

**CULVER DRIVE / ALTON PARKWAY
INTERSECTION IMPROVEMENT PROJECT
DRAINAGE REPORT**

May 2020

Prepared for:

City of Irvine
1 Civic Center Plaza
Irvine, CA 92606

Prepared on Behalf of:

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1. INTRODUCTION

The City of Irvine has retained Stantec Consulting Services Inc. (Stantec), as a subconsultant to Kreuzer Consulting Group (KGC), to provide engineering services for the design of drainage improvements in support of improvements at the Culver Drive and Alton Parkway intersection in the City of Irvine, California. Improvements include widening of northbound Culver Drive and removal of a median island. This report is prepared to document the impact of proposed improvements at the Culver Alton Intersection site on the existing storm drain system and recommend any improvements required. The Culver Alton improvement impact area encompasses approximately 4.39 acres and is located at the intersection of Culver Drive and Alton Parkway. See Figures 1 and 2 for the Vicinity and Location Maps.

Existing and Proposed Conditions

In the existing condition, runoff from the overall drainage area of 9.87 acres generally flows in a northerly direction from the existing roadway to San Diego Creek. Runoff from the impacted street improvement area is proposed to flow via the existing storm drain system in the intersection with minimal adjustments to the two of the four catch basins that currently intercept runoff. The discharge of these facilities has been characterized in this report to assist in the ultimate design. This report also includes an analysis determining whether the development has Hydrologic Conditions of Concern (HCOC) per the fourth term MS4 (Municipal) permit. The report quantifies design outflow to San Diego Creek and the discharges to the existing storm drain line.

The existing site is located within a Special Flood Hazard Area (SFHA) of the San Diego Creek Watershed. This creates a potential Hydrologic Condition of Concern (HCOC) discussed herein below.

Hydrologic Conditions of Concern

Per Figure No. XVI.3, "North Orange County Hydromodification Susceptibility Maps, Figure No. 4," of the Orange County Technical Guidance Document, the entire San Diego Creek watershed has been described as a *Potential Area of Erosion, Habitat, and Physical Structure Susceptibility*. The project location is shown in reference to the San Diego Creek watershed in Figure No. 6. The project drains to susceptible waters and must be checked for Hydrologic Conditions of Concern and hydromodification. Post-project condition runoff volume and time of concentration do not exceed that of the pre-project condition by more than 5%. Therefore, HCOCs do not exist for this Project.

2. RATIONAL METHOD HYDROLOGIC ANALYSIS

The Orange County Hydrology Manual, published in 1986, (Hydrology Manual) and Addendum No.1, published in 1996, provided the guidelines and procedures for the Rational Method analysis. The parameters used for the Rational Method are summarized below.

- The existing and proposed condition hydrologic boundaries were based on the topography as depicted on Figure 3, Existing Condition Hydrology Map.
- The underlying hydrologic soil groups are Type A, B and D as shown on Figure 5, Soil Map.
- The existing condition land uses are road (commercial) and landscape (park).
- For the 2-year storm event, Antecedent Moisture Condition (AMC) AMC-I was used; for the 10 & 25-year storm events, Antecedent Moisture Condition (AMC) AMC-II was used; and for the 100-year storm event, AMC-III was used in accordance with the OC Hydrology Manual, page C-10.

The Rational Method analysis was performed with software developed by Advanced Engineering Software (AES) for the 2-year, 10-year, 25-year and 100-year storm events. The software was designed to accept watershed data and perform Rational Method analyses in accordance with the OC Hydrology Manual. The software defines subareas and routing paths by means of upstream and downstream node numbers, node elevations, travel distance, soil group, land uses and type of conveyance. The Hydrology Map Figures 3 and 4, show the locations of all node numbers used in the Rational Method analysis.

3. CATCH BASIN ANALYSIS

The four catch basins in improved areas were analyzed in accordance with the procedures provided in the Hydraulic Engineering Circular No. 12 (HEC-12) published by the U.S. Federal Highway Administration using the FlowMaster Version 8.0 (FlowMaster) Computer Program developed by Haestad Methods, Inc. The FlowMaster input includes street cross slope, gutter slope, local depression depth, and inlet length. The program calculates inlet efficiency, intercepted flow, bypass flow, depth of flow, and spread. The existing storm drains were also analyzed with FlowMaster.

Design criteria from the Orange County Local Drainage Manual are included in Appendix A.

Table 3-1A
Catch Basin Existing Conditions

Catch Basin Area	Existing Width (FT)	Inlet Condition	Tributary Area (AC)	25-Year Flow (CFS)	25-Year Tc (MIN)	10-Year Flow (CFS)	10-Year Tc (MIN)
1	10	Flow-by	2.2	5.76	11.62	4.74	11.76
2	5	Flow-by	1.8	4.83	10.15	3.99	10.24
3	7	Sump	2.4	6.30	10.44	5.18	10.60
4	10	Sump	3.4	8.75	11.49	7.14	11.72

Table 3-1B
Catch Basin Proposed Conditions

Catch Basin Area	Proposed Width (FT)	Inlet Condition	Tributary Area (AC)	25-Year Flow (CFS)	25-Year Tc (MIN)	10-Year Flow (CFS)	10-Year Tc (MIN)
1	10	Flow-by	2.2	5.75	11.63	4.73	11.75
2	5	Flow-by	1.8	4.83	10.15	3.99	10.24
3	14	Sump	2.4	6.31	10.44	5.19	10.60
4	14	Sump	3.4	8.85	11.48	7.24	11.71

4. RESULTS

Rational Method Results:

The summary of results of the existing condition and proposed condition Rational Method hydrology analyses are listed in table 4-1 below.

Table 4-1
Rational Method Hydrology Analysis 2, 10, 25, 100-Year Storm Summary
Culver Alton Intersection

Storm Event	Condition	Rational Method Q (CFS)				Total
		Area 1	Area 2	Area 3	Area 4	
2 YR	Existing	2.45	2.06	2.67	3.65	10.83
	Proposed	2.44	2.06	2.68	3.74	10.92
10 YR	Existing	4.74	3.99	5.18	7.14	21.05
	Proposed	4.73	3.99	5.19	7.24	21.15
25 YR	Existing	5.76	4.83	6.30	8.75	25.64
	Proposed	5.75	4.83	6.31	8.85	25.74
100 YR	Existing	7.50	6.30	8.23	11.53	33.56
	Proposed	7.49	6.30	8.23	11.62	33.64
Tributary Area (AC)		2.2	1.8	2.4	3.4	9.80

Area 1 refers to the drainage management area along streamline 1 on Hydrology Map Figures 3 & 4 draining to a catch basin on the north side of Alton Parkway, west of Culver Drive. Area 2 refers to the drainage management area along streamline 2 on Hydrology Map Figures 3 & 4 draining to a catch basin on the south side of Alton Parkway, west of Culver Drive. Area 3 refers to the drainage management area along streamlines 3 and 6 on Hydrology Map Figures 3 & 4 draining to a catch basin on the south side of Alton Parkway, east of Culver Drive. Area 4 refers to the drainage management area along streamlines 4 and 5 on Hydrology Map Figures 3 & 4 draining to a catch basin on the north side of Alton Parkway, east of Culver Drive.

Rational Method analyses are included in Appendix B.

Catch Basin Analysis Results:

The proposed project increases flow to the catch basin servicing Area 4 by 0.10 cfs in the 25-year storm event from 8.75 cfs to 8.85 cfs. In the location of the widened curb, a 14-foot-wide catch basin at the northeast corner of the proposed intersection along Alton per City of Irvine Standard Plans 200 Type A-2, 302, and 303 should be installed to conduct flow. The existing outlet 24" RCP is sufficient to convey increased flow (normal depth = 8.21", flowing 34% full).

At the southeast corner of the proposed intersection, a 14-foot-wide catch basin per City of Irvine Standard Plans 200 Type A-2, 302, and 303 should be installed along Alton to conduct flow in the proposed condition. This catch basin will service flow from Area 3, which increased by 0.01 cfs in the proposed condition from 6.30 cfs to 6.31 cfs in a 25-year storm event. The existing outlet 24" RCP is sufficient to convey increased flow (normal depth = 7.62", flowing 32% full).

Existing 24-inch R.C.P. to be extended at existing slope to proposed catch basin locations. Depth of catch basin to match projected invert of pipe.

See Appendix C for supporting calculations.

Table 4-2
Catch Basin Results - FlowMaster

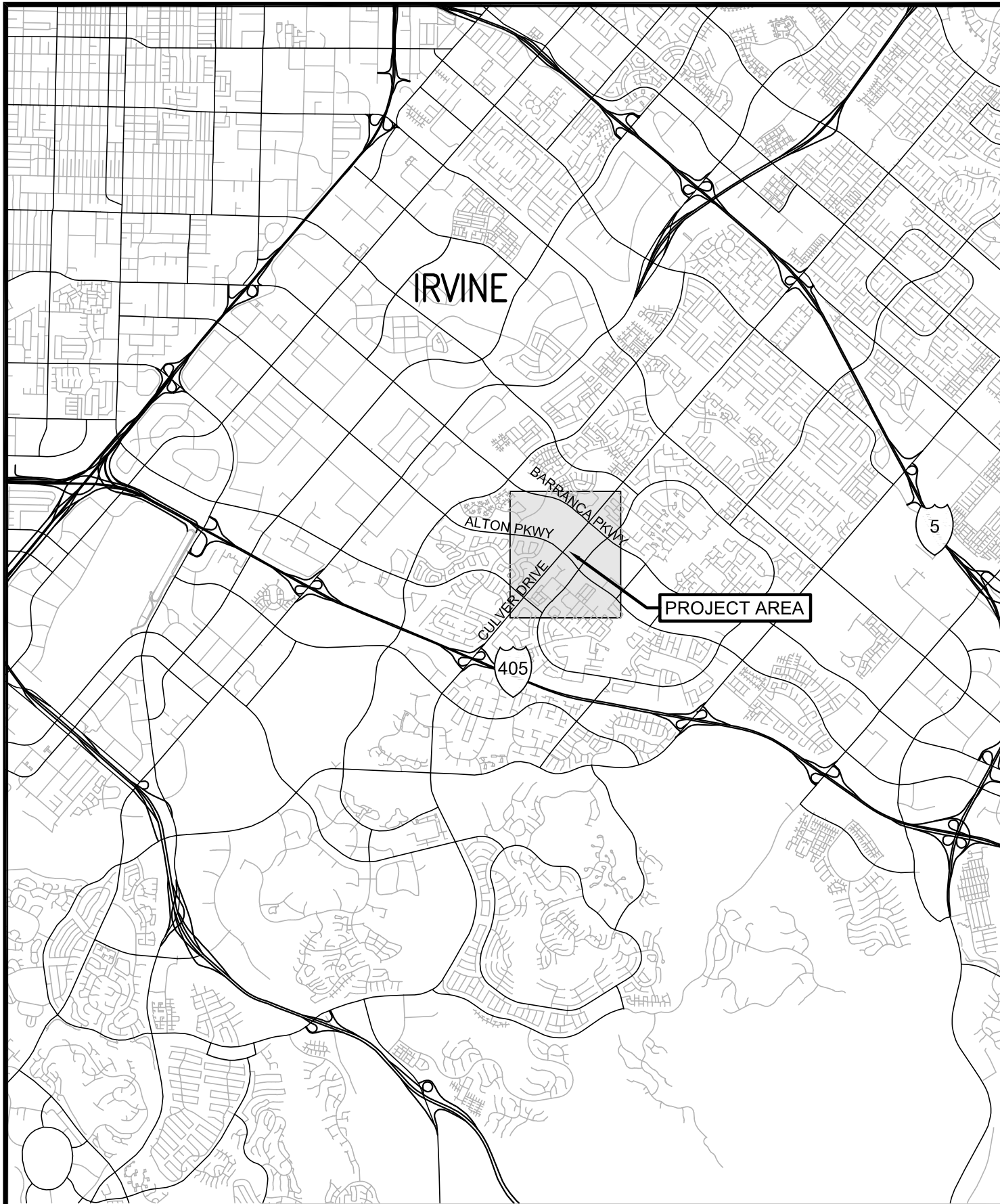
Catch Basin Area	Discharge (CFS)	Curb Opening Length (FT)	Spread (FT)	Depth (IN)	Gutter Depression (FT)	Total Depression (FT)
4	8.85	14	21.35	5.87	0.13	0.29
3	6.31	14	17.04	4.99	0.13	0.29

Hydrology for catch basins servicing Area 1 and Area 2 is unchanged. Therefore, no upsizing of catch basins or adjoining storm drains is required.

5. FIGURES

Figure 1	Vicinity Map
Figure 2	Location Map
Figure 3	Hydrology Map – Existing Condition
Figure 4	Hydrology Map – Proposed Condition
Figure 5	Soil Map
Figure 6	San Diego Creek Watershed Map (from The Orange County Technical Guidance Document Figure No. XVI.3)

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VICINITY MAP

DATE:

11/2019

FIGURE

1

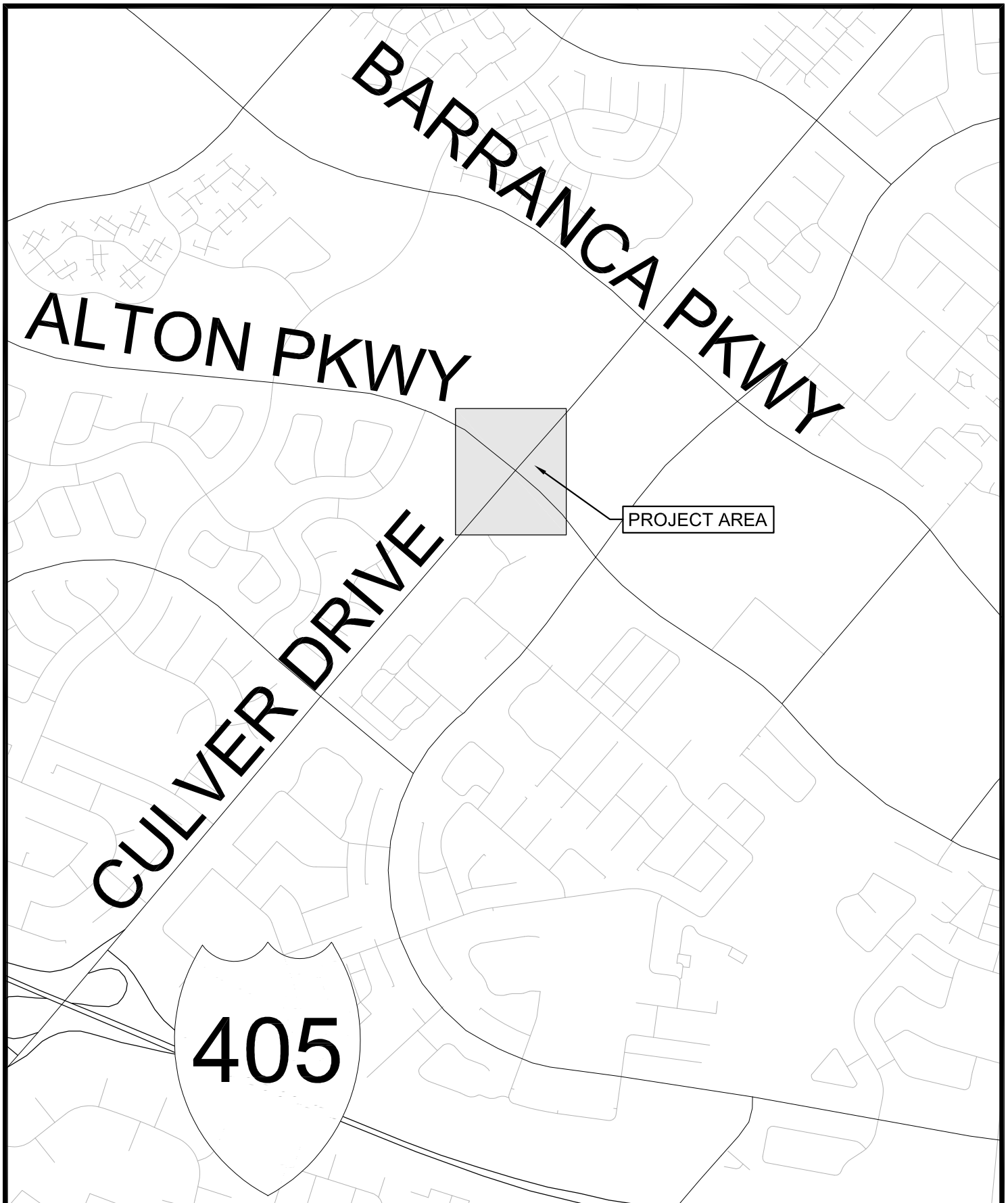
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LOCATION MAP

DATE:

11/2019

FIGURE

2

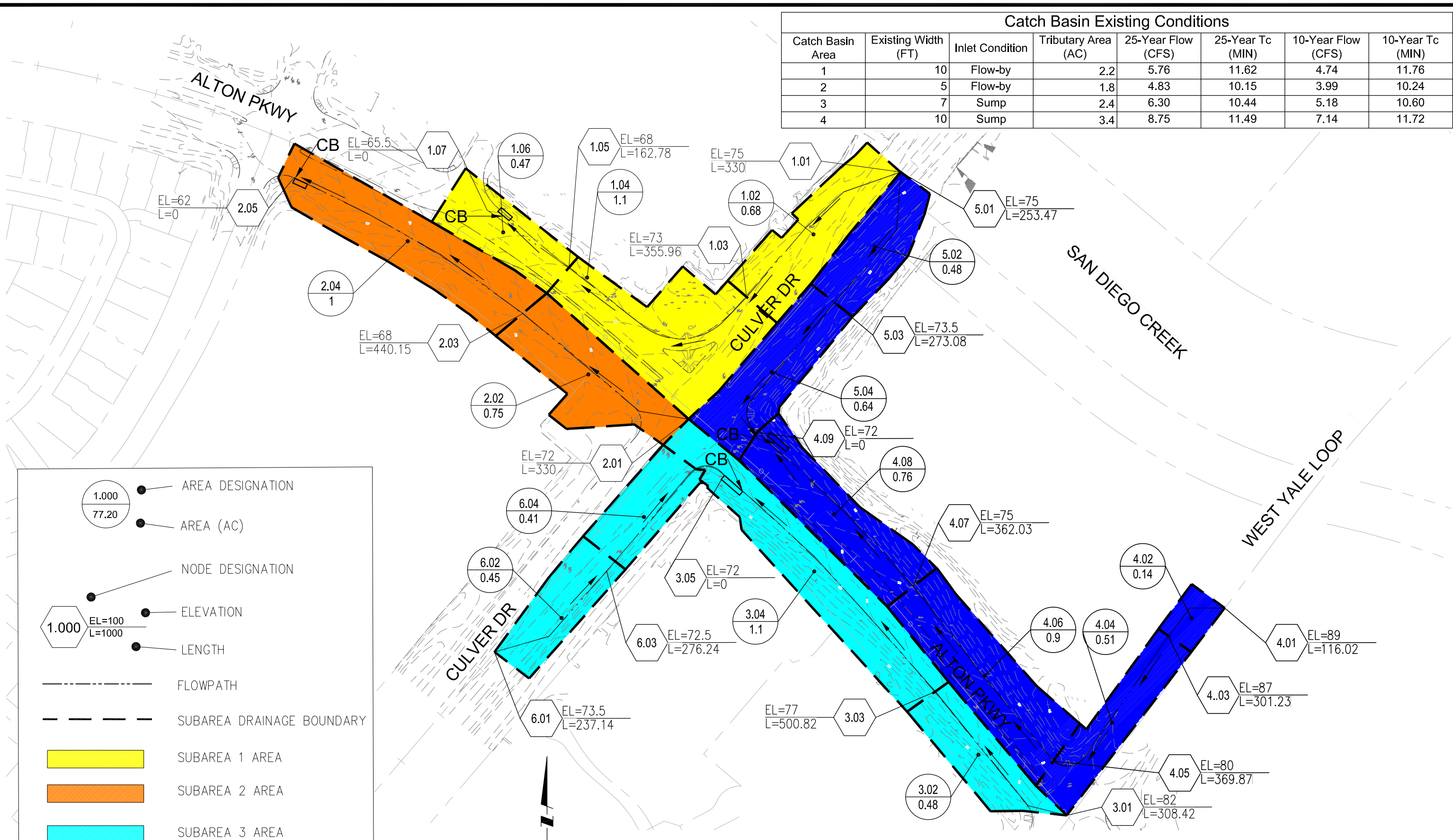
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Catch Basin Existing Conditions							
Catch Basin Area	Existing Width (FT)	Inlet Condition	Tributary Area (AC)	25-Year Flow (CFS)	25-Year Tc (MIN)	10-Year Flow (CFS)	10-Year Tc (MIN)
1	10	Flow-by	2.2	5.76	11.62	4.74	11.76
2	5	Flow-by	1.8	4.83	10.15	3.99	10.24
3	7	Sump	2.4	6.30	10.44	5.18	10.60
4	10	Sump	3.4	8.75	11.49	7.14	11.72

1.000

77.20

●

AREA DESIGNATION

1.000

EL=100
L=1000

●

AREA (AC)

1.000

EL=100
L=1000

●

NODE DESIGNATION

1.000

EL=100
L=1000

●

ELEVATION

1.000

EL=100
L=1000

●

LENGTH

FLOWPATH

SUBAREA DRAINAGE BOUNDARY

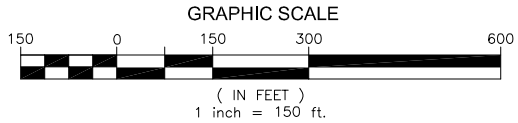
SUBAREA 1 AREA

SUBAREA 2 AREA

SUBAREA 3 AREA

SUBAREA 4 AREA

FLOW DIRECTION



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HYDROLOGY MAP
EXISTING CONDITION

DATE:
01/2020

FIGURE **3**
OF **6**

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Catch Basin Proposed Conditions							
Catch Basin Area	Existing Width (FT)	Inlet Condition	Tributary Area (AC)	25-Year Flow (CFS)	25-Year Tc (MIN)	10-Year Flow (CFS)	10-Year Tc (MIN)
1	10	Flow-by	2.2	5.75	11.63	4.73	11.75
2	5	Flow-by	1.8	4.83	10.15	3.99	10.24
3	14	Sump	2.4	6.31	10.44	5.19	10.60
4	14	Sump	3.4	8.85	11.48	7.24	11.71

1.000

77.20

●

AREA DESIGNATION

1.000

EL=100

L=1000

●

AREA (AC)

●

NODE DESIGNATION

1.000

EL=100

L=1000

●

ELEVATION

●

LENGTH

FLOWPATH

SUBAREA DRAINAGE BOUNDARY

SUBAREA 1 AREA

SUBAREA 2 AREA

SUBAREA 3 AREA

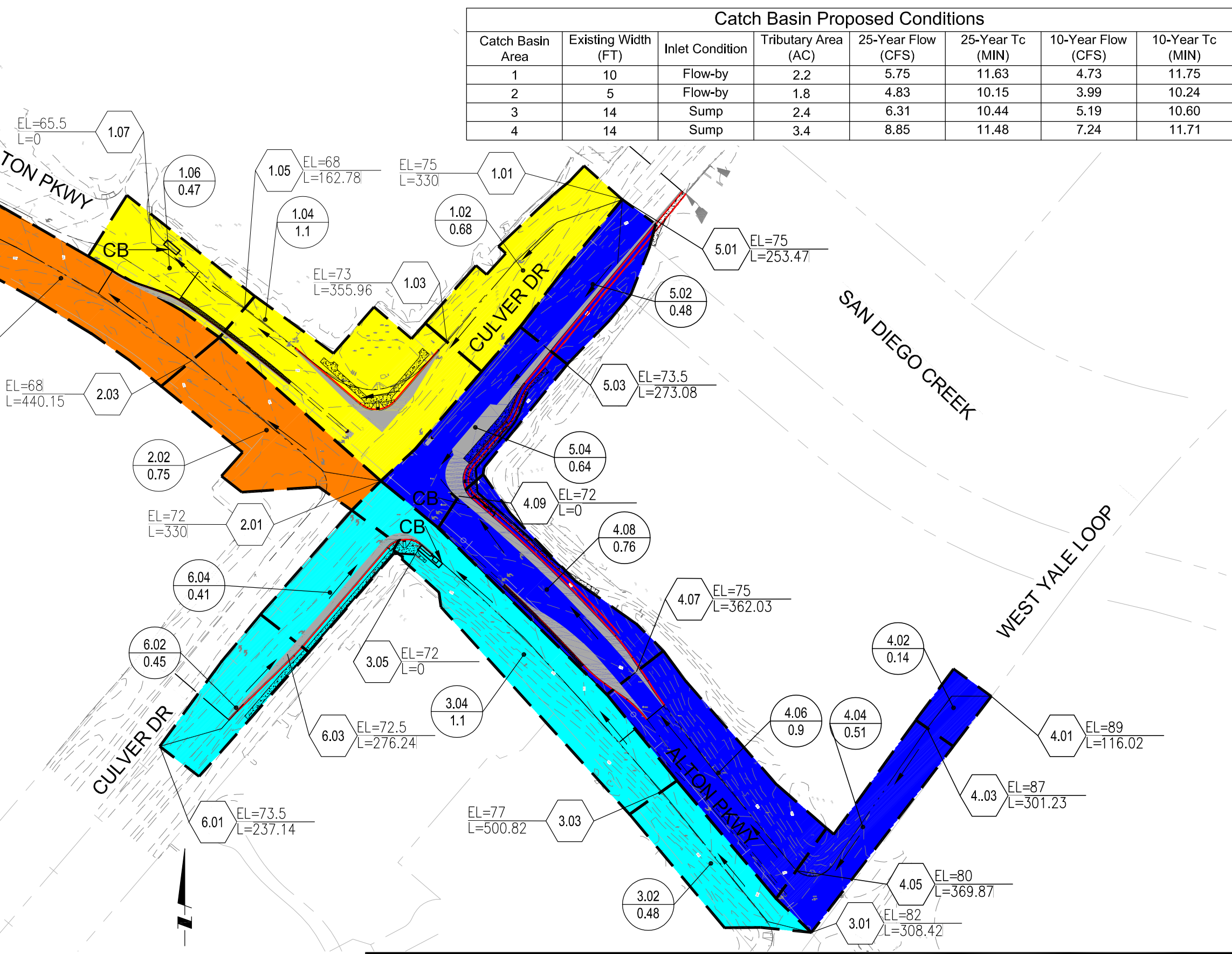
SUBAREA 4 AREA

PROPOSED PAVEMENT

PROPOSED SIDEWALK

PROPOSED CURB

FLOW DIRECTION



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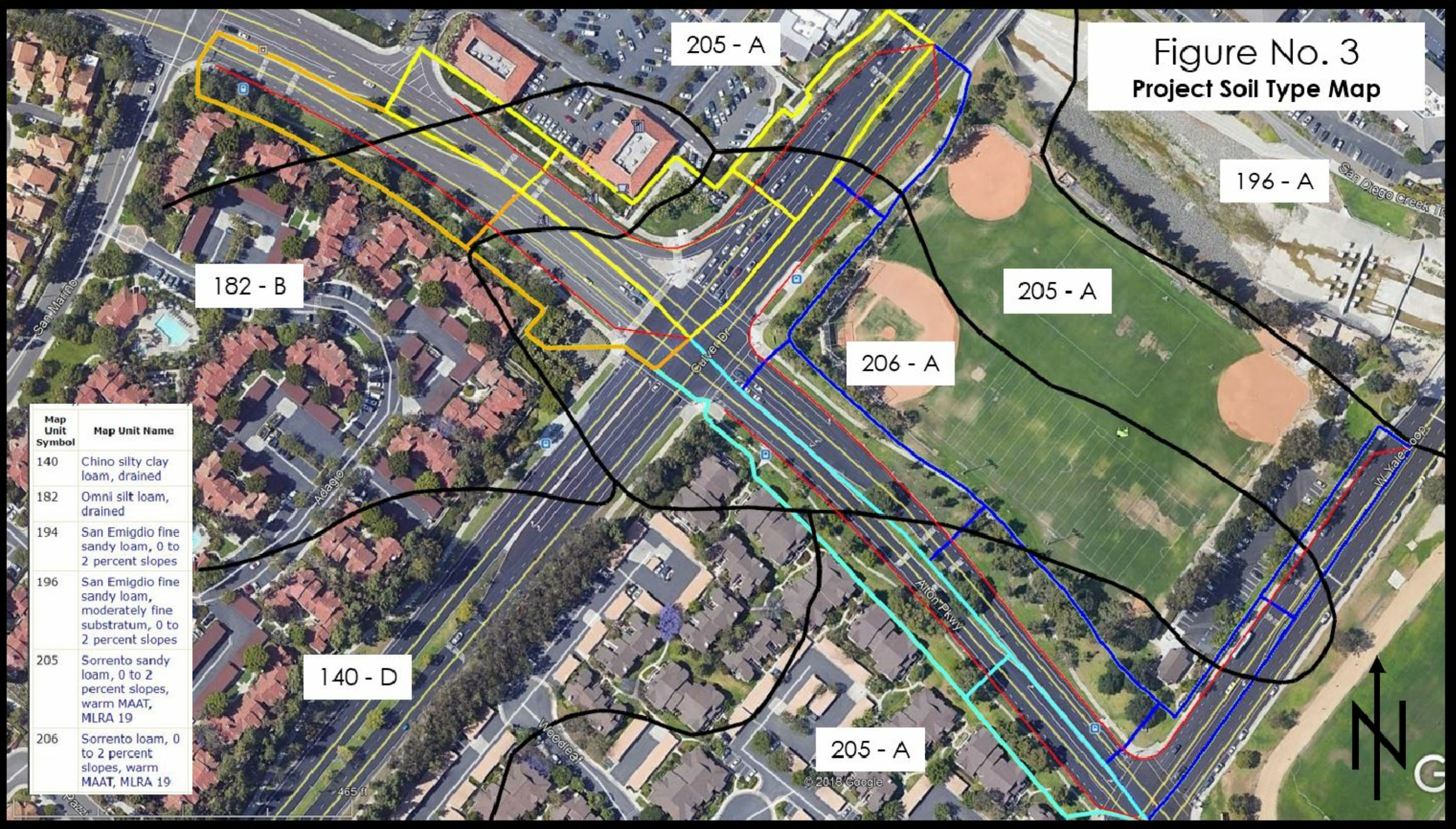
HYDROLOGY MAP
PROPOSED CONDITION

DATE:
01/2020

FIGURE
4
OF
6

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SOIL TYPE MAP

DATE:

11/2019

FIGURE

5

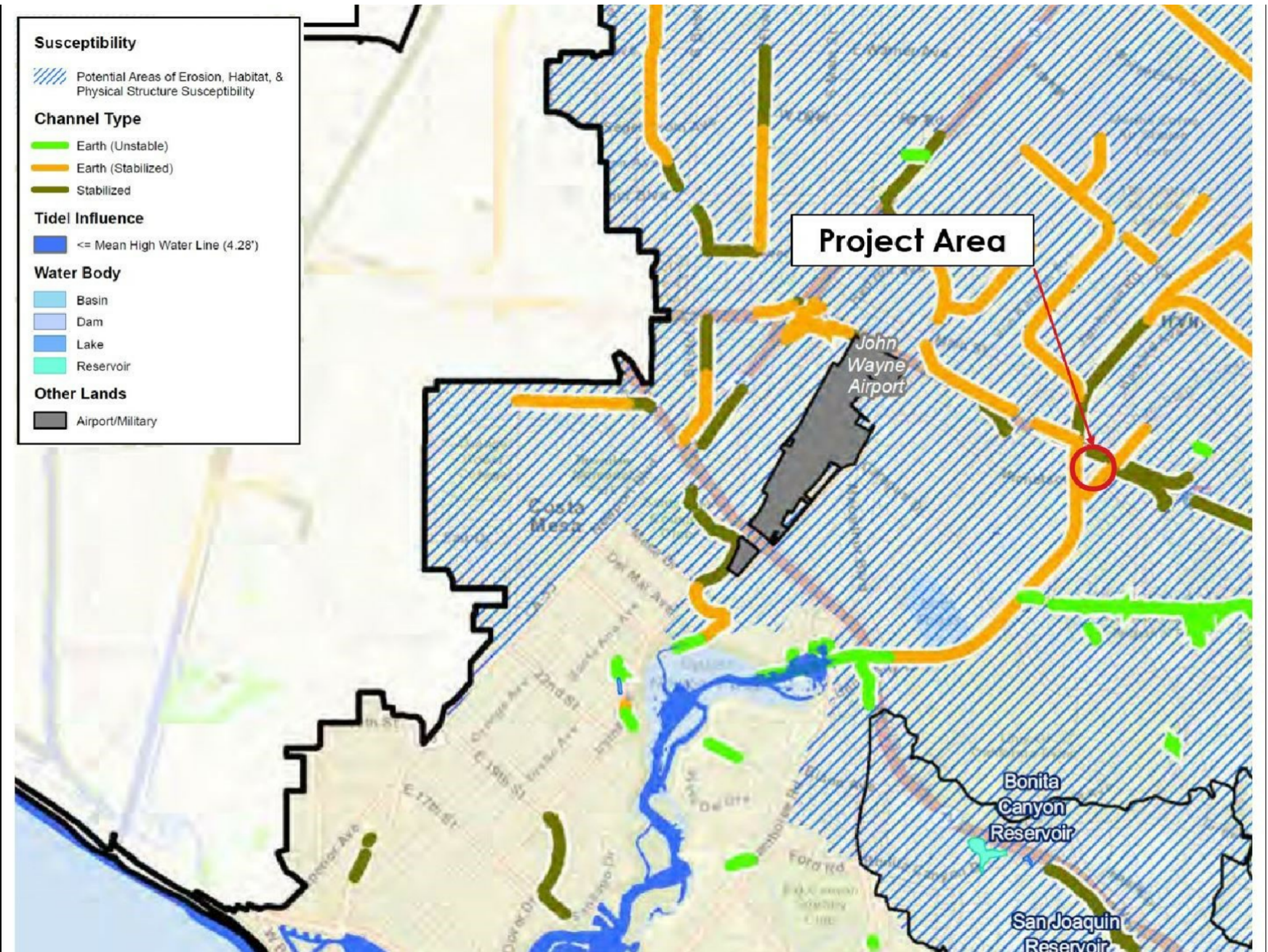
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SAN DIEGO CREEK WATERSHED MAP

DATE:

11/2019

FIGURE

6

OF

6

JOB NO.

2042558200

6. TECHNICAL APPENDICES

APPENDIX A Orange County Hydrology Manual References

APPENDIX B Rational Method Hydrology Analysis

APPENDIX C Catch Basin Calculations

A.1 APPENDIX A – Orange County Manual References

Curve Numbers of Hydrologic Soil-Cover Complexes For Pervious Areas-AMC II

Cover Type (3)	Quality of Cover (2)	Soil Group			
		A	B	C	D
<u>NATURAL COVERS -</u>					
Barren (Rockland, eroded and graded land)		78	86	91	93
Chaparral, Broadleaf (Manzonita, ceanothus and scrub oak)	Poor	53	70	80	85
	Fair	40	63	75	81
	Good	31	57	71	78
Chaparral, Narrowleaf (Chamise and redshank)	Poor	71	82	88	91
	Fair	55	72	81	86
Grass, Annual or Perennial	Poor	67	78	86	89
	Fair	50	69	79	84
	Good	38	61	74	80
Meadows or Cienegas (Areas with seasonally high water table, principal vegetation is sod forming grass)	Poor	63	77	85	88
	Fair	51	70	80	84
	Good	30	58	71	78
Open Brush (Soft wood shrubs - buckwheat, sage, etc.)	Poor	62	76	84	88
	Fair	46	66	77	83
	Good	41	63	75	81
Woodland (Coniferous or broadleaf trees predominate. Canopy density is at least 50 percent.)	Poor	45	66	77	83
	Fair	36	60	73	79
	Good	25	55	70	77
Woodland, Grass (Coniferous or broadleaf trees with canopy density from 20 to 50 percent)	Poor	57	73	82	86
	Fair	44	65	77	82
	Good	33	58	72	79
<u>URBAN COVERS -</u>					
Residential or Commercial Landscaping (Lawn, shrubs, etc.)	Good	32	56	69	75
Turf (Irrigated and mowed grass)	Poor	58	74	83	87
	Fair	44	65	77	82
	Good	33	58	72	79
<u>AGRICULTURAL COVERS -</u>					
Fallow (Land plowed but not tilled or seeded)		77	86	91	94

ORANGE COUNTY
HYDROLOGY MANUAL

**CURVE NUMBERS
FOR
PERVIOUS AREAS**

ACTUAL IMPERVIOUS COVER		
Land Use (1)	Range-Percent	Recommended Value For Average Conditions-Percent (2)
Natural or Agriculture	0 - 0	0
Public Park	10 - 25	15
School	30 - 50	40
Single Family Residential: (3)		
2.5 acre lots	5 - 15	10
1 acre lots	10 - 25	20
2 dwellings/acre	20 - 40	30
3-4 dwellings/acre	30 - 50	40
5-7 dwellings/acre	35 - 55	50
8-10 dwellings/acre	50 - 70	60
More than 10 dwellings/acre	65 - 90	80
Multiple Family Residential:		
Condominiums	45 - 70	65
Apartments	65 - 90	80
Mobile Home Park	60 - 85	75
Commercial, Downtown Business or Industrial	80 - 100	90
<p>Notes:</p> <ol style="list-style-type: none"> 1. Land use should be based on ultimate development of the watershed. Long range master plans for the County and incorporated cities should be reviewed to insure reasonable land use assumptions. 2. Recommended values are based on average conditions which may not apply to a particular study area. The percentage impervious may vary greatly even on comparable sized lots due to differences in dwelling size, improvements, etc. Landscape practices should also be considered as it is common in some areas to use ornamental gravels underlain by impervious plastic materials in place of lawns and shrubs. A field investigation of a study area shall always be made, and a review of aerial photos, where available, may assist in estimating the percentage of impervious cover in developed areas. 3. For typical equestrian subdivisions increase impervious area 5 percent over the values recommended in the table above. 		
ORANGE COUNTY HYDROLOGY MANUAL		ACTUAL IMPERVIOUS COVER FOR DEVELOPED AREAS

Figure C-4

CHAPTER 1

DESIGN CRITERIA

The following design criteria shall be used for storm drain and local drainage structures built for dedication to the County of Orange, Orange County Flood Control District, or for private facilities within unincorporated Orange County.

Regional or Sub-Regional design storm frequencies are subject to individual review by the Agency and should be in accordance with the 1986 Hydrology Manual and Flood Protection Goals. This manual does not supersede any information contained within the Orange County Drainage Area Management Plan (DAMP), and is intended to be consistent with the DAMP.

