Appendix

Appendix C Preliminary Drainage Study

Appendix

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Preliminary Drainage Study Creekside San Juan Capistrano, California



January 10, 2020

Prepared for Integral Communities

Prepared by





ATTESTATION

This report has been prepared by, and under the direction of, the undersigned, a duly Registered Civil Engineer in the State of California. Except as noted, the undersigned attests to the technical information contained herein, and has judged to be acceptable the qualifications of any technical specialists providing engineering data for this report, upon which findings, conclusions, and recommendations are based.

wamu

James H. Kawamura, P.E. Registered Civil Engineer No. C30560 Exp. 3/31/22



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Section 1 Purpose and Scope

This drainage study presents an analysis of the hydrology associated with the proposed residential development located on the intersection of Rancho Viejo Road and Malaspina Road, in the City of San Juan Capistrano, County of Orange. The study details the general project characteristics, the design, criteria and methodology applied to the analysis of the area in terms of drainage and associated conveyance facilities.

The plans and specifications in the drainage study are not for construction purposes; the contractor shall refer to final approved construction documents for plans and specifications.

Section 2 Project Information

2.1 Project Description

The proposed "Creekside" residential development entails the demolition of an existing surface parking lot, landscaping, and single story vacant building for the new construction of approximately 16.877 acres for 107 single-family residences and 81 town home units. The proposed project includes realignment of a portion of Rancho Viejo Road, private interior streets, driveways, visitor parking spaces, sidewalks, landscaping, a community recreation center, and various open space areas.

2.1.1 Project Location

Figure 1 below illustrates the project vicinity and Figure 2 provides an aerial perspective of the project site and immediate surroundings.

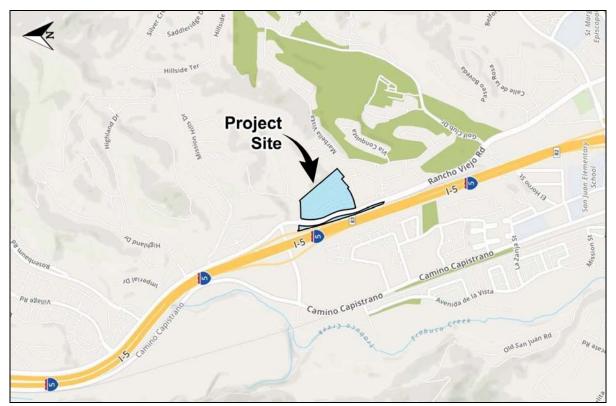


Figure 1 – Project Vicinity Map



Figure 2 – Aerial Perspective of Project Site

2.2 Hydrologic Setting

This section summarizes the project's size and location in the context of the larger watershed perspective, topography, soil and vegetation conditions, percent impervious area, natural and infrastructure drainage features, and other relevant hydrologic and environmental factors to be protected specific to the project area's watershed.

2.2.1 Watershed

The proposed project is located within the 29 square mile San Juan Creek Watershed. The receiving waters directly affected by the proposed development includes Arroyo Trabuco Creek.

2.2.2 Existing Topography, Drainage Patterns, and Facilities (Narrative)

The site topography has an elevation change of 76 feet from the east boundary to the northwest portion.

Rancho Viejo Road slopes from south to north and Malaspina Road slopes from east to west. The project site receives run-on from the hillside located on the east portion. The hillside consists of concrete storm ditches that direct runoff onto the site at two different directions towards the easterly parking lot. Runoff on the property flows westerly towards Rancho Viejo Road along the curb and gutter until it is collected by one of the six catch basins located near the westerly property line. All catch basins connect to the City's storm drain line which varies in size from 15", 18", 21", 36", 42", and 48". The City storm drain line runs from the southeast corner of the project site and travels the southern portion of the site in a westerly direction, passing through the Interstate 5 and residential areas on Camino Capistrano Street to the west. Furthermore, the runoff then travels into the San Juan Creek and disperses into the Pacific Ocean at Doheny State Beach.

2.2.3 Adjacent Land Use

The project site is bounded by community developments to both the east and south. Rancho Viejo Road and Interstate 5 freeway is located to the west. To the north is existing residential development, commercial buildings, and open space.

2.2.4 Soil Conditions

According to the County of Orange Soils Map, the soil near the project site generally consists of soil type D (see Appendix 1).

2.2.5 Downstream Conditions

This section summarizes the existing downstream conditions and any conditions of concern with respect to erosion and/or sedimentation due to the proposed project.

The project's stormwater flows westerly towards Rancho Viejo Road and will ultimately be collected by multiple catch basins that are spread out on the project site. All catch basins will be connected to the City storm drain line and will be collected by an existing 42-inch increasing to 48-inch City storm drain pipe. The storm drain system will be connecting to various residential areas therefore, the site runoff will join captured flows from different areas. All sheet flows will be discharged into the San Juan Creek.

According to the San Juan Capistrano Hydromodification Exemption Map (see Appendix 9), the proposed catch basins and associated storm drain system that collects runoff on Rancho Viejo Road is exempt from hydromodification. The runoff collected on Malaspina Road is not exempt from hydromodification requirements.

2.2.6 Impervious Cover

The proposed project will have a net increase in total impervious area compared to the existing condition of the site. Currently, the project site is being occupied by an existing building, landscape, and multiple parking lots with a total imperviousness percentage of 54% and perviousness of 46%. The proposed residential project increases the site's overall total imperviousness percentage to 86% and decreases perviousness to 14%.

