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Lico Subdivision Project - Monterey Bay Unified APCD Air District, Winter

# Lico Subdivision Project Monterey Bay Unified APCD Air District, Winter

#### 1.0 Project Characteristics

#### 1.1 Land Usage

| Land Uses             | Size           | Metric        | Lot Acreage | Floor Surface Area | Population |
|-----------------------|----------------|---------------|-------------|--------------------|------------|
| Parking Lot           | 11.18          | Acre          | 11.18       | 487,151.00         | 0          |
| City Park             | City Park 8.18 |               | 8.18        | 356,386.00         | 0          |
| Single Family Housing | 149.00         | Dwelling Unit | 30.59       | 268,200.00         | 453        |

#### 1.2 Other Project Characteristics

UrbanizationUrbanWind Speed (m/s)2.8Precipitation Freq (Days)53Climate Zone4Operational Year2025

Utility Company Pacific Gas & Electric Company

 CO2 Intensity
 298.65
 CH4 Intensity
 0.014
 N20 Intensity
 0.003

 (lb/MWhr)
 (lb/MWhr)
 (lb/MWhr)
 (lb/MWhr)

#### 1.3 User Entered Comments & Non-Default Data

Project Characteristics - Adjusted intensities for 2030 RPS

Land Use - Parking lot LU is interior roadways, City park is park/stormwater; DOF estimate for population

Construction Phase - Phases from data request; assumed arch coating to start 3/4 through each building phase

Off-road Equipment - Left as default

Off-road Equipment - Default

Off-road Equipment - Default

Off-road Equipment - Default

Off-road Equipment - From data request

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Off-road Equipment - From data request

Off-road Equipment - From data request

Off-road Equipment - From data request

Off-road Equipment - From data request, assuming 1 of each throughout

Off-road Equipment - From data request

Trips and VMT - Worker/vendor for grading and construction from data request, others left default

Demolition - From data request

Grading - From data request

Architectural Coating - MBARD Rule 426. Default values for sq ft div by 4 to account for construction phasing.

Vehicle Trips - City park/Parking Lot trips zeroed. WkDy trip rate from traffic study. Corrected model error for trip %

Woodstoves - NG fireplaces

Area Coating - MABRD Rule 426; sf adjusted per arch coating screen

Energy Use -

Water And Wastewater - 20% indoor water reduction

Solid Waste - No data to indicate waste hauler diverts more than 50%

Construction Off-road Equipment Mitigation -

Mobile Land Use Mitigation -

Area Mitigation - MBARD Rule 426

Energy Mitigation - Efficient applicanes noted in data request. Solar generation from Rincon spreadsheet.

Water Mitigation - Low flow fixures accounted for in 20% overall water use reduction

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| Table Name              | Column Name                    | Default Value | New Value  |
|-------------------------|--------------------------------|---------------|------------|
| tblArchitecturalCoating | ConstArea_Residential_Exterior | 181,035.00    | 45,259.00  |
| tblArchitecturalCoating | ConstArea_Residential_Exterior | 181,035.00    | 45,259.00  |
| tblArchitecturalCoating | ConstArea_Residential_Exterior | 181,035.00    | 45,259.00  |
| tblArchitecturalCoating | ConstArea_Residential_Exterior | 181,035.00    | 45,259.00  |
| tblArchitecturalCoating | ConstArea_Residential_Interior | 543,105.00    | 135,776.00 |
| tblArchitecturalCoating | ConstArea_Residential_Interior | 543,105.00    | 135,776.00 |
| tblArchitecturalCoating | ConstArea_Residential_Interior | 543,105.00    | 135,776.00 |
| tblArchitecturalCoating | ConstArea_Residential_Interior | 543,105.00    | 135,776.00 |
| tblArchitecturalCoating | EF_Parking                     | 150.00        | 100.00     |
| tblArchitecturalCoating | EF_Parking                     | 150.00        | 100.00     |
| tblArchitecturalCoating | EF_Parking                     | 150.00        | 100.00     |
| tblArchitecturalCoating | EF_Parking                     | 150.00        | 100.00     |
| tblArchitecturalCoating | EF_Residential_Exterior        | 100.00        | 50.00      |
| tblArchitecturalCoating | EF_Residential_Exterior        | 100.00        | 50.00      |
| tblArchitecturalCoating | EF_Residential_Exterior        | 100.00        | 50.00      |
| tblArchitecturalCoating | EF_Residential_Exterior        | 100.00        | 50.00      |
| tblArchitecturalCoating | EF_Residential_Interior        | 100.00        | 50.00      |
| tblArchitecturalCoating | EF_Residential_Interior        | 100.00        | 50.00      |
| tblArchitecturalCoating | EF_Residential_Interior        | 100.00        | 50.00      |
| tblArchitecturalCoating | EF_Residential_Interior        | 100.00        | 50.00      |
| tblAreaCoating          | Area_EF_Parking                | 150           | 100        |
| tblAreaCoating          | Area_EF_Residential_Exterior   | 100           | 50         |
| tblAreaCoating          | Area_EF_Residential_Interior   | 100           | 50         |
| tblAreaMitigation       | UseLowVOCPaintParkingCheck     | False         | True       |
| tblConstructionPhase    | NumDays                        | 55.00         | 79.00      |
| tblConstructionPhase    | NumDays                        | 55.00         | 79.00      |

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| tblConstructionPhase | NumDays     | 55.00  | 78.00  |
|----------------------|-------------|--------|--------|
| tblConstructionPhase | NumDays     | 55.00  | 79.00  |
| tblConstructionPhase | NumDays     | 740.00 | 210.00 |
| tblConstructionPhase | NumDays     | 740.00 | 210.00 |
| tblConstructionPhase | NumDays     | 740.00 | 210.00 |
| tblConstructionPhase | NumDays     | 740.00 | 210.00 |
| tblConstructionPhase | NumDays     | 50.00  | 52.00  |
| tblConstructionPhase | NumDays     | 75.00  | 104.00 |
| tblConstructionPhase | NumDays     | 55.00  | 104.00 |
| tblConstructionPhase | NumDays     | 55.00  | 104.00 |
| tblConstructionPhase | NumDays     | 55.00  | 104.00 |
| tblConstructionPhase | NumDays     | 55.00  | 104.00 |
| tblConstructionPhase | NumDays     | 30.00  | 52.00  |
| tblConstructionPhase | NumDaysWeek | 5.00   | 6.00   |
| tblConstructionPhase | NumDaysWeek | 5.00   | 6.00   |
| tblConstructionPhase | NumDaysWeek | 5.00   | 6.00   |
| tblConstructionPhase | NumDaysWeek | 5.00   | 6.00   |
| tblConstructionPhase | NumDaysWeek | 5.00   | 6.00   |
| tblConstructionPhase | NumDaysWeek | 5.00   | 6.00   |
| tblConstructionPhase | NumDaysWeek | 5.00   | 6.00   |
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| tblConstructionPhase | NumDaysWeek | 5.00   | 6.00   |
| tblConstructionPhase | NumDaysWeek | 5.00   | 6.00   |
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| tblConstructionPhase | NumDaysWeek | 5.00   | 6.00   |
| tblConstructionPhase | NumDaysWeek | 5.00   | 6.00   |
| tblConstructionPhase | NumDaysWeek | 5.00   | 6.00   |

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| tblConstructionPhase | NumDaysWeek                | 5.00       | 6.00       |
|----------------------|----------------------------|------------|------------|
| tblFireplaces        | FireplaceWoodMass          | 1,508.00   | 0.00       |
| tblFireplaces        | NumberGas                  | 81.95      | 149.00     |
| tblFireplaces        | NumberNoFireplace          | 14.90      | 0.00       |
| tblFireplaces        | NumberWood                 | 52.15      | 0.00       |
| tblGrading           | MaterialImported           | 0.00       | 32,000.00  |
| tblLandUse           | LandUseSquareFeet          | 487,000.80 | 487,151.00 |
| tblLandUse           | LandUseSquareFeet          | 356,320.80 | 356,386.00 |
| tblLandUse           | LotAcreage                 | 48.38      | 30.59      |
| tblLandUse           | Population                 | 426.00     | 453.00     |
| tblOffRoadEquipment  | OffRoadEquipmentUnitAmount | 3.00       | 1.00       |
| tblOffRoadEquipment  | OffRoadEquipmentUnitAmount | 2.00       | 1.00       |
| tblOffRoadEquipment  | OffRoadEquipmentUnitAmount | 3.00       | 0.00       |
| tblOffRoadEquipment  | OffRoadEquipmentUnitAmount | 3.00       | 0.00       |
| tblOffRoadEquipment  | OffRoadEquipmentUnitAmount | 3.00       | 0.00       |
| tblOffRoadEquipment  | OffRoadEquipmentUnitAmount | 3.00       | 0.00       |
| tblOffRoadEquipment  | OffRoadEquipmentUnitAmount | 2.00       | 1.00       |
| tblOffRoadEquipment  | OffRoadEquipmentUnitAmount | 2.00       | 1.00       |
| tblOffRoadEquipment  | OffRoadEquipmentUnitAmount | 2.00       | 1.00       |
| tblOffRoadEquipment  | OffRoadEquipmentUnitAmount | 2.00       | 1.00       |
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| tblOffRoadEquipment  | OffRoadEquipmentUnitAmount | 2.00       | 1.00       |
| tblOffRoadEquipment  | OffRoadEquipmentUnitAmount | 2.00       | 1.00       |
| tblOffRoadEquipment  | OffRoadEquipmentUnitAmount | 2.00       | 1.00       |
| tblOffRoadEquipment  | OffRoadEquipmentUnitAmount | 2.00       | 1.00       |
| tblOffRoadEquipment  | OffRoadEquipmentUnitAmount | 2.00       | 1.00       |
| tblOffRoadEquipment  | OffRoadEquipmentUnitAmount | 2.00       | 1.00       |

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|--|--------|
|  |        |

| tblOffRoadEquipment | • OffRoadEquipmentUnitAmount | 2.00 | 1.00  |
|---------------------|------------------------------|------|-------|
| tblOffRoadEquipment | OffRoadEquipmentUnitAmount   | 2.00 | 1.00  |
|                     |                              |      |       |
| tblOffRoadEquipment | OffRoadEquipmentUnitAmount   | 3.00 | 1.00  |
| tblOffRoadEquipment | OffRoadEquipmentUnitAmount   | 2.00 | 1.00  |
| tblOffRoadEquipment | OffRoadEquipmentUnitAmount   | 3.00 | 1.00  |
| tblOffRoadEquipment | OffRoadEquipmentUnitAmount   | 3.00 | 1.00  |
| tblOffRoadEquipment | OffRoadEquipmentUnitAmount   | 3.00 | 1.00  |
| tblOffRoadEquipment | OffRoadEquipmentUnitAmount   | 3.00 | 1.00  |
| tblOffRoadEquipment | OffRoadEquipmentUnitAmount   | 2.00 | 1.00  |
| tblOffRoadEquipment | OffRoadEquipmentUnitAmount   | 4.00 | 2.00  |
| tblOffRoadEquipment | OffRoadEquipmentUnitAmount   | 1.00 | 0.00  |
| tblOffRoadEquipment | OffRoadEquipmentUnitAmount   | 1.00 | 0.00  |
| tblOffRoadEquipment | OffRoadEquipmentUnitAmount   | 1.00 | 0.00  |
| tblOffRoadEquipment | OffRoadEquipmentUnitAmount   | 1.00 | 0.00  |
| tblOffRoadEquipment | UsageHours                   | 8.00 | 10.00 |
| tblOffRoadEquipment | UsageHours                   | 7.00 | 10.00 |
| tblOffRoadEquipment | UsageHours                   | 7.00 | 10.00 |
| tblOffRoadEquipment | UsageHours                   | 7.00 | 10.00 |
| tblOffRoadEquipment | UsageHours                   | 7.00 | 10.00 |
| tblOffRoadEquipment | UsageHours                   | 8.00 | 10.00 |
| tblOffRoadEquipment | UsageHours                   | 8.00 | 10.00 |
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| tblOffRoadEquipment | UsageHours                   | 8.00 | 10.00 |
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| tblOffRoadEquipment | UsageHours                   | 8.00 | 10.00 |
| tblOffRoadEquipment | UsageHours                   | 8.00 | 10.00 |
| tblOffRoadEquipment | UsageHours                   | 8.00 | 10.00 |

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| tblOffRoadEquipment | UsageHours | 8.00 | 10.00 |
|---------------------|------------|------|-------|
| tblOffRoadEquipment | UsageHours | 8.00 | 10.00 |
| tblOffRoadEquipment | UsageHours | 8.00 | 10.00 |
| tblOffRoadEquipment | UsageHours | 8.00 | 10.00 |
| tblOffRoadEquipment | UsageHours | 8.00 | 10.00 |
| tblOffRoadEquipment | UsageHours | 8.00 | 10.00 |
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| tblOffRoadEquipment | UsageHours | 8.00 | 10.00 |
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| tblOffRoadEquipment | UsageHours | 8.00 | 10.00 |
| tblOffRoadEquipment | UsageHours | 8.00 | 10.00 |
| tblOffRoadEquipment | UsageHours | 7.00 | 10.00 |
| tblOffRoadEquipment | UsageHours | 7.00 | 10.00 |
| tblOffRoadEquipment | UsageHours | 7.00 | 10.00 |
| tblOffRoadEquipment | UsageHours | 7.00 | 10.00 |
| tblOffRoadEquipment | UsageHours | 8.00 | 10.00 |
| tblOffRoadEquipment | UsageHours | 8.00 | 10.00 |
| tblOffRoadEquipment | UsageHours | 8.00 | 10.00 |
| tblOffRoadEquipment | UsageHours | 8.00 | 10.00 |
|                     |            |      |       |

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| tblOffRoadEquipment       | UsageHours               | 8.00   | 10.00  |
|---------------------------|--------------------------|--------|--------|
| tblOffRoadEquipment       | UsageHours               | 8.00   | 10.00  |
| tblProjectCharacteristics | CH4IntensityFactor       | 0.029  | 0.014  |
| tblProjectCharacteristics | CO2IntensityFactor       | 641.35 | 298.65 |
| tblProjectCharacteristics | N2OIntensityFactor       | 0.006  | 0.003  |
| tblSolidWaste             | SolidWasteGenerationRate | 199.32 | 187.44 |
| tblTripsAndVMT            | VendorTripNumber         | 0.00   | 1.00   |
| tblTripsAndVMT            | VendorTripNumber         | 0.00   | 1.00   |
| tblTripsAndVMT            | VendorTripNumber         | 154.00 | 1.00   |
| tblTripsAndVMT            | VendorTripNumber         | 0.00   | 1.00   |
| tblTripsAndVMT            | VendorTripNumber         | 0.00   | 1.00   |
| tblTripsAndVMT            | VendorTripNumber         | 154.00 | 1.00   |
| tblTripsAndVMT            | VendorTripNumber         | 0.00   | 1.00   |
| tblTripsAndVMT            | VendorTripNumber         | 0.00   | 1.00   |
| tblTripsAndVMT            | VendorTripNumber         | 0.00   | 1.00   |
| tblTripsAndVMT            | VendorTripNumber         | 0.00   | 1.00   |
| tblTripsAndVMT            | VendorTripNumber         | 154.00 | 1.00   |
| tblTripsAndVMT            | VendorTripNumber         | 0.00   | 1.00   |
| tblTripsAndVMT            | VendorTripNumber         | 0.00   | 1.00   |
| tblTripsAndVMT            | VendorTripNumber         | 154.00 | 1.00   |
| tblTripsAndVMT            | VendorTripNumber         | 0.00   | 1.00   |
| tblTripsAndVMT            | WorkerTripNumber         | 408.00 | 40.00  |
| tblTripsAndVMT            | WorkerTripNumber         | 82.00  | 40.00  |
| tblTripsAndVMT            | WorkerTripNumber         | 408.00 | 40.00  |
| tblTripsAndVMT            | WorkerTripNumber         | 82.00  | 40.00  |
| tblTripsAndVMT            | WorkerTripNumber         | 33.00  | 20.00  |
| tblTripsAndVMT            | WorkerTripNumber         | 408.00 | 40.00  |

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| tblTripsAndVMT     | WorkerTripNumber                     | 82.00        | 40.00        |
|--------------------|--------------------------------------|--------------|--------------|
| tblTripsAndVMT     | WorkerTripNumber                     | 408.00       | 40.00        |
| tblTripsAndVMT     | WorkerTripNumber                     | 82.00        | 40.00        |
| tblVehicleTrips    | CC_TL                                | 7.30         | 0.00         |
| tblVehicleTrips    | CC_TL                                | 7.30         | 0.00         |
| tblVehicleTrips    | CC_TTP                               | 48.00        | 0.00         |
| tblVehicleTrips    | CNW_TL                               | 7.30         | 0.00         |
| tblVehicleTrips    | CNW_TL                               | 7.30         | 0.00         |
| tblVehicleTrips    | CNW_TTP                              | 19.00        | 0.00         |
| tblVehicleTrips    | CW_TL                                | 9.50         | 0.00         |
| tblVehicleTrips    | CW_TL                                | 9.50         | 0.00         |
| tblVehicleTrips    | CW_TTP                               | 33.00        | 0.00         |
| tblVehicleTrips    | DV_TP                                | 28.00        | 0.00         |
| tblVehicleTrips    | HO_TTP                               | 37.20        | 37.00        |
| tblVehicleTrips    | HS_TTP                               | 18.80        | 19.00        |
| tblVehicleTrips    | PB_TP                                | 6.00         | 0.00         |
| tblVehicleTrips    | PR_TP                                | 66.00        | 0.00         |
| tblVehicleTrips    | ST_TR                                | 22.75        | 0.00         |
| tblVehicleTrips    | SU_TR                                | 16.74        | 0.00         |
| tblVehicleTrips    | WD_TR                                | 1.89         | 0.00         |
| tblVehicleTrips    | WD_TR                                | 9.52         | 9.44         |
| tblWater           | IndoorWaterUseRate                   | 9,707,949.82 | 7,766,389.00 |
| tblWaterMitigation | PercentReductionInFlowBathroomFaucet | 32           | 0            |
| tblWaterMitigation | PercentReductionInFlowKitchenFaucet  | 18           | 0            |
| tblWaterMitigation | PercentReductionInFlowShower         | 20           | 0            |
| tblWaterMitigation | PercentReductionInFlowToilet         | 20           | 0            |
| tblWoodstoves      | NumberCatalytic                      | 7.45         | 0.00         |

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| tblWoodstoves | NumberNoncatalytic | 7.45     | 0.00 |
|---------------|--------------------|----------|------|
| tblWoodstoves | WoodstoveDayYear   | 82.00    | 0.00 |
| tblWoodstoves | WoodstoveWoodMass  | 3,120.00 | 0.00 |

# 2.0 Emissions Summary

## 2.1 Overall Construction (Maximum Daily Emission)

#### **Unmitigated Construction**

|         | ROG     | NOx      | СО      | SO2    | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2       | Total CO2       | CH4    | N2O    | CO2e            |
|---------|---------|----------|---------|--------|------------------|-----------------|---------------|-------------------|------------------|-------------|----------|-----------------|-----------------|--------|--------|-----------------|
| Year    |         | lb/day   |         |        |                  |                 |               |                   |                  |             |          |                 | lb/c            | lay    |        |                 |
| 2020    | 12.7677 | 143.6579 | 83.3583 | 0.1883 | 19.6783          | 6.2938          | 25.9721       | 8.9659            | 5.8171           | 14.7830     | 0.0000   | 18,433.36<br>74 | 18,433.36<br>74 | 4.6551 | 0.0000 | 18,549.74<br>38 |
| 2021    | 10.6251 | 53.8134  | 49.6789 | 0.0936 | 0.6707           | 2.6044          | 3.1108        | 0.1782            | 2.4489           | 2.5835      | 0.0000   | 9,003.041<br>5  | 9,003.041<br>5  | 2.1433 | 0.0000 | 9,056.622<br>9  |
| 2022    | 10.2492 | 48.2605  | 49.0755 | 0.0934 | 0.6707           | 2.2736          | 2.7801        | 0.1782            | 2.1379           | 2.2725      | 0.0000   | 8,984.331<br>6  | 8,984.331<br>6  | 2.1327 | 0.0000 | 9,037.650<br>0  |
| 2023    | 10.0389 | 44.3598  | 48.7289 | 0.0932 | 0.6707           | 2.0339          | 2.5403        | 0.1782            | 1.9111           | 2.0457      | 0.0000   | 8,966.523<br>5  | 8,966.523<br>5  | 2.1197 | 0.0000 | 9,019.515<br>3  |
| 2024    | 9.8852  | 41.6320  | 48.4923 | 0.0930 | 0.6707           | 1.8581          | 2.3645        | 0.1782            | 1.7440           | 1.8787      | 0.0000   | 8,948.792<br>2  | 8,948.792<br>2  | 2.1126 | 0.0000 | 9,001.607<br>8  |
| Maximum | 12.7677 | 143.6579 | 83.3583 | 0.1883 | 19.6783          | 6.2938          | 25.9721       | 8.9659            | 5.8171           | 14.7830     | 0.0000   | 18,433.36<br>74 | 18,433.36<br>74 | 4.6551 | 0.0000 | 18,549.74<br>38 |

## Lico Subdivision Project - Monterey Bay Unified APCD Air District, Winter

## 2.1 Overall Construction (Maximum Daily Emission)

#### **Mitigated Construction**

|                      | ROG     | NOx      | CO      | SO2    | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Tota     | Bio- CO2 | NBio- CO2       | Total CO2       | CH4    | N2O    | CO2e            |
|----------------------|---------|----------|---------|--------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|-----------------|-----------------|--------|--------|-----------------|
| Year                 |         | lb/day   |         |        |                  |                 |               |                   |                  |                |          |                 | lb/             | 'day   |        |                 |
| 2020                 | 12.7677 | 143.6579 | 83.3583 | 0.1883 | 19.6783          | 6.2938          | 25.9721       | 8.9659            | 5.8171           | 14.7830        | 0.0000   | 18,433.36<br>74 | 18,433.36<br>74 | 4.6551 | 0.0000 | 18,549.74<br>38 |
| 2021                 | 10.6251 | 53.8134  | 49.6789 | 0.0936 | 0.6707           | 2.6044          | 3.1108        | 0.1782            | 2.4489           | 2.5835         | 0.0000   | 9,003.041<br>5  | 9,003.041<br>5  | 2.1433 | 0.0000 | 9,056.622<br>9  |
| 2022                 | 10.2492 | 48.2605  | 49.0755 | 0.0934 | 0.6707           | 2.2736          | 2.7801        | 0.1782            | 2.1379           | 2.2725         | 0.0000   | 8,984.331<br>6  | 8,984.331<br>6  | 2.1327 | 0.0000 | 9,037.650<br>0  |
| 2023                 | 10.0389 | 44.3598  | 48.7289 | 0.0932 | 0.6707           | 2.0339          | 2.5403        | 0.1782            | 1.9111           | 2.0457         | 0.0000   | 8,966.523<br>5  | 8,966.523<br>5  | 2.1197 | 0.0000 | 9,019.515<br>3  |
| 2024                 | 9.8852  | 41.6320  | 48.4923 | 0.0930 | 0.6707           | 1.8581          | 2.3645        | 0.1782            | 1.7440           | 1.8787         | 0.0000   | 8,948.792<br>1  | 8,948.792<br>1  | 2.1126 | 0.0000 | 9,001.607<br>8  |
| Maximum              | 12.7677 | 143.6579 | 83.3583 | 0.1883 | 19.6783          | 6.2938          | 25.9721       | 8.9659            | 5.8171           | 14.7830        | 0.0000   | 18,433.36<br>74 | 18,433.36<br>74 | 4.6551 | 0.0000 | 18,549.74<br>38 |
|                      | ROG     | NOx      | СО      | SO2    | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5<br>Total | Bio- CO2 | NBio-CO2        | Total CO2       | CH4    | N20    | CO2e            |
| Percent<br>Reduction | 0.00    | 0.00     | 0.00    | 0.00   | 0.00             | 0.00            | 0.00          | 0.00              | 0.00             | 0.00           | 0.00     | 0.00            | 0.00            | 0.00   | 0.00   | 0.00            |

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## Lico Subdivision Project - Monterey Bay Unified APCD Air District, Winter

# 2.2 Overall Operational Unmitigated Operational

|          | ROG    | NOx     | СО      | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2       | Total CO2       | CH4    | N2O    | CO2e            |
|----------|--------|---------|---------|-----------------|------------------|-----------------|---------------|-------------------|------------------|-------------|----------|-----------------|-----------------|--------|--------|-----------------|
| Category |        |         |         |                 | lb/d             | day             |               |                   |                  |             |          |                 | lb/d            | lay    |        |                 |
| Area     | 7.0854 | 2.6131  | 13.3348 | 0.0164          |                  | 0.2680          | 0.2680        |                   | 0.2680           | 0.2680      | 0.0000   | 3,177.432<br>7  | 3,177.432<br>7  | 0.0817 | 0.0579 | 3,196.713<br>2  |
| Energy   | 0.1280 | 1.0934  | 0.4653  | 6.9800e-<br>003 |                  | 0.0884          | 0.0884        |                   | 0.0884           | 0.0884      |          | 1,395.873<br>8  | 1,395.873<br>8  | 0.0268 | 0.0256 | 1,404.168<br>8  |
| Mobile   | 2.5633 | 13.7673 | 31.5154 | 0.1052          | 9.0612           | 0.0869          | 9.1481        | 2.4261            | 0.0811           | 2.5072      |          | 10,674.03<br>04 | 10,674.03<br>04 | 0.4941 | <br>   | 10,686.38<br>30 |
| Total    | 9.7767 | 17.4739 | 45.3155 | 0.1286          | 9.0612           | 0.4433          | 9.5045        | 2.4261            | 0.4375           | 2.8636      | 0.0000   | 15,247.33<br>68 | 15,247.33<br>68 | 0.6025 | 0.0834 | 15,287.26<br>49 |

## **Mitigated Operational**

|          | ROG    | NOx     | СО      | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2       | Total CO2       | CH4    | N2O    | CO2e            |
|----------|--------|---------|---------|-----------------|------------------|-----------------|---------------|-------------------|------------------|-------------|----------|-----------------|-----------------|--------|--------|-----------------|
| Category |        |         |         |                 | lb/d             | day             |               |                   |                  |             |          |                 | lb/d            | day    |        |                 |
| Area     | 7.0854 | 2.6131  | 13.3348 | 0.0164          |                  | 0.2680          | 0.2680        |                   | 0.2680           | 0.2680      | 0.0000   | 3,177.432<br>7  | 3,177.432<br>7  | 0.0817 | 0.0579 | 3,196.713<br>2  |
| Energy   | 0.1200 | 1.0252  | 0.4363  | 6.5400e-<br>003 |                  | 0.0829          | 0.0829        |                   | 0.0829           | 0.0829      |          | 1,308.769<br>1  | 1,308.769<br>1  | 0.0251 | 0.0240 | 1,316.546<br>5  |
| Mobile   | 2.5633 | 13.7673 | 31.5154 | 0.1052          | 9.0612           | 0.0869          | 9.1481        | 2.4261            | 0.0811           | 2.5072      |          | 10,674.03<br>04 | 10,674.03<br>04 | 0.4941 |        | 10,686.38<br>30 |
| Total    | 9.7687 | 17.4057 | 45.2865 | 0.1282          | 9.0612           | 0.4378          | 9.4990        | 2.4261            | 0.4320           | 2.8581      | 0.0000   | 15,160.23<br>22 | 15,160.23<br>22 | 0.6009 | 0.0818 | 15,199.64<br>26 |

#### Lico Subdivision Project - Monterey Bay Unified APCD Air District, Winter

|                      | ROG  | NOx  | СО   | SO2  | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5<br>Total | Bio- CO2 | NBio-CO2 | Total CO2 | CH4  | N20  | CO2e |
|----------------------|------|------|------|------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|----------|-----------|------|------|------|
| Percent<br>Reduction | 0.08 | 0.39 | 0.06 | 0.34 | 0.00             | 1.25            | 0.06          | 0.00              | 1.26             | 0.19           | 0.00     | 0.57     | 0.57      | 0.28 | 1.92 | 0.57 |

#### 3.0 Construction Detail

#### **Construction Phase**

| Phase<br>Number | Phase Name                        | Phase Type            | Start Date | End Date   | Num Days<br>Week | Num Days | Phase Description |
|-----------------|-----------------------------------|-----------------------|------------|------------|------------------|----------|-------------------|
| 1               | Demolition                        | Demolition            | 8/1/2020   | 9/30/2020  | 6                | 52       |                   |
| 2               | Site Preparation                  | Site Preparation      | 8/1/2020   | 9/30/2020  | 6                | 52       |                   |
| 3               | Grading                           | Grading               | 8/1/2020   | 11/30/2020 | 6                | 104      |                   |
| 4               | Paving - Phase I                  | Paving                | 12/1/2020  | 3/31/2021  | 6                | 104      |                   |
| 5               | Building Construction - Phase I   | Building Construction | 3/1/2021   | 10/31/2021 | 6                | 210      |                   |
| 6               | Architectural Coating - Phase I   | Architectural Coating | 8/1/2021   | 10/31/2021 | 6                | 78       |                   |
| 7               | Paving - Phase II                 | Paving                | 12/1/2021  | 3/31/2022  | 6                | 104      |                   |
| 8               | Building Construction - Phase II  | Building Construction | 3/1/2022   | 10/31/2022 | 6                | 210      |                   |
| 9               | Architectural Coating - Phase II  | Architectural Coating | 8/1/2022   | 10/31/2022 | 6                | 79       |                   |
| 10              | Paving - Phase III                | Paving                | 12/1/2022  | 3/31/2023  | 6                | 104      |                   |
| 11              | Building Construction - Phase III | Building Construction | 3/1/2023   | 10/31/2023 | 6                | 210      |                   |
| 12              | Architectural Coating - Phase III | Architectural Coating | 8/1/2023   | 10/31/2023 | 6                | 79       |                   |
| 13              | Paving - Phase IV                 | Paving                | 12/1/2023  | 3/31/2024  | 6                | 104      |                   |
| 14              | Building Construction - Phase IV  | Building Construction | 3/1/2024   | 10/31/2024 | 6                | 210      |                   |
| 15              | Architectural Coating - Phase IV  | Architectural Coating | 8/1/2024   | 10/31/2024 | 6                | 79       |                   |

Acres of Grading (Site Preparation Phase): 32.5

Acres of Grading (Grading Phase): 260

Acres of Paving: 11.18

#### Lico Subdivision Project - Monterey Bay Unified APCD Air District, Winter

Residential Indoor: 135,776; Residential Outdoor: 45,259; Non-Residential Indoor: 0; Non-Residential Outdoor: 0; Striped Parking Area: 29,229 (Architectural Coating – sqft)

#### OffRoad Equipment

| Phase Name       | Offroad Equipment Type       | Amount | Usage Hours | Horse Power | Load Factor |
|------------------|------------------------------|--------|-------------|-------------|-------------|
| Demolition       | Concrete/Industrial Saws     | 1      | 10.00       | 81          | 0.73        |
| Demolition       | Excavators                   | 1      | 10.00       | 158         | 0.38        |
| Demolition       | Other Construction Equipment | 1      | 10.00       | 172         | 0.42        |
| Demolition       | Rubber Tired Dozers          | 1      | 10.00       | 247         | 0.40        |
| Demolition       | Signal Boards                | 1      | 10.00       | 6           | 0.82        |
| Demolition       | Tractors/Loaders/Backhoes    | 2      | 10.00       | 97          | 0.37        |
| Site Preparation | Crawler Tractors             | 1      | 10.00       | 212         | 0.43        |
| Site Preparation | Rubber Tired Dozers          | 1      | 10.00       | 247         | 0.40        |
| Site Preparation | Signal Boards                | 1      | 10.00       | 6           | 0.82        |
| Site Preparation | Tractors/Loaders/Backhoes    | 2      | 10.00       | 97          | 0.37        |
| Grading          | Crawler Tractors             | 1      | 10.00       | 212         | 0.43        |
| Grading          | Excavators                   | 1      | 10.00       | 158         | 0.38        |
| Grading          | Graders                      | 1      | 10.00       | 187         | 0.41        |
| Grading          | Plate Compactors             | 1      | 10.00       | 8           | 0.43        |
| Grading          | Rollers                      | 1      | 10.00       | 80          | 0.38        |
| Grading          | Rough Terrain Forklifts      | 1      | 10.00       | 100         | 0.40        |
| Grading          | Rubber Tired Dozers          | 1      | 10.00       | 247         | 0.40        |
| Grading          | Rubber Tired Loaders         | 1      | 10.00       | 203         | 0.36        |
| Grading          | Scrapers                     | 1      | 10.00       | 367         | 0.48        |
| Grading          | Signal Boards                | 1      | 10.00       | 6           | 0.82        |
| Grading          | Skid Steer Loaders           | 1      | 10.00       | 65          | 0.37        |
| Grading          | Tractors/Loaders/Backhoes    | 1      | 10.00       | 97          | 0.37        |

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## Lico Subdivision Project - Monterey Bay Unified APCD Air District, Winter

| Grading                         | Trenchers                    | 1 | 10.00 | 78  | 0.50 |
|---------------------------------|------------------------------|---|-------|-----|------|
| Paving - Phase I                | Concrete/Industrial Saws     | 1 | 10.00 | 81  | 0.73 |
| Paving - Phase I                | Graders                      | 1 | 10.00 | 187 | 0.41 |
| Paving - Phase I                | Pavers                       | 1 | 10.00 | 130 | 0.42 |
| Paving - Phase I                | Paving Equipment             | 1 | 10.00 | 132 | 0.36 |
| Paving - Phase I                | Rollers                      | 1 | 10.00 | 80  | 0.38 |
| Paving - Phase I                | Signal Boards                | 1 | 10.00 | 6   | 0.82 |
| Paving - Phase I                | Skid Steer Loaders           | 1 | 10.00 | 65  | 0.37 |
| Paving - Phase I                | Surfacing Equipment          | 1 | 10.00 | 263 | 0.30 |
| Building Construction - Phase I | Concrete/Industrial Saws     | 1 | 10.00 | 81  | 0.73 |
| Building Construction - Phase I | Cranes                       | 1 | 10.00 | 231 | 0.29 |
| Building Construction - Phase I | Forklifts                    | 0 | 10.00 | 89  | 0.20 |
| Building Construction - Phase I | Generator Sets               | 1 | 10.00 | 84  | 0.74 |
| Building Construction - Phase I | Other Construction Equipment | 1 | 10.00 | 172 | 0.42 |
| Building Construction - Phase I | Rough Terrain Forklifts      | 1 | 10.00 | 100 | 0.40 |
| Building Construction - Phase I | Skid Steer Loaders           | 1 | 10.00 | 65  | 0.37 |
| Building Construction - Phase I | Tractors/Loaders/Backhoes    | 1 | 10.00 | 97  | 0.37 |
| Building Construction - Phase I | Trenchers                    | 1 | 10.00 | 78  | 0.50 |
| Building Construction - Phase I | Welders                      | 0 | 10.00 | 46  | 0.45 |
| Architectural Coating - Phase I | Air Compressors              | 1 | 6.00  | 78  | 0.48 |
| Paving - Phase II               | Concrete/Industrial Saws     | 1 | 10.00 | 81  | 0.73 |
| Paving - Phase II               | Graders                      | 1 | 10.00 | 187 | 0.41 |
| Paving - Phase II               | Pavers                       | 1 | 10.00 | 130 | 0.42 |
| Paving - Phase II               | Paving Equipment             | 1 | 10.00 | 132 | 0.36 |
| Paving - Phase II               | Rollers                      | 1 | 10.00 | 80  | 0.38 |
| Paving - Phase II               | Signal Boards                | 1 | 10.00 | 6   | 0.82 |
| Paving - Phase II               | Skid Steer Loaders           | 1 | 10.00 | 65  | 0.37 |

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## Lico Subdivision Project - Monterey Bay Unified APCD Air District, Winter

| Paving - Phase II                 | Surfacing Equipment          | 1 | 10.00 | 263 | 0.30 |
|-----------------------------------|------------------------------|---|-------|-----|------|
| Building Construction - Phase II  | Concrete/Industrial Saws     | 1 | 10.00 | 81  | 0.73 |
| Building Construction - Phase II  | Cranes                       | 1 | 10.00 | 231 | 0.29 |
| Building Construction - Phase II  | Forklifts                    | 0 | 10.00 | 89  | 0.20 |
| Building Construction - Phase II  | Generator Sets               | 1 | 10.00 | 84  | 0.74 |
| Building Construction - Phase II  | Other Construction Equipment | 1 | 10.00 | 172 | 0.42 |
| Building Construction - Phase II  | Rough Terrain Forklifts      | 1 | 10.00 | 100 | 0.40 |
| Building Construction - Phase II  | Skid Steer Loaders           | 1 | 10.00 | 65  | 0.37 |
| Building Construction - Phase II  | Tractors/Loaders/Backhoes    | 1 | 10.00 | 97  | 0.37 |
| Building Construction - Phase II  | Trenchers                    | 1 | 10.00 | 78  | 0.50 |
| Building Construction - Phase II  | Welders                      | 0 | 10.00 | 46  | 0.45 |
| Architectural Coating - Phase II  | Air Compressors              | 1 | 6.00  | 78  | 0.48 |
| Paving - Phase III                | Concrete/Industrial Saws     | 1 | 10.00 | 81  | 0.73 |
| Paving - Phase III                | Graders                      | 1 | 10.00 | 187 | 0.41 |
| Paving - Phase III                | Pavers                       | 1 | 10.00 | 130 | 0.42 |
| Paving - Phase III                | Paving Equipment             | 1 | 10.00 | 132 | 0.36 |
| Paving - Phase III                | Rollers                      | 1 | 10.00 | 80  | 0.38 |
| Paving - Phase III                | Signal Boards                | 1 | 10.00 | 6   | 0.82 |
| Paving - Phase III                | Skid Steer Loaders           | 1 | 10.00 | 65  | 0.37 |
| Paving - Phase III                | Surfacing Equipment          | 1 | 10.00 | 263 | 0.30 |
| Building Construction - Phase III | Concrete/Industrial Saws     | 1 | 10.00 | 81  | 0.73 |
| Building Construction - Phase III | Cranes                       | 1 | 10.00 | 231 | 0.29 |
| Building Construction - Phase III | Forklifts                    | 0 | 10.00 | 89  | 0.20 |
| Building Construction - Phase III | Generator Sets               | 1 | 10.00 | 84  | 0.74 |
| Building Construction - Phase III | Other Construction Equipment | 1 | 10.00 | 172 | 0.42 |
| Building Construction - Phase III | Rough Terrain Forklifts      | 1 | 10.00 | 100 | 0.40 |
| Building Construction - Phase III | Skid Steer Loaders           | 1 | 10.00 | 65  | 0.37 |

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Lico Subdivision Project - Monterey Bay Unified APCD Air District, Winter

| Building Construction - Phase III | Tractors/Loaders/Backhoes    | 1 | 10.00 | 97  | 0.37 |
|-----------------------------------|------------------------------|---|-------|-----|------|
| Building Construction - Phase III | Trenchers                    | 1 | 10.00 | 78  | 0.50 |
| Building Construction - Phase III | Welders                      | 0 | 10.00 | 46  | 0.45 |
| Architectural Coating - Phase III | Air Compressors              | 1 | 6.00  | 78  | 0.48 |
| Paving - Phase IV                 | Concrete/Industrial Saws     | 1 | 10.00 | 81  | 0.73 |
| Paving - Phase IV                 | Graders                      | 1 | 10.00 | 187 | 0.41 |
| Paving - Phase IV                 | Pavers                       | 1 | 10.00 | 130 | 0.42 |
| Paving - Phase IV                 | Paving Equipment             | 1 | 10.00 | 132 | 0.36 |
| Paving - Phase IV                 | Rollers                      | 1 | 10.00 | 80  | 0.38 |
| Paving - Phase IV                 | Signal Boards                | 1 | 10.00 | 6   | 0.82 |
| Paving - Phase IV                 | Skid Steer Loaders           | 1 | 10.00 | 65  | 0.37 |
| Paving - Phase IV                 | Surfacing Equipment          | 1 | 10.00 | 263 | 0.30 |
| Building Construction - Phase IV  | Concrete/Industrial Saws     | 1 | 10.00 | 81  | 0.73 |
| Building Construction - Phase IV  | Cranes                       | 1 | 10.00 | 231 | 0.29 |
| Building Construction - Phase IV  | Forklifts                    | 0 | 10.00 | 89  | 0.20 |
| Building Construction - Phase IV  | Generator Sets               | 1 | 10.00 | 84  | 0.74 |
| Building Construction - Phase IV  | Other Construction Equipment | 1 | 10.00 | 172 | 0.42 |
| Building Construction - Phase IV  | Rough Terrain Forklifts      | 1 | 10.00 | 100 | 0.40 |
| Building Construction - Phase IV  | Skid Steer Loaders           | 1 | 10.00 | 65  | 0.37 |
| Building Construction - Phase IV  | Tractors/Loaders/Backhoes    | 1 | 10.00 | 97  | 0.37 |
| Building Construction - Phase IV  | Trenchers                    | 1 | 10.00 | 78  | 0.50 |
| Building Construction - Phase IV  | Welders                      | 0 | 10.00 | 46  | 0.45 |
| Architectural Coating - Phase IV  | Air Compressors              | 1 | 6.00  | 78  | 0.48 |
|                                   |                              |   |       |     |      |

**Trips and VMT** 

Lico Subdivision Project - Monterey Bay Unified APCD Air District, Winter

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| Phase Name              | Offroad Equipment<br>Count | Worker Trip<br>Number | Vendor Trip<br>Number | Hauling Trip<br>Number | Worker Trip<br>Length | Vendor Trip<br>Length | Hauling Trip<br>Length | Worker Vehicle<br>Class | Vendor<br>Vehicle Class | Hauling<br>Vehicle Class |
|-------------------------|----------------------------|-----------------------|-----------------------|------------------------|-----------------------|-----------------------|------------------------|-------------------------|-------------------------|--------------------------|
| Demolition              | 7                          | 18.00                 | 1.00                  | 33.00                  | 10.80                 | 7.30                  | 20.00                  | LD_Mix                  | HDT_Mix                 | HHDT                     |
| Site Preparation        | 5                          | 13.00                 | 1.00                  | 0.00                   | 10.80                 | 7.30                  | 20.00                  | LD_Mix                  | HDT_Mix                 | HHDT                     |
| Grading                 | 13                         | 20.00                 | 1.00                  | 4,000.00               | 10.80                 | 7.30                  | 20.00                  | LD_Mix                  | HDT_Mix                 | HHDT                     |
| Paving - Phase I        | 8                          | 20.00                 | 1.00                  | 0.00                   | 10.80                 | 7.30                  | 20.00                  | LD_Mix                  | HDT_Mix                 | HHDT                     |
| Building Construction - | 8                          | 40.00                 | 1.00                  | 0.00                   | 10.80                 | 7.30                  | 20.00                  | LD_Mix                  | HDT_Mix                 | HHDT                     |
| Architectural Coating - | 1                          | 40.00                 | 1.00                  | 0.00                   | 10.80                 | 7.30                  | 20.00                  | LD_Mix                  | HDT_Mix                 | HHDT                     |
| Paving - Phase II       | 8                          | 20.00                 | 1.00                  | 0.00                   | 10.80                 | 7.30                  | 20.00                  | LD_Mix                  | HDT_Mix                 | HHDT                     |
| Building Construction - | 8                          | 40.00                 | 1.00                  | 0.00                   | 10.80                 | 7.30                  | 20.00                  | LD_Mix                  | HDT_Mix                 | HHDT                     |
| Architectural Coating - | 1                          | 40.00                 | 1.00                  | 0.00                   | 10.80                 | 7.30                  | 20.00                  | LD_Mix                  | HDT_Mix                 | HHDT                     |
| Paving - Phase III      | 8                          | 20.00                 | 1.00                  | 0.00                   | 10.80                 | 7.30                  | 20.00                  | LD_Mix                  | HDT_Mix                 | HHDT                     |
| Building Construction - | 8                          | 40.00                 | 1.00                  | 0.00                   | 10.80                 | 7.30                  | 20.00                  | LD_Mix                  | HDT_Mix                 | HHDT                     |
| Architectural Coating - | 1                          | 40.00                 | 1.00                  | 0.00                   | 10.80                 | 7.30                  | 20.00                  | LD_Mix                  | HDT_Mix                 | HHDT                     |
| Paving - Phase IV       | 8                          | 20.00                 | 1.00                  | 0.00                   | 10.80                 | 7.30                  | 20.00                  | LD_Mix                  | HDT_Mix                 | HHDT                     |
| Building Construction - | 8                          | 40.00                 | 1.00                  | 0.00                   | 10.80                 | 7.30                  | 20.00                  | LD_Mix                  | HDT_Mix                 | HHDT                     |
| Architectural Coating - | 1                          | 40.00                 | 1.00                  | 0.00                   | 10.80                 | 7.30                  | 20.00                  | LD_Mix                  | HDT_Mix                 | HHDT                     |

# **3.1 Mitigation Measures Construction**

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## Lico Subdivision Project - Monterey Bay Unified APCD Air District, Winter

3.2 Demolition - 2020
Unmitigated Construction On-Site

|               | ROG    | NOx     | CO      | SO2    | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2      | Total CO2      | CH4    | N2O | CO2e           |
|---------------|--------|---------|---------|--------|------------------|-----------------|---------------|-------------------|------------------|-------------|----------|----------------|----------------|--------|-----|----------------|
| Category      |        |         |         |        | lb/d             | day             |               |                   |                  |             |          |                | lb/d           | day    |     |                |
| Fugitive Dust |        |         |         |        | 0.1389           | 0.0000          | 0.1389        | 0.0210            | 0.0000           | 0.0210      |          | !<br>!         | 0.0000         |        |     | 0.0000         |
| Off-Road      | 3.3913 | 33.5654 | 25.0856 | 0.0413 |                  | 1.7833          | 1.7833        |                   | 1.6619           | 1.6619      |          | 3,962.225<br>3 | 3,962.225<br>3 | 1.0753 |     | 3,989.106<br>7 |
| Total         | 3.3913 | 33.5654 | 25.0856 | 0.0413 | 0.1389           | 1.7833          | 1.9222        | 0.0210            | 1.6619           | 1.6829      |          | 3,962.225<br>3 | 3,962.225      | 1.0753 |     | 3,989.106<br>7 |

|          | ROG             | NOx    | СО     | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total   | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5<br>Total  | Bio- CO2 | NBio- CO2 | Total CO2 | CH4             | N2O | CO2e     |
|----------|-----------------|--------|--------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|-----|----------|
| Category |                 |        |        |                 | lb/              | day             |                 |                   |                  |                 |          |           | lb/d      | day             |     |          |
| Hauling  | 5.3900e-<br>003 | 0.1863 | 0.0348 | 5.1000e-<br>004 | 0.0111           | 7.4000e-<br>004 | 0.0118          | 3.0400e-<br>003   | 7.1000e-<br>004  | 3.7500e-<br>003 |          | 53.4578   | 53.4578   | 2.2900e-<br>003 |     | 53.5150  |
| Vendor   | 4.6700e-<br>003 | 0.1247 | 0.0346 | 2.8000e-<br>004 | 6.7700e-<br>003  | 7.1000e-<br>004 | 7.4800e-<br>003 | 1.9500e-<br>003   | 6.8000e-<br>004  | 2.6300e-<br>003 |          | 29.5633   | 29.5633   | 1.7200e-<br>003 |     | 29.6064  |
| Worker   | 0.0860          | 0.0785 | 0.6664 | 1.4700e-<br>003 | 0.1479           | 1.2300e-<br>003 | 0.1491          | 0.0392            | 1.1300e-<br>003  | 0.0404          |          | 145.8918  | 145.8918  | 6.1500e-<br>003 |     | 146.0456 |
| Total    | 0.0961          | 0.3895 | 0.7358 | 2.2600e-<br>003 | 0.1657           | 2.6800e-<br>003 | 0.1684          | 0.0442            | 2.5200e-<br>003  | 0.0467          |          | 228.9129  | 228.9129  | 0.0102          |     | 229.1670 |

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## Lico Subdivision Project - Monterey Bay Unified APCD Air District, Winter

3.2 Demolition - 2020 <u>Mitigated Construction On-Site</u>

|               | ROG    | NOx     | СО      | SO2    | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2      | Total CO2      | CH4    | N2O | CO2e           |
|---------------|--------|---------|---------|--------|------------------|-----------------|---------------|-------------------|------------------|-------------|----------|----------------|----------------|--------|-----|----------------|
| Category      |        |         |         |        | lb/d             | day             |               |                   |                  |             |          |                | lb/c           | day    |     |                |
| Fugitive Dust |        |         |         |        | 0.1389           | 0.0000          | 0.1389        | 0.0210            | 0.0000           | 0.0210      |          |                | 0.0000         |        |     | 0.0000         |
| Off-Road      | 3.3913 | 33.5654 | 25.0856 | 0.0413 |                  | 1.7833          | 1.7833        |                   | 1.6619           | 1.6619      | 0.0000   | 3,962.225<br>3 | 3,962.225<br>3 | 1.0753 |     | 3,989.106<br>7 |
| Total         | 3.3913 | 33.5654 | 25.0856 | 0.0413 | 0.1389           | 1.7833          | 1.9222        | 0.0210            | 1.6619           | 1.6829      | 0.0000   | 3,962.225<br>3 | 3,962.225      | 1.0753 |     | 3,989.106<br>7 |

|          | ROG             | NOx    | CO     | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total   | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total     | Bio- CO2 | NBio- CO2 | Total CO2 | CH4             | N2O | CO2e     |
|----------|-----------------|--------|--------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|-----|----------|
| Category |                 |        |        |                 | lb/              | day             |                 |                   |                  |                 |          |           | lb/d      | day             |     |          |
| Hauling  | 5.3900e-<br>003 | 0.1863 | 0.0348 | 5.1000e-<br>004 | 0.0111           | 7.4000e-<br>004 | 0.0118          | 3.0400e-<br>003   | 7.1000e-<br>004  | 3.7500e-<br>003 |          | 53.4578   | 53.4578   | 2.2900e-<br>003 |     | 53.5150  |
| Vendor   | 4.6700e-<br>003 | 0.1247 | 0.0346 | 2.8000e-<br>004 | 6.7700e-<br>003  | 7.1000e-<br>004 | 7.4800e-<br>003 | 1.9500e-<br>003   | 6.8000e-<br>004  | 2.6300e-<br>003 |          | 29.5633   | 29.5633   | 1.7200e-<br>003 |     | 29.6064  |
| Worker   | 0.0860          | 0.0785 | 0.6664 | 1.4700e-<br>003 | 0.1479           | 1.2300e-<br>003 | 0.1491          | 0.0392            | 1.1300e-<br>003  | 0.0404          |          | 145.8918  | 145.8918  | 6.1500e-<br>003 |     | 146.0456 |
| Total    | 0.0961          | 0.3895 | 0.7358 | 2.2600e-<br>003 | 0.1657           | 2.6800e-<br>003 | 0.1684          | 0.0442            | 2.5200e-<br>003  | 0.0467          |          | 228.9129  | 228.9129  | 0.0102          |     | 229.1670 |

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## Lico Subdivision Project - Monterey Bay Unified APCD Air District, Winter

3.3 Site Preparation - 2020

<u>Unmitigated Construction On-Site</u>

|               | ROG    | NOx     | CO      | SO2    | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2      | Total CO2      | CH4    | N2O | CO2e           |
|---------------|--------|---------|---------|--------|------------------|-----------------|---------------|-------------------|------------------|-------------|----------|----------------|----------------|--------|-----|----------------|
| Category      |        |         |         |        | lb/d             | day             |               |                   |                  |             |          |                | lb/c           | day    |     |                |
| Fugitive Dust |        |         |         |        | 8.1904           | 0.0000          | 8.1904        | 4.2094            | 0.0000           | 4.2094      |          |                | 0.0000         |        |     | 0.0000         |
| Off-Road      | 2.6684 | 29.1870 | 14.3650 | 0.0291 |                  | 1.3948          | 1.3948        |                   | 1.2846           | 1.2846      |          | 2,798.226<br>9 | 2,798.226<br>9 | 0.8915 |     | 2,820.513<br>5 |
| Total         | 2.6684 | 29.1870 | 14.3650 | 0.0291 | 8.1904           | 1.3948          | 9.5852        | 4.2094            | 1.2846           | 5.4940      |          | 2,798.226<br>9 | 2,798.226<br>9 | 0.8915 |     | 2,820.513<br>5 |

|          | ROG             | NOx    | СО     | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total   | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total     | Bio- CO2 | NBio- CO2 | Total CO2 | CH4             | N2O | CO2e     |
|----------|-----------------|--------|--------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|-----|----------|
| Category |                 |        |        |                 | lb/              | day             |                 |                   |                  |                 |          |           | lb/d      | day             |     |          |
| Hauling  | 0.0000          | 0.0000 | 0.0000 | 0.0000          | 0.0000           | 0.0000          | 0.0000          | 0.0000            | 0.0000           | 0.0000          |          | 0.0000    | 0.0000    | 0.0000          |     | 0.0000   |
| Vendor   | 4.6700e-<br>003 | 0.1247 | 0.0346 | 2.8000e-<br>004 | 6.7700e-<br>003  | 7.1000e-<br>004 | 7.4800e-<br>003 | 1.9500e-<br>003   | 6.8000e-<br>004  | 2.6300e-<br>003 |          | 29.5633   | 29.5633   | 1.7200e-<br>003 |     | 29.6064  |
| Worker   | 0.0621          | 0.0567 | 0.4813 | 1.0600e-<br>003 | 0.1068           | 8.9000e-<br>004 | 0.1077          | 0.0283            | 8.2000e-<br>004  | 0.0292          |          | 105.3663  | 105.3663  | 4.4400e-<br>003 |     | 105.4774 |
| Total    | 0.0668          | 0.1814 | 0.5159 | 1.3400e-<br>003 | 0.1136           | 1.6000e-<br>003 | 0.1152          | 0.0303            | 1.5000e-<br>003  | 0.0318          |          | 134.9296  | 134.9296  | 6.1600e-<br>003 |     | 135.0837 |

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## Lico Subdivision Project - Monterey Bay Unified APCD Air District, Winter

3.3 Site Preparation - 2020 Mitigated Construction On-Site

|               | ROG    | NOx     | CO      | SO2    | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2      | Total CO2      | CH4    | N2O            | CO2e           |
|---------------|--------|---------|---------|--------|------------------|-----------------|---------------|-------------------|------------------|-------------|----------|----------------|----------------|--------|----------------|----------------|
| Category      |        |         |         |        | lb/d             | day             |               |                   |                  |             |          |                | lb/c           | lay    |                |                |
| Fugitive Dust |        |         |         |        | 8.1904           | 0.0000          | 8.1904        | 4.2094            | 0.0000           | 4.2094      |          | 1              | 0.0000         |        |                | 0.0000         |
| Off-Road      | 2.6684 | 29.1870 | 14.3650 | 0.0291 |                  | 1.3948          | 1.3948        |                   | 1.2846           | 1.2846      | 0.0000   | 2,798.226<br>9 | 2,798.226<br>9 | 0.8915 | <br> <br> <br> | 2,820.513<br>5 |
| Total         | 2.6684 | 29.1870 | 14.3650 | 0.0291 | 8.1904           | 1.3948          | 9.5852        | 4.2094            | 1.2846           | 5.4940      | 0.0000   | 2,798.226<br>9 | 2,798.226<br>9 | 0.8915 |                | 2,820.513<br>5 |

|          | ROG             | NOx    | СО     | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total   | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total     | Bio- CO2 | NBio- CO2 | Total CO2 | CH4             | N2O                 | CO2e     |
|----------|-----------------|--------|--------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|---------------------|----------|
| Category |                 |        |        |                 | lb/d             | day             |                 |                   |                  |                 |          |           | lb/d      | day             |                     |          |
| Hauling  | 0.0000          | 0.0000 | 0.0000 | 0.0000          | 0.0000           | 0.0000          | 0.0000          | 0.0000            | 0.0000           | 0.0000          |          | 0.0000    | 0.0000    | 0.0000          |                     | 0.0000   |
| Vendor   | 4.6700e-<br>003 | 0.1247 | 0.0346 | 2.8000e-<br>004 | 6.7700e-<br>003  | 7.1000e-<br>004 | 7.4800e-<br>003 | 1.9500e-<br>003   | 6.8000e-<br>004  | 2.6300e-<br>003 |          | 29.5633   | 29.5633   | 1.7200e-<br>003 | <br> <br> <br> <br> | 29.6064  |
| Worker   | 0.0621          | 0.0567 | 0.4813 | 1.0600e-<br>003 | 0.1068           | 8.9000e-<br>004 | 0.1077          | 0.0283            | 8.2000e-<br>004  | 0.0292          |          | 105.3663  | 105.3663  | 4.4400e-<br>003 | <br> <br> <br> <br> | 105.4774 |
| Total    | 0.0668          | 0.1814 | 0.5159 | 1.3400e-<br>003 | 0.1136           | 1.6000e-<br>003 | 0.1152          | 0.0303            | 1.5000e-<br>003  | 0.0318          |          | 134.9296  | 134.9296  | 6.1600e-<br>003 |                     | 135.0837 |

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## Lico Subdivision Project - Monterey Bay Unified APCD Air District, Winter

3.4 Grading - 2020
Unmitigated Construction On-Site

|               | ROG    | NOx     | СО      | SO2    | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2      | Total CO2      | CH4    | N2O | CO2e           |
|---------------|--------|---------|---------|--------|------------------|-----------------|---------------|-------------------|------------------|-------------|----------|----------------|----------------|--------|-----|----------------|
| Category      |        |         |         |        | lb/d             | day             |               |                   |                  |             |          |                | lb/d           | day    |     |                |
| Fugitive Dust |        |         |         |        | 10.2265          | 0.0000          | 10.2265       | 4.4313            | 0.0000           | 4.4313      |          | !<br>!         | 0.0000         |        |     | 0.0000         |
| Off-Road      | 6.1180 | 68.8321 | 39.7696 | 0.0817 |                  | 3.0645          | 3.0645        |                   | 2.8217           | 2.8217      |          | 7,877.540<br>3 | 7,877.540<br>3 | 2.5248 |     | 7,940.659<br>2 |
| Total         | 6.1180 | 68.8321 | 39.7696 | 0.0817 | 10.2265          | 3.0645          | 13.2910       | 4.4313            | 2.8217           | 7.2530      |          | 7,877.540<br>3 | 7,877.540<br>3 | 2.5248 |     | 7,940.659<br>2 |

|          | ROG             | NOx     | СО     | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total   | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5<br>Total  | Bio- CO2 | NBio- CO2      | Total CO2      | CH4             | N2O | CO2e           |
|----------|-----------------|---------|--------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|----------------|----------------|-----------------|-----|----------------|
| Category |                 |         |        |                 | lb/              | day             |                 |                   |                  |                 |          |                | lb/d           | day             |     |                |
| Hauling  | 0.3269          | 11.2907 | 2.1115 | 0.0307          | 0.6722           | 0.0449          | 0.7170          | 0.1842            | 0.0429           | 0.2272          |          | 3,239.867<br>1 | 3,239.867<br>1 | 0.1387          |     | 3,243.334<br>5 |
| Vendor   | 4.6700e-<br>003 | 0.1247  | 0.0346 | 2.8000e-<br>004 | 6.7700e-<br>003  | 7.1000e-<br>004 | 7.4800e-<br>003 | 1.9500e-<br>003   | 6.8000e-<br>004  | 2.6300e-<br>003 |          | 29.5633        | 29.5633        | 1.7200e-<br>003 |     | 29.6064        |
| Worker   | 0.0956          | 0.0872  | 0.7405 | 1.6300e-<br>003 | 0.1643           | 1.3700e-<br>003 | 0.1657          | 0.0436            | 1.2600e-<br>003  | 0.0448          |          | 162.1020       | 162.1020       | 6.8300e-<br>003 |     | 162.2729       |
| Total    | 0.4272          | 11.5026 | 2.8865 | 0.0326          | 0.8432           | 0.0470          | 0.8902          | 0.2297            | 0.0449           | 0.2746          |          | 3,431.532<br>4 | 3,431.532<br>4 | 0.1473          |     | 3,435.213<br>7 |

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## Lico Subdivision Project - Monterey Bay Unified APCD Air District, Winter

3.4 Grading - 2020

Mitigated Construction On-Site

|               | ROG    | NOx     | CO      | SO2    | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5<br>Total | Bio- CO2 | NBio- CO2      | Total CO2      | CH4    | N2O                 | CO2e           |
|---------------|--------|---------|---------|--------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|----------------|----------------|--------|---------------------|----------------|
| Category      |        |         |         |        | lb/d             | day             |               |                   |                  |                |          |                | lb/d           | day    |                     |                |
| Fugitive Dust |        |         |         |        | 10.2265          | 0.0000          | 10.2265       | 4.4313            | 0.0000           | 4.4313         |          |                | 0.0000         |        |                     | 0.0000         |
| Off-Road      | 6.1180 | 68.8321 | 39.7696 | 0.0817 |                  | 3.0645          | 3.0645        |                   | 2.8217           | 2.8217         | 0.0000   | 7,877.540<br>3 | 7,877.540<br>3 | 2.5248 | <br> <br> <br> <br> | 7,940.659<br>2 |
| Total         | 6.1180 | 68.8321 | 39.7696 | 0.0817 | 10.2265          | 3.0645          | 13.2910       | 4.4313            | 2.8217           | 7.2530         | 0.0000   | 7,877.540<br>3 | 7,877.540<br>3 | 2.5248 |                     | 7,940.659<br>2 |

|          | ROG             | NOx     | CO     | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total   | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5<br>Total  | Bio- CO2 | NBio- CO2      | Total CO2      | CH4             | N2O | CO2e           |
|----------|-----------------|---------|--------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|----------------|----------------|-----------------|-----|----------------|
| Category |                 |         |        |                 | lb/              | day             |                 |                   |                  |                 |          |                | lb/d           | day             |     |                |
| Hauling  | 0.3269          | 11.2907 | 2.1115 | 0.0307          | 0.6722           | 0.0449          | 0.7170          | 0.1842            | 0.0429           | 0.2272          |          | 3,239.867<br>1 | 3,239.867<br>1 | 0.1387          |     | 3,243.334<br>5 |
| Vendor   | 4.6700e-<br>003 | 0.1247  | 0.0346 | 2.8000e-<br>004 | 6.7700e-<br>003  | 7.1000e-<br>004 | 7.4800e-<br>003 | 1.9500e-<br>003   | 6.8000e-<br>004  | 2.6300e-<br>003 |          | 29.5633        | 29.5633        | 1.7200e-<br>003 |     | 29.6064        |
| Worker   | 0.0956          | 0.0872  | 0.7405 | 1.6300e-<br>003 | 0.1643           | 1.3700e-<br>003 | 0.1657          | 0.0436            | 1.2600e-<br>003  | 0.0448          |          | 162.1020       | 162.1020       | 6.8300e-<br>003 |     | 162.2729       |
| Total    | 0.4272          | 11.5026 | 2.8865 | 0.0326          | 0.8432           | 0.0470          | 0.8902          | 0.2297            | 0.0449           | 0.2746          |          | 3,431.532<br>4 | 3,431.532<br>4 | 0.1473          |     | 3,435.213<br>7 |

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## Lico Subdivision Project - Monterey Bay Unified APCD Air District, Winter

3.5 Paving - Phase I - 2020 Unmitigated Construction On-Site

|          | ROG    | NOx     | CO      | SO2    | Fugitive<br>PM10    | Exhaust<br>PM10 | PM10<br>Total | Fugitive<br>PM2.5   | Exhaust<br>PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2      | Total CO2      | CH4    | N2O | CO2e           |
|----------|--------|---------|---------|--------|---------------------|-----------------|---------------|---------------------|------------------|-------------|----------|----------------|----------------|--------|-----|----------------|
| Category |        |         |         |        | lb/d                | day             |               |                     |                  |             |          |                | lb/d           | day    |     |                |
| Off-Road | 2.3901 | 25.7947 | 20.2681 | 0.0423 |                     | 1.1622          | 1.1622        |                     | 1.0904           | 1.0904      |          | 4,056.296<br>3 | 4,056.296<br>3 | 1.1057 |     | 4,083.938<br>4 |
|          | 0.2817 |         |         |        | <br> <br> <br> <br> | 0.0000          | 0.0000        | <br> <br> <br> <br> | 0.0000           | 0.0000      |          |                | 0.0000         |        |     | 0.0000         |
| Total    | 2.6718 | 25.7947 | 20.2681 | 0.0423 |                     | 1.1622          | 1.1622        |                     | 1.0904           | 1.0904      |          | 4,056.296<br>3 | 4,056.296<br>3 | 1.1057 |     | 4,083.938<br>4 |

|          | ROG             | NOx    | СО     | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total   | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total     | Bio- CO2 | NBio- CO2 | Total CO2 | CH4             | N2O | CO2e     |
|----------|-----------------|--------|--------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|-----|----------|
| Category |                 |        |        |                 | lb/              | day             |                 |                   |                  |                 |          |           | lb/d      | day             |     |          |
| Hauling  | 0.0000          | 0.0000 | 0.0000 | 0.0000          | 0.0000           | 0.0000          | 0.0000          | 0.0000            | 0.0000           | 0.0000          |          | 0.0000    | 0.0000    | 0.0000          |     | 0.0000   |
| Vendor   | 4.6700e-<br>003 | 0.1247 | 0.0346 | 2.8000e-<br>004 | 6.7700e-<br>003  | 7.1000e-<br>004 | 7.4800e-<br>003 | 1.9500e-<br>003   | 6.8000e-<br>004  | 2.6300e-<br>003 |          | 29.5633   | 29.5633   | 1.7200e-<br>003 |     | 29.6064  |
| Worker   | 0.0956          | 0.0872 | 0.7405 | 1.6300e-<br>003 | 0.1643           | 1.3700e-<br>003 | 0.1657          | 0.0436            | 1.2600e-<br>003  | 0.0448          |          | 162.1020  | 162.1020  | 6.8300e-<br>003 |     | 162.2729 |
| Total    | 0.1003          | 0.2119 | 0.7750 | 1.9100e-<br>003 | 0.1711           | 2.0800e-<br>003 | 0.1731          | 0.0455            | 1.9400e-<br>003  | 0.0475          |          | 191.6653  | 191.6653  | 8.5500e-<br>003 |     | 191.8792 |

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## Lico Subdivision Project - Monterey Bay Unified APCD Air District, Winter

3.5 Paving - Phase I - 2020 Mitigated Construction On-Site

|          | ROG    | NOx     | CO      | SO2    | Fugitive<br>PM10    | Exhaust<br>PM10 | PM10<br>Total | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2      | Total CO2      | CH4    | N2O | CO2e           |
|----------|--------|---------|---------|--------|---------------------|-----------------|---------------|-------------------|------------------|-------------|----------|----------------|----------------|--------|-----|----------------|
| Category |        |         |         |        | lb/d                | day             |               |                   |                  |             |          |                | lb/c           | day    |     |                |
| Off-Road | 2.3901 | 25.7947 | 20.2681 | 0.0423 |                     | 1.1622          | 1.1622        |                   | 1.0904           | 1.0904      | 0.0000   | 4,056.296<br>3 | 4,056.296<br>3 | 1.1057 |     | 4,083.938<br>4 |
| Paving   | 0.2817 |         |         |        | <br> <br> <br> <br> | 0.0000          | 0.0000        |                   | 0.0000           | 0.0000      |          |                | 0.0000         |        |     | 0.0000         |
| Total    | 2.6718 | 25.7947 | 20.2681 | 0.0423 |                     | 1.1622          | 1.1622        |                   | 1.0904           | 1.0904      | 0.0000   | 4,056.296<br>3 | 4,056.296<br>3 | 1.1057 |     | 4,083.938      |

|          | ROG             | NOx    | CO     | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total   | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total     | Bio- CO2 | NBio- CO2 | Total CO2 | CH4             | N2O | CO2e     |
|----------|-----------------|--------|--------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|-----|----------|
| Category |                 |        |        |                 | lb/              | day             |                 |                   |                  |                 |          |           | lb/d      | day             |     |          |
| Hauling  | 0.0000          | 0.0000 | 0.0000 | 0.0000          | 0.0000           | 0.0000          | 0.0000          | 0.0000            | 0.0000           | 0.0000          |          | 0.0000    | 0.0000    | 0.0000          |     | 0.0000   |
| Vendor   | 4.6700e-<br>003 | 0.1247 | 0.0346 | 2.8000e-<br>004 | 6.7700e-<br>003  | 7.1000e-<br>004 | 7.4800e-<br>003 | 1.9500e-<br>003   | 6.8000e-<br>004  | 2.6300e-<br>003 |          | 29.5633   | 29.5633   | 1.7200e-<br>003 |     | 29.6064  |
| Worker   | 0.0956          | 0.0872 | 0.7405 | 1.6300e-<br>003 | 0.1643           | 1.3700e-<br>003 | 0.1657          | 0.0436            | 1.2600e-<br>003  | 0.0448          |          | 162.1020  | 162.1020  | 6.8300e-<br>003 |     | 162.2729 |
| Total    | 0.1003          | 0.2119 | 0.7750 | 1.9100e-<br>003 | 0.1711           | 2.0800e-<br>003 | 0.1731          | 0.0455            | 1.9400e-<br>003  | 0.0475          |          | 191.6653  | 191.6653  | 8.5500e-<br>003 |     | 191.8792 |

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## Lico Subdivision Project - Monterey Bay Unified APCD Air District, Winter

3.5 Paving - Phase I - 2021

<u>Unmitigated Construction On-Site</u>

|          | ROG    | NOx     | CO      | SO2    | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2      | Total CO2      | CH4    | N2O | CO2e           |
|----------|--------|---------|---------|--------|------------------|-----------------|---------------|-------------------|------------------|-------------|----------|----------------|----------------|--------|-----|----------------|
| Category |        |         |         |        | lb/d             | day             |               |                   |                  |             |          |                | lb/c           | day    |     |                |
| Off-Road | 2.2430 | 24.0301 | 20.1648 | 0.0423 |                  | 1.0536          | 1.0536        |                   | 0.9880           | 0.9880      |          | 4,054.914<br>2 | 4,054.914<br>2 | 1.1013 |     | 4,082.447<br>3 |
| Paving   | 0.2817 |         |         |        |                  | 0.0000          | 0.0000        |                   | 0.0000           | 0.0000      |          |                | 0.0000         |        |     | 0.0000         |
| Total    | 2.5246 | 24.0301 | 20.1648 | 0.0423 |                  | 1.0536          | 1.0536        |                   | 0.9880           | 0.9880      |          | 4,054.914<br>2 | 4,054.914<br>2 | 1.1013 |     | 4,082.447<br>3 |

|          | ROG             | NOx    | CO     | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total   | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total     | Bio- CO2 | NBio- CO2 | Total CO2 | CH4             | N2O | CO2e     |
|----------|-----------------|--------|--------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|-----|----------|
| Category |                 |        |        |                 | lb/d             | day             |                 |                   |                  |                 |          |           | lb/d      | lay             |     |          |
| Hauling  | 0.0000          | 0.0000 | 0.0000 | 0.0000          | 0.0000           | 0.0000          | 0.0000          | 0.0000            | 0.0000           | 0.0000          |          | 0.0000    | 0.0000    | 0.0000          |     | 0.0000   |
| Vendor   | 3.8400e-<br>003 | 0.1136 | 0.0301 | 2.8000e-<br>004 | 6.7700e-<br>003  | 3.6000e-<br>004 | 7.1300e-<br>003 | 1.9500e-<br>003   | 3.4000e-<br>004  | 2.2900e-<br>003 |          | 29.3041   | 29.3041   | 1.6700e-<br>003 |     | 29.3459  |
| Worker   | 0.0884          | 0.0778 | 0.6732 | 1.5800e-<br>003 | 0.1643           | 1.3300e-<br>003 | 0.1656          | 0.0436            | 1.2200e-<br>003  | 0.0448          |          | 157.0261  | 157.0261  | 6.1000e-<br>003 |     | 157.1786 |
| Total    | 0.0922          | 0.1914 | 0.7033 | 1.8600e-<br>003 | 0.1711           | 1.6900e-<br>003 | 0.1728          | 0.0455            | 1.5600e-<br>003  | 0.0471          |          | 186.3302  | 186.3302  | 7.7700e-<br>003 |     | 186.5244 |

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## Lico Subdivision Project - Monterey Bay Unified APCD Air District, Winter

3.5 Paving - Phase I - 2021 Mitigated Construction On-Site

|          | ROG    | NOx     | CO                    | SO2    | Fugitive<br>PM10    | Exhaust<br>PM10 | PM10<br>Total | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2      | Total CO2      | CH4    | N2O                 | CO2e           |
|----------|--------|---------|-----------------------|--------|---------------------|-----------------|---------------|-------------------|------------------|-------------|----------|----------------|----------------|--------|---------------------|----------------|
| Category |        |         |                       |        | lb/d                | day             |               |                   |                  |             |          |                | lb/d           | lay    |                     |                |
| Off-Road | 2.2430 | 24.0301 | 20.1648               | 0.0423 |                     | 1.0536          | 1.0536        | !<br>!            | 0.9880           | 0.9880      | 0.0000   | 4,054.914<br>2 | 4,054.914<br>2 | 1.1013 |                     | 4,082.447<br>3 |
| Paving   | 0.2817 |         | 1<br>1<br>1<br>1<br>1 |        | <br> <br> <br> <br> | 0.0000          | 0.0000        | 1                 | 0.0000           | 0.0000      |          |                | 0.0000         |        | <br> <br> <br> <br> | 0.0000         |
| Total    | 2.5246 | 24.0301 | 20.1648               | 0.0423 |                     | 1.0536          | 1.0536        |                   | 0.9880           | 0.9880      | 0.0000   | 4,054.914<br>2 | 4,054.914<br>2 | 1.1013 |                     | 4,082.447<br>3 |

|          | ROG             | NOx    | СО     | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total   | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total     | Bio- CO2 | NBio- CO2 | Total CO2 | CH4             | N2O | CO2e     |
|----------|-----------------|--------|--------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|-----|----------|
| Category |                 |        |        |                 | lb/d             | day             |                 |                   |                  |                 |          |           | lb/d      | day             |     |          |
| Hauling  | 0.0000          | 0.0000 | 0.0000 | 0.0000          | 0.0000           | 0.0000          | 0.0000          | 0.0000            | 0.0000           | 0.0000          |          | 0.0000    | 0.0000    | 0.0000          |     | 0.0000   |
| Vendor   | 3.8400e-<br>003 | 0.1136 | 0.0301 | 2.8000e-<br>004 | 6.7700e-<br>003  | 3.6000e-<br>004 | 7.1300e-<br>003 | 1.9500e-<br>003   | 3.4000e-<br>004  | 2.2900e-<br>003 |          | 29.3041   | 29.3041   | 1.6700e-<br>003 |     | 29.3459  |
| Worker   | 0.0884          | 0.0778 | 0.6732 | 1.5800e-<br>003 | 0.1643           | 1.3300e-<br>003 | 0.1656          | 0.0436            | 1.2200e-<br>003  | 0.0448          |          | 157.0261  | 157.0261  | 6.1000e-<br>003 |     | 157.1786 |
| Total    | 0.0922          | 0.1914 | 0.7033 | 1.8600e-<br>003 | 0.1711           | 1.6900e-<br>003 | 0.1728          | 0.0455            | 1.5600e-<br>003  | 0.0471          |          | 186.3302  | 186.3302  | 7.7700e-<br>003 |     | 186.5244 |

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## Lico Subdivision Project - Monterey Bay Unified APCD Air District, Winter

# 3.6 Building Construction - Phase I - 2021 <u>Unmitigated Construction On-Site</u>

|          | ROG    | NOx     | CO      | SO2    | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2      | Total CO2      | CH4    | N2O | CO2e           |
|----------|--------|---------|---------|--------|------------------|-----------------|---------------|-------------------|------------------|-------------|----------|----------------|----------------|--------|-----|----------------|
| Category |        |         |         |        | lb/d             | day             |               |                   |                  |             |          |                | lb/d           | lay    |     |                |
| Off-Road | 2.9293 | 29.3225 | 27.4342 | 0.0460 |                  | 1.5462          | 1.5462        |                   | 1.4565           | 1.4565      |          | 4,418.440<br>8 | 4,418.440<br>8 | 1.0203 |     | 4,443.948<br>2 |
| Total    | 2.9293 | 29.3225 | 27.4342 | 0.0460 |                  | 1.5462          | 1.5462        |                   | 1.4565           | 1.4565      |          | 4,418.440<br>8 | 4,418.440<br>8 | 1.0203 |     | 4,443.948<br>2 |

|          | ROG             | NOx    | СО     | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total   | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total     | Bio- CO2 | NBio- CO2 | Total CO2 | CH4             | N2O | CO2e     |
|----------|-----------------|--------|--------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|-----|----------|
| Category |                 |        |        |                 | lb/d             | day             |                 |                   |                  |                 |          |           | lb/d      | lay             |     |          |
| Hauling  | 0.0000          | 0.0000 | 0.0000 | 0.0000          | 0.0000           | 0.0000          | 0.0000          | 0.0000            | 0.0000           | 0.0000          |          | 0.0000    | 0.0000    | 0.0000          |     | 0.0000   |
| Vendor   | 3.8400e-<br>003 | 0.1136 | 0.0301 | 2.8000e-<br>004 | 6.7700e-<br>003  | 3.6000e-<br>004 | 7.1300e-<br>003 | 1.9500e-<br>003   | 3.4000e-<br>004  | 2.2900e-<br>003 |          | 29.3041   | 29.3041   | 1.6700e-<br>003 |     | 29.3459  |
| Worker   | 0.1768          | 0.1557 | 1.3464 | 3.1600e-<br>003 | 0.3286           | 2.6500e-<br>003 | 0.3312          | 0.0872            | 2.4500e-<br>003  | 0.0896          |          | 314.0522  | 314.0522  | 0.0122          |     | 314.3572 |
| Total    | 0.1806          | 0.2693 | 1.3765 | 3.4400e-<br>003 | 0.3354           | 3.0100e-<br>003 | 0.3384          | 0.0891            | 2.7900e-<br>003  | 0.0919          |          | 343.3563  | 343.3563  | 0.0139          |     | 343.7030 |

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## Lico Subdivision Project - Monterey Bay Unified APCD Air District, Winter

# 3.6 Building Construction - Phase I - 2021 Mitigated Construction On-Site

|          | ROG    | NOx     | CO      | SO2    | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2      | Total CO2      | CH4    | N2O | CO2e           |
|----------|--------|---------|---------|--------|------------------|-----------------|---------------|-------------------|------------------|-------------|----------|----------------|----------------|--------|-----|----------------|
| Category |        |         |         |        | lb/d             | day             |               |                   |                  |             |          |                | lb/d           | lay    |     |                |
| Off-Road | 2.9293 | 29.3225 | 27.4342 | 0.0460 |                  | 1.5462          | 1.5462        |                   | 1.4565           | 1.4565      | 0.0000   | 4,418.440<br>8 | 4,418.440<br>8 | 1.0203 |     | 4,443.948<br>2 |
| Total    | 2.9293 | 29.3225 | 27.4342 | 0.0460 |                  | 1.5462          | 1.5462        |                   | 1.4565           | 1.4565      | 0.0000   | 4,418.440<br>8 | 4,418.440<br>8 | 1.0203 |     | 4,443.948<br>2 |

|          | ROG             | NOx    | CO     | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total   | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total     | Bio- CO2 | NBio- CO2 | Total CO2 | CH4             | N2O | CO2e     |
|----------|-----------------|--------|--------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|-----|----------|
| Category |                 |        |        |                 | lb/d             | day             |                 |                   |                  |                 |          |           | lb/d      | lay             |     |          |
| Hauling  | 0.0000          | 0.0000 | 0.0000 | 0.0000          | 0.0000           | 0.0000          | 0.0000          | 0.0000            | 0.0000           | 0.0000          |          | 0.0000    | 0.0000    | 0.0000          |     | 0.0000   |
| Vendor   | 3.8400e-<br>003 | 0.1136 | 0.0301 | 2.8000e-<br>004 | 6.7700e-<br>003  | 3.6000e-<br>004 | 7.1300e-<br>003 | 1.9500e-<br>003   | 3.4000e-<br>004  | 2.2900e-<br>003 |          | 29.3041   | 29.3041   | 1.6700e-<br>003 |     | 29.3459  |
| Worker   | 0.1768          | 0.1557 | 1.3464 | 3.1600e-<br>003 | 0.3286           | 2.6500e-<br>003 | 0.3312          | 0.0872            | 2.4500e-<br>003  | 0.0896          |          | 314.0522  | 314.0522  | 0.0122          |     | 314.3572 |
| Total    | 0.1806          | 0.2693 | 1.3765 | 3.4400e-<br>003 | 0.3354           | 3.0100e-<br>003 | 0.3384          | 0.0891            | 2.7900e-<br>003  | 0.0919          |          | 343.3563  | 343.3563  | 0.0139          |     | 343.7030 |

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## Lico Subdivision Project - Monterey Bay Unified APCD Air District, Winter

# 3.7 Architectural Coating - Phase I - 2021 <u>Unmitigated Construction On-Site</u>

|                 | ROG    | NOx    | CO     | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5<br>Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4    | N2O                 | CO2e     |
|-----------------|--------|--------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|-----------|-----------|--------|---------------------|----------|
| Category        |        |        |        |                 | lb/d             | day             |               |                   |                  |                |          |           | lb/d      | day    |                     |          |
| Archit. Coating | 7.1157 |        |        |                 |                  | 0.0000          | 0.0000        |                   | 0.0000           | 0.0000         |          |           | 0.0000    |        |                     | 0.0000   |
|                 | 0.2189 | 1.5268 | 1.8176 | 2.9700e-<br>003 |                  | 0.0941          | 0.0941        | 1                 | 0.0941           | 0.0941         |          | 281.4481  | 281.4481  | 0.0193 | <br> <br> <br> <br> | 281.9309 |
| Total           | 7.3346 | 1.5268 | 1.8176 | 2.9700e-<br>003 |                  | 0.0941          | 0.0941        |                   | 0.0941           | 0.0941         |          | 281.4481  | 281.4481  | 0.0193 |                     | 281.9309 |

|          | ROG             | NOx    | CO     | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total   | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total     | Bio- CO2 | NBio- CO2 | Total CO2 | CH4             | N2O | CO2e     |
|----------|-----------------|--------|--------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|-----|----------|
| Category |                 |        |        |                 | lb/              | day             |                 |                   |                  |                 |          |           | lb/d      | lay             |     |          |
| Hauling  | 0.0000          | 0.0000 | 0.0000 | 0.0000          | 0.0000           | 0.0000          | 0.0000          | 0.0000            | 0.0000           | 0.0000          |          | 0.0000    | 0.0000    | 0.0000          |     | 0.0000   |
| Vendor   | 3.8400e-<br>003 | 0.1136 | 0.0301 | 2.8000e-<br>004 | 6.7700e-<br>003  | 3.6000e-<br>004 | 7.1300e-<br>003 | 1.9500e-<br>003   | 3.4000e-<br>004  | 2.2900e-<br>003 |          | 29.3041   | 29.3041   | 1.6700e-<br>003 |     | 29.3459  |
| Worker   | 0.1768          | 0.1557 | 1.3464 | 3.1600e-<br>003 | 0.3286           | 2.6500e-<br>003 | 0.3312          | 0.0872            | 2.4500e-<br>003  | 0.0896          |          | 314.0522  | 314.0522  | 0.0122          |     | 314.3572 |
| Total    | 0.1806          | 0.2693 | 1.3765 | 3.4400e-<br>003 | 0.3354           | 3.0100e-<br>003 | 0.3384          | 0.0891            | 2.7900e-<br>003  | 0.0919          | -        | 343.3563  | 343.3563  | 0.0139          |     | 343.7030 |

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## Lico Subdivision Project - Monterey Bay Unified APCD Air District, Winter

# 3.7 Architectural Coating - Phase I - 2021 Mitigated Construction On-Site

|                 | ROG    | NOx    | CO     | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4    | N2O | CO2e     |
|-----------------|--------|--------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|-------------|----------|-----------|-----------|--------|-----|----------|
| Category        |        |        |        |                 | lb/d             | day             |               |                   |                  |             |          |           | lb/d      | day    |     |          |
| Archit. Coating | 7.1157 |        | <br>   |                 |                  | 0.0000          | 0.0000        | !<br>!            | 0.0000           | 0.0000      |          |           | 0.0000    |        |     | 0.0000   |
|                 | 0.2189 | 1.5268 | 1.8176 | 2.9700e-<br>003 |                  | 0.0941          | 0.0941        | 1<br>1<br>1<br>1  | 0.0941           | 0.0941      | 0.0000   | 281.4481  | 281.4481  | 0.0193 | ,   | 281.9309 |
| Total           | 7.3346 | 1.5268 | 1.8176 | 2.9700e-<br>003 |                  | 0.0941          | 0.0941        |                   | 0.0941           | 0.0941      | 0.0000   | 281.4481  | 281.4481  | 0.0193 |     | 281.9309 |

|          | ROG             | NOx    | CO     | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total   | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total     | Bio- CO2 | NBio- CO2 | Total CO2 | CH4             | N2O | CO2e     |
|----------|-----------------|--------|--------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|-----|----------|
| Category |                 |        |        |                 | lb/d             | lb/day          |                 |                   |                  |                 |          |           |           |                 |     |          |
| Hauling  | 0.0000          | 0.0000 | 0.0000 | 0.0000          | 0.0000           | 0.0000          | 0.0000          | 0.0000            | 0.0000           | 0.0000          |          | 0.0000    | 0.0000    | 0.0000          |     | 0.0000   |
| Vendor   | 3.8400e-<br>003 | 0.1136 | 0.0301 | 2.8000e-<br>004 | 6.7700e-<br>003  | 3.6000e-<br>004 | 7.1300e-<br>003 | 1.9500e-<br>003   | 3.4000e-<br>004  | 2.2900e-<br>003 |          | 29.3041   | 29.3041   | 1.6700e-<br>003 |     | 29.3459  |
| Worker   | 0.1768          | 0.1557 | 1.3464 | 3.1600e-<br>003 | 0.3286           | 2.6500e-<br>003 | 0.3312          | 0.0872            | 2.4500e-<br>003  | 0.0896          |          | 314.0522  | 314.0522  | 0.0122          |     | 314.3572 |
| Total    | 0.1806          | 0.2693 | 1.3765 | 3.4400e-<br>003 | 0.3354           | 3.0100e-<br>003 | 0.3384          | 0.0891            | 2.7900e-<br>003  | 0.0919          |          | 343.3563  | 343.3563  | 0.0139          |     | 343.7030 |

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## Lico Subdivision Project - Monterey Bay Unified APCD Air District, Winter

3.8 Paving - Phase II - 2021

<u>Unmitigated Construction On-Site</u>

|          | ROG    | NOx     | СО      | SO2    | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total | Fugitive<br>PM2.5   | Exhaust<br>PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2                      | Total CO2      | CH4    | N2O | CO2e           |
|----------|--------|---------|---------|--------|------------------|-----------------|---------------|---------------------|------------------|-------------|----------|--------------------------------|----------------|--------|-----|----------------|
| Category |        |         |         |        | lb/d             | day             |               |                     |                  |             |          |                                | lb/c           | day    |     |                |
| Off-Road | 2.2430 | 24.0301 | 20.1648 | 0.0423 |                  | 1.0536          | 1.0536        |                     | 0.9880           | 0.9880      |          | 4,054.914<br>2                 | 4,054.914<br>2 | 1.1013 |     | 4,082.447<br>3 |
|          | 0.2817 |         | i<br>i  |        |                  | 0.0000          | 0.0000        | <br> <br> <br> <br> | 0.0000           | 0.0000      |          | <del></del><br> <br> <br> <br> | 0.0000         |        |     | 0.0000         |
| Total    | 2.5246 | 24.0301 | 20.1648 | 0.0423 |                  | 1.0536          | 1.0536        |                     | 0.9880           | 0.9880      |          | 4,054.914<br>2                 | 4,054.914<br>2 | 1.1013 |     | 4,082.447<br>3 |

|          | ROG             | NOx    | СО     | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total   | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total     | Bio- CO2 | NBio- CO2 | Total CO2 | CH4             | N2O                 | CO2e     |
|----------|-----------------|--------|--------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|---------------------|----------|
| Category |                 |        |        |                 | lb/d             | lb/day          |                 |                   |                  |                 |          |           |           |                 |                     |          |
| Hauling  | 0.0000          | 0.0000 | 0.0000 | 0.0000          | 0.0000           | 0.0000          | 0.0000          | 0.0000            | 0.0000           | 0.0000          |          | 0.0000    | 0.0000    | 0.0000          |                     | 0.0000   |
| Vendor   | 3.8400e-<br>003 | 0.1136 | 0.0301 | 2.8000e-<br>004 | 6.7700e-<br>003  | 3.6000e-<br>004 | 7.1300e-<br>003 | 1.9500e-<br>003   | 3.4000e-<br>004  | 2.2900e-<br>003 |          | 29.3041   | 29.3041   | 1.6700e-<br>003 | <br> <br> <br> <br> | 29.3459  |
| Worker   | 0.0884          | 0.0778 | 0.6732 | 1.5800e-<br>003 | 0.1643           | 1.3300e-<br>003 | 0.1656          | 0.0436            | 1.2200e-<br>003  | 0.0448          |          | 157.0261  | 157.0261  | 6.1000e-<br>003 | <br> <br> <br> <br> | 157.1786 |
| Total    | 0.0922          | 0.1914 | 0.7033 | 1.8600e-<br>003 | 0.1711           | 1.6900e-<br>003 | 0.1728          | 0.0455            | 1.5600e-<br>003  | 0.0471          |          | 186.3302  | 186.3302  | 7.7700e-<br>003 |                     | 186.5244 |

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## Lico Subdivision Project - Monterey Bay Unified APCD Air District, Winter

3.8 Paving - Phase II - 2021 Mitigated Construction On-Site

|          | ROG    | NOx     | CO      | SO2    | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2      | Total CO2      | CH4    | N2O | CO2e           |
|----------|--------|---------|---------|--------|------------------|-----------------|---------------|-------------------|------------------|-------------|----------|----------------|----------------|--------|-----|----------------|
| Category |        |         |         |        | lb/d             | day             |               |                   |                  |             |          |                | lb/c           | lay    |     |                |
| Off-Road | 2.2430 | 24.0301 | 20.1648 | 0.0423 |                  | 1.0536          | 1.0536        | 1<br>1            | 0.9880           | 0.9880      | 0.0000   | 4,054.914<br>2 | 4,054.914<br>2 | 1.1013 |     | 4,082.447<br>3 |
| Paving   | 0.2817 |         |         |        |                  | 0.0000          | 0.0000        |                   | 0.0000           | 0.0000      |          |                | 0.0000         |        |     | 0.0000         |
| Total    | 2.5246 | 24.0301 | 20.1648 | 0.0423 |                  | 1.0536          | 1.0536        |                   | 0.9880           | 0.9880      | 0.0000   | 4,054.914<br>2 | 4,054.914<br>2 | 1.1013 |     | 4,082.447<br>3 |

|          | ROG             | NOx    | CO     | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total   | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total     | Bio- CO2 | NBio- CO2 | Total CO2 | CH4             | N2O | CO2e     |
|----------|-----------------|--------|--------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|-----|----------|
| Category |                 |        |        |                 | lb/day           |                 |                 |                   |                  |                 |          |           |           |                 |     |          |
| Hauling  | 0.0000          | 0.0000 | 0.0000 | 0.0000          | 0.0000           | 0.0000          | 0.0000          | 0.0000            | 0.0000           | 0.0000          |          | 0.0000    | 0.0000    | 0.0000          |     | 0.0000   |
|          | 3.8400e-<br>003 | 0.1136 | 0.0301 | 2.8000e-<br>004 | 6.7700e-<br>003  | 3.6000e-<br>004 | 7.1300e-<br>003 | 1.9500e-<br>003   | 3.4000e-<br>004  | 2.2900e-<br>003 |          | 29.3041   | 29.3041   | 1.6700e-<br>003 |     | 29.3459  |
| Worker   | 0.0884          | 0.0778 | 0.6732 | 1.5800e-<br>003 | 0.1643           | 1.3300e-<br>003 | 0.1656          | 0.0436            | 1.2200e-<br>003  | 0.0448          |          | 157.0261  | 157.0261  | 6.1000e-<br>003 |     | 157.1786 |
| Total    | 0.0922          | 0.1914 | 0.7033 | 1.8600e-<br>003 | 0.1711           | 1.6900e-<br>003 | 0.1728          | 0.0455            | 1.5600e-<br>003  | 0.0471          |          | 186.3302  | 186.3302  | 7.7700e-<br>003 |     | 186.5244 |

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## Lico Subdivision Project - Monterey Bay Unified APCD Air District, Winter

3.8 Paving - Phase II - 2022 Unmitigated Construction On-Site

|          | ROG    | NOx     | CO      | SO2    | Fugitive<br>PM10    | Exhaust<br>PM10 | PM10<br>Total | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2      | Total CO2      | CH4    | N2O | CO2e           |  |  |  |
|----------|--------|---------|---------|--------|---------------------|-----------------|---------------|-------------------|------------------|-------------|----------|----------------|----------------|--------|-----|----------------|--|--|--|
| Category | lb/day |         |         |        |                     |                 |               |                   |                  |             |          | lb/day         |                |        |     |                |  |  |  |
| Off-Road | 2.0439 | 21.3454 | 19.9747 | 0.0423 |                     | 0.9122          | 0.9122        |                   | 0.8556           | 0.8556      |          | 4,052.801<br>4 | 4,052.801<br>4 | 1.0980 |     | 4,080.252<br>2 |  |  |  |
| Paving   | 0.2817 |         |         |        | <br> <br> <br> <br> | 0.0000          | 0.0000        |                   | 0.0000           | 0.0000      |          | 1              | 0.0000         |        |     | 0.0000         |  |  |  |
| Total    | 2.3256 | 21.3454 | 19.9747 | 0.0423 |                     | 0.9122          | 0.9122        |                   | 0.8556           | 0.8556      |          | 4,052.801<br>4 | 4,052.801<br>4 | 1.0980 |     | 4,080.252<br>2 |  |  |  |

|          | ROG             | NOx    | CO     | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total   | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total     | Bio- CO2 | NBio- CO2 | Total CO2 | CH4             | N2O | CO2e     |
|----------|-----------------|--------|--------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|-----|----------|
| Category |                 |        |        |                 | lb/d             | lb/day          |                 |                   |                  |                 |          |           |           |                 |     |          |
| Hauling  | 0.0000          | 0.0000 | 0.0000 | 0.0000          | 0.0000           | 0.0000          | 0.0000          | 0.0000            | 0.0000           | 0.0000          |          | 0.0000    | 0.0000    | 0.0000          |     | 0.0000   |
| Vendor   | 3.5300e-<br>003 | 0.1074 | 0.0273 | 2.8000e-<br>004 | 6.7700e-<br>003  | 3.1000e-<br>004 | 7.0800e-<br>003 | 1.9500e-<br>003   | 3.0000e-<br>004  | 2.2500e-<br>003 |          | 29.0344   | 29.0344   | 1.6300e-<br>003 |     | 29.0751  |
| Worker   | 0.0821          | 0.0697 | 0.6130 | 1.5200e-<br>003 | 0.1643           | 1.2800e-<br>003 | 0.1656          | 0.0436            | 1.1800e-<br>003  | 0.0448          |          | 151.4893  | 151.4893  | 5.4400e-<br>003 |     | 151.6252 |
| Total    | 0.0857          | 0.1771 | 0.6403 | 1.8000e-<br>003 | 0.1711           | 1.5900e-<br>003 | 0.1727          | 0.0455            | 1.4800e-<br>003  | 0.0470          |          | 180.5237  | 180.5237  | 7.0700e-<br>003 |     | 180.7004 |

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## Lico Subdivision Project - Monterey Bay Unified APCD Air District, Winter

3.8 Paving - Phase II - 2022 Mitigated Construction On-Site

|          | ROG    | NOx     | CO      | SO2    | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2      | Total CO2      | CH4    | N2O | CO2e           |
|----------|--------|---------|---------|--------|------------------|-----------------|---------------|-------------------|------------------|-------------|----------|----------------|----------------|--------|-----|----------------|
| Category |        |         |         |        | lb/d             | day             |               |                   |                  |             |          |                | lb/d           | lay    |     |                |
| Off-Road | 2.0439 | 21.3454 | 19.9747 | 0.0423 |                  | 0.9122          | 0.9122        | 1<br>1<br>1       | 0.8556           | 0.8556      | 0.0000   | 4,052.801<br>4 | 4,052.801<br>4 | 1.0980 |     | 4,080.252<br>2 |
| Paving   | 0.2817 |         |         |        |                  | 0.0000          | 0.0000        | <br>              | 0.0000           | 0.0000      |          | <br>           | 0.0000         |        |     | 0.0000         |
| Total    | 2.3256 | 21.3454 | 19.9747 | 0.0423 |                  | 0.9122          | 0.9122        |                   | 0.8556           | 0.8556      | 0.0000   | 4,052.801<br>4 | 4,052.801<br>4 | 1.0980 |     | 4,080.252<br>2 |

|          | ROG             | NOx    | CO     | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total   | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total     | Bio- CO2 | NBio- CO2 | Total CO2 | CH4             | N2O | CO2e     |
|----------|-----------------|--------|--------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|-----|----------|
| Category |                 |        |        |                 | lb/d             | day             |                 |                   |                  |                 |          |           | lb/d      | day             |     |          |
| Hauling  | 0.0000          | 0.0000 | 0.0000 | 0.0000          | 0.0000           | 0.0000          | 0.0000          | 0.0000            | 0.0000           | 0.0000          |          | 0.0000    | 0.0000    | 0.0000          |     | 0.0000   |
| Vendor   | 3.5300e-<br>003 | 0.1074 | 0.0273 | 2.8000e-<br>004 | 6.7700e-<br>003  | 3.1000e-<br>004 | 7.0800e-<br>003 | 1.9500e-<br>003   | 3.0000e-<br>004  | 2.2500e-<br>003 |          | 29.0344   | 29.0344   | 1.6300e-<br>003 |     | 29.0751  |
| Worker   | 0.0821          | 0.0697 | 0.6130 | 1.5200e-<br>003 | 0.1643           | 1.2800e-<br>003 | 0.1656          | 0.0436            | 1.1800e-<br>003  | 0.0448          |          | 151.4893  | 151.4893  | 5.4400e-<br>003 |     | 151.6252 |
| Total    | 0.0857          | 0.1771 | 0.6403 | 1.8000e-<br>003 | 0.1711           | 1.5900e-<br>003 | 0.1727          | 0.0455            | 1.4800e-<br>003  | 0.0470          |          | 180.5237  | 180.5237  | 7.0700e-<br>003 |     | 180.7004 |

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## Lico Subdivision Project - Monterey Bay Unified APCD Air District, Winter

# 3.9 Building Construction - Phase II - 2022 Unmitigated Construction On-Site

|          | ROG    | NOx     | CO      | SO2    | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2      | Total CO2      | CH4    | N2O | CO2e           |
|----------|--------|---------|---------|--------|------------------|-----------------|---------------|-------------------|------------------|-------------|----------|----------------|----------------|--------|-----|----------------|
| Category |        |         |         |        | lb/d             | day             |               |                   |                  |             |          |                | lb/c           | lay    |     |                |
|          | 2.6834 | 26.4913 | 27.2071 | 0.0460 |                  | 1.3570          | 1.3570        |                   | 1.2781           | 1.2781      |          | 4,418.993<br>7 | 4,418.993<br>7 | 1.0151 |     | 4,444.371<br>8 |
| Total    | 2.6834 | 26.4913 | 27.2071 | 0.0460 |                  | 1.3570          | 1.3570        |                   | 1.2781           | 1.2781      |          | 4,418.993<br>7 | 4,418.993<br>7 | 1.0151 |     | 4,444.371<br>8 |

|          | ROG             | NOx    | СО     | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total   | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total     | Bio- CO2 | NBio- CO2 | Total CO2 | CH4             | N2O | CO2e     |
|----------|-----------------|--------|--------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|-----|----------|
| Category |                 |        |        |                 | lb/d             | day             |                 |                   |                  |                 |          |           | lb/d      | day             |     |          |
| Hauling  | 0.0000          | 0.0000 | 0.0000 | 0.0000          | 0.0000           | 0.0000          | 0.0000          | 0.0000            | 0.0000           | 0.0000          |          | 0.0000    | 0.0000    | 0.0000          |     | 0.0000   |
| Vendor   | 3.5300e-<br>003 | 0.1074 | 0.0273 | 2.8000e-<br>004 | 6.7700e-<br>003  | 3.1000e-<br>004 | 7.0800e-<br>003 | 1.9500e-<br>003   | 3.0000e-<br>004  | 2.2500e-<br>003 |          | 29.0344   | 29.0344   | 1.6300e-<br>003 |     | 29.0751  |
| Worker   | 0.1643          | 0.1394 | 1.2261 | 3.0400e-<br>003 | 0.3286           | 2.5600e-<br>003 | 0.3312          | 0.0872            | 2.3600e-<br>003  | 0.0895          |          | 302.9785  | 302.9785  | 0.0109          |     | 303.2505 |
| Total    | 0.1678          | 0.2468 | 1.2534 | 3.3200e-<br>003 | 0.3354           | 2.8700e-<br>003 | 0.3382          | 0.0891            | 2.6600e-<br>003  | 0.0918          |          | 332.0129  | 332.0129  | 0.0125          |     | 332.3256 |

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## Lico Subdivision Project - Monterey Bay Unified APCD Air District, Winter

# 3.9 Building Construction - Phase II - 2022 <u>Mitigated Construction On-Site</u>

|          | ROG    | NOx     | СО      | SO2    | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2      | Total CO2      | CH4    | N2O | CO2e           |
|----------|--------|---------|---------|--------|------------------|-----------------|---------------|-------------------|------------------|-------------|----------|----------------|----------------|--------|-----|----------------|
| Category |        |         |         |        | lb/d             | day             |               |                   |                  |             |          |                | lb/c           | lay    |     |                |
|          | 2.6834 | 26.4913 | 27.2071 | 0.0460 |                  | 1.3570          | 1.3570        |                   | 1.2781           | 1.2781      | 0.0000   | 4,418.993<br>7 | 4,418.993<br>7 | 1.0151 |     | 4,444.371<br>8 |
| Total    | 2.6834 | 26.4913 | 27.2071 | 0.0460 |                  | 1.3570          | 1.3570        |                   | 1.2781           | 1.2781      | 0.0000   | 4,418.993<br>7 | 4,418.993<br>7 | 1.0151 |     | 4,444.371<br>8 |

|          | ROG             | NOx    | CO     | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total   | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total     | Bio- CO2 | NBio- CO2 | Total CO2 | CH4             | N2O | CO2e     |
|----------|-----------------|--------|--------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|-----|----------|
| Category |                 |        |        |                 | lb/d             | day             |                 |                   |                  |                 |          |           | lb/d      | day             |     |          |
| Hauling  | 0.0000          | 0.0000 | 0.0000 | 0.0000          | 0.0000           | 0.0000          | 0.0000          | 0.0000            | 0.0000           | 0.0000          |          | 0.0000    | 0.0000    | 0.0000          |     | 0.0000   |
| Vendor   | 3.5300e-<br>003 | 0.1074 | 0.0273 | 2.8000e-<br>004 | 6.7700e-<br>003  | 3.1000e-<br>004 | 7.0800e-<br>003 | 1.9500e-<br>003   | 3.0000e-<br>004  | 2.2500e-<br>003 |          | 29.0344   | 29.0344   | 1.6300e-<br>003 |     | 29.0751  |
| Worker   | 0.1643          | 0.1394 | 1.2261 | 3.0400e-<br>003 | 0.3286           | 2.5600e-<br>003 | 0.3312          | 0.0872            | 2.3600e-<br>003  | 0.0895          |          | 302.9785  | 302.9785  | 0.0109          |     | 303.2505 |
| Total    | 0.1678          | 0.2468 | 1.2534 | 3.3200e-<br>003 | 0.3354           | 2.8700e-<br>003 | 0.3382          | 0.0891            | 2.6600e-<br>003  | 0.0918          |          | 332.0129  | 332.0129  | 0.0125          |     | 332.3256 |

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## Lico Subdivision Project - Monterey Bay Unified APCD Air District, Winter

# 3.10 Architectural Coating - Phase II - 2022 <u>Unmitigated Construction On-Site</u>

|                 | ROG    | NOx    | CO     | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4    | N2O | CO2e     |
|-----------------|--------|--------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|-------------|----------|-----------|-----------|--------|-----|----------|
| Category        |        |        |        |                 | lb/d             | day             |               |                   |                  |             |          |           | lb/c      | lay    |     |          |
| Archit. Coating | 7.0256 |        |        |                 |                  | 0.0000          | 0.0000        |                   | 0.0000           | 0.0000      |          |           | 0.0000    |        |     | 0.0000   |
| Off-Road        | 0.2045 | 1.4085 | 1.8136 | 2.9700e-<br>003 | <br>             | 0.0817          | 0.0817        |                   | 0.0817           | 0.0817      |          | 281.4481  | 281.4481  | 0.0183 |     | 281.9062 |
| Total           | 7.2302 | 1.4085 | 1.8136 | 2.9700e-<br>003 |                  | 0.0817          | 0.0817        |                   | 0.0817           | 0.0817      |          | 281.4481  | 281.4481  | 0.0183 |     | 281.9062 |

|          | ROG             | NOx    | СО     | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total   | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total     | Bio- CO2 | NBio- CO2 | Total CO2 | CH4             | N2O | CO2e     |
|----------|-----------------|--------|--------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|-----|----------|
| Category |                 |        |        |                 | lb/d             | day             |                 |                   |                  |                 |          |           | lb/d      | lay             |     |          |
| Hauling  | 0.0000          | 0.0000 | 0.0000 | 0.0000          | 0.0000           | 0.0000          | 0.0000          | 0.0000            | 0.0000           | 0.0000          |          | 0.0000    | 0.0000    | 0.0000          |     | 0.0000   |
| Vendor   | 3.5300e-<br>003 | 0.1074 | 0.0273 | 2.8000e-<br>004 | 6.7700e-<br>003  | 3.1000e-<br>004 | 7.0800e-<br>003 | 1.9500e-<br>003   | 3.0000e-<br>004  | 2.2500e-<br>003 |          | 29.0344   | 29.0344   | 1.6300e-<br>003 |     | 29.0751  |
| Worker   | 0.1643          | 0.1394 | 1.2261 | 3.0400e-<br>003 | 0.3286           | 2.5600e-<br>003 | 0.3312          | 0.0872            | 2.3600e-<br>003  | 0.0895          |          | 302.9785  | 302.9785  | 0.0109          |     | 303.2505 |
| Total    | 0.1678          | 0.2468 | 1.2534 | 3.3200e-<br>003 | 0.3354           | 2.8700e-<br>003 | 0.3382          | 0.0891            | 2.6600e-<br>003  | 0.0918          |          | 332.0129  | 332.0129  | 0.0125          |     | 332.3256 |

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## Lico Subdivision Project - Monterey Bay Unified APCD Air District, Winter

# 3.10 Architectural Coating - Phase II - 2022 Mitigated Construction On-Site

|                 | ROG    | NOx    | CO     | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4    | N2O    | CO2e     |
|-----------------|--------|--------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|-------------|----------|-----------|-----------|--------|--------|----------|
| Category        |        |        |        |                 | lb/d             | day             |               |                   |                  |             |          |           | lb/d      | day    |        |          |
| Archit. Coating | 7.0256 |        |        |                 |                  | 0.0000          | 0.0000        |                   | 0.0000           | 0.0000      |          |           | 0.0000    |        |        | 0.0000   |
|                 | 0.2045 | 1.4085 | 1.8136 | 2.9700e-<br>003 |                  | 0.0817          | 0.0817        | <br>              | 0.0817           | 0.0817      | 0.0000   | 281.4481  | 281.4481  | 0.0183 | i<br>i | 281.9062 |
| Total           | 7.2302 | 1.4085 | 1.8136 | 2.9700e-<br>003 |                  | 0.0817          | 0.0817        |                   | 0.0817           | 0.0817      | 0.0000   | 281.4481  | 281.4481  | 0.0183 |        | 281.9062 |

|          | ROG             | NOx    | СО     | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total   | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total     | Bio- CO2 | NBio- CO2 | Total CO2 | CH4             | N2O                 | CO2e     |
|----------|-----------------|--------|--------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|---------------------|----------|
| Category |                 |        |        |                 | lb/d             | day             |                 |                   |                  |                 | lb/d     | lay       |           |                 |                     |          |
| Hauling  | 0.0000          | 0.0000 | 0.0000 | 0.0000          | 0.0000           | 0.0000          | 0.0000          | 0.0000            | 0.0000           | 0.0000          |          | 0.0000    | 0.0000    | 0.0000          |                     | 0.0000   |
| Vendor   | 3.5300e-<br>003 | 0.1074 | 0.0273 | 2.8000e-<br>004 | 6.7700e-<br>003  | 3.1000e-<br>004 | 7.0800e-<br>003 | 1.9500e-<br>003   | 3.0000e-<br>004  | 2.2500e-<br>003 |          | 29.0344   | 29.0344   | 1.6300e-<br>003 | <br> <br> <br>      | 29.0751  |
| Worker   | 0.1643          | 0.1394 | 1.2261 | 3.0400e-<br>003 | 0.3286           | 2.5600e-<br>003 | 0.3312          | 0.0872            | 2.3600e-<br>003  | 0.0895          |          | 302.9785  | 302.9785  | 0.0109          | <br> <br> <br> <br> | 303.2505 |
| Total    | 0.1678          | 0.2468 | 1.2534 | 3.3200e-<br>003 | 0.3354           | 2.8700e-<br>003 | 0.3382          | 0.0891            | 2.6600e-<br>003  | 0.0918          |          | 332.0129  | 332.0129  | 0.0125          |                     | 332.3256 |

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## Lico Subdivision Project - Monterey Bay Unified APCD Air District, Winter

3.11 Paving - Phase III - 2022 Unmitigated Construction On-Site

|          | ROG    | NOx     | CO      | SO2    | Fugitive<br>PM10    | Exhaust<br>PM10 | PM10<br>Total | Fugitive<br>PM2.5   | Exhaust<br>PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2      | Total CO2      | CH4    | N2O                 | CO2e           |
|----------|--------|---------|---------|--------|---------------------|-----------------|---------------|---------------------|------------------|-------------|----------|----------------|----------------|--------|---------------------|----------------|
| Category |        |         |         |        | lb/d                | day             |               |                     |                  |             |          |                | lb/d           | day    |                     |                |
| Off-Road | 2.0439 | 21.3454 | 19.9747 | 0.0423 |                     | 0.9122          | 0.9122        |                     | 0.8556           | 0.8556      |          | 4,052.801<br>4 | 4,052.801<br>4 | 1.0980 |                     | 4,080.252<br>2 |
| Paving   | 0.2817 |         |         |        | <br> <br> <br> <br> | 0.0000          | 0.0000        | <br> <br> <br> <br> | 0.0000           | 0.0000      |          | 1              | 0.0000         |        | <br> <br> <br> <br> | 0.0000         |
| Total    | 2.3256 | 21.3454 | 19.9747 | 0.0423 |                     | 0.9122          | 0.9122        |                     | 0.8556           | 0.8556      |          | 4,052.801<br>4 | 4,052.801<br>4 | 1.0980 |                     | 4,080.252<br>2 |

|          | ROG             | NOx    | СО     | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total   | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total     | Bio- CO2 | NBio- CO2 | Total CO2 | CH4             | N2O                 | CO2e     |
|----------|-----------------|--------|--------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|---------------------|----------|
| Category |                 |        |        |                 | lb/d             | day             |                 |                   |                  |                 |          |           | lb/d      | day             |                     |          |
| Hauling  | 0.0000          | 0.0000 | 0.0000 | 0.0000          | 0.0000           | 0.0000          | 0.0000          | 0.0000            | 0.0000           | 0.0000          |          | 0.0000    | 0.0000    | 0.0000          |                     | 0.0000   |
| Vendor   | 3.5300e-<br>003 | 0.1074 | 0.0273 | 2.8000e-<br>004 | 6.7700e-<br>003  | 3.1000e-<br>004 | 7.0800e-<br>003 | 1.9500e-<br>003   | 3.0000e-<br>004  | 2.2500e-<br>003 |          | 29.0344   | 29.0344   | 1.6300e-<br>003 | <br> <br> <br> <br> | 29.0751  |
| Worker   | 0.0821          | 0.0697 | 0.6130 | 1.5200e-<br>003 | 0.1643           | 1.2800e-<br>003 | 0.1656          | 0.0436            | 1.1800e-<br>003  | 0.0448          |          | 151.4893  | 151.4893  | 5.4400e-<br>003 | <br> <br> <br> <br> | 151.6252 |
| Total    | 0.0857          | 0.1771 | 0.6403 | 1.8000e-<br>003 | 0.1711           | 1.5900e-<br>003 | 0.1727          | 0.0455            | 1.4800e-<br>003  | 0.0470          |          | 180.5237  | 180.5237  | 7.0700e-<br>003 |                     | 180.7004 |

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## Lico Subdivision Project - Monterey Bay Unified APCD Air District, Winter

3.11 Paving - Phase III - 2022 Mitigated Construction On-Site

|          | ROG    | NOx     | СО      | SO2    | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2        | Total CO2      | CH4    | N2O | CO2e           |
|----------|--------|---------|---------|--------|------------------|-----------------|---------------|-------------------|------------------|-------------|----------|------------------|----------------|--------|-----|----------------|
| Category |        |         |         |        | lb/d             | day             |               |                   |                  |             |          |                  | lb/d           | day    |     |                |
| Off-Road | 2.0439 | 21.3454 | 19.9747 | 0.0423 |                  | 0.9122          | 0.9122        |                   | 0.8556           | 0.8556      | 0.0000   | 4,052.801<br>4   | 4,052.801<br>4 | 1.0980 |     | 4,080.252<br>2 |
| Paving   | 0.2817 |         |         |        | <br> <br> <br>   | 0.0000          | 0.0000        |                   | 0.0000           | 0.0000      |          | !<br>!<br>!<br>! | 0.0000         |        |     | 0.0000         |
| Total    | 2.3256 | 21.3454 | 19.9747 | 0.0423 |                  | 0.9122          | 0.9122        |                   | 0.8556           | 0.8556      | 0.0000   | 4,052.801<br>4   | 4,052.801<br>4 | 1.0980 |     | 4,080.252<br>2 |

|          | ROG             | NOx    | CO     | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total   | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total     | Bio- CO2 | NBio- CO2 | Total CO2 | CH4             | N2O | CO2e     |
|----------|-----------------|--------|--------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|-----|----------|
| Category |                 |        |        |                 | lb/d             | day             |                 |                   |                  |                 |          |           | lb/d      | day             |     |          |
| Hauling  | 0.0000          | 0.0000 | 0.0000 | 0.0000          | 0.0000           | 0.0000          | 0.0000          | 0.0000            | 0.0000           | 0.0000          |          | 0.0000    | 0.0000    | 0.0000          |     | 0.0000   |
| Vendor   | 3.5300e-<br>003 | 0.1074 | 0.0273 | 2.8000e-<br>004 | 6.7700e-<br>003  | 3.1000e-<br>004 | 7.0800e-<br>003 | 1.9500e-<br>003   | 3.0000e-<br>004  | 2.2500e-<br>003 |          | 29.0344   | 29.0344   | 1.6300e-<br>003 |     | 29.0751  |
| Worker   | 0.0821          | 0.0697 | 0.6130 | 1.5200e-<br>003 | 0.1643           | 1.2800e-<br>003 | 0.1656          | 0.0436            | 1.1800e-<br>003  | 0.0448          |          | 151.4893  | 151.4893  | 5.4400e-<br>003 |     | 151.6252 |
| Total    | 0.0857          | 0.1771 | 0.6403 | 1.8000e-<br>003 | 0.1711           | 1.5900e-<br>003 | 0.1727          | 0.0455            | 1.4800e-<br>003  | 0.0470          |          | 180.5237  | 180.5237  | 7.0700e-<br>003 |     | 180.7004 |

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## Lico Subdivision Project - Monterey Bay Unified APCD Air District, Winter

3.11 Paving - Phase III - 2023
Unmitigated Construction On-Site

|          | ROG    | NOx     | CO      | SO2    | Fugitive<br>PM10    | Exhaust<br>PM10 | PM10<br>Total | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2      | Total CO2      | CH4    | N2O | CO2e           |
|----------|--------|---------|---------|--------|---------------------|-----------------|---------------|-------------------|------------------|-------------|----------|----------------|----------------|--------|-----|----------------|
| Category |        |         |         |        | lb/d                | day             |               |                   |                  |             |          |                | lb/c           | lay    |     |                |
| Off-Road | 1.9237 | 19.5132 | 19.9341 | 0.0423 |                     | 0.8184          | 0.8184        |                   | 0.7672           | 0.7672      |          | 4,052.082<br>7 | 4,052.082<br>7 | 1.0939 |     | 4,079.429<br>9 |
| Paving   | 0.2817 |         |         |        | <br> <br> <br> <br> | 0.0000          | 0.0000        | 1                 | 0.0000           | 0.0000      |          | 1              | 0.0000         |        |     | 0.0000         |
| Total    | 2.2053 | 19.5132 | 19.9341 | 0.0423 |                     | 0.8184          | 0.8184        |                   | 0.7672           | 0.7672      |          | 4,052.082<br>7 | 4,052.082<br>7 | 1.0939 |     | 4,079.429<br>9 |

|          | ROG             | NOx    | СО     | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total   | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total     | Bio- CO2 | NBio- CO2 | Total CO2 | CH4             | N2O | CO2e     |
|----------|-----------------|--------|--------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|-----|----------|
| Category |                 |        |        |                 | lb/              | day             |                 |                   |                  |                 |          |           | lb/d      | day             |     |          |
| Hauling  | 0.0000          | 0.0000 | 0.0000 | 0.0000          | 0.0000           | 0.0000          | 0.0000          | 0.0000            | 0.0000           | 0.0000          |          | 0.0000    | 0.0000    | 0.0000          |     | 0.0000   |
| Vendor   | 2.6500e-<br>003 | 0.0883 | 0.0231 | 2.7000e-<br>004 | 6.7700e-<br>003  | 1.3000e-<br>004 | 6.9000e-<br>003 | 1.9500e-<br>003   | 1.3000e-<br>004  | 2.0800e-<br>003 |          | 28.5170   | 28.5170   | 1.2600e-<br>003 |     | 28.5485  |
| Worker   | 0.0765          | 0.0625 | 0.5579 | 1.4700e-<br>003 | 0.1643           | 1.2400e-<br>003 | 0.1655          | 0.0436            | 1.1400e-<br>003  | 0.0447          |          | 145.8660  | 145.8660  | 4.8400e-<br>003 |     | 145.9870 |
| Total    | 0.0791          | 0.1508 | 0.5810 | 1.7400e-<br>003 | 0.1711           | 1.3700e-<br>003 | 0.1724          | 0.0455            | 1.2700e-<br>003  | 0.0468          |          | 174.3829  | 174.3829  | 6.1000e-<br>003 |     | 174.5355 |

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## Lico Subdivision Project - Monterey Bay Unified APCD Air District, Winter

3.11 Paving - Phase III - 2023 Mitigated Construction On-Site

|          | ROG    | NOx     | CO      | SO2    | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5<br>Total | Bio- CO2 | NBio- CO2      | Total CO2      | CH4    | N2O | CO2e           |
|----------|--------|---------|---------|--------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|----------------|----------------|--------|-----|----------------|
| Category |        |         |         |        | lb/d             | day             |               |                   |                  |                |          |                | lb/c           | lay    |     |                |
| Off-Road | 1.9237 | 19.5132 | 19.9341 | 0.0423 |                  | 0.8184          | 0.8184        |                   | 0.7672           | 0.7672         | 0.0000   | 4,052.082<br>7 | 4,052.082<br>7 | 1.0939 |     | 4,079.429<br>9 |
| Paving   | 0.2817 |         |         |        | <br>             | 0.0000          | 0.0000        | i<br>i            | 0.0000           | 0.0000         |          | i<br>i<br>i    | 0.0000         |        |     | 0.0000         |
| Total    | 2.2053 | 19.5132 | 19.9341 | 0.0423 |                  | 0.8184          | 0.8184        |                   | 0.7672           | 0.7672         | 0.0000   | 4,052.082<br>7 | 4,052.082<br>7 | 1.0939 |     | 4,079.429<br>9 |

|          | ROG             | NOx    | CO     | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total   | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total     | Bio- CO2 | NBio- CO2 | Total CO2 | CH4             | N2O | CO2e     |
|----------|-----------------|--------|--------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|-----|----------|
| Category |                 |        |        |                 | lb/d             | day             |                 |                   |                  |                 |          |           | lb/d      | day             |     |          |
| Hauling  | 0.0000          | 0.0000 | 0.0000 | 0.0000          | 0.0000           | 0.0000          | 0.0000          | 0.0000            | 0.0000           | 0.0000          |          | 0.0000    | 0.0000    | 0.0000          |     | 0.0000   |
| Vendor   | 2.6500e-<br>003 | 0.0883 | 0.0231 | 2.7000e-<br>004 | 6.7700e-<br>003  | 1.3000e-<br>004 | 6.9000e-<br>003 | 1.9500e-<br>003   | 1.3000e-<br>004  | 2.0800e-<br>003 |          | 28.5170   | 28.5170   | 1.2600e-<br>003 |     | 28.5485  |
| Worker   | 0.0765          | 0.0625 | 0.5579 | 1.4700e-<br>003 | 0.1643           | 1.2400e-<br>003 | 0.1655          | 0.0436            | 1.1400e-<br>003  | 0.0447          |          | 145.8660  | 145.8660  | 4.8400e-<br>003 |     | 145.9870 |
| Total    | 0.0791          | 0.1508 | 0.5810 | 1.7400e-<br>003 | 0.1711           | 1.3700e-<br>003 | 0.1724          | 0.0455            | 1.2700e-<br>003  | 0.0468          |          | 174.3829  | 174.3829  | 6.1000e-<br>003 |     | 174.5355 |

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## Lico Subdivision Project - Monterey Bay Unified APCD Air District, Winter

# 3.12 Building Construction - Phase III - 2023 <u>Unmitigated Construction On-Site</u>

|          | ROG    | NOx     | CO      | SO2    | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2      | Total CO2      | CH4    | N2O | CO2e           |
|----------|--------|---------|---------|--------|------------------|-----------------|---------------|-------------------|------------------|-------------|----------|----------------|----------------|--------|-----|----------------|
| Category |        |         |         |        | lb/d             | day             |               |                   |                  |             |          |                | lb/c           | lay    |     |                |
|          | 2.5104 | 24.4825 | 27.0748 | 0.0460 |                  | 1.2115          | 1.2115        |                   | 1.1402           | 1.1402      |          | 4,419.809<br>0 | 4,419.809<br>0 | 1.0087 |     | 4,445.027<br>5 |
| Total    | 2.5104 | 24.4825 | 27.0748 | 0.0460 |                  | 1.2115          | 1.2115        |                   | 1.1402           | 1.1402      |          | 4,419.809<br>0 | 4,419.809<br>0 | 1.0087 |     | 4,445.027<br>5 |

|          | ROG             | NOx    | CO     | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total   | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total     | Bio- CO2 | NBio- CO2 | Total CO2 | CH4             | N2O | CO2e     |
|----------|-----------------|--------|--------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|-----|----------|
| Category |                 |        |        |                 | lb/d             | day             |                 |                   |                  |                 |          |           | lb/d      | lay             |     |          |
| Hauling  | 0.0000          | 0.0000 | 0.0000 | 0.0000          | 0.0000           | 0.0000          | 0.0000          | 0.0000            | 0.0000           | 0.0000          |          | 0.0000    | 0.0000    | 0.0000          |     | 0.0000   |
| Vendor   | 2.6500e-<br>003 | 0.0883 | 0.0231 | 2.7000e-<br>004 | 6.7700e-<br>003  | 1.3000e-<br>004 | 6.9000e-<br>003 | 1.9500e-<br>003   | 1.3000e-<br>004  | 2.0800e-<br>003 |          | 28.5170   | 28.5170   | 1.2600e-<br>003 |     | 28.5485  |
| Worker   | 0.1529          | 0.1249 | 1.1159 | 2.9300e-<br>003 | 0.3286           | 2.4800e-<br>003 | 0.3311          | 0.0872            | 2.2900e-<br>003  | 0.0894          |          | 291.7319  | 291.7319  | 9.6900e-<br>003 |     | 291.9740 |
| Total    | 0.1556          | 0.2133 | 1.1390 | 3.2000e-<br>003 | 0.3354           | 2.6100e-<br>003 | 0.3380          | 0.0891            | 2.4200e-<br>003  | 0.0915          |          | 320.2489  | 320.2489  | 0.0110          |     | 320.5225 |

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## Lico Subdivision Project - Monterey Bay Unified APCD Air District, Winter

# 3.12 Building Construction - Phase III - 2023 Mitigated Construction On-Site

|          | ROG    | NOx     | СО      | SO2    | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2      | Total CO2      | CH4    | N2O | CO2e           |
|----------|--------|---------|---------|--------|------------------|-----------------|---------------|-------------------|------------------|-------------|----------|----------------|----------------|--------|-----|----------------|
| Category |        |         |         |        | lb/d             | day             |               |                   |                  |             |          |                | lb/c           | lay    |     |                |
|          | 2.5104 | 24.4825 | 27.0748 | 0.0460 |                  | 1.2115          | 1.2115        |                   | 1.1402           | 1.1402      | 0.0000   | 4,419.809<br>0 | 4,419.809<br>0 | 1.0087 |     | 4,445.027<br>5 |
| Total    | 2.5104 | 24.4825 | 27.0748 | 0.0460 |                  | 1.2115          | 1.2115        |                   | 1.1402           | 1.1402      | 0.0000   | 4,419.809<br>0 | 4,419.809<br>0 | 1.0087 |     | 4,445.027<br>5 |

|          | ROG             | NOx    | CO     | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total   | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total     | Bio- CO2 | NBio- CO2 | Total CO2 | CH4             | N2O | CO2e     |
|----------|-----------------|--------|--------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|-----|----------|
| Category |                 |        |        |                 | lb/d             | day             |                 |                   |                  |                 |          |           | lb/d      | day             |     |          |
| Hauling  | 0.0000          | 0.0000 | 0.0000 | 0.0000          | 0.0000           | 0.0000          | 0.0000          | 0.0000            | 0.0000           | 0.0000          |          | 0.0000    | 0.0000    | 0.0000          |     | 0.0000   |
| Vendor   | 2.6500e-<br>003 | 0.0883 | 0.0231 | 2.7000e-<br>004 | 6.7700e-<br>003  | 1.3000e-<br>004 | 6.9000e-<br>003 | 1.9500e-<br>003   | 1.3000e-<br>004  | 2.0800e-<br>003 |          | 28.5170   | 28.5170   | 1.2600e-<br>003 |     | 28.5485  |
| Worker   | 0.1529          | 0.1249 | 1.1159 | 2.9300e-<br>003 | 0.3286           | 2.4800e-<br>003 | 0.3311          | 0.0872            | 2.2900e-<br>003  | 0.0894          |          | 291.7319  | 291.7319  | 9.6900e-<br>003 |     | 291.9740 |
| Total    | 0.1556          | 0.2133 | 1.1390 | 3.2000e-<br>003 | 0.3354           | 2.6100e-<br>003 | 0.3380          | 0.0891            | 2.4200e-<br>003  | 0.0915          |          | 320.2489  | 320.2489  | 0.0110          |     | 320.5225 |

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## Lico Subdivision Project - Monterey Bay Unified APCD Air District, Winter

# 3.13 Architectural Coating - Phase III - 2023 <u>Unmitigated Construction On-Site</u>

|                 | ROG    | NOx    | CO     | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total | Fugitive<br>PM2.5   | Exhaust<br>PM2.5 | PM2.5<br>Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4    | N2O                 | CO2e     |
|-----------------|--------|--------|--------|-----------------|------------------|-----------------|---------------|---------------------|------------------|----------------|----------|-----------|-----------|--------|---------------------|----------|
| Category        |        |        |        |                 | lb/d             | day             |               |                     |                  |                |          |           | lb/d      | day    |                     |          |
| Archit. Coating |        |        |        |                 |                  | 0.0000          | 0.0000        |                     | 0.0000           | 0.0000         |          |           | 0.0000    |        |                     | 0.0000   |
| Off-Road        | 0.1917 | 1.3030 | 1.8111 | 2.9700e-<br>003 |                  | 0.0708          | 0.0708        | <br> <br> <br> <br> | 0.0708           | 0.0708         |          | 281.4481  | 281.4481  | 0.0168 | <br> <br> <br> <br> | 281.8690 |
| Total           | 7.2173 | 1.3030 | 1.8111 | 2.9700e-<br>003 |                  | 0.0708          | 0.0708        |                     | 0.0708           | 0.0708         |          | 281.4481  | 281.4481  | 0.0168 |                     | 281.8690 |

|          | ROG             | NOx    | СО     | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total   | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total     | Bio- CO2 | NBio- CO2 | Total CO2 | CH4             | N2O | CO2e     |
|----------|-----------------|--------|--------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|-----|----------|
| Category |                 |        |        |                 | lb/d             | day             |                 |                   |                  |                 |          |           | lb/d      | day             |     |          |
| Hauling  | 0.0000          | 0.0000 | 0.0000 | 0.0000          | 0.0000           | 0.0000          | 0.0000          | 0.0000            | 0.0000           | 0.0000          |          | 0.0000    | 0.0000    | 0.0000          |     | 0.0000   |
| Vendor   | 2.6500e-<br>003 | 0.0883 | 0.0231 | 2.7000e-<br>004 | 6.7700e-<br>003  | 1.3000e-<br>004 | 6.9000e-<br>003 | 1.9500e-<br>003   | 1.3000e-<br>004  | 2.0800e-<br>003 |          | 28.5170   | 28.5170   | 1.2600e-<br>003 |     | 28.5485  |
| Worker   | 0.1529          | 0.1249 | 1.1159 | 2.9300e-<br>003 | 0.3286           | 2.4800e-<br>003 | 0.3311          | 0.0872            | 2.2900e-<br>003  | 0.0894          |          | 291.7319  | 291.7319  | 9.6900e-<br>003 |     | 291.9740 |
| Total    | 0.1556          | 0.2133 | 1.1390 | 3.2000e-<br>003 | 0.3354           | 2.6100e-<br>003 | 0.3380          | 0.0891            | 2.4200e-<br>003  | 0.0915          |          | 320.2489  | 320.2489  | 0.0110          |     | 320.5225 |

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## Lico Subdivision Project - Monterey Bay Unified APCD Air District, Winter

# 3.13 Architectural Coating - Phase III - 2023 Mitigated Construction On-Site

|                 | ROG    | NOx    | CO     | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4    | N2O | CO2e     |
|-----------------|--------|--------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|-------------|----------|-----------|-----------|--------|-----|----------|
| Category        |        |        |        |                 | lb/d             | day             |               |                   |                  |             |          |           | lb/d      | day    |     |          |
| Archit. Coating | 7.0256 |        |        |                 |                  | 0.0000          | 0.0000        |                   | 0.0000           | 0.0000      |          | 1         | 0.0000    |        |     | 0.0000   |
| Off-Road        | 0.1917 | 1.3030 | 1.8111 | 2.9700e-<br>003 |                  | 0.0708          | 0.0708        |                   | 0.0708           | 0.0708      | 0.0000   | 281.4481  | 281.4481  | 0.0168 |     | 281.8690 |
| Total           | 7.2173 | 1.3030 | 1.8111 | 2.9700e-<br>003 |                  | 0.0708          | 0.0708        |                   | 0.0708           | 0.0708      | 0.0000   | 281.4481  | 281.4481  | 0.0168 |     | 281.8690 |

|          | ROG             | NOx    | СО     | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total   | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total     | Bio- CO2 | NBio- CO2 | Total CO2 | CH4             | N2O | CO2e     |
|----------|-----------------|--------|--------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|-----|----------|
| Category |                 |        |        |                 | lb/              | day             |                 |                   |                  |                 |          |           | lb/d      | day             |     |          |
| Hauling  | 0.0000          | 0.0000 | 0.0000 | 0.0000          | 0.0000           | 0.0000          | 0.0000          | 0.0000            | 0.0000           | 0.0000          |          | 0.0000    | 0.0000    | 0.0000          |     | 0.0000   |
| Vendor   | 2.6500e-<br>003 | 0.0883 | 0.0231 | 2.7000e-<br>004 | 6.7700e-<br>003  | 1.3000e-<br>004 | 6.9000e-<br>003 | 1.9500e-<br>003   | 1.3000e-<br>004  | 2.0800e-<br>003 |          | 28.5170   | 28.5170   | 1.2600e-<br>003 |     | 28.5485  |
| Worker   | 0.1529          | 0.1249 | 1.1159 | 2.9300e-<br>003 | 0.3286           | 2.4800e-<br>003 | 0.3311          | 0.0872            | 2.2900e-<br>003  | 0.0894          |          | 291.7319  | 291.7319  | 9.6900e-<br>003 |     | 291.9740 |
| Total    | 0.1556          | 0.2133 | 1.1390 | 3.2000e-<br>003 | 0.3354           | 2.6100e-<br>003 | 0.3380          | 0.0891            | 2.4200e-<br>003  | 0.0915          |          | 320.2489  | 320.2489  | 0.0110          |     | 320.5225 |

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## Lico Subdivision Project - Monterey Bay Unified APCD Air District, Winter

3.14 Paving - Phase IV - 2023 Unmitigated Construction On-Site

|          | ROG    | NOx     | CO                    | SO2    | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2      | Total CO2      | CH4    | N2O                 | CO2e           |
|----------|--------|---------|-----------------------|--------|------------------|-----------------|---------------|-------------------|------------------|-------------|----------|----------------|----------------|--------|---------------------|----------------|
| Category |        |         |                       |        | lb/d             | day             |               |                   |                  |             |          |                | lb/d           | day    |                     |                |
| Off-Road | 1.9237 | 19.5132 | 19.9341               | 0.0423 |                  | 0.8184          | 0.8184        | !<br>!            | 0.7672           | 0.7672      |          | 4,052.082<br>7 | 4,052.082<br>7 | 1.0939 |                     | 4,079.429<br>9 |
| Paving   | 0.2817 |         | 1<br>1<br>1<br>1<br>1 |        |                  | 0.0000          | 0.0000        | 1                 | 0.0000           | 0.0000      |          |                | 0.0000         |        | <br> <br> <br> <br> | 0.0000         |
| Total    | 2.2053 | 19.5132 | 19.9341               | 0.0423 |                  | 0.8184          | 0.8184        |                   | 0.7672           | 0.7672      |          | 4,052.082<br>7 | 4,052.082<br>7 | 1.0939 |                     | 4,079.429<br>9 |

|          | ROG             | NOx    | СО     | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total   | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total     | Bio- CO2 | NBio- CO2 | Total CO2 | CH4             | N2O                 | CO2e     |
|----------|-----------------|--------|--------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|---------------------|----------|
| Category |                 |        |        |                 | lb/d             | day             |                 |                   |                  |                 |          |           | lb/d      | day             |                     |          |
| Hauling  | 0.0000          | 0.0000 | 0.0000 | 0.0000          | 0.0000           | 0.0000          | 0.0000          | 0.0000            | 0.0000           | 0.0000          |          | 0.0000    | 0.0000    | 0.0000          |                     | 0.0000   |
| Vendor   | 2.6500e-<br>003 | 0.0883 | 0.0231 | 2.7000e-<br>004 | 6.7700e-<br>003  | 1.3000e-<br>004 | 6.9000e-<br>003 | 1.9500e-<br>003   | 1.3000e-<br>004  | 2.0800e-<br>003 |          | 28.5170   | 28.5170   | 1.2600e-<br>003 | <br> <br> <br> <br> | 28.5485  |
| Worker   | 0.0765          | 0.0625 | 0.5579 | 1.4700e-<br>003 | 0.1643           | 1.2400e-<br>003 | 0.1655          | 0.0436            | 1.1400e-<br>003  | 0.0447          |          | 145.8660  | 145.8660  | 4.8400e-<br>003 | <br> <br> <br> <br> | 145.9870 |
| Total    | 0.0791          | 0.1508 | 0.5810 | 1.7400e-<br>003 | 0.1711           | 1.3700e-<br>003 | 0.1724          | 0.0455            | 1.2700e-<br>003  | 0.0468          |          | 174.3829  | 174.3829  | 6.1000e-<br>003 |                     | 174.5355 |

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## Lico Subdivision Project - Monterey Bay Unified APCD Air District, Winter

3.14 Paving - Phase IV - 2023 Mitigated Construction On-Site

|          | ROG    | NOx     | CO      | SO2    | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2      | Total CO2      | CH4    | N2O              | CO2e           |
|----------|--------|---------|---------|--------|------------------|-----------------|---------------|-------------------|------------------|-------------|----------|----------------|----------------|--------|------------------|----------------|
| Category |        |         |         |        | lb/d             | day             |               |                   |                  |             |          |                | lb/c           | lay    |                  |                |
| Off-Road | 1.9237 | 19.5132 | 19.9341 | 0.0423 |                  | 0.8184          | 0.8184        |                   | 0.7672           | 0.7672      | 0.0000   | 4,052.082<br>7 | 4,052.082<br>7 | 1.0939 |                  | 4,079.429<br>9 |
| Paving   | 0.2817 |         |         |        |                  | 0.0000          | 0.0000        |                   | 0.0000           | 0.0000      |          |                | 0.0000         |        | 1<br>1<br>1<br>1 | 0.0000         |
| Total    | 2.2053 | 19.5132 | 19.9341 | 0.0423 |                  | 0.8184          | 0.8184        |                   | 0.7672           | 0.7672      | 0.0000   | 4,052.082<br>7 | 4,052.082<br>7 | 1.0939 |                  | 4,079.429<br>9 |

|          | ROG             | NOx    | CO     | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total   | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total     | Bio- CO2 | NBio- CO2 | Total CO2 | CH4             | N2O | CO2e     |
|----------|-----------------|--------|--------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|-----|----------|
| Category |                 |        |        |                 | lb/d             | day             |                 |                   |                  |                 |          |           | lb/d      | day             |     |          |
| Hauling  | 0.0000          | 0.0000 | 0.0000 | 0.0000          | 0.0000           | 0.0000          | 0.0000          | 0.0000            | 0.0000           | 0.0000          |          | 0.0000    | 0.0000    | 0.0000          |     | 0.0000   |
| Vendor   | 2.6500e-<br>003 | 0.0883 | 0.0231 | 2.7000e-<br>004 | 6.7700e-<br>003  | 1.3000e-<br>004 | 6.9000e-<br>003 | 1.9500e-<br>003   | 1.3000e-<br>004  | 2.0800e-<br>003 |          | 28.5170   | 28.5170   | 1.2600e-<br>003 |     | 28.5485  |
| Worker   | 0.0765          | 0.0625 | 0.5579 | 1.4700e-<br>003 | 0.1643           | 1.2400e-<br>003 | 0.1655          | 0.0436            | 1.1400e-<br>003  | 0.0447          |          | 145.8660  | 145.8660  | 4.8400e-<br>003 |     | 145.9870 |
| Total    | 0.0791          | 0.1508 | 0.5810 | 1.7400e-<br>003 | 0.1711           | 1.3700e-<br>003 | 0.1724          | 0.0455            | 1.2700e-<br>003  | 0.0468          |          | 174.3829  | 174.3829  | 6.1000e-<br>003 |     | 174.5355 |

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## Lico Subdivision Project - Monterey Bay Unified APCD Air District, Winter

3.14 Paving - Phase IV - 2024 Unmitigated Construction On-Site

|            | ROG    | NOx     | CO          | SO2    | Fugitive<br>PM10    | Exhaust<br>PM10 | PM10<br>Total | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2      | Total CO2      | CH4    | N2O | CO2e           |
|------------|--------|---------|-------------|--------|---------------------|-----------------|---------------|-------------------|------------------|-------------|----------|----------------|----------------|--------|-----|----------------|
| Category   |        |         |             |        | lb/d                | day             |               |                   |                  |             |          |                | lb/d           | day    |     |                |
| - Cirrioda | 1.8342 | 18.2180 | 19.9122     | 0.0423 |                     | 0.7474          | 0.7474        |                   | 0.7000           | 0.7000      |          | 4,051.511<br>8 | 4,051.5118     | 1.0924 |     | 4,078.821<br>9 |
| Paving     | 0.2817 |         | 1<br>1<br>1 |        | <br> <br> <br> <br> | 0.0000          | 0.0000        | i<br>i            | 0.0000           | 0.0000      |          | !<br>!<br>!    | 0.0000         |        |     | 0.0000         |
| Total      | 2.1158 | 18.2180 | 19.9122     | 0.0423 |                     | 0.7474          | 0.7474        |                   | 0.7000           | 0.7000      |          | 4,051.511<br>8 | 4,051.511<br>8 | 1.0924 |     | 4,078.821<br>9 |

|          | ROG             | NOx    | СО     | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total   | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total     | Bio- CO2 | NBio- CO2 | Total CO2 | CH4             | N2O | CO2e     |
|----------|-----------------|--------|--------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|-----|----------|
| Category |                 |        |        |                 | lb/d             | day             |                 |                   |                  |                 |          |           | lb/d      | day             |     |          |
| Hauling  | 0.0000          | 0.0000 | 0.0000 | 0.0000          | 0.0000           | 0.0000          | 0.0000          | 0.0000            | 0.0000           | 0.0000          |          | 0.0000    | 0.0000    | 0.0000          |     | 0.0000   |
| Vendor   | 2.5100e-<br>003 | 0.0863 | 0.0214 | 2.7000e-<br>004 | 6.7700e-<br>003  | 1.2000e-<br>004 | 6.8900e-<br>003 | 1.9500e-<br>003   | 1.2000e-<br>004  | 2.0700e-<br>003 |          | 28.2890   | 28.2890   | 1.2500e-<br>003 |     | 28.3202  |
| Worker   | 0.0715          | 0.0561 | 0.5113 | 1.4100e-<br>003 | 0.1643           | 1.2000e-<br>003 | 0.1655          | 0.0436            | 1.1100e-<br>003  | 0.0447          |          | 140.2419  | 140.2419  | 4.3300e-<br>003 |     | 140.3500 |
| Total    | 0.0740          | 0.1424 | 0.5327 | 1.6800e-<br>003 | 0.1711           | 1.3200e-<br>003 | 0.1724          | 0.0455            | 1.2300e-<br>003  | 0.0468          |          | 168.5309  | 168.5309  | 5.5800e-<br>003 |     | 168.6702 |

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## Lico Subdivision Project - Monterey Bay Unified APCD Air District, Winter

3.14 Paving - Phase IV - 2024 Mitigated Construction On-Site

|          | ROG    | NOx     | CO      | SO2    | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2      | Total CO2      | CH4    | N2O | CO2e           |
|----------|--------|---------|---------|--------|------------------|-----------------|---------------|-------------------|------------------|-------------|----------|----------------|----------------|--------|-----|----------------|
| Category |        |         |         |        | lb/d             | day             |               |                   |                  |             |          |                | lb/d           | lay    |     |                |
| Off-Road | 1.8342 | 18.2180 | 19.9122 | 0.0423 |                  | 0.7474          | 0.7474        |                   | 0.7000           | 0.7000      | 0.0000   | 4,051.5118     | 4,051.5118     | 1.0924 |     | 4,078.821<br>9 |
| Paving   | 0.2817 | <br>    |         |        |                  | 0.0000          | 0.0000        |                   | 0.0000           | 0.0000      |          |                | 0.0000         |        |     | 0.0000         |
| Total    | 2.1158 | 18.2180 | 19.9122 | 0.0423 |                  | 0.7474          | 0.7474        |                   | 0.7000           | 0.7000      | 0.0000   | 4,051.511<br>8 | 4,051.511<br>8 | 1.0924 |     | 4,078.821<br>9 |

|          | ROG             | NOx    | СО     | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total   | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total     | Bio- CO2 | NBio- CO2 | Total CO2 | CH4             | N2O | CO2e     |
|----------|-----------------|--------|--------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|-----|----------|
| Category |                 |        |        |                 | lb/d             | day             |                 |                   |                  |                 |          |           | lb/d      | day             |     |          |
| Hauling  | 0.0000          | 0.0000 | 0.0000 | 0.0000          | 0.0000           | 0.0000          | 0.0000          | 0.0000            | 0.0000           | 0.0000          |          | 0.0000    | 0.0000    | 0.0000          |     | 0.0000   |
| Vendor   | 2.5100e-<br>003 | 0.0863 | 0.0214 | 2.7000e-<br>004 | 6.7700e-<br>003  | 1.2000e-<br>004 | 6.8900e-<br>003 | 1.9500e-<br>003   | 1.2000e-<br>004  | 2.0700e-<br>003 |          | 28.2890   | 28.2890   | 1.2500e-<br>003 |     | 28.3202  |
| Worker   | 0.0715          | 0.0561 | 0.5113 | 1.4100e-<br>003 | 0.1643           | 1.2000e-<br>003 | 0.1655          | 0.0436            | 1.1100e-<br>003  | 0.0447          |          | 140.2419  | 140.2419  | 4.3300e-<br>003 |     | 140.3500 |
| Total    | 0.0740          | 0.1424 | 0.5327 | 1.6800e-<br>003 | 0.1711           | 1.3200e-<br>003 | 0.1724          | 0.0455            | 1.2300e-<br>003  | 0.0468          |          | 168.5309  | 168.5309  | 5.5800e-<br>003 |     | 168.6702 |

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## Lico Subdivision Project - Monterey Bay Unified APCD Air District, Winter

# 3.15 Building Construction - Phase IV - 2024 Unmitigated Construction On-Site

|          | ROG    | NOx     | СО      | SO2    | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2      | Total CO2      | CH4    | N2O | CO2e           |
|----------|--------|---------|---------|--------|------------------|-----------------|---------------|-------------------|------------------|-------------|----------|----------------|----------------|--------|-----|----------------|
| Category |        |         |         |        | lb/d             | day             |               |                   |                  |             |          |                | lb/c           | lay    |     |                |
| Off-Road | 2.3878 | 23.0730 | 27.0035 | 0.0460 |                  | 1.1069          | 1.1069        |                   | 1.0404           | 1.0404      |          | 4,419.976<br>7 | 4,419.976<br>7 | 1.0048 |     | 4,445.095<br>4 |
| Total    | 2.3878 | 23.0730 | 27.0035 | 0.0460 |                  | 1.1069          | 1.1069        |                   | 1.0404           | 1.0404      |          | 4,419.976<br>7 | 4,419.976<br>7 | 1.0048 |     | 4,445.095<br>4 |

|          | ROG             | NOx    | CO     | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total   | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5<br>Total  | Bio- CO2 | NBio- CO2 | Total CO2 | CH4             | N2O | CO2e     |
|----------|-----------------|--------|--------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|-----|----------|
| Category |                 |        |        |                 | lb/d             | day             |                 |                   |                  |                 |          |           | lb/d      | lay             |     |          |
| Hauling  | 0.0000          | 0.0000 | 0.0000 | 0.0000          | 0.0000           | 0.0000          | 0.0000          | 0.0000            | 0.0000           | 0.0000          |          | 0.0000    | 0.0000    | 0.0000          |     | 0.0000   |
| Vendor   | 2.5100e-<br>003 | 0.0863 | 0.0214 | 2.7000e-<br>004 | 6.7700e-<br>003  | 1.2000e-<br>004 | 6.8900e-<br>003 | 1.9500e-<br>003   | 1.2000e-<br>004  | 2.0700e-<br>003 |          | 28.2890   | 28.2890   | 1.2500e-<br>003 |     | 28.3202  |
| Worker   | 0.1430          | 0.1123 | 1.0225 | 2.8200e-<br>003 | 0.3286           | 2.4100e-<br>003 | 0.3310          | 0.0872            | 2.2200e-<br>003  | 0.0894          |          | 280.4838  | 280.4838  | 8.6500e-<br>003 |     | 280.7001 |
| Total    | 0.1455          | 0.1986 | 1.0439 | 3.0900e-<br>003 | 0.3354           | 2.5300e-<br>003 | 0.3379          | 0.0891            | 2.3400e-<br>003  | 0.0915          |          | 308.7728  | 308.7728  | 9.9000e-<br>003 |     | 309.0203 |

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## Lico Subdivision Project - Monterey Bay Unified APCD Air District, Winter

# 3.15 Building Construction - Phase IV - 2024 Mitigated Construction On-Site

|          | ROG    | NOx     | CO      | SO2    | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2      | Total CO2      | CH4    | N2O | CO2e           |
|----------|--------|---------|---------|--------|------------------|-----------------|---------------|-------------------|------------------|-------------|----------|----------------|----------------|--------|-----|----------------|
| Category |        |         |         |        | lb/d             | day             |               |                   |                  |             |          |                | lb/c           | lay    |     |                |
| Off-Road | 2.3878 | 23.0730 | 27.0035 | 0.0460 |                  | 1.1069          | 1.1069        |                   | 1.0404           | 1.0404      | 0.0000   | 4,419.976<br>7 | 4,419.976<br>7 | 1.0048 |     | 4,445.095<br>4 |
| Total    | 2.3878 | 23.0730 | 27.0035 | 0.0460 |                  | 1.1069          | 1.1069        |                   | 1.0404           | 1.0404      | 0.0000   | 4,419.976<br>7 | 4,419.976<br>7 | 1.0048 |     | 4,445.095<br>4 |

|          | ROG             | NOx    | CO     | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total   | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total     | Bio- CO2 | NBio- CO2 | Total CO2 | CH4             | N2O | CO2e     |
|----------|-----------------|--------|--------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|-----|----------|
| Category |                 |        |        |                 | lb/              | day             |                 |                   |                  |                 |          |           | lb/d      | day             |     |          |
| Hauling  | 0.0000          | 0.0000 | 0.0000 | 0.0000          | 0.0000           | 0.0000          | 0.0000          | 0.0000            | 0.0000           | 0.0000          |          | 0.0000    | 0.0000    | 0.0000          |     | 0.0000   |
| Vendor   | 2.5100e-<br>003 | 0.0863 | 0.0214 | 2.7000e-<br>004 | 6.7700e-<br>003  | 1.2000e-<br>004 | 6.8900e-<br>003 | 1.9500e-<br>003   | 1.2000e-<br>004  | 2.0700e-<br>003 |          | 28.2890   | 28.2890   | 1.2500e-<br>003 |     | 28.3202  |
| Worker   | 0.1430          | 0.1123 | 1.0225 | 2.8200e-<br>003 | 0.3286           | 2.4100e-<br>003 | 0.3310          | 0.0872            | 2.2200e-<br>003  | 0.0894          |          | 280.4838  | 280.4838  | 8.6500e-<br>003 |     | 280.7001 |
| Total    | 0.1455          | 0.1986 | 1.0439 | 3.0900e-<br>003 | 0.3354           | 2.5300e-<br>003 | 0.3379          | 0.0891            | 2.3400e-<br>003  | 0.0915          |          | 308.7728  | 308.7728  | 9.9000e-<br>003 |     | 309.0203 |

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## Lico Subdivision Project - Monterey Bay Unified APCD Air District, Winter

# 3.16 Architectural Coating - Phase IV - 2024 <u>Unmitigated Construction On-Site</u>

|                 | ROG    | NOx    | CO     | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4    | N2O            | CO2e     |
|-----------------|--------|--------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|-------------|----------|-----------|-----------|--------|----------------|----------|
| Category        |        |        |        |                 | lb/d             | day             |               |                   |                  |             |          |           | lb/d      | day    |                |          |
| Archit. Coating | 7.0256 |        |        |                 |                  | 0.0000          | 0.0000        |                   | 0.0000           | 0.0000      |          |           | 0.0000    |        |                | 0.0000   |
|                 | 0.1808 | 1.2188 | 1.8101 | 2.9700e-<br>003 |                  | 0.0609          | 0.0609        | <br>              | 0.0609           | 0.0609      |          | 281.4481  | 281.4481  | 0.0159 | <br> <br> <br> | 281.8443 |
| Total           | 7.2064 | 1.2188 | 1.8101 | 2.9700e-<br>003 |                  | 0.0609          | 0.0609        |                   | 0.0609           | 0.0609      |          | 281.4481  | 281.4481  | 0.0159 |                | 281.8443 |

|          | ROG             | NOx    | CO     | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total   | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total     | Bio- CO2 | NBio- CO2 | Total CO2 | CH4             | N2O | CO2e     |
|----------|-----------------|--------|--------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|-----|----------|
| Category |                 |        |        |                 | lb/d             | day             |                 |                   |                  |                 |          |           | lb/d      | day             |     |          |
| Hauling  | 0.0000          | 0.0000 | 0.0000 | 0.0000          | 0.0000           | 0.0000          | 0.0000          | 0.0000            | 0.0000           | 0.0000          |          | 0.0000    | 0.0000    | 0.0000          |     | 0.0000   |
| Vollage  | 2.5100e-<br>003 | 0.0863 | 0.0214 | 2.7000e-<br>004 | 6.7700e-<br>003  | 1.2000e-<br>004 | 6.8900e-<br>003 | 1.9500e-<br>003   | 1.2000e-<br>004  | 2.0700e-<br>003 |          | 28.2890   | 28.2890   | 1.2500e-<br>003 |     | 28.3202  |
| Worker   | 0.1430          | 0.1123 | 1.0225 | 2.8200e-<br>003 | 0.3286           | 2.4100e-<br>003 | 0.3310          | 0.0872            | 2.2200e-<br>003  | 0.0894          |          | 280.4838  | 280.4838  | 8.6500e-<br>003 |     | 280.7001 |
| Total    | 0.1455          | 0.1986 | 1.0439 | 3.0900e-<br>003 | 0.3354           | 2.5300e-<br>003 | 0.3379          | 0.0891            | 2.3400e-<br>003  | 0.0915          |          | 308.7728  | 308.7728  | 9.9000e-<br>003 |     | 309.0203 |

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## Lico Subdivision Project - Monterey Bay Unified APCD Air District, Winter

# 3.16 Architectural Coating - Phase IV - 2024 <u>Mitigated Construction On-Site</u>

|                 | ROG    | NOx    | СО     | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4    | N2O | CO2e     |
|-----------------|--------|--------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|-------------|----------|-----------|-----------|--------|-----|----------|
| Category        |        |        |        |                 | lb/d             | day             |               |                   |                  |             |          |           | lb/d      | day    |     |          |
| Archit. Coating | 7.0256 |        |        |                 |                  | 0.0000          | 0.0000        |                   | 0.0000           | 0.0000      |          |           | 0.0000    |        |     | 0.0000   |
|                 | 0.1808 | 1.2188 | 1.8101 | 2.9700e-<br>003 |                  | 0.0609          | 0.0609        |                   | 0.0609           | 0.0609      | 0.0000   | 281.4481  | 281.4481  | 0.0159 | ,   | 281.8443 |
| Total           | 7.2064 | 1.2188 | 1.8101 | 2.9700e-<br>003 |                  | 0.0609          | 0.0609        |                   | 0.0609           | 0.0609      | 0.0000   | 281.4481  | 281.4481  | 0.0159 |     | 281.8443 |

## **Mitigated Construction Off-Site**

|          | ROG             | NOx    | СО     | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total   | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total     | Bio- CO2 | NBio- CO2 | Total CO2 | CH4             | N2O | CO2e     |
|----------|-----------------|--------|--------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|-----|----------|
| Category |                 |        |        |                 | lb/d             | day             |                 |                   |                  |                 |          |           | lb/d      | day             |     |          |
| Hauling  | 0.0000          | 0.0000 | 0.0000 | 0.0000          | 0.0000           | 0.0000          | 0.0000          | 0.0000            | 0.0000           | 0.0000          |          | 0.0000    | 0.0000    | 0.0000          |     | 0.0000   |
| Vendor   | 2.5100e-<br>003 | 0.0863 | 0.0214 | 2.7000e-<br>004 | 6.7700e-<br>003  | 1.2000e-<br>004 | 6.8900e-<br>003 | 1.9500e-<br>003   | 1.2000e-<br>004  | 2.0700e-<br>003 |          | 28.2890   | 28.2890   | 1.2500e-<br>003 |     | 28.3202  |
| Worker   | 0.1430          | 0.1123 | 1.0225 | 2.8200e-<br>003 | 0.3286           | 2.4100e-<br>003 | 0.3310          | 0.0872            | 2.2200e-<br>003  | 0.0894          |          | 280.4838  | 280.4838  | 8.6500e-<br>003 |     | 280.7001 |
| Total    | 0.1455          | 0.1986 | 1.0439 | 3.0900e-<br>003 | 0.3354           | 2.5300e-<br>003 | 0.3379          | 0.0891            | 2.3400e-<br>003  | 0.0915          |          | 308.7728  | 308.7728  | 9.9000e-<br>003 |     | 309.0203 |

# 4.0 Operational Detail - Mobile

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## Lico Subdivision Project - Monterey Bay Unified APCD Air District, Winter

## **4.1 Mitigation Measures Mobile**

|             | ROG    | NOx     | CO      | SO2    | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2       | Total CO2       | CH4    | N2O | CO2e            |
|-------------|--------|---------|---------|--------|------------------|-----------------|---------------|-------------------|------------------|-------------|----------|-----------------|-----------------|--------|-----|-----------------|
| Category    |        |         |         |        | lb/d             | day             |               |                   |                  |             |          |                 | lb/c            | lay    |     |                 |
| Mitigated   | 2.5633 | 13.7673 | 31.5154 | 0.1052 | 9.0612           | 0.0869          | 9.1481        | 2.4261            | 0.0811           | 2.5072      |          | 10,674.03<br>04 | 10,674.03<br>04 | 0.4941 |     | 10,686.38<br>30 |
| Unmitigated | 2.5633 | 13.7673 | 31.5154 | 0.1052 | 9.0612           | 0.0869          | 9.1481        | 2.4261            | 0.0811           | 2.5072      |          | 10,674.03<br>04 | 10,674.03<br>04 | 0.4941 |     | 10,686.38<br>30 |

## **4.2 Trip Summary Information**

|                       | Ave      | rage Daily Trip Ra | ite      | Unmitigated | Mitigated  |
|-----------------------|----------|--------------------|----------|-------------|------------|
| Land Use              | Weekday  | Saturday           | Sunday   | Annual VMT  | Annual VMT |
| City Park             | 0.00     | 0.00               | 0.00     |             |            |
| Parking Lot           | 0.00     | 0.00               | 0.00     |             |            |
| Single Family Housing | 1,406.56 | 1,476.59           | 1284.38  | 4,030,500   | 4,030,500  |
| Total                 | 1,406.56 | 1,476.59           | 1,284.38 | 4,030,500   | 4,030,500  |

## 4.3 Trip Type Information

|                       |            | Miles      |             |            | Trip %     |             |         | Trip Purpos | e %     |
|-----------------------|------------|------------|-------------|------------|------------|-------------|---------|-------------|---------|
| Land Use              | H-W or C-W | H-S or C-C | H-O or C-NW | H-W or C-W | H-S or C-C | H-O or C-NW | Primary | Diverted    | Pass-by |
| City Park             | 0.00       | 0.00       | 0.00        | 0.00       | 0.00       | 0.00        | 0       | 0           | 0       |
| Parking Lot           | 0.00       | 0.00       | 0.00        | 0.00       | 0.00       | 0.00        | 0       | 0           | 0       |
| Single Family Housing | 10.80      | 7.30       | 7.50        | 44.00      | 19.00      | 37.00       | 86      | 11          | 3       |

## Lico Subdivision Project - Monterey Bay Unified APCD Air District, Winter

#### 4.4 Fleet Mix

| Land Use              | LDA      | LDT1     | LDT2     | MDV      | LHD1     | LHD2     | MHD      | HHD      | OBUS     | UBUS     | MCY      | SBUS     | MH       |
|-----------------------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|
| City Park             | 0.556074 | 0.026253 | 0.203701 | 0.115939 | 0.017760 | 0.004663 | 0.019655 | 0.042099 | 0.003061 | 0.002272 | 0.006688 | 0.001093 | 0.000742 |
| Parking Lot           | 0.556074 | 0.026253 | 0.203701 | 0.115939 | 0.017760 | 0.004663 | 0.019655 | 0.042099 | 0.003061 | 0.002272 | 0.006688 | 0.001093 | 0.000742 |
| Single Family Housing | 0.556074 | 0.026253 | 0.203701 | 0.115939 | 0.017760 | 0.004663 | 0.019655 | 0.042099 | 0.003061 | 0.002272 | 0.006688 | 0.001093 | 0.000742 |

## 5.0 Energy Detail

Historical Energy Use: N

## **5.1 Mitigation Measures Energy**

Exceed Title 24

Kilowatt Hours of Renewable Electricity Generated

Install Energy Efficient Appliances

|                           | ROG    | NOx    | CO     | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2      | Total CO2      | CH4    | N2O    | CO2e           |
|---------------------------|--------|--------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|-------------|----------|----------------|----------------|--------|--------|----------------|
| Category                  |        |        |        |                 | lb/d             | day             |               |                   |                  |             |          |                | lb/d           | day    |        |                |
| NaturalGas<br>Mitigated   | 0.1200 | 1.0252 | 0.4363 | 6.5400e-<br>003 |                  | 0.0829          | 0.0829        | i<br>i<br>i       | 0.0829           | 0.0829      |          | 1,308.769<br>1 | 1,308.769<br>1 | 0.0251 | 0.0240 | 1,316.546<br>5 |
| NaturalGas<br>Unmitigated | 0.1280 | 1.0934 | 0.4653 | 6.9800e-<br>003 |                  | 0.0884          | 0.0884        |                   | 0.0884           | 0.0884      |          | 1,395.873<br>8 | 1,395.873<br>8 | 0.0268 | 0.0256 | 1,404.168<br>8 |

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## Lico Subdivision Project - Monterey Bay Unified APCD Air District, Winter

# 5.2 Energy by Land Use - NaturalGas <u>Unmitigated</u>

|                          | NaturalGa<br>s Use | ROG    | NOx    | CO     | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total | Fugitive<br>PM2.5   | Exhaust<br>PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2      | Total CO2      | CH4    | N2O    | CO2e           |
|--------------------------|--------------------|--------|--------|--------|-----------------|------------------|-----------------|---------------|---------------------|------------------|-------------|----------|----------------|----------------|--------|--------|----------------|
| Land Use                 | kBTU/yr            |        |        |        |                 | lb/d             | day             |               |                     |                  |             |          |                | lb/c           | lay    |        |                |
| City Park                | 0                  | 0.0000 | 0.0000 | 0.0000 | 0.0000          |                  | 0.0000          | 0.0000        |                     | 0.0000           | 0.0000      |          | 0.0000         | 0.0000         | 0.0000 | 0.0000 | 0.0000         |
| Parking Lot              | 0                  | 0.0000 | 0.0000 | 0.0000 | 0.0000          |                  | 0.0000          | 0.0000        | <br>                | 0.0000           | 0.0000      |          | 0.0000         | 0.0000         | 0.0000 | 0.0000 | 0.0000         |
| Single Family<br>Housing | 11864.9            | 0.1280 | 1.0934 | 0.4653 | 6.9800e-<br>003 |                  | 0.0884          | 0.0884        | <br> <br> <br> <br> | 0.0884           | 0.0884      |          | 1,395.873<br>8 | 1,395.873<br>8 | 0.0268 | 0.0256 | 1,404.168<br>8 |
| Total                    |                    | 0.1280 | 1.0934 | 0.4653 | 6.9800e-<br>003 |                  | 0.0884          | 0.0884        |                     | 0.0884           | 0.0884      |          | 1,395.873<br>8 | 1,395.873<br>8 | 0.0268 | 0.0256 | 1,404.168<br>8 |

## **Mitigated**

|                          | NaturalGa<br>s Use | ROG    | NOx    | СО     | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2      | Total CO2      | CH4    | N2O    | CO2e           |
|--------------------------|--------------------|--------|--------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|-------------|----------|----------------|----------------|--------|--------|----------------|
| Land Use                 | kBTU/yr            |        | lb/day |        |                 |                  |                 |               |                   | lb/day           |             |          |                |                |        |        |                |
| City Park                | 0                  | 0.0000 | 0.0000 | 0.0000 | 0.0000          |                  | 0.0000          | 0.0000        | 1<br>1<br>1<br>1  | 0.0000           | 0.0000      |          | 0.0000         | 0.0000         | 0.0000 | 0.0000 | 0.0000         |
| Parking Lot              | 0                  | 0.0000 | 0.0000 | 0.0000 | 0.0000          |                  | 0.0000          | 0.0000        | ,                 | 0.0000           | 0.0000      |          | 0.0000         | 0.0000         | 0.0000 | 0.0000 | 0.0000         |
| Single Family<br>Housing | 11.1245            | 0.1200 | 1.0252 | 0.4363 | 6.5400e-<br>003 |                  | 0.0829          | 0.0829        | ,                 | 0.0829           | 0.0829      |          | 1,308.769<br>1 | 1,308.769<br>1 | 0.0251 | 0.0240 | 1,316.546<br>5 |
| Total                    |                    | 0.1200 | 1.0252 | 0.4363 | 6.5400e-<br>003 |                  | 0.0829          | 0.0829        |                   | 0.0829           | 0.0829      |          | 1,308.769<br>1 | 1,308.769<br>1 | 0.0251 | 0.0240 | 1,316.546<br>5 |

## 6.0 Area Detail

## Lico Subdivision Project - Monterey Bay Unified APCD Air District, Winter

## **6.1 Mitigation Measures Area**

Use Low VOC Paint - Residential Interior
Use Low VOC Paint - Residential Exterior
Use only Natural Gas Hearths

|             | ROG    | NOx    | СО      | SO2    | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2      | Total CO2      | CH4    | N2O    | CO2e           |
|-------------|--------|--------|---------|--------|------------------|-----------------|---------------|-------------------|------------------|-------------|----------|----------------|----------------|--------|--------|----------------|
| Category    |        |        |         |        | lb/d             | day             |               |                   |                  |             |          |                | lb/d           | lay    |        |                |
| Mitigated   | 7.0854 | 2.6131 | 13.3348 | 0.0164 |                  | 0.2680          | 0.2680        |                   | 0.2680           | 0.2680      | 0.0000   | 3,177.432<br>7 | 3,177.432<br>7 | 0.0817 | 0.0579 | 3,196.713<br>2 |
| Unmitigated | 7.0854 | 2.6131 | 13.3348 | 0.0164 |                  | 0.2680          | 0.2680        |                   | 0.2680           | 0.2680      | 0.0000   | 3,177.432<br>7 | 3,177.432<br>7 | 0.0817 | 0.0579 | 3,196.713<br>2 |

## Lico Subdivision Project - Monterey Bay Unified APCD Air District, Winter

# 6.2 Area by SubCategory Unmitigated

|                          | ROG    | NOx    | CO      | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2      | Total CO2      | CH4    | N2O    | CO2e           |
|--------------------------|--------|--------|---------|-----------------|------------------|-----------------|---------------|-------------------|------------------|-------------|----------|----------------|----------------|--------|--------|----------------|
| SubCategory              | lb/day |        |         |                 |                  |                 | lb/day        |                   |                  |             |          |                |                |        |        |                |
| Architectural<br>Coating | 0.4969 |        |         |                 |                  | 0.0000          | 0.0000        | i<br>i            | 0.0000           | 0.0000      |          |                | 0.0000         |        | i<br>i | 0.0000         |
| Consumer<br>Products     | 5.9304 |        |         | <br> <br>       |                  | 0.0000          | 0.0000        |                   | 0.0000           | 0.0000      |          |                | 0.0000         |        |        | 0.0000         |
| Hearth                   | 0.2892 | 2.4717 | 1.0518  | 0.0158          |                  | 0.1998          | 0.1998        | i<br>i            | 0.1998           | 0.1998      | 0.0000   | 3,155.294<br>1 | 3,155.294<br>1 | 0.0605 | 0.0579 | 3,174.044<br>5 |
| Landscaping              | 0.3689 | 0.1415 | 12.2830 | 6.5000e-<br>004 |                  | 0.0682          | 0.0682        | i<br>i            | 0.0682           | 0.0682      |          | 22.1385        | 22.1385        | 0.0212 | i<br>i | 22.6687        |
| Total                    | 7.0854 | 2.6131 | 13.3348 | 0.0164          |                  | 0.2680          | 0.2680        |                   | 0.2680           | 0.2680      | 0.0000   | 3,177.432<br>7 | 3,177.432<br>7 | 0.0817 | 0.0579 | 3,196.713<br>2 |

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## Lico Subdivision Project - Monterey Bay Unified APCD Air District, Winter

# 6.2 Area by SubCategory

#### **Mitigated**

|                          | ROG    | NOx    | CO             | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2      | Total CO2      | CH4    | N2O    | CO2e           |
|--------------------------|--------|--------|----------------|-----------------|------------------|-----------------|---------------|-------------------|------------------|-------------|----------|----------------|----------------|--------|--------|----------------|
| SubCategory              | lb/day |        |                |                 |                  |                 |               | lb/day            |                  |             |          |                |                |        |        |                |
| Architectural<br>Coating | 0.4969 |        |                |                 |                  | 0.0000          | 0.0000        | i<br>i            | 0.0000           | 0.0000      |          |                | 0.0000         |        | <br>   | 0.0000         |
| Consumer<br>Products     | 5.9304 |        | <br> <br> <br> |                 |                  | 0.0000          | 0.0000        | :<br>:<br>:       | 0.0000           | 0.0000      |          |                | 0.0000         | <br>   | <br>   | 0.0000         |
| Hearth                   | 0.2892 | 2.4717 | 1.0518         | 0.0158          |                  | 0.1998          | 0.1998        | i<br>i            | 0.1998           | 0.1998      | 0.0000   | 3,155.294<br>1 | 3,155.294<br>1 | 0.0605 | 0.0579 | 3,174.044<br>5 |
| Landscaping              | 0.3689 | 0.1415 | 12.2830        | 6.5000e-<br>004 |                  | 0.0682          | 0.0682        | i<br>i            | 0.0682           | 0.0682      |          | 22.1385        | 22.1385        | 0.0212 | <br>   | 22.6687        |
| Total                    | 7.0854 | 2.6131 | 13.3348        | 0.0164          |                  | 0.2680          | 0.2680        |                   | 0.2680           | 0.2680      | 0.0000   | 3,177.432<br>7 | 3,177.432<br>7 | 0.0817 | 0.0579 | 3,196.713<br>2 |

#### 7.0 Water Detail

# 7.1 Mitigation Measures Water

#### 8.0 Waste Detail

## 8.1 Mitigation Measures Waste

## 9.0 Operational Offroad

| Fauricus and Ton a | Nivershaan | Harris /Davi | David Maari | Harras Davier | Land Factor | Fuel Tues |
|--------------------|------------|--------------|-------------|---------------|-------------|-----------|
| Equipment Type     | Number     | Hours/Day    | Days/Year   | Horse Power   | Load Factor | Fuel Type |
|                    |            |              |             |               |             |           |

## 10.0 Stationary Equipment

## Lico Subdivision Project - Monterey Bay Unified APCD Air District, Winter

## **Fire Pumps and Emergency Generators**

| Equipment Type | Number | Hours/Day | Hours/Year | Horse Power | Load Factor | Fuel Type |
|----------------|--------|-----------|------------|-------------|-------------|-----------|
|                |        |           |            |             |             |           |

#### **Boilers**

| Equipment Type | Number | Heat Input/Day | Heat Input/Year | Boiler Rating | Fuel Type |
|----------------|--------|----------------|-----------------|---------------|-----------|

## **User Defined Equipment**

| Equipment Type | Number |
|----------------|--------|
|----------------|--------|

# 11.0 Vegetation

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Lico Subdivision Project - Monterey Bay Unified APCD Air District, Annual

# Lico Subdivision Project Monterey Bay Unified APCD Air District, Annual

#### 1.0 Project Characteristics

#### 1.1 Land Usage

| Land Uses             | Size   | Metric        | Lot Acreage | Floor Surface Area | Population |
|-----------------------|--------|---------------|-------------|--------------------|------------|
| Parking Lot           | 11.18  | Acre          | 11.18       | 487,151.00         | 0          |
| City Park             | 8.18   | Acre          | 8.18        | 356,386.00         | 0          |
| Single Family Housing | 149.00 | Dwelling Unit | 30.59       | 268,200.00         | 453        |

#### 1.2 Other Project Characteristics

UrbanizationUrbanWind Speed (m/s)2.8Precipitation Freq (Days)53Climate Zone4Operational Year2030

Utility Company Pacific Gas & Electric Company

 CO2 Intensity
 298.65
 CH4 Intensity
 0.014
 N20 Intensity
 0.003

 (lb/MWhr)
 (lb/MWhr)
 (lb/MWhr)
 (lb/MWhr)

#### 1.3 User Entered Comments & Non-Default Data

Project Characteristics - Adjusted intensities for 2030 RPS

Land Use - Parking lot LU is interior roadways, City park is park/stormwater; DOF estimate for population

Construction Phase - Phases from data request; assumed arch coating to start 3/4 through each building phase

Off-road Equipment - Left as default

Off-road Equipment - Default

Off-road Equipment - Default

Off-road Equipment - Default

Off-road Equipment - From data request

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#### Lico Subdivision Project - Monterey Bay Unified APCD Air District, Annual

Off-road Equipment - From data request

Off-road Equipment - From data request

Off-road Equipment - From data request

Off-road Equipment - From data request, assuming 1 of each throughout

Off-road Equipment - From data request

Trips and VMT - Worker/vendor for grading and construction from data request, others left default

Demolition - From data request

Grading - From data request

Architectural Coating - MBARD Rule 426. Default values for sg ft div by 4 to account for construction phasing.

Vehicle Trips - City park/Parking Lot trips zeroed. WkDy trip rate from traffic study. Corrected model error for trip %

Woodstoves - NG fireplaces

Area Coating - MABRD Rule 426; sf adjusted per arch coating screen

Energy Use -

Water And Wastewater - 20% indoor water reduction

Solid Waste - No data to indicate waste hauler diverts more than 50%

Construction Off-road Equipment Mitigation -

Mobile Land Use Mitigation -

Area Mitigation - MBARD Rule 426

Energy Mitigation - Efficient applicanes noted in data request. Solar generation from Rincon spreadsheet.

Water Mitigation - Low flow fixures accounted for in 20% overall water use reduction

Lico Subdivision Project - Monterey Bay Unified APCD Air District, Annual

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| Table Name              | Column Name                    | Default Value | New Value  |
|-------------------------|--------------------------------|---------------|------------|
| tblArchitecturalCoating | ConstArea_Residential_Exterior | 181,035.00    | 45,259.00  |
| tblArchitecturalCoating | ConstArea_Residential_Exterior | 181,035.00    | 45,259.00  |
| tblArchitecturalCoating | ConstArea_Residential_Exterior | 181,035.00    | 45,259.00  |
| tblArchitecturalCoating | ConstArea_Residential_Exterior | 181,035.00    | 45,259.00  |
| tblArchitecturalCoating | ConstArea_Residential_Interior | 543,105.00    | 135,776.00 |
| tblArchitecturalCoating | ConstArea_Residential_Interior | 543,105.00    | 135,776.00 |
| tblArchitecturalCoating | ConstArea_Residential_Interior | 543,105.00    | 135,776.00 |
| tblArchitecturalCoating | ConstArea_Residential_Interior | 543,105.00    | 135,776.00 |
| tblArchitecturalCoating | EF_Parking                     | 150.00        | 100.00     |
| tblArchitecturalCoating | EF_Parking                     | 150.00        | 100.00     |
| tblArchitecturalCoating | EF_Parking                     | 150.00        | 100.00     |
| tblArchitecturalCoating | EF_Parking                     | 150.00        | 100.00     |
| tblArchitecturalCoating | EF_Residential_Exterior        | 100.00        | 50.00      |
| tblArchitecturalCoating | EF_Residential_Exterior        | 100.00        | 50.00      |
| tblArchitecturalCoating | EF_Residential_Exterior        | 100.00        | 50.00      |
| tblArchitecturalCoating | EF_Residential_Exterior        | 100.00        | 50.00      |
| tblArchitecturalCoating | EF_Residential_Interior        | 100.00        | 50.00      |
| tblArchitecturalCoating | EF_Residential_Interior        | 100.00        | 50.00      |
| tblArchitecturalCoating | EF_Residential_Interior        | 100.00        | 50.00      |
| tblArchitecturalCoating | EF_Residential_Interior        | 100.00        | 50.00      |
| tblAreaCoating          | Area_EF_Parking                | 150           | 100        |
| tblAreaCoating          | Area_EF_Residential_Exterior   | 100           | 50         |
| tblAreaCoating          | Area_EF_Residential_Interior   | 100           | 50         |
| tblAreaMitigation       | UseLowVOCPaintParkingCheck     | False         | True       |
| tblConstructionPhase    | NumDays                        | 55.00         | 79.00      |
| tblConstructionPhase    | NumDays                        | 55.00         | 79.00      |

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| tblConstructionPhase | NumDays     | 55.00  | 78.00  |
|----------------------|-------------|--------|--------|
| tblConstructionPhase | NumDays     | 55.00  | 79.00  |
| tblConstructionPhase | NumDays     | 740.00 | 210.00 |
| tblConstructionPhase | NumDays     | 740.00 | 210.00 |
| tblConstructionPhase | NumDays     | 740.00 | 210.00 |
| tblConstructionPhase | NumDays     | 740.00 | 210.00 |
| tblConstructionPhase | NumDays     | 50.00  | 52.00  |
| tblConstructionPhase | NumDays     | 75.00  | 104.00 |
| tblConstructionPhase | NumDays     | 55.00  | 104.00 |
| tblConstructionPhase | NumDays     | 55.00  | 104.00 |
| tblConstructionPhase | NumDays     | 55.00  | 104.00 |
| tblConstructionPhase | NumDays     | 55.00  | 104.00 |
| tblConstructionPhase | NumDays     | 30.00  | 52.00  |
| tblConstructionPhase | NumDaysWeek | 5.00   | 6.00   |
| tblConstructionPhase | NumDaysWeek | 5.00   | 6.00   |
| tblConstructionPhase | NumDaysWeek | 5.00   | 6.00   |
| tblConstructionPhase | NumDaysWeek | 5.00   | 6.00   |
| tblConstructionPhase | NumDaysWeek | 5.00   | 6.00   |
| tblConstructionPhase | NumDaysWeek | 5.00   | 6.00   |
| tblConstructionPhase | NumDaysWeek | 5.00   | 6.00   |
| tblConstructionPhase | NumDaysWeek | 5.00   | 6.00   |
| tblConstructionPhase | NumDaysWeek | 5.00   | 6.00   |
| tblConstructionPhase | NumDaysWeek | 5.00   | 6.00   |
| tblConstructionPhase | NumDaysWeek | 5.00   | 6.00   |
| tblConstructionPhase | NumDaysWeek | 5.00   | 6.00   |
| tblConstructionPhase | NumDaysWeek | 5.00   | 6.00   |
| tblConstructionPhase | NumDaysWeek | 5.00   | 6.00   |

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| tblConstructionPhase | NumDaysWeek                | 5.00       | 6.00       |
|----------------------|----------------------------|------------|------------|
| tblFireplaces        | FireplaceWoodMass          | 1,508.00   | 0.00       |
| tblFireplaces        | NumberGas                  | 81.95      | 149.00     |
| tblFireplaces        | NumberNoFireplace          | 14.90      | 0.00       |
| tblFireplaces        | NumberWood                 | 52.15      | 0.00       |
| tblGrading           | MaterialImported           | 0.00       | 32,000.00  |
| tblLandUse           | LandUseSquareFeet          | 487,000.80 | 487,151.00 |
| tblLandUse           | LandUseSquareFeet          | 356,320.80 | 356,386.00 |
| tblLandUse           | LotAcreage                 | 48.38      | 30.59      |
| tblLandUse           | Population                 | 426.00     | 453.00     |
| tblOffRoadEquipment  | OffRoadEquipmentUnitAmount | 3.00       | 1.00       |
| tblOffRoadEquipment  | OffRoadEquipmentUnitAmount | 2.00       | 1.00       |
| tblOffRoadEquipment  | OffRoadEquipmentUnitAmount | 3.00       | 0.00       |
| tblOffRoadEquipment  | OffRoadEquipmentUnitAmount | 3.00       | 0.00       |
| tblOffRoadEquipment  | OffRoadEquipmentUnitAmount | 3.00       | 0.00       |
| tblOffRoadEquipment  | OffRoadEquipmentUnitAmount | 3.00       | 0.00       |
| tblOffRoadEquipment  | OffRoadEquipmentUnitAmount | 2.00       | 1.00       |
| tblOffRoadEquipment  | OffRoadEquipmentUnitAmount | 2.00       | 1.00       |
| tblOffRoadEquipment  | OffRoadEquipmentUnitAmount | 2.00       | 1.00       |
| tblOffRoadEquipment  | OffRoadEquipmentUnitAmount | 2.00       | 1.00       |
| tblOffRoadEquipment  | OffRoadEquipmentUnitAmount | 2.00       | 1.00       |
| tblOffRoadEquipment  | OffRoadEquipmentUnitAmount | 2.00       | 1.00       |
| tblOffRoadEquipment  | OffRoadEquipmentUnitAmount | 2.00       | 1.00       |
| tblOffRoadEquipment  | OffRoadEquipmentUnitAmount | 2.00       | 1.00       |
| tblOffRoadEquipment  | OffRoadEquipmentUnitAmount | 2.00       | 1.00       |
| tblOffRoadEquipment  | OffRoadEquipmentUnitAmount | 2.00       | 1.00       |
| tblOffRoadEquipment  | OffRoadEquipmentUnitAmount | 2.00       | 1.00       |

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| th IOHD and Fautiness of | Off Dood Farring and Init America | 2.00 | 4.00  |
|--------------------------|-----------------------------------|------|-------|
| tblOffRoadEquipment      | OffRoadEquipmentUnitAmount        | 2.00 | 1.00  |
| tblOffRoadEquipment      | OffRoadEquipmentUnitAmount        | 2.00 | 1.00  |
| tblOffRoadEquipment      | OffRoadEquipmentUnitAmount        | 3.00 | 1.00  |
| tblOffRoadEquipment      | OffRoadEquipmentUnitAmount        | 2.00 | 1.00  |
| tblOffRoadEquipment      | OffRoadEquipmentUnitAmount        | 3.00 | 1.00  |
| tblOffRoadEquipment      | OffRoadEquipmentUnitAmount        | 3.00 | 1.00  |
| tblOffRoadEquipment      | OffRoadEquipmentUnitAmount        | 3.00 | 1.00  |
| tblOffRoadEquipment      | OffRoadEquipmentUnitAmount        | 3.00 | 1.00  |
| tblOffRoadEquipment      | OffRoadEquipmentUnitAmount        | 2.00 | 1.00  |
| tblOffRoadEquipment      | OffRoadEquipmentUnitAmount        | 4.00 | 2.00  |
| tblOffRoadEquipment      | OffRoadEquipmentUnitAmount        | 1.00 | 0.00  |
| tblOffRoadEquipment      | OffRoadEquipmentUnitAmount        | 1.00 | 0.00  |
| tblOffRoadEquipment      | OffRoadEquipmentUnitAmount        | 1.00 | 0.00  |
| tblOffRoadEquipment      | OffRoadEquipmentUnitAmount        | 1.00 | 0.00  |
| tblOffRoadEquipment      | UsageHours                        | 8.00 | 10.00 |
| tblOffRoadEquipment      | UsageHours                        | 7.00 | 10.00 |
| tblOffRoadEquipment      | UsageHours                        | 7.00 | 10.00 |
| tblOffRoadEquipment      | UsageHours                        | 7.00 | 10.00 |
| tblOffRoadEquipment      | UsageHours                        | 7.00 | 10.00 |
| tblOffRoadEquipment      | UsageHours                        | 8.00 | 10.00 |
| tblOffRoadEquipment      | UsageHours                        | 8.00 | 10.00 |
| tblOffRoadEquipment      | UsageHours                        | 8.00 | 10.00 |
| tblOffRoadEquipment      | UsageHours                        | 8.00 | 10.00 |
| tblOffRoadEquipment      | UsageHours                        | 8.00 | 10.00 |
| tblOffRoadEquipment      | UsageHours                        | 8.00 | 10.00 |
| tblOffRoadEquipment      | UsageHours                        | 8.00 | 10.00 |
| tblOffRoadEquipment      | UsageHours                        | 8.00 | 10.00 |
|                          | •                                 |      |       |

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| tblOffRoadEquipment | UsageHours | 8.00 | 10.00 |
|---------------------|------------|------|-------|
| tblOffRoadEquipment | UsageHours | 8.00 | 10.00 |
| tblOffRoadEquipment | UsageHours | 8.00 | 10.00 |
| tblOffRoadEquipment | UsageHours | 8.00 | 10.00 |
| tblOffRoadEquipment | UsageHours | 8.00 | 10.00 |
| tblOffRoadEquipment | UsageHours | 8.00 | 10.00 |
| tblOffRoadEquipment | UsageHours | 8.00 | 10.00 |
| tblOffRoadEquipment | UsageHours | 8.00 | 10.00 |
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| tblOffRoadEquipment | UsageHours | 8.00 | 10.00 |
| tblOffRoadEquipment | UsageHours | 8.00 | 10.00 |
| tblOffRoadEquipment | UsageHours | 8.00 | 10.00 |
| tblOffRoadEquipment | UsageHours | 7.00 | 10.00 |
| tblOffRoadEquipment | UsageHours | 7.00 | 10.00 |
| tblOffRoadEquipment | UsageHours | 7.00 | 10.00 |
| tblOffRoadEquipment | UsageHours | 7.00 | 10.00 |
| tblOffRoadEquipment | UsageHours | 8.00 | 10.00 |
| tblOffRoadEquipment | UsageHours | 8.00 | 10.00 |
| tblOffRoadEquipment | UsageHours | 8.00 | 10.00 |
| tblOffRoadEquipment | UsageHours | 8.00 | 10.00 |

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| tblOffRoadEquipment       | UsageHours               | 8.00   | 10.00  |
|---------------------------|--------------------------|--------|--------|
| tblOffRoadEquipment       | UsageHours               | 8.00   | 10.00  |
| tblProjectCharacteristics | CH4IntensityFactor       | 0.029  | 0.014  |
| tblProjectCharacteristics | CO2IntensityFactor       | 641.35 | 298.65 |
| tblProjectCharacteristics | N2OIntensityFactor       | 0.006  | 0.003  |
| tblSolidWaste             | SolidWasteGenerationRate | 199.32 | 187.44 |
| tblTripsAndVMT            | VendorTripNumber         | 0.00   | 1.00   |
| tblTripsAndVMT            | VendorTripNumber         | 0.00   | 1.00   |
| tblTripsAndVMT            | VendorTripNumber         | 154.00 | 1.00   |
| tblTripsAndVMT            | VendorTripNumber         | 0.00   | 1.00   |
| tblTripsAndVMT            | VendorTripNumber         | 0.00   | 1.00   |
| tblTripsAndVMT            | VendorTripNumber         | 154.00 | 1.00   |
| tblTripsAndVMT            | VendorTripNumber         | 0.00   | 1.00   |
| tblTripsAndVMT            | VendorTripNumber         | 0.00   | 1.00   |
| tblTripsAndVMT            | VendorTripNumber         | 0.00   | 1.00   |
| tblTripsAndVMT            | VendorTripNumber         | 0.00   | 1.00   |
| tblTripsAndVMT            | VendorTripNumber         | 154.00 | 1.00   |
| tblTripsAndVMT            | VendorTripNumber         | 0.00   | 1.00   |
| tblTripsAndVMT            | VendorTripNumber         | 0.00   | 1.00   |
| tblTripsAndVMT            | VendorTripNumber         | 154.00 | 1.00   |
| tblTripsAndVMT            | VendorTripNumber         | 0.00   | 1.00   |
| tblTripsAndVMT            | WorkerTripNumber         | 408.00 | 40.00  |
| tblTripsAndVMT            | WorkerTripNumber         | 82.00  | 40.00  |
| tblTripsAndVMT            | WorkerTripNumber         | 408.00 | 40.00  |
| tblTripsAndVMT            | WorkerTripNumber         | 82.00  | 40.00  |
| tblTripsAndVMT            | WorkerTripNumber         | 33.00  | 20.00  |
| tblTripsAndVMT            | WorkerTripNumber         | 408.00 | 40.00  |

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| tblTripsAndVMT     | WorkerTripNumber                     | 82.00        | 40.00        |  |  |
|--------------------|--------------------------------------|--------------|--------------|--|--|
| tblTripsAndVMT     | WorkerTripNumber                     | 408.00       | 40.00        |  |  |
| tblTripsAndVMT     | WorkerTripNumber                     | 82.00        | 40.00        |  |  |
| tblVehicleTrips    | CC_TL                                | 7.30         | 0.00         |  |  |
| tblVehicleTrips    | CC_TL                                | 7.30         | 0.00         |  |  |
| tblVehicleTrips    | CC_TTP                               | 48.00        | 0.00         |  |  |
| tblVehicleTrips    | CNW_TL                               | 7.30         | 0.00         |  |  |
| tblVehicleTrips    | CNW_TL                               | 7.30         | 0.00         |  |  |
| tblVehicleTrips    | CNW_TTP                              | 19.00        | 0.00         |  |  |
| tblVehicleTrips    | CW_TL                                | 9.50         | 0.00         |  |  |
| tblVehicleTrips    | CW_TL                                | 9.50         | 0.00         |  |  |
| tblVehicleTrips    | CW_TTP                               | 33.00        | 0.00         |  |  |
| tblVehicleTrips    | DV_TP                                | 28.00        | 0.00         |  |  |
| tblVehicleTrips    | HO_TTP                               | 37.20        | 37.00        |  |  |
| tblVehicleTrips    | HS_TTP                               | 18.80        | 19.00        |  |  |
| tblVehicleTrips    | PB_TP                                | 6.00         | 0.00         |  |  |
| tblVehicleTrips    | PR_TP                                | 66.00        | 0.00         |  |  |
| tblVehicleTrips    | ST_TR                                | 22.75        | 0.00         |  |  |
| tblVehicleTrips    | SU_TR                                | 16.74        | 0.00         |  |  |
| tblVehicleTrips    | WD_TR                                | 1.89         | 0.00         |  |  |
| tblVehicleTrips    | WD_TR                                | 9.52         | 9.44         |  |  |
| tblWater           | IndoorWaterUseRate                   | 9,707,949.82 | 7,766,389.00 |  |  |
| tblWaterMitigation | PercentReductionInFlowBathroomFaucet | 32           | 0            |  |  |
| tblWaterMitigation | PercentReductionInFlowKitchenFaucet  | 18           | 0            |  |  |
| tblWaterMitigation | PercentReductionInFlowShower         | 20           | 0            |  |  |
| tblWaterMitigation | PercentReductionInFlowToilet         | 20           | 0            |  |  |
| tblWoodstoves      | NumberCatalytic                      | 7.45         | 0.00         |  |  |

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| tblWoodstoves | NumberNoncatalytic | 7.45     | 0.00 |
|---------------|--------------------|----------|------|
| tblWoodstoves | WoodstoveDayYear   | 82.00    | 0.00 |
| tblWoodstoves | WoodstoveWoodMass  | 3,120.00 | 0.00 |

# 2.0 Emissions Summary

#### 2.1 Overall Construction

# **Unmitigated Construction**

|         | ROG    | NOx    | СО     | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4    | N2O    | CO2e     |  |
|---------|--------|--------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|-------------|----------|-----------|-----------|--------|--------|----------|--|
| Year    |        |        |        |                 | ton              | s/yr            |               |                   |                  |             | MT/yr    |           |           |        |        |          |  |
| 2020    | 0.5383 | 6.1737 | 3.5507 | 8.4900e-<br>003 | 0.8002           | 0.2602          | 1.0604        | 0.3545            | 0.2405           | 0.5950      | 0.0000   | 755.6531  | 755.6531  | 0.1861 | 0.0000 | 760.3063 |  |
| 2021    | 0.7529 | 4.4344 | 4.2255 | 7.7400e-<br>003 | 0.0554           | 0.2213          | 0.2767        | 0.0148            | 0.2085           | 0.2232      | 0.0000   | 676.0883  | 676.0883  | 0.1520 | 0.0000 | 679.8877 |  |
| 2022    | 0.7144 | 3.9900 | 4.1732 | 7.7200e-<br>003 | 0.0556           | 0.1936          | 0.2492        | 0.0148            | 0.1824           | 0.1972      | 0.0000   | 674.5569  | 674.5569  | 0.1511 | 0.0000 | 678.3344 |  |
| 2023    | 0.6864 | 3.6638 | 4.1283 | 7.6800e-<br>003 | 0.0555           | 0.1726          | 0.2281        | 0.0148            | 0.1624           | 0.1772      | 0.0000   | 670.8419  | 670.8419  | 0.1495 | 0.0000 | 674.5795 |  |
| 2024    | 0.6396 | 3.2140 | 3.8489 | 7.1100e-<br>003 | 0.0534           | 0.1482          | 0.2016        | 0.0142            | 0.1393           | 0.1536      | 0.0000   | 621.1758  | 621.1758  | 0.1364 | 0.0000 | 624.5860 |  |
| Maximum | 0.7529 | 6.1737 | 4.2255 | 8.4900e-<br>003 | 0.8002           | 0.2602          | 1.0604        | 0.3545            | 0.2405           | 0.5950      | 0.0000   | 755.6531  | 755.6531  | 0.1861 | 0.0000 | 760.3063 |  |

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# 2.1 Overall Construction Mitigated Construction

|                      | ROG    | NOx    | СО     | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total    | Bio- CO2 | NBio- CO2 | Total CO2 | CH4    | N2O    | CO2e     |
|----------------------|--------|--------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|-----------|-----------|--------|--------|----------|
| Year                 |        |        |        |                 | tor              | ns/yr           |               |                   |                  |                |          | •         | M         | Γ/yr   |        |          |
| 2020                 | 0.5383 | 6.1737 | 3.5507 | 8.4900e-<br>003 | 0.8002           | 0.2602          | 1.0604        | 0.3545            | 0.2405           | 0.5950         | 0.0000   | 755.6524  | 755.6524  | 0.1861 | 0.0000 | 760.3056 |
| 2021                 | 0.7529 | 4.4344 | 4.2255 | 7.7400e-<br>003 | 0.0554           | 0.2213          | 0.2767        | 0.0148            | 0.2085           | 0.2232         | 0.0000   | 676.0876  | 676.0876  | 0.1520 | 0.0000 | 679.8870 |
| 2022                 | 0.7144 | 3.9900 | 4.1732 | 7.7200e-<br>003 | 0.0556           | 0.1936          | 0.2492        | 0.0148            | 0.1824           | 0.1972         | 0.0000   | 674.5561  | 674.5561  | 0.1511 | 0.0000 | 678.3336 |
| 2023                 | 0.6864 | 3.6638 | 4.1283 | 7.6800e-<br>003 | 0.0555           | 0.1726          | 0.2281        | 0.0148            | 0.1624           | 0.1772         | 0.0000   | 670.8412  | 670.8412  | 0.1495 | 0.0000 | 674.5787 |
| 2021                 | 0.6396 | 3.2140 | 3.8489 | 7.1100e-<br>003 | 0.0534           | 0.1482          | 0.2016        | 0.0142            | 0.1393           | 0.1536         | 0.0000   | 621.1751  | 621.1751  | 0.1364 | 0.0000 | 624.5853 |
| Maximum              | 0.7529 | 6.1737 | 4.2255 | 8.4900e-<br>003 | 0.8002           | 0.2602          | 1.0604        | 0.3545            | 0.2405           | 0.5950         | 0.0000   | 755.6524  | 755.6524  | 0.1861 | 0.0000 | 760.3056 |
|                      | ROG    | NOx    | со     | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5<br>Total | Bio- CO2 | NBio-CO2  | Total CO2 | CH4    | N20    | CO2e     |
| Percent<br>Reduction | 0.00   | 0.00   | 0.00   | 0.00            | 0.00             | 0.00            | 0.00          | 0.00              | 0.00             | 0.00           | 0.00     | 0.00      | 0.00      | 0.00   | 0.00   | 0.00     |

| Quarter | Start Date | End Date   | Maximum Unmitigated ROG + NOX (tons/quarter) | Maximum Mitigated ROG + NOX (tons/quarter) |
|---------|------------|------------|--|--|
| 1       | 8-1-2020   | 10-31-2020 | 5.2358                                       | 5.2358                                     |
| 2       | 11-1-2020  | 1-31-2021  | 2.2125                                       | 2.2125                                     |
| 3       | 2-1-2021   | 4-30-2021  | 2.2116                                       | 2.2116                                     |
| 4       | 5-1-2021   | 7-31-2021  | 1.2875                                       | 1.2875                                     |
| 5       | 8-1-2021   | 10-31-2021 | 1.6540                                       | 1.6540                                     |
| 6       | 11-1-2021  | 1-31-2022  | 0.9925                                       | 0.9925                                     |

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| 7  | 2-1-2022  | 4-30-2022  | 1.9834 | 1.9834 |
|----|-----------|------------|--------|--------|
| 8  | 5-1-2022  | 7-31-2022  | 1.1650 | 1.1650 |
| 9  | 8-1-2022  | 10-31-2022 | 1.5214 | 1.5214 |
| 10 | 11-1-2022 | 1-31-2023  | 0.6096 | 0.6096 |
| 11 | 2-1-2023  | 4-30-2023  | 1.2698 | 1.2698 |
| 12 | 5-1-2023  | 7-31-2023  | 1.0773 | 1.0773 |
| 13 | 8-1-2023  | 10-31-2023 | 1.4273 | 1.4273 |
| 14 | 11-1-2023 | 1-31-2024  | 0.5646 | 0.5646 |
| 15 | 2-1-2024  | 4-30-2024  | 1.2026 | 1.2026 |
| 16 | 5-1-2024  | 7-31-2024  | 1.0160 | 1.0160 |
| 17 | 8-1-2024  | 9-30-2024  | 0.9020 | 0.9020 |
|    |           | Highest    | 5.2358 | 5.2358 |

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# 2.2 Overall Operational Unmitigated Operational

|          | ROG    | NOx     | CO     | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5<br>Total | Bio- CO2 | NBio- CO2      | Total CO2      | CH4             | N2O             | CO2e           |  |  |
|----------|--------|---------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|----------------|----------------|-----------------|-----------------|----------------|--|--|
| Category |        | tons/yr |        |                 |                  |                 |               |                   |                  |                |          | MT/yr          |                |                 |                 |                |  |  |
| Area     | 1.2307 | 0.1190  | 1.5759 | 7.3000e-<br>004 |                  | 0.0167          | 0.0167        |                   | 0.0167           | 0.0167         | 0.0000   | 119.8703       | 119.8703       | 4.6400e-<br>003 | 2.1500e-<br>003 | 120.6275       |  |  |
| Energy   | 0.0234 | 0.1996  | 0.0849 | 1.2700e-<br>003 |                  | 0.0161          | 0.0161        |                   | 0.0161           | 0.0161         | 0.0000   | 417.5026       | 417.5026       | 0.0132          | 6.1100e-<br>003 | 419.6524       |  |  |
| Mobile   | 0.3385 | 1.9686  | 3.8256 | 0.0162          | 1.5127           | 0.0109          | 1.5236        | 0.4058            | 0.0101           | 0.4159         | 0.0000   | 1,497.517<br>8 | 1,497.517<br>8 | 0.0608          | 0.0000          | 1,499.037<br>0 |  |  |
| Waste    |        |         |        |                 |                  | 0.0000          | 0.0000        |                   | 0.0000           | 0.0000         | 38.1907  | 0.0000         | 38.1907        | 2.2570          | 0.0000          | 94.6159        |  |  |
| Water    |        |         |        |                 |                  | 0.0000          | 0.0000        |                   | 0.0000           | 0.0000         | 2.4639   | 13.2156        | 15.6795        | 0.2537          | 6.1100e-<br>003 | 23.8419        |  |  |
| Total    | 1.5926 | 2.2871  | 5.4864 | 0.0182          | 1.5127           | 0.0437          | 1.5564        | 0.4058            | 0.0430           | 0.4488         | 40.6546  | 2,048.106<br>3 | 2,088.760<br>9 | 2.5893          | 0.0144          | 2,157.774<br>6 |  |  |

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# 2.2 Overall Operational

#### **Mitigated Operational**

|          | ROG    | NOx     | СО                        | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2      | Total CO2      | CH4             | N2O             | CO2e           |
|----------|--------|---------|---------------------------|-----------------|------------------|-----------------|---------------|-------------------|------------------|-------------|----------|----------------|----------------|-----------------|-----------------|----------------|
| Category |        | tons/yr |                           |                 |                  |                 |               |                   |                  |             |          |                |                | -/yr            |                 |                |
| Area     | 1.2307 | 0.1190  | 1.5759                    | 7.3000e-<br>004 |                  | 0.0167          | 0.0167        |                   | 0.0167           | 0.0167      | 0.0000   | 119.8703       | 119.8703       | 4.6400e-<br>003 | 2.1500e-<br>003 | 120.6275       |
| Energy   | 0.0219 | 0.1871  | 0.0796                    | 1.1900e-<br>003 |                  | 0.0151          | 0.0151        |                   | 0.0151           | 0.0151      | 0.0000   | 355.0092       | 355.0092       | 0.0106          | 5.3600e-<br>003 | 356.8731       |
| Mobile   | 0.3385 | 1.9686  | 3.8256                    | 0.0162          | 1.5127           | 0.0109          | 1.5236        | 0.4058            | 0.0101           | 0.4159      | 0.0000   | 1,497.517<br>8 | 1,497.517<br>8 | 0.0608          | 0.0000          | 1,499.037<br>0 |
| Waste    |        |         | 1<br> <br> <br> <br>      |                 |                  | 0.0000          | 0.0000        |                   | 0.0000           | 0.0000      | 38.1907  | 0.0000         | 38.1907        | 2.2570          | 0.0000          | 94.6159        |
| Water    |        |         | 1<br> <br> <br> <br> <br> |                 |                  | 0.0000          | 0.0000        |                   | 0.0000           | 0.0000      | 2.4639   | 13.2156        | 15.6795        | 0.2537          | 6.1100e-<br>003 | 23.8419        |
| Total    | 1.5911 | 2.2747  | 5.4811                    | 0.0181          | 1.5127           | 0.0427          | 1.5554        | 0.4058            | 0.0420           | 0.4478      | 40.6546  | 1,985.612<br>9 | 2,026.267<br>5 | 2.5868          | 0.0136          | 2,094.995<br>3 |

|                      | ROG  | NOx  | СО   | SO2  | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5<br>Total | Bio- CO2 | NBio-CO2 | Total CO2 | CH4  | N20  | CO2e |
|----------------------|------|------|------|------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|----------|-----------|------|------|------|
| Percent<br>Reduction | 0.09 | 0.54 | 0.10 | 0.44 | 0.00             | 2.29            | 0.06          | 0.00              | 2.33             | 0.22           | 0.00     | 3.05     | 2.99      | 0.10 | 5.22 | 2.91 |

# 3.0 Construction Detail

#### **Construction Phase**

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| Phase<br>Number | Phase Name                        | Phase Type            | Start Date | End Date   | Num Days<br>Week | Num Days | Phase Description |
|-----------------|-----------------------------------|-----------------------|------------|------------|------------------|----------|-------------------|
| 1               | Demolition                        | Demolition            | 8/1/2020   | 9/30/2020  | 6                | 52       |                   |
| 2               | Site Preparation                  | Site Preparation      | 8/1/2020   | 9/30/2020  | 6                | 52       |                   |
| 3               | Grading                           | Grading               | 8/1/2020   | 11/30/2020 | 6                | 104      |                   |
| 4               | Paving - Phase I                  | Paving                | 12/1/2020  | 3/31/2021  | 6                | 104      |                   |
| 5               | Building Construction - Phase I   | Building Construction | 3/1/2021   | 10/31/2021 | 6                | 210      |                   |
| 6               | Architectural Coating - Phase I   | Architectural Coating | 8/1/2021   | 10/31/2021 | 6                | 78       |                   |
| 7               | Paving - Phase II                 | Paving                | 12/1/2021  | 3/31/2022  | 6                | 104      |                   |
| 8               | Building Construction - Phase II  | Building Construction | 3/1/2022   | 10/31/2022 | 6                | 210      |                   |
| 9               | Architectural Coating - Phase II  | Architectural Coating | 8/1/2022   | 10/31/2022 | 6                | 79       |                   |
| 10              | Paving - Phase III                | Paving                | 12/1/2022  | 3/31/2023  | 6                | 104      |                   |
| 11              | Building Construction - Phase III | Building Construction | 3/1/2023   | 10/31/2023 | 6                | 210      |                   |
| 12              | Architectural Coating - Phase III | Architectural Coating | 8/1/2023   | 10/31/2023 | 6                | 79       |                   |
| 13              | Paving - Phase IV                 | Paving                | 12/1/2023  | 3/31/2024  | 6                | 104      |                   |
| 14              | Building Construction - Phase IV  | Building Construction | 3/1/2024   | 10/31/2024 | 6                | 210      |                   |
| 15              | Architectural Coating - Phase IV  | Architectural Coating | 8/1/2024   | 10/31/2024 | 6                | 79       |                   |

Acres of Grading (Site Preparation Phase): 32.5

Acres of Grading (Grading Phase): 260

Acres of Paving: 11.18

Residential Indoor: 135,776; Residential Outdoor: 45,259; Non-Residential Indoor: 0; Non-Residential Outdoor: 0; Striped Parking Area: 29,229 (Architectural Coating – sqft)

#### OffRoad Equipment

| Phase Name | Offroad Equipment Type   | Amount | Usage Hours | Horse Power | Load Factor |
|------------|--------------------------|--------|-------------|-------------|-------------|
| Demolition | Concrete/Industrial Saws | 1      | 10.00       | 81          | 0.73        |

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| Demolition       | Excavators                   | 1 | 10.00 | 158 | 0.38 |
|------------------|------------------------------|---|-------|-----|------|
| Demolition       | Other Construction Equipment | 1 | 10.00 | 172 | 0.42 |
| Demolition       | Rubber Tired Dozers          | 1 | 10.00 | 247 | 0.40 |
| Demolition       | Signal Boards                | 1 | 10.00 | 6   | 0.82 |
| Demolition       | Tractors/Loaders/Backhoes    | 2 | 10.00 | 97  | 0.37 |
| Site Preparation | Crawler Tractors             | 1 | 10.00 | 212 | 0.43 |
| Site Preparation | Rubber Tired Dozers          | 1 | 10.00 | 247 | 0.40 |
| Site Preparation | Signal Boards                | 1 | 10.00 | 6   | 0.82 |
| Site Preparation | Tractors/Loaders/Backhoes    | 2 | 10.00 | 97  | 0.37 |
| Grading          | Crawler Tractors             | 1 | 10.00 | 212 | 0.43 |
| Grading          | Excavators                   | 1 | 10.00 | 158 | 0.38 |
| Grading          | Graders                      | 1 | 10.00 | 187 | 0.41 |
| Grading          | Plate Compactors             | 1 | 10.00 | 8   | 0.43 |
| Grading          | Rollers                      | 1 | 10.00 | 80  | 0.38 |
| Grading          | Rough Terrain Forklifts      | 1 | 10.00 | 100 | 0.40 |
| Grading          | Rubber Tired Dozers          | 1 | 10.00 | 247 | 0.40 |
| Grading          | Rubber Tired Loaders         | 1 | 10.00 | 203 | 0.36 |
| Grading          | Scrapers                     | 1 | 10.00 | 367 | 0.48 |
| Grading          | Signal Boards                | 1 | 10.00 | 6   | 0.82 |
| Grading          | Skid Steer Loaders           | 1 | 10.00 | 65  | 0.37 |
| Grading          | Tractors/Loaders/Backhoes    | 1 | 10.00 | 97  | 0.37 |
| Grading          | Trenchers                    | 1 | 10.00 | 78  | 0.50 |
| Paving - Phase I | Concrete/Industrial Saws     | 1 | 10.00 | 81  | 0.73 |
| Paving - Phase I | Graders                      | 1 | 10.00 | 187 | 0.41 |
| Paving - Phase I | Pavers                       | 1 | 10.00 | 130 | 0.42 |
| Paving - Phase I | Paving Equipment             | 1 | 10.00 | 132 | 0.36 |
| Paving - Phase I | Rollers                      | 1 | 10.00 | 80  | 0.38 |

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| Paving - Phase I                 | Signal Boards                | 1 | 10.00 | 6   | 0.82 |
|----------------------------------|------------------------------|---|-------|-----|------|
| Paving - Phase I                 | Skid Steer Loaders           | 1 | 10.00 | 65  | 0.37 |
| Paving - Phase I                 | Surfacing Equipment          | 1 | 10.00 | 263 | 0.30 |
| Building Construction - Phase I  | Concrete/Industrial Saws     | 1 | 10.00 | 81  | 0.73 |
| Building Construction - Phase I  | Cranes                       | 1 | 10.00 | 231 | 0.29 |
| Building Construction - Phase I  | Forklifts                    | 0 | 10.00 | 89  | 0.20 |
| Building Construction - Phase I  | Generator Sets               | 1 | 10.00 | 84  | 0.74 |
| Building Construction - Phase I  | Other Construction Equipment | 1 | 10.00 | 172 | 0.42 |
| Building Construction - Phase I  | Rough Terrain Forklifts      | 1 | 10.00 | 100 | 0.40 |
| Building Construction - Phase I  | Skid Steer Loaders           | 1 | 10.00 | 65  | 0.37 |
| Building Construction - Phase I  | Tractors/Loaders/Backhoes    | 1 | 10.00 | 97  | 0.37 |
| Building Construction - Phase I  | Trenchers                    | 1 | 10.00 | 78  | 0.50 |
| Building Construction - Phase I  | Welders                      | 0 | 10.00 | 46  | 0.45 |
| Architectural Coating - Phase I  | Air Compressors              | 1 | 6.00  | 78  | 0.48 |
| Paving - Phase II                | Concrete/Industrial Saws     | 1 | 10.00 | 81  | 0.73 |
| Paving - Phase II                | Graders                      | 1 | 10.00 | 187 | 0.41 |
| Paving - Phase II                | Pavers                       | 1 | 10.00 | 130 | 0.42 |
| Paving - Phase II                | Paving Equipment             | 1 | 10.00 | 132 | 0.36 |
| Paving - Phase II                | Rollers                      | 1 | 10.00 | 80  | 0.38 |
| Paving - Phase II                | Signal Boards                | 1 | 10.00 | 6   | 0.82 |
| Paving - Phase II                | Skid Steer Loaders           | 1 | 10.00 | 65  | 0.37 |
| Paving - Phase II                | Surfacing Equipment          | 1 | 10.00 | 263 | 0.30 |
| Building Construction - Phase II | Concrete/Industrial Saws     | 1 | 10.00 | 81  | 0.73 |
| Building Construction - Phase II | Cranes                       | 1 | 10.00 | 231 | 0.29 |
| Building Construction - Phase II | Forklifts                    | 0 | 10.00 | 89  | 0.20 |
| Building Construction - Phase II | Generator Sets               | 1 | 10.00 | 84  | 0.74 |
| Building Construction - Phase II | Other Construction Equipment | 1 | 10.00 | 172 | 0.42 |

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| Building Construction - Phase II  | Rough Terrain Forklifts      | 1          | 10.00 | 100 | 0.40 |
|-----------------------------------|------------------------------|------------|-------|-----|------|
| Building Construction - Phase II  | Skid Steer Loaders           | †1<br>! 1  | 10.00 | 65  | 0.37 |
| Building Construction - Phase II  | Tractors/Loaders/Backhoes    | F1         | 10.00 | 97  | 0.37 |
| Building Construction - Phase II  | Trenchers                    | <b></b> 1  | 10.00 | 78  | 0.50 |
| Building Construction - Phase II  | Welders                      | 0          | 10.00 | 46  | 0.45 |
| Architectural Coating - Phase II  | Air Compressors              | <u></u> 1  | 6.00  | 78  | 0.48 |
| Paving - Phase III                | Concrete/Industrial Saws     | 1          | 10.00 | 81  | 0.73 |
| Paving - Phase III                | Graders                      | <u> </u> 1 | 10.00 | 187 | 0.41 |
| Paving - Phase III                | Pavers                       | <u> </u> 1 | 10.00 | 130 | 0.42 |
| Paving - Phase III                | Paving Equipment             | <u> </u> 1 | 10.00 | 132 | 0.36 |
| Paving - Phase III                | Rollers                      | <br>  1    | 10.00 | 80  | 0.38 |
| Paving - Phase III                | Signal Boards                | <br>  1    | 10.00 | 6   | 0.82 |
| Paving - Phase III                | Skid Steer Loaders           | <br>  1    | 10.00 | 65  | 0.37 |
| Paving - Phase III                | Surfacing Equipment          | <br>  1    | 10.00 | 263 | 0.30 |
| Building Construction - Phase III | Concrete/Industrial Saws     | <br>  1    | 10.00 | 81  | 0.73 |
| Building Construction - Phase III | Cranes                       | <br>  1    | 10.00 | 231 | 0.29 |
| Building Construction - Phase III | Forklifts                    | . 0        | 10.00 | 89  | 0.20 |
| Building Construction - Phase III | Generator Sets               | ! 1        | 10.00 | 84  | 0.74 |
| Building Construction - Phase III | Other Construction Equipment | ! 1        | 10.00 | 172 | 0.42 |
| Building Construction - Phase III | Rough Terrain Forklifts      | ! 1        | 10.00 | 100 | 0.40 |
| Building Construction - Phase III | Skid Steer Loaders           | ! 1        | 10.00 | 65  | 0.37 |
| Building Construction - Phase III | Tractors/Loaders/Backhoes    | ! 1        | 10.00 | 97  | 0.37 |
| Building Construction - Phase III | Trenchers                    | ! 1        | 10.00 | 78  | 0.50 |
| Building Construction - Phase III | Welders                      | 0          | 10.00 | 46  | 0.45 |
| Architectural Coating - Phase III | Air Compressors              | 1          | 6.00  | 78  | 0.48 |
| Paving - Phase IV                 | Concrete/Industrial Saws     | 1          | 10.00 | 81  | 0.73 |
| Paving - Phase IV                 | Graders                      | +          | 10.00 | 187 | 0.41 |

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| Paving - Phase IV                | Pavers                       | 1            | 10.00 | 130 | 0.42 |
|----------------------------------|------------------------------|--------------|-------|-----|------|
| Paving - Phase IV                | Paving Equipment             | 1            | 10.00 | 132 | 0.36 |
| Paving - Phase IV                | Rollers                      | 1            | 10.00 | 80  | 0.38 |
| Paving - Phase IV                | Signal Boards                | 1            | 10.00 | 6   | 0.82 |
| Paving - Phase IV                | Skid Steer Loaders           | 1            | 10.00 | 65  | 0.37 |
| Paving - Phase IV                | Surfacing Equipment          | - <b> </b> 1 | 10.00 | 263 | 0.30 |
| Building Construction - Phase IV | Concrete/Industrial Saws     | - <b> </b> 1 | 10.00 | 81  | 0.73 |
| Building Construction - Phase IV | Cranes                       | - <b> </b> 1 | 10.00 | 231 | 0.29 |
| Building Construction - Phase IV | Forklifts                    | 0            | 10.00 | 89  | 0.20 |
| Building Construction - Phase IV | Generator Sets               | - <b> </b> 1 | 10.00 | 84  | 0.74 |
| Building Construction - Phase IV | Other Construction Equipment | - <b> </b> 1 | 10.00 | 172 | 0.42 |
| Building Construction - Phase IV | Rough Terrain Forklifts      | - <b> </b> 1 | 10.00 | 100 | 0.40 |
| Building Construction - Phase IV | Skid Steer Loaders           | - <b> </b> 1 | 10.00 | 65  | 0.37 |
| Building Construction - Phase IV | Tractors/Loaders/Backhoes    | - <b> </b> 1 | 10.00 | 97  | 0.37 |
| Building Construction - Phase IV | Trenchers                    | - <b></b> 1  | 10.00 | 78  | 0.50 |
| Building Construction - Phase IV | Welders                      | 0            | 10.00 | 46  | 0.45 |
| Architectural Coating - Phase IV | Air Compressors              | <u> </u>     | 6.00  | 78  | 0.48 |

**Trips and VMT** 

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| Phase Name              | Offroad Equipment<br>Count | Worker Trip<br>Number | Vendor Trip<br>Number | Hauling Trip<br>Number | Worker Trip<br>Length | Vendor Trip<br>Length | Hauling Trip<br>Length | Worker Vehicle<br>Class | Vendor<br>Vehicle Class | Hauling<br>Vehicle Class |
|-------------------------|----------------------------|-----------------------|-----------------------|------------------------|-----------------------|-----------------------|------------------------|-------------------------|-------------------------|--------------------------|
| Demolition              | 7                          | 18.00                 | 1.00                  | 33.00                  | 10.80                 | 7.30                  | 20.00                  | LD_Mix                  | HDT_Mix                 | HHDT                     |
| Site Preparation        | 5                          | 13.00                 | 1.00                  | 0.00                   | 10.80                 | 7.30                  | 20.00                  | LD_Mix                  | HDT_Mix                 | HHDT                     |
| Grading                 | 13                         | 20.00                 | 1.00                  | 4,000.00               | 10.80                 | 7.30                  | 20.00                  | LD_Mix                  | HDT_Mix                 | HHDT                     |
| Paving - Phase I        | 8                          | 20.00                 | 1.00                  | 0.00                   | 10.80                 | 7.30                  | 20.00                  | LD_Mix                  | HDT_Mix                 | HHDT                     |
| Building Construction - | 8                          | 40.00                 | 1.00                  | 0.00                   | 10.80                 | 7.30                  | 20.00                  | LD_Mix                  | HDT_Mix                 | HHDT                     |
| Architectural Coating - | 1                          | 40.00                 | 1.00                  | 0.00                   | 10.80                 | 7.30                  | 20.00                  | LD_Mix                  | HDT_Mix                 | HHDT                     |
| Paving - Phase II       | 8                          | 20.00                 | 1.00                  | 0.00                   | 10.80                 | 7.30                  | 20.00                  | LD_Mix                  | HDT_Mix                 | HHDT                     |
| Building Construction - | 8                          | 40.00                 | 1.00                  | 0.00                   | 10.80                 | 7.30                  | 20.00                  | LD_Mix                  | HDT_Mix                 | HHDT                     |
| Architectural Coating - | 1                          | 40.00                 | 1.00                  | 0.00                   | 10.80                 | 7.30                  | 20.00                  | LD_Mix                  | HDT_Mix                 | HHDT                     |
| Paving - Phase III      | 8                          | 20.00                 | 1.00                  | 0.00                   | 10.80                 | 7.30                  | 20.00                  | LD_Mix                  | HDT_Mix                 | HHDT                     |
| Building Construction - | 8                          | 40.00                 | 1.00                  | 0.00                   | 10.80                 | 7.30                  | 20.00                  | LD_Mix                  | HDT_Mix                 | HHDT                     |
| Architectural Coating - | 1                          | 40.00                 | 1.00                  | 0.00                   | 10.80                 | 7.30                  | 20.00                  | LD_Mix                  | HDT_Mix                 | HHDT                     |
| Paving - Phase IV       | 8                          | 20.00                 | 1.00                  | 0.00                   | 10.80                 | 7.30                  | 20.00                  | LD_Mix                  | HDT_Mix                 | HHDT                     |
| Building Construction - | 8                          | 40.00                 | 1.00                  | 0.00                   | 10.80                 | 7.30                  | 20.00                  | LD_Mix                  | HDT_Mix                 | HHDT                     |
| Architectural Coating - | 1                          | 40.00                 | 1.00                  | 0.00                   | 10.80                 | 7.30                  | 20.00                  | LD_Mix                  | HDT_Mix                 | HHDT                     |

# **3.1 Mitigation Measures Construction**

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3.2 Demolition - 2020
Unmitigated Construction On-Site

|               | ROG    | NOx    | СО     | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total   | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total     | Bio- CO2 | NBio- CO2 | Total CO2 | CH4    | N2O    | CO2e    |
|---------------|--------|--------|--------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|--------|--------|---------|
| Category      |        |        |        |                 | ton              | s/yr            |                 |                   |                  |                 |          |           | MT        | /yr    |        |         |
| Fugitive Dust |        |        |        |                 | 3.6100e-<br>003  | 0.0000          | 3.6100e-<br>003 | 5.5000e-<br>004   | 0.0000           | 5.5000e-<br>004 | 0.0000   | 0.0000    | 0.0000    | 0.0000 | 0.0000 | 0.0000  |
|               | 0.0882 | 0.8727 | 0.6522 | 1.0700e-<br>003 |                  | 0.0464          | 0.0464          |                   | 0.0432           | 0.0432          | 0.0000   | 93.4562   | 93.4562   | 0.0254 | 0.0000 | 94.0903 |
| Total         | 0.0882 | 0.8727 | 0.6522 | 1.0700e-<br>003 | 3.6100e-<br>003  | 0.0464          | 0.0500          | 5.5000e-<br>004   | 0.0432           | 0.0438          | 0.0000   | 93.4562   | 93.4562   | 0.0254 | 0.0000 | 94.0903 |

|          | ROG             | NOx             | СО              | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total   | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total     | Bio- CO2 | NBio- CO2 | Total CO2 | CH4             | N2O    | CO2e   |
|----------|-----------------|-----------------|-----------------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|--------|--------|
| Category |                 |                 |                 |                 | ton              | s/yr            |                 |                   |                  |                 |          |           | MT        | /yr             |        |        |
| Hauling  | 1.4000e-<br>004 | 4.8400e-<br>003 | 8.5000e-<br>004 | 1.0000e-<br>005 | 2.8000e-<br>004  | 2.0000e-<br>005 | 3.0000e-<br>004 | 8.0000e-<br>005   | 2.0000e-<br>005  | 1.0000e-<br>004 | 0.0000   | 1.2770    | 1.2770    | 5.0000e-<br>005 | 0.0000 | 1.2783 |
| Vendor   | 1.2000e-<br>004 | 3.2500e-<br>003 | 8.3000e-<br>004 | 1.0000e-<br>005 | 1.7000e-<br>004  | 2.0000e-<br>005 | 1.9000e-<br>004 | 5.0000e-<br>005   | 2.0000e-<br>005  | 7.0000e-<br>005 | 0.0000   | 0.7103    | 0.7103    | 4.0000e-<br>005 | 0.0000 | 0.7113 |
| Worker   | 2.0300e-<br>003 | 1.8600e-<br>003 | 0.0166          | 4.0000e-<br>005 | 3.7200e-<br>003  | 3.0000e-<br>005 | 3.7600e-<br>003 | 9.9000e-<br>004   | 3.0000e-<br>005  | 1.0200e-<br>003 | 0.0000   | 3.4573    | 3.4573    | 1.4000e-<br>004 | 0.0000 | 3.4609 |
| Total    | 2.2900e-<br>003 | 9.9500e-<br>003 | 0.0183          | 6.0000e-<br>005 | 4.1700e-<br>003  | 7.0000e-<br>005 | 4.2500e-<br>003 | 1.1200e-<br>003   | 7.0000e-<br>005  | 1.1900e-<br>003 | 0.0000   | 5.4446    | 5.4446    | 2.3000e-<br>004 | 0.0000 | 5.4505 |

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3.2 Demolition - 2020 Mitigated Construction On-Site

|               | ROG    | NOx    | CO     | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total   | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total     | Bio- CO2 | NBio- CO2 | Total CO2 | CH4    | N2O    | CO2e    |
|---------------|--------|--------|--------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|--------|--------|---------|
| Category      |        |        |        |                 | ton              | s/yr            |                 |                   |                  |                 |          |           | MT        | /yr    |        |         |
| Fugitive Dust |        |        |        |                 | 3.6100e-<br>003  | 0.0000          | 3.6100e-<br>003 | 5.5000e-<br>004   | 0.0000           | 5.5000e-<br>004 | 0.0000   | 0.0000    | 0.0000    | 0.0000 | 0.0000 | 0.0000  |
| Off-Road      | 0.0882 | 0.8727 | 0.6522 | 1.0700e-<br>003 |                  | 0.0464          | 0.0464          |                   | 0.0432           | 0.0432          | 0.0000   | 93.4561   | 93.4561   | 0.0254 | 0.0000 | 94.0902 |
| Total         | 0.0882 | 0.8727 | 0.6522 | 1.0700e-<br>003 | 3.6100e-<br>003  | 0.0464          | 0.0500          | 5.5000e-<br>004   | 0.0432           | 0.0438          | 0.0000   | 93.4561   | 93.4561   | 0.0254 | 0.0000 | 94.0902 |

|          | ROG             | NOx             | СО              | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total   | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total     | Bio- CO2 | NBio- CO2 | Total CO2 | CH4             | N2O    | CO2e   |
|----------|-----------------|-----------------|-----------------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|--------|--------|
| Category |                 |                 |                 |                 | ton              | s/yr            |                 |                   |                  |                 |          |           | МТ        | /уг             |        |        |
| Hauling  | 1.4000e-<br>004 | 4.8400e-<br>003 | 8.5000e-<br>004 | 1.0000e-<br>005 | 2.8000e-<br>004  | 2.0000e-<br>005 | 3.0000e-<br>004 | 8.0000e-<br>005   | 2.0000e-<br>005  | 1.0000e-<br>004 | 0.0000   | 1.2770    | 1.2770    | 5.0000e-<br>005 | 0.0000 | 1.2783 |
| Vendor   | 1.2000e-<br>004 | 3.2500e-<br>003 | 8.3000e-<br>004 | 1.0000e-<br>005 | 1.7000e-<br>004  | 2.0000e-<br>005 | 1.9000e-<br>004 | 5.0000e-<br>005   | 2.0000e-<br>005  | 7.0000e-<br>005 | 0.0000   | 0.7103    | 0.7103    | 4.0000e-<br>005 | 0.0000 | 0.7113 |
| Worker   | 2.0300e-<br>003 | 1.8600e-<br>003 | 0.0166          | 4.0000e-<br>005 | 3.7200e-<br>003  | 3.0000e-<br>005 | 3.7600e-<br>003 | 9.9000e-<br>004   | 3.0000e-<br>005  | 1.0200e-<br>003 | 0.0000   | 3.4573    | 3.4573    | 1.4000e-<br>004 | 0.0000 | 3.4609 |
| Total    | 2.2900e-<br>003 | 9.9500e-<br>003 | 0.0183          | 6.0000e-<br>005 | 4.1700e-<br>003  | 7.0000e-<br>005 | 4.2500e-<br>003 | 1.1200e-<br>003   | 7.0000e-<br>005  | 1.1900e-<br>003 | 0.0000   | 5.4446    | 5.4446    | 2.3000e-<br>004 | 0.0000 | 5.4505 |

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# Lico Subdivision Project - Monterey Bay Unified APCD Air District, Annual

3.3 Site Preparation - 2020

<u>Unmitigated Construction On-Site</u>

|               | ROG    | NOx    | CO     | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total | Fugitive<br>PM2.5   | Exhaust<br>PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4    | N2O    | CO2e    |
|---------------|--------|--------|--------|-----------------|------------------|-----------------|---------------|---------------------|------------------|-------------|----------|-----------|-----------|--------|--------|---------|
| Category      |        |        |        |                 | ton              | s/yr            |               |                     |                  |             |          |           | MT        | /yr    |        |         |
| Fugitive Dust |        |        |        |                 | 0.2130           | 0.0000          | 0.2130        | 0.1094              | 0.0000           | 0.1094      | 0.0000   | 0.0000    | 0.0000    | 0.0000 | 0.0000 | 0.0000  |
| Off-Road      | 0.0694 | 0.7589 | 0.3735 | 7.6000e-<br>004 |                  | 0.0363          | 0.0363        | <br> <br> <br> <br> | 0.0334           | 0.0334      | 0.0000   | 66.0012   | 66.0012   | 0.0210 | 0.0000 | 66.5269 |
| Total         | 0.0694 | 0.7589 | 0.3735 | 7.6000e-<br>004 | 0.2130           | 0.0363          | 0.2492        | 0.1094              | 0.0334           | 0.1428      | 0.0000   | 66.0012   | 66.0012   | 0.0210 | 0.0000 | 66.5269 |

|          | ROG             | NOx             | СО              | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total   | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total     | Bio- CO2 | NBio- CO2 | Total CO2 | CH4             | N2O    | CO2e   |
|----------|-----------------|-----------------|-----------------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|--------|--------|
| Category |                 |                 |                 |                 | ton              | s/yr            |                 |                   |                  |                 |          |           | MT        | /yr             |        |        |
| Hauling  | 0.0000          | 0.0000          | 0.0000          | 0.0000          | 0.0000           | 0.0000          | 0.0000          | 0.0000            | 0.0000           | 0.0000          | 0.0000   | 0.0000    | 0.0000    | 0.0000          | 0.0000 | 0.0000 |
| Vendor   | 1.2000e-<br>004 | 3.2500e-<br>003 | 8.3000e-<br>004 | 1.0000e-<br>005 | 1.7000e-<br>004  | 2.0000e-<br>005 | 1.9000e-<br>004 | 5.0000e-<br>005   | 2.0000e-<br>005  | 7.0000e-<br>005 | 0.0000   | 0.7103    | 0.7103    | 4.0000e-<br>005 | 0.0000 | 0.7113 |
| Worker   | 1.4700e-<br>003 | 1.3400e-<br>003 | 0.0120          | 3.0000e-<br>005 | 2.6900e-<br>003  | 2.0000e-<br>005 | 2.7100e-<br>003 | 7.1000e-<br>004   | 2.0000e-<br>005  | 7.4000e-<br>004 | 0.0000   | 2.4969    | 2.4969    | 1.0000e-<br>004 | 0.0000 | 2.4995 |
| Total    | 1.5900e-<br>003 | 4.5900e-<br>003 | 0.0128          | 4.0000e-<br>005 | 2.8600e-<br>003  | 4.0000e-<br>005 | 2.9000e-<br>003 | 7.6000e-<br>004   | 4.0000e-<br>005  | 8.1000e-<br>004 | 0.0000   | 3.2073    | 3.2073    | 1.4000e-<br>004 | 0.0000 | 3.2108 |

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# Lico Subdivision Project - Monterey Bay Unified APCD Air District, Annual

3.3 Site Preparation - 2020 Mitigated Construction On-Site

|               | ROG    | NOx    | CO     | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4    | N2O    | CO2e    |
|---------------|--------|--------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|-------------|----------|-----------|-----------|--------|--------|---------|
| Category      |        |        |        |                 | ton              | s/yr            |               |                   |                  |             |          |           | MT        | /yr    |        |         |
| Fugitive Dust |        |        |        |                 | 0.2130           | 0.0000          | 0.2130        | 0.1094            | 0.0000           | 0.1094      | 0.0000   | 0.0000    | 0.0000    | 0.0000 | 0.0000 | 0.0000  |
| Off-Road      | 0.0694 | 0.7589 | 0.3735 | 7.6000e-<br>004 |                  | 0.0363          | 0.0363        |                   | 0.0334           | 0.0334      | 0.0000   | 66.0012   | 66.0012   | 0.0210 | 0.0000 | 66.5268 |
| Total         | 0.0694 | 0.7589 | 0.3735 | 7.6000e-<br>004 | 0.2130           | 0.0363          | 0.2492        | 0.1094            | 0.0334           | 0.1428      | 0.0000   | 66.0012   | 66.0012   | 0.0210 | 0.0000 | 66.5268 |

|          | ROG             | NOx             | СО              | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total   | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total     | Bio- CO2 | NBio- CO2 | Total CO2 | CH4             | N2O    | CO2e   |
|----------|-----------------|-----------------|-----------------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|--------|--------|
| Category |                 |                 |                 |                 | ton              | s/yr            |                 |                   |                  |                 |          |           | MT        | /yr             |        |        |
| Hauling  | 0.0000          | 0.0000          | 0.0000          | 0.0000          | 0.0000           | 0.0000          | 0.0000          | 0.0000            | 0.0000           | 0.0000          | 0.0000   | 0.0000    | 0.0000    | 0.0000          | 0.0000 | 0.0000 |
| Vendor   | 1.2000e-<br>004 | 3.2500e-<br>003 | 8.3000e-<br>004 | 1.0000e-<br>005 | 1.7000e-<br>004  | 2.0000e-<br>005 | 1.9000e-<br>004 | 5.0000e-<br>005   | 2.0000e-<br>005  | 7.0000e-<br>005 | 0.0000   | 0.7103    | 0.7103    | 4.0000e-<br>005 | 0.0000 | 0.7113 |
| VVOINGI  | 1.4700e-<br>003 | 1.3400e-<br>003 | 0.0120          | 3.0000e-<br>005 | 2.6900e-<br>003  | 2.0000e-<br>005 | 2.7100e-<br>003 | 7.1000e-<br>004   | 2.0000e-<br>005  | 7.4000e-<br>004 | 0.0000   | 2.4969    | 2.4969    | 1.0000e-<br>004 | 0.0000 | 2.4995 |
| Total    | 1.5900e-<br>003 | 4.5900e-<br>003 | 0.0128          | 4.0000e-<br>005 | 2.8600e-<br>003  | 4.0000e-<br>005 | 2.9000e-<br>003 | 7.6000e-<br>004   | 4.0000e-<br>005  | 8.1000e-<br>004 | 0.0000   | 3.2073    | 3.2073    | 1.4000e-<br>004 | 0.0000 | 3.2108 |

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# Lico Subdivision Project - Monterey Bay Unified APCD Air District, Annual

3.4 Grading - 2020
Unmitigated Construction On-Site

|               | ROG    | NOx    | СО     | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total | Fugitive<br>PM2.5   | Exhaust<br>PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4    | N2O    | CO2e     |
|---------------|--------|--------|--------|-----------------|------------------|-----------------|---------------|---------------------|------------------|-------------|----------|-----------|-----------|--------|--------|----------|
| Category      |        |        |        |                 | ton              | s/yr            |               |                     |                  |             |          |           | MT        | /yr    |        |          |
| Fugitive Dust |        |        |        |                 | 0.5318           | 0.0000          | 0.5318        | 0.2304              | 0.0000           | 0.2304      | 0.0000   | 0.0000    | 0.0000    | 0.0000 | 0.0000 | 0.0000   |
| Off-Road      | 0.3181 | 3.5793 | 2.0680 | 4.2500e-<br>003 |                  | 0.1594          | 0.1594        | <br> <br> <br> <br> | 0.1467           | 0.1467      | 0.0000   | 371.6120  | 371.6120  | 0.1191 | 0.0000 | 374.5895 |
| Total         | 0.3181 | 3.5793 | 2.0680 | 4.2500e-<br>003 | 0.5318           | 0.1594          | 0.6911        | 0.2304              | 0.1467           | 0.3772      | 0.0000   | 371.6120  | 371.6120  | 0.1191 | 0.0000 | 374.5895 |

|          | ROG             | NOx             | CO              | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total   | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total     | Bio- CO2 | NBio- CO2 | Total CO2 | CH4             | N2O    | CO2e     |
|----------|-----------------|-----------------|-----------------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|--------|----------|
| Category |                 |                 |                 |                 | ton              | s/yr            |                 |                   |                  |                 |          |           | MT        | /yr             |        |          |
| Hauling  | 0.0167          | 0.5867          | 0.1035          | 1.6200e-<br>003 | 0.0340           | 2.3000e-<br>003 | 0.0363          | 9.3400e-<br>003   | 2.2000e-<br>003  | 0.0115          | 0.0000   | 154.7874  | 154.7874  | 6.2200e-<br>003 | 0.0000 | 154.9429 |
| Vendor   | 2.3000e-<br>004 | 6.5000e-<br>003 | 1.6600e-<br>003 | 1.0000e-<br>005 | 3.4000e-<br>004  | 4.0000e-<br>005 | 3.8000e-<br>004 | 1.0000e-<br>004   | 3.0000e-<br>005  | 1.3000e-<br>004 | 0.0000   | 1.4207    | 1.4207    | 8.0000e-<br>005 | 0.0000 | 1.4226   |
| Worker   | 4.5100e-<br>003 | 4.1200e-<br>003 | 0.0370          | 9.0000e-<br>005 | 8.2700e-<br>003  | 7.0000e-<br>005 | 8.3400e-<br>003 | 2.2000e-<br>003   | 7.0000e-<br>005  | 2.2700e-<br>003 | 0.0000   | 7.6829    | 7.6829    | 3.2000e-<br>004 | 0.0000 | 7.6909   |
| Total    | 0.0214          | 0.5973          | 0.1422          | 1.7200e-<br>003 | 0.0426           | 2.4100e-<br>003 | 0.0450          | 0.0116            | 2.3000e-<br>003  | 0.0139          | 0.0000   | 163.8909  | 163.8909  | 6.6200e-<br>003 | 0.0000 | 164.0563 |

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# Lico Subdivision Project - Monterey Bay Unified APCD Air District, Annual

3.4 Grading - 2020

Mitigated Construction On-Site

|               | ROG    | NOx    | CO     | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4    | N2O    | CO2e     |
|---------------|--------|--------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|-------------|----------|-----------|-----------|--------|--------|----------|
| Category      |        |        |        |                 | ton              | s/yr            |               |                   |                  |             |          |           | МТ        | /yr    |        |          |
| Fugitive Dust | <br>   |        |        |                 | 0.5318           | 0.0000          | 0.5318        | 0.2304            | 0.0000           | 0.2304      | 0.0000   | 0.0000    | 0.0000    | 0.0000 | 0.0000 | 0.0000   |
| Off-Road      | 0.3181 | 3.5793 | 2.0680 | 4.2500e-<br>003 |                  | 0.1594          | 0.1594        | <br>              | 0.1467           | 0.1467      | 0.0000   | 371.6116  | 371.6116  | 0.1191 | 0.0000 | 374.5891 |
| Total         | 0.3181 | 3.5793 | 2.0680 | 4.2500e-<br>003 | 0.5318           | 0.1594          | 0.6911        | 0.2304            | 0.1467           | 0.3772      | 0.0000   | 371.6116  | 371.6116  | 0.1191 | 0.0000 | 374.5891 |

|          | ROG             | NOx             | CO              | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total   | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total     | Bio- CO2 | NBio- CO2 | Total CO2 | CH4             | N2O    | CO2e     |
|----------|-----------------|-----------------|-----------------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|--------|----------|
| Category |                 |                 |                 |                 | ton              | s/yr            |                 |                   |                  |                 |          |           | МТ        | √yr             |        |          |
| Hauling  | 0.0167          | 0.5867          | 0.1035          | 1.6200e-<br>003 | 0.0340           | 2.3000e-<br>003 | 0.0363          | 9.3400e-<br>003   | 2.2000e-<br>003  | 0.0115          | 0.0000   | 154.7874  | 154.7874  | 6.2200e-<br>003 | 0.0000 | 154.9429 |
| Vendor   | 2.3000e-<br>004 | 6.5000e-<br>003 | 1.6600e-<br>003 | 1.0000e-<br>005 | 3.4000e-<br>004  | 4.0000e-<br>005 | 3.8000e-<br>004 | 1.0000e-<br>004   | 3.0000e-<br>005  | 1.3000e-<br>004 | 0.0000   | 1.4207    | 1.4207    | 8.0000e-<br>005 | 0.0000 | 1.4226   |
| Worker   | 4.5100e-<br>003 | 4.1200e-<br>003 | 0.0370          | 9.0000e-<br>005 | 8.2700e-<br>003  | 7.0000e-<br>005 | 8.3400e-<br>003 | 2.2000e-<br>003   | 7.0000e-<br>005  | 2.2700e-<br>003 | 0.0000   | 7.6829    | 7.6829    | 3.2000e-<br>004 | 0.0000 | 7.6909   |
| Total    | 0.0214          | 0.5973          | 0.1422          | 1.7200e-<br>003 | 0.0426           | 2.4100e-<br>003 | 0.0450          | 0.0116            | 2.3000e-<br>003  | 0.0139          | 0.0000   | 163.8909  | 163.8909  | 6.6200e-<br>003 | 0.0000 | 164.0563 |

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# Lico Subdivision Project - Monterey Bay Unified APCD Air District, Annual

3.5 Paving - Phase I - 2020 Unmitigated Construction On-Site

|          | ROG             | NOx    | СО                  | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total | Fugitive<br>PM2.5   | Exhaust<br>PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4    | N2O    | CO2e    |
|----------|-----------------|--------|---------------------|-----------------|------------------|-----------------|---------------|---------------------|------------------|-------------|----------|-----------|-----------|--------|--------|---------|
| Category |                 |        |                     |                 | ton              | s/yr            |               |                     |                  |             |          |           | MT        | /yr    |        |         |
| Off-Road | 0.0323          | 0.3482 | 0.2736              | 5.7000e-<br>004 |                  | 0.0157          | 0.0157        |                     | 0.0147           | 0.0147      | 0.0000   | 49.6774   | 49.6774   | 0.0135 | 0.0000 | 50.0160 |
| Paving   | 3.8000e-<br>003 | <br>   | <br> <br> <br> <br> |                 |                  | 0.0000          | 0.0000        | <br> <br> <br> <br> | 0.0000           | 0.0000      | 0.0000   | 0.0000    | 0.0000    | 0.0000 | 0.0000 | 0.0000  |
| Total    | 0.0361          | 0.3482 | 0.2736              | 5.7000e-<br>004 |                  | 0.0157          | 0.0157        |                     | 0.0147           | 0.0147      | 0.0000   | 49.6774   | 49.6774   | 0.0135 | 0.0000 | 50.0160 |

|          | ROG             | NOx             | СО              | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total   | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total     | Bio- CO2 | NBio- CO2 | Total CO2 | CH4             | N2O    | CO2e   |
|----------|-----------------|-----------------|-----------------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|--------|--------|
| Category |                 |                 |                 |                 | ton              | s/yr            |                 |                   |                  |                 |          |           | МТ        | /yr             |        |        |
| Hauling  | 0.0000          | 0.0000          | 0.0000          | 0.0000          | 0.0000           | 0.0000          | 0.0000          | 0.0000            | 0.0000           | 0.0000          | 0.0000   | 0.0000    | 0.0000    | 0.0000          | 0.0000 | 0.0000 |
| Vendor   | 6.0000e-<br>005 | 1.6900e-<br>003 | 4.3000e-<br>004 | 0.0000          | 9.0000e-<br>005  | 1.0000e-<br>005 | 1.0000e-<br>004 | 3.0000e-<br>005   | 1.0000e-<br>005  | 3.0000e-<br>005 | 0.0000   | 0.3688    | 0.3688    | 2.0000e-<br>005 | 0.0000 | 0.3693 |
| Worker   | 1.1700e-<br>003 | 1.0700e-<br>003 | 9.6000e-<br>003 | 2.0000e-<br>005 | 2.1500e-<br>003  | 2.0000e-<br>005 | 2.1700e-<br>003 | 5.7000e-<br>004   | 2.0000e-<br>005  | 5.9000e-<br>004 | 0.0000   | 1.9946    | 1.9946    | 8.0000e-<br>005 | 0.0000 | 1.9967 |
| Total    | 1.2300e-<br>003 | 2.7600e-<br>003 | 0.0100          | 2.0000e-<br>005 | 2.2400e-<br>003  | 3.0000e-<br>005 | 2.2700e-<br>003 | 6.0000e-<br>004   | 3.0000e-<br>005  | 6.2000e-<br>004 | 0.0000   | 2.3634    | 2.3634    | 1.0000e-<br>004 | 0.0000 | 2.3660 |

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# Lico Subdivision Project - Monterey Bay Unified APCD Air District, Annual

3.5 Paving - Phase I - 2020 Mitigated Construction On-Site

|          | ROG             | NOx    | CO          | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4    | N2O    | CO2e    |
|----------|-----------------|--------|-------------|-----------------|------------------|-----------------|---------------|-------------------|------------------|-------------|----------|-----------|-----------|--------|--------|---------|
| Category |                 |        |             |                 | ton              | s/yr            |               |                   |                  |             |          |           | MT        | /yr    |        |         |
| Off-Road | 0.0323          | 0.3482 | 0.2736      | 5.7000e-<br>004 |                  | 0.0157          | 0.0157        | i<br>i            | 0.0147           | 0.0147      | 0.0000   | 49.6774   | 49.6774   | 0.0135 | 0.0000 | 50.0159 |
| Paving   | 3.8000e-<br>003 |        | 1<br>1<br>1 |                 |                  | 0.0000          | 0.0000        | ]<br>             | 0.0000           | 0.0000      | 0.0000   | 0.0000    | 0.0000    | 0.0000 | 0.0000 | 0.0000  |
| Total    | 0.0361          | 0.3482 | 0.2736      | 5.7000e-<br>004 |                  | 0.0157          | 0.0157        |                   | 0.0147           | 0.0147      | 0.0000   | 49.6774   | 49.6774   | 0.0135 | 0.0000 | 50.0159 |

|          | ROG             | NOx             | СО              | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total   | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total     | Bio- CO2 | NBio- CO2 | Total CO2 | CH4             | N2O    | CO2e   |
|----------|-----------------|-----------------|-----------------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|--------|--------|
| Category |                 |                 |                 |                 | ton              | s/yr            |                 |                   |                  |                 |          |           | MT        | /yr             |        |        |
| Hauling  | 0.0000          | 0.0000          | 0.0000          | 0.0000          | 0.0000           | 0.0000          | 0.0000          | 0.0000            | 0.0000           | 0.0000          | 0.0000   | 0.0000    | 0.0000    | 0.0000          | 0.0000 | 0.0000 |
| Vendor   | 6.0000e-<br>005 | 1.6900e-<br>003 | 4.3000e-<br>004 | 0.0000          | 9.0000e-<br>005  | 1.0000e-<br>005 | 1.0000e-<br>004 | 3.0000e-<br>005   | 1.0000e-<br>005  | 3.0000e-<br>005 | 0.0000   | 0.3688    | 0.3688    | 2.0000e-<br>005 | 0.0000 | 0.3693 |
| Worker   | 1.1700e-<br>003 | 1.0700e-<br>003 | 9.6000e-<br>003 | 2.0000e-<br>005 | 2.1500e-<br>003  | 2.0000e-<br>005 | 2.1700e-<br>003 | 5.7000e-<br>004   | 2.0000e-<br>005  | 5.9000e-<br>004 | 0.0000   | 1.9946    | 1.9946    | 8.0000e-<br>005 | 0.0000 | 1.9967 |
| Total    | 1.2300e-<br>003 | 2.7600e-<br>003 | 0.0100          | 2.0000e-<br>005 | 2.2400e-<br>003  | 3.0000e-<br>005 | 2.2700e-<br>003 | 6.0000e-<br>004   | 3.0000e-<br>005  | 6.2000e-<br>004 | 0.0000   | 2.3634    | 2.3634    | 1.0000e-<br>004 | 0.0000 | 2.3660 |

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# Lico Subdivision Project - Monterey Bay Unified APCD Air District, Annual

3.5 Paving - Phase I - 2021

<u>Unmitigated Construction On-Site</u>

|          | ROG    | NOx    | CO          | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4    | N2O    | CO2e     |
|----------|--------|--------|-------------|-----------------|------------------|-----------------|---------------|-------------------|------------------|-------------|----------|-----------|-----------|--------|--------|----------|
| Category |        |        |             |                 | ton              | s/yr            |               |                   |                  |             |          |           | MT        | /yr    |        |          |
| Off-Road | 0.0864 | 0.9252 | 0.7763      | 1.6300e-<br>003 |                  | 0.0406          | 0.0406        |                   | 0.0380           | 0.0380      | 0.0000   | 141.6244  | 141.6244  | 0.0385 | 0.0000 | 142.5861 |
| Paving   | 0.0108 | <br>   | 1<br>1<br>1 |                 |                  | 0.0000          | 0.0000        | 1<br>1<br>1       | 0.0000           | 0.0000      | 0.0000   | 0.0000    | 0.0000    | 0.0000 | 0.0000 | 0.0000   |
| Total    | 0.0972 | 0.9252 | 0.7763      | 1.6300e-<br>003 |                  | 0.0406          | 0.0406        |                   | 0.0380           | 0.0380      | 0.0000   | 141.6244  | 141.6244  | 0.0385 | 0.0000 | 142.5861 |

|          | ROG             | NOx             | СО              | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total   | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total     | Bio- CO2 | NBio- CO2 | Total CO2 | CH4             | N2O    | CO2e   |
|----------|-----------------|-----------------|-----------------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|--------|--------|
| Category |                 |                 |                 |                 | ton              | s/yr            |                 |                   |                  |                 |          |           | MT        | /yr             |        |        |
| Hauling  | 0.0000          | 0.0000          | 0.0000          | 0.0000          | 0.0000           | 0.0000          | 0.0000          | 0.0000            | 0.0000           | 0.0000          | 0.0000   | 0.0000    | 0.0000    | 0.0000          | 0.0000 | 0.0000 |
| Vendor   | 1.4000e-<br>004 | 4.3900e-<br>003 | 1.0700e-<br>003 | 1.0000e-<br>005 | 2.5000e-<br>004  | 1.0000e-<br>005 | 2.7000e-<br>004 | 7.0000e-<br>005   | 1.0000e-<br>005  | 9.0000e-<br>005 | 0.0000   | 1.0427    | 1.0427    | 6.0000e-<br>005 | 0.0000 | 1.0441 |
| Worker   | 3.0900e-<br>003 | 2.7300e-<br>003 | 0.0249          | 6.0000e-<br>005 | 6.1300e-<br>003  | 5.0000e-<br>005 | 6.1800e-<br>003 | 1.6300e-<br>003   | 5.0000e-<br>005  | 1.6800e-<br>003 | 0.0000   | 5.5102    | 5.5102    | 2.1000e-<br>004 | 0.0000 | 5.5155 |
| Total    | 3.2300e-<br>003 | 7.1200e-<br>003 | 0.0260          | 7.0000e-<br>005 | 6.3800e-<br>003  | 6.0000e-<br>005 | 6.4500e-<br>003 | 1.7000e-<br>003   | 6.0000e-<br>005  | 1.7700e-<br>003 | 0.0000   | 6.5529    | 6.5529    | 2.7000e-<br>004 | 0.0000 | 6.5596 |

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3.5 Paving - Phase I - 2021 Mitigated Construction On-Site

|          | ROG    | NOx    | CO          | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5<br>Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4    | N2O    | CO2e     |
|----------|--------|--------|-------------|-----------------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|-----------|-----------|--------|--------|----------|
| Category |        |        |             |                 | ton              | s/yr            |               |                   |                  |                |          |           | MT        | /yr    |        |          |
| Off-Road | 0.0864 | 0.9252 | 0.7763      | 1.6300e-<br>003 |                  | 0.0406          | 0.0406        |                   | 0.0380           | 0.0380         | 0.0000   | 141.6243  | 141.6243  | 0.0385 | 0.0000 | 142.5859 |
| Paving   | 0.0108 |        | 1<br>1<br>1 |                 |                  | 0.0000          | 0.0000        |                   | 0.0000           | 0.0000         | 0.0000   | 0.0000    | 0.0000    | 0.0000 | 0.0000 | 0.0000   |
| Total    | 0.0972 | 0.9252 | 0.7763      | 1.6300e-<br>003 |                  | 0.0406          | 0.0406        |                   | 0.0380           | 0.0380         | 0.0000   | 141.6243  | 141.6243  | 0.0385 | 0.0000 | 142.5859 |

|          | ROG             | NOx             | CO              | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total   | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total     | Bio- CO2 | NBio- CO2 | Total CO2 | CH4             | N2O    | CO2e   |
|----------|-----------------|-----------------|-----------------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|--------|--------|
| Category |                 |                 |                 |                 | ton              | s/yr            |                 |                   |                  |                 |          |           | MT        | /yr             |        |        |
| Hauling  | 0.0000          | 0.0000          | 0.0000          | 0.0000          | 0.0000           | 0.0000          | 0.0000          | 0.0000            | 0.0000           | 0.0000          | 0.0000   | 0.0000    | 0.0000    | 0.0000          | 0.0000 | 0.0000 |
| Vendor   | 1.4000e-<br>004 | 4.3900e-<br>003 | 1.0700e-<br>003 | 1.0000e-<br>005 | 2.5000e-<br>004  | 1.0000e-<br>005 | 2.7000e-<br>004 | 7.0000e-<br>005   | 1.0000e-<br>005  | 9.0000e-<br>005 | 0.0000   | 1.0427    | 1.0427    | 6.0000e-<br>005 | 0.0000 | 1.0441 |
| Worker   | 3.0900e-<br>003 | 2.7300e-<br>003 | 0.0249          | 6.0000e-<br>005 | 6.1300e-<br>003  | 5.0000e-<br>005 | 6.1800e-<br>003 | 1.6300e-<br>003   | 5.0000e-<br>005  | 1.6800e-<br>003 | 0.0000   | 5.5102    | 5.5102    | 2.1000e-<br>004 | 0.0000 | 5.5155 |
| Total    | 3.2300e-<br>003 | 7.1200e-<br>003 | 0.0260          | 7.0000e-<br>005 | 6.3800e-<br>003  | 6.0000e-<br>005 | 6.4500e-<br>003 | 1.7000e-<br>003   | 6.0000e-<br>005  | 1.7700e-<br>003 | 0.0000   | 6.5529    | 6.5529    | 2.7000e-<br>004 | 0.0000 | 6.5596 |

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# 3.6 Building Construction - Phase I - 2021 <u>Unmitigated Construction On-Site</u>

|          | ROG    | NOx    | СО     | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4    | N2O    | CO2e     |
|----------|--------|--------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|-------------|----------|-----------|-----------|--------|--------|----------|
| Category |        |        |        |                 | ton              | s/yr            |               |                   |                  |             |          |           | MT        | /yr    |        |          |
|          | 0.3076 | 3.0789 | 2.8806 | 4.8300e-<br>003 |                  | 0.1624          | 0.1624        |                   | 0.1529           | 0.1529      | 0.0000   | 420.8759  | 420.8759  | 0.0972 | 0.0000 | 423.3056 |
| Total    | 0.3076 | 3.0789 | 2.8806 | 4.8300e-<br>003 |                  | 0.1624          | 0.1624        |                   | 0.1529           | 0.1529      | 0.0000   | 420.8759  | 420.8759  | 0.0972 | 0.0000 | 423.3056 |

|          | ROG             | NOx    | СО              | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total   | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total     | Bio- CO2 | NBio- CO2 | Total CO2 | CH4              | N2O    | CO2e    |
|----------|-----------------|--------|-----------------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|------------------|--------|---------|
| Category |                 |        |                 |                 | ton              | s/yr            |                 |                   |                  |                 |          |           | MT        | <sup>-</sup> /yr |        |         |
| Hauling  | 0.0000          | 0.0000 | 0.0000          | 0.0000          | 0.0000           | 0.0000          | 0.0000          | 0.0000            | 0.0000           | 0.0000          | 0.0000   | 0.0000    | 0.0000    | 0.0000           | 0.0000 | 0.0000  |
| Vendor   | 3.9000e-<br>004 | 0.0120 | 2.9100e-<br>003 | 3.0000e-<br>005 | 6.9000e-<br>004  | 4.0000e-<br>005 | 7.3000e-<br>004 | 2.0000e-<br>004   | 3.0000e-<br>005  | 2.3000e-<br>004 | 0.0000   | 2.8438    | 2.8438    | 1.5000e-<br>004  | 0.0000 | 2.8476  |
| Worker   | 0.0169          | 0.0149 | 0.1359          | 3.3000e-<br>004 | 0.0334           | 2.8000e-<br>004 | 0.0337          | 8.8800e-<br>003   | 2.6000e-<br>004  | 9.1400e-<br>003 | 0.0000   | 30.0555   | 30.0555   | 1.1600e-<br>003  | 0.0000 | 30.0844 |
| Total    | 0.0173          | 0.0269 | 0.1388          | 3.6000e-<br>004 | 0.0341           | 3.2000e-<br>004 | 0.0344          | 9.0800e-<br>003   | 2.9000e-<br>004  | 9.3700e-<br>003 | 0.0000   | 32.8993   | 32.8993   | 1.3100e-<br>003  | 0.0000 | 32.9320 |

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# 3.6 Building Construction - Phase I - 2021 Mitigated Construction On-Site

|          | ROG    | NOx    | СО     | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4    | N2O    | CO2e     |
|----------|--------|--------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|-------------|----------|-----------|-----------|--------|--------|----------|
| Category |        |        |        |                 | ton              | s/yr            |               |                   |                  |             |          |           | MT        | /yr    |        |          |
|          | 0.3076 | 3.0789 | 2.8806 | 4.8300e-<br>003 |                  | 0.1624          | 0.1624        |                   | 0.1529           | 0.1529      | 0.0000   | 420.8754  | 420.8754  | 0.0972 | 0.0000 | 423.3051 |
| Total    | 0.3076 | 3.0789 | 2.8806 | 4.8300e-<br>003 |                  | 0.1624          | 0.1624        |                   | 0.1529           | 0.1529      | 0.0000   | 420.8754  | 420.8754  | 0.0972 | 0.0000 | 423.3051 |

|          | ROG             | NOx    | СО              | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total   | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total     | Bio- CO2 | NBio- CO2 | Total CO2 | CH4             | N2O    | CO2e    |
|----------|-----------------|--------|-----------------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|--------|---------|
| Category |                 |        |                 |                 | ton              | s/yr            |                 |                   |                  |                 |          |           | MT        | /yr             |        |         |
| Hauling  | 0.0000          | 0.0000 | 0.0000          | 0.0000          | 0.0000           | 0.0000          | 0.0000          | 0.0000            | 0.0000           | 0.0000          | 0.0000   | 0.0000    | 0.0000    | 0.0000          | 0.0000 | 0.0000  |
| Vendor   | 3.9000e-<br>004 | 0.0120 | 2.9100e-<br>003 | 3.0000e-<br>005 | 6.9000e-<br>004  | 4.0000e-<br>005 | 7.3000e-<br>004 | 2.0000e-<br>004   | 3.0000e-<br>005  | 2.3000e-<br>004 | 0.0000   | 2.8438    | 2.8438    | 1.5000e-<br>004 | 0.0000 | 2.8476  |
| Worker   | 0.0169          | 0.0149 | 0.1359          | 3.3000e-<br>004 | 0.0334           | 2.8000e-<br>004 | 0.0337          | 8.8800e-<br>003   | 2.6000e-<br>004  | 9.1400e-<br>003 | 0.0000   | 30.0555   | 30.0555   | 1.1600e-<br>003 | 0.0000 | 30.0844 |
| Total    | 0.0173          | 0.0269 | 0.1388          | 3.6000e-<br>004 | 0.0341           | 3.2000e-<br>004 | 0.0344          | 9.0800e-<br>003   | 2.9000e-<br>004  | 9.3700e-<br>003 | 0.0000   | 32.8993   | 32.8993   | 1.3100e-<br>003 | 0.0000 | 32.9320 |

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# Lico Subdivision Project - Monterey Bay Unified APCD Air District, Annual

# 3.7 Architectural Coating - Phase I - 2021 <u>Unmitigated Construction On-Site</u>

|          | ROG             | NOx    | CO     | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total   | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total     | Bio- CO2 | NBio- CO2 | Total CO2 | CH4             | N2O    | CO2e   |
|----------|-----------------|--------|--------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|--------|--------|
| Category |                 |        |        |                 | ton              | s/yr            |                 |                   |                  |                 |          |           | МТ        | /yr             |        |        |
| 7        | 0.2775          |        |        |                 |                  | 0.0000          | 0.0000          |                   | 0.0000           | 0.0000          | 0.0000   | 0.0000    | 0.0000    | 0.0000          | 0.0000 | 0.0000 |
| 1        | 8.5400e-<br>003 | 0.0596 | 0.0709 | 1.2000e-<br>004 |                  | 3.6700e-<br>003 | 3.6700e-<br>003 | <br>              | 3.6700e-<br>003  | 3.6700e-<br>003 | 0.0000   | 9.9577    | 9.9577    | 6.8000e-<br>004 | 0.0000 | 9.9748 |
| Total    | 0.2861          | 0.0596 | 0.0709 | 1.2000e-<br>004 |                  | 3.6700e-<br>003 | 3.6700e-<br>003 |                   | 3.6700e-<br>003  | 3.6700e-<br>003 | 0.0000   | 9.9577    | 9.9577    | 6.8000e-<br>004 | 0.0000 | 9.9748 |

|          | ROG             | NOx             | CO              | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total   | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total     | Bio- CO2 | NBio- CO2 | Total CO2 | CH4             | N2O    | CO2e    |
|----------|-----------------|-----------------|-----------------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|--------|---------|
| Category |                 |                 |                 |                 | ton              | s/yr            |                 |                   |                  |                 |          |           | МТ        | /yr             |        |         |
| Hauling  | 0.0000          | 0.0000          | 0.0000          | 0.0000          | 0.0000           | 0.0000          | 0.0000          | 0.0000            | 0.0000           | 0.0000          | 0.0000   | 0.0000    | 0.0000    | 0.0000          | 0.0000 | 0.0000  |
| Vendor   | 1.4000e-<br>004 | 4.4500e-<br>003 | 1.0800e-<br>003 | 1.0000e-<br>005 | 2.6000e-<br>004  | 1.0000e-<br>005 | 2.7000e-<br>004 | 7.0000e-<br>005   | 1.0000e-<br>005  | 9.0000e-<br>005 | 0.0000   | 1.0563    | 1.0563    | 6.0000e-<br>005 | 0.0000 | 1.0577  |
| Worker   | 6.2600e-<br>003 | 5.5200e-<br>003 | 0.0505          | 1.2000e-<br>004 | 0.0124           | 1.0000e-<br>004 | 0.0125          | 3.3000e-<br>003   | 1.0000e-<br>004  | 3.4000e-<br>003 | 0.0000   | 11.1635   | 11.1635   | 4.3000e-<br>004 | 0.0000 | 11.1742 |
| Total    | 6.4000e-<br>003 | 9.9700e-<br>003 | 0.0516          | 1.3000e-<br>004 | 0.0127           | 1.1000e-<br>004 | 0.0128          | 3.3700e-<br>003   | 1.1000e-<br>004  | 3.4900e-<br>003 | 0.0000   | 12.2198   | 12.2198   | 4.9000e-<br>004 | 0.0000 | 12.2319 |

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# 3.7 Architectural Coating - Phase I - 2021 <u>Mitigated Construction On-Site</u>

|                 | ROG             | NOx    | CO     | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total   | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total     | Bio- CO2 | NBio- CO2 | Total CO2 | CH4             | N2O    | CO2e   |
|-----------------|-----------------|--------|--------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|--------|--------|
| Category        |                 |        |        |                 | ton              | s/yr            |                 |                   |                  |                 |          |           | MT        | /yr             |        |        |
| Archit. Coating | 0.2775          |        |        |                 |                  | 0.0000          | 0.0000          |                   | 0.0000           | 0.0000          | 0.0000   | 0.0000    | 0.0000    | 0.0000          | 0.0000 | 0.0000 |
| Off-Road        | 8.5400e-<br>003 | 0.0596 | 0.0709 | 1.2000e-<br>004 |                  | 3.6700e-<br>003 | 3.6700e-<br>003 |                   | 3.6700e-<br>003  | 3.6700e-<br>003 | 0.0000   | 9.9577    | 9.9577    | 6.8000e-<br>004 | 0.0000 | 9.9748 |
| Total           | 0.2861          | 0.0596 | 0.0709 | 1.2000e-<br>004 |                  | 3.6700e-<br>003 | 3.6700e-<br>003 |                   | 3.6700e-<br>003  | 3.6700e-<br>003 | 0.0000   | 9.9577    | 9.9577    | 6.8000e-<br>004 | 0.0000 | 9.9748 |

|          | ROG             | NOx             | CO              | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total   | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total     | Bio- CO2 | NBio- CO2 | Total CO2 | CH4             | N2O    | CO2e    |
|----------|-----------------|-----------------|-----------------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|--------|---------|
| Category |                 |                 |                 |                 | ton              | s/yr            |                 |                   |                  |                 |          |           | MT        | /yr             |        |         |
| Hauling  | 0.0000          | 0.0000          | 0.0000          | 0.0000          | 0.0000           | 0.0000          | 0.0000          | 0.0000            | 0.0000           | 0.0000          | 0.0000   | 0.0000    | 0.0000    | 0.0000          | 0.0000 | 0.0000  |
| Vendor   | 1.4000e-<br>004 | 4.4500e-<br>003 | 1.0800e-<br>003 | 1.0000e-<br>005 | 2.6000e-<br>004  | 1.0000e-<br>005 | 2.7000e-<br>004 | 7.0000e-<br>005   | 1.0000e-<br>005  | 9.0000e-<br>005 | 0.0000   | 1.0563    | 1.0563    | 6.0000e-<br>005 | 0.0000 | 1.0577  |
| Worker   | 6.2600e-<br>003 | 5.5200e-<br>003 | 0.0505          | 1.2000e-<br>004 | 0.0124           | 1.0000e-<br>004 | 0.0125          | 3.3000e-<br>003   | 1.0000e-<br>004  | 3.4000e-<br>003 | 0.0000   | 11.1635   | 11.1635   | 4.3000e-<br>004 | 0.0000 | 11.1742 |
| Total    | 6.4000e-<br>003 | 9.9700e-<br>003 | 0.0516          | 1.3000e-<br>004 | 0.0127           | 1.1000e-<br>004 | 0.0128          | 3.3700e-<br>003   | 1.1000e-<br>004  | 3.4900e-<br>003 | 0.0000   | 12.2198   | 12.2198   | 4.9000e-<br>004 | 0.0000 | 12.2319 |

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3.8 Paving - Phase II - 2021 Unmitigated Construction On-Site

|          | ROG             | NOx    | СО                  | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4    | N2O    | CO2e    |
|----------|-----------------|--------|---------------------|-----------------|------------------|-----------------|---------------|-------------------|------------------|-------------|----------|-----------|-----------|--------|--------|---------|
| Category |                 |        |                     |                 | ton              | s/yr            |               |                   |                  |             |          |           | MT        | /yr    |        |         |
| Off-Road | 0.0303          | 0.3244 | 0.2722              | 5.7000e-<br>004 |                  | 0.0142          | 0.0142        |                   | 0.0133           | 0.0133      | 0.0000   | 49.6605   | 49.6605   | 0.0135 | 0.0000 | 49.9977 |
| Paving   | 3.8000e-<br>003 | <br>   | <br> <br> <br> <br> |                 |                  | 0.0000          | 0.0000        |                   | 0.0000           | 0.0000      | 0.0000   | 0.0000    | 0.0000    | 0.0000 | 0.0000 | 0.0000  |
| Total    | 0.0341          | 0.3244 | 0.2722              | 5.7000e-<br>004 |                  | 0.0142          | 0.0142        |                   | 0.0133           | 0.0133      | 0.0000   | 49.6605   | 49.6605   | 0.0135 | 0.0000 | 49.9977 |

|          | ROG             | NOx             | СО              | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total   | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total     | Bio- CO2 | NBio- CO2 | Total CO2 | CH4             | N2O    | CO2e   |
|----------|-----------------|-----------------|-----------------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|--------|--------|
| Category |                 |                 |                 |                 | ton              | s/yr            |                 |                   |                  |                 |          |           | МТ        | /уг             |        |        |
| Hauling  | 0.0000          | 0.0000          | 0.0000          | 0.0000          | 0.0000           | 0.0000          | 0.0000          | 0.0000            | 0.0000           | 0.0000          | 0.0000   | 0.0000    | 0.0000    | 0.0000          | 0.0000 | 0.0000 |
| Vendor   | 5.0000e-<br>005 | 1.5400e-<br>003 | 3.7000e-<br>004 | 0.0000          | 9.0000e-<br>005  | 0.0000          | 9.0000e-<br>005 | 3.0000e-<br>005   | 0.0000           | 3.0000e-<br>005 | 0.0000   | 0.3656    | 0.3656    | 2.0000e-<br>005 | 0.0000 | 0.3661 |
| Worker   | 1.0800e-<br>003 | 9.6000e-<br>004 | 8.7400e-<br>003 | 2.0000e-<br>005 | 2.1500e-<br>003  | 2.0000e-<br>005 | 2.1700e-<br>003 | 5.7000e-<br>004   | 2.0000e-<br>005  | 5.9000e-<br>004 | 0.0000   | 1.9321    | 1.9321    | 7.0000e-<br>005 | 0.0000 | 1.9340 |
| Total    | 1.1300e-<br>003 | 2.5000e-<br>003 | 9.1100e-<br>003 | 2.0000e-<br>005 | 2.2400e-<br>003  | 2.0000e-<br>005 | 2.2600e-<br>003 | 6.0000e-<br>004   | 2.0000e-<br>005  | 6.2000e-<br>004 | 0.0000   | 2.2978    | 2.2978    | 9.0000e-<br>005 | 0.0000 | 2.3001 |

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3.8 Paving - Phase II - 2021 Mitigated Construction On-Site

|          | ROG             | NOx    | CO     | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5<br>Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4    | N2O    | CO2e    |
|----------|-----------------|--------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|-----------|-----------|--------|--------|---------|
| Category |                 |        |        |                 | ton              | s/yr            |               |                   |                  |                |          |           | MT        | /yr    |        |         |
| Off-Road | 0.0303          | 0.3244 | 0.2722 | 5.7000e-<br>004 |                  | 0.0142          | 0.0142        |                   | 0.0133           | 0.0133         | 0.0000   | 49.6605   | 49.6605   | 0.0135 | 0.0000 | 49.9977 |
| Paving   | 3.8000e-<br>003 |        |        |                 |                  | 0.0000          | 0.0000        | <br>              | 0.0000           | 0.0000         | 0.0000   | 0.0000    | 0.0000    | 0.0000 | 0.0000 | 0.0000  |
| Total    | 0.0341          | 0.3244 | 0.2722 | 5.7000e-<br>004 |                  | 0.0142          | 0.0142        |                   | 0.0133           | 0.0133         | 0.0000   | 49.6605   | 49.6605   | 0.0135 | 0.0000 | 49.9977 |

|          | ROG             | NOx             | СО              | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total   | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total     | Bio- CO2 | NBio- CO2 | Total CO2 | CH4             | N2O    | CO2e   |
|----------|-----------------|-----------------|-----------------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|--------|--------|
| Category |                 |                 |                 |                 | ton              | s/yr            |                 |                   |                  |                 |          |           | МТ        | /yr             |        |        |
| Hauling  | 0.0000          | 0.0000          | 0.0000          | 0.0000          | 0.0000           | 0.0000          | 0.0000          | 0.0000            | 0.0000           | 0.0000          | 0.0000   | 0.0000    | 0.0000    | 0.0000          | 0.0000 | 0.0000 |
| Vendor   | 5.0000e-<br>005 | 1.5400e-<br>003 | 3.7000e-<br>004 | 0.0000          | 9.0000e-<br>005  | 0.0000          | 9.0000e-<br>005 | 3.0000e-<br>005   | 0.0000           | 3.0000e-<br>005 | 0.0000   | 0.3656    | 0.3656    | 2.0000e-<br>005 | 0.0000 | 0.3661 |
| Worker   | 1.0800e-<br>003 | 9.6000e-<br>004 | 8.7400e-<br>003 | 2.0000e-<br>005 | 2.1500e-<br>003  | 2.0000e-<br>005 | 2.1700e-<br>003 | 5.7000e-<br>004   | 2.0000e-<br>005  | 5.9000e-<br>004 | 0.0000   | 1.9321    | 1.9321    | 7.0000e-<br>005 | 0.0000 | 1.9340 |
| Total    | 1.1300e-<br>003 | 2.5000e-<br>003 | 9.1100e-<br>003 | 2.0000e-<br>005 | 2.2400e-<br>003  | 2.0000e-<br>005 | 2.2600e-<br>003 | 6.0000e-<br>004   | 2.0000e-<br>005  | 6.2000e-<br>004 | 0.0000   | 2.2978    | 2.2978    | 9.0000e-<br>005 | 0.0000 | 2.3001 |

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3.8 Paving - Phase II - 2022 Unmitigated Construction On-Site

|          | ROG    | NOx    | СО                  | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4    | N2O    | CO2e     |
|----------|--------|--------|---------------------|-----------------|------------------|-----------------|---------------|-------------------|------------------|-------------|----------|-----------|-----------|--------|--------|----------|
| Category |        |        |                     |                 | ton              | s/yr            |               |                   |                  |             |          |           | MT        | /yr    |        |          |
| Off-Road | 0.0787 | 0.8218 | 0.7690              | 1.6300e-<br>003 |                  | 0.0351          | 0.0351        |                   | 0.0329           | 0.0329      | 0.0000   | 141.5506  | 141.5506  | 0.0384 | 0.0000 | 142.5094 |
| Paving   | 0.0108 | <br>   | <br> <br> <br> <br> |                 |                  | 0.0000          | 0.0000        | <br>              | 0.0000           | 0.0000      | 0.0000   | 0.0000    | 0.0000    | 0.0000 | 0.0000 | 0.0000   |
| Total    | 0.0895 | 0.8218 | 0.7690              | 1.6300e-<br>003 |                  | 0.0351          | 0.0351        |                   | 0.0329           | 0.0329      | 0.0000   | 141.5506  | 141.5506  | 0.0384 | 0.0000 | 142.5094 |

|          | ROG             | NOx             | СО              | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total   | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total     | Bio- CO2 | NBio- CO2 | Total CO2 | CH4             | N2O    | CO2e   |
|----------|-----------------|-----------------|-----------------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|--------|--------|
| Category |                 |                 |                 |                 | ton              | s/yr            |                 |                   |                  |                 |          |           | МТ        | /yr             |        |        |
| Hauling  | 0.0000          | 0.0000          | 0.0000          | 0.0000          | 0.0000           | 0.0000          | 0.0000          | 0.0000            | 0.0000           | 0.0000          | 0.0000   | 0.0000    | 0.0000    | 0.0000          | 0.0000 | 0.0000 |
| Vendor   | 1.3000e-<br>004 | 4.1500e-<br>003 | 9.7000e-<br>004 | 1.0000e-<br>005 | 2.5000e-<br>004  | 1.0000e-<br>005 | 2.7000e-<br>004 | 7.0000e-<br>005   | 1.0000e-<br>005  | 8.0000e-<br>005 | 0.0000   | 1.0333    | 1.0333    | 5.0000e-<br>005 | 0.0000 | 1.0347 |
| Worker   | 2.8700e-<br>003 | 2.4400e-<br>003 | 0.0227          | 6.0000e-<br>005 | 6.1300e-<br>003  | 5.0000e-<br>005 | 6.1800e-<br>003 | 1.6300e-<br>003   | 5.0000e-<br>005  | 1.6700e-<br>003 | 0.0000   | 5.3159    | 5.3159    | 1.9000e-<br>004 | 0.0000 | 5.3206 |
| Total    | 3.0000e-<br>003 | 6.5900e-<br>003 | 0.0237          | 7.0000e-<br>005 | 6.3800e-<br>003  | 6.0000e-<br>005 | 6.4500e-<br>003 | 1.7000e-<br>003   | 6.0000e-<br>005  | 1.7500e-<br>003 | 0.0000   | 6.3492    | 6.3492    | 2.4000e-<br>004 | 0.0000 | 6.3553 |

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3.8 Paving - Phase II - 2022 Mitigated Construction On-Site

|          | ROG    | NOx    | CO     | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4    | N2O    | CO2e     |
|----------|--------|--------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|-------------|----------|-----------|-----------|--------|--------|----------|
| Category |        |        |        |                 | ton              | s/yr            |               |                   |                  |             |          |           | MT        | /yr    |        |          |
| Off-Road | 0.0787 | 0.8218 | 0.7690 | 1.6300e-<br>003 |                  | 0.0351          | 0.0351        | i<br>i            | 0.0329           | 0.0329      | 0.0000   | 141.5505  | 141.5505  | 0.0384 | 0.0000 | 142.5092 |
| Paving   | 0.0108 |        |        |                 |                  | 0.0000          | 0.0000        | ]<br>             | 0.0000           | 0.0000      | 0.0000   | 0.0000    | 0.0000    | 0.0000 | 0.0000 | 0.0000   |
| Total    | 0.0895 | 0.8218 | 0.7690 | 1.6300e-<br>003 |                  | 0.0351          | 0.0351        |                   | 0.0329           | 0.0329      | 0.0000   | 141.5505  | 141.5505  | 0.0384 | 0.0000 | 142.5092 |

|          | ROG             | NOx             | СО              | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total   | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5<br>Total  | Bio- CO2 | NBio- CO2 | Total CO2 | CH4              | N2O    | CO2e   |
|----------|-----------------|-----------------|-----------------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|------------------|--------|--------|
| Category |                 |                 |                 |                 | ton              | s/yr            |                 |                   |                  |                 |          |           | MT        | <sup>-</sup> /yr |        |        |
| Hauling  | 0.0000          | 0.0000          | 0.0000          | 0.0000          | 0.0000           | 0.0000          | 0.0000          | 0.0000            | 0.0000           | 0.0000          | 0.0000   | 0.0000    | 0.0000    | 0.0000           | 0.0000 | 0.0000 |
| Vendor   | 1.3000e-<br>004 | 4.1500e-<br>003 | 9.7000e-<br>004 | 1.0000e-<br>005 | 2.5000e-<br>004  | 1.0000e-<br>005 | 2.7000e-<br>004 | 7.0000e-<br>005   | 1.0000e-<br>005  | 8.0000e-<br>005 | 0.0000   | 1.0333    | 1.0333    | 5.0000e-<br>005  | 0.0000 | 1.0347 |
| Worker   | 2.8700e-<br>003 | 2.4400e-<br>003 | 0.0227          | 6.0000e-<br>005 | 6.1300e-<br>003  | 5.0000e-<br>005 | 6.1800e-<br>003 | 1.6300e-<br>003   | 5.0000e-<br>005  | 1.6700e-<br>003 | 0.0000   | 5.3159    | 5.3159    | 1.9000e-<br>004  | 0.0000 | 5.3206 |
| Total    | 3.0000e-<br>003 | 6.5900e-<br>003 | 0.0237          | 7.0000e-<br>005 | 6.3800e-<br>003  | 6.0000e-<br>005 | 6.4500e-<br>003 | 1.7000e-<br>003   | 6.0000e-<br>005  | 1.7500e-<br>003 | 0.0000   | 6.3492    | 6.3492    | 2.4000e-<br>004  | 0.0000 | 6.3553 |

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# 3.9 Building Construction - Phase II - 2022 Unmitigated Construction On-Site

|          | ROG    | NOx    | CO     | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4    | N2O    | CO2e     |
|----------|--------|--------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|-------------|----------|-----------|-----------|--------|--------|----------|
| Category |        |        |        |                 | ton              | s/yr            |               |                   |                  |             |          |           | MT        | /yr    |        |          |
|          | 0.2818 | 2.7816 | 2.8568 | 4.8300e-<br>003 |                  | 0.1425          | 0.1425        |                   | 0.1342           | 0.1342      | 0.0000   | 420.9286  | 420.9286  | 0.0967 | 0.0000 | 423.3460 |
| Total    | 0.2818 | 2.7816 | 2.8568 | 4.8300e-<br>003 |                  | 0.1425          | 0.1425        |                   | 0.1342           | 0.1342      | 0.0000   | 420.9286  | 420.9286  | 0.0967 | 0.0000 | 423.3460 |

|          | ROG             | NOx    | CO              | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total   | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5<br>Total  | Bio- CO2 | NBio- CO2 | Total CO2 | CH4             | N2O    | CO2e    |
|----------|-----------------|--------|-----------------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|--------|---------|
| Category |                 |        |                 |                 | ton              | s/yr            |                 |                   |                  |                 |          |           | МТ        | /yr             |        |         |
| Hauling  | 0.0000          | 0.0000 | 0.0000          | 0.0000          | 0.0000           | 0.0000          | 0.0000          | 0.0000            | 0.0000           | 0.0000          | 0.0000   | 0.0000    | 0.0000    | 0.0000          | 0.0000 | 0.0000  |
| Vendor   | 3.6000e-<br>004 | 0.0113 | 2.6300e-<br>003 | 3.0000e-<br>005 | 6.9000e-<br>004  | 3.0000e-<br>005 | 7.2000e-<br>004 | 2.0000e-<br>004   | 3.0000e-<br>005  | 2.3000e-<br>004 | 0.0000   | 2.8181    | 2.8181    | 1.5000e-<br>004 | 0.0000 | 2.8218  |
| Worker   | 0.0157          | 0.0133 | 0.1239          | 3.2000e-<br>004 | 0.0334           | 2.7000e-<br>004 | 0.0337          | 8.8800e-<br>003   | 2.5000e-<br>004  | 9.1300e-<br>003 | 0.0000   | 28.9959   | 28.9959   | 1.0300e-<br>003 | 0.0000 | 29.0217 |
| Total    | 0.0160          | 0.0247 | 0.1265          | 3.5000e-<br>004 | 0.0341           | 3.0000e-<br>004 | 0.0344          | 9.0800e-<br>003   | 2.8000e-<br>004  | 9.3600e-<br>003 | 0.0000   | 31.8140   | 31.8140   | 1.1800e-<br>003 | 0.0000 | 31.8435 |

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# 3.9 Building Construction - Phase II - 2022 Mitigated Construction On-Site

|          | ROG    | NOx    | CO     | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4    | N2O    | CO2e     |
|----------|--------|--------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|-------------|----------|-----------|-----------|--------|--------|----------|
| Category |        |        |        |                 | ton              | s/yr            |               |                   |                  |             |          |           | MT        | /yr    |        |          |
|          | 0.2818 | 2.7816 | 2.8567 | 4.8300e-<br>003 |                  | 0.1425          | 0.1425        |                   | 0.1342           | 0.1342      | 0.0000   | 420.9281  | 420.9281  | 0.0967 | 0.0000 | 423.3455 |
| Total    | 0.2818 | 2.7816 | 2.8567 | 4.8300e-<br>003 |                  | 0.1425          | 0.1425        |                   | 0.1342           | 0.1342      | 0.0000   | 420.9281  | 420.9281  | 0.0967 | 0.0000 | 423.3455 |

|          | ROG             | NOx    | СО              | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total   | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total     | Bio- CO2 | NBio- CO2 | Total CO2 | CH4             | N2O    | CO2e    |
|----------|-----------------|--------|-----------------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|--------|---------|
| Category |                 |        |                 |                 | ton              | s/yr            |                 |                   |                  |                 |          |           | MT        | /yr             |        |         |
| Hauling  | 0.0000          | 0.0000 | 0.0000          | 0.0000          | 0.0000           | 0.0000          | 0.0000          | 0.0000            | 0.0000           | 0.0000          | 0.0000   | 0.0000    | 0.0000    | 0.0000          | 0.0000 | 0.0000  |
| Vendor   | 3.6000e-<br>004 | 0.0113 | 2.6300e-<br>003 | 3.0000e-<br>005 | 6.9000e-<br>004  | 3.0000e-<br>005 | 7.2000e-<br>004 | 2.0000e-<br>004   | 3.0000e-<br>005  | 2.3000e-<br>004 | 0.0000   | 2.8181    | 2.8181    | 1.5000e-<br>004 | 0.0000 | 2.8218  |
| Worker   | 0.0157          | 0.0133 | 0.1239          | 3.2000e-<br>004 | 0.0334           | 2.7000e-<br>004 | 0.0337          | 8.8800e-<br>003   | 2.5000e-<br>004  | 9.1300e-<br>003 | 0.0000   | 28.9959   | 28.9959   | 1.0300e-<br>003 | 0.0000 | 29.0217 |
| Total    | 0.0160          | 0.0247 | 0.1265          | 3.5000e-<br>004 | 0.0341           | 3.0000e-<br>004 | 0.0344          | 9.0800e-<br>003   | 2.8000e-<br>004  | 9.3600e-<br>003 | 0.0000   | 31.8140   | 31.8140   | 1.1800e-<br>003 | 0.0000 | 31.8435 |

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# 3.10 Architectural Coating - Phase II - 2022 <u>Unmitigated Construction On-Site</u>

|          | ROG             | NOx    | CO     | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total   | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total     | Bio- CO2 | NBio- CO2 | Total CO2 | CH4             | N2O    | CO2e    |
|----------|-----------------|--------|--------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|--------|---------|
| Category |                 |        |        |                 | ton              | s/yr            |                 |                   |                  |                 |          |           | МТ        | /yr             |        |         |
| 7        | 0.2775          |        |        |                 |                  | 0.0000          | 0.0000          |                   | 0.0000           | 0.0000          | 0.0000   | 0.0000    | 0.0000    | 0.0000          | 0.0000 | 0.0000  |
| 1        | 8.0800e-<br>003 | 0.0556 | 0.0716 | 1.2000e-<br>004 |                  | 3.2300e-<br>003 | 3.2300e-<br>003 |                   | 3.2300e-<br>003  | 3.2300e-<br>003 | 0.0000   | 10.0854   | 10.0854   | 6.6000e-<br>004 | 0.0000 | 10.1018 |
| Total    | 0.2856          | 0.0556 | 0.0716 | 1.2000e-<br>004 |                  | 3.2300e-<br>003 | 3.2300e-<br>003 |                   | 3.2300e-<br>003  | 3.2300e-<br>003 | 0.0000   | 10.0854   | 10.0854   | 6.6000e-<br>004 | 0.0000 | 10.1018 |

|          | ROG             | NOx             | СО              | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total   | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total     | Bio- CO2 | NBio- CO2 | Total CO2 | CH4             | N2O    | CO2e    |
|----------|-----------------|-----------------|-----------------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|--------|---------|
| Category |                 |                 |                 |                 | ton              | s/yr            |                 |                   |                  |                 |          |           | МТ        | /yr             |        |         |
| Hauling  | 0.0000          | 0.0000          | 0.0000          | 0.0000          | 0.0000           | 0.0000          | 0.0000          | 0.0000            | 0.0000           | 0.0000          | 0.0000   | 0.0000    | 0.0000    | 0.0000          | 0.0000 | 0.0000  |
| Vendor   | 1.3000e-<br>004 | 4.2600e-<br>003 | 9.9000e-<br>004 | 1.0000e-<br>005 | 2.6000e-<br>004  | 1.0000e-<br>005 | 2.7000e-<br>004 | 8.0000e-<br>005   | 1.0000e-<br>005  | 9.0000e-<br>005 | 0.0000   | 1.0602    | 1.0602    | 5.0000e-<br>005 | 0.0000 | 1.0615  |
| Worker   | 5.8900e-<br>003 | 5.0100e-<br>003 | 0.0466          | 1.2000e-<br>004 | 0.0126           | 1.0000e-<br>004 | 0.0127          | 3.3400e-<br>003   | 9.0000e-<br>005  | 3.4400e-<br>003 | 0.0000   | 10.9080   | 10.9080   | 3.9000e-<br>004 | 0.0000 | 10.9177 |
| Total    | 6.0200e-<br>003 | 9.2700e-<br>003 | 0.0476          | 1.3000e-<br>004 | 0.0128           | 1.1000e-<br>004 | 0.0129          | 3.4200e-<br>003   | 1.0000e-<br>004  | 3.5300e-<br>003 | 0.0000   | 11.9681   | 11.9681   | 4.4000e-<br>004 | 0.0000 | 11.9792 |

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# 3.10 Architectural Coating - Phase II - 2022 Mitigated Construction On-Site

|                 | ROG             | NOx    | CO     | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total   | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total     | Bio- CO2 | NBio- CO2 | Total CO2 | CH4             | N2O    | CO2e    |
|-----------------|-----------------|--------|--------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|--------|---------|
| Category        |                 |        |        |                 | ton              | s/yr            |                 |                   |                  |                 |          |           | MT        | /yr             |        |         |
| Archit. Coating | 0.2775          |        |        |                 |                  | 0.0000          | 0.0000          |                   | 0.0000           | 0.0000          | 0.0000   | 0.0000    | 0.0000    | 0.0000          | 0.0000 | 0.0000  |
| Off-Road        | 8.0800e-<br>003 | 0.0556 | 0.0716 | 1.2000e-<br>004 |                  | 3.2300e-<br>003 | 3.2300e-<br>003 | <br>              | 3.2300e-<br>003  | 3.2300e-<br>003 | 0.0000   | 10.0853   | 10.0853   | 6.6000e-<br>004 | 0.0000 | 10.1018 |
| Total           | 0.2856          | 0.0556 | 0.0716 | 1.2000e-<br>004 |                  | 3.2300e-<br>003 | 3.2300e-<br>003 |                   | 3.2300e-<br>003  | 3.2300e-<br>003 | 0.0000   | 10.0853   | 10.0853   | 6.6000e-<br>004 | 0.0000 | 10.1018 |

|          | ROG             | NOx             | CO              | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total   | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5<br>Total  | Bio- CO2 | NBio- CO2 | Total CO2 | CH4             | N2O    | CO2e    |
|----------|-----------------|-----------------|-----------------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|--------|---------|
| Category |                 |                 |                 |                 | ton              | s/yr            |                 |                   |                  |                 |          |           | MT        | /yr             |        |         |
| Hauling  | 0.0000          | 0.0000          | 0.0000          | 0.0000          | 0.0000           | 0.0000          | 0.0000          | 0.0000            | 0.0000           | 0.0000          | 0.0000   | 0.0000    | 0.0000    | 0.0000          | 0.0000 | 0.0000  |
| Vendor   | 1.3000e-<br>004 | 4.2600e-<br>003 | 9.9000e-<br>004 | 1.0000e-<br>005 | 2.6000e-<br>004  | 1.0000e-<br>005 | 2.7000e-<br>004 | 8.0000e-<br>005   | 1.0000e-<br>005  | 9.0000e-<br>005 | 0.0000   | 1.0602    | 1.0602    | 5.0000e-<br>005 | 0.0000 | 1.0615  |
| Worker   | 5.8900e-<br>003 | 5.0100e-<br>003 | 0.0466          | 1.2000e-<br>004 | 0.0126           | 1.0000e-<br>004 | 0.0127          | 3.3400e-<br>003   | 9.0000e-<br>005  | 3.4400e-<br>003 | 0.0000   | 10.9080   | 10.9080   | 3.9000e-<br>004 | 0.0000 | 10.9177 |
| Total    | 6.0200e-<br>003 | 9.2700e-<br>003 | 0.0476          | 1.3000e-<br>004 | 0.0128           | 1.1000e-<br>004 | 0.0129          | 3.4200e-<br>003   | 1.0000e-<br>004  | 3.5300e-<br>003 | 0.0000   | 11.9681   | 11.9681   | 4.4000e-<br>004 | 0.0000 | 11.9792 |

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3.11 Paving - Phase III - 2022 Unmitigated Construction On-Site

|             | ROG             | NOx    | СО          | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4    | N2O    | CO2e    |  |  |
|-------------|-----------------|--------|-------------|-----------------|------------------|-----------------|---------------|-------------------|------------------|-------------|----------|-----------|-----------|--------|--------|---------|--|--|
| Category    | tons/yr         |        |             |                 |                  |                 |               |                   |                  |             | MT/yr    |           |           |        |        |         |  |  |
| - Cir rtodd | 0.0276          | 0.2882 | 0.2697      | 5.7000e-<br>004 |                  | 0.0123          | 0.0123        |                   | 0.0116           | 0.0116      | 0.0000   | 49.6346   | 49.6346   | 0.0135 | 0.0000 | 49.9708 |  |  |
| 1           | 3.8000e-<br>003 |        | 1<br>1<br>1 |                 |                  | 0.0000          | 0.0000        | 1<br>1<br>1       | 0.0000           | 0.0000      | 0.0000   | 0.0000    | 0.0000    | 0.0000 | 0.0000 | 0.0000  |  |  |
| Total       | 0.0314          | 0.2882 | 0.2697      | 5.7000e-<br>004 |                  | 0.0123          | 0.0123        |                   | 0.0116           | 0.0116      | 0.0000   | 49.6346   | 49.6346   | 0.0135 | 0.0000 | 49.9708 |  |  |

|          | ROG             | NOx             | СО              | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total   | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total     | Bio- CO2 | NBio- CO2 | Total CO2 | CH4             | N2O    | CO2e   |  |  |  |
|----------|-----------------|-----------------|-----------------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|--------|--------|--|--|--|
| Category | tons/yr         |                 |                 |                 |                  |                 |                 |                   |                  |                 |          | MT/yr     |           |                 |        |        |  |  |  |
| Hauling  | 0.0000          | 0.0000          | 0.0000          | 0.0000          | 0.0000           | 0.0000          | 0.0000          | 0.0000            | 0.0000           | 0.0000          | 0.0000   | 0.0000    | 0.0000    | 0.0000          | 0.0000 | 0.0000 |  |  |  |
| Vendor   | 5.0000e-<br>005 | 1.4600e-<br>003 | 3.4000e-<br>004 | 0.0000          | 9.0000e-<br>005  | 0.0000          | 9.0000e-<br>005 | 3.0000e-<br>005   | 0.0000           | 3.0000e-<br>005 | 0.0000   | 0.3623    | 0.3623    | 2.0000e-<br>005 | 0.0000 | 0.3628 |  |  |  |
| Worker   | 1.0100e-<br>003 | 8.6000e-<br>004 | 7.9600e-<br>003 | 2.0000e-<br>005 | 2.1500e-<br>003  | 2.0000e-<br>005 | 2.1700e-<br>003 | 5.7000e-<br>004   | 2.0000e-<br>005  | 5.9000e-<br>004 | 0.0000   | 1.8640    | 1.8640    | 7.0000e-<br>005 | 0.0000 | 1.8657 |  |  |  |
| Total    | 1.0600e-<br>003 | 2.3200e-<br>003 | 8.3000e-<br>003 | 2.0000e-<br>005 | 2.2400e-<br>003  | 2.0000e-<br>005 | 2.2600e-<br>003 | 6.0000e-<br>004   | 2.0000e-<br>005  | 6.2000e-<br>004 | 0.0000   | 2.2264    | 2.2264    | 9.0000e-<br>005 | 0.0000 | 2.2285 |  |  |  |

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3.11 Paving - Phase III - 2022 Mitigated Construction On-Site

|             | ROG             | NOx    | СО          | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4    | N2O    | CO2e    |  |  |
|-------------|-----------------|--------|-------------|-----------------|------------------|-----------------|---------------|-------------------|------------------|-------------|----------|-----------|-----------|--------|--------|---------|--|--|
| Category    | tons/yr         |        |             |                 |                  |                 |               |                   |                  |             | MT/yr    |           |           |        |        |         |  |  |
| - Cir rtoda | 0.0276          | 0.2882 | 0.2697      | 5.7000e-<br>004 |                  | 0.0123          | 0.0123        |                   | 0.0116           | 0.0116      | 0.0000   | 49.6346   | 49.6346   | 0.0135 | 0.0000 | 49.9708 |  |  |
| 1           | 3.8000e-<br>003 |        | 1<br>1<br>1 |                 |                  | 0.0000          | 0.0000        |                   | 0.0000           | 0.0000      | 0.0000   | 0.0000    | 0.0000    | 0.0000 | 0.0000 | 0.0000  |  |  |
| Total       | 0.0314          | 0.2882 | 0.2697      | 5.7000e-<br>004 |                  | 0.0123          | 0.0123        |                   | 0.0116           | 0.0116      | 0.0000   | 49.6346   | 49.6346   | 0.0135 | 0.0000 | 49.9708 |  |  |

|          | ROG             | NOx             | СО              | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total   | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total     | Bio- CO2 | NBio- CO2 | Total CO2 | CH4             | N2O    | CO2e   |  |  |
|----------|-----------------|-----------------|-----------------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|--------|--------|--|--|
| Category | tons/yr         |                 |                 |                 |                  |                 |                 |                   |                  |                 | MT/yr    |           |           |                 |        |        |  |  |
| Hauling  | 0.0000          | 0.0000          | 0.0000          | 0.0000          | 0.0000           | 0.0000          | 0.0000          | 0.0000            | 0.0000           | 0.0000          | 0.0000   | 0.0000    | 0.0000    | 0.0000          | 0.0000 | 0.0000 |  |  |
| Vendor   | 5.0000e-<br>005 | 1.4600e-<br>003 | 3.4000e-<br>004 | 0.0000          | 9.0000e-<br>005  | 0.0000          | 9.0000e-<br>005 | 3.0000e-<br>005   | 0.0000           | 3.0000e-<br>005 | 0.0000   | 0.3623    | 0.3623    | 2.0000e-<br>005 | 0.0000 | 0.3628 |  |  |
| Worker   | 1.0100e-<br>003 | 8.6000e-<br>004 | 7.9600e-<br>003 | 2.0000e-<br>005 | 2.1500e-<br>003  | 2.0000e-<br>005 | 2.1700e-<br>003 | 5.7000e-<br>004   | 2.0000e-<br>005  | 5.9000e-<br>004 | 0.0000   | 1.8640    | 1.8640    | 7.0000e-<br>005 | 0.0000 | 1.8657 |  |  |
| Total    | 1.0600e-<br>003 | 2.3200e-<br>003 | 8.3000e-<br>003 | 2.0000e-<br>005 | 2.2400e-<br>003  | 2.0000e-<br>005 | 2.2600e-<br>003 | 6.0000e-<br>004   | 2.0000e-<br>005  | 6.2000e-<br>004 | 0.0000   | 2.2264    | 2.2264    | 9.0000e-<br>005 | 0.0000 | 2.2285 |  |  |

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# Lico Subdivision Project - Monterey Bay Unified APCD Air District, Annual

