



BRE Space Mira Loma (MA200004)

NOISE IMPACT ANALYSIS

CITY OF JURUPA VALLEY

PREPARED BY:

Bill Lawson, PE, INCE
blawson@urbanxroads.com
(949) 584-3148

Sama Shami
sshami@urbanxroads.com
(949) 945-4407

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LIST OF ABBREVIATED TERMS

| | |
|-----------|---|
| (1) | Reference |
| ADT | Average Daily Traffic |
| ANSI | American National Standards Institute |
| Calveno | California Vehicle Noise |
| CEQA | California Environmental Quality Act |
| CNEL | Community Noise Equivalent Level |
| dBA | A-weighted decibels |
| EPA | Environmental Protection Agency |
| FHWA | Federal Highway Administration |
| FTA | Federal Transit Administration |
| INCE | Institute of Noise Control Engineering |
| L_{eq} | Equivalent continuous (average) sound level |
| L_{max} | Maximum level measured over the time interval |
| L_{min} | Minimum level measured over the time interval |
| mph | Miles per hour |
| OPR | Office of Planning and Research |
| PPV | Peak particle velocity |
| Project | BRE Space Mira Loma |
| REMEL | Reference Energy Mean Emission Level |
| RMS | Root-mean-square |
| VdB | Vibration Decibels |

EXECUTIVE SUMMARY

Urban Crossroads, Inc. has prepared this noise study to determine the potential noise impacts and the necessary noise mitigation measures, if any, for the proposed BRE Space Mira Loma development ("Project"). The Project site is located at Manitou Court and C Street in the City of Jurupa Valley. The Project is to consist of a Proposed Tentative Parcel Map for 3 parcels and a Major Site Development Permit. This study has been prepared to satisfy applicable City of Jurupa Valley standards and thresholds of significance based on guidance provided by Appendix G of the California Environmental Quality Act (CEQA) Guidelines. (1)

The results of this BRE Space Mira Loma Noise Impact Analysis are summarized below based on the significance criteria in Section 4 of this report consistent with Appendix G of the California Environmental Quality Act (CEQA) Guidelines (1). Table ES-1 shows the findings of significance for each potential noise and/or vibration impact under CEQA. All impacts are considered less than significant without mitigation.

TABLE ES-1: SUMMARY OF CEQA SIGNIFICANCE FINDINGS

| Analysis | Report Section | Significance Findings | |
|-------------------------|----------------|------------------------------|-----------|
| | | Unmitigated | Mitigated |
| Off-Site Traffic Noise | 7 | <i>Less Than Significant</i> | - |
| Operational Noise | 9 | <i>Less Than Significant</i> | - |
| Construction Noise | 10 | <i>Less Than Significant</i> | - |
| Construction Vibration | | <i>Less Than Significant</i> | - |
| Nighttime Concrete Pour | | <i>Less Than Significant</i> | - |

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1 INTRODUCTION

This noise analysis has been completed to determine the noise impacts associated with the development of the proposed BRE Space Mira Loma ("Project"). This noise study briefly describes the proposed Project, provides information regarding noise fundamentals, describes the local regulatory setting, provides the study methods and procedures for transportation related CNEL traffic noise analysis, and evaluates the future exterior noise environment. In addition, this study includes an analysis of the potential Project-related long-term stationary-source operational noise and short-term construction impacts.

1.1 SITE LOCATION

The proposed project is located at Manitou Court and C Street in the City of Jurupa Valley as shown on Exhibit 1-A. Nearest residential land uses are to the southeast and west of the Project site. The project is bordered to the north, south and east by industrial land uses, with the California State Route 60 approximately 2,330 feet south of the Project site.

1.2 PROJECT DESCRIPTION

It is our understanding that the Project is to consist of a Proposed Tentative Parcel Map for 3 parcels and a Major Site Development Permit. The Site Development Permit includes the construction of 3 parcels: Parcel 1 with a 1,379,287-square foot (sf) logistics facility, Parcel 2 with a 560,025-sf logistics facility, and Parcel 3 with the existing 172,800-sf building (which is to remain). The uses proposed on Parcel 1 and Parcel 2 are to replace the existing 9 buildings totaling 1,579,500-sf. Exhibit 1-B illustrates a preliminary site plan for the Project. It is anticipated that the Project will be operational by Year 2022.

At the time this noise analysis was prepared, the future tenants of the proposed Project were unknown. The on-site Project-related noise sources are expected to include: cold storage activity, trailer activity, truck movements, roof-top air conditioning units, trash enclosure activity, and parking lot vehicle movements. This noise analysis is intended to describe noise level impacts associated with the expected typical operational activities at the Project site. To present a conservative approach, this report assumes the Project will operate 24-hours daily for seven days per week.

EXHIBIT 1-A: LOCATION MAP

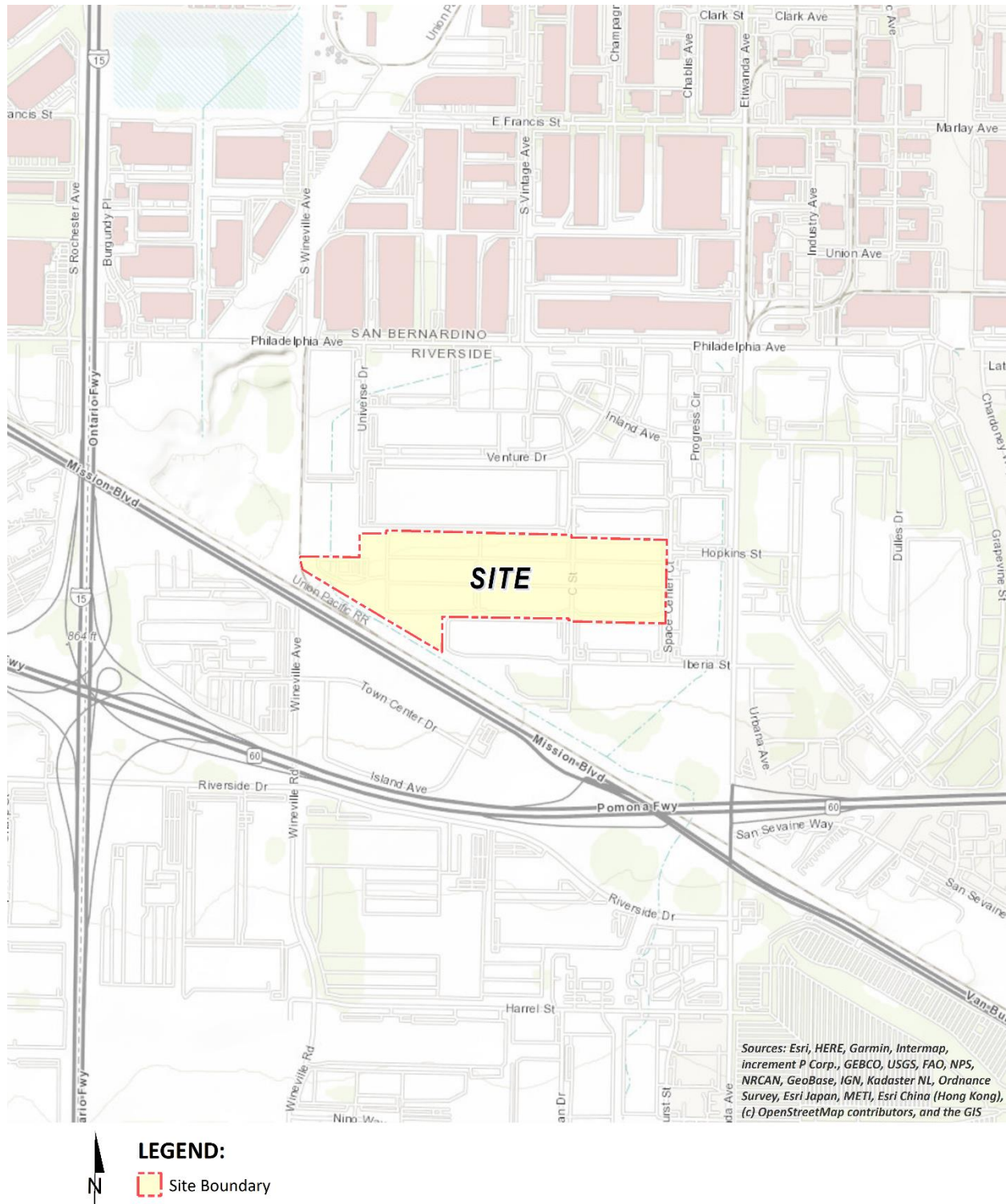
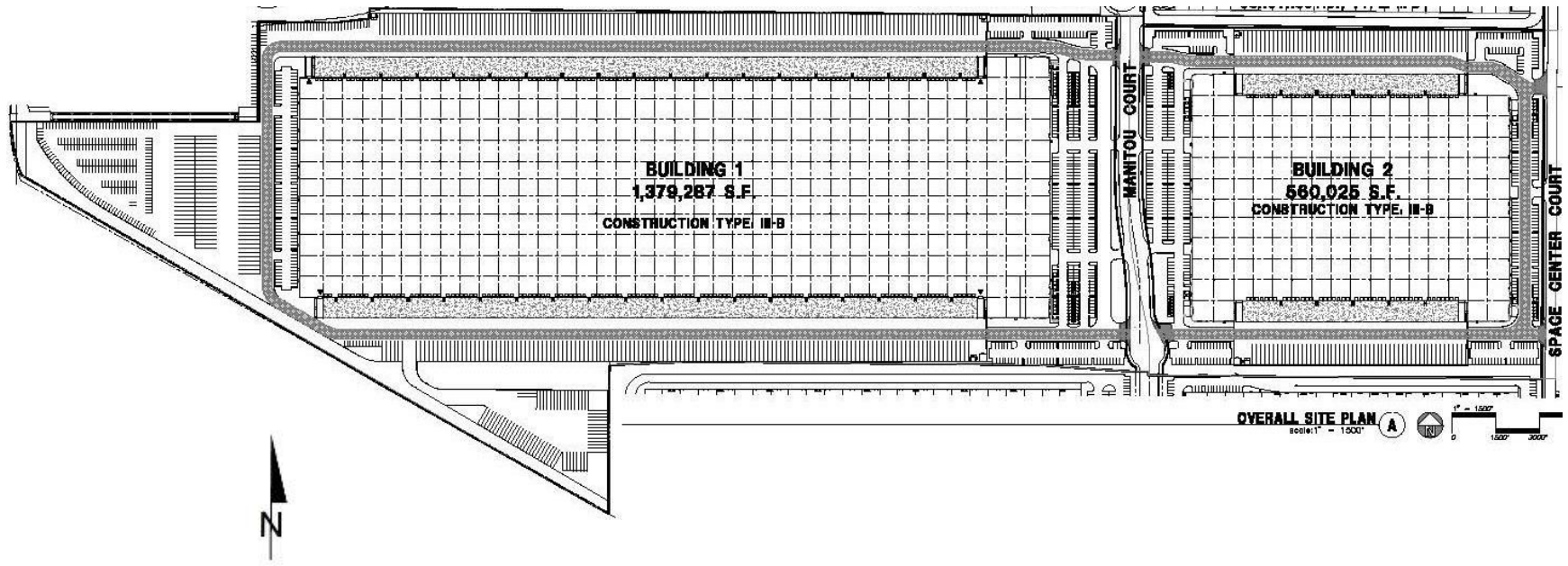


EXHIBIT 1-B: SITE PLAN



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2 FUNDAMENTALS

Noise is simply defined as "unwanted sound." Sound becomes unwanted when it interferes with normal activities, when it causes actual physical harm or when it has adverse effects on health. Noise is measured on a logarithmic scale of sound pressure level known as a decibel (dB). A-weighted decibels (dBA) approximate the subjective response of the human ear to broad frequency noise source by discriminating against very low and very high frequencies of the audible spectrum. They are adjusted to reflect only those frequencies which are audible to the human ear. Exhibit 2-A presents a summary of the typical noise levels and their subjective loudness and effects that are described in more detail below.

EXHIBIT 2-A: TYPICAL NOISE LEVELS

| COMMON OUTDOOR ACTIVITIES | COMMON INDOOR ACTIVITIES | A - WEIGHTED SOUND LEVEL dBA | SUBJECTIVE LOUDNESS | EFFECTS OF NOISE |
|--|---|------------------------------|--------------------------|---------------------|
| THRESHOLD OF PAIN | | 140 | INTOLERABLE OR DEAFENING | HEARING LOSS |
| NEAR JET ENGINE | | 130 | | |
| | | 120 | | |
| JET FLY-OVER AT 300m (1000 ft) | ROCK BAND | 110 | | |
| LOUD AUTO HORN | | 100 | VERY NOISY | SPEECH INTERFERENCE |
| GAS LAWN MOWER AT 1m (3 ft) | | 90 | | |
| DIESEL TRUCK AT 15m (50 ft), at 80 km/hr (50 mph) | FOOD BLENDER AT 1m (3 ft) | 80 | | |
| NOISY URBAN AREA, DAYTIME | VACUUM CLEANER AT 3m (10 ft) | 70 | LOUD | |
| HEAVY TRAFFIC AT 90m (300 ft) | NORMAL SPEECH AT 1m (3 ft) | 60 | | |
| QUIET URBAN DAYTIME | LARGE BUSINESS OFFICE | 50 | MODERATE | SLEEP DISTURBANCE |
| QUIET URBAN NIGHTTIME | THEATER, LARGE CONFERENCE ROOM (BACKGROUND) | 40 | | |
| QUIET SUBURBAN NIGHTTIME | LIBRARY | 30 | FAINT | NO EFFECT |
| QUIET RURAL NIGHTTIME | BEDROOM AT NIGHT, CONCERT HALL (BACKGROUND) | 20 | | |
| | BROADCAST/RECORDING STUDIO | 10 | VERY FAINT | |
| LOWEST THRESHOLD OF HUMAN HEARING | LOWEST THRESHOLD OF HUMAN HEARING | 0 | | |

Source: Environmental Protection Agency Office of Noise Abatement and Control, *Information on Levels of Environmental Noise Requisite to Protect Public Health and Welfare with an Adequate Margin of Safety* (EPA/ONAC 550/9-74-004) March 1974.

2.1 RANGE OF NOISE

Since the range of intensities that the human ear can detect is so large, the scale frequently used to measure intensity is a scale based on multiples of 10, the logarithmic scale. The scale for measuring intensity is the decibel scale. Each interval of 10 decibels indicates a sound energy ten times greater than before, which is perceived by the human ear as being roughly twice as loud (2). The most common sounds vary between 40 dBA (very quiet) to 100 dBA (very loud). Normal conversation at three feet is roughly at 60 dBA, while loud jet engine noises equate to 110 dBA

at approximately 100 feet, which can cause serious discomfort (3). Another important aspect of noise is the duration of the sound and the way it is described and distributed in time.

2.2 NOISE DESCRIPTORS

Environmental noise descriptors are generally based on averages, rather than instantaneous, noise levels. The most used figure is the equivalent level (L_{eq}). Equivalent sound levels are not measured directly but are calculated from sound pressure levels typically measured in A-weighted decibels (dBA). The equivalent sound level (L_{eq}) represents a steady state sound level containing the same total energy as a time varying signal over a given sample period (typically one hour) and is commonly used to describe the “average” noise levels within the environment.

Peak hour or average noise levels, while useful, do not completely describe a given noise environment. Noise levels lower than peak hour may be disturbing if they occur during times when quiet is most desirable, namely evening and nighttime (sleeping) hours. To account for this, the Community Noise Equivalent Level (CNEL), representing a composite 24-hour noise level is utilized. The CNEL is the weighted average of the intensity of a sound, with corrections for time of day, and averaged over 24 hours. The time-of-day corrections require the addition of 5 decibels to dBA L_{eq} sound levels in the evening from 7:00 p.m. to 10:00 p.m., and the addition of 10 decibels to dBA L_{eq} sound levels at night between 10:00 p.m. and 7:00 a.m. These additions are made to account for the noise sensitive time periods during the evening and night hours when sound appears louder. CNEL does not represent the actual sound level heard at any time, but rather represents the total sound exposure. The City of Jurupa Valley relies on the 24-hour CNEL level to assess land use compatibility with transportation related noise sources.

2.3 SOUND PROPAGATION

When sound propagates over a distance, it changes in level and frequency content. The way noise reduces with distance depends on the following factors.

2.3.1 GEOMETRIC SPREADING

Sound from a localized source (i.e., a stationary point source) propagates uniformly outward in a spherical pattern. The sound level attenuates (or decreases) at a rate of 6 dB for each doubling of distance from a point source. Highways consist of several localized noise sources on a defined path and hence can be treated as a line source, which approximates the effect of several point sources. Noise from a line source propagates outward in a cylindrical pattern, often referred to as cylindrical spreading. Sound levels attenuate at a rate of 3 dB for each doubling of distance from a line source. (2)

2.3.2 GROUND ABSORPTION

The propagation path of noise from a highway to a receiver is usually very close to the ground. Noise attenuation from ground absorption and reflective wave canceling adds to the attenuation associated with geometric spreading. Traditionally, the excess attenuation has also been expressed in terms of attenuation per doubling of distance. This approximation is usually

sufficiently accurate for distances of less than 200 feet. For acoustically hard sites (i.e., sites with a reflective surface between the source and the receiver, such as a parking lot or body of water), no excess ground attenuation is assumed. For acoustically absorptive or soft sites (i.e., those sites with an absorptive ground surface between the source and the receiver such as soft dirt, grass, or scattered bushes and trees), an excess ground attenuation value of 1.5 dB per doubling of distance is normally assumed. When added to the cylindrical spreading, the excess ground attenuation results in an overall drop-off rate of 4.5 dB per doubling of distance from a line source. (4)

2.3.3 ATMOSPHERIC EFFECTS

Receivers located downwind from a source can be exposed to increased noise levels relative to calm conditions, whereas locations upwind can have lowered noise levels. Sound levels can be increased at large distances (e.g., more than 500 feet) due to atmospheric temperature inversion (i.e., increasing temperature with elevation). Other factors such as air temperature, humidity, and turbulence can also have significant effects. (2)

2.3.4 SHIELDING

A large object or barrier in the path between a noise source and a receiver can substantially attenuate noise levels at the receiver. The amount of attenuation provided by shielding depends on the size of the object and the frequency content of the noise source. Shielding by trees and other such vegetation typically only has an “out of sight, out of mind” effect. That is, the perception of noise impact tends to decrease when vegetation blocks the line-of-sight to nearby residents. However, for vegetation to provide a substantial, or even noticeable, noise reduction, the vegetation area must be at least 15 feet in height, 100 feet wide and dense enough to completely obstruct the line-of sight between the source and the receiver. This size of vegetation may provide up to 5 dBA of noise reduction. The Federal Highway Administration (FHWA) does not consider the planting of vegetation to be a noise abatement measure. (4)

2.3.5 REFLECTION

Field studies conducted by the FHWA have shown that the reflection from barriers and buildings does not substantially increase noise levels. (4) If all the noise striking a structure was reflected back to a given receiving point, the increase would be theoretically limited to 3 dBA. Further, not all the acoustical energy is reflected back to same point. Some of the energy would go over the structure, some is reflected to points other than the given receiving point, some is scattered by ground coverings (e.g., grass and other plants), and some is blocked by intervening structures and/or obstacles (e.g., the noise source itself). Additionally, some of the reflected energy is lost due to the longer path that the noise must travel. FHWA measurements made to quantify reflective increases in traffic noise have not shown an increase of greater than 1-2 dBA; an increase that is not perceptible to the average human ear.

2.4 NOISE CONTROL

Noise control is the process of obtaining an acceptable noise environment for an observation point or receiver by controlling the noise source, transmission path, receiver, or all three. This

concept is known as the source-path-receiver concept. In general, noise control measures can be applied to these three elements.

2.5 NOISE BARRIER ATTENUATION

Effective noise barriers can reduce noise levels by up to 10 to 15 dBA, cutting the loudness of traffic noise in half. A noise barrier is most effective when placed close to the noise source or receiver. Noise barriers, however, do have limitations. For a noise barrier to work, it must be high enough and long enough to block the path of the noise source. (4)

2.6 LAND USE COMPATIBILITY WITH NOISE

Some land uses are more tolerant of noise than others. For example, schools, hospitals, churches, and residences are more sensitive to noise intrusion than are commercial or industrial developments and related activities.

As ambient noise levels affect the perceived amenity or livability of a development, so too can the mismanagement of noise impacts impair the economic health and growth potential of a community by reducing the area's desirability as a place to live, shop and work. For this reason, land use compatibility with the noise environment is an important consideration in the planning and design process. The FHWA encourages State and Local government to regulate land development in such a way that noise-sensitive land uses are either prohibited from being located adjacent to a highway, or that the developments are planned, designed, and constructed in such a way that noise impacts are minimized. (5)

2.7 COMMUNITY RESPONSE TO NOISE

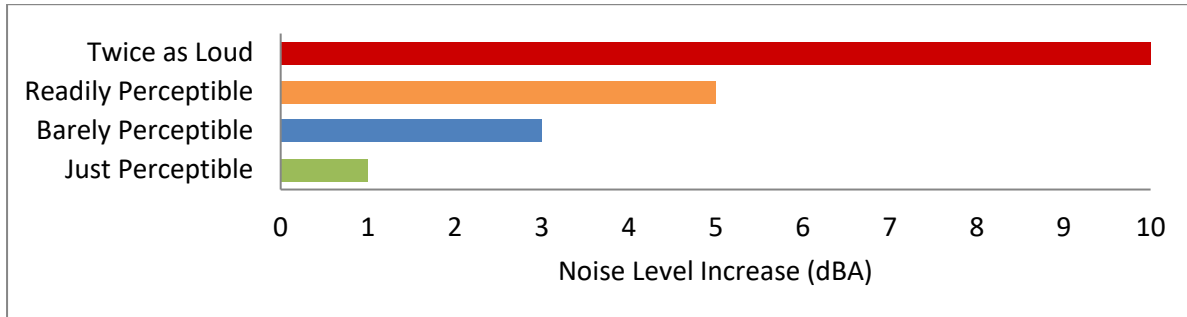
Community responses to noise may range from registering a complaint by telephone or letter, to initiating court action depending upon everyone's susceptibility to noise and personal attitudes about noise. Several factors are related to the level of community annoyance including:

- Fear associated with noise producing activities;
- Socio-economic status and educational level;
- Perception that those affected are being unfairly treated;
- Attitudes regarding the usefulness of the noise-producing activity;
- Belief that the noise source can be controlled.

Approximately ten percent of the population has a very low tolerance for noise and will object to any noise not of their making. Consequently, even in the quietest environment, some complaints will occur. Twenty-five percent of the population will not complain even in very severe noise environments. Thus, a variety of reactions can be expected from people exposed to any given noise environment. (6) Surveys have shown that about ten percent of the people exposed to traffic noise of 60 dBA will report being highly annoyed with the noise, and each increase of one dBA is associated with approximately two percent more people being highly annoyed. When traffic noise exceeds 60 dBA or aircraft noise exceeds 55 dBA, people may begin to complain. (6) Despite this variability in behavior on an individual level, the population can be expected to exhibit the following responses to changes in noise levels as shown on Exhibit 2-B. A change of

3 dBA are considered *barely perceptible*, and changes of 5 dBA are considered *readily perceptible*.
(4)

EXHIBIT 2-B: NOISE LEVEL INCREASE PERCEPTION



2.8 VIBRATION

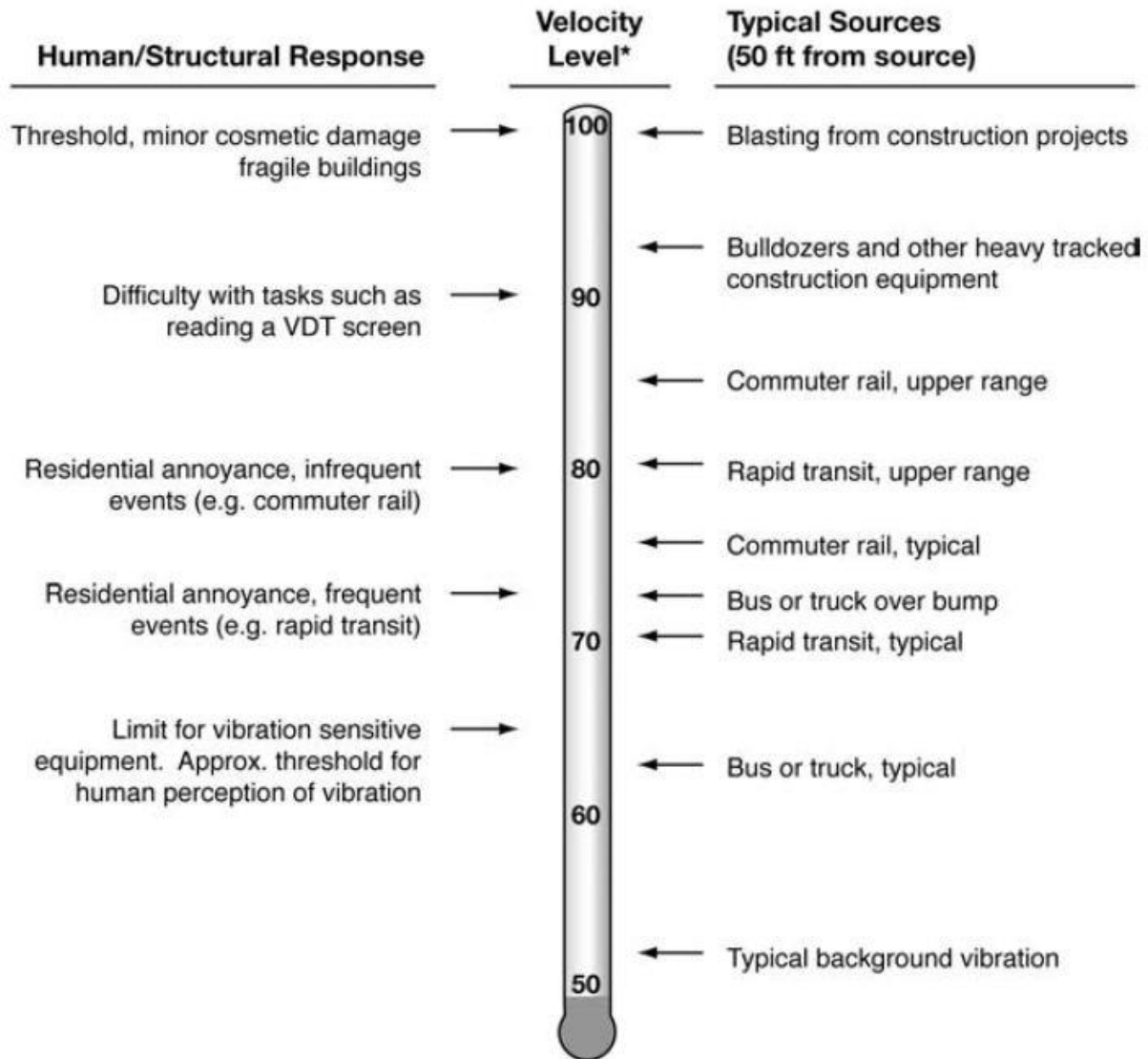
Per the Federal Transit Administration (FTA) *Transit Noise and Vibration Impact Assessment Manual* (7), vibration is the periodic oscillation of a medium or object. The rumbling sound caused by the vibration of room surfaces is called structure-borne noise. Sources of ground-borne vibrations include natural phenomena (e.g., earthquakes, volcanic eruptions, sea waves, landslides) or human-made causes (e.g., explosions, machinery, traffic, trains, construction equipment). Vibration sources may be continuous, such as factory machinery, or transient, such as explosions. As is the case with airborne sound, ground-borne vibrations may be described by amplitude and frequency.

There are several different methods that are used to quantify vibration. The peak particle velocity (PPV) is defined as the maximum instantaneous peak of the vibration signal. The PPV is most frequently used to describe vibration impacts to buildings but is not always suitable for evaluating human response (annoyance) because it takes some time for the human body to respond to vibration signals. Instead, the human body responds to average vibration amplitude often described as the root mean square (RMS). The RMS amplitude is defined as the average of the squared amplitude of the signal and is most frequently used to describe the effect of vibration on the human body. Decibel notation (VdB) is commonly used to measure RMS. Decibel notation (VdB) serves to reduce the range of numbers used to describe human response to vibration. Typically, ground-borne vibration generated by man-made activities attenuates rapidly with distance from the source of the vibration. Sensitive receivers for vibration include structures (especially older masonry structures), people (especially residents, the elderly, and sick), and vibration-sensitive equipment and/or activities.

The background vibration-velocity level in residential areas is generally 50 VdB. Ground-borne vibration is normally perceptible to humans at approximately 65 VdB. For most people, a vibration-velocity level of 75 VdB is the approximate dividing line between barely perceptible and distinctly perceptible levels. Typical outdoor sources of perceptible ground-borne vibration are construction equipment, steel-wheeled trains, and traffic on rough roads. If a roadway is smooth, the ground-borne vibration is rarely perceptible. The range of interest is from approximately 50

VdB, which is the typical background vibration-velocity level, to 100 VdB, which is the general threshold where minor damage can occur in fragile buildings. Exhibit 2-C illustrates common vibration sources and the human and structural response to ground-borne vibration.

EXHIBIT 2-C: TYPICAL LEVELS OF GROUND-BORNE VIBRATION



* RMS Vibration Velocity Level in VdB relative to 10^{-6} inches/second

Source: Federal Transit Administration (FTA) Transit Noise and Vibration Impact Assessment Manual.

3 REGULATORY SETTING

To limit population exposure to physically and/or psychologically damaging as well as intrusive noise levels, the federal government, the State of California, various county governments, and most municipalities in the state have established standards and ordinances to control noise. In most areas, automobile and truck traffic is the major source of environmental noise. Traffic activity generally produces an average sound level that remains constant with time. Air and rail traffic, and commercial and industrial activities are also major sources of noise in some areas. Federal, state, and local agencies regulate different aspects of environmental noise. Federal and state agencies generally set noise standards for mobile sources such as aircraft and motor vehicles, while regulation of stationary sources is left to local agencies.

3.1 STATE OF CALIFORNIA NOISE REQUIREMENTS

The State of California regulates freeway noise, sets standards for sound transmission, provides occupational noise control criteria, identifies noise standards, and provides guidance for local land use compatibility. State law requires that each county and city adopt a General Plan that includes a Noise Element which is to be prepared per guidelines adopted by the Governor's Office of Planning and Research (OPR). (8) The purpose of the Noise Element is to *limit the exposure of the community to excessive noise levels*. In addition, the California Environmental Quality Act (CEQA) requires that all known environmental effects of a project be analyzed, including environmental noise impacts.

3.2 CITY OF JURUPA VALLEY GENERAL PLAN

The City of Jurupa Valley adopted the General Plan on September 7, 2017 (10) The Noise Element identifies several policies to minimize the impacts of excessive noise levels throughout the community and establishes noise level compatibility guidelines for all land uses.