2.3 Proposed Runoff Management Facilities

The proposed facilities managing runoff from the area include:

- □ Water quality treatment control Best Management Practices (BMPs); specifically, Modular Wetlands stormwater systems.
- □ Three proposed detention tanks will be placed on the southwest side of the project site with a sizing of two 6.0' DIA x 143' and 6.0' DIA x 269'.
- A proposed drainage system will drain the project area to multiple catch basins draining towards Rancho Viejo Road and will connect into the City of San Juan Capistrano storm drain network.

Section 3 Design Criteria and Methodology

This section summarizes the design criteria and methodology applied during the drainage analysis of the project site. The design criteria and methodology follows the Orange County Drainage Area Management Plan (DAMP 2003) and the Orange County Hydrology Manual (October 1986).

3.1 Design Criteria

3.1.1 Drainage Design Criteria

Local storm drain facilities have been designed to conform to City of San Juan Capistrano, and Orange County Standards.

3.1.2 Volume-Based Water Quality Numeric Sizing

Volume-based BMPs are designed to capture and treat what is usually described as the "first flush" of runoff from a storm event. Volume-based BMPs include extended retention basins, wet retention basins, retention/infiltration systems and water quality treatment wetlands.

The sizing criterion used for volume-based Best Management Practices is described in this project's WQMP report.

3.1.3 Flow-Based Numeric Sizing

The capacity of the existing storm drain system has been established by analyzing the existing flow of the 25-year and 100-year storm events.

Flow-based BMPs have been designed to filter or otherwise treat the "first flush" of runoff from any given storm event. Flow-based BMPs include bio-filtration systems (e.g., Modular Wetlands Systems). The sizing criterion used for flow-based BMPs can be found in this project's WQMP.

3.1.4 Runoff Calculation Method

Runoff calculations for this study were accomplished using the Orange County Hydrology Rational Method. The Rational Method is a physically-based numerical method where runoff is assumed to be directly proportional to rainfall and area, less losses for infiltration and depression storage. Flows were computed based on the rational formula:

Q = 0.9 (I - Fm) A

Where:

Q = peak discharge (cfs, cubic feet per second)

C = runoff coefficient, based on land use and soil type

I = rainfall intensity (inches/hour)

A = watershed area (acres)

Fm = rate of runoff (inches/hour)

The watershed time of concentration at any given point is defined as the time it would theoretically take runoff to travel from the most upstream point in the watershed to a concentration point, as estimated by the Time of Concentration Nomograph for Initial Subarea (Figure D-4 within the Orange County Hydrology Manual and the appendix section of this report).

Intensity for this site was determined by the intensity-duration curves from the Orange County Hydrology Manuals Figure's B-3 and B-4. The runoff coefficient represents the ratio of rainfall that runs off the watershed versus the portion that infiltrates to the soil or is held in depression storage. The runoff coefficient (C) is dependent on rainfall intensity (I), soil infiltration rate (Fp), and impervious/pervious area fractions (ai and ap).

Rational Method calculations were accomplished using hand calculations. Peak discharges were computed for both 25-year and 100-year hypothetical storm return frequencies and can be seen in the hydrology and drainage analysis section of this report. The output results of the calculations can be found in the Appendix section of this report.

3.2 South Orange County Hydrology Model (SOCHM)

The South Orange County Hydrology Model software, developed and provided by Clear Creek Solutions, Inc., is a tool that calculates various parameters for analyzing hydromodification effects of predevelopment/post- project conditions and provides sizing solutions to mitigate the increased runoffs. It provides appropriate data and runs continuous simulations of site runoff to generate flow duration curves, a module for sizing or checking control measure to achieve the hydromodification control standard; and a reporting module. The peak flood values were computed for the 2-year through 25-year flood frequency. A comparison of the predevelopment and post-project flow duration curves is conducted for 100 flow levels between the lower and the upper limit. It produces a final model that counts the number of 15-minute intervals that predevelopment flows exceed each of the flow levels during the entire simulation period.

The design criteria and methodology follows the South Orange County Hydromodification Management Plan (HMP 2017) and the South Orange County Hydrology Model Guidance Manual (March 2012).

Section 4 Hydrology and Drainage Analysis

This section summarizes the quantitative hydrologic analysis of the existing and proposed conditions of the site.

4.1 Summary of Drainage Delineation

Existing Analysis Part 1 - Catch Basin #1 and Area 1 (City Main on Rancho Viejo):

The existing site is divided into 19 subareas (subareas A-S). An analysis of the existing 25-year and 100-year storms can be found in the Appendix section of this report.

East of the property there is an existing hill with a high point roughly near the middle from west to east that divides flows.

Area 1:

System 1: Runoff from <u>subareas B and C</u> on the same hill are directed southeast to an existing storm drain headwall #1A. This headwall directs the runoff to an existing 36" storm drain line directed towards the city's public system of drainage.