I. PROTECTION LEVELS

A. Structures

The goal is to provide 100-year protection for all habitable structures pursuant to Public Services and Facilities Element of the General Plan.

B. Streets

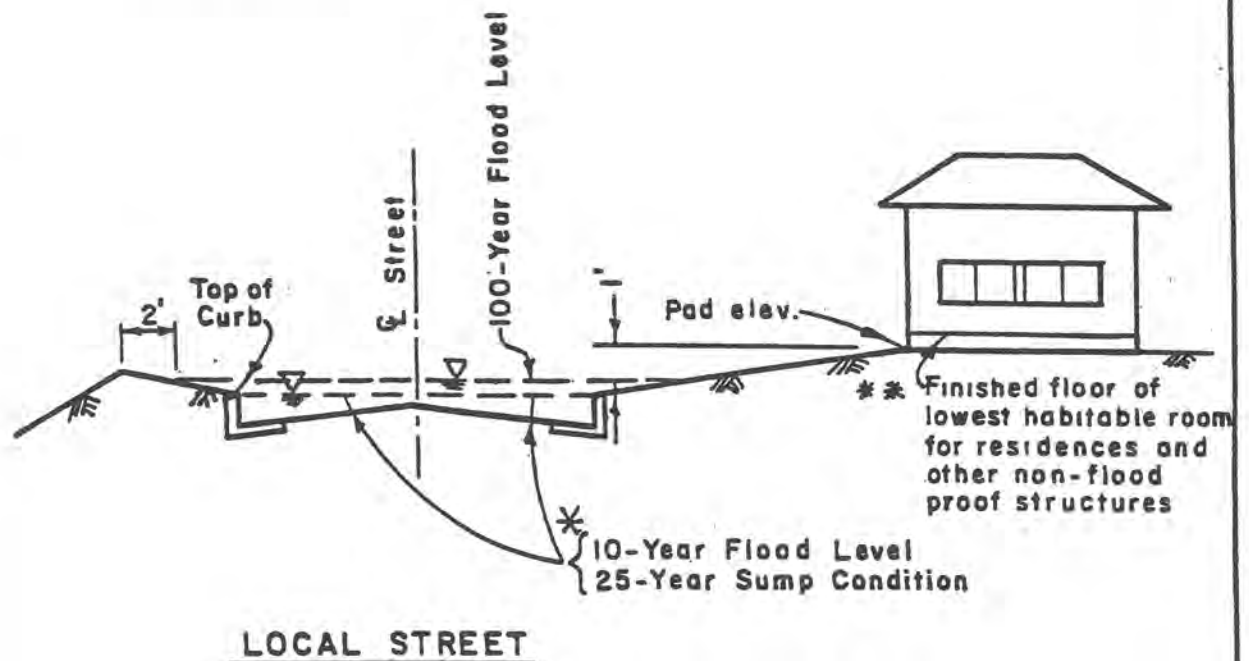
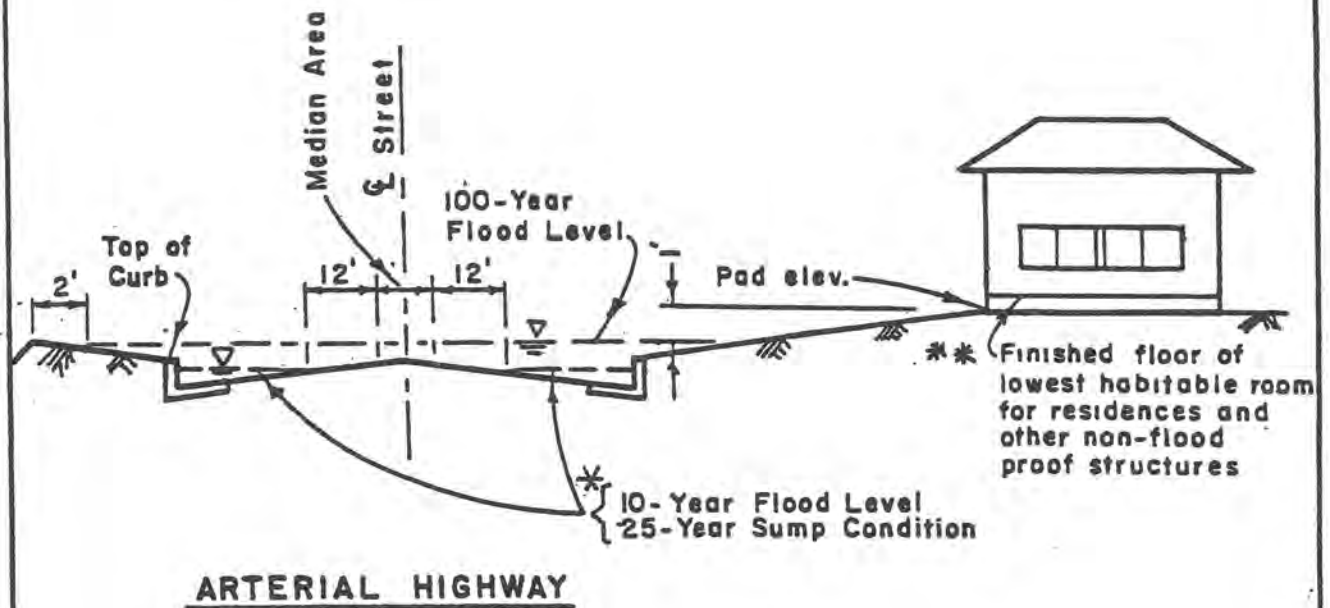
Street criteria for 100-year storm flow is shown on the attached Figure 1-1, Flood Protection Goals.

1. Arterial Highway

- a. One travel lane (use 12 foot if not determined) shall be free from inundation in each direction in a 10-year storm.
- b. In a sump condition, one travel lane (use 12 foot if not determined) shall be free from inundation in each direction in a 25-year storm.
- c. Median and left-turn pockets shall not be considered as a travel lane.
- d. In places where superelevation occurs on arterial highways an inlet shall be provided as necessary to preclude drainage across the travel lanes. The catch basin shall intercept a minimum of a 10-year storm. Local depressions are not to be used for inlets at medians; grate opening or side opening/grate combination (for which future paving overlap will not create a drop) are recommended. Flooding width from median curbs in superelevated sections shall not exceed two feet.

C. General Criteria

1. Storm drains with tributary areas of less than 640 acres are to be designed for a minimum of 10-year frequency below top of curb



NOTE

*For Arterial Hwy and Local Street, depth times velocity cannot exceed six

** The elevation of the lowest floor of buildings, including basements or cellars, must be at least 1 foot above the 100-year flood water surface elevation pursuant to Section 7-9-113.5 of the County Ordinance.

ORANGE COUNTY E.M.A.		
FLOOD PROTECTION GOALS		
1986	1 OF 1	

B.1 APPENDIX B – Rational Method Hydrology Calculations

Rational Method – 2-Year Storm Event: Existing Condition

 RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE
 (Reference: 1986 ORANGE COUNTY HYDROLOGY CRITERION)
 (c) Copyright 1983-2016 Advanced Engineering Software (aes)
 Ver. 23.0 Release Date: 07/01/2016 License ID 1535

Analysis prepared by:

Stantec

***** DESCRIPTION OF STUDY *****
 * Culver Alton - 2 Year Rational Method Study, Existing Conditions *
 * DMA 1: North Intersection Streamline, Culver to Alton *
 * 10/15/2019 - ECS *

FILE NAME: CA2DMA1.DAT
 TIME/DATE OF STUDY: 11:17 10/15/2019

=====

USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:

=====

--*TIME-OF-CONCENTRATION MODEL*--

USER SPECIFIED STORM EVENT(YEAR) = 2.00
 SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00
 SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.95
 DATA BANK RAINFALL USED
 ANTECEDENT MOISTURE CONDITION (AMC) I ASSUMED FOR RATIONAL METHOD

USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL

NO.	HALF- WIDTH	CROWN TO CROSSFALL	STREET-CROSSFALL: IN- / OUT-/PARK- SIDE / SIDE/ WAY	CURB HEIGHT	GUTTER-GEOMETRIES: WIDTH LIP HIKE	MANNING FACTOR
	(FT)	(FT)		(FT)	(FT) (FT) (FT)	(n)
1	30.0	20.0	0.018/0.018/0.020	0.67	2.00 0.0312 0.167	0.0150
2	40.0	30.0	0.018/0.018/0.020	0.67	2.00 0.0312 0.167	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:
 1. Relative Flow-Depth = 0.00 FEET
 as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
 2. (Depth)*(Velocity) Constraint = 6.0 (FT*FT/S)
 *SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
 OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*
 *USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

FLOW PROCESS FROM NODE 1.01 TO NODE 1.03 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
 >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 330.00
 ELEVATION DATA: UPSTREAM(FEET) = 75.00 DOWNSTREAM(FEET) = 73.00

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$
 SUBAREA ANALYSIS USED MINIMUM T_c (MIN.) = 8.586
 * 2 YEAR RAINFALL INTENSITY(INCH/HR) = 1.660
 SUBAREA T_c AND LOSS RATE DATA(AMC I):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	F_p (INCH/HR)	A_p (DECIMAL)	SCS CN	T_c (MIN.)
COMMERCIAL	A	0.41	0.40	0.100	17	8.59
PUBLIC PARK	A	0.27	0.40	0.850	17	13.64

SUBAREA AVERAGE PERVIOUS LOSS RATE, F_p (INCH/HR) = 0.40
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, A_p = 0.398
 SUBAREA RUNOFF(CFS) = 0.92
 TOTAL AREA(ACRES) = 0.68 PEAK FLOW RATE(CFS) = 0.92

FLOW PROCESS FROM NODE 1.03 TO NODE 1.05 IS CODE = 62

2DMA1E.RES

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<

=====

UPSTREAM ELEVATION(FEET) = 73.00 DOWNSTREAM ELEVATION(FEET) = 68.00
STREET LENGTH(FEET) = 355.96 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.56
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.29
HALFSTREET FLOOD WIDTH(FEET) = 7.34
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.31
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.68
STREET FLOW TRAVEL TIME(MIN.) = 2.57 Tc(MIN.) = 11.16
* 2 YEAR RAINFALL INTENSITY(INCH/HR) = 1.428
SUBAREA LOSS RATE DATA(AMC I):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
COMMERCIAL B 0.12 0.30 0.100 36
COMMERCIAL A 0.56 0.40 0.100 17
PUBLIC PARK B 0.20 0.30 0.850 36
PUBLIC PARK A 0.22 0.40 0.850 17
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.36
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.386
SUBAREA AREA(ACRES) = 1.10 SUBAREA RUNOFF(CFS) = 1.28
EFFECTIVE AREA(ACRES) = 1.78 AREA-AVERAGED Fm(INCH/HR) = 0.15
AREA-AVERAGED Fp(INCH/HR) = 0.37 AREA-AVERAGED Ap = 0.39
TOTAL AREA(ACRES) = 1.8 PEAK FLOW RATE(CFS) = 2.05

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.31 HALFSTREET FLOOD WIDTH(FEET) = 8.53
FLOW VELOCITY(FEET/SEC.) = 2.43 DEPTH*VELOCITY(FT*FT/SEC.) = 0.77
LONGEST FLOWPATH FROM NODE 1.01 TO NODE 1.05 = 685.96 FEET.

FLOW PROCESS FROM NODE 1.05 TO NODE 1.07 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<

=====

UPSTREAM ELEVATION(FEET) = 68.00 DOWNSTREAM ELEVATION(FEET) = 65.50
STREET LENGTH(FEET) = 162.78 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.31
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.32
HALFSTREET FLOOD WIDTH(FEET) = 8.84
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.59
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.83
STREET FLOW TRAVEL TIME(MIN.) = 1.05 Tc(MIN.) = 12.20
* 2 YEAR RAINFALL INTENSITY(INCH/HR) = 1.356
SUBAREA LOSS RATE DATA(AMC I):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
COMMERCIAL B 0.14 0.30 0.100 36

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                                2DMA1E.RES
COMMERCIAL          A      0.13      0.40      0.100      17
PUBLIC PARK         B      0.10      0.30      0.850      36
PUBLIC PARK         A      0.10      0.40      0.850      17
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.35
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.419
SUBAREA AREA(ACRES) = 0.47      SUBAREA RUNOFF(CFS) = 0.51
EFFECTIVE AREA(ACRES) = 2.25      AREA-AVERAGED Fm(INCH/HR) = 0.15
AREA-AVERAGED Fp(INCH/HR) = 0.37      AREA-AVERAGED Ap = 0.40
TOTAL AREA(ACRES) = 2.2      PEAK FLOW RATE(CFS) = 2.45

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END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH( FEET ) = 0.32      HALFSTREET FLOOD WIDTH( FEET ) = 9.09
FLOW VELOCITY( FEET/SEC. ) = 2.63      DEPTH*VELOCITY( FT*FT/SEC. ) = 0.85
LONGEST FLOWPATH FROM NODE 1.01 TO NODE 1.07 = 848.74 FEET.

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=====
END OF STUDY SUMMARY:
TOTAL AREA(ACRES) = 2.2      TC(MIN.) = 12.20
EFFECTIVE AREA(ACRES) = 2.25      AREA-AVERAGED Fm(INCH/HR)= 0.15
AREA-AVERAGED Fp(INCH/HR) = 0.37      AREA-AVERAGED Ap = 0.397
PEAK FLOW RATE(CFS) = 2.45
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END OF RATIONAL METHOD ANALYSIS

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Analysis prepared by:

Stantec

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***** DESCRIPTION OF STUDY *****
* Culver Alton - 2 Year Rational Method Study, Existing Conditions *
* DMA 2: West Intersection Streamline, Alton *
* 10/15/2019 - ECS *
*****
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FILE NAME: CA2DMA2.DAT
TIME/DATE OF STUDY: 11:21 10/15/2019

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=====
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:
=====
--*TIME-OF-CONCENTRATION MODEL*--
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USER SPECIFIED STORM EVENT(YEAR) = 2.00
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.95
DATA BANK RAINFALL USED
ANTECEDENT MOISTURE CONDITION (AMC) I ASSUMED FOR RATIONAL METHOD

USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL

NO.	HALF- WIDTH (FT)	CROWN TO CROSSFALL (FT)	STREET-CROSSFALL: IN- / OUT-/PARK- SIDE / SIDE/ WAY	CURB HEIGHT (FT)	GUTTER-GEOMETRIES:			MANNING FACTOR (n)
					WIDTH (FT)	LIP (FT)	HIKE (FT)	
1	30.0	20.0	0.018/0.018/0.020	0.67	2.00	0.0312	0.167	0.0150
2	40.0	30.0	0.018/0.018/0.020	0.67	2.00	0.0312	0.167	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:
1. Relative Flow-Depth = 0.00 FEET
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)*(Velocity) Constraint = 6.0 (FT*FT/S)
*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*
*USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

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*****
FLOW PROCESS FROM NODE 2.01 TO NODE 2.03 IS CODE = 21
*****
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>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<
=====
INITIAL SUBAREA FLOW-LENGTH(FEET) = 330.00
ELEVATION DATA: UPSTREAM(FEET) = 72.00 DOWNSTREAM(FEET) = 68.00
```

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$
SUBAREA ANALYSIS USED MINIMUM T_c (MIN.) = 7.474
* 2 YEAR RAINFALL INTENSITY(INCH/HR) = 1.797
SUBAREA T_c AND LOSS RATE DATA(AMC I):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	F_p (INCH/HR)	A_p (DECIMAL)	SCS CN	T_c (MIN.)
PUBLIC PARK	B	0.01	0.30	0.850	36	11.88
PUBLIC PARK	A	0.27	0.40	0.850	17	11.88
COMMERCIAL	B	0.07	0.30	0.100	36	7.47
COMMERCIAL	A	0.40	0.40	0.100	17	7.47

SUBAREA AVERAGE PERVIOUS LOSS RATE, F_p (INCH/HR) = 0.39
SUBAREA AVERAGE PERVIOUS AREA FRACTION, A_p = 0.380
SUBAREA RUNOFF(CFS) = 1.11
TOTAL AREA(ACRES) = 0.75 PEAK FLOW RATE(CFS) = 1.11

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*****
Page 1
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                                2DMA2E.RES
FLOW PROCESS FROM NODE      2.03 TO NODE      2.05 IS CODE = 62
-----
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<
=====
UPSTREAM ELEVATION(FEET) = 68.00 DOWNSTREAM ELEVATION(FEET) = 62.00
STREET LENGTH(FEET) = 440.15 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.70
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.30
HALFSTREET FLOOD WIDTH(FEET) = 7.72
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.34
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.70
STREET FLOW TRAVEL TIME(MIN.) = 3.14 Tc(MIN.) = 10.61
* 2 YEAR RAINFALL INTENSITY(INCH/HR) = 1.470
SUBAREA LOSS RATE DATA(AMC I):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
COMMERCIAL B 0.22 0.30 0.100 36
COMMERCIAL A 0.27 0.40 0.100 17
PUBLIC PARK B 0.23 0.30 0.850 36
PUBLIC PARK A 0.28 0.40 0.850 17
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.35
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.483
SUBAREA AREA(ACRES) = 1.00 SUBAREA RUNOFF(CFS) = 1.17
EFFECTIVE AREA(ACRES) = 1.75 AREA-AVERAGED Fm(INCH/HR) = 0.16
AREA-AVERAGED Fp(INCH/HR) = 0.37 AREA-AVERAGED Ap = 0.44
TOTAL AREA(ACRES) = 1.8 PEAK FLOW RATE(CFS) = 2.06

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.32 HALFSTREET FLOOD WIDTH(FEET) = 8.59
FLOW VELOCITY(FEET/SEC.) = 2.41 DEPTH*VELOCITY(FT*FT/SEC.) = 0.76
LONGEST FLOWPATH FROM NODE 2.01 TO NODE 2.05 = 770.15 FEET.
=====
END OF STUDY SUMMARY:
TOTAL AREA(ACRES) = 1.8 TC(MIN.) = 10.61
EFFECTIVE AREA(ACRES) = 1.75 AREA-AVERAGED Fm(INCH/HR) = 0.16
AREA-AVERAGED Fp(INCH/HR) = 0.37 AREA-AVERAGED Ap = 0.439
PEAK FLOW RATE(CFS) = 2.06
=====
END OF RATIONAL METHOD ANALYSIS

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Analysis prepared by:

Stantec

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***** DESCRIPTION OF STUDY *****
* Culver Alton - 2 Year Rational Method Study, Existing Conditions *
* DMA 3: South Intersection Streamline, Alton *
* 11/07/2019 - ECS *
*****

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FILE NAME: 2DMA3E.DAT
TIME/DATE OF STUDY: 16:41 11/07/2019

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USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:

=====

--*TIME-OF-CONCENTRATION MODEL*--

USER SPECIFIED STORM EVENT(YEAR) = 2.00
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.95
DATA BANK RAINFALL USED
ANTECEDENT MOISTURE CONDITION (AMC) I ASSUMED FOR RATIONAL METHOD

USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL

NO.	HALF- WIDTH (FT)	CROWN TO CROSSFALL (FT)	STREET-CROSSFALL: IN- / OUT-/PARK- SIDE / SIDE/ WAY	CURB HEIGHT (FT)	GUTTER-GEOMETRIES:			MANNING FACTOR (n)
					WIDTH (FT)	LIP (FT)	HIKE (FT)	
1	30.0	20.0	0.018/0.018/0.020	0.67	2.00	0.0312	0.167	0.0150
2	40.0	30.0	0.018/0.018/0.020	0.67	2.00	0.0312	0.167	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:
1. Relative Flow-Depth = 0.00 FEET
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)*(Velocity) Constraint = 6.0 (FT*FT/S)
*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*
*USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

FLOW PROCESS FROM NODE 3.01 TO NODE 3.03 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 308.42
ELEVATION DATA: UPSTREAM(FEET) = 82.00 DOWNSTREAM(FEET) = 77.00

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$
SUBAREA ANALYSIS USED MINIMUM T_c (MIN.) = 6.864
* 2 YEAR RAINFALL INTENSITY(INCH/HR) = 1.887
SUBAREA T_c AND LOSS RATE DATA(AMC I):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	F_p (INCH/HR)	A_p (DECIMAL)	SCS CN	T_c (MIN.)
COMMERCIAL	A	0.26	0.40	0.100	17	6.86
PUBLIC PARK	A	0.22	0.40	0.850	17	10.91

SUBAREA AVERAGE PERVIOUS LOSS RATE, F_p (INCH/HR) = 0.40
SUBAREA AVERAGE PERVIOUS AREA FRACTION, A_p = 0.444
SUBAREA RUNOFF(CFS) = 0.74
TOTAL AREA(ACRES) = 0.48 PEAK FLOW RATE(CFS) = 0.74

FLOW PROCESS FROM NODE 3.03 TO NODE 3.05 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<

=====

UPSTREAM ELEVATION(FEET) = 77.00 DOWNSTREAM ELEVATION(FEET) = 72.00
STREET LENGTH(FEET) = 500.82 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curb-to-curb) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.36
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.30
HALFSTREET FLOOD WIDTH(FEET) = 7.47
AVERAGE FLOW VELOCITY(FEET/SEC.) = 1.96
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.58
STREET FLOW TRAVEL TIME(MIN.) = 4.26 Tc(MIN.) = 11.12
* 2 YEAR RAINFALL INTENSITY(INCH/HR) = 1.430

SUBAREA LOSS RATE DATA(AMC I):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	A	0.53	0.40	0.100	17
PUBLIC PARK	A	0.57	0.40	0.850	17

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.40
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.489
SUBAREA AREA(ACRES) = 1.10 SUBAREA RUNOFF(CFS) = 1.22
EFFECTIVE AREA(ACRES) = 1.58 AREA-AVERAGED Fm(INCH/HR) = 0.19
AREA-AVERAGED Fp(INCH/HR) = 0.40 AREA-AVERAGED Ap = 0.48
TOTAL AREA(ACRES) = 1.6 PEAK FLOW RATE(CFS) = 1.76

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.32 HALFSTREET FLOOD WIDTH(FEET) = 8.59
FLOW VELOCITY(FEET/SEC.) = 2.07 DEPTH*VELOCITY(FT*FT/SEC.) = 0.65
LONGEST FLOWPATH FROM NODE 3.01 TO NODE 3.05 = 809.24 FEET.

FLOW PROCESS FROM NODE 3.05 TO NODE 3.05 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

=====

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 11.12
RAINFALL INTENSITY(INCH/HR) = 1.43
AREA-AVERAGED Fm(INCH/HR) = 0.19
AREA-AVERAGED Fp(INCH/HR) = 0.40
AREA-AVERAGED Ap = 0.48
EFFECTIVE STREAM AREA(ACRES) = 1.58
TOTAL STREAM AREA(ACRES) = 1.58
PEAK FLOW RATE(CFS) AT CONFLUENCE = 1.76

FLOW PROCESS FROM NODE 6.01 TO NODE 6.03 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 237.14
ELEVATION DATA: UPSTREAM(FEET) = 73.50 DOWNSTREAM(FEET) = 72.50

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 8.089
* 2 YEAR RAINFALL INTENSITY(INCH/HR) = 1.718
SUBAREA Tc AND LOSS RATE DATA(AMC I):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
PUBLIC PARK	D	0.07	0.20	0.850	57	12.85
COMMERCIAL	D	0.38	0.20	0.100	57	8.09

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                                2DMA3E.RES
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.217
SUBAREA RUNOFF(CFS) = 0.68
TOTAL AREA(ACRES) = 0.45 PEAK FLOW RATE(CFS) = 0.68
*****
FLOW PROCESS FROM NODE 6.03 TO NODE 3.05 IS CODE = 62
-----
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<
=====
UPSTREAM ELEVATION(FEET) = 72.50 DOWNSTREAM ELEVATION(FEET) = 72.00
STREET LENGTH(FEET) = 276.24 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curb) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.91
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.33
HALFSTREET FLOOD WIDTH(FEET) = 9.47
AVERAGE FLOW VELOCITY(FEET/SEC.) = 0.91
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.30
STREET FLOW TRAVEL TIME(MIN.) = 5.05 Tc(MIN.) = 13.14
* 2 YEAR RAINFALL INTENSITY(INCH/HR) = 1.300
SUBAREA LOSS RATE DATA(AMC I ):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
PUBLIC PARK A 0.03 0.40 0.850 17
COMMERCIAL A 0.25 0.40 0.100 17
COMMERCIAL B 0.09 0.30 0.100 36
PUBLIC PARK D 0.02 0.20 0.850 57
COMMERCIAL D 0.02 0.20 0.100 57
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.34
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.191
SUBAREA AREA(ACRES) = 0.41 SUBAREA RUNOFF(CFS) = 0.46
EFFECTIVE AREA(ACRES) = 0.86 AREA-AVERAGED Fm(INCH/HR) = 0.05
AREA-AVERAGED Fp(INCH/HR) = 0.26 AREA-AVERAGED Ap = 0.20
TOTAL AREA(ACRES) = 0.9 PEAK FLOW RATE(CFS) = 0.96

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.34 HALFSTREET FLOOD WIDTH(FEET) = 9.72
FLOW VELOCITY(FEET/SEC.) = 0.93 DEPTH*VELOCITY(FT*FT/SEC.) = 0.31
LONGEST FLOWPATH FROM NODE 6.01 TO NODE 3.05 = 513.38 FEET.
*****
FLOW PROCESS FROM NODE 6.03 TO NODE 3.05 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 13.14
RAINFALL INTENSITY(INCH/HR) = 1.30
AREA-AVERAGED Fm(INCH/HR) = 0.05
AREA-AVERAGED Fp(INCH/HR) = 0.26
AREA-AVERAGED Ap = 0.20
EFFECTIVE STREAM AREA(ACRES) = 0.86
TOTAL STREAM AREA(ACRES) = 0.86
PEAK FLOW RATE(CFS) AT CONFLUENCE = 0.96

** CONFLUENCE DATA **
STREAM Q Tc Intensity Fp(Fm) Ap Ae HEADWATER
NUMBER (CFS) (MIN.) (INCH/HR) (INCH/HR) (ACRES) NODE
1 1.76 11.12 1.430 0.40( 0.19) 0.48 1.6 3.01
2 0.96 13.14 1.300 0.26( 0.05) 0.20 0.9 6.01

```

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	2.67	11.12	1.430	0.38(0.15)	0.39	2.3	3.01
2	2.54	13.14	1.300	0.37(0.14)	0.38	2.4	6.01

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 2.67 Tc(MIN.) = 11.12
EFFECTIVE AREA(ACRES) = 2.31 AREA-AVERAGED Fm(INCH/HR) = 0.15
AREA-AVERAGED Fp(INCH/HR) = 0.38 AREA-AVERAGED Ap = 0.39
TOTAL AREA(ACRES) = 2.4
LONGEST FLOWPATH FROM NODE 3.01 TO NODE 3.05 = 809.24 FEET.

END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 2.4 TC(MIN.) = 11.12
EFFECTIVE AREA(ACRES) = 2.31 AREA-AVERAGED Fm(INCH/HR) = 0.15
AREA-AVERAGED Fp(INCH/HR) = 0.38 AREA-AVERAGED Ap = 0.390
PEAK FLOW RATE(CFS) = 2.67

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	2.67	11.12	1.430	0.38(0.15)	0.39	2.3	3.01
2	2.54	13.14	1.300	0.37(0.14)	0.38	2.4	6.01

END OF RATIONAL METHOD ANALYSIS

↑

 RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE
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Analysis prepared by:

Stantec

***** DESCRIPTION OF STUDY *****
 * Culver Alton - 2 Year Rational Method Study, Existing Conditions *
 * DMA 4: East Intersection Streamline, Yale to Alton to Culver *
 * 11/07/2019 - ECS *

FILE NAME: 2DMA4E.DAT
 TIME/DATE OF STUDY: 16:50 11/07/2019

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USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:

=====

--*TIME-OF-CONCENTRATION MODEL*--

USER SPECIFIED STORM EVENT(YEAR) = 2.00
 SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00
 SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.95
 DATA BANK RAINFALL USED
 ANTECEDENT MOISTURE CONDITION (AMC) I ASSUMED FOR RATIONAL METHOD

USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL

NO.	HALF- WIDTH (FT)	CROWN TO CROSSFALL (FT)	STREET-CROSSFALL: IN- / OUT-/PARK- SIDE / SIDE/ WAY	CURB HEIGHT (FT)	GUTTER-GEOMETRIES:			MANNING FACTOR (n)
					WIDTH (FT)	LIP (FT)	HIKE (FT)	
1	30.0	20.0	0.018/0.018/0.020	0.67	2.00	0.0312	0.167	0.0150
2	40.0	30.0	0.018/0.018/0.020	0.67	2.00	0.0312	0.167	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:
 1. Relative Flow-Depth = 0.00 FEET
 as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
 2. (Depth)*(Velocity) Constraint = 6.0 (FT*FT/S)
 *SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
 OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*
 *USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

FLOW PROCESS FROM NODE 4.01 TO NODE 4.03 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
 >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 116.02
 ELEVATION DATA: UPSTREAM(FEET) = 89.00 DOWNSTREAM(FEET) = 87.00

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$
 SUBAREA ANALYSIS USED MINIMUM T_c (MIN.) = 5.000
 * 2 YEAR RAINFALL INTENSITY(INCH/HR) = 2.264
 SUBAREA T_c AND LOSS RATE DATA(AMC I):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	F_p (INCH/HR)	A_p (DECIMAL)	SCS CN	T_c (MIN.)
PUBLIC PARK	A	0.01	0.40	0.850	17	7.29
COMMERCIAL	A	0.13	0.40	0.100	17	5.00

SUBAREA AVERAGE PERVIOUS LOSS RATE, F_p (INCH/HR) = 0.40
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, A_p = 0.154
 SUBAREA RUNOFF(CFS) = 0.28
 TOTAL AREA(ACRES) = 0.14 PEAK FLOW RATE(CFS) = 0.28

FLOW PROCESS FROM NODE 4.03 TO NODE 4.05 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<

=====

UPSTREAM ELEVATION(FEET) = 87.00 DOWNSTREAM ELEVATION(FEET) = 80.00
STREET LENGTH(FEET) = 301.23 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.70
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.20
HALFSTREET FLOOD WIDTH(FEET) = 2.00
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.31
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.66
STREET FLOW TRAVEL TIME(MIN.) = 1.52 Tc(MIN.) = 6.52
* 2 YEAR RAINFALL INTENSITY(INCH/HR) = 1.944
SUBAREA LOSS RATE DATA(AMC I):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
PUBLIC PARK	A	0.07	0.40	0.850	17
COMMERCIAL	A	0.44	0.40	0.100	17

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.40
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.203
SUBAREA AREA(ACRES) = 0.51 SUBAREA RUNOFF(CFS) = 0.86
EFFECTIVE AREA(ACRES) = 0.65 AREA-AVERAGED Fm(INCH/HR) = 0.08
AREA-AVERAGED Fp(INCH/HR) = 0.40 AREA-AVERAGED Ap = 0.19
TOTAL AREA(ACRES) = 0.6 PEAK FLOW RATE(CFS) = 1.09

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.25 HALFSTREET FLOOD WIDTH(FEET) = 4.72
FLOW VELOCITY(FEET/SEC.) = 2.78 DEPTH*VELOCITY(FT*FT/SEC.) = 0.69
LONGEST FLOWPATH FROM NODE 4.01 TO NODE 4.05 = 417.25 FEET.

FLOW PROCESS FROM NODE 4.05 TO NODE 4.07 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<

=====

UPSTREAM ELEVATION(FEET) = 80.00 DOWNSTREAM ELEVATION(FEET) = 75.00
STREET LENGTH(FEET) = 369.87 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.64
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.30
HALFSTREET FLOOD WIDTH(FEET) = 7.59
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.31
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.69
STREET FLOW TRAVEL TIME(MIN.) = 2.66 Tc(MIN.) = 9.18
* 2 YEAR RAINFALL INTENSITY(INCH/HR) = 1.597
SUBAREA LOSS RATE DATA(AMC I):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	A	0.27	0.40	0.100	17
PUBLIC PARK	A	0.63	0.40	0.850	17

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.40

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                                2DMA4E.RES
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.625
SUBAREA AREA(ACRES) = 0.90 SUBAREA RUNOFF(CFS) = 1.09
EFFECTIVE AREA(ACRES) = 1.55 AREA-AVERAGED Fm(INCH/HR) = 0.18
AREA-AVERAGED Fp(INCH/HR) = 0.40 AREA-AVERAGED Ap = 0.44
TOTAL AREA(ACRES) = 1.5 PEAK FLOW RATE(CFS) = 1.98

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.31 HALFSTREET FLOOD WIDTH(FEET) = 8.41
FLOW VELOCITY(FEET/SEC.) = 2.40 DEPTH*VELOCITY(FT*FT/SEC.) = 0.75
LONGEST FLOWPATH FROM NODE 4.01 TO NODE 4.07 = 787.12 FEET.

*****
FLOW PROCESS FROM NODE 4.07 TO NODE 4.09 IS CODE = 62
-----
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<
=====
UPSTREAM ELEVATION(FEET) = 75.00 DOWNSTREAM ELEVATION(FEET) = 72.00
STREET LENGTH(FEET) = 362.03 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.38
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.35
HALFSTREET FLOOD WIDTH(FEET) = 10.43
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.04
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.71
STREET FLOW TRAVEL TIME(MIN.) = 2.95 Tc(MIN.) = 12.14
* 2 YEAR RAINFALL INTENSITY(INCH/HR) = 1.361
SUBAREA LOSS RATE DATA(AMC I):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
COMMERCIAL A 0.37 0.40 0.100 17
PUBLIC PARK A 0.39 0.40 0.850 17
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.40
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.485
SUBAREA AREA(ACRES) = 0.76 SUBAREA RUNOFF(CFS) = 0.80
EFFECTIVE AREA(ACRES) = 2.31 AREA-AVERAGED Fm(INCH/HR) = 0.18
AREA-AVERAGED Fp(INCH/HR) = 0.40 AREA-AVERAGED Ap = 0.46
TOTAL AREA(ACRES) = 2.3 PEAK FLOW RATE(CFS) = 2.45

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.35 HALFSTREET FLOOD WIDTH(FEET) = 10.59
FLOW VELOCITY(FEET/SEC.) = 2.05 DEPTH*VELOCITY(FT*FT/SEC.) = 0.72
LONGEST FLOWPATH FROM NODE 4.01 TO NODE 4.09 = 1149.15 FEET.

*****
FLOW PROCESS FROM NODE 4.09 TO NODE 4.09 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 12.14
RAINFALL INTENSITY(INCH/HR) = 1.36
AREA-AVERAGED Fm(INCH/HR) = 0.18
AREA-AVERAGED Fp(INCH/HR) = 0.40
AREA-AVERAGED Ap = 0.46
EFFECTIVE STREAM AREA(ACRES) = 2.31
TOTAL STREAM AREA(ACRES) = 2.31
PEAK FLOW RATE(CFS) AT CONFLUENCE = 2.45

*****
FLOW PROCESS FROM NODE 5.01 TO NODE 5.03 IS CODE = 21
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>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<
=====
INITIAL SUBAREA FLOW-LENGTH( FEET ) =    253.47
ELEVATION DATA: UPSTREAM( FEET ) =    75.00  DOWNSTREAM( FEET ) =    73.50

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) =    7.763
*   2 YEAR RAINFALL INTENSITY(INCH/HR) =    1.759
SUBAREA Tc AND LOSS RATE DATA(AMC I ):
DEVELOPMENT TYPE/      SCS SOIL  AREA      Fp      Ap      SCS  Tc
LAND USE              GROUP  (ACRES)  (INCH/HR)  (DECIMAL)  CN  (MIN.)
COMMERCIAL             A         0.21     0.40     0.100     17   7.76
PUBLIC PARK            A         0.27     0.40     0.850     17  12.33
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) =    0.40
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap =    0.522
SUBAREA RUNOFF(CFS) =    0.67
TOTAL AREA(ACRES) =    0.48  PEAK FLOW RATE(CFS) =    0.67

*****
FLOW PROCESS FROM NODE    5.03 TO NODE    5.05 IS CODE =    62
-----
>>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>(STREET TABLE SECTION # 1 USED)<<<<<
=====
UPSTREAM ELEVATION( FEET ) =    73.50  DOWNSTREAM ELEVATION( FEET ) =    72.00
STREET LENGTH( FEET ) =    273.08  CURB HEIGHT( INCHES ) =    8.0
STREET HALFWIDTH( FEET ) =    30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK( FEET ) =    20.00
INSIDE STREET CROSSFALL( DECIMAL ) =    0.018
OUTSIDE STREET CROSSFALL( DECIMAL ) =    0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF =    1
STREET PARKWAY CROSSFALL( DECIMAL ) =    0.020
Manning's FRICTION FACTOR for Streetflow Section( curb-to-curb ) =    0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section =    0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) =    1.05
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH( FEET ) =    0.30
HALFSTREET FLOOD WIDTH( FEET ) =    7.66
AVERAGE FLOW VELOCITY( FEET/SEC. ) =    1.46
PRODUCT OF DEPTH&VELOCITY( FT*FT/SEC. ) =    0.44
STREET FLOW TRAVEL TIME( MIN. ) =    3.11  Tc( MIN. ) =    10.88
*   2 YEAR RAINFALL INTENSITY(INCH/HR) =    1.449
SUBAREA LOSS RATE DATA(AMC I ):
DEVELOPMENT TYPE/      SCS SOIL  AREA      Fp      Ap      SCS
LAND USE              GROUP  (ACRES)  (INCH/HR)  (DECIMAL)  CN
COMMERCIAL             A         0.43     0.40     0.100     17
PUBLIC PARK            A         0.21     0.40     0.850     17
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) =    0.40
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap =    0.346
SUBAREA AREA( ACRES ) =    0.64  SUBAREA RUNOFF(CFS) =    0.75
EFFECTIVE AREA( ACRES ) =    1.12  AREA-AVERAGED Fm(INCH/HR) =    0.17
AREA-AVERAGED Fp(INCH/HR) =    0.40  AREA-AVERAGED Ap =    0.42
TOTAL AREA( ACRES ) =    1.1  PEAK FLOW RATE(CFS) =    1.29

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH( FEET ) =    0.31  HALFSTREET FLOOD WIDTH( FEET ) =    8.53
FLOW VELOCITY( FEET/SEC. ) =    1.53  DEPTH*VELOCITY( FT*FT/SEC. ) =    0.48
LONGEST FLOWPATH FROM NODE    5.01 TO NODE    5.05 =    526.55 FEET.