3.2.1 POLICIES AND PROGRAMS

To protect City of Jurupa Valley residents from excessive noise, the Noise Element contains the following policies and programs related to the Project:

- NE 1.1 *Utilize the Land Use/Noise Compatibility Matrix, Figure 7-3, to determine the compatibility of proposed development, including General Plan amendments, specific plan amendments, town center plans, and rezoning's, with existing land uses and/or noise exposure due to transportation sources.*
- NE 1.3 *New or Modified Stationary Noise Sources. Noise created by new stationary noise sources, or by existing stationary noise sources that undergo modifications that may increase noise levels, shall be mitigated so as not exceed the noise level standards of Figure 7-3. This policy does not apply to noise levels associated with agricultural operations existing in 2017.*
- NE 1.4 *Acoustical Assessment. Require an acoustical assessment for proposed General Plan amendments and rezones that exceed the "Normally Acceptable" thresholds of the Land Use/Noise Compatibility Matrix.*

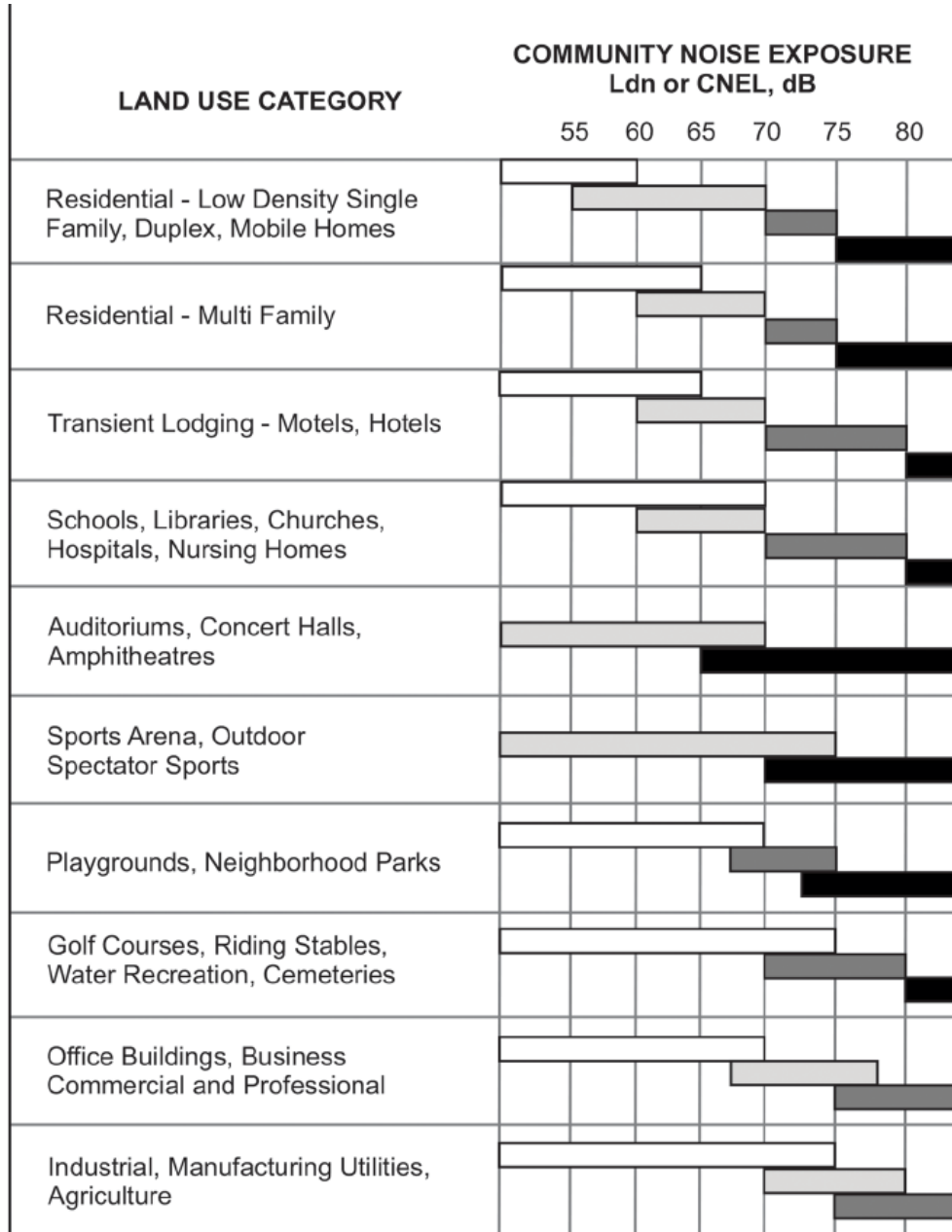
- NE 1.5 Noise-Sensitive Uses. Consider the following uses noise sensitive and discourage these uses in areas in excess of 65 CNEL: schools, hospitals, assisted living facilities, mental care facilities, residential uses, libraries, passive recreational uses, and places of worship.*
- NE 3.1 Noise Analysis. Require that a noise analysis be conducted by an acoustical specialist for all proposed development projects that have the potential to generate significant noise near a noise-sensitive land use, or on or near land designated for noise-sensitive land uses, and ensure that recommended mitigation measures are implemented.*
- NE 3.5 Construction Noise. Limit commercial construction activities adjacent to or within 200 feet of residential uses to weekdays, between 7:00 a.m. and 6:00 p.m., and limit high-noise-generating construction activities (e.g., grading, demolition, pile driving) near sensitive receptors to weekdays between 9:00 a.m. and 3:00 p.m.*





To ensure noise-sensitive land uses are protected from high levels of noise (NE 1.1), Figure 7-3 of the Noise Element identifies guidelines to evaluate proposed developments based on exterior and interior noise level limits for land uses and requires a noise analysis to determine needed mitigation measures if necessary. The Noise Element requires an acoustical assessment for proposed General Plan amendments and rezones that exceed the “Normally Acceptable” thresholds of the Land Use/Noise Compatibility Matrix (NE 1.4) and identifies residential use as a noise-sensitive land use (NE 1.5) discouraging new development in areas with transportation related levels more than 65 dBA CNEL.

To control stationary noise sources from Industrial, commercial, and manufacturing facilities that may affect sensitive land uses, Policy (NE 3.1) requires that a noise analysis be conducted by an acoustical specialist for all proposed development projects. Maximum noise exposure levels from stationary sources for noise-sensitive uses are regulated by the Municipal Code. To prevent high levels of construction noise from impacting noise-sensitive land uses, Policy NE 3.5 limits construction activities within 200 feet of residential uses to weekdays, between 7:00 a.m. and 6:00 p.m., and limit high-noise-generating construction activities (e.g., grading, demolition, pile driving) near sensitive receptors to weekdays between 9:00 a.m. and 3:00 p.m.

3.2.2 LAND USE COMPATIBILITY

The noise criteria identified in the City of Jurupa Valley Noise Element (Figure 7-3) are guidelines to evaluate the land use compatibility of transportation related noise. The compatibility criteria, shown on Exhibit 3-A, provides the city with a planning tool to gauge the compatibility of land uses relative to existing and future exterior noise levels. The *Land Use/Noise Compatibility Matrix* describes categories of compatibility and not specific noise standards. The warehouse/industrial use of the Project is considered *normally acceptable* with unmitigated exterior noise levels of less than 75 dBA CNEL based on the *Industrial, Manufacturing, Utilities, Agriculture* land use compatibility criteria shown on Exhibit 3-A.

EXHIBIT 3-A: LAND USE/NOISE COMPATIBILITY MATRIX

-  **NORMALLY ACCEPTABLE**
Specified land use is satisfactory, based upon the assumption that any buildings involved are of normal conventional construction, without any special noise insulation requirements.
-  **CONDITIONALLY ACCEPTABLE**
New construction or development should be undertaken only after a detailed analysis of the noise reduction requirements is made and needed noise insulation features included in the design. Conventional construction, but with closed windows and fresh air sup systems or air conditioning will normally suffice.
-  **NORMALLY UNACCEPTABLE**
New construction or development should generally be discouraged. If new construction or development does proceed, a detailed analysis of the noise reduction requirements must be made and needed noise reduction features included in the design.
-  **CLEARLY UNACCEPTABLE**
New construction or development should generally not be undertaken.

Source: Jurupa Valley General Plan, 2017 Figure 7-3.

Residential designated land uses in the Project study area are considered *normally acceptable* with exterior noise levels below 60 dBA CNEL, and *conditionally acceptable* with exterior noise levels of up to 70 dBA CNEL. For *conditionally acceptable* exterior noise levels, of up to 80 dBA CNEL for Project land uses, *new construction or development should be undertaken only after a detailed analysis of the noise reduction requirements is made and the needed noise insulation features are included in the design. Conventional construction, but with closed windows and fresh air supply systems or air conditioning will normally suffice.* (10)

3.3 OPERATIONAL NOISE STANDARDS

To analyze noise impacts originating from a designated fixed location or private property such as BRE Space Mira Loma Project, stationary-source (operational) noise such as the expected cold storage activity, trailer activity, truck movements, roof-top air conditioning units, trash enclosure activity, and parking lot vehicle movements are typically evaluated against standards established under a jurisdiction's Municipal Code.

However, Section 11.05.010 of the City of Jurupa Valley Municipal Code (12) indicates that this chapter is not intended to establish city-wide standards regulating noise. Therefore, potential Project related stationary-source (operational) noise impacts are limited to the generation of a substantial temporary or permanent relative increase in the ambient noise levels. The City of Jurupa Valley Municipal Code is included in Appendix 3.1

3.4 CONSTRUCTION NOISE STANDARDS

To control noise impacts associated with the construction of the proposed Project, the City of Jurupa Valley Municipal Code has established limits to the hours of operation. Section 11.05.020 indicates that noise associated with any private construction activity located within one-quarter of a mile from an inhabited dwelling is considered exempt between the hours of 6:00 a.m. and 6:00 p.m., during the months of June through September, and 7:00 a.m. and 6:00 p.m., during the months of October through May. (12) In addition, City of Jurupa Valley General Plan Noise Element Policy NE 3.5 limits commercial construction activities adjacent to or within 200 feet of residential uses to weekdays, between 7:00 a.m. and 6:00 p.m., as well as limiting high-noise-generating construction activities (e.g., grading, demolition, pile driving) near sensitive receptors to weekdays between 9:00 a.m. and 3:00 p.m. (10)

Neither the General Plan nor Municipal Code establish numeric maximum acceptable construction source noise levels at potentially affected receivers for CEQA analysis purposes. Therefore, this analysis relies on a numerical daytime construction threshold based on Federal Transit Administration (FTA) *Transit Noise and Vibration Impact Assessment Manual*. According to the FTA, local noise ordinances are typically not very useful in evaluating construction noise. They usually relate to nuisance and hours of allowed activity, and sometimes specify limits in terms of maximum levels, but are generally not practical for assessing the impact of a construction project. Project construction noise criteria should account for the existing noise environment, the absolute noise levels during construction activities, the duration of the construction, and the adjacent land use. Due to the lack of standardized construction noise

thresholds, the FTA provides guidelines that can be considered reasonable criteria for construction noise assessment. The FTA considers a daytime exterior construction noise level of 80 dBA L_{eq} as a reasonable threshold for noise sensitive land use. (7 p. 179)

3.5 CONSTRUCTION VIBRATION STANDARDS

To analyze vibration impacts originating from the operation and construction of the BRE Space Mira Loma, vibration-generating activities are evaluated against standards identified by the City of Jurupa Valley as a threshold of 0.2 inches per second (in/sec) peak-particle-velocity (PPV) during either long-term operation or construction of the Project. (13) This analysis focuses on the potential ground-borne vibration associated with vehicular traffic and construction activities. Ground-borne vibration levels from automobile traffic are generally overshadowed by vibration generated by heavy trucks that roll over the same uneven roadway surfaces. However, due to the rapid drop-off rate of ground-borne vibration and the short duration of the associated events, vehicular traffic-induced ground-borne vibration is rarely perceptible beyond the roadway right-of-way, and rarely results in vibration levels that cause damage to buildings in the vicinity.

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4 SIGNIFICANCE CRITERIA

The following significance criteria are based on currently adopted guidance provided by Appendix G of the California Environmental Quality Act (CEQA) Guidelines. (8) For the purposes of this report, impacts would be potentially significant if the Project results in or causes:

- A. (Threshold A) Generation of a substantial temporary or permanent increase in ambient noise levels in the vicinity of the project in excess of standards established in the local general plan or noise ordinance, or applicable standards of other agencies?
- B. (Threshold B) Generation of excessive ground-borne vibration or ground-borne noise levels?
- C. (Threshold C) For a project located within the vicinity of a private airstrip or an airport land use plan or, where such a plan has not been adopted, within two miles of a public airport or public use airport, would the project expose people residing or working in the project area to excessive noise levels?

4.1 NOISE LEVEL INCREASE (THRESHOLD A)

Noise level increases resulting from the Project are evaluated based on the Appendix G CEQA Guidelines described above at the closest sensitive receiver locations. Under CEQA, consideration must be given to the magnitude of the increase, the existing ambient noise levels, and the location of noise-sensitive receivers to determine if a noise increase represents a significant adverse environmental impact. According to the City of Jurupa Valley, a noticeable increase of 3 dBA or more than City standards is considered a significant impact. (13) The City of Jurupa Valley noise related CEQA thresholds guidance is provided in Appendix 4.1.

4.2 VIBRATION (THRESHOLD B)

As described in Section 3.5, the vibration impacts originating from the construction of the BRE Space Mira Loma, vibration-generating activities are appropriately evaluated the thresholds of significance identified by the City of Jurupa Valley. The City of Jurupa Valley maintains a 0.2 inches per second (in/sec) peak-particle-velocity (PPV) vibration threshold during Project construction.

4.3 CEQA GUIDELINES NOT FURTHER ANALYZED (THRESHOLD C)

As previously indicated in Section 3.6, the noise contour boundaries of Flabob Airport are presented on Exhibit 3-B of this report and show that the Project site is located outside the Airport Influence Area Boundaries. Therefore, airport noise level impacts are considered *less than significant*, and no further noise analysis is provided under Guideline C.

4.4 SIGNIFICANCE CRITERIA SUMMARY

Noise impacts shall be considered significant if any of the following occur as a direct result of the proposed development. Table 4-1 shows the significance criteria summary matrix.

TABLE 4-1: SIGNIFICANCE CRITERIA SUMMARY

| Analysis | Receiving Land Use | Condition(s) | Significance Criteria | |
|--------------|---------------------|--|---|------------|
| | | | Daytime | Nighttime |
| Off-Site | Noise-Sensitive | If ambient is < 65 dBA CNEL ¹ | Project plus ambient > 65 dBA CNEL and a ≥ 3 dBA CNEL Project increase ² | |
| | Non-Noise-Sensitive | If ambient is < 70 dBA CNEL ¹ | Project plus ambient > 70 dBA CNEL and a ≥ 3 dBA CNEL Project increase ² | |
| Operational | Noise-Sensitive | Exterior Noise Level Standards ² | 65 dBA Leq | 45 dBA Leq |
| | | If ambient is > 65 dBA Leq ¹ | ≥ 3 dBA Leq Project increase ² | |
| | | Vibration Level Threshold ² | 0.2 in/sec PPV | |
| Construction | Noise-Sensitive | Limit typical construction activities to weekdays between 7:00 a.m. and 6:00 p.m. Limit grading, demolition, pile driving to weekdays between 9:00 a.m. and 3:00 p.m. ³ | | |
| | | Noise Level Threshold ⁴ | 80 dBA Leq | 70 dBA Leq |
| | | Vibration Level Threshold ² | 0.2 in/sec PPV | |

¹ City of Jurupa Valley General Plan Noise Element Policy NE 1.5 and Figure 7-3 *normally acceptable* noise exposure.

² City of Jurupa Valley noise related CEQA thresholds guidance for noise sensitive receivers (Appendix 4.1).

³ City of Jurupa Valley Municipal Code, Section 11.05.020.(9).

⁴ Federal Transit Administration, Transit Noise and Vibration Impact Assessment Manual.

"Daytime" = 7:00 a.m. to 10:00 p.m.; "Nighttime" = 10:00 p.m. to 7:00 a.m.; "PPV" = Peak Particle Velocity

5 EXISTING NOISE LEVEL MEASUREMENTS

To assess the existing noise level environment, 24-hour noise level measurements were taken at five locations in the Project study area. The receiver locations were selected to describe and document the existing noise environment within the Project study area. Exhibit 5-A provides the boundaries of the Project study area and the noise level measurement locations. To fully describe the existing noise conditions, noise level measurements were collected by Urban Crossroads, Inc. on Wednesday, July 15th, 2020. Appendix 5.1 includes study area photos.

5.1 MEASUREMENT PROCEDURE AND CRITERIA

To describe the existing noise environment, the hourly noise levels were measured during typical weekday conditions over a 24-hour period. By collecting individual hourly noise level measurements, it is possible to describe the daytime and nighttime hourly noise levels and calculate the 24-hour CNEL. The long-term noise readings were recorded using Piccolo Type 2 integrating sound level meter and dataloggers. The Piccolo sound level meters were calibrated using a Larson-Davis calibrator, Model CAL 150. All noise meters were programmed in "slow" mode to record noise levels in "A" weighted form. The sound level meters and microphones were equipped with a windscreen during all measurements. All noise level measurement equipment satisfies the American National Standards Institute (ANSI) standard specifications for sound level meters ANSI S1.4-2014/IEC 61672-1:2013. (17)

5.2 NOISE MEASUREMENT LOCATIONS

The long-term noise level measurements were positioned as close to the nearest sensitive receiver locations as possible to assess the existing ambient hourly noise levels surrounding the Project site. Both Caltrans and the FTA recognize that it is not reasonable to collect noise level measurements that can fully represent every part of a private yard, patio, deck, or balcony normally used for human activity when estimating impacts for new development projects. This is demonstrated in the Caltrans general site location guidelines which indicate that, *sites must be free of noise contamination by sources other than sources of interest. Avoid sites located near sources such as barking dogs, lawnmowers, pool pumps, and air conditioners unless it is the express intent of the analyst to measure these sources.* (2) Further, FTA guidance states, *that it is not necessary nor recommended that existing noise exposure be determined by measuring at every noise-sensitive location in the project area. Rather, the recommended approach is to characterize the noise environment for clusters of sites based on measurements or estimates at representative locations in the community.* (7)

Based on recommendations of Caltrans and the FTA, it is not necessary to collect measurements at each individual building or residence, because each receiver measurement represents a group of buildings that share acoustical equivalence. (7) In other words, the area represented by the receiver shares similar shielding, terrain, and geometric relationship to the reference noise source. Receivers represent a location of noise sensitive areas and are used to estimate the future noise level impacts. Collecting reference ambient noise level measurements at the nearby

sensitive receiver locations allows for a comparison of the before and after Project noise levels and is necessary to assess potential noise impacts due to the Project's contribution to the ambient noise levels.

5.3 NOISE MEASUREMENT RESULTS

The noise measurements presented below focus on the average or equivalent sound levels (L_{eq}). The equivalent sound level (L_{eq}) represents a steady state sound level containing the same total energy as a time varying signal over a given sample period. Table 5-1 identifies the hourly daytime (7:00 a.m. to 10:00 p.m.) and nighttime (10:00 p.m. to 7:00 a.m.) noise levels at each noise level measurement location. Appendix 5.2 provides a summary of the existing hourly ambient noise levels.

TABLE 5-1: 24-HOUR AMBIENT NOISE LEVEL MEASUREMENTS

| Location ¹ | Description | Energy Average Noise Level (dBA L_{eq}) ² | | CNEL |
|-----------------------|---|---|-----------|------|
| | | Daytime | Nighttime | |
| L1 | Located southeast of the Project site on Etiwanda Avenue near existing single-family residential home at 10991 Iberia Street. | 66.3 | 65.0 | 71.9 |
| L2 | Located south of the Project site on Iberia Street near existing industrial uses at 11600 Iberia Street. | 64.9 | 59.2 | 67.2 |
| L3 | Located west of the Project site on Corridor Drive near the Mira Loma Assembly Hall of Jehovah's Witnesses at 3300 Cornerstone Drive. | 66.8 | 67.2 | 73.0 |
| L4 | Located northwest of the Project site on Universe Drive near existing industrial uses at 308 Venture Drive. | 57.2 | 59.5 | 65.9 |
| L5 | Located north of the Project site on Manticou Court near existing industrial uses at 1011 Space Center Court. | 60.5 | 60.8 | 67.4 |

¹ See Exhibit 5-A for the noise level measurement locations.

² Energy (logarithmic) average levels. The long-term 24-hour measurement worksheets are included in Appendix 5.2.

"Daytime" = 7:00 a.m. to 10:00 p.m.; "Nighttime" = 10:00 p.m. to 7:00 a.m.

Table 5-1 provides the (energy average) noise levels used to describe the daytime and nighttime ambient conditions. These daytime and nighttime energy average noise levels represent the average of all hourly noise levels observed during these time periods expressed as a single number. Appendix 5.2 provides summary worksheets of the noise levels for each hour as well as the minimum, maximum, L_1 , L_2 , L_5 , L_8 , L_{25} , L_{50} , L_{90} , L_{95} , and L_{99} percentile noise levels observed during the daytime and nighttime periods.

The background ambient noise levels in the Project study area are dominated by the transportation-related noise associated with surface streets in addition to background industrial land use activities. This includes the auto and heavy truck activities on study area roadway segments near the noise level measurement locations.

EXHIBIT 5-A: NOISE MEASUREMENT LOCATIONS



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6 METHODS AND PROCEDURES

The following section outlines the methods and procedures used to model and analyze the future traffic noise environment. Consistent with the City of Jurupa Valley General Plan *Land Use/Noise Compatibility Matrix*, all transportation related noise levels are presented in terms of the 24-hour CNEL's.

6.1 FHWA TRAFFIC NOISE PREDICTION MODEL

The expected roadway noise level increases from vehicular traffic were calculated by Urban Crossroads, Inc. using a computer program that replicates the Federal Highway Administration (FHWA) Traffic Noise Prediction Model- FHWA-RD-77-108. (18) The FHWA Model arrives at a predicted noise level through a series of adjustments to the Reference Energy Mean Emission Level (REMEL). In California the national REMELs are substituted with the California Vehicle Noise (Calveno) Emission Levels. (19) Adjustments are then made to the REMEL to account for: the roadway classification (e.g., collector, secondary, major or arterial), the roadway active width (i.e., the distance between the center of the outermost travel lanes on each side of the roadway), the total average daily traffic (ADT), the travel speed, the percentages of automobiles, medium trucks, and heavy trucks in the traffic volume, the roadway grade, the angle of view (e.g., whether the roadway view is blocked), the site conditions ("hard" or "soft" relates to the absorption of the ground, pavement, or landscaping), and the percentage of total ADT which flows each hour throughout a 24-hour period. Research conducted by Caltrans has shown that the use of soft site conditions is appropriate for the application of the FHWA traffic noise prediction model used in this analysis. (20)

6.2 OFF-SITE TRAFFIC NOISE PREDICTION MODEL INPUTS

Table 6-1 presents the roadway parameters used to assess the Project's off-site dBA CNEL transportation noise impacts. Table 6-1 identifies the seven study area roadway segments, the distance from the centerline to adjacent land use based on the functional roadway classifications per the City of Jurupa Valley General Plan Circulation Element, and the posted vehicle speeds. The ADT volumes used in this study area presented on Table 6-2 are based on the *BRE Space Mira Loma Traffic Analysis*, prepared by Urban Crossroads, Inc. for the following traffic scenarios under both Without and With Project alternatives: Existing 2020, Background 2022, and Background plus Cumulative Project Conditions (B+CP). (21)

The ADT volumes vary for each roadway segment based on the existing traffic volumes and the combination of project traffic distributions. This analysis relies on a comparative evaluation of the off-site traffic noise impacts, without and with project ADT traffic volumes from the Project traffic study.

TABLE 6-1: OFF-SITE ROADWAY PARAMETERS

| ID | Roadway | Segment | Receiving Existing Land Use ¹ | Distance from Centerline to Receiving Land Use (Feet) ² | Vehicle Speed (mph) ³ |
|----|--------------|------------------|--|--|----------------------------------|
| 1 | Manitou Ct. | s/o Venture Dr. | Non-Sensitive | 39' | 40 |
| 2 | C St. | n/o Iberia St. | Non-Sensitive | 39' | 40 |
| 3 | Etiwanda Av. | n/o Hopkins St. | Non-Sensitive | 76' | 55 |
| 4 | Etiwanda Av. | s/o Iberia St. | Sensitive | 76' | 55 |
| 5 | Venture Dr. | e/o Manitou Ct. | Non-Sensitive | 39' | 40 |
| 6 | Iberia St. | e/o C St. | Non-Sensitive | 39' | 40 |
| 7 | Hopkins St. | w/o Etiwanda Av. | Non-Sensitive | 39' | 15 |

¹ Based on a review of existing aerial imagery. Noise sensitive uses limited to existing residential land uses.

² Distance to receiving land use is based upon the right-of-way distances.

³ BRE Space Mira Loma (MA200004) Traffic Analysis, Urban Crossroads, Inc.

TABLE 6-2: AVERAGE DAILY TRAFFIC VOLUMES

| ID | Roadway | Segment | Average Daily Traffic Volumes ¹ | | | | | |
|----|--------------|------------------|--|--------------|------------------------------|--------------|------------------------------|--------------|
| | | | Existing 2020 | | Existing Plus Ambient Growth | | Existing Plus Ambient Growth | |
| | | | Without Project | With Project | Without Project | With Project | Without Project | With Project |
| 1 | Manitou Ct. | s/o Venture Dr. | 2,771 | 3,450 | 2,940 | 3,620 | 2,941 | 3,620 |
| 2 | C St. | n/o Iberia St. | 1,136 | 1,482 | 1,206 | 1,551 | 1,205 | 1,550 |
| 3 | Etiwanda Av. | n/o Hopkins St. | 31,755 | 31,939 | 34,696 | 34,881 | 36,115 | 36,300 |
| 4 | Etiwanda Av. | s/o Iberia St. | 34,111 | 34,423 | 37,321 | 37,633 | 38,742 | 39,053 |
| 5 | Venture Dr. | e/o Manitou Ct. | 3,503 | 4,182 | 3,717 | 4,397 | 3,717 | 4,397 |
| 6 | Iberia St. | e/o C St. | 1,405 | 1,750 | 1,671 | 2,016 | 1,669 | 2,015 |
| 7 | Hopkins St. | w/o Etiwanda Av. | 2,065 | 2,182 | 2,911 | 3,028 | 2,912 | 3,029 |

¹ BRE Space Mira Loma (MA200004) Traffic Analysis, Urban Crossroads, Inc.

To quantify the off-site noise levels, the Project related truck trips were added to the heavy truck category in the FHWA noise prediction model. The addition of the Project related truck trips increases the percentage of heavy trucks in the vehicle mix. This approach recognizes that the FHWA noise prediction model is significantly influenced by the number of heavy trucks in the vehicle mix.

Table 6-3 provides the time of day (daytime, evening, and nighttime) vehicle splits. The daily Project truck trip-ends were assigned to the individual off-site study area roadway segments based on the Project truck trip distribution percentages documented in the *Traffic Impact Analysis*. Using the Project truck trips in combination with the Project trip distribution, Urban Crossroads, Inc. calculated the number of additional Project truck trips and vehicle mix

percentages for each of the study area roadway segments. Table 6-4 shows the traffic flow by vehicle type (vehicle mix) used for all without Project traffic scenarios, and Tables 6-5 through 6-7 show the vehicle mixes used for the with Project traffic scenarios.

TABLE 6-3: TIME OF DAY VEHICLE SPLITS

| Vehicle Type | Time of Day Splits ¹ | | | Total of Time of Day Splits |
|---------------|---------------------------------|---------|-----------|-----------------------------|
| | Daytime | Evening | Nighttime | |
| Autos | 77.50% | 12.90% | 9.60% | 100.00% |
| Medium Trucks | 84.80% | 4.90% | 10.30% | 100.00% |
| Heavy Trucks | 86.50% | 2.70% | 10.80% | 100.00% |

¹ County of Riverside Office of Industrial Hygiene. Values rounded to the nearest one-hundredth.

"Daytime" = 7:00 a.m. to 7:00 p.m.; "Evening" = 7:00 p.m. to 10:00 p.m.; "Nighttime" = 10:00 p.m. to 7:00 a.m.

TABLE 6-4: WITHOUT PROJECT VEHICLE MIX

| Classification | Total % Traffic Flow | | | Total |
|----------------|----------------------|---------------|--------------|---------|
| | Autos | Medium Trucks | Heavy Trucks | |
| All Segments | 53.55% | 14.54% | 31.91% | 100.00% |

Based on an existing vehicle count taken at Manitou Court and Venture Drive (BRE Space Mira Loma (MA200004) Traffic Analysis, Urban Crossroads, Inc.). Vehicle mix percentage values rounded to the nearest one-hundredth.

Due to the added Project truck trips, the increase in Project traffic volumes and the distributions of trucks on the study area road segments, the percentage of autos, medium trucks and heavy trucks will vary for each of the traffic scenarios. This explains why the existing and future traffic volumes and vehicle mixes vary between seemingly identical study area roadway segments.

TABLE 6-5: EXISTING WITH PROJECT VEHICLE MIX

| ID | Roadway | Segment | With Project ¹ | | | |
|----|--------------|------------------|---------------------------|---------------|--------------|--------------------|
| | | | Autos | Medium Trucks | Heavy Trucks | Total ² |
| 1 | Manitou Ct. | s/o Venture Dr. | 54.96% | 12.11% | 32.93% | 100.00% |
| 2 | C St. | n/o Iberia St. | 63.23% | 11.22% | 25.56% | 100.00% |
| 3 | Etiwanda Av. | n/o Hopkins St. | 53.61% | 14.47% | 31.93% | 100.00% |
| 4 | Etiwanda Av. | s/o Iberia St. | 53.97% | 14.41% | 31.63% | 100.00% |
| 5 | Venture Dr. | e/o Manitou Ct. | 54.71% | 12.54% | 32.75% | 100.00% |
| 6 | Iberia St. | e/o C St. | 61.74% | 11.73% | 26.53% | 100.00% |
| 7 | Hopkins St. | w/o Etiwanda Av. | 53.75% | 13.89% | 32.35% | 100.00% |

¹ BRE Space Mira Loma (MA200004) Traffic Analysis, Urban Crossroads, Inc.

² Total of vehicle mix percentage values rounded to the nearest one-hundredth.

TABLE 6-6: BACKGROUND WITH PROJECT VEHICLE MIX

| ID | Roadway | Segment | With Project ¹ | | | |
|----|--------------|------------------|---------------------------|---------------|--------------|--------------------|
| | | | Autos | Medium Trucks | Heavy Trucks | Total ² |
| 1 | Manitou Ct. | s/o Venture Dr. | 54.89% | 12.22% | 32.88% | 100.00% |
| 2 | C St. | n/o Iberia St. | 62.79% | 11.37% | 25.84% | 100.00% |
| 3 | Etiwanda Av. | n/o Hopkins St. | 53.60% | 14.47% | 31.93% | 100.00% |
| 4 | Etiwanda Av. | s/o Iberia St. | 53.93% | 14.42% | 31.65% | 100.00% |
| 5 | Venture Dr. | e/o Manitou Ct. | 54.65% | 12.63% | 32.71% | 100.00% |
| 6 | Iberia St. | e/o C St. | 60.66% | 12.10% | 27.24% | 100.00% |
| 7 | Hopkins St. | w/o Etiwanda Av. | 53.70% | 14.07% | 32.23% | 100.00% |

¹ BRE Space Mira Loma (MA200004) Traffic Analysis, Urban Crossroads, Inc.² Total of vehicle mix percentage values rounded to the nearest one-hundredth.**TABLE 6-7: B+CP WITH PROJECT VEHICLE MIX**

| ID | Roadway | Segment | With Project ¹ | | | |
|----|--------------|------------------|---------------------------|---------------|--------------|--------------------|
| | | | Autos | Medium Trucks | Heavy Trucks | Total ² |
| 1 | Manitou Ct. | s/o Venture Dr. | 54.89% | 12.22% | 32.88% | 100.00% |
| 2 | C St. | n/o Iberia St. | 62.80% | 11.36% | 25.84% | 100.00% |
| 3 | Etiwanda Av. | n/o Hopkins St. | 53.60% | 14.48% | 31.93% | 100.00% |
| 4 | Etiwanda Av. | s/o Iberia St. | 53.92% | 14.42% | 31.66% | 100.00% |
| 5 | Venture Dr. | e/o Manitou Ct. | 54.65% | 12.63% | 32.71% | 100.00% |
| 6 | Iberia St. | e/o C St. | 60.67% | 12.10% | 27.24% | 100.00% |
| 7 | Hopkins St. | w/o Etiwanda Av. | 53.70% | 14.07% | 32.23% | 100.00% |

¹ BRE Space Mira Loma (MA200004) Traffic Analysis, Urban Crossroads, Inc.² Total of vehicle mix percentage values rounded to the nearest one-hundredth.