System 2: Runoff from <u>subarea L</u> flows to an existing catch basin A to combine with runoff from subarea K of the next southerly adjacent catch basin B. <u>Subareas L and K</u> combine with <u>Subarea</u> <u>J</u> in the 3^{rd} adjacent catch basin C at the east side of the property. This runoff joins runoff in the existing 36" private storm drain system 1:

Catch Basin #1:

System 3: <u>Subarea A</u> from the existing hill flows southwest into an existing storm drain inlet #2. The inlet joins an existing headwall empties near the adjacent Fluidmasters property, and enters another existing headwall flowing west to Rancho Viejo. This runoff then flows north to Rancho Viejo directly towards and entering Catch Basin #1:

System 4: <u>Subareas D and E</u> from the southerly side of the hill combine with <u>subarea F</u> flowing south towards the existing access road. This runoff flows west combing with <u>subarea G</u>, then H, flowing west towards Rancho Viejo, next to combine with <u>subarea I and S</u> on the same street to combine with System 3 to lead directly into Catch Basin #1.

Systems 1 through 4 combine in the existing 36" storm drain structure going towards the public city system.

Summary:

- Subareas entering Catch Basin #1 and #1A Directly: A, D, E, F, G, H, I, S
- Subareas entering Area #1: B, C, J, K, L.
- Note: All are combined at the City Main beyond the property line.

Existing Analysis Part 2 – Catch Basin #2 and Catch Basin #3 (City Main on Rancho Viejo / Malaspina Road)

Catch Basin #2:

System 1: Runoff generated from Q and P flow northwest towards Rancho Viejo to combine with Subarea R. The total runoff crosses an existing cross gutter to enter Catch Basin 2.

Catch Basin #3:

System 2: Subareas M and N flow northwest from the high point on the existing hill east of the property. This runoff combines with runoff generated from subarea O, runs west along Malaspina Road to an existing 18" storm drain structure. This combines with runoff generated

from System 1. The total runoff from systems 1 and 2 join an existing 48" storm piping system owned and maintained by the City.

Summary:

- Subareas entering Catch Basin #2 Directly: P, Q, R
- Subareas entering Catch Basin 3: M, N, O
- Note: All are combined at the City Main.

Proposed Analysis Part 1 – Catch Basin #1 and Area 1 (City Main on Rancho Viejo / Malaspina Road)

The proposed site is divided into 24 subareas (subareas A-W). An analysis of the proposed 25-year and 100-year storms can be found in the Appendix section of this report.

Catch Basin #1:

System 1: <u>Subareas B and C</u> are directed by drainage ditches to a proposed inlet on the east side of the proposed retaining wall. This runoff flows through a storm piping system to a proposed junction structure that joins the existing 36" storm drain line to empty near the adjacent Fluid Masters property.

System 2: <u>Subarea A</u> from the existing hill flows southwest into an existing storm drain inlet. The inlet joins the existing 36" storm drain line that empties through the same existing headwall located adjacent to the Fluidmasters property and combines with runoff generated from System 1. Next, this runoff flows through another storm piping system to empty on the south side of Rancho Viejo, flowing north.

System 3: <u>Subarea T</u> runs west along the access road to an existing inlet. This runoff combines with System 2 to flow towards Rancho Viejo Road to combine with <u>Subarea U</u> to eventually enter Catch Basin #1.

Area 1:

System 1: <u>Subarea D and Q</u> goes to a proposed catch basin, treated by a modular wetland unit, and combines on the southwest side of the proposed site.

System 2: <u>Subarea E</u> runs to a proposed inlet then through a storm piping system to the proposed tank at the southwest end of the site.

System 3: <u>Subareas M, R, and S</u> goes to a proposed catch basin, to be treated by a modular wetland unit, then enters into the proposed detention tank.

System 4: <u>Subarea G, I, J, K, L, N, O, and P</u> goes to its respective catch basin, to be treated by a modular wetlands unit, then flows towards Rancho Viejo through a storm piping structure to join the existing 36" storm drain city combining with systems 1, 2, and 3.

System 5: <u>Subarea Q-1</u> combines at an inlet and enters the proposed tank on the southwest side of the proposed site.

Summary:

- Subareas entering Catch Basin #1 Directly: A, B, C, T, U
- Subareas not entering Catch Basin #1 Directly but through City Main:
- D, E, G, I, J, K, L, M, N, O, P, Q, Q-1, R, S

Proposed Analysis Part 2 – Catch Basins #2 and Catch Basin #3 (City Main on Rancho Viejo / Malaspina Road)

Catch Basin #2:

System 1: Subarea V flows north along Rancho Viejo Road to Enter Catch Basin # 2.

Catch Basin #3:

System 2: Subarea F and H from the existing hill flows northwest to a proposed inlet on the east side of the proposed retaining wall. This runoff flows through a storm piping system northerly towards a proposed parkway culvert on Malaspina Road.

System 3: Subarea W is generated from the north side of the proposed retaining wall. This runoff enters Malaspina to combine with system 2 to eventually enter Catch Basin #3.

Both Systems 2 and 3 combine into the existing 48" storm drain city main.

Summary:

- Subareas entering Catch Basin #2 Directly: V
- Subareas entering Catch Basin #3 Directly: F, H, W
- Note: All are combined at the City Main.

4.2 Summary of Results

The <u>overall</u> stormwater runoff produced in the existing and proposed condition is displayed in the tables provided below.