3.11 Paving - Phase III - 2023
Unmitigated Construction On-Site

|          | ROG    | NOx    | CO     | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5<br>Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4    | N2O    | CO2e     |
|----------|--------|--------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|-----------|-----------|--------|--------|----------|
| Category |        |        |        |                 | ton              | s/yr            |               |                   |                  |                |          |           | MT        | /yr    |        |          |
| Off-Road | 0.0741 | 0.7513 | 0.7675 | 1.6300e-<br>003 |                  | 0.0315          | 0.0315        |                   | 0.0295           | 0.0295         | 0.0000   | 141.5255  | 141.5255  | 0.0382 | 0.0000 | 142.4807 |
| Paving   | 0.0108 | <br>   |        |                 |                  | 0.0000          | 0.0000        |                   | 0.0000           | 0.0000         | 0.0000   | 0.0000    | 0.0000    | 0.0000 | 0.0000 | 0.0000   |
| Total    | 0.0849 | 0.7513 | 0.7675 | 1.6300e-<br>003 |                  | 0.0315          | 0.0315        |                   | 0.0295           | 0.0295         | 0.0000   | 141.5255  | 141.5255  | 0.0382 | 0.0000 | 142.4807 |

|          | ROG             | NOx             | СО              | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total   | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total     | Bio- CO2 | NBio- CO2 | Total CO2 | CH4             | N2O    | CO2e   |
|----------|-----------------|-----------------|-----------------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|--------|--------|
| Category |                 |                 |                 |                 | ton              | s/yr            |                 |                   |                  |                 |          |           | МТ        | /уг             |        |        |
| Hauling  | 0.0000          | 0.0000          | 0.0000          | 0.0000          | 0.0000           | 0.0000          | 0.0000          | 0.0000            | 0.0000           | 0.0000          | 0.0000   | 0.0000    | 0.0000    | 0.0000          | 0.0000 | 0.0000 |
| Vendor   | 1.0000e-<br>004 | 3.4200e-<br>003 | 8.2000e-<br>004 | 1.0000e-<br>005 | 2.5000e-<br>004  | 0.0000          | 2.6000e-<br>004 | 7.0000e-<br>005   | 0.0000           | 8.0000e-<br>005 | 0.0000   | 1.0150    | 1.0150    | 4.0000e-<br>005 | 0.0000 | 1.0160 |
| Worker   | 2.6700e-<br>003 | 2.1900e-<br>003 | 0.0207          | 6.0000e-<br>005 | 6.1300e-<br>003  | 5.0000e-<br>005 | 6.1700e-<br>003 | 1.6300e-<br>003   | 4.0000e-<br>005  | 1.6700e-<br>003 | 0.0000   | 5.1186    | 5.1186    | 1.7000e-<br>004 | 0.0000 | 5.1228 |
| Total    | 2.7700e-<br>003 | 5.6100e-<br>003 | 0.0215          | 7.0000e-<br>005 | 6.3800e-<br>003  | 5.0000e-<br>005 | 6.4300e-<br>003 | 1.7000e-<br>003   | 4.0000e-<br>005  | 1.7500e-<br>003 | 0.0000   | 6.1336    | 6.1336    | 2.1000e-<br>004 | 0.0000 | 6.1389 |

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3.11 Paving - Phase III - 2023 Mitigated Construction On-Site

|          | ROG    | NOx    | CO     | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4    | N2O    | CO2e     |
|----------|--------|--------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|-------------|----------|-----------|-----------|--------|--------|----------|
| Category |        |        |        |                 | ton              | s/yr            |               |                   |                  |             |          |           | MT        | /yr    |        |          |
| Off-Road | 0.0741 | 0.7513 | 0.7675 | 1.6300e-<br>003 |                  | 0.0315          | 0.0315        | 1<br>1<br>1       | 0.0295           | 0.0295      | 0.0000   | 141.5254  | 141.5254  | 0.0382 | 0.0000 | 142.4805 |
| Paving   | 0.0108 |        |        |                 |                  | 0.0000          | 0.0000        | <br>              | 0.0000           | 0.0000      | 0.0000   | 0.0000    | 0.0000    | 0.0000 | 0.0000 | 0.0000   |
| Total    | 0.0849 | 0.7513 | 0.7675 | 1.6300e-<br>003 |                  | 0.0315          | 0.0315        |                   | 0.0295           | 0.0295      | 0.0000   | 141.5254  | 141.5254  | 0.0382 | 0.0000 | 142.4805 |

|          | ROG             | NOx             | СО              | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total   | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total     | Bio- CO2 | NBio- CO2 | Total CO2 | CH4             | N2O    | CO2e   |
|----------|-----------------|-----------------|-----------------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|--------|--------|
| Category |                 |                 |                 |                 | ton              | s/yr            |                 |                   |                  |                 |          |           | МТ        | /yr             |        |        |
| Hauling  | 0.0000          | 0.0000          | 0.0000          | 0.0000          | 0.0000           | 0.0000          | 0.0000          | 0.0000            | 0.0000           | 0.0000          | 0.0000   | 0.0000    | 0.0000    | 0.0000          | 0.0000 | 0.0000 |
| Vendor   | 1.0000e-<br>004 | 3.4200e-<br>003 | 8.2000e-<br>004 | 1.0000e-<br>005 | 2.5000e-<br>004  | 0.0000          | 2.6000e-<br>004 | 7.0000e-<br>005   | 0.0000           | 8.0000e-<br>005 | 0.0000   | 1.0150    | 1.0150    | 4.0000e-<br>005 | 0.0000 | 1.0160 |
| Worker   | 2.6700e-<br>003 | 2.1900e-<br>003 | 0.0207          | 6.0000e-<br>005 | 6.1300e-<br>003  | 5.0000e-<br>005 | 6.1700e-<br>003 | 1.6300e-<br>003   | 4.0000e-<br>005  | 1.6700e-<br>003 | 0.0000   | 5.1186    | 5.1186    | 1.7000e-<br>004 | 0.0000 | 5.1228 |
| Total    | 2.7700e-<br>003 | 5.6100e-<br>003 | 0.0215          | 7.0000e-<br>005 | 6.3800e-<br>003  | 5.0000e-<br>005 | 6.4300e-<br>003 | 1.7000e-<br>003   | 4.0000e-<br>005  | 1.7500e-<br>003 | 0.0000   | 6.1336    | 6.1336    | 2.1000e-<br>004 | 0.0000 | 6.1389 |

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# 3.12 Building Construction - Phase III - 2023 <u>Unmitigated Construction On-Site</u>

|          | ROG    | NOx    | СО     | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4    | N2O    | CO2e     |
|----------|--------|--------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|-------------|----------|-----------|-----------|--------|--------|----------|
| Category |        |        |        |                 | ton              | s/yr            |               |                   |                  |             |          |           | MT        | /yr    |        |          |
|          | 0.2636 | 2.5707 | 2.8429 | 4.8300e-<br>003 |                  | 0.1272          | 0.1272        |                   | 0.1197           | 0.1197      | 0.0000   | 421.0062  | 421.0062  | 0.0961 | 0.0000 | 423.4084 |
| Total    | 0.2636 | 2.5707 | 2.8429 | 4.8300e-<br>003 |                  | 0.1272          | 0.1272        |                   | 0.1197           | 0.1197      | 0.0000   | 421.0062  | 421.0062  | 0.0961 | 0.0000 | 423.4084 |

|          | ROG             | NOx             | CO              | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total   | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total     | Bio- CO2 | NBio- CO2 | Total CO2 | CH4             | N2O    | CO2e    |
|----------|-----------------|-----------------|-----------------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|--------|---------|
| Category |                 |                 |                 |                 | ton              | s/yr            |                 |                   |                  |                 |          |           | MT        | /yr             |        |         |
| Hauling  | 0.0000          | 0.0000          | 0.0000          | 0.0000          | 0.0000           | 0.0000          | 0.0000          | 0.0000            | 0.0000           | 0.0000          | 0.0000   | 0.0000    | 0.0000    | 0.0000          | 0.0000 | 0.0000  |
| Vendor   | 2.7000e-<br>004 | 9.3200e-<br>003 | 2.2500e-<br>003 | 3.0000e-<br>005 | 6.9000e-<br>004  | 1.0000e-<br>005 | 7.1000e-<br>004 | 2.0000e-<br>004   | 1.0000e-<br>005  | 2.1000e-<br>004 | 0.0000   | 2.7681    | 2.7681    | 1.1000e-<br>004 | 0.0000 | 2.7710  |
| Worker   | 0.0146          | 0.0119          | 0.1129          | 3.1000e-<br>004 | 0.0334           | 2.6000e-<br>004 | 0.0337          | 8.8800e-<br>003   | 2.4000e-<br>004  | 9.1200e-<br>003 | 0.0000   | 27.9197   | 27.9197   | 9.2000e-<br>004 | 0.0000 | 27.9427 |
| Total    | 0.0148          | 0.0213          | 0.1152          | 3.4000e-<br>004 | 0.0341           | 2.7000e-<br>004 | 0.0344          | 9.0800e-<br>003   | 2.5000e-<br>004  | 9.3300e-<br>003 | 0.0000   | 30.6878   | 30.6878   | 1.0300e-<br>003 | 0.0000 | 30.7137 |

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# 3.12 Building Construction - Phase III - 2023 <u>Mitigated Construction On-Site</u>

|          | ROG    | NOx    | CO     | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4    | N2O    | CO2e     |
|----------|--------|--------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|-------------|----------|-----------|-----------|--------|--------|----------|
| Category |        |        |        |                 | ton              | s/yr            |               |                   |                  |             |          |           | MT        | /yr    |        |          |
| Off-Road | 0.2636 | 2.5707 | 2.8429 | 4.8300e-<br>003 |                  | 0.1272          | 0.1272        |                   | 0.1197           | 0.1197      | 0.0000   | 421.0057  | 421.0057  | 0.0961 | 0.0000 | 423.4079 |
| Total    | 0.2636 | 2.5707 | 2.8429 | 4.8300e-<br>003 |                  | 0.1272          | 0.1272        |                   | 0.1197           | 0.1197      | 0.0000   | 421.0057  | 421.0057  | 0.0961 | 0.0000 | 423.4079 |

|          | ROG             | NOx             | СО              | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total   | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total     | Bio- CO2 | NBio- CO2 | Total CO2 | CH4             | N2O    | CO2e    |
|----------|-----------------|-----------------|-----------------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|--------|---------|
| Category |                 |                 |                 |                 | ton              | s/yr            |                 |                   |                  |                 |          |           | MT        | /yr             |        |         |
| Hauling  | 0.0000          | 0.0000          | 0.0000          | 0.0000          | 0.0000           | 0.0000          | 0.0000          | 0.0000            | 0.0000           | 0.0000          | 0.0000   | 0.0000    | 0.0000    | 0.0000          | 0.0000 | 0.0000  |
| Vendor   | 2.7000e-<br>004 | 9.3200e-<br>003 | 2.2500e-<br>003 | 3.0000e-<br>005 | 6.9000e-<br>004  | 1.0000e-<br>005 | 7.1000e-<br>004 | 2.0000e-<br>004   | 1.0000e-<br>005  | 2.1000e-<br>004 | 0.0000   | 2.7681    | 2.7681    | 1.1000e-<br>004 | 0.0000 | 2.7710  |
| Worker   | 0.0146          | 0.0119          | 0.1129          | 3.1000e-<br>004 | 0.0334           | 2.6000e-<br>004 | 0.0337          | 8.8800e-<br>003   | 2.4000e-<br>004  | 9.1200e-<br>003 | 0.0000   | 27.9197   | 27.9197   | 9.2000e-<br>004 | 0.0000 | 27.9427 |
| Total    | 0.0148          | 0.0213          | 0.1152          | 3.4000e-<br>004 | 0.0341           | 2.7000e-<br>004 | 0.0344          | 9.0800e-<br>003   | 2.5000e-<br>004  | 9.3300e-<br>003 | 0.0000   | 30.6878   | 30.6878   | 1.0300e-<br>003 | 0.0000 | 30.7137 |

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# 3.13 Architectural Coating - Phase III - 2023 <u>Unmitigated Construction On-Site</u>

|                 | ROG             | NOx    | CO     | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total   | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total     | Bio- CO2 | NBio- CO2 | Total CO2 | CH4             | N2O    | CO2e    |
|-----------------|-----------------|--------|--------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|--------|---------|
| Category        |                 |        |        |                 | ton              | s/yr            |                 |                   |                  |                 |          |           | МТ        | /yr             |        |         |
| Archit. Coating | 0.2775          |        | <br>   |                 |                  | 0.0000          | 0.0000          |                   | 0.0000           | 0.0000          | 0.0000   | 0.0000    | 0.0000    | 0.0000          | 0.0000 | 0.0000  |
| 1               | 7.5700e-<br>003 | 0.0515 | 0.0715 | 1.2000e-<br>004 |                  | 2.8000e-<br>003 | 2.8000e-<br>003 |                   | 2.8000e-<br>003  | 2.8000e-<br>003 | 0.0000   | 10.0854   | 10.0854   | 6.0000e-<br>004 | 0.0000 | 10.1004 |
| Total           | 0.2851          | 0.0515 | 0.0715 | 1.2000e-<br>004 |                  | 2.8000e-<br>003 | 2.8000e-<br>003 |                   | 2.8000e-<br>003  | 2.8000e-<br>003 | 0.0000   | 10.0854   | 10.0854   | 6.0000e-<br>004 | 0.0000 | 10.1004 |

|          | ROG             | NOx             | СО              | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total   | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total     | Bio- CO2 | NBio- CO2 | Total CO2 | CH4             | N2O    | CO2e    |
|----------|-----------------|-----------------|-----------------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|--------|---------|
| Category |                 |                 |                 |                 | ton              | s/yr            |                 |                   |                  |                 |          |           | MT        | /yr             |        |         |
| Hauling  | 0.0000          | 0.0000          | 0.0000          | 0.0000          | 0.0000           | 0.0000          | 0.0000          | 0.0000            | 0.0000           | 0.0000          | 0.0000   | 0.0000    | 0.0000    | 0.0000          | 0.0000 | 0.0000  |
| Vendor   | 1.0000e-<br>004 | 3.5100e-<br>003 | 8.5000e-<br>004 | 1.0000e-<br>005 | 2.6000e-<br>004  | 1.0000e-<br>005 | 2.7000e-<br>004 | 8.0000e-<br>005   | 0.0000           | 8.0000e-<br>005 | 0.0000   | 1.0414    | 1.0414    | 4.0000e-<br>005 | 0.0000 | 1.0424  |
| Worker   | 5.4800e-<br>003 | 4.4900e-<br>003 | 0.0425          | 1.2000e-<br>004 | 0.0126           | 1.0000e-<br>004 | 0.0127          | 3.3400e-<br>003   | 9.0000e-<br>005  | 3.4300e-<br>003 | 0.0000   | 10.5031   | 10.5031   | 3.5000e-<br>004 | 0.0000 | 10.5118 |
| Total    | 5.5800e-<br>003 | 8.0000e-<br>003 | 0.0433          | 1.3000e-<br>004 | 0.0128           | 1.1000e-<br>004 | 0.0129          | 3.4200e-<br>003   | 9.0000e-<br>005  | 3.5100e-<br>003 | 0.0000   | 11.5445   | 11.5445   | 3.9000e-<br>004 | 0.0000 | 11.5542 |

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# 3.13 Architectural Coating - Phase III - 2023 Mitigated Construction On-Site

|                 | ROG             | NOx    | CO     | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total   | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total     | Bio- CO2 | NBio- CO2 | Total CO2 | CH4             | N2O    | CO2e    |
|-----------------|-----------------|--------|--------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|--------|---------|
| Category        |                 |        |        |                 | ton              | s/yr            |                 |                   |                  |                 |          |           | МТ        | /yr             |        |         |
| Archit. Coating | 0.2775          |        |        |                 |                  | 0.0000          | 0.0000          |                   | 0.0000           | 0.0000          | 0.0000   | 0.0000    | 0.0000    | 0.0000          | 0.0000 | 0.0000  |
| 1               | 7.5700e-<br>003 | 0.0515 | 0.0715 | 1.2000e-<br>004 |                  | 2.8000e-<br>003 | 2.8000e-<br>003 |                   | 2.8000e-<br>003  | 2.8000e-<br>003 | 0.0000   | 10.0853   | 10.0853   | 6.0000e-<br>004 | 0.0000 | 10.1004 |
| Total           | 0.2851          | 0.0515 | 0.0715 | 1.2000e-<br>004 |                  | 2.8000e-<br>003 | 2.8000e-<br>003 |                   | 2.8000e-<br>003  | 2.8000e-<br>003 | 0.0000   | 10.0853   | 10.0853   | 6.0000e-<br>004 | 0.0000 | 10.1004 |

|          | ROG             | NOx             | СО              | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total   | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total     | Bio- CO2 | NBio- CO2 | Total CO2 | CH4             | N2O    | CO2e    |
|----------|-----------------|-----------------|-----------------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|--------|---------|
| Category |                 |                 |                 |                 | ton              | s/yr            |                 |                   |                  |                 |          |           | МТ        | /yr             |        |         |
| Hauling  | 0.0000          | 0.0000          | 0.0000          | 0.0000          | 0.0000           | 0.0000          | 0.0000          | 0.0000            | 0.0000           | 0.0000          | 0.0000   | 0.0000    | 0.0000    | 0.0000          | 0.0000 | 0.0000  |
| Vendor   | 1.0000e-<br>004 | 3.5100e-<br>003 | 8.5000e-<br>004 | 1.0000e-<br>005 | 2.6000e-<br>004  | 1.0000e-<br>005 | 2.7000e-<br>004 | 8.0000e-<br>005   | 0.0000           | 8.0000e-<br>005 | 0.0000   | 1.0414    | 1.0414    | 4.0000e-<br>005 | 0.0000 | 1.0424  |
| Worker   | 5.4800e-<br>003 | 4.4900e-<br>003 | 0.0425          | 1.2000e-<br>004 | 0.0126           | 1.0000e-<br>004 | 0.0127          | 3.3400e-<br>003   | 9.0000e-<br>005  | 3.4300e-<br>003 | 0.0000   | 10.5031   | 10.5031   | 3.5000e-<br>004 | 0.0000 | 10.5118 |
| Total    | 5.5800e-<br>003 | 8.0000e-<br>003 | 0.0433          | 1.3000e-<br>004 | 0.0128           | 1.1000e-<br>004 | 0.0129          | 3.4200e-<br>003   | 9.0000e-<br>005  | 3.5100e-<br>003 | 0.0000   | 11.5445   | 11.5445   | 3.9000e-<br>004 | 0.0000 | 11.5542 |

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3.14 Paving - Phase IV - 2023 Unmitigated Construction On-Site

|          | ROG             | NOx    | CO     | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total     | Bio- CO2 | NBio- CO2 | Total CO2 | CH4    | N2O    | CO2e    |
|----------|-----------------|--------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|-----------------|----------|-----------|-----------|--------|--------|---------|
| Category |                 |        |        |                 | ton              | s/yr            |               |                   |                  |                 |          |           | MT        | /yr    |        |         |
| Off-Road | 0.0250          | 0.2537 | 0.2591 | 5.5000e-<br>004 |                  | 0.0106          | 0.0106        |                   | 9.9700e-<br>003  | 9.9700e-<br>003 | 0.0000   | 47.7878   | 47.7878   | 0.0129 | 0.0000 | 48.1104 |
| Paving   | 3.6600e-<br>003 |        |        |                 |                  | 0.0000          | 0.0000        |                   | 0.0000           | 0.0000          | 0.0000   | 0.0000    | 0.0000    | 0.0000 | 0.0000 | 0.0000  |
| Total    | 0.0287          | 0.2537 | 0.2591 | 5.5000e-<br>004 |                  | 0.0106          | 0.0106        |                   | 9.9700e-<br>003  | 9.9700e-<br>003 | 0.0000   | 47.7878   | 47.7878   | 0.0129 | 0.0000 | 48.1104 |

|          | ROG             | NOx             | СО              | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total   | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5<br>Total  | Bio- CO2 | NBio- CO2 | Total CO2 | CH4             | N2O    | CO2e   |
|----------|-----------------|-----------------|-----------------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|--------|--------|
| Category |                 |                 |                 |                 | ton              | s/yr            |                 |                   |                  |                 |          | MT        | /yr       |                 |        |        |
| Hauling  | 0.0000          | 0.0000          | 0.0000          | 0.0000          | 0.0000           | 0.0000          | 0.0000          | 0.0000            | 0.0000           | 0.0000          | 0.0000   | 0.0000    | 0.0000    | 0.0000          | 0.0000 | 0.0000 |
| Vendor   | 3.0000e-<br>005 | 1.1500e-<br>003 | 2.8000e-<br>004 | 0.0000          | 9.0000e-<br>005  | 0.0000          | 9.0000e-<br>005 | 2.0000e-<br>005   | 0.0000           | 3.0000e-<br>005 | 0.0000   | 0.3427    | 0.3427    | 1.0000e-<br>005 | 0.0000 | 0.3431 |
| Worker   | 9.0000e-<br>004 | 7.4000e-<br>004 | 6.9900e-<br>003 | 2.0000e-<br>005 | 2.0700e-<br>003  | 2.0000e-<br>005 | 2.0800e-<br>003 | 5.5000e-<br>004   | 1.0000e-<br>005  | 5.6000e-<br>004 | 0.0000   | 1.7284    | 1.7284    | 6.0000e-<br>005 | 0.0000 | 1.7298 |
| Total    | 9.3000e-<br>004 | 1.8900e-<br>003 | 7.2700e-<br>003 | 2.0000e-<br>005 | 2.1600e-<br>003  | 2.0000e-<br>005 | 2.1700e-<br>003 | 5.7000e-<br>004   | 1.0000e-<br>005  | 5.9000e-<br>004 | 0.0000   | 2.0711    | 2.0711    | 7.0000e-<br>005 | 0.0000 | 2.0729 |

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3.14 Paving - Phase IV - 2023 Mitigated Construction On-Site

|          | ROG             | NOx    | СО     | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total     | Bio- CO2 | NBio- CO2 | Total CO2 | CH4    | N2O    | CO2e    |
|----------|-----------------|--------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|-----------------|----------|-----------|-----------|--------|--------|---------|
| Category |                 |        |        |                 | ton              | s/yr            |               |                   |                  |                 |          |           | MT        | /yr    |        |         |
| Off-Road | 0.0250          | 0.2537 | 0.2591 | 5.5000e-<br>004 |                  | 0.0106          | 0.0106        |                   | 9.9700e-<br>003  | 9.9700e-<br>003 | 0.0000   | 47.7878   | 47.7878   | 0.0129 | 0.0000 | 48.1103 |
| Paving   | 3.6600e-<br>003 |        |        |                 |                  | 0.0000          | 0.0000        |                   | 0.0000           | 0.0000          | 0.0000   | 0.0000    | 0.0000    | 0.0000 | 0.0000 | 0.0000  |
| Total    | 0.0287          | 0.2537 | 0.2591 | 5.5000e-<br>004 |                  | 0.0106          | 0.0106        |                   | 9.9700e-<br>003  | 9.9700e-<br>003 | 0.0000   | 47.7878   | 47.7878   | 0.0129 | 0.0000 | 48.1103 |

|          | ROG             | NOx             | СО              | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total   | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5<br>Total  | Bio- CO2 | NBio- CO2 | Total CO2 | CH4             | N2O    | CO2e   |
|----------|-----------------|-----------------|-----------------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|--------|--------|
| Category |                 |                 |                 |                 | ton              | s/yr            |                 |                   |                  |                 |          |           | MT        | /yr             |        |        |
| Hauling  | 0.0000          | 0.0000          | 0.0000          | 0.0000          | 0.0000           | 0.0000          | 0.0000          | 0.0000            | 0.0000           | 0.0000          | 0.0000   | 0.0000    | 0.0000    | 0.0000          | 0.0000 | 0.0000 |
| Vendor   | 3.0000e-<br>005 | 1.1500e-<br>003 | 2.8000e-<br>004 | 0.0000          | 9.0000e-<br>005  | 0.0000          | 9.0000e-<br>005 | 2.0000e-<br>005   | 0.0000           | 3.0000e-<br>005 | 0.0000   | 0.3427    | 0.3427    | 1.0000e-<br>005 | 0.0000 | 0.3431 |
| Worker   | 9.0000e-<br>004 | 7.4000e-<br>004 | 6.9900e-<br>003 | 2.0000e-<br>005 | 2.0700e-<br>003  | 2.0000e-<br>005 | 2.0800e-<br>003 | 5.5000e-<br>004   | 1.0000e-<br>005  | 5.6000e-<br>004 | 0.0000   | 1.7284    | 1.7284    | 6.0000e-<br>005 | 0.0000 | 1.7298 |
| Total    | 9.3000e-<br>004 | 1.8900e-<br>003 | 7.2700e-<br>003 | 2.0000e-<br>005 | 2.1600e-<br>003  | 2.0000e-<br>005 | 2.1700e-<br>003 | 5.7000e-<br>004   | 1.0000e-<br>005  | 5.9000e-<br>004 | 0.0000   | 2.0711    | 2.0711    | 7.0000e-<br>005 | 0.0000 | 2.0729 |

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3.14 Paving - Phase IV - 2024 Unmitigated Construction On-Site

|          | ROG    | NOx    | CO     | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5<br>Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4    | N2O    | CO2e     |
|----------|--------|--------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|-----------|-----------|--------|--------|----------|
| Category |        |        |        |                 | ton              | s/yr            |               |                   |                  |                |          |           | MT        | /yr    |        |          |
| Off-Road | 0.0715 | 0.7105 | 0.7766 | 1.6500e-<br>003 |                  | 0.0292          | 0.0292        |                   | 0.0273           | 0.0273         | 0.0000   | 143.3433  | 143.3433  | 0.0387 | 0.0000 | 144.3096 |
| Paving   | 0.0110 |        | i<br>i |                 |                  | 0.0000          | 0.0000        |                   | 0.0000           | 0.0000         | 0.0000   | 0.0000    | 0.0000    | 0.0000 | 0.0000 | 0.0000   |
| Total    | 0.0825 | 0.7105 | 0.7766 | 1.6500e-<br>003 |                  | 0.0292          | 0.0292        |                   | 0.0273           | 0.0273         | 0.0000   | 143.3433  | 143.3433  | 0.0387 | 0.0000 | 144.3096 |

|          | ROG             | NOx             | СО              | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total   | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5<br>Total  | Bio- CO2 | NBio- CO2 | Total CO2 | CH4             | N2O    | CO2e   |
|----------|-----------------|-----------------|-----------------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|--------|--------|
| Category |                 |                 |                 |                 | ton              | s/yr            |                 |                   |                  |                 |          |           | МТ        | /уг             |        |        |
| Hauling  | 0.0000          | 0.0000          | 0.0000          | 0.0000          | 0.0000           | 0.0000          | 0.0000          | 0.0000            | 0.0000           | 0.0000          | 0.0000   | 0.0000    | 0.0000    | 0.0000          | 0.0000 | 0.0000 |
| Vendor   | 9.0000e-<br>005 | 3.3800e-<br>003 | 7.7000e-<br>004 | 1.0000e-<br>005 | 2.6000e-<br>004  | 0.0000          | 2.6000e-<br>004 | 7.0000e-<br>005   | 0.0000           | 8.0000e-<br>005 | 0.0000   | 1.0198    | 1.0198    | 4.0000e-<br>005 | 0.0000 | 1.0208 |
| Worker   | 2.5300e-<br>003 | 1.9900e-<br>003 | 0.0192          | 6.0000e-<br>005 | 6.2100e-<br>003  | 5.0000e-<br>005 | 6.2500e-<br>003 | 1.6500e-<br>003   | 4.0000e-<br>005  | 1.6900e-<br>003 | 0.0000   | 4.9852    | 4.9852    | 1.5000e-<br>004 | 0.0000 | 4.9890 |
| Total    | 2.6200e-<br>003 | 5.3700e-<br>003 | 0.0200          | 7.0000e-<br>005 | 6.4700e-<br>003  | 5.0000e-<br>005 | 6.5100e-<br>003 | 1.7200e-<br>003   | 4.0000e-<br>005  | 1.7700e-<br>003 | 0.0000   | 6.0050    | 6.0050    | 1.9000e-<br>004 | 0.0000 | 6.0098 |

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3.14 Paving - Phase IV - 2024 Mitigated Construction On-Site

|          | ROG    | NOx    | CO          | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4    | N2O    | CO2e     |
|----------|--------|--------|-------------|-----------------|------------------|-----------------|---------------|-------------------|------------------|-------------|----------|-----------|-----------|--------|--------|----------|
| Category |        |        |             |                 | ton              | s/yr            |               |                   |                  |             |          |           | MT        | /yr    |        |          |
| Off-Road | 0.0715 | 0.7105 | 0.7766      | 1.6500e-<br>003 |                  | 0.0292          | 0.0292        |                   | 0.0273           | 0.0273      | 0.0000   | 143.3432  | 143.3432  | 0.0387 | 0.0000 | 144.3094 |
| Paving   | 0.0110 |        | 1<br>1<br>1 |                 |                  | 0.0000          | 0.0000        |                   | 0.0000           | 0.0000      | 0.0000   | 0.0000    | 0.0000    | 0.0000 | 0.0000 | 0.0000   |
| Total    | 0.0825 | 0.7105 | 0.7766      | 1.6500e-<br>003 |                  | 0.0292          | 0.0292        |                   | 0.0273           | 0.0273      | 0.0000   | 143.3432  | 143.3432  | 0.0387 | 0.0000 | 144.3094 |

|          | ROG             | NOx             | СО              | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total   | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total     | Bio- CO2 | NBio- CO2 | Total CO2 | CH4             | N2O    | CO2e   |
|----------|-----------------|-----------------|-----------------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|--------|--------|
| Category |                 |                 |                 |                 | ton              | s/yr            |                 |                   |                  |                 |          |           | MT        | /yr             |        |        |
| Hauling  | 0.0000          | 0.0000          | 0.0000          | 0.0000          | 0.0000           | 0.0000          | 0.0000          | 0.0000            | 0.0000           | 0.0000          | 0.0000   | 0.0000    | 0.0000    | 0.0000          | 0.0000 | 0.0000 |
| Vendor   | 9.0000e-<br>005 | 3.3800e-<br>003 | 7.7000e-<br>004 | 1.0000e-<br>005 | 2.6000e-<br>004  | 0.0000          | 2.6000e-<br>004 | 7.0000e-<br>005   | 0.0000           | 8.0000e-<br>005 | 0.0000   | 1.0198    | 1.0198    | 4.0000e-<br>005 | 0.0000 | 1.0208 |
| Worker   | 2.5300e-<br>003 | 1.9900e-<br>003 | 0.0192          | 6.0000e-<br>005 | 6.2100e-<br>003  | 5.0000e-<br>005 | 6.2500e-<br>003 | 1.6500e-<br>003   | 4.0000e-<br>005  | 1.6900e-<br>003 | 0.0000   | 4.9852    | 4.9852    | 1.5000e-<br>004 | 0.0000 | 4.9890 |
| Total    | 2.6200e-<br>003 | 5.3700e-<br>003 | 0.0200          | 7.0000e-<br>005 | 6.4700e-<br>003  | 5.0000e-<br>005 | 6.5100e-<br>003 | 1.7200e-<br>003   | 4.0000e-<br>005  | 1.7700e-<br>003 | 0.0000   | 6.0050    | 6.0050    | 1.9000e-<br>004 | 0.0000 | 6.0098 |

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# 3.15 Building Construction - Phase IV - 2024 <u>Unmitigated Construction On-Site</u>

|          | ROG    | NOx    | CO     | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4    | N2O    | CO2e     |
|----------|--------|--------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|-------------|----------|-----------|-----------|--------|--------|----------|
| Category |        |        |        |                 | ton              | s/yr            |               |                   |                  |             |          |           | MT        | /yr    |        |          |
| Off-Road | 0.2507 | 2.4227 | 2.8354 | 4.8300e-<br>003 |                  | 0.1162          | 0.1162        |                   | 0.1093           | 0.1093      | 0.0000   | 421.0222  | 421.0222  | 0.0957 | 0.0000 | 423.4149 |
| Total    | 0.2507 | 2.4227 | 2.8354 | 4.8300e-<br>003 |                  | 0.1162          | 0.1162        |                   | 0.1093           | 0.1093      | 0.0000   | 421.0222  | 421.0222  | 0.0957 | 0.0000 | 423.4149 |

|          | ROG             | NOx             | СО              | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total   | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total     | Bio- CO2 | NBio- CO2 | Total CO2 | CH4             | N2O    | CO2e    |
|----------|-----------------|-----------------|-----------------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|--------|---------|
| Category |                 |                 |                 |                 | ton              | s/yr            |                 |                   |                  |                 |          |           | MT        | /yr             |        |         |
| Hauling  | 0.0000          | 0.0000          | 0.0000          | 0.0000          | 0.0000           | 0.0000          | 0.0000          | 0.0000            | 0.0000           | 0.0000          | 0.0000   | 0.0000    | 0.0000    | 0.0000          | 0.0000 | 0.0000  |
| Vendor   | 2.5000e-<br>004 | 9.1100e-<br>003 | 2.0800e-<br>003 | 3.0000e-<br>005 | 6.9000e-<br>004  | 1.0000e-<br>005 | 7.1000e-<br>004 | 2.0000e-<br>004   | 1.0000e-<br>005  | 2.1000e-<br>004 | 0.0000   | 2.7456    | 2.7456    | 1.1000e-<br>004 | 0.0000 | 2.7484  |
| Worker   | 0.0136          | 0.0107          | 0.1036          | 3.0000e-<br>004 | 0.0334           | 2.5000e-<br>004 | 0.0337          | 8.8800e-<br>003   | 2.3000e-<br>004  | 9.1200e-<br>003 | 0.0000   | 26.8433   | 26.8433   | 8.2000e-<br>004 | 0.0000 | 26.8640 |
| Total    | 0.0139          | 0.0198          | 0.1057          | 3.3000e-<br>004 | 0.0341           | 2.6000e-<br>004 | 0.0344          | 9.0800e-<br>003   | 2.4000e-<br>004  | 9.3300e-<br>003 | 0.0000   | 29.5889   | 29.5889   | 9.3000e-<br>004 | 0.0000 | 29.6123 |

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# 3.15 Building Construction - Phase IV - 2024 <u>Mitigated Construction On-Site</u>

|          | ROG    | NOx    | CO     | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4    | N2O    | CO2e     |
|----------|--------|--------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|-------------|----------|-----------|-----------|--------|--------|----------|
| Category |        |        |        |                 | ton              | s/yr            |               |                   |                  |             |          |           | MT        | /yr    |        |          |
| Off-Road | 0.2507 | 2.4227 | 2.8354 | 4.8300e-<br>003 |                  | 0.1162          | 0.1162        |                   | 0.1093           | 0.1093      | 0.0000   | 421.0217  | 421.0217  | 0.0957 | 0.0000 | 423.4144 |
| Total    | 0.2507 | 2.4227 | 2.8354 | 4.8300e-<br>003 |                  | 0.1162          | 0.1162        |                   | 0.1093           | 0.1093      | 0.0000   | 421.0217  | 421.0217  | 0.0957 | 0.0000 | 423.4144 |

|          | ROG             | NOx             | CO              | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total   | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total     | Bio- CO2 | NBio- CO2 | Total CO2 | CH4             | N2O    | CO2e    |
|----------|-----------------|-----------------|-----------------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|--------|---------|
| Category |                 |                 |                 |                 | ton              | s/yr            |                 |                   |                  |                 |          |           | MT        | /yr             |        |         |
| Hauling  | 0.0000          | 0.0000          | 0.0000          | 0.0000          | 0.0000           | 0.0000          | 0.0000          | 0.0000            | 0.0000           | 0.0000          | 0.0000   | 0.0000    | 0.0000    | 0.0000          | 0.0000 | 0.0000  |
| Vendor   | 2.5000e-<br>004 | 9.1100e-<br>003 | 2.0800e-<br>003 | 3.0000e-<br>005 | 6.9000e-<br>004  | 1.0000e-<br>005 | 7.1000e-<br>004 | 2.0000e-<br>004   | 1.0000e-<br>005  | 2.1000e-<br>004 | 0.0000   | 2.7456    | 2.7456    | 1.1000e-<br>004 | 0.0000 | 2.7484  |
| Worker   | 0.0136          | 0.0107          | 0.1036          | 3.0000e-<br>004 | 0.0334           | 2.5000e-<br>004 | 0.0337          | 8.8800e-<br>003   | 2.3000e-<br>004  | 9.1200e-<br>003 | 0.0000   | 26.8433   | 26.8433   | 8.2000e-<br>004 | 0.0000 | 26.8640 |
| Total    | 0.0139          | 0.0198          | 0.1057          | 3.3000e-<br>004 | 0.0341           | 2.6000e-<br>004 | 0.0344          | 9.0800e-<br>003   | 2.4000e-<br>004  | 9.3300e-<br>003 | 0.0000   | 29.5889   | 29.5889   | 9.3000e-<br>004 | 0.0000 | 29.6123 |

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# 3.16 Architectural Coating - Phase IV - 2024 <u>Unmitigated Construction On-Site</u>

|                 | ROG             | NOx    | СО     | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total   | Fugitive<br>PM2.5   | Exhaust<br>PM2.5 | PM2.5 Total     | Bio- CO2 | NBio- CO2 | Total CO2 | CH4             | N2O    | CO2e    |
|-----------------|-----------------|--------|--------|-----------------|------------------|-----------------|-----------------|---------------------|------------------|-----------------|----------|-----------|-----------|-----------------|--------|---------|
| Category        |                 |        |        |                 | ton              | s/yr            |                 |                     |                  |                 |          |           | МТ        | /yr             |        |         |
| Archit. Coating | 0.2775          |        |        |                 |                  | 0.0000          | 0.0000          |                     | 0.0000           | 0.0000          | 0.0000   | 0.0000    | 0.0000    | 0.0000          | 0.0000 | 0.0000  |
| 1               | 7.1400e-<br>003 | 0.0481 | 0.0715 | 1.2000e-<br>004 |                  | 2.4100e-<br>003 | 2.4100e-<br>003 | <br> <br> <br> <br> | 2.4100e-<br>003  | 2.4100e-<br>003 | 0.0000   | 10.0854   | 10.0854   | 5.7000e-<br>004 | 0.0000 | 10.0996 |
| Total           | 0.2847          | 0.0481 | 0.0715 | 1.2000e-<br>004 |                  | 2.4100e-<br>003 | 2.4100e-<br>003 |                     | 2.4100e-<br>003  | 2.4100e-<br>003 | 0.0000   | 10.0854   | 10.0854   | 5.7000e-<br>004 | 0.0000 | 10.0996 |

|          | ROG             | NOx             | СО              | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total   | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total     | Bio- CO2 | NBio- CO2 | Total CO2 | CH4             | N2O    | CO2e    |
|----------|-----------------|-----------------|-----------------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|--------|---------|
| Category |                 |                 |                 |                 | ton              | s/yr            |                 |                   |                  |                 |          |           | MT        | /yr             |        |         |
| Hauling  | 0.0000          | 0.0000          | 0.0000          | 0.0000          | 0.0000           | 0.0000          | 0.0000          | 0.0000            | 0.0000           | 0.0000          | 0.0000   | 0.0000    | 0.0000    | 0.0000          | 0.0000 | 0.0000  |
| Vendor   | 1.0000e-<br>004 | 3.4300e-<br>003 | 7.8000e-<br>004 | 1.0000e-<br>005 | 2.6000e-<br>004  | 0.0000          | 2.7000e-<br>004 | 8.0000e-<br>005   | 0.0000           | 8.0000e-<br>005 | 0.0000   | 1.0329    | 1.0329    | 4.0000e-<br>005 | 0.0000 | 1.0339  |
| Worker   | 5.1200e-<br>003 | 4.0300e-<br>003 | 0.0390          | 1.1000e-<br>004 | 0.0126           | 1.0000e-<br>004 | 0.0127          | 3.3400e-<br>003   | 9.0000e-<br>005  | 3.4300e-<br>003 | 0.0000   | 10.0982   | 10.0982   | 3.1000e-<br>004 | 0.0000 | 10.1060 |
| Total    | 5.2200e-<br>003 | 7.4600e-<br>003 | 0.0398          | 1.2000e-<br>004 | 0.0128           | 1.0000e-<br>004 | 0.0129          | 3.4200e-<br>003   | 9.0000e-<br>005  | 3.5100e-<br>003 | 0.0000   | 11.1311   | 11.1311   | 3.5000e-<br>004 | 0.0000 | 11.1399 |

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# 3.16 Architectural Coating - Phase IV - 2024 Mitigated Construction On-Site

|                 | ROG             | NOx    | CO     | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total   | Fugitive<br>PM2.5   | Exhaust<br>PM2.5 | PM2.5 Total     | Bio- CO2 | NBio- CO2 | Total CO2 | CH4             | N2O    | CO2e    |
|-----------------|-----------------|--------|--------|-----------------|------------------|-----------------|-----------------|---------------------|------------------|-----------------|----------|-----------|-----------|-----------------|--------|---------|
| Category        |                 |        |        |                 | ton              | s/yr            |                 |                     |                  |                 |          |           | МТ        | /yr             |        |         |
| Archit. Coating | 0.2775          |        |        |                 |                  | 0.0000          | 0.0000          |                     | 0.0000           | 0.0000          | 0.0000   | 0.0000    | 0.0000    | 0.0000          | 0.0000 | 0.0000  |
| 1               | 7.1400e-<br>003 | 0.0481 | 0.0715 | 1.2000e-<br>004 |                  | 2.4100e-<br>003 | 2.4100e-<br>003 | <br> <br> <br> <br> | 2.4100e-<br>003  | 2.4100e-<br>003 | 0.0000   | 10.0853   | 10.0853   | 5.7000e-<br>004 | 0.0000 | 10.0995 |
| Total           | 0.2847          | 0.0481 | 0.0715 | 1.2000e-<br>004 |                  | 2.4100e-<br>003 | 2.4100e-<br>003 |                     | 2.4100e-<br>003  | 2.4100e-<br>003 | 0.0000   | 10.0853   | 10.0853   | 5.7000e-<br>004 | 0.0000 | 10.0995 |

#### **Mitigated Construction Off-Site**

|          | ROG             | NOx             | СО              | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total   | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total     | Bio- CO2 | NBio- CO2 | Total CO2 | CH4              | N2O    | CO2e    |
|----------|-----------------|-----------------|-----------------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|------------------|--------|---------|
| Category |                 |                 |                 |                 | ton              | s/yr            |                 |                   |                  |                 |          |           | MT        | <sup>-</sup> /yr |        |         |
| Hauling  | 0.0000          | 0.0000          | 0.0000          | 0.0000          | 0.0000           | 0.0000          | 0.0000          | 0.0000            | 0.0000           | 0.0000          | 0.0000   | 0.0000    | 0.0000    | 0.0000           | 0.0000 | 0.0000  |
| Vendor   | 1.0000e-<br>004 | 3.4300e-<br>003 | 7.8000e-<br>004 | 1.0000e-<br>005 | 2.6000e-<br>004  | 0.0000          | 2.7000e-<br>004 | 8.0000e-<br>005   | 0.0000           | 8.0000e-<br>005 | 0.0000   | 1.0329    | 1.0329    | 4.0000e-<br>005  | 0.0000 | 1.0339  |
| Worker   | 5.1200e-<br>003 | 4.0300e-<br>003 | 0.0390          | 1.1000e-<br>004 | 0.0126           | 1.0000e-<br>004 | 0.0127          | 3.3400e-<br>003   | 9.0000e-<br>005  | 3.4300e-<br>003 | 0.0000   | 10.0982   | 10.0982   | 3.1000e-<br>004  | 0.0000 | 10.1060 |
| Total    | 5.2200e-<br>003 | 7.4600e-<br>003 | 0.0398          | 1.2000e-<br>004 | 0.0128           | 1.0000e-<br>004 | 0.0129          | 3.4200e-<br>003   | 9.0000e-<br>005  | 3.5100e-<br>003 | 0.0000   | 11.1311   | 11.1311   | 3.5000e-<br>004  | 0.0000 | 11.1399 |

# 4.0 Operational Detail - Mobile

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# **4.1 Mitigation Measures Mobile**

|             | ROG    | NOx    | СО     | SO2    | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2      | Total CO2      | CH4    | N2O    | CO2e           |
|-------------|--------|--------|--------|--------|------------------|-----------------|---------------|-------------------|------------------|-------------|----------|----------------|----------------|--------|--------|----------------|
| Category    |        |        |        |        | ton              | s/yr            |               |                   |                  |             |          |                | MT             | /yr    |        |                |
| Mitigated   | 0.3385 | 1.9686 | 3.8256 | 0.0162 | 1.5127           | 0.0109          | 1.5236        | 0.4058            | 0.0101           | 0.4159      | 0.0000   | 1,497.517<br>8 | 1,497.517<br>8 | 0.0608 | 0.0000 | 1,499.037<br>0 |
| Unmitigated | 0.3385 | 1.9686 | 3.8256 | 0.0162 | 1.5127           | 0.0109          | 1.5236        | 0.4058            | 0.0101           | 0.4159      | 0.0000   | 1,497.517<br>8 | 1,497.517<br>8 | 0.0608 | 0.0000 | 1,499.037<br>0 |

# **4.2 Trip Summary Information**

|                       | Ave      | rage Daily Trip Ra | ite      | Unmitigated | Mitigated  |
|-----------------------|----------|--------------------|----------|-------------|------------|
| Land Use              | Weekday  | Saturday           | Sunday   | Annual VMT  | Annual VMT |
| City Park             | 0.00     | 0.00               | 0.00     |             |            |
| Parking Lot           | 0.00     | 0.00               | 0.00     |             |            |
| Single Family Housing | 1,406.56 | 1,476.59           | 1284.38  | 4,030,500   | 4,030,500  |
| Total                 | 1,406.56 | 1,476.59           | 1,284.38 | 4,030,500   | 4,030,500  |

# **4.3 Trip Type Information**

|                       |            | Miles      |             |            | Trip %     |             |         | Trip Purpos | e %     |
|-----------------------|------------|------------|-------------|------------|------------|-------------|---------|-------------|---------|
| Land Use              | H-W or C-W | H-S or C-C | H-O or C-NW | H-W or C-W | H-S or C-C | H-O or C-NW | Primary | Diverted    | Pass-by |
| City Park             | 0.00       | 0.00       | 0.00        | 0.00       | 0.00       | 0.00        | 0       | 0           | 0       |
| Parking Lot           | 0.00       | 0.00       | 0.00        | 0.00       | 0.00       | 0.00        | 0       | 0           | 0       |
| Single Family Housing | 10.80      | 7.30       | 7.50        | 44.00      | 19.00      | 37.00       | 86      | 11          | 3       |

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#### 4.4 Fleet Mix

| Land Use              | LDA      | LDT1     | LDT2     | MDV      | LHD1     | LHD2     | MHD      | HHD      | OBUS     | UBUS     | MCY      | SBUS     | MH       |
|-----------------------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|
| City Park             | 0.569571 | 0.024470 | 0.206145 | 0.106238 | 0.013217 | 0.004041 | 0.019725 | 0.043623 | 0.003075 | 0.001900 | 0.006327 | 0.001084 | 0.000583 |
| Parking Lot           | 0.569571 | 0.024470 | 0.206145 | 0.106238 | 0.013217 | 0.004041 | 0.019725 | 0.043623 | 0.003075 | 0.001900 | 0.006327 | 0.001084 | 0.000583 |
| Single Family Housing | 0.569571 | 0.024470 | 0.206145 | 0.106238 | 0.013217 | 0.004041 | 0.019725 | 0.043623 | 0.003075 | 0.001900 | 0.006327 | 0.001084 | 0.000583 |

# 5.0 Energy Detail

Historical Energy Use: N

#### **5.1 Mitigation Measures Energy**

Exceed Title 24

Kilowatt Hours of Renewable Electricity Generated

Install Energy Efficient Appliances

|                            | ROG    | NOx    | CO     | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4             | N2O             | CO2e     |
|----------------------------|--------|--------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|-------------|----------|-----------|-----------|-----------------|-----------------|----------|
| Category                   |        |        |        |                 | ton              | s/yr            |               |                   |                  |             |          |           | MT        | /yr             |                 |          |
| Electricity<br>Mitigated   |        |        |        |                 |                  | 0.0000          | 0.0000        |                   | 0.0000           | 0.0000      | 0.0000   | 138.3278  | 138.3278  | 6.4800e-<br>003 | 1.3900e-<br>003 | 138.9040 |
| Electricity<br>Unmitigated | 1      |        |        | ,               |                  | 0.0000          | 0.0000        | ,                 | 0.0000           | 0.0000      | 0.0000   | 186.4000  | 186.4000  | 8.7400e-<br>003 | 1.8700e-<br>003 | 187.1765 |
| NaturalGas<br>Mitigated    | 0.0219 | 0.1871 | 0.0796 | 1.1900e-<br>003 |                  | 0.0151          | 0.0151        | ,                 | 0.0151           | 0.0151      | 0.0000   | 216.6814  | 216.6814  | 4.1500e-<br>003 | 3.9700e-<br>003 | 217.9690 |
| NaturalGas<br>Unmitigated  | 0.0234 | 0.1996 | 0.0849 | 1.2700e-<br>003 |                  | 0.0161          | 0.0161        |                   | 0.0161           | 0.0161      | 0.0000   | 231.1026  | 231.1026  | 4.4300e-<br>003 | 4.2400e-<br>003 | 232.4759 |

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# 5.2 Energy by Land Use - NaturalGas <u>Unmitigated</u>

|                          | NaturalGa<br>s Use | ROG    | NOx    | CO     | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total | Fugitive<br>PM2.5    | Exhaust<br>PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4             | N2O             | CO2e     |
|--------------------------|--------------------|--------|--------|--------|-----------------|------------------|-----------------|---------------|----------------------|------------------|-------------|----------|-----------|-----------|-----------------|-----------------|----------|
| Land Use                 | kBTU/yr            |        |        |        |                 | ton              | s/yr            |               |                      |                  |             |          |           | MT        | /yr             |                 |          |
| City Park                | 0                  | 0.0000 | 0.0000 | 0.0000 | 0.0000          |                  | 0.0000          | 0.0000        | i<br>i<br>i          | 0.0000           | 0.0000      | 0.0000   | 0.0000    | 0.0000    | 0.0000          | 0.0000          | 0.0000   |
| Parking Lot              | 0                  | 0.0000 | 0.0000 | 0.0000 | 0.0000          |                  | 0.0000          | 0.0000        | ,<br> <br> <br> <br> | 0.0000           | 0.0000      | 0.0000   | 0.0000    | 0.0000    | 0.0000          | 0.0000          | 0.0000   |
| Single Family<br>Housing | 4.3307e<br>+006    | 0.0234 | 0.1996 | 0.0849 | 1.2700e-<br>003 |                  | 0.0161          | 0.0161        | ,                    | 0.0161           | 0.0161      | 0.0000   | 231.1026  | 231.1026  | 4.4300e-<br>003 | 4.2400e-<br>003 | 232.4759 |
| Total                    |                    | 0.0234 | 0.1996 | 0.0849 | 1.2700e-<br>003 |                  | 0.0161          | 0.0161        |                      | 0.0161           | 0.0161      | 0.0000   | 231.1026  | 231.1026  | 4.4300e-<br>003 | 4.2400e-<br>003 | 232.4759 |

# **Mitigated**

|                          | NaturalGa<br>s Use | ROG    | NOx    | СО     | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4             | N2O             | CO2e     |
|--------------------------|--------------------|--------|--------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|-------------|----------|-----------|-----------|-----------------|-----------------|----------|
| Land Use                 | kBTU/yr            |        |        |        |                 | ton              | s/yr            |               |                   |                  |             |          |           | MT        | /уг             |                 |          |
| City Park                | 0                  | 0.0000 | 0.0000 | 0.0000 | 0.0000          |                  | 0.0000          | 0.0000        |                   | 0.0000           | 0.0000      | 0.0000   | 0.0000    | 0.0000    | 0.0000          | 0.0000          | 0.0000   |
| Parking Lot              | 0                  | 0.0000 | 0.0000 | 0.0000 | 0.0000          |                  | 0.0000          | 0.0000        |                   | 0.0000           | 0.0000      | 0.0000   | 0.0000    | 0.0000    | 0.0000          | 0.0000          | 0.0000   |
| Single Family<br>Housing | 4.06046e<br>+006   | 0.0219 | 0.1871 | 0.0796 | 1.1900e-<br>003 |                  | 0.0151          | 0.0151        |                   | 0.0151           | 0.0151      | 0.0000   | 216.6814  | 216.6814  | 4.1500e-<br>003 | 3.9700e-<br>003 | 217.9690 |
| Total                    |                    | 0.0219 | 0.1871 | 0.0796 | 1.1900e-<br>003 |                  | 0.0151          | 0.0151        |                   | 0.0151           | 0.0151      | 0.0000   | 216.6814  | 216.6814  | 4.1500e-<br>003 | 3.9700e-<br>003 | 217.9690 |

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5.3 Energy by Land Use - Electricity Unmitigated

|                          | Electricity<br>Use | Total CO2 | CH4             | N2O             | CO2e     |
|--------------------------|--------------------|-----------|-----------------|-----------------|----------|
| Land Use                 | kWh/yr             |           | МТ              | -/yr            |          |
| City Park                | 0                  | 0.0000    | 0.0000          | 0.0000          | 0.0000   |
| Parking Lot              | 170503             | 23.0972   | 1.0800e-<br>003 | 2.3000e-<br>004 | 23.1934  |
| Single Family<br>Housing | 1.20549e<br>+006   | 163.3028  | 7.6600e-<br>003 | 1.6400e-<br>003 | 163.9830 |
| Total                    |                    | 186.4000  | 8.7400e-<br>003 | 1.8700e-<br>003 | 187.1765 |

#### **Mitigated**

|                          | Electricity<br>Use | Total CO2 | CH4             | N2O             | CO2e     |
|--------------------------|--------------------|-----------|-----------------|-----------------|----------|
| Land Use                 | kWh/yr             |           | МТ              | -/yr            |          |
| City Park                | -108807            | -14.7396  | -0.0007         | -0.0002         | -14.8010 |
| Parking Lot              | 61695.8            | 8.3577    | 3.9000e-<br>004 | 8.0000e-<br>005 | 8.3925   |
| Single Family<br>Housing | 1.06824e<br>+006   | 144.7098  | 6.7800e-<br>003 | 1.4500e-<br>003 | 145.3125 |
| Total                    |                    | 138.3278  | 6.4800e-<br>003 | 1.3800e-<br>003 | 138.9040 |

6.0 Area Detail

#### Lico Subdivision Project - Monterey Bay Unified APCD Air District, Annual

# **6.1 Mitigation Measures Area**

Use Low VOC Paint - Residential Interior
Use Low VOC Paint - Residential Exterior
Use only Natural Gas Hearths

|             | ROG    | NOx    | СО     | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4             | N2O             | CO2e     |
|-------------|--------|--------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|-------------|----------|-----------|-----------|-----------------|-----------------|----------|
| Category    |        |        |        |                 | ton              | s/yr            |               |                   |                  |             |          |           | MT        | /yr             |                 |          |
| Mitigated   | 1.2307 | 0.1190 | 1.5759 | 7.3000e-<br>004 |                  | 0.0167          | 0.0167        |                   | 0.0167           | 0.0167      | 0.0000   | 119.8703  | 119.8703  | 4.6400e-<br>003 | 2.1500e-<br>003 | 120.6275 |
| Unmitigated | 1.2307 | 0.1190 | 1.5759 | 7.3000e-<br>004 |                  | 0.0167          | 0.0167        |                   | 0.0167           | 0.0167      | 0.0000   | 119.8703  | 119.8703  | 4.6400e-<br>003 | 2.1500e-<br>003 | 120.6275 |

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# Lico Subdivision Project - Monterey Bay Unified APCD Air District, Annual

# 6.2 Area by SubCategory Unmitigated

|                          | ROG     | NOx    | CO     | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total   | Fugitive<br>PM2.5 | Exhaust<br>PM2.5 | PM2.5 Total     | Bio- CO2 | NBio- CO2 | Total CO2 | CH4             | N2O             | CO2e     |
|--------------------------|---------|--------|--------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|-----------------|----------|
| SubCategory              | tons/yr |        |        |                 |                  |                 |                 |                   | MT               | -/yr            |          |           |           |                 |                 |          |
| Architectural<br>Coating | 0.0907  |        |        |                 |                  | 0.0000          | 0.0000          | !<br>!<br>!       | 0.0000           | 0.0000          | 0.0000   | 0.0000    | 0.0000    | 0.0000          | 0.0000          | 0.0000   |
| Consumer<br>Products     | 1.0823  |        |        |                 |                  | 0.0000          | 0.0000          | i<br>!<br>!       | 0.0000           | 0.0000          | 0.0000   | 0.0000    | 0.0000    | 0.0000          | 0.0000          | 0.0000   |
| Hearth                   | 0.0119  | 0.1013 | 0.0431 | 6.5000e-<br>004 |                  | 8.1900e-<br>003 | 8.1900e-<br>003 | <br>              | 8.1900e-<br>003  | 8.1900e-<br>003 | 0.0000   | 117.3598  | 117.3598  | 2.2500e-<br>003 | 2.1500e-<br>003 | 118.0572 |
| Landscaping              | 0.0459  | 0.0177 | 1.5328 | 8.0000e-<br>005 |                  | 8.5200e-<br>003 | 8.5200e-<br>003 | !<br>!<br>!       | 8.5200e-<br>003  | 8.5200e-<br>003 | 0.0000   | 2.5105    | 2.5105    | 2.3900e-<br>003 | 0.0000          | 2.5703   |
| Total                    | 1.2307  | 0.1190 | 1.5759 | 7.3000e-<br>004 |                  | 0.0167          | 0.0167          |                   | 0.0167           | 0.0167          | 0.0000   | 119.8703  | 119.8703  | 4.6400e-<br>003 | 2.1500e-<br>003 | 120.6275 |

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# Lico Subdivision Project - Monterey Bay Unified APCD Air District, Annual

# 6.2 Area by SubCategory Mitigated

|                          | ROG    | NOx     | CO     | SO2             | Fugitive<br>PM10 | Exhaust<br>PM10 | PM10<br>Total   | Fugitive<br>PM2.5    | Exhaust<br>PM2.5 | PM2.5 Total     | Bio- CO2 | NBio- CO2 | Total CO2 | CH4             | N2O             | CO2e     |
|--------------------------|--------|---------|--------|-----------------|------------------|-----------------|-----------------|----------------------|------------------|-----------------|----------|-----------|-----------|-----------------|-----------------|----------|
| SubCategory              |        | tons/yr |        |                 |                  |                 |                 |                      | МТ               | /yr             |          |           |           |                 |                 |          |
| Architectural<br>Coating | 0.0907 |         |        |                 |                  | 0.0000          | 0.0000          |                      | 0.0000           | 0.0000          | 0.0000   | 0.0000    | 0.0000    | 0.0000          | 0.0000          | 0.0000   |
| Consumer<br>Products     | 1.0823 |         | <br>   |                 |                  | 0.0000          | 0.0000          | <br>                 | 0.0000           | 0.0000          | 0.0000   | 0.0000    | 0.0000    | 0.0000          | 0.0000          | 0.0000   |
| Hearth                   | 0.0119 | 0.1013  | 0.0431 | 6.5000e-<br>004 |                  | 8.1900e-<br>003 | 8.1900e-<br>003 | <br>                 | 8.1900e-<br>003  | 8.1900e-<br>003 | 0.0000   | 117.3598  | 117.3598  | 2.2500e-<br>003 | 2.1500e-<br>003 | 118.0572 |
| Landscaping              | 0.0459 | 0.0177  | 1.5328 | 8.0000e-<br>005 |                  | 8.5200e-<br>003 | 8.5200e-<br>003 | 1<br> <br> <br> <br> | 8.5200e-<br>003  | 8.5200e-<br>003 | 0.0000   | 2.5105    | 2.5105    | 2.3900e-<br>003 | 0.0000          | 2.5703   |
| Total                    | 1.2307 | 0.1190  | 1.5759 | 7.3000e-<br>004 |                  | 0.0167          | 0.0167          |                      | 0.0167           | 0.0167          | 0.0000   | 119.8703  | 119.8703  | 4.6400e-<br>003 | 2.1500e-<br>003 | 120.6275 |

# 7.0 Water Detail

# 7.1 Mitigation Measures Water

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|             | Total CO2 | CH4    | N2O             | CO2e    |
|-------------|-----------|--------|-----------------|---------|
| Category    |           | МТ     | -/yr            |         |
| ga.ea       | 15.6795   | 0.2537 | 6.1100e-<br>003 | 23.8419 |
| Unmitigated | 15.6795   | 0.2537 | 6.1100e-<br>003 | 23.8419 |

# 7.2 Water by Land Use <u>Unmitigated</u>

|                          | Indoor/Out<br>door Use | Total CO2 | CH4             | N2O             | CO2e    |
|--------------------------|------------------------|-----------|-----------------|-----------------|---------|
| Land Use                 | Mgal                   |           | МТ              | √yr             |         |
| City Park                | 0 /<br>9.74632         | 4.6210    | 2.2000e-<br>004 | 5.0000e-<br>005 | 4.6403  |
| Parking Lot              | 0/0                    | 0.0000    | 0.0000          | 0.0000          | 0.0000  |
| Single Family<br>Housing | 7.76639 /<br>6.12023   | 11.0585   | 0.2535          | 6.0600e-<br>003 | 19.2017 |
| Total                    |                        | 15.6795   | 0.2537          | 6.1100e-<br>003 | 23.8419 |

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# Lico Subdivision Project - Monterey Bay Unified APCD Air District, Annual

7.2 Water by Land Use Mitigated

|                          | Indoor/Out<br>door Use | Total CO2 | CH4             | N2O             | CO2e    |  |  |
|--------------------------|------------------------|-----------|-----------------|-----------------|---------|--|--|
| Land Use                 | Mgal                   | MT/yr     |                 |                 |         |  |  |
| City Park                | 0 /<br>9.74632         | 4.6210    | 2.2000e-<br>004 | 5.0000e-<br>005 | 4.6403  |  |  |
| Parking Lot              | 0/0                    | 0.0000    | 0.0000          | 0.0000          | 0.0000  |  |  |
| Single Family<br>Housing | 7.76639 /<br>6.12023   | 11.0585   | 0.2535          | 6.0600e-<br>003 | 19.2017 |  |  |
| Total                    |                        | 15.6795   | 0.2537          | 6.1100e-<br>003 | 23.8419 |  |  |

# 8.0 Waste Detail

# 8.1 Mitigation Measures Waste

Lico Subdivision Project - Monterey Bay Unified APCD Air District, Annual

# Category/Year

|             | Total CO2 | CH4    | N2O    | CO2e    |  |  |  |  |
|-------------|-----------|--------|--------|---------|--|--|--|--|
|             | MT/yr     |        |        |         |  |  |  |  |
| gatea       |           | 2.2570 | 0.0000 | 94.6159 |  |  |  |  |
| Unmitigated | 38.1907   | 2.2570 | 0.0000 | 94.6159 |  |  |  |  |

# 8.2 Waste by Land Use <u>Unmitigated</u>

|                          | Waste<br>Disposed | Total CO2 | CH4             | N2O    | CO2e    |
|--------------------------|-------------------|-----------|-----------------|--------|---------|
| Land Use                 | tons              |           | МТ              | -/yr   |         |
| City Park                | 0.7               | 0.1421    | 8.4000e-<br>003 | 0.0000 | 0.3520  |
| Parking Lot              | 0                 | 0.0000    | 0.0000          | 0.0000 | 0.0000  |
| Single Family<br>Housing | 187.44            | 38.0486   | 2.2486          | 0.0000 | 94.2639 |
| Total                    |                   | 38.1907   | 2.2570          | 0.0000 | 94.6159 |

#### Lico Subdivision Project - Monterey Bay Unified APCD Air District, Annual

# 8.2 Waste by Land Use

#### **Mitigated**

|                          | Waste<br>Disposed | Total CO2 | CH4             | N2O    | CO2e    |
|--------------------------|-------------------|-----------|-----------------|--------|---------|
| Land Use                 | tons              |           | MT              | -/yr   |         |
| City Park                | 0.7               | 0.1421    | 8.4000e-<br>003 | 0.0000 | 0.3520  |
| Parking Lot              | 0                 | 0.0000    | 0.0000          | 0.0000 | 0.0000  |
| Single Family<br>Housing | 187.44            | 38.0486   | 2.2486          | 0.0000 | 94.2639 |
| Total                    |                   | 38.1907   | 2.2570          | 0.0000 | 94.6159 |

# 9.0 Operational Offroad

| Equipment Type | Number | Hours/Day | Days/Year | Horse Power | Load Factor | Fuel Type |
|----------------|--------|-----------|-----------|-------------|-------------|-----------|

# **10.0 Stationary Equipment**

#### **Fire Pumps and Emergency Generators**

| Equipment Type | Number | Hours/Day | Hours/Year | Horse Power | Load Factor | Fuel Type |
|----------------|--------|-----------|------------|-------------|-------------|-----------|

#### **Boilers**

| Equipment Type | Number | Heat Input/Day | Heat Input/Year | Boiler Rating | Fuel Type |
|----------------|--------|----------------|-----------------|---------------|-----------|
|----------------|--------|----------------|-----------------|---------------|-----------|

#### **User Defined Equipment**

| Equipment Type | Number |
|----------------|--------|

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# 11.0 Vegetation

#### **N2O Operational GHG Emission Mobile Calculations**

Project Title: Lico Subdivision

| Vehicle Population Breakdown* |                    |  |  |
|-------------------------------|--------------------|--|--|
| 61591                         | Gasoline vehicles  |  |  |
| 5686                          | Diesel vehicles    |  |  |
| 91.5%                         | Gasoline vehicle % |  |  |
| 8.5%                          | Diesel vehicle %   |  |  |

| VMT per Vehicle Type |                               |  |
|----------------------|-------------------------------|--|
| 4030500              | Project VMT (CalEEMod output) |  |
| 3689848              | Gasoline vehicle VMT          |  |
| 340652               | Diesel vehicle VMT            |  |

| Gasoline Vehicles |  |  |
|-------------------|--|--|
| 91.5%             | Gasoline vehicle %   |  |
| 1.9686            | Tons per year mobile NOX emissions (annual output in CalEEMod) |  |
| 1.80              | Gasoline vehicle tons per year NOX emissions                   |  |
| 4.16%             | Percentage to convert NOX emissions to N2O **                  |  |
| 0.0750            | Tons per year N2O emissions for gasoline vehicles              |  |
| 0.0680            | Metric tons per year N2O emissions for gasoline vehicles       |  |

|           | Diesel Vehicles  |
|-----------|--|
| 0.3316    | grams N2O per gallon of fuel for diesel vehicles**     |
| 161563.49 | Diesel average miles per gallon*                       |
| 0.00000   | grams per mile N2O for diesel vehicles                 |
| 0.7       | grams per year N2O for diesel vehicles                 |
| 0.0000007 | Metric tons per year N2O emissions for diesel vehicles |

| CO2E Emissions from N2O |  |  |
|-------------------------|--|--|
| 0.0680                  | Metric tons per year from gasoline + diesel vehicles                       |  |
| 298                     | GWP of N2O***  |  |
| 20.3                    | CO2E emissions per year from N2O emissions from gasoline + diesel vehicles |  |

#### **Sources**

#### \*Vehicle population source:

EMFAC2014 (v1.0.7) Emissions Inventory

Region Type: County Region: SAN BENITO Calendar Year: 2030 Season: Annual

Vehicle Classification: EMFAC2011 Categories

#### \*\*Methodology source:

EMFAC2011 Frequently Asked Questions

https://www.arb.ca.gov/msei/emfac2011-faq.htm

#### \*\*\*GWP source:

Intergovernmental Panel on Climate Change (IPCC). 2007.

AR4 Climate Change 2007: The Physical Science Basis.

Contrbution of Working Group I to the Fourth Assessment Report of the Intergovernmental Panel on Climate Change.

# Solar PV Requirements for Low-Rise Residential Buildings (2019 California Energy Code Section 150.1(b)14)

**Equation 150.1-C** kWPV = (CFA x A)/1000 + (NDwell x B)

| Inputs         |                     |       |  |
|----------------|---------------------|-------|--|
| Climate Zone   |                     | 4     |  |
| Cilillate Zone |                     | 4     |  |
|                | Adjustment Factor   |       |  |
| Α              | from Table 150.1-C  | 0.586 |  |
|                | Dwelling Adjustment |       |  |
|                | Factor from Table   |       |  |
| В              | 150.1-C             | 1.21  |  |

|                       |                          | Number of             | kWPV (KWdc     |
|-----------------------|--------------------------|-----------------------|----------------|
|                       | <b>Conditioned Floor</b> | <b>Dwelling Units</b> | Size of the PV |
| Unit Type             | Area (CFA)               | (Ndwell)              | System)        |
| Average Unit          | 1800                     | 149                   | 181            |
| 2SFD P1X              | 0                        | 0                     | 0              |
| 2SFD P2               | 0                        | 0                     | 0              |
| 2SFD P3               | 0                        | 0                     | 0              |
| 3SFD P1               | 0                        | 0                     | 0              |
| 3SFD P2               | 0                        | 0                     | 0              |
| 3SFD P3               | 0                        | 0                     | 0              |
| 2TH P1                | 0                        | 0                     | 0              |
| 2TH P2                | 0                        | 0                     | 0              |
| 2TH P3                | 0                        | 0                     | 0              |
| 2TH P3X               | 0                        | 0                     | 0              |
| 2TH P3Y               | 0                        | 0                     | 0              |
|                       |                          |                       | 0              |
|                       |                          |                       | 0              |
|                       |                          |                       | 0              |
|                       |                          |                       | 0              |
| Total Size of PV      |                          |                       |                |
| System (kW)           |                          | 149                   | 181            |
| kW to kWh             |                          |                       |                |
| Conversion Factor     |                          |                       | 1800           |
|                       |                          |                       |                |
|                       |                          |                       |                |
| Amount of Electricity |                          |                       |                |
| Generated (kWh/yr)    |                          |                       | 326,421        |

| Sources   |   |  |  |
|---|---|--|--|
| Climate Zones   | California Energy Commission. "California Building Climate Zone Areas." Last modified: November 2017. https://www.energy.ca.gov/maps/renewable/building_climate zones.html  |  |  |
| 2019 California<br>Energy Code                        | California Energy Commission. 2018. 2019 Building Energy Efficiency Standards for Residential and Nonresidential Buildings. December 2018. https://www.energy.ca.gov/2018publications/CEC-400-2018-020/CEC-400-2018-020-CMF.pdf |  |  |
| kWh per kW PV Solar<br>System (see page 12<br>of PDF) | United States Department of Energy. 2003. A Consumer's Guide: Get Your Power from the Sun. https://www.nrel.gov/docs/fy04osti/35297.pdf   |  |  |

| Table 150.1-C |         |                       |  |  |
|---------------|---------|-----------------------|--|--|
| Climate Zone  | A - CFA | B - Dwelling<br>Units |  |  |
| 1             | 0.793   | 1.27                  |  |  |
| 2             | 0.621   | 1.22                  |  |  |
| 3             | 0.628   | 1.12                  |  |  |
| 4             | 0.586   | 1.21                  |  |  |
| 5             | 0.585   | 1.06                  |  |  |
| 6             | 0.594   | 1.23                  |  |  |
| 7             | 0.572   | 1.15                  |  |  |
| 8             | 0.586   | 1.37                  |  |  |
| 9             | 0.613   | 1.36                  |  |  |
| 10            | 0.627   | 1.41                  |  |  |
| 11            | 0.836   | 1.44                  |  |  |
| 12            | 0.613   | 1.40                  |  |  |
| 13            | 0.894   | 1.51                  |  |  |
| 14            | 0.741   | 1.26                  |  |  |
| 15            | 1.56    | 1.47                  |  |  |
| 16            | 0.59    | 1.22                  |  |  |

# Appendix B

**Biological Resources Assessment** 

# MONK & ASSOCIATES

# **Environmental Consultants**

# BIOLOGICAL RESOURCES ANALYSIS 213 ENTERPRISE ROAD SAN BENITO COUNTY, CALIFORNIA

July 17, 2019

#### Prepared for

Longreach Associates, Inc. 101 Berkshire Street Bellaire, Texas 77401 Attention: Mr. Ty Intravia

#### Prepared by

Monk & Associates, Inc. 1136 Saranap Avenue, Suite Q Walnut Creek, California 94595 Contact: Mr. Geoff Monk

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#### **ATTACHMENTS**

(At Back of Report)

- Attachment A. Sheet 1. Confirmed Wetland Delineation Map. Prepared October 26, 2015, revised December 17, 2015. 213 Enterprise Road Project Site, Hollister, California.
- Attachment B. Tentative Map: Subdivision. Prepared June 18, 2019 by San Benito Engineering & Surveying, Inc.

Biological Resources Analysis 213 Enterprise Road Project San Benito County, California

#### 1. INTRODUCTION

Monk & Associates, Inc. (M&A) has prepared this biological resources analysis for the proposed 213 Enterprise Road development site (herein referred to as the project site) located outside the town of Hollister in San Benito County, California (Figures 1 and 2). The purpose of our analysis is to provide a description of existing biological resources on the project site and to identify potentially significant impacts that could occur to sensitive biological resources from the construction of a proposed residential development.

Biological resources include common plant and animal species, and special-status plants and animals as designated by the U.S. Fish and Wildlife Service (USFWS), California Department of Fish and Wildlife (CDFW), National Marine Fisheries Service (NMFS), and other resource organizations including the California Native Plant Society. Biological resources also include waters of the United States and State, as regulated by the U.S. Army Corps of Engineers (Corps), California Regional Water Quality Control Board (RWQCB), and CDFW. An assessment of the potential for impacts to regulated waters and a formal delineation of "waters of the U.S." on the project site was conducted in 2015. This delineation was verified by the Corps, the regulatory agency that defines waters of the United States, on December 8, 2015, and a Preliminary Jurisdictional Determination was issued by the Corps on January 26, 2016.

This biological resources analysis also provides mitigation measures for "potentially significant" and "significant" impacts that could occur to biological resources. Whenever possible, upon implementation, the prescribed mitigation measures would reduce impacts to levels considered less than significant pursuant to the California Environmental Quality Act (CEQA) (Pub. Resources Code §§ 21000 et seq.; 14 Cal. Code Regs §§ 15000 et seq). Accordingly, this report is suitable for review and inclusion in any review being conducted by the County of San Benito for the proposed project pursuant to the CEQA.

#### 2. PROPERTY LOCATION AND SETTING

The approximately 50.7-acre project site is located on the south side of Enterprise Road between Southside Road and Fairview Road in San Benito County, south of the city of Hollister (Figure 3). The Ridgemark Golf and Country Club lies approximately 1.0 mile to the east. The San Benito River lies approximately three-quarters of a mile to the south and west. The project site is terraced, sloping south (464 feet) to north (346 feet) towards Enterprise Road. A residential inholding (i.e., not a part of the project site) and associated out-buildings are located near the northwest corner of the project site (see Figure 3). The majority of the project site is open fields that are seasonally farmed and grazed by cattle, horses, and goats. From aerial photography research it appears to have been farmed and grazed for many decades. Stand pipes and valves in the southern portions of the project site also indicate that irrigation of crops took place at some time in the past.

#### 3. PROPOSED PROJECT

Longreach Associates, Inc. (the applicant) proposes to develop 151 single-family homes along with associated public streets, sidewalks, and on-street parking. Stormwater detention ponds and a sewer lift station are proposed in the lower, northeastern portion of the site.

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#### 4. ANALYSIS METHODS AND SURVEY HISTORY

#### 4.1 Survey History

In 2015, between the months of January and September, qualified and permitted M&A biologists conducted multiple site surveys for several special-status (that is, threatened, endangered, rare) plant and animal species. Following resource agency (i.e., CDFW and USFWS) prescribed survey protocols, surveys were conducted for the California tiger salamander (*Ambystoma californiense*), California red-legged frog (*Rana draytonii*), San Joaquin kit fox (*Vulpes macrotis mutica*), western burrowing owl (*Athene cunicularia*), American badger (*Taxidea taxus*), and special-status plants. No special-status plant or animal species was identified on or adjacent to the project site during the course of the survey effort.

#### 4.2 2019 Research and Survey Methods

Prior to preparing this biological resource analysis report, M&A researched the most recent version of CDFW's Natural Diversity Database (CNDDB) (RareFind 5 application). The application (CNDDB 2019) for historic and recent records of special-status plant and animal species known to occur in the region of the project site. M&A also searched the 2019 electronic version of the California Native Plant Society's (CNPS) *Inventory of Rare and Endangered Plants of California* (CNPS 2001) for records of special-status plants known in the region of the project site. All special-status species records were compiled in tables. M&A examined all known record locations for special-status species to determine if special-status species could occur on the project site or within an area of affect.

M&A biologists, Ms. Sharon Dulava and Mr. Zachery Stratton, conducted a survey of the project site on January 28, 2019 to record biological resources and to assess the likelihood of special-status species and resource agency regulated areas on the project site. M&A biologists, Mr. Geoff Monk and Ms. Dulava, conducted a follow-up survey on April 17, 2019 to survey for special-status species and check the Corps-regulated areas for any significant changes. The surveys involved searching all habitats on the site and recording all plant and wildlife species observed. M&A cross-referenced the habitats found on the project site against the habitat requirements of local or regionally known special-status species to determine if the proposed project could directly or indirectly impact such species.

Below we provide additional details of the 2019 survey dates and methods. Focused species surveys conducted in 2019 by M&A biologists were abbreviated over prior years since M&A conducted protocol-level surveys on this project site in 2015 which yielded negative results for all special-status species.

#### 4.3 Special-Status Plant Surveys

In 2019, surveys were conducted by M&A biologists in January and April. Plants observed during these two survey months were recorded in project notes. Protocol-level, special-status plant surveys were previously conducted on the project site by M&A biologists, Ms. Sarah Lynch and Ms. Christina Owens, on March 10, April 8, and June 29, 2015. These surveys were timed to coincide with the flowering periods of all special-status plants known to occur in similar habitats in San Benito County. All surveys were conducted according to USFWS (2000), CDFW

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(2009), and CNPS (2001) published survey guidelines. Special-status plant surveys were not repeated in 2019 due to an absence of suitable special-status plant habitats onsite and a general overall absence of any type of native or naturalized plant community onsite due to years of farming and overgrazing activity which has left the landscape essentially denuded by the summer months. While cattle have historically grazed the site, goats, which are far more damaging to plant life, were observed grazing the project site during the 2019 surveys.

#### 4.4 Special-Status Wildlife Species Surveys

January and April 2019 surveys were conducted to confirm that site conditions remained the same as when the 2015 protocol-level species surveys had been conducted and to confirm that no special-status species had moved onto the project site in the intervening years (all 2015 survey findings were negative). On January 28, 2019, M&A biologists, Ms. Dulava and Mr. Stratton, conducted a survey for California tiger salamander, California red-legged frog, western spadefoot toad (*Spea hammondii*), western burrowing owl, American badger, and San Joaquin kit fox. This survey entailed walking systematic transects throughout the project site looking for suitable habitat for the species in question or sign of the animal (e.g., scat, track, feather, nest, characteristic digging/burrow, or direct observation of the species). High-powered binoculars (10x42) were used to scan the landscape and trees for animals. Notes were made in a notebook on site conditions, weather, and species observed. M&A biologists, Mr. Monk and Ms. Dulava, conducted a follow-up survey on April 17, 2019 using the same survey methods.

#### 5. RESULTS OF RESEARCH AND PROJECT SITE ANALYSES

#### 5.1 Topography

The project site is tiered and slopes south (464 feet) to north (346 feet) towards Enterprise Road. The majority of the site has a varying degree of slope ranging from 2 to 13 percent. This site drains north via sheet flow. There is also a culvert in the northeastern end of the project site that drains underneath Enterprise Road. Elevations range from an elevation of approximately 346 feet above sea level in the northwestern corner of the project site to approximately 464 feet above sea level in the southeastern corner.

#### 5.2 Hydrology

There is a remnant drainage channel that historically flowed east to west, roughly parallel with Enterprise Road, across the northern quarter of the project site. The relatively recently constructed (likely in the last 20 years) high-density residential Oak Creek Development that occurs immediately east of the project site was constructed over the historical alignment of this drainage. That development included the construction of a flood control basin on the east side of the project site (see Sheet 1) that catches all flows from the now-developed watershed under the Oak Creek Development. This flood control basin accepts stormwater flowing from two parallel, 5-foot diameter, reinforced concrete pipes (RCPs) constructed under the Oak Creek Development. The basin includes an approximate 20-foot high berm on the downstream side of the basin ensuring that flood waters are not able to flow into the historical alignment of this drainage across the project site. To the west of this flood control basin, the remnant portions of this drainage that remain on the project site no longer flow (no unvegetated scour) and currently support upland plant species. Thus, the Corps did not take jurisdiction over this remnant channel

when they confirmed their jurisdiction on the project site (see Sheet 1). The downstream reaches of the historic alignment of the now-truncated drainage are also filled by a now decades old home and outbuildings, which are inholdings within the project site. Thus, the remnant portions of the drainage on the project site are isolated from flows or connectivity to any water of the United States or State other than by sheet flow to collectors along Enterprise Road.

The flood control basin that receives flows from the watershed now composed of the Oak Creek Development jettisons stormwater through a 6-foot diameter RCP installed underneath Enterprise Road. This RCP terminates in a San Benito County maintained flood control basin off the project site immediately to the north of Enterprise Road. The County's flood control basin jettisons collected storm waters into a large diameter (~8-foot diameter) RCP that flows westward, parallel with and on the north side of Enterprise Road. This RCP presumably (not confirmed) drains to the San Benito River, a geographically appropriately positioned receiving water located approximately three-quarters of a mile to the south and west of the project site.

#### 5.3 Plant Communities and Associated Wildlife Habitats

A complete list of plant species observed on the project site is presented in Table 1. Nomenclature used for plant names follows *The Jepson Manual* Second Edition (Baldwin 2012) and changes made to this manual as published on the Jepson Interchange Project website (<a href="http://ucjeps.berkeley.edu/interchange/index.html">http://ucjeps.berkeley.edu/interchange/index.html</a>). Table 2 is a list of wildlife species observed on the project site. Nomenclature for wildlife follows CDFW's *Complete list of amphibian*, *reptile*, *bird*, *and mammal species in California* (2016) and any changes made to species nomenclature as published in scientific journals since the publication of CDFW's list.

#### 5.3.1 ANTHROPOGENIC

The entire project site can be characterized as having anthropogenic, or human-influenced, plant communities. No natural plant communities remain onsite due to years of farming practices and intensive livestock grazing, most recently by goats. Hay fields, wheat fields, and ruderal vegetation are present on this project site. The project site's interior fencing gives the appearance that this sloping site has been sectioned off into different tiers or levels (see Figure 3 or Sheet 1). The southern portion of the site has historically been used as a hayfield and appears to be routinely disked. At the time of the January and April 2019 site surveys this section was vegetated with volunteer cultivated oats (Avena sativa), red-stem filaree (Erodium cicutarium) and white-stem filaree (E. moschatum), common fiddleneck (Amsinckia menziesii), with additional non-native grasses and forb species such as ripgut grass (Bromus diandrus), foxtail barley (Hordeum murinum ssp. leporinum), winter vetch (Vicia villosa), and common hoary cress (Lepidium draba). The next section of the project site (to the north) supports a similar suite of herbaceous species as well as other non-native grass and forb species such as wild mustard (Hirschfelda incana, Brassica nigra), cheeseweed (Malva parviflora), annual bluegrass (Poa annua), Shepherd's purse (Capsella bursa-pastoris), and California burclover (Medicago polymorpha). Native grass and forb species in these areas include Miner's lettuce (Claytonia perfoliata), red maids (Calandrinia ciliata), and California poppy (Eschscholzia californica). This "non-crop" vegetation germinates in the winter months in low maintenance periods, but according to the land owner is then turned under by disking in the spring. There are also native and non-native trees that are sparsely distributed throughout the project site that include the

native valley oak (*Quercus lobata*), California buckeye (*Aesculus californica*), and Monterey pine (*Pinus radiata*) tree, and the non-natives Peruvian pepper tree (*Schinus molle*), and blue gum (*Eucalyptus globulus*).

There are remnant reaches of a historical drainage on the project site that many years ago flowed east to west, roughly south of and parallel with Enterprise Road. The relatively recently constructed high-density residential Oak Creek Development that occurs immediately east of the project site was constructed over the historical alignment of this drainage. That development included the construction of a water quality basin that now intercepts and diverts all flows from the historic watershed now under the Oak Creek Development to the County of San Benito storm drain system (see Topography and Hydrology Section above). The water quality basin onsite supports annual and perennial wetland plant species such as creeping spikerush (Eleocharis macrostachya), annual bluegrass (Poa annua), Hyssop loosestrife (Lythrum hyssopifolia), popcornflower (*Plagiobothrys* sp.), curly dock (*Rumex crispus*), water plantain (*Alisma* sp.), and spiny cocklebur (Xanthium spinosum). To the west of this water quality basin, the remnant reaches of the former drainage on the project site no longer support stormwater flows. There are no unvegetated scours or wetlands in this remnant geographic feature. The former drainage supports upland plant species such as white-stem filaree, fiddleneck (Amsinckia menziesii). California burclover, Italian thistle (Carduus pycnocephala), everlasting cudweed (Pseudognaphalium luteoalbum), stinkwort (Dittrichia graveolens), Mediterranean barley (Hordeum marinum var. gussoneanum), foxtail barley, Italian ryegrass (Festuca perennis), shortpodded mustard, common chickweed (Stellaria media), milk thistle, wild radish (Raphanus sativus), and jointed charlock (Raphanus raphanistrum). There are some native forbs such as vinegar weed (*Trichostema lanceolatum*) and California poppy around and in the remnant drainage channel.

Trees on the project site provide perching, nesting and foraging habitat for a large number of bird species. Insectivorous birds that "glean" insects from trees leaves and branches such as yellowrumped warbler (Dendroica coronata), ruby-crowned kinglet (Regulus calendula), bushtit (Psaltriparus minimus), and orange-crowned warbler (Vermivora celata) were observed in the trees on multiple occasions. As were seed-eating birds that perch and/or nest in the trees such as Eurasian collared-dove (Streptopelia decaocto), mourning dove (Zenaida macroura), lark sparrow (Chondestes grammacus), white-crowned sparrow (Zonotrichia leucophrys), dark-eyed junco (Junco hyemalis), lesser goldfinch (Spinus psaltria), and house finch (Haemorhous mexicanus). These seed-eating species will forage for seeds on the ground, in the herbaceous vegetation (thistles, for example), and from the trees. Anna's hummingbird (Calypte anna) will eat insects in addition to sipping nectar from local flowers; this hummingbird was observed during every site visit. Other birds commonly observed on the project site were Nuttall's woodpecker (Picoides nuttallii), northern flicker (Colaptes auratus), Say's phoebe (Sayornis saya), California scrub jay (Aphelocoma californica), common raven (Corvus corax), oak titmouse (Baeolophus inornatus), Bewick's wren (Thryomanes bewickii), American robin (Turdus migratorius), northern mockingbird (Mimus polyglottos), black phoebe (Sayornis nigricans), and American pipit (Anthus rubescens). The larger trees provide nesting habitat for raptors such as the red-shouldered hawk (Buteo lineatus) and red-tailed hawk (Buteo jamaicensis). While no active nests were observed during 2019 surveys, a red-tailed hawk was observed nesting adjacent to the project site during the 2015 surveys. Mammals observed on the

project site during M&A's surveys included gray fox (*Urocyon cinereoargenteus*), striped skunk (*Mephitis mephitis*), California ground squirrel (*Otospermophilus beecheyi*), Botta's pocket gopher (*Thomomys bottae*), and Columbian black-tailed deer (*Odocoileus hemionus* var. *columbianus*). Table 2 provides a complete list of wildlife observed on the project site.

#### 5.4 Wildlife Corridors

Wildlife corridors are linear and/or regional habitats that provide connectivity to other natural vegetation communities within a landscape fractured by urbanization and other development. Wildlife corridors have several functions: 1) they provide avenues along which wide-ranging animals can travel, migrate, and breed, allowing genetic interchange to occur; 2) populations can move in response to environmental changes and natural disasters; and 3) individuals can recolonize habitats from which populations have been locally extirpated (Beier and Loe 1992). All three of these functions can be met if both regional and local wildlife corridors are accessible to wildlife. Regional wildlife corridors provide foraging, breeding, and retreat areas for migrating, dispersing, immigrating, and emigrating wildlife populations. Local wildlife corridors also provide access routes to food, cover, and water resources within restricted habitats.

The project site is truncated from being a regional wildlife corridor due to the relatively recent development (last 20 years) that has occurred in the area. East, northeast, north, and south of the project site is dense residential and golf course development which restricts wildlife moving in or out from lands north, south and east. Associated with this development are heavily traveled roads such as Union Road, Southside Road, and Airline Highway which all pose obstacles to, and hazardous conditions for wildlife. Thus, the project site does not provide a thoroughfare for wildlife movement from contiguous or non-contiguous open spaces. The project site now functions as a local foraging ground for common terrestrial wildlife that reside in the immediate project site area of the project site. The project site does not provide a local or regional wildlife corridor. Thus, site development would not impact regional or local wildlife corridors.

#### 6. SPECIAL-STATUS SPECIES DEFINITION

#### 6.1 Definitions

For purposes of this analysis, special-status species are plants and animals that are legally protected under the California and Federal Endangered Species Acts (CESA and FESA, respectively) or other regulations, and species that are considered rare by the scientific community (for example, the CNPS). Special-status species are defined as:

- plants and animals that are listed or proposed for listing as threatened or endangered under the CESA (Fish and Game Code §2050 et seq.; 14 CCR §670.1 et seq.) or the FESA (50 CFR 17.12 for plants; 50 CFR 17.11 for animals; various notices in the Federal Register [FR] for proposed species);
- plants and animals that are candidates for possible future listing as threatened or endangered under the FESA (50 CFR 17; FR Vol. 64, No. 205, pages 57533-57547, October 25, 1999); and under the CESA (California Fish and Game Code §2068);

- plants and animals that meet the definition of endangered, rare, or threatened under the CEQA (14 CCR §15380) that may include species not found on either State or Federal Endangered Species lists;
- Plants occurring on Ranks 1A, 1B, 2A, 2B, 3, and 4 of CNPS' electronic *Inventory* (CNPS 2001). The CDFW recognizes that Ranks 1A, 1B, 2A and 2B of the CNPS inventory contain plants that, in the majority of cases, would qualify for State listing, and CDFW requests their inclusion in EIRs. Plants occurring on CNPS Ranks 3 and 4 are "plants about which more information is necessary," and "plants of limited distribution," respectively (CNPS 2001). Such plants may be included as special-status species on a case by case basis due to local significance or recent biological information (more on CNPS Rank species below);
- migratory nongame birds of management concern listed by USFWS (Migratory Nongame Birds of Management Concern in the United States: The list 1995; Office of Migratory Bird Management; Washington D.C.; Sept. 1995);
- animals that are designated as "species of special concern" by CDFW (2019);
- Animal species that are "fully protected" in California (Fish and Game Codes 3511, 4700, 5050, and 5515).
- Bat Species that are designated on the Western Bat Working Group's (WBWG) Regional Bat Species Priority Matrix as: "RED OR HIGH." This priority is justified by the WBWG as follows: "Based on available information on distribution, status, ecology, and known threats, this designation should result in these bat species being considered the highest priority for funding, planning, and conservation actions. Information about status and threats to most species could result in effective conservation actions being implemented should a commitment to management exist. These species are imperiled or are at high risk of imperilment."

In the paragraphs below, we provide further definitions of legal status as they pertain to the special-status species discussed in this report or in the attached tables.

<u>Federal Endangered or Threatened Species.</u> A species listed as Endangered or Threatened under the FESA is protected from unauthorized "take" (that is, harass, harm, pursue, hunt, shoot, trap) of that species. If it is necessary to take a federally-listed Endangered or Threatened species as part of an otherwise lawful activity, it would be necessary to receive permission from the USFWS prior to initiating the take.

State Threatened Species. A species listed as Threatened under the CESA (§2050 of California Fish and Game Code) is protected from unauthorized "take" (that is, harass, pursue, hunt, shoot, trap) of that species. If it is necessary to "take" a state-listed Threatened species as part of an otherwise lawful activity, it would be necessary to receive permission from CDFW prior to initiating the "take."

<u>California Species of Special Concern</u>. These are species in which their California breeding populations are seriously declining and extirpation from all or a portion of their range is possible. This designation affords no legally mandated protection; however, pursuant to the CEQA Guidelines (14 CCR §15380), some species of special concern could be considered "rare." Pursuant to its rarity status, any unmitigated impacts to rare species could be considered a "significant effect on the environment" (§15382). Thus, species of special concern must be considered in any project that will, or is currently, undergoing CEQA review, and/or that must obtain an environmental permit(s) from a public agency.

<u>CNPS Rank Species</u>. The CNPS maintains an "Inventory" of special-status plant species. This inventory has four lists of plants with varying rarity. These lists are: Rank 1, Rank 2, Rank 3, and Rank 4. Although plants on these lists have no formal legal protection (unless they are also state or federally-listed species), CDFW requests the inclusion of Rank 1 species in environmental documents. In addition, other state and local agencies may request the inclusion of species on other lists as well. The Rank 1 and 2 species are defined below:

- Rank 1A: Presumed extinct in California;
- Rank 1B: Rare, threatened, or endangered in California and elsewhere;
- Rank 2A: Plants presumed extirpated in California, but more common elsewhere;
- Rank 2B: Rare, threatened, or endangered in California, but more common elsewhere.

All of the plants constituting Rank 1B meet the definitions of Section 1901, Chapter 10 (Native Plant Protection Act) or Sections 2062 and 2067 (CESA) of the Fish and Game Code and are eligible for state listing (CNPS 2001). Rank 2 species are rare in California, but more common elsewhere. Ranks 3 and 4 contain species about which there is some concern and are reviewed by CDFW and maintained on "watch lists."

Additionally, in 2006 CNPS updated their lists to include "threat code extensions" for each list. For example, Rank 1B species would now be categorized as Rank 1B.1, Rank 1B.2, or Rank 1B.3. These threat codes are defined as follows:

- .1 is considered "seriously endangered in California (over 80% of occurrences threatened/high degree and immediacy of threat)";
- .2 is "fairly endangered in California (20-80% of occurrences threatened)";
- .3 is "not very endangered in California (less than 20% of occurrences threatened or no current threats known)."

Under the CEQA review process only CNPS Rank 1 and 2 species are considered since these are the only CNPS species that meet CEQA's definition of "rare" or "endangered." Impacts to Rank 3 and 4 species are not regarded as significant pursuant to CEQA.

<u>Fully Protected Birds</u>. Fully protected birds, such as the white-tailed kite and golden eagle, are protected under California Fish and Game Code (§3511). Fully protected birds may not be "taken" or possessed (i.e., kept in captivity) at any time.

# 6.2 Potential Special-Status Plants on the Project Site

Figure 4 provides a graphical illustration of the closest known records for special-status plant species within 3 miles of the project site and helps readers visually understand the number of sensitive species that occur in the vicinity of the project site. No special-status plants have been mapped on or adjacent the project site. However, according to the CNPS *Inventory* and CDFW's CNDDB, a total of 15 special-status plant species are known to occur in the region of the project site (Table 3). Most of these plants occur in specialized habitats such as vernal pools, alkaline substrates, or chaparral/coastal scrub communities. Additionally, owing to the excessively disturbed and unnatural conditions found at the project site, the project site has been farmed and grazed by both cattle and currently goats, special-status plants would not likely occur. In order to substantiate this premise, M&A conducted three separate project site surveys in March, April, and June 2015, in order to document plant communities, note site conditions, and survey for special-status plants. Throughout the course of the three survey months M&A Botanists observed very few native plant species and concluded that no special-status plant species are present on the project site. In addition, no special-status plant species were observed during surveys conducted in January and April 2019. Hence, project site development could take place without concerns for special-status plants; no impacts to special-status plants would occur and no mitigation for special-status plants is warranted.

# 6.3 Potential Special-Status Animals on the Project Site

Figure 4 provides a graphical illustration of the closest known records for special-status wildlife species within 3 miles of the project site and helps readers visually understand the number of sensitive species that occur in the vicinity of the project site. No special-status animal records have ever been mapped on or adjacent to the project site. However, a total of 13 special-status animal species are known to occur in the region of the project site (Table 4). Because of the sensitivity of four (4) of the special-status animal species known to occur in the area we further discuss these species below; these are the California tiger salamander, California red-legged frog, western burrowing owl, and the San Joaquin kit fox. We also discuss the greater western mastiff bat (*Eumops perotis californicus*) and western red bat (*Lasiurus blossevillii*) since suitable habitat for these bat species is provided by the project site.

#### 6.3.1 CALIFORNIA TIGER SALAMANDER

The project site is located within the known range of the Central California "Distinct Population Segment" (DPS) of the California tiger salamander. The Central California DPS of the California tiger salamander was federally-listed as threatened under the FESA on August 4, 2004. The USFWS designated critical habitat for the Central California DPS in the summer of 2004 and updated the critical habitat designations in 2005 (USFWS 2005). The project site is located *outside* of mapped Critical Habitat Unit CV-18 (Figure 5). Finally, on August 19, 2010, the California tiger salamander was also state-listed as a threatened species under the CESA.

Proposed projects may not impact the California tiger salamander without incidental taking authority from both the USFWS and the CDFW. Prior to impacting habitat that supports the California tiger salamander the USFWS must prepare an incidental take permit pursuant to either Section 7 or Section 10 of the FESA. Similarly, projects that impact the California tiger salamander also require incidental taking authority from the. Under Section 2081 of CESA, an

incidental take permit may be authorized by the CDFW for proposed projects that impact the California tiger salamander.

California tiger salamanders occur in grasslands and open oak woodlands that provide suitable over summering and/or breeding habitats. California tiger salamanders spend the majority of their lives underground. They typically only emerge from their subterranean refugia for a few nights each year during the rainy season to migrate to breeding ponds. Adult California tiger salamanders have been observed up to 2,092 meters (1.3 miles) from breeding ponds (USFWS 2004). As such, unobstructed migration corridors are an important component of California tiger salamander habitat.

California tiger salamanders emerge during the first heavy, warm rains of the year, typically in late November and early December. In most instances, larger movements of California tiger salamander do not occur unless it has been raining hard and continuously for several hours. Typically, for larger movements of California tiger salamanders to occur, nighttime temperatures also must be above 48° F. California tiger salamanders are able to move over, through or around almost all obstacles. Significant obstructions that block California tiger salamander movements include freeways and other major (heavy traffic) roads, rivers, and deep, vertical or near vertical sided, concrete irrigation/flood control ditches.

During the spring, summer, and fall months, most known populations of the California tiger salamander predominately use California ground squirrel burrows as over-summering habitat (Jennings and Hayes 1994; G. Monk personal observation). Other secondary subterranean refugia, or primary refugia where California ground squirrels are absent, likely include Botta's pocket gopher burrows, deep fissures in desiccated clay soils, and debris piles (e.g. downed wood, rock piles).

Stock ponds, seasonal wetlands, and deep vernal pools typically provide most of the breeding habitat used by the California tiger salamander. In such locations, California tiger salamanders attach their eggs to rooted, emergent vegetation, and other stable filamentous objects in the water column. Eggs are gelatinous and are laid singly or occasionally in small clusters. Eggs range in size from about ¾ the diameter of a dime to the full diameter of a dime. Occasionally California tiger salamanders are found breeding in slow-moving, streams or ditches. Ditches and/or streams that are subject to rapid flows, even if only on occasion, typically will not support or sustain California tiger salamander egg attachment through hatching, and thus, are not usually used successfully by California tiger salamanders for breeding (Mr. Monk and Ms. Lynch, pers. observations). Similarly, streams and/or ditches that support predators of the California tiger salamander or their eggs and larvae such as fish, bullfrogs, red swamp crayfish, or signal crayfish, almost never constitute suitable breeding habitat.

Typically, seasonal wetlands that are used for breeding must hold water into the month of May to allow enough time for larvae to fully metamorphose. In dry years, seasonal wetlands may dry too early to allow enough time for California tiger salamander larvae to successfully metamorphose. Under such circumstances, desiccated California tiger salamander larvae can be found in dried pools. In addition, as pools dry down to very small areas of inundation, California tiger salamander larvae become concentrated and are very susceptible to predation. However, in years

exhibiting wet springs, these same pools can remain inundated long enough through continual rewetting to allow California tiger salamander larvae ample time to successfully metamorphose.

The closest known California tiger salamander record to the project site is a 1999 record located 1.2 miles east of the project site in a seasonal detention pond at the Ridgemark Golf Course (CNDDB Occurrence No. 190). There is dense residential development between this detention pond and the project site. It is therefore highly unlikely that California tiger salamander residing on this golf course could successfully migrate overland to the project site over major roads and through solid wood-fenced backyards. The next closest California tiger salamander record is from 2003 where a single male was observed approximately 1.2 miles southwest of the project site in the San Benito River (CNDDB Occurrence No. 868). This sighting is separated from the project site by homes and intensively maintained and irrigated agricultural lands making overland migration to the project site difficult, if not impossible. Additionally, since there is no breeding habitat on or adjacent to the project site, or accessible from the project site, there would be no reason for California tiger salamander to reside on the project site.

Aquatic habitat on the project site is limited to a man-made flood control basin that was constructed over the top of a historic drainage. Water flows into this basin via culverts emanating from the adjacent development (Oak Creek) to the east and then quickly flushes out of the basin via an outlet culvert that directs flows north and under Enterprise Road. The basin maintains positive flows, only catching by design very large storm events that would exceed the flow capacity of the 6-foot RCP exiting this basin. Water does not pool in this basin for any length of time and thus, it does not provide potential California tiger salamander breeding habitat. The basin only supported a shallow (< 3 inches deep) puddle for a short time in the winter of 2018-2019, after periods of heavy rain. Thus, it did not provide suitable aquatic habitat for California tiger salamander. West of this basin on the project site is a remnant portion of the historic drainage. This drainage historically flowed west to east, but no longer supports flows owing to the flood control basin constructed to catch all watershed flows upstream of the project site from within the Oak Creek Development. M&A never observed water in this drainage during the course of our 2019 site surveys. A detention area exists just south of the project site. This feature is surrounded by dense residential development and did not hold water in the winter of 2018-2019.

The only other aquatic habitat within the project site vicinity is a San Benito County maintained flood control basin on the north side of Enterprise Road. Similar to the flood control basin onsite, this basin was constructed to contain and slow flood waters before they are discharged into the surrounding landscape; thus, water is not detained for long-duration and aquatic conditions/habitat do not persist in this basin. This basin only supports upland vegetation (coyote brush, for example). This basin does not provide any indication that it retains water (no vegetation suppression; no aquatic vegetation such as cattails).

There are no other potential breeding ponds within 1.3 miles of the project site, the distance California tiger salamander can migrate, that are not separated from the project site by developed and/or intensively maintained and irrigated farmland. Due to an absence of suitable breeding habitats onsite and within the vicinity of the project site it can be concluded that the California tiger salamander would not reside onsite and therefore that the proposed project would not result

in significant impacts to California tiger salamander. Thus, no mitigation for California tiger salamander is warranted for the proposed project.

#### 6.3.2 CALIFORNIA RED-LEGGED FROG

The California red-legged frog was federally-listed as threatened on May 23, 1996 (Federal Register 61: 25813-25833) and as such is protected pursuant to the FESA. On March 16, 2010, the USFWS issued the final designation for California red-legged frog Critical Habitat (USFWS 2010). The 2010 Critical Habitat maps (Federal Register dated March 17, 2010 (Volume 75, Number 51:12815-12864) show that the project site falls *outside* Critical Habitat Unit SNB-1 (Figure 5). The California red-legged frog is also a state "species of special concern."

The California red-legged frog is typically found in ponds, slow-flowing portions of perennial and intermittent streams that maintain water in the summer months. This frog is also found in hillside seeps that maintain pool environments or saturated soils throughout the summer months. Populations probably cannot be maintained if all surface water disappears (i.e., no available surface water for egg laying and larval development habitat). Larval California red-legged frogs require 11-20 weeks of permanent water to reach metamorphosis (i.e., to change from a tadpole into a frog), in water depths of 10 to 20 inches (USFWS 2002). Riparian vegetation such as willows and emergent vegetation such as cattails are preferred red-legged frog habitats, though not necessary for this species to be present. Populations of California red-legged frog will be reduced in size or eliminated from ponds supporting non-native species such as bullfrog, Centrarchid fish species (such as sunfish, bluegill, or largemouth bass), and signal and red swamp crayfish (*Pacifastacus leniusculus* and *Procambarus clarkii*, respectively), all of which are known California red-legged frog predators. However, the presence of these non-native species does not preclude the presence of the California red-legged frog.

California red-legged frogs use both aquatic and upland habitats for migration and dispersal. The USFWS' *Recovery Plan for the California Red-Legged Frog* states that California red-legged frog overland excursions via uplands can vary between 0.25 mile up to 3 miles during the course of a wet season, and that frogs "have been observed to make long-distance movements that are straight-line, point to point migrations rather than using corridors for moving in between habitats" (USFWS 2002). The information presented in the USFWS' Recovery Plan was obtained in part from a publication by Bulger et al. (2003).

Bulger et al. (2003) studied 19 radio tagged California red-legged frogs in Santa Cruz County and found that "most migrating individuals moved to the nearest pond to breed, and to the nearest pond or stream after breeding. The three exceptions to this pattern all resided in the same pond (not used for breeding) during the summer and then migrated to breed in a pond 2800 m distant." Bulger et al. (2003) further stated that that their data showed that "there is a relatively small segment of the adult population that is liable to migrate in any given year, and that most adults are resident year around at favorable breeding sites." Data on migration rates from this study indicate that "more than 75% of the adult population is resident at permanent aquatic sites over the course of a year." "Moreover, 90% of the radio-tagged frogs that were not migrating between aquatic sites remained within 60 m of water at all times and the farthest any non-migrating frog moved from water was 130 m." For frogs that did migrate, Bulger et al. (2003) reported that most migrating frogs moved overland in approximately straight lines to

target sites without apparent regard to vegetation type or topography. Bulger et al. (2003) also states that they did not locate individual frogs daily, and that they "do not have tightly bounded data on numbers of days spent moving versus resting..." Thus, to an extent, straight line migrations were determined by using departure and final resting/breeding locations.

Working in Point Reyes National Seashore on the coast of California, Fellers and Kleeman (2007) radio-tagged 115 California red-legged frogs in the greater Olema Valley [in Marin County] and determined that "the median distance moved from breeding sites was 0 m, but for the 36 frogs that moved  $\geq$  30 m, the median was 150 m (range = 30-1400 m). In many cases, frogs almost certainly moved more than the straight-line distance between sites. This was confirmed with individuals that were located in transit. Presumed distance moved for those frogs that moved  $\geq$  30 m was 185 m (median, range = 30-1400 m)."

As reported by Fellers and Kleeman (2007), migrations of California red-legged frogs that were radio-tagged to determine movements were conducted at study sites near the Pacific Ocean where summer fog and high relative humidity reduce the risk of desiccation for dispersing amphibians. Bulger et al. (2003) studies similarly were conducted near the Pacific Ocean where summer fog and relative humidity are much higher than in inland populations of the California red-legged. In locations that are characterized by hot and seasonally dry climates, desiccation mortality likely influences movements of the California red-legged to a greater extent. Tatarian (2005) studied an inland population of California red-legged frogs in eastern Contra Costa County where the climate is far drier than the coastal environment. Tatarian (2005) found that all movements of California red-legged frog started after the first 0.5 cm of rain in the fall, with more terrestrial movements being made in the fall pre-breeding season (57%) than in the winter breeding season (32%) or spring post-breeding season (11%). Tatarian (2007) also found that California red-legged frogs moved greater average distances aquatically (84.6 m) than terrestrially (27.7 m). Greater terrestrial distances were moved in the pre-breeding season (35.2 m) than in the breeding season (15.5 m) or post-breeding season (16.3 m) with the majority of movements occurring for only one of the 3-4 day survey periods. The majority of frogs (57%) were position faithful within a pool, indicating they did not migrate at all. These data likely suggest that long forays across the landscape that occur by a small percentage of breeding frogs in coastal populations are less likely in dry inland locations where the threat of desiccation is much higher.

The closest known CNDDB record to the project site is a 2005 record approximately 1.3 miles east of the project site in a seasonal detention pond and golf course pond (CNDDB Occurrence No. 84). There is dense residential development between this detention pond and the project site, making it highly unlikely that California red-legged frog could successfully migrate overland to the project site over major roads and through solid wood-fenced backyards. Additionally, since there is no breeding habitat on or adjacent to the project site, or accessible from the project site, there would be no reason for California red-legged frog to reside on the project site.

Aquatic habitat on the project site is limited to a man-made flood control basin that was constructed over the top of a historic drainage. Water flows into this basin via culverts emanating from the adjacent development (Oak Creek) to the east and then quickly flushes out of the basin via an outlet culvert that directs flows north and under Enterprise Road. The basin maintains

positive flows, only catching by design very large storm events that would exceed the flow capacity of the 6-foot RCP exiting this basin. Water does not pool in this basin for any length of time and thus, it does not provide potential California red-legged frog breeding habitat. The basin only supported a shallow (< 3 inches deep) puddle for a short time in the winter of 2018-2019, after periods of heavy rain. Thus, it did not provide suitable aquatic habitat for California red-legged frog. West of this basin on the project site is a remnant portion of the historic drainage. This drainage historically flowed west to east, but no longer supports flows owing to the flood control basin constructed to catch all watershed flows upstream of the project site from within the Oak Creek Development. M&A never observed water in this drainage during the course of our 2019 site surveys. A detention area exists just south of the project site. This feature is surrounded by dense residential development and did not hold water in the winter of 2018-2019.

The only other aquatic habitat within the project site vicinity is a San Benito County maintained flood control basin on the north side of Enterprise Road. Similar to the flood control basin onsite, this basin was constructed to contain and slow flood waters before they are discharged into the surrounding landscape; thus, water is not detained for long-duration and aquatic conditions/habitat does not persist in this basin. This basin only supports upland vegetation (coyote brush, for example). This basin does not provide any indication that it retains water (no vegetation suppression, no aquatic vegetation such as cattails).

There are no other potential breeding ponds that are not separated from the project site by developed and/or intensively maintained and irrigated farmland. Due to an absence of suitable breeding habitats onsite and within the vicinity of the project site it can be concluded that the California red-legged frog would not reside onsite and therefore that the proposed project would not result in significant impacts to California red-legged frog. Thus, no mitigation for California red-legged frog is warranted for the proposed project.

#### 6.3.3 Western burrowing owl

The western burrowing owl is a California "species of special concern." Its nest, eggs, and young are also protected under California Fish and Game Code (§3503, §3503.5, and §3800). The burrowing owl is also protected from direct take under the Migratory Bird Treaty Act (50 CFR 10.13). Finally, based upon this species' rarity status, any unmitigated impacts to rare species would be considered a "significant effect on the environment" pursuant to §21068 of the CEQA Statutes and §15382 of the CEQA Guidelines. Thus, this owl species must be considered in any project that will, or is currently, undergoing CEQA review, and/or that must obtain an environmental permit(s) from a public agency. When these owls occur on project sites, typically mitigation requirements are mandated in the conditions of project approval from the CEQA lead agency.

Burrowing owl habitat is usually found in annual and perennial grasslands, characterized by low-growing vegetation. Often the burrowing owl utilizes rodent burrows, typically ground squirrel burrows, for nesting and cover. They may also on occasion dig their own burrows or use human-made objects such as concrete culverts or rip-rap piles for cover. They exhibit high site fidelity, reusing burrows year after year. Occupancy of suitable burrowing owl habitat can be verified at a site by observation of these owls during the spring and summer months or, alternatively, its molted feathers, cast pellets, prey remains, eggshell fragments, or excrement (white wash) at or

near a burrow. Burrowing owls typically are not observed in grasslands with tall vegetation or wooded areas because the vegetation obscures their ability to detect avian and terrestrial predators. Since burrowing owls spend the majority of their time sitting at the entrances of their burrows, grazed grasslands seem to be their preferred habitat because it allows them to view the world at 360 degrees without obstructions.

The closest known CNDDB record to the project site is a year 2000 record located approximately 1.7 miles northeast of the project site in grazed annual grassland (Occurrence No. 758). No burrowing owls were observed onsite by M&A biologists during field surveys conducted in January and April 2019. In addition, no burrowing owls were observed onsite during multiple field surveys conducted by M&A between January and September 2015. Nonetheless, the project site does provide habitat that could be used by western burrowing owls. Therefore, M&A recommends that a preconstruction survey be conducted within 14 days of any earth-moving/site work to determine if owls could have moved onto the project site in the intervening period between 2019 surveys and when the proposed project is implemented. If no burrowing owls are observed onsite during the preconstruction survey, no mitigation would be necessary. However, if owls are observed onsite during the nesting season, mitigation would need to be prescribed to offset any project-related impact to this species to a less than significant level. See the Impacts and Mitigations section for details.

## 6.3.4 SAN JOAQUIN KIT FOX

San Joaquin kit fox is a federally-listed endangered species and a California state-listed threatened species. This species' distribution is primarily limited to the San Joaquin Valley and adjacent regions. The San Joaquin kit fox (kit fox) is the smallest fox species in North America, typically weighing between four and six pounds. It has large ears, long legs, and is generally a buffy tan color with a black-tipped tail. Kit fox live primarily in the lowlands of the San Joaquin Valley of California but are also known to occur in several counties in the coast mountain ranges including Santa Barbara, San Luis Obispo, Monterey, San Benito, Santa Clara, and Alameda Counties.

This fox species is usually found in open grassland and shrubland communities but has also been observed in orchards that border grassland or shrubland plant communities. Kit fox are carnivorous, usually feeding on small rodents such as pocket mice (*Perognathus inornatus*), deer mice (*Peromyscus maniculatus*), western harvest mice (*Reithrodontomys megalotis*), kangaroo rats (*Dipodomys* spp.), and larger rodents such California ground squirrel. Kit fox also prey upon lagomorphs such as black-tailed hare (*Lepus californicus*) and desert cottontail (*Sylvilagus audubonii*). It relies on dens for breeding, and to provide escape cover from potential predators. Kit fox are reputedly poor diggers, so dens are excavated in loose-textured soils, generally in areas with low to moderate relief, or they will utilize holes left by other species. They will utilize burrows dug by rabbits, ground squirrels, and on occasion, American badgers. Man-made structures, such as well-casings, culverts, and abandoned pipelines, are also occasionally used for dens. Typically, dens are small enough to discourage easy predation by coyotes. Populations of kit fox are thought to be related to the availability of denning sites, particularly natal denning sites, which are often moved several times throughout the season.

In 1971, this species was recorded approximately 1.3 miles east of the project site (CNDDB Occurrence No. 1024). This is the most current, known record for kit fox to the project site. This

is an old record (~48 years old) and the record location is now densely developed with residential housing; this location is separated from the project site by this residential development. Regardless, there are open scrub/grasslands to the west of the project site associated with the San Benito River, and there are California ground squirrel burrows on the project site that provide unlikely, but suitable refugia for this fox. Thus, the presence of this fox could not be ruled out without conducting formal surveys.

In September 2015, M&A biologists, Mr. Monk and Ms. Lynch, conducted an abbreviated survey using methods provided in the USFWS' San Joaquin kit fox survey protocol (dated June 1999). This survey was conducted by two M&A biologists with many years of experience conducting protocol level kit fox surveys. These surveys included walking transects over the entire project site to identify potential dens (that is, burrows greater than 4 inches in diameter), establishing scent stations (track plates) at potential den sites, conducting nocturnal spotlight surveys, and establishing camera stations at "potential den" sites. The classification of a burrow as a "potential den" is not an acknowledgement that the kit fox could be using the burrow, only that the dimensions of the burrow is large enough for a kit fox to use, but not so large that kit fox predators such as the red fox or coyote would be able to easily dislodge a kit fox. Potential dens provide escape refugia for kit fox and can also be used for denning. The combination of survey methods used by M&A resulted in multiple observations/ detections of gray fox (*Urocyon cinereoargenteus*), domestic cat (*Felis cattus*), black-tailed jackrabbit, and California ground squirrel. No observations, photographs, tracks or scat of kit fox were made on or near the project site.

In January and April 2019, M&A biologists, Mr. Monk, Ms. Dulava, and Mr. Stratton, conducted abbreviated kit fox surveys on site. This abbreviated survey included systematic walking transects on the project site searching for potential dens. No potential dens or any evidence of kit fox were made on or near the project site. Hence, based on two years of negative survey results, it can be concluded that implementation of the proposed project is not expected to result in significant impacts to the San Joaquin kit fox. Therefore, mitigation for the San Joaquin kit fox is not warranted.

#### 6.3.5 Greater Western Mastiff Bat

Greater western mastiff-bat is a California "species of special concern." It has no special federal status. The "species of special concern" status designation does not provide any special legally mandated protection for this bat species. However, this status designation likely meets the definition of "rare" pursuant to the CEQA (14 CCR §15380(2)(A)). As such, potential impacts to this bat species should be considered during any CEQA review. Any unmitigated impacts to this species would likely be regarded by the State resource agency (the CDFW) as a significant adverse impact pursuant to CEQA (§21068).

The greater western mastiff bat is the largest bat species in the United States. It typically uses crevices in cliffs, high buildings, large trees, and tunnels for roosting. Roosts are generally high above ground in order to allow for a clear vertical drop of at least 10 feet for flight. This bat forages most frequently in open areas, including chaparral, open woodlands, grasslands, meadows, and agricultural areas. This species does not hibernate and is intermittently active during the winter.

This species was recorded in 1998 approximately 1.5 miles northwest from the project site (CNDDB Occurrence No. 242). The large trees and barn on the project site provide "suitable" habitat for this bat; therefore, the presence of this species cannot be dismissed without conducting formal surveys. See the Impacts and Mitigations section for details.

#### 6.3.6 WESTERN RED BAT

The western red bat is a California "species of special concern." It has no federal status. The "species of special concern" status designation does not provide any special legally mandated protection for this bat species. However, this status designation likely meets the definition of "rare" pursuant to the CEQA (14 CCR §15380(2)(A)). As such, potential impacts to this bat species should be considered during any CEQA review. Any unmitigated impacts to this species would likely be regarded by the State resource agency (the CDFW) as a significant adverse impact pursuant to CEQA (§21068).

The western red bat occurs in southern British Columbia, the western United States, Mexico, Central Mexico, and possibly South America (Cryan 2003; Pierson et al. 2006). Although the species has a wide range, relatively few records for the western red bat exist outside of California (Pierson et al. 2006). In California, most of the records are from the Central Valley, which is the breeding center for the western red bat in the state. About 83% of the breeding records for western red bat in California are from the Sacramento and San Joaquin rivers, with other breeding records from the San Diego, Santa Ana, and Los Angeles rivers (Pierson et al. 2006). It has been recorded in California every month of the year (Pierson et al. 2006).

The western red bat is closely associated with well-developed riparian habitats that provide suitable roosting sites. It roosts primarily in trees, 2 to 40 feet above the ground, from sea level up through mixed conifer forests. It prefers habitat edges and mosaics with trees that are protected from above and open below with open areas for foraging. In addition to riparian habitats, western red bats have been observed in orchard trees, including fig (*Ficus carica*), apricot (*Prunus armeniaca*), peach (*Prunus persica*), pear (*Pyrus communis*), almond (*Prunus amygdalus*), walnut (*Juglans regia*), and orange trees (*Citrus sinensis*) (Benson 1945, as cited in Pierson et al. 2006; Constantine 1959; Grinnell 1918, as cited in Pierson et al. 2006; Pierson et al. 2006). They have also been observed to use other non-native trees, including African hemp (*Sparmannia africana*), eucalyptus (*Eucalyptus* spp.), Chinaberry (*Melia azedarach*), mulberry (*Morus rubra*), and tamarisk (*Tamarix* spp.) (Constantine 1959; Dalquest, as cited in Pierson et al. 2006).

This closest record for this species is located within the general vicinity of the project site (CNDDB Occurrence No. 83); the exact location of this record is actually unknown. It is a 1998 record mapped "in the general vicinity of Hollister." The large trees on the project site provide "suitable" habitat for this bat; therefore, the presence of this species cannot be dismissed without conducting formal surveys. See the Impacts and Mitigations section for details.

## 7. REGULATORY FRAMEWORK FOR NATIVE WILDLIFE, FISH, AND PLANTS

This section provides a discussion of those laws and regulations that are in place to protect native wildlife, fish, and plants. Under each law we discuss its relevance to the proposed project.

# 7.1 Federal Endangered Species Act

The FESA forms the basis for the federal protection of threatened or endangered plants, insects, fish and wildlife. FESA contains four main elements, they are as follows:

Section 4 (16 USCA §1533): Species listing, Critical Habitat Designation, and Recovery Planning: outlines the procedure for listing endangered plants and wildlife.

Section 7 (§1536): Federal Consultation Requirement: imposes limits on the actions of federal agencies that might impact listed species.

Section 9 (§1538): Prohibition on Take: prohibits the "taking" of a listed species by anyone, including private individuals, and State and local agencies.

Section 10: Exceptions to the Take Prohibition: non-federal agencies can obtain an incidental take permit through approval of a Habitat Conservation Plan.

In the case of salt water fish and other marine organisms, the requirements of FESA are enforced by the National Marine Fisheries Service (NMFS). The USFWS enforces all other cases. Below, Sections 9, 7, and 10 of FESA are discussed since they are the sections most relevant to the proposed project.

Section 9 of FESA as amended, prohibits the "take" of any fish or wildlife species listed under FESA as endangered. Under Federal regulation, "take" of fish or wildlife species listed as threatened is also prohibited unless otherwise specifically authorized by regulation. "Take," as defined by FESA, means "to harass, harm, pursue, hunt, shoot, wound, kill, trap, capture, or collect, or to attempt to engage in any such conduct." "Harm" includes not only the direct taking of a species itself, but the destruction or modification of the species' habitat resulting in the potential injury of the species. As such, "harm" is further defined to mean "an act which actually kills or injures wildlife; such an act may include significant habitat modification or degradation where it actually kills or injures wildlife by significantly impairing essential behavioral patterns, including breeding, feeding or sheltering" (50 CFR 17.3). A December 2001 decision by the 9th Circuit Court of Appeals (Arizona Cattle Growers' Association, Jeff Menges, vs. the USFWS and Bureau of Land Management, and the Southwest Center for Biological Diversity) ruled that the USFWS must show that a threatened or endangered species is present on a project site and that it would be taken by the project activities. According to this ruling, the USFWS can no longer require mitigation based on the probability that the species could use the site. Rather they must show that it is "reasonably certain to occur."

Section 9 applies to any person, corporation, federal agency, or any local or State agency. If "take" of a listed species (other than a plant species) is necessary to complete an otherwise lawful activity, this triggers the need to obtain an "incidental take permit" either through a Section 7

Consultation as discussed further below (for federal actions or private actions that are permitted or funded by a federal agency such as the Corps), or through Section 10 of FESA which requires preparation of a Habitat Conservation Plan (HCP) (for state and local agencies, or individuals, and projects without a federal "nexus"; for example, projects that do not need a Corps permit).

Section 7(a)(2) of the Act requires that each federal agency consult with the USFWS to ensure that any action authorized, funded or carried out by such agency is not likely to jeopardize the continued existence of an endangered or threatened species or result in the destruction or adverse modification of critical habitat for listed species. Critical habitat designations mean: (1) specific areas within a geographic region currently occupied by a listed species, on which are found those physical or biological features that are essential to the conservation of a listed species and that may require special management considerations or protection; and (2) specific areas outside the geographical area occupied by a listed species that are determined essential for the conservation of the species.

The Section 7 consultation process only applies to actions taken by federal agencies that are considering authorizing discretionary projects. Section 7 is by and between the NMFS and/or the USFWS and the federal agency contemplating a discretionary approval (that is, the federal "action agency," for example, the Corps or the Federal Highway Administration). Private parties, cities, counties, etc. (i.e., applicants) may participate in the Section 7 consultation at the discretion of the federal agencies conducting the Section 7 consultation. The Section 7 consultation process is triggered by a determination of the "action agency" – that is, the federal agency that is carrying out, funding, or approving a project - that the project "may affect" a listed species or critical habitat. If an action is likely to adversely affect a listed species or designated critical habitat, formal consultation between the nexus agency and the USFWS/NMFS is required. As part of the formal consultation, the USFWS/NMFS may resolve any issues informally with the nexus agency or may prepare a formal Biological Opinion assessing whether the proposed action would be likely to result in "jeopardy" to a listed species or if it could adversely modify designated critical habitat. If the USFWS/NMFS prepares a Biological Opinion, it will contain either a "jeopardy" or "non-jeopardy" decision. If the USFWS/NMFS concludes that a proposed project would result in adverse modification of critical habitat or would jeopardize the continued existence of a federally-listed species (that is, it will issue a jeopardy decision), the nexus federal agency would be most unlikely to authorize its discretionary permit. If the USFWS/NMFS prepares a "non-jeopardy" Biological Opinion, the nexus federal agency may authorize the discretionary permit making all conditions of the Biological Opinion conditions of its discretionary permit. A non-jeopardy Biological Opinion constitutes an "incidental take" permit that allows applicants to "take" federally-listed species while otherwise carrying out legally sanctioned projects.

For non-federal entities, for example private parties, cities, and counties that are proposing a project that might result in incidental take, Section 10 provides the mechanism for obtaining that take authorization. Under Section 10 of FESA, for the applicant to obtain an "incidental take permit," the applicant is required to submit a "conservation plan" to the USFWS or NMFS that specifies the impacts that are likely to result to federally-listed species, and the measures the applicant will undertake to minimize and mitigate such impacts, and the funding that will be available to implement those steps. Conservation plans under FESA have come to be known as

"habitat conservation plans" or "HCPs" for short. The terms incidental take permit, Section 10 permit, and Section 10(a)(1)(B) permit are used interchangeably by the USFWS. Section 10(a)(2)(B) of FESA provides statutory criteria that must be satisfied before an incidental take permit can be issued.

#### 7.1.1 RESPONSIBLE AGENCY

FESA gives regulatory authority to the USFWS for federally-listed terrestrial species and non-anadromous fish. The NMFS has regulatory authority over federally-listed marine mammals and anadromous fish.

#### 7.1.2 APPLICABILITY TO THE PROPOSED PROJECT

The project site does not provide habitat for any federally-listed fish, plant or wildlife species. CNDDB records for three federally-listed species (San Joaquin kit fox, California tiger salamander, and California red-legged frog) exist within 3 miles of the project site. These species were addressed in further research and field surveys. Abbreviated protocol level surveys for the San Joaquin kit fox were conducted onsite in 2015, using all detection methods necessary to identify the San Joaquin kit fox should it be present in the area. Further surveys were conducted in 2019. No kit fox were observed on or adjacent to the project site during nocturnal spotlighting surveys, track plate study, and camera stations surveys in 2015. No sign of kit fox or potential dens were observed during 2019 surveys. The project would not impact the San Joaquin kit fox and authorization pursuant to the FESA would not be necessary. Similarly, the project site does not provide breeding habitat for California tiger salamander or California red-legged frog and there are no accessible California tiger salamander or California red-legged frog breeding habitats within 1.3 miles of the project site. Hence, the project site does not provide upland oversummering habitat or breeding habitat. Impacts to California tiger salamander and California red-legged frog from project implementation are not anticipated and authorization pursuant to the FESA would not be necessary. Protocol level special-status plant surveys were conducted on the project site in the spring and summer of 2015; no federally-listed plants were identified onsite during these appropriately timed surveys. Similarly, during January and April 2019 site surveys, no federally-listed plants were identified on the project site.

### 7.2 Federal Migratory Bird Treaty Act

The Migratory Bird Treaty Act of 1918 (16 U.S.C. §§ 703-712, July 3, 1918, as amended 1936, 1960, 1968, 1969, 1974, 1978, 1986 and 1989) makes it unlawful to "take" (kill, harm, harass, shoot, etc.) any migratory bird listed in Title 50 of the Code of Federal Regulations, Section 10.13, including their nests, eggs, or young. Migratory birds include geese, ducks, shorebirds, raptors, songbirds, wading birds, seabirds, and passerine birds (such as warblers, flycatchers, swallows, etc.).

Executive Order 13186 for conservation of migratory birds (January 11, 2001) requires that any project with federal involvement address impacts of federal actions on migratory birds. The order is designed to assist federal agencies in their efforts to comply with the Migratory Bird Treaty Act and does not constitute any legal authorization to take migratory birds. The order also requires federal agencies to work with the USFWS to develop a memorandum of understanding

(MOU). Protocols developed under the MOU must promote the conservation of migratory bird populations through the following means:

- avoid and minimize, to the extent practicable, adverse impacts on migratory bird resources when conducting agency actions;
- restore and enhance habitat of migratory birds, as practicable; and prevent or abate the pollution or detrimental alteration of the environment for the benefit of migratory birds, as practicable.

In 2017, the Solicitor for the USFWS opined that the Migratory Bird Treaty Act only prohibits intentional take of bird species listed under the Act and does not prohibit unintentional take incidental to otherwise lawful activities. Accordingly, it is unlikely that development of the project would implicate the take prohibitions under the Migratory Bird Treaty Act. As of March 2019, however, the California Legislature was considering a bill (AB 454) that would make illegal, in California, the incidental take of bird species listed under the Act. The State's protections for avian species are more fully described in the California Fish and Game Code Section below.

#### 7.2.1 APPLICABILITY TO THE PROPOSED PROJECT

White-tailed kite (*Elanus leucurus*), red-tailed hawk, and red-shouldered hawk could nest on the project site. In 2015, a pair of red-tailed hawks nested in a large tree adjacent to the project site; while these hawks were not observed nesting in 2019, trees on and near the project site provide suitable nesting habitat and these birds may nest in the vicinity in subsequent years. These raptors (birds of prey) would be protected by the Migratory Bird Treaty Act. Also, the common songbirds that could occur on the site would be protected pursuant to this Act. As long as there is no direct mortality of species protected pursuant to this Act caused by development of the site, there should be no constraints to development of the site. To comply with the Migratory Bird Treaty Act, all active nest sites would have to be avoided while such birds were nesting. Upon completion of nesting, the project could commence as otherwise planned. Please review specific requirements for avoidance of nest sites for potentially occurring species in the Impacts and Mitigations section below.

## 7.3 California Endangered Species Act

#### 7.3.1 SECTION 2081 OF THE CALIFORNIA ENDANGERED SPECIES ACT

In 1984, the state legislated the CESA (Fish and Game Code §2050). The basic policy of CESA is to conserve and enhance endangered species and their habitats. State agencies will not approve private or public projects under their jurisdiction that would impact threatened or endangered species if reasonable and prudent alternatives are available. Because CESA does not have a provision for "harm" (see discussion of FESA, above), CDFW considerations pursuant to CESA are limited to those actions that would result in the direct take of a listed species.

If CDFW determines that a proposed project could impact a state-listed threatened or endangered species, CDFW will provide recommendations for "reasonable and prudent" project alternatives. The CEQA lead agency can only approve a project if these alternatives are implemented, unless it finds that the project's benefits clearly outweigh the costs, reasonable mitigation measures are adopted, there has been no "irreversible or irretrievable" commitment of resources made in the

interim, and the resulting project would not result in the extinction of the species. In addition, if there would be impacts to threatened or endangered species, the lead agency typically requires project applicants to demonstrate that they have acquired "incidental take" permits from CDFW and/or USFWS (if it is a federally-listed species) prior to allowing/permitting impacts to such species.

If proposed projects would result in impacts to a state-listed species, an "incidental take" permit pursuant to §2081 of the Fish and Game Code would be necessary (versus a federal incidental take permit for federally-listed species). CDFW will issue an incidental take permit only if:

- 1) The authorized take is incidental to an otherwise lawful activity;
- 2) the impacts of the authorized take are minimized and fully mitigated;
- 3) measures required to minimize and fully mitigate the impacts of the authorized take:
  - a) are roughly proportional in extent to the impact of the taking on the species;
  - b) maintain the project applicant's objectives to the greatest extent possible; and,
  - c) capable of successful implementation; and,
- 4) adequate funding is provided to implement the required minimization and mitigation measures and to monitor compliance with, and the effectiveness of, the measures.

If an applicant is preparing a HCP as part of the federal 10(a) permit process, the HCP might be incorporated into the §2081 permit if it meets the substantive criteria of §2081(b). To ensure that an HCP meets the mitigation and monitoring standards in Section 2081(b), an applicant should involve CDFW staff in development of the HCP. If a final Biological Opinion (federal action) has been issued for the project pursuant to Section 7 of the FESA, it might also be incorporated into the §2081 permit if it meets the standards of §2081(b).

No §2081 permit may authorize the take of a species for which the Legislature has imposed strict prohibitions on all forms of "take." These species are listed in several statutes that identify "fully protected" species and "specified birds." *See* Fish and Game Code §§ 3505, 3511, 4700, 5050, 5515, and 5517. If a project is planned in an area where a "fully protected" species or a "specified bird" occurs, an applicant must design the project to avoid all take.

Fish and Game Code §2080.1 allows an applicant who has obtained a "non-jeopardy" federal Biological Opinion pursuant to Section 7 of the FESA, or who has received a federal 10(a) permit (federal incidental take permit) pursuant to the FESA, to submit the federal opinion or permit to CDFW for a determination as to whether the federal document is "consistent" with CESA. If after 30 days CDFW determines that the federal incidental take permit is consistent with state law, and that all state-listed species under consideration have been considered in the federal Biological Opinion, then no further permit or consultation is required under CESA for the project. However, if CDFW determines that the federal opinion or permit is not consistent with CESA, or that there are state-listed species that were not considered in the federal Biological Opinion, then the applicant must apply for a state CESA permit under Section 2081(b). Section 2081(b) is of no use if an affected species is state-listed, but not federally-listed.

State and federal incidental take permits are issued on a discretionary basis and are typically only authorized if applicants are able to demonstrate that impacts to the listed species in question are

unavoidable and can be mitigated to an extent that the reviewing agency can conclude that the proposed impacts would not jeopardize the continued existence of the listed species under review. Typically, if there would be impacts to a listed species, mitigation that includes habitat avoidance, preservation, and creation of endangered species habitat is necessary to demonstrate that projects would not threaten the continued existence of a species. In addition, management endowment fees are usually collected as part of the agreement for the incidental take permit(s). The endowment is used to manage any lands set-aside to protect listed species, and for biological mitigation monitoring of these lands over (typically) a five-year period.

#### 7.3.2 APPLICABILITY TO THE PROPOSED PROJECT

No state-listed plant or animal species would likely be impacted by the proposed project (Tables 3 and 4, respectively). The project site does not provide habitat for any state-listed fish, plant or wildlife species. A record search of the CNDDB identified a historical record of San Joaquin kit fox within 1.3 miles of the project site. That record is approximately 48 years old and the record location is now under high-density residential development. In 2015, a formal San Joaquin kit fox survey was conducted on the project site to corroborate M&A's initial assessment that this fox was cut off from migration to/from the project site by residential development and intensively farmed areas, and thus would not occur on the project site (See San Joaquin kit fox species discussion above). M&A's surveys used all detection methods necessary to identify the San Joaquin kit fox should it be present in the area. No kit fox were observed on or adjacent to the project site during nocturnal spotlighting surveys, track plate studies, and camera station surveys. M&A biologists found no evidence of kit fox or potential dens during 2019 surveys. 2019 surveys identified a small California ground squirrel colony on the project site but no burrows with dimensions that constitute "potential" San Joaquin kit fox dens. M&A's findings were that the San Joaquin kit fox does not occur on the project site and would not be expected to occur on the project site. Accordingly, the project would not impact the San Joaquin kit fox. Thus, a CESA authorization is not required for the proposed project.

M&A reached a similar conclusion for the state-listed California tiger salamander. The project site does not provide breeding habitat for California tiger salamander and there are no accessible California tiger salamander breeding habitats within 1.3 miles of the project site. Dense development and/or intensively managed and irrigated agricultural lands occurs between all record locations and the project site. Hence, the project site does not provide over-summering habitat either and impacts to California tiger salamander from project implementation are not anticipated and authorization pursuant to the CESA is therefore not required.

Protocol-level special-status plant surveys were conducted on the project site in the spring and summer of 2015; no state-listed plants were identified onsite during these appropriately timed surveys. No special-status plants were observed during 2019 field surveys. Thus, the project would not impact plants protected pursuant to the CESA.

#### 7.4 California Fish and Game Code § 3503, 3503.5, 3511, and 3513

California Fish and Game Code §3503, 3503.5, 3511, and 3513 prohibit the "take, possession, or destruction of birds, their nests or eggs." Disturbance that causes nest abandonment and/or loss

of reproductive effort (killing or abandonment of eggs or young) is considered "take." Such a take would also violate federal law protecting migratory birds (Migratory Bird Treaty Act).

All raptors (that is, hawks, eagles, owls) their nests, eggs, and young are protected under California Fish and Game Code (§3503.5). Additionally, "fully protected" birds, such as the white-tailed kite and golden eagle (*Aquila chrysaetos*), are protected under California Fish and Game Code (§3511). "Fully protected" birds may not be taken or possessed (that is, kept in captivity) at any time.

#### 7.4.1 APPLICABILITY TO THE PROPOSED PROJECT

Raptors that could be impacted by the project include white-tailed kite, red-tailed hawk, and red-shouldered hawk. Preconstruction surveys would have to be conducted for these species to ensure that there is no direct take of these birds including their eggs, or young. Similarly, a survey for nesting passerine birds must be conducted. Any active nests that were found during preconstruction surveys would have to be avoided by the project. Suitable non-disturbance buffers would have to be established around nest sites until the nesting cycle is complete. More specifics on the size of buffers are provided below in the Impacts and Mitigations section.

# 7.5 San Benito County General Plan

San Benito County's 2035 General Plan, adopted by the Board of Supervisors on July 21, 2015, includes a Natural and Cultural Resources Element. This Element provides goals and policies that the County will follow when approving new developments to ensure that significant and sensitive natural and cultural resources within San Benito County are protected to the greatest extent possible. Below we present the Natural Resources goals that pertain to the project site.

## Natural and Cultural Resources Element: Open Space

**Goal NCR-1.** To preserve and enhance valuable open space lands that provide wildlife habitat and conserve natural, historical, archaeological, paleontological, tribal, and visual resources of San Benito County.

## NCR-1.1 Maintenance of Open Space

The County shall support and encourage maintenance of open space lands that support natural resources, agricultural resources, recreation, tribal resources, wildlife habitat, water management, scenic quality, and other beneficial uses.

## NCR-1.2 Conservation Easements

The County shall support and encourage the use of conservation easements to protect open space that contains valuable natural resources.

## NCR-1.3 Open Space Overlay District

The County shall continue to protect and preserve the rural landscape and implement open space policies for: public health, safety, and welfare; continued agricultural uses; scenic viewscape preservation, including scenic highway corridors; park and recreation uses; conservation of

significant natural resources; the containment and definition of limits to urbanization; and the preservation of the natural habitat for threatened and/or endangered plant and animal species.

#### 7.5.1 APPLICABILITY TO THE PROPOSED PROJECT

The project site is located adjacent to medium-density residential development; hence, development of the project site would be a continuation of residential development in this area. Due to decades of agricultural use, the project site does not provide native plant habitats (other than a few native oak trees), nor does it support special-status animal or plant habitats. In recent years the project site has been used for hay farming and livestock grazing, with goats most recently grazing the site. Since development of the project site would not impact any significant or valuable natural resources, site development should not necessitate conservation easements or open space dedication.

#### Natural and Cultural Resources Element: Wildlife Habitat

**Goal NCR-2.** To protect and enhance wildlife communities through a comprehensive approach that conserves, maintains, and restores important habitat areas.

## NCR-2.1 Coordination for Habitat Preservation

The County shall work with property owners and Federal and State agencies to identify feasible and economically-viable methods of protecting and enhancing natural habitats and biological resources in the county.

#### NCR-2.2 Habitat Protection

The County shall require major subdivisions within potential habitat of federal- or state-listed rare, threatened, or endangered plant or animal species to mitigate the effects of development. Mitigation for impacts to species may be accomplished on land preserved for open space, agricultural, or natural resources protection purposes.

## NCR-2.3 Habitat Conservation Plan

The County shall consider working with federal and state agencies to develop and adopt an HCP and a Natural Community Conservation Plan (NCCP) for listed and candidate species in San Benito County in order to manage their habitats and ensure their long-term protection.

## NCR-2.4 Maintain Corridors for Habitat

The County shall protect and enhance wildlife migration and movement corridors to ensure the health and long-term survival of local animal and plant populations, in particular contiguous habitat areas, in order to increase habitat value and lower land management costs. As part of this effort, the County shall require road and development sites in rural areas to:

- a. Be designed to maintain habitat connectivity with a system of corridors for wildlife or plant species and avoiding fragmentation of open space areas; and
- b. Incorporate measures to maintain the long-term health of the plant and animal

Communities in the area, such as buffers, consolidation of/or rerouting access, transitional landscaping, linking nearby open space areas, and habitat corridors.

# NCR-2.5 Mitigation for Wetland Disturbance or Removal

The County shall encourage the protection of the habitat value and biological functions of oak woodlands, native grasslands, riparian and aquatic resources, and vernal pools and wetlands. The County shall require that development avoid encroachment and require buffers around these habitats to the extent practicable. The County shall further require mitigation for any development proposals that have the potential to reduce these habitats. Recreational trails and other features established within natural wetlands and aquatic and riparian buffer areas shall be, as long as such areas are not required to meet the Americans with Disabilities Act, located along the outside of the sensitive habitat whenever possible to minimize intrusions and maintain the integrity of the habitat. Exceptions to this action include irrigation pumps, roads and bridges, levees, docks, public boat ramps, and similar uses. In all cases where intrusions into these buffers are made, only the minimum amount of vegetation necessary to construct the feature shall be removed.

#### NCR-2.8 Pre-Development Biological Resource Assessment

The County shall require the preparation of biological resource assessments for new development proposals as appropriate. The assessment shall include the following: a biological resource inventory based on a reconnaissance-level site survey, and an analysis of anticipated project impacts to: potentially occurring special-status species (which may require focused special-status plant and/or animal surveys); an analysis of sensitive natural communities; wildlife movement corridors and nursery sites on or adjacent to the project site; potentially jurisdictional wetlands/waterways; and locally protected biological resources such as trees. The assessment shall contain suggested avoidance, minimization, and/or mitigation measures for significant impacts to biological resources.

## NCR-2.9 Mitigation Funding and Site Protection

The County shall require that project applicants demonstrate that adequate funding can be provided to implement all required biological mitigation and monitoring activities. Habitat preserved as part of any mitigation and monitoring plan shall be preserved through a conservation easement, deed restriction, or other method to ensure that the habitat remains protected.

# NCR- 2.10 Invasive Species

The County shall require that new developments avoids the introduction or spread of invasive plant species during construction by minimizing surface disturbance, seeding and mulching disturbed areas with certified weed-free native mixes, and using native or noninvasive species in erosion control plantings.

#### 7.5.2 APPLICABILITY TO THE PROPOSED PROJECT

This report serves as the pre-development biological resources assessment required by the County pursuant to NCR-2.8. The project site does not support any special-status species or their habitats. Similarly, there are no native or significant habitats onsite, specifically, there are no riparian habitats or oak woodlands onsite. The project site can be classified as an anthropogenic (man-altered) community. Thus, it should not be necessary to prepare an HCP or NCCP for this project site. Numerous wildlife and botanical surveys have been conducted onsite and have not identified any special-status species. Hence, mitigation for project-related impacts to specialstatus species is not warranted. Similarly, the only agency regulated "waters" present on the project site are a man-made flood control basin that intercepted a natural drainage channel that at one time, long ago, flowed through the project site. This basin does not provide native wildlife, plant, or special-status species habitat; regardless, mitigation for impacts to these waters would likely be imposed by the Corps if the water quality basin would be impacted by the proposed project. Prior to impacting these features and implementing any required mitigation, the project applicant will submit proof to the County of San Benito that applicable agency permits have been obtained (e.g., a Corps permit and a RWQCB permit) and that adequate funding is available for any required mitigation. Finally, any revegetation or hydroseed mix used on barren soils onsite as part of the proposed development would not include invasive species in the seed mix and necessary precautions will be in place during site grading, development and landscaping to ensure that invasive species are not introduced.

## 7.6 San Benito County Management and Conservation of Woodlands

In the San Benito County Code of Ordinances, Title 19, Land Use and Environmental Regulations, there is a chapter that discusses the management and conservation of woodlands. This chapter, Chapter 19.33, pertains to rural zoned properties such as the project site which is zoned R/PUD (that is, Rural/Planned Use Development). The purpose of this chapter is to establish regulations for the conservation and protection of woodlands in the unincorporated areas of San Benito County by limiting tree removal in a manner which allows for reasonable use and enjoyment of the property. A discretionary permit shall be required for the removal of woodlands when: (A) The removal of individual and or masses of trees within woodlands of between 90% and 100% as per the canopy retention standard in Table 19.33.007(1) (below) within a period of ten years; or (B) Any tree removal is located on slopes greater than or equal to 30%. (1966 Code, § 33-5) (Ord. 757, § 1(part)).

(A) <u>Table 19.33.007(1)</u> shall be used to determine the minimum amounts of woodland canopy that must be retained during site modification or maintenance on any parcel:

| Table 19.33.007(1) Canopy Retention Standard                            |  |
|---|--|
| Canopy Retention Standard Shall Be the Greater of Column a or Column B: |  |
| Baseline Canopy Cover (1)<br>Column A (2)                               | Column B (2)                                 |
| 80-100%   | .75 x baseline canopy cover 65% canopy cover |
| 60-79%  | .80 x baseline canopy cover 51% canopy cover |

| 40-59%      | .85 x baseline canopy cover 36% canopy cover |
|-------------|--|
| 20-39%      | .90 x baseline canopy cover 19% canopy cover |
| 19% or less | 1.0 x baseline canopy cover                  |

- (B) Individual trees and or massed individual trees shall be included in the calculation of canopy retention standard. Example: For 50% baseline canopy, the minimum allowable canopy after modification and maintenance would be the greater of Column A, (0.85 times 50% equals 42.5% canopy) or Column B, (36% canopy). In this example, the minimum allowable canopy after modification and maintenance would be 42.5%. Pursuant to §19.33.005, if the canopy is located on a slope of 30% or greater the canopy retention area (the percentage of removal of individual and/or masses of woodland trees is equal to the baseline percentage of the canopy retention percentage in this table subtracted from 100%) must be increased by a factor of 50%.
- (C) Canopy retention standard shall be applied to retain undisturbed woodlands as a priority over retention of individual trees. No more than 10% of the canopy retention standard may be met by individual trees not included within designated woodlands (1966 Code, § 33-7) (Ord. 757, § 1(part)).

#### 7.6.1 APPLICABILITY TO THE PROPOSED PROJECT

Since the project site currently supports less than 19% canopy cover, in order to meet the County's "Canopy Retention Standards" it would be necessary to retain 100% of the native trees onsite. Native trees onsite are the oak trees, buckeye trees, and according to San Benito County's native tree list, pepper trees (*Schinus molle*) are considered "native" trees. If retention of 100% of the native trees onsite is not practical, it would be necessary to obtain a discretionary permit from the County prior to tree removal. The County may require replacement planting for tree removal.

# 8. REGULATORY REQUIREMENTS PERTAINING TO WATERS OF THE UNITED STATES AND STATE

This section presents an overview of the criteria used by the Corps, the RWQCB, the State Water Resources Control Board (SWRCB), and the CDFW to determine those areas within a project area that would be subject to their regulation.

# 8.1 U.S. Army Corps of Engineers Jurisdiction and Permitting

#### 8.1.1 SECTION 404 OF THE CLEAN WATER ACT

Congress enacted the Clean Water Act "to restore and maintain the chemical, physical, and biological integrity of the Nation's waters" (33 U.S.C. §1251(a)). Pursuant to Section 404 of the Clean Water Act (33 U.S.C. 1344), the Corps regulates the disposal of dredged or fill material into "waters of the United States" (33 CFR Parts 328 through 330). This requires project applicants to obtain authorization from the Corps prior to discharging dredged or fill materials into any water of the United States.

In the Federal Register "waters of the United States" are defined as, "...all interstate waters including interstate wetlands...intrastate lakes, rivers, streams (including intermittent streams), wetlands, [and] natural ponds, the use, degradation or destruction of which could affect interstate or foreign commerce..." (33 CFR Section 328.3).

# Limits of Corps' jurisdiction:

- (a) Territorial Seas. The limit of jurisdiction in the territorial seas is measured from the baseline in a seaward direction a distance of three nautical miles. (See 33 CFR 329.12)
- (b) Tidal Waters of the United States. The landward limits of jurisdiction in tidal waters:
  - (1) Extends to the high tide line, or
  - (2) When adjacent non-tidal waters of the United States are present, the jurisdiction extends to the limits identified in paragraph (c) of this section.
- (c) Non-Tidal Waters of the United States. The limits of jurisdiction in non-tidal waters:
  - (1) In the absence of adjacent wetlands, the jurisdiction extends to the ordinary high water mark, or
  - (2) When adjacent wetlands are present, the jurisdiction extends beyond the ordinary high water mark to the limit of the adjacent wetlands.
  - (3) When the water of the United States consists only of wetlands the jurisdiction extends to the limit of the wetland.

Section 404 jurisdiction in "other waters" such as lakes, ponds, and streams, extends to the upward limit of the OHWM or the upward extent of any adjacent wetland. The OHWM on a non-tidal water is:

• the "line on shore established by the fluctuations of water and indicated by physical characteristics such as a clear natural line impressed on the bank; shelving; changes in the character of soil; destruction of terrestrial vegetation; the presence of litter or debris; or other appropriate means that consider the characteristics of the surrounding areas" (33 CFR Section 328.3[e]).

Wetlands are defined as: "...those areas that are inundated or saturated by surface or ground water at a frequency and duration to support a prevalence of vegetation adapted for life in saturated soil conditions" (33 CFR Section 328.8 [b]). Wetlands usually must possess hydrophytic vegetation (i.e., plants adapted to inundated or saturated conditions), wetland hydrology (e.g., topographic low areas, exposed water tables, stream channels), and hydric soils (i.e., soils that are periodically or permanently saturated, inundated or flooded) to be regulated by the Corps pursuant to Section 404 of the Clean Water Act.

#### 8.1.1.1 Clean Water Rule 2015

In 2015, the Environmental Protection Agency (EPA) and the Corps published the Clean Water Rule: Definition of "Waters of the United States"; Final Rule which defines the scope of waters

protected under the Clean Water Act. This Final Rule was published in light of the statute, science, Supreme Court decisions in *U.S.* v. *Riverside Bayview Homes, Solid Waste Agency of Northern Cook County* v. *U.S. Army Corps of Engineers (SWANCC)*, and *Rapanos* v. *United States (Rapanos)*, and the agencies' experience and technical expertise. The Clean Water Rule reflects consideration of the extensive public comments received on the proposed rule. The Clean Water Rule was stayed in federal court shortly after it was adopted in 2015. In August 2018, the stay was lifted and the Clean Water Rule (Rule) became effective once again and remains in effect today. The Rule ensures protection for the nation's public health and aquatic resources and increases Clean Water Act program predictability and consistency by clarifying the scope of "waters of the United States" protected under the Act.

The Rule only protects waters that have been historically covered by the Clean Water Act. A tributary, or upstream water, must show physical features of flowing water – a bed, bank, and ordinary high-water mark – to warrant protection. The Rule provides protection for headwaters that have these features and have a significant connection to downstream waters. Adjacent waters are defined by three qualifying circumstances established by the Rule. These can include wetlands, ponds, impoundments, and lakes which can impact the chemical, biological or physical integrity of neighboring waters. All existing exclusions from longstanding agency practices are officially established for the first time. Waters used in normal agricultural, ranching, or silvicultural activities, as well as certain defined ditches, prior converted cropland, and waste treatment systems continue to be excluded from Clean Water Act protection.

# 8.1.1.2 Permitting Corps Jurisdictional Areas

To remain in compliance with Section 404 of the Clean Water Act, project proponents and property owners (applicants) are required to be permitted by the Corps prior to discharging or otherwise impacting waters of the United States. In many cases, the Corps must visit a proposed project area (to conduct a "jurisdictional determination") to confirm the extent of area falling under their jurisdiction prior to authorizing any permit for that project area. Typically, at the time the jurisdictional determination is conducted, applicants (or their representative) will discuss the appropriate permit application that would be filed with the Corps for permitting the proposed impact(s) to "waters of the United States."

Pursuant to Section 404, the Corps normally provides two alternatives for permitting impacts to the type of waters of the United States found in the project area. The first alternative would be to use Nationwide Permit(s) (NWP). The second alternative is to apply to the Corps for an Individual Permit (33 CFR Section 235.5(2)(b)). The application process for Individual Permits is extensive and includes public interest review procedures (i.e., public notice and receipt of public comments) and must contain an "alternatives analysis" that is prepared pursuant to Section 404(b) of the Clean Water Act (33 U.S.C. 1344(b)). The alternatives analysis is also typically reviewed by the federal EPA and thus brings another resource agency into the permitting framework. Both the Corps and EPA take the initial viewpoint that there are practical alternatives to the proposed project if there would be impacts to waters of the United States, and the proposed permitted action is not a water dependent project (e.g., a pier or a dredging project). Alternative analyses therefore must provide convincing reasons that the proposed permitted

impacts are unavoidable. Individual Permits may be available for use in the event that discharges into regulated waters fail to meet conditions of NWP(s).

NWPs are a type of general permit administered by the Corps and issued on a nationwide basis that authorize minor activities that affect Corps regulated waters. Under NWP, if certain conditions are met, the specified activities can take place without the need for an individual or regional permit from the Corps (33 CFR, Section 235.5[c][2]). In order to use NWP(s), a project must meet 27 general nationwide permit conditions, and all specific conditions pertaining to the NWP being used (as presented at 33 CFR Section 330, Appendices A and C). It is also important to note that pursuant to 33 CFR Section 330.4(e), there may be special regional conditions or modifications to NWPs that could have relevance to individual proposed projects. Finally, pursuant to 33 CFR Section 330.6(a), Nationwide permittees may, and in some cases must, request from the Corps confirmation that an activity complies with the terms and conditions of the NWP intended for use (*i.e.*, must receive "verification" from the Corps).

Prior to finalizing design plans, the applicant needs to be aware that the Corps maintains a policy of "no net loss" of wetlands (waters of the United States) from project area development. Therefore, it is incumbent upon applicants that propose to impact Corps regulated areas to submit a mitigation plan that demonstrates that impacted regulated areas would be recreated (*i.e.*, impacts would be mitigated). Typically, the Corps requires mitigation to be "in-kind" (i.e., seasonal wetlands would be filled, mitigation would include seasonal wetland mitigation), and at a minimum of a 1:1 replacement ratio (i.e., one acre or fraction there of recreated for each acre or fraction thereof lost). Often a 2:1 replacement ratio is required if the Permittee is responsible for the mitigation. In some cases, the Corps allows "out-of-kind" mitigation if the compensation site has greater value than the impacted site. Finally, there are many Corps approved wetland mitigation banks where wetland mitigation credits can be purchased by applicants to meet mitigation compensation requirements. Mitigation banks have defined service areas and the Corps may only allow their use when a project would have minimal impacts to wetlands.

#### 8.1.2 APPLICABILITY TO THE PROPOSED PROJECT

On September 22, 2015, M&A biologists conducted a formal wetland delineation on the project site. M&A mapped areas within a flood control basin in the northeastern portion of the project site as potential "other waters of the United States" (see Sheet 1, OW 1 through OW 6). The flood control basin was constructed to intercept a blue line tributary that historically occurred under what is now the Oak Manor development immediately east of the project site. An extension of the blue line drainage now courses through the flood control basin and where a flow pattern is apparent, it was mapped by M&A as potential other waters. M&A did not map "wetlands" as the flow areas do not exhibit the three parameters required to define an area as "wetland." On December 8, 2015, M&A biologists met with the Corps on the project site to have our preliminary wetland delineation map verified. The Corps concurred with M&A's wetland delineation map and exerted their jurisdiction over the other waters that are mapped within the flood control basin. The Corps has confirmed their jurisdiction over 0.24-acre of other waters of the United States on the project site (see Sheet 1). Thus, prior authorization from the Corps (a permit) would be necessary before filling or otherwise impacting the Corps' regulated features shown on Sheet 1, attached. The current site development plan (dated June 18, 2019) shows that all waters of the United States on the project site will be avoided by the proposed project (see

Attachment B: Tentative Map: Subdivision). Thus, there would be no impacts to waters of the United States and mitigation is not warranted.

#### 8.2 California Regional Water Quality Control Board (RWQCB)

#### 8.2.1 Section 401 of the Clean Water Act

The SWRCB and RWQCB regulate activities in "waters of the State" (which includes wetlands) through Section 401 of the Clean Water Act. While the Corps administers a permitting program that authorizes impacts to waters of the United States, including wetlands and other waters, any Corps permit authorized for a proposed project would be inoperative unless it is an NWP that has been certified for use in California by the SWRCB, or if the RWQCB has issued a project specific certification of water quality. Certification of NWPs requires a finding by the SWRCB that the activities permitted by the NWP will not violate water quality standards individually or cumulatively over the term of the permit (the term is typically for five years). Certification must be consistent with the requirements of the federal Clean Water Act, the California Environmental Quality Act, the CESA, and the SWRCB's mandate to protect beneficial uses of waters of the State. Any denied (i.e., not certified) NWPs, and all Individual Corps permits, would require a project specific RWQCB certification of water quality. Where a project will result in dredge or fill of non-federal waters of the State, the RWQCB will authorize those fills through waste discharge requirements issued under the Porter Cologne Water Quality Control Act.

On April 2, 2019, the SWRCB adopted a state-level definition of "wetlands, which is broader than the federal definition in that unvegetated areas may be considered a "water of the State." As a part of the same policy, the Water Board adopted permit procedures and standards governing the discharge of dredged or fill material into wetlands and other waters of the State. The policy includes, among other things, requirements for analyses to identify the least environmentally damaging practicable alternative (LEDPA) and compensatory mitigation standards including a minimum 1:1 ratio for wetlands and streams, and full functional replacement of all waters on top of this minimum where applicable. The policy, which will govern both Section 401 certifications and WDRs, is scheduled to become effective nine months following the completion of review by the California Office of Administrative Law.

#### 8.2.2 APPLICABILITY TO THE PROPOSED PROJECT

The Corps has confirmed their jurisdiction over 0.24-acre of other waters onsite; thus, any Section 404 permit authorized by the Corps for the project would be inoperative without also obtaining authorization from the RWQCB pursuant to Section 401 of the Clean Water Act (i.e., without obtaining a certification of water quality). Since the RWQCB does not have a formal method for technically defining what constitutes waters of the State, M&A expect that the RWQCB should remain consistent with the Corps' determination.

Any impacts to waters of the State would have to be mitigated to the satisfaction of the RWQCB prior to the time this resource agency would issue a permit for impacts to such features. The RWQCB requirements for issuance of a "401 Permit" typically parallel the Corps requirements for permitting impacts to Corps regulated areas pursuant to Section 404 of the Clean Water Act. Please refer to the Corps "Applicability" section above for likely mitigation requirements for impacts to RWQCB regulated waters. Also, please refer to the applicability section of the Porter-

Cologne Water Quality Control Act below for other applicable actions that may be imposed on the project by the RWQCB prior to the time any certification of water quality is authorized for the project. Please note that any isolated wetlands or other waters that are determined to be on the project site that are not regulated by the Corps pursuant to the SWANCC decision, would still be regulated by the RWQCB pursuant to the Porter-Cologne Water Quality Control Act (see below).

The current site development plan (dated June 18, 2019) shows that all waters of the State on the project site will be avoided by the proposed project (see Attachment B: Tentative Map: Subdivision). Thus, there would be no impacts to waters of the State and mitigation is not warranted.

## 8.2.3 PORTER-COLOGNE WATER QUALITY CONTROL ACT

The uncontrolled discharge of pollutants into impaired water bodies is considered particularly detrimental. According to the EPA, **sediment is one of the most widespread pollutants contaminating U.S. rivers and streams**. Sediment runoff from construction sites is 10 to 20 times greater than from agricultural lands and 1,000 to 2,000 times greater than from forest lands (EPA 2005). Consequently, the discharge of stormwater from large construction sites is regulated by the RWQCB under the federal Clean Water Act and California's Porter-Cologne Water Quality Control Act.

The Porter-Cologne Water Quality Control Act, Water Code § 13260, requires that "any person discharging waste, or proposing to discharge waste, that could affect the <u>waters of the State</u> to file a report of discharge" with the RWQCB through an application for waste discharge (Water Code Section 13260(a)(1). The term "waters of the State" is defined as any surface water or groundwater, including saline waters, within the boundaries of the State (Water Code § 13050(e)). It should be noted that pursuant to the Porter-Cologne Water Quality Control Act, the RWQCB also regulates "isolated wetlands," or those wetlands considered to be outside of the Corps' jurisdiction pursuant to the SWANCC decision (see Corps Section above).

The RWQCB generally considers filling in waters of the State to constitute "pollution." Pollution is defined as an alteration of the quality of the waters of the state by waste that unreasonably affects its beneficial uses (Water Code §13050(1)). The RWQCB litmus test for determining if a project should be regulated pursuant to the Porter-Cologne Water Quality Control Act is if the action could result in any "threat" to water quality.

The RWQCB requires complete pre- and post-development Best Management Practices Plan (BMPs) of any portion of the project site that is developed. This means that a water quality treatment plan for the pre- and post-developed project site must be prepared and implemented. Preconstruction requirements must be consistent with the requirements of the National Pollutant Discharge Elimination System (NPDES). That is, a *Stormwater Pollution Prevention Plan* (SWPPP) must be developed prior to the time that a site is graded (see NPDES section below). In addition, a post construction BMPs plan, or a Stormwater Management Plan (SWMP) must be developed and incorporated into any site development plan.

#### 8.2.4 APPLICABILITY TO THE PROPOSED PROJECT

The project site falls within the Central Valley Region (Region 3) of the RWQCB. The Corps has confirmed that there are waters of the United States/waters of the State on the project site. The RWQCB would have jurisdiction over these areas pursuant to the Porter-Cologne Water Quality Control Act. Since any "threat" to water quality could conceivably be regulated pursuant to the Porter-Cologne Water Quality Control Act, care will be required when constructing the proposed project to be sure that adequate pre-and post-construction BMPs are incorporated into the project implementation plans.

It should also be noted that prior to issuance of any permit from the RWQCB this agency will require submittal of a Notice of Determination from San Benito County indicating that the proposed project has completed a review conducted pursuant to CEQA. The pertinent sections of the CEQA document (typically the biology section) are often submitted to the RWQCB for review prior to the time this agency will issue a permit for a proposed project.

# 9. STATE WATER RESOURCES CONTROL BOARD (SWRCB)/RWQCB – STORM WATER MANAGEMENT

#### 9.1 Construction General Permit

While federal Clean Water Act NPDES regulations allow two permitting options for construction related stormwater discharges (individual permits and General Permits), the State Water Resources Control Board (SWRCB) has elected to adopt only one statewide Construction General Permit at this time that will apply to all stormwater discharges associated with construction activity, except from those on Tribal Lands, in the Lake Tahoe Hydrologic Unit, and those performed by the California Department of Transportation (CalTrans).

The Construction General Permit requires all dischargers where construction activity disturbs greater than one acre of land or those sites less than one acre that are part of a common plan of development or sale that disturbs more than one acre of land surface to:

- 1. Develop and implement a SWPPP which specifies BMPs that will prevent all construction pollutants from contacting stormwater with the intent of keeping all products of erosion from moving off site into receiving waters.
- 2. Eliminate or reduce non-stormwater discharges to storm sewer systems and other waters of the nation. Achieve quantitatively-defined (i.e., numeric) pollutant-specific discharge standards, and conduct much more rigorous monitoring based on the project's projected risk level.
- 3. Perform inspections of all BMPs.

This Construction General Permit is implemented and enforced by the nine RWQCBs. It is also enforceable through citizens' suits and represents a dramatic shift in the State Water Board's approach to regulating new and redevelopment sites, imposing new affirmative duties and fixed standards on builders and developers.

# Types of Construction Activity Covered by the Construction General Permit

- clearing,
- grading,
- disturbances to the ground such as stockpiling, or excavation that results in soil disturbances of at least one acre or more of total land area.

Construction activity that results in soil disturbances to a smaller area would still be subject to this General Permit if the construction activity is part of a larger common plan of development that encompasses greater than one acre of soil disturbance, or if there is significant water quality impairment resulting from the activity.

# Construction activity does not include:

- routine maintenance to maintain original line and grade,
- hydraulic capacity, or original purpose of the facility,
- nor does it include emergency construction activities required to protect public health and safety.

The Construction General Permit includes several "post-construction" requirements. These requirements entail that site designs provide no net increase in overall site runoff and match preproject hydrology by maintaining runoff volume and drainage concentrations. To achieve the required results where impervious surfaces such as roofs and paved surfaces are being increased, developers must implement non-structural off-setting BMPs, such as landform grading, site design BMPs, and distributed structural BMPs (bioretention cells, rain gardens, and rain cisterns). This "runoff reduction" approach is essentially a State Water Board-imposed regulatory requirement to implement Low Impact Development ("LID") design features. Volume that cannot be addressed using non-structural BMPs must be captured in structural BMPs that are approved by the RWQCB.

Improving the quality of site runoff is necessary to improve water quality in impaired and threatened streams, rivers, and lakes (that is, water bodies on the EPA's 303(d) list). The RWQCB prioritizes the water bodies on the 303(d) list according to potential impacts to beneficial uses. Beneficial uses can include a wide range of uses, such as nautical navigation; wildlife habitat; fish spawning and migration; commercial fishing, including shellfish harvesting; recreation, including swimming, surfing, fishing, boating, beachcombing, and more; water supply for domestic consumption or industrial processes; and groundwater recharge, among other uses. The State is required to develop action plans and establish Total Maximum Daily Loads (TMDLs) to improve water quality within these impaired water bodies. The TMDL is the quantity of a pollutant that can be safely assimilated by a water body without violating the applicable water quality standards.

Pursuant to the Clean Water Act, the RWQCB regulates construction discharges under the National Pollutant Discharge Elimination System (NPDES). The project sponsor of construction

or other activities that disturb more than one acre of land must obtain coverage under NPDES Construction General Permit Order 2009-0009-DWQ, administered by the RWQCB<sup>1</sup>.

#### 9.1.1 APPLICABILITY TO THE PROPOSED PROJECT

To obtain coverage under the SWRCB administered Construction General Permit, the applicant (typically through its civil engineer) must electronically file a number of permit-related compliance documents (Permit Registration Documents (PRDs), including a Notice of Intent (NOI), a risk assessment, site map, signed certification, SWPPP, Notice of Termination (NOT), NAL exceedance reports, and other site-specific PRDs that may be required. The PRDs must be prepared by a Qualified SWPPP Practitioner (QSP) or Qualified SWPPP Developer (QSD) and filed by a Legally Responsible Person (LRP) on the RWQCB's Stormwater Multi-Application Report Tracking System (SMARTS). (QSDs are typically civil engineers, professional hydrologists, engineering geologists, or landscape architects.) Once filed, these documents become immediately available to the public for review and comment. At a minimum, the SWPPP shall identify BMPs for implementation during project construction that are in accordance with the applicable guidance and procedures contained in the California Stormwater Quality Association's *California Stormwater Best Management Practices Handbook* (2015).

## 9.2 RWQCB Municipal Storm Water Permitting Programs

The federal Clean Water Act was amended in 1987 to address urban stormwater runoff pollution of the nation's waters. In 1990, the EPA promulgated rules establishing Phase 1 of the NPDES stormwater program. The Phase 1 program for Municipal Separate Storm Sewer System (MS4s) requires operators that serve populations of 100,000 or greater to implement a stormwater management program to control polluted discharges from these MS4s. While Phase 1 of the municipal stormwater program has focused on large urban areas, Phase 2 of the municipal stormwater program was promulgated by the USEPA for smaller urban areas including non-traditional Small MS4s, which are governmental facilities such as military bases, public campuses, and prison and hospital complexes.

MS4 permits require the discharger (or dischargers that are permitted by the MS4 permittees) to develop and implement a SWMP with the goal of reducing the discharge of pollutants to the maximum extent practicable (MEP). MEP is the performance standard specified in Section 402(p) of the Clean Water Act. The management programs specify what BMPs will be used to address certain program areas. The program areas include public education and outreach; illicit discharge detection and elimination; construction and post-construction; and good housekeeping for municipal operations. In general, medium and large municipalities are required to conduct chemical monitoring, though small municipalities are not.

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<sup>&</sup>lt;sup>1</sup> CGP Order 2009-0009-DWQ remains in effect, but has been amended by CGP Order 2009-0014-DWQ, effective February 14, 2011, and CGP Order 2009-0016-DWQ, effective July 17, 2012. The first amendment merely provided additional clarification to Order 2009-0009-DWQ, while Order 2009-0016-DWQ eliminated numeric effluent limits on pH and turbidity (except in the case of active treatment systems), in response to a legal challenge to the original order.

#### 9.2.1 NPDES C.3 REQUIREMENTS

The NPDES C.3 requirements went into effect for any project (public or private) that is "deemed complete" by the City or County (Lead Agency) on or after February 15, 2005, and which will result in the creation or replacement (other than normal maintenance) of at least 10,000 square feet of impervious surface area (roofs, streets, patios, parking lots, etc. Provision C.3 requires the onsite treatment of stormwater prior to its discharge into downstream receiving waters. Note that these requirements are in addition to the existing NPDES requirements for erosion and sedimentation controls during project construction that are typically addressed through acquisition of coverage under the SWRCB administered Construction General Permit. The C.3 requirements are typically required to be implemented by MS4 permittees (and their constituencies).

Projects subject to Provision C3 must include the capture and onsite treatment of all stormwater from the site prior to its discharge, including rainwater falling on building rooftops. Project applicants are required to implement appropriate source control and site design measures and to design and implement stormwater treatment measures in order to reduce the discharge of stormwater pollutants to the *maximum extent practicable*. While the Clean Water Act does not define "maximum extent practicable," the Stormwater Quality Management Plans required as a condition of the municipal NPDES permits identify control measures (BMPs) and, where applicable, performance standards, to establish the level of effort required to satisfy the maximum extent practicable criterion. It is ultimately up to the professional judgment of the reviewing municipal staff in the individual jurisdictions to determine whether a project's proposed stormwater controls will satisfy the maximum extent practicable criterion. However, there are numeric criteria used to ensure that treatment BMPs have been adequately sized to accommodate and treat a site's stormwater. The C3 requirements are quite extensive, and their complete explanation is not provided here. However, the following are minimums that should be understood and adhered to:

- The applicant must provide a detailed and realistic site design and impervious surface area calculations. This site design and calculations will be used by the Lead Agency (County or City) to determine/verify the amount of impervious surface area that is being created or replaced. It should include all proposed buildings, roads, walkways, parking lots, landscape areas, etc., that are being created or redeveloped. If large (greater than 10,000 square feet) lots are being created an effort will need to be made to determine the total impervious surface area that could be created on that parcel. For example, if only a portion of the lot is shown as a "building envelope" then the lead agency will need to consider that a driveway will have to be constructed to access the envelope and that the envelope will then be developed as shown. If the C.3 thresholds are met (creation/redevelopment of 10,000 square feet of impervious surface area), a Stormwater Control Plan (SWCP) (if required by the Lead Agency, or whatever steps for compliance with Provision C3 are required locally) must accompany the application.
- If a SWCP is required by the Lead Agency for the project it must be stamped by a Licensed Civil Engineer, Architect, or Landscape Architect.

#### 9.2.2 APPLICABILITY TO THE PROPOSED PROJECT

The project site is located in an unincorporated area of San Benito County. San Benito County is an MS4 permittee and thus is required to enforce development of a project specific SWMP that incorporates pre and post construction BMPs. It is the applicant's responsibility to ensure that the project civil engineer prepares all required Storm Water Planning documents for submittal to San Benito County so that compliance with its MS4 permit requirements can be verified as reported to the RWQCB or as otherwise necessary to comply with the Clean Water Act NPDES requirements. In addition, if the project includes a requirement to obtain a Clean Water Act Section 401 permit from the RWQCB, the Storm Water Management Plan (or equivalent plan) must be submitted to the RWQCB with the application package submitted for acquisition of a Section 401 permit (aka "water quality certification").

# 9.3 California Department of Fish and Wildlife Protections

#### 9.3.1 SECTION 1602 OF CALIFORNIA FISH AND GAME CODE

Pursuant to Section 1602 of the California Fish and Game Code: "An entity may not substantially divert or obstruct the natural flow of, or substantially change or use any material from the bed, channel, or bank of, any river, stream, or lake, or deposit or dispose of debris, waste, or other material containing crumbled, flaked, or ground pavement where it may pass into any river, stream, or lake, unless all of the following occur:

- (1) CDFW receives written notification regarding the activity in the manner prescribed by CDFW. The notification shall include, but is not limited to, all of the following:
  - (A) A detailed description of the project's location and a map.
  - (B) The name, if any, of the river, stream, or lake affected.
  - (C) A detailed project description, including, but not limited to, construction plans and drawings, if applicable.
  - (D) A copy of any document prepared pursuant to Division 13 (commencing with Section 21000) of the Public Resources Code.
  - (E) A copy of any other applicable local, state, or federal permit or agreement already issued.
  - (F) Any other information required by CDFW" (Fish & Game Code 2014).

Please see Section 1602 of the current California Fish and Game Code for further details.

Please also note that while not stated in the regulations above, CDFW typically considers its jurisdiction to include riparian vegetation (that is, the trees and bushes growing along the stream). Thus, any proposed activity in a natural stream channel that would substantially adversely affect an existing fish and/or wildlife resource, including its riparian vegetation, would require entering into a Streambed Alteration Agreement (SBAA) with CDFW prior to commencing with work in the stream. However, prior to authorizing such permits, CDFW typically reviews an analysis of the expected biological impacts, any proposed mitigation plans that would be implemented to offset biological impacts and engineering and erosion control plans.

#### 9.3.2 APPLICABILITY TO THE PROPOSED PROJECT

There are two linear features on the project site: a short reach of roadside ditch in the project site's northwestern corner and a remnant drainage channel that no longer appears to convey flows. The Corps did not take jurisdiction over either of these features and M&A does not believe either of these linear features meets the CDFW's criteria as regulated streams pursuant to Section 1602 of the California Fish and Game Code. First, the roadside ditch emanates from a pipe where it daylights for approximately 20 linear feet before entering a box culvert and traveling underneath Enterprise Road and entering the County stormdrain system. Second, the unnamed drainage channel is very shallowly incised with less than six inches between natural grade and the bottom of the channel and this vertical difference is not even apparent during the winter and spring months when upland grasses obscure the channel. This remnant channel appears in the field as more of an upland swale rather than an incised drainage. Thus, it is our professional opinion that neither the roadside ditch nor the drainage channel meets the CDFW's criteria pursuant Section 1602 of California Fish and Game Code. Regardless, since only the CDFW can make the final determination as to what constitutes a regulated stream, M&A has prescribed a mitigation measure that would reduce impacts to CDFW-regulated stream channels to a less than significant level pursuant to CEQA (please see the Impacts and Mitigations section for details).

# 10. CALIFORNIA ENVIRONMENTAL QUALITY ACT (CEQA) REGULATIONS

A CEQA lead agency must determine if a proposed activity constitutes a project requiring further review pursuant to the CEQA. Pursuant to CEQA, a lead agency would have to determine if there could be significant adverse impacts to the environment from a proposed project. Typically, if within the city limits, the city would be the CEQA lead agency. If a discretionary permit (i.e., conditional use permit) would be required for a project (e.g. an occupancy permit must be issued), the lead agency typically must determine if there could be significant environmental impacts. This is usually accomplished by an "Initial Study." If there could be significant environmental impacts, the lead agency must determine an appropriate level of environmental review prior to approving and/or otherwise permitting the impacts. In some cases, there are "Categorical Exemptions" that apply to the proposed activity; thus, the activity is exempt from CEQA. The Categorical Exemptions are provided in CEQA. There are also Statutory Exemptions in CEQA that must be investigated for any proposed project. If the project is not exempt from CEQA, the lowest level of review typically reserved for projects with no significant effects on the environment would be for the lead agency to prepare a "Negative Declaration." If a proposed project would have only minimal impacts that can be mitigated to a level of no significance pursuant to the CEQA, then a "Mitigated Negative Declaration" is typically prepared by the lead agency. Finally, those projects that may have significant effects on the environment, or that have impacts that can't be mitigated to a level considered less than significant pursuant to the CEQA, typically must be reviewed via an Environmental Impact Report (EIR). All CEQA review documents are subject to public circulation, and comment periods.

Section 15380 of CEQA defines "endangered" species as those whose survival and reproduction in the wild are in immediate jeopardy from one or more causes, including loss of habitat, change in habitat, overexploitation, predation, competition, disease, or other factors. "Rare" species are

defined by CEQA as those who are in such low numbers that they could become endangered if their environment worsens; or the species is likely to become endangered within the foreseeable future throughout all or a significant portion of its range and may be considered "threatened" as that term is used in FESA. The CEQA Guidelines also state that a project will normally have a significant effect on the environment if it will "substantially affect a rare or endangered species of animal or plant or the habitat of the species." The significance of impacts to a species under CEQA, therefore, must be based on analyzing actual rarity and threat of extinction to that species despite its legal status or lack thereof.

#### 10.1.1 APPLICABILITY TO THE PROPOSED PROJECT

This report has been prepared as a Biology section that is suitable for incorporation by the CEQA lead agency (in this case San Benito County) into a CEQA review document such as a Mitigated Negative Declaration or an Environmental Impact Report. This document addresses potential impacts to species that would be defined as endangered or rare pursuant to Section 15380 of the CEOA.

#### 11. IMPACTS ANALYSIS

Below the criteria used in assessing impacts to Biological Resources is presented.

#### 11.1 Significance Criteria

A significant impact is determined using CEQA and CEQA Guidelines. Pursuant to CEQA §21068, a significant effect on the environment means a substantial, or potentially substantial, adverse change in the environment. Pursuant to CEQA Guideline §15382, a significant effect on the environment is further defined as a substantial, or potentially substantial, adverse change in any of the physical conditions within the area affected by the project including land, air, water, minerals, flora, fauna, ambient noise, and objects of historical or aesthetic significance. Other Federal, State, and local agencies' considerations and regulations are also used in the evaluation of significance of proposed actions.

Direct and indirect adverse impacts to biological resources are classified as "significant," "potentially significant," or "less than significant." Biological resources are broken down into four categories: vegetation, wildlife, threatened and endangered species, and regulated "waters of the United States" and/or stream channels.

#### 11.1.1 THRESHOLDS OF SIGNIFICANCE

#### 11.1.1.1 Plants, Wildlife, Waters

In accordance with Appendix G (Environmental Checklist Form) of the CEQA Guidelines, implementing the project would have a significant biological impact if it would:

 Have a substantial adverse effect, either directly or through habitat modifications, on any species identified as a candidate, sensitive, or special-status species in local or regional plans, policies, or regulations, or by the CDFW or USFWS.

- Have a substantial adverse effect on any riparian habitat or other sensitive natural community identified in local or regional plans, policies, regulations or by the CDFW or USFWS.
- Have a substantial adverse effect on federally protected "wetlands" as defined by Section 404 of the Clean Water Act (including, but not limited to, marsh, vernal pool, coastal, etc.) through direct removal, filling, hydrological interruption, or other means.
- Interfere substantially with the movement of any native resident or migratory fish or
  wildlife species or with established native resident or migratory wildlife corridors or
  impede the use of native wildlife nursery sites.
- Conflict with any local policies or ordinances protecting biological resources, such as a tree preservation policy or ordinance.
- Conflict with the provisions of an adopted Habitat Conservation Plan, Natural Community Conservation Plan, or other approved local, regional, or state habitat conservation plan.

#### 11.1.1.2 Waters of the United States and State.

Pursuant to Section 404 of the Clean Water Act (33 U.S.C. 1344), the Corps regulates the discharge of dredged or fill material into waters of the United States, which includes wetlands, as discussed in the bulleted item above, and also includes "other waters" (stream channels, rivers) (33 CFR Parts 328 through 330). Substantial impacts to Corps regulated areas on a project site would be considered a significant adverse impact. Similarly, pursuant to Section 401 of the Clean Water Act, and to the Porter-Cologne Water Quality Control Act, the RWQCB regulates impacts to waters of the state. Thus, substantial impacts to RWQCB regulated areas on a project site would also be considered a significant adverse impact.

#### 11.1.1.3 Stream Channels

Pursuant to Section 1602 of the California Fish and Game Code, CDFW regulates activities that divert, obstruct, or alter stream flow, or substantially modify the bed, channel, or bank of a stream which CDFW typically considers to include riparian vegetation. Any proposed activity that would result in substantial modifications to a natural stream channel would be considered a significant adverse impact.

#### 12. IMPACT ASSESSMENT AND PROPOSED MITIGATION

In this section we discuss potential impacts to sensitive biological resources including special-status animal species and nesting birds. We follow each impact with a mitigation prescription that when implemented would reduce impacts to the greatest extent possible. This impact analysis is based on a Tentative Map prepared by San Benito Engineering & Surveying, Inc., on June 18, 2019 (see Attachment B).

# 12.1 Impact BIO-1. Development of the Project Would Have a Significant Adverse Impact on County Protected Trees (Significant)

In the San Benito County Code of Ordinances, Title 19, Land Use and Environmental Regulations, there is a chapter that discusses the management and conservation of woodlands. This chapter, Chapter 19.33, pertains to rural zoned properties such as the project site which is zoned R/PUD. Since the project site currently supports less than 19% canopy cover, in order to meet the County's "Canopy Retention Standards" it would be necessary to retain 100% of the native trees onsite. Native trees onsite are the oak trees, buckeye trees, and according to San Benito County's native tree list, pepper trees are considered "native" trees. If retention of 100% of the native trees onsite is not practical, it would be necessary to obtain a discretionary permit from the County prior to tree removal. Removal of native trees onsite without a discretionary permit issued by the County of San Benito would be in conflict with a local ordinance protecting biological resources and would be considered a significant adverse impact pursuant to CEQA. This impact could be mitigated to a less than significant level by obtaining a discretionary permit from the County as discussed in the mitigation measure below.

#### 12.2 Mitigation Measure BIO-1 County Protected Trees

Prior to any tree removal on the project site the applicant should apply for a discretionary permit from San Benito County. Any conditions imposed by San Benito County for tree removal onsite would become conditions of project approval. *This mitigation measure would reduce the project's impact on County protected trees to a level considered less than significant*.

# 12.3 Impact BIO-2. Development of The Project Would Have a Potentially Significant Adverse Impact on Nesting Birds (Potentially Significant)

Red-tailed hawk, white-tailed kite, and red-shouldered hawk are all known from the area and could nest on the project site. Common song birds (passerine birds) could also nest on the project site. All of these birds are protected under the Migratory Bird Treaty Act (50 CFR 10.13) and their eggs and young are protected under California Fish and Game Code Sections 3503, 3503.5. Any project-related impacts to these species would be considered a significant adverse impact. Potential impacts to these species from the proposed project include disturbance to nesting birds and possibly death of adults and/or young. In the absence of survey results, it must be concluded that impacts to nesting raptors and song birds from the proposed project would be **potentially significant pursuant to CEQA.** This impact could be mitigated to a level considered less than significant.

#### 12.4 Mitigation Measure BIO-2. Nesting Birds

To avoid impacts to nesting birds, a nesting survey should be conducted within 15 days of commencing with construction work or tree removal if this work would commence between February 1st and August 31<sup>st</sup>. The nesting survey should include an examination of all buildings onsite and all trees onsite and within 200 feet of the entire project site (i.e., within a zone of influence of nesting birds), not just trees slated for removal. The zone of influence includes those areas outside the project site where birds could be disturbed by earth- moving vibrations and/or other construction-related noise.

If birds are identified nesting on or within the zone of influence of the construction project, a qualified biologist should establish a temporary protective nest buffer around the nest(s). The nest buffer should be staked with orange construction fencing. The buffer must be of sufficient size to protect the nesting site from construction-related disturbance and should be established by a qualified ornithologist or biologist with extensive experience working with nesting birds near and on construction sites. Typically, adequate nesting buffers are 50 feet from the nest site or nest tree dripline for small birds and up to 300 feet for sensitive nesting birds that include several raptor species known the region of the project site but that are not expected to occur on the project site. Upon completion of nesting surveys, if nesting birds are identified on or within a zone of influence of the project site, a qualified ornithologist/biologist that frequently works with nesting birds should prescribe adequate nesting buffers to protect the nesting birds from harm while the project is constructed.

No construction or earth-moving activity should occur within any established nest protection buffer prior to September 1 unless it is determined by a qualified ornithologist/biologist that the young have fledged (that is, left the nest) and have attained sufficient flight skills to avoid project construction zones, or that the nesting cycle is otherwise completed. In the region of the project site, most species complete nesting by mid-July. This date can be significantly earlier or later and would have to be determined by the qualified biologist. At the end of the nesting cycle, and fledging from the nest by its occupants, as determined by a qualified biologist, temporary nesting buffers may be removed, and construction may commence in established nesting buffers without further regard for the nest site. *Implementation of these mitigation measures would reduce impacts to nesting birds to a level regarded as less than significant pursuant to CEQA*.

# 12.5 Impact BIO-3. Development of the Project Could Have a Potentially Significant Adverse Impact on Western Burrowing Owl (Potentially Significant)

The western burrowing owl is a California species of special concern. This raptor (that is, bird of prey) is also protected under the Migratory Bird Treaty Act (50 CFR 10.13) and its nest, eggs, and young are protected under California Fish and Game Code Sections 3503, 3503.5. The closest known record of western burrowing owl to the project site is 1.7 miles to the northeast (Occurrence No. 758) and was recorded in 2000. While western burrowing owls have not been observed on the project site during two separate survey years (2015 and 2019) and their likelihood of presence is low, suitable nesting and foraging habitat (e.g., California ground squirrel burrows) occurs on the project site. Since the western burrowing owl is a mobile species and could move onsite, impact avoidance measures are warranted. Impacts to the western burrowing owl would be **potentially significant.** This impact could be mitigated to a level considered less than significant pursuant to CEQA.

#### 12.6 Mitigation Measure BIO-3. Western Burrowing Owl

Based on the presence for this species in the project vicinity and the potential habitat found on the project site, a preconstruction survey for burrowing owls should be conducted.

CDFW's 2012 *Staff Report* states that take avoidance (preconstruction) surveys should be conducted 14 days prior or less to initiating ground disturbance. As burrowing owls may recolonize a site after only a few days, time lapses between project activities trigger subsequent

take avoidance surveys including, but not limited to, a final survey conducted within 24 hours prior to ground disturbance to ensure absence. If no owls are found during these surveys, no further regard for the burrowing owl would be necessary.

a. Burrowing owl surveys should be conducted by walking the entire project site and (where possible) in areas within 150 meters (approx. 500 feet) of the project impact zone. The 150-meter buffer zone is surveyed to identify burrows and owls outside of the project area which may be impacted by factors such as noise and vibration (heavy equipment) during project construction.

Pedestrian survey transects should be spaced to allow 100 percent visual coverage of the ground surface. The distance between transect center lines should be 7 meters to 20 meters and should be reduced to account for differences in terrain, vegetation density, and ground surface visibility. Poor weather may affect the surveyor's ability to detect burrowing owls thus, avoid conducting surveys when wind speed is greater than 20 kilometers per hour and there is precipitation or dense fog. To avoid impacts to owls from surveyors, owls and/or occupied burrows should be avoided by a minimum of 50 meters (approx. 160 ft.) wherever practical to avoid flushing occupied burrows. Disturbance to occupied burrows should be avoided during all seasons.

- b. If burrowing owls are detected on the site, the following restricted activity dates and setback distances are recommended per CDFW's *Staff Report* (2012).
  - From April 1 through October 15, <u>low disturbance</u> activities should have a 200-meter buffer while <u>high disturbance</u> activities should have a 500-meter buffer from occupied nests.
  - From April 1 through August 15, however, <u>medium disturbance</u> activities should have a 500-meter buffer from occupied nests. Medium disturbance activities can have a reduced buffer of 200 meters starting August 16 through October 15.
  - From October 16 through March 31, low disturbance activities should have a 50-meter buffer, medium disturbance activities should have a 100-meter buffer, and high disturbance activities should have a 500-meter buffer from occupied nests, or as otherwise determined by a qualified WBO biologist to be an adequate buffer that will protect the nesting burrowing owls.
  - No earth-moving activities or other disturbance should occur within the aforementioned buffer zones of occupied burrows. These buffer zones should be fenced as well. If burrowing owls were found in the project area, a qualified biologist would also need to delineate the extent of burrowing owl habitat on the site.
  - If western burrowing owls are found occupying the project site they may be passively relocated from the project site between October 1 and February 1. Passive removal shall be conducted by a qualified biologist with demonstrated experience with passive relocation.
- c. Finally, in accordance with the 2012 *Staff Report*, if burrowing owls were found nesting onsite, credits would have to be purchased from a mitigation bank to offset the project's habitat

loss on the burrowing owl. This would be developed in coordination with CDFW and San Benito County.

These mitigation measures would reduce impacts to western burrowing owl to a level considered less than significant.

# 12.7 Impact BIO-4. Bats – Tree Removal and Site Development May Have a Potentially Significant Impact on Greater Western Mastiff Bat and Western Red Bat (Potentially Significant)

The trees and buildings onsite may provide roosting and maternity habitat for special-status bats including the greater western mastiff bat and the western red bat. These bat species are designated by the State as "species of special concern." In accordance with the CEQA Guidelines (Section 15380) which protects "rare" and "endangered" species as defined by CEQA (species of special concern meet this CEQA definition), impacts to these bat species would be considered a **potentially significant adverse impact**. Potential impacts to special-status bats from the proposed project include loss of maternity and/or roosting habitat, death of individual adult bats and/or young. This impact could be mitigated to a less than significant level.

#### 12.8 Mitigation Measure BIO-4. Bats

In order to avoid impacts to the greater western mastiff bat, western red bat, and other special-status bat species, a biologist should survey trees and buildings 15 days prior to commencing with any removal or demolition. All bat surveys should be conducted by a biologist with known experience surveying for bats. If no special-status bats are found during the surveys, then there would be no further regard for these bat species.

If special-status bat species are found on the project site a determination should be if there are young bats present. If young are found roosting in any tree or building, impacts to the tree or building should be avoided until the young have reached independence. A non-disturbance buffer fenced with orange construction fencing should also be established around the maternity site. The size of the buffer zone should be determined by a qualified bat biologist at the time of the surveys. If adults are found roosting in a tree or building on the project site but no maternal sites are found, the following measures should be undertaken to avoid impacting the bats:

Tree Trimming and/or removal should only be conducted during seasonal periods of bat activity: between August 31 and October 15, when bats would be able to fly and feed independently, and between March 1 and April 15 to avoid hibernating bats, and prior to the formation of maternity colonies.

Any trees that will be removed, and that the biologist has identified as having potentially suitable bat roost habitat, should be removed using a two-day phased removal method:

- On day one, in the afternoon, limbs and branches should be removed using chainsaws only. Limbs with cavities, crevices, and deep bark fissures should be avoided.
- On day two, the rest of the tree should be removed under the direct supervision of the biologist.

If tree removal must occur outside of the seasonal activity periods mentioned above (i.e., between October 16 and February 28/29, or between April 16 and April 30), then a qualified biologist, one with at least two years of experience surveying for bats, should do preconstruction surveys within 14 days of starting work. If the qualified biologist finds evidence of bat presence during the surveys, then he/she should develop a plan for removal and exclusion, in conjunction with CDFW.

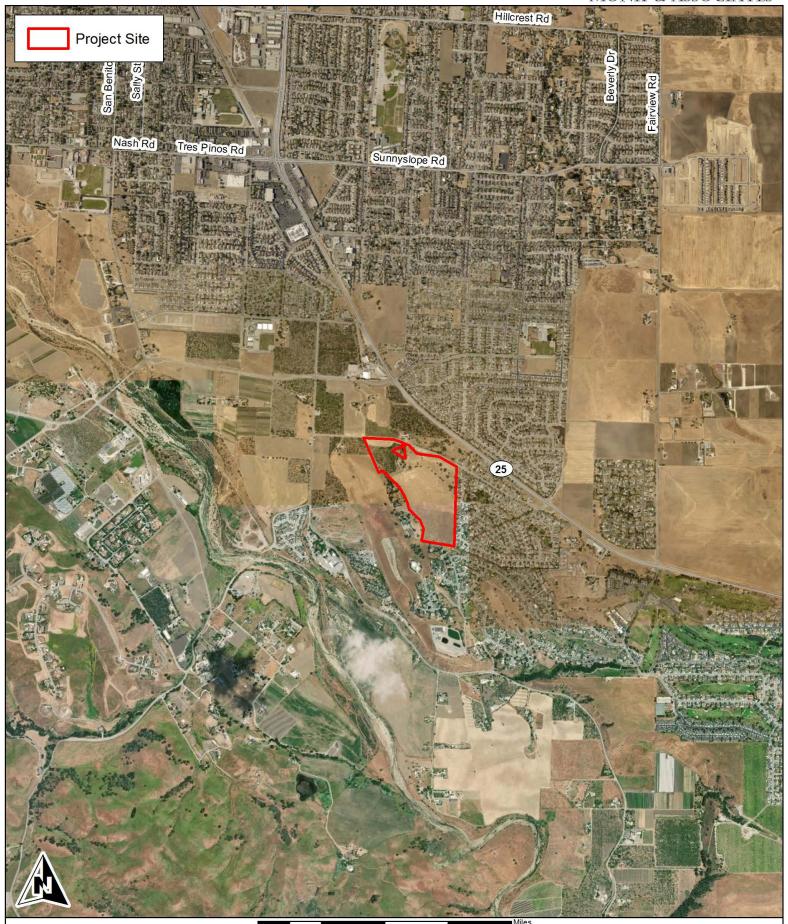
This mitigation measure would reduce the project's impact to special-status bats to a level considered less than significant.

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Figure 2. 213 Enterprise Road Project Site Project Site Location Map Hollister, California

0.125

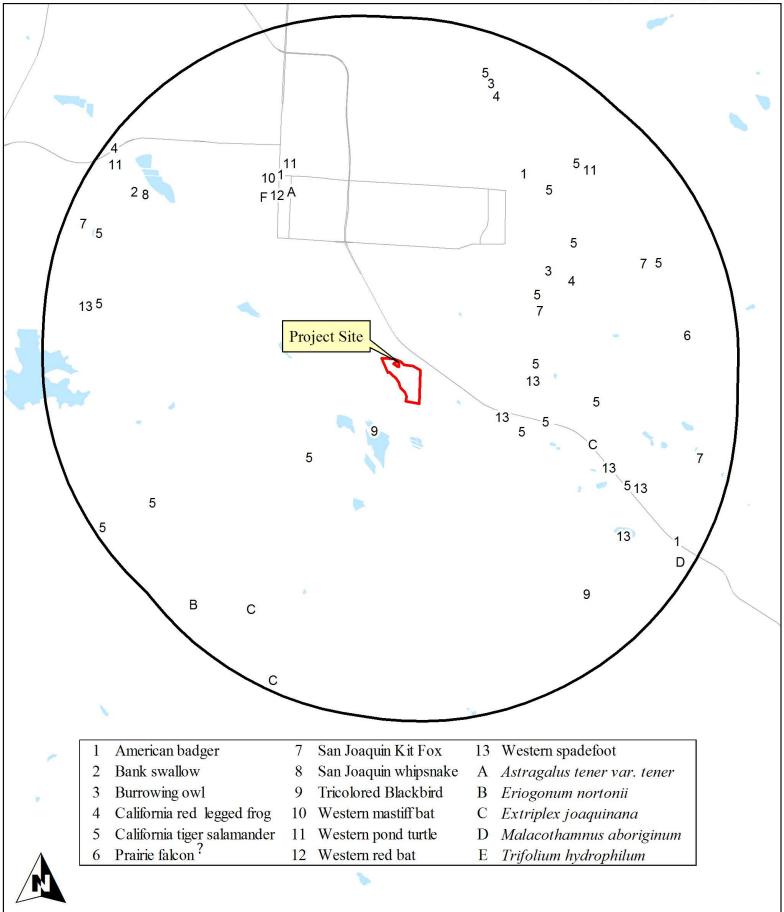
Land Grant 7.5-Minute Hollister quadrangle Aerial Photograph Source: ESRI Map Preparation Date: April 23, 2019



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Figure 3. Aerial Photograph of the 213 Enterprise Road Project Site Hollister, California

Aerial Photograph Source: ESRI Map Preparation Date: April 23, 2019





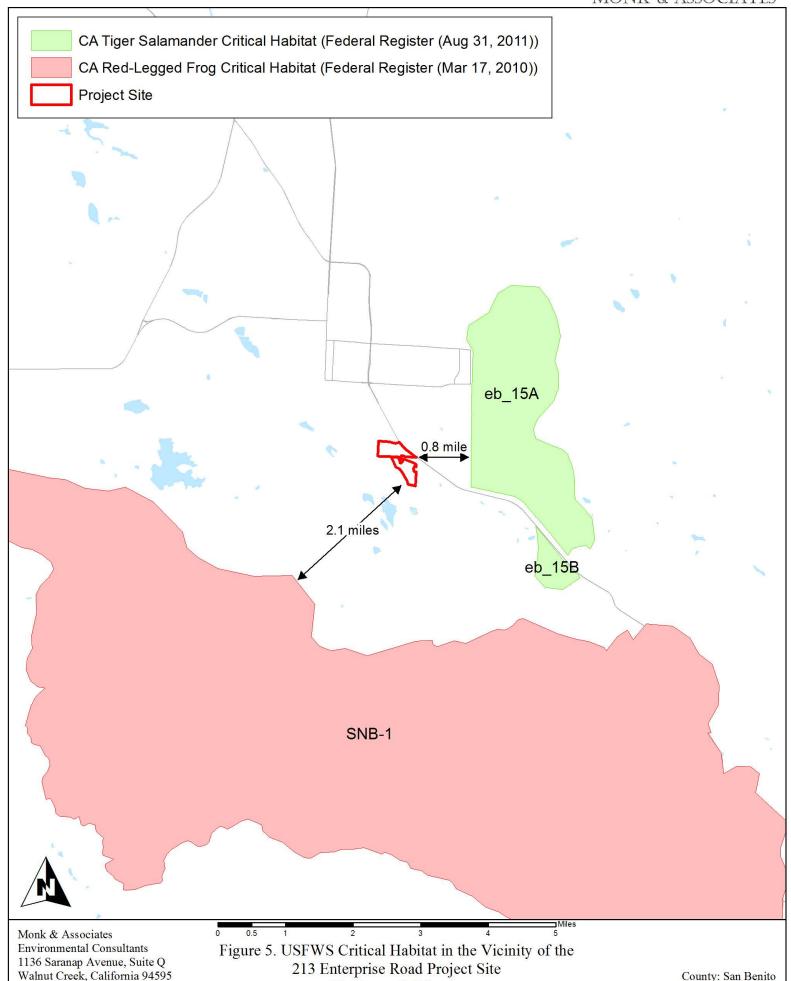
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Figure 4. CNDDB Special-Status Occurences

Within 3 Miles of the 213 Enterprise Road Project Site Hollister, California

Map Preparation Date: June 26, 2019 3-Mile Radius Source: CDFW.

California Natural Diversity Data Base, 2019



Hollister, California

(925) 947-4867

County: San Benito Map Preparation Date: June 24, 2019

# Table 1 Plants Species Observed on the 213 Enterprise Road Project Site.

#### **Angiosperms - Dicots**

Asteraceae

\*Carduus pycnocephalus subsp. pycnocephalus Italian thistle
Xanthium spinosum Spiny cocklebur

Boraginaceae

Amsinckia menziesii Common fiddleneck

Brassicaceae

\*Brassica nigra Black mustard \*Capsella bursa-pastoris Shepherd's purse

\*Lepidium draba Heart-podded hoary cress

\*Raphanus sativus Wild radish \*Sinapis arvensis Wild mustard

Caryophyllaceae

\*Stellaria media Common chickweed

**Fabaceae** 

\*Vicia villosa Winter vetch

Geraniaceae

\*Erodium botrys Broad-leaf filaree

Lythraceae

\*Lythrum hyssopifolia Hyssop loosestrife

Plantaginaceae

\*Veronica persica Persian speedwell

Polygonaceae

\*Rumex crispus Curly dock

#### **Angiosperms - Monocots**

#### Alismataceae

Alisma sp. Water plantain

Juncaceae

Juncus bufonius Toad rush

Poaceae

\*Avena sativa Cultivated oat

\*Bromus diandrus Ripgut grass

\*Bromus hordeaceus Soft chess

\*Festuca perennis perennial ryegrass

\*Hordeum murinum Wall barley

\*Poa annua Annual bluegrass

\*Triticum aestivum Wheat

<sup>\*</sup> Indicates a non-native species

# Table 2 Wildlife Species Observed on the 213 Enterprise Road Project Site

| Amphibians              |                           |
|-------------------------|---------------------------|
| Sierran treefrog        | Pseudacris sierra         |
| Reptiles                |                           |
| Western fence lizard    | Sceloporus occidentalis   |
| Birds                   |                           |
| Turkey vulture          | Cathartes aura            |
| Red-shouldered hawk     | Buteo lineatus            |
| Red-tailed hawk         | Buteo jamaicensis         |
| California quail        | Callipepla californica    |
| Eurasian collared-dove  | Streptopelia decaocto     |
| Mourning dove           | Zenaida macroura          |
| Anna's hummingbird      | Calypte anna              |
| Acorn woodpecker        | Melanerpes formicivorus   |
| Nuttall's woodpecker    | Picoides nuttallii        |
| Black phoebe            | Sayornis nigricans        |
| Say's phoebe            | Sayornis saya             |
| California scrub jay    | Aphelocoma californica    |
| American crow           | Corvus brachyrhynchos     |
| Common raven            | Corvus corax              |
| Oak titmouse            | Baeolophus inornatus      |
| Bushtit                 | Psaltriparus minimus      |
| Bewick's wren           | Thryomanes bewickii       |
| Western bluebird        | Sialia mexicana           |
| American robin          | Turdus migratorius        |
| Northern mockingbird    | Mimus polyglottos         |
| European starling       | Sturnus vulgaris          |
| Cedar waxwing           | Bombycilla cedrorum       |
| Yellow-rumped warbler   | Setophaga coronata        |
| Savannah sparrow        | Passerculus sandwichensis |
| White-crowned sparrow   | Zonotrichia leucophrys    |
| Dark-eyed junco         | Junco hyemalis            |
| House finch             | Haemorhous mexicanus      |
| Mammals                 |                           |
| Virginia opossum        | Didelphis virginiana      |
| Black-tailed jackrabbit | Lepus californicus        |

Virginia opossumDidelphis virginianaBlack-tailed jackrabbitLepus californicusCalifornia ground squirrelOtospermophilus beecheyiBotta's pocket gopherThomomys bottaeRaccoonProcyon lotor

Table 3

Special-Status Plant Species Known to Occur Within 3 Miles of the 213 Enterprise Road, Hollister Project Site

| Family<br>Taxon<br>Common Name                                    | Statu                      | us* Flowering Period             | Habitat   | Area Locations  | Probability on Project Site  |
|---|----------------------------|----------------------------------|---|---|--|
| Apiaceae  Eryngium aristulatum hooveri  Hoover's button-celery    | Fed:<br>State:<br>CNPS: R  | - July-July<br>-<br>ank 1B       | Vernal pools.   | CNPS nine-quad search   | None. No vernal pool habitat on the project site. No impact expected.                                |
| Asteraceae  Centromadia parryi congdonii  Congdon's tarplant      | Fed:<br>State:<br>CNPS: Ra | - May-November<br>-<br>ank 1B.2  | Valley and foothill grassland (alkaline).                           | CNPS nine-quad search   | None. No alkaline habitat on the project site. Was not observed onsite. No impact expected.          |
| Boraginaceae Plagiobothrys glaber Hairless popcornflower          | Fed:<br>State:<br>CNPS: R  | - April-May<br>-<br>ank 1A       | Meadows (alkaline); marshes and swamps (coastal salt).              | CNPS nine-quad search   | None. No alkaline meadowsn,<br>marshes, or swamp habitat on the<br>project site. No impact expected. |
| Brassicaceae Streptanthus albidus peramoenus Uncommon jewelflower | Fed:<br>State:<br>CNPS: Ra | - April-June<br>-<br>unk 1B.2    | Chaparral; valley and foothill grassland; [serpentinite].           | CNPS nine-quad search   | None. No serpentine habitat on the project site. No impact expected.                                 |
| Chenopodiaceae Extriplex joaquinana San Joaquin spearscale        | Fed:<br>State:<br>CNPS: Ra | - April-October<br>-<br>unk 1B.2 | Chenopod scrub; meadows; valley and foothill grassland; [alkaline]. | Closest known occurrence is approximately 1.3 miles southeast of the project site (CNDDB Occurrence No. 114). | None. No alkaline habitat on the project site. Was not observed during surveys. No impact expected.  |

Table 3

Special-Status Plant Species Known to Occur Within 3 Miles of the 213 Enterprise Road, Hollister Project Site

| Family Taxon Common Name    | Status*         | Flowering Period   | Habitat                                      | Area Locations   | Probability on Project Site  |
|-----------------------------|-----------------|--------------------|--|--|--|
|                             | Status          | Tio worming Torrou | - Tuoruu                                     | . Non Boundary   | 11000001110,000  |
| Ericaceae                   |                 |                    | a  | an ma  |  |
| Arctostaphylos gabilanensis | Fed: -          | January-January    | Chaparral; cis-montane woodlands [granitic]. | CNPS nine-quad search  | None. No chaparral or granitic habitat on the project site. No                                 |
| Gabilan manzanita           | State: -        |                    | woodiands (gramtie).                         |  | manzanita species occur on the   |
|                             | CNPS: Rank 1B   |                    |  |  | project site. No impact expected.  |
| Arctostaphylos pajaroensis  | Fed: -          | January-December   | Chaparral (sandy).                           | CNPS nine-quad search  | None. No sandy chaparral on the  |
| Pajaro manzanita            | State: -        |                    |  |  | project site. No manzanita species occur on the project site.                                  |
|                             | CNPS: Rank 1B   |                    |  |  | No impact expected.  |
| Fabaceae                    |                 |                    |  |  |  |
| Astragalus tener tener      | Fed: -          | March-June         | Playas; mesic grasslands                     | Closest known occurrence is                                  | None. No playas, mesic   |
| Alkali milkvetch            | State: -        |                    | (adobe clay), vernal pools (alkaline).       | approximately 1.9 miles northwest of the project site (CNDDB | grassland, or vernal pool habitat on the project site. No impact                               |
|                             | CNPS: Rank 1B.  | 2                  | (aikainie).                                  | Occurrence No. 2).   | expected.  |
| Trifolium hydrophilum       | Fed: -          | April-June         | Marshes and swamps; valley                   | Closest known occurrence is                                  | None. No marshes, swamps,  |
| Saline clover               | State: -        | 7 ipin vane        | and foothill grassland                       | approximately 1.5 miles northwest                            | mesic or alkaline grassland, or  |
|                             | CNPS: Rank 1B.2 | 2                  | (mesic, alkaline); vernal pools. 0-300 m.    | of the project site (CNDDB Occurrence No. 21).               | vernal pool habitat on the projec<br>site. Not observed during<br>surveys. No impact expected. |
| Malvaceae                   |                 |                    |  |  |  |
| Malacothamnus aboriginum    | Fed: -          | April-October      | Chaparral; cismontane                        | Closest known occurrence is                                  | None. No chaparral or cismontane woodland habitat on   |
| Indian Valley bush mallow   | State: -        |                    | woodland; [rocky].                           | approximately 3.3 miles southeast of the project site (CNDDB | the project site. No impact  |
|                             | CNPS: Rank 1B   |                    |  | Occurrence No. 24).  | expected.  |

Table 3

Special-Status Plant Species Known to Occur Within 3 Miles of the 213 Enterprise Road, Hollister Project Site

| Family                             |                 |              |                  |   |  |   |
|------------------------------------|-----------------|--------------|------------------|---|--|---|
| Taxon Common Name                  |                 | Status*      | Flowering Period | Habitat   | Area Locations   | Probability on Project Site   |
| Orobanchaceae                      |                 |              |                  |   |  |   |
| Castilleja rubicundula rubicundula | Fed:            | -            | April-June       | Chaparral; cismontane                                       | CNPS nine-quad search  | None. Was not observed during   |
| Pink creamsacs                     | State:<br>CNPS: | -<br>Rank 1B |                  | woodland; valley and foothill grassland; meadows and seeps. |  | appropriately timed special-status plant surveys. No impact expected. |
| Polemoniaceae                      |                 |              |                  |   |  |   |
| Navarretia prostrata               | Fed:            |              | April-July       | Coastal scrub, meadows and                                  | CNPS nine-quad search  | None. No coastal scrub,   |
| Prostrate vernal pool navarretia   | State:          |              |                  | seeps, valley and foothill grassland (alkaline), and        |  | meadows, seeps, alkaline<br>grassland, or vernal pool habitat         |
|                                    | CNPS:           | Rank 1B.1    |                  | vernal pools (mesic).<br>Elevation 15-1210 m.               |  | on the project site. Was not observed. No impact expected.            |
| Polygonaceae                       |                 |              |                  |   |  |   |
| Chorizanthe biloba immemora        | Fed:            | -            | May-September    | Chaparral; cismontane                                       | CNPS nine-quad search  | None. No chaparral or   |
| Hernandez spineflower              | State:          | -            |                  | woodland.   |  | cismontane woodland on the project site. No impact expected.          |
|                                    | CNPS:           | Rank 1B      |                  |   |  |   |
| Chorizanthe pungens pungens        | Fed:            | FT           | April-June       | Coastal dunes; coastal scrub.                               | CNPS nine-quad search  | None. No coastal dunes or scrub                                       |
| Monterey spineflower               | State:          | -            | •                |   |  | on the project site. No impact expected.                              |
|                                    | CNPS:           | Rank 1B.2    |                  |   |  | опрестем.   |
| Eriogonum nortonii                 | Fed:            | -            | May-June         | Chaparral; valley and                                       | Closest known occurrence is                                  | None. Was not observed during   |
| Pinnacles buckwheat                | State:          | -            |                  | foothill grassland; [sandy, often on recent burns].         | approximately 2.9 miles southwest of the project site (CNDDB | appropriately timed special-status plant surveys. No impact           |
|                                    | CNPS:           | Rank 1B      |                  |   | Occurrence No. 24).  | expected.   |

Table 3

### Special-Status Plant Species Known to Occur Within 3 Miles of the 213 Enterprise Road, Hollister Project Site

| Family   | ·                                       |                    | ·  |                               |  |  |  |
|--|---|--------------------|--|-------------------------------|--|--|--|
| Taxon  |   |                    |  |                               |  |  |  |
| Common Name                                    | Status* Flowering                       | Period Habitat     | Area Locations   | Probability on Project Site   |  |  |  |
|  |   |                    |  |                               |  |  |  |
| *Status  |   |                    |  |                               |  |  |  |
| Federal:                                       | State:                                  | CNPS Cor           | ntinued:   |                               |  |  |  |
| FE - Federal Endangered                        | CE - California Endangered              | Rank 2             | - Plants rare, threatened, or endangered in  | n California, but more common |  |  |  |
| FT - Federal Threatened                        | CT - California Threatened              |                    | elsewhere  |                               |  |  |  |
| FPE - Federal Proposed Endangered              | CR - California Rare                    |                    | Rank 2A - Extirpated in California, common elsewhere Rank 2B.1 - Seriously endangered in California, but more common elsewhere |                               |  |  |  |
| FPT - Federal Proposed Threatened              | CC - California Candidate               |                    |  |                               |  |  |  |
| FC - Federal Candidate                         | CSC - California Species of Special C   |                    | Rank 2B.2 - Fairly endangered in California, but more common elsewhere   |                               |  |  |  |
|  |   |                    | <ul> <li>Not very endangered in California, but m</li> </ul>   |                               |  |  |  |
| CNDC   |   | Rank 3<br>Rank 3.1 | - Plants about which we need more inform   | ,                             |  |  |  |
| CNPS: Rank 1A - Presumed extinct in California |   |                    | - Plants about which we need more inform   | ation (Review List)           |  |  |  |
|  |   |                    | Seriously endangered in California   |                               |  |  |  |
|  | or endangered in California and elsewhe |                    | - Plants about which we need more inform   | ation (Review List)           |  |  |  |
| Rank 1B.1 - Seriously endangered in            | California (over 80% occurrences threat | eneu/              | Fairly endangered in California  |                               |  |  |  |

Rank 4

- Plants of limited distribution - a watch list

high degree and immediacy of threat)

Rank 1B.2 - Fairly endangered in California (20-80% occurrences threatened)
Rank 1B.3 - Not very endangered in California (<20% of occurrences threatened or no current threats known)

Table 4

Special-Status Animal Species Known to Occur Within 3 Miles of the 213 Enterprise Road, Hollister Project Site

| Species  | *Status                         | Habitat  | Closest Locations   | Probability on Project Site  |
|--|---------------------------------|--|---|--|
| Amphibians   |                                 |  |   |  |
| California tiger salamander (Cnt Vly DPS)  Ambystoma californiense | Fed: FT<br>State: CT<br>Other:  | Found in grassland habitats of the valleys and foothills. Requires burrows for aestivation and standing water until late spring (May) for larvae to metamorphose.  | Closest record is from 1999 and is located approximately 1.2 miles east of the project site (Occurrence No. 190) in a seasonal detention pond at the Ridgemark Golf Course. | None. No potential breeding habitat on the project site. Site is isolated from records in the area. None seen during multiple surveys. No suitable aquatic habitat onsite. No aquatic habitats within 1.3 miles. No impact expected.                           |
| Western spadefoot  Spea hammondii                                  | Fed:<br>State: CSC<br>Other:    | Found primarily in grassland habitats, but may occur in valley and foothill woodlands. Requires vernal pools, seasonal wetlands, or stock ponds for breeding and egg laying. Eggs are typically laid in March. Eggs hatch and larval metamorphose quickly. | Closest record is from 2005 and is located approximately 1.1 miles east of the project site (Occurrence No. 115) in a detention pond at the Ridgemark Golf Course.          | None. The project site does not provide potential breeding habitat and is isolated by farming and high density development from current records. No impact expected.   |
| California red-legged frog  Rana draytonii                         | Fed: FT<br>State: CSC<br>Other: | Occurs in lowlands and foothills in deeper pools and streams, usually with emergent wetland vegetation. Requires 11-20 weeks of permanent water for larval development.  | Closest record is from 2005 and is located approximately 1.3 miles east of the project site (Occurrence No. 84) in a seasonal detention pond and a golf course pond.        | None. There is no potential pool habitat on the project site. The project site is isolated by farming and high density residential development from records in the area. None seen during January thru June surveys nor in September 2015. No impact expected. |
| Reptiles   |                                 |  |   |  |
| Western pond turtle **  Emys marmorata                             | Fed: -<br>State: CSC<br>Other:  | Inhabits ponds, marshes, rivers, streams, and irrigation ditches with aquatic vegetation. Needs suitable basking sites and upland habitat for egg laying. Occurs in the Central Valley and Contra Costa County.  | Closest record located approximately 1.3 miles northwest of the project site (Occurrence No. 31).   | None. No suitable aquatic habitat on the project site. None seen during multiple surveys. No impact expected.  |
| San Joaquin coachwhip  Masticophis flagellum ruddocki              | Fed:<br>State: CSC<br>Other:    | Arid regions below 1,800 meters in open terrain. Most abundant in grassland, desert, scrub, chaparral, and pasture lands. Uses rodent burrows for retreats.  | Closest record is from 1996 and is located approximately 2.7 miles northwest of the project site (Occurrence No. 1) in San Benito river channel.                            | Unlikely. The project site provides farmed, ruderal habitats. The project site is isolated by farming and high density residential development from records in the area. No impact.  |

Table 4

Special-Status Animal Species Known to Occur Within 3 Miles of the 213 Enterprise Road, Hollister Project Site

| Species  | *Status                           | Habitat   | Closest Locations   | Probability on Project Site   |
|--|-----------------------------------|---|---|---|
| Birds  |                                   |   |   |   |
| Prairie falcon Falco mexicanus                     | Fed: -<br>State: WL<br>Other:     | Inhabits dry, open terrain. Nests on cliffs and forages over wide areas.  | Closest nesting record is from 1978 and is located approximately 0.8 mile east of the project site (Occurrence No. 347).                          | None. Nest sites are the concern. No cliff nesting habitat on or near the project site. No impact expected.             |
| Western burrowing owl  Athene cunicularia hypugaea | Fed:<br>State: CSC<br>Other:      | Found in open, dry annual or perennial grasslands, deserts and scrublands characterized by low-growing vegetation. Subterranean nester, dependent upon burrowing mammals, most notably, the California ground squirrel. | Closest record is from 2000 and is located approximately 1.7 miles northeast of the project site (Occurrence No. 758) in grazed annual grassland. | Low. Potential burrows on the project site, but<br>this owl was not observed during multiple<br>surveys. See text.      |
| Bank swallow Riparia riparia                       | Fed: -<br>State: CT<br>Other:     | Colonial nester near riparian and other lowland habitats. Requires vertical banks or cliffs with fine-textured, sandy soils usually near streams, rivers, and lakes.  | Closest record is from 1922 and is located approximately 2.4 miles northwest of the project site (Occurrence No. 290) in San Benito River.        | None. No suitable banks on the project site. No nests of any kind on cobbly banks on and near site. No impact expected. |
| Tricolored blackbird  Agelaius tricolor            | Fed: -<br>State: CC<br>Other: CSC | Colonial nester in dense cattails, tules, brambles or other dense vegetation. Requires open water, dense vegetation, and open grassy areas for foraging.  | Closest record located approximately 0.4 miles south of the project site (Occurrence No. 992).  | None. No suitable nesting habitat on the project site. No impact expected.  |
| Mammals  |                                   |   |   |   |
| Western red bat  Lasiurus blossevillii             | Fed:<br>State: CSC<br>Other:      | Prefers riparian areas where they roost in tree foliage. This bat is occasionally captured in riparian habitats dominated by cottonwoods, oaks, sycamores, and walnuts and is rarely found in desert habitats.          | Closest record located within general vicinity of the project site; exact location unknown (Occurrence No. 83).                                   | Low. Potential roosting habitat on the project site. See text.  |

Table 4

Special-Status Animal Species Known to Occur Within 3 Miles of the 213 Enterprise Road, Hollister Project Site

| Species  | *Status                        | Habitat   | Closest Locations   | Probability on Project Site   |
|--|--------------------------------|---|---|---|
| Greater western mastiff bat  Eumops perotis californicus | Fed:<br>State: CSC<br>Other:   | Inhabits open habitats including conifer and broad-leaved woodlands, coastal scrub, chaparral, and grassland. Roosts in crevices, high buildings, trees, and tunnels.   | Closest record is from 1998 and is located approximately 1.5 miles northwest of the project site (Occurrence No. 242) | Low. Potential roosting habitat on the project site. See text.  |
| San Joaquin kit fox Vulpes macrotis mutica               | Fed: FE<br>State: CT<br>Other: | Inhabits open grasslands with scattered shrubs. Needs loose-textured sand soils for burrowing.  | Closest record is from 1971 and is located approximately 1.3 miles east of the project site (Occurrence No. 1024).    | None. No kit fox observed or photographed during an abbreviated protocol survey. Too much recent development in the area discourages this shy fox. See text.  |
| American badger  Taxidea taxus                           | Fed: -<br>State: CSC<br>Other: | Most abundant in drier open stages of most shrub, forest, and herbaceous habitats, with friable soils. Need sufficient food, friable soils & open, uncultivated ground. Prey on burrowing rodents. Dig burrows. | Closest record located approximately 1.9 miles northwest of the project site (Occurrence No. 121).                    | Low. Potential herbaceaous habitat on the project site. No evidence of badger use on the site found. Likely CA ground squirrel populations too low from control programs owing to onsite farming practices. No impact expected. |

#### \*Status

Federal: State:

FE - Federal Endangered CE - California Endangered CT - California Threatened FPE - Federal Proposed Endangered FPT - Federal Proposed Threatened CC - California Candidate

FC - Federal Candidate CSC - California Species of Special Concern

FPD - Federally Proposed for delisting FP - Fully Protected

WL - Watch List. Not protected pursuant to CEQA

<sup>\*\*</sup>The USFWS hopes to finish a 12-month finding for western pond turtle in 2021 but until formally listed, it is not afforded the protections of FESA.



#### DEPARTMENT OF THE ARMY

SAN FRANCISCO DISTRICT, U.S. ARMY CORPS OF ENGINEERS
1455 MARKET STREET, 16<sup>TH</sup> FLOOR
SAN FRANCISCO. CALIFORNIA 94103-1398

JAN 26 2016

**Regulatory Division** 

Subject: File No. 2015-00438S

Ms. Christy Owens Monk & Associates, Inc. 1136 Saranap Ave., Suite Q Walnut Creek, California 94595

Dear Ms. Owens:

This correspondence is in reference to your submittal of November 12, 2015, on behalf of Pacific Union Land Company, requesting a preliminary jurisdictional determination of the extent of navigable waters of the United States (U.S.) and waters of the U.S. occurring on a 51.2-acre project site located to the south of Enterprise Road between Southside Road and Fairfield Road in the City of Hollister, San Benito County, California (APN 020-290-040 and 029-290-029).

All proposed discharges of dredged or fill material occurring below the plane of ordinary high water in non-tidal waters of the U.S.; or below the high tide line in tidal waters of the U.S.; and within the lateral extent of wetlands adjacent to these waters, typically require Department of the Army authorization and the issuance of a permit under Section 404 of the Clean Water Act of 1972, as amended (33 U.S.C. § 1344 et seq.). Waters of the U.S. generally include the territorial seas; all traditional navigable waters which are currently used, or were used in the past, or may be susceptible to use in interstate or foreign commerce, including waters subject to the ebb and flow of the tide; wetlands adjacent to traditional navigable waters; non-navigable tributaries of traditional navigable waters that are relatively permanent, where the tributaries typically flow year-round or have continuous flow at least seasonally; and wetlands directly abutting such tributaries. Where a case-specific analysis determines the existence of a "significant nexus" effect with a traditional navigable water, waters of the U.S. may also include non-navigable tributaries that are not relatively permanent; wetlands adjacent to non-navigable tributaries that are not relatively permanent; wetlands adjacent to but not directly abutting a relatively permanent non-navigable tributary; and certain ephemeral streams in the arid West.

The enclosed delineation map entitled, "Preliminary Jurisdictional Determination, 213 Enterprise Road, Hollister, San Benito County," in one sheet and date certified January 6, 2016, depicts the extent and location of other waters of the U.S. within the boundary area of the site that **may be** subject to U.S. Army Corps of Engineers' regulatory authority under Section 404 of the Clean Water Act. This preliminary jurisdictional determination is based on the current conditions of the site, as verified during a field investigation of December 8, 2015, and a review of other data included in your submittal. While this preliminary jurisdictional determination was conducted pursuant to Regulatory Guidance Letter No. 08-02, *Jurisdictional Determinations*, it

may be subject to future revision if new information or a change in field conditions becomes subsequently apparent. The basis for this preliminary jurisdictional determination is fully explained in the enclosed *Preliminary Jurisdictional Determination Form*. You are requested to sign and date this form and return it to this office within two weeks of receipt.

You are advised that the preliminary jurisdictional determination may **not** be appealed through the U.S. Army Corps of Engineers' *Administrative Appeal Process*, as described in 33 C.F.R. Part 331 (65 Fed. Reg. 16,486; Mar. 28, 2000). Under the provisions of 33 C.F.R § 331.5(b)(9), non-appealable actions include preliminary jurisdictional determinations since they are considered to be only advisory in nature and make no definitive conclusions on the jurisdictional status of the water bodies in question. However, you may request this office to provide an approved jurisdictional determination that precisely identifies the scope of jurisdictional waters on the site; an approved jurisdictional determination may be appealed through the *Administrative Appeal Process*. If you anticipate requesting an approved jurisdictional determination at some future date, you are advised not to engage in any on-site grading or other construction activity in the interim to avoid potential violations and penalties under Section 404 of the Clean Water Act. Finally, you may provide this office new information for further consideration and request a reevaluation of this preliminary jurisdictional determination.

You may refer any questions on this matter to Naomi Schowalter of my Regulatory staff by telephone at 415-503-6763 or by e-mail at naomi.a.schowalter@usace.army.mil. All correspondence should be addressed to the Regulatory Division, South Branch, referencing the file number at the head of this letter.

The San Francisco District is committed to improving service to our customers. My Regulatory staff seeks to achieve the goals of the Regulatory Program in an efficient and cooperative manner, while preserving and protecting our nation's aquatic resources. If you would like to provide comments on our Regulatory Program, please complete the Customer Service Survey Form available on our website: http://www.spn.usace.army.mil/Missions/Regulatory.aspx.

Sincerely,

Kahnine Jalach

Tori White

Acting Chief, Regulatory Division

Enclosures

Copy Furnished (w/ enclosures):

Pacific Union Land Company, Danville, CA (Attn: Bruce Myers)

### PRELIMINARY JURISDICTIONAL DETERMINATION FORM San Francisco District

| review area and identifies all such aq  | ds that there "may be" waters of the United States in the subject uatic features, based on the following information:   |
|---|---|
| Regulatory Division: South Branch File Number: 2  |   |
| Review Area Location City/County: San Benito County Nearest Named Waterbody: San Benito River Approximate Center Coordinates of Review Area Latitude (degree decimal format): 36.82034°N Longitude (degree decimal format): -121.38106°W Approximate Total Acreage of Review Area: 51.2 acres   | File Name: 213 Enterprise Rd, Hollister, San Benito  Applicant or Requestor Information  Name: Christy Owens  Company Name: Monk and Associates, Inc.  Street/P.O. Box: 1136 Saranap Ave., Suite Q  City/State/Zip Code: Walnut Creek, CA 94595 |
| Estimated Total Amount of Waters in Review Area  Non-Wetland Waters: lineal feet feet wide and  | Name of Section 10 Waters Occurring in Review Area Tidal: N/A Non-Tidal: N/A  |
| 0.24 acre(s) Flow Regime: Ephemeral  Wetlands: lineal feet feet wide and/or acre(s) Cowardin Class: Select  | ☐ Office (Desk) Determination ☐ Field Determination: Date(s) of Site Visit(s): 12-08-2015   |
| SUPPORTING DATA: Data reviewed for Preliminary JD and, where checked and requested, appropriately reference   Maps. Plans, plots or plat submitted by or on behalf of applicant/request   Data sheets submitted by or on behalf of applicant/request   Corps concurs with data sheets/delineation report.   Corps does not concur with data sheets/delineation report.   Corps navigable waters' study (specify):   U.S. Geological Survey Hydrologic Atlas:   USGS NHD data.   USGS HUC maps.   U.S. Geological Survey map(s) (cite quad name/scale):   USDA Natural Resources Conservation Service Soil Surver   National wetlands inventory map(s) (specify):   State/Local wetland inventory map(s) (specify):   FEMA/FIRM maps.   100-year Floodplain Elevation (specify, if known):   Photographs:   Aerial (specify name and date):   Other (specify name and date):   Previous JD determination(s) (specify File No. and date of Other information (specify): | olicant/requestor (specify):  or (specify);  oort.  |
| SCHOWALIER.NAO SCHOWALIER.NAOMI.ANN.151558447  MI.ANN.1515584478  8 Date: 2019.06.27 10:04:02 -07'00'  Signature and Date of Regulatory Project Manager   | Signature and Date of Person Requesting Preliminary JD  (REQUIRED, unless obtaining the signature is impracticable)   |

#### EXPLANATION OF PRELIMINARY AND APPROVED JURISDICTIONAL DETERMINATIONS:

1. The Corps of Engineers believes that there may be jurisdictional waters of the United States on the subject site, and the permit applicant or other affected party who requested this preliminary JD is hereby advised of his or her option to request and obtain an approved jurisdictional determination (JD) for that site. Nevertheless, the permit applicant or other person who requested this preliminary JD has declined to exercise the option to obtain an approved JD in this instance and at this time.

2. In any circumstance where a permit applicant obtains an individual permit, or a Nationwide General Permit (NWP) or other general permit verification requiring "preconstruction notification" (PCN), or requests verification for a non-reporting NWP or other general permit, and the permit applicant has not requested an approved JD for the activity, the permit applicant is hereby made aware of the following: (1) the permit applicant has elected to seek a permit authorization based on a preliminary JD, which does not make an official determination of jurisdictional waters; (2) that the applicant has the option to request an approved JD before accepting the terms and conditions of the permit authorization, and that basing a permit authorization on an approved JD could possibly result in less compensatory mitigation being required or different special conditions; (3) that the applicant has the right to request an individual permit rather than accepting the terms and conditions of the NWP or other general permit authorization; (4) that the applicant can accept a permit authorization and thereby agree to comply with all the terms and conditions of that permit, including whatever mitigation requirements the Corps has determined to be necessary; (5) that undertaking any activity in reliance upon the subject permit authorization without requesting an approved JD constitutes the applicant's acceptance of the use of the preliminary JD, but that either form of JD will be processed as soon as is practicable; (6) accepting a permit authorization without requesting an approved JD or undertaking any activity in reliance on any form of Corps permit authorization based on a preliminary JD constitutes agreement that all wetlands and other water bodies on the site affected in any way by that activity are jurisdictional waters of the United States, and precludes any challenge to such jurisdiction in any administrative or judicial compliance or enforcement action, or in any administrative appeal or in any Federal court; and (7) wheth

| Aquatic<br>Resource<br>I.D. | Latitude (degree decimal format) | Longitude (degree decimal format) | Cowardin<br>Class and<br>Flow Regime | Estimated Area or Lineal<br>Feet of Aquatic<br>Resource | Type of Aquatic Resource |
|-----------------------------|----------------------------------|-----------------------------------|--------------------------------------|---|--------------------------|
| ow 1                        | 36.821326°N                      | -121.378122°W                     | Riverine<br>Flow: Ephemeral          | lineal ft ft wide 0.192 acre(s)                         | Natural Creek            |
| ow 2                        | 36.821000°N                      | -121.377952°W                     | Riverine<br>Flow: Ephemeral          | lineal ft ft wide 0.006 acre(s)                         | Natural Creek            |
| ow 3                        | 36.820823°N                      | -121.377934°W                     | Riverine<br>Flow: Ephemeral          | lineal ft ft wide 0.006 acre(s)                         | Natural Creek            |
| ow 4                        | 36.820734°N                      | -121.377933°W                     | Riverine<br>Flow: Ephemeral          | lineal ft ft wide 0.001 acre(s)                         | Natural Creek            |
| ow 5                        | 36.820641°N                      | -121.37792°W                      | Riverine<br>Flow: Ephemeral          | lineal ft ft wide 0.017 acre(s)                         | Natural Creek            |
| ow 6                        | 36.821772°N                      | -121.378248°W                     | Riverine<br>Flow: Ephemeral          | lineal ft ft wide 0.021 acre(s)                         | Channelized Creek        |
|                             | °Select                          | - °Select                         | Select<br>Flow: Select               | lineal ft ft wide acre(s)                               | Select                   |
|                             | °Select                          | - °Select                         | Select<br>Flow: Select               | lineal ft ft wide acre(s)                               | Select                   |
|                             | °Select                          | - °Select                         | Select<br>Flow: Select               | lineal ft ft wide acre(s)                               | Select                   |
|                             | °Select                          | - °Select                         | Select<br>Flow: Select               | lineal ft ft wide acre(s)                               | Select                   |
|                             | °Select                          | - °Select                         | Select<br>Flow: Select               | lineal ft ft wide acre(s)                               | Select                   |
|                             | °Select                          | - °Select                         | Select<br>Flow: Select               | lineal ft ft wide acre(s)                               | Select                   |
|                             | °Select                          | - °Select                         | Select<br>Flow: Select               | lineal ft ft wide acre(s)                               | Select                   |
|                             | °Select                          | - °Select                         | Select<br>Flow: Select               | lineal ft ft wide acre(s)                               | Select                   |
|                             | °Select                          | - °Select                         | Select<br>Flow: Select               | lineal ft ft wide acre(s)                               | Select                   |
|                             | °Select                          | - °Select                         | Select<br>Flow: Select               | lineal ft ft wide acre(s)                               | Select                   |
|                             | °Select                          | - °Select                         | Select<br>Flow: Select               | lineal ft ft wide acre(s)                               | Select                   |
|                             | °Select                          | - °Select                         | Select<br>Flow: Select               | lineal ft ft wide acre(s)                               | Select                   |



# Appendix C

Arborist Report



### Enterprise Road San Benito County, CA

Prepared for: TTI Developers, Inc. 601 McCray Street Hollister, CA 95023

Prepared by:
HortScience | Bartlett Consulting
325 Ray Street
Pleasanton, CA 94566

**December 28, 2019** 



## **Preliminary Arborist Report**

### Enterprise Rd. Hollister, CA

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Tree Inventory Map Tree Assessment

### **Preliminary Arborist Report Enterprise Road** San Benito County, CA

#### Introduction and Overview

TTI Developers, Inc. is proposing to develop the site at 395 Enterprise Road in San Benito County, CA, HortScience | Bartlett Consulting was asked to prepare a Preliminary Arborist Report for the site as part of the tentative map application for San Benito County. This report is considered preliminary because detailed site and civil plans were not provided.

This report provides the following information:

- 1. An evaluation of the health and structural condition of the trees within the proposed project area based on a visual inspection from the ground.
- 2. General guidelines for tree preservation during the design, construction, and maintenance phases of development.

#### Assessment Methods

Trees were assessed on December 11, 2015, and conditions updated on November 25, 2019. In the four years since our initial assessment, 10 trees were removed. Five new trees were added to the assessment. The assessment included all trees within proposed construction areas measuring 8" and greater in diameter. The assessment procedure consisted of the following steps:

- 1. Identifying the tree species;
- 2. Tagging each tree with a numerically coded metal tag and recording its location on a map;
- 3. Measuring the trunk diameter at a point 54" above grade;
- 4. Evaluating the health and structural condition using a scale of 1 to 5:
  - 5 A healthy, vigorous tree, reasonably free of signs and symptoms of disease, with good structure and form typical of the species.
  - 4 Tree with slight decline in vigor, small amount of twig dieback, minor structural defects that could be corrected.
  - 3 Tree with moderate vigor, moderate twig and small branch dieback, thinning of crown, poor leaf color, moderate structural defects that might be mitigated with regular care.
  - 2 Tree in decline, epicormic growth, extensive dieback of medium to large branches, significant structural defects that cannot be abated.
  - 1 Tree in severe decline, dieback of scaffold branches and/or trunk; most of foliage from epicormics; extensive structural defects that cannot be abated.
- Rating the suitability for preservation as "high", "moderate" or "low". Suitability for preservation considers the health, age, and structural condition of the tree species and its potential to remain an asset to the site.

High: Trees with good health and structural stability that have the

potential for longevity at the site.

**Moderate:** Trees with somewhat declining health and/or structural defects

than can be abated with treatment. The tree will require more intense management and monitoring, and may have shorter life

span than those in 'high' category.

Low: Trees in poor health or with significant structural defects that cannot be mitigated. Tree is expected to continue to decline. regardless of treatment. The species or individual tree may have

characteristics that are undesirable for landscapes, and

generally are unsuited for use areas.

#### Description of Trees

Eighty-nine (89) trees, representing seven species, were evaluated (Table 1), including nine off-site trees (#62, 77-81, 92, 93, and 94) whose canopies extended onto the site. Walnut trees located in the orchard were not included in the assessment. There were three species of indigenous oaks – blue oak, coast live oak, and valley oak – concentrated in the northeast quadrant of the site. In general, trees appeared unmaintained – particularly those in and around the pastures – resulting in a history of branch failures and canopies that extended to the ground.

For all trees combined, 45% were in good condition, 48% were in fair condition, and 7% were poor. Descriptions of each tree are found in the *Tree Assessment* and approximate locations are plotted on the *Tree Inventory Map* (see Exhibits).

Table 1. Condition ratings and frequency of occurrence of trees Enterprise Rd., Hollister, CA

| Common Name        | Scientific Name      | Condition     |             | Total         |    |
|--------------------|----------------------|---------------|-------------|---------------|----|
|                    |                      | Poor<br>(1-2) | Fair<br>(3) | Good<br>(4-5) |    |
| California buckeye | Aesculus californica | -             | 1           | -             | 1  |
| Deodar cedar       | Cedrus deodara       | -             | 5           | 4             | 9  |
| Coast live oak     | Quercus agrifolia    | 1             | 6           | 11            | 18 |
| Blue oak           | Quercus douglasii    | 1             | 2           | 5             | 8  |
| Valley oak         | Quercus lobata       | -             | 3           | 7             | 10 |
| California pepper  | Schinus molle        | 3             | 26          | 13            | 42 |
| Xylosma            | Xylosma congestum    | 1             | -           | -             | 1  |
| Total              |                      | 6             | 43          | 40            | 89 |



**Photo 1**: Mature coast live oak #20, located near the walnut orchard, had a 32-inch diameter trunk and was in good condition, with dense crown and branches that extended to the ground.

Thirty-six (36) indigenous oaks were assessed at the site. They were in their natural habitat and appeared not to have been maintained, but many were in good (23 trees) and fair (11 trees) condition.

Coast live oak was the most numerous oak species, with 18 trees, including off-site tree #95. Trees were semi-mature to mature in development, with trunk diameters from nine to 32 inches. The average trunk diameter of the 10 singletrunk trees was 18 inches. Trees were mostly in good and fair condition, with one tree (#64) in poor condition. Trees in good condition had good form and dense crowns. Trees in fair condition had minor structural defects such as codominant trunks with narrow attachments. Tree #20, in good condition, had a 32-inch diameter trunk, spreading form, and branches that extended to the ground (Photo 1).

A total of 10 valley oaks were evaluated at the site. Five trees had trunk diameters greater than 32 inches. Most trees (7 trees) were in good condition with good form and structure. Three trees in fair condition had crowded form and fair structure, and tree #69 had a basal wound with decay that had spread around more than 50% of the trunk's circumference. One tree (#62) was in poor condition.

The most significant tree on the site was valley oak #70, with a 70-inch diameter trunk, located in shallow valley on the north end of the site (Photo 2). The tree was in excellent condition, with good form and structure, symmetrical crown, and no visible significant defects.



**Photo 2**: Valley oak #70 (looking east) was mature in form and development with good structure. It was in very good condition with no visible defects.



**Photo 3**: Blue oak #58, like many oaks on the site, was in good condition with spreading form and good structure.

Eight blue oaks were located on the east edge of the site. Five trees were in good condition, with good form and structure, dense crowns, and minor twig dieback (Photo 3). Tree #57, in poor condition, was suppressed under blue oak #58. Tree #93 was off site.

California pepper was the most common species, with 42 trees (47% of the population). California peppers were growing close to the house and out buildings and bordering the pasture. Trees were semi-mature to mature in development, and they were characterized as having codominant or multiple trunks; only 12 trees were single-trunked. Most trees (26 trees) were in fair condition, with fair form and/or structure, broken limbs, and/or trunk wounds with decay. Thirteen (13) trees were in good condition, with good form and structure and no significant defects. Tree #23, in good condition, had a 46-inch diameter trunk, dense crown, and branches that extended over the coops and touching the ground.

The remaining species included the following.

- Nine deodar cedars in good and fair condition that lined the driveway leading to the house
- One California buckeye in fair condition

San Benito County protects all 89 trees included in this assessment (§25.29.213), and trees cannot be removed without a permit. Three of the trees evaluated qualified as *Heritage* trees (§25.29.212): California pepper #23, and valley oaks #65 and 70.

#### Suitability for Preservation

Before evaluating the impacts that will occur during development, it is important to consider the quality of the tree resource itself, and the potential for individual trees to function well over an extended length of time. Trees that are preserved on development sites must be carefully selected to provide greater assurance they survive development impacts, adapt to a new environment, and perform well in the landscape.

Our goal is to identify trees that have the potential for long-term health, structural stability and longevity. Evaluation of suitability for preservation considers several factors:

#### Tree health

Healthy, vigorous trees are better able to tolerate impacts such as root injury, demolition of existing structures, changes in soil grade, soil moisture, and soil compaction than are non-vigorous trees.

#### Structural integrity

Trees with significant amounts of wood decay and other structural defects that cannot be corrected are likely to fail. Such trees should not be preserved in areas where damage to people or property is likely. For example, coast live oak #69 with decay around the trunk should not be retained.

#### Species response

There is a wide variation in the response of individual species to construction impacts and changes in the environment. In general, coast live oak is relatively tolerant of construction impacts and site changes, and valley oak is considered moderately tolerant.

#### Tree age and longevity

Old trees, while having significant emotional and aesthetic appeal, have limited physiological capacity to adjust to an altered environment. Young trees are better able to generate new tissue and respond to change.

#### Invasiveness

Species that spread across a site and displace desired vegetation are not always appropriate for retention. This is particularly true when indigenous species are displaced. The California Invasive Plant Inventory Database (<a href="http://www.cal-ipc.org/paf/">http://www.cal-ipc.org/paf/</a>) lists species identified as being invasive. Hollister is part of the Central West Floristic Province.

California pepper is considered *limited* for invasiveness. Limited is defined as "species [that] are invasive but their ecological impacts are minor on a statewide level or there was not enough information to justify a higher score. Their reproductive biology and other attributes result in low to moderate rates of invasiveness. Ecological amplitude and distribution are generally limited, but these species may be locally persistent and problematic."

Each tree was rated for suitability for preservation based upon its age, health, structural condition and ability to safely coexist within a development environment. Table 2 provides a summary of suitability ratings. Suitability ratings for individual trees are provided in the *Tree Assessment* (see *Exhibits*). Off-site trees did not receive a suitability rating.

We consider trees with high suitability for preservation to be the best candidates for preservation. We do not recommend retention of trees with low suitability for preservation in areas where people or property will be present. Retention of trees with moderate suitability for preservation depends upon the intensity of proposed site changes.

# Table 2: Tree suitability for preservation Enterprise Rd., Hollister CA.

#### High

These are trees with good health and structural stability that have the potential for longevity at the site. Twenty-seven (27) trees were in this category.

#### Moderate

Trees in this category have fair health and/or structural defects that may be abated with treatment. These trees require more intense management and monitoring, and may have shorter life-spans than those in the "high" category. Forty-six (46) trees were in this category.

#### Low

Trees in this category are in poor health or have significant defects in structure that cannot be abated with treatment. These trees can be expected to decline regardless of management. The species or individual tree may possess either characteristics that are undesirable in landscape settings or be unsuited for use areas. Sixteen (16) trees were in this category.

#### Preliminary Evaluation of Impacts and Recommendations

Appropriate tree retention develops a practical match between the location and intensity of construction activities and the quality and health of trees. The *Tree Assessment* was the reference point for tree condition and quality. Potential impacts from construction were estimated for each tree given the project information available to date. We referred to the Grading Plan in the Vesting Tentative Map plan set (San Benito Engineering & Surveying, Inc., dated 12 November 2019). Surveyed tree locations were not included on plans.

Plans show grading across the entire site for roads, lot subdivisions, and flood hazard zone mitigation. There is little opportunity to preserve any trees on the site. Only off-site trees may be preserved given grading activities do not encroach on trees' critical root zones (=3x trunk diameter). Preservation is predicated on following the *Tree Preservation Guidelines* (next section).

Based on my evaluation of the plans, 67 trees would require removal due to grading Three trees identified for removal were *Heritage* trees: 36" valley oak #65, 70" valley oak #70, and 38" California pepper #72.

Twenty-two (22) off-site trees were identified for preservation (Table 3).

Preservation of these trees depends on the extent and intensity of construction around trees and following the *Tree Preservation Guidelines*. Surveyed tree locations should be plotted on all future plans to determine if trees can be retained and how they can be preserved.

Table 3. Trees identified for possible preservation Enterprise Rd., Hollister, CA

| Tree<br>no. | Species      | Trunk<br>diam. | Tree<br>no. | Species        | Trunk<br>diam. |
|-------------|--------------|----------------|-------------|----------------|----------------|
| 4           | Deodar cedar | 19             | 23          | Ca. pepper     | 46             |
| 5           | Deodar cedar | 21             | 25          | Ca. pepper     | 16,11          |
| 6           | Deodar cedar | 20             | 62          | Ca. pepper     | 9,5            |
| 7           | Deodar cedar | 15             | 77          | Ca. pepper     | 17,9,8,7       |
| 8           | Deodar cedar | 18             | 78          | Ca. pepper     | 27,19,15,14    |
| 9           | Deodar cedar | 17             | 79          | Coast live oak | 8,7,7          |
| 10          | Deodar cedar | 19             | 80          | Coast live oak | 8,6            |
| 11          | Deodar cedar | 18             | 81          | Valley oak     | 12             |
| 12          | Deodar cedar | 12             | 92          | Ca. pepper     | 26,24          |
| 13          | Ca. pepper   | 10             | 93          | Blue oak       | 27             |
| 19          | Ca. pepper   | 11,9           | 94          | Coast live oak | 28             |

#### **Tree Preservation Guidelines**

The goal of tree preservation is not merely tree survival during development but maintenance of tree health and beauty for many years. Trees retained at Enterprise Rd. that are either subject to extensive injury during construction or are inadequately maintained become a liability rather than an asset. The response of individual trees will depend on the amount of excavation and grading and the construction methods. Impacts can be minimized by coordinating any construction activities inside the **TREE PROTECTION ZONE**.

The following recommendations will help reduce impacts to trees from development and maintain and improve their health and vitality through the clearing, grading, and construction phases.

#### Design recommendations

- 1. Establish horizontal and vertical elevations of perimeter and off-site trees identified for possible preservation. Overlay tree locations with precise grading plans to determine which trees may be preserved and should be protected.
- 2. Any changes to the plans affecting the trees shall be reviewed by the Consulting Arborist regarding tree impacts. These include, but are not limited to, demolition plans, site plans, improvement plans, utility and drainage plans, grading plans, and landscape and irrigation plans.
- 3. A TREE PROTECTION ZONE (TPZ) shall be established around each tree to be preserved. No grading, excavation, construction or storage of materials shall occur within that zone. The TPZ shall be established at the tree's dripline or 10' from the trunk, whichever is greater. TPZ dimensions may be adjusted by the Consulting Arborist to accommodate site design or construction access.
- 4. No underground services including utilities, sub-drains, water or sewer shall be placed in the **Tree Protection Zone**.
- 5. Irrigation systems must be designed so that no trenching will occur within the **TREE PROTECTION ZONE**.
- 6. As trees withdraw water from the soil, expansive soils may shrink within the root area. Therefore, foundations, footings and pavements on expansive soils near trees should be designed to withstand differential displacement.

- 7. **Tree Preservation Guidelines**, prepared by the Consulting Arborist, should be included on all plans.
- 8. Any herbicides placed under paving materials must be safe for use around trees and labeled for that use.

#### Pre-construction treatments and recommendations

- Fence all trees to be retained to completely enclose the TREE PROTECTION ZONE prior to demolition, grubbing or grading. Fences shall be 6 ft. chain link or equivalent as approved by the Consulting Arborist or the County of San Benito. Fences are to remain until all grading and construction are completed.
- 2. Trees may require pruning to provide construction clearance. All pruning shall be completed by a Certified Arborist or Tree Worker and adhere to the latest edition of the ANSI Z133 and A300 standards as well as the *Best Management Practices -- Tree Pruning* published by the International Society of Arboriculture. Brush shall be chipped and spread beneath the trees within the **Tree Protection Zone**.
- 3. Tree(s) to be removed that have branches extending into the canopy of tree(s) to remain must be removed by a qualified arborist and not by construction contractors. The qualified arborist shall remove the tree in a manner that causes no damage to the tree(s) and understory to remain. Tree stumps shall be ground 12" below ground surface.
- 4. Structures and underground features to be removed within the **TREE PROTECTION ZONE** shall use the smallest equipment, and operate from outside the **TREE PROTECTION ZONE**. The Consulting Arborist shall be on-site during all operations within the **TREE PROTECTION ZONE** to monitor demolition activity.
- 5. Apply and maintain 4-6" wood chip mulch within the TREE PROTECTION ZONE.

#### Recommendations for tree protection during construction

- 1. Prior to beginning work, the contractors working in the vicinity of trees to be preserved are required to meet with the Consulting Arborist at the site to review all work procedures, access routes, storage areas, and tree protection measures.
- 2. All contractors shall conduct operations in a manner that will prevent damage to trees to be preserved.
- Fences have been erected to protect trees to be preserved. Fences define a specific
   TREE PROTECTION ZONE for each tree or group of trees. Fences are to remain until all site
   work has been completed. Fences may not be relocated or removed without permission
   of the Consulting Arborist.
- 4. Any grading, construction, demolition, or other work that is expected to encounter tree roots should be monitored by the Consulting Arborist.
- 5. All underground utilities, drain lines, or irrigation lines shall be routed outside the **TREE PROTECTION ZONE**. If lines must traverse through the protection area, they shall be tunneled or bored under the tree as directed by the Consulting Arborist.
- 6. Construction trailers, traffic, and storage areas must always remain outside fenced areas.
- 7. Any root pruning required for construction purposes shall receive the prior approval of and be supervised by the Consulting Arborist.
- 8. If injury should occur to any tree during construction, it should be evaluated as soon as possible by the Consulting Arborist so that appropriate treatments can be applied.
- 9. No excess soil, chemicals, debris, equipment or other materials shall be dumped or stored within the **Tree Protection Zone**.

10. Any additional tree pruning needed for clearance during construction must be performed by a Certified Arborist and not by construction personnel.

#### Maintenance of impacted trees

Our procedures included assessing trees for observable defects in structure. This is not to say that trees without significant defects will not fail. Failure of apparently defect-free trees does occur, especially during storm events. Wind forces, for example, can exceed the strength of defect-free wood causing branches and trunks to break. Wind forces coupled with rain can saturate soils, reducing their ability to hold roots, and blow over defect-free trees. Although we cannot predict all failures, identifying those trees with observable defects is a critical component of enhancing public safety.

Furthermore, trees change over time. Our inspections represent the condition of the tree at the time of inspection. As trees age, the likelihood of failure of branches or entire trees increases. Annual tree inspections are recommended to identify changes to tree health and structure. In addition, trees should be inspected after storms of unusual severity to evaluate damage and structural changes. Initiating these inspections is the responsibility of the client and/or tree owner.

Preserved trees will experience a physical environment different from that pre-development. As a result, tree health and structural stability should be monitored. Occasional pruning, fertilization, mulch, pest management, replanting and irrigation may be required. In addition, provisions for monitoring both tree health and structural stability following construction must be made a priority.

HortScience | Bartlett Consulting

anne Geblynd

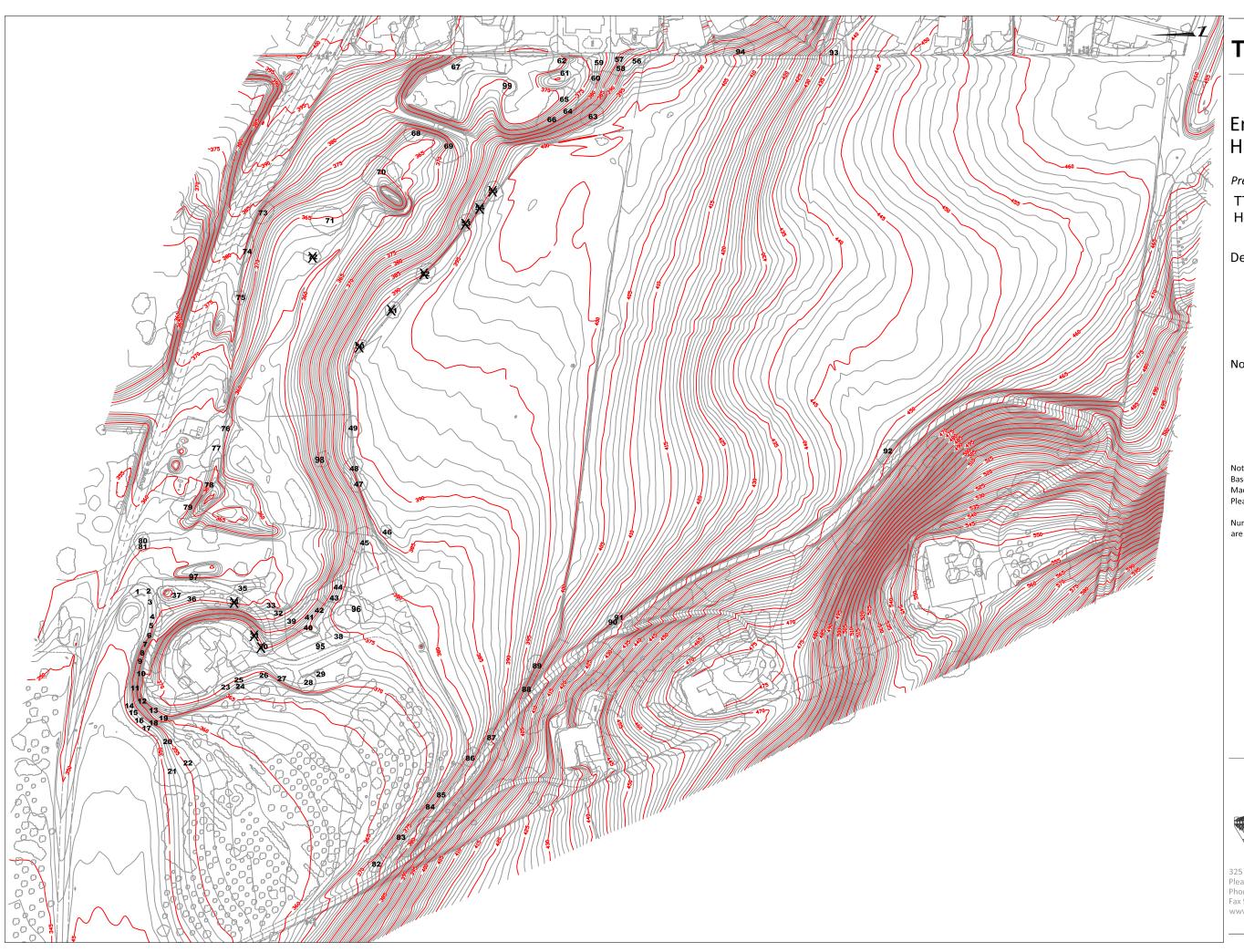
Deanne Ecklund

Registered Consulting Arborist #647



Tree Inventory Map
Tree Assessment





# Tree Inventory Map

# Enterprise Road Hollister, CA

Prepared for:

TTI Developers, Inc. Hollister, CA

December 2019

No Scale

Notes:
Base map provided by:
MacKay & Somps
Pleasanton, CA

Numbered tree locations are approximate.



325 Ray Street Pleasanton, CA 94566 Phone 925.484.0211 Fax 925.484.0596 www.hortscience.com



| Tree<br>No. | Species           | Trunk<br>Diameter<br>(in.) | Condition<br>1=poor<br>5=excellent | Suitability for<br>Preservation | Comments  |
|-------------|-------------------|----------------------------|------------------------------------|---------------------------------|---|
| 1           | Coast live oak    | 14                         | 4                                  | Moderate                        | Codominant trunks at 5' and 7'; dense crown; narrow form; growing on drainage   |
| 2           | Coast live oak    | 14,7                       | 3                                  | Moderate                        | Codominant trunks at 4'; slightly thin crown; growing on slope of drainage ditch.   |
| 3           | Coast live oak    | 6,5                        | 3                                  | Moderate                        | Codominant trunks at 3'; asymmetrical crown; crowded on east; growing on slope of   |
| 4           | Deodar cedar      | 19                         | 3                                  | Moderate                        | Slightly thin crown; lower twig and branch dieback; good form.  |
| 5           | Deodar cedar      | 21                         | 4                                  | High                            | Good form and structure; dense crown  |
| 6           | Deodar cedar      | 20                         | 4                                  | High                            | Good form and structure; dense crown  |
| 7           | Deodar cedar      | 15                         | 3                                  | Moderate                        | Fair form and structure; slightly thin crown.   |
| 8           | Deodar cedar      | 18                         | 4                                  | High                            | Good form and structure; lower branches pruned for driveway clearance.  |
| 9           | Deodar cedar      | 17                         | 4                                  | High                            | Good form and structure; dense crown.   |
| 10          | Deodar cedar      | 19                         | 3                                  | Moderate                        | Slightly thin crown; good form and structure.   |
| 11          | Deodar cedar      | 18                         | 3                                  | Moderate                        | Slightly thin crown; good form and structure.   |
| 12          | Deodar cedar      | 12                         | 3                                  | Moderate                        | Good form, fair structure; slightly thin crown.   |
| 13          | California pepper | 10                         | 3                                  | Low                             | Trunk bows east; base outside of dripline.  |
| 14          | California pepper | 18                         | 3                                  | Low                             | Trunk bows east; base outside of dripline; crowded by #15.  |
| 15          | California pepper | 26,25                      | 3                                  | Moderate                        | No tag; multiple attachments at 3'; broken stem lying on ground; good form.   |
| 16          | California pepper | 24,16,14,<br>12            | 3                                  | Moderate                        | Multiple attachments at base and 2'; spreading form; broken stems; topped for overhead utilities.                             |
| 17          | California pepper | 18                         | 3                                  | Moderate                        | Codominant trunks at 9'; trunk bows west; dense crown.  |
| 18          | California pepper | 11                         | 3                                  | Moderate                        | Codominant trunks at base; one stem bows south; dense crown.  |
| 19          | California pepper | 11,9                       | 3                                  | Moderate                        | Codominant trunks at 3'; trunk bows southwest; base outside of dripline; dense  |
| 20          | Coast live oak    | 32                         | 4                                  | High                            | Codominant trunks at 5' with narrow attachments; spreading form; heavy lateral  |
| 21          | California pepper | 32,25                      | 3                                  | Moderate                        | Codominant trunks at 2'; smaller stem bows south; large stem failure; history of branch failure; spreading form.              |
| 22          | California pepper | 14                         | 4                                  | High                            | Codominant trunks at 10'; slightly one-sided on south; crowded by #21 on northeast;   |
| 23          | California pepper | 46                         | 4                                  | High                            | Multiple attachments at 9'; heavy lateral limb extends southwest over coops, touches ground; large upright stem; dense crown. |
| 24          | California pepper | 13,8                       | 3                                  | Moderate                        | Codominant trunks at 1'; good form, fair structure; twig dieback.   |
| 25          | California pepper | 16,11                      | 4                                  | High                            | Codominant trunks at 3' and 8'; good form and structure; twig dieback.  |



| Tree<br>No.   | Species                 | Trunk<br>Diameter<br>(in.) | Condition<br>1=poor<br>5=excellent | Suitability for<br>Preservation | Comments  |
|---------------|-------------------------|----------------------------|------------------------------------|---------------------------------|---|
| 26            | California pepper       | 17,11                      | 3                                  | Moderate                        | Codominant trunks at 3'; thin crown; grown around old water tank.                     |
| 27            | California pepper       | 16,12,11,<br>10,8          | 2                                  | Low                             | Multiple attachments at 2'; spreading crown; dieback in upper crown.                  |
| 28            | California pepper       | 8,6                        | 2                                  | Low                             | Codominant trunks at 4'; thin crown; topped.  |
| 29            | California pepper       | 11,7,5                     | 2                                  | Low                             | Multiple attachments at 3'; thin crown; topped.                                       |
| <del>30</del> | California pepper       | <del>23</del>              | 4                                  | High                            | Removed   |
| 31            | California pepper       | <del>17,16</del>           | 3                                  | <b>Moderate</b>                 | Removed   |
| 32            | California pepper       | 15,8                       | 3                                  | Low                             | Trunk bows west with branches touching ground; base outside of dripline; dense crown. |
| 33            | California pepper       | 12,9                       | 3                                  | Moderate                        | Codominant trunks at 2'; fair structure; dense crown.                                 |
| 34            | <del>Siberian elm</del> | <del>9,9</del>             | 3                                  | <b>Moderate</b>                 | Removed   |
| 35            | Coast live oak          | 8,5,4                      | 3                                  | Moderate                        | Codominant trunks at 2' and 4'; dense crown; good form.                               |
| 36            | Valley oak              | 16                         | 4                                  | High                            | Codominant trunks at 10'; twig dieback.   |
| 37            | Coast live oak          | 12                         | 4                                  | Moderate                        | Codominant trunks at 14'; good form; dense crown; growing on slope of drainage ditch. |
| 38            | California pepper       | 27                         | 3                                  | Low                             | Codominant trunks at 7'; spreading form; thin crown.                                  |
| 39            | Valley oak              | 9,8                        | 4                                  | Moderate                        | Codominant trunks at 4'; good form and structure; twig dieback.                       |
| 40            | California pepper       | 14,14,13,                  | 3                                  | Moderate                        | Multiple attachments at 2'; spreading form; dense crown; heavy lateral limb.          |
| 41            | California pepper       | 17                         | 3                                  | Moderate                        | Codominant trunks at 9'; fair form and structure; lower branch dieback.               |
| 42            | California pepper       | 17,12                      | 4                                  | Moderate                        | Codominant trunks at 11'; heavy lateral limb extends to ground; trunk wound; dense    |
| 43            | Valley oak              | 8                          | 3                                  | Moderate                        | Fair form and structure; twig dieback; slightly crowded by #44.                       |
| 44            | Valley oak              | 15                         | 5                                  | High                            | Good form and structure; multiple attachments at 7' with good attachments.            |
| 45            | California pepper       | 32,18,24                   | 4                                  | High                            | Multiple attachments at 4'; spreading crown; dense crown; heavy laterals.             |
| 46            | California pepper       | 10                         | 4                                  | High                            | Good form and structure; good young tree.   |
| 47            | California pepper       | 14,8                       | 4                                  | High                            | Codominant trunks at 3'; good form and structure; low canopy.                         |
| 48            | California pepper       | 14,14                      | 4                                  | High                            | Codominant trunks at 3'; good form and structure; low canopy.                         |
| 49            | California pepper       | 14,11,6                    | 4                                  | High                            | Codominant trunks at base; spreading form, limbs extend to ground.                    |
| <del>50</del> | California pepper       | 8,5,4,4,3                  | 3                                  | Moderate                        | Removed   |



| Tree<br>No.   | Species           | Trunk<br>Diameter<br>(in.) | Condition<br>1=poor<br>5=excellent | Suitability for<br>Preservation | Comments   |
|---------------|-------------------|----------------------------|------------------------------------|---------------------------------|--|
| 51            | California pepper | 10,8,6,5,5                 | 3                                  | Moderate                        | Removed  |
| <del>52</del> | California pepper | <del>11,19,7,6,</del>      | 4                                  | <b>Moderate</b>                 | Removed  |
| <del>53</del> | California pepper | <del>10,10,9,8,</del>      | 3                                  | Moderate                        | Removed  |
| <del>54</del> | California pepper | <del>8,7,6,5,4,</del>      | 3                                  | <b>Moderate</b>                 | Removed  |
| <del>55</del> | California pepper | <del>14,12,9,6</del>       | 4                                  | Moderate                        | Removed  |
| 56            | Blue oak          | 17,15,15                   | 4                                  | Moderate                        | Multiple attachments at 1'; good form, fair structure; history of branch failure; twig dieback.      |
| 57            | Blue oak          | 21                         | 2                                  | Low                             | Suppressed under #58; poor form and structure; trunk bows east.                                      |
| 58            | Blue oak          | 30                         | 5                                  | High                            | Good form and structure; spreading form; lower twig dieback.   |
| 59            | Blue oak          | 16                         | 3                                  | Moderate                        | Codominant trunks at 10'; trunk bows south; fair form and structure.                                 |
| 60            | Blue oak          | 10                         | 3                                  | Low                             | Trunk bows south; poor form, fair structure.   |
| 61            | Valley oak        | 35                         | 4                                  | High                            | Codominant trunks at 9'; spreading form; good structure; twig dieback.                               |
| 62            | California pepper | 9,5                        | 3                                  | off-site                        | tag on fence; base on wall; entire canopy over pond; dense crown.                                    |
| 63            | Blue oak          | 20                         | 4                                  | High                            | Codominant trunks at 7'; good form and structure.  |
| 64            | Coast live oak    | 19                         | 2                                  | Low                             | Codominant trunks at 6'; stem failure; crowded form.   |
| 65            | Valley oak        | 36                         | 4                                  | High                            | Codominant trunks at 7'; good form and structure; spreading crown; twig dieback.                     |
| 66            | Blue oak          | 25                         | 4                                  | High                            | Codominant trunks at 5' and 7'; good form and structure.   |
| 67            | California pepper | 29,24                      | 3                                  | Low                             | Codominant trunks at 3'; large stem failed at 5'; dense, spreading crown.                            |
| 68            | California pepper | 26,17,13                   | 3                                  | Low                             | Multiple attachments at base; spreading crown; dense crown; numerous trunk cavities with decay.      |
| 69            | Valley oak        | 33,29,                     | 3                                  | Low                             | Multiple attachments at 3'; spreading crown; basal wound with decay around 50% of                    |
| 70            | Valley oak        | 70                         | 5                                  | High                            | Multiple attachments at 7' and 10'; good form and structure; spreading crown; beautiful mature tree. |
| 71            | Valley oak        | 33,30                      | 4                                  | High                            | Codominant trunks at base; spreading form; dead twigs and small branches; beautiful mature tree.     |
| <del>72</del> | California pepper | <del>38</del>              | 3                                  | Low                             | Removed  |
| 73            | California pepper | 19,15,11,                  | 3                                  | Moderate                        | Multiple attachments at base; spreading form; branches extend to ground.                             |
| 74            | California pepper | 17,11,11,                  | 3                                  | Moderate                        | Multiple attachments at base; fair form and structure; slightly thin crown.                          |



| Tree<br>No. | Species            | Trunk<br>Diameter<br>(in.) | Condition<br>1=poor<br>5=excellent | Suitability for<br>Preservation | Comments  |
|-------------|--------------------|----------------------------|------------------------------------|---------------------------------|---|
| 75          | California pepper  | 11,8,8,6,5                 | 3                                  | Moderate                        | Multiple attachments at base; fair form and structure; slightly thin crown.                   |
| 76          | California pepper  | 25,17,12,                  | 4                                  | Moderate                        | Multiple attachments at 2'; dense, spreading crown.   |
| 77          | California pepper  | 17,9,8,7                   | 3                                  | Moderate                        | Multiple attachments at 1'; spreading crown; fair structure.                                  |
| 78          | California pepper  | 27,19,15,                  | 3                                  | Moderate                        | Multiple attachments at base; spreading crown; fair structure.                                |
| 79          | Coast live oak     | 8,7,7                      | 4                                  | Moderate                        | Codominant trunks at 1' and 4'; fair structure; dense crown.                                  |
| 80          | Coast live oak     | 8,6                        | 3                                  | Low                             | Codominant trunks at 4'; crowded by #81; fair form and structure; beneath overhead utilities. |
| 81          | Valley oak         | 12                         | 3                                  | Low                             | Fair form and structure; crowded by #80; beneath overhead utilities.                          |
| 82          | California buckeye | 8,7,65,5,5                 | 3                                  | Moderate                        | Multiple attachments at 1'; fair form and structure.  |
| 83          | Coast live oak     | 11                         | 3                                  | Moderate                        | Codominant trunks at 8';/fair structure; small crown.   |
| 84          | Coast live oak     | 13,10,8                    | 4                                  | Moderate                        | Multiple attachments at 3'; good form, fair structure; dense crown.                           |
| 85          | Coast live oak     | 23                         | 4                                  | High                            | Codominant trunks at 5'; good form and structure; vehicle damage on 7" limb.                  |
| 86          | Coast live oak     | 16                         | 4                                  | Moderate                        | Codominant trunks at 5' and 10'; fair form and structure; dense crown.                        |
| 87          | Coast live oak     | 15                         | 3                                  | Moderate                        | Codominant trunks at 6'; trunk canker; good form.   |
| 88          | Coast live oak     | 11,9,8,5                   | 4                                  | Moderate                        | Multiple attachments at 4'; canker on limb; good form; dense crown.                           |
| 89          | California pepper  | 11,9,8,6,5                 | 3                                  | Moderate                        | Multiple attachments at 1'; spreading, dense crown; fair form and structure.                  |
| 90          | California pepper  | 14                         | 4                                  | Moderate                        | Codominant trunks at 5'; good structure, fair form.   |
| 91          | California pepper  | 9,8                        | 3                                  | Moderate                        | Codominant trunks at 2'; fair form and structure; twig dieback.                               |
| 92          | California pepper  | 26,24                      | 4                                  | High                            | Codominant trunks at 3'; good form; dense crown.  |
| 93          | Blue oak           | 27                         | 4                                  | off-site                        | no tag; Codominant trunks at 6'; good form and structure; canopy extends 16' over fence.      |
| 94          | Coast live oak     | 28                         | 5                                  | off-site                        | no tag; Multiple attachments at 6'; good form and structure; canopy extends 23' over fence.   |

# Appendix D

**Historical Resource Evaluation** 



February 5, 2020 Project No: 19-08643

Ty Intravia Longreach Associates, Inc. 601 McCray Street, Suite 205 Hollister, California 95023

Via email: <u>Ty@ttidevelopers.com</u>

Historic Resource Evaluation of 213 Enterprise Road, Unincorporated San Benito

County, California

Dear Mr. Intravia:

**Subject:** 

This report presents the findings of a historical resources study of 213 Enterprise Road, located on Assessor Parcel Number (APN) 020-290-029 in unincorporated San Benito County (subject property). Longreach Associates retained Rincon to complete the study as part of the Initial Study-Mitigated Negative Declaration (IS-MND) for the Lico Major Subdivision Project (project). Currently an approximately 50.7-acre agricultural property, APN 020-290-029would be subdivided and redeveloped with 149 residential units under the project, resulting in the the demolition of a barn and livestock pen dating from circa 1950 and two ancillary buildings constructed sometime between 1960 and 1974. The present study was completed to determine if the extant buildings are historical resources and includes background and archival research, an intensive-level survey, and an evaluation of the barn, livestock pen, and ancillary buildings for inclusion in the National Register of Historic Places (NRHP) and the California Register of Historical Resources (CRHR). All work was completed in compliance with the California Environmental Quality Act (CEQA).

This historical resources evaluation was completed by Senior Architectural Historian Steven Treffers, MHP and Architectural Historian James Williams, MA. Mr. Treffers and Mr. Williams meet the Secretary of the Interior's Professional Qualification Standards for architectural history and/or history (NPS 1983). Rincon Principal Shannon Carmack reviewed this report for quality control.

## Methods

## Archival and Background Research

Archival research was completed in February 2020 and focused on the review of a variety of primary and secondary source materials relating to the history and development of the subject property and its surroundings. Sources included, but were not limited to, historic maps and photographs and written histories of the area. The following is a list of publications consulted and repositories visited in order to conduct research pertaining to properties within the subject property.

 Historic United States Geological Survey topographical maps, aerial photographs, and city directory listings acquired via Environmental Data Resources (EDR), Inc.

Rincon Consultants, Inc.

831 333 0310 OFFICE AND FAX

info@rinconconsultants.com www.rinconconsultants.com

437 Figueroa Street, Suite 203 Monterey, California 93940



- Historic aerial photographs accessed digitally via Nationwide Environmental Title Research (NETR)
   Online, Inc. and the University of California, Santa Barbara Map & Imagery Lab
- Historic newspaper articles accessed digitally via newspapers.com and the California Digital Newspaper Collection

#### Intensive-Level Field Survey

Rincon conducted a historical resources field survey of the project site on February 3, 2020. The survey consisted of a visual inspection of the subject residence to assess overall condition and integrity, and to identify and document any potential character-defining features. Observations were recorded using detailed notes and digital photographs. The barn, livestock pen, and ancillary buildings were the only potential cultural resources identified within the project site. They were recorded and evaluated on California Department Parks and Recreation (DPR) 523 series forms, which are included in Attachment A.

## **Findings**

The subject property consists of a barn, livestock pen, and two ancillary buildings dating from the midtwentieth century (Figure 1). Although the buildings and features on the subject property may have been historically associated with a circa 1969 residence at 394 Enterprise Road (APN 020-290-030), the properties have since been subdivided and the current study was limited to the current project area APN 020-290-030). The area in which it is located, just south of the city of Hollister, has been associated with intensive farming and ranching since the arrival of Euro-Americans in the mid-nineteenth century. In the 1870s, the Southern Pacific Railroad constructed a branch line to Hollister and nearby Tres Pinos, thereby connecting the region's area hay, grain, and ranching operations to important markets in San Francisco. This development helped to sustain the local agricultural economy for decades (SBCCC 2020).

The earliest available source with information pertinent to the subject property is an 1891 map of San Benito County identifying the property as that of M. Caldera. At the time, the property was substantially larger and spanned both sides of Enterprise Road. Its owner may have been Manuel de Caldera, who is listed as a resident of the "Enterprise District" in an 1892 state voter roll and later appears in the 1900 U.S. Census rolls for the area. Although the census entry does not include an address or other specific locational information, the family is listed in the census as a neighbor of Robinson Ruckledge, whose first initial and surname label a parcel immediately adjacent to the Caldera property in the 1891 map. In 1900, Manuel reported his occupation as farmer and resided with his wife, Mary, and their children, Antonio, Jose, and Rosa (McCray and McCray 1891; Ancestry 2004; 2011).

The earliest available aerial photograph of the property reveals the land was still agricultural in character and contained no buildings as of 1939. Orchards occupied the northernmost portion of the parcel, immediately south of Enterprise Road. No buildings are visible in 1939 imagery (EDR 2019). Available sources suggest Joseph A. and Lena Doris Lico acquired the Caldera property in 1948. Lico was a partner in the firm of Lico & Greco, which operated a grocery store and tavern in Watsonville and a garage in Pajaro (Hollister Free Lance 11/19/2012; The Californian 9/14/1964). According to Joseph's obituary, he and Lena acquired an unspecified Enterprise Road property in 1948 and began a career in ranching. It appears likely the subject property is the property the Licos purchased that year given historic newspaper articles and other sources indicate the Lico family and the Lico & Greco firm had a long association with 213 Enterprise Road, the primary address with which the subject property is



associated (The Californian 9/18/1951; 7/31/1975; Santa Cruz Sentinel 6/14/1976; TTI Developers 2020). Other individuals associated with Lico & Greco business interests include Ralph Lico, Elmer Lico, Annie Greco, and Albert Greco (The Californian 9/18/1951; Santa Cruz Sentinel 7/11/2000). Research conducted for this study failed to identify additional substantial information about the Licos or any individual associated with the subject property.

Historic aerial imagery indicates that sometime between 1947 and 1953, within a half-decade of the Licos' acquisition of land along Enterprise Road, the subject barn and, possibly, the adjacent feeding pens were completed. Between 1953 and 1974, the orchard at the north end of the property was removed and replanted. Sometime between 1960 and 1974, the ancillary buildings were constructed. So too was the residence at 394 Enterprise Road, though that property is no longer part of the subject property (EDR 2019). As of 1975, 213 Enterprise Road was identified as the address of Lico & Greco Farms, which grew apricots and cherries in the 1970s (The Californian 7/31/1975; Santa Cruz Sentinel 6/14/1976). The livestock pen and large expanses of open grassland suggest the land was also used for grazing.

There have been few documented changes to the property since the 1970s. The most notable alterations have been the southward expansion of the orchard between 1981 and 1998, the removal of orchard trees along Enterprise Road in the years between 1998 and 2006, and the construction of a rear addition to the barn between 2009 and 2012 (EDR 2019aerials). According to city directory listings, as of 1995, the property was still associated with the Lico family and the Lico-Greco firm. A succession of owners and/or occupants followed. These included Maria Arreguin, Juana Elias, Maria Gallo, Jacabo Gonzales in 2000; Richard Galvan, Victor Luna, Adela Rodriguez, Celeste Salazar, Jose L Sandoval in 2005; and Maria Fonseca, Rios Gonzales, J Jimenez, Samuel Luna; Filiberto Rios, Adela Rodriguez, Idineo Santiago, and Zepeda, Mario in 2010 and 2014. The 2010 and 2014 listings also identify "Part, Lico" as an owner or occupant of the property, suggesting the Lico family business retained an association with the property (TTI Developers 2020).

The subject property is recommended ineligible for listing in the NRHP and the CRHR under all significance criteria. While the property has an association with agriculture in the areas around Hollister dating from the late nineteenth century, the extant buildings and structures on the property date to the 1950s and are not directly associated or representative of early American-era agriculture in the Hollister area. In addition, there is no indication the property is historically significant for its associations with twentieth-century agriculture in the area, or with any other event significant in the history of the locality, region, state, or nation. The property is, therefore, recommended ineligible under Criteria A/1.

Research conducted for this study uncovered no evidence that Manuel Caldera, Mary Caldera, Joseph A. Lico, Lena Doris Lico, Ralph Lico, Elmer Lico, Annie Greco, Albert Greco, or any other individual associated with the property has made significant historical contributions to local, regional, state, or national history. Further, any potentially notable contributions of these individuals would be more closely associated with the retail businesses operated by the Lico-Greco partnership, including the tavern and grocery store in Watsonville. None of these individuals are known to have made important contributions to the history of agriculture in San Benito County in the twentieth century. In light of this, the subject property is recommended ineligible under Criteria B/2.

Architecturally, the property consists of a barn, a livestock pen, and two ancillary buildings. All of these feature utilitarian designs and are unremarkable examples of their respective building or structure types. Neither the individual built elements nor the property as a whole embody the distinctive



characteristics of a type, period, or method of construction; represent the work of a master; or possess high artistic values. Therefore, the property is recommended ineligible under Criteria C/3.

A review of available evidence and records search results did not indicate that it may yield important information about prehistory or history. As a result, the property is recommended ineligible under Criteria D/4. Finally, the property is also not recommended eligible as a contributor to any existing or potential historic districts.

## Conclusions

As detailed above, the subject property was found ineligible for listing in the NRHP or CRHR. As such, it does not qualify as a historical resource as defined by CEQA.

Should you have any questions concerning this study, please do not hesitate to contact the undersigned at (805) 644-4455 x2028 or jwilliams@rinconconsultants.com.

Should you have any questions concerning this study, please do not hesitate to contact any of the undersigned.

Sincerely,

Rincon Consultants, Inc.

James Williams, MA Architectural Historian Steven Treffers, MHP

Senior Architectural Historian

#### **Attachments**

Figure Site Map

Attachment A California DPR 523 Series Forms

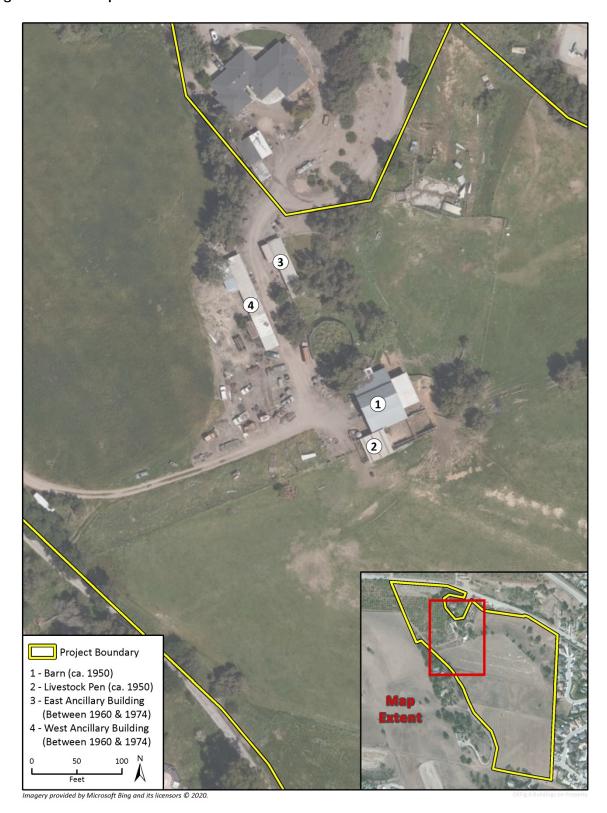


## References





Figure 1 Site Map





# Attachment A

California DPR 523 Series Forms

State of California – The Resources Agency
DEPARTMENT OF PARKS AND RECREATION

#### PRIMARY RECORD

Primary # HRI # Trinomial

NRHP Status Code 6Z

Other Listings

Review Code Reviewer

Date

Page 1 of 6 \*Res

\*Resource Name or #: 213 Enterprise Road

P1. Other Identifier:

\*P2. Location: □ Not for Publication ■ Unrestricted \*a. County: Los Angeles

\*b. USGS 7.5' Quad: Hollister Date: 2012 Township 13S, Range 5E, Section 11, 12 M.D.B.M.
c. Address: 213 Enterprise Road City: Hollister Zip: 95023

d. UTM: Zone: mE/ mN (G.P.S.)e. Other Locational Data: APN: 0202900520; 0202900510

#### \*P3a. Description:

The subject property is an approximately 50-acre farm, on which there are four built-environment features, a barn and livestock pen constructed sometime ca. 1950 and two ancillary buildings dating from between 1960 and 1974 (EDR 2019a. The buildings are clustered in the north-central section of the property.

One story in height, the barn has an irregular plan and a concrete foundation. Typical of a monitor-roof barn, its three-bay configuration consists of a central gable-roof bay flanked by pent-roof bays. The roof is clad in corrugated metal throughout, while vertical plank siding conceals the wood-frame structural system. The front (west) elevation features three openings, a comparatively large opening in the central bay and two smaller openings on the wings. None of these includes a door. A centrally placed hinged, wood-plank door opens at the rear of the building. A hay hoist extends beneath the peak of the front-facing gable. Alterations include the replacement of roofing materials and the construction of a rear addition sometime between 2009 and 2012.

The partially sheltered livestock pen is located immediately adjacent to the barn's south elevation. It is enclosed with a combination of wood and metal-rail fencing. An open-frame, pent-roof structure covers the south one third of the feature.

Two ancillary buildings, utilitarian in design, are clustered southwest of the barn. Long and rectangular in form, the buildings sit parallel to one another with a roughly north-to-south aspect. The east ancillary building is the shorter of the two. It possesses a flat roof sheathed in corrugated metal, vertical plank and plywood siding, and at least one horizontal-sliding aluminum-frame window. Limited visibility prevented the recording of further details. The west ancillary building is also has a flat roof with corrugated metal sheeting and plywood and vertical plank siding. A wood panel door is located on the north elevation. A breezeway near the building's south end functions as a utility room. **See continuation sheet, p. 4** 

\*P3b. Resource Attributes: HP4. Ancillary buildings; HP39. Other (feeding pen)

\*P4. Resources Present: ■ Building ■ Structure □ Object □ Site □ District □ Element of District □ Other (Isolates, etc.)



P5b. Description of Photo:

Overview of barn and feeding pen; camera facing east.

#### \*P6. Date Constructed/Age and Sources:

■ Historic □ Prehistoric □ Both

Ca. 1950; between 1960 and 1974 (EDR 2019a)

\*P7. Owner and Address:

N/A

#### \*P8. Recorded by:

James Williams Rincon Consultants 250 E. First Street, Ste. 1400 Los Angeles, CA 90012

#### \*P9. Date Recorded:

February 3, 2020

#### \*P10. Survey Type:

Intensive

| *P11. F | Report | Citation: |
|---------|--------|-----------|
|---------|--------|-----------|

Williams, James and Steven Treffers. 2020. Historic Resource Evaluation of 213 Enterprise Road, Hollister, San Benito County, California. Rincon Project 19-08643. February 5.

| *Attachments: □ NONE ■ Location Map □ Sketch Map ■ Continuation Sheet ■ Building, Structure, and Object Re   | cord |
|--|------|
| □ Archaeological Record □ District Record □ Linear Feature Record □ Milling Station Record □ Rock Art Record | d    |
| □ Artifact Record □ Photograph Record □ Other (List):  |      |

DPR 523A (1/95) \*Required information

State of California  $\mathbf X$  Natural Resources Agency DEPARTMENT OF PARKS AND RECREATION

**LOCATION MAP** 

Primary # HRI#

Trinomial

Page 2 of 6 \*Resource Name or # 213 Enterprise Road \*Map Name: Hollister \*Scale: 1:24,000 \*Date of map: 2012

Subject Property 1,000 2,000 N Enterprise Sch

State of California X The Resources Agency

**DEPARTMENT OF PARKS AND RECREATION** 

Primary # HRI#

#### **BUILDING, STRUCTURE, AND OBJECT RECORD**

\*Resource Name or # 213 Enterprise Road

\*NRHP Status Code 6Z

**Page** 3 of 6

B1. Historic Name: Lico & Greco Farms

B2. Common Name: N/A

B3. Original Use: Agriculture B4. Present Use: Agriculture

\*B5. Architectural Style: N/A

\*B6. Construction History:

Aerial photographs indicate the barn and livestock pen were constructed ca. 1950 and that the ancillary buildings date from sometime between 1960 and 1974 (EDR 2019). A rear addition to the barn was constructed sometime between 1998 and 2006, and it is likely that the roofing material on the barn is non-original, given its condition.

\*B7. Moved? □ No □ Yes ■ Unknown Date: N/A Original Location: N/A

\*B8. Related Features: None

B9a. Architect: Unknown b. Builder: Unknown

\*B10. Significance: Theme N/A Area N/A

Period of Significance N/A Property Type N/A Applicable Criteria N/A

The subject property consists of two parcels of farm and ranch land containing a barn, livestock pen, and two ancillary buildings dating from the mid-twentieth century. Excluded from the present evaluation are two properties that were historically associated with the subject property. One is 394 Enterprise Road (APN 0202900300), which contains a single-family residence constructed sometime between 1960 and 1974 (EDR 2020). It is situated on a separate parcel that was divided from one of the subject property. The other is APN 0202900450. Despite being situated on opposite sides of Enterprise Road, this parcel and the subject property have addresses within a close range of odd-numbered designations: 209 and 211 Enterprise Road for APN 0202900450 and 213 Enterprise Road in the case of the subject property. All three properties share associations with the Caldera and Lico families (see below for additional details). However, because the subject property alone was recently subdivided for residential development, it is regarded as a distinct property for the purposes of this evaluation.

The area in which it is located, just south of the city of Hollister, has been associated with intensive farming and ranching since the arrival of Euro-Americans in the mid-nineteenth century. In the 1870s, the Southern Pacific Railroad constructed a branch line to Hollister and nearby Tres Pinos, thereby connecting the region's area hay, grain, and ranching operations to important markets in San Francisco. This development helped to sustain the local agricultural economy for decades (SBCCC 2020).

#### See continuation sheet, p. 4.

B11. Additional Resource Attributes: N/A

#### \*B12. References:

Ancestry.com

2004 1900 United States Federal Census [database on-line]. Provo, UT, USA: Ancestry.com Operations Inc. https://search.ancestry.com, accessed

February 2, 2020.

. 2011. California, Voter Registers, 1866-1898 [database on-line].

Provo, UT, USA: Ancestry.com Operations, Inc.

https://search.ancestry.com, accessed February 2, 2020.

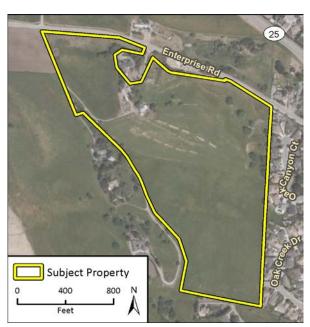
#### See continuation sheet, p. 5.

B13. Remarks:

**\*B14. Evaluator**: James Williams, Rincon Consultants

\*Date of Evaluation: February 4, 2020

(This space reserved for official comments.)



DPR 523B (9/2013) \*Required information

NT/ A

State of California -- The Resources Agency DEPARTMENT OF PARKS AND RECREATION CONTINUATION SHEET

Primary # HRI# Trinomial

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\*Resource Name or # 213 Enterprise Road

\*Recorded by: James Williams, Rincon Consultants \*Date: February 2, 2020 ■Continuation □Update

#### P3a. Description (continued):

The property is on sloping terrain at the base of a hill. Most of the land is open and has been used historically for livestock grazing. A small orchard occupies part of the north end of the property. A residence constructed sometime between 1960 and 1974 is located immediately east of the orchard (APN 0202900300). Although it was historically a part of the subject property, it was eventually subdivided from the subject parcel and is not subject to this evaluation.

#### **B10. Significance (continued):**

The earliest available source with information pertinent to the subject property is an 1891 map of San Benito County identifying the property as that of M. Caldera. At the time, the property was substantially larger and spanned both sides of Enterprise Road. Its owner may have been Manuel de Caldera, who is listed as a resident of the "Enterprise District" in an 1892 state voter roll and later appears in the 1900 U.S. Census rolls for the area. Although the census entry does not include an address or other specific locational information, the family is listed in the census as a neighbor of Robinson Ruckledge, whose first initial and surname label a parcel immediately adjacent to the Caldera property in the aforementioned 1891 map. In 1900, Manuel reported his occupation as farmer and resided with his wife, Mary, and their children, Antonio, Jose, and Rosa (McCray and McCray 1891; Ancestry 2004; 2011).

The earliest available aerial photograph of the property reveals the land was still agricultural in character and contained no buildings as of 1939. Orchards occupied the northernmost portion of the parcel, immediately south of Enterprise Road. No buildings are visible in 1939 imagery (EDR 2019). Available sources suggest Joseph A. and Lena Doris Lico acquired the Caldera property in 1948. Lico was a partner in the firm of Lico & Greco, which operated a grocery store and tavern in Watsonville and a garage in Pajaro (*Hollister Free Lance* 11/19/2012; *The Californian* 9/14/1964). According to Joseph's obituary, he and Lena acquired an unspecified Enterprise Road property in 1948 and began a career in ranching. It appears likely the subject property is the property the Licos purchased that year given historic newspaper articles and other sources indicate the Lico family and the Lico & Greco firm had a long association with 213 Enterprise Road, the primary address with which the subject property is associated (*The Californian* 9/18/1951; 7/31/1975; *Santa Cruz Sentinel* 6/14/1976; TTI Developers 2020). Other individuals associated with Lico & Greco business interests include Ralph Lico, Elmer Lico, Annie Greco, and Albert Greco (*The Californian* 9/18/1951; *Santa Cruz Sentinel* 7/11/2000). Research conducted for this study failed to identify additional substantial information about the Licos or any individual associated with the subject property.

Historic aerial imagery indicates that sometime between 1947 and 1953, within a half-decade of the Licos' acquisition of land along Enterprise Road, the subject barn and, possibly, the adjacent feeding pens were completed. Between 1953 and 1974, the orchard at the north end of the property was removed and replanted. Sometime between 1960 and 1974, the ancillary buildings were constructed. So too was the residence at 394 Enterprise Road, though that property is no longer part of the subject property (EDR 2019). As of 1975, 213 Enterprise Road was identified as the address of Lico & Greco Farms, which grew apricots and cherries in the 1970s (*The Californian* 7/31/1975; *Santa Cruz Sentinel* 6/14/1976). The livestock pen and large expanses of open grassland suggest the land was also used for grazing.

There have been few documented changes to the property since the 1970s. The most notable alterations have been the southward expansion of the orchard between 1981 and 1998, the removal of orchard trees along Enterprise Road in the years between 1998 and 2006, and the construction of a rear addition to the barn between 2009 and 2012 (EDR 2019aerials). According to city directory listings, as of 1995, the property was still associated with the Lico family and the Lico-Greco firm. A succession of owners and/or occupants followed. These included Maria Arreguin, Juana Elias, Maria Gallo, Jacabo Gonzales in 2000; Richard Galvan, Victor Luna, Adela Rodriguez, Celeste Salazar, Jose L Sandoval in 2005; and Maria Fonseca, Rios Gonzales, J Jimenez, Samuel Luna; Filiberto Rios, Adela Rodriguez, Idineo Santiago, and Zepeda, Mario in 2010 and 2014. The 2010 and 2014 listings also identify "Part, Lico" as an owner or occupant of the property, suggesting the Lico family business retained an association with the property (TTI Developers 2020).

The subject property is recommended ineligible for listing in the National Register of Historic Places and the California Register of Historical Resources under all significance criteria. While the property has an association with agriculture in the areas around Hollister dating from the late nineteenth century, the extant buildings and structures on the property date to the 1950s and are not directly associated or representative of early American-era agriculture in the Hollister area. In addition, there is no indication the property is historically significant for its associations with twentieth-century agriculture in the area, or with any other event significant in the history of the locality, region, state, or nation. The property is, therefore, recommended ineligible under Criteria A/1.

Research conducted for this study uncovered no evidence that Manuel Caldera, Mary Caldera, Joseph A. Lico, Lena Doris Lico, Ralph Lico, Elmer Lico, Annie Greco, Albert Greco, or any other individual associated with the property has made significant historical contributions to local, regional, state, or national history. Further, any potentially notable contributions of these individuals would be more closely associated with the retail businesses operated by the Lico-Greco partnership, including the tavern and grocery store in Watsonville. None of these individuals are known to have made important contributions to the history of agriculture in San Benito County in the twentieth century. In light of this, the subject property is recommended ineligible under Criteria B/2.

Architecturally, the property consists of a barn, a livestock pen, and two ancillary buildings. All of these feature utilitarian designs and are unremarkable examples of their respective building or structure types. Neither the individual built elements nor the property as a whole embody the distinctive characteristics of a type, period, or method of construction; represent the work of a master; or possess high artistic values. Therefore, the property is recommended ineligible under Criteria C/3.

A review of available evidence and records search results did not indicate that it may yield important information about prehistory or history. As a result, the property is recommended ineligible under Criteria D/4. Finally, the property is also not recommended eligible as a contributor to any existing or potential historic districts.

DPR 523L (1/95) \*Required information

State of California -- The Resources Agency DEPARTMENT OF PARKS AND RECREATION CONTINUATION SHEET

Primary # HRI# Trinomial

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\*Resource Name or # 213 Enterprise Road

#### **B12. References (continued):**

Californian, The

1951 Fictitious Name Statement for Lico & Greco, September 18. www.newspapers.com, accessed February 3, 2020.

1964 "Window Broken," September 14. www.newspapers.com, accessed February 3, 2020.

1975 Classified advertisement for Lico & Greco Farms, July 31. www.newspapers.com, accessed February 3, 2020.

Environmental Data Resources (EDR), Inc.

2019 The EDR Aerial Photo Decade Package. Vista Del Calabria Phase I ESA, Southside Rd/Enterprise Rd, Hollister, CA 95023Inquiry Number: 5914923.8. December 23.

Haas, H. and L. Hoffman

2016 Cultural Resources Study for the Lico Major Subdivision Project, San Benito County, California. Rincon Consultants Project No. 16-02351. Report on file at the Northwest Information Center, Sonoma State University, Rohnert Park, California.

Hollister Free Lance

"Archived Obituaries: Joseph A. Lico June 27, 1915- November 18, 2012," https://sanbenito.com/2012/11/19/joseph-a-lico-june-27-1915-november-18-2012/, accessed February 3, 2020.

McCray, V.T. and Harry McCray

Official map of San Benito County, California / compiled from public records and private surveys by Vic. T. & Harry W. McCray [map]. http://digitalcollections.ucsc.edu/cdm/ref/collection/p15130coll3/id/1729, accessed February 3, 2020.

San Benito County Chamber of Commerce (SBCCC)

"History," http://www.discoversanbenitocounty.com/discover-san-benito-county/history/, accessed February 4, 2020.

Santa Cruz Sentinel

1976 Classified advertisement for Lico & Greco Farms. June 14. www.newspapers.com, accessed February 3, 2020.

2000 "Annie D. Greco," July 11. www.newspapers.com, accessed February 3, 2020.

TTI Developers

2020 Phase I Environmental Site Assessment: Vista Del Calabria, Enterprise Road (APNs 020-290-051 & -052), Hollister, California. January 16.

P5a. Photographs (continued):



Photograph 2. Barn, main (west) elevation. Camera facing east.

DPR 523L (1/95) \*Required information

State of California -- The Resources Agency DEPARTMENT OF PARKS AND RECREATION

## **CONTINUATION SHEET**

Primary # HRI# Trinomial

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\*Resource Name or # 213 Enterprise Road

\*Recorded by: James Williams, Rincon Consultants \*Date: February 3, 2020 ■Continuation □Update



Photograph 3. East Ancillary Building, west elevation. Camera facing northeast.



Photograph 4. West Ancillary Building, east elevation. Camera facing south.

DPR 523L (1/95) \*Required information

# Appendix E

Fault Evaluation Report

# FAULT EVALUATION REPORT LICO PROPERTY (APN 020-290-029) 213 ENTERPRISE ROAD SAN BENITO COUNTY, CALIFORNIA

# Expect Excellence ——

Mr. Bruce Myers Pacific Union Land Company, Inc. 675 Hartz Avenue, Suite 300

Danville, CA 94526

Submitted to:

Prepared by: ENGEO Incorporated

September 15, 2015

Project No: 11227.000.100

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Project No. **11227.000.100** 

September 30, 2015

Mr. Bruce Myers Pacific Union Land Company, Inc. 675 Hartz Avenue, Suite 300 Danville, CA 94526

Subject: Lico Property (APN 020-290-029)

213 Enterprise Road Hollister, California

#### **FAULT EVALUATION REPORT**

Dear Mr. Myers:

With your authorization, we prepared this report describing the results of our fault exploration at the Lico Property (APN 020-290-029) located at 213 Enterprise Road in Hollister, California. The accompanying report presents the findings of our exploration and our conclusions and recommendations regarding potential fault hazards at the site.

Evidence of faulting was encountered on the western portion of the site. In our opinion, hazards associated with fault rupture at the site can be mitigated by implementation of the fault setback recommendations provided in this report. Additional design-level exploration services will be required in the future in order to present grading, drainage, and foundation design recommendations. We are pleased to have been of service to you on this project and are prepared to consult further with you and your design team as the project progresses.

Sincerely,

**ENGEO** Incorporated

J. Brooks Ramsdell, CEG

\* CERTIFIED ENGINEERING GEOLOGIST ATE OF CALIFORNIA

Phillip Stuecheli, CEG

\*

CERTIFIED ENGINEERING GEOLOGIST OF CALFORD

\*

OF CALF

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#### **SELECTED REFERENCES**

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Figure 5 – USGS Earthquakes and Faults

Figure 6 – Compilation of Previous Fault Explorations

Figure 7 – Site plan

Figure 8 through 10 – Trench Logs

**APPENDIX A** – Soil Tectonics Report



#### 1.0 EXECUTIVE SUMMARY

The purpose of this investigation was to evaluate the potential for surface fault rupture along the eastern trace of the East Branch Calaveras Fault as identified on the Alquist-Priolo Earthquake Fault Zone map for the Hollister Quadrangle within the subject site. Our scope of work included the following:

- Review of regional geologic maps, publications, and consultant reports.
- Review of aerial photographs.
- Excavation and logging of five trenches at the proposed site and soil profile age assessment.
- Preparation of this report discussing our findings and providing recommendations for the mitigation of the impacts of surface fault rupture at the site.

#### 1.1 ALQUIST-PRIOLO EARTHQUAKE FAULT ZONE ACT

The Alquist-Priolo program requires the State Geologist, via the California Geological Survey (CGS) to establish regulatory zones around fault traces that are considered active and sufficiently well defined to create the potential for surface fault rupture hazards to structures. A fault trace is considered "active" if it is judged to have had identifiable surface rupture during the Holocene (defined by the CGS as the last 11,000 years). The State requires geological investigations prior to construction of new structures within Earthquake Fault hazard zones as described in CGS Special Publication 42 and Note 49. The policies and criteria of the State Mining and Geology Board with reference to the Alquist-Priolo Earthquake Fault Zoning Act are described in CGS Special Publication 42, Specific Criteria that include:

**Appendix B Section 3603 (a):** No structure for human occupancy, identified as a project under Section 2621.6 of the Act, shall be permitted to be placed across the trace of an active fault. Furthermore, as the area within fifty (50) feet of such active faults shall be presumed to be underlain by active branches of that fault unless proven otherwise by an appropriate geologic investigation and report prepared as specified in Section 3603(d) of this subchapter, no such structures shall be permitted in this area.