7 OFF-SITE TRANSPORTATION NOISE IMPACTS

To assess the off-site transportation CNEL noise level impacts associated with the proposed Project, noise contours were developed based on the *BRE Space Mira Loma Traffic Analysis*. (21) Noise contour boundaries represent the equal levels of noise exposure and are measured in CNEL from the center of the roadway.

7.1 TRAFFIC NOISE CONTOURS

Noise contours were used to assess the Project's incremental 24-hour dBA CNEL traffic-related noise impacts at land uses adjacent to roadways conveying Project traffic. The noise contours represent the distance to noise levels of a constant value and are measured from the center of the roadway for the 70, 65, and 60 dBA CNEL noise levels. The noise contours do not consider the effect of any existing noise barriers or topography that may attenuate ambient noise levels. In addition, because the noise contours reflect modeling of vehicular noise on area roadways, they appropriately do not reflect noise contributions from the surrounding stationary noise sources within the Project study area. Tables 7-1 through 7-6 present a summary of the exterior dBA CNEL traffic noise levels without barrier attenuation. Roadway segments are analyzed from the without Project to the with Project conditions in each of the following timeframes: Existing 2020, Background 2022, and Background plus Cumulative Project Conditions (B+CP).

Consistent with the *BRE Space Mira Loma Traffic Analysis*, the Background (2022) condition is intended to identify "Opening Year" deficiencies associated with the development of the proposed Project based on the expected background growth within the study area. The Background plus Cumulative Project conditions includes an ambient growth (4.04%) applied to existing traffic volumes up to the Project's proposed opening year, traffic from the Project, plus traffic from other approved and pending projects (even those not anticipated to be occupied by the Project's opening year). Appendix 7.1 includes a summary of the dBA CNEL traffic noise level contours for each of the traffic scenarios.

TABLE 7-1: EXISTING WITHOUT PROJECT NOISE CONTOURS

| ID | Road | Segment | Receiving Existing Land Use ¹ | CNEL at Receiving Land Use (dBA) ² | Distance to Contour from Centerline (Feet) | | |
|----|--------------|------------------|--|---|--|-------------|-------------|
| | | | | | 70 dBA CNEL | 65 dBA CNEL | 60 dBA CNEL |
| 1 | Manitou Ct. | s/o Venture Dr. | Non-Sensitive | 71.7 | 51 | 110 | 236 |
| 2 | C St. | n/o Iberia St. | Non-Sensitive | 67.9 | RW | 60 | 130 |
| 3 | Etiwanda Av. | n/o Hopkins St. | Non-Sensitive | 80.9 | 406 | 875 | 1886 |
| 4 | Etiwanda Av. | s/o Iberia St. | Sensitive | 81.2 | 426 | 918 | 1978 |
| 5 | Venture Dr. | e/o Manitou Ct. | Non-Sensitive | 72.7 | 59 | 128 | 276 |
| 6 | Iberia St. | e/o C St. | Non-Sensitive | 68.8 | RW | 70 | 150 |
| 7 | Hopkins St. | w/o Etiwanda Av. | Non-Sensitive | 63.8 | RW | RW | 70 |

¹ Based on a review of existing aerial imagery. Noise sensitive uses limited to existing residential land uses.

² The CNEL is calculated at the boundary of the right-of-way of the receiving adjacent land use.

"RW" = Location of the respective noise contour falls within the right-of-way of the road.

TABLE 7-2: EXISTING WITH PROJECT NOISE CONTOURS

| ID | Road | Segment | Receiving Existing Land Use ¹ | CNEL at Receiving Land Use (dBA) ² | Distance to Contour from Centerline (Feet) | | |
|----|--------------|------------------|--|---|--|-------------|-------------|
| | | | | | 70 dBA CNEL | 65 dBA CNEL | 60 dBA CNEL |
| 1 | Manitou Ct. | s/o Venture Dr. | Non-Sensitive | 72.7 | 59 | 127 | 275 |
| 2 | C St. | n/o Iberia St. | Non-Sensitive | 68.1 | RW | 63 | 135 |
| 3 | Etiwanda Av. | n/o Hopkins St. | Non-Sensitive | 80.9 | 408 | 879 | 1893 |
| 4 | Etiwanda Av. | s/o Iberia St. | Sensitive | 81.2 | 426 | 919 | 1979 |
| 5 | Venture Dr. | e/o Manitou Ct. | Non-Sensitive | 73.5 | 67 | 145 | 312 |
| 6 | Iberia St. | e/o C St. | Non-Sensitive | 69.0 | RW | 72 | 155 |
| 7 | Hopkins St. | w/o Etiwanda Av. | Non-Sensitive | 64.1 | RW | RW | 73 |

¹ Based on a review of existing aerial imagery. Noise sensitive uses limited to existing residential land uses.

² The CNEL is calculated at the boundary of the right-of-way of the receiving adjacent land use.

"RW" = Location of the respective noise contour falls within the right-of-way of the road.

TABLE 7-3: BACKGROUND CONDITIONS WITHOUT PROJECT NOISE CONTOURS

| ID | Road | Segment | Receiving Existing Land Use ¹ | CNEL at Receiving Land Use (dBA) ² | Distance to Contour from Centerline (Feet) | | |
|----|--------------|------------------|--|---|--|-------------|-------------|
| | | | | | 70 dBA CNEL | 65 dBA CNEL | 60 dBA CNEL |
| 1 | Manitou Ct. | s/o Venture Dr. | Non-Sensitive | 72.0 | 53 | 114 | 245 |
| 2 | C St. | n/o Iberia St. | Non-Sensitive | 68.1 | RW | 63 | 136 |
| 3 | Etiwanda Av. | n/o Hopkins St. | Non-Sensitive | 81.3 | 431 | 929 | 2001 |
| 4 | Etiwanda Av. | s/o Iberia St. | Sensitive | 81.6 | 453 | 975 | 2101 |
| 5 | Venture Dr. | e/o Manitou Ct. | Non-Sensitive | 73.0 | 62 | 133 | 287 |
| 6 | Iberia St. | e/o C St. | Non-Sensitive | 69.5 | RW | 78 | 168 |
| 7 | Hopkins St. | w/o Etiwanda Av. | Non-Sensitive | 65.3 | RW | 41 | 88 |

¹ Based on a review of existing aerial imagery. Noise sensitive uses limited to existing residential land uses.

² The CNEL is calculated at the boundary of the right-of-way of the receiving adjacent land use.

"RW" = Location of the respective noise contour falls within the right-of-way of the road.

TABLE 7-4: BACKGROUND CONDITIONS WITH PROJECT NOISE CONTOURS

| ID | Road | Segment | Receiving Existing Land Use ¹ | CNEL at Receiving Land Use (dBA) ² | Distance to Contour from Centerline (Feet) | | |
|----|--------------|------------------|--|---|--|-------------|-------------|
| | | | | | 70 dBA CNEL | 65 dBA CNEL | 60 dBA CNEL |
| 1 | Manitou Ct. | s/o Venture Dr. | Non-Sensitive | 72.9 | 61 | 132 | 284 |
| 2 | C St. | n/o Iberia St. | Non-Sensitive | 68.3 | RW | 65 | 140 |
| 3 | Etiwanda Av. | n/o Hopkins St. | Non-Sensitive | 81.3 | 433 | 932 | 2008 |
| 4 | Etiwanda Av. | s/o Iberia St. | Sensitive | 81.6 | 453 | 975 | 2102 |
| 5 | Venture Dr. | e/o Manitou Ct. | Non-Sensitive | 73.8 | 69 | 150 | 322 |
| 6 | Iberia St. | e/o C St. | Non-Sensitive | 69.7 | RW | 80 | 173 |
| 7 | Hopkins St. | w/o Etiwanda Av. | Non-Sensitive | 65.5 | RW | 42 | 91 |

¹ Based on a review of existing aerial imagery. Noise sensitive uses limited to existing residential land uses.

² The CNEL is calculated at the boundary of the right-of-way of the receiving adjacent land use.

"RW" = Location of the respective noise contour falls within the right-of-way of the road.

TABLE 7-5: B+CP WITHOUT PROJECT NOISE CONTOURS

| ID | Road | Segment | Receiving Existing Land Use ¹ | CNEL at Receiving Land Use (dBA) ² | Distance to Contour from Centerline (Feet) | | |
|----|--------------|------------------|--|---|--|-------------|-------------|
| | | | | | 70 dBA CNEL | 65 dBA CNEL | 60 dBA CNEL |
| 1 | Manitou Ct. | s/o Venture Dr. | Non-Sensitive | 72.0 | 53 | 114 | 245 |
| 2 | C St. | n/o Iberia St. | Non-Sensitive | 68.1 | RW | 63 | 135 |
| 3 | Etiwanda Av. | n/o Hopkins St. | Non-Sensitive | 81.5 | 443 | 954 | 2055 |
| 4 | Etiwanda Av. | s/o Iberia St. | Sensitive | 81.8 | 464 | 1000 | 2153 |
| 5 | Venture Dr. | e/o Manitou Ct. | Non-Sensitive | 73.0 | 62 | 133 | 287 |
| 6 | Iberia St. | e/o C St. | Non-Sensitive | 69.5 | RW | 78 | 168 |
| 7 | Hopkins St. | w/o Etiwanda Av. | Non-Sensitive | 65.3 | RW | 41 | 88 |

¹ Based on a review of existing aerial imagery. Noise sensitive uses limited to existing residential land uses.

² The CNEL is calculated at the boundary of the right-of-way of the receiving adjacent land use.

"RW" = Location of the respective noise contour falls within the right-of-way of the road.

TABLE 7-6: B+CP WITH PROJECT NOISE CONTOURS

| ID | Road | Segment | Receiving Existing Land Use ¹ | CNEL at Receiving Land Use (dBA) ² | Distance to Contour from Centerline (Feet) | | |
|----|--------------|------------------|--|---|--|-------------|-------------|
| | | | | | 70 dBA CNEL | 65 dBA CNEL | 60 dBA CNEL |
| 1 | Manitou Ct. | s/o Venture Dr. | Non-Sensitive | 72.9 | 61 | 132 | 284 |
| 2 | C St. | n/o Iberia St. | Non-Sensitive | 68.3 | RW | 65 | 140 |
| 3 | Etiwanda Av. | n/o Hopkins St. | Non-Sensitive | 81.5 | 444 | 957 | 2062 |
| 4 | Etiwanda Av. | s/o Iberia St. | Sensitive | 81.8 | 464 | 1000 | 2155 |
| 5 | Venture Dr. | e/o Manitou Ct. | Non-Sensitive | 73.8 | 69 | 150 | 322 |
| 6 | Iberia St. | e/o C St. | Non-Sensitive | 69.7 | RW | 80 | 173 |
| 7 | Hopkins St. | w/o Etiwanda Av. | Non-Sensitive | 65.5 | RW | 42 | 91 |

¹ Based on a review of existing aerial imagery. Noise sensitive uses limited to existing residential land uses.

² The CNEL is calculated at the boundary of the right-of-way of the receiving adjacent land use.

"RW" = Location of the respective noise contour falls within the right-of-way of the road.

7.2 EXISTING PROJECT TRAFFIC NOISE LEVEL INCREASES

An analysis of existing traffic noise levels plus traffic noise generated by the proposed Project has been included in this report to fully analyze all the existing traffic scenarios identified in the *BRE Space Mira Loma Traffic Analysis*. This condition is provided solely for informational purposes and will not occur, since the Project will not be fully developed and occupied under Existing conditions. Table 7-1 shows the Existing without Project conditions CNEL noise levels. The Existing without Project exterior noise levels are expected to range from 63.8 to 81.2 dBA CNEL, without accounting for any noise attenuation features such as noise barriers or topography. Table 7-2 shows the Existing with Project conditions will range from 64.1 to 81.2 dBA CNEL. Table 7-7 shows that the Project off-site traffic noise level impacts will range from 0.0 to 1.0 dBA CNEL. Based on the significance criteria for off-site traffic noise presented in Table 4-1, land uses adjacent to the study area roadway segments would experience *less than significant* noise level increases on receiving land uses due to the Project-related traffic.

7.3 BACKGROUND CONDITIONS PROJECT TRAFFIC NOISE LEVEL INCREASES

Table 7-3 presents the Background Conditions without Project conditions CNEL noise levels. The Background Conditions without Project exterior noise levels are expected to range from 65.3 to 81.6 dBA CNEL, without accounting for any noise attenuation features such as noise barriers or topography. Table 7-4 shows the Background Conditions with Project conditions will range from 65.5 to 81.6 dBA CNEL. Table 7-8 shows that the Project off-site traffic noise level increases will range from 0.0 to 0.9 dBA CNEL. Based on the significance criteria for off-site traffic noise presented in Table 4-1, land uses adjacent to the study area roadway segments would experience *less than significant* noise level increases on receiving land uses due to the Project-related traffic.

7.4 B+CP PROJECT TRAFFIC NOISE LEVEL INCREASES

Table 7-5 presents the B+CP without Project conditions CNEL noise levels. The B+CP without Project exterior noise levels are expected to range from 65.3 to 81.8 dBA CNEL, without accounting for any noise attenuation features such as noise barriers or topography. Table 7-6 shows the B+CP with Project conditions will range from 65.5 to 81.8 dBA CNEL. Table 7-9 shows that the Project off-site traffic noise level increases will range from 0.0 to 0.9 dBA CNEL. Based on the significance criteria for off-site traffic noise presented in Table 4-1, land uses adjacent to the study area roadway segments would experience *less than significant* noise level increases on receiving land uses due to the Project-related traffic.

TABLE 7-7: EXISTING WITH PROJECT TRAFFIC NOISE LEVEL INCREASES

| ID | Road | Segment | Receiving Existing Land Use ¹ | CNEL at Receiving Land Use (dBA) ² | | | Noise Sensitive Land Use? | Exterior Noise Standard | Incremental Noise Level Increase Threshold ³ | |
|----|--------------|------------------|--|---|--------------|------------------|---------------------------|-------------------------|---|-----------|
| | | | | No Project | With Project | Project Addition | | | Limit | Exceeded? |
| 1 | Manitou Ct. | s/o Venture Dr. | Non-Sensitive | 71.7 | 72.7 | 1.0 | No | 70 | 3 | No |
| 2 | C St. | n/o Iberia St. | Non-Sensitive | 67.9 | 68.1 | 0.2 | No | 70 | 3 | No |
| 3 | Etiwanda Av. | n/o Hopkins St. | Non-Sensitive | 80.9 | 80.9 | 0.0 | No | 70 | 3 | No |
| 4 | Etiwanda Av. | s/o Iberia St. | Sensitive | 81.2 | 81.2 | 0.0 | Yes | 65 | 3 | No |
| 5 | Venture Dr. | e/o Manitou Ct. | Non-Sensitive | 72.7 | 73.5 | 0.8 | No | 70 | 3 | No |
| 6 | Iberia St. | e/o C St. | Non-Sensitive | 68.8 | 69.0 | 0.2 | No | 70 | 3 | No |
| 7 | Hopkins St. | w/o Etiwanda Av. | Non-Sensitive | 63.8 | 64.1 | 0.3 | No | 70 | 3 | No |

¹ Noise sensitive uses limited to existing residential land uses.

² The CNEL is calculated at the boundary of the right-of-way of each roadway and the property line of the receiving land use.

³ Does the Project create an incremental noise level increase exceeding the significance criteria (Table 4-1)?

TABLE 7-8: BACKGROUND CONDITIONS WITH PROJECT TRAFFIC NOISE INCREASES

| ID | Road | Segment | Receiving Existing Land Use ¹ | CNEL at Receiving Land Use (dBA) ² | | | Noise Sensitive Land Use? | Exterior Noise Standard | Incremental Noise Level Increase Threshold ³ | |
|----|--------------|------------------|--|---|--------------|------------------|---------------------------|-------------------------|---|-----------|
| | | | | No Project | With Project | Project Addition | | | Limit | Exceeded? |
| 1 | Manitou Ct. | s/o Venture Dr. | Non-Sensitive | 72.0 | 72.9 | 0.9 | No | 70 | 3 | No |
| 2 | C St. | n/o Iberia St. | Non-Sensitive | 68.1 | 68.3 | 0.2 | No | 70 | 3 | No |
| 3 | Etiwanda Av. | n/o Hopkins St. | Non-Sensitive | 81.3 | 81.3 | 0.0 | No | 70 | 3 | No |
| 4 | Etiwanda Av. | s/o Iberia St. | Sensitive | 81.6 | 81.6 | 0.0 | Yes | 65 | 3 | No |
| 5 | Venture Dr. | e/o Manitou Ct. | Non-Sensitive | 73.0 | 73.8 | 0.8 | No | 70 | 3 | No |
| 6 | Iberia St. | e/o C St. | Non-Sensitive | 69.5 | 69.7 | 0.2 | No | 70 | 3 | No |
| 7 | Hopkins St. | w/o Etiwanda Av. | Non-Sensitive | 65.3 | 65.5 | 0.2 | No | 70 | 3 | No |

¹ Noise sensitive uses limited to existing residential land uses.

² The CNEL is calculated at the boundary of the right-of-way of each roadway and the property line of the receiving land use.

³ Does the Project create an incremental noise level increase exceeding the significance criteria (Table 4-1)?

TABLE 7-9: B+CP WITH PROJECT TRAFFIC NOISE INCREASES

| ID | Road | Segment | Receiving Existing Land Use ¹ | CNEL at Receiving Land Use (dBA) ² | | | Noise Sensitive Land Use? | Exterior Noise Standard | Incremental Noise Level Increase Threshold ³ | |
|----|--------------|------------------|--|---|--------------|------------------|---------------------------|-------------------------|---|-----------|
| | | | | No Project | With Project | Project Addition | | | Limit | Exceeded? |
| 1 | Manitou Ct. | s/o Venture Dr. | Non-Sensitive | 72.0 | 72.9 | 0.9 | No | 70 | 3 | No |
| 2 | C St. | n/o Iberia St. | Non-Sensitive | 68.1 | 68.3 | 0.2 | No | 70 | 3 | No |
| 3 | Etiwanda Av. | n/o Hopkins St. | Non-Sensitive | 81.5 | 81.5 | 0.0 | No | 70 | 3 | No |
| 4 | Etiwanda Av. | s/o Iberia St. | Sensitive | 81.8 | 81.8 | 0.0 | Yes | 65 | 3 | No |
| 5 | Venture Dr. | e/o Manitou Ct. | Non-Sensitive | 73.0 | 73.8 | 0.8 | No | 70 | 3 | No |
| 6 | Iberia St. | e/o C St. | Non-Sensitive | 69.5 | 69.7 | 0.2 | No | 70 | 3 | No |
| 7 | Hopkins St. | w/o Etiwanda Av. | Non-Sensitive | 65.3 | 65.5 | 0.2 | No | 70 | 3 | No |

¹ Noise sensitive uses limited to existing residential land uses.

² The CNEL is calculated at the boundary of the right-of-way of each roadway and the property line of the receiving land use.

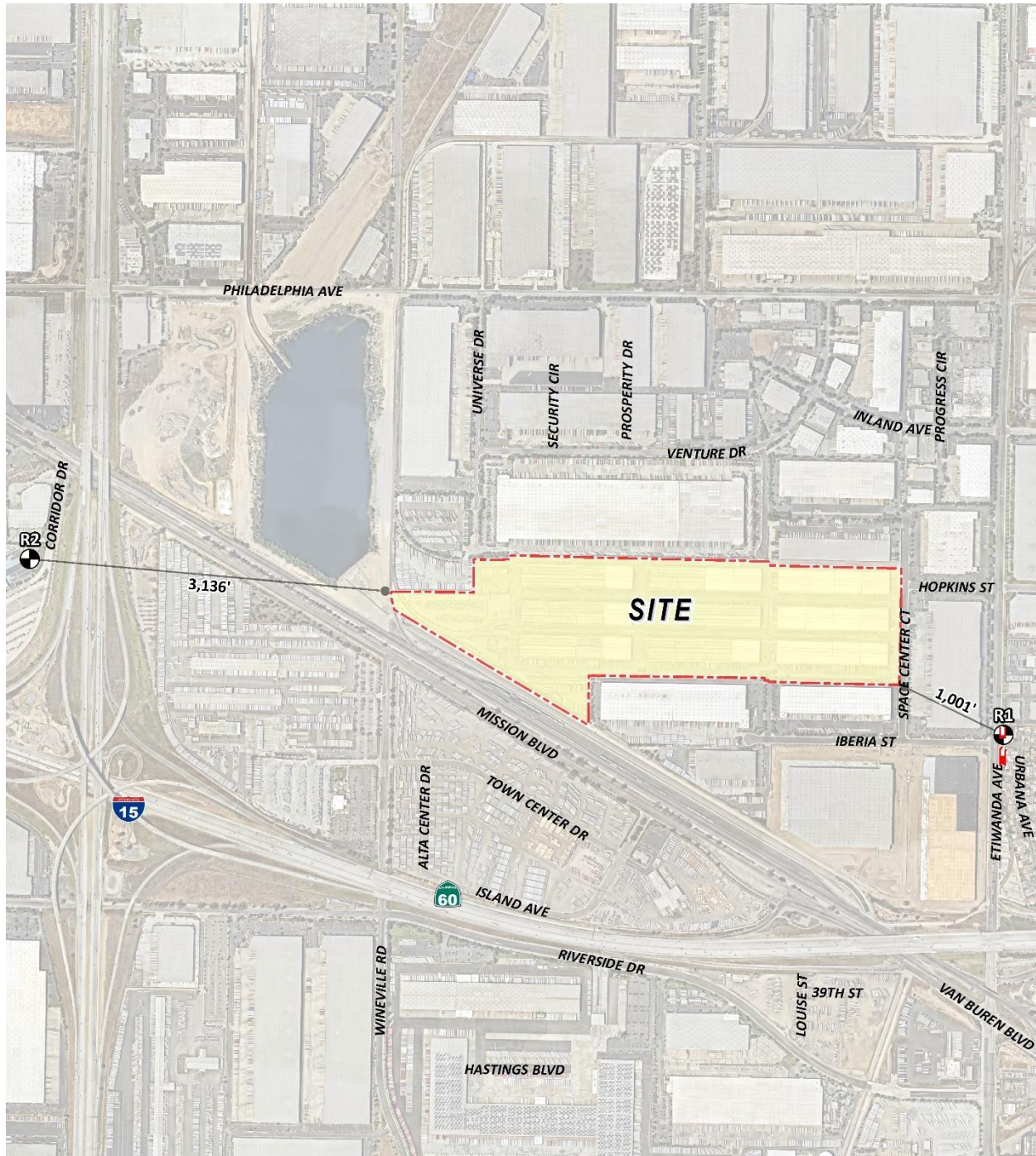
³ Does the Project create an incremental noise level increase exceeding the significance criteria (Table 4-1)?

8 SENSITIVE RECEIVER LOCATIONS

To assess the potential for long-term operational and short-term construction noise impacts, the following sensitive receiver locations, as shown on Exhibit 8-A, were identified as representative locations for analysis. Sensitive receivers are generally defined as locations where people reside or where the presence of unwanted sound could otherwise adversely affect the use of the land. Noise-sensitive land uses are generally considered to include schools, hospitals, single-family dwellings, mobile home parks, churches, libraries, and recreation areas. Moderately noise-sensitive land uses typically include multi-family dwellings, hotels, motels, dormitories, outpatient clinics, cemeteries, golf courses, country clubs, athletic/tennis clubs, and equestrian clubs. Land uses that are considered relatively insensitive to noise include business, commercial, and professional developments. Land uses that are typically not affected by noise include: industrial, manufacturing, utilities, agriculture, undeveloped land, parking lots, warehousing, liquid and solid waste facilities, salvage yards, and transit terminals.

To describe the potential off-site Project noise levels, two receiver locations in the vicinity of the Project site were identified. All distances are measured from the Project site boundary to the outdoor living areas (e.g., private backyards) or at the building façade, whichever is closer to the Project site. The selection of receiver locations is based on FHWA guidelines and is consistent with additional guidance provided by Caltrans and the FTA, as previously described in Section 5.2. Other sensitive land uses in the Project study area that are located at greater distances than those identified in this noise study will experience lower noise levels than those presented in this report due to the additional attenuation from distance and the shielding of intervening structures. Distance is measured in a straight line from the project boundary to each receiver location.

- R1: Location R1 represents the existing noise sensitive residence at 10991 Iberia Street, approximately 1,001 feet southeast of the Project site. Receiver R1 is placed at the private outdoor living area (backyard). A 24-hour noise measurement was taken near this location, L1, to describe the existing ambient noise environment.
- R2: Location R2 represents the Mira Loma Assembly Hall of Jehovah's Witnesses at 3300 Cornerstone Drive, approximately 3,136 feet west of the Project site. Since there are no private outdoor living areas (backyards) facing the Project site, receiver R2 is placed at the building façade. A 24-hour noise measurement was taken near this location, L3, to describe the existing ambient noise environment.

EXHIBIT 8-A: SENSITIVE RECEIVER LOCATIONS

- LEGEND:**
- Existing 6' Foot High Barrier
 - Receiver Locations
 - Distance from receiver to Project site boundary (in feet)

9 OPERATIONAL NOISE IMPACTS

This section analyzes the potential stationary-source operational noise impacts at the nearest receiver locations, identified in Section 8, resulting from the operation of the proposed BRE Space Mira Loma Project. Exhibit 9-A identifies the representative receiver locations and noise source locations used to assess the hourly average L_{eq} operational noise levels consistent with the City of Jurupa Valley Municipal Code, 11.05.040.

9.1 OPERATIONAL NOISE SOURCES

This operational noise analysis is intended to describe noise level impacts associated with the expected typical of daytime and nighttime activities at the Project site. To present the potential worst-case noise conditions, this analysis assumes the Project would be operational 24 hours per day, seven days per week. Consistent with similar warehouse uses, the Project business operations would primarily be conducted within the enclosed buildings, except for traffic movement, parking, as well as loading and unloading of trucks at designated loading bays. The on-site Project-related noise sources are expected to include: cold storage activity, trailer activity, truck movements, roof-top air conditioning units, trash enclosure activity, and parking lot vehicle movements.

9.2 REFERENCE NOISE LEVELS

To estimate the Project operational noise impacts, reference noise level measurements were collected from similar types of activities to represent the noise levels expected with the development of the proposed Project. This section provides a detailed description of the reference noise level measurements shown on Table 9-1 used to estimate the Project operational noise impacts. It is important to note that the following projected noise levels assume the worst-case noise environment with the cold storage activity, trailer activity, truck movements, roof-top air conditioning units, trash enclosure activity, and parking lot vehicle movements all operating continuously. These sources of noise activity will likely vary throughout the day.

EXHIBIT 9-A: OPERATIONAL NOISE SOURCE LOCATIONS

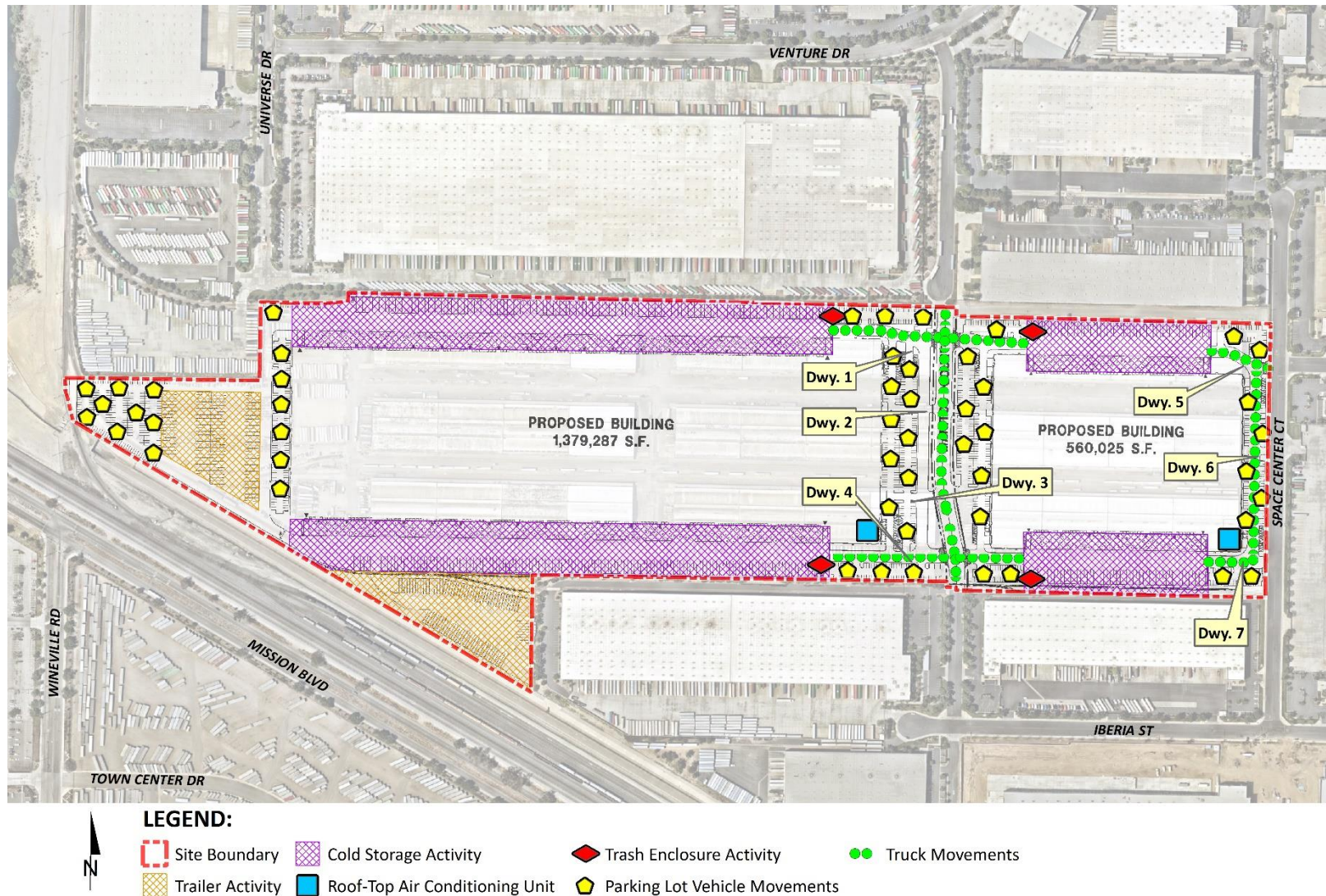


TABLE 9-1: REFERENCE NOISE LEVEL MEASUREMENTS

| Noise Source ¹ | Noise Source Height (Feet) | Min./Hour ² | | Reference Noise Level (dBA Leq) @ 50 Feet | Sound Power Level (dBA) ³ |
|---------------------------------|----------------------------|------------------------|----------------|---|--------------------------------------|
| | | Day | Night | | |
| Cold Storage Activity | 8' | 60 | 60 | 65.7 | 111.5 |
| Trailer Activity | 8' | 60 | 60 | 62.8 | 103.4 |
| Truck Movements | 8' | - ⁴ | - ⁴ | 58.0 | 89.7 |
| Roof-Top Air Conditioning Units | 5' | 39 | 28 | 57.2 | 88.9 |
| Trash Enclosure Activity | 5' | 5 | 5 | 57.3 | 89.0 |
| Parking Lot Vehicle Movements | 5' | 60 | 60 | 52.6 | 79.0 |

¹ As measured by Urban Crossroads, Inc.