Existing Conditions

	Q ₂₅ (cfs)	Q ₁₀₀ (cfs)	Area (ac)
Catch Basin 1 & 1A	31.18	39.99	10.50
Area 1	39.28	50.27	11.93
Combined	70.46	90.26	22.43

	Q25	Q100	Area
	(cfs)	(cfs)	(ac)
Catch Basin 2	8.71	11.13	2.74
Catch Basin 3	8.45	10.80	2.68
Combined	17.16	21.93	5.42

 $Q_{(25)total} = 87.62 \text{ cfs}$ $Q_{(100)total} = 112.19 \text{ cfs}$

Proposed Conditions

	Q25 (cfs)	Q ₁₀₀ (cfs)	Area (ac)
Catch Basin 1	27.98	35.98	9.96
Area 1	49.09	62.85	14.72
Combined	77.07	98.83	24.68

Area Q_{25} **Q**₁₀₀ (cfs) (cfs) (ac) **Catch Basin 2** 5.45 6.99 1.69 **Catch Basin 3** 5.98 7.72 1.72 Combined 11.43 14.71 3.41

 $Q_{(25)total} = 88.50 \text{ cfs}$

 $Q_{(100)total} = 113.54 \text{ cfs}$

The following tables below summarizes the results of a storm event of 100-years for the <u>on-site</u> peak runoff for existing conditions for comparison to the proposed conditions on discharge point #1. The proposed on-site conditions has a higher flowrate of 62.85 cfs compared to the existing on-site rate of 52.09 due to an increase of imperviousness, the design of the private storm drain system, and the lot line adjustment. A portion of the water will be needed to be detained on-site and will be directed to the tanks (See appendix 7 for Hydrograph).

Existing Conditions

Point of Discharge	Area	Q ₁₀₀ (cfs)
1	On-site	52.09

00 S)	Point of Discharge	Area	Q100 (cfs)
09	1	On-site	62.85

Tank Storage Capacity			
Tank	Detention volume needed (ft ³)	CMP Diameter & Length (ft.)	Vstorage tank provided (ft ³)
Α		6'x143'	4,043
В	15,300	6'x143'	4,043
С		6'x269'	7,606
Total 15,692			

4.3 Hydromodification

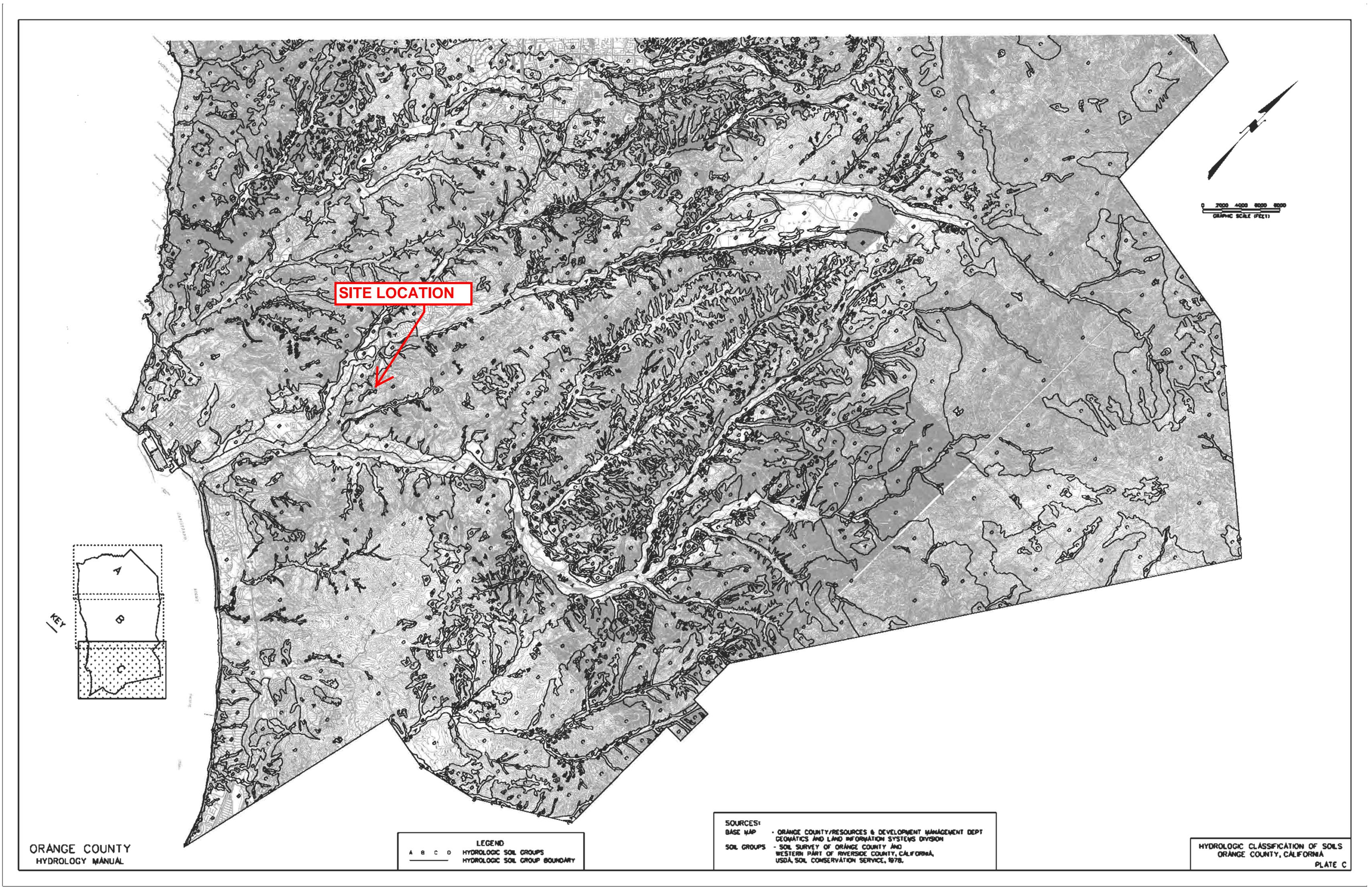
SOCHM software by Clear Creek Solutions, Inc. was used to analyze the hydromodification effects for the off-site hillside area draining to Malaspina Road. According to the calculations, at the project's flow level the flow control standards were met (see Appendix 8 for the SOHM calculations). The proposed flow rates did not exceed the pre development flow rates and are within the threshold therefore, the project does not require any hydromodification mitigation controls.