*****
FLOW PROCESS FROM NODE    5.05 TO NODE    4.09 IS CODE =    1
-----
>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<
=====
TOTAL NUMBER OF STREAMS =    2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION( MIN. ) =    10.88
RAINFALL INTENSITY(INCH/HR) =    1.45
AREA-AVERAGED Fm(INCH/HR) =    0.17

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AREA-AVERAGED F_p (INCH/HR) = 0.40
 AREA-AVERAGED A_p = 0.42
 EFFECTIVE STREAM AREA(ACRES) = 1.12
 TOTAL STREAM AREA(ACRES) = 1.12
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 1.29

** CONFLUENCE DATA **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	$F_p(F_m)$ (INCH/HR)	A_p	A_e (ACRES)	HEADWATER NODE
1	2.45	12.14	1.361	0.40(0.18)	0.46	2.3	4.01
2	1.29	10.88	1.449	0.40(0.17)	0.42	1.1	5.01

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	$F_p(F_m)$ (INCH/HR)	A_p	A_e (ACRES)	HEADWATER NODE
1	3.65	10.88	1.449	0.40(0.18)	0.44	3.2	5.01
2	3.65	12.14	1.361	0.40(0.18)	0.45	3.4	4.01

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 3.65 Tc(MIN.) = 12.14
 EFFECTIVE AREA(ACRES) = 3.43 AREA-AVERAGED F_m (INCH/HR) = 0.18
 AREA-AVERAGED F_p (INCH/HR) = 0.40 AREA-AVERAGED A_p = 0.45
 TOTAL AREA(ACRES) = 3.4
 LONGEST FLOWPATH FROM NODE 4.01 TO NODE 4.09 = 1149.15 FEET.

END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 3.4 TC(MIN.) = 12.14
 EFFECTIVE AREA(ACRES) = 3.43 AREA-AVERAGED F_m (INCH/HR) = 0.18
 AREA-AVERAGED F_p (INCH/HR) = 0.40 AREA-AVERAGED A_p = 0.445
 PEAK FLOW RATE(CFS) = 3.65

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	$F_p(F_m)$ (INCH/HR)	A_p	A_e (ACRES)	HEADWATER NODE
1	3.65	10.88	1.449	0.40(0.18)	0.44	3.2	5.01
2	3.65	12.14	1.361	0.40(0.18)	0.45	3.4	4.01

END OF RATIONAL METHOD ANALYSIS

Rational Method – 2-Year Storm Event: Proposed Condition

 RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE
 (Reference: 1986 ORANGE COUNTY HYDROLOGY CRITERION)
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Analysis prepared by:

Stantec

***** DESCRIPTION OF STUDY *****
 * Culver Alton - 2 Year Rational Method Study, Proposed Conditions *
 * DMA 1: North Intersection Streamline, Culver to Alton *
 * 11/07/2019 - ECS *

FILE NAME: 2DMA1P.DAT
 TIME/DATE OF STUDY: 16:58 11/07/2019

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USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:

=====

--*TIME-OF-CONCENTRATION MODEL*--

USER SPECIFIED STORM EVENT(YEAR) = 2.00
 SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00
 SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.95
 DATA BANK RAINFALL USED
 ANTECEDENT MOISTURE CONDITION (AMC) I ASSUMED FOR RATIONAL METHOD

USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL

NO.	HALF-	CROWN TO	STREET-CROSSFALL:	CURB	GUTTER-GEOMETRIES:			MANNING
	WIDTH	CROSSFALL	IN- / OUT-/PARK-	HEIGHT	WIDTH	LIP	HIKE	FACTOR
	(FT)	(FT)	SIDE / SIDE/ WAY	(FT)	(FT)	(FT)	(FT)	(n)
1	30.0	20.0	0.018/0.018/0.020	0.67	2.00	0.0312	0.167	0.0150
2	40.0	30.0	0.018/0.018/0.020	0.67	2.00	0.0312	0.167	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:
 1. Relative Flow-Depth = 0.00 FEET
 as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
 2. (Depth)*(Velocity) Constraint = 6.0 (FT*FT/S)
 *SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
 OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*
 *USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

FLOW PROCESS FROM NODE 1.01 TO NODE 1.03 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
 >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 330.00
 ELEVATION DATA: UPSTREAM(FEET) = 75.00 DOWNSTREAM(FEET) = 73.00

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$
 SUBAREA ANALYSIS USED MINIMUM T_c (MIN.) = 8.586
 * 2 YEAR RAINFALL INTENSITY(INCH/HR) = 1.660
 SUBAREA T_c AND LOSS RATE DATA(AMC I):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	F_p (INCH/HR)	A_p (DECIMAL)	SCS CN	T_c (MIN.)
COMMERCIAL	A	0.41	0.40	0.100	17	8.59
PUBLIC PARK	A	0.27	0.40	0.850	17	13.64

SUBAREA AVERAGE PERVIOUS LOSS RATE, F_p (INCH/HR) = 0.40
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, A_p = 0.398
 SUBAREA RUNOFF(CFS) = 0.92
 TOTAL AREA(ACRES) = 0.68 PEAK FLOW RATE(CFS) = 0.92

FLOW PROCESS FROM NODE 1.03 TO NODE 1.05 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<

=====

UPSTREAM ELEVATION(FEET) = 73.00 DOWNSTREAM ELEVATION(FEET) = 68.00
STREET LENGTH(FEET) = 355.96 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.55
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.29
HALFSTREET FLOOD WIDTH(FEET) = 7.28
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.33
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.68
STREET FLOW TRAVEL TIME(MIN.) = 2.55 Tc(MIN.) = 11.13
* 2 YEAR RAINFALL INTENSITY(INCH/HR) = 1.430
SUBAREA LOSS RATE DATA(AMC I):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	B	0.12	0.30	0.100	36
COMMERCIAL	A	0.52	0.40	0.100	17
PUBLIC PARK	B	0.20	0.30	0.850	36
PUBLIC PARK	A	0.26	0.40	0.850	17

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.36
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.414
SUBAREA AREA(ACRES) = 1.10 SUBAREA RUNOFF(CFS) = 1.27
EFFECTIVE AREA(ACRES) = 1.78 AREA-AVERAGED Fm(INCH/HR) = 0.15
AREA-AVERAGED Fp(INCH/HR) = 0.37 AREA-AVERAGED Ap = 0.41
TOTAL AREA(ACRES) = 1.8 PEAK FLOW RATE(CFS) = 2.05

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.31 HALFSTREET FLOOD WIDTH(FEET) = 8.47
FLOW VELOCITY(FEET/SEC.) = 2.45 DEPTH*VELOCITY(FT*FT/SEC.) = 0.77
LONGEST FLOWPATH FROM NODE 1.01 TO NODE 1.05 = 685.96 FEET.

FLOW PROCESS FROM NODE 1.05 TO NODE 1.07 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<

=====

UPSTREAM ELEVATION(FEET) = 68.00 DOWNSTREAM ELEVATION(FEET) = 65.50
STREET LENGTH(FEET) = 162.78 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.30
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.32
HALFSTREET FLOOD WIDTH(FEET) = 8.84
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.58
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.83
STREET FLOW TRAVEL TIME(MIN.) = 1.05 Tc(MIN.) = 12.19
* 2 YEAR RAINFALL INTENSITY(INCH/HR) = 1.357
SUBAREA LOSS RATE DATA(AMC I):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	B	0.14	0.30	0.100	36

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                                2DMA1P.RES
COMMERCIAL          A      0.13      0.40      0.100      17
PUBLIC PARK         B      0.10      0.30      0.850      36
PUBLIC PARK         A      0.10      0.40      0.850      17
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.35
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.419
SUBAREA AREA(ACRES) = 0.47      SUBAREA RUNOFF(CFS) = 0.51
EFFECTIVE AREA(ACRES) = 2.25      AREA-AVERAGED Fm(INCH/HR) = 0.15
AREA-AVERAGED Fp(INCH/HR) = 0.37      AREA-AVERAGED Ap = 0.41
TOTAL AREA(ACRES) = 2.2      PEAK FLOW RATE(CFS) = 2.44

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END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.32      HALFSTREET FLOOD WIDTH(FEET) = 9.09
FLOW VELOCITY(FEET/SEC.) = 2.62      DEPTH*VELOCITY(FT*FT/SEC.) = 0.85
LONGEST FLOWPATH FROM NODE 1.01 TO NODE 1.07 = 848.74 FEET.

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=====
END OF STUDY SUMMARY:
TOTAL AREA(ACRES) = 2.2      TC(MIN.) = 12.19
EFFECTIVE AREA(ACRES) = 2.25      AREA-AVERAGED Fm(INCH/HR) = 0.15
AREA-AVERAGED Fp(INCH/HR) = 0.37      AREA-AVERAGED Ap = 0.410
PEAK FLOW RATE(CFS) = 2.44
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END OF RATIONAL METHOD ANALYSIS

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Analysis prepared by:

Stantec

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***** DESCRIPTION OF STUDY *****
* Culver Alton - 2 Year Rational Method Study, Proposed Conditions *
* DMA 2: West Intersection Streamline, Alton *
* 10/25/2019 - ECS *
*****

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FILE NAME: CA2DMA2.DAT
TIME/DATE OF STUDY: 14:06 10/25/2019

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=====
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:
=====
--*TIME-OF-CONCENTRATION MODEL*--

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USER SPECIFIED STORM EVENT(YEAR) = 2.00
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.95
DATA BANK RAINFALL USED
ANTECEDENT MOISTURE CONDITION (AMC) I ASSUMED FOR RATIONAL METHOD

USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL

NO.	HALF- WIDTH (FT)	CROWN TO CROSSFALL (FT)	STREET-CROSSFALL: IN- / OUT-/PARK- SIDE / SIDE/ WAY	CURB HEIGHT (FT)	GUTTER-GEOMETRIES: WIDTH LIP HIKE (FT) (FT) (FT)	MANNING FACTOR (n)
1	30.0	20.0	0.018/0.018/0.020	0.67	2.00 0.0312 0.167	0.0150
2	40.0	30.0	0.018/0.018/0.020	0.67	2.00 0.0312 0.167	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:
1. Relative Flow-Depth = 0.00 FEET
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)*(Velocity) Constraint = 6.0 (FT*FT/S)
*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*
*USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

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*****
FLOW PROCESS FROM NODE 2.01 TO NODE 2.03 IS CODE = 21

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>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<
=====
INITIAL SUBAREA FLOW-LENGTH(FEET) = 330.00
ELEVATION DATA: UPSTREAM(FEET) = 72.00 DOWNSTREAM(FEET) = 68.00

```

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$
SUBAREA ANALYSIS USED MINIMUM T_c (MIN.) = 7.474
* 2 YEAR RAINFALL INTENSITY(INCH/HR) = 1.797
SUBAREA T_c AND LOSS RATE DATA(AMC I):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	F_p (INCH/HR)	A_p (DECIMAL)	SCS CN	T_c (MIN.)
PUBLIC PARK	B	0.01	0.30	0.850	36	11.88
PUBLIC PARK	A	0.27	0.40	0.850	17	11.88
COMMERCIAL	B	0.07	0.30	0.100	36	7.47
COMMERCIAL	A	0.40	0.40	0.100	17	7.47

SUBAREA AVERAGE PERVIOUS LOSS RATE, F_p (INCH/HR) = 0.39
SUBAREA AVERAGE PERVIOUS AREA FRACTION, A_p = 0.380
SUBAREA RUNOFF(CFS) = 1.11
TOTAL AREA(ACRES) = 0.75 PEAK FLOW RATE(CFS) = 1.11

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Page 1

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                                2DMA2P.RES
FLOW PROCESS FROM NODE      2.03 TO NODE      2.05 IS CODE = 62
-----
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<
=====
UPSTREAM ELEVATION(FEET) = 68.00 DOWNSTREAM ELEVATION(FEET) = 62.00
STREET LENGTH(FEET) = 440.15 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.70
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.30
HALFSTREET FLOOD WIDTH(FEET) = 7.72
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.34
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.70
STREET FLOW TRAVEL TIME(MIN.) = 3.14 Tc(MIN.) = 10.61
* 2 YEAR RAINFALL INTENSITY(INCH/HR) = 1.470
SUBAREA LOSS RATE DATA(AMC I):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
COMMERCIAL B 0.22 0.30 0.100 36
COMMERCIAL A 0.27 0.40 0.100 17
PUBLIC PARK B 0.23 0.30 0.850 36
PUBLIC PARK A 0.28 0.40 0.850 17
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.35
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.483
SUBAREA AREA(ACRES) = 1.00 SUBAREA RUNOFF(CFS) = 1.17
EFFECTIVE AREA(ACRES) = 1.75 AREA-AVERAGED Fm(INCH/HR) = 0.16
AREA-AVERAGED Fp(INCH/HR) = 0.37 AREA-AVERAGED Ap = 0.44
TOTAL AREA(ACRES) = 1.8 PEAK FLOW RATE(CFS) = 2.06

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.32 HALFSTREET FLOOD WIDTH(FEET) = 8.59
FLOW VELOCITY(FEET/SEC.) = 2.41 DEPTH*VELOCITY(FT*FT/SEC.) = 0.76
LONGEST FLOWPATH FROM NODE 2.01 TO NODE 2.05 = 770.15 FEET.
=====
END OF STUDY SUMMARY:
TOTAL AREA(ACRES) = 1.8 TC(MIN.) = 10.61
EFFECTIVE AREA(ACRES) = 1.75 AREA-AVERAGED Fm(INCH/HR) = 0.16
AREA-AVERAGED Fp(INCH/HR) = 0.37 AREA-AVERAGED Ap = 0.439
PEAK FLOW RATE(CFS) = 2.06
=====
END OF RATIONAL METHOD ANALYSIS

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Analysis prepared by:

Stantec

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***** DESCRIPTION OF STUDY *****
* Culver Alton - 2 Year Rational Method Study, Proposed Conditions *
* DMA 3: South Intersection Streamline, Alton *
* 11/07/2019 - ECS *
*****
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FILE NAME: 2DMA3P.DAT

TIME/DATE OF STUDY: 17:04 11/07/2019

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=====
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:
=====
--*TIME-OF-CONCENTRATION MODEL*--
```

USER SPECIFIED STORM EVENT(YEAR) = 2.00
 SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00
 SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.95
 DATA BANK RAINFALL USED
 ANTECEDENT MOISTURE CONDITION (AMC) I ASSUMED FOR RATIONAL METHOD

USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL

NO.	HALF-CROWN TO STREET-CROSSFALL:		CURB HEIGHT (FT)	GUTTER-GEOMETRIES:			MANNING FACTOR (n)
	WIDTH (FT)	CROSSFALL (FT)		IN- / OUT- / PARK- SIDE / SIDE / WAY	WIDTH (FT)	LIP HIKE (FT)	
1	30.0	20.0	0.018/0.018/0.020	0.67	2.00	0.0312	0.167
2	40.0	30.0	0.018/0.018/0.020	0.67	2.00	0.0312	0.167

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET
 as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)*(Velocity) Constraint = 6.0 (FT*FT/S)

*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
 OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*

*USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

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*****
FLOW PROCESS FROM NODE 3.01 TO NODE 3.03 IS CODE = 21
-----
```

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

```
=====
INITIAL SUBAREA FLOW-LENGTH(FEET) = 308.42
ELEVATION DATA: UPSTREAM(FEET) = 82.00 DOWNSTREAM(FEET) = 77.00
```

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$

SUBAREA ANALYSIS USED MINIMUM T_c (MIN.) = 6.864

* 2 YEAR RAINFALL INTENSITY(INCH/HR) = 1.887

SUBAREA T_c AND LOSS RATE DATA(AMC I):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
COMMERCIAL	A	0.26	0.40	0.100	17	6.86
PUBLIC PARK	A	0.22	0.40	0.850	17	10.91

SUBAREA AVERAGE PERVIOUS LOSS RATE, F_p (INCH/HR) = 0.40

SUBAREA AVERAGE PERVIOUS AREA FRACTION, A_p = 0.444

SUBAREA RUNOFF(CFS) = 0.74

TOTAL AREA(ACRES) = 0.48 PEAK FLOW RATE(CFS) = 0.74

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*****
FLOW PROCESS FROM NODE 3.03 TO NODE 3.05 IS CODE = 62
-----
```

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<

=====

UPSTREAM ELEVATION(FEET) = 77.00 DOWNSTREAM ELEVATION(FEET) = 72.00
STREET LENGTH(FEET) = 500.82 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.36
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.30
HALFSTREET FLOOD WIDTH(FEET) = 7.47
AVERAGE FLOW VELOCITY(FEET/SEC.) = 1.96
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.58
STREET FLOW TRAVEL TIME(MIN.) = 4.26 Tc(MIN.) = 11.12
* 2 YEAR RAINFALL INTENSITY(INCH/HR) = 1.430

SUBAREA LOSS RATE DATA(AMC I):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	A	0.53	0.40	0.100	17
PUBLIC PARK	A	0.57	0.40	0.850	17

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.40
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.489
SUBAREA AREA(ACRES) = 1.10 SUBAREA RUNOFF(CFS) = 1.22
EFFECTIVE AREA(ACRES) = 1.58 AREA-AVERAGED Fm(INCH/HR) = 0.19
AREA-AVERAGED Fp(INCH/HR) = 0.40 AREA-AVERAGED Ap = 0.48
TOTAL AREA(ACRES) = 1.6 PEAK FLOW RATE(CFS) = 1.76

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.32 HALFSTREET FLOOD WIDTH(FEET) = 8.59
FLOW VELOCITY(FEET/SEC.) = 2.07 DEPTH*VELOCITY(FT*FT/SEC.) = 0.65
LONGEST FLOWPATH FROM NODE 3.01 TO NODE 3.05 = 809.24 FEET.

FLOW PROCESS FROM NODE 3.05 TO NODE 3.05 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

=====

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 11.12
RAINFALL INTENSITY(INCH/HR) = 1.43
AREA-AVERAGED Fm(INCH/HR) = 0.19
AREA-AVERAGED Fp(INCH/HR) = 0.40
AREA-AVERAGED Ap = 0.48
EFFECTIVE STREAM AREA(ACRES) = 1.58
TOTAL STREAM AREA(ACRES) = 1.58
PEAK FLOW RATE(CFS) AT CONFLUENCE = 1.76

FLOW PROCESS FROM NODE 6.01 TO NODE 6.03 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 237.14
ELEVATION DATA: UPSTREAM(FEET) = 73.50 DOWNSTREAM(FEET) = 72.50

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 8.089
* 2 YEAR RAINFALL INTENSITY(INCH/HR) = 1.718
SUBAREA Tc AND LOSS RATE DATA(AMC I):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
PUBLIC PARK	D	0.06	0.20	0.850	57	12.85
COMMERCIAL	D	0.39	0.20	0.100	57	8.09


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SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.200
SUBAREA RUNOFF(CFS) = 0.68
TOTAL AREA(ACRES) = 0.45 PEAK FLOW RATE(CFS) = 0.68

*****
FLOW PROCESS FROM NODE 6.03 TO NODE 3.05 IS CODE = 62
-----
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<
=====
UPSTREAM ELEVATION(FEET) = 72.50 DOWNSTREAM ELEVATION(FEET) = 72.00
STREET LENGTH(FEET) = 276.24 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curb) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.91
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.33
HALFSTREET FLOOD WIDTH(FEET) = 9.47
AVERAGE FLOW VELOCITY(FEET/SEC.) = 0.92
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.30
STREET FLOW TRAVEL TIME(MIN.) = 5.02 Tc(MIN.) = 13.11
* 2 YEAR RAINFALL INTENSITY(INCH/HR) = 1.302
SUBAREA LOSS RATE DATA(AMC I ):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
PUBLIC PARK A 0.01 0.40 0.850 17
COMMERCIAL A 0.27 0.40 0.100 17
COMMERCIAL B 0.09 0.30 0.100 36
PUBLIC PARK D 0.01 0.20 0.850 57
COMMERCIAL D 0.03 0.20 0.100 57
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.34
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.137
SUBAREA AREA(ACRES) = 0.41 SUBAREA RUNOFF(CFS) = 0.46
EFFECTIVE AREA(ACRES) = 0.86 AREA-AVERAGED Fm(INCH/HR) = 0.04
AREA-AVERAGED Fp(INCH/HR) = 0.25 AREA-AVERAGED Ap = 0.17
TOTAL AREA(ACRES) = 0.9 PEAK FLOW RATE(CFS) = 0.97

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.34 HALFSTREET FLOOD WIDTH(FEET) = 9.78
FLOW VELOCITY(FEET/SEC.) = 0.93 DEPTH*VELOCITY(FT*FT/SEC.) = 0.31
LONGEST FLOWPATH FROM NODE 6.01 TO NODE 3.05 = 513.38 FEET.

*****
FLOW PROCESS FROM NODE 6.03 TO NODE 3.05 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 13.11
RAINFALL INTENSITY(INCH/HR) = 1.30
AREA-AVERAGED Fm(INCH/HR) = 0.04
AREA-AVERAGED Fp(INCH/HR) = 0.25
AREA-AVERAGED Ap = 0.17
EFFECTIVE STREAM AREA(ACRES) = 0.86
TOTAL STREAM AREA(ACRES) = 0.86
PEAK FLOW RATE(CFS) AT CONFLUENCE = 0.97

** CONFLUENCE DATA **
STREAM Q Tc Intensity Fp(Fm) Ap Ae HEADWATER
NUMBER (CFS) (MIN.) (INCH/HR) (INCH/HR) (ACRES) NODE
1 1.76 11.12 1.430 0.40( 0.19) 0.48 1.6 3.01
2 0.97 13.11 1.302 0.25( 0.04) 0.17 0.9 6.01

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2DMA3P.RES

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	2.68	11.12	1.430	0.38(0.14)	0.38	2.3	3.01
2	2.56	13.11	1.302	0.38(0.14)	0.37	2.4	6.01

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 2.68 Tc(MIN.) = 11.12
EFFECTIVE AREA(ACRES) = 2.31 AREA-AVERAGED Fm(INCH/HR) = 0.14
AREA-AVERAGED Fp(INCH/HR) = 0.38 AREA-AVERAGED Ap = 0.38
TOTAL AREA(ACRES) = 2.4
LONGEST FLOWPATH FROM NODE 3.01 TO NODE 3.05 = 809.24 FEET.

END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 2.4 TC(MIN.) = 11.12
EFFECTIVE AREA(ACRES) = 2.31 AREA-AVERAGED Fm(INCH/HR) = 0.14
AREA-AVERAGED Fp(INCH/HR) = 0.38 AREA-AVERAGED Ap = 0.379
PEAK FLOW RATE(CFS) = 2.68

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	2.68	11.12	1.430	0.38(0.14)	0.38	2.3	3.01
2	2.56	13.11	1.302	0.38(0.14)	0.37	2.4	6.01

END OF RATIONAL METHOD ANALYSIS

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Analysis prepared by:

Stantec

***** DESCRIPTION OF STUDY *****
 * Culver Alton - 2 Year Rational Method Study, Proposed Conditions *
 * DMA 4: East Intersection Streamline, Yale to Alton to Culver *
 * 11/07/2019 - ECS *

FILE NAME: 2DMA4P.DAT
 TIME/DATE OF STUDY: 17:11 11/07/2019

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USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:

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--*TIME-OF-CONCENTRATION MODEL*--

USER SPECIFIED STORM EVENT(YEAR) = 2.00
 SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00
 SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.95
 DATA BANK RAINFALL USED
 ANTECEDENT MOISTURE CONDITION (AMC) I ASSUMED FOR RATIONAL METHOD

USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL

NO.	HALF- WIDTH	CROWN TO CROSSFALL	STREET-CROSSFALL: IN- / OUT-/PARK- SIDE / SIDE/ WAY	CURB HEIGHT	GUTTER-GEOMETRIES: WIDTH LIP HIKE	MANNING FACTOR
	(FT)	(FT)		(FT)	(FT) (FT) (FT)	(n)
1	30.0	20.0	0.018/0.018/0.020	0.67	2.00 0.0312 0.167	0.0150
2	40.0	30.0	0.018/0.018/0.020	0.67	2.00 0.0312 0.167	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:
 1. Relative Flow-Depth = 0.00 FEET
 as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
 2. (Depth)*(Velocity) Constraint = 6.0 (FT*FT/S)
 *SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
 OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*
 *USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

FLOW PROCESS FROM NODE 4.01 TO NODE 4.03 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
 >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

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INITIAL SUBAREA FLOW-LENGTH(FEET) = 116.02
 ELEVATION DATA: UPSTREAM(FEET) = 89.00 DOWNSTREAM(FEET) = 87.00

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$
 SUBAREA ANALYSIS USED MINIMUM T_c (MIN.) = 5.000
 * 2 YEAR RAINFALL INTENSITY(INCH/HR) = 2.264
 SUBAREA T_c AND LOSS RATE DATA(AMC I):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	F_p (INCH/HR)	A_p (DECIMAL)	SCS CN	T_c (MIN.)
PUBLIC PARK	A	0.01	0.40	0.850	17	7.29
COMMERCIAL	A	0.13	0.40	0.100	17	5.00

SUBAREA AVERAGE PERVIOUS LOSS RATE, F_p (INCH/HR) = 0.40
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, A_p = 0.154
 SUBAREA RUNOFF(CFS) = 0.28
 TOTAL AREA(ACRES) = 0.14 PEAK FLOW RATE(CFS) = 0.28

FLOW PROCESS FROM NODE 4.03 TO NODE 4.05 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<

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UPSTREAM ELEVATION(FEET) = 87.00 DOWNSTREAM ELEVATION(FEET) = 80.00
STREET LENGTH(FEET) = 301.23 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.70
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.20
HALFSTREET FLOOD WIDTH(FEET) = 2.00
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.31
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.66
STREET FLOW TRAVEL TIME(MIN.) = 1.52 Tc(MIN.) = 6.52
* 2 YEAR RAINFALL INTENSITY(INCH/HR) = 1.944
SUBAREA LOSS RATE DATA(AMC I):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
PUBLIC PARK	A	0.07	0.40	0.850	17
COMMERCIAL	A	0.44	0.40	0.100	17

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.40
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.203
SUBAREA AREA(ACRES) = 0.51 SUBAREA RUNOFF(CFS) = 0.86
EFFECTIVE AREA(ACRES) = 0.65 AREA-AVERAGED Fm(INCH/HR) = 0.08
AREA-AVERAGED Fp(INCH/HR) = 0.40 AREA-AVERAGED Ap = 0.19
TOTAL AREA(ACRES) = 0.6 PEAK FLOW RATE(CFS) = 1.09

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.25 HALFSTREET FLOOD WIDTH(FEET) = 4.72
FLOW VELOCITY(FEET/SEC.) = 2.78 DEPTH*VELOCITY(FT*FT/SEC.) = 0.69
LONGEST FLOWPATH FROM NODE 4.01 TO NODE 4.05 = 417.25 FEET.

FLOW PROCESS FROM NODE 4.05 TO NODE 4.07 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<

=====

UPSTREAM ELEVATION(FEET) = 80.00 DOWNSTREAM ELEVATION(FEET) = 75.00
STREET LENGTH(FEET) = 369.87 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.64
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.30
HALFSTREET FLOOD WIDTH(FEET) = 7.59
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.31
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.69
STREET FLOW TRAVEL TIME(MIN.) = 2.66 Tc(MIN.) = 9.18
* 2 YEAR RAINFALL INTENSITY(INCH/HR) = 1.597
SUBAREA LOSS RATE DATA(AMC I):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	A	0.27	0.40	0.100	17
PUBLIC PARK	A	0.63	0.40	0.850	17

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.40

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SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.625
SUBAREA AREA(ACRES) = 0.90 SUBAREA RUNOFF(CFS) = 1.09
EFFECTIVE AREA(ACRES) = 1.55 AREA-AVERAGED Fm(INCH/HR) = 0.18
AREA-AVERAGED Fp(INCH/HR) = 0.40 AREA-AVERAGED Ap = 0.44
TOTAL AREA(ACRES) = 1.5 PEAK FLOW RATE(CFS) = 1.98

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.31 HALFSTREET FLOOD WIDTH(FEET) = 8.41
FLOW VELOCITY(FEET/SEC.) = 2.40 DEPTH*VELOCITY(FT*FT/SEC.) = 0.75
LONGEST FLOWPATH FROM NODE 4.01 TO NODE 4.07 = 787.12 FEET.

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FLOW PROCESS FROM NODE 4.07 TO NODE 4.09 IS CODE = 62
-----
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<
=====
UPSTREAM ELEVATION(FEET) = 75.00 DOWNSTREAM ELEVATION(FEET) = 72.00
STREET LENGTH(FEET) = 362.03 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.40
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.35
HALFSTREET FLOOD WIDTH(FEET) = 10.51
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.04
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.71
STREET FLOW TRAVEL TIME(MIN.) = 2.96 Tc(MIN.) = 12.14
* 2 YEAR RAINFALL INTENSITY(INCH/HR) = 1.360
SUBAREA LOSS RATE DATA(AMC I ):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
COMMERCIAL A 0.54 0.40 0.100 17
PUBLIC PARK A 0.22 0.40 0.850 17
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.40
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.317
SUBAREA AREA(ACRES) = 0.76 SUBAREA RUNOFF(CFS) = 0.84
EFFECTIVE AREA(ACRES) = 2.31 AREA-AVERAGED Fm(INCH/HR) = 0.16
AREA-AVERAGED Fp(INCH/HR) = 0.40 AREA-AVERAGED Ap = 0.40
TOTAL AREA(ACRES) = 2.3 PEAK FLOW RATE(CFS) = 2.49

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.35 HALFSTREET FLOOD WIDTH(FEET) = 10.66
FLOW VELOCITY(FEET/SEC.) = 2.06 DEPTH*VELOCITY(FT*FT/SEC.) = 0.73
LONGEST FLOWPATH FROM NODE 4.01 TO NODE 4.09 = 1149.15 FEET.

*****
FLOW PROCESS FROM NODE 4.09 TO NODE 4.09 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 12.14
RAINFALL INTENSITY(INCH/HR) = 1.36
AREA-AVERAGED Fm(INCH/HR) = 0.16
AREA-AVERAGED Fp(INCH/HR) = 0.40
AREA-AVERAGED Ap = 0.40
EFFECTIVE STREAM AREA(ACRES) = 2.31
TOTAL STREAM AREA(ACRES) = 2.31
PEAK FLOW RATE(CFS) AT CONFLUENCE = 2.49

*****
FLOW PROCESS FROM NODE 5.01 TO NODE 5.03 IS CODE = 21
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>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<
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INITIAL SUBAREA FLOW-LENGTH(FEET) = 253.47
ELEVATION DATA: UPSTREAM(FEET) = 75.00 DOWNSTREAM(FEET) = 73.50

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 7.763
* 2 YEAR RAINFALL INTENSITY(INCH/HR) = 1.759
SUBAREA Tc AND LOSS RATE DATA(AMC I ):
DEVELOPMENT TYPE/      SCS SOIL  AREA      Fp      Ap      SCS  Tc
LAND USE              GROUP  (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)
COMMERCIAL            A      0.24      0.40      0.100    17   7.76
PUBLIC PARK           A      0.24      0.40      0.850    17  12.33
SUBAREA AVERAGE PVIOUS LOSS RATE, Fp(INCH/HR) = 0.40
SUBAREA AVERAGE PVIOUS AREA FRACTION, Ap = 0.475
SUBAREA RUNOFF(CFS) = 0.68
TOTAL AREA(ACRES) = 0.48 PEAK FLOW RATE(CFS) = 0.68

*****
FLOW PROCESS FROM NODE 5.03 TO NODE 5.05 IS CODE = 62
-----
>>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>(STREET TABLE SECTION # 1 USED)<<<<<
=====
UPSTREAM ELEVATION(FEET) = 73.50 DOWNSTREAM ELEVATION(FEET) = 72.00
STREET LENGTH(FEET) = 273.08 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.08
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.30
HALFSTREET FLOOD WIDTH(FEET) = 7.72
AVERAGE FLOW VELOCITY(FEET/SEC.) = 1.48
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.44
STREET FLOW TRAVEL TIME(MIN.) = 3.07 Tc(MIN.) = 10.84
* 2 YEAR RAINFALL INTENSITY(INCH/HR) = 1.452
SUBAREA LOSS RATE DATA(AMC I ):
DEVELOPMENT TYPE/      SCS SOIL  AREA      Fp      Ap      SCS
LAND USE              GROUP  (ACRES) (INCH/HR) (DECIMAL) CN
COMMERCIAL            A      0.57      0.40      0.100    17
PUBLIC PARK           A      0.07      0.40      0.850    17
SUBAREA AVERAGE PVIOUS LOSS RATE, Fp(INCH/HR) = 0.40
SUBAREA AVERAGE PVIOUS AREA FRACTION, Ap = 0.182
SUBAREA AREA(ACRES) = 0.64 SUBAREA RUNOFF(CFS) = 0.79
EFFECTIVE AREA(ACRES) = 1.12 AREA-AVERAGED Fm(INCH/HR) = 0.12
AREA-AVERAGED Fp(INCH/HR) = 0.40 AREA-AVERAGED Ap = 0.31
TOTAL AREA(ACRES) = 1.1 PEAK FLOW RATE(CFS) = 1.34

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.32 HALFSTREET FLOOD WIDTH(FEET) = 8.72
FLOW VELOCITY(FEET/SEC.) = 1.54 DEPTH*VELOCITY(FT*FT/SEC.) = 0.49
LONGEST FLOWPATH FROM NODE 5.01 TO NODE 5.05 = 526.55 FEET.

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FLOW PROCESS FROM NODE 5.05 TO NODE 4.09 IS CODE = 1
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>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 10.84
RAINFALL INTENSITY(INCH/HR) = 1.45
AREA-AVERAGED Fm(INCH/HR) = 0.12

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AREA-AVERAGED F_p (INCH/HR) = 0.40
 AREA-AVERAGED A_p = 0.31
 EFFECTIVE STREAM AREA(ACRES) = 1.12
 TOTAL STREAM AREA(ACRES) = 1.12
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 1.34

** CONFLUENCE DATA **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	$F_p(F_m)$ (INCH/HR)	A_p	A_e (ACRES)	HEADWATER NODE
1	2.49	12.14	1.360	0.40(0.16)	0.40	2.3	4.01
2	1.34	10.84	1.452	0.40(0.12)	0.31	1.1	5.01

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	$F_p(F_m)$ (INCH/HR)	A_p	A_e (ACRES)	HEADWATER NODE
1	3.74	10.84	1.452	0.40(0.15)	0.37	3.2	5.01
2	3.74	12.14	1.360	0.40(0.15)	0.37	3.4	4.01

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 3.74 Tc(MIN.) = 12.14
 EFFECTIVE AREA(ACRES) = 3.43 AREA-AVERAGED F_m (INCH/HR) = 0.15
 AREA-AVERAGED F_p (INCH/HR) = 0.40 AREA-AVERAGED A_p = 0.37
 TOTAL AREA(ACRES) = 3.4
 LONGEST FLOWPATH FROM NODE 4.01 TO NODE 4.09 = 1149.15 FEET.

END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 3.4 TC(MIN.) = 12.14
 EFFECTIVE AREA(ACRES) = 3.43 AREA-AVERAGED F_m (INCH/HR) = 0.15
 AREA-AVERAGED F_p (INCH/HR) = 0.40 AREA-AVERAGED A_p = 0.371
 PEAK FLOW RATE(CFS) = 3.74

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	$F_p(F_m)$ (INCH/HR)	A_p	A_e (ACRES)	HEADWATER NODE
1	3.74	10.84	1.452	0.40(0.15)	0.37	3.2	5.01
2	3.74	12.14	1.360	0.40(0.15)	0.37	3.4	4.01

END OF RATIONAL METHOD ANALYSIS

Rational Method – 10-Year Storm Event: Existing Condition

 RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE
 (Reference: 1986 ORANGE COUNTY HYDROLOGY CRITERION)
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Analysis prepared by:

Stantec

***** DESCRIPTION OF STUDY *****
 * Culver Alton - 10 Year Rational Method Study, Existing Conditions *
 * DMA 1: North Intersection Streamline, Culver to Alton *
 * 10/15/2019 - ECS *

FILE NAME: CA10DMA1.DAT
 TIME/DATE OF STUDY: 11:18 10/15/2019

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USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:

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--*TIME-OF-CONCENTRATION MODEL*--

USER SPECIFIED STORM EVENT(YEAR) = 10.00
 SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00
 SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.95
 DATA BANK RAINFALL USED
 ANTECEDENT MOISTURE CONDITION (AMC) II ASSUMED FOR RATIONAL METHOD

USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL

NO.	HALF- WIDTH	CROWN TO CROSSFALL	STREET-CROSSFALL: IN- / OUT-/PARK- SIDE / SIDE/ WAY	CURB HEIGHT	GUTTER-GEOMETRIES: WIDTH LIP HIKE	MANNING FACTOR
	(FT)	(FT)		(FT)	(FT) (FT) (FT)	(n)
1	30.0	20.0	0.018/0.018/0.020	0.67	2.00 0.0313 0.167	0.0150
2	40.0	30.0	0.018/0.018/0.020	0.67	2.00 0.0313 0.167	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:
 1. Relative Flow-Depth = 0.00 FEET
 as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
 2. (Depth)*(Velocity) Constraint = 6.0 (FT*FT/S)
 *SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
 OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*
 *USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

FLOW PROCESS FROM NODE 1.01 TO NODE 1.03 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
 >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

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INITIAL SUBAREA FLOW-LENGTH(FEET) = 330.00
 ELEVATION DATA: UPSTREAM(FEET) = 75.00 DOWNSTREAM(FEET) = 73.00

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$
 SUBAREA ANALYSIS USED MINIMUM T_c (MIN.) = 8.586
 * 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.978
 SUBAREA T_c AND LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	F_p (INCH/HR)	A_p (DECIMAL)	SCS CN	T_c (MIN.)
COMMERCIAL	A	0.41	0.40	0.100	32	8.59
PUBLIC PARK	A	0.27	0.40	0.850	32	13.64

SUBAREA AVERAGE PERVIOUS LOSS RATE, F_p (INCH/HR) = 0.40
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, A_p = 0.398
 SUBAREA RUNOFF(CFS) = 1.73
 TOTAL AREA(ACRES) = 0.68 PEAK FLOW RATE(CFS) = 1.73

FLOW PROCESS FROM NODE 1.03 TO NODE 1.05 IS CODE = 62

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>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<

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UPSTREAM ELEVATION(FEET) = 73.00 DOWNSTREAM ELEVATION(FEET) = 68.00
STREET LENGTH(FEET) = 355.96 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.95
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.34
HALFSTREET FLOOD WIDTH(FEET) = 10.20
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.63
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.91
STREET FLOW TRAVEL TIME(MIN.) = 2.26 Tc(MIN.) = 10.84
* 10 YEAR RAINFALL INTENSITY (INCH/HR) = 2.605

SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	B	0.12	0.30	0.100	56
COMMERCIAL	A	0.56	0.40	0.100	32
PUBLIC PARK	B	0.20	0.30	0.850	56
PUBLIC PARK	A	0.22	0.40	0.850	32

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.36
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.386
SUBAREA AREA(ACRES) = 1.10 SUBAREA RUNOFF(CFS) = 2.44
EFFECTIVE AREA(ACRES) = 1.78 AREA-AVERAGED Fm(INCH/HR) = 0.15
AREA-AVERAGED Fp(INCH/HR) = 0.37 AREA-AVERAGED Ap = 0.39
TOTAL AREA(ACRES) = 1.8 PEAK FLOW RATE(CFS) = 3.94

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.37 HALFSTREET FLOOD WIDTH(FEET) = 11.68
FLOW VELOCITY(FEET/SEC.) = 2.79 DEPTH*VELOCITY(FT*FT/SEC.) = 1.04
LONGEST FLOWPATH FROM NODE 1.01 TO NODE 1.05 = 685.96 FEET.