Appendix C Guidelines for Evaluating the Hazards of Surface Rupture: Setback distances of proposed structures from hazardous faults. The setback distance generally will depend on the quality of data and type and complexity of fault(s) encountered at the site.

#### 1.2 FAULT ZONE AND GEOLOGIC CONDITIONS

The CGS Alquist-Priolo (AP) Earthquake Fault Hazard Zone map for the Hollister Quadrangle depicts three traces of the Calaveras fault south of Hollister. The three traces comprise the West Branch Calaveras fault, located approximately ½ mile southwest of the subject property, and the



East Branch Calaveras fault, which consists of two fault traces on the southwestern and northeastern flanks of Hill 668 (Figure 3). The eastern trace of the east branch of the Calaveras fault is mapped near the western boundary of the subject site as shown on Figures 6 and 7. The site has been mapped as underlain by both Plio-Pleistocene-age San Benito Gravels (Rogers, 1993) and late Pleistocene to Holocene-age alluvium (Majmundar 1994 and Wagner, 2002).

#### 1.3 FINDINGS FROM TRENCH EXCAVATIONS

ENGEO excavated and logged five trenches across the mapped fault zone as depicted on Figure 7. The following is a summary of observed soil conditions exposed in the trench walls.

Evidence of faulting was observed in four out of the five trenches excavated at the site. The observed faults cut across the San Benito Gravels and offset the alluvial sediments, with evidence of vertical uplift on the west side. The faults observed in the trenches dipped towards the west, which is consistent with uplift along the pressure ridge to the west. The interpreted surface trace of the fault zone is depicted on Figure 7.

Soil weathering profile dating in Trenches T-1 and T-2 by Soil Tectonics provided an estimate of relative soil ages. Two paleosols were observed in the trenches. The paleosols were interpreted as late Pleistocene relict paleosols of approximately 40,000 and 80,000 years in age. The age dating of the soils exposed within the trenches indicates sufficient age for evaluation of fault activity. Pleistocene age alluvium was exposed in all of the trenches.

Based on the geologic conditions exposed in the trenches, we conclude that the trace of the East Branch Calaveras Fault at the west portion of the site shows evidence of movement during the Holocene. As described above, the guidelines for implementation of the Alquist-Priolo act state that fault setbacks should be based on the level of detail of the characterization and the complexity of the faulting, but do not mandate a 50-foot distance. The 50-foot clearance from traces shown on State maps is a requirement for construction within the zone in the absence of a site-specific geologic study. In our opinion, ENGEO has fulfilled the requirements for conducting a site-specific and detailed fault investigation. The fault zone exposed in the trenches is relatively well defined, and alluvial sediments estimated to be greater than 11,000 year in age are un-faulted east of the identified fault trace. It is, therefore, our opinion that habitable structures can be located as close as 25 feet from the eastern side of the identified fault trace. The recommended setbacks are depicted on Figure 7.

#### 2.0 INTRODUCTION

#### 2.1 PURPOSE AND SCOPE

The purpose of this investigation was to evaluate the potential for surface fault rupture along the eastern trace of the east branch Calaveras fault at the subject site as identified on the Alquist-Priolo Earthquake Fault Zone map for the Hollister Quadrangle. Our scope of work included the following:



- Review of regional geologic maps published by the U.S. Geological Survey (USGS), and California Geological Survey (CGS)
- Review of the California Geological Survey (CGS) Alquist Priolo Earthquake Fault Hazard Map for the Hollister Quadrangle and supporting documentation provided in the CGS Fault Evaluation Report for the Calaveras Fault.
- Review of stereo-paired historic aerial images flown in 1939, and available historic topographic maps.
- Review of selected fault hazard reports prepared for the subject site and adjacent parcels.
- Excavation and logging of five trenches at the site.
- Soil profile dating by Soil Tectonics, Inc.
- Preparation of this report.

The documents and maps reviewed for this study are described in the References. The results of the Soil Tectonics soil profile analysis are summarized in Appendix A.

This report was prepared for the exclusive use of our client and their consultants. In the event that any changes are made in the character, design or layout of the development, we must be contacted to review the conclusions and recommendations contained in this report to determine whether modifications are necessary.

#### 2.2 ALQUIST-PRIOLO EARTHQUAKE FAULT ZONE ACT

The Alquist-Priolo program requires the State Geologist, via the California Geological Survey (CGS) to establish regulatory zones around fault traces that are considered active and sufficiently well defined to create the potential for surface fault rupture hazards to structures. A fault trace is considered "active" if it is judged to have had identifiable surface rupture during the Holocene (defined by the CGS as the last 11,000 years). The State requires geological investigations prior to construction of new structures within Earthquake Fault hazard zones as described in CGS Special Publication 42 and Note 49. The policies and criteria of the State Mining and Geology Board with reference to the Alquist-Priolo Earthquake Fault Zoning Act are described in CGS Special Publication 42, Specific Criteria that include:

**Appendix B Section 3603 (a):** No structure for human occupancy, identified as a project under Section 2621.6 of the Act, shall be permitted to be placed across the trace of an active fault. Furthermore, as the area within fifty (50) feet of such active faults shall be presumed to be underlain by active branches of that fault unless proven otherwise by an appropriate geologic investigation and report prepared as specified in Section 3603(d) of this subchapter, no such structures shall be permitted in this area.



Appendix C Guidelines for Evaluating the Hazards of Surface Rupture: Setback distances of proposed structures from hazardous faults. The setback distance generally will depend on the quality of data and type and complexity of fault(s) encountered at the site.

#### 2.3 PROJECT LOCATION

The site consists of a single parcel (APN 020-290-029) located between south of Enterprise Road in San Benito County just south of Hollister, California (Figure 1). APN 020-290-029 is bordered by Enterprise Road on the north, and existing residential development on the south, east and west.

The current topography of the site can generally be characterized as gently sloping towards the north with steeper slopes near the flanks of the northwest-trending elongate hill (Hill 668) along the west property line. Current elevations range from a high of about 480 feet (NAVD88) in the southwest corner of the site to approximately 345 feet in the northwest corner of the site.

The southern parcel is currently occupied by grassland and orchards with a farmhouse and related structures located in the northern portion of the site.

#### 2.4 PROJECT DESCRIPTION

Although no formal plans are available at this time, preliminary plans prepared by MacKay and Somps (April 14, 2015) show the proposed development of approximately 150 single-family residential lots, with interior roadways, and open space areas.

#### 2.5 REGIONAL GEOLOGY

The site is located within the Coast Ranges geomorphic province of California. The Coast Ranges province is typified by a system of northwest trending, fault-bounded mountain ranges and intervening alluviated valleys. Bedrock in the Coast Ranges consists of igneous, metamorphic, and sedimentary rocks that range in age from Jurassic to Pleistocene. The present geology of the Coast Ranges is the result of deformation and deposition along the tectonic boundary between the North American plate and the Pacific plate. Plate boundary fault movements are largely concentrated along the well-known fault zones, which in the area include the San Andreas, Calaveras, and Hayward faults, as well as other lesser-order faults.

#### 2.6 LOCAL GEOLOGY

The site is located approximately 4 miles northeast of the San Andreas fault in the southern portion of the Hollister Valley. The local site geology has been shaped predominately by deformation along the Calaveras fault, with linear fault-bounded pressure ridges exposing Plio-Pleistocene San Benito Gravels elevated above the surrounding Pleistocene and Holocene alluvium.



The site is underlain primarily by terrestrial granular sedimentary deposits ranging from Holocene to Plio-Pleistocene Age. The site geology has been mapped by Wagner (2002), Majmundar (1994), Rogers (1993), and Dibblee and Rogers (1975) as underlain by the following (Figure 2):

- <u>Holocene Alluvium (Q)</u> located at the former creek channel in the northeastern most portion of the site.
- <u>Late Pleistocene Alluvium (Qo) or Pleistocene terrace deposits</u> across the majority of the site located east of the prominent fault bound pressure ridge (Hill 668). Majmundar (1994) maps these deposits continuing towards the west and underlying Hill 668.
- <u>Plio-Pleistocene Continental Deposits (QT) or San Benito Gravels</u> underlying Hill 668 along the west site boundary. Rogers (1993) interprets areas mapped by others as Pleistocene terrace deposits as underlain by the San Benito Gravels and thus maps the majority of the site as underlain by the San Benito Gravels.

The Holocene and Pleistocene alluvium is characterized as undifferentiated floodplain deposits comprising unconsolidated to semi consolidated sand, gravel, silt and clay. Pleistocene alluvium typically occupies terraces that are elevated above the current drainage courses. The Plio-Pleistocene San Benito Gravels generally comprises poorly bedded sandy gravels with cobbles and moderately well bedded and commonly crossbedded gravelly sands with some silt. In the vicinity of the site, bedding within the Pleistocene alluvium has been mapped as gently dipping 10 to 20 degrees in a variably northern direction. The Plio-Pleistocene San Benito Gravels has been mapped as generally northwest to east-west striking and dipping to the north from 20 to 40 degrees (Wagner, 2002).

#### 2.7 CALAVERAS FAULT

The Calaveras fault is a major branch of the overall San Andreas fault system in northern California. The Calaveras fault diverges towards the east from the San Andreas fault approximately 5 to 10 miles south of the site and extends approximately 80 miles to the north-northwest where it dies out near the town of Danville.

The history of mapping and identification of the Calaveras fault zone in the vicinity of the site as identified on the Hollister 7.5 minute Quadrangle is described in the Fault Evaluation Report (FER-94) by Hart (1979). In 1974, the CDMG established Special Studies Zones (SSZ) around the Calaveras fault zone based on the mapping of Nason (1971), Radbruch (1968), Rogers (1973), and Taliaferro (1948).

South of Hollister the Calaveras fault zone is mapped as three fault traces. The three fault traces comprise the West Branch Calaveras fault, located approximately ½ mile southwest of the subject property, and the East Branch Calaveras fault, which comprises two fault traces on the southwest and northeast flanks of Hill 668 (Figure 3).



According to FER-94, the West Branch Calaveras fault is described as the main trace of the fault. Fault creep is well documented along this trace of the fault with evidence of 13 inches of right lateral strike slip displacement from 1909 through 1971 (Hart, 1979). More recent evaluations of creep along this trace of the fault by Galehouse and Lienkaemper (2003), documented creep rates of 6.4 and 12.2 mm/year at two sites in the Hollister area. Creep along the main trace occurs in a zone that varies from approximately 10 to 50 feet wide (Hart, 1979).

The East Branch Calaveras fault comprises two fault traces on both sides of Hill 668 based on Radbruch (1968) and Rogers (1973). According to Kilburn (1972) the East Branch Calaveras fault acts as a groundwater barrier and the water table is 20 to 25 feet higher on the east side of the fault(Hart, 1972). The east trace of the East Branch Calaveras fault is mapped in the vicinity of the west property line of the subject site (Figure 3).

The epicenters for earthquakes and numerous micro-earthquakes have been plotted near the mapped surface traces of the Calaveras fault (Hart, 1979, Sleeter, et al., 2004). The distribution of earthquakes clearly defines the overall trend and approximate location of the Calaveras fault as it diverges from the San Andreas fault in a northwesterly direction (Figure 4).

The most recent earthquake on the Calaveras fault with a moment magnitude of 6 or greater occurred on April 24, 1984, in the vicinity of Morgan Hill. The 1984 Morgan Hill Earthquake had an approximate moment magnitude of 6.2. A larger (M~6.5) earthquake is thought to have occurred on the Calaveras fault on July 1, 1911. Other relatively recent notable earthquakes attributed to the Calaveras fault include the October 30, 2007, moment magnitude 5.6, Alum Rock Earthquake; the August 6, 1979, moment magnitude 5.7 Coyote Lake Earthquake; January 7, 2010 moment magnitude 4.1.

The USGS has published the Quaternary Fault and Fold Database (QFFD) a nationwide database of Quaternary-active faults. According to the QFFD, the above-described traces of the Calaveras fault at and in the vicinity of the site are considered to be Holocene to Latest Pleistocene age faults (defined as active within the last 15,000 years by the Database). As shown on Figures 3 and 6, the CGS and USGS have mapped the eastern trace of the East Branch Calaveras Fault through western portions of the subject property.

#### 2.8 REGIONAL SEISMICITY

Because of the presence of nearby active faults, the Central Coast Region of California is considered seismically active. Numerous small earthquakes occur every year in the region, and large (>M7) earthquakes have been recorded and can be expected to occur in the future. The site is located within the Earthquake Fault Hazard Zone for the Calaveras Fault (Figure 3). Figure 4 shows the approximate location of active and potentially active faults and significant historic earthquakes mapped within the Central Coast Region. Based on the 2008 USGS National Seismic Hazard Maps database, the nearest active fault is the Calaveras fault, located very near the western boundary of the subject site. Other active faults located near the site include the San Andreas fault, located approximately 4 miles to the southwest, the Quien Sabe fault, located approximately 5 miles to the northeast; the Zayante Vergeles fault located approximately 5 miles



to the west, the Ortigalita fault located approximately 20 miles to the northeast and the Rinconada fault located approximately 21 miles to the southwest. These faults have estimated maximum moment magnitudes (Mw) of 7.0, 7.9, 6.6, 7.0, 7.1 and 7.5, respectively. Although not included on the 2008 National Seismic Hazard Maps database the Sargent fault is also considered active by the CGS and USGS and is located approximately 4 miles northwest of the site.

The Uniform California Earthquake Rupture Forecast (UCERF 2013) evaluated the 30-year probability of a M6.7 or greater earthquake occurring on the known active fault systems in California. The UCERF generated a probability of 16 percent for the Calaveras fault, 15 percent for the San Andreas fault, 0.72 percent for the Sargent fault, 0.3 percent for the Quien Sabe fault, 0.1 percent for the Zayante Vergeles fault, 1.9 percent for the Ortigalita fault and 0.3 percent for the Rinconada fault.

### 2.9 GEOMORPHOLOGY

The subject site is located on an elevated alluvial terrace on the east side of a northwest trending fault-bound pressure ridge (Figure 6). A relatively prominent break in slope occurs along the east edge of the pressure ridge at the western portion of the site. At a few locations, the break in slope along the property line is relatively linear and at others, it is more subdued. An access road to neighboring properties was graded along the east flank of the pressure ridge slightly obscuring the current geomorphology in the area. In 1939, stereo-paired aerial photographs covering the site shows a relatively linear, northwest trending trough is visible along the pressure ridge approximately 275 feet west of the property line. A more subdued northwest trending swale is visible at the base of the pressure ridge along the west side of the property. Northwest trending, linear tonal variations are visible in the 1939 aerial photographs at the west portion of the site. These tonal variations correspond closely with the location of the CGS mapped fault trace at the site. Based on our review, the geomorphology visible in the 1939 aerial photographs is suggestive of an anastomosing series of faults that straddle and crosscut the pressure ridge.

### 2.10 PREVIOUS INVESTIGATIONS

The following section provides a summary of pertinent aspects of previous fault explorations performed by others at the site.

### 2.10.1 Leighton Associates 1974

Lieghton Associates (LA) performed a fault hazard study (1974) on selected portions of the roughly 400-acre Ridgemark Estates development located just south of the Lico Property. The scope of work included review of published geologic maps and reports, geologic mapping, aerial photograph interpretations, and excavation and logging of eleven exploratory trenches. Leighton Associates identified the eastern trace of the East Branch Calaveras fault in trenches T-2 and T-4 excavated across the mapped fault trace. The LA Trench T-2 was located approximately 150 feet south of the Lico Property along the mapped fault trace (Figure 6). Based on their observations with regard to the cross cutting relationships exposed in the two trenches it was concluded that the



fault is potentially active to active. The fault trace exposed in trench T-2 was mapped extending into the Lico Property along a northwesterly trend. An active east-west trending secondary fault trace was identified by LA on the south flank of Hill 668. This secondary fault is located approximately 1500 feet southwest of the Lico Property.

### 2.10.2 Earth Systems 2004

Earth Systems (ES) performed a geological fault investigation at the southern portion of the subject site in 2004. The scope of work included review of geologic reports and maps, aerial photograph interpretations, and excavation and logging of two exploratory trenches. As part of the ES investigation, they reviewed an unpublished Pacific Geotechnical Engineering report covering the property near the southeast corner of the Lico Property. According to the ES 2004 report, the Pacific Geotechnical Engineering investigation found no evidence of faulting on the property located to the southeast.

Earth Systems exploration included the excavation of two trenches T-1 and T-2. The approximate locations of the ES trenches are shown on Figure 6. The ES trenches encountered clay and sand beds overlying sand and gravel beds interpreted as overbank and stream channel deposits of the San Benito Formation. The ES report concluded that no evidence of faulting was observed in the trench exposures at the site.

Soil Tectonics prepared a pedochronological report as an appendix to the ES 2004 report. A soil profile survey was performed at the location of both trenches T-1 and T-2. The soil profiles exposed at the locations of the trenches were concluded to be considerably greater than 10,000 years old (34,000 to 40,000 years old).

### **2.10.3 Earth Systems 2007**

Earth Systems (ES) performed a geological fault investigation at the Lico Property Parcel located on the north side of Enterprise Road just north of the subject site. The scope of work included a site reconnaissance, review of available geologic reports and maps, review of stereo-paired aerial photographs, and excavation and logging of seven exploratory trenches.

The ES trenches encountered lake/alluvial deposits and San Benito formation (Figure 6). According to the ES report marker, beds within the lake alluvial deposits and the San Benito formation were observed to be relatively unbroken within the trench exposures. Radiocarbon testing of the lake alluvial deposits indicate an age of about 2000 years at a depth of about 8 feet below the ground surface. ES concluded that no fault related features were observed within the trench exposures at the site and that the lake alluvial deposits at a depth of about 10 feet should be old enough to have exhibited fault related features if the Eastern Branch Calaveras fault crossed the portion of the site that had been explored.



### 2.10.4 Earth Systems Unpublished Trench Log, 2008

In 2008, Earth Systems performed additional fault trenching on the Lico Property Parcel located north of Enterprise Road (Figure 6). Based on our review of the ES trench log, exposures within the trench walls comprised Holocene alluvial flood plain deposits underlain by fluvial sands and gravels. The fault trench was approximately 20 feet deep with a deepened section up to 30 feet in depth. Radiocarbon dating yielded an age of 2510 year for the fluvial sands and gravels at the base of the trench and an age of 7720 for a consolidated clay layer at a depth of approximately 25 feet below the ground surface. No reference to fault related features is depicted on the trench log.

### 3.0 SITE EXPLORATION

### 3.1 TRENCH EXCAVATIONS

We excavated and logged a total of approximately 1,150 feet of trench as depicted on Figures 8, 9, and 10. The trenches were excavated with a tracked excavator to depths ranging from approximately 5 to 16 feet. The excavations were benched or shored for safety and the south walls of the trenches were cleaned of smeared materials and logged by ENGEO geologists as noted on the logs. The trench locations and significant features were located by measuring from existing fence lines. The location of the trenches are shown on Figure 7.

The purpose of the trench excavations was to expose the alluvial deposits and San Benito Gravels so that they could be closely examined for evidence of recent fault displacement. The geologic logging process included description of soil color, estimated grain size, structure and interpretation of geologic features such as development of soil weathering profiles, depositional layering and contacts between differing soil layers.

Soil features described on the log include the soil color based on the Munsell color chart, the relative development of blocky prismatic structure, the relative accumulation of translocated clay as films on soils grains and fracture surfaces, and the accumulation of pedogenic (weathering-derived) calcium carbonate, gypsum, and manganese oxides.

We retained Dr. Glenn Borchardt to provide detailed pedochronologic descriptions of represented weathering profiles developed in the Trenches 1 and 2 at the locations noted on the log. The purpose of the pedochronologic description was to correlate the soils observed onsite with nearby dated profiles and to estimate the age of weathering profiles. The results of Dr. Borchardt's study are presented in Appendix A.

The trenches were northeast trending and oriented roughly perpendicular with previously mapped fault traces. Trench T-1 was excavated from the west property line across the west portion of the site to the east limit of the AP Earthquake Fault Hazard Zone (Figure 7). Trench T-2 was excavated from the east edge of the paved driveway at the west property line, through the west portion of the orchard in the northern portion of the site. Trench T-3 was excavated from the west property line towards the northeast. Trench T-4 was excavated from the southwest property corner towards the northeast and Trench T-5 was excavated across the northwestward



projection of the fault exposed in the 1974 Leighton Associates fault trench located south of the subject site. Evidence of faulting was encountered in trenches T-1, T-3, T-4, and T-5.

#### 3.2 SUBSURFACE CONDITIONS

### 3.2.1 Fill (F)

A wedge of fill was encountered adjacent to the driveway at the west end of trenches T-1 and T-2. The fill was likely generated from adjacent cuts during grading for the driveway. The fill encountered generally consists of lean sandy clay with scattered gravel.

### 3.2.2 Modern to Holocene Age soils and Alluvium (2A, 2B and 3)

The uppermost soil layers in all five trenches is a dark gray brown to dark yellowish brown sandy clay. These soils appear to be disturbed from bioturbation with many krotovina throughout the soil column. These soils are slightly plastic when wet. At many locations in the trenches, the contact between these upper soils and the underlying deposits is sharp. We interpret this as likely indicating an unconformity and deposition on an erosional surface. At locations where these soils overly faults, they are not visibly sheared but they do show minor to more significant changes in thickness. This type of soil would be unlikely to preserve subtle fractures or shearing that could result from small surface fault displacements.

### 3.2.3 Pleistocene Alluvium (4A, 4B, 4C, 4D and 5)

Interbedded sandy clay and sandy to clayey gravel with cobbles were encountered in the trenches below the younger Holocene soils. These deposits generally display strong clay film development, blocky ped structures, with manganese oxide coatings, and well-developed carbonate horizons. Relatively thick clay films are present coating the gravels and cobbles. These deposits are interpreted to be older alluvium of Pleistocene age. In the trenches where faulting was observed, these units are visibly offset, tilted and deformed near the fault.

### 3.2.4 Plio Pleistocene San Benito Gravels (6A and 6B)

Coarse sands and gravels interbedded with finer grained dense sand to clayey sand was encountered below the Pleistocene alluvium within all of the trenches with the exceptions of trench T-2 located in the northern portion of the site. At some locations, the sands and gravels displayed planar beds and some cross beds. Coarse gravels and cobbles within the unit generally comprised granodiorite, sandstone, volcanics, chert, and greenstone. We interpret these deposits as San Benito Gravels.

Bedding within the sands and gravels generally dips gently towards the north except where it was observed to be tilted near the fault. Near the fault in trench T-1 bedding was observed striking towards the northwest and dipping from 30 to 40 degrees. A drag fold was observed within the



San Benito Gravels adjacent to the fault. Within a distance of less than 20 feet from west to east, bedding was observed to go from a dip of 40 degrees to 15 degrees.

#### 3.3 FAULTING

### 3.3.1 T-1

Trench T-1 was excavated from the west property line towards the northeast at the northern half of the site (Figure 7). In T-1, we encountered a well-defined fault at the extreme southwest end of the trench. Our trench appeared to intersect the eastern edge of the fault zone at a point where the fault was transitioning (rolling over) to a relatively low angle as it approached the surface. The fault comprised a southwest-dipping zone of sheared and disrupted clayey sand that truncates northeast dipping sand and gravel beds of the San Benito Gravels. The approximate strike and dip of the fault zone was measured as N47W 14SW Bedding within the sands and gravels near the base of the fault were disrupted to the point where no bedding or sedimentary structures were discernible. The fault appeared to steepen towards the southwest near the end of the trench. The overlying Pleistocene alluvium was tilted and offset and the younger Holocene soils were very thin overlying the fault. The thin modern soils is likely related to the uplift and erosion adjacent to the fault. The modern soils were observed to thicken towards the northeast of the fault and appeared to be slightly warped. A sharp linear contact within the Holocene soils interpreted as evidence of ponding water was observed within the soils east of the fault. This contact was tilted towards the southwest by approximately 2 degrees.

#### 3.3.2 T-2

Trench T-2 was excavated at the northern portion of the site just east of the paved access roadway/driveway (Figure 7). No evidence of faulting was observed in trench T-2. Based on the geomorphology, review of aerial photographs and the mapped location of the fault we interpret the location of the fault to be just west of the southwest end of the fault trench.

#### 3.3.3 T-3

Trench T-3 was excavated south of Trench T-1 from the west property line towards the northeast (Figure 7). Evidence of faulting was observed near the southwest end of the trench. A southwest dipping fault was observed to offset the San Benito Gravels near Station 0+35. The approximate strike and dip of the fault zone was measured as N45W 16SW. A dense fine-grained sand interpreted as San Benito formation was offset and disrupted at the location of the fault. The younger overlying soils were relatively thin and were observed to thicken slightly towards the southwest. No evidence of faulting was observed within the thin soils overlying the fault. We interpret the relatively thin and at one location completely absent Holocene soils at this location as related to uplift, warping and erosion on the northeast flank of the pressure ridge.



#### 3.3.4 T-4

Trench T-4 was excavated from the southwest corner of the property towards the northeast. In T-4 we encountered a fault at approximately Station 1+45 near the northeast end of the trench. The fault comprised a southwest-dipping zone of sheared and disrupted gravel and clayey sand. The approximate strike and dip of the fault zone was measured as N55W 35SW. A highly disrupted zone of clayey sand of the San Benito formation is present southwest of the fault. The overlying soils were observed to be offset slightly (less than 6 inches). The rough sense of movement was up on the southwest indicating that the southwest dipping fault was accommodating transpressional deformation and uplift along the pressure ridge located to the southwest.

#### 3.3.5 T-5

Trench T-5 was excavated near the southern property boundary across the northern projection of the mapped fault trace (Figure 7). Two fault zones were encountered at the southwest portion of Trench T-5. At approximately Station 0+10 a southwest dipping fault was encountered. The approximate strike and dip of the fault zone was measured as N45W 55SW The fault was observed to slightly offset sand and gravel beds within the San Benito Gravels. A disrupted zone of Pleistocene alluvium was observed overlying the fault. The overlying Holocene soils did not appear to be disrupted by the fault at this location.

At approximately Station 0+45 a southwest dipping fault was encountered. The approximate strike and dip of the fault zone was measured as N35W 30SW. The fault was observed to truncate sand and gravel units of the San Benito formation and the sense of movement was up on the southwest. Wedges of disrupted San Benito sands and gravels were observed within the fault zone. The overlying Pleistocene alluvium was disrupted and offset within the zone of faulting. A slight warping of the overlying surficial soils was observed near the fault.

### 4.0 DISCUSSION AND CONCLUSIONS

Previous consultant studies along the East Branch Calaveras have discovered evidence of fault rupture in soils interpreted to be latest Pleistocene to Holocene age. Based on the Leighton Associates (1974) fault investigation for the Ridgemark Development a structural setback for dwellings was established just south of the Lico Property. Earth Systems (2004) performed a fault exploration at the southern portion of the subject property and concluded that no evidence of active faulting was observed within the two trench exposures at the site. A 50-foot setback for structures for human occupancy was recommended from the west ends of the Earth Systems trenches to account for uncertainty with regards to faulting west of the trenches.

Trenches excavated for this study found evidence for surface faulting that is likely to be of Holocene age based on the following observations:

• The Holocene/modern soil horizon is warped and thickens towards the east at the approximate location of the fault zone in Trench T-1.



- A Holocene soil horizon indicative of ponding water located just east of the fault in Trench T-1 is visibly tilted towards the southwest by approximately 2 degrees indicating Holocene tilting of a localized area just east of the fault.
- The Holocene/modern soil horizon thickens near the west end of the trench and thins towards the east in Trench T-3. We interpret this as evidence of tilting towards the southwest similar to what was observed in Trench T-1.
- Alluvium of latest Pleistocene to Holocene age is offset by faults in Trenches T-1, T-4 and T-5. Layers identifiable across the faults are offset up to 6 inches vertically.
- In Trench T-1 and T-5, the alluvium is relatively thin west of the fault and thickens significantly east of the fault. The faults exposed in the trenches all dip towards the southwest. These observations suggests that the fault has a vertical component of up on the west movement. This is consistent with the geomorphology at the site, which indicates the presence of a linear pressure ridge west of the site. The geometry of faults exposed in the trenches are consistent with the interpretation that they are located on the east edge of a fault flower structure that underlies the pressure ridge west of the site.

### 5.0 **RECOMMENDATIONS**

Four of the five trench excavations encountered relatively narrow zones of faulting. Pleistocene age and older deposits east of the faults exposed in the trenches are continuous and show no evidence of ground surface rupture. The guidelines for implementation of the Alquist-Priolo act state that fault setbacks should be based on the level of detail of the characterization and the complexity of the faulting, but do not mandate a 50-foot distance. The 50-foot clearance from traces shown on State maps is a requirement for construction within the zone in the absence of a site-specific geologic study. In our opinion, ENGEO has fulfilled the requirements for conducting a site-specific and detailed fault investigation. The fault zone exposed in the trenches is relatively simple and well defined, and alluvial sediments estimated to be greater than 11,000 year in age are un-faulted east of the identified fault trace. Based on the results of this study we have the following recommendations:

- Structures intended for human occupancy should be set back from the fault zone trace a minimum of 25 feet as depicted on Figure 7.
- It will be acceptable to construct improvements such as roads, parking lots, detention basins, parks, and underground utilities within the recommended fault setback zones. However, these improvements may be susceptible to damage in the event of fault rupture.
- If possible, lifeline utilities such as fire protection water lines should be situated to avoid
  crossing the active fault trace where possible, or provided with shutoff valves at fault
  crossings.



### 6.0 LIMITATIONS AND UNIFORMITY OF CONDITIONS

If changes occur in the nature or design of the project, we should be allowed to review this report and provide additional recommendations, if any. It is the responsibility of the owner to transmit the information and recommendations of this report to the appropriate organizations or people involved in design of the project, including, but not limited to, developers, owners, buyers, architects, engineers, and designers. The conclusions and recommendations contained in this report are solely professional opinions and are valid for a period of no more than 2 years from the date of report issuance.

We strived to perform our professional services in accordance with generally accepted geotechnical engineering principles and practices currently employed in the area; no warranty is expressed or implied. There are risks of earth movement and property damages inherent in building on or with earth materials. We are unable to eliminate all risks or provide insurance; therefore, we are unable to guarantee or warrant the results of our services.

This report is based upon field and other conditions discovered at the time of report preparation. We developed this report with limited subsurface exploration data. We assumed that our subsurface exploration data is representative of the actual subsurface conditions across the site. If unexpected conditions are encountered, notify ENGEO immediately to review these conditions and provide additional and/or modified recommendations, as necessary.

Actual field or other conditions will necessitate clarifications, adjustments, modifications or other changes to ENGEO's documents. Therefore, ENGEO must be engaged to prepare the necessary clarifications, adjustments, modifications or other changes before construction activities commence or further activity proceeds. If ENGEO's scope of services does not include on-site construction observation, or if other persons or entities are retained to provide such services, ENGEO cannot be held responsible for any or all claims arising from or resulting from the performance of such services by other persons or entities, and from any or all claims arising from or resulting from clarifications, adjustments, modifications, discrepancies or other changes necessary to reflect changed field or other conditions.



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### **FIGURES**

Figure 1 – Vicinity Map

Figure 2 – Regional Geology Map

Figure 3 – Earthquake Fault Zone Map

Figure 4 – Regional Faulting and Seismicity

Figure 5 – USGS Earthquakes and Faults

**Figure 6 – Compilation of Previous Fault Explorations** 

Figure 7 – Site plan

Figure 8 through 10 – Trench Logs











BASE MAP SOURCE: GOOGLE EARTH PRO



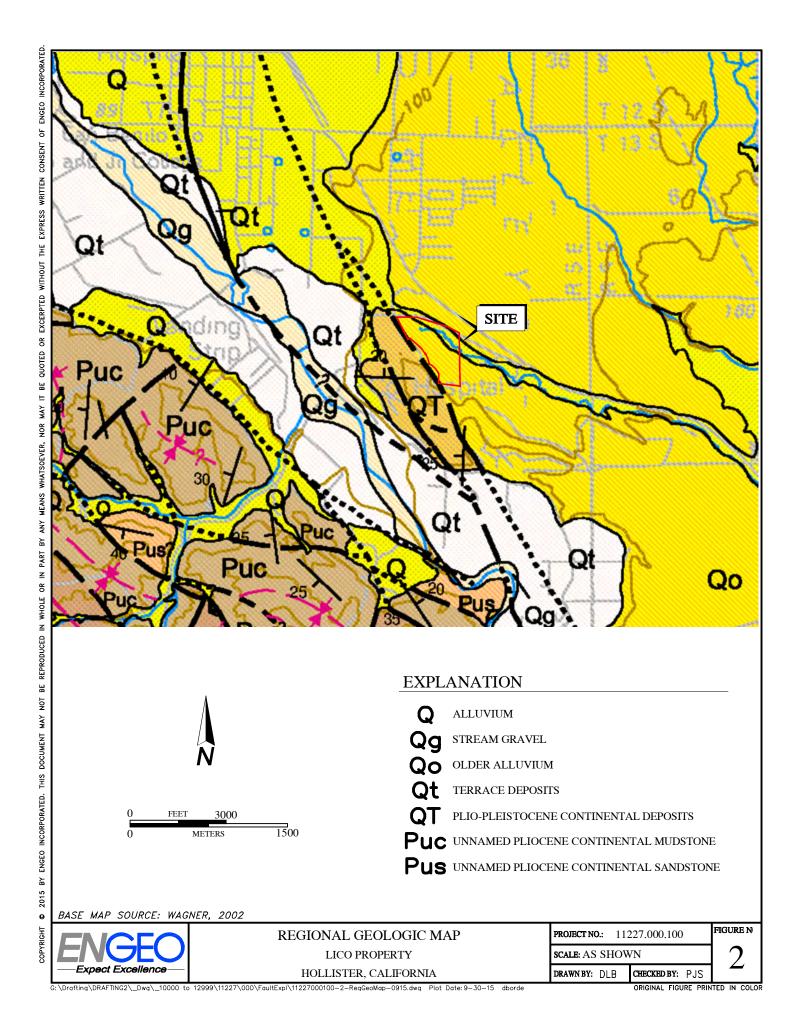
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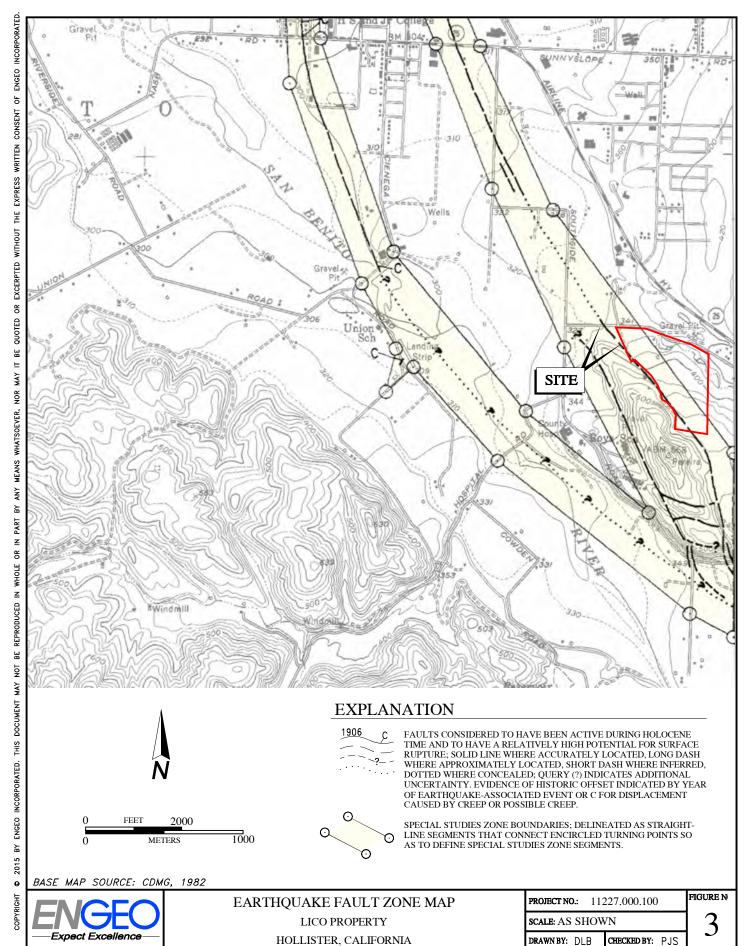
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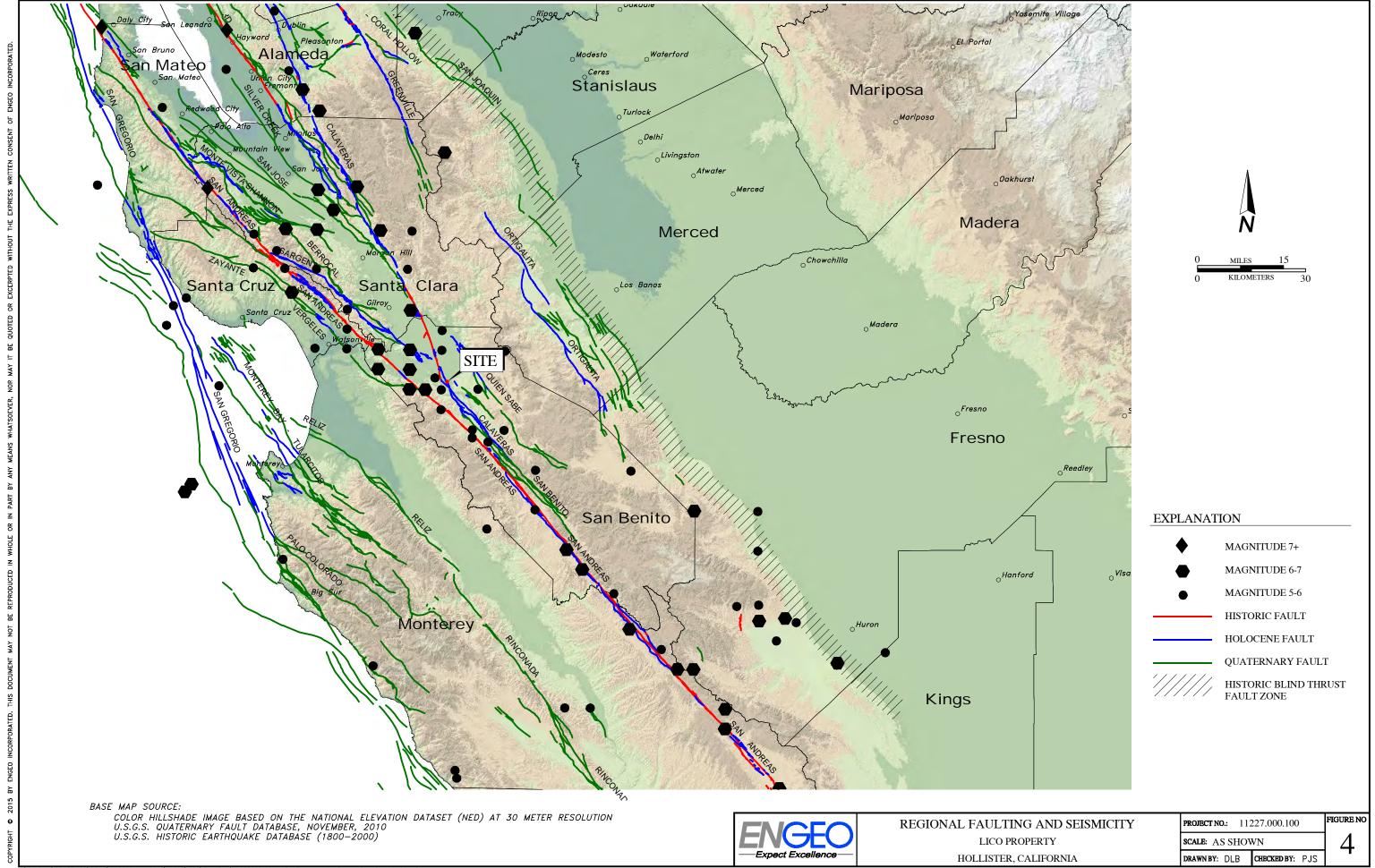
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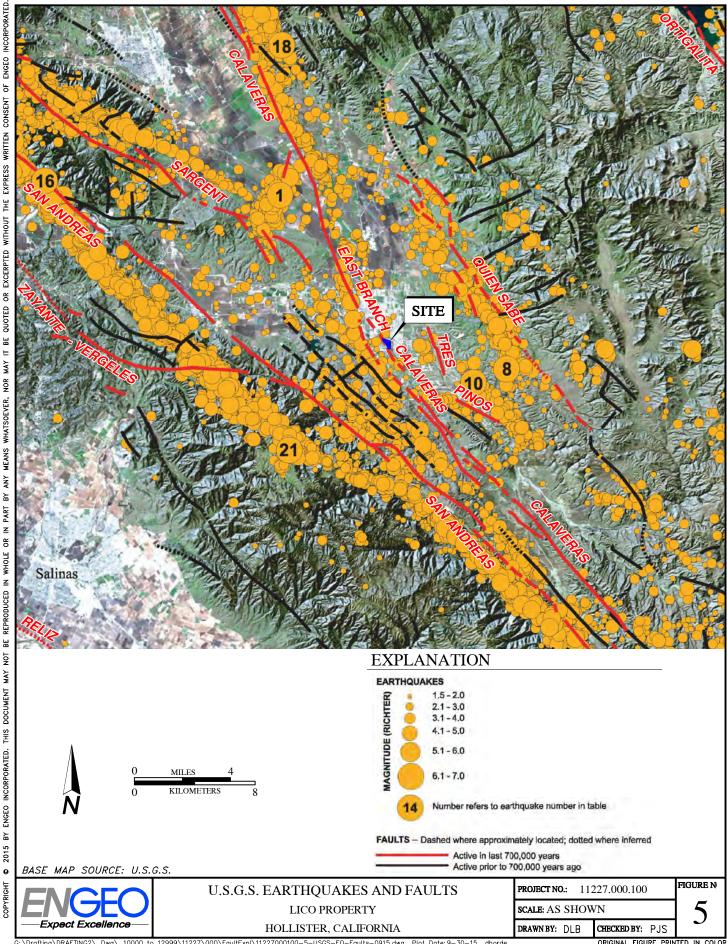
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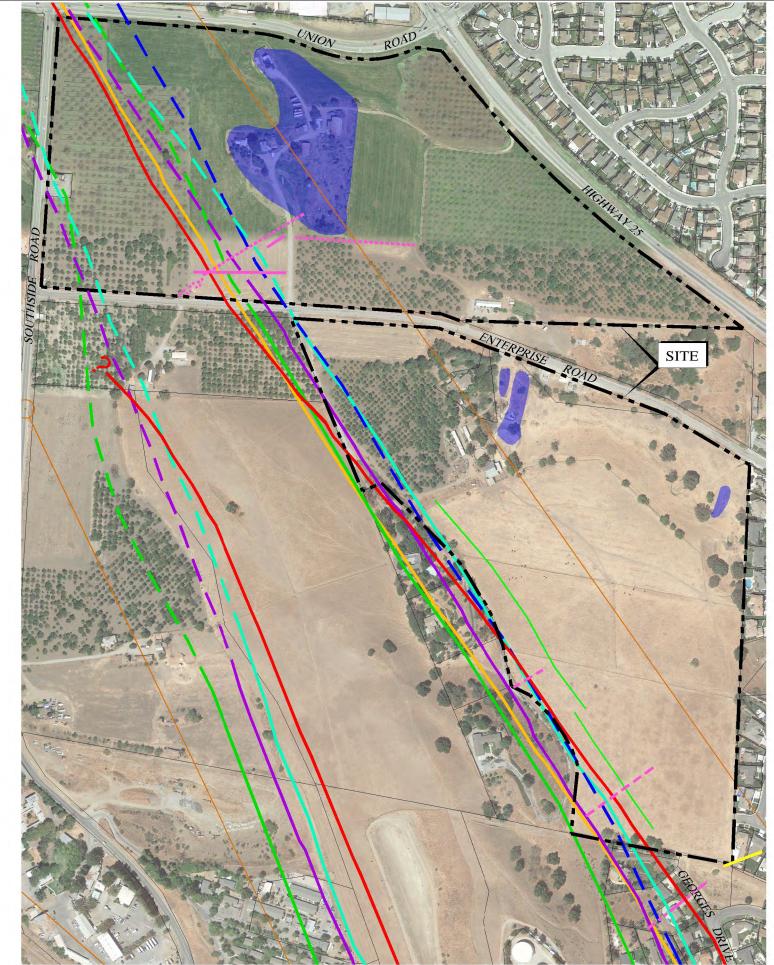
FIGURE N















### **EXPLANATION**

ALL LOCATIONS ARE APPROXIMATE FAULT LOCATION - WAGNER, 2002 FAULT LOCATION - MAJMUNDAR, 1994 FAULT LOCATION - ROGERS, 1993 FAULT LOCATION - ALQUIST-PRIOLO, 1982 FAULT LOCATION - DIBBLEE, 1975 FAULT LOCATION - RADBRUCH-HALL, 1974 LIMIT OF SPECIAL STUDIES ZONE PREVIOUS FAULT TRENCH (EARTH SY STEMS, 2008) PREVIOUS FAULT TRENCH (EARTH SY STEMS, 2007) PREVIOUS FAULT TRENCH (EARTH SY STEMS, 2004) PREVIOUS FAULT TRENCH (PACIFIC GEOTECHNICAL, 1991) FAULT TRENCH (LEIGHTON AND ASSOCIATES 1974) TONAL LINEAMENT (1998 AERIAL PHO/TO) UNDOCUMENTED FILL

BASE MAP SOURCE: GOOGLE EARTH PRO



COMPILATION OF PREVIOUS FAULT EXPLORATION | PROJECT NO.: 11227.000.000 LICO PROPERTY

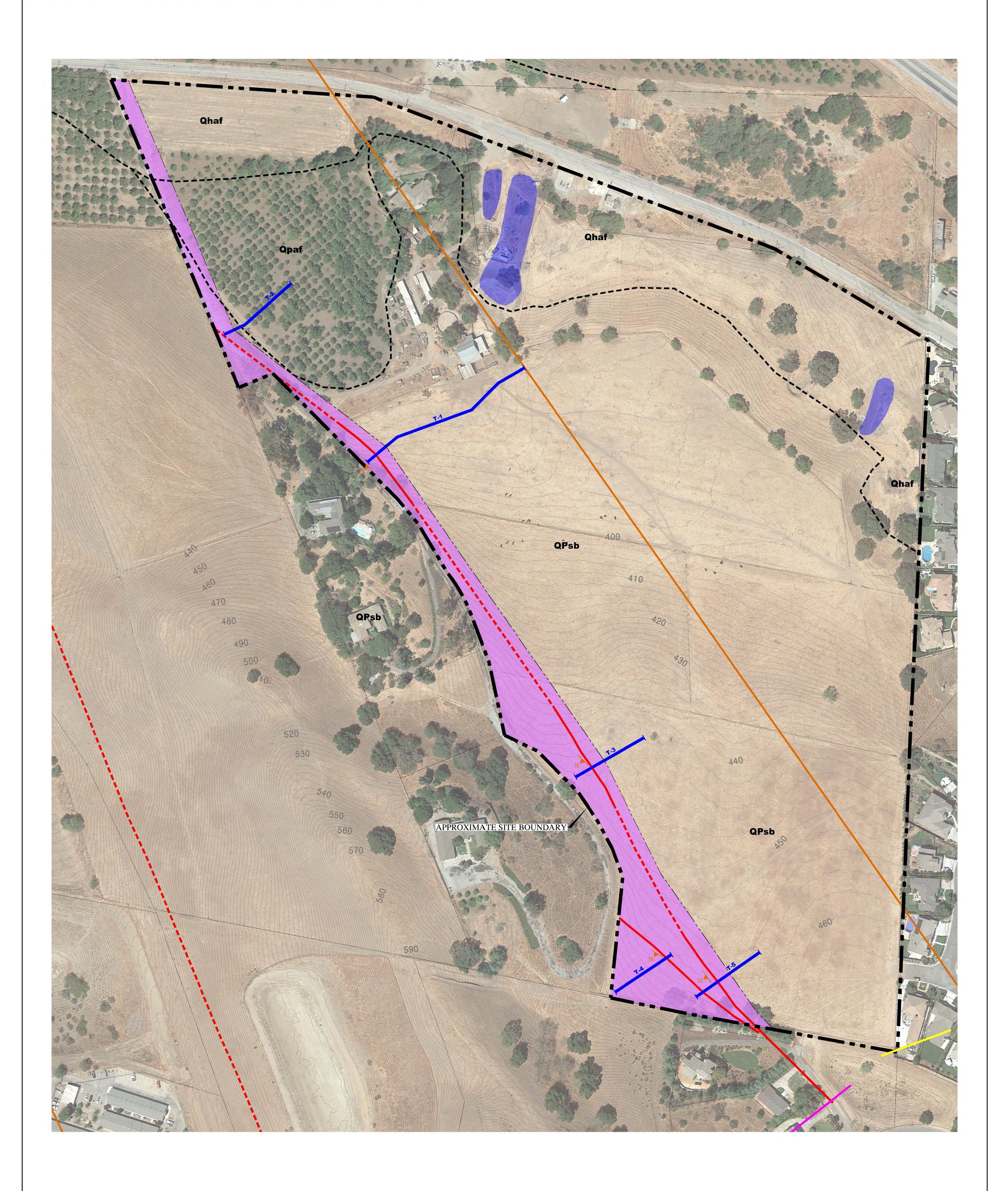
HOLLISTER, CALIFORNIA

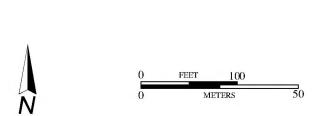
SCALE: AS SHOWN

DRAWN BY: DLB CHECKED BY: PJS

FIGURE NO

6





EXPLANATION

ALL LOCATIONS ARE APPROXIMATE

LIMIT OF SPECIAL STUDIES ZONE

FAULT TRENCH (ENGEO, 2015)

PREVIOUS FAULT TRENCH (PACIFIC GEOTECHNICAL, 1991)

FAULT TRENCH (LEIGHTON AND ASSOCIATES 1974)

EXISTING FILL

■ ■ ■ ■ ■ GEOLOGIC CONTACT

Qhaf ALLUVIUM (HOLOCENE)

Qpaf ALLUVIUM (PLEISTOCENE)

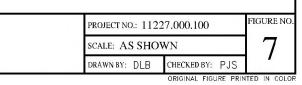
QPsb SAN BENITO FORMATION (PLIO-PLEISTOCENE)

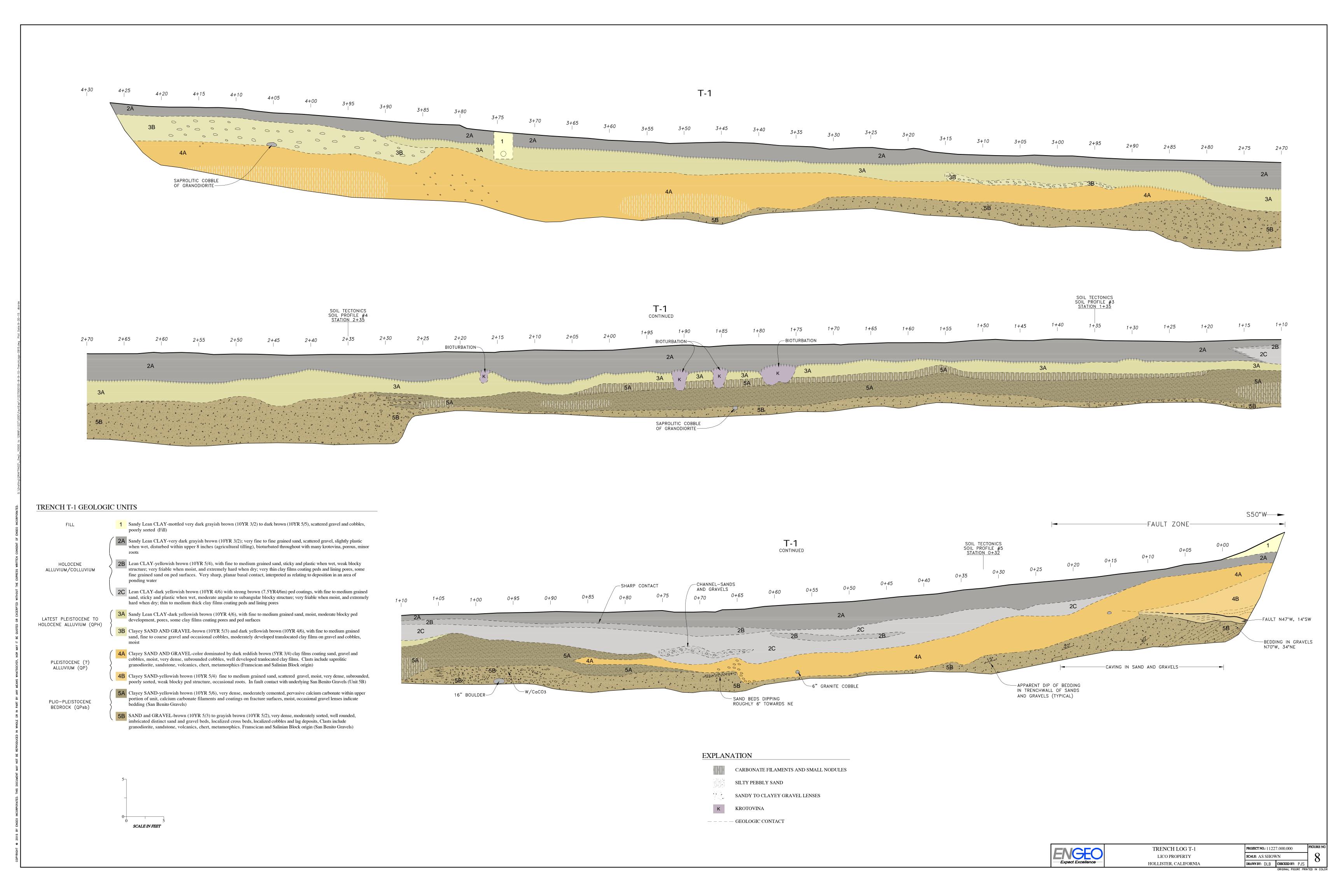
STRIKE AND DIP OF SHEAR PLANE

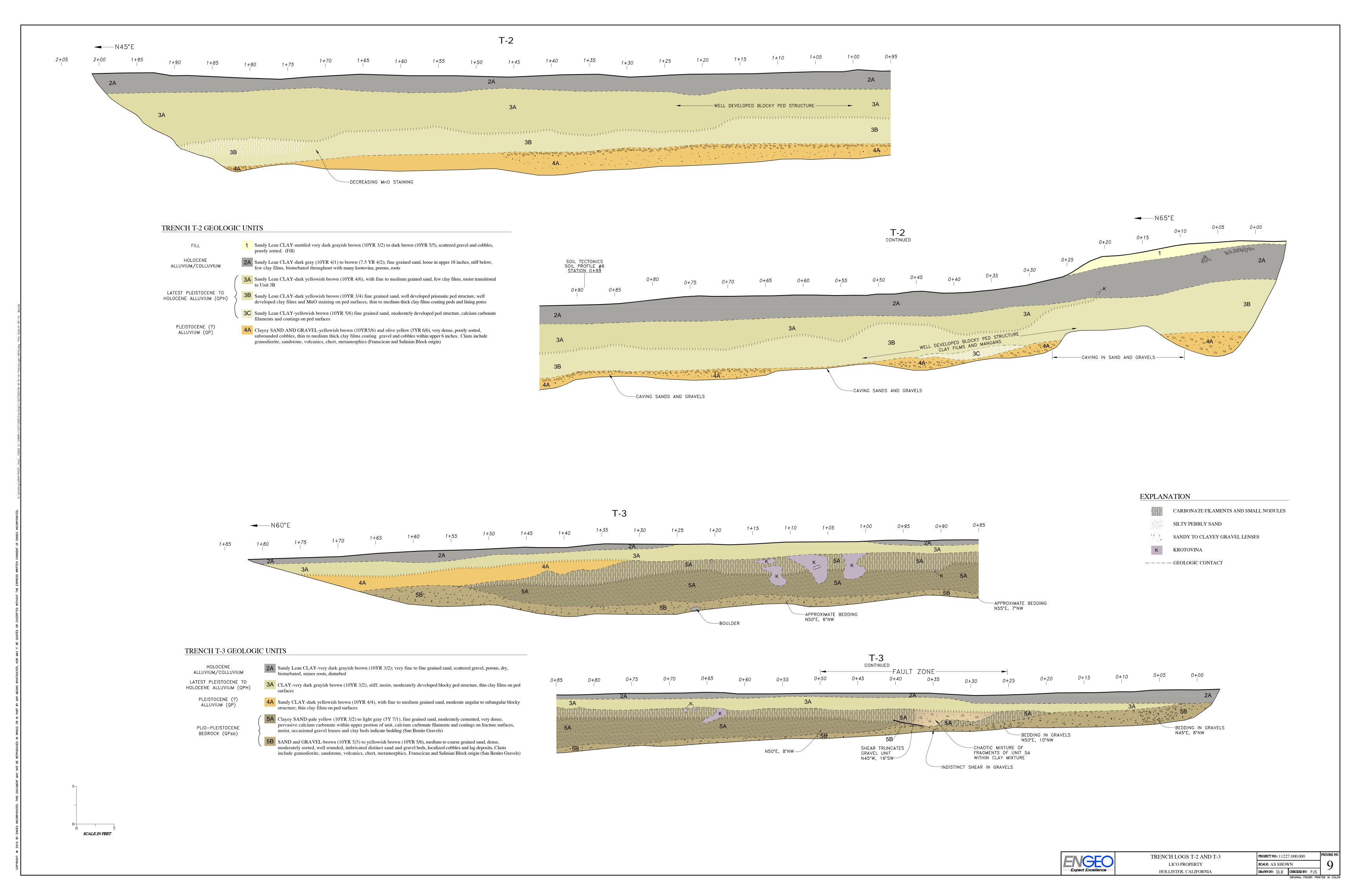
RECOMMENDED FAULT SETBACK ZONE

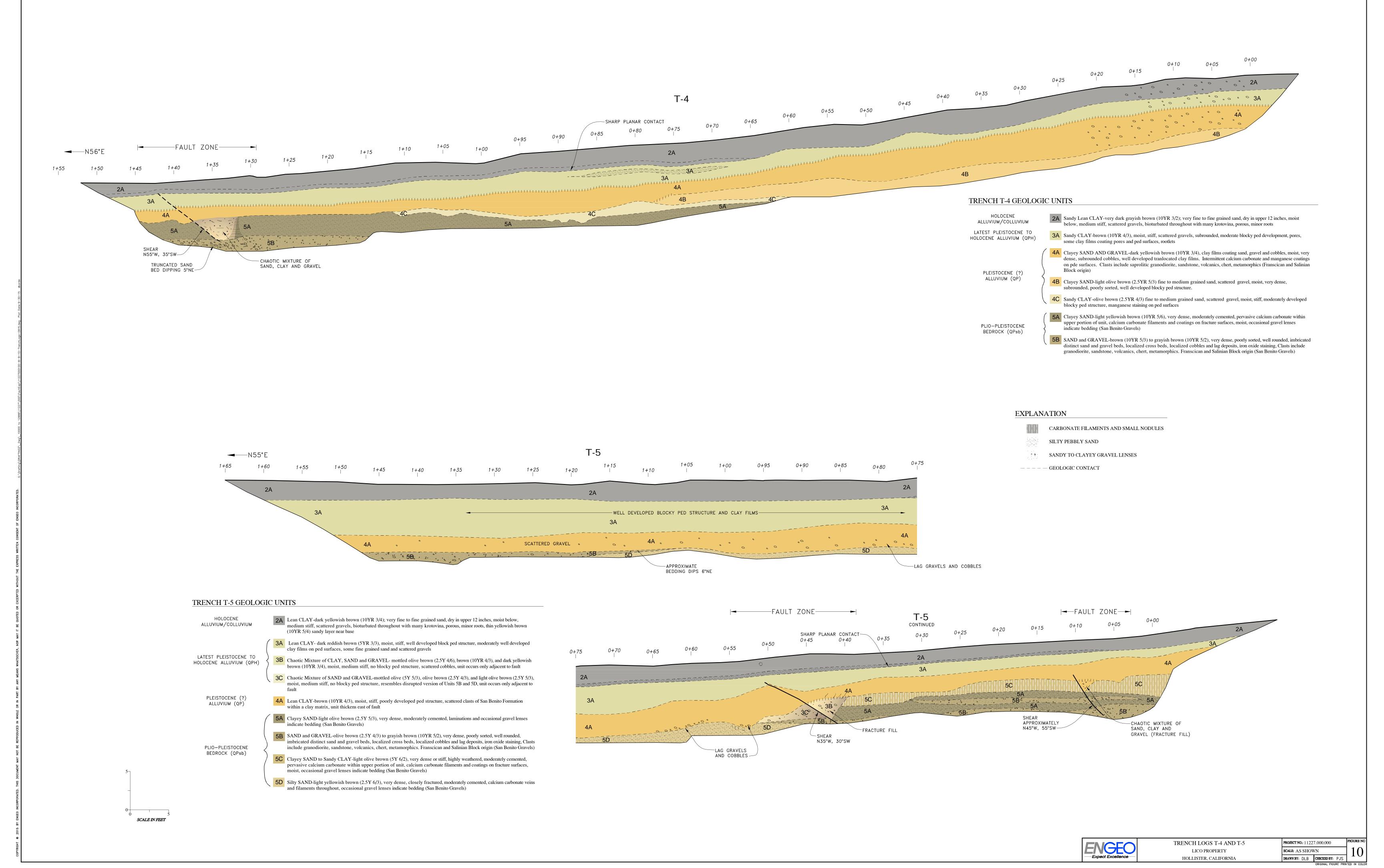
PROPOSED HABITABLE STRUCTURE EXCLUSION ZONE

BASE MAP SOURCE: UNKN









# APPENDIX A

**Soil Tectonics Report** 





### APPENDIX A

# PEDOCHRONOLOGICAL REPORT FOR THE LICO SUBDIVISION, ENTERPRISE ROAD, HOLLISTER, CALIFORNIA II

Prepared for ENGEO, Inc., San Ramon, California, Project No. 11227.000.000

2015-09-30

Soil Tectonics P.O. Box 5335 Berkeley, CA 94705

Glenn Borchardt

Principal Soil Scientist

Certified Professional Soil Scientist No. 24836

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# PEDOCHRONOLOGICAL REPORT FOR THE LICO SUBDIVISION, ENTERPRISE ROAD, HOLLISTER, CALIFORNIA II

Prepared for ENGEO, Inc., San Ramon, California, Project No. 11227.000.000

2015-09-30

Glenn Borchardt

### INTRODUCTION

An assessment of seismic and landslide risk due to ground movement can be aided greatly by the techniques of pedochronology (Borchardt, 1992, 1998), soil dating. This is because the youngest geological unit overlying fault traces is generally a soil horizon. The age and relative activity of ground movement often can be estimated by evaluating the age and relative disturbance of overlying soil units, as well as buried soils called paleosols. Terms, prefixes, and suffixes are defined in the Soils Glossary at the end of this report.

Soil horizons exhibit a wide range of physical, chemical, and mineralogical properties that evolve at varying rates. Soil scientists use various terms to describe these properties. A black, highly organic "A" horizon, for example, may form within a few centuries, while a dark brown, clayey "Bt" horizon may take up to 40,000 years to form. Certain soil properties are invariably absent in young soils. For instance, soils developed in granitic alluvium of the San Joaquin Valley do not have Munsell hues redder than 10YR until they are at least 100,000 years old (Birkeland, 1999; Harden, 1982). Still other properties, such as the movement and deposition of clay-size particles and the precipitation of calcium carbonate at extraordinary depths, indicate soil formation during a climate much wetter than at present. In the absence of a radiometric age date for the material from which a particular soil formed, an estimate of its age must take into account all the known properties of the soil and the landscape and climate in which it evolved.

### **METHOD**

The first step in studying a soil is the compilation of the data necessary for describing it (Birkeland, 1999; Borchardt, 2010). At minimum, this requires a Munsell color chart, hand lens, acid bottle, and instruments for 1:1 soil:water pH and electrical conductivity (EC) measurements. The second step may involve collecting samples of each horizon of the soil profile column for

laboratory analysis of particle size. This is done to check the textural classifications made in the field and to evaluate the genetic relationships between horizons and between different soils in the landscape. When warranted, the clay mineralogy and chemistry of the soil also is analyzed to provide additional information on the changes undergone by the initial material from which the soil weathered. The last step is the comparison of this accumulated soil data with that for soils having developed under similar conditions, preferably in the same region. Such information is scattered in soil survey reports (e.g., Welch, 1981), soil science journals, and consulting reports. In a particular locality, there is seldom enough comparative data available for this purpose. That is why, at the very least, the study of one soil profile always makes the evaluation of the next that much easier.

### **RESULTS OF THIS EVALUATION**

Soil profiles were studied to assess the age of the soil in Trench T-1 excavated northeast of a pressure ridge formed by the Calaveras fault at Enterprise Road, Hollister, California (Table 1).

# Soil Profile No. 3

This profile was developed in fine overbank deposits overlying a relatively unweathered portion of the San Benito Formation, which consisted of well-rounded cobble and coarse sand. This profile is very similar to Soil Profile No. 2 in the previous study (Borchardt, 2004). It has a 32-cm thick dark brown silt loam A1 horizon overlying an 18-cm thick brown silty clay A2 horizon. This overlies a 60-cm thick strong brown silty clay Bt/A with many coarse pronounced brown krotovinas (upper right corner of Figure 1). It has medium strong angular to subangular blocky structure and a few thin patchy clay films coating peds and clasts in the Bt portion. This overlies a 20-cm thick strong brown silty clay Bt horizon with a few thin to medium thick clay films coating peds and lining pores.

The Bt overlies two reddish yellow silty clay loam Bk horizons (Figure 1). The Bk1 is 23-cm thick with many fine to medium pronounced white mottles due to violently effervescent calcite coatings and soft nodules. It has common thin to medium thick clay films coating peds and lining pores. The matrix is slightly to strongly effervescent. The Bk2 is 122-cm thick with common fine to medium pronounced white mottles due to violently effervescent calcite coatings and soft nodules. It has medium strong subangular to angular blocky structure and a few thin clay films lining pores with some previously lined with calcite. The matrix is slightly effervescent.

This overlies a brown to light brown 2Bk horizon comprised of sandy rounded cobble to 6 cm with fine to medium pronounced white mottles due to violently effervescent calcite coatings and soft nodules mostly on upper surfaces of clasts. The structure is loose and there are a few thin clay films bridging sand grains. The matrix is noneffervescent. Except for the pedogenic calcite that trickled down from the overlying Bk horizons this is a relatively unweathered portion of the San Benito Formation. At the southeastern end of the trench, a

similar completely unweathered portion of the formation is uplifted along the eastern side of a pressure ridge along the Calaveras fault (Figure 2).

# Soil Profile No. 4

This partial profile was sampled at station 2+35' to include an underlying paleosol remnant developed on the San Benito Formation (Figure 3). Unlike the 2Bk horizon in Soil Profile No. 3, it consists of a 160-cm thick strong brown 2Btb horizon with coarse sandy cobble to 6 cm. It has loose structure with many thin to medium thick clay films coating clasts, lining pores, and bridging sand grains. This overlies a strong brown 2CBtb horizon consisting of coarse sandy cobble to 5 cm. It has loose structure with many thin patchy clay films coating clasts, lining pores, and bridging sand grains.

# Soil Profile No. 5

This partial profile, also in the weathered portion of the San Benito Formation, was selected to compare to the 2Btb horizon of Soil Profile No. 4. It has a 90-cm thick strong brown 2Btb horizon consisting of coarse sandy cobble to 3 cm. Like Soil Profile No. 4, it has loose structure and many thin to medium thick clay films coating clasts, lining pores, and bridging sand grains (Figure 4).

# Soil Profile No. 6

This profile, from Trench T-2, also was developed on Pleistocene alluvium and has characteristics similar to the soils in Trench T-1. (Table 2). It has a 17-cm thick dark brown silty clay loam Ap horizon overlying a 36-cm thick brown silty clay loam A horizon with fine to medium strong granular to subangular blocky structure. There is a brown transitional AB horizon overlying a 118-cm thick brown clay to silty clay loam Bt horizon with medium moderate angular blocky structure with medium thick clay films lining pores and peds. This is underlain by a 72-cm thick brown clayey Btb horizon with medium strong prismatic to angular blocky structure (Figure 5) coated with silvery back mangans (Figure 6). It has many medium thick clay films lining pores and coating peds. This overlies a pinkish gray gravelly sandy clay loam 2CBtb horizon.

# Soil pH and Electrical Conductivity

The properties of young sediments of consistent texture generally are not expected to show much change with depth. That is why changes in chemical properties, such as soil pH and electrical conductivity (EC), supply information on the degree soil weathering. Such "depth functions" prove that pedogenesis indeed did occur, and help to support the judgements involved in preparing soil descriptions (Borchardt, 2015).

The pH in Soil Profile No. 3 gradually increased from 6.5 to 9.5, a process that often reflects the high pH typical of soils in equilibrium with calcite (Figure 7). Normally, high amounts of calcite in combination with salts, particularly sodium, can result in pHs greater than 8.4. However, the EC in the 2CBk horizon is only 110  $\mu$ S/cm, which does not seem to be enough to boost the pH to the 9.5 measured there (Figure 7 and Figure 8). The 2Btb paleosol remnant in Soil Profile No. 4 also had a relatively high pH (8.7) without correspondingly high conductivity (Table 1). The equilibrium pH for calcareous soils usually is around 8.3, so the reason for values higher than this remains to be discovered.

Soil Profile No. 6 is typical of cultivated soils in which the pH tends to be slightly elevated in the surface, probably due to leaf drop or fertilization (Figure 9). The increase in pH in the B horizon is common. The EC pattern is typical of fine-textured cumulic soils in which additions of overbank materials can leave high salt contents at depth as the wetting front rises in the soil. Here, the maximum EC exists at the 250-cm depth (Figure 10). The low annual precipitation of only 13.82 in/yr is currently insufficient for producing a wetting front that low (Table 2).

# Soil Ages

This landscape has soil development representing two major time periods: Early Wisconsin (80-40 ka) and Late Wisconsin to the present (<40 ka).

Remnants of the Early Wisconsin paleosol appear as a strong brown (7.5YR5/6m) cobbly 2Btb horizon that is up to 160 cm thick (Table 1, Soil Profile No. 4). In other places, it is only 90 cm thick (Table 1, Soil Profile No. 5) or nonexistent (Table 1, Soil Profile No. 3). These variations are due to significant erosion and channelization of the Early Wisconsin surface, which formed on the cobbly phase of the San Benito Formation (Figure 2). For instance, cobble is encountered at a depth of 160 cm in Soil Profile Nos. 4 and 5 at stations 2+35' (Figure 3) and 0+32' (Figure 4), where the erosion was less, and at a depth of 275 cm in Soil Profile No. 3 at station 1+35' where the erosion was greater (Table 1). Where it was uplifted along the northeastern margin of the pressure ridge, the Early Wisconsin paleosol escaped channelization altogether (Figure 11).

The Late Wisconsin relict paleosol was formed in fine-textured overbank deposits that filled in the channels and depressions in the eroded Early Wisconsin surface. Minor folding near the pressure ridge at the southwest end of Trench T-1 indicates that some downwarping is occurring at present (Figure 12). Where the channels were cut deeply and the subsequent

overbank deposits were especially thick, the Late Wisconsin soil had a tendency to trap pedogenic calcite (Soil Profile No. 3, Table 1; Figure 1). In such soils, the pH tends to increase with depth (Figure 7; Borchardt, 2004, Figure 3). Judging by the electrical conductivity measurements, soluble salts also were trapped in the finer portions of these materials (Figure 8).

The analysis for Soil Profile No. 6 in Trench T-2 is similar. A period of extensive pedogenesis occurred during the Early Wisconsin, as indicated by the prismatic structure in the Btb horizon formed at depth (Figure 5). The 118-cm thick Bt horizon in the upper portion of the profile is indicative of pedogenesis during the Late Wisconsin (Table 2).

### CONCLUSIONS

- 1. Both the Late Wisconsin relict paleosol and the underlying Early Wisconsin paleosol can be used to evaluate surface fault rupture (SFR) at this site.
- 2. If any offsets or warping of either solum is discovered during subsequent investigations, they should be considered potential for SFR.

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Table 1. Soil profiles described northeast of the eastern trace of the Calaveras fault on the Lico property at Hollister, California. Abbreviations and definitions are given in Schoeneberger and others (2012) and Soil Survey Staff (1993, 1999, 2010).

Description of soils developed in alluvium/bedrock by Glenn Borchardt, who measured and sampled the soil on July 23, 2015 at latitude N36.82114° and longitude W121.38189° in the southeast wall of Trench T-1 at an elevation of 385'(385' Google Earth and 349' GPS) for station 1+35'. Mediterranean climate with mean annual precipitation of 13.82"/yr at Hollister (1948-2010). Slope 1% along trench. Aspect northeast. Excellent drainage. Water table deep. The parent material is overbank silts, clays, and fine sands over San Benito cobbly gravel. Soil pH increases from slightly acid in the surface to very strongly alkaline at the bottom of the profile. Soil in the area is variously mapped as: Antioch loam, *Typic Natrixeralfs*, 2-5% slopes, with a solum thickness of 152 cm and an A horizon thickness of 48 cm.

Horizon Depth, cm Description

### Soil Profile No. 3 at Station 1+35'

A1 0-32 Dark brown (7.5YR3/2m; 6/2d) silt loam; medium strong subangular to angular blocky structure; slightly sticky and slightly plastic when wet, very friable when moist, and extremely hard when dry; common very fine to fine roots; common fine to medium continuous random tubular and irregular pores; clear smooth boundary; pH 6.48; conductivity 310 uS; Sample No. 15B091.

A2 32-50 Brown (7.5YR4/2m; 4/2d) silty clay; medium strong subangular blocky structure; sticky and plastic when wet, very friable when moist, and extremely hard when dry; few very fine roots; common fine to medium continuous random tubular and irregular pores; gradual wavy boundary; pH 6.80; conductivity 300 uS; Sample No. 15B092.

Bt/A 50-110 Strong brown (7.5YR5/6m; 6/4d) silty clay with many coarse pronounced brown (7.5YR4/2m) krotovinas; medium strong angular to subangular blocky structure; sticky and plastic when wet, very friable when moist, and extremely hard when dry; few very fine roots; common fine to medium continuous random tubular and irregular pores; few thin patchy clay films coating peds and clasts in the Bt; abrupt wavy boundary; pH 7.60; conductivity 360 uS; Sample No. 15B093.

Bt 110-130 Strong brown (7.5YR5/6m; 6/4d) silty clay with few medium distinct strong brown (7.5YR4/6m) ped coatings; fine to medium moderate angular to subangular blocky structure; sticky and plastic when wet, very friable when moist, and extremely hard when dry; few fine to medium continuous random tubular and irregular pores; few thin to medium

thick clay films coating peds and lining pores; clear wavy boundary; pH 8.10; conductivity 360 uS; Sample No. 15B094. [Level line at 130 cm.]

Bk1 130-153 Reddish yellow (7.5YR6/6m; 6/4d) silty clay loam with many fine to medium pronounced white mottles due to violently effervescent calcite coatings and soft nodules; medium strong subangular blocky structure; sticky and plastic when wet, very friable when moist, and extremely hard when dry; few fine to medium continuous random tubular and irregular pores; common thin to medium thick clay films coating peds and lining pores; matrix is slightly to strongly effervescent; abrupt wavy boundary; pH 8.95; conductivity 410 uS; Sample No. 15B095.

Bk2 153-275 Reddish yellow (7.5YR6/6m; 6/4d) silty clay loam with many fine to medium pronounced white mottles due to violently effervescent calcite coatings and soft nodules; medium strong subangular to angular blocky structure; slightly sticky and slightly plastic when wet, very friable when moist, and very hard when dry; few fine to medium continuous random tubular and irregular pores; few thin clay films lining pores previously lined with calcite; matrix is slightly effervescent; abrupt smooth boundary; pH 8.95; conductivity 310 uS; Sample No. 15B096.

2Bk 275-280+ Brown to light brown (7.5YR4/2-6/4md) sandy rounded cobble to 6 cm with fine to medium pronounced white mottles due to violently effervescent calcite coatings and soft nodules mostly on upper surfaces of clasts; loose structure; nonsticky and nonplastic when wet, loose when moist, and soft when dry; many fine interstitial pores; few thin clay films bridging sand grains; matrix is noneffervescent; pH 9.50; conductivity 110 uS; Sample No. 15B097. San Benito Formation.

| *ESTIMATED AGE: | t <sub>o</sub> | = | 40 | ka |
|-----------------|----------------|---|----|----|
|                 | t <sub>b</sub> | = | 0  | ka |
|                 | t <sub>d</sub> | = | 40 | ky |

### Soil Profile No. 4 at Station 2+35'

2Btb 160-320 Strong brown (7.5YR5/6m; 5/6d) coarse sandy cobble to 6 cm; loose structure; slightly sticky and nonplastic when wet, loose when moist, and soft when dry; many fine interstitial pores; many thin to medium thick clay films coating clasts, lining pores, and bridging sand grains; clear wavy boundary; pH 8.70; conductivity 170 uS; Sample No. 15B098.

2CBtb 320-360+ Strong brown (7.5YR5/6m; 5/6d) coarse sandy cobble to 5 cm; loose structure; nonsticky and nonplastic when wet, loose when moist, and soft when dry; many

fine interstitial pores; many thin patchy clay films coating clasts, lining pores, and bridging sand grains; pH 7.60; conductivity 350 uS; Sample No. 15B099. San Benito Formation.

| *ESTIMATED AGE: | t <sub>o</sub> | = | 80 | ka |
|-----------------|----------------|---|----|----|
|                 | t <sub>b</sub> | = | 40 | ka |
|                 | t <sub>d</sub> | = | 40 | ky |

### Soil Profile No. 5 at Station 0+32'

2Btb 160-250 Strong brown (7.5YR5/6m; 5/6d) coarse sandy cobble to 3 cm; loose structure; slightly sticky and nonplastic when wet, loose when moist, and soft when dry; many fine interstitial pores; many thin to medium thick clay films coating clasts, lining pores, and bridging sand grains; clear smooth boundary; pH 7.60; conductivity 380 uS; Sample No. 15B100. San Benito Formation.

| *ESTIMATED AGE: | t <sub>o</sub> | = | 80 | ka |
|-----------------|----------------|---|----|----|
|                 | t <sub>b</sub> | = | 40 | ka |
|                 | t <sub>d</sub> | = | 40 | ky |

<sup>\*</sup>Pedochronological estimates based on available information. All ages should be considered subject to ±50% variation unless otherwise indicated (Borchardt, 1992). Bold dates are absolute.

t<sub>o</sub> = date when soil formation or aggradation began, ka

t<sub>b</sub> = date when soil or strata was buried, ka

t<sub>d</sub> = duration of soil development or aggradation, ky

Table 2. Soil profile described northeast of the eastern trace of the Calaveras fault on the Lico property at Hollister, California. Abbreviations and definitions are given in Schoeneberger and others (2012) and Soil Survey Staff (1993, 1999, 2010).

Description of soil developed in alluvium by Glenn Borchardt, who measured and sampled the soil on August 5, 2015 at latitude N36.82190° and longitude W121.38319° in the southeast wall of Trench T-2 at an elevation of 364'(364' Google Earth and 365' GPS) for station 0+89'. Mediterranean climate with mean annual precipitation of 13.82"/yr at Hollister (1948-2010). Slope 1% along trench. Aspect northeast. Excellent drainage. Water table deep. The parent material is overbank silts and clays over gravelly sandy clay loam alluvium. Soil pH increases from mildly alkaline in the surface to very strongly alkaline in the B horizon. Soil in the area is variously mapped as: Antioch loam, *Typic Natrixeralfs*, 2-5% slopes, with a solum thickness of 152 cm and an A horizon thickness of 48 cm.

Horizon Depth, cm Description

### Soil Profile No. 6 at Station 0+89'

Ap 0-17 Dark brown (7.5YR3/2m; 5/2d) silty clay loam; medium to coarse strong subangular blocky structure; slightly sticky and slightly plastic when wet, very friable when moist, and extremely hard when dry; common fine to medium roots; many fine to medium continuous random tubular pores; clear smooth boundary; pH 7.82; conductivity 580 uS; Sample No. 15B101.

A 17-53 Brown (7.5YR4/2m; 5/2d) silty clay loam; fine to medium strong granular to subangular blocky structure; slightly sticky and plastic when wet, very friable when moist, and extremely hard when dry; common fine to medium roots; common fine continuous random tubular pores; diffuse smooth boundary; pH 8.84; conductivity 370 uS; Sample No. 15B102.

AB 53-70 Brown (7.5YR4/2m; 5/2d) silty clay loam; medium to fine strong subangular blocky to granular structure; sticky and plastic when wet, very friable when moist, and very hard when dry; few fine to medium roots; common fine continuous random tubular and irregular pores; few thin clay films lining pores; clear smooth boundary; pH 8.89; conductivity 470 uS; Sample No. 15B103.

Bt1 70-139 Brown (7.5YR5/2m; 10YR7/4d) clay; medium moderate angular blocky structure; very sticky and very plastic when wet, very friable when moist, and very hard when dry; common fine continuous random tubular pores; few medium thick clay films lining

pores and few thin clay films on peds; gradual smooth boundary; pH 8.55; conductivity 940 uS; Sample No. 15B104.

Bt2 139-188 Brown (7.5YR5/2m; 10YR7/4d) silty clay loam; medium moderate angular blocky structure; sticky and plastic when wet, very friable when moist, and very hard when dry; common fine continuous random tubular pores; many medium thick clay films lining pores and many thin clay films on peds; clear wavy boundary; pH 8.14; conductivity 1350 uS; Sample No. 15B105.

| *ESTIMATED AGE: | t <sub>o</sub> | = | 40 | ka |
|-----------------|----------------|---|----|----|
|                 | t <sub>b</sub> | = | 0  | ka |
|                 | t <sub>d</sub> | = | 40 | ky |

Btb 188-260 Brown (7.5YR5/2m; 10YR7/4d) clay with many medium prominent black to blue mangans; medium strong prismatic to angular blocky structure; very sticky and very plastic when wet, very friable when moist, and very hard when dry; common fine continuous random tubular pores; many medium thick clay films lining pores and coating peds; abrupt wavy boundary; pH 8.12; conductivity 1530 uS; Sample No. 15B106. [Level line at 218 cm.]

2CBtb 260-280 Pinkish gray (7.5YR6/2m; 10YR7/4d) gravelly sandy clay loam with few fine prominent distinct black to blue mangans in pores; medium moderate subangular blocky structure; sticky and plastic when wet, very friable when moist, and very hard when dry; common fine continuous random tubular pores; few thin to medium thick clay films lining pores; pH 8.52; conductivity 910 uS; Sample No. 15B107.

| *ESTIMATED AGE: | t <sub>o</sub> | = | 80 | ka |
|-----------------|----------------|---|----|----|
|                 | $t_{b}$        | = | 40 | ka |
|                 | t <sub>d</sub> | Ш | 40 | ky |

<sup>\*</sup>Pedochronological estimates based on available information. All ages should be considered subject to +50% variation unless otherwise indicated (Borchardt, 1992). Bold dates are absolute.

 $t_o$  = date when soil formation or aggradation began, ka

 $t_b$  = date when soil or strata was buried, ka

t<sub>d</sub> = duration of soil development or aggradation, ky

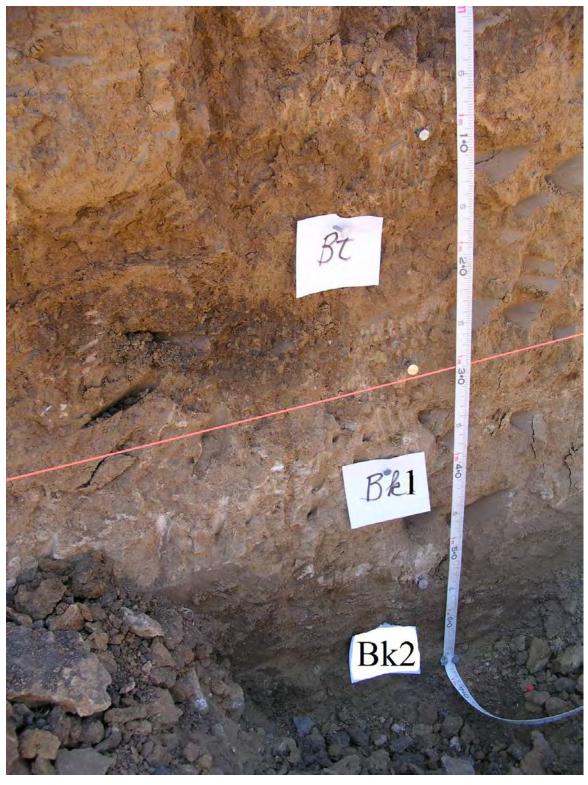


Figure 1. Soil Profile No. 3 showing the strong brown Bt overlying the Bk horizons at the 130-cm depth in Trench T-1. View SE.



Figure 2. Relatively unweathered San Benito Formation dipping NE against the eastern side of the pressure ridge along the Calaveras fault.. View SE.

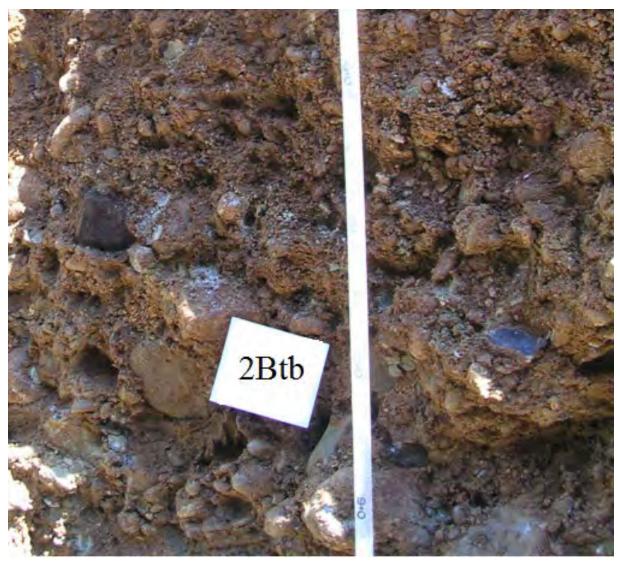


Figure 3. The 2Btb horizon in Soil Profile No. 4. Measurements taken from the top of the paleosol, which was about 160 cm below ground surface



Figure 4. The 2Btb paleosol horizon in Soil Profile No. 5 at base of Trench T-1 at station 0+32'. The shore is 122 cm long. View SE.



Figure 5. Prismatic structure typical of the Btb horizon in Soil Profile No. 6. Level line is at 218 cm. View SE.



Figure 6. Close up of the Btb of the Early Wisconsin paleosol in Soil Profile No. 6. Note the silvery mangans above the knife handle. View SE.

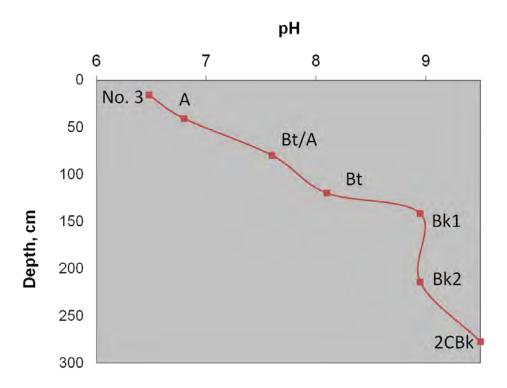


Figure 7. Depth function for pH in Soil Profile No. 3 at the Lico property, Hollister, California.

## Conductivity, uS

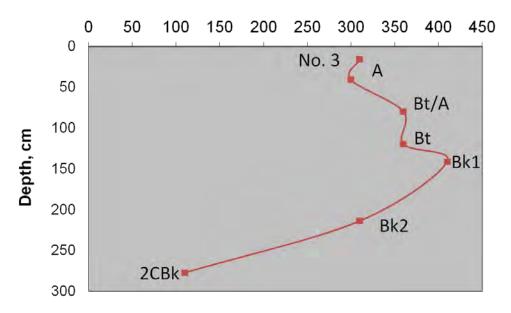


Figure 8. Depth function for electrical conductivity in Soil Profile No. 3 at the Lico property, Hollister, California. The maximum indicates an area of salt entrapment. These often exist at the base of fine-textured soils (Borchardt, 2015).

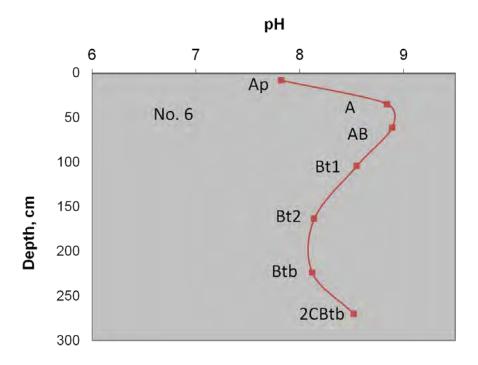


Figure 9. Depth function for pH in Soil Profile No. 6 at the Lico property, Hollister, California.

## Conductivity, uS

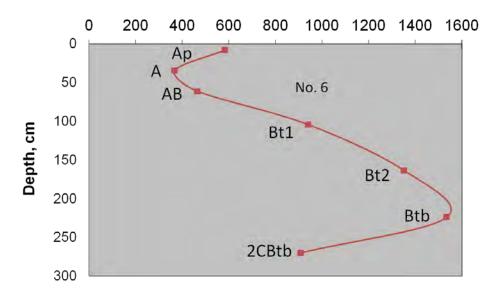


Figure 10. Depth function for electrical conductivity in Soil Profile No. 6 at the Lico property, Hollister, California. The maximum indicates an area of salt entrapment. These often exist at the base of fine-textured paleosols (Borchardt, 2015). The size of the peak and the extreme depth of the maximum in the Btb is indicative of an age greater than in Soil Profile No. 3.



Figure 11. Early Wisconsin paleosol uplifted against the northeastern side of the pressure ridge in the vicinity of stations 0+10 and 0+15. Elsewhere, this weathered cobble of the San Benito Formation is at least 160 cm beneath the surface. View SE.



Figure 12. A and E horizons formed over the Bt horizon in a downwarp along the Calaveras fault in Trench T-1. Orange line is level. Bk horizon formation is minimal here due to the shallow presence of the underlying gravels. View S.

## **SOILS GLOSSARY**

AGE. Elapsed time in calendar years. Because the cosmic production of C-14 has varied during the Quaternary, radiocarbon years (expressed as ky B.P.) must be corrected by using tree-ring and other data. Abbreviations used for corrected ages are: ka (kilo anno or years in thousands) or Ma (millions of years). Abbreviations used for intervals are: yr (years), ky (thousands of years). radiocarbon ages = yr B.P. Calibrated ages are calculated from process assumptions, relative ages fit in a sequence, and correlated ages refer to a matching unit. (See also yr B.P., HOLOCENE, PLEISTOCENE, QUATERNARY, PEDOCHRONOLOGY).

AGGRADATION. Deposition on the earth's surface in the direction of uniformity of grade.

ALKALI (SODIC) SOIL. A soil having so high a degree of alkalinity (pH 8.5 or higher) or so high a percentage of exchangeable sodium (15 % or more of the total exchangeable bases) that plant growth is restricted.

ALKALINE SOIL. Any soil that has a pH greater than 7.3. (See Reaction, Soil.)

ANGULAR ORPHANS. Angular fragments separated from weathered, well-rounded cobbles in colluvium derived from conglomerate.

ARGILLAN. (See Clay Film.)

ARGILLIC horizon. A horizon containing clay either translocated from above or formed in place through pedogenesis.

ALLUVIATION. The process of building up of sediments by a stream at places where stream velocity is decreased. The coarsest particles settle first and the finest particles settle last.

ANOXIC. (See also GLEYED SOIL). A soil having a low redox potential.

AQUICLUDE. A saturated body of sediment or rock that is incapable of transmitting significant quantities of water under ordinary hydraulic gradients.

AQUITARD. A body of rock or sediment that retards but does not prevent the flow of water to or from an adjacent aquifer. It does not readily yield water to wells or springs but may serve as a storage unit for groundwater.

ATTERBERG LIMITS. The moisture content at which a soil passes from a semi-solid to a plastic state (plastic limit, PL) and from a plastic to a liquid state (liquid limit, LL). The plasticity index (PI) is the numerical difference between the LL and the PL.

BEDROCK. The solid rock that underlies the soil and other unconsolidated material or that is exposed at the surface.

BISEQUUM. Two soils in vertical sequence, each soil containing an eluvial horizon and its underlying B horizon.

BOUDIN, BOUDINAGE. From a French word for sausage, describes the way that layers of rock break up under extension. Imagine the hand, fingers together, flat on the table, encased in soft clay and being squeezed from above, as being like a layer of rock. As the spreading clay moves

the fingers (sausages) apart, the most mobile rock fractions are drawn or squeezed into the developing gaps.

BURIED SOIL. A developed soil that was once exposed but is now overlain by a more recently formed soil.

CALCAREOUS SOIL. A soil containing enough calcium carbonate (commonly with magnesium carbonate) to effervesce (fizz) visibly when treated with cold, dilute hydrochloric acid. A soil having measurable amounts of calcium carbonate or magnesium carbonate.

CARBONATE MORPHOLOGY STAGES. Descriptive classes of calcite precipitation indicating increasing pedogenesis over time:

| Stage | Description   | Percent<br>Carbonate |
|-------|---|----------------------|
| Ι     | Bk horizon with few filaments and coatings                              | <10                  |
| I+    | Bk with common filaments and continuous clast coatings                  | <10                  |
| II    | Bk with continuous clast coatings, white masses, few nodules            | >10                  |
| II+   | Bk as above, but matrix is completely whitened, common nodules          | >15                  |
| >II   | K horizon that is 90% white, many nodules                               | >20                  |
| III+  | K that is completely plugged  | >40                  |
| IV    | K as above, but upper part cemented and has weak platy structure        | >50                  |
| V     | K same as above, but laminar layer is strong with incipient brecciation | >50                  |
| VI    | K brecciation and recementation, as well as pisoliths, are common       | >50                  |

CATENA. A sequence of soils of about the same age, derived from similar parent material and forming under similar climatic conditions, but having different characteristics due to variation in relief and drainage. (See also TOPOSEQUENCE.)

CEC. Cation exchange capacity. The amount of negative charge balanced by positively charged ions (cations) that are exchangeable by other cations in solution (meq/100 g soil = cmol(+)/kg soil).

CLAY. As a soil separate, the mineral soil particles are less than 0.002 mm in diameter. As a soil textural class, soil material that is 40 percent or more clay, less than 45 percent sand, and less than 40 percent silt.

CLAY FILM. A coating of oriented clay on the surface of a sand grain, pebble, soil aggregate, or ped. Clay films also line pores or root channels and bridge sand grains. Frequency classification is based on the percent of the ped faces and/or pores that contain films: very few--<5%; few--5-25%; common--25-50%; many--50-90%; and continuous--90-100%. Thickness classification is based on visibility of sand grains: thin--very fine sand grains standout; moderately thick--very fine sand grains impart microrelief to film; thick--fine sand grains enveloped by clay and films visible without magnification. Synonyms: clay skin, clay coat, argillan, illuviation cutan.

CLAY LAMELLAE. Thin, generally wavy bands that appear as multiple micro-Bt horizons at the base of the solum in sandy Holocene deposits. The lamellae generally are 1-3 cm in thickness and 5 to 30 cm apart. There may be two to six or more clay lamellae comprising the Bt horizon of such a soil.

COBBLE. Rounded or partially rounded fragments of rock ranging from 7.5 to 25 cm in diameter.

COLLUVIUM. Any loose mass of soil or rock fragments that moves downslope largely by the force of gravity. Usually it is thicker at the base of the slope.

COLLUVIUM-FILLED SWALE. The prefailure topography of the source area of a debris flow.

COMPARATIVE PEDOLOGY. The comparison of soils, particularly through examination of features known to evolve through time.

CONCRETIONS. Grains, pellets, or nodules of various sizes, shapes, and colors consisting of concentrated compounds or cemented soil grains. The composition of most concretions is unlike that of the surrounding soil. Calcium carbonate and iron oxide are common compounds in concretions.

CONDUCTIVITY. The ability of a soil solution to conduct electricity, generally expressed as the reciprocal of the electrical resistivity. Electrical conductance is the reciprocal of the resistance  $(1/R = 1/\text{ohm} = \text{ohm}^{-1} = \text{mho} [\text{reverse of ohm}] = \text{siemens} = S)$ , while electrical conductivity is the reciprocal of the electrical resistivity (EC = 1/r = 1/ohm-cm = mho/cm = S/cm or mmho/cm = dS/m). EC, expressed as uS/cm, is equivalent to the ppm of salt in solution when multiplied by 0.640. Pure rain water has an EC of 0, standard 0.01 N KCl is 1411.8 uS at 25C, and the growth of salt-sensitive crops is restricted in soils having saturation extracts with an EC greater than 2,000 uS/cm. Measurements in soils are usually performed on 1:1 suspensions containing one part by weight of soil and one part by weight of distilled water.

CONSISTENCE, SOIL. The feel of the soil and the ease with which a lump can be crushed by the fingers. Terms commonly used to describe consistence are --

Loose.--Noncoherent when dry or moist; does not hold together in a mass.

Friable.--When moist, crushes easily under gentle pressure between thumb and forefinger and can be pressed together into a lump.

Firm.--When moist, crushes under moderate pressure between thumb and forefinger, but resistance is distinctly noticeable.

Plastic.--When wet, readily deformed by moderate pressure but can be pressed into a lump; will form a "wire" when rolled between thumb and forefinger.

Sticky.--When wet, adheres to other material, and tends to stretch somewhat and pull apart, rather than to pull free from other material.

Hard.--When dry, moderately resistant to pressure; can be broken with difficulty between thumb and forefinger.

Soft.--When dry, breaks into powder or individual grains under very slight pressure.

Cemented.--Hard and brittle; little affected by moistening.

CTPOT. Easily remembered acronym for climate, topography, parent material, organisms, and time; the five factors of soil formation.

CUMULIC. A soil horizon that has undergone aggradation coincident with its active development.

CUTAN. (See Clay Film.)

DEBRIS FLOW. Incoherent or broken masses of rock, soil, and other debris that move downslope in a manner similar to a viscous fluid.

DEBRIS SLOPE. A constant slope with debris on it from the free face above.

DEGRADATION. A modification of the earth's surface by erosion.

DOWNWARP. A segment of the earth's crust that is broadly bent downward.

DURIPAN. A subsurface soil horizon that is cemented by illuvial silica, generally deposited as opal or microcrystalline silica, to the degree that less than 50 percent of the volume of air-dry fragments will slake in water or HCl.

ELUVIATION. The removal of soluble material and solid particles, mostly clay and humus, from a soil horizon by percolating water.

EOLIAN. Deposits laid down by the wind, landforms eroded by the wind, or structures such as ripple marks made by the wind.

FAULT-LINE SCARP. A scarp that has been produced by differential erosion along an old fault line.

FAULTSLIDE. A landslide that shows physical evidence of its interaction with a fault.

FIRST-ORDER DRAINAGE. The most upstream, field-discernible concavity that conducts water and sediments to lower parts of a watershed.

FLOOD PLAIN. A nearly level alluvial plain that borders a stream and is subject to flooding unless protected artificially.

FOSSIL FISSURE. A buried rectilinear chamber associated with extension due to ground movement. The chamber must be oriented along the strike of the shear and must have vertical and horizontal dimensions greater than its width. It must show no evidence of faunal activity and its walls may have silt or clay coatings indicative of frequent temporary saturation with ground water. May be mistaken for an animal burrow. Also known as a paleofissure.

FRIABILITY. Term for the ease with which soil crumbles. A friable soil is one that crumbles easily.

GENESIS, SOIL. The mode of origin of the soil. Refers especially to the processes or soil-forming factors responsible for the formation of the solum (A and B horizons) from the unconsolidated parent material.

GEOMORPHIC. Pertaining to the form of the surface features of the earth. Specifically, geomorphology is the analysis of landforms and their mode of origin.

GLEYED SOIL. A soil having one or more neutral gray horizons as a result of water logging and lack of oxygen. The term "gleyed" also designates gray horizons and horizons having yellow and gray mottles as a result of intermittent water logging.

GRAVEL. Rounded or angular fragments of rock 2 to 75 mm in diameter. Soil textures with >15% gravel have the prefix "gravelly" and those with >90% gravel have the suffix "gravel."

HIGHSTAND. The highest elevation reached by the ocean during an interglacial period.

HOLOCENE. The most recent epoch of geologic time, extending from 10 ka to the present.

HORIZON, SOIL. A layer of soil, approximately parallel to the surface, that has distinct characteristics produced by soil-forming processes. These are the major soil horizons:

O horizon.--The layer of organic matter on the surface of a mineral soil. This layer consists of decaying plant residues.

A horizon.--The mineral horizon at the surface or just below an O horizon. This horizon is the one in which living organisms are most active and therefore is marked by the accumulation of humus. The horizon may have lost one or more of soluble salts, clay, and sesquioxides (iron and aluminum oxides).

E horizon -- This eluvial horizon is light in color, lying beneath the A horizon and above the B horizon. It is made up mostly of sand and silt, having lost most of its clay and iron oxides through reduction, chelation, and translocation.

B horizon.--The mineral horizon below an A horizon. The B horizon is in part a layer of change from the overlying A to the underlying C horizon. The B horizon also has distinctive characteristics caused (1) by accumulation of clay, sesquioxides, humus, or some combination of these; (2) by prismatic or blocky structure; (3) by redder or stronger colors than the A horizon; or (4) by some combination of these.

C horizon.--The relatively unweathered material immediately beneath the solum. Included are sediment, saprolite, organic matter, and bedrock excavatable with a spade. In most soils this material is presumed to be like that from which the overlying horizons were formed. If the material is known to be different from that in the solum, a number precedes the letter C.

R horizon.--Consolidated rock not excavatable with a spade. It may contain a few cracks filled with roots or clay or oxides. The rock usually underlies a C horizon but may be immediately beneath an A or B horizon.

Major horizons may be further distinguished by applying prefix Arabic numbers to designate differences in parent materials as they are encountered (e.g., 2B, 2BC, 3C) or by applying suffix numerals to designate minor changes (e.g., B1, B2).

The following is from the Natural Resources Conservation Service, except for the proposed addition of mn:

#### "Suffix Symbols

Lowercase letters are used as suffixes to designate specific kinds of master horizons and layers. The term "accumulation" is used in many of the definitions of such horizons to indicate that these horizons must contain more of the material in question than is presumed to have been present in the parent material. The suffix symbols and their meanings are as follows:

#### a Highly decomposed organic material

This symbol is used with O to indicate the most highly decomposed organic materials, which have a fiber content of less than 17 percent (by volume) after rubbing.

#### b Buried genetic horizon

This symbol is used in mineral soils to indicate identifiable buried horizons with major genetic features that were developed before burial. Genetic horizons may or may not have formed in the overlying material, which may be either like or unlike the assumed parent material of the buried soil. This symbol is not used in organic soils, nor is it used to separate an organic layer from a mineral layer.

#### c Concretions or nodules

This symbol indicates a significant accumulation of concretions or nodules. Cementation is required. The cementing agent commonly is iron, aluminum, manganese, or titanium. It cannot be silica, dolomite, calcite, or more soluble salts.

#### co Coprogenous earth

This symbol, used only with L, indicates a limnic layer of coprogenous earth (or sedimentary peat).

#### d Physical root restriction

This symbol indicates noncemented, root-restricting layers in natural or human-made sediments or materials. Examples are dense basal till, plowpans, and other mechanically compacted zones.

#### di Diatomaceous earth

This symbol, used only with L, indicates a limnic layer of diatomaceous earth.

#### e Organic material of intermediate decomposition

This symbol is used with O to indicate organic materials of intermediate decomposition. The fiber content of these materials is 17 to 40 percent (by volume) after rubbing.

#### f Frozen soil or water

This symbol indicates that a horizon or layer contains permanent ice. The symbol is not used for seasonally frozen layers or for dry permafrost.

#### ff Dry permafrost

This symbol indicates a horizon or layer that is continually colder than  $0^{\circ}$  C and does not contain enough ice to be cemented by ice. This suffix is not used for horizons or layers that have a temperature warmer than  $0^{\circ}$  C at some time of the year.

#### g Strong gleying

This symbol indicates either that iron has been reduced and removed during soil formation or that saturation with stagnant water has preserved it in a reduced state. Most of the affected layers have chroma of 2 or less, and many have redox concentrations. The low chroma can represent either the color of reduced iron or the color of uncoated sand and silt particles from which iron has been removed. The symbol g is not used for materials of low chroma that have no history of wetness, such as some slates or E horizons. If g is used with B, pedogenic change in addition to gleying is implied. If no other pedogenic change besides gleying has taken place, the horizon is designated Cg.

#### h Illuvial accumulation of organic matter

This symbol is used with B to indicate the accumulation of illuvial, amorphous, dispersible complexes of organic matter and sesquioxides if the sesquioxide component is dominated by aluminum but is present only in very small quantities. The organo-sesquioxide material coats sand and silt particles. In some horizons these coatings have coalesced, filled pores, and cemented the horizon. The symbol h is also used in combination with s as "Bhs" if the amount of the sesquioxide component is significant but the color value and chroma, moist, of the horizon are 3 or less.

#### i Slightly decomposed organic material

This symbol is used with O to indicate the least decomposed of the organic materials. The fiber content of these materials is 40 percent or more (by volume) after rubbing.

#### *j* Accumulation of jarosite

Jarosite is a potassium or iron sulfate mineral that is commonly an alteration product of pyrite that has been exposed to an oxidizing environment. Jarosite has hue of 2.5Y or yellower and normally has chroma of 6 or more, although chromas as low as 3 or 4 have been reported. [Note: No longer used to indicate "juvenile."]

#### ii Evidence of cryoturbation

Evidence of cryoturbation includes irregular and broken horizon boundaries, sorted rock fragments, and organic soil materials existing as bodies and broken layers within and/or between mineral soil layers. The organic bodies and layers are most commonly at the contact between the active layer and the permafrost.

#### k Accumulation of secondary carbonates

This symbol indicates an accumulation of visible pedogenic calcium carbonate (less than 50 percent, by volume). Carbonate accumulations exist as carbonate filaments, coatings, masses, nodules, disseminated carbonate, or other forms.

#### kk Engulfment of horizon by secondary carbonates

This symbol indicates major accumulations of pedogenic calcium carbonate. The suffix kk is used when the soil fabric is plugged with fine grained pedogenic carbonate (50 percent or more, by volume) that exists as an essentially continuous medium. The suffix corresponds to the stage III plugged horizon or higher of the carbonate morphogenetic stages (Gile et al., 1966).

#### m Cementation or induration

This symbol indicates continuous or nearly continuous cementation. It is used only for horizons that are more than 90 percent cemented, although they may be fractured. The cemented layer is physically root-restrictive. The dominant cementing agent (or the two dominant ones) may be indicated by adding defined letter suffixes, singly or in pairs. The horizon suffix km or kkm indicates cementation by carbonates; qm, cementation by silica; sm, cementation by iron; yym, cementation by gypsum; kqm, cementation by lime and silica; and zm, cementation by salts more soluble than gypsum.

ma Marl

This symbol, used only with L, indicates a limnic layer of marl.

mn Mangans

This symbol indicates an accumulation of manganese oxide, generally as ped coatings called mangans (First used by Borchardt on 20130418.)

n Accumulation of sodium

This symbol indicates an accumulation of exchangeable sodium.

o Residual accumulation of sesquioxides

This symbol indicates a residual accumulation of sesquioxides.

p Tillage or other disturbance

This symbol indicates a disturbance of the surface layer by mechanical means, pasturing, or similar uses. A disturbed organic horizon is designated Op. A disturbed mineral horizon is designated Ap even though it is clearly a former E, B, or C horizon.

q Accumulation of silica

This symbol indicates an accumulation of secondary silica.

r Weathered or soft bedrock

This symbol is used with C to indicate cemented layers (moderately cemented or less cemented). Examples are weathered igneous rock and partly consolidated sandstone, siltstone, or slate. The excavation difficulty is low to high.

s Illuvial accumulation of sesquioxides and organic matter

This symbol is used with B to indicate an accumulation of illuvial, amorphous, dispersible complexes of organic matter and sesquioxides if both the organic-matter and sesquioxide components are significant and if either the color value or chroma, moist, of the horizon is 4 or more. The symbol is also used in combination with h as "Bhs" if both the organic-matter and sesquioxide components are significant and if the color value and chroma, moist, are 3 or less.

se Presence of sulfides

Typically dark colors (e.g., value <4, chroma <2); may have a sulphurous odor.

ss Presence of slickensides

This symbol indicates the presence of slickensides. Slickensides result directly from the swelling of clay minerals and shear failure, commonly at angles of 20 to 60 degrees above horizontal.

They are indicators that other vertic characteristics, such as wedge-shaped peds and surface cracks, may be present.

## t Accumulation of silicate clay

This symbol indicates an accumulation of silicate clay that either has formed *in situ* within a horizon or has been moved into the horizon by illuviation, or both. At least some part of the horizon should show evidence of clay accumulation either as coatings on surfaces of peds or in pores, as lamellae, or as bridges between mineral grains.

## u Presence of human-manufactured materials (artifacts)

This symbol indicates the presence of manufactured artifacts that have been created or modified by humans, usually for a practical purpose in habitation, manufacturing, excavation, or construction activities. Examples of artifacts are processed wood products, liquid petroleum products, coal, combustion by-products, asphalt, fibers and fabrics, bricks, cinder blocks, concrete, plastic, glass, rubber, paper, cardboard, iron and steel, altered metals and minerals, sanitary and medical waste, garbage, and landfill waste.

#### v Plinthite

This symbol indicates the presence of iron-rich, humus-poor, reddish material that is firm or very firm when moist and hardens irreversibly when exposed to the atmosphere and to repeated wetting and drying.

#### w Development of color or structure

This symbol is used with B to indicate the development of color or structure, or both, with little or no apparent illuvial accumulation of material. It should not be used to indicate a transitional horizon.

#### x Fragipan character

This symbol indicates a genetically developed layer that has a combination of firmness and brittleness and commonly a higher bulk density than the adjacent layers. Some part of the layer is physically root-restrictive.

#### y Accumulation of gypsum

This symbol indicates an accumulation of gypsum (<50% by volume).

#### yy Dominance of gypsum

This symbol indicates an accumulation of gypsum (>50% by volume); light colored (e.g., value >7, chroma <4); may be pedogenically derived or inherited transformation of primary gypsum from parent material.

#### z Accumulation of salts more soluble than gypsum

This symbol indicates an accumulation of salts that are more soluble than gypsum; e.g., NaCl.

HUMUS. The well-decomposed, more or less stable part of the organic matter in mineral soils.

ILLUVIATION. The deposition by percolating water of solid particles, mostly clay or humus, within a soil horizon.

INTERFLUVE. The land lying between streams.

ISOCHRONOUS BOUNDARY. A gradational boundary between two sedimentary units indicating that they are approximately the same age. Opposed to a nonisochronous boundary, which by its abruptness indicates that it delineates units having significant age differences.

KROTOVINA. An animal burrow filled with soil.

LEACHING. The removal of soluble material from soil or other material by percolating water.

LOWSTAND. The lowest elevation reached by the ocean during a glacial period.

MANGAN. A thin coating of manganese oxide (cutan) on the surface of a sand grain, pebble, soil aggregate, or ped. Mangans also line pores or root channels and bridge sand grains.

MAP. Mean annual precipitation.

MODERN SOIL. The portion of a soil section that is under the influence of current pedogenetic conditions. It generally refers to the uppermost soil regardless of age.

MODERN SOLUM. The combination of the A and B horizons in the modern soil.

MORPHOLOGY, SOIL. The physical make-up of the soil, including the texture, structure, porosity, consistence, color, and other physical, mineral, and biological properties of the various horizons, and the thickness and arrangement of those horizons in the soil profile.

MOTTLING, SOIL. Irregularly marked with spots of different colors that vary in number and size. Mottling in soils usually indicates poor aeration and lack of drainage. Descriptive terms are as follows: abundance--few, common, and many; size--fine, medium, and coarse; and contrast-faint, distinct and prominent. The size measurements are these: fine, less than 5 mm in diameter along the greatest dimension; medium, from 5 to 15 mm, and coarse, more than 15 mm.

MRT (MEAN RESIDENCE TIME.) The average age of the carbon atoms within a soil horizon. Under ideal reducing conditions, the humus in a soil will have a C-14 age that is half the true age of the soil. In oxic soils humus is typically destroyed as fast as it is produced, generally yielding MRT ages no older than 300-1000 years, regardless of the true age of the soil.

MUNSELL COLOR NOTATION. Scientific description of color determined by comparing soil to a Munsell Soil Color Chart (Available from Macbeth Division of Kollmorgen Corp., 2441 N. Calvert St., Baltimore, MD 21218). For example, dark yellowish brown is denoted as 10YR3/4m in which the 10YR refers to the hue or proportions of yellow and red, 3 refers to value or lightness (0 is black and 10 is white), 4 refers to chroma (0 is pure black and white and 20 is the pure color), and m refers to the moist condition rather than the dry (d) condition.

OVERBANK DEPOSIT. Fine-grained alluvial sediments deposited from floodwaters outside of the fluvial channel.

OXIC. A soil having a high redox potential. Such soils typically are well drained, seldom being waterlogged or lacking in oxygen. Rubification in such soils tends to increase with age.

PALEO SOIL TONGUE. A soil tongue that formed during a previous soil-forming interval.

PALEOSEISMOLOGY. The study of prehistoric earthquakes through the examination of soils, sediments, and rocks.

PALEOSOL. A soil that formed on a landscape in the past with distinctive morphological features resulting from a soil-forming environment that no longer exists at the site. The former

pedogenic process was either altered because of external environmental change or interrupted by burial.

PALINSPASTIC RECONSTRUCTION. Diagrammatic reconstruction used to obtain a picture of what geologic and/or soil units looked like before their tectonic deformation.

PARENT MATERIAL. The great variety of unconsolidated organic and mineral material in which soil forms. Consolidated bedrock is not yet parent material by this concept.

PED. An individual natural soil aggregate, such as a granule, a prism, or a block.

PEDOCHRONOLOGY. The study of pedogenesis with regard to the determination of when soil formation began, how long it occurred, and when it stopped. Also known as soil dating. Two ages and the calculated duration are important:

t<sub>o</sub> = age when soil formation or aggradation began, ka

 $t_b$  = age when the soil or stratum was buried, ka

 $t_d$  = duration of soil development or aggradation, ky

Pedochronological estimates are based on available information. All ages should be considered subject to  $\pm 50\%$  variation unless otherwise indicated.

PEDOCHRONOPALEOSEISMOLOGY. The study of prehistoric earthquakes by using pedochronology.

PEDOLOGY. The study of the process through which rocks, sediments, and their constituent minerals are transformed into soils and their constituent minerals at or near the surface of the earth.

PEDOGENESIS. The process through which rocks, sediments, and their constituent minerals are transformed into soils and their constituent minerals at or near the surface of the earth.

PERCOLATION. The downward movement of water through the soil.

pH VALUE. The negative log of the hydrogen ion concentration. Measurements in soils are usually performed on 1:1 suspensions containing one part by weight of soil and one part by weight of distilled water. A soil with a pH of 7.0 is precisely neutral in reaction because it is neither acid nor alkaline. An acid or "sour" soil is one that gives an acid reaction; an alkaline soil is one that gives an alkaline reaction. In words, the degrees of acidity or alkalinity are expressed as:

| Extremely acid      | <4.5       |
|---------------------|------------|
| Very strongly acid  | 4.5 to 5.0 |
| Strongly acid       | 5.1 to 5.5 |
| Medium acid         | 5.6 to 6.0 |
| Slightly acid       | 6.1 to 6.5 |
| Neutral             | 6.6 to 7.3 |
| Mildly alkaline     | 7.4 to 7.8 |
| Moderately alkaline | 7.9 to 8.4 |

| Strongly alkaline      | 8.5 to 9.0 |
|------------------------|------------|
| Very strongly alkaline | >9.0       |
|                        |            |
| Used if significant:   |            |
| Very slightly acid     | 6.6 to 6.9 |
| Very mildly alkaline   | 7.1 to 7.3 |

#### PHREATIC SURFACE. (See Water Table.)

PLANATION. The process of erosion whereby a portion of the surface of the Earth is reduced to a fundamentally even, flat, or level surface by a meandering stream, waves, currents, glaciers, or wind.

PLEISTOCENE. An epoch of geologic time extending from 10 ka to 1.8 Ma; it includes the last Ice Age.

PROFILE, SOIL. A vertical section of the soil through all its horizons and extending into the parent material.

QUATERNARY. A period of geologic time that includes the past 1.8 Ma. It consists of two epochs--the Pleistocene and Holocene.

PROGRADATION. The building outward toward the sea of a shoreline or coastline by nearshore deposition.

REFUGIUM. A place of refuge. Plants, animals, and soil minerals tend to accumulate only in the most ideal areas when surrounded by a hostile environment.

RELICT SOIL. A surface soil that was partly formed under climatic conditions significantly different from the present.

RUBIFICATION. The reddening of soils through the release and precipitation of iron as an oxide during weathering. Munsell hues and chromas of well-drained soils generally increase with soil age.

SALINE SOIL. A soil that contains soluble salts in amounts that impair the growth of crop plants but that does not contain excess exchangeable sodium.

SAND. Individual rock or mineral fragments in a soil that range in diameter from 0.05 to 2.0 mm. Most sand grains consist of quartz, but they may be of any mineral composition. The textural class name of any soil that contains 85 percent or more sand and not more than 10 percent clay.

SECONDARY FAULT. A minor fault that bifurcates from or is associated with a primary fault. Movement on a secondary fault never occurs independently of movement on the primary, seismogenic fault.

SHORELINE ANGLE. The line formed by the intersection of the wave-cut platform and the sea cliff. It approximates the position of sea level at the time the platform was formed.

SILT. Individual mineral particles in a soil that range in diameter from the upper limit of clay (0.002 mm) to the lower limit of very find sand (0.05 mm.) Soil of the silt textural class is 80 percent or more silt and less than 12 percent clay.

SLICKENSIDES. Polished and grooved surfaces produced by one mass sliding past another. In soils, slickensides may form along a fault plane; at the bases of slip surfaces on steep slopes; on faces of blocks, prisms, and columns undergoing shrink-swell. In tectonic slickensides the striations are strictly parallel.

SLIP RATE. The rate at which the geologic materials on the two sides of a fault move past each other over geologic time. The slip rate is expressed in mm/yr, and the applicable duration is stated. Faults having slip rates less than 0.01 mm/yr are generally considered inactive, while faults with Holocene slip rates greater than 0.1 mm/yr generally display tectonic geomorphology.

SMECTITE. A fine, platy, aluminosilicate clay mineral that expands and contracts with the absorption and loss of water. It has a high cation-exchange capacity and is plastic and sticky when moist.

SOIL. A natural, three-dimensional body at the earth's surface that is capable of supporting plants and has properties resulting from the integrated effect of climate and living matter acting on earthy parent material, as conditioned by relief over periods of time.

SOIL SEISMOLOGIST. Soil scientist who studies the effects of earthquakes on soils.

SOIL SLICKS. Curvilinear striations that form in swelling clayey soils, where there is marked change in moisture content. Clayey slopes buttressed by rigid materials may allow minor amounts of gravitationally driven plastic flow, forming soil slicks sometimes mistaken for evidence of tectonism. Soil slicks disappear with depth and the striations are seldom strictly parallel as they are when movement is major. (See also SLICKENSIDES.)

SOIL TECTONICS. The study of the interactions between soil formation and tectonism.

SOIL TONGUE. That portion of a soil horizon extending into a lower horizon.

SOLUM. Combined A and B horizons. Also called the true soil. If a soil lacks a B horizon, the A horizon alone is the solum.

STONELINE. A thin, buried, planar layer of stones, cobbles, or bedrock fragments. Stonelines of geological origin may have been deposited upon a former land surface. The fragments are more often pebbles or cobbles than stones. A stoneline generally overlies material that was subject to weathering, soil formation, and erosion before deposition of the overlying material. Many stonelines seem to be buried erosion pavements, originally formed by running water on the land surface and concurrently covered by surficial sediment.

STRATH TERRACE. A gently sloping terrace surface bearing little evidence of aggradation.

STRUCTURE, SOIL. The arrangement of primary soil particles into compound particles or aggregates that are separated from adjoining aggregates. The principal forms of soil structure are--platy (laminated), prismatic (vertical axis of aggregates longer than horizontal), columnar (prisms with rounded tops), blocky (angular or subangular), and granular. Structureless soils are either single grained (each grain by itself, as in dune sand) or massive (the particles adhering without any regular cleavage, as in many hardpans).

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SUBSIDIARY FAULT. A branch fault that extends a substantial distance from the main fault zone.

SURFACE FAULT RUPTURE (SFR). Permanent disturbance of soil surface occurring as a result of tectonic offset. This may produce ground cracks, offsets, and warping of soil horizons.

TECTOTURBATION. Soil disturbance resulting from tectonic movement.

TEXTURE, SOIL. Particle size classification of a soil, generally given in terms of the USDA system which uses the term "loam" for a soil having equal properties of sand, silt, and clay. The basic textural classes, in order of their increasing proportions of fine particles are sand, loamy sand, sandy loam, loam, silt loam, silt, sandy clay loam, clay loam, silty clay loam, sand clay, silty clay, and clay. The sand, loamy sand, and sandy loam classes may be further divided by specifying "coarse," "fine," or "very fine."

TOPOSEQUENCE. A sequence of kinds of soil in relation to position on a slope. (See also CATENA.)

TRANSLOCATION. The physical movement of soil particles, particularly fine clay, from one soil horizon to another under the influence of gravity.

UNIFIED SOIL CLASSIFICATION SYSTEM. The particle size classification system used by the U.S. Army Corps of Engineers and the Bureau of Reclamation. Like the ASTM and AASHO systems, the sand/silt boundary is at 80 um instead of 50 um used by the USDA. Unlike all other systems, the gravel/sand boundary is at 4 mm instead of 2 mm and the silt/clay boundary is determined by using Atterberg limits.

VERTISOL. A soil with at least 30% clay, usually smectite, that fosters pronounced changes in volume with change in moisture. Cracks greater than 1 cm wide appear at a depth of 50 cm during the dry season each year. One of the ten USDA soil orders.

WATER TABLE. The upper limit of the soil or underlying rock material that is wholly saturated with water. Also called the phreatic surface.

WAVE-CUT PLATFORM. The relatively smooth, slightly seaward-dipping surface formed along the coast by the action of waves generally accompanied by abrasive materials.

WEATHERING. All physical and chemical changes produced in rocks or other deposits at or near the earth's surface by atmospheric agents. These changes result in disintegration and decomposition of the material.

WETTING FRONT. The greatest depth affected by moisture due to precipitation.

yr B.P. Uncorrected radiocarbon age expressed in years before present, calculated from 1950. Calendar-corrected ages are expressed in ka, or, if warranted, as A.D. or B.C.

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# Appendix F

Geotechnical Engineering Report

May 17, 2019 File No.: 302615-001

Mr. Ty Intravia TTI Developers 601 McCray Street, Ste. 205 Hollister, CA 95023

PROJECT: LICO PROPERTY DEVELOPMENT

ENTERPRISE ROAD, APNS 020-290-051 & -052 HOLLISTER, SAN BENITO COUNTY, CALIFORNIA

SUBJECT: Geotechnical Engineering Report

REF.: Proposal for a Geotechnical Engineering Investigation, Lico Property

Development, Enterprise Road, APNs 020-290-051 & -052, Hollister, San Benito County, California, by Earth Systems Pacific, dated May 16, 2019

#### Dear Mr. Intravia:

In accordance with your authorization of the above-referenced proposal, this geotechnical engineering report was prepared for use in development of plans and specifications for the planned development of the approximately 50-acre property located on Enterprise Road (APNs 020-290-051 and -052) in the Hollister area of San Benito County. As shown on the Vesting Tentative Map by MacKay & Somps, the development will consist of 151 detached single-family residential lots that will be accessed by several new interior streets originating at Enterprise Road. Extensive site grading is planned, including cuts and fills on the order of 25 feet. Maximum slope heights in excess of 30 feet are planned upon completion of grading. Retaining walls up to about four feet in height will be constructed between some of the lots. Two stormwater detention basins, having maximum depths of approximately 11 feet, are planned along the northern edge of the property.

An existing residence on the northwest section of the site is to remain, but other nearby structures are to be demolished to accommodate the development. Plans for the new residences are not currently available, but we understand that they will be one or two story conventional light frame structures supported by either reinforced concrete structural mat foundations or post-tensioned concrete slabs-on-grade. The project will be served by public utilities.



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A Fault Evaluation Report was prepared by ENGEO Incorporated (Project No. 11227.000.100, dated September 15, 2015). That report provided a fault exclusion zone for structures along the southwestern property edge that was incorporated in the project design. Information contained in the ENGEO report, as well as the results of a preliminary geologic fault study for the project and a geotechnical subsurface investigation and laboratory testing program conducted by Earth Systems Pacific (ESP) during 2008 for a portion of the site (APN 020-290-51), were utilized in our analysis and report.

#### **Scope of Services**

The scope of work for the geotechnical engineering investigation included a general site reconnaissance, subsurface exploration, laboratory testing of soil samples, engineering evaluation of the data collected, review of information contained in the Fault Evaluation Report by ENGEO, and preparation of this report. The analysis and subsequent recommendations were based on the Vesting Tentative Map by MacKay & Somps (Sheets 1 through 11, dated November 2015), and verbal information provided by the client.

The report and recommendations are intended to comply with the considerations of Sections 1803.1 through 1803.6, and 1803.7 (portions of) of the 2016 California Building Code (CBC), and common geotechnical engineering practice in this area at this time under similar conditions. The tests were performed in general conformance with the standards noted, as modified by common geotechnical practice in this area at this time under similar conditions.

Preliminary geotechnical recommendations for site preparation and grading, post-tensioned slab-on-grade and structural mat foundations, exterior flatwork, retaining walls, asphalt concrete pavement sections, utility trenches, site drainage and finish improvements, and geotechnical observation and testing are presented to guide the development of project plans and specifications. It is our intent that this report be used by the client to form the geotechnical basis of the design of the project as described herein, and in the preparation of plans and specifications.

Evaluation of the site geology, and analyses of the soil for infiltration rates, mold or other microbial content, lead, asbestos, corrosion potential, radioisotopes, hydrocarbons, or other chemical properties are beyond the scope of this report. This report does not address issues in



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the domain of contractors such as, but not limited to, site safety, loss of volume due to stripping of the site, shrinkage of soils during compaction, excavatability, shoring, temporary slope angles, and construction means and methods. Ancillary features such as temporary access roads, fences, light poles, signs, effluent disposal systems, swimming pools, LID/BMP improvements, and nonstructural fills are not within our scope and are also not addressed.

To verify that pertinent issues have been addressed and to aid in conformance with the intent of this report, it is requested that grading and foundation plans be submitted to the geotechnical engineer for review as they near completion. In the event that there are any changes in the nature, design, or locations of improvements, or if any assumptions used in the preparation of this report prove to be incorrect, the conclusions and recommendations contained herein should not be considered valid unless the changes are reviewed and the conclusions of this report are verified or modified in writing by the geotechnical engineer. The criteria presented in this report are considered preliminary until such time as they are verified or modified in writing by the geotechnical engineer in the field during construction.

#### **Site Setting**

The site consists of two irregularly-shaped parcels (APNs 020-290-051 and -052) located on the south side of Enterprise Road in the Hollister area of San Benito County, California. At the time of the investigation, the properties immediately to the southwest were occupied by rural singlefamily residences, and the Oak Creek residential development was to the east. Two residences and a few agricultural out-buildings were present on the northwest section of the subject site, and the remainder of the site was undeveloped. The site is located on the northeast flank of a northwest-southeast trending broad topographic ridge. Locally, the site topography is characterized by broad rolling ridges and valleys descending toward a wide natural drainage channel roughly paralleling Enterprise Road and seasonally flowing in a northwest direction. In some areas, the channel has been modified by previous grading, particularly to construct a cut basin and fill berm for stormwater management on an easement near the northeast site corner, just beyond the proposed development area. The ground elevations range from approximately 480 feet at the southwest corner to 345 feet at the northwest corner, with a distinctly steeper slope having inclinations greater than 20 percent crossing the approximate center of the property. The site was vegetated with a variable cover of weeds and grass, with an orchard and mature trees present on the northwestern portion of the property near the existing structures.



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#### **Subsurface Investigation and Laboratory Testing**

To supplement the six borings drilled by Earth Systems Pacific on the southern portion of the site in 2008, eight additional borings were advanced on November 1, 2018. The supplemental borings were drilled using a Mobile Drill rig, Model B-53, equipped with an 8-inch outside diameter, continuous flight, hollow stem auger. The approximate boring locations are shown on the attached Boring Location Map. For numerical continuity, the 2008 borings were identified as Borings 1 through 6, and the supplemental borings were identified as Borings 7 through 14.

Soils encountered in the borings were categorized and logged in general accordance with the Unified Soil Classification System and ASTM D 2488-17. Soil samples were obtained from the borings using an internally-lined barrel sampler (ASTM D 3550-17, with shoe similar to D 2937-17), Standard Penetration Tests - SPT (ASTM D 1586-11) were conducted at selected depths, and bulk soil samples were obtained from the auger cuttings. Copies of the boring logs are attached (please note that the original borings describe the site APN using a previous designation).

The previous laboratory testing program included unit weight and moisture tests on selected liner samples (ASTM D 2937-04, modified for ring liners), particle size distribution tests on four liner samples and one bulk sample (ASTM D 422-07 and D 1140-06), and R-value tests on two bulk samples (ASTM D 2844-07). For the supplemental investigation, ten liner samples were tested for unit weight and/or moisture (ASTM D 2937-17e1, modified for internal liners), and two bulk samples and two ring samples were tested for particle size distribution (ASTM D 1140-17 and D 422-63/07, or D 7928-17). Two of these samples were also tested for plasticity index (ASTM D 4318-17). Copies of the laboratory test results are attached.

#### **General Subsurface Profile**

In general, the soils encountered in the borings were mixtures of lean and fat clays, silts, sands, and gravels. Some occasional cobbles were also encountered. These predominantly fine-grained deposits had very stiff to hard consistencies, and these predominantly coarse-grained materials were typically medium dense to very dense. Drilling refusal was experienced in Boring 10 at an approximate depth of 7 feet due to the presence of hard cemented clay with cobbles. Except for some slightly moist surface material, the soils were generally moist at the time of the investigation. Free subsurface water was not encountered within the maximum 20-foot depth of exploration.



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#### **Conclusions**

#### Site Suitability:

Based on the results of the subsurface investigation and laboratory testing program, in our opinion, the site is geotechnically suitable for the proposed Lico Property residential development provided that the recommendations contained herein are implemented in the design and construction. The primary geotechnical consideration is the high expansion potential of the clay soils at the site, as discussed below. Due to the sloping nature of the site and the planned differential thicknesses of cuts and fills within the building pads, measures should be taken during grading to provide more uniform support for the proposed improvements.

#### Soil Expansion Potential:

Plasticity index tests performed on four samples of the upper clay soils from the site resulted in liquid limits (LL) ranging from 21 to 48 and plasticity indices (PI) ranging from 6 to 32. The greater values indicate that soils having high expansion potentials are present at the site. Expansive soils tend to swell with increases in soil moisture and shrink as the soil moisture decreases. The volume changes that the soils undergo in this cyclical pattern can stress and damage foundations, exterior flatwork, and other improvements if precautionary measures are not incorporated into the design and construction procedures. To help mitigate the effects of the expansive soils, the post-tensioned slabs or structural mat foundations should be designed to withstand forces related to soil expansion and contraction. The upper soils should also be removed, moisture conditioned, and blended during grading to help reduce the amount of future expansion. Exterior concrete flatwork should be constructed over a layer of nonexpansive imported material.

#### Seismic Setting:

Details of the seismic setting of the site are provided in Fault Evaluation Report by ENGEO, and the report provided a fault exclusion zone for structures along the southwestern property edge that was incorporated in the project design. Severe ground shaking should be expected during the design life of the planned residences. At a minimum, the planned improvements should be designed to resist seismic shaking in accordance with current California Building Code (CBC) requirements. Seismic design parameters based on the 2016 edition of the CBC are presented later in the report.



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#### <u>Liquefaction Potential:</u>

The term liquefaction refers to the liquefied condition and subsequent softening that can occur in soils when they are subjected to cyclic strains, such as those generated during a seismic event. Studies of areas where liquefaction has occurred have led to the conclusion that saturated soil conditions, low soil density, grain sizes within a certain range, and a sufficiently strong earthquake, in combination, create a potential for liquefaction. According to the document "Liquefaction Susceptibility of the Hollister Area San Benito County, California, Final Technical Report", USGS Award No. 1434-HQ-97-GR-03125, by Lewis Rosenberg, the site is located in an area having a very low liquefaction potential, and potentially liquefiable soils were not encountered in our exploratory borings. Thus, measures to mitigate potential soil liquefaction are not considered necessary for the project.

#### Recommendations

#### Site Preparation and Grading

- The site should be prepared for grading by removing existing trees and other vegetation, roots larger than 1 inch in diameter, foundations and demolition debris, and other potentially deleterious materials from areas to receive improvements. The site preparation operations should be observed by the geotechnical engineer prior to continuing grading.
- Existing utility lines that will not remain in service should be either removed or abandoned. The appropriate method of utility abandonment will depend upon the type, depth, and location of the utility. Recommendations for abandonment can be made as necessary.
- 3. The soil in the building areas and in areas to receive exterior flatwork and other improvements should be removed (overexcavated) to minimum depths of 1 foot below existing grade, or 1 foot below the planned building pad elevations, whichever is deeper. The overexcavated areas should extend a minimum of 5 feet beyond the planned building foundation perimeters, and 2 feet beyond the edges of exterior flatwork and other improvements.



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- 4. Where a building pad will span cuts and fills, or where the depth of fill will vary significantly across the building area, the soil should be removed (overexcavated) and replaced as compacted fill to provide a relatively uniform depth of compacted fill beneath the structure. For cut/fill building pads, the soil should be overexcavated as necessary to provide a minimum 2 feet of compacted fill material below the planned building area. Additional depth of overexcavation may be necessary where the depth of fill beneath the building area will vary by more than 50 percent (see following paragraph).
- 5. For building pads in fill where the planned fill depth (including replaced overexcavated material per above) will vary by more than 50 percent, the exposed soil surfaces should be overexcavated as necessary so that the thickness of fill material within the building area will not vary by more than 50 percent. For example, if a building pad is to receive 2 feet of fill at one edge and 10 feet of fill at the opposite edge, the side of the pad to receive 2 feet of fill should be overexcavated so that a minimum of 5 feet of compacted fill is present across the pad.
- 6. The overexcavation should be observed by the geotechnical engineer prior to continuing grading. If soft soils, buried objects, existing undocumented fill, or other potentially deleterious conditions are observed during overexcavation, additional depth of overexcavation or other remedial measures may be recommended by the geotechnical engineer.
- 7. The overexcavated surfaces should be cross-scarified to an approximate depth of 8 inches. The soil should then be moisture conditioned to a level above optimum moisture content and recompacted to a minimum of 90 percent of maximum dry density. Cut surfaces to receive improvements should be scarified and recompacted in a similar manner.
- 8. The previously overexcavated material can be re-used as fill provided that it is cleared of excessive quantities of debris, organics, or other potentially deleterious materials. Fill should be placed in moisture conditioned lifts not exceeding 8 inches in loose thickness and compacted to a minimum of 90 percent of maximum dry density. Large roots, rock, debris, and irreducible material larger than 4 inches in diameter should be removed from the soil prior to compaction.



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- 9. In areas where fill will be placed above a cut slope, the fill should be keyed into the cut. The keyway should extend from approximately 2 feet behind the face of the cut portion of the slope, back into the slope for a minimum distance of 8 feet or 1-½ times the width of the compaction equipment, whichever is wider. The keyway should penetrate a minimum of 3 feet into firm native soil at the front edge of the keyway. The actual configuration and depth of the keyway should be recommended by the geotechnical engineer based on conditions observed at the time of grading.
- 10. The slope above the keyway, as well as any surfaces steeper than 10 percent to receive fill, should be cut to create benches. The benches should be a minimum of 6 feet wide and should be bottomed into firm native soil. Other slopes steeper than 10 percent to receive fill should be benched in a similar manner.
- 11. The bottoms of the keyways and benches should be angled 2 to 3 percent back into the slope. The soil at the bottoms of the keyways and benches should be cross-scarified to an approximate depth of 8 inches, moisture conditioned to a level above optimum moisture content, and recompacted. The keying and benching operations should be observed by the geotechnical engineer during grading.
- 12. Due to the potential that seepage of subsurface water could destabilize the fill, a subsurface drain should be installed in each keyway. The subsurface drain should consist of a minimum 4-inch diameter rigid perforated pipe covered with gravel surrounded by filter fabric, or encased in Caltrans Class 2 permeable material. Alternatively, a prefabricated synthetic drain could be utilized. The locations and configuration of the drains should be as recommended by the geotechnical engineer based on conditions observed at the time of grading. The subsurface drain system should be connected to one or more non-perforated pipes that discharge in a non-erosive manner away from slopes, foundations, and other improvements. Depending on the observed conditions, installation of one or more drains in the benches may also be recommended.
- 13. Fill should be placed in lifts not exceeding 8 inches in loose thickness, moisture conditioned to a level above optimum moisture content, and compacted to a minimum of 90 percent of maximum dry density. Organics and rock, debris, and irreducible material larger than 4 inches in diameter should be removed from the soil to be compacted.

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- 14. If fill is to be imported for general use at the site (other than nonexpansive imported material), the fill should be coarse grained (ASTM D 2487-17) with a plasticity index (ASTM D 4318-17) of 20 or less. Nonexpansive imported material should be placed in areas to receive exterior concrete (refer to Exterior Concrete Flatwork below). Proposed imported soils should be evaluated by the geotechnical engineer before being transported to the site, and on an intermittent basis during placement and compaction on the site.
- 15. Due to the fine-grained nature of the site soils, and depending on moisture conditions at the time of construction, there is a potential for the soils to become unstable during grading. Unstable soils hinder compactive effort and are inappropriate for placement of additional fill. Alternatives to correct instability include aeration to dry the soils, lime treatment, and the use of gravel or geotextiles as stabilizing measures. Recommendations for stabilization should be provided by a representative of this firm as needed during construction.
- 16. Cut and fill slopes should not be steeper than 2:1, measured horizontally to vertically.

#### **Foundations**

1. The residences should be supported by post-tensioned slab or structural mat foundations designed to resist soil expansion and contraction. Post-tensioned slabs should be designed in accordance with the provisions of the current edition of the California Building Code and the recommendations of the Post-Tensioning Institute. The following design criteria were developed for the post construction case in general accordance with the recommendations contained in the document "Design and Construction of Post-Tensioned Slabs-on-Ground", 3<sup>rd</sup> Edition published by the Post-Tensioning Institute. The criteria were based on Thornthwaite Moisture Indices ranging from -20 for dry conditions to +10 for irrigated conditions.

Edge Moisture Variation Distance (e<sub>m</sub>)

Center Lift Condition 8.0 feet Edge Lift Condition 4.4 feet

Estimated Differential Swell (y<sub>m</sub>)

Center Lift Condition 0.9 inches
Edge Lift Condition 2.4 inches



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2. For design of structural mat foundations, the effective plasticity index (PI) based on the method presented in Section 1808.6.2 of the California Building Code should be 30. The following design parameters should also pertain for design of structural mat foundations.

Edge cantilever length 8 feet
Interior free span 12 feet

3. Additional design criteria for both post-tensioned slabs and structural mat foundations are as follows:

| Allowable Bearing Capacity (dead loads)             | 1,500 psf |
|---|-----------|
| Allowable Bearing Capacity (dead + live loads)      | 2,000 psf |
| Allowable Bearing Capacity (DL+LL+ wind or seismic) | 2,500 psf |

Subgrade Friction Factor (slab against subgrade) 0.25

Modulus of subgrade reaction (K<sub>30</sub>) 20 psi/inch

Total settlement 1 inch
Differential settlement, within 25 feet ½ inch

4. The seismic design parameters for the site per Chapter 16 of the California Building Code (2016 Edition) are as follows. The values were determined utilizing the SEAOC/OSHPD web-based tool and the provisions of ASCE 7-10. The site coordinates were determined using the Google Earth web site.

Site Class = D

Short Term Spectral Acceleration Parameter,  $S_s = 2.273 g$ 

1 Second Spectral Acceleration Parameter, S<sub>1</sub> = 0.872 g

Site Coefficient, Fa = 1.00

Site Coefficient,  $F_v = 1.50$ 

Adjusted Spectral Acceleration Parameter, S<sub>MS</sub> = 2.273 g

Adjusted Spectral Acceleration Parameter, S<sub>M1</sub> = 1.307 g

Design Spectral Acceleration Parameter, S<sub>DS</sub> = 1.515 g

Design Spectral Acceleration Parameter, S<sub>D1</sub> = 0.872 g



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- 5. The building pads should be periodically moisture conditioned as necessary to maintain the soil moisture content at a minimum of 2 percent above optimum to a minimum depth of 12 inches at the time of placement of concrete or vapor retarding membranes. The moisture content of the soil should be tested by the geotechnical engineer prior to placement of the concrete or vapor retarding membranes.
- 6. In areas where moisture transmitted from the subgrade would be undesirable, a vapor retarder should be utilized beneath the post-tensioned slab foundation. The vapor retarder should comply with ASTM Standard Specification E 1745-17 and the latest recommendations of ACI Committee 302. The vapor retarder should be installed in accordance with ASTM Standard Practice E 1643-18a. Care should be taken to properly lap and seal the vapor retarder, particularly around utilities, and to protect it from damage during construction.
- 7. If sand, gravel or other permeable material is to be placed over the vapor retarder, the material over the vapor retarder should be only lightly moistened and not saturated prior to casting the slab concrete. Recent studies, including those by ACI Committee 302, have concluded that excess water above the vapor retarder would increase the potential for moisture damage to floor coverings and could increase the potential for mold growth or other microbial contamination. The studies also concluded that it is preferable to eliminate the sand layer and place the slab concrete in direct contact with the vapor retarder, particularly during wet weather construction. However, placing the concrete directly on the vapor retarder would require special attention to using the proper vapor retarder, concrete mix design, and finishing and curing techniques.
- 8. When concrete slabs are in direct contact with vapor retarders, the concrete water to cement (w/c) ratio should be correctly specified to control bleed water and plastic shrinkage cracking. Also, the concrete could be proportioned to reduce its porosity (and its corresponding potential for transmitting moisture) by limiting the w/c ratio. Concrete materials, placement and curing methods should be specified by the design professional.
- 9. To further protect moisture-sensitive floor coverings, the perimeters of the posttensioned slabs and structural mat foundations should be deepened to penetrate a minimum of 6 inches into the subgrade soil.



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The post-tensioned slabs and structural mat foundations should be constructed and maintained in accordance with the publication Construction and Maintenance Manual for Post-tensioned Slab-on-Ground Foundations by the Post-Tensioning Institute. Particular attention should be paid to the "Property Owner Maintenance" and "Landscaping" sections of the Manual.

#### **Exterior Flatwork**

- 1. Exterior concrete flatwork should have a minimum thickness of 4 full inches and should be reinforced as directed by the architect/engineer. Due to the soil expansion potential, exterior flatwork should be cast on a minimum 8-inch layer of compacted, nonexpansive material such as clean sand or aggregate base. However, a greater thickness of nonexpansive material would enhance flatwork performance. Prior to placement of the nonexpansive material, the soil surface in the flatwork area should be at or above optimum moisture content, and no desiccation cracks should be present.
- Exterior flatwork adjacent to the structure should be designed to be independent of the
  post-tensioned slab or structural mat foundation. The flatwork should not be doweled to
  foundations, and a separator should be placed between the two.
- 3. Prior to placement of the concrete, the nonexpansive material in the flatwork area should moistened, and no desiccation cracks should be present.
- 4. To reduce shrinkage cracks in concrete, the concrete aggregates should be of appropriate size and proportion, the water/cement ratio should be low, the concrete should be properly placed and finished, contraction joints should be installed, and the concrete should be properly cured. Concrete materials, placement and curing specifications should be at the direction of the architect/engineer.

#### **Retaining Walls**

Retaining walls should be supported by conventional spread footings. The footings should
have minimum depths of 30 inches below lowest adjacent grade and should bear in firm
native soil or compacted engineered fill. The footing reinforcement should be specified
by the design engineer. The footing excavations should be observed by the geotechnical



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engineer to verify penetration into firm native material prior to placement of formwork and should be moisture conditioned to close any desiccation cracks prior to concrete placement.

- 2. Footings should be designed using a maximum allowable bearing capacity of 2,500 psf dead plus live load. This value may be increased by one-third when transient loads such as wind or seismicity are included. Using these criteria, long term total and differential foundation settlements are expected to be on the order of ½ inch.
- 3. Resistance to lateral loads should be calculated based on a passive equivalent fluid pressure of 250 pcf and a friction factor of 0.25. Passive and frictional resistance can be combined in the calculations without reductions. These values are based on the assumption that backfill adjacent to foundations is adequately compacted.
- 4. Lateral earth pressures for wall design should be based on the following parameters.

| Active equivalent fluid pressure (horizontal backfill)  | 60 pcf  |
|---|---------|
| At-rest equivalent fluid pressure (horizontal backfill) | 75 pcf  |
| Active equivalent fluid pressure (sloping backfill)     | 85 pcf  |
| At-rest equivalent fluid pressure (sloping backfill)1   | .10 pcf |

- 5. If seismic forces are to be considered in the retaining wall design, the seismic increment of earth pressure should be 10H pounds per square foot, where H is the height of the retained soil. The seismic pressure should be applied uniformly on the back of the wall along the height of the retained material.
- 6. Retaining wall backfill should be fully drained utilizing either a free draining gravel blanket, permeable material, or a manufactured synthetic drainage system. Water from the drainage medium should be collected and discharged via either a rigid perforated pipe or weep holes. Collection pipes should be placed perforations downward near the bottom of the drainage medium and should discharge in a nonerosive manner away from foundations, slopes, and other improvements. Drainage medium consisting of a gravel blanket or permeable material should have a width of approximately 1 foot and should extend upward to within 1 foot of the top of the wall backfill. The upper foot of backfill



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over the drainage medium should consist of native soil to reduce the flow of surface drainage into the wall drain system. Gravel blankets should be separated from the backfill soil using a permeable synthetic fabric conforming to Caltrans Standard Specifications, Section 88-1.02B, Class A. Permeable material should conform to Section 68-2.02F(3), Class 2, of the Caltrans Standard Specifications. Manufactured synthetic drains such as Miradrain or Enkadrain should be installed in accordance with the recommendations of the manufacturer.

- 7. Water from the drainage medium can be drained using weep holes, provided that seepage at the base of the wall is acceptable. The weep holes should consist of minimum 1-½ inch diameter holes at 10-foot maximum spacings. The weep holes should be placed as low as possible on the wall. Corrosion-resistant screens or filter fabric should be placed behind the weep holes to reduce the chance of the drainage medium from washing out from behind the wall.
- 8. Retaining wall backfill should be placed in thin, moisture conditioned, lifts, compacted to a minimum 90 percent of maximum dry density, as tested by the geotechnical engineer.
- 9. The architect/engineer should bear in mind that retaining walls by their nature are flexible structures, and this flexibility can result in cracking of surface coatings. Where walls are to be plastered or will otherwise have a finish surface applied, this flexibility should be considered in determining the suitability of the surfacing material, spacing of horizontal and vertical joints, connections to structures, etc.
- 10. Long-term settlement of properly compacted sand or gravel retaining wall backfill should be assumed to be about ¼ percent of the depth of the backfill. Long-term settlement of properly compacted clayey retaining wall backfill should be assumed to be about ½ to 1 percent of the depth of the backfill. Improvements constructed near the tops of retaining walls should be designed to accommodate the estimated settlement.

#### **Pavement Sections**

1. Three R-value tests performed on samples of the upper clay soils from the site resulted in R-values of 10 and less than 5. The following pavement sections were based on the lower



R-value. The asphalt concrete (AC) sections were designed in accordance with the Caltrans Highway Design Method for Traffic Indices (TIs) of 4.0 through 8.0. Determination of the appropriate TI for each area to be paved is the province of the design engineer. The calculated base and AC thicknesses are for compacted material. Normal Caltrans construction tolerances should apply. The aggregate base should conform to Caltrans Class 2.

| R-value | Traffic | AC        | Class 2 Base |
|---------|---------|-----------|--------------|
|         | Index   | Thickness | Thickness    |
| <5      | 4.0     | 2.5"      | 8"           |
| <5      | 4.5     | 2.5"      | 10"          |
| <5      | 5.0     | 3.0"      | 10"          |
| <5      | 5.5     | 3.0"      | 12"          |
| <5      | 6.0     | 3.5"      | 13"          |
| <5      | 6.5     | 3.5"      | 15"          |
| <5      | 7.0     | 4.0"      | 16"          |
| <5      | 7.5     | 4.5"      | 17"          |
| <5      | 8.0     | 4.5"      | 19"          |

- 2. The upper 12 inches of subgrade soil in areas to receive public street improvements should be compacted to a minimum 95 percent of maximum dry density. In private driveway and parking areas, the upper 8 inches of subgrade soil should be compacted to a minimum 92 percent of maximum dry density.
- 3. The aggregate base courses should be compacted to a minimum 95 percent of maximum dry density. The subgrade and base should be firm and unyielding when proofrolled with heavy, rubber-tired equipment prior to paving. The pavement subgrade soils should be periodically moistened as necessary prior to placement of the aggregate base to maintain the soil moisture content near optimum.
- 4. As an alternative to conventional pavement sections using aggregate base courses, the subgrade soil can be chemically treated with quicklime and/or Portland cement, and the aggregate base can be eliminated. Recommendations for chemical treatment of the



May 17, 2019

subgrade soil, if desired, should be provided by the geotechnical engineer based on the conditions observed at the time of construction.

- 5. To provide stability for curbs, they should be set back a minimum of 3 feet from the tops of slopes. Foundations may be provided to increase curb stability, particularly atop slopes.
- 6. Pavement longevity will be enhanced if the surface grade drains away from the edges of the pavement. Finished AC surfaces should slope toward drainage facilities at 2 percent where practicable, but in no case should water be allowed to pond.
- 7. Cutoff walls below curbs and around landscape islands may be used to extend the life of the pavement by reducing irrigation water and runoff that seeps into the aggregate base. Where utilized, cutoff walls should extend through the aggregate base to penetrate a minimum of 3 inches into the subgrade soils.
- 8. To reduce migration of surface drainage into the subgrade, maintenance of the paved areas is critical. Any cracks that develop in the AC should be promptly sealed.

#### **Utility Trenches**

- 1. A select, noncorrosive, granular, easily compacted material should be used as bedding and shading immediately around utility pipes. The site soils may be used for trench backfill above the select material. However, if obtaining compaction is difficult with the site soils, use of a more easily compacted sand may be desirable. The upper foot of backfill in unimproved areas should consist of native material to reduce the potential for seepage of water into the backfill.
- In private driveway and parking areas, the upper 8 inches of trench backfill should be compacted to a minimum 92 percent of maximum dry density. Trench backfill in other areas should be compacted to a minimum of 90 percent of maximum dry density. For public street improvements, the trench backfill materials and compaction should be in accordance with County of San Benito standards. Jetting of utility trench backfill should not be allowed.



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3. Where utility trenches extend under perimeter foundations, exterior flatwork, or pavement the trenches should be backfilled entirely with compacted native soil. The zone of native soil should extend to a minimum distance of 2 feet on both sides of the foundation, flatwork, or pavement edges. If utility pipes pass through sleeves cast into the perimeter foundations, the annulus between the pipes and sleeves should be sealed.

#### Site Drainage and Finish Improvements

- 1. Unpaved ground surfaces should be finish graded to direct surface runoff away from site improvements at a minimum 5 percent grade for a minimum distance of 10 feet. The site should be similarly sloped to drain away from improvements during construction. If this is not practicable due to the terrain, property lines, or other site features, swales with improved surfaces or other drainage facilities should be provided to divert runoff from those areas. The landscape should be planned and installed to maintain proper surface drainage conditions.
- 2. Raised planter beds adjacent to foundations should be provided with sealed sides and bottoms so that irrigation water is not allowed to penetrate the subsurface beneath foundations. Outlets should be provided in the planters to direct accumulated irrigation water away from foundations.
- 3. Runoff should discharge in a non-erosive manner away from foundations, exterior flatwork, pavement, and other improvements in accordance with the requirements of the governing jurisdiction.
- 4. Stabilization of surface soils, particularly those disturbed during construction, by vegetation or other means during and following construction is essential to protect the site from erosion damage. Care should be taken to establish and maintain vegetation.
- 5. Due to the soil expansion potential, open areas adjacent to foundations, exterior flatwork, and other improvements should be irrigated or otherwise maintained so that constant moisture conditions are created throughout the year. Irrigation systems should be controlled to the minimum levels that will sustain the vegetation without saturating the soil.



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#### **Geotechnical Observation and Testing**

- It must be recognized that the recommendations contained in this report are based on a limited subsurface investigation and rely on continuity of the subsurface conditions encountered.
- 2. It is assumed that the geotechnical engineer will be retained to provide consultation during the design phase, to interpret this report during construction, and to provide construction monitoring in the form of testing and observation.
- 3. Unless otherwise stated, the terms "compacted" and "recompacted" refer to soils placed in level lifts not exceeding 8 inches in loose thickness and compacted to a minimum of 90 percent of maximum dry density. The standard tests used to define maximum dry density and field density should be ASTM D 1557-12 and ASTM D 6938-17, respectively, or other methods acceptable to the geotechnical engineer and jurisdiction.
- 4. Unless otherwise stated, "moisture conditioning" refers to adjusting the soil moisture to at least optimum moisture prior to application of compactive effort.
- 5. At a minimum, the following should be provided by the geotechnical engineer:
  - Review of grading and foundation plans as they near completion
  - Professional observation during site preparation, grading, and foundation construction
  - Oversight of soil compaction testing during grading
  - Oversight of soils special inspection during grading
- 6. Special inspection of grading should be provided as per Section 1705.6 and Table 1705.6 of the CBC; the soils special inspector should be under the direction of the geotechnical engineer. In our opinion, the following operations should be subject to *continuous* soils special inspection:
  - Slope keying and benching
  - Overexcavation to the recommended depths
  - Scarification and recompaction
  - Fill placement and compaction



May 17, 2019

- 7. In our opinion, the following operations may be subject to *periodic* soils special inspection; subject to approval by the Building Official:
  - Site preparation
  - Proposed imported materials
  - Compaction of utility trench backfill
  - Compaction of pavement subgrade and aggregate base
  - Compaction retaining wall backfill
  - Building pad moisture conditioning
- 8. It will be necessary to develop a program of quality control prior to beginning grading. It is the responsibility of the owner, contractor, or project manager to determine any additional inspection items required by the architect/engineer or the governing jurisdiction.
- 9. The locations and frequencies of compaction tests should be as per the recommendations of the geotechnical engineer at the time of construction. The recommended test locations and frequencies may be subject to modification by the geotechnical engineer based upon soil and moisture conditions encountered, the size and type of equipment used by the contractor, the general trend of the compaction test results, and other factors.
- 10. A preconstruction conference among a representative of the owner, the geotechnical engineer, the soils special inspector, the architect/engineer, and contractors is recommended to discuss planned construction procedures and quality control requirements. The geotechnical engineer should be notified at least 48 hours prior to beginning grading operations.

#### Closure

This report is valid for conditions as they exist at this time for the type of project described herein. Our intent was to perform the investigation in a manner consistent with the level of care and skill ordinarily exercised by members of the profession currently practicing in the locality of this project under similar conditions. No representation, warranty, or guarantee is either expressed or implied. This report is intended for the exclusive use by the client for the subject project. Application beyond the stated intent is strictly at the user's risk.



May 17, 2019

If changes with respect to the project type or location become necessary, if items not addressed in this report are incorporated into plans, or if any of the assumptions stated in this report are not correct, the geotechnical engineer should be notified for modifications to this report. Any items not specifically addressed in this report should comply with the California Building Code and the requirements of the governing jurisdiction.

The preliminary recommendations of this report are based upon the geotechnical conditions encountered during the investigation, and may be augmented by additional requirements of the architect/engineer, or by additional recommendations provided by the geotechnical engineer based on conditions exposed at the time of construction.

If Earth Systems Pacific is not retained to provide construction observation and testing services, it shall not be responsible for the interpretation of the information by others or any consequences arising there from.

This document, the data, conclusions, and recommendations contained herein are the property of Earth Systems Pacific. This report shall be used in its entirety, with no individual sections reproduced or used out of context. Copies may be made only by Earth Systems Pacific, the client, and his authorized agents for use exclusively on the subject project. Any other use is subject to federal copyright laws and the written approval of Earth Systems Pacific.

Thank you for this opportunity to have been of service. Please do not hesitate to contact this office if you have any questions regarding this report.

Sincerely,

Earth Systems Pac

George J. Barnett

Geotechnical Engineer

Attachments:

**Boring Location Map** 

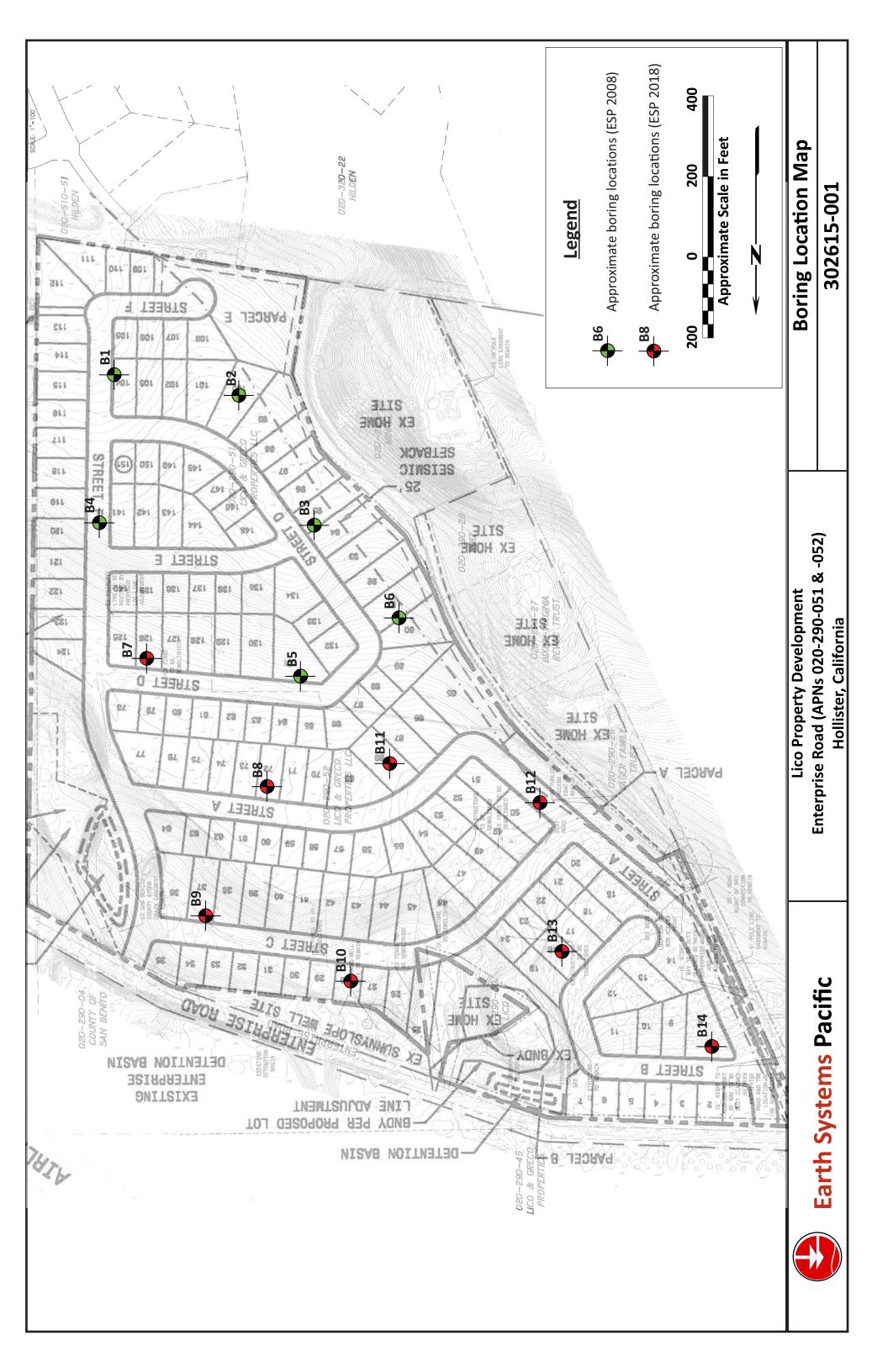
**Boring Logs** 

**Laboratory Test Results** 

Doc. No.:

1905-031.SER/ev

Phillip Penrose Staff Engineer





LOGGED BY: B. Faust DRILL RIG: B-40

AUGER TYPE: 8" Hollow Stem

Boring No. 1 PAGE 1 OF 1

JOB NO.: SH-10127-SC

DATE: 09/08/08

|                              | T               | 1                                       | CTTTE. O TIONOW Stell  |                    |                |                      |                 | 1 E. 09/00/00       |  |
|------------------------------|-----------------|---|--|--------------------|----------------|----------------------|-----------------|---------------------|--|
|                              | ြက္လ            |   | LICO RESIDENTIAL DEVELOPMENT   |                    | SAI            | MPLE [               | DATA            |                     |  |
| DEPTH<br>(feet)              | USCS CLASS      | SYMBOL                                  | Enterprise Road ~ APN 020-290-029<br>Hollister, San Benito County, California  | INTERVAL<br>(feet) | SAMPLE<br>TYPE | DRY DENSITY<br>(pcf) | MOISTURE<br>(%) | BLOWS<br>PER 12 IN. |  |
| <b>—</b> 0—                  | ) >             |   | SOIL DESCRIPTION   | Ξ                  | S.             | DRY                  | MO              | PE B                |  |
| 1 - 2                        | SC<br>CL/<br>CH |   | Yellow brown CLAYEY SAND, slightly moist, medium dense; disked Yellow brown SANDY LEAN to FAT CLAY, moist, hard, fine to medium sand | 1.0-5.0<br>2.0-2.5 |                | 118.2                | 13.5            | 71                  |  |
| 3<br>-<br>4<br>-<br>5        |                 |   |  | 4.0-4.5            | -              | 118.3                | 10.7            | 50/2"               |  |
| 8 - 7 - 8 - 9 - 10 - 11 - 12 | GM              | 000000000000000000000000000000000000000 | Dark yellow brown SILTY GRAVEL with sand, moist, dense   | 8.5-10.0           | •              |                      |                 | 34                  |  |
| 13<br>-<br>14<br>-           |                 | 000000000000000000000000000000000000000 |  | 13.5–15.0          | •              |                      |                 | 40                  |  |
| 18 19 20 21 22 24 25 26      |                 |   | End of Boring @ 15.0' No subsurface water encountered  |                    |                |                      |                 |                     |  |



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AUGER TYPE: 8" Hollow Stem

Boring No. 2

PAGE 1 OF 1

JOB NO.: SH-10127-SC

DATE: 09/08/08

|                               | (0         |        | LICO RESIDENTIAL DEVELOPMENT   |                    | SAI            | MPLE [               | DATA            | 12. 03/00/00        |
|-------------------------------|------------|--------|--|--------------------|----------------|----------------------|-----------------|---------------------|
| DEPTH<br>(feet)               | USCS CLASS | SYMBOL | Enterprise Road ~ APN 020-290-029<br>Hollister, San Benito County, California  | INTERVAL<br>(feet) | SAMPLE<br>TYPE | DRY DENSITY<br>(pcf) | MOISTURE<br>(%) | BLOWS<br>PER 12 IN. |
| -0-                           | ä          |        | SOIL DESCRIPTION   | Ā                  | S/             | DRY                  | MO              | 8 11                |
| - 1                           | SC         |        | Yellow CLAYEY SAND   |                    |                |                      |                 |                     |
| 2 - 3                         | CL/<br>CH  |        | Olive to yellow brown SANDY LEAN to FAT CLAY, moist, hard, fine to medium sand | 2.0-2.5            |                | 112.4                | 14.1            | 37                  |
| 5                             |            |        |  | 4.5-5.0            |                | 122.8                | 13.4            | 68                  |
| - 6 - 7 - 8                   | SC         |        | Light yellow brown CLAYEY SAND, moist, medium dense, mostly medium sand        | 8.5–10.0           | •              |                      |                 | 21                  |
| 10 - 11 - 12 - 13             |            |        | -some gravel   |                    |                |                      |                 |                     |
| 13<br>-<br>14<br>-<br>15<br>- | CL         |        | Olive SANDY LEAN CLAY, moist, hard, mostly fine sand                           | 13.5-15.0          | •              |                      |                 | 30                  |
| 17<br>-<br>18<br>-<br>19      |            |        |  | 18.5–20.0          | •              |                      |                 | 31                  |
| 21<br>-<br>22<br>-<br>23      |            |        | End of Boring @ 20.0' No subsurface water encountered                          |                    |                |                      |                 |                     |
| -<br>24<br>-<br>25<br>-<br>26 |            |        |  |                    |                |                      |                 |                     |



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AUGER TYPE: 8" Hollow Stem

Boring No. 3

PAGE 1 OF 1

JOB NO.: SH-10127-SC DATE: 09/08/08

|                          |            |   | LICO RESIDENTIAL DEVELOPMENT   |                    | SA     | MPLE [               |                 | 12. 00/00/00        |
|--------------------------|------------|---|--|--------------------|--------|----------------------|-----------------|---------------------|
| DEPTH<br>(feet)          | USCS CLASS | SYMBOL                                  | Enterprise Road ~ APN 020-290-029 Hollister, San Benito County, California                                     | INTERVAL<br>(feet) | SAMPLE | DRY DENSITY<br>(pcf) | MOISTURE<br>(%) | BLOWS<br>PER 12 IN. |
|                          | Š          |   | SOIL DESCRIPTION   | Ā                  | S T    | DRY (                | MO              | 18 H                |
| -0-<br>1<br>-            | SC<br>CL/  |   | Dark yellow brown CLAYEY SAND, slightly<br>moist, medium dense; disked<br>Yellow brown SANDY LEAN to FAT CLAY, |                    |        |                      |                 |                     |
| 3                        | CH         |   | moist, hard, fine to medium sand   | 2.0-2.5            |        | 110.3                | 8.9             | 73                  |
| 4 -                      |            |   | -less plastic  | 4.0-4.5            | -      | 132.7                | 11.7            | 50/6"               |
| 6<br>-<br>7<br>-<br>8    | GC         | 000000000000000000000000000000000000000 | Dark yellow brown CLAYEY GRAVEL with sand, moist, dense, mostly fine gravel                                    |                    |        |                      |                 |                     |
| 9                        |            |   |  | 8.5-10.0           |        |                      |                 | 22                  |
| 10<br>-<br>11<br>-<br>12 | SM         |   | Light yellow brown SILTY SAND, moist, medium dense   |                    |        |                      |                 |                     |
| 13<br>                   | CL         |   | Olive to yellow brown LEAN CLAY, moist, very stiff   | 13.5-15.0          | •      |                      |                 | 21                  |
| 15<br>-<br>16            |            |   | End of Boring @ 15.0'<br>No subsurface water encountered   |                    |        |                      |                 |                     |
| 17<br>-<br>18            |            |   |  |                    |        |                      |                 |                     |
| 19                       |            |   |  |                    |        |                      |                 |                     |
| 21                       |            |   |  |                    |        |                      |                 |                     |
| 22                       |            |   |  |                    |        |                      |                 |                     |
| 23                       |            |   |  |                    |        |                      |                 |                     |
| 24                       |            |   |  |                    |        |                      |                 |                     |
| 25                       |            |   |  |                    |        |                      |                 |                     |
| 26                       |            |   |  |                    |        |                      |                 |                     |



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AUGER TYPE: 8" Hollow Stem

Boring No. 4

PAGE 1 OF 1 JOB NO.: SH-10127-SC

DATE: 09/08/08

|                 | DATE: 09/08/08 |        |  |                    |        |                      |                 |                     |
|-----------------|----------------|--------|--|--------------------|--------|----------------------|-----------------|---------------------|
|                 | SS             |        | LICO RESIDENTIAL DEVELOPMENT   |                    | SA     | MPLE [               | DATA            |                     |
| DEPTH<br>(feet) | USCS CLASS     | SYMBOL | Enterprise Road ~ APN 020-290-029<br>Hollister, San Benito County, California                                  | INTERVAL<br>(feet) | SAMPLE | DRY DENSITY<br>(pcf) | MOISTURE<br>(%) | BLOWS<br>PER 12 IN. |
|                 | ם              |        | SOIL DESCRIPTION   | Ξ                  | /s     | DRY                  | Θ               | 18 19               |
| 1               | SC             |        | Yellow brown CLAYEY SAND, slightly moist,<br>medium dense; disked<br>Yellow brown SANDY LEAN CLAY, moist, hard |                    |        |                      |                 |                     |
| 2 -             | CL<br>SC       |        | Yellow brown CLAYEY SAND with gravel.  | 1.5-2.0            |        | 124.0                | 11.3            | 50/6"               |
| 3 -             |                |        | moist, very dense, mostly fine to medium sand, fine gravel   |                    |        |                      |                 |                     |
| 5               |                |        |  | 4.5-5.0            |        | 113.8                | 3.7             | 83                  |
| 6               |                |        |  |                    |        |                      |                 |                     |
| 7<br>-<br>8     |                |        |  |                    |        |                      |                 |                     |
| 9               | -014           |        | Valley by CHTV CAND III  | 8.5-10.0           |        |                      |                 | 53                  |
| 10              | SM             |        | Yellow brown SILTY SAND with gravel, moist, very dense, mostly medium sand, fine to coarse gravel              |                    |        |                      |                 |                     |
| 11              |                |        |  |                    |        |                      |                 |                     |
| 12<br>-<br>13   |                |        |  |                    |        |                      |                 |                     |
| 14              |                |        |  | 13.5-14.5          |        |                      |                 | 50/4"               |
| 15              |                |        | End of Boring @ 14.5'<br>No subsurface water encountered   |                    |        |                      |                 |                     |
| 16              |                |        |  |                    |        |                      |                 |                     |
| 17 - 18         |                | 1      |  |                    |        |                      |                 |                     |
| 19              |                | 1      | ×  |                    |        |                      |                 |                     |
| 20              |                |        |  |                    |        |                      |                 |                     |
| 21              |                |        |  |                    |        |                      |                 |                     |
| 22              |                |        |  |                    |        |                      |                 |                     |
| 23              |                |        |  |                    |        |                      |                 |                     |
| 24              |                |        |  |                    |        |                      |                 |                     |
| 25              |                |        |  |                    |        |                      |                 |                     |
| 26              |                |        |  |                    |        |                      |                 |                     |



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AUGER TYPE: 8" Hollow Stem

Boring No. 5 PAGE 1 OF 1

JOB NO.: SH-10127-SC DATE: 09/08/08

|                 | 1          |        | TIPE. 8 Hollow Stelli   | 1                  |                |                      |                 | 1 2. 09/06/06       |
|-----------------|------------|--------|---|--------------------|----------------|----------------------|-----------------|---------------------|
|                 | ဖွ         |        | LICO RESIDENTIAL DEVELOPMENT  |                    | SA             | MPLE [               | DATA            |                     |
| DEPTH<br>(feet) | USCS CLASS | SYMBOL | Enterprise Road ~ APN 020-290-029<br>Hollister, San Benito County, California | INTERVAL<br>(feet) | SAMPLE<br>TYPE | DRY DENSITY<br>(pcf) | MOISTURE<br>(%) | BLOWS<br>PER 12 IN. |
|                 | ő          |        | SOIL DESCRIPTION  | Ē                  | /s             | DRY                  | MO              | <u>B</u> <u>B</u>   |
| 1               | SC         |        | Yellow brown CLAYEY SAND, slightly moist, medium dense; disked                | 0.0-3.0            | 0              |                      |                 |                     |
| - 2             |            |        | -very dense   |                    |                |                      |                 |                     |
| 3               |            |        |   | 2.5-3.0            |                | 129.2                | 11.2            | 76                  |
| 4 - 5           |            |        | -orange brown   | 4.0-4.5            | =              | 122.3                | 9.3             | 50/5"               |
| 6 - 7           | SM         |        | Yellow SILTY SAND, moist, medium dense, fine to medium sand                   |                    |                |                      |                 |                     |
| 8 -             |            |        |   | 8.5-10.0           | •              |                      |                 | 16                  |
| 10<br>-<br>11   |            |        |   |                    |                |                      |                 |                     |
| 12<br>-<br>13   |            |        |   | 13.5–15.0          |                |                      |                 | 74                  |
| 14<br>-<br>15   | GC         | 00000  | Yellow brown CLAYEY GRAVEL with sand,<br>moist, very dense, fine gravel       | 13.5-15.0          |                |                      |                 | 71                  |
| 16<br>-         |            |        | End of Boring @ 15.0'<br>No subsurface water encountered                      |                    |                |                      |                 |                     |
| 17<br>-<br>18   |            |        |   |                    |                |                      |                 |                     |
| 19              |            |        |   |                    |                |                      |                 |                     |
| 20              |            |        |   |                    |                |                      |                 |                     |
| 21              |            |        |   |                    |                |                      |                 |                     |
| 22              |            |        |   |                    |                |                      |                 |                     |
| 23              |            |        |   |                    |                |                      |                 |                     |
| 24<br>-<br>25   |            |        |   |                    |                |                      |                 |                     |
| 26              |            |        |   |                    |                |                      |                 |                     |
| -               |            |        |   |                    |                |                      |                 |                     |



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AUGER TYPE: 8" Hollow Stem

Boring No. 6

PAGE 1 OF 1 JOB NO.: SH-10127-SC

DATE: 09/08/08

|  | AUGER TYPE: 8" Hollow Stem DATE: 09/08/08 |   |   |                    |                |                      |                 |                     |  |  |
|--|---|---|---|--------------------|----------------|----------------------|-----------------|---------------------|--|--|
|  | က္က                                       |   | LICO RESIDENTIAL DEVELOPMENT  |                    | SAI            | MPLE [               | DATA            |                     |  |  |
| DEPTH<br>(feet)                                | USCS CLASS                                | SYMBOL                                  | Enterprise Road ~ APN 020-290-029<br>Hollister, San Benito County, California | INTERVAL<br>(feet) | SAMPLE<br>TYPE | DRY DENSITY<br>(pcf) | MOISTURE<br>(%) | BLOWS<br>PER 12 IN. |  |  |
|  | s   |   | SOIL DESCRIPTION  | Ĭ,                 | \S'_           | DRY                  | MO              | PE 81               |  |  |
| -0-  | CL-<br>ML                                 |   | Dark yellow brown SILTY CLAY with sand,<br>moist, hard, mostly fine sand      | 0.0-3.0            | 0              |                      |                 |                     |  |  |
| 1 <del>2</del> 2                               |   |   |   | 1.5-2.0            |                | 112.8                | 5.3             | 50/6"               |  |  |
| 3 - 4 - 5 - 6                                  |   |   | —more clayey  | 4.0-4.5            |                | 116.4                | 12.0            | 50/6"               |  |  |
| 9<br>-10<br>-11                                | SM  |   | Yellow brown SILTY SAND, moist, medium dense, fine to medium sand             | 8.5–10.0           | •              |                      |                 | 13                  |  |  |
| 12<br>13<br>-<br>14<br>-<br>15                 | GM  | 000000000000000000000000000000000000000 | Yellow brown SILTY GRAVEL with sand, moist, dense, fine to coarse gravel      | 13.5–15.0          | •              |                      |                 | 50                  |  |  |
| - 18 - 19 - 20 - 21 - 22 - 23 - 24 - 25 - 26 - |   |   | End of Boring © 15.0' No subsurface water encountered                         |                    |                |                      |                 |                     |  |  |



Boring No. 7 PAGE 1 OF 1 FILE NO.: 302615-001 DATE: 11/1/18

LOGGED BY: D. Teimoorian DRILL RIG: Mobile B-53 Red AUGER TYPE: 8" Hollow Stem

|                 | SS         |        | Lico Property Development   |                    | S                | AMF           | LE DA                | ATA             |                    |                       |
|-----------------|------------|--------|---|--------------------|------------------|---------------|----------------------|-----------------|--------------------|-----------------------|
| DEPTH<br>(feet) | USCS CLASS | SYMBOL | Enterprise Road, APNs 020-290-051 & 052<br>Hollister, California                  | INTERVAL<br>(feet) | SAMPLE<br>NUMBER | AMPLE<br>TYPE | DRY DENSITY<br>(pcf) | MOISTURE<br>(%) | BLOWS<br>PER 6 IN. | POCKET PEN<br>(t.s.f) |
| 0_              | n          |        | SOIL DESCRIPTION  | Z                  | /S<br>N          | Ś             | DRY                  | MC              | B<br>Pf            | POC                   |
| -               | CL         |        | SANDY LEAN CLAY; very stiff, brown, moist, fine sand                              |                    |                  |               |                      |                 |                    |                       |
| 1 -             |            |        |   | 0.0-4.0            | Bag A            |               |                      |                 | 9                  |                       |
| 2 -             |            |        |   | 1.5-3.0            | 7-1              |               |                      | 7.9             | 18<br>23           |                       |
| -<br>-          |            |        |   |                    | -                |               |                      |                 |                    |                       |
| 4 -             |            |        | -hard, dark yellow brown  |                    |                  |               |                      |                 | 17<br>26           |                       |
| 5 -             |            |        |   | 3.5-5.0            | 7-2              |               | 100.7                | 19.5            | 30                 |                       |
| 6 -             |            |        |   |                    |                  |               |                      |                 |                    |                       |
| 7 -             |            |        |   |                    |                  |               |                      |                 |                    |                       |
| 8               |            |        |   |                    |                  |               |                      |                 |                    |                       |
| 9               |            |        |   |                    |                  |               |                      |                 | 29<br>26           |                       |
| 10              |            |        | - layer of well graded sand with clay approximately<br>6-inches thick             | 8.5-10.0           | 7-3              |               |                      |                 | 35                 |                       |
| 11              |            |        | o-inches thick  |                    |                  |               |                      |                 |                    |                       |
| -<br>12         |            |        |   |                    |                  |               |                      |                 |                    |                       |
| -<br>13         |            |        |   |                    |                  |               |                      |                 |                    |                       |
| -<br>14         | SC         |        | CLAYEY SAND; very dense, gray brown, moist, fine to coarse sand, few fine greavel |                    |                  |               |                      |                 | 33                 |                       |
| -<br>15         |            |        |   | 13.5-15.0          | 7-4              |               |                      |                 | 40<br>45           |                       |
| -               |            |        | Bottom of boring at 15  |                    |                  |               |                      |                 |                    |                       |
| 16              |            |        | Groundwater not encountered   |                    |                  |               |                      |                 |                    |                       |
| 17              |            |        |   |                    |                  |               |                      |                 |                    |                       |
| 18              |            |        |   |                    |                  |               |                      |                 |                    |                       |
| 19<br>-         |            |        |   |                    |                  |               |                      |                 |                    |                       |
| 20              |            |        |   |                    |                  |               |                      |                 |                    |                       |
| 21              |            |        |   |                    |                  |               |                      |                 |                    |                       |
| 22              |            |        |   |                    |                  |               |                      |                 |                    |                       |
| 23              |            |        |   |                    |                  |               |                      |                 |                    |                       |
| -<br>24         |            |        |   |                    |                  |               |                      |                 |                    |                       |
| -<br>25         |            |        |   |                    |                  |               |                      |                 |                    |                       |
| -<br>26         |            |        |   |                    |                  |               |                      |                 |                    |                       |
| -               |            |        |   |                    |                  |               |                      |                 |                    | <u> </u>              |



Boring No. 8 PAGE 1 OF 1

LOGGED BY: D. Teimoorian PAGE 1 OF 1
DRILL RIG: Mobile B-53 Red FILE NO.: 302615-001
AUGER TYPE: 8" Hollow Stem DATE: 11/1/18

|                 | 7.0        |        | RTYPE: 8 Hollow Stem   | SAMPLE DATA        |                  |               |                  |                 |                    |                       |  |
|-----------------|------------|--------|--|--------------------|------------------|---------------|------------------|-----------------|--------------------|-----------------------|--|
|                 | SS         |        | Lico Property Development  |                    | S                | AMF           |                  |                 | ı                  |                       |  |
| DEPTH<br>(feet) | USCS CLASS | SYMBOL | Enterprise Road, APNs 020-290-051 & 052<br>Hollister, California | INTERVAL<br>(feet) | SAMPLE<br>NUMBER | AMPLE<br>TYPE | DENSITY<br>(pcf) | MOISTURE<br>(%) | BLOWS<br>PER 6 IN. | POCKET PEN<br>(t.s.f) |  |
|                 | ñ          |        | SOIL DESCRIPTION   | N N                | S UN             | /S '          | DRY              | MO              |                    | Poc                   |  |
| -               | CL         | /      | SANDY LEAN CLAY; hard, brown, moist, fine sand                   |                    |                  |               |                  |                 |                    |                       |  |
| 1 -             |            |        |  |                    |                  |               |                  |                 |                    |                       |  |
| 2 -             |            |        | [LL=27, PI=11]   | 0.0-3.5            | Bag B            |               |                  |                 | 21<br>30           |                       |  |
| 3               |            |        |  | 1.5-3.0            | 8-1              |               | 121.5            | 13.8            | 47                 |                       |  |
| 4               |            |        | -dark yellow brown   |                    |                  |               |                  |                 | 18<br>25           |                       |  |
| 5               |            |        |  | 3.5-5.0            | 8-2              |               | 114.8            | 13.7            | 50/4"              |                       |  |
| 6               |            |        |  |                    |                  |               |                  |                 |                    |                       |  |
| 7               |            |        |  |                    |                  |               |                  |                 |                    |                       |  |
| 8               | SC         |        | CLAYEY SAND; very dense, gray brown, moist, fine to              |                    |                  |               |                  |                 |                    |                       |  |
| 9               | 50         |        | coarse sand, few fine gravel                                     |                    |                  |               |                  |                 | 33<br>37           |                       |  |
| 10              |            |        |  | 8.5-10.0           | 8-3              |               |                  |                 | 43                 |                       |  |
| 11              |            |        |  | 8.0-12.0           | Bag C            |               |                  |                 |                    |                       |  |
| -<br>12         |            |        |  |                    |                  |               |                  |                 |                    |                       |  |
| -<br>13         |            | X      |  |                    |                  |               |                  |                 |                    |                       |  |
| 14              |            |        |  |                    |                  |               |                  |                 | 26                 |                       |  |
| - 15            |            |        |  | 13.5-15.0          | 8-4              |               |                  |                 | 33<br>46           |                       |  |
| - 16            |            |        | Bottom of boring at 15'  |                    |                  |               |                  |                 |                    |                       |  |
| 17              |            |        | Groundwater not encountered                                      |                    |                  |               |                  |                 |                    |                       |  |
| 17              |            |        |  |                    |                  |               |                  |                 |                    |                       |  |
| -               |            |        |  |                    |                  |               |                  |                 |                    |                       |  |
| 19              |            |        |  |                    |                  |               |                  |                 |                    |                       |  |
| 20              |            |        |  |                    |                  |               |                  |                 |                    |                       |  |
| 21              |            |        |  |                    |                  |               |                  |                 |                    |                       |  |
| 22              |            |        |  |                    |                  |               |                  |                 |                    |                       |  |
| 23<br>-         |            |        |  |                    |                  |               |                  |                 |                    |                       |  |
| 24              |            |        |  |                    |                  |               |                  |                 |                    |                       |  |
| 25<br>-         |            |        |  |                    |                  |               |                  |                 |                    |                       |  |
| 26              |            |        |  |                    |                  |               |                  |                 |                    |                       |  |
| $\Box$          |            |        |  |                    |                  |               | L                |                 | <u> </u>           | ш                     |  |



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DATE: 11/1/18

LOGGED BY: D. Teimoorian DRILL RIG: Mobile B-53 Red AUGER TYPE: 8" Hollow Stem

|                 |            |        | Lico Property Development  |                    | S                | AMF           | PLE DA           |                 | <u> </u>           |                       |
|-----------------|------------|--------|--|--------------------|------------------|---------------|------------------|-----------------|--------------------|-----------------------|
| DEPTH<br>(feet) | USCS CLASS | SYMBOL | Enterprise Road, APNs 020-290-051 & 052<br>Hollister, California                   | INTERVAL<br>(feet) | SAMPLE<br>NUMBER | AMPLE<br>TYPE | DENSITY<br>(pcf) | MOISTURE<br>(%) | BLOWS<br>PER 6 IN. | POCKET PEN<br>(t.s.f) |
|                 | ň          |        | SOIL DESCRIPTION   | N                  | S ∪<br>N         | /S            | DRY              | MO              | 8 문                | POC                   |
| -               | SC         |        | CLAYEY SAND; very dense, dark brown, moist, fine to medium sand, trace fine gravel |                    |                  |               |                  |                 |                    |                       |
| 1<br>-<br>2     |            | X      | [LL=27, PI=11]   | 0.0-4.0            | Bag D            |               |                  |                 | 19                 |                       |
| - 3             |            |        |  | 1.5-3.0            | 9-1              |               | 102.9            | 5.1             | 26<br>50/6''       |                       |
| - 4             |            |        |  |                    |                  |               |                  |                 | 30                 |                       |
| - 5             |            |        | -dense, few fine to coarse gravel  | 3.5-5.0            | 9-2              |               | 111.9            | 14.1            | 26<br>23           |                       |
| -<br>6          |            |        |  |                    |                  |               |                  |                 |                    |                       |
| - 7             | CL         |        | SANDY LEAN CLAY; hard, dark yellow brown, moist,                                   |                    |                  |               |                  |                 |                    |                       |
| - 8             |            |        | mostly fine sand   |                    |                  |               |                  |                 |                    |                       |
| 9               |            |        |  |                    |                  |               |                  |                 | 13                 |                       |
| -<br>10         |            |        |  | 8.5-10.0           | 9-3              | •             |                  |                 | 26<br>31           |                       |
| -<br>11         |            |        |  |                    |                  |               |                  |                 |                    |                       |
| -<br>12         |            |        |  |                    |                  |               |                  |                 |                    |                       |
| -<br>13         |            |        |  |                    |                  |               |                  |                 |                    |                       |
| -<br>14         |            |        | - caliche cemented in shoe   | 13.5-14.5          | 9-4              |               |                  |                 | 26<br>50/5"        |                       |
| -<br>15         |            |        | Bottom of boring at 14.5'  | 13.3-14.3          | 9-4              |               |                  |                 | 50/5               |                       |
| -<br>16         |            |        | Groundwater not encountered  |                    |                  |               |                  |                 |                    |                       |
| 17              |            |        |  |                    |                  |               |                  |                 |                    |                       |
| -<br>18         |            |        |  |                    |                  |               |                  |                 |                    |                       |
| -<br>19         |            |        |  |                    |                  |               |                  |                 |                    |                       |
| 20              |            |        |  |                    |                  |               |                  |                 |                    |                       |
| -<br>21         |            |        |  |                    |                  |               |                  |                 |                    |                       |
| 22              |            |        |  |                    |                  |               |                  |                 |                    |                       |
| 23              |            |        |  |                    |                  |               |                  |                 |                    |                       |
| -<br>24         |            |        |  |                    |                  |               |                  |                 |                    |                       |
| -<br>25         |            |        |  |                    |                  |               |                  |                 |                    |                       |
| -<br>26         |            |        |  |                    |                  |               |                  |                 |                    |                       |
| -               |            |        |  |                    |                  |               |                  |                 |                    |                       |



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LOGGED BY: D. Teimoorian DRILL RIG: Mobile B-53 Red AUGER TYPE: 8" Hollow Stem

|                  |            | Ĭ      | THE. 6 Hollow Stelli  |                    | S                | AMF | PLE DA |                 | <u> </u>           | ., ., .o              |
|------------------|------------|--------|---|--------------------|------------------|-----|--------|-----------------|--------------------|-----------------------|
| DEPTH<br>(feet)  | USCS CLASS | SYMBOL | Lico Property Development<br>Enterprise Road, APNs 020-290-051 & 052<br>Hollister, California | INTERVAL<br>(feet) | SAMPLE<br>NUMBER |     |        | MOISTURE<br>(%) | BLOWS<br>PER 6 IN. | POCKET PEN<br>(t.s.f) |
|                  | Š          |        | SOIL DESCRIPTION  | Σ                  | S N              | S/  | DRY    | MO              | B H                | POC                   |
| -0-<br>-<br>1    | CL         |        | SANDY LEAN CLAY; very stiff, brown, moist, few fine to medium sand                            |                    |                  |     |        |                 |                    |                       |
| -<br>2           |            |        |   |                    |                  |     |        |                 | 10                 |                       |
| - 3              |            |        |   | 1.5-3.0            | 10-1             |     | 102.9  | 5.1             | 16<br>25           |                       |
| -<br>4<br>-      |            |        | -hard, dark brown, fine to coarse sand, few fine gravel, cobble fragment in shoe              | 3.5-4.5            | 10-2             |     | 102.9  | 5.1             | 23<br>50/6''       |                       |
| 5<br>-<br>6<br>- |            |        | - caliche cemented in shoe  |                    |                  |     |        |                 |                    |                       |
| 7<br>-<br>8<br>- |            |        | Bottom of boring at 7' due to auger and sampler refusal<br>Groundwater not encountered        |                    |                  |     |        |                 |                    |                       |
| 9<br>-<br>10     |            |        |   |                    |                  |     |        |                 |                    |                       |
| -<br>11<br>-     |            |        |   |                    |                  |     |        |                 |                    |                       |
| 12<br>-          |            |        |   |                    |                  |     |        |                 |                    |                       |
| 13<br>-          |            |        |   |                    |                  |     |        |                 |                    |                       |
| 14 -             |            |        |   |                    |                  |     |        |                 |                    |                       |
| 15<br>-<br>16    |            |        |   |                    |                  |     |        |                 |                    |                       |
| -<br>17          |            |        |   |                    |                  |     |        |                 |                    |                       |
| -<br>18          |            |        |   |                    |                  |     |        |                 |                    |                       |
| -<br>19<br>-     |            |        |   |                    |                  |     |        |                 |                    |                       |
| 20               |            |        |   |                    |                  |     |        |                 |                    |                       |
| 21<br>-          |            |        |   |                    |                  |     |        |                 |                    |                       |
| 22<br>-          |            |        |   |                    |                  |     |        |                 |                    |                       |
| 23<br>-<br>24    |            |        |   |                    |                  |     |        |                 |                    |                       |
| -<br>25          |            |        |   |                    |                  |     |        |                 |                    |                       |
| -<br>26          |            |        |   |                    |                  |     |        |                 |                    |                       |
| -                |            |        |   |                    |                  |     |        |                 |                    |                       |



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LOGGED BY: D. Teimoorian DRILL RIG: Mobile B-53 Red FILE NO.: 302615-001 AUGER TYPE: 8" Hollow Stem DATE: 11/1/18

|                 | 7.0        |        | TIPE: 8 Hollow Stern   | SAMPLE DATA        |                  |             |             |                 |                    |                       |  |
|-----------------|------------|--------|--|--------------------|------------------|-------------|-------------|-----------------|--------------------|-----------------------|--|
|                 | SS         |        | Lico Property Development  |                    | <u>S</u>         | AIVIF       |             |                 |                    | Z                     |  |
| DEPTH<br>(feet) | USCS CLASS | SYMBOL | Enterprise Road, APNs 020-290-051 & 052<br>Hollister, California                                     | INTERVAL<br>(feet) | SAMPLE<br>NUMBER | MPLE<br>YPE | DENSIT pcf) | MOISTURE<br>(%) | BLOWS<br>PER 6 IN. | POCKET PEN<br>(t.s.f) |  |
|                 | SN         |        | SOIL DESCRIPTION   | Z<br>Z             | SAI              | SA          | DRY (       | MOM             | 밀                  | POC <sub>(</sub>      |  |
| -               | SC         |        | CLAYEY SAND with GRAVEL; dense, dark yellow brown, moist, fine to coarse sand, fine to coarse gravel |                    |                  |             |             |                 |                    |                       |  |
| -               |            |        | ,  |                    |                  |             |             |                 | 13                 |                       |  |
| 2<br>-<br>3     |            |        |  | 1.5-3.0            | 11-1             |             |             |                 | 34<br>40           |                       |  |
| - 4             |            |        |  |                    |                  |             |             |                 | 30                 |                       |  |
| 5               |            |        | -very dense, fine gravel   | 3.5-4.5            | 11-2             |             |             |                 | 50/6''             |                       |  |
| - 6             |            |        |  |                    |                  |             |             |                 |                    |                       |  |
| 7               |            |        |  |                    |                  |             |             |                 |                    |                       |  |
| 8               |            |        |  |                    |                  |             |             |                 |                    |                       |  |
| 9               |            |        |  |                    |                  |             |             |                 | 16<br>19           |                       |  |
| 10              |            |        |  | 8.5-10.0           | 11-3             |             |             |                 | 31                 |                       |  |
| 11              |            |        |  |                    |                  |             |             |                 |                    |                       |  |
| 12              |            |        |  |                    |                  |             |             |                 |                    |                       |  |
| 13              |            |        |  |                    |                  |             |             |                 | 20                 |                       |  |
| 14              |            | Z      |  | 13.5-14.5          | 11-4             |             |             |                 | 30<br>50/3''       |                       |  |
| 15<br>-         |            |        | Bottom of boring at 14.5'<br>Groundwater not encountered   |                    |                  |             |             |                 |                    |                       |  |
| 16<br>-         |            |        |  |                    |                  |             |             |                 |                    |                       |  |
| 17 -            |            |        |  |                    |                  |             |             |                 |                    |                       |  |
| 18<br>-<br>19   |            |        |  |                    |                  |             |             |                 |                    |                       |  |
| -<br>20         |            |        |  |                    |                  |             |             |                 |                    |                       |  |
| -<br>21         |            |        |  |                    |                  |             |             |                 |                    |                       |  |
| 22              |            |        |  |                    |                  |             |             |                 |                    |                       |  |
| -<br>23         |            |        |  |                    |                  |             |             |                 |                    |                       |  |
| -<br>24         |            |        |  |                    |                  |             |             |                 |                    |                       |  |
| -<br>25         |            |        |  |                    |                  |             |             |                 |                    |                       |  |
| -<br>26         |            |        |  |                    |                  |             |             |                 |                    |                       |  |
|                 |            |        |  |                    |                  | <u></u>     |             |                 | <u> </u>           | ш                     |  |



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DRILL RIG: Mobile B-53 Red AUGER TYPE: 8" Hollow Stem

LOGGED BY: D. Teimoorian

|                 |            |        | Lica Property Dayslanment   |                    | S                | AMF           | PLE DA           |                 | <u> </u>           |                       |
|-----------------|------------|--------|---|--------------------|------------------|---------------|------------------|-----------------|--------------------|-----------------------|
| DEPTH<br>(feet) | USCS CLASS | SYMBOL | Lico Property Development<br>Enterprise Road, APNs 020-290-051 & 052<br>Hollister, California | INTERVAL<br>(feet) | SAMPLE<br>NUMBER | \MPLE<br>\YPE | DENSITY<br>(pcf) | MOISTURE<br>(%) | BLOWS<br>PER 6 IN. | POCKET PEN<br>(t.s.f) |
|                 | ñ          |        | SOIL DESCRIPTION  | N N                | S U              | S.            | DRY              | MO              | ᄪᇤ                 | POC)                  |
| -0              | CL         |        | SANDY LEAN CLAY; very stiff, brown, moist, fine sand  |                    |                  |               |                  |                 |                    |                       |
| 1 -             |            |        |   |                    |                  |               |                  |                 | 14                 |                       |
| 2 -             |            |        |   | 1.5-3.0            | 12-1             |               |                  |                 | 15<br>23           |                       |
| -<br>-          |            |        | -caliche cemented, hard   |                    |                  |               |                  |                 | 37                 |                       |
| -               |            |        | ednere cemented, nard   | 3.5-4.5            | 12-2             |               | 102.6            | 5.6             | 50/5"              |                       |
| 5 -             |            |        |   |                    |                  |               |                  |                 |                    |                       |
| 6 -             |            |        |   |                    |                  |               |                  |                 |                    |                       |
| 7 -             |            |        |   |                    |                  |               |                  |                 |                    |                       |
| 8 -             |            |        |   |                    |                  |               |                  |                 |                    |                       |
| 9 -             |            |        |   | 8.5-9.0            | 12-3             |               |                  | 7.1             | 50/5.5"            |                       |
| 10              |            |        |   |                    |                  |               |                  |                 |                    |                       |
| 11 -            |            |        |   |                    |                  |               |                  |                 |                    |                       |
| 12              |            |        |   |                    |                  |               |                  |                 |                    |                       |
| 13              |            |        |   |                    |                  |               |                  |                 |                    |                       |
| 14              |            |        |   | 13.5-14.5          | 12-4             |               |                  |                 | 32<br>50/5''       |                       |
| 15              |            |        | Bottom of boring at 14.5'<br>Groundwater not encountered                                      | •                  |                  |               |                  |                 |                    |                       |
| 16              |            |        | Groundwater not encountered   |                    |                  |               |                  |                 |                    |                       |
| 17              |            |        |   |                    |                  |               |                  |                 |                    |                       |
| 18              |            |        |   |                    |                  |               |                  |                 |                    |                       |
| 19              |            |        |   |                    |                  |               |                  |                 |                    |                       |
| 20              |            |        |   |                    |                  |               |                  |                 |                    |                       |
| 21              |            |        |   |                    |                  |               |                  |                 |                    |                       |
| 22              |            |        |   |                    |                  |               |                  |                 |                    |                       |
| -<br>23         |            |        |   |                    |                  |               |                  |                 |                    |                       |
| -<br>24         |            |        |   |                    |                  |               |                  |                 |                    |                       |
| -<br>25         |            |        |   |                    |                  |               |                  |                 |                    |                       |
| -<br>26         |            |        |   |                    |                  |               |                  |                 |                    |                       |
| -               |            |        |   |                    |                  |               |                  |                 |                    |                       |



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LOGGED BY: D. Teimoorian DRILL RIG: Mobile B-53 Red AUGER TYPE: 8" Hollow Stem

|                     |            |        | Lice Property Development   |                    | SAMPLE DATA      |               |                   |              |                    |                       |
|---------------------|------------|--------|---|--------------------|------------------|---------------|-------------------|--------------|--------------------|-----------------------|
| DEPTH<br>(feet)     | USCS CLASS | SYMBOL | Lico Property Development<br>Enterprise Road, APNs 020-290-051 & 052<br>Hollister, California | INTERVAL<br>(feet) | SAMPLE<br>NUMBER | \MPLE<br>FYPE | DRY DENSITY (pcf) | MOISTURE (%) | BLOWS<br>PER 6 IN. | POCKET PEN<br>(t.s.f) |
|                     | ñ          |        | SOIL DESCRIPTION  | Z O                | SA               | /s            | DRY               | MO           | 묘믮                 | POC                   |
| -0                  | CL         |        | SANDY LEAN CLAY; very stiff, brown, moist, fine to medium sand                                |                    |                  |               |                   |              |                    |                       |
| 1 -                 |            |        |   |                    |                  |               |                   |              | 13                 |                       |
| 2 -                 |            |        | [LL=27, PI=13]  | 1.5-3.0            | 13-1             |               |                   |              | 13<br>13           |                       |
| 3 -                 |            |        | , ,   | 1.5 5.0            |                  | _             |                   |              |                    |                       |
| 4 -                 |            |        | -dark yellow brown, mostly fine sand  |                    |                  |               |                   |              | 11<br>27           |                       |
| 5 -                 |            |        |   | 3.5-5.0            | 13-2             |               | 109.0             | 11.6         | 23                 |                       |
| 6 -                 |            |        | -hard   |                    |                  |               |                   |              |                    |                       |
| 7 -                 |            |        |   |                    |                  |               |                   |              |                    |                       |
| 8 -                 |            |        |   |                    |                  |               |                   |              |                    |                       |
| 9                   |            |        |   |                    |                  | _             |                   |              | 30<br>40           |                       |
| 10                  |            |        |   | 8.5-10.0           | 13-3             |               |                   |              | 50/5"              |                       |
| 11                  |            |        |   |                    |                  |               |                   |              |                    |                       |
| 12                  |            |        |   |                    |                  |               |                   |              |                    |                       |
| 13                  | SP-        | 1      | Poorly-graded SAND with CLAY; dense, gray brown,  |                    |                  |               |                   |              |                    |                       |
| 14                  | SC         |        | moist, fine to medium sand  |                    |                  |               |                   |              | 18<br>22           |                       |
| -<br>15             |            | 1      |   | 13.5-15.0          | 13-4             |               |                   |              | 24                 |                       |
| -<br>16             |            |        | Bottom of boring at 15'<br>Groundwater not encountered  |                    |                  |               |                   |              |                    |                       |
| -<br>17             |            |        |   |                    |                  |               |                   |              |                    |                       |
| -<br>18             |            |        |   |                    |                  |               |                   |              |                    |                       |
| -<br>19             |            |        |   |                    |                  |               |                   |              |                    |                       |
| -<br>20             |            |        |   |                    |                  |               |                   |              |                    |                       |
| -<br>21             |            |        |   |                    |                  |               |                   |              |                    |                       |
| - 22                |            |        |   |                    |                  |               |                   |              |                    |                       |
| -                   |            |        |   |                    |                  |               |                   |              |                    |                       |
| 23                  |            |        |   |                    |                  |               |                   |              |                    |                       |
| 2 <del>4</del><br>- |            |        |   |                    |                  |               |                   |              |                    |                       |
| 25<br>-             |            |        |   |                    |                  |               |                   |              |                    |                       |
| 26<br>-             |            |        |   |                    |                  |               |                   |              |                    |                       |



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LOGGED BY: D. Teimoorian DRILL RIG: Mobile B-53 Red AUGER TYPE: 8" Hollow Stem

|                 |            |        | CTT E. O TIONOW CLOTT  |                    |                  |               |                      |                 |                    |                       |
|-----------------|------------|--------|--|--------------------|------------------|---------------|----------------------|-----------------|--------------------|-----------------------|
|                 | ဟ          |        | Lico Property Development  |                    | S                | AMP           | LE DA                | AIA             |                    |                       |
| DEPTH<br>(feet) | USCS CLASS | SYMBOL | Enterprise Road, APNs 020-290-051 & 052<br>Hollister, California                             | INTERVAL<br>(feet) | SAMPLE<br>NUMBER | \MPLE<br>FYPE | DRY DENSITY<br>(pcf) | MOISTURE<br>(%) | BLOWS<br>PER 6 IN. | POCKET PEN<br>(t.s.f) |
|                 | ñ          |        | SOIL DESCRIPTION   | LNI                | SA<br>NU         | /S            | DRY                  | MO              | B H                | POC                   |
| -               | CL         |        | SANDY LEAN CLAY with GRAVEL; very stiff, dark brown, moist, fine to coarse sand, fine gravel |                    |                  |               |                      |                 |                    |                       |
| 1 -             |            |        | most, fine to course saind, fine graver  |                    |                  |               |                      |                 |                    |                       |
| 2               |            |        |  |                    |                  |               |                      |                 | 8<br>17            |                       |
| 3               |            |        |  | 1.5-3.0            | 14-1             |               |                      |                 | 22                 |                       |
| -               |            |        |  |                    |                  |               |                      |                 | 16                 |                       |
| -               |            |        |  |                    |                  |               |                      |                 | 17                 |                       |
| 5               |            |        |  | 3.5-5.0            | 14-2             |               |                      |                 | 14                 |                       |
| 6               |            |        |  |                    |                  |               |                      |                 |                    |                       |
| - 7             |            |        |  |                    |                  |               |                      |                 |                    |                       |
| -               |            |        |  |                    |                  |               |                      |                 |                    |                       |
| 8 -             | SC         |        | CLAYEY SAND; medium dense, dark yellow brown,  |                    |                  |               |                      |                 |                    |                       |
| 9               |            |        | moist, mostly fine sand  |                    |                  |               |                      |                 | 4<br>5             |                       |
| 10              |            | 8      |  | 8.5-10.0           | 14-3             |               |                      |                 | 6                  |                       |
| -               |            |        |  |                    |                  |               |                      |                 |                    |                       |
| 11 -            | SP-<br>SC  |        | Poorly-graded SAND with CLAY; dense, dark yellow brown to gray brown, moist, fine sand       |                    |                  |               |                      |                 |                    |                       |
| 12              | SC         |        | brown to gray brown, moist, fine sand  |                    |                  |               |                      |                 |                    |                       |
| 13              |            |        |  |                    |                  |               |                      |                 |                    |                       |
| 14              |            |        |  |                    |                  |               |                      |                 | 14                 |                       |
| -               |            |        |  | 13.5-15.0          | 14-4             |               |                      |                 | 18<br>26           |                       |
| 15              |            | -1     | Bottom of boring at 15'  |                    |                  |               |                      |                 |                    |                       |
| 16              |            |        | Groundwater not encountered  |                    |                  |               |                      |                 |                    |                       |
| 17              |            |        |  |                    |                  |               |                      |                 |                    |                       |
| -<br>18         |            |        |  |                    |                  |               |                      |                 |                    |                       |
| -               |            |        |  |                    |                  |               |                      |                 |                    |                       |
| 19              |            |        |  |                    |                  |               |                      |                 |                    |                       |
| 20              |            |        |  |                    |                  |               |                      |                 |                    |                       |
| 21              |            |        |  |                    |                  |               |                      |                 |                    |                       |
| -               |            |        |  |                    |                  |               |                      |                 |                    |                       |
| 22              |            |        |  |                    |                  |               |                      |                 |                    |                       |
| 23              |            |        |  |                    |                  |               |                      |                 |                    |                       |
| -<br>24         |            |        |  |                    |                  |               |                      |                 |                    |                       |
| - 25            |            |        |  |                    |                  |               |                      |                 |                    |                       |
| 25              |            |        |  |                    |                  |               |                      |                 |                    |                       |
| 26              |            |        |  |                    |                  |               |                      |                 |                    |                       |



File No. SH-10127-SC

## **BULK DENSITY TEST RESULTS**

ASTM D 2937-04 (modified for ring liners)

October, 2008

| BORING<br>NO. | DEPTH<br>feet | MOISTURE CONTENT, % | WET<br>DENSITY, pcf | DRY<br>DENSITY, pcf |
|---------------|---------------|---------------------|---------------------|---------------------|
| B-1           | 2.0 - 2.5     | 13.5                | 134.1               | 118.2               |
| B-1           | 4.0 - 4.5     | 10.7                | 131.0               | 118.3               |
| B-2           | 2.0 - 2.5     | 14.1                | 128.2               | 112.4               |
| B-2           | 4.5 - 5.0     | 13.4                | 139.3               | 122.8               |
| B-3           | 2.0 - 2.5     | 8.9                 | 120.1               | 110.3               |
| B-3           | 4.0 - 4.5     | 11.7                | 148.2               | 132.7               |
| B-4           | 1.5 - 2.0     | 11.3                | 138.0               | 124.0               |
| B-4           | 4.5 - 5.0     | 3.7                 | 118.1               | 113.8               |
| B-5           | 2.5 - 3.0     | 11.2                | 143.7               | 129.2               |
| B-5           | 4.0 - 4.5     | 9.3                 | 133.7               | 122.3               |
| B-6           | 1.5 - 2.0     | 5.3                 | 118.8               | 112.8               |
| B-6           | 4.0 - 4.5     | 12.0                | 130.3               | 116.4               |



File No. SH-10127-SC

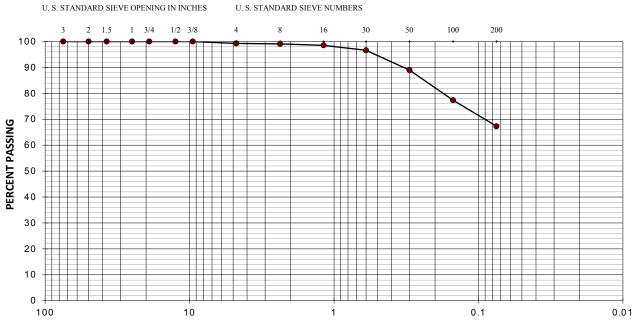
## **PARTICLE SIZE ANALYSIS**

ASTM D 422-07; D 1140-06

Boring #1 @ 2.0 - 2.5' Sandy Lean Clay to Fat Clay (CL/CH)

October, 2008

| Sieve size     | % Retained | % Passing |
|----------------|------------|-----------|
| 3" (75-mm)     | 0          | 100       |
| 2" (50-mm)     | 0          | 100       |
| 1.5" (37.5-mm) | 0          | 100       |
| 1" (25-mm)     | 0          | 100       |
| 3/4" (19-mm)   | 0          | 100       |
| 1/2" (12.5-mm) | 0          | 100       |
| 3/8" (9.5-mm)  | 0          | 100       |
| #4 (4.75-mm)   | 1          | 99        |
| #8 (2.36-mm)   | 1          | 99        |
| #16 (1.18-mm)  | 1          | 99        |
| #30 (600-μm)   | 3          | 97        |
| #50 (300-μm)   | 11         | 89        |
| #100 (150-μm)  | 23         | 77        |
| #200 (75-μm)   | 33         | 67        |
| ` ' '          |            |           |



**GRAIN SIZE, mm** 



File No. SH-10715-SB

## **PARTICLE SIZE ANALYSIS**

ASTM D 422-07; D 1140-06

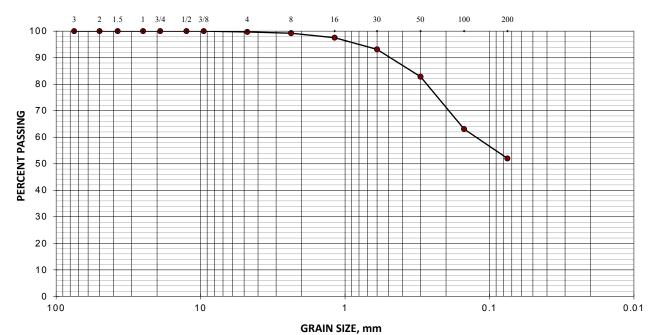
Boring #2 @ 2.0 - 2.5' Sandy Lean to Fat Clay (CL/CH)

October, 2008

| Sieve size     | % Retained | % Passing |
|----------------|------------|-----------|
| 3" (75-mm)     | 0          | 100       |
| 2" (50-mm)     | 0          | 100       |
| 1.5" (37.5-mm) | 0          | 100       |
| 1" (25-mm)     | 0          | 100       |
| 3/4" (19-mm)   | 0          | 100       |
| 1/2" (12.5-mm) | 0          | 100       |
| 3/8" (9.5-mm)  | 0          | 100       |
| #4 (4.75-mm)   | 0          | 100       |
| #8 (2.36-mm)   | 1          | 99        |
| #16 (1.18-mm)  | 2          | 98        |
| #30 (600-μm)   | 7          | 93        |
| #50 (300-μm)   | 17         | 83        |
| #100 (150-μm)  | 37         | 63        |
| #200 (75-μm)   | 48         | 52        |
|                |            |           |

U. S. STANDARD SIEVE OPENING IN INCHES

U. S. STANDARD SIEVE NUMBERS





File No. SH-10715-SB

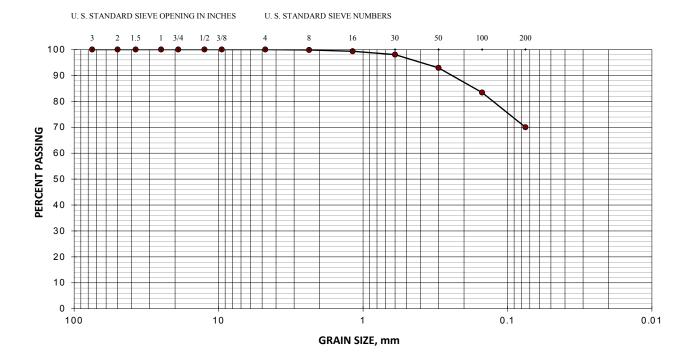
## **PARTICLE SIZE ANALYSIS**

ASTM D 422-07; D 1140-06

Boring #3 @ 2.0 - 2.5' Sandy Lean to Fat Clay (CL/CH)

October, 2008

| Sieve size     | % Retained | % Passing |
|----------------|------------|-----------|
| 3" (75-mm)     | 0          | 100       |
| 2" (50-mm)     | 0          | 100       |
| 1.5" (37.5-mm) | 0          | 100       |
| 1" (25-mm)     | 0          | 100       |
| 3/4" (19-mm)   | 0          | 100       |
| 1/2" (12.5-mm) | 0          | 100       |
| 3/8" (9.5-mm)  | 0          | 100       |
| #4 (4.75-mm)   | 0          | 100       |
| #8 (2.36-mm)   | 0          | 100       |
| #16 (1.18-mm)  | 1          | 99        |
| #30 (600-μm)   | 2          | 98        |
| #50 (300-μm)   | 7          | 93        |
| #100 (150-μm)  | 17         | 83        |
| #200 (75-μm)   | 30         | 70        |





File No. SH-10715-SB

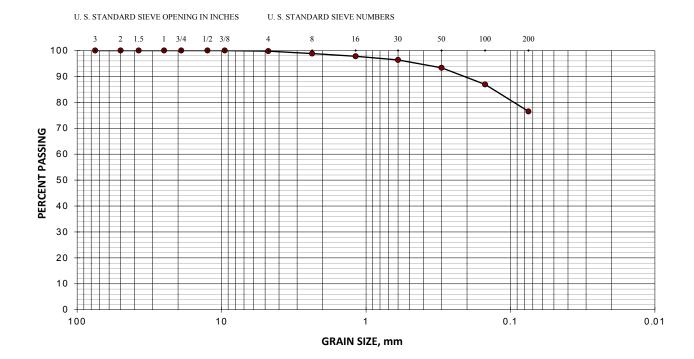
## **PARTICLE SIZE ANALYSIS**

ASTM D 422-07; D 1140-06

Boring #4 @ 1.5 - 2.0' Sandy Lean Clay (CL)

October, 2008

| Sieve size     | % Retained | % Passing |
|----------------|------------|-----------|
| 3" (75-mm)     | 0          | 100       |
| 2" (50-mm)     | 0          | 100       |
| 1.5" (37.5-mm) | 0          | 100       |
| 1" (25-mm)     | 0          | 100       |
| 3/4" (19-mm)   | 0          | 100       |
| 1/2" (12.5-mm) | 0          | 100       |
| 3/8" (9.5-mm)  | 0          | 100       |
| #4 (4.75-mm)   | 0          | 100       |
| #8 (2.36-mm)   | 1          | 99        |
| #16 (1.18-mm)  | 2          | 98        |
| #30 (600-μm)   | 4          | 96        |
| #50 (300-μm)   | 7          | 93        |
| #100 (150-μm)  | 13         | 87        |
| #200 (75-μm)   | 23         | 77        |



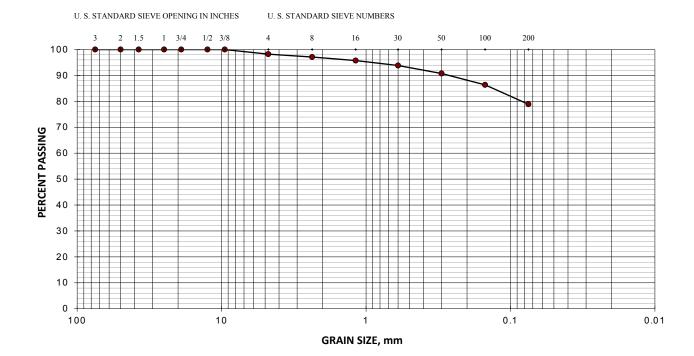
## **PARTICLE SIZE ANALYSIS**

ASTM D 422-07; D 1140-06

Boring #6 @ 0.0 - 3.0' Silty Clay with sand (CL-ML)

|  | Octo | ber, | 2008 |
|--|------|------|------|
|--|------|------|------|

| Sieve size     | % Retained | % Passing |
|----------------|------------|-----------|
| 3" (75-mm)     | 0          | 100       |
| 2" (50-mm)     | 0          | 100       |
| 1.5" (37.5-mm) | 0          | 100       |
| 1" (25-mm)     | 0          | 100       |
| 3/4" (19-mm)   | 0          | 100       |
| 1/2" (12.5-mm) | 0          | 100       |
| 3/8" (9.5-mm)  | 0          | 100       |
| #4 (4.75-mm)   | 2          | 98        |
| #8 (2.36-mm)   | 3          | 97        |
| #16 (1.18-mm)  | 4          | 96        |
| #30 (600-μm)   | 6          | 94        |
| #50 (300-μm)   | 9          | 91        |
| #100 (150-μm)  | 14         | 86        |
| #200 (75-μm)   | 21         | 79        |
|                |            |           |





File No. SH-10127-SC

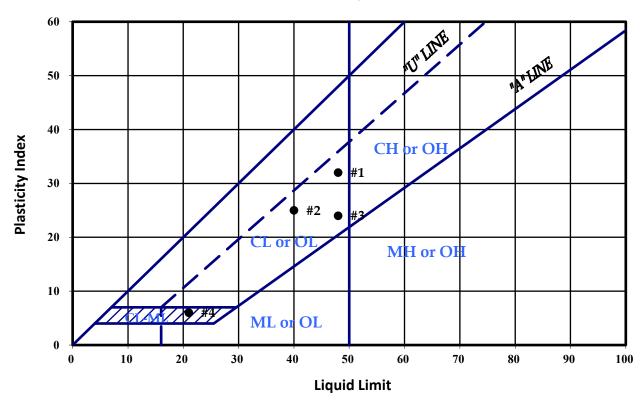
#### **PLASTICITY INDEX**

ASTM D 4318-00

October, 2008

| Test No.:         | 1          | 2          | 3          | 4          | 5 |
|-------------------|------------|------------|------------|------------|---|
| Boring No.:       | 3          | 4          | 5          | 6          |   |
| Sample Depth:     | 2.0 - 2.5' | 1.5 - 2.0' | 0.0 - 3.0' | 0.0 - 3.0' |   |
| Liquid Limit:     | 48         | 40         | 48         | 21         |   |
| Plastic Limit:    | 16         | 16         | 18         | 15         |   |
| Plasticity Index: | 32         | 24         | 30         | 6          | - |

# **Plasticity Chart**





File No.SH-10127-SC

#### RESISTANCE 'R' VALUE AND EXPANSION PRESSURE

**ASTM D 2844-07** 

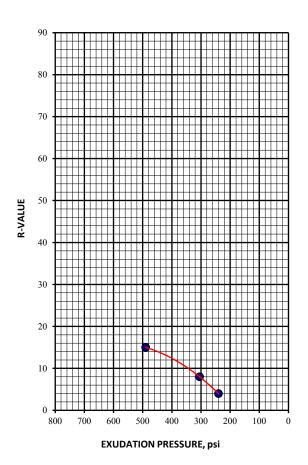
November, 2008

Boring #1 @ 1.0 - 5.0' Yellow brown Sandy Lean to Fat Clay (CL/CH) Specified Traffic Index: 5.0

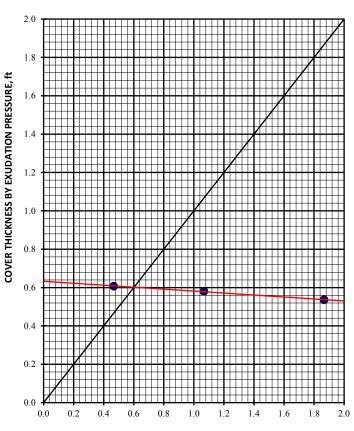
Dry Density @ 300 psi Exudation Pressure: 102.5-pcf %Moisture @ 300 psi Exudation Pressure: 21.9%

R-Value - Exudation Pressure: 8 R-Value - Expansion Pressure: 4 R-Value @ Equilibrium: 4

#### **EXUDATION PRESSURE CHART**



#### **EXPANSION PRESSURE CHART**



**COVER THICKNESS BY EXPANSION PRESSURE, ft** 



File No. SH-10715-SC

#### RESISTANCE 'R' VALUE AND EXPANSION PRESSURE

**ASTM D 2844-07** 

November, 2008

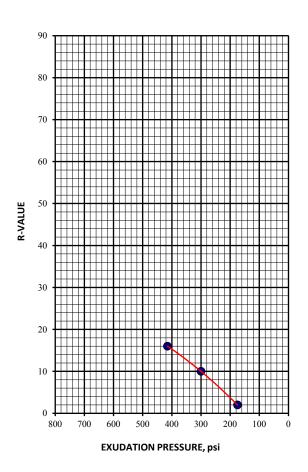
Boring #5 @ 0.0 - 3.0' Yellow brown Clayey Sand (SC) Specified Traffic Index: 5.0

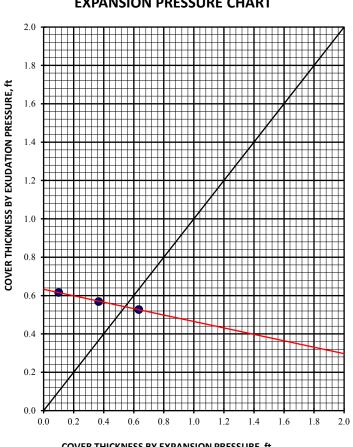
Dry Density @ 300 psi Exudation Pressure: 101.1-pcf %Moisture @ 300 psi Exudation Pressure: 16.8%

R-Value - Exudation Pressure: 10 R-Value - Expansion Pressure: 14 R-Value @ Equilibrium: 10

#### **EXUDATION PRESSURE CHART**

#### **EXPANSION PRESSURE CHART**





**COVER THICKNESS BY EXPANSION PRESSURE, ft** 



File No. 302615-001

## **BULK DENSITY TEST RESULTS**

ASTM D 2937-17 (modified for ring liners)

November 13, 2018

| BORING<br>NO. | DEPTH<br>feet | MOISTURE CONTENT, % | WET<br>DENSITY, pcf | DRY<br>DENSITY, pcf |
|---------------|---------------|---------------------|---------------------|---------------------|
|               |               |                     | <u> </u>            | DENOTT, per         |
| В7            | 2.5 - 3.0     | 7.9                 |                     |                     |
| B7            | 4.5 - 5.0     | 19.5                | 120.3               | 100.7               |
|               |               |                     |                     |                     |
| B8            | 2.5 - 3.0     | 13.8                | 138.2               | 121.5               |
| В8            | 4.5 - 5.0     | 13.7                | 130.5               | 114.8               |
|               |               |                     |                     |                     |
| В9            | 2.5 - 3.0     | 5.1                 | 108.1               | 102.9               |
| В9            | 4.5 - 5.0     | 14.1                | 127.7               | 111.9               |
|               |               |                     |                     |                     |
| B12           | 4.0 - 4.5     | 5.6                 | 108.4               | 102.6               |
| B12           | 8.5 - 9.0     | 7.1                 |                     |                     |
|               |               |                     |                     |                     |
| B13           | 4.5 - 5.0     | 11.6                | 121.6               | 109.0               |
|               |               |                     |                     |                     |
| B14           | 2.5 - 3.0     | 9.1                 | 123.0               | 112.7               |
|               |               |                     |                     |                     |



File No. 302615-001

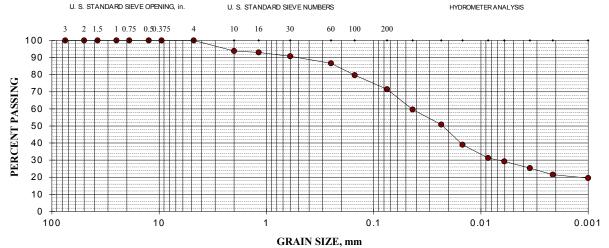
#### **PARTICLE SIZE ANALYSIS**

**ASTM D 7928-16** 

Boring #8 @ 0.0 - 3.5' **Sandy Lean Clay (CL)**LL = 27; PL = 16; PI = 11

November 13, 2018 Specific Gravity = 2.65 (assumed) Gravel = 0%; Sand = 29%; Silt = 46%; Clay = 25%

| Sieve size          | % Retained | % Passing |
|---------------------|------------|-----------|
| 3" (75.0-mm)        | 0          | 100       |
| 2" (50.0-mm)        | 0          | 100       |
| 1-1/2" (37.5-mm)    | 0          | 100       |
| 1" (25.0-mm)        | 0          | 100       |
| 3/4" (19.0-mm)      | 0          | 100       |
| 1/2" (12.5-mm)      | 0          | 100       |
| 3/8" (9.5-mm)       | 0          | 100       |
| #4 (4.75-mm)        | 0          | 100       |
| #10 (2.00-mm)       | 6          | 94        |
| #16 (1.18-mm)       | 7          | 93        |
| #30 (600-μm)        | 9          | 91        |
| #60 (250-μm)        | 13         | 87        |
| #100 (150-μm)       | 20         | 80        |
| #200 (75-μm)        | 29         | 71        |
| Hydrometer Analysis |            |           |
| 43-μm               |            | 60        |
| 23-μm               |            | 51        |
| 15-μm               |            | 39        |
| 9-μm                |            | 31        |
| 6-μm                |            | 29        |
| 3.5-µm              |            | 25        |
| 2.1-μm              |            | 21        |
| Colloids            |            | 20        |





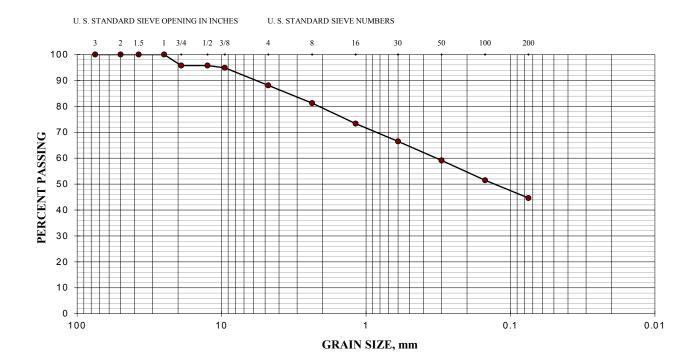
File No. 302615-001

## **PARTICLE SIZE ANALYSIS**

ASTM D 422-63/07; D 1140-17

Boring #9 @ 0.0 - 4.0' Clayey Sand (SC) November 13, 2018

| Sieve size     | % Retained | % Passing |
|----------------|------------|-----------|
| 3" (75-mm)     | 0          | 100       |
| 2" (50-mm)     | 0          | 100       |
| 1.5" (37.5-mm) | 0          | 100       |
| 1" (25-mm)     | 0          | 100       |
| 3/4" (19-mm)   | 4          | 96        |
| 1/2" (12.5-mm) | 4          | 96        |
| 3/8" (9.5-mm)  | 5          | 95        |
| #4 (4.75-mm)   | 12         | 88        |
| #8 (2.36-mm)   | 19         | 81        |
| #16 (1.18-mm)  | 27         | 73        |
| #30 (600-μm)   | 34         | 66        |
| #50 (300-μm)   | 41         | 59        |
| #100 (150-μm)  | 49         | 51        |
| #200 (75-μm)   | 55         | 45        |
|                |            |           |





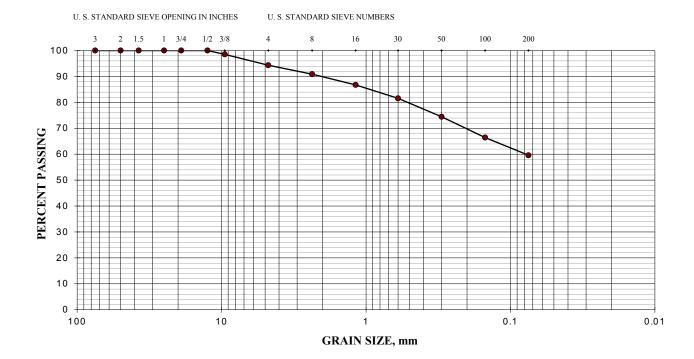
File No. 302615-001

## **PARTICLE SIZE ANALYSIS**

ASTM D 422-63/07; D 1140-17

Boring #12 @ 2.5 - 3.0' Sandy Lean Clay (CL) November 13, 2018

| Sieve size     | % Retained | % Passing |
|----------------|------------|-----------|
| 3" (75-mm)     | 0          | 100       |
| 2" (50-mm)     | 0          | 100       |
| 1.5" (37.5-mm) | 0          | 100       |
| 1" (25-mm)     | 0          | 100       |
| 3/4" (19-mm)   | 0          | 100       |
| 1/2" (12.5-mm) | 0          | 100       |
| 3/8" (9.5-mm)  | 1          | 99        |
| #4 (4.75-mm)   | 6          | 94        |
| #8 (2.36-mm)   | 9          | 91        |
| #16 (1.18-mm)  | 13         | 87        |
| #30 (600-μm)   | 18         | 82        |
| #50 (300-μm)   | 26         | 74        |
| #100 (150-μm)  | 34         | 66        |
| #200 (75-μm)   | 40         | 60        |
|                |            |           |





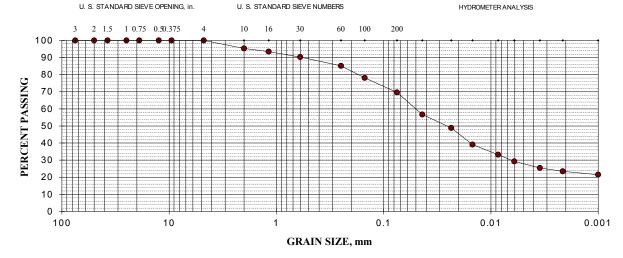
File No. 302615-001

#### **PARTICLE SIZE ANALYSIS**

**ASTM D 7928-16** 

Boring #13 @ 2.5 - 3.0' **Sandy Lean Clay (CL)** LL = 27; PL = 14; PI = 13 November 13, 2018 Specific Gravity = 2.65 (assumed) Gravel = 0%; Sand = 30%; Silt = 45%; Clay = 25%

| Sieve size          | % Retained | % Passing |
|---------------------|------------|-----------|
| 3" (75.0-mm)        | 0          | 100       |
| 2" (50.0-mm)        | 0          | 100       |
| 1-1/2" (37.5-mm)    | 0          | 100       |
| 1" (25.0-mm)        | 0          | 100       |
| 3/4" (19.0-mm)      | 0          | 100       |
| 1/2" (12.5-mm)      | 0          | 100       |
| 3/8" (9.5-mm)       | 0          | 100       |
| #4 (4.75-mm)        | 0          | 100       |
| #10 (2.00-mm)       | 5          | 95        |
| #16 (1.18-mm)       | 6          | 94        |
| #30 (600-μm)        | 10         | 90        |
| #60 (250-μm)        | 15         | 85        |
| #100 (150-μm)       | 22         | 78        |
| #200 (75-μm)        | 30         | 70        |
| Hydrometer Analysis |            |           |
| 44-μm               |            | 57        |
| 23-μm               |            | 49        |
| 15-μm               |            | 39        |
| 9-μm                |            | 33        |
| 6-μm                |            | 29        |
| 3.5-μm              |            | 25        |
| 2.1-μm              |            | 23        |
| Colloids            |            | 22        |
|                     |            |           |





Lico Property Development Hollister, California File No. 302615-001

**PLASTICITY INDEX** 

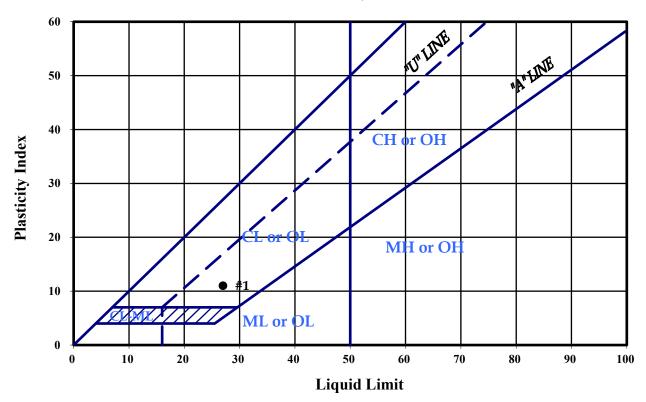
ASTM D 4318-17

Sandy Lean Clay (CL)

November 13, 2018

| Test No.:         | 1          | 2 | 3 | 4 | 5 |
|-------------------|------------|---|---|---|---|
| Boring No.:       | 8          |   |   |   |   |
| Sample Depth:     | 0.0 - 3.5' |   |   |   |   |
| Liquid Limit:     | 27         |   |   |   |   |
| Plastic Limit:    | 16         |   |   |   |   |
| Plasticity Index: | 11         |   |   |   |   |

# **Plasticity Chart**





Lico Property Development Hollister, California

File No. 302615-001

**PLASTICITY INDEX** 

**ASTM D 4318-17** November 13, 2018

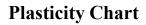
Sandy Lean Lean Clay (CL)

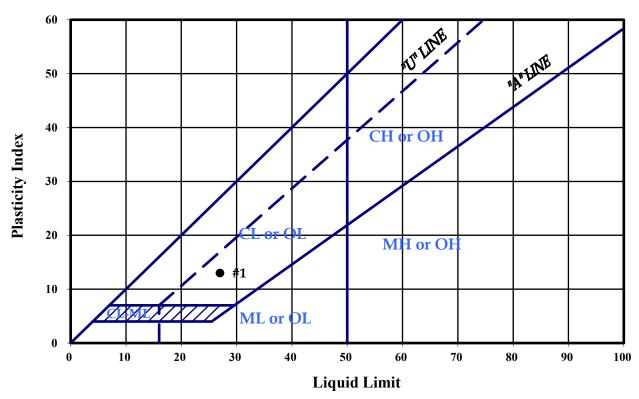
Test No.:

1

| 2 | 3 | 4 | 5 |
|---|---|---|---|
|   |   |   |   |
|   |   |   |   |
|   |   |   |   |

#### **Boring No.:** 13 Sample Depth: 2.5 - 3.0' **Liquid Limit:** 27 **Plastic Limit:** 14 **Plasticity Index:** 13





# Appendix G

Phase I Environmental Assessment

# PHASE I ENVIRONMENTAL SITE ASSESSMENT VISTA DEL CALABRIA ENTERPRISE ROAD (APNS 020-290-051 & -052) HOLLISTER, CALIFORNIA

January 16, 2020

Prepared for:

TTI Developers 601 McCray Street, Suite 205 Hollister, CA 95023

Prepared by:

Earth Systems Pacific 500 Park Center Drive, Suite 1 Hollister, CA 95023

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January 16, 2020 File No.: 302615-002

Mr. Ty Intravia TTI Developers 601 McCray Street, Suite 205 Hollister, CA 95023

PROJECT: VISTA DEL CALABRIA - ESA

ENTERPRISE ROAD (APNs 020-290-051 & -052)

HOLLISTER, CALIFORNIA

SUBJECT: Report of Phase I Environmental Site Assessment

REF.: Change order for a Phase I Environmental Site Assessment, Lico Property

Development, Enterprise Road (APNs 020-290-051 & -052), Hollister, California, Doc. No. 1912-007.PRP.CO1/ev., dated December 11, 2019.

#### Dear Mr. Intravia:

As authorized by you, Earth Systems Pacific (ESP) has completed this Phase I Environmental Site Assessment (ESA) at the above-referenced site. It was prepared to stand as a whole, and no part should be excerpted or used in exclusion of any other part. This project was conducted in accordance with our proposal dated December 11, 2019. If you have any questions regarding this report or the information contained herein, please contact the undersigned at your convenience.

I declare that I meet the definition of an Environmental Professional as defined in 40CFR 312.10. I have the specific qualifications based on education, training and experience to assess a property of the nature, history and setting of the subject site. I have endeavored to perform this project in conformance with the standards and practices set forth in ASTM Standard E1527-13.

Sincerely,

Earth Systems Pacific

David Teimoorian Staff Geologist

Doc. No.: 2001-014.RPT/ev

Senior Geologist

**Brett Faust** 

No. 2386 CERTIFIED ENGINEERING

**GEOLOGIST** 



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#### 1.0 INTRODUCTION

#### **Project Information**

This report presents the findings of a Phase I Environmental Site Assessment (ESA) conducted by Earth Systems Pacific (ESP) for two parcels located approximately 1,000 feet east of the intersection of Southside Road and Enterprise Road in Hollister, California. The site encompasses a total of about 50.4-acres and identified as San Benito County Assessor Parcel Numbers (APN) 020-290-051 & -052. The subject site is undeveloped and accessed via Enterprise Road (see Vicinity Map and Overall Site Map in Appendix A). This project was conducted for Mr. Ty Intravia in accordance with our proposal dated December 11, 2019. The work was performed in connection with residential development of the site.

#### **Purpose and Scope of Work**

The purpose of an ESA is to evaluate the potential for soil or groundwater contamination at a site due to the possible past use, storage, or handling of hazardous materials or petroleum products on or near the site, based on a visit to the site and a review of readily obtainable information concerning site activities and conditions. The scope of work is based on United States Environmental Protection Agency Final All Appropriate Inquiry Rule (2006) [US EPA AAI] and ASTM Standard E-1527-13, Standard Practice for Environmental Site Assessments, and consisted of the tasks listed below. A search for environmental liens on the site was not performed.

<u>Site Reconnaissance</u>: This involved: a visual reconnaissance of the site, noting physical evidence of potential contamination or possible sources of contamination; and observation of adjacent properties to identify readily observable visual evidence of possible impacts to the subject site. Site conditions are shown on a Overall and Detail Site Maps in Appendix A. Significant on-site features were photographed to document current conditions. Selected site photographs are presented in Appendix B.

<u>Records Review</u>: Records regarding the regulatory status and history of the site were evaluated regarding the possible presence of Recognized Environmental Conditions (RECs). Regulatory agency records were reviewed by obtaining a report listing known sites that generate, store, use, and/or have released hazardous materials from a firm that specializes in maintaining a database of this type of information. A copy of the agency database search report is presented in Appendix E and is discussed in Section 5.0. The search radii for the agency database search were in general accordance with the US EPA AAI and ASTM E1527-13, as measured from the site perimeter.

Other sources of information are listed in the references section of this report and may include the following categories of information (note that each category is utilized at the discretion of EP until, in the EP's opinion, sufficient data has been obtained):

- Aerial photographs
- Topographic maps
- Oil and gas production maps and records.
- Fire insurance maps
- Land title information
- Local street directories
- Zoning/land use records
- Interviews with current and/or former owners, occupants, and operators
- Engineering and institutional controls, such as deed restrictions and restrictive zoning to a radius of ½ mile, if contained in publicly available lists/registries
- Tribal records of subject property and adjoining properties (if tribal land)
- Local government records such as building department files

<u>Interviews:</u> Persons familiar with the site were interviewed (if possible) regarding the potential presence of RECs on the site or in a position to affect the site, including the site owner/operator/occupant, former site owners/operators/occupants (if reasonably accessible), neighboring property occupants (if the site is abandoned), and selected government personnel likely to have information regarding environmental conditions at or near the site. Information from persons who were contacted is presented in Section 6.0.

Report Preparation: This report was prepared to present our findings, conclusions, and recommendations.

#### **Definitions**

ASTM E1527-13 provides definitions of various terms and acronyms used in the ESA process. ESP endeavors to use these terms and acronyms within the meaning provided by the ASTM standard. The majority of these terms are either obvious in their meaning or are seldom used in this report, but a few are significant enough to warrant defining here, as follows:



<u>Site</u>: The term "site" is used in place of the term "property," and is the physical location that is the subject of the assessment. The site can include more than one parcel of land, or a portion of a parcel of land, depending on the needs of the client. ESAs focus primarily on activities that occur within the boundaries of the site, or that could potentially affect conditions and activities within the boundaries of the site. RECs on off-site properties that are not likely to affect the site are not considered to be RECs for the subject site.

<u>Recognized Environmental Condition</u> (REC): the presence or likely presence of any hazardous substances or petroleum products in, on, or at a property: due to a release to the environment; under conditions indicative of a release to the environment; or under conditions that pose a material threat of a future release to the environment. The term does <u>not</u> include *de minimis* conditions.

<u>Controlled Recognized Environmental Condition (CREC)</u>: An REC resulting from a past release of hazardous substances or petroleum products that has been addressed to the satisfaction of the applicable regulatory authority, with hazardous substances or petroleum projects allowed to remain in place subject to the implementation of required controls.

<u>Historic Recognized Environmental Condition</u> (HREC): A past release of any hazardous substances or petroleum products that has occurred in connection with the property and has been addressed to the satisfaction of the regulatory authority, or meeting unrestricted land use criteria, without subjecting the property to any required controls (such as a deed restriction). HRECs are no longer RECs for a site.

<u>De Minimis Condition</u>: A condition that does not present a significant threat to human health or the environment, and that generally would not be the subject of an enforcement action if brought to the attention of appropriate governmental agencies.

<u>Environmental Professional</u> (EP): An EP is defined as "a person who possesses sufficient specific education, training, and experience necessary to exercise professional judgment to develop opinions and conclusions regarding conditions indicative of releases or threatened releases (of hazardous substances) on, at, in, or to a property, sufficient to meet the objectives and performance factors (of the rule)." Specific minimum credentials are required to be identified as an EP.

<u>User</u>: The "user" of the report is defined as the party for whom the assessment is being conducted (i.e., the Client).

#### Qualifications

Work on this project was performed under the direct supervision of an EP, in accordance with ASTM E1527-13 requirements. Brett Faust (PG, CEG) was the lead EP and project manager. David Teimoorian (Staff Geologist), conducted the site reconnaissance, historical research, agency database review, and report preparation. Qualifications statements are presented in Appendix G.

#### **Exclusions and Data Gaps**

The scope of work for this ESA did not includez testing soil, air, groundwater, or building materials for the presence of hazardous constituents.

ASTM E1527-13 requires that gaps in the data used to evaluate the site be identified. Data gaps encountered in this project, and their significance to the project, are summarized below.

- Chain-of-title information was not provided, and therefore, not reviewed.
- No Sanborn maps are available for the site. Because of the availability of other data sources, the absence of the maps is not considered to be a significant data gap.
- A search for environmental liens on the site was not performed

Because of the availability of other data sources, the absence of these items is not considered to be significant data gaps and in our opinion, further assessment regarding these data gaps is not warranted.

#### **Limitation and Reliance**

This ESA has been prepared for the exclusive use of TTI Developers for the subject site. Any other use of, or reliance on the information and opinions contained in this report without the express written authorization of ESP is at the sole risk of the user.

The conclusions and recommendations rendered in this report are based on readily available information obtained to date within the scope of the work authorized by the client, and apply only to site conditions as of the date of the site visit. The scope of work for this project was developed to address the needs of the client related residential development of the site.

A Phase I ESA cannot ascertain that a property is completely free of chemical or toxic substances. We believe the scope of work has been appropriate to allow the client to make an informed business decision. According to ASTM E1527-13, the "shelf life" of an ESA report is six months; an update can be provided to the client within the first year of the report's publication. Changes in site conditions/use could render this report obsolete within a shorter period of time. Use of this report outside of these time frames or after site conditions/uses have changed is at the sole risk of the user.

The results contained in this report are based upon the information acquired during the assessment, including information obtained from third parties. ESP makes no warranty as to the accuracy of the information obtained from others. In addition, it is possible that variations exist beyond or between points evaluated during this assessment, and that changes in conditions could occur due to the works of man, contaminant migration, variations in rainfall or temperature, changes in regulatory standards, or other circumstances not existent at the time the assessment was prepared.

The services performed by ESP have been conducted in a manner consistent with the level of care and skill ordinarily exercised by members of our profession currently practicing under similar conditions in the site vicinity. No other warranty, express or implied, is offered.

#### 2.0 GENERAL SITE INFORMATION

#### Size and Location

The site is located about 1,100 feet east of the intersection of the Southside Road and Enterprise Road in Hollister, California. The site encompasses two parcels and a total of approximately 50.4-acres with a separate approximate 1.4-acre rural residential property at 394 Enterprise Road and an approximate 1.9-acre well easement (San Benito County Water District) along Enterprise Road that are not included in this ESA.



#### Assessor's Parcel Number

The site is identified as San Benito County Assessor's Parcel Numbers 020-290-051 and -052.

#### **Site Boundaries**

The property is bounded on the north and northeast by Enterprise Road. A northwest trending ridge and rural residential and agricultural lands are present to the west, Quail Oak subdivision is present on the east, and Ridgemark Golf and Country Club is present on the south.

#### **Current Development and Access**

The site is accessed from Enterprise Road and is currently undeveloped, The site is used for cattle grazing and growing dryland crops.

#### Land Use/Zoning

Land use/zoning information was obtained from the San Benito County Zoning Map. The site is zoned rual residential.

#### **Site Topography**

Elevations on site range from about 464 feet at its south end to about 349 feet at Enterprise Road. Topographically the site consist of a gently to moderately sloping terrace surface on its south and central sections that descends across a terrace face about 8 feet in height at its northen edge and about 10 feet in height on its eastern edge. A broad swale that drains northward is present east of the terrace face and essentiall flat areas are present to the north. Overall the site is drained by northeast-directed sheetflow to a the broad swale.

#### **Surface Water Bodies**

No natural surface water bodies are located on the property. The San Benito River is located about 2,400 feet to the west and flows to the northwest. Based on Environmental Data Resources' (EDR) Radius Map Report with GeoCheck (Appendix E), the eastern portion of the site associated with the broad swale lies within a 1% Special Flood Hazard Area.

#### **Geology and Hydrogeology**

Based on mapping by Rosenberg (1998), the entire site is underlain by Pleistocene-age, older flood-plain deposits (Qof). Pleistocene to Pliocene-age, San Benito Gravels are mapped on the

rdidge west of the site and a trace of the East Branch Calaveras fault is mapped along its eastern base.

Based on Environmental Data Resources Radius Map report (see Appendix E) soils at the site mostly consist of Antioch Loam with Reiff sandy loam along the northern edge of the site and terrace escarpment soils within the broad swale. Antioch loam is described as moderately well drained with a high corrosion potential and very slow infiltration rates. Reiff sandy loam is described as moderately well and well drained with a moderate corrosion potential and moderate infiltration rates. The terrace escarpments soils are described as having slow infiltration rates.

Site specific hydrogeologic data was not available to Environmental Data Resources Radius Map report (see Appendix E). Based on San Benito County's Annual Groundwater Report (Todd Groundwater, 2018), depth to first groundwater in the site vicinity measured December 2018 is on the order of 100 feet below ground surface and flows to the northwest.

#### 3.0 SITE RECONNAISSANCE

#### **Site Observations**

On December 31, 2019, and again on January 14, 2020, Earth Systems Pacific personnel visited the site. The purpose of the reconnoitering was to evaluate current site conditions and adjacent land use. Photographs of the site are presented in Appendix B. A summary of our observations is presented below.

The northern portion of the site was developed with a barn and two long sheds used for farm equipment maintenance and storage. The central and southern portions of the site were undeveloped and used for cattle grazing and dryland farming. House keeping in the area of the sheds and barns was generally poor and surrounded with dilapidated farm equipment, cars, trucks, and trailers. Deteriorated bags of powdered herbicides and small containers of what appeared to be fuel were present in the sheds. There were two drums with unknown contents resting on their side and what appeared to be an old fuel tank in the general area of the barn and sheds. There was no obvious evidence that the drums or tank leaked.



#### **Site Vicinity Observations**

The property opposite the site on Enterprise Road was occupied by farm structures, associated farming equipment and a small abandoned gravel quarry; activity of the farm is unknown however conditions of tooling suggests no current farming activities associated with this address/property. Two water wells are present on San Benito County Water District easement. We did not observe evidence that environmental conditions at the site have been impacted by use or activities in the surrounding areas.

#### 4.0 HISTORICAL INFORMATION

Information regarding the history of the site was obtained from various sources, as discussed below.

#### **Sanborn Fire Insurance Maps**

To evaluate past site uses, a search for Sanborn Fire Insurance Company maps was performed by EDR. According to EDR, Sanborn map coverage is not available for is area of Hollister.

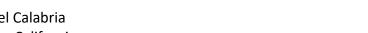
#### **Aerial Photographs**

To assist in determining past uses that could have an environmental impact on the property, historical aerial photographs were reviewed. The information below is a summary of the review of photographs of the site taken between 1939 and 2016. Features on the site and adjacent areas are described below. Copies of the aerial photographs are presented in Appendix C.

<u>1937</u> – Enterprise Road and incipient Airline Highway are present. The northern half of the site is primarily used to grow dryland crops, with the southern half appearing to be fallow. Orchards are seen at the northwest corner of the site. Bundles of dry crops are seen at then northeastern area of the site. The site is bounded by agricultural fields used to grow dry crops to the west, south, and east, and by Enterprise Road to the north.

<u>1949</u>– A majority of the orchards on the site have been removed with a small portion remaining along Enterprise road. Elsewhere the site and vicinity appear similar to the 1937 photograph.

<u>1953</u> – The barn is present on the northern portion of the site. Elsewhere the site and vicinity appear similar to the 1949 photograph.



Vista Del Calabria Hollister, California

1960 – Low resolution. Possible structures present on the western-bounding property.

1971 - No discernible image.

<u>1974</u> – The barn and sheds are present on the northern portion of the site. Structures referenced in the 1960 imagery are visable and a building is constructed on the southeast bouding property. Elsewhere the site and vicinity appear similar to the 1953 and 1960 photograph.

<u>1981 (infrared, low-resolution)</u> - Site conditions appear similar to 1974. A stormwater-type basin appears to be developed on the south-bounding parcel. Ridgemark Golf and Country Club is developed on the southeast-bounding property. Elsewhere the site and vicinity appear similar to the 1974 photograph.

<u>1998</u> – Additional orchards are established at the northwestern corner of the site and occupy an area similar to that of 1949 imagery. Qual Hallow residential development is under construction on the eastern-bounding property. Elsewhere the site and vicinity appear similar to the 1981 photograph.

<u>2006</u> – What appears to be plastic sheeting is present covering the ground on the northwest site corner that may have been placed in connection with preparing for growing row-crops. What appears to be a storm water pond is present just east of the barn and sheds. The Quail Oak residential development is completed on the eastern-bounding property. Elsewhere the site and vicinity appear similar to the 1974 photograph.

<u>2009</u> – The plastic sheeting is absent and the land appears to be fallow. Elsewhere the site and vicinity appear similar to the 2006 photograph.

<u>2012</u> and <u>2016</u> – Site and vicinity conditions appear similar to 2009 imagery, except that the storm water pond is no longer present in the 2016 photograph.

Earth Systems also reviewed historic images dated later than 2016 available through Google Earth. The northest portion of the site was used to grow orchard crops until February 2018. The orchards are absent in later images. Elsewhere, the site appears similar to the 2016 photograph.



#### **Historic Topographic Maps**

Topographic maps published by the U.S. Geological Survey were reviewed to evaluate past land use on the site. The maps available for the Hollister area date from 1921-2012. In general, the maps indicate a use history similar to that present in the aerial photographs. Features depicted on the site and adjacent areas are described below. Copies of the topographic maps are attached with this report in Appendix D.

<u>1919, 1921, and 1923 (15-minute quadrangles)</u> – Enterprise Road and railroad tracks are shown and there are no features or indicated land use depicted on the site.

1955, 1971 (both 7.5-minute quadrangles); 1987 (15-minute quadrangle) – A building structure is depicted on the site. A gravel pit is labeled directly accoss the northeast corner of the site along Enterprise Road. Structures are depicted on the western-bounding property and development of Ridgemark Golf and Country Club is seen at the southeast-bounding property. Elsewhere the site and vicinity are depicted similar to the 1923 map.

<u>1993, 1995 (7.5-minute quadrangles)</u> – wells are depicted at the northeastern portion of the site. Elsewhere the site and vicinity are depicted similar to the 1987 map.

<u>2012 (7.5-minute quadrangle)</u> – Wells are not depicted on the site. Roads related to Qual Hallow residential development is seen to the east of the site. Elsewhere the site and vicinity are depicted similar to the 1995 map.

#### **City Directory Listings**

City directories, which contain telephone book listings alphanumerically by their street address, were also researched by EDR for information regarding past site use. The directories were reviewed in 5-year intervals dating from 1964 to 2014. The address associated with the site is 213 Enterprise Road. Below are the directory listings associated with the address aforementioned.

#### 1992

Elias, Ralph; L&G Transportation; Lico & Greco; Russell, Waler

#### 1995

Elias, Ralph; L&G Transportation; Lico, Joe A; Russell, Waler

#### 2000

Arreguin, Maria J; Elias, Juana; Gallo, Maria I; Gonzales, Jacabo

#### 2005

Galvan, Richard; Luna, Victor; Part, Lico; Rodriguez, Adela; Salazar, Celeste; Sandoval, Jose L

#### <u>2010</u>

Fonseca, Maria E; Gonzales, Rios F; Jimenez, J; Luna Samuel; Part, Lico; Rios, Filiberto G; Rodriguez, Adela; Santiago, Idineo; Zepeda, Mario

#### 2014

Fonseca, Maria E; Gonzales, Rios F; Jimenez, Valentin; Luna Samuel; Ortiz, Jorge; Part, Lico; Zepeda, Mario

Based on the city directory listing review, there is no record of listing(s) on the site with the potential to impact the subject site.

#### 5.0 RECORDS REVIEW

#### **Agency Database Search Report**

A report summarizing the information available from regulatory agencies regarding sites that generate, store, use, and/or have released hazardous materials was prepared by Environmental Data Resources (EDR). Search distances used for each list are in accordance with ASTM E1527-13 guidelines as measured from the site perimeter. The subject property and additional facilities are listed in the report within 1-mile of the site. No orphan sites were listed in the EDR report.

Facilities of interest within the search radius are detailed below. A copy of the database summary report is included as Appendix E.



## Vista Del Calabria Hollister, California

January 16, 2020

| Listing                     | <u>Location</u>     | <u>Database</u>    | <u>Distance</u> |
|-----------------------------|---------------------|--------------------|-----------------|
| Enterprise Well #7          | 600 Enterprise Road | CUPA, et. al       | 0.068 mi.       |
| Sunnyslope CWD Well #11     | 2783 Southside Road | CUPA, et. al       | 0.250 mi.       |
| Sunnyside Estates           | 2780 Southside Road | Envirostor, et. al | 0.251 mi        |
| Southside Road Project Area | 3110 Southside Road | Envirostar         | 0.305 mi        |
|                             |                     | Brownfields        |                 |
| Carolyn Hamilton            | 161 Ladd Lane       | Envirostor, et. Al | 0.655 mi.       |
| Hazel Hawkins Hospital      | 911 Sunset Drive    | LUST, et. Al       | 0.802 mi.       |

Based on the types, status of listing, distance, and relative elevation from the subject site, none of the identified facilities appear to have the potential to impact the site nor indicate the likelihood for the presence of RECs at the site.

#### **California Department of Toxic Substances Control**

The California Department of Toxic Substances Control (DTSC) *Envirostor* database was queried to research records on file regarding known problems at the site address or in the site vicinity. No sites within a 0.5-mile radius not already listed in Section 5.0 were found in the *Envirostor* database.

#### **Tribal Records**

This site is not located on or near tribal lands; therefore, tribal records were not researched.

#### **Engineering and Institutional Controls**

No Engineering or Institutional Controls (Waste Discharge Requirements, etc.) were identified for the site.

#### Oil and Gas Maps

The California Department of Conservation, Division of Oil, Gas and Geothermal Resources (DOGGR) online mapping service was reviewed for information regarding historic oil or gas well drilling activities on or near the site. According to the map, no oil or gas wells have been drilled on the subject site. The nearest well is shown about 6,500 feet to the southwest and listed as a plugged dry hole. Based on the status of the well, it does not present a REC to the site.



#### 6.0 INTERVIEWS AND GENERAL RESEARCH

#### **Current Owners/Occupants/Operators**

Mr. Anthony Lico, owner representative, was briefly interviewed on January 15, 2020. Mr. Lico stated that he was not aware of underground storage tanks on the site or known environmental concerns.

#### **Previous Report**

Earth Systems was provided with an Agrichemical Assessment - Phase II ESA report completed by Engeo (2014) that included the northwest section of the subject site where orchard crops, and possibly row crops, were grown. Below is a summary of our review of laboratory results of samples collected on the subject site. A copy of Engeo's report is presented in Appendix F.

Composite samples S-17, S-18, S-19, and S-20 were collected on the subject site. The samples were tested for organochlorine pesticides and the metal arsenic. Trace amounts of the pesticides DDE and dieldrin were detected in the samples. The levels were compared to California Regional Water Quality Control Board 2019 (rev. 2) Environmental Screening Levels (ESLs) for direct human exposure in residential settings. The pesticide levels are below their respective ESLs. Arsenic was detected in all of the samples at levels above its ESL. However, the levels are within the range found to naturally occur in this region of California (Duvergé, 2011). It is our opinion that the levels of pesticides and arsenic detected in shallow soil on the site do not present a recognized environmental condition at the site.

#### Past Owners/Occupants/Operators

Contact information for past owner/occupants/operators was not provided to us and, therefore, no interviews were conducted.

#### **Local Agency Records**

We requested to review San Benito County hazardous material files pertaining to the subject site. There was no response to our request by the time of this report.

#### 7.0 SUMMARY, CONCLUSIONS, AND RECOMMENDATIONS

This report presents the findings of the Phase I ESA conducted for the Vista Del Calabria residential development located at Enterprise Road on APNs 020-290-051 & -052, in Hollister,



Hollister, California

California. We understand that the requested ESA is in connection with development of the property. We have endeavored to perform this ESA in general conformance with the scope and limitations of the ASTM Standard E1527-13. Exceptions to or deviations from this scope are described in Section 1.0 of this report. The purpose of this assessment was to evaluate the site for the presence of Recognized Environmental Conditions (RECs) related to the current or past use, handling, storage, or disposal of hazardous materials or petroleum products on or near the subject property. This assessment has identified the following information:

- The site is occupied by a barn and sheds that were constructed between 1959 and 1974. The northwest portion of the site was used to grow orchards between at least 1939 and February 2018. Other site areas have been used for cattle grazing and to grow dryland crops since at least 1939. There was no evidence of water wells on the site. San Benito County Water District wells # 6 and 7 are located adjacent to Enterprise Road and outside the boundaries of the subject site.
- Because the northwest portion of the site was previously used for growing crops, shallow soils were previously sampled and analyzed for organochlorine pesticides and arsenic. Based on an Agrichemical Assessment - Phase II ESA report by Engeo (2014), trace levels of the pesticides DDE and dieldrin are present on the site. However, the levels are below Regional Water Quality Control Board Environmental Screening Levels (ESIs), direct human exposure in residential settings. Whereas arsenic levels exceeded its ESL, the levels are within the range found to naturally occur in this region of California (Duvergé, 2011). As such, prior use of the site for agricultural purposes does not constitute a REC at the site.
- During our reconnaissance, dilapidated farm equipment, vehicles, and trailers were present in the area of the barn and sheds. We also observed two drums resting on their side, what appeared to be an old fuel tank, deteriorated packages of dry herbicides, and a few small containers that appeared to contain fuel. There was no obvious evidence that the drums, tank or fuel containers leaked. However, it is possible that there are limited areas of oil staining on the site in connection with the dilapidated equipment and vehicles.



## Vista Del Calabria Hollister, California

January 16, 2020

 There was no evidence that conditions on adjacent properties observed during the site reconnaissance were likely to adversely affect the subject property.

#### **Recognized Environmental Conditions (REC)**

Based on the work for this Phase I Environmental Site Assessment, there were no recognized environmental conditions identified at the site.

#### Recommendations

Whereas there were no RECs identified on the site, Earth Systems has developed the following recommendations regarding de minimis conditions observed at the site.

- The drums and old fuel tank, as well as any their contents if any, should be recycled or disposed of in a regulatory approved manner.
- The deteriorated bags of dry herbicide should be repackaged, if planned for future use, or disposed of in a regulatory approved manner.
- It is possible that petroleum staining associated with the dilapidated farm equipment and vehicles not obvious at the time of our reconnaissance is present at the site. It is assumed that such staining would be limited to small areas and less than a foot in depth. During site development if staining is present to a greater degree, Earth Systems should be contacted to assess their possible impacts.

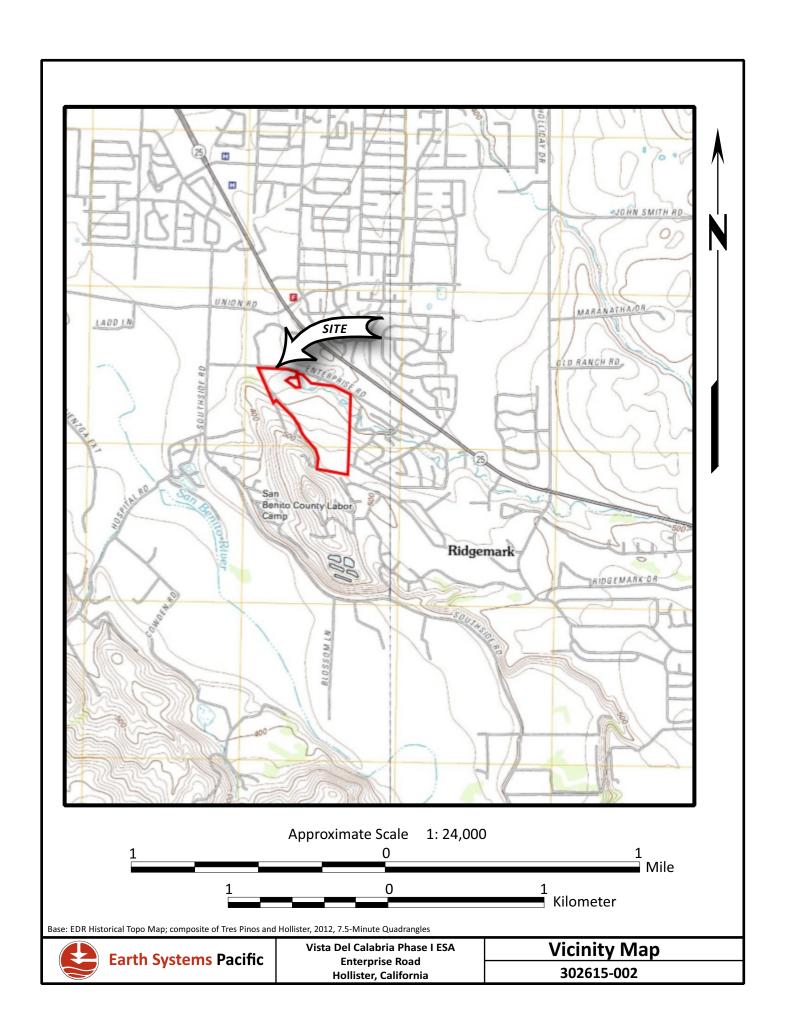


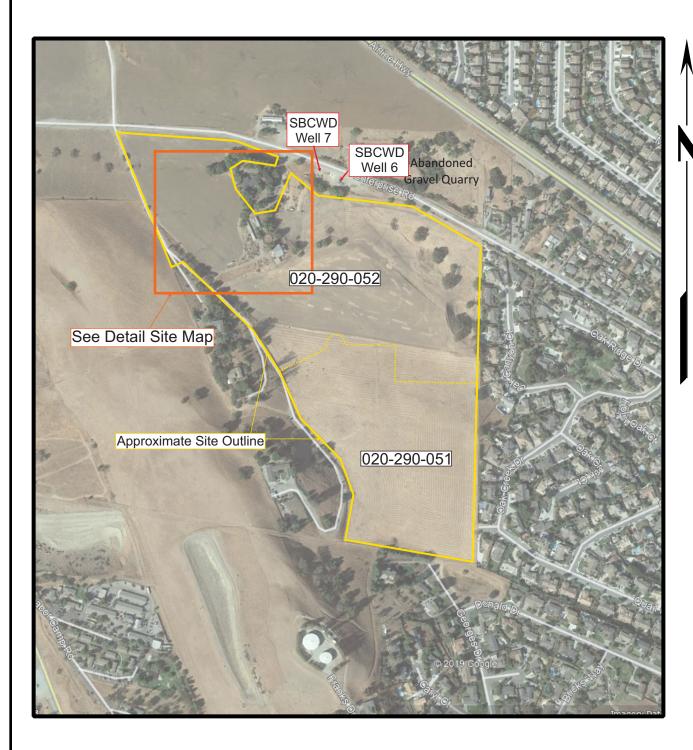
#### **REFERENCES**

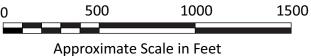
- American Society for Testing and Materials (ASTM) Standard E1527-13, Standard Practice for Environmental Site Assessments: Phase I Environmental Site Assessments.
- California Department of Conservation, Division of Oil, Gas and Geothermal Resources, *DOGGR*Online Mapping Service (DOMS), <a href="http://maps.conservation.ca.gov/doms/doms-app.html">http://maps.conservation.ca.gov/doms/doms-app.html</a>.
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- Duvergé, D.J., 2011, Establishing Background Arsenic in Soil of the Urbanized San Francisco Bay Region, Thesis, San Francisco State University
- ENGEO, 2014, Agrichemical Assessment-Phase II ESA, 213 Enterprise Road, Hollister, California, Project No. 11227.000.000.
- Environmental Data Resources, 2019, EDR Radius Map with GeoCheck Report for Vista Del Calabria, Southside Road and Enterprise Road, Hollister, California, EDR Inquiry No. 5914923.2s, dated December 30, 2019.
- Rosenberg, L., 1998, Liquefaction Susceptibility of the Hollister Area, San Benito County, California, Relative Liquefaction Susceptibility Map.
- Rosenberg, L., 1998, Liquefaction Susceptibility of the Hollister Area, San Benito County, California, Quaternary Geologic Map.
- San Benito County, 2019, Assessor Map, WebGIS search tool.
- San Benito County Water District, 2018, Annual Groundwater Report.

# **APPENDIX A**

**FIGURES** 



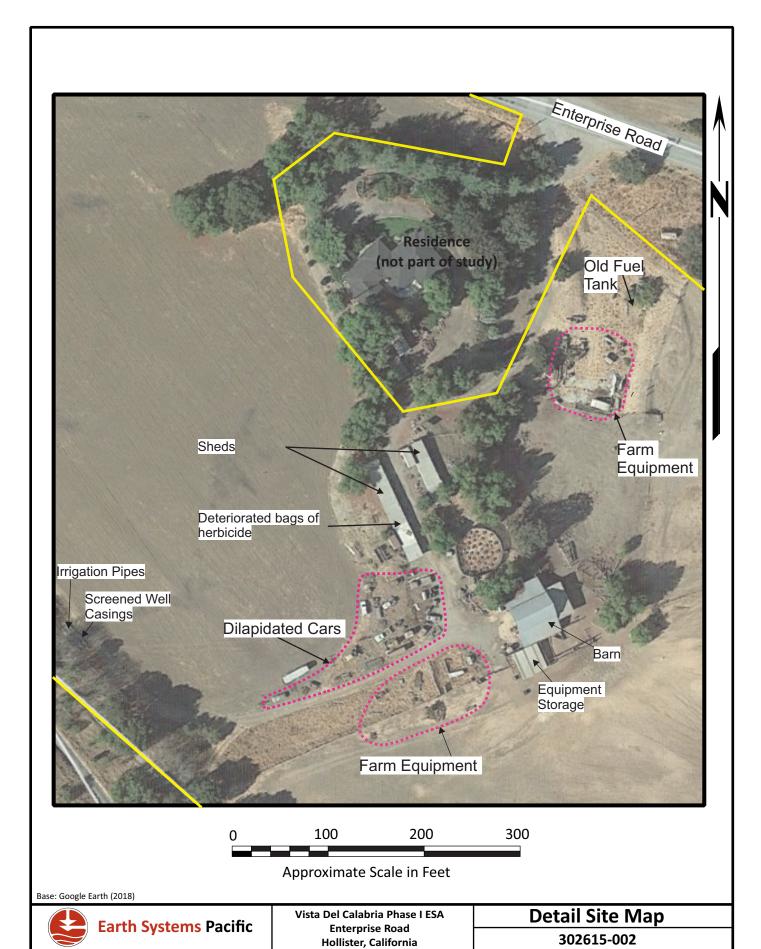




Base: Google Earth (2018)



Vista Del Calabria Phase I ESA Enterprise Road Hollister, California Overall Site Map 302615-002



#### **APPENDIX B**

### **PHOTOGRAPHS**



Dilapidated Vehicles and possible old fuel storage tank.



View of dilapidated vehicles and barn, looking east.



View of shed and deteriorated bags of herbicide.



Southern portion of the site with cattle grazing. Picture taken facing northeast.



Qual Oak Hallow at top left and Ridgemark at top right. Picture taken facing southeast.



Small containers with possible fuel.



Drum resting on its side rear of shed.



Drum resting on its side, west site boundary.

# APPENDIX C AERIAL PHOTOGRAPHS

# Vista Del Calabria Phase I ESA

Southside Rd/Enterprise Rd Hollister, CA 95023

Inquiry Number: 5914923.8

December 23, 2019

# The EDR Aerial Photo Decade Package



# **EDR Aerial Photo Decade Package**

12/23/19

Site Name: Client Name:

Vista Del Calabria Phase I ESA Southside Rd/Enterprise Rd Hollister, CA 95023 EDR Inquiry # 5914923.8 Earth Systems Pacific, Northern CA 500 Park Center Drive Hollister, CA 95023

Contact: David Teimoorian



Environmental Data Resources, Inc. (EDR) Aerial Photo Decade Package is a screening tool designed to assist environmental professionals in evaluating potential liability on a target property resulting from past activities. EDR's professional researchers provide digitally reproduced historical aerial photographs, and when available, provide one photo per decade.

#### Search Results:

| <u>Scale</u> | <u>Details</u>  | Source   |
|--------------|---|--|
| 1"=500'      | Flight Year: 2016   | USDA/NAIP  |
| 1"=500'      | Flight Year: 2012   | USDA/NAIP  |
| 1"=500'      | Flight Year: 2009   | USDA/NAIP  |
| 1"=500'      | Flight Year: 2006   | USDA/NAIP  |
| 1"=500'      | Acquisition Date: August 17, 1998   | USGS/DOQQ  |
| 1"=500'      | Flight Date: August 03, 1981  | USDA   |
| 1"=500'      | Flight Date: July 12, 1974  | USGS   |
| 1"=500'      | Flight Date: July 04, 1971  | USGS   |
| 1"=500'      | Flight Date: April 02, 1960   | USGS   |
| 1"=500'      | Flight Date: July 15, 1953  | USGS   |
| 1"=500'      | Flight Date: August 01, 1949  | USDA   |
| 1"=500'      | Flight Date: May 25, 1939   | USDA   |
|              | 1"=500' 1"=500' 1"=500' 1"=500' 1"=500' 1"=500' 1"=500' 1"=500' 1"=500' 1"=500' | 1"=500' Flight Year: 2016 1"=500' Flight Year: 2012 1"=500' Flight Year: 2009 1"=500' Flight Year: 2006 1"=500' Acquisition Date: August 17, 1998 1"=500' Flight Date: August 03, 1981 1"=500' Flight Date: July 12, 1974 1"=500' Flight Date: July 04, 1971 1"=500' Flight Date: April 02, 1960 1"=500' Flight Date: July 15, 1953 1"=500' Flight Date: August 01, 1949 |

When delivered electronically by EDR, the aerial photo images included with this report are for ONE TIME USE ONLY. Further reproduction of these aerial photo images is prohibited without permission from EDR. For more information contact your EDR Account Executive.

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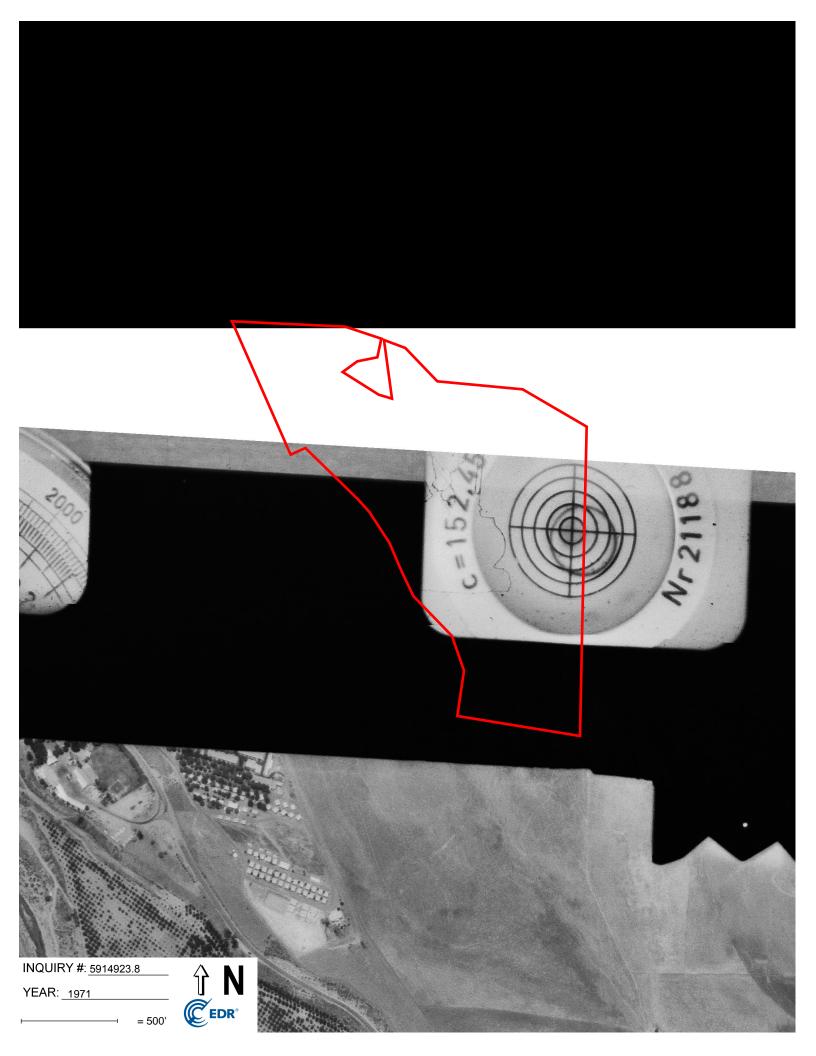






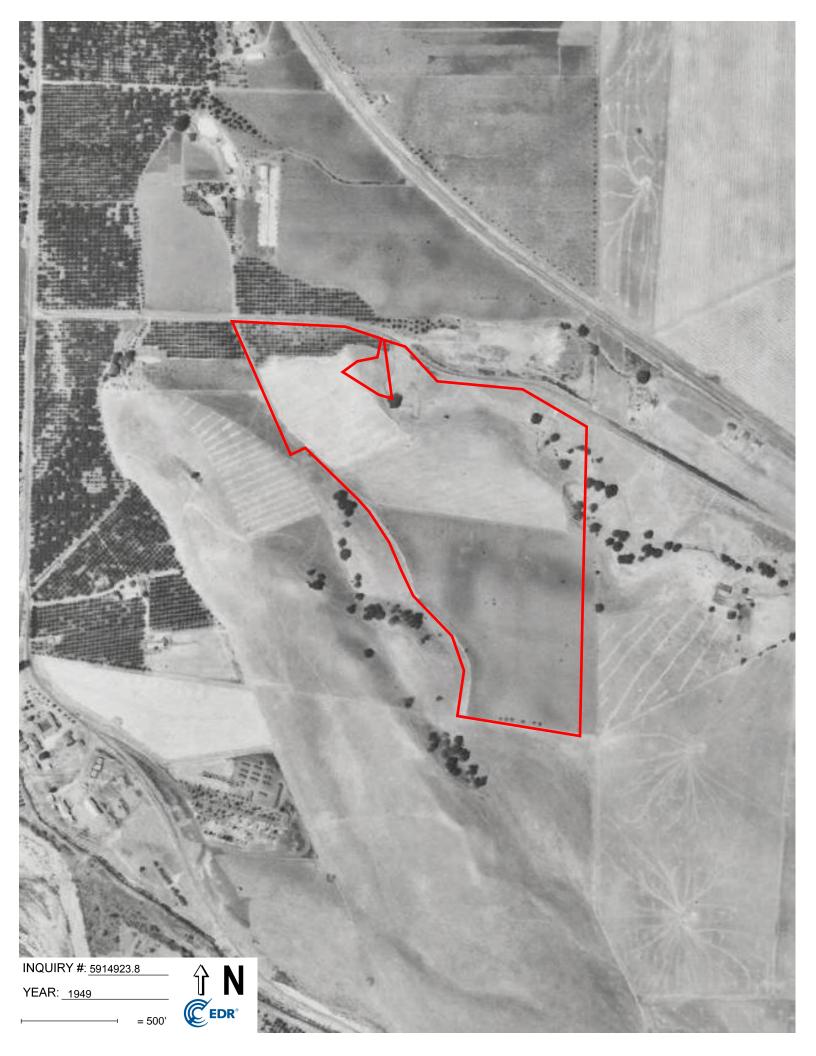














## APPENDIX D

**TOPOGRAPHIC MAPS** 

Vista Del Calabria Phase I ESA Southside Rd/Enterprise Rd Hollister, CA 95023

Inquiry Number: 5914923.4

December 23, 2019

## **EDR Historical Topo Map Report**

with QuadMatch™



## **EDR Historical Topo Map Report**

Site Name: **Client Name:** 

Vista Del Calabria Phase I ESA Southside Rd/Enterprise Rd Hollister, CA 95023

EDR Inquiry # 5914923.4

Earth Systems Pacific, Northern CA 500 Park Center Drive

Hollister, CA 95023

Contact: David Teimoorian



12/23/19

EDR Topographic Map Library has been searched by EDR and maps covering the target property location as provided by Earth Systems Pacific, Northern CA were identified for the years listed below. EDR's Historical Topo Map Report is designed to assist professionals in evaluating potential liability on a target property resulting from past activities. EDRs Historical Topo Map Report includes a search of a collection of public and private color historical topographic maps, dating back to the late 1800s.

| Search Res  | ults:                     | Coordinates:  |                                |
|-------------|---------------------------|---------------|--------------------------------|
| P.O.#       | 302615-002                | Latitude:     | 36.818916 36° 49' 8" North     |
| Project:    | Lico Property Development | Longitude:    | -121.379382 -121° 22' 46" West |
| -           | , , ,                     | UTM Zone:     | Zone 10 North                  |
|             |                           | UTM X Meters: | 644542.92                      |
|             |                           | UTM Y Meters: | 4076009.70                     |
|             |                           | Elevation:    | 453.82' above sea level        |
| Mans Provid | ded:                      |               |                                |

#### waps Provided:

2012 1919 1995 1993 1987 1971 1955 1923 1921

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## Topo Sheet Key

This EDR Topo Map Report is based upon the following USGS topographic map sheets.

## 2012 Source Sheets



Tres Pinos 2012 7.5-minute, 24000



Hollister 2012 7.5-minute, 24000

## 1995 Source Sheets



Hollister 1995 7.5-minute, 24000 Aerial Photo Revised 1987

## 1993 Source Sheets



Hollister 1993 7.5-minute, 24000 Aerial Photo Revised 1987

### 1987 Source Sheets



HOLLISTER 1987 15-minute, 50000

## Topo Sheet Key

This EDR Topo Map Report is based upon the following USGS topographic map sheets.

## 1971 Source Sheets



Hollister 1971 7.5-minute, 24000 Aerial Photo Revised 1971



Tres Pinos 1971 7.5-minute, 24000 Aerial Photo Revised 1971

## 1955 Source Sheets



Hollister 1955 7.5-minute, 24000 Aerial Photo Revised 1952



Tres Pinos 1955 7.5-minute, 24000 Aerial Photo Revised 1953

## 1923 Source Sheets



Hollister 1923 15-minute, 62500

### 1921 Source Sheets



Hollister 1921 15-minute, 62500

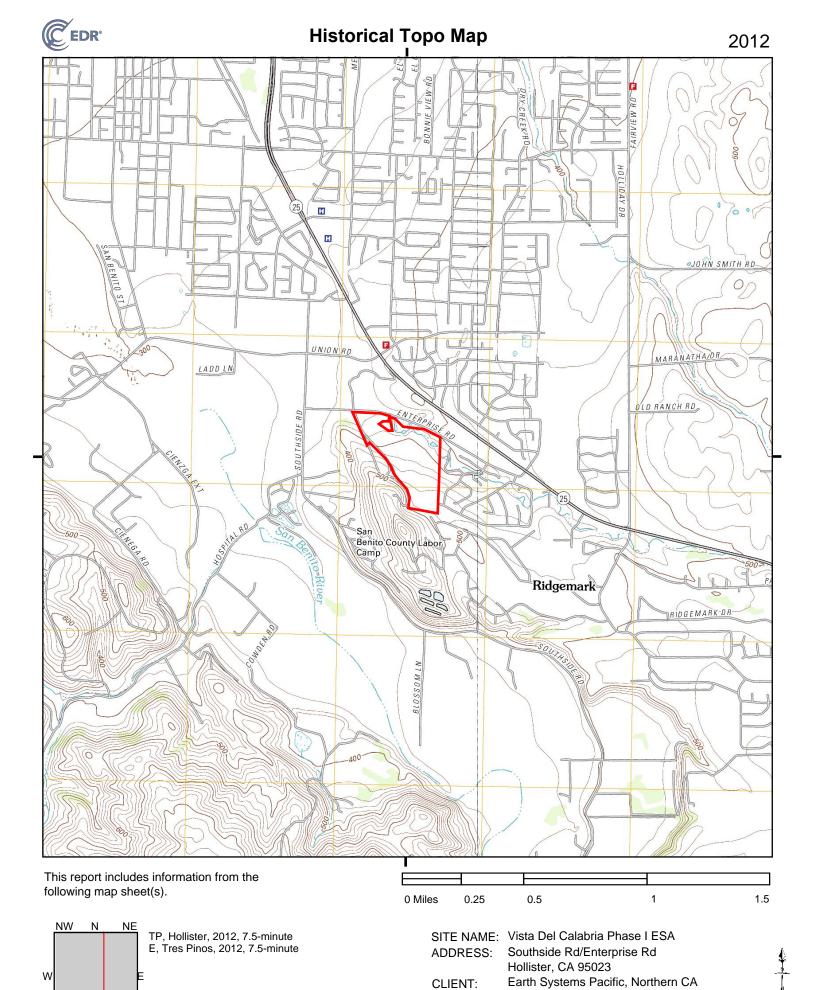
## Topo Sheet Key

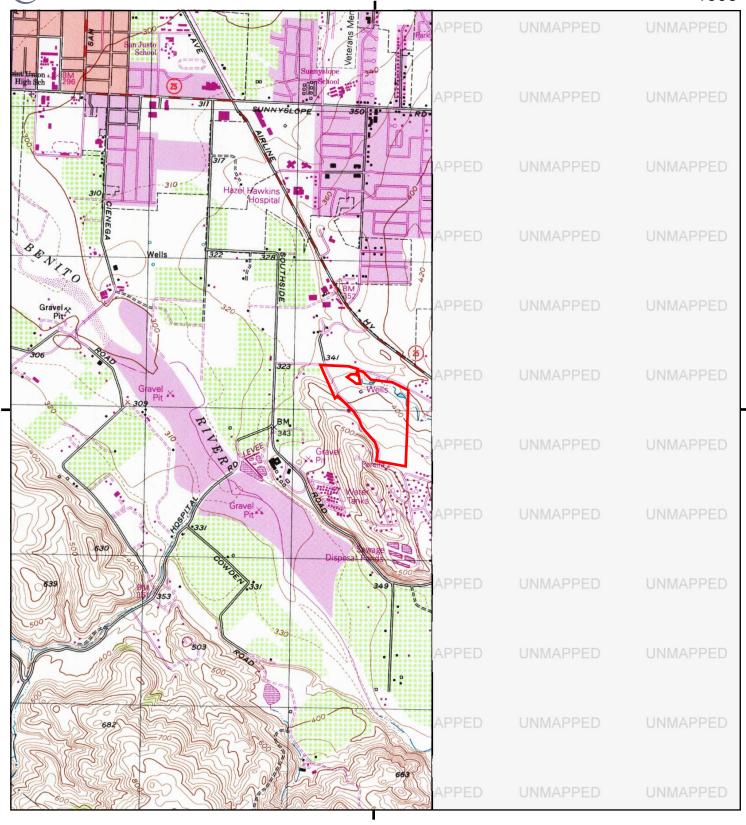
This EDR Topo Map Report is based upon the following USGS topographic map sheets.

## 1919 Source Sheets

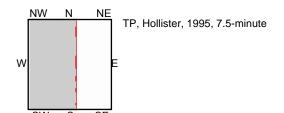


Hollister 1919 15-minute, 48000





This report includes information from the following map sheet(s).



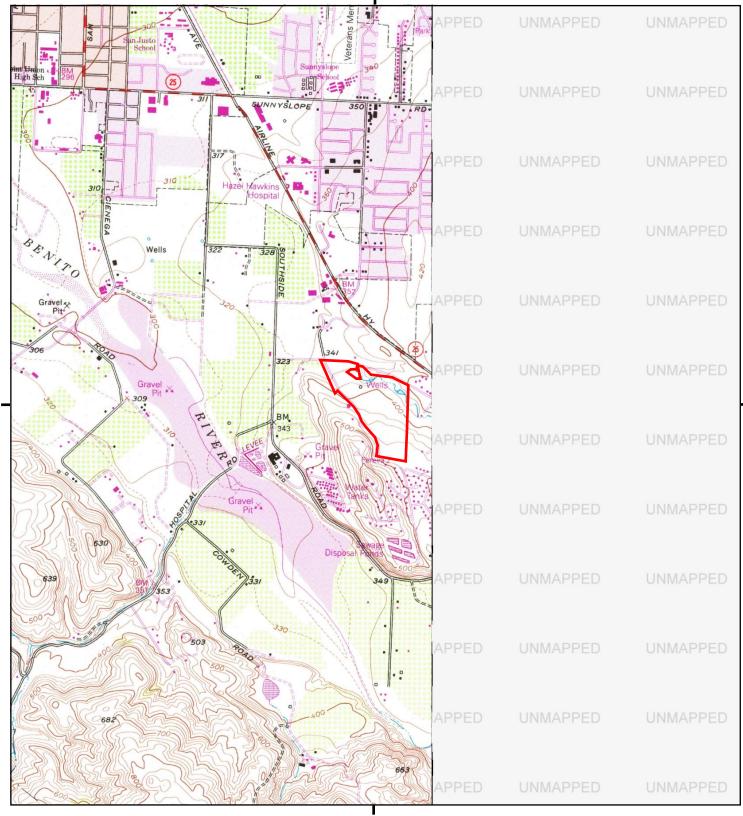
0 Miles 0.25 0.5 1 1.5

SITE NAME: Vista Del Calabria Phase I ESA ADDRESS: Southside Rd/Enterprise Rd

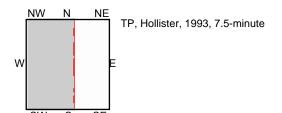
Hollister, CA 95023

CLIENT: Earth Systems Pacific, Northern CA





This report includes information from the following map sheet(s).



0.5 1.5 0 Miles 0.25

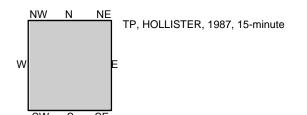
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Hollister, CA 95023

Earth Systems Pacific, Northern CA CLIENT:



This report includes information from the following map sheet(s).



0 Miles 0.25 0.5 1

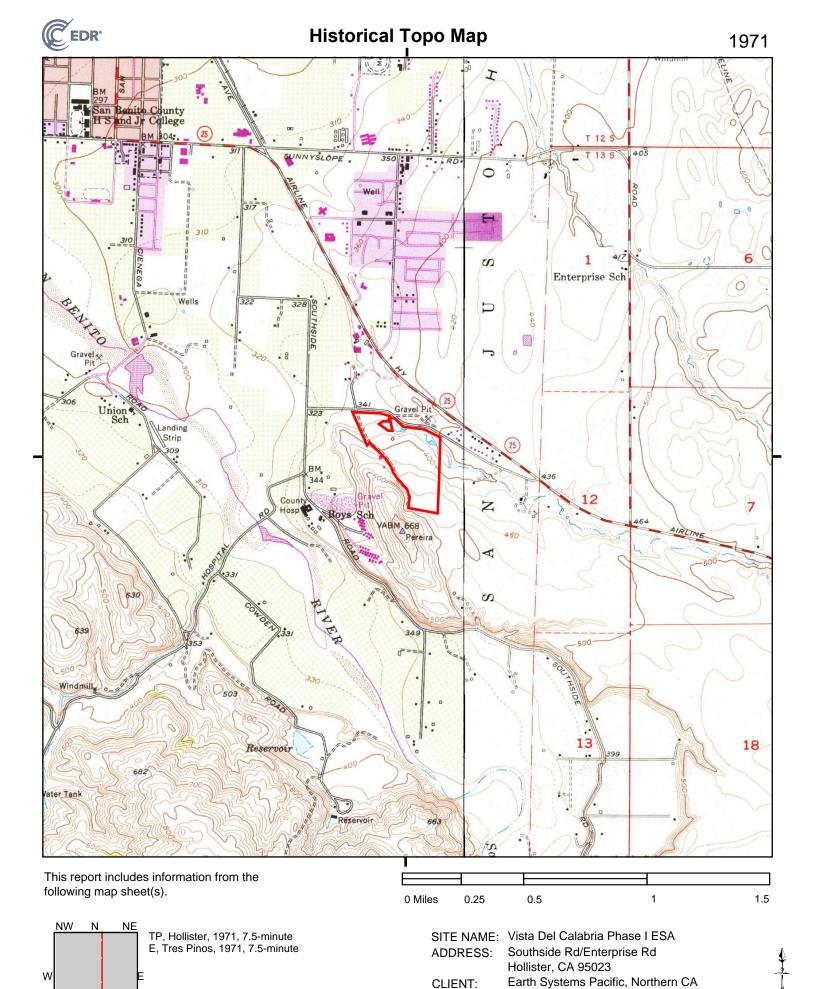
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Hollister, CA 95023

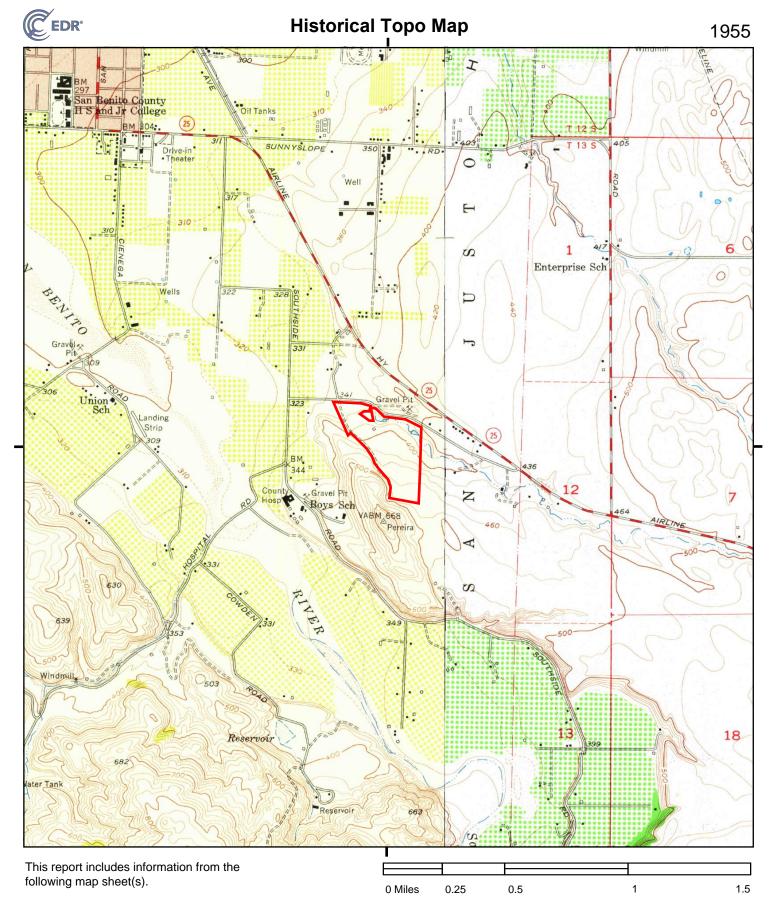
CLIENT: Earth Systems Pacific, Northern CA

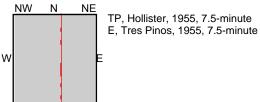


1.5



SW



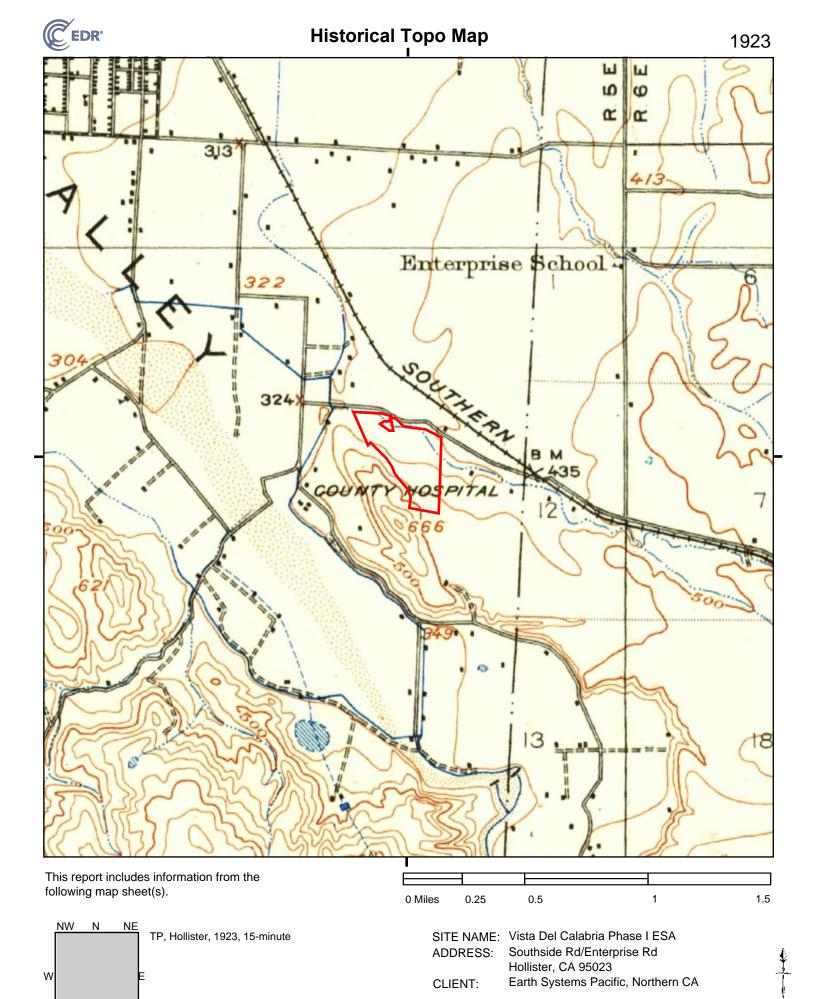


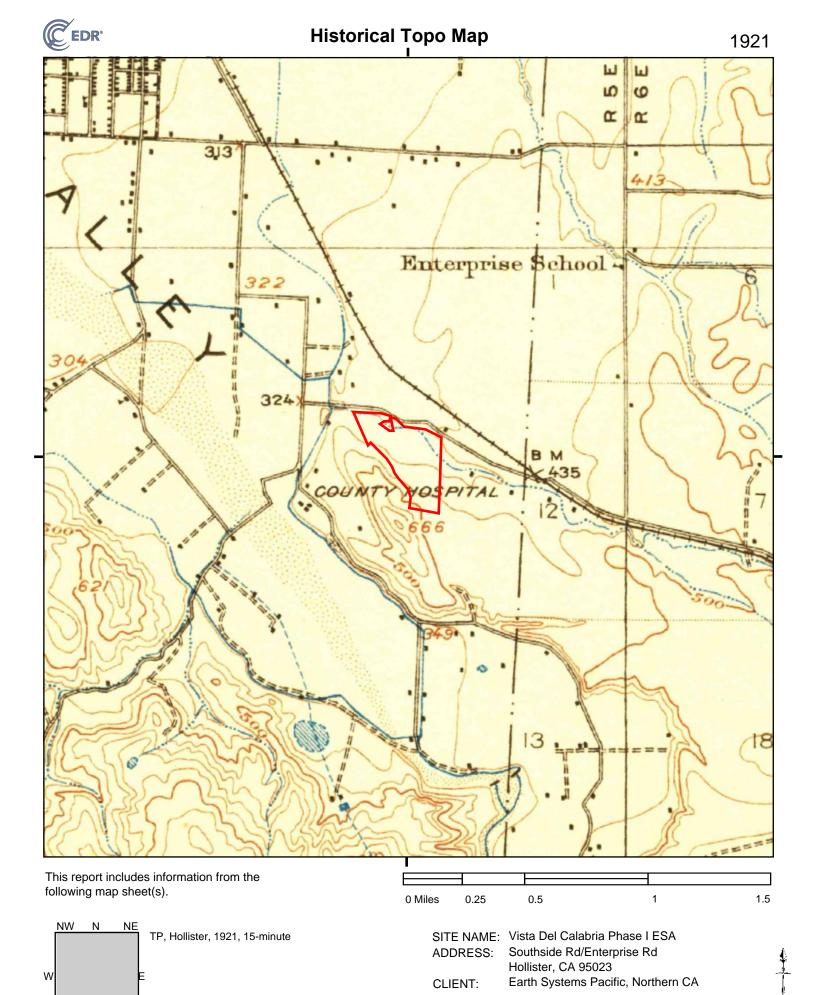
SW

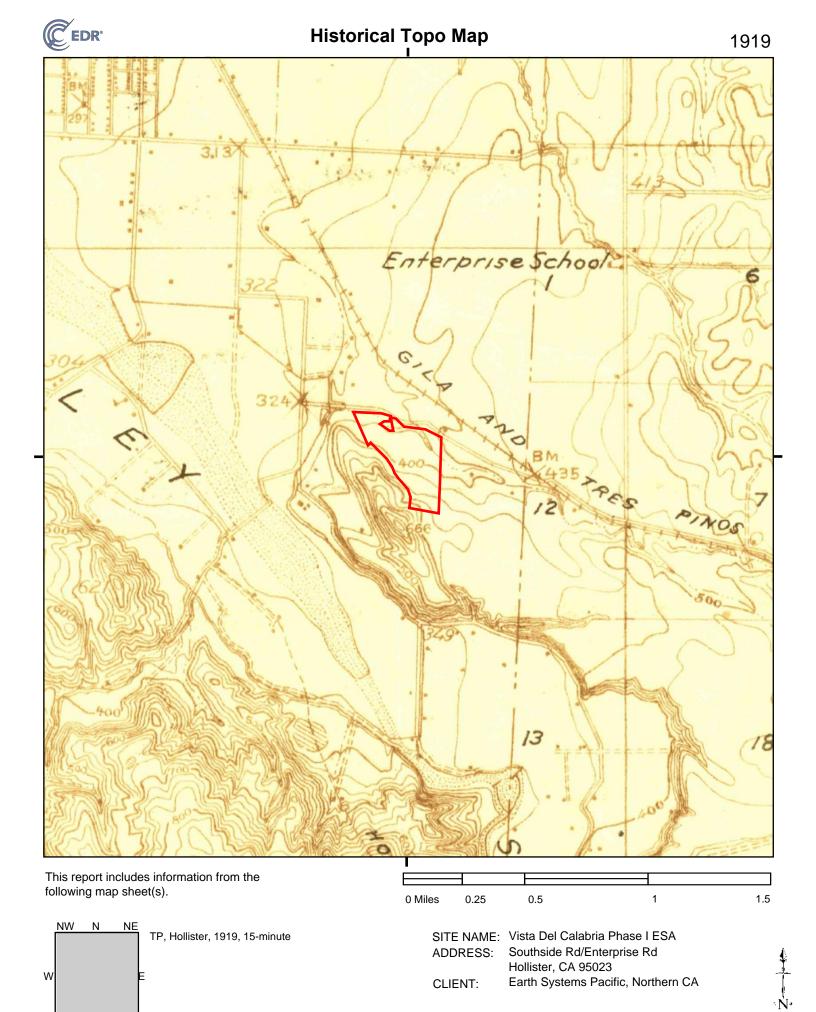
SITE NAME: Vista Del Calabria Phase I ESA ADDRESS: Southside Rd/Enterprise Rd

Hollister, CA 95023

CLIENT: Earth Systems Pacific, Northern CA







## APPENDIX E

**AGENCY DATABASE SEARCH REPORT** 

## Vista Del Calabria Phase I ESA

Southside Rd/Enterprise Rd Hollister, CA 95023

Inquiry Number: 5914923.2s

December 30, 2019

# **EDR Summary Radius Map Report**



6 Armstrong Road, 4th floor Shelton, CT 06484 Toll Free: 800.352.0050 www.edrnet.com

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**Thank you for your business.**Please contact EDR at 1-800-352-0050 with any questions or comments.