4.4 Conclusion

The proposed conditions has a higher flow rate compared to the existing flow rate due to an increase of imperviousness, the design of the proposed storm drain system, and lot line adjustment. The proposed stormwater runoff will be picked up by the private storm drain system and will flow into multiple modular wetland units for pre-treatment, then will be routed to the City storm drain network. In order for the stormwater in the proposed conditions to match with the existing conditions, the proposed tanks need to hold 15,300 cubic feet of water. The tanks has the capacity to store up to 15,692 cubic feet, which detains more than the required detention volume of 15,300 cubic feet. All tanks are sufficient to hold the required volume of stormwater before the runoff is allowed to be discharged onto the existing storm drain pipe.

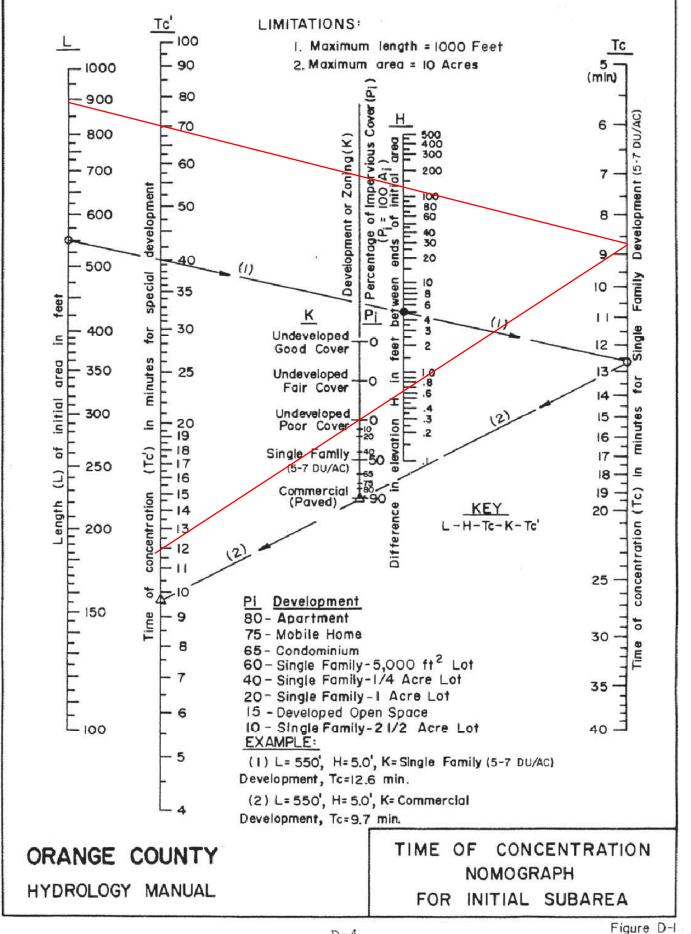
APPENDIX

Appendix 1 Soils Map



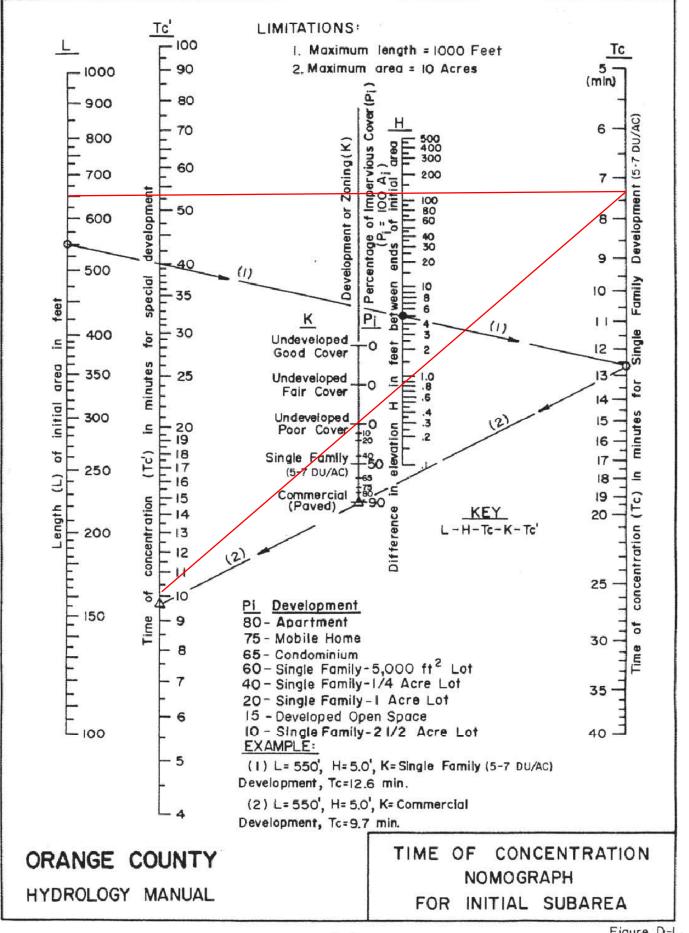
Appendix 2 Initial Subarea Time of Concentration Nomographs