FLOW PROCESS FROM NODE 1.05 TO NODE 1.07 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<

=====

UPSTREAM ELEVATION(FEET) = 68.00 DOWNSTREAM ELEVATION(FEET) = 65.50
STREET LENGTH(FEET) = 162.78 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 4.43
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.38
HALFSTREET FLOOD WIDTH(FEET) = 12.07
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.97
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 1.12
STREET FLOW TRAVEL TIME(MIN.) = 0.91 Tc(MIN.) = 11.76
* 10 YEAR RAINFALL INTENSITY (INCH/HR) = 2.487

SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	B	0.14	0.30	0.100	56

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                                10DMA1E.RES
COMMERCIAL          A      0.13      0.40      0.100      32
PUBLIC PARK         B      0.10      0.30      0.850      56
PUBLIC PARK         A      0.10      0.40      0.850      32
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.35
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.419
SUBAREA AREA(ACRES) = 0.47      SUBAREA RUNOFF(CFS) = 0.99
EFFECTIVE AREA(ACRES) = 2.25      AREA-AVERAGED Fm(INCH/HR) = 0.15
AREA-AVERAGED Fp(INCH/HR) = 0.37      AREA-AVERAGED Ap = 0.40
TOTAL AREA(ACRES) = 2.2      PEAK FLOW RATE(CFS) = 4.74

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END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.38      HALFSTREET FLOOD WIDTH(FEET) = 12.38
FLOW VELOCITY(FEET/SEC.) = 3.03      DEPTH*VELOCITY(FT*FT/SEC.) = 1.16
LONGEST FLOWPATH FROM NODE 1.01 TO NODE 1.07 = 848.74 FEET.

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=====
END OF STUDY SUMMARY:
TOTAL AREA(ACRES) = 2.2      TC(MIN.) = 11.76
EFFECTIVE AREA(ACRES) = 2.25      AREA-AVERAGED Fm(INCH/HR) = 0.15
AREA-AVERAGED Fp(INCH/HR) = 0.37      AREA-AVERAGED Ap = 0.397
PEAK FLOW RATE(CFS) = 4.74
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END OF RATIONAL METHOD ANALYSIS

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 Ver. 23.0 Release Date: 07/01/2016 License ID 1535

Analysis prepared by:

Stantec

***** DESCRIPTION OF STUDY *****
 * Culver Alton - 10 Year Rational Method Study, Existing Conditions *
 * DMA 2: West Intersection Streamline, Alton *
 * 10/15/2019 - ECS *

FILE NAME: CA10DMA2.DAT
 TIME/DATE OF STUDY: 11:22 10/15/2019

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USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:

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--*TIME-OF-CONCENTRATION MODEL*--

USER SPECIFIED STORM EVENT(YEAR) = 10.00
 SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00
 SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.95
 DATA BANK RAINFALL USED
 ANTECEDENT MOISTURE CONDITION (AMC) II ASSUMED FOR RATIONAL METHOD

USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL

NO.	HALF- WIDTH (FT)	CROWN TO CROSSFALL (FT)	STREET-CROSSFALL: IN- / OUT-/PARK- SIDE / SIDE/ WAY	CURB HEIGHT (FT)	GUTTER-GEOMETRIES:			MANNING FACTOR (n)
					WIDTH (FT)	LIP (FT)	HIKE (FT)	
1	30.0	20.0	0.018/0.018/0.020	0.67	2.00	0.0313	0.167	0.0150
2	40.0	30.0	0.018/0.018/0.020	0.67	2.00	0.0313	0.167	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:
 1. Relative Flow-Depth = 0.00 FEET
 as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
 2. (Depth)*(Velocity) Constraint = 6.0 (FT*FT/S)
 *SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
 OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*
 *USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

FLOW PROCESS FROM NODE 2.01 TO NODE 2.03 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
 >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 330.00
 ELEVATION DATA: UPSTREAM(FEET) = 72.00 DOWNSTREAM(FEET) = 68.00

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$
 SUBAREA ANALYSIS USED MINIMUM T_c (MIN.) = 7.474
 * 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.224
 SUBAREA T_c AND LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	F_p (INCH/HR)	A_p (DECIMAL)	SCS CN	T_c (MIN.)
PUBLIC PARK	B	0.01	0.30	0.850	56	11.88
PUBLIC PARK	A	0.27	0.40	0.850	32	11.88
COMMERCIAL	B	0.07	0.30	0.100	56	7.47
COMMERCIAL	A	0.40	0.40	0.100	32	7.47

SUBAREA AVERAGE PERVIOUS LOSS RATE, F_p (INCH/HR) = 0.39
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, A_p = 0.380
 SUBAREA RUNOFF(CFS) = 2.08
 TOTAL AREA(ACRES) = 0.75 PEAK FLOW RATE(CFS) = 2.08

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                                10DMA2E.RES
FLOW PROCESS FROM NODE      2.03 TO NODE      2.05 IS CODE = 62
-----
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<
=====
UPSTREAM ELEVATION(FEET) = 68.00 DOWNSTREAM ELEVATION(FEET) = 62.00
STREET LENGTH(FEET) = 440.15 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.21
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.35
HALFSTREET FLOOD WIDTH(FEET) = 10.66
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.66
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.94
STREET FLOW TRAVEL TIME(MIN.) = 2.76 Tc(MIN.) = 10.24
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.693
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
COMMERCIAL B 0.22 0.30 0.100 56
COMMERCIAL A 0.27 0.40 0.100 32
PUBLIC PARK B 0.23 0.30 0.850 56
PUBLIC PARK A 0.28 0.40 0.850 32
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.35
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.483
SUBAREA AREA(ACRES) = 1.00 SUBAREA RUNOFF(CFS) = 2.27
EFFECTIVE AREA(ACRES) = 1.75 AREA-AVERAGED Fm(INCH/HR) = 0.16
AREA-AVERAGED Fp(INCH/HR) = 0.37 AREA-AVERAGED Ap = 0.44
TOTAL AREA(ACRES) = 1.8 PEAK FLOW RATE(CFS) = 3.99

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.37 HALFSTREET FLOOD WIDTH(FEET) = 11.76
FLOW VELOCITY(FEET/SEC.) = 2.79 DEPTH*VELOCITY(FT*FT/SEC.) = 1.04
LONGEST FLOWPATH FROM NODE 2.01 TO NODE 2.05 = 770.15 FEET.
=====
END OF STUDY SUMMARY:
TOTAL AREA(ACRES) = 1.8 TC(MIN.) = 10.24
EFFECTIVE AREA(ACRES) = 1.75 AREA-AVERAGED Fm(INCH/HR) = 0.16
AREA-AVERAGED Fp(INCH/HR) = 0.37 AREA-AVERAGED Ap = 0.439
PEAK FLOW RATE(CFS) = 3.99
=====
END OF RATIONAL METHOD ANALYSIS

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Analysis prepared by:

Stantec

***** DESCRIPTION OF STUDY *****
 * Culver Alton - 10 Year Rational Method Study, Existing Conditions *
 * DMA 3: South Intersection Streamline, Alton *
 * 11/20/2019 - ECS *

FILE NAME: 10DMA3E.DAT
 TIME/DATE OF STUDY: 11:25 11/20/2019

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USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:

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--TIME-OF-CONCENTRATION MODEL*--

USER SPECIFIED STORM EVENT(YEAR) = 10.00
 SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00
 SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.95
 DATA BANK RAINFALL USED
 ANTECEDENT MOISTURE CONDITION (AMC) II ASSUMED FOR RATIONAL METHOD

USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL

NO.	HALF- WIDTH	CROWN TO CROSSFALL	STREET-CROSSFALL: IN- / OUT-/PARK- SIDE / SIDE/ WAY	CURB HEIGHT	GUTTER-GEOMETRIES: WIDTH LIP HIKE	MANNING FACTOR
	(FT)	(FT)		(FT)	(FT) (FT) (FT)	(n)
1	30.0	20.0	0.018/0.018/0.020	0.67	2.00 0.0312 0.167	0.0150
2	40.0	30.0	0.018/0.018/0.020	0.67	2.00 0.0312 0.167	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:
 1. Relative Flow-Depth = 0.00 FEET
 as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
 2. (Depth)*(Velocity) Constraint = 6.0 (FT*FT/S)
 *SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
 OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*
 *USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

FLOW PROCESS FROM NODE 3.01 TO NODE 3.03 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
 >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 308.42
 ELEVATION DATA: UPSTREAM(FEET) = 82.00 DOWNSTREAM(FEET) = 77.00

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$
 SUBAREA ANALYSIS USED MINIMUM T_c (MIN.) = 6.864
 * 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.386
 SUBAREA T_c AND LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	F_p (INCH/HR)	A_p (DECIMAL)	SCS CN	T_c (MIN.)
COMMERCIAL	A	0.26	0.40	0.100	32	6.86
PUBLIC PARK	A	0.22	0.40	0.850	32	10.91

SUBAREA AVERAGE PERVIOUS LOSS RATE, F_p (INCH/HR) = 0.40
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, A_p = 0.444
 SUBAREA RUNOFF(CFS) = 1.39
 TOTAL AREA(ACRES) = 0.48 PEAK FLOW RATE(CFS) = 1.39

FLOW PROCESS FROM NODE 3.03 TO NODE 3.05 IS CODE = 62

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                                10DMA3E.RES
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<
=====
UPSTREAM ELEVATION(FEET) = 77.00 DOWNSTREAM ELEVATION(FEET) = 72.00
STREET LENGTH(FEET) = 500.82 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.60
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.35
HALFSTREET FLOOD WIDTH(FEET) = 10.43
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.24
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.78
STREET FLOW TRAVEL TIME(MIN.) = 3.73 Tc(MIN.) = 10.60
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.640
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
COMMERCIAL A 0.53 0.40 0.100 32
PUBLIC PARK A 0.57 0.40 0.850 32
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.40
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.489
SUBAREA AREA(ACRES) = 1.10 SUBAREA RUNOFF(CFS) = 2.42
EFFECTIVE AREA(ACRES) = 1.58 AREA-AVERAGED Fm(INCH/HR) = 0.19
AREA-AVERAGED Fp(INCH/HR) = 0.40 AREA-AVERAGED Ap = 0.48
TOTAL AREA(ACRES) = 1.6 PEAK FLOW RATE(CFS) = 3.48

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.38 HALFSTREET FLOOD WIDTH(FEET) = 11.91
FLOW VELOCITY(FEET/SEC.) = 2.38 DEPTH*VELOCITY(FT*FT/SEC.) = 0.89
LONGEST FLOWPATH FROM NODE 3.01 TO NODE 3.05 = 809.24 FEET.

*****
FLOW PROCESS FROM NODE 3.05 TO NODE 3.05 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 10.60
RAINFALL INTENSITY(INCH/HR) = 2.64
AREA-AVERAGED Fm(INCH/HR) = 0.19
AREA-AVERAGED Fp(INCH/HR) = 0.40
AREA-AVERAGED Ap = 0.48
EFFECTIVE STREAM AREA(ACRES) = 1.58
TOTAL STREAM AREA(ACRES) = 1.58
PEAK FLOW RATE(CFS) AT CONFLUENCE = 3.48

*****
FLOW PROCESS FROM NODE 6.01 TO NODE 6.03 IS CODE = 21
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<
=====
INITIAL SUBAREA FLOW-LENGTH(FEET) = 237.14
ELEVATION DATA: UPSTREAM(FEET) = 73.50 DOWNSTREAM(FEET) = 72.50

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 8.089
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.082
SUBAREA Tc AND LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS Tc
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)
PUBLIC PARK D 0.07 0.20 0.850 75 12.85
COMMERCIAL D 0.38 0.20 0.100 75 8.09

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SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.217
SUBAREA RUNOFF(CFS) = 1.23
TOTAL AREA(ACRES) = 0.45 PEAK FLOW RATE(CFS) = 1.23
*****
FLOW PROCESS FROM NODE 6.03 TO NODE 3.05 IS CODE = 62
-----
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<
=====
UPSTREAM ELEVATION(FEET) = 72.50 DOWNSTREAM ELEVATION(FEET) = 72.00
STREET LENGTH(FEET) = 276.24 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curb) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.66
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.39
HALFSTREET FLOOD WIDTH(FEET) = 12.54
AVERAGE FLOW VELOCITY(FEET/SEC.) = 1.04
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.40
STREET FLOW TRAVEL TIME(MIN.) = 4.42 Tc(MIN.) = 12.51
* 10 YEAR RAINFALL INTENSITY (INCH/HR) = 2.400
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
PUBLIC PARK A 0.03 0.40 0.850 32
COMMERCIAL A 0.25 0.40 0.100 32
COMMERCIAL B 0.09 0.30 0.100 56
PUBLIC PARK D 0.02 0.20 0.850 75
COMMERCIAL D 0.02 0.20 0.100 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.34
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.191
SUBAREA AREA(ACRES) = 0.41 SUBAREA RUNOFF(CFS) = 0.86
EFFECTIVE AREA(ACRES) = 0.86 AREA-AVERAGED Fm(INCH/HR) = 0.05
AREA-AVERAGED Fp(INCH/HR) = 0.26 AREA-AVERAGED Ap = 0.20
TOTAL AREA(ACRES) = 0.9 PEAK FLOW RATE(CFS) = 1.82

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.39 HALFSTREET FLOOD WIDTH(FEET) = 13.01
FLOW VELOCITY(FEET/SEC.) = 1.07 DEPTH*VELOCITY(FT*FT/SEC.) = 0.42
LONGEST FLOWPATH FROM NODE 6.01 TO NODE 3.05 = 513.38 FEET.
*****
FLOW PROCESS FROM NODE 6.03 TO NODE 3.05 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 12.51
RAINFALL INTENSITY(INCH/HR) = 2.40
AREA-AVERAGED Fm(INCH/HR) = 0.05
AREA-AVERAGED Fp(INCH/HR) = 0.26
AREA-AVERAGED Ap = 0.20
EFFECTIVE STREAM AREA(ACRES) = 0.86
TOTAL STREAM AREA(ACRES) = 0.86
PEAK FLOW RATE(CFS) AT CONFLUENCE = 1.82

** CONFLUENCE DATA **
STREAM Q Tc Intensity Fp(Fm) Ap Ae HEADWATER
NUMBER (CFS) (MIN.) (INCH/HR) (INCH/HR) (ACRES) NODE
1 3.48 10.60 2.640 0.40( 0.19) 0.48 1.6 3.01
2 1.82 12.51 2.400 0.26( 0.05) 0.20 0.9 6.01

```

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	5.18	10.60	2.640	0.38(0.15)	0.39	2.3	3.01
2	4.96	12.51	2.400	0.37(0.14)	0.38	2.4	6.01

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 5.18 Tc(MIN.) = 10.60
EFFECTIVE AREA(ACRES) = 2.31 AREA-AVERAGED Fm(INCH/HR) = 0.15
AREA-AVERAGED Fp(INCH/HR) = 0.38 AREA-AVERAGED Ap = 0.39
TOTAL AREA(ACRES) = 2.4
LONGEST FLOWPATH FROM NODE 3.01 TO NODE 3.05 = 809.24 FEET.

END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 2.4 TC(MIN.) = 10.60
EFFECTIVE AREA(ACRES) = 2.31 AREA-AVERAGED Fm(INCH/HR) = 0.15
AREA-AVERAGED Fp(INCH/HR) = 0.38 AREA-AVERAGED Ap = 0.390
PEAK FLOW RATE(CFS) = 5.18

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	5.18	10.60	2.640	0.38(0.15)	0.39	2.3	3.01
2	4.96	12.51	2.400	0.37(0.14)	0.38	2.4	6.01

END OF RATIONAL METHOD ANALYSIS

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Analysis prepared by:

Stantec

***** DESCRIPTION OF STUDY *****
 * Culver Alton - 10 Year Rational Method Study, Existing Conditions *
 * DMA 4: East Intersection Streamline, Yale to Alton to Culver *
 * 11/20/2019 - ECS *

FILE NAME: 10DMA4E.DAT
 TIME/DATE OF STUDY: 11:28 11/20/2019

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USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:

=====

--*TIME-OF-CONCENTRATION MODEL*--

USER SPECIFIED STORM EVENT(YEAR) = 10.00
 SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00
 SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.95
 DATA BANK RAINFALL USED
 ANTECEDENT MOISTURE CONDITION (AMC) II ASSUMED FOR RATIONAL METHOD

USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL

NO.	HALF- WIDTH (FT)	CROWN TO CROSSFALL (FT)	STREET-CROSSFALL: IN- / OUT-/PARK- SIDE / SIDE/ WAY	CURB HEIGHT (FT)	GUTTER-GEOMETRIES:			MANNING FACTOR (n)
					WIDTH (FT)	LIP (FT)	HIKE (FT)	
1	30.0	20.0	0.018/0.018/0.020	0.67	2.00	0.0312	0.167	0.0150
2	40.0	30.0	0.018/0.018/0.020	0.67	2.00	0.0312	0.167	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:
 1. Relative Flow-Depth = 0.00 FEET
 as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
 2. (Depth)*(Velocity) Constraint = 6.0 (FT*FT/S)
 *SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
 OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*
 *USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

FLOW PROCESS FROM NODE 4.01 TO NODE 4.03 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
 >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 116.02
 ELEVATION DATA: UPSTREAM(FEET) = 89.00 DOWNSTREAM(FEET) = 87.00

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$
 SUBAREA ANALYSIS USED MINIMUM T_c (MIN.) = 5.000
 * 10 YEAR RAINFALL INTENSITY(INCH/HR) = 4.060
 SUBAREA T_c AND LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	F_p (INCH/HR)	A_p (DECIMAL)	SCS CN	T_c (MIN.)
PUBLIC PARK	A	0.01	0.40	0.850	32	7.29
COMMERCIAL	A	0.13	0.40	0.100	32	5.00

SUBAREA AVERAGE PERVIOUS LOSS RATE, F_p (INCH/HR) = 0.40
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, A_p = 0.154
 SUBAREA RUNOFF(CFS) = 0.50
 TOTAL AREA(ACRES) = 0.14 PEAK FLOW RATE(CFS) = 0.50

FLOW PROCESS FROM NODE 4.03 TO NODE 4.05 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<

=====

UPSTREAM ELEVATION(FEET) = 87.00 DOWNSTREAM ELEVATION(FEET) = 80.00
STREET LENGTH(FEET) = 301.23 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.27
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.26
HALFSTREET FLOOD WIDTH(FEET) = 5.41
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.79
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.72
STREET FLOW TRAVEL TIME(MIN.) = 1.80 Tc(MIN.) = 6.80
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.404
SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
PUBLIC PARK	A	0.07	0.40	0.850	32
COMMERCIAL	A	0.44	0.40	0.100	32

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.40
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.203
SUBAREA AREA(ACRES) = 0.51 SUBAREA RUNOFF(CFS) = 1.53
EFFECTIVE AREA(ACRES) = 0.65 AREA-AVERAGED Fm(INCH/HR) = 0.08
AREA-AVERAGED Fp(INCH/HR) = 0.40 AREA-AVERAGED Ap = 0.19
TOTAL AREA(ACRES) = 0.6 PEAK FLOW RATE(CFS) = 1.95

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.29 HALFSTREET FLOOD WIDTH(FEET) = 7.22
FLOW VELOCITY(FEET/SEC.) = 2.95 DEPTH*VELOCITY(FT*FT/SEC.) = 0.86
LONGEST FLOWPATH FROM NODE 4.01 TO NODE 4.05 = 417.25 FEET.

FLOW PROCESS FROM NODE 4.05 TO NODE 4.07 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<

=====

UPSTREAM ELEVATION(FEET) = 80.00 DOWNSTREAM ELEVATION(FEET) = 75.00
STREET LENGTH(FEET) = 369.87 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.01
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.35
HALFSTREET FLOOD WIDTH(FEET) = 10.35
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.62
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.91
STREET FLOW TRAVEL TIME(MIN.) = 2.36 Tc(MIN.) = 9.16
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.870
SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	A	0.27	0.40	0.100	32
PUBLIC PARK	A	0.63	0.40	0.850	32

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.40

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                                10DMA4E.RES
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.625
SUBAREA AREA(ACRES) = 0.90 SUBAREA RUNOFF(CFS) = 2.12
EFFECTIVE AREA(ACRES) = 1.55 AREA-AVERAGED Fm(INCH/HR) = 0.18
AREA-AVERAGED Fp(INCH/HR) = 0.40 AREA-AVERAGED Ap = 0.44
TOTAL AREA(ACRES) = 1.5 PEAK FLOW RATE(CFS) = 3.76

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.37 HALFSTREET FLOOD WIDTH(FEET) = 11.52
FLOW VELOCITY(FEET/SEC.) = 2.72 DEPTH*VELOCITY(FT*FT/SEC.) = 1.00
LONGEST FLOWPATH FROM NODE 4.01 TO NODE 4.07 = 787.12 FEET.

*****
FLOW PROCESS FROM NODE 4.07 TO NODE 4.09 IS CODE = 62
-----
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<
=====
UPSTREAM ELEVATION(FEET) = 75.00 DOWNSTREAM ELEVATION(FEET) = 72.00
STREET LENGTH(FEET) = 362.03 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 4.54
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.41
HALFSTREET FLOOD WIDTH(FEET) = 13.95
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.35
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.97
STREET FLOW TRAVEL TIME(MIN.) = 2.56 Tc(MIN.) = 11.72
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.492
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
COMMERCIAL A 0.37 0.40 0.100 32
PUBLIC PARK A 0.39 0.40 0.850 32
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.40
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.485
SUBAREA AREA(ACRES) = 0.76 SUBAREA RUNOFF(CFS) = 1.57
EFFECTIVE AREA(ACRES) = 2.31 AREA-AVERAGED Fm(INCH/HR) = 0.18
AREA-AVERAGED Fp(INCH/HR) = 0.40 AREA-AVERAGED Ap = 0.46
TOTAL AREA(ACRES) = 2.3 PEAK FLOW RATE(CFS) = 4.80

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.42 HALFSTREET FLOOD WIDTH(FEET) = 14.26
FLOW VELOCITY(FEET/SEC.) = 2.39 DEPTH*VELOCITY(FT*FT/SEC.) = 1.00
LONGEST FLOWPATH FROM NODE 4.01 TO NODE 4.09 = 1149.15 FEET.

*****
FLOW PROCESS FROM NODE 4.09 TO NODE 4.09 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 11.72
RAINFALL INTENSITY(INCH/HR) = 2.49
AREA-AVERAGED Fm(INCH/HR) = 0.18
AREA-AVERAGED Fp(INCH/HR) = 0.40
AREA-AVERAGED Ap = 0.46
EFFECTIVE STREAM AREA(ACRES) = 2.31
TOTAL STREAM AREA(ACRES) = 2.31
PEAK FLOW RATE(CFS) AT CONFLUENCE = 4.80

*****
FLOW PROCESS FROM NODE 5.01 TO NODE 5.03 IS CODE = 21
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>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<
=====
INITIAL SUBAREA FLOW-LENGTH(FEET) = 253.47
ELEVATION DATA: UPSTREAM(FEET) = 75.00 DOWNSTREAM(FEET) = 73.50

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 7.763
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.155
SUBAREA Tc AND LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/      SCS SOIL  AREA      Fp          Ap      SCS  Tc
LAND USE              GROUP  (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)
COMMERCIAL            A        0.21    0.40    0.100    32   7.76
PUBLIC PARK           A        0.27    0.40    0.850    32  12.33
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.40
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.522
SUBAREA RUNOFF(CFS) = 1.27
TOTAL AREA(ACRES) = 0.48 PEAK FLOW RATE(CFS) = 1.27

*****
FLOW PROCESS FROM NODE 5.03 TO NODE 5.05 IS CODE = 62
-----
>>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>(STREET TABLE SECTION # 1 USED)<<<<<
=====
UPSTREAM ELEVATION(FEET) = 73.50 DOWNSTREAM ELEVATION(FEET) = 72.00
STREET LENGTH(FEET) = 273.08 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.00
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.35
HALFSTREET FLOOD WIDTH(FEET) = 10.59
AVERAGE FLOW VELOCITY(FEET/SEC.) = 1.67
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.59
STREET FLOW TRAVEL TIME(MIN.) = 2.72 Tc(MIN.) = 10.48
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.656
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/      SCS SOIL  AREA      Fp          Ap      SCS
LAND USE              GROUP  (ACRES) (INCH/HR) (DECIMAL) CN
COMMERCIAL            A        0.43    0.40    0.100    32
PUBLIC PARK           A        0.21    0.40    0.850    32
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.40
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.346
SUBAREA AREA(ACRES) = 0.64 SUBAREA RUNOFF(CFS) = 1.45
EFFECTIVE AREA(ACRES) = 1.12 AREA-AVERAGED Fm(INCH/HR) = 0.17
AREA-AVERAGED Fp(INCH/HR) = 0.40 AREA-AVERAGED Ap = 0.42
TOTAL AREA(ACRES) = 1.1 PEAK FLOW RATE(CFS) = 2.51

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.37 HALFSTREET FLOOD WIDTH(FEET) = 11.76
FLOW VELOCITY(FEET/SEC.) = 1.76 DEPTH*VELOCITY(FT*FT/SEC.) = 0.65
LONGEST FLOWPATH FROM NODE 5.01 TO NODE 5.05 = 526.55 FEET.

*****
FLOW PROCESS FROM NODE 5.05 TO NODE 4.09 IS CODE = 1
-----
>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 10.48
RAINFALL INTENSITY(INCH/HR) = 2.66
AREA-AVERAGED Fm(INCH/HR) = 0.17

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AREA-AVERAGED F_p (INCH/HR) = 0.40
 AREA-AVERAGED A_p = 0.42
 EFFECTIVE STREAM AREA(ACRES) = 1.12
 TOTAL STREAM AREA(ACRES) = 1.12
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 2.51

** CONFLUENCE DATA **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	$F_p(F_m)$ (INCH/HR)	A_p	A_e (ACRES)	HEADWATER NODE
1	4.80	11.72	2.492	0.40(0.18)	0.46	2.3	4.01
2	2.51	10.48	2.656	0.40(0.17)	0.42	1.1	5.01

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	$F_p(F_m)$ (INCH/HR)	A_p	A_e (ACRES)	HEADWATER NODE
1	7.11	10.48	2.656	0.40(0.18)	0.44	3.2	5.01
2	7.14	11.72	2.492	0.40(0.18)	0.45	3.4	4.01

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 7.14 Tc(MIN.) = 11.72
 EFFECTIVE AREA(ACRES) = 3.43 AREA-AVERAGED F_m (INCH/HR) = 0.18
 AREA-AVERAGED F_p (INCH/HR) = 0.40 AREA-AVERAGED A_p = 0.45
 TOTAL AREA(ACRES) = 3.4
 LONGEST FLOWPATH FROM NODE 4.01 TO NODE 4.09 = 1149.15 FEET.

END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 3.4 TC(MIN.) = 11.72
 EFFECTIVE AREA(ACRES) = 3.43 AREA-AVERAGED F_m (INCH/HR) = 0.18
 AREA-AVERAGED F_p (INCH/HR) = 0.40 AREA-AVERAGED A_p = 0.445
 PEAK FLOW RATE(CFS) = 7.14

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	$F_p(F_m)$ (INCH/HR)	A_p	A_e (ACRES)	HEADWATER NODE
1	7.11	10.48	2.656	0.40(0.18)	0.44	3.2	5.01
2	7.14	11.72	2.492	0.40(0.18)	0.45	3.4	4.01

END OF RATIONAL METHOD ANALYSIS

Rational Method – 10-Year Storm Event: Proposed Condition

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RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE
(Reference: 1986 ORANGE COUNTY HYDROLOGY CRITERION)
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Analysis prepared by:

Stantec

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***** DESCRIPTION OF STUDY *****
* Culver Alton - 10 Year Rational Method Study, Proposed Conditions *
* DMA 1: North Intersection Streamline, Culver to Alton *
* 11/07/2019 - ECS *
*****

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FILE NAME: 10DMA1P.DAT
TIME/DATE OF STUDY: 16:56 11/07/2019

=====

USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:

=====

--*TIME-OF-CONCENTRATION MODEL*--

USER SPECIFIED STORM EVENT(YEAR) = 10.00
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.95
DATA BANK RAINFALL USED
ANTECEDENT MOISTURE CONDITION (AMC) II ASSUMED FOR RATIONAL METHOD

USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL

NO.	HALF- WIDTH	CROWN TO CROSSFALL	STREET-CROSSFALL: IN- / OUT-/PARK- SIDE / SIDE/ WAY	CURB HEIGHT	GUTTER-GEOMETRIES: WIDTH LIP HIKE	MANNING FACTOR
	(FT)	(FT)		(FT)	(FT) (FT) (FT)	(n)
1	30.0	20.0	0.018/0.018/0.020	0.67	2.00 0.0312 0.167	0.0150
2	40.0	30.0	0.018/0.018/0.020	0.67	2.00 0.0312 0.167	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:
1. Relative Flow-Depth = 0.00 FEET
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)*(Velocity) Constraint = 6.0 (FT*FT/S)
*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*
*USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

FLOW PROCESS FROM NODE 1.01 TO NODE 1.03 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 330.00
ELEVATION DATA: UPSTREAM(FEET) = 75.00 DOWNSTREAM(FEET) = 73.00

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$
SUBAREA ANALYSIS USED MINIMUM T_c (MIN.) = 8.586
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.978
SUBAREA T_c AND LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	F_p (INCH/HR)	A_p (DECIMAL)	SCS CN	T_c (MIN.)
COMMERCIAL	A	0.41	0.40	0.100	32	8.59
PUBLIC PARK	A	0.27	0.40	0.850	32	13.64

SUBAREA AVERAGE PERVIOUS LOSS RATE, F_p (INCH/HR) = 0.40
SUBAREA AVERAGE PERVIOUS AREA FRACTION, A_p = 0.398
SUBAREA RUNOFF(CFS) = 1.73
TOTAL AREA(ACRES) = 0.68 PEAK FLOW RATE(CFS) = 1.73

FLOW PROCESS FROM NODE 1.03 TO NODE 1.05 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<

=====

UPSTREAM ELEVATION(FEET) = 73.00 DOWNSTREAM ELEVATION(FEET) = 68.00
STREET LENGTH(FEET) = 355.96 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.94
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.34
HALFSTREET FLOOD WIDTH(FEET) = 10.20
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.62
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.90
STREET FLOW TRAVEL TIME(MIN.) = 2.26 Tc(MIN.) = 10.85
* 10 YEAR RAINFALL INTENSITY (INCH/HR) = 2.605

SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	B	0.12	0.30	0.100	56
COMMERCIAL	A	0.52	0.40	0.100	32
PUBLIC PARK	B	0.20	0.30	0.850	56
PUBLIC PARK	A	0.26	0.40	0.850	32

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.36
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.414
SUBAREA AREA(ACRES) = 1.10 SUBAREA RUNOFF(CFS) = 2.43
EFFECTIVE AREA(ACRES) = 1.78 AREA-AVERAGED Fm(INCH/HR) = 0.15
AREA-AVERAGED Fp(INCH/HR) = 0.37 AREA-AVERAGED Ap = 0.41
TOTAL AREA(ACRES) = 1.8 PEAK FLOW RATE(CFS) = 3.93

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.37 HALFSTREET FLOOD WIDTH(FEET) = 11.60
FLOW VELOCITY(FEET/SEC.) = 2.81 DEPTH*VELOCITY(FT*FT/SEC.) = 1.04
LONGEST FLOWPATH FROM NODE 1.01 TO NODE 1.05 = 685.96 FEET.

FLOW PROCESS FROM NODE 1.05 TO NODE 1.07 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<

=====

UPSTREAM ELEVATION(FEET) = 68.00 DOWNSTREAM ELEVATION(FEET) = 65.50
STREET LENGTH(FEET) = 162.78 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 4.42
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.38
HALFSTREET FLOOD WIDTH(FEET) = 11.99
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.99
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 1.13
STREET FLOW TRAVEL TIME(MIN.) = 0.91 Tc(MIN.) = 11.75
* 10 YEAR RAINFALL INTENSITY (INCH/HR) = 2.488

SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	B	0.14	0.30	0.100	56

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                                10DMA1P.RES
COMMERCIAL          A      0.13      0.40      0.100      32
PUBLIC PARK         B      0.10      0.30      0.850      56
PUBLIC PARK         A      0.10      0.40      0.850      32
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.35
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.419
SUBAREA AREA(ACRES) = 0.47      SUBAREA RUNOFF(CFS) = 0.99
EFFECTIVE AREA(ACRES) = 2.25      AREA-AVERAGED Fm(INCH/HR) = 0.15
AREA-AVERAGED Fp(INCH/HR) = 0.37      AREA-AVERAGED Ap = 0.41
TOTAL AREA(ACRES) = 2.2      PEAK FLOW RATE(CFS) = 4.73

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END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.38      HALFSTREET FLOOD WIDTH(FEET) = 12.38
FLOW VELOCITY(FEET/SEC.) = 3.03      DEPTH*VELOCITY(FT*FT/SEC.) = 1.16
LONGEST FLOWPATH FROM NODE 1.01 TO NODE 1.07 = 848.74 FEET.

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END OF STUDY SUMMARY:
TOTAL AREA(ACRES) = 2.2      TC(MIN.) = 11.75
EFFECTIVE AREA(ACRES) = 2.25      AREA-AVERAGED Fm(INCH/HR) = 0.15
AREA-AVERAGED Fp(INCH/HR) = 0.37      AREA-AVERAGED Ap = 0.410
PEAK FLOW RATE(CFS) = 4.73
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END OF RATIONAL METHOD ANALYSIS

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Analysis prepared by:

Stantec

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***** DESCRIPTION OF STUDY *****
* Culver Alton - 10 Year Rational Method Study, Proposed Conditions *
* DMA 2: West Intersection Streamline, Alton *
* 10/25/2019 - ECS *
*****

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FILE NAME: CA10DMA2.DAT
TIME/DATE OF STUDY: 14:07 10/25/2019

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=====
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:
=====
--TIME-OF-CONCENTRATION MODEL*--

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USER SPECIFIED STORM EVENT(YEAR) = 10.00
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.95
DATA BANK RAINFALL USED
ANTECEDENT MOISTURE CONDITION (AMC) II ASSUMED FOR RATIONAL METHOD

USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL									
NO.	HALF- WIDTH	CROWN TO CROSSFALL	STREET-CROSSFALL: IN- / OUT-/PARK- SIDE / SIDE/ WAY	CURB HEIGHT	GUTTER-GEOMETRIES: WIDTH LIP HIKE	MANNING			
	(FT)	(FT)		(FT)	(FT) (FT) (FT)	(n)			
1	30.0	20.0	0.018/0.018/0.020	0.67	2.00 0.0312 0.167	0.0150			
2	40.0	30.0	0.018/0.018/0.020	0.67	2.00 0.0312 0.167	0.0150			

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:
1. Relative Flow-Depth = 0.00 FEET
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)*(Velocity) Constraint = 6.0 (FT*FT/S)
*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*
*USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

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*****
FLOW PROCESS FROM NODE      2.01 TO NODE      2.03 IS CODE = 21
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>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

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=====
INITIAL SUBAREA FLOW-LENGTH(FEET) = 330.00
ELEVATION DATA: UPSTREAM(FEET) = 72.00 DOWNSTREAM(FEET) = 68.00

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Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 7.474
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.224
SUBAREA Tc AND LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
PUBLIC PARK	B	0.01	0.30	0.850	56	11.88
PUBLIC PARK	A	0.27	0.40	0.850	32	11.88
COMMERCIAL	B	0.07	0.30	0.100	56	7.47
COMMERCIAL	A	0.40	0.40	0.100	32	7.47

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.39
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.380
SUBAREA RUNOFF(CFS) = 2.08
TOTAL AREA(ACRES) = 0.75 PEAK FLOW RATE(CFS) = 2.08

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Page 1

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                                10DMA2P.RES
FLOW PROCESS FROM NODE      2.03 TO NODE      2.05 IS CODE = 62
-----
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<
=====
UPSTREAM ELEVATION(FEET) = 68.00 DOWNSTREAM ELEVATION(FEET) = 62.00
STREET LENGTH(FEET) = 440.15 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.21
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.35
HALFSTREET FLOOD WIDTH(FEET) = 10.66
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.66
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.94
STREET FLOW TRAVEL TIME(MIN.) = 2.76 Tc(MIN.) = 10.24
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.693
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
COMMERCIAL B 0.22 0.30 0.100 56
COMMERCIAL A 0.27 0.40 0.100 32
PUBLIC PARK B 0.23 0.30 0.850 56
PUBLIC PARK A 0.28 0.40 0.850 32
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.35
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.483
SUBAREA AREA(ACRES) = 1.00 SUBAREA RUNOFF(CFS) = 2.27
EFFECTIVE AREA(ACRES) = 1.75 AREA-AVERAGED Fm(INCH/HR) = 0.16
AREA-AVERAGED Fp(INCH/HR) = 0.37 AREA-AVERAGED Ap = 0.44
TOTAL AREA(ACRES) = 1.8 PEAK FLOW RATE(CFS) = 3.99

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.37 HALFSTREET FLOOD WIDTH(FEET) = 11.76
FLOW VELOCITY(FEET/SEC.) = 2.79 DEPTH*VELOCITY(FT*FT/SEC.) = 1.04
LONGEST FLOWPATH FROM NODE 2.01 TO NODE 2.05 = 770.15 FEET.
=====
END OF STUDY SUMMARY:
TOTAL AREA(ACRES) = 1.8 TC(MIN.) = 10.24
EFFECTIVE AREA(ACRES) = 1.75 AREA-AVERAGED Fm(INCH/HR) = 0.16
AREA-AVERAGED Fp(INCH/HR) = 0.37 AREA-AVERAGED Ap = 0.439
PEAK FLOW RATE(CFS) = 3.99
=====
END OF RATIONAL METHOD ANALYSIS

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Analysis prepared by:

Stantec

***** DESCRIPTION OF STUDY *****
 * Culver Alton - 10 Year Rational Method Study, Proposed Conditions *
 * DMA 3: South Intersection Streamline, Alton *
 * 11/20/2019 - ECS *

FILE NAME: 10DMA3P.DAT
 TIME/DATE OF STUDY: 11:37 11/20/2019

=====

USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:

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--TIME-OF-CONCENTRATION MODEL*--

USER SPECIFIED STORM EVENT(YEAR) = 10.00
 SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00
 SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.95
 DATA BANK RAINFALL USED
 ANTECEDENT MOISTURE CONDITION (AMC) II ASSUMED FOR RATIONAL METHOD

USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL

NO.	HALF- WIDTH (FT)	CROWN TO CROSSFALL (FT)	STREET-CROSSFALL: IN- / OUT-/PARK- SIDE / SIDE/ WAY	CURB HEIGHT (FT)	GUTTER-GEOMETRIES:			MANNING FACTOR (n)
					WIDTH (FT)	LIP (FT)	HIKE (FT)	
1	30.0	20.0	0.018/0.018/0.020	0.67	2.00	0.0312	0.167	0.0150
2	40.0	30.0	0.018/0.018/0.020	0.67	2.00	0.0312	0.167	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:
 1. Relative Flow-Depth = 0.00 FEET
 as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
 2. (Depth)*(Velocity) Constraint = 6.0 (FT*FT/S)
 *SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
 OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*
 *USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

FLOW PROCESS FROM NODE 3.01 TO NODE 3.03 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
 >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 308.42
 ELEVATION DATA: UPSTREAM(FEET) = 82.00 DOWNSTREAM(FEET) = 77.00

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$
 SUBAREA ANALYSIS USED MINIMUM T_c (MIN.) = 6.864
 * 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.386
 SUBAREA T_c AND LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	F_p (INCH/HR)	A_p (DECIMAL)	SCS CN	T_c (MIN.)
COMMERCIAL	A	0.26	0.40	0.100	32	6.86
PUBLIC PARK	A	0.22	0.40	0.850	32	10.91

SUBAREA AVERAGE PERVIOUS LOSS RATE, F_p (INCH/HR) = 0.40
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, A_p = 0.444
 SUBAREA RUNOFF(CFS) = 1.39
 TOTAL AREA(ACRES) = 0.48 PEAK FLOW RATE(CFS) = 1.39

FLOW PROCESS FROM NODE 3.03 TO NODE 3.05 IS CODE = 62

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                                10DMA3P.RES
>>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>(STREET TABLE SECTION # 1 USED)<<<<<
=====
UPSTREAM ELEVATION(FEET) = 77.00 DOWNSTREAM ELEVATION(FEET) = 72.00
STREET LENGTH(FEET) = 500.82 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.60
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.35
HALFSTREET FLOOD WIDTH(FEET) = 10.43
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.24
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.78
STREET FLOW TRAVEL TIME(MIN.) = 3.73 Tc(MIN.) = 10.60
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.640
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
COMMERCIAL A 0.53 0.40 0.100 32
PUBLIC PARK A 0.57 0.40 0.850 32
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.40
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.489
SUBAREA AREA(ACRES) = 1.10 SUBAREA RUNOFF(CFS) = 2.42
EFFECTIVE AREA(ACRES) = 1.58 AREA-AVERAGED Fm(INCH/HR) = 0.19
AREA-AVERAGED Fp(INCH/HR) = 0.40 AREA-AVERAGED Ap = 0.48
TOTAL AREA(ACRES) = 1.6 PEAK FLOW RATE(CFS) = 3.48

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.38 HALFSTREET FLOOD WIDTH(FEET) = 11.91
FLOW VELOCITY(FEET/SEC.) = 2.38 DEPTH*VELOCITY(FT*FT/SEC.) = 0.89
LONGEST FLOWPATH FROM NODE 3.01 TO NODE 3.05 = 809.24 FEET.

*****
FLOW PROCESS FROM NODE 3.05 TO NODE 3.05 IS CODE = 1
-----
>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 10.60
RAINFALL INTENSITY(INCH/HR) = 2.64
AREA-AVERAGED Fm(INCH/HR) = 0.19
AREA-AVERAGED Fp(INCH/HR) = 0.40
AREA-AVERAGED Ap = 0.48
EFFECTIVE STREAM AREA(ACRES) = 1.58
TOTAL STREAM AREA(ACRES) = 1.58
PEAK FLOW RATE(CFS) AT CONFLUENCE = 3.48

*****
FLOW PROCESS FROM NODE 6.01 TO NODE 6.03 IS CODE = 21
-----
>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<
=====
INITIAL SUBAREA FLOW-LENGTH(FEET) = 237.14
ELEVATION DATA: UPSTREAM(FEET) = 73.50 DOWNSTREAM(FEET) = 72.50

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 8.089
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.082
SUBAREA Tc AND LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS Tc
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)
PUBLIC PARK D 0.06 0.20 0.850 75 12.85
COMMERCIAL D 0.39 0.20 0.100 75 8.09

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                                10DMA3P.RES
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.200
SUBAREA RUNOFF(CFS) = 1.23
TOTAL AREA(ACRES) = 0.45 PEAK FLOW RATE(CFS) = 1.23
*****
FLOW PROCESS FROM NODE 6.03 TO NODE 3.05 IS CODE = 62
-----
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<
=====
UPSTREAM ELEVATION(FEET) = 72.50 DOWNSTREAM ELEVATION(FEET) = 72.00
STREET LENGTH(FEET) = 276.24 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curb) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.67
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.39
HALFSTREET FLOOD WIDTH(FEET) = 12.54
AVERAGE FLOW VELOCITY(FEET/SEC.) = 1.04
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.40
STREET FLOW TRAVEL TIME(MIN.) = 4.41 Tc(MIN.) = 12.50
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.401
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
PUBLIC PARK A 0.01 0.40 0.850 32
COMMERCIAL A 0.27 0.40 0.100 32
COMMERCIAL B 0.09 0.30 0.100 56
PUBLIC PARK D 0.01 0.20 0.850 75
COMMERCIAL D 0.03 0.20 0.100 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.34
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.137
SUBAREA AREA(ACRES) = 0.41 SUBAREA RUNOFF(CFS) = 0.87
EFFECTIVE AREA(ACRES) = 0.86 AREA-AVERAGED Fm(INCH/HR) = 0.04
AREA-AVERAGED Fp(INCH/HR) = 0.25 AREA-AVERAGED Ap = 0.17
TOTAL AREA(ACRES) = 0.9 PEAK FLOW RATE(CFS) = 1.83

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.39 HALFSTREET FLOOD WIDTH(FEET) = 13.01
FLOW VELOCITY(FEET/SEC.) = 1.07 DEPTH*VELOCITY(FT*FT/SEC.) = 0.42
LONGEST FLOWPATH FROM NODE 6.01 TO NODE 3.05 = 513.38 FEET.
*****
FLOW PROCESS FROM NODE 6.03 TO NODE 3.05 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 12.50
RAINFALL INTENSITY(INCH/HR) = 2.40
AREA-AVERAGED Fm(INCH/HR) = 0.04
AREA-AVERAGED Fp(INCH/HR) = 0.25
AREA-AVERAGED Ap = 0.17
EFFECTIVE STREAM AREA(ACRES) = 0.86
TOTAL STREAM AREA(ACRES) = 0.86
PEAK FLOW RATE(CFS) AT CONFLUENCE = 1.83

** CONFLUENCE DATA **
STREAM Q Tc Intensity Fp(Fm) Ap Ae HEADWATER
NUMBER (CFS) (MIN.) (INCH/HR) (INCH/HR) (ACRES) NODE
1 3.48 10.60 2.640 0.40( 0.19) 0.48 1.6 3.01
2 1.83 12.50 2.401 0.25( 0.04) 0.17 0.9 6.01