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A search of available environmental records was conducted by Environmental Data Resources, Inc (EDR). The report was designed to assist parties seeking to meet the search requirements of EPA's Standards and Practices for All Appropriate Inquiries (40 CFR Part 312), the ASTM Standard Practice for Environmental Site Assessments (E 1527-13), the ASTM Standard Practice for Environmental Site Assessments for Forestland or Rural Property (E 2247-16), the ASTM Standard Practice for Limited Environmental Due Diligence: Transaction Screen Process (E 1528-14) or custom requirements developed for the evaluation of environmental risk associated with a parcel of real estate.

#### TARGET PROPERTY INFORMATION

#### **ADDRESS**

SOUTHSIDE RD/ENTERPRISE RD HOLLISTER, CA 95023

#### **COORDINATES**

Latitude (North): 36.8189160 - 36° 49' 8.09" Longitude (West): 121.3793820 - 121° 22' 45.77"

Universal Tranverse Mercator: Zone 10 UTM X (Meters): 644546.4 UTM Y (Meters): 4075807.0

Elevation: 454 ft. above sea level

## USGS TOPOGRAPHIC MAP ASSOCIATED WITH TARGET PROPERTY

Target Property: TF

Source: U.S. Geological Survey

Target Property: E

Source: U.S. Geological Survey

#### **AERIAL PHOTOGRAPHY IN THIS REPORT**

Portions of Photo from: 20140609 Source: USDA

## MAPPED SITES SUMMARY

Target Property Address: SOUTHSIDE RD/ENTERPRISE RD HOLLISTER, CA 95023

Click on Map ID to see full detail.

| MAP<br>ID | SITE NAME            | ADDRESS              | DATABASE ACRONYMS                           | RELATIVE<br>ELEVATION | DIST (ft. & mi.)<br>DIRECTION |
|-----------|----------------------|----------------------|---|-----------------------|-------------------------------|
| 1         | ENTERPRISE WELL # 7  | 600 ENTERPRISE RD    | CUPA Listings, CERS                         | Lower                 | 361, 0.068, NE                |
| A2        | VERIZON WIRELESS HOL | 25 FRANKS DR         | CUPA Listings, CERS                         | Higher                | 844, 0.160, South             |
| A3        | AT&T MOBILITY - HILD | 25 FRANKS DR         | CUPA Listings                               | Higher                | 844, 0.160, South             |
| 4         | SEXTON TRUCKING      | 2411 PARADISE CIRCLE | RCRA NonGen / NLR                           | Lower                 | 991, 0.188, NNE               |
| B5        | K HOVNANIAN HOMES    | 3061 SOUTHSIDE RD    | RCRA NonGen / NLR                           | Lower                 | 1305, 0.247, WNW              |
| B6        | SUNNYSLOPE CWD SOUTH | 2783 SOUTHSIDE RD    | CUPA Listings, CERS                         | Lower                 | 1320, 0.250, WNW              |
| B7        | SUNNYSIDE ESTATES    | 2780 SOUTHSIDE ROAD  | ENVIROSTOR, VCP                             | Lower                 | 1326, 0.251, WNW              |
| C8        | SOUTHSIDE ROAD PROJE | 3110 SOUTHSIDE ROAD  | ENVIROSTOR, VCP                             | Lower                 | 1610, 0.305, West             |
| C9        | SOUTHSIDE ROAD PROJE | 3110 SOUTHSIDE ROAD  | US BROWNFIELDS                              | Lower                 | 1610, 0.305, West             |
| 10        | CAROLYN S HAMILTON   | 161 LADD LANE        | ENVIROSTOR, SCH, HIST UST                   | Lower                 | 3456, 0.655, NW               |
| 11        | HAZEL HAWKINS HOSPIT | 911 SUNSET DR        | LUST, AST, CERS HAZ WASTE, CERS TANKS, CUPA | . Lower               | 4232, 0.802, NNW              |

### TARGET PROPERTY SEARCH RESULTS

The target property was not listed in any of the databases searched by EDR.

#### SURROUNDING SITES: SEARCH RESULTS

Surrounding sites were identified in the following databases.

Elevations have been determined from the USGS Digital Elevation Model and should be evaluated on a relative (not an absolute) basis. Relative elevation information between sites of close proximity should be field verified. Sites with an elevation equal to or higher than the target property have been differentiated below from sites with an elevation lower than the target property.

Page numbers and map identification numbers refer to the EDR Radius Map report where detailed data on individual sites can be reviewed.

Sites listed in **bold italics** are in multiple databases.

Unmappable (orphan) sites are not considered in the foregoing analysis.

#### STANDARD ENVIRONMENTAL RECORDS

#### State- and tribal - equivalent CERCLIS

ENVIROSTOR: A review of the ENVIROSTOR list, as provided by EDR, and dated 07/29/2019 has revealed that there are 3 ENVIROSTOR sites within approximately 1 mile of the target property.

| Lower Elevation  | Address             | Direction / Distance      | Map ID | Page |
|--|---------------------|---------------------------|--------|------|
| SUNNYSIDE ESTATES Status: Active Facility ld: 60002575               | 2780 SOUTHSIDE ROAD | WNW 1/4 - 1/2 (0.251 mi.) | B7     | 9    |
| SOUTHSIDE ROAD PROJE Status: No Further Action Facility Id: 60002236 | 3110 SOUTHSIDE ROAD | W 1/4 - 1/2 (0.305 mi.)   | C8     | 9    |
| CAROL YN S HAMILTON Status: No Further Action Facility Id: 35010003  | 161 LADD LANE       | NW 1/2 - 1 (0.655 mi.)    | 10     | 10   |

#### State and tribal voluntary cleanup sites

VCP: A review of the VCP list, as provided by EDR, and dated 07/29/2019 has revealed that there are 2 VCP sites within approximately 0.5 miles of the target property.

| Lower Elevation                         | Address             | Direction / Distance      | Map ID | Page |  |
|---|---------------------|---------------------------|--------|------|--|
| SUNNYSIDE ESTATES                       | 2780 SOUTHSIDE ROAD | WNW 1/4 - 1/2 (0.251 mi.) | B7     | 9    |  |
| Status: Active<br>Facility Id: 60002575 |                     |                           |        |      |  |
| SOUTHSIDE ROAD PROJE                    | 3110 SOUTHSIDE ROAD | W 1/4 - 1/2 (0.305 mi.)   | C8     | 9    |  |

Status: No Further Action Facility Id: 60002236

#### ADDITIONAL ENVIRONMENTAL RECORDS

#### Local Brownfield lists

US BROWNFIELDS: A review of the US BROWNFIELDS list, as provided by EDR, and dated 06/03/2019 has revealed that there is 1 US BROWNFIELDS site within approximately 0.5 miles of the target property.

| Lower Elevation                                   | Address             | Direction / Distance    | Map ID | Page |  |
|---|---------------------|-------------------------|--------|------|--|
| SOUTHSIDE ROAD PROJE<br>ACRES property ID: 219288 | 3110 SOUTHSIDE ROAD | W 1/4 - 1/2 (0.305 mi.) | C9     | 9    |  |

#### Other Ascertainable Records

RCRA NonGen / NLR: A review of the RCRA NonGen / NLR list, as provided by EDR, and dated 12/16/2019 has revealed that there are 2 RCRA NonGen / NLR sites within approximately 0.25 miles of the target property.

| Lower Elevation                            | Address              | Direction / Distance      | Map ID | Page |
|--|----------------------|---------------------------|--------|------|
| SEXTON TRUCKING<br>EPA ID:: CAR000182212   | 2411 PARADISE CIRCLE | NNE 1/8 - 1/4 (0.188 mi.) | 4      | 8    |
| K HOVNANIAN HOMES<br>EPA ID:: CAC002978541 | 3061 SOUTHSIDE RD    | WNW 1/8 - 1/4 (0.247 mi.) | B5     | 8    |

CUPA Listings: A review of the CUPA Listings list, as provided by EDR, has revealed that there are 4 CUPA Listings sites within approximately 0.25 miles of the target property.

| Equal/Higher Elevation                                | Address   | Direction / Distance      | Map ID | Page |
|---|---|---------------------------|--------|------|
| VERIZON WIRELESS HOL Database: CUPA SAN BENITO, Da    | 25 FRANKS DR<br>te of Government Version: 07/16/2019      | S 1/8 - 1/4 (0.160 mi.)   | A2     | 8    |
| AT&T MOBILITY - HILD<br>Database: CUPA SAN BENITO, Da | 25 FRANKS DR<br>te of Government Version: 07/16/2019      | S 1/8 - 1/4 (0.160 mi.)   | A3     | 8    |
| Lower Elevation                                       | Address   | Direction / Distance      | Map ID | Page |
| ENTERPRISE WELL # 7 Database: CUPA SAN BENITO, Da     | 600 ENTERPRISE RD<br>te of Government Version: 07/16/2019 | NE 0 - 1/8 (0.068 mi.)    | 1      | 8    |
| SUNNYSLOPE CWD SOUTH Database: CUPA SAN BENITO, Da    | 2783 SOUTHSIDE RD te of Government Version: 07/16/2019    | WNW 1/8 - 1/4 (0.250 mi.) | B6     | 9    |

Notify 65: A review of the Notify 65 list, as provided by EDR, and dated 09/16/2019 has revealed that there is 1 Notify 65 site within approximately 1 mile of the target property.

| Lower Elevation      | Address       | Direction / Distance    | Map ID | Page |
|----------------------|---------------|-------------------------|--------|------|
| HAZEL HAWKINS HOSPIT | 911 SUNSET DR | NNW 1/2 - 1 (0.802 mi.) | 11     | 10   |

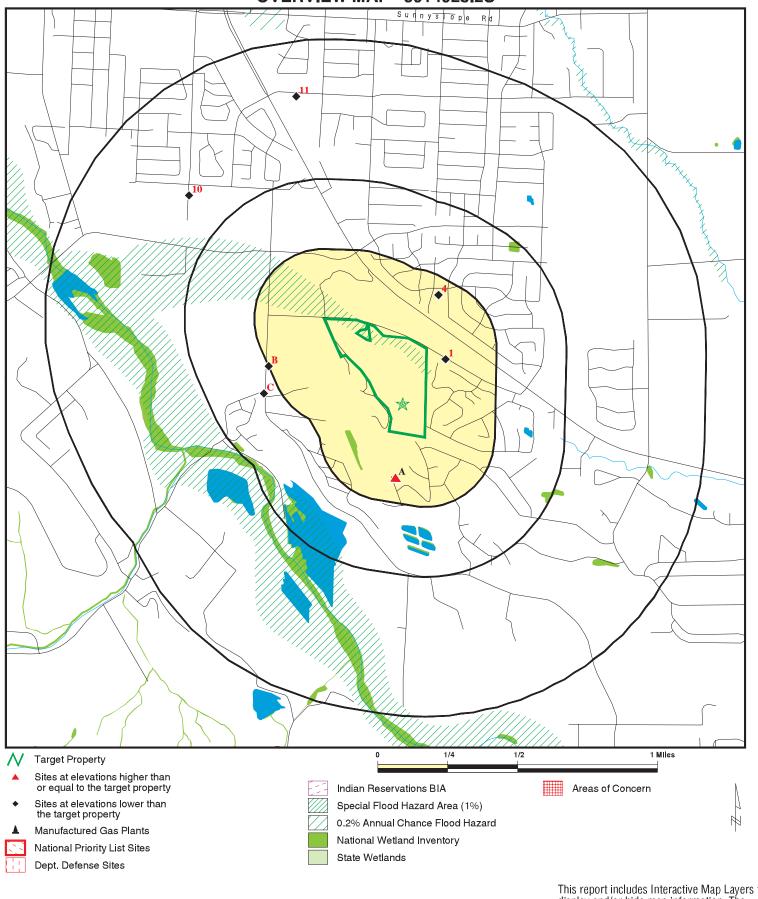
| Database(s)  |  |
|--------------|--|
| Zip          |  |
| Site Address |  |
| Site Name    |  |
| EDR ID       |  |
| City         |  |

ORPHAN SUMMARY

Count: 0 records.

NO SITES FOUND

## **OVERVIEW MAP - 5914923.2S**



This report includes Interactive Map Layers to display and/or hide map information. The legend includes only those icons for the default map view.

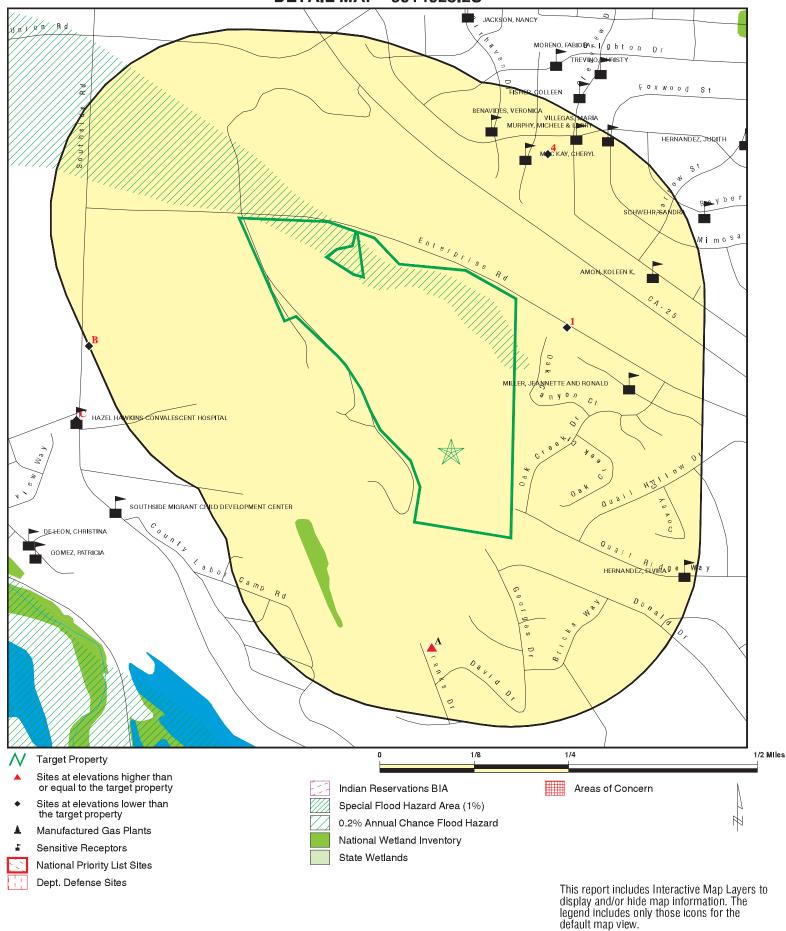
SITE NAME: Vista Del Calabria Phase I ESA ADDRESS: Southside Rd/Enterprise Rd

Hollister CA 95023 LAT/LONG: 36.818916 / 121.379382 CLIENT: CONTACT: Earth Systems Pacific, Northern CA David Teimoorian

INQUIRY#: 5914923.2s

DATE: December 30, 2019 12:27 pm

## **DETAIL MAP - 5914923.2S**



SITE NAME: Vista Del Calabria Phase I ESA
ADDRESS: Southside Rd/Enterprise Rd
Hollister CA 95023

CLIENT: Earth Systems Pacific, Northern CA
CONTACT: David Teimoorian
INQUIRY #: 5914923.2s

DATE:

LAT/LONG:

36.818916 / 121.379382

December 30, 2019 12:28 pm Copyright © 2019 EDR, Inc. © 2015 TomTom Rel. 2015.

## **MAP FINDINGS SUMMARY**

| Database  | Search<br>Distance<br>(Miles) | Target<br>Property | < 1/8       | 1/8 - 1/4   | 1/4 - 1/2      | 1/2 - 1        | > 1            | Total<br>Plotted |
|---|-------------------------------|--------------------|-------------|-------------|----------------|----------------|----------------|------------------|
| STANDARD ENVIRONMENT                                  | TAL RECORDS                   |                    |             |             |                |                |                |                  |
| Federal NPL site list                                 |                               |                    |             |             |                |                |                |                  |
| NPL<br>Proposed NPL<br>NPL LIENS                      | 1.000<br>1.000<br>1.000       |                    | 0<br>0<br>0 | 0<br>0<br>0 | 0<br>0<br>0    | 0<br>0<br>0    | NR<br>NR<br>NR | 0<br>0<br>0      |
| Federal Delisted NPL sit                              | e list                        |                    |             |             |                |                |                |                  |
| Delisted NPL  | 1.000                         |                    | 0           | 0           | 0              | 0              | NR             | 0                |
| Federal CERCLIS list                                  |                               |                    |             |             |                |                |                |                  |
| FEDERAL FACILITY<br>SEMS                              | 0.500<br>0.500                |                    | 0<br>0      | 0<br>0      | 0<br>0         | NR<br>NR       | NR<br>NR       | 0<br>0           |
| Federal CERCLIS NFRA                                  | P site list                   |                    |             |             |                |                |                |                  |
| SEMS-ARCHIVE  | 0.500                         |                    | 0           | 0           | 0              | NR             | NR             | 0                |
| Federal RCRA CORRAC                                   | TS facilities li              | st                 |             |             |                |                |                |                  |
| CORRACTS  | 1.000                         |                    | 0           | 0           | 0              | 0              | NR             | 0                |
| Federal RCRA non-COR                                  | RACTS TSD fa                  | acilities list     |             |             |                |                |                |                  |
| RCRA-TSDF   | 0.500                         |                    | 0           | 0           | 0              | NR             | NR             | 0                |
| Federal RCRA generator                                | rs list                       |                    |             |             |                |                |                |                  |
| RCRA-LQG<br>RCRA-SQG<br>RCRA-VSQG                     | 0.250<br>0.250<br>0.250       |                    | 0<br>0<br>0 | 0<br>0<br>0 | NR<br>NR<br>NR | NR<br>NR<br>NR | NR<br>NR<br>NR | 0<br>0<br>0      |
| Federal institutional con<br>engineering controls reg |                               |                    |             |             |                |                |                |                  |
| LUCIS<br>US ENG CONTROLS<br>US INST CONTROL           | 0.500<br>0.500<br>0.500       |                    | 0<br>0<br>0 | 0<br>0<br>0 | 0<br>0<br>0    | NR<br>NR<br>NR | NR<br>NR<br>NR | 0<br>0<br>0      |
| Federal ERNS list                                     |                               |                    |             |             |                |                |                |                  |
| ERNS  | 0.001                         |                    | 0           | NR          | NR             | NR             | NR             | 0                |
| State- and tribal - equiva                            | alent NPL                     |                    |             |             |                |                |                |                  |
| RESPONSE  | 1.000                         |                    | 0           | 0           | 0              | 0              | NR             | 0                |
| State- and tribal - equiva                            | alent CERCLIS                 | ;                  |             |             |                |                |                |                  |
| ENVIROSTOR  | 1.000                         |                    | 0           | 0           | 2              | 1              | NR             | 3                |
| State and tribal landfill a solid waste disposal site |                               |                    |             |             |                |                |                |                  |
| SWF/LF  | 0.500                         |                    | 0           | 0           | 0              | NR             | NR             | 0                |
| State and tribal leaking                              | storage tank l                | ists               |             |             |                |                |                |                  |
| LUST  | 0.500                         |                    | 0           | 0           | 0              | NR             | NR             | 0                |

## **MAP FINDINGS SUMMARY**

| Database   | Search<br>Distance<br>(Miles)  | Target<br>Property | < 1/8                      | 1/8 - 1/4                               | 1/4 - 1/2                                 | 1/2 - 1                                    | > 1                                    | Total<br>Plotted           |
|--|--|--------------------|----------------------------|---|---|--|--|----------------------------|
| INDIAN LUST<br>CPS-SLIC  | 0.500<br>0.500   |                    | 0                          | 0<br>0                                  | 0<br>0                                    | NR<br>NR                                   | NR<br>NR                               | 0<br>0                     |
| State and tribal registere   | d storage tar  | ık lists           |                            |   |   |  |  |                            |
| FEMA UST<br>UST<br>AST<br>INDIAN UST   | 0.250<br>0.250<br>0.250<br>0.250                                     |                    | 0<br>0<br>0<br>0           | 0<br>0<br>0<br>0                        | NR<br>NR<br>NR<br>NR                      | NR<br>NR<br>NR<br>NR                       | NR<br>NR<br>NR<br>NR                   | 0<br>0<br>0<br>0           |
| State and tribal voluntary   | cleanup site   | es                 |                            |   |   |  |  |                            |
| VCP<br>INDIAN VCP  | 0.500<br>0.500   |                    | 0                          | 0<br>0                                  | 2<br>0                                    | NR<br>NR                                   | NR<br>NR                               | 2<br>0                     |
| State and tribal Brownfie  | lds sites  |                    |                            |   |   |  |  |                            |
| BROWNFIELDS  | 0.500  |                    | 0                          | 0                                       | 0   | NR   | NR                                     | 0                          |
| ADDITIONAL ENVIRONMEN  | TAL RECORDS  | <u>3</u>           |                            |   |   |  |  |                            |
| Local Brownfield lists   |  |                    |                            |   |   |  |  |                            |
| US BROWNFIELDS   | 0.500  |                    | 0                          | 0                                       | 1   | NR   | NR                                     | 1                          |
| Local Lists of Landfill / S<br>Waste Disposal Sites                                      | olid   |                    |                            |   |   |  |  |                            |
| WMUDS/SWAT<br>SWRCY<br>HAULERS<br>INDIAN ODI<br>ODI<br>DEBRIS REGION 9<br>IHS OPEN DUMPS | 0.500<br>0.500<br>0.001<br>0.500<br>0.500<br>0.500<br>0.500          |                    | 0<br>0<br>0<br>0<br>0      | 0<br>0<br>NR<br>0<br>0<br>0             | 0<br>0<br>NR<br>0<br>0<br>0               | NR<br>NR<br>NR<br>NR<br>NR<br>NR           | NR<br>NR<br>NR<br>NR<br>NR<br>NR       | 0<br>0<br>0<br>0<br>0<br>0 |
| Local Lists of Hazardous<br>Contaminated Sites   | waste/   |                    |                            |   |   |  |  |                            |
| US HIST CDL HIST Cal-Sites SCH CDL Toxic Pits CERS HAZ WASTE US CDL PFAS                 | 0.001<br>1.000<br>0.250<br>0.001<br>1.000<br>0.250<br>0.001<br>0.500 |                    | 0<br>0<br>0<br>0<br>0<br>0 | NR<br>0<br>0<br>NR<br>0<br>0<br>NR<br>0 | NR<br>O<br>NR<br>NR<br>O<br>NR<br>NR<br>O | NR<br>0<br>NR<br>NR<br>0<br>NR<br>NR<br>NR | NR<br>NR<br>NR<br>NR<br>NR<br>NR<br>NR | 0<br>0<br>0<br>0<br>0<br>0 |
| Local Lists of Registered  | Storage Tan  | ks                 |                            |   |   |  |  |                            |
| SWEEPS UST<br>HIST UST<br>CA FID UST<br>CERS TANKS                                       | 0.250<br>0.250<br>0.250<br>0.250                                     |                    | 0<br>0<br>0                | 0<br>0<br>0<br>0                        | NR<br>NR<br>NR<br>NR                      | NR<br>NR<br>NR<br>NR                       | NR<br>NR<br>NR<br>NR                   | 0<br>0<br>0<br>0           |
| Local Land Records   |  |                    |                            |   |   |  |  |                            |
| LIENS  | 0.001  |                    | 0                          | NR                                      | NR  | NR   | NR                                     | 0                          |

# **MAP FINDINGS SUMMARY**

| Database   | Search<br>Distance<br>(Miles)   | Target<br>Property | < 1/8                                | 1/8 - 1/4   | 1/4 - 1/2   | 1/2 - 1   | > 1  | Total<br>Plotted   |
|--|---|--------------------|--------------------------------------|---|---|---|--|--|
| LIENS 2<br>DEED  | 0.001<br>0.500  |                    | 0                                    | NR<br>0   | NR<br>0   | NR<br>NR  | NR<br>NR   | 0<br>0   |
| Records of Emergency I   | Release Repo  | orts               |                                      |   |   |   |  |  |
| HMIRS<br>CHMIRS<br>LDS<br>MCS<br>SPILLS 90   | 0.001<br>0.001<br>0.001<br>0.001<br>0.001   |                    | 0<br>0<br>0<br>0                     | NR<br>NR<br>NR<br>NR<br>NR  | NR<br>NR<br>NR<br>NR<br>NR  | NR<br>NR<br>NR<br>NR<br>NR                        | NR<br>NR<br>NR<br>NR<br>NR                               | 0<br>0<br>0<br>0   |
| Other Ascertainable Rec  | ords  |                    |                                      |   |   |   |  |  |
| RCRA NonGen / NLR FUDS DOD SCRD DRYCLEANERS US FIN ASSUR EPA WATCH LIST 2020 COR ACTION TSCA TRIS SSTS ROD RMP RAATS PRP PADS ICIS FTTS MLTS COAL ASH DOE COAL ASH DOE COAL ASH EPA PCB TRANSFORMER RADINFO HIST FTTS DOT OPS CONSENT INDIAN RESERV FUSRAP UMTRA LEAD SMELTERS | 0.250 1.000 1.000 0.500 0.001 0.001 0.001 0.001 1.000 0.001 |                    |                                      | 2 0 0 0 RR ORRRORR ORRRRORR ORRRRORR ORRRR ORRRRRORR ORRRR ORRRROOO OOR | NOOORRRRRORRNNNNOORRNNNNNNNNNNNNNNNNNN                            | N O O R R R R R R O R R R R R R R R R R           | N R R R R R R R R R R R R R R R R R R R                  | 2<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0 |
| US AIRS US MINES ABANDONED MINES FINDS DOCKET HWC UXO ECHO FUELS PROGRAM CA BOND EXP. PLAN Cortese CUPA Listings   | 0.001<br>0.250<br>0.250<br>0.001<br>0.001<br>1.000<br>0.001<br>0.250<br>1.000<br>0.500<br>0.250   |                    | 0<br>0<br>0<br>0<br>0<br>0<br>0<br>0 | NR<br>0<br>0<br>NR<br>NR<br>0<br>NR<br>0<br>0<br>0                      | NR<br>NR<br>NR<br>NR<br>NR<br>NR<br>O<br>NR<br>NR<br>O<br>O<br>NR | NR<br>NR<br>NR<br>NR<br>NR<br>NR<br>O<br>NR<br>NR | NR<br>NR<br>NR<br>NR<br>NR<br>NR<br>NR<br>NR<br>NR<br>NR | 0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0  |

# **MAP FINDINGS SUMMARY**

| Database                | Search<br>Distance<br>(Miles) | Target<br>Property | < 1/8 | 1/8 - 1/4 | 1/4 - 1/2 | 1/2 - 1 | > 1  | Total<br>Plotted |
|-------------------------|-------------------------------|--------------------|-------|-----------|-----------|---------|------|------------------|
| DRYCLEANERS             | 0.250                         |                    | 0     | 0         | NR        | NR      | NR   | 0                |
| EMI                     | 0.001                         |                    | 0     | NR        | NR        | NR      | NR   | 0                |
| ENF                     | 0.001                         |                    | 0     | NR        | NR        | NR      | NR   | 0                |
| Financial Assurance     | 0.001                         |                    | 0     | NR        | NR        | NR      | NR   | 0                |
| HAZNET                  | 0.001                         |                    | Ö     | NR        | NR        | NR      | NR   | 0                |
| ICE                     | 0.001                         |                    | Ö     | NR        | NR        | NR      | NR   | Õ                |
| HIST CORTESE            | 0.500                         |                    | Ö     | 0         | 0         | NR      | NR   | Ö                |
| HWP                     | 1.000                         |                    | Ö     | Ö         | Ö         | 0       | NR   | Õ                |
| HWT                     | 0.250                         |                    | 0     | Ō         | NR        | NR      | NR   | Ō                |
| MINES                   | 0.250                         |                    | 0     | 0         | NR        | NR      | NR   | 0                |
| MWMP                    | 0.250                         |                    | 0     | 0         | NR        | NR      | NR   | 0                |
| NPDES                   | 0.001                         |                    | 0     | NR        | NR        | NR      | NR   | 0                |
| PEST LIC                | 0.001                         |                    | 0     | NR        | NR        | NR      | NR   | 0                |
| PROC                    | 0.500                         |                    | 0     | 0         | 0         | NR      | NR   | 0                |
| Notify 65               | 1.000                         |                    | 0     | 0         | 0         | 1       | NR   | 1                |
| UIC                     | 0.001                         |                    | 0     | NR        | NR        | NR      | NR   | 0                |
| UIC GEO                 | 0.001                         |                    | 0     | NR        | NR        | NR      | NR   | 0                |
| WASTEWATER PITS         | 0.500                         |                    | 0     | 0         | 0         | NR      | NR   | 0                |
| WDS                     | 0.001                         |                    | 0     | NR        | NR        | NR      | NR   | 0                |
| WIP                     | 0.250                         |                    | 0     | 0         | NR        | NR      | NR   | 0                |
| MILITARY PRIV SITES     | 0.001                         |                    | 0     | NR        | NR        | NR      | NR   | 0                |
| PROJECT                 | 0.001                         |                    | 0     | NR        | NR        | NR      | NR   | 0                |
| WDR                     | 0.001                         |                    | 0     | NR        | NR        | NR      | NR   | 0                |
| CIWQS                   | 0.001                         |                    | 0     | NR        | NR        | NR      | NR   | 0                |
| CERS                    | 0.001                         |                    | 0     | NR        | NR        | NR      | NR   | 0                |
| NON-CASE INFO           | 0.001                         |                    | 0     | NR        | NR        | NR      | NR   | 0                |
| OTHER OIL GAS           | 0.001                         |                    | 0     | NR        | NR        | NR      | NR   | 0                |
| PROD WATER PONDS        | 0.001                         |                    | 0     | NR        | NR        | NR      | NR   | 0                |
| SAMPLING POINT          | 0.001                         |                    | 0     | NR        | NR        | NR      | NR   | 0                |
| WELL STIM PROJ          | 0.001                         |                    | 0     | NR        | NR        | NR      | NR   | 0                |
| MINES MRDS              | 0.001                         |                    | 0     | NR        | NR        | NR      | NR   | 0                |
| EDR HIGH RISK HISTORICA | AL RECORDS                    |                    |       |           |           |         |      |                  |
| EDR Exclusive Records   |                               |                    |       |           |           |         |      |                  |
| EDR MGP                 | 1.000                         |                    | 0     | 0         | 0         | 0       | NR   | 0                |
| EDR Hist Auto           | 0.125                         |                    | 0     | NR        | NR        | NR      | NR   | 0                |
| EDR Hist Cleaner        | 0.125                         |                    | 0     | NR        | NR        | NR      | NR   | 0                |
| EDIT HISt Gleaner       | 0.123                         |                    | O     | INIX      | IVIX      | IVIX    | INIX | U                |
| EDR RECOVERED GOVERN    | IMENT ARCHIV                  | <u>VES</u>         |       |           |           |         |      |                  |
| Exclusive Recovered Go  | vt. Archives                  |                    |       |           |           |         |      |                  |
| RGA LF                  | 0.001                         |                    | 0     | NR        | NR        | NR      | NR   | 0                |
| RGA LUST                | 0.001                         |                    | 0     | NR        | NR        | NR      | NR   | 0                |
|                         | 0.001                         |                    | J     | 1411      | 1417      | 1411    | 1411 | J                |
| - Totals                |                               | 0                  | 1     | 5         | 5         | 2       | 0    | 13               |

## NOTES:

TP = Target Property

NR = Not Requested at this Search Distance

Sites may be listed in more than one database

Map ID MAP FINDINGS

Direction Distance

**EDR ID Number** Database(s) Elevation Site **EPA ID Number** 

**ENTERPRISE WELL #7 CUPA Listings** S120050442 NE **600 ENTERPRISE RD CERS** N/A

HOLLISTER, CA 95023 < 1/8 0.068 mi.

361 ft.

Click here for full text details

Relative: Lower

**CUPA Listings A2 VERIZON WIRELESS HOLLISTER SOUTH** S120050465 **CERS** N/A

South 25 FRANKS DR 1/8-1/4 HOLLISTER, CA 95023

0.160 mi. 844 ft.

Relative:

Click here for full text details

Higher

А3 **AT&T MOBILITY - HILDEN HILLTOP (51620) CUPA Listings** S120050195 N/A

South 25 FRANKS DR 1/8-1/4 HOLLISTER, CA

0.160 mi. 844 ft.

Click here for full text details

Relative: Higher

**SEXTON TRUCKING** RCRA NonGen / NLR 1010314115

NNE **2411 PARADISE CIRCLE** 1/8-1/4 HOLLISTER, CA 95023

0.188 mi. 991 ft.

Click here for full text details Relative:

Lower

**RCRA NonGen / NLR** EPA Id CAR000182212

**B5** K HOVNANIAN HOMES RCRA NonGen / NLR 1024758696

WNW 3061 SOUTHSIDE RD 1/8-1/4 HOLLISTER, CA 95023

0.247 mi. 1305 ft.

Click here for full text details

Relative: Lower

RCRA NonGen / NLR

EPA Id CAC002978541

CAR000182212

CAC002978541

MAP FINDINGS Map ID

Direction Distance

**EDR ID Number** Elevation Site Database(s) **EPA ID Number** 

**B6** SUNNYSLOPE CWD SOUTHSIDE WELL #11 WNW

**CUPA Listings** S120984096 **2783 SOUTHSIDE RD CERS** N/A

1/8-1/4 HOLLISTER, CA 95023 0.250 mi.

1320 ft.

Click here for full text details

Relative: Lower

**B7 SUNNYSIDE ESTATES ENVIROSTOR** S121475148 WNW **2780 SOUTHSIDE ROAD VCP** N/A

1/4-1/2 HOLLISTER, CA 95023 0.251 mi. 1326 ft.

Click here for full text details

Relative: Lower

**ENVIROSTOR** Status Active Facility Id 60002575

**VCP** 

Facility Id 60002575 Status Active

C8 **SOUTHSIDE ROAD PROJECT AREA ENVIROSTOR** S118353722 **VCP** N/A

West 3110 SOUTHSIDE ROAD 1/4-1/2 HOLLISTER, CA 95023

0.305 mi. 1610 ft.

Click here for full text details

Relative: Lower

**ENVIROSTOR** 

Status No Further Action Facility Id 60002236

**VCP** 

Facility Id 60002236 Status No Further Action

1019322169 C9 SOUTHSIDE ROAD PROJECT AREA - COUNTY OF SAN BENITO **US BROWNFIELDS** West 3110 SOUTHSIDE ROAD N/A

1/4-1/2 HOLLISTER, CA 95023 0.305 mi.

1610 ft.

Click here for full text details

Relative: Lower

**US BROWNFIELDS** 

ACRES property ID 219288

Map ID MAP FINDINGS

Direction Distance

**EDR ID Number** Elevation Site Database(s) **EPA ID Number** 

10 **CAROLYN S HAMILTON ENVIROSTOR** S107736581 NW **161 LADD LANE** SCH N/A

1/2-1 HOLLISTER, CA 95023 0.655 mi.

3456 ft.

Click here for full text details

Relative: Lower

**ENVIROSTOR** 

Status No Further Action Facility Id 35010003

SCH

Facility Id 35010003 Status No Further Action

**HAZEL HAWKINS HOSPITAL** LUST S100231923 11 **AST** N/A

NNW 911 SUNSET DR 1/2-1 HOLLISTER, CA 95023

0.802 mi. 4232 ft.

Click here for full text details Relative: Lower

Notify 65 **CIWQS CERS** 

LUST

Status Case Closed Status Completed - Case Closed Global Id T0606900020 Global ID T0606900020

HIST CORTESE

Reg Id 61

**HIST UST** 

**CERS HAZ WASTE** 

**CERS TANKS** 

**CUPA Listings** HIST CORTESE

**NPDES** 

| St | Acronym                   | Full Name  | Government Agency                             | Gov Date   | Arvl. Date | Active Date |
|----|---------------------------|--|---|------------|------------|-------------|
| CA | AST                       | Aboveground Petroleum Storage Tank Facilities                | California Environmental Protection Agency    | 07/06/2016 | 07/12/2016 | 09/19/2016  |
| CA | BROWNFIELDS               | Considered Brownfieds Sites Listing                          | State Water Resources Control Board           | 09/23/2019 | 09/24/2019 | 11/06/2019  |
| CA | CA BOND EXP. PLAN         | Bond Expenditure Plan  | Department of Health Services                 | 01/01/1989 | 07/27/1994 | 08/02/1994  |
| CA | CA FID UST                | Facility Inventory Database                                  | California Environmental Protection Agency    | 10/31/1994 | 09/05/1995 | 09/29/1995  |
| CA | CDL                       | Clandestine Drug Labs  | Department of Toxic Substances Control        | 06/30/2018 | 07/16/2019 | 09/24/2019  |
| CA | CERS                      | CalEPA Regulated Site Portal Data                            | California Environmental Protection Agency    | 08/14/2019 | 08/14/2019 | 08/21/2019  |
| CA | CERS HAZ WASTE            | CERS HAZ WASTE   | CalEPA  | 08/14/2019 | 08/14/2019 | 08/21/2019  |
| CA | CERS TANKS                | California Environmental Reporting System (CERS) Tanks       | California Environmental Protection Agency    | 08/14/2019 | 08/14/2019 | 08/21/2019  |
| CA | CHMIRS                    | California Hazardous Material Incident Report System         | Office of Emergency Services                  | 05/15/2019 | 06/24/2019 | 08/21/2019  |
| CA | CIWQS                     | California Integrated Water Quality System                   | State Water Resources Control Board           | 09/03/2019 | 09/04/2019 | 11/05/2019  |
| CA | CORTESE                   | "Cortese" Hazardous Waste & Substances Sites List            | CAL EPA/Office of Emergency Information       | 09/23/2019 | 09/24/2019 | 11/06/2019  |
| CA | CPS-SLIC                  | Statewide SLIC Cases (GEOTRACKER)                            | State Water Resources Control Board           | 09/09/2019 | 09/09/2019 | 11/06/2019  |
| CA | CUPA LIVERMORE-PLEASANTON | I CUPA Facility Listing                                      | Livermore-Pleasanton Fire Department          | 05/01/2019 | 05/14/2019 | 07/17/2019  |
| CA | CUPA SAN FRANCISCO CO     | CUPA Facility Listing  | San Francisco County Department of Environmen | 10/31/2019 | 11/01/2019 | 12/11/2019  |
| CA | DEED                      | Deed Restriction Listing                                     | DTSC and SWRCB                                | 09/03/2019 | 09/04/2019 | 11/05/2019  |
| CA | DRYCLEAN AVAQMD           | Antelope Valley Air Quality Management District Drycleaner L | Antelope Valley Air Quality Management Distri | 08/28/2019 | 08/30/2019 | 10/29/2019  |
| CA | DRYCLEAN SOUTH COAST      | South Coast Air Quality Management District Drycleaner Listi | South Coast Air Quality Management District   | 09/27/2019 | 10/01/2019 | 11/07/2019  |
| CA | DRYCLEANERS               | Cleaner Facilities   | Department of Toxic Substance Control         | 09/06/2019 | 10/11/2019 | 12/12/2019  |
| CA | EMI                       | Emissions Inventory Data                                     | California Air Resources Board                | 12/31/2017 | 06/24/2019 | 08/22/2019  |
| CA | ENF                       | Enforcement Action Listing                                   | State Water Resoruces Control Board           | 07/19/2019 | 07/22/2019 | 09/26/2019  |
| CA | ENVIROSTOR                | EnviroStor Database  | Department of Toxic Substances Control        | 07/29/2019 | 07/31/2019 | 10/08/2019  |
| CA | Financial Assurance 1     | Financial Assurance Information Listing                      | Department of Toxic Substances Control        | 07/19/2019 | 07/23/2019 | 09/30/2019  |
| CA | Financial Assurance 2     | Financial Assurance Information Listing                      | California Integrated Waste Management Board  | 08/16/2019 | 08/20/2019 | 10/18/2019  |
| CA | HAULERS                   | Registered Waste Tire Haulers Listing                        | Integrated Waste Management Board             | 03/26/2019 | 03/27/2019 | 04/30/2019  |
| CA | HAZNET                    | Facility and Manifest Data                                   | California Environmental Protection Agency    | 12/31/2017 | 05/29/2019 | 07/22/2019  |
| CA | HIST CAL-SITES            | Calsites Database  | Department of Toxic Substance Control         | 08/08/2005 | 08/03/2006 | 08/24/2006  |
| CA | HIST CORTESE              | Hazardous Waste & Substance Site List                        | Department of Toxic Substances Control        | 04/01/2001 | 01/22/2009 | 04/08/2009  |
| CA | HIST UST                  | Hazardous Substance Storage Container Database               | State Water Resources Control Board           | 10/15/1990 | 01/25/1991 | 02/12/1991  |
| CA | HWP                       | EnviroStor Permitted Facilities Listing                      | Department of Toxic Substances Control        | 08/19/2019 | 08/20/2019 | 10/18/2019  |
| CA | HWT                       | Registered Hazardous Waste Transporter Database              | Department of Toxic Substances Control        | 10/07/2019 | 10/08/2019 | 11/07/2019  |
| CA | ICE                       | ICE  | Department of Toxic Subsances Control         | 08/19/2019 | 08/20/2019 | 10/18/2019  |
| CA | LDS                       | Land Disposal Sites Listing (GEOTRACKER)                     | State Water Quality Control Board             | 09/09/2019 | 09/09/2019 | 11/05/2019  |
| CA | LIENS                     | Environmental Liens Listing                                  | Department of Toxic Substances Control        | 08/29/2019 | 08/30/2019 | 10/29/2019  |
| CA | LUST                      | Leaking Underground Fuel Tank Report (GEOTRACKER)            | State Water Resources Control Board           | 09/09/2019 | 09/09/2019 | 10/31/2019  |
| CA | LUST REG 1                | Active Toxic Site Investigation                              | California Regional Water Quality Control Boa | 02/01/2001 | 02/28/2001 | 03/29/2001  |
| -  | LUST REG 2                | Fuel Leak List   | California Regional Water Quality Control Boa | 09/30/2004 | 10/20/2004 | 11/19/2004  |
|    | LUST REG 3                | Leaking Underground Storage Tank Database                    | California Regional Water Quality Control Boa | 05/19/2003 | 05/19/2003 | 06/02/2003  |
|    | LUST REG 4                | Underground Storage Tank Leak List                           | California Regional Water Quality Control Boa | 09/07/2004 | 09/07/2004 | 10/12/2004  |
| -  | LUST REG 5                | Leaking Underground Storage Tank Database                    | California Regional Water Quality Control Boa | 07/01/2008 | 07/22/2008 | 07/31/2008  |
|    | LUST REG 6L               | Leaking Underground Storage Tank Case Listing                | California Regional Water Quality Control Boa | 09/09/2003 | 09/10/2003 | 10/07/2003  |
|    | LUST REG 6V               | Leaking Underground Storage Tank Case Listing                | California Regional Water Quality Control Boa | 06/07/2005 | 06/07/2005 | 06/29/2005  |
|    | LUST REG 7                | Leaking Underground Storage Tank Case Listing                | California Regional Water Quality Control Boa | 02/26/2004 | 02/26/2004 | 03/24/2004  |
|    | LUST REG 8                | Leaking Underground Storage Tanks                            | California Regional Water Quality Control Boa | 02/14/2005 | 02/15/2005 | 03/28/2005  |
|    | LUST REG 9                | Leaking Underground Storage Tank Report                      | California Regional Water Quality Control Boa | 03/01/2001 | 04/23/2001 | 05/21/2001  |
|    | MCS                       | Military Cleanup Sites Listing (GEOTRACKER)                  | State Water Resources Control Board           | 09/09/2019 | 09/09/2019 | 11/05/2019  |
| CA | MILITARY PRIV SITES       | Military Privatized Sites (GEOTRACKER)                       | State Water Resources Control Board           | 09/09/2019 | 09/09/2019 | 11/01/2019  |
| CA | MILITARY UST SITES        | Military UST Sites (GEOTRACKER)                              | State Water Resources Control Board           | 09/09/2019 |            | 11/01/2019  |
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| St | Acronym           | Full Name  | Government Agency                             | Gov Date   | Arvl. Date | Active Date |
|----|-------------------|--|---|------------|------------|-------------|
| CA | ,                 | Mines Site Location Listing                                  | Department of Conservation                    | 09/09/2019 | 09/09/2019 | 11/05/2019  |
| CA | MWMP              | Medical Waste Management Program Listing                     | Department of Public Health                   | 07/19/2019 | 09/04/2019 | 11/05/2019  |
| CA | NON-CASE INFO     | Non-Case Information Sites (GEOTRACKER)                      | State Water Resources Control Board           | 09/09/2019 | 09/09/2019 | 11/01/2019  |
| CA | NOTIFY 65         | Proposition 65 Records                                       | State Water Resources Control Board           | 09/16/2019 | 09/18/2019 | 11/06/2019  |
| CA | NPDES             | NPDES Permits Listing  | State Water Resources Control Board           | 08/12/2019 | 08/13/2019 | 10/16/2019  |
| CA | OTHER OIL GAS     | Other Oil & Gas Projects Sites (GEOTRACKER)                  | State Water Resources Control Board           | 09/09/2019 | 09/09/2019 | 11/01/2019  |
| CA | PEST LIC          | Pesticide Regulation Licenses Listing                        | Department of Pesticide Regulation            | 09/03/2019 | 09/04/2019 | 11/05/2019  |
| CA | PFAS              | PFAS Contamination Site Location Listing                     | State Water Resources Control Board           | 09/09/2019 | 09/09/2019 | 11/05/2019  |
| CA | PROC              | Certified Processors Database                                | Department of Conservation                    | 09/09/2019 | 09/09/2019 | 11/05/2019  |
| CA | PROD WATER PONDS  | Produced Water Ponds Sites (GEOTRACKER)                      | State Water Resources Control Board           | 09/09/2019 | 09/09/2019 | 11/01/2019  |
| CA | PROJECT           | Project Sites (GEOTRACKER)                                   | State Water Resources Control Board           | 09/09/2019 | 09/09/2019 | 11/01/2019  |
| CA | RESPONSE          | State Response Sites   | Department of Toxic Substances Control        | 07/29/2019 | 07/31/2019 | 10/08/2019  |
| CA | RGA LF            | Recovered Government Archive Solid Waste Facilities List     | Department of Resources Recycling and Recover | 0.720720.0 | 07/01/2013 | 01/13/2014  |
| CA | RGA LUST          | Recovered Government Archive Leaking Underground Storage Tan | State Water Resources Control Board           |            | 07/01/2013 | 12/30/2013  |
| CA | SAMPLING POINT    | Sampling Point ? Public Sites (GEOTRACKER)                   | State Water Resources Control Board           | 09/09/2019 | 09/09/2019 | 11/01/2019  |
| CA | SAN FRANCISCO AST | Aboveground Storage Tank Site Listing                        | San Francisco County Department of Public Hea | 08/01/2019 | 08/02/2019 | 10/11/2019  |
| CA | SCH               | School Property Evaluation Program                           | Department of Toxic Substances Control        | 07/29/2019 | 07/31/2019 | 10/08/2019  |
| CA | SLIC REG 1        | Active Toxic Site Investigations                             | California Regional Water Quality Control Boa | 04/03/2003 | 04/07/2003 | 04/25/2003  |
| CA | SLIC REG 2        | Spills, Leaks, Investigation & Cleanup Cost Recovery Listing | Regional Water Quality Control Board San Fran | 09/30/2004 | 10/20/2004 | 11/19/2004  |
|    | SLIC REG 3        | Spills, Leaks, Investigation & Cleanup Cost Recovery Listing | California Regional Water Quality Control Boa | 05/18/2006 | 05/18/2006 | 06/15/2006  |
| CA | SLIC REG 4        | Spills, Leaks, Investigation & Cleanup Cost Recovery Listing | Region Water Quality Control Board Los Angele | 11/17/2004 | 11/18/2004 | 01/04/2005  |
|    | SLIC REG 5        | Spills, Leaks, Investigation & Cleanup Cost Recovery Listing | Regional Water Quality Control Board Central  | 04/01/2005 | 04/05/2005 | 04/21/2005  |
| CA | SLIC REG 6L       | SLIC Sites   | California Regional Water Quality Control Boa | 09/07/2004 | 09/07/2004 | 10/12/2004  |
| -  |                   | Spills, Leaks, Investigation & Cleanup Cost Recovery Listing | Regional Water Quality Control Board, Victory | 05/24/2005 | 05/25/2005 | 06/16/2005  |
| CA | SLIC REG 7        | SLIC List  | California Regional Quality Control Board, Co | 11/24/2004 | 11/29/2004 | 01/04/2005  |
| CA | SLIC REG 8        | Spills, Leaks, Investigation & Cleanup Cost Recovery Listing | California Region Water Quality Control Board | 04/03/2008 | 04/03/2008 | 04/14/2008  |
| CA | SLIC REG 9        | Spills, Leaks, Investigation & Cleanup Cost Recovery Listing | California Regional Water Quality Control Boa | 09/10/2007 | 09/11/2007 | 09/28/2007  |
| CA | SPILLS 90         | SPILLS90 data from FirstSearch                               | FirstSearch                                   | 06/06/2012 | 01/03/2013 | 02/22/2013  |
| CA | SWEEPS UST        | SWEEPS UST Listing   | State Water Resources Control Board           | 06/01/1994 | 07/07/2005 | 08/11/2005  |
| CA | SWF/LF (SWIS)     | Solid Waste Information System                               | Department of Resources Recycling and Recover | 08/12/2019 | 08/13/2019 | 10/09/2019  |
| CA | SWRCY             | Recycler Database  | Department of Conservation                    | 09/09/2019 | 09/09/2019 | 11/07/2019  |
| CA | TOXIC PITS        | Toxic Pits Cleanup Act Sites                                 | State Water Resources Control Board           | 07/01/1995 | 08/30/1995 | 09/26/1995  |
| CA | UIC               | UIC Listing  | Deaprtment of Conservation                    | 08/20/2019 | 08/20/2019 | 11/18/2019  |
| CA | UIC GEO           | Underground Injection Control Sites (GEOTRACKER)             | State Water Resource Control Board            | 09/09/2019 | 09/09/2019 | 11/01/2019  |
| CA | UST               | Active UST Facilities  | SWRCB   | 09/09/2019 | 09/09/2019 | 10/31/2019  |
| CA | UST CLOSURE       | Proposed Closure of Underground Storage Tank (UST) Cases     | State Water Resources Control Board           | 09/06/2019 | 09/09/2019 | 10/31/2019  |
| CA | UST MENDOCINO     | Mendocino County UST Database                                | Department of Public Health                   | 08/20/2019 | 09/09/2019 | 10/31/2019  |
| CA | VCP               | Voluntary Cleanup Program Properties                         | Department of Toxic Substances Control        | 07/29/2019 | 07/31/2019 | 10/08/2019  |
| CA | WASTEWATER PITS   | Oil Wastewater Pits Listing                                  | RWQCB, Central Valley Region                  | 05/08/2018 | 07/11/2018 | 09/13/2018  |
| CA | WDR               | Waste Discharge Requirements Listing                         | State Water Resources Control Board           | 09/09/2019 | 09/09/2019 | 11/06/2019  |
| CA | WDS               | Waste Discharge System                                       | State Water Resources Control Board           | 06/19/2007 | 06/20/2007 | 06/29/2007  |
| CA | WELL STIM PROJ    | Well Stimulation Project (GEOTRACKER)                        | State Water Resources Control Board           | 09/09/2019 | 09/09/2019 | 11/01/2019  |
| CA |                   | Well Investigation Program Case List                         | Los Angeles Water Quality Control Board       | 07/03/2009 | 07/21/2009 | 08/03/2009  |
| CA | WMUDS/SWAT        | Waste Management Unit Database                               | State Water Resources Control Board           | 04/01/2000 | 04/10/2000 | 05/10/2000  |
| US | 2020 COR ACTION   | 2020 Corrective Action Program List                          | Environmental Protection Agency               | 09/30/2017 | 05/08/2018 | 07/20/2018  |
| US | ABANDONED MINES   | Abandoned Mines  | Department of Interior                        | 09/10/2019 | 09/10/2019 | 10/17/2019  |
| US | BRS               | Biennial Reporting System                                    | EPA/NTIS                                      | 12/31/2015 | 02/22/2017 | 09/28/2017  |
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| St | Acronym          | Full Name  | Government Agency                             | Gov Date   | Arvl. Date | Active Date     |
|----|------------------|--|---|------------|------------|-----------------|
| US | COAL ASH DOE     | Steam-Electric Plant Operation Data                          | Department of Energy                          | 12/31/2005 | 08/07/2009 | 10/22/2009      |
| US | COAL ASH EPA     | Coal Combustion Residues Surface Impoundments List           | Environmental Protection Agency               | 01/12/2017 | 03/05/2019 | 11/11/2019      |
| US | CONSENT          | Superfund (CERCLA) Consent Decrees                           | Department of Justice, Consent Decree Library | 09/30/2019 | 10/09/2019 | 12/20/2019      |
| US | CORRACTS         | Corrective Action Report                                     | EPA   | 12/16/2019 | 12/16/2019 | 12/20/2019      |
| US | DEBRIS REGION 9  | Torres Martinez Reservation Illegal Dump Site Locations      | EPA, Region 9                                 | 01/12/2009 | 05/07/2009 | 09/21/2009      |
| US | DOCKET HWC       | Hazardous Waste Compliance Docket Listing                    | Environmental Protection Agency               | 05/31/2018 | 07/26/2018 | 10/05/2018      |
| US | DOD              | Department of Defense Sites                                  | USGS  | 12/31/2005 | 11/10/2006 | 01/11/2007      |
| US | DOT OPS          | Incident and Accident Data                                   | Department of Transporation, Office of Pipeli | 07/01/2019 | 07/31/2019 | 10/24/2019      |
| US | Delisted NPL     | National Priority List Deletions                             | EPA   | 10/25/2019 | 11/07/2019 | 11/20/2019      |
| US | ECHO             | Enforcement & Compliance History Information                 | Environmental Protection Agency               | 07/06/2019 | 07/09/2019 | 10/02/2019      |
| US | EDR Hist Auto    | EDR Exclusive Historical Auto Stations                       | EDR. Inc.                                     | 0.700,20.0 | 0.700720.0 | . 0, 02, 20 . 0 |
| US | EDR Hist Cleaner | EDR Exclusive Historical Cleaners                            | EDR, Inc.                                     |            |            |                 |
| US | EDR MGP          | EDR Proprietary Manufactured Gas Plants                      | EDR, Inc.                                     |            |            |                 |
| US | EPA WATCH LIST   | EPA WATCH LIST   | Environmental Protection Agency               | 08/30/2013 | 03/21/2014 | 06/17/2014      |
| US | ERNS             | Emergency Response Notification System                       | National Response Center, United States Coast | 09/09/2019 | 09/09/2019 | 09/23/2019      |
| US | FEDERAL FACILITY | Federal Facility Site Information listing                    | Environmental Protection Agency               | 04/03/2019 | 04/05/2019 | 05/14/2019      |
| US | FEDLAND          | Federal and Indian Lands                                     | U.S. Geological Survey                        | 04/02/2018 | 04/11/2018 | 11/06/2019      |
| US | FEMA UST         | Underground Storage Tank Listing                             | FEMA  | 08/27/2019 | 08/28/2019 | 11/11/2019      |
| US | FINDS            | Facility Index System/Facility Registry System               | EPA   | 08/12/2019 | 09/04/2019 | 12/03/2019      |
| US | FTTS             | FIFRA/ TSCA Tracking System - FIFRA (Federal Insecticide, Fu | EPA/Office of Prevention, Pesticides and Toxi | 04/09/2009 | 04/16/2009 | 05/11/2009      |
| US | FTTS INSP        | FIFRA/ TSCA Tracking System - FIFRA (Federal Insecticide, Fu | EPA   | 04/09/2009 | 04/16/2009 | 05/11/2009      |
| US | FUDS             | Formerly Used Defense Sites                                  | U.S. Army Corps of Engineers                  | 05/15/2019 | 05/21/2019 | 08/08/2019      |
| US | FUELS PROGRAM    | EPA Fuels Program Registered Listing                         | EPA   | 08/19/2019 | 08/20/2019 | 11/11/2019      |
|    | FUSRAP           | Formerly Utilized Sites Remedial Action Program              | Department of Energy                          | 08/08/2017 | 09/11/2018 | 09/14/2018      |
| US | HIST FTTS        | FIFRA/TSCA Tracking System Administrative Case Listing       | Environmental Protection Agency               | 10/19/2006 | 03/01/2007 | 04/10/2007      |
| US | HIST FTTS INSP   | FIFRA/TSCA Tracking System Inspection & Enforcement Case Lis | Environmental Protection Agency               | 10/19/2006 | 03/01/2007 | 04/10/2007      |
| US | HMIRS            | Hazardous Materials Information Reporting System             | U.S. Department of Transportation             | 06/24/2019 | 06/26/2019 | 09/23/2019      |
| US | ICIS             | Integrated Compliance Information System                     | Environmental Protection Agency               | 11/18/2016 | 11/23/2016 | 02/10/2017      |
| US | IHS OPEN DUMPS   | Open Dumps on Indian Land                                    | Department of Health & Human Serivces, Indian | 04/01/2014 | 08/06/2014 | 01/29/2015      |
| US | INDIAN LUST R1   | Leaking Underground Storage Tanks on Indian Land             | EPA Region 1                                  | 04/11/2019 | 07/29/2019 | 10/17/2019      |
| US | INDIAN LUST R10  | Leaking Underground Storage Tanks on Indian Land             | EPA Region 10                                 | 04/16/2019 | 07/29/2019 | 10/17/2019      |
| US | INDIAN LUST R4   | Leaking Underground Storage Tanks on Indian Land             | EPA Region 4                                  | 04/12/2019 | 07/29/2019 | 10/17/2019      |
| US | INDIAN LUST R5   | Leaking Underground Storage Tanks on Indian Land             | EPA, Region 5                                 | 04/08/2019 | 07/30/2019 | 10/17/2019      |
| US | INDIAN LUST R6   | Leaking Underground Storage Tanks on Indian Land             | EPA Region 6                                  | 05/01/2019 | 07/29/2019 | 10/17/2019      |
| US | INDIAN LUST R7   | Leaking Underground Storage Tanks on Indian Land             | EPA Region 7                                  | 07/02/2019 | 10/16/2019 | 10/24/2019      |
| US | INDIAN LUST R8   | Leaking Underground Storage Tanks on Indian Land             | EPA Region 8                                  | 05/02/2019 | 10/22/2019 | 11/11/2019      |
| US | INDIAN LUST R9   | Leaking Underground Storage Tanks on Indian Land             | Environmental Protection Agency               | 04/08/2019 | 07/29/2019 | 10/17/2019      |
| US | INDIAN ODI       | Report on the Status of Open Dumps on Indian Lands           | Environmental Protection Agency               | 12/31/1998 | 12/03/2007 | 01/24/2008      |
| US | INDIAN RESERV    | Indian Reservations  | USGS  | 12/31/1990 | 07/14/2015 | 01/10/2017      |
| US | INDIAN UST R1    | Underground Storage Tanks on Indian Land                     | EPA, Region 1                                 | 04/11/2019 | 07/30/2019 | 10/17/2019      |
| US | INDIAN UST R10   | Underground Storage Tanks on Indian Land                     | EPA Region 10                                 | 04/16/2019 | 07/30/2019 | 10/17/2019      |
| US | INDIAN UST R4    | Underground Storage Tanks on Indian Land                     | EPA Region 4                                  | 04/12/2019 | 07/29/2019 | 10/17/2019      |
| US | INDIAN UST R5    | Underground Storage Tanks on Indian Land                     | EPA Region 5                                  | 04/08/2019 | 07/29/2019 | 10/17/2019      |
| US | INDIAN UST R6    | Underground Storage Tanks on Indian Land                     | EPA Region 6                                  | 05/01/2019 | 07/29/2019 | 10/17/2019      |
| US | INDIAN UST R7    | Underground Storage Tanks on Indian Land                     | EPA Region 7                                  | 05/02/2019 | 07/29/2019 | 10/17/2019      |
| US | INDIAN UST R8    | Underground Storage Tanks on Indian Land                     | EPA Region 8                                  | 05/02/2019 | 10/22/2019 | 11/11/2019      |
| US | INDIAN UST R9    | Underground Storage Tanks on Indian Land                     | EPA Region 9                                  | 04/08/2019 | 07/29/2019 | 10/17/2019      |
| 03 | HADIVIA OOT IVA  | Onderground Storage Tanks on Indian Land                     | LI A Negion 3                                 | 04/00/2019 | 01/23/2019 | 10/11/2018      |

| St | Acronym           | Full Name  | Government Agency                             | Gov Date   | Arvl. Date | Active Date |
|----|-------------------|--|---|------------|------------|-------------|
| US | INDIAN VCP R1     | Voluntary Cleanup Priority Listing                           | EPA, Region 1                                 | 07/27/2015 | 09/29/2015 | 02/18/2016  |
| US | INDIAN VCP R7     | Voluntary Cleanup Priority Lisitng                           | EPA, Region 7                                 | 03/20/2008 | 04/22/2008 | 05/19/2008  |
| US | LEAD SMELTER 1    | Lead Smelter Sites   | Environmental Protection Agency               | 10/25/2019 | 11/07/2019 | 11/20/2019  |
| US | LEAD SMELTER 2    | Lead Smelter Sites   | American Journal of Public Health             | 04/05/2001 | 10/27/2010 | 12/02/2010  |
| US | LIENS 2           | CERCLA Lien Information                                      | Environmental Protection Agency               | 10/25/2019 | 11/07/2019 | 11/20/2019  |
| US | LUCIS             | Land Use Control Information System                          | Department of the Navy                        | 08/13/2019 | 08/20/2019 | 08/26/2019  |
| US | MINES MRDS        | Mineral Resources Data System                                | USGS  | 04/06/2018 | 10/21/2019 | 10/24/2019  |
| US | MINES VIOLATIONS  | MSHA Violation Assessment Data                               | DOL, Mine Safety & Health Admi                | 09/17/2019 | 09/18/2019 | 12/03/2019  |
| US | MLTS              | Material Licensing Tracking System                           | Nuclear Regulatory Commission                 | 06/20/2019 | 06/20/2019 | 08/08/2019  |
| US | NPL               | National Priority List                                       | EPA   | 10/25/2019 | 11/07/2019 | 11/20/2019  |
| US | NPL LIENS         | Federal Superfund Liens                                      | EPA   | 10/15/1991 | 02/02/1994 | 03/30/1994  |
| US | ODI               | Open Dump Inventory  | Environmental Protection Agency               | 06/30/1985 | 08/09/2004 | 09/17/2004  |
| US | PADS              | PCB Activity Database System                                 | EPA   | 10/09/2019 | 10/11/2019 | 12/20/2019  |
| US | PCB TRANSFORMER   | PCB Transformer Registration Database                        | Environmental Protection Agency               | 05/24/2017 | 11/30/2017 | 12/15/2017  |
| US | PRP               | Potentially Responsible Parties                              | EPA   | 10/25/2019 | 11/07/2019 | 11/21/2019  |
| US | Proposed NPL      | Proposed National Priority List Sites                        | EPA   | 10/25/2019 | 11/07/2019 | 11/20/2019  |
| US | RAATS             | RCRA Administrative Action Tracking System                   | EPA   | 04/17/1995 | 07/03/1995 | 08/07/1995  |
| US | RADINFO           | Radiation Information Database                               | Environmental Protection Agency               | 07/01/2019 | 07/01/2019 | 09/23/2019  |
| US | RCRA NonGen / NLR | RCRA - Non Generators / No Longer Regulated                  | Environmental Protection Agency               | 12/16/2019 | 12/16/2019 | 12/20/2019  |
| US | RCRA-LQG          | RCRA - Large Quantity Generators                             | Environmental Protection Agency               | 12/16/2019 | 12/16/2019 | 12/20/2019  |
| US | RCRA-SQG          | RCRA - Small Quantity Generators                             | Environmental Protection Agency               | 12/16/2019 | 12/16/2019 | 12/20/2019  |
| US | RCRA-TSDF         | RCRA - Treatment, Storage and Disposal                       | Environmental Protection Agency               | 12/16/2019 | 12/16/2019 | 12/20/2019  |
| US | RCRA-VSQG         | RCRA - Very Small Quantity Generators (Formerly Conditionall | Environmental Protection Agency               | 12/16/2019 | 12/16/2019 | 12/20/2019  |
| US | RMP               | Risk Management Plans  | Environmental Protection Agency               | 04/25/2019 | 05/02/2019 | 05/23/2019  |
| US | ROD               | Records Of Decision  | EPA   | 10/25/2019 | 11/07/2019 | 11/20/2019  |
| US | SCRD DRYCLEANERS  | State Coalition for Remediation of Drycleaners Listing       | Environmental Protection Agency               | 01/01/2017 | 02/03/2017 | 04/07/2017  |
| US | SEMS              | Superfund Enterprise Management System                       | EPA   | 10/25/2019 | 11/07/2019 | 11/21/2019  |
| US | SEMS-ARCHIVE      | Superfund Enterprise Management System Archive               | EPA   | 10/25/2019 | 11/07/2019 | 11/21/2019  |
| US | SSTS              | Section 7 Tracking Systems                                   | EPA   | 09/30/2018 | 04/24/2019 | 08/08/2019  |
| US | TRIS              | Toxic Chemical Release Inventory System                      | EPA   | 12/31/2017 | 11/16/2018 | 11/21/2019  |
| US | TSCA              | Toxic Substances Control Act                                 | EPA   | 12/31/2016 | 06/21/2017 | 01/05/2018  |
| US | UMTRA             | Uranium Mill Tailings Sites                                  | Department of Energy                          | 08/01/2019 | 08/21/2019 | 11/11/2019  |
| US | US AIRS (AFS)     | Aerometric Information Retrieval System Facility Subsystem ( | EPA   | 10/12/2016 | 10/26/2016 | 02/03/2017  |
| US | US AIRS MINOR     | Air Facility System Data                                     | EPA   | 10/12/2016 | 10/26/2016 | 02/03/2017  |
| US | US BROWNFIELDS    | A Listing of Brownfields Sites                               | Environmental Protection Agency               | 06/03/2019 | 06/04/2019 | 08/26/2019  |
| US | US CDL            | Clandestine Drug Labs  | Drug Enforcement Administration               | 06/11/2019 | 06/13/2019 | 09/03/2019  |
| US | US ENG CONTROLS   | Engineering Controls Sites List                              | Environmental Protection Agency               | 08/19/2019 | 08/20/2019 | 08/26/2019  |
| US | US FIN ASSUR      | Financial Assurance Information                              | Environmental Protection Agency               | 09/23/2019 | 09/24/2019 | 12/20/2019  |
| US | US HIST CDL       | National Clandestine Laboratory Register                     | Drug Enforcement Administration               | 06/11/2019 | 06/13/2019 | 09/03/2019  |
| US | US INST CONTROL   | Sites with Institutional Controls                            | Environmental Protection Agency               | 08/19/2019 | 08/20/2019 | 08/26/2019  |
| US | US MINES          | Mines Master Index File                                      | Department of Labor, Mine Safety and Health A | 08/01/2019 | 08/27/2019 | 11/11/2019  |
| US | US MINES 2        | Ferrous and Nonferrous Metal Mines Database Listing          | USGS  | 12/05/2005 | 02/29/2008 | 04/18/2008  |
| US | US MINES 3        | Active Mines & Mineral Plants Database Listing               | USGS  | 04/14/2011 | 06/08/2011 | 09/13/2011  |
| US | UXO               | Unexploded Ordnance Sites                                    | Department of Defense                         | 12/31/2017 | 01/17/2019 | 04/01/2019  |

| St | Acronym                               | Full Name                               | Government Agency                             | Gov Date   | Arvl. Date | <b>Active Date</b> |
|----|---------------------------------------|---|---|------------|------------|--------------------|
| CT | CT MANIFEST                           | Hazardous Waste Manifest Data           | Department of Energy & Environmental Protecti | 05/14/2019 | 05/14/2019 | 08/05/2019         |
| NJ | NJ MANIFEST                           | Manifest Information                    | Department of Environmental Protection        | 12/31/2018 | 04/10/2019 | 05/16/2019         |
| NY | NY MANIFEST                           | Facility and Manifest Data              | Department of Environmental Conservation      | 01/01/2019 | 05/01/2019 | 06/21/2019         |
| PA | PA MANIFEST                           | Manifest Information                    | Department of Environmental Protection        | 06/30/2018 | 07/19/2019 | 09/10/2019         |
| RI | RI MANIFEST                           | Manifest information                    | Department of Environmental Management        | 12/31/2018 | 10/02/2019 | 12/10/2019         |
| WI | WI MANIFEST                           | Manifest Information                    | Department of Natural Resources               | 05/31/2018 | 06/19/2019 | 09/03/2019         |
| US | AHA Hospitals                         | Sensitive Receptor: AHA Hospitals       | American Hospital Association, Inc.           |            |            |                    |
| US | Medical Centers                       | Sensitive Receptor: Medical Centers     | Centers for Medicare & Medicaid Services      |            |            |                    |
| US | Nursing Homes                         | Sensitive Receptor: Nursing Homes       | National Institutes of Health                 |            |            |                    |
| US | Public Schools                        | Sensitive Receptor: Public Schools      | National Center for Education Statistics      |            |            |                    |
| US | Private Schools                       | Sensitive Receptor: Private Schools     | National Center for Education Statistics      |            |            |                    |
| CA | Daycare Centers                       | Sensitive Receptor: Licensed Facilities | Department of Social Services                 |            |            |                    |
| US | Flood Zones                           | 100-year and 500-year flood zones       | Emergency Management Agency (FEMA)            |            |            |                    |
| US | NWI                                   | National Wetlands Inventory             | U.S. Fish and Wildlife Service                |            |            |                    |
| CA | State Wetlands                        | Wetland Inventory                       | Department of Fish and Wildlife               |            |            |                    |
| US | Topographic Map                       | welland inventory                       | U.S. Geological Survey                        |            |            |                    |
| US | Oil/Gas Pipelines                     |   | Endeavor Business Media                       |            |            |                    |
| US | Electric Power Transmission Line D    | lata                                    | Endeavor Business Media                       |            |            |                    |
| US | LIECTIFC FOWER TRAINSTILISSION LINE L | vala                                    | Lilucavoi Dubilicoo ivicuid                   |            |            |                    |

#### STREET AND ADDRESS INFORMATION

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## **GEOCHECK®-PHYSICAL SETTING SOURCE ADDENDUM**

#### **TARGET PROPERTY ADDRESS**

VISTA DEL CALABRIA PHASE I ESA SOUTHSIDE RD/ENTERPRISE RD HOLLISTER, CA 95023

## TARGET PROPERTY COORDINATES

Latitude (North): 36.818916 - 36° 49' 8.10" Longitude (West): 121.379382 - 121° 22' 45.78"

Universal Tranverse Mercator: Zone 10 UTM X (Meters): 644546.4 UTM Y (Meters): 4075807.0

Elevation: 454 ft. above sea level

#### **USGS TOPOGRAPHIC MAP**

Target Property Map: 5619826 HOLLISTER, CA

Version Date: 2012

East Map: 5603776 TRES PINOS, CA

Version Date: 2012

EDR's GeoCheck Physical Setting Source Addendum is provided to assist the environmental professional in forming an opinion about the impact of potential contaminant migration.

Assessment of the impact of contaminant migration generally has two principle investigative components:

- 1. Groundwater flow direction, and
- 2. Groundwater flow velocity.

Groundwater flow direction may be impacted by surface topography, hydrology, hydrogeology, characteristics of the soil, and nearby wells. Groundwater flow velocity is generally impacted by the nature of the geologic strata.

## **GROUNDWATER FLOW DIRECTION INFORMATION**

Groundwater flow direction for a particular site is best determined by a qualified environmental professional using site-specific well data. If such data is not reasonably ascertainable, it may be necessary to rely on other sources of information, such as surface topographic information, hydrologic information, hydrogeologic data collected on nearby properties, and regional groundwater flow information (from deep aquifers).

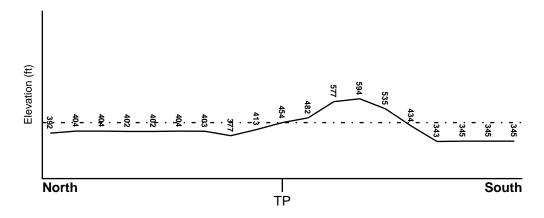
#### **TOPOGRAPHIC INFORMATION**

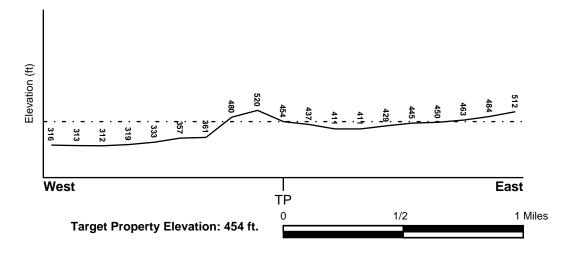
Surface topography may be indicative of the direction of surficial groundwater flow. This information can be used to assist the environmental professional in forming an opinion about the impact of nearby contaminated properties or, should contamination exist on the target property, what downgradient sites might be impacted.

#### TARGET PROPERTY TOPOGRAPHY

General Topographic Gradient: General North

#### SURROUNDING TOPOGRAPHY: ELEVATION PROFILES





Source: Topography has been determined from the USGS 7.5' Digital Elevation Model and should be evaluated on a relative (not an absolute) basis. Relative elevation information between sites of close proximity should be field verified.

#### HYDROLOGIC INFORMATION

Surface water can act as a hydrologic barrier to groundwater flow. Such hydrologic information can be used to assist the environmental professional in forming an opinion about the impact of nearby contaminated properties or, should contamination exist on the target property, what downgradient sites might be impacted.

Refer to the Physical Setting Source Map following this summary for hydrologic information (major waterways and bodies of water).

#### **FEMA FLOOD ZONE**

Flood Plain Panel at Target Property FEMA Source Type

06069C0185D FEMA FIRM Flood data

Additional Panels in search area: FEMA Source Type

06069C0205DFEMA FIRM Flood data06069C0195DFEMA FIRM Flood data06069C0215DFEMA FIRM Flood data

**NATIONAL WETLAND INVENTORY** 

NWI Quad at Target Property Data Coverage

HOLLISTER YES - refer to the Overview Map and Detail Map

## HYDROGEOLOGIC INFORMATION

Hydrogeologic information obtained by installation of wells on a specific site can often be an indicator of groundwater flow direction in the immediate area. Such hydrogeologic information can be used to assist the environmental professional in forming an opinion about the impact of nearby contaminated properties or, should contamination exist on the target property, what downgradient sites might be impacted.

#### Site-Specific Hydrogeological Data\*:

Search Radius: 1.25 miles Status: Not found

#### **AQUIFLOW®**

Search Radius: 1.000 Mile.

EDR has developed the AQUIFLOW Information System to provide data on the general direction of groundwater flow at specific points. EDR has reviewed reports submitted by environmental professionals to regulatory authorities at select sites and has extracted the date of the report, groundwater flow direction as determined hydrogeologically, and the depth to water table.

LOCATION GENERAL DIRECTION

MAP ID FROM TP GROUNDWATER FLOW

Not Reported

## **GROUNDWATER FLOW VELOCITY INFORMATION**

Groundwater flow velocity information for a particular site is best determined by a qualified environmental professional using site specific geologic and soil strata data. If such data are not reasonably ascertainable, it may be necessary to rely on other sources of information, including geologic age identification, rock stratigraphic unit and soil characteristics data collected on nearby properties and regional soil information. In general, contaminant plumes move more quickly through sandy-gravelly types of soils than silty-clayey types of soils.

## GEOLOGIC INFORMATION IN GENERAL AREA OF TARGET PROPERTY

Geologic information can be used by the environmental professional in forming an opinion about the relative speed at which contaminant migration may be occurring.

#### **ROCK STRATIGRAPHIC UNIT**

## **GEOLOGIC AGE IDENTIFICATION**

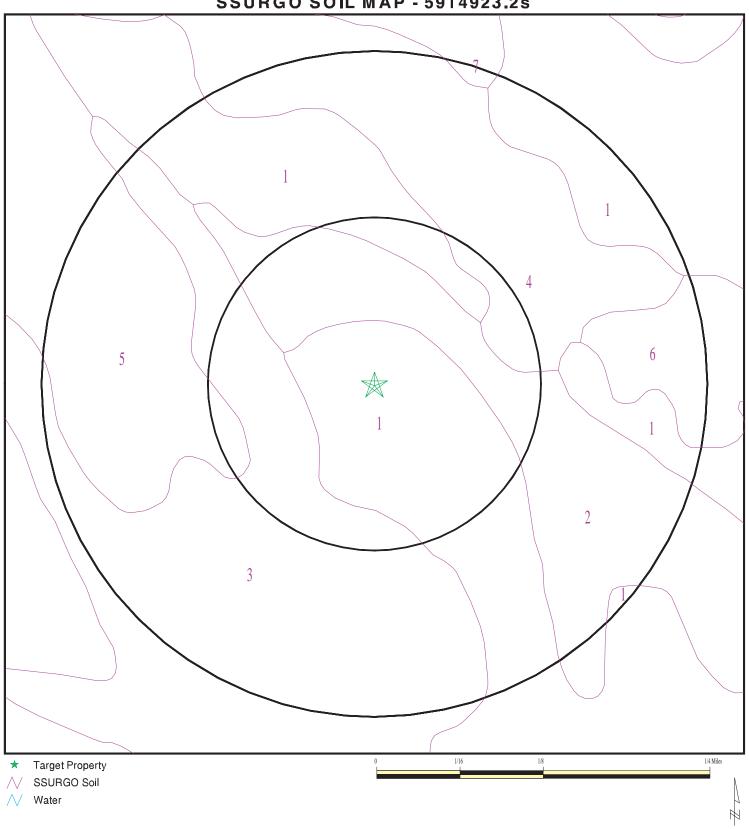
Era: Cenozoic Category: Stratifed Sequence

System: Quaternary Series: Quaternary

Code: Q (decoded above as Era, System & Series)

Geologic Age and Rock Stratigraphic Unit Source: P.G. Schruben, R.E. Arndt and W.J. Bawiec, Geology of the Conterminous U.S. at 1:2,500,000 Scale - a digital representation of the 1974 P.B. King and H.M. Beikman Map, USGS Digital Data Series DDS - 11 (1994).

# **SSURGO SOIL MAP - 5914923.2s**



SITE NAME: Vista Del Calabria Phase I ESA ADDRESS: Southside Rd/Enterprise Rd Hollister CA 95023

LAT/LONG: 36.818916 / 121.379382 CLIENT: Earth Systems Pacific, Northern CA
CONTACT: David Teimoorian
INQUIRY #: 5914923.2s

DATE: December 30, 2019 12:28 pm

## DOMINANT SOIL COMPOSITION IN GENERAL AREA OF TARGET PROPERTY

The U.S. Department of Agriculture's (USDA) Soil Conservation Service (SCS) leads the National Cooperative Soil Survey (NCSS) and is responsible for collecting, storing, maintaining and distributing soil survey information for privately owned lands in the United States. A soil map in a soil survey is a representation of soil patterns in a landscape. The following information is based on Soil Conservation Service SSURGO data.

Soil Map ID: 1

Soil Component Name: Antioch

Soil Surface Texture: loam

Hydrologic Group: Class D - Very slow infiltration rates. Soils are clayey, have a high

water table, or are shallow to an impervious layer.

Soil Drainage Class: Moderately well drained

Hydric Status: Unknown

Corrosion Potential - Uncoated Steel: High

Depth to Bedrock Min: > 0 inches

Depth to Watertable Min: > 0 inches

|       | Soil Layer Information |           |                    |   |   |                             |                      |  |  |  |  |  |
|-------|------------------------|-----------|--------------------|---|---|-----------------------------|----------------------|--|--|--|--|--|
|       | Bou                    | ındary    |                    | Classi  | fication  | Saturated<br>hydraulic      |                      |  |  |  |  |  |
| Layer | Upper                  | Lower     | Soil Texture Class | AASHTO Group  | Unified Soil  | conductivity<br>micro m/sec |                      |  |  |  |  |  |
| 1     | 0 inches               | 12 inches | loam               | Silt-Clay Materials (more than 35 pct. passing No. 200), Clayey Soils.                | FINE-GRAINED<br>SOILS, Silts and<br>Clays (liquid<br>limit less than<br>50%), Lean Clay | Max: 14<br>Min: 4           | Max: 8.4<br>Min: 7.4 |  |  |  |  |  |
| 2     | 12 inches              | 37 inches | clay               | Silt-Clay<br>Materials (more<br>than 35 pct.<br>passing No.<br>200), Clayey<br>Soils. | FINE-GRAINED<br>SOILS, Silts and<br>Clays (liquid<br>limit less than<br>50%), Lean Clay | Max: 14<br>Min: 4           | Max: 8.4<br>Min: 7.4 |  |  |  |  |  |
| 3     | 37 inches              | 75 inches | loam               | Silt-Clay<br>Materials (more<br>than 35 pct.<br>passing No.<br>200), Clayey<br>Soils. | FINE-GRAINED<br>SOILS, Silts and<br>Clays (liquid<br>limit less than<br>50%), Lean Clay | Max: 14<br>Min: 4           | Max: 8.4<br>Min: 7.4 |  |  |  |  |  |

Soil Map ID: 2

Soil Component Name: Antioch

Soil Surface Texture: loam

Hydrologic Group: Class D - Very slow infiltration rates. Soils are clayey, have a high

water table, or are shallow to an impervious layer.

Soil Drainage Class: Moderately well drained

Hydric Status: Unknown

Corrosion Potential - Uncoated Steel: High

Depth to Bedrock Min: > 0 inches

Depth to Watertable Min: > 0 inches

|       | Воц       | ındary    |                    | Classif  | fication  | Saturated<br>hydraulic      |                      |
|-------|-----------|-----------|--------------------|--|---|-----------------------------|----------------------|
| Layer | Upper     | Lower     | Soil Texture Class | AASHTO Group   | Unified Soil  | conductivity<br>micro m/sec | Soil Reaction (pH)   |
| 1     | 0 inches  | 5 inches  | loam               | Silt-Clay<br>Materials (more<br>than 35 pct.<br>passing No.<br>200), Silty<br>Soils. | FINE-GRAINED<br>SOILS, Silts and<br>Clays (liquid<br>limit less than<br>50%), Lean Clay.<br>FINE-GRAINED<br>SOILS, Silts and<br>Clays (liquid<br>limit less than<br>50%), silt. | Max: 14<br>Min: 4           | Max: 8.4<br>Min: 7.4 |
| 2     | 5 inches  | 29 inches | clay               | Silt-Clay<br>Materials (more<br>than 35 pct.<br>passing No.<br>200), Silty<br>Soils. | FINE-GRAINED<br>SOILS, Silts and<br>Clays (liquid<br>limit less than<br>50%), Lean Clay.<br>FINE-GRAINED<br>SOILS, Silts and<br>Clays (liquid<br>limit less than<br>50%), silt. | Max: 14<br>Min: 4           | Max: 8.4<br>Min: 7.4 |
| 3     | 29 inches | 68 inches | loam               | Silt-Clay<br>Materials (more<br>than 35 pct.<br>passing No.<br>200), Silty<br>Soils. | FINE-GRAINED<br>SOILS, Silts and<br>Clays (liquid<br>limit less than<br>50%), Lean Clay.<br>FINE-GRAINED<br>SOILS, Silts and<br>Clays (liquid<br>limit less than<br>50%), silt  | Max: 14<br>Min: 4           | Max: 8.4<br>Min: 7.4 |

Soil Map ID: 3

Soil Component Name: Soper

Soil Surface Texture: gravelly loam

Hydrologic Group: Class C - Slow infiltration rates. Soils with layers impeding downward

movement of water, or soils with moderately fine or fine textures.

Soil Drainage Class: Well drained

Hydric Status: Unknown

Corrosion Potential - Uncoated Steel: Moderate

Depth to Bedrock Min: > 0 inches

Depth to Watertable Min: > 0 inches

#### **Soil Layer Information** Saturated **Boundary** Classification hydraulic conductivity **AASHTO Group Unified Soil Soil Reaction** Layer Upper Lower Soil Texture Class micro m/sec (pH) 1 0 inches 16 inches gravelly loam Silt-Clay Not reported Max: 4 Max: Min: Materials (more Min: 1.4 than 35 pct. passing No. 200), Clayey Soils. 2 16 inches 29 inches sandy clay loam Silt-Clay Not reported Max: 4 Max: Min: Materials (more Min: 1.4 than 35 pct. passing No. 200), Clayey Soils. 3 29 inches 35 inches loamy sand Silt-Clay Not reported Max: 4 Max: Min: Min: 1.4 Materials (more than 35 pct. passing No. 200), Clayey Soils. 4 35 inches 40 inches weathered Silt-Clay Not reported Max: 4 Max: Min: Materials (more bedrock Min: 1.4 than 35 pct. passing No. 200), Clayey Soils.

Soil Map ID: 4

Soil Component Name: Terrace escarpments

Soil Surface Texture: variable

Hydrologic Group: Class C - Slow infiltration rates. Soils with layers impeding downward

movement of water, or soils with moderately fine or fine textures.

Soil Drainage Class: Hydric Status: Not hydric

Corrosion Potential - Uncoated Steel: Not Reported

Depth to Bedrock Min: > 0 inches

Depth to Watertable Min: > 0 inches

|       | Soil Layer Information |           |                    |              |              |                     |                    |  |  |  |  |  |
|-------|------------------------|-----------|--------------------|--------------|--------------|---------------------|--------------------|--|--|--|--|--|
|       | Bou                    | ndary     | Clas               |              | ication      | Saturated hydraulic |                    |  |  |  |  |  |
| Layer | Upper                  | Lower     | Soil Texture Class | AASHTO Group | Unified Soil |                     | Soil Reaction (pH) |  |  |  |  |  |
| 1     | 0 inches               | 59 inches | variable           | Not reported | Not reported | Max:<br>Min:        | Max: Min:          |  |  |  |  |  |

Soil Map ID: 5

Soil Component Name: Soper

Soil Surface Texture: gravelly loam

Hydrologic Group: Class C - Slow infiltration rates. Soils with layers impeding downward

movement of water, or soils with moderately fine or fine textures.

Soil Drainage Class: Well drained

Hydric Status: Unknown

Corrosion Potential - Uncoated Steel: Moderate

Depth to Bedrock Min: > 0 inches

Depth to Watertable Min: > 0 inches

|       |           |           | Soil Layer           | Information   |              |                             |                    |
|-------|-----------|-----------|----------------------|---|--------------|-----------------------------|--------------------|
|       | Bou       | ındary    |                      | Classi  | fication     | Saturated hydraulic         |                    |
| Layer | Upper     | Lower     | Soil Texture Class   | AASHTO Group  | Unified Soil | conductivity<br>micro m/sec | Soil Reaction (pH) |
| 1     | 0 inches  | 16 inches | gravelly loam        | Silt-Clay<br>Materials (more<br>than 35 pct.<br>passing No.<br>200), Clayey<br>Soils. | Not reported | Max: 4<br>Min: 1.4          | Max: Min:          |
| 2     | 16 inches | 29 inches | sandy clay loam      | Silt-Clay Materials (more than 35 pct. passing No. 200), Clayey Soils.                | Not reported | Max: 4<br>Min: 1.4          | Max: Min:          |
| 3     | 29 inches | 35 inches | loamy sand           | Silt-Clay<br>Materials (more<br>than 35 pct.<br>passing No.<br>200), Clayey<br>Soils. | Not reported | Max: 4<br>Min: 1.4          | Max: Min:          |
| 4     | 35 inches | 40 inches | weathered<br>bedrock | Silt-Clay<br>Materials (more<br>than 35 pct.<br>passing No.<br>200), Clayey<br>Soils. | Not reported | Max: 4<br>Min: 1.4          | Max: Min:          |

## Soil Map ID: 6

Soil Component Name: Antioch
Soil Surface Texture: clay loam

Hydrologic Group: Class D - Very slow infiltration rates. Soils are clayey, have a high

water table, or are shallow to an impervious layer.

Soil Drainage Class: Moderately well drained

Hydric Status: Unknown

Corrosion Potential - Uncoated Steel: High

Depth to Bedrock Min: > 0 inches

Depth to Watertable Min: > 0 inches

|       | Soil Layer Information |           |                    |   |   |                             |                      |  |  |  |  |  |  |
|-------|------------------------|-----------|--------------------|---|---|-----------------------------|----------------------|--|--|--|--|--|--|
|       | Воц                    | ındary    |                    | Classi  | fication  | Saturated<br>hydraulic      |                      |  |  |  |  |  |  |
| Layer | Upper                  | Lower     | Soil Texture Class | AASHTO Group  | Unified Soil  | conductivity<br>micro m/sec | Soil Reaction (pH)   |  |  |  |  |  |  |
| 1     | 0 inches               | 5 inches  | clay loam          | Silt-Clay<br>Materials (more<br>than 35 pct.<br>passing No.<br>200), Clayey<br>Soils. | FINE-GRAINED<br>SOILS, Silts and<br>Clays (liquid<br>limit less than<br>50%), Lean Clay | Max: 14<br>Min: 4           | Max: 8.4<br>Min: 7.4 |  |  |  |  |  |  |
| 2     | 5 inches               | 29 inches | clay               | Silt-Clay<br>Materials (more<br>than 35 pct.<br>passing No.<br>200), Clayey<br>Soils. | FINE-GRAINED<br>SOILS, Silts and<br>Clays (liquid<br>limit less than<br>50%), Lean Clay | Max: 14<br>Min: 4           | Max: 8.4<br>Min: 7.4 |  |  |  |  |  |  |
| 3     | 29 inches              | 68 inches | loam               | Silt-Clay<br>Materials (more<br>than 35 pct.<br>passing No.<br>200), Clayey<br>Soils. | FINE-GRAINED<br>SOILS, Silts and<br>Clays (liquid<br>limit less than<br>50%), Lean Clay | Max: 14<br>Min: 4           | Max: 8.4<br>Min: 7.4 |  |  |  |  |  |  |

Soil Map ID: 7

Soil Component Name: Rieff

Soil Surface Texture: sandy loam

Class B - Moderate infiltration rates. Deep and moderately deep, moderately well and well drained soils with moderately coarse Hydrologic Group:

textures.

Soil Drainage Class: Well drained

Hydric Status: Unknown

Corrosion Potential - Uncoated Steel: Moderate

Depth to Bedrock Min: > 0 inches

Depth to Watertable Min: > 0 inches

| Soil Layer Information |           |           |                    |   |   |                             |                      |
|------------------------|-----------|-----------|--------------------|---|---|-----------------------------|----------------------|
|                        | Boundary  |           |                    | Classification  |   | Saturated<br>hydraulic      |                      |
| Layer                  | Upper     | Lower     | Soil Texture Class | AASHTO Group  | Unified Soil  | conductivity<br>micro m/sec | Soil Reaction (pH)   |
| 1                      | 0 inches  | 24 inches | sandy loam         | Granular<br>materials (35<br>pct. or less<br>passing No.<br>200), Silty, or<br>Clayey Gravel<br>and Sand. | FINE-GRAINED<br>SOILS, Silts and<br>Clays (liquid<br>limit less than<br>50%), Lean Clay | Max: 42<br>Min: 4           | Max: 8.4<br>Min: 7.9 |
| 2                      | 24 inches | 42 inches | sandy loam         | Granular<br>materials (35<br>pct. or less<br>passing No.<br>200), Silty, or<br>Clayey Gravel<br>and Sand. | FINE-GRAINED<br>SOILS, Silts and<br>Clays (liquid<br>limit less than<br>50%), Lean Clay | Max: 42<br>Min: 4           | Max: 8.4<br>Min: 7.9 |
| 3                      | 42 inches | 59 inches | loam               | Granular<br>materials (35<br>pct. or less<br>passing No.<br>200), Silty, or<br>Clayey Gravel<br>and Sand. | FINE-GRAINED<br>SOILS, Silts and<br>Clays (liquid<br>limit less than<br>50%), Lean Clay | Max: 42<br>Min: 4           | Max: 8.4<br>Min: 7.9 |

## **LOCAL / REGIONAL WATER AGENCY RECORDS**

EDR Local/Regional Water Agency records provide water well information to assist the environmental professional in assessing sources that may impact ground water flow direction, and in forming an opinion about the impact of contaminant migration on nearby drinking water wells.

## WELL SEARCH DISTANCE INFORMATION

DATABASE SEARCH DISTANCE (miles)

Federal USGS 1.000

Federal FRDS PWS Nearest PWS within 1 mile

State Database 1.000

#### FEDERAL USGS WELL INFORMATION

LOCATION MAP ID WELL ID FROM TP

A2 USGS40000178177 1/8 - 1/4 Mile North USGS40000178129 1/8 - 1/4 Mile NE

## FEDERAL USGS WELL INFORMATION

| MAP ID | WELL ID         | LOCATION<br>FROM TP |
|--------|-----------------|---------------------|
| 7      | USGS40000178097 | 1/4 - 1/2 Mile East |
| 8      | USGS40000178084 | 1/4 - 1/2 Mile WSW  |
| 9      | USGS40000178124 | 1/4 - 1/2 Mile WNW  |
| 11     | USGS40000178024 | 1/2 - 1 Mile SSW    |
| B12    | USGS40000178091 | 1/2 - 1 Mile East   |
| C13    | USGS40000178198 | 1/2 - 1 Mile NW     |
| 14     | USGS40000178236 | 1/2 - 1 Mile North  |
| C16    | USGS40000178204 | 1/2 - 1 Mile NW     |
| D17    | USGS40000178008 | 1/2 - 1 Mile South  |
| E18    | USGS40000178069 | 1/2 - 1 Mile ESE    |
| 22     | USGS40000177990 | 1/2 - 1 Mile South  |
| 23     | USGS40000178220 | 1/2 - 1 Mile NW     |
| 25     | USGS40000177972 | 1/2 - 1 Mile South  |
| F26    | USGS40000178028 | 1/2 - 1 Mile SW     |
| 27     | USGS40000178281 | 1/2 - 1 Mile NNW    |
| 28     | USGS40000177991 | 1/2 - 1 Mile SW     |
| G29    | USGS40000178230 | 1/2 - 1 Mile NW     |
| G30    | USGS40000178231 | 1/2 - 1 Mile NW     |
| 31     | USGS40000178209 | 1/2 - 1 Mile ENE    |
| H32    | USGS40000178058 | 1/2 - 1 Mile WSW    |
| H33    | USGS40000178053 | 1/2 - 1 Mile WSW    |
| 134    | USGS40000177926 | 1/2 - 1 Mile SSE    |
| 37     | USGS40000177987 | 1/2 - 1 Mile SE     |
| 38     | USGS40000177911 | 1/2 - 1 Mile South  |
| 40     | USGS40000178239 | 1/2 - 1 Mile NW     |

#### FEDERAL FRDS PUBLIC WATER SUPPLY SYSTEM INFORMATION

| MAP ID              | WELL ID | LOCATION<br>FROM TP |
|---------------------|---------|---------------------|
| No PWS System Found |         |                     |

Note: PWS System location is not always the same as well location.

#### STATE DATABASE WELL INFORMATION

| MAP ID | WELL ID         | LOCATION<br>FROM TP  |
|--------|-----------------|----------------------|
| A1     | 11544           | 1/8 - 1/4 Mile North |
| 4      | 11552           | 1/4 - 1/2 Mile NNW   |
| A5     | CADWR8000030230 | 1/4 - 1/2 Mile North |
| A6     | CADWR8000030231 | 1/4 - 1/2 Mile NNW   |
| B10    | CADWR8000030157 | 1/2 - 1 Mile ESE     |
| D15    | CADWR8000030105 | 1/2 - 1 Mile South   |
| E19    | 11545           | 1/2 - 1 Mile ESE     |
| E20    | 11546           | 1/2 - 1 Mile ESE     |
| E21    | 18666           | 1/2 - 1 Mile ESE     |
| F24    | CADWR8000030120 | 1/2 - 1 Mile SW      |
| 135    | CADWR8000030040 | 1/2 - 1 Mile SSE     |
| 136    | 19862           | 1/2 - 1 Mile SSE     |

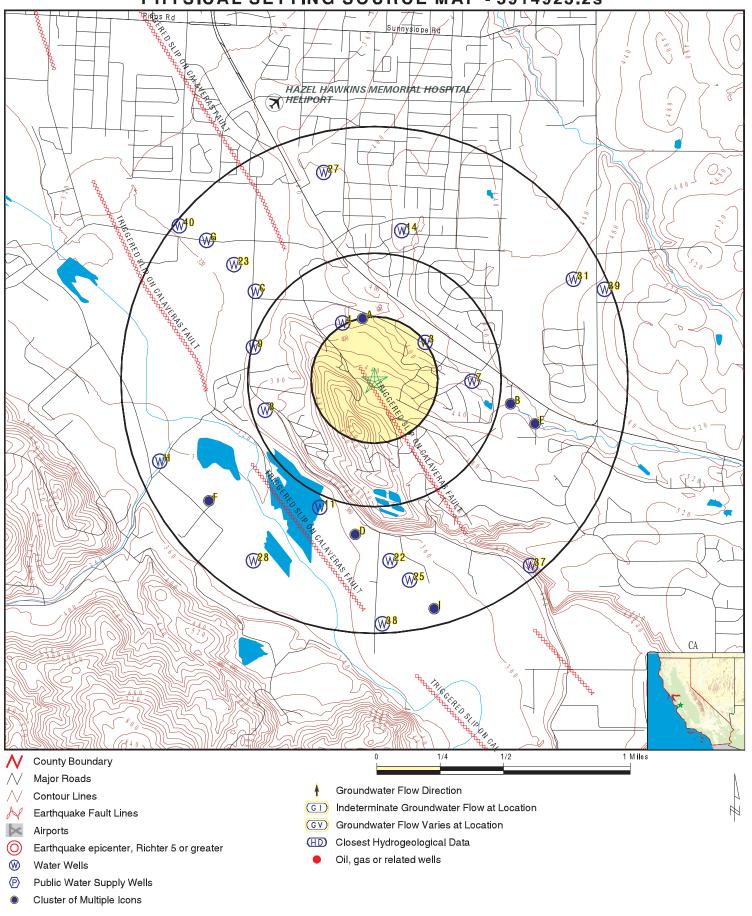
# **GEOCHECK<sup>®</sup> - PHYSICAL SETTING SOURCE SUMMARY**

## STATE DATABASE WELL INFORMATION

MAP ID WELL ID FROM TP

39 CADWR8000030238 1/2 - 1 Mile ENE

# PHYSICAL SETTING SOURCE MAP - 5914923.2s



SITE NAME: Vista Del Calabria Phase I ESA ADDRESS: Southside Rd/Enterprise Rd

Hollister CA 95023 LAT/LONG: 36.818916 / 121.379382 CLIENT: Earth Systems Pacific, Northern CA CONTACT: David Teimoorian

INQUIRY#: 5914923.2s

DATE: December 30, 2019 12:28 pm

| Map ID Direction Distance Elevation  | Database | EDR ID Number   |
|--|----------|-----------------|
| A1 North 1/8 - 1/4 Mile Lower  | CA WELLS | 11544           |
| A2 North 1/8 - 1/4 Mile Lower  | FED USGS | USGS40000178177 |
| 3<br>NE <u>Click here for full text details</u><br>1/8 - 1/4 Mile<br>Lower | FED USGS | USGS40000178129 |
| 4 NNW 1/4 - 1/2 Mile Lower   | CA WELLS | 11552           |
| A5 North Click here for full text details 1/4 - 1/2 Mile Lower             | CA WELLS | CADWR8000030230 |
| A6 NNW 1/4 - 1/2 Mile Lower  | CA WELLS | CADWR8000030231 |
| 7 East Click here for full text details 1/4 - 1/2 Mile Lower               | FED USGS | USGS40000178097 |
| 8 WSW Click here for full text details 1/4 - 1/2 Mile Lower                | FED USGS | USGS40000178084 |

| Map ID<br>Direction<br>Distance<br>Elevation |                                  | Database | EDR ID Number   |
|--|----------------------------------|----------|-----------------|
| 9<br>WNW<br>1/4 - 1/2 Mile<br>Lower          | Click here for full text details | FED USGS | USGS40000178124 |
| B10<br>ESE<br>1/2 - 1 Mile<br>Higher         | Click here for full text details | CA WELLS | CADWR8000030157 |
| 11<br>SSW<br>1/2 - 1 Mile<br>Lower           | Click here for full text details | FED USGS | USGS40000178024 |
| B12<br>East<br>1/2 - 1 Mile<br>Lower         | Click here for full text details | FED USGS | USGS40000178091 |
| C13<br>NW<br>1/2 - 1 Mile<br>Lower           | Click here for full text details | FED USGS | USGS40000178198 |
| 14<br>North<br>1/2 - 1 Mile<br>Lower         | Click here for full text details | FED USGS | USGS40000178236 |
| D15<br>South<br>1/2 - 1 Mile<br>Lower        | Click here for full text details | CA WELLS | CADWR8000030105 |
| C16<br>NW<br>1/2 - 1 Mile<br>Lower           | Click here for full text details | FED USGS | USGS40000178204 |
| D17<br>South<br>1/2 - 1 Mile<br>Lower        | Click here for full text details | FED USGS | USGS40000178008 |

| Map ID<br>Direction<br>Distance<br>Elevation |                                  | Database | EDR ID Number   |
|--|----------------------------------|----------|-----------------|
| E18<br>ESE<br>1/2 - 1 Mile<br>Higher         | Click here for full text details | FED USGS | USGS40000178069 |
| E19<br>ESE<br>1/2 - 1 Mile<br>Lower          | Click here for full text details | CA WELLS | 11545           |
| E20<br>ESE<br>1/2 - 1 Mile<br>Lower          | Click here for full text details | CA WELLS | 11546           |
| E21<br>ESE<br>1/2 - 1 Mile<br>Lower          | Click here for full text details | CA WELLS | 18666           |
| 22<br>South<br>1/2 - 1 Mile<br>Lower         | Click here for full text details | FED USGS | USGS40000177990 |
| 23<br>NW<br>1/2 - 1 Mile<br>Lower            | Click here for full text details | FED USGS | USGS40000178220 |
| F24<br>SW<br>1/2 - 1 Mile<br>Lower           | Click here for full text details | CA WELLS | CADWR8000030120 |
| 25<br>South<br>1/2 - 1 Mile<br>Lower         | Click here for full text details | FED USGS | USGS40000177972 |
| F26<br>SW<br>1/2 - 1 Mile<br>Lower           | Click here for full text details | FED USGS | USGS40000178028 |

| Map ID<br>Direction<br>Distance<br>Elevation |                                  | Database | EDR ID Number   |
|--|----------------------------------|----------|-----------------|
| 27<br>NNW<br>1/2 - 1 Mile<br>Lower           | Click here for full text details | FED USGS | USGS40000178281 |
| 28<br>SW<br>1/2 - 1 Mile<br>Lower            | Click here for full text details | FED USGS | USGS40000177991 |
| G29<br>NW<br>1/2 - 1 Mile<br>Lower           | Click here for full text details | FED USGS | USGS40000178230 |
| G30<br>NW<br>1/2 - 1 Mile<br>Lower           | Click here for full text details | FED USGS | USGS40000178231 |
| 31<br>ENE<br>1/2 - 1 Mile<br>Higher          | Click here for full text details | FED USGS | USGS40000178209 |
| H32<br>WSW<br>1/2 - 1 Mile<br>Lower          | Click here for full text details | FED USGS | USGS40000178058 |
| H33<br>WSW<br>1/2 - 1 Mile<br>Lower          | Click here for full text details | FED USGS | USGS40000178053 |
| I34<br>SSE<br>1/2 - 1 Mile<br>Lower          | Click here for full text details | FED USGS | USGS40000177926 |
| 135<br>SSE<br>1/2 - 1 Mile<br>Lower          | Click here for full text details | CA WELLS | CADWR8000030040 |

| Map ID<br>Direction<br>Distance<br>Elevation |                                  | Database | EDR ID Number   |
|--|----------------------------------|----------|-----------------|
| I36<br>SSE<br>1/2 - 1 Mile<br>Lower          | Click here for full text details | CA WELLS | 19862           |
| 37<br>SE<br>1/2 - 1 Mile<br>Higher           | Click here for full text details | FED USGS | USGS40000177987 |
| 38<br>South<br>1/2 - 1 Mile<br>Lower         | Click here for full text details | FED USGS | USGS40000177911 |
| 39<br>ENE<br>1/2 - 1 Mile<br>Higher          | Click here for full text details | CA WELLS | CADWR8000030238 |
| 40<br>NW<br>1/2 - 1 Mile<br>Lower            | Click here for full text details | FED USGS | USGS40000178239 |

## AREA RADON INFORMATION

State Database: CA Radon

Radon Test Results

| Zipcode | Num Tests | > 4 pCi/L |
|---------|-----------|-----------|
|         |           |           |
| 95023   | 13        | 0         |

## Federal EPA Radon Zone for SAN BENITO County: 2

Note: Zone 1 indoor average level > 4 pCi/L.

: Zone 2 indoor average level >= 2 pCi/L and <= 4 pCi/L.

: Zone 3 indoor average level < 2 pCi/L.

Federal Area Radon Information for Zip Code: 95023

Number of sites tested: 2

Area Average Activity % <4 pCi/L % 4-20 pCi/L % >20 pCi/L 0.350 pCi/L Living Area - 1st Floor 100% 0% 0% Living Area - 2nd Floor Not Reported Not Reported Not Reported Not Reported Not Reported Not Reported Basement Not Reported Not Reported

## PHYSICAL SETTING SOURCE RECORDS SEARCHED

#### **TOPOGRAPHIC INFORMATION**

USGS 7.5' Digital Elevation Model (DEM)

Source: United States Geologic Survey

EDR acquired the USGS 7.5' Digital Elevation Model in 2002 and updated it in 2006. The 7.5 minute DEM corresponds to the USGS 1:24,000- and 1:25,000-scale topographic quadrangle maps. The DEM provides elevation data with consistent elevation units and projection.

Source: U.S. Geological Survey

#### HYDROLOGIC INFORMATION

Flood Zone Data: This data was obtained from the Federal Emergency Management Agency (FEMA). It depicts 100-year and 500-year flood zones as defined by FEMA. It includes the National Flood Hazard Layer (NFHL) which incorporates Flood Insurance Rate Map (FIRM) data and Q3 data from FEMA in areas not covered by NFHL.

Source: FEMA

Telephone: 877-336-2627

Date of Government Version: 2003, 2015

NWI: National Wetlands Inventory. This data, available in select counties across the country, was obtained by EDR in 2002, 2005 and 2010 from the U.S. Fish and Wildlife Service.

State Wetlands Data: Wetland Inventory Source: Department of Fish and Wildlife

Telephone: 916-445-0411

#### HYDROGEOLOGIC INFORMATION

AQUIFLOW<sup>R</sup> Information System

Source: EDR proprietary database of groundwater flow information

EDR has developed the AQUIFLOW Information System (AIS) to provide data on the general direction of groundwater flow at specific points. EDR has reviewed reports submitted to regulatory authorities at select sites and has extracted the date of the report, hydrogeologically determined groundwater flow direction and depth to water table information.

#### **GEOLOGIC INFORMATION**

Geologic Age and Rock Stratigraphic Unit

Source: P.G. Schruben, R.E. Arndt and W.J. Bawiec, Geology of the Conterminous U.S. at 1:2,500,000 Scale - A digital representation of the 1974 P.B. King and H.M. Beikman Map, USGS Digital Data Series DDS - 11 (1994).

STATSGO: State Soil Geographic Database

Source: Department of Agriculture, Natural Resources Conservation Service (NRCS)

The U.S. Department of Agriculture's (USDA) Natural Resources Conservation Service (NRCS) leads the national Conservation Soil Survey (NCSS) and is responsible for collecting, storing, maintaining and distributing soil survey information for privately owned lands in the United States. A soil map in a soil survey is a representation of soil patterns in a landscape. Soil maps for STATSGO are compiled by generalizing more detailed (SSURGO) soil survey maps.

SSURGO: Soil Survey Geographic Database

Source: Department of Agriculture, Natural Resources Conservation Service (NRCS)

Telephone: 800-672-5559

SSURGO is the most detailed level of mapping done by the Natural Resources Conservation Service, mapping scales generally range from 1:12,000 to 1:63,360. Field mapping methods using national standards are used to construct the soil maps in the Soil Survey Geographic (SSURGO) database. SSURGO digitizing duplicates the original soil survey maps. This level of mapping is designed for use by landowners, townships and county natural resource planning and management.

## PHYSICAL SETTING SOURCE RECORDS SEARCHED

#### LOCAL / REGIONAL WATER AGENCY RECORDS

#### FEDERAL WATER WELLS

PWS: Public Water Systems

Source: EPA/Office of Drinking Water

Telephone: 202-564-3750

Public Water System data from the Federal Reporting Data System. A PWS is any water system which provides water to at least 25 people for at least 60 days annually. PWSs provide water from wells, rivers and other sources.

PWS ENF: Public Water Systems Violation and Enforcement Data

Source: EPA/Office of Drinking Water

Telephone: 202-564-3750

Violation and Enforcement data for Public Water Systems from the Safe Drinking Water Information System (SDWIS) after August 1995. Prior to August 1995, the data came from the Federal Reporting Data System (FRDS).

USGS Water Wells: USGS National Water Inventory System (NWIS)

This database contains descriptive information on sites where the USGS collects or has collected data on surface water and/or groundwater. The groundwater data includes information on wells, springs, and other sources of groundwater.

#### STATE RECORDS

Water Well Database

Source: Department of Water Resources

Telephone: 916-651-9648

California Drinking Water Quality Database Source: Department of Public Health

Telephone: 916-324-2319

The database includes all drinking water compliance and special studies monitoring for the state of California since 1984. It consists of over 3,200,000 individual analyses along with well and water system information.

## OTHER STATE DATABASE INFORMATION

California Oil and Gas Well Locations Source: Department of Conservation

Telephone: 916-323-1779

Oil and Gas well locations in the state.

#### California Earthquake Fault Lines

Source: California Division of Mines and Geology

The fault lines displayed on EDR's Topographic map are digitized quaternary fault lines prepared in 1975 by the United State Geological Survey. Additional information (also from 1975) regarding activity at specific fault lines comes from California's Preliminary Fault Activity Map prepared by the California Division of Mines and Geology.

#### **RADON**

State Database: CA Radon

Source: Department of Public Health

Telephone: 916-210-8558 Radon Database for California

Area Radon Information

Source: USGS

Telephone: 703-356-4020

The National Radon Database has been developed by the U.S. Environmental Protection Agency

(USEPA) and is a compilation of the EPA/State Residential Radon Survey and the National Residential Radon Survey. The study covers the years 1986 - 1992. Where necessary data has been supplemented by information collected at

private sources such as universities and research institutions.

## PHYSICAL SETTING SOURCE RECORDS SEARCHED

EPA Radon Zones Source: EPA

Telephone: 703-356-4020

Sections 307 & 309 of IRAA directed EPA to list and identify areas of U.S. with the potential for elevated indoor

radon levels.

#### OTHER

Airport Landing Facilities: Private and public use landing facilities

Source: Federal Aviation Administration, 800-457-6656

Epicenters: World earthquake epicenters, Richter 5 or greater

Source: Department of Commerce, National Oceanic and Atmospheric Administration

California Earthquake Fault Lines: The fault lines displayed on EDR's Topographic map are digitized quaternary fault lines, prepared in 1975 by the United State Geological Survey. Additional information (also from 1975) regarding activity at specific fault lines comes from California's Preliminary Fault Activity Map prepared by the California Division of Mines and Geology.

## STREET AND ADDRESS INFORMATION

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# **APPENDIX F**

AGRICHEMICAL ASSESSMENT - PHASE II ESA REPORT, 2014





Project No. **11227.000.000** 

December 23, 2014

Mr. Chris Garwood Pacific Union Land Company, Inc. 675 Hartz Avenue, Suite 300 Danville, CA 94526

Subject:

213 Enterprise Road Hollister, California

AGRICHEMICAL ASSESSMENT – PHASE II ESA

Reference:

ENGEO, Phase I Environmental Site Assessment, 213 Enterprise Road, Hollister,

California, Project No. 11227.000.000, June 13, 2014.

Dear Mr. Garwood:

We are pleased to submit our agrichemical assessment conducted at the subject property (Property) in Hollister, California. While no Recognized Environmental Conditions (RECs) were identified within our reference Phase I ESA, a potential environmental condition was identified for a portion of the Property that was previously utilized for agriculture production. The purpose of this assessment was to determine if past agricultural uses have impacted site soils.

## BACKGROUND

The Property is located at 213 Enterprise Road in Hollister, California (Figure 1). The Property is approximately 106 acres with Enterprise Road bisecting the Property. The northern area is currently occupied by orchards, farm fields, and related structures. The southern area is primarily open grassland, with orchards and structures limited to the northern corner. Historic agricultural activities occurred within the northern portion, with limited activity within the southern portion.

## SCOPE OF FIELD EXPLORATION

The Property has historically been used for agricultural purposes. As such, agrichemicals may have been utilized for pest and weed control. A soil sampling and laboratory-testing program was implemented to evaluate the soil conditions. The scope of the work included:

- Recovery of 80 soil samples from approximately 3 to 9 inches below the ground surface.
- Laboratory analysis of 20 four-point composites for Organochlorine Pesticides.
- Laboratory analysis of 20 discrete samples for Arsenic.
- Analysis of laboratory data with an evaluation of our findings.

11227.000.000 December 23, 2014 Page 2

#### SAMPLING ACTIVITIES

On December 10, 2014, a total of 80 soil samples were collected from the Property where agricultural activities have been performed. Soil samples were collected from approximately 3 to 9 inches below the existing ground surface. Sample locations are shown on Figure 2.

Soil samples were recovered using laboratory provided glass jars. The samples were preserved in an ice chest and transported under documented chain-of-custody to California Laboratory Services, a fixed-base California-certified laboratory in Rancho Cordova, California.

#### ANALYTICAL RESULTS

The reported laboratory concentrations were compared to the applicable US Environmental Protection Agency (EPA) Regional Screening Levels (RSLs) developed by the United States Environmental Protection Agency (EPA) assuming a residential land scenario.

Organochlorine pesticides were not detected (ND) in five of the composite samples. Organochlorine pesticides in the form of chlordane, dieldrin, DDT and DDE were detected in 15 of the composite samples at low concentrations, below their respective RSLs. The detections were concentrated primarily in the western half of the northern portion of the site (north of Enterprise Road). The detection locations correspond to historically active agricultural areas indicated on the aerial photographs and topographic maps of the site.

Arsenic concentrations ranged from 2.3 to 9.2 mg/kg. These concentrations are above the EPA RSL but below typical background levels for California (Bradford, 1996). Laboratory reports are presented in Appendix A.

#### **DISCUSSION**

While analytes were detected in the soil samples, none of the reported concentrations exceeded the applicable screening levels or typical background levels for the area. Based on the independent laboratory results, it is our opinion that the Property has not been significantly impacted by past agricultural activities and is suitable for redevelopment.

If you have any questions regarding this report, please do not hesitate to contact us.

Sincerely,

**ENGEO** Incorporated

Scott Johns, PE

Attachments: Figures

Scott Johns

Appendix A – Laboratory Analysis Report

Shawn Munger, CHG







BASE MAP SOURCE: GOOGLE EARTH PRO



2014

VICINITY MAP 213 ENTERPRISE ROAD HOLLISTER, CALIFORNIA PROJECT NO.: 11227,000,000

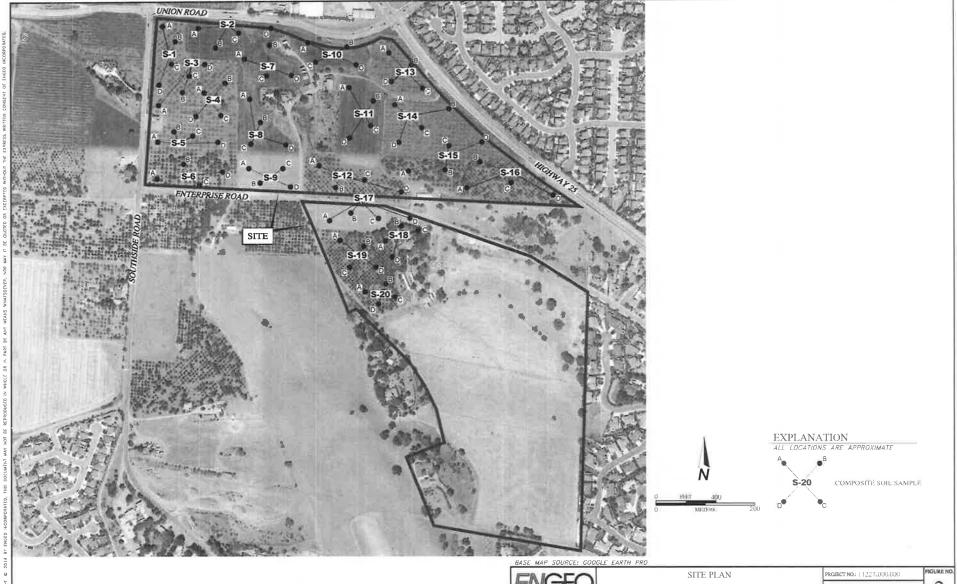
SCALE: AS SHOWN

DRAWN BY: SRP

1

FIGURE NO.

CHECKED BY: SM



213 ENTERPRISE ROAD HOLLISTER, CALIFORNIA SCALE: AS SHOWN DRAWN BY: LL

CHECKED BY: BF



### APPENDIX A

**Laboratory Analysis Report** 

3249 Fitzgerald Road Rancho Cordova, CA 95742

December 18, 2014

CLS Work Order #: CXL0724 COC #:

Shawn Munger Engeo- San Ramon 2010 Crow Canyon Pl. suite 250 San Ramon, CA 94583

Project Name: Enterprise Road Hollister

Enclosed are the results of analyses for samples received by the laboratory on 12/11/14 16:20. Samples were analyzed pursuant to client request utilizing EPA or other ELAP approved methodologies. I certify that the results are in compliance both technically and for completeness.

Analytical results are attached to this letter. Please call if we can provide additional assistance.

Sincerely,

James Liang, Ph.D. Laboratory Director

CA DOHS ELAP Accreditation/Registration number 1233

Page 1 of 30

12/18/14 14:01

Engeo- San Ramon

2010 Crow Canyon Pl, suite 250

San Ramon, CA 94583

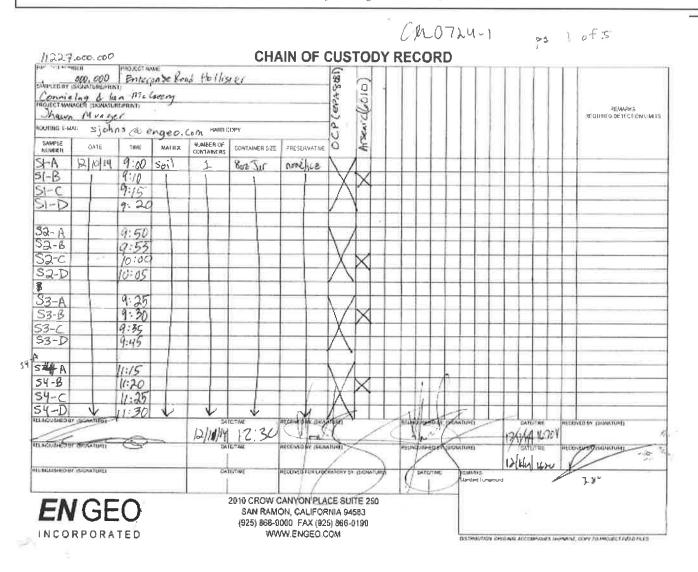
Project: Enterprise Road Hollister

Project Number: 11227,000,000

Project Manager: Shawn Munger

CLS Work Order #: CX1.0724

COC #:



Page 2 of 30

12/18/14 14:01

Engeo- San Ramon

2010 Crow Canyon Pl. suite 250

San Ramon, CA 94583

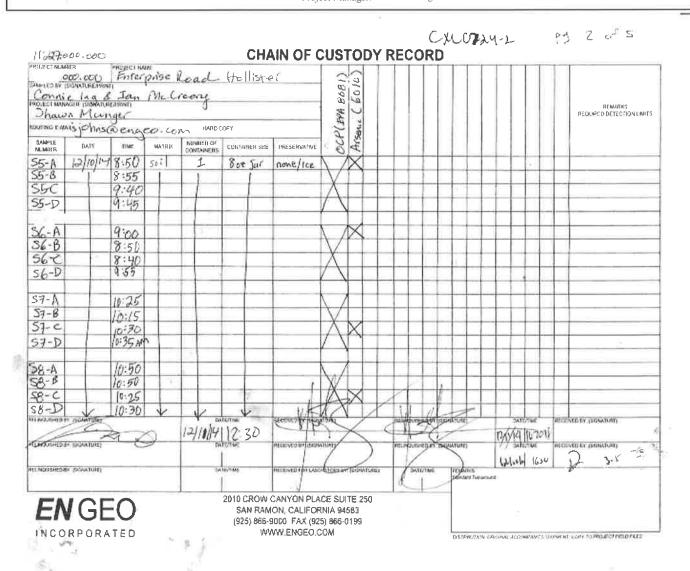
Project: Enterprise Road Hollister

Project Number: 11227 000 000

Project Manager: Shawn Munger

CLS Work Order #: CXL0724

COC #:



Page 3 of 30 12/18/14 14:01

Engeo- San Ramon

San Ramon, CA 94583

Project: Enterprise Road Hollister

2010 Crow Canyon Pl. suite 250

Project Number: 11227,000,000 Project Manager: Shawn Munger CLS Work Order #: CXL0724

COC #:

CXLC724-3 **CHAIN OF CUSTODY RECORD** Enterpise Road Hollister Connie Ira & I. Thawn Minger OCP (FIR REQUIRED CONTROL OF THE CONTROL OF T Arsenic Sjohns @ engeo. Con SAMPLE NUMBER ۵ CONTAINERS CONTAINERS SUE MATRIX 12/10/14 1:55 PM Soil 520-A 802 Jar nonelice 30-B 2:00 PM 300-C1 14:05 520-D 19:10 59-A 8:354 S9-B 59 - C 59 - D 10:15 8:30 S10-A SIO- B 11:50 810- C 1:40 510-D 511-B 12:30 12:35 sil-V 12:40 14/11/14/ 12:30 WELLOW TO CHARLES 2010 CROW CANYON PLACE SUITE 250 SAN RAMON, CALIFORNIA 94583 (925) 866-9000 FAX (925) 866-0199 INCORPORATED WWW.ENGEO.COM

Page 4 of 30

12/18/14 14:01

Engeo- San Ramon

2010 Crow Canyon Pl. suite 250

San Ramon, CA 94583

Project: Enterprise Road Hollister

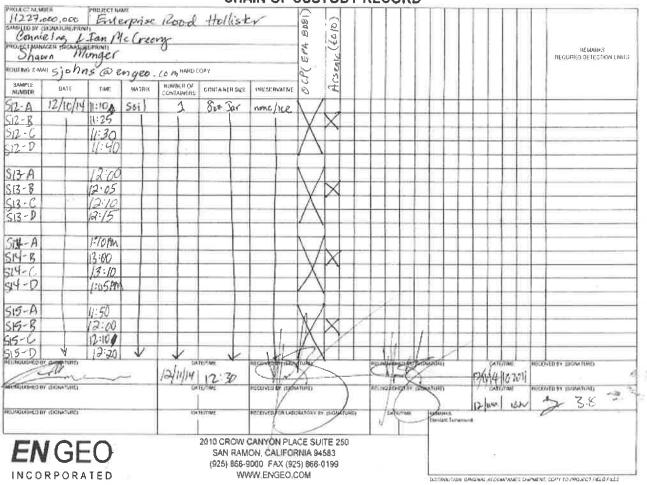
Project Number: 11227,000,000

Project Manager: Shawn Munger

CLS Work Order #: CXL0724

COC #:

CHAIN OF CUSTODY RECORD



Page 5 of 30

12/18/14 14:01

Engeo- San Ramon

2010 Crow Canyon Pl. suite 250

San Ramon, CA 94583

Project: E

Enterprise Road Hollister

Project Number: 11227\_000\_000

Project Manager: Shawn Munger

CLS Work Order #: CXL0724

COC#:

CALL)24-5 pg 50= 5 **CHAIN OF CUSTODY RECORD** DIDECTHONER

11227, 800, COU Enterprise Food, Hollister

Connie I no L Fan Mc Croery

PROJECTHONOR PROJECTION

Shawn Munger まないといの REMARKS REQUIRED DE TEOTION LIAMES BUTHO E WAL 5 johns @ engeo. Com 1440 com NUMBER OF CONTAINERS TMAE CONTAINER SIZE S-16-A 12/10/14 /2:30 soil 800500 nanclice 516-B 12:40 12:50 516-C 517-A 517-B 14:15 14:20 517-C 517-P SIB-A 14:28 518-6 14:25 S18-C S18-D 4:30 519-B TELEFORE TRESPERSIONE 2010 CROW CANYON PLACE SUITE 250 SAN RAMON, CALIFORNIA 94583 (925) 866-9000 FAX (925) 866-0199 INCORPORATED WWW.ENGEO.COM DESTRUCTION DESCRIPT ACCOUNTAGES SHAWNY, COPY TO PARCHOL PERDICAGE

Page 6 of 30 12/18/14 14:01

Engeo- San Ramon

Project: Enterprise Road Hollister

2010 Crow Canyon Pl. suite 250 San Ramon, CA 94583 Project Number: 11227.000.000 Project Manager: Shawn Munger CLS Work Order #: CXL0724

COC #:

#### Metals by EPA 6000/7000 Series Methods

| Analyte                  |                         | Result     | Reporting<br>Limit | Units  | Dilution | Batch   | Prepared | Analyzed | Method   | Notes |
|--------------------------|-------------------------|------------|--------------------|--------|----------|---------|----------|----------|----------|-------|
| S1 - B (CXL0724-02) Soil | Sampled: 12/10/14 09:10 | Received:  | 12/11/14 16:       | 20     |          |         |          |          |          |       |
| Arsenic                  |                         | 9.2        | 1.0                | mg/kg  | 10       | CX08883 | 12/12/14 | 12/12/14 | EPA 6020 |       |
| S2 - C (CXL0724-08) Soil | Sampled: 12/10/14 10:00 | Received:  | 12/11/14 16:       | 20     |          |         |          |          |          |       |
| Arsenic                  |                         | 8.0        | 1.0                | mg/kg  | 10       | CX08883 | 12/12/14 | 12/12/14 | EPA 6020 |       |
| S3 - B (CXL0724-12) Soil | Sampled: 12/10/14 09:30 | Received:  | 12/11/14 16:       | 20     |          |         |          |          |          |       |
| Arsenic                  |                         | 7.1        | 1_0                | mg/kg  | 10       | CX08883 | 12/12/14 | 12/12/14 | EPA 6020 |       |
| S4 - B (CXL0724-17) Soil | Sampled: 12/10/14 11:20 | Received:  | 12/11/14 16:       | 20     |          |         |          |          |          |       |
| Arsenic                  |                         | 7.1        | 1.0                | mg/kg  | 10       | CX08883 | 12/12/14 | 12/12/14 | EPA 6020 |       |
| S5 - A (CXL0724-21) Soil | Sampled: 12/10/14 08:50 | Received:  | 12/11/14 16:       | 20     |          |         |          |          |          |       |
| Arsenic                  |                         | 6.2        | 1.0                | mg/kg  | 10       | CX08883 | 12/12/14 | 12/12/14 | EPA 6020 |       |
| S6 - A (CXL0724-26) Soil | Sampled: 12/10/14 09:00 | Received   | 12/11/14 16:       | 20     |          |         |          |          |          |       |
| Arsenic                  |                         | 7.8        | 1.0                | ıng/kg | 10       | CX08883 | 12/12/14 | 12/12/14 | EPA 6020 |       |
| S7 - C (CXL0724-33) Soil | Sampled: 12/10/14 10:30 | Received   | 12/11/14 16:       | 20     |          |         |          |          |          |       |
| Arsenic                  |                         | 6.2        | 1,0                | mg/kg  | 10       | CX08883 | 12/12/14 | 12/12/14 | EPA 6020 |       |
| S8 - C (CXL0724-38) Soil | Sampled: 12/10/14 10:25 | Received   | 12/11/14 16:       | 20     |          |         |          |          |          |       |
| Arsenic                  |                         | 6.6        | 1.0                | mg/kg  | 10       | CX08883 | 12/12/14 | 12/12/14 | EPA 6020 |       |
| S20 - D (CXL0724-44) Soi | Sampled: 12/10/14 14:10 | 0 Received | 1: 12/11/14 16     | 5:20   |          |         |          |          |          |       |
| Arsenic                  |                         | 2.5        | 1.0                | ıng/kg | 10       | CX08883 | 12/12/14 | 12/12/14 | EPA 6020 |       |

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Engeo- San Ramon

San Ramon, CA 94583

Project: Enterprise Road Hollister

2010 Crow Canyon Pl. suite 250

Project Number: 11227,000,000 Project Manager: Shawn Munger CLS Work Order #: CXL0724

COC#:

### Metals by EPA 6000/7000 Series Methods

| Analyte                   |                         | Result    | Reporting<br>Limit | Units | Dilution | Batch   | Prepared | Analyzed | Method   | Notes |
|---------------------------|-------------------------|-----------|--------------------|-------|----------|---------|----------|----------|----------|-------|
| S9 - B (CXL0724-47) Soil  | Sampled: 12/10/14 08:35 | Received: | 12/11/14 16:       | 20    |          |         |          |          |          |       |
| Arsenic                   |                         | 4.9       | 1.0                | mg/kg | 10       | CX08883 | 12/12/14 | 12/12/14 | EPA 6020 |       |
| S10 - B (CXL0724-52) Soil | Sampled: 12/10/14 11:50 | Received  | : 12/11/14 16      | :20   |          |         |          |          |          |       |
| Arsenic                   |                         | 2.6       | 1.0                | mg/kg | 10       | CX08883 | 12/12/14 | 12/12/14 | EPA 6020 |       |
| S11 - C (CXL0724-58) Soil | Sampled: 12/10/14 12:35 | Received  | : 12/11/14 16      | :20   |          |         |          |          |          |       |
| Arsenic                   |                         | 3.1       | 1.0                | mg/kg | 10       | CX08883 | 12/12/14 | 12/12/14 | EPA 6020 |       |
| S12 - B (CXL0724-62) Soil | Sampled: 12/10/14 11:25 | Received  | : 12/11/14 16      | :20   |          |         |          |          |          |       |
| Arsenic                   |                         | 5.6       | 1_0                | mg/kg | 10       | CX08883 | 12/12/14 | 12/12/14 | EPA 6020 |       |
| S13 - B (CXL0724-67) Soil | Sampled: 12/10/14 12:05 | Received  | : 12/11/14 16      | :20   |          |         |          |          |          |       |
| Arsenic                   |                         | 2.9       | 1_0                | mg/kg | 10       | CX08883 | 12/12/14 | 12/12/14 | EPA 6020 |       |
| S14 - B (CXL0724-72) Soil | Sampled: 12/10/14 13:00 | Received  | : 12/11/14 16      | :20   |          |         |          |          |          |       |
| Arsenic                   |                         | 4.1       | 1_0                | mg/kg | 10       | CX08883 | 12/12/14 | 12/12/14 | EPA 6020 |       |
| S15 - B (CXL0724-77) Soil | Sampled: 12/10/14 12:00 | Received  | : 12/11/14 16      | :20   |          |         |          |          |          |       |
| Arsenic                   |                         | 2.3       | 1.0                | mg/kg | 10       | CX08883 | 12/12/14 | 12/12/14 | EPA 6020 |       |
| S16 - D (CXL0724-84) Soil | Sampled: 12/10/14 12:55 | Received  | : 12/11/14 16      | :20   |          |         |          |          |          |       |
| Arsenic                   |                         | 3.2       | 1.0                | mg/kg | 10       | CX08883 | 12/12/14 | 12/12/14 | EPA 6020 |       |
| S17 - B (CXL0724-87) Soil | Sampled: 12/10/14 14:20 | Received  | 12/11/14 16        | :20   |          |         |          |          |          |       |
| Arsenic                   |                         | 3.5       | 10                 | mg/kg | 10       | CX08883 | 12/12/14 | 12/12/14 | EPA 6020 |       |

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Engeo- San Ramon

Project: Enterprise Road Hollister

2010 Crow Canyon Pl. suite 250 San Ramon, CA 94583 Project Number: 11227\_000\_000

CLS Work Order #: CXL0724

Project Manager: Shawn Munger COC

### Metals by EPA 6000/7000 Series Methods

| Analyte                   |                         | Result    | Reporting<br>Limit | Units | Dilution | Batch   | Prepared | Analyzed | Method   | Notes |
|---------------------------|-------------------------|-----------|--------------------|-------|----------|---------|----------|----------|----------|-------|
| S18 - C (CXL0724-93) Soil | Sampled: 12/10/14 14:30 | Received: | 12/11/14 16        | :20   |          |         |          |          |          |       |
| Arsenic                   |                         | 2.7       | 1.0                | mg/kg | 10       | CX08883 | 12/12/14 | 12/12/14 | EPA 6020 |       |
| S19 - C (CXL0724-98) Soil | Sampled: 12/10/14 14:00 | Received: | 12/11/14 16        | :20   |          |         |          |          |          |       |
| Arsenic                   |                         | 4.4       | 1.0                | mg/kg | 10       | CX08883 | 12/12/14 | 12/12/14 | EPA 6020 |       |

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San Ramon, CA 94583

Project: Enterprise Road Hollister

2010 Crow Canyon Pl. suite 250

Project Number: 11227,000,000 Project Manager: Shawn Munger CLS Work Order #: CXL0724

COC #:

| Analyte                              | Result                  | Reporting<br>Limit | Units      | Dilution  | Batch     | Prepared | Analyzed | Method         | Notes |
|--------------------------------------|-------------------------|--------------------|------------|-----------|-----------|----------|----------|----------------|-------|
| S1 - A-D Composite (CXL0724-05) Soil |                         |                    |            |           | Batch     | Терагец  | Analyzeu | Wiethod        | Notes |
| Aldrin                               |                         |                    | _          |           | GM 0000 I |          |          |                |       |
| alpha-BHC                            | ND<br>ND                | 2.0                | μg/kg<br>" | 2         | CX08894   | 12/12/14 | 12/15/14 | EPA 8081A      |       |
| beta-BHC                             | ND<br>ND                | 4.0                | **         | 144       | w         |          |          | . 49.          |       |
| delta-BHC                            | ND                      | 20<br>20           | ж          |           | w.        | -        | *        |                |       |
| gamma-BHC (Lindane)                  | ND                      | 20                 | ŵ.         |           | н         |          |          | 0.40           |       |
| Chlordane-technical                  | 110                     | 40                 | W          |           | **        |          | -        |                |       |
| 4,4 -DDD                             | ND                      | 15                 |            | т.        |           |          | 100      | 57443          |       |
| 4,4'-DDE                             | 110                     | 38                 |            | 5         | W:        |          | . 10     | **             |       |
| 4,4'-DDT                             | ND                      | 15                 | **         | 2         | *         |          | *        | 5W2            |       |
| Dieldrin                             | 2.2                     | 2.0                | #          | *         | #         | e e      | 100      | (40)           |       |
| Endosulfan I                         | ND                      | 30                 |            | <b>**</b> | ¥         | *        |          | **             |       |
| Endosulfan II                        | ND                      | 30                 | *          |           |           |          |          |                |       |
| Endosulfan sulfate                   | ND                      | 30                 | **         | н.        | **        | W        | **       | 34             |       |
| Endrin                               | ND                      | 30                 | **         |           | #         | <b>3</b> | 36       | 1940           |       |
| Endrin aldehyde                      | ND                      | 30                 | ₩.         | **        | #         |          | W        | !/ <b>m</b> ?! |       |
| Heptachlor                           | ND                      | 10                 | <b>10</b>  |           | ***       | 77       | ₩        |                |       |
| Heptachlor epoxide                   | ND                      | 4.0                | Ĥ.         | H         | 77        |          | 7        | 100            |       |
| Methoxychlor                         | ND                      | 30                 | 95         | 17.       | **        | 36       | *        | 500.0          |       |
| Mirex                                | ND                      | 20                 | **5        | #         | **        | W        | •        | **             |       |
| Гохарhene                            | ND                      | 40                 |            | HI.       | #0.       | H        | *        | (40)           |       |
| Surrogate: Tetrachloro-meta-xylene   |                         | 50 %               | 46         | -139      |           | *        |          | (#)            |       |
| Surrogate: Decachlorobiphenyl        |                         | 34 %               |            | -141      | m         | ж        | (#67)    | (96)           | QS-   |
| S2 - A-D Composite (CXL0724-10) Soil | Sampled: 12/10/14 09:50 | Received           | : 12/11/1  | 4 16:20   |           |          |          |                |       |
| Aldrin                               | ND                      | 2.0                | μg/kg      | 2         | CX08894   | 12/12/14 | 12/15/14 | EPA 8081A      |       |
| ılpha-BHC                            | ND                      | 4.0                | 1100       | *5        | 196       | **       | w        | 30003          |       |
| peta-BHC                             | ND                      | 20                 | ( #)       | 91        | 1000      | *        | W        | 94e li         |       |
| lelta-BHC                            | ND                      | 20                 | THE        |           |           | *        | **       | w              |       |
| gamma-BHC (Lindane)                  | ND                      | 20                 | u          | ¥.        |           | **       | #        |                |       |
| Chlordane-technical                  | 260                     | 40                 | •          | *         | (10)      | **       | 7.00     | 141            |       |

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Engeo- San Ramon

Project: Enterprise Road Hollister

2010 Crow Canyon Plusuite 250 San Ramon, CA 94583 Project Number: 11227,000,000
Project Manager: Shawn Munger

CLS Work Order #: CXL0724

COC #:

### Organochlorine Pesticides by EPA Method 8081A

| Analyte                              | Result                  | Reporting<br>Limit | Units      | Dilution | Batch                | Prepared | Analyzed | Method    | Notes |
|--------------------------------------|-------------------------|--------------------|------------|----------|----------------------|----------|----------|-----------|-------|
| S2 - A-D Composite (CXL0724-10) Soil | Sampled: 12/10/14 09:50 | Received           | : 12/11/1  | 4 16:20  |                      |          |          |           |       |
| 4,4 -DDD                             | ND                      | 15                 | μg/kg      | 2        | CX08894              |          | 12/15/14 | EPA 8081A |       |
| 4,4′-DDE                             | 370                     | 150                | **         | 20       |                      | 9.89     | *        |           |       |
| 4,4′-DDT                             | 64                      | 15                 | 200        | 2        | 177                  | 0.00     | .17      | 77        |       |
| Dieldrin                             | 4.8                     | 2.0                |            | U        | (0)                  | 3.46     | 111      | **        |       |
| Endosulfan I                         | ND                      | 30                 | 363        | 2007     | (1 <del>1)</del> (1) | **       | 1300     | **        |       |
| Endosulfan II                        | ND                      | 30                 |            | **       | 140                  | *        |          | in .      |       |
| Endosulfan sulfate                   | ND                      | 30                 |            | **       |                      | 0.990    | (*)      | <u> </u>  |       |
| Endrin                               | ND                      | 30                 |            | . 11     | (7.0)                | 0.00(0   |          | T.        |       |
| Endrin aldehyde                      | ND                      | 30                 | 390        | (#)      | 11911                | 3840     | 0.00     |           |       |
| Heptachlor                           | ND                      | 10                 | 300        | - 0      | 01000                | 1144     | 5(m)     | w         |       |
| Heptachlor epoxide                   | ND                      | 4.0                | 300        | . 46     | 114411               | **       |          | 764       |       |
| Methoxychlor                         | ND                      | 30                 | **         |          | **                   |          | -        | **        |       |
| Mirex                                | ND                      | 20                 | **         | .**      | (4)                  | 5.993    |          |           |       |
| Toxaphene                            | ND                      | 40                 | 13#1       | (3.99)   | <b>.</b> #5          | (10)     |          | 77        |       |
| Surrogate: Tetrachloro-meta-xylene   |                         | 82 %               | 40         | 5-139    | TWO                  | 4        | W        | W.C       |       |
| Surrogate: Decachlorobiphenyl        |                         | 61%                | 52         | ?-141    |                      |          | *        |           |       |
| S3 - A-D Composite (CXL0724-15) Soil | Sampled: 12/10/14 09:25 | Received           | l: 12/11/1 | 4 16:20  |                      |          |          |           |       |
| Aldrin                               | ND                      | 2.0                | μg/kg      | 2        | CX08894              | 12/12/14 | 12/15/14 | EPA 8081A |       |
| alpha-BHC                            | ND                      | 4.0                |            |          | 38                   |          | 144      |           |       |
| beta-BHC                             | ND                      | 20                 | 99         |          | **                   | 1.96     | **       | 36        |       |
| delta-BHC                            | ND                      | 20                 | 1990       | 3392     | (29.2                | ( 0)     | 277      | .77       |       |
| gamma-BHC (Lindane)                  | ND                      | 20                 | (0)        | ((#))    | 300                  | 100      |          | .9        |       |
| Chlordane-technical                  | 150                     | 40                 | 1967       | 2340     | 1941                 | - 67     | 46.7     | 99        |       |
| 4,4´-DDD                             | ND                      | 15                 | ù.         |          |                      |          | **       | /4        |       |
| 4,4´-DDE                             | 180                     | 75                 |            | 10       |                      | I Mi     | 140      | -         |       |
| 4,4´-DDT                             | 19                      | 15                 | . 95       | 2        | 580                  | м.       | 290      | 177       |       |
| Dieldrin                             | 3.8                     | 2.0                | 60         | п        | 300                  | W        | 300      | 20        |       |
| Endosulfan I                         | ND                      | 30                 | #          | 1000     | 59                   | **)      | F 942    | M         |       |
|                                      |                         | 30                 | *          |          |                      |          | u.       | 44        |       |

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Engeo- San Ramon

2010 Crow Canyon Pl, suite 250

San Ramon, CA 94583

Project: Enterprise Road Hollister

Project Number: 11227,000,000 Project Manager: Shawn Munger CLS Work Order #: CXL0724

COC #:

| Analyte                              | Result                  | Reporting<br>Limit | Units      | Dilution | Batch      | Prepared       | Analyzed | Method              | Notes |
|--------------------------------------|-------------------------|--------------------|------------|----------|------------|----------------|----------|---------------------|-------|
| S3 - A-D Composite (CXL0724-15) Soil | Sampled: 12/10/14 09:25 | Received           | l: 12/11/1 | 4 16:20  |            |                |          |                     |       |
| Endosulfan sulfate                   | ND                      | 30                 | μg/kg      | 2        | CX08894    |                | 12/15/14 | EPA 8081A           |       |
| Endrin                               | ND                      | 30                 | 20         |          | *          |                | **       | 100                 |       |
| Endrin aldehyde                      | ND                      | 30                 | (##        | 34       | **         | **             | ja .     | 40.                 |       |
| Heptachlor                           | ND                      | 10                 | 36         |          | -          | 177            | 9        | (10)                |       |
| Heptachlor epoxide                   | ND                      | 4.0                | 98         | 77       |            |                | 77       | 246                 |       |
| Methoxychlor                         | ND                      | 30                 | -22.       | 22       | 395        | 9              | 299      | (1 <b>44</b> );     |       |
| Mirex                                | ND                      | 20                 | 144        | **       | **         |                | *        | ((44)               |       |
| Toxaphene                            | ND                      | 40                 | **         | **       | #          |                | W.       | Tall                |       |
| Surrogate: Tetrachloro-meta-xylene   |                         | 50 %               | 46         | 5-139    |            | 39             | (8)      | . M.S.              |       |
| Surrogate: Decachlorobiphenyl        |                         | 27 %               | 52         | ?-141    | .**        | 599            | 3#8      | (0.46)              | QS-   |
| S4 - A-D Composite (CXL0724-20) Soil | Sampled: 12/10/14 11:15 | Received           | : 12/11/1  | 4 16:20  |            |                |          |                     |       |
| Aldrin                               | ND                      | 2.0                | μg/kg      | 2        | CX08894    | 12/12/14       | 12/15/14 | EPA 8081A           |       |
| alpha-BHC                            | ND                      | 4.0                |            | 22.      | #          | \w.            | 29       | 1,00                |       |
| beta-BHC                             | ND                      | 20                 | ×          | ж.       | **         | H              | *        | (( <del>40</del> )) |       |
| delta-BHC                            | ND                      | 20                 | **         | ×        | **         | **             | *        | 1940                |       |
| gamma-BHC (Lindane)                  | ND                      | 20                 | **         | ж        | **         | $\overline{x}$ | *        | **                  |       |
| Chlordane-technical                  | 160                     | 40                 | *          | (#)      | *          | 395            | w        | 100                 |       |
| 4,4´-DDD                             | ND                      | 15                 |            | 75       |            | 300            | **       | 2963                |       |
| 4,4´-DDE                             | 230                     | 75                 | #6         | 10       | <b>#</b> 2 | W              | (20%     | ) <b>**</b>         |       |
| 4,4′-DDT                             | 17                      | 15                 |            | 2        | <b>6</b> 0 | *              | 200      | 300                 |       |
| Dieldrin                             | 3.8                     | 2.0                | #          | **       | 95         | <b>W</b>       |          |                     |       |
| Endosulfan I                         | ND                      | 30                 | *          | #        | *          | 27.            | ×        |                     |       |
| Endosulfan II                        | ND                      | 30                 |            |          | 77.        | w              | #.       | (#).f               |       |
| Endosulfan sulfate                   | ND                      | 30                 | #6         | #1       | <b>W</b> . | W              | ₩.       | [[00]]              |       |
| Endrin                               | ND                      | 30                 | **         | **       | ¥47        | *              | **       | 1991                |       |
| Endrin aldehyde                      | ND                      | 30                 | **         | <b>H</b> | 10         |                | *        | (ab)                |       |
| Heptachlor                           | ND                      | 10                 | *          |          | **         |                | <b>#</b> | .00                 |       |
| Heptachlor epoxide                   | ND                      | 4.0                | 95         | 25       | **         | M.             | **       | 2001                |       |
| Methoxychlor                         | ND                      | 30                 | 100        | 16       | •          | ×              | .00      | 200                 |       |

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San Ramon, CA 94583

Project: Enterprise Road Hollister

2010 Crow Canyon Pl. suite 250

Project Number: 11227,000,000 Project Manager: Shawn Munger CLS Work Order #: CXL0724

COC #:

| Analyte  | Result                  | Reporting<br>Limit | Units              | Dilution            | Batch            | Prepared | Analyzed | Method    | Notes |
|--|-------------------------|--------------------|--------------------|---------------------|------------------|----------|----------|-----------|-------|
| S4 - A-D Composite (CXL0724-20) Soil                             | Sampled: 12/10/14 11:15 | Received           | l: <b>12/11</b> /1 | 14 16:20            |                  |          |          |           |       |
| Mirex  | ND                      | 20                 | μg/kg              | 2                   | CX08894          | (1997)   | 12/15/14 | EPA 8081A |       |
| Toxaphene  | ND                      | 40                 | 5.05               | \( <del>!!</del> )} | 5/#15            | - 000    | 0.00     |           |       |
| Surrogate: Tetrachloro-meta-xylene                               |                         | 72 %               | 4                  | 6-139               | 545              | 02       | w        | ) Al      |       |
| Surrogate: Tetrachioro-meta-xytene Surrogate: Decachlorobiphenyl |                         | 49 %               |                    | 2-141               | (#)              | 170      | a a      | -         | OS-   |
| Surrogute. Decuction outpitenyi                                  |                         | 42.70              | 32                 | 2-141               |                  |          |          |           | 20-   |
| S5 - A-D Composite (CXL0724-25) Soil                             | Sampled: 12/10/14 08:50 | Received           | l: 12/11/1         | 14 16:20            |                  |          |          |           |       |
| Aldrin   | ND                      | 2.0                | μg/kg              | 2                   | CX08894          | 12/12/14 | 12/15/14 | EPA 8081A |       |
| alpha-BHC  | ND                      | 4.0                | **                 | Add                 | **               | 4.99     |          | **        |       |
| beta-BHC   | ND                      | 20                 | **                 | 77                  | w                | 396      | **       | 98        |       |
| delta-BHC  | ND                      | 20                 | (.41)              | Attil               | ((0))            | 0,965    | 5.00     | .00       |       |
| gamma-BHC (Lindane)  | ND                      | 20                 | 300                | ((44))              | (1991)           | 000      | (34)     | 99        |       |
| Chlordane-technical  | 67                      | 40                 | 000                | 19447               | 5002             |          | (64      | (ee       |       |
| 4,4´-DDD   | ND                      | 15                 | **                 | 41                  | (4)              | **       | **       | 99        |       |
| 4,4'-DDE   | 140                     | 38                 |                    | 5                   | *                | 5595     | ě        | ₩.        |       |
| 4,4′-DDT   | ND                      | 15                 | 2.2%               | 2                   | 3897             | 0.00     | .7       |           |       |
| Dieldrin   | 2.3                     | 2.0                | (0)                | 99                  | (0)              | 1040     | .8       | 175       |       |
| Endosulfan I   | ND                      | 30                 | 0000               | 2:00                | (044)            | 48       | ::#::    | ж         |       |
| Endosulfan II  | ND                      | 30                 | 100                | 41                  | 77411            | -        | 1941     | "         |       |
| Endosulfan sulfate   | ND                      | 30                 |                    |                     |                  | 1(95)    | . **     | *         |       |
| Endrin   | ND                      | 30                 | w                  | 100                 | (77)             | 20992    | **       | 77        |       |
| Endrin aldehyde  | ND                      | 30                 | 3.90               | 493                 | 11#11            | 2540     | 10#10    | **        |       |
| Heptachlor   | ND                      | 10                 | 0000               | 540                 | ((**))           | in       | : [4]    | *         |       |
| Heptachlor epoxide   | ND                      | 4.0                | 1.44               | 200                 | 1140             | M        | 046      | **        |       |
| Methoxychlor   | ND                      | 30                 | **                 |                     | *                | 1,99     | *        | 94        |       |
| Mirex  | ND                      | 20                 | (17)               | (0)                 | (77)             | 5965     | **       | T.        |       |
| Toxaphene  | ND                      | 40                 | (5 <del>11</del> ) | 3.0%                | 181              | Cast     | 19#0     | *         |       |
| Surrogate: Tetrachloro-meta-xylene                               |                         | 81%                | 4                  | 6-139               |                  | · m      | **       | (in)      |       |
| Surrogate: Decachlorobiphenyl                                    |                         | 63 %               | 5.                 | 2-141               | ( <del>9</del> ) | 195      | *        | m.        |       |

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Engeo- San Ramon

San Ramon, CA 94583

Project: Enterprise Road Hollister

2010 Crow Canyon Pl. suite 250

Project Number: 11227,000,000 Project Manager: Shawn Munger CLS Work Order #: CXL0724

COC #:

| Sef-A-D Composite (CXL0724-30) Soil  | Analyte                              | Result                  | Reporting<br>Limit | Units      | Dilution | Batch       | Prepared | Analyzed | Method    | Notes |
|--|--------------------------------------|-------------------------|--------------------|------------|----------|-------------|----------|----------|-----------|-------|
| Alpha-BHC  | S6 - A-D Composite (CXL0724-30) Soil | Sampled: 12/10/14 08:40 | Received           | l: 12/11/1 | 4 16:20  |             |          |          |           |       |
| Delica BHC   ND   20   "   "   "   "   "   "   "   "   "   | Aldrin                               | ND                      | 2.0                | μg/kg      | 2        | CX08894     | 12/12/14 | 12/15/14 | EPA 8081A |       |
| delta-BHC ND 20 " " " " " " " " " " " " " " " " " "  | alpha-BHC                            | ND                      | 4.0                | .27        | 395      | 38          | 900      | 199      | ***       |       |
| Samma-BHC (Lindane)   ND   20   "  | peta-BHC                             | ND                      | 20                 | 711        |          | (#          | **       | ÷        | #0        |       |
| Mathematical   Math | delta-BHC                            | ND                      | 20                 | 744        | 99       | **          | *        |          |           |       |
| 4,4'-DDD   | gamma-BHC (Lindane)                  | ND                      | 20                 |            |          | <u> </u>    | .40.1    | *        |           |       |
| 100   38   | Chlordane-technical                  | 41                      | 40                 | *          | ₩        | 77          | **       | 77.      | 1.00      |       |
| A4-DDT   | 1,4´-DDD                             | ND                      | 15                 | 37.        | 325      | **          | 79       | W        |           |       |
| Dieldrin   ND   2.0  | 1,4'-DDE                             | 100                     | 38                 | 395        | 5        | <b>36</b> . | 1.0      | 60       | 5,465     |       |
| Endosulfan I   ND   30   | 1,4´-DDT                             | ND                      | 15                 | 34.        | 2        | H           |          | **       | 104/      |       |
| Endosulfan II ND 30 " " " " " " " " " " " " " " " " " "  | Dieldrin                             | ND                      | 2.0                | 54         | п        | *           |          | *        | **        |       |
| Endosulfan sulfate ND 30 " " " " " " " " " " " " " " " " " "   | Endosulfan I                         | ND                      | 30                 | *          | Ħ        | #           |          |          |           |       |
| Endrin ND 30 " " " " " " " " " " " " " " " " " "   | Endosulfan II                        | ND                      | 30                 |            |          |             | »        | :#       | 2000      |       |
| Endrin aldehyde ND 30 " " " " " " " " " " " " " " " " " "  | Endosulfan sulfate                   | ND                      | 30                 | 38         | W        | 99.         | W        | .#       | 3900      |       |
| Heptachlor         ND         10         "         <   | Endrin                               | ND                      | 30                 | *          | ж        | **          |          | **       | 500       |       |
| Heptachlor epoxide   | Endrin aldehyde                      | ND                      | 30                 | W          | 90       | **          | 77       |          | *         |       |
| Methoxychlor         ND         30         "   | Heptachlor                           | ND                      | 10                 | <u>**</u>  | 70       | +           | 29       | 9        |           |       |
| ND   20    "   | leptachlor epoxide                   | ND                      | 4.0                | #          | 7        |             | 39       |          | B#4       |       |
| Toxaphene ND 40 " " " " " " " " " " " " " " " " " "  | Methoxychlor                         | ND                      | 30                 | 25         | **:      | 49          | **       | ×        | ((10))    |       |
| Surrogate: Tetrachloro-meta-xylene 61 % 46-139 " " " " " " " " " " " " " " " " " " "   | Mirex                                | ND                      | 20                 | 346        | **       | HE          | **       | Ä        | 11411     |       |
| Surrogate: Decachlorobiphenyl         29 %         52-141         "  | oxaphene                             | ND                      | 40                 | **         | **)      | *           | *        | н        | 0         |       |
| S7 - A-D Composite (CXL0724-35) Soil Sampled: 12/10/14 10:15 Received: 12/11/14 16:20  Aldrin ND 2.0 μg/kg 2 CX08894 12/12/14 12/15/14 EPA 8081 A alpha-BHC ND 4.0 " " " " " " " " " beta-BHC ND 20 " " " " " " " " " " delta-BHC ND 20 " " " " " " " " " " " " " " " " " "  | urrogate: Tetrachloro-meta-xylene    |                         | 61 %               | 46         | -139     | *           | *        | (#6)     | 10.00%    |       |
| Aldrin ND 2.0 μg/kg 2 CX08894 12/12/14 12/15/14 EPA 8081A alpha-BHC ND 4.0 " " " " " " " " " " " " " " " " " " "   | urrogate: Decachlorobiphenyl         |                         | 29 %               | 52         | -141     | *           | H        | (96)     | 200       | QS-4  |
| alpha-BHC       ND       4.0       " <t< td=""><td>7 - A-D Composite (CXL0724-35) Soil</td><td>Sampled: 12/10/14 10:15</td><td>Received</td><td>: 12/11/1</td><td>4 16:20</td><td></td><td></td><td></td><td></td><td></td></t<>   | 7 - A-D Composite (CXL0724-35) Soil  | Sampled: 12/10/14 10:15 | Received           | : 12/11/1  | 4 16:20  |             |          |          |           |       |
| beta-BHC         ND         20         "   | Aldrin                               | ND                      | 2.0                | μg/kg      | 2        | CX08894     | 12/12/14 | 12/15/14 | EPA 8081A |       |
| delta-BHC ND 20 " " " " " " " " " " " " " " " " " "  | lpha-BHC                             | ND                      | 4.0                | **         | #.       | #0          | *        | ×        | (967)     |       |
| gamma-BHC (Lindane) ND 20 " " " " "  | eta-BHC                              | ND                      | 20                 |            | #1       | #           | #        | W.       | 100       |       |
|  | elta-BHC                             | ND                      | 20                 | **         | 10       | a.          |          | #        | (46)      |       |
| Chlordane-technical 93 40 " " " " " " " " " " " " " " " " " "  | amma-BHC (Lindane)                   | ND                      | 20                 | **         | ž.       | *           | **       |          | 25.4      |       |
|  | Chlordane-technical                  | 93                      | 40                 | **         | 95       | 1320        | *        | 5,445    | (m):      |       |

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Engeo- San Ramon

Project: Enterprise Road Hollister

2010 Crow Canyon Pl. suite 250 San Ramon, CA 94583 Project Number: 11227,000,000
Project Manager: Shawn Munger

CLS Work Order #: CXL0724

COC #:

| Analyte                              | Result                  | Reporting<br>Limit | Units      | Dilution | Batch   | Prepared | Analyzed | Method         | Notes |
|--------------------------------------|-------------------------|--------------------|------------|----------|---------|----------|----------|----------------|-------|
| S7 - A-D Composite (CXL0724-35) Soil | Sampled: 12/10/14 10:15 | Received           | l: 12/11/1 | 4 16:20  |         |          |          |                |       |
| 4,4*-DDD                             | ND                      | 15                 | μg/kg      | 2        | CX08894 | Ř.       | 12/15/14 | EPA 8081A      |       |
| 4,4′-DDE                             | 82                      | 30                 | **         | 4        |         |          | *        |                |       |
| 4,4′-DDT                             | 17                      | 15                 | 3000       | 2        | 1996    | 9)       | 325.0    |                |       |
| Dieldrin                             | 3.4                     | 2.0                | 5940       | (10)     | ((4))   | W.       | 2003     | 19             |       |
| Endosulfan I                         | ND                      | 30                 |            | . 0      | 202     | <i>W</i> | (60)     | 90             |       |
| Endosulfan II                        | ND                      | 30                 | **         | **       | **      | **       | 10       |                |       |
| Endosulfan sulfate                   | ND                      | 30                 | .99        |          | 3.00    |          | 14       | 44             |       |
| Endrin                               | ND                      | 30                 | 0.00       | 9.9%     | (9)     | 66       |          | ,,             |       |
| Endrin aldehyde                      | ND                      | 30                 | ((#)       | 0.00     | (00)    | H.       | 1990     | **             |       |
| Heptachlor                           | ND                      | 10                 | ((4)       | (00)     | (90)    | #        | ( 0)     | *              |       |
| Heptachlor epoxide                   | ND                      | 4.0                | 146        | 100      | 100     | +        |          | **             |       |
| Methoxychlor                         | ND                      | 30                 |            | **       | (*)     | 10       |          |                |       |
| Mirex                                | ND                      | 20                 |            | 1.77     | . 47    | #3       | 7        | 77             |       |
| Toxaphene                            | ND                      | 40                 | 1995       | 10#0     | 19#6    | #        | MI       | I <del>M</del> |       |
| Surrogate: Tetrachloro-meta-xylene   |                         | 79 %               | 40         | 5-139    | er.     | *        | **       | 300            |       |
| Surrogate: Decachlorobiphenyl        |                         | 72 %               | 52         | 2-141    | *       | **       | *        | iii            |       |
| S8 - A-D Composite (CXL0724-40) Soil | Sampled: 12/10/14 10:25 | Received           | 1: 12/11/1 | 4 16:20  |         |          |          |                |       |
| Aldrin                               | ND                      | 2.0                | μg/kg      | 2        | CX08894 | 12/12/14 | 12/15/14 | EPA 8081A      |       |
| alpha-BHC                            | ND                      | 4.0                | #3         | *        |         | 77       | ěs.      |                |       |
| beta-BHC                             | ND                      | 20                 | m          |          |         | #1       | **       | (8.)           |       |
| delta-BHC                            | ND                      | 20                 | 45         | 1990     | 0.9%    | ¥C       | **       | 1990           |       |
| gamma-BHC (Lindane)                  | ND                      | 20                 | 40         |          | (10)    | ű        | 96       | 2#92           |       |
| Chlordane-technical                  | 91                      | 40                 | 447        | H-       |         | <u> </u> | 200      | (64.5)         |       |
| 4,4'-DDD                             | ND                      | 15                 | *          | **       | *       | 777      | **       | 188            |       |
| 4,4′-DDE                             | 150                     | 38                 | **         | 5        | **      | w        | (40)     | (**)           |       |
| 4,4´-DDT                             | ND                      | 15                 | (4)        | 2        | M.C     | W        | #5       | 775)           |       |
| Dieldrin                             | ND                      | 2.0                | W.         | п        | W1      | 14       | 66       | (1995)         |       |
| Endosulfan I                         | ND                      | 30                 | H.         | **       | **      | **       | **       | 5 <b>6</b> 3.  |       |
|                                      | ND                      | 30                 | **         | **       | 20      |          | 14       | M.             |       |

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Project: Enterprise Road Hollister

2010 Crow Canyon Pl. suite 250

Project Number: 11227 000 000

CLS Work Order #: CXL0724

San Ramon, CA 94583

Project Manager: Shawn Munger

COC #:

| Analyte                               | Result                  | Reporting<br>Limit | Units      | Dilution | Batch   | Prepared       | Analyzed             | Method         | Notes |
|---------------------------------------|-------------------------|--------------------|------------|----------|---------|----------------|----------------------|----------------|-------|
| S8 - A-D Composite (CXL0724-40) Soil  | Sampled: 12/10/14 10:25 | Received           | l: 12/11/1 | 4 16:20  |         |                |                      |                |       |
| Endosulfan sulfate                    | ND                      | 30                 | μg/kg      | 2        | CX08894 | (100)          | 12/15/14             | EPA 8081A      |       |
| Endrin                                | ND                      | 30                 | 1,00       | 39       |         | 100            | 39                   | #1             |       |
| Endrin aldehyde                       | ND                      | 30                 | 100        | 344      | W       | 44             | 174                  | W.             |       |
| Heptachlor                            | ND                      | 10                 |            | 10       |         |                | **                   | <del>R</del> ( |       |
| Heptachlor epoxide                    | ND                      | 4.0                | **         | **       | *       | 2007           | "                    |                |       |
| Methoxychlor                          | ND                      | 30                 | 71         |          | .**     | (M)            | 29                   | 1.00           |       |
| Mirex                                 | ND                      | 20                 | 38         | ***      | **      | 46             |                      | (4)            |       |
| Foxaphene                             | ND                      | 40                 | 94         | **       | 346     | 94             | iii                  | 660            |       |
| Surrogate: Tetrachloro-meta-xylene    |                         | 80 %               | 46         | 5-139    | Ĥ       | 94             | ( <b>19</b> )        | **             |       |
| Surrogate: Decachlorobiphenyl         |                         | 58 %               | 52         | 2-141    | 72      |                | )( <del>17</del> .); | W)             |       |
| S20 - A-D Composite (CXL0724-45) Soil | Sampled: 12/10/14 13;55 | Receive            | d: 12/11/  | 14 16:20 |         |                |                      |                |       |
| Aldrin                                | ND                      | 2.0                | μg/kg      | 2        | CX08894 | 12/12/14       | 12/15/14             | EPA 8081A      |       |
| llpha-BHC                             | ND                      | 4.0                | 77.        |          |         |                | #                    | 200            |       |
| peta-BHC                              | ND                      | 20                 | 25         | 77       | W       | 34             | **                   | 1000           |       |
| telta-BHC                             | ND                      | 20                 | .16        | M:       | ₩.      | An             | **                   | 990            |       |
| gamma-BHC (Lindane)                   | ND                      | 20                 | H          | **       | *       | 77             |                      | **             |       |
| Chlordane-technical                   | ND                      | 40                 | *          | -        | Ħ       | 25             | Ħ                    | .*)            |       |
| -,4'-DDD                              | ND                      | 15                 | 8          | 15       |         |                | 75                   | 3897           |       |
| ,4′-DDE                               | 47                      | 15                 | #          | 49       | **      | **             | (30)                 | ((40))         |       |
| -,4'-DDT                              | ND                      | 15                 | **         | **:      | #.      | *              | **                   | U#U            |       |
| Dieldrin                              | 16                      | 2.0                | **         | #        | ***     | **             |                      | <b>(a)</b>     |       |
| Endosulfan I                          | ND                      | 30                 | **         | **       | **      | #              | **                   | (**)           |       |
| Endosulfan II                         | ND                      | 30                 | **         | 7        |         | **             | ***                  |                |       |
| Endosulfan sulfate                    | ND                      | 30                 | **         | #        | 22.     | 36             | **                   | G#C C          |       |
| Endrin                                | ND                      | 30                 | <b>H</b>   | **       | **      | ü              | #1                   | 0001           |       |
| indrin aldehyde                       | ND                      | 30                 | #          | **       | 60      | ( <del>)</del> | **                   |                |       |
| Ieptachlor                            | ND                      | 10                 | *          | *        | *       | M              | **                   |                |       |
| leptachlor epoxide                    | ND                      | 4.0                | 75         | 75       | **      | ж              | #:                   | 000            |       |
| Methoxychlor                          | ND                      | 30                 | 25         | **       | 115     | ŵ              | w                    | (947)          |       |

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Engeo- San Ramon

San Ramon, CA 94583

Project: Enterprise Road Hollister

2010 Crow Canyon PL suite 250

Project Number: 11227.000.000

CLS Work Order #: CXL0724

Project Manager: Shawn Munger COC #:

| Analyte                               | Result                  | Reporting<br>Limit | Units      | Dilution | Batch        | Prepared | Analyzed      | Method    | Notes      |
|---------------------------------------|-------------------------|--------------------|------------|----------|--------------|----------|---------------|-----------|------------|
| S20 - A-D Composite (CXL0724-45) Soil | Sampled: 12/10/14 13:55 | Receive            | ed: 12/11/ | 14 16:20 |              |          |               |           |            |
| Mirex                                 | ND                      | 20                 | μg/kg      | 2        | CX08894      | (0)      | 12/15/14      | EPA 8081A |            |
| Toxaphene                             | ND                      | 40                 | (17)       | (M)      | ( <b>a</b> . | 3.00     | (**/)         | 7         |            |
| Surrogate: Tetrachloro-meta-xylene    |                         | 75 %               | 46         | 5-139    | 740          | -        | W             | 100       |            |
| Surrogate: Decachlorobiphenyl         |                         | 45 %               | 52         | 2 141    |              |          | 74            | 199       | QS         |
| S9 - A-D Composite (CXL0724-50) Soil  | Sampled: 12/10/14 08:30 | Received           | l: 12/11/1 | 4 16:20  |              |          |               |           |            |
| Aldrin                                | ND                      | 2.0                | μg/kg      | 2        | CX08894      | 12/12/14 | 12/15/14      | EPA 8081A |            |
| alpha-BHC                             | ND                      | 4.0                | 040        | 1146     | 100          | .00      | **            | **        |            |
| beta-BHC                              | ND                      | 20                 | 44         | -        |              | 5.9%     |               | ₩         |            |
| delta-BHC                             | ND                      | 20                 | **         | **       | **           | (900);   | **            | **        |            |
| gamma-BHC (Lindane)                   | ND                      | 20                 | 2.9%       | 241      | 5110         | (%)      | 0.00          | .17.      |            |
| Chlordane-technical                   | 82                      | 40                 | 1000       |          | ) <b>(4)</b> |          | 100           | #         |            |
| 4,4´-DDD                              | ND                      | 15                 | 949        | 5000     | 1041         |          | 0.000         | (#        |            |
| 4,4'-DDE                              | 160                     | 75                 |            | 10       | *            |          | in .          |           |            |
| 4,4'-DDT                              | ND                      | 15                 | **         | 2        |              | 1986)    | (*)           | #         |            |
| Dieldrin                              | ND                      | 2.0                | (0.99)     | 11       | 3(#7)        | ((e)     | 9.9%          | 77        |            |
| Endosulfan I                          | ND                      | 30                 | (30)       | 500      | ((**))       | 3000     | (39);         | 98        |            |
| Endosulfan II                         | ND                      | 30                 | .00        | 300      | 343          |          | 7997          | (#        |            |
| Endosulfan sulfate                    | ND                      | 30                 |            | - 11     | 40           | (47)     | (10)          | 54        |            |
| Endrin                                | ND                      | 30                 | **         |          | (4)          | (1947)   | (0)           | <u> </u>  |            |
| Endrin aldehyde                       | ND                      | 30                 | 1,90       | 0,000    | 1 10         | - 10     |               |           |            |
| Heptachlor                            | ND                      | 10                 | ((#)       | (100)    | 599)         | 996      | ((#)          | 386       |            |
| Heptachlor epoxide                    | ND                      | 4.0                | (0.44)     | 9.40     | 447          | 40       | 7/ <b>m</b> 3 |           |            |
| Methoxychlor                          | ND                      | 30                 | 140        | 1(4)     | **           | 100      | 846           | **        |            |
| Mirex                                 | ND                      | 20                 |            | *        |              | 1990     | (*)           |           |            |
| Toxaphene                             | ND                      | 40                 | 199        | 11,997   | 539.0        | 200      | 040           | 77        |            |
| Surrogate: Tetrachloro-meta-xylene    |                         | 77 %               | 40         | 5-139    | 140          | (4)      | w             | 940       |            |
| Surrogate: Decachlorobiphenyl         |                         | 50 %               | 52         | ?-141    | 70           | 1.00     | 2             |           | <u>O</u> S |

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Engeo- San Ramon

2010 Crow Canyon PI, suite 250 Project Number: 11227,000,000

San Ramon, CA 94583

Project: Enterprise Road Hollister

Project Manager: Shawn Munger

CLS Work Order #: CXL0724

COC #:

| Analyte                               | R<br>Result             | eporting<br>Limit | Units      | Dilution | Batch    | Prepared | Analyzed   | Method          | Notes |
|---------------------------------------|-------------------------|-------------------|------------|----------|----------|----------|------------|-----------------|-------|
| S10 - A-D Composite (CXL0724-55) Soil | Sampled: 12/10/14 11:40 | Receive           | d: 12/11/  | 14 16:20 |          |          |            |                 |       |
| Aldrin                                | ND                      | 2.0               | μg/kg      | 2        | CX08894  | 12/12/14 | 12/15/14   | EPA 8081A       |       |
| alpha-BHC                             | ND                      | 4.0               |            | 54       | **       |          | 39         | 199             |       |
| beta-BHC                              | ND                      | 20                | **         | **       | н        |          | *          |                 |       |
| delta-BHC                             | ND                      | 20                | **         | #        | (#)      | M.1      |            |                 |       |
| gamma-BHC (Lindane)                   | ND                      | 20                | 77         | 77.      |          | 3.00     | **         | 1000            |       |
| Chlordane-technical                   | 100                     | 40                | ##         | .85      | **       |          |            | \$( <b>66</b> ) |       |
| 4,4´-DDD                              | ND                      | 15                | 300        |          | **       | *        | <b>(46</b> | (9)             |       |
| 4,4′-DDE                              | 64                      | 15                | H          | ¥        | ₩.       |          | 4          | (4)             |       |
| 4,4´-DDT                              | ND                      | 15                |            | *        | #        | 38       | H          | (4)             |       |
| Dieldrin                              | 28                      | 2.0               | (#)        | #        | *        |          | 195        | (39)            |       |
| Endosulfan I                          | ND                      | 30                | 77.        | **       | .00      | 394      |            | (10)            |       |
| Endosulfan II                         | ND                      | 30                | 39.        | 36       | #:       | 30       | 34         | (1990)          |       |
| Endosulfan sulfate                    | ND                      | 30                | M          | **       | ₩.       | ₩        | н          | (20)            |       |
| Endrin                                | ND                      | 30                | 340        | in.      | **       |          | Ħ          |                 |       |
| Endrin aldehyde                       | ND                      | 30                | *          | *        | **       | .**      |            | ( <b>!!</b>     |       |
| Heptachlor                            | ND                      | 10                | 77         | **       | *        | **       | #.         | 500             |       |
| Heptachlor epoxide                    | ND                      | 4.0               | **         | **       | 10.      | **       | **         | (90)            |       |
| Methoxychlor                          | ND                      | 30                | ₩:         | 16       | iii.     | *        | *          | ***             |       |
| Mirex                                 | ND                      | 20                | #          | **       | 10       | *        |            | (*)             |       |
| Гохарhene                             | ND                      | 40                |            | *        | *        | Ж.       | *          |                 |       |
| Surrogate: Tetrachloro-meta-xylene    |                         | 84 %              | 46         | -139     | *        | <u> </u> | Ján i      | 1(44)           |       |
| Surrogate: Decachlorobiphenyl         |                         | 66 %              | 52         | -141     | <i>w</i> | (#)      | **         | *               |       |
| S11 - A-D Composite (CXL0724-60) Soil | Sampled: 12/10/14 12:25 | Receive           | d: 12/11/  | 14 16:20 |          |          |            |                 |       |
| Aldrin                                | ND                      | 2.0               | μg/kg      | 2        | CX08894  | 12/12/14 | 12/15/14   | EPA 8081A       |       |
| llpha-BHC                             | ND                      | 4.0               | <b>6</b> E | W.       |          | H        | **         | 146             |       |
| peta-BHC                              | ND                      | 20                | 00         | w        |          | **       | #          | ) <del>(i</del> |       |
| lelta-BHC                             | ND                      | 20                | *          |          | •        | *        | *1         | 199             |       |
| gamma-BHC (Lindane)                   | ND                      | 20                |            | 196      | 10997    | #        | 16         | **              |       |
| Chlordane-technical                   | ND                      | 40                | ( 0)       | (00)     | (100)    |          | 166        | *               |       |

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Engeo- San Ramon

Project: Enterprise Road Hollister

2010 Crow Canyon Pl. suite 250 San Ramon, CA 94583 Project Number: 11227.000.000 Project Manager: Shawn Munger CLS Work Order #: CXL0724

COC #:

| Analyte                               | R<br>Result             | eporting<br>Limit | Units     | Dilution  | Batch   | Prepared | Analyzed | Method    | Notes |
|---------------------------------------|-------------------------|-------------------|-----------|-----------|---------|----------|----------|-----------|-------|
| S11 - A-D Composite (CXL0724-60) Soil | Sampled: 12/10/14 12:25 | Receive           | d: 12/11  | /14 16:20 |         |          |          |           |       |
| 4,4′-DDD                              | ND                      | 15                | μg/kg     | 2         | CX08894 | (99)     | 12/15/14 | EPA 8081A |       |
| 4,4′-DDE                              | 22                      | 15                |           |           |         | (0)      | **       | *         |       |
| 4,4´-DDT                              | ND                      | 15                | (#)       | :#X       | 36.2    | 700      | (9.5)    |           |       |
| Dieldrin                              | ND                      | 2.0               | (981)     | 300.0     | 900     | 16       | 3000     | **        |       |
| Endosulfan I                          | ND                      | 30                | 160       |           | **      |          | 347      | **        |       |
| Endosulfan II                         | ND                      | 30                | 48        | **        | W.      | 7.50     | **       | *         |       |
| Endosulfan sulfate                    | ND                      | 30                | **        | (10)      | n       | 2,00%    | 0.7      | 70        |       |
| Endrin                                | ND                      | 30                | (##)(     | 3807      | 3#63    | (90)     | (0.0     | #.        |       |
| Endrin aldehyde                       | ND                      | 30                | (19)      | (94))     | (40)    | 100      | 3€0      | XX        |       |
| Heptachlor                            | ND                      | 10                | (40)      | (**)      | 946.5   | **       | 30.5     | AN.       |       |
| Heptachlor epoxide                    | ND                      | 4.0               | **        | (AB       |         | **       | at .     | **        |       |
| Methoxychlor                          | ND                      | 30                | **        | *         | 77      | (rec)    |          | 44        |       |
| Mirex                                 | ND                      | 20                | (#4.5)    | (8.5      | 7#0     | (94):    | (95)     | 70        |       |
| Toxaphene                             | ND                      | 40                | 2000      | 300       | (00)    | 11411    | \mu_1    | .85       |       |
| Surrogate: Tetrachloro-meta-xylene    |                         | 75 %              | 40        | 6-139     |         | 1000)    | E        |           |       |
| Surrogate: Decachlorobiphenyl         |                         | 50 %              | 5.        | 2-141     | *       | 0#2      | "        | #         | QS-   |
| S12 - A-D Composite (CXL0724-65) Soil | Sampled: 12/10/14 11:10 | Receive           | ed: 12/11 | /14 16:20 |         |          |          |           |       |
| Aldrin                                | ND                      | 2.0               | μg/kg     | 2         | CX08894 | 12/12/14 | 12/15/14 | EPA 8081A |       |
| alpha-BHC                             | ND                      | 4.0               | **        | **        | (+)     | 970      | **       | *         |       |
| beta-BHC                              | ND                      | 20                | 1(#0)     | (90)      | (9)     | (990)    | 020      |           |       |
| delta-BHC                             | ND                      | 20                | ((#))     | (90)      | 190     | . 41     | (m.)     | .85       |       |
| gamma-BHC (Lindane)                   | ND                      | 20                | 141       | 104417    | 300     | ak)      | 334431   | 36        |       |
| Chlordane-technical                   | 86                      | 40                | 30        | (44)      |         | (*)      | in       | **        |       |
| 4,4'-DDD                              | ND                      | 15                | 40        |           | **      |          | **       | *         |       |
| 4,4′-DDE                              | 250                     | 75                | (.99)     | 10        | 200     | 1.00     | $\pi$    | 77        |       |
| 4,4'-DDT                              | 34                      | 15                | 30)       | 2         | 000     | 240      | 144      | 28.       |       |
| Dieldrin                              | 4.7                     | 2.0               | 000       | 111       | SWILL   |          | **       | 36        |       |
| Endosulfan I                          | ND                      | 30                |           | - 00      | AB      |          |          | 36        |       |
| Endosulfan II                         | ND                      | 30                |           | 11        | 19      | 2000     | **       | W         |       |

# California Laboratory Services

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Engeo- San Ramon

San Ramon, CA 94583

Project: Enterprise Road Hollister

2010 Crow Canyon Pl. suite 250

Project Number: 11227 000 000 Project Manager: Shawn Munger CLS Work Order #: CXL0724

COC #:

| Analyte                               | Result                  | eporting<br>Limit | Units     | Dilution  | Batch   | Prepared   | Analyzed            | Method         | Notes |
|---------------------------------------|-------------------------|-------------------|-----------|-----------|---------|------------|---------------------|----------------|-------|
| S12 - A-D Composite (CXL0724-65) Soil | Sampled: 12/10/14 11:10 | Receive           | d: 12/11  | /14 16:20 |         |            |                     |                |       |
| Endosulfan sulfate                    | ND                      | 30                | μg/kg     | 2         | CX08894 | *          | 12/15/14            | EPA 8081A      |       |
| Endrin                                | ND                      | 30                | *         | **        |         | ii .       | **                  | 1966           |       |
| Endrin aldehyde                       | ND                      | 30                |           | **        | **      |            | **                  |                |       |
| Heptachlor                            | ND                      | 10                |           | *         | *       | .77        | (**                 | w              |       |
| Heptachlor epoxide                    | ND                      | 4.0               | 9         | ,,        | "       | (#         | .**                 | 1000           |       |
| Methoxychlor                          | ND                      | 30                |           | *         | **      |            | **                  | 200            |       |
| Mirex                                 | ND                      | 20                | **        | ж         | *       | *          | W.                  | 500            |       |
| Toxaphene                             | ND                      | 40                | *         | ¥         | W       | Œ          | ü                   |                |       |
| Surrogate: Tetrachloro-meta-xylene    |                         | 57%               | 46        | 5-139     | ×       |            | S#02                | 3#2            |       |
| Surrogate: Decachlorobiphenyl         |                         | 29 %              |           | 2-141     | 295     | 34         | ( <del>100</del> 0) | 3.00           | QS'   |
| S13 - A-D Composite (CXL0724-70) Soil | Sampled: 12/10/14 12:00 | Receive           | d: 12/11/ | 14 16:20  |         |            |                     |                |       |
| Aldrin                                | ND                      | 2.0               | μg/kg     | 2         | CX08895 | 12/12/14   | 12/16/14            | EPA 8081A      |       |
| alpha-BHC                             | ND                      | 4.0               | 25        | ***       | #5      | 940        | **                  | **             |       |
| beta-BHC                              | ND                      | 20                | 96        | (6)       | **      | <u>iii</u> | **                  | Se 2           |       |
| delta-BHC                             | ND                      | 20                | 60        | **        | **      | #          | #                   | **             |       |
| gamma-BHC (Lindane)                   | ND                      | 20                | **        | 94        | #       | 77         | *                   |                |       |
| Chlordane-technical                   | ND                      | 40                | *         | #         | **      | **         | 75                  | 7751           |       |
| 4,4´-DDD                              | ND                      | 15                | 75        | **        | **:     | **         | ***                 | ( <b>0</b> /   |       |
| 4,4´-DDE                              | ND                      | 15                | 99        | **        | #5      | *          | <b>80</b>           | (40)           |       |
| 1,4'-DDT                              | ND                      | 15                | 14        | #1        | #       | #          | #2                  |                |       |
| Dieldrin                              | ND                      | 2.0               | 7.60      |           | *       | 7          |                     | ( <del>)</del> |       |
| Endosulfan I                          | ND                      | 30                |           | **        | #(      | **         | 75                  | 175            |       |
| Endosulfan II                         | ND                      | 30                | *         | 190       | 7.985   | **         | 191                 | 199            |       |
| Endosulfan sulfate                    | ND                      | 30                | (4)       | (49)      | (00)    | **         | 0.00                | 744            |       |
| Endrin                                | ND                      | 30                | ((46)     | (44)      | (4)     | #          | 186                 | 100            |       |
| Endrin aldehyde                       | ND                      | 30                |           | 48        | **      | 7.         | *                   | - 9            |       |
| feptachlor                            | ND                      | 10                |           |           | •       | **         | 1199                | *              |       |
| Heptachlor epoxide                    | ND                      | 4.0               | 100       | (196)     | 0#0     | •          | (100)               | ж              |       |
| Methoxychlor                          | ND                      | 30                | (300)     | (100)     | (4)     |            | 046                 | **             |       |

# California Laboratory Services

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Engeo- San Ramon

2010 Crow Canyon Pl. suite 250

San Ramon, CA 94583

Project: Enterprise Road Hollister

Project Number: 11227 000 000

CLS Work Order #: CXL0724 COC #:

Project Manager: Shawn Munger CO

| Analyte                               | R<br>Result             | eporting<br>Limit | Units      | Dilution | Batch   | Prepared           | Analyzed      | Method    | Notes |
|---------------------------------------|-------------------------|-------------------|------------|----------|---------|--------------------|---------------|-----------|-------|
| S13 - A-D Composite (CXL0724-70) Soil | Sampled: 12/10/14 12:00 | Receive           | ed: 12/11/ | 14 16:20 |         |                    |               |           |       |
| Mirex                                 | ND                      | 20                | μg/kg      | 2        | CX08895 | S#77               | 12/16/14      | EPA 8081A |       |
| Toxaphene                             | ND                      | 40                | 5465       | AME      | 3402    | :(+0)              |               |           |       |
| Surrogate: Tetrachloro-meta-xylene    |                         | 49 %              | 46         | -139     | 1040    | -                  | ₩.            | 39        |       |
| Surrogate, Decachlorobiphenyl         |                         | 23 %              | 52         | -141     |         | *                  | 2             | **        | QS-   |
| S14 - A-D Composite (CXL0724-75) Soil | Sampled: 12/10/14 13:00 | Receive           | ed: 12/11/ | 14 16:20 |         |                    |               |           |       |
| Aldrin                                | ND                      | 2.0               | μg/kg      | 2        | CX08895 | 12/12/14           | 12/16/14      | EPA 8081A |       |
| alpha-BHC                             | ND                      | 4.0               | 48.        | (48      |         | **                 |               | hr.       |       |
| beta-BHC                              | ND                      | 20                | **         | *        |         | :#ii               |               | M         |       |
| delta-BHC                             | ND                      | 20                | 7(#1)      | 10110    | (100)   | 3 4(1)             |               |           |       |
| gamma-BHC (Lindane)                   | ND                      | 20                | ((40)      | - 11)    | ((e))   |                    | (0)           | .#.       |       |
| Chlordane-technical                   | ND                      | 40                |            |          | (141)   |                    | 700           | 344       |       |
| 4,4´-DDD                              | ND                      | 15                | **         | **       | 144     |                    | 500           |           |       |
| 4,4'-DDE                              | 25                      | 15                | **/        |          |         | 1,99               |               | *         |       |
| 4,4'-DDT                              | ND                      | 15                | 1,90       | (10)     | (4)     | (200)              |               | **        |       |
| Dieldrin                              | ND                      | 2.0               | 300        | 898      | (.*)    | (64)               | 0#0           |           |       |
| Endosulfan I                          | ND                      | 30                | 600        | (30)     | (90)    | (1 <del>44</del> ) | ((00)         | w         |       |
| Endosulfan II                         | ND                      | 30                | 5000       | 5045     | 41      | **                 | 15 <b>0</b> 0 | 346       |       |
| Endosulfan sulfate                    | ND                      | 30                |            | 44       | **      |                    |               | 10        |       |
| Endrin                                | ND                      | 30                | **         |          |         | 30#0               | . 47          | *         |       |
| Endrin aldehyde                       | ND                      | 30                | 13#0       | 13593    | 0.00    |                    | 9.947         | 37        |       |
| Heptachlor                            | ND                      | 10                | (160)      | [[(e]    | **      | 1.00               | . 10          |           |       |
| Heptachlor epoxide                    | ND                      | 4.0               |            | 51946    | w       |                    | 1040          | (66       |       |
| Methoxychlor                          | ND                      | 30                | (44)       | (44)     | 7.00    |                    | 40            | **        |       |
| Mirex                                 | ND                      | 20                | 41         | ***      | .44     | 1.0%               | 10            | *         |       |
| Toxaphene                             | ND                      | 40                | 0.002      | C.#0     | (#)     | (0)                | 1980          | /15       |       |
| Surrogate: Tetrachloro-meta-xylene    |                         | 50 %              | 40         | 5-139    | 2       | #3                 | w             | 500.0     |       |
| Surrogate: Decachlorobiphenyl         |                         | 29 %              | 52         | ?-141    | #       | 90                 | ¥             |           | QS-   |

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Engeo- San Ramon

Proj

2010 Crow Canyon Pl, suite 250 San Ramon, CA 94583 Project: Enterprise Road Hollister

Project Number: 11227,000,000 Project Manager: Shawn Munger

CLS Work Order #: CXL0724

COC #:

| Analyte                               | Result                  | eporting<br>Limit | Units     | Dilution    | Batch         | Prepared  | Analyzed       | Method        | Notes |
|---------------------------------------|-------------------------|-------------------|-----------|-------------|---------------|-----------|----------------|---------------|-------|
| S15 - A-D Composite (CXL0724-80) Soil | Sampled: 12/10/14 11:50 | Receive           | ed: 12/11 | /14 16:20   |               |           |                |               |       |
| Aldrin                                | ND                      | 2.0               | μg/kg     | 2           | CX08895       | 12/12/14  | 12/16/14       | EPA 8081A     |       |
| alpha-BHC                             | ND                      | 4.0               | **        | **          | **            | W .       | *              | н.            |       |
| beta-BHC                              | ND                      | 20                | **        | **          | 34            |           | M.             | (99)          |       |
| delta-BHC                             | ND                      | 20                | (A)       | *           | *             | 189       |                |               |       |
| gamma-BHC (Lindane)                   | ND                      | 20                |           |             | 77            | 39        | **             | (5.00)        |       |
| Chlordane-technical                   | ND                      | 40                | *         | **          | (0)           | *         | (#             | (144)         |       |
| 4,4´-DDD                              | ND                      | 15                | ж         | **          | W             |           | *              | 51445         |       |
| 4,4´-DDE                              | ND                      | 15                | **        | ¥.          | н             | 7         | *              |               |       |
| 4,4´-DDT                              | ND                      | 15                | *         | *           | $\mathcal{H}$ | 385       | **             | (10)          |       |
| Dieldrin                              | ND                      | 2.0               | **        |             | <u> </u>      | **        |                | 6 <b>9</b> 90 |       |
| Endosulfan I                          | ND                      | 30                | ***       | #1.         | **            |           | **             | 5940)         |       |
| Endosulfan II                         | ND                      | 30                | **        | <b>X</b> E. | ***           | .iii      | Ä              | 596           |       |
| Endosulfan sulfate                    | ND                      | 30                | **        | **          | **            | *         | H              |               |       |
| Endrin                                | ND                      | 30                | **        | W           | *             |           | <b>#</b>       | •             |       |
| Endrin aldehyde                       | ND                      | 30                | £         | *           | *             | <b>**</b> | 75             | 7(41)         |       |
| Heptachlor                            | ND                      | 10                | 100       | 25          | **            | 30        | 34%            | (00)          |       |
| Heptachlor epoxide                    | ND                      | 4.0               | **        | w           | 66            | **        | **             | 990           |       |
| Methoxychlor                          | ND                      | 30                | **        | W.          | 147           | *         | **             |               |       |
| Mirex                                 | ND                      | 20                | 447       | 46          | 10            |           | *              |               |       |
| Toxaphene                             | ND                      | 40                | *         | #           | #             | *         | 75             | (.77.)        |       |
| Surrogate: Tetrachloro-meta-xylene    |                         | 50 %              | 46        | -139        | **            | Ж         |                | 1(20)         |       |
| Surrogate: Decachlorobiphenyl         |                         | 30 %              | 52        | -141        | W:            | H         | 18             |               | QS-4  |
| S16 - A-D Composite (CXL0724-85) Soil | Sampled: 12/10/14 12:30 | Receive           | d: 12/11/ | 14 16:20    |               |           |                |               |       |
| Aldrin                                | ND                      | 2.0               | μg/kg     | 2           | CX08895       | 12/12/14  | 12/16/14       | EPA 8081A     | "     |
| alpha-BHC                             | ND                      | 4.0               | 2000      | **          | н.            | *         | ě              | 56            |       |
| peta-BHC                              | ND                      | 20                |           |             |               | **        | <del>(</del> ) | 99            |       |
| delta-BHC                             | ND                      | 20                |           |             |               | ж.        | 180            | 18            |       |
| gamma-BHC (Lindane)                   | ND                      | 20                | 686       | 1000        | 3.00          | **        |                | 700           |       |
| Chlordane-technical                   | ND                      | 40                | ((*)      | (100)       | 2.00          | *         | 7.80           | 94            |       |

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Engeo- San Ramon

Project: Enterprise Road Hollister

2010 Crow Canyon Pl., suite 250 San Ramon, CA 94583 Project Number: 11227,000,000 Project Manager: Shawn Munger CLS Work Order #: CXL0724

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COC #:

### Organochlorine Pesticides by EPA Method 8081A

| Analyte                               | Result                  | eporting<br>Limit | Units         | Dilution  | Batch   | Prepared | Analyzed | Method          | Notes |
|---------------------------------------|-------------------------|-------------------|---------------|-----------|---------|----------|----------|-----------------|-------|
| S16 - A-D Composite (CXL0724-85) Soil | Sampled: 12/10/14 12:30 | Receive           | d: 12/11      | /14 16:20 |         |          |          |                 |       |
| 4,4′-DDD                              | ND                      | 15                | μg/kg         | 2         | CX08895 | 808      | 12/16/14 | EPA 8081A       |       |
| 4,4 -DDE                              | ND                      | 15                | 397           | 9#3       | 3#31    | (90)     |          | #5              |       |
| 4,4 -DDT                              | ND                      | 15                | 900           | (900)     | 346.0   | 100      | 000      | 385             |       |
| Dieldrin                              | ND                      | 2.0               | 10            | 140       | *       |          | 346      | **              |       |
| Endosulfan l                          | ND                      | 30                | 10            | (4)       | Mr.     | (25)     | ár.      | M               |       |
| Endosulfan II                         | ND                      | 30                | n.            | (10)      | (0)     | (99)     | 14       | *               |       |
| Endosulfan sulfate                    | ND                      | 30                | **            | 5#86      | 9#87    | 7000     | 995      | 45              |       |
| Endrin                                | ND                      | 30                | 300           | (199)     | (40)    |          | (9)      | (44)            |       |
| Endrin aldehyde                       | ND                      | 30                | 500           | (40)      | 590     |          | 0463     | **              |       |
| Heptachlor                            | ND                      | 10                |               |           |         |          |          | 34              |       |
| Heptachlor epoxide                    | ND                      | 4.0               | 79/           |           | (10)    |          |          | #               |       |
| Methoxychlor                          | ND                      | 30                | 5863          | (100)     | (#)     | (94)     | 377      | *               |       |
| Mirex                                 | ND                      | 20                | ) <b>W</b> (C | (90)      | (96)    | 1940     | (041)    | *               |       |
| Toxaphene                             | ND                      | 40                | 100.2         | ***       | 2000    | 100      | (600)    | н               |       |
| Surrogate: Tetrachloro-meta-xylene    |                         | 67 %              | 40            | 6-139     | *       | 6#8      |          | *               |       |
| Surrogate: Decachlorobiphenyl         |                         | 43 %              |               | 2-141     | 395     | (100)    | **       |                 | QS-   |
| S17 - A-D Composite (CXL0724-90) Soil | Sampled: 12/10/14 14:15 | Receive           | ed: 12/11     | /14 16:20 |         |          |          |                 |       |
| Aldrin                                | ND                      | 2.0               | μg/kg         | 2         | CX08895 | 12/12/14 | 12/16/14 | EPA 8081A       |       |
| alpha-BHC                             | ND                      | 4.0               | 1990          | 87%       | 7.5%    | (300)    | **       | <b>m</b>        |       |
| beta-BHC                              | ND                      | 20                | (00)          | (190)     | (0)     | 5140     | 1.99     |                 |       |
| delta-BHC                             | ND                      | 20                | 10#0          | ((44));   | 7540    |          | (34)     | 36              |       |
| gamma-BHC (Lindane)                   | ND                      | 20                | (44)          | - 90      | 100     | •        |          | *               |       |
| Chlordane-technical                   | ND                      | 40                | *             | **        |         | 3.90     | **       | <b>%</b>        |       |
| 4,4'-DDD                              | ND                      | 15                | (1990)        |           | ((99))  | 580      |          | *               |       |
| 4,4'-DDE                              | ND                      | 15                | (300)         | (40)      | ((#))   |          | (190)    | **              |       |
| 4,4'-DDT                              | ND                      | 15                | *             | 500       | 141     |          | ( e)     | #               |       |
| Dieldrin                              | ND                      | 2.0               |               |           | 10.     | **       | •        | iii             |       |
| Endosulfan I                          | ND                      | 30                |               | (0)       |         | 1001     |          | ( <del>**</del> |       |
| Endosulfan II                         | ND                      | 30                | (90)          | (39)      | .49     | (16)     | 5.90     | 77              |       |

CA DOHS ELAP Accreditation/Registration Number 1233

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Engeo- San Ramon

2010 Crow Canyon Pl. suite 250

San Ramon, CA 94583

Project: Enterprise Road Hollister

Project Number: 11227.000.000

Project Manager: Shawn Munger

CLS Work Order #: CXL0724

COC #:

| Analyte                               | Result                  | eporting<br>Limit | Units     | Dilution  | Batch     | Prepared  | Analyzed            | Method    | Notes |
|---------------------------------------|-------------------------|-------------------|-----------|-----------|-----------|-----------|---------------------|-----------|-------|
| S17 - A-D Composite (CXL0724-90) Soil | Sampled: 12/10/14 14:15 | Receive           | d: 12/11  | /14 16:20 |           |           |                     |           |       |
| Endosulfan sulfate                    | ND                      | 30                | μg/kg     | 2         | CX08895   |           | 12/16/14            | EPA 8081A |       |
| Endrin                                | ND                      | 30                | **        | **        | 39        | 100       | (#                  | 40        |       |
| Endrin aldehyde                       | ND                      | 30                | (#4       | 144       | 34        | 40        | 36                  | ů.        |       |
| Heptachlor                            | ND                      | 10                | #         |           | *         |           | ***                 | #0        |       |
| Heptachlor epoxide                    | ND                      | 4.0               | **        | **        | .77       | 2007      | 377                 | 1.89      |       |
| Methoxychlor                          | ND                      | 30                | 115       | 311.      | 19        | 340       | 175                 | (40)      |       |
| Mirex                                 | ND                      | 20                | 399.      | 36        | **        |           | **                  | (40)      |       |
| Toxaphene                             | ND                      | 40                | **        | н         | **        | 39        | 94                  | 16        |       |
| Surrogate: Tetrachloro-meta-xylene    |                         | 73 %              | 40        | 5-139     |           | 39        | ( <b>(%</b> )       | **        |       |
| Surrogate: Decachlorobiphenyl         |                         | 54%               |           | ?-141     | 177       | <b>(4</b> | .0 <del>10</del> 71 | 16        |       |
| S18 - A-D Composite (CXL0724-95) Soil | Sampled: 12/10/14 14:15 | Receive           | d: 12/11/ | 14 16:20  |           |           |                     |           |       |
| Aldrin                                | ND                      | 2.0               | μg/kg     | 2         | CX08895   | 12/12/14  | 12/16/14            | EPA 8081A |       |
| llpha-BHC                             | ND                      | 4.0               | 75        | 75        | .#1       | 30        | 38                  | 1000      |       |
| peta-BHC                              | ND                      | 20                | 347.      | **        | **        | 34        | 900                 | 5.00      |       |
| lelta-BHC                             | ND                      | 20                | **        | .44       | ×         |           | *                   | -         |       |
| gamma-BHC (Lindane)                   | ND                      | 20                | **        | **        | н         | 77        | *                   |           |       |
| Chlordane-technical                   | ND                      | 40                | *         | #         | #         | *         |                     | •         |       |
| ,4′-DDD                               | ND                      | 15                |           | #         | 75        | 98        | #                   | 9#0       |       |
| ,4'-DDE                               | ND                      | 15                | 96        | 20        | 317       | 56        | **                  | [94]      |       |
| ,4'-DDT                               | ND                      | 15                | 9.        | **.       | #.        | W         | W                   | (in 2     |       |
| Dieldrin                              | 2.7                     | 2.0               | ***       | **        |           | **        |                     |           |       |
| Endosulfan I                          | ND                      | 30                | *         | #         | **        | ***       | *                   |           |       |
| Endosulfan II                         | ND                      | 30                | 70        | "         | <b>II</b> | *         | **                  | 385       |       |
| Endosulfan sulfate                    | ND                      | 30                | **        | **        | #         | *         | #:                  | 1.00()    |       |
| Endrin                                | ND                      | 30                | •         | **        | W.        |           | 10                  | 1441      |       |
| indrin aldehyde                       | ND                      | 30                | **        | #1        | ěC.       |           | *                   | an l      |       |
| leptachlor                            | ND                      | 10                | *         | #         | #         | 25        | <u> </u>            | 770       |       |
| leptachlor epoxide                    | ND                      | 4.0               | 9         | 7         |           | A.        | #:                  | (997)     |       |
| Methoxychlor                          | ND                      | 30                | **!       | +1        | **        | ¥         | W                   | 100       |       |

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Engeo- San Ramon

2010 Crow Canyon Pl. suite 250

San Ramon, CA 94583

Project: Enterprise Road Hollister

Project Number: 11227.000.000 Project Manager: Shawn Munger CLS Work Order #: CXL0724

COC #:

| Analyte                               | R<br>Result             | eporting<br>Limit | Units     | Dilution  | Batch   | Prepared | Analyzed   | Method          | Notes |
|---------------------------------------|-------------------------|-------------------|-----------|-----------|---------|----------|------------|-----------------|-------|
| S18 - A-D Composite (CXL0724-95) Soil | Sampled: 12/10/14 14:15 | Receive           | d: 12/11/ | 14 16:20  |         |          |            |                 |       |
| Mirex                                 | ND                      | 20                | μg/kg     | 2         | CX08895 | (1990)   | 12/16/14   | EPA 8081A       |       |
| Toxaphene                             | ND                      | 40                | 189       | (111)     | 195     | ((#))    |            |                 |       |
| Surrogate: Tetrachloro-meta-xylene    |                         | 61%               | 46        | -139      | (%)     |          | W          | 500             |       |
| Surrogate: Decachlorobiphenyl         |                         | 28 %              | 52        | -141      | 14      | w        | Ã.         | 1900            | QS-   |
| S19 - A-D Composite (CXL0724-AA) Soil | Sampled: 12/10/14 14:00 | Receiv            | ed: 12/11 | /14 16:20 |         |          |            |                 |       |
| Aldrin                                | ND                      | 2.0               | μg/kg     | 2         | CX08895 | 12/12/14 | 12/16/14   | EPA 8081A       |       |
| alpha-BHC                             | ND                      | 4.0               | 11        | -11       | ***     |          | **         | **              |       |
| beta-BHC                              | ND                      | 20                | **        |           |         | 1980     |            | 'AM             |       |
| delta-BHC                             | ND                      | 20                | 0.99.0    | 9.99      | (90)    | 0000     | w          | in .            |       |
| gamma-BHC (Lindane)                   | ND                      | 20                | 996       | 0.000     | 898     | (4)      | 10#10      | .17             |       |
| Chlordane-technical                   | ND                      | 40                | 5900      | ((#)      | 2905    | 10       | 0.000      | 344             |       |
| 4,4´-DDD                              | ND                      | 15                |           | (100)     | 5.995   | ( (H)    | 2047       | *               |       |
| 4,4′-DDE                              | 18                      | 15                | (**)      | **        | -       | .199     |            |                 |       |
| 4,4´-DDT                              | ND                      | 15                | **        | (4)       |         | (10)     | 197        | (iii            |       |
| Dieldrin                              | 2.4                     | 2.0               | 10910     | (9#):     | 988     | (4)      | IMU.       | 7               |       |
| Endosulfan I                          | ND                      | 30                | ((00)     | - 300     | ÷(e)    |          |            | 799             |       |
| Endosulfan II                         | ND                      | 30                | 296       | . 11      | 200     | W        | **         | 50              |       |
| Endosulfan sulfate                    | ND                      | 30                |           |           |         |          | 40         | 59              |       |
| Endrin                                | ND                      | 30                | 10        |           | **      | M        |            | X <del>II</del> |       |
| Endrin aldehyde                       | ND                      | 30                | (1990)    | 1.96      | 11,850  |          |            | 199             |       |
| Heptachlor                            | ND                      | 10                | (100)     | ( #)      | (1000)  | H        | (96)       | 249             |       |
| Heptachlor epoxide                    | ND                      | 4.0               | . 100     |           |         | 4        | (166)      | 346             |       |
| Methoxychlor                          | ND                      | 30                | u.        | w.        | (44)    | 70       | 100        | (44.            |       |
| Mirex                                 | ND                      | 20                | -7        | <b>R</b>  | 100     | 90       | 94         | **              |       |
| Toxaphene                             | ND                      | 40                | M         | **        | 5.95    | w(       | 1.00       |                 |       |
| Surrogate: Tetrachloro-meta-xylene    |                         | 65 %              | 40        | 5-139     | W.      |          | <i>3</i> # | (ie)            |       |
| Surrogate: Decachlorobiphenyl         |                         | 43 %              | 52        | ?-141     | #       | *5       | #          | *               | QS    |

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Engeo- San Ramon

Project: Enterprise Road Hollister

2010 Crow Canyon Pl. suite 250 San Ramon, CA 94583 Project Number: 11227,000,000 Project Manager: Shawn Munger CLS Work Order #: CXL0724

COC #:

### Metals by EPA 6000/7000 Series Methods - Quality Control

|                                 |        | Reporting   |              | Spike      | Source      |            | %REC   |     | RPD   |       |
|---------------------------------|--------|-------------|--------------|------------|-------------|------------|--------|-----|-------|-------|
| Analyte                         | Result | Limit       | Units        | Level      | Result      | %REC       | Limits | RPD | Limit | Notes |
| Batch CX08883 - EPA 3050B       |        |             |              |            |             |            |        |     |       |       |
| Blank (CX08883-BLK1)            |        |             |              | Prepared & | Analyzed    | : 12/12/14 |        |     |       |       |
| Arsenic                         | ND     | 0.10        | mg/kg        |            |             |            |        |     |       |       |
| LCS (CX08883-BS1)               |        |             |              | Prepared & | : Analyzed: | 12/12/14   |        |     |       |       |
| Arsenic                         | 8,55   | 0.10        | mg/kg        | 10.0       |             | 85         | 75-125 |     |       |       |
| Matrix Spike (CX08883-MS1)      | Sour   | ce: CXL0724 | I-0 <b>2</b> | Prepared & | : Analyzed: | 12/12/14   |        |     |       |       |
| Arsenic                         | 16.1   | 1,0         | mg/kg        | 10.0       | 9.16        | 70         | 75-125 |     |       | QM-5  |
| Matrix Spike Dup (CX08883-MSD1) | Sour   | ce: CXL0724 | 1-02         | Prepared & | : Analyzed: | 12/12/14   |        |     |       |       |
| Arsenic                         | 16,1   | 1.0         | ıng/kg       | 10.0       | 9_16        | 69         | 75-125 | 0.5 | 30    | QM-5  |

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Engeo- San Ramon

Enterprise Road Hollister

2010 Crow Canyon Pl. suite 250

Project Number: 11227 000 000

CLS Work Order #: CXL0724

San Ramon, CA 94583

Project Manager: Shawn Munger

COC#:

| Analista                           | Result | Reporting<br>Limit | Units              | Spike<br>Level | Source<br>Result | %REC        | %REC<br>Limits | RPD | RPD<br>Limit | Notes  |
|------------------------------------|--------|--------------------|--------------------|----------------|------------------|-------------|----------------|-----|--------------|--------|
| Analyte                            | Result | Litilit            | Ullits             | Level          | Result           | 76KEC       | Lillins        | KID | Lillin       | 140163 |
| Batch CX08894 - LUFT-DHS GCNV      |        |                    |                    |                |                  |             |                |     |              |        |
| Blank (CX08894-BLK1)               |        |                    |                    | Prepared:      | 12/12/14 A       | nalyzed: 12 | /15/14         |     |              |        |
| Aldrin                             | ND     | 1.0                | μg/kg              |                |                  |             |                |     |              |        |
| alpha-BHC                          | ND     | 2_0                | 2003               |                |                  |             |                |     |              |        |
| peta-BHC                           | ND     | 10                 | S <b>95</b> S      |                |                  |             |                |     |              |        |
| delta-BHC                          | ND     | 10                 | (1 <del>11</del> ) |                |                  |             |                |     |              |        |
| gamma-BHC (Lindane)                | ND     | 10                 | (40)               |                |                  |             |                |     |              |        |
| Chlordane-technical                | ND     | 20                 | (# <b>*</b> 5)     |                |                  |             |                |     |              |        |
| 1,4´-DDD                           | ND     | 7.5                | 31.5               |                |                  |             |                |     |              |        |
| 4,4´-DDE                           | ND     | 7.5                | 9#3                |                |                  |             |                |     |              |        |
| 4,4*-DDT                           | ND     | 7.5                | **                 |                |                  |             |                |     |              |        |
| Dieldrin                           | ND     | 1.0                | **                 |                |                  |             |                |     |              |        |
| Endosulfan l                       | ND     | 15                 | 3907               |                |                  |             |                |     |              |        |
| Endosulfan II                      | ND     | 15                 | 575                |                |                  |             |                |     |              |        |
| Endosulfan sulfate                 | ND     | 15                 | 77.5               |                |                  |             |                |     |              |        |
| Endrin                             | ND     | 15                 | 100                |                |                  |             |                |     |              |        |
| Endrin aldehyde                    | ND     | 15                 | 770                |                |                  |             |                |     |              |        |
| Heptachlor                         | ND     | 5,0                | ***                |                |                  |             |                |     |              |        |
| Heptachlor epoxide                 | ND     | 2,0                |                    |                |                  |             |                |     |              |        |
| Methoxychlor                       | ND     | 15                 | (1)                |                |                  |             |                |     |              |        |
| Mirex                              | ND     | 10                 |                    |                |                  |             |                |     |              |        |
| Гохарhene                          | ND     | 20                 |                    |                |                  |             |                |     |              |        |
| Surrogate: Tetrachloro-meta-xylene | 7.23   |                    |                    | 8.33           |                  | 87          | 46-139         |     |              |        |
| Surrogate: Decachlorobiphenyl      | 8.84   |                    | 10                 | 8.33           |                  | 106         | 52-141         |     |              |        |
| LCS (CX08894-BS1)                  |        |                    |                    | Prepared:      | 12/12/14 A       | nalyzed: 12 | 2/15/14        |     |              |        |
| Aldrin                             | 14.8   | 1.0                | μg/kg              | 16.7           |                  | 89          | 47-132         |     |              |        |
| gamma-BHC (Lindane)                | 14.8   | 10                 | ((4))              | 16.7           |                  | 89          | 56-133         |     |              |        |
| 4,4′-DDT                           | 17.1   | 7.5                | (100)              | 16.7           |                  | 103         | 46-137         |     |              |        |
| Dieldrin                           | 15.7   | 1.0                | 230                | 16.7           |                  | 94          | 44-143         |     |              |        |
| Endrin                             | 16,1   | 15                 | (66)               | 16.7           |                  | 97          | 30-147         |     |              |        |
| Heptachlor                         | 15,8   | 5.0                | 0.00               | 16.7           |                  | 95          | 33-148         |     |              |        |
| Surrogate: Tetrachloro-meta-xylene | 7,14   |                    | #0                 | 8,33           |                  | 86          | 46-139         |     |              |        |
| -                                  |        |                    |                    |                |                  |             |                |     |              |        |

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Engeo- San Ramon

Project: Enterprise Road Hollister

2010 Crow Canyon Pl\_ suite 250

Project Number: 11227 000 000

CLS Work Order #: CXL0724

San Ramon, CA 94583

Project Manager: Shawn Munger

COC #:

|                                    |        | Reporting    |          | Spike       | Source     |              | %REC    |      | RPD   |       |
|------------------------------------|--------|--------------|----------|-------------|------------|--------------|---------|------|-------|-------|
| Analyte                            | Result | Limit        | Units    | Level       | Result     | %REC         | Limits  | RPD  | Limit | Notes |
| Batch CX08894 - LUFT-DHS GCNV      |        |              |          |             |            |              |         |      |       |       |
| LCS (CX08894-BS1)                  |        |              |          | Prepared:   | 12/12/14 A | nalyzed: 12  | 2/15/14 |      |       |       |
| Surrogate: Decachlorobiphenyl      | 8.61   |              | μg kg    | 8.33        |            | 103          | 52-141  |      |       |       |
| LCS Dup (CX08894-BSD1)             |        |              |          | Prepared:   | 12/12/14 A | nalyzed: 12  | /15/14  |      |       |       |
| Aldrin                             | 15.2   | 1.0          | μg/kg    | 16.7        |            | 91           | 47-132  | 2    | 30    |       |
| gamma-BHC (Lindane)                | 15:1   | 10           | **       | 16.7        |            | 90           | 56-133  | 2    | 30    |       |
| 1,4"-DDT                           | 17.3   | 7.5          | <b>3</b> | 16.7        |            | 104          | 46-137  | 0.9  | 30    |       |
| Dieldrin                           | 15.7   | 1,0          | **       | 16.7        |            | 94           | 44-143  | 0.04 | 30    |       |
| Endrin                             | 15.9   | 15           | W        | 16.7        |            | 95           | 30-147  | 1    | 30    |       |
| Heptachlor                         | 15.9   | 5.0          | H        | 16.7        |            | 95           | 33-148  | 0_9  | 30    |       |
| Surrogate: Tetrachloro-meta-xylene | 7.11   |              | e        | 8.33        |            | 85           | 46-139  |      |       |       |
| surrogate: Decachlorobiphenyl      | 8.71   |              | æ        | 8,33        |            | 104          | 52-141  |      |       |       |
| Matrix Spike (CX08894-MS1)         | Sou    | rce: CXL0726 | 5-28     | Prepared: 1 | 2/12/14 Ai | nalyzed: 12  | /15/14  |      |       |       |
| Aldrin                             | 15.7   | 10           | μg/kg    | 16.7        | ND         | 94           | 47-138  |      |       |       |
| gamma-BHC (Lindane)                | 15.4   | 100          | **       | 16.7        | ND         | 92           | 38-144  |      |       |       |
| 4,4′-DDT                           | 20.0   | 75           | *        | 16.7        | 3.47       | 99           | 41-157  |      |       |       |
| Dieldrin                           | 17:1   | 10           | *        | 16.7        | ND         | 103          | 46-155  |      |       |       |
| Endrin                             | 19.4   | 150          | *        | 16.7        | ND         | 116          | 34-149  |      |       |       |
| Heptachlor                         | 14.0   | 50           | #        | 16.7        | ND         | 84           | 36-155  |      |       |       |
| Surrogate: Tetrachloro-meta-xylene | 18,7   |              | 33       | 20.8        |            | 90           | 46-139  |      |       |       |
| Surrogate: Decachlorobiphenyl      | 20.8   |              | W        | 20.8        |            | 100          | 52-141  |      |       |       |
| Matrix Spike Dup (CX08894-MSD1)    | Sou    | rce: CXL0726 | -28      | Prepared: 1 | 2/12/14 An | nalyzed: 12. | /15/14  |      |       |       |
| Aldrin                             | 14.4   | 10           | μg/kg    | 16.7        | ND         | 87           | 47-138  | 8    | 35    |       |
| aınma-BHC (Lindane)                | 14.0   | 100          | 41       | 16.7        | ND         | 84           | 38-144  | 9    | 35    |       |
| ,4´-DDT                            | 18.8   | 75           | 60       | 16.7        | 3.47       | 92           | 41-157  | 6    | 35    |       |
| Dieldrin                           | 15.9   | 10           | 0.00     | 16.7        | ND         | 95           | 46-155  | 8    | 35    |       |
| Endrin                             | 17.3   | 150          | 0.000    | 16.7        | ND         | 104          | 34-149  | 11   | 35    |       |
| deptachlor                         | 12.8   | 50           | ( 00)    | 16.7        | ND         | 77           | 36-155  | 9    | 35    |       |
| Gurrogate: Tetrachloro-meta-xylene | 17.2   |              | #1       | 20.8        |            | 82           | 46-139  |      |       |       |
| arrogate: Decachlorohiphenyl       | 18.5   |              | #0.      | 20.8        |            | 89           | 52-141  |      |       |       |

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Engeo- San Ramon

Project: Enterprise Road Hollister

2010 Crow Canyon Pl\_suite 250 San Ramon, CA 94583

Project Number: 11227\_000\_000 Project Manager: Shawn Munger CLS Work Order #: CXL0724

COC #:

| Analyte                            | Result | Reporting<br>Limit | Units             | Spike<br>Level | Source<br>Result | %REC        | %REC<br>Limits | RPD | RPD<br>Limit | Notes |
|------------------------------------|--------|--------------------|-------------------|----------------|------------------|-------------|----------------|-----|--------------|-------|
| Batch CX08895 - LUFT-DHS GCNV      |        |                    |                   |                |                  |             |                |     |              |       |
| Blank (CX08895-BLK1)               |        |                    |                   | Prepared:      | 12/12/14 A       | nalyzed: 12 | /16/14         |     |              |       |
| Aldrin                             | ND     | 1.0                | μg/kg             |                |                  |             |                |     |              |       |
| alpha-BHC                          | ND     | 2.0                | 1,00              |                |                  |             |                |     |              |       |
| beta-BHC                           | ND     | 10                 | 1,140.0           |                |                  |             |                |     |              |       |
| delta-BHC                          | ND     | 10                 | (ME)              |                |                  |             |                |     |              |       |
| gamma-BHC (Lindane)                | ND     | 10                 | 2963              |                |                  |             |                |     |              |       |
| Chlordane-technical                | ND     | 20                 | ( e. )            |                |                  |             |                |     |              |       |
| 4,4*-DDD                           | ND     | 7.5                | 0.967             |                |                  |             |                |     |              |       |
| 4,4*-DDE                           | ND     | 7.5                | 5 <del>11</del> 6 |                |                  |             |                |     |              |       |
| 4,4′-DDT                           | ND     | 7.5                | 5#3               |                |                  |             |                |     |              |       |
| Dieldrin                           | ND     | 1.0                | 31777             |                |                  |             |                |     |              |       |
| Endosulfan I                       | ND     | 15                 | 59%               |                |                  |             |                |     |              |       |
| Endosulfan II                      | ND     | 15                 | (.45)             |                |                  |             |                |     |              |       |
| Endosulfan sulfate                 | ND     | 15                 | 5.40              |                |                  |             |                |     |              |       |
| Endrin                             | ND     | 15                 | 25%               |                |                  |             |                |     |              |       |
| Endrin aldehyde                    | ND     | 15                 | 8.9%              |                |                  |             |                |     |              |       |
| Heptachlor                         | ND     | 5_0                | 0.097             |                |                  |             |                |     |              |       |
| Heptachlor epoxide                 | ND     | 2.0                | 0.000             |                |                  |             |                |     |              |       |
| Methoxychlor                       | ND     | 15                 |                   |                |                  |             |                |     |              |       |
| Mirex                              | ND     | 10                 | **                |                |                  |             |                |     |              |       |
| Toxaphene                          | ND     | 20                 |                   |                |                  |             |                |     |              |       |
| Surrogate: Tetrachloro-meta-xylene | 7.13   |                    | *                 | 8,33           |                  | 86          | 46-139         |     |              |       |
| Surrogate: Decachlorobiphenyl      | 8.29   |                    |                   | 8,33           |                  | 100         | 52-141         |     |              |       |
| LCS (CX08895-BS1)                  |        |                    |                   | Prepared:      | 12/12/14 A       | nalyzed: 12 | ./16/14        |     |              |       |
| Aldrin                             | 15.1   | 1.0                | μg/kg             | 16.7           |                  | 90          | 47-132         |     |              |       |
| gamma-BHC (Lindane)                | 14.9   | 10                 | 2002              | 16.7           |                  | 90          | 56-133         |     |              |       |
| 4,4´-DDT                           | 16.6   | 7,5                | 190               | 16.7           |                  | 100         | 46-137         |     |              |       |
| Dieldrin                           | 16,2   | 1,0                | 1002              | 16.7           |                  | 97          | 44-143         |     |              |       |
| Endrin                             | 17,2   | 15                 | 60                | 16.7           |                  | 103         | 30-147         |     |              |       |
| Heptachlor                         | 15.8   | 5.0                | #                 | 16.7           |                  | 95          | 33-148         |     |              |       |
| Surrogate: Tetrachloro-meta-xylene | 7,04   |                    | 85                | 8.33           |                  | 84          | 46-139         |     |              |       |

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Engeo- San Ramon

2010 Crow Canyon Pl. suite 250

San Ramon, CA 94583

Project: Enterprise Road Hollister

Project Number: 11227\_000\_000

CLS Work Order #: CXL0724 COC #:

Project Manager: Shawn Munger

|                                    |        | Reporting   |       | Spike       | Source     |             | %REC    |     | RPD   |       |
|------------------------------------|--------|-------------|-------|-------------|------------|-------------|---------|-----|-------|-------|
| Analyte                            | Result | Limit       | Units | Level       | Result     | %REC        | Limits  | RPD | Limit | Notes |
| Batch CX08895 - LUFT-DHS GCNV      |        |             |       |             |            |             |         |     |       |       |
| LCS (CX08895-BS1)                  |        |             |       | Prepared:   | 12/12/14 A | nalyzed: 12 | 2/16/14 |     |       |       |
| Surrogate: Decachlorobiphenyl      | 9.04   |             | μg kg | 8.33        |            | 108         | 52-141  |     |       |       |
| LCS Dup (CX08895-BSD1)             |        |             |       | Prepared:   | 12/12/14 A | nalyzed: 12 | 2/16/14 |     |       |       |
| Aldrin                             | 14.6   | 1,0         | μg/kg | 16,7        |            | 88          | 47-132  | 3   | 30    |       |
| gamma-BHC (Lindane)                | 14.2   | 10          | H     | 16.7        |            | 85          | 56-133  | 5   | 30    |       |
| 4,4'-DDT                           | 13.7   | 7,5         |       | 16.7        |            | 82          | 46-137  | 19  | 30    |       |
| Dieldrin                           | 15,5   | 1.0         | **    | 16_7        |            | 93          | 44-143  | 4   | 30    |       |
| Endrin                             | 14,5   | 15          | *     | 16.7        |            | 87          | 30-147  | 17  | 30    |       |
| Heptachlor                         | 14.1   | 5.0         | **    | 16.7        |            | 84          | 33-148  | 12  | 30    |       |
| Surrogate: Tetrachloro-meta-xylene | 6.51   |             |       | 8.33        |            | 78          | 46-139  |     |       |       |
| Surrogate: Decachlorobiphenyl      | 9.06   |             | 98    | 8.33        |            | 109         | 52-141  |     |       |       |
| Matrix Spike (CX08895-MS1)         | Sour   | ce: CXL0724 | I-75  | Prepared: 1 | 12/12/14 A | nalyzed: 12 | 2/16/14 |     |       |       |
| Aldrin                             | 10_6   | 2.0         | μg/kg | 16.7        | ND         | 63          | 47-138  |     |       |       |
| gamma-BHC (Lindane)                | 12.9   | 20          | **    | 16.7        | ND         | 77          | 38-144  |     |       |       |
| 4,4′-DDT                           | 13.3   | 15          | *     | 16.7        | 3.53       | 58          | 41-157  |     |       |       |
| Dieldrin                           | 12.3   | 2.0         |       | 16.7        | ND         | 74          | 46-155  |     |       |       |
| Endrin                             | 12.8   | 30          | **    | 16_7        | ND         | 77          | 34-149  |     |       |       |
| Heptachlor                         | 10.0   | 10          | **    | 16 7        | ND         | 60          | 36-155  |     |       |       |
| Surrogate: Tetrachloro-meta-xylene | 13.1   |             | "     | 20.8        |            | 63          | 46-139  |     |       |       |
| Surrogate: Decachlorobiphenyl      | 9.21   |             | **    | 20.8        |            | 44          | 52-141  |     |       | OS    |
| Matrix Spike Dup (CX08895-MSD1)    | Sour   | ce: CXL0724 | l-75  | Prepared: 1 | 2/12/14 A  | nalyzed: 12 | /16/14  |     |       |       |
| Aldrin                             | 10.4   | 2,0         | μg/kg | 16,7        | ND         | 62          | 47-138  | 2   | 35    |       |
| gamma-BHC (Lindane)                | 12.8   | 20          | 11:   | 16.7        | ND         | 77          | 38-144  | 0.5 | 35    |       |
| 1,4'-DDT                           | 13.5   | 15          | æ     | 16.7        | 3.53       | 60          | 41-157  | 2   | 35    |       |
| Dieldrin                           | 12,2   | 2.0         | **0   | 16.7        | ND         | 73          | 46-155  | 0.9 | 35    |       |
| Endrin                             | 13.0   | 30          | •6    | 16.7        | ND         | 78          | 34-149  | 2   | 35    |       |
| Heptachlor                         | 10 2   | 10          | •0    | 16.7        | ND         | 61          | 36-155  | 1.  | 35    |       |
| Surrogate: Tetrachloro-meta-xylene | 12.9   |             | 17    | 20.8        |            | 62          | 46-139  |     |       |       |
| Surrogate: Decachlorobiphenyl      | 9-14   |             | 45    | 20.8        |            | 44          | 52-141  |     |       | OS-4  |
|                                    |        |             |       |             |            |             |         |     |       |       |

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Engeo- San Ramon

San Ramon, CA 94583

Enterprise Road Hollister Project:

2010 Crow Canyon Pl. suite 250

Project Number: 11227.000.000

CLS Work Order #: CXL0724

Project Manager: Shawn Munger COC #:

**Notes and Definitions** 

The surrogate recovery for this sample is outside of established control limits due to a sample matrix effect. QS-4

The spike recovery was outside acceptance limits for the MS and/or MSD due to matrix interference. The LCS and/or LCSD were QM-5

within acceptance limits showing that the laboratory is in control and the data is acceptable.

Analyte DETECTED DET

Analyte NOT DETECTED at or above the reporting limit (or method detection limit when specified) ND

NR

Sample results reported on a dry weight basis dry

Relative Percent Difference RPD

# APPENDIX G QUALIFICATIONS STATEMENT



# EARTH SYSTEMS PACIFIC QUALIFICATIONS STATEMENT FOR ENVIRONMENTAL WORK

The Environmental Professional who provided oversight for this project meets the qualifications specified by US EPA AAI and ASTM E1527-05. An EP is defined by US EPA AAI as "a person who possesses sufficient specific education, training, and experience necessary to exercise professional judgment to develop opinions and conclusions regarding conditions indicative of releases or threatened releases (of hazardous substances) on, at, in, or to a property, sufficient to meet the objectives and performance factors (of the rule)." In addition, an environmental professional must have:

- A state, tribal, or territory-issued certification or license (Professional Engineer or Professional Geologist) and three years of relevant full-time work experience; or
- A Baccalaureate degree or higher in science or engineering and five years of relevant full-time work experience; or
- Ten years of relevant full-time work experience.

The attached resume(s) describe the credentials of the environmental professionals who directed field work, research and/or report preparation work on the project.



**BRETT FAUST**Senior Geologist

Years of Experience: 26

#### **QUALIFICATIONS**

Professional Geologist, California, No. 7025 Certified Engineering Geologist, California, No. 2386 B.S. Geology, 1993, San Jose State University, (CA, USA)

#### **PROFESSIONAL EXPERIENCE**

Employed with Earth Systems Pacific Hollister Office, Mr. Faust is a professional geologist with more than 20 years' experience in managing environmental and engineering geologic projects and performing soils and materials testing. Specific experience includes: soil and ground water contamination studies measuring and modeling fate and transport, Phase I and II environmental site assessments, and geologic fault and landslide studies.

Association of Engineering Geologists, Member

# Appendix H

Drainage Study



1171 Homestead Road., Suite 255 Santa Clara, CA 95050-5485 t. 408-246-4848 f. 408-246-5624 s&w@swsv.com

#### **MEMORANDUM**

TO: Longreach Associates Inc. DATE: February 27, 2020

FROM: Fidel Salamanca, PE JOB#: LNGR.01.19

Caitlin J. Gilmore, PE Katie Hogan, PE

SUBJECT: Lico South – Intravia Property Drainage Study

#### Introduction

Longreach Associates, Inc with the assistance of San Benito Engineering intends to develop an approximately 49-acre portion of agricultural land into single family homes within unincorporated San Benito County near Hollister. The project area, hereafter referred to as Lico South, is partially shown on Figure 1 along with the existing flood hazards.

Longreach Associates has hired Schaaf & Wheeler to develop improvement options that can alleviate or remove existing flooding hazards within the project site. This memorandum has been developed to summarize the existing flooding conditions under the FEMA flood hazard maps and determine which alternatives could be implemented to remove the existing flooding from the Lico South site. The analysis performed as part of this study builds on the previous hydrologic modeling of the Enterprise watershed. Five (5) different alternatives were explored to determine the option that could potentially eliminate flooding within the Lico South site. A summary of the alternatives and their respective results and impacts are included as part of this drainage study.

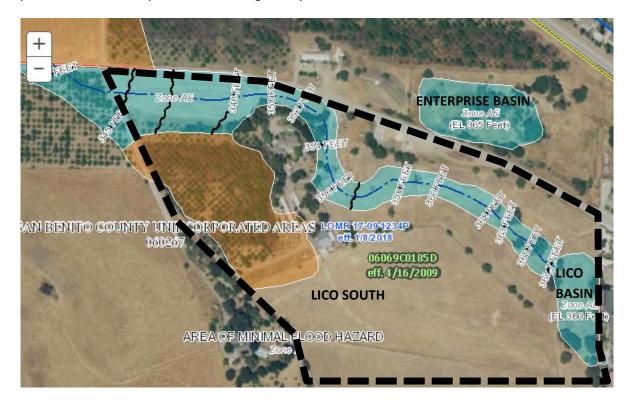


Figure 1: Existing FEMA Special Flood Hazard

The existing Lico South site has an existing FEMA Special Flood Hazard designation of Zone AE. The flood hazard is depicted in the FEMA Flood Insurance Rate Map (FIRM) for San Benito County, on Panel 185D, map 060267, a clip from that map is shown on Figure 1. This designation was concluded from a previous study submitted to FEMA in 2016 which incorporated the Enterprise sedimentation and drainage basin (Enterprise Basin) and the existing sedimentation and drainage basin within the Lico South property (Lico Basin). This study incorporates new as-built data obtained in 2019 and provides options for eliminating the existing special flood hazard from the Lico South site.

### **Existing Conditions**

The drainage basins were delineated by Schaaf & Wheeler using ArcGIS for the development of the 2D mapping submittal to FEMA in 2016. It was determined that the Enterprise Basin and Lico Basin each route waters from approximately 4.2 square miles of upstream watershed. Water flows into the Lico basin through the Oak Canyon Ct. storm drain line, flows are then routed to the Enterprise basin through a 72-inch RCP under Enterprise Road. A spillway on the Lico Basin allows water to spill overland when the water surface in the basin reaches Elevation 372 –feet on the North American Vertical Datum of 1988, (NAVD). The peak inflow into the Lico Basin is approximately 691 cfs.

The Enterprise Basin receives water from the aforementioned 72-inch RCP under Enterprise Road which routes flows from the Lico Basin. Additional runoff from the Valley View development is also conveyed into the Enterprise Basin through a 48-inch RCP across Airport Highway. The peak inflow into the Enterprise Basin is approximately 471 cfs. The Enterprise Basin discharges through an outlet structure that utilizes a 72-inch RCP and has a spillway elevation of 365 NAVD88. The 72-inch RCP conveys flows from the Enterprise basin, down Enterprise Rd, picking up flows along the way and being upsized to an 84-inch RCP before discharging into the San Benito River (SBR). Figure 2 illustrates the existing configuration of the two basins.

The current configuration yields 100-year flooding within the Lico South site as depicted in Figure 1. This flooding results from water overtopping the Lico Basin spillway and flowing overland through the site. Portions of the existing flooding are over 1-ft in depth and are mapped as Zone AE on the FEMA Flood Hazard maps. The peak discharge over the Lico Basin spillway is 227 cfs, and the total volume spilled is approximately 38.5 acre-ft. The Lico Basin has approximately 10 acre-feet of storage. There is also an existing spill over the Enterprise Basin spillway during the 100yr-24hr storm event; however, the flood depth on average does not exceed 1-ft depth and is not included on the FEMA flood maps. The peak discharge from the Enterprise Basin discharge pipe is 462 cfs and the total volume is 527.3 acre-ft, all of which is diverted to SBR.

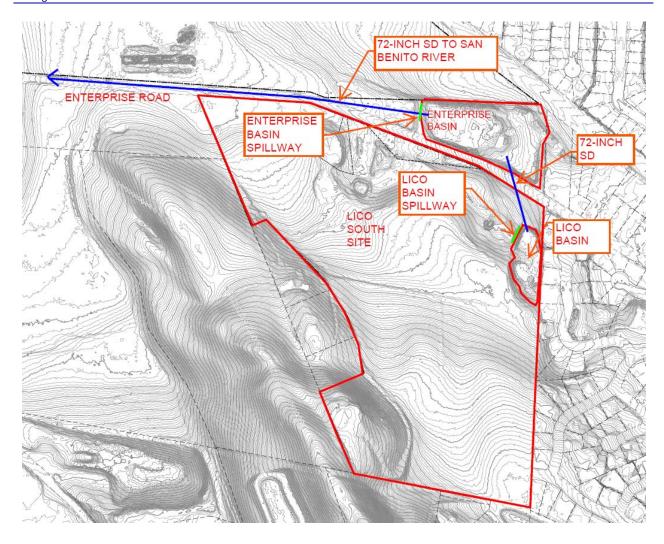


Figure 2: Existing Enterprise and Lico Basin Configuration

# **Proposed Improvements**

Schaaf & Wheeler has developed alternatives that can eliminate flooding within the Lico South site. This section describes the four different scenarios whose flooding impacts were evaluated as potential alternatives to remove the existing flooding from the Lico South property.

#### **Alternative 1: Double 72-inch Lico SD**

Alternative 1 explores the addition of a new 72-inch pipe across Enterprise Road to increase discharge capacity from the Lico Basin into Enterprise Basin (configuration shown on Figure 3). The existing configuration has overflows from the Lico Basin Spillway, resulting in flooding within the Lico South site (as mapped by FEMA). The addition of a new 72-inch SD culvert would significantly reduce discharge from Lico Basin by conveying additional flows north. The new 72-inch RCP is proposed to follow the proposed development road alignment and the upstream invert elevation is to be set at a minimum of 368 feet (NAVD 88) or lower. The downstream invert elevation is to match existing (356 feet NAVD88).

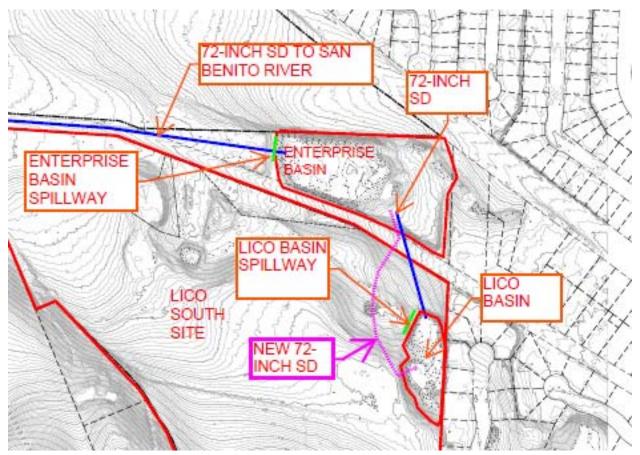


Figure 3: New 72-inch SD

#### **Alternative 2: Lico Basin Floodwall**

In this scenario, the incoming flow into Lico Basin was assumed to be contained by a floodwall set to elevation 389.4-ft (Figure 4). It was assumed that there was no flow via the spillway or the dam overtopping. The only outflow from the Lico Basin was assumed to be via the existing 72-inch pipe conveying water to the Enterprise Basin.

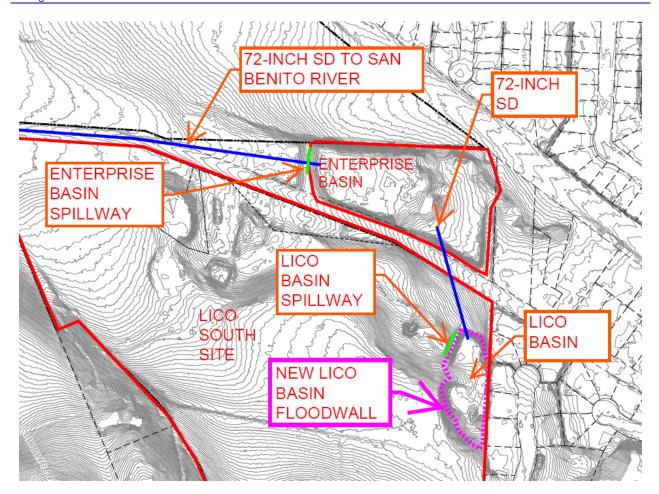


Figure 4: Lico Basin Floodwall

#### **Alternative 3: Lico Basin Raised Crest and Spillway**

In this scenario, the spillway was raised from existing 376.7-ft. to 381-ft. and top of dam was raised from 379.8-ft. to 383-ft (Figure 4). These elevations were chosen as the new spillway and crest elevations because they correspond to the low spot on the existing crest and the high spot on the existing crest respectively, and modifying the existing basin to meet these elevations would require relatively small changes to the existing basin footprint. This configuration would still have overtopping but the total volume of discharge is reduced.

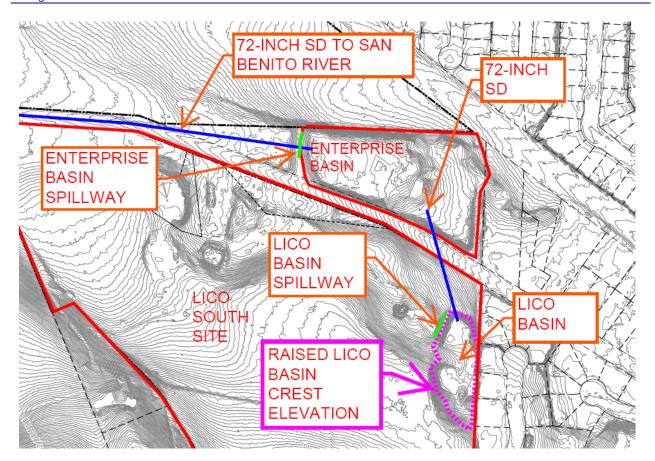


Figure 5: Raise Lico Basin Spillway and Crest

#### **Alternative 4: Increase Lico South Basin and Raise Spillway Elevation**

This scenario involves increasing the capacity of the Lico South Basin and raising the spillway to prevent overflow on the spillway. The spillway elevation would be increased to elevation 381 feet, and the dam elevation to 383 feet. The existing pond currently detains approximately 10 acre-feet.

#### **Alternative 5: New Storage Facility Downstream of Lico South Basin**

This scenario includes constructing a new storage facility downstream of the existing Lico Basin. The storage facility would capture the 225 cfs overflow (approximately 40 acre-ft) and release it to an outfall location where it can safely be conveyed without causing flooding.

#### Results

#### Alternative 1: Double 72-inch Lico SD

Adding a second 72-inch pipe to convey water to the Enterprise Pond detention basin eliminated any flow from the Lico Basin to the Lico South Property. As a result, flooding is greatly reduced in the Lico South property compared to the existing conditions. For most of the Lico South property, the flooding depth is less than 1-foot (Figure 6). Except for a small area immediately downstream of the Enterprise Pond detention basin, the flooding depth is less than 1-foot north of Enterprise Road. The additional pipe, however, causes the Enterprise basin water surface elevation to increase from 365 to 366.6 feet,

and the discharge over the spillway increases from 0 cfs to 170 cfs downstream of the Enterprise Basin. Even though the floodplain is not required to be mapped as Zone AE, the 170 cfs over the Enterprise Basin spillway must be safely conveyed towards the San Benito River and not cause inundation of structures downstream. The flow path will follow along the north side of Enterprise Road where it joins with the existing conditions runoff from Lico South. This area will likely be mapped as a Zone X Shaded Area.



Figure 6: Results for Double 72-inch Lico SD

#### Alternative 2: Lico Basin Floodwall

Alternative 2 assumes that a vertical floodwall is erected to contain all the inflow to Lico Basin, this results in no flow entering the Lico South property. As a result, flooding is greatly reduced compared to existing conditions. This eliminates flooding at the site, and water is impounded to 388.2 feet NAVD88. As the water that was previously going to Lico South property is redirected towards the Enterprise Pond, flooding in the area downstream of the Enterprise pond is increased. Except for a small area immediately downstream of the Enterprise Pond detention basin, the flooding depth is less than 1-foot.

A more detailed assessment of the upstream storm drain system would need to be considered to verify that upstream storm drain lines are not adversely affected by this higher tailwater condition



Figure 7: Results for Lico Basin with Floodwall

#### **Alternative 3: Lico Basin Raised Crest and Spillway**

Raising the spillway and dam overtopping elevation allowed more water to pass to the Enterprise Pond detention basin compared to the existing conditions. However, 18 ac-ft of flow still entered the Lico South property via the Lico Basin spillway and basin overtopping. The reduction in the level of flooding within the Lico South Property as a result of raising the spillway and dam overtopping elevation was not enough to remove the 1-ft of flooding within the Lico South property (Figure 8). In addition, the Lico Basin water surface elevation will increase and could have upstream impacts on the inflow storm drain system.

Longreach Associates Inc. February 27, 2020

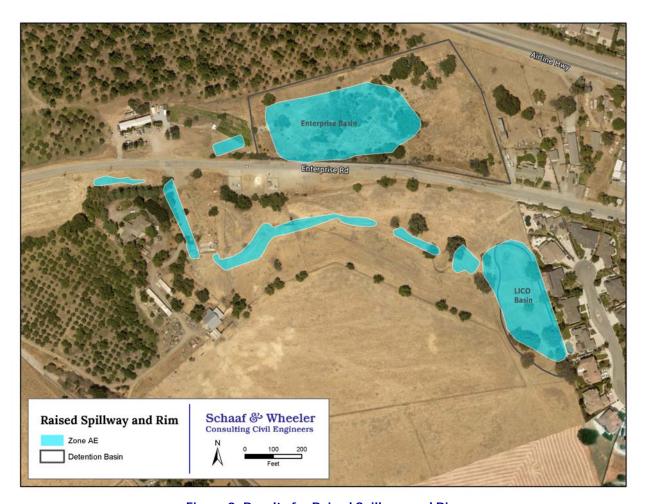


Figure 8: Results for Raised Spillway and Rim

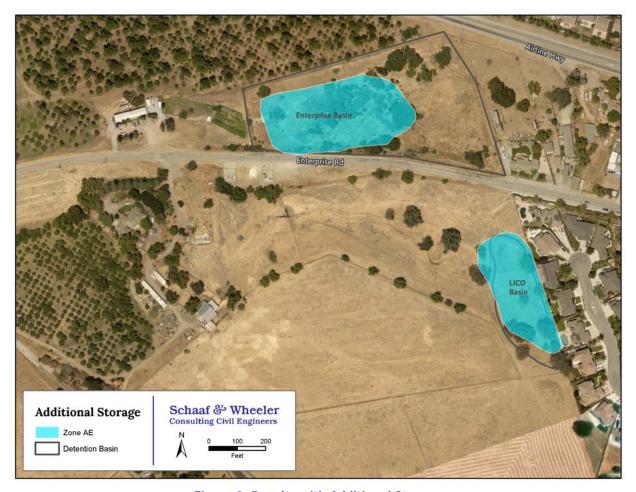


Figure 9: Results with Additional Storage

#### **Alternative 4: Increase Lico South Basin and Raise Spillway**

Increasing the size of the Existing Lico South Basin to capture the 38 acre-feet of overflow from the spillway would require the additional storage to be provided at the correct elevation (between 376.6 and 381) to maintain the existing pond water surface elevation. Two scenarios were investigated with this alternative. The first is if the storage was added below the existing spillway and the second is if the additional storage is added above the existing spillway elevation.

Adding storage below elevation 376.6 (spillway elevation) reduces the water surface in the basin causing the 72" RCP to release discharge at a slower rate than under existing conditions. Having a slower release rate increases the water volume is held in the pond, and some of the newly added storage ends up being filled before the peak runoff hits, this results in a total volume of 105 acre-ft being required if the basin is expanded. Adding approximately 40 acre-feet of storage above the spillway elevation, in contrast, would mimic the existing conditions timing of discharge release through the 72" RCP. But the surface area would be very large to maintain the water surface elevations in the basin at levels equal to or lower than the existing condition.

A comparison of the two described storage curves is provided in Figure 10, and the outflow curves are provided in Figure 11 to further illustrate the hydrograph timing. The storage added below the spillway results in approximately 105 acre-feet of storage to maintain the 380.4 feet pond water surface elevation.

The storage added above the spillway results in approximately 50.1 acre-feet of storage required at a peak elevation of 380.5 feet.

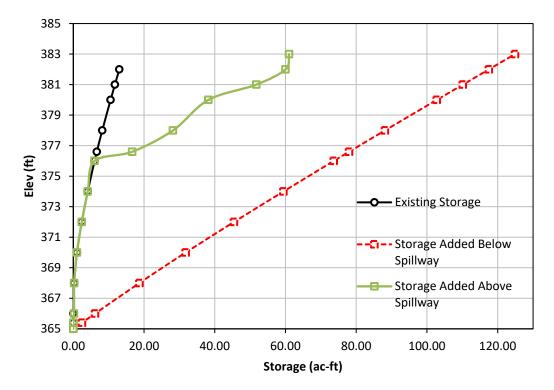


Figure 10: Storage Elevation Curves

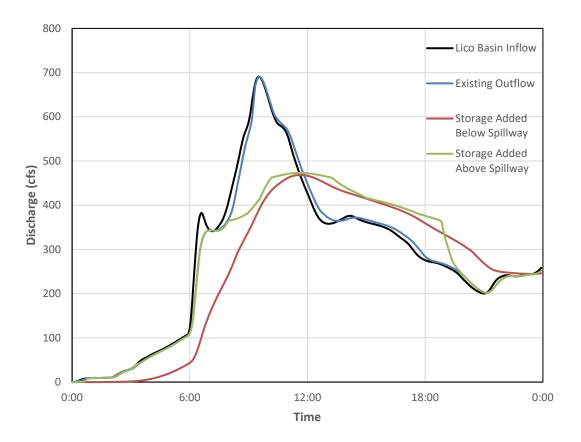


Figure 11: Outflow Discharge Curves

#### **Alternative 5: New Storage Facility Downstream of Lico South Basin**

All discharge from the existing Lico Basin is contained within a new detention pond or underground storage facility. All AE zones within the Lico South site are removed, except for the existing basin, and there are no impacts upstream or downstream (Figure 9). This alternative requires capturing the overflow volume downstream of the existing Lico Basin spillway and providing approximately 42 acrefeet of storage onsite separate from the Lico South Basin. The water surface elevation in the new storage facility should be lower than the Lico Basin Spillway elevation to avoid backwater conditions.

#### Conclusion

Five (5) potential improvement options were considered to eliminate flooding over 1-ft within the Lico South property. Of the alternatives explored, only Alternatives 4 and 5 remove flooding and do not impact upstream or downstream drainage. Alternative 1 impacts flood levels downstream and may require adding additional areas to the flood hazard map and overflow form the Enterprise Basin will need to be safely conveyed during the 100-year storm, although the additional mapping would be minimal (as shown on Figure 6). Alternative 2 may have impacts upstream due to a higher tailwater condition in the Lico South Basin. Alternative 4 requires potentially using developable area to provide the storage needed to maintain the existing pond water surface elevation. Alternative 4 also potentially requires more storage than Alternative 5, depending on where the additional storage is provided. Alternative 5 would reduce flooding onsite, but an outfall location would need to be identified to convey

pond discharge. Table 1 summarizes the potential implications that should be considered for each of the alternatives explored.

**Table 1: Alternative Analysis Summary** 

| Alternative  | Eliminates Flooding within Lico South Site?  | Potential US<br>Impact? | Potential DS Impact? | Potential Impacts usable space on site? |
|--|--|-------------------------|----------------------|---|
| Double 72-inch Lico SD                               | Yes  | No                      | Yes                  | No                                      |
| Lico Basin Floodwall                                 | Yes  | Yes                     | Yes                  | No                                      |
| Raise Lico Basin<br>Spillway and Crest               | Not without additional 18 acre-ft of storage | Yes                     | Yes                  | No                                      |
| Increase storage at Lico<br>Pond (up to 105 acre-ft) | Yes  | No                      | No                   | Yes                                     |
| New Basin with 42<br>Acre-ft of storage              | Yes  | No                      | No                   | Yes                                     |

As noted in Table 1, most of the options that are capable of eliminating flooding on-site without impacting the usable space but also have the potential for impacting upstream or downstream drainage systems. Alternative 1 does not require additional storage, uses the least amount of developable area, and has minimal impacts on the downstream FEMA Special Hazard Flood Zones. However, this alternative does cause the Enterprise Basin spillway to overtop during the 100-year storm. While the majority of the resulting flood depth downstream of the basin may be less than 1 foot deep, design should accommodate a safe discharge prevent downstream impacts. There would not be impacts on the upstream drainage system. If any of the above alternatives are constructed, a FEMA submittal will be required to remove the flood zone from within the Lico South site. Alternatives with potential upstream impacts would need to be further assessed to verify existing upstream systems are not significantly impacted.