EXISTING CONDITIONS - AREA A

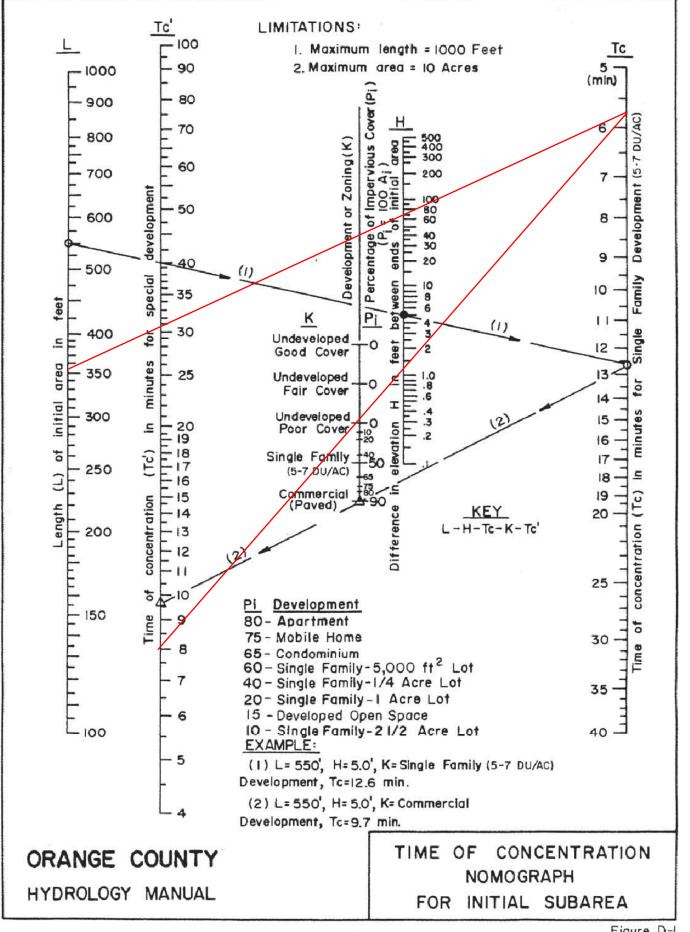


D-4

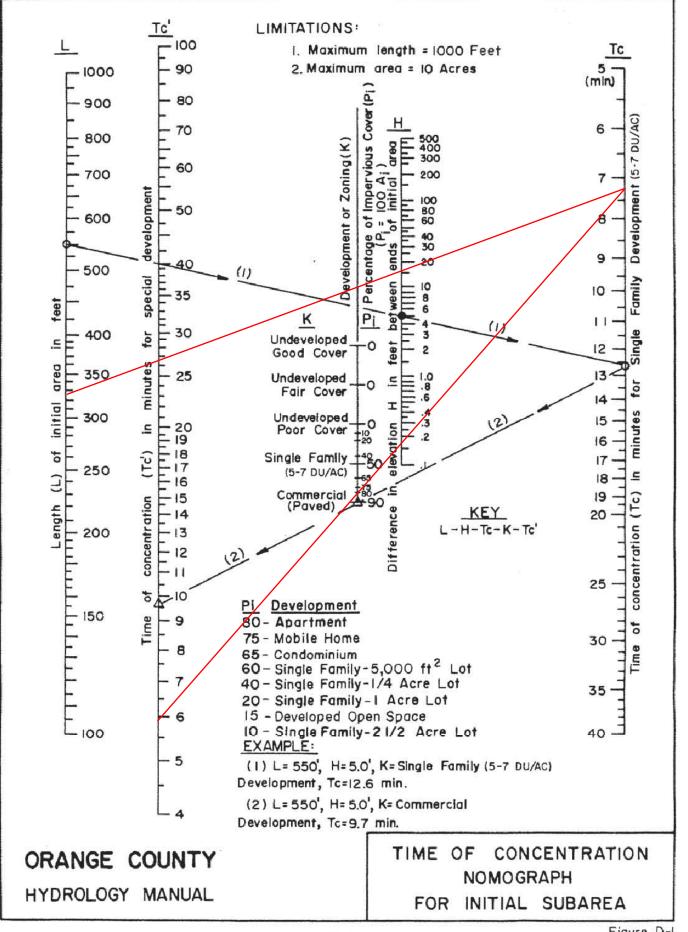
EXISTING CONDITIONS - AREA