² Anticipated duration (minutes within the hour) of noise activity during typical hourly conditions expected at the Project site. "Daytime" = 7:00 a.m. - 10:00 p.m.; "Nighttime" = 10:00 p.m. - 7:00 a.m.

³ Sound power level represents the total amount of acoustical energy (noise level) produced by a sound source independent of distance or surroundings. Sound power levels calculated using the CadnaA noise model at the reference distance to the noise source. Numbers may vary due to size differences between point and area noise sources.

⁴ Truck Movements are calculate based on the number of events by time of day (See Table 9-2).

9.2.1 MEASUREMENT PROCEDURES

The reference noise level measurements presented in this section were collected using a Larson Davis LxT Type 1 precisions sound level meter (serial number 01146). The LxT sound level meter was calibrated using a Larson-Davis calibrator, Model CAL 200, was programmed in "slow" mode to record noise levels in "A" weighted form and was located at approximately five feet above the ground elevation for each measurement. The sound level meters and microphones were equipped with a windscreen during all measurements. All noise level measurement equipment satisfies the American National Standards Institute (ANSI) standard specifications for sound level meters ANSI S1.4-2014/IEC 61672-1:2013. (17)

9.2.2 COLD STORAGE ACTIVITY

To describe the loading dock activities, a reference noise level measurement was collected to represent the truck activities. The reference noise level measurement was taken in the center of the loading dock activity area and represents multiple concurrent noise sources resulting in a combined noise level of 65.7 dBA Leq at a uniform distance of 50 feet. Specifically, the reference noise level measurement represents one truck located approximately 30 feet from the noise level meter with another truck passing by to park roughly 20 feet away, both with their engines idling. Throughout the reference noise level measurement, a separate docked and running reefer truck was located approximately 50 feet east of the measurement location. Additional background noise sources included truck pass-by noise, truck drivers talking to each other next to docked trucks, and air brake release noise when trucks parked.

9.2.3 TRAILER ACTIVITY

To evaluate the noise levels associated with truck idling, backup alarms, trailer movements and storage activities, Urban Crossroads collected a reference noise level measurement at an existing

parcel hub facility to describe the potential operational noise levels associated with Project operational activities. The measured reference noise level at 50 feet from activity was measured at 62.8 dBA L_{eq} . The reference noise level measurement includes a semi-truck with trailer pass-by event, background switcher cab trailer towing, drop-off, idling, and backup alarm events. Noise associated with trailer storage activity is expected to operate for the entire hour (60 minutes).

9.2.4 TRUCK MOVEMENTS

An entry gate and truck movements reference noise level measurement were taken over a 15-minute period and represents multiple noise sources producing a reference noise level of 58.0 dBA L_{eq} at 50 feet. The noise sources included at this measurement location account for the rattling and squeaking during normal opening and closing operations, the gate closure equipment, truck engines idling outside the entry gate, truck movements through the entry gate, and background truck court activities and forklift backup alarm noise.

Consistent with the *BRE Space Mira Loma Traffic Analysis*, the Project is expected to generate a total of approximately 3,928 trip-ends per day (actual vehicles) and includes 908 truck trip-ends per day. This analysis, as per the *Traffic Analysis*, depends on the net new project trip generation less traffic associated with the existing uses, with a total of approximately 1,176 trip-ends per day (actual vehicles) and includes 334 truck trip-ends per day. (21) This noise study relies on the actual Project trips (as opposed to the passenger car equivalents) to accurately account for the effect of individual truck trips on the study area roadway network. Using the estimated number of truck trips in combination with time-of-day vehicle splits, the number of entry gate and truck movements by driveway location were calculated. As shown on Table 9-2, this information is then used to calculate the entry gate and truck movements operational noise source activity based on the number of events by time of day.

TABLE 9-2: ENTRY GATE & TRUCK MOVEMENTS BY LOCATION

| Entry Gate & Truck Movement Location ¹ | Total Project Truck Trips ² | Trip Dist. ³ | Truck Trips by Location ⁴ | Time of Day Vehicle Splits ⁵ | | | Truck Movements ⁶ | | |
|---|--|-------------------------|--------------------------------------|---|---------|--------|------------------------------|---------|-------|
| | | | | Day | Evening | Night | Day | Evening | Night |
| Driveway 1 | 334 | 42% | 140 | 86.50% | 2.70% | 10.80% | 121 | 4 | 15 |
| Driveway 4 | | 43% | 144 | 86.50% | 2.70% | 10.80% | 125 | 4 | 16 |
| Driveway 5 | | 8% | 27 | 86.50% | 2.70% | 10.80% | 23 | 1 | 3 |
| Driveway 7 | | 7% | 23 | 86.50% | 2.70% | 10.80% | 20 | 1 | 2 |

¹ Driveway locations as shown on Exhibit 9-A.

² Net New Project truck trips according to Table 4-3 of the BRE Space Mira Loma Traffic Analysis.

³ Project truck trip distribution according to Exhibit 4-1 of the BRE Space Mira Loma Traffic Analysis.

⁴ Calculated trip trucks per location represents the product of the total (inbound and outbound) project truck trips by and the trip distribution.

⁵ Heavy truck time of day vehicle splits as shown on Table 6-3.

⁶ Calculated time of day entry gate and truck movements by location.

9.2.5 ROOF-TOP AIR CONDITIONING UNITS

The noise level measurements describe a single mechanical roof-top air conditioning unit. The reference noise level represents a Lennox SCA120 series 10-ton model packaged air conditioning unit. At the uniform reference distance of 50 feet, the reference noise levels are 57.2 dBA L_{eq} . Based on the typical operating conditions observed over a four-day measurement period, the roof-top air conditioning units are estimated to operate for an average 39 minutes per hour during the daytime hours, and 28 minutes per hour during the nighttime hours. These operating conditions reflect peak summer cooling requirements with measured temperatures approaching 96 degrees Fahrenheit (°F) with average daytime temperatures of 82°F. For this noise analysis, the air conditioning units are expected to be located on the roof of the Project buildings.

9.2.6 TRASH ENCLOSURE ACTIVITY

The measured reference noise level at the uniform 50-foot reference distance is 57.3 dBA L_{eq} for the trash enclosure activity. The trash enclosure activity noise levels include two metal gates opening and closing, metal scraping against concrete floor sounds, dumpster movement on metal wheels, trash dropping into the metal dumpster, and background parking lot vehicle movements. Noise associated with trash enclosure activities is conservatively expected to occur for 5 minutes per hour.

9.2.7 PARKING LOT VEHICLE MOVEMENTS

To describe the on-site parking lot activity a reference noise level of 52.6 dBA L_{eq} at 50 feet is used. Parking activities are expected to take place during the full hour (60 minutes) throughout the daytime and evening hours. The parking lot noise levels are mainly due cars pulling in and out of parking spaces.

9.3 CADNAA NOISE PREDICTION MODEL

To fully describe the exterior operational noise levels from the Project, Urban Crossroads, Inc. developed a noise prediction model using the CadnaA (Computer Aided Noise Abatement) computer program. CadnaA can analyze multiple types of noise sources using the spatially accurate Project site plan, georeferenced Nearmap aerial imagery, topography, buildings, and barriers in its calculations to predict outdoor noise levels.

Using the ISO 9613-2 protocol, CadnaA will calculate the distance from each noise source to the noise receiver locations, using the ground absorption, distance, and barrier/building attenuation inputs to provide a summary of noise level at each receiver and the partial noise level contributions by noise source. Consistent with the ISO 9613-2 protocol, the CadnaA noise prediction model relies on the reference sound power level (L_w) to describe individual noise sources. While sound pressure levels (e.g. L_{eq}) quantify in decibels the intensity of given sound sources at a reference distance, sound power levels (L_w) are connected to the sound source and are independent of distance. Sound pressure levels vary substantially with distance from the source and diminish as a result of intervening obstacles and barriers, air absorption, wind, and other factors. Sound power is the acoustical energy emitted by the sound source and is an absolute value that is not affected by the environment.

The operational noise level calculations provided in this noise study account for the distance attenuation provided due to geometric spreading, when sound from a localized stationary source (i.e., a point source) propagates uniformly outward in a spherical pattern. A default ground attenuation factor of 0.5 was used in the noise analysis to account for mixed ground representing a combination of hard and soft surfaces. Appendix 9.1 includes the detailed noise model inputs used to estimate the Project operational noise levels presented in this section.

9.4 PROJECT OPERATIONAL NOISE LEVELS

Using the reference noise levels to represent the proposed Project operations that include cold storage activity, trailer activity, truck movements, roof-top air conditioning units, trash enclosure activity, and parking lot vehicle movements, Urban Crossroads, Inc. calculated the operational source noise levels that are expected to be generated at the Project site and the Project-related noise level increases that would be experienced at each of the sensitive receiver locations. Tables 9-3 shows the Project operational noise levels during the daytime hours of 7:00 a.m. to 10:00 p.m. The daytime hourly noise levels at the off-site receiver locations are expected to range from 38.0 to 42.9 dBA L_{eq} .

TABLE 9-3: DAYTIME PROJECT OPERATIONAL NOISE LEVELS

| Noise Source ¹ | Operational Noise Levels by Receiver Location (dBA L_{eq}) | |
|----------------------------------|---|-------------|
| | R1 | R2 |
| Cold Storage Activity | 42.8 | 36.9 |
| Trailer Activity | 24.0 | 31.0 |
| Truck Movements | 23.5 | 16.1 |
| Roof-Top Air Conditioning Units | 20.1 | 4.3 |
| Trash Enclosure Activity | 9.0 | 9.0 |
| Parking Lot Vehicle Movements | 18.6 | 15.7 |
| Total (All Noise Sources) | 42.9 | 38.0 |

¹ See Exhibit 9-A for the noise source locations. CadnaA noise model calculations are included in Appendix 9.1.

Table 9-4 shows the Project operational noise levels during the nighttime hours of 10:00 p.m. to 7:00 a.m. The nighttime hourly noise levels at the off-site receiver locations are expected to range from 37.2 to 41.9 dBA L_{eq} . The differences between the daytime and nighttime noise levels are largely related to the duration of noise activity (Table 9-1).

9.5 PROJECT OPERATIONAL NOISE LEVEL COMPLIANCE

To demonstrate compliance with local noise regulations, the Project-only operational noise levels are evaluated against exterior noise level thresholds based on the City of Jurupa Valley exterior noise level standards at nearby noise-sensitive receiver locations. Table 9-5 shows the operational noise levels associated with BRE Space Mira Loma Project will satisfy the City of Jurupa Valley 65 dBA L_{eq} daytime and 45 dBA L_{eq} nighttime exterior noise level standards at all nearby receiver locations. Therefore, the operational noise impacts are considered *less than significant* at the nearby noise-sensitive receiver locations.

TABLE 9-4: NIGHTTIME PROJECT OPERATIONAL NOISE LEVELS

| Noise Source ¹ | Operational Noise Levels by Receiver Location (dBA Leq) | |
|----------------------------------|---|-------------|
| | R1 | R2 |
| Cold Storage Activity | 41.8 | 36.0 |
| Trailer Activity | 24.0 | 31.0 |
| Truck Movements | 14.3 | 7.1 |
| Roof-Top Air Conditioning Units | 17.6 | 6.0 |
| Trash Enclosure Activity | 6.0 | 6.0 |
| Parking Lot Vehicle Movements | 18.6 | 15.7 |
| Total (All Noise Sources) | 41.9 | 37.2 |

¹ See Exhibit 9-A for the noise source locations. CadnaA noise model calculations are included in Appendix 9.1.

TABLE 9-5: OPERATIONAL NOISE LEVEL COMPLIANCE

| Receiver Location ¹ | Project Operational Noise Levels (dBA Leq) ² | | Noise Level Standards (dBA Leq) ³ | | Noise Level Standards Exceeded? ⁴ | |
|--------------------------------|---|-----------|--|-----------|--|-----------|
| | Daytime | Nighttime | Daytime | Nighttime | Daytime | Nighttime |
| R1 | 42.9 | 41.9 | 65 | 45 | No | No |
| R2 | 38.0 | 37.2 | 65 | 45 | No | No |

¹ See Exhibit 10-A for the receiver locations.

² Proposed Project operational noise levels as shown on Tables 9-3 and 9-4.

³ Exterior noise level standards for source (commercial) land use, as shown on Table 4-1.

⁴ Do the estimated Project operational noise source activities exceed the noise level standards?

"Daytime" = 7:00 a.m. - 10:00 p.m.; "Nighttime" = 10:00 p.m. - 7:00 a.m.

9.6 PROJECT OPERATIONAL NOISE LEVEL INCREASES

To describe the Project operational noise level increases, the Project operational noise levels are combined with the existing ambient noise levels measurements for the nearby receiver locations potentially impacted by Project operational noise sources. Since the units used to measure noise, decibels (dB), are logarithmic units, the Project-operational and existing ambient noise levels cannot be combined using standard arithmetic equations. (2) Instead, they must be logarithmically added using the following base equation:

$$SPL_{Total} = 10\log_{10}[10^{SPL1/10} + 10^{SPL2/10} + \dots 10^{SPLn/10}]$$

Where "SPL1," "SPL2," etc. are equal to the sound pressure levels being combined, or in this case, the Project-operational and existing ambient noise levels. The difference between the combined Project and ambient noise levels describes the Project noise level increases to the existing ambient noise environment. As indicated on Tables 9-6 and 9-7, the Project will not generate a daytime and nighttime operational noise level increase at the nearby receiver locations. Project-related operational noise level increases will satisfy the operational noise level increase significance criteria presented on Table 4-1. Therefore, the incremental Project operational noise level increase is considered *less than significant* at all receiver locations.

TABLE 9-6: DAYTIME PROJECT OPERATIONAL NOISE LEVEL INCREASES

| Receiver Location ¹ | Total Project Operational Noise Level ² | Measurement Location ³ | Reference Ambient Noise Levels ⁴ | Combined Project and Ambient ⁵ | Project Increase ⁶ | Increase Criteria ⁷ | Increase Criteria Exceeded? |
|--------------------------------|--|-----------------------------------|---|---|-------------------------------|--------------------------------|-----------------------------|
| R1 | 42.9 | L1 | 66.3 | 66.3 | 0.0 | 3 | No |
| R2 | 38.0 | L3 | 66.8 | 66.8 | 0.0 | 3 | No |

¹ See Exhibit 10-A for the receiver locations.

² Total Project daytime operational noise levels as shown on Table 9-3.

³ Reference noise level measurement locations as shown on Exhibit 5-A.

⁴ Observed daytime ambient noise levels as shown on Table 5-1.

⁵ Represents the combined ambient conditions plus the Project activities.

⁶ The noise level increase expected with the addition of the proposed Project activities.

⁷ Significance increase criteria as shown on Table 4-1.

TABLE 9-7: NIGHTTIME OPERATIONAL NOISE LEVEL INCREASES

| Receiver Location ¹ | Total Project Operational Noise Level ² | Measurement Location ³ | Reference Ambient Noise Levels ⁴ | Combined Project and Ambient ⁵ | Project Increase ⁶ | Increase Criteria ⁷ | Increase Criteria Exceeded? |
|--------------------------------|--|-----------------------------------|---|---|-------------------------------|--------------------------------|-----------------------------|
| R1 | 41.9 | L1 | 65.0 | 65.0 | 0.0 | 3 | No |
| R2 | 37.2 | L3 | 67.2 | 67.2 | 0.0 | 3 | No |

¹ See Exhibit 10-A for the receiver locations.

² Total Project nighttime operational noise levels as shown on Table 9-4.

³ Reference noise level measurement locations as shown on Exhibit 5-A.

⁴ Observed nighttime ambient noise levels as shown on Table 5-1.

⁵ Represents the combined ambient conditions plus the Project activities.

⁶ The noise level increase expected with the addition of the proposed Project activities.

⁷ Significance increase criteria as shown on Table 4-1.

10 CONSTRUCTION IMPACTS

This section analyzes potential equivalent dBA L_{eq} impacts resulting from the short-term construction activities associated with the development of the Project. Exhibit 10-A shows the construction noise source locations in relation to the nearest sensitive receiver locations previously described in Section 8.

To prevent high levels of construction noise from impacting noise-sensitive land uses, City of Jurupa Valley General Plan Noise Element Policy NE 3.5 limits construction activities within 200 feet of residential uses to weekdays, between 7:00 a.m. and 6:00 p.m., and limit high-noise-generating construction activities (e.g., grading, demolition, pile driving) near sensitive receptors to weekdays between 9:00 a.m. and 3:00 p.m.

10.1 CONSTRUCTION NOISE LEVELS

Noise generated by the Project construction equipment will include a combination of trucks, power tools, concrete mixers, and portable generators that when combined can reach high levels. The number and mix of construction equipment are expected to occur in the following stages:

- Demolition
- Site Preparation
- Grading
- Building Construction
- Paving
- Architectural Coating

This construction noise analysis was prepared using reference noise level measurements taken by Urban Crossroads, Inc. to describe the typical construction activity noise levels for each stage of Project construction.

10.2 CONSTRUCTION REFERENCE NOISE LEVELS

To describe the Project construction noise levels, measurements were collected for similar activities at several construction sites. Table 10-1 provides a summary of the construction reference noise level measurements. Since the reference noise levels were collected at varying distances of 30 feet and 50 feet, all construction noise level measurements presented on Table 10-1 have been adjusted for consistency to describe a uniform reference distance of 50 feet.

EXHIBIT 10-A: CONSTRUCTION NOISE SOURCE LOCATIONS

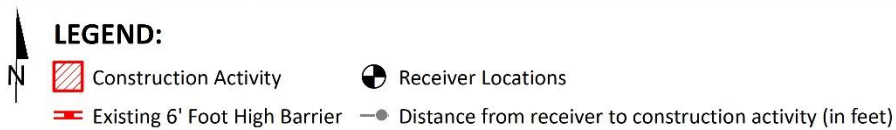


TABLE 10-1: CONSTRUCTION REFERENCE NOISE LEVELS

| Construction Stage | Reference Construction Activity ¹ | Reference Noise Level @ 50 Feet (dBA L _{eq}) | Highest Reference Noise Level (dBA L _{eq}) |
|-----------------------|--|--|--|
| Demolition | Demolition Activity | 67.9 | 71.9 |
| | Backhoe | 64.2 | |
| | Water Truck Pass-By & Backup Alarm | 71.9 | |
| Site Preparation | Scraper, Water Truck, & Dozer Activity | 75.3 | 75.3 |
| | Backhoe | 64.2 | |
| | Water Truck Pass-By & Backup Alarm | 71.9 | |
| Grading | Rough Grading Activities | 73.5 | 73.5 |
| | Water Truck Pass-By & Backup Alarm | 71.9 | |
| | Construction Vehicle Maintenance Activities | 67.5 | |
| Building Construction | Foundation Trenching | 68.2 | 71.6 |
| | Framing | 62.3 | |
| | Concrete Mixer Backup Alarms & Air Brakes | 71.6 | |
| Paving | Concrete Mixer Truck Movements | 71.2 | 71.2 |
| | Concrete Paver Activities | 65.6 | |
| | Concrete Mixer Pour & Paving Activities | 65.9 | |
| Architectural Coating | Air Compressors | 65.2 | 65.2 |
| | Generator | 64.9 | |
| | Crane | 62.3 | |

¹ Reference construction noise level measurements taken by Urban Crossroads, Inc.

10.3 CONSTRUCTION NOISE ANALYSIS

Using the reference construction equipment noise levels and the CadnaA noise prediction model, calculations of the Project construction noise level impacts at the nearest sensitive receiver locations were completed. To assess the worst-case construction noise levels, the Project construction noise analysis relies on the highest noise level impacts when the equipment with the highest reference noise level is operating at the closest point from the edge of primary construction activity (Project site boundary) to each receiver location. As shown on Table 10-2, the construction noise levels are expected to range from 53.1 to 56.2 dBA L_{eq} at the nearest receiver locations. Appendix 10.1 includes the detailed CadnaA construction noise model inputs.

TABLE 10-2: CONSTRUCTION EQUIPMENT NOISE LEVEL SUMMARY

| Receiver Location ¹ | Construction Noise Levels (dBA L _{eq}) | | | | | |
|--------------------------------|--|---------|-----------------------|--------|-----------------------|-----------------------------|
| | Site Preparation | Grading | Building Construction | Paving | Architectural Coating | Highest Levels ² |
| R1 | 56.2 | 54.4 | 52.5 | 52.1 | 46.1 | 56.2 |
| R2 | 53.1 | 51.3 | 49.4 | 49.0 | 43.0 | 53.1 |

¹ Noise receiver locations are shown on Exhibit 10-A.

² Construction noise level calculations based on distance from the project site boundaries (construction activity area) to the nearest receiver locations. CadnaA construction noise model inputs are included in Appendix 10.1.

10.4 CONSTRUCTION NOISE LEVEL COMPLIANCE

To evaluate whether the Project will generate potentially significant short-term noise levels at nearest receiver locations, a construction-related daytime noise level threshold of 80 dBA L_{eq} is used as a reasonable threshold to assess the daytime construction noise level impacts. The construction noise analysis shows that the nearest receiver locations will satisfy the reasonable daytime 80 dBA L_{eq} significance threshold during Project construction activities as shown on Table 10-3. Therefore, the noise impacts due to Project construction noise is considered *less than significant* at all receiver locations.

TABLE 10-3: CONSTRUCTION NOISE LEVEL COMPLIANCE

| Receiver Location ¹ | Construction Noise Levels (dBA L _{eq}) | | |
|--------------------------------|--|------------------------|----------------------------------|
| | Highest Construction Noise Levels ² | Threshold ³ | Threshold Exceeded? ⁴ |
| R1 | 56.2 | 80 | No |
| R2 | 53.1 | 80 | No |

¹ Noise receiver locations are shown on Exhibit 10-A.

² Highest construction noise level calculations based on distance from the construction noise source activity to the nearest receiver locations as shown on Table 10-2.

³ Construction noise level thresholds as shown on Table 4-1.

⁴ Do the estimated Project construction noise levels exceed the construction noise level threshold?

10.5 NIGHTTIME CONCRETE POUR NOISE ANALYSIS

The Project may require nighttime concrete pouring activities as a part of Project construction. Nighttime concrete pouring activities are often used to support reduced concrete mixer truck transit times and lower air temperatures than during the daytime hours. Since the nighttime concrete pours may take place outside the permitted City of Jurupa Valley General Plan Noise Element Policy NE 3.5 hourly limits, the Project Applicant will be required to obtain authorization for nighttime work from the City of Jurupa Valley. The reference paving equipment activity noise levels, shown on Table 10-1, were collected during a nighttime concrete pour at an industrial construction site to represent these activities. As shown on Table 10-2, the concrete pouring equipment noise levels are expected to range from 49.0 to 52.1 dBA L_{eq} when equipment is operating at the closest point from the edge of Project construction activities to the nearby receiver locations. Appendix 10.1 includes the detailed CadnaA construction noise model inputs.

TABLE 10-4: NIGHTTIME CONCRETE POUR NOISE LEVEL COMPLIANCE

| Receiver Location ¹ | Construction Noise Levels (dBA Leq) | | |
|--------------------------------|-------------------------------------|--|----------------------------------|
| | Paving Construction ² | Nighttime Construction Standard ³ | Threshold Exceeded? ⁴ |
| R1 | 48.5 | 70 | No |
| R2 | 44.9 | 70 | No |

¹ Noise receiver locations are shown on Exhibit 10-A.

² Construction noise level calculations based on distance from the center of project construction activity to the property line of adjacent uses as shown on Table 10-4.

³ Construction noise level standards as shown on Table 4-1.

⁴ Do the estimated Project construction noise levels exceed the construction noise level threshold?

10.6 CONSTRUCTION VIBRATION IMPACTS

This analysis focuses on the potential ground-borne vibration associated with vehicular traffic and construction activities. Ground-borne vibration levels from automobile traffic are generally overshadowed by vibration generated by heavy trucks that roll over the same uneven roadway surfaces. However, due to the rapid drop-off rate of ground-borne vibration and the short duration of the associated events, vehicular traffic-induced ground-borne vibration is rarely perceptible beyond the roadway right-of-way, and rarely results in vibration levels that cause damage to buildings in the vicinity.

However, while vehicular traffic is rarely perceptible, construction has the potential to result in varying degrees of temporary ground vibration, depending on the specific construction activities and equipment used. Ground vibration levels associated with various types of construction equipment are summarized on Table 10-5. Based on the representative vibration levels presented for various construction equipment types, it is possible to estimate the potential Project construction vibration levels using the following vibration assessment methods defined by the FTA. The FTA provides the following equation: $PPV_{\text{equip}} = PPV_{\text{ref}} \times (25/D)^{1.5}$

TABLE 10-5: VIBRATION SOURCE LEVELS FOR CONSTRUCTION EQUIPMENT

| Equipment | PPV (in/sec) at 25 feet |
|-----------------|-------------------------|
| Small bulldozer | 0.003 |
| Jackhammer | 0.035 |
| Loaded Trucks | 0.076 |
| Large bulldozer | 0.089 |

Source: Federal Transit Administration, Transit Noise and Vibration Impact Assessment

Construction activity can result in varying degrees of ground vibration, depending on the equipment and methods used, distance to the affected structures and soil type. It is expected that ground-borne vibration from Project construction activities would cause only intermittent, localized intrusion. The proposed Project's construction activities most likely to cause vibration impacts are:

- **Heavy Construction Equipment:** Although all heavy mobile construction equipment has the potential of causing at least some perceptible vibration while operating close to buildings, the vibration is usually short-term and is not of sufficient magnitude to cause building damage.
- **Trucks:** Trucks hauling building materials to construction sites can be sources of vibration intrusion if the haul routes pass through residential neighborhoods on streets with bumps or potholes. Repairing the bumps and potholes generally eliminates the problem.

Ground-borne vibration levels resulting from construction activities occurring within the Project site were estimated by data published by the FTA. Construction activities that would have the potential to generate low levels of ground-borne vibration within the Project site include grading. Using the vibration source level of construction equipment provided on Table 10-5 and the construction vibration assessment methodology published by the FTA, it is possible to estimate the Project vibration impacts. Table 10-6 presents the expected Project related vibration levels at the nearest sensitive receiver locations.

TABLE 10-6: PROJECT CONSTRUCTION VIBRATION LEVELS

| Receiver ¹ | Distance to Const. Activity (Feet) | Receiver PPV Levels (in/sec) ² | | | | | Threshold PPV (in/sec) ³ | Threshold Exceeded? ⁴ |
|-----------------------|------------------------------------|---|-------------|---------------|-----------------|----------------|-------------------------------------|----------------------------------|
| | | Small Bulldozer | Jack-hammer | Loaded Trucks | Large Bulldozer | Peak Vibration | | |
| R1 | 1,001' | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.2 | No |
| R2 | 3,136' | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.2 | No |

¹ Receiver locations are shown on Exhibit 10-A.

² Based on the Vibration Source Levels of Construction Equipment included on Table 10-5.

³ Based on guidance from the City of Jurupa Valley Planning Department

⁴ Does the vibration level exceed the maximum acceptable vibration threshold?

At distances ranging from 1,001 to 3,136 feet from Project construction activities, construction vibration velocity levels are estimated to be 0.000 in/sec PPV and will remain below the City of Jurupa Valley threshold of 0.2 in/sec PPV at all receiver locations, as shown on Table 10-5. Therefore, the Project-related vibration impacts are considered *less than significant* during the construction activities at the Project site.

Moreover, the impacts at the site of the closest sensitive receivers are unlikely to be sustained during the entire construction period but will occur rather only during the times that heavy construction equipment is operating adjacent to the Project site perimeter.

EXHIBIT 10-B: NIGHTTIME CONCRETE POUR NOISE SOURCE AND RECEIVER LOCATIONS

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11 REFERENCES

1. **State of California.** *California Environmental Quality Act, Appendix G.* 2018.
2. **California Department of Transportation Environmental Program.** *Technical Noise Supplement - A Technical Supplement to the Traffic Noise Analysis Protocol.* Sacramento, CA : s.n., September 2013.
3. **Environmental Protection Agency Office of Noise Abatement and Control.** *Information on Levels of Environmental Noise Requisite to Protect Public Health and Welfare with an Adequate Margin of Safety.* March 1974. EPA/ONAC 550/9/74-004.
4. **U.S. Department of Transportation, Federal Highway Administration, Office of Environment and Planning, Noise and Air Quality Branch.** *Highway Traffic Noise Analysis and Abatement Policy and Guidance.* December 2011.
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10. **City of Jurupa Valley.** *General Plan Noise Element.* September 2017.
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13. **City of Jurupa Valley Planning Department.** *Noise Thresholds of Significance Guidance (MA16170, Project: Agua Mansa Commerce Park Specific Plan, Noise Comment 2).* December 19, 2018.
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15. **California Court of Appeal.** *Gray v. County of Madera, F053661.* 167 Cal.App.4th 1099; - Cal.Rptr.3d, October 2008.
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19. **California Department of Transportation Environmental Program, Office of Environmental Engineering.** *Use of California Vehicle Noise Reference Energy Mean Emission Levels (Calveno REMELs) in FHWA Highway Traffic Noise Prediction.* September 1995. TAN 95-03.
20. **California Department of Transportation.** *Traffic Noise Attenuation as a Function of Ground and Vegetation Final Report.* June 1995. FHWA/CA/TL-95/23.
21. **Urban Crossroads, Inc.** *BRE Space Mira Loma (MA200004) Traffic Analysis.* December 2020.

13 CERTIFICATION

The contents of this noise study report represent an accurate depiction of the noise environment and impacts associated with the proposed BRE Space Mira Loma Project. The information contained in this noise study report is based on the best available data at the time of preparation. If you have any questions, please contact me directly at (949) 584-3148.

Bill Lawson, P.E., INCE
Principal
URBAN CROSSROADS, INC.
1133 Camelback #8329
Newport Beach, CA 92658
(949) 581-3148
blawson@urbanxroads.com



EDUCATION

Master of Science in Civil and Environmental Engineering
California Polytechnic State University, San Luis Obispo • December, 1993

Bachelor of Science in City and Regional Planning
California Polytechnic State University, San Luis Obispo • June, 1992

PROFESSIONAL REGISTRATIONS

PE – Registered Professional Traffic Engineer – TR 2537 • January, 2009
AICP – American Institute of Certified Planners – 013011 • June, 1997–January 1, 2012
PTP – Professional Transportation Planner • May, 2007 – May, 2013
INCE – Institute of Noise Control Engineering • March, 2004

PROFESSIONAL AFFILIATIONS

ASA – Acoustical Society of America
ITE – Institute of Transportation Engineers

PROFESSIONAL CERTIFICATIONS

Certified Acoustical Consultant – County of San Diego • March, 2018
Certified Acoustical Consultant – County of Orange • February, 2011
FHWA-NHI-142051 Highway Traffic Noise Certificate of Training • February, 2013

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APPENDIX 3.1:

CITY OF JURUPA VALLEY DEVELOPMENT CODE

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CHAPTER 11.05. - NOISE REGULATIONS

Sec. 11.05.010. - Intent.

At certain levels, sound becomes noise and may jeopardize the health, safety or general welfare of City of Jurupa Valley residents and degrade their quality of life. Pursuant to its police power, the City Council declares that noise shall be regulated in the manner described in this chapter. This chapter is intended to establish city-wide standards regulating noise. This chapter is not intended to establish thresholds of significance for the purpose of any analysis required by the California Environmental Quality Act (Pub. Resources Code Section 21000 *et seq.*) and no such thresholds are established.