```

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	5.19	10.60	2.640	0.38(0.14)	0.38	2.3	3.01
2	4.97	12.50	2.401	0.38(0.14)	0.37	2.4	6.01

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 5.19 Tc(MIN.) = 10.60
EFFECTIVE AREA(ACRES) = 2.31 AREA-AVERAGED Fm(INCH/HR) = 0.14
AREA-AVERAGED Fp(INCH/HR) = 0.38 AREA-AVERAGED Ap = 0.38
TOTAL AREA(ACRES) = 2.4
LONGEST FLOWPATH FROM NODE 3.01 TO NODE 3.05 = 809.24 FEET.

END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 2.4 TC(MIN.) = 10.60
EFFECTIVE AREA(ACRES) = 2.31 AREA-AVERAGED Fm(INCH/HR) = 0.14
AREA-AVERAGED Fp(INCH/HR) = 0.38 AREA-AVERAGED Ap = 0.379
PEAK FLOW RATE(CFS) = 5.19

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	5.19	10.60	2.640	0.38(0.14)	0.38	2.3	3.01
2	4.97	12.50	2.401	0.38(0.14)	0.37	2.4	6.01

END OF RATIONAL METHOD ANALYSIS

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Analysis prepared by:

Stantec

***** DESCRIPTION OF STUDY *****
 * Culver Alton - 10 Year Rational Method Study, Proposed Conditions *
 * DMA 4: East Intersection Streamline, Yale to Alton to Culver *
 * 11/20/2019 - ECS *

FILE NAME: 10DMA4P.DAT
 TIME/DATE OF STUDY: 11:40 11/20/2019

=====

USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:

=====

--*TIME-OF-CONCENTRATION MODEL*--

USER SPECIFIED STORM EVENT(YEAR) = 10.00
 SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00
 SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.95
 DATA BANK RAINFALL USED
 ANTECEDENT MOISTURE CONDITION (AMC) II ASSUMED FOR RATIONAL METHOD

USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL

NO.	HALF- WIDTH (FT)	CROWN TO CROSSFALL (FT)	STREET-CROSSFALL: IN- / OUT-/PARK- SIDE / SIDE/ WAY	CURB HEIGHT (FT)	GUTTER-GEOMETRIES:			MANNING FACTOR (n)
					WIDTH (FT)	LIP (FT)	HIKE (FT)	
1	30.0	20.0	0.018/0.018/0.020	0.67	2.00	0.0312	0.167	0.0150
2	40.0	30.0	0.018/0.018/0.020	0.67	2.00	0.0312	0.167	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:
 1. Relative Flow-Depth = 0.00 FEET
 as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
 2. (Depth)*(Velocity) Constraint = 6.0 (FT*FT/S)
 *SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
 OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*
 *USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

FLOW PROCESS FROM NODE 4.01 TO NODE 4.03 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
 >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 116.02
 ELEVATION DATA: UPSTREAM(FEET) = 89.00 DOWNSTREAM(FEET) = 87.00

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$
 SUBAREA ANALYSIS USED MINIMUM T_c (MIN.) = 5.000
 * 10 YEAR RAINFALL INTENSITY(INCH/HR) = 4.060
 SUBAREA T_c AND LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	F_p (INCH/HR)	A_p (DECIMAL)	SCS CN	T_c (MIN.)
PUBLIC PARK	A	0.01	0.40	0.850	32	7.29
COMMERCIAL	A	0.13	0.40	0.100	32	5.00

SUBAREA AVERAGE PERVIOUS LOSS RATE, F_p (INCH/HR) = 0.40
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, A_p = 0.154
 SUBAREA RUNOFF(CFS) = 0.50
 TOTAL AREA(ACRES) = 0.14 PEAK FLOW RATE(CFS) = 0.50

FLOW PROCESS FROM NODE 4.03 TO NODE 4.05 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<

=====

UPSTREAM ELEVATION(FEET) = 87.00 DOWNSTREAM ELEVATION(FEET) = 80.00
STREET LENGTH(FEET) = 301.23 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.27
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.26
HALFSTREET FLOOD WIDTH(FEET) = 5.41
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.79
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.72
STREET FLOW TRAVEL TIME(MIN.) = 1.80 Tc(MIN.) = 6.80
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.404
SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
PUBLIC PARK	A	0.07	0.40	0.850	32
COMMERCIAL	A	0.44	0.40	0.100	32

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.40
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.203
SUBAREA AREA(ACRES) = 0.51 SUBAREA RUNOFF(CFS) = 1.53
EFFECTIVE AREA(ACRES) = 0.65 AREA-AVERAGED Fm(INCH/HR) = 0.08
AREA-AVERAGED Fp(INCH/HR) = 0.40 AREA-AVERAGED Ap = 0.19
TOTAL AREA(ACRES) = 0.6 PEAK FLOW RATE(CFS) = 1.95

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.29 HALFSTREET FLOOD WIDTH(FEET) = 7.22
FLOW VELOCITY(FEET/SEC.) = 2.95 DEPTH*VELOCITY(FT*FT/SEC.) = 0.86
LONGEST FLOWPATH FROM NODE 4.01 TO NODE 4.05 = 417.25 FEET.

FLOW PROCESS FROM NODE 4.05 TO NODE 4.07 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<

=====

UPSTREAM ELEVATION(FEET) = 80.00 DOWNSTREAM ELEVATION(FEET) = 75.00
STREET LENGTH(FEET) = 369.87 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.01
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.35
HALFSTREET FLOOD WIDTH(FEET) = 10.35
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.62
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.91
STREET FLOW TRAVEL TIME(MIN.) = 2.36 Tc(MIN.) = 9.16
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.870
SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	A	0.27	0.40	0.100	32
PUBLIC PARK	A	0.63	0.40	0.850	32

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.40

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SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.625
SUBAREA AREA(ACRES) = 0.90 SUBAREA RUNOFF(CFS) = 2.12
EFFECTIVE AREA(ACRES) = 1.55 AREA-AVERAGED Fm(INCH/HR) = 0.18
AREA-AVERAGED Fp(INCH/HR) = 0.40 AREA-AVERAGED Ap = 0.44
TOTAL AREA(ACRES) = 1.5 PEAK FLOW RATE(CFS) = 3.76

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.37 HALFSTREET FLOOD WIDTH(FEET) = 11.52
FLOW VELOCITY(FEET/SEC.) = 2.72 DEPTH*VELOCITY(FT*FT/SEC.) = 1.00
LONGEST FLOWPATH FROM NODE 4.01 TO NODE 4.07 = 787.12 FEET.

*****
FLOW PROCESS FROM NODE 4.07 TO NODE 4.09 IS CODE = 62
-----
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<
=====
UPSTREAM ELEVATION(FEET) = 75.00 DOWNSTREAM ELEVATION(FEET) = 72.00
STREET LENGTH(FEET) = 362.03 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 4.57
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.41
HALFSTREET FLOOD WIDTH(FEET) = 13.95
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.37
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.97
STREET FLOW TRAVEL TIME(MIN.) = 2.55 Tc(MIN.) = 11.71
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.493
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
COMMERCIAL A 0.54 0.40 0.100 32
PUBLIC PARK A 0.22 0.40 0.850 32
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.40
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.317
SUBAREA AREA(ACRES) = 0.76 SUBAREA RUNOFF(CFS) = 1.62
EFFECTIVE AREA(ACRES) = 2.31 AREA-AVERAGED Fm(INCH/HR) = 0.16
AREA-AVERAGED Fp(INCH/HR) = 0.40 AREA-AVERAGED Ap = 0.40
TOTAL AREA(ACRES) = 2.3 PEAK FLOW RATE(CFS) = 4.85

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.42 HALFSTREET FLOOD WIDTH(FEET) = 14.34
FLOW VELOCITY(FEET/SEC.) = 2.39 DEPTH*VELOCITY(FT*FT/SEC.) = 1.00
LONGEST FLOWPATH FROM NODE 4.01 TO NODE 4.09 = 1149.15 FEET.

*****
FLOW PROCESS FROM NODE 4.09 TO NODE 4.09 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 11.71
RAINFALL INTENSITY(INCH/HR) = 2.49
AREA-AVERAGED Fm(INCH/HR) = 0.16
AREA-AVERAGED Fp(INCH/HR) = 0.40
AREA-AVERAGED Ap = 0.40
EFFECTIVE STREAM AREA(ACRES) = 2.31
TOTAL STREAM AREA(ACRES) = 2.31
PEAK FLOW RATE(CFS) AT CONFLUENCE = 4.85

*****
FLOW PROCESS FROM NODE 5.01 TO NODE 5.03 IS CODE = 21
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>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<
=====
INITIAL SUBAREA FLOW-LENGTH(FEET) = 253.47
ELEVATION DATA: UPSTREAM(FEET) = 75.00 DOWNSTREAM(FEET) = 73.50

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 7.763
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.155
SUBAREA Tc AND LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/      SCS SOIL  AREA      Fp      Ap      SCS  Tc
LAND USE              GROUP  (ACRES)  (INCH/HR)  (DECIMAL)  CN  (MIN.)
COMMERCIAL             A      0.24      0.40      0.100     32   7.76
PUBLIC PARK            A      0.24      0.40      0.850     32  12.33
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.40
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.475
SUBAREA RUNOFF(CFS) = 1.28
TOTAL AREA(ACRES) = 0.48 PEAK FLOW RATE(CFS) = 1.28

*****
FLOW PROCESS FROM NODE 5.03 TO NODE 5.05 IS CODE = 62
-----
>>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>(STREET TABLE SECTION # 1 USED)<<<<<
=====
UPSTREAM ELEVATION(FEET) = 73.50 DOWNSTREAM ELEVATION(FEET) = 72.00
STREET LENGTH(FEET) = 273.08 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.03
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.35
HALFSTREET FLOOD WIDTH(FEET) = 10.66
AVERAGE FLOW VELOCITY(FEET/SEC.) = 1.68
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.59
STREET FLOW TRAVEL TIME(MIN.) = 2.72 Tc(MIN.) = 10.48
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.657
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/      SCS SOIL  AREA      Fp      Ap      SCS
LAND USE              GROUP  (ACRES)  (INCH/HR)  (DECIMAL)  CN
COMMERCIAL             A      0.57      0.40      0.100     32
PUBLIC PARK            A      0.07      0.40      0.850     32
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.40
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.182
SUBAREA AREA(ACRES) = 0.64 SUBAREA RUNOFF(CFS) = 1.49
EFFECTIVE AREA(ACRES) = 1.12 AREA-AVERAGED Fm(INCH/HR) = 0.12
AREA-AVERAGED Fp(INCH/HR) = 0.40 AREA-AVERAGED Ap = 0.31
TOTAL AREA(ACRES) = 1.1 PEAK FLOW RATE(CFS) = 2.55

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.37 HALFSTREET FLOOD WIDTH(FEET) = 11.84
FLOW VELOCITY(FEET/SEC.) = 1.77 DEPTH*VELOCITY(FT*FT/SEC.) = 0.66
LONGEST FLOWPATH FROM NODE 5.01 TO NODE 5.05 = 526.55 FEET.

*****
FLOW PROCESS FROM NODE 5.05 TO NODE 4.09 IS CODE = 1
-----
>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 10.48
RAINFALL INTENSITY(INCH/HR) = 2.66
AREA-AVERAGED Fm(INCH/HR) = 0.12

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AREA-AVERAGED F_p (INCH/HR) = 0.40
 AREA-AVERAGED A_p = 0.31
 EFFECTIVE STREAM AREA(ACRES) = 1.12
 TOTAL STREAM AREA(ACRES) = 1.12
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 2.55

** CONFLUENCE DATA **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	$F_p(F_m)$ (INCH/HR)	A_p	A_e (ACRES)	HEADWATER NODE
1	4.85	11.71	2.493	0.40(0.16)	0.40	2.3	4.01
2	2.55	10.48	2.657	0.40(0.12)	0.31	1.1	5.01

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	$F_p(F_m)$ (INCH/HR)	A_p	A_e (ACRES)	HEADWATER NODE
1	7.20	10.48	2.657	0.40(0.15)	0.37	3.2	5.01
2	7.24	11.71	2.493	0.40(0.15)	0.37	3.4	4.01

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 7.24 Tc(MIN.) = 11.71
 EFFECTIVE AREA(ACRES) = 3.43 AREA-AVERAGED F_m (INCH/HR) = 0.15
 AREA-AVERAGED F_p (INCH/HR) = 0.40 AREA-AVERAGED A_p = 0.37
 TOTAL AREA(ACRES) = 3.4
 LONGEST FLOWPATH FROM NODE 4.01 TO NODE 4.09 = 1149.15 FEET.

END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 3.4 TC(MIN.) = 11.71
 EFFECTIVE AREA(ACRES) = 3.43 AREA-AVERAGED F_m (INCH/HR) = 0.15
 AREA-AVERAGED F_p (INCH/HR) = 0.40 AREA-AVERAGED A_p = 0.371
 PEAK FLOW RATE(CFS) = 7.24

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	$F_p(F_m)$ (INCH/HR)	A_p	A_e (ACRES)	HEADWATER NODE
1	7.20	10.48	2.657	0.40(0.15)	0.37	3.2	5.01
2	7.24	11.71	2.493	0.40(0.15)	0.37	3.4	4.01

END OF RATIONAL METHOD ANALYSIS

Rational Method – 25-Year Storm Event: Existing Condition

 RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE
 (Reference: 1986 ORANGE COUNTY HYDROLOGY CRITERION)
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 Ver. 23.0 Release Date: 07/01/2016 License ID 1535

Analysis prepared by:

Stantec

***** DESCRIPTION OF STUDY *****
 * Culver Alton - 25 Year Rational Method Study, Existing Conditions *
 * DMA 1: North Intersection Streamline, Culver to Alton *
 * 11/20/2019 - ECS *

FILE NAME: 25DMA1E.DAT
 TIME/DATE OF STUDY: 11:14 11/20/2019

=====

USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:

=====

--*TIME-OF-CONCENTRATION MODEL*--

USER SPECIFIED STORM EVENT(YEAR) = 25.00
 SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00
 SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.95
 DATA BANK RAINFALL USED
 ANTECEDENT MOISTURE CONDITION (AMC) II ASSUMED FOR RATIONAL METHOD

USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL

NO.	HALF- WIDTH	CROWN TO CROSSFALL	STREET-CROSSFALL: IN- / OUT-/PARK- SIDE / SIDE/ WAY	CURB HEIGHT	GUTTER-GEOMETRIES: WIDTH LIP HIKE	MANNING FACTOR
	(FT)	(FT)		(FT)	(FT) (FT) (FT)	(n)
1	30.0	20.0	0.018/0.018/0.020	0.67	2.00 0.0313 0.167	0.0150
2	40.0	30.0	0.018/0.018/0.020	0.67	2.00 0.0313 0.167	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:
 1. Relative Flow-Depth = 0.00 FEET
 as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
 2. (Depth)*(Velocity) Constraint = 6.0 (FT*FT/S)
 *SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
 OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*
 *USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

FLOW PROCESS FROM NODE 1.01 TO NODE 1.03 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
 >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 330.00
 ELEVATION DATA: UPSTREAM(FEET) = 75.00 DOWNSTREAM(FEET) = 73.00

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$
 SUBAREA ANALYSIS USED MINIMUM T_c (MIN.) = 8.586
 * 25 YEAR RAINFALL INTENSITY(INCH/HR) = 3.552
 SUBAREA T_c AND LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	F_p (INCH/HR)	A_p (DECIMAL)	SCS CN	T_c (MIN.)
COMMERCIAL	A	0.41	0.40	0.100	32	8.59
PUBLIC PARK	A	0.27	0.40	0.850	32	13.64

SUBAREA AVERAGE PERVIOUS LOSS RATE, F_p (INCH/HR) = 0.40
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, A_p = 0.398
 SUBAREA RUNOFF(CFS) = 2.08
 TOTAL AREA(ACRES) = 0.68 PEAK FLOW RATE(CFS) = 2.08

FLOW PROCESS FROM NODE 1.03 TO NODE 1.05 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<

=====

UPSTREAM ELEVATION(FEET) = 73.00 DOWNSTREAM ELEVATION(FEET) = 68.00
STREET LENGTH(FEET) = 355.96 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.56
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.36
HALFSTREET FLOOD WIDTH(FEET) = 11.13
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.74
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.99
STREET FLOW TRAVEL TIME(MIN.) = 2.17 Tc(MIN.) = 10.75
* 25 YEAR RAINFALL INTENSITY (INCH/HR) = 3.127

SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	B	0.12	0.30	0.100	56
COMMERCIAL	A	0.56	0.40	0.100	32
PUBLIC PARK	B	0.20	0.30	0.850	56
PUBLIC PARK	A	0.22	0.40	0.850	32

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.36
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.386
SUBAREA AREA(ACRES) = 1.10 SUBAREA RUNOFF(CFS) = 2.96
EFFECTIVE AREA(ACRES) = 1.78 AREA-AVERAGED Fm(INCH/HR) = 0.15
AREA-AVERAGED Fp(INCH/HR) = 0.37 AREA-AVERAGED Ap = 0.39
TOTAL AREA(ACRES) = 1.8 PEAK FLOW RATE(CFS) = 4.78

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.39 HALFSTREET FLOOD WIDTH(FEET) = 12.70
FLOW VELOCITY(FEET/SEC.) = 2.92 DEPTH*VELOCITY(FT*FT/SEC.) = 1.14
LONGEST FLOWPATH FROM NODE 1.01 TO NODE 1.05 = 685.96 FEET.

FLOW PROCESS FROM NODE 1.05 TO NODE 1.07 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<

=====

UPSTREAM ELEVATION(FEET) = 68.00 DOWNSTREAM ELEVATION(FEET) = 65.50
STREET LENGTH(FEET) = 162.78 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 5.38
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.40
HALFSTREET FLOOD WIDTH(FEET) = 13.09
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.12
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 1.24
STREET FLOW TRAVEL TIME(MIN.) = 0.87 Tc(MIN.) = 11.62
* 25 YEAR RAINFALL INTENSITY (INCH/HR) = 2.993

SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	B	0.14	0.30	0.100	56

25DMA1E.RES

COMMERCIAL	A	0.13	0.40	0.100	32
PUBLIC PARK	B	0.10	0.30	0.850	56
PUBLIC PARK	A	0.10	0.40	0.850	32

SUBAREA AVERAGE PERVIOUS LOSS RATE, F_p (INCH/HR) = 0.35
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, A_p = 0.419
 SUBAREA AREA(ACRES) = 0.47 SUBAREA RUNOFF(CFS) = 1.20
 EFFECTIVE AREA(ACRES) = 2.25 AREA-AVERAGED F_m (INCH/HR) = 0.15
 AREA-AVERAGED F_p (INCH/HR) = 0.37 AREA-AVERAGED A_p = 0.40
 TOTAL AREA(ACRES) = 2.2 PEAK FLOW RATE(CFS) = 5.76

END OF SUBAREA STREET FLOW HYDRAULICS:
 DEPTH(FEET) = 0.40 HALFSTREET FLOOD WIDTH(FEET) = 13.48
 FLOW VELOCITY(FEET/SEC.) = 3.17 DEPTH*VELOCITY(FT*FT/SEC.) = 1.28
 LONGEST FLOWPATH FROM NODE 1.01 TO NODE 1.07 = 848.74 FEET.

=====

END OF STUDY SUMMARY:

TOTAL AREA(ACRES)	=	2.2	TC(MIN.)	=	11.62
EFFECTIVE AREA(ACRES)	=	2.25	AREA-AVERAGED F_m (INCH/HR)	=	0.15
AREA-AVERAGED F_p (INCH/HR)	=	0.37	AREA-AVERAGED A_p	=	0.397
PEAK FLOW RATE(CFS)	=	5.76			

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END OF RATIONAL METHOD ANALYSIS

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Analysis prepared by:

Stantec

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***** DESCRIPTION OF STUDY *****
* Culver Alton - 25 Year Rational Method Study, Existing Conditions *
* DMA 2: West Intersection Streamline, Alton *
* 11/20/2019 - ECS *
*****
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FILE NAME: 25DMA2E.DAT
TIME/DATE OF STUDY: 11:19 11/20/2019

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=====
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:
=====
--*TIME-OF-CONCENTRATION MODEL*--
```

USER SPECIFIED STORM EVENT(YEAR) = 25.00
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.95
DATA BANK RAINFALL USED
ANTECEDENT MOISTURE CONDITION (AMC) II ASSUMED FOR RATIONAL METHOD

USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL									
NO.	HALF- WIDTH (FT)	CROWN TO CROSSFALL (FT)	STREET-CROSSFALL: IN- / OUT-/PARK- SIDE / SIDE/ WAY	CURB HEIGHT (FT)	GUTTER-GEOMETRIES: WIDTH LIP HIKE (FT) (FT) (FT)	MANNING FACTOR (n)			
	1	30.0	20.0	0.018/0.018/0.020	0.67	2.00 0.0312 0.167	0.0150		
2	40.0	30.0	0.018/0.018/0.020	0.67	2.00 0.0312 0.167	0.0150			

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:
1. Relative Flow-Depth = 0.00 FEET
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)*(Velocity) Constraint = 6.0 (FT*FT/S)
*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*
*USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

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*****
FLOW PROCESS FROM NODE 2.01 TO NODE 2.03 IS CODE = 21
*****
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>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<
=====
INITIAL SUBAREA FLOW-LENGTH(FEET) = 330.00
ELEVATION DATA: UPSTREAM(FEET) = 72.00 DOWNSTREAM(FEET) = 68.00
```

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$
SUBAREA ANALYSIS USED MINIMUM T_c (MIN.) = 7.474
* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 3.842
SUBAREA T_c AND LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	F_p (INCH/HR)	A_p (DECIMAL)	SCS CN	T_c (MIN.)
PUBLIC PARK	B	0.01	0.30	0.850	56	11.88
PUBLIC PARK	A	0.27	0.40	0.850	32	11.88
COMMERCIAL	B	0.07	0.30	0.100	56	7.47
COMMERCIAL	A	0.40	0.40	0.100	32	7.47

SUBAREA AVERAGE PERVIOUS LOSS RATE, F_p (INCH/HR) = 0.39
SUBAREA AVERAGE PERVIOUS AREA FRACTION, A_p = 0.380
SUBAREA RUNOFF(CFS) = 2.49
TOTAL AREA(ACRES) = 0.75 PEAK FLOW RATE(CFS) = 2.49

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Page 1
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                                25DMA2E.RES
FLOW PROCESS FROM NODE      2.03 TO NODE      2.05 IS CODE = 62
-----
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<
=====
UPSTREAM ELEVATION(FEET) = 68.00 DOWNSTREAM ELEVATION(FEET) = 62.00
STREET LENGTH(FEET) = 440.15 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.87
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.37
HALFSTREET FLOOD WIDTH(FEET) = 11.68
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.74
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 1.02
STREET FLOW TRAVEL TIME(MIN.) = 2.67 Tc(MIN.) = 10.15
* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 3.231
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/      SCS SOIL      AREA      Fp      Ap      SCS
LAND USE      GROUP      (ACRES)      (INCH/HR)      (DECIMAL)      CN
COMMERCIAL      B      0.22      0.30      0.100      56
COMMERCIAL      A      0.27      0.40      0.100      32
PUBLIC PARK      B      0.23      0.30      0.850      56
PUBLIC PARK      A      0.28      0.40      0.850      32
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.35
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.483
SUBAREA AREA(ACRES) = 1.00 SUBAREA RUNOFF(CFS) = 2.75
EFFECTIVE AREA(ACRES) = 1.75 AREA-AVERAGED Fm(INCH/HR) = 0.16
AREA-AVERAGED Fp(INCH/HR) = 0.37 AREA-AVERAGED Ap = 0.44
TOTAL AREA(ACRES) = 1.8 PEAK FLOW RATE(CFS) = 4.83

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.39 HALFSTREET FLOOD WIDTH(FEET) = 12.85
FLOW VELOCITY(FEET/SEC.) = 2.90 DEPTH*VELOCITY(FT*FT/SEC.) = 1.14
LONGEST FLOWPATH FROM NODE 2.01 TO NODE 2.05 = 770.15 FEET.
=====
END OF STUDY SUMMARY:
TOTAL AREA(ACRES) = 1.8 TC(MIN.) = 10.15
EFFECTIVE AREA(ACRES) = 1.75 AREA-AVERAGED Fm(INCH/HR) = 0.16
AREA-AVERAGED Fp(INCH/HR) = 0.37 AREA-AVERAGED Ap = 0.439
PEAK FLOW RATE(CFS) = 4.83
=====
END OF RATIONAL METHOD ANALYSIS

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Analysis prepared by:

Stantec

***** DESCRIPTION OF STUDY *****
 * Culver Alton - 25 Year Rational Method Study, Existing Conditions *
 * DMA 3: South Intersection Streamline, Alton *
 * 11/07/2019 - ECS *

FILE NAME: 25DMA3E.DAT
 TIME/DATE OF STUDY: 16:39 11/07/2019

=====

USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:

=====

--*TIME-OF-CONCENTRATION MODEL*--

USER SPECIFIED STORM EVENT(YEAR) = 25.00
 SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00
 SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.95
 DATA BANK RAINFALL USED
 ANTECEDENT MOISTURE CONDITION (AMC) II ASSUMED FOR RATIONAL METHOD

USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL

NO.	HALF- WIDTH	CROWN TO CROSSFALL	STREET-CROSSFALL: IN- / OUT-/PARK- SIDE / SIDE/ WAY	CURB HEIGHT	GUTTER-GEOMETRIES: WIDTH LIP HIKE	MANNING FACTOR
	(FT)	(FT)		(FT)	(FT) (FT) (FT)	(n)
1	30.0	20.0	0.018/0.018/0.020	0.67	2.00 0.0312 0.167	0.0150
2	40.0	30.0	0.018/0.018/0.020	0.67	2.00 0.0312 0.167	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:
 1. Relative Flow-Depth = 0.00 FEET
 as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
 2. (Depth)*(Velocity) Constraint = 6.0 (FT*FT/S)
 *SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
 OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*
 *USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

FLOW PROCESS FROM NODE 3.01 TO NODE 3.03 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
 >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 308.42
 ELEVATION DATA: UPSTREAM(FEET) = 82.00 DOWNSTREAM(FEET) = 77.00

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$
 SUBAREA ANALYSIS USED MINIMUM T_c (MIN.) = 6.864
 * 25 YEAR RAINFALL INTENSITY(INCH/HR) = 4.032
 SUBAREA T_c AND LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	F_p (INCH/HR)	A_p (DECIMAL)	SCS CN	T_c (MIN.)
COMMERCIAL	A	0.26	0.40	0.100	32	6.86
PUBLIC PARK	A	0.22	0.40	0.850	32	10.91

SUBAREA AVERAGE PERVIOUS LOSS RATE, F_p (INCH/HR) = 0.40
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, A_p = 0.444
 SUBAREA RUNOFF(CFS) = 1.67
 TOTAL AREA(ACRES) = 0.48 PEAK FLOW RATE(CFS) = 1.67

FLOW PROCESS FROM NODE 3.03 TO NODE 3.05 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<

=====

UPSTREAM ELEVATION(FEET) = 77.00 DOWNSTREAM ELEVATION(FEET) = 72.00
STREET LENGTH(FEET) = 500.82 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curb-to-curb) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.15
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.37
HALFSTREET FLOOD WIDTH(FEET) = 11.37
AVERAGE FLOW VELOCITY(FT/SEC.) = 2.34
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.85
STREET FLOW TRAVEL TIME(MIN.) = 3.57 Tc(MIN.) = 10.44
* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 3.181

SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	A	0.53	0.40	0.100	32
PUBLIC PARK	A	0.57	0.40	0.850	32

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.40
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.489
SUBAREA AREA(ACRES) = 1.10 SUBAREA RUNOFF(CFS) = 2.96
EFFECTIVE AREA(ACRES) = 1.58 AREA-AVERAGED Fm(INCH/HR) = 0.19
AREA-AVERAGED Fp(INCH/HR) = 0.40 AREA-AVERAGED Ap = 0.48
TOTAL AREA(ACRES) = 1.6 PEAK FLOW RATE(CFS) = 4.25

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.39 HALFSTREET FLOOD WIDTH(FEET) = 13.01
FLOW VELOCITY(FT/SEC.) = 2.49 DEPTH*VELOCITY(FT*FT/SEC.) = 0.99
LONGEST FLOWPATH FROM NODE 3.01 TO NODE 3.05 = 809.24 FEET.

FLOW PROCESS FROM NODE 3.05 TO NODE 3.05 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

=====

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 10.44
RAINFALL INTENSITY(INCH/HR) = 3.18
AREA-AVERAGED Fm(INCH/HR) = 0.19
AREA-AVERAGED Fp(INCH/HR) = 0.40
AREA-AVERAGED Ap = 0.48
EFFECTIVE STREAM AREA(ACRES) = 1.58
TOTAL STREAM AREA(ACRES) = 1.58
PEAK FLOW RATE(CFS) AT CONFLUENCE = 4.25

FLOW PROCESS FROM NODE 6.01 TO NODE 6.03 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 237.14
ELEVATION DATA: UPSTREAM(FEET) = 73.50 DOWNSTREAM(FEET) = 72.50

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 8.089
* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 3.674
SUBAREA Tc AND LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
PUBLIC PARK	D	0.07	0.20	0.850	75	12.85
COMMERCIAL	D	0.38	0.20	0.100	75	8.09

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                                25DMA3E.RES
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.217
SUBAREA RUNOFF(CFS) = 1.47
TOTAL AREA(ACRES) = 0.45 PEAK FLOW RATE(CFS) = 1.47

*****
FLOW PROCESS FROM NODE 6.03 TO NODE 3.05 IS CODE = 62
-----
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<
=====
UPSTREAM ELEVATION(FEET) = 72.50 DOWNSTREAM ELEVATION(FEET) = 72.00
STREET LENGTH(FEET) = 276.24 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curb) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.99
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.40
HALFSTREET FLOOD WIDTH(FEET) = 13.55
AVERAGE FLOW VELOCITY(FEET/SEC.) = 1.09
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.44
STREET FLOW TRAVEL TIME(MIN.) = 4.23 Tc(MIN.) = 12.32
* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 2.895
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
PUBLIC PARK A 0.03 0.40 0.850 32
COMMERCIAL A 0.25 0.40 0.100 32
COMMERCIAL B 0.09 0.30 0.100 56
PUBLIC PARK D 0.02 0.20 0.850 75
COMMERCIAL D 0.02 0.20 0.100 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.34
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.191
SUBAREA AREA(ACRES) = 0.41 SUBAREA RUNOFF(CFS) = 1.04
EFFECTIVE AREA(ACRES) = 0.86 AREA-AVERAGED Fm(INCH/HR) = 0.05
AREA-AVERAGED Fp(INCH/HR) = 0.26 AREA-AVERAGED Ap = 0.20
TOTAL AREA(ACRES) = 0.9 PEAK FLOW RATE(CFS) = 2.20

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.41 HALFSTREET FLOOD WIDTH(FEET) = 14.10
FLOW VELOCITY(FEET/SEC.) = 1.12 DEPTH*VELOCITY(FT*FT/SEC.) = 0.46
LONGEST FLOWPATH FROM NODE 6.01 TO NODE 3.05 = 513.38 FEET.

