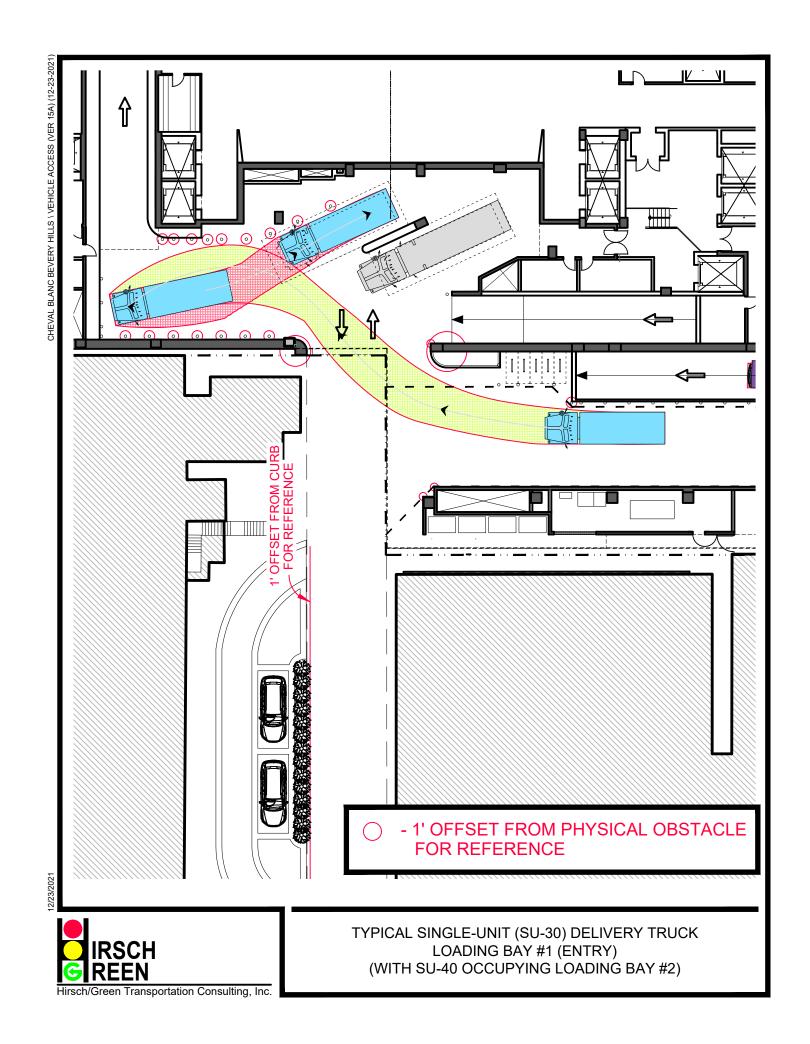


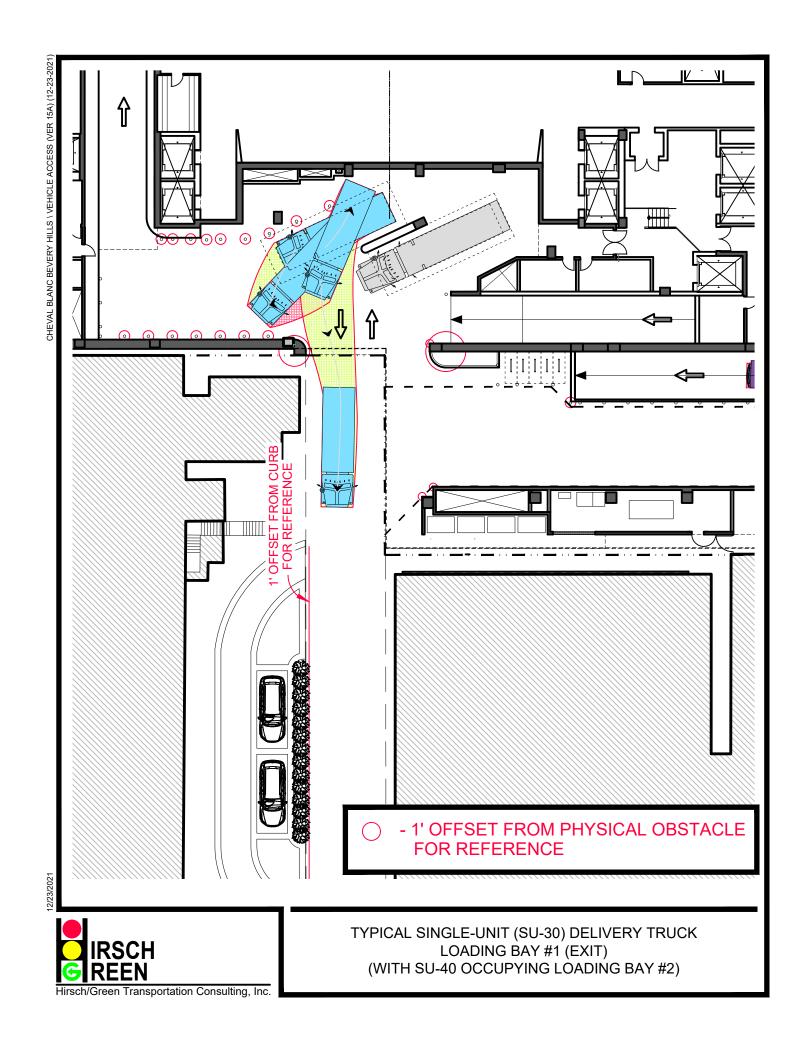








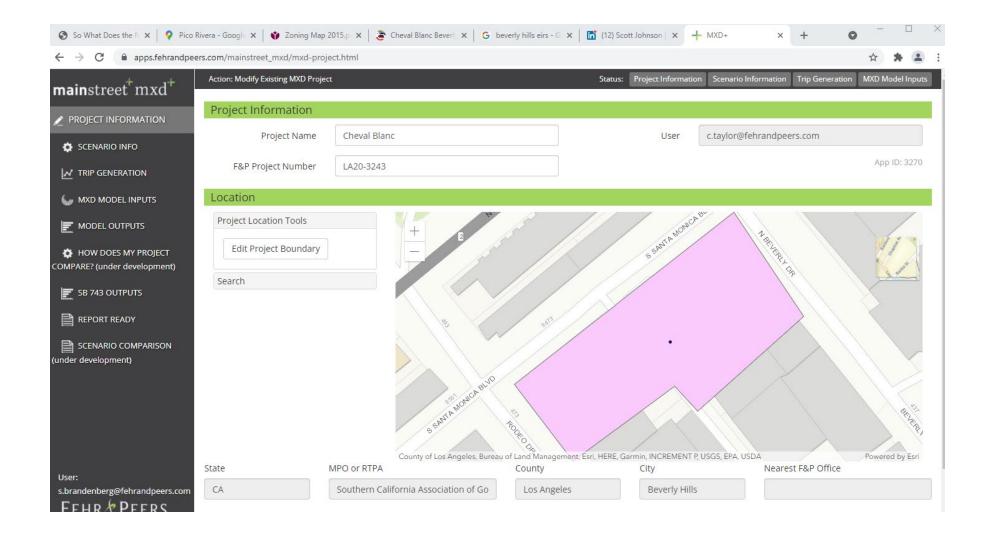






Chavel Blanc MXD+ Model

Fehr & Peers, December 2021



Model Outputs (Vehicle Trips)