(Ord. No. 2012-01, § 1(11.10.010), 2-16-2012)

Sec. 11.05.020. - Exemptions.

Sound emanating from the following sources is exempt from the provisions of this chapter:

- (1) Facilities owned or operated by or for a governmental agency;
- (2) Capital improvement projects of a governmental agency;
- (3) The maintenance or repair of public properties;
- (4) Public safety personnel in the course of executing their official duties, including, but not limited to, sworn peace officers, emergency personnel and public utility personnel. This exemption includes, without limitation, sound emanating from all equipment used by such personnel, whether stationary or mobile;
- (5) Public or private schools and school-sponsored activities;
- (6) Agricultural operations on land designated "agriculture" in the Jurupa Valley General Plan, or land zoned A-1 (light agriculture), A-P (light agriculture with poultry), A-2 (heavy agriculture), or A-D (agriculture-dairy), provided such operations are carried out in a manner consistent with accepted industry standards. This exemption includes, without limitation, sound emanating from all equipment used during such operations, whether stationary or mobile;
- (7) Wind energy conversion systems (WECS), provided such systems comply with the WECS noise provisions of Jurupa Valley Municipal Code or Title 9;
- (8) Private construction projects located one-quarter (¼) of a mile or more from an inhabited dwelling;
- (9) **Private construction projects located within one-quarter (¼) of a mile from an inhabited dwelling, provided that:**
 - (a) **Construction does not occur between the hours of six (6:00) p.m. and six (6:00) a.m. during the months of June through September; and**
 - (b) **Construction does not occur between the hours of six (6:00) p.m. and seven (7:00) a.m. during the months of October through May;**
- (10) Property maintenance, including, but not limited to, the operation of lawnmowers, leaf blowers, etc., provided such maintenance occurs between the hours of seven (7:00) a.m. and eight (8:00) p.m.;
- (11) Motor vehicles, other than off-highway vehicles. This exemption does not include sound emanating from motor vehicle sound systems;
- (12) Heating and air conditioning equipment;
- (13) Safety, warning and alarm devices, including, but not limited to, house and car alarms, and other warning devices that are designed to protect the public health, safety, and welfare; or

(14) The discharge of firearms consistent with all state laws.

(Ord. No. 2012-01, § 1(11.10.020), 2-16-2012)

Sec. 11.05.030. - Definitions.

The following words, terms and phrases, when used in this chapter, shall have the meanings ascribed to them in this section, except where the context clearly indicates a different meaning:

Audio equipment means a television, stereo, radio, tape player, compact disc player, mp3 player, iPod or other similar device.

Decibel (dB) means a unit for measuring the relative amplitude of a sound equal approximately to the smallest difference normally detectable by the human ear, the range of which includes approximately one hundred and thirty (130) decibels on a scale beginning with zero decibels for the faintest detectable sound. Decibels are measured with a sound level meter using different methodologies as defined below:

- (1) "A-weighting (dBA)" means the standard A-weighted frequency response of a sound level meter, which de-emphasizes low and high frequencies of sound in a manner similar to the human ear for moderate sounds.
- (2) "Maximum sound level (Lmax)" means the maximum sound level measured on a sound level meter.

Governmental agency means the United States, the State of California, Riverside County, City of Jurupa Valley, any city within Riverside County, any special district within Riverside County or any combination of these agencies.

Land use permit means a discretionary permit issued by Jurupa Valley pursuant to Jurupa Valley Municipal Code or Title 9.

Motor vehicle means a vehicle that is self-propelled.

Motor vehicle sound system means a stereo, radio, tape player, compact disc player, mp3 player, iPod or other similar device.

Noise means any loud, discordant or disagreeable sound.

Occupied property means property upon which is located a residence, business or industrial or manufacturing use.

Off-highway vehicle means a motor vehicle designed to travel over any terrain.

Public or private school means an institution conducting academic instruction at the preschool, elementary school, junior high school, high school, or college level.

Public property means property owned by a governmental agency or held open to the public, including, but not limited to, parks, streets, sidewalks, and alleys.

Sensitive receptor means a land use that is identified as sensitive to noise in the noise element of the Jurupa Valley General Plan, as applicable to the City of Jurupa Valley by Chapter 1.35, including, but not limited to, residences, schools, hospitals, churches, rest homes, cemeteries or public libraries.

Sound-amplifying equipment means a loudspeaker, microphone, megaphone or other similar device.

Sound level meter means an instrument meeting the standards of the American National Standards Institute for Type 1 or Type 2 sound level meters or an instrument that provides equivalent data.

(Ord. No. 2012-01, § 1(11.10.040), 2-16-2012)

Sec. 11.05.040. - General sound level standards.

No person shall create any sound, or allow the creation of any sound, on any property that causes the exterior sound level on any other occupied property to exceed the sound level standards set forth in Table 1 of this section or that violates the special sound source standards set forth in Section 11.05.060.

Table 1
Sound Level Standards (Db Lmax)

| <i>General Plan Foundation Component</i> | <i>General Plan Land Use Designation</i> | <i>General Plan Land Use Designation Name</i> | <i>Density</i> | <i>Maximum Decibel Level</i> | |
|--|--|---|----------------|----------------------------------|--------------------------------|
| | | | | <i>7 a.m.— 10 p.m.</i> | <i>10 p.m.— 7 a.m.</i> |
| <i>Community Development</i> | EDR | Estate density residential | 2 AC | 55 | 45 |
| | VLDR | Very low density residential | 1 AC | 55 | 45 |
| | LDR | Low density residential | 1/2 AC | 55 | 45 |
| | MDR | Medium density residential | 2—5 | 55 | 45 |
| | MHDR | Medium high density residential | 5—8 | 55 | 45 |
| | HDR | High density residential | 8—14 | 55 | 45 |
| | VHDR | Very high density residential | 14—20 | 55 | 45 |
| | HTDR | Highest density residential | 20+ | 55 | 45 |
| | CR | Retail commercial | | 65 | 55 |
| | CO | Office commercial | | 65 | 55 |
| | CT | Tourist commercial | | 65 | 55 |
| | CC | Community center | | 65 | 55 |
| | I | Light industrial | | 75 | 55 |
| | HI | Heavy industrial | | 75 | 75 |

| | | | | | |
|------------------------|------|--------------------------------|--------|----|----|
| | BP | Business park | | 65 | 45 |
| | PF | Public facility | | 65 | 45 |
| | SP | Specific plan—Residential | | 55 | 45 |
| | | Specific plan—Commercial | | 65 | 55 |
| | | Specific plan—Light Industrial | | 75 | 55 |
| | | Specific plan—Heavy Industrial | | 75 | 75 |
| <i>Rural Community</i> | EDR | Estate density residential | 2 AC | 55 | 45 |
| | VLDR | Very low density residential | AC | 55 | 45 |
| | LDR | Low density residential | 1/2 AC | 55 | 45 |
| <i>Rural</i> | RR | Rural residential | 5 AC | 45 | 45 |
| | RM | Rural mountainous | 10 AC | 45 | 45 |
| | RD | Rural desert | 0 AC | 45 | 45 |
| <i>Agriculture</i> | AG | Agriculture | 10 AC | 45 | 45 |
| <i>Open Space</i> | C | Conservation | | 45 | 45 |
| | CH | Conservation habitat | | 45 | 45 |
| | REC | Recreation | | 45 | 45 |
| | RUR | Rural | 20 AC | 45 | 45 |
| | W | Watershed | | 45 | 45 |
| | MR | Mineral resources | | 75 | 45 |

(Ord. No. 2012-01, § 1(11.10.040), 2-16-2012)

Sec. 11.05.050. - Sound level measurement methodology.

If the sound standard being applied is measured in decibels, then sound level measurements pursuant to this section shall be required to establish a violation of this chapter. If the sound standard being applied is not measured in decibels, then sound level measurements are not required to establish a violation of this chapter. Sound level measurements may be made anywhere within the boundaries of an occupied property. The actual location of a sound level measurement shall be at the discretion of the Enforcement Officials identified in Section 11.05.080. Sound level measurements shall be made with a sound level meter. Immediately before a measurement is made, the sound level meter shall be calibrated utilizing an acoustical calibrator meeting the standards of the American National Standards Institute. Following a sound level measurement, the calibration of the sound level meter shall be re-verified. Sound level meters and calibration equipment shall be certified annually.

(Ord. No. 2012-01, § 1(11.10.050), 2-16-2012)

Sec. 11.05.060. - Special sound sources standards.

The general sound level standards set forth in Section 11.05.040 apply to sound emanating from all sources, including the following special sound sources, and the person creating, or allowing the creation of, the sound is subject to the requirements of that section. The following special sound sources are also subject to the following additional standards, the failure to comply with which constitute separate violations of this chapter:

(1) *Motor vehicles.*

(a) *Off-highway vehicles.*

- (i) No person shall operate an off-highway vehicle unless it is equipped with a USDA-qualified spark arrester and a constantly operating and properly maintained muffler. A muffler is not considered constantly operating and properly maintained if it is equipped with a cutout, bypass or similar device.
- (ii) No person shall operate an off-highway vehicle unless the noise emitted by the vehicle is not more than ninety-six (96) dBA if the vehicle was manufactured on or after January 1, 1986, or is not more than one hundred and one (101) dBA if the vehicle was manufactured before January 1, 1986. For purposes of this subsection, emitted noise shall be measured a distance of twenty (20) inches from the vehicle tailpipe using test procedures established by the Society of Automotive Engineers under Standard J-1287.

- (b) *Sound systems.* No person shall operate a motor vehicle sound system, whether affixed to the vehicle or not, between the hours of ten (10:00) p.m. and eight (8:00) a.m., such that the sound system is audible to the human ear inside any inhabited dwelling. No person shall operate a motor vehicle sound system, whether affixed to the vehicle or not, at any other time such that the sound system is audible to the human ear at a distance greater than one hundred (100) feet from the vehicle. Sound level measurements may be used, but are not required to establish a violation of this subsection.

- (2) *Power tools and equipment.* No person shall operate any power tools or equipment between the hours of ten (10:00) p.m. and eight (8:00) a.m. such that the power tools or equipment are audible to the human ear inside an inhabited dwelling other than a dwelling in which the power tools or equipment may be located. No person shall operate any power tools or equipment at any other time such that the power tools or equipment are audible to the human ear at a

distance greater than one hundred (100) feet from the power tools or equipment. Sound level measurements may be used, but are not required to establish a violation of this subsection.

- (3) *Audio equipment.* No person shall operate any audio equipment, whether portable or not, such that the equipment is audible to the human ear at a distance greater than one hundred (100) feet from the equipment. Sound level measurements may be used, but are not required to establish a violation of this subsection.
- (4) *Sound-amplifying equipment and live music.* No person shall install, use or operate sound-amplifying equipment, or perform, or allow to be performed, live music if the sound emanating from sound-amplifying equipment or live music is audible to the human ear at a distance greater than one hundred (100) feet from the equipment or music. To the extent that these requirements conflict with any conditions of approval attached to an underlying land use permit, these requirements shall control. Sound level measurements may be used, but are not required to establish a violation of this subsection.

(Ord. No. 2012-01, § 1(11.10.060), 2-16-2012; Ord. No. 2015-08, § 1, 6-18-2015)

Sec. 11.05.070. - Exceptions.

Exceptions may be requested from the standards set forth in Section 11.10.040 or 11.10.060 of this chapter and may be characterized as construction-related or continuous-events exceptions.

- (1) *Application and processing.*
 - (a) *Construction-related exceptions.* An application for a construction-related exception shall be made to and considered by the Building Official of the city on forms provided by the Building and Safety Division and shall be accompanied by the appropriate filing fee. No public hearing is required.
 - (b) *Continuous events exceptions.* An application for a continuous events exception shall be made to the Planning Director on forms provided by the Planning Department and shall be accompanied by the appropriate filing fee. Upon receipt of an application for a continuous events exception, the Planning Director shall set the matter for public hearing before the Planning Commission, notice of which shall be given as provided in Section 9.240.250 of this Code. Notwithstanding the above, an application for a continuous events exception that is associated with an application for a land use permit shall be processed concurrently with the land use permit in the same manner that the land use permit is required to be processed.
- (2) *Requirements for approval.* The appropriate decision-making body or officer shall not approve an exception application unless the applicant demonstrates that the activities described in the application would not be detrimental to the health, safety or general welfare of the community. In determining whether activities are detrimental to the health, safety or general welfare of the community, the appropriate decision-making body or officer shall consider such factors as the proposed duration of the activities and their location in relation to sensitive receptors. If an exception application is approved, reasonable conditions may be imposed to minimize the public detriment, including, but not limited to, restrictions on sound level, sound duration and operating hours.
- (3) *Appeals.* The Building Official's decision on an application for a construction-related exception is considered final. After making a decision on an application for a continuous-events exception, the appropriate decision-making body or officer shall mail notice of the decision to the applicant. Within ten (10) calendar days after the mailing of such notice, the applicant or interested person may appeal the decision pursuant to and in accordance with the provisions of Chapter 2.40 of this Code.

(Ord. No. 2012-01, § 1(11.10.070), 2-16-2012; Ord. No. 2015-08, § 2, 6-18-2015; Ord. No. 2016-04, § 11(11.10.070), 4-7-2016)

Sec. 11.05.080. - Violations and penalties.

- A. Violation of the provisions of this chapter may be enforced pursuant to the enforcement provisions set forth in Title 1 of this Code, including Chapter 1.10, Code Enforcement Generally, Chapter 1.15, Criminal Prosecution, Chapter 1.20, Administrative Penalties, or Chapter 1.25, Public Nuisance Injunctions.
- B. The fine schedule for a violation of this chapter enforced pursuant to Chapter 1.20, shall be in the amount of:
 - (1) Two hundred dollars (\$200) for the first violation occurring within a three hundred and sixty-six (366) day period;
 - (2) Five hundred dollars (\$500) for a second violation occurring within three hundred and sixty-six (366) days of the first violation;
 - (3) Seven hundred and fifty dollars (\$750) for a third violation occurring within three hundred and sixty-six (366) days of the first violation; or
 - (4) One thousand dollars (\$1,000) for a fourth violation and each subsequent violation occurring within three hundred and sixty-six (366) days of the first violation.
- C. The fines set forth in subsection (B) of this section may be modified by a resolution of the City Council establishing an administrative citation schedule not to exceed one thousand dollars (\$1,000) per violation and which may include increased fines for repeat violations and penalties.
- D. The City Manager or his designee may reduce the fines set forth in subsections (B) or (C) of this section in the event he or she finds that the violation is not likely to reoccur, the violator cooperated with Enforcement Officials in attempting to enforce the provisions of this chapter and resolve the issues giving rise to the violation, the actions of the violator giving rise to the violation were not malicious and were not taken in deliberate disregard of the provisions of this chapter, and the ends of justice would not be served by imposing the full fine.

(Ord. No. 2012-01, § 1(11.10.080), 2-16-2012)

Sec. 11.05.090. - Duty to cooperate.

No person shall refuse to cooperate with, or obstruct, the Enforcement Officials identified in Section 11.05.080 when they are engaged in the process of enforcing the provisions of this chapter. This duty to cooperate may require a person to extinguish a sound source so that it can be determined whether sound emanating from the source violates the provisions of this chapter.

(Ord. No. 2012-01, § 1(11.10.090), 2-16-2012)

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APPENDIX 4.1:

CITY OF JURUPA VALLEY CEQA THRESHOLDS

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| Noise Impact Analysis October 30, 2018 | | Comment |
|---|--------------------|---|
| | | increase and, if appropriate, the project's contribution to a potentially significant cumulative traffic noise increase. |
| 2 | Global | <p>Sec. 11.05.010 of the Municipal Code states in part: "...This chapter is intended to establish city-wide standards regulating noise. This chapter is not intended to establish thresholds of significance for the purpose of any analysis required by the California Environmental Quality Act (Pub. Resources Code Section 21000 et seq.) and no such thresholds are established..."</p> <p>Please use the following standards for CEQA significance thresholds and revise report throughout:</p> <ul style="list-style-type: none"> Construction Noise: For sensitive residential land uses nearby, the daytime and nighttime 8-hour standards are 80 dBA Leq and 70 dBA Leq, respectively (FTA Transit Noise and Vibration Impact Assessment). Operational Noise (stationary): During operation of the Project, a significant noise-related impact would occur if Project operational noise at a noise-sensitive receptor exceeds: <ul style="list-style-type: none"> 65 dBA Leq (10 minutes) between 7:00 a.m. and 10:00 p.m., or 45 dBA Leq (10 min) between 10:00 p.m. and 7:00 a.m. Operational Noise (traffic): Project-related traffic increases the noise level at a: <ul style="list-style-type: none"> Residential land use by 3 dBA or more to 65 dBA CNEL or above; or Commercial land use by 3 dBA or more to 70 dBA CNEL or above. Vibration: A significant vibration-related impact would occur if the Project would expose a vibration-sensitive receptor to vibration levels that exceed 0.2 in/sec PPV during either long-term operation or construction of the Project <p><i>Note: The Municipal Code noise standards may be used for planning purposes only (i.e. to demonstrate that the project meets the City code requirements for site plan approval).</i></p> |
| 3 | Page 23 | Construction exemptions for San Bernardino County are not discussed and are contained in Section 83.01.080(g) (3), i.e., 7 am – 7pm, except Sundays and federal holidays. |
| 4 | Page 24 and global | Policy NE 4.4 is intended for train operation but is being used to assess projects. Please convert this RMS level to VdB so that it can |

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APPENDIX 5.1:

STUDY AREA PHOTOS

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JN: 13575 Study Area Photos



L1_E
34, 1' 22.180000", 117, 31' 26.600000"



L1_N
34, 1' 22.040000", 117, 31' 26.680000"



L1_S
34, 1' 22.160000", 117, 31' 26.600000"



L1_W
34, 1' 22.180000", 117, 31' 26.630000"



L2_E
34, 1' 22.010000", 117, 31' 51.840000"



L2_N
34, 1' 21.050000", 117, 31' 52.030000"

JN: 13575 Study Area Photos



L2_S
34, 1' 22.300000", 117, 31' 51.840000"



L2_W
34, 1' 21.960000", 117, 31' 51.810000"



L3_E



L3_N



L3_S



L3_W

JN: 13575 Study Area Photos



L4_E
34, 1' 43.270000", 117, 32' 22.520000"



L4_N
34, 1' 43.520000", 117, 32' 22.550000"



L4_S
34, 1' 43.270000", 117, 32' 22.520000"



L4_W
34, 1' 43.270000", 117, 32' 22.580000"



L5_E
34, 1' 40.280000", 117, 31' 52.610000"



L5_N
34, 1' 43.080000", 117, 32' 20.410000"

JN: 13575 Study Area Photos



L5_S

34, 1' 40.260000", 117, 31' 52.660000"



L5_W

34, 1' 40.290000", 117, 31' 52.580000"

APPENDIX 5.2:

NOISE LEVEL MEASUREMENT WORKSHEETS

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24-Hour Noise Level Measurement Summary

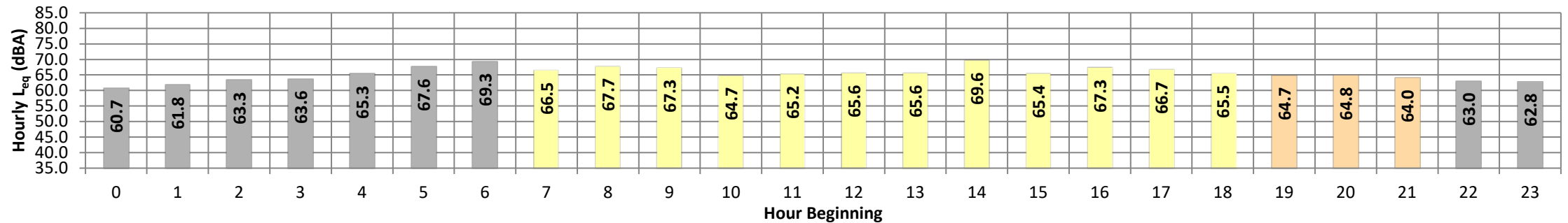
Date: Wednesday, July 15, 2020
Project: MA 20004 BRE SPACE CENTER

Location: L1 - Located southeast of the Project site on Etiwanda Avenue near existing single-family residential home at 10991 Iberia Street.

Meter: Piccolo II

JN: 13575
Analyst: P. Mara

Hourly L_{eq} dBA Readings (unadjusted)



| Timeframe | Hour | L _{eq} | L _{max} | L _{min} | L1% | L2% | L5% | L8% | L25% | L50% | L90% | L95% | L99% | L _{eq} | Adj. | Adj. L _{eq} | | |
|----------------|------|-----------------|------------------|------------------|------|------|------|------|------|------|------|------|------|-----------------------|---------|----------------------|--|--|
| Night | 0 | 60.7 | 70.7 | 49.4 | 70.2 | 69.5 | 67.5 | 66.0 | 60.5 | 55.2 | 50.4 | 49.9 | 49.5 | 60.7 | 10.0 | 70.7 | | |
| | 1 | 61.8 | 73.7 | 48.7 | 73.3 | 72.4 | 69.6 | 66.4 | 59.1 | 54.6 | 49.6 | 49.2 | 48.8 | 61.8 | 10.0 | 71.8 | | |
| | 2 | 63.3 | 73.9 | 49.9 | 73.4 | 72.8 | 70.5 | 68.6 | 62.4 | 56.9 | 51.2 | 50.6 | 50.0 | 63.3 | 10.0 | 73.3 | | |
| | 3 | 63.6 | 74.1 | 50.7 | 73.8 | 73.1 | 70.4 | 68.5 | 63.1 | 58.7 | 52.1 | 51.4 | 50.8 | 63.6 | 10.0 | 73.6 | | |
| | 4 | 65.3 | 75.0 | 52.3 | 74.6 | 74.0 | 72.1 | 70.5 | 65.2 | 60.7 | 53.9 | 53.2 | 52.5 | 65.3 | 10.0 | 75.3 | | |
| | 5 | 67.6 | 77.6 | 55.6 | 77.2 | 76.4 | 74.1 | 72.2 | 67.5 | 63.6 | 57.3 | 56.4 | 55.9 | 67.6 | 10.0 | 77.6 | | |
| | 6 | 69.3 | 79.4 | 62.5 | 78.9 | 78.0 | 74.8 | 72.8 | 69.0 | 66.5 | 63.7 | 63.3 | 62.7 | 69.3 | 10.0 | 79.3 | | |
| Day | 7 | 66.5 | 75.2 | 55.5 | 74.8 | 74.1 | 72.4 | 71.0 | 67.3 | 63.7 | 56.8 | 56.2 | 55.7 | 66.5 | 0.0 | 66.5 | | |
| | 8 | 67.7 | 78.0 | 55.3 | 77.6 | 76.9 | 74.1 | 72.1 | 67.7 | 63.6 | 57.1 | 56.3 | 55.5 | 67.7 | 0.0 | 67.7 | | |
| | 9 | 67.3 | 77.2 | 55.3 | 76.7 | 76.2 | 73.6 | 71.5 | 67.4 | 63.5 | 57.1 | 56.4 | 55.5 | 67.3 | 0.0 | 67.3 | | |
| | 10 | 64.7 | 73.1 | 54.1 | 72.6 | 72.0 | 70.4 | 69.4 | 65.8 | 61.9 | 55.8 | 54.9 | 54.2 | 64.7 | 0.0 | 64.7 | | |
| | 11 | 65.2 | 73.9 | 54.4 | 73.5 | 73.0 | 71.0 | 69.8 | 65.9 | 62.2 | 56.0 | 55.3 | 54.6 | 65.2 | 0.0 | 65.2 | | |
| | 12 | 65.6 | 74.5 | 54.2 | 74.1 | 73.5 | 72.0 | 70.7 | 66.0 | 62.0 | 55.9 | 55.1 | 54.3 | 65.6 | 0.0 | 65.6 | | |
| | 13 | 65.6 | 74.5 | 54.6 | 74.1 | 73.6 | 71.7 | 70.1 | 66.3 | 62.1 | 56.3 | 55.5 | 54.8 | 65.6 | 0.0 | 65.6 | | |
| | 14 | 69.6 | 80.4 | 56.2 | 79.8 | 79.1 | 77.0 | 75.1 | 68.5 | 63.5 | 57.8 | 57.1 | 56.4 | 69.6 | 0.0 | 69.6 | | |
| | 15 | 65.4 | 74.1 | 56.1 | 73.7 | 73.1 | 71.2 | 70.1 | 66.0 | 62.3 | 57.4 | 56.8 | 56.2 | 65.4 | 0.0 | 65.4 | | |
| | 16 | 67.3 | 78.2 | 55.6 | 77.6 | 76.4 | 73.4 | 71.8 | 67.1 | 63.1 | 57.2 | 56.4 | 55.8 | 67.3 | 0.0 | 67.3 | | |
| | 17 | 66.7 | 77.3 | 55.6 | 76.8 | 76.0 | 73.5 | 71.4 | 66.3 | 62.5 | 56.8 | 56.3 | 55.7 | 66.7 | 0.0 | 66.7 | | |
| | 18 | 65.5 | 76.5 | 55.0 | 75.8 | 74.9 | 72.3 | 70.1 | 64.9 | 60.4 | 55.9 | 55.5 | 55.1 | 65.5 | 0.0 | 65.5 | | |
| Evening | 19 | 64.7 | 75.7 | 53.2 | 75.2 | 74.5 | 72.2 | 69.8 | 63.7 | 59.1 | 54.4 | 53.8 | 53.3 | 64.7 | 5.0 | 69.7 | | |
| | 20 | 64.8 | 75.4 | 53.0 | 74.8 | 74.2 | 71.6 | 69.9 | 64.4 | 59.6 | 54.2 | 53.7 | 53.1 | 64.8 | 5.0 | 69.8 | | |
| | 21 | 64.0 | 75.2 | 52.2 | 74.5 | 73.7 | 71.2 | 68.8 | 63.1 | 58.5 | 53.3 | 52.9 | 52.4 | 64.0 | 5.0 | 69.0 | | |
| Night | 22 | 63.0 | 74.8 | 50.8 | 74.1 | 73.2 | 70.3 | 67.9 | 61.6 | 56.4 | 51.9 | 51.4 | 51.0 | 63.0 | 10.0 | 73.0 | | |
| | 23 | 62.8 | 74.0 | 50.2 | 73.7 | 73.0 | 70.0 | 67.6 | 61.5 | 56.6 | 51.5 | 50.9 | 50.3 | 62.8 | 10.0 | 72.8 | | |
| Timeframe | Hour | L _{eq} | L _{max} | L _{min} | L1% | L2% | L5% | L8% | L25% | L50% | L90% | L95% | L99% | L _{eq} (dBA) | | | | |
| Day | Min | 64.7 | 73.1 | 54.1 | 72.6 | 72.0 | 70.4 | 69.4 | 64.9 | 60.4 | 55.8 | 54.9 | 54.2 | 24-Hour | Daytime | Nighttime | | |
| | Max | 69.6 | 80.4 | 56.2 | 79.8 | 79.1 | 77.0 | 75.1 | 68.5 | 63.7 | 57.8 | 57.1 | 56.4 | | | | | |
| Energy Average | | 66.6 | Average: | | 75.6 | 74.9 | 72.7 | 71.1 | 66.6 | 62.6 | 56.7 | 56.0 | 55.3 | 65.966.365.0 | | | | |
| Evening | Min | 64.0 | 75.2 | 52.2 | 74.5 | 73.7 | 71.2 | 68.8 | 63.1 | 58.5 | 53.3 | 52.9 | 52.4 | | | | | |
| | Max | 64.8 | 75.7 | 53.2 | 75.2 | 74.5 | 72.2 | 69.9 | 64.4 | 59.6 | 54.4 | 53.8 | 53.3 | 24-Hour CNEL (dBA) | | | | |
| Energy Average | | 64.5 | Average: | | 74.9 | 74.1 | 71.7 | 69.5 | 63.7 | 59.1 | 54.0 | 53.4 | 52.9 | 71.9 | | | | |
| Night | Min | 60.7 | 70.7 | 48.7 | 70.2 | 69.5 | 67.5 | 66.0 | 59.1 | 54.6 | 49.6 | 49.2 | 48.8 | | | | | |
| | Max | 69.3 | 79.4 | 62.5 | 78.9 | 78.0 | 74.8 | 72.8 | 69.0 | 66.5 | 63.7 | 63.3 | 62.7 | | | | | |
| Energy Average | | 65.0 | Average: | | 74.3 | 73.6 | 71.0 | 69.0 | 63.3 | 58.8 | 53.5 | 52.9 | 52.4 | | | | | |

24-Hour Noise Level Measurement Summary

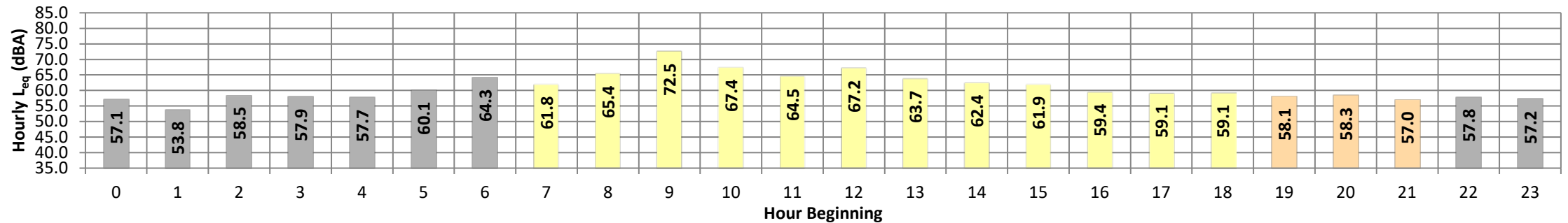
Date: Wednesday, July 15, 2020
Project: MA 20004 BRE SPACE CENTER

Location: L2 - Located south of the Project site on Iberia Street near
existing industrial uses at 11600 Iberia Street.