Noise Measurements and Calculations

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285
      2019/10/17 12:35:10
                              44.5
286
      2019/10/17 12:35:13
                              44.9
287
      2019/10/17 12:35:16
                              44.1
      2019/10/17 12:35:19
288
                              45.7
289
      2019/10/17 12:35:22
                              45.3
290
      2019/10/17 12:35:25
                              46.6
291
      2019/10/17 12:35:28
                              48.5
      2019/10/17 12:35:31
292
                              48.4
293
      2019/10/17 12:35:34
                              47.5
294
      2019/10/17 12:35:37
                              46.9
295
      2019/10/17 12:35:40
                              48.2
      2019/10/17 12:35:43
296
                              65.7
297
      2019/10/17 12:35:46
                              66.9
298
      2019/10/17 12:35:49
                              58.5
299
      2019/10/17 12:35:52
                              54.1
300
      2019/10/17 12:35:55
                              52.5
```

## Roadway Construction Noise Model (RCNM), Version 1.1

Report date: 10/17/2019
Case Description: Lico Subdivision

---- Receptor #1 ----

Baselines (dBA)

Description Land Use Daytime Evening Night

Single-Family Resic Residential 80 80 80

Equipment

|                  |        | Spec           | Actual | Receptor | Estimated |
|------------------|--------|----------------|--------|----------|-----------|
|                  | Impact | Lmax           | Lmax   | Distance | Shielding |
| Description      | Device | Usage(%) (dBA) | (dBA)  | (feet)   | (dBA)     |
| Front End Loader | No     | 40             | 79.1   | L 50     | 0         |
| Dozer            | No     | 40             | 81.7   | 7 50     | 0         |

## Calculated (dBA)

 Equipment
 \*Lmax
 Leq

 Front End Loader
 79.1
 75.1

 Dozer
 81.7
 77.7

 Total
 81.7
 79.6

<sup>\*</sup>Calculated Lmax is the Loudest value.

#### **ELECTRICAL DATA**

| 38HDR        |              | VOLTAGE RANGE* |     | COMPRESSOR |       | OUTDOOR FAN MOTOR |           |           | MIN         | FUSE/            |
|--------------|--------------|----------------|-----|------------|-------|-------------------|-----------|-----------|-------------|------------------|
| UNIT<br>SIZE | V-PH-Hz      | Min            | Max | RLA        | LRA   | FLA               | NEC<br>Hp | kW<br>Out | CKT<br>AMPS | HACR BKR<br>AMPS |
| 018          | 208/230-1-60 | 187            | 253 | 9.0        | 48.0  | 0.80              | 0.125     | 0.09      | 12.1        | 20               |
| 024          | 208/230-1-60 | 187            | 253 | 12.8       | 58.3  | 0.80              | 0.125     | 0.09      | 16.8        | 25               |
| 030          | 208/230-1-60 | 187            | 253 | 14.1       | 73.0  | 1.45              | 0.25      | 0.19      | 19.1        | 30               |
|              | 208/230-1-60 | 187            | 253 | 14.1       | 77.0  | 1.45              | 0.25      | 0.19      | 19.1        | 30               |
| 036          | 208/230-3-60 | 187            | 253 | 9.0        | 71.0  | 1.45              | 0.25      | 0.19      | 12.7        | 20               |
|              | 460-3-60     | 414            | 506 | 5.6        | 38.0  | 0.80              | 0.25      | 0.19      | 7.8         | 15               |
|              | 208/230-1-60 | 187            | 253 | 21.8       | 117.0 | 1.45              | 0.25      | 0.19      | 28.7        | 50               |
| 048          | 208/230-3-60 | 187            | 253 | 13.7       | 83.1  | 1.45              | 0.25      | 0.19      | 18.6        | 30               |
|              | 460-3-60     | 414            | 506 | 6.2        | 41.0  | 0.80              | 0.25      | 0.19      | 8.6         | 15               |
|              | 208/230-1-60 | 187            | 253 | 26.4       | 134.0 | 1.45              | 0.25      | 0.19      | 34.5        | 60               |
| 060          | 208/230-3-60 | 187            | 253 | 16.0       | 110.0 | 1.45              | 0.25      | 0.19      | 21.5        | 35               |
|              | 460-3-60     | 414            | 506 | 7.8        | 52.0  | 0.80              | 0.25      | 0.19      | 10.6        | 15               |

<sup>\*</sup> Permissible limits of the voltage range at which the unit will operate satisfactorily

- Full Load Amps

HACR – Heating, Air Conditininng, Refrigeration

LRA – Locked Rotor Amps
NEC – National Electrical Code

- Rated Load Amps (compressor)

NOTE: Control circuit is 24—V on all units and requires external power source. Copper wire must be used from service disconnect to unit.

All motors/compressors contain internal overload protection.

#### **SOUND LEVEL**

| Unit Size | Standard    |      | Typical | Octave Band | Spectrum ( dBA | ) (without tone | adjustment) |      |
|-----------|-------------|------|---------|-------------|----------------|-----------------|-------------|------|
| Unit Size | Rating (dB) | 125  | 250     | 500         | 1000           | 2000            | 4000        | 8000 |
| 018       | 68          | 52.0 | 57.5    | 60.5        | 63.5           | 60.5            | 57.5        | 46.5 |
| 024       | 69          | 57.5 | 61.5    | 63.0        | 61.0           | 60.0            | 56.0        | 45.0 |
| 030       | 72          | 56.5 | 63.0    | 65.0        | 66.0           | 64.0            | 62.5        | 57.0 |
| 036       | 72          | 65.0 | 61.5    | 63.5        | 65.0           | 64.5            | 61.0        | 54.5 |
| 048       | 72          | 58.5 | 61.0    | 64.0        | 67.5           | 66.0            | 64.0        | 57.0 |
| 060       | 72          | 63.0 | 61.5    | 64.0        | 66.5           | 66.0            | 64.5        | 55.5 |

#### CHARGING SUBCOOLING (TXV-TYPE EXPANSION DEVICE)

| UNIT SIZE-VOLTAGE, SERIES | REQUIRED SUBCOOLING °F (°C) |
|---------------------------|-----------------------------|
| 018                       | 12 (6.7)                    |
| 024                       | 12 (6.7)                    |
| 030                       | 12 (6.7)                    |
| 036                       | 12 (6.7)                    |
| 048                       | 12 (6.7)                    |
| 060                       | 12 (6.7)                    |

# Appendix J

Traffic Impact Analysis

# Keith Higgins

# **Traffic Engineer**

# LICO SUBDIVISION TRAFFIC IMPACT ANALYSIS

## **ADMINISTRATIVE DRAFT REPORT**

SAN BENITO COUNTY, CALIFORNIA

Prepared for TTI Developers, Inc. Hollister, CA 95023

Prepared by Keith Higgins, Traffic Engineer Gilroy, CA 95020

November 14, 2019

Lico Subdivision Traffic Impact Analysis

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# 1 INTRODUCTION

A 149-unit residential subdivision is proposed on the south side of Enterprise Road, between Airline Highway (State Route 25) and Southside Road, adjacent to the existing Oak Creek and Quail Hollow subdivisions and just south of Hollister, in San Benito County, California. The location of the project and study area are indicated on **Exhibit 1**. The site plan is shown on **Exhibit 2**.

This report presents the findings of an analysis of vehicular, pedestrian, bicycle and transit circulation at the project site and the immediately surrounding street network.

# 1.1 Scope of Work

This report addresses the following topics:

- Existing vehicular, pedestrian and bicycle circulation at the two project access points and the surrounding street network.
- Assessment of potential impacts to vehicular, pedestrian, bicycle and transit circulation due to the Project, and recommendations to minimize or alleviate those impacts.
- Assessment of potential Background and Cumulative traffic impacts with and without the project and recommendations to minimize or alleviate project impacts.
- Assessment of site access and on-site circulation.
- Estimate of vehicle-miles traveled for the project.

#### 1.2 Study Network

The AM and PM peak periods are analyzed at the following intersections:

- 1. Ridgemark Drive Fairview Road / Airline Highway (State Route 25)
- 2. Enterprise Road / Airline Highway (State Route 25)
- Southside Road / Enterprise Road
- 4. Airline Highway (State Route 25) / Union Road
- Southside Road / Union Road
- 6. San Benito Street / Union Road
- Union Road Mitchell Road / State Route 156
- 8. Airline Highway (State Route 25) Pinnacles National Park Highway (State Route 25) / Tres Pinos Road Sunnyslope Road
- 9. San Benito Street / Nash Road

## 1.3 Traffic Operation Evaluation Methodologies

Intersection traffic operations were evaluated based upon the level of service (LOS) concept. LOS is a qualitative description of an intersection's operations, ranging from LOS A to LOS F. Level of Service "A" represents free flow uncongested traffic conditions. Level of Service "F" represents highly congested traffic conditions with unacceptable delay to vehicles at intersections. The intermediate levels of service represent incremental levels of congestion and delay between these two extremes. The analysis was performed using the 2010 and 2000 Highway Capacity Manual methodologies. LOS descriptions for each type of existing traffic control at the study intersections (i.e., signal and one-way stop) are included as **Appendix A**.

Intersection traffic operations were evaluated using the Synchro© traffic analysis software (Version 10). The average delay is then correlated to a level of service. For two-way stop-controlled intersections, only the vehicle delay for side street traffic is analyzed. LOS for each side street movement is based on the distribution of gaps in the major street traffic stream and driver judgment in selecting gaps. For signalized intersections, the overall intersection delay is used to determine LOS.

#### 1.4 Level of Service Standards

The study intersections are under the jurisdictions of San Benito County, the City of Hollister and Caltrans. San Benito County has jurisdiction over Intersections 3, 5 and 6. The City of Hollister has jurisdiction over Intersection 9. Caltrans has jurisdiction over Intersections 1, 2, 4, 7 and 8.

#### 1.4.1 San Benito County

The overall standard for congestion levels in San Juan Bautista is LOS D. LOS D is also considered the maximum acceptable level of service for side-street operations at one-and two-way stop-controlled intersections.

# 1.4.2 City of Hollister

The overall standard for congestion levels in the City of Hollister is LOS C.

#### 1.4.3 Caltrans

The Caltrans level of service standard is the transition from LOS C to LOS D (abbreviated as C-D in this report). This is essentially LOS C, which is identical to the City of Hollister level of service.

However, San Benito County General Plan Policy C-1.12 states that a standard of LOS D shall be used for all state highway facilities within the county, consistent with its countywide level of service standard. The following quote is from the *2035 San Benito County General Plan Update Revised Draft Environmental Impact Report*, EMC Planning Group, March 16, 2015:

As the LOS policy for such highways primarily affects local residents and local development, 2035 General Plan Policy C-1.12 proposes a LOS standard of D for state highway facilities within the County to accommodate expected development growth within the County while still providing reasonable operating conditions for auto traffic.

In addition to the fact that the Board of Supervisors has indicated that it wants to use LOS D as its new roadway improvement for General Plan consistency purposes, the County believes that LOS D is an appropriate threshold of significance for CEQA purposes, particularly if development becomes denser in the Hollister area and in the northern parts of the County nearer the Bay Area. Use of LOS D as a CEQA threshold of significance is consistent with the practice of many other public agencies in California and it is the recommended threshold of significance by the County's traffic experts. Use of LOS C as a threshold of significance for CEQA purposes is also likely to result in mitigation measures that result in overbuilding roadway improvements based on the County's policy priorities. Roadway improvements necessary to meet an [sic] LOS C in the buildout condition are not considered fundable, necessary or desirable.

For this reason, this report will apply a standard of LOS C to Caltrans intersections located in the City of Hollister (i.e., Intersection 8) and LOS D to Caltrans intersections located in unincorporated San Benito County (i.e., Intersections 1, 4, and 7). The San Benito County side-street LOS standard of LOS D will also apply to Caltrans intersections that have side-street stop control (i.e., Intersection 2).

# 1.5 Modeling of Right Turn on Red (RTOR)

All signalized study intersections allow right turns on red (RTOR), which generally reduce the overall intersection delay, thus improving the overall intersection level of service. There are several options to model right turns on red with different traffic analysis software packages, but the only method prescribed by the HCM for modeling RTOR is to reduce the input volumes to account for vehicles turning right on red. Where an exclusive right turn lane movement runs concurrent with a protected left turn phase from the cross street, the HCM allows for the right turn volume to be reduced by the number of simultaneous left turns. However, the length of the right turn lane affects the number of vehicles that can turn right on red. This is because a short right turn lane can result in right turning vehicles being trapped in the queue with vehicles in the through lane. For the purposes of this analysis, it is assumed that no vehicles would be able to turn right on red at any of the study intersections.

## 1.6 Significance Criteria

According to the California Environmental Quality Act (CEQA) guidelines, a project may have a significant effect on the environment if it would cause an increase in traffic that is substantial in relation to the existing traffic load and capacity of the street system. Neither San Benito County, the City of Hollister nor Caltrans have established formal significance criteria for roadways under their jurisdiction. Therefore, the following significance criteria have been used within this study, based upon the jurisdiction of each study intersection:

## 1.6.1 San Benito County

# Signalized or All-Way Stop-Controlled Intersections (Intersections 5, 6):

An impact at a signalized or all-way stop-controlled intersection under San Benito County jurisdiction is defined to occur under the following conditions:

- A significant impact would occur if an intersection operating at LOS A, B, C or D degrades to LOS E or F due to the addition of project trips; or
- For intersections already operating at LOS E or F, a significant impact would occur
  if the addition of project trips causes the intersection delay to increase by more
  than 4.0 seconds.

## One- or Two-Way Stop-Controlled Intersections (Intersection 3):

An impact at a one-way or two-way stop-controlled intersection under San Benito County jurisdiction is defined to occur under the following conditions:

- A significant impact would occur if side-street operations at an intersection operating at LOS A, B, C or D degrades to LOS E or F due to the addition of project trips <u>and</u> the traffic volumes with the addition of project trips are sufficiently high enough to satisfy the peak hour traffic signal warrant adopted by Caltrans in its Manual of Uniform Traffic Control Devices (CA MUTCD).
- For intersections with side-street operations already at E or F, a significant impact
  would occur if the project adds at least one trip to the intersection <u>and</u> the traffic
  volumes with the addition of project trips are sufficiently high enough to satisfy the
  peak hour traffic signal warrant adopted by Caltrans in its Manual of Uniform Traffic
  Control Devices (CA MUTCD).

# 1.6.2 City of Hollister

#### Signalized Intersections (Intersection 9):

An impact at a signalized intersection under the City of Hollister jurisdiction is defined to occur under the following conditions:

- A significant impact would occur if an intersection operating at LOS A, B or C degrades to LOS D, E or F due to the addition of project trips; or
- For intersections and roadway segments already operating at LOS D, E or F, a significant impact would occur if the addition of project trips causes the intersection delay to increase by more than 5.0 seconds.

#### 1.6.3 Caltrans

The significance criteria of San Benito County apply to intersections under Caltrans jurisdiction if the intersection is located in unincorporated San Benito County (i.e., Intersections 1, 2, 4 and 7).

An impact at a signalized study intersection under Caltrans jurisdiction and located in the City of Hollister (i.e., Intersection 8) is defined to occur under the following conditions:

- A significant impact would occur if an intersection operating at LOS A, B, or C preproject degrades to D, E or F due to the addition of project traffic; or
- For intersections already operating at LOS D, E or F, a significant impact would occur if the addition of project trips causes the overall intersection delay to increase by more than 1.0 seconds.

# 1.7 Regional Transportation Impact Mitigation Fee

The Council of San Benito County Governments (COG) administers the San Benito County Regional Transportation Impact Mitigation Fee (TIMF). This fee funds construction of traffic improvements on the regional highway system throughout northern San Benito County, including the following improvements in the study area (segment and intersection numbers are referenced from the TIMF study:

#### Segments:

- 1. Widen SR 156 to four lanes between The Alameda and Union Road.
- 4. Widen SR 25 to four lanes between Sunset Drive and Fairview Road.
- 5. estside Boulevard extension Nash Road to Southside Road / San Benito Street intersection.
- Widen Fairview Road between McCloskey Road and Airline Highway (SR 25).
- 8. Widen Union Road to four lanes between San Benito Street and Airline Highway (SR 25).
- 9. Widen Union Road to four lanes between San Benito Street and SR 156.
- 11. Widen SR 25 to four lanes between San Felipe Road and the Santa Clara County Line (Phases I and II).

## Intersections:

- 4. Signalize the Fairview Road Ridgemark Drive / Airline Highway (SR 25) intersection.
- 7. Signalize the Enterprise Road / Airline Highway (SR 25) intersection.
- 9. Convert the Rancho Drive / Nash Road Tres Pinos Road intersection into a roundabout.
- 10. Signalize the future San Benito Street / Westside Boulevard Southside Road intersection.

The TIMF is assessed based upon the square footage of the proposed building to be occupied by the Project. The Project's TIMF assessment will be determined by San Benito County, based upon the project definition and the fee rates established in *Regional Transportation Impact Mitigation Fee Nexus Study*, Michael Baker International, January 2016.

# 2 EXISTING TRAFFIC CONDITIONS

This chapter evaluates Existing traffic conditions and includes a description of the project setting.

# 2.1 Existing Traffic Network

The project site is located on the south side of Enterprise Road, between Southside Road and Airline Highway (State Route 25). Regional access to the project site is provided by State Route 25, State Route 156, Fairview Road and Union Road. Other roadways in the study area include Mitchell Road, Nash Road, Ridgemark Drive, San Benito Street, Southside Road, Sunnyslope Road, and Tres Pinos Road. The following is a brief description of each roadway in the study area.

State Route 25 (SR 25) is a two- to six-lane state highway in San Benito County, extending from US 101 south of Gilroy to Hollister, Pinnacles National Park, and State Route 198 in southern Monterey County. SR 25 is a major commute corridor between Hollister and Gilroy in route to San Jose and the greater San Francisco Bay Area. Within greater Hollister, SR 25 serves as the backbone for north-south intercity circulation, providing access to both residential neighborhoods and retail shopping areas. North of Tres Pinos Road – Sunnyslope Road, SR 25 is named Pinnacles National Park Highway, while south of Tres Pinos Road – Sunnyslope Road it is named Airline Highway. In the study area, the speed limit on SR 25 is 45 miles per hour (mph) north of Tres Pinos Road – Sunnyslope Road and Sunset Drive, and 55 mph south of Sunset Drive.

**State Route 156 (SR 156)** is a two- to four-lane state highway in San Benito County, connecting US 101 west of San Juan Bautista with State Route 152 north of Hollister. Due to its connections, SR 156 is a major commercial corridor that facilitates connections between Monterey County and the Central Valley of California. It also serves as a major commute corridor for residents of Hollister and San Juan Bautista. In the study area, SR 156 is a two-lane highway. The speed limit on SR 156 is 55 miles per hour (mph).

Caltrans will begin construction of the widening of SR 156 to a four-lane expressway from The Alameda to 4<sup>th</sup> Street (San Juan Road) west of Hollister in 2020. Construction is scheduled for completion in 2022.

**Enterprise Road** is a two-lane, east-west roadway in San Benito County, south of Hollister, providing access to rural residences and urban neighborhoods. The speed limit on Enterprise Road is 45 mph west of the project site and 30 mph east of the project site.

**Fairview Road** is a two-lane, north-south major thoroughfare in San Benito County, on the eastern border of Hollister. Due to its connections to both SR 25 and SR 156, Fairview Road serves as both an eastern and northern bypass roadway of Hollister. It also provides access to various urban neighborhoods in Hollister and rural residences east of Hollister. The speed limit on Fairview Road is 55 mph.

**Mitchell Road** is a two-lane rural roadway connecting to the agricultural fields and orchards north of SR 156 between Hollister and San Juan Bautista. The presumed speed limit on Mitchell Road is 55 mph.

Nash Road is a two-lane, east-west collector street in southern Hollister. West of San Benito Street, Nash Road provides access to San Benito High School, residential neighborhoods in western Hollister, and rural residential areas southwest of Hollister. East of San Benito Street, Nash Road provides access to both residential neighborhoods and commercial uses. East of Rancho Drive, Nash Road becomes **Tres Pinos Road**. The speed limit on Nash Road in the study area 30 mph west of San Benito Street and 35 mph east of San Benito Street.

**Ridgemark Drive** is a two-lane roadway that provides access to the Ridgemark neighborhood and the Ridgemark Golf Club and Resort. The speed limit on Ridgemark Drive is 25 mph.

San Benito Street is a two- to four-lane, north-south street in central Hollister. San Benito Street extends from Union Road south of Hollister to Santa Ana Road in northern Hollister, passing through the central business district of the city. It is a collector street between Union Road and South Street, a major collector between South Street and Fourth Street, and a major arterial between Fourth Street and Santa Ana Road. North of Santa Ana Road, San Benito Street changes names to San Felipe Road, connecting to both SR 25 and SR 156. The speed limit on San Benito Street is 55 mph (presumed) south of Nash Road and 30 mph north of Nash Road.

**Southside Road** is a two-lane roadway in southern Hollister and San Benito County. North of Union Road, Southside Road provides direct access to residential neighborhoods in southern Hollister. South of Union Road, Southside Road provides access to both urban neighborhoods and rural residential areas in unincorporated San Benito County. The speed limit on Southside Road is 45 mph.

**Sunnyslope Road** is a two- to four-lane, east-west major collector street in southeastern Hollister, providing access to various residential neighborhoods. The speed limit on Sunnyslope Road is 35 mph.

**Tres Pinos Road** is a four-lane, east-west major collector street in southwestern Hollister, providing access to commercial areas and residential neighborhoods. West of Rancho Drive, Tres Pinos Road becomes **Nash Road**. The speed limit on Tres Pinos Road is 35 mph.

**Union Road** is a two-lane, east-west major thoroughfare in San Benito County, south of Hollister. Due to its connections to both SR 156 and SR 25, Union Road serves as a southern bypass of Hollister. Union Road also extends east of SR 25 as a four-lane collector street, providing access to residential neighborhoods in southeastern Hollister. The speed limit on Union Road is 55 mph west of SR 25 and 35 mph east of SR 25.

# 2.2 Existing Pedestrian Network

Sidewalks are not currently provided on either side of Enterprise Road along the project frontage, nor to the west of the project site. However, a sidewalk exists on the south side of Enterprise Road between the eastern boundary of the project site and Airline Highway (SR 25). This connects to sidewalks within the adjacent Oak Creek and Quail Hollow subdivision. Segments of sidewalk are also provided along the residences fronting the north side of Enterprise Road east of the project site between the project site and Airline Highway (SR 25).

Sidewalks also exist on streets in the City of Hollister including Nash Road, San Benito Street, Sunnyslope Road and Tres Pinos Road. However, they do not extend to the immediate project site.

There are no marked crosswalks at intersections near the project site, such as on Enterprise Road or Southside Road. Crosswalks are present at the Southside Road / Union Road intersection, but do not connect to any sidewalks on either street. All other study intersections in the City of Hollister have crosswalks which connect to sidewalks.

## 2.3 Existing Bicycle Network

There are four types of bicycle facilities defined by Caltrans. Each type is described below:

- 1. <u>Bike path (Class I)</u> A separate right-of-way designed for the exclusive use of bicycle and pedestrian traffic with minimal cross-traffic.
- 2. <u>Bike lane (Class II)</u> A striped lane for one-way bike travel on a street or highway, typically including signs placed along the street segment.
- 3. <u>Bike route (Class III)</u> Provides a shared use with pedestrian or motor vehicle traffic. Typically, these facilities are city streets with signage designating the segment for Bike Route without additional striping or facilities.

4. <u>Separated bikeways (Class IV)</u> – A bikeway for the exclusive use of bicycles and includes a separation between the bikeway and the through vehicular traffic. The separation may include, but is not limited to, grade separation, flexible posts, inflexible posts, inflexible barriers, or on-street parking.

According to the San Benito County Bicycle and Pedestrian Master Plan, Alta Planning + Design, December 2009, bicycle facilities are located on the following roadways:

#### Class II:

- 1. Nash Road, between Quail Run and Monterey Street (eastbound only).
- 2. Pinnacles National Park Highway (SR 25), between San Felipe Road and Tres Pinos Road (both directions).
- 3. San Benito Street, between Nash Road and Union Road (both directions).
- 4. Southside Road, between Carousel Drive and south of County Labor Camp Road (both directions).
- 5. Sunnyslope Road, between Airline Highway (SR 25) and Memorial Drive and between Cerra Vista Drive and Fairview Road (both directions).
- 6. Union Road, between Airline Highway (SR 25) and Calistoga Drive (both directions).

In addition, the shoulders of Airline Highway (SR 25) and SR 156 provide enough width to accommodate bicycle traffic.

# 2.4 Existing Transit Service

San Benito County Local Transportation Authority (LTA) provides fixed-route bus service in San Benito County. Operating as County Express, it provides three lines in Hollister, plus intra-county service to Gilroy via San Juan Bautista, Dial-a-Ride and Paratransit services.

There is no bus service to the immediate project vicinity. The nearest bus stop is located on Sunrise Drive east of Airline Highway (SR 25), an over 30-minute walks from the project site.

# 2.5 Existing Traffic Conditions

#### 2.5.1 Vehicle Circulation

Intersection turning movement volumes including cars, trucks, buses, bicyclists, and pedestrians were collected on Wednesday, September 25, 2019 during the AM (7:00 - 9:00 AM) and PM (4:00 - 6:00) peak hours. From these counts, the AM and PM peak hour volumes were derived. **Appendix B** contains the new traffic count data collected at these study intersections.

**Exhibit 3** depicts the AM and PM peak hour turning movement volumes for the study intersections under Existing Conditions.

Existing levels of service at the study intersections are summarized on **Exhibit 4A**. Recommended intersection improvements are summarized on **Exhibit 4B**. The LOS calculation sheets for Existing conditions can be found in **Appendix C**.

Most of the study intersections currently operate at or better than their respective level of service standards. However, the following intersection currently has a deficient level of service:

1. Intersection 4: Airline Highway (SR 25) / Union Road – Overall LOS E (AM), which is below the County standard of LOS D.

#### 2.5.2 Pedestrian Circulation

There is minimal pedestrian activity in most of the study area. The highest volume of intersection pedestrian crossings at most of the study intersection approaches was just one pedestrian during either peak hour. However, two intersections have much higher pedestrian crossings during the peak hours:

- 1. Airline Highway (State Route 25) Pinnacles National Park Highway (State Route 25) / Tres Pinos Road Sunnyslope Road: 48 crossings (AM), 17 crossings (PM).
- 2. San Benito Street / Nash Road: 217 crossings (AM), 38 crossings (PM).

These higher pedestrian crossing volumes are due to the proximity of these intersections to commercial shopping centers and Sunnyslope Elementary School (Intersection 1) and San Benito High School (Intersection 2).

# 2.5.3 Bicycle Circulation

Little to no bicycle traffic was counted at the study intersections during either of the peak periods. The highest number of bicyclists at any of the intersections was 7 bicyclists at the San Benito Street / Nash Road intersection during the PM peak hour.

# 3 EXISTING PLUS PROJECT CONDITIONS

# 3.1 Project Trip Generation

The project includes 149 single-family homes.

Trip generation for the project was estimated using trip rates published in *Trip Generation Manual*, Institute of Transportation Engineers (ITE), 10th Edition, 2017. This is the most recent version of the primary trip generation data source used by the traffic engineering and transportation planning industry.

**Exhibit 5** summarizes the project trip generation. The project would generate an estimated 1,407 daily trips, with 110 trips (28 in, 82 out) during the AM peak hour and 148 trips (93 in, 85 out) during the PM peak hour.

## 3.2 Project Trip Distribution and Assignment

**Exhibit 6** depicts the trip distribution for the project. This distribution was derived based upon existing traffic patterns at the study intersections as well as the locations of population subareas within commute distance of the project. The project trip distribution was combined with the project trip generation to estimate the project trip assignment depicted on **Exhibit 7**.

# 3.3 Existing Plus Project Traffic Conditions

#### 3.3.1 Vehicle Circulation

The project would have three access points – two on Enterprise Road and one via an extension of Quail Ridge Way from the adjacent Oak Creek residential subdivision. The trip assignment was added to the existing traffic volumes in **Exhibit 3** to estimate Existing Plus Project volumes, which are depicted on **Exhibit 8**.

Existing Plus Project intersection levels of service are summarized on **Exhibit 4A**. Recommended intersection improvements are summarized on **Exhibit 4B**. The LOS calculation sheets for Existing Plus Project conditions can be found in **Appendix D**.

Most of the study intersections under Existing Plus Project conditions would continue to operate at or better than their respective level of service standards. However, the following two intersections would operate at deficient levels of service under Existing Plus Project conditions:

- 1. Intersection 4: Airline Highway (SR 25) / Union Road Overall LOS E (AM)
- 2. Intersection 7: Union Road Mitchell Road / SR 156 Overall LOS E (AM)

Below is a discussion of the recommended improvements at the study intersections operating with deficient operations under Existing Plus Project conditions. These improvements would be necessary to improve operations to acceptable or better level of service.

#### 1. Intersection 4 – Airline Highway (SR 25) / Union Road:

The overall level of service under AM conditions would be a deficient LOS E, compared to LOS E without the Project. Vehicle delays at this intersection would increase by 0.0 seconds (AM) with the addition of project traffic. Per the significance criteria in Section 1.6, the Project would <u>not</u> result in a significant impact at this intersection. The Project would <u>not</u> be responsible for any improvements at this intersection.

## 2. Intersection 7 – Union Road – Mitchell Road / SR 156:

The overall level of service under AM conditions would be a deficient LOS E, compared to LOS D without the Project. Per the significance criteria in Section 1.6, the Project would result in a significant impact at this intersection.

- Recommendation: Implement the following, all of which are part of the San Benito County TIMF Segment 1 improvement:
  - a. Add a second eastbound SR 156 through lane and a second westbound SR 156 through lane
  - Widen and restripe northbound Union Road as two left turn lanes and one shared through/right turn lane
  - c. Restripe southbound Mitchell Road as one left turn lane and one shared through/right turn lane.
  - d. Add a westbound SR 156 right turn lane
  - e. Convert the north/south (Union Road and Mitchell Road) left turn phasing to Protected phasing.
- Operations after Implementation of Improvement: Overall LOS B (AM and PM).
- Responsibility for Improvement: Payment of San Benito County TIMF would constitute Project's responsibility towards this improvement. Construction of this improvement is planned to be completed by 2022.

The following improvement is also recommended to improve intersection safety and overall circulation:

## 3. Intersection 3 – Southside Road / Enterprise Road:

The left turn lane warrant is met for the southbound Southside Road left turn movement at this intersection. (See **Appendix I** for this warrant.)

- Recommendation: Implement the following:
  - a. Widen Southside Road at Enterprise Road to add a southbound left turn lane.
  - b. As an alternative or interim improvement, convert the Southside Road / Enterprise Road intersection into an all-way stop-controlled intersection.
- Operations after Implementation of Improvement:
  - o Recommendation: Side-Street LOS B (AM) and LOS A (PM).
  - Alternative/Interim: Overall LOS A (AM and PM)
- Responsibility for Improvement: The Project would be responsible for implementation of this improvement, subject to design approval by San Benito County.

#### 3.3.2 Pedestrian Circulation

The lack of sidewalks near the project site – combined with no sidewalk connections to the City of Hollister – will result in minimal generation of pedestrian traffic from the project site. Therefore, the project would not represent a significant impact to pedestrian circulation. The project will construct a sidewalk along its entire Enterprise Road frontage.

## 3.3.3 Bicycle Circulation

The project is anticipated to generate minimal bicycle traffic. Therefore, the project would not represent a significant impact to bicycle circulation. Pavement widening along Enterprise Road as a part of standard frontage improvements will be constructed by the project that will be able to accommodate a future Class II bike lane.

#### 3.3.4 Transit Circulation

The project would not increase transit usage, as there is no bus service within walking distance of the project site. Therefore, the project would not represent a significant impact to transit service.

#### 3.3.5 Regional Transportation Impact Mitigation Fee

The project would be responsible for payment of the San Benito County Regional Transportation Impact Mitigation Fee (TIMF), which would represent the project's fair

share contribution towards countywide roadway improvements funded by the fee program. San Benito County will determine the project's TIMF fee.

# 4 BACKGROUND CONDITIONS

This chapter describes Background Conditions, which represents traffic conditions with the additional traffic from land development that is approved but not yet built. This scenario does not include trips from the proposed project.

# 4.1 Background Traffic Volumes

Background traffic growth on the study street network was estimated based on traffic growth anticipated from approved projects throughout the study area and the adjacent City of Hollister. A list of approved residential and commercial projects in the City of Hollister – last updated by the City in July 2019 – was obtained from the City of Hollister web site – <a href="http://www.hollister.ca.gov/">http://www.hollister.ca.gov/</a>. The approved San Benito County projects in the immediate study area were estimated based on observations of developments currently under construction on Southside Road near the project. Background development includes about 2,600 dwelling units, which take approximately 10 years to be completed and occupied, or about the Year 2030. **Exhibits 9A and 9B** summarize the trip generation for these residential and commercial projects, respectively. Major Background projects in the study area include the following:

- West of Fairview 667-unit subdivision located on Fairview Road north of Airline Highway (SR 25).
- 2. Roberts Ranch 241-unit subdivision located north of Airline Highway (SR 25) and east of Enterprise Road.
- 3. <u>Fairview Corners</u> 220-unit subdivision located north of Airline Highway (SR 25) and east of Fairview Road.
- 4. <u>Santana Ranch</u> over 1,000-unit subdivision, plus commercial retail and an elementary school. Partially constructed.
- 5. <u>Sunnyside Estates</u> 200-unit subdivision located on Southside Road north of Hospital Road. Currently under construction.
- 6. <u>Bennett Ranch</u> 84-unit subdivision located on Southside Road south of Enterprise Road. Currently under construction.
- 7. <u>Bluffs at Ridgemark</u> 93-unit subdivision located adjacent to Southside Road south of Hospital Road but with vehicular access from Ridgemark Drive.
- 8. <u>San Juan Oaks Specific Plan</u> nearly 1,200-unit senior housing development with a resort hotel, retail, office space and medical offices, located adjacent to and existing golf course.
- Silver Oaks 170-unit senior housing subdivision on Valley View Road north of Union Road.

- Los Pinars 85-unit subdivision located east of San Benito Street and south of Nash Road.
- 11. <u>Hawkins Companies (Hollister Farms)</u> a nearly 166,000 square foot retail shopping center at west of Pinnacles National Park Highway (SR 25) and both north and south of Park Street. Under construction.

Background traffic growth in the study area was derived based on projected background project trip activity and growth trends from the traffic studies for these and other approved development projects. A full list of these traffic studies can be found in **Exhibits 9A and 9B.** 

The Background traffic growth was added to the Existing traffic volumes on **Exhibit 3** to estimate the Background traffic volumes depicted in **Exhibit 10**.

## 4.2 Background Traffic Conditions

#### 4.2.1 Vehicle Circulation

Background intersection levels of service are summarized on **Exhibit 4A**. Recommended intersection improvements are summarized on **Exhibit 4B**. **Appendix E** contains the level of service calculations under Background conditions.

Some of the study intersections under Existing Plus Project conditions would continue to operate at or better than their respective level of service standards. However, the following six intersections would operate at deficient levels of service under Existing Plus Project conditions. Intersections 2, 4 5 and 7 have a County standard of LOS D. Intersections 8 and 9 have a City LOS standard of C.

- 1. Intersection 2: Enterprise Road / Airline Highway Side-street LOS E (PM), whi
- 2. Intersection 4: Airline Highway (SR 25) / Union Road Overall LOS F (AM and PM)
- 3. Intersection 5: Southside Road / Union Road Overall LOS F (PM)
- Intersection 7: Union Road Mitchell Road / SR 156 Overall LOS F (AM and PM)
- Intersection 8: Airline Highway (SR 25) Pinnacles National Park Highway (SR 25) / Tres Pinos Road Sunnyslope Road Overall LOS D (AM and PM)
- 6. Intersection 9: San Benito Street / Nash Road Overall LOS E (AM and PM)

#### 4.2.2 Pedestrian Circulation

Background pedestrian volumes are anticipated to be similar to existing conditions near the project site. Background projects will be required to provide frontage improvements

including sidewalks to accommodate pedestrian traffic at each individual site. Background pedestrian traffic increases will not represent a significant impact to pedestrian circulation.

## 4.2.3 Bicycle Circulation

Background bicycle volumes are anticipated to be similar to existing conditions near the project site. Background projects will be required to provide frontage improvements including shoulder widening consistent with County and City requirements, which generally include bike lanes on collector and arterial streets. This will accommodate bicycle traffic at each individual site. Background bicycle traffic increases will not represent a significant impact to bicycle circulation.

#### 4.2.4 Transit Circulation

Background projects are anticipated to generate a minimal increase in transit usage, although the lack of bus service to the southernmost study intersections will concentrate usage increases to within central Hollister. Therefore, background projects would not represent a significant demand for, or impact to, transit service to the project vicinity.

# 5 BACKGROUND PLUS PROJECT CONDITIONS

This chapter describes Background Conditions plus traffic from the proposed project.

# 5.1 Background Plus Project Traffic Volumes

Project trips (**Exhibit 7**) described in the Existing Plus Project development scenario included in Chapter 3 were added to the Background volumes (**Exhibit 10**) to estimate Background Plus Project volumes, which are shown in **Exhibit 11**.

## 5.2 Background Plus Project Conditions Traffic Conditions

#### 5.2.1 Vehicle Circulation

Background Plus Project intersection levels of service are summarized on **Exhibit 4A**. Recommended intersection improvements are summarized on **Exhibit 4B**. The LOS calculation sheets for Background Plus Project traffic conditions can be found in **Appendix F**.

Some of the study intersections under Background Plus Project conditions would continue to operate at or better than their respective level of service standards. However, the following six intersections would operate at deficient levels of service under Background Plus Project conditions. These are the same intersections that will operate deficiently under Background Without Project conditions. Intersections 2, 4 5 and 7 have a County standard of LOS D. Intersections 8 and 9 have a City standard of LOS C.

- 1. Intersection 2: Enterprise Road / Airline Highway Side-street LOS E (PM)
- 2. Intersection 4: Airline Highway (SR 25) / Union Road Overall LOS F (AM and PM)
- 3. Intersection 5: Southside Road / Union Road Overall LOS F (PM)
- Intersection 7: Union Road Mitchell Road / SR 156 Overall LOS F (AM and PM)
- Intersection 8: Airline Highway (SR 25) Pinnacles National Park Highway (SR 25) / Tres Pinos Road Sunnyslope Road Overall LOS D (AM) and LOS E (PM)
- 6. Intersection 9: San Benito Street / Nash Road Overall LOS E (AM and PM)

Below is a discussion of the recommended improvements at the study intersections operating with deficient operations under Background Plus Project conditions. These improvements would be necessary to improve operations to acceptable or better level of service.

1. Intersection 2 – Enterprise Road – Airline Highway (SR 25):

The northbound Enterprise Road side-street level of service under PM conditions would be a deficient LOS E, compared to LOS E without the Project. The Project

would add 17 trips to the intersection during the PM peak hour. This intersection would also meet the Caltrans peak hour signal warrant. (See **Appendix I** for the warrant.) Per the significance criteria in Section 1.6, the Project would result in a significant impact at this intersection.

- Recommendation: Implement the following:
  - a. Signalize the intersection. This is the San Benito County TIMF Intersection 7 improvement.
  - b. Add a second eastbound Airline Highway (SR 25) through lane and a second westbound Airline Highway (SR 25) through lane. This is a part of the San Benito County TIMF Segment 4 improvement.
- Operations after Implementation of Improvement: Overall LOS A (AM) and LOS B (PM).
- Responsibility for Improvement: Payment of San Benito County TIMF would constitute Project's responsibility towards improvement.

# 2. Intersection 4 - Airline Highway (SR 25) / Union Road:

The overall level of service under AM conditions would be a deficient LOS F, compared to LOS F without the Project. Vehicle delays at this intersection would decrease by 0.5 seconds (AM) with the addition of project traffic. This is due to a peculiarity in the traffic analysis software. Essentially, the project will represent no increase in delay. Per the significance criteria in Section 1.6, the Project would <u>not</u> result in a significant impact at this intersection. The Project would <u>not</u> be responsible for any improvements at this intersection.

#### 3. Intersection 5 – Southside Road / Union Road:

The overall level of service under PM conditions would be a deficient LOS F, which is expected to be experienced under Background without Project conditions. Vehicle delays at this intersection would increase by 20.3 seconds (PM) with the addition of project traffic. Per the significance criteria in Section 1.6, the Project would result in a significant impact at this intersection.

- Recommendation: Implement the following, all of which are part of the San Benito County TIMF Segment 8 improvement:
  - a. Add a second eastbound Union Road through lane and a second westbound Union Road through lane
- Operations after Implementation of Improvement: LOS C (AM and PM).
- Responsibility for Improvement: Payment of San Benito County TIMF would constitute Project's responsibility towards improvement.

## 4. Intersection 7 – Union Road – Mitchell Road / SR 156:

The overall level of service under AM and PM conditions would be a deficient LOS F, which is expected under Background condition without the Project. Vehicle delays at this intersection would increase by 4.5 seconds (AM) and 2.9 seconds (PM). Per the significance criteria in Section 1.6, the Project would result in a significant impact at this intersection.

- Recommendation: Implement the following, all of which are part of the San Benito County TIMF Segment 1 improvement:
  - Add a second eastbound SR 156 through lane and a second westbound SR 156 through lane
  - b. Widen and restripe northbound Union Road as two left turn lanes and one shared through/right turn lane
  - c. Restripe southbound Mitchell Road as one left turn lane and one shared through/right turn lane.
  - d. Add a westbound SR 156 right turn lane
  - e. Convert the north/south (Union Road and Mitchell Road) left turn phasing to Protected phasing.
- Operations after Implementation of Improvement: LOS C (AM and PM).
- Responsibility for Improvement: Payment of San Benito County TIMF would constitute Project's responsibility towards improvement. Construction of this improvement will be completed by 2022.

# 5. <u>Intersection 8 – Airline Highway (SR 25) – Pinnacles National Park Highway (SR 25) / Tres Pinos Road – Sunnyslope Road:</u>

The overall level of service would be a deficient LOS D (AM) and LOS E (PM), which is expected under Background conditions without the Project. Vehicle delays at this intersection would increase by 0.0 seconds (AM) and 4.6 seconds (PM) with the addition of Project traffic. Per the significance criteria in Section 1.6, the Project would result in a significant impact at this intersection.

- Recommendation: Implement the following:
  - a. Optimize the intersection signal timing to better balance the lengths of the green times for all of the signal phases, including potential lengthening of the overall cycle length.

- b. Consider modifying the westbound Sunnyslope Road approach to add a second westbound left turn lane. This would require modifying the existing raised median and narrowing the travel lanes.
- Operations after Implementation of traffic signal optimization: Overall LOS C (AM and PM).
- Responsibility for Improvement: Caltrans would be responsible for implementation of this improvement, as part of its typical maintenance schedule for signal operations at this intersection.

## 6. Intersection 9 – San Benito Street / Nash Road:

The overall level of service would be a deficient LOS E (AM and PM), compared to LOS E without the Project. Vehicle delays at this intersection would decrease by 0.2 seconds (AM) and 0.3 seconds (PM) with the addition of project traffic. Per the significance criteria in Section 1.6, the Project would <u>not</u> result in a significant impact at this intersection. The Project would <u>not</u> be responsible for any improvements at this intersection. The Westside Boulevard extension – Nash Road to Southside Road / San Benito Street intersection (TIMF 5), would divert some traffic from this intersection which will result in some improvement in traffic operations. The following improvement is also recommended to improve intersection safety and overall circulation:

# 7. Intersection 3 – Southside Road / Enterprise Road:

The left turn lane warrant is met for the southbound Southside Road movement at this intersection. (See **Appendix I** for this warrant.)

- Recommendation: Implement the following:
  - a. Widen Southside Road at Enterprise Road to add a southbound left turn lane.
  - As an alternative or interim improvement, convert the Southside Road / Enterprise Road intersection into an all-way stop-controlled intersection.
- Operations after Implementation of Improvement:
  - Recommendation: Side-Street LOS B (AM and PM).
  - Alternative/Interim: Overall LOS B (AM and PM)
- Responsibility for Improvement: The Project would be responsible for implementation of this improvement, pending design approval by San Benito County.

#### 5.2.2 Pedestrian Circulation

Pedestrian traffic under Background Plus Project conditions is not anticipated to significantly increase over Existing Plus Project conditions. Therefore, the project would not represent a significant impact to pedestrian circulation under Background Plus Project conditions. The project will construct a sidewalk along its entire Enterprise Road frontage.

## 5.2.3 Bicycle Circulation

Bicycle traffic under Background Plus Project conditions is not anticipated to significantly increase over Existing Plus Project conditions. Therefore, the project would not represent a significant impact to bicycle circulation under Background Plus Project conditions. Pavement widening along Enterprise Road as a part of standard frontage improvements will be constructed by the project that will be able to accommodate a future Class II bike lane.

#### 5.2.4 Transit Circulation

Transit demand under Background Plus Project conditions is not anticipated to significantly increase over Existing Plus Project conditions. Therefore, the project would not represent a significant impact to transit circulation under Background Plus Project conditions.

# 6 CUMULATIVE WITHOUT PROJECT CONDITIONS

This chapter describes Cumulative Conditions which represent traffic operations anticipated in the Year 2035, or later, which is about 16 years or more in the future.

# 6.1 Cumulative Without Project Traffic Volumes

**Exhibit 12** depicts the Cumulative Without Project condition traffic volumes at the study intersections. These traffic volumes include the previously described background traffic growth plus additional future traffic growth in the study network, based on projections from the traffic analyses for the background projects cited on **Exhibits 9A and 9B.**Overall, these forecasts represent approximately the Year 2035, the buildout year of the San Benito County General Plan.

## 6.2 Cumulative Without Project Traffic Conditions

#### 6.2.1 Vehicle Circulation

**Exhibit 5A** summarizes the levels of service of the study intersections under Cumulative Without Project conditions. Recommended intersection improvements are summarized on **Exhibit 5B**. **Appendix G** contains the level of service calculations under Cumulative Without Project conditions.

Some of the study intersections under Cumulative Without Project conditions would continue to operate at or better than their respective level of service standards. However, the following six intersections would operate at deficient levels of service under Cumulative Without Project conditions.

- Intersection 2: Enterprise Road / Airline Highway Side-street LOS E (AM), LOS F (PM)
- 2. Intersection 4: Airline Highway (SR 25) / Union Road Overall LOS F (AM and PM)
- 3. Intersection 5: Southside Road / Union Road Overall LOS E (AM), LOS F (PM)
- Intersection 7: Union Road Mitchell Road / SR 156 Overall LOS F (AM and PM)
- Intersection 8: Airline Highway (SR 25) Pinnacles National Park Highway (SR 25) / Tres Pinos Road Sunnyslope Road Overall LOS D (AM) and LOS F (PM)
- 6. Intersection 9: San Benito Street / Nash Road Overall LOS F (AM and PM)

#### 6.2.2 Pedestrian Circulation

Sidewalks will be constructed as standard frontage improvements for all development in the City of Hollister and for County projects as determined by San Benito County. If

segments are missing because older land uses did not include sidewalk construction at the time they were developed, they should be constructed.

## 6.2.3 Bicycle Circulation

According to the *San Benito County Bicycle and Pedestrian Master Plan*, Alta Planning + Design, December 2009, the following bicycle infrastructure improvements are proposed in the study area:

#### Class I (Bike Path):

1. <u>U-38:</u> Southside Road, between Carousel Drive and south of County Labor Camp Road (east frontage of street).

## Class II (Bike Lanes):

- 1. <u>H-3 and U-3:</u> Airline Highway (SR 25), between Sunset Drive and Fairview Road (both directions).
- 2. <u>U-8:</u> Fairview Road, between Spring Grove Road and Airline Highway (SR 25) (both directions).
- 3. <u>U-11:</u> SR 156, between The Alameda and Buena Vista Road (both directions).
- 4. <u>U-21:</u> Union Road, between San Benito Street and Airline Highway (SR 25) (both directions).
- 5. U-22: Union Road, between Calistoga Road and Fairview Road (both directions).
- 6. <u>H-24:</u> Sunnyslope Road, between Memorial Drive and Cerra Vista Drive (both directions).
- 7. <u>H-25:</u> Nash Road and Tres Pinos Road, between west of Westside Boulevard and Airline Highway (SR 25) (both directions).

## Class III (Bike Route):

1. U-35: Union Road, between SR 156 and San Benito Street (both directions).

These bicycle improvements will be constructed as funding becomes available.

#### 6.2.4 Transit Circulation

San Benito County Local Transportation Authority (LTA) should consider extending bus service into southern Hollister. This would provide improved transit access to the vicinity of the project site.

# 7 CUMULATIVE PLUS PROJECT CONDITIONS

This section describes anticipated traffic conditions with the addition of Project traffic to Cumulative Without Project traffic volumes.

# 7.1 Derivation of Cumulative Plus Project Condition Traffic Volumes

The project trip assignment depicted on **Exhibit 7** was combined with the Cumulative Without Project volumes (**Exhibit 12**) to forecast Cumulative Plus Project volumes, which are depicted on **Exhibit 13**.

# 7.2 Cumulative Plus Project Traffic Conditions

#### 7.2.1 Vehicle Circulation

Cumulative Plus Project AM and PM intersection levels of service are summarized on **Exhibit 4A**. Recommended intersection improvements are summarized on **Exhibit 4B**. The LOS calculation sheets for Cumulative Plus Project traffic conditions can be found in **Appendix H**.

Some of the study intersections under Cumulative Plus Project conditions would continue to operate at or better than their respective level of service standards. However, the following six intersections would operate at deficient levels of service under Cumulative Plus Project conditions These are the same intersections that will operate deficiently under Background Without Project conditions. Intersections 2, 4 5 and 7 have a County standard of LOS D. Intersections 8 and 9 have a City standard of LOS C.

- Intersection 2: Enterprise Road / Airline Highway Side-street LOS E (AM), LOS F (PM)
- 2. Intersection 4: Airline Highway (SR 25) / Union Road Overall LOS F (AM and PM)
- 3. Intersection 5: Southside Road / Union Road Overall LOS E (AM), LOS F (PM)
- Intersection 7: Union Road Mitchell Road / SR 156 Overall LOS F (AM and PM)
- Intersection 8: Airline Highway (SR 25) Pinnacles National Park Highway (SR 25) / Tres Pinos Road Sunnyslope Road Overall LOS D (AM) and LOS F (PM)
- 6. Intersection 9: San Benito Street / Nash Road Overall LOS F (AM and PM)

Below is a discussion of the recommended improvements at the study intersections operating with deficient operations under Background Plus Project conditions. These improvements would be necessary to improve operations to acceptable or better level of service.

# 1. Intersection 2 – Enterprise Road – Airline Highway (SR 25):

The northbound Enterprise Road side-street level of service would be a deficient LOS E (AM) and LOS F (PM), compared to LOS E (AM) and LOS F (PM) without the Project. The Project would add 12 trips (AM) and 17 trips (PM) to the intersection. This intersection would also meet the Caltrans peak hour signal warrant. (See **Appendix I** for the warrant.) Per the significance criteria in Section 1.6, the Project would result in a significant impact at this intersection.

- Recommendation: Implement the following:
  - a. Signalize the intersection. This is the San Benito County TIMF Intersection 7 improvement.
  - b. Add a second eastbound Airline Highway (SR 25) through lane and a second westbound Airline Highway (SR 25) through lane. This is the San Benito County TIMF Segment 4 improvement.
- Operations after Implementation of Improvement: Overall LOS B (AM and PM).
- Responsibility for Improvement: Payment of San Benito County TIMF would constitute Project's responsibility towards improvement.

# 2. Intersection 4 – Airline Highway (SR 25) / Union Road:

The overall level of service would be a deficient LOS F (AM and PM), compared to LOS F (AM and PM) without the Project. Vehicle delays at this intersection would decrease by 0.5 seconds (AM) and increase by 16.1 second (PM) with the addition of project traffic. Per the significance criteria in Section 1.6, the Project would result in a significant impact at this intersection.

- Recommendation: Implement the following, all of which are San Benito County TIMF Segment 4 and 8 improvements:
  - a. Add a second eastbound Union Road through lane and a second westbound Union Road through lane.
  - b. Add a second northbound Airline Highway (SR 25) through lane and a second southbound Airline Highway (SR 25) through lane.
- Operations after Implementation of Improvement: Overall LOS D (AM and PM).
- Responsibility for Improvement: Payment of San Benito County TIMF would constitute Project's responsibility towards improvement.

#### 3. Intersection 5 – Southside Road / Union Road:

The overall level of service would be a deficient LOS E (AM) and LOS F (PM), compared to LOS E (AM) and LOS F (PM) without the Project. Vehicle delays at this intersection would increase by 3.0 seconds (AM) and 19.3 seconds (PM) with the addition of project traffic. Per the significance criteria in Section 1.6, the Project would result in a significant impact at this intersection.

- Recommendation: Implement the following, all of which are part of the San Benito County TIMF Segment 8 improvement:
  - a. Add a second eastbound Union Road through lane and a second westbound Union Road through lane
- Operations after Implementation of Improvement: LOS C (AM and PM).
- Responsibility for Improvement: Payment of San Benito County TIMF would constitute Project's responsibility towards improvement.

## 4. Intersection 7 – Union Road – Mitchell Road / SR 156:

The overall level of service under AM and PM conditions would be a deficient LOS F, compared to LOS F without the Project. Vehicle delays at this intersection would increase by 4.1 seconds (AM) and 3.1 seconds (PM). Per the significance criteria in Section 1.6, the Project would result in a significant impact at this intersection.

- Recommendation: Implement the following, all of which are part of the San Benito County TIMF Segment 1 improvement:
  - a. Add a second eastbound SR 156 through lane and a second westbound SR 156 through lane
  - b. Widen and restripe northbound Union Road as two left turn lanes and one shared through/right turn lane
  - c. Restripe southbound Mitchell Road as one left turn lane and one shared through/right turn lane.
  - d. Add a westbound SR 156 right turn lane
  - e. Convert the north/south (Union Road and Mitchell Road) left turn phasing to Protected phasing.
- Operations after Implementation of Improvement: LOS C (AM) and LOS D (PM).

- Responsibility for Improvement: Payment of San Benito County TIMF would constitute Project's responsibility towards improvement. Construction of this improvement is planned to be completed by 2022.
- 5. <u>Intersection 8 Airline Highway (SR 25) Pinnacles National Park Highway (SR 25) / Tres Pinos Road Sunnyslope Road:</u>

The overall level of service would be a deficient LOS D (AM) and LOS F (PM), compared to LOS D (AM) and LOS F(PM) without the Project. Vehicle delays at this intersection would decrease by 0.1 seconds (AM) and 0.2 seconds (PM) with the addition of Project traffic. Per the significance criteria in Section 1.6, the Project, the Project would <u>not</u> result in a significant impact at this intersection. The Project would <u>not</u> be responsible for any improvements at this intersection.

## 6. Intersection 9 – San Benito Street / Nash Road:

The overall level of service would be a deficient LOS F (AM and PM), compared to LOS F without the Project. Vehicle delays at this intersection would decrease by 0.8 seconds (AM) and 1.5 seconds (PM) with the addition of Project traffic. Per the significance criteria in Section 1.6, the Project would <u>not</u> result in a significant impact at this intersection. The Project would <u>not</u> be responsible for any improvements at this intersection. The Westside Boulevard extension – Nash Road to Southside Road / San Benito Street intersection (TIMF 5), would divert some traffic from this intersection which will result in some improvement in traffic operations.

The following improvement is also recommended to improve intersection safety and overall circulation:

#### 7. Intersection 3 – Southside Road / Enterprise Road:

The left turn lane warrant is met for the southbound Southside Road movement at this intersection. (See **Appendix I** for this warrant.)

- Recommendation: Implement the following:
  - a. Widen Southside Road at Enterprise Road to add a southbound left turn lane.
  - b. As an alternative or interim improvement, convert the Southside Road / Enterprise Road intersection into an all-way stop-controlled intersection.
- Operations after Implementation of Improvement:
  - Recommendation: Side-Street LOS B (AM and PM).
  - Alternative/Interim: Overall LOS B (AM and PM)

 Responsibility for Improvement: The Project would be responsible for implementation of this improvement, pending design approval by San Benito County.

## 7.2.2 Pedestrian Circulation

The Project will not noticeably increase pedestrian activity above levels expected under Cumulative Without Project conditions. Therefore, the Project would not represent a significant contribution to Cumulative Plus Project impacts to pedestrian circulation.

# 7.2.3 Bicycle Circulation

The Project will not noticeably increase bicycle activity above levels expected under Cumulative Without Project conditions. Therefore, the Project would not represent a significant contribution to Cumulative Plus Project impacts to bicycle circulation.

#### 7.2.4 Transit Circulation

The Project will not noticeably increase transit demand above levels expected under Cumulative Plus Project conditions. The Project would therefore not represent a significant contribution to Cumulative Plus Project transit demand. However, the City of Hollister should coordinate with the San Benito County Local Transportation Authority (LTA) regarding extending transit service to southern Hollister. This would add transit service as an option to southern Hollister and place transit service closer to the Project site.

# 8 SITE ACCESS AND INTERNAL CIRCULATION

This section summarizes the site access and internal circulation analysis, including operations of the Project driveway operations.

#### 8.1 Site Access

## 8.1.1 Project Access Operations

The project site plan depicted on **Exhibit 2** proposes two project access points onto Enterprise Road – one on the northwest side of the project site ("Project Access West") and one on the northeast side ("Project Access East). Due to the relatively modest traffic volumes on Enterprise Road, these driveways will operate acceptably through Cumulative Plus Project conditions. Left turn warrant evaluations at both project access points on Enterprise Road indicate that left turn lanes will not be warranted at either project access.

## 8.1.2 Project Access Sight Distance

The available vehicle sight distance at both project access points to Enterprise Road was evaluated. The signed speed limit on Enterprise Road is 45 mph, hence a design speed of 50 mph was used for this evaluation. For a design speed of 50 mph, Caltrans sight distance standard standards require a minimum stopping sight distance of 430 feet.

At the Project Access West, the available sight distance towards the east and west is approximately 500 feet, exceeding the minimum standard,.

At the Project Access East, the available sight distance to the east and west is also 500 feet.

1. There are no sight distance deficiencies. However, all fences, retaining walls, sound walls, entry signs and vegetation over three feet in height above the pavement elevation of either project access points shall be located no closer than 15 feet from the shoulder edge line on Enterprise Road.

#### 8.2 Internal Circulation

The project also proposes a connection to Quail Ridge Way at the southeastern corner of the project site. This street extension would also allow project traffic to travel into and out of the adjacent Oak Creek and Quail Hollow subdivisions. However, due to the slightly more circuitous access to Enterprise Road through those subdivisions compared to the project's more direct internal street circulation, few project trips are expected to use Quail Ridge Way to access the project site. About 15 homes in the southwestern corner of the existing Oak Creek and Quail Hollow residents may also use the easterly project access point on Enterprise Road while in transit to and from their homes, again because the project internal street system will provide a slightly more directly route to and from Enterprise Road than from within their own subdivision. Overall, the net traffic intrusion from the project into the Oak Creek and Quail Hollow subdivisions (and vice versa) will be minimal.

The internal street circulation will adequately serve the projected traffic demand. The internal street along the project's easterly boundary will provide the primary internal circulation. The proposed roundabout midway on this roadway will discourage higher travel speeds. The maximum volume on this street will be about 1,300 vehicles per day at its connection with Enterprise Road. Also, this section of street will have no residential driveway access. This volume is below thresholds where traffic calming could be considered. The volume is well within acceptable levels. The first section of this street that will have direct residential driveway access is south of the proposed roundabout. This section is expected to carry about 600 vehicles per day, which is well within acceptable levels for a local residential street.

The roundabout should have signs to indicate the circulation pattern around it and include either a mountable apron or mountable island to accommodate the wider turn radii of typical delivery and moving trucks. The entry vehicle deflections and signs for a standard roundabout would not be necessary for a traffic circle.

The project site plan proposes sidewalks along all of the internal streets. This will accommodate all internal pedestrian activity and connections into the adjacent Oak Creek and Quail Hollow neighborhoods. A sidewalk is also recommended along the project's Enterprise Road frontage.

The internal project streets will also provide for good internal circulation for bicycles within the project site. Vehicles will need to share the roadway with bicycles, which is typical of residential streets.

# 9 PROJECT VEHICLE MILES TRAVELED

**Exhibit 14** summarizes the total Vehicle Miles Traveled (VMT) for the Project. The VMT was calculated using the project trip generation (**Exhibit 6**) and project trip distribution (**Exhibit 7**), as well as the approximate distances between the project site and the destinations of the residents traveling to and from the project site. These distances and the percentage of project trips traveling to/from those locations are also shown on **Exhibit 14**.

The Project would have an estimated VMT of 12.0 miles per vehicle. This is slightly higher than the estimated 11.7 VMT per household for San Benito County as whole, per 2017 California Emissions Estimator Model (CalEEMod) data. The higher VMT for the project is due to the project's distance from the more-developed areas of Hollister, which will require more longer vehicle trips for work, school and shopping.

# 10 SUMMARY OF PROJECT RESPONSIBILITIES

- 1. Pay the San Benito County Regional Transportation Impact Mitigation Fee (TIMF). San Benito County will determine the Project's TIMF fee.
- Widen Southside Road to add a southbound left turn lane. An alternative or interim
  improvement would be to convert the Southside Road / Enterprise Road
  intersection into an all-way stop-controlled intersection. This improvement will
  require design approval by San Benito County.
- 3. To prevent sight distance deficiencies at both project access points to Enterprise Road, implement the following:
  - a. All fences, retaining walls, sound walls, entry monument signs and vegetation over three feet in height above the pavement elevation of either project access points shall be located no closer than 15 feet from the shoulder edge line on Enterprise Road.
- 4. Incorporate the following elements into the design of the roundabout to be constructed inside the project site:
  - a. Add signs to indicate the circulation pattern around the traffic circle
  - b. Incorporate either a mountable apron or mountable island to accommodate the wider turn radii of typical delivery and moving trucks.
- 5. Construct a sidewalk along the project's Enterprise Road frontage.

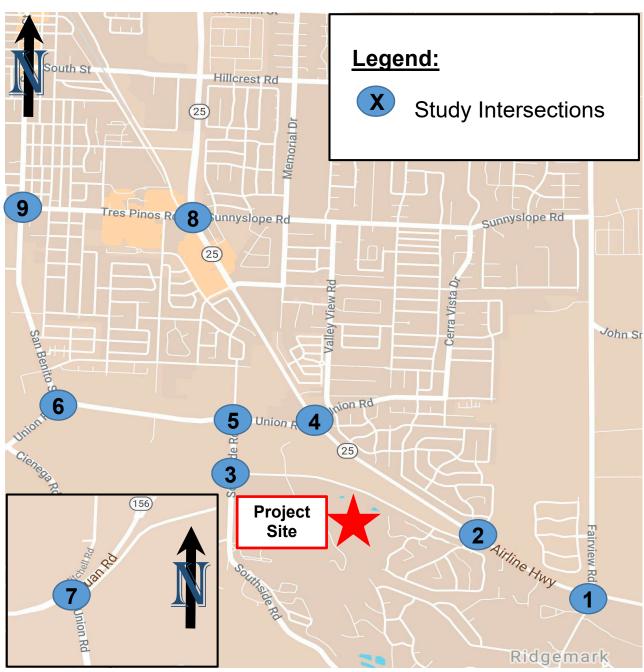
## 11 REFERENCES

#### 11.1 List of References

- 1. 2000 Highway Capacity Manual, Transportation Research Board, 2000.
- 2. 2010 Highway Capacity Manual, Transportation Research Board, 2010.
- 3. 2035 San Benito County General Plan Update Revised Draft Environmental Impact Report, EMC Planning Group, March 16, 2015.
- 4. Guide for the Preparation of Traffic Impact Studies, California Department of Transportation (Caltrans), December 2002.
- 5. Regional Transportation Impact Mitigation Fee Nexus Study, Michael Baker International, January 2016.
- 6. San Benito County Bicycle and Pedestrian Master Plan, Alta Planning + Design, December 2009.
- 7. San Benito County Express web site, <a href="http://www.sanbenitocountyexpress.org/">http://www.sanbenitocountyexpress.org/</a>. Accessed November 4, 2019.
- 8. Highway Design Manual, California Department of Transportation, Updated December 2018.
- 9. *Trip Generation Manual*, 10<sup>th</sup> Edition, Institute of Transportation Engineers, 2017.
- 10. City of Hollister web site, <a href="http://www.hollister.ca.gov/">http://www.hollister.ca.gov/</a>. Accessed October 30, 2019.
- 11. Google Maps web site, <a href="http://www.google.com/maps/">http://www.google.com/maps/</a>. Accessed November 12, 2019.
- 12. California Emissions Estimator Model Appendix D Default Data Tables, BREEZE Software in collaboration with South Coast Air Quality Management District and the California Air Districts, October 2017.
- 13. Traffic Impact Analyses in the Hollister vicinity listed on Exhibits 9A and 9B.

#### 11.2 List of Contacts

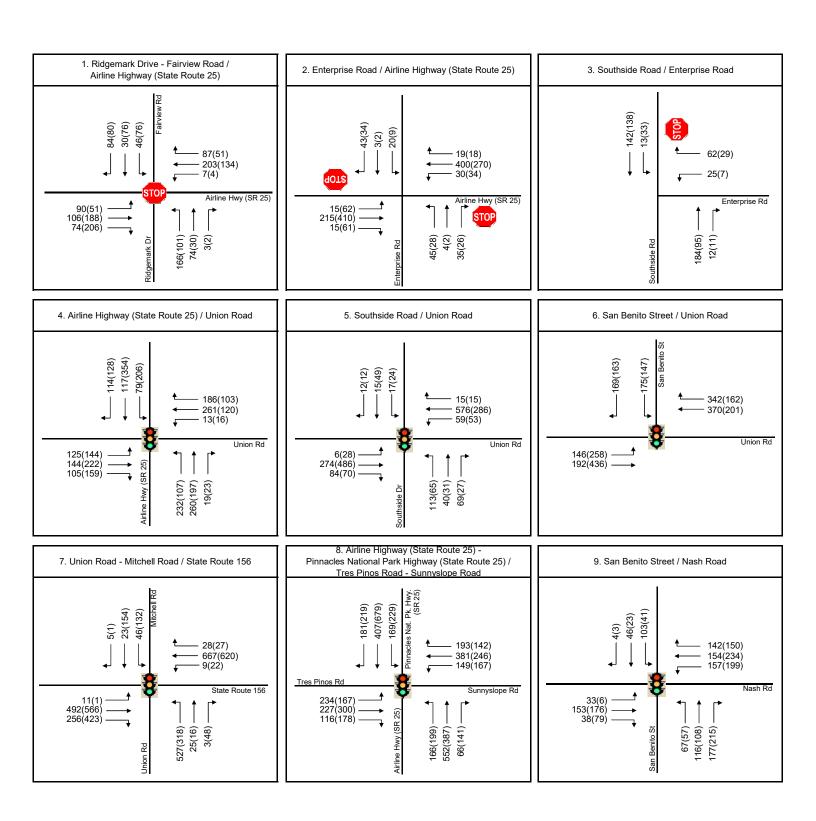
- 1. Ty Intravia, TTI Developers, Inc., Hollister, California.
- 2. Anne Hall, San Benito Engineering & Surveying, Inc., Hollister, California



Basemap Source: Google Maps, 2019.



Source: Sen Benito Engineering and Surveying, November 12, 2019.



- L, T, R = Left, Through, Right.
- 2. NB, SB, EB, WB = Left, Through, Right, Northbound, Southbound, Eastbound, Westbound.
- Per the San Benito County General Plan, all Caltrans intersections in unincorporated San Benito County also have the same level of service standards as San Benito County, 3. Overall and side-street level of service standard for San Benito County is LOS D. Overall and side-street level of service standard for the City of Hollister is LOS C.
- 4. For signalized and all-way stop intersection analysis, delay is average overall delay in seconds per vehicle (sec/veh). For one- and two-way stop intersections, namely LOS D. Overall Caltrans level of service standard in the City of Hollister is the transition between LOS C and LOS D, abbreviated as "LOS C-D".
  - delays are side-street approach operations, also in seconds per vehicle (sec/veh).

- 5. Analysis performed using 2000 and 2010 Highway Capacity Manual methodologies.
  - 6. Level of service calculations can be found in Appendices C through H.
- 7. LOS highlighted in red indicates intersection operating below level of service standard.
- recommended improvements noted under "With Improvements". A list of applied improvements 8. LOS with a thick black border represents a significant impact. Resulting levels of service with

can be found on Exhibit 4B.

Keith Higgins Traffic Engineer

Intersection Levels of Service **Exhibit 4A** 

|   | N-S<br>Street  | E-W<br>Street                              | Existing<br>Intersection<br>Control | Existing<br>Plus Project<br>Conditions   | Background<br>Plus Project<br>Conditions   | Cumulative<br>Plus Project<br>Conditions   |
|---|--|--|-------------------------------------|--|--|--|
| 1 | Ridgemark<br>Drive -<br>Fairview<br>Road   | Airline Highway (State Route 25)           | All-Way<br>Stop                     | None Required  | None Required  | None Required  |
| 2 | Enterprise<br>Road   | Airline<br>Highway<br>(State Route 25)     | Two-Way<br>Stop                     | None Required  | a. Signalize Intersection<br>b. Add 2nd EB T, 2nd WB T<br>(TIMF Intersection 7 and<br>Segment 4)   | a. Signalize Intersection<br>b. Add 2nd EB T, 2nd WB T<br>(TIMF Intersection 7 and<br>Segment 4)   |
| 3 | Southside<br>Road  | Enterprise<br>Road                         | One-Way<br>Stop                     | Add SB L<br>(OR, Convert to<br>All-Way Stop-Controlled<br>Intersection)  | Add SB L<br>(OR, Convert to<br>All-Way Stop-Controlled<br>Intersection)  | Add SB L<br>(OR, Convert to<br>All-Way Stop-Controlled<br>Intersection)  |
| 4 | Airline<br>Highway<br>(State Route 25)   | Union<br>Road                              | Signal                              | None Required  | None Required  | a. Add 2nd EB T, 2nd WB T<br>b. Add 2nd NB T, 2nd SB T<br>c. Add EB R<br>d. Convert E/W Left Turn<br>Phasing to Protected<br>(all are TIMF Segment 4<br>or TIMF Segment 8)       |
| 5 | Southside<br>Road  | Union<br>Road                              | Signal                              | None Required  | Add 2nd EB T, 2nd WB T<br>(TIMF Intersection 8)  | Add 2nd EB T, 2nd WB T<br>(TIMF Intersection 8)  |
| 6 | San Benito<br>Street   | Union<br>Road                              | Signal                              | None Required  | None Required  | None Required  |
| 7 | Union<br>Road -<br>Mitchell<br>Road  | State Route 156                            | Signal                              | a. Add 2nd EB T, 2nd WB T b. Widen and restripe NB as 2-L, 1-T/R c. Restripe SB as 1-L, 1-T/R d. Add WB R e. Convert N/S Left Turn Phasing to Protected (all are TIMF Segment 1) | a. Add 2nd EB T, 2nd WB T b. Widen and restripe NB as 2-L, 1-T/R c. Restripe SB as 1-L, 1-T/R d. Add WB R e. Convert N/S Left Turn Phasing to Protected (all are TIMF Segment 1) | a. Add 2nd EB T, 2nd WB T b. Widen and restripe NB as 2-L, 1-T/R c. Restripe SB as 1-L, 1-T/R d. Add WB R e. Convert N/S Left Turn Phasing to Protected (all are TIMF Segment 1) |
| 8 | Airline Highway (State Route 25) - Pinnacles National Park Hwy. (State Route 25) | Tres Pinos<br>Road -<br>Sunnyslope<br>Road | Signal                              | None Required  | Optimize Intersection<br>Signal Timing   | None Required  |
| 9 | San Benito<br>Street   | Nash<br>Road                               | Signal                              | None Required  | None Required  | None Required  |

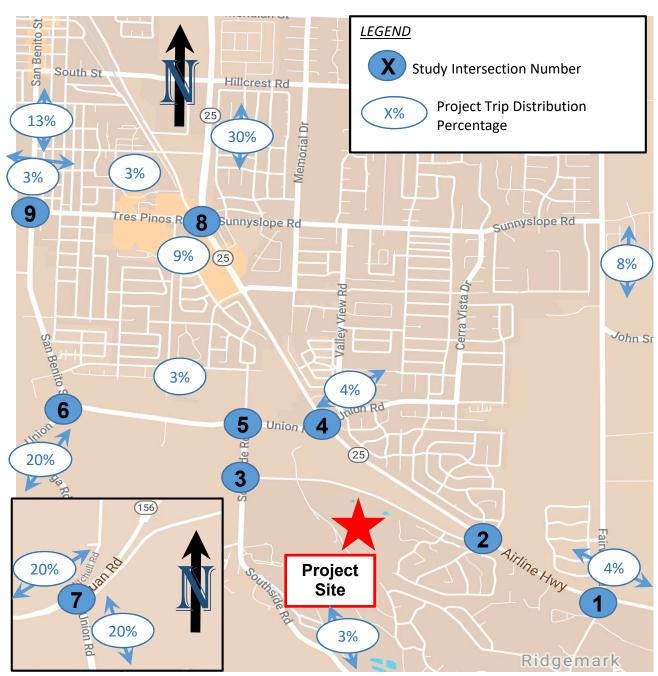
<sup>1.</sup> L, T, R = Left, Through, Right.

 $<sup>2. \</sup> NB, SB, EB, WB, N/S, E/W = Northbound, Southbound, Eastbound, Westbound, North/South, East/West. \\$ 

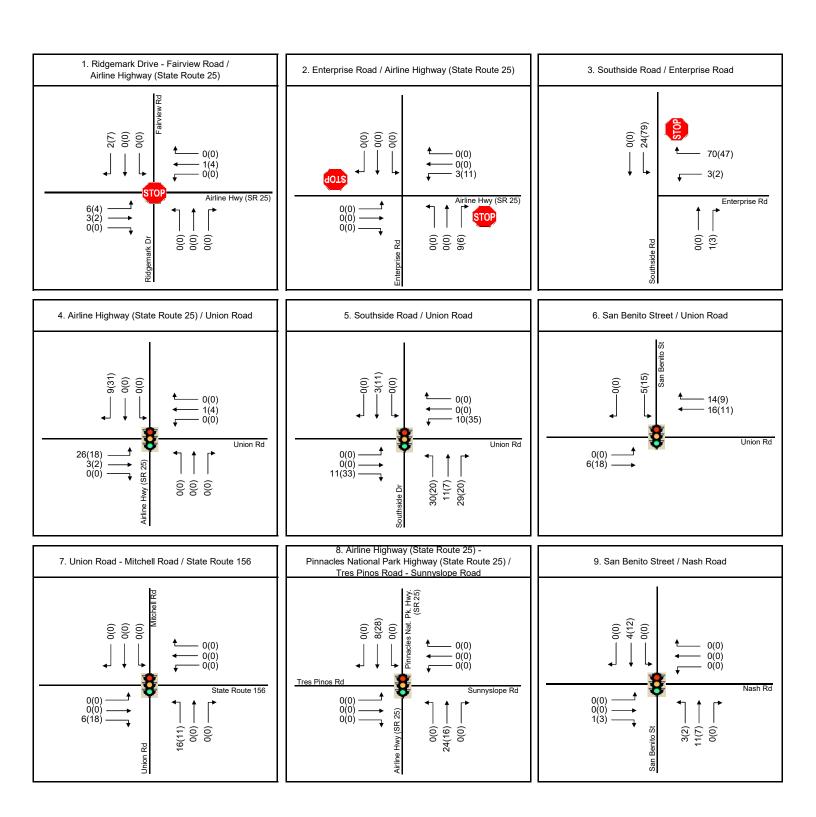
<sup>3.</sup> TIMF - San Benito County Regional Transportation Impact Mitigation Fee.

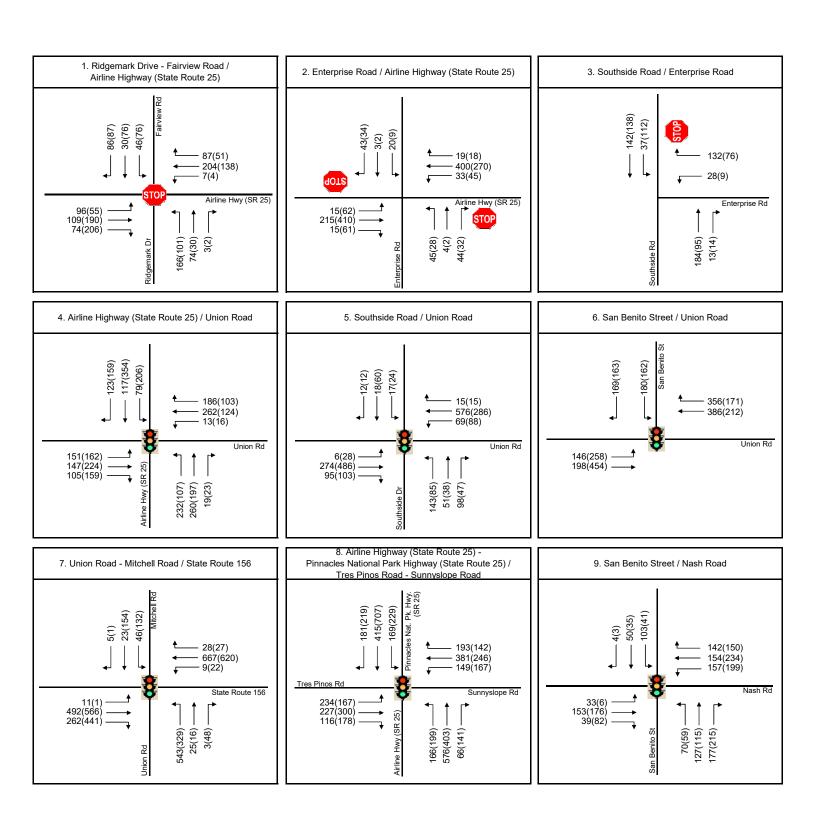
<u>Note:</u> 1. Trip generation rates from Institute of Transportation Engineers (ITE), *Trip Generation Manual* , 10th Edition, 2017.

Exhibit 5
Project Trip
Generation



Basemap Source: Google Maps, 2019.





#### List of Approved Projects - Residential

|                                      |                 |                |               | AM PE     | AK HOUR     |              |               | PM PEA    | K HOUR      |       |
|--------------------------------------|-----------------|----------------|---------------|-----------|-------------|--------------|---------------|-----------|-------------|-------|
|                                      |                 |                | PEAK          | %         |             |              | PEAK          | %         |             |       |
| PROJECT NAME                         | PROJECT<br>SIZE | DAILY<br>TRIPS | HOUR<br>TRIPS | OF<br>ADT | TRIPS<br>IN | TRIPS<br>OUT | HOUR<br>TRIPS | OF<br>ADT | TRIPS<br>IN | TRIPS |
| 1. West of Fairview                  | <u> </u>        |                |               | 7.5.      |             |              |               | 7.5.      |             |       |
| Single-Family Units                  | 507 units       | 4,786          | 375           | 8%        | 94          | 281          | 502           | 10%       | 316         | 186   |
| Duet Units                           | 60 units        | 439            | 28            | 6%        | 6           | 22           | 34            | 8%        | 21          | 13    |
| Multi-Family Units                   | 100 units       | 544            | 36            | 7%        | 9           | 27           | 44            | 8%        | 27          | 17    |
| 2. Silver Oaks                       | 170 units       | 726            | 41            | 6%        | 14          | 27           | 51            | 7%        | 31          | 20    |
| 3. Bella Serra                       | 63 units        | 461            | 29            | 6%        | 7           | 22           | 35            | 8%        | 22          | 13    |
| 4. Cerrato                           | 241 units       | 2,275          | 178           | 8%        | 45          | 133          | 239           | 11%       | 151         | 88    |
| 5. Orchard Park                      | 81 units        | 765            | 60            | 8%        | 15          | 45           | 80            | 10%       | 50          | 30    |
| 6. 540 Line St                       | 7 units         | 51             | 3             | 6%        | 1           | 2            | 4             | 8%        | 3           | 1     |
| 7. The Cottages                      | 39 units        | 368            | 29            | 8%        | 7           | 22           | 39            | 11%       | 25          | 14    |
| 8. El Cerro                          | 22 units        | 208            | 16            | 8%        | 4           | 12           | 22            | 11%       | 14          | 8     |
| 9. Farmstead                         | 13 units        | 123            | 10            | 8%        | 3           | 7            | 13            | 11%       | 8           | 5     |
| 10. James Mathews                    | 8 units         | 76             | 6             | 8%        | 2           | 4            | 8             | 11%       | 5           | 3     |
| 11. Sandra Cross                     | 3 units         | 28             | 2             | 7%        | 1           | 1            | 3             | 11%       | 2           | 1     |
| 12. Hillcrest Meadows                | 49 units        | 463            | 36            | 8%        | 9           | 27           | 49            | 11%       | 31          | 18    |
| 13. Falconi Way                      | 3 units         | 28             | 2             | 7%        | 1           | 1            | 3             | 11%       | 2           | 1     |
| •                                    | J units         | 20             |               | 1 70      | -           | - 1          | 3             | 1170      |             |       |
| 14. Allendale Single Family Units    | 279 units       | 2,634          | 206           | 8%        | 52          | 154          | 276           | 10%       | 174         | 102   |
| Single-Family Units                  |                 |                |               |           |             |              |               |           |             |       |
| Multi-Family Units                   | 60 units        | 439            | 28            | 6%        | 6           | 22           | 34            | 8%        | 21          | 13    |
| 15. Los Pinars                       | 45 "            | 440            |               | 00/       |             |              | 45            | 440/      |             | •     |
| Single-Family Units                  | 15 units        | 142            | 11            | 8%        | 3           | 8            | 15            | 11%       | 9           | 6     |
| Multi-Family Units                   | 44 units        | 322            | 20            | 6%        | 5           | 15           | 25            | 8%        | 16          | 9     |
| Attached Single-Family Units         | 26 units        | 245            | 19            | 8%        | 5           | 14           | 26            | 11%       | 16          | 10    |
| 16. CHISPA Sunrise Senior Apartments | 49 units        | 181            | 10            | 6%        | 4           | 6            | 13            | 7%        | 7           | 6     |
| 17. Pine Drive                       | 3 units         | 22             | 1             | 5%        | 0           | 1            | 2             | 9%        | 1           | 1     |
| 18. Roberts Ranch <sup>4</sup>       |                 |                |               |           |             |              |               |           |             |       |
| Single-Family Units                  | 192 units       | 1,828          | 144           | 8%        | 36          | 108          | 192           | 11%       | 121         | 71    |
| Multi-Family Units                   | 49 units        | 203            | 15            | 7%        | 3           | 12           | 18            | 9%        | 12          | 6     |
| 19. Lynn Lake                        | 5 units         | 47             | 4             | 9%        | 1           | 3            | 5             | 11%       | 3           | 2     |
| 20. Solorio Park I                   | 76 units        | 717            | 56            | 8%        | 14          | 42           | 75            | 10%       | 47          | 28    |
| 21. Solorio Park II                  | 25 units        | 236            | 19            | 8%        | 5           | 14           | 25            | 11%       | 16          | 9     |
| 22. Mirabella II                     |                 |                |               |           |             |              |               |           |             |       |
| Single-Family Units                  | 157 units       | 1,482          | 116           | 8%        | 29          | 87           | 155           | 10%       | 98          | 57    |
| Multi-Family Units                   | 26 units        | 190            | 12            | 6%        | 3           | 9            | 15            | 8%        | 9           | 6     |
| 23. 240 Sally St                     | 1 units         | 7              | 0             | 0%        | 0           | 0            | 1             | 14%       | 1           | 0     |
| 24. 811 Santa Ana Rd                 |                 |                |               |           |             |              |               |           |             |       |
| Single-Family Units                  | 9 units         | 85             | 7             | 8%        | 2           | 5            | 9             | 11%       | 6           | 3     |
| Multi-Family Units                   | 3 units         | 22             | 1             | 5%        | 0           | 1            | 2             | 9%        | 1           | 1     |
| 25. 221 Hawkins St                   | 3 units         | 28             | 2             | 7%        | 1           | 1            | 3             | 11%       | 2           | 1     |
| 26. Maple Park                       | 49 units        | 463            | 36            | 8%        | 9           | 27           | 49            | 11%       | 31          | 18    |
| 27. 400 Block                        | 22 units        | 161            | 10            | 6%        | 2           | 8            | 12            | 7%        | 8           | 4     |
| 28. Trillo Apartments                | 2 units         | 15             | 1             | 7%        | 0           | 1            | 1             | 7%        | 1           | 0     |
| 29. 638 Line St                      | 2 units         | 15             | 1             | 7%        | 0           | 1            | 1             | 7%        | 1           | 0     |
| 30. Maggie Lesende                   | 4 units         | 29             | 2             | 7%        | 0           | 2            | 2             | 7%        | 1           | 1     |
| 31. Bennet Ranch <sup>5</sup>        | 84 units        | 895            | 69            | 8%        | 17          | 52           | 90            | 10%       | 57          | 33    |
| 32. Sunnyside Estates <sup>6</sup>   | 200 units       | 1,904          | 150           | 8%        | 38          | 112          | 200           | 11%       | 126         | 74    |
| 33. Bluffs at Ridgemark <sup>9</sup> | 93 units        | 885            | 70            | 8%        | 17          | 53           | 93            | 11%       | 59          | 34    |
| 34. Santana Ranch <sup>10</sup>      |                 |                |               |           |             |              |               |           |             |       |
| Single-Family Units (remainder)      | 369 units       | 3,483          | 273           | 8%        | 68          | 205          | 365           | 10%       | 230         | 135   |
| Mulit-Family Units                   | 318 units       | 3,002          | 235           | 8%        | 59          | 176          | 315           | 10%       | 198         | 117   |
| Elementary School                    | 700 students    | 1,323          | 469           | 35%       | 253         | 216          | 119           | 9%        | 57          | 62    |
| 35. Fairview Corners <sup>11</sup>   | 220 units       | 2,105          | 165           | 8%        | 41          | 124          | 222           | 11%       | 140         | 82    |
| 36. San Juan Oaks <sup>12</sup>      |                 | ,              |               |           |             |              |               |           |             |       |
| Senior Adult Housing                 | 1,017 units     | 3,725          | 203           | 5%        | 71          | 132          | 256           | 7%        | 156         | 100   |
| Single-Family Units                  | 67 units        | 727            | 57            | 8%        | 14          | 43           | 73            | 10%       | 46          | 27    |
| Resort Hotel                         | 200 rooms       | 1,600          | 62            | 4%        | 45          | 17           | 84            | 5%        | 36          | 48    |
| ACOUNT HOLD                          |                 |                | 14            |           |             |              |               |           |             | 12    |
| Assisted Living                      | 100 beds        | 266            |               | 5%        | 9           | 5            | 22            | 8%        | 10          |       |

- Notes:
  1. Trip generation rates published by Institute of Transportation Engineers (ITE) Trip Generation Manual, 10th Edition, 2017, unless otherwise noted.
  2. sq. ft. = square feet.
  3. Source for city-approved projects: Residential-Commercial Project List July 2019, City of Hollister, July 2019.
  Source for county-approved projects: Observations and aerial review of under-construction projects, other research by Keith Higgins Traffic Engineer.
  4. Trip generation source: Roberts Ranch Property Residential Development, Hexagon Transportation Consultants, November 22, 2016.
  5. Trip generation source: Bennett Ranch Project 3061 Southside Road Initial Study / Mitigated Negative Declaration, FirstCarbon Solutions, no date available. 5. Trip generation source: Sunnyside Estates Residential Subdivision Transportation Impact Study. Wood Rodgers, October 2015.

  7. Trip generation source: Riverview II Subdivision, San Benito County, California, Keith Higgins Traffic Engineer, Fehr & Peers, June 21, 2019.

  8. Trip generation source: Ridgemark Assisted Care Community Traffic Impact Analysis, Pinnacle Traffic Engineering, August 3, 2018.

  9. Trip generation source: The Bluffs at Ridgemark Residential Subdivision Transportation Impact Analysis, Hexagon Transportation Consultants,
- October 21, 2016.

  10. Project Definition Source: Santana Ranch Specific Plan, Ruggeri-Jensen-Azar, November 6, 2009. Constructed units removed from total definition, based on review of Google Earth aerials.

  11. Trip generation source: Fairview Comers Residential, Hexagon Transportation Consultants, April 29, 2011.

  12. Trip generation source: San Juan Oaks Specific Plan Draft Transportation Impact Analysis, Fehr & Peers, June 2015.



#### **List of Approved Projects - Commercial**

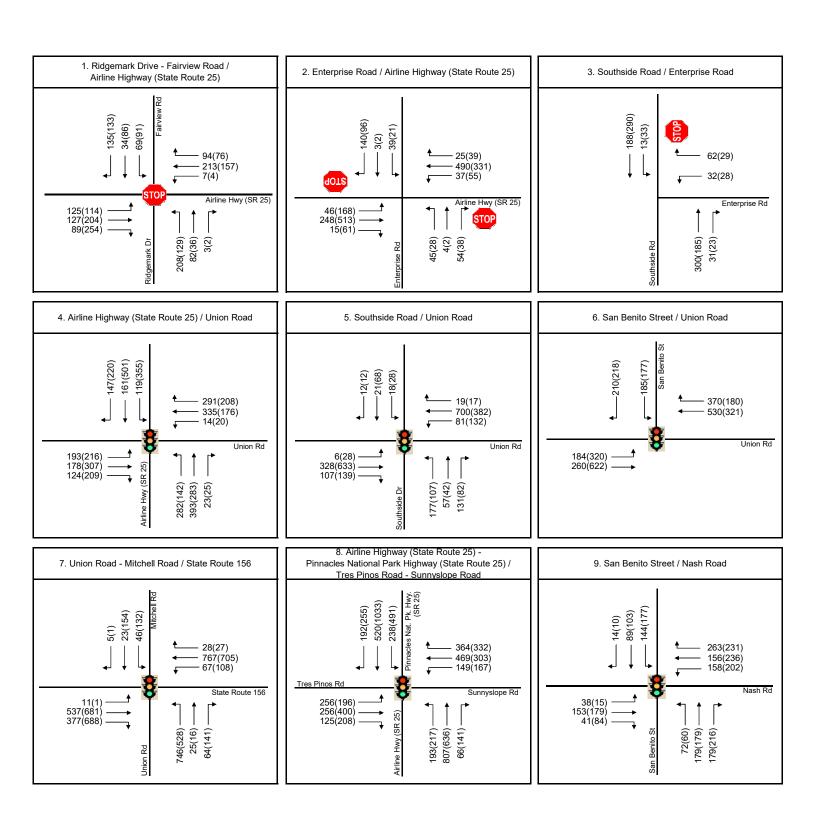
|  |                 |        |              |         | AK HOUR |       |              | PM PEAI | K HOUR |       |
|--|-----------------|--------|--------------|---------|---------|-------|--------------|---------|--------|-------|
|  | PROJECT         | DAILY  | PEAK<br>HOUR | %<br>OF | TRIPS   | TRIPS | PEAK<br>HOUR | %<br>OF | TRIPS  | TRIPS |
| PROJECT NAME                                       | SIZE            | TRIPS  | TRIPS        | ADT     | IN      | OUT   | TRIPS        | ADT     | IN     | OUT   |
| 1. Robert Cain                                     | 1,350 sq. ft.   | 39     | 4            | 10%     | 3       | 1     | 5            | 13%     | 2      | 3     |
| 2. Pride Conveyance, Inc.                          | 12,000 sq. ft.  | 60     | 8            | 13%     | 7       | 1     | 8            | 13%     | 1      | 7     |
| 3. Rong Chang USA/John Wynn                        | 151,200 sq. ft. | 750    | 266          | 35%     | 234     | 32    | 95           | 13%     | 12     | 83    |
| 4. Hawkins Companies/Christian Samples, AICP       | 165,533 sq. ft. | 6,249  | 156          | 2%      | 97      | 59    | 631          | 10%     | 303    | 328   |
| 5. Randy Griffith                                  | 5.5 acres       | 297    | 42           | 14%     | 37      | 5     | 38           | 13%     | 5      | 33    |
| 6. Anthony Gaetani/Gery Gaetani                    | 7,700 sq. ft.   | 38     | 5            | 13%     | 4       | 1     | 5            | 13%     | 1      | 4     |
| 7. Lynn Lake                                       | 2,183 sq. ft.   | 82     | 2            | 2%      | 1       | 1     | 8            | 10%     | 4      | 4     |
| 8. Gleanomic, LLC                                  | 79,400 sq. ft.  | 2,997  | 75           | 3%      | 47      | 28    | 303          | 10%     | 145    | 158   |
| 9. San Felipe Storage                              | 16,000 sq. ft.  | 24     | 2            | 8%      | 1       | 1     | 3            | 13%     | 1      | 2     |
| 10. Robert Enz                                     | 15,000 sq. ft.  | 26     | 3            | 12%     | 2       | 1     | 3            | 12%     | 1      | 2     |
| 11. American Casting                               | 21,200 sq. ft.  | 105    | 15           | 14%     | 13      | 2     | 13           | 12%     | 2      | 11    |
| 12. RSI Group/Nina Raey/Panera Bread               | 3,851 sq. ft.   | 1,214  | 8            | 1%      | 5       | 3     | 54           | 4%      | 30     | 24    |
| 13. DelCurto Brothers Construction                 | 8,846 sq. ft.   | 334    | 8            | 2%      | 5       | 3     | 34           | 10%     | 16     | 18    |
| 14. Community Foundation                           | 10,858 sq. ft.  | 313    | 19           | 6%      | 13      | 6     | 25           | 8%      | 12     | 13    |
| 15. Hawkins Companies/Brandon Whallon              | 5,495 sq. ft.   | 2,588  | 221          | 9%      | 113     | 108   | 180          | 7%      | 94     | 86    |
| 16. Clearist Park, LLC <sup>4</sup>                | 207 acres       | 2,388  | 396          | 17%     | 323     | 73    | 374          | 16%     | 92     | 282   |
| 17. L.A. Hearn                                     | 15,000 sq. ft.  | 26     | 3            | 12%     | 2       | 1     | 3            | 12%     | 0      | 3     |
| 18. Hollister Paint Co.                            | 3,135 sq. ft.   | 5      | 1            | 20%     | 1       | 0     | 1            | 20%     | 0      | 1     |
| 19. Steel Solutions (Gillian Enz)                  | 22,800 sq. ft.  | 113    | 16           | 14%     | 14      | 2     | 14           | 12%     | 2      | 12    |
| 20. Jose Rodriguez                                 | 10,000 sq. ft.  | 17     | 2            | 12%     | 2       | 0     | 2            | 12%     | 1      | 1     |
| 21. RSI Group/Nina Raey/Denny's                    | 4,331 sq. ft.   | 486    | 43           | 9%      | 24      | 19    | 42           | 9%      | 26     | 16    |
| 22. Geary Coats                                    | 2,400 sq. ft.   | 91     | 2            | 2%      | 1       | 1     | 9            | 10%     | 4      | 5     |
| 23. Brandon Whallon/Hawkins Companies              | 9,017 sq. ft.   | 314    | 25           | 8%      | 20      | 5     | 31           | 10%     | 9      | 22    |
| 24. INCO Investments, LLC                          | 19,200 sq. ft.  | 33     | 3            | 9%      | 2       | 1     | 4            | 12%     | 1      | 3     |
| 25. Amanda Thai Bach/Victor Pascua                 | 13,752 sq. ft.  | 3,475  | 144          | 4%      | 81      | 63    | 300          | 9%      | 150    | 150   |
| 26. Carl Wood/Dollar General                       | 9,100 sq. ft.   | 578    | 29           | 5%      | 17      | 12    | 62           | 11%     | 32     | 30    |
| 27. Santana Ranch (Commercial) <sup>5</sup>        | 65,000 sq. ft.  | 2,454  | 61           | 2%      | 38      | 23    | 248          | 10%     | 119    | 129   |
| 28. San Juan Oaks (Commercial) <sup>6</sup>        |                 |        |              |         |         |       |              |         |        |       |
| Commercial/Retail                                  | 50,000 sq. ft.  | 2,216  | 48           | 2%      | 30      | 18    | 141          | 6%      | 62     | 79    |
| Office   | 7,500 sq. ft.   | 183    | 24           | 13%     | 21      | 3     | 87           | 48%     | 15     | 72    |
| Medical Office                                     | 7,500 sq. ft.   | 92     | 18           | 20%     | 14      | 4     | 27           | 29%     | 8      | 19    |
| Total Commercial Background Trips:                 |                 | 27,587 | 1,649        |         | 1,172   | 477   | 2,750        |         | 1,150  | 1,600 |
| Total Residential Background Trips (from Exhibit 9 | A):             | 40,769 | 3,339        |         | 1,030   | 2,309 | 3,921        |         | 2,425  | 1,496 |
| Total Background Trips (Residential and Commerci   | al):            | 68,356 | 4,988        |         | 2,202   | 2,786 | 6,671        |         | 3,575  | 3,096 |

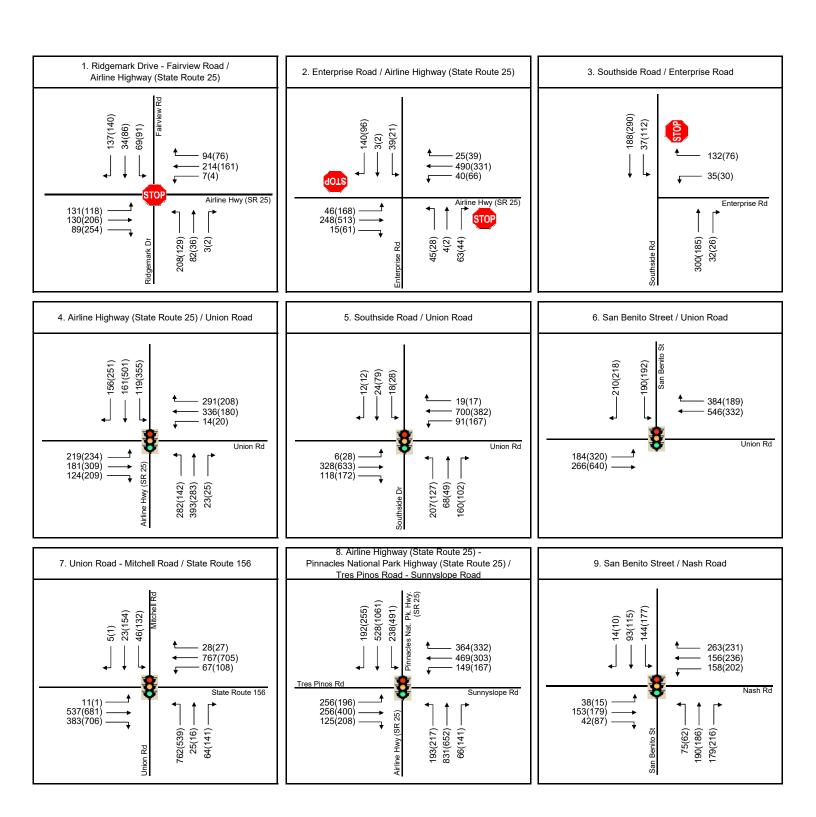
#### Notes:

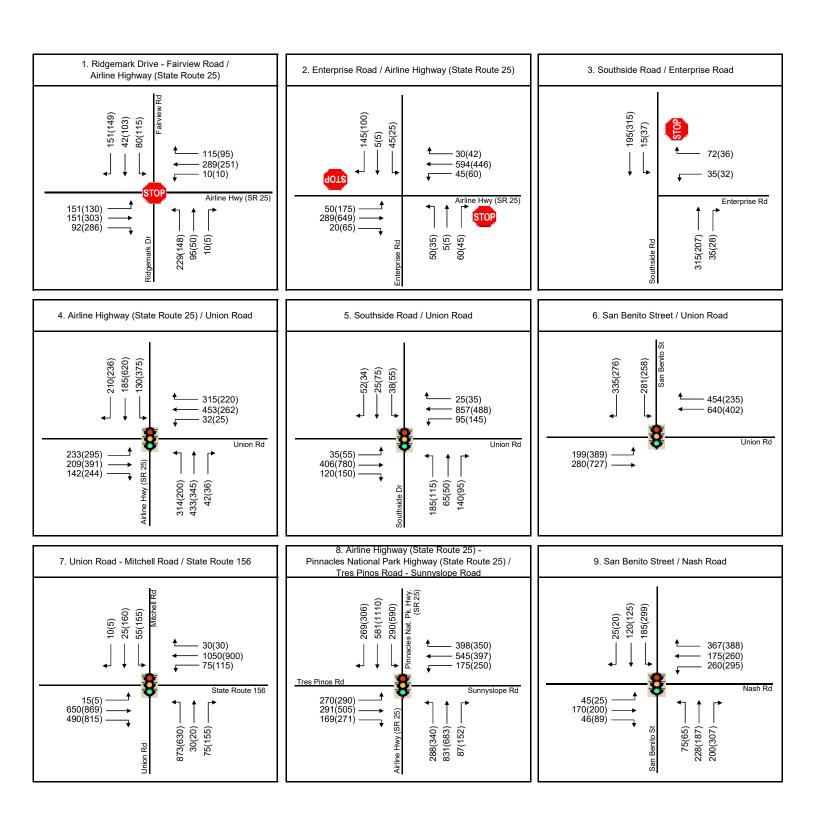
- 1. Trip generation rates published by Institute of Transportation Engineers (ITE) Trip Generation Manual, 10th Edition, 2017, unless otherwise noted.
- 2. sq. ft. = square feet.
- 3. Source for city-approved projects: Residential-Commercial Project List July 2019, City of Hollister, July 2019.

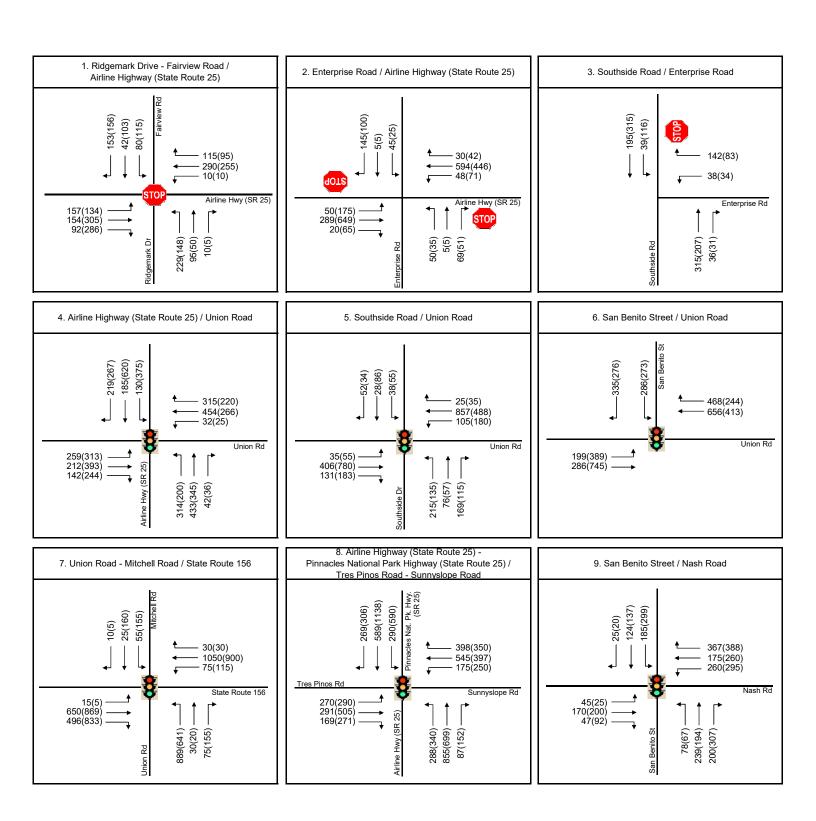
  Source for county-approved projects: Observations and aerial review of under-construction projects, other research by Keith Higgins Traffic Engineer staff.
- 4. Trip generation source: Traffic Impact Analysis 156 Business Parkway Project, Michael Baker International, January 15, 2019.
- 5. Project Definition Source: Santana Ranch Specific Plan, Ruggeri-Jensen-Azar, November 6, 2009.
- 6. Trip generation source: San Juan Oaks Specific Plan Draft Transportation Impact Analysis, Fehr & Peers, June 2015.











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Average Vehicle Miles Traveled per Household (San Benito Co.):

# Notes:

- 1. Total daily project trips cited from trip generation on Exhibit 5.
- 2. Trip destinations derived from project trip distribution on Exhibit 6.
- 3. Average vehicle-miles traveled for San Benito County quantified using data from BREEZE Software in collaboration with South Coast Air Quality Management California Emissions Estimator Model - Appendix D - Default Data Tables, District and the California Air Districts, October 2017.

# Keith Higgins Traffic Engineer

Exhibit 14
Project Vehicle Miles Traveled
Calculation

### Appendix A

Level of Service

Descriptions

### **APPENDIX A1**

### LEVEL OF SERVICE (LOS) DESCRIPTION SIGNALIZED INTERSECTIONS

The capacity of an urban street is related primarily to the signal timing and the geometric characteristics of the facility as well as to the composition of traffic on the facility. Geometrics are a fixed characteristic of a facility. Thus, while traffic composition may vary somewhat over time, the capacity of a facility is generally a stable value that can be significantly improved only by initiating geometric improvements. A traffic signal essentially allocates time among conflicting traffic movements that seek to use the same space. The way in which time is allocated significantly affects the operation and the capacity of the intersection and its approaches.

The methodology for signalized intersection is designed to consider individual intersection approaches and individual lane groups within approaches. A lane group consists of one or more lanes on an intersection approach. The outputs from application of the method described in the HCM 2010 and 2000are reported on the basis of each lane. For a given lane group at a signalized intersection, three indications are displayed: green, yellow and red. The red indication may include a short period during which all indications are red, referred to as an all-red interval and the yellow indication forms the change and clearance interval between two green phases.

The methodology for analyzing the capacity and level of service must consider a wide variety of prevailing conditions, including the amount and distribution of traffic movements, traffic composition, geometric characteristics, and details of intersection signalization. The methodology addresses the capacity, LOS, and other performance measures for lane groups and the intersection approaches and the LOS for the intersection as a whole.

Capacity is evaluated in terms of the ratio of demand flow rate to capacity (v/c ratio), whereas LOS is evaluated on the basis of control delay per vehicle (in seconds per vehicle). The methodology does not take into account the potential impact of downstream congestion on intersection operation, nor does the methodology detect and adjust for the impacts of turn-pocket overflows on through traffic and intersection operation.

### LEVEL OF SERVICE (LOS) CRITERIA FOR SIGNALIZED INTERSECTIONS

(Reference 2010 and 2000 Highway Capacity Manual)

| Level of Service | Control Delay (seconds / vehicle) |
|------------------|-----------------------------------|
| Α                | <10                               |
| В                | >10 - 20                          |
| С                | >20 - 35                          |
| D                | >35 - 55                          |
| E                | >55 - 80                          |
| F                | >80                               |

#### **APPENDIX A2**

## LEVEL OF SERVICE (LOS) DESCRIPTION UNSIGNALIZED INTERSECTIONS WITH ALL-WAY STOP CONTROL (AWSC)

AWSC intersections require every vehicle to stop at the intersection before proceeding. Since each driver must stop, the judgement as to whether to proceed into the intersection is a function of traffic conditions on the other approaches. While giving priority to the driver on the right is a recognized rule in some areas, it is not a good descriptor of actual intersection operations. What happens is the development of a consensus of right-of-way that alternates between the drivers on the intersection approaches, a consensus that depends primarily on the intersection geometry and the arrival patterns at the stop line.

If no traffic is present on the other approaches, a driver can proceed immediately after the stop is made. If there is traffic on one or more of the other approaches, a driver proceeds only after determining that there are no vehicles currently in the intersection and that it is the driver's turn to proceed. Since no traffic signal controls the stream movement or allocates the right-of-way to each conflicting stream, the rate of departure is controlled by the interaction between the traffic streams themselves.

For AWSC intersections, the average control delay (in seconds per vehicle) is used as the primary measure of performance. Control delay is the increased time of travel for a vehicle approaching and passing through an AWSC intersection, compared with a free-flow vehicle if it were not required to slow down or stop at the intersection.

The criteria for AWSC intersections have different threshold values than do those for signalized intersections, primarily because drivers expect different levels of performance from different kinds of traffic control devices (i.e., traffic signals, two way stop or all way stop, etc.). The expectation is that a signalized intersection is designed to carry higher traffic volumes than an AWSC intersection and a higher level of control delay is acceptable at a signalized intersection for the same LOS.

For AWSC analysis using the HCM 2010 method, the LOS shown reflects the weighted average of the delay on each of the approaches.

## LEVEL OF SERVICE (LOS) CRITERIA FOR AWSC INTERSECTIONS (Reference 2010 Highway Capacity Manual)

| Level of Service | Control Delay (seconds / vehicle) |
|------------------|-----------------------------------|
| Α                | 0 - 10                            |
| В                | >10 - 15                          |
| С                | >15 - 25                          |
| D                | >25 - 35                          |
| E                | >35 - 50                          |
| F                | >50                               |

#### **APPENDIX A3**

### LEVEL OF SERVICE (LOS) DESCRIPTION UNSIGNALIZED INTERSECTIONS WITH TWO-WAY STOP CONTROL (TWSC)

TWSC intersections are widely used and stop signs are used to control vehicle movements at such intersections. At TWSC intersections, the stop-controlled approaches are referred to as the minor street approaches; they can be either public streets or private driveways. The intersection approaches that are not controlled by stop signs are referred to as the major street approaches. A three-leg intersection is considered to be a standard type of TWSC intersection if the single minor street approach (i.e. the stem of the T configuration) is controlled by a stop sign. Three-leg intersections where two of the three approaches are controlled by stop signs are a special form of unsignalized intersection control.

At TWSC intersections, drivers on the controlled approaches are required to select gaps in the major street flow through which to execute crossing or turning maneuvers on the basis of judgment. In the presence of a queue, each driver on the controlled approach must use some time to move into the front-of-queue position and prepare to evaluate gaps in the major street flow. Capacity analysis at TWSC intersections depends on a clear description and understanding of the interaction of drivers on the minor or stop-controlled approach with drivers on the major street. Both gap acceptance and empirical models have been developed to describe this interaction.

Thus, the capacity of the controlled legs is based on three factors:

- the distribution of gaps in the major street traffic stream;
- driver judgment in selecting gaps through which to execute the desired maneuvers; and
- the follow-up time required by each driver in a queue.

The delay experienced by a motorist is made up of a number of factors that relate to control, geometrics, traffic and incidents. Total delay is the difference between the travel time actually experienced and the reference travel time that would result during base conditions, in the absence of incident, control, traffic or geometric delay. Average control delay for any particular minor movement is a function of the capacity of the approach and the degree of saturation and referred to as level of service.

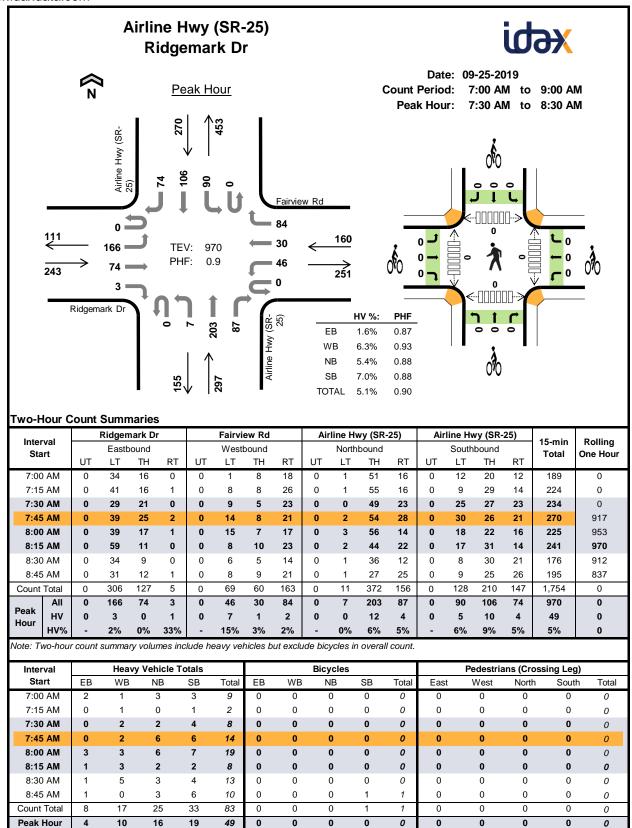
### LEVEL OF SERVICE (LOS) CRITERIA FOR TWSC INTERSECTIONS

(Reference 2010 Highway Capacity Manual)

| , | 5 · · · · · · · · · · ·           |
|---|-----------------------------------|
| Level of Service                        | Control Delay (seconds / vehicle) |
| A                                       | 0 - 10                            |
| В                                       | >10 - 15                          |
| С                                       | >15 - 25                          |
| D                                       | >25 - 35                          |
| E                                       | >35 - 50                          |
| F                                       | >50                               |

### Appendix B

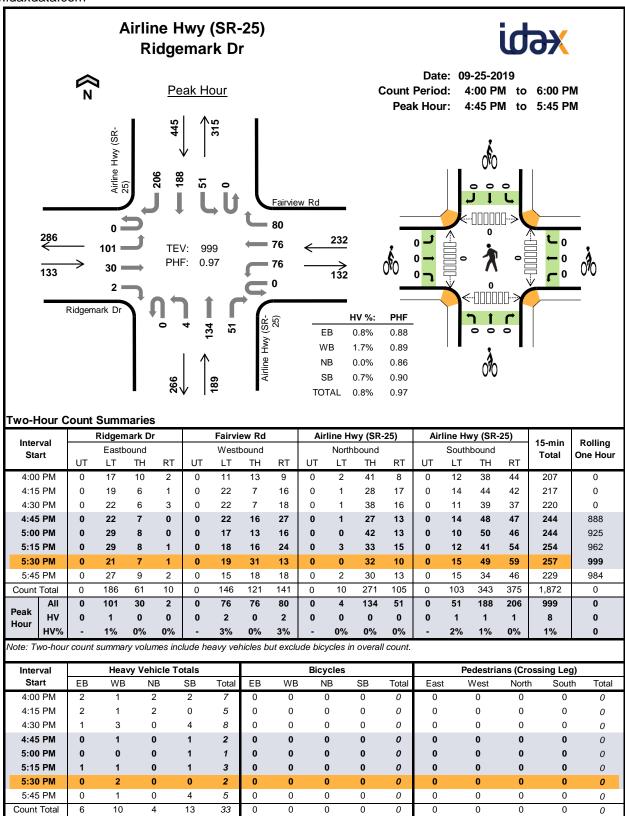
Intersection
Traffic Volume
Counts



| Interval    |    | Ridgen | nark Dr |    |    | Fairvi | ew Rd |    | Air | line Hv | vy (SR- | 25) | Air | line Hv | vy (SR- | 15-min | Rolling   |           |
|-------------|----|--------|---------|----|----|--------|-------|----|-----|---------|---------|-----|-----|---------|---------|--------|-----------|-----------|
| Start       |    | Eastb  | ound    |    |    | West   | bound |    |     | North   | bound   |     |     | South   | bound   |        | Total     | One Hour  |
|             | UT | LT     | TH      | RT | UT | LT     | TH    | RT | UT  | LT      | TH      | RT  | UT  | LT      | TH      | RT     | . • • • • | 0.10 1.10 |
| 7:00 AM     | 0  | 2      | 0       | 0  | 0  | 0      | 0     | 1  | 0   | 0       | 2       | 1   | 0   | 2       | 0       | 1      | 9         | 0         |
| 7:15 AM     | 0  | 0      | 0       | 0  | 0  | 1      | 0     | 0  | 0   | 0       | 0       | 0   | 0   | 0       | 0       | 1      | 2         | 0         |
| 7:30 AM     | 0  | 0      | 0       | 0  | 0  | 1      | 0     | 1  | 0   | 0       | 2       | 0   | 0   | 0       | 3       | 1      | 8         | 0         |
| 7:45 AM     | 0  | 0      | 0       | 0  | 0  | 2      | 0     | 0  | 0   | 0       | 5       | 1   | 0   | 2       | 3       | 1      | 14        | 33        |
| 8:00 AM     | 0  | 2      | 0       | 1  | 0  | 2      | 1     | 0  | 0   | 0       | 3       | 3   | 0   | 3       | 2       | 2      | 19        | 43        |
| 8:15 AM     | 0  | 1      | 0       | 0  | 0  | 2      | 0     | 1  | 0   | 0       | 2       | 0   | 0   | 0       | 2       | 0      | 8         | 49        |
| 8:30 AM     | 0  | 1      | 0       | 0  | 0  | 2      | 0     | 3  | 0   | 1       | 2       | 0   | 0   | 1       | 2       | 1      | 13        | 54        |
| 8:45 AM     | 0  | 0      | 0       | 1  | 0  | 0      | 0     | 0  | 0   | 0       | 1       | 2   | 0   | 0       | 5       | 1      | 10        | 50        |
| Count Total | 0  | 6      | 0       | 2  | 0  | 10     | 1     | 6  | 0   | 1       | 17      | 7   | 0   | 8       | 17      | 8      | 83        | 0         |
| Peak Hour   | 0  | 3      | 0       | 1  | 0  | 7      | 1     | 2  | 0   | 0       | 12      | 4   | 0   | 5       | 10      | 4      | 49        | 0         |

| Intonial          | Ric | dgemark | Dr | F  | airview F | ₹d | Airlin | e Hwy (S  | SR-25) | Airlin | e Hwy (S | R-25) | 45              | Dalling             |
|-------------------|-----|---------|----|----|-----------|----|--------|-----------|--------|--------|----------|-------|-----------------|---------------------|
| Interval<br>Start | Е   | astboun | d  | ٧  | Vestboun  | d  | ١      | Northbour | nd     | s      | outhbour | nd    | 15-min<br>Total | Rolling<br>One Hour |
| - Ciant           | LT  | TH      | RT | LT | TH        | RT | LT     | TH        | RT     | LT     | TH       | RT    | . • • • •       | 0.10 1.10 4.1       |
| 7:00 AM           | 0   | 0       | 0  | 0  | 0         | 0  | 0      | 0         | 0      | 0      | 0        | 0     | 0               | 0                   |
| 7:15 AM           | 0   | 0       | 0  | 0  | 0         | 0  | 0      | 0         | 0      | 0      | 0        | 0     | 0               | 0                   |
| 7:30 AM           | 0   | 0       | 0  | 0  | 0         | 0  | 0      | 0         | 0      | 0      | 0        | 0     | 0               | 0                   |
| 7:45 AM           | 0   | 0       | 0  | 0  | 0         | 0  | 0      | 0         | 0      | 0      | 0        | 0     | 0               | 0                   |
| 8:00 AM           | 0   | 0       | 0  | 0  | 0         | 0  | 0      | 0         | 0      | 0      | 0        | 0     | 0               | 0                   |
| 8:15 AM           | 0   | 0       | 0  | 0  | 0         | 0  | 0      | 0         | 0      | 0      | 0        | 0     | 0               | 0                   |
| 8:30 AM           | 0   | 0       | 0  | 0  | 0         | 0  | 0      | 0         | 0      | 0      | 0        | 0     | 0               | 0                   |
| 8:45 AM           | 0   | 0       | 0  | 0  | 0         | 0  | 0      | 0         | 0      | 0      | 1        | 0     | 1               | 1                   |
| Count Total       | 0   | 0       | 0  | 0  | 0         | 0  | 0      | 0         | 0      | 0      | 1        | 0     | 1               | 0                   |
| Peak Hour         | 0   | 0       | 0  | 0  | 0         | 0  | 0      | 0         | 0      | 0      | 0        | 0     | 0               | 0                   |

Note: U-Turn volumes for bikes are included in Left-Turn, if any.

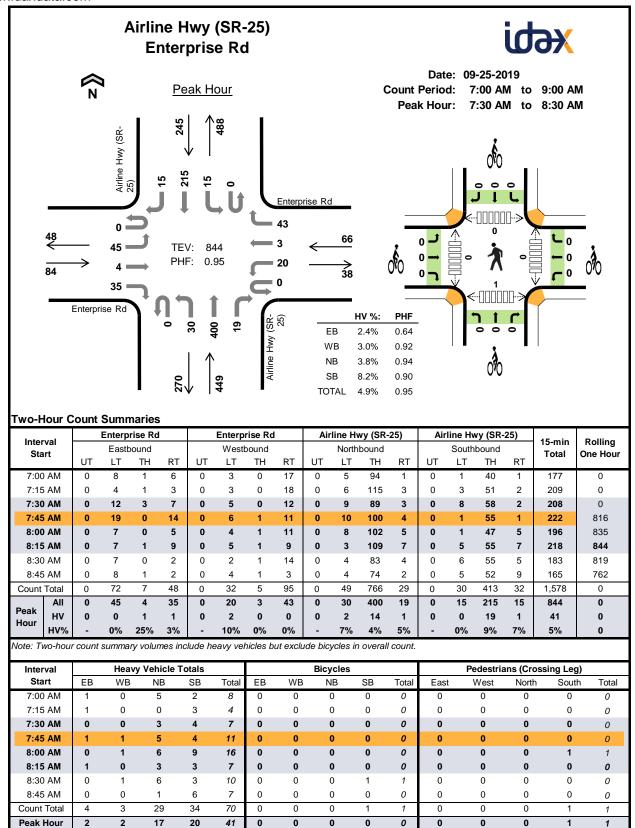


**Peak Hour** 

| Interval    |    | Ridger | nark Dr |    |    | Fairvi | ew Rd |    | Air | line Hv | vy (SR- | 25) | Airline Hwy (SR-25) |       |       |    | 15-min | Rolling  |
|-------------|----|--------|---------|----|----|--------|-------|----|-----|---------|---------|-----|---------------------|-------|-------|----|--------|----------|
| Start       |    | Eastb  | ound    |    |    | Westl  | bound |    |     | North   | bound   |     |                     | South | bound |    | Total  | One Hour |
|             | UT | LT     | TH      | RT | UT | LT     | TH    | RT | UT  | LT      | TH      | RT  | UT                  | LT    | TH    | RT |        | One Hou  |
| 4:00 PM     | 0  | 0      | 1       | 1  | 0  | 0      | 0     | 1  | 0   | 0       | 1       | 1   | 0                   | 0     | 1     | 1  | 7      | 0        |
| 4:15 PM     | 0  | 2      | 0       | 0  | 0  | 1      | 0     | 0  | 0   | 0       | 1       | 1   | 0                   | 0     | 0     | 0  | 5      | 0        |
| 4:30 PM     | 0  | 1      | 0       | 0  | 0  | 2      | 0     | 1  | 0   | 0       | 0       | 0   | 0                   | 1     | 1     | 2  | 8      | 0        |
| 4:45 PM     | 0  | 0      | 0       | 0  | 0  | 0      | 0     | 1  | 0   | 0       | 0       | 0   | 0                   | 1     | 0     | 0  | 2      | 22       |
| 5:00 PM     | 0  | 0      | 0       | 0  | 0  | 0      | 0     | 0  | 0   | 0       | 0       | 0   | 0                   | 0     | 1     | 0  | 1      | 16       |
| 5:15 PM     | 0  | 1      | 0       | 0  | 0  | 0      | 0     | 1  | 0   | 0       | 0       | 0   | 0                   | 0     | 0     | 1  | 3      | 14       |
| 5:30 PM     | 0  | 0      | 0       | 0  | 0  | 2      | 0     | 0  | 0   | 0       | 0       | 0   | 0                   | 0     | 0     | 0  | 2      | 8        |
| 5:45 PM     | 0  | 0      | 0       | 0  | 0  | 0      | 0     | 1  | 0   | 0       | 0       | 0   | 0                   | 3     | 1     | 0  | 5      | 11       |
| Count Total | 0  | 4      | 1       | 1  | 0  | 5      | 0     | 5  | 0   | 0       | 2       | 2   | 0                   | 5     | 4     | 4  | 33     | 0        |
| Peak Hour   | 0  | 1      | 0       | 0  | 0  | 2      | 0     | 2  | 0   | 0       | 0       | 0   | 0                   | 1     | 1     | 1  | 8      | 0        |

| last a moral      | Ric | dgemark  | Dr | F  | airview F | ₹d | Airlin | e Hwy (   | SR-25) | Airlin | e Hwy (S | SR-25) | 45              | D - III             |
|-------------------|-----|----------|----|----|-----------|----|--------|-----------|--------|--------|----------|--------|-----------------|---------------------|
| Interval<br>Start | E   | Eastboun | d  | V  | Vestboun  | ıd | ١      | Northbour | nd     | S      | outhbour | nd     | 15-min<br>Total | Rolling<br>One Hour |
| J.L               | LT  | TH       | RT | LT | TH        | RT | LT     | TH        | RT     | LT     | TH       | RT     | . • • • •       | 0.10 1.10 4.1       |
| 4:00 PM           | 0   | 0        | 0  | 0  | 0         | 0  | 0      | 0         | 0      | 0      | 0        | 0      | 0               | 0                   |
| 4:15 PM           | 0   | 0        | 0  | 0  | 0         | 0  | 0      | 0         | 0      | 0      | 0        | 0      | 0               | 0                   |
| 4:30 PM           | 0   | 0        | 0  | 0  | 0         | 0  | 0      | 0         | 0      | 0      | 0        | 0      | 0               | 0                   |
| 4:45 PM           | 0   | 0        | 0  | 0  | 0         | 0  | 0      | 0         | 0      | 0      | 0        | 0      | 0               | 0                   |
| 5:00 PM           | 0   | 0        | 0  | 0  | 0         | 0  | 0      | 0         | 0      | 0      | 0        | 0      | 0               | 0                   |
| 5:15 PM           | 0   | 0        | 0  | 0  | 0         | 0  | 0      | 0         | 0      | 0      | 0        | 0      | 0               | 0                   |
| 5:30 PM           | 0   | 0        | 0  | 0  | 0         | 0  | 0      | 0         | 0      | 0      | 0        | 0      | 0               | 0                   |
| 5:45 PM           | 0   | 0        | 0  | 0  | 0         | 0  | 0      | 0         | 0      | 0      | 0        | 0      | 0               | 0                   |
| Count Total       | 0   | 0        | 0  | 0  | 0         | 0  | 0      | 0         | 0      | 0      | 0        | 0      | 0               | 0                   |
| Peak Hour         | 0   | 0        | 0  | 0  | 0         | 0  | 0      | 0         | 0      | 0      | 0        | 0      | 0               | 0                   |

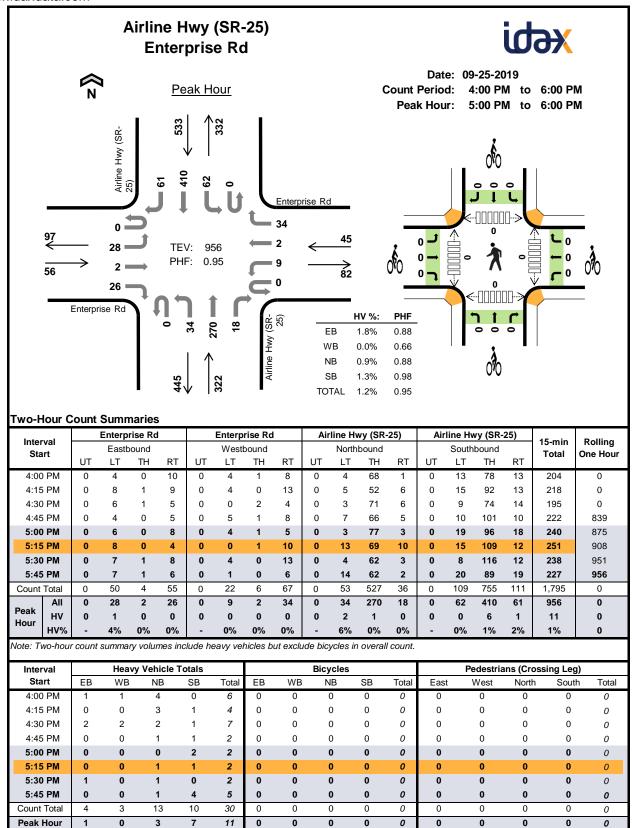
Note: U-Turn volumes for bikes are included in Left-Turn, if any.



| Interval    |    | Enterp | rise Rd |    |    | Enterp | rise Rd |    | Air | line Hv | vy (SR- | 25) | Air | line Hv | vy (SR- | 15-min | Rolling |          |
|-------------|----|--------|---------|----|----|--------|---------|----|-----|---------|---------|-----|-----|---------|---------|--------|---------|----------|
| Start       |    | Eastb  | ound    |    |    | Westl  | bound   |    |     | North   | bound   |     |     | South   | bound   |        | Total   | One Hour |
|             | UT | LT     | TH      | RT | UT | LT     | TH      | RT | UT  | LT      | TH      | RT  | UT  | LT      | TH      | RT     |         | One Hour |
| 7:00 AM     | 0  | 0      | 0       | 1  | 0  | 0      | 0       | 0  | 0   | 0       | 5       | 0   | 0   | 0       | 2       | 0      | 8       | 0        |
| 7:15 AM     | 0  | 0      | 1       | 0  | 0  | 0      | 0       | 0  | 0   | 0       | 0       | 0   | 0   | 1       | 1       | 1      | 4       | 0        |
| 7:30 AM     | 0  | 0      | 0       | 0  | 0  | 0      | 0       | 0  | 0   | 0       | 2       | 1   | 0   | 0       | 4       | 0      | 7       | 0        |
| 7:45 AM     | 0  | 0      | 0       | 1  | 0  | 1      | 0       | 0  | 0   | 0       | 5       | 0   | 0   | 0       | 4       | 0      | 11      | 30       |
| 8:00 AM     | 0  | 0      | 0       | 0  | 0  | 1      | 0       | 0  | 0   | 2       | 4       | 0   | 0   | 0       | 8       | 1      | 16      | 38       |
| 8:15 AM     | 0  | 0      | 1       | 0  | 0  | 0      | 0       | 0  | 0   | 0       | 3       | 0   | 0   | 0       | 3       | 0      | 7       | 41       |
| 8:30 AM     | 0  | 0      | 0       | 0  | 0  | 0      | 0       | 1  | 0   | 1       | 5       | 0   | 0   | 0       | 3       | 0      | 10      | 44       |
| 8:45 AM     | 0  | 0      | 0       | 0  | 0  | 0      | 0       | 0  | 0   | 0       | 1       | 0   | 0   | 0       | 5       | 1      | 7       | 40       |
| Count Total | 0  | 0      | 2       | 2  | 0  | 2      | 0       | 1  | 0   | 3       | 25      | 1   | 0   | 1       | 30      | 3      | 70      | 0        |
| Peak Hour   | 0  | 0      | 1       | 1  | 0  | 2      | 0       | 0  | 0   | 2       | 14      | 1   | 0   | 0       | 19      | 1      | 41      | 0        |

| lutamal.          | En | terprise | Rd | Er | terprise | Rd | Airlin | e Hwy (S  | SR-25) | Airlin | e Hwy (S | SR-25) | 45              | D - III             |
|-------------------|----|----------|----|----|----------|----|--------|-----------|--------|--------|----------|--------|-----------------|---------------------|
| Interval<br>Start | E  | Eastboun | d  | V  | Vestboun | d  | N      | lorthbour | nd     | S      | outhbour | nd     | 15-min<br>Total | Rolling<br>One Hour |
| Otart             | LT | TH       | RT | LT | TH       | RT | LT     | TH        | RT     | LT     | TH       | RT     | rotar           | One riou            |
| 7:00 AM           | 0  | 0        | 0  | 0  | 0        | 0  | 0      | 0         | 0      | 0      | 0        | 0      | 0               | 0                   |
| 7:15 AM           | 0  | 0        | 0  | 0  | 0        | 0  | 0      | 0         | 0      | 0      | 0        | 0      | 0               | 0                   |
| 7:30 AM           | 0  | 0        | 0  | 0  | 0        | 0  | 0      | 0         | 0      | 0      | 0        | 0      | 0               | 0                   |
| 7:45 AM           | 0  | 0        | 0  | 0  | 0        | 0  | 0      | 0         | 0      | 0      | 0        | 0      | 0               | 0                   |
| 8:00 AM           | 0  | 0        | 0  | 0  | 0        | 0  | 0      | 0         | 0      | 0      | 0        | 0      | 0               | 0                   |
| 8:15 AM           | 0  | 0        | 0  | 0  | 0        | 0  | 0      | 0         | 0      | 0      | 0        | 0      | 0               | 0                   |
| 8:30 AM           | 0  | 0        | 0  | 0  | 0        | 0  | 0      | 0         | 0      | 0      | 1        | 0      | 1               | 1                   |
| 8:45 AM           | 0  | 0        | 0  | 0  | 0        | 0  | 0      | 0         | 0      | 0      | 0        | 0      | 0               | 1                   |
| Count Total       | 0  | 0        | 0  | 0  | 0        | 0  | 0      | 0         | 0      | 0      | 1        | 0      | 1               | 0                   |
| Peak Hour         | 0  | 0        | 0  | 0  | 0        | 0  | 0      | 0         | 0      | 0      | 0        | 0      | 0               | 0                   |

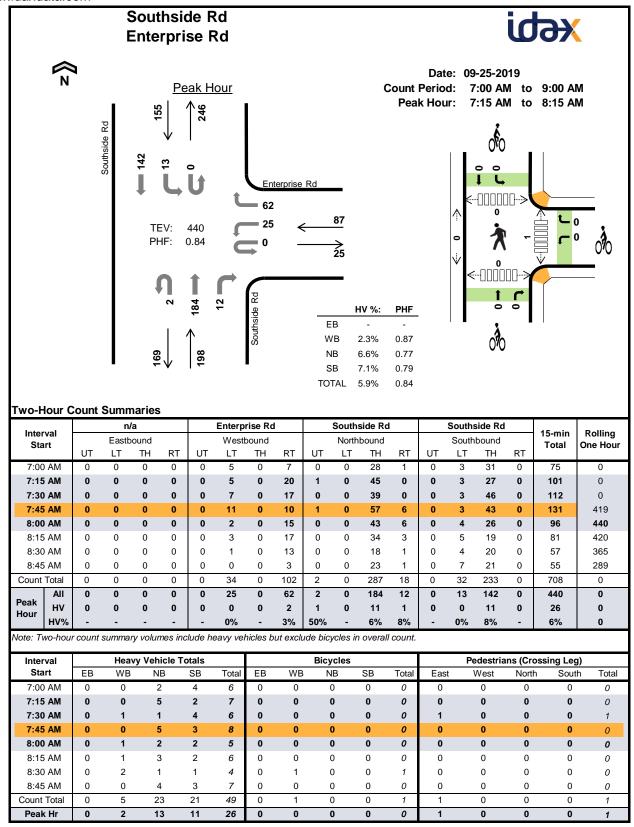
Note: U-Turn volumes for bikes are included in Left-Turn, if any.



| lute med          |    | Enterp | rise Rd |    |    | Enterp | rise Ro | l  | Air | line Hy | vy (SR- | ·25) | Air | line Hv | vy (SR- | 25) | 45              | Dalling             |
|-------------------|----|--------|---------|----|----|--------|---------|----|-----|---------|---------|------|-----|---------|---------|-----|-----------------|---------------------|
| Interval<br>Start |    | Eastb  | ound    |    |    | West   | bound   |    |     | North   | bound   |      |     | South   | bound   |     | 15-min<br>Total | Rolling<br>One Hour |
| Otari             | UT | LT     | TH      | RT | UT | LT     | TH      | RT | UT  | LT      | TH      | RT   | UT  | LT      | TH      | RT  | Total           | One near            |
| 4:00 PM           | 0  | 0      | 0       | 1  | 0  | 1      | 0       | 0  | 0   | 0       | 4       | 0    | 0   | 0       | 0       | 0   | 6               | 0                   |
| 4:15 PM           | 0  | 0      | 0       | 0  | 0  | 0      | 0       | 0  | 0   | 1       | 2       | 0    | 0   | 0       | 1       | 0   | 4               | 0                   |
| 4:30 PM           | 0  | 0      | 0       | 2  | 0  | 0      | 1       | 1  | 0   | 0       | 2       | 0    | 0   | 0       | 1       | 0   | 7               | 0                   |
| 4:45 PM           | 0  | 0      | 0       | 0  | 0  | 0      | 0       | 0  | 0   | 0       | 1       | 0    | 0   | 0       | 1       | 0   | 2               | 19                  |
| 5:00 PM           | 0  | 0      | 0       | 0  | 0  | 0      | 0       | 0  | 0   | 0       | 0       | 0    | 0   | 0       | 2       | 0   | 2               | 15                  |
| 5:15 PM           | 0  | 0      | 0       | 0  | 0  | 0      | 0       | 0  | 0   | 1       | 0       | 0    | 0   | 0       | 0       | 1   | 2               | 13                  |
| 5:30 PM           | 0  | 1      | 0       | 0  | 0  | 0      | 0       | 0  | 0   | 0       | 1       | 0    | 0   | 0       | 0       | 0   | 2               | 8                   |
| 5:45 PM           | 0  | 0      | 0       | 0  | 0  | 0      | 0       | 0  | 0   | 1       | 0       | 0    | 0   | 0       | 4       | 0   | 5               | 11                  |
| Count Total       | 0  | 1      | 0       | 3  | 0  | 1      | 1       | 1  | 0   | 3       | 10      | 0    | 0   | 0       | 9       | 1   | 30              | 0                   |
| Peak Hour         | 0  | 1      | 0       | 0  | 0  | 0      | 0       | 0  | 0   | 2       | 1       | 0    | 0   | 0       | 6       | 1   | 11              | 0                   |

| Interval          | En | terprise | Rd | En | terprise | Rd | Airlin | e Hwy (   | SR-25) | Airlin | e Hwy (S | SR-25) | 45 min          | Dalling             |
|-------------------|----|----------|----|----|----------|----|--------|-----------|--------|--------|----------|--------|-----------------|---------------------|
| Interval<br>Start | E  | Eastboun | d  | v  | Vestboun | ıd | 1      | Northbour | nd     | s      | outhbour | nd     | 15-min<br>Total | Rolling<br>One Hour |
| <b>3.</b>         | LT | TH       | RT | LT | TH       | RT | LT     | TH        | RT     | LT     | TH       | RT     | . • • • •       | 0.10 1.10           |
| 4:00 PM           | 0  | 0        | 0  | 0  | 0        | 0  | 0      | 0         | 0      | 0      | 0        | 0      | 0               | 0                   |
| 4:15 PM           | 0  | 0        | 0  | 0  | 0        | 0  | 0      | 0         | 0      | 0      | 0        | 0      | 0               | 0                   |
| 4:30 PM           | 0  | 0        | 0  | 0  | 0        | 0  | 0      | 0         | 0      | 0      | 0        | 0      | 0               | 0                   |
| 4:45 PM           | 0  | 0        | 0  | 0  | 0        | 0  | 0      | 0         | 0      | 0      | 0        | 0      | 0               | 0                   |
| 5:00 PM           | 0  | 0        | 0  | 0  | 0        | 0  | 0      | 0         | 0      | 0      | 0        | 0      | 0               | 0                   |
| 5:15 PM           | 0  | 0        | 0  | 0  | 0        | 0  | 0      | 0         | 0      | 0      | 0        | 0      | 0               | 0                   |
| 5:30 PM           | 0  | 0        | 0  | 0  | 0        | 0  | 0      | 0         | 0      | 0      | 0        | 0      | 0               | 0                   |
| 5:45 PM           | 0  | 0        | 0  | 0  | 0        | 0  | 0      | 0         | 0      | 0      | 0        | 0      | 0               | 0                   |
| Count Total       | 0  | 0        | 0  | 0  | 0        | 0  | 0      | 0         | 0      | 0      | 0        | 0      | 0               | 0                   |
| Peak Hour         | 0  | 0        | 0  | 0  | 0        | 0  | 0      | 0         | 0      | 0      | 0        | 0      | 0               | 0                   |

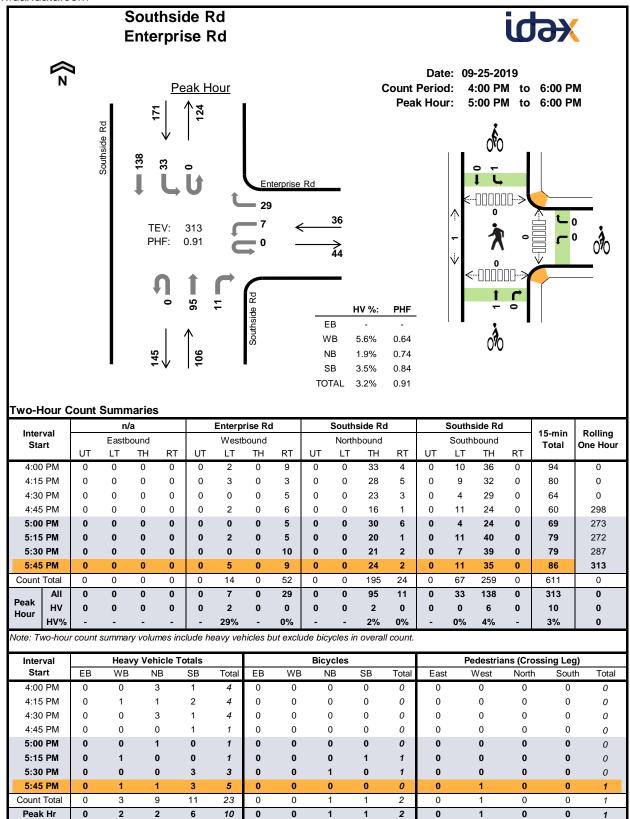
Note: U-Turn volumes for bikes are included in Left-Turn, if any.



| lusta musal       |    | n,    | /a   |    |    | Enterp | rise Ro | i  |    | Souths | side Rd |    |    | Souths | side Rd |    | 45              | Dalling             |
|-------------------|----|-------|------|----|----|--------|---------|----|----|--------|---------|----|----|--------|---------|----|-----------------|---------------------|
| Interval<br>Start |    | Eastb | ound |    |    | Westl  | bound   |    |    | North  | bound   |    |    | South  | bound   |    | 15-min<br>Total | Rolling<br>One Hour |
| Otart             | UT | LT    | TH   | RT | UT | LT     | TH      | RT | UT | LT     | TH      | RT | UT | LT     | TH      | RT | Total           | One near            |
| 7:00 AM           | 0  | 0     | 0    | 0  | 0  | 0      | 0       | 0  | 0  | 0      | 1       | 1  | 0  | 0      | 4       | 0  | 6               | 0                   |
| 7:15 AM           | 0  | 0     | 0    | 0  | 0  | 0      | 0       | 0  | 0  | 0      | 5       | 0  | 0  | 0      | 2       | 0  | 7               | 0                   |
| 7:30 AM           | 0  | 0     | 0    | 0  | 0  | 0      | 0       | 1  | 0  | 0      | 1       | 0  | 0  | 0      | 4       | 0  | 6               | 0                   |
| 7:45 AM           | 0  | 0     | 0    | 0  | 0  | 0      | 0       | 0  | 1  | 0      | 3       | 1  | 0  | 0      | 3       | 0  | 8               | 27                  |
| 8:00 AM           | 0  | 0     | 0    | 0  | 0  | 0      | 0       | 1  | 0  | 0      | 2       | 0  | 0  | 0      | 2       | 0  | 5               | 26                  |
| 8:15 AM           | 0  | 0     | 0    | 0  | 0  | 1      | 0       | 0  | 0  | 0      | 3       | 0  | 0  | 0      | 2       | 0  | 6               | 25                  |
| 8:30 AM           | 0  | 0     | 0    | 0  | 0  | 1      | 0       | 1  | 0  | 0      | 0       | 1  | 0  | 0      | 1       | 0  | 4               | 23                  |
| 8:45 AM           | 0  | 0     | 0    | 0  | 0  | 0      | 0       | 0  | 0  | 0      | 3       | 1  | 0  | 0      | 3       | 0  | 7               | 22                  |
| Count Total       | 0  | 0     | 0    | 0  | 0  | 2      | 0       | 3  | 1  | 0      | 18      | 4  | 0  | 0      | 21      | 0  | 49              | 0                   |
| Peak Hour         | 0  | 0     | 0    | 0  | 0  | 0      | 0       | 2  | 1  | 0      | 11      | 1  | 0  | 0      | 11      | 0  | 26              | 0                   |

| Interval          |    | n/a      |    | Er | terprise | Rd | Sc | uthside   | Rd | So | uthside  | Rd | 45              | Dalling             |
|-------------------|----|----------|----|----|----------|----|----|-----------|----|----|----------|----|-----------------|---------------------|
| Interval<br>Start | E  | Eastboun | d  | V  | Vestboun | ıd | N  | lorthboun | nd | S  | outhbour | nd | 15-min<br>Total | Rolling<br>One Hour |
| J.a. i            | LT | TH       | RT | LT | TH       | RT | LT | TH        | RT | LT | TH       | RT | . • • • •       | 0.10 1.10           |
| 7:00 AM           | 0  | 0        | 0  | 0  | 0        | 0  | 0  | 0         | 0  | 0  | 0        | 0  | 0               | 0                   |
| 7:15 AM           | 0  | 0        | 0  | 0  | 0        | 0  | 0  | 0         | 0  | 0  | 0        | 0  | 0               | 0                   |
| 7:30 AM           | 0  | 0        | 0  | 0  | 0        | 0  | 0  | 0         | 0  | 0  | 0        | 0  | 0               | 0                   |
| 7:45 AM           | 0  | 0        | 0  | 0  | 0        | 0  | 0  | 0         | 0  | 0  | 0        | 0  | 0               | 0                   |
| 8:00 AM           | 0  | 0        | 0  | 0  | 0        | 0  | 0  | 0         | 0  | 0  | 0        | 0  | 0               | 0                   |
| 8:15 AM           | 0  | 0        | 0  | 0  | 0        | 0  | 0  | 0         | 0  | 0  | 0        | 0  | 0               | 0                   |
| 8:30 AM           | 0  | 0        | 0  | 0  | 0        | 1  | 0  | 0         | 0  | 0  | 0        | 0  | 1               | 1                   |
| 8:45 AM           | 0  | 0        | 0  | 0  | 0        | 0  | 0  | 0         | 0  | 0  | 0        | 0  | 0               | 1                   |
| Count Total       | 0  | 0        | 0  | 0  | 0        | 1  | 0  | 0         | 0  | 0  | 0        | 0  | 1               | 0                   |
| Peak Hour         | 0  | 0        | 0  | 0  | 0        | 0  | 0  | 0         | 0  | 0  | 0        | 0  | 0               | 0                   |

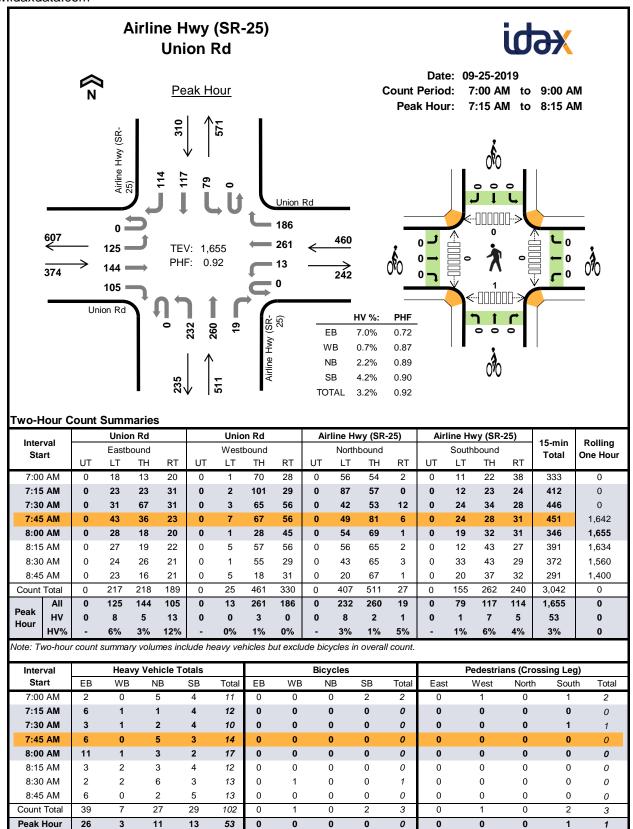
Note: U-Turn volumes for bikes are included in Left-Turn, if any.



| lutemal           |    | n,    | /a   |    |    | Enterp | rise Rd |    |    | Souths | side Rd |    |    | Souths | side Rd |    | 45 :            | Dalling             |
|-------------------|----|-------|------|----|----|--------|---------|----|----|--------|---------|----|----|--------|---------|----|-----------------|---------------------|
| Interval<br>Start |    | Eastb | ound |    |    | Westl  | bound   |    |    | North  | bound   |    |    | South  | bound   |    | 15-min<br>Total | Rolling<br>One Hour |
| Otart             | UT | LT    | TH   | RT | UT | LT     | TH      | RT | UT | LT     | TH      | RT | UT | LT     | TH      | RT | Total           | One near            |
| 4:00 PM           | 0  | 0     | 0    | 0  | 0  | 0      | 0       | 0  | 0  | 0      | 2       | 1  | 0  | 0      | 1       | 0  | 4               | 0                   |
| 4:15 PM           | 0  | 0     | 0    | 0  | 0  | 1      | 0       | 0  | 0  | 0      | 1       | 0  | 0  | 0      | 2       | 0  | 4               | 0                   |
| 4:30 PM           | 0  | 0     | 0    | 0  | 0  | 0      | 0       | 0  | 0  | 0      | 2       | 1  | 0  | 0      | 1       | 0  | 4               | 0                   |
| 4:45 PM           | 0  | 0     | 0    | 0  | 0  | 0      | 0       | 0  | 0  | 0      | 0       | 0  | 0  | 0      | 1       | 0  | 1               | 13                  |
| 5:00 PM           | 0  | 0     | 0    | 0  | 0  | 0      | 0       | 0  | 0  | 0      | 1       | 0  | 0  | 0      | 0       | 0  | 1               | 10                  |
| 5:15 PM           | 0  | 0     | 0    | 0  | 0  | 1      | 0       | 0  | 0  | 0      | 0       | 0  | 0  | 0      | 0       | 0  | 1               | 7                   |
| 5:30 PM           | 0  | 0     | 0    | 0  | 0  | 0      | 0       | 0  | 0  | 0      | 0       | 0  | 0  | 0      | 3       | 0  | 3               | 6                   |
| 5:45 PM           | 0  | 0     | 0    | 0  | 0  | 1      | 0       | 0  | 0  | 0      | 1       | 0  | 0  | 0      | 3       | 0  | 5               | 10                  |
| Count Total       | 0  | 0     | 0    | 0  | 0  | 3      | 0       | 0  | 0  | 0      | 7       | 2  | 0  | 0      | 11      | 0  | 23              | 0                   |
| Peak Hour         | 0  | 0     | 0    | 0  | 0  | 2      | 0       | 0  | 0  | 0      | 2       | 0  | 0  | 0      | 6       | 0  | 10              | 0                   |

| lu (a maal        |     | n/a      |    | Er | terprise | Rd | Sc | outhside  | Rd | Sc | uthside  | Rd | 45              | D - 111             |
|-------------------|-----|----------|----|----|----------|----|----|-----------|----|----|----------|----|-----------------|---------------------|
| Interval<br>Start | - 1 | Eastboun | d  | ٧  | Vestboun | nd | N  | lorthbour | nd | S  | outhbour | nd | 15-min<br>Total | Rolling<br>One Hour |
| <b>-</b>          | LT  | TH       | RT | LT | TH       | RT | LT | TH        | RT | LT | TH       | RT |                 | 0.10 1.10           |
| 4:00 PM           | 0   | 0        | 0  | 0  | 0        | 0  | 0  | 0         | 0  | 0  | 0        | 0  | 0               | 0                   |
| 4:15 PM           | 0   | 0        | 0  | 0  | 0        | 0  | 0  | 0         | 0  | 0  | 0        | 0  | 0               | 0                   |
| 4:30 PM           | 0   | 0        | 0  | 0  | 0        | 0  | 0  | 0         | 0  | 0  | 0        | 0  | 0               | 0                   |
| 4:45 PM           | 0   | 0        | 0  | 0  | 0        | 0  | 0  | 0         | 0  | 0  | 0        | 0  | 0               | 0                   |
| 5:00 PM           | 0   | 0        | 0  | 0  | 0        | 0  | 0  | 0         | 0  | 0  | 0        | 0  | 0               | 0                   |
| 5:15 PM           | 0   | 0        | 0  | 0  | 0        | 0  | 0  | 0         | 0  | 1  | 0        | 0  | 1               | 1                   |
| 5:30 PM           | 0   | 0        | 0  | 0  | 0        | 0  | 0  | 1         | 0  | 0  | 0        | 0  | 1               | 2                   |
| 5:45 PM           | 0   | 0        | 0  | 0  | 0        | 0  | 0  | 0         | 0  | 0  | 0        | 0  | 0               | 2                   |
| Count Total       | 0   | 0        | 0  | 0  | 0        | 0  | 0  | 1         | 0  | 1  | 0        | 0  | 2               | 0                   |
| Peak Hour         | 0   | 0        | 0  | 0  | 0        | 0  | 0  | 1         | 0  | 1  | 0        | 0  | 2               | 0                   |

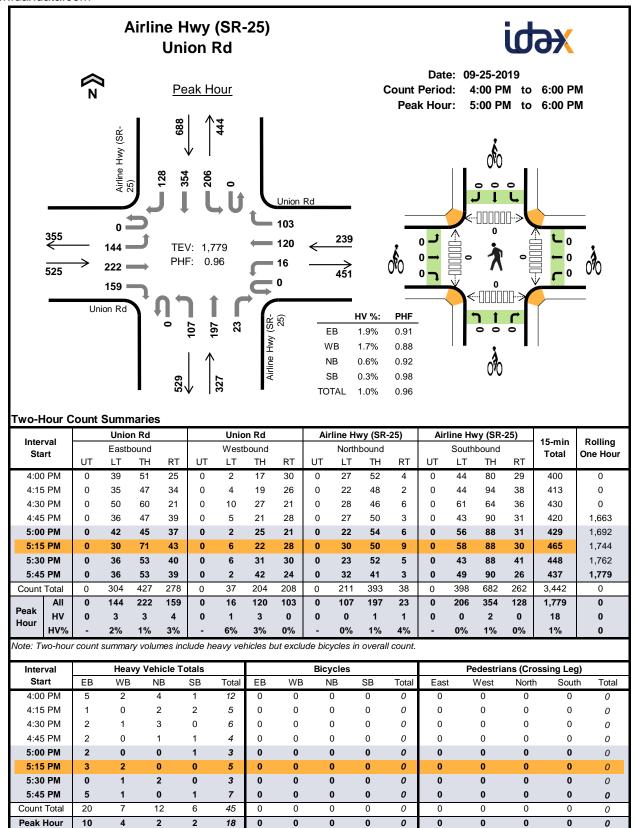
Note: U-Turn volumes for bikes are included in Left-Turn, if any.



| lutamal.          |    | Unio  | n Rd |    |    | Unio | n Rd  |    | Air | line Hv | vy (SR- | 25) | Air | line Hv | y (SR- | 25) | 15-min    | Dallina             |
|-------------------|----|-------|------|----|----|------|-------|----|-----|---------|---------|-----|-----|---------|--------|-----|-----------|---------------------|
| Interval<br>Start |    | Eastb | ound |    |    | West | bound |    |     | North   | bound   |     |     | South   | bound  |     | Total     | Rolling<br>One Hour |
| ••••              | UT | LT    | TH   | RT | UT | LT   | TH    | RT | UT  | LT      | TH      | RT  | UT  | LT      | TH     | RT  | . • • • • | 0.10 1.10           |
| 7:00 AM           | 0  | 0     | 0    | 2  | 0  | 0    | 0     | 0  | 0   | 2       | 3       | 0   | 0   | 0       | 0      | 4   | 11        | 0                   |
| 7:15 AM           | 0  | 3     | 2    | 1  | 0  | 0    | 1     | 0  | 0   | 1       | 0       | 0   | 0   | 1       | 2      | 1   | 12        | 0                   |
| 7:30 AM           | 0  | 1     | 0    | 2  | 0  | 0    | 1     | 0  | 0   | 2       | 0       | 0   | 0   | 0       | 2      | 2   | 10        | 0                   |
| 7:45 AM           | 0  | 2     | 1    | 3  | 0  | 0    | 0     | 0  | 0   | 3       | 1       | 1   | 0   | 0       | 1      | 2   | 14        | 47                  |
| 8:00 AM           | 0  | 2     | 2    | 7  | 0  | 0    | 1     | 0  | 0   | 2       | 1       | 0   | 0   | 0       | 2      | 0   | 17        | 53                  |
| 8:15 AM           | 0  | 1     | 1    | 1  | 0  | 0    | 1     | 1  | 0   | 3       | 0       | 0   | 0   | 1       | 2      | 1   | 12        | 53                  |
| 8:30 AM           | 0  | 1     | 1    | 0  | 0  | 0    | 2     | 0  | 0   | 1       | 5       | 0   | 0   | 0       | 2      | 1   | 13        | 56                  |
| 8:45 AM           | 0  | 1     | 1    | 4  | 0  | 0    | 0     | 0  | 0   | 1       | 1       | 0   | 0   | 0       | 3      | 2   | 13        | 55                  |
| Count Total       | 0  | 11    | 8    | 20 | 0  | 0    | 6     | 1  | 0   | 15      | 11      | 1   | 0   | 2       | 14     | 13  | 102       | 0                   |
| Peak Hour         | 0  | 8     | 5    | 13 | 0  | 0    | 3     | 0  | 0   | 8       | 2       | 1   | 0   | 1       | 7      | 5   | 53        | 0                   |

| last a moral      |    | Union Ro | t  |    | Union Ro | t  | Airlin | e Hwy (S  | SR-25) | Airlin | e Hwy (S | SR-25) | 45              | D - III             |
|-------------------|----|----------|----|----|----------|----|--------|-----------|--------|--------|----------|--------|-----------------|---------------------|
| Interval<br>Start | E  | astbound | d  | V  | Vestboun | ıd | ١      | Northbour | nd     | S      | outhbour | nd     | 15-min<br>Total | Rolling<br>One Hour |
| Otart             | LT | TH       | RT | LT | TH       | RT | LT     | TH        | RT     | LT     | TH       | RT     | - Otal          | One riou            |
| 7:00 AM           | 0  | 0        | 0  | 0  | 0        | 0  | 0      | 0         | 0      | 0      | 0        | 2      | 2               | 0                   |
| 7:15 AM           | 0  | 0        | 0  | 0  | 0        | 0  | 0      | 0         | 0      | 0      | 0        | 0      | 0               | 0                   |
| 7:30 AM           | 0  | 0        | 0  | 0  | 0        | 0  | 0      | 0         | 0      | 0      | 0        | 0      | 0               | 0                   |
| 7:45 AM           | 0  | 0        | 0  | 0  | 0        | 0  | 0      | 0         | 0      | 0      | 0        | 0      | 0               | 2                   |
| 8:00 AM           | 0  | 0        | 0  | 0  | 0        | 0  | 0      | 0         | 0      | 0      | 0        | 0      | 0               | 0                   |
| 8:15 AM           | 0  | 0        | 0  | 0  | 0        | 0  | 0      | 0         | 0      | 0      | 0        | 0      | 0               | 0                   |
| 8:30 AM           | 0  | 0        | 0  | 1  | 0        | 0  | 0      | 0         | 0      | 0      | 0        | 0      | 1               | 1                   |
| 8:45 AM           | 0  | 0        | 0  | 0  | 0        | 0  | 0      | 0         | 0      | 0      | 0        | 0      | 0               | 1                   |
| Count Total       | 0  | 0        | 0  | 1  | 0        | 0  | 0      | 0         | 0      | 0      | 0        | 2      | 3               | 0                   |
| Peak Hour         | 0  | 0        | 0  | 0  | 0        | 0  | 0      | 0         | 0      | 0      | 0        | 0      | 0               | 0                   |

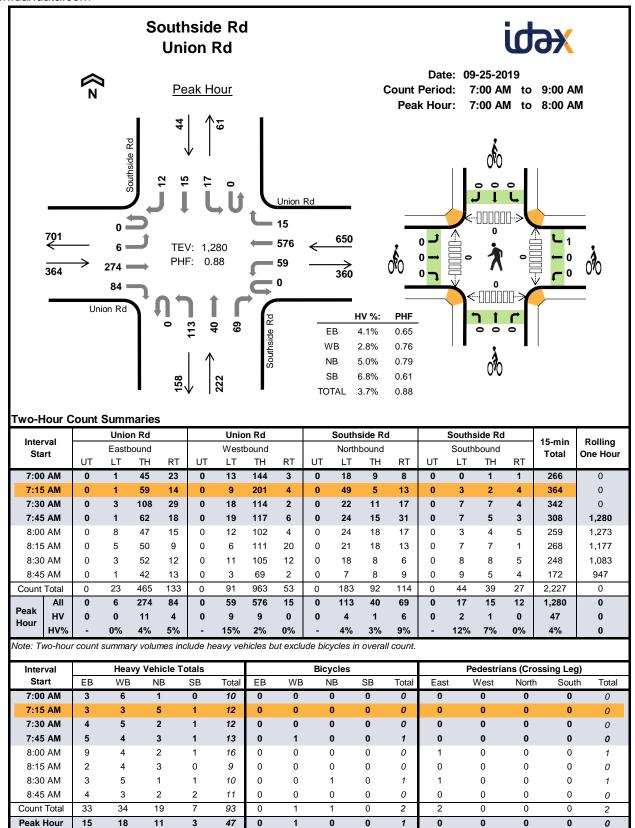
Note: U-Turn volumes for bikes are included in Left-Turn, if any.



| lusta musal       |    | Unio  | n Rd  |    |    | Unio  | n Rd  |    | Air | line Hv | vy (SR- | ·25) | Air | line Hv | vy (SR- | 25) | 15-min    | Dallina             |
|-------------------|----|-------|-------|----|----|-------|-------|----|-----|---------|---------|------|-----|---------|---------|-----|-----------|---------------------|
| Interval<br>Start |    | Eastb | oound |    |    | Westl | bound |    |     | North   | bound   |      |     | South   | bound   |     | Total     | Rolling<br>One Hour |
|                   | UT | LT    | TH    | RT | UT | LT    | TH    | RT | UT  | LT      | TH      | RT   | UT  | LT      | TH      | RT  | . • • • • | 011011041           |
| 4:00 PM           | 0  | 3     | 2     | 0  | 0  | 0     | 1     | 1  | 0   | 2       | 2       | 0    | 0   | 1       | 0       | 0   | 12        | 0                   |
| 4:15 PM           | 0  | 0     | 0     | 1  | 0  | 0     | 0     | 0  | 0   | 2       | 0       | 0    | 0   | 0       | 1       | 1   | 5         | 0                   |
| 4:30 PM           | 0  | 1     | 1     | 0  | 0  | 0     | 0     | 1  | 0   | 1       | 1       | 1    | 0   | 0       | 0       | 0   | 6         | 0                   |
| 4:45 PM           | 0  | 1     | 0     | 1  | 0  | 0     | 0     | 0  | 0   | 0       | 1       | 0    | 0   | 0       | 0       | 1   | 4         | 27                  |
| 5:00 PM           | 0  | 1     | 0     | 1  | 0  | 0     | 0     | 0  | 0   | 0       | 0       | 0    | 0   | 0       | 1       | 0   | 3         | 18                  |
| 5:15 PM           | 0  | 1     | 2     | 0  | 0  | 1     | 1     | 0  | 0   | 0       | 0       | 0    | 0   | 0       | 0       | 0   | 5         | 18                  |
| 5:30 PM           | 0  | 0     | 0     | 0  | 0  | 0     | 1     | 0  | 0   | 0       | 1       | 1    | 0   | 0       | 0       | 0   | 3         | 15                  |
| 5:45 PM           | 0  | 1     | 1     | 3  | 0  | 0     | 1     | 0  | 0   | 0       | 0       | 0    | 0   | 0       | 1       | 0   | 7         | 18                  |
| Count Total       | 0  | 8     | 6     | 6  | 0  | 1     | 4     | 2  | 0   | 5       | 5       | 2    | 0   | 1       | 3       | 2   | 45        | 0                   |
| Peak Hour         | 0  | 3     | 3     | 4  | 0  | 1     | 3     | 0  | 0   | 0       | 1       | 1    | 0   | 0       | 2       | 0   | 18        | 0                   |

|                   |    | Union Ro | i  |    | Union Ro | d  | Airlin | e Hwy (   | SR-25) | Airlin | e Hwy (S | SR-25) | 45 .            | - ···               |
|-------------------|----|----------|----|----|----------|----|--------|-----------|--------|--------|----------|--------|-----------------|---------------------|
| Interval<br>Start |    | Eastboun | d  | \  | Vestboun | ıd | ١      | Northbour | nd     | S      | outhbour | nd     | 15-min<br>Total | Rolling<br>One Hour |
| Otart             | LT | TH       | RT | LT | TH       | RT | LT     | TH        | RT     | LT     | TH       | RT     | rotar           | One riou            |
| 4:00 PM           | 0  | 0        | 0  | 0  | 0        | 0  | 0      | 0         | 0      | 0      | 0        | 0      | 0               | 0                   |
| 4:15 PM           | 0  | 0        | 0  | 0  | 0        | 0  | 0      | 0         | 0      | 0      | 0        | 0      | 0               | 0                   |
| 4:30 PM           | 0  | 0        | 0  | 0  | 0        | 0  | 0      | 0         | 0      | 0      | 0        | 0      | 0               | 0                   |
| 4:45 PM           | 0  | 0        | 0  | 0  | 0        | 0  | 0      | 0         | 0      | 0      | 0        | 0      | 0               | 0                   |
| 5:00 PM           | 0  | 0        | 0  | 0  | 0        | 0  | 0      | 0         | 0      | 0      | 0        | 0      | 0               | 0                   |
| 5:15 PM           | 0  | 0        | 0  | 0  | 0        | 0  | 0      | 0         | 0      | 0      | 0        | 0      | 0               | 0                   |
| 5:30 PM           | 0  | 0        | 0  | 0  | 0        | 0  | 0      | 0         | 0      | 0      | 0        | 0      | 0               | 0                   |
| 5:45 PM           | 0  | 0        | 0  | 0  | 0        | 0  | 0      | 0         | 0      | 0      | 0        | 0      | 0               | 0                   |
| Count Total       | 0  | 0        | 0  | 0  | 0        | 0  | 0      | 0         | 0      | 0      | 0        | 0      | 0               | 0                   |
| Peak Hour         | 0  | 0        | 0  | 0  | 0        | 0  | 0      | 0         | 0      | 0      | 0        | 0      | 0               | 0                   |

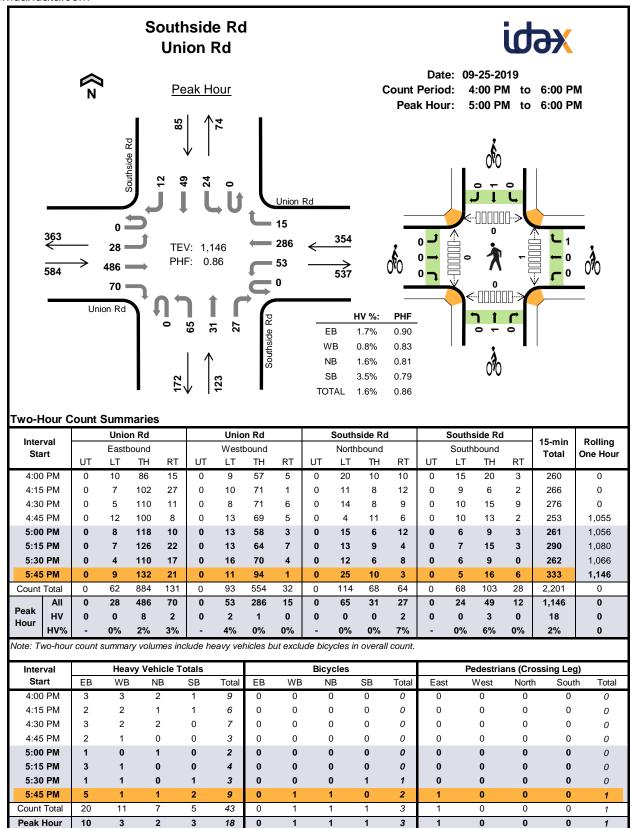
Note: U-Turn volumes for bikes are included in Left-Turn, if any.



| Interval          |    | Unio  | n Rd  |    |    | Unio  | n Rd  |    |    | Souths | side Rd |    |    | Souths | side Rd |    | 45              | Dalling             |
|-------------------|----|-------|-------|----|----|-------|-------|----|----|--------|---------|----|----|--------|---------|----|-----------------|---------------------|
| Interval<br>Start |    | Eastb | oound |    |    | Westl | bound |    |    | North  | bound   |    |    | South  | bound   |    | 15-min<br>Total | Rolling<br>One Hour |
| Otari             | UT | LT    | TH    | RT | UT | LT    | TH    | RT | UT | LT     | TH      | RT | UT | LT     | TH      | RT | rotar           | One riou            |
| 7:00 AM           | 0  | 0     | 2     | 1  | 0  | 4     | 2     | 0  | 0  | 0      | 1       | 0  | 0  | 0      | 0       | 0  | 10              | 0                   |
| 7:15 AM           | 0  | 0     | 3     | 0  | 0  | 2     | 1     | 0  | 0  | 2      | 0       | 3  | 0  | 1      | 0       | 0  | 12              | 0                   |
| 7:30 AM           | 0  | 0     | 2     | 2  | 0  | 2     | 3     | 0  | 0  | 0      | 0       | 2  | 0  | 0      | 1       | 0  | 12              | 0                   |
| 7:45 AM           | 0  | 0     | 4     | 1  | 0  | 1     | 3     | 0  | 0  | 2      | 0       | 1  | 0  | 1      | 0       | 0  | 13              | 47                  |
| 8:00 AM           | 0  | 0     | 8     | 1  | 0  | 1     | 3     | 0  | 0  | 0      | 1       | 1  | 0  | 1      | 0       | 0  | 16              | 53                  |
| 8:15 AM           | 0  | 0     | 2     | 0  | 0  | 1     | 3     | 0  | 0  | 1      | 1       | 1  | 0  | 0      | 0       | 0  | 9               | 50                  |
| 8:30 AM           | 0  | 0     | 2     | 1  | 0  | 0     | 4     | 1  | 0  | 0      | 0       | 1  | 0  | 1      | 0       | 0  | 10              | 48                  |
| 8:45 AM           | 0  | 0     | 3     | 1  | 0  | 1     | 2     | 0  | 0  | 1      | 0       | 1  | 0  | 2      | 0       | 0  | 11              | 46                  |
| Count Total       | 0  | 0     | 26    | 7  | 0  | 12    | 21    | 1  | 0  | 6      | 3       | 10 | 0  | 6      | 1       | 0  | 93              | 0                   |
| Peak Hour         | 0  | 0     | 11    | 4  | 0  | 9     | 9     | 0  | 0  | 4      | 1       | 6  | 0  | 2      | 1       | 0  | 47              | 0                   |

| lasta maral       |    | Union Ro | ł  |    | Union Ro | t  | Sc | uthside   | Rd | Sc | outhside | Rd | 45              | D - III             |
|-------------------|----|----------|----|----|----------|----|----|-----------|----|----|----------|----|-----------------|---------------------|
| Interval<br>Start | ı  | Eastboun | d  | V  | Vestboun | ıd | N  | lorthbour | nd | S  | outhbour | nd | 15-min<br>Total | Rolling<br>One Hour |
| Otart             | LT | TH       | RT | LT | TH       | RT | LT | TH        | RT | LT | TH       | RT | Total           | One riou            |
| 7:00 AM           | 0  | 0        | 0  | 0  | 0        | 0  | 0  | 0         | 0  | 0  | 0        | 0  | 0               | 0                   |
| 7:15 AM           | 0  | 0        | 0  | 0  | 0        | 0  | 0  | 0         | 0  | 0  | 0        | 0  | 0               | 0                   |
| 7:30 AM           | 0  | 0        | 0  | 0  | 0        | 0  | 0  | 0         | 0  | 0  | 0        | 0  | 0               | 0                   |
| 7:45 AM           | 0  | 0        | 0  | 0  | 0        | 1  | 0  | 0         | 0  | 0  | 0        | 0  | 1               | 1                   |
| 8:00 AM           | 0  | 0        | 0  | 0  | 0        | 0  | 0  | 0         | 0  | 0  | 0        | 0  | 0               | 1                   |
| 8:15 AM           | 0  | 0        | 0  | 0  | 0        | 0  | 0  | 0         | 0  | 0  | 0        | 0  | 0               | 1                   |
| 8:30 AM           | 0  | 0        | 0  | 0  | 0        | 0  | 0  | 1         | 0  | 0  | 0        | 0  | 1               | 2                   |
| 8:45 AM           | 0  | 0        | 0  | 0  | 0        | 0  | 0  | 0         | 0  | 0  | 0        | 0  | 0               | 1                   |
| Count Total       | 0  | 0        | 0  | 0  | 0        | 1  | 0  | 1         | 0  | 0  | 0        | 0  | 2               | 0                   |
| Peak Hour         | 0  | 0        | 0  | 0  | 0        | 1  | 0  | 0         | 0  | 0  | 0        | 0  | 1               | 0                   |

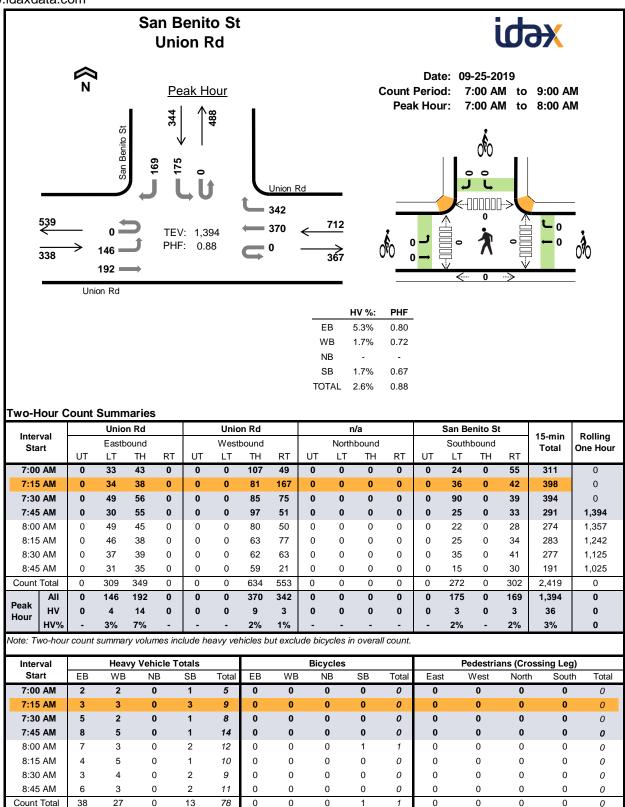
Note: U-Turn volumes for bikes are included in Left-Turn, if any.



| lusta usual       |    | Unio  | n Rd  |    |    | Unio  | n Rd  |    |    | Souths | side Rd |    |    | Souths | side Rd |    | 45              | Dalling             |
|-------------------|----|-------|-------|----|----|-------|-------|----|----|--------|---------|----|----|--------|---------|----|-----------------|---------------------|
| Interval<br>Start |    | Eastb | oound |    |    | Westl | bound |    |    | North  | bound   |    |    | South  | bound   |    | 15-min<br>Total | Rolling<br>One Hour |
| Otart             | UT | LT    | TH    | RT | UT | LT    | TH    | RT | UT | LT     | TH      | RT | UT | LT     | TH      | RT | rotar           | One near            |
| 4:00 PM           | 0  | 0     | 3     | 0  | 0  | 0     | 3     | 0  | 0  | 0      | 0       | 2  | 0  | 0      | 1       | 0  | 9               | 0                   |
| 4:15 PM           | 0  | 0     | 0     | 2  | 0  | 0     | 2     | 0  | 0  | 1      | 0       | 0  | 0  | 1      | 0       | 0  | 6               | 0                   |
| 4:30 PM           | 0  | 0     | 2     | 1  | 0  | 0     | 1     | 1  | 0  | 1      | 0       | 1  | 0  | 0      | 0       | 0  | 7               | 0                   |
| 4:45 PM           | 0  | 1     | 1     | 0  | 0  | 1     | 0     | 0  | 0  | 0      | 0       | 0  | 0  | 0      | 0       | 0  | 3               | 25                  |
| 5:00 PM           | 0  | 0     | 1     | 0  | 0  | 0     | 0     | 0  | 0  | 0      | 0       | 1  | 0  | 0      | 0       | 0  | 2               | 18                  |
| 5:15 PM           | 0  | 0     | 3     | 0  | 0  | 1     | 0     | 0  | 0  | 0      | 0       | 0  | 0  | 0      | 0       | 0  | 4               | 16                  |
| 5:30 PM           | 0  | 0     | 0     | 1  | 0  | 1     | 0     | 0  | 0  | 0      | 0       | 0  | 0  | 0      | 1       | 0  | 3               | 12                  |
| 5:45 PM           | 0  | 0     | 4     | 1  | 0  | 0     | 1     | 0  | 0  | 0      | 0       | 1  | 0  | 0      | 2       | 0  | 9               | 18                  |
| Count Total       | 0  | 1     | 14    | 5  | 0  | 3     | 7     | 1  | 0  | 2      | 0       | 5  | 0  | 1      | 4       | 0  | 43              | 0                   |
| Peak Hour         | 0  | 0     | 8     | 2  | 0  | 2     | 1     | 0  | 0  | 0      | 0       | 2  | 0  | 0      | 3       | 0  | 18              | 0                   |

| lu ta musil       |    | Union Ro | t  |    | Union Ro | l  | Sc | outhside  | Rd | Sc | uthside  | Rd | 45              | D - III             |
|-------------------|----|----------|----|----|----------|----|----|-----------|----|----|----------|----|-----------------|---------------------|
| Interval<br>Start | 1  | Eastboun | d  | V  | Vestboun | d  | N  | lorthbour | nd | S  | outhbour | nd | 15-min<br>Total | Rolling<br>One Hour |
| Otari             | LT | TH       | RT | LT | TH       | RT | LT | TH        | RT | LT | TH       | RT | rotar           | One riou            |
| 4:00 PM           | 0  | 0        | 0  | 0  | 0        | 0  | 0  | 0         | 0  | 0  | 0        | 0  | 0               | 0                   |
| 4:15 PM           | 0  | 0        | 0  | 0  | 0        | 0  | 0  | 0         | 0  | 0  | 0        | 0  | 0               | 0                   |
| 4:30 PM           | 0  | 0        | 0  | 0  | 0        | 0  | 0  | 0         | 0  | 0  | 0        | 0  | 0               | 0                   |
| 4:45 PM           | 0  | 0        | 0  | 0  | 0        | 0  | 0  | 0         | 0  | 0  | 0        | 0  | 0               | 0                   |
| 5:00 PM           | 0  | 0        | 0  | 0  | 0        | 0  | 0  | 0         | 0  | 0  | 0        | 0  | 0               | 0                   |
| 5:15 PM           | 0  | 0        | 0  | 0  | 0        | 0  | 0  | 0         | 0  | 0  | 0        | 0  | 0               | 0                   |
| 5:30 PM           | 0  | 0        | 0  | 0  | 0        | 0  | 0  | 0         | 0  | 0  | 1        | 0  | 1               | 1                   |
| 5:45 PM           | 0  | 0        | 0  | 0  | 0        | 1  | 0  | 1         | 0  | 0  | 0        | 0  | 2               | 3                   |
| Count Total       | 0  | 0        | 0  | 0  | 0        | 1  | 0  | 1         | 0  | 0  | 1        | 0  | 3               | 0                   |
| Peak Hour         | 0  | 0        | 0  | 0  | 0        | 1  | 0  | 1         | 0  | 0  | 1        | 0  | 3               | 0                   |

Note: U-Turn volumes for bikes are included in Left-Turn, if any.



Peak Hr

| Interval    |    | Unio  | n Rd |    |    | Unio  | n Rd  |    |    | n     | /a    |    |    | San Be | nito St |    | 45              | Dalling             |
|-------------|----|-------|------|----|----|-------|-------|----|----|-------|-------|----|----|--------|---------|----|-----------------|---------------------|
| Start       |    | Eastb | ound |    |    | Westl | bound |    |    | North | bound |    |    | South  | bound   |    | 15-min<br>Total | Rolling<br>One Hour |
| Otart       | UT | LT    | TH   | RT | UT | LT    | TH    | RT | UT | LT    | TH    | RT | UT | LT     | TH      | RT | Total           | One riou            |
| 7:00 AM     | 0  | 0     | 2    | 0  | 0  | 0     | 2     | 0  | 0  | 0     | 0     | 0  | 0  | 1      | 0       | 0  | 5               | 0                   |
| 7:15 AM     | 0  | 1     | 2    | 0  | 0  | 0     | 1     | 2  | 0  | 0     | 0     | 0  | 0  | 1      | 0       | 2  | 9               | 0                   |
| 7:30 AM     | 0  | 2     | 3    | 0  | 0  | 0     | 1     | 1  | 0  | 0     | 0     | 0  | 0  | 1      | 0       | 0  | 8               | 0                   |
| 7:45 AM     | 0  | 1     | 7    | 0  | 0  | 0     | 5     | 0  | 0  | 0     | 0     | 0  | 0  | 0      | 0       | 1  | 14              | 36                  |
| 8:00 AM     | 0  | 2     | 5    | 0  | 0  | 0     | 2     | 1  | 0  | 0     | 0     | 0  | 0  | 2      | 0       | 0  | 12              | 43                  |
| 8:15 AM     | 0  | 3     | 1    | 0  | 0  | 0     | 2     | 3  | 0  | 0     | 0     | 0  | 0  | 1      | 0       | 0  | 10              | 44                  |
| 8:30 AM     | 0  | 0     | 3    | 0  | 0  | 0     | 3     | 1  | 0  | 0     | 0     | 0  | 0  | 0      | 0       | 2  | 9               | 45                  |
| 8:45 AM     | 0  | 2     | 4    | 0  | 0  | 0     | 2     | 1  | 0  | 0     | 0     | 0  | 0  | 0      | 0       | 2  | 11              | 42                  |
| Count Total | 0  | 11    | 27   | 0  | 0  | 0     | 18    | 9  | 0  | 0     | 0     | 0  | 0  | 6      | 0       | 7  | 78              | 0                   |
| Peak Hour   | 0  | 4     | 14   | 0  | 0  | 0     | 9     | 3  | 0  | 0     | 0     | 0  | 0  | 3      | 0       | 3  | 36              | 0                   |

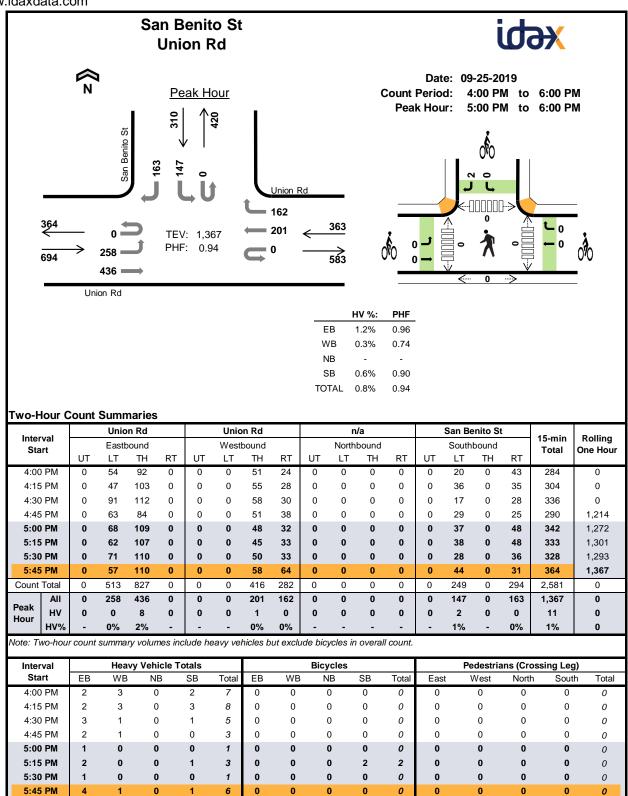
| Interval          |    | Union Ro | t  |    | Union Ro | d  |    | n/a       |    | Sa | n Benito | St | 45              | Dalling             |
|-------------------|----|----------|----|----|----------|----|----|-----------|----|----|----------|----|-----------------|---------------------|
| Interval<br>Start | E  | Eastboun | d  | ٧  | Vestboun | nd | N  | lorthboun | nd | S  | outhbour | nd | 15-min<br>Total | Rolling<br>One Hour |
| O tail t          | LT | TH       | RT | LT | TH       | RT | LT | TH        | RT | LT | TH       | RT | . • • • •       | 0.10 1.10           |
| 7:00 AM           | 0  | 0        | 0  | 0  | 0        | 0  | 0  | 0         | 0  | 0  | 0        | 0  | 0               | 0                   |
| 7:15 AM           | 0  | 0        | 0  | 0  | 0        | 0  | 0  | 0         | 0  | 0  | 0        | 0  | 0               | 0                   |
| 7:30 AM           | 0  | 0        | 0  | 0  | 0        | 0  | 0  | 0         | 0  | 0  | 0        | 0  | 0               | 0                   |
| 7:45 AM           | 0  | 0        | 0  | 0  | 0        | 0  | 0  | 0         | 0  | 0  | 0        | 0  | 0               | 0                   |
| 8:00 AM           | 0  | 0        | 0  | 0  | 0        | 0  | 0  | 0         | 0  | 0  | 0        | 1  | 1               | 1                   |
| 8:15 AM           | 0  | 0        | 0  | 0  | 0        | 0  | 0  | 0         | 0  | 0  | 0        | 0  | 0               | 1                   |
| 8:30 AM           | 0  | 0        | 0  | 0  | 0        | 0  | 0  | 0         | 0  | 0  | 0        | 0  | 0               | 1                   |
| 8:45 AM           | 0  | 0        | 0  | 0  | 0        | 0  | 0  | 0         | 0  | 0  | 0        | 0  | 0               | 1                   |
| Count Total       | 0  | 0        | 0  | 0  | 0        | 0  | 0  | 0         | 0  | 0  | 0        | 1  | 1               | 0                   |
| Peak Hour         | 0  | 0        | 0  | 0  | 0        | 0  | 0  | 0         | 0  | 0  | 0        | 0  | 0               | 0                   |

Note: U-Turn volumes for bikes are included in Left-Turn, if any.

Count Total

Peak Hr

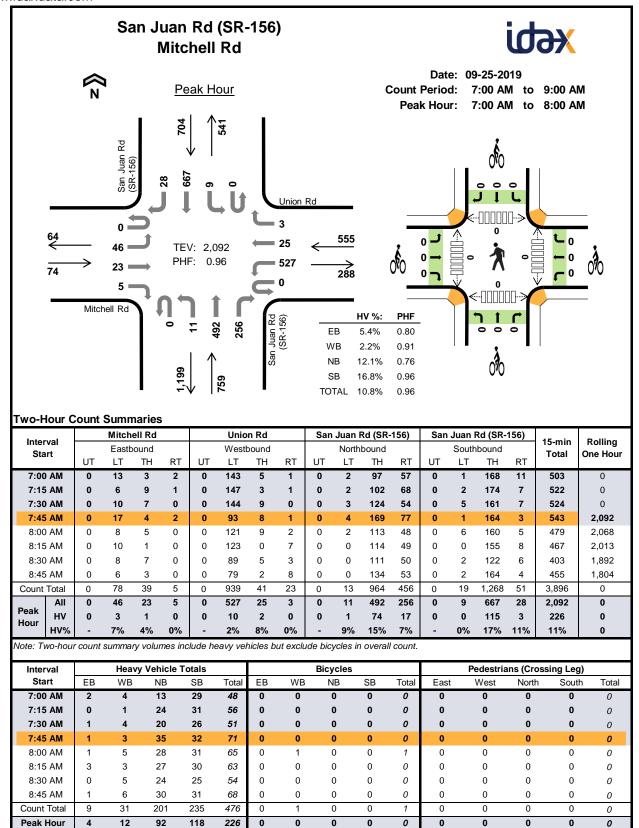
Project Manager: (415) 310-6469



| lusta usual       |    | Unio  | n Rd |    |    | Unio  | n Rd  |    |    | n     | /a    |    |    | San Be | nito St |    | 45              | Dalling             |
|-------------------|----|-------|------|----|----|-------|-------|----|----|-------|-------|----|----|--------|---------|----|-----------------|---------------------|
| Interval<br>Start |    | Eastb | ound |    |    | Westl | bound |    |    | North | bound |    |    | South  | bound   |    | 15-min<br>Total | Rolling<br>One Hour |
| Otart             | UT | LT    | TH   | RT | UT | LT    | TH    | RT | UT | LT    | TH    | RT | UT | LT     | TH      | RT | Total           | One riou            |
| 4:00 PM           | 0  | 0     | 2    | 0  | 0  | 0     | 2     | 1  | 0  | 0     | 0     | 0  | 0  | 1      | 0       | 1  | 7               | 0                   |
| 4:15 PM           | 0  | 2     | 0    | 0  | 0  | 0     | 2     | 1  | 0  | 0     | 0     | 0  | 0  | 2      | 0       | 1  | 8               | 0                   |
| 4:30 PM           | 0  | 0     | 3    | 0  | 0  | 0     | 1     | 0  | 0  | 0     | 0     | 0  | 0  | 0      | 0       | 1  | 5               | 0                   |
| 4:45 PM           | 0  | 0     | 2    | 0  | 0  | 0     | 1     | 0  | 0  | 0     | 0     | 0  | 0  | 0      | 0       | 0  | 3               | 23                  |
| 5:00 PM           | 0  | 0     | 1    | 0  | 0  | 0     | 0     | 0  | 0  | 0     | 0     | 0  | 0  | 0      | 0       | 0  | 1               | 17                  |
| 5:15 PM           | 0  | 0     | 2    | 0  | 0  | 0     | 0     | 0  | 0  | 0     | 0     | 0  | 0  | 1      | 0       | 0  | 3               | 12                  |
| 5:30 PM           | 0  | 0     | 1    | 0  | 0  | 0     | 0     | 0  | 0  | 0     | 0     | 0  | 0  | 0      | 0       | 0  | 1               | 8                   |
| 5:45 PM           | 0  | 0     | 4    | 0  | 0  | 0     | 1     | 0  | 0  | 0     | 0     | 0  | 0  | 1      | 0       | 0  | 6               | 11                  |
| Count Total       | 0  | 2     | 15   | 0  | 0  | 0     | 7     | 2  | 0  | 0     | 0     | 0  | 0  | 5      | 0       | 3  | 34              | 0                   |
| Peak Hour         | 0  | 0     | 8    | 0  | 0  | 0     | 1     | 0  | 0  | 0     | 0     | 0  | 0  | 2      | 0       | 0  | 11              | 0                   |

| Intonial          |     | Union Ro | t  |    | Union Ro | k  |    | n/a       |    | Sa | n Benito | St | 45 main         | Dalling             |
|-------------------|-----|----------|----|----|----------|----|----|-----------|----|----|----------|----|-----------------|---------------------|
| Interval<br>Start | - 1 | Eastboun | d  | ٧  | Vestboun | d  | N  | lorthbour | nd | S  | outhbour | nd | 15-min<br>Total | Rolling<br>One Hour |
| - Clair           | LT  | TH       | RT | LT | TH       | RT | LT | TH        | RT | LT | TH       | RT | . • • • •       | 0.10 1.10           |
| 4:00 PM           | 0   | 0        | 0  | 0  | 0        | 0  | 0  | 0         | 0  | 0  | 0        | 0  | 0               | 0                   |
| 4:15 PM           | 0   | 0        | 0  | 0  | 0        | 0  | 0  | 0         | 0  | 0  | 0        | 0  | 0               | 0                   |
| 4:30 PM           | 0   | 0        | 0  | 0  | 0        | 0  | 0  | 0         | 0  | 0  | 0        | 0  | 0               | 0                   |
| 4:45 PM           | 0   | 0        | 0  | 0  | 0        | 0  | 0  | 0         | 0  | 0  | 0        | 0  | 0               | 0                   |
| 5:00 PM           | 0   | 0        | 0  | 0  | 0        | 0  | 0  | 0         | 0  | 0  | 0        | 0  | 0               | 0                   |
| 5:15 PM           | 0   | 0        | 0  | 0  | 0        | 0  | 0  | 0         | 0  | 0  | 0        | 2  | 2               | 2                   |
| 5:30 PM           | 0   | 0        | 0  | 0  | 0        | 0  | 0  | 0         | 0  | 0  | 0        | 0  | 0               | 2                   |
| 5:45 PM           | 0   | 0        | 0  | 0  | 0        | 0  | 0  | 0         | 0  | 0  | 0        | 0  | 0               | 2                   |
| Count Total       | 0   | 0        | 0  | 0  | 0        | 0  | 0  | 0         | 0  | 0  | 0        | 2  | 2               | 0                   |
| Peak Hour         | 0   | 0        | 0  | 0  | 0        | 0  | 0  | 0         | 0  | 0  | 0        | 2  | 2               | 0                   |

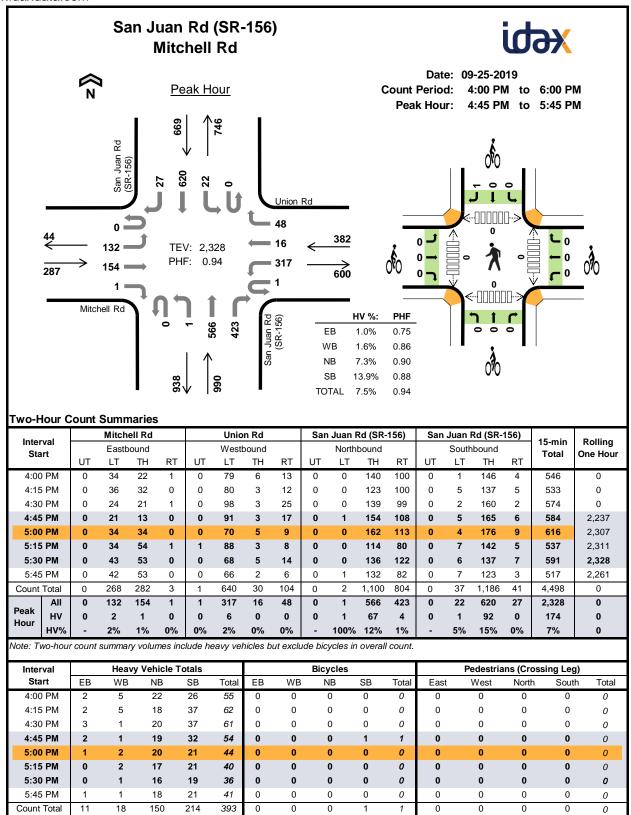
Note: U-Turn volumes for bikes are included in Left-Turn, if any.



|                   |    | Mitch | ell Rd |    |    | Unio  | n Rd  |    | San | Juan I | Rd (SR- | 156) | San | Juan I | Rd (SR- | 156) |                 |                     |
|-------------------|----|-------|--------|----|----|-------|-------|----|-----|--------|---------|------|-----|--------|---------|------|-----------------|---------------------|
| Interval<br>Start |    | Easth | ound   |    |    | Westl | bound |    |     | North  | bound   |      |     | South  | bound   |      | 15-min<br>Total | Rolling<br>One Hour |
| Start             | UT | LT    | TH     | RT | UT | LT    | TH    | RT | UT  | LT     | TH      | RT   | UT  | LT     | TH      | RT   | Total           | One rioui           |
| 7:00 AM           | 0  | 2     | 0      | 0  | 0  | 3     | 1     | 0  | 0   | 0      | 10      | 3    | 0   | 0      | 28      | 1    | 48              | 0                   |
| 7:15 AM           | 0  | 0     | 0      | 0  | 0  | 0     | 1     | 0  | 0   | 1      | 19      | 4    | 0   | 0      | 30      | 1    | 56              | 0                   |
| 7:30 AM           | 0  | 1     | 0      | 0  | 0  | 4     | 0     | 0  | 0   | 0      | 16      | 4    | 0   | 0      | 25      | 1    | 51              | 0                   |
| 7:45 AM           | 0  | 0     | 1      | 0  | 0  | 3     | 0     | 0  | 0   | 0      | 29      | 6    | 0   | 0      | 32      | 0    | 71              | 226                 |
| 8:00 AM           | 0  | 0     | 1      | 0  | 0  | 5     | 0     | 0  | 0   | 1      | 24      | 3    | 0   | 3      | 28      | 0    | 65              | 243                 |
| 8:15 AM           | 0  | 2     | 1      | 0  | 0  | 3     | 0     | 0  | 0   | 0      | 24      | 3    | 0   | 0      | 28      | 2    | 63              | 250                 |
| 8:30 AM           | 0  | 0     | 0      | 0  | 0  | 4     | 1     | 0  | 0   | 0      | 21      | 3    | 0   | 0      | 24      | 1    | 54              | 253                 |
| 8:45 AM           | 0  | 0     | 1      | 0  | 0  | 3     | 1     | 2  | 0   | 0      | 25      | 5    | 0   | 0      | 31      | 0    | 68              | 250                 |
| Count Total       | 0  | 5     | 4      | 0  | 0  | 25    | 4     | 2  | 0   | 2      | 168     | 31   | 0   | 3      | 226     | 6    | 476             | 0                   |
| Peak Hour         | 0  | 3     | 1      | 0  | 0  | 10    | 2     | 0  | 0   | 1      | 74      | 17   | 0   | 0      | 115     | 3    | 226             | 0                   |

| Interval    | N  | litchell R | ld |    | Union Ro | t  | San Ju | uan Rd (S | SR-156) | San Ju | ıan Rd (S | R-156) | 15-min | Rolling    |
|-------------|----|------------|----|----|----------|----|--------|-----------|---------|--------|-----------|--------|--------|------------|
| Start       | E  | Eastboun   | d  | v  | Vestboun | ıd | ١      | Northbour | nd      | s      | outhbour  | nd     | Total  | One Hour   |
| O.L         | LT | TH         | RT | LT | TH       | RT | LT     | TH        | RT      | LT     | TH        | RT     |        | Cilo Iloui |
| 7:00 AM     | 0  | 0          | 0  | 0  | 0        | 0  | 0      | 0         | 0       | 0      | 0         | 0      | 0      | 0          |
| 7:15 AM     | 0  | 0          | 0  | 0  | 0        | 0  | 0      | 0         | 0       | 0      | 0         | 0      | 0      | 0          |
| 7:30 AM     | 0  | 0          | 0  | 0  | 0        | 0  | 0      | 0         | 0       | 0      | 0         | 0      | 0      | 0          |
| 7:45 AM     | 0  | 0          | 0  | 0  | 0        | 0  | 0      | 0         | 0       | 0      | 0         | 0      | 0      | 0          |
| 8:00 AM     | 0  | 0          | 0  | 0  | 1        | 0  | 0      | 0         | 0       | 0      | 0         | 0      | 1      | 1          |
| 8:15 AM     | 0  | 0          | 0  | 0  | 0        | 0  | 0      | 0         | 0       | 0      | 0         | 0      | 0      | 1          |
| 8:30 AM     | 0  | 0          | 0  | 0  | 0        | 0  | 0      | 0         | 0       | 0      | 0         | 0      | 0      | 1          |
| 8:45 AM     | 0  | 0          | 0  | 0  | 0        | 0  | 0      | 0         | 0       | 0      | 0         | 0      | 0      | 1          |
| Count Total | 0  | 0          | 0  | 0  | 1        | 0  | 0      | 0         | 0       | 0      | 0         | 0      | 1      | 0          |
| Peak Hour   | 0  | 0          | 0  | 0  | 0        | 0  | 0      | 0         | 0       | 0      | 0         | 0      | 0      | 0          |

Note: U-Turn volumes for bikes are included in Left-Turn, if any.

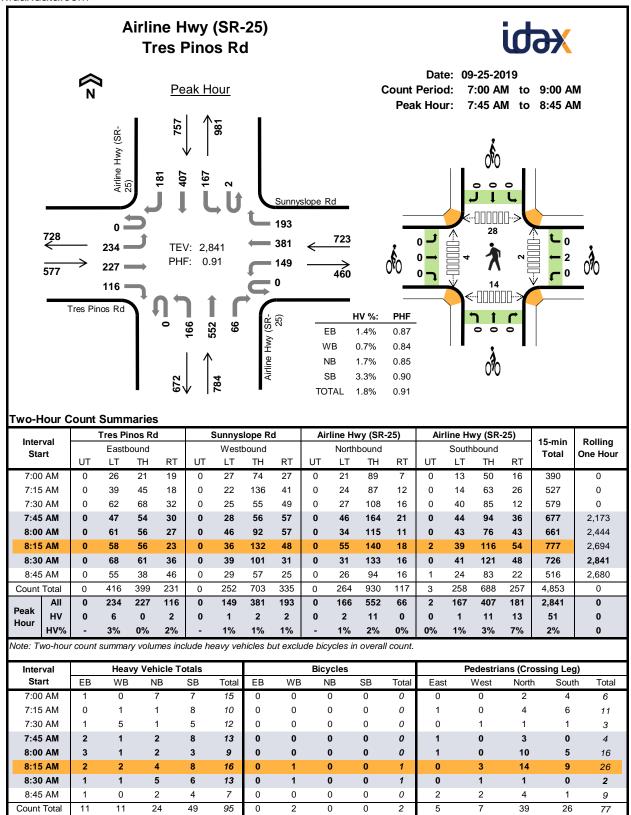


**Peak Hour** 

| lusta musal       |    | Mitch | ell Rd |    |    | Unio | n Rd  |    | San | Juan F | Rd (SR- | 156) | San | Juan F | Rd (SR- | 156) | 15-min    | Dallina             |
|-------------------|----|-------|--------|----|----|------|-------|----|-----|--------|---------|------|-----|--------|---------|------|-----------|---------------------|
| Interval<br>Start |    | Eastb | ound   |    |    | West | bound |    |     | North  | bound   |      |     | South  | bound   |      | Total     | Rolling<br>One Hour |
|                   | UT | LT    | TH     | RT | UT | LT   | TH    | RT | UT  | LT     | TH      | RT   | UT  | LT     | TH      | RT   | . • • • • | 0.10 1.10 4.1       |
| 4:00 PM           | 0  | 1     | 0      | 1  | 0  | 2    | 0     | 3  | 0   | 0      | 21      | 1    | 0   | 0      | 25      | 1    | 55        | 0                   |
| 4:15 PM           | 0  | 2     | 0      | 0  | 0  | 4    | 0     | 1  | 0   | 0      | 16      | 2    | 0   | 0      | 36      | 1    | 62        | 0                   |
| 4:30 PM           | 0  | 2     | 1      | 0  | 0  | 1    | 0     | 0  | 0   | 0      | 18      | 2    | 0   | 0      | 37      | 0    | 61        | 0                   |
| 4:45 PM           | 0  | 1     | 1      | 0  | 0  | 1    | 0     | 0  | 0   | 1      | 17      | 1    | 0   | 0      | 32      | 0    | 54        | 232                 |
| 5:00 PM           | 0  | 1     | 0      | 0  | 0  | 2    | 0     | 0  | 0   | 0      | 20      | 0    | 0   | 0      | 21      | 0    | 44        | 221                 |
| 5:15 PM           | 0  | 0     | 0      | 0  | 0  | 2    | 0     | 0  | 0   | 0      | 15      | 2    | 0   | 0      | 21      | 0    | 40        | 199                 |
| 5:30 PM           | 0  | 0     | 0      | 0  | 0  | 1    | 0     | 0  | 0   | 0      | 15      | 1    | 0   | 1      | 18      | 0    | 36        | 174                 |
| 5:45 PM           | 0  | 0     | 1      | 0  | 0  | 1    | 0     | 0  | 0   | 0      | 16      | 2    | 0   | 0      | 21      | 0    | 41        | 161                 |
| Count Total       | 0  | 7     | 3      | 1  | 0  | 14   | 0     | 4  | 0   | 1      | 138     | 11   | 0   | 1      | 211     | 2    | 393       | 0                   |
| Peak Hour         | 0  | 2     | 1      | 0  | 0  | 6    | 0     | 0  | 0   | 1      | 67      | 4    | 0   | 1      | 92      | 0    | 174       | 0                   |

| I( I              | N  | litchell R | ld |    | Union Ro | l  | San Ju | ıan Rd (S | SR-156) | San Ju | ıan Rd (S | R-156) | 45!             | D - III             |
|-------------------|----|------------|----|----|----------|----|--------|-----------|---------|--------|-----------|--------|-----------------|---------------------|
| Interval<br>Start | E  | Eastboun   | d  | V  | Vestboun | d  | ١      | lorthbour | nd      | S      | outhbour  | nd     | 15-min<br>Total | Rolling<br>One Hour |
| Otart             | LT | TH         | RT | LT | TH       | RT | LT     | TH        | RT      | LT     | TH        | RT     | Total           | One riou            |
| 4:00 PM           | 0  | 0          | 0  | 0  | 0        | 0  | 0      | 0         | 0       | 0      | 0         | 0      | 0               | 0                   |
| 4:15 PM           | 0  | 0          | 0  | 0  | 0        | 0  | 0      | 0         | 0       | 0      | 0         | 0      | 0               | 0                   |
| 4:30 PM           | 0  | 0          | 0  | 0  | 0        | 0  | 0      | 0         | 0       | 0      | 0         | 0      | 0               | 0                   |
| 4:45 PM           | 0  | 0          | 0  | 0  | 0        | 0  | 0      | 0         | 0       | 0      | 0         | 1      | 1               | 1                   |
| 5:00 PM           | 0  | 0          | 0  | 0  | 0        | 0  | 0      | 0         | 0       | 0      | 0         | 0      | 0               | 1                   |
| 5:15 PM           | 0  | 0          | 0  | 0  | 0        | 0  | 0      | 0         | 0       | 0      | 0         | 0      | 0               | 1                   |
| 5:30 PM           | 0  | 0          | 0  | 0  | 0        | 0  | 0      | 0         | 0       | 0      | 0         | 0      | 0               | 1                   |
| 5:45 PM           | 0  | 0          | 0  | 0  | 0        | 0  | 0      | 0         | 0       | 0      | 0         | 0      | 0               | 0                   |
| Count Total       | 0  | 0          | 0  | 0  | 0        | 0  | 0      | 0         | 0       | 0      | 0         | 1      | 1               | 0                   |
| Peak Hour         | 0  | 0          | 0  | 0  | 0        | 0  | 0      | 0         | 0       | 0      | 0         | 1      | 1               | 0                   |

Note: U-Turn volumes for bikes are included in Left-Turn, if any.

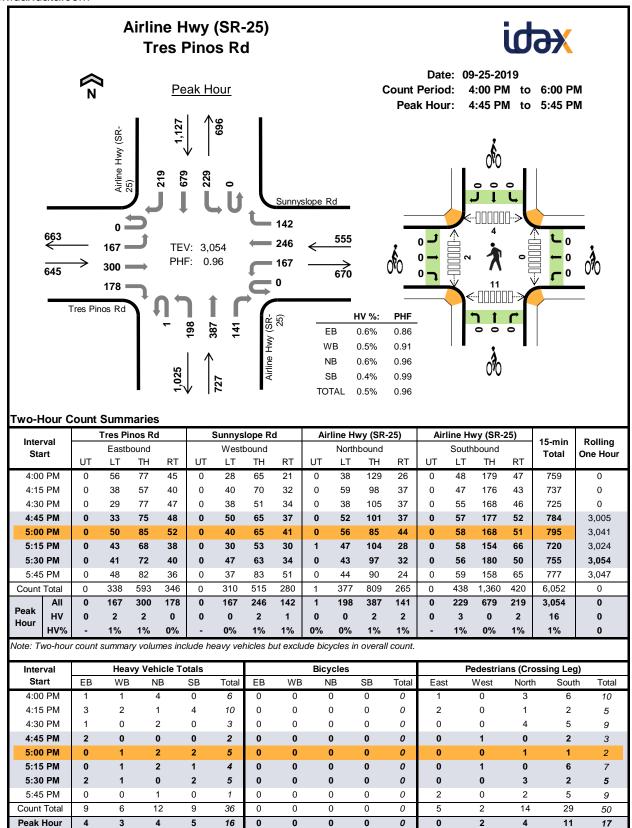


**Peak Hour** 

| Interval    |    | Tres Pi | nos Rd |    | 5  | Sunnys | lope R | d  | Air | line Hv | vy (SR- | 25) | Air | line Hv | vy (SR- | 25) | 15-min    | Rolling   |
|-------------|----|---------|--------|----|----|--------|--------|----|-----|---------|---------|-----|-----|---------|---------|-----|-----------|-----------|
| Start       |    | Eastb   | ound   |    |    | Westl  | bound  |    |     | North   | bound   |     |     | South   | bound   |     | Total     | One Hour  |
| ••••        | UT | LT      | TH     | RT | UT | LT     | TH     | RT | UT  | LT      | TH      | RT  | UT  | LT      | TH      | RT  | . • • • • | 0.10 1.10 |
| 7:00 AM     | 0  | 1       | 0      | 0  | 0  | 0      | 0      | 0  | 0   | 1       | 5       | 1   | 0   | 0       | 6       | 1   | 15        | 0         |
| 7:15 AM     | 0  | 0       | 0      | 0  | 0  | 0      | 1      | 0  | 0   | 0       | 1       | 0   | 0   | 1       | 4       | 3   | 10        | 0         |
| 7:30 AM     | 0  | 0       | 0      | 1  | 0  | 1      | 3      | 1  | 0   | 0       | 1       | 0   | 0   | 0       | 2       | 3   | 12        | 0         |
| 7:45 AM     | 0  | 1       | 0      | 1  | 0  | 0      | 1      | 0  | 0   | 0       | 2       | 0   | 0   | 0       | 5       | 3   | 13        | 50        |
| 8:00 AM     | 0  | 3       | 0      | 0  | 0  | 0      | 0      | 1  | 0   | 0       | 2       | 0   | 0   | 0       | 1       | 2   | 9         | 44        |
| 8:15 AM     | 0  | 1       | 0      | 1  | 0  | 0      | 1      | 1  | 0   | 1       | 3       | 0   | 0   | 0       | 4       | 4   | 16        | 50        |
| 8:30 AM     | 0  | 1       | 0      | 0  | 0  | 1      | 0      | 0  | 0   | 1       | 4       | 0   | 0   | 1       | 1       | 4   | 13        | 51        |
| 8:45 AM     | 0  | 0       | 1      | 0  | 0  | 0      | 0      | 0  | 0   | 0       | 2       | 0   | 0   | 0       | 3       | 1   | 7         | 45        |
| Count Total | 0  | 7       | 1      | 3  | 0  | 2      | 6      | 3  | 0   | 3       | 20      | 1   | 0   | 2       | 26      | 21  | 95        | 0         |
| Peak Hour   | 0  | 6       | 0      | 2  | 0  | 1      | 2      | 2  | 0   | 2       | 11      | 0   | 0   | 1       | 11      | 13  | 51        | 0         |

| last a moral      | Tre | es Pinos | Rd | Sui | nnyslope | Rd | Airlin | e Hwy (   | SR-25) | Airlin | e Hwy (S | SR-25) | 45              | D - III             |
|-------------------|-----|----------|----|-----|----------|----|--------|-----------|--------|--------|----------|--------|-----------------|---------------------|
| Interval<br>Start | E   | Eastboun | d  | V   | Vestboun | ıd | 1      | Northbour | nd     | S      | outhbour | nd     | 15-min<br>Total | Rolling<br>One Hour |
| Otare             | LT  | TH       | RT | LT  | TH       | RT | LT     | TH        | RT     | LT     | TH       | RT     | - Otal          | One riou            |
| 7:00 AM           | 0   | 0        | 0  | 0   | 0        | 0  | 0      | 0         | 0      | 0      | 0        | 0      | 0               | 0                   |
| 7:15 AM           | 0   | 0        | 0  | 0   | 0        | 0  | 0      | 0         | 0      | 0      | 0        | 0      | 0               | 0                   |
| 7:30 AM           | 0   | 0        | 0  | 0   | 0        | 0  | 0      | 0         | 0      | 0      | 0        | 0      | 0               | 0                   |
| 7:45 AM           | 0   | 0        | 0  | 0   | 0        | 0  | 0      | 0         | 0      | 0      | 0        | 0      | 0               | 0                   |
| 8:00 AM           | 0   | 0        | 0  | 0   | 0        | 0  | 0      | 0         | 0      | 0      | 0        | 0      | 0               | 0                   |
| 8:15 AM           | 0   | 0        | 0  | 0   | 1        | 0  | 0      | 0         | 0      | 0      | 0        | 0      | 1               | 1                   |
| 8:30 AM           | 0   | 0        | 0  | 0   | 1        | 0  | 0      | 0         | 0      | 0      | 0        | 0      | 1               | 2                   |
| 8:45 AM           | 0   | 0        | 0  | 0   | 0        | 0  | 0      | 0         | 0      | 0      | 0        | 0      | 0               | 2                   |
| Count Total       | 0   | 0        | 0  | 0   | 2        | 0  | 0      | 0         | 0      | 0      | 0        | 0      | 2               | 0                   |
| Peak Hour         | 0   | 0        | 0  | 0   | 2        | 0  | 0      | 0         | 0      | 0      | 0        | 0      | 2               | 0                   |

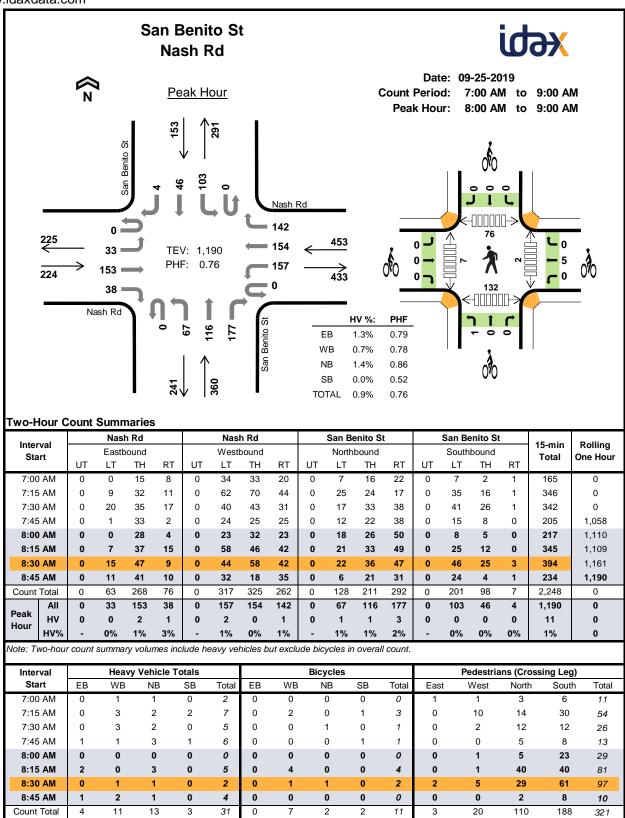
Note: U-Turn volumes for bikes are included in Left-Turn, if any.



| Interval                                | ,  | Tres Pi | nos Rd |    | 5  | Sunnys | lope R | d  | Air | line Hv | vy (SR- | 25) | Air | line Hv | vy (SR- | 25) | 15-min    | Rolling    |
|---|----|---------|--------|----|----|--------|--------|----|-----|---------|---------|-----|-----|---------|---------|-----|-----------|------------|
| Start                                   |    | Eastb   | ound   |    |    | Westl  | bound  |    |     | North   | bound   |     |     | South   | bound   |     | Total     | One Hour   |
| • | UT | LT      | TH     | RT | UT | LT     | TH     | RT | UT  | LT      | TH      | RT  | UT  | LT      | TH      | RT  | . • • • • | 0.10 1.00. |
| 4:00 PM                                 | 0  | 0       | 0      | 1  | 0  | 0      | 1      | 0  | 0   | 0       | 3       | 1   | 0   | 0       | 0       | 0   | 6         | 0          |
| 4:15 PM                                 | 0  | 2       | 1      | 0  | 0  | 0      | 2      | 0  | 0   | 0       | 1       | 0   | 0   | 0       | 4       | 0   | 10        | 0          |
| 4:30 PM                                 | 0  | 1       | 0      | 0  | 0  | 0      | 0      | 0  | 0   | 0       | 1       | 1   | 0   | 0       | 0       | 0   | 3         | 0          |
| 4:45 PM                                 | 0  | 1       | 1      | 0  | 0  | 0      | 0      | 0  | 0   | 0       | 0       | 0   | 0   | 0       | 0       | 0   | 2         | 21         |
| 5:00 PM                                 | 0  | 0       | 0      | 0  | 0  | 0      | 1      | 0  | 0   | 0       | 2       | 0   | 0   | 1       | 0       | 1   | 5         | 20         |
| 5:15 PM                                 | 0  | 0       | 0      | 0  | 0  | 0      | 1      | 0  | 0   | 0       | 0       | 2   | 0   | 0       | 0       | 1   | 4         | 14         |
| 5:30 PM                                 | 0  | 1       | 1      | 0  | 0  | 0      | 0      | 1  | 0   | 0       | 0       | 0   | 0   | 2       | 0       | 0   | 5         | 16         |
| 5:45 PM                                 | 0  | 0       | 0      | 0  | 0  | 0      | 0      | 0  | 0   | 0       | 1       | 0   | 0   | 0       | 0       | 0   | 1         | 15         |
| Count Total                             | 0  | 5       | 3      | 1  | 0  | 0      | 5      | 1  | 0   | 0       | 8       | 4   | 0   | 3       | 4       | 2   | 36        | 0          |
| Peak Hour                               | 0  | 2       | 2      | 0  | 0  | 0      | 2      | 1  | 0   | 0       | 2       | 2   | 0   | 3       | 0       | 2   | 16        | 0          |

| last a moral      | Tre | es Pinos | Rd | Sui | nnyslope | Rd | Airlin | e Hwy (   | SR-25) | Airlin | e Hwy (S | R-25) | 45              | D. III.             |
|-------------------|-----|----------|----|-----|----------|----|--------|-----------|--------|--------|----------|-------|-----------------|---------------------|
| Interval<br>Start | E   | astboun  | d  | V   | Vestboun | ıd | 1      | Northbour | nd     | S      | outhbour | nd    | 15-min<br>Total | Rolling<br>One Hour |
| J.L               | LT  | TH       | RT | LT  | TH       | RT | LT     | TH        | RT     | LT     | TH       | RT    |                 | 0.10 1.10 4.1       |
| 4:00 PM           | 0   | 0        | 0  | 0   | 0        | 0  | 0      | 0         | 0      | 0      | 0        | 0     | 0               | 0                   |
| 4:15 PM           | 0   | 0        | 0  | 0   | 0        | 0  | 0      | 0         | 0      | 0      | 0        | 0     | 0               | 0                   |
| 4:30 PM           | 0   | 0        | 0  | 0   | 0        | 0  | 0      | 0         | 0      | 0      | 0        | 0     | 0               | 0                   |
| 4:45 PM           | 0   | 0        | 0  | 0   | 0        | 0  | 0      | 0         | 0      | 0      | 0        | 0     | 0               | 0                   |
| 5:00 PM           | 0   | 0        | 0  | 0   | 0        | 0  | 0      | 0         | 0      | 0      | 0        | 0     | 0               | 0                   |
| 5:15 PM           | 0   | 0        | 0  | 0   | 0        | 0  | 0      | 0         | 0      | 0      | 0        | 0     | 0               | 0                   |
| 5:30 PM           | 0   | 0        | 0  | 0   | 0        | 0  | 0      | 0         | 0      | 0      | 0        | 0     | 0               | 0                   |
| 5:45 PM           | 0   | 0        | 0  | 0   | 0        | 0  | 0      | 0         | 0      | 0      | 0        | 0     | 0               | 0                   |
| Count Total       | 0   | 0        | 0  | 0   | 0        | 0  | 0      | 0         | 0      | 0      | 0        | 0     | 0               | 0                   |
| Peak Hour         | 0   | 0        | 0  | 0   | 0        | 0  | 0      | 0         | 0      | 0      | 0        | 0     | 0               | 0                   |

Note: U-Turn volumes for bikes are included in Left-Turn, if any.

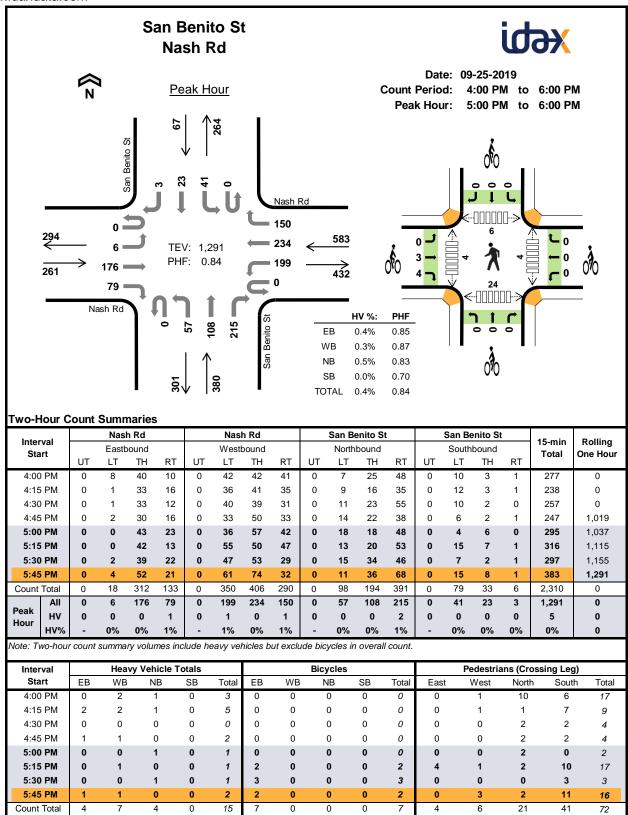


Peak Hour

| Interval    |    | Nas   | h Rd  |    |    | Nas   | h Rd  |    |    | San Be | enito St | t  |    | San Be | enito St |    | 15-min    | Rolling   |
|-------------|----|-------|-------|----|----|-------|-------|----|----|--------|----------|----|----|--------|----------|----|-----------|-----------|
| Start       |    | Eastb | oound |    |    | Westl | bound |    |    | North  | bound    |    |    | South  | bound    |    | Total     | One Hour  |
|             | UT | LT    | TH    | RT | UT | LT    | TH    | RT | UT | LT     | TH       | RT | UT | LT     | TH       | RT | . • • • • | 0.10 1.10 |
| 7:00 AM     | 0  | 0     | 0     | 0  | 0  | 0     | 0     | 1  | 0  | 0      | 1        | 0  | 0  | 0      | 0        | 0  | 2         | 0         |
| 7:15 AM     | 0  | 0     | 0     | 0  | 0  | 3     | 0     | 0  | 0  | 0      | 1        | 1  | 0  | 0      | 1        | 1  | 7         | 0         |
| 7:30 AM     | 0  | 0     | 0     | 0  | 0  | 0     | 2     | 1  | 0  | 0      | 1        | 1  | 0  | 0      | 0        | 0  | 5         | 0         |
| 7:45 AM     | 0  | 0     | 1     | 0  | 0  | 1     | 0     | 0  | 0  | 0      | 1        | 2  | 0  | 1      | 0        | 0  | 6         | 20        |
| 8:00 AM     | 0  | 0     | 0     | 0  | 0  | 0     | 0     | 0  | 0  | 0      | 0        | 0  | 0  | 0      | 0        | 0  | 0         | 18        |
| 8:15 AM     | 0  | 0     | 2     | 0  | 0  | 0     | 0     | 0  | 0  | 0      | 1        | 2  | 0  | 0      | 0        | 0  | 5         | 16        |
| 8:30 AM     | 0  | 0     | 0     | 0  | 0  | 0     | 0     | 1  | 0  | 0      | 0        | 1  | 0  | 0      | 0        | 0  | 2         | 13        |
| 8:45 AM     | 0  | 0     | 0     | 1  | 0  | 2     | 0     | 0  | 0  | 1      | 0        | 0  | 0  | 0      | 0        | 0  | 4         | 11        |
| Count Total | 0  | 0     | 3     | 1  | 0  | 6     | 2     | 3  | 0  | 1      | 5        | 7  | 0  | 1      | 1        | 1  | 31        | 0         |
| Peak Hour   | 0  | 0     | 2     | 1  | 0  | 2     | 0     | 1  | 0  | 1      | 1        | 3  | 0  | 0      | 0        | 0  | 11        | 0         |

|                   |    | Nash Rd  | l  |    | Nash Rd  | ı  | Sa | ın Benito | St | Sa | n Benito | St | 4               |                     |
|-------------------|----|----------|----|----|----------|----|----|-----------|----|----|----------|----|-----------------|---------------------|
| Interval<br>Start | I  | Eastboun | d  | ١  | Westboun | nd | ١  | lorthbour | nd | S  | outhbour | nd | 15-min<br>Total | Rolling<br>One Hour |
| Otart             | LT | TH       | RT | LT | TH       | RT | LT | TH        | RT | LT | TH       | RT | Total           | One nou             |
| 7:00 AM           | 0  | 0        | 0  | 0  | 0        | 0  | 0  | 0         | 0  | 0  | 0        | 0  | 0               | 0                   |
| 7:15 AM           | 0  | 0        | 0  | 0  | 2        | 0  | 0  | 0         | 0  | 0  | 1        | 0  | 3               | 0                   |
| 7:30 AM           | 0  | 0        | 0  | 0  | 0        | 0  | 0  | 0         | 1  | 0  | 0        | 0  | 1               | 0                   |
| 7:45 AM           | 0  | 0        | 0  | 0  | 0        | 0  | 0  | 0         | 0  | 0  | 0        | 1  | 1               | 5                   |
| 8:00 AM           | 0  | 0        | 0  | 0  | 0        | 0  | 0  | 0         | 0  | 0  | 0        | 0  | 0               | 5                   |
| 8:15 AM           | 0  | 0        | 0  | 0  | 4        | 0  | 0  | 0         | 0  | 0  | 0        | 0  | 4               | 6                   |
| 8:30 AM           | 0  | 0        | 0  | 0  | 1        | 0  | 1  | 0         | 0  | 0  | 0        | 0  | 2               | 7                   |
| 8:45 AM           | 0  | 0        | 0  | 0  | 0        | 0  | 0  | 0         | 0  | 0  | 0        | 0  | 0               | 6                   |
| Count Total       | 0  | 0        | 0  | 0  | 7        | 0  | 1  | 0         | 1  | 0  | 1        | 1  | 11              | 0                   |
| Peak Hour         | 0  | 0        | 0  | 0  | 5        | 0  | 1  | 0         | 0  | 0  | 0        | 0  | 6               | 0                   |

Note: U-Turn volumes for bikes are included in Left-Turn, if any.



**Peak Hour** 

| Interval    |    | Nas   | h Rd  |    |    | Nas   | h Rd  |    |    | San Be | enito St | t  |    | San Be | enito St |    | 15-min | Dalling             |
|-------------|----|-------|-------|----|----|-------|-------|----|----|--------|----------|----|----|--------|----------|----|--------|---------------------|
| Start       |    | Eastb | oound |    |    | Westl | bound |    |    | North  | bound    |    |    | South  | bound    |    | Total  | Rolling<br>One Hour |
| Otari       | UT | LT    | TH    | RT | UT | LT    | TH    | RT | UT | LT     | TH       | RT | UT | LT     | TH       | RT | Total  | One neur            |
| 4:00 PM     | 0  | 0     | 0     | 0  | 0  | 1     | 1     | 0  | 0  | 0      | 0        | 1  | 0  | 0      | 0        | 0  | 3      | 0                   |
| 4:15 PM     | 0  | 0     | 0     | 2  | 0  | 1     | 0     | 1  | 0  | 0      | 0        | 1  | 0  | 0      | 0        | 0  | 5      | 0                   |
| 4:30 PM     | 0  | 0     | 0     | 0  | 0  | 0     | 0     | 0  | 0  | 0      | 0        | 0  | 0  | 0      | 0        | 0  | 0      | 0                   |
| 4:45 PM     | 0  | 0     | 0     | 1  | 0  | 1     | 0     | 0  | 0  | 0      | 0        | 0  | 0  | 0      | 0        | 0  | 2      | 10                  |
| 5:00 PM     | 0  | 0     | 0     | 0  | 0  | 0     | 0     | 0  | 0  | 0      | 0        | 1  | 0  | 0      | 0        | 0  | 1      | 8                   |
| 5:15 PM     | 0  | 0     | 0     | 0  | 0  | 1     | 0     | 0  | 0  | 0      | 0        | 0  | 0  | 0      | 0        | 0  | 1      | 4                   |
| 5:30 PM     | 0  | 0     | 0     | 0  | 0  | 0     | 0     | 0  | 0  | 0      | 0        | 1  | 0  | 0      | 0        | 0  | 1      | 5                   |
| 5:45 PM     | 0  | 0     | 0     | 1  | 0  | 0     | 0     | 1  | 0  | 0      | 0        | 0  | 0  | 0      | 0        | 0  | 2      | 5                   |
| Count Total | 0  | 0     | 0     | 4  | 0  | 4     | 1     | 2  | 0  | 0      | 0        | 4  | 0  | 0      | 0        | 0  | 15     | 0                   |
| Peak Hour   | 0  | 0     | 0     | 1  | 0  | 1     | 0     | 1  | 0  | 0      | 0        | 2  | 0  | 0      | 0        | 0  | 5      | 0                   |

| la ta maal        |    | Nash Rd  |    |    | Nash Rd  | l  | Sa | n Benito  | St | Sa | n Benito | St | 45              | D - III             |
|-------------------|----|----------|----|----|----------|----|----|-----------|----|----|----------|----|-----------------|---------------------|
| Interval<br>Start | ı  | Eastboun | d  | V  | Vestboun | ıd | ١  | Northbour | nd | S  | outhbour | nd | 15-min<br>Total | Rolling<br>One Hour |
| Otare             | LT | TH       | RT | LT | TH       | RT | LT | TH        | RT | LT | TH       | RT | rotar           | One near            |
| 4:00 PM           | 0  | 0        | 0  | 0  | 0        | 0  | 0  | 0         | 0  | 0  | 0        | 0  | 0               | 0                   |
| 4:15 PM           | 0  | 0        | 0  | 0  | 0        | 0  | 0  | 0         | 0  | 0  | 0        | 0  | 0               | 0                   |
| 4:30 PM           | 0  | 0        | 0  | 0  | 0        | 0  | 0  | 0         | 0  | 0  | 0        | 0  | 0               | 0                   |
| 4:45 PM           | 0  | 0        | 0  | 0  | 0        | 0  | 0  | 0         | 0  | 0  | 0        | 0  | 0               | 0                   |
| 5:00 PM           | 0  | 0        | 0  | 0  | 0        | 0  | 0  | 0         | 0  | 0  | 0        | 0  | 0               | 0                   |
| 5:15 PM           | 0  | 0        | 2  | 0  | 0        | 0  | 0  | 0         | 0  | 0  | 0        | 0  | 2               | 2                   |
| 5:30 PM           | 0  | 2        | 1  | 0  | 0        | 0  | 0  | 0         | 0  | 0  | 0        | 0  | 3               | 5                   |
| 5:45 PM           | 0  | 1        | 1  | 0  | 0        | 0  | 0  | 0         | 0  | 0  | 0        | 0  | 2               | 7                   |
| Count Total       | 0  | 3        | 4  | 0  | 0        | 0  | 0  | 0         | 0  | 0  | 0        | 0  | 7               | 0                   |
| Peak Hour         | 0  | 3        | 4  | 0  | 0        | 0  | 0  | 0         | 0  | 0  | 0        | 0  | 7               | 0                   |

Note: U-Turn volumes for bikes are included in Left-Turn, if any.

# Appendix C

Level of Service
Calculations

Existing

Conditions

HCM 2010 AWSC Existing AM

| ntersection              |      |
|--------------------------|------|
| ntersection Delay, s/veh | 12.8 |
| ntersection LOS          | В    |

| Intersection Loo           | U    |         |      |      |         |      |      |      |      |      |         |      |
|----------------------------|------|---------|------|------|---------|------|------|------|------|------|---------|------|
|                            |      |         |      |      |         |      |      |      |      |      |         |      |
| Movement                   | EBL  | EBT     | EBR  | WBL  | WBT     | WBR  | NBL  | NBT  | NBR  | SBL  | SBT     | SBR  |
| Lane Configurations        | 7    | <b></b> | 7    | , N  | <b></b> | 7    | Ĭ    | f)   |      | Ţ    | <b></b> | 7    |
| Traffic Vol, veh/h         | 90   | 106     | 74   | 7    | 203     | 87   | 166  | 74   | 3    | 46   | 30      | 84   |
| Future Vol, veh/h          | 90   | 106     | 74   | 7    | 203     | 87   | 166  | 74   | 3    | 46   | 30      | 84   |
| Peak Hour Factor           | 0.90 | 0.90    | 0.90 | 0.90 | 0.90    | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90    | 0.90 |
| Heavy Vehicles, %          | 7    | 7       | 7    | 5    | 5       | 5    | 2    | 2    | 2    | 6    | 6       | 6    |
| Mvmt Flow                  | 100  | 118     | 82   | 8    | 226     | 97   | 184  | 82   | 3    | 51   | 33      | 93   |
| Number of Lanes            | 1    | 1       | 1    | 1    | 1       | 1    | 1    | 1    | 0    | 1    | 1       | 1    |
| Approach                   | EB   |         |      | WB   |         |      | NB   |      |      | SB   |         |      |
| Opposing Approach          | WB   |         |      | EB   |         |      | SB   |      |      | NB   |         |      |
| Opposing Lanes             | 3    |         |      | 3    |         |      | 3    |      |      | 2    |         |      |
| Conflicting Approach Left  | SB   |         |      | NB   |         |      | EB   |      |      | WB   |         |      |
| Conflicting Lanes Left     | 3    |         |      | 2    |         |      | 3    |      |      | 3    |         |      |
| Conflicting Approach Right | NB   |         |      | SB   |         |      | WB   |      |      | EB   |         |      |
| Conflicting Lanes Right    | 2    |         |      | 3    |         |      | 3    |      |      | 3    |         |      |
| HCM Control Delay          | 11.7 |         |      | 13.8 |         |      | 13.8 |      |      | 11.2 |         |      |
| HCM LOS                    | В    |         |      | В    |         |      | В    |      |      | В    |         |      |

| Lane                   | NBLn1 | NBLn2 | EBLn1 | EBLn2 | EBLn3 | WBLn1 | WBLn2 | WBLn3 | SBLn1 | SBLn2 | SBLn3 |
|------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Vol Left, %            | 100%  | 0%    | 100%  | 0%    | 0%    | 100%  | 0%    | 0%    | 100%  | 0%    | 0%    |
| Vol Thru, %            | 0%    | 96%   | 0%    | 100%  | 0%    | 0%    | 100%  | 0%    | 0%    | 100%  | 0%    |
| Vol Right, %           | 0%    | 4%    | 0%    | 0%    | 100%  | 0%    | 0%    | 100%  | 0%    | 0%    | 100%  |
| Sign Control           | Stop  |
| Traffic Vol by Lane    | 166   | 77    | 90    | 106   | 74    | 7     | 203   | 87    | 46    | 30    | 84    |
| LT Vol                 | 166   | 0     | 90    | 0     | 0     | 7     | 0     | 0     | 46    | 0     | 0     |
| Through Vol            | 0     | 74    | 0     | 106   | 0     | 0     | 203   | 0     | 0     | 30    | 0     |
| RT Vol                 | 0     | 3     | 0     | 0     | 74    | 0     | 0     | 87    | 0     | 0     | 84    |
| Lane Flow Rate         | 184   | 86    | 100   | 118   | 82    | 8     | 226   | 97    | 51    | 33    | 93    |
| Geometry Grp           | 8     | 8     | 8     | 8     | 8     | 8     | 8     | 8     | 8     | 8     | 8     |
| Degree of Util (X)     | 0.388 | 0.167 | 0.213 | 0.235 | 0.148 | 0.016 | 0.444 | 0.171 | 0.114 | 0.069 | 0.176 |
| Departure Headway (Hd) | 7.568 | 7.041 | 7.679 | 7.172 | 6.463 | 7.595 | 7.089 | 6.358 | 7.995 | 7.491 | 6.785 |
| Convergence, Y/N       | Yes   |
| Cap                    | 478   | 512   | 468   | 501   | 555   | 473   | 510   | 565   | 449   | 478   | 528   |
| Service Time           | 5.28  | 4.753 | 5.419 | 4.913 | 4.204 | 5.31  | 4.804 | 4.096 | 5.74  | 5.236 | 4.53  |
| HCM Lane V/C Ratio     | 0.385 | 0.168 | 0.214 | 0.236 | 0.148 | 0.017 | 0.443 | 0.172 | 0.114 | 0.069 | 0.176 |
| HCM Control Delay      | 15    | 11.2  | 12.5  | 12.1  | 10.3  | 10.4  | 15.4  | 10.4  | 11.8  | 10.8  | 11    |
| HCM Lane LOS           | В     | В     | В     | В     | В     | В     | С     | В     | В     | В     | В     |
| HCM 95th-tile Q        | 1.8   | 0.6   | 8.0   | 0.9   | 0.5   | 0     | 2.3   | 0.6   | 0.4   | 0.2   | 0.6   |

| Intersection           |         |          |        |        |          |      |        |          |       |        |          |       |       |  |
|------------------------|---------|----------|--------|--------|----------|------|--------|----------|-------|--------|----------|-------|-------|--|
| Int Delay, s/veh       | 3       |          |        |        |          |      |        |          |       |        |          |       |       |  |
| Movement               | EBL     | EBT      | EBR    | WBL    | WBT      | WBR  | NBL    | NBT      | NBR   | SBL    | SBT      | SBR   |       |  |
| Lane Configurations    | ሻ       | <u> </u> | 7      | ሻ      | <u> </u> | 7    | ሻ      | <u> </u> | 7     | )<br>j | <u> </u> | 7     |       |  |
| Traffic Vol, veh/h     | 15      | 215      | 15     | 30     | 400      | 19   | 45     | 4        | 35    | 20     | 3        | 43    |       |  |
| Future Vol, veh/h      | 15      | 215      | 15     | 30     | 400      | 19   | 45     | 4        | 35    | 20     | 3        | 43    |       |  |
| Conflicting Peds, #/hr | 0       | 0        | 1      | 0      | 0        | 0    | 0      | 0        | 0     | 0      | 0        | 0     |       |  |
| Sign Control           | Free    | Free     | Free   | Free   | Free     | Free | Stop   | Stop     | Stop  | Stop   | Stop     | Stop  |       |  |
| RT Channelized         | _       | -        | None   | _      | _        | None | -      | -        | None  | -      | -        | None  |       |  |
| Storage Length         | 320     | _        | 505    | 360    | -        | 195  | 60     | _        | 0     | 100    | -        | 100   |       |  |
| Veh in Median Storage, | # -     | 0        | -      | -      | 0        | -    | -      | 0        | -     | -      | 0        | _     |       |  |
| Grade, %               | -       | 0        | -      | -      | 0        | -    | -      | 0        | -     | -      | 0        | -     |       |  |
| Peak Hour Factor       | 95      | 95       | 95     | 95     | 95       | 95   | 95     | 95       | 95    | 95     | 95       | 95    |       |  |
| Heavy Vehicles, %      | 8       | 8        | 8      | 4      | 4        | 4    | 2      | 2        | 2     | 3      | 3        | 3     |       |  |
| Mvmt Flow              | 16      | 226      | 16     | 32     | 421      | 20   | 47     | 4        | 37    | 21     | 3        | 45    |       |  |
|                        |         |          |        |        |          |      |        |          |       |        |          |       |       |  |
| Major/Minor N          | /lajor1 |          |        | Major2 |          | ı    | Minor1 |          |       | Minor2 |          |       |       |  |
| Conflicting Flow All   | 441     | 0        | 0      | 243    | 0        | 0    | 778    | 764      | 227   | 772    | 760      | 421   |       |  |
| Stage 1                | -       | -        | -      | -      | -        | -    | 259    | 259      | -     | 485    | 485      | -     |       |  |
| Stage 2                | _       | _        | -      | -      | _        | _    | 519    | 505      | _     | 287    | 275      | -     |       |  |
| Critical Hdwy          | 4.18    | -        | -      | 4.14   | -        | -    | 7.12   | 6.52     | 6.22  | 7.13   | 6.53     | 6.23  |       |  |
| Critical Hdwy Stg 1    | -       | -        | -      | -      | -        | -    | 6.12   | 5.52     | -     | 6.13   | 5.53     | -     |       |  |
| Critical Hdwy Stg 2    | -       | -        | -      | -      | -        | -    | 6.12   | 5.52     | -     | 6.13   | 5.53     | -     |       |  |
| Follow-up Hdwy         | 2.272   | -        | -      | 2.236  | -        | -    | 3.518  | 4.018    | 3.318 | 3.527  | 4.027    | 3.327 |       |  |
| Pot Cap-1 Maneuver     | 1088    | -        | -      | 1312   | -        | -    | 314    | 334      | 812   | 315    | 334      | 630   |       |  |
| Stage 1                | -       | -        | -      | -      | -        | -    | 746    | 694      | -     | 561    | 550      | -     |       |  |
| Stage 2                | -       | -        | -      | -      | -        | -    | 540    | 540      | -     | 718    | 681      | -     |       |  |
| Platoon blocked, %     |         | -        | -      |        | -        | -    |        |          |       |        |          |       |       |  |
| Mov Cap-1 Maneuver     | 1088    | -        | -      | 1311   | -        | -    | 280    | 321      | 811   | 289    | 321      | 630   |       |  |
| Mov Cap-2 Maneuver     | -       | -        | -      | -      | -        | -    | 280    | 321      | -     | 289    | 321      | -     |       |  |
| Stage 1                | -       | -        | -      | -      | -        | -    | 734    | 683      | -     | 553    | 537      | -     |       |  |
| Stage 2                | -       | -        | -      | -      | -        | -    | 486    | 527      | -     | 671    | 670      | -     |       |  |
|                        |         |          |        |        |          |      |        |          |       |        |          |       |       |  |
| Approach               | EB      |          |        | WB     |          |      | NB     |          |       | SB     |          |       |       |  |
| HCM Control Delay, s   | 0.5     |          |        | 0.5    |          |      | 15.8   |          |       | 13.6   |          |       |       |  |
| HCM LOS                |         |          |        |        |          |      | С      |          |       | В      |          |       |       |  |
|                        |         |          |        |        |          |      |        |          |       |        |          |       |       |  |
| Minor Lane/Major Mvmt  | t 1     | NBLn11   | NBLn21 | NBLn3  | EBL      | EBT  | EBR    | WBL      | WBT   | WBR    | SBLn1    | SBLn2 | SBLn3 |  |
| Capacity (veh/h)       |         | 280      | 321    | 811    | 1088     | -    |        | 1311     | -     | -      |          | 321   | 630   |  |
| HCM Lane V/C Ratio     |         |          | 0.013  |        |          | -    |        | 0.024    | -     | -      | 0.073    |       | 0.072 |  |
| HCM Control Delay (s)  |         | 20.5     | 16.4   | 9.7    | 8.4      | -    | -      | 7.8      | -     | -      |          | 16.3  | 11.2  |  |
| HCM Lane LOS           |         | С        | С      | Α      | Α        | -    | -      | Α        | -     | -      | С        | С     | В     |  |
| HCM 95th %tile Q(veh)  |         | 0.6      | 0      | 0.1    | 0        | _    | _      | 0.1      | _     | _      | 0.2      | 0     | 0.2   |  |

| Intersection  |          |       |        |       |        |      |
|---|----------|-------|--------|-------|--------|------|
| Int Delay, s/veh  | 2.4      |       |        |       |        |      |
|   |          | WDD   | NDT    | NDD   | CDI    | SBT  |
| Movement  | WBL      | WBR   | NBT    | NBR   | SBL    |      |
| Lane Configurations                                       | <b>\</b> | 60    | 104    | 10    | 10     | 4    |
| Traffic Vol, veh/h  | 25       | 62    | 184    | 12    | 13     | 142  |
| Future Vol, veh/h   | 25       | 62    | 184    | 12    | 13     | 142  |
| Conflicting Peds, #/hr                                    | 0        | 0     | 0      | _ 1   | _ 1    | _ 0  |
| Sign Control  | Stop     | Stop  | Free   | Free  | Free   | Free |
| RT Channelized  | -        | None  | -      | None  | -      | None |
| Storage Length  | 0        | -     | -      | -     | -      | -    |
| Veh in Median Storage                                     |          | -     | 0      | -     | -      | 0    |
| Grade, %  | 0        | -     | 0      | -     | -      | 0    |
| Peak Hour Factor  | 84       | 84    | 84     | 84    | 84     | 84   |
| Heavy Vehicles, %   | 2        | 2     | 7      | 7     | 7      | 7    |
| Mvmt Flow   | 30       | 74    | 219    | 14    | 15     | 169  |
|   |          |       |        |       |        |      |
| Major/Minor N   | Minor1   | N     | Major1 |       | Major2 |      |
| Conflicting Flow All                                      | 426      | 227   | 0      | 0     | 234    | 0    |
|   | 227      |       |        | U     |        |      |
| Stage 1   |          | -     | -      | -     | -      | -    |
| Stage 2   | 199      | -     | -      | -     | - 4.47 | -    |
| Critical Hdwy   | 6.42     | 6.22  | -      | -     | 4.17   | -    |
| Critical Hdwy Stg 1                                       | 5.42     | -     | -      | -     | -      | -    |
| Critical Hdwy Stg 2                                       | 5.42     | -     | -      | -     | -      | -    |
| Follow-up Hdwy  | 3.518    | 3.318 | -      | -     | 00     | -    |
| Pot Cap-1 Maneuver  | 585      | 812   | -      | -     | 1305   | -    |
| Stage 1   | 811      | -     | -      | -     | -      | -    |
| Stage 2   | 835      | -     | -      | -     | -      | -    |
| Platoon blocked, %  |          |       | -      | -     |        | -    |
| Mov Cap-1 Maneuver  | 577      | 811   | -      | -     | 1304   | -    |
| Mov Cap-2 Maneuver  | 577      | -     | -      | -     | -      | -    |
| Stage 1   | 800      | -     | -      | -     | -      | -    |
| Stage 2   | 835      | -     | -      | -     | -      | -    |
|   |          |       |        |       |        |      |
| A mara a a b  | WD       |       | ND     |       | CD     |      |
| Approach  | WB       |       | NB     |       | SB     |      |
| HCM Control Delay, s                                      | 10.8     |       | 0      |       | 0.7    |      |
| HCM LOS   | В        |       |        |       |        |      |
|   |          |       |        |       |        |      |
| Minor Lane/Major Mvm                                      | ıt       | NBT   | NBRV   | VBLn1 | SBL    | SBT  |
| IVIII IOI Lano/Iviajoi Iviviii                            |          | _     | _      |       | 1304   | _    |
|   |          |       |        |       |        | _    |
| Capacity (veh/h)  |          | _     | _      | 0 143 | 0.012  |      |
| Capacity (veh/h)<br>HCM Lane V/C Ratio                    |          | -     |        | 0.143 |        |      |
| Capacity (veh/h) HCM Lane V/C Ratio HCM Control Delay (s) |          | -     | -      | 10.8  | 7.8    | 0    |
| Capacity (veh/h)<br>HCM Lane V/C Ratio                    |          |       |        |       |        |      |

|                              | •    | <b>→</b> | `    | <b>√</b> | <b>←</b> | •     | •    | †        | ~    | <b>/</b> | <b></b>  | ✓    |
|------------------------------|------|----------|------|----------|----------|-------|------|----------|------|----------|----------|------|
| Movement                     | EBL  | EBT      | EBR  | WBL      | WBT      | WBR   | NBL  | NBT      | NBR  | SBL      | SBT      | SBR  |
| Lane Configurations          | 7    | ĵ»       |      | ň        | ĵ.       |       | Ţ    | <b>†</b> | 7    | 7        | <b>†</b> | 7    |
| Traffic Volume (veh/h)       | 125  | 144      | 105  | 13       | 261      | 186   | 232  | 260      | 19   | 79       | 117      | 114  |
| Future Volume (veh/h)        | 125  | 144      | 105  | 13       | 261      | 186   | 232  | 260      | 19   | 79       | 117      | 114  |
| Number                       | 7    | 4        | 14   | 3        | 8        | 18    | 5    | 2        | 12   | 1        | 6        | 16   |
| Initial Q (Qb), veh          | 0    | 0        | 0    | 0        | 0        | 0     | 0    | 0        | 0    | 0        | 0        | 0    |
| Ped-Bike Adj(A_pbT)          | 1.00 |          | 1.00 | 1.00     |          | 1.00  | 1.00 |          | 1.00 | 1.00     |          | 1.00 |
| Parking Bus, Adj             | 1.00 | 1.00     | 1.00 | 1.00     | 1.00     | 1.00  | 1.00 | 1.00     | 1.00 | 1.00     | 1.00     | 1.00 |
| Adj Sat Flow, veh/h/ln       | 1776 | 1776     | 1900 | 1863     | 1863     | 1900  | 1863 | 1863     | 1863 | 1827     | 1827     | 1827 |
| Adj Flow Rate, veh/h         | 136  | 157      | 114  | 14       | 284      | 202   | 252  | 283      | 21   | 86       | 127      | 124  |
| Adj No. of Lanes             | 1    | 1        | 0    | 1        | 1        | 0     | 1    | 1        | 1    | 1        | 1        | 1    |
| Peak Hour Factor             | 0.92 | 0.92     | 0.92 | 0.92     | 0.92     | 0.92  | 0.92 | 0.92     | 0.92 | 0.92     | 0.92     | 0.92 |
| Percent Heavy Veh, %         | 7    | 7        | 7    | 2        | 2        | 2     | 2    | 2        | 2    | 4        | 4        | 4    |
| Cap, veh/h                   | 316  | 179      | 130  | 439      | 251      | 178   | 258  | 558      | 474  | 109      | 396      | 337  |
| Arrive On Green              | 0.19 | 0.19     | 0.19 | 0.25     | 0.25     | 0.25  | 0.15 | 0.30     | 0.30 | 0.06     | 0.22     | 0.22 |
| Sat Flow, veh/h              | 1691 | 956      | 694  | 1774     | 1014     | 721   | 1774 | 1863     | 1583 | 1740     | 1827     | 1553 |
| Grp Volume(v), veh/h         | 136  | 0        | 271  | 14       | 0        | 486   | 252  | 283      | 21   | 86       | 127      | 124  |
| Grp Sat Flow(s),veh/h/ln     | 1691 | 0        | 1651 | 1774     | 0        | 1735  | 1774 | 1863     | 1583 | 1740     | 1827     | 1553 |
| Q Serve(g_s), s              | 6.3  | 0.0      | 14.1 | 0.5      | 0.0      | 21.9  | 12.5 | 11.1     | 0.8  | 4.3      | 5.2      | 6.0  |
| Cycle Q Clear(g_c), s        | 6.3  | 0.0      | 14.1 | 0.5      | 0.0      | 21.9  | 12.5 | 11.1     | 0.8  | 4.3      | 5.2      | 6.0  |
| Prop In Lane                 | 1.00 |          | 0.42 | 1.00     |          | 0.42  | 1.00 |          | 1.00 | 1.00     |          | 1.00 |
| Lane Grp Cap(c), veh/h       | 316  | 0        | 309  | 439      | 0        | 429   | 258  | 558      | 474  | 109      | 396      | 337  |
| V/C Ratio(X)                 | 0.43 | 0.00     | 0.88 | 0.03     | 0.00     | 1.13  | 0.98 | 0.51     | 0.04 | 0.79     | 0.32     | 0.37 |
| Avail Cap(c_a), veh/h        | 344  | 0        | 336  | 439      | 0        | 429   | 258  | 558      | 474  | 143      | 396      | 337  |
| HCM Platoon Ratio            | 1.00 | 1.00     | 1.00 | 1.00     | 1.00     | 1.00  | 1.00 | 1.00     | 1.00 | 1.00     | 1.00     | 1.00 |
| Upstream Filter(I)           | 1.00 | 0.00     | 1.00 | 1.00     | 0.00     | 1.00  | 1.00 | 1.00     | 1.00 | 1.00     | 1.00     | 1.00 |
| Uniform Delay (d), s/veh     | 31.8 | 0.0      | 35.0 | 25.3     | 0.0      | 33.3  | 37.7 | 25.6     | 22.0 | 40.9     | 29.2     | 29.5 |
| Incr Delay (d2), s/veh       | 0.9  | 0.0      | 21.1 | 0.0      | 0.0      | 84.8  | 48.9 | 3.3      | 0.2  | 18.8     | 2.1      | 3.1  |
| Initial Q Delay(d3),s/veh    | 0.0  | 0.0      | 0.0  | 0.0      | 0.0      | 0.0   | 0.0  | 0.0      | 0.0  | 0.0      | 0.0      | 0.0  |
| %ile BackOfQ(50%),veh/ln     | 3.0  | 0.0      | 8.2  | 0.3      | 0.0      | 20.5  | 9.6  | 6.2      | 0.4  | 2.7      | 2.8      | 2.9  |
| LnGrp Delay(d),s/veh         | 32.8 | 0.0      | 56.1 | 25.3     | 0.0      | 118.1 | 86.6 | 28.9     | 22.2 | 59.8     | 31.3     | 32.6 |
| LnGrp LOS                    | С    |          | E    | С        |          | F     | F    | С        | С    | E        | С        | С    |
| Approach Vol, veh/h          |      | 407      |      |          | 500      |       |      | 556      |      |          | 337      |      |
| Approach Delay, s/veh        |      | 48.3     |      |          | 115.5    |       |      | 54.8     |      |          | 39.0     |      |
| Approach LOS                 |      | D        |      |          | F        |       |      | D        |      |          | D        |      |
| Timer                        | 1    | 2        | 3    | 4        | 5        | 6     | 7    | 8        |      |          |          |      |
| Assigned Phs                 | 1    | 2        |      | 4        | 5        | 6     |      | 8        |      |          |          |      |
| Phs Duration (G+Y+Rc), s     | 10.1 | 31.0     |      | 21.1     | 17.4     | 23.7  |      | 26.4     |      |          |          |      |
| Change Period (Y+Rc), s      | 4.5  | 4.5      |      | 4.5      | 4.5      | 4.5   |      | 4.5      |      |          |          |      |
| Max Green Setting (Gmax), s  | 7.3  | 24.8     |      | 18.0     | 12.9     | 19.2  |      | 21.9     |      |          |          |      |
| Max Q Clear Time (g_c+l1), s | 6.3  | 13.1     |      | 16.1     | 14.5     | 8.0   |      | 23.9     |      |          |          |      |
| Green Ext Time (p_c), s      | 0.0  | 1.3      |      | 0.4      | 0.0      | 0.8   |      | 0.0      |      |          |          |      |
| Intersection Summary         |      |          |      |          |          |       |      |          |      |          |          |      |
| HCM 2010 Ctrl Delay          |      |          | 67.3 |          |          |       |      |          |      |          |          |      |
| HCM 2010 LOS                 |      |          | Е    |          |          |       |      |          |      |          |          |      |

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|                              | •    | <b>→</b> | •    | <b>√</b> | <b>←</b> | •    | •    | †    | <i>&gt;</i> | <b>&gt;</b> | ţ    | ✓    |
|------------------------------|------|----------|------|----------|----------|------|------|------|-------------|-------------|------|------|
| Movement                     | EBL  | EBT      | EBR  | WBL      | WBT      | WBR  | NBL  | NBT  | NBR         | SBL         | SBT  | SBR  |
| Lane Configurations          | 7    | f)       |      | 7        | f)       |      |      | 4    |             |             | 4    |      |
| Traffic Volume (veh/h)       | 6    | 274      | 84   | 59       | 576      | 15   | 113  | 40   | 69          | 17          | 15   | 12   |
| Future Volume (veh/h)        | 6    | 274      | 84   | 59       | 576      | 15   | 113  | 40   | 69          | 17          | 15   | 12   |
| Number                       | 7    | 4        | 14   | 3        | 8        | 18   | 5    | 2    | 12          | 1           | 6    | 16   |
| Initial Q (Qb), veh          | 0    | 0        | 0    | 0        | 0        | 0    | 0    | 0    | 0           | 0           | 0    | 0    |
| Ped-Bike Adj(A_pbT)          | 1.00 |          | 1.00 | 1.00     |          | 1.00 | 1.00 |      | 1.00        | 1.00        |      | 1.00 |
| Parking Bus, Adj             | 1.00 | 1.00     | 1.00 | 1.00     | 1.00     | 1.00 | 1.00 | 1.00 | 1.00        | 1.00        | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln       | 1827 | 1827     | 1900 | 1845     | 1845     | 1900 | 1900 | 1810 | 1900        | 1900        | 1776 | 1900 |
| Adj Flow Rate, veh/h         | 7    | 311      | 95   | 67       | 655      | 17   | 128  | 45   | 78          | 19          | 17   | 14   |
| Adj No. of Lanes             | 1    | 1        | 0    | 1        | 1        | 0    | 0    | 1    | 0           | 0           | 1    | 0    |
| Peak Hour Factor             | 0.88 | 0.88     | 0.88 | 0.88     | 0.88     | 0.88 | 0.88 | 0.88 | 0.88        | 0.88        | 0.88 | 0.88 |
| Percent Heavy Veh, %         | 4    | 4        | 4    | 3        | 3        | 3    | 5    | 5    | 5           | 7           | 7    | 7    |
| Cap, veh/h                   | 16   | 494      | 151  | 101      | 745      | 19   | 321  | 119  | 155         | 248         | 213  | 145  |
| Arrive On Green              | 0.01 | 0.37     | 0.37 | 0.06     | 0.42     | 0.42 | 0.34 | 0.34 | 0.34        | 0.34        | 0.34 | 0.34 |
| Sat Flow, veh/h              | 1740 | 1344     | 411  | 1757     | 1790     | 46   | 670  | 356  | 463         | 477         | 635  | 433  |
| Grp Volume(v), veh/h         | 7    | 0        | 406  | 67       | 0        | 672  | 251  | 0    | 0           | 50          | 0    | 0    |
| Grp Sat Flow(s),veh/h/ln     | 1740 | 0        | 1754 | 1757     | 0        | 1836 | 1489 | 0    | 0           | 1545        | 0    | 0    |
| Q Serve(g_s), s              | 0.2  | 0.0      | 10.7 | 2.1      | 0.0      | 19.0 | 5.4  | 0.0  | 0.0         | 0.0         | 0.0  | 0.0  |
| Cycle Q Clear(g_c), s        | 0.2  | 0.0      | 10.7 | 2.1      | 0.0      | 19.0 | 7.4  | 0.0  | 0.0         | 1.1         | 0.0  | 0.0  |
| Prop In Lane                 | 1.00 |          | 0.23 | 1.00     |          | 0.03 | 0.51 |      | 0.31        | 0.38        |      | 0.28 |
| Lane Grp Cap(c), veh/h       | 16   | 0        | 645  | 101      | 0        | 764  | 596  | 0    | 0           | 606         | 0    | 0    |
| V/C Ratio(X)                 | 0.44 | 0.00     | 0.63 | 0.66     | 0.00     | 0.88 | 0.42 | 0.00 | 0.00        | 0.08        | 0.00 | 0.00 |
| Avail Cap(c_a), veh/h        | 157  | 0        | 800  | 215      | 0        | 896  | 596  | 0    | 0           | 606         | 0    | 0    |
| HCM Platoon Ratio            | 1.00 | 1.00     | 1.00 | 1.00     | 1.00     | 1.00 | 1.00 | 1.00 | 1.00        | 1.00        | 1.00 | 1.00 |
| Upstream Filter(I)           | 1.00 | 0.00     | 1.00 | 1.00     | 0.00     | 1.00 | 1.00 | 0.00 | 0.00        | 1.00        | 0.00 | 0.00 |
| Uniform Delay (d), s/veh     | 27.8 | 0.0      | 14.7 | 26.0     | 0.0      | 15.2 | 14.8 | 0.0  | 0.0         | 12.8        | 0.0  | 0.0  |
| Incr Delay (d2), s/veh       | 17.6 | 0.0      | 1.1  | 7.2      | 0.0      | 9.0  | 2.2  | 0.0  | 0.0         | 0.3         | 0.0  | 0.0  |
| Initial Q Delay(d3),s/veh    | 0.0  | 0.0      | 0.0  | 0.0      | 0.0      | 0.0  | 0.0  | 0.0  | 0.0         | 0.0         | 0.0  | 0.0  |
| %ile BackOfQ(50%),veh/ln     | 0.2  | 0.0      | 5.4  | 1.2      | 0.0      | 11.4 | 3.4  | 0.0  | 0.0         | 0.6         | 0.0  | 0.0  |
| LnGrp Delay(d),s/veh         | 45.4 | 0.0      | 15.7 | 33.2     | 0.0      | 24.1 | 17.0 | 0.0  | 0.0         | 13.1        | 0.0  | 0.0  |
| LnGrp LOS                    | D    |          | В    | С        |          | С    | В    |      |             | В           |      |      |
| Approach Vol, veh/h          |      | 413      |      |          | 739      |      |      | 251  |             |             | 50   |      |
| Approach Delay, s/veh        |      | 16.2     |      |          | 25.0     |      |      | 17.0 |             |             | 13.1 |      |
| Approach LOS                 |      | В        |      |          | С        |      |      | В    |             |             | В    |      |
| Timer                        | 1    | 2        | 3    | 4        | 5        | 6    | 7    | 8    |             |             |      |      |
| Assigned Phs                 |      | 2        | 3    | 4        |          | 6    | 7    | 8    |             |             |      |      |
| Phs Duration (G+Y+Rc), s     |      | 23.4     | 7.7  | 25.2     |          | 23.4 | 5.0  | 28.0 |             |             |      |      |
| Change Period (Y+Rc), s      |      | 4.5      | 4.5  | 4.5      |          | 4.5  | 4.5  | 4.5  |             |             |      |      |
| Max Green Setting (Gmax), s  |      | 18.9     | 6.9  | 25.7     |          | 18.9 | 5.1  | 27.5 |             |             |      |      |
| Max Q Clear Time (g_c+l1), s |      | 9.4      | 4.1  | 12.7     |          | 3.1  | 2.2  | 21.0 |             |             |      |      |
| Green Ext Time (p_c), s      |      | 1.0      | 0.0  | 2.1      |          | 0.1  | 0.0  | 2.5  |             |             |      |      |
| Intersection Summary         |      |          |      |          |          |      |      |      |             |             |      |      |
| HCM 2010 Ctrl Delay          |      |          | 20.7 |          |          |      |      |      |             |             |      |      |
| HCM 2010 LOS                 |      |          | С    |          |          |      |      |      |             |             |      |      |

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|                              |      | <b>→</b> | <b>←</b> | •    | <u> </u> | 4    |      |      |  |      |
|------------------------------|------|----------|----------|------|----------|------|------|------|--|------|
| Movement                     | EBL  | EBT      | WBT      | WBR  | SBL      | SBR  |      |      |  |      |
| Lane Configurations          | *    | <b>†</b> | <b>^</b> | 7    | ች        | 7    |      |      |  | <br> |
| Traffic Volume (veh/h)       | 146  | 192      | 370      | 342  | 175      | 169  |      |      |  |      |
| Future Volume (veh/h)        | 146  | 192      | 370      | 342  | 175      | 169  |      |      |  |      |
| Number                       | 7    | 4        | 8        | 18   | 1        | 16   |      |      |  |      |
| Initial Q (Qb), veh          | 0    | 0        | 0        | 0    | 0        | 0    |      |      |  |      |
| Ped-Bike Adj(A_pbT)          | 1.00 |          |          | 1.00 | 1.00     | 1.00 |      |      |  |      |
| Parking Bus, Adj             | 1.00 | 1.00     | 1.00     | 1.00 | 1.00     | 1.00 |      |      |  |      |
| Adj Sat Flow, veh/h/ln       | 1810 | 1810     | 1863     | 1863 | 1863     | 1863 |      |      |  |      |
| Adj Flow Rate, veh/h         | 166  | 218      | 420      | 389  | 199      | 192  |      |      |  |      |
| Adj No. of Lanes             | 1    | 1        | 1        | 1    | 1        | 1    |      |      |  |      |
| Peak Hour Factor             | 0.88 | 0.88     | 0.88     | 0.88 | 0.88     | 0.88 |      |      |  |      |
| Percent Heavy Veh, %         | 5    | 5        | 2        | 2    | 2        | 2    |      |      |  |      |
| Cap, veh/h                   | 213  | 970      | 596      | 507  | 494      | 441  |      |      |  |      |
| Arrive On Green              | 0.12 | 0.54     | 0.32     | 0.32 | 0.28     | 0.28 |      |      |  |      |
| Sat Flow, veh/h              | 1723 | 1810     | 1863     | 1583 | 1774     | 1583 |      |      |  |      |
| Grp Volume(v), veh/h         | 166  | 218      | 420      | 389  | 199      | 192  |      |      |  |      |
| Grp Sat Flow(s), veh/h/ln    | 1723 | 1810     | 1863     | 1583 | 1774     | 1583 |      |      |  |      |
| Q Serve(g_s), s              | 4.5  | 3.1      | 9.6      | 10.7 | 4.4      | 4.8  |      |      |  |      |
| Cycle Q Clear(g_c), s        | 4.5  | 3.1      | 9.6      | 10.7 | 4.4      | 4.8  |      |      |  |      |
| Prop In Lane                 | 1.00 | 0.1      | 0.0      | 1.00 | 1.00     | 1.00 |      |      |  |      |
| Lane Grp Cap(c), veh/h       | 213  | 970      | 596      | 507  | 494      | 441  |      |      |  |      |
| V/C Ratio(X)                 | 0.78 | 0.22     | 0.70     | 0.77 | 0.40     | 0.44 |      |      |  |      |
| Avail Cap(c_a), veh/h        | 408  | 1398     | 825      | 702  | 494      | 441  |      |      |  |      |
| HCM Platoon Ratio            | 1.00 | 1.00     | 1.00     | 1.00 | 1.00     | 1.00 |      |      |  |      |
| Upstream Filter(I)           | 1.00 | 1.00     | 1.00     | 1.00 | 1.00     | 1.00 |      |      |  |      |
| Uniform Delay (d), s/veh     | 20.6 | 5.9      | 14.5     | 14.9 | 14.2     | 14.4 |      |      |  |      |
| Incr Delay (d2), s/veh       | 6.1  | 0.1      | 1.6      | 3.4  | 2.4      | 3.1  |      |      |  |      |
| Initial Q Delay(d3),s/veh    | 0.0  | 0.0      | 0.0      | 0.0  | 0.0      | 0.0  |      |      |  |      |
| %ile BackOfQ(50%),veh/ln     | 2.5  | 1.5      | 5.2      | 5.1  | 2.5      | 4.8  |      |      |  |      |
| LnGrp Delay(d),s/veh         | 26.7 | 6.0      | 16.1     | 18.3 | 16.7     | 17.5 |      |      |  |      |
| LnGrp LOS                    | C    | A        | В        | В    | В        | В    |      |      |  |      |
| Approach Vol, veh/h          |      | 384      | 809      |      | 391      |      |      |      |  |      |
| Approach Delay, s/veh        |      | 15.0     | 17.2     |      | 17.1     |      |      |      |  |      |
| Approach LOS                 |      | В        | В        |      | В        |      |      |      |  |      |
| Timer                        | 1    | 2        | 3        | 4    | 5        | 6    | 7    | 8    |  |      |
| Assigned Phs                 |      |          |          | 4    |          | 6    | 7    | 8    |  |      |
| Phs Duration (G+Y+Rc), s     |      |          |          | 30.5 |          | 18.0 | 10.5 | 20.0 |  |      |
| Change Period (Y+Rc), s      |      |          |          | 4.5  |          | 4.5  | 4.5  | 4.5  |  |      |
| Max Green Setting (Gmax), s  |      |          |          | 37.5 |          | 13.5 | 11.5 | 21.5 |  |      |
| Max Q Clear Time (g_c+l1), s |      |          |          | 5.1  |          | 6.8  | 6.5  | 12.7 |  |      |
| Green Ext Time (p_c), s      |      |          |          | 1.3  |          | 0.7  | 0.2  | 2.8  |  |      |
| Intersection Summary         |      |          |          |      |          |      |      |      |  |      |
| HCM 2010 Ctrl Delay          |      |          | 16.6     |      |          |      |      |      |  |      |
| HCM 2010 LOS                 |      |          | В        |      |          |      |      |      |  |      |
|                              |      |          |          |      |          |      |      |      |  |      |

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|-------------------------------|------------|----------|-------|-------|-------------|------------|---------|----------|----------|----------|----------|------|
| Movement                      | EBL        | EBT      | EBR   | WBL   | WBT         | WBR        | NBL     | NBT      | NBR      | SBL      | SBT      | SBR  |
| Lane Configurations           | *          | <b>†</b> | 7     | Ţ     | ĵ.          |            |         | ર્ન      | 7        |          | ર્ન      | 7    |
| Traffic Volume (vph)          | 11         | 492      | 256   | 9     | 667         | 28         | 527     | 25       | 3        | 46       | 23       | 5    |
| Future Volume (vph)           | 11         | 492      | 256   | 9     | 667         | 28         | 527     | 25       | 3        | 46       | 23       | 5    |
| Ideal Flow (vphpl)            | 1900       | 1900     | 1900  | 1900  | 1900        | 1900       | 1900    | 1900     | 1900     | 1900     | 1900     | 1900 |
| Total Lost time (s)           | 4.5        | 4.5      | 4.5   | 4.5   | 4.5         |            |         | 4.5      | 4.5      |          | 4.5      | 4.5  |
| Lane Util. Factor             | 1.00       | 1.00     | 1.00  | 1.00  | 1.00        |            |         | 1.00     | 1.00     |          | 1.00     | 1.00 |
| Frt                           | 1.00       | 1.00     | 0.85  | 1.00  | 0.99        |            |         | 1.00     | 0.85     |          | 1.00     | 0.85 |
| Flt Protected                 | 0.95       | 1.00     | 1.00  | 0.95  | 1.00        |            |         | 0.95     | 1.00     |          | 0.97     | 1.00 |
| Satd. Flow (prot)             | 1612       | 1696     | 1442  | 1543  | 1614        |            |         | 1778     | 1583     |          | 1751     | 1538 |
| Flt Permitted                 | 0.95       | 1.00     | 1.00  | 0.95  | 1.00        |            |         | 0.95     | 1.00     |          | 0.97     | 1.00 |
| Satd. Flow (perm)             | 1612       | 1696     | 1442  | 1543  | 1614        |            |         | 1778     | 1583     |          | 1751     | 1538 |
| Peak-hour factor, PHF         | 0.96       | 0.96     | 0.96  | 0.96  | 0.96        | 0.96       | 0.96    | 0.96     | 0.96     | 0.96     | 0.96     | 0.96 |
| Adj. Flow (vph)               | 11         | 512      | 267   | 9     | 695         | 29         | 549     | 26       | 3        | 48       | 24       | 5    |
| RTOR Reduction (vph)          | 0          | 0        | 147   | 0     | 1           | 0          | 0       | 0        | 2        | 0        | 0        | 5    |
| Lane Group Flow (vph)         | 11         | 513      | 120   | 9     | 723         | 0          | 0       | 575      | 1        | 0        | 72       | 0    |
| Heavy Vehicles (%)            | 12%        | 12%      | 12%   | 17%   | 17%         | 17%        | 2%      | 2%       | 2%       | 5%       | 5%       | 5%   |
| Turn Type                     | Prot       | NA       | Perm  | Prot  | NA          |            | Split   | NA       | Perm     | Split    | NA       | Perm |
| Protected Phases              | 7          | 4        |       | 3     | 8           |            | 5       | 5        |          | 6        | 6        |      |
| Permitted Phases              |            |          | 4     |       |             |            |         |          | 5        |          |          | 6    |
| Actuated Green, G (s)         | 0.9        | 51.7     | 51.7  | 0.9   | 51.7        |            |         | 38.6     | 38.6     |          | 5.5      | 5.5  |
| Effective Green, g (s)        | 0.9        | 51.7     | 51.7  | 0.9   | 51.7        |            |         | 38.6     | 38.6     |          | 5.5      | 5.5  |
| Actuated g/C Ratio            | 0.01       | 0.45     | 0.45  | 0.01  | 0.45        |            |         | 0.34     | 0.34     |          | 0.05     | 0.05 |
| Clearance Time (s)            | 4.5        | 4.5      | 4.5   | 4.5   | 4.5         |            |         | 4.5      | 4.5      |          | 4.5      | 4.5  |
| Vehicle Extension (s)         | 3.0        | 3.0      | 3.0   | 3.0   | 3.0         |            |         | 3.0      | 3.0      |          | 3.0      | 3.0  |
| Lane Grp Cap (vph)            | 12         | 764      | 649   | 12    | 727         |            |         | 598      | 532      |          | 83       | 73   |
| v/s Ratio Prot                | c0.01      | 0.30     |       | 0.01  | c0.45       |            |         | c0.32    |          |          | c0.04    |      |
| v/s Ratio Perm                |            |          | 0.08  |       |             |            |         |          | 0.00     |          |          | 0.00 |
| v/c Ratio                     | 0.92       | 0.67     | 0.19  | 0.75  | 0.99        |            |         | 0.96     | 0.00     |          | 0.87     | 0.00 |
| Uniform Delay, d1             | 56.9       | 24.8     | 18.9  | 56.8  | 31.4        |            |         | 37.3     | 25.3     |          | 54.2     | 52.0 |
| Progression Factor            | 1.00       | 1.00     | 1.00  | 1.00  | 1.00        |            |         | 1.00     | 1.00     |          | 1.00     | 1.00 |
| Incremental Delay, d2         | 212.2      | 4.7      | 0.6   | 128.3 | 32.0        |            |         | 27.3     | 0.0      |          | 56.5     | 0.0  |
| Delay (s)                     | 269.0      | 29.5     | 19.5  | 185.1 | 63.4        |            |         | 64.6     | 25.3     |          | 110.8    | 52.0 |
| Level of Service              | F          | С        | В     | F     | E           |            |         | Е        | С        |          | F        | D    |
| Approach Delay (s)            |            | 29.4     |       |       | 64.9        |            |         | 64.4     |          |          | 107.0    |      |
| Approach LOS                  |            | С        |       |       | E           |            |         | E        |          |          | F        |      |
| Intersection Summary          |            |          |       |       |             |            |         |          |          |          |          |      |
| HCM 2000 Control Delay        |            |          | 53.4  | Н     | CM 2000     | Level of S | Service |          | D        |          |          |      |
| HCM 2000 Volume to Capa       | city ratio |          | 0.97  |       |             |            |         |          |          |          |          |      |
| Actuated Cycle Length (s)     |            |          | 114.7 |       | um of lost  |            |         |          | 18.0     |          |          |      |
| Intersection Capacity Utiliza | ation      |          | 82.7% | IC    | CU Level of | of Service |         |          | Е        |          |          |      |
| Analysis Period (min)         |            |          | 15    |       |             |            |         |          |          |          |          |      |
| c Critical Lane Group         |            |          |       |       |             |            |         |          |          |          |          |      |

# 8: Airline Hwy (SR 25)/Pinnacles Nat Pk Hwy (SR 25) & Tres Pinos Rd/Sunnslope Rd

|                              | ۶     | <b>→</b> | •    | •     | <b>←</b> | •    | 1    | <b>†</b> | <i>&gt;</i> | <b>/</b> | <b>+</b> | ✓    |
|------------------------------|-------|----------|------|-------|----------|------|------|----------|-------------|----------|----------|------|
| Movement                     | EBL   | EBT      | EBR  | WBL   | WBT      | WBR  | NBL  | NBT      | NBR         | SBL      | SBT      | SBR  |
| Lane Configurations          | 14.54 | <b>^</b> | 7    | ሻ     | <b>^</b> | 7    | ሻሻ   | ተተኈ      |             | ሻሻ       | ተተተ      | 7    |
| Traffic Volume (veh/h)       | 234   | 227      | 116  | 149   | 381      | 193  | 166  | 552      | 66          | 169      | 407      | 181  |
| Future Volume (veh/h)        | 234   | 227      | 116  | 149   | 381      | 193  | 166  | 552      | 66          | 169      | 407      | 181  |
| Number                       | 7     | 4        | 14   | 3     | 8        | 18   | 5    | 2        | 12          | 1        | 6        | 16   |
| Initial Q (Qb), veh          | 0     | 0        | 0    | 0     | 0        | 0    | 0    | 0        | 0           | 0        | 0        | 0    |
| Ped-Bike Adj(A_pbT)          | 1.00  |          | 0.98 | 1.00  |          | 0.96 | 1.00 |          | 1.00        | 1.00     |          | 1.00 |
| Parking Bus, Adj             | 1.00  | 1.00     | 1.00 | 1.00  | 1.00     | 1.00 | 1.00 | 1.00     | 1.00        | 1.00     | 1.00     | 1.00 |
| Adj Sat Flow, veh/h/ln       | 1863  | 1863     | 1863 | 1863  | 1863     | 1863 | 1863 | 1863     | 1900        | 1845     | 1845     | 1845 |
| Adj Flow Rate, veh/h         | 257   | 249      | 127  | 164   | 419      | 212  | 182  | 607      | 73          | 186      | 447      | 199  |
| Adj No. of Lanes             | 2     | 2        | 1    | 1     | 2        | 1    | 2    | 3        | 0           | 2        | 3        | 1    |
| Peak Hour Factor             | 0.91  | 0.91     | 0.91 | 0.91  | 0.91     | 0.91 | 0.91 | 0.91     | 0.91        | 0.91     | 0.91     | 0.91 |
| Percent Heavy Veh, %         | 2     | 2        | 2    | 2     | 2        | 2    | 2    | 2        | 2           | 3        | 3        | 3    |
| Cap, veh/h                   | 307   | 796      | 477  | 161   | 802      | 346  | 277  | 1406     | 167         | 280      | 1546     | 619  |
| Arrive On Green              | 0.09  | 0.23     | 0.23 | 0.09  | 0.23     | 0.23 | 0.08 | 0.31     | 0.31        | 0.08     | 0.31     | 0.31 |
| Sat Flow, veh/h              | 3442  | 3539     | 1554 | 1774  | 3539     | 1525 | 3442 | 4607     | 548         | 3408     | 5036     | 1562 |
| Grp Volume(v), veh/h         | 257   | 249      | 127  | 164   | 419      | 212  | 182  | 445      | 235         | 186      | 447      | 199  |
| Grp Sat Flow(s),veh/h/ln     | 1721  | 1770     | 1554 | 1774  | 1770     | 1525 | 1721 | 1695     | 1765        | 1704     | 1679     | 1562 |
| Q Serve(g_s), s              | 4.5   | 3.6      | 3.7  | 5.5   | 6.3      | 7.6  | 3.1  | 6.4      | 6.5         | 3.2      | 4.1      | 5.3  |
| Cycle Q Clear(g_c), s        | 4.5   | 3.6      | 3.7  | 5.5   | 6.3      | 7.6  | 3.1  | 6.4      | 6.5         | 3.2      | 4.1      | 5.3  |
| Prop In Lane                 | 1.00  |          | 1.00 | 1.00  |          | 1.00 | 1.00 |          | 0.31        | 1.00     |          | 1.00 |
| Lane Grp Cap(c), veh/h       | 307   | 796      | 477  | 161   | 802      | 346  | 277  | 1034     | 539         | 280      | 1546     | 619  |
| V/C Ratio(X)                 | 0.84  | 0.31     | 0.27 | 1.02  | 0.52     | 0.61 | 0.66 | 0.43     | 0.44        | 0.66     | 0.29     | 0.32 |
| Avail Cap(c_a), veh/h        | 307   | 1051     | 589  | 161   | 1057     | 455  | 284  | 1034     | 539         | 281      | 1546     | 619  |
| HCM Platoon Ratio            | 1.00  | 1.00     | 1.00 | 1.00  | 1.00     | 1.00 | 1.00 | 1.00     | 1.00        | 1.00     | 1.00     | 1.00 |
| Upstream Filter(I)           | 1.00  | 1.00     | 1.00 | 1.00  | 1.00     | 1.00 | 1.00 | 1.00     | 1.00        | 1.00     | 1.00     | 1.00 |
| Uniform Delay (d), s/veh     | 27.2  | 19.6     | 15.9 | 27.6  | 20.6     | 21.1 | 27.1 | 16.8     | 16.9        | 27.0     | 16.0     | 12.7 |
| Incr Delay (d2), s/veh       | 18.2  | 0.2      | 0.3  | 76.0  | 0.5      | 1.8  | 5.3  | 1.3      | 2.6         | 5.7      | 0.5      | 1.4  |
| Initial Q Delay(d3),s/veh    | 0.0   | 0.0      | 0.0  | 0.2   | 0.0      | 0.0  | 0.0  | 0.0      | 0.0         | 0.0      | 0.0      | 0.0  |
| %ile BackOfQ(50%),veh/ln     | 2.9   | 1.8      | 1.6  | 6.0   | 3.1      | 3.3  | 1.7  | 3.2      | 3.5         | 1.7      | 2.0      | 2.5  |
| LnGrp Delay(d),s/veh         | 45.4  | 19.8     | 16.2 | 103.8 | 21.1     | 22.8 | 32.4 | 18.2     | 19.5        | 32.7     | 16.5     | 14.0 |
| LnGrp LOS                    | D     | В        | В    | F     | С        | С    | С    | В        | В           | С        | В        | В    |
| Approach Vol, veh/h          |       | 633      |      |       | 795      |      |      | 862      |             |          | 832      |      |
| Approach Delay, s/veh        |       | 29.5     |      |       | 38.6     |      |      | 21.5     |             |          | 19.5     |      |
| Approach LOS                 |       | C        |      |       | D        |      |      | C C      |             |          | В        |      |
|                              |       |          |      |       |          |      |      |          |             |          |          |      |
| Timer                        | 1     | 2        | 3    | 4     | 5        | 6    | 7    | 8        |             |          |          |      |
| Assigned Phs                 | 1     | 2        | 3    | 4     | 5        | 6    | 7    | 8        |             |          |          |      |
| Phs Duration (G+Y+Rc), s     | 9.5   | 23.0     | 10.0 | 18.1  | 9.4      | 23.1 | 9.9  | 18.2     |             |          |          |      |
| Change Period (Y+Rc), s      | 4.5   | 4.5      | 4.5  | 4.5   | 4.5      | 4.5  | 4.5  | 4.5      |             |          |          |      |
| Max Green Setting (Gmax), s  | 5.0   | 18.5     | 5.5  | 18.0  | 5.0      | 18.5 | 5.4  | 18.1     |             |          |          |      |
| Max Q Clear Time (g_c+I1), s | 5.2   | 8.5      | 7.5  | 5.7   | 5.1      | 7.3  | 6.5  | 9.6      |             |          |          |      |
| Green Ext Time (p_c), s      | 0.0   | 3.1      | 0.0  | 1.6   | 0.0      | 2.8  | 0.0  | 2.3      |             |          |          |      |
| Intersection Summary         |       |          |      |       |          |      |      |          |             |          |          |      |
| HCM 2010 Ctrl Delay          |       |          | 26.9 |       |          |      |      |          |             |          |          |      |
| HCM 2010 LOS                 |       |          | С    |       |          |      |      |          |             |          |          |      |

Lico Subdivision Keith Higgins Traffic Engineer

|                              | ۶    | <b>→</b> | •    | •    | <b>←</b> | •    | •    | <b>†</b> | ~    | <b>/</b> | ļ    | ✓        |
|------------------------------|------|----------|------|------|----------|------|------|----------|------|----------|------|----------|
| Movement                     | EBL  | EBT      | EBR  | WBL  | WBT      | WBR  | NBL  | NBT      | NBR  | SBL      | SBT  | SBR      |
| Lane Configurations          | J.   | ĵ.       |      | *    | ĵ»       |      | J.   | <b></b>  | 7    | Ť        | f)   |          |
| Traffic Volume (veh/h)       | 33   | 153      | 38   | 157  | 154      | 142  | 67   | 116      | 177  | 103      | 46   | 4        |
| Future Volume (veh/h)        | 33   | 153      | 38   | 157  | 154      | 142  | 67   | 116      | 177  | 103      | 46   | 4        |
| Number                       | 7    | 4        | 14   | 3    | 8        | 18   | 5    | 2        | 12   | 1        | 6    | 16       |
| Initial Q (Qb), veh          | 0    | 0        | 0    | 0    | 0        | 0    | 0    | 0        | 0    | 0        | 0    | 0        |
| Ped-Bike Adj(A_pbT)          | 1.00 |          | 0.73 | 1.00 |          | 0.89 | 1.00 |          | 0.99 | 1.00     |      | 0.99     |
| Parking Bus, Adj             | 1.00 | 1.00     | 1.00 | 1.00 | 1.00     | 1.00 | 1.00 | 1.00     | 1.00 | 1.00     | 1.00 | 1.00     |
| Adj Sat Flow, veh/h/ln       | 1863 | 1863     | 1900 | 1863 | 1863     | 1900 | 1863 | 1863     | 1863 | 1863     | 1863 | 1900     |
| Adj Flow Rate, veh/h         | 43   | 201      | 50   | 207  | 203      | 187  | 88   | 153      | 233  | 136      | 61   | 5        |
| Adj No. of Lanes             | 1    | 1        | 0    | 1    | 1        | 0    | 1    | 1        | 1    | 1        | 1    | 0        |
| Peak Hour Factor             | 0.76 | 0.76     | 0.76 | 0.76 | 0.76     | 0.76 | 0.76 | 0.76     | 0.76 | 0.76     | 0.76 | 0.76     |
| Percent Heavy Veh, %         | 2    | 2        | 2    | 2    | 2        | 2    | 2    | 2        | 2    | 2        | 2    | 2        |
| Cap, veh/h                   | 72   | 332      | 82   | 236  | 286      | 263  | 113  | 492      | 416  | 167      | 500  | 41       |
| Arrive On Green              | 0.04 | 0.25     | 0.25 | 0.13 | 0.34     | 0.34 | 0.06 | 0.26     | 0.26 | 0.09     | 0.29 | 0.29     |
| Sat Flow, veh/h              | 1774 | 1332     | 331  | 1774 | 838      | 772  | 1774 | 1863     | 1574 | 1774     | 1697 | 139      |
| Grp Volume(v), veh/h         | 43   | 0        | 251  | 207  | 0        | 390  | 88   | 153      | 233  | 136      | 0    | 66       |
| Grp Sat Flow(s),veh/h/ln     | 1774 | 0        | 1664 | 1774 | 0        | 1611 | 1774 | 1863     | 1574 | 1774     | 0    | 1836     |
| Q Serve(g_s), s              | 1.6  | 0.0      | 9.2  | 7.9  | 0.0      | 14.6 | 3.4  | 4.6      | 8.8  | 5.2      | 0.0  | 1.8      |
| Cycle Q Clear(g_c), s        | 1.6  | 0.0      | 9.2  | 7.9  | 0.0      | 14.6 | 3.4  | 4.6      | 8.8  | 5.2      | 0.0  | 1.8      |
| Prop In Lane                 | 1.00 |          | 0.20 | 1.00 |          | 0.48 | 1.00 |          | 1.00 | 1.00     |      | 0.08     |
| Lane Grp Cap(c), veh/h       | 72   | 0        | 414  | 236  | 0        | 550  | 113  | 492      | 416  | 167      | 0    | 541      |
| V/C Ratio(X)                 | 0.60 | 0.00     | 0.61 | 0.88 | 0.00     | 0.71 | 0.78 | 0.31     | 0.56 | 0.82     | 0.00 | 0.12     |
| Avail Cap(c_a), veh/h        | 131  | 0        | 433  | 236  | 0        | 550  | 159  | 492      | 416  | 167      | 0    | 541      |
| HCM Platoon Ratio            | 1.00 | 1.00     | 1.00 | 1.00 | 1.00     | 1.00 | 1.00 | 1.00     | 1.00 | 1.00     | 1.00 | 1.00     |
| Upstream Filter(I)           | 1.00 | 0.00     | 1.00 | 1.00 | 0.00     | 1.00 | 1.00 | 1.00     | 1.00 | 1.00     | 0.00 | 1.00     |
| Uniform Delay (d), s/veh     | 32.7 | 0.0      | 23.0 | 29.5 | 0.0      | 19.8 | 31.9 | 20.4     | 22.0 | 30.8     | 0.0  | 17.9     |
| Incr Delay (d2), s/veh       | 7.7  | 0.0      | 2.3  | 29.1 | 0.0      | 4.2  | 14.8 | 1.6      | 5.4  | 26.0     | 0.0  | 0.5      |
| Initial Q Delay(d3),s/veh    | 0.0  | 0.0      | 0.0  | 0.0  | 0.0      | 0.0  | 0.0  | 0.0      | 0.0  | 0.0      | 0.0  | 0.0      |
| %ile BackOfQ(50%),veh/ln     | 1.0  | 0.0      | 4.5  | 5.8  | 0.0      | 7.0  | 2.1  | 2.6      | 4.4  | 3.7      | 0.0  | 1.0      |
| LnGrp Delay(d),s/veh         | 40.3 | 0.0      | 25.3 | 58.5 | 0.0      | 24.1 | 46.7 | 22.0     | 27.3 | 56.8     | 0.0  | 18.3     |
| LnGrp LOS                    | D    |          | С    | E    |          | С    | D    | С        | С    | E        |      | <u>B</u> |
| Approach Vol, veh/h          |      | 294      |      |      | 597      |      |      | 474      |      |          | 202  |          |
| Approach Delay, s/veh        |      | 27.5     |      |      | 36.0     |      |      | 29.2     |      |          | 44.2 |          |
| Approach LOS                 |      | С        |      |      | D        |      |      | С        |      |          | D    |          |
| Timer                        | 1    | 2        | 3    | 4    | 5        | 6    | 7    | 8        |      |          |      |          |
| Assigned Phs                 | 1    | 2        | 3    | 4    | 5        | 6    | 7    | 8        |      |          |      |          |
| Phs Duration (G+Y+Rc), s     | 11.0 | 22.8     | 13.7 | 21.7 | 8.9      | 24.9 | 7.3  | 28.1     |      |          |      |          |
| Change Period (Y+Rc), s      | 4.5  | 4.5      | 4.5  | 4.5  | 4.5      | 4.5  | 4.5  | 4.5      |      |          |      |          |
| Max Green Setting (Gmax), s  | 6.5  | 18.3     | 9.2  | 18.0 | 6.2      | 18.6 | 5.1  | 22.1     |      |          |      |          |
| Max Q Clear Time (g_c+l1), s | 7.2  | 10.8     | 9.9  | 11.2 | 5.4      | 3.8  | 3.6  | 16.6     |      |          |      |          |
| Green Ext Time (p_c), s      | 0.0  | 1.0      | 0.0  | 0.8  | 0.0      | 0.2  | 0.0  | 1.2      |      |          |      |          |
| Intersection Summary         |      |          |      |      |          |      |      |          |      |          |      |          |
| HCM 2010 Ctrl Delay          |      |          | 33.4 |      |          |      |      |          |      |          |      |          |
| HCM 2010 LOS                 |      |          | С    |      |          |      |      |          |      |          |      |          |

HCM 2010 AWSC Existing PM

| ntersection              |      |
|--------------------------|------|
| ntersection Delay, s/veh | 11.4 |
| ntersection LOS          | В    |

| Intersection LOS           | В    |          |      |      |          |      |      |      |      |      |          |      |
|----------------------------|------|----------|------|------|----------|------|------|------|------|------|----------|------|
|                            |      |          |      |      |          |      |      |      |      |      |          |      |
| Movement                   | EBL  | EBT      | EBR  | WBL  | WBT      | WBR  | NBL  | NBT  | NBR  | SBL  | SBT      | SBR  |
| Lane Configurations        | ¥    | <b>†</b> | 7    | ¥    | <b>†</b> | 7    | Ť    | ĵ»   |      | J.   | <b>†</b> | 7    |
| Traffic Vol, veh/h         | 51   | 188      | 206  | 4    | 134      | 51   | 101  | 30   | 2    | 76   | 76       | 80   |
| Future Vol, veh/h          | 51   | 188      | 206  | 4    | 134      | 51   | 101  | 30   | 2    | 76   | 76       | 80   |
| Peak Hour Factor           | 0.97 | 0.97     | 0.97 | 0.97 | 0.97     | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97     | 0.97 |
| Heavy Vehicles, %          | 2    | 2        | 2    | 2    | 2        | 2    | 2    | 2    | 2    | 2    | 2        | 2    |
| Mvmt Flow                  | 53   | 194      | 212  | 4    | 138      | 53   | 104  | 31   | 2    | 78   | 78       | 82   |
| Number of Lanes            | 1    | 1        | 1    | 1    | 1        | 1    | 1    | 1    | 0    | 1    | 1        | 1    |
| Approach                   | EB   |          |      | WB   |          |      | NB   |      |      | SB   |          |      |
| Opposing Approach          | WB   |          |      | EB   |          |      | SB   |      |      | NB   |          |      |
| Opposing Lanes             | 3    |          |      | 3    |          |      | 3    |      |      | 2    |          |      |
| Conflicting Approach Left  | SB   |          |      | NB   |          |      | EB   |      |      | WB   |          |      |
| Conflicting Lanes Left     | 3    |          |      | 2    |          |      | 3    |      |      | 3    |          |      |
| Conflicting Approach Right | NB   |          |      | SB   |          |      | WB   |      |      | EB   |          |      |
| Conflicting Lanes Right    | 2    |          |      | 3    |          |      | 3    |      |      | 3    |          |      |
| HCM Control Delay          | 11.6 |          |      | 11.4 |          |      | 11.8 |      |      | 10.7 |          |      |
| HCM LOS                    | В    |          |      | В    |          |      | В    |      |      | В    |          |      |

| Lane                   | NBLn1 | NBLn2 | EBLn1 | EBLn2 | EBLn3 | WBLn1 | WBLn2 | WBLn3 | SBLn1 | SBLn2 | SBLn3 |
|------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Vol Left, %            | 100%  | 0%    | 100%  | 0%    | 0%    | 100%  | 0%    | 0%    | 100%  | 0%    | 0%    |
| Vol Thru, %            | 0%    | 94%   | 0%    | 100%  | 0%    | 0%    | 100%  | 0%    | 0%    | 100%  | 0%    |
| Vol Right, %           | 0%    | 6%    | 0%    | 0%    | 100%  | 0%    | 0%    | 100%  | 0%    | 0%    | 100%  |
| Sign Control           | Stop  |
| Traffic Vol by Lane    | 101   | 32    | 51    | 188   | 206   | 4     | 134   | 51    | 76    | 76    | 80    |
| LT Vol                 | 101   | 0     | 51    | 0     | 0     | 4     | 0     | 0     | 76    | 0     | 0     |
| Through Vol            | 0     | 30    | 0     | 188   | 0     | 0     | 134   | 0     | 0     | 76    | 0     |
| RT Vol                 | 0     | 2     | 0     | 0     | 206   | 0     | 0     | 51    | 0     | 0     | 80    |
| Lane Flow Rate         | 104   | 33    | 53    | 194   | 212   | 4     | 138   | 53    | 78    | 78    | 82    |
| Geometry Grp           | 8     | 8     | 8     | 8     | 8     | 8     | 8     | 8     | 8     | 8     | 8     |
| Degree of Util (X)     | 0.216 | 0.063 | 0.1   | 0.342 | 0.333 | 0.008 | 0.263 | 0.09  | 0.159 | 0.148 | 0.14  |
| Departure Headway (Hd) | 7.465 | 6.921 | 6.861 | 6.357 | 5.651 | 7.37  | 6.864 | 6.157 | 7.32  | 6.818 | 6.116 |
| Convergence, Y/N       | Yes   |
| Cap                    | 479   | 515   | 521   | 564   | 633   | 483   | 521   | 578   | 488   | 523   | 583   |
| Service Time           | 5.24  | 4.696 | 4.624 | 4.12  | 3.414 | 5.147 | 4.641 | 3.934 | 5.093 | 4.591 | 3.888 |
| HCM Lane V/C Ratio     | 0.217 | 0.064 | 0.102 | 0.344 | 0.335 | 0.008 | 0.265 | 0.092 | 0.16  | 0.149 | 0.141 |
| HCM Control Delay      | 12.3  | 10.2  | 10.4  | 12.4  | 11.2  | 10.2  | 12.1  | 9.5   | 11.5  | 10.8  | 9.9   |
| HCM Lane LOS           | В     | В     | В     | В     | В     | В     | В     | Α     | В     | В     | Α     |
| HCM 95th-tile Q        | 0.8   | 0.2   | 0.3   | 1.5   | 1.5   | 0     | 1     | 0.3   | 0.6   | 0.5   | 0.5   |

| Intersection           |        |          |        |        |          |      |        |          |       |        |          |       |        |
|------------------------|--------|----------|--------|--------|----------|------|--------|----------|-------|--------|----------|-------|--------|
| Int Delay, s/veh       | 2.5    |          |        |        |          |      |        |          |       |        |          |       |        |
| Movement               | EBL    | EBT      | EBR    | WBL    | WBT      | WBR  | NBL    | NBT      | NBR   | SBL    | SBT      | SBR   |        |
| Lane Configurations    | ች      | <b>†</b> | 7      | ች      | <b>†</b> | 7    | *      | <b>↑</b> | 7     |        | <b>↑</b> | 1     |        |
| Traffic Vol, veh/h     | 62     | 410      | 61     | 34     | 270      | 18   | 28     | 2        | 26    | 9      | 2        | 34    |        |
| Future Vol, veh/h      | 62     | 410      | 61     | 34     | 270      | 18   | 28     | 2        | 26    | 9      | 2        | 34    |        |
| Conflicting Peds, #/hr | 0      | 0        | 0      | 0      | 0        | 0    | 0      | 0        | 0     | 0      | 0        | 0     |        |
| Sign Control           | Free   | Free     | Free   | Free   | Free     | Free | Stop   | Stop     | Stop  | Stop   | Stop     | Stop  |        |
| RT Channelized         | -      | -        | None   | -      | -        | None | -      | -        | None  | -      | -        | None  |        |
| Storage Length         | 320    | -        | 505    | 360    | -        | 195  | 60     | -        | 0     | 100    | -        | 100   |        |
| Veh in Median Storage  | ,# -   | 0        | -      | -      | 0        | -    | -      | 0        | _     | -      | 0        | -     |        |
| Grade, %               | -      | 0        | -      | -      | 0        | -    | -      | 0        | -     | -      | 0        | -     |        |
| Peak Hour Factor       | 95     | 95       | 95     | 95     | 95       | 95   | 95     | 95       | 95    | 95     | 95       | 95    |        |
| Heavy Vehicles, %      | 2      | 2        | 2      | 2      | 2        | 2    | 2      | 2        | 2     | 2      | 2        | 2     |        |
| Mvmt Flow              | 65     | 432      | 64     | 36     | 284      | 19   | 29     | 2        | 27    | 9      | 2        | 36    |        |
|                        |        |          |        |        |          |      |        |          |       |        |          |       |        |
| Major/Minor N          | Major1 |          |        | Major2 |          | ľ    | Minor1 |          | 1     | Minor2 |          |       |        |
| Conflicting Flow All   | 303    | 0        | 0      | 496    | 0        | 0    | 947    | 937      | 432   | 965    | 982      | 284   |        |
| Stage 1                | -      | _        | -      | -      | _        | -    | 562    | 562      | -     | 356    | 356      |       |        |
| Stage 2                | _      | _        | _      | _      | _        | _    | 385    | 375      | _     | 609    | 626      | _     |        |
| Critical Hdwy          | 4.12   | _        | _      | 4.12   | _        | _    | 7.12   | 6.52     | 6.22  | 7.12   | 6.52     | 6.22  |        |
| Critical Hdwy Stg 1    | -      | _        | _      |        | _        | _    | 6.12   | 5.52     | -     | 6.12   | 5.52     | -     |        |
| Critical Hdwy Stg 2    | _      | _        | _      | _      | _        | _    | 6.12   | 5.52     | _     | 6.12   | 5.52     | _     |        |
| Follow-up Hdwy         | 2.218  | _        | _      | 2.218  | _        | _    | 3.518  | 4.018    | 3.318 | 3.518  | 4.018    | 3.318 |        |
| Pot Cap-1 Maneuver     | 1258   | _        | _      | 1068   | _        | _    | 241    | 265      | 624   | 234    | 249      | 755   |        |
| Stage 1                | 1200   | _        | _      | 1000   | _        | _    | 512    | 510      | -     | 661    | 629      | -     |        |
| Stage 2                | _      | _        | _      | _      | _        | _    | 638    | 617      | _     | 482    | 477      | _     |        |
| Platoon blocked, %     |        | _        | _      |        | _        | _    | 000    | 011      |       | 102    |          |       |        |
| Mov Cap-1 Maneuver     | 1258   | _        | _      | 1068   | _        | _    | 213    | 243      | 624   | 208    | 228      | 755   |        |
| Mov Cap-2 Maneuver     | -      | _        | _      | -      | _        | _    | 213    | 243      | -     | 208    | 228      | -     |        |
| Stage 1                | _      | _        | _      | _      | _        | _    | 485    | 483      | _     | 627    | 608      | _     |        |
| Stage 2                | _      | _        | _      | _      | _        | _    | 585    | 596      | _     | 435    | 452      | _     |        |
|                        |        |          |        |        |          |      | 300    | 300      |       | .00    | .02      |       |        |
| Approach               | EB     |          |        | WB     |          |      | NB     |          |       | SB     |          |       |        |
| HCM Control Delay, s   | 0.9    |          |        | 0.9    |          |      | 18.1   |          |       | 13.1   |          |       |        |
| HCM LOS                | 0.0    |          |        | 0.0    |          |      | С      |          |       | В      |          |       |        |
|                        |        |          |        |        |          |      |        |          |       |        |          |       |        |
| Minor Lane/Major Mvm   | it I   | NBL n1   | NBLn21 | VBLn3  | EBL      | EBT  | EBR    | WBL      | WBT   | WBR    | SBL n1   | SBLn2 | SBL n3 |
| Capacity (veh/h)       |        | 213      | 243    | 624    | 1258     |      |        | 1068     | -     | -      |          | 228   | 755    |
| HCM Lane V/C Ratio     |        |          | 0.009  |        |          | _    |        | 0.034    | _     | _      |          | 0.009 |        |
| HCM Control Delay (s)  |        | 24.6     | 19.9   | 11     | 8        | _    | -      | 8.5      | _     | -      |          | 20.9  | 10     |
| HCM Lane LOS           |        | C        | C      | В      | A        | _    | _      | A        | _     | _      | C        | C     | В      |
| HCM 95th %tile Q(veh)  |        | 0.5      | 0      | 0.1    | 0.2      | -    | -      | 0.1      | -     | -      | 0.1      | 0     | 0.1    |
|                        |        |          |        |        |          |      |        |          |       |        |          |       |        |

| Intersection              |        |       |          |              |        |      |
|---------------------------|--------|-------|----------|--------------|--------|------|
| Int Delay, s/veh          | 1.9    |       |          |              |        |      |
| Movement                  | WBL    | WBR   | NBT      | NBR          | SBL    | SBT  |
| Lane Configurations       | ¥      |       | <b>f</b> |              |        | 4    |
| Traffic Vol, veh/h        | 7      | 29    | 95       | 11           | 33     | 138  |
| Future Vol, veh/h         | 7      | 29    | 95       | 11           | 33     | 138  |
| Conflicting Peds, #/hr    | 1      | 0     | 0        | 0            | 0      | 0    |
| Sign Control              | Stop   | Stop  | Free     | Free         | Free   | Free |
| RT Channelized            | _      | None  | -        |              | _      |      |
| Storage Length            | 0      | -     | -        | -            | _      | -    |
| Veh in Median Storage     |        | _     | 0        | _            | _      | 0    |
| Grade, %                  | 0      | _     | 0        | _            | _      | 0    |
| Peak Hour Factor          | 91     | 91    | 91       | 91           | 91     | 91   |
| Heavy Vehicles, %         | 6      | 6     | 2        | 2            | 3      | 3    |
| Mymt Flow                 | 8      | 32    | 104      | 12           | 36     | 152  |
| WWIIICI IOW               | U      | 02    | 104      | 12           | 00     | 102  |
|                           |        |       |          |              |        |      |
| Major/Minor N             | Minor1 |       | Major1   |              | Major2 |      |
| Conflicting Flow All      | 335    | 110   | 0        | 0            | 116    | 0    |
| Stage 1                   | 110    | -     | -        | -            | -      | -    |
| Stage 2                   | 225    | -     | -        | -            | -      | -    |
| Critical Hdwy             | 6.46   | 6.26  | -        | -            | 4.13   | -    |
| Critical Hdwy Stg 1       | 5.46   | -     | -        | -            | -      | -    |
| Critical Hdwy Stg 2       | 5.46   | -     | -        | -            | -      | -    |
| Follow-up Hdwy            | 3.554  | 3.354 | -        | -            | 2.227  | -    |
| Pot Cap-1 Maneuver        | 652    | 933   | -        | -            | 1466   | -    |
| Stage 1                   | 905    | -     | -        | -            | -      | -    |
| Stage 2                   | 803    | -     | -        | _            | -      | -    |
| Platoon blocked, %        |        |       | -        | -            |        | -    |
| Mov Cap-1 Maneuver        | 634    | 933   | _        | _            | 1466   | -    |
| Mov Cap-2 Maneuver        | 634    | -     | -        | -            | -      | -    |
| Stage 1                   | 881    | _     | _        | -            | _      | -    |
| Stage 2                   | 802    | _     | _        | -            | _      | _    |
| 5.tag5 2                  | 002    |       |          |              |        |      |
|                           |        |       |          |              |        |      |
| Approach                  | WB     |       | NB       |              | SB     |      |
| HCM Control Delay, s      | 9.4    |       | 0        |              | 1.5    |      |
| HCM LOS                   | Α      |       |          |              |        |      |
|                           |        |       |          |              |        |      |
| Minor Lane/Major Mvm      | nt     | NBT   | NRRV     | VBLn1        | SBL    | SBT  |
|                           | ıı     | NDT   |          | 855          | 1466   |      |
| Capacity (veh/h)          |        | -     | -        |              |        | -    |
| HCM Control Polov (a)     |        | -     |          | 0.046<br>9.4 |        | -    |
| HCM Lang LOS              |        | -     | -        |              | 7.5    | 0    |
| HCM OF the % tills O(vob) | ١      | -     | -        | Α            | Α      | Α    |
| HCM 95th %tile Q(veh)     | )      | -     | -        | 0.1          | 0.1    | -    |

|                              | •    | <b>→</b> | •    | •    | <b>—</b> | •     | •    | <b>†</b> | <i>&gt;</i> | <b>/</b> | <b>+</b> | ✓    |
|------------------------------|------|----------|------|------|----------|-------|------|----------|-------------|----------|----------|------|
| Movement                     | EBL  | EBT      | EBR  | WBL  | WBT      | WBR   | NBL  | NBT      | NBR         | SBL      | SBT      | SBR  |
| Lane Configurations          | ሻ    | <b>₽</b> |      | ሻ    | <b>₽</b> |       | ሻ    | <b>↑</b> | 7           | ሻ        | <b>•</b> | 7    |
| Traffic Volume (veh/h)       | 144  | 222      | 159  | 16   | 120      | 103   | 107  | 197      | 23          | 206      | 354      | 128  |
| Future Volume (veh/h)        | 144  | 222      | 159  | 16   | 120      | 103   | 107  | 197      | 23          | 206      | 354      | 128  |
| Number                       | 7    | 4        | 14   | 3    | 8        | 18    | 5    | 2        | 12          | 1        | 6        | 16   |
| Initial Q (Qb), veh          | 0    | 0        | 0    | 0    | 0        | 0     | 0    | 0        | 0           | 0        | 0        | 0    |
| Ped-Bike Adj(A_pbT)          | 1.00 |          | 1.00 | 1.00 |          | 1.00  | 1.00 |          | 1.00        | 1.00     |          | 1.00 |
| Parking Bus, Adj             | 1.00 | 1.00     | 1.00 | 1.00 | 1.00     | 1.00  | 1.00 | 1.00     | 1.00        | 1.00     | 1.00     | 1.00 |
| Adj Sat Flow, veh/h/ln       | 1863 | 1863     | 1900 | 1863 | 1863     | 1900  | 1863 | 1863     | 1863        | 1863     | 1863     | 1863 |
| Adj Flow Rate, veh/h         | 150  | 231      | 166  | 17   | 125      | 107   | 111  | 205      | 24          | 215      | 369      | 133  |
| Adj No. of Lanes             | 1    | 1        | 0    | 1    | 1        | 0     | 1    | 1        | 1           | 1        | 1        | 1    |
| Peak Hour Factor             | 0.96 | 0.96     | 0.96 | 0.96 | 0.96     | 0.96  | 0.96 | 0.96     | 0.96        | 0.96     | 0.96     | 0.96 |
| Percent Heavy Veh, %         | 2    | 2        | 2    | 2    | 2        | 2     | 2    | 2        | 2           | 2        | 2        | 2    |
| Cap, veh/h                   | 426  | 242      | 174  | 218  | 114      | 97    | 141  | 479      | 407         | 248      | 592      | 503  |
| Arrive On Green              | 0.24 | 0.24     | 0.24 | 0.12 | 0.12     | 0.12  | 0.08 | 0.26     | 0.26        | 0.14     | 0.32     | 0.32 |
| Sat Flow, veh/h              | 1774 | 1009     | 725  | 1774 | 928      | 794   | 1774 | 1863     | 1583        | 1774     | 1863     | 1583 |
| Grp Volume(v), veh/h         | 150  | 0        | 397  | 17   | 0        | 232   | 111  | 205      | 24          | 215      | 369      | 133  |
| Grp Sat Flow(s),veh/h/ln     | 1774 | 0        | 1735 | 1774 | 0        | 1723  | 1774 | 1863     | 1583        | 1774     | 1863     | 1583 |
| Q Serve(g_s), s              | 5.3  | 0.0      | 16.9 | 0.6  | 0.0      | 9.2   | 4.6  | 6.9      | 0.9         | 8.9      | 12.6     | 4.7  |
| Cycle Q Clear(g_c), s        | 5.3  | 0.0      | 16.9 | 0.6  | 0.0      | 9.2   | 4.6  | 6.9      | 0.9         | 8.9      | 12.6     | 4.7  |
| Prop In Lane                 | 1.00 |          | 0.42 | 1.00 |          | 0.46  | 1.00 |          | 1.00        | 1.00     |          | 1.00 |
| Lane Grp Cap(c), veh/h       | 426  | 0        | 416  | 218  | 0        | 211   | 141  | 479      | 407         | 248      | 592      | 503  |
| V/C Ratio(X)                 | 0.35 | 0.00     | 0.95 | 0.08 | 0.00     | 1.10  | 0.79 | 0.43     | 0.06        | 0.87     | 0.62     | 0.26 |
| Avail Cap(c_a), veh/h        | 426  | 0        | 416  | 218  | 0        | 211   | 177  | 479      | 407         | 248      | 592      | 503  |
| HCM Platoon Ratio            | 1.00 | 1.00     | 1.00 | 1.00 | 1.00     | 1.00  | 1.00 | 1.00     | 1.00        | 1.00     | 1.00     | 1.00 |
| Upstream Filter(I)           | 1.00 | 0.00     | 1.00 | 1.00 | 0.00     | 1.00  | 1.00 | 1.00     | 1.00        | 1.00     | 1.00     | 1.00 |
| Uniform Delay (d), s/veh     | 23.7 | 0.0      | 28.1 | 29.1 | 0.0      | 32.9  | 33.9 | 23.2     | 21.0        | 31.6     | 21.8     | 19.1 |
| Incr Delay (d2), s/veh       | 0.5  | 0.0      | 32.3 | 0.2  | 0.0      | 90.6  | 16.5 | 2.8      | 0.3         | 25.8     | 4.9      | 1.3  |
| Initial Q Delay(d3),s/veh    | 0.0  | 0.0      | 0.0  | 0.0  | 0.0      | 0.0   | 0.0  | 0.0      | 0.0         | 0.0      | 0.0      | 0.0  |
| %ile BackOfQ(50%),veh/ln     | 2.6  | 0.0      | 11.8 | 0.3  | 0.0      | 9.7   | 2.9  | 3.9      | 0.4         | 6.1      | 7.3      | 2.2  |
| LnGrp Delay(d),s/veh         | 24.2 | 0.0      | 60.4 | 29.3 | 0.0      | 123.5 | 50.4 | 26.0     | 21.3        | 57.4     | 26.7     | 20.3 |
| LnGrp LOS                    | С    |          | Е    | С    |          | F     | D    | С        | С           | Е        | С        | С    |
| Approach Vol, veh/h          |      | 547      |      |      | 249      |       |      | 340      |             |          | 717      |      |
| Approach Delay, s/veh        |      | 50.5     |      |      | 117.0    |       |      | 33.6     |             |          | 34.7     |      |
| Approach LOS                 |      | D        |      |      | F        |       |      | С        |             |          | С        |      |
| Timer                        | 1    | 2        | 3    | 4    | 5        | 6     | 7    | 8        |             |          |          |      |
| Assigned Phs                 | 1    | 2        |      | 4    | 5        | 6     |      | 8        |             |          |          |      |
| Phs Duration (G+Y+Rc), s     | 15.0 | 23.8     |      | 22.5 | 10.5     | 28.3  |      | 13.7     |             |          |          |      |
| Change Period (Y+Rc), s      | 4.5  | 4.5      |      | 4.5  | 4.5      | 4.5   |      | 4.5      |             |          |          |      |
| Max Green Setting (Gmax), s  | 10.5 | 19.3     |      | 18.0 | 7.5      | 22.3  |      | 9.2      |             |          |          |      |
| Max Q Clear Time (g_c+l1), s | 10.9 | 8.9      |      | 18.9 | 6.6      | 14.6  |      | 11.2     |             |          |          |      |
| Green Ext Time (p_c), s      | 0.0  | 0.8      |      | 0.0  | 0.0      | 1.7   |      | 0.0      |             |          |          |      |
| Intersection Summary         |      |          |      |      |          |       |      |          |             |          |          |      |
| HCM 2010 Ctrl Delay          |      |          | 50.2 |      |          |       |      |          |             |          |          |      |
| HCM 2010 LOS                 |      |          | D    |      |          |       |      |          |             |          |          |      |
| 110W 2010 LOG                |      |          |      |      |          |       |      |          |             |          |          |      |

|                              | ۶    | <b>→</b> | •    | •    | <b>←</b> | •    | •    | †    | ~    | <b>&gt;</b> | Ţ    |      |
|------------------------------|------|----------|------|------|----------|------|------|------|------|-------------|------|------|
| Movement                     | EBL  | EBT      | EBR  | WBL  | WBT      | WBR  | NBL  | NBT  | NBR  | SBL         | SBT  | SBR  |
| Lane Configurations          | 7    | ĵ.       |      | 7    | f)       |      |      | 4    |      |             | 4    |      |
| Traffic Volume (veh/h)       | 28   | 486      | 70   | 53   | 286      | 15   | 65   | 31   | 27   | 24          | 49   | 12   |
| Future Volume (veh/h)        | 28   | 486      | 70   | 53   | 286      | 15   | 65   | 31   | 27   | 24          | 49   | 12   |
| Number                       | 7    | 4        | 14   | 3    | 8        | 18   | 5    | 2    | 12   | 1           | 6    | 16   |
| Initial Q (Qb), veh          | 0    | 0        | 0    | 0    | 0        | 0    | 0    | 0    | 0    | 0           | 0    | 0    |
| Ped-Bike Adj(A_pbT)          | 1.00 |          | 1.00 | 1.00 |          | 1.00 | 1.00 |      | 1.00 | 1.00        |      | 1.00 |
| Parking Bus, Adj             | 1.00 | 1.00     | 1.00 | 1.00 | 1.00     | 1.00 | 1.00 | 1.00 | 1.00 | 1.00        | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln       | 1863 | 1863     | 1900 | 1863 | 1863     | 1900 | 1900 | 1863 | 1900 | 1900        | 1827 | 1900 |
| Adj Flow Rate, veh/h         | 33   | 565      | 81   | 62   | 333      | 17   | 76   | 36   | 31   | 28          | 57   | 14   |
| Adj No. of Lanes             | 1    | 1        | 0    | 1    | 1        | 0    | 0    | 1    | 0    | 0           | 1    | 0    |
| Peak Hour Factor             | 0.86 | 0.86     | 0.86 | 0.86 | 0.86     | 0.86 | 0.86 | 0.86 | 0.86 | 0.86        | 0.86 | 0.86 |
| Percent Heavy Veh, %         | 2    | 2        | 2    | 2    | 2        | 2    | 2    | 2    | 2    | 4           | 4    | 4    |
| Cap, veh/h                   | 63   | 609      | 87   | 97   | 705      | 36   | 333  | 155  | 108  | 191         | 355  | 77   |
| Arrive On Green              | 0.04 | 0.38     | 0.38 | 0.05 | 0.40     | 0.40 | 0.33 | 0.33 | 0.33 | 0.33        | 0.33 | 0.33 |
| Sat Flow, veh/h              | 1774 | 1594     | 229  | 1774 | 1757     | 90   | 720  | 472  | 330  | 337         | 1079 | 233  |
| Grp Volume(v), veh/h         | 33   | 0        | 646  | 62   | 0        | 350  | 143  | 0    | 0    | 99          | 0    | 0    |
| Grp Sat Flow(s),veh/h/ln     | 1774 | 0        | 1822 | 1774 | 0        | 1847 | 1522 | 0    | 0    | 1650        | 0    | 0    |
| Q Serve(g_s), s              | 1.1  | 0.0      | 19.5 | 2.0  | 0.0      | 8.1  | 1.3  | 0.0  | 0.0  | 0.0         | 0.0  | 0.0  |
| Cycle Q Clear(g_c), s        | 1.1  | 0.0      | 19.5 | 2.0  | 0.0      | 8.1  | 3.6  | 0.0  | 0.0  | 2.3         | 0.0  | 0.0  |
| Prop In Lane                 | 1.00 |          | 0.13 | 1.00 |          | 0.05 | 0.53 |      | 0.22 | 0.28        |      | 0.14 |
| Lane Grp Cap(c), veh/h       | 63   | 0        | 696  | 97   | 0        | 741  | 596  | 0    | 0    | 622         | 0    | 0    |
| V/C Ratio(X)                 | 0.52 | 0.00     | 0.93 | 0.64 | 0.00     | 0.47 | 0.24 | 0.00 | 0.00 | 0.16        | 0.00 | 0.00 |
| Avail Cap(c_a), veh/h        | 170  | 0        | 713  | 157  | 0        | 741  | 596  | 0    | 0    | 622         | 0    | 0    |
| HCM Platoon Ratio            | 1.00 | 1.00     | 1.00 | 1.00 | 1.00     | 1.00 | 1.00 | 1.00 | 1.00 | 1.00        | 1.00 | 1.00 |
| Upstream Filter(I)           | 1.00 | 0.00     | 1.00 | 1.00 | 0.00     | 1.00 | 1.00 | 0.00 | 0.00 | 1.00        | 0.00 | 0.00 |
| Uniform Delay (d), s/veh     | 27.2 | 0.0      | 17.0 | 26.6 | 0.0      | 12.7 | 14.1 | 0.0  | 0.0  | 13.7        | 0.0  | 0.0  |
| Incr Delay (d2), s/veh       | 6.5  | 0.0      | 18.2 | 6.8  | 0.0      | 0.5  | 1.0  | 0.0  | 0.0  | 0.5         | 0.0  | 0.0  |
| Initial Q Delay(d3),s/veh    | 0.0  | 0.0      | 0.0  | 0.0  | 0.0      | 0.0  | 0.0  | 0.0  | 0.0  | 0.0         | 0.0  | 0.0  |
| %ile BackOfQ(50%),veh/ln     | 0.6  | 0.0      | 13.2 | 1.1  | 0.0      | 4.2  | 1.8  | 0.0  | 0.0  | 1.2         | 0.0  | 0.0  |
| LnGrp Delay(d),s/veh         | 33.8 | 0.0      | 35.2 | 33.5 | 0.0      | 13.2 | 15.1 | 0.0  | 0.0  | 14.3        | 0.0  | 0.0  |
| LnGrp LOS                    | С    |          | D    | С    |          | В    | В    |      |      | В           |      |      |
| Approach Vol, veh/h          |      | 679      |      |      | 412      |      |      | 143  |      |             | 99   |      |
| Approach Delay, s/veh        |      | 35.1     |      |      | 16.2     |      |      | 15.1 |      |             | 14.3 |      |
| Approach LOS                 |      | D        |      |      | В        |      |      | В    |      |             | В    |      |
| Timer                        | 1    | 2        | 3    | 4    | 5        | 6    | 7    | 8    |      |             |      |      |
| Assigned Phs                 |      | 2        | 3    | 4    |          | 6    | 7    | 8    |      |             |      |      |
| Phs Duration (G+Y+Rc), s     |      | 23.4     | 7.6  | 26.5 |          | 23.4 | 6.5  | 27.6 |      |             |      |      |
| Change Period (Y+Rc), s      |      | 4.5      | 4.5  | 4.5  |          | 4.5  | 4.5  | 4.5  |      |             |      |      |
| Max Green Setting (Gmax), s  |      | 18.9     | 5.1  | 22.5 |          | 18.9 | 5.5  | 22.1 |      |             |      |      |
| Max Q Clear Time (g_c+l1), s |      | 5.6      | 4.0  | 21.5 |          | 4.3  | 3.1  | 10.1 |      |             |      |      |
| Green Ext Time (p_c), s      |      | 0.6      | 0.0  | 0.4  |          | 0.4  | 0.0  | 1.6  |      |             |      |      |
| Intersection Summary         |      |          |      |      |          |      |      |      |      |             |      |      |
| HCM 2010 Ctrl Delay          |      |          | 25.6 |      |          |      |      |      |      |             |      |      |
| HCM 2010 LOS                 |      |          | С    |      |          |      |      |      |      |             |      |      |

| Section   Configurations   Configurati   |                              |   | <b>→</b> | <b>←</b> | •    | <u> </u> | 4    |      |      |  |  |
|--|------------------------------|---|----------|----------|------|----------|------|------|------|--|--|
| ## Configurations ## ## ## ## ## ## ## ## ## ## ## ## ##   | Movement                     |   | EBT      | WBT      | WBR  | SBL      | SBR  |      |      |  |  |
| affic Volume (veh/h)   |                              |   |          |          |      |          |      |      |      |  |  |
| tuture Volume (veh/h)  |                              |   |          |          |      |          |      |      |      |  |  |
| Imber  | ,                            |   |          |          |      |          |      |      |      |  |  |
| taial Q (ob), veh  | Number                       |   |          |          |      |          |      |      |      |  |  |
| sel-Bike Adj(A. pbT)   |                              |   |          |          |      |          |      |      |      |  |  |
| urking Bus, Adj  | . ,                          |   |          |          |      |          |      |      |      |  |  |
| ij Sat Flow, veh/h/ln 1863 1863 1863 1863 1863 1863 1863   ij Flow Rate, veh/h 274 464 214 172 156 173   ij No. of Lanes 1 1 1 1 1 1 1   sak Hour Factor 0.94 0.94 0.94 0.94 0.94 0.94 0.94   sak Hour Factor 0.94 0.94 0.94 0.94 0.94 0.94   sak Hour Factor 0.95 0.95 0.95 0.95 0.95 0.95 0.95 0.95  | Parking Bus, Adj             |   | 1.00     | 1.00     |      |          |      |      |      |  |  |
| Flow Rate, veh/h   274    464    214    172    156    173    1   |                              |   |          |          |      |          |      |      |      |  |  |
| No. of Lanes   |                              |   |          |          |      |          |      |      |      |  |  |
| Ask Hour Factor  |                              |   |          |          |      |          |      |      |      |  |  |
| Servent Heavy Veh, %   2   2   2   2   2   2   2   2   2   | Peak Hour Factor             |   |          |          |      |          |      |      |      |  |  |
| ap, veh/h  352 896 333 283 553 493 rive On Green  0.20 0.48 0.18 0.18 0.18 0.31 0.31 0.31  p Volume(v), veh/h 1774 1863 1863 1583 1774 1583  p Sat Flow(s), veh/h/ln 1774 1863 1863 1583 1774 1583  p Sat Flow(s), veh/h/ln 1774 1863 1863 1583 1774 1583  serve(g_s), s 6.3 7.5 4.6 4.3 2.9 3.7 cole Q Clear(g_c), s 6.3 493 Clear(g_c), s | Percent Heavy Veh, %         |   |          |          |      |          |      |      |      |  |  |
| rive On Green  | Cap, veh/h                   |   |          |          |      |          |      |      |      |  |  |
| 18   18   18   18   18   18   18   18  | Arrive On Green              |   |          |          |      |          |      |      |      |  |  |
| p Volume(v), veh/h p Sat Flow(s),veh/h/ln 1774   | Sat Flow, veh/h              |   |          |          |      |          |      |      |      |  |  |
| p Sat Flow(s),veh/h/ln   | ·                            |   |          |          |      |          |      |      |      |  |  |
| Serve(g_s), s 6.3 7.5 4.6 4.3 2.9 3.7  cole Q Clear(g_c), s 6.3 7.5 4.6 4.3 2.9 3.7  op ln Lane 1.00 1.00 1.00 1.00  me Grp Cap(c), veh/h 352 896 333 283 553 493  C Ratio(X) 0.78 0.52 0.64 0.61 0.28 0.35  vail Cap(c_a), veh/h 757 1612 623 530 553 493  CM Platoon Ratio 1.00 1.00 1.00 1.00 1.00 1.00  softream Filter(I) 1.00 1.00 1.00 1.00 1.00 1.00  softream Filter(I) 1.00 1.00 1.00 1.00 1.00 1.00  softream Filter(I) 1.00 0.0 0.0 0.0 0.0 0.0  softream Filter(I) 3.7 0.5 2.1 2.1 1.3 2.0  tial Q Delay(d3),s/veh 0.0 0.0 0.0 0.0 0.0 0.0  ile BackOfQ(50%),veh/ln 3.4 3.9 2.6 2.0 1.6 3.8  Grap Delay (d,s/veh 20.2 8.2 18.6 18.5 12.5 13.5  Grap LOS C A B B B B  softre LOS B B B  mer 1 2 3 4 5 6 7 8  signed Phs  signed Phs  sa Duration (G+Y+Rc), s  and Grap Period (Y+Rc), s  and  | 1 ( ),                       |   |          |          |      |          |      |      |      |  |  |
| Vacle Q Clear(g_c), s  |                              |   |          |          |      |          |      |      |      |  |  |
| Description   Continue   | (6= ):                       |   |          |          |      |          |      |      |      |  |  |
| Ine Grp Cap(c), veh/h 352 896 333 283 553 493 C Ratio(X) 0.78 0.52 0.64 0.61 0.28 0.35 (all Cap(c_a), veh/h 757 1612 623 530 553 493 (black)   |                              |   |          |          |      |          |      |      |      |  |  |
| C Ratio(X)   | •                            |   | 896      | 333      |      |          |      |      |      |  |  |
| rail Cap(c_a), veh/h 757 1612 623 530 553 493  CM Platoon Ratio 1.00 1.00 1.00 1.00 1.00 1.00  costream Filter(I) 1.00 1.00 1.00 1.00 1.00 1.00  costream Filter(I) 1.00 1.00 1.00 1.00 1.00 1.00  costream Filter(I) 1.00 1.00 1.00 1.00  costream Filter(I) 1.00 1.00 1.00 1.00  costream Filter(I) 1.00 1.00  costream Fi |                              |   |          |          |      |          |      |      |      |  |  |
| CM Platoon Ratio 1.00 1.00 1.00 1.00 1.00 1.00 1.00 obstream Filter(I) 1.00 1.00 1.00 1.00 1.00 1.00 1.00 obstream Filter(I) 1.00 obstream Filt | ` ,                          |   |          |          |      |          |      |      |      |  |  |
| pstream Filter(I)     1.00     1.00     1.00     1.00     1.00     1.00       pniform Delay (d), s/veh     16.5     7.8     16.5     16.4     11.3     11.5       por Delay (d2), s/veh     3.7     0.5     2.1     2.1     1.3     2.0       tial Q Delay(d3),s/veh     0.0     0.0     0.0     0.0     0.0     0.0       group Delay(d),s/veh     3.4     3.9     2.6     2.0     1.6     3.8       Grp Delay(d),s/veh     20.2     8.2     18.6     18.5     12.5     13.5       Grp LOS     C     A     B     B     B       pproach Vol, veh/h     738     386     329       pproach LOS     B     B     B       mer     1     2     3     4     5     6     7     8       sisgned Phs     4     6     7     8       sis Duration (G+Y+Rc), s     25.3     18.0     13.1     12.2       nange Period (Y+Rc), s     4.5     4.5     4.5     4.5       ax Green Setting (Gmax), s     37.5     13.5     18.5     14.5       ax Q Clear Time (g_c+I1), s     9.5     5.7     8.3     6.6       reen Ext Time (p_c), s     3.1     0.7   | HCM Platoon Ratio            |   |          |          |      |          |      |      |      |  |  |
| niform Delay (d), s/veh 16.5 7.8 16.5 16.4 11.3 11.5 cr Delay (d2), s/veh 3.7 0.5 2.1 2.1 1.3 2.0 tial Q Delay(d3), s/veh 0.0 0.0 0.0 0.0 0.0 0.0 0.0 ile BackOfQ(50%), veh/ln 3.4 3.9 2.6 2.0 1.6 3.8 in tight of the property of the propert |                              |   |          |          |      |          |      |      |      |  |  |
| cr Delay (d2), s/veh 3.7 0.5 2.1 2.1 1.3 2.0  tial Q Delay(d3),s/veh 0.0 0.0 0.0 0.0 0.0  ile BackOfQ(50%),veh/ln 3.4 3.9 2.6 2.0 1.6 3.8  iGrp Delay(d),s/veh 20.2 8.2 18.6 18.5 12.5 13.5  iGrp LOS C A B B B B  oproach Vol, veh/h 738 386 329  oproach Delay, s/veh 12.7 18.6 13.0  oproach LOS B B B B  oproach LOS B B B B  oproach LOS B B B B  oproach Vol, veh/h 12.7 18.6 13.0  oproach LOS B B B B  oproach LOS B B B B  oproach LOS B B B B  oproach Vol, veh/h 13.1 12.2  oproach LOS B B B B  oproach LOS B B B B  oproach LOS B B B B B B  oproach LOS B B B B B B  oproach LOS B B B B B B B B  oproach LOS B B B B B B B B  oproach LOS B B B B B B B B B B B  oproach LOS B B B B B B B B B B B B B B B B B B B   |                              |   |          |          |      |          |      |      |      |  |  |
| tital Q Delay(d3),s/veh 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.   |                              |   |          |          |      |          |      |      |      |  |  |
| ile BackOfQ(50%),veh/ln 3.4 3.9 2.6 2.0 1.6 3.8 iGrp Delay(d),s/veh 20.2 8.2 18.6 18.5 12.5 13.5 iGrp LOS C A B B B B opproach Vol, veh/h 738 386 329 opproach Delay, s/veh 12.7 18.6 13.0 opproach LOS B B B B B B B opproach LOS B B B B B opproach LOS B B B B B B opproach LOS B B B B B B B B B opproach LOS B B B B B B B B B B B opproach LOS B B B B B B B B B B B B B B B B opproach LOS B B B B B B B B B B B B B B B B B B B   |                              |   |          |          |      |          |      |      |      |  |  |
| AGRIP Delay(d), s/veh 20.2 8.2 18.6 18.5 12.5 13.5 AGRIP LOS C A B B B B B B B B B B B B B B B B B B   | %ile BackOfQ(50%),veh/ln     |   |          |          |      |          |      |      |      |  |  |
| A B B B B B B B B B B B B B B B B B B B  | LnGrp Delay(d),s/veh         |   |          |          |      |          |      |      |      |  |  |
| Opproach Vol, veh/h         738         386         329           Opproach Delay, s/veh         12.7         18.6         13.0           Opproach LOS         B         B         B           Image Period (Phs         4         5         6         7         8           Insigned Phs         4         5         4.5         4.5           Insigned Phs         4         5         5         4.5         4.5 <tr< td=""><td>LnGrp LOS</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></tr<>  | LnGrp LOS                    |   |          |          |      |          |      |      |      |  |  |
| Opproach Delay, s/veh         12.7         18.6         13.0           Opproach LOS         B         B         B           Image Period (Phs are Green Setting (G+Y+Rc), star Green Setting (Gmax), star Q Clear Time (g_c+I1), star Q Clear Time (g_c+I1), star Q Clear Time (p_c), star Q Clear T  | •                            |   |          |          |      |          |      |      |      |  |  |
| Operoach LOS         B         B         B           mer         1         2         3         4         5         6         7         8           ssigned Phs         4         6         7         8           ssigned Phs         25.3         18.0         13.1         12.2           nange Period (Y+Rc), s         4.5         4.5         4.5         4.5           ax Green Setting (Gmax), s         37.5         13.5         18.5         14.5           ax Q Clear Time (g_c+l1), s         9.5         5.7         8.3         6.6           een Ext Time (p_c), s         3.1         0.7         0.6         1.1           tersection Summary         14.3   | •                            |   |          |          |      |          |      |      |      |  |  |