| Land Use | | ITE Code | Quantity | Deily | Α | M Peak | Hour | PM Peak Hour | | |
|--|--------------------|------------------|----------|--------|-----|--------|-------|--------------|-----|-------|
| Land Ose | Units ¹ | ITE Code | Quantity | Daily | In | Out | Total | ln | Out | Total |
| Net New Uses | | | | | | | | | | |
| (931) - Quality Restaurant (Adj Streets, 7-9A, 4-6P) | 1000 Sq. Ft. FLA | 931 ² | 25.094 | 2104 | 0 | 0 | 18 | 131 | 65 | 196 |
| (918) - Hair Salon (Adj Streets, 7-9A, 4-6P) | 1000 Sq. Ft. FLA | 918 ³ | 12.936 | 0 | 0 | 0 | 16 | 3 | 16 | 19 |
| Custom | Custom | 000 ⁴ | 500 | 180 | 16 | 4 | 20 | 32 | 8 | 40 |
| (310) - Hotel (Adj Streets, 7-9A, 4-6P) | Rooms | 310 ⁵ | 115 | 961 | 32 | 22 | 54 | 35 | 34 | 69 |
| (820) - Shopping Center (Adj Street, 7-9A, 4-6P) | 1000 Sq. Ft. | 820 ⁶ | 24.976 | 943 | 14 | 9 | 23 | 46 | 49 | 95 |
| Reductions | | | | | | | | | | |
| Internal Capture | | | | -24 | -2 | -2 | -4 | -28 | -20 | -48 |
| External Walk, Bike, and Transit | | | | -1,420 | -23 | -24 | -47 | -74 | -51 | -125 |
| Total Reductions | | | | -1,444 | -25 | -26 | -51 | -102 | -71 | -173 |
| Net New Project Trips | | | | 2,744 | 37 | 9 | 80 | 145 | 101 | 246 |

1. DU = dweling units. KSF = 1000 square feet 2. ITE Trip Generation land use category (931) - Quality Restaurant (Adj Streets, 7-9A, 4-6P) Daily: T = 83.84(X) AM Peak Hour: T = 0.73(X) (0% in, 0% out)
 PM Peak Hour: T = 7.80(X) (67% in, 33% out) 3. ITE Trip Generation land use category (918) - Hair Salon (Adj Streets, 7-9A, 4-6P) Daily: T = 0.00(X) AM Peak Hour: T = 1.21(X) (0% in, 0% out) PM Peak Hour: T = 1.45(X) (17% in, 83% out) 4. ITE Trip Generation land use category Custom Daily: T = 0.00(X) AM Peak Hour: T = 0.00(X) PM Peak Hour: T = 0.00(X) 5. ITE Trip Generation land use category (310) - Hotel (Adj Streets, 7-9A, 4-6P) Daily: T = 8.36(X) AM Peak Hour: T = 0.47(X) (59% in, 41% out)
 PM Peak Hour: T = 0.60(X) (51% in, 49% out) 6. ITE Trip Generation land use category (820) - Shopping Center (Adj Street, 7-9A, 4-6P) Daily: T = 37.75(X)
 AM Peak Hour: T = 0.94(X) (62% in, 38% out)
 PM Peak Hour: T = 3.81(X) (48% in, 52% out) 7. Reductions based on application of MXD+ model: • Total Reductions: Daily = 34.5%, AM Peak Hour = 39.3%, PM Peak Hour = 41.3% Internal Capture: Daily = 0.6%, AM Peak Hour = 3.1%, PM Peak Hour = 11.5% External Walk, Bike, and Transit: Daily = 33.9%, AM Peak Hour = 36.2%, PM Peak Hour = 29.8% 8. Sources: ITE Trip Generation Manual, 9th and 10th Edition
 Fehr and Peers 9. Person Trips: Person Trips derived using the following average vehicle occupancy rates, applied to ITE Vehicle Trip Generation:

HBW AVO:1.05
 HBO AVO:1.05
 NHW AVO:1.05

Model Inputs

| Input Variable | Input Value | Source |
|---|-------------|--|
| MXD specific inputs | | |
| Project Area (Acres) | 1.277 | GIS |
| Intersections per Square Mile | 191 | EPA Smart Location Database (2013) - 2010 Scenario |
| Employment within 1 mile of Project Site | 38862 | City Model 2035 |
| Share of regional employment within a 30 minute trip by transit | 0.04497502 | EPA Smart Location Database (2013) - 2010 Scenario |
| Surrounding Household Size | 1.97 | Census 2010 - All Housing Types |
| Surrounding Vehicle Ownership | 1.40 | Census 2000 - All Housing Types |
| Site Household Size | 1.97 | Census 2010 - All Housing Types |
| Site Vehicle Ownership | 1.37 | ACS 2012 (5-year) - All Housing Types |
| Average Vehicle Occupancy (HBW Trips) | 1.0 | NCHRP 758 |
| Average Vehicle Occupancy (HBO Trips) | 1.0 | NCHRP 758 |
| Average Vehicle Occupancy (NHB Trips) | 1.0 | NCHRP 758 |