*****
FLOW PROCESS FROM NODE 6.03 TO NODE 3.05 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 12.32
RAINFALL INTENSITY(INCH/HR) = 2.90
AREA-AVERAGED Fm(INCH/HR) = 0.05
AREA-AVERAGED Fp(INCH/HR) = 0.26
AREA-AVERAGED Ap = 0.20
EFFECTIVE STREAM AREA(ACRES) = 0.86
TOTAL STREAM AREA(ACRES) = 0.86
PEAK FLOW RATE(CFS) AT CONFLUENCE = 2.20

** CONFLUENCE DATA **
STREAM Q Tc Intensity Fp(Fm) Ap Ae HEADWATER
NUMBER (CFS) (MIN.) (INCH/HR) (INCH/HR) (ACRES) NODE
1 4.25 10.44 3.181 0.40( 0.19) 0.48 1.6 3.01
2 2.20 12.32 2.895 0.26( 0.05) 0.20 0.9 6.01

```


RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	6.30	10.44	3.181	0.38(0.15)	0.39	2.3	3.01
2	6.05	12.32	2.895	0.37(0.14)	0.38	2.4	6.01

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 6.30 Tc(MIN.) = 10.44
EFFECTIVE AREA(ACRES) = 2.31 AREA-AVERAGED Fm(INCH/HR) = 0.15
AREA-AVERAGED Fp(INCH/HR) = 0.38 AREA-AVERAGED Ap = 0.39
TOTAL AREA(ACRES) = 2.4
LONGEST FLOWPATH FROM NODE 3.01 TO NODE 3.05 = 809.24 FEET.

=====

END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 2.4 TC(MIN.) = 10.44
EFFECTIVE AREA(ACRES) = 2.31 AREA-AVERAGED Fm(INCH/HR) = 0.15
AREA-AVERAGED Fp(INCH/HR) = 0.38 AREA-AVERAGED Ap = 0.390
PEAK FLOW RATE(CFS) = 6.30

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	6.30	10.44	3.181	0.38(0.15)	0.39	2.3	3.01
2	6.05	12.32	2.895	0.37(0.14)	0.38	2.4	6.01

=====

END OF RATIONAL METHOD ANALYSIS

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Analysis prepared by:

Stantec

***** DESCRIPTION OF STUDY *****
 * Culver Alton - 25 Year Rational Method Study, Existing Conditions *
 * DMA 4: East Intersection Streamline, Yale to Alton to Culver *
 * 11/07/2019 - ECS *

FILE NAME: 25DMA4E.DAT
 TIME/DATE OF STUDY: 16:47 11/07/2019

=====

USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:

=====

--*TIME-OF-CONCENTRATION MODEL*--

USER SPECIFIED STORM EVENT(YEAR) = 25.00
 SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00
 SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.95
 DATA BANK RAINFALL USED
 ANTECEDENT MOISTURE CONDITION (AMC) II ASSUMED FOR RATIONAL METHOD

USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL

NO.	HALF- WIDTH (FT)	CROWN TO CROSSFALL (FT)	STREET-CROSSFALL: IN- / OUT-/PARK- SIDE / SIDE/ WAY	CURB HEIGHT (FT)	GUTTER-GEOMETRIES:			MANNING FACTOR (n)
					WIDTH (FT)	LIP (FT)	HIKE (FT)	
1	30.0	20.0	0.018/0.018/0.020	0.67	2.00	0.0312	0.167	0.0150
2	40.0	30.0	0.018/0.018/0.020	0.67	2.00	0.0312	0.167	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:
 1. Relative Flow-Depth = 0.00 FEET
 as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
 2. (Depth)*(Velocity) Constraint = 6.0 (FT*FT/S)
 *SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
 OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*
 *USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

FLOW PROCESS FROM NODE 4.01 TO NODE 4.03 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
 >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 116.02
 ELEVATION DATA: UPSTREAM(FEET) = 89.00 DOWNSTREAM(FEET) = 87.00

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$
 SUBAREA ANALYSIS USED MINIMUM T_c (MIN.) = 5.000
 * 25 YEAR RAINFALL INTENSITY(INCH/HR) = 4.824
 SUBAREA T_c AND LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	F_p (INCH/HR)	A_p (DECIMAL)	SCS CN	T_c (MIN.)
PUBLIC PARK	A	0.01	0.40	0.850	32	7.29
COMMERCIAL	A	0.13	0.40	0.100	32	5.00

SUBAREA AVERAGE PERVIOUS LOSS RATE, F_p (INCH/HR) = 0.40
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, A_p = 0.154
 SUBAREA RUNOFF(CFS) = 0.60
 TOTAL AREA(ACRES) = 0.14 PEAK FLOW RATE(CFS) = 0.60

FLOW PROCESS FROM NODE 4.03 TO NODE 4.05 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<

=====

UPSTREAM ELEVATION(FEET) = 87.00 DOWNSTREAM ELEVATION(FEET) = 80.00
STREET LENGTH(FEET) = 301.23 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.52
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.27
HALFSTREET FLOOD WIDTH(FEET) = 6.16
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.85
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.78
STREET FLOW TRAVEL TIME(MIN.) = 1.76 Tc(MIN.) = 6.76
* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 4.066
SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
PUBLIC PARK	A	0.07	0.40	0.850	32
COMMERCIAL	A	0.44	0.40	0.100	32

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.40
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.203
SUBAREA AREA(ACRES) = 0.51 SUBAREA RUNOFF(CFS) = 1.83
EFFECTIVE AREA(ACRES) = 0.65 AREA-AVERAGED Fm(INCH/HR) = 0.08
AREA-AVERAGED Fp(INCH/HR) = 0.40 AREA-AVERAGED Ap = 0.19
TOTAL AREA(ACRES) = 0.6 PEAK FLOW RATE(CFS) = 2.33

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.30 HALFSTREET FLOOD WIDTH(FEET) = 7.97
FLOW VELOCITY(FEET/SEC.) = 3.07 DEPTH*VELOCITY(FT*FT/SEC.) = 0.94
LONGEST FLOWPATH FROM NODE 4.01 TO NODE 4.05 = 417.25 FEET.

FLOW PROCESS FROM NODE 4.05 TO NODE 4.07 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<

=====

UPSTREAM ELEVATION(FEET) = 80.00 DOWNSTREAM ELEVATION(FEET) = 75.00
STREET LENGTH(FEET) = 369.87 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.63
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.37
HALFSTREET FLOOD WIDTH(FEET) = 11.37
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.70
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.99
STREET FLOW TRAVEL TIME(MIN.) = 2.29 Tc(MIN.) = 9.05
* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 3.448
SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	A	0.27	0.40	0.100	32
PUBLIC PARK	A	0.63	0.40	0.850	32

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.40

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SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.625
SUBAREA AREA(ACRES) = 0.90 SUBAREA RUNOFF(CFS) = 2.59
EFFECTIVE AREA(ACRES) = 1.55 AREA-AVERAGED Fm(INCH/HR) = 0.18
AREA-AVERAGED Fp(INCH/HR) = 0.40 AREA-AVERAGED Ap = 0.44
TOTAL AREA(ACRES) = 1.5 PEAK FLOW RATE(CFS) = 4.56

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.39 HALFSTREET FLOOD WIDTH(FEET) = 12.54
FLOW VELOCITY(FEET/SEC.) = 2.86 DEPTH*VELOCITY(FT*FT/SEC.) = 1.10
LONGEST FLOWPATH FROM NODE 4.01 TO NODE 4.07 = 787.12 FEET.

*****
FLOW PROCESS FROM NODE 4.07 TO NODE 4.09 IS CODE = 62
-----
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<
=====
UPSTREAM ELEVATION(FEET) = 75.00 DOWNSTREAM ELEVATION(FEET) = 72.00
STREET LENGTH(FEET) = 362.03 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 5.53
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.43
HALFSTREET FLOOD WIDTH(FEET) = 15.12
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.47
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 1.07
STREET FLOW TRAVEL TIME(MIN.) = 2.44 Tc(MIN.) = 11.49
* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 3.013
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
COMMERCIAL A 0.37 0.40 0.100 32
PUBLIC PARK A 0.39 0.40 0.850 32
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.40
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.485
SUBAREA AREA(ACRES) = 0.76 SUBAREA RUNOFF(CFS) = 1.93
EFFECTIVE AREA(ACRES) = 2.31 AREA-AVERAGED Fm(INCH/HR) = 0.18
AREA-AVERAGED Fp(INCH/HR) = 0.40 AREA-AVERAGED Ap = 0.46
TOTAL AREA(ACRES) = 2.3 PEAK FLOW RATE(CFS) = 5.88

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.44 HALFSTREET FLOOD WIDTH(FEET) = 15.51
FLOW VELOCITY(FEET/SEC.) = 2.51 DEPTH*VELOCITY(FT*FT/SEC.) = 1.10
LONGEST FLOWPATH FROM NODE 4.01 TO NODE 4.09 = 1149.15 FEET.

*****
FLOW PROCESS FROM NODE 4.09 TO NODE 4.09 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 11.49
RAINFALL INTENSITY(INCH/HR) = 3.01
AREA-AVERAGED Fm(INCH/HR) = 0.18
AREA-AVERAGED Fp(INCH/HR) = 0.40
AREA-AVERAGED Ap = 0.46
EFFECTIVE STREAM AREA(ACRES) = 2.31
TOTAL STREAM AREA(ACRES) = 2.31
PEAK FLOW RATE(CFS) AT CONFLUENCE = 5.88

*****
FLOW PROCESS FROM NODE 5.01 TO NODE 5.03 IS CODE = 21
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>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<
=====
INITIAL SUBAREA FLOW-LENGTH(FEET) = 253.47
ELEVATION DATA: UPSTREAM(FEET) = 75.00 DOWNSTREAM(FEET) = 73.50

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 7.763
* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 3.761
SUBAREA Tc AND LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/      SCS SOIL  AREA      Fp      Ap      SCS  Tc
LAND USE              GROUP  (ACRES)  (INCH/HR)  (DECIMAL)  CN  (MIN.)
COMMERCIAL             A      0.21      0.40      0.100     32   7.76
PUBLIC PARK            A      0.27      0.40      0.850     32  12.33
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.40
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.522
SUBAREA RUNOFF(CFS) = 1.53
TOTAL AREA(ACRES) = 0.48 PEAK FLOW RATE(CFS) = 1.53

*****
FLOW PROCESS FROM NODE 5.03 TO NODE 5.05 IS CODE = 62
-----
>>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>(STREET TABLE SECTION # 1 USED)<<<<<
=====
UPSTREAM ELEVATION(FEET) = 73.50 DOWNSTREAM ELEVATION(FEET) = 72.00
STREET LENGTH(FEET) = 273.08 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.42
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.37
HALFSTREET FLOOD WIDTH(FEET) = 11.52
AVERAGE FLOW VELOCITY(FEET/SEC.) = 1.75
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.64
STREET FLOW TRAVEL TIME(MIN.) = 2.60 Tc(MIN.) = 10.36
* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 3.193
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/      SCS SOIL  AREA      Fp      Ap      SCS
LAND USE              GROUP  (ACRES)  (INCH/HR)  (DECIMAL)  CN
COMMERCIAL             A      0.43      0.40      0.100     32
PUBLIC PARK            A      0.21      0.40      0.850     32
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.40
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.346
SUBAREA AREA(ACRES) = 0.64 SUBAREA RUNOFF(CFS) = 1.76
EFFECTIVE AREA(ACRES) = 1.12 AREA-AVERAGED Fm(INCH/HR) = 0.17
AREA-AVERAGED Fp(INCH/HR) = 0.40 AREA-AVERAGED Ap = 0.42
TOTAL AREA(ACRES) = 1.1 PEAK FLOW RATE(CFS) = 3.05

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.39 HALFSTREET FLOOD WIDTH(FEET) = 12.77
FLOW VELOCITY(FEET/SEC.) = 1.85 DEPTH*VELOCITY(FT*FT/SEC.) = 0.72
LONGEST FLOWPATH FROM NODE 5.01 TO NODE 5.05 = 526.55 FEET.

*****
FLOW PROCESS FROM NODE 5.05 TO NODE 4.09 IS CODE = 1
-----
>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 10.36
RAINFALL INTENSITY(INCH/HR) = 3.19
AREA-AVERAGED Fm(INCH/HR) = 0.17

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AREA-AVERAGED F_p (INCH/HR) = 0.40
 AREA-AVERAGED A_p = 0.42
 EFFECTIVE STREAM AREA(ACRES) = 1.12
 TOTAL STREAM AREA(ACRES) = 1.12
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 3.05

** CONFLUENCE DATA **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	$F_p(F_m)$ (INCH/HR)	A_p	A_e (ACRES)	HEADWATER NODE
1	5.88	11.49	3.013	0.40(0.18)	0.46	2.3	4.01
2	3.05	10.36	3.193	0.40(0.17)	0.42	1.1	5.01

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	$F_p(F_m)$ (INCH/HR)	A_p	A_e (ACRES)	HEADWATER NODE
1	8.70	10.36	3.193	0.40(0.18)	0.44	3.2	5.01
2	8.75	11.49	3.013	0.40(0.18)	0.45	3.4	4.01

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 8.75 Tc(MIN.) = 11.49
 EFFECTIVE AREA(ACRES) = 3.43 AREA-AVERAGED F_m (INCH/HR) = 0.18
 AREA-AVERAGED F_p (INCH/HR) = 0.40 AREA-AVERAGED A_p = 0.45
 TOTAL AREA(ACRES) = 3.4
 LONGEST FLOWPATH FROM NODE 4.01 TO NODE 4.09 = 1149.15 FEET.

END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 3.4 TC(MIN.) = 11.49
 EFFECTIVE AREA(ACRES) = 3.43 AREA-AVERAGED F_m (INCH/HR) = 0.18
 AREA-AVERAGED F_p (INCH/HR) = 0.40 AREA-AVERAGED A_p = 0.445
 PEAK FLOW RATE(CFS) = 8.75

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	$F_p(F_m)$ (INCH/HR)	A_p	A_e (ACRES)	HEADWATER NODE
1	8.70	10.36	3.193	0.40(0.18)	0.44	3.2	5.01
2	8.75	11.49	3.013	0.40(0.18)	0.45	3.4	4.01

END OF RATIONAL METHOD ANALYSIS

Rational Method – 25-Year Storm Event: Proposed Condition

 RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE
 (Reference: 1986 ORANGE COUNTY HYDROLOGY CRITERION)
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 Ver. 23.0 Release Date: 07/01/2016 License ID 1535

Analysis prepared by:

Stantec

***** DESCRIPTION OF STUDY *****
 * Culver Alton - 25 Year Rational Method Study, Proposed Conditions *
 * DMA 1: North Intersection Streamline, Culver to Alton *
 * 11/20/2019 - ECS *

FILE NAME: 25DMA1P.DAT
 TIME/DATE OF STUDY: 11:32 11/20/2019

=====

USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:

=====

--*TIME-OF-CONCENTRATION MODEL*--

USER SPECIFIED STORM EVENT(YEAR) = 25.00
 SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00
 SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.95
 DATA BANK RAINFALL USED
 ANTECEDENT MOISTURE CONDITION (AMC) II ASSUMED FOR RATIONAL METHOD

USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL

NO.	HALF- WIDTH	CROWN TO CROSSFALL	STREET-CROSSFALL: IN- / OUT-/PARK- SIDE / SIDE/ WAY	CURB HEIGHT	GUTTER-GEOMETRIES: WIDTH LIP HIKE	MANNING FACTOR
	(FT)	(FT)		(FT)	(FT) (FT) (FT)	(n)
1	30.0	20.0	0.018/0.018/0.020	0.67	2.00 0.0312 0.167	0.0150
2	40.0	30.0	0.018/0.018/0.020	0.67	2.00 0.0312 0.167	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:
 1. Relative Flow-Depth = 0.00 FEET
 as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
 2. (Depth)*(Velocity) Constraint = 6.0 (FT*FT/S)
 *SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
 OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*
 *USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

FLOW PROCESS FROM NODE 1.01 TO NODE 1.03 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
 >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 330.00
 ELEVATION DATA: UPSTREAM(FEET) = 75.00 DOWNSTREAM(FEET) = 73.00

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$
 SUBAREA ANALYSIS USED MINIMUM T_c (MIN.) = 8.586
 * 25 YEAR RAINFALL INTENSITY(INCH/HR) = 3.552
 SUBAREA T_c AND LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	F_p (INCH/HR)	A_p (DECIMAL)	SCS CN	T_c (MIN.)
COMMERCIAL	A	0.41	0.40	0.100	32	8.59
PUBLIC PARK	A	0.27	0.40	0.850	32	13.64

SUBAREA AVERAGE PERVIOUS LOSS RATE, F_p (INCH/HR) = 0.40
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, A_p = 0.398
 SUBAREA RUNOFF(CFS) = 2.08
 TOTAL AREA(ACRES) = 0.68 PEAK FLOW RATE(CFS) = 2.08

FLOW PROCESS FROM NODE 1.03 TO NODE 1.05 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<

=====

UPSTREAM ELEVATION(FEET) = 73.00 DOWNSTREAM ELEVATION(FEET) = 68.00
STREET LENGTH(FEET) = 355.96 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curb-to-curb) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.55
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.36
HALFSTREET FLOOD WIDTH(FEET) = 11.13
AVERAGE FLOW VELOCITY(FT/SEC.) = 2.73
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.99
STREET FLOW TRAVEL TIME(MIN.) = 2.17 Tc(MIN.) = 10.76
* 25 YEAR RAINFALL INTENSITY (INCH/HR) = 3.127

SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	B	0.12	0.30	0.100	56
COMMERCIAL	A	0.52	0.40	0.100	32
PUBLIC PARK	B	0.20	0.30	0.850	56
PUBLIC PARK	A	0.26	0.40	0.850	32

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.36
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.414
SUBAREA AREA(ACRES) = 1.10 SUBAREA RUNOFF(CFS) = 2.95
EFFECTIVE AREA(ACRES) = 1.78 AREA-AVERAGED Fm(INCH/HR) = 0.15
AREA-AVERAGED Fp(INCH/HR) = 0.37 AREA-AVERAGED Ap = 0.41
TOTAL AREA(ACRES) = 1.8 PEAK FLOW RATE(CFS) = 4.76

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.39 HALFSTREET FLOOD WIDTH(FEET) = 12.70
FLOW VELOCITY(FT/SEC.) = 2.92 DEPTH*VELOCITY(FT*FT/SEC.) = 1.14
LONGEST FLOWPATH FROM NODE 1.01 TO NODE 1.05 = 685.96 FEET.

FLOW PROCESS FROM NODE 1.05 TO NODE 1.07 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<

=====

UPSTREAM ELEVATION(FEET) = 68.00 DOWNSTREAM ELEVATION(FEET) = 65.50
STREET LENGTH(FEET) = 162.78 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curb-to-curb) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 5.37
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.40
HALFSTREET FLOOD WIDTH(FEET) = 13.09
AVERAGE FLOW VELOCITY(FT/SEC.) = 3.11
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 1.23
STREET FLOW TRAVEL TIME(MIN.) = 0.87 Tc(MIN.) = 11.63
* 25 YEAR RAINFALL INTENSITY (INCH/HR) = 2.992

SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	B	0.14	0.30	0.100	56

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COMMERCIAL	A	0.13	0.40	0.100	32
PUBLIC PARK	B	0.10	0.30	0.850	56
PUBLIC PARK	A	0.10	0.40	0.850	32

SUBAREA AVERAGE PERVIOUS LOSS RATE, F_p (INCH/HR) = 0.35
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, A_p = 0.419
 SUBAREA AREA(ACRES) = 0.47 SUBAREA RUNOFF(CFS) = 1.20
 EFFECTIVE AREA(ACRES) = 2.25 AREA-AVERAGED F_m (INCH/HR) = 0.15
 AREA-AVERAGED F_p (INCH/HR) = 0.37 AREA-AVERAGED A_p = 0.41
 TOTAL AREA(ACRES) = 2.2 PEAK FLOW RATE(CFS) = 5.75

END OF SUBAREA STREET FLOW HYDRAULICS:
 DEPTH(FEET) = 0.40 HALFSTREET FLOOD WIDTH(FEET) = 13.48
 FLOW VELOCITY(FEET/SEC.) = 3.17 DEPTH*VELOCITY(FT*FT/SEC.) = 1.28
 LONGEST FLOWPATH FROM NODE 1.01 TO NODE 1.07 = 848.74 FEET.

=====

END OF STUDY SUMMARY:

TOTAL AREA(ACRES)	=	2.2	TC(MIN.)	=	11.63
EFFECTIVE AREA(ACRES)	=	2.25	AREA-AVERAGED F_m (INCH/HR)	=	0.15
AREA-AVERAGED F_p (INCH/HR)	=	0.37	AREA-AVERAGED A_p	=	0.410
PEAK FLOW RATE(CFS)	=	5.75			

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END OF RATIONAL METHOD ANALYSIS

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Analysis prepared by:

Stantec

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***** DESCRIPTION OF STUDY *****
* Culver Alton - 25 Year Rational Method Study, Proposed Conditions *
* DMA 2: West Intersection Streamline, Alton *
* 11/20/2019 - ECS *
*****
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FILE NAME: 25DMA2P.DAT
TIME/DATE OF STUDY: 11:35 11/20/2019

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=====
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:
=====
--*TIME-OF-CONCENTRATION MODEL*--
```

USER SPECIFIED STORM EVENT(YEAR) = 25.00
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.95
DATA BANK RAINFALL USED
ANTECEDENT MOISTURE CONDITION (AMC) II ASSUMED FOR RATIONAL METHOD

```
*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL*
      HALF- CROWN TO STREET-CROSSFALL: CURB GUTTER-GEOMETRIES: MANNING
      WIDTH CROSSFALL IN- / OUT-/PARK- HEIGHT WIDTH LIP HIKE FACTOR
NO. (FT) (FT) SIDE / SIDE/ WAY (FT) (FT) (FT) (FT) (n)
=== =====
1 30.0 20.0 0.018/0.018/0.020 0.67 2.00 0.0312 0.167 0.0150
2 40.0 30.0 0.018/0.018/0.020 0.67 2.00 0.0312 0.167 0.0150
```

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:
1. Relative Flow-Depth = 0.00 FEET
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)*(Velocity) Constraint = 6.0 (FT*FT/S)
*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*
*USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

```
*****
FLOW PROCESS FROM NODE 2.01 TO NODE 2.03 IS CODE = 21
*****
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>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<
=====
INITIAL SUBAREA FLOW-LENGTH(FEET) = 330.00
ELEVATION DATA: UPSTREAM(FEET) = 72.00 DOWNSTREAM(FEET) = 68.00
```

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$
SUBAREA ANALYSIS USED MINIMUM T_c (MIN.) = 7.474
* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 3.842
SUBAREA T_c AND LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	F_p (INCH/HR)	A_p (DECIMAL)	SCS CN	T_c (MIN.)
PUBLIC PARK	B	0.01	0.30	0.850	56	11.88
PUBLIC PARK	A	0.27	0.40	0.850	32	11.88
COMMERCIAL	B	0.07	0.30	0.100	56	7.47
COMMERCIAL	A	0.40	0.40	0.100	32	7.47

SUBAREA AVERAGE PERVIOUS LOSS RATE, F_p (INCH/HR) = 0.39
SUBAREA AVERAGE PERVIOUS AREA FRACTION, A_p = 0.380
SUBAREA RUNOFF(CFS) = 2.49
TOTAL AREA(ACRES) = 0.75 PEAK FLOW RATE(CFS) = 2.49

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Page 1
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                                25DMA2P.RES
FLOW PROCESS FROM NODE      2.03 TO NODE      2.05 IS CODE = 62
-----
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<
=====
UPSTREAM ELEVATION(FEET) = 68.00 DOWNSTREAM ELEVATION(FEET) = 62.00
STREET LENGTH(FEET) = 440.15 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.87
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.37
HALFSTREET FLOOD WIDTH(FEET) = 11.68
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.74
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 1.02
STREET FLOW TRAVEL TIME(MIN.) = 2.67 Tc(MIN.) = 10.15
* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 3.231
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/      SCS SOIL      AREA      Fp      Ap      SCS
LAND USE      GROUP      (ACRES)      (INCH/HR)      (DECIMAL)      CN
COMMERCIAL      B      0.22      0.30      0.100      56
COMMERCIAL      A      0.27      0.40      0.100      32
PUBLIC PARK      B      0.23      0.30      0.850      56
PUBLIC PARK      A      0.28      0.40      0.850      32
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.35
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.483
SUBAREA AREA(ACRES) = 1.00 SUBAREA RUNOFF(CFS) = 2.75
EFFECTIVE AREA(ACRES) = 1.75 AREA-AVERAGED Fm(INCH/HR) = 0.16
AREA-AVERAGED Fp(INCH/HR) = 0.37 AREA-AVERAGED Ap = 0.44
TOTAL AREA(ACRES) = 1.8 PEAK FLOW RATE(CFS) = 4.83

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.39 HALFSTREET FLOOD WIDTH(FEET) = 12.85
FLOW VELOCITY(FEET/SEC.) = 2.90 DEPTH*VELOCITY(FT*FT/SEC.) = 1.14
LONGEST FLOWPATH FROM NODE 2.01 TO NODE 2.05 = 770.15 FEET.
=====
END OF STUDY SUMMARY:
TOTAL AREA(ACRES) = 1.8 TC(MIN.) = 10.15
EFFECTIVE AREA(ACRES) = 1.75 AREA-AVERAGED Fm(INCH/HR) = 0.16
AREA-AVERAGED Fp(INCH/HR) = 0.37 AREA-AVERAGED Ap = 0.439
PEAK FLOW RATE(CFS) = 4.83
=====
END OF RATIONAL METHOD ANALYSIS

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Analysis prepared by:

Stantec

***** DESCRIPTION OF STUDY *****
 * Culver Alton - 25 Year Rational Method Study, Proposed Conditions *
 * DMA 3: South Intersection Streamline, Alton *
 * 11/07/2019 - ECS *

FILE NAME: 25DMA3P.DAT
 TIME/DATE OF STUDY: 17:03 11/07/2019

=====

USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:

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--*TIME-OF-CONCENTRATION MODEL*--

USER SPECIFIED STORM EVENT(YEAR) = 25.00
 SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00
 SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.95
 DATA BANK RAINFALL USED
 ANTECEDENT MOISTURE CONDITION (AMC) II ASSUMED FOR RATIONAL METHOD

USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL

NO.	HALF- WIDTH	CROWN TO CROSSFALL	STREET-CROSSFALL: IN- / OUT-/PARK- SIDE / SIDE/ WAY	CURB HEIGHT	GUTTER-GEOMETRIES: WIDTH LIP HIKE	MANNING FACTOR
	(FT)	(FT)		(FT)	(FT) (FT) (FT)	(n)
1	30.0	20.0	0.018/0.018/0.020	0.67	2.00 0.0312 0.167	0.0150
2	40.0	30.0	0.018/0.018/0.020	0.67	2.00 0.0312 0.167	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:
 1. Relative Flow-Depth = 0.00 FEET
 as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
 2. (Depth)*(Velocity) Constraint = 6.0 (FT*FT/S)
 *SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
 OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*
 *USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

FLOW PROCESS FROM NODE 3.01 TO NODE 3.03 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
 >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 308.42
 ELEVATION DATA: UPSTREAM(FEET) = 82.00 DOWNSTREAM(FEET) = 77.00

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$
 SUBAREA ANALYSIS USED MINIMUM T_c (MIN.) = 6.864
 * 25 YEAR RAINFALL INTENSITY(INCH/HR) = 4.032
 SUBAREA T_c AND LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	F_p (INCH/HR)	A_p (DECIMAL)	SCS CN	T_c (MIN.)
COMMERCIAL	A	0.26	0.40	0.100	32	6.86
PUBLIC PARK	A	0.22	0.40	0.850	32	10.91

SUBAREA AVERAGE PERVIOUS LOSS RATE, F_p (INCH/HR) = 0.40
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, A_p = 0.444
 SUBAREA RUNOFF(CFS) = 1.67
 TOTAL AREA(ACRES) = 0.48 PEAK FLOW RATE(CFS) = 1.67

FLOW PROCESS FROM NODE 3.03 TO NODE 3.05 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<

=====

UPSTREAM ELEVATION(FEET) = 77.00 DOWNSTREAM ELEVATION(FEET) = 72.00
STREET LENGTH(FEET) = 500.82 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.15
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.37
HALFSTREET FLOOD WIDTH(FEET) = 11.37
AVERAGE FLOW VELOCITY(FT/SEC.) = 2.34
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.85
STREET FLOW TRAVEL TIME(MIN.) = 3.57 Tc(MIN.) = 10.44
* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 3.181

SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	A	0.53	0.40	0.100	32
PUBLIC PARK	A	0.57	0.40	0.850	32

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.40
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.489
SUBAREA AREA(ACRES) = 1.10 SUBAREA RUNOFF(CFS) = 2.96
EFFECTIVE AREA(ACRES) = 1.58 AREA-AVERAGED Fm(INCH/HR) = 0.19
AREA-AVERAGED Fp(INCH/HR) = 0.40 AREA-AVERAGED Ap = 0.48
TOTAL AREA(ACRES) = 1.6 PEAK FLOW RATE(CFS) = 4.25

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.39 HALFSTREET FLOOD WIDTH(FEET) = 13.01
FLOW VELOCITY(FT/SEC.) = 2.49 DEPTH*VELOCITY(FT*FT/SEC.) = 0.99
LONGEST FLOWPATH FROM NODE 3.01 TO NODE 3.05 = 809.24 FEET.

FLOW PROCESS FROM NODE 3.05 TO NODE 3.05 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

=====

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 10.44
RAINFALL INTENSITY(INCH/HR) = 3.18
AREA-AVERAGED Fm(INCH/HR) = 0.19
AREA-AVERAGED Fp(INCH/HR) = 0.40
AREA-AVERAGED Ap = 0.48
EFFECTIVE STREAM AREA(ACRES) = 1.58
TOTAL STREAM AREA(ACRES) = 1.58
PEAK FLOW RATE(CFS) AT CONFLUENCE = 4.25

FLOW PROCESS FROM NODE 6.01 TO NODE 6.03 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 237.14
ELEVATION DATA: UPSTREAM(FEET) = 73.50 DOWNSTREAM(FEET) = 72.50

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 8.089
* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 3.674
SUBAREA Tc AND LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
PUBLIC PARK	D	0.06	0.20	0.850	75	12.85
COMMERCIAL	D	0.39	0.20	0.100	75	8.09

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                                25DMA3P.RES
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.200
SUBAREA RUNOFF(CFS) = 1.47
TOTAL AREA(ACRES) = 0.45 PEAK FLOW RATE(CFS) = 1.47

*****
FLOW PROCESS FROM NODE 6.03 TO NODE 3.05 IS CODE = 62
-----
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<
=====
UPSTREAM ELEVATION(FEET) = 72.50 DOWNSTREAM ELEVATION(FEET) = 72.00
STREET LENGTH(FEET) = 276.24 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curb) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.00
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.40
HALFSTREET FLOOD WIDTH(FEET) = 13.55
AVERAGE FLOW VELOCITY(FEET/SEC.) = 1.09
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.44
STREET FLOW TRAVEL TIME(MIN.) = 4.22 Tc(MIN.) = 12.31
* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 2.896
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
PUBLIC PARK A 0.01 0.40 0.850 32
COMMERCIAL A 0.27 0.40 0.100 32
COMMERCIAL B 0.09 0.30 0.100 56
PUBLIC PARK D 0.01 0.20 0.850 75
COMMERCIAL D 0.03 0.20 0.100 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.34
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.137
SUBAREA AREA(ACRES) = 0.41 SUBAREA RUNOFF(CFS) = 1.05
EFFECTIVE AREA(ACRES) = 0.86 AREA-AVERAGED Fm(INCH/HR) = 0.04
AREA-AVERAGED Fp(INCH/HR) = 0.25 AREA-AVERAGED Ap = 0.17
TOTAL AREA(ACRES) = 0.9 PEAK FLOW RATE(CFS) = 2.21

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.42 HALFSTREET FLOOD WIDTH(FEET) = 14.18
FLOW VELOCITY(FEET/SEC.) = 1.11 DEPTH*VELOCITY(FT*FT/SEC.) = 0.46
LONGEST FLOWPATH FROM NODE 6.01 TO NODE 3.05 = 513.38 FEET.

*****
FLOW PROCESS FROM NODE 6.03 TO NODE 3.05 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 12.31
RAINFALL INTENSITY(INCH/HR) = 2.90
AREA-AVERAGED Fm(INCH/HR) = 0.04
AREA-AVERAGED Fp(INCH/HR) = 0.25
AREA-AVERAGED Ap = 0.17
EFFECTIVE STREAM AREA(ACRES) = 0.86
TOTAL STREAM AREA(ACRES) = 0.86
PEAK FLOW RATE(CFS) AT CONFLUENCE = 2.21