Meter: Piccolo II

JN: 13575
Analyst: P. Mara

Hourly L_{eq} dBA Readings (unadjusted)



| Timeframe | Hour | L_{eq} | L_{max} | L_{min} | L1% | L2% | L5% | L8% | L25% | L50% | L90% | L95% | L99% | L_{eq} | Adj. | Adj. L_{eq} | | |
|----------------|------|----------|-----------|-----------|------|------|------|------|------|------|------|------|------|--------------------|---------|---------------|--|--|
| Night | 0 | 57.1 | 64.6 | 48.4 | 64.3 | 64.0 | 63.1 | 62.5 | 57.8 | 53.0 | 49.6 | 49.1 | 48.6 | 57.1 | 10.0 | 67.1 | | |
| | 1 | 53.8 | 61.2 | 48.4 | 60.8 | 60.4 | 59.0 | 58.1 | 54.2 | 51.2 | 48.9 | 48.7 | 48.5 | 53.8 | 10.0 | 63.8 | | |
| | 2 | 58.5 | 67.0 | 49.6 | 66.6 | 66.0 | 64.9 | 64.2 | 59.0 | 52.3 | 50.0 | 49.9 | 49.7 | 58.5 | 10.0 | 68.5 | | |
| | 3 | 57.9 | 65.4 | 52.8 | 65.0 | 64.5 | 63.0 | 61.7 | 58.4 | 55.9 | 53.7 | 53.4 | 52.9 | 57.9 | 10.0 | 67.9 | | |
| | 4 | 57.7 | 65.9 | 52.1 | 65.4 | 65.0 | 63.6 | 62.3 | 57.8 | 54.7 | 52.8 | 52.5 | 52.2 | 57.7 | 10.0 | 67.7 | | |
| | 5 | 60.1 | 69.1 | 53.7 | 68.7 | 68.2 | 66.4 | 64.8 | 59.4 | 56.9 | 54.4 | 54.1 | 53.8 | 60.1 | 10.0 | 70.1 | | |
| | 6 | 64.3 | 73.0 | 58.2 | 72.3 | 71.4 | 69.4 | 68.4 | 64.6 | 61.7 | 59.1 | 58.8 | 58.4 | 64.3 | 10.0 | 74.3 | | |
| Day | 7 | 61.8 | 71.7 | 53.3 | 71.1 | 70.1 | 68.2 | 67.6 | 61.1 | 57.3 | 54.0 | 53.7 | 53.4 | 61.8 | 0.0 | 61.8 | | |
| | 8 | 65.4 | 75.6 | 54.0 | 75.1 | 74.2 | 72.3 | 70.7 | 65.0 | 60.4 | 55.6 | 54.9 | 54.2 | 65.4 | 0.0 | 65.4 | | |
| | 9 | 72.5 | 81.4 | 67.1 | 80.5 | 79.6 | 77.9 | 76.8 | 72.6 | 69.6 | 67.5 | 67.4 | 67.2 | 72.5 | 0.0 | 72.5 | | |
| | 10 | 67.4 | 77.7 | 61.6 | 76.7 | 75.7 | 73.2 | 71.4 | 66.9 | 64.3 | 62.3 | 62.1 | 61.7 | 67.4 | 0.0 | 67.4 | | |
| | 11 | 64.5 | 74.3 | 56.9 | 73.8 | 73.1 | 70.8 | 69.2 | 63.9 | 60.6 | 57.7 | 57.3 | 57.0 | 64.5 | 0.0 | 64.5 | | |
| | 12 | 67.2 | 77.5 | 62.9 | 76.3 | 74.7 | 72.2 | 70.5 | 66.5 | 65.0 | 63.5 | 63.3 | 63.1 | 67.2 | 0.0 | 67.2 | | |
| | 13 | 63.7 | 74.4 | 53.2 | 73.8 | 72.9 | 70.5 | 68.9 | 62.9 | 59.3 | 54.2 | 53.7 | 53.3 | 63.7 | 0.0 | 63.7 | | |
| | 14 | 62.4 | 72.8 | 52.6 | 72.3 | 71.3 | 69.2 | 67.8 | 61.6 | 57.3 | 53.5 | 53.1 | 52.8 | 62.4 | 0.0 | 62.4 | | |
| | 15 | 61.9 | 73.1 | 54.1 | 72.3 | 71.0 | 67.9 | 66.4 | 61.0 | 57.5 | 54.8 | 54.5 | 54.2 | 61.9 | 0.0 | 61.9 | | |
| | 16 | 59.4 | 67.3 | 53.8 | 66.9 | 66.3 | 65.0 | 64.0 | 59.6 | 56.6 | 54.5 | 54.2 | 53.9 | 59.4 | 0.0 | 59.4 | | |
| | 17 | 59.1 | 68.6 | 52.9 | 67.7 | 66.6 | 64.6 | 63.7 | 59.2 | 56.3 | 53.5 | 53.3 | 53.0 | 59.1 | 0.0 | 59.1 | | |
| | 18 | 59.1 | 67.6 | 53.1 | 66.8 | 66.0 | 64.3 | 63.3 | 59.8 | 56.3 | 53.8 | 53.5 | 53.2 | 59.1 | 0.0 | 59.1 | | |
| Evening | 19 | 58.1 | 66.7 | 52.9 | 66.2 | 65.8 | 63.8 | 62.5 | 57.8 | 55.3 | 53.4 | 53.2 | 53.0 | 58.1 | 5.0 | 63.1 | | |
| | 20 | 58.3 | 66.0 | 54.2 | 65.4 | 64.7 | 63.2 | 62.3 | 58.4 | 56.1 | 54.7 | 54.5 | 54.3 | 58.3 | 5.0 | 63.3 | | |
| | 21 | 57.0 | 64.7 | 52.5 | 64.0 | 63.2 | 61.7 | 60.6 | 57.4 | 55.1 | 53.2 | 52.9 | 52.6 | 57.0 | 5.0 | 62.0 | | |
| Night | 22 | 57.8 | 68.5 | 50.9 | 67.5 | 66.1 | 64.2 | 62.5 | 57.1 | 54.2 | 51.7 | 51.4 | 51.0 | 57.8 | 10.0 | 67.8 | | |
| | 23 | 57.2 | 66.4 | 52.8 | 65.5 | 64.4 | 62.3 | 60.6 | 57.1 | 54.8 | 53.2 | 53.0 | 52.9 | 57.2 | 10.0 | 67.2 | | |
| Timeframe | Hour | L_{eq} | L_{max} | L_{min} | L1% | L2% | L5% | L8% | L25% | L50% | L90% | L95% | L99% | L_{eq} (dBA) | | | | |
| Day | Min | 59.1 | 67.3 | 52.6 | 66.8 | 66.0 | 64.3 | 63.3 | 59.2 | 56.3 | 53.5 | 53.1 | 52.8 | 24-Hour | Daytime | Nighttime | | |
| | Max | 72.5 | 81.4 | 67.1 | 80.5 | 79.6 | 77.9 | 76.8 | 72.6 | 69.6 | 67.5 | 67.4 | 67.2 | | | | | |
| Energy Average | | 65.7 | Average: | | 72.8 | 71.8 | 69.7 | 68.4 | 63.3 | 60.0 | 57.1 | 56.7 | 56.4 | 63.5 64.9 59.2 | | | | |
| Evening | Min | 57.0 | 64.7 | 52.5 | 64.0 | 63.2 | 61.7 | 60.6 | 57.4 | 55.1 | 53.2 | 52.9 | 52.6 | | | | | |
| | Max | 58.3 | 66.7 | 54.2 | 66.2 | 65.8 | 63.8 | 62.5 | 58.4 | 56.1 | 54.7 | 54.5 | 54.3 | 24-Hour CNEL (dBA) | | | | |
| Energy Average | | 57.8 | Average: | | 65.2 | 64.6 | 62.9 | 61.8 | 57.9 | 55.5 | 53.7 | 53.5 | 53.3 | 67.2 | | | | |
| Night | Min | 53.8 | 61.2 | 48.4 | 60.8 | 60.4 | 59.0 | 58.1 | 54.2 | 51.2 | 48.9 | 48.7 | 48.5 | | | | | |
| | Max | 64.3 | 73.0 | 58.2 | 72.3 | 71.4 | 69.4 | 68.4 | 64.6 | 61.7 | 59.1 | 58.8 | 58.4 | | | | | |
| Energy Average | | 59.2 | Average: | | 66.2 | 65.6 | 64.0 | 62.8 | 58.4 | 55.0 | 52.6 | 52.3 | 52.0 | | | | | |

24-Hour Noise Level Measurement Summary

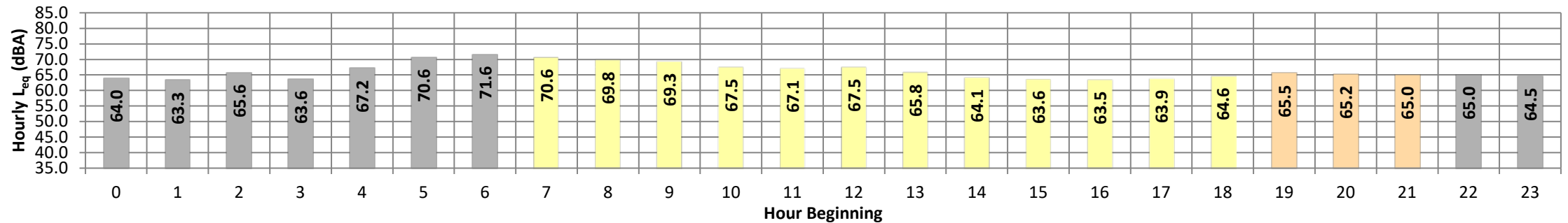
Date: Wednesday, July 15, 2020
Project: MA 20004 BRE SPACE CENTER

Location: L3 - Located west of the Project site on Corridor Drive near the Mira Loma Assembly Hall of Jehovah's Witnesses at 3300 Cornerstone Drive.

Meter: Piccolo II

JN: 13575
Analyst: P. Mara

Hourly L_{eq} dBA Readings (unadjusted)



| Timeframe | Hour | L_{eq} | L_{max} | L_{min} | L1% | L2% | L5% | L8% | L25% | L50% | L90% | L95% | L99% | L_{eq} | Adj. | Adj. L_{eq} | | |
|----------------|------|----------|-----------|-----------|------|------|------|------|------|------|------|------|------|--------------------|---------|---------------|--|--|
| Night | 0 | 64.0 | 71.5 | 55.7 | 71.2 | 70.9 | 69.5 | 68.4 | 64.9 | 61.4 | 57.4 | 56.5 | 55.9 | 64.0 | 10.0 | 74.0 | | |
| | 1 | 63.3 | 71.2 | 54.5 | 70.9 | 70.5 | 69.4 | 68.2 | 63.8 | 60.5 | 56.4 | 55.5 | 54.7 | 63.3 | 10.0 | 73.3 | | |
| | 2 | 65.6 | 72.8 | 56.2 | 72.6 | 72.3 | 71.5 | 70.8 | 66.5 | 62.1 | 57.8 | 57.1 | 56.4 | 65.6 | 10.0 | 75.6 | | |
| | 3 | 63.6 | 69.0 | 57.9 | 68.7 | 68.4 | 67.6 | 66.9 | 64.5 | 62.6 | 59.4 | 58.7 | 58.1 | 63.6 | 10.0 | 73.6 | | |
| | 4 | 67.2 | 70.6 | 63.8 | 70.4 | 70.1 | 69.6 | 69.2 | 67.9 | 66.9 | 64.8 | 64.4 | 63.9 | 67.2 | 10.0 | 77.2 | | |
| | 5 | 70.6 | 74.7 | 68.1 | 74.4 | 74.0 | 72.9 | 72.2 | 71.1 | 70.2 | 68.8 | 68.5 | 68.2 | 70.6 | 10.0 | 80.6 | | |
| | 6 | 71.6 | 75.4 | 69.2 | 75.2 | 74.9 | 74.2 | 73.7 | 72.0 | 71.0 | 69.8 | 69.5 | 69.3 | 71.6 | 10.0 | 81.6 | | |
| Day | 7 | 70.6 | 73.1 | 68.7 | 72.8 | 72.6 | 72.2 | 72.0 | 71.1 | 70.4 | 69.2 | 69.0 | 68.8 | 70.6 | 0.0 | 70.6 | | |
| | 8 | 69.8 | 72.9 | 67.6 | 72.6 | 72.3 | 71.7 | 71.4 | 70.4 | 69.6 | 68.2 | 68.0 | 67.7 | 69.8 | 0.0 | 69.8 | | |
| | 9 | 69.3 | 72.3 | 66.5 | 72.0 | 71.7 | 71.2 | 70.9 | 70.0 | 69.1 | 67.4 | 67.0 | 66.6 | 69.3 | 0.0 | 69.3 | | |
| | 10 | 67.5 | 71.3 | 64.5 | 71.0 | 70.6 | 69.7 | 69.4 | 68.2 | 67.2 | 65.4 | 65.1 | 64.7 | 67.5 | 0.0 | 67.5 | | |
| | 11 | 67.1 | 70.4 | 64.3 | 70.1 | 69.9 | 69.3 | 68.9 | 67.8 | 66.8 | 65.1 | 64.8 | 64.4 | 67.1 | 0.0 | 67.1 | | |
| | 12 | 67.5 | 72.7 | 64.7 | 71.5 | 71.0 | 69.9 | 69.3 | 68.0 | 67.1 | 65.5 | 65.1 | 64.8 | 67.5 | 0.0 | 67.5 | | |
| | 13 | 65.8 | 70.1 | 62.7 | 69.8 | 69.5 | 68.6 | 68.0 | 66.4 | 65.2 | 63.5 | 63.2 | 62.8 | 65.8 | 0.0 | 65.8 | | |
| | 14 | 64.1 | 68.2 | 60.8 | 67.8 | 67.5 | 66.9 | 66.4 | 64.9 | 63.6 | 61.7 | 61.3 | 60.9 | 64.1 | 0.0 | 64.1 | | |
| | 15 | 63.6 | 68.1 | 60.3 | 67.7 | 67.3 | 66.4 | 66.0 | 64.4 | 63.1 | 61.2 | 60.8 | 60.4 | 63.6 | 0.0 | 63.6 | | |
| | 16 | 63.5 | 68.1 | 60.3 | 67.8 | 67.5 | 66.7 | 65.8 | 64.0 | 62.9 | 61.1 | 60.8 | 60.4 | 63.5 | 0.0 | 63.5 | | |
| | 17 | 63.9 | 68.2 | 61.0 | 67.9 | 67.5 | 66.5 | 65.8 | 64.4 | 63.4 | 61.8 | 61.5 | 61.2 | 63.9 | 0.0 | 63.9 | | |
| | 18 | 64.6 | 69.1 | 61.4 | 68.8 | 68.5 | 67.7 | 66.9 | 65.3 | 64.1 | 62.3 | 61.9 | 61.5 | 64.6 | 0.0 | 64.6 | | |
| Evening | 19 | 65.5 | 70.6 | 62.4 | 70.2 | 69.8 | 68.5 | 67.7 | 66.0 | 64.9 | 63.2 | 62.8 | 62.5 | 65.5 | 5.0 | 70.5 | | |
| | 20 | 65.2 | 69.0 | 62.1 | 68.8 | 68.5 | 67.8 | 67.3 | 65.8 | 64.8 | 63.2 | 62.8 | 62.3 | 65.2 | 5.0 | 70.2 | | |
| | 21 | 65.0 | 69.2 | 61.7 | 68.9 | 68.7 | 68.0 | 67.3 | 65.8 | 64.5 | 62.6 | 62.2 | 61.8 | 65.0 | 5.0 | 70.0 | | |
| Night | 22 | 65.0 | 69.7 | 60.5 | 69.5 | 69.2 | 68.4 | 67.8 | 65.9 | 64.3 | 61.7 | 61.2 | 60.6 | 65.0 | 10.0 | 75.0 | | |
| | 23 | 64.5 | 68.9 | 60.6 | 68.6 | 68.4 | 67.8 | 67.2 | 65.3 | 64.0 | 61.6 | 61.2 | 60.7 | 64.5 | 10.0 | 74.5 | | |
| Timeframe | Hour | L_{eq} | L_{max} | L_{min} | L1% | L2% | L5% | L8% | L25% | L50% | L90% | L95% | L99% | L_{eq} (dBA) | | | | |
| Day | Min | 63.5 | 68.1 | 60.3 | 67.7 | 67.3 | 66.4 | 65.8 | 64.0 | 62.9 | 61.1 | 60.8 | 60.4 | 24-Hour | Daytime | Nighttime | | |
| | Max | 70.6 | 73.1 | 68.7 | 72.8 | 72.6 | 72.2 | 72.0 | 71.1 | 70.4 | 69.2 | 69.0 | 68.8 | | | | | |
| Energy Average | | 67.1 | Average: | | 70.0 | 69.7 | 68.9 | 68.4 | 67.1 | 66.0 | 64.4 | 64.0 | 63.7 | 67.066.867.2 | | | | |
| Evening | Min | 65.0 | 69.0 | 61.7 | 68.8 | 68.5 | 67.8 | 67.3 | 65.8 | 64.5 | 62.6 | 62.2 | 61.8 | | | | | |
| | Max | 65.5 | 70.6 | 62.4 | 70.2 | 69.8 | 68.5 | 67.7 | 66.0 | 64.9 | 63.2 | 62.8 | 62.5 | 24-Hour CNEL (dBA) | | | | |
| Energy Average | | 65.3 | Average: | | 69.3 | 69.0 | 68.1 | 67.4 | 65.9 | 64.7 | 63.0 | 62.6 | 62.2 | 73.8 | | | | |
| Night | Min | 63.3 | 68.9 | 54.5 | 68.6 | 68.4 | 67.6 | 66.9 | 63.8 | 60.5 | 56.4 | 55.5 | 54.7 | | | | | |
| | Max | 71.6 | 75.4 | 69.2 | 75.2 | 74.9 | 74.2 | 73.7 | 72.0 | 71.0 | 69.8 | 69.5 | 69.3 | | | | | |
| Energy Average | | 67.2 | Average: | | 71.3 | 71.0 | 70.1 | 69.4 | 66.9 | 64.8 | 62.0 | 61.4 | 60.9 | | | | | |

24-Hour Noise Level Measurement Summary

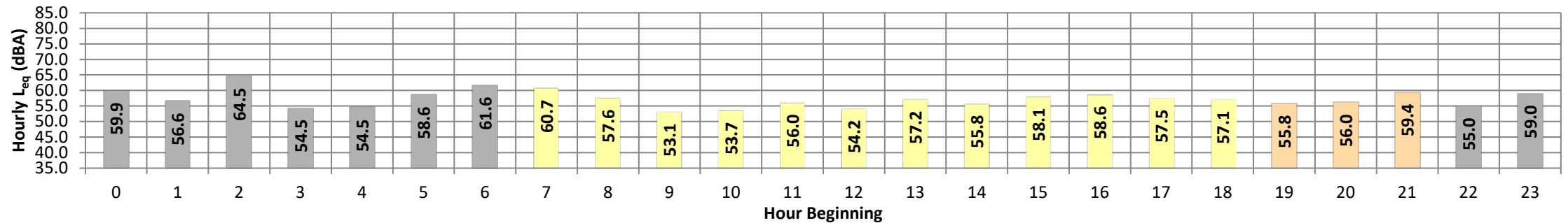
Date: Wednesday, July 15, 2020
Project: MA 20004 BRE SPACE CENTER

Location: L4 - Located northwest of the Project site on Universe Drive
near existing industrial uses at 308 Venture Drive.

Meter: Piccolo II

JN: 13575
Analyst: P. Mara

Hourly L_{eq} dBA Readings (unadjusted)



| Timeframe | Hour | L _{eq} | L _{max} | L _{min} | L1% | L2% | L5% | L8% | L25% | L50% | L90% | L95% | L99% | L _{eq} | Adj. | Adj. L _{eq} | | |
|----------------|------|-----------------|------------------|------------------|------|------|------|------|------|------|------|------|------|-----------------------|---------|----------------------|--|--|
| Night | 0 | 59.9 | 68.1 | 49.7 | 67.7 | 67.2 | 66.2 | 65.5 | 61.2 | 54.7 | 50.5 | 50.1 | 49.8 | 59.9 | 10.0 | 69.9 | | |
| | 1 | 56.6 | 64.7 | 48.8 | 64.3 | 63.8 | 62.6 | 61.6 | 56.9 | 52.9 | 50.1 | 49.6 | 49.0 | 56.6 | 10.0 | 66.6 | | |
| | 2 | 64.5 | 73.5 | 49.2 | 73.2 | 73.0 | 72.1 | 71.0 | 63.9 | 54.6 | 50.1 | 49.7 | 49.3 | 64.5 | 10.0 | 74.5 | | |
| | 3 | 54.5 | 62.2 | 51.1 | 61.5 | 60.5 | 58.3 | 57.1 | 54.8 | 53.0 | 51.6 | 51.4 | 51.2 | 54.5 | 10.0 | 64.5 | | |
| | 4 | 54.5 | 63.2 | 49.3 | 62.7 | 61.8 | 60.4 | 59.1 | 54.1 | 51.6 | 49.8 | 49.6 | 49.4 | 54.5 | 10.0 | 64.5 | | |
| | 5 | 58.6 | 67.5 | 50.4 | 66.9 | 66.5 | 65.0 | 63.7 | 59.1 | 52.7 | 50.9 | 50.7 | 50.5 | 58.6 | 10.0 | 68.6 | | |
| | 6 | 61.6 | 70.6 | 50.4 | 70.3 | 69.7 | 68.7 | 67.7 | 61.9 | 54.3 | 51.0 | 50.8 | 50.5 | 61.6 | 10.0 | 71.6 | | |
| Day | 7 | 60.7 | 69.5 | 50.0 | 69.0 | 68.6 | 67.1 | 65.8 | 60.1 | 57.1 | 50.8 | 50.5 | 50.1 | 60.7 | 0.0 | 60.7 | | |
| | 8 | 57.6 | 70.7 | 48.5 | 69.8 | 68.5 | 64.9 | 60.8 | 54.9 | 51.6 | 49.4 | 48.8 | 48.5 | 57.6 | 0.0 | 57.6 | | |
| | 9 | 53.1 | 62.5 | 47.5 | 62.0 | 61.1 | 59.1 | 57.3 | 52.6 | 50.3 | 48.2 | 47.9 | 47.6 | 53.1 | 0.0 | 53.1 | | |
| | 10 | 53.7 | 62.7 | 49.1 | 62.2 | 61.4 | 58.8 | 57.6 | 53.3 | 51.2 | 49.6 | 49.4 | 49.2 | 53.7 | 0.0 | 53.7 | | |
| | 11 | 56.0 | 65.3 | 49.2 | 64.9 | 64.2 | 62.4 | 60.7 | 55.8 | 52.6 | 49.8 | 49.5 | 49.3 | 56.0 | 0.0 | 56.0 | | |
| | 12 | 54.2 | 64.6 | 48.4 | 63.8 | 62.5 | 59.8 | 58.2 | 53.7 | 50.9 | 48.8 | 48.6 | 48.4 | 54.2 | 0.0 | 54.2 | | |
| | 13 | 57.2 | 64.7 | 53.2 | 64.2 | 63.6 | 62.0 | 60.9 | 57.2 | 55.3 | 53.7 | 53.5 | 53.3 | 57.2 | 0.0 | 57.2 | | |
| | 14 | 55.8 | 64.5 | 51.8 | 63.8 | 62.7 | 60.3 | 59.1 | 55.8 | 53.7 | 52.2 | 52.1 | 51.9 | 55.8 | 0.0 | 55.8 | | |
| | 15 | 58.1 | 67.2 | 54.4 | 66.4 | 65.3 | 62.6 | 60.8 | 57.8 | 56.2 | 54.9 | 54.7 | 54.4 | 58.1 | 0.0 | 58.1 | | |
| | 16 | 58.6 | 65.9 | 54.3 | 65.4 | 64.7 | 63.2 | 62.1 | 59.4 | 56.7 | 54.9 | 54.6 | 54.4 | 58.6 | 0.0 | 58.6 | | |
| | 17 | 57.5 | 64.7 | 54.6 | 64.1 | 63.0 | 61.1 | 60.2 | 57.5 | 56.4 | 55.2 | 55.0 | 54.7 | 57.5 | 0.0 | 57.5 | | |
| | 18 | 57.1 | 64.5 | 53.1 | 63.9 | 63.3 | 61.9 | 61.0 | 57.3 | 55.1 | 53.5 | 53.3 | 53.1 | 57.1 | 0.0 | 57.1 | | |
| Evening | 19 | 55.8 | 61.7 | 53.1 | 61.2 | 60.7 | 59.5 | 58.5 | 56.2 | 54.7 | 53.5 | 53.3 | 53.1 | 55.8 | 5.0 | 60.8 | | |
| | 20 | 56.0 | 63.1 | 53.0 | 62.7 | 61.8 | 60.2 | 59.3 | 55.9 | 54.5 | 53.5 | 53.3 | 53.1 | 56.0 | 5.0 | 61.0 | | |
| | 21 | 59.4 | 66.1 | 55.0 | 65.8 | 65.5 | 64.3 | 63.6 | 59.5 | 57.6 | 56.0 | 55.6 | 55.1 | 59.4 | 5.0 | 64.4 | | |
| Night | 22 | 55.0 | 63.6 | 51.5 | 62.8 | 61.7 | 59.2 | 57.9 | 55.0 | 53.2 | 52.0 | 51.8 | 51.6 | 55.0 | 10.0 | 65.0 | | |
| | 23 | 59.0 | 67.2 | 53.7 | 66.7 | 66.2 | 64.7 | 63.6 | 59.1 | 56.3 | 54.1 | 53.9 | 53.7 | 59.0 | 10.0 | 69.0 | | |
| Timeframe | Hour | L _{eq} | L _{max} | L _{min} | L1% | L2% | L5% | L8% | L25% | L50% | L90% | L95% | L99% | L _{eq} (dBA) | | | | |
| Day | Min | 53.1 | 62.5 | 47.5 | 62.0 | 61.1 | 58.8 | 57.3 | 52.6 | 50.3 | 48.2 | 47.9 | 47.6 | 24-Hour | Daytime | Nighttime | | |
| | Max | 60.7 | 70.7 | 54.6 | 69.8 | 68.6 | 67.1 | 65.8 | 60.1 | 57.1 | 55.2 | 55.0 | 54.7 | | | | | |
| Energy Average | | 57.1 | Average: | | 65.0 | 64.1 | 61.9 | 60.4 | 56.3 | 53.9 | 51.8 | 51.5 | 51.2 | 58.257.259.5 | | | | |
| Evening | Min | 55.8 | 61.7 | 53.0 | 61.2 | 60.7 | 59.5 | 58.5 | 55.9 | 54.5 | 53.5 | 53.3 | 53.1 | | | | | |
| | Max | 59.4 | 66.1 | 55.0 | 65.8 | 65.5 | 64.3 | 63.6 | 59.5 | 57.6 | 56.0 | 55.6 | 55.1 | 24-Hour CNEL (dBA) | | | | |
| Energy Average | | 57.4 | Average: | | 63.2 | 62.7 | 61.3 | 60.4 | 57.2 | 55.6 | 54.3 | 54.1 | 53.8 | 65.9 | | | | |
| Night | Min | 54.5 | 62.2 | 48.8 | 61.5 | 60.5 | 58.3 | 57.1 | 54.1 | 51.6 | 49.8 | 49.6 | 49.0 | | | | | |
| | Max | 64.5 | 73.5 | 53.7 | 73.2 | 73.0 | 72.1 | 71.0 | 63.9 | 56.3 | 54.1 | 53.9 | 53.7 | | | | | |
| Energy Average | | 59.5 | Average: | | 66.2 | 65.6 | 64.1 | 63.0 | 58.4 | 53.7 | 51.1 | 50.8 | 50.6 | | | | | |

24-Hour Noise Level Measurement Summary

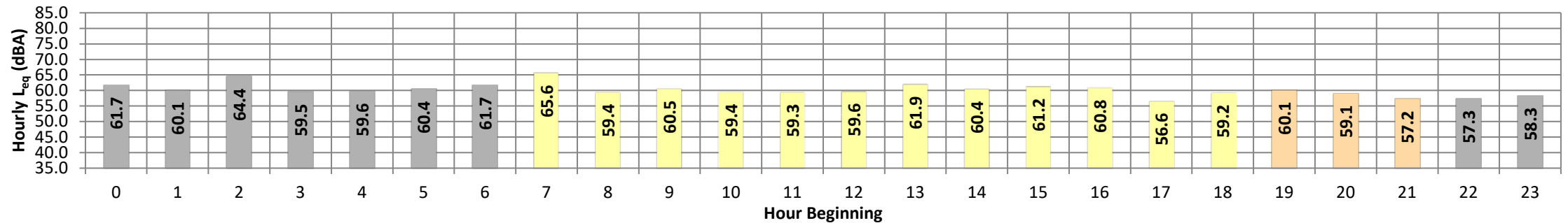
Date: Wednesday, July 15, 2020
Project: MA 20004 BRE SPACE CENTER

Location: L5 - Located north of the Project site on Manitou Court near existing industrial uses at 1011 Space Center Court.