| Assigned Phs     4     6     7     8       Ans Duration (G+Y+Rc), s     25.3     18.0     13.1     12.2       Anange Period (Y+Rc), s     4.5     4.5     4.5     4.5       Asx Green Setting (Gmax), s     37.5     13.5     18.5     14.5       Anax Q Clear Time (g_c+l1), s     9.5     5.7     8.3     6.6       Areen Ext Time (p_c), s     3.1     0.7     0.6     1.1       Attersection Summary       CM 2010 Ctrl Delay     14.3   | Approach LOS                 |   |          |          |      |          |      |      |      |  |  |
| 18.0 13.1 12.2 18.0 13.1 12.2 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0  | Timer                        | 1 | 2        | 3        | 4    | 5        | 6    | 7    | 8    |  |  |
| 18.0 Uration (G+Y+Rc), s 25.3 18.0 13.1 12.2 18.0 18.0 18.0 18.1 12.2 18.0 18.0 18.1 18.2 18.2 18.2 18.2 18.2 18.2 18.2  | Assigned Phs                 |   |          |          | 4    |          | 6    | 7    | 8    |  |  |
| nange Period (Y+Rc), s       4.5       4.5       4.5       4.5         ax Green Setting (Gmax), s       37.5       13.5       18.5       14.5         ax Q Clear Time (g_c+I1), s       9.5       5.7       8.3       6.6         reen Ext Time (p_c), s       3.1       0.7       0.6       1.1         tersection Summary         CM 2010 Ctrl Delay       14.3  | Phs Duration (G+Y+Rc), s     |   |          |          | 25.3 |          | 18.0 | 13.1 | 12.2 |  |  |
| ax Green Setting (Gmax), s 37.5 13.5 14.5   ax Q Clear Time (g_c+l1), s 9.5 5.7 8.3 6.6   een Ext Time (p_c), s 3.1 0.7 0.6 1.1   ersection Summary    CM 2010 Ctrl Delay 14.3   | Change Period (Y+Rc), s      |   |          |          |      |          | 4.5  | 4.5  | 4.5  |  |  |
| ax Q Clear Time (g_c+I1), s     9.5     5.7     8.3     6.6       reen Ext Time (p_c), s     3.1     0.7     0.6     1.1   CM 2010 Ctrl Delay 14.3   | Max Green Setting (Gmax), s  |   |          |          | 37.5 |          | 13.5 | 18.5 | 14.5 |  |  |
| tersection Summary  CM 2010 Ctrl Delay  14.3   | Max Q Clear Time (g_c+l1), s |   |          |          | 9.5  |          | 5.7  | 8.3  | 6.6  |  |  |
| CM 2010 Ctrl Delay 14.3  | Green Ext Time (p_c), s      |   |          |          |      |          | 0.7  |      |      |  |  |
| ·  | Intersection Summary         |   |          |          |      |          |      |      |      |  |  |
| DM 2010 LOS B  | HCM 2010 Ctrl Delay          |   |          |          |      |          |      |      |      |  |  |
|  | HCM 2010 LOS                 |   |          | В        |      |          |      |      |      |  |  |

|                               | ۶          | -        | •     | •     | <b>—</b>   | •          | •       | <b>†</b> | ~    | <b>\</b> | <del> </del> | -√   |
|-------------------------------|------------|----------|-------|-------|------------|------------|---------|----------|------|----------|--------------|------|
| Movement                      | EBL        | EBT      | EBR   | WBL   | WBT        | WBR        | NBL     | NBT      | NBR  | SBL      | SBT          | SBR  |
| Lane Configurations           | *          | <b>↑</b> | 7     | 7     | 1>         |            |         | 4        | 7    |          | 4            | 7    |
| Traffic Volume (vph)          | 1          | 566      | 423   | 22    | 620        | 27         | 318     | 16       | 48   | 132      | 154          | 1    |
| Future Volume (vph)           | 1          | 566      | 423   | 22    | 620        | 27         | 318     | 16       | 48   | 132      | 154          | 1    |
| Ideal Flow (vphpl)            | 1900       | 1900     | 1900  | 1900  | 1900       | 1900       | 1900    | 1900     | 1900 | 1900     | 1900         | 1900 |
| Total Lost time (s)           | 4.5        | 4.5      | 4.5   | 4.5   | 4.5        |            |         | 4.5      | 4.5  |          | 4.5          | 4.5  |
| Lane Util. Factor             | 1.00       | 1.00     | 1.00  | 1.00  | 1.00       |            |         | 1.00     | 1.00 |          | 1.00         | 1.00 |
| Frt                           | 1.00       | 1.00     | 0.85  | 1.00  | 0.99       |            |         | 1.00     | 0.85 |          | 1.00         | 0.85 |
| Flt Protected                 | 0.95       | 1.00     | 1.00  | 0.95  | 1.00       |            |         | 0.95     | 1.00 |          | 0.98         | 1.00 |
| Satd. Flow (prot)             | 1687       | 1776     | 1509  | 1583  | 1656       |            |         | 1778     | 1583 |          | 1821         | 1583 |
| Flt Permitted                 | 0.95       | 1.00     | 1.00  | 0.95  | 1.00       |            |         | 0.95     | 1.00 |          | 0.98         | 1.00 |
| Satd. Flow (perm)             | 1687       | 1776     | 1509  | 1583  | 1656       |            |         | 1778     | 1583 |          | 1821         | 1583 |
| Peak-hour factor, PHF         | 0.94       | 0.94     | 0.94  | 0.94  | 0.94       | 0.94       | 0.94    | 0.94     | 0.94 | 0.94     | 0.94         | 0.94 |
| Adj. Flow (vph)               | 1          | 602      | 450   | 23    | 660        | 29         | 338     | 17       | 51   | 140      | 164          | 1    |
| RTOR Reduction (vph)          | 0          | 0        | 259   | 0     | 1          | 0          | 0       | 0        | 40   | 0        | 0            | 1    |
| Lane Group Flow (vph)         | 1          | 602      | 191   | 23    | 688        | 0          | 0       | 355      | 11   | 0        | 304          | 0    |
| Heavy Vehicles (%)            | 7%         | 7%       | 7%    | 14%   | 14%        | 14%        | 2%      | 2%       | 2%   | 2%       | 2%           | 2%   |
| Turn Type                     | Prot       | NA       | Perm  | Prot  | NA         |            | Split   | NA       | Perm | Split    | NA           | Perm |
| Protected Phases              | 7          | 4        |       | 3     | 8          |            | 5       | 5        |      | 6        | 6            |      |
| Permitted Phases              |            | •        | 4     | -     |            |            | -       | •        | 5    | •        | -            | 6    |
| Actuated Green, G (s)         | 0.9        | 45.4     | 45.4  | 1.9   | 46.4       |            |         | 22.2     | 22.2 |          | 19.7         | 19.7 |
| Effective Green, g (s)        | 0.9        | 45.4     | 45.4  | 1.9   | 46.4       |            |         | 22.2     | 22.2 |          | 19.7         | 19.7 |
| Actuated g/C Ratio            | 0.01       | 0.42     | 0.42  | 0.02  | 0.43       |            |         | 0.21     | 0.21 |          | 0.18         | 0.18 |
| Clearance Time (s)            | 4.5        | 4.5      | 4.5   | 4.5   | 4.5        |            |         | 4.5      | 4.5  |          | 4.5          | 4.5  |
| Vehicle Extension (s)         | 3.0        | 3.0      | 3.0   | 3.0   | 3.0        |            |         | 3.0      | 3.0  |          | 3.0          | 3.0  |
| Lane Grp Cap (vph)            | 14         | 752      | 639   | 28    | 716        |            |         | 368      | 327  |          | 334          | 290  |
| v/s Ratio Prot                | 0.00       | 0.34     | 000   | c0.01 | c0.42      |            |         | c0.20    | 02.  |          | c0.17        | 200  |
| v/s Ratio Perm                | 0.00       | 0.01     | 0.13  | 00.01 | 00.12      |            |         | 00.20    | 0.01 |          | 00.11        | 0.00 |
| v/c Ratio                     | 0.07       | 0.80     | 0.30  | 0.82  | 0.96       |            |         | 0.96     | 0.03 |          | 0.91         | 0.00 |
| Uniform Delay, d1             | 52.7       | 27.0     | 20.4  | 52.5  | 29.5       |            |         | 42.1     | 33.9 |          | 42.9         | 35.7 |
| Progression Factor            | 1.00       | 1.00     | 1.00  | 1.00  | 1.00       |            |         | 1.00     | 1.00 |          | 1.00         | 1.00 |
| Incremental Delay, d2         | 2.2        | 8.8      | 1.2   | 96.0  | 25.3       |            |         | 37.3     | 0.0  |          | 27.7         | 0.0  |
| Delay (s)                     | 54.9       | 35.7     | 21.6  | 148.4 | 54.8       |            |         | 79.4     | 34.0 |          | 70.6         | 35.7 |
| Level of Service              | D          | D        | C     | F     | D          |            |         | E        | С    |          | E            | D    |
| Approach Delay (s)            |            | 29.7     |       | •     | 57.8       |            |         | 73.7     |      |          | 70.5         | _    |
| Approach LOS                  |            | C        |       |       | E          |            |         | E        |      |          | E            |      |
| Intersection Summary          |            |          |       |       |            |            |         |          |      |          |              |      |
| HCM 2000 Control Delay        |            |          | 50.0  | Н     | CM 2000    | Level of S | Service |          | D    |          |              |      |
| HCM 2000 Volume to Capa       | city ratio |          | 0.96  |       |            |            |         |          |      |          |              |      |
| Actuated Cycle Length (s)     |            |          | 107.2 | S     | um of lost | time (s)   |         |          | 18.0 |          |              |      |
| Intersection Capacity Utiliza | ition      |          | 79.4% | IC    | CU Level   | of Service | !       |          | D    |          |              |      |
| Analysis Period (min)         |            |          | 15    |       |            |            |         |          |      |          |              |      |
| c Critical Lane Group         |            |          |       |       |            |            |         |          |      |          |              |      |

## 8: Airline Hwy (SR 25)/Pinnacles Nat Pk Hwy (SR 25) & Tres Pinos Rd/Sunnslope Rd

| Movement Lane Configurations Traffic Volume (veh/h) Future Volume (veh/h) Number Initial Q (Qb), veh Ped-Bike Adj(A_pbT) Parking Bus, Adj Adj Sat Flow, veh/h/ln Adj Flow Rate, veh/h Adj No. of Lanes Peak Hour Factor | 167<br>167<br>7<br>0<br>1.00<br>1.00<br>1863<br>174<br>2<br>0.96<br>2<br>273 | *** September 1.00    1.00   1863   312   2   0.96       | 178<br>178<br>178<br>14<br>0<br>0.98<br>1.00<br>1863<br>185 | WBL  167 167 3 0 1.00 1.00 1863 174          | WBT  246 246 8 0  1.00 | WBR<br>142<br>142<br>18<br>0<br>0.99 | NBL<br>199<br>199<br>5<br>0<br>1.00 | NBT  ↑↑  387  387  2  0 | 141<br>141<br>12<br>0<br>1.00 | SBL<br>229<br>229<br>1<br>0<br>1.00 | \$BT<br>679<br>679<br>6<br>0 | SBR<br>219<br>219<br>16 |
|---|--|--|---|--|------------------------|--------------------------------------|-------------------------------------|-------------------------|-------------------------------|-------------------------------------|------------------------------|-------------------------|
| Traffic Volume (veh/h) Future Volume (veh/h) Number Initial Q (Qb), veh Ped-Bike Adj(A_pbT) Parking Bus, Adj Adj Sat Flow, veh/h/ln Adj Flow Rate, veh/h Adj No. of Lanes   | 167<br>167<br>7<br>0<br>1.00<br>1.00<br>1863<br>174<br>2<br>0.96             | 300<br>300<br>4<br>0<br>1.00<br>1863<br>312<br>2<br>0.96 | 178<br>178<br>14<br>0<br>0.98<br>1.00<br>1863<br>185        | 167<br>167<br>3<br>0<br>1.00<br>1.00<br>1863 | 246<br>246<br>8<br>0   | 142<br>142<br>18<br>0<br>0.99        | 199<br>199<br>5<br>0                | 387<br>387<br>2         | 141<br>12<br>0                | 229<br>229<br>1<br>0                | 679<br>679<br>6              | 219<br>219              |
| Future Volume (veh/h) Number Initial Q (Qb), veh Ped-Bike Adj(A_pbT) Parking Bus, Adj Adj Sat Flow, veh/h/ln Adj Flow Rate, veh/h Adj No. of Lanes  | 167<br>7<br>0<br>1.00<br>1.00<br>1863<br>174<br>2<br>0.96                    | 300<br>4<br>0<br>1.00<br>1863<br>312<br>2<br>0.96        | 178<br>14<br>0<br>0.98<br>1.00<br>1863<br>185               | 167<br>3<br>0<br>1.00<br>1.00<br>1863        | 246<br>8<br>0          | 142<br>18<br>0<br>0.99               | 199<br>5<br>0                       | 387<br>2                | 141<br>12<br>0                | 229<br>1<br>0                       | 679<br>6                     | 219                     |
| Number Initial Q (Qb), veh Ped-Bike Adj(A_pbT) Parking Bus, Adj Adj Sat Flow, veh/h/ln Adj Flow Rate, veh/h Adj No. of Lanes  | 7<br>0<br>1.00<br>1.00<br>1863<br>174<br>2<br>0.96                           | 1.00<br>1863<br>312<br>2<br>0.96                         | 14<br>0<br>0.98<br>1.00<br>1863<br>185                      | 3<br>0<br>1.00<br>1.00<br>1863               | 1.00                   | 18<br>0<br>0.99                      | 5<br>0                              | 2                       | 12<br>0                       | 1                                   | 6                            |                         |
| Initial Q (Qb), veh Ped-Bike Adj(A_pbT) Parking Bus, Adj Adj Sat Flow, veh/h/ln Adj Flow Rate, veh/h Adj No. of Lanes   | 0<br>1.00<br>1.00<br>1863<br>174<br>2<br>0.96<br>2                           | 1.00<br>1863<br>312<br>2<br>0.96                         | 0<br>0.98<br>1.00<br>1863<br>185                            | 0<br>1.00<br>1.00<br>1863                    | 1.00                   | 0<br>0.99                            | 0                                   |                         | 0                             | 0                                   |                              | 16                      |
| Ped-Bike Adj(A_pbT) Parking Bus, Adj Adj Sat Flow, veh/h/ln Adj Flow Rate, veh/h Adj No. of Lanes   | 1.00<br>1.00<br>1863<br>174<br>2<br>0.96                                     | 1.00<br>1863<br>312<br>2<br>0.96                         | 0.98<br>1.00<br>1863<br>185                                 | 1.00<br>1.00<br>1863                         | 1.00                   | 0.99                                 |                                     | 0                       |                               |                                     | 0                            |                         |
| Parking Bus, Adj<br>Adj Sat Flow, veh/h/ln<br>Adj Flow Rate, veh/h<br>Adj No. of Lanes  | 1.00<br>1863<br>174<br>2<br>0.96   | 1863<br>312<br>2<br>0.96                                 | 1.00<br>1863<br>185   | 1.00<br>1863                                 |                        |                                      | 1.00                                |                         | 1.00                          | 1 00                                |                              | 0                       |
| Adj Sat Flow, veh/h/ln<br>Adj Flow Rate, veh/h<br>Adj No. of Lanes  | 1863<br>174<br>2<br>0.96<br>2  | 1863<br>312<br>2<br>0.96                                 | 1863<br>185   | 1863   |                        | 4 00                                 |                                     |                         |                               | 1.00                                |                              | 1.00                    |
| Adj Flow Rate, veh/h<br>Adj No. of Lanes  | 174<br>2<br>0.96<br>2  | 312<br>2<br>0.96   | 185   |  | 1062                   | 1.00                                 | 1.00                                | 1.00                    | 1.00                          | 1.00                                | 1.00                         | 1.00                    |
| Adj No. of Lanes  | 2<br>0.96<br>2   | 2<br>0.96  |   | 174  | 1863                   | 1863                                 | 1863                                | 1863                    | 1900                          | 1863                                | 1863                         | 1863                    |
|   | 0.96<br>2  | 0.96   | 1   | 117  | 256                    | 148                                  | 207                                 | 403                     | 147                           | 239                                 | 707                          | 228                     |
| Peak Hour Factor  | 2  |  |   | 1  | 2                      | 1                                    | 2                                   | 3                       | 0                             | 2                                   | 3                            | 1                       |
|   |  | ^  | 0.96  | 0.96   | 0.96                   | 0.96                                 | 0.96                                | 0.96                    | 0.96                          | 0.96                                | 0.96                         | 0.96                    |
| Percent Heavy Veh, %  | 273  | 2  | 2   | 2  | 2                      | 2                                    | 2                                   | 2                       | 2                             | 2                                   | 2                            | 2                       |
| Cap, veh/h  |  | 631  | 418   | 216  | 782                    | 348                                  | 307                                 | 1150                    | 401                           | 339                                 | 1618                         | 628                     |
| Arrive On Green   | 0.08   | 0.18   | 0.18  | 0.12   | 0.22                   | 0.22                                 | 0.09                                | 0.31                    | 0.31                          | 0.10                                | 0.32                         | 0.32                    |
| Sat Flow, veh/h   | 3442   | 3539   | 1554  | 1774   | 3539                   | 1575                                 | 3442                                | 3724                    | 1299                          | 3442                                | 5085                         | 1580                    |
| Grp Volume(v), veh/h  | 174  | 312  | 185   | 174  | 256                    | 148                                  | 207                                 | 365                     | 185                           | 239                                 | 707                          | 228                     |
| Grp Sat Flow(s),veh/h/ln  | 1721   | 1770   | 1554  | 1774   | 1770                   | 1575                                 | 1721                                | 1695                    | 1633                          | 1721                                | 1695                         | 1580                    |
| Q Serve(g_s), s   | 3.0  | 4.9  | 6.1   | 5.9  | 3.7                    | 5.0                                  | 3.6                                 | 5.1                     | 5.4                           | 4.1                                 | 6.8                          | 6.3                     |
| Cycle Q Clear(g_c), s   | 3.0  | 4.9  | 6.1   | 5.9  | 3.7                    | 5.0                                  | 3.6                                 | 5.1                     | 5.4                           | 4.1                                 | 6.8                          | 6.3                     |
| Prop In Lane  | 1.00   |  | 1.00  | 1.00   | <u> </u>               | 1.00                                 | 1.00                                |                         | 0.80                          | 1.00                                |                              | 1.00                    |
| Lane Grp Cap(c), veh/h  | 273  | 631  | 418   | 216  | 782                    | 348                                  | 307                                 | 1047                    | 504                           | 339                                 | 1618                         | 628                     |
| V/C Ratio(X)  | 0.64   | 0.49   | 0.44  | 0.80   | 0.33                   | 0.43                                 | 0.67                                | 0.35                    | 0.37                          | 0.70                                | 0.44                         | 0.36                    |
| Avail Cap(c_a), veh/h   | 419  | 1035   | 596   | 245  | 1093                   | 486                                  | 363                                 | 1047                    | 504                           | 363                                 | 1618                         | 628                     |
| HCM Platoon Ratio   | 1.00   | 1.00   | 1.00  | 1.00   | 1.00                   | 1.00                                 | 1.00                                | 1.00                    | 1.00                          | 1.00                                | 1.00                         | 1.00                    |
| Upstream Filter(I)  | 1.00   | 1.00   | 1.00  | 1.00   | 1.00                   | 1.00                                 | 1.00                                | 1.00                    | 1.00                          | 1.00                                | 1.00                         | 1.00                    |
| Uniform Delay (d), s/veh  | 27.5   | 22.8   | 18.7  | 26.3   | 20.1                   | 20.6                                 | 27.2                                | 16.5                    | 16.6                          | 26.9                                | 16.6                         | 13.1                    |
| Incr Delay (d2), s/veh  | 2.5  | 0.6  | 0.7   | 15.8   | 0.2                    | 0.8                                  | 3.9                                 | 0.9                     | 2.1                           | 5.6                                 | 0.9                          | 1.6                     |
| Initial Q Delay(d3),s/veh   | 0.0  | 0.0  | 0.0   | 0.0  | 0.0                    | 0.0                                  | 0.0                                 | 0.0                     | 0.0                           | 0.0                                 | 0.0                          | 0.0                     |
| %ile BackOfQ(50%),veh/ln  | 1.5  | 2.4  | 2.7   | 3.8  | 1.8                    | 2.2                                  | 1.9                                 | 2.5                     | 2.7                           | 2.2                                 | 3.3                          | 3.0                     |
| LnGrp Delay(d),s/veh  | 29.9   | 23.4   | 19.5  | 42.2   | 20.4                   | 21.4                                 | 31.0                                | 17.4                    | 18.6                          | 32.5                                | 17.5                         | 14.7                    |
| LnGrp LOS   | C  | C  | В   | D  | C                      | C                                    | C                                   | В                       | В                             | C                                   | В                            | В                       |
| Approach Vol, veh/h   |  | 671  |   |  | 578                    |                                      |                                     | 757                     |                               |                                     | 1174                         |                         |
| Approach Delay, s/veh   |  | 24.0   |   |  | 27.2                   |                                      |                                     | 21.4                    |                               |                                     | 20.0                         |                         |
| Approach LOS  |  | 24.0<br>C  |   |  | C C                    |                                      |                                     | C C                     |                               |                                     | 20.0<br>B                    |                         |
| •   |  |  |   |  |                        |                                      |                                     |                         |                               |                                     | ь                            |                         |
| Timer   | 1  | 2  | 3   | 4  | 5                      | 6                                    | 7                                   | 8                       |                               |                                     |                              |                         |
| Assigned Phs  | 1  | 2  | 3   | 4  | 5                      | 6                                    | 7                                   | 8                       |                               |                                     |                              |                         |
| Phs Duration (G+Y+Rc), s  | 10.6   | 23.5   | 12.0  | 15.5   | 10.0                   | 24.1                                 | 9.4                                 | 18.1                    |                               |                                     |                              |                         |
| Change Period (Y+Rc), s   | 4.5  | 4.5  | 4.5   | 4.5  | 4.5                    | 4.5                                  | 4.5                                 | 4.5                     |                               |                                     |                              |                         |
| Max Green Setting (Gmax), s   | 6.5  | 19.0   | 8.5   | 18.0   | 6.5                    | 19.0                                 | 7.5                                 | 19.0                    |                               |                                     |                              |                         |
| Max Q Clear Time (g_c+l1), s  | 6.1  | 7.4  | 7.9   | 8.1  | 5.6                    | 8.8                                  | 5.0                                 | 7.0                     |                               |                                     |                              |                         |
| Green Ext Time (p_c), s   | 0.0  | 2.8  | 0.0   | 1.9  | 0.1                    | 4.1                                  | 0.1                                 | 1.7                     |                               |                                     |                              |                         |
| Intersection Summary  |  |  |   |  |                        |                                      |                                     |                         |                               |                                     |                              |                         |
| HCM 2010 Ctrl Delay   |  |  | 22.5  |  |                        |                                      |                                     |                         |                               |                                     |                              |                         |
| HCM 2010 LOS  |  |  | С   |  |                        |                                      |                                     |                         |                               |                                     |                              |                         |

Lico Subdivision Keith Higgins Traffic Engineer

|                              | ᄼ    | <b>→</b> | •    | •    | <b>←</b> | •    | 1    | <b>†</b> | <b>/</b> | <b>/</b> | <b></b> | 4    |
|------------------------------|------|----------|------|------|----------|------|------|----------|----------|----------|---------|------|
| Movement                     | EBL  | EBT      | EBR  | WBL  | WBT      | WBR  | NBL  | NBT      | NBR      | SBL      | SBT     | SBR  |
| Lane Configurations          | ሻ    | f)       |      | ሻ    | <b>₽</b> |      | 7    | <b>↑</b> | 7        | 7        | ĵ∍      |      |
| Traffic Volume (veh/h)       | 6    | 176      | 79   | 199  | 234      | 150  | 57   | 108      | 215      | 41       | 23      | 3    |
| Future Volume (veh/h)        | 6    | 176      | 79   | 199  | 234      | 150  | 57   | 108      | 215      | 41       | 23      | 3    |
| Number                       | 7    | 4        | 14   | 3    | 8        | 18   | 5    | 2        | 12       | 1        | 6       | 16   |
| Initial Q (Qb), veh          | 0    | 0        | 0    | 0    | 0        | 0    | 0    | 0        | 0        | 0        | 0       | 0    |
| Ped-Bike Adj(A_pbT)          | 1.00 |          | 0.95 | 1.00 |          | 0.99 | 1.00 |          | 0.99     | 1.00     |         | 0.99 |
| Parking Bus, Adj             | 1.00 | 1.00     | 1.00 | 1.00 | 1.00     | 1.00 | 1.00 | 1.00     | 1.00     | 1.00     | 1.00    | 1.00 |
| Adj Sat Flow, veh/h/ln       | 1863 | 1863     | 1900 | 1863 | 1863     | 1900 | 1863 | 1863     | 1863     | 1863     | 1863    | 1900 |
| Adj Flow Rate, veh/h         | 7    | 210      | 94   | 237  | 279      | 179  | 68   | 129      | 256      | 49       | 27      | 4    |
| Adj No. of Lanes             | 1    | 1        | 0    | 1    | 1        | 0    | 1    | 1        | 1        | 1        | 1       | 0    |
| Peak Hour Factor             | 0.84 | 0.84     | 0.84 | 0.84 | 0.84     | 0.84 | 0.84 | 0.84     | 0.84     | 0.84     | 0.84    | 0.84 |
| Percent Heavy Veh, %         | 2    | 2        | 2    | 2    | 2        | 2    | 2    | 2        | 2        | 2        | 2       | 2    |
| Cap, veh/h                   | 16   | 269      | 120  | 281  | 396      | 254  | 97   | 548      | 463      | 80       | 452     | 67   |
| Arrive On Green              | 0.01 | 0.22     | 0.22 | 0.16 | 0.37     | 0.37 | 0.05 | 0.29     | 0.29     | 0.05     | 0.29    | 0.29 |
| Sat Flow, veh/h              | 1774 | 1197     | 536  | 1774 | 1058     | 679  | 1774 | 1863     | 1573     | 1774     | 1585    | 235  |
| Grp Volume(v), veh/h         | 7    | 0        | 304  | 237  | 0        | 458  | 68   | 129      | 256      | 49       | 0       | 31   |
| Grp Sat Flow(s),veh/h/ln     | 1774 | 0        | 1733 | 1774 | 0        | 1738 | 1774 | 1863     | 1573     | 1774     | 0       | 1819 |
| Q Serve(g_s), s              | 0.3  | 0.0      | 10.7 | 8.4  | 0.0      | 14.5 | 2.4  | 3.4      | 8.9      | 1.8      | 0.0     | 0.8  |
| Cycle Q Clear(g_c), s        | 0.3  | 0.0      | 10.7 | 8.4  | 0.0      | 14.5 | 2.4  | 3.4      | 8.9      | 1.8      | 0.0     | 8.0  |
| Prop In Lane                 | 1.00 |          | 0.31 | 1.00 |          | 0.39 | 1.00 |          | 1.00     | 1.00     |         | 0.13 |
| Lane Grp Cap(c), veh/h       | 16   | 0        | 389  | 281  | 0        | 650  | 97   | 548      | 463      | 80       | 0       | 519  |
| V/C Ratio(X)                 | 0.43 | 0.00     | 0.78 | 0.84 | 0.00     | 0.71 | 0.70 | 0.24     | 0.55     | 0.61     | 0.00    | 0.06 |
| Avail Cap(c_a), veh/h        | 137  | 0        | 481  | 287  | 0        | 650  | 137  | 548      | 463      | 137      | 0       | 519  |
| HCM Platoon Ratio            | 1.00 | 1.00     | 1.00 | 1.00 | 1.00     | 1.00 | 1.00 | 1.00     | 1.00     | 1.00     | 1.00    | 1.00 |
| Upstream Filter(I)           | 1.00 | 0.00     | 1.00 | 1.00 | 0.00     | 1.00 | 1.00 | 1.00     | 1.00     | 1.00     | 0.00    | 1.00 |
| Uniform Delay (d), s/veh     | 32.0 | 0.0      | 23.7 | 26.5 | 0.0      | 17.3 | 30.2 | 17.4     | 19.3     | 30.4     | 0.0     | 16.9 |
| Incr Delay (d2), s/veh       | 17.1 | 0.0      | 6.6  | 19.6 | 0.0      | 3.5  | 9.0  | 1.0      | 4.7      | 7.3      | 0.0     | 0.2  |
| Initial Q Delay(d3),s/veh    | 0.0  | 0.0      | 0.0  | 0.0  | 0.0      | 0.0  | 0.0  | 0.0      | 0.0      | 0.0      | 0.0     | 0.0  |
| %ile BackOfQ(50%),veh/ln     | 0.2  | 0.0      | 5.8  | 5.6  | 0.0      | 7.5  | 1.4  | 1.9      | 4.4      | 1.0      | 0.0     | 0.4  |
| LnGrp Delay(d),s/veh         | 49.1 | 0.0      | 30.2 | 46.1 | 0.0      | 20.7 | 39.1 | 18.4     | 24.0     | 37.7     | 0.0     | 17.1 |
| LnGrp LOS                    | D    |          | С    | D    |          | С    | D    | В        | С        | D        |         | В    |
| Approach Vol, veh/h          |      | 311      |      |      | 695      |      |      | 453      |          |          | 80      |      |
| Approach Delay, s/veh        |      | 30.6     |      |      | 29.4     |      |      | 24.7     |          |          | 29.7    |      |
| Approach LOS                 |      | С        |      |      | С        |      |      | С        |          |          | С       |      |
| Timer                        | 1    | 2        | 3    | 4    | 5        | 6    | 7    | 8        |          |          |         |      |
| Assigned Phs                 | 1    | 2        | 3    | 4    | 5        | 6    | 7    | 8        |          |          |         |      |
| Phs Duration (G+Y+Rc), s     | 7.4  | 23.6     | 14.8 | 19.1 | 8.0      | 23.0 | 5.1  | 28.8     |          |          |         |      |
| Change Period (Y+Rc), s      | 4.5  | 4.5      | 4.5  | 4.5  | 4.5      | 4.5  | 4.5  | 4.5      |          |          |         |      |
| Max Green Setting (Gmax), s  | 5.0  | 18.5     | 10.5 | 18.0 | 5.0      | 18.5 | 5.0  | 23.5     |          |          |         |      |
| Max Q Clear Time (g_c+l1), s | 3.8  | 10.9     | 10.4 | 12.7 | 4.4      | 2.8  | 2.3  | 16.5     |          |          |         |      |
| Green Ext Time (p_c), s      | 0.0  | 1.0      | 0.0  | 0.8  | 0.0      | 0.1  | 0.0  | 1.7      |          |          |         |      |
| Intersection Summary         |      |          |      |      |          |      |      |          |          |          |         |      |
| HCM 2010 Ctrl Delay          |      |          | 28.3 |      |          |      |      |          |          |          |         |      |
| HCM 2010 LOS                 |      |          | С    |      |          |      |      |          |          |          |         |      |
|                              |      |          |      |      |          |      |      |          |          |          |         |      |

## Appendix D

Level of Service
Calculations

Existing Plus Project
Conditions

0

0

8

184

0.389

7.594

Yes

474

5.325

0.388

15.1

C

1.8

74

3

86

8

0.169

7.098

Yes

508

4.798

0.169

11.2

В

0.6

0

0

8

107

0.228

7.705

Yes

466

5.441

0.23

12.7

В

0.9

109

121

0.242

7.199

Yes

499

4.934

0.242

12.2

В

0.9

0

8

74

82

8

0.148

6.49

Yes

553

4.225

0.148

10.4

В

0.5

| Intersection               |      |          |       |       |          |       |       |       |       |       |          |       |
|----------------------------|------|----------|-------|-------|----------|-------|-------|-------|-------|-------|----------|-------|
| Intersection Delay, s/veh  | 12.9 |          |       |       |          |       |       |       |       |       |          |       |
| Intersection LOS           | В    |          |       |       |          |       |       |       |       |       |          |       |
|                            |      |          |       |       |          |       |       |       |       |       |          |       |
| Movement                   | EBL  | EBT      | EBR   | WBL   | WBT      | WBR   | NBL   | NBT   | NBR   | SBL   | SBT      | SBR   |
| Lane Configurations        | ሻ    | <b>†</b> | 7     | ሻ     | <b>†</b> | 7     | ሻ     | f)    |       | ሻ     | <b>†</b> | 7     |
| Traffic Vol, veh/h         | 96   | 109      | 74    | 7     | 204      | 87    | 166   | 74    | 3     | 46    | 30       | 86    |
| Future Vol, veh/h          | 96   | 109      | 74    | 7     | 204      | 87    | 166   | 74    | 3     | 46    | 30       | 86    |
| Peak Hour Factor           | 0.90 | 0.90     | 0.90  | 0.90  | 0.90     | 0.90  | 0.90  | 0.90  | 0.90  | 0.90  | 0.90     | 0.90  |
| Heavy Vehicles, %          | 7    | 7        | 7     | 5     | 5        | 5     | 2     | 2     | 2     | 6     | 6        | 6     |
| Mvmt Flow                  | 107  | 121      | 82    | 8     | 227      | 97    | 184   | 82    | 3     | 51    | 33       | 96    |
| Number of Lanes            | 1    | 1        | 1     | 1     | 1        | 1     | 1     | 1     | 0     | 1     | 1        | 1     |
| Approach                   | EB   |          |       | WB    |          |       | NB    |       |       | SB    |          |       |
| Opposing Approach          | WB   |          |       | EB    |          |       | SB    |       |       | NB    |          |       |
| Opposing Lanes             | 3    |          |       | 3     |          |       | 3     |       |       | 2     |          |       |
| Conflicting Approach Left  | SB   |          |       | NB    |          |       | EB    |       |       | WB    |          |       |
| Conflicting Lanes Left     | 3    |          |       | 2     |          |       | 3     |       |       | 3     |          |       |
| Conflicting Approach Right | NB   |          |       | SB    |          |       | WB    |       |       | EB    |          |       |
| Conflicting Lanes Right    | 2    |          |       | 3     |          |       | 3     |       |       | 3     |          |       |
| HCM Control Delay          | 11.9 |          |       | 13.9  |          |       | 13.9  |       |       | 11.3  |          |       |
| HCM LOS                    | В    |          |       | В     |          |       | В     |       |       | В     |          |       |
|                            |      |          |       |       |          |       |       |       |       |       |          |       |
| Lane                       |      | NBLn1    | NBLn2 | EBLn1 | EBLn2    | EBLn3 | WBLn1 | WBLn2 | WBLn3 | SBLn1 | SBLn2    | SBLn3 |
| Vol Left, %                |      | 100%     | 0%    | 100%  | 0%       | 0%    | 100%  | 0%    | 0%    | 100%  | 0%       | 0%    |
| Vol Thru, %                |      | 0%       | 96%   | 0%    | 100%     | 0%    | 0%    | 100%  | 0%    | 0%    | 100%     | 0%    |
| Vol Right, %               |      | 0%       | 4%    | 0%    | 0%       | 100%  | 0%    | 0%    | 100%  | 0%    | 0%       | 100%  |
| Sign Control               |      | Stop     | Stop  | Stop  | Stop     | Stop  | Stop  | Stop  | Stop  | Stop  | Stop     | Stop  |
| Traffic Vol by Lane        |      | 166      | 77    | 96    | 109      | 74    | 7     | 204   | 87    | 46    | 30       | 86    |
| LT Vol                     |      | 166      | 0     | 96    | 0        | 0     | 7     | 0     | 0     | 46    | 0        | 0     |
|                            |      |          |       |       |          |       |       |       |       |       |          |       |

204

227

0.448

7.115

Yes

508

4.847

0.447

15.5

C

2.3

0

8

0

8

8

0.016

7.622

Yes

470

5.354

0.017

10.5

В

0

0

87

97

8

0.172

6.407

Yes

561

4.139

0.173

10.5

В

0.6

30

0

33

8

0.07

7.542

Yes

475

5.281

0.069

10.9

В

0.2

0

51

8

0.114

8.046

Yes

446

5.785

0.114

11.8

В

0.4

0

86

96

8

0.181

6.836

Yes

525

4.575

0.183

11.1

В

0.7

Through Vol

Lane Flow Rate

Degree of Util (X)

Convergence, Y/N

HCM Lane V/C Ratio

**HCM Control Delay** 

**HCM Lane LOS** 

HCM 95th-tile Q

Departure Headway (Hd)

Geometry Grp

Service Time

RT Vol

Cap

| Intersection           |        |         |        |        |         |      |        |          |       |        |         |       |       |  |
|------------------------|--------|---------|--------|--------|---------|------|--------|----------|-------|--------|---------|-------|-------|--|
| Int Delay, s/veh       | 3.2    |         |        |        |         |      |        |          |       |        |         |       |       |  |
| Movement               | EBL    | EBT     | EBR    | WBL    | WBT     | WBR  | NBL    | NBT      | NBR   | SBL    | SBT     | SBR   |       |  |
| Lane Configurations    | ች      | <b></b> | 7      | ች      | <b></b> | 1    | ች      | <b>†</b> | 1     | ች      | <b></b> | 1     |       |  |
| Traffic Vol. veh/h     | 15     | 215     | 15     | 33     | 400     | 19   | 45     | 4        | 44    | 20     | 3       | 43    |       |  |
| Future Vol, veh/h      | 15     | 215     | 15     | 33     | 400     | 19   | 45     | 4        | 44    | 20     | 3       | 43    |       |  |
| Conflicting Peds, #/hr | 0      | 0       | 1      | 0      | 0       | 0    | 0      | 0        | 0     | 0      | 0       | 0     |       |  |
| Sign Control           | Free   | Free    | Free   | Free   | Free    | Free | Stop   | Stop     | Stop  | Stop   | Stop    | Stop  |       |  |
| RT Channelized         | -      |         | None   | -      | -       | None | -      | -        |       | -      | -       | None  |       |  |
| Storage Length         | 320    | _       | 505    | 360    | _       | 195  | 60     | -        | 0     | 100    | -       | 100   |       |  |
| Veh in Median Storage  |        | 0       | _      | _      | 0       | -    | -      | 0        | -     | -      | 0       | _     |       |  |
| Grade, %               | -      | 0       | _      | _      | 0       | -    | -      | 0        | _     | -      | 0       | _     |       |  |
| Peak Hour Factor       | 95     | 95      | 95     | 95     | 95      | 95   | 95     | 95       | 95    | 95     | 95      | 95    |       |  |
| Heavy Vehicles, %      | 8      | 8       | 8      | 4      | 4       | 4    | 2      | 2        | 2     | 3      | 3       | 3     |       |  |
| Mvmt Flow              | 16     | 226     | 16     | 35     | 421     | 20   | 47     | 4        | 46    | 21     | 3       | 45    |       |  |
|                        |        |         |        |        |         | _,   |        |          |       |        | _       |       |       |  |
| Major/Minor N          | Major1 |         |        | Major2 |         |      | Minor1 |          |       | Minor2 |         |       |       |  |
| Conflicting Flow All   | 441    | 0       | 0      | 243    | 0       | 0    | 784    | 770      | 227   | 782    | 766     | 421   |       |  |
| Stage 1                | -      | _       | _      |        | -       | -    | 259    | 259      |       | 491    | 491     |       |       |  |
| Stage 2                | _      | _       | -      | -      | _       | _    | 525    | 511      | -     | 291    | 275     | -     |       |  |
| Critical Hdwy          | 4.18   | -       | -      | 4.14   | -       | -    | 7.12   | 6.52     | 6.22  | 7.13   | 6.53    | 6.23  |       |  |
| Critical Hdwy Stg 1    | -      | _       | -      | -      | -       | -    | 6.12   | 5.52     | -     | 6.13   | 5.53    | -     |       |  |
| Critical Hdwy Stg 2    | _      | -       | -      | -      | -       | -    | 6.12   | 5.52     | -     | 6.13   | 5.53    | -     |       |  |
| Follow-up Hdwy         | 2.272  | -       | -      | 2.236  | -       | -    | 3.518  | 4.018    | 3.318 | 3.527  | 4.027   | 3.327 |       |  |
| Pot Cap-1 Maneuver     | 1088   | -       | -      | 1312   | -       | -    | 311    | 331      | 812   | 310    | 332     | 630   |       |  |
| Stage 1                | -      | -       | -      | -      | -       | -    | 746    | 694      | -     | 557    | 546     | -     |       |  |
| Stage 2                | -      | -       | -      | -      | -       | -    | 536    | 537      | -     | 715    | 681     | -     |       |  |
| Platoon blocked, %     |        | -       | -      |        | -       | -    |        |          |       |        |         |       |       |  |
| Mov Cap-1 Maneuver     | 1088   | _       | _      | 1311   | -       | -    | 277    | 317      | 811   | 280    | 318     | 630   |       |  |
| Mov Cap-2 Maneuver     | -      | -       | -      | -      | -       | -    | 277    | 317      | -     | 280    | 318     | -     |       |  |
| Stage 1                | _      | -       | _      | -      | -       | -    | 734    | 683      | -     | 549    | 531     | -     |       |  |
| Stage 2                | -      | -       | -      | -      | -       | -    | 481    | 523      | -     | 660    | 670     | -     |       |  |
| ,                      |        |         |        |        |         |      |        |          |       |        |         |       |       |  |
| Approach               | EB     |         |        | WB     |         |      | NB     |          |       | SB     |         |       |       |  |
| HCM Control Delay, s   | 0.5    |         |        | 0.6    |         |      | 15.3   |          |       | 13.8   |         |       |       |  |
| HCM LOS                |        |         |        |        |         |      | С      |          |       | В      |         |       |       |  |
|                        |        |         |        |        |         |      |        |          |       |        |         |       |       |  |
| Minor Lane/Major Mvm   | t      | NBLn1 I | NBLn21 | NBLn3  | EBL     | EBT  | EBR    | WBL      | WBT   | WBR    | SBLn1   | SBLn2 | SBLn3 |  |
| Capacity (veh/h)       |        | 277     | 317    | 811    | 1088    | -    | -      | 1311     | -     | -      | 280     | 318   | 630   |  |
| HCM Lane V/C Ratio     |        | 0.171   | 0.013  | 0.057  | 0.015   | -    | -      | 0.026    | -     | -      | 0.075   | 0.01  | 0.072 |  |
| HCM Control Delay (s)  |        | 20.7    | 16.5   | 9.7    | 8.4     | -    | -      | 7.8      | -     | -      | 18.9    | 16.4  | 11.2  |  |
| HCM Lane LOS           |        | С       | С      | Α      | Α       | -    | -      | Α        | -     | -      | С       | С     | В     |  |
| HCM 95th %tile Q(veh)  | 1      | 0.6     | 0      | 0.2    | 0       | _    | -      | 0.1      | _     | -      | 0.2     | 0     | 0.2   |  |

| Intersection           |        |          |        |           |          |      |
|------------------------|--------|----------|--------|-----------|----------|------|
| Int Delay, s/veh       | 4      |          |        |           |          |      |
|                        |        | 14/55    |        |           | 0        | 05-  |
| Movement               | WBL    | WBR      | NBT    | NBR       | SBL      | SBT  |
| Lane Configurations    | N/     |          | ₽      |           |          | 4    |
| Traffic Vol, veh/h     | 28     | 132      | 184    | 13        | 37       | 142  |
| Future Vol, veh/h      | 28     | 132      | 184    | 13        | 37       | 142  |
| Conflicting Peds, #/hr | 0      | 0        | 0      | 1         | 1        | 0    |
| Sign Control           | Stop   | Stop     | Free   | Free      | Free     | Free |
| RT Channelized         | -      | None     | -      | None      | -        | None |
| Storage Length         | 0      | -        | -      | -         | -        | -    |
| Veh in Median Storage  | e, # 0 | -        | 0      | -         | -        | 0    |
| Grade, %               | 0      | -        | 0      | -         | -        | 0    |
| Peak Hour Factor       | 84     | 84       | 84     | 84        | 84       | 84   |
| Heavy Vehicles, %      | 2      | 2        | 7      | 7         | 7        | 7    |
| Mvmt Flow              | 33     | 157      | 219    | 15        | 44       | 169  |
|                        |        |          |        |           |          |      |
| Majar/Minar            | Minord |          | 10:04  |           | \4-:Q    |      |
|                        | Minor1 |          | Major1 |           | Major2   |      |
| Conflicting Flow All   | 485    | 228      | 0      | 0         | 235      | 0    |
| Stage 1                | 228    | -        | -      | -         | -        | -    |
| Stage 2                | 257    | -        | -      | -         | -        | -    |
| Critical Hdwy          | 6.42   | 6.22     | -      | -         | 4.17     | -    |
| Critical Hdwy Stg 1    | 5.42   | -        | -      | -         | -        | -    |
| Critical Hdwy Stg 2    | 5.42   | -        | -      | -         | -        | -    |
| Follow-up Hdwy         |        | 3.318    | -      | -         | 2.263    | -    |
| Pot Cap-1 Maneuver     | 541    | 811      | -      | -         | 1303     | -    |
| Stage 1                | 810    | -        | -      | -         | -        | -    |
| Stage 2                | 786    | -        | -      | -         | -        | -    |
| Platoon blocked, %     |        |          | -      | -         |          | -    |
| Mov Cap-1 Maneuver     | 520    | 810      | -      | -         | 1302     | -    |
| Mov Cap-2 Maneuver     | 520    | -        | -      | -         | -        | -    |
| Stage 1                | 779    | -        | -      | -         | -        | -    |
| Stage 2                | 786    | -        | -      | _         | -        | -    |
| <b></b>                |        |          |        |           |          |      |
| A                      | \A/D   |          | ND     |           | OB       |      |
| Approach               | WB     |          | NB     |           | SB       |      |
| HCM Control Delay, s   | 11.6   |          | 0      |           | 1.6      |      |
| HCM LOS                | В      |          |        |           |          |      |
|                        |        |          |        |           |          |      |
| Minor Lane/Major Mvm   | nt     | NBT      | NBRV   | VBLn1     | SBL      | SBT  |
| Capacity (veh/h)       |        |          |        | 738       | 1302     |      |
| HCM Lane V/C Ratio     |        | <u>-</u> |        | 0.258     |          | _    |
| HCM Control Delay (s)  |        |          | _      | 11.6      | 7.9      | 0    |
| HCM Lane LOS           |        | -        | _      | 11.0<br>B | 7.9<br>A | A    |
| HCM 95th %tile Q(veh   | ١      | _        | _      | 1         | 0.1      | -    |
|                        | )      | _        | -      |           | U. I     | _    |

|                              | ၨ    | <b>→</b> | •    | <b>√</b> | <b>←</b> | •     | •    | †       | ~    | <b>/</b> | Ţ        |          |
|------------------------------|------|----------|------|----------|----------|-------|------|---------|------|----------|----------|----------|
| Movement                     | EBL  | EBT      | EBR  | WBL      | WBT      | WBR   | NBL  | NBT     | NBR  | SBL      | SBT      | SBR      |
| Lane Configurations          | ,    | ĵ»       |      | *        | ĵ.       |       | Ť    | <b></b> | 7    | ¥        | <b>+</b> | 7        |
| Traffic Volume (veh/h)       | 151  | 147      | 105  | 13       | 262      | 186   | 232  | 260     | 19   | 79       | 117      | 123      |
| Future Volume (veh/h)        | 151  | 147      | 105  | 13       | 262      | 186   | 232  | 260     | 19   | 79       | 117      | 123      |
| Number                       | 7    | 4        | 14   | 3        | 8        | 18    | 5    | 2       | 12   | 1        | 6        | 16       |
| Initial Q (Qb), veh          | 0    | 0        | 0    | 0        | 0        | 0     | 0    | 0       | 0    | 0        | 0        | 0        |
| Ped-Bike Adj(A_pbT)          | 1.00 |          | 1.00 | 1.00     |          | 1.00  | 1.00 |         | 1.00 | 1.00     |          | 1.00     |
| Parking Bus, Adj             | 1.00 | 1.00     | 1.00 | 1.00     | 1.00     | 1.00  | 1.00 | 1.00    | 1.00 | 1.00     | 1.00     | 1.00     |
| Adj Sat Flow, veh/h/ln       | 1776 | 1776     | 1900 | 1863     | 1863     | 1900  | 1863 | 1863    | 1863 | 1827     | 1827     | 1827     |
| Adj Flow Rate, veh/h         | 164  | 160      | 114  | 14       | 285      | 202   | 252  | 283     | 21   | 86       | 127      | 134      |
| Adj No. of Lanes             | 1    | 1        | 0    | 1        | 1        | 0     | 1    | 1       | 1    | 1        | 1        | 1        |
| Peak Hour Factor             | 0.92 | 0.92     | 0.92 | 0.92     | 0.92     | 0.92  | 0.92 | 0.92    | 0.92 | 0.92     | 0.92     | 0.92     |
| Percent Heavy Veh, %         | 7    | 7        | 7    | 2        | 2        | 2     | 2    | 2       | 2    | 4        | 4        | 4        |
| Cap, veh/h                   | 319  | 182      | 130  | 438      | 251      | 178   | 258  | 557     | 473  | 109      | 395      | 336      |
| Arrive On Green              | 0.19 | 0.19     | 0.19 | 0.25     | 0.25     | 0.25  | 0.15 | 0.30    | 0.30 | 0.06     | 0.22     | 0.22     |
| Sat Flow, veh/h              | 1691 | 965      | 687  | 1774     | 1016     | 720   | 1774 | 1863    | 1583 | 1740     | 1827     | 1553     |
| Grp Volume(v), veh/h         | 164  | 0        | 274  | 14       | 0        | 487   | 252  | 283     | 21   | 86       | 127      | 134      |
| Grp Sat Flow(s),veh/h/ln     | 1691 | 0        | 1652 | 1774     | 0        | 1736  | 1774 | 1863    | 1583 | 1740     | 1827     | 1553     |
| Q Serve(g_s), s              | 7.7  | 0.0      | 14.3 | 0.5      | 0.0      | 21.9  | 12.6 | 11.1    | 0.8  | 4.3      | 5.2      | 6.6      |
| Cycle Q Clear(g_c), s        | 7.7  | 0.0      | 14.3 | 0.5      | 0.0      | 21.9  | 12.6 | 11.1    | 0.8  | 4.3      | 5.2      | 6.6      |
| Prop In Lane                 | 1.00 |          | 0.42 | 1.00     |          | 0.41  | 1.00 |         | 1.00 | 1.00     |          | 1.00     |
| Lane Grp Cap(c), veh/h       | 319  | 0        | 311  | 438      | 0        | 428   | 258  | 557     | 473  | 109      | 395      | 336      |
| V/C Ratio(X)                 | 0.51 | 0.00     | 0.88 | 0.03     | 0.00     | 1.14  | 0.98 | 0.51    | 0.04 | 0.79     | 0.32     | 0.40     |
| Avail Cap(c_a), veh/h        | 343  | 0        | 335  | 438      | 0        | 428   | 258  | 557     | 473  | 143      | 395      | 336      |
| HCM Platoon Ratio            | 1.00 | 1.00     | 1.00 | 1.00     | 1.00     | 1.00  | 1.00 | 1.00    | 1.00 | 1.00     | 1.00     | 1.00     |
| Upstream Filter(I)           | 1.00 | 0.00     | 1.00 | 1.00     | 0.00     | 1.00  | 1.00 | 1.00    | 1.00 | 1.00     | 1.00     | 1.00     |
| Uniform Delay (d), s/veh     | 32.4 | 0.0      | 35.0 | 25.4     | 0.0      | 33.4  | 37.8 | 25.7    | 22.1 | 41.0     | 29.3     | 29.8     |
| Incr Delay (d2), s/veh       | 1.3  | 0.0      | 21.6 | 0.0      | 0.0      | 86.4  | 49.5 | 3.3     | 0.2  | 18.9     | 2.1      | 3.5      |
| Initial Q Delay(d3),s/veh    | 0.0  | 0.0      | 0.0  | 0.0      | 0.0      | 0.0   | 0.0  | 0.0     | 0.0  | 0.0      | 0.0      | 0.0      |
| %ile BackOfQ(50%),veh/ln     | 3.7  | 0.0      | 8.4  | 0.3      | 0.0      | 20.6  | 9.6  | 6.2     | 0.4  | 2.7      | 2.8      | 3.2      |
| LnGrp Delay(d),s/veh         | 33.6 | 0.0      | 56.6 | 25.4     | 0.0      | 119.8 | 87.2 | 29.0    | 22.3 | 59.9     | 31.4     | 33.3     |
| LnGrp LOS                    | С    |          | Е    | С        |          | F     | F    | С       | С    | E        | С        | <u>C</u> |
| Approach Vol, veh/h          |      | 438      |      |          | 501      |       |      | 556     |      |          | 347      |          |
| Approach Delay, s/veh        |      | 48.0     |      |          | 117.2    |       |      | 55.1    |      |          | 39.2     |          |
| Approach LOS                 |      | D        |      |          | F        |       |      | Е       |      |          | D        |          |
| Timer                        | 1    | 2        | 3    | 4        | 5        | 6     | 7    | 8       |      |          |          |          |
| Assigned Phs                 | 1    | 2        |      | 4        | 5        | 6     |      | 8       |      |          |          |          |
| Phs Duration (G+Y+Rc), s     | 10.1 | 31.0     |      | 21.2     | 17.4     | 23.7  |      | 26.4    |      |          |          |          |
| Change Period (Y+Rc), s      | 4.5  | 4.5      |      | 4.5      | 4.5      | 4.5   |      | 4.5     |      |          |          |          |
| Max Green Setting (Gmax), s  | 7.3  | 24.8     |      | 18.0     | 12.9     | 19.2  |      | 21.9    |      |          |          |          |
| Max Q Clear Time (g_c+l1), s | 6.3  | 13.1     |      | 16.3     | 14.6     | 8.6   |      | 23.9    |      |          |          |          |
| Green Ext Time (p_c), s      | 0.0  | 1.3      |      | 0.4      | 0.0      | 8.0   |      | 0.0     |      |          |          |          |
| Intersection Summary         |      |          |      |          |          |       |      |         |      |          |          |          |
| HCM 2010 Ctrl Delay          |      |          | 67.3 |          |          |       |      |         |      |          |          |          |
| HCM 2010 LOS                 |      |          | Е    |          |          |       |      |         |      |          |          |          |

| Traffic Volume (veh/h)         6         274         95         69         576         15         143         51         98         17           Future Volume (veh/h)         6         274         95         69         576         15         143         51         98         17           Number         7         4         14         3         8         18         5         2         12         1           Initial Q (Qb), veh         0         1         0         0         1         0         0         1         0         0         1   | 8 12<br>8 12<br>6 16<br>0 0<br>1.00<br>0 1.00<br>6 1900<br>0 14<br>1 0 |
|--|--|
| Traffic Volume (veh/h) 6 274 95 69 576 15 143 51 98 17  Future Volume (veh/h) 6 274 95 69 576 15 143 51 98 17  Number 7 4 14 3 8 18 5 2 12 1  Initial Q (Qb), veh 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0  Ped-Bike Adj(A_pbT) 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.0  | 8 12<br>8 12<br>6 16<br>0 0<br>1.00<br>0 1.00<br>6 1900<br>0 14<br>1 0 |
| Traffic Volume (veh/h) 6 274 95 69 576 15 143 51 98 17  Future Volume (veh/h) 6 274 95 69 576 15 143 51 98 17  Number 7 4 14 3 8 18 5 2 12 1  Initial Q (Qb), veh 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0  Ped-Bike Adj(A_pbT) 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.0  | 8 12<br>8 12<br>6 16<br>0 0<br>1.00<br>0 1.00<br>6 1900<br>0 14<br>1 0 |
| Future Volume (veh/h)         6         274         95         69         576         15         143         51         98         17           Number         7         4         14         3         8         18         5         2         12         1           Initial Q (Qb), veh         0         1         0         0         1  | 8 12<br>6 16<br>0 0<br>1.00<br>0 1.00<br>6 1900<br>0 14<br>1 0         |
| Number         7         4         14         3         8         18         5         2         12         1           Initial Q (Qb), veh         0         1         0.00         1         1.00         1         1.00         1         1.00         1         1.00         1         1.00         0         1         0         0         0         0         0         0         0         0         0         0         0         0 </td <td>6 16<br/>0 0<br/>1.00<br/>0 1.00<br/>6 1900<br/>0 14<br/>1 0</td>   | 6 16<br>0 0<br>1.00<br>0 1.00<br>6 1900<br>0 14<br>1 0                 |
| Ped-Bike Adj(A_pbT)         1.00 </td <td>0 0<br/>1.00<br/>0 1.00<br/>6 1900<br/>0 14<br/>1 0</td> | 0 0<br>1.00<br>0 1.00<br>6 1900<br>0 14<br>1 0                         |
| Ped-Bike Adj(A_pbT)         1.00 </td <td>0 1.00<br/>6 1900<br/>0 14<br/>1 0</td>                  | 0 1.00<br>6 1900<br>0 14<br>1 0  |
| Parking Bus, Adj         1.00  | 0 1.00<br>6 1900<br>0 14<br>1 0  |
| Adj Sat Flow, veh/h/ln         1827         1827         1900         1845         1845         1900         1900         1810         1900         1900         17           Adj Flow Rate, veh/h         7         311         108         78         655         17         162         58         111         19         1846         1900 <td>0 14<br/>1 0</td>   | 0 14<br>1 0  |
| Adj Flow Rate, veh/h       7       311       108       78       655       17       162       58       111       19       19         Adj No. of Lanes       1       1       0       1       1       0       0       1       0       0         Peak Hour Factor       0.88<   | 0 14<br>1 0  |
| Adj No. of Lanes         1         1         0         1         1         0         0         1         0         0           Peak Hour Factor         0.88         0.84         0.34         0.34         0.34 <td>1 0</td>   | 1 0  |
| Peak Hour Factor         0.88         0.85         0.0           Cap, veh/h         16         470         163         110         745         19         310         118         168         230         22           Grp Volume(v), veh/h         7         0         419         78         0         672         331   | 3 0.88   |
| Percent Heavy Veh, %         4         4         4         4         3         3         3         5         5         5         7           Cap, veh/h         16         470         163         110         745         19         310         118         168         230         22           Arrive On Green         0.01         0.36         0.36         0.06         0.42         0.42         0.34         <   |  |
| Cap, veh/h         16         470         163         110         745         19         310         118         168         230         22           Arrive On Green         0.01         0.36         0.36         0.06         0.42         0.42         0.34 <td< td=""><td>7 7</td></td<>  | 7 7  |
| $ \begin{array}{c ccccccccccccccccccccccccccccccccccc$   |  |
| Sat Flow, veh/h         1740         1297         450         1757         1790         46         640         351         500         428         68           Grp Volume(v), veh/h         7         0         419         78         0         672         331         0         0         53           Grp Sat Flow(s),veh/h/ln         1740         0         1747         1757         0         1836         1491         0         0         1511           Q Serve(g_s), s         0.2         0.0         11.3         2.5         0.0         19.0         8.5         0.0  | 4 0.34   |
| Grp Volume(v), veh/h         7         0         419         78         0         672         331         0         0         53           Grp Sat Flow(s),veh/h/ln         1740         0         1747         1757         0         1836         1491         0         0         1511           Q Serve(g_s), s         0.2         0.0         11.3         2.5         0.0         19.0         8.5         0.0  |  |
| $ \begin{array}{cccccccccccccccccccccccccccccccccccc$  | 0 0  |
| $ \begin{array}{cccccccccccccccccccccccccccccccccccc$  | 0 0  |
| $ \begin{array}{cccccccccccccccccccccccccccccccccccc$  |  |
| Prop In Lane       1.00       0.26       1.00       0.03       0.49       0.34       0.36         Lane Grp Cap(c), veh/h       16       0       634       110       0       764       595       0       0       593  |  |
| Lane Grp Cap(c), veh/h 16 0 634 110 0 764 595 0 0 593  | 0.26   |
|  | 0 0  |
| V/C Ratio(X) 0.44 0.00 0.66 0.71 0.00 0.88 0.56 0.00 0.00 0.09 0.0   |  |
| Avail Cap(c_a), veh/h 157 0 797 215 0 896 595 0 0 593  | 0 0  |
| HCM Platoon Ratio 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.0   |  |
| Upstream Filter(I) 1.00 0.00 1.00 1.00 0.00 1.00 0.00 0.0  |  |
| Uniform Delay (d), s/veh 27.8 0.0 15.1 25.9 0.0 15.2 15.8 0.0 0.0 12.9 0   |  |
| Incr Delay (d2), s/veh 17.6 0.0 1.4 8.1 0.0 9.0 3.7 0.0 0.0 0.3 0  |  |
| Initial Q Delay(d3),s/veh 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.   |  |
| %ile BackOfQ(50%),veh/ln 0.2 0.0 5.7 1.4 0.0 11.4 4.9 0.0 0.0 0.6 0  |  |
| LnGrp Delay(d),s/veh 45.4 0.0 16.5 34.1 0.0 24.1 19.6 0.0 0.0 13.2 0   |  |
| LnGrp LOS D B C C B B  |  |
|  | 3  |
| Approach Delay, s/veh 16.9 25.2 19.6 13  |  |
| Approach LOS B C B   | 3  |
| Timer 1 2 3 4 5 6 7 8  |  |
| Assigned Phs 2 3 4 6 7 8   |  |
| Phs Duration (G+Y+Rc), s 23.4 8.0 24.9 23.4 5.0 28.0   |  |
| Change Period (Y+Rc), s 4.5 4.5 4.5 4.5 4.5  |  |
| Max Green Setting (Gmax), s 18.9 6.9 25.7 18.9 5.1 27.5  |  |
| Max Q Clear Time (g_c+l1), s 12.5 4.5 13.3 3.2 2.2 21.0  |  |
| Green Ext Time (p_c), s 1.1 0.0 2.1 0.2 0.0 2.5  |  |
| Intersection Summary   |  |
| HCM 2010 Ctrl Delay 21.3   |  |
| HCM 2010 LOS C   |  |

|                              |      | <b>→</b> | <b>←</b> | •    | <b>\</b> | 4    |      |      |  |  |
|------------------------------|------|----------|----------|------|----------|------|------|------|--|--|
| Movement                     | EBL  | EBT      | WBT      | WBR  | SBL      | SBR  |      |      |  |  |
| Lane Configurations          | ሻ    | <b>1</b> | <b>^</b> | 7    | ሻ        | 7    |      |      |  |  |
| Traffic Volume (veh/h)       | 146  | 198      | 386      | 356  | 180      | 169  |      |      |  |  |
| Future Volume (veh/h)        | 146  | 198      | 386      | 356  | 180      | 169  |      |      |  |  |
| Number                       | 7    | 4        | 8        | 18   | 1        | 16   |      |      |  |  |
| Initial Q (Qb), veh          | 0    | 0        | 0        | 0    | 0        | 0    |      |      |  |  |
| Ped-Bike Adj(A_pbT)          | 1.00 |          |          | 1.00 | 1.00     | 1.00 |      |      |  |  |
| Parking Bus, Adj             | 1.00 | 1.00     | 1.00     | 1.00 | 1.00     | 1.00 |      |      |  |  |
| Adj Sat Flow, veh/h/ln       | 1810 | 1810     | 1863     | 1863 | 1863     | 1863 |      |      |  |  |
| Adj Flow Rate, veh/h         | 166  | 225      | 439      | 405  | 205      | 192  |      |      |  |  |
| Adj No. of Lanes             | 1    | 1        | 1        | 1    | 1        | 1    |      |      |  |  |
| Peak Hour Factor             | 0.88 | 0.88     | 0.88     | 0.88 | 0.88     | 0.88 |      |      |  |  |
| Percent Heavy Veh, %         | 5    | 5        | 2        | 2    | 2        | 2    |      |      |  |  |
| Cap, veh/h                   | 213  | 983      | 611      | 520  | 486      | 434  |      |      |  |  |
| Arrive On Green              | 0.12 | 0.54     | 0.33     | 0.33 | 0.27     | 0.27 |      |      |  |  |
| Sat Flow, veh/h              | 1723 | 1810     | 1863     | 1583 | 1774     | 1583 |      |      |  |  |
| Grp Volume(v), veh/h         | 166  | 225      | 439      | 405  | 205      | 192  |      |      |  |  |
| Grp Sat Flow(s), veh/h/ln    | 1723 | 1810     | 1863     | 1583 | 1774     | 1583 |      |      |  |  |
| Q Serve(g_s), s              | 4.6  | 3.2      | 10.2     | 11.4 | 4.7      | 4.9  |      |      |  |  |
| Cycle Q Clear(g_c), s        | 4.6  | 3.2      | 10.2     | 11.4 | 4.7      | 4.9  |      |      |  |  |
|                              | 1.00 | 3.2      | 10.2     | 1.00 | 1.00     | 1.00 |      |      |  |  |
| Prop In Lane                 | 213  | 983      | 611      | 520  | 486      | 434  |      |      |  |  |
| Lane Grp Cap(c), veh/h       | 0.78 | 0.23     | 0.72     | 0.78 | 0.42     | 0.44 |      |      |  |  |
| V/C Ratio(X)                 | 403  | 1378     | 813      | 691  | 486      | 434  |      |      |  |  |
| Avail Cap(c_a), veh/h        |      |          |          |      |          | 1.00 |      |      |  |  |
| HCM Platoon Ratio            | 1.00 | 1.00     | 1.00     | 1.00 | 1.00     |      |      |      |  |  |
| Upstream Filter(I)           | 1.00 | 1.00     | 1.00     | 1.00 | 1.00     | 1.00 |      |      |  |  |
| Uniform Delay (d), s/veh     | 20.9 | 5.9      | 14.5     | 14.9 | 14.7     | 14.8 |      |      |  |  |
| Incr Delay (d2), s/veh       | 6.1  | 0.1      | 2.1      | 4.1  | 2.7      | 3.2  |      |      |  |  |
| Initial Q Delay(d3),s/veh    | 0.0  | 0.0      | 0.0      | 0.0  | 0.0      | 0.0  |      |      |  |  |
| %ile BackOfQ(50%),veh/ln     | 2.5  | 1.6      | 5.5      | 5.5  | 2.6      | 4.9  |      |      |  |  |
| LnGrp Delay(d),s/veh         | 27.0 | 6.0      | 16.6     | 19.1 | 17.3     | 18.0 |      |      |  |  |
| LnGrp LOS                    | С    | Α        | В        | В    | В        | В    |      |      |  |  |
| Approach Vol, veh/h          |      | 391      | 844      |      | 397      |      |      |      |  |  |
| Approach Delay, s/veh        |      | 14.9     | 17.8     |      | 17.7     |      |      |      |  |  |
| Approach LOS                 |      | В        | В        |      | В        |      |      |      |  |  |
| Timer                        | 1    | 2        | 3        | 4    | 5        | 6    | 7    | 8    |  |  |
| Assigned Phs                 |      |          |          | 4    |          | 6    | 7    | 8    |  |  |
| Phs Duration (G+Y+Rc), s     |      |          |          | 31.2 |          | 18.0 | 10.6 | 20.7 |  |  |
| Change Period (Y+Rc), s      |      |          |          | 4.5  |          | 4.5  | 4.5  | 4.5  |  |  |
| Max Green Setting (Gmax), s  |      |          |          | 37.5 |          | 13.5 | 11.5 | 21.5 |  |  |
| Max Q Clear Time (g_c+I1), s |      |          |          | 5.2  |          | 6.9  | 6.6  | 13.4 |  |  |
| Green Ext Time (p_c), s      |      |          |          | 1.4  |          | 0.7  | 0.2  | 2.8  |  |  |
| ntersection Summary          |      |          |          |      |          |      |      |      |  |  |
| HCM 2010 Ctrl Delay          |      |          | 17.1     |      |          |      |      |      |  |  |
| HCM 2010 LOS                 |      |          | В        |      |          |      |      |      |  |  |

|                                | ۶         | <b>→</b> | •     | •     | <b>—</b>    | •          | •        | <b>†</b> | ~    | <b>\</b> | <b>↓</b> | ✓    |
|--------------------------------|-----------|----------|-------|-------|-------------|------------|----------|----------|------|----------|----------|------|
| Movement                       | EBL       | EBT      | EBR   | WBL   | WBT         | WBR        | NBL      | NBT      | NBR  | SBL      | SBT      | SBR  |
| Lane Configurations            | ሻ         | <b>†</b> | 7     | 7     | ₽           |            |          | ર્ન      | 7    |          | 4        | 7    |
| Traffic Volume (vph)           | 11        | 492      | 262   | 9     | 667         | 28         | 543      | 25       | 3    | 46       | 23       | 5    |
| Future Volume (vph)            | 11        | 492      | 262   | 9     | 667         | 28         | 543      | 25       | 3    | 46       | 23       | 5    |
| Ideal Flow (vphpl)             | 1900      | 1900     | 1900  | 1900  | 1900        | 1900       | 1900     | 1900     | 1900 | 1900     | 1900     | 1900 |
| Total Lost time (s)            | 4.5       | 4.5      | 4.5   | 4.5   | 4.5         |            |          | 4.5      | 4.5  |          | 4.5      | 4.5  |
| Lane Util. Factor              | 1.00      | 1.00     | 1.00  | 1.00  | 1.00        |            |          | 1.00     | 1.00 |          | 1.00     | 1.00 |
| Frt                            | 1.00      | 1.00     | 0.85  | 1.00  | 0.99        |            |          | 1.00     | 0.85 |          | 1.00     | 0.85 |
| Flt Protected                  | 0.95      | 1.00     | 1.00  | 0.95  | 1.00        |            |          | 0.95     | 1.00 |          | 0.97     | 1.00 |
| Satd. Flow (prot)              | 1612      | 1696     | 1442  | 1543  | 1614        |            |          | 1778     | 1583 |          | 1751     | 1538 |
| Flt Permitted                  | 0.95      | 1.00     | 1.00  | 0.95  | 1.00        |            |          | 0.95     | 1.00 |          | 0.97     | 1.00 |
| Satd. Flow (perm)              | 1612      | 1696     | 1442  | 1543  | 1614        |            |          | 1778     | 1583 |          | 1751     | 1538 |
| Peak-hour factor, PHF          | 0.96      | 0.96     | 0.96  | 0.96  | 0.96        | 0.96       | 0.96     | 0.96     | 0.96 | 0.96     | 0.96     | 0.96 |
| Adj. Flow (vph)                | 11        | 512      | 273   | 9     | 695         | 29         | 566      | 26       | 3    | 48       | 24       | 5    |
| RTOR Reduction (vph)           | 0         | 0        | 150   | 0     | 1           | 0          | 0        | 0        | 2    | 0        | 0        | 5    |
| Lane Group Flow (vph)          | 11        | 513      | 123   | 9     | 723         | 0          | 0        | 592      | 1    | 0        | 72       | 0    |
| Heavy Vehicles (%)             | 12%       | 12%      | 12%   | 17%   | 17%         | 17%        | 2%       | 2%       | 2%   | 5%       | 5%       | 5%   |
| Turn Type                      | Prot      | NA       | Perm  | Prot  | NA          |            | Split    | NA       | Perm | Split    | NA       | Perm |
| Protected Phases               | 7         | 4        |       | 3     | 8           |            | 5        | 5        |      | 6        | 6        |      |
| Permitted Phases               |           |          | 4     |       |             |            |          |          | 5    |          |          | 6    |
| Actuated Green, G (s)          | 0.9       | 51.7     | 51.7  | 0.9   | 51.7        |            |          | 38.6     | 38.6 |          | 5.5      | 5.5  |
| Effective Green, g (s)         | 0.9       | 51.7     | 51.7  | 0.9   | 51.7        |            |          | 38.6     | 38.6 |          | 5.5      | 5.5  |
| Actuated g/C Ratio             | 0.01      | 0.45     | 0.45  | 0.01  | 0.45        |            |          | 0.34     | 0.34 |          | 0.05     | 0.05 |
| Clearance Time (s)             | 4.5       | 4.5      | 4.5   | 4.5   | 4.5         |            |          | 4.5      | 4.5  |          | 4.5      | 4.5  |
| Vehicle Extension (s)          | 3.0       | 3.0      | 3.0   | 3.0   | 3.0         |            |          | 3.0      | 3.0  |          | 3.0      | 3.0  |
| Lane Grp Cap (vph)             | 12        | 764      | 649   | 12    | 727         |            |          | 598      | 532  |          | 83       | 73   |
| v/s Ratio Prot                 | c0.01     | 0.30     |       | 0.01  | c0.45       |            |          | c0.33    |      |          | c0.04    |      |
| v/s Ratio Perm                 |           |          | 0.09  |       |             |            |          |          | 0.00 |          |          | 0.00 |
| v/c Ratio                      | 0.92      | 0.67     | 0.19  | 0.75  | 0.99        |            |          | 0.99     | 0.00 |          | 0.87     | 0.00 |
| Uniform Delay, d1              | 56.9      | 24.8     | 18.9  | 56.8  | 31.4        |            |          | 37.9     | 25.3 |          | 54.2     | 52.0 |
| Progression Factor             | 1.00      | 1.00     | 1.00  | 1.00  | 1.00        |            |          | 1.00     | 1.00 |          | 1.00     | 1.00 |
| Incremental Delay, d2          | 212.2     | 4.7      | 0.6   | 128.3 | 32.0        |            |          | 33.8     | 0.0  |          | 56.5     | 0.0  |
| Delay (s)                      | 269.0     | 29.5     | 19.6  | 185.1 | 63.4        |            |          | 71.7     | 25.3 |          | 110.8    | 52.0 |
| Level of Service               | F         | С        | В     | F     | E           |            |          | E        | С    |          | F        | D    |
| Approach Delay (s)             |           | 29.4     |       |       | 64.9        |            |          | 71.5     |      |          | 107.0    |      |
| Approach LOS                   |           | С        |       |       | E           |            |          | E        |      |          | F        |      |
| Intersection Summary           |           |          |       |       | 011 0000    | 1          | <u> </u> |          |      |          |          |      |
| HCM 2000 Control Delay         |           |          | 55.3  | Н     | CM 2000     | Level of   | Service  |          | E    |          |          |      |
| HCM 2000 Volume to Capac       | ity ratio |          | 0.98  |       |             |            |          |          | 40.0 |          |          |      |
| Actuated Cycle Length (s)      |           |          | 114.7 |       | um of lost  |            |          |          | 18.0 |          |          |      |
| Intersection Capacity Utilizat | ion       |          | 83.6% | IC    | CU Level of | of Service |          |          | Е    |          |          |      |
| Analysis Period (min)          |           |          | 15    |       |             |            |          |          |      |          |          |      |
| c Critical Lane Group          |           |          |       |       |             |            |          |          |      |          |          |      |

|                              | ۶     | <b>→</b> | •    | •     | <b>←</b> | •    | •    | <b>†</b>    | <b>/</b> | <b>/</b> | <b>↓</b> | 4    |
|------------------------------|-------|----------|------|-------|----------|------|------|-------------|----------|----------|----------|------|
| Movement                     | EBL   | EBT      | EBR  | WBL   | WBT      | WBR  | NBL  | NBT         | NBR      | SBL      | SBT      | SBR  |
| Lane Configurations          | 14.54 | <b>^</b> | 7    | 7     | <b>^</b> | 7    | ሻሻ   | <b>↑</b> ↑↑ |          | ሻሻ       | <b>^</b> | 7    |
| Traffic Volume (veh/h)       | 234   | 227      | 116  | 149   | 381      | 193  | 166  | 576         | 66       | 169      | 415      | 181  |
| Future Volume (veh/h)        | 234   | 227      | 116  | 149   | 381      | 193  | 166  | 576         | 66       | 169      | 415      | 181  |
| Number                       | 7     | 4        | 14   | 3     | 8        | 18   | 5    | 2           | 12       | 1        | 6        | 16   |
| Initial Q (Qb), veh          | 0     | 0        | 0    | 0     | 0        | 0    | 0    | 0           | 0        | 0        | 0        | 0    |
| Ped-Bike Adj(A_pbT)          | 1.00  |          | 0.98 | 1.00  |          | 0.96 | 1.00 |             | 1.00     | 1.00     |          | 1.00 |
| Parking Bus, Adj             | 1.00  | 1.00     | 1.00 | 1.00  | 1.00     | 1.00 | 1.00 | 1.00        | 1.00     | 1.00     | 1.00     | 1.00 |
| Adj Sat Flow, veh/h/ln       | 1863  | 1863     | 1863 | 1863  | 1863     | 1863 | 1863 | 1863        | 1900     | 1845     | 1845     | 1845 |
| Adj Flow Rate, veh/h         | 257   | 249      | 127  | 164   | 419      | 212  | 182  | 633         | 73       | 186      | 456      | 199  |
| Adj No. of Lanes             | 2     | 2        | 1    | 1     | 2        | 1    | 2    | 3           | 0        | 2        | 3        | 1    |
| Peak Hour Factor             | 0.91  | 0.91     | 0.91 | 0.91  | 0.91     | 0.91 | 0.91 | 0.91        | 0.91     | 0.91     | 0.91     | 0.91 |
| Percent Heavy Veh, %         | 2     | 2        | 2    | 2     | 2        | 2    | 2    | 2           | 2        | 3        | 3        | 3    |
| Cap, veh/h                   | 307   | 796      | 477  | 161   | 802      | 346  | 277  | 1413        | 161      | 280      | 1546     | 619  |
| Arrive On Green              | 0.09  | 0.23     | 0.23 | 0.09  | 0.23     | 0.23 | 0.08 | 0.31        | 0.31     | 0.08     | 0.31     | 0.31 |
| Sat Flow, veh/h              | 3442  | 3539     | 1554 | 1774  | 3539     | 1525 | 3442 | 4630        | 529      | 3408     | 5036     | 1562 |
| Grp Volume(v), veh/h         | 257   | 249      | 127  | 164   | 419      | 212  | 182  | 462         | 244      | 186      | 456      | 199  |
| Grp Sat Flow(s),veh/h/ln     | 1721  | 1770     | 1554 | 1774  | 1770     | 1525 | 1721 | 1695        | 1768     | 1704     | 1679     | 1562 |
| Q Serve(g_s), s              | 4.5   | 3.6      | 3.7  | 5.5   | 6.3      | 7.6  | 3.1  | 6.6         | 6.7      | 3.2      | 4.2      | 5.3  |
| Cycle Q Clear(g_c), s        | 4.5   | 3.6      | 3.7  | 5.5   | 6.3      | 7.6  | 3.1  | 6.6         | 6.7      | 3.2      | 4.2      | 5.3  |
| Prop In Lane                 | 1.00  |          | 1.00 | 1.00  |          | 1.00 | 1.00 |             | 0.30     | 1.00     |          | 1.00 |
| Lane Grp Cap(c), veh/h       | 307   | 796      | 477  | 161   | 802      | 346  | 277  | 1034        | 540      | 280      | 1546     | 619  |
| V/C Ratio(X)                 | 0.84  | 0.31     | 0.27 | 1.02  | 0.52     | 0.61 | 0.66 | 0.45        | 0.45     | 0.66     | 0.29     | 0.32 |
| Avail Cap(c_a), veh/h        | 307   | 1051     | 589  | 161   | 1057     | 455  | 284  | 1034        | 540      | 281      | 1546     | 619  |
| HCM Platoon Ratio            | 1.00  | 1.00     | 1.00 | 1.00  | 1.00     | 1.00 | 1.00 | 1.00        | 1.00     | 1.00     | 1.00     | 1.00 |
| Upstream Filter(I)           | 1.00  | 1.00     | 1.00 | 1.00  | 1.00     | 1.00 | 1.00 | 1.00        | 1.00     | 1.00     | 1.00     | 1.00 |
| Uniform Delay (d), s/veh     | 27.2  | 19.6     | 15.9 | 27.6  | 20.6     | 21.1 | 27.1 | 16.9        | 17.0     | 27.0     | 16.0     | 12.7 |
| Incr Delay (d2), s/veh       | 18.2  | 0.2      | 0.3  | 76.0  | 0.5      | 1.8  | 5.3  | 1.4         | 2.7      | 5.7      | 0.5      | 1.4  |
| Initial Q Delay(d3),s/veh    | 0.0   | 0.0      | 0.0  | 0.2   | 0.0      | 0.0  | 0.0  | 0.0         | 0.0      | 0.0      | 0.0      | 0.0  |
| %ile BackOfQ(50%),veh/ln     | 2.9   | 1.8      | 1.6  | 6.0   | 3.1      | 3.3  | 1.7  | 3.3         | 3.7      | 1.7      | 2.0      | 2.5  |
| LnGrp Delay(d),s/veh         | 45.4  | 19.8     | 16.2 | 103.8 | 21.1     | 22.8 | 32.4 | 18.3        | 19.7     | 32.7     | 16.5     | 14.0 |
| LnGrp LOS                    | D     | В        | В    | F     | С        | С    | С    | В           | В        | С        | В        | В    |
| Approach Vol, veh/h          |       | 633      |      |       | 795      |      |      | 888         |          |          | 841      |      |
| Approach Delay, s/veh        |       | 29.5     |      |       | 38.6     |      |      | 21.6        |          |          | 19.5     |      |
| Approach LOS                 |       | С        |      |       | D        |      |      | С           |          |          | В        |      |
| Timer                        | 1     | 2        | 3    | 4     | 5        | 6    | 7    | 8           |          |          |          |      |
| Assigned Phs                 | 1     | 2        | 3    | 4     | 5        | 6    | 7    | 8           |          |          |          |      |
| Phs Duration (G+Y+Rc), s     | 9.5   | 23.0     | 10.0 | 18.1  | 9.4      | 23.1 | 9.9  | 18.2        |          |          |          |      |
| Change Period (Y+Rc), s      | 4.5   | 4.5      | 4.5  | 4.5   | 4.5      | 4.5  | 4.5  | 4.5         |          |          |          |      |
| Max Green Setting (Gmax), s  | 5.0   | 18.5     | 5.5  | 18.0  | 5.0      | 18.5 | 5.4  | 18.1        |          |          |          |      |
| Max Q Clear Time (g_c+l1), s | 5.2   | 8.7      | 7.5  | 5.7   | 5.1      | 7.3  | 6.5  | 9.6         |          |          |          |      |
| Green Ext Time (p_c), s      | 0.0   | 3.2      | 0.0  | 1.6   | 0.0      | 2.9  | 0.0  | 2.3         |          |          |          |      |
| Intersection Summary         |       |          |      |       |          |      |      |             |          |          |          |      |
| HCM 2010 Ctrl Delay          |       |          | 26.9 |       |          |      |      |             |          |          |          |      |
| HCM 2010 LOS                 |       |          | С    |       |          |      |      |             |          |          |          |      |

Lico Subdivision Keith Higgins Traffic Engineer

|                              | •    | <b>→</b> | •    | •    | <b>←</b> | •    | •    | †        | ~    | <b>\</b> | <b></b> |      |
|------------------------------|------|----------|------|------|----------|------|------|----------|------|----------|---------|------|
| Movement                     | EBL  | EBT      | EBR  | WBL  | WBT      | WBR  | NBL  | NBT      | NBR  | SBL      | SBT     | SBR  |
| Lane Configurations          | ሻ    | 1}•      |      | ሻ    | ĵ»       |      | ሻ    | <b>†</b> | 7    | ሻ        | 1}•     |      |
| Traffic Volume (veh/h)       | 33   | 153      | 39   | 157  | 154      | 142  | 70   | 127      | 177  | 103      | 50      | 4    |
| Future Volume (veh/h)        | 33   | 153      | 39   | 157  | 154      | 142  | 70   | 127      | 177  | 103      | 50      | 4    |
| Number                       | 7    | 4        | 14   | 3    | 8        | 18   | 5    | 2        | 12   | 1        | 6       | 16   |
| Initial Q (Qb), veh          | 0    | 0        | 0    | 0    | 0        | 0    | 0    | 0        | 0    | 0        | 0       | 0    |
| Ped-Bike Adj(A_pbT)          | 1.00 |          | 0.73 | 1.00 |          | 0.89 | 1.00 |          | 0.99 | 1.00     |         | 0.99 |
| Parking Bus, Adj             | 1.00 | 1.00     | 1.00 | 1.00 | 1.00     | 1.00 | 1.00 | 1.00     | 1.00 | 1.00     | 1.00    | 1.00 |
| Adj Sat Flow, veh/h/ln       | 1863 | 1863     | 1900 | 1863 | 1863     | 1900 | 1863 | 1863     | 1863 | 1863     | 1863    | 1900 |
| Adj Flow Rate, veh/h         | 43   | 201      | 51   | 207  | 203      | 187  | 92   | 167      | 233  | 136      | 66      | 5    |
| Adj No. of Lanes             | 1    | 1        | 0    | 1    | 1        | 0    | 1    | 1        | 1    | 1        | 1       | 0    |
| Peak Hour Factor             | 0.76 | 0.76     | 0.76 | 0.76 | 0.76     | 0.76 | 0.76 | 0.76     | 0.76 | 0.76     | 0.76    | 0.76 |
| Percent Heavy Veh, %         | 2    | 2        | 2    | 2    | 2        | 2    | 2    | 2        | 2    | 2        | 2       | 2    |
| Cap, veh/h                   | 72   | 330      | 84   | 236  | 286      | 264  | 118  | 492      | 416  | 167      | 498     | 38   |
| Arrive On Green              | 0.04 | 0.25     | 0.25 | 0.13 | 0.34     | 0.34 | 0.07 | 0.26     | 0.26 | 0.09     | 0.29    | 0.29 |
| Sat Flow, veh/h              | 1774 | 1325     | 336  | 1774 | 838      | 772  | 1774 | 1863     | 1574 | 1774     | 1709    | 129  |
| Grp Volume(v), veh/h         | 43   | 0        | 252  | 207  | 0        | 390  | 92   | 167      | 233  | 136      | 0       | 71   |
| Grp Sat Flow(s),veh/h/ln     | 1774 | 0        | 1661 | 1774 | 0        | 1611 | 1774 | 1863     | 1574 | 1774     | 0       | 1838 |
| Q Serve(g_s), s              | 1.7  | 0.0      | 9.3  | 7.9  | 0.0      | 14.6 | 3.5  | 5.0      | 8.8  | 5.2      | 0.0     | 2.0  |
| Cycle Q Clear(g_c), s        | 1.7  | 0.0      | 9.3  | 7.9  | 0.0      | 14.6 | 3.5  | 5.0      | 8.8  | 5.2      | 0.0     | 2.0  |
| Prop In Lane                 | 1.00 |          | 0.20 | 1.00 |          | 0.48 | 1.00 |          | 1.00 | 1.00     |         | 0.07 |
| Lane Grp Cap(c), veh/h       | 72   | 0        | 413  | 236  | 0        | 550  | 118  | 492      | 416  | 167      | 0       | 536  |
| V/C Ratio(X)                 | 0.60 | 0.00     | 0.61 | 0.88 | 0.00     | 0.71 | 0.78 | 0.34     | 0.56 | 0.82     | 0.00    | 0.13 |
| Avail Cap(c_a), veh/h        | 131  | 0        | 432  | 236  | 0        | 550  | 159  | 492      | 416  | 167      | 0       | 536  |
| HCM Platoon Ratio            | 1.00 | 1.00     | 1.00 | 1.00 | 1.00     | 1.00 | 1.00 | 1.00     | 1.00 | 1.00     | 1.00    | 1.00 |
| Upstream Filter(I)           | 1.00 | 0.00     | 1.00 | 1.00 | 0.00     | 1.00 | 1.00 | 1.00     | 1.00 | 1.00     | 0.00    | 1.00 |
| Uniform Delay (d), s/veh     | 32.7 | 0.0      | 23.0 | 29.5 | 0.0      | 19.8 | 31.8 | 20.6     | 22.0 | 30.8     | 0.0     | 18.1 |
| Incr Delay (d2), s/veh       | 7.7  | 0.0      | 2.3  | 29.1 | 0.0      | 4.2  | 15.9 | 1.9      | 5.4  | 26.1     | 0.0     | 0.5  |
| Initial Q Delay(d3),s/veh    | 0.0  | 0.0      | 0.0  | 0.0  | 0.0      | 0.0  | 0.0  | 0.0      | 0.0  | 0.0      | 0.0     | 0.0  |
| %ile BackOfQ(50%),veh/ln     | 1.0  | 0.0      | 4.5  | 5.8  | 0.0      | 7.0  | 2.3  | 2.8      | 4.4  | 3.7      | 0.0     | 1.1  |
| LnGrp Delay(d),s/veh         | 40.3 | 0.0      | 25.3 | 58.6 | 0.0      | 24.0 | 47.7 | 22.4     | 27.4 | 56.8     | 0.0     | 18.6 |
| LnGrp LOS                    | D    |          | С    | E    |          | С    | D    | С        | С    | E        |         | B    |
| Approach Vol, veh/h          |      | 295      |      |      | 597      |      |      | 492      |      |          | 207     |      |
| Approach Delay, s/veh        |      | 27.5     |      |      | 36.0     |      |      | 29.5     |      |          | 43.7    |      |
| Approach LOS                 |      | С        |      |      | D        |      |      | С        |      |          | D       |      |
| Timer                        | 1    | 2        | 3    | 4    | 5        | 6    | 7    | 8        |      |          |         |      |
| Assigned Phs                 | 1    | 2        | 3    | 4    | 5        | 6    | 7    | 8        |      |          |         |      |
| Phs Duration (G+Y+Rc), s     | 11.0 | 22.8     | 13.7 | 21.7 | 9.1      | 24.7 | 7.3  | 28.1     |      |          |         |      |
| Change Period (Y+Rc), s      | 4.5  | 4.5      | 4.5  | 4.5  | 4.5      | 4.5  | 4.5  | 4.5      |      |          |         |      |
| Max Green Setting (Gmax), s  | 6.5  | 18.3     | 9.2  | 18.0 | 6.2      | 18.6 | 5.1  | 22.1     |      |          |         |      |
| Max Q Clear Time (g_c+l1), s | 7.2  | 10.8     | 9.9  | 11.3 | 5.5      | 4.0  | 3.7  | 16.6     |      |          |         |      |
| Green Ext Time (p_c), s      | 0.0  | 1.1      | 0.0  | 0.8  | 0.0      | 0.2  | 0.0  | 1.2      |      |          |         |      |
| Intersection Summary         |      |          |      |      |          |      |      |          |      |          |         |      |
| HCM 2010 Ctrl Delay          |      |          | 33.4 |      |          |      |      |          |      |          |         |      |
| HCM 2010 LOS                 |      |          | С    |      |          |      |      |          |      |          |         |      |

| •                          |      |          |       |       |          |       |       |       |       |       |          |       |
|----------------------------|------|----------|-------|-------|----------|-------|-------|-------|-------|-------|----------|-------|
| Intersection               |      |          |       |       |          |       |       |       |       |       |          |       |
| Intersection Delay, s/veh  | 11.5 |          |       |       |          |       |       |       |       |       |          |       |
| Intersection LOS           | В    |          |       |       |          |       |       |       |       |       |          |       |
|                            |      |          |       |       |          |       |       |       |       |       |          |       |
| Movement                   | EBL  | EBT      | EBR   | WBL   | WBT      | WBR   | NBL   | NBT   | NBR   | SBL   | SBT      | SBR   |
| Lane Configurations        | ሻ    | <b>↑</b> | 7     | ሻ     | <b>†</b> | 7     | ሻ     | f)    |       | ሻ     | <b>†</b> | 7     |
| Traffic Vol, veh/h         | 55   | 190      | 206   | 4     | 138      | 51    | 101   | 30    | 2     | 76    | 76       | 87    |
| Future Vol, veh/h          | 55   | 190      | 206   | 4     | 138      | 51    | 101   | 30    | 2     | 76    | 76       | 87    |
| Peak Hour Factor           | 0.97 | 0.97     | 0.97  | 0.97  | 0.97     | 0.97  | 0.97  | 0.97  | 0.97  | 0.97  | 0.97     | 0.97  |
| Heavy Vehicles, %          | 2    | 2        | 2     | 2     | 2        | 2     | 2     | 2     | 2     | 2     | 2        | 2     |
| Mvmt Flow                  | 57   | 196      | 212   | 4     | 142      | 53    | 104   | 31    | 2     | 78    | 78       | 90    |
| Number of Lanes            | 1    | 1        | 1     | 1     | 1        | 1     | 1     | 1     | 0     | 1     | 1        | 1     |
| Approach                   | EB   |          |       | WB    |          |       | NB    |       |       | SB    |          |       |
| Opposing Approach          | WB   |          |       | EB    |          |       | SB    |       |       | NB    |          |       |
| Opposing Lanes             | 3    |          |       | 3     |          |       | 3     |       |       | 2     |          |       |
| Conflicting Approach Left  | SB   |          |       | NB    |          |       | EB    |       |       | WB    |          |       |
| Conflicting Lanes Left     | 3    |          |       | 2     |          |       | 3     |       |       | 3     |          |       |
| Conflicting Approach Right | NB   |          |       | SB    |          |       | WB    |       |       | EB    |          |       |
| Conflicting Lanes Right    | 2    |          |       | 3     |          |       | 3     |       |       | 3     |          |       |
| HCM Control Delay          | 11.8 |          |       | 11.5  |          |       | 11.9  |       |       | 10.8  |          |       |
| HCM LOS                    | В    |          |       | В     |          |       | В     |       |       | В     |          |       |
|                            |      |          |       |       |          |       |       |       |       |       |          |       |
| Lane                       |      | NBLn1    | NBLn2 | EBLn1 | EBLn2    | EBLn3 | WBLn1 | WBLn2 | WBLn3 | SBLn1 | SBLn2    | SBLn3 |
| Vol Left, %                |      | 100%     | 0%    | 100%  | 0%       | 0%    | 100%  | 0%    | 0%    | 100%  | 0%       | 0%    |
| Vol Thru, %                |      | 0%       | 94%   | 0%    | 100%     | 0%    | 0%    | 100%  | 0%    | 0%    | 100%     | 0%    |
| Vol Right, %               |      | 0%       | 6%    | 0%    | 0%       | 100%  | 0%    | 0%    | 100%  | 0%    | 0%       | 100%  |
| Sign Control               |      | Stop     | Stop  | Stop  | Stop     | Stop  | Stop  | Stop  | Stop  | Stop  | Stop     | Stop  |
| Traffic Vol by Lane        |      | 101      | 32    | 55    | 190      | 206   | 4     | 138   | 51    | 76    | 76       | 87    |
| LT Val                     |      | 101      | Λ     | 55    | Λ        | Λ     | 1     | Λ     | Λ     | 76    | Λ        | 0     |

| Vol Left, %            | 100%  | 0%    | 100%  | 0%    | 0%    | 100%  | 0%    | 0%    | 100%  | 0%    | 0%    |
|------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Vol Thru, %            | 0%    | 94%   | 0%    | 100%  | 0%    | 0%    | 100%  | 0%    | 0%    | 100%  | 0%    |
| Vol Right, %           | 0%    | 6%    | 0%    | 0%    | 100%  | 0%    | 0%    | 100%  | 0%    | 0%    | 100%  |
| Sign Control           | Stop  |
| Traffic Vol by Lane    | 101   | 32    | 55    | 190   | 206   | 4     | 138   | 51    | 76    | 76    | 87    |
| LT Vol                 | 101   | 0     | 55    | 0     | 0     | 4     | 0     | 0     | 76    | 0     | 0     |
| Through Vol            | 0     | 30    | 0     | 190   | 0     | 0     | 138   | 0     | 0     | 76    | 0     |
| RT Vol                 | 0     | 2     | 0     | 0     | 206   | 0     | 0     | 51    | 0     | 0     | 87    |
| Lane Flow Rate         | 104   | 33    | 57    | 196   | 212   | 4     | 142   | 53    | 78    | 78    | 90    |
| Geometry Grp           | 8     | 8     | 8     | 8     | 8     | 8     | 8     | 8     | 8     | 8     | 8     |
| Degree of Util (X)     | 0.217 | 0.064 | 0.109 | 0.348 | 0.336 | 0.008 | 0.273 | 0.091 | 0.16  | 0.149 | 0.153 |
| Departure Headway (Hd) | 7.519 | 6.975 | 6.904 | 6.399 | 5.694 | 7.416 | 6.911 | 6.203 | 7.359 | 6.858 | 6.155 |
| Convergence, Y/N       | Yes   |
| Сар                    | 475   | 511   | 518   | 560   | 629   | 480   | 518   | 574   | 485   | 520   | 579   |
| Service Time           | 5.299 | 4.755 | 4.668 | 4.163 | 3.457 | 5.196 | 4.69  | 3.983 | 5.137 | 4.636 | 3.933 |
| HCM Lane V/C Ratio     | 0.219 | 0.065 | 0.11  | 0.35  | 0.337 | 0.008 | 0.274 | 0.092 | 0.161 | 0.15  | 0.155 |
| HCM Control Delay      | 12.4  | 10.2  | 10.5  | 12.6  | 11.3  | 10.3  | 12.3  | 9.6   | 11.5  | 10.8  | 10.1  |
| HCM Lane LOS           | В     | В     | В     | В     | В     | В     | В     | Α     | В     | В     | В     |
| HCM 95th-tile Q        | 8.0   | 0.2   | 0.4   | 1.5   | 1.5   | 0     | 1.1   | 0.3   | 0.6   | 0.5   | 0.5   |

| Intersection   Int Delay, s/veh   2.7  |
|--|
| Lane Configurations  |
| Lane Configurations  |
| Traffic Vol, veh/h   |
| Future Vol, veh/h Conflicting Peds, #/hr O O O O O O O O O O O O O O O O O O O   |
| Conflicting Peds, #/hr   |
| Sign Control   Free   Free   Free   Free   Free   Free   Free   Free   Free   Stop   Stop |
| RT Channelized   |
| Storage Length   320   |
| Veh in Median Storage, # - 0   |
| Grade, %         -         0         -         -         0         -         -         0         -         -         0         -         -         0         -         -         0         -         -         0         -         -         0         -         -         0         -         -         0         -         -         0         -         -         0         -         -         0         -         -         0         -         -         0         0         -         95<   |
| Heavy Vehicles, %   2   2   2   2   2   2   2   2   2  |
| Momit Flow         65         432         64         47         284         19         29         2         34         9         2         36           Major/Minor         Major1         Major2         Minor1         Minor2           Conflicting Flow All         303         0         0         496         0         0         969         959         432         990         1004         284           Stage 1         -         -         -         -         -         562         562         -         378         378         -           Stage 2         -         -         -         -         -         407         397         -         612         626         -           Critical Hdwy         4.12         -         4.12         -         7.12         6.52         6.22         7.12         6.52         6.22         7.12         6.52         6.22         7.12         6.52         6.22         7.12         6.52         6.22         7.12         6.52         6.22         7.12         6.52         6.22         7.12         6.52         6.22         7.12         6.52         6.22         7.12         6.52         6.22  |
| Major/Minor   Major1   Major2   Minor1   Minor2  |
| Conflicting Flow All         303         0         496         0         0         969         959         432         990         1004         284           Stage 1         -         -         -         -         562         562         -         378         378         -           Stage 2         -         -         -         -         407         397         -         612         626         -           Critical Hdwy         4.12         -         -         4.12         -         7.12         6.52         6.22         7.12         6.52         6.22           Critical Hdwy Stg 1         -         -         -         -         6.12         5.52         -         6.12         5.52         -           Critical Hdwy Stg 2         -         -         -         -         6.12         5.52         -         6.12         5.52         -           Follow-up Hdwy         2.218         -         2.218         -         3.518         4.018         3.318         3.518         4.018         3.318           Pot Cap-1 Maneuver         1258         -         1068         -         233         257         624         225  |
| Conflicting Flow All         303         0         496         0         0         969         959         432         990         1004         284           Stage 1         -         -         -         -         -         562         562         -         378         378         -           Stage 2         -         -         -         -         407         397         -         612         626         -           Critical Hdwy         4.12         -         -         4.12         -         7.12         6.52         6.22         7.12         6.52         6.22           Critical Hdwy Stg 1         -         -         -         -         6.12         5.52         -         6.12         5.52         -           Critical Hdwy Stg 2         -         -         -         -         6.12         5.52         -         6.12         5.52         -         6.12         5.52         -         6.12         5.52         -         6.12         5.52         -         6.12         5.52         -         6.12         5.52         -         6.12         5.52         -         6.12         5.52         -         6.12   |
| Conflicting Flow All         303         0         496         0         0         969         959         432         990         1004         284           Stage 1         -         -         -         -         562         562         -         378         378         -           Stage 2         -         -         -         -         407         397         -         612         626         -           Critical Hdwy         4.12         -         -         4.12         -         7.12         6.52         6.22         7.12         6.52         6.22           Critical Hdwy Stg 1         -         -         -         -         6.12         5.52         -         6.12         5.52         -           Critical Hdwy Stg 2         -         -         -         -         6.12         5.52         -         6.12         5.52         -           Follow-up Hdwy         2.218         -         2.218         -         3.518         4.018         3.318         3.518         4.018         3.318           Pot Cap-1 Maneuver         1258         -         1068         -         233         257         624         252  |
| Stage 1       -       -       -       -       562       562       -       378       378       -         Stage 2       -       -       -       -       -       407       397       -       612       626       -         Critical Hdwy       4.12       -       4.12       -       7.12       6.52       6.22       7.12       6.52       6.22         Critical Hdwy Stg 1       -       -       -       -       6.12       5.52       -       6.12       5.52       -         Critical Hdwy Stg 2       -       -       -       -       6.12       5.52       -       6.12       5.52       -         Follow-up Hdwy       2.218       -       2.218       -       3.518       4.018       3.318       3.518       4.018       3.318         Pot Cap-1 Maneuver       1258       -       1068       -       233       257       624       225       242       755         Stage 1       -       -       -       -       512       510       -       644       615       -         Platoon blocked, %       -       -       -       -       205       233   |
| Stage 2       -       -       -       -       407       397       -       612       626       -         Critical Hdwy       4.12       -       4.12       -       7.12       6.52       6.22       7.12       6.52       6.22         Critical Hdwy Stg 1       -       -       -       -       6.12       5.52       -       6.12       5.52       -         Critical Hdwy Stg 2       -       -       -       -       6.12       5.52       -       6.12       5.52       -         Follow-up Hdwy       2.218       -       -       2.218       -       -       3.518       4.018       3.318       3.518       4.018       3.318         Pot Cap-1 Maneuver       1258       -       1068       -       233       257       624       225       242       755         Stage 1       -       -       -       -       621       603       -       480       477       -         Platoon blocked, %       -       -       -       -       205       233       624       196       219       755         Mov Cap-2 Maneuver       -       -       -       - <t< td=""></t<>  |
| Critical Hdwy  |
| Critical Hdwy Stg 1 6.12 5.52 - 6.12 5.52 Critical Hdwy Stg 2 6.12 5.52 - 6.12 5.52 Critical Hdwy Stg 2 6.12 5.52 - 6.12 5.52 Critical Hdwy Stg 2 6.12 5.52 - 6.12 5.52 Critical Hdwy Stg 2 6.12 5.52 6.12 5.52 Critical Hdwy Stg 2 6.12 5.52 6.12 5.52 6.12 5.52  |
| Follow-up Hdwy 2.218 2.218 3.518 4.018 3.318 3.518 4.018 3.318  Pot Cap-1 Maneuver 1258 1068 233 257 624 225 242 755  Stage 1 512 510 - 644 615 -  Stage 2 621 603 - 480 477 -  Platoon blocked, % 621 603 - 480 477 -  Mov Cap-1 Maneuver 1258 - 1068 205 233 624 196 219 755  Mov Cap-2 Maneuver 205 233 - 196 219 -  Stage 1 485 483 - 611 588 -  Stage 2 564 576 - 429 452 -  Approach EB WB NB SB  HCM Control Delay, s 0.9 1.2 17.9 13.4  HCM LOS C B  |
| Pot Cap-1 Maneuver 1258 1068 233 257 624 225 242 755  Stage 1 512 510 - 644 615 -  Stage 2 621 603 - 480 477 -  Platoon blocked, % 621 603 - 480 477 -  Mov Cap-1 Maneuver 1258 - 1068 205 233 624 196 219 755  Mov Cap-2 Maneuver 205 233 - 196 219 -  Stage 1 485 483 - 611 588 -  Stage 2 564 576 - 429 452 -  Approach EB WB NB SB  HCM Control Delay, s 0.9 1.2 17.9 13.4  HCM LOS C B  |
| Stage 1       -       -       -       -       512       510       -       644       615       -         Stage 2       -       -       -       -       621       603       -       480       477       -         Platoon blocked, %       -   |
| Stage 2       -       -       -       -       621       603       -       480       477       -         Platoon blocked, %       - <t< td=""></t<>   |
| Platoon blocked, %   |
| Mov Cap-1 Maneuver         1258         -         -         1068         -         -         205         233         624         196         219         755           Mov Cap-2 Maneuver         -         -         -         -         205         233         -         196         219         -           Stage 1         -         -         -         -         -         485         483         -         611         588         -           Stage 2         -         -         -         -         564         576         -         429         452         -           Approach         EB         WB         NB         SB         -         -         -         -         -         564         576         -         429         452         -         -         -         -         -         -         564         576         -         429         452         -   |
| Mov Cap-2 Maneuver         -         -         -         -         205         233         -         196         219         -           Stage 1         -         -         -         -         -         485         483         -         611         588         -           Stage 2         -         -         -         -         564         576         -         429         452         -           Approach         EB         WB         NB         SB         SB           HCM Control Delay, s         0.9         1.2         17.9         13.4           HCM LOS         C         B   Minor Lane/Major Mvmt  NBLn1 NBLn2 NBLn3  EBL  EBT  EBR  WBL  WBT  WBR SBLn1 SBLn2 SBLn3   |
| Stage 1         -         -         -         -         485         483         -         611         588         -           Stage 2         -         -         -         -         564         576         -         429         452         -           Approach         EB         WB         NB         SB           HCM Control Delay, s         0.9         1.2         17.9         13.4           HCM LOS         C         B   Minor Lane/Major Mvmt  NBLn1 NBLn2 NBLn3  EBL  EBT  EBR  WBL  WBT  WBR SBLn1 SBLn2 SBLn3   |
| Stage 2         -         -         -         -         564         576         -         429         452         -           Approach         EB         WB         NB         SB           HCM Control Delay, s         0.9         1.2         17.9         13.4           HCM LOS         C         B   Minor Lane/Major Mvmt  NBLn1 NBLn2 NBLn3  EBL  EBT  EBR  WBL  WBT  WBR SBLn1 SBLn2 SBLn3   |
| Approach         EB         WB         NB         SB           HCM Control Delay, s         0.9         1.2         17.9         13.4           HCM LOS         C         B             Minor Lane/Major Mvmt         NBLn1 NBLn2 NBLn3         EBL         EBT         EBR         WBL         WBT         WBR SBLn1 SBLn2 SBLn3  |
| HCM Control Delay, s   0.9   1.2   17.9   13.4     HCM LOS   C   B   |
| HCM Control Delay, s   0.9   1.2   17.9   13.4     HCM LOS   C   B   |
| HCM LOS         C         B           Minor Lane/Major Mvmt         NBLn1 NBLn2 NBLn3         EBL         EBT         EBR         WBL         WBT         WBR SBLn1 SBLn2 SBLn3  |
| Minor Lane/Major Mvmt NBLn1 NBLn2 NBLn3 EBL EBT EBR WBL WBT WBR SBLn1 SBLn2 SBLn3  |
| ,  |
| ,  |
| Canacity (yeh/h) 205 233 624 1258 - 1068 - 196 219 755   |
|  |
| HCM Lane V/C Ratio 0.144 0.009 0.054 0.052 0.044 0.048 0.01 0.047  |
| HCM Control Delay (s) 25.5 20.6 11.1 8 8.5 24.3 21.6 10  |
| HCM Lane LOS D C B A A C C B   |
| HCM 95th %tile Q(veh) 0.5 0 0.2 0.2 0.1 0.2 0 0.1  |

| Intersection           |        |          |           |       |        |          |
|------------------------|--------|----------|-----------|-------|--------|----------|
| Int Delay, s/veh       | 3.8    |          |           |       |        |          |
|                        |        | WED      | NET       | NDD   | ODI    | ODT      |
| Movement               | WBL    | WBR      | NBT       | NBR   | SBL    | SBT      |
| Lane Configurations    | ¥      | 70       | <b>\$</b> | 4.4   | 440    | <u>ન</u> |
| Traffic Vol, veh/h     | 9      | 76       | 95        | 14    | 112    | 138      |
| Future Vol, veh/h      | 9      | 76       | 95        | 14    | 112    | 138      |
| Conflicting Peds, #/hr | 1      | 0        | 0         | _ 0   | _ 0    | _ 0      |
| Sign Control           | Stop   | Stop     | Free      | Free  | Free   | Free     |
| RT Channelized         | -      | None     | -         |       | -      | None     |
| Storage Length         | 0      | -        | -         | -     | -      | -        |
| Veh in Median Storage  |        | -        | 0         | -     | -      | 0        |
| Grade, %               | 0      | -        | 0         | -     | -      | 0        |
| Peak Hour Factor       | 91     | 91       | 91        | 91    | 91     | 91       |
| Heavy Vehicles, %      | 6      | 6        | 2         | 2     | 3      | 3        |
| Mvmt Flow              | 10     | 84       | 104       | 15    | 123    | 152      |
|                        |        |          |           |       |        |          |
| Major/Minor I          | Minor1 | N        | /lajor1   |       | Major2 |          |
| Conflicting Flow All   | 511    | 112      | 0         | 0     | 119    | 0        |
| Stage 1                | 112    | -        | -         | -     | -      | -        |
| Stage 2                | 399    | <u>-</u> | _         | _     | _      | _        |
| Critical Hdwy          | 6.46   | 6.26     |           |       | 4.13   | _        |
| Critical Hdwy Stg 1    | 5.46   | 0.20     | _         | _     | 7.10   | _        |
| Critical Hdwy Stg 2    | 5.46   | _        | -         | _     | -      |          |
| Follow-up Hdwy         | 3.554  | 3.354    | _         | _     |        | _        |
| Pot Cap-1 Maneuver     | 516    | 930      |           | -     | 1463   | -        |
| •                      | 903    | 930      | -         | _     | 1403   | -        |
| Stage 1                |        |          | -         | -     | -      |          |
| Stage 2                | 669    | -        | -         | -     | -      | -        |
| Platoon blocked, %     | 460    | 020      | -         | -     | 1460   | -        |
| Mov Cap-1 Maneuver     | 468    | 930      | -         | -     | 1463   | -        |
| Mov Cap-2 Maneuver     | 468    | -        | -         | -     | -      | -        |
| Stage 1                | 820    | -        | -         | -     | -      | -        |
| Stage 2                | 668    | -        | -         | -     | -      | -        |
|                        |        |          |           |       |        |          |
| Approach               | WB     |          | NB        |       | SB     |          |
| HCM Control Delay, s   | 9.8    |          | 0         |       | 3.4    |          |
| HCM LOS                | Α      |          | U         |       | 0.4    |          |
|                        | , (    |          |           |       |        |          |
|                        |        |          |           |       |        |          |
| Minor Lane/Major Mvm   | nt     | NBT      | NBRV      | VBLn1 | SBL    | SBT      |
| Capacity (veh/h)       |        | -        | -         |       | 1463   | -        |
| HCM Lane V/C Ratio     |        | -        | -         | 0.111 |        | -        |
| HCM Control Delay (s)  |        | -        | -         | 9.8   | 7.7    | 0        |
| HCM Lane LOS           |        | -        | -         | Α     | Α      | Α        |
| HCM 95th %tile Q(veh)  |        | -        | -         | 0.4   | 0.3    | -        |
|                        |        |          |           |       |        |          |

|                              | •    | <b>→</b> | `*   | •    | <b>←</b> | •     | •    | <b>†</b> | ~    | <b>&gt;</b> | <b></b>  | ✓    |
|------------------------------|------|----------|------|------|----------|-------|------|----------|------|-------------|----------|------|
| Movement                     | EBL  | EBT      | EBR  | WBL  | WBT      | WBR   | NBL  | NBT      | NBR  | SBL         | SBT      | SBR  |
| Lane Configurations          | ř    | ĵ.       |      | ሻ    | ĵ»       |       | ሻ    | <b>†</b> | 7    | ሻ           | <b>1</b> | 7    |
| Traffic Volume (veh/h)       | 162  | 224      | 159  | 16   | 124      | 103   | 107  | 197      | 23   | 206         | 354      | 159  |
| Future Volume (veh/h)        | 162  | 224      | 159  | 16   | 124      | 103   | 107  | 197      | 23   | 206         | 354      | 159  |
| Number                       | 7    | 4        | 14   | 3    | 8        | 18    | 5    | 2        | 12   | 1           | 6        | 16   |
| Initial Q (Qb), veh          | 0    | 0        | 0    | 0    | 0        | 0     | 0    | 0        | 0    | 0           | 0        | 0    |
| Ped-Bike Adj(A_pbT)          | 1.00 |          | 1.00 | 1.00 |          | 1.00  | 1.00 |          | 1.00 | 1.00        |          | 1.00 |
| Parking Bus, Adj             | 1.00 | 1.00     | 1.00 | 1.00 | 1.00     | 1.00  | 1.00 | 1.00     | 1.00 | 1.00        | 1.00     | 1.00 |
| Adj Sat Flow, veh/h/ln       | 1863 | 1863     | 1900 | 1863 | 1863     | 1900  | 1863 | 1863     | 1863 | 1863        | 1863     | 1863 |
| Adj Flow Rate, veh/h         | 169  | 233      | 166  | 17   | 129      | 107   | 111  | 205      | 24   | 215         | 369      | 166  |
| Adj No. of Lanes             | 1    | 1        | 0    | 1    | 1        | 0     | 1    | 1        | 1    | 1           | 1        | 1    |
| Peak Hour Factor             | 0.96 | 0.96     | 0.96 | 0.96 | 0.96     | 0.96  | 0.96 | 0.96     | 0.96 | 0.96        | 0.96     | 0.96 |
| Percent Heavy Veh, %         | 2    | 2        | 2    | 2    | 2        | 2     | 2    | 2        | 2    | 2           | 2        | 2    |
| Cap, veh/h                   | 426  | 243      | 173  | 218  | 116      | 96    | 141  | 479      | 407  | 248         | 592      | 503  |
| Arrive On Green              | 0.24 | 0.24     | 0.24 | 0.12 | 0.12     | 0.12  | 0.08 | 0.26     | 0.26 | 0.14        | 0.32     | 0.32 |
| Sat Flow, veh/h              | 1774 | 1013     | 722  | 1774 | 943      | 782   | 1774 | 1863     | 1583 | 1774        | 1863     | 1583 |
| Grp Volume(v), veh/h         | 169  | 0        | 399  | 17   | 0        | 236   | 111  | 205      | 24   | 215         | 369      | 166  |
| Grp Sat Flow(s),veh/h/ln     | 1774 | 0        | 1735 | 1774 | 0        | 1725  | 1774 | 1863     | 1583 | 1774        | 1863     | 1583 |
| Q Serve(g_s), s              | 6.0  | 0.0      | 17.0 | 0.6  | 0.0      | 9.2   | 4.6  | 6.9      | 0.9  | 8.9         | 12.6     | 6.0  |
| Cycle Q Clear(g_c), s        | 6.0  | 0.0      | 17.0 | 0.6  | 0.0      | 9.2   | 4.6  | 6.9      | 0.9  | 8.9         | 12.6     | 6.0  |
| Prop In Lane                 | 1.00 |          | 0.42 | 1.00 |          | 0.45  | 1.00 |          | 1.00 | 1.00        |          | 1.00 |
| Lane Grp Cap(c), veh/h       | 426  | 0        | 416  | 218  | 0        | 212   | 141  | 479      | 407  | 248         | 592      | 503  |
| V/C Ratio(X)                 | 0.40 | 0.00     | 0.96 | 0.08 | 0.00     | 1.12  | 0.79 | 0.43     | 0.06 | 0.87        | 0.62     | 0.33 |
| Avail Cap(c_a), veh/h        | 426  | 0        | 416  | 218  | 0        | 212   | 177  | 479      | 407  | 248         | 592      | 503  |
| HCM Platoon Ratio            | 1.00 | 1.00     | 1.00 | 1.00 | 1.00     | 1.00  | 1.00 | 1.00     | 1.00 | 1.00        | 1.00     | 1.00 |
| Upstream Filter(I)           | 1.00 | 0.00     | 1.00 | 1.00 | 0.00     | 1.00  | 1.00 | 1.00     | 1.00 | 1.00        | 1.00     | 1.00 |
| Uniform Delay (d), s/veh     | 23.9 | 0.0      | 28.1 | 29.1 | 0.0      | 32.9  | 33.9 | 23.2     | 21.0 | 31.6        | 21.8     | 19.5 |
| Incr Delay (d2), s/veh       | 0.6  | 0.0      | 33.3 | 0.2  | 0.0      | 96.3  | 16.5 | 2.8      | 0.3  | 25.8        | 4.9      | 1.8  |
| Initial Q Delay(d3),s/veh    | 0.0  | 0.0      | 0.0  | 0.0  | 0.0      | 0.0   | 0.0  | 0.0      | 0.0  | 0.0         | 0.0      | 0.0  |
| %ile BackOfQ(50%),veh/ln     | 3.0  | 0.0      | 11.9 | 0.3  | 0.0      | 10.0  | 2.9  | 3.9      | 0.4  | 6.1         | 7.3      | 2.9  |
| LnGrp Delay(d),s/veh         | 24.5 | 0.0      | 61.5 | 29.3 | 0.0      | 129.2 | 50.4 | 26.0     | 21.3 | 57.4        | 26.7     | 21.3 |
| LnGrp LOS                    | С    |          | Е    | С    |          | F     | D    | С        | С    | Е           | С        | С    |
| Approach Vol, veh/h          |      | 568      |      |      | 253      |       |      | 340      |      |             | 750      |      |
| Approach Delay, s/veh        |      | 50.5     |      |      | 122.5    |       |      | 33.6     |      |             | 34.3     |      |
| Approach LOS                 |      | D        |      |      | F        |       |      | С        |      |             | С        |      |
| Timer                        | 1    | 2        | 3    | 4    | 5        | 6     | 7    | 8        |      |             |          |      |
| Assigned Phs                 | 1    | 2        |      | 4    | 5        | 6     |      | 8        |      |             |          |      |
| Phs Duration (G+Y+Rc), s     | 15.0 | 23.8     |      | 22.5 | 10.5     | 28.3  |      | 13.7     |      |             |          |      |
| Change Period (Y+Rc), s      | 4.5  | 4.5      |      | 4.5  | 4.5      | 4.5   |      | 4.5      |      |             |          |      |
| Max Green Setting (Gmax), s  | 10.5 | 19.3     |      | 18.0 | 7.5      | 22.3  |      | 9.2      |      |             |          |      |
| Max Q Clear Time (g_c+l1), s | 10.9 | 8.9      |      | 19.0 | 6.6      | 14.6  |      | 11.2     |      |             |          |      |
| Green Ext Time (p_c), s      | 0.0  | 0.8      |      | 0.0  | 0.0      | 1.7   |      | 0.0      |      |             |          |      |
| Intersection Summary         |      |          |      |      |          |       |      |          |      |             |          |      |
| HCM 2010 Ctrl Delay          |      |          | 50.7 |      |          |       |      |          |      |             |          |      |
| HCM 2010 LOS                 |      |          | D    |      |          |       |      |          |      |             |          |      |

|                              | •    | <b>→</b> | •    | •    | <b>←</b> | •    | •    | <b>†</b> | ~    | <b>/</b> | <b></b> |      |
|------------------------------|------|----------|------|------|----------|------|------|----------|------|----------|---------|------|
| Movement                     | EBL  | EBT      | EBR  | WBL  | WBT      | WBR  | NBL  | NBT      | NBR  | SBL      | SBT     | SBR  |
| Lane Configurations          | ,    | ĵ»       |      | *    | f)       |      |      | 4        |      |          | 4       |      |
| Traffic Volume (veh/h)       | 28   | 486      | 103  | 88   | 286      | 15   | 85   | 38       | 47   | 24       | 60      | 12   |
| Future Volume (veh/h)        | 28   | 486      | 103  | 88   | 286      | 15   | 85   | 38       | 47   | 24       | 60      | 12   |
| Number                       | 7    | 4        | 14   | 3    | 8        | 18   | 5    | 2        | 12   | 1        | 6       | 16   |
| Initial Q (Qb), veh          | 0    | 0        | 0    | 0    | 0        | 0    | 0    | 0        | 0    | 0        | 0       | 0    |
| Ped-Bike Adj(A_pbT)          | 1.00 |          | 1.00 | 1.00 |          | 1.00 | 1.00 |          | 1.00 | 1.00     |         | 1.00 |
| Parking Bus, Adj             | 1.00 | 1.00     | 1.00 | 1.00 | 1.00     | 1.00 | 1.00 | 1.00     | 1.00 | 1.00     | 1.00    | 1.00 |
| Adj Sat Flow, veh/h/ln       | 1863 | 1863     | 1900 | 1863 | 1863     | 1900 | 1900 | 1863     | 1900 | 1900     | 1827    | 1900 |
| Adj Flow Rate, veh/h         | 33   | 565      | 120  | 102  | 333      | 17   | 99   | 44       | 55   | 28       | 70      | 14   |
| Adj No. of Lanes             | 1    | 1        | 0    | 1    | 1        | 0    | 0    | 1        | 0    | 0        | 1       | 0    |
| Peak Hour Factor             | 0.86 | 0.86     | 0.86 | 0.86 | 0.86     | 0.86 | 0.86 | 0.86     | 0.86 | 0.86     | 0.86    | 0.86 |
| Percent Heavy Veh, %         | 2    | 2        | 2    | 2    | 2        | 2    | 2    | 2        | 2    | 4        | 4       | 4    |
| Cap, veh/h                   | 63   | 566      | 120  | 130  | 734      | 37   | 304  | 138      | 135  | 166      | 374     | 66   |
| Arrive On Green              | 0.04 | 0.38     | 0.38 | 0.07 | 0.42     | 0.42 | 0.32 | 0.32     | 0.32 | 0.32     | 0.32    | 0.32 |
| Sat Flow, veh/h              | 1774 | 1490     | 317  | 1774 | 1757     | 90   | 667  | 432      | 422  | 284      | 1173    | 208  |
| Grp Volume(v), veh/h         | 33   | 0        | 685  | 102  | 0        | 350  | 198  | 0        | 0    | 112      | 0       | 0    |
| Grp Sat Flow(s),veh/h/ln     | 1774 | 0        | 1807 | 1774 | 0        | 1847 | 1521 | 0        | 0    | 1664     | 0       | 0    |
| Q Serve(g_s), s              | 1.1  | 0.0      | 22.4 | 3.3  | 0.0      | 8.1  | 2.9  | 0.0      | 0.0  | 0.0      | 0.0     | 0.0  |
| Cycle Q Clear(g_c), s        | 1.1  | 0.0      | 22.4 | 3.3  | 0.0      | 8.1  | 5.6  | 0.0      | 0.0  | 2.7      | 0.0     | 0.0  |
| Prop In Lane                 | 1.00 |          | 0.18 | 1.00 |          | 0.05 | 0.50 |          | 0.28 | 0.25     |         | 0.12 |
| Lane Grp Cap(c), veh/h       | 63   | 0        | 686  | 130  | 0        | 772  | 576  | 0        | 0    | 607      | 0       | 0    |
| V/C Ratio(X)                 | 0.53 | 0.00     | 1.00 | 0.78 | 0.00     | 0.45 | 0.34 | 0.00     | 0.00 | 0.18     | 0.00    | 0.00 |
| Avail Cap(c_a), veh/h        | 165  | 0        | 686  | 153  | 0        | 772  | 576  | 0        | 0    | 607      | 0       | 0    |
| HCM Platoon Ratio            | 1.00 | 1.00     | 1.00 | 1.00 | 1.00     | 1.00 | 1.00 | 1.00     | 1.00 | 1.00     | 1.00    | 1.00 |
| Upstream Filter(I)           | 1.00 | 0.00     | 1.00 | 1.00 | 0.00     | 1.00 | 1.00 | 0.00     | 0.00 | 1.00     | 0.00    | 0.00 |
| Uniform Delay (d), s/veh     | 28.1 | 0.0      | 18.4 | 27.0 | 0.0      | 12.4 | 15.5 | 0.0      | 0.0  | 14.7     | 0.0     | 0.0  |
| Incr Delay (d2), s/veh       | 6.7  | 0.0      | 33.9 | 19.9 | 0.0      | 0.4  | 1.6  | 0.0      | 0.0  | 0.7      | 0.0     | 0.0  |
| Initial Q Delay(d3),s/veh    | 0.0  | 0.0      | 0.0  | 0.0  | 0.0      | 0.0  | 0.0  | 0.0      | 0.0  | 0.0      | 0.0     | 0.0  |
| %ile BackOfQ(50%),veh/ln     | 0.6  | 0.0      | 17.5 | 2.4  | 0.0      | 4.2  | 2.7  | 0.0      | 0.0  | 1.5      | 0.0     | 0.0  |
| LnGrp Delay(d),s/veh         | 34.8 | 0.0      | 52.3 | 46.8 | 0.0      | 12.8 | 17.2 | 0.0      | 0.0  | 15.3     | 0.0     | 0.0  |
| LnGrp LOS                    | С    |          | D    | D    |          | В    | В    |          |      | В        |         |      |
| Approach Vol, veh/h          |      | 718      |      |      | 452      |      |      | 198      |      |          | 112     |      |
| Approach Delay, s/veh        |      | 51.5     |      |      | 20.5     |      |      | 17.2     |      |          | 15.3    |      |
| Approach LOS                 |      | D        |      |      | С        |      |      | В        |      |          | В       |      |
| Timer                        | 1    | 2        | 3    | 4    | 5        | 6    | 7    | 8        |      |          |         |      |
| Assigned Phs                 |      | 2        | 3    | 4    |          | 6    | 7    | 8        |      |          |         |      |
| Phs Duration (G+Y+Rc), s     |      | 23.4     | 8.9  | 27.0 |          | 23.4 | 6.6  | 29.3     |      |          |         |      |
| Change Period (Y+Rc), s      |      | 4.5      | 4.5  | 4.5  |          | 4.5  | 4.5  | 4.5      |      |          |         |      |
| Max Green Setting (Gmax), s  |      | 18.9     | 5.1  | 22.5 |          | 18.9 | 5.5  | 22.1     |      |          |         |      |
| Max Q Clear Time (g_c+I1), s |      | 7.6      | 5.3  | 24.4 |          | 4.7  | 3.1  | 10.1     |      |          |         |      |
| Green Ext Time (p_c), s      |      | 8.0      | 0.0  | 0.0  |          | 0.4  | 0.0  | 1.6      |      |          |         |      |
| Intersection Summary         |      |          |      |      |          |      |      |          |      |          |         |      |
| HCM 2010 Ctrl Delay          |      |          | 34.7 |      |          |      |      |          |      |          |         |      |
| HCM 2010 LOS                 |      |          | С    |      |          |      |      |          |      |          |         |      |

|                              |      | <b>→</b> | <b>←</b> | •    | <u> </u> | 1    |      |      |  |  |   |
|------------------------------|------|----------|----------|------|----------|------|------|------|--|--|---|
| Movement                     | EBL  | EBT      | WBT      | WBR  | SBL      | SBR  |      |      |  |  |   |
| Lane Configurations          | *    | <b>1</b> | <b>^</b> | 7    | *        | 7    |      |      |  |  | _ |
| Traffic Volume (veh/h)       | 258  | 454      | 212      | 171  | 162      | 163  |      |      |  |  |   |
| Future Volume (veh/h)        | 258  | 454      | 212      | 171  | 162      | 163  |      |      |  |  |   |
| Number                       | 7    | 4        | 8        | 18   | 1        | 16   |      |      |  |  |   |
| Initial Q (Qb), veh          | 0    | 0        | 0        | 0    | 0        | 0    |      |      |  |  |   |
| Ped-Bike Adj(A_pbT)          | 1.00 |          |          | 1.00 | 1.00     | 1.00 |      |      |  |  |   |
| Parking Bus, Adj             | 1.00 | 1.00     | 1.00     | 1.00 | 1.00     | 1.00 |      |      |  |  |   |
| Adj Sat Flow, veh/h/ln       | 1863 | 1863     | 1863     | 1863 | 1863     | 1863 |      |      |  |  |   |
| Adj Flow Rate, veh/h         | 274  | 483      | 226      | 182  | 172      | 173  |      |      |  |  |   |
| Adj No. of Lanes             | 1    | 1        | 1        | 1    | 1        | 1    |      |      |  |  |   |
| Peak Hour Factor             | 0.94 | 0.94     | 0.94     | 0.94 | 0.94     | 0.94 |      |      |  |  |   |
| Percent Heavy Veh, %         | 2    | 2        | 2        | 2    | 2        | 2    |      |      |  |  |   |
| Cap, veh/h                   | 351  | 905      | 344      | 293  | 547      | 488  |      |      |  |  |   |
| Arrive On Green              | 0.20 | 0.49     | 0.18     | 0.18 | 0.31     | 0.31 |      |      |  |  |   |
| Sat Flow, veh/h              | 1774 | 1863     | 1863     | 1583 | 1774     | 1583 |      |      |  |  |   |
| Grp Volume(v), veh/h         | 274  | 483      | 226      | 182  | 172      | 173  |      |      |  |  |   |
| Grp Sat Flow(s), veh/h/ln    | 1774 | 1863     | 1863     | 1583 | 1774     | 1583 |      |      |  |  |   |
| Q Serve(g_s), s              | 6.4  | 7.9      | 4.9      | 4.6  | 3.2      | 3.7  |      |      |  |  |   |
| Cycle Q Clear(g_c), s        | 6.4  | 7.9      | 4.9      | 4.6  | 3.2      | 3.7  |      |      |  |  |   |
| Prop In Lane                 | 1.00 |          |          | 1.00 | 1.00     | 1.00 |      |      |  |  |   |
| Lane Grp Cap(c), veh/h       | 351  | 905      | 344      | 293  | 547      | 488  |      |      |  |  |   |
| V/C Ratio(X)                 | 0.78 | 0.53     | 0.66     | 0.62 | 0.31     | 0.35 |      |      |  |  |   |
| Avail Cap(c_a), veh/h        | 750  | 1596     | 617      | 525  | 547      | 488  |      |      |  |  |   |
| HCM Platoon Ratio            | 1.00 | 1.00     | 1.00     | 1.00 | 1.00     | 1.00 |      |      |  |  |   |
| Upstream Filter(I)           | 1.00 | 1.00     | 1.00     | 1.00 | 1.00     | 1.00 |      |      |  |  |   |
| Uniform Delay (d), s/veh     | 16.6 | 7.8      | 16.5     | 16.4 | 11.6     | 11.7 |      |      |  |  |   |
| Incr Delay (d2), s/veh       | 3.8  | 0.5      | 2.1      | 2.2  | 1.5      | 2.0  |      |      |  |  |   |
| Initial Q Delay(d3),s/veh    | 0.0  | 0.0      | 0.0      | 0.0  | 0.0      | 0.0  |      |      |  |  |   |
| %ile BackOfQ(50%),veh/ln     | 3.5  | 4.1      | 2.7      | 2.2  | 1.8      | 3.8  |      |      |  |  |   |
| LnGrp Delay(d),s/veh         | 20.4 | 8.3      | 18.7     | 18.6 | 13.1     | 13.8 |      |      |  |  |   |
| LnGrp LOS                    | С    | Α        | В        | В    | В        | В    |      |      |  |  |   |
| Approach Vol, veh/h          |      | 757      | 408      |      | 345      |      |      |      |  |  |   |
| Approach Delay, s/veh        |      | 12.7     | 18.6     |      | 13.4     |      |      |      |  |  |   |
| Approach LOS                 |      | В        | В        |      | В        |      |      |      |  |  |   |
| Timer                        | 1    | 2        | 3        | 4    | 5        | 6    | 7    | 8    |  |  |   |
| Assigned Phs                 |      |          |          | 4    |          | 6    | 7    | 8    |  |  |   |
| Phs Duration (G+Y+Rc), s     |      |          |          | 25.8 |          | 18.0 | 13.2 | 12.6 |  |  |   |
| Change Period (Y+Rc), s      |      |          |          | 4.5  |          | 4.5  | 4.5  | 4.5  |  |  |   |
| Max Green Setting (Gmax), s  |      |          |          | 37.5 |          | 13.5 | 18.5 | 14.5 |  |  |   |
| Max Q Clear Time (g_c+l1), s |      |          |          | 9.9  |          | 5.7  | 8.4  | 6.9  |  |  |   |
| Green Ext Time (p_c), s      |      |          |          | 3.3  |          | 0.7  | 0.6  | 1.2  |  |  |   |
| Intersection Summary         |      |          |          |      |          |      |      |      |  |  |   |
| HCM 2010 Ctrl Delay          |      |          | 14.5     |      |          |      |      |      |  |  |   |
| HCM 2010 LOS                 |      |          | В        |      |          |      |      |      |  |  |   |

|                                 | ۶         | <b>→</b> | •     | •     | <b>←</b>    | 4          | 1       | <b>†</b> | ~    | <b>/</b> | <del> </del> | ✓    |
|---------------------------------|-----------|----------|-------|-------|-------------|------------|---------|----------|------|----------|--------------|------|
| Movement                        | EBL       | EBT      | EBR   | WBL   | WBT         | WBR        | NBL     | NBT      | NBR  | SBL      | SBT          | SBR  |
| Lane Configurations             | Ť         | <b>†</b> | 7     | 7     | ₽           |            |         | र्स      | 7    |          | र्स          | 7    |
| Traffic Volume (vph)            | 1         | 566      | 441   | 22    | 620         | 27         | 329     | 16       | 48   | 132      | 154          | 1    |
| Future Volume (vph)             | 1         | 566      | 441   | 22    | 620         | 27         | 329     | 16       | 48   | 132      | 154          | 1    |
| Ideal Flow (vphpl)              | 1900      | 1900     | 1900  | 1900  | 1900        | 1900       | 1900    | 1900     | 1900 | 1900     | 1900         | 1900 |
| Total Lost time (s)             | 4.5       | 4.5      | 4.5   | 4.5   | 4.5         |            |         | 4.5      | 4.5  |          | 4.5          | 4.5  |
| Lane Util. Factor               | 1.00      | 1.00     | 1.00  | 1.00  | 1.00        |            |         | 1.00     | 1.00 |          | 1.00         | 1.00 |
| Frt                             | 1.00      | 1.00     | 0.85  | 1.00  | 0.99        |            |         | 1.00     | 0.85 |          | 1.00         | 0.85 |
| Flt Protected                   | 0.95      | 1.00     | 1.00  | 0.95  | 1.00        |            |         | 0.95     | 1.00 |          | 0.98         | 1.00 |
| Satd. Flow (prot)               | 1687      | 1776     | 1509  | 1583  | 1656        |            |         | 1778     | 1583 |          | 1821         | 1583 |
| Flt Permitted                   | 0.95      | 1.00     | 1.00  | 0.95  | 1.00        |            |         | 0.95     | 1.00 |          | 0.98         | 1.00 |
| Satd. Flow (perm)               | 1687      | 1776     | 1509  | 1583  | 1656        |            |         | 1778     | 1583 |          | 1821         | 1583 |
| Peak-hour factor, PHF           | 0.94      | 0.94     | 0.94  | 0.94  | 0.94        | 0.94       | 0.94    | 0.94     | 0.94 | 0.94     | 0.94         | 0.94 |
| Adj. Flow (vph)                 | 1         | 602      | 469   | 23    | 660         | 29         | 350     | 17       | 51   | 140      | 164          | 1    |
| RTOR Reduction (vph)            | 0         | 0        | 270   | 0     | 1           | 0          | 0       | 0        | 40   | 0        | 0            | 1    |
| Lane Group Flow (vph)           | 1         | 602      | 199   | 23    | 688         | 0          | 0       | 367      | 11   | 0        | 304          | 0    |
| Heavy Vehicles (%)              | 7%        | 7%       | 7%    | 14%   | 14%         | 14%        | 2%      | 2%       | 2%   | 2%       | 2%           | 2%   |
| Turn Type                       | Prot      | NA       | Perm  | Prot  | NA          |            | Split   | NA       | Perm | Split    | NA           | Perm |
| Protected Phases                | 7         | 4        |       | 3     | 8           |            | 5       | 5        |      | 6        | 6            |      |
| Permitted Phases                |           |          | 4     |       |             |            |         |          | 5    |          |              | 6    |
| Actuated Green, G (s)           | 0.9       | 45.4     | 45.4  | 1.9   | 46.4        |            |         | 22.2     | 22.2 |          | 19.7         | 19.7 |
| Effective Green, g (s)          | 0.9       | 45.4     | 45.4  | 1.9   | 46.4        |            |         | 22.2     | 22.2 |          | 19.7         | 19.7 |
| Actuated g/C Ratio              | 0.01      | 0.42     | 0.42  | 0.02  | 0.43        |            |         | 0.21     | 0.21 |          | 0.18         | 0.18 |
| Clearance Time (s)              | 4.5       | 4.5      | 4.5   | 4.5   | 4.5         |            |         | 4.5      | 4.5  |          | 4.5          | 4.5  |
| Vehicle Extension (s)           | 3.0       | 3.0      | 3.0   | 3.0   | 3.0         |            |         | 3.0      | 3.0  |          | 3.0          | 3.0  |
| Lane Grp Cap (vph)              | 14        | 752      | 639   | 28    | 716         |            |         | 368      | 327  |          | 334          | 290  |
| v/s Ratio Prot                  | 0.00      | 0.34     |       | c0.01 | c0.42       |            |         | c0.21    |      |          | c0.17        |      |
| v/s Ratio Perm                  |           |          | 0.13  |       |             |            |         |          | 0.01 |          |              | 0.00 |
| v/c Ratio                       | 0.07      | 0.80     | 0.31  | 0.82  | 0.96        |            |         | 1.00     | 0.03 |          | 0.91         | 0.00 |
| Uniform Delay, d1               | 52.7      | 27.0     | 20.5  | 52.5  | 29.5        |            |         | 42.5     | 33.9 |          | 42.9         | 35.7 |
| Progression Factor              | 1.00      | 1.00     | 1.00  | 1.00  | 1.00        |            |         | 1.00     | 1.00 |          | 1.00         | 1.00 |
| Incremental Delay, d2           | 2.2       | 8.8      | 1.3   | 96.0  | 25.3        |            |         | 45.9     | 0.0  |          | 27.7         | 0.0  |
| Delay (s)                       | 54.9      | 35.7     | 21.8  | 148.4 | 54.8        |            |         | 88.3     | 34.0 |          | 70.6         | 35.7 |
| Level of Service                | D         | D        | С     | F     | D           |            |         | F        | С    |          | E            | D    |
| Approach Delay (s)              |           | 29.6     |       |       | 57.8        |            |         | 81.7     |      |          | 70.5         |      |
| Approach LOS                    |           | С        |       |       | E           |            |         | F        |      |          | E            |      |
| Intersection Summary            |           |          |       |       |             |            |         |          |      |          |              |      |
| HCM 2000 Control Delay          |           |          | 51.3  | Н     | CM 2000     | Level of S | Service |          | D    |          |              |      |
| HCM 2000 Volume to Capac        | ity ratio |          | 0.97  |       |             |            |         |          |      |          |              |      |
| Actuated Cycle Length (s)       |           |          | 107.2 |       | um of lost  |            |         |          | 18.0 |          |              |      |
| Intersection Capacity Utilizati | on        |          | 80.0% | IC    | CU Level of | of Service |         |          | D    |          |              |      |
| Analysis Period (min)           |           |          | 15    |       |             |            |         |          |      |          |              |      |
| c Critical Lane Group           |           |          |       |       |             |            |         |          |      |          |              |      |

|                              | ᄼ     | <b>→</b> | •    | •    | <b>←</b> | •    | •    | <b>†</b>    | ~    | <b>/</b> | <b></b>  |      |
|------------------------------|-------|----------|------|------|----------|------|------|-------------|------|----------|----------|------|
| Movement                     | EBL   | EBT      | EBR  | WBL  | WBT      | WBR  | NBL  | NBT         | NBR  | SBL      | SBT      | SBR  |
| Lane Configurations          | 14.54 | <b>^</b> | 7    | 7    | <b>^</b> | 7    | ሻሻ   | <b>↑</b> ↑₽ |      | ሻሻ       | <b>^</b> | 7    |
| Traffic Volume (veh/h)       | 167   | 300      | 178  | 167  | 246      | 142  | 199  | 403         | 141  | 229      | 707      | 219  |
| Future Volume (veh/h)        | 167   | 300      | 178  | 167  | 246      | 142  | 199  | 403         | 141  | 229      | 707      | 219  |
| Number                       | 7     | 4        | 14   | 3    | 8        | 18   | 5    | 2           | 12   | 1        | 6        | 16   |
| Initial Q (Qb), veh          | 0     | 0        | 0    | 0    | 0        | 0    | 0    | 0           | 0    | 0        | 0        | 0    |
| Ped-Bike Adj(A_pbT)          | 1.00  |          | 0.98 | 1.00 |          | 0.99 | 1.00 |             | 1.00 | 1.00     |          | 1.00 |
| Parking Bus, Adj             | 1.00  | 1.00     | 1.00 | 1.00 | 1.00     | 1.00 | 1.00 | 1.00        | 1.00 | 1.00     | 1.00     | 1.00 |
| Adj Sat Flow, veh/h/ln       | 1863  | 1863     | 1863 | 1863 | 1863     | 1863 | 1863 | 1863        | 1900 | 1863     | 1863     | 1863 |
| Adj Flow Rate, veh/h         | 174   | 312      | 185  | 174  | 256      | 148  | 207  | 420         | 147  | 239      | 736      | 228  |
| Adj No. of Lanes             | 2     | 2        | 1    | 1    | 2        | 1    | 2    | 3           | 0    | 2        | 3        | 1    |
| Peak Hour Factor             | 0.96  | 0.96     | 0.96 | 0.96 | 0.96     | 0.96 | 0.96 | 0.96        | 0.96 | 0.96     | 0.96     | 0.96 |
| Percent Heavy Veh, %         | 2     | 2        | 2    | 2    | 2        | 2    | 2    | 2           | 2    | 2        | 2        | 2    |
| Cap, veh/h                   | 273   | 631      | 418  | 216  | 782      | 348  | 307  | 1162        | 390  | 339      | 1618     | 628  |
| Arrive On Green              | 0.08  | 0.18     | 0.18 | 0.12 | 0.22     | 0.22 | 0.09 | 0.31        | 0.31 | 0.10     | 0.32     | 0.32 |
| Sat Flow, veh/h              | 3442  | 3539     | 1554 | 1774 | 3539     | 1575 | 3442 | 3765        | 1265 | 3442     | 5085     | 1580 |
| Grp Volume(v), veh/h         | 174   | 312      | 185  | 174  | 256      | 148  | 207  | 376         | 191  | 239      | 736      | 228  |
| Grp Sat Flow(s),veh/h/ln     | 1721  | 1770     | 1554 | 1774 | 1770     | 1575 | 1721 | 1695        | 1640 | 1721     | 1695     | 1580 |
| Q Serve(g_s), s              | 3.0   | 4.9      | 6.1  | 5.9  | 3.7      | 5.0  | 3.6  | 5.3         | 5.6  | 4.1      | 7.1      | 6.3  |
| Cycle Q Clear(g_c), s        | 3.0   | 4.9      | 6.1  | 5.9  | 3.7      | 5.0  | 3.6  | 5.3         | 5.6  | 4.1      | 7.1      | 6.3  |
| Prop In Lane                 | 1.00  |          | 1.00 | 1.00 |          | 1.00 | 1.00 |             | 0.77 | 1.00     |          | 1.00 |
| Lane Grp Cap(c), veh/h       | 273   | 631      | 418  | 216  | 782      | 348  | 307  | 1047        | 506  | 339      | 1618     | 628  |
| V/C Ratio(X)                 | 0.64  | 0.49     | 0.44 | 0.80 | 0.33     | 0.43 | 0.67 | 0.36        | 0.38 | 0.70     | 0.45     | 0.36 |
| Avail Cap(c_a), veh/h        | 419   | 1035     | 596  | 245  | 1093     | 486  | 363  | 1047        | 506  | 363      | 1618     | 628  |
| HCM Platoon Ratio            | 1.00  | 1.00     | 1.00 | 1.00 | 1.00     | 1.00 | 1.00 | 1.00        | 1.00 | 1.00     | 1.00     | 1.00 |
| Upstream Filter(I)           | 1.00  | 1.00     | 1.00 | 1.00 | 1.00     | 1.00 | 1.00 | 1.00        | 1.00 | 1.00     | 1.00     | 1.00 |
| Uniform Delay (d), s/veh     | 27.5  | 22.8     | 18.7 | 26.3 | 20.1     | 20.6 | 27.2 | 16.5        | 16.6 | 26.9     | 16.7     | 13.1 |
| Incr Delay (d2), s/veh       | 2.5   | 0.6      | 0.7  | 15.8 | 0.2      | 8.0  | 3.9  | 1.0         | 2.1  | 5.6      | 0.9      | 1.6  |
| Initial Q Delay(d3),s/veh    | 0.0   | 0.0      | 0.0  | 0.0  | 0.0      | 0.0  | 0.0  | 0.0         | 0.0  | 0.0      | 0.0      | 0.0  |
| %ile BackOfQ(50%),veh/ln     | 1.5   | 2.4      | 2.7  | 3.8  | 1.8      | 2.2  | 1.9  | 2.6         | 2.8  | 2.2      | 3.4      | 3.0  |
| LnGrp Delay(d),s/veh         | 29.9  | 23.4     | 19.5 | 42.2 | 20.4     | 21.4 | 31.0 | 17.5        | 18.8 | 32.5     | 17.7     | 14.7 |
| LnGrp LOS                    | С     | С        | В    | D    | С        | С    | С    | В           | В    | С        | В        | В    |
| Approach Vol, veh/h          |       | 671      |      |      | 578      |      |      | 774         |      |          | 1203     |      |
| Approach Delay, s/veh        |       | 24.0     |      |      | 27.2     |      |      | 21.4        |      |          | 20.0     |      |
| Approach LOS                 |       | С        |      |      | С        |      |      | С           |      |          | С        |      |
| Timer                        | 1     | 2        | 3    | 4    | 5        | 6    | 7    | 8           |      |          |          |      |
| Assigned Phs                 | 1     | 2        | 3    | 4    | 5        | 6    | 7    | 8           |      |          |          |      |
| Phs Duration (G+Y+Rc), s     | 10.6  | 23.5     | 12.0 | 15.5 | 10.0     | 24.1 | 9.4  | 18.1        |      |          |          |      |
| Change Period (Y+Rc), s      | 4.5   | 4.5      | 4.5  | 4.5  | 4.5      | 4.5  | 4.5  | 4.5         |      |          |          |      |
| Max Green Setting (Gmax), s  | 6.5   | 19.0     | 8.5  | 18.0 | 6.5      | 19.0 | 7.5  | 19.0        |      |          |          |      |
| Max Q Clear Time (g_c+l1), s | 6.1   | 7.6      | 7.9  | 8.1  | 5.6      | 9.1  | 5.0  | 7.0         |      |          |          |      |
| Green Ext Time (p_c), s      | 0.0   | 2.8      | 0.0  | 1.9  | 0.1      | 4.1  | 0.1  | 1.7         |      |          |          |      |
| Intersection Summary         |       |          |      |      |          |      |      |             |      |          |          |      |
| HCM 2010 Ctrl Delay          |       |          | 22.5 |      |          |      |      |             |      |          |          |      |
| HCM 2010 LOS                 |       |          | С    |      |          |      |      |             |      |          |          |      |
|                              |       |          |      |      |          |      |      |             |      |          |          |      |

Lico Subdivision Keith Higgins Traffic Engineer

|                              | ۶    | <b>→</b> | •    | <b>√</b> | <b>←</b> | •    | •    | †        | ~    | <b>\</b> | <b></b> | ✓        |
|------------------------------|------|----------|------|----------|----------|------|------|----------|------|----------|---------|----------|
| Movement                     | EBL  | EBT      | EBR  | WBL      | WBT      | WBR  | NBL  | NBT      | NBR  | SBL      | SBT     | SBR      |
| Lane Configurations          | 7    | f.       |      | *        | f)       |      | 7    | <b>^</b> | 7    | 7        | ĵ»      |          |
| Traffic Volume (veh/h)       | 6    | 176      | 82   | 199      | 234      | 150  | 59   | 115      | 215  | 41       | 35      | 3        |
| Future Volume (veh/h)        | 6    | 176      | 82   | 199      | 234      | 150  | 59   | 115      | 215  | 41       | 35      | 3        |
| Number                       | 7    | 4        | 14   | 3        | 8        | 18   | 5    | 2        | 12   | 1        | 6       | 16       |
| Initial Q (Qb), veh          | 0    | 0        | 0    | 0        | 0        | 0    | 0    | 0        | 0    | 0        | 0       | 0        |
| Ped-Bike Adj(A_pbT)          | 1.00 |          | 0.95 | 1.00     |          | 0.99 | 1.00 |          | 0.99 | 1.00     |         | 0.99     |
| Parking Bus, Adj             | 1.00 | 1.00     | 1.00 | 1.00     | 1.00     | 1.00 | 1.00 | 1.00     | 1.00 | 1.00     | 1.00    | 1.00     |
| Adj Sat Flow, veh/h/ln       | 1863 | 1863     | 1900 | 1863     | 1863     | 1900 | 1863 | 1863     | 1863 | 1863     | 1863    | 1900     |
| Adj Flow Rate, veh/h         | 7    | 210      | 98   | 237      | 279      | 179  | 70   | 137      | 256  | 49       | 42      | 4        |
| Adj No. of Lanes             | 1    | 1        | 0    | 1        | 1        | 0    | 1    | 1        | 1    | 1        | 1       | 0        |
| Peak Hour Factor             | 0.84 | 0.84     | 0.84 | 0.84     | 0.84     | 0.84 | 0.84 | 0.84     | 0.84 | 0.84     | 0.84    | 0.84     |
| Percent Heavy Veh, %         | 2    | 2        | 2    | 2        | 2        | 2    | 2    | 2        | 2    | 2        | 2       | 2        |
| Cap, veh/h                   | 16   | 267      | 124  | 281      | 397      | 255  | 98   | 548      | 462  | 80       | 475     | 45       |
| Arrive On Green              | 0.01 | 0.23     | 0.23 | 0.16     | 0.38     | 0.38 | 0.06 | 0.29     | 0.29 | 0.05     | 0.28    | 0.28     |
| Sat Flow, veh/h              | 1774 | 1179     | 550  | 1774     | 1058     | 679  | 1774 | 1863     | 1573 | 1774     | 1674    | 159      |
| Grp Volume(v), veh/h         | 7    | 0        | 308  | 237      | 0        | 458  | 70   | 137      | 256  | 49       | 0       | 46       |
| Grp Sat Flow(s),veh/h/ln     | 1774 | 0        | 1729 | 1774     | 0        | 1738 | 1774 | 1863     | 1573 | 1774     | 0       | 1833     |
| Q Serve(g_s), s              | 0.3  | 0.0      | 10.9 | 8.5      | 0.0      | 14.6 | 2.5  | 3.7      | 8.9  | 1.8      | 0.0     | 1.2      |
| Cycle Q Clear(g_c), s        | 0.3  | 0.0      | 10.9 | 8.5      | 0.0      | 14.6 | 2.5  | 3.7      | 8.9  | 1.8      | 0.0     | 1.2      |
| Prop In Lane                 | 1.00 |          | 0.32 | 1.00     |          | 0.39 | 1.00 |          | 1.00 | 1.00     |         | 0.09     |
| Lane Grp Cap(c), veh/h       | 16   | 0        | 391  | 281      | 0        | 652  | 98   | 548      | 462  | 80       | 0       | 521      |
| V/C Ratio(X)                 | 0.43 | 0.00     | 0.79 | 0.84     | 0.00     | 0.70 | 0.72 | 0.25     | 0.55 | 0.61     | 0.00    | 0.09     |
| Avail Cap(c_a), veh/h        | 136  | 0        | 478  | 286      | 0        | 652  | 136  | 548      | 462  | 136      | 0       | 521      |
| HCM Platoon Ratio            | 1.00 | 1.00     | 1.00 | 1.00     | 1.00     | 1.00 | 1.00 | 1.00     | 1.00 | 1.00     | 1.00    | 1.00     |
| Upstream Filter(I)           | 1.00 | 0.00     | 1.00 | 1.00     | 0.00     | 1.00 | 1.00 | 1.00     | 1.00 | 1.00     | 0.00    | 1.00     |
| Uniform Delay (d), s/veh     | 32.1 | 0.0      | 23.7 | 26.6     | 0.0      | 17.3 | 30.3 | 17.5     | 19.4 | 30.5     | 0.0     | 17.1     |
| Incr Delay (d2), s/veh       | 17.1 | 0.0      | 7.0  | 19.8     | 0.0      | 3.4  | 10.2 | 1.1      | 4.7  | 7.4      | 0.0     | 0.3      |
| Initial Q Delay(d3),s/veh    | 0.0  | 0.0      | 0.0  | 0.0      | 0.0      | 0.0  | 0.0  | 0.0      | 0.0  | 0.0      | 0.0     | 0.0      |
| %ile BackOfQ(50%),veh/ln     | 0.2  | 0.0      | 6.0  | 5.7      | 0.0      | 7.5  | 1.5  | 2.0      | 4.4  | 1.0      | 0.0     | 0.6      |
| LnGrp Delay(d),s/veh         | 49.2 | 0.0      | 30.8 | 46.4     | 0.0      | 20.6 | 40.5 | 18.6     | 24.1 | 37.9     | 0.0     | 17.5     |
| LnGrp LOS                    | D    |          | С    | D        |          | С    | D    | В        | С    | D        |         | <u>B</u> |
| Approach Vol, veh/h          |      | 315      |      |          | 695      |      |      | 463      |      |          | 95      |          |
| Approach Delay, s/veh        |      | 31.2     |      |          | 29.4     |      |      | 25.0     |      |          | 28.0    |          |
| Approach LOS                 |      | С        |      |          | С        |      |      | С        |      |          | С       |          |
| Timer                        | 1    | 2        | 3    | 4        | 5        | 6    | 7    | 8        |      |          |         |          |
| Assigned Phs                 | 1    | 2        | 3    | 4        | 5        | 6    | 7    | 8        |      |          |         |          |
| Phs Duration (G+Y+Rc), s     | 7.4  | 23.7     | 14.8 | 19.2     | 8.1      | 23.0 | 5.1  | 28.9     |      |          |         |          |
| Change Period (Y+Rc), s      | 4.5  | 4.5      | 4.5  | 4.5      | 4.5      | 4.5  | 4.5  | 4.5      |      |          |         |          |
| Max Green Setting (Gmax), s  | 5.0  | 18.5     | 10.5 | 18.0     | 5.0      | 18.5 | 5.0  | 23.5     |      |          |         |          |
| Max Q Clear Time (g_c+l1), s | 3.8  | 10.9     | 10.5 | 12.9     | 4.5      | 3.2  | 2.3  | 16.6     |      |          |         |          |
| Green Ext Time (p_c), s      | 0.0  | 1.0      | 0.0  | 0.8      | 0.0      | 0.1  | 0.0  | 1.7      |      |          |         |          |
| Intersection Summary         |      |          |      |          |          |      |      |          |      |          |         |          |
| HCM 2010 Ctrl Delay          |      |          | 28.4 |          |          |      |      |          |      |          |         |          |
| HCM 2010 LOS                 |      |          | С    |          |          |      |      |          |      |          |         |          |

| Intersection           |             |          |        |          |        |                |
|------------------------|-------------|----------|--------|----------|--------|----------------|
| Int Delay, s/veh       | 4           |          |        |          |        |                |
| Movement               | WBL         | WBR      | NBT    | NBR      | SBL    | SBT            |
| Lane Configurations    | ¥           |          | 1>     |          | ሻ      | <u>□ □ □ □</u> |
| Traffic Vol, veh/h     | 28          | 132      | 184    | 13       | 37     | 142            |
| Future Vol, veh/h      | 28          | 132      | 184    | 13       | 37     | 142            |
| Conflicting Peds, #/hr | 0           | 0        | 0      | 1        | 1      | 0              |
| Sign Control           | Stop        | Stop     | Free   | Free     | Free   | Free           |
| RT Channelized         | -           | None     | -      | None     | -      | None           |
| Storage Length         | 0           | -        | _      | -        | 0      | -              |
| Veh in Median Storage  |             | _        | 0      | _        | -      | 0              |
| Grade, %               | 5, # 0<br>0 | <u> </u> | 0      | _        | _      | 0              |
|                        | 84          |          | 84     | 84       | 84     | 84             |
| Peak Hour Factor       |             | 84       |        |          |        |                |
| Heavy Vehicles, %      | 2           | 2        | 7      | 7        | 7      | 7              |
| Mvmt Flow              | 33          | 157      | 219    | 15       | 44     | 169            |
|                        |             |          |        |          |        |                |
| Major/Minor            | Minor1      | N        | Major1 | 1        | Major2 |                |
| Conflicting Flow All   | 485         | 228      | 0      | 0        | 235    | 0              |
| Stage 1                | 228         |          | _      | _        |        | _              |
| Stage 2                | 257         | _        | _      | _        | _      | _              |
| Critical Hdwy          | 6.42        | 6.22     | _      | _        | 4.17   | _              |
| Critical Hdwy Stg 1    | 5.42        | -        | _      | _        | -      | _              |
| Critical Hdwy Stg 2    | 5.42        | _        | _      | _        | _      | _              |
| Follow-up Hdwy         | 3.518       |          | _      | <u> </u> | 2.263  | _              |
| Pot Cap-1 Maneuver     | 541         | 811      | _      | _        | 1303   | _              |
|                        | 810         | -        | _      | _        | 1303   | _              |
| Stage 1                |             |          | _      | -        |        |                |
| Stage 2                | 786         | -        | -      | -        | -      | -              |
| Platoon blocked, %     | 500         | 040      | -      | -        | 4000   | -              |
| Mov Cap-1 Maneuver     | 522         | 810      | -      | -        | 1302   | -              |
| Mov Cap-2 Maneuver     | 522         | -        | -      | -        | -      | -              |
| Stage 1                | 782         | -        | -      | -        | -      | -              |
| Stage 2                | 786         | -        | -      | -        | -      | -              |
|                        |             |          |        |          |        |                |
| Approach               | WB          |          | NB     |          | SB     |                |
| HCM Control Delay, s   | 11.6        |          | 0      |          | 1.6    |                |
| HCM LOS                | В           |          | U      |          | 1.0    |                |
| I IOW LOG              | ь           |          |        |          |        |                |
|                        |             |          |        |          |        |                |
| Minor Lane/Major Mvn   | nt          | NBT      | NBRV   | VBLn1    | SBL    | SBT            |
| Capacity (veh/h)       |             | -        | -      | 739      | 1302   | -              |
| HCM Lane V/C Ratio     |             | _        | -      | 0.258    |        | _              |
| HCM Control Delay (s)  |             | -        | _      | 11.6     | 7.9    | -              |
| HCM Lane LOS           |             | _        | -      | В        | Α      | -              |
| HCM 95th %tile Q(veh   | )           | -        | -      | 1        | 0.1    | -              |
|                        | ,           |          |        |          |        |                |

| Intersection  |          |  |   |  |      |      |
|---|----------|--|---|--|------|------|
| Intersection Delay, s/veh   | 9.5      |  |   |  |      |      |
| Intersection LOS  | 9.5<br>A |  |   |  |      |      |
| Intoroccion LOO   |          |  |   |  |      |      |
| M   | MO       | WDD  | NET   | NDD  | ODI  | ODT  |
| Movement  | WBL      | WBR  | NBT   | NBR  | SBL  | SBT  |
| Lane Configurations   | ¥        | 400  | <b>f</b>  | 40   | 07   | 4    |
| Traffic Vol, veh/h  | 28       | 132  | 184   | 13   | 37   | 142  |
| Future Vol, veh/h   | 28       | 132  | 184   | 13   | 37   | 142  |
| Peak Hour Factor  | 0.84     | 0.84   | 0.84  | 0.84   | 0.84 | 0.84 |
| Heavy Vehicles, %   | 2        | 2  | 7   | 7  | 7    | 7    |
| Mvmt Flow   | 33       | 157  | 219   | 15   | 44   | 169  |
| Number of Lanes   | 1        | 0  | 1   | 0  | 0    | 1    |
| Approach  | WB       |  | NB  |  | SB   |      |
| Opposing Approach   |          |  | SB  |  | NB   |      |
| Opposing Lanes  | 0        |  | 1   |  | 1    |      |
| Conflicting Approach Left   | NB       |  |   |  | WB   |      |
| Conflicting Lanes Left  | 1        |  | 0   |  | 1    |      |
| Conflicting Approach Right  | SB       |  | WB  |  |      |      |
| Conflicting Lanes Right   | 1        |  | 1   |  | 0    |      |
| HCM Control Delay   | 9        |  | 9.8   |  | 9.7  |      |
| HCM LOS   | Α        |  | Α   |  | Α    |      |
|   |          |  |   |  |      |      |
| Lane  |          | NBLn1  | WBLn1   | SBLn1  |      |      |
| Vol Left, %   |          | 0%   | 17%   | 21%  |      |      |
| Vol Thru, %   |          | 93%  | 0%  | 79%  |      |      |
| Vol Right, %  |          | 7%   | 82%   | 0%   |      |      |
| Sign Control  |          | Stop   |   |  |      |      |
| Traffic Vol by Lane   |          |  | Stop  | Stop   |      |      |
|   |          | 197  | 5top<br>160   | Stop<br>179  |      |      |
| LT Vol  |          |  |   |  |      |      |
| LT Vol<br>Through Vol   |          | 197  | 160   | 179  |      |      |
|   |          | 197<br>0   | 160<br>28   | 179<br>37  |      |      |
| Through Vol   |          | 197<br>0<br>184  | 160<br>28<br>0  | 179<br>37<br>142   |      |      |
| Through Vol<br>RT Vol   |          | 197<br>0<br>184<br>13  | 160<br>28<br>0<br>132   | 179<br>37<br>142<br>0  |      |      |
| Through Vol<br>RT Vol<br>Lane Flow Rate   |          | 197<br>0<br>184<br>13<br>235   | 160<br>28<br>0<br>132<br>190  | 179<br>37<br>142<br>0<br>213   |      |      |
| Through Vol RT Vol Lane Flow Rate Geometry Grp Degree of Util (X)   |          | 197<br>0<br>184<br>13<br>235   | 160<br>28<br>0<br>132<br>190  | 179<br>37<br>142<br>0<br>213   |      |      |
| Through Vol<br>RT Vol<br>Lane Flow Rate<br>Geometry Grp   |          | 197<br>0<br>184<br>13<br>235<br>1<br>0.304<br>4.671<br>Yes                                 | 160<br>28<br>0<br>132<br>190<br>1<br>0.239<br>4.516<br>Yes                              | 179<br>37<br>142<br>0<br>213<br>1<br>0.282<br>4.772<br>Yes                                 |      |      |
| Through Vol RT Vol Lane Flow Rate Geometry Grp Degree of Util (X) Departure Headway (Hd) Convergence, Y/N Cap   |          | 197<br>0<br>184<br>13<br>235<br>1<br>0.304<br>4.671<br>Yes<br>767                          | 160<br>28<br>0<br>132<br>190<br>1<br>0.239<br>4.516                                     | 179<br>37<br>142<br>0<br>213<br>1<br>0.282<br>4.772<br>Yes<br>750                          |      |      |
| Through Vol RT Vol Lane Flow Rate Geometry Grp Degree of Util (X) Departure Headway (Hd) Convergence, Y/N Cap Service Time                                      |          | 197<br>0<br>184<br>13<br>235<br>1<br>0.304<br>4.671<br>Yes<br>767<br>2.715                 | 160<br>28<br>0<br>132<br>190<br>1<br>0.239<br>4.516<br>Yes<br>792<br>2.556              | 179<br>37<br>142<br>0<br>213<br>1<br>0.282<br>4.772<br>Yes<br>750<br>2.817                 |      |      |
| Through Vol RT Vol Lane Flow Rate Geometry Grp Degree of Util (X) Departure Headway (Hd) Convergence, Y/N Cap Service Time HCM Lane V/C Ratio                   |          | 197<br>0<br>184<br>13<br>235<br>1<br>0.304<br>4.671<br>Yes<br>767<br>2.715<br>0.306        | 160<br>28<br>0<br>132<br>190<br>1<br>0.239<br>4.516<br>Yes<br>792                       | 179<br>37<br>142<br>0<br>213<br>1<br>0.282<br>4.772<br>Yes<br>750<br>2.817<br>0.284        |      |      |
| Through Vol RT Vol Lane Flow Rate Geometry Grp Degree of Util (X) Departure Headway (Hd) Convergence, Y/N Cap Service Time HCM Lane V/C Ratio HCM Control Delay |          | 197<br>0<br>184<br>13<br>235<br>1<br>0.304<br>4.671<br>Yes<br>767<br>2.715<br>0.306<br>9.8 | 160<br>28<br>0<br>132<br>190<br>1<br>0.239<br>4.516<br>Yes<br>792<br>2.556<br>0.24<br>9 | 179<br>37<br>142<br>0<br>213<br>1<br>0.282<br>4.772<br>Yes<br>750<br>2.817<br>0.284<br>9.7 |      |      |
| Through Vol RT Vol Lane Flow Rate Geometry Grp Degree of Util (X) Departure Headway (Hd) Convergence, Y/N Cap Service Time HCM Lane V/C Ratio                   |          | 197<br>0<br>184<br>13<br>235<br>1<br>0.304<br>4.671<br>Yes<br>767<br>2.715<br>0.306        | 160<br>28<br>0<br>132<br>190<br>1<br>0.239<br>4.516<br>Yes<br>792<br>2.556<br>0.24      | 179<br>37<br>142<br>0<br>213<br>1<br>0.282<br>4.772<br>Yes<br>750<br>2.817<br>0.284        |      |      |

|                               | ٠          | <b>→</b> | •     | •    | +          | •          | •       | <b>†</b> | <i>&gt;</i> | <b>/</b> | <b>↓</b> | 4    |
|-------------------------------|------------|----------|-------|------|------------|------------|---------|----------|-------------|----------|----------|------|
| Movement                      | EBL        | EBT      | EBR   | WBL  | WBT        | WBR        | NBL     | NBT      | NBR         | SBL      | SBT      | SBR  |
| Lane Configurations           | Ť          | <b>^</b> | 7     | Ţ    | <b>†</b> † | 7          | ሻሻ      | f)       |             | Ţ        | ĵ.       | _    |
| Traffic Volume (vph)          | 11         | 492      | 262   | 9    | 667        | 28         | 543     | 25       | 3           | 46       | 23       | 5    |
| Future Volume (vph)           | 11         | 492      | 262   | 9    | 667        | 28         | 543     | 25       | 3           | 46       | 23       | 5    |
| Ideal Flow (vphpl)            | 1900       | 1900     | 1900  | 1900 | 1900       | 1900       | 1900    | 1900     | 1900        | 1900     | 1900     | 1900 |
| Total Lost time (s)           | 4.5        | 4.5      | 4.5   | 4.5  | 4.5        | 4.5        | 4.5     | 4.5      |             | 4.5      | 4.5      |      |
| Lane Util. Factor             | 1.00       | 0.95     | 1.00  | 1.00 | 0.95       | 1.00       | 0.97    | 1.00     |             | 1.00     | 1.00     |      |
| Frt                           | 1.00       | 1.00     | 0.85  | 1.00 | 1.00       | 0.85       | 1.00    | 0.98     |             | 1.00     | 0.97     |      |
| Flt Protected                 | 0.95       | 1.00     | 1.00  | 0.95 | 1.00       | 1.00       | 0.95    | 1.00     |             | 0.95     | 1.00     |      |
| Satd. Flow (prot)             | 1612       | 3223     | 1442  | 1543 | 3085       | 1380       | 3433    | 1834     |             | 1719     | 1763     |      |
| Flt Permitted                 | 0.95       | 1.00     | 1.00  | 0.95 | 1.00       | 1.00       | 0.95    | 1.00     |             | 0.95     | 1.00     |      |
| Satd. Flow (perm)             | 1612       | 3223     | 1442  | 1543 | 3085       | 1380       | 3433    | 1834     |             | 1719     | 1763     |      |
| Peak-hour factor, PHF         | 0.96       | 0.96     | 0.96  | 0.96 | 0.96       | 0.96       | 0.96    | 0.96     | 0.96        | 0.96     | 0.96     | 0.96 |
| Adj. Flow (vph)               | 11         | 512      | 273   | 9    | 695        | 29         | 566     | 26       | 3           | 48       | 24       | 5    |
| RTOR Reduction (vph)          | 0          | 0        | 172   | 0    | 0          | 18         | 0       | 2        | 0           | 0        | 5        | 0    |
| Lane Group Flow (vph)         | 11         | 513      | 101   | 9    | 695        | 11         | 566     | 27       | 0           | 48       | 24       | 0    |
| Heavy Vehicles (%)            | 12%        | 12%      | 12%   | 17%  | 17%        | 17%        | 2%      | 2%       | 2%          | 5%       | 5%       | 5%   |
| Turn Type                     | Prot       | NA       | Perm  | Prot | NA         | Perm       | Prot    | NA       |             | Prot     | NA       |      |
| Protected Phases              | 7          | 4        |       | 3    | 8          |            | 1       | 6        |             | 5        | 2        |      |
| Permitted Phases              |            |          | 4     |      |            | 8          |         |          |             |          |          |      |
| Actuated Green, G (s)         | 0.7        | 18.2     | 18.2  | 0.7  | 18.2       | 18.2       | 11.6    | 8.8      |             | 3.7      | 0.9      |      |
| Effective Green, g (s)        | 0.7        | 18.2     | 18.2  | 0.7  | 18.2       | 18.2       | 11.6    | 8.8      |             | 3.7      | 0.9      |      |
| Actuated g/C Ratio            | 0.01       | 0.37     | 0.37  | 0.01 | 0.37       | 0.37       | 0.23    | 0.18     |             | 0.07     | 0.02     |      |
| Clearance Time (s)            | 4.5        | 4.5      | 4.5   | 4.5  | 4.5        | 4.5        | 4.5     | 4.5      |             | 4.5      | 4.5      |      |
| Vehicle Extension (s)         | 3.0        | 3.0      | 3.0   | 3.0  | 3.0        | 3.0        | 3.0     | 3.0      |             | 3.0      | 3.0      |      |
| Lane Grp Cap (vph)            | 22         | 1187     | 531   | 21   | 1136       | 508        | 806     | 326      |             | 128      | 32       |      |
| v/s Ratio Prot                | c0.01      | 0.16     |       | 0.01 | c0.23      |            | c0.16   | 0.01     |             | 0.03     | c0.01    |      |
| v/s Ratio Perm                |            |          | 0.07  |      |            | 0.01       |         |          |             |          |          |      |
| v/c Ratio                     | 0.50       | 0.43     | 0.19  | 0.43 | 0.61       | 0.02       | 0.70    | 0.08     |             | 0.38     | 0.75     |      |
| Uniform Delay, d1             | 24.2       | 11.7     | 10.6  | 24.2 | 12.7       | 9.9        | 17.3    | 16.9     |             | 21.7     | 24.1     |      |
| Progression Factor            | 1.00       | 1.00     | 1.00  | 1.00 | 1.00       | 1.00       | 1.00    | 1.00     |             | 1.00     | 1.00     |      |
| Incremental Delay, d2         | 16.8       | 1.1      | 8.0   | 13.4 | 2.5        | 0.1        | 2.8     | 0.1      |             | 1.8      | 65.7     |      |
| Delay (s)                     | 40.9       | 12.9     | 11.4  | 37.6 | 15.2       | 10.0       | 20.1    | 17.0     |             | 23.6     | 89.8     |      |
| Level of Service              | D          | В        | В     | D    | В          | В          | С       | В        |             | С        | F        |      |
| Approach Delay (s)            |            | 12.7     |       |      | 15.3       |            |         | 20.0     |             |          | 48.5     |      |
| Approach LOS                  |            | В        |       |      | В          |            |         | В        |             |          | D        |      |
| Intersection Summary          |            |          |       |      |            |            |         |          |             |          |          |      |
| HCM 2000 Control Delay        |            |          | 16.8  | Н    | CM 2000    | Level of   | Service |          | В           |          |          |      |
| HCM 2000 Volume to Capa       | city ratio |          | 0.65  |      |            |            |         |          |             |          |          |      |
| Actuated Cycle Length (s)     |            |          | 49.4  |      | um of los  |            |         |          | 18.0        |          |          |      |
| Intersection Capacity Utiliza | ation      |          | 48.1% | IC   | CU Level   | of Service | 1       |          | Α           |          |          |      |
| Analysis Period (min)         |            |          | 15    |      |            |            |         |          |             |          |          |      |
| c Critical Lane Group         |            |          |       |      |            |            |         |          |             |          |          |      |

| Intersection           |        |          |          |       |          |      |
|------------------------|--------|----------|----------|-------|----------|------|
| Int Delay, s/veh       | 3.8    |          |          |       |          |      |
|                        |        | WDD      | NDT      | NDD   | CDI      | CDT  |
| Movement               | WBL    | WBR      | NBT      | NBR   | SBL      | SBT  |
| Lane Configurations    | ¥      | 70       | <b>₽</b> | 4.4   | <b>\</b> | 100  |
| Traffic Vol, veh/h     | 9      | 76       | 95       | 14    | 112      | 138  |
| Future Vol, veh/h      | 9      | 76       | 95       | 14    | 112      | 138  |
| Conflicting Peds, #/hr | 1      | 0        | 0        | 0     | _ 0      | _ 0  |
| Sign Control           | Stop   | Stop     | Free     | Free  | Free     | Free |
| RT Channelized         | -      | None     | -        |       | 450      | None |
| Storage Length         | 0      | -        | -        | -     | 150      | -    |
| Veh in Median Storage  |        | -        | 0        | -     | -        | 0    |
| Grade, %               | 0      | -        | 0        | -     | -        | 0    |
| Peak Hour Factor       | 91     | 91       | 91       | 91    | 91       | 91   |
| Heavy Vehicles, %      | 6      | 6        | 2        | 2     | 3        | 3    |
| Mvmt Flow              | 10     | 84       | 104      | 15    | 123      | 152  |
|                        |        |          |          |       |          |      |
| Major/Minor I          | Minor1 | N        | Major1   | -     | Major2   |      |
| Conflicting Flow All   | 511    | 112      | 0        | 0     | 119      | 0    |
| Stage 1                | 112    | -        | -        | -     | -        | -    |
| Stage 2                | 399    | <u>-</u> | _        | _     | _        | _    |
| Critical Hdwy          | 6.46   | 6.26     |          |       | 4.13     | _    |
| Critical Hdwy Stg 1    | 5.46   | 0.20     |          | _     | 7.10     | _    |
| Critical Hdwy Stg 2    | 5.46   | _        | -        | _     | -        |      |
| Follow-up Hdwy         | 3.554  | 3.354    | _        | _     |          | _    |
| Pot Cap-1 Maneuver     | 516    | 930      |          | _     | 1463     | -    |
| •                      | 903    | 930      | -        | -     | 1403     | -    |
| Stage 1                |        |          | -        | -     | -        |      |
| Stage 2                | 669    | -        | -        | -     | -        | -    |
| Platoon blocked, %     | 470    | 000      | -        | -     | 4.400    | -    |
| Mov Cap-1 Maneuver     | 472    | 930      | -        | -     | 1463     | -    |
| Mov Cap-2 Maneuver     | 472    | -        | -        | -     | -        | -    |
| Stage 1                | 827    | -        | -        | -     | -        | -    |
| Stage 2                | 668    | -        | -        | -     | -        | -    |
|                        |        |          |          |       |          |      |
| Approach               | WB     |          | NB       |       | SB       |      |
| HCM Control Delay, s   | 9.8    |          | 0        |       | 3.4      |      |
| HCM LOS                | Α      |          | U        |       | 0.7      |      |
| TIOW EOO               | , ,    |          |          |       |          |      |
|                        |        |          |          |       |          |      |
| Minor Lane/Major Mvm   | nt     | NBT      | NBRV     | VBLn1 | SBL      | SBT  |
| Capacity (veh/h)       |        | -        | -        |       | 1463     | -    |
| HCM Lane V/C Ratio     |        | -        | -        | 0.111 | 0.084    | -    |
| HCM Control Delay (s)  |        | -        | -        | 9.8   | 7.7      | -    |
| HCM Lane LOS           |        | -        | -        | Α     | Α        | -    |
| HCM 95th %tile Q(veh)  | )      | -        | -        | 0.4   | 0.3      | -    |
|                        |        |          |          |       |          |      |

| Intersection  |          |  |  |  |          |      |  |
|---|----------|--|--|--|----------|------|--|
| Intersection Delay, s/veh   | 8.9      |  |  |  |          |      |  |
| Intersection LOS  | A        |  |  |  |          |      |  |
|   |          |  |  |  |          |      |  |
| Movement  | WBL      | WBR  | NBT  | NBR  | CDI      | SBT  |  |
| Movement  |          | WBK  |  | INDK   | SBL      |      |  |
| Lane Configurations   | À        | 70   | <u>4</u>   | 4.4  | 440      | 4    |  |
| Traffic Vol, veh/h  | 9        | 76   | 95   | 14   | 112      | 138  |  |
| Future Vol, veh/h   | 9        | 76   | 95   | 14   | 112      | 138  |  |
| Peak Hour Factor  | 0.91     | 0.91   | 0.91   | 0.91   | 0.91     | 0.91 |  |
| Heavy Vehicles, %   | 6        | 6  | 2  | 2  | 3        | 3    |  |
| Mvmt Flow   | 10       | 84   | 104  | 15   | 123      | 152  |  |
| Number of Lanes   | 1        | 0  | 1  | 0  | 0        | 1    |  |
| Approach  | WB       |  | NB   |  | SB       |      |  |
| Opposing Approach   |          |  | SB   |  | NB       |      |  |
| Opposing Lanes  | 0        |  | 1  |  | 1        |      |  |
| Conflicting Approach Left   | NB       |  |  |  | WB       |      |  |
| Conflicting Lanes Left  | 1        |  | 0  |  | 1        |      |  |
| Conflicting Approach Right  | SB       |  | WB   |  | •        |      |  |
| Conflicting Lanes Right   | 1        |  | 1  |  | 0        |      |  |
| HCM Control Delay   | 7.9      |  | 8.1  |  | 9.5      |      |  |
| HCM LOS   | 7.5<br>A |  | Α  |  | 3.5<br>A |      |  |
|   |          |  |  |  |          |      |  |
| TIOWI LOO   | 7.       |  | , ,  |  | , ,      |      |  |
|   |          | NRI n1   |  | QRI n1   | ,,       |      |  |
| Lane  | A        | NBLn1  | WBLn1  | SBLn1  |          |      |  |
| Lane<br>Vol Left, %   |          | 0%   | WBLn1<br>11%   | 45%  |          |      |  |
| Lane Vol Left, % Vol Thru, %  |          | 0%<br>87%  | WBLn1<br>11%<br>0%   | 45%<br>55%   |          |      |  |
| Lane Vol Left, % Vol Thru, % Vol Right, %   |          | 0%<br>87%<br>13%   | WBLn1<br>11%<br>0%<br>89%  | 45%<br>55%<br>0%   |          |      |  |
| Lane Vol Left, % Vol Thru, % Vol Right, % Sign Control  | 7        | 0%<br>87%<br>13%<br>Stop   | WBLn1<br>11%<br>0%<br>89%<br>Stop                                    | 45%<br>55%<br>0%<br>Stop   |          |      |  |
| Lane Vol Left, % Vol Thru, % Vol Right, % Sign Control Traffic Vol by Lane  |          | 0%<br>87%<br>13%<br>Stop<br>109  | WBLn1 11% 0% 89% Stop 85   | 45%<br>55%<br>0%<br>Stop<br>250  |          |      |  |
| Lane Vol Left, % Vol Thru, % Vol Right, % Sign Control Traffic Vol by Lane LT Vol   |          | 0%<br>87%<br>13%<br>Stop<br>109  | WBLn1 11% 0% 89% Stop 85 9   | 45%<br>55%<br>0%<br>Stop<br>250<br>112   |          |      |  |
| Lane Vol Left, % Vol Thru, % Vol Right, % Sign Control Traffic Vol by Lane LT Vol Through Vol   |          | 0%<br>87%<br>13%<br>Stop<br>109<br>0   | WBLn1 11% 0% 89% Stop 85 9 0   | 45%<br>55%<br>0%<br>Stop<br>250<br>112<br>138  |          |      |  |
| Lane Vol Left, % Vol Thru, % Vol Right, % Sign Control Traffic Vol by Lane LT Vol Through Vol RT Vol  |          | 0%<br>87%<br>13%<br>Stop<br>109<br>0<br>95   | WBLn1 11% 0% 89% Stop 85 9 0 76                                      | 45%<br>55%<br>0%<br>Stop<br>250<br>112<br>138  |          |      |  |
| Lane Vol Left, % Vol Thru, % Vol Right, % Sign Control Traffic Vol by Lane LT Vol Through Vol RT Vol Lane Flow Rate   |          | 0%<br>87%<br>13%<br>Stop<br>109<br>0<br>95<br>14   | WBLn1 11% 0% 89% Stop 85 9 0 76                                      | 45%<br>55%<br>0%<br>Stop<br>250<br>112<br>138  |          |      |  |
| Lane Vol Left, % Vol Thru, % Vol Right, % Sign Control Traffic Vol by Lane LT Vol Through Vol RT Vol Lane Flow Rate Geometry Grp  |          | 0%<br>87%<br>13%<br>Stop<br>109<br>0<br>95<br>14<br>120  | WBLn1 11% 0% 89% Stop 85 9 0 76 93                                   | 45%<br>55%<br>0%<br>Stop<br>250<br>112<br>138<br>0<br>275  |          |      |  |
| Lane Vol Left, % Vol Thru, % Vol Right, % Sign Control Traffic Vol by Lane LT Vol Through Vol RT Vol Lane Flow Rate   |          | 0%<br>87%<br>13%<br>Stop<br>109<br>0<br>95<br>14   | WBLn1 11% 0% 89% Stop 85 9 0 76                                      | 45%<br>55%<br>0%<br>Stop<br>250<br>112<br>138<br>0   |          |      |  |
| Lane Vol Left, % Vol Thru, % Vol Right, % Sign Control Traffic Vol by Lane LT Vol Through Vol RT Vol Lane Flow Rate Geometry Grp  |          | 0%<br>87%<br>13%<br>Stop<br>109<br>0<br>95<br>14<br>120  | WBLn1 11% 0% 89% Stop 85 9 0 76 93                                   | 45%<br>55%<br>0%<br>Stop<br>250<br>112<br>138<br>0<br>275  |          |      |  |
| Lane Vol Left, % Vol Thru, % Vol Right, % Sign Control Traffic Vol by Lane LT Vol Through Vol RT Vol Lane Flow Rate Geometry Grp Degree of Util (X)   |          | 0%<br>87%<br>13%<br>Stop<br>109<br>0<br>95<br>14<br>120<br>1   | WBLn1 11% 0% 89% Stop 85 9 0 76 93 1 0.113                           | 45%<br>55%<br>0%<br>Stop<br>250<br>112<br>138<br>0<br>275<br>1   |          |      |  |
| Lane Vol Left, % Vol Thru, % Vol Right, % Sign Control Traffic Vol by Lane LT Vol Through Vol RT Vol Lane Flow Rate Geometry Grp Degree of Util (X) Departure Headway (Hd)  |          | 0%<br>87%<br>13%<br>Stop<br>109<br>0<br>95<br>14<br>120<br>1<br>0.145<br>4.358                                 | WBLn1 11% 0% 89% Stop 85 9 0 76 93 1 0.113 4.368                     | 45%<br>55%<br>0%<br>Stop<br>250<br>112<br>138<br>0<br>275<br>1<br>0.328<br>4.297                                 |          |      |  |
| Lane  Vol Left, %  Vol Thru, %  Vol Right, %  Sign Control  Traffic Vol by Lane  LT Vol  Through Vol  RT Vol  Lane Flow Rate  Geometry Grp  Degree of Util (X)  Departure Headway (Hd)  Convergence, Y/N  |          | 0%<br>87%<br>13%<br>Stop<br>109<br>0<br>95<br>14<br>120<br>1<br>0.145<br>4.358<br>Yes                          | WBLn1 11% 0% 89% Stop 85 9 0 76 93 1 0.113 4.368 Yes                 | 45%<br>55%<br>0%<br>Stop<br>250<br>112<br>138<br>0<br>275<br>1<br>0.328<br>4.297<br>Yes                          |          |      |  |
| Lane  Vol Left, %  Vol Thru, %  Vol Right, %  Sign Control  Traffic Vol by Lane  LT Vol  Through Vol  RT Vol  Lane Flow Rate  Geometry Grp  Degree of Util (X)  Departure Headway (Hd)  Convergence, Y/N  Cap  Service Time                     |          | 0%<br>87%<br>13%<br>Stop<br>109<br>0<br>95<br>14<br>120<br>1<br>0.145<br>4.358<br>Yes<br>826                   | WBLn1 11% 0% 89% Stop 85 9 0 76 93 1 0.113 4.368 Yes 824             | 45%<br>55%<br>0%<br>Stop<br>250<br>112<br>138<br>0<br>275<br>1<br>0.328<br>4.297<br>Yes<br>824                   |          |      |  |
| Lane  Vol Left, %  Vol Thru, %  Vol Right, %  Sign Control  Traffic Vol by Lane  LT Vol  Through Vol  RT Vol  Lane Flow Rate  Geometry Grp  Degree of Util (X)  Departure Headway (Hd)  Convergence, Y/N  Cap  Service Time  HCM Lane V/C Ratio |          | 0%<br>87%<br>13%<br>Stop<br>109<br>0<br>95<br>14<br>120<br>1<br>0.145<br>4.358<br>Yes<br>826<br>2.368<br>0.145 | WBLn1 11% 0% 89% Stop 85 9 0 76 93 1 0.113 4.368 Yes 824 2.375 0.113 | 45%<br>55%<br>0%<br>Stop<br>250<br>112<br>138<br>0<br>275<br>1<br>0.328<br>4.297<br>Yes<br>824<br>2.392<br>0.334 |          |      |  |
| Lane  Vol Left, %  Vol Thru, %  Vol Right, %  Sign Control  Traffic Vol by Lane  LT Vol  Through Vol  RT Vol  Lane Flow Rate  Geometry Grp  Degree of Util (X)  Departure Headway (Hd)  Convergence, Y/N  Cap  Service Time                     |          | 0%<br>87%<br>13%<br>Stop<br>109<br>0<br>95<br>14<br>120<br>1<br>0.145<br>4.358<br>Yes<br>826<br>2.368          | WBLn1 11% 0% 89% Stop 85 9 0 76 93 1 0.113 4.368 Yes 824 2.375       | 45%<br>55%<br>0%<br>Stop<br>250<br>112<br>138<br>0<br>275<br>1<br>0.328<br>4.297<br>Yes<br>824<br>2.392          |          |      |  |

0.5

0.4

1.4

HCM 95th-tile Q

|                               | ۶          | <b>→</b>   | •     | •     | +         | •          | •       | <b>†</b> | <i>&gt;</i> | <b>/</b> | <b>↓</b> | 4    |
|-------------------------------|------------|------------|-------|-------|-----------|------------|---------|----------|-------------|----------|----------|------|
| Movement                      | EBL        | EBT        | EBR   | WBL   | WBT       | WBR        | NBL     | NBT      | NBR         | SBL      | SBT      | SBR  |
| Lane Configurations           | ۲          | <b>†</b> † | 7     | , j   | <b>†</b>  | 7          | ሻሻ      | f)       |             | ¥        | ĵ.       |      |
| Traffic Volume (vph)          | 1          | 566        | 441   | 22    | 620       | 27         | 329     | 16       | 48          | 132      | 154      | 1    |
| Future Volume (vph)           | 1          | 566        | 441   | 22    | 620       | 27         | 329     | 16       | 48          | 132      | 154      | 1    |
| Ideal Flow (vphpl)            | 1900       | 1900       | 1900  | 1900  | 1900      | 1900       | 1900    | 1900     | 1900        | 1900     | 1900     | 1900 |
| Total Lost time (s)           | 4.5        | 4.5        | 4.5   | 4.5   | 4.5       | 4.5        | 4.5     | 4.5      |             | 4.5      | 4.5      |      |
| Lane Util. Factor             | 1.00       | 0.95       | 1.00  | 1.00  | 0.95      | 1.00       | 0.97    | 1.00     |             | 1.00     | 1.00     |      |
| Frt                           | 1.00       | 1.00       | 0.85  | 1.00  | 1.00      | 0.85       | 1.00    | 0.89     |             | 1.00     | 1.00     |      |
| Flt Protected                 | 0.95       | 1.00       | 1.00  | 0.95  | 1.00      | 1.00       | 0.95    | 1.00     |             | 0.95     | 1.00     |      |
| Satd. Flow (prot)             | 1687       | 3374       | 1509  | 1583  | 3167      | 1417       | 3433    | 1653     |             | 1770     | 1861     |      |
| Flt Permitted                 | 0.95       | 1.00       | 1.00  | 0.95  | 1.00      | 1.00       | 0.95    | 1.00     |             | 0.95     | 1.00     |      |
| Satd. Flow (perm)             | 1687       | 3374       | 1509  | 1583  | 3167      | 1417       | 3433    | 1653     |             | 1770     | 1861     |      |
| Peak-hour factor, PHF         | 0.94       | 0.94       | 0.94  | 0.94  | 0.94      | 0.94       | 0.94    | 0.94     | 0.94        | 0.94     | 0.94     | 0.94 |
| Adj. Flow (vph)               | 1          | 602        | 469   | 23    | 660       | 29         | 350     | 17       | 51          | 140      | 164      | 1    |
| RTOR Reduction (vph)          | 0          | 0          | 311   | 0     | 0         | 19         | 0       | 44       | 0           | 0        | 0        | 0    |
| Lane Group Flow (vph)         | 1          | 602        | 158   | 23    | 660       | 10         | 350     | 24       | 0           | 140      | 165      | 0    |
| Heavy Vehicles (%)            | 7%         | 7%         | 7%    | 14%   | 14%       | 14%        | 2%      | 2%       | 2%          | 2%       | 2%       | 2%   |
| Turn Type                     | Prot       | NA         | Perm  | Prot  | NA        | Perm       | Prot    | NA       |             | Prot     | NA       |      |
| Protected Phases              | 7          | 4          |       | 3     | 8         |            | 1       | 6        |             | 5        | 2        |      |
| Permitted Phases              |            |            | 4     |       |           | 8          |         |          |             |          |          |      |
| Actuated Green, G (s)         | 8.0        | 18.2       | 18.2  | 0.8   | 18.2      | 18.2       | 9.0     | 7.2      |             | 9.8      | 8.0      |      |
| Effective Green, g (s)        | 8.0        | 18.2       | 18.2  | 8.0   | 18.2      | 18.2       | 9.0     | 7.2      |             | 9.8      | 8.0      |      |
| Actuated g/C Ratio            | 0.01       | 0.34       | 0.34  | 0.01  | 0.34      | 0.34       | 0.17    | 0.13     |             | 0.18     | 0.15     |      |
| Clearance Time (s)            | 4.5        | 4.5        | 4.5   | 4.5   | 4.5       | 4.5        | 4.5     | 4.5      |             | 4.5      | 4.5      |      |
| Vehicle Extension (s)         | 3.0        | 3.0        | 3.0   | 3.0   | 3.0       | 3.0        | 3.0     | 3.0      |             | 3.0      | 3.0      |      |
| Lane Grp Cap (vph)            | 24         | 1137       | 508   | 23    | 1067      | 477        | 572     | 220      |             | 321      | 275      |      |
| v/s Ratio Prot                | 0.00       | 0.18       |       | c0.01 | c0.21     |            | c0.10   | 0.01     |             | 0.08     | c0.09    |      |
| v/s Ratio Perm                |            |            | 0.10  |       |           | 0.01       |         |          |             |          |          |      |
| v/c Ratio                     | 0.04       | 0.53       | 0.31  | 1.00  | 0.62      | 0.02       | 0.61    | 0.11     |             | 0.44     | 0.60     |      |
| Uniform Delay, d1             | 26.2       | 14.4       | 13.3  | 26.6  | 15.0      | 11.9       | 20.9    | 20.6     |             | 19.6     | 21.5     |      |
| Progression Factor            | 1.00       | 1.00       | 1.00  | 1.00  | 1.00      | 1.00       | 1.00    | 1.00     |             | 1.00     | 1.00     |      |
| Incremental Delay, d2         | 0.7        | 1.8        | 1.6   | 187.7 | 2.7       | 0.1        | 1.9     | 0.2      |             | 1.0      | 3.5      |      |
| Delay (s)                     | 26.9       | 16.2       | 14.8  | 214.3 | 17.7      | 12.0       | 22.8    | 20.8     |             | 20.6     | 25.0     |      |
| Level of Service              | С          | В          | В     | F     | В         | В          | С       | С        |             | С        | С        |      |
| Approach Delay (s)            |            | 15.6       |       |       | 23.8      |            |         | 22.5     |             |          | 23.0     |      |
| Approach LOS                  |            | В          |       |       | С         |            |         | С        |             |          | С        |      |
| Intersection Summary          |            |            |       |       |           |            |         |          |             |          |          |      |
| HCM 2000 Control Delay        |            |            | 20.0  | Н     | CM 2000   | Level of   | Service |          | В           |          |          |      |
| HCM 2000 Volume to Capa       | city ratio |            | 0.62  |       |           |            |         |          |             |          |          |      |
| Actuated Cycle Length (s)     |            |            | 54.0  |       | um of los |            |         |          | 18.0        |          |          |      |
| Intersection Capacity Utiliza | tion       |            | 50.9% | IC    | CU Level  | of Service |         |          | Α           |          |          |      |
| Analysis Period (min)         |            |            | 15    |       |           |            |         |          |             |          |          |      |
| c Critical Lane Group         |            |            |       |       |           |            |         |          |             |          |          |      |

## Appendix E

Level of Service

Calculations

Background

Conditions

| Intersection               |      |         |       |       |         |       |       |          |       |       |         |       |
|----------------------------|------|---------|-------|-------|---------|-------|-------|----------|-------|-------|---------|-------|
| Intersection Delay, s/veh  | 15.7 |         |       |       |         |       |       |          |       |       |         |       |
| Intersection LOS           | С    |         |       |       |         |       |       |          |       |       |         |       |
|                            |      |         |       |       |         |       |       |          |       |       |         |       |
| Movement                   | EBL  | EBT     | EBR   | WBL   | WBT     | WBR   | NBL   | NBT      | NBR   | SBL   | SBT     | SBR   |
| Lane Configurations        | J.   | <u></u> | 7     | 7     | <b></b> | 7     | ሻ     | <b>₽</b> |       | , Y   | <u></u> | 7     |
| Traffic Vol, veh/h         | 125  | 127     | 89    | 7     | 213     | 94    | 208   | 82       | 3     | 69    | 34      | 135   |
| Future Vol, veh/h          | 125  | 127     | 89    | 7     | 213     | 94    | 208   | 82       | 3     | 69    | 34      | 135   |
| Peak Hour Factor           | 0.90 | 0.90    | 0.90  | 0.90  | 0.90    | 0.90  | 0.90  | 0.90     | 0.90  | 0.90  | 0.90    | 0.90  |
| Heavy Vehicles, %          | 7    | 7       | 7     | 5     | 5       | 5     | 2     | 2        | 2     | 6     | 6       | 6     |
| Mvmt Flow                  | 139  | 141     | 99    | 8     | 237     | 104   | 231   | 91       | 3     | 77    | 38      | 150   |
| Number of Lanes            | 1    | 1       | 1     | 1     | 1       | 1     | 1     | 1        | 0     | 1     | 1       | 1     |
| Approach                   | EB   |         |       | WB    |         |       | NB    |          |       | SB    |         |       |
| Opposing Approach          | WB   |         |       | EB    |         |       | SB    |          |       | NB    |         |       |
| Opposing Lanes             | 3    |         |       | 3     |         |       | 3     |          |       | 2     |         |       |
| Conflicting Approach Left  | SB   |         |       | NB    |         |       | EB    |          |       | WB    |         |       |
| Conflicting Lanes Left     | 3    |         |       | 2     |         |       | 3     |          |       | 3     |         |       |
| Conflicting Approach Right | NB   |         |       | SB    |         |       | WB    |          |       | EB    |         |       |
| Conflicting Lanes Right    | 2    |         |       | 3     |         |       | 3     |          |       | 3     |         |       |
| HCM Control Delay          | 14.1 |         |       | 17.1  |         |       | 18    |          |       | 13.5  |         |       |
| HCM LOS                    | В    |         |       | С     |         |       | С     |          |       | В     |         |       |
|                            |      |         |       |       |         |       |       |          |       |       |         |       |
| Lane                       |      | NBLn1   | NBLn2 | EBLn1 | EBLn2   | EBLn3 | WBLn1 | WBLn2    | WBLn3 | SBLn1 | SBLn2   | SBLn3 |
| Vol Left, %                |      | 100%    | 0%    | 100%  | 0%      | 0%    | 100%  | 0%       | 0%    | 100%  | 0%      | 0%    |
| Vol Thru, %                |      | 0%      | 96%   | 0%    | 100%    | 0%    | 0%    | 100%     | 0%    | 0%    | 100%    | 0%    |
| Vol Right, %               |      | 0%      | 4%    | 0%    | 0%      | 100%  | 0%    | 0%       | 100%  | 0%    | 0%      | 100%  |
| Sign Control               |      | Stop    | Stop  | Stop  | Stop    | Stop  | Stop  | Stop     | Stop  | Stop  | Stop    | Stop  |
| Traffic Vol by Lane        |      | 208     | 85    | 125   | 127     | 89    | 7     | 213      | 94    | 69    | 34      | 135   |

| Lane                   | NBLn1 | NBLn2 | EBLn1 | EBLn2 | EBLn3 | WBLn1 | WBLn2 | WBLn3 | SBLn1 | SBLn2 | SBLn3 |
|------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Vol Left, %            | 100%  | 0%    | 100%  | 0%    | 0%    | 100%  | 0%    | 0%    | 100%  | 0%    | 0%    |
| Vol Thru, %            | 0%    | 96%   | 0%    | 100%  | 0%    | 0%    | 100%  | 0%    | 0%    | 100%  | 0%    |
| Vol Right, %           | 0%    | 4%    | 0%    | 0%    | 100%  | 0%    | 0%    | 100%  | 0%    | 0%    | 100%  |
| Sign Control           | Stop  |
| Traffic Vol by Lane    | 208   | 85    | 125   | 127   | 89    | 7     | 213   | 94    | 69    | 34    | 135   |
| LT Vol                 | 208   | 0     | 125   | 0     | 0     | 7     | 0     | 0     | 69    | 0     | 0     |
| Through Vol            | 0     | 82    | 0     | 127   | 0     | 0     | 213   | 0     | 0     | 34    | 0     |
| RT Vol                 | 0     | 3     | 0     | 0     | 89    | 0     | 0     | 94    | 0     | 0     | 135   |
| Lane Flow Rate         | 231   | 94    | 139   | 141   | 99    | 8     | 237   | 104   | 77    | 38    | 150   |
| Geometry Grp           | 8     | 8     | 8     | 8     | 8     | 8     | 8     | 8     | 8     | 8     | 8     |
| Degree of Util (X)     | 0.533 | 0.204 | 0.328 | 0.313 | 0.2   | 0.018 | 0.527 | 0.212 | 0.187 | 0.087 | 0.315 |
| Departure Headway (Hd) | 8.3   | 7.775 | 8.496 | 7.987 | 7.273 | 8.527 | 8.017 | 7.304 | 8.774 | 8.268 | 7.558 |
| Convergence, Y/N       | Yes   |
| Cap                    | 434   | 460   | 422   | 449   | 491   | 418   | 447   | 489   | 408   | 432   | 474   |
| Service Time           | 6.071 | 5.547 | 6.275 | 5.765 | 5.051 | 6.305 | 5.795 | 5.081 | 6.556 | 6.049 | 5.34  |
| HCM Lane V/C Ratio     | 0.532 | 0.204 | 0.329 | 0.314 | 0.202 | 0.019 | 0.53  | 0.213 | 0.189 | 0.088 | 0.316 |
| HCM Control Delay      | 20.2  | 12.5  | 15.4  | 14.4  | 11.9  | 11.5  | 19.5  | 12.1  | 13.6  | 11.8  | 13.8  |
| HCM Lane LOS           | С     | В     | С     | В     | В     | В     | С     | В     | В     | В     | В     |
| HCM 95th-tile Q        | 3.1   | 0.8   | 1.4   | 1.3   | 0.7   | 0.1   | 3     | 8.0   | 0.7   | 0.3   | 1.3   |

| Intersection           |         |          |        |        |          |      |        |          |       |        |          |       |      |
|------------------------|---------|----------|--------|--------|----------|------|--------|----------|-------|--------|----------|-------|------|
| Int Delay, s/veh       | 5.5     |          |        |        |          |      |        |          |       |        |          |       |      |
| Movement               | EBL     | EBT      | EBR    | WBL    | WBT      | WBR  | NBL    | NBT      | NBR   | SBL    | SBT      | SBR   |      |
| Lane Configurations    | ች       | <b>†</b> | 7      | ች      | <b>†</b> | 7    | *      | <b>†</b> | 7     | 1      | <b>↑</b> | 1     |      |
| Traffic Vol, veh/h     | 46      | 248      | 15     | 37     | 490      | 25   | 45     | 4        | 54    | 39     | 3        | 140   |      |
| -uture Vol, veh/h      | 46      | 248      | 15     | 37     | 490      | 25   | 45     | 4        | 54    | 39     | 3        | 140   |      |
| Conflicting Peds, #/hr | 0       | 0        | 1      | 0      | 0        | 0    | 0      | 0        | 0     | 0      | 0        | 0     |      |
| Sign Control           | Free    | Free     | Free   | Free   | Free     | Free | Stop   | Stop     | Stop  | Stop   | Stop     | Stop  |      |
| RT Channelized         | -       | -        | None   | -      | -        | None | -      | -        | None  | -      | -        | None  |      |
| Storage Length         | 320     | -        | 505    | 360    | -        | 195  | 60     | -        | 0     | 100    | -        | 100   |      |
| Veh in Median Storage, | # -     | 0        | -      | _      | 0        | -    | -      | 0        | -     | -      | 0        | -     |      |
| Grade, %               | _       | 0        | -      | -      | 0        | -    | -      | 0        | -     | -      | 0        | -     |      |
| Peak Hour Factor       | 95      | 95       | 95     | 95     | 95       | 95   | 95     | 95       | 95    | 95     | 95       | 95    |      |
| Heavy Vehicles, %      | 8       | 8        | 8      | 4      | 4        | 4    | 2      | 2        | 2     | 3      | 3        | 3     |      |
| Mvmt Flow              | 48      | 261      | 16     | 39     | 516      | 26   | 47     | 4        | 57    | 41     | 3        | 147   |      |
|                        |         |          |        |        |          |      |        |          |       |        |          |       |      |
| Major/Minor N          | /lajor1 |          | -      | Major2 |          | ı    | Minor1 |          | - 1   | Minor2 |          |       |      |
| Conflicting Flow All   | 542     | 0        | 0      | 278    | 0        | 0    | 1040   | 978      | 262   | 990    | 968      | 516   |      |
| Stage 1                | -       | -        | _      |        | _        | _    | 358    | 358      |       | 594    | 594      | -     |      |
| Stage 2                | _       | _        | _      | _      | _        | _    | 682    | 620      | _     | 396    | 374      | _     |      |
| Critical Hdwy          | 4.18    | _        | _      | 4.14   | _        | _    | 7.12   | 6.52     | 6.22  | 7.13   | 6.53     | 6.23  |      |
| Critical Hdwy Stg 1    | -       | _        | _      | -      | _        | _    | 6.12   | 5.52     | -     | 6.13   | 5.53     | -     |      |
| Critical Hdwy Stg 2    | -       | -        | _      | _      | _        | -    | 6.12   | 5.52     | _     | 6.13   | 5.53     | -     |      |
|                        | 2.272   | _        | _      | 2.236  | _        | _    | 3.518  |          | 3.318 | 3.527  | 4.027    | 3.327 |      |
| Pot Cap-1 Maneuver     | 997     | -        | _      | 1273   | _        | _    | 208    | 250      | 777   | 224    | 253      | 557   |      |
| Stage 1                | -       | _        | -      | -      | _        | _    | 660    | 628      | -     | 490    | 491      | -     |      |
| Stage 2                | -       | -        | _      | _      | -        | -    | 440    | 480      | -     | 627    | 616      | -     |      |
| Platoon blocked, %     |         | _        | -      |        | _        | _    |        |          |       | ·      |          |       |      |
| Mov Cap-1 Maneuver     | 997     | -        | -      | 1272   | _        | _    | 142    | 231      | 776   | 193    | 233      | 557   |      |
| Mov Cap-2 Maneuver     | -       | -        | -      | -      | -        | -    | 142    | 231      | -     | 193    | 233      | -     |      |
| Stage 1                | -       | -        | -      | -      | -        | -    | 628    | 597      | -     | 466    | 476      | -     |      |
| Stage 2                | _       | -        | -      | -      | -        | _    | 312    | 465      | -     | 549    | 586      | _     |      |
| Ü                      |         |          |        |        |          |      |        |          |       |        |          |       |      |
| Approach               | EB      |          |        | WB     |          |      | NB     |          |       | SB     |          |       |      |
| HCM Control Delay, s   | 1.3     |          |        | 0.5    |          |      | 24.6   |          |       | 17.1   |          |       |      |
| HCM LOS                |         |          |        |        |          |      | C      |          |       | С      |          |       |      |
|                        |         |          |        |        |          |      |        |          |       |        |          |       |      |
| Minor Lane/Major Mvmt  | 1       | NBLn1    | NBLn21 | VBLn3  | EBL      | EBT  | EBR    | WBL      | WBT   | WBR    | SBLn1    | SBLn2 | SBLn |
| Capacity (veh/h)       |         | 142      | 231    | 776    | 997      | -    |        | 1272     | -     | -      |          | 233   | 557  |
| HCM Lane V/C Ratio     |         |          | 0.018  |        |          | -    |        | 0.031    | -     | -      |          | 0.014 |      |
| HCM Control Delay (s)  |         | 42.5     | 20.9   | 10     | 8.8      | _    | _      | 7.9      | _     | -      |          | 20.7  | 13.8 |
| HCM Lane LOS           |         | E        | C      | В      | A        | _    | _      | A        | _     | -      | D        | C     | В    |
| HCM 95th %tile Q(veh)  |         | 1.3      | 0.1    | 0.2    | 0.2      | -    | -      | 0.1      | -     | -      | 0.8      | 0     | 1.1  |
|                        |         |          |        |        |          |      |        |          |       |        |          |       |      |

| Intersection           |        |          |           |       |        |      |
|------------------------|--------|----------|-----------|-------|--------|------|
| Int Delay, s/veh       | 2.1    |          |           |       |        |      |
|                        |        | W/DD     | NET       | NEE   | 051    | 057  |
| Movement               | WBL    | WBR      | NBT       | NBR   | SBL    | SBT  |
| Lane Configurations    | ¥      |          | <b>\$</b> |       | 10     | 4    |
| Traffic Vol, veh/h     | 32     | 62       | 300       | 31    | 13     | 188  |
| Future Vol, veh/h      | 32     | 62       | 300       | 31    | 13     | 188  |
| Conflicting Peds, #/hr | 0      | 0        | _ 0       | _ 1   | _ 1    | _ 0  |
| Sign Control           | Stop   | Stop     | Free      | Free  | Free   | Free |
| RT Channelized         | -      | None     | -         |       | -      | None |
| Storage Length         | 0      | -        | -         | -     | -      | -    |
| Veh in Median Storage  |        | -        | 0         | -     | -      | 0    |
| Grade, %               | 0      | -        | 0         | -     | -      | 0    |
| Peak Hour Factor       | 84     | 84       | 84        | 84    | 84     | 84   |
| Heavy Vehicles, %      | 2      | 2        | 7         | 7     | 7      | 7    |
| Mvmt Flow              | 38     | 74       | 357       | 37    | 15     | 224  |
|                        |        |          |           |       |        |      |
| Major/Minor I          | Minor1 | N        | /lajor1   |       | Major2 |      |
| Conflicting Flow All   | 631    | 377      | 0         | 0     | 395    | 0    |
| Stage 1                | 377    | -        | -         | -     | -      | -    |
| Stage 2                | 254    | <u> </u> | _         | _     | _      | _    |
| Critical Hdwy          | 6.42   | 6.22     | -         | _     | 4.17   | _    |
| Critical Hdwy Stg 1    | 5.42   | 0.22     |           | _     | 4.17   | _    |
| Critical Hdwy Stg 2    | 5.42   |          | -         | -     | -      | -    |
| Follow-up Hdwy         | 3.518  |          | _         | -     | 2.263  | -    |
| Pot Cap-1 Maneuver     | 445    | 670      | -         | -     | 1137   | -    |
| •                      | 694    | - 070    | _         | -     | -      | -    |
| Stage 1                |        |          | -         | -     |        | -    |
| Stage 2                | 788    | -        | -         | -     | -      | -    |
| Platoon blocked, %     | 400    | 000      | -         | -     | 4400   | -    |
| Mov Cap-1 Maneuver     | 438    | 669      | -         | -     | 1136   | -    |
| Mov Cap-2 Maneuver     | 438    | -        | -         | -     | -      | -    |
| Stage 1                | 683    | -        | -         | -     | -      | -    |
| Stage 2                | 788    | -        | -         | -     | -      | -    |
|                        |        |          |           |       |        |      |
| Approach               | WB     |          | NB        |       | SB     |      |
| HCM Control Delay, s   | 12.9   |          | 0         |       | 0.5    |      |
| HCM LOS                | В      |          | v         |       | 0.0    |      |
| TIOM LOO               |        |          |           |       |        |      |
|                        |        |          |           |       |        |      |
| Minor Lane/Major Mvm   | nt     | NBT      | NBRV      | VBLn1 | SBL    | SBT  |
| Capacity (veh/h)       |        | -        | -         | 567   | 1136   | -    |
| HCM Lane V/C Ratio     |        | -        | -         | 0.197 |        | -    |
| HCM Control Delay (s)  |        | -        | -         |       | 8.2    | 0    |
| HCM Lane LOS           |        | -        | -         | В     | Α      | Α    |
| HCM 95th %tile Q(veh   | )      | -        | -         | 0.7   | 0      | -    |
|                        |        |          |           |       |        |      |

| Movement   EBL   EBT   EBR   WBL   WBT   WBR   NBL   NBT   NBR   SBL   SBR   SBR   Lane Configurations   1  |                          | •    | <b>→</b> | •     | <b>√</b> | <b>←</b> | •    | •   | <b>†</b> | ~   | <b>/</b> | <b></b>  | ✓   |
|---|--------------------------|------|----------|-------|----------|----------|------|-----|----------|-----|----------|----------|-----|
| Traffic Volume (veh/h)  | Movement                 | EBL  | EBT      | EBR   | WBL      | WBT      | WBR  | NBL | NBT      | NBR | SBL      | SBT      | SBR |
| Future Volume (veh/h)  193  178  124  144  385  291  282  393  23  119  161  147  Number  7  4  144  385  291  282  393  23  119  161  147  Number  7  4  144  385  8  8  8  8  8  8  8  8  8  8  2  2  12  1   | Lane Configurations      | 7    | 1>       |       | ሻ        |          |      | ሻ   | <b>↑</b> | 7   | ሻ        | <b>↑</b> |     |
| Number 7 4 14 3 8 18 5 2 112 1 6 16 16 16 Initial Q (Qb), veh 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0   | Traffic Volume (veh/h)   |      |          |       |          |          |      |     |          |     |          |          |     |
| Initial Q (Qb), weh   | Future Volume (veh/h)    | 193  |          |       |          | 335      |      |     | 393      |     | 119      |          |     |
| Ped-Bike Adj(A_pbT)   | Number                   | 7    | 4        | 14    | 3        | 8        | 18   | 5   | 2        | 12  | 1        | 6        | 16  |
| Parking Bus, Adj  | , , ,                    |      | 0        |       |          | 0        |      |     | 0        |     |          | 0        | -   |
| Adj Sat Flow, veh/h/ln         1776         1776         1900         1863         1863         1863         1863         1827         1827         1827           Adj No. of Lanes         1         1         0         1         1         0         1   | <b>;</b> , ,             |      |          |       |          |          |      |     |          |     |          |          |     |
| Adj Flow Rate, veh/h         210         193         135         15         364         316         307         427         25         129         175         160           Adj No of Lanes         1         1         0         1  | -                        |      |          |       |          |          |      |     |          |     |          |          |     |
| Adj No. of Lanes         1         1         0         1         1         0         1         2         2         2         2         2         2         4         4         4         4         4         Cape, weln/h         338         195         136         432         224         195         254         513         436         141         300         331           Arrivo On Green         0.20         0.20         0.20         0.22         0.01         0.21         0.02         0.02         10.22         0.01         0.03         10.22         10.01         0.03         10.1         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0   |                          |      |          |       |          |          |      |     |          |     |          |          |     |
| Peak Hour Factor         0.92         4         2   | -                        |      |          |       |          |          |      |     |          |     |          |          | 160 |
| Percent Heavy Veh, %  |                          |      | *        |       |          |          |      |     |          |     |          |          | 1   |
| Cap, veh/h  338  195  136  432  224  195  254  513  436  141  390  331  Arrive On Green  0.20  0.20  0.20  0.20  0.24  0.24  0.14  0.14  0.28  0.28  0.08  0.21  0.21  0.21  321  Sat Flow, veh/h  1691  973  681  1774  922  800  1774  1863  1583  1740  1827  1553  Grp Volume(v), veh/h  1691  0  1654  1774  0  1722  1774  1863  1583  1740  1827  1553  Q Serve(g_ s), s  10.2  0.0  17.8  0.6  0.0  21.9  12.9  12.9  12.9  13.0  14.0  1.0  1.0  1.0  1.0  1.0  1.0  |                          |      |          |       |          |          |      |     |          |     |          |          |     |
| Arrive On Green   | •                        |      |          |       |          |          |      |     |          |     |          |          | -   |
| Sat Flow, veh/h         1691         973         681         1774         922         800         1774         1863         1583         1740         1827         1553           Gry Volume(v), veh/h         210         0         328         15         0         680         307         427         25         129         175         160           Gry Sat Flow(s), veh/h/ln         1691         0         1654         1774         0         1722         1774         1863         1583         1740         1827         1553           Qserve(g. s), s         10.2         0.0         17.8         0.6         0.0         21.9         12.9         19.4         1.0         6.6         7.5         8.1           Cycle Q Clear(g. c), s         10.2         0.0         17.8         0.6         0.0         21.9         12.9         19.4         1.0         6.6         7.5         8.1           Cycle Q Clear(g. c), s         10.0         0.41         1.00         0.46         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00<   |                          |      |          |       |          |          |      |     |          |     |          |          |     |
| Grp Volume(v), veh/h         210         0         328         15         0         680         307         427         25         129         175         160           Grp Sat Flow(s), veh/h/ln         1691         0         1654         1774         0         1722         1774         1863         1583         1740         1827         1553           Q Serve(g_s), s         10.2         0.0         17.8         0.6         0.0         21.9         12.9         19.4         1.0         6.6         7.5         8.1           Cycle Q Clear(g_c), s         10.2         0.0         17.8         0.6         0.0         21.9         12.9         19.4         1.0         6.6         7.5         8.1           Prop In Lane         1.00         0.41         1.00         0.46         1.00         1.00         1.00           Lane Grp Cap(c), veh/h         338         0         331         432         0         419         254         513         436         141         390         331           V/C Ratio(X)         0.62         0.00         0.99         0.03         0.00         1.60         1.21         0.83         0.06         0.91         0.48 </td <td></td>  |                          |      |          |       |          |          |      |     |          |     |          |          |     |
| Grp Sat Flow(s), veh/h/ln 1691 0 1654 1774 0 1722 1774 1863 1583 1740 1827 1553 Q Serve(g, s), s 10.2 0.0 17.8 0.6 0.0 21.9 12.9 19.4 1.0 6.6 7.5 8.1 Cycle Q Clear(g, c), s 10.2 0.0 17.8 0.6 0.0 21.9 12.9 19.4 1.0 6.6 7.5 8.1 Cycle Q Clear(g, c), s 10.2 0.0 17.8 0.6 0.0 21.9 12.9 19.4 1.0 6.6 7.5 8.1 Cycle Q Clear(g, c), s 10.2 0.0 17.8 0.6 0.0 21.9 12.9 19.4 1.0 6.6 7.5 8.1 Cycle Q Clear(g, c), s 10.2 0.0 1.0 1.00 0.46 1.00 1.00 1.00 1.00 1.00 Lane Grp Cap(c), veh/h 338 0 331 432 0 419 254 513 436 141 390 331 V/C Ratio(X) 0.62 0.00 0.99 0.03 0.00 1.62 1.21 0.83 0.06 0.91 0.45 0.48 Avail Cap(c, a), veh/h 338 0 331 432 0 419 254 513 436 141 390 331 V/C Ratio(X) 0.62 0.00 0.99 0.03 0.00 1.62 1.21 0.83 0.06 0.91 0.45 0.48 Avail Cap(c, a), veh/h 338 0 331 432 0 419 254 513 436 141 390 331 CMC Patio(X) 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.0   |                          |      | 973      |       |          | 922      | 800  |     |          |     |          | 1827     |     |
| Q Serve(g_s), s   | 1 7,                     |      |          |       |          |          |      |     |          |     |          |          |     |
| Cycle Q Clear(g_c), s         10.2         0.0         17.8         0.6         0.0         21.9         12.9         19.4         1.0         6.6         7.5         8.1           Prop In Lane         1.00         0.41         1.00         0.46         1.00         1.00         1.00         1.00           Lane GFD Cap(c), veh/h         338         0         331         432         0         419         254         513         436         141         390         331           V/C Ratio(X)         0.62         0.00         0.99         0.03         0.00         1.62         1.21         0.83         0.06         0.91         0.45         0.48           Avail Cap(c_a), veh/h         338         0         331         432         0         419         254         513         436         141         390         331           HCM Platoon Ratio         1.00   | Grp Sat Flow(s),veh/h/ln |      |          |       |          |          |      |     |          |     |          |          |     |
| Prop In Lane         1.00         0.41         1.00         0.46         1.00         1.00         1.00         1.00           Lane Grp Cap(c), veh/h         338         0         331         432         0         419         254         513         436         141         390         331           V/C Ratio(X)         0.62         0.00         0.99         0.03         0.00         1.62         1.21         0.83         0.06         0.91         0.45         0.48           Avail Cap(c_a), veh/h         338         0         331         432         0         419         254         513         436         141         390         331           HCM Platoon Ratio         1.00         1  |                          |      |          |       |          |          |      |     |          |     |          |          |     |
| Lane Grp Cap(c), veh/h 338 0 331 432 0 419 254 513 436 141 390 331 V/C Ratio(X) 0.62 0.00 0.99 0.03 0.00 1.62 1.21 0.83 0.06 0.91 0.45 0.48 Avail Cap(c_a), veh/h 338 0 331 432 0 419 254 513 436 141 390 331 HCM Platoon Ratio 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.0  |                          |      | 0.0      |       |          | 0.0      |      |     | 19.4     |     |          | 7.5      |     |
| V/C Ratio(X)         0.62         0.00         0.99         0.03         0.00         1.62         1.21         0.83         0.06         0.91         0.45         0.48           Avail Cap(c_a), veh/h         338         0         331         432         0         419         254         513         436         141         390         331           HCM Platoon Ratio         1.00<  |                          |      |          |       |          |          |      |     |          |     |          |          |     |
| Avail Cap(c_a), veh/h Blatoon Ratio  1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.  |                          |      |          |       |          |          |      |     |          |     |          |          |     |
| HCM Platoon Ratio   | ` '                      |      |          |       |          |          |      |     |          |     |          |          |     |
| Upstream Filter(I)  |                          |      |          |       |          |          |      |     |          |     |          |          |     |
| Uniform Delay (d), s/veh 32.9 0.0 35.9 26.0 0.0 34.1 38.5 30.6 24.0 41.0 30.8 31.0 Incr Delay (d2), s/veh 3.5 0.0 47.2 0.0 0.0 291.2 124.3 14.6 0.3 50.8 3.7 5.0 Initial Q Delay(d3), s/veh 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.  |                          |      |          |       |          |          |      |     |          |     |          |          |     |
| Incr Delay (d2), s/veh   3.5   0.0   47.2   0.0   0.0   291.2   124.3   14.6   0.3   50.8   3.7   5.0     Initial Q Delay(d3), s/veh   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0     Wile BackOfQ(50%), veh/ln   5.1   0.0   12.4   0.3   0.0   44.2   15.1   12.0   0.5   5.2   4.2   3.9     InGrp Delay(d), s/veh   36.3   0.0   83.1   26.0   0.0   325.3   162.8   45.2   24.2   91.8   34.5   36.0     InGrp LOS   D   F   C   F   F   D   C   F   C   D     Approach Vol, veh/h   538   695   759   464     Approach Delay, s/veh   64.8   318.8   92.1   51.0     Approach LOS   E   F   F   D     Timer   1   2   3   4   5   6   7   8     Assigned Phs   1   2   4   5   6   8     Phs Duration (G+Y+Rc), s   11.8   29.3   22.5   17.4   23.7   26.4     Change Period (Y+Rc), s   4.5   4.5   4.5   4.5   4.5     Max Green Setting (Gmax), s   7.3   24.8   18.0   12.9   19.2   21.9     Max Q Clear Time (g_c+I1), s   8.6   21.4   19.8   14.9   10.1   23.9     Green Ext Time (p_c), s   0.0   0.9   0.0   0.0   0.0     Intersection Summary   HCM 2010 Ctrl Delay   142.5  |                          |      |          |       |          |          |      |     |          |     |          |          |     |
| Initial Q Delay(d3),s/veh   0.0 |                          |      |          |       |          |          |      |     |          |     |          |          |     |
| %ile BackOfQ(50%), veh/ln       5.1       0.0       12.4       0.3       0.0       44.2       15.1       12.0       0.5       5.2       4.2       3.9         LnGrp Delay(d), s/veh       36.3       0.0       83.1       26.0       0.0       325.3       162.8       45.2       24.2       91.8       34.5       36.0         LnGrp LOS       D       F       C       F       F       D       C       F       C       D         Approach Vol, veh/h       538       695       759       464         Approach Delay, s/veh       64.8       318.8       92.1       51.0         Approach LOS       E       F       F       F       D         Timer       1       2       3       4       5       6       7       8         Assigned Phs       1       2       3       4       5       6       8       8         Phs Duration (G+Y+Rc), s       11.8       29.3       22.5       17.4       23.7       26.4       26.4         Change Period (Y+Rc), s       4.5       4.5       4.5       4.5       4.5       4.5         Max Q Clear Time (g_c+l1), s       8.6       21.4       1  |                          |      |          |       |          |          |      |     |          |     |          |          |     |
| LnGrp Delay(d),s/veh         36.3         0.0         83.1         26.0         0.0         325.3         162.8         45.2         24.2         91.8         34.5         36.0           LnGrp LOS         D         F         C         F         F         D         C         F         C         D           Approach Vol, veh/h         538         695         759         464           Approach Delay, s/veh         64.8         318.8         92.1         51.0           Approach LOS         E         F         F         F         D           Timer         1         2         3         4         5         6         7         8           Assigned Phs         1         2         4         5         6         8         8           Phs Duration (G+Y+Rc), s         11.8         29.3         22.5         17.4         23.7         26.4           Change Period (Y+Rc), s         4.5         4.5         4.5         4.5         4.5           Max Green Setting (Gmax), s         7.3         24.8         18.0         12.9         19.2         21.9           Max Q Clear Time (g_c+I), s         8.6         21.4         19.8   |                          |      |          |       |          |          |      |     |          |     |          |          |     |
| LnGrp LOS         D         F         C         F         F         D         C         F         C         D           Approach Vol, veh/h         538         695         759         464           Approach Delay, s/veh         64.8         318.8         92.1         51.0           Approach LOS         E         F         F         F         D           Timer         1         2         3         4         5         6         7         8           Assigned Phs         1         2         4         5         6         8         8           Phs Duration (G+Y+Rc), s         11.8         29.3         22.5         17.4         23.7         26.4           Change Period (Y+Rc), s         4.5         4.5         4.5         4.5         4.5           Max Green Setting (Gmax), s         7.3         24.8         18.0         12.9         19.2         21.9           Max Q Clear Time (g_c+l1), s         8.6         21.4         19.8         14.9         10.1         23.9           Green Ext Time (p_c), s         0.0         0.9         0.0         0.0         1.0         0.0    Intersection Summary  HCM 2010 Ctrl Delay   142.5   | ` '                      |      |          |       |          |          |      |     |          |     |          |          |     |
| Approach Vol, veh/h       538       695       759       464         Approach Delay, s/veh       64.8       318.8       92.1       51.0         Approach LOS       E       F       F       F         Timer       1       2       3       4       5       6       7       8         Assigned Phs       1       2       4       5       6       8       8         Phs Duration (G+Y+Rc), s       11.8       29.3       22.5       17.4       23.7       26.4         Change Period (Y+Rc), s       4.5       4.5       4.5       4.5       4.5         Max Green Setting (Gmax), s       7.3       24.8       18.0       12.9       19.2       21.9         Max Q Clear Time (g_c+l1), s       8.6       21.4       19.8       14.9       10.1       23.9         Green Ext Time (p_c), s       0.0       0.9       0.0       0.0       1.0       0.0         Intersection Summary         HCM 2010 Ctrl Delay       142.5   |                          |      | 0.0      |       |          | 0.0      |      |     |          |     |          |          |     |
| Approach Delay, s/veh       64.8       318.8       92.1       51.0         Approach LOS       E       F       F       D         Timer       1       2       3       4       5       6       7       8         Assigned Phs       1       2       4       5       6       8         Phs Duration (G+Y+Rc), s       11.8       29.3       22.5       17.4       23.7       26.4         Change Period (Y+Rc), s       4.5       4.5       4.5       4.5       4.5         Max Green Setting (Gmax), s       7.3       24.8       18.0       12.9       19.2       21.9         Max Q Clear Time (g_c+I1), s       8.6       21.4       19.8       14.9       10.1       23.9         Green Ext Time (p_c), s       0.0       0.9       0.0       0.0       1.0       0.0         Intersection Summary         HCM 2010 Ctrl Delay       142.5   | LnGrp LOS                | D    |          | F     | С        |          | F    | F   |          | С   | F        |          | D   |
| Approach LOS E F F D  Timer 1 2 3 4 5 6 7 8  Assigned Phs 1 2 4 5 6 8  Phs Duration (G+Y+Rc), s 11.8 29.3 22.5 17.4 23.7 26.4  Change Period (Y+Rc), s 4.5 4.5 4.5 4.5 4.5  Max Green Setting (Gmax), s 7.3 24.8 18.0 12.9 19.2 21.9  Max Q Clear Time (g_c+I1), s 8.6 21.4 19.8 14.9 10.1 23.9  Green Ext Time (p_c), s 0.0 0.9 0.0 0.0 1.0 0.0  Intersection Summary  HCM 2010 Ctrl Delay 142.5   | Approach Vol, veh/h      |      |          |       |          |          |      |     |          |     |          |          |     |
| Timer         1         2         3         4         5         6         7         8           Assigned Phs         1         2         4         5         6         8           Phs Duration (G+Y+Rc), s         11.8         29.3         22.5         17.4         23.7         26.4           Change Period (Y+Rc), s         4.5         4.5         4.5         4.5         4.5           Max Green Setting (Gmax), s         7.3         24.8         18.0         12.9         19.2         21.9           Max Q Clear Time (g_c+I1), s         8.6         21.4         19.8         14.9         10.1         23.9           Green Ext Time (p_c), s         0.0         0.9         0.0         0.0         1.0         0.0           Intersection Summary           HCM 2010 Ctrl Delay         142.5         142.5         142.5   |                          |      |          |       |          | 318.8    |      |     | 92.1     |     |          | 51.0     |     |
| Assigned Phs 1 2 4 5 6 8 Phs Duration (G+Y+Rc), s 11.8 29.3 22.5 17.4 23.7 26.4 Change Period (Y+Rc), s 4.5 4.5 4.5 4.5 4.5 Max Green Setting (Gmax), s 7.3 24.8 18.0 12.9 19.2 21.9 Max Q Clear Time (g_c+I1), s 8.6 21.4 19.8 14.9 10.1 23.9 Green Ext Time (p_c), s 0.0 0.9 0.0 0.0 1.0 0.0  Intersection Summary HCM 2010 Ctrl Delay 142.5  | Approach LOS             |      | Е        |       |          | F        |      |     | F        |     |          | D        |     |
| Phs Duration (G+Y+Rc), s       11.8       29.3       22.5       17.4       23.7       26.4         Change Period (Y+Rc), s       4.5       4.5       4.5       4.5       4.5         Max Green Setting (Gmax), s       7.3       24.8       18.0       12.9       19.2       21.9         Max Q Clear Time (g_c+l1), s       8.6       21.4       19.8       14.9       10.1       23.9         Green Ext Time (p_c), s       0.0       0.9       0.0       0.0       1.0       0.0         Intersection Summary         HCM 2010 Ctrl Delay       142.5  | Timer                    | 1    | 2        | 3     | 4        | 5        | 6    | 7   | 8        |     |          |          |     |
| Change Period (Y+Rc), s 4.5 4.5 4.5 4.5 4.5 4.5 4.5 Max Green Setting (Gmax), s 7.3 24.8 18.0 12.9 19.2 21.9 Max Q Clear Time (g_c+I1), s 8.6 21.4 19.8 14.9 10.1 23.9 Green Ext Time (p_c), s 0.0 0.9 0.0 0.0 1.0 0.0 Intersection Summary  HCM 2010 Ctrl Delay 142.5  | Assigned Phs             | 1    | 2        |       | 4        | 5        | 6    |     | 8        |     |          |          |     |
| Max Green Setting (Gmax), s       7.3       24.8       18.0       12.9       19.2       21.9         Max Q Clear Time (g_c+I1), s       8.6       21.4       19.8       14.9       10.1       23.9         Green Ext Time (p_c), s       0.0       0.9       0.0       0.0       1.0       0.0         Intersection Summary         HCM 2010 Ctrl Delay       142.5   | Phs Duration (G+Y+Rc), s | 11.8 | 29.3     |       | 22.5     | 17.4     | 23.7 |     | 26.4     |     |          |          |     |
| Max Q Clear Time (g_c+l1), s       8.6       21.4       19.8       14.9       10.1       23.9         Green Ext Time (p_c), s       0.0       0.9       0.0       0.0       1.0       0.0         Intersection Summary         HCM 2010 Ctrl Delay       142.5  | Change Period (Y+Rc), s  | 4.5  | 4.5      |       | 4.5      | 4.5      | 4.5  |     | 4.5      |     |          |          |     |
| Max Q Clear Time (g_c+l1), s       8.6       21.4       19.8       14.9       10.1       23.9         Green Ext Time (p_c), s       0.0       0.9       0.0       0.0       1.0       0.0         Intersection Summary         HCM 2010 Ctrl Delay       142.5  |                          |      |          |       |          | 12.9     |      |     |          |     |          |          |     |
| Intersection Summary HCM 2010 Ctrl Delay 142.5  |                          | 8.6  | 21.4     |       | 19.8     | 14.9     | 10.1 |     | 23.9     |     |          |          |     |
| HCM 2010 Ctrl Delay 142.5   |                          | 0.0  | 0.9      |       | 0.0      | 0.0      | 1.0  |     | 0.0      |     |          |          |     |
|   | Intersection Summary     |      |          |       |          |          |      |     |          |     |          |          |     |
|   | HCM 2010 Ctrl Delay      |      |          | 142.5 |          |          |      |     |          |     |          |          |     |
|   | HCM 2010 LOS             |      |          | F     |          |          |      |     |          |     |          |          |     |

|                              |      | <b>→</b> | •    | <b>√</b> | <b>←</b> | •    | •    | †    | <i>&gt;</i> | <b>/</b> | ţ    | ✓    |
|------------------------------|------|----------|------|----------|----------|------|------|------|-------------|----------|------|------|
| Movement                     | EBL  | EBT      | EBR  | WBL      | WBT      | WBR  | NBL  | NBT  | NBR         | SBL      | SBT  | SBR  |
| Lane Configurations          | 7    | f)       |      | 7        | f)       |      |      | 4    |             |          | 4    |      |
| Traffic Volume (veh/h)       | 6    | 328      | 107  | 81       | 700      | 19   | 177  | 57   | 131         | 18       | 21   | 12   |
| Future Volume (veh/h)        | 6    | 328      | 107  | 81       | 700      | 19   | 177  | 57   | 131         | 18       | 21   | 12   |
| Number                       | 7    | 4        | 14   | 3        | 8        | 18   | 5    | 2    | 12          | 1        | 6    | 16   |
| Initial Q (Qb), veh          | 0    | 0        | 0    | 0        | 0        | 0    | 0    | 0    | 0           | 0        | 0    | 0    |
| Ped-Bike Adj(A_pbT)          | 1.00 |          | 1.00 | 1.00     |          | 1.00 | 1.00 |      | 1.00        | 1.00     |      | 1.00 |
| Parking Bus, Adj             | 1.00 | 1.00     | 1.00 | 1.00     | 1.00     | 1.00 | 1.00 | 1.00 | 1.00        | 1.00     | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln       | 1827 | 1827     | 1900 | 1845     | 1845     | 1900 | 1900 | 1810 | 1900        | 1900     | 1776 | 1900 |
| Adj Flow Rate, veh/h         | 7    | 373      | 122  | 92       | 795      | 22   | 201  | 65   | 149         | 20       | 24   | 14   |
| Adj No. of Lanes             | 1    | 1        | 0    | 1        | 1        | 0    | 0    | 1    | 0           | 0        | 1    | 0    |
| Peak Hour Factor             | 0.88 | 0.88     | 0.88 | 0.88     | 0.88     | 0.88 | 0.88 | 0.88 | 0.88        | 0.88     | 0.88 | 0.88 |
| Percent Heavy Veh, %         | 4    | 4        | 4    | 3        | 3        | 3    | 5    | 5    | 5           | 7        | 7    | 7    |
| Cap, veh/h                   | 16   | 524      | 171  | 118      | 813      | 22   | 299  | 86   | 166         | 200      | 223  | 109  |
| Arrive On Green              | 0.01 | 0.40     | 0.40 | 0.07     | 0.45     | 0.45 | 0.31 | 0.31 | 0.31        | 0.31     | 0.31 | 0.31 |
| Sat Flow, veh/h              | 1740 | 1319     | 432  | 1757     | 1786     | 49   | 674  | 274  | 531         | 382      | 713  | 349  |
| Grp Volume(v), veh/h         | 7    | 0        | 495  | 92       | 0        | 817  | 415  | 0    | 0           | 58       | 0    | 0    |
| Grp Sat Flow(s),veh/h/ln     | 1740 | 0        | 1751 | 1757     | 0        | 1836 | 1479 | 0    | 0           | 1444     | 0    | 0    |
| Q Serve(g_s), s              | 0.2  | 0.0      | 14.4 | 3.1      | 0.0      | 26.4 | 14.7 | 0.0  | 0.0         | 0.0      | 0.0  | 0.0  |
| Cycle Q Clear(g_c), s        | 0.2  | 0.0      | 14.4 | 3.1      | 0.0      | 26.4 | 16.1 | 0.0  | 0.0         | 1.5      | 0.0  | 0.0  |
| Prop In Lane                 | 1.00 |          | 0.25 | 1.00     |          | 0.03 | 0.48 |      | 0.36        | 0.34     |      | 0.24 |
| Lane Grp Cap(c), veh/h       | 16   | 0        | 695  | 118      | 0        | 835  | 551  | 0    | 0           | 532      | 0    | 0    |
| V/C Ratio(X)                 | 0.44 | 0.00     | 0.71 | 0.78     | 0.00     | 0.98 | 0.75 | 0.00 | 0.00        | 0.11     | 0.00 | 0.00 |
| Avail Cap(c_a), veh/h        | 147  | 0        | 744  | 201      | 0        | 835  | 551  | 0    | 0           | 532      | 0    | 0    |
| HCM Platoon Ratio            | 1.00 | 1.00     | 1.00 | 1.00     | 1.00     | 1.00 | 1.00 | 1.00 | 1.00        | 1.00     | 1.00 | 1.00 |
| Upstream Filter(I)           | 1.00 | 0.00     | 1.00 | 1.00     | 0.00     | 1.00 | 1.00 | 0.00 | 0.00        | 1.00     | 0.00 | 0.00 |
| Uniform Delay (d), s/veh     | 29.8 | 0.0      | 15.3 | 27.8     | 0.0      | 16.2 | 19.7 | 0.0  | 0.0         | 14.8     | 0.0  | 0.0  |
| Incr Delay (d2), s/veh       | 17.8 | 0.0      | 3.0  | 10.7     | 0.0      | 25.8 | 9.2  | 0.0  | 0.0         | 0.4      | 0.0  | 0.0  |
| Initial Q Delay(d3),s/veh    | 0.0  | 0.0      | 0.0  | 0.0      | 0.0      | 0.0  | 0.0  | 0.0  | 0.0         | 0.0      | 0.0  | 0.0  |
| %ile BackOfQ(50%),veh/ln     | 0.2  | 0.0      | 7.4  | 1.9      | 0.0      | 19.1 | 8.0  | 0.0  | 0.0         | 0.8      | 0.0  | 0.0  |
| LnGrp Delay(d),s/veh         | 47.6 | 0.0      | 18.3 | 38.5     | 0.0      | 42.0 | 28.9 | 0.0  | 0.0         | 15.2     | 0.0  | 0.0  |
| LnGrp LOS                    | D    |          | В    | D        |          | D    | С    |      |             | В        |      |      |
| Approach Vol, veh/h          |      | 502      |      |          | 909      |      |      | 415  |             |          | 58   |      |
| Approach Delay, s/veh        |      | 18.7     |      |          | 41.6     |      |      | 28.9 |             |          | 15.2 |      |
| Approach LOS                 |      | В        |      |          | D        |      |      | С    |             |          | В    |      |
| Timer                        | 1    | 2        | 3    | 4        | 5        | 6    | 7    | 8    |             |          |      |      |
| Assigned Phs                 |      | 2        | 3    | 4        |          | 6    | 7    | 8    |             |          |      |      |
| Phs Duration (G+Y+Rc), s     |      | 23.4     | 8.5  | 28.5     |          | 23.4 | 5.1  | 32.0 |             |          |      |      |
| Change Period (Y+Rc), s      |      | 4.5      | 4.5  | 4.5      |          | 4.5  | 4.5  | 4.5  |             |          |      |      |
| Max Green Setting (Gmax), s  |      | 18.9     | 6.9  | 25.7     |          | 18.9 | 5.1  | 27.5 |             |          |      |      |
| Max Q Clear Time (g_c+l1), s |      | 18.1     | 5.1  | 16.4     |          | 3.5  | 2.2  | 28.4 |             |          |      |      |
| Green Ext Time (p_c), s      |      | 0.2      | 0.0  | 2.2      |          | 0.2  | 0.0  | 0.0  |             |          |      |      |
| Intersection Summary         |      |          |      |          |          |      |      |      |             |          |      |      |
| HCM 2010 Ctrl Delay          |      |          | 31.9 |          |          |      |      |      |             |          |      |      |
| HCM 2010 LOS                 |      |          | С    |          |          |      |      |      |             |          |      |      |

|                              |      | <b>→</b> | <b>←</b> | •    | <u> </u>    | 4    |     |      |  |  |
|------------------------------|------|----------|----------|------|-------------|------|-----|------|--|--|
| Movement                     | EBL  | EBT      | WBT      | WBR  | SBL         | SBR  |     |      |  |  |
| Lane Configurations          | ሻ    | <b>1</b> | <b>^</b> | 7    | ኻ           | 7    |     |      |  |  |
| Traffic Volume (veh/h)       | 184  | 260      | 530      | 370  | 185         | 210  |     |      |  |  |
| Future Volume (veh/h)        | 184  | 260      | 530      | 370  | 185         | 210  |     |      |  |  |
| Number                       | 7    | 4        | 8        | 18   | 1           | 16   |     |      |  |  |
| Initial Q (Qb), veh          | 0    | 0        | 0        | 0    | 0           | 0    |     |      |  |  |
| Ped-Bike Adj(A_pbT)          | 1.00 |          |          | 1.00 | 1.00        | 1.00 |     |      |  |  |
| Parking Bus, Adj             | 1.00 | 1.00     | 1.00     | 1.00 | 1.00        | 1.00 |     |      |  |  |
| Adj Sat Flow, veh/h/ln       | 1810 | 1810     | 1863     | 1863 | 1863        | 1863 |     |      |  |  |
| Adj Flow Rate, veh/h         | 209  | 295      | 602      | 420  | 210         | 239  |     |      |  |  |
| Adj No. of Lanes             | 1    | 1        | 1        | 1    | 1           | 1    |     |      |  |  |
| Peak Hour Factor             | 0.88 | 0.88     | 0.88     | 0.88 | 0.88        | 0.88 |     |      |  |  |
| Percent Heavy Veh, %         | 5    | 5        | 2        | 2    | 2           | 2    |     |      |  |  |
| Cap, veh/h                   | 259  | 1078     | 680      | 578  | 430         | 384  |     |      |  |  |
| Arrive On Green              | 0.15 | 0.60     | 0.36     | 0.36 | 0.24        | 0.24 |     |      |  |  |
| Sat Flow, veh/h              | 1723 | 1810     | 1863     | 1583 | 1774        | 1583 |     |      |  |  |
| Grp Volume(v), veh/h         | 209  | 295      | 602      | 420  | 210         | 239  |     |      |  |  |
|                              | 1723 | 1810     | 1863     | 1583 | 1774        | 1583 |     |      |  |  |
| Grp Sat Flow(s),veh/h/ln     | 6.5  | 4.4      | 16.9     | 12.8 | 5.7         | 7.5  |     |      |  |  |
| Q Serve(g_s), s              |      |          |          |      |             | 7.5  |     |      |  |  |
| Cycle Q Clear(g_c), s        | 6.5  | 4.4      | 16.9     | 12.8 | 5.7         | 1.00 |     |      |  |  |
| Prop In Lane                 | 1.00 | 1070     | 600      | 1.00 | 1.00<br>430 | 384  |     |      |  |  |
| Lane Grp Cap(c), veh/h       | 259  | 1078     | 680      | 578  |             |      |     |      |  |  |
| V/C Ratio(X)                 | 0.81 | 0.27     | 0.89     | 0.73 | 0.49        | 0.62 |     |      |  |  |
| Avail Cap(c_a), veh/h        | 356  | 1219     | 719      | 611  | 430         | 384  |     |      |  |  |
| HCM Platoon Ratio            | 1.00 | 1.00     | 1.00     | 1.00 | 1.00        | 1.00 |     |      |  |  |
| Upstream Filter(I)           | 1.00 | 1.00     | 1.00     | 1.00 | 1.00        | 1.00 |     |      |  |  |
| Uniform Delay (d), s/veh     | 22.9 | 5.4      | 16.6     | 15.3 | 18.1        | 18.8 |     |      |  |  |
| Incr Delay (d2), s/veh       | 9.3  | 0.1      | 12.3     | 4.1  | 3.9         | 7.4  |     |      |  |  |
| Initial Q Delay(d3),s/veh    | 0.0  | 0.0      | 0.0      | 0.0  | 0.0         | 0.0  |     |      |  |  |
| %ile BackOfQ(50%),veh/ln     | 3.7  | 2.2      | 10.9     | 6.1  | 3.2         | 7.2  |     |      |  |  |
| LnGrp Delay(d),s/veh         | 32.2 | 5.6      | 28.9     | 19.4 | 22.0        | 26.2 |     |      |  |  |
| LnGrp LOS                    | С    | A        | С        | В    | С           | С    |     |      |  |  |
| Approach Vol, veh/h          |      | 504      | 1022     |      | 449         |      |     |      |  |  |
| Approach Delay, s/veh        |      | 16.6     | 25.0     |      | 24.3        |      |     |      |  |  |
| Approach LOS                 |      | В        | С        |      | С           |      |     |      |  |  |
| Timer                        | 1    | 2        | 3        | 4    | 5           | 6    | 7   | 8    |  |  |
| Assigned Phs                 |      |          |          | 4    |             | 6    | 7   | 8    |  |  |
| Phs Duration (G+Y+Rc), s     |      |          |          | 37.7 |             | 18.0 |     | 24.8 |  |  |
| Change Period (Y+Rc), s      |      |          |          | 4.5  |             | 4.5  | 4.5 | 4.5  |  |  |
| Max Green Setting (Gmax), s  |      |          |          | 37.5 |             | 13.5 |     | 21.5 |  |  |
| Max Q Clear Time (g_c+I1), s |      |          |          | 6.4  |             | 9.5  | 8.5 | 18.9 |  |  |
| Green Ext Time (p_c), s      |      |          |          | 1.9  |             | 0.6  | 0.2 | 1.4  |  |  |
| ntersection Summary          |      |          |          |      |             |      |     |      |  |  |
| HCM 2010 Ctrl Delay          |      |          | 22.7     |      |             |      |     |      |  |  |
| HCM 2010 LOS                 |      |          | С        |      |             |      |     |      |  |  |

|                               | ۶          | <b>→</b> | •      | •     | <b>—</b>    | •          | •       | <b>†</b> | /    | <b>/</b> | ţ     | 4    |
|-------------------------------|------------|----------|--------|-------|-------------|------------|---------|----------|------|----------|-------|------|
| Movement                      | EBL        | EBT      | EBR    | WBL   | WBT         | WBR        | NBL     | NBT      | NBR  | SBL      | SBT   | SBR  |
| Lane Configurations           | ň          | <b>†</b> | 7      | Ţ     | f)          |            |         | ર્ન      | 7    |          | ર્ન   | 7    |
| Traffic Volume (vph)          | 11         | 537      | 377    | 67    | 767         | 28         | 746     | 25       | 64   | 46       | 23    | 5    |
| Future Volume (vph)           | 11         | 537      | 377    | 67    | 767         | 28         | 746     | 25       | 64   | 46       | 23    | 5    |
| Ideal Flow (vphpl)            | 1900       | 1900     | 1900   | 1900  | 1900        | 1900       | 1900    | 1900     | 1900 | 1900     | 1900  | 1900 |
| Total Lost time (s)           | 4.5        | 4.5      | 4.5    | 4.5   | 4.5         |            |         | 4.5      | 4.5  |          | 4.5   | 4.5  |
| Lane Util. Factor             | 1.00       | 1.00     | 1.00   | 1.00  | 1.00        |            |         | 1.00     | 1.00 |          | 1.00  | 1.00 |
| Frt                           | 1.00       | 1.00     | 0.85   | 1.00  | 0.99        |            |         | 1.00     | 0.85 |          | 1.00  | 0.85 |
| Flt Protected                 | 0.95       | 1.00     | 1.00   | 0.95  | 1.00        |            |         | 0.95     | 1.00 |          | 0.97  | 1.00 |
| Satd. Flow (prot)             | 1612       | 1696     | 1442   | 1543  | 1615        |            |         | 1777     | 1583 |          | 1751  | 1538 |
| Flt Permitted                 | 0.95       | 1.00     | 1.00   | 0.95  | 1.00        |            |         | 0.95     | 1.00 |          | 0.97  | 1.00 |
| Satd. Flow (perm)             | 1612       | 1696     | 1442   | 1543  | 1615        |            |         | 1777     | 1583 |          | 1751  | 1538 |
| Peak-hour factor, PHF         | 0.96       | 0.96     | 0.96   | 0.96  | 0.96        | 0.96       | 0.96    | 0.96     | 0.96 | 0.96     | 0.96  | 0.96 |
| Adj. Flow (vph)               | 11         | 559      | 393    | 70    | 799         | 29         | 777     | 26       | 67   | 48       | 24    | 5    |
| RTOR Reduction (vph)          | 0          | 0        | 216    | 0     | 1           | 0          | 0       | 0        | 46   | 0        | 0     | 5    |
| Lane Group Flow (vph)         | 11         | 559      | 177    | 70    | 827         | 0          | 0       | 803      | 21   | 0        | 72    | 0    |
| Heavy Vehicles (%)            | 12%        | 12%      | 12%    | 17%   | 17%         | 17%        | 2%      | 2%       | 2%   | 5%       | 5%    | 5%   |
| Turn Type                     | Prot       | NA       | Perm   | Prot  | NA          |            | Split   | NA       | Perm | Split    | NA    | Perm |
| Protected Phases              | 7          | 4        |        | 3     | 8           |            | 5       | 5        |      | 6        | 6     |      |
| Permitted Phases              |            |          | 4      |       |             |            |         |          | 5    |          |       | 6    |
| Actuated Green, G (s)         | 1.0        | 55.2     | 55.2   | 5.0   | 59.2        |            |         | 38.6     | 38.6 |          | 5.5   | 5.5  |
| Effective Green, g (s)        | 1.0        | 55.2     | 55.2   | 5.0   | 59.2        |            |         | 38.6     | 38.6 |          | 5.5   | 5.5  |
| Actuated g/C Ratio            | 0.01       | 0.45     | 0.45   | 0.04  | 0.48        |            |         | 0.32     | 0.32 |          | 0.04  | 0.04 |
| Clearance Time (s)            | 4.5        | 4.5      | 4.5    | 4.5   | 4.5         |            |         | 4.5      | 4.5  |          | 4.5   | 4.5  |
| Vehicle Extension (s)         | 3.0        | 3.0      | 3.0    | 3.0   | 3.0         |            |         | 3.0      | 3.0  |          | 3.0   | 3.0  |
| Lane Grp Cap (vph)            | 13         | 765      | 650    | 63    | 781         |            |         | 560      | 499  |          | 78    | 69   |
| v/s Ratio Prot                | 0.01       | 0.33     |        | c0.05 | c0.51       |            |         | c0.45    |      |          | c0.04 |      |
| v/s Ratio Perm                |            |          | 0.12   |       |             |            |         |          | 0.01 |          |       | 0.00 |
| v/c Ratio                     | 0.85       | 0.73     | 0.27   | 1.11  | 1.06        |            |         | 1.43     | 0.04 |          | 0.92  | 0.00 |
| Uniform Delay, d1             | 60.6       | 27.5     | 21.0   | 58.6  | 31.5        |            |         | 41.8     | 29.0 |          | 58.2  | 55.8 |
| Progression Factor            | 1.00       | 1.00     | 1.00   | 1.00  | 1.00        |            |         | 1.00     | 1.00 |          | 1.00  | 1.00 |
| Incremental Delay, d2         | 166.4      | 6.1      | 1.0    | 147.1 | 48.9        |            |         | 205.4    | 0.0  |          | 75.7  | 0.0  |
| Delay (s)                     | 227.0      | 33.5     | 22.0   | 205.8 | 80.5        |            |         | 247.2    | 29.1 |          | 133.9 | 55.8 |
| Level of Service              | F          | С        | С      | F     | F           |            |         | F        | С    |          | F     | Е    |
| Approach Delay (s)            |            | 31.1     |        |       | 90.2        |            |         | 230.4    |      |          | 128.9 |      |
| Approach LOS                  |            | С        |        |       | F           |            |         | F        |      |          | F     |      |
| Intersection Summary          |            |          |        |       |             |            |         |          |      |          |       |      |
| HCM 2000 Control Delay        |            |          | 114.4  | Н     | CM 2000     | Level of S | Service |          | F    |          |       |      |
| HCM 2000 Volume to Capa       | city ratio |          | 1.21   |       |             |            |         |          |      |          |       |      |
| Actuated Cycle Length (s)     |            |          | 122.3  |       | um of lost  |            |         |          | 18.0 |          |       |      |
| Intersection Capacity Utiliza | ition      |          | 106.8% | IC    | CU Level of | of Service |         |          | G    |          |       |      |
| Analysis Period (min)         |            |          | 15     |       |             |            |         |          |      |          |       |      |
| c Critical Lane Group         |            |          |        |       |             |            |         |          |      |          |       |      |

## 8: Airline Hwy (SR 25)/Pinnacles Nat Pk Hwy (SR 25) & Tres Pinos Rd/Sunnslope Rd

|                              | ۶    | <b>→</b> | •    | •     | <b>←</b> | •    | 1    | <b>†</b>    | ~    | <b>/</b> | Ţ        | ✓    |
|------------------------------|------|----------|------|-------|----------|------|------|-------------|------|----------|----------|------|
| Movement                     | EBL  | EBT      | EBR  | WBL   | WBT      | WBR  | NBL  | NBT         | NBR  | SBL      | SBT      | SBR  |
| Lane Configurations          | 1,1  | <b>^</b> | 7    | ሻ     | <b>^</b> | 7    | ሻሻ   | <b>↑</b> ↑₽ |      | ሻሻ       | <b>^</b> | 7    |
| Traffic Volume (veh/h)       | 256  | 256      | 125  | 149   | 469      | 364  | 193  | 807         | 66   | 238      | 520      | 192  |
| Future Volume (veh/h)        | 256  | 256      | 125  | 149   | 469      | 364  | 193  | 807         | 66   | 238      | 520      | 192  |
| Number                       | 7    | 4        | 14   | 3     | 8        | 18   | 5    | 2           | 12   | 1        | 6        | 16   |
| Initial Q (Qb), veh          | 0    | 0        | 0    | 0     | 0        | 0    | 0    | 0           | 0    | 0        | 0        | 0    |
| Ped-Bike Adj(A_pbT)          | 1.00 |          | 0.98 | 1.00  |          | 0.97 | 1.00 |             | 1.00 | 1.00     |          | 1.00 |
| Parking Bus, Adj             | 1.00 | 1.00     | 1.00 | 1.00  | 1.00     | 1.00 | 1.00 | 1.00        | 1.00 | 1.00     | 1.00     | 1.00 |
| Adj Sat Flow, veh/h/ln       | 1863 | 1863     | 1863 | 1863  | 1863     | 1863 | 1863 | 1863        | 1900 | 1845     | 1845     | 1845 |
| Adj Flow Rate, veh/h         | 281  | 281      | 137  | 164   | 515      | 400  | 212  | 887         | 73   | 262      | 571      | 211  |
| Adj No. of Lanes             | 2    | 2        | 1    | 1     | 2        | 1    | 2    | 3           | 0    | 2        | 3        | 1    |
| Peak Hour Factor             | 0.91 | 0.91     | 0.91 | 0.91  | 0.91     | 0.91 | 0.91 | 0.91        | 0.91 | 0.91     | 0.91     | 0.91 |
| Percent Heavy Veh, %         | 2    | 2        | 2    | 2     | 2        | 2    | 2    | 2           | 2    | 3        | 3        | 3    |
| Cap, veh/h                   | 286  | 980      | 554  | 150   | 986      | 428  | 265  | 1363        | 112  | 262      | 1433     | 575  |
| Arrive On Green              | 0.08 | 0.28     | 0.28 | 0.08  | 0.28     | 0.28 | 0.08 | 0.28        | 0.28 | 0.08     | 0.28     | 0.28 |
| Sat Flow, veh/h              | 3442 | 3539     | 1559 | 1774  | 3539     | 1536 | 3442 | 4790        | 393  | 3408     | 5036     | 1561 |
| Grp Volume(v), veh/h         | 281  | 281      | 137  | 164   | 515      | 400  | 212  | 627         | 333  | 262      | 571      | 211  |
| Grp Sat Flow(s),veh/h/ln     | 1721 | 1770     | 1559 | 1774  | 1770     | 1536 | 1721 | 1695        | 1792 | 1704     | 1679     | 1561 |
| Q Serve(g_s), s              | 5.3  | 4.1      | 4.0  | 5.5   | 8.0      | 16.5 | 3.9  | 10.6        | 10.6 | 5.0      | 5.9      | 6.4  |
| Cycle Q Clear(g_c), s        | 5.3  | 4.1      | 4.0  | 5.5   | 8.0      | 16.5 | 3.9  | 10.6        | 10.6 | 5.0      | 5.9      | 6.4  |
| Prop In Lane                 | 1.00 |          | 1.00 | 1.00  |          | 1.00 | 1.00 |             | 0.22 | 1.00     |          | 1.00 |
| Lane Grp Cap(c), veh/h       | 286  | 980      | 554  | 150   | 986      | 428  | 265  | 965         | 510  | 262      | 1433     | 575  |
| V/C Ratio(X)                 | 0.98 | 0.29     | 0.25 | 1.09  | 0.52     | 0.94 | 0.80 | 0.65        | 0.65 | 1.00     | 0.40     | 0.37 |
| Avail Cap(c_a), veh/h        | 286  | 980      | 554  | 150   | 986      | 428  | 265  | 965         | 510  | 262      | 1433     | 575  |
| HCM Platoon Ratio            | 1.00 | 1.00     | 1.00 | 1.00  | 1.00     | 1.00 | 1.00 | 1.00        | 1.00 | 1.00     | 1.00     | 1.00 |
| Upstream Filter(I)           | 1.00 | 1.00     | 1.00 | 1.00  | 1.00     | 1.00 | 1.00 | 1.00        | 1.00 | 1.00     | 1.00     | 1.00 |
| Uniform Delay (d), s/veh     | 29.8 | 18.5     | 14.9 | 29.7  | 19.8     | 22.9 | 29.5 | 20.4        | 20.4 | 30.0     | 18.8     | 15.0 |
| Incr Delay (d2), s/veh       | 48.3 | 0.2      | 0.2  | 100.4 | 0.5      | 27.9 | 16.0 | 3.4         | 6.4  | 55.4     | 8.0      | 1.8  |
| Initial Q Delay(d3),s/veh    | 0.0  | 0.0      | 0.0  | 0.0   | 0.0      | 0.0  | 0.0  | 0.0         | 0.0  | 0.0      | 0.0      | 0.0  |
| %ile BackOfQ(50%),veh/ln     | 4.4  | 2.0      | 1.7  | 6.9   | 3.9      | 10.3 | 2.4  | 5.3         | 6.1  | 4.3      | 2.9      | 3.0  |
| LnGrp Delay(d),s/veh         | 78.1 | 18.6     | 15.1 | 130.1 | 20.3     | 50.8 | 45.5 | 23.8        | 26.8 | 85.4     | 19.6     | 16.8 |
| LnGrp LOS                    | Ε    | В        | В    | F     | С        | D    | D    | С           | С    | F        | В        | В    |
| Approach Vol, veh/h          |      | 699      |      |       | 1079     |      |      | 1172        |      |          | 1044     |      |
| Approach Delay, s/veh        |      | 41.8     |      |       | 48.3     |      |      | 28.6        |      |          | 35.5     |      |
| Approach LOS                 |      | D        |      |       | D        |      |      | С           |      |          | D        |      |
| Timer                        | 1    | 2        | 3    | 4     | 5        | 6    | 7    | 8           |      |          |          |      |
| Assigned Phs                 | 1    | 2        | 3    | 4     | 5        | 6    | 7    | 8           |      |          |          |      |
| Phs Duration (G+Y+Rc), s     | 9.5  | 23.0     | 10.0 | 22.5  | 9.5      | 23.0 | 9.9  | 22.6        |      |          |          |      |
| Change Period (Y+Rc), s      | 4.5  | 4.5      | 4.5  | 4.5   | 4.5      | 4.5  | 4.5  | 4.5         |      |          |          |      |
| Max Green Setting (Gmax), s  | 5.0  | 18.5     | 5.5  | 18.0  | 5.0      | 18.5 | 5.4  | 18.1        |      |          |          |      |
| Max Q Clear Time (g_c+l1), s | 7.0  | 12.6     | 7.5  | 6.1   | 5.9      | 8.4  | 7.3  | 18.5        |      |          |          |      |
| Green Ext Time (p_c), s      | 0.0  | 3.0      | 0.0  | 1.8   | 0.0      | 3.3  | 0.0  | 0.0         |      |          |          |      |
| Intersection Summary         |      |          |      |       |          |      |      |             |      |          |          |      |
| HCM 2010 Ctrl Delay          |      |          | 38.0 |       |          |      |      |             |      |          |          |      |
| HCM 2010 LOS                 |      |          | D    |       |          |      |      |             |      |          |          |      |
|                              |      |          |      |       |          |      |      |             |      |          |          |      |

|                              | ۶    | <b>→</b> | •    | <b>√</b> | <b>←</b> | •    | •    | <b>†</b> | ~    | <b>/</b> | ļ    | ✓        |
|------------------------------|------|----------|------|----------|----------|------|------|----------|------|----------|------|----------|
| Movement                     | EBL  | EBT      | EBR  | WBL      | WBT      | WBR  | NBL  | NBT      | NBR  | SBL      | SBT  | SBR      |
| Lane Configurations          | 7    | f)       |      | *        | f)       |      | Ĭ    | <b>†</b> | 7    | 7        | f)   |          |
| Traffic Volume (veh/h)       | 38   | 153      | 41   | 158      | 156      | 263  | 72   | 179      | 179  | 144      | 89   | 14       |
| Future Volume (veh/h)        | 38   | 153      | 41   | 158      | 156      | 263  | 72   | 179      | 179  | 144      | 89   | 14       |
| Number                       | 7    | 4        | 14   | 3        | 8        | 18   | 5    | 2        | 12   | 1        | 6    | 16       |
| Initial Q (Qb), veh          | 0    | 0        | 0    | 0        | 0        | 0    | 0    | 0        | 0    | 0        | 0    | 0        |
| Ped-Bike Adj(A_pbT)          | 1.00 |          | 0.74 | 1.00     |          | 0.89 | 1.00 |          | 0.99 | 1.00     |      | 0.99     |
| Parking Bus, Adj             | 1.00 | 1.00     | 1.00 | 1.00     | 1.00     | 1.00 | 1.00 | 1.00     | 1.00 | 1.00     | 1.00 | 1.00     |
| Adj Sat Flow, veh/h/ln       | 1863 | 1863     | 1900 | 1863     | 1863     | 1900 | 1863 | 1863     | 1863 | 1863     | 1863 | 1900     |
| Adj Flow Rate, veh/h         | 50   | 201      | 54   | 208      | 205      | 346  | 95   | 236      | 236  | 189      | 117  | 18       |
| Adj No. of Lanes             | 1    | 1        | 0    | 1        | 1        | 0    | 1    | 1        | 1    | 1        | 1    | 0        |
| Peak Hour Factor             | 0.76 | 0.76     | 0.76 | 0.76     | 0.76     | 0.76 | 0.76 | 0.76     | 0.76 | 0.76     | 0.76 | 0.76     |
| Percent Heavy Veh, %         | 2    | 2        | 2    | 2        | 2        | 2    | 2    | 2        | 2    | 2        | 2    | 2        |
| Cap, veh/h                   | 79   | 325      | 87   | 236      | 194      | 327  | 122  | 492      | 416  | 166      | 456  | 70       |
| Arrive On Green              | 0.04 | 0.25     | 0.25 | 0.13     | 0.34     | 0.34 | 0.07 | 0.26     | 0.26 | 0.09     | 0.29 | 0.29     |
| Sat Flow, veh/h              | 1774 | 1303     | 350  | 1774     | 575      | 970  | 1774 | 1863     | 1574 | 1774     | 1574 | 242      |
| Grp Volume(v), veh/h         | 50   | 0        | 255  | 208      | 0        | 551  | 95   | 236      | 236  | 189      | 0    | 135      |
| Grp Sat Flow(s),veh/h/ln     | 1774 | 0        | 1653 | 1774     | 0        | 1545 | 1774 | 1863     | 1574 | 1774     | 0    | 1817     |
| Q Serve(g_s), s              | 1.9  | 0.0      | 9.5  | 8.0      | 0.0      | 23.4 | 3.7  | 7.4      | 9.0  | 6.5      | 0.0  | 4.0      |
| Cycle Q Clear(g_c), s        | 1.9  | 0.0      | 9.5  | 8.0      | 0.0      | 23.4 | 3.7  | 7.4      | 9.0  | 6.5      | 0.0  | 4.0      |
| Prop In Lane                 | 1.00 |          | 0.21 | 1.00     |          | 0.63 | 1.00 |          | 1.00 | 1.00     |      | 0.13     |
| Lane Grp Cap(c), veh/h       | 79   | 0        | 412  | 236      | 0        | 521  | 122  | 492      | 416  | 166      | 0    | 526      |
| V/C Ratio(X)                 | 0.63 | 0.00     | 0.62 | 0.88     | 0.00     | 1.06 | 0.78 | 0.48     | 0.57 | 1.14     | 0.00 | 0.26     |
| Avail Cap(c_a), veh/h        | 131  | 0        | 429  | 236      | 0        | 521  | 159  | 492      | 416  | 166      | 0    | 526      |
| HCM Platoon Ratio            | 1.00 | 1.00     | 1.00 | 1.00     | 1.00     | 1.00 | 1.00 | 1.00     | 1.00 | 1.00     | 1.00 | 1.00     |
| Upstream Filter(I)           | 1.00 | 0.00     | 1.00 | 1.00     | 0.00     | 1.00 | 1.00 | 1.00     | 1.00 | 1.00     | 0.00 | 1.00     |
| Uniform Delay (d), s/veh     | 32.5 | 0.0      | 23.1 | 29.5     | 0.0      | 22.9 | 31.7 | 21.5     | 22.1 | 31.4     | 0.0  | 18.9     |
| Incr Delay (d2), s/veh       | 8.0  | 0.0      | 2.5  | 29.9     | 0.0      | 55.4 | 16.7 | 3.3      | 5.5  | 110.7    | 0.0  | 1.2      |
| Initial Q Delay(d3),s/veh    | 0.0  | 0.0      | 0.0  | 0.0      | 0.0      | 0.0  | 0.0  | 0.0      | 0.0  | 0.0      | 0.0  | 0.0      |
| %ile BackOfQ(50%),veh/ln     | 1.1  | 0.0      | 4.6  | 5.8      | 0.0      | 17.9 | 2.4  | 4.3      | 4.5  | 8.3      | 0.0  | 2.2      |
| LnGrp Delay(d),s/veh         | 40.6 | 0.0      | 25.6 | 59.4     | 0.0      | 78.3 | 48.4 | 24.8     | 27.6 | 142.1    | 0.0  | 20.1     |
| LnGrp LOS                    | D    |          | С    | E        |          | F    | D    | С        | С    | F        |      | <u>C</u> |
| Approach Vol, veh/h          |      | 305      |      |          | 759      |      |      | 567      |      |          | 324  |          |
| Approach Delay, s/veh        |      | 28.1     |      |          | 73.1     |      |      | 29.9     |      |          | 91.3 |          |
| Approach LOS                 |      | С        |      |          | E        |      |      | С        |      |          | F    |          |
| Timer                        | 1    | 2        | 3    | 4        | 5        | 6    | 7    | 8        |      |          |      |          |
| Assigned Phs                 | 1    | 2        | 3    | 4        | 5        | 6    | 7    | 8        |      |          |      |          |
| Phs Duration (G+Y+Rc), s     | 11.0 | 22.8     | 13.7 | 21.8     | 9.3      | 24.5 | 7.6  | 27.9     |      |          |      |          |
| Change Period (Y+Rc), s      | 4.5  | 4.5      | 4.5  | 4.5      | 4.5      | 4.5  | 4.5  | 4.5      |      |          |      |          |
| Max Green Setting (Gmax), s  | 6.5  | 18.3     | 9.2  | 18.0     | 6.2      | 18.6 | 5.1  | 22.1     |      |          |      |          |
| Max Q Clear Time (g_c+l1), s | 8.5  | 11.0     | 10.0 | 11.5     | 5.7      | 6.0  | 3.9  | 25.4     |      |          |      |          |
| Green Ext Time (p_c), s      | 0.0  | 1.3      | 0.0  | 0.8      | 0.0      | 0.5  | 0.0  | 0.0      |      |          |      |          |
| Intersection Summary         |      |          |      |          |          |      |      |          |      |          |      |          |
| HCM 2010 Ctrl Delay          |      |          | 56.6 |          |          |      |      |          |      |          |      |          |
| HCM 2010 LOS                 |      |          | Е    |          |          |      |      |          |      |          |      |          |

| Intersection               |      |         |       |       |         |       |       |       |       |       |         |       |
|----------------------------|------|---------|-------|-------|---------|-------|-------|-------|-------|-------|---------|-------|
| Intersection Delay, s/veh  | 13.9 |         |       |       |         |       |       |       |       |       |         |       |
| Intersection LOS           | В    |         |       |       |         |       |       |       |       |       |         |       |
|                            |      |         |       |       |         |       |       |       |       |       |         |       |
| Movement                   | EBL  | EBT     | EBR   | WBL   | WBT     | WBR   | NBL   | NBT   | NBR   | SBL   | SBT     | SBR   |
| Lane Configurations        | 7    | <u></u> | 7     | 7     | <u></u> | 7     | ሻ     | 4Î    |       | *     | <u></u> | 7     |
| Traffic Vol, veh/h         | 114  | 204     | 254   | 4     | 157     | 76    | 129   | 36    | 2     | 91    | 86      | 133   |
| Future Vol, veh/h          | 114  | 204     | 254   | 4     | 157     | 76    | 129   | 36    | 2     | 91    | 86      | 133   |
| Peak Hour Factor           | 0.97 | 0.97    | 0.97  | 0.97  | 0.97    | 0.97  | 0.97  | 0.97  | 0.97  | 0.97  | 0.97    | 0.97  |
| Heavy Vehicles, %          | 2    | 2       | 2     | 2     | 2       | 2     | 2     | 2     | 2     | 2     | 2       | 2     |
| Mvmt Flow                  | 118  | 210     | 262   | 4     | 162     | 78    | 133   | 37    | 2     | 94    | 89      | 137   |
| Number of Lanes            | 1    | 1       | 1     | 1     | 1       | 1     | 1     | 1     | 0     | 1     | 1       | 1     |
| Approach                   | EB   |         |       | WB    |         |       | NB    |       |       | SB    |         |       |
| Opposing Approach          | WB   |         |       | EB    |         |       | SB    |       |       | NB    |         |       |
| Opposing Lanes             | 3    |         |       | 3     |         |       | 3     |       |       | 2     |         |       |
| Conflicting Approach Left  | SB   |         |       | NB    |         |       | EB    |       |       | WB    |         |       |
| Conflicting Lanes Left     | 3    |         |       | 2     |         |       | 3     |       |       | 3     |         |       |
| Conflicting Approach Right | NB   |         |       | SB    |         |       | WB    |       |       | EB    |         |       |
| Conflicting Lanes Right    | 2    |         |       | 3     |         |       | 3     |       |       | 3     |         |       |
| HCM Control Delay          | 14.5 |         |       | 13.7  |         |       | 14.2  |       |       | 12.6  |         |       |
| HCM LOS                    | В    |         |       | В     |         |       | В     |       |       | В     |         |       |
|                            |      |         |       |       |         |       |       |       |       |       |         |       |
| Lane                       |      | NBLn1   | NBLn2 | EBLn1 | EBLn2   | EBLn3 | WBLn1 | WBLn2 | WBLn3 | SBLn1 | SBLn2   | SBLn3 |
| Vol Left, %                |      | 100%    | 0%    | 100%  | 0%      | 0%    | 100%  | 0%    | 0%    | 100%  | 0%      | 0%    |
| Vol Thru %                 |      | 0%      | 95%   | 0%    | 100%    | 0%    | 0%    | 100%  | 0%    | 0%    | 100%    | 0%    |

| Lane                   | NBLn1 | NBLn2 | EBLn1 | EBLn2 | EBLn3 | WBLn1 | WBLn2 | WBLn3 | SBLn1 | SBLn2 | SBLn3 |
|------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Vol Left, %            | 100%  | 0%    | 100%  | 0%    | 0%    | 100%  | 0%    | 0%    | 100%  | 0%    | 0%    |
| Vol Thru, %            | 0%    | 95%   | 0%    | 100%  | 0%    | 0%    | 100%  | 0%    | 0%    | 100%  | 0%    |
| Vol Right, %           | 0%    | 5%    | 0%    | 0%    | 100%  | 0%    | 0%    | 100%  | 0%    | 0%    | 100%  |
| Sign Control           | Stop  |
| Traffic Vol by Lane    | 129   | 38    | 114   | 204   | 254   | 4     | 157   | 76    | 91    | 86    | 133   |
| LT Vol                 | 129   | 0     | 114   | 0     | 0     | 4     | 0     | 0     | 91    | 0     | 0     |
| Through Vol            | 0     | 36    | 0     | 204   | 0     | 0     | 157   | 0     | 0     | 86    | 0     |
| RT Vol                 | 0     | 2     | 0     | 0     | 254   | 0     | 0     | 76    | 0     | 0     | 133   |
| Lane Flow Rate         | 133   | 39    | 118   | 210   | 262   | 4     | 162   | 78    | 94    | 89    | 137   |
| Geometry Grp           | 8     | 8     | 8     | 8     | 8     | 8     | 8     | 8     | 8     | 8     | 8     |
| Degree of Util (X)     | 0.311 | 0.086 | 0.25  | 0.418 | 0.469 | 0.01  | 0.354 | 0.156 | 0.214 | 0.19  | 0.267 |
| Departure Headway (Hd) | 8.429 | 7.892 | 7.656 | 7.15  | 6.441 | 8.381 | 7.872 | 7.161 | 8.221 | 7.718 | 7.012 |
| Convergence, Y/N       | Yes   |
| Сар                    | 426   | 453   | 469   | 503   | 558   | 427   | 456   | 500   | 436   | 465   | 511   |
| Service Time           | 6.188 | 5.651 | 5.404 | 4.898 | 4.188 | 6.138 | 5.63  | 4.918 | 5.977 | 5.473 | 4.768 |
| HCM Lane V/C Ratio     | 0.312 | 0.086 | 0.252 | 0.417 | 0.47  | 0.009 | 0.355 | 0.156 | 0.216 | 0.191 | 0.268 |
| HCM Control Delay      | 15    | 11.4  | 13    | 15    | 14.8  | 11.2  | 14.9  | 11.2  | 13.2  | 12.3  | 12.3  |
| HCM Lane LOS           | В     | В     | В     | В     | В     | В     | В     | В     | В     | В     | В     |
| HCM 95th-tile Q        | 1.3   | 0.3   | 1     | 2     | 2.5   | 0     | 1.6   | 0.5   | 8.0   | 0.7   | 1.1   |
|                        |       |       |       |       |       |       |       |       |       |       |       |

| Intersection           |        |                  |        |        |                  |      |           |          |       |           |          |       |      |
|------------------------|--------|------------------|--------|--------|------------------|------|-----------|----------|-------|-----------|----------|-------|------|
| Int Delay, s/veh       | 5.1    |                  |        |        |                  |      |           |          |       |           |          |       |      |
| Movement               | EBL    | EBT              | EBR    | WBL    | WBT              | WBR  | NBL       | NBT      | NBR   | SBL       | SBT      | SBR   |      |
| Lane Configurations    | ች      | <b>†</b>         | 7      | ሻ      | <b></b>          | 7    | ች         | <b>†</b> | 7     | 1         | <b>↑</b> | 7     |      |
| Traffic Vol., veh/h    | 168    | 513              | 61     | 55     | 331              | 39   | 28        | 2        | 38    | 21        | 2        | 96    |      |
| Future Vol, veh/h      | 168    | 513              | 61     | 55     | 331              | 39   | 28        | 2        | 38    | 21        | 2        | 96    |      |
| Conflicting Peds, #/hr | 0      | 0                | 0      | 0      | 0                | 0    | 0         | 0        | 0     | 0         | 0        | 0     |      |
| Sign Control           | Free   | Free             | Free   | Free   | Free             | Free | Stop      | Stop     | Stop  | Stop      | Stop     | Stop  |      |
| RT Channelized         | -      | -                | None   | -      | -                | None | -         | - Olop   |       | - Olop    | - Clop   | None  |      |
| Storage Length         | 320    | _                | 505    | 360    | _                | 195  | 60        | _        | 0     | 100       | _        | 100   |      |
| Veh in Median Storage  |        | 0                | -      | -      | 0                | -    | -         | 0        | -     | -         | 0        | -     |      |
| Grade, %               | , π -  | 0                | _      | _      | 0                | _    | _         | 0        | _     | _         | 0        | _     |      |
| Peak Hour Factor       | 95     | 95               | 95     | 95     | 95               | 95   | 95        | 95       | 95    | 95        | 95       | 95    |      |
| Heavy Vehicles, %      | 2      | 2                | 2      | 2      | 2                | 2    | 2         | 2        | 2     | 2         | 2        | 2     |      |
| Mvmt Flow              | 177    | 540              | 64     | 58     | 348              | 41   | 29        | 2        | 40    | 22        | 2        | 101   |      |
| IVIVIIILI IOW          | 177    | J <del>4</del> 0 | 04     | 50     | J <del>4</del> 0 | 41   | 23        |          | 40    | 22        |          | 101   |      |
|                        |        |                  |        |        |                  |      |           |          |       |           |          |       |      |
| Major/Minor N          | Major1 |                  |        | Major2 |                  |      | Minor1    |          |       | Minor2    |          |       |      |
| Conflicting Flow All   | 389    | 0                | 0      | 604    | 0                | 0    | 1430      | 1399     | 540   | 1411      | 1422     | 348   |      |
| Stage 1                | -      | -                | -      | -      | -                | -    | 894       | 894      | -     | 464       | 464      | -     |      |
| Stage 2                | -      | -                | -      | -      | -                | -    | 536       | 505      | -     | 947       | 958      | -     |      |
| Critical Hdwy          | 4.12   | -                | -      | 4.12   | -                | -    | 7.12      | 6.52     | 6.22  | 7.12      | 6.52     | 6.22  |      |
| Critical Hdwy Stg 1    | -      | -                | -      | -      | -                | -    | 6.12      | 5.52     | -     | 6.12      | 5.52     | -     |      |
| Critical Hdwy Stg 2    | -      | -                | -      | -      | -                | -    | 6.12      | 5.52     | -     | 6.12      | 5.52     | -     |      |
| Follow-up Hdwy         | 2.218  | -                | -      | 2.218  | -                | -    | 3.518     | 4.018    | 3.318 | 3.518     | 4.018    | 3.318 |      |
| Pot Cap-1 Maneuver     | 1170   | -                | -      | 974    | -                | -    | 112       | 141      | 542   | 116       | 136      | 695   |      |
| Stage 1                | -      | -                | -      | -      | -                | -    | 336       | 360      | -     | 578       | 564      | -     |      |
| Stage 2                | -      | -                | -      | -      | -                | -    | 529       | 540      | -     | 314       | 336      | -     |      |
| Platoon blocked, %     |        | -                | -      |        | -                | -    |           |          |       |           |          |       |      |
| Mov Cap-1 Maneuver     | 1170   | -                | -      | 974    | -                | -    | 80        | 113      | 542   | 90        | 109      | 695   |      |
| Mov Cap-2 Maneuver     | -      | -                | -      | -      | -                | -    | 80        | 113      | -     | 90        | 109      | -     |      |
| Stage 1                | -      | -                | -      | -      | -                | -    | 285       | 306      | -     | 491       | 530      | -     |      |
| Stage 2                | -      | -                | -      | -      | -                | -    | 423       | 508      | -     | 245       | 285      | -     |      |
|                        |        |                  |        |        |                  |      |           |          |       |           |          |       |      |
| Approach               | EB     |                  |        | WB     |                  |      | NB        |          |       | SB        |          |       |      |
| HCM Control Delay, s   | 2      |                  |        | 1.2    |                  |      | 38.5      |          |       | 19.8      |          |       |      |
| HCM LOS                | 2      |                  |        | 1.2    |                  |      | 30.5<br>E |          |       | 19.0<br>C |          |       |      |
| TICWI LOS              |        |                  |        |        |                  |      |           |          |       | U         |          |       |      |
|                        |        |                  |        |        |                  |      |           |          |       |           |          |       |      |
| Minor Lane/Major Mvm   | t I    |                  | NBLn21 |        | EBL              | EBT  | EBR       | WBL      | WBT   | WBR       |          | SBLn2 |      |
| Capacity (veh/h)       |        | 80               | 113    | 542    | 1170             | -    | -         | 974      | -     | -         | 90       | 109   | 695  |
| HCM Lane V/C Ratio     |        | 0.368            | 0.019  |        |                  | -    | -         |          | -     | -         |          | 0.019 |      |
| HCM Control Delay (s)  |        | 74.2             | 37.5   | 12.2   | 8.6              | -    | -         | 8.9      | -     | -         | 57.6     | 38.7  | 11.1 |
| HCM Lane LOS           |        | F                | Е      | В      | Α                | -    | -         | Α        | -     | -         | F        | Ε     | В    |
| HCM 95th %tile Q(veh)  |        | 1.4              | 0.1    | 0.2    | 0.5              | -    | -         | 0.2      | -     | -         | 0.9      | 0.1   | 0.5  |
|                        |        |                  |        |        |                  |      |           |          |       |           |          |       |      |

| Intersection   |                 |               |                |                     |                                    |             |
|--|-----------------|---------------|----------------|---------------------|------------------------------------|-------------|
| Int Delay, s/veh   | 1.6             |               |                |                     |                                    |             |
|  |                 | WPD           | NDT            | NDD                 | CDI                                | SBT         |
| Movement   | WBL             | WBR           | NBT            | NBR                 | SBL                                |             |
| Lane Configurations  | 70              | 20            | 105            | 00                  | 22                                 | 4           |
| Traffic Vol, veh/h   | 28              | 29            | 185            | 23                  | 33                                 | 290         |
| Future Vol, veh/h  | 28              | 29            | 185            | 23                  | 33                                 | 290         |
| Conflicting Peds, #/hr   | 1               | 0             | 0              | 0                   | 0                                  | _ 0         |
| Sign Control   | Stop            | Stop          | Free           | Free                | Free                               | Free        |
| RT Channelized   | -               | None          | -              | None                | -                                  | None        |
| Storage Length   | 0               | -             | -              | -                   | -                                  | -           |
| Veh in Median Storage,   |                 | -             | 0              | -                   | -                                  | 0           |
| Grade, %   | 0               | -             | 0              | -                   | -                                  | 0           |
| Peak Hour Factor   | 91              | 91            | 91             | 91                  | 91                                 | 91          |
| Heavy Vehicles, %  | 6               | 6             | 2              | 2                   | 3                                  | 3           |
| Mvmt Flow  | 31              | 32            | 203            | 25                  | 36                                 | 319         |
|  |                 |               |                |                     |                                    |             |
| Major/Minor N  | /linor1         | ı             | Acior1         | N                   | Major?                             |             |
|  |                 |               | Major1         |                     | Major2                             |             |
| Conflicting Flow All   | 608             | 216           | 0              | 0                   | 228                                | 0           |
| Stage 1  | 216             | -             | -              | -                   | -                                  | -           |
| Stage 2  | 392             | -             | -              | -                   | -                                  | -           |
| Critical Hdwy  | 6.46            | 6.26          | -              | -                   | 4.13                               | -           |
| Critical Hdwy Stg 1  | 5.46            | -             | -              | -                   | -                                  | -           |
| Critical Hdwy Stg 2  | 5.46            | -             | -              | -                   | -                                  | -           |
|  | 3.554           | 3.354         | -              | -                   |                                    | -           |
| Pot Cap-1 Maneuver   | 452             | 814           | -              | -                   | 1334                               | -           |
| Stage 1  | 811             | -             | -              | -                   | -                                  | -           |
| Stage 2  | 674             | -             | -              | -                   | -                                  | -           |
| Platoon blocked, %   |                 |               | -              | -                   |                                    | -           |
| Mov Cap-1 Maneuver   | 437             | 814           | -              | -                   | 1334                               | -           |
| Mov Cap-2 Maneuver   | 437             | _             | -              | -                   | -                                  | _           |
| Stage 1  | 784             | -             | _              | -                   | -                                  | _           |
| •  |                 |               | _              | _                   | _                                  | _           |
| Stage 2  | 673             | _             |                |                     |                                    |             |
| Stage 2  | 673             | -             |                |                     |                                    |             |
|  |                 | -             |                |                     |                                    |             |
| Stage 2 Approach   | 673<br>WB       |               | NB             |                     | SB                                 |             |
|  |                 |               | NB<br>0        |                     | SB<br>0.8                          |             |
| Approach   | WB              |               |                |                     |                                    |             |
| Approach HCM Control Delay, s  | WB<br>12.1      |               |                |                     |                                    |             |
| Approach HCM Control Delay, s HCM LOS  | WB<br>12.1<br>B |               | 0              | \/DI                | 0.8                                | CDT         |
| Approach HCM Control Delay, s HCM LOS Minor Lane/Major Mvmt  | WB<br>12.1<br>B | NBT           | 0<br>NBRW      | VBLn1               | 0.8<br>SBL                         | SBT         |
| Approach HCM Control Delay, s HCM LOS  Minor Lane/Major Mvmt Capacity (veh/h)  | WB<br>12.1<br>B | NBT<br>-      | 0<br>NBRV      | 572                 | 0.8<br>SBL<br>1334                 | -           |
| Approach HCM Control Delay, s HCM LOS  Minor Lane/Major Mvmt Capacity (veh/h) HCM Lane V/C Ratio                       | WB<br>12.1<br>B | NBT<br>-      | 0<br>NBRV<br>- | 572<br>0.11         | 0.8<br>SBL<br>1334<br>0.027        | -           |
| Approach HCM Control Delay, s HCM LOS  Minor Lane/Major Mvmt Capacity (veh/h) HCM Lane V/C Ratio HCM Control Delay (s) | WB<br>12.1<br>B | NBT<br>-<br>- | 0<br>NBRV      | 572<br>0.11<br>12.1 | 0.8<br>SBL<br>1334<br>0.027<br>7.8 | -<br>-<br>0 |
| Approach HCM Control Delay, s HCM LOS  Minor Lane/Major Mvmt Capacity (veh/h) HCM Lane V/C Ratio                       | WB<br>12.1<br>B | NBT<br>-      | 0<br>NBRV<br>- | 572<br>0.11         | 0.8<br>SBL<br>1334<br>0.027        | -           |

|                              | ۶    | <b>→</b> | •     | •    | <b>←</b> | •     | •    | <b>†</b> | <b>/</b> | <b>/</b> | <b></b>  | 4    |
|------------------------------|------|----------|-------|------|----------|-------|------|----------|----------|----------|----------|------|
| Movement                     | EBL  | EBT      | EBR   | WBL  | WBT      | WBR   | NBL  | NBT      | NBR      | SBL      | SBT      | SBR  |
| Lane Configurations          | 1    | f)       |       | ሻ    | ₽        |       | 7    | <b>↑</b> | 7        | 7        | <b>^</b> | 7    |
| Traffic Volume (veh/h)       | 216  | 307      | 209   | 20   | 176      | 208   | 142  | 283      | 25       | 355      | 501      | 220  |
| Future Volume (veh/h)        | 216  | 307      | 209   | 20   | 176      | 208   | 142  | 283      | 25       | 355      | 501      | 220  |
| Number                       | 7    | 4        | 14    | 3    | 8        | 18    | 5    | 2        | 12       | 1        | 6        | 16   |
| Initial Q (Qb), veh          | 0    | 0        | 0     | 0    | 0        | 0     | 0    | 0        | 0        | 0        | 0        | 0    |
| Ped-Bike Adj(A_pbT)          | 1.00 |          | 1.00  | 1.00 |          | 1.00  | 1.00 |          | 1.00     | 1.00     |          | 1.00 |
| Parking Bus, Adj             | 1.00 | 1.00     | 1.00  | 1.00 | 1.00     | 1.00  | 1.00 | 1.00     | 1.00     | 1.00     | 1.00     | 1.00 |
| Adj Sat Flow, veh/h/ln       | 1863 | 1863     | 1900  | 1863 | 1863     | 1900  | 1863 | 1863     | 1863     | 1863     | 1863     | 1863 |
| Adj Flow Rate, veh/h         | 225  | 320      | 218   | 21   | 183      | 217   | 148  | 295      | 26       | 370      | 522      | 229  |
| Adj No. of Lanes             | 1    | 1        | 0     | 1    | 1        | 0     | 1    | 1        | 1        | 1        | 1        | 1    |
| Peak Hour Factor             | 0.96 | 0.96     | 0.96  | 0.96 | 0.96     | 0.96  | 0.96 | 0.96     | 0.96     | 0.96     | 0.96     | 0.96 |
| Percent Heavy Veh, %         | 2    | 2        | 2     | 2    | 2        | 2     | 2    | 2        | 2        | 2        | 2        | 2    |
| Cap, veh/h                   | 426  | 248      | 169   | 218  | 95       | 113   | 177  | 479      | 407      | 248      | 554      | 471  |
| Arrive On Green              | 0.24 | 0.24     | 0.24  | 0.12 | 0.12     | 0.12  | 0.10 | 0.26     | 0.26     | 0.14     | 0.30     | 0.30 |
| Sat Flow, veh/h              | 1774 | 1034     | 704   | 1774 | 778      | 922   | 1774 | 1863     | 1583     | 1774     | 1863     | 1583 |
| Grp Volume(v), veh/h         | 225  | 0        | 538   | 21   | 0        | 400   | 148  | 295      | 26       | 370      | 522      | 229  |
| Grp Sat Flow(s),veh/h/ln     | 1774 | 0        | 1738  | 1774 | 0        | 1700  | 1774 | 1863     | 1583     | 1774     | 1863     | 1583 |
| Q Serve(g_s), s              | 8.3  | 0.0      | 18.0  | 0.8  | 0.0      | 9.2   | 6.1  | 10.5     | 0.9      | 10.5     | 20.5     | 8.9  |
| Cycle Q Clear(g_c), s        | 8.3  | 0.0      | 18.0  | 0.8  | 0.0      | 9.2   | 6.1  | 10.5     | 0.9      | 10.5     | 20.5     | 8.9  |
| Prop In Lane                 | 1.00 |          | 0.41  | 1.00 |          | 0.54  | 1.00 |          | 1.00     | 1.00     |          | 1.00 |
| Lane Grp Cap(c), veh/h       | 426  | 0        | 417   | 218  | 0        | 209   | 177  | 479      | 407      | 248      | 554      | 471  |
| V/C Ratio(X)                 | 0.53 | 0.00     | 1.29  | 0.10 | 0.00     | 1.92  | 0.83 | 0.62     | 0.06     | 1.49     | 0.94     | 0.49 |
| Avail Cap(c_a), veh/h        | 426  | 0        | 417   | 218  | 0        | 209   | 177  | 479      | 407      | 248      | 554      | 471  |
| HCM Platoon Ratio            | 1.00 | 1.00     | 1.00  | 1.00 | 1.00     | 1.00  | 1.00 | 1.00     | 1.00     | 1.00     | 1.00     | 1.00 |
| Upstream Filter(I)           | 1.00 | 0.00     | 1.00  | 1.00 | 0.00     | 1.00  | 1.00 | 1.00     | 1.00     | 1.00     | 1.00     | 1.00 |
| Uniform Delay (d), s/veh     | 24.8 | 0.0      | 28.5  | 29.2 | 0.0      | 32.9  | 33.1 | 24.6     | 21.0     | 32.3     | 25.7     | 21.6 |
| Incr Delay (d2), s/veh       | 1.2  | 0.0      | 147.3 | 0.2  | 0.0      | 430.5 | 27.6 | 5.8      | 0.3      | 240.6    | 26.4     | 3.6  |
| Initial Q Delay(d3),s/veh    | 0.0  | 0.0      | 0.0   | 0.0  | 0.0      | 0.0   | 0.0  | 0.0      | 0.0      | 0.0      | 0.0      | 0.0  |
| %ile BackOfQ(50%),veh/ln     | 4.2  | 0.0      | 25.6  | 0.4  | 0.0      | 29.2  | 4.4  | 6.1      | 0.4      | 21.7     | 14.5     | 4.3  |
| LnGrp Delay(d),s/veh         | 26.0 | 0.0      | 175.8 | 29.4 | 0.0      | 463.4 | 60.7 | 30.4     | 21.3     | 272.8    | 52.1     | 25.2 |
| LnGrp LOS                    | С    |          | F     | С    |          | F     | Е    | С        | С        | F        | D        | С    |
| Approach Vol, veh/h          |      | 763      |       |      | 421      |       |      | 469      |          |          | 1121     |      |
| Approach Delay, s/veh        |      | 131.6    |       |      | 441.7    |       |      | 39.5     |          |          | 119.5    |      |
| Approach LOS                 |      | F        |       |      | F        |       |      | D        |          |          | F        |      |
| Timer                        | 1    | 2        | 3     | 4    | 5        | 6     | 7    | 8        |          |          |          |      |
| Assigned Phs                 | 1    | 2        |       | 4    | 5        | 6     |      | 8        |          |          |          |      |
| Phs Duration (G+Y+Rc), s     | 15.0 | 23.8     |       | 22.5 | 12.0     | 26.8  |      | 13.7     |          |          |          |      |
| Change Period (Y+Rc), s      | 4.5  | 4.5      |       | 4.5  | 4.5      | 4.5   |      | 4.5      |          |          |          |      |
| Max Green Setting (Gmax), s  | 10.5 | 19.3     |       | 18.0 | 7.5      | 22.3  |      | 9.2      |          |          |          |      |
| Max Q Clear Time (g_c+l1), s | 12.5 | 12.5     |       | 20.0 | 8.1      | 22.5  |      | 11.2     |          |          |          |      |