** CONFLUENCE DATA **
STREAM Q Tc Intensity Fp(Fm) Ap Ae HEADWATER
NUMBER (CFS) (MIN.) (INCH/HR) (INCH/HR) (ACRES) NODE
1 4.25 10.44 3.181 0.40( 0.19) 0.48 1.6 3.01
2 2.21 12.31 2.896 0.25( 0.04) 0.17 0.9 6.01

```

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	6.31	10.44	3.181	0.38(0.14)	0.38	2.3	3.01
2	6.06	12.31	2.896	0.38(0.14)	0.37	2.4	6.01

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 6.31 Tc(MIN.) = 10.44
EFFECTIVE AREA(ACRES) = 2.31 AREA-AVERAGED Fm(INCH/HR) = 0.14
AREA-AVERAGED Fp(INCH/HR) = 0.38 AREA-AVERAGED Ap = 0.38
TOTAL AREA(ACRES) = 2.4
LONGEST FLOWPATH FROM NODE 3.01 TO NODE 3.05 = 809.24 FEET.

END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 2.4 TC(MIN.) = 10.44
EFFECTIVE AREA(ACRES) = 2.31 AREA-AVERAGED Fm(INCH/HR) = 0.14
AREA-AVERAGED Fp(INCH/HR) = 0.38 AREA-AVERAGED Ap = 0.379
PEAK FLOW RATE(CFS) = 6.31

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	6.31	10.44	3.181	0.38(0.14)	0.38	2.3	3.01
2	6.06	12.31	2.896	0.38(0.14)	0.37	2.4	6.01

END OF RATIONAL METHOD ANALYSIS

↑

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Analysis prepared by:

Stantec

***** DESCRIPTION OF STUDY *****
 * Culver Alton - 25 Year Rational Method Study, Proposed Conditions *
 * DMA 4: East Intersection Streamline, Yale to Alton to Culver *
 * 11/07/2019 - ECS *

FILE NAME: 25DMA4P.DAT
 TIME/DATE OF STUDY: 17:10 11/07/2019

=====

USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:

=====

--*TIME-OF-CONCENTRATION MODEL*--

USER SPECIFIED STORM EVENT(YEAR) = 25.00
 SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00
 SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.95
 DATA BANK RAINFALL USED
 ANTECEDENT MOISTURE CONDITION (AMC) II ASSUMED FOR RATIONAL METHOD

USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL

NO.	HALF- WIDTH (FT)	CROWN TO CROSSFALL (FT)	STREET-CROSSFALL: IN- / OUT-/PARK- SIDE / SIDE/ WAY	CURB HEIGHT (FT)	GUTTER-GEOMETRIES:			MANNING FACTOR (n)
					WIDTH (FT)	LIP (FT)	HIKE (FT)	
1	30.0	20.0	0.018/0.018/0.020	0.67	2.00	0.0312	0.167	0.0150
2	40.0	30.0	0.018/0.018/0.020	0.67	2.00	0.0312	0.167	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:
 1. Relative Flow-Depth = 0.00 FEET
 as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
 2. (Depth)*(Velocity) Constraint = 6.0 (FT*FT/S)
 *SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
 OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*
 *USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

FLOW PROCESS FROM NODE 4.01 TO NODE 4.03 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
 >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 116.02
 ELEVATION DATA: UPSTREAM(FEET) = 89.00 DOWNSTREAM(FEET) = 87.00

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$
 SUBAREA ANALYSIS USED MINIMUM T_c (MIN.) = 5.000
 * 25 YEAR RAINFALL INTENSITY(INCH/HR) = 4.824
 SUBAREA T_c AND LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	F_p (INCH/HR)	A_p (DECIMAL)	SCS CN	T_c (MIN.)
PUBLIC PARK	A	0.01	0.40	0.850	32	7.29
COMMERCIAL	A	0.13	0.40	0.100	32	5.00

SUBAREA AVERAGE PERVIOUS LOSS RATE, F_p (INCH/HR) = 0.40
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, A_p = 0.154
 SUBAREA RUNOFF(CFS) = 0.60
 TOTAL AREA(ACRES) = 0.14 PEAK FLOW RATE(CFS) = 0.60

FLOW PROCESS FROM NODE 4.03 TO NODE 4.05 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<

=====

UPSTREAM ELEVATION(FEET) = 87.00 DOWNSTREAM ELEVATION(FEET) = 80.00
STREET LENGTH(FEET) = 301.23 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.52
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.27
HALFSTREET FLOOD WIDTH(FEET) = 6.16
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.85
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.78
STREET FLOW TRAVEL TIME(MIN.) = 1.76 Tc(MIN.) = 6.76
* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 4.066
SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
PUBLIC PARK	A	0.07	0.40	0.850	32
COMMERCIAL	A	0.44	0.40	0.100	32

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.40
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.203
SUBAREA AREA(ACRES) = 0.51 SUBAREA RUNOFF(CFS) = 1.83
EFFECTIVE AREA(ACRES) = 0.65 AREA-AVERAGED Fm(INCH/HR) = 0.08
AREA-AVERAGED Fp(INCH/HR) = 0.40 AREA-AVERAGED Ap = 0.19
TOTAL AREA(ACRES) = 0.6 PEAK FLOW RATE(CFS) = 2.33

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.30 HALFSTREET FLOOD WIDTH(FEET) = 7.97
FLOW VELOCITY(FEET/SEC.) = 3.07 DEPTH*VELOCITY(FT*FT/SEC.) = 0.94
LONGEST FLOWPATH FROM NODE 4.01 TO NODE 4.05 = 417.25 FEET.

FLOW PROCESS FROM NODE 4.05 TO NODE 4.07 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<

=====

UPSTREAM ELEVATION(FEET) = 80.00 DOWNSTREAM ELEVATION(FEET) = 75.00
STREET LENGTH(FEET) = 369.87 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.63
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.37
HALFSTREET FLOOD WIDTH(FEET) = 11.37
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.70
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.99
STREET FLOW TRAVEL TIME(MIN.) = 2.29 Tc(MIN.) = 9.05
* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 3.448
SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	A	0.27	0.40	0.100	32
PUBLIC PARK	A	0.63	0.40	0.850	32

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.40

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SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.625
SUBAREA AREA(ACRES) = 0.90 SUBAREA RUNOFF(CFS) = 2.59
EFFECTIVE AREA(ACRES) = 1.55 AREA-AVERAGED Fm(INCH/HR) = 0.18
AREA-AVERAGED Fp(INCH/HR) = 0.40 AREA-AVERAGED Ap = 0.44
TOTAL AREA(ACRES) = 1.5 PEAK FLOW RATE(CFS) = 4.56

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.39 HALFSTREET FLOOD WIDTH(FEET) = 12.54
FLOW VELOCITY(FEET/SEC.) = 2.86 DEPTH*VELOCITY(FT*FT/SEC.) = 1.10
LONGEST FLOWPATH FROM NODE 4.01 TO NODE 4.07 = 787.12 FEET.

*****
FLOW PROCESS FROM NODE 4.07 TO NODE 4.09 IS CODE = 62
-----
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<
=====
UPSTREAM ELEVATION(FEET) = 75.00 DOWNSTREAM ELEVATION(FEET) = 72.00
STREET LENGTH(FEET) = 362.03 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 5.55
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.43
HALFSTREET FLOOD WIDTH(FEET) = 15.12
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.48
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 1.07
STREET FLOW TRAVEL TIME(MIN.) = 2.43 Tc(MIN.) = 11.48
* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 3.014
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
COMMERCIAL A 0.54 0.40 0.100 32
PUBLIC PARK A 0.22 0.40 0.850 32
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.40
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.317
SUBAREA AREA(ACRES) = 0.76 SUBAREA RUNOFF(CFS) = 1.97
EFFECTIVE AREA(ACRES) = 2.31 AREA-AVERAGED Fm(INCH/HR) = 0.16
AREA-AVERAGED Fp(INCH/HR) = 0.40 AREA-AVERAGED Ap = 0.40
TOTAL AREA(ACRES) = 2.3 PEAK FLOW RATE(CFS) = 5.93

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.44 HALFSTREET FLOOD WIDTH(FEET) = 15.59
FLOW VELOCITY(FEET/SEC.) = 2.51 DEPTH*VELOCITY(FT*FT/SEC.) = 1.11
LONGEST FLOWPATH FROM NODE 4.01 TO NODE 4.09 = 1149.15 FEET.

*****
FLOW PROCESS FROM NODE 4.09 TO NODE 4.09 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 11.48
RAINFALL INTENSITY(INCH/HR) = 3.01
AREA-AVERAGED Fm(INCH/HR) = 0.16
AREA-AVERAGED Fp(INCH/HR) = 0.40
AREA-AVERAGED Ap = 0.40
EFFECTIVE STREAM AREA(ACRES) = 2.31
TOTAL STREAM AREA(ACRES) = 2.31
PEAK FLOW RATE(CFS) AT CONFLUENCE = 5.93

*****
FLOW PROCESS FROM NODE 5.01 TO NODE 5.03 IS CODE = 21
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>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<
=====
INITIAL SUBAREA FLOW-LENGTH(FEET) = 253.47
ELEVATION DATA: UPSTREAM(FEET) = 75.00 DOWNSTREAM(FEET) = 73.50

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 7.763
* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 3.761
SUBAREA Tc AND LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/      SCS SOIL  AREA      Fp      Ap      SCS  Tc
LAND USE              GROUP  (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)
COMMERCIAL             A        0.24    0.40    0.100    32   7.76
PUBLIC PARK            A        0.24    0.40    0.850    32  12.33
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.40
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.475
SUBAREA RUNOFF(CFS) = 1.54
TOTAL AREA(ACRES) = 0.48 PEAK FLOW RATE(CFS) = 1.54

*****
FLOW PROCESS FROM NODE 5.03 TO NODE 5.05 IS CODE = 62
-----
>>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>(STREET TABLE SECTION # 1 USED)<<<<<
=====
UPSTREAM ELEVATION(FEET) = 73.50 DOWNSTREAM ELEVATION(FEET) = 72.00
STREET LENGTH(FEET) = 273.08 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.44
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.37
HALFSTREET FLOOD WIDTH(FEET) = 11.60
AVERAGE FLOW VELOCITY(FEET/SEC.) = 1.75
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.65
STREET FLOW TRAVEL TIME(MIN.) = 2.60 Tc(MIN.) = 10.36
* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 3.193
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/      SCS SOIL  AREA      Fp      Ap      SCS
LAND USE              GROUP  (ACRES) (INCH/HR) (DECIMAL) CN
COMMERCIAL             A        0.57    0.40    0.100    32
PUBLIC PARK            A        0.07    0.40    0.850    32
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.40
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.182
SUBAREA AREA(ACRES) = 0.64 SUBAREA RUNOFF(CFS) = 1.80
EFFECTIVE AREA(ACRES) = 1.12 AREA-AVERAGED Fm(INCH/HR) = 0.12
AREA-AVERAGED Fp(INCH/HR) = 0.40 AREA-AVERAGED Ap = 0.31
TOTAL AREA(ACRES) = 1.1 PEAK FLOW RATE(CFS) = 3.09

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.39 HALFSTREET FLOOD WIDTH(FEET) = 12.93
FLOW VELOCITY(FEET/SEC.) = 1.83 DEPTH*VELOCITY(FT*FT/SEC.) = 0.72
LONGEST FLOWPATH FROM NODE 5.01 TO NODE 5.05 = 526.55 FEET.

*****
FLOW PROCESS FROM NODE 5.05 TO NODE 4.09 IS CODE = 1
-----
>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 10.36
RAINFALL INTENSITY(INCH/HR) = 3.19
AREA-AVERAGED Fm(INCH/HR) = 0.12

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AREA-AVERAGED F_p (INCH/HR) = 0.40
 AREA-AVERAGED A_p = 0.31
 EFFECTIVE STREAM AREA(ACRES) = 1.12
 TOTAL STREAM AREA(ACRES) = 1.12
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 3.09

** CONFLUENCE DATA **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	$F_p(F_m)$ (INCH/HR)	A_p	A_e (ACRES)	HEADWATER NODE
1	5.93	11.48	3.014	0.40(0.16)	0.40	2.3	4.01
2	3.09	10.36	3.193	0.40(0.12)	0.31	1.1	5.01

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	$F_p(F_m)$ (INCH/HR)	A_p	A_e (ACRES)	HEADWATER NODE
1	8.79	10.36	3.193	0.40(0.15)	0.37	3.2	5.01
2	8.85	11.48	3.014	0.40(0.15)	0.37	3.4	4.01

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 8.85 Tc(MIN.) = 11.48
 EFFECTIVE AREA(ACRES) = 3.43 AREA-AVERAGED F_m (INCH/HR) = 0.15
 AREA-AVERAGED F_p (INCH/HR) = 0.40 AREA-AVERAGED A_p = 0.37
 TOTAL AREA(ACRES) = 3.4
 LONGEST FLOWPATH FROM NODE 4.01 TO NODE 4.09 = 1149.15 FEET.

END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 3.4 TC(MIN.) = 11.48
 EFFECTIVE AREA(ACRES) = 3.43 AREA-AVERAGED F_m (INCH/HR) = 0.15
 AREA-AVERAGED F_p (INCH/HR) = 0.40 AREA-AVERAGED A_p = 0.371
 PEAK FLOW RATE(CFS) = 8.85

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	$F_p(F_m)$ (INCH/HR)	A_p	A_e (ACRES)	HEADWATER NODE
1	8.79	10.36	3.193	0.40(0.15)	0.37	3.2	5.01
2	8.85	11.48	3.014	0.40(0.15)	0.37	3.4	4.01

END OF RATIONAL METHOD ANALYSIS

Rational Method – 100-Year Storm Event: Existing Condition

 RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE
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Analysis prepared by:

Stantec

***** DESCRIPTION OF STUDY *****
 * Culver Alton - 100 Year Rational Method Study, Existing Conditions *
 * DMA 1: North Intersection Streamline, Culver to Alton *
 * 10/25/2019 - ECS *

FILE NAME: 100DMA1.DAT
 TIME/DATE OF STUDY: 14:16 10/25/2019

=====

USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:

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--*TIME-OF-CONCENTRATION MODEL*--

USER SPECIFIED STORM EVENT(YEAR) = 100.00
 SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00
 SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.95
 DATA BANK RAINFALL USED
 ANTECEDENT MOISTURE CONDITION (AMC) III ASSUMED FOR RATIONAL METHOD

USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL

NO.	HALF- WIDTH	CROWN TO CROSSFALL	STREET-CROSSFALL: IN- / OUT-/PARK- SIDE / SIDE/ WAY	CURB HEIGHT (FT)	GUTTER-GEOMETRIES: WIDTH LIP HIKE (FT) (FT) (FT)	MANNING FACTOR (n)
	(FT)	(FT)				
1	30.0	20.0	0.018/0.018/0.020	0.67	2.00 0.0312 0.167	0.0150
2	40.0	30.0	0.018/0.018/0.020	0.67	2.00 0.0312 0.167	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:
 1. Relative Flow-Depth = 0.00 FEET
 as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
 2. (Depth)*(Velocity) Constraint = 6.0 (FT*FT/S)
 *SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
 OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*
 *USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

FLOW PROCESS FROM NODE 1.01 TO NODE 1.03 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
 >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 330.00
 ELEVATION DATA: UPSTREAM(FEET) = 75.00 DOWNSTREAM(FEET) = 73.00

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$
 SUBAREA ANALYSIS USED MINIMUM T_c (MIN.) = 8.586
 * 100 YEAR RAINFALL INTENSITY(INCH/HR) = 4.539
 SUBAREA T_c AND LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	F_p (INCH/HR)	A_p (DECIMAL)	SCS CN	T_c (MIN.)
COMMERCIAL	A	0.41	0.40	0.100	52	8.59
PUBLIC PARK	A	0.27	0.40	0.850	52	13.64

SUBAREA AVERAGE PERVIOUS LOSS RATE, F_p (INCH/HR) = 0.40
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, A_p = 0.398
 SUBAREA RUNOFF(CFS) = 2.68
 TOTAL AREA(ACRES) = 0.68 PEAK FLOW RATE(CFS) = 2.68

FLOW PROCESS FROM NODE 1.03 TO NODE 1.05 IS CODE = 62

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>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<

=====

UPSTREAM ELEVATION(FEET) = 73.00 DOWNSTREAM ELEVATION(FEET) = 68.00
STREET LENGTH(FEET) = 355.96 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 4.60
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.39
HALFSTREET FLOOD WIDTH(FEET) = 12.46
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.91
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 1.12
STREET FLOW TRAVEL TIME(MIN.) = 2.04 Tc(MIN.) = 10.62
* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 4.018

SUBAREA LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	B	0.12	0.30	0.100	76
COMMERCIAL	A	0.56	0.40	0.100	52
PUBLIC PARK	B	0.20	0.30	0.850	76
PUBLIC PARK	A	0.22	0.40	0.850	52

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.36
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.386
SUBAREA AREA(ACRES) = 1.10 SUBAREA RUNOFF(CFS) = 3.84
EFFECTIVE AREA(ACRES) = 1.78 AREA-AVERAGED Fm(INCH/HR) = 0.15
AREA-AVERAGED Fp(INCH/HR) = 0.37 AREA-AVERAGED Ap = 0.39
TOTAL AREA(ACRES) = 1.8 PEAK FLOW RATE(CFS) = 6.20

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.42 HALFSTREET FLOOD WIDTH(FEET) = 14.18
FLOW VELOCITY(FEET/SEC.) = 3.12 DEPTH*VELOCITY(FT*FT/SEC.) = 1.30
LONGEST FLOWPATH FROM NODE 1.01 TO NODE 1.05 = 685.96 FEET.

FLOW PROCESS FROM NODE 1.05 TO NODE 1.07 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<

=====

UPSTREAM ELEVATION(FEET) = 68.00 DOWNSTREAM ELEVATION(FEET) = 65.50
STREET LENGTH(FEET) = 162.78 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 6.99
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.42
HALFSTREET FLOOD WIDTH(FEET) = 14.65
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.31
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 1.40
STREET FLOW TRAVEL TIME(MIN.) = 0.82 Tc(MIN.) = 11.44
* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 3.850

SUBAREA LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	B	0.14	0.30	0.100	76

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COMMERCIAL	A	0.13	0.40	0.100	52
PUBLIC PARK	B	0.10	0.30	0.850	76
PUBLIC PARK	A	0.10	0.40	0.850	52

SUBAREA AVERAGE PERVIOUS LOSS RATE, F_p (INCH/HR) = 0.35
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, A_p = 0.419
 SUBAREA AREA(ACRES) = 0.47 SUBAREA RUNOFF(CFS) = 1.57
 EFFECTIVE AREA(ACRES) = 2.25 AREA-AVERAGED F_m (INCH/HR) = 0.15
 AREA-AVERAGED F_p (INCH/HR) = 0.37 AREA-AVERAGED A_p = 0.40
 TOTAL AREA(ACRES) = 2.2 PEAK FLOW RATE(CFS) = 7.50

END OF SUBAREA STREET FLOW HYDRAULICS:
 DEPTH(FEET) = 0.43 HALFSTREET FLOOD WIDTH(FEET) = 15.12
 FLOW VELOCITY(FEET/SEC.) = 3.36 DEPTH*VELOCITY(FT*FT/SEC.) = 1.45
 LONGEST FLOWPATH FROM NODE 1.01 TO NODE 1.07 = 848.74 FEET.

=====

END OF STUDY SUMMARY:
 TOTAL AREA(ACRES) = 2.2 TC(MIN.) = 11.44
 EFFECTIVE AREA(ACRES) = 2.25 AREA-AVERAGED F_m (INCH/HR) = 0.15
 AREA-AVERAGED F_p (INCH/HR) = 0.37 AREA-AVERAGED A_p = 0.397
 PEAK FLOW RATE(CFS) = 7.50

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END OF RATIONAL METHOD ANALYSIS

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RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE
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Ver. 23.0 Release Date: 07/01/2016 License ID 1535

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Analysis prepared by:

Stantec

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***** DESCRIPTION OF STUDY *****
* Culver Alton - 100 Year Rational Method Study, Existing Conditions *
* DMA 2: West Intersection Streamline, Alton *
* 10/25/2019 - ECS *
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FILE NAME: 100DMA2.DAT
TIME/DATE OF STUDY: 13:44 10/25/2019

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USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:
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--*TIME-OF-CONCENTRATION MODEL*--

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USER SPECIFIED STORM EVENT(YEAR) = 100.00
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.95
DATA BANK RAINFALL USED
ANTECEDENT MOISTURE CONDITION (AMC) III ASSUMED FOR RATIONAL METHOD

USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL									
NO.	HALF- WIDTH	CROWN TO CROSSFALL	STREET-CROSSFALL: IN- / OUT-/PARK- SIDE / SIDE/ WAY	CURB HEIGHT	GUTTER-GEOMETRIES: WIDTH LIP HIKE	MANNING			
	(FT)	(FT)		(FT)	(FT) (FT) (FT)	FACTOR			
	(FT)	(FT)		(FT)	(FT) (FT) (FT)	(n)			
1	30.0	20.0	0.018/0.018/0.020	0.67	2.00 0.0312 0.167	0.0150			
2	40.0	30.0	0.018/0.018/0.020	0.67	2.00 0.0312 0.167	0.0150			

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:
1. Relative Flow-Depth = 0.00 FEET
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)*(Velocity) Constraint = 6.0 (FT*FT/S)
*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*
*USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

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FLOW PROCESS FROM NODE      2.01 TO NODE      2.03 IS CODE = 21
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>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<
=====
INITIAL SUBAREA FLOW-LENGTH(FEET) = 330.00
ELEVATION DATA: UPSTREAM(FEET) = 72.00 DOWNSTREAM(FEET) = 68.00

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Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 7.474
* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 4.914
SUBAREA Tc AND LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
PUBLIC PARK	B	0.01	0.30	0.850	76	11.88
PUBLIC PARK	A	0.27	0.40	0.850	52	11.88
COMMERCIAL	B	0.07	0.30	0.100	76	7.47
COMMERCIAL	A	0.40	0.40	0.100	52	7.47

SUBAREA AVERAGE PVIOUS LOSS RATE, Fp(INCH/HR) = 0.39
SUBAREA AVERAGE PVIOUS AREA FRACTION, Ap = 0.380
SUBAREA RUNOFF(CFS) = 3.22
TOTAL AREA(ACRES) = 0.75 PEAK FLOW RATE(CFS) = 3.22

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                                100DMA2E.RES
FLOW PROCESS FROM NODE      2.03 TO NODE      2.05 IS CODE = 62
-----
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<
=====
UPSTREAM ELEVATION(FEET) = 68.00 DOWNSTREAM ELEVATION(FEET) = 62.00
STREET LENGTH(FEET) = 440.15 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 5.02
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.40
HALFSTREET FLOOD WIDTH(FEET) = 13.09
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.91
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 1.15
STREET FLOW TRAVEL TIME(MIN.) = 2.52 Tc(MIN.) = 9.99
* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 4.161
SUBAREA LOSS RATE DATA(AMC III):
DEVELOPMENT TYPE/      SCS SOIL      AREA      Fp      Ap      SCS
LAND USE      GROUP      (ACRES)      (INCH/HR)      (DECIMAL)      CN
COMMERCIAL      B      0.22      0.30      0.100      76
COMMERCIAL      A      0.27      0.40      0.100      52
PUBLIC PARK      B      0.23      0.30      0.850      76
PUBLIC PARK      A      0.28      0.40      0.850      52
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.35
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.483
SUBAREA AREA(ACRES) = 1.00 SUBAREA RUNOFF(CFS) = 3.59
EFFECTIVE AREA(ACRES) = 1.75 AREA-AVERAGED Fm(INCH/HR) = 0.16
AREA-AVERAGED Fp(INCH/HR) = 0.37 AREA-AVERAGED Ap = 0.44
TOTAL AREA(ACRES) = 1.8 PEAK FLOW RATE(CFS) = 6.30

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.42 HALFSTREET FLOOD WIDTH(FEET) = 14.41
FLOW VELOCITY(FEET/SEC.) = 3.07 DEPTH*VELOCITY(FT*FT/SEC.) = 1.29
LONGEST FLOWPATH FROM NODE 2.01 TO NODE 2.05 = 770.15 FEET.
=====
END OF STUDY SUMMARY:
TOTAL AREA(ACRES) = 1.8 TC(MIN.) = 9.99
EFFECTIVE AREA(ACRES) = 1.75 AREA-AVERAGED Fm(INCH/HR) = 0.16
AREA-AVERAGED Fp(INCH/HR) = 0.37 AREA-AVERAGED Ap = 0.439
PEAK FLOW RATE(CFS) = 6.30
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END OF RATIONAL METHOD ANALYSIS

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Analysis prepared by:

Stantec

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***** DESCRIPTION OF STUDY *****
* Culver Alton - 100 Year Rational Method Study, Existing Conditions *
* DMA 3: South Intersection Streamline, Alton *
* 11/07/2019 - ECS *
*****

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FILE NAME: 100DMA3.DAT
TIME/DATE OF STUDY: 12:42 11/07/2019

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USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:

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--*TIME-OF-CONCENTRATION MODEL*--

USER SPECIFIED STORM EVENT(YEAR) = 100.00
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.95
DATA BANK RAINFALL USED
ANTECEDENT MOISTURE CONDITION (AMC) III ASSUMED FOR RATIONAL METHOD

USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL

NO.	HALF-CROWN TO		STREET-CROSSFALL:		CURB HEIGHT (FT)	GUTTER-GEOMETRIES:			MANNING FACTOR (n)
	WIDTH (FT)	CROSSFALL (FT)	IN- / SIDE	OUT- / SIDE		WIDTH (FT)	LIP (FT)	HIKE (FT)	
1	30.0	20.0	0.018/0.018	0.020	0.67	2.00	0.0312	0.167	0.0150
2	40.0	30.0	0.018/0.018	0.020	0.67	2.00	0.0312	0.167	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:
1. Relative Flow-Depth = 0.00 FEET
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)*(Velocity) Constraint = 6.0 (FT*FT/S)
*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*
*USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

FLOW PROCESS FROM NODE 3.01 TO NODE 3.03 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 308.42
ELEVATION DATA: UPSTREAM(FEET) = 82.00 DOWNSTREAM(FEET) = 77.00

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$
SUBAREA ANALYSIS USED MINIMUM T_c (MIN.) = 6.864
* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 5.160
SUBAREA T_c AND LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	F_p (INCH/HR)	A_p (DECIMAL)	SCS CN	T_c (MIN.)
COMMERCIAL	A	0.26	0.40	0.100	52	6.86
PUBLIC PARK	A	0.22	0.40	0.850	52	10.91

SUBAREA AVERAGE PERVIOUS LOSS RATE, F_p (INCH/HR) = 0.40
SUBAREA AVERAGE PERVIOUS AREA FRACTION, A_p = 0.444
SUBAREA RUNOFF(CFS) = 2.15
TOTAL AREA(ACRES) = 0.48 PEAK FLOW RATE(CFS) = 2.15

FLOW PROCESS FROM NODE 3.03 TO NODE 3.05 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<

=====

UPSTREAM ELEVATION(FEET) = 77.00 DOWNSTREAM ELEVATION(FEET) = 72.00
STREET LENGTH(FEET) = 500.82 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 4.10
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.39
HALFSTREET FLOOD WIDTH(FEET) = 12.77
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.48
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.97
STREET FLOW TRAVEL TIME(MIN.) = 3.36 Tc(MIN.) = 10.23
* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 4.106

SUBAREA LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	A	0.53	0.40	0.100	52
PUBLIC PARK	A	0.57	0.40	0.850	52

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.40
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.489
SUBAREA AREA(ACRES) = 1.10 SUBAREA RUNOFF(CFS) = 3.87
EFFECTIVE AREA(ACRES) = 1.58 AREA-AVERAGED Fm(INCH/HR) = 0.19
AREA-AVERAGED Fp(INCH/HR) = 0.40 AREA-AVERAGED Ap = 0.48
TOTAL AREA(ACRES) = 1.6 PEAK FLOW RATE(CFS) = 5.57

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.42 HALFSTREET FLOOD WIDTH(FEET) = 14.57
FLOW VELOCITY(FEET/SEC.) = 2.67 DEPTH*VELOCITY(FT*FT/SEC.) = 1.13
LONGEST FLOWPATH FROM NODE 3.01 TO NODE 3.05 = 809.24 FEET.

FLOW PROCESS FROM NODE 3.05 TO NODE 3.05 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

=====

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 10.23
RAINFALL INTENSITY(INCH/HR) = 4.11
AREA-AVERAGED Fm(INCH/HR) = 0.19
AREA-AVERAGED Fp(INCH/HR) = 0.40
AREA-AVERAGED Ap = 0.48
EFFECTIVE STREAM AREA(ACRES) = 1.58
TOTAL STREAM AREA(ACRES) = 1.58
PEAK FLOW RATE(CFS) AT CONFLUENCE = 5.57

FLOW PROCESS FROM NODE 6.01 TO NODE 6.03 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 237.14
ELEVATION DATA: UPSTREAM(FEET) = 73.50 DOWNSTREAM(FEET) = 72.50

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 8.089
* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 4.697
SUBAREA Tc AND LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
PUBLIC PARK	D	0.07	0.20	0.850	91	12.85
COMMERCIAL	D	0.38	0.20	0.100	91	8.09

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                                100DMA3E.RES
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.217
SUBAREA RUNOFF(CFS) = 1.88
TOTAL AREA(ACRES) = 0.45 PEAK FLOW RATE(CFS) = 1.88

*****
FLOW PROCESS FROM NODE 6.03 TO NODE 3.05 IS CODE = 62
-----
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<
=====
UPSTREAM ELEVATION(FEET) = 72.50 DOWNSTREAM ELEVATION(FEET) = 72.00
STREET LENGTH(FEET) = 276.24 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curb) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.56
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.43
HALFSTREET FLOOD WIDTH(FEET) = 15.04
AVERAGE FLOW VELOCITY(FEET/SEC.) = 1.16
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.50
STREET FLOW TRAVEL TIME(MIN.) = 3.98 Tc(MIN.) = 12.06
* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 3.735
SUBAREA LOSS RATE DATA(AMC III):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
PUBLIC PARK A 0.03 0.40 0.850 52
COMMERCIAL A 0.25 0.40 0.100 52
COMMERCIAL B 0.09 0.30 0.100 76
PUBLIC PARK D 0.02 0.20 0.850 91
COMMERCIAL D 0.02 0.20 0.100 91
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.34
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.191
SUBAREA AREA(ACRES) = 0.41 SUBAREA RUNOFF(CFS) = 1.35
EFFECTIVE AREA(ACRES) = 0.86 AREA-AVERAGED Fm(INCH/HR) = 0.05
AREA-AVERAGED Fp(INCH/HR) = 0.26 AREA-AVERAGED Ap = 0.20
TOTAL AREA(ACRES) = 0.9 PEAK FLOW RATE(CFS) = 2.85

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.44 HALFSTREET FLOOD WIDTH(FEET) = 15.74
FLOW VELOCITY(FEET/SEC.) = 1.18 DEPTH*VELOCITY(FT*FT/SEC.) = 0.53
LONGEST FLOWPATH FROM NODE 6.01 TO NODE 3.05 = 513.38 FEET.

*****
FLOW PROCESS FROM NODE 6.03 TO NODE 3.05 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 12.06
RAINFALL INTENSITY(INCH/HR) = 3.74
AREA-AVERAGED Fm(INCH/HR) = 0.05
AREA-AVERAGED Fp(INCH/HR) = 0.26
AREA-AVERAGED Ap = 0.20
EFFECTIVE STREAM AREA(ACRES) = 0.86
TOTAL STREAM AREA(ACRES) = 0.86
PEAK FLOW RATE(CFS) AT CONFLUENCE = 2.85

** CONFLUENCE DATA **
STREAM Q Tc Intensity Fp(Fm) Ap Ae HEADWATER
NUMBER (CFS) (MIN.) (INCH/HR) (INCH/HR) (DECIMAL) (ACRES) NODE
1 5.57 10.23 4.106 0.40( 0.19) 0.48 1.6 3.01
2 2.85 12.06 3.735 0.26( 0.05) 0.20 0.9 6.01

```

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	8.23	10.23	4.106	0.38(0.15)	0.39	2.3	3.01
2	7.89	12.06	3.735	0.37(0.14)	0.38	2.4	6.01

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 8.23 Tc(MIN.) = 10.23
EFFECTIVE AREA(ACRES) = 2.31 AREA-AVERAGED Fm(INCH/HR) = 0.15
AREA-AVERAGED Fp(INCH/HR) = 0.38 AREA-AVERAGED Ap = 0.39
TOTAL AREA(ACRES) = 2.4
LONGEST FLOWPATH FROM NODE 3.01 TO NODE 3.05 = 809.24 FEET.

=====

END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 2.4 TC(MIN.) = 10.23
EFFECTIVE AREA(ACRES) = 2.31 AREA-AVERAGED Fm(INCH/HR) = 0.15
AREA-AVERAGED Fp(INCH/HR) = 0.38 AREA-AVERAGED Ap = 0.390
PEAK FLOW RATE(CFS) = 8.23

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	8.23	10.23	4.106	0.38(0.15)	0.39	2.3	3.01
2	7.89	12.06	3.735	0.37(0.14)	0.38	2.4	6.01

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END OF RATIONAL METHOD ANALYSIS

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RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE
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*****
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Analysis prepared by:

Stantec

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***** DESCRIPTION OF STUDY *****
* Culver Alton - 100 Year Rational Method Study, Existing Conditions *
* DMA 4: East Intersection Streamline, Yale to Alton to Culver *
* 11/07/2019 - ECS *
*****
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FILE NAME: 100DMA4E.DAT
TIME/DATE OF STUDY: 15:10 11/07/2019

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=====
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:
=====
--*TIME-OF-CONCENTRATION MODEL*--
```

USER SPECIFIED STORM EVENT(YEAR) = 100.00
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.95
DATA BANK RAINFALL USED
ANTECEDENT MOISTURE CONDITION (AMC) III ASSUMED FOR RATIONAL METHOD

```
*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL*
      HALF- CROWN TO STREET-CROSSFALL: CURB GUTTER-GEOMETRIES: MANNING
      WIDTH CROSSFALL IN- / OUT-/PARK- HEIGHT WIDTH LIP HIKE FACTOR
NO. (FT) (FT) SIDE / SIDE/ WAY (FT) (FT) (FT) (FT) (n)
=== =====
1 30.0 20.0 0.018/0.018/0.020 0.67 2.00 0.0312 0.167 0.0150
2 40.0 30.0 0.018/0.018/0.020 0.67 2.00 0.0312 0.167 0.0150
```

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:
1. Relative Flow-Depth = 0.00 FEET
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)*(Velocity) Constraint = 6.0 (FT*FT/S)
*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*
*USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

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*****
FLOW PROCESS FROM NODE 4.01 TO NODE 4.03 IS CODE = 21
-----
>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<
=====
INITIAL SUBAREA FLOW-LENGTH(FEET) = 116.02
ELEVATION DATA: UPSTREAM(FEET) = 89.00 DOWNSTREAM(FEET) = 87.00
```

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$
SUBAREA ANALYSIS USED MINIMUM T_c (MIN.) = 5.000
* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 6.187
SUBAREA T_c AND LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	F_p (INCH/HR)	A_p (DECIMAL)	SCS CN	T_c (MIN.)
PUBLIC PARK	A	0.01	0.40	0.850	52	7.29
COMMERCIAL	A	0.13	0.40	0.100	52	5.00

SUBAREA AVERAGE PERVIOUS LOSS RATE, F_p (INCH/HR) = 0.40
SUBAREA AVERAGE PERVIOUS AREA FRACTION, A_p = 0.154
SUBAREA RUNOFF(CFS) = 0.77
TOTAL AREA(ACRES) = 0.14 PEAK FLOW RATE(CFS) = 0.77

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*****
FLOW PROCESS FROM NODE 4.03 TO NODE 4.05 IS CODE = 62
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>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<

=====

UPSTREAM ELEVATION(FEET) = 87.00 DOWNSTREAM ELEVATION(FEET) = 80.00
STREET LENGTH(FEET) = 301.23 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.96
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.29
HALFSTREET FLOOD WIDTH(FEET) = 7.22
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.97
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.87
STREET FLOW TRAVEL TIME(MIN.) = 1.69 Tc(MIN.) = 6.69
* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 5.237
SUBAREA LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
PUBLIC PARK	A	0.07	0.40	0.850	52
COMMERCIAL	A	0.44	0.40	0.100	52

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.40
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.203
SUBAREA AREA(ACRES) = 0.51 SUBAREA RUNOFF(CFS) = 2.37
EFFECTIVE AREA(ACRES) = 0.65 AREA-AVERAGED Fm(INCH/HR) = 0.08
AREA-AVERAGED Fp(INCH/HR) = 0.40 AREA-AVERAGED Ap = 0.19
TOTAL AREA(ACRES) = 0.6 PEAK FLOW RATE(CFS) = 3.02

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.32 HALFSTREET FLOOD WIDTH(FEET) = 9.09
FLOW VELOCITY(FEET/SEC.) = 3.24 DEPTH*VELOCITY(FT*FT/SEC.) = 1.05
LONGEST FLOWPATH FROM NODE 4.01 TO NODE 4.05 = 417.25 FEET.

FLOW PROCESS FROM NODE 4.05 TO NODE 4.07 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<

=====

UPSTREAM ELEVATION(FEET) = 80.00 DOWNSTREAM ELEVATION(FEET) = 75.00
STREET LENGTH(FEET) = 369.87 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 4.73
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.39
HALFSTREET FLOOD WIDTH(FEET) = 12.77
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.87
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 1.12
STREET FLOW TRAVEL TIME(MIN.) = 2.15 Tc(MIN.) = 8.84
* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 4.464
SUBAREA LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	A	0.27	0.40	0.100	52
PUBLIC PARK	A	0.63	0.40	0.850	52

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.40

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SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.625
SUBAREA AREA(ACRES) = 0.90 SUBAREA RUNOFF(CFS) = 3.41
EFFECTIVE AREA(ACRES) = 1.55 AREA-AVERAGED Fm(INCH/HR) = 0.18
AREA-AVERAGED Fp(INCH/HR) = 0.40 AREA-AVERAGED Ap = 0.44
TOTAL AREA(ACRES) = 1.5 PEAK FLOW RATE(CFS) = 5.98

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.41 HALFSTREET FLOOD WIDTH(FEET) = 14.10
FLOW VELOCITY(FEET/SEC.) = 3.04 DEPTH*VELOCITY(FT*FT/SEC.) = 1.26
LONGEST FLOWPATH FROM NODE 4.01 TO NODE 4.07 = 787.12 FEET.

*****
FLOW PROCESS FROM NODE 4.07 TO NODE 4.09 IS CODE = 62
-----
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<
=====
UPSTREAM ELEVATION(FEET) = 75.00 DOWNSTREAM ELEVATION(FEET) = 72.00
STREET LENGTH(FEET) = 362.03 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 7.25
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.46
HALFSTREET FLOOD WIDTH(FEET) = 16.91
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.64
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 1.23
STREET FLOW TRAVEL TIME(MIN.) = 2.29 Tc(MIN.) = 11.13
* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 3.912
SUBAREA LOSS RATE DATA(AMC III):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
COMMERCIAL A 0.37 0.40 0.100 52
PUBLIC PARK A 0.39 0.40 0.850 52
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.40
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.485
SUBAREA AREA(ACRES) = 0.76 SUBAREA RUNOFF(CFS) = 2.54
EFFECTIVE AREA(ACRES) = 2.31 AREA-AVERAGED Fm(INCH/HR) = 0.18
AREA-AVERAGED Fp(INCH/HR) = 0.40 AREA-AVERAGED Ap = 0.46
TOTAL AREA(ACRES) = 2.3 PEAK FLOW RATE(CFS) = 7.75

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.47 HALFSTREET FLOOD WIDTH(FEET) = 17.38
FLOW VELOCITY(FEET/SEC.) = 2.68 DEPTH*VELOCITY(FT*FT/SEC.) = 1.27
LONGEST FLOWPATH FROM NODE 4.01 TO NODE 4.09 = 1149.15 FEET.

*****
FLOW PROCESS FROM NODE 4.09 TO NODE 4.09 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 11.13
RAINFALL INTENSITY(INCH/HR) = 3.91
AREA-AVERAGED Fm(INCH/HR) = 0.18
AREA-AVERAGED Fp(INCH/HR) = 0.40
AREA-AVERAGED Ap = 0.46
EFFECTIVE STREAM AREA(ACRES) = 2.31
TOTAL STREAM AREA(ACRES) = 2.31
PEAK FLOW RATE(CFS) AT CONFLUENCE = 7.75

*****
FLOW PROCESS FROM NODE 5.01 TO NODE 5.03 IS CODE = 21
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>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<
=====
INITIAL SUBAREA FLOW-LENGTH(FEET) = 253.47
ELEVATION DATA: UPSTREAM(FEET) = 75.00 DOWNSTREAM(FEET) = 73.50

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 7.763
* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 4.809
SUBAREA Tc AND LOSS RATE DATA(AMC III):
DEVELOPMENT TYPE/      SCS SOIL  AREA      Fp          Ap      SCS  Tc
LAND USE              GROUP  (ACRES)  (INCH/HR)  (DECIMAL)  CN  (MIN.)
COMMERCIAL              A      0.21      0.40      0.100     52   7.76
PUBLIC PARK              A      0.27      0.40      0.850     52  12.33
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.40
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.522
SUBAREA RUNOFF(CFS) = 1.99
TOTAL AREA(ACRES) = 0.48 PEAK FLOW RATE(CFS) = 1.99

*****
FLOW PROCESS FROM NODE 5.03 TO NODE 5.05 IS CODE = 62
-----
>>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>(STREET TABLE SECTION # 1 USED)<<<<<
=====
UPSTREAM ELEVATION(FEET) = 73.50 DOWNSTREAM ELEVATION(FEET) = 72.00
STREET LENGTH(FEET) = 273.08 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.13
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.39
HALFSTREET FLOOD WIDTH(FEET) = 12.93
AVERAGE FLOW VELOCITY(FEET/SEC.) = 1.86
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.73
STREET FLOW TRAVEL TIME(MIN.) = 2.45 Tc(MIN.) = 10.21
* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 4.109
SUBAREA LOSS RATE DATA(AMC III):
DEVELOPMENT TYPE/      SCS SOIL  AREA      Fp          Ap      SCS
LAND USE              GROUP  (ACRES)  (INCH/HR)  (DECIMAL)  CN
COMMERCIAL              A      0.43      0.40      0.100     52
PUBLIC PARK              A      0.21      0.40      0.850     52
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.40
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.346
SUBAREA AREA(ACRES) = 0.64 SUBAREA RUNOFF(CFS) = 2.29
EFFECTIVE AREA(ACRES) = 1.12 AREA-AVERAGED Fm(INCH/HR) = 0.17
AREA-AVERAGED Fp(INCH/HR) = 0.40 AREA-AVERAGED Ap = 0.42
TOTAL AREA(ACRES) = 1.1 PEAK FLOW RATE(CFS) = 3.97

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.42 HALFSTREET FLOOD WIDTH(FEET) = 14.34
FLOW VELOCITY(FEET/SEC.) = 1.96 DEPTH*VELOCITY(FT*FT/SEC.) = 0.82
LONGEST FLOWPATH FROM NODE 5.01 TO NODE 5.05 = 526.55 FEET.