Meter: Piccolo II

JN: 13575
Analyst: P. Mara

Hourly L_{eq} dBA Readings (unadjusted)



| Timeframe | Hour | L _{eq} | L _{max} | L _{min} | L1% | L2% | L5% | L8% | L25% | L50% | L90% | L95% | L99% | L _{eq} | Adj. | Adj. L _{eq} | | |
|----------------|------|-----------------|------------------|------------------|------|------|------|------|------|------|------|------|------|-----------------------|---------|----------------------|--|--|
| Night | 0 | 61.7 | 69.0 | 56.0 | 68.7 | 68.1 | 66.7 | 65.8 | 62.7 | 59.3 | 56.7 | 56.4 | 56.1 | 61.7 | 10.0 | 71.7 | | |
| | 1 | 60.1 | 67.2 | 56.2 | 66.7 | 66.3 | 64.9 | 63.9 | 60.3 | 58.1 | 56.7 | 56.5 | 56.3 | 60.1 | 10.0 | 70.1 | | |
| | 2 | 64.4 | 72.8 | 56.9 | 72.3 | 71.7 | 70.6 | 69.7 | 64.9 | 60.2 | 57.5 | 57.3 | 57.1 | 64.4 | 10.0 | 74.4 | | |
| | 3 | 59.5 | 66.2 | 56.4 | 65.8 | 65.3 | 64.1 | 63.2 | 59.3 | 58.1 | 56.8 | 56.7 | 56.5 | 59.5 | 10.0 | 69.5 | | |
| | 4 | 59.6 | 67.7 | 55.1 | 67.1 | 66.5 | 65.1 | 63.6 | 59.9 | 56.9 | 55.6 | 55.4 | 55.2 | 59.6 | 10.0 | 69.6 | | |
| | 5 | 60.4 | 69.6 | 49.8 | 69.3 | 68.7 | 67.8 | 66.4 | 59.9 | 53.1 | 50.7 | 50.4 | 50.0 | 60.4 | 10.0 | 70.4 | | |
| | 6 | 61.7 | 70.6 | 50.4 | 70.2 | 69.8 | 68.4 | 67.4 | 61.8 | 55.1 | 51.5 | 51.1 | 50.7 | 61.7 | 10.0 | 71.7 | | |
| Day | 7 | 65.6 | 74.5 | 52.0 | 74.1 | 73.5 | 72.9 | 72.2 | 64.5 | 58.8 | 54.0 | 52.9 | 52.2 | 65.6 | 0.0 | 65.6 | | |
| | 8 | 59.4 | 69.0 | 50.4 | 68.5 | 67.8 | 66.5 | 64.9 | 58.4 | 54.3 | 51.4 | 51.0 | 50.6 | 59.4 | 0.0 | 59.4 | | |
| | 9 | 60.5 | 70.3 | 51.2 | 69.8 | 69.1 | 67.2 | 65.7 | 60.0 | 56.2 | 52.1 | 51.8 | 51.3 | 60.5 | 0.0 | 60.5 | | |
| | 10 | 59.4 | 70.0 | 49.2 | 69.6 | 68.9 | 66.7 | 65.1 | 58.3 | 52.7 | 50.2 | 49.9 | 49.4 | 59.4 | 0.0 | 59.4 | | |
| | 11 | 59.3 | 70.3 | 49.2 | 69.7 | 68.9 | 67.0 | 65.3 | 57.7 | 52.7 | 50.1 | 49.8 | 49.4 | 59.3 | 0.0 | 59.3 | | |
| | 12 | 59.6 | 69.6 | 51.4 | 69.1 | 68.4 | 66.7 | 65.2 | 58.4 | 54.8 | 52.3 | 52.0 | 51.6 | 59.6 | 0.0 | 59.6 | | |
| | 13 | 61.9 | 72.4 | 50.9 | 72.0 | 71.2 | 69.0 | 66.8 | 61.3 | 56.0 | 51.8 | 51.4 | 51.1 | 61.9 | 0.0 | 61.9 | | |
| | 14 | 60.4 | 71.3 | 49.4 | 70.7 | 69.6 | 67.5 | 65.8 | 59.5 | 54.1 | 50.3 | 50.0 | 49.6 | 60.4 | 0.0 | 60.4 | | |
| | 15 | 61.2 | 71.0 | 50.1 | 70.5 | 69.9 | 68.5 | 66.9 | 60.7 | 54.6 | 51.1 | 50.7 | 50.3 | 61.2 | 0.0 | 61.2 | | |
| | 16 | 60.8 | 71.1 | 52.1 | 70.6 | 70.0 | 68.1 | 66.1 | 58.9 | 55.4 | 53.0 | 52.7 | 52.3 | 60.8 | 0.0 | 60.8 | | |
| | 17 | 56.6 | 64.6 | 51.7 | 64.3 | 63.8 | 62.4 | 60.6 | 56.1 | 54.2 | 52.6 | 52.3 | 51.9 | 56.6 | 0.0 | 56.6 | | |
| | 18 | 59.2 | 69.2 | 51.6 | 68.8 | 68.1 | 65.7 | 64.3 | 58.2 | 54.6 | 52.6 | 52.2 | 51.8 | 59.2 | 0.0 | 59.2 | | |
| Evening | 19 | 60.1 | 70.6 | 51.3 | 70.3 | 70.0 | 68.1 | 66.0 | 56.6 | 53.8 | 52.3 | 52.0 | 51.5 | 60.1 | 5.0 | 65.1 | | |
| | 20 | 59.1 | 68.4 | 51.5 | 68.2 | 67.8 | 66.4 | 64.8 | 57.4 | 53.8 | 52.3 | 52.1 | 51.7 | 59.1 | 5.0 | 64.1 | | |
| | 21 | 57.2 | 67.1 | 50.8 | 66.6 | 66.1 | 64.4 | 62.6 | 55.4 | 53.0 | 51.6 | 51.4 | 50.9 | 57.2 | 5.0 | 62.2 | | |
| Night | 22 | 57.3 | 66.6 | 50.2 | 66.3 | 65.8 | 64.5 | 63.1 | 55.6 | 52.4 | 51.1 | 50.8 | 50.4 | 57.3 | 10.0 | 67.3 | | |
| | 23 | 58.3 | 67.6 | 49.8 | 67.3 | 66.9 | 65.8 | 64.3 | 57.0 | 52.5 | 50.6 | 50.4 | 50.0 | 58.3 | 10.0 | 68.3 | | |
| Timeframe | Hour | L _{eq} | L _{max} | L _{min} | L1% | L2% | L5% | L8% | L25% | L50% | L90% | L95% | L99% | L _{eq} (dBA) | | | | |
| Day | Min | 56.6 | 64.6 | 49.2 | 64.3 | 63.8 | 62.4 | 60.6 | 56.1 | 52.7 | 50.1 | 49.8 | 49.4 | 24-Hour | Daytime | Nighttime | | |
| | Max | 65.6 | 74.5 | 52.1 | 74.1 | 73.5 | 72.9 | 72.2 | 64.5 | 58.8 | 54.0 | 52.9 | 52.3 | | | | | |
| Energy Average | | 60.9 | Average: | | 69.8 | 69.1 | 67.3 | 65.7 | 59.3 | 54.9 | 51.8 | 51.4 | 51.0 | 60.660.560.8 | | | | |
| Evening | Min | 57.2 | 67.1 | 50.8 | 66.6 | 66.1 | 64.4 | 62.6 | 55.4 | 53.0 | 51.6 | 51.4 | 50.9 | | | | | |
| | Max | 60.1 | 70.6 | 51.5 | 70.3 | 70.0 | 68.1 | 66.0 | 57.4 | 53.8 | 52.3 | 52.1 | 51.7 | 24-Hour CNEL (dBA) | | | | |
| Energy Average | | 59.0 | Average: | | 68.4 | 67.9 | 66.3 | 64.4 | 56.5 | 53.5 | 52.1 | 51.8 | 51.4 | 67.4 | | | | |
| Night | Min | 57.3 | 66.2 | 49.8 | 65.8 | 65.3 | 64.1 | 63.1 | 55.6 | 52.4 | 50.6 | 50.4 | 50.0 | | | | | |
| | Max | 64.4 | 72.8 | 56.9 | 72.3 | 71.7 | 70.6 | 69.7 | 64.9 | 60.2 | 57.5 | 57.3 | 57.1 | | | | | |
| Energy Average | | 60.8 | Average: | | 68.2 | 67.7 | 66.4 | 65.3 | 60.2 | 56.2 | 54.1 | 53.9 | 53.6 | | | | | |

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APPENDIX 7.1:

OFF-SITE TRAFFIC NOISE CONTOURS

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Monday, December 21, 2020

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| FHWA-RD-77-108 HIGHWAY NOISE PREDICTION MODEL | | | | | | | | | |
|---|-------|----------------|----------|-------------|--|---------------|------------|-------|-------|
| Scenario: Background 2022 + Project Road Name: C St. Road Segment: n/o Iberia St. | | | | | Project Name: BRE Space Mira Loma Job Number: 13575 | | | | |
| SITE SPECIFIC INPUT DATA | | | | | NOISE MODEL INPUTS | | | | |
| Highway Data | | | | | Site Conditions (Hard = 10, Soft = 15) | | | | |
| Average Daily Traffic (Adt): | | 1,551 vehicles | | | Autos: 15 | | | | |
| Peak Hour Percentage: | | 6.99% | | | Medium Trucks (2 Axles): 15 | | | | |
| Peak Hour Volume: | | 109 vehicles | | | Heavy Trucks (3+ Axles): 15 | | | | |
| Vehicle Speed: | | 40 mph | | | | | | | |
| Near/Far Lane Distance: | | 24 feet | | | | | | | |
| Site Data | | | | | Vehicle Mix | | | | |
| | | | | | Vehicle Type | Day | Evening | Night | Daily |
| Barrier Height: | | 0.0 feet | | | Autos: 77.5% 12.9% 9.6% 62.79% | | | | |
| Barrier Type (0-Wall, 1-Berm): | | 0.0 | | | Medium Trucks: 84.8% 4.9% 10.3% 11.37% | | | | |
| Centerline Dist. to Barrier: | | 39.0 feet | | | Heavy Trucks: 86.5% 2.7% 10.8% 25.84% | | | | |
| Centerline Dist. to Observer: | | 39.0 feet | | | | | | | |
| Barrier Distance to Observer: | | 0.0 feet | | | | | | | |
| Observer Height (Above Pad): | | 5.0 feet | | | | | | | |
| Pad Elevation: | | 0.0 feet | | | Autos: 0.000 | | | | |
| Road Elevation: | | 0.0 feet | | | Medium Trucks: 2.297 | | | | |
| Road Grade: | | 0.0% | | | Heavy Trucks: 8.004 Grade Adjustment: 0.0 | | | | |
| Left View: | | -90.0 degrees | | | | | | | |
| Right View: | | 90.0 degrees | | | | | | | |
| FHWA Noise Model Calculations | | | | | | | | | |
| Vehicle Type | RECEL | Traffic Flow | Distance | Finite Road | Fresnel | Barrier Atten | Berm Atten | | |
| Autos: | 66.51 | -12.99 | 1.78 | -1.20 | -4.58 | 0.000 | 0.000 | | |
| Medium Trucks: | 77.72 | -20.41 | 1.82 | -1.20 | -4.87 | 0.000 | 0.000 | | |
| Heavy Trucks: | 82.99 | -16.85 | 1.82 | -1.20 | -5.57 | 0.000 | 0.000 | | |

| Unmitigated Noise Levels (without Topo and barrier attenuation) | | | | | | |
|---|---------------|---------|-------------|-----------|------|-------|
| VehicleType | Leq Peak Hour | Leq Day | Leq Evening | Leq Night | Ldn | CNEL |
| Autos: | 54.1 | 53.8 | 52.0 | 45.9 | 54.6 | 55.25 |
| Medium Trucks: | 57.9 | 58.0 | 51.6 | 50.1 | 58.5 | 58.88 |
| Heavy Trucks: | 66.8 | 66.9 | 57.9 | 59.1 | 67.5 | 67.66 |
| Vehicle Noise: | 67.5 | 67.6 | 59.6 | 59.8 | 68.2 | 68.33 |
| Centerline Distance to Noise Contour (in feet) | | | | | | |
| | 70 dBA | 65 dBA | 60 dBA | 55 dBA | | |
| Ldn: | 29 | 64 | 137 | 295 | | |
| CNEL: | 30 | 65 | 140 | 302 | | |

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| FHWA-RD-77-108 HIGHWAY NOISE PREDICTION MODEL | | | | | | | | | |
|---|---------------|--------------|-------------|-------------|--|---------------|------------|-------|-------|
| Scenario: Background 2022 + Project Road Name: Etiwanda Av. Road Segment: n/o Hopkins St. | | | | | Project Name: BRE Space Mira Loma Job Number: 13575 | | | | |
| SITE SPECIFIC INPUT DATA | | | | | NOISE MODEL INPUTS | | | | |
| Highway Data | | | | | Site Conditions (Hard = 10, Soft = 15) | | | | |
| Average Daily Traffic (Adt): 34,881 vehicles | | | | | Autos: 15 | | | | |
| Peak Hour Percentage: 6.99% | | | | | Medium Trucks (2 Axles): 15 | | | | |
| Peak Hour Volume: 2,440 vehicles | | | | | Heavy Trucks (3+ Axles): 15 | | | | |
| Vehicle Speed: 55 mph | | | | | Vehicle Mix | | | | |
| Near/Far Lane Distance: 78 feet | | | | | VehicleType | Day | Evening | Night | Daily |
| Site Data | | | | | Autos: 77.5% 12.9% 9.6% 53.60% | | | | |
| Barrier Height: 0.0 feet | | | | | Medium Trucks: 84.8% 4.9% 10.3% 14.47% | | | | |
| Barrier Type (0-Wall, 1-Berm): 0.0 | | | | | Heavy Trucks: 86.5% 2.7% 10.8% 31.93% | | | | |
| Centerline Dist. to Barrier: 76.0 feet | | | | | Noise Source Elevations (in feet) | | | | |
| Centerline Dist. to Observer: 76.0 feet | | | | | Autos: 0.000 | | | | |
| Barrier Distance to Observer: 0.0 feet | | | | | Medium Trucks: 2.297 | | | | |
| Observer Height (Above Pad): 5.0 feet | | | | | Heavy Trucks: 8.004 Grade Adjustment: 0.0 | | | | |
| Pad Elevation: 0.0 feet | | | | | Noise Source Elevations (in feet) | | | | |
| Road Elevation: 0.0 feet | | | | | Autos: 65.422 | | | | |
| Road Grade: 0.0% | | | | | Medium Trucks: 65.286 | | | | |
| Left View: -90.0 degrees | | | | | Heavy Trucks: 65.299 | | | | |
| Right View: 90.0 degrees | | | | | | | | | |
| FHWA Noise Model Calculations | | | | | | | | | |
| VehicleType | REMEL | Traffic Flow | Distance | Finite Road | Fresnel | Barrier Atten | Berm Atten | | |
| Autos: | 71.78 | -1.54 | -1.85 | -1.20 | -4.73 | 0.000 | 0.000 | | |
| Medium Trucks: | 82.40 | -7.23 | -1.84 | -1.20 | -4.88 | 0.000 | 0.000 | | |
| Heavy Trucks: | 86.40 | -3.79 | -1.84 | -1.20 | -5.25 | 0.000 | 0.000 | | |
| Unmitigated Noise Levels (without Topo and barrier attenuation) | | | | | | | | | |
| VehicleType | Leq Peak Hour | Leq Day | Leq Evening | Leq Night | Ldn | CNEL | | | |
| Autos: | 67.2 | 66.8 | 65.1 | 59.0 | 67.6 | 68.2 | | | |
| Medium Trucks: | 72.1 | 72.2 | 65.8 | 64.3 | 72.7 | 73.0 | | | |
| Heavy Trucks: | 79.6 | 79.7 | 70.7 | 71.9 | 80.3 | 80.4 | | | |
| Vehicle Noise: | 80.5 | 80.6 | 72.7 | 72.8 | 81.2 | 81.3 | | | |
| Centerline Distance to Noise Contour (in feet) | | | | | | | | | |
| | | | | 70 dBA | 65 dBA | 60 dBA | 55 dBA | | |
| Ldn: | | | | 422 | 909 | 1,957 | 4,217 | | |
| CNEL: | | | | 433 | 932 | 2,008 | 4,325 | | |

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| FHWA-RD-77-108 HIGHWAY NOISE PREDICTION MODEL | | | | | | | | | |
|---|---------------|----------------|-------------|--|---------|---------------|------------|-----------------------|--------|
| Scenario: Background + CP + P | | | | Project Name: BRE Space Mira Loma | | | | | |
| Road Name: Iberia St. | | | | Job Number: 13575 | | | | | |
| Road Segment: e/o C St. | | | | | | | | | |
| SITE SPECIFIC INPUT DATA | | | | NOISE MODEL INPUTS | | | | | |
| Highway Data | | | | Site Conditions (Hard = 10, Soft = 15) | | | | | |
| Average Daily Traffic (Adt): | | 2,015 vehicles | | Autos: | | 15 | | | |
| Peak Hour Percentage: | | 6.99% | | Medium Trucks (2 Axles): | | 15 | | | |
| Peak Hour Volume: | | 141 vehicles | | Heavy Trucks (3+ Axles): | | 15 | | | |
| Vehicle Speed: | | 40 mph | | Vehicle Mix | | | | | |
| Near/Far Lane Distance: | | 24 feet | | | | | | | |
| Site Data | | | | Vehicle Type | | Day | Evening | Night | Daily |
| Barrier Height: | | 0.0 feet | | Autos: | | 77.5% | 12.9% | 9.6% | 60.67% |
| Barrier Type (0-Wall, 1-Berm): | | 0.0 | | Medium Trucks: | | 84.8% | 4.9% | 10.3% | 12.10% |
| Centerline Dist. to Barrier: | | 39.0 feet | | Heavy Trucks: | | 86.5% | 2.7% | 10.8% | 27.24% |
| Centerline Dist. to Observer: | | 39.0 feet | | Noise Source Elevations (in feet) | | | | | |
| Barrier Distance to Observer: | | 0.0 feet | | | | | | | |
| Observer Height (Above Pad): | | 5.0 feet | | Autos: | | 0.000 | | | |
| Pad Elevation: | | 0.0 feet | | Medium Trucks: | | 2.297 | | | |
| Road Elevation: | | 0.0 feet | | Heavy Trucks: | | 8.004 | | Grade Adjustment: 0.0 | |
| Road Grade: | | 0.0% | | Lane Equivalent Distance (in feet) | | | | | |
| Left View: | | -90.0 degrees | | | | | | | |
| Right View: | | 90.0 degrees | | Autos: | | 37.443 | | | |
| | | | | Medium Trucks: | | 37.206 | | | |
| | | | | Heavy Trucks: | | 37.229 | | | |
| FHWA Noise Model Calculations | | | | | | | | | |
| VehicleType | REMEL | Traffic Flow | Distance | Finite Road | Fresnel | Barrier Atten | Berm Atten | | |
| Autos: | 66.51 | -12.01 | 1.78 | -1.20 | -4.58 | 0.000 | 0.000 | | |
| Medium Trucks: | 77.72 | -19.01 | 1.82 | -1.20 | -4.87 | 0.000 | 0.000 | | |
| Heavy Trucks: | 82.99 | -15.48 | 1.82 | -1.20 | -5.57 | 0.000 | 0.000 | | |
| Unmitigated Noise Levels (without Topo and barrier attenuation) | | | | | | | | | |
| VehicleType | Leq Peak Hour | Leq Day | Leq Evening | Leq Night | Ldn | CNEL | | | |
| Autos: | 55.1 | 54.7 | 53.0 | 46.9 | 55.5 | 56.1 | | | |
| Medium Trucks: | 59.3 | 59.4 | 53.0 | 51.5 | 59.9 | 60.2 | | | |
| Heavy Trucks: | 68.1 | 68.3 | 59.2 | 60.5 | 68.8 | 69.0 | | | |
| Vehicle Noise: | 68.9 | 69.0 | 60.9 | 61.2 | 69.5 | 69.7 | | | |
| Centerline Distance to Noise Contour (in feet) | | | | | | | | | |
| | | | 70 dBA | 65 dBA | 60 dBA | 55 dBA | | | |
| Ldn: | | | 36 | 78 | 168 | 363 | | | |
| CNEL: | | | 37 | 80 | 173 | 372 | | | |

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| FHWA-RD-77-108 HIGHWAY NOISE PREDICTION MODEL | | | | | | | | | |
|---|---------------|----------------|-------------|--|---------|---------------|------------|-----------------------|--------|
| Scenario: Background + CP + P | | | | Project Name: BRE Space Mira Loma | | | | | |
| Road Name: Hopkins St. | | | | Job Number: 13575 | | | | | |
| Road Segment: w/o Etiwanda Av. | | | | | | | | | |
| SITE SPECIFIC INPUT DATA | | | | NOISE MODEL INPUTS | | | | | |
| Highway Data | | | | Site Conditions (Hard = 10, Soft = 15) | | | | | |
| Average Daily Traffic (Adt): | | 3,029 vehicles | | Autos: | | 15 | | | |
| Peak Hour Percentage: | | 6.99% | | Medium Trucks (2 Axles): | | 15 | | | |
| Peak Hour Volume: | | 212 vehicles | | Heavy Trucks (3+ Axles): | | 15 | | | |
| Vehicle Speed: | | 15 mph | | Vehicle Mix | | | | | |
| Near/Far Lane Distance: | | 24 feet | | | | | | | |
| Site Data | | | | Vehicle Type | | Day | Evening | Night | Daily |
| Barrier Height: | | 0.0 feet | | Autos: | | 77.5% | 12.9% | 9.6% | 53.70% |
| Barrier Type (0-Wall, 1-Berm): | | 0.0 | | Medium Trucks: | | 84.8% | 4.9% | 10.3% | 14.07% |
| Centerline Dist. to Barrier: | | 39.0 feet | | Heavy Trucks: | | 86.5% | 2.7% | 10.8% | 32.23% |
| Centerline Dist. to Observer: | | 39.0 feet | | Noise Source Elevations (in feet) | | | | | |
| Barrier Distance to Observer: | | 0.0 feet | | | | | | | |
| Observer Height (Above Pad): | | 5.0 feet | | Autos: | | 0.000 | | | |
| Pad Elevation: | | 0.0 feet | | Medium Trucks: | | 2.297 | | | |
| Road Elevation: | | 0.0 feet | | Heavy Trucks: | | 8.004 | | Grade Adjustment: 0.0 | |
| Road Grade: | | 0.0% | | Lane Equivalent Distance (in feet) | | | | | |
| Left View: | | -90.0 degrees | | | | | | | |
| Right View: | | 90.0 degrees | | Autos: | | 37.443 | | | |
| | | | | Medium Trucks: | | 37.206 | | | |
| | | | | Heavy Trucks: | | 37.229 | | | |
| FHWA Noise Model Calculations | | | | | | | | | |
| VehicleType | REMEL | Traffic Flow | Distance | Finite Road | Fresnel | Barrier Atten | Berm Atten | | |
| Autos: | 50.28 | -6.51 | 1.78 | -1.20 | -4.58 | 0.000 | 0.000 | | |
| Medium Trucks: | 63.27 | -12.32 | 1.82 | -1.20 | -4.87 | 0.000 | 0.000 | | |
| Heavy Trucks: | 72.52 | -8.72 | 1.82 | -1.20 | -5.57 | 0.000 | 0.000 | | |
| Unmitigated Noise Levels (without Topo and barrier attenuation) | | | | | | | | | |
| VehicleType | Leq Peak Hour | Leq Day | Leq Evening | Leq Night | Ldn | CNEL | | | |
| Autos: | 44.4 | 44.0 | 42.2 | 36.2 | 44.8 | 45.4 | | | |
| Medium Trucks: | 51.6 | 51.6 | 45.3 | 43.7 | 52.2 | 52.4 | | | |
| Heavy Trucks: | 64.4 | 64.5 | 55.5 | 56.8 | 65.1 | 65.2 | | | |
| Vehicle Noise: | 64.7 | 64.8 | 56.1 | 57.0 | 65.4 | 65.5 | | | |
| Centerline Distance to Noise Contour (in feet) | | | | | | | | | |
| | | | | 70 dBA | 65 dBA | 60 dBA | 55 dBA | | |
| Ldn: | | | | 19 | 41 | 89 | 191 | | |
| CNEL: | | | | 20 | 42 | 91 | 195 | | |

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APPENDIX 9.1:

CADNAA OPERATIONAL NOISE MODEL INPUTS

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13575 -BRE Space Mira Loma

CadnaA Noise Prediction Model: 13575-03.cna

Date: 24.06.21

Analyst: B. Lawson

Calculation Configuration

| Configuration | |
|--------------------------------------|--------------------------------|
| Parameter | Value |
| General | |
| Country | (user defined) |
| Max. Error (dB) | 0.00 |
| Max. Search Radius (#(Unit,LEN)) | 2000.01 |
| Min. Dist Src to Rcvr | 0.00 |
| Partition | |
| Raster Factor | 0.50 |
| Max. Length of Section (#(Unit,LEN)) | 999.99 |
| Min. Length of Section (#(Unit,LEN)) | 1.01 |
| Min. Length of Section (%) | 0.00 |
| Proj. Line Sources | On |
| Proj. Area Sources | On |
| Ref. Time | |
| Reference Time Day (min) | 960.00 |
| Reference Time Night (min) | 480.00 |
| Daytime Penalty (dB) | 0.00 |
| Recr. Time Penalty (dB) | 5.00 |
| Night-time Penalty (dB) | 10.00 |
| DTM | |
| Standard Height (m) | 0.00 |
| Model of Terrain | Triangulation |
| Reflection | |
| max. Order of Reflection | 2 |
| Search Radius Src | 100.00 |
| Search Radius Rcvr | 100.00 |
| Max. Distance Source - Rcvr | 1000.00 1000.00 |
| Min. Distance Rcvr - Reflector | 1.00 1.00 |
| Min. Distance Source - Reflector | 0.10 |
| Industrial (ISO 9613) | |
| Lateral Diffraction | some Obj |
| Obst. within Area Src do not shield | On |
| Screening | Incl. Ground Att. over Barrier |
| | Dz with limit (20/25) |
| Barrier Coefficients C1,2,3 | 3.0 20.0 0.0 |
| Temperature (#(Unit,TEMP)) | 10 |
| rel. Humidity (%) | 70 |
| Ground Absorption G | 0.50 |
| Wind Speed for Dir. (#(Unit,SPEED)) | 3.0 |
| Roads (RLS-90) | |
| Strictly acc. to RLS-90 | |
| Railways (FTA/FRA) | |
| Aircraft (???) | |
| Strictly acc. to AzB | |

Receiver Noise Levels

| Name | M. | ID | Level Lr | | | Limit. Value | | | Land Use | | | Height | Coordinates | | |
|-----------|----|------|----------|-------|-------|--------------|-------|-------|----------|------|------------|--------|-------------|------------|------|
| | | | Day | Night | CNEL | Day | Night | CNEL | Type | Auto | Noise Type | | X | Y | Z |
| | | | (dBA) | (dBA) | (dBA) | (dBA) | (dBA) | (dBA) | | | | (ft) | (ft) | (ft) | (ft) |
| RECEIVERS | R1 | 42.9 | 41.9 | 48.3 | 55.0 | 45.0 | 0.0 | 0.0 | | | | 5.00 a | 6175558.12 | 2318277.05 | 5.00 |
| RECEIVERS | R2 | 38.0 | 37.2 | 43.7 | 55.0 | 45.0 | 0.0 | 0.0 | | | | 5.00 a | 6167131.81 | 2319797.25 | 5.00 |

Point Source(s)

| Name | M. | ID | Result. PWL | | | Lw / Li | | Operating Time | | | K0 | Height | Coordinates | | | |
|-------------|----|-----------|-------------|---------|-------|---------|-------|----------------|--------|---------|--------|--------|-------------|------------|------------|-------|
| | | | Day | Evening | Night | Type | Value | norm. | Day | Special | Night | | | X | Y | Z |
| | | | (dBA) | (dBA) | (dBA) | | | dB(A) | (min) | (min) | (min) | (dB) | (ft) | (ft) | (ft) | (ft) |
| POINTSOURCE | | TRASH04 | 89.0 | 89.0 | 89.0 | Lw | 89.0 | | 75.00 | 0.00 | 45.00 | 0.0 | 5.00 a | 6173028.35 | 2318828.20 | 5.00 |
| POINTSOURCE | | TRASH03 | 89.0 | 89.0 | 89.0 | Lw | 89.0 | | 75.00 | 0.00 | 45.00 | 0.0 | 5.00 a | 6173797.77 | 2318776.80 | 5.00 |
| POINTSOURCE | | TRASH02 | 89.0 | 89.0 | 89.0 | Lw | 89.0 | | 75.00 | 0.00 | 45.00 | 0.0 | 5.00 a | 6173804.49 | 2319683.87 | 5.00 |
| POINTSOURCE | | TRASH01 | 89.0 | 89.0 | 89.0 | Lw | 89.0 | | 75.00 | 0.00 | 45.00 | 0.0 | 5.00 a | 6173072.11 | 2319741.39 | 5.00 |
| POINTSOURCE | | AC01 | 88.9 | 88.9 | 88.9 | Lw | 88.9 | | 585.00 | 0.00 | 252.00 | 0.0 | 5.00 g | 6173197.97 | 2318953.96 | 50.00 |
| POINTSOURCE | | AC02 | 88.9 | 88.9 | 88.9 | Lw | 88.9 | | 585.00 | 0.00 | 252.00 | 0.0 | 5.00 g | 6174524.56 | 2318921.97 | 50.00 |
| POINTSOURCE | | PARKING01 | 79.0 | 79.0 | 79.0 | Lw | 79 | | | | | 0.0 | 5.00 a | 6170332.93 | 2319477.06 | 5.00 |
| POINTSOURCE | | PARKING02 | 79.0 | 79.0 | 79.0 | Lw | 79 | | | | | 0.0 | 5.00 a | 6170334.11 | 2319372.02 | 5.00 |
| POINTSOURCE | | PARKING03 | 79.0 | 79.0 | 79.0 | Lw | 79 | | | | | 0.0 | 5.00 a | 6170393.13 | 2319420.41 | 5.00 |
| POINTSOURCE | | PARKING04 | 79.0 | 79.0 | 79.0 | Lw | 79 | | | | | 0.0 | 5.00 a | 6170453.32 | 2319480.60 | 5.00 |
| POINTSOURCE | | PARKING05 | 79.0 | 79.0 | 79.0 | Lw | 79 | | | | | 0.0 | 5.00 a | 6170446.24 | 2319318.91 | 5.00 |
| POINTSOURCE | | PARKING06 | 79.0 | 79.0 | 79.0 | Lw | 79 | | | | | 0.0 | 5.00 a | 6170515.87 | 2319388.55 | 5.00 |
| POINTSOURCE | | PARKING07 | 79.0 | 79.0 | 79.0 | Lw | 79 | | | | | 0.0 | 5.00 a | 6170580.79 | 2319472.34 | 5.00 |
| POINTSOURCE | | PARKING08 | 79.0 | 79.0 | 79.0 | Lw | 79 | | | | | 0.0 | 5.00 a | 6170579.61 | 2319351.96 | 5.00 |

| Name | M. | ID | Result. PWL | | | Lw / Li | | | Operating Time | | | KO | Height | Coordinates | | |
|-------------|----|-----------|-------------|---------|-------|---------|-------|-------|----------------|---------|-------|------|--------|--------------|------------|------|
| | | | Day | Evening | Night | Type | Value | norm. | Day | Special | Night | | | X | Y | Z |
| | | | (dBA) | (dBA) | (dBA) | | | dB(A) | (min) | (min) | (min) | (dB) | (ft) | (ft) | (ft) | (ft) |
| POINTSOURCE | | PARKING09 | 79.0 | 79.0 | 79.0 | Lw | 79 | | | | | 0.0 | 5.00 | a 6170579.61 | 2319241.01 | 5.00 |
| POINTSOURCE | | PARKING10 | 79.0 | 79.0 | 79.0 | Lw | 79 | | | | | 0.0 | 5.00 | a 6171049.34 | 2319605.71 | 5.00 |
| POINTSOURCE | | PARKING11 | 79.0 | 79.0 | 79.0 | Lw | 79 | | | | | 0.0 | 5.00 | a 6171049.34 | 2319512.47 | 5.00 |
| POINTSOURCE | | PARKING12 | 79.0 | 79.0 | 79.0 | Lw | 79 | | | | | 0.0 | 5.00 | a 6171048.16 | 2319419.23 | 5.00 |
| POINTSOURCE | | PARKING13 | 79.0 | 79.0 | 79.0 | Lw | 79 | | | | | 0.0 | 5.00 | a 6171048.16 | 2319318.91 | 5.00 |
| POINTSOURCE | | PARKING14 | 79.0 | 79.0 | 79.0 | Lw | 79 | | | | | 0.0 | 5.00 | a 6171045.80 | 2319215.05 | 5.00 |
| POINTSOURCE | | PARKING15 | 79.0 | 79.0 | 79.0 | Lw | 79 | | | | | 0.0 | 5.00 | a 6171043.44 | 2319108.83 | 5.00 |
| POINTSOURCE | | PARKING16 | 79.0 | 79.0 | 79.0 | Lw | 79 | | | | | 0.0 | 5.00 | a 6171018.66 | 2319756.78 | 5.00 |
| POINTSOURCE | | PARKING17 | 79.0 | 79.0 | 79.0 | Lw | 79 | | | | | 0.0 | 5.00 | a 6173143.42 | 2319743.91 | 5.00 |
| POINTSOURCE | | PARKING18 | 79.0 | 79.0 | 79.0 | Lw | 79 | | | | | 0.0 | 5.00 | a 6173262.68 | 2319743.91 | 5.00 |
| POINTSOURCE | | PARKING19 | 79.0 | 79.0 | 79.0 | Lw | 79 | | | | | 0.0 | 5.00 | a 6173402.17 | 2319739.87 | 5.00 |
| POINTSOURCE | | PARKING20 | 79.0 | 79.0 | 79.0 | Lw | 79 | | | | | 0.0 | 5.00 | a 6173293.01 | 2319596.34 | 5.00 |
| POINTSOURCE | | PARKING21 | 79.0 | 79.0 | 79.0 | Lw | 79 | | | | | 0.0 | 5.00 | a 6173286.94 | 2319485.16 | 5.00 |
| POINTSOURCE | | PARKING22 | 79.0 | 79.0 | 79.0 | Lw | 79 | | | | | 0.0 | 5.00 | a 6173284.92 | 2319363.87 | 5.00 |
| POINTSOURCE | | PARKING23 | 79.0 | 79.0 | 79.0 | Lw | 79 | | | | | 0.0 | 5.00 | a 6173282.90 | 2319218.32 | 5.00 |
| POINTSOURCE | | PARKING24 | 79.0 | 79.0 | 79.0 | Lw | 79 | | | | | 0.0 | 5.00 | a 6173276.84 | 2319040.43 | 5.00 |
| POINTSOURCE | | PARKING25 | 79.0 | 79.0 | 79.0 | Lw | 79 | | | | | 0.0 | 5.00 | a 6173125.22 | 2318807.96 | 5.00 |
| POINTSOURCE | | PARKING26 | 79.0 | 79.0 | 79.0 | Lw | 79 | | | | | 0.0 | 5.00 | a 6173250.56 | 2318803.92 | 5.00 |
| POINTSOURCE | | PARKING27 | 79.0 | 79.0 | 79.0 | Lw | 79 | | | | | 0.0 | 5.00 | a 6173367.80 | 2318801.90 | 5.00 |
| POINTSOURCE | | PARKING28 | 79.0 | 79.0 | 79.0 | Lw | 79 | | | | | 0.0 | 5.00 | a 6173624.53 | 2318795.83 | 5.00 |
| POINTSOURCE | | PARKING29 | 79.0 | 79.0 | 79.0 | Lw | 79 | | | | | 0.0 | 5.00 | a 6173723.58 | 2318795.83 | 5.00 |
| POINTSOURCE | | PARKING30 | 79.0 | 79.0 | 79.0 | Lw | 79 | | | | | 0.0 | 5.00 | a 6173343.54 | 2318953.51 | 5.00 |
| POINTSOURCE | | PARKING31 | 79.0 | 79.0 | 79.0 | Lw | 79 | | | | | 0.0 | 5.00 | a 6173349.61 | 2319149.59 | 5.00 |
| POINTSOURCE | | PARKING32 | 79.0 | 79.0 | 79.0 | Lw | 79 | | | | | 0.0 | 5.00 | a 6173347.59 | 2319295.14 | 5.00 |
| POINTSOURCE | | PARKING33 | 79.0 | 79.0 | 79.0 | Lw | 79 | | | | | 0.0 | 5.00 | a 6173357.69 | 2319438.66 | 5.00 |
| POINTSOURCE | | PARKING34 | 79.0 | 79.0 | 79.0 | Lw | 79 | | | | | 0.0 | 5.00 | a 6173351.63 | 2319547.82 | 5.00 |
| POINTSOURCE | | PARKING35 | 79.0 | 79.0 | 79.0 | Lw | 79 | | | | | 0.0 | 5.00 | a 6173565.91 | 2319594.32 | 5.00 |
| POINTSOURCE | | PARKING36 | 79.0 | 79.0 | 79.0 | Lw | 79 | | | | | 0.0 | 5.00 | a 6173671.03 | 2319693.37 | 5.00 |
| POINTSOURCE | | PARKING37 | 79.0 | 79.0 | 79.0 | Lw | 79 | | | | | 0.0 | 5.00 | a 6173624.53 | 2319483.14 | 5.00 |
| POINTSOURCE | | PARKING38 | 79.0 | 79.0 | 79.0 | Lw | 79 | | | | | 0.0 | 5.00 | a 6173559.84 | 2319402.28 | 5.00 |
| POINTSOURCE | | PARKING39 | 79.0 | 79.0 | 79.0 | Lw | 79 | | | | | 0.0 | 5.00 | a 6173628.57 | 2319317.37 | 5.00 |
| POINTSOURCE | | PARKING40 | 79.0 | 79.0 | 79.0 | Lw | 79 | | | | | 0.0 | 5.00 | a 6173551.76 | 2319272.90 | 5.00 |
| POINTSOURCE | | PARKING41 | 79.0 | 79.0 | 79.0 | Lw | 79 | | | | | 0.0 | 5.00 | a 6173616.45 | 2319157.68 | 5.00 |
| POINTSOURCE | | PARKING42 | 79.0 | 79.0 | 79.0 | Lw | 79 | | | | | 0.0 | 5.00 | a 6173612.40 | 2319006.07 | 5.00 |
| POINTSOURCE | | PARKING43 | 79.0 | 79.0 | 79.0 | Lw | 79 | | | | | 0.0 | 5.00 | a 6174501.86 | 2318787.75 | 5.00 |
| POINTSOURCE | | PARKING44 | 79.0 | 79.0 | 79.0 | Lw | 79 | | | | | 0.0 | 5.00 | a 6174606.97 | 2318787.75 | 5.00 |
| POINTSOURCE | | PARKING45 | 79.0 | 79.0 | 79.0 | Lw | 79 | | | | | 0.0 | 5.00 | a 6174542.29 | 2319669.11 | 5.00 |
| POINTSOURCE | | PARKING46 | 79.0 | 79.0 | 79.0 | Lw | 79 | | | | | 0.0 | 5.00 | a 6174637.30 | 2319618.58 | 5.00 |
| POINTSOURCE | | PARKING47 | 79.0 | 79.0 | 79.0 | Lw | 79 | | | | | 0.0 | 5.00 | a 6174594.85 | 2319428.56 | 5.00 |
| POINTSOURCE | | PARKING48 | 79.0 | 79.0 | 79.0 | Lw | 79 | | | | | 0.0 | 5.00 | a 6174647.40 | 2319311.31 | 5.00 |
| POINTSOURCE | | PARKING49 | 79.0 | 79.0 | 79.0 | Lw | 79 | | | | | 0.0 | 5.00 | a 6174588.78 | 2319173.85 | 5.00 |
| POINTSOURCE | | PARKING50 | 79.0 | 79.0 | 79.0 | Lw | 79 | | | | | 0.0 | 5.00 | a 6174643.36 | 2319074.80 | 5.00 |
| POINTSOURCE | | PARKING51 | 79.0 | 79.0 | 79.0 | Lw | 79 | | | | | 0.0 | 5.00 | a 6174586.76 | 2318993.94 | 5.00 |