| Green Ext Time (p_c), s      | 0.0  | 1.0      |       | 0.0  | 0.0      | 0.0   |      | 0.0      |          |          |          |      |
| Intersection Summary         |      |          |       |      |          |       |      |          |          |          |          |      |
| HCM 2010 Ctrl Delay          |      |          | 158.2 |      |          |       |      |          |          |          |          |      |
| HCM 2010 LOS                 |      |          | F     |      |          |       |      |          |          |          |          |      |

|                              | ۶    | <b>→</b> | •     | <b>√</b> | <b>←</b> | •    | •    | †    | ~    | <b>/</b> | ļ    | ✓    |
|------------------------------|------|----------|-------|----------|----------|------|------|------|------|----------|------|------|
| Movement                     | EBL  | EBT      | EBR   | WBL      | WBT      | WBR  | NBL  | NBT  | NBR  | SBL      | SBT  | SBR  |
| Lane Configurations          | ሻ    | f)       |       | ሻ        | ₽        |      |      | 4    |      |          | 4    |      |
| Traffic Volume (veh/h)       | 28   | 633      | 139   | 132      | 382      | 17   | 107  | 42   | 82   | 28       | 68   | 12   |
| Future Volume (veh/h)        | 28   | 633      | 139   | 132      | 382      | 17   | 107  | 42   | 82   | 28       | 68   | 12   |
| Number                       | 7    | 4        | 14    | 3        | 8        | 18   | 5    | 2    | 12   | 1        | 6    | 16   |
| Initial Q (Qb), veh          | 0    | 0        | 0     | 0        | 0        | 0    | 0    | 0    | 0    | 0        | 0    | 0    |
| Ped-Bike Adj(A_pbT)          | 1.00 |          | 1.00  | 1.00     |          | 1.00 | 1.00 |      | 1.00 | 1.00     |      | 1.00 |
| Parking Bus, Adj             | 1.00 | 1.00     | 1.00  | 1.00     | 1.00     | 1.00 | 1.00 | 1.00 | 1.00 | 1.00     | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln       | 1863 | 1863     | 1900  | 1863     | 1863     | 1900 | 1900 | 1863 | 1900 | 1900     | 1827 | 1900 |
| Adj Flow Rate, veh/h         | 33   | 736      | 162   | 153      | 444      | 20   | 124  | 49   | 95   | 33       | 79   | 14   |
| Adj No. of Lanes             | 1    | 1        | 0     | 1        | 1        | 0    | 0    | 1    | 0    | 0        | 1    | 0    |
| Peak Hour Factor             | 0.86 | 0.86     | 0.86  | 0.86     | 0.86     | 0.86 | 0.86 | 0.86 | 0.86 | 0.86     | 0.86 | 0.86 |
| Percent Heavy Veh, %         | 2    | 2        | 2     | 2        | 2        | 2    | 2    | 2    | 2    | 4        | 4    | 4    |
| Cap, veh/h                   | 63   | 555      | 122   | 151      | 751      | 34   | 278  | 119  | 170  | 173      | 373  | 59   |
| Arrive On Green              | 0.04 | 0.38     | 0.38  | 0.09     | 0.42     | 0.42 | 0.31 | 0.31 | 0.31 | 0.31     | 0.31 | 0.31 |
| Sat Flow, veh/h              | 1774 | 1480     | 326   | 1774     | 1769     | 80   | 605  | 378  | 539  | 308      | 1185 | 187  |
| Grp Volume(v), veh/h         | 33   | 0        | 898   | 153      | 0        | 464  | 268  | 0    | 0    | 126      | 0    | 0    |
| Grp Sat Flow(s),veh/h/ln     | 1774 | 0        | 1805  | 1774     | 0        | 1849 | 1522 | 0    | 0    | 1679     | 0    | 0    |
| Q Serve(g_s), s              | 1.1  | 0.0      | 22.5  | 5.1      | 0.0      | 11.6 | 5.3  | 0.0  | 0.0  | 0.0      | 0.0  | 0.0  |
| Cycle Q Clear(g_c), s        | 1.1  | 0.0      | 22.5  | 5.1      | 0.0      | 11.6 | 8.4  | 0.0  | 0.0  | 3.1      | 0.0  | 0.0  |
| Prop In Lane                 | 1.00 |          | 0.18  | 1.00     |          | 0.04 | 0.46 |      | 0.35 | 0.26     |      | 0.11 |
| Lane Grp Cap(c), veh/h       | 63   | 0        | 677   | 151      | 0        | 785  | 567  | 0    | 0    | 605      | 0    | 0    |
| V/C Ratio(X)                 | 0.53 | 0.00     | 1.33  | 1.01     | 0.00     | 0.59 | 0.47 | 0.00 | 0.00 | 0.21     | 0.00 | 0.00 |
| Avail Cap(c_a), veh/h        | 163  | 0        | 677   | 151      | 0        | 785  | 567  | 0    | 0    | 605      | 0    | 0    |
| HCM Platoon Ratio            | 1.00 | 1.00     | 1.00  | 1.00     | 1.00     | 1.00 | 1.00 | 1.00 | 1.00 | 1.00     | 1.00 | 1.00 |
| Upstream Filter(I)           | 1.00 | 0.00     | 1.00  | 1.00     | 0.00     | 1.00 | 1.00 | 0.00 | 0.00 | 1.00     | 0.00 | 0.00 |
| Uniform Delay (d), s/veh     | 28.5 | 0.0      | 18.8  | 27.5     | 0.0      | 13.3 | 16.8 | 0.0  | 0.0  | 15.1     | 0.0  | 0.0  |
| Incr Delay (d2), s/veh       | 6.7  | 0.0      | 157.0 | 77.2     | 0.0      | 1.2  | 2.8  | 0.0  | 0.0  | 8.0      | 0.0  | 0.0  |
| Initial Q Delay(d3),s/veh    | 0.0  | 0.0      | 0.0   | 0.1      | 0.0      | 0.0  | 0.0  | 0.0  | 0.0  | 0.0      | 0.0  | 0.0  |
| %ile BackOfQ(50%),veh/ln     | 0.6  | 0.0      | 40.6  | 5.7      | 0.0      | 6.1  | 4.1  | 0.0  | 0.0  | 1.7      | 0.0  | 0.0  |
| LnGrp Delay(d),s/veh         | 35.2 | 0.0      | 175.8 | 104.8    | 0.0      | 14.4 | 19.6 | 0.0  | 0.0  | 15.9     | 0.0  | 0.0  |
| LnGrp LOS                    | D    |          | F     | F        |          | В    | В    |      |      | В        |      |      |
| Approach Vol, veh/h          |      | 931      |       |          | 617      |      |      | 268  |      |          | 126  |      |
| Approach Delay, s/veh        |      | 170.8    |       |          | 36.8     |      |      | 19.6 |      |          | 15.9 |      |
| Approach LOS                 |      | F        |       |          | D        |      |      | В    |      |          | В    |      |
| Timer                        | 1    | 2        | 3     | 4        | 5        | 6    | 7    | 8    |      |          |      |      |
| Assigned Phs                 |      | 2        | 3     | 4        |          | 6    | 7    | 8    |      |          |      |      |
| Phs Duration (G+Y+Rc), s     |      | 23.4     | 9.6   | 27.0     |          | 23.4 | 6.6  | 30.0 |      |          |      |      |
| Change Period (Y+Rc), s      |      | 4.5      | 4.5   | 4.5      |          | 4.5  | 4.5  | 4.5  |      |          |      |      |
| Max Green Setting (Gmax), s  |      | 18.9     | 5.1   | 22.5     |          | 18.9 | 5.5  | 22.1 |      |          |      |      |
| Max Q Clear Time (g_c+l1), s |      | 10.4     | 7.1   | 24.5     |          | 5.1  | 3.1  | 13.6 |      |          |      |      |
| Green Ext Time (p_c), s      |      | 1.0      | 0.0   | 0.0      |          | 0.5  | 0.0  | 1.9  |      |          |      |      |
| Intersection Summary         |      |          |       |          |          |      |      |      |      |          |      |      |
| HCM 2010 Ctrl Delay          |      |          | 97.3  |          |          |      |      |      |      |          |      |      |
| HCM 2010 LOS                 |      |          | F     |          |          |      |      |      |      |          |      |      |

|  |           | <b>→</b>  | ←         | •         | <b>\</b>  | 4         |      |      |  |  |
|--|-----------|-----------|-----------|-----------|-----------|-----------|------|------|--|--|
| Movement   | EBL       | EBT       | WBT       | WBR       | SBL       | SBR       |      |      |  |  |
| Lane Configurations                                | ሻ         | <u> </u>  |           | 7         | )         | 7         |      |      |  |  |
| Traffic Volume (veh/h)                             | 320       | 622       | 321       | 180       | 177       | 218       |      |      |  |  |
| Future Volume (veh/h)                              | 320       | 622       | 321       | 180       | 177       | 218       |      |      |  |  |
| Number   | 7         | 4         | 8         | 18        | 1         | 16        |      |      |  |  |
| Initial Q (Qb), veh                                | 0         | 0         | 0         | 0         | 0         | 0         |      |      |  |  |
| Ped-Bike Adj(A_pbT)                                | 1.00      | - U       | U         | 1.00      | 1.00      | 1.00      |      |      |  |  |
| Parking Bus, Adj                                   | 1.00      | 1.00      | 1.00      | 1.00      | 1.00      | 1.00      |      |      |  |  |
| Adj Sat Flow, veh/h/ln                             | 1863      | 1863      | 1863      | 1863      | 1863      | 1863      |      |      |  |  |
| Adj Flow Rate, veh/h                               | 340       | 662       | 341       | 191       | 188       | 232       |      |      |  |  |
| Adj No. of Lanes                                   | 1         | 1         | 1         | 1         | 100       | 1         |      |      |  |  |
| Peak Hour Factor                                   | 0.94      | 0.94      | 0.94      | 0.94      | 0.94      | 0.94      |      |      |  |  |
| Percent Heavy Veh, %                               | 2         | 2         | 2         | 2         | 2         | 2         |      |      |  |  |
| Cap, veh/h   | 412       | 1031      | 432       | 367       | 475       | 424       |      |      |  |  |
| Arrive On Green                                    | 0.23      | 0.55      | 0.23      | 0.23      | 0.27      | 0.27      |      |      |  |  |
| Sat Flow, veh/h                                    | 1774      | 1863      | 1863      | 1583      | 1774      | 1583      |      |      |  |  |
| Grp Volume(v), veh/h                               | 340       | 662       | 341       | 191       | 188       | 232       |      |      |  |  |
| 1 7  | 1774      | 1863      | 1863      | 1583      | 1774      | 1583      |      |      |  |  |
| Grp Sat Flow(s),veh/h/ln                           | 9.2       | 12.4      | 8.7       | 5.3       | 4.4       | 6.3       |      |      |  |  |
| Q Serve(g_s), s<br>Cycle Q Clear(g_c), s           | 9.2       | 12.4      | 8.7       | 5.3       | 4.4       | 6.3       |      |      |  |  |
| Prop In Lane                                       | 1.00      | 12.4      | 0.7       | 1.00      | 1.00      | 1.00      |      |      |  |  |
| •  | 412       | 1031      | 432       | 367       | 475       | 424       |      |      |  |  |
| Lane Grp Cap(c), veh/h<br>V/C Ratio(X)             | 0.82      | 0.64      | 0.79      | 0.52      | 0.40      | 0.55      |      |      |  |  |
| Avail Cap(c_a), veh/h                              | 651       | 1386      | 536       | 455       | 475       | 424       |      |      |  |  |
| HCM Platoon Ratio                                  | 1.00      | 1.00      | 1.00      | 1.00      | 1.00      | 1.00      |      |      |  |  |
| Upstream Filter(I)                                 | 1.00      | 1.00      | 1.00      | 1.00      | 1.00      | 1.00      |      |      |  |  |
|  | 18.4      | 7.8       | 18.2      | 16.9      | 15.1      | 15.8      |      |      |  |  |
| Uniform Delay (d), s/veh<br>Incr Delay (d2), s/veh | 4.9       | 0.7       | 6.3       | 1.1       | 2.5       | 5.0       |      |      |  |  |
| Initial Q Delay(d3),s/veh                          | 0.0       | 0.7       | 0.0       | 0.0       | 0.0       | 0.0       |      |      |  |  |
| %ile BackOfQ(50%),veh/ln                           | 5.0       | 6.4       | 5.2       | 2.4       | 2.5       | 6.2       |      |      |  |  |
| LnGrp Delay(d),s/veh                               | 23.2      | 8.5       | 24.5      | 18.0      | 17.6      | 20.8      |      |      |  |  |
| LnGrp LOS  | 23.2<br>C | 6.5<br>A  | 24.5<br>C | 10.0<br>B | 17.0<br>B | 20.6<br>C |      |      |  |  |
|  | U         |           |           | D         |           | U         |      |      |  |  |
| Approach Vol, veh/h                                |           | 1002      | 532       |           | 420       |           |      |      |  |  |
| Approach LOS                                       |           | 13.5<br>B | 22.2      |           | 19.4      |           |      |      |  |  |
| Approach LOS<br>                                   |           |           | С         |           | В         |           |      |      |  |  |
| Timer  | 1         | 2         | 3         | 4         | 5         | 6         | 7    | 8    |  |  |
| Assigned Phs                                       |           |           |           | 4         |           | 6         | 7    | 8    |  |  |
| Phs Duration (G+Y+Rc), s                           |           |           |           | 32.4      |           | 18.0      | 16.2 | 16.2 |  |  |
| Change Period (Y+Rc), s                            |           |           |           | 4.5       |           | 4.5       | 4.5  | 4.5  |  |  |
| Max Green Setting (Gmax), s                        |           |           |           | 37.5      |           | 13.5      | 18.5 | 14.5 |  |  |
| Max Q Clear Time (g_c+l1), s                       |           |           |           | 14.4      |           | 8.3       | 11.2 | 10.7 |  |  |
| Green Ext Time (p_c), s                            |           |           |           | 4.8       |           | 0.7       | 0.6  | 1.0  |  |  |
| Intersection Summary                               |           |           |           |           |           |           |      |      |  |  |
| HCM 2010 Ctrl Delay                                |           |           | 17.1      |           |           |           |      |      |  |  |
| HCM 2010 LOS                                       |           |           | В         |           |           |           |      |      |  |  |

|                                | ۶          | <b>→</b> | •      | •     | <b>←</b>    | •          | •       | <b>†</b> | /    | <b>/</b> | ţ     | ✓    |
|--------------------------------|------------|----------|--------|-------|-------------|------------|---------|----------|------|----------|-------|------|
| Movement                       | EBL        | EBT      | EBR    | WBL   | WBT         | WBR        | NBL     | NBT      | NBR  | SBL      | SBT   | SBR  |
| Lane Configurations            | 7          | <b>†</b> | 7      | Ţ     | f)          |            |         | ર્ન      | 7    |          | ર્ન   | 7    |
| Traffic Volume (vph)           | 1          | 681      | 688    | 108   | 705         | 27         | 528     | 16       | 141  | 132      | 154   | 1    |
| Future Volume (vph)            | 1          | 681      | 688    | 108   | 705         | 27         | 528     | 16       | 141  | 132      | 154   | 1    |
| Ideal Flow (vphpl)             | 1900       | 1900     | 1900   | 1900  | 1900        | 1900       | 1900    | 1900     | 1900 | 1900     | 1900  | 1900 |
| Total Lost time (s)            | 4.5        | 4.5      | 4.5    | 4.5   | 4.5         |            |         | 4.5      | 4.5  |          | 4.5   | 4.5  |
| Lane Util. Factor              | 1.00       | 1.00     | 1.00   | 1.00  | 1.00        |            |         | 1.00     | 1.00 |          | 1.00  | 1.00 |
| Frt                            | 1.00       | 1.00     | 0.85   | 1.00  | 0.99        |            |         | 1.00     | 0.85 |          | 1.00  | 0.85 |
| Flt Protected                  | 0.95       | 1.00     | 1.00   | 0.95  | 1.00        |            |         | 0.95     | 1.00 |          | 0.98  | 1.00 |
| Satd. Flow (prot)              | 1687       | 1776     | 1509   | 1583  | 1657        |            |         | 1777     | 1583 |          | 1821  | 1583 |
| Flt Permitted                  | 0.95       | 1.00     | 1.00   | 0.95  | 1.00        |            |         | 0.95     | 1.00 |          | 0.98  | 1.00 |
| Satd. Flow (perm)              | 1687       | 1776     | 1509   | 1583  | 1657        |            |         | 1777     | 1583 |          | 1821  | 1583 |
| Peak-hour factor, PHF          | 0.94       | 0.94     | 0.94   | 0.94  | 0.94        | 0.94       | 0.94    | 0.94     | 0.94 | 0.94     | 0.94  | 0.94 |
| Adj. Flow (vph)                | 1          | 724      | 732    | 115   | 750         | 29         | 562     | 17       | 150  | 140      | 164   | 1    |
| RTOR Reduction (vph)           | 0          | 0        | 379    | 0     | 1           | 0          | 0       | 0        | 84   | 0        | 0     | 1    |
| Lane Group Flow (vph)          | 1          | 724      | 353    | 115   | 778         | 0          | 0       | 579      | 66   | 0        | 304   | 0    |
| Heavy Vehicles (%)             | 7%         | 7%       | 7%     | 14%   | 14%         | 14%        | 2%      | 2%       | 2%   | 2%       | 2%    | 2%   |
| Turn Type                      | Prot       | NA       | Perm   | Prot  | NA          |            | Split   | NA       | Perm | Split    | NA    | Perm |
| Protected Phases               | 7          | 4        |        | 3     | 8           |            | 5       | 5        |      | 6        | 6     |      |
| Permitted Phases               |            |          | 4      |       |             |            |         |          | 5    |          |       | 6    |
| Actuated Green, G (s)          | 1.0        | 48.1     | 48.1   | 5.0   | 52.1        |            |         | 22.1     | 22.1 |          | 19.9  | 19.9 |
| Effective Green, g (s)         | 1.0        | 48.1     | 48.1   | 5.0   | 52.1        |            |         | 22.1     | 22.1 |          | 19.9  | 19.9 |
| Actuated g/C Ratio             | 0.01       | 0.43     | 0.43   | 0.04  | 0.46        |            |         | 0.20     | 0.20 |          | 0.18  | 0.18 |
| Clearance Time (s)             | 4.5        | 4.5      | 4.5    | 4.5   | 4.5         |            |         | 4.5      | 4.5  |          | 4.5   | 4.5  |
| Vehicle Extension (s)          | 3.0        | 3.0      | 3.0    | 3.0   | 3.0         |            |         | 3.0      | 3.0  |          | 3.0   | 3.0  |
| Lane Grp Cap (vph)             | 14         | 755      | 641    | 69    | 763         |            |         | 347      | 309  |          | 320   | 278  |
| v/s Ratio Prot                 | 0.00       | 0.41     |        | c0.07 | c0.47       |            |         | c0.33    |      |          | c0.17 |      |
| v/s Ratio Perm                 |            |          | 0.23   |       |             |            |         |          | 0.04 |          |       | 0.00 |
| v/c Ratio                      | 0.07       | 0.96     | 0.55   | 1.67  | 1.02        |            |         | 1.67     | 0.21 |          | 0.95  | 0.00 |
| Uniform Delay, d1              | 55.6       | 31.5     | 24.4   | 54.0  | 30.5        |            |         | 45.5     | 38.2 |          | 46.1  | 38.4 |
| Progression Factor             | 1.00       | 1.00     | 1.00   | 1.00  | 1.00        |            |         | 1.00     | 1.00 |          | 1.00  | 1.00 |
| Incremental Delay, d2          | 2.2        | 24.1     | 3.4    | 355.1 | 37.6        |            |         | 313.3    | 0.3  |          | 36.7  | 0.0  |
| Delay (s)                      | 57.8       | 55.7     | 27.8   | 409.1 | 68.1        |            |         | 358.8    | 38.6 |          | 82.8  | 38.4 |
| Level of Service               | E          | E        | С      | F     | E           |            |         | F        | D    |          | F     | D    |
| Approach Delay (s)             |            | 41.7     |        |       | 112.0       |            |         | 292.9    |      |          | 82.7  |      |
| Approach LOS                   |            | D        |        |       | F           |            |         | F        |      |          | F     |      |
| Intersection Summary           |            |          |        |       |             |            |         |          |      |          |       |      |
| HCM 2000 Control Delay         |            |          | 118.0  | Н     | CM 2000     | Level of S | Service |          | F    |          |       |      |
| HCM 2000 Volume to Capac       | city ratio |          | 1.20   |       |             |            |         |          |      |          |       |      |
| Actuated Cycle Length (s)      |            |          | 113.1  |       | um of lost  |            |         |          | 18.0 |          |       |      |
| Intersection Capacity Utilizat | tion       |          | 103.4% | IC    | CU Level of | of Service |         |          | G    |          |       |      |
| Analysis Period (min)          |            |          | 15     |       |             |            |         |          |      |          |       |      |
| c Critical Lane Group          |            |          |        |       |             |            |         |          |      |          |       |      |

## 8: Airline Hwy (SR 25)/Pinnacles Nat Pk Hwy (SR 25) & Tres Pinos Rd/Sunnslope Rd

|                              | ۶    | <b>→</b> | •         | •    | <b>←</b> | •    | 1    | <b>†</b>    | <b>/</b> | <b>/</b> | Ţ        | ✓    |
|------------------------------|------|----------|-----------|------|----------|------|------|-------------|----------|----------|----------|------|
| Movement                     | EBL  | EBT      | EBR       | WBL  | WBT      | WBR  | NBL  | NBT         | NBR      | SBL      | SBT      | SBR  |
| Lane Configurations          | 1,1  | <b>^</b> | 7         | ሻ    | <b>^</b> | 7    | ሻሻ   | <b>↑</b> ↑₽ |          | ሻሻ       | <b>^</b> | 7    |
| Traffic Volume (veh/h)       | 196  | 400      | 208       | 167  | 303      | 332  | 217  | 636         | 141      | 491      | 1033     | 255  |
| Future Volume (veh/h)        | 196  | 400      | 208       | 167  | 303      | 332  | 217  | 636         | 141      | 491      | 1033     | 255  |
| Number                       | 7    | 4        | 14        | 3    | 8        | 18   | 5    | 2           | 12       | 1        | 6        | 16   |
| Initial Q (Qb), veh          | 0    | 0        | 0         | 0    | 0        | 0    | 0    | 0           | 0        | 0        | 0        | 0    |
| Ped-Bike Adj(A_pbT)          | 1.00 |          | 0.99      | 1.00 |          | 1.00 | 1.00 |             | 1.00     | 1.00     |          | 1.00 |
| Parking Bus, Adj             | 1.00 | 1.00     | 1.00      | 1.00 | 1.00     | 1.00 | 1.00 | 1.00        | 1.00     | 1.00     | 1.00     | 1.00 |
| Adj Sat Flow, veh/h/ln       | 1863 | 1863     | 1863      | 1863 | 1863     | 1863 | 1863 | 1863        | 1900     | 1863     | 1863     | 1863 |
| Adj Flow Rate, veh/h         | 204  | 417      | 217       | 174  | 316      | 346  | 226  | 662         | 147      | 511      | 1076     | 266  |
| Adj No. of Lanes             | 2    | 2        | 1         | 1    | 2        | 1    | 2    | 3           | 0        | 2        | 3        | 1    |
| Peak Hour Factor             | 0.96 | 0.96     | 0.96      | 0.96 | 0.96     | 0.96 | 0.96 | 0.96        | 0.96     | 0.96     | 0.96     | 0.96 |
| Percent Heavy Veh, %         | 2    | 2        | 2         | 2    | 2        | 2    | 2    | 2           | 2        | 2        | 2        | 2    |
| Cap, veh/h                   | 300  | 792      | 496       | 214  | 910      | 405  | 319  | 1196        | 262      | 337      | 1482     | 599  |
| Arrive On Green              | 0.09 | 0.22     | 0.22      | 0.12 | 0.26     | 0.26 | 0.09 | 0.29        | 0.29     | 0.10     | 0.29     | 0.29 |
| Sat Flow, veh/h              | 3442 | 3539     | 1560      | 1774 | 3539     | 1576 | 3442 | 4177        | 915      | 3442     | 5085     | 1580 |
| Grp Volume(v), veh/h         | 204  | 417      | 217       | 174  | 316      | 346  | 226  | 536         | 273      | 511      | 1076     | 266  |
| Grp Sat Flow(s),veh/h/ln     | 1721 | 1770     | 1560      | 1774 | 1770     | 1576 | 1721 | 1695        | 1701     | 1721     | 1695     | 1580 |
| Q Serve(g_s), s              | 3.8  | 6.9      | 7.3       | 6.3  | 4.8      | 13.9 | 4.2  | 8.9         | 9.1      | 6.5      | 12.6     | 8.3  |
| Cycle Q Clear(g_c), s        | 3.8  | 6.9      | 7.3       | 6.3  | 4.8      | 13.9 | 4.2  | 8.9         | 9.1      | 6.5      | 12.6     | 8.3  |
| Prop In Lane                 | 1.00 |          | 1.00      | 1.00 |          | 1.00 | 1.00 |             | 0.54     | 1.00     |          | 1.00 |
| Lane Grp Cap(c), veh/h       | 300  | 792      | 496       | 214  | 910      | 405  | 319  | 971         | 487      | 337      | 1482     | 599  |
| V/C Ratio(X)                 | 0.68 | 0.53     | 0.44      | 0.81 | 0.35     | 0.85 | 0.71 | 0.55        | 0.56     | 1.52     | 0.73     | 0.44 |
| Avail Cap(c_a), veh/h        | 389  | 960      | 570       | 227  | 1013     | 451  | 337  | 971         | 487      | 337      | 1482     | 599  |
| HCM Platoon Ratio            | 1.00 | 1.00     | 1.00      | 1.00 | 1.00     | 1.00 | 1.00 | 1.00        | 1.00     | 1.00     | 1.00     | 1.00 |
| Upstream Filter(I)           | 1.00 | 1.00     | 1.00      | 1.00 | 1.00     | 1.00 | 1.00 | 1.00        | 1.00     | 1.00     | 1.00     | 1.00 |
| Uniform Delay (d), s/veh     | 29.4 | 22.7     | 18.0      | 28.4 | 20.1     | 23.5 | 29.2 | 20.1        | 20.1     | 29.9     | 21.1     | 15.4 |
| Incr Delay (d2), s/veh       | 3.2  | 0.5      | 0.6       | 18.8 | 0.2      | 13.6 | 6.3  | 2.3         | 4.6      | 246.9    | 3.1      | 2.4  |
| Initial Q Delay(d3),s/veh    | 0.0  | 0.0      | 0.0       | 0.0  | 0.0      | 0.0  | 0.0  | 0.0         | 0.0      | 0.0      | 0.0      | 0.0  |
| %ile BackOfQ(50%),veh/ln     | 1.9  | 3.4      | 3.2       | 4.2  | 2.4      | 7.5  | 2.3  | 4.5         | 4.9      | 14.6     | 6.3      | 4.0  |
| LnGrp Delay(d),s/veh         | 32.5 | 23.2     | 18.6      | 47.2 | 20.3     | 37.1 | 35.5 | 22.3        | 24.8     | 276.8    | 24.3     | 17.8 |
| LnGrp LOS                    | С    | С        | В         | D    | С        | D    | D    | С           | С        | F        | С        | В    |
| Approach Vol, veh/h          |      | 838      |           |      | 836      |      |      | 1035        |          |          | 1853     |      |
| Approach Delay, s/veh        |      | 24.3     |           |      | 32.8     |      |      | 25.9        |          |          | 93.0     |      |
| Approach LOS                 |      | С        |           |      | С        |      |      | С           |          |          | F        |      |
| Timer                        | 1    | 2        | 3         | 4    | 5        | 6    | 7    | 8           |          |          |          |      |
| Assigned Phs                 | 1    | 2        | 3         | 4    | 5        | 6    | 7    | 8           |          |          |          |      |
| Phs Duration (G+Y+Rc), s     | 11.0 | 23.5     | 12.5      | 19.3 | 10.7     | 23.8 | 10.3 | 21.6        |          |          |          |      |
| Change Period (Y+Rc), s      | 4.5  | 4.5      | 4.5       | 4.5  | 4.5      | 4.5  | 4.5  | 4.5         |          |          |          |      |
| Max Green Setting (Gmax), s  | 6.5  | 19.0     | 8.5       | 18.0 | 6.5      | 19.0 | 7.5  | 19.0        |          |          |          |      |
| Max Q Clear Time (g_c+l1), s | 8.5  | 11.1     | 8.3       | 9.3  | 6.2      | 14.6 | 5.8  | 15.9        |          |          |          |      |
| Green Ext Time (p_c), s      | 0.0  | 3.2      | 0.0       | 2.3  | 0.0      | 3.0  | 0.1  | 1.1         |          |          |          |      |
| Intersection Summary         |      |          |           |      |          |      |      |             |          |          |          |      |
| HCM 2010 Ctrl Delay          |      |          | 54.1      |      |          |      |      |             |          |          |          |      |
| HCM 2010 Cur belay           |      |          | 04.1<br>D |      |          |      |      |             |          |          |          |      |
| HOW ZO TO LOS                |      |          | U         |      |          |      |      |             |          |          |          |      |

| Movement   BBL   BBT   BBR   WBL   WBT   WBR   NBL   NBT   NBR   SBL   SBR   SBR   Lane Configurations   1  | -                         | ۶    | <b>→</b> | `*   | <b>√</b> | <b>←</b> | •    | 1    | †        | _    | <b>\</b> | <b></b> | <b>√</b> |
|---|---------------------------|------|----------|------|----------|----------|------|------|----------|------|----------|---------|----------|
| Traffic Volume (veh/h) 15 179 84 202 236 231 60 179 216 177 103 10   Number 7 4 14 3 3 8 18 5 2 12 1 6 16   Initial Q(b), veh 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0   | Movement                  | EBL  | EBT      | EBR  | WBL      | WBT      | WBR  | NBL  | NBT      | NBR  | SBL      | SBT     | SBR      |
| Future Volume (veh/h)  15   | Lane Configurations       | 7    | <b>₽</b> |      | 7        | f)       |      | Ţ    | <b>†</b> | 7    | Ţ        | f)      |          |
| Number 7 4 14 3 8 18 5 2 112 1 6 16 16 Initial Q (Qb), veh 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0  | Traffic Volume (veh/h)    |      | 179      |      | 202      | 236      |      |      |          | 216  | 177      |         |          |
| Initial Q (Qb), veh   | Future Volume (veh/h)     |      | 179      |      | 202      | 236      |      |      | 179      |      | 177      | 103     |          |
| Pack-Bisk Adji(A, pbT)         1.00         0.95         1.00         0.99         1.00         0.99         1.00         0.09           Parking Bus, Adj         1.00   |                           |      | 4        | 14   | 3        | 8        | 18   | 5    | 2        | 12   | 1        | 6       |          |
| Parking Bus, Adj  | \ //                      |      | 0        |      |          | 0        |      |      | 0        |      |          | 0       |          |
| Adj Sat Flow, veh/h/ln         1863         1863         1900         1863         1863         1863         1863         1863         1863         1863         1863         1863         1863         1863         1863         1863         1863         1863         1863         1863         1900           Adj Ro, of Lanes         1         1         0         1         1         0         1 <td>, —, ,</td> <td></td>  | , —, ,                    |      |          |      |          |          |      |      |          |      |          |         |          |
| Adj Flow Rate, veh/h         18         213         100         240         281         275         71         213         257         211         123         12           Adj No, of Lanes         1         1         0         1         1         0         1         1         1         1         1         0           Peak Hour Factor         0.84   |                           |      |          |      |          |          |      |      |          |      |          |         |          |
| Adj No. of Lanes         1         1         0         1         1         0         1         1         0         1         0         1         1         0         1         1         0         0         0         0         2  |                           |      |          |      |          |          |      |      |          |      |          |         |          |
| Peak Hour Factor         0.84 <td>_ ·</td> <td></td> <td>213</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>211</td> <td></td> <td></td>      | _ ·                       |      | 213      |      |          |          |      |      |          |      | 211      |         |          |
| Percent Heavy Veh, %  |                           |      |          |      |          |          |      |      |          |      |          |         |          |
| Cap, veh/h         38         265         125         277         311         305         97         513         433         132         493         48           Arrive On Green         0.02         0.23         0.23         0.16         0.36         0.05         0.28         0.028         0.07         0.30         0.30           Sat Flow, veh/h         1774         1176         552         1774         863         844         1774         1863         1572         1774         1670         163           Grp Sat Flow(s), veh/h/ln         1774         1729         1774         0         150         1772         1774         1863         1572         1774         0         133           Grp Sat Flow(s), veh/h/ln         1774         0         1729         1774         0         1707         1774         1863         1572         1774         0         133           Qserve(g. s), so.         0.7         0.0         11.5         8.9         0.0         20.7         2.6         6.3         9.5         5.0         0.0         3.8           Cycle Q Clear(g. sc)         8.0         0.7         0.0         11.5         8.9         0.0         20.7  |                           |      |          |      |          |          |      |      |          |      |          |         |          |
| Arrive On Green   | •                         |      |          |      |          |          |      |      |          |      |          |         |          |
| Sat Flow, veh/h         1774         1176         552         1774         863         844         1774         1863         1572         1774         1670         163           Gry Volume(v), veh/h         18         0         313         240         0         556         71         213         257         211         0         135           Gry Sat Flow(s), veh/h/ln         1774         0         1729         1774         0         1707         1774         1863         1572         1774         0         183           Qserve(g, s), s         0.7         0.0         11.5         8.9         0.0         20.7         2.6         6.3         9.5         5.0         0.0         3.8           Cycle Q Clear(g, c), s         0.7         0.0         11.5         8.9         0.0         20.7         2.6         6.3         9.5         5.0         0.0         3.8           Prop In Lane         1.00         0.032         1.00         0.49         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00  |                           |      |          |      |          |          |      |      |          |      |          |         |          |
| Grp Volume(v), veh/h         18         0         313         240         0         556         71         213         257         211         0         135           Grp Sat Flow(s), veh/h/ln         1774         0         1729         1774         0         1707         1774         1863         1572         1774         0         1833           Q Serve(g_s), s         0.7         0.0         11.5         8.9         0.0         20.7         2.6         6.3         9.5         5.0         0.0         3.8           Cycle Q Clear(g_c), s         0.7         0.0         11.5         8.9         0.0         20.7         2.6         6.3         9.5         5.0         0.0         3.8           Prop In Lane         1.00         0.32         1.00         0.49         1.00         1.00         1.00         0.09           Lane Grp Cap(c), veh/h         38         0         390         277         0         616         97         513         433         132         0         541           V/C Ratio(X)         0.48         0.00         0.87         0.00         0.07         0.02         1.50         1.00         1.00         1.00         1.00   |                           |      |          |      |          |          |      |      |          |      |          |         |          |
| Grp Sat Flow(s), veh/h/ln   | ·                         |      | 1176     |      |          | 863      |      |      | 1863     |      |          | 1670    |          |
| QServe(g_s), s  | 1 ( ),                    |      | 0        |      | 240      | 0        |      |      |          |      |          | 0       |          |
| Cycle Q Clear(g_c), s         0.7         0.0         11.5         8.9         0.0         20.7         2.6         6.3         9.5         5.0         0.0         3.8           Prop In Lane         1.00         0.32         1.00         0.49         1.00         1.00         1.00         0.09           Lane Grp Cap(c), veh/h         38         0         390         277         0         616         97         513         433         132         0         541           V/C Ratio(X)         0.48         0.00         0.80         0.87         0.00         0.90         0.73         0.42         0.59         1.60         0.00         0.25           Avail Cap(c_a), veh/h         132         0         463         277         0         616         132         513         433         132         0         541           HCM Platoon Ratio         1.00         1.0  | Grp Sat Flow(s),veh/h/ln  |      |          |      |          |          |      |      |          |      |          | 0       |          |
| Prop In Lane  |                           |      | 0.0      |      |          |          |      |      |          | 9.5  |          | 0.0     |          |
| Lane Grp Cap(c), veh/h 38 0 390 277 0 616 97 513 433 132 0 541  V/C Ratio(X) 0.48 0.00 0.80 0.87 0.00 0.90 0.73 0.42 0.59 1.60 0.00 0.25  Avail Cap(c_a), veh/h 132 0 463 277 0 616 132 513 433 132 0 541  HCM Platoon Ratio 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.0   |                           |      | 0.0      |      |          | 0.0      | 20.7 |      | 6.3      | 9.5  |          | 0.0     |          |
| V/C Ratio(X)         0.48         0.00         0.80         0.87         0.00         0.90         0.73         0.42         0.59         1.60         0.00         0.25           Avail Cap(c_a), veh/h         132         0         463         277         0         616         132         513         433         132         0         541           HCM Platoon Ratio         1.00 <td></td> <td></td> <td></td> <td>0.32</td> <td>1.00</td> <td></td> <td>0.49</td> <td>1.00</td> <td></td> <td>1.00</td> <td>1.00</td> <td></td> <td>0.09</td> |                           |      |          | 0.32 | 1.00     |          | 0.49 | 1.00 |          | 1.00 | 1.00     |         | 0.09     |
| Avail Cap(c_a), veh/h         132         0         463         277         0         616         132         513         433         132         0         541           HCM Platoon Ratio         1.00  | Lane Grp Cap(c), veh/h    |      |          |      |          |          |      | 97   |          | 433  |          |         |          |
| HCM Platoon Ratio   |                           |      | 0.00     |      |          | 0.00     |      |      |          |      |          | 0.00    |          |
| Upstream Filter(I)  | Avail Cap(c_a), veh/h     |      |          |      |          |          |      | 132  |          |      |          |         | 541      |
| Uniform Delay (d), s/veh 32.5 0.0 24.6 27.6 0.0 20.3 31.3 19.9 21.1 31.1 0.0 18.0 Incr Delay (d2), s/veh 9.1 0.0 8.4 23.6 0.0 16.7 12.6 2.5 5.9 301.3 0.0 1.1 Initial Q Delay(d3), s/veh 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.   | HCM Platoon Ratio         |      | 1.00     |      |          |          |      | 1.00 |          |      |          | 1.00    |          |
| Incr Delay (d2), s/veh  | Upstream Filter(I)        |      | 0.00     |      |          | 0.00     |      |      |          |      |          |         |          |
| Initial Q Delay(d3),s/veh   | Uniform Delay (d), s/veh  |      | 0.0      |      | 27.6     |          |      |      |          |      |          | 0.0     | 18.0     |
| %ile BackOfQ(50%), veh/In       0.4       0.0       6.4       6.2       0.0       12.6       1.6       3.5       4.8       13.5       0.0       2.1         LnGrp Delay(d),s/veh       41.6       0.0       33.0       51.3       0.0       37.0       43.9       22.4       26.9       332.4       0.0       19.1         LnGrp LOS       D       C       D       D       D       C       C       F       B         Approach Vol, veh/h       331       796       541       346         Approach Delay, s/veh       33.5       41.3       27.4       210.1         Approach LOS       C       D       C       F         Timer       1       2       3       4       5       6       7       8         Assigned Phs       1       2       3       4       5       6       7       8         Phs Duration (G+Y+Rc), s       9.5       23.0       15.0       19.6       8.2       24.3       5.9       28.7         Change Period (Y+Rc), s       4.5       4.5       4.5       4.5       4.5       4.5       4.5         Max Q Clear Time (g_c+l1), s       7.0       11.5       10.9  | Incr Delay (d2), s/veh    |      | 0.0      |      |          |          | 16.7 | 12.6 |          | 5.9  |          | 0.0     |          |
| LnGrp Delay(d),s/veh         41.6         0.0         33.0         51.3         0.0         37.0         43.9         22.4         26.9         332.4         0.0         19.1           LnGrp LOS         D         C         D         D         D         C         C         F         B           Approach Vol, veh/h         33.1         796         541         346           Approach Delay, s/veh         33.5         41.3         27.4         210.1           Approach LOS         C         D         C         F           Timer         1         2         3         4         5         6         7         8           Assigned Phs         1         2         3         4         5         6         7         8           Phs Duration (G+Y+Rc), s         9.5         23.0         15.0         19.6         8.2         24.3         5.9         28.7           Change Period (Y+Rc), s         4.5         4.5         4.5         4.5         4.5         4.5         4.5           Max Green Setting (Gmax), s         5.0         18.5         10.9         13.5         4.6         5.8         2.7         22.7           Gr   | Initial Q Delay(d3),s/veh |      | 0.0      |      |          |          |      |      |          | 0.0  |          | 0.0     |          |
| LnGrp LOS         D         C         D         D         D         C         F         B           Approach Vol, veh/h         331         796         541         346           Approach Delay, s/veh         33.5         41.3         27.4         210.1           Approach LOS         C         D         C         F           Timer         1         2         3         4         5         6         7         8           Assigned Phs         1         2         3         4         5         6         7         8           Phs Duration (G+Y+Rc), s         9.5         23.0         15.0         19.6         8.2         24.3         5.9         28.7           Change Period (Y+Rc), s         4.5  | %ile BackOfQ(50%),veh/ln  |      |          |      |          |          |      |      |          |      |          |         |          |
| Approach Vol, veh/h       331       796       541       346         Approach Delay, s/veh       33.5       41.3       27.4       210.1         Approach LOS       C       D       C       F         Timer       1       2       3       4       5       6       7       8         Assigned Phs       1       2       3       4       5       6       7       8         Phs Duration (G+Y+Rc), s       9.5       23.0       15.0       19.6       8.2       24.3       5.9       28.7         Change Period (Y+Rc), s       4.5       4.5       4.5       4.5       4.5       4.5       4.5       4.5         Max Green Setting (Gmax), s       5.0       18.5       10.5       18.0       5.0       18.5       5.0       23.5         Max Q Clear Time (g_c+I1), s       7.0       11.5       10.9       13.5       4.6       5.8       2.7       22.7         Green Ext Time (p_c), s       0.0       1.3       0.0       0.7       0.0       0.5       0.0       0.3         Intersection Summary         HCM 2010 Ctrl Delay       65.3  | LnGrp Delay(d),s/veh      | 41.6 | 0.0      |      | 51.3     | 0.0      | 37.0 | 43.9 | 22.4     |      | 332.4    | 0.0     | 19.1     |
| Approach Delay, s/veh 33.5 41.3 27.4 210.1  Approach LOS C D C F  Timer 1 2 3 4 5 6 7 8  Assigned Phs 1 2 3 4 5 6 7 8  Phs Duration (G+Y+Rc), s 9.5 23.0 15.0 19.6 8.2 24.3 5.9 28.7  Change Period (Y+Rc), s 4.5 4.5 4.5 4.5 4.5 4.5 4.5  Max Green Setting (Gmax), s 5.0 18.5 10.5 18.0 5.0 18.5 5.0 23.5  Max Q Clear Time (g_c+I1), s 7.0 11.5 10.9 13.5 4.6 5.8 2.7 22.7  Green Ext Time (p_c), s 0.0 1.3 0.0 0.7 0.0 0.5 0.0 0.3  Intersection Summary  HCM 2010 Ctrl Delay 65.3  | LnGrp LOS                 | D    |          | С    | D        |          | D    | D    | С        | С    | F        |         | <u> </u> |
| Approach LOS C D C F  Timer 1 2 3 4 5 6 7 8  Assigned Phs 1 2 3 4 5 6 7 8  Phs Duration (G+Y+Rc), s 9.5 23.0 15.0 19.6 8.2 24.3 5.9 28.7  Change Period (Y+Rc), s 4.5 4.5 4.5 4.5 4.5 4.5 4.5  Max Green Setting (Gmax), s 5.0 18.5 10.5 18.0 5.0 18.5 5.0 23.5  Max Q Clear Time (g_c+I1), s 7.0 11.5 10.9 13.5 4.6 5.8 2.7 22.7  Green Ext Time (p_c), s 0.0 1.3 0.0 0.7 0.0 0.5 0.0 0.3  Intersection Summary  HCM 2010 Ctrl Delay 65.3  | Approach Vol, veh/h       |      | 331      |      |          | 796      |      |      | 541      |      |          | 346     |          |
| Timer 1 2 3 4 5 6 7 8  Assigned Phs 1 2 3 4 5 6 7 8  Phs Duration (G+Y+Rc), s 9.5 23.0 15.0 19.6 8.2 24.3 5.9 28.7  Change Period (Y+Rc), s 4.5 4.5 4.5 4.5 4.5 4.5  Max Green Setting (Gmax), s 5.0 18.5 10.5 18.0 5.0 18.5 5.0 23.5  Max Q Clear Time (g_c+I1), s 7.0 11.5 10.9 13.5 4.6 5.8 2.7 22.7  Green Ext Time (p_c), s 0.0 1.3 0.0 0.7 0.0 0.5 0.0 0.3  Intersection Summary  HCM 2010 Ctrl Delay 65.3  | Approach Delay, s/veh     |      | 33.5     |      |          | 41.3     |      |      | 27.4     |      |          | 210.1   |          |
| Assigned Phs 1 2 3 4 5 6 7 8 Phs Duration (G+Y+Rc), s 9.5 23.0 15.0 19.6 8.2 24.3 5.9 28.7 Change Period (Y+Rc), s 4.5 4.5 4.5 4.5 4.5 4.5 4.5 Max Green Setting (Gmax), s 5.0 18.5 10.5 18.0 5.0 18.5 5.0 23.5 Max Q Clear Time (g_c+I1), s 7.0 11.5 10.9 13.5 4.6 5.8 2.7 22.7 Green Ext Time (p_c), s 0.0 1.3 0.0 0.7 0.0 0.5 0.0 0.3  Intersection Summary HCM 2010 Ctrl Delay 65.3   | Approach LOS              |      | С        |      |          | D        |      |      | С        |      |          | F       |          |
| Phs Duration (G+Y+Rc), s 9.5 23.0 15.0 19.6 8.2 24.3 5.9 28.7  Change Period (Y+Rc), s 4.5 4.5 4.5 4.5 4.5 4.5 4.5  Max Green Setting (Gmax), s 5.0 18.5 10.5 18.0 5.0 18.5 5.0 23.5  Max Q Clear Time (g_c+I1), s 7.0 11.5 10.9 13.5 4.6 5.8 2.7 22.7  Green Ext Time (p_c), s 0.0 1.3 0.0 0.7 0.0 0.5 0.0 0.3  Intersection Summary  HCM 2010 Ctrl Delay 65.3   | Timer                     | 1    | 2        | 3    | 4        | 5        | 6    | 7    | 8        |      |          |         |          |
| Change Period (Y+Rc), s 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 Max Green Setting (Gmax), s 5.0 18.5 10.5 18.0 5.0 18.5 5.0 23.5 Max Q Clear Time (g_c+I1), s 7.0 11.5 10.9 13.5 4.6 5.8 2.7 22.7 Green Ext Time (p_c), s 0.0 1.3 0.0 0.7 0.0 0.5 0.0 0.3 Intersection Summary  HCM 2010 Ctrl Delay 65.3  | Assigned Phs              | 1    | 2        | 3    | 4        | 5        | 6    | 7    | 8        |      |          |         |          |
| Max Green Setting (Gmax), s       5.0       18.5       10.5       18.0       5.0       18.5       5.0       23.5         Max Q Clear Time (g_c+l1), s       7.0       11.5       10.9       13.5       4.6       5.8       2.7       22.7         Green Ext Time (p_c), s       0.0       1.3       0.0       0.7       0.0       0.5       0.0       0.3         Intersection Summary         HCM 2010 Ctrl Delay       65.3   | Phs Duration (G+Y+Rc), s  | 9.5  | 23.0     | 15.0 | 19.6     | 8.2      | 24.3 | 5.9  | 28.7     |      |          |         |          |
| Max Green Setting (Gmax), s       5.0       18.5       10.5       18.0       5.0       18.5       5.0       23.5         Max Q Clear Time (g_c+l1), s       7.0       11.5       10.9       13.5       4.6       5.8       2.7       22.7         Green Ext Time (p_c), s       0.0       1.3       0.0       0.7       0.0       0.5       0.0       0.3         Intersection Summary         HCM 2010 Ctrl Delay       65.3   |                           | 4.5  | 4.5      | 4.5  | 4.5      | 4.5      | 4.5  | 4.5  | 4.5      |      |          |         |          |
| Max Q Clear Time (g_c+l1), s       7.0       11.5       10.9       13.5       4.6       5.8       2.7       22.7         Green Ext Time (p_c), s       0.0       1.3       0.0       0.7       0.0       0.5       0.0       0.3         Intersection Summary         HCM 2010 Ctrl Delay       65.3  |                           |      |          |      |          |          |      |      |          |      |          |         |          |
| Green Ext Time (p_c), s 0.0 1.3 0.0 0.7 0.0 0.5 0.0 0.3  Intersection Summary  HCM 2010 Ctrl Delay 65.3   |                           |      |          |      |          |          |      |      |          |      |          |         |          |
| HCM 2010 Ctrl Delay 65.3  |                           | 0.0  | 1.3      | 0.0  | 0.7      | 0.0      | 0.5  | 0.0  | 0.3      |      |          |         |          |
|   | Intersection Summary      |      |          |      |          |          |      |      |          |      |          |         |          |
|   | HCM 2010 Ctrl Delay       |      |          | 65.3 |          |          |      |      |          |      |          |         |          |
|   |                           |      |          |      |          |          |      |      |          |      |          |         |          |

## Appendix F

Level of Service
Calculations

Background Plus Project
Conditions

231

0.536

8.353

Yes

430

6.127

0.537

20.4

C

3.1

8

94

8

0.205

7.828

Yes

457

5.602

0.206

12.6

В

8.0

146

0.345

8.528

Yes

421

6.306

0.347

15.8

С

1.5

8

| Intersection               |      |          |       |       |          |       |       |       |       |       |          |       |
|----------------------------|------|----------|-------|-------|----------|-------|-------|-------|-------|-------|----------|-------|
| Intersection Delay, s/veh  | 15.9 |          |       |       |          |       |       |       |       |       |          |       |
| Intersection LOS           | С    |          |       |       |          |       |       |       |       |       |          |       |
|                            |      |          |       |       |          |       |       |       |       |       |          |       |
| Movement                   | EBL  | EBT      | EBR   | WBL   | WBT      | WBR   | NBL   | NBT   | NBR   | SBL   | SBT      | SBR   |
| Lane Configurations        | ሻ    | <b>^</b> | 7     | ሻ     | <b>1</b> | 7     | ሻ     | î,    |       | ሻ     | <b>^</b> | 7     |
| Traffic Vol, veh/h         | 131  | 130      | 89    | 7     | 214      | 94    | 208   | 82    | 3     | 69    | 34       | 137   |
| Future Vol, veh/h          | 131  | 130      | 89    | 7     | 214      | 94    | 208   | 82    | 3     | 69    | 34       | 137   |
| Peak Hour Factor           | 0.90 | 0.90     | 0.90  | 0.90  | 0.90     | 0.90  | 0.90  | 0.90  | 0.90  | 0.90  | 0.90     | 0.90  |
| Heavy Vehicles, %          | 7    | 7        | 7     | 5     | 5        | 5     | 2     | 2     | 2     | 6     | 6        | 6     |
| Mvmt Flow                  | 146  | 144      | 99    | 8     | 238      | 104   | 231   | 91    | 3     | 77    | 38       | 152   |
| Number of Lanes            | 1    | 1        | 1     | 1     | 1        | 1     | 1     | 1     | 0     | 1     | 1        | 1     |
| Approach                   | EB   |          |       | WB    |          |       | NB    |       |       | SB    |          |       |
| Opposing Approach          | WB   |          |       | EB    |          |       | SB    |       |       | NB    |          |       |
| Opposing Lanes             | 3    |          |       | 3     |          |       | 3     |       |       | 2     |          |       |
| Conflicting Approach Left  | SB   |          |       | NB    |          |       | EB    |       |       | WB    |          |       |
| Conflicting Lanes Left     | 3    |          |       | 2     |          |       | 3     |       |       | 3     |          |       |
| Conflicting Approach Right | NB   |          |       | SB    |          |       | WB    |       |       | EB    |          |       |
| Conflicting Lanes Right    | 2    |          |       | 3     |          |       | 3     |       |       | 3     |          |       |
| HCM Control Delay          | 14.4 |          |       | 17.3  |          |       | 18.1  |       |       | 13.6  |          |       |
| HCM LOS                    | В    |          |       | С     |          |       | С     |       |       | В     |          |       |
|                            |      |          |       |       |          |       |       |       |       |       |          |       |
| Lane                       |      | NBLn1    | NBLn2 | EBLn1 | EBLn2    | EBLn3 | WBLn1 | WBLn2 | WBLn3 | SBLn1 | SBLn2    | SBLn3 |
| Vol Left, %                |      | 100%     | 0%    | 100%  | 0%       | 0%    | 100%  | 0%    | 0%    | 100%  | 0%       | 0%    |
| Vol Thru, %                |      | 0%       | 96%   | 0%    | 100%     | 0%    | 0%    | 100%  | 0%    | 0%    | 100%     | 0%    |
| Vol Right, %               |      | 0%       | 4%    | 0%    | 0%       | 100%  | 0%    | 0%    | 100%  | 0%    | 0%       | 100%  |
| Sign Control               |      | Stop     | Stop  | Stop  | Stop     | Stop  | Stop  | Stop  | Stop  | Stop  | Stop     | Stop  |
| Traffic Vol by Lane        |      | 208      | 85    | 131   | 130      | 89    | 7     | 214   | 94    | 69    | 34       | 137   |
| LT Vol                     |      | 208      | 0     | 131   | 0        | 0     | 7     | 0     | 0     | 69    | 0        | 0     |
| Through Vol                |      | 0        | 82    | 0     | 130      | 0     | 0     | 214   | 0     | 0     | 34       | 0     |
| RT Vol                     |      | 0        | 3     | 0     | 0        | 89    | 0     | 0     | 94    | 0     | 0        | 137   |
|                            |      |          |       |       |          |       |       |       |       |       |          |       |

144

0.322

8.019

Yes

446

5.796

0.323

14.6

В

1.4

8

99

8

0.201

7.305

Yes

490

5.082

0.202

11.9

В

0.7

238

0.533

8.07

Yes

445

5.848

0.535

19.8

C

3.1

8

8

8

0.019

8.579

Yes

416

6.358

0.019

11.5

В

0.1

104

0.213

7.356

Yes

486

5.135

0.214

12.1

В

8.0

8

38

8

0.087

8.322

Yes

429

6.105

0.089

11.9

В

0.3

152

0.322

7.613

Yes

470

5.395

0.323

14

В

1.4

8

77

8

0.188

8.829

Yes

405

6.612

0.19

13.7

В

0.7

Lane Flow Rate

Degree of Util (X)

Convergence, Y/N

HCM Lane V/C Ratio

**HCM Control Delay** 

**HCM Lane LOS** 

HCM 95th-tile Q

Departure Headway (Hd)

Geometry Grp

Service Time

Cap

| Intersection           |         |         |        |        |          |      |        |          |       |        |          |       |       |
|------------------------|---------|---------|--------|--------|----------|------|--------|----------|-------|--------|----------|-------|-------|
| Int Delay, s/veh       | 5.6     |         |        |        |          |      |        |          |       |        |          |       |       |
| Movement               | EBL     | EBT     | EBR    | WBL    | WBT      | WBR  | NBL    | NBT      | NBR   | SBL    | SBT      | SBR   |       |
| Lane Configurations    | ች       | <b></b> | 7      | ች      | <b>†</b> | 7    | ች      | <b>†</b> | 7     | *      | <b>↑</b> | 1     |       |
| Traffic Vol, veh/h     | 46      | 248     | 15     | 40     | 490      | 25   | 45     | 4        | 63    | 39     | 3        | 140   |       |
| Future Vol, veh/h      | 46      | 248     | 15     | 40     | 490      | 25   | 45     | 4        | 63    | 39     | 3        | 140   |       |
| Conflicting Peds, #/hr | 0       | 0       | 1      | 0      | 0        | 0    | 0      | 0        | 0     | 0      | 0        | 0     |       |
| Sign Control           | Free    | Free    | Free   | Free   | Free     | Free | Stop   | Stop     | Stop  | Stop   | Stop     | Stop  |       |
| RT Channelized         | -       | -       | None   | -      | -        | None | -      | -        | None  | _      | -        | None  |       |
| Storage Length         | 320     | -       | 505    | 360    | -        | 195  | 60     | -        | 0     | 100    | -        | 100   |       |
| Veh in Median Storage  | , # -   | 0       | -      | -      | 0        | -    | -      | 0        | -     | -      | 0        | -     |       |
| Grade, %               | _       | 0       | -      | -      | 0        | -    | -      | 0        | -     | -      | 0        | -     |       |
| Peak Hour Factor       | 95      | 95      | 95     | 95     | 95       | 95   | 95     | 95       | 95    | 95     | 95       | 95    |       |
| Heavy Vehicles, %      | 8       | 8       | 8      | 4      | 4        | 4    | 2      | 2        | 2     | 3      | 3        | 3     |       |
| Mvmt Flow              | 48      | 261     | 16     | 42     | 516      | 26   | 47     | 4        | 66    | 41     | 3        | 147   |       |
|                        |         |         |        |        |          |      |        |          |       |        |          |       |       |
| Major/Minor N          | /lajor1 |         |        | Major2 |          | ı    | Minor1 |          |       | Minor2 |          |       |       |
| Conflicting Flow All   | 542     | 0       | 0      | 278    | 0        | 0    | 1046   | 984      | 262   | 1000   | 974      | 516   |       |
| Stage 1                | -       | -       | -      | -      | -        | -    | 358    | 358      | -     | 600    | 600      | -     |       |
| Stage 2                | -       | -       | -      | -      | -        | -    | 688    | 626      | -     | 400    | 374      | -     |       |
| Critical Hdwy          | 4.18    | _       | -      | 4.14   | -        | -    | 7.12   | 6.52     | 6.22  | 7.13   | 6.53     | 6.23  |       |
| Critical Hdwy Stg 1    | -       | -       | -      | -      | -        | -    | 6.12   | 5.52     | -     | 6.13   | 5.53     | -     |       |
| Critical Hdwy Stg 2    | -       | -       | -      | -      | -        | -    | 6.12   | 5.52     | -     | 6.13   | 5.53     | -     |       |
|                        | 2.272   | -       | -      | 2.236  | -        | -    | 3.518  | 4.018    | 3.318 | 3.527  | 4.027    | 3.327 |       |
| Pot Cap-1 Maneuver     | 997     | _       | -      | 1273   | -        | -    | 206    | 248      | 777   | 221    | 251      | 557   |       |
| Stage 1                | -       | -       | -      | -      | -        | -    | 660    | 628      | -     | 486    | 488      | -     |       |
| Stage 2                | -       | -       | -      | -      | -        | -    | 436    | 477      | -     | 624    | 616      | -     |       |
| Platoon blocked, %     |         | -       | -      |        | -        | -    |        |          |       |        |          |       |       |
| Mov Cap-1 Maneuver     | 997     | -       | -      | 1272   | -        | -    | 141    | 228      | 776   | 187    | 231      | 557   |       |
| Mov Cap-2 Maneuver     | -       | -       | -      | -      | -        | -    | 141    | 228      | -     | 187    | 231      | -     |       |
| Stage 1                | -       | -       | -      | -      | -        | -    | 628    | 597      | -     | 463    | 472      | -     |       |
| Stage 2                | -       | -       | -      | -      | -        | -    | 308    | 461      | -     | 539    | 586      | -     |       |
|                        |         |         |        |        |          |      |        |          |       |        |          |       |       |
| Approach               | EB      |         |        | WB     |          |      | NB     |          |       | SB     |          |       |       |
| HCM Control Delay, s   | 1.3     |         |        | 0.6    |          |      | 23.7   |          |       | 17.3   |          |       |       |
| HCM LOS                |         |         |        |        |          |      | С      |          |       | С      |          |       |       |
|                        |         |         |        |        |          |      |        |          |       |        |          |       |       |
| Minor Lane/Major Mvm   | t       | NBLn11  | NBLn21 | NBLn3  | EBL      | EBT  | EBR    | WBL      | WBT   | WBR :  | SBLn1    | SBLn2 | SBLn3 |
| Capacity (veh/h)       |         | 141     | 228    | 776    | 997      | -    |        | 1272     | -     | -      | 187      | 231   | 557   |
| HCM Lane V/C Ratio     |         |         |        | 0.085  |          | _    |        | 0.033    | _     | _      |          | 0.014 |       |
| HCM Control Delay (s)  |         | 42.9    | 21.1   | 10.1   | 8.8      | _    | _      | 7.9      | -     | -      |          | 20.8  | 13.8  |
| HCM Lane LOS           |         | E       | С      | В      | A        | _    | _      | A        | _     | -      | D        | C     | В     |
| HCM 95th %tile Q(veh)  |         | 1.4     | 0.1    | 0.3    | 0.2      | -    | -      | 0.1      | -     | -      | 0.8      | 0     | 1.1   |
|                        |         |         |        |        |          |      |        |          |       |        |          |       |       |

| Intersection           |           |          |         |       |        |          |
|------------------------|-----------|----------|---------|-------|--------|----------|
| Int Delay, s/veh       | 3.7       |          |         |       |        |          |
| Movement               | WBL       | WBR      | NBT     | NBR   | SBL    | SBT      |
|                        |           | WDN      |         | NDN   | SDL    |          |
| Lane Configurations    | <b>\</b>  | 122      | 200     | 20    | 27     | <b>€</b> |
| Traffic Vol, veh/h     | 35        | 132      | 300     | 32    | 37     | 188      |
| Future Vol, veh/h      | 35        | 132      | 300     | 32    | 37     | 188      |
| Conflicting Peds, #/hr | 0         | 0        | _ 0     | _ 1   | _ 1    | _ 0      |
| Sign Control           | Stop      | Stop     | Free    | Free  | Free   | Free     |
| RT Channelized         | -         | None     | -       | None  | -      | None     |
| Storage Length         | 0         | -        | -       | -     | -      | -        |
| Veh in Median Storage  | e, # 0    | -        | 0       | -     | -      | 0        |
| Grade, %               | 0         | -        | 0       | -     | -      | 0        |
| Peak Hour Factor       | 84        | 84       | 84      | 84    | 84     | 84       |
| Heavy Vehicles, %      | 2         | 2        | 7       | 7     | 7      | 7        |
| Mvmt Flow              | 42        | 157      | 357     | 38    | 44     | 224      |
|                        |           |          |         |       |        |          |
|                        |           |          |         |       | _      |          |
|                        | Minor1    |          | //ajor1 |       | Major2 |          |
| Conflicting Flow All   | 689       | 377      | 0       | 0     | 396    | 0        |
| Stage 1                | 377       | -        | -       | -     | -      | -        |
| Stage 2                | 312       | -        | -       | -     | -      | -        |
| Critical Hdwy          | 6.42      | 6.22     | -       | -     | 4.17   | -        |
| Critical Hdwy Stg 1    | 5.42      | -        | -       | -     | _      | -        |
| Critical Hdwy Stg 2    | 5.42      | _        | _       | _     | -      | _        |
| Follow-up Hdwy         |           | 3.318    | _       | _     | 2.263  | _        |
| Pot Cap-1 Maneuver     | 412       | 670      | _       | _     | 1136   | -        |
| Stage 1                | 694       | -        | _       | _     |        | _        |
| Stage 2                | 742       | _        |         |       | _      |          |
| Platoon blocked, %     | 142       | _        |         |       |        | _        |
| •                      | 393       | 669      | -       | -     | 1135   | -        |
| Mov Cap-1 Maneuver     |           |          | -       | -     |        | -        |
| Mov Cap-2 Maneuver     | 393       | -        | -       | -     | -      | -        |
| Stage 1                | 663       | -        | -       | -     | -      | -        |
| Stage 2                | 742       | -        | -       | -     | -      | -        |
|                        |           |          |         |       |        |          |
| Approach               | WB        |          | NB      |       | SB     |          |
| HCM Control Delay, s   | 14.3      |          | 0       |       | 1.4    |          |
| HCM LOS                | 14.3<br>B |          | U       |       | 1.4    |          |
| I IOWI LOS             | Ď         |          |         |       |        |          |
|                        |           |          |         |       |        |          |
| Minor Lane/Major Mvn   | nt        | NBT      | NBRV    | VBLn1 | SBL    | SBT      |
| Capacity (veh/h)       |           | _        | _       | 583   | 1135   | -        |
| HCM Lane V/C Ratio     |           | _        | _       | 0.341 |        | _        |
| HCM Control Delay (s   | )         | _        | _       | 440   | 8.3    | 0        |
| HCM Lane LOS           |           |          |         | В     | Α      | A        |
| HCM 95th %tile Q(veh   | .)        | <u>-</u> |         | 1.5   | 0.1    | -        |
| TION SOUT WITE Q(VEI)  | )         | -        | -       | 1.3   | 0.1    | -        |

|                              | ۶    | <b>→</b> | •     | <b>√</b> | <b>←</b> | •     | 1     | <b>†</b> | <i>&gt;</i> | <b>\</b> | <b></b> | 4    |
|------------------------------|------|----------|-------|----------|----------|-------|-------|----------|-------------|----------|---------|------|
| Movement                     | EBL  | EBT      | EBR   | WBL      | WBT      | WBR   | NBL   | NBT      | NBR         | SBL      | SBT     | SBR  |
| Lane Configurations          | ች    | 1>       |       | ሻ        | 1>       |       | *     | <b>^</b> | 7           | *        | •       | 1    |
| Traffic Volume (veh/h)       | 219  | 181      | 124   | 14       | 336      | 291   | 282   | 393      | 23          | 119      | 161     | 156  |
| Future Volume (veh/h)        | 219  | 181      | 124   | 14       | 336      | 291   | 282   | 393      | 23          | 119      | 161     | 156  |
| Number                       | 7    | 4        | 14    | 3        | 8        | 18    | 5     | 2        | 12          | 1        | 6       | 16   |
| Initial Q (Qb), veh          | 0    | 0        | 0     | 0        | 0        | 0     | 0     | 0        | 0           | 0        | 0       | 0    |
| Ped-Bike Adj(A_pbT)          | 1.00 |          | 1.00  | 1.00     |          | 1.00  | 1.00  |          | 1.00        | 1.00     |         | 1.00 |
| Parking Bus, Adj             | 1.00 | 1.00     | 1.00  | 1.00     | 1.00     | 1.00  | 1.00  | 1.00     | 1.00        | 1.00     | 1.00    | 1.00 |
| Adj Sat Flow, veh/h/ln       | 1776 | 1776     | 1900  | 1863     | 1863     | 1900  | 1863  | 1863     | 1863        | 1827     | 1827    | 1827 |
| Adj Flow Rate, veh/h         | 238  | 197      | 135   | 15       | 365      | 316   | 307   | 427      | 25          | 129      | 175     | 170  |
| Adj No. of Lanes             | 1    | 1        | 0     | 1        | 1        | 0     | 1     | 1        | 1           | 1        | 1       | 1    |
| Peak Hour Factor             | 0.92 | 0.92     | 0.92  | 0.92     | 0.92     | 0.92  | 0.92  | 0.92     | 0.92        | 0.92     | 0.92    | 0.92 |
| Percent Heavy Veh, %         | 7    | 7        | 7     | 2        | 2        | 2     | 2     | 2        | 2           | 4        | 4       | 4    |
| Cap, veh/h                   | 338  | 196      | 135   | 432      | 225      | 194   | 254   | 513      | 436         | 141      | 390     | 331  |
| Arrive On Green              | 0.20 | 0.20     | 0.20  | 0.24     | 0.24     | 0.24  | 0.14  | 0.28     | 0.28        | 0.08     | 0.21    | 0.21 |
| Sat Flow, veh/h              | 1691 | 982      | 673   | 1774     | 923      | 799   | 1774  | 1863     | 1583        | 1740     | 1827    | 1553 |
| Grp Volume(v), veh/h         | 238  | 0        | 332   | 15       | 0        | 681   | 307   | 427      | 25          | 129      | 175     | 170  |
| Grp Sat Flow(s),veh/h/ln     | 1691 | 0        | 1655  | 1774     | 0        | 1722  | 1774  | 1863     | 1583        | 1740     | 1827    | 1553 |
| Q Serve(g_s), s              | 11.8 | 0.0      | 18.0  | 0.6      | 0.0      | 21.9  | 12.9  | 19.4     | 1.0         | 6.6      | 7.5     | 8.7  |
| Cycle Q Clear(g_c), s        | 11.8 | 0.0      | 18.0  | 0.6      | 0.0      | 21.9  | 12.9  | 19.4     | 1.0         | 6.6      | 7.5     | 8.7  |
| Prop In Lane                 | 1.00 |          | 0.41  | 1.00     |          | 0.46  | 1.00  |          | 1.00        | 1.00     |         | 1.00 |
| Lane Grp Cap(c), veh/h       | 338  | 0        | 331   | 432      | 0        | 419   | 254   | 513      | 436         | 141      | 390     | 331  |
| V/C Ratio(X)                 | 0.70 | 0.00     | 1.00  | 0.03     | 0.00     | 1.63  | 1.21  | 0.83     | 0.06        | 0.91     | 0.45    | 0.51 |
| Avail Cap(c_a), veh/h        | 338  | 0        | 331   | 432      | 0        | 419   | 254   | 513      | 436         | 141      | 390     | 331  |
| HCM Platoon Ratio            | 1.00 | 1.00     | 1.00  | 1.00     | 1.00     | 1.00  | 1.00  | 1.00     | 1.00        | 1.00     | 1.00    | 1.00 |
| Upstream Filter(I)           | 1.00 | 0.00     | 1.00  | 1.00     | 0.00     | 1.00  | 1.00  | 1.00     | 1.00        | 1.00     | 1.00    | 1.00 |
| Uniform Delay (d), s/veh     | 33.5 | 0.0      | 36.0  | 26.0     | 0.0      | 34.1  | 38.5  | 30.6     | 24.0        | 41.0     | 30.8    | 31.3 |
| Incr Delay (d2), s/veh       | 6.5  | 0.0      | 50.2  | 0.0      | 0.0      | 292.2 | 124.3 | 14.6     | 0.3         | 50.8     | 3.7     | 5.6  |
| Initial Q Delay(d3),s/veh    | 0.0  | 0.0      | 0.0   | 0.0      | 0.0      | 0.0   | 0.0   | 0.0      | 0.0         | 0.0      | 0.0     | 0.0  |
| %ile BackOfQ(50%),veh/ln     | 6.1  | 0.0      | 12.8  | 0.3      | 0.0      | 44.4  | 15.1  | 12.0     | 0.5         | 5.2      | 4.2     | 4.2  |
| LnGrp Delay(d),s/veh         | 40.0 | 0.0      | 86.2  | 26.0     | 0.0      | 326.3 | 162.8 | 45.2     | 24.2        | 91.8     | 34.5    | 36.9 |
| LnGrp LOS                    | D    |          | F     | С        |          | F     | F     | D        | С           | F        | С       | D    |
| Approach Vol, veh/h          |      | 570      |       |          | 696      |       |       | 759      |             |          | 474     |      |
| Approach Delay, s/veh        |      | 66.9     |       |          | 319.8    |       |       | 92.1     |             |          | 50.9    |      |
| Approach LOS                 |      | E        |       |          | F        |       |       | F        |             |          | D       |      |
| Timer                        | 1    | 2        | 3     | 4        | 5        | 6     | 7     | 8        |             |          |         |      |
| Assigned Phs                 | 1    | 2        |       | 4        | 5        | 6     |       | 8        |             |          |         |      |
| Phs Duration (G+Y+Rc), s     | 11.8 | 29.3     |       | 22.5     | 17.4     | 23.7  |       | 26.4     |             |          |         |      |
| Change Period (Y+Rc), s      | 4.5  | 4.5      |       | 4.5      | 4.5      | 4.5   |       | 4.5      |             |          |         |      |
| Max Green Setting (Gmax), s  | 7.3  | 24.8     |       | 18.0     | 12.9     | 19.2  |       | 21.9     |             |          |         |      |
| Max Q Clear Time (g_c+l1), s | 8.6  | 21.4     |       | 20.0     | 14.9     | 10.7  |       | 23.9     |             |          |         |      |
| Green Ext Time (p_c), s      | 0.0  | 0.9      |       | 0.0      | 0.0      | 1.0   |       | 0.0      |             |          |         |      |
| Intersection Summary         |      |          |       |          |          |       |       |          |             |          |         |      |
| HCM 2010 Ctrl Delay          |      |          | 142.0 |          |          |       |       |          |             |          |         |      |
| HCM 2010 LOS                 |      |          | F     |          |          |       |       |          |             |          |         |      |

|                              | •    | <b>→</b> | •    | •    | <b>←</b> | •    | 1    | <b>†</b> | <b>/</b> | <b>/</b> | <b></b> | 4    |
|------------------------------|------|----------|------|------|----------|------|------|----------|----------|----------|---------|------|
| Movement                     | EBL  | EBT      | EBR  | WBL  | WBT      | WBR  | NBL  | NBT      | NBR      | SBL      | SBT     | SBR  |
| Lane Configurations          | J.   | ĵ»       |      | ¥    | ĵ»       |      |      | 4        |          |          | 4       |      |
| Traffic Volume (veh/h)       | 6    | 328      | 118  | 91   | 700      | 19   | 207  | 68       | 160      | 18       | 24      | 12   |
| Future Volume (veh/h)        | 6    | 328      | 118  | 91   | 700      | 19   | 207  | 68       | 160      | 18       | 24      | 12   |
| Number                       | 7    | 4        | 14   | 3    | 8        | 18   | 5    | 2        | 12       | 1        | 6       | 16   |
| Initial Q (Qb), veh          | 0    | 0        | 0    | 0    | 0        | 0    | 0    | 0        | 0        | 0        | 0       | 0    |
| Ped-Bike Adj(A_pbT)          | 1.00 |          | 1.00 | 1.00 |          | 1.00 | 1.00 |          | 1.00     | 1.00     |         | 1.00 |
| Parking Bus, Adj             | 1.00 | 1.00     | 1.00 | 1.00 | 1.00     | 1.00 | 1.00 | 1.00     | 1.00     | 1.00     | 1.00    | 1.00 |
| Adj Sat Flow, veh/h/ln       | 1827 | 1827     | 1900 | 1845 | 1845     | 1900 | 1900 | 1810     | 1900     | 1900     | 1776    | 1900 |
| Adj Flow Rate, veh/h         | 7    | 373      | 134  | 103  | 795      | 22   | 235  | 77       | 182      | 20       | 27      | 14   |
| Adj No. of Lanes             | 1    | 1        | 0    | 1    | 1        | 0    | 0    | 1        | 0        | 0        | 1       | 0    |
| Peak Hour Factor             | 0.88 | 0.88     | 0.88 | 0.88 | 0.88     | 0.88 | 0.88 | 0.88     | 0.88     | 0.88     | 0.88    | 0.88 |
| Percent Heavy Veh, %         | 4    | 4        | 4    | 3    | 3        | 3    | 5    | 5        | 5        | 7        | 7       | 7    |
| Cap, veh/h                   | 16   | 500      | 179  | 132  | 813      | 22   | 302  | 78       | 171      | 188      | 235     | 102  |
| Arrive On Green              | 0.01 | 0.39     | 0.39 | 0.07 | 0.45     | 0.45 | 0.31 | 0.31     | 0.31     | 0.31     | 0.31    | 0.31 |
| Sat Flow, veh/h              | 1740 | 1284     | 461  | 1757 | 1786     | 49   | 685  | 251      | 546      | 349      | 750     | 327  |
| Grp Volume(v), veh/h         | 7    | 0        | 507  | 103  | 0        | 817  | 494  | 0        | 0        | 61       | 0       | 0    |
| Grp Sat Flow(s),veh/h/ln     | 1740 | 0        | 1746 | 1757 | 0        | 1836 | 1482 | 0        | 0        | 1427     | 0       | 0    |
| Q Serve(g_s), s              | 0.2  | 0.0      | 15.1 | 3.5  | 0.0      | 26.4 | 17.4 | 0.0      | 0.0      | 0.0      | 0.0     | 0.0  |
| Cycle Q Clear(g_c), s        | 0.2  | 0.0      | 15.1 | 3.5  | 0.0      | 26.4 | 18.9 | 0.0      | 0.0      | 1.5      | 0.0     | 0.0  |
| Prop In Lane                 | 1.00 |          | 0.26 | 1.00 |          | 0.03 | 0.48 |          | 0.37     | 0.33     |         | 0.23 |
| Lane Grp Cap(c), veh/h       | 16   | 0        | 679  | 132  | 0        | 835  | 551  | 0        | 0        | 525      | 0       | 0    |
| V/C Ratio(X)                 | 0.44 | 0.00     | 0.75 | 0.78 | 0.00     | 0.98 | 0.90 | 0.00     | 0.00     | 0.12     | 0.00    | 0.00 |
| Avail Cap(c_a), veh/h        | 147  | 0        | 742  | 201  | 0        | 835  | 551  | 0        | 0        | 525      | 0       | 0    |
| HCM Platoon Ratio            | 1.00 | 1.00     | 1.00 | 1.00 | 1.00     | 1.00 | 1.00 | 1.00     | 1.00     | 1.00     | 1.00    | 1.00 |
| Upstream Filter(I)           | 1.00 | 0.00     | 1.00 | 1.00 | 0.00     | 1.00 | 1.00 | 0.00     | 0.00     | 1.00     | 0.00    | 0.00 |
| Uniform Delay (d), s/veh     | 29.8 | 0.0      | 15.9 | 27.5 | 0.0      | 16.2 | 21.2 | 0.0      | 0.0      | 14.8     | 0.0     | 0.0  |
| Incr Delay (d2), s/veh       | 17.8 | 0.0      | 3.8  | 10.5 | 0.0      | 25.8 | 19.8 | 0.0      | 0.0      | 0.4      | 0.0     | 0.0  |
| Initial Q Delay(d3),s/veh    | 0.0  | 0.0      | 0.0  | 0.0  | 0.0      | 0.0  | 0.0  | 0.0      | 0.0      | 0.0      | 0.0     | 0.0  |
| %ile BackOfQ(50%),veh/ln     | 0.2  | 0.0      | 7.9  | 2.1  | 0.0      | 19.1 | 11.1 | 0.0      | 0.0      | 8.0      | 0.0     | 0.0  |
| LnGrp Delay(d),s/veh         | 47.6 | 0.0      | 19.7 | 38.0 | 0.0      | 42.0 | 41.0 | 0.0      | 0.0      | 15.3     | 0.0     | 0.0  |
| LnGrp LOS                    | D    |          | В    | D    |          | D    | D    |          |          | В        |         |      |
| Approach Vol, veh/h          |      | 514      |      |      | 920      |      |      | 494      |          |          | 61      |      |
| Approach Delay, s/veh        |      | 20.1     |      |      | 41.5     |      |      | 41.0     |          |          | 15.3    |      |
| Approach LOS                 |      | С        |      |      | D        |      |      | D        |          |          | В       |      |
| Timer                        | 1    | 2        | 3    | 4    | 5        | 6    | 7    | 8        |          |          |         |      |
| Assigned Phs                 |      | 2        | 3    | 4    |          | 6    | 7    | 8        |          |          |         |      |
| Phs Duration (G+Y+Rc), s     |      | 23.4     | 9.0  | 28.0 |          | 23.4 | 5.1  | 32.0     |          |          |         |      |
| Change Period (Y+Rc), s      |      | 4.5      | 4.5  | 4.5  |          | 4.5  | 4.5  | 4.5      |          |          |         |      |
| Max Green Setting (Gmax), s  |      | 18.9     | 6.9  | 25.7 |          | 18.9 | 5.1  | 27.5     |          |          |         |      |
| Max Q Clear Time (g_c+l1), s |      | 20.9     | 5.5  | 17.1 |          | 3.5  | 2.2  | 28.4     |          |          |         |      |
| Green Ext Time (p_c), s      |      | 0.0      | 0.0  | 2.2  |          | 0.2  | 0.0  | 0.0      |          |          |         |      |
| Intersection Summary         |      |          |      |      |          |      |      |          |          |          |         |      |
| HCM 2010 Ctrl Delay          |      |          | 35.1 |      |          |      |      |          |          |          |         |      |
| HCM 2010 LOS                 |      |          | D    |      |          |      |      |          |          |          |         |      |

|                              | ۶         | <b>→</b>  | <b>←</b>  | •         | <b>\</b>  | 4         |      |      |  |  |
|------------------------------|-----------|-----------|-----------|-----------|-----------|-----------|------|------|--|--|
| Movement                     | EBL       | EBT       | WBT       | WBR       | SBL       | SBR       |      |      |  |  |
| Lane Configurations          | *         | <b>1</b>  | <b></b>   | 7         | ች         | 7         |      |      |  |  |
| Traffic Volume (veh/h)       | 184       | 266       | 546       | 384       | 190       | 210       |      |      |  |  |
| Future Volume (veh/h)        | 184       | 266       | 546       | 384       | 190       | 210       |      |      |  |  |
| Number                       | 7         | 4         | 8         | 18        | 1         | 16        |      |      |  |  |
| Initial Q (Qb), veh          | 0         | 0         | 0         | 0         | 0         | 0         |      |      |  |  |
| Ped-Bike Adj(A_pbT)          | 1.00      |           |           | 1.00      | 1.00      | 1.00      |      |      |  |  |
| Parking Bus, Adj             | 1.00      | 1.00      | 1.00      | 1.00      | 1.00      | 1.00      |      |      |  |  |
| Adj Sat Flow, veh/h/ln       | 1810      | 1810      | 1863      | 1863      | 1863      | 1863      |      |      |  |  |
| Adj Flow Rate, veh/h         | 209       | 302       | 620       | 436       | 216       | 239       |      |      |  |  |
| Adj No. of Lanes             | 1         | 1         | 1         | 1         | 1         | 1         |      |      |  |  |
| Peak Hour Factor             | 0.88      | 0.88      | 0.88      | 0.88      | 0.88      | 0.88      |      |      |  |  |
| Percent Heavy Veh, %         | 5         | 5         | 2         | 2         | 2         | 2         |      |      |  |  |
| Cap, veh/h                   | 258       | 1085      | 688       | 585       | 426       | 381       |      |      |  |  |
| Arrive On Green              | 0.15      | 0.60      | 0.37      | 0.37      | 0.24      | 0.24      |      |      |  |  |
| Sat Flow, veh/h              | 1723      | 1810      | 1863      | 1583      | 1774      | 1583      |      |      |  |  |
| Grp Volume(v), veh/h         | 209       | 302       | 620       | 436       | 216       | 239       |      |      |  |  |
| Grp Sat Flow(s), veh/h/ln    | 1723      | 1810      | 1863      | 1583      | 1774      | 1583      |      |      |  |  |
| Q Serve(g_s), s              | 6.6       | 4.5       | 17.7      | 13.5      | 5.9       | 7.6       |      |      |  |  |
| Cycle Q Clear(g_c), s        | 6.6       | 4.5       | 17.7      | 13.5      | 5.9       | 7.6       |      |      |  |  |
| Prop In Lane                 | 1.00      | 7.0       | 17.7      | 1.00      | 1.00      | 1.00      |      |      |  |  |
| Lane Grp Cap(c), veh/h       | 258       | 1085      | 688       | 585       | 426       | 381       |      |      |  |  |
| V/C Ratio(X)                 | 0.81      | 0.28      | 0.90      | 0.75      | 0.51      | 0.63      |      |      |  |  |
| Avail Cap(c_a), veh/h        | 353       | 1208      | 713       | 606       | 426       | 381       |      |      |  |  |
| HCM Platoon Ratio            | 1.00      | 1.00      | 1.00      | 1.00      | 1.00      | 1.00      |      |      |  |  |
| Upstream Filter(I)           | 1.00      | 1.00      | 1.00      | 1.00      | 1.00      | 1.00      |      |      |  |  |
| Uniform Delay (d), s/veh     | 23.1      | 5.4       | 16.7      | 15.4      | 18.4      | 19.1      |      |      |  |  |
| Incr Delay (d2), s/veh       | 9.6       | 0.1       | 14.3      | 4.8       | 4.2       | 7.6       |      |      |  |  |
| Initial Q Delay(d3),s/veh    | 0.0       | 0.0       | 0.0       | 0.0       | 0.0       | 0.0       |      |      |  |  |
| %ile BackOfQ(50%),veh/ln     | 3.8       | 2.2       | 11.7      | 6.6       | 3.4       | 7.4       |      |      |  |  |
| LnGrp Delay(d),s/veh         | 32.7      | 5.5       | 31.1      | 20.3      | 22.7      | 26.7      |      |      |  |  |
| _nGrp LOS                    | 32.7<br>C | 3.5<br>A  | 31.1<br>C | 20.3<br>C | 22.7<br>C | 20.7<br>C |      |      |  |  |
| Approach Vol, veh/h          |           | 511       | 1056      | U         | 455       |           |      |      |  |  |
|                              |           | 16.6      | 26.6      |           | 24.8      |           |      |      |  |  |
| Approach LOS                 |           | 16.6<br>B | 26.6<br>C |           | 24.8<br>C |           |      |      |  |  |
| Approach LOS<br>             |           |           |           |           |           |           |      |      |  |  |
| Timer                        | 1         | 2         | 3         | 4         | 5         | 6         | 7    | 8    |  |  |
| Assigned Phs                 |           |           |           | 4         |           | 6         | 7    | 8    |  |  |
| Phs Duration (G+Y+Rc), s     |           |           |           | 38.2      |           | 18.0      | 12.9 | 25.2 |  |  |
| Change Period (Y+Rc), s      |           |           |           | 4.5       |           | 4.5       | 4.5  | 4.5  |  |  |
| Max Green Setting (Gmax), s  |           |           |           | 37.5      |           | 13.5      | 11.5 | 21.5 |  |  |
| Max Q Clear Time (g_c+I1), s |           |           |           | 6.5       |           | 9.6       | 8.6  | 19.7 |  |  |
| Green Ext Time (p_c), s      |           |           |           | 1.9       |           | 0.6       | 0.2  | 1.1  |  |  |
| ntersection Summary          |           |           |           |           |           |           |      |      |  |  |
| HCM 2010 Ctrl Delay          |           |           | 23.7      |           |           |           |      |      |  |  |
| HCM 2010 LOS                 |           |           | С         |           |           |           |      |      |  |  |

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|-------------------------------|-------------|------|--------|-------|------------|------------|---------|--------|------|----------|----------|------|
| Movement                      | EBL         | EBT  | EBR    | WBL   | WBT        | WBR        | NBL     | NBT    | NBR  | SBL      | SBT      | SBR  |
| Lane Configurations           | ሻ           |      | 7      | ሻ     | ₽          |            |         | र्स    | 7    |          | र्स      | 7    |
| Traffic Volume (vph)          | 11          | 537  | 383    | 67    | 767        | 28         | 762     | 25     | 64   | 46       | 23       | 5    |
| Future Volume (vph)           | 11          | 537  | 383    | 67    | 767        | 28         | 762     | 25     | 64   | 46       | 23       | 5    |
| Ideal Flow (vphpl)            | 1900        | 1900 | 1900   | 1900  | 1900       | 1900       | 1900    | 1900   | 1900 | 1900     | 1900     | 1900 |
| Total Lost time (s)           | 4.5         | 4.5  | 4.5    | 4.5   | 4.5        |            |         | 4.5    | 4.5  |          | 4.5      | 4.5  |
| Lane Util. Factor             | 1.00        | 1.00 | 1.00   | 1.00  | 1.00       |            |         | 1.00   | 1.00 |          | 1.00     | 1.00 |
| Frt                           | 1.00        | 1.00 | 0.85   | 1.00  | 0.99       |            |         | 1.00   | 0.85 |          | 1.00     | 0.85 |
| Flt Protected                 | 0.95        | 1.00 | 1.00   | 0.95  | 1.00       |            |         | 0.95   | 1.00 |          | 0.97     | 1.00 |
| Satd. Flow (prot)             | 1612        | 1696 | 1442   | 1543  | 1615       |            |         | 1777   | 1583 |          | 1751     | 1538 |
| Flt Permitted                 | 0.95        | 1.00 | 1.00   | 0.95  | 1.00       |            |         | 0.95   | 1.00 |          | 0.97     | 1.00 |
| Satd. Flow (perm)             | 1612        | 1696 | 1442   | 1543  | 1615       |            |         | 1777   | 1583 |          | 1751     | 1538 |
| Peak-hour factor, PHF         | 0.96        | 0.96 | 0.96   | 0.96  | 0.96       | 0.96       | 0.96    | 0.96   | 0.96 | 0.96     | 0.96     | 0.96 |
| Adj. Flow (vph)               | 11          | 559  | 399    | 70    | 799        | 29         | 794     | 26     | 67   | 48       | 24       | 5    |
| RTOR Reduction (vph)          | 0           | 0    | 219    | 0     | 1          | 0          | 0       | 0      | 46   | 0        | 0        | 5    |
| Lane Group Flow (vph)         | 11          | 559  | 180    | 70    | 827        | 0          | 0       | 820    | 21   | 0        | 72       | 0    |
| Heavy Vehicles (%)            | 12%         | 12%  | 12%    | 17%   | 17%        | 17%        | 2%      | 2%     | 2%   | 5%       | 5%       | 5%   |
| Turn Type                     | Prot        | NA   | Perm   | Prot  | NA         |            | Split   | NA     | Perm | Split    | NA       | Perm |
| Protected Phases              | 7           | 4    |        | 3     | 8          |            | 5       | 5      |      | 6        | 6        |      |
| Permitted Phases              | •           | •    | 4      | -     |            |            |         |        | 5    | •        | -        | 6    |
| Actuated Green, G (s)         | 1.0         | 55.2 | 55.2   | 5.0   | 59.2       |            |         | 38.6   | 38.6 |          | 5.5      | 5.5  |
| Effective Green, g (s)        | 1.0         | 55.2 | 55.2   | 5.0   | 59.2       |            |         | 38.6   | 38.6 |          | 5.5      | 5.5  |
| Actuated g/C Ratio            | 0.01        | 0.45 | 0.45   | 0.04  | 0.48       |            |         | 0.32   | 0.32 |          | 0.04     | 0.04 |
| Clearance Time (s)            | 4.5         | 4.5  | 4.5    | 4.5   | 4.5        |            |         | 4.5    | 4.5  |          | 4.5      | 4.5  |
| Vehicle Extension (s)         | 3.0         | 3.0  | 3.0    | 3.0   | 3.0        |            |         | 3.0    | 3.0  |          | 3.0      | 3.0  |
| Lane Grp Cap (vph)            | 13          | 765  | 650    | 63    | 781        |            |         | 560    | 499  |          | 78       | 69   |
| v/s Ratio Prot                | 0.01        | 0.33 |        | c0.05 | c0.51      |            |         | c0.46  |      |          | c0.04    |      |
| v/s Ratio Perm                | 0.0.        | 0.00 | 0.12   | 00.00 |            |            |         | 001.10 | 0.01 |          |          | 0.00 |
| v/c Ratio                     | 0.85        | 0.73 | 0.28   | 1.11  | 1.06       |            |         | 1.46   | 0.04 |          | 0.92     | 0.00 |
| Uniform Delay, d1             | 60.6        | 27.5 | 21.0   | 58.6  | 31.5       |            |         | 41.8   | 29.0 |          | 58.2     | 55.8 |
| Progression Factor            | 1.00        | 1.00 | 1.00   | 1.00  | 1.00       |            |         | 1.00   | 1.00 |          | 1.00     | 1.00 |
| Incremental Delay, d2         | 166.4       | 6.1  | 1.1    | 147.1 | 48.9       |            |         | 218.6  | 0.0  |          | 75.7     | 0.0  |
| Delay (s)                     | 227.0       | 33.5 | 22.1   | 205.8 | 80.5       |            |         | 260.5  | 29.1 |          | 133.9    | 55.8 |
| Level of Service              | F           | С    | С      | F     | F          |            |         | F      | С    |          | F        | E    |
| Approach Delay (s)            |             | 31.0 |        |       | 90.2       |            |         | 243.0  |      |          | 128.9    |      |
| Approach LOS                  |             | С    |        |       | F          |            |         | F      |      |          | F        |      |
| Intersection Summary          |             |      |        |       |            |            |         |        |      |          |          |      |
| HCM 2000 Control Delay        |             |      | 118.9  | Н     | CM 2000    | Level of   | Service |        | F    |          |          |      |
| HCM 2000 Volume to Capa       | acity ratio |      | 1.22   |       |            |            |         |        |      |          |          |      |
| Actuated Cycle Length (s)     |             |      | 122.3  | S     | um of lost | t time (s) |         |        | 18.0 |          |          |      |
| Intersection Capacity Utiliza | ation       |      | 107.7% | IC    | CU Level   | of Service |         |        | G    |          |          |      |
| Analysis Period (min)         |             |      | 15     |       |            |            |         |        |      |          |          |      |
| c Critical Lane Group         |             |      |        |       |            |            |         |        |      |          |          |      |

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|------------------------------|------|----------|------|-------|----------|------|------|-----------------|------|----------|------------|------|
| Movement                     | EBL  | EBT      | EBR  | WBL   | WBT      | WBR  | NBL  | NBT             | NBR  | SBL      | SBT        | SBR  |
| Lane Configurations          | 1,4  | <b>^</b> | 7    | ሻ     | <b>^</b> | 7    | ሻሻ   | ተተ <sub>ጉ</sub> |      | ሻሻ       | <b>^</b> ^ | 7    |
| Traffic Volume (veh/h)       | 256  | 256      | 125  | 149   | 469      | 364  | 193  | 831             | 66   | 238      | 528        | 192  |
| Future Volume (veh/h)        | 256  | 256      | 125  | 149   | 469      | 364  | 193  | 831             | 66   | 238      | 528        | 192  |
| Number                       | 7    | 4        | 14   | 3     | 8        | 18   | 5    | 2               | 12   | 1        | 6          | 16   |
| Initial Q (Qb), veh          | 0    | 0        | 0    | 0     | 0        | 0    | 0    | 0               | 0    | 0        | 0          | 0    |
| Ped-Bike Adj(A_pbT)          | 1.00 |          | 0.98 | 1.00  |          | 0.97 | 1.00 |                 | 1.00 | 1.00     |            | 1.00 |
| Parking Bus, Adj             | 1.00 | 1.00     | 1.00 | 1.00  | 1.00     | 1.00 | 1.00 | 1.00            | 1.00 | 1.00     | 1.00       | 1.00 |
| Adj Sat Flow, veh/h/ln       | 1863 | 1863     | 1863 | 1863  | 1863     | 1863 | 1863 | 1863            | 1900 | 1845     | 1845       | 1845 |
| Adj Flow Rate, veh/h         | 281  | 281      | 137  | 164   | 515      | 400  | 212  | 913             | 73   | 262      | 580        | 211  |
| Adj No. of Lanes             | 2    | 2        | 1    | 1     | 2        | 1    | 2    | 3               | 0    | 2        | 3          | 1    |
| Peak Hour Factor             | 0.91 | 0.91     | 0.91 | 0.91  | 0.91     | 0.91 | 0.91 | 0.91            | 0.91 | 0.91     | 0.91       | 0.91 |
| Percent Heavy Veh, %         | 2    | 2        | 2    | 2     | 2        | 2    | 2    | 2               | 2    | 3        | 3          | 3    |
| Cap, veh/h                   | 286  | 980      | 554  | 150   | 986      | 428  | 265  | 1367            | 109  | 262      | 1433       | 575  |
| Arrive On Green              | 0.08 | 0.28     | 0.28 | 0.08  | 0.28     | 0.28 | 0.08 | 0.28            | 0.28 | 0.08     | 0.28       | 0.28 |
| Sat Flow, veh/h              | 3442 | 3539     | 1559 | 1774  | 3539     | 1536 | 3442 | 4802            | 383  | 3408     | 5036       | 1561 |
| Grp Volume(v), veh/h         | 281  | 281      | 137  | 164   | 515      | 400  | 212  | 644             | 342  | 262      | 580        | 211  |
| Grp Sat Flow(s),veh/h/ln     | 1721 | 1770     | 1559 | 1774  | 1770     | 1536 | 1721 | 1695            | 1794 | 1704     | 1679       | 1561 |
| Q Serve(g_s), s              | 5.3  | 4.1      | 4.0  | 5.5   | 8.0      | 16.5 | 3.9  | 10.9            | 11.0 | 5.0      | 6.1        | 6.4  |
| Cycle Q Clear(g_c), s        | 5.3  | 4.1      | 4.0  | 5.5   | 8.0      | 16.5 | 3.9  | 10.9            | 11.0 | 5.0      | 6.1        | 6.4  |
| Prop In Lane                 | 1.00 |          | 1.00 | 1.00  |          | 1.00 | 1.00 |                 | 0.21 | 1.00     |            | 1.00 |
| Lane Grp Cap(c), veh/h       | 286  | 980      | 554  | 150   | 986      | 428  | 265  | 965             | 511  | 262      | 1433       | 575  |
| V/C Ratio(X)                 | 0.98 | 0.29     | 0.25 | 1.09  | 0.52     | 0.94 | 0.80 | 0.67            | 0.67 | 1.00     | 0.40       | 0.37 |
| Avail Cap(c_a), veh/h        | 286  | 980      | 554  | 150   | 986      | 428  | 265  | 965             | 511  | 262      | 1433       | 575  |
| HCM Platoon Ratio            | 1.00 | 1.00     | 1.00 | 1.00  | 1.00     | 1.00 | 1.00 | 1.00            | 1.00 | 1.00     | 1.00       | 1.00 |
| Upstream Filter(I)           | 1.00 | 1.00     | 1.00 | 1.00  | 1.00     | 1.00 | 1.00 | 1.00            | 1.00 | 1.00     | 1.00       | 1.00 |
| Uniform Delay (d), s/veh     | 29.8 | 18.5     | 14.9 | 29.7  | 19.8     | 22.9 | 29.5 | 20.5            | 20.6 | 30.0     | 18.8       | 15.0 |
| Incr Delay (d2), s/veh       | 48.3 | 0.2      | 0.2  | 100.4 | 0.5      | 27.9 | 16.0 | 3.7             | 6.8  | 55.4     | 0.9        | 1.8  |
| Initial Q Delay(d3),s/veh    | 0.0  | 0.0      | 0.0  | 0.0   | 0.0      | 0.0  | 0.0  | 0.0             | 0.0  | 0.0      | 0.0        | 0.0  |
| %ile BackOfQ(50%),veh/ln     | 4.4  | 2.0      | 1.7  | 6.9   | 3.9      | 10.3 | 2.4  | 5.6             | 6.4  | 4.3      | 2.9        | 3.0  |
| LnGrp Delay(d),s/veh         | 78.1 | 18.6     | 15.1 | 130.1 | 20.3     | 50.8 | 45.5 | 24.2            | 27.4 | 85.4     | 19.6       | 16.8 |
| LnGrp LOS                    | Ε    | В        | В    | F     | С        | D    | D    | С               | С    | F        | В          | В    |
| Approach Vol, veh/h          |      | 699      |      |       | 1079     |      |      | 1198            |      |          | 1053       |      |
| Approach Delay, s/veh        |      | 41.8     |      |       | 48.3     |      |      | 28.9            |      |          | 35.4       |      |
| Approach LOS                 |      | D        |      |       | D        |      |      | С               |      |          | D          |      |
| Timer                        | 1    | 2        | 3    | 4     | 5        | 6    | 7    | 8               |      |          |            |      |
| Assigned Phs                 | 1    | 2        | 3    | 4     | 5        | 6    | 7    | 8               |      |          |            |      |
| Phs Duration (G+Y+Rc), s     | 9.5  | 23.0     | 10.0 | 22.5  | 9.5      | 23.0 | 9.9  | 22.6            |      |          |            |      |
| Change Period (Y+Rc), s      | 4.5  | 4.5      | 4.5  | 4.5   | 4.5      | 4.5  | 4.5  | 4.5             |      |          |            |      |
| Max Green Setting (Gmax), s  | 5.0  | 18.5     | 5.5  | 18.0  | 5.0      | 18.5 | 5.4  | 18.1            |      |          |            |      |
| Max Q Clear Time (g_c+l1), s | 7.0  | 13.0     | 7.5  | 6.1   | 5.9      | 8.4  | 7.3  | 18.5            |      |          |            |      |
| Green Ext Time (p_c), s      | 0.0  | 3.0      | 0.0  | 1.8   | 0.0      | 3.4  | 0.0  | 0.0             |      |          |            |      |
| Intersection Summary         |      |          |      |       |          |      |      |                 |      |          |            |      |
| HCM 2010 Ctrl Delay          |      |          | 38.0 |       |          |      |      |                 |      |          |            |      |
| HCM 2010 LOS                 |      |          | D    |       |          |      |      |                 |      |          |            |      |
|                              |      |          |      |       |          |      |      |                 |      |          |            |      |

|                              | _    |      |      |          |      |      |      |          |      |       |      |          |
|------------------------------|------|------|------|----------|------|------|------|----------|------|-------|------|----------|
|                              | •    | -    | •    | •        | •    | _    |      | T        |      | -     | ¥    | *        |
| Movement                     | EBL  | EBT  | EBR  | WBL      | WBT  | WBR  | NBL  | NBT      | NBR  | SBL   | SBT  | SBR      |
| Lane Configurations          | 7    | ₽    |      | ሻ        | 1>   |      | 7    | <b>↑</b> | 7    | ሻ     | ₽    |          |
| Traffic Volume (veh/h)       | 38   | 153  | 42   | 158      | 156  | 263  | 75   | 190      | 179  | 144   | 93   | 14       |
| Future Volume (veh/h)        | 38   | 153  | 42   | 158      | 156  | 263  | 75   | 190      | 179  | 144   | 93   | 14       |
| Number                       | 7    | 4    | 14   | 3        | 8    | 18   | 5    | 2        | 12   | 1     | 6    | 16       |
| Initial Q (Qb), veh          | 0    | 0    | 0    | 0        | 0    | 0    | 0    | 0        | 0    | 0     | 0    | 0        |
| Ped-Bike Adj(A_pbT)          | 1.00 |      | 0.74 | 1.00     |      | 0.89 | 1.00 |          | 0.99 | 1.00  |      | 0.99     |
| Parking Bus, Adj             | 1.00 | 1.00 | 1.00 | 1.00     | 1.00 | 1.00 | 1.00 | 1.00     | 1.00 | 1.00  | 1.00 | 1.00     |
| Adj Sat Flow, veh/h/ln       | 1863 | 1863 | 1900 | 1863     | 1863 | 1900 | 1863 | 1863     | 1863 | 1863  | 1863 | 1900     |
| Adj Flow Rate, veh/h         | 50   | 201  | 55   | 208      | 205  | 346  | 99   | 250      | 236  | 189   | 122  | 18       |
| Adj No. of Lanes             | 1    | 1    | 0    | 1        | 1    | 0    | 1    | 1        | 1    | 1     | 1    | 0        |
| Peak Hour Factor             | 0.76 | 0.76 | 0.76 | 0.76     | 0.76 | 0.76 | 0.76 | 0.76     | 0.76 | 0.76  | 0.76 | 0.76     |
| Percent Heavy Veh, %         | 2    | 2    | 2    | 2        | 2    | 2    | 2    | 2        | 2    | 2     | 2    | 2        |
| Cap, veh/h                   | 79   | 323  | 88   | 236      | 194  | 327  | 127  | 492      | 416  | 166   | 454  | 67       |
| Arrive On Green              | 0.04 | 0.25 | 0.25 | 0.13     | 0.34 | 0.34 | 0.07 | 0.26     | 0.26 | 0.09  | 0.29 | 0.29     |
| Sat Flow, veh/h              | 1774 | 1296 | 355  | 1774     | 575  | 970  | 1774 | 1863     | 1574 | 1774  | 1584 | 234      |
| Grp Volume(v), veh/h         | 50   | 0    | 256  | 208      | 0    | 551  | 99   | 250      | 236  | 189   | 0    | 140      |
| Grp Sat Flow(s),veh/h/ln     | 1774 | 0    | 1650 | 1774     | 0    | 1545 | 1774 | 1863     | 1574 | 1774  | 0    | 1818     |
| Q Serve(g_s), s              | 1.9  | 0.0  | 9.5  | 8.0      | 0.0  | 23.4 | 3.8  | 7.9      | 9.0  | 6.5   | 0.0  | 4.1      |
| Cycle Q Clear(g_c), s        | 1.9  | 0.0  | 9.5  | 8.0      | 0.0  | 23.4 | 3.8  | 7.9      | 9.0  | 6.5   | 0.0  | 4.1      |
| Prop In Lane                 | 1.00 |      | 0.21 | 1.00     |      | 0.63 | 1.00 |          | 1.00 | 1.00  |      | 0.13     |
| Lane Grp Cap(c), veh/h       | 79   | 0    | 411  | 236      | 0    | 521  | 127  | 492      | 416  | 166   | 0    | 521      |
| V/C Ratio(X)                 | 0.63 | 0.00 | 0.62 | 0.88     | 0.00 | 1.06 | 0.78 | 0.51     | 0.57 | 1.14  | 0.00 | 0.27     |
| Avail Cap(c_a), veh/h        | 131  | 0    | 429  | 236      | 0    | 521  | 159  | 492      | 416  | 166   | 0    | 521      |
| HCM Platoon Ratio            | 1.00 | 1.00 | 1.00 | 1.00     | 1.00 | 1.00 | 1.00 | 1.00     | 1.00 | 1.00  | 1.00 | 1.00     |
| Upstream Filter(I)           | 1.00 | 0.00 | 1.00 | 1.00     | 0.00 | 1.00 | 1.00 | 1.00     | 1.00 | 1.00  | 0.00 | 1.00     |
| Uniform Delay (d), s/veh     | 32.5 | 0.0  | 23.1 | 29.5     | 0.0  | 22.9 | 31.6 | 21.7     | 22.1 | 31.4  | 0.0  | 19.1     |
| Incr Delay (d2), s/veh       | 8.0  | 0.0  | 2.6  | 30.0     | 0.0  | 55.3 | 17.7 | 3.7      | 5.5  | 110.8 | 0.0  | 1.3      |
| Initial Q Delay(d3),s/veh    | 0.0  | 0.0  | 0.0  | 0.0      | 0.0  | 0.0  | 0.0  | 0.0      | 0.0  | 0.0   | 0.0  | 0.0      |
| %ile BackOfQ(50%),veh/ln     | 1.1  | 0.0  | 4.6  | 5.8      | 0.0  | 17.9 | 2.5  | 4.5      | 4.5  | 8.3   | 0.0  | 2.2      |
| LnGrp Delay(d),s/veh         | 40.6 | 0.0  | 25.7 | 59.5     | 0.0  | 78.2 | 49.3 | 25.4     | 27.6 | 142.2 | 0.0  | 20.4     |
| LnGrp LOS                    | D    |      | С    | <u>E</u> |      | F    | D    | С        | С    | F     |      | <u>C</u> |
| Approach Vol, veh/h          |      | 306  |      |          | 759  |      |      | 585      |      |       | 329  |          |
| Approach Delay, s/veh        |      | 28.1 |      |          | 73.1 |      |      | 30.3     |      |       | 90.3 |          |
| Approach LOS                 |      | С    |      |          | Е    |      |      | С        |      |       | F    |          |
| Timer                        | 1    | 2    | 3    | 4        | 5    | 6    | 7    | 8        |      |       |      |          |
| Assigned Phs                 | 1    | 2    | 3    | 4        | 5    | 6    | 7    | 8        |      |       |      |          |
| Phs Duration (G+Y+Rc), s     | 11.0 | 22.8 | 13.7 | 21.8     | 9.4  | 24.4 | 7.6  | 27.9     |      |       |      |          |
| Change Period (Y+Rc), s      | 4.5  | 4.5  | 4.5  | 4.5      | 4.5  | 4.5  | 4.5  | 4.5      |      |       |      |          |
| Max Green Setting (Gmax), s  | 6.5  | 18.3 | 9.2  | 18.0     | 6.2  | 18.6 | 5.1  | 22.1     |      |       |      |          |
| Max Q Clear Time (g_c+l1), s | 8.5  | 11.0 | 10.0 | 11.5     | 5.8  | 6.1  | 3.9  | 25.4     |      |       |      |          |
| Green Ext Time (p_c), s      | 0.0  | 1.4  | 0.0  | 0.8      | 0.0  | 0.5  | 0.0  | 0.0      |      |       |      |          |
| Intersection Summary         |      |      |      |          |      |      |      |          |      |       |      |          |
| HCM 2010 Ctrl Delay          |      |      | 56.4 |          |      |      |      |          |      |       |      |          |
| HCM 2010 LOS                 |      |      | Е    |          |      |      |      |          |      |       |      |          |

## 1: Ridgemark Dr/Fairview Rd & Airline Highway (SR 25)

| -                          |      |          |       |       |          |       |       |       |       |       |          |       |
|----------------------------|------|----------|-------|-------|----------|-------|-------|-------|-------|-------|----------|-------|
| Intersection               |      |          |       |       |          |       |       |       |       |       |          |       |
| Intersection Delay, s/veh  | 14   |          |       |       |          |       |       |       |       |       |          |       |
| Intersection LOS           | В    |          |       |       |          |       |       |       |       |       |          |       |
|                            |      |          |       |       |          |       |       |       |       |       |          |       |
| Movement                   | EBL  | EBT      | EBR   | WBL   | WBT      | WBR   | NBL   | NBT   | NBR   | SBL   | SBT      | SBR   |
| Lane Configurations        | 7    | <b>†</b> | 7     | 7     | <b>†</b> | 7     | ሻ     | £     |       | 7     | <b>†</b> | 7     |
| Traffic Vol, veh/h         | 118  | 206      | 254   | 4     | 161      | 76    | 129   | 36    | 2     | 91    | 86       | 140   |
| Future Vol, veh/h          | 118  | 206      | 254   | 4     | 161      | 76    | 129   | 36    | 2     | 91    | 86       | 140   |
| Peak Hour Factor           | 0.97 | 0.97     | 0.97  | 0.97  | 0.97     | 0.97  | 0.97  | 0.97  | 0.97  | 0.97  | 0.97     | 0.97  |
| Heavy Vehicles, %          | 2    | 2        | 2     | 2     | 2        | 2     | 2     | 2     | 2     | 2     | 2        | 2     |
| Mvmt Flow                  | 122  | 212      | 262   | 4     | 166      | 78    | 133   | 37    | 2     | 94    | 89       | 144   |
| Number of Lanes            | 1    | 1        | 1     | 1     | 1        | 1     | 1     | 1     | 0     | 1     | 1        | 1     |
| Approach                   | EB   |          |       | WB    |          |       | NB    |       |       | SB    |          |       |
| Opposing Approach          | WB   |          |       | EB    |          |       | SB    |       |       | NB    |          |       |
| Opposing Lanes             | 3    |          |       | 3     |          |       | 3     |       |       | 2     |          |       |
| Conflicting Approach Left  | SB   |          |       | NB    |          |       | EB    |       |       | WB    |          |       |
| Conflicting Lanes Left     | 3    |          |       | 2     |          |       | 3     |       |       | 3     |          |       |
| Conflicting Approach Right | NB   |          |       | SB    |          |       | WB    |       |       | EB    |          |       |
| Conflicting Lanes Right    | 2    |          |       | 3     |          |       | 3     |       |       | 3     |          |       |
| HCM Control Delay          | 14.7 |          |       | 13.9  |          |       | 14.3  |       |       | 12.7  |          |       |
| HCM LOS                    | В    |          |       | В     |          |       | В     |       |       | В     |          |       |
|                            |      |          |       |       |          |       |       |       |       |       |          |       |
| Lane                       |      | NBLn1    | NBLn2 | EBLn1 | EBLn2    | EBLn3 | WBLn1 | WBLn2 | WBLn3 | SBLn1 | SBLn2    | SBLn3 |
| Vol Left, %                |      | 100%     | 0%    | 100%  | 0%       | 0%    | 100%  | 0%    | 0%    | 100%  | 0%       | 0%    |
| Vol Thru, %                |      | 0%       | 95%   | 0%    | 100%     | 0%    | 0%    | 100%  | 0%    | 0%    | 100%     | 0%    |
| Vol Right, %               |      | 0%       | 5%    | 0%    | 0%       | 100%  | 0%    | 0%    | 100%  | 0%    | 0%       | 100%  |
| Sign Control               |      | Stop     | Stop  | Stop  | Stop     | Stop  | Stop  | Stop  | Stop  | Stop  | Stop     | Stop  |

| Lane                   | INBLIT | NBLn2 | ERFUL | EBLNZ | EBLN3 | WBLNI | WBLnZ | WBLN3 | SBLIT | SBLNZ | SBLn3 |
|------------------------|--------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Vol Left, %            | 100%   | 0%    | 100%  | 0%    | 0%    | 100%  | 0%    | 0%    | 100%  | 0%    | 0%    |
| Vol Thru, %            | 0%     | 95%   | 0%    | 100%  | 0%    | 0%    | 100%  | 0%    | 0%    | 100%  | 0%    |
| Vol Right, %           | 0%     | 5%    | 0%    | 0%    | 100%  | 0%    | 0%    | 100%  | 0%    | 0%    | 100%  |
| Sign Control           | Stop   | Stop  | Stop  | Stop  | Stop  | Stop  | Stop  | Stop  | Stop  | Stop  | Stop  |
| Traffic Vol by Lane    | 129    | 38    | 118   | 206   | 254   | 4     | 161   | 76    | 91    | 86    | 140   |
| LT Vol                 | 129    | 0     | 118   | 0     | 0     | 4     | 0     | 0     | 91    | 0     | 0     |
| Through Vol            | 0      | 36    | 0     | 206   | 0     | 0     | 161   | 0     | 0     | 86    | 0     |
| RT Vol                 | 0      | 2     | 0     | 0     | 254   | 0     | 0     | 76    | 0     | 0     | 140   |
| Lane Flow Rate         | 133    | 39    | 122   | 212   | 262   | 4     | 166   | 78    | 94    | 89    | 144   |
| Geometry Grp           | 8      | 8     | 8     | 8     | 8     | 8     | 8     | 8     | 8     | 8     | 8     |
| Degree of Util (X)     | 0.314  | 0.087 | 0.26  | 0.425 | 0.472 | 0.01  | 0.366 | 0.157 | 0.215 | 0.191 | 0.283 |
| Departure Headway (Hd) | 8.493  | 7.957 | 7.707 | 7.201 | 6.491 | 8.438 | 7.93  | 7.218 | 8.268 | 7.765 | 7.059 |
| Convergence, Y/N       | Yes    | Yes   | Yes   | Yes   | Yes   | Yes   | Yes   | Yes   | Yes   | Yes   | Yes   |
| Cap                    | 423    | 450   | 466   | 499   | 555   | 424   | 453   | 496   | 433   | 462   | 508   |
| Service Time           | 6.252  | 5.716 | 5.457 | 4.95  | 4.241 | 6.196 | 5.687 | 4.975 | 6.027 | 5.523 | 4.818 |
| HCM Lane V/C Ratio     | 0.314  | 0.087 | 0.262 | 0.425 | 0.472 | 0.009 | 0.366 | 0.157 | 0.217 | 0.193 | 0.283 |
| HCM Control Delay      | 15.1   | 11.5  | 13.2  | 15.2  | 15    | 11.3  | 15.2  | 11.3  | 13.3  | 12.4  | 12.6  |
| HCM Lane LOS           | С      | В     | В     | С     | В     | В     | С     | В     | В     | В     | В     |
| HCM 95th-tile Q        | 1.3    | 0.3   | 1     | 2.1   | 2.5   | 0     | 1.7   | 0.6   | 8.0   | 0.7   | 1.2   |

| Intersection           |              |              |        |           |              |       |          |          |          |          |               |          |       |
|------------------------|--------------|--------------|--------|-----------|--------------|-------|----------|----------|----------|----------|---------------|----------|-------|
| Int Delay, s/veh       | 5.4          |              |        |           |              |       |          |          |          |          |               |          |       |
| Movement               | EBL          | EBT          | EBR    | WBL       | WBT          | WBR   | NBL      | NBT      | NBR      | SBL      | SBT           | SBR      |       |
| Lane Configurations    | T T          | <u></u>      | T T    | VVDL<br>Š |              | WBK 7 | NDL<br>T |          | NDK      | SBL<br>Š |               | JDK<br>7 |       |
| Traffic Vol, veh/h     | 168          | <b>T</b> 513 | 61     | 66        | <b>↑</b> 331 | 39    | 28       | <b>↑</b> | 44       | 21       | <b>↑</b><br>2 | 96       |       |
| Future Vol, veh/h      | 168          | 513          | 61     | 66        | 331          | 39    | 28       | 2        | 44       | 21       | 2             | 96       |       |
| Conflicting Peds, #/hr | 0            | 0            | 0      | 0         | 0            | 0     | 0        | 0        | 0        | 0        | 0             | 0        |       |
| Sign Control           | Free         | Free         | Free   | Free      | Free         | Free  | Stop     | Stop     | Stop     | Stop     | Stop          | Stop     |       |
| RT Channelized         | -            | -            | None   | -         | -            | None  | - Otop   | - Otop   | None     | - Olop   | - Clop        | None     |       |
| Storage Length         | 320          | _            | 505    | 360       | <u>-</u>     | 195   | 60       | _        | 0        | 100      | _             | 100      |       |
| Veh in Median Storage  |              | 0            | -      | -         | 0            | -     | -        | 0        | -        | -        | 0             | -        |       |
| Grade, %               | ·, <i>''</i> | 0            | _      | _         | 0            | _     | _        | 0        | <u>-</u> | _        | 0             | _        |       |
| Peak Hour Factor       | 95           | 95           | 95     | 95        | 95           | 95    | 95       | 95       | 95       | 95       | 95            | 95       |       |
| Heavy Vehicles, %      | 2            | 2            | 2      | 2         | 2            | 2     | 2        | 2        | 2        | 2        | 2             | 2        |       |
| Mvmt Flow              | 177          | 540          | 64     | 69        | 348          | 41    | 29       | 2        | 46       | 22       | 2             | 101      |       |
| WWW. TOW               |              | 010          | 01     | 00        | 010          | • • • | 20       | _        | 10       |          | _             | 101      |       |
| Major/Minor I          | Major1       |              |        | Major2    |              |       | Minor1   |          |          | Minor2   |               |          |       |
| Conflicting Flow All   | 389          | 0            | 0      | 604       | 0            | 0     | 1452     | 1421     | 540      | 1436     | 1444          | 348      |       |
| Stage 1                | 309          | -            | U      | 004       |              | U     | 894      | 894      | 540      | 486      | 486           | 340      |       |
| Stage 1                | _            | _            | -      | -         | -            | -     | 558      | 527      | _        | 950      | 958           | _        |       |
| Critical Hdwy          | 4.12         | -            | -      | 4.12      | -            | -     | 7.12     | 6.52     | 6.22     | 7.12     | 6.52          | 6.22     |       |
| Critical Hdwy Stg 1    | 4.12         | _            | _      | 4.12      | _            | _     | 6.12     | 5.52     | 0.22     | 6.12     | 5.52          | 0.22     |       |
| Critical Hdwy Stg 2    | -            |              |        |           |              |       | 6.12     | 5.52     | <u>-</u> | 6.12     | 5.52          |          |       |
| Follow-up Hdwy         | 2.218        | _            | _      | 2.218     | _            | _     | 3.518    |          | 3.318    | 3.518    | 4.018         | 3.318    |       |
| Pot Cap-1 Maneuver     | 1170         | _            | _      | 974       | _            | _     | 108      | 136      | 542      | 111      | 132           | 695      |       |
| Stage 1                | -            | <u>-</u>     | _      | -         | _            | _     | 336      | 360      | -        | 563      | 551           | -        |       |
| Stage 2                | _            | -            | _      | -         | _            | _     | 514      | 528      | _        | 312      | 336           | _        |       |
| Platoon blocked, %     |              | -            | -      |           | -            | -     | J 1 1    | 323      |          | J.E      | 300           |          |       |
| Mov Cap-1 Maneuver     | 1170         | _            | -      | 974       | _            | -     | 76       | 107      | 542      | 84       | 104           | 695      |       |
| Mov Cap-2 Maneuver     | -            | _            | -      | -         | _            | -     | 76       | 107      | -        | 84       | 104           | -        |       |
| Stage 1                | -            | -            | -      | -         | -            | -     | 285      | 306      | -        | 478      | 512           | -        |       |
| Stage 2                | -            | -            | -      | -         | -            | -     | 406      | 491      | -        | 241      | 285           | -        |       |
| ·                      |              |              |        |           |              |       |          |          |          |          |               |          |       |
| Approach               | EB           |              |        | WB        |              |       | NB       |          |          | SB       |               |          |       |
| HCM Control Delay, s   | 2            |              |        | 1.4       |              |       | 38.5     |          |          | 20.7     |               |          |       |
| HCM LOS                |              |              |        |           |              |       | Е        |          |          | С        |               |          |       |
|                        |              |              |        |           |              |       |          |          |          |          |               |          |       |
| Minor Lane/Major Mvm   | nt I         | NBLn1        | NBLn21 | NBLn3     | EBL          | EBT   | EBR      | WBL      | WBT      | WBR      | SBLn1         | SBLn2    | SBLn3 |
| Capacity (veh/h)       |              | 76           | 107    | 542       | 1170         | _     | -        | 974      | _        | -        | 84            | 104      | 695   |
| HCM Lane V/C Ratio     |              | 0.388        |        |           | 0.151        | -     | -        | 0.071    | -        | _        | 0.263         |          | 0.145 |
| HCM Control Delay (s)  |              | 79.7         | 39.3   | 12.3      | 8.6          | -     | -        | 9        | -        | -        |               | 40.3     | 11.1  |
| HCM Lane LOS           |              | F            | E      | В         | Α            | -     | -        | A        | -        | -        | F             | Е        | В     |
| HCM 95th %tile Q(veh)  | )            | 1.5          | 0.1    | 0.3       | 0.5          | -     | -        | 0.2      | -        | -        |               | 0.1      | 0.5   |
| ,                      |              |              |        |           |              |       |          |          |          |          |               |          |       |

| Intersection           |          |       |          |       |        |      |
|------------------------|----------|-------|----------|-------|--------|------|
| Int Delay, s/veh       | 3.2      |       |          |       |        |      |
| Movement               | WBL      | WBR   | NBT      | NBR   | SBL    | SBT  |
|                        |          | WDK   |          | NDK   | ODL    |      |
| Lane Configurations    | <b>Y</b> | 70    | <b>}</b> | 00    | 440    | 4    |
| Traffic Vol, veh/h     | 30       | 76    | 185      | 26    | 112    | 290  |
| Future Vol, veh/h      | 30       | 76    | 185      | 26    | 112    | 290  |
| Conflicting Peds, #/hr |          | 0     | _ 0      | _ 0   | _ 0    | _ 0  |
| Sign Control           | Stop     | Stop  | Free     | Free  | Free   | Free |
| RT Channelized         | -        | None  | -        | None  | -      | None |
| Storage Length         | 0        | -     | -        | -     | -      | -    |
| Veh in Median Storag   | e, # 0   | -     | 0        | -     | -      | 0    |
| Grade, %               | 0        | -     | 0        | -     | -      | 0    |
| Peak Hour Factor       | 91       | 91    | 91       | 91    | 91     | 91   |
| Heavy Vehicles, %      | 6        | 6     | 2        | 2     | 3      | 3    |
| Mvmt Flow              | 33       | 84    | 203      | 29    | 123    | 319  |
|                        |          |       |          |       |        |      |
|                        | N. 11. 1 |       |          |       |        |      |
| Major/Minor            | Minor1   |       | //ajor1  |       | Major2 | _    |
| Conflicting Flow All   | 784      | 218   | 0        | 0     | 232    | 0    |
| Stage 1                | 218      | -     | -        | -     | -      | -    |
| Stage 2                | 566      | -     | -        | -     | -      | -    |
| Critical Hdwy          | 6.46     | 6.26  | -        | -     | 4.13   | -    |
| Critical Hdwy Stg 1    | 5.46     | -     | -        | -     | -      | -    |
| Critical Hdwy Stg 2    | 5.46     | -     | -        | -     | -      | -    |
| Follow-up Hdwy         | 3.554    | 3.354 | -        | -     | 2.227  | -    |
| Pot Cap-1 Maneuver     | 356      | 812   | -        | -     | 1330   | -    |
| Stage 1                | 809      | -     | -        | -     | _      | -    |
| Stage 2                | 560      | _     | _        | _     | -      | _    |
| Platoon blocked, %     |          |       | _        | _     |        | _    |
| Mov Cap-1 Maneuver     | 316      | 812   | _        | _     | 1330   | _    |
| Mov Cap-2 Maneuver     |          | -     | _        | _     | -      | _    |
| Stage 1                | 718      | _     | _        |       | _      |      |
|                        | 559      | _     | _        | _     | _      | _    |
| Stage 2                | 559      | -     | -        | -     | -      | -    |
|                        |          |       |          |       |        |      |
| Approach               | WB       |       | NB       |       | SB     |      |
| HCM Control Delay, s   | 13.1     |       | 0        |       | 2.2    |      |
| HCM LOS                | В        |       |          |       |        |      |
|                        | _        |       |          |       |        |      |
|                        |          |       |          |       |        |      |
| Minor Lane/Major Mvr   | nt       | NBT   | NBRV     | VBLn1 | SBL    | SBT  |
| Capacity (veh/h)       |          | -     | -        | 562   |        | -    |
| HCM Lane V/C Ratio     |          | -     | -        | 0.207 | 0.093  | -    |
| HCM Control Delay (s   | 5)       | -     | -        | 13.1  | 8      | 0    |
| HCM Lane LOS           |          | -     | -        | В     | Α      | Α    |
| HCM 95th %tile Q(vel   | າ)       | -     | -        | 0.8   | 0.3    | -    |
|                        | ')       |       |          | 0.0   | 0.0    |      |

|                              | ۶    | <b>→</b> | •     | •    | -     | •     | 1    | <b>†</b> | <b>/</b> | <b>/</b> | Ţ        | 4    |
|------------------------------|------|----------|-------|------|-------|-------|------|----------|----------|----------|----------|------|
| Movement                     | EBL  | EBT      | EBR   | WBL  | WBT   | WBR   | NBL  | NBT      | NBR      | SBL      | SBT      | SBR  |
| Lane Configurations          | ¥    | f)       |       | ň    | f)    |       | Ţ    | <b>†</b> | 7        | ħ        | <b>†</b> | 7    |
| Traffic Volume (veh/h)       | 234  | 309      | 209   | 20   | 180   | 208   | 142  | 283      | 25       | 355      | 501      | 251  |
| Future Volume (veh/h)        | 234  | 309      | 209   | 20   | 180   | 208   | 142  | 283      | 25       | 355      | 501      | 251  |
| Number                       | 7    | 4        | 14    | 3    | 8     | 18    | 5    | 2        | 12       | 1        | 6        | 16   |
| Initial Q (Qb), veh          | 0    | 0        | 0     | 0    | 0     | 0     | 0    | 0        | 0        | 0        | 0        | 0    |
| Ped-Bike Adj(A_pbT)          | 1.00 |          | 1.00  | 1.00 |       | 1.00  | 1.00 |          | 1.00     | 1.00     |          | 1.00 |
| Parking Bus, Adj             | 1.00 | 1.00     | 1.00  | 1.00 | 1.00  | 1.00  | 1.00 | 1.00     | 1.00     | 1.00     | 1.00     | 1.00 |
| Adj Sat Flow, veh/h/ln       | 1863 | 1863     | 1900  | 1863 | 1863  | 1900  | 1863 | 1863     | 1863     | 1863     | 1863     | 1863 |
| Adj Flow Rate, veh/h         | 244  | 322      | 218   | 21   | 188   | 217   | 148  | 295      | 26       | 370      | 522      | 261  |
| Adj No. of Lanes             | 1    | 1        | 0     | 1    | 1     | 0     | 1    | 1        | 1        | 1        | 1        | 1    |
| Peak Hour Factor             | 0.96 | 0.96     | 0.96  | 0.96 | 0.96  | 0.96  | 0.96 | 0.96     | 0.96     | 0.96     | 0.96     | 0.96 |
| Percent Heavy Veh, %         | 2    | 2        | 2     | 2    | 2     | 2     | 2    | 2        | 2        | 2        | 2        | 2    |
| Cap, veh/h                   | 426  | 249      | 168   | 218  | 97    | 112   | 177  | 479      | 407      | 248      | 554      | 471  |
| Arrive On Green              | 0.24 | 0.24     | 0.24  | 0.12 | 0.12  | 0.12  | 0.10 | 0.26     | 0.26     | 0.14     | 0.30     | 0.30 |
| Sat Flow, veh/h              | 1774 | 1037     | 702   | 1774 | 790   | 912   | 1774 | 1863     | 1583     | 1774     | 1863     | 1583 |
| Grp Volume(v), veh/h         | 244  | 0        | 540   | 21   | 0     | 405   | 148  | 295      | 26       | 370      | 522      | 261  |
| Grp Sat Flow(s),veh/h/ln     | 1774 | 0        | 1739  | 1774 | 0     | 1702  | 1774 | 1863     | 1583     | 1774     | 1863     | 1583 |
| Q Serve(g_s), s              | 9.1  | 0.0      | 18.0  | 0.8  | 0.0   | 9.2   | 6.1  | 10.5     | 0.9      | 10.5     | 20.5     | 10.4 |
| Cycle Q Clear(g_c), s        | 9.1  | 0.0      | 18.0  | 0.8  | 0.0   | 9.2   | 6.1  | 10.5     | 0.9      | 10.5     | 20.5     | 10.4 |
| Prop In Lane                 | 1.00 |          | 0.40  | 1.00 |       | 0.54  | 1.00 |          | 1.00     | 1.00     |          | 1.00 |
| Lane Grp Cap(c), veh/h       | 426  | 0        | 417   | 218  | 0     | 209   | 177  | 479      | 407      | 248      | 554      | 471  |
| V/C Ratio(X)                 | 0.57 | 0.00     | 1.29  | 0.10 | 0.00  | 1.94  | 0.83 | 0.62     | 0.06     | 1.49     | 0.94     | 0.55 |
| Avail Cap(c_a), veh/h        | 426  | 0        | 417   | 218  | 0     | 209   | 177  | 479      | 407      | 248      | 554      | 471  |
| HCM Platoon Ratio            | 1.00 | 1.00     | 1.00  | 1.00 | 1.00  | 1.00  | 1.00 | 1.00     | 1.00     | 1.00     | 1.00     | 1.00 |
| Upstream Filter(I)           | 1.00 | 0.00     | 1.00  | 1.00 | 0.00  | 1.00  | 1.00 | 1.00     | 1.00     | 1.00     | 1.00     | 1.00 |
| Uniform Delay (d), s/veh     | 25.1 | 0.0      | 28.5  | 29.2 | 0.0   | 32.9  | 33.1 | 24.6     | 21.0     | 32.3     | 25.7     | 22.2 |
| Incr Delay (d2), s/veh       | 1.9  | 0.0      | 149.1 | 0.2  | 0.0   | 440.1 | 27.6 | 5.8      | 0.3      | 240.6    | 26.4     | 4.6  |
| Initial Q Delay(d3),s/veh    | 0.0  | 0.0      | 0.0   | 0.0  | 0.0   | 0.0   | 0.0  | 0.0      | 0.0      | 0.0      | 0.0      | 0.0  |
| %ile BackOfQ(50%),veh/ln     | 4.6  | 0.0      | 25.9  | 0.4  | 0.0   | 29.8  | 4.4  | 6.1      | 0.4      | 21.7     | 14.5     | 5.1  |
| LnGrp Delay(d),s/veh         | 27.0 | 0.0      | 177.6 | 29.4 | 0.0   | 473.0 | 60.7 | 30.4     | 21.3     | 272.8    | 52.1     | 26.8 |
| LnGrp LOS                    | С    |          | F     | С    |       | F     | Е    | С        | С        | F        | D        | С    |
| Approach Vol, veh/h          |      | 784      |       |      | 426   |       |      | 469      |          |          | 1153     |      |
| Approach Delay, s/veh        |      | 130.7    |       |      | 451.2 |       |      | 39.5     |          |          | 117.2    |      |
| Approach LOS                 |      | F        |       |      | F     |       |      | D        |          |          | F        |      |
| Timer                        | 1    | 2        | 3     | 4    | 5     | 6     | 7    | 8        |          |          |          |      |
| Assigned Phs                 | 1    | 2        |       | 4    | 5     | 6     |      | 8        |          |          |          |      |
| Phs Duration (G+Y+Rc), s     | 15.0 | 23.8     |       | 22.5 | 12.0  | 26.8  |      | 13.7     |          |          |          |      |
| Change Period (Y+Rc), s      | 4.5  | 4.5      |       | 4.5  | 4.5   | 4.5   |      | 4.5      |          |          |          |      |
| Max Green Setting (Gmax), s  | 10.5 | 19.3     |       | 18.0 | 7.5   | 21.9  |      | 9.2      |          |          |          |      |
| Max Q Clear Time (g_c+l1), s | 12.5 | 12.5     |       | 20.0 | 8.1   | 22.5  |      | 11.2     |          |          |          |      |
| Green Ext Time (p_c), s      | 0.0  | 1.0      |       | 0.0  | 0.0   | 0.0   |      | 0.0      |          |          |          |      |
| Intersection Summary         |      |          |       |      |       |       |      |          |          |          |          |      |
| HCM 2010 Ctrl Delay          |      |          | 158.3 |      |       |       |      |          |          |          |          |      |
| HCM 2010 LOS                 |      |          | F     |      |       |       |      |          |          |          |          |      |

|                              |      | <b>→</b> | •     | •     | <b>←</b> | •    | •    | <b>†</b> | ~    | <b>\</b> | <b></b> | <b>√</b> |
|------------------------------|------|----------|-------|-------|----------|------|------|----------|------|----------|---------|----------|
| Movement                     | EBL  | EBT      | EBR   | WBL   | WBT      | WBR  | NBL  | NBT      | NBR  | SBL      | SBT     | SBR      |
| Lane Configurations          | ሻ    | f)       |       | ሻ     | ĵ»       |      |      | 4        |      |          | 4       |          |
| Traffic Volume (veh/h)       | 28   | 633      | 172   | 167   | 382      | 17   | 127  | 49       | 102  | 28       | 79      | 12       |
| Future Volume (veh/h)        | 28   | 633      | 172   | 167   | 382      | 17   | 127  | 49       | 102  | 28       | 79      | 12       |
| Number                       | 7    | 4        | 14    | 3     | 8        | 18   | 5    | 2        | 12   | 1        | 6       | 16       |
| Initial Q (Qb), veh          | 0    | 0        | 0     | 0     | 0        | 0    | 0    | 0        | 0    | 0        | 0       | 0        |
| Ped-Bike Adj(A_pbT)          | 1.00 |          | 1.00  | 1.00  |          | 1.00 | 1.00 |          | 1.00 | 1.00     |         | 1.00     |
| Parking Bus, Adj             | 1.00 | 1.00     | 1.00  | 1.00  | 1.00     | 1.00 | 1.00 | 1.00     | 1.00 | 1.00     | 1.00    | 1.00     |
| Adj Sat Flow, veh/h/ln       | 1863 | 1863     | 1900  | 1863  | 1863     | 1900 | 1900 | 1863     | 1900 | 1900     | 1827    | 1900     |
| Adj Flow Rate, veh/h         | 33   | 736      | 200   | 194   | 444      | 20   | 148  | 57       | 119  | 33       | 92      | 14       |
| Adj No. of Lanes             | 1    | 1        | 0     | 1     | 1        | 0    | 0    | 1        | 0    | 0        | 1       | 0        |
| Peak Hour Factor             | 0.86 | 0.86     | 0.86  | 0.86  | 0.86     | 0.86 | 0.86 | 0.86     | 0.86 | 0.86     | 0.86    | 0.86     |
| Percent Heavy Veh, %         | 2    | 2        | 2     | 2     | 2        | 2    | 2    | 2        | 2    | 4        | 4       | 4        |
| Cap, veh/h                   | 63   | 529      | 144   | 151   | 751      | 34   | 278  | 113      | 176  | 159      | 395     | 54       |
| Arrive On Green              | 0.04 | 0.38     | 0.38  | 0.09  | 0.42     | 0.42 | 0.31 | 0.31     | 0.31 | 0.31     | 0.31    | 0.31     |
| Sat Flow, veh/h              | 1774 | 1411     | 384   | 1774  | 1769     | 80   | 604  | 358      | 559  | 268      | 1254    | 170      |
| Grp Volume(v), veh/h         | 33   | 0        | 936   | 194   | 0        | 464  | 324  | 0        | 0    | 139      | 0       | 0        |
| Grp Sat Flow(s),veh/h/ln     | 1774 | 0        | 1795  | 1774  | 0        | 1849 | 1521 | 0        | 0    | 1692     | 0       | 0        |
| Q Serve(g_s), s              | 1.1  | 0.0      | 22.5  | 5.1   | 0.0      | 11.6 | 7.3  | 0.0      | 0.0  | 0.0      | 0.0     | 0.0      |
| Cycle Q Clear(g_c), s        | 1.1  | 0.0      | 22.5  | 5.1   | 0.0      | 11.6 | 10.7 | 0.0      | 0.0  | 3.4      | 0.0     | 0.0      |
| Prop In Lane                 | 1.00 |          | 0.21  | 1.00  |          | 0.04 | 0.46 |          | 0.37 | 0.24     |         | 0.10     |
| Lane Grp Cap(c), veh/h       | 63   | 0        | 673   | 151   | 0        | 785  | 567  | 0        | 0    | 607      | 0       | 0        |
| V/C Ratio(X)                 | 0.53 | 0.00     | 1.39  | 1.29  | 0.00     | 0.59 | 0.57 | 0.00     | 0.00 | 0.23     | 0.00    | 0.00     |
| Avail Cap(c_a), veh/h        | 163  | 0        | 673   | 151   | 0        | 785  | 567  | 0        | 0    | 607      | 0       | 0        |
| HCM Platoon Ratio            | 1.00 | 1.00     | 1.00  | 1.00  | 1.00     | 1.00 | 1.00 | 1.00     | 1.00 | 1.00     | 1.00    | 1.00     |
| Upstream Filter(I)           | 1.00 | 0.00     | 1.00  | 1.00  | 0.00     | 1.00 | 1.00 | 0.00     | 0.00 | 1.00     | 0.00    | 0.00     |
| Uniform Delay (d), s/veh     | 28.5 | 0.0      | 18.8  | 27.5  | 0.0      | 13.3 | 17.6 | 0.0      | 0.0  | 15.3     | 0.0     | 0.0      |
| Incr Delay (d2), s/veh       | 6.7  | 0.0      | 184.8 | 169.7 | 0.0      | 1.2  | 4.2  | 0.0      | 0.0  | 0.9      | 0.0     | 0.0      |
| Initial Q Delay(d3),s/veh    | 0.0  | 0.0      | 0.0   | 0.0   | 0.0      | 0.0  | 0.0  | 0.0      | 0.0  | 0.0      | 0.0     | 0.0      |
| %ile BackOfQ(50%),veh/ln     | 0.6  | 0.0      | 45.6  | 9.6   | 0.0      | 6.1  | 5.2  | 0.0      | 0.0  | 1.8      | 0.0     | 0.0      |
| LnGrp Delay(d),s/veh         | 35.2 | 0.0      | 203.5 | 197.1 | 0.0      | 14.4 | 21.7 | 0.0      | 0.0  | 16.1     | 0.0     | 0.0      |
| LnGrp LOS                    | D    |          | F     | F     |          | В    | С    |          |      | В        |         |          |
| Approach Vol, veh/h          |      | 969      |       |       | 658      |      |      | 324      |      |          | 139     |          |
| Approach Delay, s/veh        |      | 197.8    |       |       | 68.3     |      |      | 21.7     |      |          | 16.1    |          |
| Approach LOS                 |      | F        |       |       | Е        |      |      | С        |      |          | В       |          |
| Timer                        | 1    | 2        | 3     | 4     | 5        | 6    | 7    | 8        |      |          |         |          |
| Assigned Phs                 |      | 2        | 3     | 4     |          | 6    | 7    | 8        |      |          |         |          |
| Phs Duration (G+Y+Rc), s     |      | 23.4     | 9.6   | 27.0  |          | 23.4 | 6.6  | 30.0     |      |          |         |          |
| Change Period (Y+Rc), s      |      | 4.5      | 4.5   | 4.5   |          | 4.5  | 4.5  | 4.5      |      |          |         |          |
| Max Green Setting (Gmax), s  |      | 18.9     | 5.1   | 22.5  |          | 18.9 | 5.5  | 22.1     |      |          |         |          |
| Max Q Clear Time (g_c+l1), s |      | 12.7     | 7.1   | 24.5  |          | 5.4  | 3.1  | 13.6     |      |          |         |          |
| Green Ext Time (p_c), s      |      | 1.0      | 0.0   | 0.0   |          | 0.6  | 0.0  | 1.9      |      |          |         |          |
| Intersection Summary         |      |          |       |       |          |      |      |          |      |          |         |          |
| HCM 2010 Ctrl Delay          |      |          | 117.6 |       |          |      |      |          |      |          |         |          |
| HCM 2010 LOS                 |      |          | F     |       |          |      |      |          |      |          |         |          |

|                              |           | <b>→</b>  | <b>←</b>  | •    | <u> </u> | 4    |      |      |  |  |
|------------------------------|-----------|-----------|-----------|------|----------|------|------|------|--|--|
| Movement                     | EBL       | EBT       | WBT       | WBR  | SBL      | SBR  |      |      |  |  |
| Lane Configurations          | *         | <b>1</b>  | <b></b>   | 7    | *        | 7    |      |      |  |  |
| Traffic Volume (veh/h)       | 320       | 640       | 332       | 189  | 192      | 218  |      |      |  |  |
| Future Volume (veh/h)        | 320       | 640       | 332       | 189  | 192      | 218  |      |      |  |  |
| Number                       | 7         | 4         | 8         | 18   | 1        | 16   |      |      |  |  |
| Initial Q (Qb), veh          | 0         | 0         | 0         | 0    | 0        | 0    |      |      |  |  |
| Ped-Bike Adj(A_pbT)          | 1.00      | -         | -         | 1.00 | 1.00     | 1.00 |      |      |  |  |
| Parking Bus, Adj             | 1.00      | 1.00      | 1.00      | 1.00 | 1.00     | 1.00 |      |      |  |  |
| Adj Sat Flow, veh/h/ln       | 1863      | 1863      | 1863      | 1863 | 1863     | 1863 |      |      |  |  |
| Adj Flow Rate, veh/h         | 340       | 681       | 353       | 201  | 204      | 232  |      |      |  |  |
| Adj No. of Lanes             | 1         | 1         | 1         | 1    | 1        | 1    |      |      |  |  |
| Peak Hour Factor             | 0.94      | 0.94      | 0.94      | 0.94 | 0.94     | 0.94 |      |      |  |  |
| Percent Heavy Veh, %         | 2         | 2         | 2         | 2    | 2        | 2    |      |      |  |  |
| Cap, veh/h                   | 412       | 1038      | 441       | 375  | 471      | 420  |      |      |  |  |
| Arrive On Green              | 0.23      | 0.56      | 0.24      | 0.24 | 0.27     | 0.27 |      |      |  |  |
| Sat Flow, veh/h              | 1774      | 1863      | 1863      | 1583 | 1774     | 1583 |      |      |  |  |
| Grp Volume(v), veh/h         | 340       | 681       | 353       | 201  | 204      | 232  |      |      |  |  |
| Grp Sat Flow(s), veh/h/ln    | 1774      | 1863      | 1863      | 1583 | 1774     | 1583 |      |      |  |  |
| Q Serve(g_s), s              | 9.3       | 13.0      | 9.1       | 5.6  | 4.9      | 6.4  |      |      |  |  |
| Cycle Q Clear(g_c), s        | 9.3       | 13.0      | 9.1       | 5.6  | 4.9      | 6.4  |      |      |  |  |
| Prop In Lane                 | 1.00      | 10.0      | J. 1      | 1.00 | 1.00     | 1.00 |      |      |  |  |
| Lane Grp Cap(c), veh/h       | 412       | 1038      | 441       | 375  | 471      | 420  |      |      |  |  |
| V/C Ratio(X)                 | 0.83      | 0.66      | 0.80      | 0.54 | 0.43     | 0.55 |      |      |  |  |
| Avail Cap(c_a), veh/h        | 646       | 1374      | 531       | 452  | 471      | 420  |      |      |  |  |
| HCM Platoon Ratio            | 1.00      | 1.00      | 1.00      | 1.00 | 1.00     | 1.00 |      |      |  |  |
| Upstream Filter(I)           | 1.00      | 1.00      | 1.00      | 1.00 | 1.00     | 1.00 |      |      |  |  |
| Uniform Delay (d), s/veh     | 18.5      | 7.8       | 18.3      | 17.0 | 15.5     | 16.1 |      |      |  |  |
| Incr Delay (d2), s/veh       | 5.0       | 0.7       | 7.2       | 1.2  | 2.9      | 5.1  |      |      |  |  |
| Initial Q Delay(d3),s/veh    | 0.0       | 0.0       | 0.0       | 0.0  | 0.0      | 0.0  |      |      |  |  |
| %ile BackOfQ(50%),veh/ln     | 5.1       | 6.8       | 5.5       | 2.6  | 2.8      | 6.2  |      |      |  |  |
| LnGrp Delay(d),s/veh         | 23.6      | 8.6       | 25.4      | 18.1 | 18.4     | 21.2 |      |      |  |  |
| LnGrp LOS                    | 20.0<br>C | Α         | C         | В    | В        | C    |      |      |  |  |
| Approach Vol, veh/h          |           | 1021      | 554       |      | 436      |      |      |      |  |  |
| Approach Vol, ven/n          |           | 13.6      | 22.8      |      | 19.9     |      |      |      |  |  |
| Approach LOS                 |           | 13.0<br>B | 22.0<br>C |      | 19.9     |      |      |      |  |  |
| •                            |           |           |           | ,    |          | ^    | 7    | 0    |  |  |
| Timer                        | Т         | 2         | 3         | 4    | 5        | 6    |      | 8    |  |  |
| Assigned Phs                 |           |           |           | 4    |          | 6    | 7    | 8    |  |  |
| Phs Duration (G+Y+Rc), s     |           |           |           | 32.8 |          | 18.0 | 16.3 | 16.5 |  |  |
| Change Period (Y+Rc), s      |           |           |           | 4.5  |          | 4.5  | 4.5  | 4.5  |  |  |
| Max Green Setting (Gmax), s  |           |           |           | 37.5 |          | 13.5 | 18.5 | 14.5 |  |  |
| Max Q Clear Time (g_c+l1), s |           |           |           | 15.0 |          | 8.4  | 11.3 | 11.1 |  |  |
| Green Ext Time (p_c), s      |           |           |           | 5.0  |          | 0.7  | 0.6  | 1.0  |  |  |
| Intersection Summary         |           |           | 4==       |      |          |      |      |      |  |  |
| HCM 2010 Ctrl Delay          |           |           | 17.5      |      |          |      |      |      |  |  |
| HCM 2010 LOS                 |           |           | В         |      |          |      |      |      |  |  |

|                                | ۶          | <b>→</b> | •      | •     | <b>←</b>    | •          | 1       | <b>†</b> | <b>/</b> | -     | <b>↓</b> | 4    |
|--------------------------------|------------|----------|--------|-------|-------------|------------|---------|----------|----------|-------|----------|------|
| Movement                       | EBL        | EBT      | EBR    | WBL   | WBT         | WBR        | NBL     | NBT      | NBR      | SBL   | SBT      | SBR  |
| Lane Configurations            | ሻ          | <b>†</b> | 7      | 7     | 1>          |            |         | ર્ન      | 7        |       | ર્ન      | 7    |
| Traffic Volume (vph)           | 1          | 681      | 706    | 108   | 705         | 27         | 539     | 16       | 141      | 132   | 154      | 1    |
| Future Volume (vph)            | 1          | 681      | 706    | 108   | 705         | 27         | 539     | 16       | 141      | 132   | 154      | 1    |
| Ideal Flow (vphpl)             | 1900       | 1900     | 1900   | 1900  | 1900        | 1900       | 1900    | 1900     | 1900     | 1900  | 1900     | 1900 |
| Total Lost time (s)            | 4.5        | 4.5      | 4.5    | 4.5   | 4.5         |            |         | 4.5      | 4.5      |       | 4.5      | 4.5  |
| Lane Util. Factor              | 1.00       | 1.00     | 1.00   | 1.00  | 1.00        |            |         | 1.00     | 1.00     |       | 1.00     | 1.00 |
| Frt                            | 1.00       | 1.00     | 0.85   | 1.00  | 0.99        |            |         | 1.00     | 0.85     |       | 1.00     | 0.85 |
| Flt Protected                  | 0.95       | 1.00     | 1.00   | 0.95  | 1.00        |            |         | 0.95     | 1.00     |       | 0.98     | 1.00 |
| Satd. Flow (prot)              | 1687       | 1776     | 1509   | 1583  | 1657        |            |         | 1776     | 1583     |       | 1821     | 1583 |
| Flt Permitted                  | 0.95       | 1.00     | 1.00   | 0.95  | 1.00        |            |         | 0.95     | 1.00     |       | 0.98     | 1.00 |
| Satd. Flow (perm)              | 1687       | 1776     | 1509   | 1583  | 1657        |            |         | 1776     | 1583     |       | 1821     | 1583 |
| Peak-hour factor, PHF          | 0.94       | 0.94     | 0.94   | 0.94  | 0.94        | 0.94       | 0.94    | 0.94     | 0.94     | 0.94  | 0.94     | 0.94 |
| Adj. Flow (vph)                | 1          | 724      | 751    | 115   | 750         | 29         | 573     | 17       | 150      | 140   | 164      | 1    |
| RTOR Reduction (vph)           | 0          | 0        | 379    | 0     | 1           | 0          | 0       | 0        | 84       | 0     | 0        | 1    |
| Lane Group Flow (vph)          | 1          | 724      | 372    | 115   | 778         | 0          | 0       | 590      | 66       | 0     | 304      | 0    |
| Heavy Vehicles (%)             | 7%         | 7%       | 7%     | 14%   | 14%         | 14%        | 2%      | 2%       | 2%       | 2%    | 2%       | 2%   |
| Turn Type                      | Prot       | NA       | Perm   | Prot  | NA          |            | Split   | NA       | Perm     | Split | NA       | Perm |
| Protected Phases               | 7          | 4        |        | 3     | 8           |            | 5       | 5        |          | 6     | 6        |      |
| Permitted Phases               |            |          | 4      |       |             |            |         |          | 5        |       |          | 6    |
| Actuated Green, G (s)          | 1.0        | 48.1     | 48.1   | 5.0   | 52.1        |            |         | 22.1     | 22.1     |       | 19.9     | 19.9 |
| Effective Green, g (s)         | 1.0        | 48.1     | 48.1   | 5.0   | 52.1        |            |         | 22.1     | 22.1     |       | 19.9     | 19.9 |
| Actuated g/C Ratio             | 0.01       | 0.43     | 0.43   | 0.04  | 0.46        |            |         | 0.20     | 0.20     |       | 0.18     | 0.18 |
| Clearance Time (s)             | 4.5        | 4.5      | 4.5    | 4.5   | 4.5         |            |         | 4.5      | 4.5      |       | 4.5      | 4.5  |
| Vehicle Extension (s)          | 3.0        | 3.0      | 3.0    | 3.0   | 3.0         |            |         | 3.0      | 3.0      |       | 3.0      | 3.0  |
| Lane Grp Cap (vph)             | 14         | 755      | 641    | 69    | 763         |            |         | 347      | 309      |       | 320      | 278  |
| v/s Ratio Prot                 | 0.00       | 0.41     |        | c0.07 | c0.47       |            |         | c0.33    |          |       | c0.17    |      |
| v/s Ratio Perm                 |            |          | 0.25   |       |             |            |         |          | 0.04     |       |          | 0.00 |
| v/c Ratio                      | 0.07       | 0.96     | 0.58   | 1.67  | 1.02        |            |         | 1.70     | 0.21     |       | 0.95     | 0.00 |
| Uniform Delay, d1              | 55.6       | 31.5     | 24.8   | 54.0  | 30.5        |            |         | 45.5     | 38.2     |       | 46.1     | 38.4 |
| Progression Factor             | 1.00       | 1.00     | 1.00   | 1.00  | 1.00        |            |         | 1.00     | 1.00     |       | 1.00     | 1.00 |
| Incremental Delay, d2          | 2.2        | 24.1     | 3.8    | 355.1 | 37.6        |            |         | 327.3    | 0.3      |       | 36.7     | 0.0  |
| Delay (s)                      | 57.8       | 55.7     | 28.6   | 409.1 | 68.1        |            |         | 372.8    | 38.6     |       | 82.8     | 38.4 |
| Level of Service               | Е          | Е        | С      | F     | Е           |            |         | F        | D        |       | F        | D    |
| Approach Delay (s)             |            | 41.9     |        |       | 112.0       |            |         | 305.0    |          |       | 82.7     |      |
| Approach LOS                   |            | D        |        |       | F           |            |         | F        |          |       | F        |      |
| Intersection Summary           |            |          |        |       |             |            |         |          |          |       |          |      |
| HCM 2000 Control Delay         |            |          | 120.9  | Н     | CM 2000     | Level of S | Service |          | F        |       |          |      |
| HCM 2000 Volume to Capac       | city ratio |          | 1.20   |       |             |            |         |          |          |       |          |      |
| Actuated Cycle Length (s)      |            |          | 113.1  |       | um of lost  |            |         |          | 18.0     |       |          |      |
| Intersection Capacity Utilizat | tion       |          | 104.0% | IC    | CU Level of | of Service |         |          | G        |       |          |      |
| Analysis Period (min)          |            |          | 15     |       |             |            |         |          |          |       |          |      |
| c Critical Lane Group          |            |          |        |       |             |            |         |          |          |       |          |      |

|                              | ۶    | <b>→</b> | •    | €    | <b>←</b> | •    | 1     | <b>†</b>    | <b>/</b> | <b>/</b> | <b>↓</b> | 4    |
|------------------------------|------|----------|------|------|----------|------|-------|-------------|----------|----------|----------|------|
| Movement                     | EBL  | EBT      | EBR  | WBL  | WBT      | WBR  | NBL   | NBT         | NBR      | SBL      | SBT      | SBR  |
| Lane Configurations          | 1,1  | <b>^</b> | 7    | 7    | <b>^</b> | 7    | ሻሻ    | <b>↑</b> ↑₽ |          | ሻሻ       | ተተተ      | 7    |
| Traffic Volume (veh/h)       | 196  | 400      | 208  | 167  | 303      | 332  | 491   | 1061        | 255      | 217      | 652      | 141  |
| Future Volume (veh/h)        | 196  | 400      | 208  | 167  | 303      | 332  | 491   | 1061        | 255      | 217      | 652      | 141  |
| Number                       | 7    | 4        | 14   | 3    | 8        | 18   | 5     | 2           | 12       | 1        | 6        | 16   |
| Initial Q (Qb), veh          | 0    | 0        | 0    | 0    | 0        | 0    | 0     | 0           | 0        | 0        | 0        | 0    |
| Ped-Bike Adj(A_pbT)          | 1.00 |          | 0.99 | 1.00 |          | 1.00 | 1.00  |             | 1.00     | 1.00     |          | 1.00 |
| Parking Bus, Adj             | 1.00 | 1.00     | 1.00 | 1.00 | 1.00     | 1.00 | 1.00  | 1.00        | 1.00     | 1.00     | 1.00     | 1.00 |
| Adj Sat Flow, veh/h/ln       | 1863 | 1863     | 1863 | 1863 | 1863     | 1863 | 1863  | 1863        | 1900     | 1863     | 1863     | 1863 |
| Adj Flow Rate, veh/h         | 204  | 417      | 217  | 174  | 316      | 346  | 511   | 1105        | 266      | 226      | 679      | 147  |
| Adj No. of Lanes             | 2    | 2        | 1    | 1    | 2        | 1    | 2     | 3           | 0        | 2        | 3        | 1    |
| Peak Hour Factor             | 0.96 | 0.96     | 0.96 | 0.96 | 0.96     | 0.96 | 0.96  | 0.96        | 0.96     | 0.96     | 0.96     | 0.96 |
| Percent Heavy Veh, %         | 2    | 2        | 2    | 2    | 2        | 2    | 2     | 2           | 2        | 2        | 2        | 2    |
| Cap, veh/h                   | 300  | 792      | 504  | 214  | 910      | 405  | 337   | 1193        | 287      | 319      | 1456     | 591  |
| Arrive On Green              | 0.09 | 0.22     | 0.22 | 0.12 | 0.26     | 0.26 | 0.10  | 0.29        | 0.29     | 0.09     | 0.29     | 0.29 |
| Sat Flow, veh/h              | 3442 | 3539     | 1560 | 1774 | 3539     | 1576 | 3442  | 4094        | 985      | 3442     | 5085     | 1580 |
| Grp Volume(v), veh/h         | 204  | 417      | 217  | 174  | 316      | 346  | 511   | 915         | 456      | 226      | 679      | 147  |
| Grp Sat Flow(s),veh/h/ln     | 1721 | 1770     | 1560 | 1774 | 1770     | 1576 | 1721  | 1695        | 1689     | 1721     | 1695     | 1580 |
| Q Serve(g_s), s              | 3.8  | 6.9      | 7.3  | 6.3  | 4.8      | 13.9 | 6.5   | 17.4        | 17.4     | 4.2      | 7.3      | 4.3  |
| Cycle Q Clear(g_c), s        | 3.8  | 6.9      | 7.3  | 6.3  | 4.8      | 13.9 | 6.5   | 17.4        | 17.4     | 4.2      | 7.3      | 4.3  |
| Prop In Lane                 | 1.00 |          | 1.00 | 1.00 |          | 1.00 | 1.00  |             | 0.58     | 1.00     |          | 1.00 |
| Lane Grp Cap(c), veh/h       | 300  | 792      | 504  | 214  | 910      | 405  | 337   | 988         | 492      | 319      | 1456     | 591  |
| V/C Ratio(X)                 | 0.68 | 0.53     | 0.43 | 0.81 | 0.35     | 0.85 | 1.52  | 0.93        | 0.93     | 0.71     | 0.47     | 0.25 |
| Avail Cap(c_a), veh/h        | 389  | 960      | 578  | 227  | 1013     | 451  | 337   | 988         | 492      | 337      | 1456     | 591  |
| HCM Platoon Ratio            | 1.00 | 1.00     | 1.00 | 1.00 | 1.00     | 1.00 | 1.00  | 1.00        | 1.00     | 1.00     | 1.00     | 1.00 |
| Upstream Filter(I)           | 1.00 | 1.00     | 1.00 | 1.00 | 1.00     | 1.00 | 1.00  | 1.00        | 1.00     | 1.00     | 1.00     | 1.00 |
| Uniform Delay (d), s/veh     | 29.4 | 22.7     | 17.7 | 28.4 | 20.1     | 23.5 | 29.9  | 22.8        | 22.8     | 29.2     | 19.5     | 14.4 |
| Incr Delay (d2), s/veh       | 3.2  | 0.5      | 0.6  | 18.8 | 0.2      | 13.6 | 246.9 | 15.5        | 25.8     | 6.3      | 1.1      | 1.0  |
| Initial Q Delay(d3),s/veh    | 0.0  | 0.0      | 0.0  | 0.0  | 0.0      | 0.0  | 0.0   | 0.0         | 0.0      | 0.0      | 0.0      | 0.0  |
| %ile BackOfQ(50%),veh/ln     | 1.9  | 3.4      | 3.2  | 4.2  | 2.4      | 7.5  | 14.6  | 10.3        | 11.6     | 2.3      | 3.5      | 2.0  |
| LnGrp Delay(d),s/veh         | 32.5 | 23.2     | 18.3 | 47.2 | 20.3     | 37.1 | 276.8 | 38.3        | 48.6     | 35.5     | 20.6     | 15.4 |
| LnGrp LOS                    | С    | С        | В    | D    | С        | D    | F     | D           | D        | D        | С        | В    |
| Approach Vol, veh/h          |      | 838      |      |      | 836      |      |       | 1882        |          |          | 1052     |      |
| Approach Delay, s/veh        |      | 24.2     |      |      | 32.8     |      |       | 105.6       |          |          | 23.1     |      |
| Approach LOS                 |      | С        |      |      | С        |      |       | F           |          |          | С        |      |
| Timer                        | 1    | 2        | 3    | 4    | 5        | 6    | 7     | 8           |          |          |          |      |
| Assigned Phs                 | 1    | 2        | 3    | 4    | 5        | 6    | 7     | 8           |          |          |          |      |
| Phs Duration (G+Y+Rc), s     | 10.7 | 23.8     | 12.5 | 19.3 | 11.0     | 23.5 | 10.3  | 21.6        |          |          |          |      |
| Change Period (Y+Rc), s      | 4.5  | 4.5      | 4.5  | 4.5  | 4.5      | 4.5  | 4.5   | 4.5         |          |          |          |      |
| Max Green Setting (Gmax), s  | 6.5  | 19.0     | 8.5  | 18.0 | 6.5      | 19.0 | 7.5   | 19.0        |          |          |          |      |
| Max Q Clear Time (g_c+l1), s | 6.2  | 19.4     | 8.3  | 9.3  | 8.5      | 9.3  | 5.8   | 15.9        |          |          |          |      |
| Green Ext Time (p_c), s      | 0.0  | 0.0      | 0.0  | 2.3  | 0.0      | 3.6  | 0.1   | 1.1         |          |          |          |      |
| Intersection Summary         |      |          |      |      |          |      |       |             |          |          |          |      |
| HCM 2010 Ctrl Delay          |      |          | 58.7 |      |          |      |       |             |          |          |          |      |
| HCM 2010 LOS                 |      |          | Е    |      |          |      |       |             |          |          |          |      |
|                              |      |          |      |      |          |      |       |             |          |          |          |      |

|                              | •    | -    | •    | •    | •    | •    | 1    | Ť        | ~    | -     | ¥     | 4    |
|------------------------------|------|------|------|------|------|------|------|----------|------|-------|-------|------|
| Movement                     | EBL  | EBT  | EBR  | WBL  | WBT  | WBR  | NBL  | NBT      | NBR  | SBL   | SBT   | SBR  |
| Lane Configurations          | Ť    | ĵ.   |      | 7    | ĵ.   |      | Ţ    | <b>^</b> | 7    | 7     | f)    |      |
| Traffic Volume (veh/h)       | 15   | 179  | 87   | 202  | 236  | 231  | 62   | 186      | 216  | 177   | 115   | 10   |
| Future Volume (veh/h)        | 15   | 179  | 87   | 202  | 236  | 231  | 62   | 186      | 216  | 177   | 115   | 10   |
| Number                       | 7    | 4    | 14   | 3    | 8    | 18   | 5    | 2        | 12   | 1     | 6     | 16   |
| Initial Q (Qb), veh          | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0        | 0    | 0     | 0     | 0    |
| Ped-Bike Adj(A_pbT)          | 1.00 |      | 0.95 | 1.00 |      | 0.99 | 1.00 |          | 0.99 | 1.00  |       | 0.99 |
| Parking Bus, Adj             | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00     | 1.00 | 1.00  | 1.00  | 1.00 |
| Adj Sat Flow, veh/h/ln       | 1863 | 1863 | 1900 | 1863 | 1863 | 1900 | 1863 | 1863     | 1863 | 1863  | 1863  | 1900 |
| Adj Flow Rate, veh/h         | 18   | 213  | 104  | 240  | 281  | 275  | 74   | 221      | 257  | 211   | 137   | 12   |
| Adj No. of Lanes             | 1    | 1    | 0    | 1    | 1    | 0    | 1    | 1        | 1    | 1     | 1     | 0    |
| Peak Hour Factor             | 0.84 | 0.84 | 0.84 | 0.84 | 0.84 | 0.84 | 0.84 | 0.84     | 0.84 | 0.84  | 0.84  | 0.84 |
| Percent Heavy Veh, %         | 2    | 2    | 2    | 2    | 2    | 2    | 2    | 2        | 2    | 2     | 2     | 2    |
| Cap, veh/h                   | 38   | 264  | 129  | 277  | 312  | 306  | 99   | 512      | 432  | 132   | 495   | 43   |
| Arrive On Green              | 0.02 | 0.23 | 0.23 | 0.16 | 0.36 | 0.36 | 0.06 | 0.27     | 0.27 | 0.07  | 0.29  | 0.29 |
| Sat Flow, veh/h              | 1774 | 1160 | 566  | 1774 | 863  | 844  | 1774 | 1863     | 1572 | 1774  | 1688  | 148  |
| Grp Volume(v), veh/h         | 18   | 0    | 317  | 240  | 0    | 556  | 74   | 221      | 257  | 211   | 0     | 149  |
| Grp Sat Flow(s),veh/h/ln     | 1774 | 0    | 1726 | 1774 | 0    | 1707 | 1774 | 1863     | 1572 | 1774  | 0     | 1835 |
| Q Serve(g_s), s              | 0.7  | 0.0  | 11.7 | 8.9  | 0.0  | 20.7 | 2.8  | 6.6      | 9.5  | 5.0   | 0.0   | 4.2  |
| Cycle Q Clear(g_c), s        | 0.7  | 0.0  | 11.7 | 8.9  | 0.0  | 20.7 | 2.8  | 6.6      | 9.5  | 5.0   | 0.0   | 4.2  |
| Prop In Lane                 | 1.00 |      | 0.33 | 1.00 |      | 0.49 | 1.00 |          | 1.00 | 1.00  |       | 0.08 |
| Lane Grp Cap(c), veh/h       | 38   | 0    | 392  | 277  | 0    | 618  | 99   | 512      | 432  | 132   | 0     | 539  |
| V/C Ratio(X)                 | 0.48 | 0.00 | 0.81 | 0.87 | 0.00 | 0.90 | 0.75 | 0.43     | 0.59 | 1.60  | 0.00  | 0.28 |
| Avail Cap(c_a), veh/h        | 132  | 0    | 462  | 277  | 0    | 618  | 132  | 512      | 432  | 132   | 0     | 539  |
| HCM Platoon Ratio            | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00     | 1.00 | 1.00  | 1.00  | 1.00 |
| Upstream Filter(I)           | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00     | 1.00 | 1.00  | 0.00  | 1.00 |
| Uniform Delay (d), s/veh     | 32.6 | 0.0  | 24.6 | 27.7 | 0.0  | 20.3 | 31.3 | 20.1     | 21.1 | 31.1  | 0.0   | 18.3 |
| Incr Delay (d2), s/veh       | 9.1  | 0.0  | 8.9  | 24.0 | 0.0  | 16.2 | 15.0 | 2.6      | 5.9  | 302.8 | 0.0   | 1.3  |
| Initial Q Delay(d3),s/veh    | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0      | 0.0  | 0.0   | 0.0   | 0.0  |
| %ile BackOfQ(50%),veh/ln     | 0.4  | 0.0  | 6.5  | 6.2  | 0.0  | 12.5 | 1.8  | 3.8      | 4.8  | 13.5  | 0.0   | 2.3  |
| LnGrp Delay(d),s/veh         | 41.7 | 0.0  | 33.5 | 51.7 | 0.0  | 36.5 | 46.3 | 22.7     | 27.1 | 334.0 | 0.0   | 19.5 |
| LnGrp LOS                    | D    |      | С    | D    |      | D    | D    | C        | C    | F     |       | B    |
| Approach Vol, veh/h          |      | 335  |      |      | 796  |      |      | 552      |      |       | 360   |      |
| Approach Delay, s/veh        |      | 34.0 |      |      | 41.1 |      |      | 27.9     |      |       | 203.8 |      |
| Approach LOS                 |      | С    |      |      | D    |      |      | С        |      |       | F     |      |
| Timer                        | 1    | 2    | 3    | 4    | 5    | 6    | 7    | 8        |      |       |       |      |
| Assigned Phs                 | 1    | 2    | 3    | 4    | 5    | 6    | 7    | 8        |      |       |       |      |
| Phs Duration (G+Y+Rc), s     | 9.5  | 23.0 | 15.0 | 19.8 | 8.2  | 24.3 | 5.9  | 28.9     |      |       |       |      |
| Change Period (Y+Rc), s      | 4.5  | 4.5  | 4.5  | 4.5  | 4.5  | 4.5  | 4.5  | 4.5      |      |       |       |      |
| Max Green Setting (Gmax), s  | 5.0  | 18.5 | 10.5 | 18.0 | 5.0  | 18.5 | 5.0  | 23.5     |      |       |       |      |
| Max Q Clear Time (g_c+l1), s | 7.0  | 11.5 | 10.9 | 13.7 | 4.8  | 6.2  | 2.7  | 22.7     |      |       |       |      |
| Green Ext Time (p_c), s      | 0.0  | 1.3  | 0.0  | 0.7  | 0.0  | 0.6  | 0.0  | 0.3      |      |       |       |      |
| Intersection Summary         |      |      |      |      |      |      |      |          |      |       |       |      |
| HCM 2010 Ctrl Delay          |      |      | 65.0 |      |      |      |      |          |      |       |       |      |
| HCM 2010 LOS                 |      |      | Е    |      |      |      |      |          |      |       |       |      |

|                              | ۶    | <b>→</b> | •    | •    | <b>←</b> | •    | 1    | <b>†</b> | <b>/</b> | <b>/</b> | <b>+</b> | 4    |
|------------------------------|------|----------|------|------|----------|------|------|----------|----------|----------|----------|------|
| Movement                     | EBL  | EBT      | EBR  | WBL  | WBT      | WBR  | NBL  | NBT      | NBR      | SBL      | SBT      | SBR  |
| Lane Configurations          | ,    | <b>^</b> | 7    | , J  | <b>^</b> | 7    | J.   | <b>†</b> | 7        | J.       | <b>†</b> | 7    |
| Traffic Volume (veh/h)       | 46   | 248      | 15   | 40   | 490      | 25   | 45   | 4        | 63       | 39       | 3        | 140  |
| Future Volume (veh/h)        | 46   | 248      | 15   | 40   | 490      | 25   | 45   | 4        | 63       | 39       | 3        | 140  |
| Number                       | 7    | 4        | 14   | 3    | 8        | 18   | 5    | 2        | 12       | 1        | 6        | 16   |
| Initial Q (Qb), veh          | 0    | 0        | 0    | 0    | 0        | 0    | 0    | 0        | 0        | 0        | 0        | 0    |
| Ped-Bike Adj(A_pbT)          | 1.00 |          | 1.00 | 1.00 |          | 1.00 | 1.00 |          | 1.00     | 1.00     |          | 1.00 |
| Parking Bus, Adj             | 1.00 | 1.00     | 1.00 | 1.00 | 1.00     | 1.00 | 1.00 | 1.00     | 1.00     | 1.00     | 1.00     | 1.00 |
| Adj Sat Flow, veh/h/ln       | 1759 | 1759     | 1759 | 1827 | 1827     | 1827 | 1863 | 1863     | 1863     | 1845     | 1845     | 1845 |
| Adj Flow Rate, veh/h         | 48   | 261      | 16   | 42   | 516      | 26   | 47   | 4        | 66       | 41       | 3        | 147  |
| Adj No. of Lanes             | 1    | 2        | 1    | 1    | 2        | 1    | 1    | 1        | 1        | 1        | 1        | 1    |
| Peak Hour Factor             | 0.95 | 0.95     | 0.95 | 0.95 | 0.95     | 0.95 | 0.95 | 0.95     | 0.95     | 0.95     | 0.95     | 0.95 |
| Percent Heavy Veh, %         | 8    | 8        | 8    | 4    | 4        | 4    | 2    | 2        | 2        | 3        | 3        | 3    |
| Cap, veh/h                   | 93   | 1017     | 454  | 86   | 1036     | 463  | 465  | 325      | 276      | 478      | 322      | 274  |
| Arrive On Green              | 0.06 | 0.30     | 0.30 | 0.05 | 0.30     | 0.30 | 0.17 | 0.17     | 0.17     | 0.17     | 0.17     | 0.17 |
| Sat Flow, veh/h              | 1675 | 3343     | 1493 | 1740 | 3471     | 1553 | 1232 | 1863     | 1583     | 1312     | 1845     | 1568 |
| Grp Volume(v), veh/h         | 48   | 261      | 16   | 42   | 516      | 26   | 47   | 4        | 66       | 41       | 3        | 147  |
| Grp Sat Flow(s),veh/h/ln     | 1675 | 1671     | 1493 | 1740 | 1736     | 1553 | 1232 | 1863     | 1583     | 1312     | 1845     | 1568 |
| Q Serve(g_s), s              | 0.8  | 1.7      | 0.2  | 0.7  | 3.5      | 0.3  | 0.9  | 0.1      | 1.0      | 0.8      | 0.0      | 2.4  |
| Cycle Q Clear(g_c), s        | 0.8  | 1.7      | 0.2  | 0.7  | 3.5      | 0.3  | 1.0  | 0.1      | 1.0      | 0.8      | 0.0      | 2.4  |
| Prop In Lane                 | 1.00 |          | 1.00 | 1.00 |          | 1.00 | 1.00 |          | 1.00     | 1.00     |          | 1.00 |
| Lane Grp Cap(c), veh/h       | 93   | 1017     | 454  | 86   | 1036     | 463  | 465  | 325      | 276      | 478      | 322      | 274  |
| V/C Ratio(X)                 | 0.52 | 0.26     | 0.04 | 0.49 | 0.50     | 0.06 | 0.10 | 0.01     | 0.24     | 0.09     | 0.01     | 0.54 |
| Avail Cap(c_a), veh/h        | 380  | 2276     | 1017 | 395  | 2364     | 1058 | 1132 | 1334     | 1134     | 1189     | 1321     | 1123 |
| HCM Platoon Ratio            | 1.00 | 1.00     | 1.00 | 1.00 | 1.00     | 1.00 | 1.00 | 1.00     | 1.00     | 1.00     | 1.00     | 1.00 |
| Upstream Filter(I)           | 1.00 | 1.00     | 1.00 | 1.00 | 1.00     | 1.00 | 1.00 | 1.00     | 1.00     | 1.00     | 1.00     | 1.00 |
| Uniform Delay (d), s/veh     | 13.2 | 7.5      | 7.0  | 13.3 | 8.3      | 7.2  | 10.2 | 9.8      | 10.2     | 10.1     | 9.8      | 10.8 |
| Incr Delay (d2), s/veh       | 4.4  | 0.1      | 0.0  | 4.2  | 0.4      | 0.0  | 0.1  | 0.0      | 0.4      | 0.1      | 0.0      | 1.6  |
| Initial Q Delay(d3),s/veh    | 0.0  | 0.0      | 0.0  | 0.0  | 0.0      | 0.0  | 0.0  | 0.0      | 0.0      | 0.0      | 0.0      | 0.0  |
| %ile BackOfQ(50%),veh/ln     | 0.5  | 0.8      | 0.1  | 0.4  | 1.7      | 0.2  | 0.3  | 0.0      | 0.5      | 0.3      | 0.0      | 1.2  |
| LnGrp Delay(d),s/veh         | 17.5 | 7.6      | 7.0  | 17.4 | 8.6      | 7.2  | 10.3 | 9.8      | 10.6     | 10.2     | 9.8      | 12.4 |
| LnGrp LOS                    | В    | Α        | Α    | В    | Α        | Α    | В    | Α        | В        | В        | Α        | В    |
| Approach Vol, veh/h          |      | 325      |      |      | 584      |      |      | 117      |          |          | 191      |      |
| Approach Delay, s/veh        |      | 9.1      |      |      | 9.2      |      |      | 10.4     |          |          | 11.9     |      |
| Approach LOS                 |      | Α        |      |      | А        |      |      | В        |          |          | В        |      |
| Timer                        | 1    | 2        | 3    | 4    | 5        | 6    | 7    | 8        |          |          |          |      |
| Assigned Phs                 |      | 2        | 3    | 4    |          | 6    | 7    | 8        |          |          |          |      |
| Phs Duration (G+Y+Rc), s     |      | 9.5      | 5.9  | 13.2 |          | 9.5  | 6.1  | 13.0     |          |          |          |      |
| Change Period (Y+Rc), s      |      | 4.5      | 4.5  | 4.5  |          | 4.5  | 4.5  | 4.5      |          |          |          |      |
| Max Green Setting (Gmax), s  |      | 20.5     | 6.5  | 19.5 |          | 20.5 | 6.5  | 19.5     |          |          |          |      |
| Max Q Clear Time (g_c+l1), s |      | 3.0      | 2.7  | 3.7  |          | 4.4  | 2.8  | 5.5      |          |          |          |      |
| Green Ext Time (p_c), s      |      | 0.3      | 0.0  | 1.5  |          | 0.5  | 0.0  | 3.0      |          |          |          |      |
| Intersection Summary         |      |          |      |      |          |      |      |          |          |          |          |      |
| HCM 2010 Ctrl Delay          |      |          | 9.7  |      |          |      |      |          |          |          |          |      |
| HCM 2010 LOS                 |      |          | Α    |      |          |      |      |          |          |          |          |      |

| Intersection                                |        |             |             |              |              |          |
|---|--------|-------------|-------------|--------------|--------------|----------|
| Int Delay, s/veh                            | 3.7    |             |             |              |              |          |
| Movement                                    | WBL    | WBR         | NBT         | NBR          | SBL          | SBT      |
| Lane Configurations                         | */*    |             | ₽           |              | ሻ            | <b>†</b> |
| Traffic Vol, veh/h                          | 35     | 132         | 300         | 32           | 37           | 188      |
| Future Vol, veh/h                           | 35     | 132         | 300         | 32           | 37           | 188      |
| Conflicting Peds, #/hr                      | 0      | 0           | 0           | 1            | 1            | 0        |
| Sign Control                                | Stop   | Stop        | Free        | Free         | Free         | Free     |
| RT Channelized                              | -      | None        | -           | None         | -            | None     |
| Storage Length                              | 0      | -           | _           | -            | 150          | -        |
| Veh in Median Storage                       |        | _           | 0           | _            | -            | 0        |
| Grade, %                                    | 0      | _           | 0           | _            | _            | 0        |
| Peak Hour Factor                            | 84     | 84          | 84          | 84           | 84           | 84       |
| Heavy Vehicles, %                           | 2      | 2           | 7           | 7            | 7            | 7        |
| Mymt Flow                                   | 42     | 157         | 357         | 38           | 44           | 224      |
| IVIVIIIL FIOW                               | 42     | 157         | 331         | 30           | 44           | 224      |
|   |        |             |             |              |              |          |
| Major/Minor N                               | Minor1 | N           | Major1      | 1            | Major2       |          |
| Conflicting Flow All                        | 689    | 377         | 0           | 0            | 396          | 0        |
| Stage 1                                     | 377    | -           | -           | -            | -            | -        |
| Stage 2                                     | 312    | -           | -           | -            | -            | -        |
| Critical Hdwy                               | 6.42   | 6.22        | -           | -            | 4.17         | -        |
| Critical Hdwy Stg 1                         | 5.42   | -           | -           | -            | _            | -        |
| Critical Hdwy Stg 2                         | 5.42   | -           | -           | -            | -            | -        |
| Follow-up Hdwy                              |        | 3.318       | _           | _            | 2.263        | -        |
| Pot Cap-1 Maneuver                          | 412    | 670         | -           | -            | 1136         | -        |
| Stage 1                                     | 694    | -           | _           | _            | _            | _        |
| Stage 2                                     | 742    | _           | -           | -            | -            | _        |
| Platoon blocked, %                          |        |             | _           | _            |              | _        |
| Mov Cap-1 Maneuver                          | 396    | 669         | _           | _            | 1135         | _        |
| Mov Cap-2 Maneuver                          | 396    | -           | _           | _            | -            | _        |
| Stage 1                                     | 666    | _           | _           | _            | _            | _        |
| Stage 2                                     | 742    | _           | _           | _            | _            | _        |
| Glage 2                                     | 142    |             |             |              |              |          |
|   |        |             |             |              |              |          |
| Approach                                    | WB     |             | NB          |              | SB           |          |
| HCM Control Delay, s                        | 14.3   |             | 0           |              | 1.4          |          |
| HCM LOS                                     | В      |             |             |              |              |          |
|   |        |             |             |              |              |          |
| Minor Long/Major Mars                       | .+     | NBT         | NBRV        | VDI -1       | SBL          | SBT      |
| Minor Lane/Major Mvm                        | IL     | INDI        | NDKV        |              |              | SDI      |
|   |        |             |             |              |              | _        |
| Capacity (veh/h)                            |        | -           | -           | 585          | 1135         |          |
| HCM Lane V/C Ratio                          |        | -           | -           | 0.34         | 0.039        | -        |
| HCM Lane V/C Ratio<br>HCM Control Delay (s) |        | -           | -<br>-<br>- | 0.34<br>14.3 | 0.039<br>8.3 | -        |
| HCM Lane V/C Ratio                          |        | -<br>-<br>- | -<br>-<br>- | 0.34         | 0.039        |          |

| Intersection  |      |  |  |   |      |      |
|---|------|--|--|---|------|------|
| Intersection Delay, s/veh   | 11.8 |  |  |   |      |      |
| Intersection LOS  | В    |  |  |   |      |      |
|   |      |  |  |   |      |      |
| Mayamant  | WDI  | WDD  | NDT  | NDD   | CDL  | CDT  |
| Movement  | WBL  | WBR  | NBT  | NBR   | SBL  | SBT  |
| Lane Configurations   | ¥    | 400  | <b>}</b>   | 20  | 07   | 4    |
| Traffic Vol, veh/h  | 35   | 132  | 300  | 32  | 37   | 188  |
| Future Vol, veh/h   | 35   | 132  | 300  | 32  | 37   | 188  |
| Peak Hour Factor  | 0.84 | 0.84   | 0.84   | 0.84  | 0.84 | 0.84 |
| Heavy Vehicles, %   | 2    | 2  | 7  | 7   | 7    | 7    |
| Mvmt Flow   | 42   | 157  | 357  | 38  | 44   | 224  |
| Number of Lanes   | 1    | 0  | 1  | 0   | 0    | 1    |
| Approach  | WB   |  | NB   |   | SB   |      |
| Opposing Approach   |      |  | SB   |   | NB   |      |
| Opposing Lanes  | 0    |  | 1  |   | 1    |      |
| Conflicting Approach Left   | NB   |  |  |   | WB   |      |
| Conflicting Lanes Left  | 1    |  | 0  |   | 1    |      |
| Conflicting Approach Right  | SB   |  | WB   |   |      |      |
| Conflicting Lanes Right   | 1    |  | 1  |   | 0    |      |
| HCM Control Delay   | 10.1 |  | 13.1   |   | 11.1 |      |
| HCM LOS   | В    |  | В  |   | В    |      |
|   |      |  |  |   |      |      |
| Lane  |      | NBLn1  | WBLn1  | SBLn1   |      |      |
| Vol Left, %   |      | 0%   | 21%  | 16%   |      |      |
| Vol Thru, %   |      |  |  |   |      |      |
|   |      | 90%  | 0%   | 84%   |      |      |
| Vol Right, %  |      | 90%  | 0%<br>79%  | 84%<br>0%   |      |      |
| Vol Right, %<br>Sign Control  |      |  |  |   |      |      |
|   |      | 10%  | 79%  | 0%  |      |      |
| Sign Control  |      | 10%<br>Stop  | 79%<br>Stop  | 0%<br>Stop  |      |      |
| Sign Control<br>Traffic Vol by Lane<br>LT Vol   |      | 10%<br>Stop<br>332   | 79%<br>Stop<br>167   | 0%<br>Stop<br>225<br>37   |      |      |
| Sign Control Traffic Vol by Lane  |      | 10%<br>Stop<br>332<br>0  | 79%<br>Stop<br>167<br>35   | 0%<br>Stop<br>225   |      |      |
| Sign Control Traffic Vol by Lane LT Vol Through Vol   |      | 10%<br>Stop<br>332<br>0<br>300<br>32   | 79%<br>Stop<br>167<br>35<br>0  | 0%<br>Stop<br>225<br>37<br>188  |      |      |
| Sign Control Traffic Vol by Lane LT Vol Through Vol RT Vol Lane Flow Rate   |      | 10%<br>Stop<br>332<br>0<br>300   | 79%<br>Stop<br>167<br>35<br>0<br>132   | 0%<br>Stop<br>225<br>37<br>188<br>0   |      |      |
| Sign Control Traffic Vol by Lane LT Vol Through Vol RT Vol Lane Flow Rate Geometry Grp  |      | 10%<br>Stop<br>332<br>0<br>300<br>32<br>395  | 79%<br>Stop<br>167<br>35<br>0<br>132<br>199  | 0%<br>Stop<br>225<br>37<br>188<br>0<br>268                                      |      |      |
| Sign Control Traffic Vol by Lane LT Vol Through Vol RT Vol Lane Flow Rate Geometry Grp Degree of Util (X)   |      | 10%<br>Stop<br>332<br>0<br>300<br>32<br>395  | 79%<br>Stop<br>167<br>35<br>0<br>132<br>199  | 0%<br>Stop<br>225<br>37<br>188<br>0<br>268                                      |      |      |
| Sign Control Traffic Vol by Lane LT Vol Through Vol RT Vol Lane Flow Rate Geometry Grp Degree of Util (X) Departure Headway (Hd)  |      | 10%<br>Stop<br>332<br>0<br>300<br>32<br>395<br>1<br>0.526  | 79%<br>Stop<br>167<br>35<br>0<br>132<br>199<br>1   | 0%<br>Stop<br>225<br>37<br>188<br>0<br>268<br>1<br>0.374                        |      |      |
| Sign Control Traffic Vol by Lane LT Vol Through Vol RT Vol Lane Flow Rate Geometry Grp Degree of Util (X)   |      | 10%<br>Stop<br>332<br>0<br>300<br>32<br>395<br>1<br>0.526<br>4.793                                 | 79%<br>Stop<br>167<br>35<br>0<br>132<br>199<br>1<br>0.278<br>5.033                                 | 0%<br>Stop<br>225<br>37<br>188<br>0<br>268<br>1<br>0.374<br>5.022               |      |      |
| Sign Control Traffic Vol by Lane LT Vol Through Vol RT Vol Lane Flow Rate Geometry Grp Degree of Util (X) Departure Headway (Hd) Convergence, Y/N                                     |      | 10%<br>Stop<br>332<br>0<br>300<br>32<br>395<br>1<br>0.526<br>4.793<br>Yes                          | 79%<br>Stop<br>167<br>35<br>0<br>132<br>199<br>1<br>0.278<br>5.033<br>Yes                          | 0%<br>Stop<br>225<br>37<br>188<br>0<br>268<br>1<br>0.374<br>5.022<br>Yes        |      |      |
| Sign Control Traffic Vol by Lane LT Vol Through Vol RT Vol Lane Flow Rate Geometry Grp Degree of Util (X) Departure Headway (Hd) Convergence, Y/N Cap                                 |      | 10%<br>Stop<br>332<br>0<br>300<br>32<br>395<br>1<br>0.526<br>4.793<br>Yes<br>747                   | 79% Stop 167 35 0 132 199 1 0.278 5.033 Yes 706  | 0%<br>Stop<br>225<br>37<br>188<br>0<br>268<br>1<br>0.374<br>5.022<br>Yes<br>710 |      |      |
| Sign Control Traffic Vol by Lane LT Vol Through Vol RT Vol Lane Flow Rate Geometry Grp Degree of Util (X) Departure Headway (Hd) Convergence, Y/N Cap Service Time                    |      | 10%<br>Stop<br>332<br>0<br>300<br>32<br>395<br>1<br>0.526<br>4.793<br>Yes<br>747<br>2.866          | 79%<br>Stop<br>167<br>35<br>0<br>132<br>199<br>1<br>0.278<br>5.033<br>Yes<br>706<br>3.119          | 0% Stop 225 37 188 0 268 1 0.374 5.022 Yes 710 3.102                            |      |      |
| Sign Control Traffic Vol by Lane LT Vol Through Vol RT Vol Lane Flow Rate Geometry Grp Degree of Util (X) Departure Headway (Hd) Convergence, Y/N Cap Service Time HCM Lane V/C Ratio |      | 10%<br>Stop<br>332<br>0<br>300<br>32<br>395<br>1<br>0.526<br>4.793<br>Yes<br>747<br>2.866<br>0.529 | 79%<br>Stop<br>167<br>35<br>0<br>132<br>199<br>1<br>0.278<br>5.033<br>Yes<br>706<br>3.119<br>0.282 | 0% Stop 225 37 188 0 268 1 0.374 5.022 Yes 710 3.102 0.377                      |      |      |

|                              | ۶    | <b>→</b>   | •    | <b>√</b> | <b>←</b>   | •    | 4    | †    | ~    | <b>\</b> | <b></b> | 4    |
|------------------------------|------|------------|------|----------|------------|------|------|------|------|----------|---------|------|
| Movement                     | EBL  | EBT        | EBR  | WBL      | WBT        | WBR  | NBL  | NBT  | NBR  | SBL      | SBT     | SBR  |
| Lane Configurations          | ሻ    | <b>↑</b> ↑ |      | ሻ        | <b>∱</b> } |      |      | 4    |      |          | 4       | •    |
| Traffic Volume (veh/h)       | 6    | 328        | 118  | 91       | 700        | 19   | 207  | 68   | 160  | 18       | 24      | 12   |
| Future Volume (veh/h)        | 6    | 328        | 118  | 91       | 700        | 19   | 207  | 68   | 160  | 18       | 24      | 12   |
| Number                       | 7    | 4          | 14   | 3        | 8          | 18   | 5    | 2    | 12   | 1        | 6       | 16   |
| Initial Q (Qb), veh          | 0    | 0          | 0    | 0        | 0          | 0    | 0    | 0    | 0    | 0        | 0       | 0    |
| Ped-Bike Adj(A_pbT)          | 1.00 |            | 1.00 | 1.00     |            | 1.00 | 1.00 |      | 1.00 | 1.00     |         | 1.00 |
| Parking Bus, Adj             | 1.00 | 1.00       | 1.00 | 1.00     | 1.00       | 1.00 | 1.00 | 1.00 | 1.00 | 1.00     | 1.00    | 1.00 |
| Adj Sat Flow, veh/h/ln       | 1827 | 1827       | 1900 | 1845     | 1845       | 1900 | 1900 | 1810 | 1900 | 1900     | 1776    | 1900 |
| Adj Flow Rate, veh/h         | 7    | 373        | 134  | 103      | 795        | 22   | 235  | 77   | 182  | 20       | 27      | 14   |
| Adj No. of Lanes             | 1    | 2          | 0    | 1        | 2          | 0    | 0    | 1    | 0    | 0        | 1       | 0    |
| Peak Hour Factor             | 0.88 | 0.88       | 0.88 | 0.88     | 0.88       | 0.88 | 0.88 | 0.88 | 0.88 | 0.88     | 0.88    | 0.88 |
| Percent Heavy Veh, %         | 4    | 4          | 4    | 3        | 3          | 3    | 5    | 5    | 5    | 7        | 7       | 7    |
| Cap, veh/h                   | 16   | 574        | 203  | 131      | 1023       | 28   | 385  | 125  | 239  | 259      | 328     | 147  |
| Arrive On Green              | 0.01 | 0.23       | 0.23 | 0.07     | 0.29       | 0.29 | 0.44 | 0.44 | 0.44 | 0.44     | 0.44    | 0.44 |
| Sat Flow, veh/h              | 1740 | 2514       | 891  | 1757     | 3484       | 96   | 646  | 285  | 543  | 381      | 746     | 336  |
| Grp Volume(v), veh/h         | 7    | 256        | 251  | 103      | 400        | 417  | 494  | 0    | 0    | 61       | 0       | 0    |
| Grp Sat Flow(s),veh/h/ln     | 1740 | 1736       | 1670 | 1757     | 1752       | 1828 | 1475 | 0    | 0    | 1463     | 0       | 0    |
| Q Serve(g_s), s              | 0.2  | 7.0        | 7.2  | 3.0      | 10.9       | 10.9 | 13.1 | 0.0  | 0.0  | 0.0      | 0.0     | 0.0  |
| Cycle Q Clear(g_c), s        | 0.2  | 7.0        | 7.2  | 3.0      | 10.9       | 10.9 | 14.6 | 0.0  | 0.0  | 1.1      | 0.0     | 0.0  |
| Prop In Lane                 | 1.00 |            | 0.53 | 1.00     |            | 0.05 | 0.48 |      | 0.37 | 0.33     |         | 0.23 |
| Lane Grp Cap(c), veh/h       | 16   | 396        | 381  | 131      | 515        | 537  | 749  | 0    | 0    | 734      | 0       | 0    |
| V/C Ratio(X)                 | 0.44 | 0.65       | 0.66 | 0.79     | 0.78       | 0.78 | 0.66 | 0.00 | 0.00 | 0.08     | 0.00    | 0.00 |
| Avail Cap(c_a), veh/h        | 166  | 597        | 574  | 185      | 619        | 646  | 749  | 0    | 0    | 734      | 0       | 0    |
| HCM Platoon Ratio            | 1.00 | 1.00       | 1.00 | 1.00     | 1.00       | 1.00 | 1.00 | 1.00 | 1.00 | 1.00     | 1.00    | 1.00 |
| Upstream Filter(I)           | 1.00 | 1.00       | 1.00 | 1.00     | 1.00       | 1.00 | 1.00 | 0.00 | 0.00 | 1.00     | 0.00    | 0.00 |
| Uniform Delay (d), s/veh     | 25.8 | 18.3       | 18.3 | 23.8     | 16.9       | 16.9 | 12.2 | 0.0  | 0.0  | 8.5      | 0.0     | 0.0  |
| Incr Delay (d2), s/veh       | 17.4 | 1.8        | 1.9  | 13.6     | 5.2        | 5.0  | 4.5  | 0.0  | 0.0  | 0.2      | 0.0     | 0.0  |
| Initial Q Delay(d3),s/veh    | 0.0  | 0.0        | 0.0  | 0.0      | 0.0        | 0.0  | 0.0  | 0.0  | 0.0  | 0.0      | 0.0     | 0.0  |
| %ile BackOfQ(50%),veh/ln     | 0.2  | 3.5        | 3.5  | 2.0      | 6.0        | 6.2  | 6.8  | 0.0  | 0.0  | 0.6      | 0.0     | 0.0  |
| LnGrp Delay(d),s/veh         | 43.2 | 20.1       | 20.3 | 37.4     | 22.1       | 21.9 | 16.8 | 0.0  | 0.0  | 8.8      | 0.0     | 0.0  |
| LnGrp LOS                    | D    | С          | С    | D        | С          | С    | В    |      |      | Α        |         |      |
| Approach Vol, veh/h          |      | 514        |      |          | 920        |      |      | 494  |      |          | 61      |      |
| Approach Delay, s/veh        |      | 20.5       |      |          | 23.7       |      |      | 16.8 |      |          | 8.8     |      |
| Approach LOS                 |      | C          |      |          | C          |      |      | В    |      |          | A       |      |
| Timer                        | 1    | 2          | 3    | 4        | 5          | 6    | 7    | 8    |      |          |         |      |
| Assigned Phs                 |      | 2          | 3    | 4        |            | 6    | 7    | 8    |      |          |         |      |
| Phs Duration (G+Y+Rc), s     |      | 27.5       | 8.4  | 16.5     |            | 27.5 | 5.0  | 19.9 |      |          |         |      |
| Change Period (Y+Rc), s      |      | 4.5        | 4.5  | 4.5      |            | 4.5  | 4.5  | 4.5  |      |          |         |      |
| Max Green Setting (Gmax), s  |      | 23.0       | 5.5  | 18.0     |            | 23.0 | 5.0  | 18.5 |      |          |         |      |
| Max Q Clear Time (g_c+l1), s |      | 16.6       | 5.0  | 9.2      |            | 3.1  | 2.2  | 12.9 |      |          |         |      |
| Green Ext Time (p_c), s      |      | 1.7        | 0.0  | 2.1      |            | 0.2  | 0.0  | 2.4  |      |          |         |      |
| Intersection Summary         |      |            |      |          |            |      |      |      |      |          |         |      |
| HCM 2010 Ctrl Delay          |      |            | 20.7 |          |            |      |      |      |      |          |         |      |
| HCM 2010 LOS                 |      |            | С    |          |            |      |      |      |      |          |         |      |
|                              |      |            |      |          |            |      |      |      |      |          |         |      |

|                              | ۶    | <b>→</b> | •    | •    | <b>←</b> | •    | 1    | <b>†</b> | <b>/</b> | <b>/</b> | Ţ    | 4    |
|------------------------------|------|----------|------|------|----------|------|------|----------|----------|----------|------|------|
| Movement                     | EBL  | EBT      | EBR  | WBL  | WBT      | WBR  | NBL  | NBT      | NBR      | SBL      | SBT  | SBR  |
| Lane Configurations          | , J  | <b>^</b> | 7    | 7    | <b>^</b> | 7    | ሻሻ   | f)       |          | 7        | f)   |      |
| Traffic Volume (veh/h)       | 11   | 537      | 383  | 67   | 767      | 28   | 762  | 25       | 64       | 46       | 23   | 5    |
| Future Volume (veh/h)        | 11   | 537      | 383  | 67   | 767      | 28   | 762  | 25       | 64       | 46       | 23   | 5    |
| Number                       | 7    | 4        | 14   | 3    | 8        | 18   | 5    | 2        | 12       | 1        | 6    | 16   |
| Initial Q (Qb), veh          | 0    | 0        | 0    | 0    | 0        | 0    | 0    | 0        | 0        | 0        | 0    | 0    |
| Ped-Bike Adj(A_pbT)          | 1.00 |          | 1.00 | 1.00 |          | 1.00 | 1.00 |          | 1.00     | 1.00     |      | 1.00 |
| Parking Bus, Adj             | 1.00 | 1.00     | 1.00 | 1.00 | 1.00     | 1.00 | 1.00 | 1.00     | 1.00     | 1.00     | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln       | 1696 | 1696     | 1696 | 1624 | 1624     | 1624 | 1863 | 1863     | 1900     | 1810     | 1810 | 1900 |
| Adj Flow Rate, veh/h         | 11   | 559      | 399  | 70   | 799      | 29   | 794  | 26       | 67       | 48       | 24   | 5    |
| Adj No. of Lanes             | 1    | 2        | 1    | 1    | 2        | 1    | 2    | 1        | 0        | 1        | 1    | 0    |
| Peak Hour Factor             | 0.96 | 0.96     | 0.96 | 0.96 | 0.96     | 0.96 | 0.96 | 0.96     | 0.96     | 0.96     | 0.96 | 0.96 |
| Percent Heavy Veh, %         | 12   | 12       | 12   | 17   | 17       | 17   | 2    | 2        | 2        | 5        | 5    | 5    |
| Cap, veh/h                   | 23   | 976      | 815  | 89   | 1068     | 478  | 903  | 119      | 306      | 143      | 114  | 24   |
| Arrive On Green              | 0.01 | 0.30     | 0.30 | 0.06 | 0.35     | 0.35 | 0.26 | 0.26     | 0.26     | 0.08     | 0.08 | 0.08 |
| Sat Flow, veh/h              | 1616 | 3223     | 1442 | 1547 | 3085     | 1380 | 3442 | 462      | 1191     | 1723     | 1453 | 303  |
| Grp Volume(v), veh/h         | 11   | 559      | 399  | 70   | 799      | 29   | 794  | 0        | 93       | 48       | 0    | 29   |
| Grp Sat Flow(s),veh/h/ln     | 1616 | 1612     | 1442 | 1547 | 1543     | 1380 | 1721 | 0        | 1653     | 1723     | 0    | 1756 |
| Q Serve(g_s), s              | 0.4  | 8.8      | 10.0 | 2.7  | 13.7     | 0.8  | 13.3 | 0.0      | 2.7      | 1.6      | 0.0  | 0.9  |
| Cycle Q Clear(g_c), s        | 0.4  | 8.8      | 10.0 | 2.7  | 13.7     | 8.0  | 13.3 | 0.0      | 2.7      | 1.6      | 0.0  | 0.9  |
| Prop In Lane                 | 1.00 |          | 1.00 | 1.00 |          | 1.00 | 1.00 |          | 0.72     | 1.00     |      | 0.17 |
| Lane Grp Cap(c), veh/h       | 23   | 976      | 815  | 89   | 1068     | 478  | 903  | 0        | 425      | 143      | 0    | 138  |
| V/C Ratio(X)                 | 0.49 | 0.57     | 0.49 | 0.79 | 0.75     | 0.06 | 0.88 | 0.00     | 0.22     | 0.33     | 0.00 | 0.21 |
| Avail Cap(c_a), veh/h        | 134  | 976      | 815  | 136  | 1068     | 478  | 945  | 0        | 476      | 178      | 0    | 204  |
| HCM Platoon Ratio            | 1.00 | 1.00     | 1.00 | 1.00 | 1.00     | 1.00 | 1.00 | 1.00     | 1.00     | 1.00     | 1.00 | 1.00 |
| Upstream Filter(I)           | 1.00 | 1.00     | 1.00 | 1.00 | 1.00     | 1.00 | 1.00 | 0.00     | 1.00     | 1.00     | 0.00 | 1.00 |
| Uniform Delay (d), s/veh     | 29.4 | 17.7     | 7.9  | 28.0 | 17.3     | 13.1 | 21.3 | 0.0      | 17.6     | 26.0     | 0.0  | 26.0 |
| Incr Delay (d2), s/veh       | 15.4 | 2.4      | 2.1  | 15.5 | 4.8      | 0.2  | 9.3  | 0.0      | 0.3      | 1.4      | 0.0  | 0.8  |
| Initial Q Delay(d3),s/veh    | 0.0  | 0.0      | 0.0  | 0.0  | 0.0      | 0.0  | 0.0  | 0.0      | 0.0      | 0.0      | 0.0  | 0.0  |
| %ile BackOfQ(50%),veh/ln     | 0.3  | 4.2      | 4.4  | 1.5  | 6.5      | 0.3  | 7.5  | 0.0      | 1.2      | 8.0      | 0.0  | 0.5  |
| LnGrp Delay(d),s/veh         | 44.8 | 20.1     | 10.0 | 43.5 | 22.2     | 13.4 | 30.6 | 0.0      | 17.8     | 27.4     | 0.0  | 26.7 |
| LnGrp LOS                    | D    | С        | Α    | D    | С        | В    | С    |          | В        | С        |      | С    |
| Approach Vol, veh/h          |      | 969      |      |      | 898      |      |      | 887      |          |          | 77   |      |
| Approach Delay, s/veh        |      | 16.2     |      |      | 23.5     |      |      | 29.3     |          |          | 27.1 |      |
| Approach LOS                 |      | В        |      |      | С        |      |      | С        |          |          | С    |      |
| Timer                        | 1    | 2        | 3    | 4    | 5        | 6    | 7    | 8        |          |          |      |      |
| Assigned Phs                 | 1    | 2        | 3    | 4    | 5        | 6    | 7    | 8        |          |          |      |      |
| Phs Duration (G+Y+Rc), s     | 9.5  | 20.0     | 7.9  | 22.7 | 20.3     | 9.2  | 5.3  | 25.3     |          |          |      |      |
| Change Period (Y+Rc), s      | 4.5  | 4.5      | 4.5  | 4.5  | 4.5      | 4.5  | 4.5  | 4.5      |          |          |      |      |
| Max Green Setting (Gmax), s  | 6.2  | 17.3     | 5.3  | 18.2 | 16.5     | 7.0  | 5.0  | 18.5     |          |          |      |      |
| Max Q Clear Time (g_c+l1), s | 3.6  | 4.7      | 4.7  | 12.0 | 15.3     | 2.9  | 2.4  | 15.7     |          |          |      |      |
| Green Ext Time (p_c), s      | 0.0  | 0.3      | 0.0  | 2.8  | 0.5      | 0.0  | 0.0  | 1.5      |          |          |      |      |
| Intersection Summary         |      |          |      |      |          |      |      |          |          |          |      |      |
| HCM 2010 Ctrl Delay          |      |          | 22.9 |      |          |      |      |          |          |          |      |      |
| HCM 2010 LOS                 |      |          | С    |      |          |      |      |          |          |          |      |      |

| -                            | ۶    | <b>→</b> | •    | •    | <b>←</b> | •    | •    | <b>†</b>    | ~    | <b>/</b> | <b>+</b> | ✓    |
|------------------------------|------|----------|------|------|----------|------|------|-------------|------|----------|----------|------|
| Movement                     | EBL  | EBT      | EBR  | WBL  | WBT      | WBR  | NBL  | NBT         | NBR  | SBL      | SBT      | SBR  |
| Lane Configurations          | 1,1  | <b>^</b> | 7    | 7    | <b>^</b> | 7    | ሻሻ   | <b>↑</b> ↑₽ |      | ሻሻ       | ተተተ      | 7    |
| Traffic Volume (veh/h)       | 256  | 256      | 125  | 149  | 469      | 364  | 193  | 831         | 66   | 238      | 528      | 192  |
| Future Volume (veh/h)        | 256  | 256      | 125  | 149  | 469      | 364  | 193  | 831         | 66   | 238      | 528      | 192  |
| Number                       | 7    | 4        | 14   | 3    | 8        | 18   | 5    | 2           | 12   | 1        | 6        | 16   |
| Initial Q (Qb), veh          | 0    | 0        | 0    | 0    | 0        | 0    | 0    | 0           | 0    | 0        | 0        | 0    |
| Ped-Bike Adj(A_pbT)          | 1.00 |          | 0.98 | 1.00 |          | 0.97 | 1.00 |             | 1.00 | 1.00     |          | 1.00 |
| Parking Bus, Adj             | 1.00 | 1.00     | 1.00 | 1.00 | 1.00     | 1.00 | 1.00 | 1.00        | 1.00 | 1.00     | 1.00     | 1.00 |
| Adj Sat Flow, veh/h/ln       | 1863 | 1863     | 1863 | 1863 | 1863     | 1863 | 1863 | 1863        | 1900 | 1845     | 1845     | 1845 |
| Adj Flow Rate, veh/h         | 281  | 281      | 137  | 164  | 515      | 400  | 212  | 913         | 73   | 262      | 580      | 211  |
| Adj No. of Lanes             | 2    | 2        | 1    | 1    | 2        | 1    | 2    | 3           | 0    | 2        | 3        | 1    |
| Peak Hour Factor             | 0.91 | 0.91     | 0.91 | 0.91 | 0.91     | 0.91 | 0.91 | 0.91        | 0.91 | 0.91     | 0.91     | 0.91 |
| Percent Heavy Veh, %         | 2    | 2        | 2    | 2    | 2        | 2    | 2    | 2           | 2    | 3        | 3        | 3    |
| Cap, veh/h                   | 373  | 918      | 529  | 202  | 938      | 406  | 273  | 1314        | 105  | 319      | 1451     | 620  |
| Arrive On Green              | 0.11 | 0.26     | 0.26 | 0.11 | 0.26     | 0.26 | 0.08 | 0.27        | 0.27 | 0.09     | 0.29     | 0.29 |
| Sat Flow, veh/h              | 3442 | 3539     | 1558 | 1774 | 3539     | 1533 | 3442 | 4802        | 383  | 3408     | 5036     | 1561 |
| Grp Volume(v), veh/h         | 281  | 281      | 137  | 164  | 515      | 400  | 212  | 644         | 342  | 262      | 580      | 211  |
| Grp Sat Flow(s),veh/h/ln     | 1721 | 1770     | 1558 | 1774 | 1770     | 1533 | 1721 | 1695        | 1794 | 1704     | 1679     | 1561 |
| Q Serve(g_s), s              | 5.5  | 4.4      | 4.4  | 6.3  | 8.7      | 18.0 | 4.2  | 11.8        | 11.9 | 5.2      | 6.4      | 6.5  |
| Cycle Q Clear(g_c), s        | 5.5  | 4.4      | 4.4  | 6.3  | 8.7      | 18.0 | 4.2  | 11.8        | 11.9 | 5.2      | 6.4      | 6.5  |
| Prop In Lane                 | 1.00 |          | 1.00 | 1.00 |          | 1.00 | 1.00 |             | 0.21 | 1.00     |          | 1.00 |
| Lane Grp Cap(c), veh/h       | 373  | 918      | 529  | 202  | 938      | 406  | 273  | 928         | 491  | 319      | 1451     | 620  |
| V/C Ratio(X)                 | 0.75 | 0.31     | 0.26 | 0.81 | 0.55     | 0.98 | 0.78 | 0.69        | 0.70 | 0.82     | 0.40     | 0.34 |
| Avail Cap(c_a), veh/h        | 401  | 918      | 529  | 217  | 938      | 406  | 273  | 928         | 491  | 319      | 1451     | 620  |
| HCM Platoon Ratio            | 1.00 | 1.00     | 1.00 | 1.00 | 1.00     | 1.00 | 1.00 | 1.00        | 1.00 | 1.00     | 1.00     | 1.00 |
| Upstream Filter(I)           | 1.00 | 1.00     | 1.00 | 1.00 | 1.00     | 1.00 | 1.00 | 1.00        | 1.00 | 1.00     | 1.00     | 1.00 |
| Uniform Delay (d), s/veh     | 30.0 | 20.7     | 16.7 | 30.0 | 21.9     | 25.4 | 31.4 | 22.6        | 22.6 | 30.9     | 19.9     | 14.6 |
| Incr Delay (d2), s/veh       | 7.3  | 0.2      | 0.3  | 19.1 | 0.7      | 40.4 | 13.3 | 4.3         | 8.0  | 15.6     | 8.0      | 1.5  |
| Initial Q Delay(d3),s/veh    | 0.0  | 0.0      | 0.0  | 0.0  | 0.0      | 0.0  | 0.0  | 0.0         | 0.0  | 0.0      | 0.0      | 0.0  |
| %ile BackOfQ(50%),veh/ln     | 3.0  | 2.2      | 1.9  | 4.1  | 4.3      | 12.1 | 2.5  | 6.1         | 7.0  | 3.2      | 3.1      | 3.1  |
| LnGrp Delay(d),s/veh         | 37.3 | 20.9     | 16.9 | 49.1 | 22.6     | 65.8 | 44.6 | 26.9        | 30.6 | 46.5     | 20.7     | 16.1 |
| LnGrp LOS                    | D    | С        | В    | D    | С        | Е    | D    | С           | С    | D        | С        | В    |
| Approach Vol, veh/h          |      | 699      |      |      | 1079     |      |      | 1198        |      |          | 1053     |      |
| Approach Delay, s/veh        |      | 26.7     |      |      | 42.7     |      |      | 31.1        |      |          | 26.2     |      |
| Approach LOS                 |      | С        |      |      | D        |      |      | С           |      |          | С        |      |
| Timer                        | 1    | 2        | 3    | 4    | 5        | 6    | 7    | 8           |      |          |          |      |
| Assigned Phs                 | 1    | 2        | 3    | 4    | 5        | 6    | 7    | 8           |      |          |          |      |
| Phs Duration (G+Y+Rc), s     | 11.0 | 23.5     | 12.4 | 22.5 | 10.0     | 24.5 | 12.0 | 22.9        |      |          |          |      |
| Change Period (Y+Rc), s      | 4.5  | 4.5      | 4.5  | 4.5  | 4.5      | 4.5  | 4.5  | 4.5         |      |          |          |      |
| Max Green Setting (Gmax), s  | 6.5  | 19.0     | 8.5  | 18.0 | 5.5      | 20.0 | 8.1  | 18.4        |      |          |          |      |
| Max Q Clear Time (g_c+l1), s | 7.2  | 13.9     | 8.3  | 6.4  | 6.2      | 8.5  | 7.5  | 20.0        |      |          |          |      |
| Green Ext Time (p_c), s      | 0.0  | 2.8      | 0.0  | 1.7  | 0.0      | 3.7  | 0.1  | 0.0         |      |          |          |      |
| Intersection Summary         |      |          |      |      |          |      |      |             |      |          |          |      |
| HCM 2010 Ctrl Delay          |      |          | 32.2 |      |          |      |      |             |      |          |          |      |
| HCM 2010 LOS                 |      |          | С    |      |          |      |      |             |      |          |          |      |

|                              | •    | <b>→</b> | •    | •    | <b>←</b> | •    | 1    | <b>†</b> | <b>/</b> | <b>/</b> | <b>+</b> | 4    |
|------------------------------|------|----------|------|------|----------|------|------|----------|----------|----------|----------|------|
| Movement                     | EBL  | EBT      | EBR  | WBL  | WBT      | WBR  | NBL  | NBT      | NBR      | SBL      | SBT      | SBR  |
| Lane Configurations          | ř    | <b>^</b> | 7    | Ť    | <b>^</b> | 7    | Ţ    | <b>†</b> | 7        | Ť        | <b>†</b> | 7    |
| Traffic Volume (veh/h)       | 168  | 513      | 61   | 66   | 331      | 39   | 28   | 2        | 44       | 21       | 2        | 96   |
| Future Volume (veh/h)        | 168  | 513      | 61   | 66   | 331      | 39   | 28   | 2        | 44       | 21       | 2        | 96   |
| Number                       | 7    | 4        | 14   | 3    | 8        | 18   | 5    | 2        | 12       | 1        | 6        | 16   |
| Initial Q (Qb), veh          | 0    | 0        | 0    | 0    | 0        | 0    | 0    | 0        | 0        | 0        | 0        | 0    |
| Ped-Bike Adj(A_pbT)          | 1.00 |          | 1.00 | 1.00 |          | 1.00 | 1.00 |          | 1.00     | 1.00     |          | 1.00 |
| Parking Bus, Adj             | 1.00 | 1.00     | 1.00 | 1.00 | 1.00     | 1.00 | 1.00 | 1.00     | 1.00     | 1.00     | 1.00     | 1.00 |
| Adj Sat Flow, veh/h/ln       | 1863 | 1863     | 1863 | 1863 | 1863     | 1863 | 1863 | 1863     | 1863     | 1863     | 1863     | 1863 |
| Adj Flow Rate, veh/h         | 177  | 540      | 64   | 69   | 348      | 41   | 29   | 2        | 46       | 22       | 2        | 101  |
| Adj No. of Lanes             | 1    | 2        | 1    | 1    | 2        | 1    | 1    | 1        | 1        | 1        | 1        | 1    |
| Peak Hour Factor             | 0.95 | 0.95     | 0.95 | 0.95 | 0.95     | 0.95 | 0.95 | 0.95     | 0.95     | 0.95     | 0.95     | 0.95 |
| Percent Heavy Veh, %         | 2    | 2        | 2    | 2    | 2        | 2    | 2    | 2        | 2        | 2        | 2        | 2    |
| Cap, veh/h                   | 233  | 1091     | 488  | 129  | 885      | 396  | 455  | 312      | 265      | 466      | 312      | 265  |
| Arrive On Green              | 0.13 | 0.31     | 0.31 | 0.07 | 0.25     | 0.25 | 0.17 | 0.17     | 0.17     | 0.17     | 0.17     | 0.17 |
| Sat Flow, veh/h              | 1774 | 3539     | 1583 | 1774 | 3539     | 1583 | 1286 | 1863     | 1583     | 1352     | 1863     | 1583 |
| Grp Volume(v), veh/h         | 177  | 540      | 64   | 69   | 348      | 41   | 29   | 2        | 46       | 22       | 2        | 101  |
| Grp Sat Flow(s),veh/h/ln     | 1774 | 1770     | 1583 | 1774 | 1770     | 1583 | 1286 | 1863     | 1583     | 1352     | 1863     | 1583 |
| Q Serve(g_s), s              | 2.9  | 3.7      | 0.9  | 1.1  | 2.4      | 0.6  | 0.6  | 0.0      | 0.7      | 0.4      | 0.0      | 1.7  |
| Cycle Q Clear(g_c), s        | 2.9  | 3.7      | 0.9  | 1.1  | 2.4      | 0.6  | 0.6  | 0.0      | 0.7      | 0.4      | 0.0      | 1.7  |
| Prop In Lane                 | 1.00 |          | 1.00 | 1.00 |          | 1.00 | 1.00 |          | 1.00     | 1.00     |          | 1.00 |
| Lane Grp Cap(c), veh/h       | 233  | 1091     | 488  | 129  | 885      | 396  | 455  | 312      | 265      | 466      | 312      | 265  |
| V/C Ratio(X)                 | 0.76 | 0.49     | 0.13 | 0.53 | 0.39     | 0.10 | 0.06 | 0.01     | 0.17     | 0.05     | 0.01     | 0.38 |
| Avail Cap(c_a), veh/h        | 623  | 2592     | 1160 | 392  | 2131     | 953  | 1014 | 1121     | 953      | 1053     | 1121     | 953  |
| HCM Platoon Ratio            | 1.00 | 1.00     | 1.00 | 1.00 | 1.00     | 1.00 | 1.00 | 1.00     | 1.00     | 1.00     | 1.00     | 1.00 |
| Upstream Filter(I)           | 1.00 | 1.00     | 1.00 | 1.00 | 1.00     | 1.00 | 1.00 | 1.00     | 1.00     | 1.00     | 1.00     | 1.00 |
| Uniform Delay (d), s/veh     | 12.5 | 8.4      | 7.5  | 13.4 | 9.3      | 8.6  | 10.6 | 10.4     | 10.7     | 10.6     | 10.4     | 11.1 |
| Incr Delay (d2), s/veh       | 5.1  | 0.3      | 0.1  | 3.4  | 0.3      | 0.1  | 0.1  | 0.0      | 0.3      | 0.0      | 0.0      | 0.9  |
| Initial Q Delay(d3),s/veh    | 0.0  | 0.0      | 0.0  | 0.0  | 0.0      | 0.0  | 0.0  | 0.0      | 0.0      | 0.0      | 0.0      | 0.0  |
| %ile BackOfQ(50%),veh/ln     | 1.7  | 1.9      | 0.4  | 0.7  | 1.2      | 0.3  | 0.2  | 0.0      | 0.3      | 0.2      | 0.0      | 0.8  |
| LnGrp Delay(d),s/veh         | 17.6 | 8.8      | 7.6  | 16.7 | 9.6      | 8.7  | 10.7 | 10.4     | 11.0     | 10.6     | 10.4     | 12.0 |
| LnGrp LOS                    | В    | Α        | Α    | В    | Α        | Α    | В    | В        | В        | В        | В        | В    |
| Approach Vol, veh/h          |      | 781      |      |      | 458      |      |      | 77       |          |          | 125      |      |
| Approach Delay, s/veh        |      | 10.7     |      |      | 10.6     |      |      | 10.9     |          |          | 11.7     |      |
| Approach LOS                 |      | В        |      |      | В        |      |      | В        |          |          | В        |      |
| Timer                        | 1    | 2        | 2    | 1    | 5        | 6    | 7    | 8        |          |          |          |      |
|                              | - 1  |          | 3    | 4    | 3        |      | 7    |          |          |          |          |      |
| Assigned Phs                 |      | 2        | 3    | 4    |          | 6    | 7    | 8        |          |          |          |      |
| Phs Duration (G+Y+Rc), s     |      | 9.5      | 6.7  | 13.7 |          | 9.5  | 8.4  | 12.0     |          |          |          |      |
| Change Period (Y+Rc), s      |      | 4.5      | 4.5  | 4.5  |          | 4.5  | 4.5  | 4.5      |          |          |          |      |
| Max Green Setting (Gmax), s  |      | 18.0     | 6.6  | 21.9 |          | 18.0 | 10.5 | 18.0     |          |          |          |      |
| Max Q Clear Time (g_c+l1), s |      | 2.7      | 3.1  | 5.7  |          | 3.7  | 4.9  | 4.4      |          |          |          |      |
| Green Ext Time (p_c), s      |      | 0.1      | 0.0  | 3.5  |          | 0.3  | 0.2  | 2.0      |          |          |          |      |
| Intersection Summary         |      |          | 40.0 |      |          |      |      |          |          |          |          |      |
| HCM 2010 Ctrl Delay          |      |          | 10.8 |      |          |      |      |          |          |          |          |      |
| HCM 2010 LOS                 |      |          | В    |      |          |      |      |          |          |          |          |      |

| Intersection  |         |               |                     |                    |                           |             |
|---|---------|---------------|---------------------|--------------------|---------------------------|-------------|
| Int Delay, s/veh  | 3.1     |               |                     |                    |                           |             |
| Movement  | WBL     | WBR           | NBT                 | NBR                | SBL                       | SBT         |
| Lane Configurations   | ₩.      | וטוי          | 1\D1                | HUIN               | JDL<br>Š                  | <u> </u>    |
| Traffic Vol, veh/h  | 30      | 76            | 185                 | 26                 | 112                       | 290         |
| Future Vol, veh/h   | 30      | 76            | 185                 | 26                 | 112                       | 290         |
| Conflicting Peds, #/hr  | 1       | 0             | 0                   | 0                  | 0                         | 0           |
| Sign Control  | Stop    | Stop          | Free                | Free               | Free                      | Free        |
| RT Channelized  | -       | None          | -                   |                    | -                         | None        |
| Storage Length  | 0       | -             | _                   | -                  | 150                       | -           |
| Veh in Median Storage,  |         | _             | 0                   | _                  | -                         | 0           |
| Grade, %  | , # 0   | <u>-</u>      | 0                   | _                  | _                         | 0           |
| Peak Hour Factor  | 91      | 91            | 91                  | 91                 | 91                        | 91          |
|   | 6       | 6             | 2                   | 2                  | 3                         | 3           |
| Heavy Vehicles, %   | 33      | 84            |                     |                    |                           | 319         |
| Mvmt Flow   | 33      | 84            | 203                 | 29                 | 123                       | 319         |
|   |         |               |                     |                    |                           |             |
| Major/Minor N   | /linor1 | N             | Major1              | 1                  | Major2                    |             |
| Conflicting Flow All  | 784     | 218           | 0                   | 0                  | 232                       | 0           |
| Stage 1   | 218     | _             | _                   | -                  | _                         | _           |
| Stage 2   | 566     | -             | -                   | -                  | _                         | -           |
| Critical Hdwy   | 6.46    | 6.26          | -                   | -                  | 4.13                      | _           |
| Critical Hdwy Stg 1   | 5.46    | -             | _                   | _                  | -                         | _           |
| Critical Hdwy Stg 2   | 5.46    | _             | _                   | _                  | _                         | _           |
|   |         | 3.354         | _                   | -                  | 2.227                     | _           |
| Pot Cap-1 Maneuver  | 356     | 812           | _                   | _                  | 1330                      | _           |
| Stage 1   | 809     | -             | _                   | _                  | -                         | _           |
| Stage 2   | 560     | _             | _                   | _                  | _                         | _           |
| Platoon blocked, %  | 000     |               | _                   | _                  |                           | _           |
| Mov Cap-1 Maneuver  | 323     | 812           | _                   | _                  | 1330                      | _           |
| Mov Cap-1 Maneuver  | 323     | - 012         | _                   | _                  | -                         | _           |
| Stage 1   | 735     | _             | _                   | _                  | _                         | _           |
| Stage 2   | 559     | _             | _                   | _                  | _                         | _           |
| Staye 2   | 555     | -             | -                   | -                  | -                         | -           |
|   |         |               |                     |                    |                           |             |
|   |         |               | NB                  |                    | SB                        |             |
| Approach  | WB      |               | שוו                 |                    |                           |             |
| Approach HCM Control Delay, s   | 13      |               | 0                   |                    | 2.2                       |             |
|   |         |               |                     |                    | 2.2                       |             |
| HCM Control Delay, s  | 13      |               |                     |                    | 2.2                       |             |
| HCM Control Delay, s<br>HCM LOS   | 13<br>B | NDT           | 0                   | VDI =4             |                           | CDT         |
| HCM Control Delay, s<br>HCM LOS<br>Minor Lane/Major Mvm                                 | 13<br>B | NBT           | 0<br>NBRV           | VBLn1              | SBL                       | SBT         |
| HCM Control Delay, s HCM LOS  Minor Lane/Major Mvm Capacity (veh/h)                     | 13<br>B | -             | 0<br>NBRV           | 568                | SBL<br>1330               | -           |
| HCM Control Delay, s HCM LOS  Minor Lane/Major Mvm Capacity (veh/h) HCM Lane V/C Ratio  | 13<br>B | NBT<br>-<br>- | 0<br>NBRV<br>-      | 568<br>0.205       | SBL<br>1330<br>0.093      | -           |
| Minor Lane/Major Mvm<br>Capacity (veh/h)<br>HCM Lane V/C Ratio<br>HCM Control Delay (s) | 13<br>B | -<br>-<br>-   | 0<br>NBRV<br>-<br>- | 568<br>0.205<br>13 | SBL<br>1330<br>0.093<br>8 | -<br>-<br>- |
| HCM Control Delay, s HCM LOS  Minor Lane/Major Mvm Capacity (veh/h) HCM Lane V/C Ratio  | 13<br>B | -             | 0<br>NBRV<br>-      | 568<br>0.205       | SBL<br>1330<br>0.093      | -           |

| Intersection   |      |   |  |  |      |      |
|--|------|---|--|--|------|------|
|  | 11.6 |   |  |  |      |      |
| Intersection Delay, s/veh  | 11.6 |   |  |  |      |      |
| Intersection LOS   | В    |   |  |  |      |      |
|  |      |   |  |  |      |      |
| Movement   | WBL  | WBR   | NBT  | NBR  | SBL  | SBT  |
| Lane Configurations  | ¥    | •   | ą.   |  |      | 4    |
| Traffic Vol, veh/h   | 30   | 76  | 185  | 26   | 112  | 290  |
| Future Vol, veh/h  | 30   | 76  | 185  | 26   | 112  | 290  |
| Peak Hour Factor   | 0.91 | 0.91  | 0.91   | 0.91   | 0.91 | 0.91 |
| Heavy Vehicles, %  | 6    | 6   | 2  | 2  | 3    | 3    |
| Mvmt Flow  | 33   | 84  | 203  | 29   | 123  | 319  |
| Number of Lanes  | 1    | 0   | 1  | 0  | 0    | 1    |
|  | MA   |   | ND   |  | CD   |      |
| Approach   | WB   |   | NB   |  | SB   |      |
| Opposing Approach  |      |   | SB   |  | NB   |      |
| Opposing Lanes   | 0    |   | 1  |  | 1    |      |
| Conflicting Approach Left  | NB   |   |  |  | WB   |      |
| Conflicting Lanes Left   | 1    |   | 0  |  | 1    |      |
| Conflicting Approach Right   | SB   |   | WB   |  |      |      |
| Conflicting Lanes Right  | 1    |   | 1  |  | 0    |      |
| HCM Control Delay  | 9.2  |   | 9.7  |  | 13.3 |      |
| HCM LOS  | Α    |   | Α  |  | В    |      |
|  |      |   |  |  |      |      |
|  |      |   |  |  |      |      |
| Lane   |      | NBLn1   | WBLn1  | SBLn1  |      |      |
| Lane Vol Left %  |      | NBLn1   | WBLn1 28%  | SBLn1  |      |      |
| Vol Left, %  |      | 0%  | 28%  | 28%  |      |      |
| Vol Left, %<br>Vol Thru, %   |      | 0%<br>88%   | 28%<br>0%  | 28%<br>72%   |      |      |
| Vol Left, %<br>Vol Thru, %<br>Vol Right, %   |      | 0%<br>88%<br>12%  | 28%<br>0%<br>72%   | 28%<br>72%<br>0%   |      |      |
| Vol Left, %<br>Vol Thru, %<br>Vol Right, %<br>Sign Control   |      | 0%<br>88%<br>12%<br>Stop  | 28%<br>0%<br>72%<br>Stop   | 28%<br>72%<br>0%<br>Stop   |      |      |
| Vol Left, % Vol Thru, % Vol Right, % Sign Control Traffic Vol by Lane  |      | 0%<br>88%<br>12%<br>Stop<br>211   | 28%<br>0%<br>72%<br>Stop<br>106  | 28%<br>72%<br>0%<br>Stop<br>402                                    |      |      |
| Vol Left, % Vol Thru, % Vol Right, % Sign Control Traffic Vol by Lane LT Vol   |      | 0%<br>88%<br>12%<br>Stop<br>211   | 28%<br>0%<br>72%<br>Stop<br>106<br>30  | 28%<br>72%<br>0%<br>Stop<br>402<br>112                             |      |      |
| Vol Left, % Vol Thru, % Vol Right, % Sign Control Traffic Vol by Lane LT Vol Through Vol   |      | 0%<br>88%<br>12%<br>Stop<br>211<br>0<br>185   | 28%<br>0%<br>72%<br>Stop<br>106<br>30<br>0   | 28%<br>72%<br>0%<br>Stop<br>402<br>112<br>290                      |      |      |
| Vol Left, % Vol Thru, % Vol Right, % Sign Control Traffic Vol by Lane LT Vol Through Vol RT Vol  |      | 0%<br>88%<br>12%<br>Stop<br>211<br>0<br>185<br>26   | 28%<br>0%<br>72%<br>Stop<br>106<br>30<br>0   | 28%<br>72%<br>0%<br>Stop<br>402<br>112<br>290                      |      |      |
| Vol Left, % Vol Thru, % Vol Right, % Sign Control Traffic Vol by Lane LT Vol Through Vol RT Vol Lane Flow Rate   |      | 0%<br>88%<br>12%<br>Stop<br>211<br>0<br>185<br>26<br>232  | 28%<br>0%<br>72%<br>Stop<br>106<br>30<br>0<br>76   | 28% 72% 0% Stop 402 112 290 0 442                                  |      |      |
| Vol Left, % Vol Thru, % Vol Right, % Sign Control Traffic Vol by Lane LT Vol Through Vol RT Vol Lane Flow Rate Geometry Grp  |      | 0%<br>88%<br>12%<br>Stop<br>211<br>0<br>185<br>26<br>232  | 28%<br>0%<br>72%<br>Stop<br>106<br>30<br>0<br>76<br>116  | 28% 72% 0% Stop 402 112 290 0 442                                  |      |      |
| Vol Left, % Vol Thru, % Vol Right, % Sign Control Traffic Vol by Lane LT Vol Through Vol RT Vol Lane Flow Rate Geometry Grp Degree of Util (X)   |      | 0%<br>88%<br>12%<br>Stop<br>211<br>0<br>185<br>26<br>232<br>1<br>0.299  | 28%<br>0%<br>72%<br>Stop<br>106<br>30<br>0<br>76<br>116<br>1   | 28% 72% 0% Stop 402 112 290 0 442 1 0.56                           |      |      |
| Vol Left, % Vol Thru, % Vol Right, % Sign Control Traffic Vol by Lane LT Vol Through Vol RT Vol Lane Flow Rate Geometry Grp Degree of Util (X) Departure Headway (Hd)  |      | 0%<br>88%<br>12%<br>Stop<br>211<br>0<br>185<br>26<br>232<br>1<br>0.299<br>4.645                                 | 28%<br>0%<br>72%<br>Stop<br>106<br>30<br>0<br>76<br>116<br>1<br>0.166<br>5.128                                 | 28% 72% 0% Stop 402 112 290 0 442 1 0.56 4.564                     |      |      |
| Vol Left, % Vol Thru, % Vol Right, % Sign Control Traffic Vol by Lane LT Vol Through Vol RT Vol Lane Flow Rate Geometry Grp Degree of Util (X) Departure Headway (Hd) Convergence, Y/N                                     |      | 0%<br>88%<br>12%<br>Stop<br>211<br>0<br>185<br>26<br>232<br>1<br>0.299<br>4.645<br>Yes                          | 28%<br>0%<br>72%<br>Stop<br>106<br>30<br>0<br>76<br>116<br>1<br>0.166<br>5.128<br>Yes                          | 28% 72% 0% Stop 402 112 290 0 442 1 0.56 4.564 Yes                 |      |      |
| Vol Left, % Vol Thru, % Vol Right, % Sign Control Traffic Vol by Lane LT Vol Through Vol RT Vol Lane Flow Rate Geometry Grp Degree of Util (X) Departure Headway (Hd) Convergence, Y/N Cap                                 |      | 0%<br>88%<br>12%<br>Stop<br>211<br>0<br>185<br>26<br>232<br>1<br>0.299<br>4.645<br>Yes<br>770                   | 28%<br>0%<br>72%<br>Stop<br>106<br>30<br>0<br>76<br>116<br>1<br>0.166<br>5.128<br>Yes<br>695                   | 28% 72% 0% Stop 402 112 290 0 442 1 0.56 4.564 Yes 786             |      |      |
| Vol Left, % Vol Thru, % Vol Right, % Sign Control Traffic Vol by Lane LT Vol Through Vol RT Vol Lane Flow Rate Geometry Grp Degree of Util (X) Departure Headway (Hd) Convergence, Y/N Cap Service Time                    |      | 0%<br>88%<br>12%<br>Stop<br>211<br>0<br>185<br>26<br>232<br>1<br>0.299<br>4.645<br>Yes<br>770<br>2.693          | 28%<br>0%<br>72%<br>Stop<br>106<br>30<br>0<br>76<br>116<br>1<br>0.166<br>5.128<br>Yes<br>695<br>3.188          | 28% 72% 0% Stop 402 112 290 0 442 1 0.56 4.564 Yes 786 2.605       |      |      |
| Vol Left, % Vol Thru, % Vol Right, % Sign Control Traffic Vol by Lane LT Vol Through Vol RT Vol Lane Flow Rate Geometry Grp Degree of Util (X) Departure Headway (Hd) Convergence, Y/N Cap Service Time HCM Lane V/C Ratio |      | 0%<br>88%<br>12%<br>Stop<br>211<br>0<br>185<br>26<br>232<br>1<br>0.299<br>4.645<br>Yes<br>770<br>2.693<br>0.301 | 28%<br>0%<br>72%<br>Stop<br>106<br>30<br>0<br>76<br>116<br>1<br>0.166<br>5.128<br>Yes<br>695<br>3.188<br>0.167 | 28% 72% 0% Stop 402 112 290 0 442 1 0.56 4.564 Yes 786 2.605 0.562 |      |      |
| Vol Left, % Vol Thru, % Vol Right, % Sign Control Traffic Vol by Lane LT Vol Through Vol RT Vol Lane Flow Rate Geometry Grp Degree of Util (X) Departure Headway (Hd) Convergence, Y/N Cap Service Time                    |      | 0%<br>88%<br>12%<br>Stop<br>211<br>0<br>185<br>26<br>232<br>1<br>0.299<br>4.645<br>Yes<br>770<br>2.693          | 28%<br>0%<br>72%<br>Stop<br>106<br>30<br>0<br>76<br>116<br>1<br>0.166<br>5.128<br>Yes<br>695<br>3.188          | 28% 72% 0% Stop 402 112 290 0 442 1 0.56 4.564 Yes 786 2.605       |      |      |

1.3

0.6

3.5

HCM 95th-tile Q

|                              | ≯    | <b>→</b> | •    | •        | <b>←</b> | •    | •    | †    | ~    | <b>\</b> | ţ    | ✓    |
|------------------------------|------|----------|------|----------|----------|------|------|------|------|----------|------|------|
| Movement                     | EBL  | EBT      | EBR  | WBL      | WBT      | WBR  | NBL  | NBT  | NBR  | SBL      | SBT  | SBR  |
| Lane Configurations          | ሻ    | ∱β       |      | <b>ነ</b> | ∱β       |      |      | 4    |      |          | 4    |      |
| Traffic Volume (veh/h)       | 28   | 633      | 172  | 167      | 382      | 17   | 127  | 49   | 102  | 28       | 79   | 12   |
| Future Volume (veh/h)        | 28   | 633      | 172  | 167      | 382      | 17   | 127  | 49   | 102  | 28       | 79   | 12   |
| Number                       | 7    | 4        | 14   | 3        | 8        | 18   | 5    | 2    | 12   | 1        | 6    | 16   |
| Initial Q (Qb), veh          | 0    | 0        | 0    | 0        | 0        | 0    | 0    | 0    | 0    | 0        | 0    | 0    |
| Ped-Bike Adj(A_pbT)          | 1.00 |          | 1.00 | 1.00     |          | 1.00 | 1.00 |      | 1.00 | 1.00     |      | 1.00 |
| Parking Bus, Adj             | 1.00 | 1.00     | 1.00 | 1.00     | 1.00     | 1.00 | 1.00 | 1.00 | 1.00 | 1.00     | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln       | 1863 | 1863     | 1900 | 1863     | 1863     | 1900 | 1900 | 1863 | 1900 | 1900     | 1827 | 1900 |
| Adj Flow Rate, veh/h         | 33   | 736      | 200  | 194      | 444      | 20   | 148  | 57   | 119  | 33       | 92   | 14   |
| Adj No. of Lanes             | 1    | 2        | 0    | 1        | 2        | 0    | 0    | 1    | 0    | 0        | 1    | 0    |
| Peak Hour Factor             | 0.86 | 0.86     | 0.86 | 0.86     | 0.86     | 0.86 | 0.86 | 0.86 | 0.86 | 0.86     | 0.86 | 0.86 |
| Percent Heavy Veh, %         | 2    | 2        | 2    | 2        | 2        | 2    | 2    | 2    | 2    | 4        | 4    | 4    |
| Cap, veh/h                   | 63   | 836      | 227  | 239      | 1390     | 63   | 287  | 121  | 185  | 166      | 415  | 57   |
| Arrive On Green              | 0.04 | 0.30     | 0.30 | 0.13     | 0.40     | 0.40 | 0.33 | 0.33 | 0.33 | 0.33     | 0.33 | 0.33 |
| Sat Flow, veh/h              | 1774 | 2752     | 748  | 1774     | 3450     | 155  | 596  | 363  | 557  | 272      | 1251 | 171  |
| Grp Volume(v), veh/h         | 33   | 473      | 463  | 194      | 227      | 237  | 324  | 0    | 0    | 139      | 0    | 0    |
| Grp Sat Flow(s),veh/h/ln     | 1774 | 1770     | 1731 | 1774     | 1770     | 1835 | 1516 | 0    | 0    | 1693     | 0    | 0    |
| Q Serve(g_s), s              | 1.1  | 14.9     | 14.9 | 6.2      | 5.2      | 5.2  | 7.0  | 0.0  | 0.0  | 0.0      | 0.0  | 0.0  |
| Cycle Q Clear(g_c), s        | 1.1  | 14.9     | 14.9 | 6.2      | 5.2      | 5.2  | 10.3 | 0.0  | 0.0  | 3.3      | 0.0  | 0.0  |
| Prop In Lane                 | 1.00 |          | 0.43 | 1.00     |          | 0.08 | 0.46 |      | 0.37 | 0.24     |      | 0.10 |
| Lane Grp Cap(c), veh/h       | 63   | 538      | 526  | 239      | 713      | 740  | 592  | 0    | 0    | 638      | 0    | 0    |
| V/C Ratio(X)                 | 0.52 | 0.88     | 0.88 | 0.81     | 0.32     | 0.32 | 0.55 | 0.00 | 0.00 | 0.22     | 0.00 | 0.00 |
| Avail Cap(c_a), veh/h        | 163  | 557      | 545  | 257      | 713      | 740  | 592  | 0    | 0    | 638      | 0    | 0    |
| HCM Platoon Ratio            | 1.00 | 1.00     | 1.00 | 1.00     | 1.00     | 1.00 | 1.00 | 1.00 | 1.00 | 1.00     | 1.00 | 1.00 |
| Upstream Filter(I)           | 1.00 | 1.00     | 1.00 | 1.00     | 1.00     | 1.00 | 1.00 | 0.00 | 0.00 | 1.00     | 0.00 | 0.00 |
| Uniform Delay (d), s/veh     | 27.9 | 19.4     | 19.4 | 24.7     | 12.0     | 12.0 | 16.4 | 0.0  | 0.0  | 14.2     | 0.0  | 0.0  |
| Incr Delay (d2), s/veh       | 6.6  | 14.7     | 15.0 | 16.8     | 0.3      | 0.2  | 3.6  | 0.0  | 0.0  | 8.0      | 0.0  | 0.0  |
| Initial Q Delay(d3),s/veh    | 0.0  | 0.0      | 0.0  | 0.0      | 0.0      | 0.0  | 0.0  | 0.0  | 0.0  | 0.0      | 0.0  | 0.0  |
| %ile BackOfQ(50%),veh/ln     | 0.6  | 9.4      | 9.3  | 4.2      | 2.6      | 2.7  | 5.0  | 0.0  | 0.0  | 1.8      | 0.0  | 0.0  |
| LnGrp Delay(d),s/veh         | 34.5 | 34.2     | 34.4 | 41.5     | 12.3     | 12.3 | 20.0 | 0.0  | 0.0  | 15.0     | 0.0  | 0.0  |
| LnGrp LOS                    | С    | С        | С    | D        | В        | В    | В    |      |      | В        |      |      |
| Approach Vol, veh/h          |      | 969      |      |          | 658      |      |      | 324  |      |          | 139  |      |
| Approach Delay, s/veh        |      | 34.3     |      |          | 20.9     |      |      | 20.0 |      |          | 15.0 |      |
| Approach LOS                 |      | С        |      |          | С        |      |      | В    |      |          | В    |      |
| Timer                        | 1    | 2        | 3    | 4        | 5        | 6    | 7    | 8    |      |          |      |      |
| Assigned Phs                 |      | 2        | 3    | 4        |          | 6    | 7    | 8    |      |          |      |      |
| Phs Duration (G+Y+Rc), s     |      | 24.0     | 12.4 | 22.4     |          | 24.0 | 6.6  | 28.2 |      |          |      |      |
| Change Period (Y+Rc), s      |      | 4.5      | 4.5  | 4.5      |          | 4.5  | 4.5  | 4.5  |      |          |      |      |
| Max Green Setting (Gmax), s  |      | 19.5     | 8.5  | 18.5     |          | 19.5 | 5.4  | 21.6 |      |          |      |      |
| Max Q Clear Time (g_c+l1), s |      | 12.3     | 8.2  | 16.9     |          | 5.3  | 3.1  | 7.2  |      |          |      |      |
| Green Ext Time (p_c), s      |      | 1.2      | 0.0  | 0.9      |          | 0.6  | 0.0  | 2.4  |      |          |      |      |
| Intersection Summary         |      |          |      |          |          |      |      |      |      |          |      |      |
| HCM 2010 Ctrl Delay          |      |          | 26.6 |          |          |      |      |      |      |          |      |      |
| HCM 2010 LOS                 |      |          | С    |          |          |      |      |      |      |          |      |      |
|                              |      |          | •    |          |          |      |      |      |      |          |      |      |

|                              | ≯    | <b>→</b> | •    | •        | <b>←</b> | •    | •    | †        | ~    | <b>&gt;</b> | Ţ    |      |
|------------------------------|------|----------|------|----------|----------|------|------|----------|------|-------------|------|------|
| Movement                     | EBL  | EBT      | EBR  | WBL      | WBT      | WBR  | NBL  | NBT      | NBR  | SBL         | SBT  | SBR  |
| Lane Configurations          | ሻ    | <b>^</b> | 7    | <b>ነ</b> | <b>^</b> | 7    | ሻሻ   | <b>₽</b> |      | <b>ነ</b>    | ₽    |      |
| Traffic Volume (veh/h)       | 1    | 681      | 706  | 108      | 705      | 27   | 539  | 16       | 141  | 132         | 154  | 1    |
| Future Volume (veh/h)        | 1    | 681      | 706  | 108      | 705      | 27   | 539  | 16       | 141  | 132         | 154  | 1    |
| Number                       | 7    | 4        | 14   | 3        | 8        | 18   | 5    | 2        | 12   | 1           | 6    | 16   |
| Initial Q (Qb), veh          | 0    | 0        | 0    | 0        | 0        | 0    | 0    | 0        | 0    | 0           | 0    | 0    |
| Ped-Bike Adj(A_pbT)          | 1.00 |          | 1.00 | 1.00     |          | 1.00 | 1.00 |          | 1.00 | 1.00        |      | 1.00 |
| Parking Bus, Adj             | 1.00 | 1.00     | 1.00 | 1.00     | 1.00     | 1.00 | 1.00 | 1.00     | 1.00 | 1.00        | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln       | 1776 | 1776     | 1776 | 1667     | 1667     | 1667 | 1863 | 1863     | 1900 | 1863        | 1863 | 1900 |
| Adj Flow Rate, veh/h         | 1    | 724      | 751  | 115      | 750      | 29   | 573  | 17       | 150  | 140         | 164  | 1    |
| Adj No. of Lanes             | 1    | 2        | 1    | 1        | 2        | 1    | 2    | 1        | 0    | 1           | 1    | 0    |
| Peak Hour Factor             | 0.94 | 0.94     | 0.94 | 0.94     | 0.94     | 0.94 | 0.94 | 0.94     | 0.94 | 0.94        | 0.94 | 0.94 |
| Percent Heavy Veh, %         | 7    | 7        | 7    | 14       | 14       | 14   | 2    | 2        | 2    | 2           | 2    | 2    |
| Cap, veh/h                   | 3    | 947      | 741  | 142      | 1167     | 522  | 725  | 36       | 320  | 198         | 227  | 1    |
| Arrive On Green              | 0.00 | 0.28     | 0.28 | 0.09     | 0.37     | 0.37 | 0.21 | 0.22     | 0.22 | 0.11        | 0.12 | 0.12 |
| Sat Flow, veh/h              | 1691 | 3374     | 1509 | 1587     | 3167     | 1417 | 3442 | 164      | 1444 | 1774        | 1849 | 11   |
| Grp Volume(v), veh/h         | 1    | 724      | 751  | 115      | 750      | 29   | 573  | 0        | 167  | 140         | 0    | 165  |
| Grp Sat Flow(s),veh/h/ln     | 1691 | 1687     | 1509 | 1587     | 1583     | 1417 | 1721 | 0        | 1608 | 1774        | 0    | 1861 |
| Q Serve(g_s), s              | 0.0  | 11.9     | 17.0 | 4.3      | 11.9     | 0.8  | 9.6  | 0.0      | 5.5  | 4.6         | 0.0  | 5.2  |
| Cycle Q Clear(g_c), s        | 0.0  | 11.9     | 17.0 | 4.3      | 11.9     | 0.8  | 9.6  | 0.0      | 5.5  | 4.6         | 0.0  | 5.2  |
| Prop In Lane                 | 1.00 |          | 1.00 | 1.00     |          | 1.00 | 1.00 |          | 0.90 | 1.00        |      | 0.01 |
| Lane Grp Cap(c), veh/h       | 3    | 947      | 741  | 142      | 1167     | 522  | 725  | 0        | 356  | 198         | 0    | 228  |
| V/C Ratio(X)                 | 0.36 | 0.76     | 1.01 | 0.81     | 0.64     | 0.06 | 0.79 | 0.00     | 0.47 | 0.71        | 0.00 | 0.72 |
| Avail Cap(c_a), veh/h        | 140  | 947      | 741  | 170      | 1167     | 522  | 994  | 0        | 435  | 354         | 0    | 338  |
| HCM Platoon Ratio            | 1.00 | 1.00     | 1.00 | 1.00     | 1.00     | 1.00 | 1.00 | 1.00     | 1.00 | 1.00        | 1.00 | 1.00 |
| Upstream Filter(I)           | 1.00 | 1.00     | 1.00 | 1.00     | 1.00     | 1.00 | 1.00 | 0.00     | 1.00 | 1.00        | 0.00 | 1.00 |
| Uniform Delay (d), s/veh     | 30.2 | 20.0     | 15.4 | 27.1     | 15.8     | 12.3 | 22.7 | 0.0      | 20.5 | 26.0        | 0.0  | 25.6 |
| Incr Delay (d2), s/veh       | 63.7 | 5.9      | 36.4 | 21.5     | 2.7      | 0.2  | 3.1  | 0.0      | 1.0  | 4.6         | 0.0  | 4.3  |
| Initial Q Delay(d3),s/veh    | 0.0  | 0.0      | 0.0  | 0.0      | 0.0      | 0.0  | 0.0  | 0.0      | 0.0  | 0.0         | 0.0  | 0.0  |
| %ile BackOfQ(50%),veh/ln     | 0.1  | 6.3      | 19.6 | 2.7      | 5.5      | 0.3  | 4.8  | 0.0      | 2.5  | 2.5         | 0.0  | 2.9  |
| LnGrp Delay(d),s/veh         | 93.9 | 25.8     | 51.8 | 48.6     | 18.6     | 12.5 | 25.7 | 0.0      | 21.4 | 30.5        | 0.0  | 29.9 |
| LnGrp LOS                    | F    | С        | F    | D        | В        | В    | С    |          | С    | С           |      | С    |
| Approach Vol, veh/h          |      | 1476     |      |          | 894      |      |      | 740      |      |             | 305  |      |
| Approach Delay, s/veh        |      | 39.1     |      |          | 22.2     |      |      | 24.7     |      |             | 30.2 |      |
| Approach LOS                 |      | D        |      |          | С        |      |      | С        |      |             | С    |      |
| Timer                        | 1    | 2        | 3    | 4        | 5        | 6    | 7    | 8        |      |             |      |      |
| Assigned Phs                 | 1    | 2        | 3    | 4        | 5        | 6    | 7    | 8        |      |             |      |      |
| Phs Duration (G+Y+Rc), s     | 11.3 | 17.9     | 9.9  | 21.5     | 17.3     | 11.9 | 4.6  | 26.8     |      |             |      |      |
| Change Period (Y+Rc), s      | 4.5  | 4.5      | 4.5  | 4.5      | 4.5      | 4.5  | 4.5  | 4.5      |      |             |      |      |
| Max Green Setting (Gmax), s  | 12.1 | 16.4     | 6.5  | 17.0     | 17.5     | 11.0 | 5.0  | 18.5     |      |             |      |      |
| Max Q Clear Time (g_c+l1), s | 6.6  | 7.5      | 6.3  | 19.0     | 11.6     | 7.2  | 2.0  | 13.9     |      |             |      |      |
| Green Ext Time (p_c), s      | 0.2  | 0.6      | 0.0  | 0.0      | 1.2      | 0.3  | 0.0  | 2.1      |      |             |      |      |
| Intersection Summary         |      |          |      |          |          |      |      |          |      |             |      |      |
| HCM 2010 Ctrl Delay          |      |          | 30.8 |          |          |      |      |          |      |             |      |      |
| HCM 2010 LOS                 |      |          | С    |          |          |      |      |          |      |             |      |      |
| 110111 2010 200              |      |          | U    |          |          |      |      |          |      |             |      |      |

| Lane Configurations         To the properties of the | 4            |
|--|--------------|
| Traffic Volume (veh/h)         196         400         208         167         303         332         491         1061         255         217         652         7           Future Volume (veh/h)         196         400         208         167         303         332         491         1061         255         217         652         7           Number         7         4         14         3         8         18         5         2         12         1         6           Initial Q (Qb), veh         0   | SBR          |
| Traffic Volume (veh/h)         196         400         208         167         303         332         491         1061         255         217         652         7           Future Volume (veh/h)         196         400         208         167         303         332         491         1061         255         217         652         7           Number         7         4         14         3         8         18         5         2         12         1         6           Initial Q (Qb), veh         0   | 7            |
| Number         7         4         14         3         8         18         5         2         12         1         6           Initial Q (Qb), veh         0         1         0         1         0         1         0         1         0         1         0         1         0         1         0         1         0         1         0<   | 141          |
| Initial Q (Qb), veh         0         1         0         1         0         1         0         1         0         1         0         1         0         1         0         1         0         1         0         1         0         1  | 141          |
| Ped-Bike Adj(A_pbT)         1.00         0.98         1.00 </td <td>16</td>  | 16           |
| Parking Bus, Adj       1.00       1.0  | 0            |
| Adj Sat Flow, veh/h/ln       1863       1863       1863       1863       1863       1863       1863       1863       1900       1863       <  | 1.00         |
| Adj Flow Rate, veh/h       204       417       217       174       316       346       511       1105       266       226       679         Adj No. of Lanes       2       2       1       1       2       1       2       3       0       2       3   | 1.00         |
| Adj No. of Lanes 2 2 1 1 2 1 2 3 0 2 3   | 1863         |
|  | 147          |
|  | 1            |
|  | 0.96         |
| Percent Heavy Veh, % 2 2 2 2 2 2 2 2 2 2   | 2            |
|  | 534          |
|  | 0.25         |
| Sat Flow, veh/h 3442 3539 1559 1774 3539 1576 3442 4094 985 3442 5085 15   | <u> 1580</u> |
| Grp Volume(v), veh/h 204 417 217 174 316 346 511 915 456 226 679   | 147          |
| Grp Sat Flow(s), veh/h/ln 1721 1770 1559 1774 1770 1576 1721 1695 1689 1721 1695 15  | 1580         |
| Q Serve(g_s), s 4.4 8.0 7.5 7.3 5.6 16.1 11.0 18.6 18.6 4.9 8.8  | 5.2          |
| Cycle Q Clear(g_c), s 4.4 8.0 7.5 7.3 5.6 16.1 11.0 18.6 18.6 4.9 8.8  | 5.2          |
| Prop In Lane 1.00 1.00 1.00 1.00 0.58 1.00 1   | 1.00         |
| Lane Grp Cap(c), veh/h 288 761 612 212 888 396 601 1148 572 311 1293 5   | 534          |
| V/C Ratio(X) 0.71 0.55 0.35 0.82 0.36 0.87 0.85 0.80 0.80 0.73 0.53 0  | 0.28         |
| Avail Cap(c_a), veh/h 330 836 645 245 985 439 655 1148 572 348 1293 5  | 534          |
| HCM Platoon Ratio 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.0   | 1.00         |
| Upstream Filter(I) 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.0  | 1.00         |
| Uniform Delay (d), s/veh 34.0 26.6 16.5 32.7 23.5 27.4 30.5 22.8 22.8 33.7 24.4 1  | 18.4         |
| Incr Delay (d2), s/veh 5.8 0.6 0.3 17.4 0.2 16.5 9.7 5.8 11.0 6.6 1.5  | 1.3          |
| Initial Q Delay(d3),s/veh 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0  | 0.0          |
| %ile BackOfQ(50%),veh/ln 2.3 3.9 3.3 4.6 2.8 8.7 6.0 9.6 10.4 2.6 4.3  | 2.5          |
| LnGrp Delay(d),s/veh 39.8 27.2 16.8 50.1 23.7 43.8 40.1 28.6 33.8 40.3 26.0 1  | 19.7         |
| LnGrp LOS D C B D C D D C C D C  | В            |
| Approach Vol, veh/h 838 836 1882 1052  |              |
| Approach Delay, s/veh 27.6 37.5 33.0 28.2  |              |
| Approach LOS C D C   |              |
| Timer 1 2 3 4 5 6 7 8  |              |
| Assigned Phs 1 2 3 4 5 6 7 8   |              |
| Phs Duration (G+Y+Rc), s 11.4 30.3 13.6 20.9 17.8 23.9 10.9 23.6   |              |
| Change Period (Y+Rc), s 4.5 4.5 4.5 4.5 4.5 4.5  |              |
| Max Green Setting (Gmax), s 7.7 25.8 10.5 18.0 14.5 19.0 7.3 21.2  |              |
| Max Q Clear Time (g_c+l1), s 6.9 20.6 9.3 10.0 13.0 10.8 6.4 18.1  |              |
| Green Ext Time (p_c), s 0.1 3.6 0.1 2.2 0.4 3.2 0.1 1.1  |              |
| Intersection Summary   |              |
| HCM 2010 Ctrl Delay 31.7   |              |
| HCM 2010 LOS C   |              |

## Appendix G

Level of Service
Calculations

Cumulative Without Project
Conditions

## 1: Ridgemark Dr/Fairview Rd & Airline Highway (SR 25)

0.637

27

D

4.3

0.275

14.7

В

1.1

0.433

19.3

С

2.1

0.408

17.8

C

1.9

0.23

13.5

В

0.9

0.029

12.4

В

0.1

0.77

35.8

Ε

6.5

0.282

14.1

В

1.1

0.239

15.7

C

0.9

| 21.9 |  |   |   |   |  |   |   |   |   |   |  |
|------|--|---|---|---|--|---|---|---|---|---|--|
| С    |  |   |   |   |  |   |   |   |   |   |  |
|      |  |   |   |   |  |   |   |   |   |   |  |
| EBL  | EBT  | EBR   | WBL   | WBT   | WBR  | NBL   | NBT   | NBR   | SBL   | SBT   | SBR  |
| ř    | <u></u>  | 7   | *   | <u></u>   | 7  | ň   | ĵ.  |   | Ť   | <u></u>   | 7  |
| 151  | 151  | 92  | 10  | 289   | 115  | 229   | 95  | 10  | 80  | 42  | 151  |
| 151  | 151  | 92  | 10  | 289   | 115  | 229   | 95  | 10  | 80  | 42  | 151  |
| 0.92 | 0.92   | 0.92  | 0.92  | 0.92  | 0.92   | 0.92  | 0.92  | 0.92  | 0.92  | 0.92  | 0.92   |
| 7    | 7  | 7   | 5   | 5   | 5  | 2   | 2   | 2   | 6   | 6   | 6  |
| 164  | 164  | 100   | 11  | 314   | 125  | 249   | 103   | 11  | 87  | 46  | 164  |
| 1    | 1  | 1   | 1   | 1   | 1  | 1   | 1   | 0   | 1   | 1   | 1  |
| EB   |  |   | WB  |   |  | NB  |   |   | SB  |   |  |
| WB   |  |   | EB  |   |  | SB  |   |   | NB  |   |  |
| 3    |  |   | 3   |   |  | 3   |   |   | 2   |   |  |
| SB   |  |   | NB  |   |  | EB  |   |   | WB  |   |  |
| 3    |  |   | 2   |   |  | 3   |   |   | 3   |   |  |
| NB   |  |   | SB  |   |  | WB  |   |   | EB  |   |  |
| 2    |  |   | 3   |   |  | 3   |   |   | 3   |   |  |
| 17.4 |  |   | 29.2  |   |  | 23.1  |   |   | 16  |   |  |
|      |  |   |   |   |  |   |   |   |   |   |  |
| С    |  |   | D   |   |  | С   |   |   | С   |   |  |
| С    |  |   | D   |   |  | С   |   |   | С   |   |  |
| С    | NBLn1  | NBLn2   | D<br>EBLn1  | EBLn2   | EBLn3  | C<br>WBLn1  | WBLn2   | WBLn3   | C<br>SBLn1  | SBLn2   | SBLn3  |
| С    | NBLn1<br>100%  | NBLn2   |   | EBLn2<br>0%   | EBLn3  |   | WBLn2   | WBLn3   |   | SBLn2   | SBLn3  |
| С    |  |   | EBLn1   |   |  | WBLn1   |   |   | SBLn1   |   |  |
| С    | 100%   | 0%  | EBLn1<br>100%   | 0%  | 0%   | WBLn1<br>100%   | 0%  | 0%  | SBLn1<br>100%   | 0%  | 0%   |
| С    | 100%<br>0%<br>0%<br>Stop   | 0%<br>90%<br>10%<br>Stop  | EBLn1<br>100%<br>0%   | 0%<br>100%  | 0%<br>0%   | WBLn1<br>100%<br>0%   | 0%<br>100%<br>0%<br>Stop  | 0%<br>0%<br>100%<br>Stop  | SBLn1<br>100%<br>0%   | 0%<br>100%<br>0%<br>Stop  | 0%<br>0%   |
| С    | 100%<br>0%<br>0%<br>Stop<br>229  | 0%<br>90%<br>10%<br>Stop<br>105   | EBLn1 100% 0% 0% Stop 151   | 0%<br>100%<br>0%<br>Stop<br>151   | 0%<br>0%<br>100%<br>Stop<br>92   | WBLn1 100% 0% 0% Stop 10  | 0%<br>100%<br>0%  | 0%<br>0%<br>100%<br>Stop<br>115   | SBLn1<br>100%<br>0%<br>0%<br>Stop<br>80   | 0%<br>100%<br>0%<br>Stop<br>42  | 0%<br>0%<br>100%<br>Stop<br>151  |
| С    | 100%<br>0%<br>0%<br>Stop   | 0%<br>90%<br>10%<br>Stop<br>105   | EBLn1 100% 0% 0% Stop   | 0%<br>100%<br>0%<br>Stop<br>151   | 0%<br>0%<br>100%<br>Stop   | WBLn1 100% 0% 0% Stop   | 0%<br>100%<br>0%<br>Stop<br>289   | 0%<br>0%<br>100%<br>Stop  | SBLn1<br>100%<br>0%<br>0%<br>Stop   | 0%<br>100%<br>0%<br>Stop  | 0%<br>0%<br>100%<br>Stop   |
| С    | 100%<br>0%<br>0%<br>Stop<br>229  | 0%<br>90%<br>10%<br>Stop<br>105<br>0  | EBLn1 100% 0% 0% Stop 151   | 0%<br>100%<br>0%<br>Stop<br>151   | 0%<br>0%<br>100%<br>Stop<br>92<br>0  | WBLn1 100% 0% 0% Stop 10  | 0%<br>100%<br>0%<br>Stop<br>289   | 0%<br>0%<br>100%<br>Stop<br>115<br>0  | SBLn1<br>100%<br>0%<br>0%<br>Stop<br>80   | 0%<br>100%<br>0%<br>Stop<br>42  | 0%<br>0%<br>100%<br>Stop<br>151<br>0   |
| С    | 100%<br>0%<br>0%<br>Stop<br>229<br>229<br>0                                    | 0%<br>90%<br>10%<br>Stop<br>105<br>0<br>95  | EBLn1 100% 0% 0% Stop 151 151 0   | 0%<br>100%<br>0%<br>Stop<br>151<br>0<br>151   | 0%<br>0%<br>100%<br>Stop<br>92<br>0<br>0   | WBLn1 100% 0% 0% Stop 10 10 0   | 0%<br>100%<br>0%<br>Stop<br>289<br>0<br>289   | 0%<br>0%<br>100%<br>Stop<br>115<br>0  | SBLn1 100% 0% 0% Stop 80 80 0   | 0%<br>100%<br>0%<br>Stop<br>42<br>0<br>42   | 0%<br>0%<br>100%<br>Stop<br>151<br>0<br>0  |
| С    | 100%<br>0%<br>0%<br>Stop<br>229<br>229<br>0<br>0                               | 0%<br>90%<br>10%<br>Stop<br>105<br>0<br>95<br>10                                      | EBLn1 100% 0% 0% Stop 151 151 0 0   | 0%<br>100%<br>0%<br>Stop<br>151<br>0<br>151<br>0  | 0%<br>0%<br>100%<br>Stop<br>92<br>0<br>0<br>92<br>100  | WBLn1 100% 0% 0% Stop 10 0 0 11   | 0%<br>100%<br>0%<br>Stop<br>289<br>0<br>289<br>0<br>314   | 0%<br>0%<br>100%<br>Stop<br>115<br>0<br>0<br>115  | SBLn1 100% 0% 0% Stop 80 80 0 0   | 0%<br>100%<br>0%<br>Stop<br>42<br>0<br>42<br>0<br>46  | 0%<br>0%<br>100%<br>Stop<br>151<br>0<br>0<br>151<br>164  |
| C    | 100%<br>0%<br>0%<br>Stop<br>229<br>229<br>0<br>0<br>249                        | 0%<br>90%<br>10%<br>Stop<br>105<br>0<br>95<br>10                                      | EBLn1 100% 0% 0% Stop 151 151 0 0 164   | 0%<br>100%<br>0%<br>Stop<br>151<br>0<br>151<br>0<br>164   | 0%<br>0%<br>100%<br>Stop<br>92<br>0<br>0<br>92<br>100  | WBLn1 100% 0% 0% Stop 10 0 01 11  | 0%<br>100%<br>0%<br>Stop<br>289<br>0<br>289<br>0<br>314   | 0%<br>0%<br>100%<br>Stop<br>115<br>0<br>0<br>115<br>125   | SBLn1 100% 0% 0% Stop 80 0 0 87   | 0%<br>100%<br>0%<br>Stop<br>42<br>0<br>42<br>0<br>46  | 0%<br>0%<br>100%<br>Stop<br>151<br>0<br>0<br>151<br>164  |
| C    | 100%<br>0%<br>0%<br>Stop<br>229<br>229<br>0<br>0<br>249<br>8                   | 0%<br>90%<br>10%<br>Stop<br>105<br>0<br>95<br>10<br>114<br>8                          | EBLn1 100% 0% 0% Stop 151 151 0 0 164 8 0.432   | 0%<br>100%<br>0%<br>Stop<br>151<br>0<br>151<br>0<br>164<br>8<br>0.409   | 0%<br>0%<br>100%<br>Stop<br>92<br>0<br>0<br>92<br>100<br>8   | WBLn1 100% 0% 0% Stop 10 0 11 8 0.028   | 0%<br>100%<br>0%<br>Stop<br>289<br>0<br>289<br>0<br>314<br>8  | 0%<br>0%<br>100%<br>Stop<br>115<br>0<br>0<br>115<br>125<br>8<br>0.282   | SBLn1 100% 0% 0% Stop 80 80 0 87 8  | 0%<br>100%<br>0%<br>Stop<br>42<br>0<br>42<br>0<br>46<br>8   | 0%<br>0%<br>100%<br>Stop<br>151<br>0<br>0<br>151<br>164<br>8<br>0.393  |
| C    | 100%<br>0%<br>0%<br>Stop<br>229<br>229<br>0<br>0<br>249<br>8<br>0.638<br>9.233 | 0%<br>90%<br>10%<br>Stop<br>105<br>0<br>95<br>10<br>114<br>8<br>0.275<br>8.666        | EBLn1 100% 0% 0% Stop 151 151 0 0 164 8 0.432 9.481   | 0% 100% 0% Stop 151 0 151 0 164 8 0.409 8.968   | 0%<br>0%<br>100%<br>Stop<br>92<br>0<br>0<br>92<br>100<br>8<br>0.229<br>8.249   | WBLn1 100% 0% 0% Stop 10 00 11 8 0.028 9.352  | 0%<br>100%<br>0%<br>Stop<br>289<br>0<br>289<br>0<br>314<br>8<br>0.771<br>8.839  | 0%<br>0%<br>100%<br>Stop<br>115<br>0<br>0<br>115<br>125<br>8<br>0.282<br>8.122  | SBLn1 100% 0% 0% Stop 80 0 0 87   | 0%<br>100%<br>0%<br>Stop<br>42<br>0<br>42<br>0<br>46<br>8<br>0.118<br>9.342   | 0%<br>0%<br>100%<br>Stop<br>151<br>0<br>0<br>151<br>164<br>8<br>0.393<br>8.628   |
| C    | 100%<br>0%<br>0%<br>Stop<br>229<br>0<br>0<br>249<br>8<br>0.638<br>9.233<br>Yes | 0%<br>90%<br>10%<br>Stop<br>105<br>0<br>95<br>10<br>114<br>8<br>0.275<br>8.666<br>Yes | EBLn1 100% 0% 0% Stop 151 151 0 0164 8 0.432 9.481 Yes  | 0% 100% 0% Stop 151 0 151 0 164 8 0.409 8.968 Yes   | 0%<br>0%<br>100%<br>Stop<br>92<br>0<br>0<br>92<br>100<br>8<br>0.229<br>8.249<br>Yes  | WBLn1 100% 0% 0% Stop 10 0 11 8 0.028 9.352 Yes   | 0%<br>100%<br>0%<br>Stop<br>289<br>0<br>289<br>0<br>314<br>8<br>0.771<br>8.839<br>Yes   | 0%<br>0%<br>100%<br>Stop<br>115<br>0<br>0<br>115<br>125<br>8<br>0.282<br>8.122<br>Yes   | SBLn1 100% 0% 0% Stop 80 0 0 87 8 0.238 9.852 Yes   | 0%<br>100%<br>0%<br>Stop<br>42<br>0<br>42<br>0<br>46<br>8<br>0.118<br>9.342<br>Yes  | 0%<br>0%<br>100%<br>Stop<br>151<br>0<br>0<br>151<br>164<br>8<br>0.393<br>8.628<br>Yes  |
| C    | 100%<br>0%<br>0%<br>Stop<br>229<br>229<br>0<br>0<br>249<br>8<br>0.638<br>9.233 | 0%<br>90%<br>10%<br>Stop<br>105<br>0<br>95<br>10<br>114<br>8<br>0.275<br>8.666        | EBLn1 100% 0% 0% Stop 151 151 0 0 164 8 0.432 9.481   | 0% 100% 0% Stop 151 0 151 0 164 8 0.409 8.968   | 0%<br>0%<br>100%<br>Stop<br>92<br>0<br>0<br>92<br>100<br>8<br>0.229<br>8.249   | WBLn1 100% 0% 0% Stop 10 00 11 8 0.028 9.352  | 0%<br>100%<br>0%<br>Stop<br>289<br>0<br>289<br>0<br>314<br>8<br>0.771<br>8.839  | 0%<br>0%<br>100%<br>Stop<br>115<br>0<br>0<br>115<br>125<br>8<br>0.282<br>8.122  | SBLn1 100% 0% 0% Stop 80 0 0 87 8 0.238 9.852   | 0%<br>100%<br>0%<br>Stop<br>42<br>0<br>42<br>0<br>46<br>8<br>0.118<br>9.342   | 0%<br>0%<br>100%<br>Stop<br>151<br>0<br>0<br>151<br>164<br>8<br>0.393<br>8.628   |
|      | C EBL 151 151 0.92 7 164 1 EB WB 3 SB 3 NB 2 17.4                              | C  EBL EBT  151 151 151 151 0.92 0.92 7 7 164 164 1 1  EB  WB 3 SB 3 NB 2             | C  EBL EBT EBR  151 151 92 151 151 92 0.92 0.92 0.92 7 7 7 164 164 100 1 1 1  EB  WB 3 SB 3 NB 2 17.4 | EBL EBT EBR WBL  151 151 92 10 151 151 92 10 0.92 0.92 0.92 0.92 7 7 7 7 5 164 164 100 11 1 1 1 1  EB WB  WB EB 3 3 3 SB NB 3 3 SB NB 3 2 NB SB 2 3 17.4 29.2 | EBL EBT EBR WBL WBT  151 151 92 10 289 151 151 92 10 289 0.92 0.92 0.92 0.92 7 7 7 7 5 5 164 164 100 11 314 1 1 1 1 1  EB WB  WB  WB  WB  SB  NB  3  2  NB  SB  SB  SB  SB  SB  SB  SB  SB  SB | C         EBL         EBT         EBR         WBL         WBT         WBR           151         151         92         10         289         115           151         151         92         10         289         115           0.92         0.92         0.92         0.92         0.92         0.92           7         7         7         5         5         5           164         164         100         11         314         125           1         1         1         1         1         1           EB         WB           WB         EB         3         3         3           SB         NB         3         2         NB           NB         SB         3         3         3         3           17.4         29.2         2         2         3 | EBL         EBT         EBR         WBL         WBT         WBR         NBL           151         151         92         10         289         115         229           151         151         92         10         289         115         229           0.92 | C         EBL         EBT         EBR         WBL         WBT         WBR         NBL         NBT           151         151         92         10         289         115         229         95           151         151         92         10         289         115         229         95           0.92         < | C         EBL         EBT         EBR         WBL         WBT         WBR         NBL         NBT         NBR           151         151         92         10         289         115         229         95         10           151         151         92         10         289         115         229         95         10           0.92         0. | EBL         EBT         EBR         WBL         WBT         WBR         NBL         NBT         NBR         SBL           151         151         92         10         289         115         229         95         10         80           151         151         92         10         289         115         229         95         10         80           0.92 | EBL         EBT         EBR         WBL         WBT         WBR         NBL         NBT         NBR         SBL         SBT           151         151         92         10         289         115         229         95         10         80         42           151         151         92         10         289         115         229         95         10         80         42           0.92 |

HCM Lane V/C Ratio

**HCM Control Delay** 

HCM Lane LOS

HCM 95th-tile Q

0.12

13.4

В

0.4

0.393

16.9

C

1.8

| Intersection           |          |          |        |        |         |      |            |            |        |            |            |       |       |
|------------------------|----------|----------|--------|--------|---------|------|------------|------------|--------|------------|------------|-------|-------|
| Int Delay, s/veh       | 7.4      |          |        |        |         |      |            |            |        |            |            |       |       |
| Movement               | EBL      | EBT      | EBR    | WBL    | WBT     | WBR  | NBL        | NBT        | NBR    | SBL        | SBT        | SBR   |       |
| Lane Configurations    | <u> </u> | <u> </u> | 7      | ነ ነ    | <u></u> | 7    | ሻ          | <u> </u>   | 7      | <u> </u>   | <u> </u>   | 7     |       |
| Traffic Vol. veh/h     | 50       | 289      | 20     | 45     | 594     | 30   | 50         | 5          | 60     | 45         | 5          | 145   |       |
| Future Vol, veh/h      | 50       | 289      | 20     | 45     | 594     | 30   | 50         | 5          | 60     | 45         | 5          | 145   |       |
| Conflicting Peds, #/hr | 0        | 0        | 1      | 0      | 0       | 0    | 0          | 0          | 0      | 0          | 0          | 0     |       |
| Sign Control           | Free     | Free     | Free   | Free   | Free    | Free | Stop       | Stop       | Stop   | Stop       | Stop       | Stop  |       |
| RT Channelized         | -        | -        | None   | -      | -       | None | -          | -          | None   | -          | -          | None  |       |
| Storage Length         | 320      | -        | 505    | 360    | -       | 195  | 60         | -          | 0      | 100        | -          | 100   |       |
| Veh in Median Storage  | , # -    | 0        | -      | -      | 0       | -    | -          | 0          | -      | -          | 0          | -     |       |
| Grade, %               | -        | 0        | -      | -      | 0       | -    | -          | 0          | -      | -          | 0          | -     |       |
| Peak Hour Factor       | 95       | 95       | 95     | 95     | 95      | 95   | 95         | 95         | 95     | 95         | 95         | 95    |       |
| Heavy Vehicles, %      | 8        | 8        | 8      | 4      | 4       | 4    | 2          | 2          | 2      | 3          | 3          | 3     |       |
| Mvmt Flow              | 53       | 304      | 21     | 47     | 625     | 32   | 53         | 5          | 63     | 47         | 5          | 153   |       |
|                        |          |          |        |        |         |      |            |            |        |            |            |       |       |
| Major/Minor N          | Major1   |          |        | Major2 |         | 1    | Minor1     |            |        | Minor2     |            |       |       |
| Conflicting Flow All   | 657      | 0        | 0      | 326    | 0       | 0    | 1225       | 1162       | 305    | 1174       | 1151       | 625   |       |
| Stage 1                | -        | -        | -      | -      | -       | -    | 411        | 411        | -      | 719        | 719        | -     |       |
| Stage 2                | -        | -        | -      | -      | -       | -    | 814        | 751        | -      | 455        | 432        | -     |       |
| Critical Hdwy          | 4.18     | -        | -      | 4.14   | -       | -    | 7.12       | 6.52       | 6.22   | 7.13       | 6.53       | 6.23  |       |
| Critical Hdwy Stg 1    | -        | -        | -      | -      | -       | -    | 6.12       | 5.52       | -      | 6.13       | 5.53       | -     |       |
| Critical Hdwy Stg 2    | -        | -        | -      | -      | -       | -    | 6.12       | 5.52       | -      | 6.13       | 5.53       | -     |       |
| Follow-up Hdwy         | 2.272    | -        | -      | 2.236  | -       | -    | 3.518      | 4.018      | 3.318  | 3.527      | 4.027      | 3.327 |       |
| Pot Cap-1 Maneuver     | 903      | -        | -      | 1222   | -       | -    | 156        | 195        | 735    | 168        | 197        | 483   |       |
| Stage 1                | -        | -        | -      | -      | -       | -    | 618        | 595        | -      | 418        | 431        | -     |       |
| Stage 2                | -        | -        | -      | -      | -       | -    | 372        | 418        | -      | 583        | 581        | -     |       |
| Platoon blocked, %     | 000      | -        | -      | 4004   | -       | -    | 07         | 470        | 704    | 400        | 470        | 400   |       |
| Mov Cap-1 Maneuver     | 903      | -        | _      | 1221   | -       | -    | 97         | 176        | 734    | 139        | 178        | 483   |       |
| Mov Cap-2 Maneuver     | -        | -        | -      | -      | -       | -    | 97         | 176        | -      | 139        | 178        | -     |       |
| Stage 1                | -        | -        |        | -      | -       | -    | 581<br>242 | 559<br>402 | -<br>- | 393<br>497 | 415<br>546 | -     |       |
| Stage 2                | _        | _        | _      | _      | _       | _    | 242        | 402        | _      | 497        | 540        | -     |       |
|                        |          |          |        |        |         |      |            |            |        |            |            |       |       |
| Approach               | EB       |          |        | WB     |         |      | NB         |            |        | SB         |            |       |       |
| HCM Control Delay, s   | 1.3      |          |        | 0.5    |         |      | 41.1       |            |        | 22.6       |            |       |       |
| HCM LOS                |          |          |        |        |         |      | Е          |            |        | С          |            |       |       |
|                        |          |          |        |        |         |      |            |            |        |            |            |       |       |
| Minor Lane/Major Mvm   | nt       | NBLn11   | NBLn21 | VBLn3  | EBL     | EBT  | EBR        | WBL        | WBT    | WBR        | SBLn1      | SBLn2 | SBLn3 |
| Capacity (veh/h)       |          | 97       | 176    | 734    | 903     | -    | -          | 1221       | -      | -          | 139        | 178   | 483   |
| HCM Lane V/C Ratio     |          | 0.543    |        | 0.086  |         | -    |            | 0.039      | -      | -          | 0.341      |       | 0.316 |
| HCM Control Delay (s)  |          | 79.4     | 26.1   | 10.4   | 9.2     | -    | -          | 8.1        | -      | -          | 43.7       | 25.8  | 15.9  |
| HCM Lane LOS           |          | F        | D      | В      | Α       | -    | -          | Α          | -      | -          | Е          | D     | С     |
| HCM 95th %tile Q(veh)  | )        | 2.5      | 0.1    | 0.3    | 0.2     | -    | -          | 0.1        | -      | -          | 1.4        | 0.1   | 1.3   |
|                        |          |          |        |        |         |      |            |            |        |            |            |       |       |

| Intersection           |             |       |                 |       |        |                   |
|------------------------|-------------|-------|-----------------|-------|--------|-------------------|
| Int Delay, s/veh       | 2.2         |       |                 |       |        |                   |
| Movement               | WBL         | WBR   | NBT             | NBR   | SBL    | SBT               |
| Lane Configurations    | WBL         | אטוע  |                 | NDI   | ODL    |                   |
|                        | <b>T</b> 35 | 72    | <b>♣</b><br>315 | 35    | 15     | <b>र्ध</b><br>195 |
| Traffic Vol, veh/h     |             |       |                 |       |        |                   |
| Future Vol, veh/h      | 35          | 72    | 315             | 35    | 15     | 195               |
| Conflicting Peds, #/hr |             | 0     | 0               | _ 1   | _ 1    | _ 0               |
| Sign Control           | Stop        | Stop  | Free            | Free  | Free   | Free              |
| RT Channelized         | -           | None  | -               | None  | -      | None              |
| Storage Length         | 0           | -     | -               | -     | -      | -                 |
| Veh in Median Storag   | e, # 0      | -     | 0               | -     | -      | 0                 |
| Grade, %               | 0           | -     | 0               | -     | -      | 0                 |
| Peak Hour Factor       | 86          | 86    | 86              | 25    | 86     | 86                |
| Heavy Vehicles, %      | 2           | 2     | 7               | 7     | 7      | 7                 |
| Mvmt Flow              | 41          | 84    | 366             | 140   | 17     | 227               |
|                        |             |       |                 |       |        |                   |
| N.A. ' (N.A.           | N 4: 4      |       |                 |       |        |                   |
| Major/Minor            | Minor1      |       | //ajor1         |       | Major2 |                   |
| Conflicting Flow All   | 698         | 437   | 0               | 0     | 507    | 0                 |
| Stage 1                | 437         | -     | -               | -     | -      | -                 |
| Stage 2                | 261         | -     | -               | -     | -      | -                 |
| Critical Hdwy          | 6.42        | 6.22  | -               | -     | 4.17   | -                 |
| Critical Hdwy Stg 1    | 5.42        | -     | -               | -     | -      | -                 |
| Critical Hdwy Stg 2    | 5.42        | -     | -               | -     | -      | -                 |
| Follow-up Hdwy         | 3.518       | 3.318 | -               | -     | 2.263  | -                 |
| Pot Cap-1 Maneuver     | 407         | 620   | -               | -     | 1033   | -                 |
| Stage 1                | 651         | -     | -               | _     | -      | _                 |
| Stage 2                | 783         | _     | _               | _     | -      | _                 |
| Platoon blocked, %     | , 00        |       | _               |       |        | _                 |
| Mov Cap-1 Maneuver     | 399         | 619   |                 | _     | 1032   |                   |
| Mov Cap-1 Maneuver     |             | 019   | _               | -     | 1032   |                   |
|                        | 638         |       | -               | -     |        | -                 |
| Stage 1                |             | -     | -               | -     | -      | -                 |
| Stage 2                | 783         | -     | -               | -     | -      | -                 |
|                        |             |       |                 |       |        |                   |
| Approach               | WB          |       | NB              |       | SB     |                   |
| HCM Control Delay, s   |             |       | 0               |       | 0.6    |                   |
| HCM LOS                | В           |       | · ·             |       | 0.0    |                   |
| HOW LOO                | <u> </u>    |       |                 |       |        |                   |
|                        |             |       |                 |       |        |                   |
| Minor Lane/Major Mvr   | nt          | NBT   | NBRV            | VBLn1 | SBL    | SBT               |
| Capacity (veh/h)       |             | -     | _               | 524   | 1032   | -                 |
| HCM Lane V/C Ratio     |             | -     | _               | 0.237 |        | -                 |
| HCM Control Delay (s   | (           | _     | _               | 14    | 8.5    | 0                 |
| HCM Lane LOS           | 1           | _     | _               | В     | A      | A                 |
| HCM 95th %tile Q(vel   | 1)          | _     | _               | 0.9   | 0.1    | -                 |
| HOW SOUT WITH Q(VEI    | IJ          | _     |                 | 0.9   | 0.1    | _                 |

|                              |      | <b>→</b> | •     | •    | <b>—</b> | •     | •     | †        | ~    | <b>/</b> | ţ        | ✓    |
|------------------------------|------|----------|-------|------|----------|-------|-------|----------|------|----------|----------|------|
| Movement                     | EBL  | EBT      | EBR   | WBL  | WBT      | WBR   | NBL   | NBT      | NBR  | SBL      | SBT      | SBR  |
| Lane Configurations          | ň    | ĵ.       |       | ħ    | f)       |       | 7     | <b>^</b> | 7    | 7        | <b>^</b> | 7    |
| Traffic Volume (veh/h)       | 233  | 209      | 142   | 32   | 453      | 315   | 314   | 433      | 42   | 130      | 185      | 210  |
| Future Volume (veh/h)        | 233  | 209      | 142   | 32   | 453      | 315   | 314   | 433      | 42   | 130      | 185      | 210  |
| Number                       | 7    | 4        | 14    | 3    | 8        | 18    | 5     | 2        | 12   | 1        | 6        | 16   |
| Initial Q (Qb), veh          | 0    | 0        | 0     | 0    | 0        | 0     | 0     | 0        | 0    | 0        | 0        | 0    |
| Ped-Bike Adj(A_pbT)          | 1.00 |          | 1.00  | 1.00 |          | 1.00  | 1.00  |          | 1.00 | 1.00     |          | 1.00 |
| Parking Bus, Adj             | 1.00 | 1.00     | 1.00  | 1.00 | 1.00     | 1.00  | 1.00  | 1.00     | 1.00 | 1.00     | 1.00     | 1.00 |
| Adj Sat Flow, veh/h/ln       | 1776 | 1776     | 1900  | 1863 | 1863     | 1900  | 1863  | 1863     | 1863 | 1827     | 1827     | 1827 |
| Adj Flow Rate, veh/h         | 248  | 222      | 151   | 34   | 482      | 335   | 334   | 461      | 45   | 138      | 197      | 223  |
| Adj No. of Lanes             | 1    | 1        | 0     | 1    | 1        | 0     | 1     | 1        | 1    | 1        | 1        | 1    |
| Peak Hour Factor             | 0.94 | 0.94     | 0.94  | 0.94 | 0.94     | 0.94  | 0.94  | 0.94     | 0.94 | 0.94     | 0.94     | 0.94 |
| Percent Heavy Veh, %         | 7    | 7        | 7     | 2    | 2        | 2     | 2     | 2        | 2    | 4        | 4        | 4    |
| Cap, veh/h                   | 338  | 197      | 134   | 432  | 249      | 173   | 254   | 513      | 436  | 141      | 390      | 331  |
| Arrive On Green              | 0.20 | 0.20     | 0.20  | 0.24 | 0.24     | 0.24  | 0.14  | 0.28     | 0.28 | 0.08     | 0.21     | 0.21 |
| Sat Flow, veh/h              | 1691 | 985      | 670   | 1774 | 1025     | 712   | 1774  | 1863     | 1583 | 1740     | 1827     | 1553 |
| Grp Volume(v), veh/h         | 248  | 0        | 373   | 34   | 0        | 817   | 334   | 461      | 45   | 138      | 197      | 223  |
| Grp Sat Flow(s),veh/h/ln     | 1691 | 0        | 1655  | 1774 | 0        | 1737  | 1774  | 1863     | 1583 | 1740     | 1827     | 1553 |
| Q Serve(g_s), s              | 12.4 | 0.0      | 18.0  | 1.3  | 0.0      | 21.9  | 12.9  | 21.4     | 1.9  | 7.1      | 8.6      | 11.9 |
| Cycle Q Clear(g_c), s        | 12.4 | 0.0      | 18.0  | 1.3  | 0.0      | 21.9  | 12.9  | 21.4     | 1.9  | 7.1      | 8.6      | 11.9 |
| Prop In Lane                 | 1.00 |          | 0.40  | 1.00 |          | 0.41  | 1.00  |          | 1.00 | 1.00     |          | 1.00 |
| Lane Grp Cap(c), veh/h       | 338  | 0        | 331   | 432  | 0        | 423   | 254   | 513      | 436  | 141      | 390      | 331  |
| V/C Ratio(X)                 | 0.73 | 0.00     | 1.13  | 0.08 | 0.00     | 1.93  | 1.31  | 0.90     | 0.10 | 0.98     | 0.51     | 0.67 |
| Avail Cap(c_a), veh/h        | 338  | 0        | 331   | 432  | 0        | 423   | 254   | 513      | 436  | 141      | 390      | 331  |
| HCM Platoon Ratio            | 1.00 | 1.00     | 1.00  | 1.00 | 1.00     | 1.00  | 1.00  | 1.00     | 1.00 | 1.00     | 1.00     | 1.00 |
| Upstream Filter(I)           | 1.00 | 0.00     | 1.00  | 1.00 | 0.00     | 1.00  | 1.00  | 1.00     | 1.00 | 1.00     | 1.00     | 1.00 |
| Uniform Delay (d), s/veh     | 33.7 | 0.0      | 36.0  | 26.3 | 0.0      | 34.1  | 38.5  | 31.4     | 24.3 | 41.3     | 31.2     | 32.5 |
| Incr Delay (d2), s/veh       | 8.0  | 0.0      | 88.2  | 0.1  | 0.0      | 428.4 | 166.2 | 21.2     | 0.5  | 68.8     | 4.6      | 10.4 |
| Initial Q Delay(d3),s/veh    | 0.0  | 0.0      | 0.0   | 0.0  | 0.0      | 0.0   | 0.0   | 0.0      | 0.0  | 0.0      | 0.0      | 0.0  |
| %ile BackOfQ(50%),veh/ln     | 6.5  | 0.0      | 16.3  | 0.7  | 0.0      | 60.8  | 18.0  | 14.0     | 0.9  | 6.1      | 4.8      | 6.0  |
| LnGrp Delay(d),s/veh         | 41.7 | 0.0      | 124.2 | 26.3 | 0.0      | 462.5 | 204.8 | 52.5     | 24.8 | 110.1    | 35.8     | 43.0 |
| LnGrp LOS                    | D    |          | F     | С    |          | F     | F     | D        | С    | F        | D        | D    |
| Approach Vol, veh/h          |      | 621      |       |      | 851      |       |       | 840      |      |          | 558      |      |
| Approach Delay, s/veh        |      | 91.3     |       |      | 445.1    |       |       | 111.6    |      |          | 57.0     |      |
| Approach LOS                 |      | F        |       |      | F        |       |       | F        |      |          | Е        |      |
| Timer                        | 1    | 2        | 3     | 4    | 5        | 6     | 7     | 8        |      |          |          |      |
| Assigned Phs                 | 1    | 2        |       | 4    | 5        | 6     |       | 8        |      |          |          |      |
| Phs Duration (G+Y+Rc), s     | 11.8 | 29.3     |       | 22.5 | 17.4     | 23.7  |       | 26.4     |      |          |          |      |
| Change Period (Y+Rc), s      | 4.5  | 4.5      |       | 4.5  | 4.5      | 4.5   |       | 4.5      |      |          |          |      |
| Max Green Setting (Gmax), s  | 7.3  | 24.8     |       | 18.0 | 12.9     | 19.2  |       | 21.9     |      |          |          |      |
| Max Q Clear Time (g_c+l1), s | 9.1  | 23.4     |       | 20.0 | 14.9     | 13.9  |       | 23.9     |      |          |          |      |
| Green Ext Time (p_c), s      | 0.0  | 0.4      |       | 0.0  | 0.0      | 0.9   |       | 0.0      |      |          |          |      |
| Intersection Summary         |      |          |       |      |          |       |       |          |      |          |          |      |
| HCM 2010 Ctrl Delay          |      |          | 195.5 |      |          |       |       |          |      |          |          |      |
| HCM 2010 LOS                 |      |          | F     |      |          |       |       |          |      |          |          |      |
| HOW ZOTO LOO                 |      |          |       |      |          |       |       |          |      |          |          |      |

|                              | •    |          |      |      | <b>←</b> | •     | •    | •    |      |      | 1    |      |
|------------------------------|------|----------|------|------|----------|-------|------|------|------|------|------|------|
|                              |      | <b>→</b> | *    | ₩    |          |       | -7   | ı    |      | _    | *    | _    |
| Movement                     | EBL  | EBT      | EBR  | WBL  | WBT      | WBR   | NBL  | NBT  | NBR  | SBL  | SBT  | SBR  |
| Lane Configurations          |      | ĵ∍       |      | ሻ    | f)       |       |      | ↔    |      |      | 4    |      |
| Traffic Volume (veh/h)       | 35   | 406      | 120  | 95   | 857      | 25    | 185  | 65   | 140  | 38   | 25   | 52   |
| Future Volume (veh/h)        | 35   | 406      | 120  | 95   | 857      | 25    | 185  | 65   | 140  | 38   | 25   | 52   |
| Number                       | 7    | 4        | 14   | 3    | 8        | 18    | 5    | 2    | 12   | 1    | 6    | 16   |
| Initial Q (Qb), veh          | 0    | 0        | 0    | 0    | 0        | 0     | 0    | 0    | 0    | 0    | 0    | 0    |
| Ped-Bike Adj(A_pbT)          | 1.00 |          | 1.00 | 1.00 |          | 1.00  | 1.00 |      | 1.00 | 1.00 |      | 1.00 |
| Parking Bus, Adj             | 1.00 | 1.00     | 1.00 | 1.00 | 1.00     | 1.00  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln       | 1827 | 1827     | 1900 | 1845 | 1845     | 1900  | 1900 | 1810 | 1900 | 1900 | 1776 | 1900 |
| Adj Flow Rate, veh/h         | 39   | 451      | 133  | 106  | 952      | 28    | 206  | 72   | 156  | 42   | 28   | 58   |
| Adj No. of Lanes             | 1    | 1        | 0    | 1    | 1        | 0     | 0    | 1    | 0    | 0    | 1    | 0    |
| Peak Hour Factor             | 0.90 | 0.90     | 0.90 | 0.90 | 0.90     | 0.90  | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Percent Heavy Veh, %         | 4    | 4        | 4    | 3    | 3        | 3     | 5    | 5    | 5    | 7    | 7    | 7    |
| Cap, veh/h                   | 69   | 547      | 161  | 135  | 786      | 23    | 290  | 85   | 163  | 184  | 129  | 195  |
| Arrive On Green              | 0.04 | 0.40     | 0.40 | 0.08 | 0.44     | 0.44  | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 |
| Sat Flow, veh/h              | 1740 | 1356     | 400  | 1757 | 1783     | 52    | 675  | 281  | 536  | 353  | 425  | 645  |
| Grp Volume(v), veh/h         | 39   | 0        | 584  | 106  | 0        | 980   | 434  | 0    | 0    | 128  | 0    | 0    |
| Grp Sat Flow(s),veh/h/ln     | 1740 | 0        | 1756 | 1757 | 0        | 1835  | 1492 | 0    | 0    | 1423 | 0    | 0    |
| Q Serve(g_s), s              | 1.4  | 0.0      | 18.5 | 3.7  | 0.0      | 27.5  | 14.1 | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  |
| Cycle Q Clear(g_c), s        | 1.4  | 0.0      | 18.5 | 3.7  | 0.0      | 27.5  | 17.7 | 0.0  | 0.0  | 3.7  | 0.0  | 0.0  |
| Prop In Lane                 | 1.00 |          | 0.23 | 1.00 |          | 0.03  | 0.47 |      | 0.36 | 0.33 |      | 0.45 |
| Lane Grp Cap(c), veh/h       | 69   | 0        | 708  | 135  | 0        | 809   | 538  | 0    | 0    | 508  | 0    | 0    |
| V/C Ratio(X)                 | 0.57 | 0.00     | 0.82 | 0.78 | 0.00     | 1.21  | 0.81 | 0.00 | 0.00 | 0.25 | 0.00 | 0.00 |
| Avail Cap(c_a), veh/h        | 142  | 0        | 724  | 194  | 0        | 809   | 538  | 0    | 0    | 508  | 0    | 0    |
| HCM Platoon Ratio            | 1.00 | 1.00     | 1.00 | 1.00 | 1.00     | 1.00  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I)           | 1.00 | 0.00     | 1.00 | 1.00 | 0.00     | 1.00  | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| Uniform Delay (d), s/veh     | 29.4 | 0.0      | 16.6 | 28.3 | 0.0      | 17.4  | 21.0 | 0.0  | 0.0  | 16.4 | 0.0  | 0.0  |
| Incr Delay (d2), s/veh       | 7.2  | 0.0      | 7.6  | 12.2 | 0.0      | 106.2 | 12.3 | 0.0  | 0.0  | 1.2  | 0.0  | 0.0  |
| Initial Q Delay(d3),s/veh    | 0.0  | 0.0      | 0.0  | 0.0  | 0.0      | 0.0   | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  |
| %ile BackOfQ(50%),veh/ln     | 8.0  | 0.0      | 10.4 | 2.3  | 0.0      | 37.6  | 9.1  | 0.0  | 0.0  | 1.8  | 0.0  | 0.0  |
| LnGrp Delay(d),s/veh         | 36.7 | 0.0      | 24.2 | 40.5 | 0.0      | 123.6 | 33.3 | 0.0  | 0.0  | 17.6 | 0.0  | 0.0  |
| LnGrp LOS                    | D    |          | С    | D    |          | F     | С    |      |      | В    |      |      |
| Approach Vol, veh/h          |      | 623      |      |      | 1086     |       |      | 434  |      |      | 128  |      |
| Approach Delay, s/veh        |      | 25.0     |      |      | 115.5    |       |      | 33.3 |      |      | 17.6 |      |
| Approach LOS                 |      | С        |      |      | F        |       |      | С    |      |      | В    |      |
| Timer                        | 1    | 2        | 3    | 4    | 5        | 6     | 7    | 8    |      |      |      |      |
| Assigned Phs                 |      | 2        | 3    | 4    |          | 6     | 7    | 8    |      |      |      |      |
| Phs Duration (G+Y+Rc), s     |      | 23.4     | 9.3  | 29.6 |          | 23.4  | 7.0  | 32.0 |      |      |      |      |
| Change Period (Y+Rc), s      |      | 4.5      | 4.5  | 4.5  |          | 4.5   | 4.5  | 4.5  |      |      |      |      |
| Max Green Setting (Gmax), s  |      | 18.9     | 6.9  | 25.7 |          | 18.9  | 5.1  | 27.5 |      |      |      |      |
| Max Q Clear Time (g_c+l1), s |      | 19.7     | 5.7  | 20.5 |          | 5.7   | 3.4  | 29.5 |      |      |      |      |
| Green Ext Time (p_c), s      |      | 0.0      | 0.0  | 1.8  |          | 0.5   | 0.0  | 0.0  |      |      |      |      |
| Intersection Summary         |      |          |      |      |          |       |      |      |      |      |      |      |
| HCM 2010 Ctrl Delay          |      |          | 69.5 |      |          |       |      |      |      |      |      |      |
| HCM 2010 LOS                 |      |          | Е    |      |          |       |      |      |      |      |      |      |
|                              |      |          |      |      |          |       |      |      |      |      |      |      |

|                              |             | <b>→</b>   | <b>←</b> | •    | <b>\</b>    | 4    |      |      |  |  |
|------------------------------|-------------|------------|----------|------|-------------|------|------|------|--|--|
| Movement                     | EBL         | EBT        | WBT      | WBR  | SBL         | SBR  |      |      |  |  |
| Lane Configurations          | *           | <b></b>    | <b></b>  | #    | ች           | #    |      |      |  |  |
| Traffic Volume (veh/h)       | 199         | 280        | 640      | 454  | 281         | 335  |      |      |  |  |
| Future Volume (veh/h)        | 199         | 280        | 640      | 454  | 281         | 335  |      |      |  |  |
| Number                       | 7           | 4          | 8        | 18   | 1           | 16   |      |      |  |  |
| Initial Q (Qb), veh          | 0           | 0          | 0        | 0    | 0           | 0    |      |      |  |  |
| Ped-Bike Adj(A_pbT)          | 1.00        |            |          | 1.00 | 1.00        | 1.00 |      |      |  |  |
| Parking Bus, Adj             | 1.00        | 1.00       | 1.00     | 1.00 | 1.00        | 1.00 |      |      |  |  |
| Adj Sat Flow, veh/h/ln       | 1810        | 1810       | 1863     | 1863 | 1863        | 1863 |      |      |  |  |
| Adj Flow Rate, veh/h         | 221         | 311        | 711      | 504  | 312         | 372  |      |      |  |  |
| Adj No. of Lanes             | 1           | 1          | 1        | 1    | 1           | 1    |      |      |  |  |
| Peak Hour Factor             | 0.90        | 0.90       | 0.90     | 0.90 | 0.90        | 0.90 |      |      |  |  |
| Percent Heavy Veh, %         | 5           | 5          | 2        | 2    | 2           | 2    |      |      |  |  |
| Cap, veh/h                   | 270         | 1102       | 696      | 592  | 416         | 372  |      |      |  |  |
| Arrive On Green              | 0.16        | 0.61       | 0.37     | 0.37 | 0.23        | 0.23 |      |      |  |  |
| Sat Flow, veh/h              | 1723        | 1810       | 1863     | 1583 | 1774        | 1583 |      |      |  |  |
| Grp Volume(v), veh/h         | 221         | 311        | 711      | 504  | 312         | 372  |      |      |  |  |
| Grp Sat Flow(s), veh/h/ln    | 1723        | 1810       | 1863     | 1583 | 1774        | 1583 |      |      |  |  |
| . ,                          | 7.1         |            | 21.5     | 16.8 | 9.4         | 13.5 |      |      |  |  |
| Q Serve(g_s), s              | 7.1         | 4.7<br>4.7 | 21.5     | 16.8 | 9.4         | 13.5 |      |      |  |  |
| Cycle Q Clear(g_c), s        |             | 4.7        | 21.5     |      |             | 1.00 |      |      |  |  |
| Prop In Lane                 | 1.00<br>270 | 1100       | coc      | 1.00 | 1.00<br>416 | 372  |      |      |  |  |
| Lane Grp Cap(c), veh/h       |             | 1102       | 696      | 592  |             |      |      |      |  |  |
| V/C Ratio(X)                 | 0.82        | 0.28       | 1.02     | 0.85 | 0.75        | 1.00 |      |      |  |  |
| Avail Cap(c_a), veh/h        | 345         | 1180       | 696      | 592  | 416         | 372  |      |      |  |  |
| HCM Platoon Ratio            | 1.00        | 1.00       | 1.00     | 1.00 | 1.00        | 1.00 |      |      |  |  |
| Upstream Filter(I)           | 1.00        | 1.00       | 1.00     | 1.00 | 1.00        | 1.00 |      |      |  |  |
| Uniform Delay (d), s/veh     | 23.5        | 5.3        | 18.0     | 16.5 | 20.4        | 22.0 |      |      |  |  |
| Incr Delay (d2), s/veh       | 11.5        | 0.1        | 39.5     | 11.4 | 11.7        | 46.9 |      |      |  |  |
| Initial Q Delay(d3),s/veh    | 0.0         | 0.0        | 0.0      | 0.0  | 0.0         | 0.0  |      |      |  |  |
| %ile BackOfQ(50%),veh/ln     | 4.2         | 2.3        | 18.5     | 9.2  | 5.9         | 15.3 |      |      |  |  |
| LnGrp Delay(d),s/veh         | 35.0        | 5.5        | 57.5     | 28.0 | 32.1        | 68.9 |      |      |  |  |
| LnGrp LOS                    | С           | Α          | F        | С    | С           | F    |      |      |  |  |
| Approach Vol, veh/h          |             | 532        | 1215     |      | 684         |      |      |      |  |  |
| Approach Delay, s/veh        |             | 17.7       | 45.3     |      | 52.1        |      |      |      |  |  |
| Approach LOS                 |             | В          | D        |      | D           |      |      |      |  |  |
| Timer                        | 1           | 2          | 3        | 4    | 5           | 6    | 7    | 8    |  |  |
| Assigned Phs                 |             |            |          | 4    |             | 6    | 7    | 8    |  |  |
| Phs Duration (G+Y+Rc), s     |             |            |          | 39.5 |             | 18.0 | 13.5 | 26.0 |  |  |
| Change Period (Y+Rc), s      |             |            |          | 4.5  |             | 4.5  | 4.5  | 4.5  |  |  |
| Max Green Setting (Gmax), s  |             |            |          | 37.5 |             | 13.5 | 11.5 | 21.5 |  |  |
| Max Q Clear Time (g_c+l1), s |             |            |          | 6.7  |             | 15.5 | 9.1  | 23.5 |  |  |
| Green Ext Time (p_c), s      |             |            |          | 2.0  |             | 0.0  | 0.1  | 0.0  |  |  |
| Intersection Summary         |             |            |          |      |             |      |      |      |  |  |
| HCM 2010 Ctrl Delay          |             |            | 41.2     |      |             |      |      |      |  |  |
| HCM 2010 LOS                 |             |            | D        |      |             |      |      |      |  |  |

|                               | ۶          | -        | •      | •     | <b>—</b>   | •          | •       | <b>†</b> | ~    | <b>\</b> | <b>↓</b> | -√   |
|-------------------------------|------------|----------|--------|-------|------------|------------|---------|----------|------|----------|----------|------|
| Movement                      | EBL        | EBT      | EBR    | WBL   | WBT        | WBR        | NBL     | NBT      | NBR  | SBL      | SBT      | SBR  |
| Lane Configurations           | *          | <b>†</b> | 7      | Ţ     | f)         |            |         | ર્ન      | 7    |          | 4        | 7    |
| Traffic Volume (vph)          | 15         | 650      | 490    | 75    | 1050       | 30         | 873     | 30       | 75   | 55       | 25       | 10   |
| Future Volume (vph)           | 15         | 650      | 490    | 75    | 1050       | 30         | 873     | 30       | 75   | 55       | 25       | 10   |
| Ideal Flow (vphpl)            | 1900       | 1900     | 1900   | 1900  | 1900       | 1900       | 1900    | 1900     | 1900 | 1900     | 1900     | 1900 |
| Total Lost time (s)           | 4.5        | 4.5      | 4.5    | 4.5   | 4.5        |            |         | 4.5      | 4.5  |          | 4.5      | 4.5  |
| Lane Util. Factor             | 1.00       | 1.00     | 1.00   | 1.00  | 1.00       |            |         | 1.00     | 1.00 |          | 1.00     | 1.00 |
| Frt                           | 1.00       | 1.00     | 0.85   | 1.00  | 1.00       |            |         | 1.00     | 0.85 |          | 1.00     | 0.85 |
| Flt Protected                 | 0.95       | 1.00     | 1.00   | 0.95  | 1.00       |            |         | 0.95     | 1.00 |          | 0.97     | 1.00 |
| Satd. Flow (prot)             | 1612       | 1696     | 1442   | 1543  | 1617       |            |         | 1777     | 1583 |          | 1749     | 1538 |
| Flt Permitted                 | 0.95       | 1.00     | 1.00   | 0.95  | 1.00       |            |         | 0.95     | 1.00 |          | 0.97     | 1.00 |
| Satd. Flow (perm)             | 1612       | 1696     | 1442   | 1543  | 1617       |            |         | 1777     | 1583 |          | 1749     | 1538 |
| Peak-hour factor, PHF         | 0.96       | 0.96     | 0.96   | 0.96  | 0.96       | 0.96       | 0.96    | 0.96     | 0.96 | 0.96     | 0.96     | 0.96 |
| Adj. Flow (vph)               | 16         | 677      | 510    | 78    | 1094       | 31         | 909     | 31       | 78   | 57       | 26       | 10   |
| RTOR Reduction (vph)          | 0          | 0        | 285    | 0     | 1          | 0          | 0       | 0        | 54   | 0        | 0        | 9    |
| Lane Group Flow (vph)         | 16         | 677      | 225    | 78    | 1124       | 0          | 0       | 940      | 24   | 0        | 83       | 1    |
| Heavy Vehicles (%)            | 12%        | 12%      | 12%    | 17%   | 17%        | 17%        | 2%      | 2%       | 2%   | 5%       | 5%       | 5%   |
| Turn Type                     | Prot       | NA       | Perm   | Prot  | NA         |            | Split   | NA       | Perm | Split    | NA       | Perm |
| Protected Phases              | 7          | 4        |        | 3     | 8          |            | 5       | 5        |      | 6        | 6        |      |
| Permitted Phases              |            |          | 4      |       |            |            |         |          | 5    |          |          | 6    |
| Actuated Green, G (s)         | 2.0        | 54.2     | 54.2   | 5.0   | 57.2       |            |         | 38.5     | 38.5 |          | 7.0      | 7.0  |
| Effective Green, g (s)        | 2.0        | 54.2     | 54.2   | 5.0   | 57.2       |            |         | 38.5     | 38.5 |          | 7.0      | 7.0  |
| Actuated g/C Ratio            | 0.02       | 0.44     | 0.44   | 0.04  | 0.47       |            |         | 0.31     | 0.31 |          | 0.06     | 0.06 |
| Clearance Time (s)            | 4.5        | 4.5      | 4.5    | 4.5   | 4.5        |            |         | 4.5      | 4.5  |          | 4.5      | 4.5  |
| Vehicle Extension (s)         | 3.0        | 3.0      | 3.0    | 3.0   | 3.0        |            |         | 3.0      | 3.0  |          | 3.0      | 3.0  |
| Lane Grp Cap (vph)            | 26         | 749      | 636    | 62    | 753        |            |         | 557      | 496  |          | 99       | 87   |
| v/s Ratio Prot                | 0.01       | 0.40     |        | c0.05 | c0.70      |            |         | c0.53    |      |          | c0.05    |      |
| v/s Ratio Perm                |            |          | 0.16   |       |            |            |         |          | 0.02 |          |          | 0.00 |
| v/c Ratio                     | 0.62       | 0.90     | 0.35   | 1.26  | 1.49       |            |         | 1.69     | 0.05 |          | 0.84     | 0.01 |
| Uniform Delay, d1             | 60.0       | 31.8     | 22.7   | 58.9  | 32.8       |            |         | 42.1     | 29.3 |          | 57.3     | 54.6 |
| Progression Factor            | 1.00       | 1.00     | 1.00   | 1.00  | 1.00       |            |         | 1.00     | 1.00 |          | 1.00     | 1.00 |
| Incremental Delay, d2         | 36.3       | 16.4     | 1.5    | 198.8 | 229.0      |            |         | 317.2    | 0.0  |          | 43.1     | 0.0  |
| Delay (s)                     | 96.2       | 48.2     | 24.2   | 257.7 | 261.8      |            |         | 359.3    | 29.4 |          | 100.4    | 54.6 |
| Level of Service              | F          | D        | С      | F     | F          |            |         | F        | С    |          | F        | D    |
| Approach Delay (s)            |            | 38.7     |        |       | 261.5      |            |         | 334.0    |      |          | 95.5     |      |
| Approach LOS                  |            | D        |        |       | F          |            |         | F        |      |          | F        |      |
| Intersection Summary          |            |          |        |       |            |            |         |          |      |          |          |      |
| HCM 2000 Control Delay        |            |          | 201.9  | Н     | CM 2000    | Level of   | Service |          | F    |          |          |      |
| HCM 2000 Volume to Capa       | city ratio |          | 1.54   |       |            |            |         |          |      |          |          |      |