*****
FLOW PROCESS FROM NODE 5.05 TO NODE 4.09 IS CODE = 1
-----
>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 10.21
RAINFALL INTENSITY(INCH/HR) = 4.11
AREA-AVERAGED Fm(INCH/HR) = 0.17

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AREA-AVERAGED F_p (INCH/HR) = 0.40
 AREA-AVERAGED A_p = 0.42
 EFFECTIVE STREAM AREA(ACRES) = 1.12
 TOTAL STREAM AREA(ACRES) = 1.12
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 3.97

** CONFLUENCE DATA **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	$F_p(F_m)$ (INCH/HR)	A_p	A_e (ACRES)	HEADWATER NODE
1	7.75	11.13	3.912	0.40(0.18)	0.46	2.3	4.01
2	3.97	10.21	4.109	0.40(0.17)	0.42	1.1	5.01

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	$F_p(F_m)$ (INCH/HR)	A_p	A_e (ACRES)	HEADWATER NODE
1	11.46	10.21	4.109	0.40(0.18)	0.44	3.2	5.01
2	11.53	11.13	3.912	0.40(0.18)	0.45	3.4	4.01

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 11.53 Tc(MIN.) = 11.13
 EFFECTIVE AREA(ACRES) = 3.43 AREA-AVERAGED F_m (INCH/HR) = 0.18
 AREA-AVERAGED F_p (INCH/HR) = 0.40 AREA-AVERAGED A_p = 0.45
 TOTAL AREA(ACRES) = 3.4
 LONGEST FLOWPATH FROM NODE 4.01 TO NODE 4.09 = 1149.15 FEET.

END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 3.4 TC(MIN.) = 11.13
 EFFECTIVE AREA(ACRES) = 3.43 AREA-AVERAGED F_m (INCH/HR) = 0.18
 AREA-AVERAGED F_p (INCH/HR) = 0.40 AREA-AVERAGED A_p = 0.445
 PEAK FLOW RATE(CFS) = 11.53

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	$F_p(F_m)$ (INCH/HR)	A_p	A_e (ACRES)	HEADWATER NODE
1	11.46	10.21	4.109	0.40(0.18)	0.44	3.2	5.01
2	11.53	11.13	3.912	0.40(0.18)	0.45	3.4	4.01

END OF RATIONAL METHOD ANALYSIS

Rational Method – 100-Year Storm Event: Proposed Condition

 RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE
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Analysis prepared by:

Stantec

***** DESCRIPTION OF STUDY *****
 * Culver Alton - 100 Year Rational Method Study, Proposed Conditions *
 * DMA 1: North Intersection Streamline, Culver to Alton *
 * 11/07/2019 - ECS *

FILE NAME: 100DMA1P.DAT
 TIME/DATE OF STUDY: 16:03 11/07/2019

=====

USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:

=====

--*TIME-OF-CONCENTRATION MODEL*--

USER SPECIFIED STORM EVENT(YEAR) = 100.00
 SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00
 SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.95
 DATA BANK RAINFALL USED
 ANTECEDENT MOISTURE CONDITION (AMC) III ASSUMED FOR RATIONAL METHOD

USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL

NO.	HALF- WIDTH (FT)	CROWN TO CROSSFALL (FT)	STREET-CROSSFALL: IN- / OUT-/PARK- SIDE / SIDE/ WAY	CURB HEIGHT (FT)	GUTTER-GEOMETRIES:			MANNING FACTOR (n)
					WIDTH (FT)	LIP (FT)	HIKE (FT)	
1	30.0	20.0	0.018/0.018/0.020	0.67	2.00	0.0312	0.167	0.0150
2	40.0	30.0	0.018/0.018/0.020	0.67	2.00	0.0312	0.167	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:
 1. Relative Flow-Depth = 0.00 FEET
 as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
 2. (Depth)*(Velocity) Constraint = 6.0 (FT*FT/S)
 *SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
 OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*
 *USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

FLOW PROCESS FROM NODE 1.01 TO NODE 1.03 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
 >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 330.00
 ELEVATION DATA: UPSTREAM(FEET) = 75.00 DOWNSTREAM(FEET) = 73.00

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$
 SUBAREA ANALYSIS USED MINIMUM T_c (MIN.) = 8.586
 * 100 YEAR RAINFALL INTENSITY(INCH/HR) = 4.539
 SUBAREA T_c AND LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	F_p (INCH/HR)	A_p (DECIMAL)	SCS CN	T_c (MIN.)
COMMERCIAL	A	0.41	0.40	0.100	52	8.59
PUBLIC PARK	A	0.27	0.40	0.850	52	13.64

SUBAREA AVERAGE PERVIOUS LOSS RATE, F_p (INCH/HR) = 0.40
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, A_p = 0.398
 SUBAREA RUNOFF(CFS) = 2.68
 TOTAL AREA(ACRES) = 0.68 PEAK FLOW RATE(CFS) = 2.68

FLOW PROCESS FROM NODE 1.03 TO NODE 1.05 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<

=====

UPSTREAM ELEVATION(FEET) = 73.00 DOWNSTREAM ELEVATION(FEET) = 68.00
STREET LENGTH(FEET) = 355.96 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 4.60
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.39
HALFSTREET FLOOD WIDTH(FEET) = 12.46
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.91
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 1.12
STREET FLOW TRAVEL TIME(MIN.) = 2.04 Tc(MIN.) = 10.63
* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 4.017

SUBAREA LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	B	0.12	0.30	0.100	76
COMMERCIAL	A	0.52	0.40	0.100	52
PUBLIC PARK	B	0.20	0.30	0.850	76
PUBLIC PARK	A	0.26	0.40	0.850	52

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.36
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.414
SUBAREA AREA(ACRES) = 1.10 SUBAREA RUNOFF(CFS) = 3.83
EFFECTIVE AREA(ACRES) = 1.78 AREA-AVERAGED Fm(INCH/HR) = 0.15
AREA-AVERAGED Fp(INCH/HR) = 0.37 AREA-AVERAGED Ap = 0.41
TOTAL AREA(ACRES) = 1.8 PEAK FLOW RATE(CFS) = 6.19

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.42 HALFSTREET FLOOD WIDTH(FEET) = 14.18
FLOW VELOCITY(FEET/SEC.) = 3.11 DEPTH*VELOCITY(FT*FT/SEC.) = 1.29
LONGEST FLOWPATH FROM NODE 1.01 TO NODE 1.05 = 685.96 FEET.

FLOW PROCESS FROM NODE 1.05 TO NODE 1.07 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<

=====

UPSTREAM ELEVATION(FEET) = 68.00 DOWNSTREAM ELEVATION(FEET) = 65.50
STREET LENGTH(FEET) = 162.78 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 6.97
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.42
HALFSTREET FLOOD WIDTH(FEET) = 14.65
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.31
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 1.40
STREET FLOW TRAVEL TIME(MIN.) = 0.82 Tc(MIN.) = 11.45
* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 3.849

SUBAREA LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	B	0.14	0.30	0.100	76

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COMMERCIAL	A	0.13	0.40	0.100	52
PUBLIC PARK	B	0.10	0.30	0.850	76
PUBLIC PARK	A	0.10	0.40	0.850	52

SUBAREA AVERAGE PERVIOUS LOSS RATE, F_p (INCH/HR) = 0.35
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, A_p = 0.419
 SUBAREA AREA(ACRES) = 0.47 SUBAREA RUNOFF(CFS) = 1.57
 EFFECTIVE AREA(ACRES) = 2.25 AREA-AVERAGED F_m (INCH/HR) = 0.15
 AREA-AVERAGED F_p (INCH/HR) = 0.37 AREA-AVERAGED A_p = 0.41
 TOTAL AREA(ACRES) = 2.2 PEAK FLOW RATE(CFS) = 7.49

END OF SUBAREA STREET FLOW HYDRAULICS:
 DEPTH(Feet) = 0.43 HALFSTREET FLOOD WIDTH(Feet) = 15.12
 FLOW VELOCITY(Feet/Sec.) = 3.35 DEPTH*VELOCITY(FT*FT/SEC.) = 1.45
 LONGEST FLOWPATH FROM NODE 1.01 TO NODE 1.07 = 848.74 FEET.

=====

END OF STUDY SUMMARY:

TOTAL AREA(ACRES)	=	2.2	TC(MIN.)	=	11.45
EFFECTIVE AREA(ACRES)	=	2.25	AREA-AVERAGED F_m (INCH/HR)	=	0.15
AREA-AVERAGED F_p (INCH/HR)	=	0.37	AREA-AVERAGED A_p	=	0.410
PEAK FLOW RATE(CFS)	=	7.49			

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END OF RATIONAL METHOD ANALYSIS

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Analysis prepared by:

Stantec

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***** DESCRIPTION OF STUDY *****
* Culver Alton - 100 Year Rational Method Study, Proposed Conditions *
* DMA 2: West Intersection Streamline, Alton *
* 10/25/2019 - ECS *
*****
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FILE NAME: 100DMA2.DAT
TIME/DATE OF STUDY: 14:09 10/25/2019

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=====
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:
=====
--*TIME-OF-CONCENTRATION MODEL*--
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USER SPECIFIED STORM EVENT(YEAR) = 100.00
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.95
DATA BANK RAINFALL USED
ANTECEDENT MOISTURE CONDITION (AMC) III ASSUMED FOR RATIONAL METHOD

USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL

NO.	HALF-CROWN TO		STREET-CROSSFALL:		CURB HEIGHT (FT)	GUTTER-GEOMETRIES:			MANNING FACTOR (n)
	WIDTH (FT)	CROSSFALL (FT)	IN- / SIDE	OUT- / SIDE		WIDTH (FT)	LIP (FT)	HIKE (FT)	
1	30.0	20.0	0.018/0.018	0.020	0.67	2.00	0.0312	0.167	0.0150
2	40.0	30.0	0.018/0.018	0.020	0.67	2.00	0.0312	0.167	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:
1. Relative Flow-Depth = 0.00 FEET
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)*(Velocity) Constraint = 6.0 (FT*FT/S)
*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*
*USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

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*****
FLOW PROCESS FROM NODE 2.01 TO NODE 2.03 IS CODE = 21
*****
```

```
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<
=====
INITIAL SUBAREA FLOW-LENGTH(FEET) = 330.00
ELEVATION DATA: UPSTREAM(FEET) = 72.00 DOWNSTREAM(FEET) = 68.00
```

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$
SUBAREA ANALYSIS USED MINIMUM T_c (MIN.) = 7.474
* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 4.914
SUBAREA T_c AND LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	F_p (INCH/HR)	A_p (DECIMAL)	SCS CN	T_c (MIN.)
PUBLIC PARK	B	0.01	0.30	0.850	76	11.88
PUBLIC PARK	A	0.27	0.40	0.850	52	11.88
COMMERCIAL	B	0.07	0.30	0.100	76	7.47
COMMERCIAL	A	0.40	0.40	0.100	52	7.47

SUBAREA AVERAGE PVIOUS LOSS RATE, F_p (INCH/HR) = 0.39
SUBAREA AVERAGE PVIOUS AREA FRACTION, A_p = 0.380
SUBAREA RUNOFF(CFS) = 3.22
TOTAL AREA(ACRES) = 0.75 PEAK FLOW RATE(CFS) = 3.22

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*****
Page 1
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                                100DMA2P.RES
FLOW PROCESS FROM NODE      2.03 TO NODE      2.05 IS CODE =  62
-----
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION #  1 USED)<<<<
=====
UPSTREAM ELEVATION(FEET) =   68.00  DOWNSTREAM ELEVATION(FEET) =   62.00
STREET LENGTH(FEET) =   440.15  CURB HEIGHT(INCHES) =   8.0
STREET HALFWIDTH(FEET) =   30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) =   20.00
INSIDE STREET CROSSFALL(DECIMAL) =   0.018
OUTSIDE STREET CROSSFALL(DECIMAL) =   0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF =  1
STREET PARKWAY CROSSFALL(DECIMAL) =   0.020
Manning's FRICTION FACTOR for Streetflow Section(curb-to-curb) =   0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section =   0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) =           5.02
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) =   0.40
HALFSTREET FLOOD WIDTH(FEET) =   13.09
AVERAGE FLOW VELOCITY(FEET/SEC.) =   2.91
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) =   1.15
STREET FLOW TRAVEL TIME(MIN.) =   2.52  Tc(MIN.) =   9.99
* 100 YEAR RAINFALL INTENSITY(INCH/HR) =   4.161
SUBAREA LOSS RATE DATA(AMC III):
DEVELOPMENT TYPE/      SCS SOIL      AREA      Fp      Ap      SCS
LAND USE      GROUP      (ACRES)  (INCH/HR)  (DECIMAL)  CN
COMMERCIAL      B      0.22      0.30      0.100      76
COMMERCIAL      A      0.27      0.40      0.100      52
PUBLIC PARK      B      0.23      0.30      0.850      76
PUBLIC PARK      A      0.28      0.40      0.850      52
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) =   0.35
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap =   0.483
SUBAREA AREA(ACRES) =   1.00      SUBAREA RUNOFF(CFS) =   3.59
EFFECTIVE AREA(ACRES) =   1.75      AREA-AVERAGED Fm(INCH/HR) =   0.16
AREA-AVERAGED Fp(INCH/HR) =   0.37  AREA-AVERAGED Ap =   0.44
TOTAL AREA(ACRES) =   1.8      PEAK FLOW RATE(CFS) =   6.30

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) =   0.42  HALFSTREET FLOOD WIDTH(FEET) =   14.41
FLOW VELOCITY(FEET/SEC.) =   3.07  DEPTH*VELOCITY(FT*FT/SEC.) =   1.29
LONGEST FLOWPATH FROM NODE      2.01 TO NODE      2.05 =   770.15 FEET.
=====
END OF STUDY SUMMARY:
TOTAL AREA(ACRES) =   1.8  TC(MIN.) =   9.99
EFFECTIVE AREA(ACRES) =   1.75  AREA-AVERAGED Fm(INCH/HR)=   0.16
AREA-AVERAGED Fp(INCH/HR) =   0.37  AREA-AVERAGED Ap =   0.439
PEAK FLOW RATE(CFS) =   6.30
=====
END OF RATIONAL METHOD ANALYSIS

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Analysis prepared by:

Stantec

***** DESCRIPTION OF STUDY *****
 * Culver Alton - 100 Year Rational Method Study, Proposed Conditions *
 * DMA 3: South Intersection Streamline, Alton *
 * 11/07/2019 - ECS *

FILE NAME: 100DMA3P.DAT
 TIME/DATE OF STUDY: 12:49 11/07/2019

=====

USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:

=====

--*TIME-OF-CONCENTRATION MODEL*--

USER SPECIFIED STORM EVENT(YEAR) = 100.00
 SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00
 SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.95
 DATA BANK RAINFALL USED
 ANTECEDENT MOISTURE CONDITION (AMC) III ASSUMED FOR RATIONAL METHOD

USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL

NO.	HALF- WIDTH	CROWN TO CROSSFALL	STREET-CROSSFALL: IN- / OUT-/PARK- SIDE / SIDE/ WAY	CURB HEIGHT	GUTTER-GEOMETRIES: WIDTH LIP HIKE	MANNING FACTOR
	(FT)	(FT)		(FT)	(FT) (FT) (FT)	(n)
1	30.0	20.0	0.018/0.018/0.020	0.67	2.00 0.0312 0.167	0.0150
2	40.0	30.0	0.018/0.018/0.020	0.67	2.00 0.0312 0.167	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:
 1. Relative Flow-Depth = 0.00 FEET
 as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
 2. (Depth)*(Velocity) Constraint = 6.0 (FT*FT/S)
 *SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
 OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*
 *USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

FLOW PROCESS FROM NODE 3.01 TO NODE 3.03 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
 >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 308.42
 ELEVATION DATA: UPSTREAM(FEET) = 82.00 DOWNSTREAM(FEET) = 77.00

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$
 SUBAREA ANALYSIS USED MINIMUM T_c (MIN.) = 6.864
 * 100 YEAR RAINFALL INTENSITY(INCH/HR) = 5.160
 SUBAREA T_c AND LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	F_p (INCH/HR)	A_p (DECIMAL)	SCS CN	T_c (MIN.)
COMMERCIAL	A	0.26	0.40	0.100	52	6.86
PUBLIC PARK	A	0.22	0.40	0.850	52	10.91

SUBAREA AVERAGE PERVIOUS LOSS RATE, F_p (INCH/HR) = 0.40
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, A_p = 0.444
 SUBAREA RUNOFF(CFS) = 2.15
 TOTAL AREA(ACRES) = 0.48 PEAK FLOW RATE(CFS) = 2.15

FLOW PROCESS FROM NODE 3.03 TO NODE 3.05 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<

=====

UPSTREAM ELEVATION(FEET) = 77.00 DOWNSTREAM ELEVATION(FEET) = 72.00
STREET LENGTH(FEET) = 500.82 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 4.10
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.39
HALFSTREET FLOOD WIDTH(FEET) = 12.77
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.48
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.97
STREET FLOW TRAVEL TIME(MIN.) = 3.36 Tc(MIN.) = 10.23
* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 4.106

SUBAREA LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	A	0.53	0.40	0.100	52
PUBLIC PARK	A	0.57	0.40	0.850	52

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.40
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.489
SUBAREA AREA(ACRES) = 1.10 SUBAREA RUNOFF(CFS) = 3.87
EFFECTIVE AREA(ACRES) = 1.58 AREA-AVERAGED Fm(INCH/HR) = 0.19
AREA-AVERAGED Fp(INCH/HR) = 0.40 AREA-AVERAGED Ap = 0.48
TOTAL AREA(ACRES) = 1.6 PEAK FLOW RATE(CFS) = 5.57

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.42 HALFSTREET FLOOD WIDTH(FEET) = 14.57
FLOW VELOCITY(FEET/SEC.) = 2.67 DEPTH*VELOCITY(FT*FT/SEC.) = 1.13
LONGEST FLOWPATH FROM NODE 3.01 TO NODE 3.05 = 809.24 FEET.

FLOW PROCESS FROM NODE 3.05 TO NODE 3.05 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

=====

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 10.23
RAINFALL INTENSITY(INCH/HR) = 4.11
AREA-AVERAGED Fm(INCH/HR) = 0.19
AREA-AVERAGED Fp(INCH/HR) = 0.40
AREA-AVERAGED Ap = 0.48
EFFECTIVE STREAM AREA(ACRES) = 1.58
TOTAL STREAM AREA(ACRES) = 1.58
PEAK FLOW RATE(CFS) AT CONFLUENCE = 5.57

FLOW PROCESS FROM NODE 6.01 TO NODE 6.03 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 237.14
ELEVATION DATA: UPSTREAM(FEET) = 73.50 DOWNSTREAM(FEET) = 72.50

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 8.089
* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 4.697
SUBAREA Tc AND LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
PUBLIC PARK	D	0.06	0.20	0.850	91	12.85
COMMERCIAL	D	0.39	0.20	0.100	91	8.09

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                                100DMA3P.RES
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.200
SUBAREA RUNOFF(CFS) = 1.89
TOTAL AREA(ACRES) = 0.45 PEAK FLOW RATE(CFS) = 1.89

*****
FLOW PROCESS FROM NODE 6.03 TO NODE 3.05 IS CODE = 62
-----
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<
=====
UPSTREAM ELEVATION(FEET) = 72.50 DOWNSTREAM ELEVATION(FEET) = 72.00
STREET LENGTH(FEET) = 276.24 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curb) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.57
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.43
HALFSTREET FLOOD WIDTH(FEET) = 15.12
AVERAGE FLOW VELOCITY(FEET/SEC.) = 1.15
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.50
STREET FLOW TRAVEL TIME(MIN.) = 4.01 Tc(MIN.) = 12.09
* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 3.730
SUBAREA LOSS RATE DATA(AMC III):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
PUBLIC PARK A 0.01 0.40 0.850 52
COMMERCIAL A 0.27 0.40 0.100 52
COMMERCIAL B 0.09 0.30 0.100 76
PUBLIC PARK D 0.01 0.20 0.850 91
COMMERCIAL D 0.03 0.20 0.100 91
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.34
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.137
SUBAREA AREA(ACRES) = 0.41 SUBAREA RUNOFF(CFS) = 1.36
EFFECTIVE AREA(ACRES) = 0.86 AREA-AVERAGED Fm(INCH/HR) = 0.04
AREA-AVERAGED Fp(INCH/HR) = 0.25 AREA-AVERAGED Ap = 0.17
TOTAL AREA(ACRES) = 0.9 PEAK FLOW RATE(CFS) = 2.85

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.44 HALFSTREET FLOOD WIDTH(FEET) = 15.74
FLOW VELOCITY(FEET/SEC.) = 1.19 DEPTH*VELOCITY(FT*FT/SEC.) = 0.53
LONGEST FLOWPATH FROM NODE 6.01 TO NODE 3.05 = 513.38 FEET.

*****
FLOW PROCESS FROM NODE 6.03 TO NODE 3.05 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 12.09
RAINFALL INTENSITY(INCH/HR) = 3.73
AREA-AVERAGED Fm(INCH/HR) = 0.04
AREA-AVERAGED Fp(INCH/HR) = 0.25
AREA-AVERAGED Ap = 0.17
EFFECTIVE STREAM AREA(ACRES) = 0.86
TOTAL STREAM AREA(ACRES) = 0.86
PEAK FLOW RATE(CFS) AT CONFLUENCE = 2.85

** CONFLUENCE DATA **
STREAM Q Tc Intensity Fp(Fm) Ap Ae HEADWATER
NUMBER (CFS) (MIN.) (INCH/HR) (INCH/HR) (ACRES) NODE
1 5.57 10.23 4.106 0.40( 0.19) 0.48 1.6 3.01
2 2.85 12.09 3.730 0.25( 0.04) 0.17 0.9 6.01

```

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	8.23	10.23	4.106	0.38(0.14)	0.38	2.3	3.01
2	7.89	12.09	3.730	0.38(0.14)	0.37	2.4	6.01

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 8.23 Tc(MIN.) = 10.23
EFFECTIVE AREA(ACRES) = 2.31 AREA-AVERAGED Fm(INCH/HR) = 0.14
AREA-AVERAGED Fp(INCH/HR) = 0.38 AREA-AVERAGED Ap = 0.38
TOTAL AREA(ACRES) = 2.4
LONGEST FLOWPATH FROM NODE 3.01 TO NODE 3.05 = 809.24 FEET.

=====

END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 2.4 TC(MIN.) = 10.23
EFFECTIVE AREA(ACRES) = 2.31 AREA-AVERAGED Fm(INCH/HR) = 0.14
AREA-AVERAGED Fp(INCH/HR) = 0.38 AREA-AVERAGED Ap = 0.379
PEAK FLOW RATE(CFS) = 8.23

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	8.23	10.23	4.106	0.38(0.14)	0.38	2.3	3.01
2	7.89	12.09	3.730	0.38(0.14)	0.37	2.4	6.01

=====

END OF RATIONAL METHOD ANALYSIS

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Analysis prepared by:

Stantec

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***** DESCRIPTION OF STUDY *****
* Culver Alton - 100 Year Rational Method Study, Proposed Conditions *
* DMA 4: East Intersection Streamline, Yale to Alton to Culver *
* 11/07/2019 - ECS *
*****

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FILE NAME: 100DMA4P.DAT
TIME/DATE OF STUDY: 15:27 11/07/2019

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=====
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:
=====
--*TIME-OF-CONCENTRATION MODEL*--

```

USER SPECIFIED STORM EVENT(YEAR) = 100.00
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.95
DATA BANK RAINFALL USED
ANTECEDENT MOISTURE CONDITION (AMC) III ASSUMED FOR RATIONAL METHOD

```

*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL*
  HALF- CROWN TO STREET-CROSSFALL: CURB GUTTER-GEOMETRIES: MANNING
  WIDTH CROSSFALL IN- / OUT-/PARK- HEIGHT WIDTH LIP HIKE FACTOR
NO. (FT) (FT) SIDE / SIDE/ WAY (FT) (FT) (FT) (FT) (n)
=== =====
1 30.0 20.0 0.018/0.018/0.020 0.67 2.00 0.0312 0.167 0.0150
2 40.0 30.0 0.018/0.018/0.020 0.67 2.00 0.0312 0.167 0.0150

```

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:
1. Relative Flow-Depth = 0.00 FEET
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)*(Velocity) Constraint = 6.0 (FT*FT/S)
*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*
*USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

```

*****
FLOW PROCESS FROM NODE 4.01 TO NODE 4.03 IS CODE = 21
-----
>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<
=====
INITIAL SUBAREA FLOW-LENGTH(FEET) = 116.02
ELEVATION DATA: UPSTREAM(FEET) = 89.00 DOWNSTREAM(FEET) = 87.00

```

$T_c = K[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20$
SUBAREA ANALYSIS USED MINIMUM T_c (MIN.) = 5.000
* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 6.187
SUBAREA T_c AND LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	F_p (INCH/HR)	A_p (DECIMAL)	SCS CN	T_c (MIN.)
PUBLIC PARK	A	0.01	0.40	0.850	52	7.29
COMMERCIAL	A	0.13	0.40	0.100	52	5.00

SUBAREA AVERAGE PERVIOUS LOSS RATE, F_p (INCH/HR) = 0.40
SUBAREA AVERAGE PERVIOUS AREA FRACTION, A_p = 0.154
SUBAREA RUNOFF(CFS) = 0.77
TOTAL AREA(ACRES) = 0.14 PEAK FLOW RATE(CFS) = 0.77

```

*****
FLOW PROCESS FROM NODE 4.03 TO NODE 4.05 IS CODE = 62
-----

```

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<

=====

UPSTREAM ELEVATION(FEET) = 87.00 DOWNSTREAM ELEVATION(FEET) = 80.00
STREET LENGTH(FEET) = 301.23 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.96
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.29
HALFSTREET FLOOD WIDTH(FEET) = 7.22
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.97
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.87
STREET FLOW TRAVEL TIME(MIN.) = 1.69 Tc(MIN.) = 6.69
* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 5.237
SUBAREA LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
PUBLIC PARK	A	0.07	0.40	0.850	52
COMMERCIAL	A	0.44	0.40	0.100	52

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.40
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.203
SUBAREA AREA(ACRES) = 0.51 SUBAREA RUNOFF(CFS) = 2.37
EFFECTIVE AREA(ACRES) = 0.65 AREA-AVERAGED Fm(INCH/HR) = 0.08
AREA-AVERAGED Fp(INCH/HR) = 0.40 AREA-AVERAGED Ap = 0.19
TOTAL AREA(ACRES) = 0.6 PEAK FLOW RATE(CFS) = 3.02

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.32 HALFSTREET FLOOD WIDTH(FEET) = 9.09
FLOW VELOCITY(FEET/SEC.) = 3.24 DEPTH*VELOCITY(FT*FT/SEC.) = 1.05
LONGEST FLOWPATH FROM NODE 4.01 TO NODE 4.05 = 417.25 FEET.

FLOW PROCESS FROM NODE 4.05 TO NODE 4.07 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<

=====

UPSTREAM ELEVATION(FEET) = 80.00 DOWNSTREAM ELEVATION(FEET) = 75.00
STREET LENGTH(FEET) = 369.87 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 4.73
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.39
HALFSTREET FLOOD WIDTH(FEET) = 12.77
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.87
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 1.12
STREET FLOW TRAVEL TIME(MIN.) = 2.15 Tc(MIN.) = 8.84
* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 4.464
SUBAREA LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	A	0.27	0.40	0.100	52
PUBLIC PARK	A	0.63	0.40	0.850	52

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.40


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SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.625
SUBAREA AREA(ACRES) = 0.90 SUBAREA RUNOFF(CFS) = 3.41
EFFECTIVE AREA(ACRES) = 1.55 AREA-AVERAGED Fm(INCH/HR) = 0.18
AREA-AVERAGED Fp(INCH/HR) = 0.40 AREA-AVERAGED Ap = 0.44
TOTAL AREA(ACRES) = 1.5 PEAK FLOW RATE(CFS) = 5.98

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.41 HALFSTREET FLOOD WIDTH(FEET) = 14.10
FLOW VELOCITY(FEET/SEC.) = 3.04 DEPTH*VELOCITY(FT*FT/SEC.) = 1.26
LONGEST FLOWPATH FROM NODE 4.01 TO NODE 4.07 = 787.12 FEET.

*****
FLOW PROCESS FROM NODE 4.07 TO NODE 4.09 IS CODE = 62
-----
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<
=====
UPSTREAM ELEVATION(FEET) = 75.00 DOWNSTREAM ELEVATION(FEET) = 72.00
STREET LENGTH(FEET) = 362.03 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 7.27
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.46
HALFSTREET FLOOD WIDTH(FEET) = 16.91
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.65
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 1.23
STREET FLOW TRAVEL TIME(MIN.) = 2.28 Tc(MIN.) = 11.12
* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 3.914
SUBAREA LOSS RATE DATA(AMC III):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
COMMERCIAL A 0.54 0.40 0.100 52
PUBLIC PARK A 0.22 0.40 0.850 52
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.40
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.317
SUBAREA AREA(ACRES) = 0.76 SUBAREA RUNOFF(CFS) = 2.59
EFFECTIVE AREA(ACRES) = 2.31 AREA-AVERAGED Fm(INCH/HR) = 0.16
AREA-AVERAGED Fp(INCH/HR) = 0.40 AREA-AVERAGED Ap = 0.40
TOTAL AREA(ACRES) = 2.3 PEAK FLOW RATE(CFS) = 7.80

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.47 HALFSTREET FLOOD WIDTH(FEET) = 17.46
FLOW VELOCITY(FEET/SEC.) = 2.68 DEPTH*VELOCITY(FT*FT/SEC.) = 1.27
LONGEST FLOWPATH FROM NODE 4.01 TO NODE 4.09 = 1149.15 FEET.

*****
FLOW PROCESS FROM NODE 4.09 TO NODE 4.09 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 11.12
RAINFALL INTENSITY(INCH/HR) = 3.91
AREA-AVERAGED Fm(INCH/HR) = 0.16
AREA-AVERAGED Fp(INCH/HR) = 0.40
AREA-AVERAGED Ap = 0.40
EFFECTIVE STREAM AREA(ACRES) = 2.31
TOTAL STREAM AREA(ACRES) = 2.31
PEAK FLOW RATE(CFS) AT CONFLUENCE = 7.80

*****
FLOW PROCESS FROM NODE 5.01 TO NODE 5.03 IS CODE = 21
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>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<
=====
INITIAL SUBAREA FLOW-LENGTH(FEET) = 253.47
ELEVATION DATA: UPSTREAM(FEET) = 75.00 DOWNSTREAM(FEET) = 73.50

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 7.763
* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 4.809
SUBAREA Tc AND LOSS RATE DATA(AMC III):
DEVELOPMENT TYPE/      SCS SOIL  AREA      Fp          Ap      SCS  Tc
LAND USE              GROUP  (ACRES)  (INCH/HR)  (DECIMAL)  CN  (MIN.)
COMMERCIAL             A      0.24      0.40      0.100     52   7.76
PUBLIC PARK            A      0.24      0.40      0.850     52  12.33
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.40
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.475
SUBAREA RUNOFF(CFS) = 2.00
TOTAL AREA(ACRES) = 0.48 PEAK FLOW RATE(CFS) = 2.00

*****
FLOW PROCESS FROM NODE 5.03 TO NODE 5.05 IS CODE = 62
-----
>>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>(STREET TABLE SECTION # 1 USED)<<<<<
=====
UPSTREAM ELEVATION(FEET) = 73.50 DOWNSTREAM ELEVATION(FEET) = 72.00
STREET LENGTH(FEET) = 273.08 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.16
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.39
HALFSTREET FLOOD WIDTH(FEET) = 13.01
AVERAGE FLOW VELOCITY(FEET/SEC.) = 1.85
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.73
STREET FLOW TRAVEL TIME(MIN.) = 2.46 Tc(MIN.) = 10.22
* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 4.108
SUBAREA LOSS RATE DATA(AMC III):
DEVELOPMENT TYPE/      SCS SOIL  AREA      Fp          Ap      SCS
LAND USE              GROUP  (ACRES)  (INCH/HR)  (DECIMAL)  CN
COMMERCIAL             A      0.57      0.40      0.100     52
PUBLIC PARK            A      0.07      0.40      0.850     52
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.40
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.182
SUBAREA AREA(ACRES) = 0.64 SUBAREA RUNOFF(CFS) = 2.32
EFFECTIVE AREA(ACRES) = 1.12 AREA-AVERAGED Fm(INCH/HR) = 0.12
AREA-AVERAGED Fp(INCH/HR) = 0.40 AREA-AVERAGED Ap = 0.31
TOTAL AREA(ACRES) = 1.1 PEAK FLOW RATE(CFS) = 4.02

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.42 HALFSTREET FLOOD WIDTH(FEET) = 14.41
FLOW VELOCITY(FEET/SEC.) = 1.96 DEPTH*VELOCITY(FT*FT/SEC.) = 0.82
LONGEST FLOWPATH FROM NODE 5.01 TO NODE 5.05 = 526.55 FEET.

*****
FLOW PROCESS FROM NODE 5.05 TO NODE 4.09 IS CODE = 1
-----
>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 10.22
RAINFALL INTENSITY(INCH/HR) = 4.11
AREA-AVERAGED Fm(INCH/HR) = 0.12

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AREA-AVERAGED F_p (INCH/HR) = 0.40
 AREA-AVERAGED A_p = 0.31
 EFFECTIVE STREAM AREA(ACRES) = 1.12
 TOTAL STREAM AREA(ACRES) = 1.12
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 4.02

** CONFLUENCE DATA **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	$F_p(F_m)$ (INCH/HR)	A_p	A_e (ACRES)	HEADWATER NODE
1	7.80	11.12	3.914	0.40(0.16)	0.40	2.3	4.01
2	4.02	10.22	4.108	0.40(0.12)	0.31	1.1	5.01

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	$F_p(F_m)$ (INCH/HR)	A_p	A_e (ACRES)	HEADWATER NODE
1	11.56	10.22	4.108	0.40(0.15)	0.37	3.2	5.01
2	11.62	11.12	3.914	0.40(0.15)	0.37	3.4	4.01

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 11.62 Tc(MIN.) = 11.12
 EFFECTIVE AREA(ACRES) = 3.43 AREA-AVERAGED F_m (INCH/HR) = 0.15
 AREA-AVERAGED F_p (INCH/HR) = 0.40 AREA-AVERAGED A_p = 0.37
 TOTAL AREA(ACRES) = 3.4
 LONGEST FLOWPATH FROM NODE 4.01 TO NODE 4.09 = 1149.15 FEET.

END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 3.4 TC(MIN.) = 11.12
 EFFECTIVE AREA(ACRES) = 3.43 AREA-AVERAGED F_m (INCH/HR) = 0.15
 AREA-AVERAGED F_p (INCH/HR) = 0.40 AREA-AVERAGED A_p = 0.371
 PEAK FLOW RATE(CFS) = 11.62

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	$F_p(F_m)$ (INCH/HR)	A_p	A_e (ACRES)	HEADWATER NODE
1	11.56	10.22	4.108	0.40(0.15)	0.37	3.2	5.01
2	11.62	11.12	3.914	0.40(0.15)	0.37	3.4	4.01

END OF RATIONAL METHOD ANALYSIS

C.1 APPENDIX C – Catch Basin Calculations

Worksheet for Curb Inlet In Sag - DMA4

Project Description

Solve For Spread

Input Data

Discharge		8.85	ft ³ /s
Gutter Width		2.00	ft
Gutter Cross Slope		0.08	ft/ft
Road Cross Slope		0.02	ft/ft
Curb Opening Length		14.00	ft
Opening Height		5.50	in
Curb Throat Type	Horizontal		
Local Depression		2.00	in
Local Depression Width		2.00	ft
Throat Incline Angle		90.00	degrees

Results

Spread	21.35	ft
Depth	5.87	in
Gutter Depression	0.13	ft
Total Depression	0.29	ft

Worksheet for Circular Pipe - DMA4

Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

Input Data

Roughness Coefficient	0.013	
Channel Slope	0.02410	ft/ft
Diameter	24.00	in
Discharge	8.85	ft ³ /s

Results

Normal Depth	8.21	in
Flow Area	0.95	ft ²
Wetted Perimeter	2.50	ft
Hydraulic Radius	4.56	in
Top Width	1.90	ft
Critical Depth	1.06	ft
Percent Full	34.2	%
Critical Slope	0.00501	ft/ft
Velocity	9.31	ft/s
Velocity Head	1.35	ft
Specific Energy	2.03	ft
Froude Number	2.32	
Maximum Discharge	37.78	ft ³ /s
Discharge Full	35.12	ft ³ /s
Slope Full	0.00153	ft/ft
Flow Type	SuperCritical	

GVF Input Data

Downstream Depth	0.00	in
Length	0.00	ft
Number Of Steps	0	

GVF Output Data

Upstream Depth	0.00	in
Profile Description		
Profile Headloss	0.00	ft
Average End Depth Over Rise	0.00	%
Normal Depth Over Rise	34.22	%
Downstream Velocity	Infinity	ft/s

Worksheet for Circular Pipe - DMA4

GVF Output Data

Upstream Velocity	Infinity	ft/s
Normal Depth	8.21	in
Critical Depth	1.06	ft
Channel Slope	0.02410	ft/ft
Critical Slope	0.00501	ft/ft

Worksheet for Curb Inlet In Sag - DMA3

Project Description

Solve For Spread

Input Data

Discharge		6.31	ft ³ /s
Gutter Width		2.00	ft
Gutter Cross Slope		0.08	ft/ft
Road Cross Slope		0.02	ft/ft
Curb Opening Length		14.00	ft
Opening Height		5.50	in
Curb Throat Type	Horizontal		
Local Depression		2.00	in
Local Depression Width		2.00	ft
Throat Incline Angle		90.00	degrees

Results

Spread	17.04	ft
Depth	4.99	in
Gutter Depression	0.13	ft
Total Depression	0.29	ft

Worksheet for Circular Pipe - DMA3

Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

Input Data

Roughness Coefficient	0.013	
Channel Slope	0.01630	ft/ft
Diameter	24.00	in
Discharge	6.31	ft ³ /s

Results

Normal Depth	7.62	in
Flow Area	0.86	ft ²
Wetted Perimeter	2.39	ft
Hydraulic Radius	4.30	in
Top Width	1.86	ft
Critical Depth	0.89	ft
Percent Full	31.8	%
Critical Slope	0.00468	ft/ft
Velocity	7.36	ft/s
Velocity Head	0.84	ft
Specific Energy	1.48	ft
Froude Number	1.91	
Maximum Discharge	31.07	ft ³ /s
Discharge Full	28.88	ft ³ /s
Slope Full	0.00078	ft/ft
Flow Type	SuperCritical	

GVF Input Data

Downstream Depth	0.00	in
Length	0.00	ft
Number Of Steps	0	

GVF Output Data

Upstream Depth	0.00	in
Profile Description		
Profile Headloss	0.00	ft
Average End Depth Over Rise	0.00	%
Normal Depth Over Rise	31.75	%
Downstream Velocity	Infinity	ft/s

Worksheet for Circular Pipe - DMA3

GVF Output Data

Upstream Velocity	Infinity	ft/s
Normal Depth	7.62	in
Critical Depth	0.89	ft
Channel Slope	0.01630	ft/ft
Critical Slope	0.00468	ft/ft