Line Source(s)

| Name | M. | ID | Result. PWL | | | Result. PWL' | | | Lw / Li | | | Operating Time | | | Moving Pt. Src | | | Height | |
|------------|----|----------|-------------|---------|-------|--------------|---------|-------|---------|-------|-------|----------------|---------|-------|----------------|---------|-------|--------|------|
| | | | Day | Evening | Night | Day | Evening | Night | Type | Value | norm. | Day | Special | Night | Day | Number | Speed | | |
| | | | (dBA) | (dBA) | (dBA) | (dBA) | (dBA) | (dBA) | | dB(A) | | (min) | (min) | (min) | Day | Evening | Night | (mph) | (ft) |
| LINESOURCE | | DWY. 5&7 | 84.4 | 71.1 | 75.1 | 66.0 | 52.7 | 56.7 | PWL-Pt | 89.7 | | | | | 43.0 | 2.0 | 5.0 | 6.2 | 8 |
| LINESOURCE | | DWY. 7 | 87.1 | 74.1 | 77.1 | 62.7 | 49.7 | 52.7 | PWL-Pt | 89.7 | | | | | 20.0 | 1.0 | 2.0 | 6.2 | 8 |
| LINESOURCE | | DWY. 1 | 92.6 | 77.8 | 83.5 | 70.5 | 55.7 | 61.5 | PWL-Pt | 89.7 | | | | | 121.0 | 4.0 | 15.0 | 6.2 | 8 |
| LINESOURCE | | DWY. 1 | 90.2 | 75.4 | 81.1 | 70.5 | 55.7 | 61.5 | PWL-Pt | 89.7 | | | | | 121.0 | 4.0 | 15.0 | 6.2 | 8 |
| LINESOURCE | | DWY. 4 | 96.6 | 81.6 | 87.6 | 70.7 | 55.7 | 61.7 | PWL-Pt | 89.7 | | | | | 125.0 | 4.0 | 16.0 | 6.2 | 8 |
| LINESOURCE | | DWY. 4 | 85.9 | 71.0 | 77.0 | 70.7 | 55.7 | 61.7 | PWL-Pt | 89.7 | | | | | 125.0 | 4.0 | 16.0 | 6.2 | 8 |
| LINESOURCE | | DWY. 4 | 89.5 | 74.5 | 80.6 | 70.7 | 55.7 | 61.7 | PWL-Pt | 89.7 | | | | | 125.0 | 4.0 | 16.0 | 6.2 | 8 |

| Name | Height | | Coordinates | | | |
|------------|--------|------|-------------|------------|------|--------|
| | Begin | End | x | y | z | Ground |
| | (ft) | (ft) | (ft) | (ft) | (ft) | (ft) |
| LINESOURCE | 8.00 | a | 6174458.35 | 2319613.56 | 8.00 | 0.00 |
| | | | 6174521.56 | 2319606.29 | 8.00 | 0.00 |
| | | | 6174673.28 | 2319545.35 | 8.00 | 0.00 |
| LINESOURCE | 8.00 | a | 6174447.10 | 2318839.05 | 8.00 | 0.00 |
| | | | 6174612.76 | 2318836.58 | 8.00 | 0.00 |
| | | | 6174625.71 | 2319564.46 | 8.00 | 0.00 |
| LINESOURCE | 8.00 | a | 6173071.57 | 2319688.99 | 8.00 | 0.00 |
| | | | 6173244.77 | 2319688.98 | 8.00 | 0.00 |
| | | | 6173314.08 | 2319670.74 | 8.00 | 0.00 |
| | | | 6173481.89 | 2319662.23 | 8.00 | 0.00 |
| | | | 6173484.53 | 2319774.03 | 8.00 | 0.00 |
| LINESOURCE | 8.00 | a | 6173783.03 | 2319641.49 | 8.00 | 0.00 |
| | | | 6173481.89 | 2319662.23 | 8.00 | 0.00 |
| LINESOURCE | 8.00 | a | 6173481.89 | 2319662.23 | 8.00 | 0.00 |
| | | | 6173468.51 | 2319140.57 | 8.00 | 0.00 |
| | | | 6173487.97 | 2319033.57 | 8.00 | 0.00 |
| | | | 6173522.02 | 2318857.25 | 8.00 | 0.00 |

| Name | Height | | | Coordinates | | | |
|------------|--------|------|--|-------------|------------|------|--------|
| | Begin | End | | x | y | z | Ground |
| | (ft) | (ft) | | (ft) | (ft) | (ft) | (ft) |
| | | | | 6173058.76 | 2318859.69 | 8.00 | 0.00 |
| LINESOURCE | 8.00 | a | | 6173522.02 | 2318857.25 | 8.00 | 0.00 |
| | | | | 6173523.72 | 2318746.73 | 8.00 | 0.00 |
| LINESOURCE | 8.00 | a | | 6173771.82 | 2318851.23 | 8.00 | 0.00 |
| | | | | 6173522.02 | 2318857.25 | 8.00 | 0.00 |

Area Source(s)

| Name | M. | ID | Result. PWL | | | Result. PWL" | | | Lw / Li | | | Operating Time | | | Height (ft) |
|------------|----|-----------|-------------|---------|-------|--------------|---------|-------|---------|-------|-------|----------------|---------|--------|----------------|
| | | | Day | Evening | Night | Day | Evening | Night | Type | Value | norm. | Day | Special | Night | |
| | | | (dBA) | (dBA) | (dBA) | (dBA) | (dBA) | (dBA) | | | dB(A) | (min) | (min) | (min) | |
| AREASOURCE | | DOCK01 | 111.5 | 111.5 | 111.5 | 70.7 | 70.7 | 70.7 | Lw | 111.5 | | 900.00 | 0.00 | 540.00 | 8 |
| AREASOURCE | | DOCK02 | 111.5 | 111.5 | 111.5 | 70.0 | 70.0 | 70.0 | Lw | 111.5 | | 900.00 | 0.00 | 540.00 | 8 |
| AREASOURCE | | DOCK03 | 111.5 | 111.5 | 111.5 | 66.1 | 66.1 | 66.1 | Lw | 111.5 | | 900.00 | 0.00 | 540.00 | 8 |
| AREASOURCE | | DOCK04 | 111.5 | 111.5 | 111.5 | 66.1 | 66.1 | 66.1 | Lw | 111.5 | | 900.00 | 0.00 | 540.00 | 8 |
| AREASOURCE | | TRAILER01 | 103.4 | 103.4 | 103.4 | 61.6 | 61.6 | 61.6 | Lw | 103.4 | | | | | 8 |
| AREASOURCE | | TRAILER02 | 103.4 | 103.4 | 103.4 | 62.9 | 62.9 | 62.9 | Lw | 103.4 | | | | | 8 |

| Name | Height | | | Coordinates | | | |
|------------|--------|------|--|-------------|------------|------|--------|
| | Begin | End | | x | y | z | Ground |
| | (ft) | (ft) | | (ft) | (ft) | (ft) | (ft) |
| AREASOURCE | 8.00 | a | | 6173781.71 | 2319539.18 | 8.00 | 0.00 |
| | | | | 6173784.22 | 2319734.80 | 8.00 | 0.00 |
| | | | | 6174459.82 | 2319718.30 | 8.00 | 0.00 |
| | | | | 6174457.20 | 2319531.31 | 8.00 | 0.00 |
| AREASOURCE | 8.00 | a | | 6173770.77 | 2318949.16 | 8.00 | 0.00 |
| | | | | 6174445.79 | 2318939.91 | 8.00 | 0.00 |
| | | | | 6174448.73 | 2318712.98 | 8.00 | 0.00 |
| | | | | 6173773.14 | 2318729.39 | 8.00 | 0.00 |
| AREASOURCE | 8.00 | a | | 6173059.86 | 2318970.00 | 8.00 | 0.00 |
| | | | | 6173057.91 | 2318774.21 | 8.00 | 0.00 |
| | | | | 6171211.98 | 2318806.02 | 8.00 | 0.00 |
| | | | | 6171077.58 | 2318885.83 | 8.00 | 0.00 |
| | | | | 6171079.54 | 2318995.94 | 8.00 | 0.00 |
| AREASOURCE | 8.00 | a | | 6173072.54 | 2319783.95 | 8.00 | 0.00 |
| | | | | 6173070.67 | 2319601.28 | 8.00 | 0.00 |
| | | | | 6171087.11 | 2319629.38 | 8.00 | 0.00 |
| | | | | 6171087.32 | 2319790.03 | 8.00 | 0.00 |
| | | | | 6171197.55 | 2319788.58 | 8.00 | 0.00 |
| | | | | 6171262.40 | 2319793.71 | 8.00 | 0.00 |
| | | | | 6171293.03 | 2319796.39 | 8.00 | 0.00 |
| | | | | 6171293.03 | 2319826.77 | 8.00 | 0.00 |
| AREASOURCE | 8.00 | a | | 6171211.98 | 2318806.02 | 8.00 | 0.00 |
| | | | | 6171969.41 | 2318790.09 | 8.00 | 0.00 |
| | | | | 6171962.47 | 2318362.05 | 8.00 | 0.00 |
| AREASOURCE | 8.00 | a | | 6170610.29 | 2319467.62 | 8.00 | 0.00 |
| | | | | 6170972.63 | 2319461.72 | 8.00 | 0.00 |
| | | | | 6170964.37 | 2319028.57 | 8.00 | 0.00 |
| | | | | 6170606.75 | 2319238.65 | 8.00 | 0.00 |

Barrier(s)

| Name | M. | ID | Absorption | | Z-Ext. | | Cantilever | | Height | | Coordinates | | | |
|-----------------|----|----|------------|-------|--------|------|------------|-------|--------|------|-------------|------------|------|--------|
| | | | left | right | | | horz. | vert. | Begin | End | x | y | z | Ground |
| | | | | | (ft) | (ft) | (ft) | (ft) | (ft) | (ft) | (ft) | (ft) | (ft) | (ft) |
| BARRIEREXISTING | | 0 | | | | | | | 6.00 | a | 6175552.67 | 2318346.43 | 6.00 | 0.00 |
| | | | | | | | | | | | 6175552.15 | 2318243.83 | 6.00 | 0.00 |
| BARRIEREXISTING | | 0 | | | | | | | 6.00 | a | 6175565.69 | 2318164.14 | 6.00 | 0.00 |
| | | | | | | | | | | | 6175550.07 | 2318142.27 | 6.00 | 0.00 |
| | | | | | | | | | | | 6175547.72 | 2318007.53 | 6.00 | 0.00 |

Building(s)

| Name | M. | ID | RB | Residents | Absorption | Height | | Coordinates | | | |
|----------|----|---------------|----|-----------|------------|--------|---|-------------|------------|-------|--------|
| | | | | | | Begin | | x | y | z | Ground |
| | | | | | | (ft) | | (ft) | (ft) | (ft) | (ft) |
| BUILDING | | BUILDING00001 | x | 0 | | 45.00 | a | 6171087.11 | 2319629.38 | 45.00 | 0.00 |
| | | | | | | | | 6173070.67 | 2319601.28 | 45.00 | 0.00 |
| | | | | | | | | 6173070.67 | 2319660.73 | 45.00 | 0.00 |
| | | | | | | | | 6173252.27 | 2319660.73 | 45.00 | 0.00 |
| | | | | | | | | 6173239.30 | 2318906.22 | 45.00 | 0.00 |
| | | | | | | | | 6173060.94 | 2318906.22 | 45.00 | 0.00 |
| | | | | | | | | 6173059.86 | 2318970.00 | 45.00 | 0.00 |
| | | | | | | | | 6171079.54 | 2318995.94 | 45.00 | 0.00 |
| BUILDING | | BUILDING00002 | x | 0 | | 45.00 | a | 6173662.19 | 2319601.46 | 45.00 | 0.00 |
| | | | | | | | | 6173784.24 | 2319600.62 | 45.00 | 0.00 |
| | | | | | | | | 6173781.71 | 2319539.18 | 45.00 | 0.00 |

| Name | M. | ID | RB | Residents | Absorption | Height | Coordinates | | | |
|------|----|----|----|-----------|------------|--------|-------------|------------|-------|--------|
| | | | | | | Begin | x | y | z | Ground |
| | | | | | | (ft) | (ft) | (ft) | (ft) | (ft) |
| | | | | | | | 6174576.25 | 2319529.92 | 45.00 | 0.00 |
| | | | | | | | 6174568.68 | 2318875.94 | 45.00 | 0.00 |
| | | | | | | | 6174446.63 | 2318878.46 | 45.00 | 0.00 |
| | | | | | | | 6174445.79 | 2318939.91 | 45.00 | 0.00 |
| | | | | | | | 6173770.77 | 2318949.16 | 45.00 | 0.00 |
| | | | | | | | 6173772.45 | 2318886.88 | 45.00 | 0.00 |
| | | | | | | | 6173651.25 | 2318891.09 | 45.00 | 0.00 |

APPENDIX 10.1:

CADNAA CONSTRUCTION NOISE MODEL INPUTS

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13575 -BRE Space Mira Loma

CadnaA Noise Prediction Model: 13575_Construction.cna

Date: 22.12.20

Analyst: S. Shami

Calculation Configuration

| Configuration | |
|--------------------------------------|--------------------------------|
| Parameter | Value |
| General | |
| Country | (user defined) |
| Max. Error (dB) | 0.00 |
| Max. Search Radius (#(Unit,LEN)) | 2000.01 |
| Min. Dist Src to Rcvr | 0.00 |
| Partition | |
| Raster Factor | 0.50 |
| Max. Length of Section (#(Unit,LEN)) | 999.99 |
| Min. Length of Section (#(Unit,LEN)) | 1.01 |
| Min. Length of Section (%) | 0.00 |
| Proj. Line Sources | On |
| Proj. Area Sources | On |
| Ref. Time | |
| Reference Time Day (min) | 960.00 |
| Reference Time Night (min) | 480.00 |
| Daytime Penalty (dB) | 0.00 |
| Recr. Time Penalty (dB) | 5.00 |
| Night-time Penalty (dB) | 10.00 |
| DTM | |
| Standard Height (m) | 0.00 |
| Model of Terrain | Triangulation |
| Reflection | |
| max. Order of Reflection | 2 |
| Search Radius Src | 100.00 |
| Search Radius Rcvr | 100.00 |
| Max. Distance Source - Rcvr | 1000.00 1000.00 |
| Min. Distance Rcvr - Reflector | 1.00 1.00 |
| Min. Distance Source - Reflector | 0.10 |
| Industrial (ISO 9613) | |
| Lateral Diffraction | some Obj |
| Obst. within Area Src do not shield | On |
| Screening | Incl. Ground Att. over Barrier |
| | Dz with limit (20/25) |
| Barrier Coefficients C1,2,3 | 3.0 20.0 0.0 |
| Temperature (#(Unit,TEMP)) | 10 |
| rel. Humidity (%) | 70 |
| Ground Absorption G | 0.50 |
| Wind Speed for Dir. (#(Unit,SPEED)) | 3.0 |
| Roads (RLS-90) | |
| Strictly acc. to RLS-90 | |
| Railways (FTA/FRA) | |
| Aircraft (???) | |
| Strictly acc. to AzB | |

Receiver Noise Levels

| Name | M. | ID | Level Lr | | | Limit. Value | | | Land Use | | | Height | Coordinates | | |
|-----------|----|------|----------|-------|-------|--------------|-------|-------|----------|------|------------|--------|-------------|------------|------|
| | | | Day | Night | CNEL | Day | Night | CNEL | Type | Auto | Noise Type | | X | Y | Z |
| | | | (dBA) | (dBA) | (dBA) | (dBA) | (dBA) | (dBA) | | | | (ft) | (ft) | (ft) | (ft) |
| RECEIVERS | R1 | 56.2 | 56.2 | 62.8 | 55.0 | 55.0 | 45.0 | 0.0 | | | | 5.00 a | 6175558.12 | 2318277.05 | 5.00 |
| RECEIVERS | R2 | 53.1 | 53.1 | 59.8 | 55.0 | 45.0 | 0.0 | | | | | 5.00 a | 6167131.81 | 2319797.25 | 5.00 |

Area Source(s)

| Name | M. | ID | Result. PWL | | | Result. PWL" | | | Lw / Li | | | Operating Time | | | Height |
|--------------|----|--------------|-------------|---------|-------|--------------|---------|-------|---------|-------|-------|----------------|---------|-------|--------|
| | | | Day | Evening | Night | Day | Evening | Night | Type | Value | norm. | Day | Special | Night | (ft) |
| | | | (dBA) | (dBA) | (dBA) | (dBA) | (dBA) | (dBA) | | | dB(A) | (min) | (min) | (min) | |
| SITEBOUNDARY | | CONSTRUCTION | 131.1 | 131.1 | 131.1 | 75.3 | 75.3 | 75.3 | Lw" | 75.3 | | | | | 8 |

| Name | Height | | Coordinates | | | |
|--------------|--------|------|-------------|------------|------|--------|
| | Begin | End | x | y | z | Ground |
| | (ft) | (ft) | (ft) | (ft) | (ft) | (ft) |
| SITEBOUNDARY | 8.00 a | | 6170255.13 | 2319515.29 | 8.00 | 0.00 |
| | | | 6170968.67 | 2319504.00 | 8.00 | 0.00 |
| | | | 6170973.01 | 2319793.06 | 8.00 | 0.00 |
| | | | 6171141.99 | 2319788.58 | 8.00 | 0.00 |
| | | | 6171197.55 | 2319788.58 | 8.00 | 0.00 |
| | | | 6171243.55 | 2319792.05 | 8.00 | 0.00 |
| | | | 6171293.03 | 2319796.39 | 8.00 | 0.00 |
| | | | 6171293.03 | 2319826.77 | 8.00 | 0.00 |
| | | | 6173524.57 | 2319773.07 | 8.00 | 0.00 |

| Name | Height | | | Coordinates | | | |
|------|--------|------|--|-------------|------------|------|--------|
| | Begin | End | | x | y | z | Ground |
| | (ft) | (ft) | | (ft) | (ft) | (ft) | (ft) |
| | | | | 6173525.27 | 2319741.13 | 8.00 | 0.00 |
| | | | | 6174676.66 | 2319713.00 | 8.00 | 0.00 |
| | | | | 6174656.42 | 2318707.93 | 8.00 | 0.00 |
| | | | | 6173523.72 | 2318735.44 | 8.00 | 0.00 |
| | | | | 6173523.72 | 2318746.73 | 8.00 | 0.00 |
| | | | | 6173488.13 | 2318746.22 | 8.00 | 0.00 |
| | | | | 6173488.99 | 2318767.92 | 8.00 | 0.00 |
| | | | | 6171969.41 | 2318790.09 | 8.00 | 0.00 |
| | | | | 6171962.47 | 2318362.05 | 8.00 | 0.00 |
| | | | | 6171161.86 | 2318835.67 | 8.00 | 0.00 |
| | | | | 6170282.95 | 2319358.68 | 8.00 | 0.00 |
| | | | | 6170256.47 | 2319465.67 | 8.00 | 0.00 |
| | | | | 6170256.04 | 2319493.01 | 8.00 | 0.00 |

Barrier(s)

| Name | M. | ID | Absorption | | Z-Ext. | Cantilever | | Height | | Coordinates | | | |
|-----------------|----|----|------------|-------|--------|------------|-------|--------|------|-------------|------------|------|--------|
| | | | left | right | | horz. | vert. | Begin | End | x | y | z | Ground |
| | | | | | | (ft) | (ft) | (ft) | (ft) | (ft) | (ft) | (ft) | (ft) |
| BARRIEREXISTING | | 0 | | | | | | 6.00 | a | 6175552.67 | 2318346.43 | 6.00 | 0.00 |
| | | | | | | | | | | 6175552.15 | 2318243.83 | 6.00 | 0.00 |
| BARRIEREXISTING | | 0 | | | | | | 6.00 | a | 6175565.69 | 2318164.14 | 6.00 | 0.00 |
| | | | | | | | | | | 6175550.07 | 2318142.27 | 6.00 | 0.00 |
| | | | | | | | | | | 6175547.72 | 2318007.53 | 6.00 | 0.00 |

13575 -BRE Space Mira Loma

CadnaA Noise Prediction Model: 13575_ConcretePour.cna

Date: 22.12.20

Analyst: S. Shami

Calculation Configuration

| Configuration | |
|--------------------------------------|--------------------------------|
| Parameter | Value |
| General | |
| Country | (user defined) |
| Max. Error (dB) | 0.00 |
| Max. Search Radius (#(Unit,LEN)) | 2000.01 |
| Min. Dist Src to Rcvr | 0.00 |
| Partition | |
| Raster Factor | 0.50 |
| Max. Length of Section (#(Unit,LEN)) | 999.99 |
| Min. Length of Section (#(Unit,LEN)) | 1.01 |
| Min. Length of Section (%) | 0.00 |
| Proj. Line Sources | On |
| Proj. Area Sources | On |
| Ref. Time | |
| Reference Time Day (min) | 960.00 |
| Reference Time Night (min) | 480.00 |
| Daytime Penalty (dB) | 0.00 |
| Recr. Time Penalty (dB) | 5.00 |
| Night-time Penalty (dB) | 10.00 |
| DTM | |
| Standard Height (m) | 0.00 |
| Model of Terrain | Triangulation |
| Reflection | |
| max. Order of Reflection | 2 |
| Search Radius Src | 100.00 |
| Search Radius Rcvr | 100.00 |
| Max. Distance Source - Rcvr | 1000.00 1000.00 |
| Min. Distance Rcvr - Reflector | 1.00 1.00 |
| Min. Distance Source - Reflector | 0.10 |
| Industrial (ISO 9613) | |
| Lateral Diffraction | some Obj |
| Obst. within Area Src do not shield | On |
| Screening | Incl. Ground Att. over Barrier |
| | Dz with limit (20/25) |
| Barrier Coefficients C1,2,3 | 3.0 20.0 0.0 |
| Temperature (#(Unit,TEMP)) | 10 |
| rel. Humidity (%) | 70 |
| Ground Absorption G | 0.50 |
| Wind Speed for Dir. (#(Unit,SPEED)) | 3.0 |
| Roads (RLS-90) | |
| Strictly acc. to RLS-90 | |
| Railways (FTA/FRA) | |
| Aircraft (???) | |
| Strictly acc. to AzB | |

Receiver Noise Levels

| Name | M. | ID | Level Lr | | | Limit. Value | | | Land Use | | | Height | Coordinates | | |
|-----------|----|------|----------|-------|-------|--------------|-------|-------|----------|------|------------|--------|-------------|------------|------|
| | | | Day | Night | CNEL | Day | Night | CNEL | Type | Auto | Noise Type | | X | Y | Z |
| | | | (dBA) | (dBA) | (dBA) | (dBA) | (dBA) | (dBA) | | | | (ft) | (ft) | (ft) | (ft) |
| RECEIVERS | R1 | 48.5 | 48.5 | 55.2 | 55.0 | 45.0 | 0.0 | | | | | 5.00 a | 6175558.12 | 2318277.05 | 5.00 |
| RECEIVERS | R2 | 44.9 | 44.9 | 51.6 | 55.0 | 45.0 | 0.0 | | | | | 5.00 a | 6167131.81 | 2319797.25 | 5.00 |

Area Source(s)

| Name | M. | ID | Result. PWL | | | Result. PWL" | | | Lw / Li | | | Operating Time | | | Height |
|----------|----|---------------|-------------|---------|-------|--------------|---------|-------|---------|-------|-------|----------------|---------|-------|--------|
| | | | Day | Evening | Night | Day | Evening | Night | Type | Value | norm. | Day | Special | Night | (ft) |
| | | | (dBA) | (dBA) | (dBA) | (dBA) | (dBA) | (dBA) | | | | (min) | (min) | (min) | |
| BUILDING | | BUILDING00001 | 122.3 | 122.3 | 122.3 | 71.2 | 71.2 | 71.2 | Lw" | 71.2 | | | | | 45 |
| BUILDING | | BUILDING00002 | 118.4 | 118.4 | 118.4 | 71.2 | 71.2 | 71.2 | Lw" | 71.2 | | | | | 45 |

| Name | Height | | Coordinates | | | |
|----------|---------|------|-------------|------------|-------|--------|
| | Begin | End | x | y | z | Ground |
| | (ft) | (ft) | (ft) | (ft) | (ft) | (ft) |
| BUILDING | 45.00 a | | 6171087.11 | 2319629.38 | 45.00 | 0.00 |
| | | | 6173070.67 | 2319601.28 | 45.00 | 0.00 |
| | | | 6173070.67 | 2319660.73 | 45.00 | 0.00 |
| | | | 6173252.27 | 2319660.73 | 45.00 | 0.00 |
| | | | 6173239.30 | 2318906.22 | 45.00 | 0.00 |
| | | | 6173060.94 | 2318906.22 | 45.00 | 0.00 |
| | | | 6173059.86 | 2318970.00 | 45.00 | 0.00 |
| | | | 6171079.54 | 2318995.94 | 45.00 | 0.00 |

| Name | Height | | Coordinates | | | |
|----------|--------|------|-------------|------------|-------|--------|
| | Begin | End | x | y | z | Ground |
| | (ft) | (ft) | (ft) | (ft) | (ft) | (ft) |
| BUILDING | 45.00 | a | 6173662.19 | 2319601.46 | 45.00 | 0.00 |
| | | | 6173784.24 | 2319600.62 | 45.00 | 0.00 |
| | | | 6173781.71 | 2319539.18 | 45.00 | 0.00 |
| | | | 6174576.25 | 2319529.92 | 45.00 | 0.00 |
| | | | 6174568.68 | 2318875.94 | 45.00 | 0.00 |
| | | | 6174446.63 | 2318878.46 | 45.00 | 0.00 |
| | | | 6174445.79 | 2318939.91 | 45.00 | 0.00 |
| | | | 6173770.77 | 2318949.16 | 45.00 | 0.00 |
| | | | 6173772.45 | 2318886.88 | 45.00 | 0.00 |
| | | | 6173651.25 | 2318891.09 | 45.00 | 0.00 |

Barrier(s)

| Name | M. | ID | Absorption | | Z-Ext. | Cantilever | | Height | | Coordinates | | | |
|-----------------|----|----|------------|-------|--------|------------|-------|--------|------|-------------|------------|------|--------|
| | | | left | right | | horz. | vert. | Begin | End | x | y | z | Ground |
| | | | | | (ft) | (ft) | (ft) | (ft) | (ft) | (ft) | (ft) | (ft) | (ft) |
| BARRIEREXISTING | | 0 | | | | | | 6.00 | a | 6175552.67 | 2318346.43 | 6.00 | 0.00 |
| | | | | | | | | | | 6175552.15 | 2318243.83 | 6.00 | 0.00 |
| BARRIEREXISTING | | 0 | | | | | | 6.00 | a | 6175565.69 | 2318164.14 | 6.00 | 0.00 |
| | | | | | | | | | | 6175550.07 | 2318142.27 | 6.00 | 0.00 |
| | | | | | | | | | | 6175547.72 | 2318007.53 | 6.00 | 0.00 |