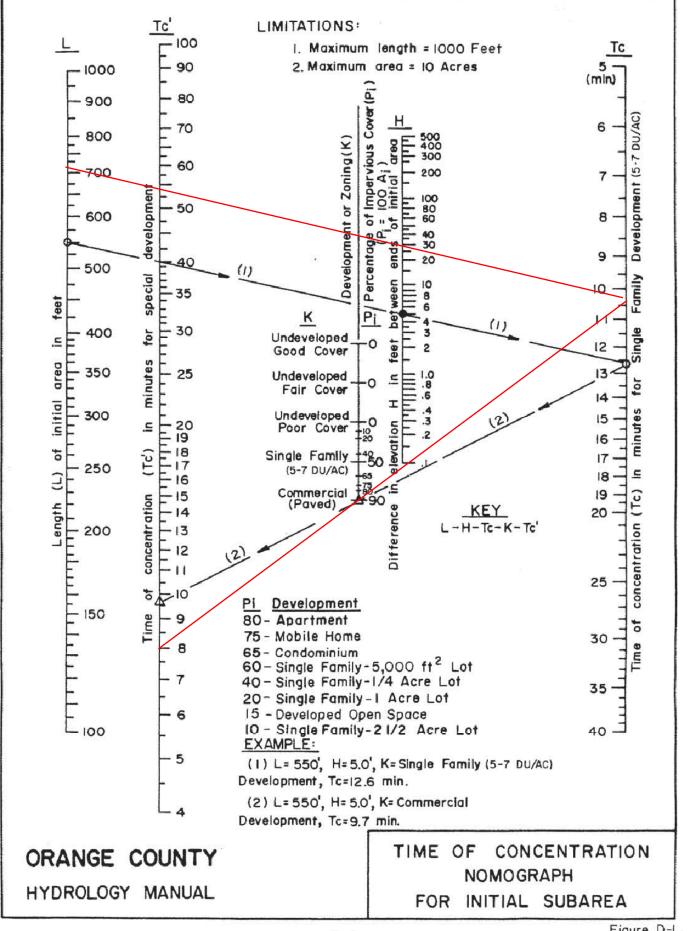
EXISTING CONDITIONS - AREA



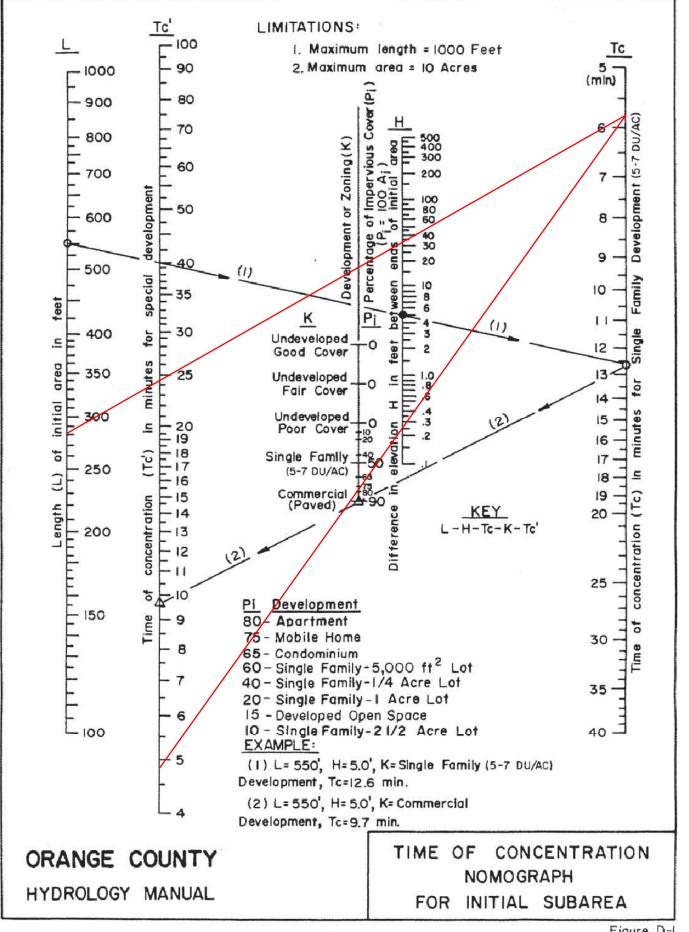
EXISTING CONDITIONS - AREA H



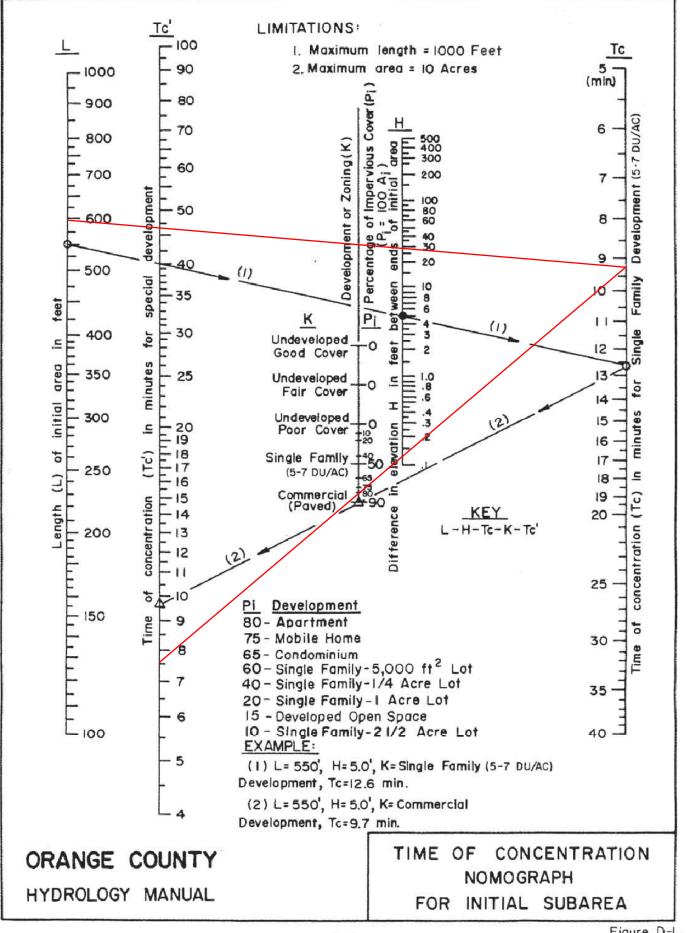