| Actuated Cycle Length (s)     |            |          | 122.7  |       | um of lost |            |         |          | 18.0 |          |          |      |
| Intersection Capacity Utiliza | ation      |          | 126.4% | IC    | CU Level   | of Service |         |          | Н    |          |          |      |
| Analysis Period (min)         |            |          | 15     |       |            |            |         |          |      |          |          |      |
| c Critical Lane Group         |            |          |        |       |            |            |         |          |      |          |          |      |

|                              | ۶    | <b>→</b> | •    | <b>√</b> | <b>←</b> | •    | •     | <b>†</b>    | <u> </u> | <b>\</b> | <b></b> | ✓    |
|------------------------------|------|----------|------|----------|----------|------|-------|-------------|----------|----------|---------|------|
| Movement                     | EBL  | EBT      | EBR  | WBL      | WBT      | WBR  | NBL   | NBT         | NBR      | SBL      | SBT     | SBR  |
| Lane Configurations          | 1,1  | <b>^</b> | 7    | 7        | <b>^</b> | 7    | ሻሻ    | <b>↑</b> ↑₽ |          | ሻሻ       | ተተተ     | 7    |
| Traffic Volume (veh/h)       | 270  | 291      | 169  | 175      | 545      | 398  | 288   | 831         | 87       | 290      | 581     | 269  |
| Future Volume (veh/h)        | 270  | 291      | 169  | 175      | 545      | 398  | 288   | 831         | 87       | 290      | 581     | 269  |
| Number                       | 7    | 4        | 14   | 3        | 8        | 18   | 5     | 2           | 12       | 1        | 6       | 16   |
| Initial Q (Qb), veh          | 0    | 0        | 0    | 0        | 0        | 0    | 0     | 0           | 0        | 0        | 0       | 0    |
| Ped-Bike Adj(A_pbT)          | 1.00 |          | 0.98 | 1.00     |          | 0.97 | 1.00  |             | 1.00     | 1.00     |         | 1.00 |
| Parking Bus, Adj             | 1.00 | 1.00     | 1.00 | 1.00     | 1.00     | 1.00 | 1.00  | 1.00        | 1.00     | 1.00     | 1.00    | 1.00 |
| Adj Sat Flow, veh/h/ln       | 1863 | 1863     | 1863 | 1863     | 1863     | 1863 | 1863  | 1863        | 1900     | 1845     | 1845    | 1845 |
| Adj Flow Rate, veh/h         | 290  | 313      | 182  | 188      | 586      | 428  | 310   | 894         | 94       | 312      | 625     | 289  |
| Adj No. of Lanes             | 2    | 2        | 1    | 1        | 2        | 1    | 2     | 3           | 0        | 2        | 3       | 1    |
| Peak Hour Factor             | 0.93 | 0.93     | 0.93 | 0.93     | 0.93     | 0.93 | 0.93  | 0.93        | 0.93     | 0.93     | 0.93    | 0.93 |
| Percent Heavy Veh, %         | 2    | 2        | 2    | 2        | 2        | 2    | 2     | 2           | 2        | 3        | 3       | 3    |
| Cap, veh/h                   | 286  | 980      | 554  | 150      | 986      | 428  | 265   | 1331        | 139      | 262      | 1433    | 575  |
| Arrive On Green              | 0.08 | 0.28     | 0.28 | 0.08     | 0.28     | 0.28 | 0.08  | 0.28        | 0.28     | 0.08     | 0.28    | 0.28 |
| Sat Flow, veh/h              | 3442 | 3539     | 1559 | 1774     | 3539     | 1536 | 3442  | 4675        | 490      | 3408     | 5036    | 1561 |
| Grp Volume(v), veh/h         | 290  | 313      | 182  | 188      | 586      | 428  | 310   | 647         | 341      | 312      | 625     | 289  |
| Grp Sat Flow(s),veh/h/ln     | 1721 | 1770     | 1559 | 1774     | 1770     | 1536 | 1721  | 1695        | 1775     | 1704     | 1679    | 1561 |
| Q Serve(g_s), s              | 5.4  | 4.6      | 5.5  | 5.5      | 9.3      | 18.1 | 5.0   | 11.0        | 11.0     | 5.0      | 6.6     | 9.3  |
| Cycle Q Clear(g_c), s        | 5.4  | 4.6      | 5.5  | 5.5      | 9.3      | 18.1 | 5.0   | 11.0        | 11.0     | 5.0      | 6.6     | 9.3  |
| Prop In Lane                 | 1.00 |          | 1.00 | 1.00     |          | 1.00 | 1.00  |             | 0.28     | 1.00     |         | 1.00 |
| Lane Grp Cap(c), veh/h       | 286  | 980      | 554  | 150      | 986      | 428  | 265   | 965         | 505      | 262      | 1433    | 575  |
| V/C Ratio(X)                 | 1.01 | 0.32     | 0.33 | 1.25     | 0.59     | 1.00 | 1.17  | 0.67        | 0.67     | 1.19     | 0.44    | 0.50 |
| Avail Cap(c_a), veh/h        | 286  | 980      | 554  | 150      | 986      | 428  | 265   | 965         | 505      | 262      | 1433    | 575  |
| HCM Platoon Ratio            | 1.00 | 1.00     | 1.00 | 1.00     | 1.00     | 1.00 | 1.00  | 1.00        | 1.00     | 1.00     | 1.00    | 1.00 |
| Upstream Filter(I)           | 1.00 | 1.00     | 1.00 | 1.00     | 1.00     | 1.00 | 1.00  | 1.00        | 1.00     | 1.00     | 1.00    | 1.00 |
| Uniform Delay (d), s/veh     | 29.8 | 18.6     | 15.4 | 29.7     | 20.3     | 23.4 | 30.0  | 20.6        | 20.6     | 30.0     | 19.0    | 15.9 |
| Incr Delay (d2), s/veh       | 56.9 | 0.2      | 0.3  | 156.7    | 1.0      | 43.8 | 109.6 | 3.7         | 7.0      | 117.0    | 1.0     | 3.1  |
| Initial Q Delay(d3),s/veh    | 0.1  | 0.0      | 0.0  | 0.0      | 0.0      | 0.0  | 0.0   | 0.0         | 0.0      | 0.0      | 0.0     | 0.0  |
| %ile BackOfQ(50%),veh/ln     | 4.8  | 2.2      | 2.4  | 9.2      | 4.7      | 12.8 | 6.4   | 5.6         | 6.4      | 6.6      | 3.1     | 4.5  |
| LnGrp Delay(d),s/veh         | 86.8 | 18.8     | 15.7 | 186.5    | 21.2     | 67.2 | 139.6 | 24.3        | 27.6     | 147.0    | 20.0    | 19.1 |
| LnGrp LOS                    | F    | В        | В    | F        | С        | F    | F     | С           | С        | F        | В       | В    |
| Approach Vol, veh/h          |      | 785      |      |          | 1202     |      |       | 1298        |          |          | 1226    |      |
| Approach Delay, s/veh        |      | 43.2     |      |          | 63.5     |      |       | 52.7        |          |          | 52.1    |      |
| Approach LOS                 |      | D        |      |          | Е        |      |       | D           |          |          | D       |      |
| Timer                        | 1    | 2        | 3    | 4        | 5        | 6    | 7     | 8           |          |          |         |      |
| Assigned Phs                 | 1    | 2        | 3    | 4        | 5        | 6    | 7     | 8           |          |          |         |      |
| Phs Duration (G+Y+Rc), s     | 9.5  | 23.0     | 10.0 | 22.5     | 9.5      | 23.0 | 9.9   | 22.6        |          |          |         |      |
| Change Period (Y+Rc), s      | 4.5  | 4.5      | 4.5  | 4.5      | 4.5      | 4.5  | 4.5   | 4.5         |          |          |         |      |
| Max Green Setting (Gmax), s  | 5.0  | 18.5     | 5.5  | 18.0     | 5.0      | 18.5 | 5.4   | 18.1        |          |          |         |      |
| Max Q Clear Time (g_c+l1), s | 7.0  | 13.0     | 7.5  | 7.5      | 7.0      | 11.3 | 7.4   | 20.1        |          |          |         |      |
| Green Ext Time (p_c), s      | 0.0  | 2.9      | 0.0  | 2.0      | 0.0      | 3.1  | 0.0   | 0.0         |          |          |         |      |
| Intersection Summary         |      |          |      |          |          |      |       |             |          |          |         |      |
| HCM 2010 Ctrl Delay          |      |          | 53.7 |          |          |      |       |             |          |          |         |      |
| HCM 2010 LOS                 |      |          | D    |          |          |      |       |             |          |          |         |      |
|                              |      |          |      |          |          |      |       |             |          |          |         |      |

|                              |      | <b>→</b> | •     | •     | +     | •     | •    | <b>†</b> | <u> </u> | <b>/</b> | <b></b> | 1    |
|------------------------------|------|----------|-------|-------|-------|-------|------|----------|----------|----------|---------|------|
| Movement                     | EBL  | EBT      | EBR   | WBL   | WBT   | WBR   | NBL  | NBT      | NBR      | SBL      | SBT     | SBR  |
| Lane Configurations          |      | 1>       |       | ች     | 1>    |       | ሻ    | <b>1</b> | 7        | ሻ        | 1>      |      |
| Traffic Volume (veh/h)       | 45   | 170      | 46    | 260   | 175   | 367   | 75   | 228      | 200      | 185      | 120     | 25   |
| Future Volume (veh/h)        | 45   | 170      | 46    | 260   | 175   | 367   | 75   | 228      | 200      | 185      | 120     | 25   |
| Number                       | 7    | 4        | 14    | 3     | 8     | 18    | 5    | 2        | 12       | 1        | 6       | 16   |
| Initial Q (Qb), veh          | 0    | 0        | 0     | 0     | 0     | 0     | 0    | 0        | 0        | 0        | 0       | 0    |
| Ped-Bike Adj(A_pbT)          | 1.00 |          | 0.74  | 1.00  |       | 0.89  | 1.00 |          | 0.99     | 1.00     |         | 0.99 |
| Parking Bus, Adj             | 1.00 | 1.00     | 1.00  | 1.00  | 1.00  | 1.00  | 1.00 | 1.00     | 1.00     | 1.00     | 1.00    | 1.00 |
| Adj Sat Flow, veh/h/ln       | 1863 | 1863     | 1900  | 1863  | 1863  | 1900  | 1863 | 1863     | 1863     | 1863     | 1863    | 1900 |
| Adj Flow Rate, veh/h         | 57   | 215      | 58    | 329   | 222   | 465   | 95   | 289      | 253      | 234      | 152     | 32   |
| Adj No. of Lanes             | 1    | 1        | 0     | 1     | 1     | 0     | 1    | 1        | 1        | 1        | 1       | 0    |
| Peak Hour Factor             | 0.79 | 0.79     | 0.79  | 0.79  | 0.79  | 0.79  | 0.79 | 0.79     | 0.79     | 0.79     | 0.79    | 0.79 |
| Percent Heavy Veh, %         | 2    | 2        | 2     | 2     | 2     | 2     | 2    | 2        | 2        | 2        | 2       | 2    |
| Cap, veh/h                   | 85   | 326      | 88    | 235   | 165   | 345   | 122  | 491      | 415      | 166      | 430     | 91   |
| Arrive On Green              | 0.05 | 0.25     | 0.25  | 0.13  | 0.33  | 0.33  | 0.07 | 0.26     | 0.26     | 0.09     | 0.29    | 0.29 |
| Sat Flow, veh/h              | 1774 | 1302     | 351   | 1774  | 492   | 1031  | 1774 | 1863     | 1574     | 1774     | 1489    | 314  |
| Grp Volume(v), veh/h         | 57   | 0        | 273   | 329   | 0     | 687   | 95   | 289      | 253      | 234      | 0       | 184  |
| Grp Sat Flow(s),veh/h/ln     | 1774 | 0        | 1653  | 1774  | 0     | 1523  | 1774 | 1863     | 1574     | 1774     | 0       | 1803 |
| Q Serve(g_s), s              | 2.2  | 0.0      | 10.3  | 9.2   | 0.0   | 23.2  | 3.7  | 9.4      | 9.8      | 6.5      | 0.0     | 5.6  |
| Cycle Q Clear(g_c), s        | 2.2  | 0.0      | 10.3  | 9.2   | 0.0   | 23.2  | 3.7  | 9.4      | 9.8      | 6.5      | 0.0     | 5.6  |
| Prop In Lane                 | 1.00 |          | 0.21  | 1.00  |       | 0.68  | 1.00 |          | 1.00     | 1.00     |         | 0.17 |
| Lane Grp Cap(c), veh/h       | 85   | 0        | 414   | 235   | 0     | 510   | 122  | 491      | 415      | 166      | 0       | 521  |
| V/C Ratio(X)                 | 0.67 | 0.00     | 0.66  | 1.40  | 0.00  | 1.35  | 0.78 | 0.59     | 0.61     | 1.41     | 0.00    | 0.35 |
| Avail Cap(c_a), veh/h        | 130  | 0        | 429   | 235   | 0     | 510   | 159  | 491      | 415      | 166      | 0       | 521  |
| HCM Platoon Ratio            | 1.00 | 1.00     | 1.00  | 1.00  | 1.00  | 1.00  | 1.00 | 1.00     | 1.00     | 1.00     | 1.00    | 1.00 |
| Upstream Filter(I)           | 1.00 | 0.00     | 1.00  | 1.00  | 0.00  | 1.00  | 1.00 | 1.00     | 1.00     | 1.00     | 0.00    | 1.00 |
| Uniform Delay (d), s/veh     | 32.5 | 0.0      | 23.3  | 30.1  | 0.0   | 23.1  | 31.8 | 22.2     | 22.4     | 31.4     | 0.0     | 19.5 |
| Incr Delay (d2), s/veh       | 8.7  | 0.0      | 3.5   | 202.9 | 0.0   | 168.6 | 16.7 | 5.1      | 6.5      | 215.3    | 0.0     | 1.9  |
| Initial Q Delay(d3),s/veh    | 0.0  | 0.0      | 0.0   | 0.0   | 0.0   | 0.0   | 0.0  | 0.0      | 0.0      | 0.0      | 0.0     | 0.0  |
| %ile BackOfQ(50%),veh/ln     | 1.3  | 0.0      | 5.1   | 17.7  | 0.0   | 33.5  | 2.4  | 5.5      | 5.0      | 13.1     | 0.0     | 3.0  |
| LnGrp Delay(d),s/veh         | 41.2 | 0.0      | 26.9  | 233.0 | 0.0   | 191.7 | 48.5 | 27.3     | 28.9     | 246.7    | 0.0     | 21.4 |
| LnGrp LOS                    | D    |          | С     | F     |       | F     | D    | С        | С        | F        |         | С    |
| Approach Vol, veh/h          |      | 330      |       |       | 1016  |       |      | 637      |          |          | 418     |      |
| Approach Delay, s/veh        |      | 29.4     |       |       | 205.1 |       |      | 31.1     |          |          | 147.5   |      |
| Approach LOS                 |      | С        |       |       | F     |       |      | С        |          |          | F       |      |
| Timer                        | 1    | 2        | 3     | 4     | 5     | 6     | 7    | 8        |          |          |         |      |
| Assigned Phs                 | 1    | 2        | 3     | 4     | 5     | 6     | 7    | 8        |          |          |         |      |
| Phs Duration (G+Y+Rc), s     | 11.0 | 22.8     | 13.7  | 21.9  | 9.3   | 24.5  | 7.8  | 27.7     |          |          |         |      |
| Change Period (Y+Rc), s      | 4.5  | 4.5      | 4.5   | 4.5   | 4.5   | 4.5   | 4.5  | 4.5      |          |          |         |      |
| Max Green Setting (Gmax), s  | 6.5  | 18.3     | 9.2   | 18.0  | 6.2   | 18.6  | 5.1  | 22.1     |          |          |         |      |
| Max Q Clear Time (g_c+l1), s | 8.5  | 11.8     | 11.2  | 12.3  | 5.7   | 7.6   | 4.2  | 25.2     |          |          |         |      |
| Green Ext Time (p_c), s      | 0.0  | 1.5      | 0.0   | 8.0   | 0.0   | 0.7   | 0.0  | 0.0      |          |          |         |      |
| Intersection Summary         |      |          |       |       |       |       |      |          |          |          |         |      |
| HCM 2010 Ctrl Delay          |      |          | 124.8 |       |       |       |      |          |          |          |         |      |
| HCM 2010 LOS                 |      |          | F     |       |       |       |      |          |          |          |         |      |

0.423

19.8

С

2

0.149

13.8

В

0.5

0.333

16

C

1.4

0.724

30.7

D

5.7

0.629

22.6

С

4.2

0.027

12.8

В

0.1

0.659

28.3

D

4.6

| Interception               |           |          |       |       |          |       |       |       |       |       |          |       |
|----------------------------|-----------|----------|-------|-------|----------|-------|-------|-------|-------|-------|----------|-------|
| Intersection Delay a half  | 04.0      |          |       |       |          |       |       |       |       |       |          |       |
| Intersection Delay, s/veh  | 21.9<br>C |          |       |       |          |       |       |       |       |       |          |       |
| Intersection LOS           | C         |          |       |       |          |       |       |       |       |       |          |       |
|                            |           |          |       |       |          |       |       |       |       |       |          |       |
| Movement                   | EBL       | EBT      | EBR   | WBL   | WBT      | WBR   | NBL   | NBT   | NBR   | SBL   | SBT      | SBR   |
| Lane Configurations        | 7         | <b>†</b> | 7     | 7     | <b>↑</b> | 7     | ሻ     | f)    |       | *     | <b>↑</b> | 7     |
| Traffic Vol, veh/h         | 130       | 303      | 286   | 10    | 251      | 95    | 148   | 50    | 5     | 115   | 103      | 149   |
| Future Vol, veh/h          | 130       | 303      | 286   | 10    | 251      | 95    | 148   | 50    | 5     | 115   | 103      | 149   |
| Peak Hour Factor           | 0.97      | 0.97     | 0.97  | 0.97  | 0.97     | 0.97  | 0.97  | 0.97  | 0.97  | 0.97  | 0.97     | 0.97  |
| Heavy Vehicles, %          | 2         | 2        | 2     | 2     | 2        | 2     | 2     | 2     | 2     | 2     | 2        | 2     |
| Mvmt Flow                  | 134       | 312      | 295   | 10    | 259      | 98    | 153   | 52    | 5     | 119   | 106      | 154   |
| Number of Lanes            | 1         | 1        | 1     | 1     | 1        | 1     | 1     | 1     | 0     | 1     | 1        | 1     |
| Approach                   | EB        |          |       | WB    |          |       | NB    |       |       | SB    |          |       |
| Opposing Approach          | WB        |          |       | EB    |          |       | SB    |       |       | NB    |          |       |
| Opposing Lanes             | 3         |          |       | 3     |          |       | 3     |       |       | 2     |          |       |
| Conflicting Approach Left  | SB        |          |       | NB    |          |       | EB    |       |       | WB    |          |       |
| Conflicting Lanes Left     | 3         |          |       | 2     |          |       | 3     |       |       | 3     |          |       |
| Conflicting Approach Right | NB        |          |       | SB    |          |       | WB    |       |       | EB    |          |       |
| Conflicting Lanes Right    | 2         |          |       | 3     |          |       | 3     |       |       | 3     |          |       |
| HCM Control Delay          | 24.8      |          |       | 24    |          |       | 18.2  |       |       | 16.2  |          |       |
| HCM LOS                    | С         |          |       | С     |          |       | С     |       |       | С     |          |       |
|                            |           |          |       |       |          |       |       |       |       |       |          |       |
| Lane                       |           | NBLn1    | NBLn2 | EBLn1 | EBLn2    | EBLn3 | WBLn1 | WBLn2 | WBLn3 | SBLn1 | SBLn2    | SBLn3 |
| Vol Left, %                |           | 100%     | 0%    | 100%  | 0%       | 0%    | 100%  | 0%    | 0%    | 100%  | 0%       | 0%    |
| Vol Thru, %                |           | 0%       | 91%   | 0%    | 100%     | 0%    | 0%    | 100%  | 0%    | 0%    | 100%     | 0%    |
| Vol Right, %               |           | 0%       | 9%    | 0%    | 0%       | 100%  | 0%    | 0%    | 100%  | 0%    | 0%       | 100%  |
| Sign Control               |           | Stop     | Stop  | Stop  | Stop     | Stop  | Stop  | Stop  | Stop  | Stop  | Stop     | Stop  |
| Traffic Vol by Lane        |           | 148      | 55    | 130   | 303      | 286   | 10    | 251   | 95    | 115   | 103      | 149   |
| LT Vol                     |           | 148      | 0     | 130   | 0        | 0     | 10    | 0     | 0     | 115   | 0        | 0     |
| Through Vol                |           | 0        | 50    | 0     | 303      | 0     | 0     | 251   | 0     | 0     | 103      | 0     |
| RT Vol                     |           | 0        | 5     | 0     | 0        | 286   | 0     | 0     | 95    | 0     | 0        | 149   |
| Lane Flow Rate             |           | 153      | 57    | 134   | 312      | 295   | 10    | 259   | 98    | 119   | 106      | 154   |
| Geometry Grp               |           | 8        | 8     | 8     | 8        | 8     | 8     | 8     | 8     | 8     | 8        | 8     |
| Degree of Util (X)         |           | 0.421    | 0.148 | 0.331 | 0.728    | 0.629 | 0.028 | 0.661 | 0.231 | 0.32  | 0.272    | 0.363 |
| Departure Headway (Hd)     |           | 9.939    | 9.375 | 8.904 | 8.393    | 7.678 | 9.711 | 9.198 | 8.481 | 9.723 | 9.215    | 8.503 |
| Convergence, Y/N           |           | Yes      | Yes   | Yes   | Yes      | Yes   | Yes   | Yes   | Yes   | Yes   | Yes      | Yes   |
| Cap                        |           | 362      | 382   | 403   | 431      | 469   | 368   | 393   | 423   | 370   | 390      | 422   |
| Service Time               |           | 7.702    | 7.139 | 6.659 | 6.148    | 5.432 | 7.474 | 6.961 | 6.243 | 7.487 | 6.978    | 6.266 |
|                            |           |          |       |       |          |       | ~ ~~= |       |       |       |          |       |

HCM Lane V/C Ratio

**HCM Control Delay** 

HCM Lane LOS

HCM 95th-tile Q

0.365

16.1

C

1.6

0.272

15.4

C

1.1

0.232

13.8

В

0.9

0.322

17

C

1.4

| Intersection           |        |            |           |         |          |      |          |          |              |        |          |           |           |
|------------------------|--------|------------|-----------|---------|----------|------|----------|----------|--------------|--------|----------|-----------|-----------|
| Int Delay, s/veh       | 9.7    |            |           |         |          |      |          |          |              |        |          |           |           |
| Movement               | EBL    | EBT        | EBR       | WBL     | WBT      | WBR  | NBL      | NBT      | NBR          | SBL    | SBT      | SBR       |           |
| Lane Configurations    | ሻ      | <b>^</b>   | 7         | *       | <b>†</b> | 7    | ሻ        | <b>↑</b> | 7            | ሻ      | <b>†</b> | 7         |           |
| Traffic Vol, veh/h     | 175    | 649        | 95        | 60      | 446      | 42   | 35       | 5        | 45           | 25     | 5        | 100       |           |
| Future Vol, veh/h      | 175    | 649        | 95        | 60      | 446      | 42   | 35       | 5        | 45           | 25     | 5        | 100       |           |
| Conflicting Peds, #/hr | 0      | 0          | 0         | 0       | 0        | 0    | 0        | 0        | 0            | 0      | 0        | 0         |           |
| Sign Control           | Free   | Free       | Free      | Free    | Free     | Free | Stop     | Stop     | Stop         | Stop   | Stop     | Stop      |           |
| RT Channelized         | -      | -          | None      | -       | -        | None | -        | -        | None         | -      | -        | None      |           |
| Storage Length         | 320    | -          | 505       | 360     | -        | 195  | 60       | -        | 0            | 100    | -        | 100       |           |
| Veh in Median Storage  | e, # - | 0          | -         | -       | 0        | -    | -        | 0        | -            | -      | 0        | -         |           |
| Grade, %               | -      | 0          | -         | -       | 0        | -    | -        | 0        | -            | -      | 0        | -         |           |
| Peak Hour Factor       | 95     | 95         | 95        | 95      | 95       | 95   | 95       | 95       | 95           | 95     | 95       | 95        |           |
| Heavy Vehicles, %      | 2      | 2          | 2         | 2       | 2        | 2    | 2        | 2        | 2            | 2      | 2        | 2         |           |
| Mvmt Flow              | 184    | 683        | 100       | 63      | 469      | 44   | 37       | 5        | 47           | 26     | 5        | 105       |           |
|                        |        |            |           |         |          |      |          |          |              |        |          |           |           |
| Major/Minor I          | Major1 |            | 1         | Major2  |          |      | Minor1   |          |              | Minor2 |          |           |           |
| Conflicting Flow All   | 513    | 0          | 0         | 783     | 0        | 0    | 1723     | 1690     | 683          | 1722   | 1746     | 469       |           |
| Stage 1                | -      | -          | -         | _       | -        | -    | 1051     | 1051     | -            | 595    | 595      |           |           |
| Stage 2                | _      | -          | -         | _       | _        | _    | 672      | 639      | -            | 1127   | 1151     | _         |           |
| Critical Hdwy          | 4.12   | -          | -         | 4.12    | -        | -    | 7.12     | 6.52     | 6.22         | 7.12   | 6.52     | 6.22      |           |
| Critical Hdwy Stg 1    | _      | -          | -         | -       | -        | -    | 6.12     | 5.52     | _            | 6.12   | 5.52     | -         |           |
| Critical Hdwy Stg 2    | -      | -          | -         | -       | -        | -    | 6.12     | 5.52     | -            | 6.12   | 5.52     | -         |           |
| Follow-up Hdwy         | 2.218  | -          | -         | 2.218   | -        | -    | 3.518    | 4.018    | 3.318        | 3.518  | 4.018    | 3.318     |           |
| Pot Cap-1 Maneuver     | 1052   | -          | -         | 835     | -        | -    | 70       | 93       | 449          | 70     | 86       | 594       |           |
| Stage 1                | -      | -          | -         | -       | -        | -    | 274      | 304      | -            | 491    | 492      | -         |           |
| Stage 2                | -      | -          | -         | -       | -        | -    | 445      | 470      | -            | 249    | 272      | -         |           |
| Platoon blocked, %     |        | -          | -         |         | -        | -    |          |          |              |        |          |           |           |
| Mov Cap-1 Maneuver     | 1052   | -          | -         | 835     | -        | -    | 44       | 71       | 449          | 48     | 66       | 594       |           |
| Mov Cap-2 Maneuver     | -      | -          | -         | -       | -        | -    | 44       | 71       | -            | 48     | 66       | -         |           |
| Stage 1                | -      | -          | -         | -       | -        | -    | 226      | 251      | -            | 405    | 455      | -         |           |
| Stage 2                | -      | -          | -         | -       | -        | -    | 335      | 435      | -            | 180    | 224      | -         |           |
|                        |        |            |           |         |          |      |          |          |              |        |          |           |           |
| Approach               | EB     |            |           | WB      |          |      | NB       |          |              | SB     |          |           |           |
| HCM Control Delay, s   | 1.7    |            |           | 1.1     |          |      | 105.5    |          |              | 40.5   |          |           |           |
| HCM LOS                |        |            |           |         |          |      | F        |          |              | E      |          |           |           |
|                        |        |            |           |         |          |      |          |          |              |        |          |           |           |
| Minor Lane/Major Mvm   | nt     | NBLn11     | VRI n21   | VRI n3  | EBL      | EBT  | EBR      | WBL      | WBT          | WRR    | SBL n1   | SBLn2 S   | SBI n3    |
| Capacity (veh/h)       |        | 44         | 71        | 449     | 1052     | LDI  | LDI      | 835      | 7701         | WDIN   | 48       | 66        | 594       |
| HCM Lane V/C Ratio     |        |            |           | 0.105   |          | -    | _        | 0.076    | -            | _      | 0.548    |           | 0.177     |
| HCM Control Delay (s)  |        | 229.6      | 59.7      | 14      | 9.1      | -    | -        | 9.7      | <del>-</del> | -      | 4400     | 64.2      | 12.4      |
| HCM Lane LOS           |        | 229.0<br>F | 59.7<br>F | 14<br>B | 9.1<br>A | -    | <u>-</u> | 9.7<br>A | -            | _      | 140.Z    | 04.Z<br>F | 12.4<br>B |
| HCM 95th %tile Q(veh)  | ١      | 3.3        | 0.2       | 0.4     | 0.6      | -    | -        | 0.2      | _            | -      | 2.1      | 0.3       | 0.6       |
| How Jour Joure Wind    |        | 0.0        | 0.2       | 0.4     | 0.0      | _    | _        | 0.2      | _            | _      | ۷. ۱     | 0.0       | 0.0       |

| Intersection           |           |       |         |       |        |              |
|------------------------|-----------|-------|---------|-------|--------|--------------|
| Int Delay, s/veh       | 1.7       |       |         |       |        |              |
|                        |           | WDD   | NDT     | NDD   | ODI    | ODT          |
| Movement               | WBL       | WBR   | NBT     | NBR   | SBL    | SBT          |
| Lane Configurations    | ¥         |       | ĵ.      |       |        | र्स          |
| Traffic Vol, veh/h     | 32        | 36    | 207     | 28    | 37     | 315          |
| Future Vol, veh/h      | 32        | 36    | 207     | 28    | 37     | 315          |
| Conflicting Peds, #/hr | 1         | 0     | 0       | 0     | 0      | 0            |
| Sign Control           | Stop      | Stop  | Free    | Free  | Free   | Free         |
| RT Channelized         | -         | None  | -       | None  | -      | None         |
| Storage Length         | 0         | -     | -       | -     | -      | _            |
| Veh in Median Storage  | e, # 0    | -     | 0       | -     | -      | 0            |
| Grade, %               | 0         | -     | 0       | -     | -      | 0            |
| Peak Hour Factor       | 93        | 93    | 93      | 93    | 93     | 93           |
| Heavy Vehicles, %      | 6         | 6     | 2       | 2     | 3      | 3            |
| Mvmt Flow              | 34        | 39    | 223     | 30    | 40     | 339          |
| WWW.CT IOW             | V I       | 00    | 220     | 00    | 10     | 000          |
|                        |           |       |         |       |        |              |
|                        | Minor1    |       | //ajor1 |       | Major2 |              |
| Conflicting Flow All   | 658       | 238   | 0       | 0     | 253    | 0            |
| Stage 1                | 238       | -     | -       | -     | -      | -            |
| Stage 2                | 420       | -     | -       | -     | -      | -            |
| Critical Hdwy          | 6.46      | 6.26  | -       | -     | 4.13   | -            |
| Critical Hdwy Stg 1    | 5.46      | -     | -       | _     | _      | _            |
| Critical Hdwy Stg 2    | 5.46      | _     | _       | -     | -      | _            |
| Follow-up Hdwy         | 3.554     | 3.354 | -       | _     | 2.227  | _            |
| Pot Cap-1 Maneuver     | 423       | 791   | _       | _     | 1306   | _            |
| Stage 1                | 792       | -     | _       | _     | -      | _            |
| Stage 2                | 654       | _     | _       | _     | _      | _            |
| Platoon blocked, %     | 004       |       |         | _     |        | _            |
| Mov Cap-1 Maneuver     | 407       | 791   | -       | _     | 1306   | _            |
|                        |           |       |         |       |        | <del>-</del> |
| Mov Cap-2 Maneuver     | 407       | -     | -       | -     | -      | -            |
| Stage 1                | 762       | -     | -       | -     | -      | -            |
| Stage 2                | 653       | -     | -       | -     | -      | -            |
|                        |           |       |         |       |        |              |
| Approach               | WB        |       | NB      |       | SB     |              |
| HCM Control Delay, s   | 12.6      |       | 0       |       | 0.8    |              |
| HCM LOS                | 12.0<br>B |       | U       |       | 0.0    |              |
| TIOW LOO               |           |       |         |       |        |              |
|                        |           |       |         |       |        |              |
| Minor Lane/Major Mvn   | nt        | NBT   | NBRV    | VBLn1 | SBL    | SBT          |
| Capacity (veh/h)       |           | _     | -       | 548   | 1306   | _            |
| HCM Lane V/C Ratio     |           | -     | -       | 0.133 | 0.03   | _            |
| HCM Control Delay (s   | )         | -     | _       |       | 7.8    | 0            |
| HCM Lane LOS           |           | _     | _       | В     | A      | A            |
| HCM 95th %tile Q(veh   | 1)        | _     | _       |       | 0.1    | -            |
| HOW SOUT MILE Q(VEH    | 1)        |       | _       | 0.5   | 0.1    | _            |

|                              | ۶    | <b>→</b> | •     | •    | <b>←</b> | •     | •     | †        | ~    | <b>/</b> | <b>↓</b> | 4    |
|------------------------------|------|----------|-------|------|----------|-------|-------|----------|------|----------|----------|------|
| Movement                     | EBL  | EBT      | EBR   | WBL  | WBT      | WBR   | NBL   | NBT      | NBR  | SBL      | SBT      | SBR  |
| Lane Configurations          |      | £        |       | ሻ    | ₽        |       | ሻ     | <b>•</b> | 7    | ች        | <b>↑</b> | 7    |
| Traffic Volume (veh/h)       | 295  | 391      | 244   | 25   | 262      | 220   | 200   | 345      | 36   | 375      | 620      | 236  |
| Future Volume (veh/h)        | 295  | 391      | 244   | 25   | 262      | 220   | 200   | 345      | 36   | 375      | 620      | 236  |
| Number                       | 7    | 4        | 14    | 3    | 8        | 18    | 5     | 2        | 12   | 1        | 6        | 16   |
| Initial Q (Qb), veh          | 0    | 0        | 0     | 0    | 0        | 0     | 0     | 0        | 0    | 0        | 0        | 0    |
| Ped-Bike Adj(A_pbT)          | 1.00 |          | 1.00  | 1.00 |          | 1.00  | 1.00  |          | 1.00 | 1.00     |          | 1.00 |
| Parking Bus, Adj             | 1.00 | 1.00     | 1.00  | 1.00 | 1.00     | 1.00  | 1.00  | 1.00     | 1.00 | 1.00     | 1.00     | 1.00 |
| Adj Sat Flow, veh/h/ln       | 1863 | 1863     | 1900  | 1863 | 1863     | 1900  | 1863  | 1863     | 1863 | 1863     | 1863     | 1863 |
| Adj Flow Rate, veh/h         | 307  | 407      | 254   | 26   | 273      | 229   | 208   | 359      | 38   | 391      | 646      | 246  |
| Adj No. of Lanes             | 1    | 1        | 0     | 1    | 1        | 0     | 1     | 1        | 1    | 1        | 1        | 1    |
| Peak Hour Factor             | 0.96 | 0.96     | 0.96  | 0.96 | 0.96     | 0.96  | 0.96  | 0.96     | 0.96 | 0.96     | 0.96     | 0.96 |
| Percent Heavy Veh, %         | 2    | 2        | 2     | 2    | 2        | 2     | 2     | 2        | 2    | 2        | 2        | 2    |
| Cap, veh/h                   | 426  | 258      | 161   | 218  | 115      | 96    | 177   | 479      | 407  | 248      | 554      | 471  |
| Arrive On Green              | 0.24 | 0.24     | 0.24  | 0.12 | 0.12     | 0.12  | 0.10  | 0.26     | 0.26 | 0.14     | 0.30     | 0.30 |
| Sat Flow, veh/h              | 1774 | 1074     | 670   | 1774 | 938      | 786   | 1774  | 1863     | 1583 | 1774     | 1863     | 1583 |
| Grp Volume(v), veh/h         | 307  | 0        | 661   | 26   | 0        | 502   | 208   | 359      | 38   | 391      | 646      | 246  |
| Grp Sat Flow(s),veh/h/ln     | 1774 | 0        | 1744  | 1774 | 0        | 1724  | 1774  | 1863     | 1583 | 1774     | 1863     | 1583 |
| Q Serve(g_s), s              | 11.9 | 0.0      | 18.0  | 1.0  | 0.0      | 9.2   | 7.5   | 13.3     | 1.4  | 10.5     | 22.3     | 9.7  |
| Cycle Q Clear(g_c), s        | 11.9 | 0.0      | 18.0  | 1.0  | 0.0      | 9.2   | 7.5   | 13.3     | 1.4  | 10.5     | 22.3     | 9.7  |
| Prop In Lane                 | 1.00 |          | 0.38  | 1.00 |          | 0.46  | 1.00  |          | 1.00 | 1.00     |          | 1.00 |
| Lane Grp Cap(c), veh/h       | 426  | 0        | 419   | 218  | 0        | 211   | 177   | 479      | 407  | 248      | 554      | 471  |
| V/C Ratio(X)                 | 0.72 | 0.00     | 1.58  | 0.12 | 0.00     | 2.37  | 1.17  | 0.75     | 0.09 | 1.57     | 1.17     | 0.52 |
| Avail Cap(c_a), veh/h        | 426  | 0        | 419   | 218  | 0        | 211   | 177   | 479      | 407  | 248      | 554      | 471  |
| HCM Platoon Ratio            | 1.00 | 1.00     | 1.00  | 1.00 | 1.00     | 1.00  | 1.00  | 1.00     | 1.00 | 1.00     | 1.00     | 1.00 |
| Upstream Filter(I)           | 1.00 | 0.00     | 1.00  | 1.00 | 0.00     | 1.00  | 1.00  | 1.00     | 1.00 | 1.00     | 1.00     | 1.00 |
| Uniform Delay (d), s/veh     | 26.2 | 0.0      | 28.5  | 29.3 | 0.0      | 32.9  | 33.8  | 25.6     | 21.2 | 32.3     | 26.4     | 21.9 |
| Incr Delay (d2), s/veh       | 5.9  | 0.0      | 271.7 | 0.2  | 0.0      | 632.6 | 121.6 | 10.3     | 0.5  | 277.0    | 93.2     | 4.1  |
| Initial Q Delay(d3),s/veh    | 0.0  | 0.0      | 0.0   | 0.0  | 0.0      | 0.0   | 0.0   | 0.0      | 0.0  | 0.0      | 0.0      | 0.0  |
| %ile BackOfQ(50%),veh/ln     | 6.5  | 0.0      | 40.2  | 0.5  | 0.0      | 41.5  | 9.6   | 8.1      | 0.7  | 24.2     | 25.7     | 4.8  |
| LnGrp Delay(d),s/veh         | 32.1 | 0.0      | 300.2 | 29.5 | 0.0      | 665.5 | 155.4 | 35.9     | 21.6 | 309.2    | 119.5    | 26.0 |
| LnGrp LOS                    | С    |          | F     | С    |          | F     | F     | D        | С    | F        | F        | С    |
| Approach Vol, veh/h          |      | 968      |       |      | 528      |       |       | 605      |      |          | 1283     |      |
| Approach Delay, s/veh        |      | 215.2    |       |      | 634.2    |       |       | 76.1     |      |          | 159.4    |      |
| Approach LOS                 |      | F        |       |      | F        |       |       | Е        |      |          | F        |      |
| Timer                        | 1    | 2        | 3     | 4    | 5        | 6     | 7     | 8        |      |          |          |      |
| Assigned Phs                 | 1    | 2        |       | 4    | 5        | 6     |       | 8        |      |          |          |      |
| Phs Duration (G+Y+Rc), s     | 15.0 | 23.8     |       | 22.5 | 12.0     | 26.8  |       | 13.7     |      |          |          |      |
| Change Period (Y+Rc), s      | 4.5  | 4.5      |       | 4.5  | 4.5      | 4.5   |       | 4.5      |      |          |          |      |
| Max Green Setting (Gmax), s  | 10.5 | 19.3     |       | 18.0 | 7.5      | 22.3  |       | 9.2      |      |          |          |      |
| Max Q Clear Time (g_c+l1), s | 12.5 | 15.3     |       | 20.0 | 9.5      | 24.3  |       | 11.2     |      |          |          |      |
| Green Ext Time (p_c), s      | 0.0  | 0.8      |       | 0.0  | 0.0      | 0.0   |       | 0.0      |      |          |          |      |
| Intersection Summary         |      |          |       |      |          |       |       |          |      |          |          |      |
| HCM 2010 Ctrl Delay          |      |          | 234.5 |      |          |       |       |          |      |          |          |      |
| HCM 2010 LOS                 |      |          | F     |      |          |       |       |          |      |          |          |      |

|                              | •    |          |       |       | 4    | •    | _    | •    | _    |      | 1    |      |
|------------------------------|------|----------|-------|-------|------|------|------|------|------|------|------|------|
|                              |      | <b>→</b> | *     | •     | •    | _    | 7    | ı    |      | *    | +    | *    |
| Movement                     | EBL  | EBT      | EBR   | WBL   | WBT  | WBR  | NBL  | NBT  | NBR  | SBL  | SBT  | SBR  |
| Lane Configurations          | - 1  | î»       |       |       | ₽    |      |      | 4    |      |      | - 4  |      |
| Traffic Volume (veh/h)       | 55   | 780      | 150   | 145   | 488  | 35   | 115  | 50   | 95   | 55   | 75   | 34   |
| Future Volume (veh/h)        | 55   | 780      | 150   | 145   | 488  | 35   | 115  | 50   | 95   | 55   | 75   | 34   |
| Number                       | 7    | 4        | 14    | 3     | 8    | 18   | 5    | 2    | 12   | 1    | 6    | 16   |
| Initial Q (Qb), veh          | 0    | 0        | 0     | 0     | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |
| Ped-Bike Adj(A_pbT)          | 1.00 |          | 1.00  | 1.00  |      | 1.00 | 1.00 |      | 1.00 | 1.00 |      | 1.00 |
| Parking Bus, Adj             | 1.00 | 1.00     | 1.00  | 1.00  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln       | 1863 | 1863     | 1900  | 1863  | 1863 | 1900 | 1900 | 1863 | 1900 | 1900 | 1827 | 1900 |
| Adj Flow Rate, veh/h         | 62   | 886      | 170   | 165   | 555  | 40   | 131  | 57   | 108  | 62   | 85   | 39   |
| Adj No. of Lanes             | 1    | 1        | 0     | 1     | 1    | 0    | 0    | 1    | 0    | 0    | 1    | 0    |
| Peak Hour Factor             | 0.88 | 0.88     | 0.88  | 0.88  | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 |
| Percent Heavy Veh, %         | 2    | 2        | 2     | 2     | 2    | 2    | 2    | 2    | 2    | 4    | 4    | 4    |
| Cap, veh/h                   | 95   | 570      | 109   | 151   | 698  | 50   | 269  | 126  | 178  | 210  | 269  | 106  |
| Arrive On Green              | 0.05 | 0.38     | 0.38  | 0.09  | 0.41 | 0.41 | 0.31 | 0.31 | 0.31 | 0.31 | 0.31 | 0.31 |
| Sat Flow, veh/h              | 1774 | 1520     | 292   | 1774  | 1717 | 124  | 581  | 400  | 564  | 413  | 854  | 336  |
| Grp Volume(v), veh/h         | 62   | 0        | 1056  | 165   | 0    | 595  | 296  | 0    | 0    | 186  | 0    | 0    |
| Grp Sat Flow(s),veh/h/ln     | 1774 | 0        | 1811  | 1774  | 0    | 1841 | 1544 | 0    | 0    | 1602 | 0    | 0    |
| Q Serve(g_s), s              | 2.1  | 0.0      | 22.5  | 5.1   | 0.0  | 17.0 | 4.2  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  |
| Cycle Q Clear(g_c), s        | 2.1  | 0.0      | 22.5  | 5.1   | 0.0  | 17.0 | 9.1  | 0.0  | 0.0  | 4.9  | 0.0  | 0.0  |
| Prop In Lane                 | 1.00 |          | 0.16  | 1.00  |      | 0.07 | 0.44 |      | 0.36 | 0.33 |      | 0.21 |
| Lane Grp Cap(c), veh/h       | 95   | 0        | 679   | 151   | 0    | 748  | 573  | 0    | 0    | 585  | 0    | 0    |
| V/C Ratio(X)                 | 0.65 | 0.00     | 1.55  | 1.09  | 0.00 | 0.80 | 0.52 | 0.00 | 0.00 | 0.32 | 0.00 | 0.00 |
| Avail Cap(c_a), veh/h        | 163  | 0        | 679   | 151   | 0    | 748  | 573  | 0    | 0    | 585  | 0    | 0    |
| HCM Platoon Ratio            | 1.00 | 1.00     | 1.00  | 1.00  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I)           | 1.00 | 0.00     | 1.00  | 1.00  | 0.00 | 1.00 | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| Uniform Delay (d), s/veh     | 27.8 | 0.0      | 18.8  | 27.5  | 0.0  | 15.6 | 17.0 | 0.0  | 0.0  | 15.7 | 0.0  | 0.0  |
| Incr Delay (d2), s/veh       | 7.3  | 0.0      | 256.8 | 100.7 | 0.0  | 6.0  | 3.3  | 0.0  | 0.0  | 1.4  | 0.0  | 0.0  |
| Initial Q Delay(d3),s/veh    | 0.0  | 0.0      | 0.0   | 0.0   | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  |
| %ile BackOfQ(50%),veh/ln     | 1.2  | 0.0      | 59.6  | 6.7   | 0.0  | 9.8  | 4.6  | 0.0  | 0.0  | 2.6  | 0.0  | 0.0  |
| LnGrp Delay(d),s/veh         | 35.1 | 0.0      | 275.6 | 128.2 | 0.0  | 21.6 | 20.3 | 0.0  | 0.0  | 17.2 | 0.0  | 0.0  |
| LnGrp LOS                    | D    |          | F     | F     |      | C    | С    |      |      | В    |      |      |
| Approach Vol, veh/h          |      | 1118     |       |       | 760  |      |      | 296  |      |      | 186  |      |
| Approach Delay, s/veh        |      | 262.2    |       |       | 44.7 |      |      | 20.3 |      |      | 17.2 |      |
| Approach LOS                 |      | F        |       |       | D    |      |      | C    |      |      | В    |      |
|                              |      |          |       |       |      |      |      |      |      |      |      |      |
| Timer                        | 1    | 2        | 3     | 4     | 5    | 6    | 7    | 8    |      |      |      |      |
| Assigned Phs                 |      | 2        | 3     | 4     |      | 6    | 7    | 8    |      |      |      |      |
| Phs Duration (G+Y+Rc), s     |      | 23.4     | 9.6   | 27.0  |      | 23.4 | 7.7  | 28.9 |      |      |      |      |
| Change Period (Y+Rc), s      |      | 4.5      | 4.5   | 4.5   |      | 4.5  | 4.5  | 4.5  |      |      |      |      |
| Max Green Setting (Gmax), s  |      | 18.9     | 5.1   | 22.5  |      | 18.9 | 5.5  | 22.1 |      |      |      |      |
| Max Q Clear Time (g_c+l1), s |      | 11.1     | 7.1   | 24.5  |      | 6.9  | 4.1  | 19.0 |      |      |      |      |
| Green Ext Time (p_c), s      |      | 1.1      | 0.0   | 0.0   |      | 0.8  | 0.0  | 1.2  |      |      |      |      |
| Intersection Summary         |      |          | 440.5 |       |      |      |      |      |      |      |      |      |
| HCM 2010 Ctrl Delay          |      |          | 142.5 |       |      |      |      |      |      |      |      |      |
| HCM 2010 LOS                 |      |          | F     |       |      |      |      |      |      |      |      |      |

|                              |      | <b>→</b> | <b>←</b> | •    | <b>\</b>  | 4    |      |      |  |  |
|------------------------------|------|----------|----------|------|-----------|------|------|------|--|--|
| Movement                     | EBL  | EBT      | WBT      | WBR  | SBL       | SBR  |      |      |  |  |
| Lane Configurations          | ሻ    | <b>1</b> | <b>^</b> | 7    | ኻ         | 7    |      |      |  |  |
| Traffic Volume (veh/h)       | 389  | 727      | 402      | 235  | 258       | 276  |      |      |  |  |
| Future Volume (veh/h)        | 389  | 727      | 402      | 235  | 258       | 276  |      |      |  |  |
| Number                       | 7    | 4        | 8        | 18   | 1         | 16   |      |      |  |  |
| Initial Q (Qb), veh          | 0    | 0        | 0        | 0    | 0         | 0    |      |      |  |  |
| Ped-Bike Adj(A_pbT)          | 1.00 |          |          | 1.00 | 1.00      | 1.00 |      |      |  |  |
| Parking Bus, Adj             | 1.00 | 1.00     | 1.00     | 1.00 | 1.00      | 1.00 |      |      |  |  |
| Adj Sat Flow, veh/h/ln       | 1863 | 1863     | 1863     | 1863 | 1863      | 1863 |      |      |  |  |
| Adj Flow Rate, veh/h         | 405  | 757      | 419      | 245  | 269       | 288  |      |      |  |  |
| Adj No. of Lanes             | 1    | 1        | 1        | 1    | 1         | 1    |      |      |  |  |
| Peak Hour Factor             | 0.96 | 0.96     | 0.96     | 0.96 | 0.96      | 0.96 |      |      |  |  |
| Percent Heavy Veh, %         | 2    | 2        | 2        | 2    | 2         | 2    |      |      |  |  |
| Cap, veh/h                   | 467  | 1115     | 475      | 403  | 428       | 382  |      |      |  |  |
| Arrive On Green              | 0.26 | 0.60     | 0.25     | 0.25 | 0.24      | 0.24 |      |      |  |  |
| Sat Flow, veh/h              | 1774 | 1863     | 1863     | 1583 | 1774      | 1583 |      |      |  |  |
| Grp Volume(v), veh/h         | 405  | 757      | 419      | 245  | 269       | 288  |      |      |  |  |
| Grp Sat Flow(s), veh/h/ln    | 1774 | 1863     | 1863     | 1583 | 1774      | 1583 |      |      |  |  |
| Q Serve(g_s), s              | 12.2 | 15.4     | 12.1     | 7.6  | 7.6       | 9.5  |      |      |  |  |
| Cycle Q Clear(g_c), s        | 12.2 | 15.4     | 12.1     | 7.6  | 7.6       | 9.5  |      |      |  |  |
| Prop In Lane                 | 1.00 | 13.4     | 12.1     | 1.00 | 1.00      | 1.00 |      |      |  |  |
| Lane Grp Cap(c), veh/h       | 467  | 1115     | 475      | 403  | 428       | 382  |      |      |  |  |
| V/C Ratio(X)                 | 0.87 | 0.68     | 0.88     | 0.61 | 0.63      | 0.75 |      |      |  |  |
| Avail Cap(c_a), veh/h        | 586  | 1247     | 482      | 410  | 428       | 382  |      |      |  |  |
| HCM Platoon Ratio            | 1.00 | 1.00     | 1.00     | 1.00 | 1.00      | 1.00 |      |      |  |  |
| Upstream Filter(I)           | 1.00 | 1.00     | 1.00     | 1.00 | 1.00      | 1.00 |      |      |  |  |
|                              | 19.7 | 7.6      | 20.1     | 18.4 | 19.0      | 19.7 |      |      |  |  |
| Uniform Delay (d), s/veh     | 11.0 | 1.3      | 17.1     | 2.5  | 6.9       | 13.0 |      |      |  |  |
| Incr Delay (d2), s/veh       | 0.0  | 0.0      | 0.0      | 0.0  | 0.0       | 0.0  |      |      |  |  |
| Initial Q Delay(d3),s/veh    | 7.4  | 8.2      | 8.4      | 3.6  | 4.6       | 5.5  |      |      |  |  |
| %ile BackOfQ(50%),veh/ln     |      |          | 37.2     |      | 25.9      |      |      |      |  |  |
| LnGrp Delay(d),s/veh         | 30.7 | 8.9      |          | 20.9 | 25.9<br>C | 32.7 |      |      |  |  |
| LnGrp LOS                    | С    | A 4400   | D        | С    |           | С    |      |      |  |  |
| Approach Vol, veh/h          |      | 1162     | 664      |      | 557       |      |      |      |  |  |
| Approach Delay, s/veh        |      | 16.5     | 31.2     |      | 29.4      |      |      |      |  |  |
| Approach LOS                 |      | В        | С        |      | С         |      |      |      |  |  |
| Timer                        | 1    | 2        | 3        | 4    | 5         | 6    | 7    | 8    |  |  |
| Assigned Phs                 |      |          |          | 4    |           | 6    | 7    | 8    |  |  |
| Phs Duration (G+Y+Rc), s     |      |          |          | 38.0 |           | 18.0 | 19.2 | 18.8 |  |  |
| Change Period (Y+Rc), s      |      |          |          | 4.5  |           | 4.5  | 4.5  | 4.5  |  |  |
| Max Green Setting (Gmax), s  |      |          |          | 37.5 |           | 13.5 | 18.5 | 14.5 |  |  |
| Max Q Clear Time (g_c+I1), s |      |          |          | 17.4 |           | 11.5 | 14.2 | 14.1 |  |  |
| Green Ext Time (p_c), s      |      |          |          | 5.5  |           | 0.5  | 0.6  | 0.2  |  |  |
| Intersection Summary         |      |          |          |      |           |      |      |      |  |  |
| HCM 2010 Ctrl Delay          |      |          | 23.6     |      |           |      |      |      |  |  |
| HCM 2010 LOS                 |      |          | С        |      |           |      |      |      |  |  |

|                                | ۶          | <b>→</b> | •      | •     | <b>—</b>  | •          | •       | †     | ~    | <b>\</b> | <del> </del> | -√   |
|--------------------------------|------------|----------|--------|-------|-----------|------------|---------|-------|------|----------|--------------|------|
| Movement                       | EBL        | EBT      | EBR    | WBL   | WBT       | WBR        | NBL     | NBT   | NBR  | SBL      | SBT          | SBR  |
| Lane Configurations            | ሻ          | <b>↑</b> | 7      | 7     | ₽         |            |         | 4     | 7    |          | 4            | 7    |
| Traffic Volume (vph)           | 5          | 869      | 815    | 115   | 900       | 30         | 630     | 20    | 155  | 155      | 160          | 5    |
| Future Volume (vph)            | 5          | 869      | 815    | 115   | 900       | 30         | 630     | 20    | 155  | 155      | 160          | 5    |
| Ideal Flow (vphpl)             | 1900       | 1900     | 1900   | 1900  | 1900      | 1900       | 1900    | 1900  | 1900 | 1900     | 1900         | 1900 |
| Total Lost time (s)            | 4.5        | 4.5      | 4.5    | 4.5   | 4.5       |            |         | 4.5   | 4.5  |          | 4.5          | 4.5  |
| Lane Util. Factor              | 1.00       | 1.00     | 1.00   | 1.00  | 1.00      |            |         | 1.00  | 1.00 |          | 1.00         | 1.00 |
| Frt                            | 1.00       | 1.00     | 0.85   | 1.00  | 1.00      |            |         | 1.00  | 0.85 |          | 1.00         | 0.85 |
| Flt Protected                  | 0.95       | 1.00     | 1.00   | 0.95  | 1.00      |            |         | 0.95  | 1.00 |          | 0.98         | 1.00 |
| Satd. Flow (prot)              | 1687       | 1776     | 1509   | 1583  | 1659      |            |         | 1777  | 1583 |          | 1818         | 1583 |
| Flt Permitted                  | 0.95       | 1.00     | 1.00   | 0.95  | 1.00      |            |         | 0.95  | 1.00 |          | 0.98         | 1.00 |
| Satd. Flow (perm)              | 1687       | 1776     | 1509   | 1583  | 1659      |            |         | 1777  | 1583 |          | 1818         | 1583 |
| Peak-hour factor, PHF          | 0.96       | 0.96     | 0.96   | 0.96  | 0.96      | 0.96       | 0.96    | 0.96  | 0.96 | 0.96     | 0.96         | 0.96 |
| Adj. Flow (vph)                | 5          | 905      | 849    | 120   | 938       | 31         | 656     | 21    | 161  | 161      | 167          | 5    |
| RTOR Reduction (vph)           | 0          | 0        | 378    | 0     | 1         | 0          | 0       | 0     | 84   | 0        | 0            | 4    |
| Lane Group Flow (vph)          | 5          | 905      | 471    | 120   | 968       | 0          | 0       | 677   | 77   | 0        | 328          | 1    |
| Heavy Vehicles (%)             | 7%         | 7%       | 7%     | 14%   | 14%       | 14%        | 2%      | 2%    | 2%   | 2%       | 2%           | 2%   |
| Turn Type                      | Prot       | NA       | Perm   | Prot  | NA        |            | Split   | NA    | Perm | Split    | NA           | Perm |
| Protected Phases               | 7          | 4        |        | 3     | 8         |            | 5       | 5     |      | 6        | 6            |      |
| Permitted Phases               | •          |          | 4      | -     |           |            | •       |       | 5    | -        |              | 6    |
| Actuated Green, G (s)          | 1.0        | 48.1     | 48.1   | 5.0   | 52.1      |            |         | 22.1  | 22.1 |          | 20.4         | 20.4 |
| Effective Green, g (s)         | 1.0        | 48.1     | 48.1   | 5.0   | 52.1      |            |         | 22.1  | 22.1 |          | 20.4         | 20.4 |
| Actuated g/C Ratio             | 0.01       | 0.42     | 0.42   | 0.04  | 0.46      |            |         | 0.19  | 0.19 |          | 0.18         | 0.18 |
| Clearance Time (s)             | 4.5        | 4.5      | 4.5    | 4.5   | 4.5       |            |         | 4.5   | 4.5  |          | 4.5          | 4.5  |
| Vehicle Extension (s)          | 3.0        | 3.0      | 3.0    | 3.0   | 3.0       |            |         | 3.0   | 3.0  |          | 3.0          | 3.0  |
| Lane Grp Cap (vph)             | 14         | 751      | 638    | 69    | 760       |            |         | 345   | 307  |          | 326          | 284  |
| v/s Ratio Prot                 | 0.00       | 0.51     |        | c0.08 | c0.58     |            |         | c0.38 |      |          | c0.18        |      |
| v/s Ratio Perm                 | 0.00       | 0.0.     | 0.31   | 00.00 | 00.00     |            |         | 00.00 | 0.05 |          | 001.0        | 0.00 |
| v/c Ratio                      | 0.36       | 1.21     | 0.74   | 1.74  | 1.27      |            |         | 1.96  | 0.25 |          | 1.01         | 0.00 |
| Uniform Delay, d1              | 56.0       | 32.8     | 27.5   | 54.3  | 30.7      |            |         | 45.7  | 38.7 |          | 46.6         | 38.3 |
| Progression Factor             | 1.00       | 1.00     | 1.00   | 1.00  | 1.00      |            |         | 1.00  | 1.00 |          | 1.00         | 1.00 |
| Incremental Delay, d2          | 14.9       | 104.7    | 7.5    | 385.6 | 133.3     |            |         | 443.4 | 0.4  |          | 51.4         | 0.0  |
| Delay (s)                      | 70.9       | 137.4    | 34.9   | 439.9 | 164.0     |            |         | 489.2 | 39.2 |          | 98.0         | 38.3 |
| Level of Service               | E          | F        | С      | F     | F         |            |         | F     | D    |          | F            | D    |
| Approach Delay (s)             |            | 87.8     |        |       | 194.4     |            |         | 402.7 |      |          | 97.1         | _    |
| Approach LOS                   |            | F        |        |       | F         |            |         | F     |      |          | F            |      |
| Intersection Summary           |            |          |        |       |           |            |         |       |      |          |              |      |
| HCM 2000 Control Delay         |            |          | 183.1  | Н     | CM 2000   | Level of S | Service |       | F    |          |              |      |
| HCM 2000 Volume to Capac       | city ratio |          | 1.41   |       |           |            |         |       |      |          |              |      |
| Actuated Cycle Length (s)      |            |          | 113.6  |       | um of los |            |         |       | 18.0 |          |              |      |
| Intersection Capacity Utilizat | tion       |          | 121.3% | IC    | CU Level  | of Service |         |       | Н    |          |              |      |
| Analysis Period (min)          |            |          | 15     |       |           |            |         |       |      |          |              |      |
| c Critical Lane Group          |            |          |        |       |           |            |         |       |      |          |              |      |

|                              | ۶     | <b>→</b> | •    | ✓     | <b>←</b> | •    | •     | †               | ~    | <b>\</b> | <b></b> | <b>√</b> |
|------------------------------|-------|----------|------|-------|----------|------|-------|-----------------|------|----------|---------|----------|
| Movement                     | EBL   | EBT      | EBR  | WBL   | WBT      | WBR  | NBL   | NBT             | NBR  | SBL      | SBT     | SBR      |
| Lane Configurations          | 16.54 | <b>^</b> | 7    | 7     | <b>^</b> | 7    | ሻሻ    | <del>ተ</del> ቀጭ |      | 16.5%    | ተተተ     | 7        |
| Traffic Volume (veh/h)       | 290   | 505      | 271  | 250   | 397      | 350  | 340   | 683             | 152  | 590      | 1110    | 306      |
| Future Volume (veh/h)        | 290   | 505      | 271  | 250   | 397      | 350  | 340   | 683             | 152  | 590      | 1110    | 306      |
| Number                       | 7     | 4        | 14   | 3     | 8        | 18   | 5     | 2               | 12   | 1        | 6       | 16       |
| Initial Q (Qb), veh          | 0     | 0        | 0    | 0     | 0        | 0    | 0     | 0               | 0    | 0        | 0       | 0        |
| Ped-Bike Adj(A_pbT)          | 1.00  |          | 0.99 | 1.00  |          | 1.00 | 1.00  |                 | 1.00 | 1.00     |         | 1.00     |
| Parking Bus, Adj             | 1.00  | 1.00     | 1.00 | 1.00  | 1.00     | 1.00 | 1.00  | 1.00            | 1.00 | 1.00     | 1.00    | 1.00     |
| Adj Sat Flow, veh/h/ln       | 1863  | 1863     | 1863 | 1863  | 1863     | 1863 | 1863  | 1863            | 1900 | 1863     | 1863    | 1863     |
| Adj Flow Rate, veh/h         | 302   | 526      | 282  | 260   | 414      | 365  | 354   | 711             | 158  | 615      | 1156    | 319      |
| Adj No. of Lanes             | 2     | 2        | 1    | 1     | 2        | 1    | 2     | 3               | 0    | 2        | 3       | 1        |
| Peak Hour Factor             | 0.96  | 0.96     | 0.96 | 0.96  | 0.96     | 0.96 | 0.96  | 0.96            | 0.96 | 0.96     | 0.96    | 0.96     |
| Percent Heavy Veh, %         | 2     | 2        | 2    | 2     | 2        | 2    | 2     | 2               | 2    | 2        | 2       | 2        |
| Cap, veh/h                   | 374   | 875      | 535  | 218   | 927      | 413  | 324   | 1148            | 252  | 324      | 1398    | 606      |
| Arrive On Green              | 0.11  | 0.25     | 0.25 | 0.12  | 0.26     | 0.26 | 0.09  | 0.28            | 0.28 | 0.09     | 0.28    | 0.28     |
| Sat Flow, veh/h              | 3442  | 3539     | 1562 | 1774  | 3539     | 1576 | 3442  | 4174            | 917  | 3442     | 5085    | 1580     |
| Grp Volume(v), veh/h         | 302   | 526      | 282  | 260   | 414      | 365  | 354   | 576             | 293  | 615      | 1156    | 319      |
| Grp Sat Flow(s),veh/h/ln     | 1721  | 1770     | 1562 | 1774  | 1770     | 1576 | 1721  | 1695            | 1701 | 1721     | 1695    | 1580     |
| Q Serve(g_s), s              | 5.9   | 9.1      | 10.0 | 8.5   | 6.8      | 15.4 | 6.5   | 10.3            | 10.4 | 6.5      | 14.7    | 10.8     |
| Cycle Q Clear(g_c), s        | 5.9   | 9.1      | 10.0 | 8.5   | 6.8      | 15.4 | 6.5   | 10.3            | 10.4 | 6.5      | 14.7    | 10.8     |
| Prop In Lane                 | 1.00  |          | 1.00 | 1.00  |          | 1.00 | 1.00  |                 | 0.54 | 1.00     |         | 1.00     |
| Lane Grp Cap(c), veh/h       | 374   | 875      | 535  | 218   | 927      | 413  | 324   | 932             | 468  | 324      | 1398    | 606      |
| V/C Ratio(X)                 | 0.81  | 0.60     | 0.53 | 1.19  | 0.45     | 0.88 | 1.09  | 0.62            | 0.63 | 1.90     | 0.83    | 0.53     |
| Avail Cap(c_a), veh/h        | 374   | 922      | 556  | 218   | 973      | 433  | 324   | 932             | 468  | 324      | 1398    | 606      |
| HCM Platoon Ratio            | 1.00  | 1.00     | 1.00 | 1.00  | 1.00     | 1.00 | 1.00  | 1.00            | 1.00 | 1.00     | 1.00    | 1.00     |
| Upstream Filter(I)           | 1.00  | 1.00     | 1.00 | 1.00  | 1.00     | 1.00 | 1.00  | 1.00            | 1.00 | 1.00     | 1.00    | 1.00     |
| Uniform Delay (d), s/veh     | 30.1  | 23.0     | 18.3 | 30.3  | 21.3     | 24.5 | 31.3  | 21.9            | 21.9 | 31.3     | 23.5    | 16.4     |
| Incr Delay (d2), s/veh       | 12.4  | 1.0      | 0.8  | 122.2 | 0.3      | 18.5 | 77.4  | 3.1             | 6.2  | 416.1    | 5.7     | 3.2      |
| Initial Q Delay(d3),s/veh    | 0.0   | 0.0      | 0.0  | 0.0   | 0.0      | 0.0  | 0.0   | 0.0             | 0.0  | 0.0      | 0.0     | 0.0      |
| %ile BackOfQ(50%),veh/ln     | 3.5   | 4.6      | 4.4  | 11.5  | 3.3      | 8.8  | 6.5   | 5.2             | 5.7  | 21.8     | 7.6     | 5.2      |
| LnGrp Delay(d),s/veh         | 42.5  | 24.0     | 19.1 | 152.5 | 21.7     | 43.0 | 108.6 | 24.9            | 28.2 | 447.4    | 29.2    | 19.7     |
| LnGrp LOS                    | D     | С        | В    | F     | С        | D    | F     | С               | С    | F        | С       | В        |
| Approach Vol, veh/h          |       | 1110     |      |       | 1039     |      |       | 1223            |      |          | 2090    |          |
| Approach Delay, s/veh        |       | 27.8     |      |       | 61.9     |      |       | 49.9            |      |          | 150.8   |          |
| Approach LOS                 |       | С        |      |       | E        |      |       | D               |      |          | F       |          |
| Timer                        | 1     | 2        | 3    | 4     | 5        | 6    | 7     | 8               |      |          |         |          |
| Assigned Phs                 | 1     | 2        | 3    | 4     | 5        | 6    | 7     | 8               |      |          |         |          |
| Phs Duration (G+Y+Rc), s     | 11.0  | 23.5     | 13.0 | 21.6  | 11.0     | 23.5 | 12.0  | 22.6            |      |          |         |          |
| Change Period (Y+Rc), s      | 4.5   | 4.5      | 4.5  | 4.5   | 4.5      | 4.5  | 4.5   | 4.5             |      |          |         |          |
| Max Green Setting (Gmax), s  | 6.5   | 19.0     | 8.5  | 18.0  | 6.5      | 19.0 | 7.5   | 19.0            |      |          |         |          |
| Max Q Clear Time (g_c+l1), s | 8.5   | 12.4     | 10.5 | 12.0  | 8.5      | 16.7 | 7.9   | 17.4            |      |          |         |          |
| Green Ext Time (p_c), s      | 0.0   | 3.0      | 0.0  | 2.3   | 0.0      | 1.7  | 0.0   | 0.7             |      |          |         |          |
| Intersection Summary         |       |          |      |       |          |      |       |                 |      |          |         |          |
| HCM 2010 Ctrl Delay          |       |          | 86.3 |       |          |      |       |                 |      |          |         |          |
| HCM 2010 LOS                 |       |          | F    |       |          |      |       |                 |      |          |         |          |

| Movement   EBL   EBT   EBR   WBL   WBT   WBR   NBL   NBT   NBR   SBL   SBT   SBR   |
|--|
| Lane Configurations  |
| Traffic Volume (veh/h)         25         200         89         295         260         388         65         187         307         299         125         20           Future Volume (veh/h)         25         200         89         295         260         388         65         187         307         299         125         20           Number         7         4         14         3         8         18         5         2         12         1         6         16           Initial Q (Qb), veh         0  |
| Future Volume (veh/h)         25         200         89         295         260         388         65         187         307         299         125         20           Number         7         4         14         3         8         18         5         2         12         1         6         16           Initial Q (Qb), veh         0 <th< td=""></th<>   |
| Number   7   |
| Initial Q (Qb), veh   0  |
| Ped-Bike Adji(A_pbT)         1.00         0.95         1.00         0.99         1.00         0.99         1.00         0.99         1.00         0.99         1.00         0.99         1.00         0.99         1.00         0.99         1.00         0.99         1.00< |
| Parking Bus, Adj         1.00      |
| Adj Sat Flow, veh/h/ln         1863         1863         1900         1863         1863         1900         1863         186 |
| Adj Flow Rate, veh/h         29         233         103         343         302         451         76         217         357         348         145         23           Adj No. of Lanes         1         1         0         1         1         0         1         0         0.86         0.86         0.86         0.86         0.86         0.86         0.86         0.86         0.86         0.86         0.86         0.86         0.86         0.86         0.86         0.86         0.86 <t< td=""></t<>  |
| Adj No. of Lanes         1         1         0         1         1         0         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         0         0.86 <th< td=""></th<>                           |
| Peak Hour Factor         0.86         0.29         0.22         2         2         2               |
| Percent Heavy Veh, %         2   |
| Cap, veh/h         55         281         124         275         240         359         100         508         429         131         455         72           Arrive On Green         0.03         0.23         0.23         0.15         0.36         0.36         0.06         0.27         0.27         0.07         0.29         0.29           Sat Flow, veh/h         1774         1203         532         1774         673         1005         1774         1863         1572         1774         1568         249           Grp Volume(v), veh/h         29         0         336         343         0         753         76         217         357         348         0         168           Grp Sat Flow(s), veh/h/ln         1774         0         1735         1774         0         1677         1774         1863         1572         1774         0         1817           Q Serve(g_s), s         1.1         0.0         12.5         10.5         0.0         24.2         2.9         6.5         14.5         5.0         0.0         4.9           Cycle Q Clear(g_c), s         1.1         0.0         12.5         10.5         0.0         24.2         2.9   |
| Arrive On Green         0.03         0.23         0.23         0.15         0.36         0.36         0.06         0.27         0.27         0.07         0.29         0.29           Sat Flow, veh/h         1774         1203         532         1774         673         1005         1774         1863         1572         1774         1568         249           Grp Volume(v), veh/h         29         0         336         343         0         753         76         217         357         348         0         168           Grp Sat Flow(s), veh/h/ln         1774         0         1735         1774         0         1677         1774         1863         1572         1774         0         1817           Q Serve(g_s), s         1.1         0.0         12.5         10.5         0.0         24.2         2.9         6.5         14.5         5.0         0.0         4.9           Cycle Q Clear(g_c), s         1.1         0.0         12.5         10.5         0.0         24.2         2.9         6.5         14.5         5.0         0.0         4.9           Prop In Lane         1.00         0.31         1.00         0.60         1.00         1.00  |
| Sat Flow, veh/h         1774         1203         532         1774         673         1005         1774         1863         1572         1774         1568         249           Grp Volume(v), veh/h         29         0         336         343         0         753         76         217         357         348         0         168           Grp Sat Flow(s),veh/h/ln         1774         0         1735         1774         0         1677         1774         1863         1572         1774         0         1817           Q Serve(g_s), s         1.1         0.0         12.5         10.5         0.0         24.2         2.9         6.5         14.5         5.0         0.0         4.9           Cycle Q Clear(g_c), s         1.1         0.0         12.5         10.5         0.0         24.2         2.9         6.5         14.5         5.0         0.0         4.9           Prop In Lane         1.00         0.31         1.00         0.60         1.00         1.00         1.00         1.00         1.00         1.00         0.14           Lane Grp Cap(c), veh/h         55         0         405         275         0         599         100 <t< td=""></t<>  |
| Grp Volume(v), veh/h         29         0         336         343         0         753         76         217         357         348         0         168           Grp Sat Flow(s),veh/h/ln         1774         0         1677         1774         1863         1572         1774         0         1817           Q Serve(g_s), s         1.1         0.0         12.5         10.5         0.0         24.2         2.9         6.5         14.5         5.0         0.0         4.9           Cycle Q Clear(g_c), s         1.1         0.0         12.5         10.5         0.0         24.2         2.9         6.5         14.5         5.0         0.0         4.9           Prop In Lane         1.00         0.31         1.00         0.60         1.00         1.00         1.00         0.14           Lane Grp Cap(c), veh/h         55         0         405         275         0         599         100         508         429         131         0         527           V/C Ratio(X)         0.53         0.00         0.83         1.25         0.00         1.26         0.76         0.43         0.83         2.66         0.00         0.32           Avail   |
| Grp Sat Flow(s),veh/h/ln         1774         0         1774         0         1677         1774         1863         1572         1774         0         1817           Q Serve(g_s), s         1.1         0.0         12.5         10.5         0.0         24.2         2.9         6.5         14.5         5.0         0.0         4.9           Cycle Q Clear(g_c), s         1.1         0.0         12.5         10.5         0.0         24.2         2.9         6.5         14.5         5.0         0.0         4.9           Prop In Lane         1.00         0.31         1.00         0.60         1.00         1.00         1.00         0.14           Lane Grp Cap(c), veh/h         55         0         405         275         0         599         100         508         429         131         0         527           V/C Ratio(X)         0.53         0.00         0.83         1.25         0.00         1.26         0.76         0.43         0.83         2.66         0.00         0.32           Avail Cap(c_a), veh/h         131         0         460         275         0         599         131         508         429         131         0         5   |
| Q Serve(g_s), s         1.1         0.0         12.5         10.5         0.0         24.2         2.9         6.5         14.5         5.0         0.0         4.9           Cycle Q Clear(g_c), s         1.1         0.0         12.5         10.5         0.0         24.2         2.9         6.5         14.5         5.0         0.0         4.9           Prop In Lane         1.00         0.31         1.00         0.60         1.00         1.00         1.00         0.14           Lane Grp Cap(c), veh/h         55         0         405         275         0         599         100         508         429         131         0         527           V/C Ratio(X)         0.53         0.00         0.83         1.25         0.00         1.26         0.76         0.43         0.83         2.66         0.00         0.32           Avail Cap(c_a), veh/h         131         0         460         275         0         599         131         508         429         131         0         527           HCM Platoon Ratio         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00  |
| Cycle Q Clear(g_c), s         1.1         0.0         12.5         10.5         0.0         24.2         2.9         6.5         14.5         5.0         0.0         4.9           Prop In Lane         1.00         0.31         1.00         0.60         1.00         1.00         1.00         0.14           Lane Grp Cap(c), veh/h         55         0         405         275         0         599         100         508         429         131         0         527           V/C Ratio(X)         0.53         0.00         0.83         1.25         0.00         1.26         0.76         0.43         0.83         2.66         0.00         0.32           Avail Cap(c_a), veh/h         131         0         460         275         0         599         131         508         429         131         0         527           HCM Platoon Ratio         1.00  |
| Prop In Lane         1.00         0.31         1.00         0.60         1.00         1.00         1.00         0.14           Lane Grp Cap(c), veh/h         55         0         405         275         0         599         100         508         429         131         0         527           V/C Ratio(X)         0.53         0.00         0.83         1.25         0.00         1.26         0.76         0.43         0.83         2.66         0.00         0.32           Avail Cap(c_a), veh/h         131         0         460         275         0         599         131         508         429         131         0         527           HCM Platoon Ratio         1.00 </td                              |
| Lane Grp Cap(c), veh/h         55         0         405         275         0         599         100         508         429         131         0         527           V/C Ratio(X)         0.53         0.00         0.83         1.25         0.00         1.26         0.76         0.43         0.83         2.66         0.00         0.32           Avail Cap(c_a), veh/h         131         0         460         275         0         599         131         508         429         131         0         527           HCM Platoon Ratio         1.00                                |
| V/C Ratio(X)         0.53         0.00         0.83         1.25         0.00         1.26         0.76         0.43         0.83         2.66         0.00         0.32           Avail Cap(c_a), veh/h         131         0         460         275         0         599         131         508         429         131         0         527           HCM Platoon Ratio         1.00                    |
| Avail Cap(c_a), veh/h       131       0       460       275       0       599       131       508       429       131       0       527         HCM Platoon Ratio       1.00  |
| HCM Platoon Ratio         1.00     |
| Upstream Filter(I)       1.00       0.00       1.00       0.00       1.00       1.00       1.00       1.00       1.00       1.00       0.00       1.00         Uniform Delay (d), s/veh       32.4       0.0       24.7       28.7       0.0       21.8       31.6       20.3       23.2       31.4       0.0       18.8         Incr Delay (d2), s/veh       7.6       0.0       10.9       138.7       0.0       128.7       17.3       2.6       17.1       769.2       0.0       1.6   |
| Uniform Delay (d), s/veh 32.4 0.0 24.7 28.7 0.0 21.8 31.6 20.3 23.2 31.4 0.0 18.8 Incr Delay (d2), s/veh 7.6 0.0 10.9 138.7 0.0 128.7 17.3 2.6 17.1 769.2 0.0 1.6  |
| Incr Delay (d2), s/veh 7.6 0.0 10.9 138.7 0.0 128.7 17.3 2.6 17.1 769.2 0.0 1.6  |
|  |
| Initial O Delay(d3) s/yeh  |
|  |
| %ile BackOfQ(50%),veh/ln 0.6 0.0 7.2 15.6 0.0 32.4 1.9 3.7 8.3 30.3 0.0 2.7  |
| LnGrp Delay(d),s/veh 40.0 0.0 35.6 167.4 0.0 150.5 48.8 22.9 40.3 800.7 0.0 20.4   |
| <u>LnGrp LOS</u> D D F F D C D F C   |
| Approach Vol, veh/h 365 1096 650 516   |
| Approach Delay, s/veh 35.9 155.8 35.5 546.6  |
| Approach LOS D F D F   |
| Timer 1 2 3 4 5 6 7 8  |
| Assigned Phs 1 2 3 4 5 6 7 8   |
| Phs Duration (G+Y+Rc), s 9.5 23.0 15.0 20.3 8.3 24.2 6.6 28.7  |
| Change Period (Y+Rc), s 4.5 4.5 4.5 4.5 4.5 4.5 4.5  |
| Max Green Setting (Gmax), s 5.0 18.5 10.5 18.0 5.0 18.5 5.0 23.5   |
| Max Q Clear Time (g_c+I1), s 7.0 16.5 12.5 14.5 4.9 6.9 3.1 26.2   |
| Green Ext Time (p_c), s 0.0 0.6 0.0 0.7 0.0 0.6 0.0 0.0  |
| Intersection Summary   |
| HCM 2010 Ctrl Delay 186.1  |
| HCM 2010 LOS F   |

## Appendix H

Level of Service
Calculations

Cumulative Plus Project
Conditions

## 1: Ridgemark Dr/Fairview Rd & Airline Highway (SR 25)

9.293

Yes

388

7.047

0.642

27.4

D

4.3

8.727

Yes

412

6.481

0.277

14.8

В

1.1

9.521

Yes

379

7.279

0.451

19.9

С

2.3

9.007

Yes

400

6.765

0.417

18.1

C

2

8.288

Yes

433

6.046

0.231

13.5

В

0.9

9.413

Yes

380

7.17

0.029

12.4

В

0.1

8.9

Yes

407

6.657

0.774

36.8

Ε

6.6

8.182

Yes

439

5.939

0.285

14.2

В

1.2

9.915

Yes

362

7.68

0.24

15.8

C

0.9

9.405

Yes

381

7.169

0.121

13.4

В

0.4

8.69

Yes

414

6.454

0.401

17.2

C

1.9

| Intersection               |      |          |       |       |          |       |       |       |       |       |          |       |
|----------------------------|------|----------|-------|-------|----------|-------|-------|-------|-------|-------|----------|-------|
| Intersection Delay, s/veh  | 22.3 |          |       |       |          |       |       |       |       |       |          |       |
| Intersection LOS           | С    |          |       |       |          |       |       |       |       |       |          |       |
|                            |      |          |       |       |          |       |       |       |       |       |          |       |
| Movement                   | EBL  | EBT      | EBR   | WBL   | WBT      | WBR   | NBL   | NBT   | NBR   | SBL   | SBT      | SBR   |
| Lane Configurations        | ሻ    | <b>†</b> | 7     | ሻ     | <b>†</b> | 7     | ሻ     | f)    |       | *     | <b>†</b> | 7     |
| Traffic Vol, veh/h         | 157  | 154      | 92    | 10    | 290      | 115   | 229   | 95    | 10    | 80    | 42       | 153   |
| Future Vol, veh/h          | 157  | 154      | 92    | 10    | 290      | 115   | 229   | 95    | 10    | 80    | 42       | 153   |
| Peak Hour Factor           | 0.92 | 0.92     | 0.92  | 0.92  | 0.92     | 0.92  | 0.92  | 0.92  | 0.92  | 0.92  | 0.92     | 0.92  |
| Heavy Vehicles, %          | 7    | 7        | 7     | 5     | 5        | 5     | 2     | 2     | 2     | 6     | 6        | 6     |
| Mvmt Flow                  | 171  | 167      | 100   | 11    | 315      | 125   | 249   | 103   | 11    | 87    | 46       | 166   |
| Number of Lanes            | 1    | 1        | 1     | 1     | 1        | 1     | 1     | 1     | 0     | 1     | 1        | 1     |
| Approach                   | EB   |          |       | WB    |          |       | NB    |       |       | SB    |          |       |
| Opposing Approach          | WB   |          |       | EB    |          |       | SB    |       |       | NB    |          |       |
| Opposing Lanes             | 3    |          |       | 3     |          |       | 3     |       |       | 2     |          |       |
| Conflicting Approach Left  | SB   |          |       | NB    |          |       | EB    |       |       | WB    |          |       |
| Conflicting Lanes Left     | 3    |          |       | 2     |          |       | 3     |       |       | 3     |          |       |
| Conflicting Approach Right | NB   |          |       | SB    |          |       | WB    |       |       | EB    |          |       |
| Conflicting Lanes Right    | 2    |          |       | 3     |          |       | 3     |       |       | 3     |          |       |
| HCM Control Delay          | 17.8 |          |       | 29.9  |          |       | 23.4  |       |       | 16.2  |          |       |
| HCM LOS                    | С    |          |       | D     |          |       | С     |       |       | С     |          |       |
|                            |      |          |       |       |          |       |       |       |       |       |          |       |
| Lane                       |      | NBLn1    | NBLn2 | EBLn1 | EBLn2    | EBLn3 | WBLn1 | WBLn2 | WBLn3 | SBLn1 | SBLn2    | SBLn3 |
| Vol Left, %                |      | 100%     | 0%    | 100%  | 0%       | 0%    | 100%  | 0%    | 0%    | 100%  | 0%       | 0%    |
| Vol Thru, %                |      | 0%       | 90%   | 0%    | 100%     | 0%    | 0%    | 100%  | 0%    | 0%    | 100%     | 0%    |
| Vol Right, %               |      | 0%       | 10%   | 0%    | 0%       | 100%  | 0%    | 0%    | 100%  | 0%    | 0%       | 100%  |
| Sign Control               |      | Stop     | Stop  | Stop  | Stop     | Stop  | Stop  | Stop  | Stop  | Stop  | Stop     | Stop  |
| Traffic Vol by Lane        |      | 229      | 105   | 157   | 154      | 92    | 10    | 290   | 115   | 80    | 42       | 153   |
| LT Vol                     |      | 229      | 0     | 157   | 0        | 0     | 10    | 0     | 0     | 80    | 0        | 0     |
| Through Vol                |      | 0        | 95    | 0     | 154      | 0     | 0     | 290   | 0     | 0     | 42       | 0     |
| RT Vol                     |      | 0        | 10    | 0     | 0        | 92    | 0     | 0     | 115   | 0     | 0        | 153   |
| Lane Flow Rate             |      | 249      | 114   | 171   | 167      | 100   | 11    | 315   | 125   | 87    | 46       | 166   |
| Geometry Grp               |      | 8        | 8     | 8     | 8        | 8     | 8     | 8     | 8     | 8     | 8        | 8     |
| Degree of Util (X)         |      | 0.643    | 0.277 | 0.451 | 0.419    | 0.23  | 0.028 | 0.779 | 0.284 | 0.239 | 0.119    | 0.401 |
| D ( 11 1 (/11)             |      | 0.000    | 0 707 | 0.504 | 0.00=    | 0.000 | 0.440 |       | 0.400 | 0.045 | 0.40=    | 0.00  |

Departure Headway (Hd)

Convergence, Y/N

HCM Lane V/C Ratio

**HCM Control Delay** 

**HCM Lane LOS** 

HCM 95th-tile Q

Service Time

Cap

| Intersection                                |             |              |           |           |                 |          |             |               |            |         |               |           |           |
|---|-------------|--------------|-----------|-----------|-----------------|----------|-------------|---------------|------------|---------|---------------|-----------|-----------|
| Int Delay, s/veh                            | 7.7         |              |           |           |                 |          |             |               |            |         |               |           |           |
| Movement                                    | EBL         | EBT          | EBR       | WBL       | WBT             | WBR      | NBL         | NBT           | NBR        | SBL     | SBT           | SBR       |           |
| Lane Configurations                         | CDL         | <u></u>      | EDK.      |           |                 | WDK      | NDL         |               | INDIC      |         |               | JDK<br>7  |           |
| Traffic Vol, veh/h                          | <b>1</b> 50 | <b>T</b> 289 | 20        | ሻ<br>48   | <b>↑</b><br>594 | 30       | <b>1</b> 50 | <b>↑</b><br>5 | <b>6</b> 9 | ሻ<br>45 | <b>↑</b><br>5 | 145       |           |
| Future Vol, veh/h                           | 50          | 289          | 20        | 48        | 594             | 30       | 50          | 5             | 69         | 45      | 5             | 145       |           |
| Conflicting Peds, #/hr                      | 0           | 209          | 1         | 0         | 0               | 0        | 0           | 0             | 09         | 0       | 0             | 0         |           |
| Sign Control                                | Free        | Free         | Free      | Free      | Free            | Free     | Stop        | Stop          | Stop       | Stop    | Stop          | Stop      |           |
| RT Channelized                              | -           | -            | None      | -         | -               | None     | - Otop      | - Olop        | None       | - Olop  | - Otop        | None      |           |
| Storage Length                              | 320         | _            | 505       | 360       | _               | 195      | 60          | _             | 0          | 100     | <u>-</u>      | 100       |           |
| Veh in Median Storage                       |             | 0            | -         | -         | 0               | -        | -           | 0             | -          | -       | 0             | -         |           |
| Grade, %                                    | -, "        | 0            | _         | _         | 0               | _        | _           | 0             | _          | _       | 0             | _         |           |
| Peak Hour Factor                            | 95          | 95           | 95        | 95        | 95              | 95       | 95          | 95            | 95         | 95      | 95            | 95        |           |
| Heavy Vehicles, %                           | 8           | 8            | 8         | 4         | 4               | 4        | 2           | 2             | 2          | 3       | 3             | 3         |           |
| Mvmt Flow                                   | 53          | 304          | 21        | 51        | 625             | 32       | 53          | 5             | 73         | 47      | 5             | 153       |           |
|   |             |              |           |           |                 |          |             |               |            |         |               |           |           |
| Major/Minor I                               | Major1      |              |           | Major2    |                 | ı        | Minor1      |               |            | Minor2  |               |           |           |
| Conflicting Flow All                        | 657         | 0            | 0         | 326       | 0               | 0        | 1233        | 1170          | 305        | 1187    | 1159          | 625       |           |
| Stage 1                                     | 007         | U            | U         | 320       | -               | U        | 411         | 411           | 305        | 727     | 727           |           |           |
| Stage 2                                     | _           | -            | -         | -         | _               | -        | 822         | 759           | -          | 460     | 432           | -         |           |
| Critical Hdwy                               | 4.18        | _            | -         | 4.14      | -               | -        | 7.12        | 6.52          | 6.22       | 7.13    | 6.53          | 6.23      |           |
| Critical Hdwy Stg 1                         | 4.10        | _            | _         | 4.14      | _               | _        | 6.12        | 5.52          | 0.22       | 6.13    | 5.53          | 0.23      |           |
| Critical Hdwy Stg 2                         | _           | _            | _         | _         | _               |          | 6.12        | 5.52          | _          | 6.13    | 5.53          | _         |           |
| Follow-up Hdwy                              | 2.272       | _            | _         | 2.236     | _               | _        | 3.518       | 4.018         | 3.318      | 3.527   |               | 3.327     |           |
| Pot Cap-1 Maneuver                          | 903         | _            | _         | 1222      | _               | _        | 154         | 193           | 735        | 165     | 195           | 483       |           |
| Stage 1                                     | -           | <u>-</u>     | _         | -         | _               | _        | 618         | 595           | -          | 414     | 428           | -         |           |
| Stage 2                                     | -           | _            | _         | _         | _               | _        | 368         | 415           | _          | 579     | 581           | _         |           |
| Platoon blocked, %                          |             | _            | -         |           | -               | -        |             |               |            |         |               |           |           |
| Mov Cap-1 Maneuver                          | 903         | -            | -         | 1221      | -               | -        | 95          | 174           | 734        | 134     | 176           | 483       |           |
| Mov Cap-2 Maneuver                          | -           | -            | -         | -         | -               | -        | 95          | 174           | -          | 134     | 176           | -         |           |
| Stage 1                                     | -           | -            | -         | -         | -               | -        | 581         | 559           | -          | 390     | 410           | -         |           |
| Stage 2                                     | -           | -            | -         | -         | -               | -        | 238         | 398           | -          | 486     | 546           | -         |           |
|   |             |              |           |           |                 |          |             |               |            |         |               |           |           |
| Approach                                    | EB          |              |           | WB        |                 |          | NB          |               |            | SB      |               |           |           |
| HCM Control Delay, s                        | 1.3         |              |           | 0.6       |                 |          | 40          |               |            | 23.1    |               |           |           |
| HCM LOS                                     |             |              |           |           |                 |          | E           |               |            | С       |               |           |           |
|   |             |              |           |           |                 |          |             |               |            |         |               |           |           |
| Minor Lane/Major Mvm                        | n#          | NBLn11       | UDI 221   | VIDI 22   | EBL             | EBT      | EPD         | WBL           | WBT        | WPD     | CDI 51        | SBLn2     | 201.52    |
|   | IL I        |              |           |           |                 | EDI      | EBR         |               | VVDI       |         |               |           |           |
| Capacity (veh/h)                            |             | 95           | 174       | 734       | 903             | -        | -           | 1221          | -          | -       |               | 176       | 483       |
| HCM Lane V/C Ratio<br>HCM Control Delay (s) |             | 0.554        |           |           | 0.058<br>9.2    | -        | -           |               | -          |         | 0.353         |           | 0.316     |
| HCM Lane LOS                                |             | 82.3<br>F    | 26.3<br>D | 10.4<br>B | 9.2<br>A        | -        | -           | 8.1<br>A      | -<br>-     | -       | 45.9<br>E     | 26.1<br>D | 15.9<br>C |
| HCM 95th %tile Q(veh)                       | )           | 2.5          | 0.1       | 0.3       | 0.2             | -        | -           | 0.1           | -          |         | 1.4           | 0.1       | 1.3       |
| HOW JOHN JOHNE W(VEI)                       | 1           | 2.0          | 0.1       | 0.0       | 0.2             | <u>-</u> | _           | 0.1           |            | -       | 1.4           | 0.1       | 1.0       |

| 3.0                    |   |  |   |   |  |
|------------------------|---|--|---|---|--|
|                        |   |  |   |   |  |
|                        | WBR   |  | NBR   | SBL   | SBT  |
|                        |   |  |   |   | 4  |
|                        |   |  |   |   | 195  |
|                        |   |  |   |   | 195  |
| 0                      | 0   | 0  | 1   | 1   | 0  |
| Stop                   | Stop  | Free   | Free  | Free  | Free   |
| -                      | None  | -  | None  | -   | None   |
| 0                      | -   | -  | -   | -   | -  |
| e, # 0                 | -   | 0  | _   | -   | 0  |
| 0                      | -   | 0  | -   | -   | 0  |
| 86                     | 86  | 86   | 86  | 86  | 86   |
|                        |   |  |   |   | 7  |
|                        |   |  |   |   | 227  |
|                        | 100   | 000  |   | 10  |  |
|                        |   |  |   |   |  |
| Minor1                 | N   | /lajor1  | N   | Major2  |  |
| 705                    | 388   | 0  | 0   | 409   | 0  |
| 388                    | -   | -  | -   | -   | -  |
| 317                    | -   | -  | -   | -   | -  |
| 6.42                   | 6.22  | -  | -   | 4.17  | -  |
| 5.42                   | -   | -  | -   | -   | -  |
|                        | -   | _  | -   | -   | -  |
|                        | 3.318   | _  | -   | 2.263   | _  |
|                        |   | _  | _   |   | -  |
|                        |   | _  | _   | -   | _  |
|                        |   | _  | _   | _   | _  |
| 700                    |   | _  | _   |   | _  |
| 38/                    | 650   |  |   | 1122  | _  |
|                        |   |  |   |   | _  |
|                        |   | _  | -   | <u>-</u>  | -  |
| (1:14                  | _   | _  |   | _   | _  |
|                        |   |  |   |   |  |
| 738                    | -   | -  | -   | -   | -  |
|                        | -   | -  | -   | -   | -  |
|                        | -   | -<br>NB  | -   | SB  | -  |
| 738<br>WB              | -   |  | -   | SB  |  |
| 738                    | -   | NB   | _   |   |  |
| 738<br>WB<br>14.9      | -   | NB   |   | SB  |  |
| 738<br>WB<br>14.9<br>B |   | NB<br>0  |   | SB<br>1.4   |  |
| 738<br>WB<br>14.9      | NBT   | NB<br>0  | WBLn1   | SB<br>1.4<br>SBL  | SBT  |
| 738<br>WB<br>14.9<br>B |   | NB<br>0<br>NBRW  | WBLn1<br>572  | SB 1.4 SBL 1122   |  |
| 738<br>WB<br>14.9<br>B |   | NB<br>0<br>NBRW  | WBLn1<br>572<br>0.366   | SB 1.4  SBL 1122 0.04   | SBT<br>-   |
| 738<br>WB<br>14.9<br>B |   | NB<br>0<br>NBRW  | WBLn1<br>572  | SB 1.4 SBL 1122   |  |
| 738<br>WB<br>14.9<br>B |   | NB<br>0<br>NBRV  | WBLn1<br>572<br>0.366   | SB 1.4  SBL 1122 0.04   | SBT<br>-   |
|                        | Stop - 0 - 0 - 8, # 0 - 0 - 86 - 2 - 44  Minor1 - 705 - 388 - 317 - 6.42 - 5.42 - 5.42 - 5.42 - 3.518 - 403 - 686 - 738 - 384 - 384 - 384 | WBL WBR  38 142 38 142 0 0 Stop Stop - None 0 8, # 0 86 86 2 2 44 165  Minor1 N  705 388 388 317 6.42 6.22 5.42 5.42 5.42 3.518 3.318 403 660 686 738  384 659 | WBL WBR NBT  38 142 315 38 142 315 0 0 0 0 Stop Stop Free - None - 0 9, # 0 - 0 86 86 86 2 2 7 44 165 366  Minor1 Major1  705 388 0 388 317 6.42 6.22 - 5.42 5.42 5.42 5.42 3.518 3.318 - 403 660 - 686 738 384 659 - 384 384 659 - 384 | WBL         WBR         NBT         NBR           38         142         315         36           0         0         0         1           Stop         Stop         Free         Free           -         None         -         None           0         -         -         -           0         -         0         -           86         86         86         86           2         2         7         7           44         165         366         42           Minor1         Major1         I           705         388         0         0           388         -         -         -           6.42         6.22         -         -           5.42         -         -         -           5.42         -         -         -           3.518         3.318         -         -           403         660         -         -           738         -         -         -           384         659         -         -           384         -         - | WBL         WBR         NBT         NBR         SBL           Y         Image: Control of the control of th |

|                              | ۶    | <b>→</b> | •     | •    | <b>←</b> | •     | 1     | <b>†</b> | <b>/</b> | <b>/</b> | <b>+</b> | 4    |
|------------------------------|------|----------|-------|------|----------|-------|-------|----------|----------|----------|----------|------|
| Movement                     | EBL  | EBT      | EBR   | WBL  | WBT      | WBR   | NBL   | NBT      | NBR      | SBL      | SBT      | SBR  |
| Lane Configurations          | 7    | î»       |       | 7    | f)       |       | 7     | <b>†</b> | 7        | 7        | <b>†</b> | 7    |
| Traffic Volume (veh/h)       | 259  | 212      | 142   | 32   | 454      | 315   | 314   | 433      | 42       | 130      | 185      | 219  |
| Future Volume (veh/h)        | 259  | 212      | 142   | 32   | 454      | 315   | 314   | 433      | 42       | 130      | 185      | 219  |
| Number                       | 7    | 4        | 14    | 3    | 8        | 18    | 5     | 2        | 12       | 1        | 6        | 16   |
| Initial Q (Qb), veh          | 0    | 0        | 0     | 0    | 0        | 0     | 0     | 0        | 0        | 0        | 0        | 0    |
| Ped-Bike Adj(A_pbT)          | 1.00 |          | 1.00  | 1.00 |          | 1.00  | 1.00  |          | 1.00     | 1.00     |          | 1.00 |
| Parking Bus, Adj             | 1.00 | 1.00     | 1.00  | 1.00 | 1.00     | 1.00  | 1.00  | 1.00     | 1.00     | 1.00     | 1.00     | 1.00 |
| Adj Sat Flow, veh/h/ln       | 1776 | 1776     | 1900  | 1863 | 1863     | 1900  | 1863  | 1863     | 1863     | 1827     | 1827     | 1827 |
| Adj Flow Rate, veh/h         | 276  | 226      | 151   | 34   | 483      | 335   | 334   | 461      | 45       | 138      | 197      | 233  |
| Adj No. of Lanes             | 1    | 1        | 0     | 1    | 1        | 0     | 1     | 1        | 1        | 1        | 1        | 1    |
| Peak Hour Factor             | 0.94 | 0.94     | 0.94  | 0.94 | 0.94     | 0.94  | 0.94  | 0.94     | 0.94     | 0.94     | 0.94     | 0.94 |
| Percent Heavy Veh, %         | 7    | 7        | 7     | 2    | 2        | 2     | 2     | 2        | 2        | 4        | 4        | 4    |
| Cap, veh/h                   | 338  | 199      | 133   | 432  | 250      | 173   | 254   | 513      | 436      | 141      | 390      | 331  |
| Arrive On Green              | 0.20 | 0.20     | 0.20  | 0.24 | 0.24     | 0.24  | 0.14  | 0.28     | 0.28     | 0.08     | 0.21     | 0.21 |
| Sat Flow, veh/h              | 1691 | 993      | 664   | 1774 | 1026     | 711   | 1774  | 1863     | 1583     | 1740     | 1827     | 1553 |
| Grp Volume(v), veh/h         | 276  | 0        | 377   | 34   | 0        | 818   | 334   | 461      | 45       | 138      | 197      | 233  |
| Grp Sat Flow(s),veh/h/ln     | 1691 | 0        | 1657  | 1774 | 0        | 1737  | 1774  | 1863     | 1583     | 1740     | 1827     | 1553 |
| Q Serve(g_s), s              | 14.0 | 0.0      | 18.0  | 1.3  | 0.0      | 21.9  | 12.9  | 21.4     | 1.9      | 7.1      | 8.6      | 12.5 |
| Cycle Q Clear(g_c), s        | 14.0 | 0.0      | 18.0  | 1.3  | 0.0      | 21.9  | 12.9  | 21.4     | 1.9      | 7.1      | 8.6      | 12.5 |
| Prop In Lane                 | 1.00 |          | 0.40  | 1.00 |          | 0.41  | 1.00  |          | 1.00     | 1.00     |          | 1.00 |
| Lane Grp Cap(c), veh/h       | 338  | 0        | 331   | 432  | 0        | 423   | 254   | 513      | 436      | 141      | 390      | 331  |
| V/C Ratio(X)                 | 0.82 | 0.00     | 1.14  | 0.08 | 0.00     | 1.94  | 1.31  | 0.90     | 0.10     | 0.98     | 0.51     | 0.70 |
| Avail Cap(c_a), veh/h        | 338  | 0        | 331   | 432  | 0        | 423   | 254   | 513      | 436      | 141      | 390      | 331  |
| HCM Platoon Ratio            | 1.00 | 1.00     | 1.00  | 1.00 | 1.00     | 1.00  | 1.00  | 1.00     | 1.00     | 1.00     | 1.00     | 1.00 |
| Upstream Filter(I)           | 1.00 | 0.00     | 1.00  | 1.00 | 0.00     | 1.00  | 1.00  | 1.00     | 1.00     | 1.00     | 1.00     | 1.00 |
| Uniform Delay (d), s/veh     | 34.4 | 0.0      | 36.0  | 26.3 | 0.0      | 34.1  | 38.5  | 31.4     | 24.3     | 41.3     | 31.2     | 32.8 |
| Incr Delay (d2), s/veh       | 14.3 | 0.0      | 92.2  | 0.1  | 0.0      | 429.4 | 166.2 | 21.2     | 0.5      | 68.8     | 4.6      | 11.8 |
| Initial Q Delay(d3),s/veh    | 0.0  | 0.0      | 0.0   | 0.0  | 0.0      | 0.0   | 0.0   | 0.0      | 0.0      | 0.0      | 0.0      | 0.0  |
| %ile BackOfQ(50%),veh/ln     | 7.9  | 0.0      | 16.7  | 0.7  | 0.0      | 60.9  | 18.0  | 14.0     | 0.9      | 6.1      | 4.8      | 6.5  |
| LnGrp Delay(d),s/veh         | 48.7 | 0.0      | 128.2 | 26.3 | 0.0      | 463.5 | 204.8 | 52.5     | 24.8     | 110.1    | 35.8     | 44.6 |
| LnGrp LOS                    | D    |          | F     | С    |          | F     | F     | D        | С        | F        | D        | D    |
| Approach Vol, veh/h          |      | 653      |       |      | 852      |       |       | 840      |          |          | 568      |      |
| Approach Delay, s/veh        |      | 94.6     |       |      | 446.0    |       |       | 111.6    |          |          | 57.5     |      |
| Approach LOS                 |      | F        |       |      | F        |       |       | F        |          |          | E        |      |
| Timer                        | 1    | 2        | 3     | 4    | 5        | 6     | 7     | 8        |          |          |          |      |
| Assigned Phs                 | 1    | 2        |       | 4    | 5        | 6     |       | 8        |          |          |          |      |
| Phs Duration (G+Y+Rc), s     | 11.8 | 29.3     |       | 22.5 | 17.4     | 23.7  |       | 26.4     |          |          |          |      |
| Change Period (Y+Rc), s      | 4.5  | 4.5      |       | 4.5  | 4.5      | 4.5   |       | 4.5      |          |          |          |      |
| Max Green Setting (Gmax), s  | 7.3  | 24.8     |       | 18.0 | 12.9     | 19.2  |       | 21.9     |          |          |          |      |
| Max Q Clear Time (g_c+l1), s | 9.1  | 23.4     |       | 20.0 | 14.9     | 14.5  |       | 23.9     |          |          |          |      |
| Green Ext Time (p_c), s      | 0.0  | 0.4      |       | 0.0  | 0.0      | 0.9   |       | 0.0      |          |          |          |      |
| Intersection Summary         |      |          |       |      |          |       |       |          |          |          |          |      |
| HCM 2010 Ctrl Delay          |      |          | 195.0 |      |          |       |       |          |          |          |          |      |
| HCM 2010 LOS                 |      |          | F     |      |          |       |       |          |          |          |          |      |

|                              | ۶    | <b>→</b> | •    | •    | <b>←</b> | •     | •    | †    | ~    | <b>/</b> | <b>+</b> | ✓    |
|------------------------------|------|----------|------|------|----------|-------|------|------|------|----------|----------|------|
| Movement                     | EBL  | EBT      | EBR  | WBL  | WBT      | WBR   | NBL  | NBT  | NBR  | SBL      | SBT      | SBR  |
| Lane Configurations          | 7    | <b>₽</b> |      | ሻ    | ₽        |       |      | 4    |      |          | 4        |      |
| Traffic Volume (veh/h)       | 35   | 406      | 131  | 105  | 857      | 25    | 215  | 76   | 169  | 38       | 28       | 52   |
| Future Volume (veh/h)        | 35   | 406      | 131  | 105  | 857      | 25    | 215  | 76   | 169  | 38       | 28       | 52   |
| Number                       | 7    | 4        | 14   | 3    | 8        | 18    | 5    | 2    | 12   | 1        | 6        | 16   |
| Initial Q (Qb), veh          | 0    | 0        | 0    | 0    | 0        | 0     | 0    | 0    | 0    | 0        | 0        | 0    |
| Ped-Bike Adj(A_pbT)          | 1.00 |          | 1.00 | 1.00 |          | 1.00  | 1.00 |      | 1.00 | 1.00     |          | 1.00 |
| Parking Bus, Adj             | 1.00 | 1.00     | 1.00 | 1.00 | 1.00     | 1.00  | 1.00 | 1.00 | 1.00 | 1.00     | 1.00     | 1.00 |
| Adj Sat Flow, veh/h/ln       | 1827 | 1827     | 1900 | 1845 | 1845     | 1900  | 1900 | 1810 | 1900 | 1900     | 1776     | 1900 |
| Adj Flow Rate, veh/h         | 39   | 451      | 146  | 117  | 952      | 28    | 239  | 84   | 188  | 42       | 31       | 58   |
| Adj No. of Lanes             | 1    | 1        | 0    | 1    | 1        | 0     | 0    | 1    | 0    | 0        | 1        | 0    |
| Peak Hour Factor             | 0.90 | 0.90     | 0.90 | 0.90 | 0.90     | 0.90  | 0.90 | 0.90 | 0.90 | 0.90     | 0.90     | 0.90 |
| Percent Heavy Veh, %         | 4    | 4        | 4    | 3    | 3        | 3     | 5    | 5    | 5    | 7        | 7        | 7    |
| Cap, veh/h                   | 69   | 523      | 169  | 149  | 786      | 23    | 293  | 78   | 167  | 179      | 137      | 190  |
| Arrive On Green              | 0.04 | 0.40     | 0.40 | 0.08 | 0.44     | 0.44  | 0.30 | 0.30 | 0.30 | 0.30     | 0.30     | 0.30 |
| Sat Flow, veh/h              | 1740 | 1323     | 428  | 1757 | 1783     | 52    | 686  | 259  | 550  | 339      | 451      | 627  |
| Grp Volume(v), veh/h         | 39   | 0        | 597  | 117  | 0        | 980   | 511  | 0    | 0    | 131      | 0        | 0    |
| Grp Sat Flow(s),veh/h/ln     | 1740 | 0        | 1751 | 1757 | 0        | 1835  | 1495 | 0    | 0    | 1416     | 0        | 0    |
| Q Serve(g_s), s              | 1.4  | 0.0      | 19.5 | 4.1  | 0.0      | 27.5  | 15.1 | 0.0  | 0.0  | 0.0      | 0.0      | 0.0  |
| Cycle Q Clear(g_c), s        | 1.4  | 0.0      | 19.5 | 4.1  | 0.0      | 27.5  | 18.9 | 0.0  | 0.0  | 3.8      | 0.0      | 0.0  |
| Prop In Lane                 | 1.00 |          | 0.24 | 1.00 |          | 0.03  | 0.47 |      | 0.37 | 0.32     |          | 0.44 |
| Lane Grp Cap(c), veh/h       | 69   | 0        | 693  | 149  | 0        | 809   | 538  | 0    | 0    | 506      | 0        | 0    |
| V/C Ratio(X)                 | 0.57 | 0.00     | 0.86 | 0.79 | 0.00     | 1.21  | 0.95 | 0.00 | 0.00 | 0.26     | 0.00     | 0.00 |
| Avail Cap(c_a), veh/h        | 142  | 0        | 722  | 194  | 0        | 809   | 538  | 0    | 0    | 506      | 0        | 0    |
| HCM Platoon Ratio            | 1.00 | 1.00     | 1.00 | 1.00 | 1.00     | 1.00  | 1.00 | 1.00 | 1.00 | 1.00     | 1.00     | 1.00 |
| Upstream Filter(I)           | 1.00 | 0.00     | 1.00 | 1.00 | 0.00     | 1.00  | 1.00 | 0.00 | 0.00 | 1.00     | 0.00     | 0.00 |
| Uniform Delay (d), s/veh     | 29.4 | 0.0      | 17.3 | 28.0 | 0.0      | 17.4  | 22.5 | 0.0  | 0.0  | 16.5     | 0.0      | 0.0  |
| Incr Delay (d2), s/veh       | 7.2  | 0.0      | 10.1 | 14.4 | 0.0      | 106.2 | 28.2 | 0.0  | 0.0  | 1.2      | 0.0      | 0.0  |
| Initial Q Delay(d3),s/veh    | 0.0  | 0.0      | 0.0  | 0.0  | 0.0      | 0.0   | 0.0  | 0.0  | 0.0  | 0.0      | 0.0      | 0.0  |
| %ile BackOfQ(50%),veh/ln     | 8.0  | 0.0      | 11.2 | 2.6  | 0.0      | 37.6  | 12.9 | 0.0  | 0.0  | 1.9      | 0.0      | 0.0  |
| LnGrp Delay(d),s/veh         | 36.7 | 0.0      | 27.4 | 42.4 | 0.0      | 123.6 | 50.7 | 0.0  | 0.0  | 17.7     | 0.0      | 0.0  |
| LnGrp LOS                    | D    |          | С    | D    |          | F     | D    |      |      | В        |          |      |
| Approach Vol, veh/h          |      | 636      |      |      | 1097     |       |      | 511  |      |          | 131      |      |
| Approach Delay, s/veh        |      | 28.0     |      |      | 115.0    |       |      | 50.7 |      |          | 17.7     |      |
| Approach LOS                 |      | С        |      |      | F        |       |      | D    |      |          | В        |      |
| Timer                        | 1    | 2        | 3    | 4    | 5        | 6     | 7    | 8    |      |          |          |      |
| Assigned Phs                 |      | 2        | 3    | 4    |          | 6     | 7    | 8    |      |          |          |      |
| Phs Duration (G+Y+Rc), s     |      | 23.4     | 9.8  | 29.2 |          | 23.4  | 7.0  | 32.0 |      |          |          |      |
| Change Period (Y+Rc), s      |      | 4.5      | 4.5  | 4.5  |          | 4.5   | 4.5  | 4.5  |      |          |          |      |
| Max Green Setting (Gmax), s  |      | 18.9     | 6.9  | 25.7 |          | 18.9  | 5.1  | 27.5 |      |          |          |      |
| Max Q Clear Time (g_c+l1), s |      | 20.9     | 6.1  | 21.5 |          | 5.8   | 3.4  | 29.5 |      |          |          |      |
| Green Ext Time (p_c), s      |      | 0.0      | 0.0  | 1.5  |          | 0.5   | 0.0  | 0.0  |      |          |          |      |
| Intersection Summary         |      |          |      |      |          |       |      |      |      |          |          |      |
| HCM 2010 Ctrl Delay          |      |          | 72.5 |      |          |       |      |      |      |          |          |      |
| HCM 2010 LOS                 |      |          | Е    |      |          |       |      |      |      |          |          |      |

|                              |      | <b>→</b> | <b>←</b> | •    | <b>\</b> | 4    |         |     |  |  |
|------------------------------|------|----------|----------|------|----------|------|---------|-----|--|--|
| Movement                     | EBL  | EBT      | WBT      | WBR  | SBL      | SBR  |         |     |  |  |
| Lane Configurations          | *    | <b>†</b> | <b>†</b> | 7    | *        | 7    |         |     |  |  |
| Traffic Volume (veh/h)       | 199  | 286      | 656      | 468  | 286      | 335  |         |     |  |  |
| Future Volume (veh/h)        | 199  | 286      | 656      | 468  | 286      | 335  |         |     |  |  |
| Number                       | 7    | 4        | 8        | 18   | 1        | 16   |         |     |  |  |
| Initial Q (Qb), veh          | 0    | 0        | 0        | 0    | 0        | 0    |         |     |  |  |
| Ped-Bike Adj(A_pbT)          | 1.00 |          |          | 1.00 | 1.00     | 1.00 |         |     |  |  |
| Parking Bus, Adj             | 1.00 | 1.00     | 1.00     | 1.00 | 1.00     | 1.00 |         |     |  |  |
| Adj Sat Flow, veh/h/ln       | 1810 | 1810     | 1863     | 1863 | 1863     | 1863 |         |     |  |  |
| Adj Flow Rate, veh/h         | 221  | 318      | 729      | 520  | 318      | 372  |         |     |  |  |
| Adj No. of Lanes             | 1    | 1        | 1        | 1    | 1        | 1    |         |     |  |  |
| Peak Hour Factor             | 0.90 | 0.90     | 0.90     | 0.90 | 0.90     | 0.90 |         |     |  |  |
| Percent Heavy Veh, %         | 5    | 5        | 2        | 2    | 2        | 2    |         |     |  |  |
| Cap, veh/h                   | 270  | 1102     | 696      | 592  | 416      | 372  |         |     |  |  |
| Arrive On Green              | 0.16 | 0.61     | 0.37     | 0.37 | 0.23     | 0.23 |         |     |  |  |
| Sat Flow, veh/h              | 1723 | 1810     | 1863     | 1583 | 1774     | 1583 |         |     |  |  |
| Grp Volume(v), veh/h         | 221  | 318      | 729      | 520  | 318      | 372  |         |     |  |  |
| Grp Sat Flow(s), veh/h/ln    | 1723 | 1810     | 1863     | 1583 | 1774     | 1583 |         |     |  |  |
| Q Serve(g_s), s              | 7.1  | 4.8      | 21.5     | 17.6 | 9.6      | 13.5 |         |     |  |  |
| Cycle Q Clear(g_c), s        | 7.1  | 4.8      | 21.5     | 17.6 | 9.6      | 13.5 |         |     |  |  |
| Prop In Lane                 | 1.00 | 1.0      | 21.0     | 1.00 | 1.00     | 1.00 |         |     |  |  |
| Lane Grp Cap(c), veh/h       | 270  | 1102     | 696      | 592  | 416      | 372  |         |     |  |  |
| V/C Ratio(X)                 | 0.82 | 0.29     | 1.05     | 0.88 | 0.76     | 1.00 |         |     |  |  |
| Avail Cap(c_a), veh/h        | 345  | 1180     | 696      | 592  | 416      | 372  |         |     |  |  |
| HCM Platoon Ratio            | 1.00 | 1.00     | 1.00     | 1.00 | 1.00     | 1.00 |         |     |  |  |
| Upstream Filter(I)           | 1.00 | 1.00     | 1.00     | 1.00 | 1.00     | 1.00 |         |     |  |  |
| Uniform Delay (d), s/veh     | 23.5 | 5.3      | 18.0     | 16.8 | 20.5     | 22.0 |         |     |  |  |
| Incr Delay (d2), s/veh       | 11.5 | 0.1      | 47.0     | 14.1 | 12.5     | 46.9 |         |     |  |  |
| Initial Q Delay(d3),s/veh    | 0.0  | 0.0      | 0.0      | 0.0  | 0.0      | 0.0  |         |     |  |  |
| %ile BackOfQ(50%),veh/ln     | 4.2  | 2.4      | 19.9     | 10.0 | 6.1      | 15.3 |         |     |  |  |
| LnGrp Delay(d),s/veh         | 35.0 | 5.5      | 65.0     | 30.9 | 33.0     | 68.9 |         |     |  |  |
| LnGrp LOS                    | C    | A        | F        | C    | C        | F    |         |     |  |  |
| Approach Vol, veh/h          |      | 539      | 1249     |      | 690      | •    |         |     |  |  |
| Approach Delay, s/veh        |      | 17.6     | 50.8     |      | 52.4     |      |         |     |  |  |
| Approach LOS                 |      | В        | D        |      | D        |      |         |     |  |  |
| Timer                        | 1    | 2        | 3        | 4    | 5        | 6    | 7       | 8   |  |  |
| Assigned Phs                 |      |          |          | 4    |          | 6    | 7       | 8   |  |  |
| Phs Duration (G+Y+Rc), s     |      |          |          | 39.5 |          | 18.0 | 13.5 26 | 6.0 |  |  |
| Change Period (Y+Rc), s      |      |          |          | 4.5  |          | 4.5  |         | l.5 |  |  |
| Max Green Setting (Gmax), s  |      |          |          | 37.5 |          | 13.5 |         | .5  |  |  |
| Max Q Clear Time (g_c+l1), s |      |          |          | 6.8  |          | 15.5 |         | 3.5 |  |  |
| Green Ext Time (p_c), s      |      |          |          | 2.0  |          | 0.0  |         | 0.0 |  |  |
| Intersection Summary         |      |          |          |      |          |      |         |     |  |  |
| HCM 2010 Ctrl Delay          |      |          | 44.0     |      |          |      |         |     |  |  |
| HCM 2010 LOS                 |      |          | D        |      |          |      |         |     |  |  |

|                                | ۶         | <b>→</b> | •      | •     | +           | •          | 1       | <b>†</b> | <b>/</b> | <b>/</b> | <b>↓</b> | ✓    |
|--------------------------------|-----------|----------|--------|-------|-------------|------------|---------|----------|----------|----------|----------|------|
| Movement                       | EBL       | EBT      | EBR    | WBL   | WBT         | WBR        | NBL     | NBT      | NBR      | SBL      | SBT      | SBR  |
| Lane Configurations            | , J       | <b>†</b> | 7      | J.    | f)          |            |         | ર્ન      | 7        |          | ર્ન      | 7    |
| Traffic Volume (vph)           | 15        | 650      | 496    | 75    | 1050        | 30         | 889     | 30       | 75       | 55       | 25       | 10   |
| Future Volume (vph)            | 15        | 650      | 496    | 75    | 1050        | 30         | 889     | 30       | 75       | 55       | 25       | 10   |
| Ideal Flow (vphpl)             | 1900      | 1900     | 1900   | 1900  | 1900        | 1900       | 1900    | 1900     | 1900     | 1900     | 1900     | 1900 |
| Total Lost time (s)            | 4.5       | 4.5      | 4.5    | 4.5   | 4.5         |            |         | 4.5      | 4.5      |          | 4.5      | 4.5  |
| Lane Util. Factor              | 1.00      | 1.00     | 1.00   | 1.00  | 1.00        |            |         | 1.00     | 1.00     |          | 1.00     | 1.00 |
| Frt                            | 1.00      | 1.00     | 0.85   | 1.00  | 1.00        |            |         | 1.00     | 0.85     |          | 1.00     | 0.85 |
| FIt Protected                  | 0.95      | 1.00     | 1.00   | 0.95  | 1.00        |            |         | 0.95     | 1.00     |          | 0.97     | 1.00 |
| Satd. Flow (prot)              | 1612      | 1696     | 1442   | 1543  | 1617        |            |         | 1777     | 1583     |          | 1749     | 1538 |
| Flt Permitted                  | 0.95      | 1.00     | 1.00   | 0.95  | 1.00        |            |         | 0.95     | 1.00     |          | 0.97     | 1.00 |
| Satd. Flow (perm)              | 1612      | 1696     | 1442   | 1543  | 1617        |            |         | 1777     | 1583     |          | 1749     | 1538 |
| Peak-hour factor, PHF          | 0.96      | 0.96     | 0.96   | 0.96  | 0.96        | 0.96       | 0.96    | 0.96     | 0.96     | 0.96     | 0.96     | 0.96 |
| Adj. Flow (vph)                | 16        | 677      | 517    | 78    | 1094        | 31         | 926     | 31       | 78       | 57       | 26       | 10   |
| RTOR Reduction (vph)           | 0         | 0        | 289    | 0     | 1           | 0          | 0       | 0        | 54       | 0        | 0        | 9    |
| Lane Group Flow (vph)          | 16        | 677      | 228    | 78    | 1124        | 0          | 0       | 957      | 24       | 0        | 83       | 1    |
| Heavy Vehicles (%)             | 12%       | 12%      | 12%    | 17%   | 17%         | 17%        | 2%      | 2%       | 2%       | 5%       | 5%       | 5%   |
| Turn Type                      | Prot      | NA       | Perm   | Prot  | NA          |            | Split   | NA       | Perm     | Split    | NA       | Perm |
| Protected Phases               | 7         | 4        |        | 3     | 8           |            | 5       | 5        |          | 6        | 6        |      |
| Permitted Phases               |           |          | 4      |       |             |            |         |          | 5        |          |          | 6    |
| Actuated Green, G (s)          | 2.0       | 54.2     | 54.2   | 5.0   | 57.2        |            |         | 38.5     | 38.5     |          | 7.0      | 7.0  |
| Effective Green, g (s)         | 2.0       | 54.2     | 54.2   | 5.0   | 57.2        |            |         | 38.5     | 38.5     |          | 7.0      | 7.0  |
| Actuated g/C Ratio             | 0.02      | 0.44     | 0.44   | 0.04  | 0.47        |            |         | 0.31     | 0.31     |          | 0.06     | 0.06 |
| Clearance Time (s)             | 4.5       | 4.5      | 4.5    | 4.5   | 4.5         |            |         | 4.5      | 4.5      |          | 4.5      | 4.5  |
| Vehicle Extension (s)          | 3.0       | 3.0      | 3.0    | 3.0   | 3.0         |            |         | 3.0      | 3.0      |          | 3.0      | 3.0  |
| Lane Grp Cap (vph)             | 26        | 749      | 636    | 62    | 753         |            |         | 557      | 496      |          | 99       | 87   |
| v/s Ratio Prot                 | 0.01      | 0.40     |        | c0.05 | c0.70       |            |         | c0.54    |          |          | c0.05    |      |
| v/s Ratio Perm                 |           |          | 0.16   | 4.00  | 4 40        |            |         |          | 0.02     |          |          | 0.00 |
| v/c Ratio                      | 0.62      | 0.90     | 0.36   | 1.26  | 1.49        |            |         | 1.72     | 0.05     |          | 0.84     | 0.01 |
| Uniform Delay, d1              | 60.0      | 31.8     | 22.7   | 58.9  | 32.8        |            |         | 42.1     | 29.3     |          | 57.3     | 54.6 |
| Progression Factor             | 1.00      | 1.00     | 1.00   | 1.00  | 1.00        |            |         | 1.00     | 1.00     |          | 1.00     | 1.00 |
| Incremental Delay, d2          | 36.3      | 16.4     | 1.6    | 198.8 | 229.0       |            |         | 330.7    | 0.0      |          | 43.1     | 0.0  |
| Delay (s)                      | 96.2      | 48.2     | 24.3   | 257.7 | 261.8       |            |         | 372.8    | 29.4     |          | 100.4    | 54.6 |
| Level of Service               | F         | D        | С      | F     | F           |            |         | F        | С        |          | F        | D    |
| Approach Delay (s)             |           | 38.6     |        |       | 261.5       |            |         | 346.9    |          |          | 95.5     |      |
| Approach LOS                   |           | D        |        |       | F           |            |         | F        |          |          | F        |      |
| Intersection Summary           |           |          |        |       |             |            |         |          |          |          |          |      |
| HCM 2000 Control Delay         |           |          | 206.0  | Н     | CM 2000     | Level of S | Service |          | F        |          |          |      |
| HCM 2000 Volume to Capac       | ity ratio |          | 1.55   |       |             |            |         |          | 4.5.5    |          |          |      |
| Actuated Cycle Length (s)      |           |          | 122.7  |       | um of lost  | . ,        |         |          | 18.0     |          |          |      |
| Intersection Capacity Utilizat | ion       |          | 127.3% | IC    | CU Level of | of Service |         |          | Н        |          |          |      |
| Analysis Period (min)          |           |          | 15     |       |             |            |         |          |          |          |          |      |
| c Critical Lane Group          |           |          |        |       |             |            |         |          |          |          |          |      |

|                                     | ۶    | <b>→</b> | •         | •     | <b>←</b> | •    | 1     | <b>†</b> | ~    | <b>/</b> | <b></b> | 4        |
|-------------------------------------|------|----------|-----------|-------|----------|------|-------|----------|------|----------|---------|----------|
| Movement                            | EBL  | EBT      | EBR       | WBL   | WBT      | WBR  | NBL   | NBT      | NBR  | SBL      | SBT     | SBR      |
| Lane Configurations                 | 44   | <b>^</b> | 7         | 7     | <b>^</b> | 7    | ሻሻ    | ተተኈ      |      | 1/1      | ተተተ     | 7        |
| Traffic Volume (veh/h)              | 270  | 291      | 169       | 175   | 545      | 398  | 288   | 855      | 87   | 290      | 589     | 269      |
| Future Volume (veh/h)               | 270  | 291      | 169       | 175   | 545      | 398  | 288   | 855      | 87   | 290      | 589     | 269      |
| Number                              | 7    | 4        | 14        | 3     | 8        | 18   | 5     | 2        | 12   | 1        | 6       | 16       |
| Initial Q (Qb), veh                 | 0    | 0        | 0         | 0     | 0        | 0    | 0     | 0        | 0    | 0        | 0       | 0        |
| Ped-Bike Adj(A_pbT)                 | 1.00 |          | 0.98      | 1.00  |          | 0.97 | 1.00  |          | 1.00 | 1.00     |         | 1.00     |
| Parking Bus, Adj                    | 1.00 | 1.00     | 1.00      | 1.00  | 1.00     | 1.00 | 1.00  | 1.00     | 1.00 | 1.00     | 1.00    | 1.00     |
| Adj Sat Flow, veh/h/ln              | 1863 | 1863     | 1863      | 1863  | 1863     | 1863 | 1863  | 1863     | 1900 | 1845     | 1845    | 1845     |
| Adj Flow Rate, veh/h                | 290  | 313      | 182       | 188   | 586      | 428  | 310   | 919      | 94   | 312      | 633     | 289      |
| Adj No. of Lanes                    | 2    | 2        | 1         | 1     | 2        | 1    | 2     | 3        | 0    | 2        | 3       | 1        |
| Peak Hour Factor                    | 0.93 | 0.93     | 0.93      | 0.93  | 0.93     | 0.93 | 0.93  | 0.93     | 0.93 | 0.93     | 0.93    | 0.93     |
| Percent Heavy Veh, %                | 2    | 2        | 2         | 2     | 2        | 2    | 2     | 2        | 2    | 3        | 3       | 3        |
| Cap, veh/h                          | 286  | 980      | 554       | 150   | 986      | 428  | 265   | 1335     | 136  | 262      | 1433    | 575      |
| Arrive On Green                     | 0.08 | 0.28     | 0.28      | 0.08  | 0.28     | 0.28 | 0.08  | 0.28     | 0.28 | 0.08     | 0.28    | 0.28     |
| Sat Flow, veh/h                     | 3442 | 3539     | 1559      | 1774  | 3539     | 1536 | 3442  | 4689     | 478  | 3408     | 5036    | 1561     |
| Grp Volume(v), veh/h                | 290  | 313      | 182       | 188   | 586      | 428  | 310   | 664      | 349  | 312      | 633     | 289      |
| Grp Sat Flow(s),veh/h/ln            | 1721 | 1770     | 1559      | 1774  | 1770     | 1536 | 1721  | 1695     | 1777 | 1704     | 1679    | 1561     |
| Q Serve(g_s), s                     | 5.4  | 4.6      | 5.5       | 5.5   | 9.3      | 18.1 | 5.0   | 11.3     | 11.4 | 5.0      | 6.7     | 9.3      |
| Cycle Q Clear(g_c), s               | 5.4  | 4.6      | 5.5       | 5.5   | 9.3      | 18.1 | 5.0   | 11.3     | 11.4 | 5.0      | 6.7     | 9.3      |
| Prop In Lane                        | 1.00 |          | 1.00      | 1.00  |          | 1.00 | 1.00  |          | 0.27 | 1.00     |         | 1.00     |
| Lane Grp Cap(c), veh/h              | 286  | 980      | 554       | 150   | 986      | 428  | 265   | 965      | 506  | 262      | 1433    | 575      |
| V/C Ratio(X)                        | 1.01 | 0.32     | 0.33      | 1.25  | 0.59     | 1.00 | 1.17  | 0.69     | 0.69 | 1.19     | 0.44    | 0.50     |
| Avail Cap(c_a), veh/h               | 286  | 980      | 554       | 150   | 986      | 428  | 265   | 965      | 506  | 262      | 1433    | 575      |
| HCM Platoon Ratio                   | 1.00 | 1.00     | 1.00      | 1.00  | 1.00     | 1.00 | 1.00  | 1.00     | 1.00 | 1.00     | 1.00    | 1.00     |
| Upstream Filter(I)                  | 1.00 | 1.00     | 1.00      | 1.00  | 1.00     | 1.00 | 1.00  | 1.00     | 1.00 | 1.00     | 1.00    | 1.00     |
| Uniform Delay (d), s/veh            | 29.8 | 18.6     | 15.4      | 29.7  | 20.3     | 23.4 | 30.0  | 20.7     | 20.7 | 30.0     | 19.0    | 15.9     |
| Incr Delay (d2), s/veh              | 56.9 | 0.2      | 0.3       | 156.7 | 1.0      | 43.8 | 109.6 | 4.0      | 7.5  | 117.0    | 1.0     | 3.1      |
| Initial Q Delay(d3),s/veh           | 0.1  | 0.0      | 0.0       | 0.0   | 0.0      | 0.0  | 0.0   | 0.0      | 0.0  | 0.0      | 0.0     | 0.0      |
| %ile BackOfQ(50%),veh/ln            | 4.8  | 2.2      | 2.4       | 9.2   | 4.7      | 12.8 | 6.4   | 5.8      | 6.6  | 6.6      | 3.2     | 4.5      |
| LnGrp Delay(d),s/veh                | 86.8 | 18.8     | 15.7      | 186.5 | 21.2     | 67.2 | 139.6 | 24.7     | 28.2 | 147.0    | 20.0    | 19.1     |
| LnGrp LOS                           | F    | В        | B         | F     | С        | F    | F     | С        | С    | F        | С       | <u>B</u> |
| Approach Vol, veh/h                 |      | 785      |           |       | 1202     |      |       | 1323     |      |          | 1234    |          |
| Approach Delay, s/veh               |      | 43.2     |           |       | 63.5     |      |       | 52.5     |      |          | 51.9    |          |
| Approach LOS                        |      | D        |           |       | E        |      |       | D        |      |          | D       |          |
| Timer                               | 1    | 2        | 3         | 4     | 5        | 6    | 7     | 8        |      |          |         |          |
| Assigned Phs                        | 1    | 2        | 3         | 4     | 5        | 6    | 7     | 8        |      |          |         |          |
| Phs Duration (G+Y+Rc), s            | 9.5  | 23.0     | 10.0      | 22.5  | 9.5      | 23.0 | 9.9   | 22.6     |      |          |         |          |
| Change Period (Y+Rc), s             | 4.5  | 4.5      | 4.5       | 4.5   | 4.5      | 4.5  | 4.5   | 4.5      |      |          |         |          |
| Max Green Setting (Gmax), s         | 5.0  | 18.5     | 5.5       | 18.0  | 5.0      | 18.5 | 5.4   | 18.1     |      |          |         |          |
| Max Q Clear Time (g_c+I1), s        | 7.0  | 13.4     | 7.5       | 7.5   | 7.0      | 11.3 | 7.4   | 20.1     |      |          |         |          |
| Green Ext Time (p_c), s             | 0.0  | 2.8      | 0.0       | 2.0   | 0.0      | 3.1  | 0.0   | 0.0      |      |          |         |          |
| Intersection Summary                |      |          |           |       |          |      |       |          |      |          |         |          |
|                                     |      |          |           |       |          |      |       |          |      |          |         |          |
| HCM 2010 Ctrl Delay<br>HCM 2010 LOS |      |          | 53.6<br>D |       |          |      |       |          |      |          |         |          |

|                              | ۶    | <b>→</b> | •     | •     | <b>←</b> | •     | 1    | <b>†</b> | ~    | <b>/</b> | <b></b> | 4    |
|------------------------------|------|----------|-------|-------|----------|-------|------|----------|------|----------|---------|------|
| Movement                     | EBL  | EBT      | EBR   | WBL   | WBT      | WBR   | NBL  | NBT      | NBR  | SBL      | SBT     | SBR  |
| Lane Configurations          | ň    | f)       |       | 7     | ĵ.       |       | Ţ    | <b>†</b> | 7    | Ţ        | ĵ.      |      |
| Traffic Volume (veh/h)       | 45   | 170      | 47    | 260   | 175      | 367   | 78   | 239      | 200  | 185      | 124     | 25   |
| Future Volume (veh/h)        | 45   | 170      | 47    | 260   | 175      | 367   | 78   | 239      | 200  | 185      | 124     | 25   |
| Number                       | 7    | 4        | 14    | 3     | 8        | 18    | 5    | 2        | 12   | 1        | 6       | 16   |
| Initial Q (Qb), veh          | 0    | 0        | 0     | 0     | 0        | 0     | 0    | 0        | 0    | 0        | 0       | 0    |
| Ped-Bike Adj(A_pbT)          | 1.00 |          | 0.74  | 1.00  |          | 0.89  | 1.00 |          | 0.99 | 1.00     |         | 0.99 |
| Parking Bus, Adj             | 1.00 | 1.00     | 1.00  | 1.00  | 1.00     | 1.00  | 1.00 | 1.00     | 1.00 | 1.00     | 1.00    | 1.00 |
| Adj Sat Flow, veh/h/ln       | 1863 | 1863     | 1900  | 1863  | 1863     | 1900  | 1863 | 1863     | 1863 | 1863     | 1863    | 1900 |
| Adj Flow Rate, veh/h         | 57   | 215      | 59    | 329   | 222      | 465   | 99   | 303      | 253  | 234      | 157     | 32   |
| Adj No. of Lanes             | 1    | 1        | 0     | 1     | 1        | 0     | 1    | 1        | 1    | 1        | 1       | 0    |
| Peak Hour Factor             | 0.79 | 0.79     | 0.79  | 0.79  | 0.79     | 0.79  | 0.79 | 0.79     | 0.79 | 0.79     | 0.79    | 0.79 |
| Percent Heavy Veh, %         | 2    | 2        | 2     | 2     | 2        | 2     | 2    | 2        | 2    | 2        | 2       | 2    |
| Cap, veh/h                   | 85   | 324      | 89    | 235   | 165      | 345   | 127  | 491      | 415  | 166      | 429     | 87   |
| Arrive On Green              | 0.05 | 0.25     | 0.25  | 0.13  | 0.34     | 0.34  | 0.07 | 0.26     | 0.26 | 0.09     | 0.29    | 0.29 |
| Sat Flow, veh/h              | 1774 | 1295     | 355   | 1774  | 492      | 1031  | 1774 | 1863     | 1574 | 1774     | 1499    | 306  |
| Grp Volume(v), veh/h         | 57   | 0        | 274   | 329   | 0        | 687   | 99   | 303      | 253  | 234      | 0       | 189  |
| Grp Sat Flow(s),veh/h/ln     | 1774 | 0        | 1650  | 1774  | 0        | 1523  | 1774 | 1863     | 1574 | 1774     | 0       | 1804 |
| Q Serve(g_s), s              | 2.2  | 0.0      | 10.4  | 9.2   | 0.0      | 23.2  | 3.8  | 9.9      | 9.8  | 6.5      | 0.0     | 5.8  |
| Cycle Q Clear(g_c), s        | 2.2  | 0.0      | 10.4  | 9.2   | 0.0      | 23.2  | 3.8  | 9.9      | 9.8  | 6.5      | 0.0     | 5.8  |
| Prop In Lane                 | 1.00 |          | 0.22  | 1.00  |          | 0.68  | 1.00 |          | 1.00 | 1.00     |         | 0.17 |
| Lane Grp Cap(c), veh/h       | 85   | 0        | 413   | 235   | 0        | 510   | 127  | 491      | 415  | 166      | 0       | 516  |
| V/C Ratio(X)                 | 0.67 | 0.00     | 0.66  | 1.40  | 0.00     | 1.35  | 0.78 | 0.62     | 0.61 | 1.41     | 0.00    | 0.37 |
| Avail Cap(c_a), veh/h        | 130  | 0        | 428   | 235   | 0        | 510   | 159  | 491      | 415  | 166      | 0       | 516  |
| HCM Platoon Ratio            | 1.00 | 1.00     | 1.00  | 1.00  | 1.00     | 1.00  | 1.00 | 1.00     | 1.00 | 1.00     | 1.00    | 1.00 |
| Upstream Filter(I)           | 1.00 | 0.00     | 1.00  | 1.00  | 0.00     | 1.00  | 1.00 | 1.00     | 1.00 | 1.00     | 0.00    | 1.00 |
| Uniform Delay (d), s/veh     | 32.5 | 0.0      | 23.4  | 30.1  | 0.0      | 23.1  | 31.7 | 22.5     | 22.4 | 31.4     | 0.0     | 19.7 |
| Incr Delay (d2), s/veh       | 8.7  | 0.0      | 3.6   | 203.0 | 0.0      | 168.5 | 17.7 | 5.7      | 6.5  | 215.4    | 0.0     | 2.0  |
| Initial Q Delay(d3),s/veh    | 0.0  | 0.0      | 0.0   | 0.0   | 0.0      | 0.0   | 0.0  | 0.0      | 0.0  | 0.0      | 0.0     | 0.0  |
| %ile BackOfQ(50%),veh/ln     | 1.3  | 0.0      | 5.1   | 17.7  | 0.0      | 33.5  | 2.5  | 5.8      | 5.0  | 13.1     | 0.0     | 3.2  |
| LnGrp Delay(d),s/veh         | 41.2 | 0.0      | 27.0  | 233.1 | 0.0      | 191.5 | 49.4 | 28.2     | 28.9 | 246.8    | 0.0     | 21.7 |
| LnGrp LOS                    | D    |          | С     | F     |          | F     | D    | С        | С    | F        |         | С    |
| Approach Vol, veh/h          |      | 331      |       |       | 1016     |       |      | 655      |      |          | 423     |      |
| Approach Delay, s/veh        |      | 29.4     |       |       | 205.0    |       |      | 31.7     |      |          | 146.2   |      |
| Approach LOS                 |      | С        |       |       | F        |       |      | С        |      |          | F       |      |
| Timer                        | 1    | 2        | 3     | 4     | 5        | 6     | 7    | 8        |      |          |         |      |
| Assigned Phs                 | 1    | 2        | 3     | 4     | 5        | 6     | 7    | 8        |      |          |         |      |
| Phs Duration (G+Y+Rc), s     | 11.0 | 22.8     | 13.7  | 21.9  | 9.5      | 24.3  | 7.8  | 27.7     |      |          |         |      |
| Change Period (Y+Rc), s      | 4.5  | 4.5      | 4.5   | 4.5   | 4.5      | 4.5   | 4.5  | 4.5      |      |          |         |      |
| Max Green Setting (Gmax), s  | 6.5  | 18.3     | 9.2   | 18.0  | 6.2      | 18.6  | 5.1  | 22.1     |      |          |         |      |
| Max Q Clear Time (g_c+l1), s | 8.5  | 11.9     | 11.2  | 12.4  | 5.8      | 7.8   | 4.2  | 25.2     |      |          |         |      |
| Green Ext Time (p_c), s      | 0.0  | 1.5      | 0.0   | 0.8   | 0.0      | 0.7   | 0.0  | 0.0      |      |          |         |      |
| Intersection Summary         |      |          |       |       |          |       |      |          |      |          |         |      |
| HCM 2010 Ctrl Delay          |      |          | 124.0 |       |          |       |      |          |      |          |         |      |
| HCM 2010 LOS                 |      |          | F     |       |          |       |      |          |      |          |         |      |

7.787

0.426

20

С

2.1

7.224

0.15

13.9

В

0.5

6.727

0.344

16.4

С

1.5

6.216

0.734

31.7

D

5.9

5.499

0.633

23.1

C

4.3

7.549

0.027

12.8

В

0.1

7.036

0.676

29.5

D

4.8

6.318

0.234

13.9

В

0.9

7.554

0.323

17.2

C

1.4

7.045

0.274

15.5

C

1.1

6.332

0.383

16.6

C

1.8

| Intersection               |      |         |       |       |         |       |       |       |       |       |         |       |
|----------------------------|------|---------|-------|-------|---------|-------|-------|-------|-------|-------|---------|-------|
| Intersection Delay, s/veh  | 22.5 |         |       |       |         |       |       |       |       |       |         |       |
| Intersection LOS           | С    |         |       |       |         |       |       |       |       |       |         |       |
|                            |      |         |       |       |         |       |       |       |       |       |         |       |
| Movement                   | EBL  | EBT     | EBR   | WBL   | WBT     | WBR   | NBL   | NBT   | NBR   | SBL   | SBT     | SBR   |
| Lane Configurations        | Ť    | <u></u> | 7     | Ť     | <u></u> | 7     | ř     | ĵ.    |       | *     | <b></b> | 7     |
| Traffic Vol, veh/h         | 134  | 305     | 286   | 10    | 255     | 95    | 148   | 50    | 5     | 115   | 103     | 156   |
| Future Vol, veh/h          | 134  | 305     | 286   | 10    | 255     | 95    | 148   | 50    | 5     | 115   | 103     | 156   |
| Peak Hour Factor           | 0.97 | 0.97    | 0.97  | 0.97  | 0.97    | 0.97  | 0.97  | 0.97  | 0.97  | 0.97  | 0.97    | 0.97  |
| Heavy Vehicles, %          | 2    | 2       | 2     | 2     | 2       | 2     | 2     | 2     | 2     | 2     | 2       | 2     |
| Mvmt Flow                  | 138  | 314     | 295   | 10    | 263     | 98    | 153   | 52    | 5     | 119   | 106     | 161   |
| Number of Lanes            | 1    | 1       | 1     | 1     | 1       | 1     | 1     | 1     | 0     | 1     | 1       | 1     |
| Approach                   | EB   |         |       | WB    |         |       | NB    |       |       | SB    |         |       |
| Opposing Approach          | WB   |         |       | EB    |         |       | SB    |       |       | NB    |         |       |
| Opposing Lanes             | 3    |         |       | 3     |         |       | 3     |       |       | 2     |         |       |
| Conflicting Approach Left  | SB   |         |       | NB    |         |       | EB    |       |       | WB    |         |       |
| Conflicting Lanes Left     | 3    |         |       | 2     |         |       | 3     |       |       | 3     |         |       |
| Conflicting Approach Right | NB   |         |       | SB    |         |       | WB    |       |       | EB    |         |       |
| Conflicting Lanes Right    | 2    |         |       | 3     |         |       | 3     |       |       | 3     |         |       |
| HCM Control Delay          | 25.5 |         |       | 24.9  |         |       | 18.3  |       |       | 16.5  |         |       |
| HCM LOS                    | D    |         |       | С     |         |       | С     |       |       | С     |         |       |
|                            |      |         |       |       |         |       |       |       |       |       |         |       |
| Lane                       |      | NBLn1   | NBLn2 | EBLn1 | EBLn2   | EBLn3 | WBLn1 | WBLn2 | WBLn3 | SBLn1 | SBLn2   | SBLn3 |
| Vol Left, %                |      | 100%    | 0%    | 100%  | 0%      | 0%    | 100%  | 0%    | 0%    | 100%  | 0%      | 0%    |
| Vol Thru, %                |      | 0%      | 91%   | 0%    | 100%    | 0%    | 0%    | 100%  | 0%    | 0%    | 100%    | 0%    |
| Vol Right, %               |      | 0%      | 9%    | 0%    | 0%      | 100%  | 0%    | 0%    | 100%  | 0%    | 0%      | 100%  |
| Sign Control               |      | Stop    | Stop  | Stop  | Stop    | Stop  | Stop  | Stop  | Stop  | Stop  | Stop    | Stop  |
| Traffic Vol by Lane        |      | 148     | 55    | 134   | 305     | 286   | 10    | 255   | 95    | 115   | 103     | 156   |
| LT Vol                     |      | 148     | 0     | 134   | 0       | 0     | 10    | 0     | 0     | 115   | 0       | 0     |
| Through Vol                |      | 0       | 50    | 0     | 305     | 0     | 0     | 255   | 0     | 0     | 103     | 0     |
| RT Vol                     |      | 0       | 5     | 0     | 0       | 286   | 0     | 0     | 95    | 0     | 0       | 156   |
| Lane Flow Rate             |      | 153     | 57    | 138   | 314     | 295   | 10    | 263   | 98    | 119   | 106     | 161   |
| Geometry Grp               |      | 8       | 8     | 8     | 8       | 8     | 8     | 8     | 8     | 8     | 8       | 8     |
| Degree of Util (X)         |      | 0.425   | 0.149 | 0.344 | 0.739   | 0.634 | 0.028 | 0.677 | 0.233 | 0.322 | 0.274   | 0.383 |
| Departure Headway (Hd)     |      | 10.02   | 9.457 | 8.969 | 8.458   | 7.742 | 9.782 | 9.269 | 8.551 | 9.788 | 9.28    | 8.567 |
| Convergence, Y/N           |      | Yes     | Yes   | Yes   | Yes     | Yes   | Yes   | Yes   | Yes   | Yes   | Yes     | Yes   |
| Cap                        |      | 359     | 379   | 401   | 428     | 466   | 366   | 389   | 419   | 368   | 387     | 420   |

Service Time

HCM Lane V/C Ratio

**HCM Control Delay** 

**HCM Lane LOS** 

HCM 95th-tile Q

| Intersection           |         |         |          |        |       |      |        |       |       |        |       |       |       |  |
|------------------------|---------|---------|----------|--------|-------|------|--------|-------|-------|--------|-------|-------|-------|--|
| nt Delay, s/veh        | 10.5    |         |          |        |       |      |        |       |       |        |       |       |       |  |
| Movement               | EBL     | EBT     | EBR      | WBL    | WBT   | WBR  | NBL    | NBT   | NBR   | SBL    | SBT   | SBR   |       |  |
| ane Configurations     | ሻ       |         | 7        | Ť      |       | 7    | ř      |       | 7     | ሻ      |       | 7     |       |  |
| Fraffic Vol, veh/h     | 175     | 649     | 65       | 71     | 446   | 42   | 35     | 5     | 51    | 25     | 5     | 100   |       |  |
| uture Vol, veh/h       | 175     | 649     | 65       | 71     | 446   | 42   | 35     | 5     | 51    | 25     | 5     | 100   |       |  |
| Conflicting Peds, #/hr | 0       | 0       | 0        | 0      | 0     | 0    | 0      | 0     | 0     | 0      | 0     | 0     |       |  |
| Sign Control           | Free    | Free    | Free     | Free   | Free  | Free | Stop   | Stop  | Stop  | Stop   | Stop  | Stop  |       |  |
| RT Channelized         | -       | _       | None     | -      | -     | None | -      | -     | None  | -      | -     | None  |       |  |
| Storage Length         | 320     | -       | 505      | 360    | -     | 195  | 60     | -     | 0     | 100    | -     | 100   |       |  |
| Veh in Median Storage, | , # -   | 0       | -        | -      | 0     | -    | -      | 0     | -     | -      | 0     | -     |       |  |
| Grade, %               | -       | 0       | -        | -      | 0     | -    | -      | 0     | -     | -      | 0     | -     |       |  |
| Peak Hour Factor       | 95      | 95      | 95       | 95     | 95    | 95   | 95     | 95    | 95    | 95     | 95    | 95    |       |  |
| Heavy Vehicles, %      | 2       | 2       | 2        | 2      | 2     | 2    | 2      | 2     | 2     | 2      | 2     | 2     |       |  |
| Mvmt Flow              | 184     | 683     | 68       | 75     | 469   | 44   | 37     | 5     | 54    | 26     | 5     | 105   |       |  |
|                        |         |         |          |        |       |      |        |       |       |        |       |       |       |  |
| Major/Minor N          | /lajor1 |         | <u> </u> | Major2 |       |      | Minor1 |       |       | Minor2 |       |       |       |  |
| Conflicting Flow All   | 513     | 0       | 0        | 751    | 0     | 0    | 1747   | 1714  | 683   | 1734   | 1738  | 469   |       |  |
| Stage 1                | -       | _       | -        | -      | -     | -    | 1051   | 1051  | -     | 619    | 619   | -     |       |  |
| Stage 2                | -       | -       | -        | -      | -     | -    | 696    | 663   | -     | 1115   | 1119  | -     |       |  |
| Critical Hdwy          | 4.12    | _       | -        | 4.12   | -     | -    | 7.12   | 6.52  | 6.22  | 7.12   | 6.52  | 6.22  |       |  |
| Critical Hdwy Stg 1    | -       | -       | -        | -      | -     | -    | 6.12   | 5.52  | -     | 6.12   | 5.52  | -     |       |  |
| Critical Hdwy Stg 2    | -       | _       | -        | -      | -     | -    | 6.12   | 5.52  | -     | 6.12   | 5.52  | -     |       |  |
|                        | 2.218   | -       | -        | 2.218  | -     | -    | 3.518  | 4.018 | 3.318 | 3.518  | 4.018 | 3.318 |       |  |
| Pot Cap-1 Maneuver     | 1052    | _       | -        | 858    | -     | -    | 67     | 90    | 449   | 69     | 87    | 594   |       |  |
| Stage 1                | -       | -       | -        | -      | -     | -    | 274    | 304   | -     | 476    | 480   | -     |       |  |
| Stage 2                | -       | _       | -        | -      | -     | -    | 432    | 459   | -     | 252    | 282   | -     |       |  |
| Platoon blocked, %     |         | -       | -        |        | -     | -    |        |       |       |        |       |       |       |  |
| Mov Cap-1 Maneuver     | 1052    | -       | -        | 858    | -     | -    | 42     | 68    | 449   | 46     | 66    | 594   |       |  |
| Mov Cap-2 Maneuver     | -       | -       | -        | -      | -     | -    | 42     | 68    | -     | 46     | 66    | -     |       |  |
| Stage 1                | -       | -       | -        | -      | -     | -    | 226    | 251   | -     | 393    | 438   | -     |       |  |
| Stage 2                | -       | -       | -        | -      | -     | -    | 320    | 419   | -     | 179    | 233   | -     |       |  |
| _                      |         |         |          |        |       |      |        |       |       |        |       |       |       |  |
| Approach               | EB      |         |          | WB     |       |      | NB     |       |       | SB     |       |       |       |  |
| HCM Control Delay, s   | 1.8     |         |          | 1.2    |       |      | 107.1  |       |       | 42.5   |       |       |       |  |
| HCM LOS                |         |         |          |        |       |      | F      |       |       | Е      |       |       |       |  |
|                        |         |         |          |        |       |      |        |       |       |        |       |       |       |  |
| Minor Lane/Major Mvm   | t       | NBLn1 I | NBLn21   | NBLn3  | EBL   | EBT  | EBR    | WBL   | WBT   | WBR    | SBLn1 | SBLn2 | SBLn3 |  |
| Capacity (veh/h)       |         | 42      | 68       | 449    | 1052  | _    | _      | 858   | -     | -      | 46    | 66    | 594   |  |
| HCM Lane V/C Ratio     |         | 0.877   | 0.077    | 0.12   | 0.175 | -    | -      | 0.087 | -     | -      | 0.572 | 0.08  | 0.177 |  |
| HCM Control Delay (s)  |         | 249.1   | 62.3     | 14.1   | 9.1   | -    | -      | 9.6   | -     | -      | 158.5 | 64.2  | 12.4  |  |
|                        |         |         |          |        |       |      |        |       |       |        |       |       |       |  |
| HCM Lane LOS           |         | F       | F        | В      | Α     | -    | -      | Α     | -     | -      | F     | F     | В     |  |

| Intersection           |        |       |           |       |        |      |
|------------------------|--------|-------|-----------|-------|--------|------|
| Int Delay, s/veh       | 3.3    |       |           |       |        |      |
| Movement               | WBL    | WBR   | NBT       | NBR   | SBL    | SBT  |
|                        |        | WDK   |           | NDK   | ODL    |      |
| Lane Configurations    | ¥      | 00    | <b>\$</b> | 0.4   | 440    | 4    |
| Traffic Vol, veh/h     | 34     | 83    | 207       | 31    | 116    | 315  |
| Future Vol, veh/h      | 34     | 83    | 207       | 31    | 116    | 315  |
| Conflicting Peds, #/hr | 1      | 0     | 0         | 0     | 0      | 0    |
| Sign Control           | Stop   | Stop  | Free      | Free  | Free   | Free |
| RT Channelized         | -      | None  | -         | None  | -      | None |
| Storage Length         | 0      | -     | -         | -     | -      | -    |
| Veh in Median Storage  | e, # 0 | -     | 0         | -     | -      | 0    |
| Grade, %               | 0      | -     | 0         | -     | -      | 0    |
| Peak Hour Factor       | 93     | 93    | 93        | 93    | 93     | 93   |
| Heavy Vehicles, %      | 6      | 6     | 2         | 2     | 3      | 3    |
| Mymt Flow              | 37     | 89    | 223       | 33    | 125    | 339  |
| WWW.CT IOW             | O1     | 00    | LLU       | 00    | 120    | 000  |
|                        |        |       |           |       |        |      |
|                        | Minor1 |       | Major1    |       | Major2 |      |
| Conflicting Flow All   | 830    | 240   | 0         | 0     | 256    | 0    |
| Stage 1                | 240    | -     | -         | -     | -      | -    |
| Stage 2                | 590    | -     | -         | -     | -      | -    |
| Critical Hdwy          | 6.46   | 6.26  | -         | -     | 4.13   | -    |
| Critical Hdwy Stg 1    | 5.46   | _     | -         | -     | _      | _    |
| Critical Hdwy Stg 2    | 5.46   | _     | _         | _     | _      | _    |
| Follow-up Hdwy         | 3.554  | 3.354 | _         | _     | 2.227  | _    |
| Pot Cap-1 Maneuver     | 335    | 789   | _         | _     | 1303   | _    |
| Stage 1                | 791    | - 100 | _         | _     | -      | _    |
| Stage 2                | 546    | _     |           |       | _      | _    |
| Platoon blocked, %     | 340    | -     |           | -     | _      |      |
| •                      | 295    | 789   | -         | _     | 1202   | -    |
| Mov Cap-1 Maneuver     |        |       | -         | -     | 1303   | -    |
| Mov Cap-2 Maneuver     | 295    | -     | -         | -     | -      | -    |
| Stage 1                | 698    | -     | -         | -     | -      | -    |
| Stage 2                | 545    | -     | -         | -     | -      | -    |
|                        |        |       |           |       |        |      |
| Approach               | WB     |       | NB        |       | SB     |      |
| HCM Control Delay, s   | 13.9   |       | 0         |       | 2.2    |      |
| HCM LOS                |        |       | U         |       | 2.2    |      |
| I IOWI LOS             | В      |       |           |       |        |      |
|                        |        |       |           |       |        |      |
| Minor Lane/Major Mvn   | nt     | NBT   | NBRV      | VBLn1 | SBL    | SBT  |
| Capacity (veh/h)       |        | _     | -         |       | 1303   | _    |
| HCM Lane V/C Ratio     |        | _     | _         | 0.237 |        | _    |
| HCM Control Delay (s   | 1      | _     | _         | 13.9  | 8.1    | 0    |
| HCM Lane LOS           |        | _     |           | В     | Α      | A    |
| HCM 95th %tile Q(veh   | )      |       |           | 0.9   | 0.3    | -    |
| TION JOHN JOHN W(VEI)  | 1)     | _     | _         | 0.9   | 0.5    | _    |

|                              | ۶    | <b>→</b> | •     | •    | <b>←</b> | •     | •     | <b>†</b> | ~    | <b>&gt;</b> | <b>↓</b> | ✓    |
|------------------------------|------|----------|-------|------|----------|-------|-------|----------|------|-------------|----------|------|
| Movement                     | EBL  | EBT      | EBR   | WBL  | WBT      | WBR   | NBL   | NBT      | NBR  | SBL         | SBT      | SBR  |
| Lane Configurations          | Ť    | f.       |       | J.   | f)       |       | *     | <b></b>  | 7    | Ť           | <b>†</b> | 7    |
| Traffic Volume (veh/h)       | 313  | 393      | 244   | 25   | 266      | 220   | 200   | 645      | 36   | 375         | 620      | 267  |
| Future Volume (veh/h)        | 313  | 393      | 244   | 25   | 266      | 220   | 200   | 645      | 36   | 375         | 620      | 267  |
| Number                       | 7    | 4        | 14    | 3    | 8        | 18    | 5     | 2        | 12   | 1           | 6        | 16   |
| Initial Q (Qb), veh          | 0    | 0        | 0     | 0    | 0        | 0     | 0     | 0        | 0    | 0           | 0        | 0    |
| Ped-Bike Adj(A_pbT)          | 1.00 |          | 1.00  | 1.00 |          | 1.00  | 1.00  |          | 1.00 | 1.00        |          | 1.00 |
| Parking Bus, Adj             | 1.00 | 1.00     | 1.00  | 1.00 | 1.00     | 1.00  | 1.00  | 1.00     | 1.00 | 1.00        | 1.00     | 1.00 |
| Adj Sat Flow, veh/h/ln       | 1863 | 1863     | 1900  | 1863 | 1863     | 1900  | 1863  | 1863     | 1863 | 1863        | 1863     | 1863 |
| Adj Flow Rate, veh/h         | 326  | 409      | 254   | 26   | 277      | 229   | 208   | 672      | 38   | 391         | 646      | 278  |
| Adj No. of Lanes             | 1    | 1        | 0     | 1    | 1        | 0     | 1     | 1        | 1    | 1           | 1        | 1    |
| Peak Hour Factor             | 0.96 | 0.96     | 0.96  | 0.96 | 0.96     | 0.96  | 0.96  | 0.96     | 0.96 | 0.96        | 0.96     | 0.96 |
| Percent Heavy Veh, %         | 2    | 2        | 2     | 2    | 2        | 2     | 2     | 2        | 2    | 2           | 2        | 2    |
| Cap, veh/h                   | 426  | 258      | 160   | 218  | 116      | 96    | 177   | 479      | 407  | 248         | 554      | 471  |
| Arrive On Green              | 0.24 | 0.24     | 0.24  | 0.12 | 0.12     | 0.12  | 0.10  | 0.26     | 0.26 | 0.14        | 0.30     | 0.30 |
| Sat Flow, veh/h              | 1774 | 1076     | 668   | 1774 | 944      | 781   | 1774  | 1863     | 1583 | 1774        | 1863     | 1583 |
| Grp Volume(v), veh/h         | 326  | 0        | 663   | 26   | 0        | 506   | 208   | 672      | 38   | 391         | 646      | 278  |
| Grp Sat Flow(s),veh/h/ln     | 1774 | 0        | 1745  | 1774 | 0        | 1725  | 1774  | 1863     | 1583 | 1774        | 1863     | 1583 |
| Q Serve(g_s), s              | 12.8 | 0.0      | 18.0  | 1.0  | 0.0      | 9.2   | 7.5   | 19.3     | 1.4  | 10.5        | 22.3     | 11.2 |
| Cycle Q Clear(g_c), s        | 12.8 | 0.0      | 18.0  | 1.0  | 0.0      | 9.2   | 7.5   | 19.3     | 1.4  | 10.5        | 22.3     | 11.2 |
| Prop In Lane                 | 1.00 |          | 0.38  | 1.00 |          | 0.45  | 1.00  |          | 1.00 | 1.00        |          | 1.00 |
| Lane Grp Cap(c), veh/h       | 426  | 0        | 419   | 218  | 0        | 212   | 177   | 479      | 407  | 248         | 554      | 471  |
| V/C Ratio(X)                 | 0.77 | 0.00     | 1.58  | 0.12 | 0.00     | 2.39  | 1.17  | 1.40     | 0.09 | 1.57        | 1.17     | 0.59 |
| Avail Cap(c_a), veh/h        | 426  | 0        | 419   | 218  | 0        | 212   | 177   | 479      | 407  | 248         | 554      | 471  |
| HCM Platoon Ratio            | 1.00 | 1.00     | 1.00  | 1.00 | 1.00     | 1.00  | 1.00  | 1.00     | 1.00 | 1.00        | 1.00     | 1.00 |
| Upstream Filter(I)           | 1.00 | 0.00     | 1.00  | 1.00 | 0.00     | 1.00  | 1.00  | 1.00     | 1.00 | 1.00        | 1.00     | 1.00 |
| Uniform Delay (d), s/veh     | 26.5 | 0.0      | 28.5  | 29.3 | 0.0      | 32.9  | 33.8  | 27.9     | 21.2 | 32.3        | 26.4     | 22.5 |
| Incr Delay (d2), s/veh       | 8.1  | 0.0      | 273.7 | 0.2  | 0.0      | 640.4 | 121.6 | 193.1    | 0.5  | 277.0       | 93.2     | 5.4  |
| Initial Q Delay(d3),s/veh    | 0.0  | 0.0      | 0.0   | 0.0  | 0.0      | 0.0   | 0.0   | 0.0      | 0.0  | 0.0         | 0.0      | 0.0  |
| %ile BackOfQ(50%),veh/ln     | 7.2  | 0.0      | 40.4  | 0.5  | 0.0      | 42.0  | 9.6   | 35.6     | 0.7  | 24.2        | 25.7     | 5.6  |
| LnGrp Delay(d),s/veh         | 34.7 | 0.0      | 302.2 | 29.5 | 0.0      | 673.3 | 155.4 | 221.0    | 21.6 | 309.2       | 119.5    | 27.8 |
| LnGrp LOS                    | С    |          | F     | С    |          | F     | F     | F        | С    | F           | F        | С    |
| Approach Vol, veh/h          |      | 989      |       |      | 532      |       |       | 918      |      |             | 1315     |      |
| Approach Delay, s/veh        |      | 214.0    |       |      | 641.8    |       |       | 197.9    |      |             | 156.5    |      |
| Approach LOS                 |      | F        |       |      | F        |       |       | F        |      |             | F        |      |
| Timer                        | 1    | 2        | 3     | 4    | 5        | 6     | 7     | 8        |      |             |          |      |
| Assigned Phs                 | 1    | 2        |       | 4    | 5        | 6     |       | 8        |      |             |          |      |
| Phs Duration (G+Y+Rc), s     | 15.0 | 23.8     |       | 22.5 | 12.0     | 26.8  |       | 13.7     |      |             |          |      |
| Change Period (Y+Rc), s      | 4.5  | 4.5      |       | 4.5  | 4.5      | 4.5   |       | 4.5      |      |             |          |      |
| Max Green Setting (Gmax), s  | 10.5 | 19.3     |       | 18.0 | 7.5      | 22.3  |       | 9.2      |      |             |          |      |
| Max Q Clear Time (g_c+l1), s | 12.5 | 21.3     |       | 20.0 | 9.5      | 24.3  |       | 11.2     |      |             |          |      |
| Green Ext Time (p_c), s      | 0.0  | 0.0      |       | 0.0  | 0.0      | 0.0   |       | 0.0      |      |             |          |      |
| Intersection Summary         |      |          |       |      |          |       |       |          |      |             |          |      |
| HCM 2010 Ctrl Delay          |      |          | 250.6 |      |          |       |       |          |      |             |          |      |
| HCM 2010 LOS                 |      |          | F     |      |          |       |       |          |      |             |          |      |

|                              | •    |            |          |          | _     | •    |      | _    | _    |      |      |      |
|------------------------------|------|------------|----------|----------|-------|------|------|------|------|------|------|------|
|                              |      | <b>→</b>   | *        | •        | •     |      | 7    | T    |      | *    | +    | *    |
| Movement                     | EBL  | EBT        | EBR      | WBL      | WBT   | WBR  | NBL  | NBT  | NBR  | SBL  | SBT  | SBR  |
| Lane Configurations          | 7    | f)         |          | ሻ        | ₽     |      |      | 4    |      |      | 4    |      |
| Traffic Volume (veh/h)       | 55   | 780        | 183      | 180      | 488   | 35   | 135  | 57   | 115  | 55   | 86   | 34   |
| Future Volume (veh/h)        | 55   | 780        | 183      | 180      | 488   | 35   | 135  | 57   | 115  | 55   | 86   | 34   |
| Number                       | 7    | 4          | 14       | 3        | 8     | 18   | 5    | 2    | 12   | 1    | 6    | 16   |
| Initial Q (Qb), veh          | 0    | 0          | 0        | 0        | 0     | 0    | 0    | 0    | 0    | 0    | 0    | 0    |
| Ped-Bike Adj(A_pbT)          | 1.00 |            | 1.00     | 1.00     |       | 1.00 | 1.00 |      | 1.00 | 1.00 |      | 1.00 |
| Parking Bus, Adj             | 1.00 | 1.00       | 1.00     | 1.00     | 1.00  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln       | 1863 | 1863       | 1900     | 1863     | 1863  | 1900 | 1900 | 1863 | 1900 | 1900 | 1827 | 1900 |
| Adj Flow Rate, veh/h         | 62   | 886        | 208      | 205      | 555   | 40   | 153  | 65   | 131  | 62   | 98   | 39   |
| Adj No. of Lanes             | 1    | 1          | 0        | 1        | 1     | 0    | 0    | 1    | 0    | 0    | 1    | 0    |
| Peak Hour Factor             | 0.88 | 0.88       | 0.88     | 0.88     | 0.88  | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 |
| Percent Heavy Veh, %         | 2    | 2          | 2        | 2        | 2     | 2    | 2    | 2    | 2    | 4    | 4    | 4    |
| Cap, veh/h                   | 95   | 547        | 128      | 151      | 698   | 50   | 274  | 117  | 183  | 195  | 285  | 98   |
| Arrive On Green              | 0.05 | 0.38       | 0.38     | 0.09     | 0.41  | 0.41 | 0.31 | 0.31 | 0.31 | 0.31 | 0.31 | 0.31 |
| Sat Flow, veh/h              | 1774 | 1460       | 343      | 1774     | 1717  | 124  | 597  | 370  | 581  | 369  | 905  | 311  |
| Grp Volume(v), veh/h         | 62   | 0          | 1094     | 205      | 0     | 595  | 349  | 0    | 0    | 199  | 0    | 0    |
| Grp Sat Flow(s),veh/h/ln     | 1774 | 0          | 1802     | 1774     | 0     | 1841 | 1549 | 0    | 0    | 1585 | 0    | 0    |
| Q Serve(g_s), s              | 2.1  | 0.0        | 22.5     | 5.1      | 0.0   | 17.0 | 6.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  |
| Cycle Q Clear(g_c), s        | 2.1  | 0.0        | 22.5     | 5.1      | 0.0   | 17.0 | 11.3 | 0.0  | 0.0  | 5.4  | 0.0  | 0.0  |
| Prop In Lane                 | 1.00 |            | 0.19     | 1.00     |       | 0.07 | 0.44 |      | 0.38 | 0.31 |      | 0.20 |
| Lane Grp Cap(c), veh/h       | 95   | 0          | 676      | 151      | 0     | 748  | 574  | 0    | 0    | 578  | 0    | 0    |
| V/C Ratio(X)                 | 0.65 | 0.00       | 1.62     | 1.36     | 0.00  | 0.80 | 0.61 | 0.00 | 0.00 | 0.34 | 0.00 | 0.00 |
| Avail Cap(c_a), veh/h        | 163  | 0          | 676      | 151      | 0     | 748  | 574  | 0    | 0    | 578  | 0    | 0    |
| HCM Platoon Ratio            | 1.00 | 1.00       | 1.00     | 1.00     | 1.00  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I)           | 1.00 | 0.00       | 1.00     | 1.00     | 0.00  | 1.00 | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| Uniform Delay (d), s/veh     | 27.8 | 0.0        | 18.8     | 27.5     | 0.0   | 15.6 | 17.7 | 0.0  | 0.0  | 15.9 | 0.0  | 0.0  |
| Incr Delay (d2), s/veh       | 7.3  | 0.0        | 285.2    | 198.5    | 0.0   | 6.0  | 4.7  | 0.0  | 0.0  | 1.6  | 0.0  | 0.0  |
| Initial Q Delay(d3),s/veh    | 0.0  | 0.0        | 0.0      | 0.0      | 0.0   | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  |
| %ile BackOfQ(50%),veh/ln     | 1.2  | 0.0        | 64.6     | 10.8     | 0.0   | 9.8  | 5.8  | 0.0  | 0.0  | 2.8  | 0.0  | 0.0  |
| LnGrp Delay(d),s/veh         | 35.1 | 0.0        | 304.0    | 226.0    | 0.0   | 21.6 | 22.4 | 0.0  | 0.0  | 17.5 | 0.0  | 0.0  |
| LnGrp LOS                    | D    | 0.0        | F        | F        | 0.0   | C    | C    | 0.0  | 0.0  | В    | 0.0  | 0.0  |
| Approach Vol, veh/h          |      | 1156       | <u> </u> | <u> </u> | 800   |      |      | 349  |      |      | 199  |      |
| Approach Delay, s/veh        |      | 289.5      |          |          | 74.0  |      |      | 22.4 |      |      | 17.5 |      |
| Approach LOS                 |      | 203.5<br>F |          |          | 7 T.0 |      |      | C C  |      |      | В    |      |
|                              |      |            |          |          |       |      |      |      |      |      | D    |      |
| Timer                        | 1    | 2          | 3        | 4        | 5     | 6    | 7    | 8    |      |      |      |      |
| Assigned Phs                 |      | 2          | 3        | 4        |       | 6    | 7    | 8    |      |      |      |      |
| Phs Duration (G+Y+Rc), s     |      | 23.4       | 9.6      | 27.0     |       | 23.4 | 7.7  | 28.9 |      |      |      |      |
| Change Period (Y+Rc), s      |      | 4.5        | 4.5      | 4.5      |       | 4.5  | 4.5  | 4.5  |      |      |      |      |
| Max Green Setting (Gmax), s  |      | 18.9       | 5.1      | 22.5     |       | 18.9 | 5.5  | 22.1 |      |      |      |      |
| Max Q Clear Time (g_c+I1), s |      | 13.3       | 7.1      | 24.5     |       | 7.4  | 4.1  | 19.0 |      |      |      |      |
| Green Ext Time (p_c), s      |      | 1.1        | 0.0      | 0.0      |       | 0.8  | 0.0  | 1.2  |      |      |      |      |
| Intersection Summary         |      |            |          |          |       |      |      |      |      |      |      |      |
| HCM 2010 Ctrl Delay          |      |            | 161.8    |          |       |      |      |      |      |      |      |      |
| HCM 2010 LOS                 |      |            | F        |          |       |      |      |      |      |      |      |      |

|                              |      | <b>→</b> | <b>←</b> | •    | <u> </u> | 4    |      |      |  |  |
|------------------------------|------|----------|----------|------|----------|------|------|------|--|--|
| Movement                     | EBL  | EBT      | WBT      | WBR  | SBL      | SBR  |      |      |  |  |
| Lane Configurations          | ሻ    | <b>1</b> | <b>^</b> | 7    | ሻ        | 7    |      |      |  |  |
| Traffic Volume (veh/h)       | 389  | 745      | 413      | 244  | 273      | 276  |      |      |  |  |
| Future Volume (veh/h)        | 389  | 745      | 413      | 244  | 273      | 276  |      |      |  |  |
| Number                       | 7    | 4        | 8        | 18   | 1        | 16   |      |      |  |  |
| Initial Q (Qb), veh          | 0    | 0        | 0        | 0    | 0        | 0    |      |      |  |  |
| Ped-Bike Adj(A_pbT)          | 1.00 |          |          | 1.00 | 1.00     | 1.00 |      |      |  |  |
| Parking Bus, Adj             | 1.00 | 1.00     | 1.00     | 1.00 | 1.00     | 1.00 |      |      |  |  |
| Adj Sat Flow, veh/h/ln       | 1863 | 1863     | 1863     | 1863 | 1863     | 1863 |      |      |  |  |
| Adj Flow Rate, veh/h         | 405  | 776      | 430      | 254  | 284      | 288  |      |      |  |  |
| Adj No. of Lanes             | 1    | 1        | 1        | 1    | 1        | 1    |      |      |  |  |
| Peak Hour Factor             | 0.96 | 0.96     | 0.96     | 0.96 | 0.96     | 0.96 |      |      |  |  |
| Percent Heavy Veh, %         | 2    | 2        | 2        | 2    | 2        | 2    |      |      |  |  |
| Cap, veh/h                   | 466  | 1118     | 480      | 408  | 425      | 380  |      |      |  |  |
| Arrive On Green              | 0.26 | 0.60     | 0.26     | 0.26 | 0.24     | 0.24 |      |      |  |  |
| Sat Flow, veh/h              | 1774 | 1863     | 1863     | 1583 | 1774     | 1583 |      |      |  |  |
| Grp Volume(v), veh/h         | 405  | 776      | 430      | 254  | 284      | 288  |      |      |  |  |
| Grp Sat Flow(s), veh/h/ln    | 1774 | 1863     | 1863     | 1583 | 1774     | 1583 |      |      |  |  |
| Q Serve(g_s), s              | 12.3 | 16.1     | 12.5     | 8.0  | 8.2      | 9.5  |      |      |  |  |
| Cycle Q Clear(g_c), s        | 12.3 | 16.1     | 12.5     | 8.0  | 8.2      | 9.5  |      |      |  |  |
| Prop In Lane                 | 1.00 | 10.1     | 12.5     | 1.00 | 1.00     | 1.00 |      |      |  |  |
| Lane Grp Cap(c), veh/h       | 466  | 1118     | 480      | 408  | 425      | 380  |      |      |  |  |
| V/C Ratio(X)                 | 0.87 | 0.69     | 0.90     | 0.62 | 0.67     | 0.76 |      |      |  |  |
| Avail Cap(c_a), veh/h        | 583  | 1241     | 480      | 408  | 425      | 380  |      |      |  |  |
| HCM Platoon Ratio            | 1.00 | 1.00     | 1.00     | 1.00 | 1.00     | 1.00 |      |      |  |  |
| Upstream Filter(I)           | 1.00 | 1.00     | 1.00     | 1.00 | 1.00     | 1.00 |      |      |  |  |
|                              | 19.8 | 7.7      | 20.2     | 18.5 | 19.4     | 19.9 |      |      |  |  |
| Uniform Delay (d), s/veh     | 11.2 | 1.5      | 19.2     | 2.9  | 8.1      | 13.3 |      |      |  |  |
| Incr Delay (d2), s/veh       | 0.0  | 0.0      | 0.0      | 0.0  | 0.0      | 0.0  |      |      |  |  |
| Initial Q Delay(d3),s/veh    | 7.4  |          |          |      |          | 9.3  |      |      |  |  |
| %ile BackOfQ(50%),veh/ln     |      | 8.4      | 9.0      | 3.8  | 4.9      |      |      |      |  |  |
| LnGrp Delay(d),s/veh         | 31.0 | 9.2      | 39.4     | 21.4 | 27.4     | 33.2 |      |      |  |  |
| LnGrp LOS                    | С    | A        | D        | С    | CC       | С    |      |      |  |  |
| Approach Vol, veh/h          |      | 1181     | 684      |      | 572      |      |      |      |  |  |
| Approach Delay, s/veh        |      | 16.7     | 32.7     |      | 30.3     |      |      |      |  |  |
| Approach LOS                 |      | В        | С        |      | С        |      |      |      |  |  |
| Timer                        | 1    | 2        | 3        | 4    | 5        | 6    | 7    | 8    |  |  |
| Assigned Phs                 |      |          |          | 4    |          | 6    | 7    | 8    |  |  |
| Phs Duration (G+Y+Rc), s     |      |          |          | 38.3 |          | 18.0 |      | 19.0 |  |  |
| Change Period (Y+Rc), s      |      |          |          | 4.5  |          | 4.5  | 4.5  | 4.5  |  |  |
| Max Green Setting (Gmax), s  |      |          |          | 37.5 |          | 13.5 | 18.5 | 14.5 |  |  |
| Max Q Clear Time (g_c+l1), s |      |          |          | 18.1 |          | 11.5 | 14.3 | 14.5 |  |  |
| Green Ext Time (p_c), s      |      |          |          | 5.7  |          | 0.5  | 0.6  | 0.0  |  |  |
| Intersection Summary         |      |          |          |      |          |      |      |      |  |  |
| HCM 2010 Ctrl Delay          |      |          | 24.4     |      |          |      |      |      |  |  |
| HCM 2010 LOS                 |      |          | С        |      |          |      |      |      |  |  |

|                                   | ۶        | <b>→</b> | •      | •     | +           | •          | 1       | <b>†</b> | <i>&gt;</i> | <b>/</b> | <b>↓</b> | ✓    |
|-----------------------------------|----------|----------|--------|-------|-------------|------------|---------|----------|-------------|----------|----------|------|
| Movement                          | EBL      | EBT      | EBR    | WBL   | WBT         | WBR        | NBL     | NBT      | NBR         | SBL      | SBT      | SBR  |
| Lane Configurations               | 7        | <b>†</b> | 7      | 7     | ĵ.          |            |         | ર્ન      | 7           |          | ર્ન      | 7    |
| Traffic Volume (vph)              | 5        | 869      | 833    | 115   | 900         | 30         | 641     | 20       | 155         | 155      | 160      | 5    |
| Future Volume (vph)               | 5        | 869      | 833    | 115   | 900         | 30         | 641     | 20       | 155         | 155      | 160      | 5    |
| Ideal Flow (vphpl)                | 1900     | 1900     | 1900   | 1900  | 1900        | 1900       | 1900    | 1900     | 1900        | 1900     | 1900     | 1900 |
| Total Lost time (s)               | 4.5      | 4.5      | 4.5    | 4.5   | 4.5         |            |         | 4.5      | 4.5         |          | 4.5      | 4.5  |
| Lane Util. Factor                 | 1.00     | 1.00     | 1.00   | 1.00  | 1.00        |            |         | 1.00     | 1.00        |          | 1.00     | 1.00 |
| Frt                               | 1.00     | 1.00     | 0.85   | 1.00  | 1.00        |            |         | 1.00     | 0.85        |          | 1.00     | 0.85 |
| Flt Protected                     | 0.95     | 1.00     | 1.00   | 0.95  | 1.00        |            |         | 0.95     | 1.00        |          | 0.98     | 1.00 |
| Satd. Flow (prot)                 | 1687     | 1776     | 1509   | 1583  | 1659        |            |         | 1777     | 1583        |          | 1818     | 1583 |
| Flt Permitted                     | 0.95     | 1.00     | 1.00   | 0.95  | 1.00        |            |         | 0.95     | 1.00        |          | 0.98     | 1.00 |
| Satd. Flow (perm)                 | 1687     | 1776     | 1509   | 1583  | 1659        |            |         | 1777     | 1583        |          | 1818     | 1583 |
| Peak-hour factor, PHF             | 0.96     | 0.96     | 0.96   | 0.96  | 0.96        | 0.96       | 0.96    | 0.96     | 0.96        | 0.96     | 0.96     | 0.96 |
| Adj. Flow (vph)                   | 5        | 905      | 868    | 120   | 938         | 31         | 668     | 21       | 161         | 161      | 167      | 5    |
| RTOR Reduction (vph)              | 0        | 0        | 378    | 0     | 1           | 0          | 0       | 0        | 84          | 0        | 0        | 4    |
| Lane Group Flow (vph)             | 5        | 905      | 490    | 120   | 968         | 0          | 0       | 689      | 77          | 0        | 328      | 1    |
| Heavy Vehicles (%)                | 7%       | 7%       | 7%     | 14%   | 14%         | 14%        | 2%      | 2%       | 2%          | 2%       | 2%       | 2%   |
| Turn Type                         | Prot     | NA       | Perm   | Prot  | NA          |            | Split   | NA       | Perm        | Split    | NA       | Perm |
| Protected Phases                  | 7        | 4        |        | 3     | 8           |            | 5       | 5        |             | 6        | 6        |      |
| Permitted Phases                  |          |          | 4      |       |             |            |         |          | 5           |          |          | 6    |
| Actuated Green, G (s)             | 1.0      | 48.1     | 48.1   | 5.0   | 52.1        |            |         | 22.1     | 22.1        |          | 20.4     | 20.4 |
| Effective Green, g (s)            | 1.0      | 48.1     | 48.1   | 5.0   | 52.1        |            |         | 22.1     | 22.1        |          | 20.4     | 20.4 |
| Actuated g/C Ratio                | 0.01     | 0.42     | 0.42   | 0.04  | 0.46        |            |         | 0.19     | 0.19        |          | 0.18     | 0.18 |
| Clearance Time (s)                | 4.5      | 4.5      | 4.5    | 4.5   | 4.5         |            |         | 4.5      | 4.5         |          | 4.5      | 4.5  |
| Vehicle Extension (s)             | 3.0      | 3.0      | 3.0    | 3.0   | 3.0         |            |         | 3.0      | 3.0         |          | 3.0      | 3.0  |
| Lane Grp Cap (vph)                | 14       | 751      | 638    | 69    | 760         |            |         | 345      | 307         |          | 326      | 284  |
| v/s Ratio Prot                    | 0.00     | 0.51     |        | c0.08 | c0.58       |            |         | c0.39    |             |          | c0.18    |      |
| v/s Ratio Perm                    |          |          | 0.32   |       |             |            |         |          | 0.05        |          |          | 0.00 |
| v/c Ratio                         | 0.36     | 1.21     | 0.77   | 1.74  | 1.27        |            |         | 2.00     | 0.25        |          | 1.01     | 0.00 |
| Uniform Delay, d1                 | 56.0     | 32.8     | 28.0   | 54.3  | 30.7        |            |         | 45.7     | 38.7        |          | 46.6     | 38.3 |
| Progression Factor                | 1.00     | 1.00     | 1.00   | 1.00  | 1.00        |            |         | 1.00     | 1.00        |          | 1.00     | 1.00 |
| Incremental Delay, d2             | 14.9     | 104.7    | 8.6    | 385.6 | 133.3       |            |         | 458.9    | 0.4         |          | 51.4     | 0.0  |
| Delay (s)                         | 70.9     | 137.4    | 36.6   | 439.9 | 164.0       |            |         | 504.7    | 39.2        |          | 98.0     | 38.3 |
| Level of Service                  | Е        | F        | D      | F     | F           |            |         | F        | D           |          | F        | D    |
| Approach Delay (s)                |          | 88.0     |        |       | 194.4       |            |         | 416.5    |             |          | 97.1     |      |
| Approach LOS                      |          | F        |        |       | F           |            |         | F        |             |          | F        |      |
| Intersection Summary              |          |          |        |       |             |            |         |          |             |          |          |      |
| HCM 2000 Control Delay            |          |          | 186.3  | Н     | CM 2000     | Level of S | Service |          | F           |          |          |      |
| HCM 2000 Volume to Capaci         | ty ratio |          | 1.42   |       |             |            |         |          |             |          |          |      |
| Actuated Cycle Length (s)         |          |          | 113.6  |       | um of lost  |            |         |          | 18.0        |          |          |      |
| Intersection Capacity Utilization | on       |          | 121.9% | IC    | CU Level of | of Service |         |          | Н           |          |          |      |
| Analysis Period (min)             |          |          | 15     |       |             |            |         |          |             |          |          |      |
| c Critical Lane Group             |          |          |        |       |             |            |         |          |             |          |          |      |

|                              | ≯     | <b>→</b> | •    | •     | <b>←</b> | •    | •     | <b>†</b>    | ~    | <b>\</b> | <b>↓</b> |      |
|------------------------------|-------|----------|------|-------|----------|------|-------|-------------|------|----------|----------|------|
| Movement                     | EBL   | EBT      | EBR  | WBL   | WBT      | WBR  | NBL   | NBT         | NBR  | SBL      | SBT      | SBR  |
| Lane Configurations          | 14.54 | ^↑       | 7    | ሻ     | <b>^</b> | 7    | ሻሻ    | <b>↑</b> ↑₽ |      | 77       | <b>^</b> | 7    |
| Traffic Volume (veh/h)       | 290   | 505      | 271  | 250   | 397      | 350  | 340   | 699         | 152  | 590      | 1138     | 306  |
| Future Volume (veh/h)        | 290   | 505      | 271  | 250   | 397      | 350  | 340   | 699         | 152  | 590      | 1138     | 306  |
| Number                       | 7     | 4        | 14   | 3     | 8        | 18   | 5     | 2           | 12   | 1        | 6        | 16   |
| Initial Q (Qb), veh          | 0     | 0        | 0    | 0     | 0        | 0    | 0     | 0           | 0    | 0        | 0        | 0    |
| Ped-Bike Adj(A_pbT)          | 1.00  |          | 0.99 | 1.00  |          | 1.00 | 1.00  |             | 1.00 | 1.00     |          | 1.00 |
| Parking Bus, Adj             | 1.00  | 1.00     | 1.00 | 1.00  | 1.00     | 1.00 | 1.00  | 1.00        | 1.00 | 1.00     | 1.00     | 1.00 |
| Adj Sat Flow, veh/h/ln       | 1863  | 1863     | 1863 | 1863  | 1863     | 1863 | 1863  | 1863        | 1900 | 1863     | 1863     | 1863 |
| Adj Flow Rate, veh/h         | 302   | 526      | 282  | 260   | 414      | 365  | 354   | 728         | 158  | 615      | 1185     | 319  |
| Adj No. of Lanes             | 2     | 2        | 1    | 1     | 2        | 1    | 2     | 3           | 0    | 2        | 3        | 1    |
| Peak Hour Factor             | 0.96  | 0.96     | 0.96 | 0.96  | 0.96     | 0.96 | 0.96  | 0.96        | 0.96 | 0.96     | 0.96     | 0.96 |
| Percent Heavy Veh, %         | 2     | 2        | 2    | 2     | 2        | 2    | 2     | 2           | 2    | 2        | 2        | 2    |
| Cap, veh/h                   | 374   | 875      | 535  | 218   | 927      | 413  | 324   | 1153        | 248  | 324      | 1398     | 606  |
| Arrive On Green              | 0.11  | 0.25     | 0.25 | 0.12  | 0.26     | 0.26 | 0.09  | 0.28        | 0.28 | 0.09     | 0.28     | 0.28 |
| Sat Flow, veh/h              | 3442  | 3539     | 1562 | 1774  | 3539     | 1576 | 3442  | 4194        | 900  | 3442     | 5085     | 1580 |
| Grp Volume(v), veh/h         | 302   | 526      | 282  | 260   | 414      | 365  | 354   | 587         | 299  | 615      | 1185     | 319  |
| Grp Sat Flow(s),veh/h/ln     | 1721  | 1770     | 1562 | 1774  | 1770     | 1576 | 1721  | 1695        | 1704 | 1721     | 1695     | 1580 |
| Q Serve(g_s), s              | 5.9   | 9.1      | 10.0 | 8.5   | 6.8      | 15.4 | 6.5   | 10.5        | 10.7 | 6.5      | 15.2     | 10.8 |
| Cycle Q Clear(g_c), s        | 5.9   | 9.1      | 10.0 | 8.5   | 6.8      | 15.4 | 6.5   | 10.5        | 10.7 | 6.5      | 15.2     | 10.8 |
| Prop In Lane                 | 1.00  |          | 1.00 | 1.00  |          | 1.00 | 1.00  |             | 0.53 | 1.00     |          | 1.00 |
| Lane Grp Cap(c), veh/h       | 374   | 875      | 535  | 218   | 927      | 413  | 324   | 932         | 469  | 324      | 1398     | 606  |
| V/C Ratio(X)                 | 0.81  | 0.60     | 0.53 | 1.19  | 0.45     | 0.88 | 1.09  | 0.63        | 0.64 | 1.90     | 0.85     | 0.53 |
| Avail Cap(c_a), veh/h        | 374   | 922      | 556  | 218   | 973      | 433  | 324   | 932         | 469  | 324      | 1398     | 606  |
| HCM Platoon Ratio            | 1.00  | 1.00     | 1.00 | 1.00  | 1.00     | 1.00 | 1.00  | 1.00        | 1.00 | 1.00     | 1.00     | 1.00 |
| Upstream Filter(I)           | 1.00  | 1.00     | 1.00 | 1.00  | 1.00     | 1.00 | 1.00  | 1.00        | 1.00 | 1.00     | 1.00     | 1.00 |
| Uniform Delay (d), s/veh     | 30.1  | 23.0     | 18.3 | 30.3  | 21.3     | 24.5 | 31.3  | 22.0        | 22.0 | 31.3     | 23.7     | 16.4 |
| Incr Delay (d2), s/veh       | 12.4  | 1.0      | 0.8  | 122.2 | 0.3      | 18.5 | 77.4  | 3.2         | 6.5  | 416.1    | 6.5      | 3.2  |
| Initial Q Delay(d3),s/veh    | 0.0   | 0.0      | 0.0  | 0.0   | 0.0      | 0.0  | 0.0   | 0.0         | 0.0  | 0.0      | 0.0      | 0.0  |
| %ile BackOfQ(50%),veh/ln     | 3.5   | 4.6      | 4.4  | 11.5  | 3.3      | 8.8  | 6.5   | 5.3         | 5.8  | 21.8     | 8.0      | 5.2  |
| LnGrp Delay(d),s/veh         | 42.5  | 24.0     | 19.1 | 152.5 | 21.7     | 43.0 | 108.6 | 25.2        | 28.5 | 447.4    | 30.2     | 19.7 |
| LnGrp LOS                    | D     | С        | В    | F     | С        | D    | F     | С           | С    | F        | С        | В    |
| Approach Vol, veh/h          |       | 1110     |      |       | 1039     |      |       | 1240        |      |          | 2119     |      |
| Approach Delay, s/veh        |       | 27.8     |      |       | 61.9     |      |       | 49.8        |      |          | 149.7    |      |
| Approach LOS                 |       | C        |      |       | E        |      |       | D           |      |          | F        |      |
| Timer                        | 1     | 2        | 3    | 4     | 5        | 6    | 7     | 8           |      |          |          |      |
| Assigned Phs                 | 1     | 2        | 3    | 4     | 5        | 6    | 7     | 8           |      |          |          |      |
| Phs Duration (G+Y+Rc), s     | 11.0  | 23.5     | 13.0 | 21.6  | 11.0     | 23.5 | 12.0  | 22.6        |      |          |          |      |
| Change Period (Y+Rc), s      | 4.5   | 4.5      | 4.5  | 4.5   | 4.5      | 4.5  | 4.5   | 4.5         |      |          |          |      |
| Max Green Setting (Gmax), s  | 6.5   | 19.0     | 8.5  | 18.0  | 6.5      | 19.0 | 7.5   | 19.0        |      |          |          |      |
| Max Q Clear Time (g_c+l1), s | 8.5   | 12.7     | 10.5 | 12.0  | 8.5      | 17.2 | 7.9   | 17.4        |      |          |          |      |
| Green Ext Time (p_c), s      | 0.0   | 3.0      | 0.0  | 2.3   | 0.0      | 1.4  | 0.0   | 0.7         |      |          |          |      |
| Intersection Summary         |       |          |      |       |          |      |       |             |      |          |          |      |
| HCM 2010 Ctrl Delay          |       |          | 86.1 |       |          |      |       |             |      |          |          |      |
| HCM 2010 LOS                 |       |          | 00.1 |       |          |      |       |             |      |          |          |      |
| TION ZUTU LUS                |       |          | Г    |       |          |      |       |             |      |          |          |      |

Lico Subdivision Keith Higgins Traffic Engineer

|                              | ۶    | <b>→</b> | •     | •     | <b>←</b> | 4     | 1    | <b>†</b> | ~    | /     | <b>↓</b> | 4    |
|------------------------------|------|----------|-------|-------|----------|-------|------|----------|------|-------|----------|------|
| Movement                     | EBL  | EBT      | EBR   | WBL   | WBT      | WBR   | NBL  | NBT      | NBR  | SBL   | SBT      | SBR  |
| Lane Configurations          | Ž    | f)       |       | ¥     | ĵ.       |       | 7    | <b></b>  | 7    | Ť     | ĥ        |      |
| Traffic Volume (veh/h)       | 25   | 200      | 92    | 295   | 260      | 388   | 67   | 194      | 307  | 299   | 137      | 20   |
| Future Volume (veh/h)        | 25   | 200      | 92    | 295   | 260      | 388   | 67   | 194      | 307  | 299   | 137      | 20   |
| Number                       | 7    | 4        | 14    | 3     | 8        | 18    | 5    | 2        | 12   | 1     | 6        | 16   |
| Initial Q (Qb), veh          | 0    | 0        | 0     | 0     | 0        | 0     | 0    | 0        | 0    | 0     | 0        | 0    |
| Ped-Bike Adj(A_pbT)          | 1.00 |          | 0.95  | 1.00  |          | 0.99  | 1.00 |          | 0.99 | 1.00  |          | 0.99 |
| Parking Bus, Adj             | 1.00 | 1.00     | 1.00  | 1.00  | 1.00     | 1.00  | 1.00 | 1.00     | 1.00 | 1.00  | 1.00     | 1.00 |
| Adj Sat Flow, veh/h/ln       | 1863 | 1863     | 1900  | 1863  | 1863     | 1900  | 1863 | 1863     | 1863 | 1863  | 1863     | 1900 |
| Adj Flow Rate, veh/h         | 29   | 233      | 107   | 343   | 302      | 451   | 78   | 226      | 357  | 348   | 159      | 23   |
| Adj No. of Lanes             | 1    | 1        | 0     | 1     | 1        | 0     | 1    | 1        | 1    | 1     | 1        | 0    |
| Peak Hour Factor             | 0.86 | 0.86     | 0.86  | 0.86  | 0.86     | 0.86  | 0.86 | 0.86     | 0.86 | 0.86  | 0.86     | 0.86 |
| Percent Heavy Veh, %         | 2    | 2        | 2     | 2     | 2        | 2     | 2    | 2        | 2    | 2     | 2        | 2    |
| Cap, veh/h                   | 55   | 279      | 128   | 274   | 241      | 360   | 101  | 507      | 428  | 130   | 460      | 66   |
| Arrive On Green              | 0.03 | 0.24     | 0.24  | 0.15  | 0.36     | 0.36  | 0.06 | 0.27     | 0.27 | 0.07  | 0.29     | 0.29 |
| Sat Flow, veh/h              | 1774 | 1187     | 545   | 1774  | 673      | 1005  | 1774 | 1863     | 1572 | 1774  | 1590     | 230  |
| Grp Volume(v), veh/h         | 29   | 0        | 340   | 343   | 0        | 753   | 78   | 226      | 357  | 348   | 0        | 182  |
| Grp Sat Flow(s), veh/h/ln    | 1774 | 0        | 1732  | 1774  | 0        | 1677  | 1774 | 1863     | 1572 | 1774  | 0        | 1820 |
| Q Serve(g_s), s              | 1.1  | 0.0      | 12.7  | 10.5  | 0.0      | 24.4  | 2.9  | 6.8      | 14.5 | 5.0   | 0.0      | 5.4  |
| Cycle Q Clear(g_c), s        | 1.1  | 0.0      | 12.7  | 10.5  | 0.0      | 24.4  | 2.9  | 6.8      | 14.5 | 5.0   | 0.0      | 5.4  |
| Prop In Lane                 | 1.00 |          | 0.31  | 1.00  |          | 0.60  | 1.00 |          | 1.00 | 1.00  |          | 0.13 |
| Lane Grp Cap(c), veh/h       | 55   | 0        | 407   | 274   | 0        | 601   | 101  | 507      | 428  | 130   | 0        | 526  |
| V/C Ratio(X)                 | 0.53 | 0.00     | 0.83  | 1.25  | 0.00     | 1.25  | 0.78 | 0.45     | 0.83 | 2.67  | 0.00     | 0.35 |
| Avail Cap(c_a), veh/h        | 130  | 0        | 459   | 274   | 0        | 601   | 130  | 507      | 428  | 130   | 0        | 526  |
| HCM Platoon Ratio            | 1.00 | 1.00     | 1.00  | 1.00  | 1.00     | 1.00  | 1.00 | 1.00     | 1.00 | 1.00  | 1.00     | 1.00 |
| Upstream Filter(I)           | 1.00 | 0.00     | 1.00  | 1.00  | 0.00     | 1.00  | 1.00 | 1.00     | 1.00 | 1.00  | 0.00     | 1.00 |
| Uniform Delay (d), s/veh     | 32.4 | 0.0      | 24.7  | 28.7  | 0.0      | 21.8  | 31.6 | 20.5     | 23.3 | 31.5  | 0.0      | 19.1 |
| Incr Delay (d2), s/veh       | 7.6  | 0.0      | 11.5  | 139.8 | 0.0      | 126.7 | 19.2 | 2.8      | 17.3 | 771.8 | 0.0      | 1.8  |
| Initial Q Delay(d3),s/veh    | 0.0  | 0.0      | 0.0   | 0.0   | 0.0      | 0.0   | 0.0  | 0.0      | 0.0  | 0.0   | 0.0      | 0.0  |
| %ile BackOfQ(50%),veh/ln     | 0.6  | 0.0      | 7.3   | 15.7  | 0.0      | 32.4  | 2.0  | 3.9      | 8.3  | 30.4  | 0.0      | 2.9  |
| LnGrp Delay(d),s/veh         | 40.1 | 0.0      | 36.2  | 168.6 | 0.0      | 148.5 | 50.9 | 23.3     | 40.6 | 803.3 | 0.0      | 20.9 |
| LnGrp LOS                    | D    |          | D     | F     |          | F     | D    | С        | D    | F     |          | С    |
| Approach Vol, veh/h          |      | 369      |       |       | 1096     |       |      | 661      |      |       | 530      |      |
| Approach Delay, s/veh        |      | 36.5     |       |       | 154.8    |       |      | 35.9     |      |       | 534.6    |      |
| Approach LOS                 |      | D        |       |       | F        |       |      | D        |      |       | F        |      |
| Timer                        | 1    | 2        | 3     | 4     | 5        | 6     | 7    | 8        |      |       |          |      |
| Assigned Phs                 | 1    | 2        | 3     | 4     | 5        | 6     | 7    | 8        |      |       |          |      |
| Phs Duration (G+Y+Rc), s     | 9.5  | 23.0     | 15.0  | 20.5  | 8.4      | 24.1  | 6.6  | 28.9     |      |       |          |      |
| Change Period (Y+Rc), s      | 4.5  | 4.5      | 4.5   | 4.5   | 4.5      | 4.5   | 4.5  | 4.5      |      |       |          |      |
| Max Green Setting (Gmax), s  | 5.0  | 18.5     | 10.5  | 18.0  | 5.0      | 18.5  | 5.0  | 23.5     |      |       |          |      |
| Max Q Clear Time (g_c+l1), s | 7.0  | 16.5     | 12.5  | 14.7  | 4.9      | 7.4   | 3.1  | 26.4     |      |       |          |      |
| Green Ext Time (p_c), s      | 0.0  | 0.6      | 0.0   | 0.6   | 0.0      | 0.7   | 0.0  | 0.0      |      |       |          |      |
| Intersection Summary         |      |          |       |       |          |       |      |          |      |       |          |      |
| HCM 2010 Ctrl Delay          |      |          | 184.6 |       |          |       |      |          |      |       |          |      |
| HCM 2010 LOS                 |      |          | F     |       |          |       |      |          |      |       |          |      |

|                              | ۶    | <b>→</b> | •    | •    | <b>←</b> | •    | 1    | <b>†</b> | <b>/</b> | <b>/</b> | <b>+</b> | 1    |
|------------------------------|------|----------|------|------|----------|------|------|----------|----------|----------|----------|------|
| Movement                     | EBL  | EBT      | EBR  | WBL  | WBT      | WBR  | NBL  | NBT      | NBR      | SBL      | SBT      | SBR  |
| Lane Configurations          | ň    | <b>^</b> | 7    | ň    | <b>^</b> | 7    | 7    | <b>^</b> | 7        | Ţ        | <b>†</b> | 7    |
| Traffic Volume (veh/h)       | 50   | 289      | 20   | 48   | 594      | 30   | 50   | 5        | 69       | 45       | 5        | 145  |
| Future Volume (veh/h)        | 50   | 289      | 20   | 48   | 594      | 30   | 50   | 5        | 69       | 45       | 5        | 145  |
| Number                       | 7    | 4        | 14   | 3    | 8        | 18   | 5    | 2        | 12       | 1        | 6        | 16   |
| Initial Q (Qb), veh          | 0    | 0        | 0    | 0    | 0        | 0    | 0    | 0        | 0        | 0        | 0        | 0    |
| Ped-Bike Adj(A_pbT)          | 1.00 |          | 1.00 | 1.00 |          | 1.00 | 1.00 |          | 1.00     | 1.00     |          | 1.00 |
| Parking Bus, Adj             | 1.00 | 1.00     | 1.00 | 1.00 | 1.00     | 1.00 | 1.00 | 1.00     | 1.00     | 1.00     | 1.00     | 1.00 |
| Adj Sat Flow, veh/h/ln       | 1759 | 1759     | 1759 | 1827 | 1827     | 1827 | 1863 | 1863     | 1863     | 1845     | 1845     | 1845 |
| Adj Flow Rate, veh/h         | 53   | 304      | 21   | 51   | 625      | 32   | 53   | 5        | 73       | 47       | 5        | 153  |
| Adj No. of Lanes             | 1    | 2        | 1    | 1    | 2        | 1    | 1    | 1        | 1        | 1        | 1        | 1    |
| Peak Hour Factor             | 0.95 | 0.95     | 0.95 | 0.95 | 0.95     | 0.95 | 0.95 | 0.95     | 0.95     | 0.95     | 0.95     | 0.95 |
| Percent Heavy Veh, %         | 8    | 8        | 8    | 4    | 4        | 4    | 2    | 2        | 2        | 3        | 3        | 3    |
| Cap, veh/h                   | 99   | 1108     | 495  | 100  | 1145     | 512  | 442  | 321      | 273      | 456      | 318      | 270  |
| Arrive On Green              | 0.06 | 0.33     | 0.33 | 0.06 | 0.33     | 0.33 | 0.17 | 0.17     | 0.17     | 0.17     | 0.17     | 0.17 |
| Sat Flow, veh/h              | 1675 | 3343     | 1493 | 1740 | 3471     | 1553 | 1223 | 1863     | 1583     | 1303     | 1845     | 1568 |
| Grp Volume(v), veh/h         | 53   | 304      | 21   | 51   | 625      | 32   | 53   | 5        | 73       | 47       | 5        | 153  |
| Grp Sat Flow(s),veh/h/ln     | 1675 | 1671     | 1493 | 1740 | 1736     | 1553 | 1223 | 1863     | 1583     | 1303     | 1845     | 1568 |
| Q Serve(g_s), s              | 0.9  | 2.1      | 0.3  | 0.9  | 4.5      | 0.4  | 1.2  | 0.1      | 1.2      | 1.0      | 0.1      | 2.8  |
| Cycle Q Clear(g_c), s        | 0.9  | 2.1      | 0.3  | 0.9  | 4.5      | 0.4  | 1.2  | 0.1      | 1.2      | 1.0      | 0.1      | 2.8  |
| Prop In Lane                 | 1.00 |          | 1.00 | 1.00 |          | 1.00 | 1.00 |          | 1.00     | 1.00     |          | 1.00 |
| Lane Grp Cap(c), veh/h       | 99   | 1108     | 495  | 100  | 1145     | 512  | 442  | 321      | 273      | 456      | 318      | 270  |
| V/C Ratio(X)                 | 0.53 | 0.27     | 0.04 | 0.51 | 0.55     | 0.06 | 0.12 | 0.02     | 0.27     | 0.10     | 0.02     | 0.57 |
| Avail Cap(c_a), veh/h        | 354  | 2117     | 946  | 367  | 2199     | 984  | 1046 | 1241     | 1054     | 1099     | 1228     | 1044 |
| HCM Platoon Ratio            | 1.00 | 1.00     | 1.00 | 1.00 | 1.00     | 1.00 | 1.00 | 1.00     | 1.00     | 1.00     | 1.00     | 1.00 |
| Upstream Filter(I)           | 1.00 | 1.00     | 1.00 | 1.00 | 1.00     | 1.00 | 1.00 | 1.00     | 1.00     | 1.00     | 1.00     | 1.00 |
| Uniform Delay (d), s/veh     | 14.1 | 7.6      | 7.0  | 14.1 | 8.4      | 7.1  | 11.1 | 10.6     | 11.0     | 11.0     | 10.6     | 11.7 |
| Incr Delay (d2), s/veh       | 4.4  | 0.1      | 0.0  | 4.0  | 0.4      | 0.1  | 0.1  | 0.0      | 0.5      | 0.1      | 0.0      | 1.9  |
| Initial Q Delay(d3),s/veh    | 0.0  | 0.0      | 0.0  | 0.0  | 0.0      | 0.0  | 0.0  | 0.0      | 0.0      | 0.0      | 0.0      | 0.0  |
| %ile BackOfQ(50%),veh/ln     | 0.5  | 0.9      | 0.1  | 0.5  | 2.2      | 0.2  | 0.4  | 0.0      | 0.6      | 0.4      | 0.0      | 1.3  |
| LnGrp Delay(d),s/veh         | 18.5 | 7.7      | 7.0  | 18.1 | 8.8      | 7.1  | 11.2 | 10.6     | 11.6     | 11.1     | 10.6     | 13.5 |
| LnGrp LOS                    | В    | Α        | Α    | В    | Α        | Α    | В    | В        | В        | В        | В        | В    |
| Approach Vol, veh/h          |      | 378      |      |      | 708      |      |      | 131      |          |          | 205      |      |
| Approach Delay, s/veh        |      | 9.2      |      |      | 9.4      |      |      | 11.4     |          |          | 12.9     |      |
| Approach LOS                 |      | Α        |      |      | Α        |      |      | В        |          |          | В        |      |
| Timer                        | 1    | 2        | 3    | 4    | 5        | 6    | 7    | 8        |          |          |          |      |
| Assigned Phs                 |      | 2        | 3    | 4    |          | 6    | 7    | 8        |          |          |          |      |
| Phs Duration (G+Y+Rc), s     |      | 9.8      | 6.3  | 14.7 |          | 9.8  | 6.3  | 14.7     |          |          |          |      |
| Change Period (Y+Rc), s      |      | 4.5      | 4.5  | 4.5  |          | 4.5  | 4.5  | 4.5      |          |          |          |      |
| Max Green Setting (Gmax), s  |      | 20.5     | 6.5  | 19.5 |          | 20.5 | 6.5  | 19.5     |          |          |          |      |
| Max Q Clear Time (g_c+l1), s |      | 3.2      | 2.9  | 4.1  |          | 4.8  | 2.9  | 6.5      |          |          |          |      |
| Green Ext Time (p_c), s      |      | 0.3      | 0.0  | 1.7  |          | 0.6  | 0.0  | 3.6      |          |          |          |      |
| Intersection Summary         |      |          |      |      |          |      |      |          |          |          |          |      |
| HCM 2010 Ctrl Delay          |      |          | 10.0 |      |          |      |      |          |          |          |          |      |
| HCM 2010 LOS                 |      |          | В    |      |          |      |      |          |          |          |          |      |

| Int Delay, s/veh         3.9           Movement         WBL         WBR         NBT         NBR         SBL         SB           Lane Configurations         Y         Image: Configuration of the configuration o |
|--|
| Movement         WBL         WBR         NBT         NBR         SBL         SB           Lane Configurations         Y         L         Y  |
| Lane Configurations       Y       Langle Configurations       A       A       A       A       A       A       B       A       B       A       B  |
| Traffic Vol, veh/h 38 142 315 36 39 19<br>Future Vol, veh/h 38 142 315 36 39 19  |
| Future Vol, veh/h 38 142 315 36 39 19  |
| ·  |
| Confidence reas, #/fil 0 0 0 1 1   |
| Sign Control Stop Stop Free Free Free Free   |
|  |
|  |
| Clorago Longin 0 100   |
| Veh in Median Storage, # 0 - 0   |
| Grade, % 0 - 0   |
| Peak Hour Factor 86 86 86 86 86 8  |
| Heavy Vehicles, % 2 2 7 7 7  |
| Mvmt Flow 44 165 366 42 45 22  |
|  |
| Major/Minor Minor1 Major1 Major2   |
| Conflicting Flow All 705 388 0 0 409   |
| Stage 1 388  |
| Stage 2 317  |
| Critical Hdwy 6.42 6.22 4.17   |
| Critical Hdwy Stg 1 5.42   |
| Critical Hdwy Stg 2 5.42   |
| Follow-up Hdwy 3.518 3.318 2.263   |
| Pot Cap-1 Maneuver 403 660 1123  |
| Stage 1 686  |
| Stage 2 738  |
| Platoon blocked, %   |
|  |
|  |
| Mov Cap-2 Maneuver 386   |
| Stage 1 658  |
| Stage 2 738  |
|  |
| Approach WB NB SB  |
| HCM Control Delay, s 14.9 0 1.4  |
| HCM LOS B  |
|  |
| M. I M. M. C. NOT MEDIATE  |
| Minor Lane/Major Mvmt NBT NBRWBLn1 SBL SB  |
| Capacity (veh/h) 573 1122  |
| HCM Lane V/C Ratio 0.365 0.04  |
| HCM Control Delay (s) 14.9 8.3   |
|  |
| HCM Lane LOS B A HCM 95th %tile Q(veh) 1.7 0.1   |

| Intersection               |           |       |         |       |      |      |
|----------------------------|-----------|-------|---------|-------|------|------|
| Intersection Delay, s/veh  | 12.2      |       |         |       |      |      |
| Intersection Delay, s/ven  | 12.2<br>B |       |         |       |      |      |
| IIILEISECLIOII LOS         | D         |       |         |       |      |      |
|                            |           |       |         |       |      |      |
| Movement                   | WBL       | WBR   | NBT     | NBR   | SBL  | SBT  |
| Lane Configurations        | **        |       | ₽       |       |      | र्स  |
| Traffic Vol, veh/h         | 38        | 142   | 315     | 36    | 39   | 195  |
| Future Vol, veh/h          | 38        | 142   | 315     | 36    | 39   | 195  |
| Peak Hour Factor           | 0.86      | 0.86  | 0.86    | 0.86  | 0.86 | 0.86 |
| Heavy Vehicles, %          | 2         | 2     | 7       | 7     | 7    | 7    |
| Mvmt Flow                  | 44        | 165   | 366     | 42    | 45   | 227  |
| Number of Lanes            | 1         | 0     | 1       | 0     | 0    | 1    |
| Approach                   | WB        |       | NB      |       | SB   |      |
| Opposing Approach          | 115       |       | SB      |       | NB   |      |
| Opposing Lanes             | 0         |       | 1       |       | 1    |      |
| Conflicting Approach Left  | NB        |       |         |       | WB   |      |
| Conflicting Lanes Left     | 1         |       | 0       |       | 1    |      |
| Conflicting Approach Right | SB        |       | WB      |       |      |      |
| Conflicting Lanes Right    | 1         |       | 1       |       | 0    |      |
| HCM Control Delay          | 10.3      |       | 13.7    |       | 11.3 |      |
| HCM LOS                    | 10.3      |       | В       |       | В    |      |
| HOW LOO                    |           |       | D       |       | ט    |      |
|                            |           | NDL   | 14/D; ć | 001 1 |      |      |
| Lane                       |           | NBLn1 | WBLn1   | SBLn1 |      |      |
| Vol Left, %                |           | 0%    | 21%     | 17%   |      |      |
| Vol Thru, %                |           | 90%   | 0%      | 83%   |      |      |
| Vol Right, %               |           | 10%   | 79%     | 0%    |      |      |
| Sign Control               |           | Stop  | Stop    | Stop  |      |      |
| Traffic Vol by Lane        |           | 351   | 180     | 234   |      |      |
| LT Vol                     |           | 0     | 38      | 39    |      |      |
| Through Vol                |           | 315   | 0       | 195   |      |      |
| RT Vol                     |           | 36    | 142     | 0     |      |      |
| Lane Flow Rate             |           | 408   | 209     | 272   |      |      |
| Geometry Grp               |           | 1     | 1       | 1     |      |      |
| Degree of Util (X)         |           | 0.547 | 0.295   | 0.383 |      |      |
| Departure Headway (Hd)     |           | 4.829 | 5.078   | 5.072 |      |      |
| Convergence, Y/N           |           | Yes   | Yes     | Yes   |      |      |
| Сар                        |           | 739   | 699     | 702   |      |      |
| Service Time               |           | 2.907 | 3.17    | 3.16  |      |      |
| HCM Lane V/C Ratio         |           | 0.552 | 0.299   | 0.387 |      |      |
| HCM Control Delay          |           | 13.7  | 10.3    | 11.3  |      |      |
| HCM Lane LOS               |           | В     | В       | В     |      |      |
| HOW Lake LOS               |           | D     | D       | D     |      |      |

3.4

1.2

1.8

HCM 95th-tile Q

|                              | ۶    | <b>→</b> | •    | •    | <b>←</b> | •    | 1    | <b>†</b> | <i>&gt;</i> | <b>/</b> | <b></b>  | 1    |
|------------------------------|------|----------|------|------|----------|------|------|----------|-------------|----------|----------|------|
| Movement                     | EBL  | EBT      | EBR  | WBL  | WBT      | WBR  | NBL  | NBT      | NBR         | SBL      | SBT      | SBR  |
| Lane Configurations          | 7    | <b>^</b> | 7    | 7    | ħβ       |      | 7    | <b>^</b> | 7           | ሻ        | <b>^</b> | 7    |
| Traffic Volume (veh/h)       | 259  | 212      | 142  | 32   | 454      | 315  | 314  | 433      | 42          | 130      | 185      | 219  |
| Future Volume (veh/h)        | 259  | 212      | 142  | 32   | 454      | 315  | 314  | 433      | 42          | 130      | 185      | 219  |
| Number                       | 7    | 4        | 14   | 3    | 8        | 18   | 5    | 2        | 12          | 1        | 6        | 16   |
| Initial Q (Qb), veh          | 0    | 0        | 0    | 0    | 0        | 0    | 0    | 0        | 0           | 0        | 0        | 0    |
| Ped-Bike Adj(A_pbT)          | 1.00 |          | 1.00 | 1.00 |          | 1.00 | 1.00 |          | 1.00        | 1.00     |          | 1.00 |
| Parking Bus, Adj             | 1.00 | 1.00     | 1.00 | 1.00 | 1.00     | 1.00 | 1.00 | 1.00     | 1.00        | 1.00     | 1.00     | 1.00 |
| Adj Sat Flow, veh/h/ln       | 1776 | 1776     | 1776 | 1863 | 1863     | 1900 | 1863 | 1863     | 1863        | 1827     | 1827     | 1827 |
| Adj Flow Rate, veh/h         | 276  | 226      | 151  | 34   | 483      | 335  | 334  | 461      | 45          | 138      | 197      | 233  |
| Adj No. of Lanes             | 1    | 2        | 1    | 1    | 2        | 0    | 1    | 2        | 1           | 1        | 2        | 1    |
| Peak Hour Factor             | 0.94 | 0.94     | 0.94 | 0.94 | 0.94     | 0.94 | 0.94 | 0.94     | 0.94        | 0.94     | 0.94     | 0.94 |
| Percent Heavy Veh, %         | 7    | 7        | 7    | 2    | 2        | 2    | 2    | 2        | 2           | 4        | 4        | 4    |
| Cap, veh/h                   | 306  | 1273     | 881  | 85   | 489      | 338  | 366  | 1083     | 484         | 168      | 681      | 305  |
| Arrive On Green              | 0.18 | 0.38     | 0.38 | 0.05 | 0.24     | 0.24 | 0.21 | 0.31     | 0.31        | 0.10     | 0.20     | 0.20 |
| Sat Flow, veh/h              | 1691 | 3374     | 1508 | 1774 | 2003     | 1385 | 1774 | 3539     | 1583        | 1740     | 3471     | 1553 |
| Grp Volume(v), veh/h         | 276  | 226      | 151  | 34   | 427      | 391  | 334  | 461      | 45          | 138      | 197      | 233  |
| Grp Sat Flow(s),veh/h/ln     | 1691 | 1687     | 1508 | 1774 | 1770     | 1618 | 1774 | 1770     | 1583        | 1740     | 1736     | 1553 |
| Q Serve(g_s), s              | 16.7 | 4.7      | 4.8  | 1.9  | 25.1     | 25.2 | 19.2 | 10.9     | 2.1         | 8.1      | 5.1      | 14.8 |
| Cycle Q Clear(g_c), s        | 16.7 | 4.7      | 4.8  | 1.9  | 25.1     | 25.2 | 19.2 | 10.9     | 2.1         | 8.1      | 5.1      | 14.8 |
| Prop In Lane                 | 1.00 |          | 1.00 | 1.00 |          | 0.86 | 1.00 |          | 1.00        | 1.00     |          | 1.00 |
| Lane Grp Cap(c), veh/h       | 306  | 1273     | 881  | 85   | 432      | 395  | 366  | 1083     | 484         | 168      | 681      | 305  |
| V/C Ratio(X)                 | 0.90 | 0.18     | 0.17 | 0.40 | 0.99     | 0.99 | 0.91 | 0.43     | 0.09        | 0.82     | 0.29     | 0.76 |
| Avail Cap(c_a), veh/h        | 348  | 1314     | 899  | 107  | 432      | 395  | 416  | 1083     | 484         | 273      | 681      | 305  |
| HCM Platoon Ratio            | 1.00 | 1.00     | 1.00 | 1.00 | 1.00     | 1.00 | 1.00 | 1.00     | 1.00        | 1.00     | 1.00     | 1.00 |
| Upstream Filter(I)           | 1.00 | 1.00     | 1.00 | 1.00 | 1.00     | 1.00 | 1.00 | 1.00     | 1.00        | 1.00     | 1.00     | 1.00 |
| Uniform Delay (d), s/veh     | 41.9 | 21.7     | 10.1 | 48.3 | 39.4     | 39.4 | 40.5 | 28.9     | 25.9        | 46.3     | 35.8     | 39.7 |
| Incr Delay (d2), s/veh       | 23.6 | 0.1      | 0.1  | 3.0  | 40.0     | 42.9 | 22.4 | 1.2      | 0.4         | 9.8      | 1.1      | 16.6 |
| Initial Q Delay(d3),s/veh    | 0.0  | 0.0      | 0.0  | 0.0  | 0.0      | 0.0  | 0.0  | 0.0      | 0.0         | 0.0      | 0.0      | 0.0  |
| %ile BackOfQ(50%),veh/ln     | 9.8  | 2.2      | 2.0  | 1.0  | 17.0     | 15.9 | 11.7 | 5.5      | 1.0         | 4.4      | 2.5      | 7.7  |
| LnGrp Delay(d),s/veh         | 65.5 | 21.8     | 10.2 | 51.3 | 79.4     | 82.3 | 63.0 | 30.2     | 26.3        | 56.1     | 36.9     | 56.3 |
| LnGrp LOS                    | Е    | С        | В    | D    | Е        | F    | Е    | С        | С           | Е        | D        | Е    |
| Approach Vol, veh/h          |      | 653      |      |      | 852      |      |      | 840      |             |          | 568      |      |
| Approach Delay, s/veh        |      | 37.6     |      |      | 79.6     |      |      | 43.0     |             |          | 49.5     |      |
| Approach LOS                 |      | D        |      |      | Е        |      |      | D        |             |          | D        |      |
| Timer                        | 1    | 2        | 3    | 4    | 5        | 6    | 7    | 8        |             |          |          |      |
| Assigned Phs                 | 1    | 2        | 3    | 4    | 5        | 6    | 7    | 8        |             |          |          |      |
| Phs Duration (G+Y+Rc), s     | 14.6 | 36.5     | 9.5  | 43.9 | 26.1     | 25.0 | 23.4 | 30.0     |             |          |          |      |
| Change Period (Y+Rc), s      | 4.5  | 4.5      | 4.5  | 4.5  | 4.5      | 4.5  | 4.5  | 4.5      |             |          |          |      |
| Max Green Setting (Gmax), s  | 16.4 | 28.6     | 6.3  | 40.7 | 24.5     | 20.5 | 21.5 | 25.5     |             |          |          |      |
| Max Q Clear Time (g_c+l1), s | 10.1 | 12.9     | 3.9  | 6.8  | 21.2     | 16.8 | 18.7 | 27.2     |             |          |          |      |
| Green Ext Time (p_c), s      | 0.2  | 2.9      | 0.0  | 2.1  | 0.3      | 0.7  | 0.2  | 0.0      |             |          |          |      |
| Intersection Summary         |      |          |      |      |          |      |      |          |             |          |          |      |
| HCM 2010 Ctrl Delay          |      |          | 53.8 |      |          |      |      |          |             |          |          |      |
| HCM 2010 LOS                 |      |          | D    |      |          |      |      |          |             |          |          |      |
|                              |      |          |      |      |          |      |      |          |             |          |          |      |

|                              | •    | <b>→</b> | •    | •        | <b>←</b>   | •    | •    | †    | <i>&gt;</i> | <b>\</b> | <b>+</b> | ✓    |
|------------------------------|------|----------|------|----------|------------|------|------|------|-------------|----------|----------|------|
| Movement                     | EBL  | EBT      | EBR  | WBL      | WBT        | WBR  | NBL  | NBT  | NBR         | SBL      | SBT      | SBR  |
| Lane Configurations          | 7    | ħβ       |      | <b>ነ</b> | <b>ተ</b> ኈ |      |      | 4    |             |          | 4        |      |
| Traffic Volume (veh/h)       | 35   | 406      | 131  | 105      | 857        | 25   | 215  | 76   | 169         | 38       | 28       | 52   |
| Future Volume (veh/h)        | 35   | 406      | 131  | 105      | 857        | 25   | 215  | 76   | 169         | 38       | 28       | 52   |
| Number                       | 7    | 4        | 14   | 3        | 8          | 18   | 5    | 2    | 12          | 1        | 6        | 16   |
| Initial Q (Qb), veh          | 0    | 0        | 0    | 0        | 0          | 0    | 0    | 0    | 0           | 0        | 0        | 0    |
| Ped-Bike Adj(A_pbT)          | 1.00 |          | 1.00 | 1.00     |            | 1.00 | 1.00 |      | 1.00        | 1.00     |          | 1.00 |
| Parking Bus, Adj             | 1.00 | 1.00     | 1.00 | 1.00     | 1.00       | 1.00 | 1.00 | 1.00 | 1.00        | 1.00     | 1.00     | 1.00 |
| Adj Sat Flow, veh/h/ln       | 1827 | 1827     | 1900 | 1845     | 1845       | 1900 | 1900 | 1810 | 1900        | 1900     | 1776     | 1900 |
| Adj Flow Rate, veh/h         | 39   | 451      | 146  | 117      | 952        | 28   | 239  | 84   | 188         | 42       | 31       | 58   |
| Adj No. of Lanes             | 1    | 2        | 0    | 1        | 2          | 0    | 0    | 1    | 0           | 0        | 1        | 0    |
| Peak Hour Factor             | 0.90 | 0.90     | 0.90 | 0.90     | 0.90       | 0.90 | 0.90 | 0.90 | 0.90        | 0.90     | 0.90     | 0.90 |
| Percent Heavy Veh, %         | 4    | 4        | 4    | 3        | 3          | 3    | 5    | 5    | 5           | 7        | 7        | 7    |
| Cap, veh/h                   | 69   | 701      | 225  | 149      | 1100       | 32   | 360  | 118  | 228         | 232      | 177      | 264  |
| Arrive On Green              | 0.04 | 0.27     | 0.27 | 0.08     | 0.32       | 0.32 | 0.42 | 0.42 | 0.42        | 0.42     | 0.42     | 0.42 |
| Sat Flow, veh/h              | 1740 | 2586     | 830  | 1757     | 3477       | 102  | 647  | 279  | 539         | 365      | 419      | 623  |
| Grp Volume(v), veh/h         | 39   | 302      | 295  | 117      | 480        | 500  | 511  | 0    | 0           | 131      | 0        | 0    |
| Grp Sat Flow(s),veh/h/ln     | 1740 | 1736     | 1680 | 1757     | 1752       | 1827 | 1466 | 0    | 0           | 1406     | 0        | 0    |
| Q Serve(g_s), s              | 1.3  | 9.4      | 9.5  | 4.0      | 15.8       | 15.8 | 15.6 | 0.0  | 0.0         | 0.0      | 0.0      | 0.0  |
| Cycle Q Clear(g_c), s        | 1.3  | 9.4      | 9.5  | 4.0      | 15.8       | 15.8 | 18.6 | 0.0  | 0.0         | 3.0      | 0.0      | 0.0  |
| Prop In Lane                 | 1.00 |          | 0.49 | 1.00     |            | 0.06 | 0.47 |      | 0.37        | 0.32     |          | 0.44 |
| Lane Grp Cap(c), veh/h       | 69   | 470      | 455  | 149      | 554        | 578  | 707  | 0    | 0           | 673      | 0        | 0    |
| V/C Ratio(X)                 | 0.57 | 0.64     | 0.65 | 0.78     | 0.87       | 0.87 | 0.72 | 0.00 | 0.00        | 0.19     | 0.00     | 0.00 |
| Avail Cap(c_a), veh/h        | 145  | 522      | 505  | 207      | 587        | 612  | 707  | 0    | 0           | 673      | 0        | 0    |
| HCM Platoon Ratio            | 1.00 | 1.00     | 1.00 | 1.00     | 1.00       | 1.00 | 1.00 | 1.00 | 1.00        | 1.00     | 1.00     | 1.00 |
| Upstream Filter(I)           | 1.00 | 1.00     | 1.00 | 1.00     | 1.00       | 1.00 | 1.00 | 0.00 | 0.00        | 1.00     | 0.00     | 0.00 |
| Uniform Delay (d), s/veh     | 28.9 | 19.7     | 19.7 | 27.4     | 19.7       | 19.7 | 15.3 | 0.0  | 0.0         | 11.1     | 0.0      | 0.0  |
| Incr Delay (d2), s/veh       | 7.1  | 2.3      | 2.5  | 12.4     | 12.4       | 11.9 | 6.3  | 0.0  | 0.0         | 0.6      | 0.0      | 0.0  |
| Initial Q Delay(d3),s/veh    | 0.0  | 0.0      | 0.0  | 0.0      | 0.0        | 0.0  | 0.0  | 0.0  | 0.0         | 0.0      | 0.0      | 0.0  |
| %ile BackOfQ(50%),veh/ln     | 8.0  | 4.7      | 4.7  | 2.4      | 9.5        | 9.8  | 8.8  | 0.0  | 0.0         | 1.5      | 0.0      | 0.0  |
| LnGrp Delay(d),s/veh         | 36.0 | 22.0     | 22.2 | 39.8     | 32.1       | 31.6 | 21.6 | 0.0  | 0.0         | 11.7     | 0.0      | 0.0  |
| LnGrp LOS                    | D    | С        | С    | D        | С          | С    | С    |      |             | В        |          |      |
| Approach Vol, veh/h          |      | 636      |      |          | 1097       |      |      | 511  |             |          | 131      |      |
| Approach Delay, s/veh        |      | 22.9     |      |          | 32.7       |      |      | 21.6 |             |          | 11.7     |      |
| Approach LOS                 |      | С        |      |          | С          |      |      | С    |             |          | В        |      |
| Timer                        | 1    | 2        | 3    | 4        | 5          | 6    | 7    | 8    |             |          |          |      |
| Assigned Phs                 |      | 2        | 3    | 4        |            | 6    | 7    | 8    |             |          |          |      |
| Phs Duration (G+Y+Rc), s     |      | 30.4     | 9.7  | 21.1     |            | 30.4 | 6.9  | 23.9 |             |          |          |      |
| Change Period (Y+Rc), s      |      | 4.5      | 4.5  | 4.5      |            | 4.5  | 4.5  | 4.5  |             |          |          |      |
| Max Green Setting (Gmax), s  |      | 25.9     | 7.2  | 18.4     |            | 25.9 | 5.1  | 20.5 |             |          |          |      |
| Max Q Clear Time (g_c+l1), s |      | 20.6     | 6.0  | 11.5     |            | 5.0  | 3.3  | 17.8 |             |          |          |      |
| Green Ext Time (p_c), s      |      | 1.6      | 0.0  | 2.1      |            | 0.7  | 0.0  | 1.6  |             |          |          |      |
| Intersection Summary         |      |          |      |          |            |      |      |      |             |          |          |      |
| HCM 2010 Ctrl Delay          |      |          | 26.5 |          |            |      |      |      |             |          |          |      |
| HCM 2010 LOS                 |      |          | С    |          |            |      |      |      |             |          |          |      |
|                              |      |          |      |          |            |      |      |      |             |          |          |      |

|                              | ۶    | <b>→</b> | •    | •        | <b>←</b> | •    | 1    | <b>†</b> | <b>/</b> | <b>/</b> | <b></b> | 4    |
|------------------------------|------|----------|------|----------|----------|------|------|----------|----------|----------|---------|------|
| Movement                     | EBL  | EBT      | EBR  | WBL      | WBT      | WBR  | NBL  | NBT      | NBR      | SBL      | SBT     | SBR  |
| Lane Configurations          | ሻ    | <b>^</b> | 7    | <b>ነ</b> | <b>^</b> | 7    | ሻሻ   | <b>₽</b> |          | ሻ        | ₽       |      |
| Traffic Volume (veh/h)       | 15   | 650      | 496  | 75       | 1050     | 30   | 889  | 30       | 75       | 55       | 25      | 10   |
| Future Volume (veh/h)        | 15   | 650      | 496  | 75       | 1050     | 30   | 889  | 30       | 75       | 55       | 25      | 10   |
| Number                       | 7    | 4        | 14   | 3        | 8        | 18   | 5    | 2        | 12       | 1        | 6       | 16   |
| Initial Q (Qb), veh          | 0    | 0        | 0    | 0        | 0        | 0    | 0    | 0        | 0        | 0        | 0       | 0    |
| Ped-Bike Adj(A_pbT)          | 1.00 |          | 1.00 | 1.00     |          | 1.00 | 1.00 |          | 1.00     | 1.00     |         | 1.00 |
| Parking Bus, Adj             | 1.00 | 1.00     | 1.00 | 1.00     | 1.00     | 1.00 | 1.00 | 1.00     | 1.00     | 1.00     | 1.00    | 1.00 |
| Adj Sat Flow, veh/h/ln       | 1696 | 1696     | 1696 | 1624     | 1624     | 1624 | 1863 | 1863     | 1900     | 1810     | 1810    | 1900 |
| Adj Flow Rate, veh/h         | 16   | 677      | 517  | 78       | 1094     | 31   | 926  | 31       | 78       | 57       | 26      | 10   |
| Adj No. of Lanes             | 1    | 2        | 1    | 1        | 2        | 1    | 2    | 1        | 0        | 1        | 1       | 0    |
| Peak Hour Factor             | 0.96 | 0.96     | 0.96 | 0.96     | 0.96     | 0.96 | 0.96 | 0.96     | 0.96     | 0.96     | 0.96    | 0.96 |
| Percent Heavy Veh, %         | 12   | 12       | 12   | 17       | 17       | 17   | 2    | 2        | 2        | 5        | 5       | 5    |
| Cap, veh/h                   | 30   | 1185     | 958  | 96       | 1269     | 568  | 1021 | 139      | 350      | 103      | 74      | 28   |
| Arrive On Green              | 0.02 | 0.37     | 0.37 | 0.06     | 0.41     | 0.41 | 0.30 | 0.30     | 0.30     | 0.06     | 0.06    | 0.06 |
| Sat Flow, veh/h              | 1616 | 3223     | 1442 | 1547     | 3085     | 1380 | 3442 | 470      | 1184     | 1723     | 1246    | 479  |
| Grp Volume(v), veh/h         | 16   | 677      | 517  | 78       | 1094     | 31   | 926  | 0        | 109      | 57       | 0       | 36   |
| Grp Sat Flow(s),veh/h/ln     | 1616 | 1612     | 1442 | 1547     | 1543     | 1380 | 1721 | 0        | 1654     | 1723     | 0       | 1725 |
| Q Serve(g_s), s              | 0.8  | 14.1     | 15.7 | 4.2      | 27.1     | 1.1  | 21.7 | 0.0      | 4.2      | 2.7      | 0.0     | 1.7  |
| Cycle Q Clear(g_c), s        | 0.8  | 14.1     | 15.7 | 4.2      | 27.1     | 1.1  | 21.7 | 0.0      | 4.2      | 2.7      | 0.0     | 1.7  |
| Prop In Lane                 | 1.00 |          | 1.00 | 1.00     |          | 1.00 | 1.00 |          | 0.72     | 1.00     |         | 0.28 |
| Lane Grp Cap(c), veh/h       | 30   | 1185     | 958  | 96       | 1269     | 568  | 1021 | 0        | 490      | 103      | 0       | 102  |
| V/C Ratio(X)                 | 0.53 | 0.57     | 0.54 | 0.81     | 0.86     | 0.05 | 0.91 | 0.00     | 0.22     | 0.55     | 0.00    | 0.35 |
| Avail Cap(c_a), veh/h        | 96   | 1185     | 958  | 199      | 1269     | 568  | 1087 | 0        | 497      | 150      | 0       | 123  |
| HCM Platoon Ratio            | 1.00 | 1.00     | 1.00 | 1.00     | 1.00     | 1.00 | 1.00 | 1.00     | 1.00     | 1.00     | 1.00    | 1.00 |
| Upstream Filter(I)           | 1.00 | 1.00     | 1.00 | 1.00     | 1.00     | 1.00 | 1.00 | 0.00     | 1.00     | 1.00     | 0.00    | 1.00 |
| Uniform Delay (d), s/veh     | 40.8 | 21.2     | 7.4  | 38.8     | 22.5     | 14.9 | 28.4 | 0.0      | 22.3     | 38.4     | 0.0     | 37.9 |
| Incr Delay (d2), s/veh       | 13.9 | 2.0      | 2.2  | 14.7     | 7.9      | 0.2  | 10.6 | 0.0      | 0.2      | 4.6      | 0.0     | 2.1  |
| Initial Q Delay(d3),s/veh    | 0.0  | 0.0      | 0.0  | 0.0      | 0.0      | 0.0  | 0.0  | 0.0      | 0.0      | 0.0      | 0.0     | 0.0  |
| %ile BackOfQ(50%),veh/ln     | 0.5  | 6.5      | 6.8  | 2.2      | 12.8     | 0.5  | 11.8 | 0.0      | 1.9      | 1.4      | 0.0     | 0.9  |
| LnGrp Delay(d),s/veh         | 54.7 | 23.2     | 9.6  | 53.6     | 30.4     | 15.1 | 39.0 | 0.0      | 22.5     | 43.0     | 0.0     | 40.0 |
| LnGrp LOS                    | D    | С        | Α    | D        | С        | В    | D    |          | С        | D        |         | D    |
| Approach Vol, veh/h          |      | 1210     |      |          | 1203     |      |      | 1035     |          |          | 93      |      |
| Approach Delay, s/veh        |      | 17.8     |      |          | 31.5     |      |      | 37.2     |          |          | 41.8    |      |
| Approach LOS                 |      | В        |      |          | С        |      |      | D        |          |          | D       |      |
| Timer                        | 1    | 2        | 3    | 4        | 5        | 6    | 7    | 8        |          |          |         |      |
| Assigned Phs                 | 1    | 2        | 3    | 4        | 5        | 6    | 7    | 8        |          |          |         |      |
| Phs Duration (G+Y+Rc), s     | 9.5  | 29.3     | 9.7  | 35.3     | 29.4     | 9.5  | 6.1  | 39.0     |          |          |         |      |
| Change Period (Y+Rc), s      | 4.5  | 4.5      | 4.5  | 4.5      | 4.5      | 4.5  | 4.5  | 4.5      |          |          |         |      |
| Max Green Setting (Gmax), s  | 7.3  | 25.2     | 10.8 | 28.7     | 26.5     | 6.0  | 5.0  | 34.5     |          |          |         |      |
| Max Q Clear Time (g_c+l1), s | 4.7  | 6.2      | 6.2  | 17.7     | 23.7     | 3.7  | 2.8  | 29.1     |          |          |         |      |
| Green Ext Time (p_c), s      | 0.0  | 0.5      | 0.1  | 5.1      | 1.2      | 0.0  | 0.0  | 3.4      |          |          |         |      |
| Intersection Summary         |      |          |      |          |          |      |      |          |          |          |         |      |
| HCM 2010 Ctrl Delay          |      |          | 28.8 |          |          |      |      |          |          |          |         |      |
| HCM 2010 LOS                 |      |          | С    |          |          |      |      |          |          |          |         |      |

| Movement Lane Configurations Traffic Volume (veh/h) Future Volume (veh/h) Number Initial Q (Qb), veh Ped-Bike Adj(A_pbT) Parking Bus, Adj Adj Sat Flow, veh/h/In Adj Flow Rate, veh/h Adj No. of Lanes Peak Hour Factor Percent Heavy Veh, % Cap, veh/h Arrive On Green Sat Flow, veh/h | 175<br>175<br>7<br>0<br>1.00<br>1.00<br>1863<br>184 | 649<br>649<br>4<br>0 | EBR<br>65<br>65<br>14<br>0 | WBL<br>71<br>71<br>71<br>3 | WBT<br>↑↑<br>446 | WBR<br>r 42 | NBL  | NBT  | NBR  | SBL  | SBT  | SBR  |
|---|---|----------------------|----------------------------|----------------------------|------------------|-------------|------|------|------|------|------|------|
| Traffic Volume (veh/h) Future Volume (veh/h) Number Initial Q (Qb), veh Ped-Bike Adj(A_pbT) Parking Bus, Adj Adj Sat Flow, veh/h/In Adj Flow Rate, veh/h Adj No. of Lanes Peak Hour Factor Percent Heavy Veh, % Cap, veh/h Arrive On Green  | 175<br>175<br>7<br>0<br>1.00<br>1.00<br>1863<br>184 | 649<br>649<br>4<br>0 | 65<br>65<br>14             | 71<br>71                   | 446              |             |      |      | 7    | 7    | *    | -    |
| Future Volume (veh/h) Number Initial Q (Qb), veh Ped-Bike Adj(A_pbT) Parking Bus, Adj Adj Sat Flow, veh/h/ln Adj Flow Rate, veh/h Adj No. of Lanes Peak Hour Factor Percent Heavy Veh, % Cap, veh/h Arrive On Green   | 175<br>7<br>0<br>1.00<br>1.00<br>1863<br>184        | 649<br>649<br>4<br>0 | 65<br>14                   | 71                         | 446              | 42          | 0.5  |      |      |      |      | 7    |
| Number Initial Q (Qb), veh Ped-Bike Adj(A_pbT) Parking Bus, Adj Adj Sat Flow, veh/h/In Adj Flow Rate, veh/h Adj No. of Lanes Peak Hour Factor Percent Heavy Veh, % Cap, veh/h Arrive On Green   | 7<br>0<br>1.00<br>1.00<br>1863<br>184               | 4                    | 14                         |                            | 110              | - '-        | 35   | 5    | 51   | 25   | 5    | 100  |
| Initial Q (Qb), veh Ped-Bike Adj(A_pbT) Parking Bus, Adj Adj Sat Flow, veh/h/In Adj Flow Rate, veh/h Adj No. of Lanes Peak Hour Factor Percent Heavy Veh, % Cap, veh/h Arrive On Green  | 0<br>1.00<br>1.00<br>1863<br>184                    | 0                    |                            | 2                          | 446              | 42          | 35   | 5    | 51   | 25   | 5    | 100  |
| Ped-Bike Adj(A_pbT) Parking Bus, Adj Adj Sat Flow, veh/h/ln Adj Flow Rate, veh/h Adj No. of Lanes Peak Hour Factor Percent Heavy Veh, % Cap, veh/h Arrive On Green  | 1.00<br>1.00<br>1863<br>184                         |                      | 0                          | J                          | 8                | 18          | 5    | 2    | 12   | 1    | 6    | 16   |
| Parking Bus, Adj Adj Sat Flow, veh/h/ln Adj Flow Rate, veh/h Adj No. of Lanes Peak Hour Factor Percent Heavy Veh, % Cap, veh/h Arrive On Green  | 1.00<br>1863<br>184                                 | 1 00                 | -                          | 0                          | 0                | 0           | 0    | 0    | 0    | 0    | 0    | 0    |
| Adj Sat Flow, veh/h/ln Adj Flow Rate, veh/h Adj No. of Lanes Peak Hour Factor Percent Heavy Veh, % Cap, veh/h Arrive On Green   | 1863<br>184   | 1 00                 | 1.00                       | 1.00                       |                  | 1.00        | 1.00 |      | 1.00 | 1.00 |      | 1.00 |
| Adj Flow Rate, veh/h Adj No. of Lanes Peak Hour Factor Percent Heavy Veh, % Cap, veh/h Arrive On Green  | 184   |                      | 1.00                       | 1.00                       | 1.00             | 1.00        | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj No. of Lanes<br>Peak Hour Factor<br>Percent Heavy Veh, %<br>Cap, veh/h<br>Arrive On Green   |   | 1863                 | 1863                       | 1863                       | 1863             | 1863        | 1863 | 1863 | 1863 | 1863 | 1863 | 1863 |
| Peak Hour Factor Percent Heavy Veh, % Cap, veh/h Arrive On Green  | 1   | 683                  | 68                         | 75                         | 469              | 44          | 37   | 5    | 54   | 26   | 5    | 105  |
| Percent Heavy Veh, %<br>Cap, veh/h<br>Arrive On Green   |   | 2                    | 1                          | 1                          | 2                | 1           | 1    | 1    | 1    | 1    | 1    | 1    |
| Cap, veh/h<br>Arrive On Green   | 0.95  | 0.95                 | 0.95                       | 0.95                       | 0.95             | 0.95        | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Arrive On Green   | 2   | 2                    | 2                          | 2                          | 2                | 2           | 2    | 2    | 2    | 2    | 2    | 2    |
|   | 242   | 1242                 | 555                        | 135                        | 1028             | 460         | 418  | 289  | 245  | 428  | 289  | 245  |
| Sat Flow, veh/h   | 0.14  | 0.35                 | 0.35                       | 0.08                       | 0.29             | 0.29        | 0.15 | 0.15 | 0.15 | 0.15 | 0.15 | 0.15 |
|   | 1774  | 3539                 | 1583                       | 1774                       | 3539             | 1583        | 1278 | 1863 | 1583 | 1338 | 1863 | 1583 |
| Grp Volume(v), veh/h  | 184   | 683                  | 68                         | 75                         | 469              | 44          | 37   | 5    | 54   | 26   | 5    | 105  |
| Grp Sat Flow(s),veh/h/ln  | 1774  | 1770                 | 1583                       | 1774                       | 1770             | 1583        | 1278 | 1863 | 1583 | 1338 | 1863 | 1583 |
| Q Serve(g_s), s   | 3.2   | 5.0                  | 0.9                        | 1.3                        | 3.5              | 0.7         | 0.8  | 0.1  | 1.0  | 0.5  | 0.1  | 1.9  |
| Cycle Q Clear(g_c), s   | 3.2   | 5.0                  | 0.9                        | 1.3                        | 3.5              | 0.7         | 0.9  | 0.1  | 1.0  | 0.6  | 0.1  | 1.9  |
| Prop In Lane  | 1.00  |                      | 1.00                       | 1.00                       |                  | 1.00        | 1.00 |      | 1.00 | 1.00 |      | 1.00 |
| Lane Grp Cap(c), veh/h  | 242   | 1242                 | 555                        | 135                        | 1028             | 460         | 418  | 289  | 245  | 428  | 289  | 245  |
| V/C Ratio(X)  | 0.76  | 0.55                 | 0.12                       | 0.56                       | 0.46             | 0.10        | 0.09 | 0.02 | 0.22 | 0.06 | 0.02 | 0.43 |
| Avail Cap(c_a), veh/h   | 577   | 2380                 | 1065                       | 374                        | 1974             | 883         | 933  | 1039 | 883  | 967  | 1039 | 883  |
| HCM Platoon Ratio   | 1.00  | 1.00                 | 1.00                       | 1.00                       | 1.00             | 1.00        | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I)  | 1.00  | 1.00                 | 1.00                       | 1.00                       | 1.00             | 1.00        | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh  | 13.4  | 8.4                  | 7.1                        | 14.4                       | 9.4              | 8.4         | 11.9 | 11.6 | 11.9 | 11.8 | 11.6 | 12.3 |
| Incr Delay (d2), s/veh  | 4.9   | 0.4                  | 0.1                        | 3.6                        | 0.3              | 0.1         | 0.1  | 0.0  | 0.4  | 0.1  | 0.0  | 1.2  |
| Initial Q Delay(d3),s/veh   | 0.0   | 0.0                  | 0.0                        | 0.0                        | 0.0              | 0.0         | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  |
| %ile BackOfQ(50%),veh/ln  | 1.9   | 2.4                  | 0.4                        | 0.8                        | 1.7              | 0.3         | 0.3  | 0.0  | 0.4  | 0.2  | 0.0  | 0.9  |
| LnGrp Delay(d),s/veh  | 18.3  | 8.8                  | 7.2                        | 18.0                       | 9.7              | 8.4         | 12.0 | 11.6 | 12.4 | 11.9 | 11.6 | 13.5 |
| LnGrp LOS   | В   | Α                    | Α                          | В                          | Α                | Α           | В    | В    | В    | В    | В    | В    |
| Approach Vol, veh/h   |   | 935                  |                            |                            | 588              |             |      | 96   |      |      | 136  |      |
| Approach Delay, s/veh   |   | 10.6                 |                            |                            | 10.6             |             |      | 12.2 |      |      | 13.1 |      |
| Approach LOS  |   | В                    |                            |                            | В                |             |      | В    |      |      | В    |      |
| Timer   | 1   | 2                    | 3                          | 4                          | 5                | 6           | 7    | 8    |      |      |      |      |
| Assigned Phs  |   | 2                    | 3                          | 4                          |                  | 6           | 7    | 8    |      |      |      |      |
| Phs Duration (G+Y+Rc), s  |   | 9.5                  | 6.9                        | 15.8                       |                  | 9.5         | 8.9  | 13.9 |      |      |      |      |
| Change Period (Y+Rc), s   |   | 4.5                  | 4.5                        | 4.5                        |                  | 4.5         | 4.5  | 4.5  |      |      |      |      |
| Max Green Setting (Gmax), s   |   | 18.0                 | 6.8                        | 21.7                       |                  | 18.0        | 10.5 | 18.0 |      |      |      |      |
| Max Q Clear Time (g_c+l1), s  |   | 3.0                  | 3.3                        | 7.0                        |                  | 3.9         | 5.2  | 5.5  |      |      |      |      |
| Green Ext Time (p_c), s   |   | 0.2                  | 0.0                        | 4.3                        |                  | 0.3         | 0.2  | 2.6  |      |      |      |      |
| Intersection Summary  |   |                      |                            |                            |                  |             |      |      |      |      |      |      |
| HCM 2010 Ctrl Delay   |   |                      |                            |                            |                  |             |      |      |      |      |      |      |
| HCM 2010 LOS  |   |                      | 10.9<br>B                  |                            |                  |             |      |      |      |      |      |      |

| Intersection           |                |      |          |       |        |              |
|------------------------|----------------|------|----------|-------|--------|--------------|
| Int Delay, s/veh       | 3.2            |      |          |       |        |              |
| Movement               | WBL            | WBR  | NBT      | NBR   | SBL    | SBT          |
| Lane Configurations    | WDL            | אטוע |          | NON   | SDL    | <u>361</u>   |
| Traffic Vol, veh/h     | 34             | 83   | <b>₽</b> | 31    | 116    | <b>T</b> 315 |
| Future Vol, veh/h      | 34             | 83   | 207      | 31    | 116    | 315          |
|                        | 3 <del>4</del> | 03   | 0        | 0     | 0      | 0            |
| Conflicting Peds, #/hr |                |      |          | Free  |        | Free         |
| Sign Control           | Stop           | Stop | Free     |       | Free   |              |
| RT Channelized         | -              | None | -        |       | 450    | None         |
| Storage Length         | 0              | -    | -        | -     | 150    | -            |
| Veh in Median Storage  |                | -    | 0        | -     | -      | 0            |
| Grade, %               | 0              | -    | 0        | -     | -      | 0            |
| Peak Hour Factor       | 93             | 93   | 93       | 93    | 93     | 93           |
| Heavy Vehicles, %      | 6              | 6    | 2        | 2     | 3      | 3            |
| Mvmt Flow              | 37             | 89   | 223      | 33    | 125    | 339          |
|                        |                |      |          |       |        |              |
| Major/Minor I          | Minor1         | N    | Major1   |       | Major2 |              |
|                        |                | 240  |          | 0     | 256    | 0            |
| Conflicting Flow All   | 830            |      | 0        | U     | ∠50    |              |
| Stage 1                | 240            | -    | -        | -     | -      | -            |
| Stage 2                | 590            | -    | -        | -     | -      | -            |
| Critical Hdwy          | 6.46           | 6.26 | -        | -     | 4.13   | -            |
| Critical Hdwy Stg 1    | 5.46           | -    | -        | -     | -      | -            |
| Critical Hdwy Stg 2    | 5.46           | -    | -        | -     | -      | -            |
| Follow-up Hdwy         | 3.554          |      | -        | -     | 2.227  | -            |
| Pot Cap-1 Maneuver     | 335            | 789  | -        | -     | 1303   | -            |
| Stage 1                | 791            | -    | -        | -     | -      | -            |
| Stage 2                | 546            | -    | -        | -     | -      | -            |
| Platoon blocked, %     |                |      | -        | -     |        | -            |
| Mov Cap-1 Maneuver     | 303            | 789  | -        | -     | 1303   | -            |
| Mov Cap-2 Maneuver     | 303            | -    | -        | -     | -      | -            |
| Stage 1                | 715            | -    | -        | -     | -      | -            |
| Stage 2                | 545            | _    | -        | -     | -      | -            |
| <b>J</b>               |                |      |          |       |        |              |
|                        | VA/P           |      | NE       |       | 0.5    |              |
| Approach               | WB             |      | NB       |       | SB     |              |
| HCM Control Delay, s   | 13.7           |      | 0        |       | 2.2    |              |
| HCM LOS                | В              |      |          |       |        |              |
|                        |                |      |          |       |        |              |
| Minor Lanc/Major Mum   | <b>1</b>       | NBT  | NDDV     | VBLn1 | SBL    | SBT          |
| Minor Lane/Major Mvm   | IL             |      |          |       |        |              |
| Capacity (veh/h)       |                | -    | -        |       | 1303   | -            |
| HCM Lane V/C Ratio     |                | -    |          | 0.234 |        | -            |
| HCM Control Delay (s)  |                | -    | -        |       | 8.1    | -            |
| HCM Lane LOS           |                | -    | -        | В     | Α      | -            |
| HCM 95th %tile Q(veh   | )              | -    | -        | 0.9   | 0.3    | -            |
| HCM 95th %tile Q(veh   | )              | -    |          | 0.9   | 0.3    |              |

| Intersection  |               |   |   |  |      |          |
|---|---------------|---|---|--|------|----------|
| Intersection Delay, s/veh   | 12.3          |   |   |  |      |          |
| Intersection LOS  | В             |   |   |  |      |          |
|   |               |   |   |  |      |          |
| Movement  | WBL           | WBR   | NBT   | NBR  | SBL  | SBT      |
|   |               | WDK   |   | NDK  | SDL  |          |
| Lane Configurations   | 34            | 0.2   | 207   | 24   | 110  | <b>€</b> |
| Traffic Vol, veh/h  | 34            | 83  | 207   | 31   | 116  | 315      |
| Future Vol, veh/h   | 34            | 83  | 207   | 31   | 116  | 315      |
| Peak Hour Factor  | 0.93          | 0.93  | 0.93  | 0.93   | 0.93 | 0.93     |
| Heavy Vehicles, %   | 6             | 6   | 2   | 2  | 3    | 3        |
| Mvmt Flow   | 37            | 89  | 223   | 33   | 125  | 339      |
| Number of Lanes   | 1             | 0   | 1   | 0  | 0    | 1        |
| Approach  | WB            |   | NB  |  | SB   |          |
| Opposing Approach   |               |   | SB  |  | NB   |          |
| Opposing Lanes  | 0             |   | 1   |  | 1    |          |
| Conflicting Approach Left   | NB            |   |   |  | WB   |          |
| Conflicting Lanes Left  | 1             |   | 0   |  | 1    |          |
| Conflicting Approach Right  | SB            |   | WB  |  |      |          |
| Conflicting Lanes Right   | 1             |   | 1   |  | 0    |          |
| HCM Control Delay   | 9.5           |   | 10.1  |  | 14.3 |          |
| HCM LOS   | Α             |   | В   |  | В    |          |
| I IOW LOO   | $\overline{}$ |   | ט   |  | ט    |          |
| HOW LOS   | Λ.            |   | Ь   |  | Ь    |          |
|   |               | NBI n1  | _   | SBLn1  | Ь    |          |
| Lane  | A             | NBLn1   | WBLn1   | SBLn1  | В    |          |
| Lane<br>Vol Left, %   |               | 0%  | WBLn1<br>29%  | 27%  |      |          |
| Lane<br>Vol Left, %<br>Vol Thru, %  | ^             | 0%<br>87%   | WBLn1<br>29%<br>0%  | 27%<br>73%   |      |          |
| Lane Vol Left, % Vol Thru, % Vol Right, %   | ^             | 0%<br>87%<br>13%  | WBLn1<br>29%<br>0%<br>71%   | 27%<br>73%<br>0%   | D    |          |
| Lane Vol Left, % Vol Thru, % Vol Right, % Sign Control  | ^             | 0%<br>87%<br>13%<br>Stop  | WBLn1 29% 0% 71% Stop   | 27%<br>73%<br>0%<br>Stop   | D    |          |
| Lane Vol Left, % Vol Thru, % Vol Right, % Sign Control Traffic Vol by Lane  | ^             | 0%<br>87%<br>13%<br>Stop<br>238   | WBLn1 29% 0% 71% Stop 117   | 27%<br>73%<br>0%<br>Stop<br>431  | D    |          |
| Lane Vol Left, % Vol Thru, % Vol Right, % Sign Control Traffic Vol by Lane LT Vol   | ^             | 0%<br>87%<br>13%<br>Stop<br>238   | WBLn1 29% 0% 71% Stop 117 34  | 27%<br>73%<br>0%<br>Stop<br>431<br>116                                   | В    |          |
| Lane Vol Left, % Vol Thru, % Vol Right, % Sign Control Traffic Vol by Lane LT Vol Through Vol   | ^             | 0%<br>87%<br>13%<br>Stop<br>238<br>0<br>207   | WBLn1 29% 0% 71% Stop 117 34 0  | 27%<br>73%<br>0%<br>Stop<br>431<br>116<br>315                            | В    |          |
| Lane  Vol Left, %  Vol Thru, %  Vol Right, %  Sign Control  Traffic Vol by Lane  LT Vol  Through Vol  RT Vol  |               | 0%<br>87%<br>13%<br>Stop<br>238<br>0<br>207<br>31   | WBLn1 29% 0% 71% Stop 117 34 0 83   | 27%<br>73%<br>0%<br>Stop<br>431<br>116<br>315                            | D    |          |
| Lane Vol Left, % Vol Thru, % Vol Right, % Sign Control Traffic Vol by Lane LT Vol Through Vol RT Vol Lane Flow Rate   |               | 0%<br>87%<br>13%<br>Stop<br>238<br>0<br>207<br>31<br>256  | WBLn1 29% 0% 71% Stop 117 34 0 83 126                                       | 27% 73% 0% Stop 431 116 315 0 463  | В    |          |
| Lane Vol Left, % Vol Thru, % Vol Right, % Sign Control Traffic Vol by Lane LT Vol Through Vol RT Vol Lane Flow Rate Geometry Grp  |               | 0%<br>87%<br>13%<br>Stop<br>238<br>0<br>207<br>31<br>256  | WBLn1 29% 0% 71% Stop 117 34 0 83 126                                       | 27% 73% 0% Stop 431 116 315 0 463  |      |          |
| Lane Vol Left, % Vol Thru, % Vol Right, % Sign Control Traffic Vol by Lane LT Vol Through Vol RT Vol Lane Flow Rate Geometry Grp Degree of Util (X)   |               | 0%<br>87%<br>13%<br>Stop<br>238<br>0<br>207<br>31<br>256<br>1<br>0.334  | WBLn1 29% 0% 71% Stop 117 34 0 83 126 1 0.183                               | 27% 73% 0% Stop 431 116 315 0 463 1 0.595                                |      |          |
| Lane Vol Left, % Vol Thru, % Vol Right, % Sign Control Traffic Vol by Lane LT Vol Through Vol RT Vol Lane Flow Rate Geometry Grp Degree of Util (X) Departure Headway (Hd)  |               | 0%<br>87%<br>13%<br>Stop<br>238<br>0<br>207<br>31<br>256<br>1<br>0.334<br>4.702                                 | WBLn1 29% 0% 71% Stop 117 34 0 83 126 1 0.183 5.238                         | 27% 73% 0% Stop 431 116 315 0 463 1 0.595 4.623                          |      |          |
| Lane  Vol Left, %  Vol Thru, %  Vol Right, %  Sign Control  Traffic Vol by Lane  LT Vol  Through Vol  RT Vol  Lane Flow Rate  Geometry Grp  Degree of Util (X)  Departure Headway (Hd)  Convergence, Y/N  |               | 0%<br>87%<br>13%<br>Stop<br>238<br>0<br>207<br>31<br>256<br>1<br>0.334<br>4.702<br>Yes                          | WBLn1 29% 0% 71% Stop 117 34 0 83 126 1 0.183 5.238 Yes                     | 27% 73% 0% Stop 431 116 315 0 463 1 0.595 4.623 Yes                      |      |          |
| Lane  Vol Left, %  Vol Thru, %  Vol Right, %  Sign Control  Traffic Vol by Lane  LT Vol  Through Vol  RT Vol  Lane Flow Rate  Geometry Grp  Degree of Util (X)  Departure Headway (Hd)  Convergence, Y/N  Cap                                     |               | 0%<br>87%<br>13%<br>Stop<br>238<br>0<br>207<br>31<br>256<br>1<br>0.334<br>4.702<br>Yes<br>760                   | WBLn1 29% 0% 71% Stop 117 34 0 83 126 1 0.183 5.238 Yes 679                 | 27% 73% 0% Stop 431 116 315 0 463 1 0.595 4.623 Yes 779                  |      |          |
| Lane Vol Left, % Vol Thru, % Vol Right, % Sign Control Traffic Vol by Lane LT Vol Through Vol RT Vol Lane Flow Rate Geometry Grp Degree of Util (X) Departure Headway (Hd) Convergence, Y/N Cap Service Time                                      |               | 0%<br>87%<br>13%<br>Stop<br>238<br>0<br>207<br>31<br>256<br>1<br>0.334<br>4.702<br>Yes<br>760<br>2.758          | WBLn1 29% 0% 71% Stop 117 34 0 83 126 1 0.183 5.238 Yes 679 3.309           | 27% 73% 0% Stop 431 116 315 0 463 1 0.595 4.623 Yes 779 2.671            |      |          |
| Lane Vol Left, % Vol Thru, % Vol Right, % Sign Control Traffic Vol by Lane LT Vol Through Vol RT Vol Lane Flow Rate Geometry Grp Degree of Util (X) Departure Headway (Hd) Convergence, Y/N Cap Service Time HCM Lane V/C Ratio                   |               | 0%<br>87%<br>13%<br>Stop<br>238<br>0<br>207<br>31<br>256<br>1<br>0.334<br>4.702<br>Yes<br>760<br>2.758<br>0.337 | WBLn1 29% 0% 71% Stop 117 34 0 83 126 1 0.183 5.238 Yes 679 3.309 0.186     | 27% 73% 0% Stop 431 116 315 0 463 1 0.595 4.623 Yes 779 2.671 0.594      |      |          |
| Lane Vol Left, % Vol Thru, % Vol Right, % Sign Control Traffic Vol by Lane LT Vol Through Vol RT Vol Lane Flow Rate Geometry Grp Degree of Util (X) Departure Headway (Hd) Convergence, Y/N Cap Service Time HCM Lane V/C Ratio HCM Control Delay |               | 0% 87% 13% Stop 238 0 207 31 256 1 0.334 4.702 Yes 760 2.758 0.337 10.1   | WBLn1 29% 0% 71% Stop 117 34 0 83 126 1 0.183 5.238 Yes 679 3.309 0.186 9.5 | 27% 73% 0% Stop 431 116 315 0 463 1 0.595 4.623 Yes 779 2.671 0.594 14.3 |      |          |
| Lane Vol Left, % Vol Thru, % Vol Right, % Sign Control Traffic Vol by Lane LT Vol Through Vol RT Vol Lane Flow Rate Geometry Grp Degree of Util (X) Departure Headway (Hd) Convergence, Y/N Cap Service Time HCM Lane V/C Ratio                   |               | 0%<br>87%<br>13%<br>Stop<br>238<br>0<br>207<br>31<br>256<br>1<br>0.334<br>4.702<br>Yes<br>760<br>2.758<br>0.337 | WBLn1 29% 0% 71% Stop 117 34 0 83 126 1 0.183 5.238 Yes 679 3.309 0.186     | 27% 73% 0% Stop 431 116 315 0 463 1 0.595 4.623 Yes 779 2.671 0.594      |      |          |

|                              | •    | <b>→</b> | •    | •    | <b>←</b>   | •     | 1    | <b>†</b> | <i>&gt;</i> | <b>/</b> | <b></b>  | 4    |
|------------------------------|------|----------|------|------|------------|-------|------|----------|-------------|----------|----------|------|
| Movement                     | EBL  | EBT      | EBR  | WBL  | WBT        | WBR   | NBL  | NBT      | NBR         | SBL      | SBT      | SBR  |
| Lane Configurations          | , A  | <b>^</b> | 7    | ¥    | <b>↑</b> ↑ |       | 7    | <b>^</b> | 7           | ¥        | <b>^</b> | 7    |
| Traffic Volume (veh/h)       | 313  | 393      | 244  | 25   | 266        | 220   | 200  | 645      | 36          | 375      | 620      | 267  |
| Future Volume (veh/h)        | 313  | 393      | 244  | 25   | 266        | 220   | 200  | 645      | 36          | 375      | 620      | 267  |
| Number                       | 7    | 4        | 14   | 3    | 8          | 18    | 5    | 2        | 12          | 1        | 6        | 16   |
| Initial Q (Qb), veh          | 0    | 0        | 0    | 0    | 0          | 0     | 0    | 0        | 0           | 0        | 0        | 0    |
| Ped-Bike Adj(A_pbT)          | 1.00 |          | 1.00 | 1.00 |            | 1.00  | 1.00 |          | 1.00        | 1.00     |          | 1.00 |
| Parking Bus, Adj             | 1.00 | 1.00     | 1.00 | 1.00 | 1.00       | 1.00  | 1.00 | 1.00     | 1.00        | 1.00     | 1.00     | 1.00 |
| Adj Sat Flow, veh/h/ln       | 1863 | 1863     | 1863 | 1863 | 1863       | 1900  | 1863 | 1863     | 1863        | 1863     | 1863     | 1863 |
| Adj Flow Rate, veh/h         | 326  | 409      | 254  | 26   | 277        | 229   | 208  | 672      | 38          | 391      | 646      | 278  |
| Adj No. of Lanes             | 1    | 2        | 1    | 1    | 2          | 0     | 1    | 2        | 1           | 1        | 2        | 1    |
| Peak Hour Factor             | 0.96 | 0.96     | 0.96 | 0.96 | 0.96       | 0.96  | 0.96 | 0.96     | 0.96        | 0.96     | 0.96     | 0.96 |
| Percent Heavy Veh, %         | 2    | 2        | 2    | 2    | 2          | 2     | 2    | 2        | 2           | 2        | 2        | 2    |
| Cap, veh/h                   | 359  | 1016     | 670  | 88   | 252        | 202   | 241  | 865      | 387         | 424      | 1230     | 550  |
| Arrive On Green              | 0.20 | 0.29     | 0.29 | 0.05 | 0.13       | 0.13  | 0.14 | 0.24     | 0.24        | 0.24     | 0.35     | 0.35 |
| Sat Flow, veh/h              | 1774 | 3539     | 1583 | 1774 | 1870       | 1498  | 1774 | 3539     | 1583        | 1774     | 3539     | 1583 |
| Grp Volume(v), veh/h         | 326  | 409      | 254  | 26   | 262        | 244   | 208  | 672      | 38          | 391      | 646      | 278  |
| Grp Sat Flow(s),veh/h/ln     | 1774 | 1770     | 1583 | 1774 | 1770       | 1598  | 1774 | 1770     | 1583        | 1774     | 1770     | 1583 |
| Q Serve(g_s), s              | 18.0 | 9.3      | 11.1 | 1.4  | 13.5       | 13.5  | 11.5 | 17.7     | 1.9         | 21.6     | 14.6     | 13.9 |
| Cycle Q Clear(g_c), s        | 18.0 | 9.3      | 11.1 | 1.4  | 13.5       | 13.5  | 11.5 | 17.7     | 1.9         | 21.6     | 14.6     | 13.9 |
| Prop In Lane                 | 1.00 |          | 1.00 | 1.00 |            | 0.94  | 1.00 |          | 1.00        | 1.00     |          | 1.00 |
| Lane Grp Cap(c), veh/h       | 359  | 1016     | 670  | 88   | 238        | 215   | 241  | 865      | 387         | 424      | 1230     | 550  |
| V/C Ratio(X)                 | 0.91 | 0.40     | 0.38 | 0.29 | 1.10       | 1.13  | 0.86 | 0.78     | 0.10        | 0.92     | 0.53     | 0.51 |
| Avail Cap(c_a), veh/h        | 398  | 1066     | 692  | 103  | 238        | 215   | 292  | 865      | 387         | 469      | 1230     | 550  |
| HCM Platoon Ratio            | 1.00 | 1.00     | 1.00 | 1.00 | 1.00       | 1.00  | 1.00 | 1.00     | 1.00        | 1.00     | 1.00     | 1.00 |
| Upstream Filter(I)           | 1.00 | 1.00     | 1.00 | 1.00 | 1.00       | 1.00  | 1.00 | 1.00     | 1.00        | 1.00     | 1.00     | 1.00 |
| Uniform Delay (d), s/veh     | 39.1 | 28.8     | 19.9 | 45.9 | 43.4       | 43.4  | 42.4 | 35.3     | 29.3        | 37.2     | 26.1     | 25.9 |
| Incr Delay (d2), s/veh       | 22.9 | 0.3      | 0.4  | 1.8  | 86.9       | 102.4 | 19.5 | 6.8      | 0.5         | 22.6     | 1.6      | 3.3  |
| Initial Q Delay(d3),s/veh    | 0.0  | 0.0      | 0.0  | 0.0  | 0.0        | 0.0   | 0.0  | 0.0      | 0.0         | 0.0      | 0.0      | 0.0  |
| %ile BackOfQ(50%),veh/ln     | 11.1 | 4.6      | 4.9  | 0.7  | 12.3       | 12.0  | 7.0  | 9.5      | 0.9         | 13.2     | 7.4      | 6.6  |
| LnGrp Delay(d),s/veh         | 62.0 | 29.1     | 20.2 | 47.7 | 130.3      | 145.8 | 61.9 | 42.1     | 29.8        | 59.8     | 27.7     | 29.2 |
| LnGrp LOS                    | Е    | С        | С    | D    | F          | F     | Е    | D        | С           | Е        | С        | С    |
| Approach Vol, veh/h          |      | 989      |      |      | 532        |       |      | 918      |             |          | 1315     |      |
| Approach Delay, s/veh        |      | 37.6     |      |      | 133.4      |       |      | 46.1     |             |          | 37.6     |      |
| Approach LOS                 |      | D        |      |      | F          |       |      | D        |             |          | D        |      |
| Timer                        | 1    | 2        | 3    | 4    | 5          | 6     | 7    | 8        |             |          |          |      |
| Assigned Phs                 | 1    | 2        | 3    | 4    | 5          | 6     | 7    | 8        |             |          |          |      |
| Phs Duration (G+Y+Rc), s     | 28.5 | 29.0     | 9.5  | 33.3 | 18.1       | 39.3  | 24.8 | 18.0     |             |          |          |      |
| Change Period (Y+Rc), s      | 4.5  | 4.5      | 4.5  | 4.5  | 4.5        | 4.5   | 4.5  | 4.5      |             |          |          |      |
| Max Green Setting (Gmax), s  | 26.5 | 24.5     | 5.8  | 30.2 | 16.5       | 34.5  | 22.5 | 13.5     |             |          |          |      |
| Max Q Clear Time (g_c+l1), s | 23.6 | 19.7     | 3.4  | 13.1 | 13.5       | 16.6  | 20.0 | 15.5     |             |          |          |      |
| Green Ext Time (p_c), s      | 0.4  | 2.0      | 0.0  | 3.3  | 0.2        | 5.2   | 0.3  | 0.0      |             |          |          |      |
| Intersection Summary         |      |          |      |      |            |       |      |          |             |          |          |      |
| HCM 2010 Ctrl Delay          |      |          | 53.2 |      |            |       |      |          |             |          |          |      |
| HCM 2010 LOS                 |      |          | D    |      |            |       |      |          |             |          |          |      |

| 55<br>55<br>7<br>0<br>1.00         | **************************************   | 183<br>183<br>14<br>0 | WBL<br>180<br>180<br>3 | WBT<br><b>↑</b> ;<br>488 | WBR  | NBL   | NBT  | NBR  | SBL  | SBT  | SBR  |
|------------------------------------|--|-----------------------|------------------------|--------------------------|------|---|--|--|--|------|------|
| 55<br>55<br>7<br>0<br>1.00<br>1.00 | 780<br>780<br>4  | 183<br>14             | 180<br>180             | 488                      |      |   |  |  |  |      |      |
| 55<br>7<br>0<br>1.00<br>1.00       | 780<br>780<br>4  | 183<br>14             | 180                    |                          |      |   | ቆ  |  |  | ↔    |      |
| 7<br>0<br>1.00<br>1.00             | 4  | 14                    |                        |                          | 35   | 135   | 57   | 115  | 55   | 86   | 34   |
| 0<br>1.00<br>1.00                  |  |                       | 2                      | 488                      | 35   | 135   | 57   | 115  | 55   | 86   | 34   |
| 1.00<br>1.00                       | 0  | 0                     | 3                      | 8                        | 18   | 5   | 2  | 12   | 1  | 6    | 16   |
| 1.00                               |  |                       | 0                      | 0                        | 0    | 0   | 0  | 0  | 0  | 0    | 0    |
|                                    |  | 1.00                  | 1.00                   |                          | 1.00 | 1.00  |  | 1.00   | 1.00   |      | 1.00 |
| 1000                               |  |                       |                        |                          |      |   |  |  |  |      | 1.00 |
|                                    |  |                       |                        |                          | 1900 |   |  |  |  |      | 1900 |
|                                    |  | 208                   | 205                    |                          | 40   |   |  | 131  |  | 98   | 39   |
|                                    |  | 0                     | 1                      |                          | 0    |   |  | 0  |  | 1    | 0    |
| 0.88                               |  |                       |                        |                          |      |   |  |  |  |      | 0.88 |
|                                    |  |                       |                        |                          |      |   |  |  |  |      | 4    |
|                                    |  |                       |                        |                          |      |   |  |  |  |      | 98   |
| 0.05                               | 0.33   |                       | 0.14                   |                          |      |   |  | 0.32   |  |      | 0.32 |
| 1774                               | 2847   | 668                   | 1774                   | 3349                     | 241  | 603   | 365  | 582  | 373  | 889  | 307  |
| 62                                 | 551  | 543                   | 205                    | 293                      | 302  | 349   | 0  | 0  | 199  | 0    | 0    |
| 1774                               | 1770   | 1745                  | 1774                   | 1770                     | 1820 | 1549  | 0  | 0  | 1569   | 0    | 0    |
| 2.2                                | 19.4   | 19.5                  | 7.2                    | 7.4                      | 7.4  | 6.3   | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  |
| 2.2                                | 19.4   | 19.5                  | 7.2                    | 7.4                      | 7.4  | 12.1  | 0.0  | 0.0  | 5.8  | 0.0  | 0.0  |
| 1.00                               |  | 0.38                  | 1.00                   |                          | 0.13 | 0.44  |  | 0.38   | 0.31   |      | 0.20 |
| 92                                 | 589  | 581                   | 248                    | 745                      | 766  | 573   | 0  | 0  | 572  | 0    | 0    |
| 0.67                               | 0.93   | 0.94                  | 0.83                   | 0.39                     | 0.39 | 0.61  | 0.00   | 0.00   | 0.35   | 0.00 | 0.00 |
| 181                                | 590  | 581                   | 261                    | 745                      | 766  | 573   | 0  | 0  | 572  | 0    | 0    |
| 1.00                               | 1.00   | 1.00                  | 1.00                   | 1.00                     | 1.00 | 1.00  | 1.00   | 1.00   | 1.00   | 1.00 | 1.00 |
| 1.00                               | 1.00   | 1.00                  | 1.00                   | 1.00                     | 1.00 | 1.00  | 0.00   | 0.00   | 1.00   | 0.00 | 0.00 |
| 30.0                               | 20.8   | 20.8                  | 27.0                   | 13.0                     | 13.0 | 18.9  | 0.0  | 0.0  | 16.9   | 0.0  | 0.0  |
| 8.2                                | 22.2   | 22.6                  | 18.4                   | 0.3                      | 0.3  | 4.8   | 0.0  | 0.0  | 1.7  | 0.0  | 0.0  |
| 0.0                                | 0.0  | 0.0                   | 0.0                    | 0.0                      | 0.0  | 0.0   | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  |
| 1.3                                | 13.1   | 13.0                  | 4.8                    | 3.6                      | 3.8  | 6.1   | 0.0  | 0.0  | 3.0  | 0.0  | 0.0  |
| 38.2                               | 43.0   | 43.4                  | 45.4                   | 13.3                     | 13.3 | 23.7  | 0.0  | 0.0  | 18.6   | 0.0  | 0.0  |
| D                                  | D  | D                     | D                      | В                        | В    | С   |  |  | В  |      |      |
|                                    | 1156   |                       |                        | 800                      |      |   | 349  |  |  | 199  |      |
|                                    | 43.0   |                       |                        | 21.5                     |      |   | 23.7   |  |  | 18.6 |      |
|                                    | D  |                       |                        | С                        |      |   | С  |  |  | В    |      |
| 1                                  | 2  | 3                     | 4                      | 5                        | 6    | 7   | 8  |  |  |      |      |
|                                    | 2  | 3                     | 4                      |                          | 6    | 7   | 8  |  |  |      |      |
|                                    | 25.0   | 13.5                  | 26.0                   |                          | 25.0 | 7.9   | 31.7   |  |  |      |      |
|                                    | 4.5  | 4.5                   | 4.5                    |                          | 4.5  | 4.5   | 4.5  |  |  |      |      |
|                                    | 20.5   | 9.5                   | 21.5                   |                          | 20.5 | 6.6   | 24.4   |  |  |      |      |
|                                    |  | 9.2                   |                        |                          |      | 4.2   |  |  |  |      |      |
|                                    | 1.2  | 0.0                   | 0.0                    |                          | 0.9  | 0.0   | 3.2  |  |  |      |      |
|                                    |  |                       |                        |                          |      |   |  |  |  |      |      |
|                                    |  | 31.5                  |                        |                          |      |   |  |  |  |      |      |
|                                    |  | С                     |                        |                          |      |   |  |  |  |      |      |
|                                    | 1.00<br>1863<br>62<br>1<br>0.88<br>2<br>92<br>0.05<br>1774<br>62<br>1774<br>2.2<br>2.2<br>1.00<br>92<br>0.67<br>181<br>1.00<br>1.00<br>30.0<br>8.2<br>0.0<br>1.3<br>38.2 | 1.00                  | 1.00                   | 1.00                     | 1.00 | 1.00       1.00       1.00       1.00       1.00       1.00         1863       1863       1900       1863       1863       1900         62       886       208       205       555       40         1       2       0       1       2       0         0.88       0.88       0.88       0.88       0.88       0.88         2       2       2       2       2       2       2         92       948       222       248       1410       101       100       0.05       0.33       0.33       0.14       0.42       0.42       14774       2847       668       1774       3349       241       241       1774       2847       668       1774       3349       241       1774       1770       17820       293       302       1774       1770       17820       293       302       1774       1770       17820       293       302       1774       1770       1820       22       19.4       19.5       7.2       7.4       7.4       7.4       1.2       2       19.4       19.5       7.2       7.4       7.4       7.4       1.00       0.03       1.00 | 1.00       1.00 | 1.00       1.863       1863       1900       1900       1863       65       4       153       65       65       1       2       0       0       1       153       65       1       2       0       0       1       0.08       8.88       0.82       0.32       0.32       0.32       0.32       < | 1.00       0.08       0.82 | 1.00 | 1.00 |

| Movement         EBL         EBT         EBR         WBL         WBR         NBL         NBT         NBR         SBL         SBT           Lane Configurations         1< | 4    |
|---|------|
| Lane Configurations ነ ተተ ሶ ነ ነ ተ  |      |
|   | SBR  |
| Traffic Volume (veh/b) 5 860 933 115 000 30 641 30 155 155 160  |      |
|   | 5    |
| Future Volume (veh/h) 5 869 833 115 900 30 641 20 155 155 160   | 5    |
| Number 7 4 14 3 8 18 5 2 12 1 6   | 16   |
| Initial Q (Qb), veh 0 0 0 0 0 0 0 0 0   | 0    |
| Ped-Bike Adj(A_pbT) 1.00 1.00 1.00 1.00 1.00 1.00   | 1.00 |
| Parking Bus, Adj 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.0   | 1.00 |
| Adj Sat Flow, veh/h/ln 1776 1776 1667 1667 1667 1863 1863 1900 1863 1863  | 1900 |
| Adj Flow Rate, veh/h 5 905 868 120 938 31 668 21 161 161 167  | 5    |
| Adj No. of Lanes 1 2 1 1 2 1 0 1 1  | 0    |
| Peak Hour Factor         0.96         0.96         0.96         0.96         0.96         0.96         0.96         0.96         0.96         0.96  | 0.96 |
| Percent Heavy Veh, % 7 7 7 14 14 14 2 2 2 2 2 2   | 2    |
| Cap, veh/h 11 1034 807 147 1243 556 786 43 328 209 215  | 6    |
| Arrive On Green 0.01 0.31 0.31 0.09 0.39 0.39 0.23 0.23 0.23 0.12 0.12  | 0.12 |
| Sat Flow, veh/h 1691 3374 1509 1587 3167 1417 3442 186 1425 1774 1799   | 54   |
| Grp Volume(v), veh/h 5 905 868 120 938 31 668 0 182 161 0   | 172  |
| Grp Sat Flow(s), veh/h/ln 1691 1687 1509 1587 1583 1417 1721 0 1611 1774 0  | 1853 |
| Q Serve(g_s), s 0.2 18.1 21.8 5.3 18.2 1.0 13.2 0.0 7.0 6.3 0.0   | 6.4  |
| Cycle Q Clear(g_c), s 0.2 18.1 21.8 5.3 18.2 1.0 13.2 0.0 7.0 6.3 0.0   | 6.4  |
| Prop In Lane 1.00 1.00 1.00 1.00 0.88 1.00  | 0.03 |
| Lane Grp Cap(c), veh/h 11 1034 807 147 1243 556 786 0 370 209 0   | 221  |
| V/C Ratio(X) 0.45 0.88 1.08 0.82 0.75 0.06 0.85 0.00 0.49 0.77 0.00   | 0.78 |
| Avail Cap(c_a), veh/h 119 1034 807 149 1243 556 914 0 381 292 0   | 250  |
| HCM Platoon Ratio 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.0  | 1.00 |
| Upstream Filter(I) 1.00 1.00 1.00 1.00 1.00 1.00 0.00 1.00 0.00   | 1.00 |
| Uniform Delay (d), s/veh 35.2 23.4 16.6 31.7 18.6 13.4 26.3 0.0 23.8 30.4 0.0   | 30.4 |
| Incr Delay (d2), s/veh 25.5 10.3 54.0 27.9 4.3 0.2 6.8 0.0 1.0 7.9 0.0  | 12.8 |
| Initial Q Delay(d3),s/veh 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0   | 0.0  |
| %ile BackOfQ(50%),veh/ln 0.2 9.9 27.6 3.4 8.7 0.4 7.1 0.0 3.2 3.5 0.0   | 4.1  |
| LnGrp Delay(d),s/veh 60.7 33.7 70.5 59.5 22.9 13.6 33.1 0.0 24.8 38.4 0.0   | 43.2 |
| LnGrp LOS E C F E C B C C D   | D    |
| Approach Vol, veh/h 1778 1089 850 333   |      |
| Approach Delay, s/veh 51.8 26.7 31.3 40.9   |      |
| Approach LOS D C C D  |      |
| Timer 1 2 3 4 5 6 7 8   |      |
| Assigned Phs 1 2 3 4 5 6 7 8  |      |
| Phs Duration (G+Y+Rc), s 12.9 20.8 11.1 26.3 20.7 13.0 5.0 32.4   |      |
| Change Period (Y+Rc), s 4.5 4.5 4.5 4.5 4.5 4.5   |      |
| Max Green Setting (Gmax), s 11.7 16.8 6.7 21.8 18.9 9.6 5.0 23.5  |      |
| Max Q Clear Time (g_c+l1), s 8.3 9.0 7.3 23.8 15.2 8.4 2.2 20.2   |      |
| Green Ext Time (p_c), s 0.1 0.6 0.0 0.0 1.0 0.1 0.0 2.0   |      |
| Intersection Summary  |      |
|   |      |
| HCM 2010 Ctrl Delay 39.8 HCM 2010 LOS D   |      |

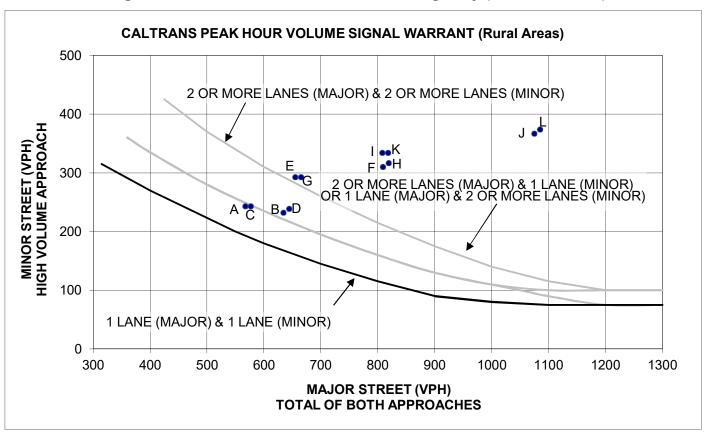
Lico Subdivision Keith Higgins Traffic Engineer

## Appendix I

Warrant

Worksheets

Intersection #1
Ridgemark Drive - Fairview Road / Airline Highway (State Route 25)



|    | Scenario    | Airline-SR 25 | RidgeFair.  | Warrant  |
|----|-------------|---------------|-------------|----------|
|    |             | East/West     | North/South | Met?     |
|    |             | (Major)       | (Minor)     | (Yes/No) |
| A. | Exist AM    | 567           | 243         | Yes      |
| B. | Exist PM    | 634           | 232         | Yes      |
| C. | Ex+Pro AM   | 577           | 243         | Yes      |
| D. | Ex+Pro PM   | 644           | 239         | Yes      |
| E. | Bkgnd AM    | 655           | 293         | Yes      |
| F. | Bkgnd PM    | 809           | 310         | Yes      |
| G. | Bk+Pro AM   | 665           | 293         | Yes      |
| Н. | Bk+Pro PM   | 819           | 317         | Yes      |
| I. | CumNoPro AM | 808           | 334         | Yes      |
| J. | CumNoPro PM | 1075          | 367         | Yes      |
| K. | Cum+Pro AM  | 818           | 334         | Yes      |
| L. | Cum+Pro PM  | 1085          | 374         | Yes      |

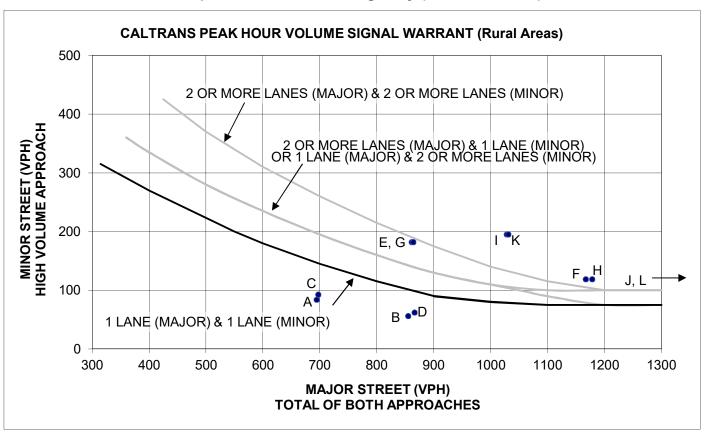
- 1. 100 VPH applies as the lower threshold volume for a minor street approach with two or more lanes and 75 VPH applies as the lower threshold volume for a minor street approaching with one lane.
- 2. Bold line applies to intersection geometry.

Warrant 3 (Part B) - Peak Hour Delay #1 - Ridgemark Drive - Fairview Road / Airline Highway (State Route 25)

| Number of Approaches to Intersection:<br>Number of Approach Lanes: | <u>iion:</u><br>NB Ridgemark:<br>SB Fairview:                          | 4 approaches<br>1 lanes<br>1 lanes   | Minimum Entering Vehicles:   | -   | 300 vehicles |
|--|--|--|--|---|--------------|
| Total Entering Volumes:  | Existing AM: Existing PM: Exist+Proj AM: Exist+Proj PM: Background AM: | 970 vehicles<br>999 vehicles<br>982 vehicles<br>1,016 vehicles<br>1,186 vehicles | Back+Proj AM:<br>Back+Proj PM:<br>CumNoPro AM:<br>CumNoPro PM:<br>Cum+Proj AM: | 1,198 vehides<br>1,303 vehides<br>1,415 vehides<br>1,645 vehides<br>1,427 vehides |              |
|  | Background PM:   | 1,286 vehicles   | Cum+Proj PM:   | 1,662 vehicles  |              |

- Notes:
  1. Warrant based on level of service calculations.
  2. NB, SB, EB, WB = Northbound, Southbound, Eastbound, Westbound.
  3. N/A = Not Applicable this evaluation does not apply to that approach.

# Intersection #2 Enterprise Road / Airline Highway (State Route 25)



|    | Scenario    | Airline-SR 25 | Enterprise  | Warrant  |
|----|-------------|---------------|-------------|----------|
|    |             | East/West     | North/South | Met?     |
|    |             | (Major)       | (Minor)     | (Yes/No) |
| A. | Exist AM    | 694           | 84          | No       |
| B. | Exist PM    | 855           | 56          | No       |
| C. | Ex+Pro AM   | 697           | 93          | No       |
| D. | Ex+Pro PM   | 866           | 62          | No       |
| E. | Bkgnd AM    | 861           | 182         | Yes      |
| F. | Bkgnd PM    | 1167          | 119         | Yes      |
| G. | Bk+Pro AM   | 864           | 182         | Yes      |
| H. | Bk+Pro PM   | 1178          | 119         | Yes      |
| I. | CumNoPro AM | 1028          | 195         | Yes      |
| J. | CumNoPro PM | 1437          | 130         | Yes      |
| K. | Cum+Pro AM  | 1031          | 195         | Yes      |
| L. | Cum+Pro PM  | 1448          | 130         | Yes      |

- 1. 100 VPH applies as the lower threshold volume for a minor street approach with two or more lanes and 75 VPH applies as the lower threshold volume for a minor street approaching with one lane.
- 2. Bold line applies to intersection geometry.

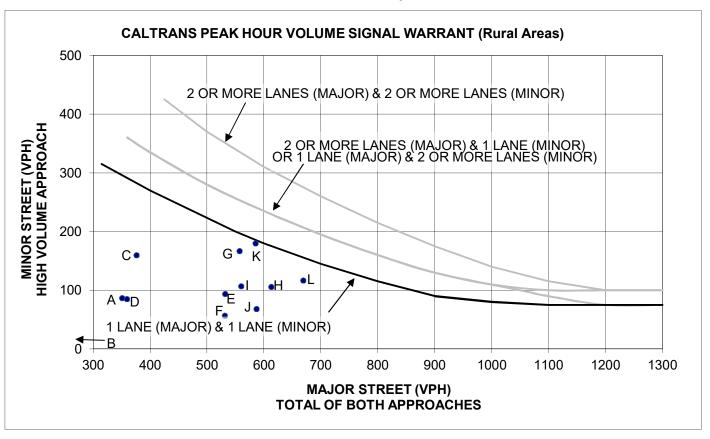
# Warrant 3 (Part B) - Peak Hour Delay #2 - Enterprise Road / Airline Highway (State Route 25)

| sels  |  |
|---|--|
| y Vehicles: 800 vehicles  | 1,158 vehides 1,371 vehides 1,338 vehides 1,652 vehides 1,350 vehides 1,669 vehides              |
| Minimum Entering Vehicles:                                      | Back+Proj AM: Back+Proj PM: CumNoPro AM: CumNoPro PM: Cum+Proj AM: Cum+Proj AM:                  |
| 4 approaches<br>1 lanes<br>1 lanes                              | 844 vehicles<br>956 vehicles<br>856 vehicles<br>973 vehicles<br>1,146 vehicles<br>1,354 vehicles |
| <u>ction:</u><br>NB Enterprise:<br>SB Enterprise:               | Existing AM: Existing PM: Exist+Proj AM: Exist+Proj PM: Background AM: Background PM:            |
| Number of Approaches to Intersection: Number of Approach Lanes: | Total Entering Volumes:  |

|                      | n                  |                |            |            |            |            |            |            |            |            |            |            |            |            |            |            |            |            |            |            |            |            |            |            |            |             |
|----------------------|--------------------|----------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|-------------|
|                      | Warrant            | ) Met?         | ON         | 9          | ON         | NO         | ON         | 9          | ON         | NO         | ON         | NO         | ON         | NO         | ON         | ON         | ON         | NO         | ON         | NO         | ON         | NO         | ON         | NO         | ON         | 2           |
| At least             | 800 Veh?           | (Intersection) | YES        | \<br>\<br>\ |
| Min. Approach Vols?  | 150 Veh            | (Two-Lane)     | N/A        | N/A        | V/A        | N/A        | A/N        | N/A        | V/A        | N/A        | N/A        | N/A        | V/A        | N/A        | V/A        | N/A        | V/V        | V/N         |
| Min. Appre           | 100 Veh            | (One-Lane)     | ON         | ON.        | ON         | ON         | ON         | ON         | ON         | ON         | YES        | YES        | ON         | YES        | YES        | YES        | ON         | YES        | YES        | YES        | ON         | YES        | YES        | YES        | ON         | VEV.        |
| ach Delay?           | 5 Veh-Hrs          | (Two-Lane)     | N/A        | N/A        | N/A        | N/A        | N/A        | A/N        | A/N        | N/A        | A/N        | N/A        | N/A        | N/A        | A/N        | N/A        | A/N        | N/A        | N/A        | Δ/N         |
| Min. Approach Delay? | 4 Veh-Hrs          | (One-Lane)     | ON         | ON         | ON         | NO         | ON         | ON         | ON         | NO         | ON         | NO         | ON         | ON         | ON         | ON         | ON         | NO         | ON         | ON         | ON         | NO         | ON         | ON         | ON         | CZ          |
|                      | <b>Total Delay</b> | (hours)        | 0.37       | 0.25       | 0.28       | 0.16       | 0.40       | 0.25       | 0.31       | 0.17       | 0.70       | 0.89       | 0.73       | 0.65       | 0.74       | 0.87       | 62'0       | 0.68       | 1.31       | 1.22       | 2.49       | 1.46       | 1.38       | 1.25       | 2.71       | 1 53        |
| <b>Total Vehicle</b> | Delay              | (sec)          | 1,327      | 868        | 1,014      | 290        | 1,423      | 911        | 1,110      | 603        | 2,534      | 3,221      | 2,618      | 2,356      | 2,654      | 3,149      | 2,849      | 2,463      | 4,727      | 4,407      | 8,968      | 5,265      | 4,960      | 4,505      | 9,746      | 5 525       |
| Average              | Vehicle Delay      | (sec)          | 15.8       | 13.6       | 18.1       | 13.1       | 15.3       | 13.8       | 17.9       | 13.4       | 24.6       | 17.7       | 38.5       | 19.8       | 23.7       | 17.3       | 38.5       | 20.7       | 41.1       | 22.6       | 105.5      | 40.5       | 40.0       | 23.1       | 107.1      | 10 E        |
| No. of               | Stopped            | Vehicles       | 84         | 99         | 99         | 45         | 63         | 99         | 62         | 45         | 103        | 182        | 89         | 119        | 112        | 182        | 74         | 119        | 115        | 195        | 85         | 130        | 124        | 195        | 91         | 130         |
|                      | Peak               | Hour           | AM         | AM         | PM         | PM         | AM         | AM         | PM         | DM          |
|                      |                    | Scenario       | Existing   | Existing   | Existing   | Existing   | Exist+Proj | Exist+Proj | Exist+Proj | Exist+Proj | Background | Background | Background | Background | Back+Proj  | Back+Proj  | Back+Proj  | Back+Proj  | CumNoPro   | CumNoPro   | CumNoPro   | CumNoPro   | Cum+Proj   | Cum+Proj   | Cum+Proj   | Cum+Proi    |
|                      |                    | Direction      | NB         | SB         | NB         | a<br>a      |
|                      |                    | Street         | Enterprise  |

- Notes:
  1. Warrant based on level of service calculations.
  2. NB, SB, EB, WB = Northbound, Southbound, Eastbound, Westbound.
  3. N/A = Not Applicable this evaluation does not apply to that approach.

# Intersection #3 Southside Road / Enterprise Road



|    | Scenario    | Southside   | Enterprise | Warrant  |
|----|-------------|-------------|------------|----------|
|    |             | North/South | East/West  | Met?     |
|    |             | (Major)     | (Minor)    | (Yes/No) |
| A. | Exist AM    | 351         | 87         | No       |
| B. | Exist PM    | 277         | 36         | No       |
| C. | Ex+Pro AM   | 376         | 160        | No       |
| D. | Ex+Pro PM   | 359         | 85         | No       |
| E. | Bkgnd AM    | 532         | 94         | No       |
| F. | Bkgnd PM    | 531         | 57         | No       |
| G. | Bk+Pro AM   | 557         | 167        | No       |
| Н. | Bk+Pro PM   | 613         | 106        | No       |
| I. | CumNoPro AM | 560         | 107        | No       |
| J. | CumNoPro PM | 587         | 68         | No       |
| K. | Cum+Pro AM  | 585         | 180        | No       |
| L. | Cum+Pro PM  | 669         | 117        | No       |

- 1. 100 VPH applies as the lower threshold volume for a minor street approach with two or more lanes and 75 VPH applies as the lower threshold volume for a minor street approaching with one lane.
- 2. Bold line applies to intersection geometry.

# Warrant 3 (Part B) - Peak Hour Delay #3 - Southside Road / Enterprise Road

Total Entering Volumes:

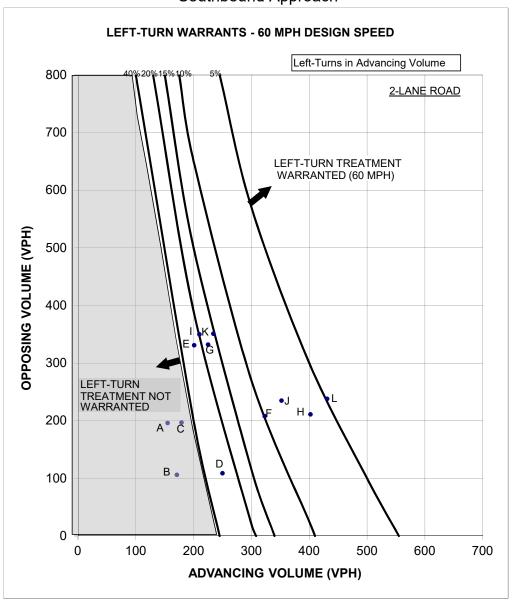
650 vehicles Minimum Entering Vehicles: 3 approaches 1 lanes WB Enterprise: Number of Approaches to Intersection: Number of Approach Lanes:

724 vehicles 719 vehicles 667 vehicles 655 vehicles 765 vehicles 786 vehicles Back+Proj AM: Back+Proj PM: CumNoPro AM: CumNoPro PM: Cum+Proj AM: Cum+Proj PM: 438 vehicles 313 vehicles 536 vehicles 444 vehicles 626 vehicles 588 vehicles Existing AM:
Existing PM:
Exist+Proj AM:
Exist+Proj PM: Background AM: Background PM:

|                      |                    | -              |           |           |            |            |            |            |           |           |           |           |           |           |
|----------------------|--------------------|----------------|-----------|-----------|------------|------------|------------|------------|-----------|-----------|-----------|-----------|-----------|-----------|
|                      | Warrant            | Met?           | ON        | ON        | ON         | ON         | ON         | ON         | ON        | ON        | ON        | ON        | ON        | ON        |
| At least             | 650 Veh?           | (Intersection) | ON        | ON        | ON         | ON         | ON         | ON         | YES       | YES       | YES       | YES       | YES       | YES       |
| Min. Approach Vols?  | 150 Veh            | (Two-Lane)     | N/A       | N/A       | N/A        | N/A        | N/A        | N/A        | N/A       | N/A       | N/A       | N/A       | N/A       | N/A       |
| Min. Appro           | 100 Veh            | (One-Lane)     | ON        | ON        | YES        | ON         | ON         | ON         | YES       | YES       | YES       | ON        | YES       | YES       |
| Min. Approach Delay? | 5 Veh-Hrs          | (Two-Lane)     | N/A       | N/A       | N/A        | N/A        | N/A        | N/A        | N/A       | N/A       | N/A       | N/A       | N/A       | N/A       |
| Min. Appro           | 4 Veh-Hrs          | (One-Lane)     | ON        | ON        | ON         | ON         | ON         | ON         | ON        | ON        | ON        | NO        | ON        | ON        |
|                      | <b>Total Delay</b> | (hours)        | 0.26      | 60'0      | 0.52       | 0.23       | 0.34       | 0.19       | 99.0      | 0.38      | 0.42      | 0.24      | 0.75      | 0.45      |
| Total Vehicle        | Delay              | (sec)          | 940       | 338       | 1,856      | 833        | 1,213      | 069        | 2,388     | 1,378     | 1,498     | 857       | 2,682     | 1,626     |
| Average              | Vehicle Delay      | (sec)          | 10.8      | 9.4       | 11.6       | 8.6        | 12.9       | 12.1       | 14.3      | 13.0      | 14.0      | 12.6      | 14.9      | 13.9      |
| No. of               | Stopped            | Vehicles       | 87        | 36        | 160        | 85         | 94         | 22         | 167       | 106       | 107       | 89        | 180       | 117       |
|                      | Peak               | Hour           | AM        | PM        | AM         | PM         | AM         | ЬM         | AM        | PM        | AM        | PM        | AM        | PM        |
|                      |                    | Scenario       | Existing  | Existing  | Exist+Proj | Exist+Proj | Background | Background | Back+Proj | Back+Proj | CumNoPro  | CumNoPro  | Cum+Proj  | Cum+Proj  |
|                      |                    | Direction      | WB        | WB        | WB         | WB         | WB         | WB         | WB        | WB        | WB        | WB        | WB        | WB        |
|                      |                    | Street         | El Rancho | El Rancho | El Rancho  | El Rancho  | El Rancho  | El Rancho  | El Rancho | El Rancho | El Rancho | El Rancho | El Rancho | El Rancho |

- Warrant based on level of service calculations.
   NB, SB, EB, WB = Northbound, Southbound, Eastbound, Westbound.
   N/A = Not Applicable this evaluation does not apply to that approach.

# Intersection #3 Southside Road / Enterprise Road Southbound Approach

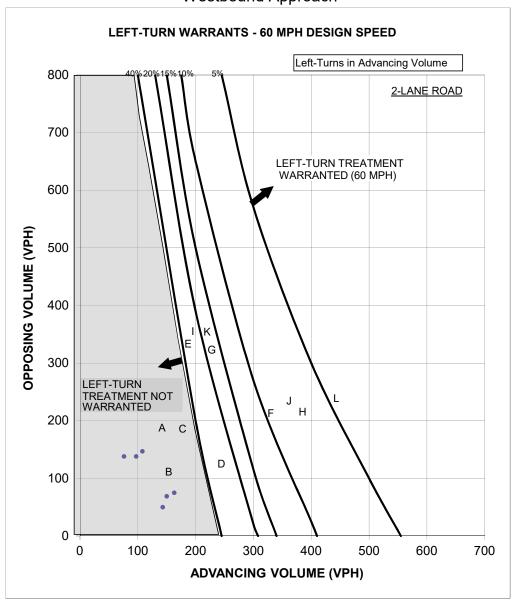


|    | Scenario    | Advancing | Opposing | % Left-Turn | Warrant Met? |
|----|-------------|-----------|----------|-------------|--------------|
| A. | Existing AM | 155       | 196      | 8%          | No           |
| B. | Existing PM | 171       | 106      | 19%         | No           |
| C. | Ex+Pro AM   | 179       | 197      | 21%         | No           |
| D. | Ex+Pro PM   | 250       | 109      | 45%         | Yes          |
| E. | Bkgnd AM    | 201       | 331      | 6%          | No           |
| F. | Bkgnd PM    | 323       | 208      | 10%         | Yes          |
| G. | Bk+Pro AM   | 225       | 332      | 16%         | No           |
| Н. | Bk+Pro PM   | 402       | 211      | 28%         | Yes          |
| I. | CumNoPro AM | 210       | 350      | 7%          | No           |
| J  | CumNoPro PM | 352       | 235      | 11%         | Yes          |
| K  | Cum+Pro AM  | 234       | 351      | 17%         | No           |
| L  | Cum+Pro PM  | 431       | 238      | 27%         | Yes          |

Source: Transportation Research Board, "Intersection Channelization Guide", NCHRP Report 279, November, 1985

# Keith Higgins Traffic Engineer

# Intersection #10 Project Access West / Enterprise Road Westbound Approach

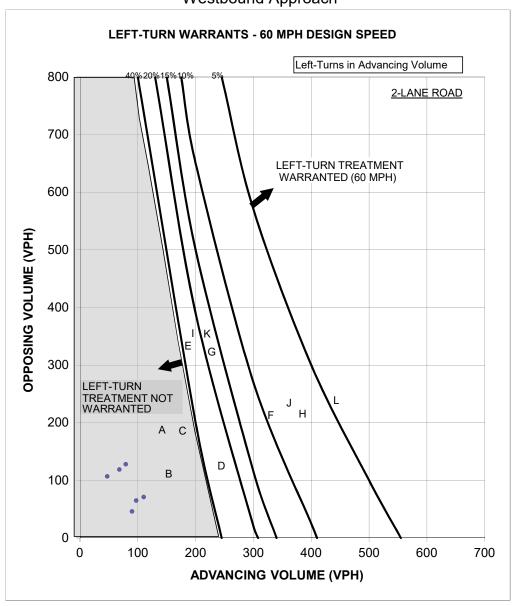


|    | Scenario   | Advancing | Opposing | % Left-Turn | Warrant Met? |
|----|------------|-----------|----------|-------------|--------------|
| A. | Ex+Pro AM  | 143       | 50       | 1%          | No           |
| B. | Ex+Pro PM  | 76        | 138      | 4%          | No           |
| C. | Bk+Pro AM  | 150       | 69       | 1%          | No           |
| D. | Bk+Pro PM  | 97        | 138      | 3%          | No           |
| E. | Cum+Pro AM | 163       | 75       | 1%          | No           |
| F. | Cum+Pro PM | 108       | 147      | 3%          | No           |

Source: Transportation Research Board, "Intersection Channelization Guide", NCHRP Report 279, November, 1985

# Keith Higgins Traffic Engineer

# Intersection #11 Project Access East / Enterprise Road Westbound Approach



|    | Scenario   | Advancing | Opposing | % Left-Turn | Warrant Met? |
|----|------------|-----------|----------|-------------|--------------|
|    |            | ŭ         | •        |             |              |
| A. | Ex+Pro AM  | 90        | 46       | 2%          | No           |
| В. | Ex+Pro PM  | 47        | 107      | 17%         | No           |
| C. | Bk+Pro AM  | 97        | 65       | 2%          | No           |
| D. | Bk+Pro PM  | 68        | 119      | 12%         | No           |
| E. | Cum+Pro AM | 110       | 71       | 2%          | No           |
| F. | Cum+Pro PM | 79        | 128      | 10%         | No           |

Source: Transportation Research Board, "Intersection Channelization Guide", NCHRP Report 279, November, 1985

# Appendix K

Will Serve Letter

## Sunnyslope County Water District

3570 Airline Highway Hollister, California 95023-9702

Phone (831) 637-4670 Fax (831) 637-1399

November 26, 2019

San Benito Engineering & Surveying, Inc. Attn. Anne Hall 502 Monterey St. Hollister, CA, 95023

Re: Letter of Intent to Provide Water and Sanitary Sewer Service to Proposed Vista Del

Calabria Development on Enterprise Road

Ms. Hall:

The Sunnyslope County Water District intends to provide water service to the proposed Vista Del Calabria development south of Enterprise Road and east of the existing Oak Creek subdivision. This is within the District boundary and adjacent to existing District water distribution pipelines. The District currently has the water supplies and infrastructure necessary to serve additional development within the Hollister Urban Area defined in the Hollister Urban Area Water and Wastewater Master Plan (HUAWWMP) including this development, especially as it was specifically anticipated in this plan's update in 2017.

Additionally, Sunnyslope County Water District intends to provide sanitary sewer service for this development as it lies within the District's sanitary sewer service area identified in the HUAWWMP. There is sufficient capacity at the District's Ridgemark Wastewater Treatment Plant to serve this development. However, the developer is required to ensure that the existing collections system has capacity to properly serve the development and shall be responsible for upsizing any sewer lines if needed.

Sunnyslope County Water District shall review, comment, and sign the development Improvement Plans prior start of construction. Additionally the developer must enter into a Facilities and Service Agreement with the District further dictating the specific terms and conditions of water and wastewater service for the development. The District may rescind or withdraw its intent to serve this Development if emergency drought measures require the cessation of new water meter connections within the District, or if other unforeseen circumstances limit either the capacity or ability for the District to provide water services.

Please do not hesitate to give me a call at 831-637-4670 if you have any clarifying questions. Thank you.

Sincerely,

Rob Hillebrecht, P.E.

ett Ment