EXISTING CONDITIONS - AREA J



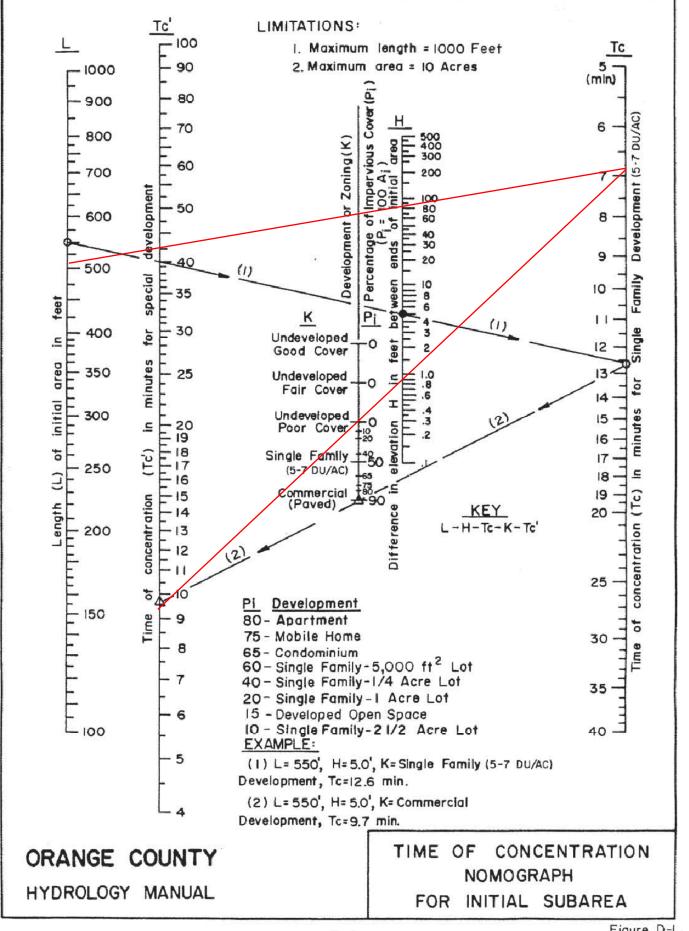
EXISTING CONDITIONS – AREA K



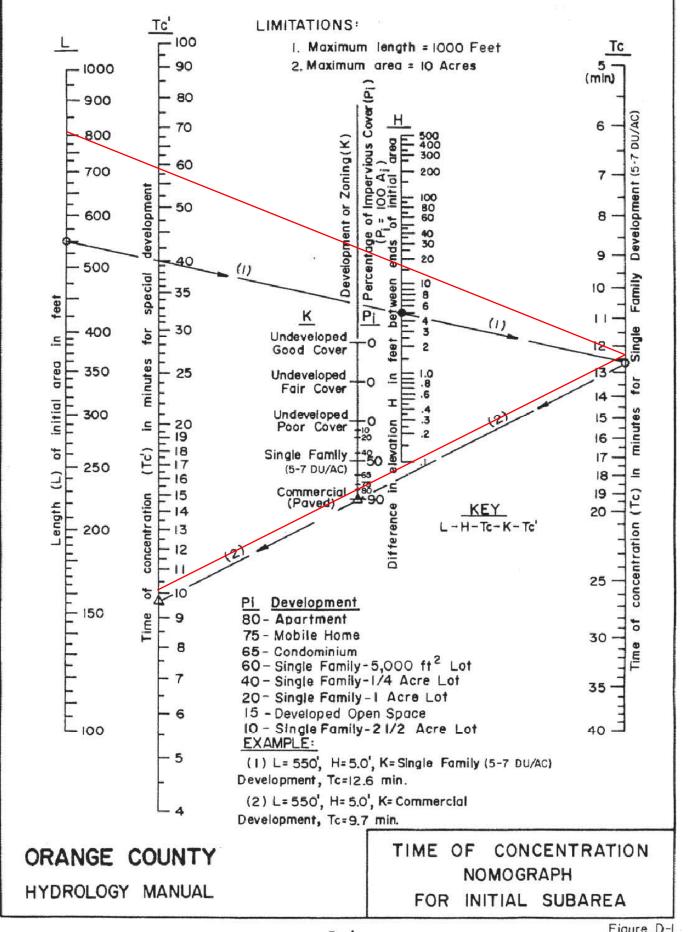
EXISTING CONDITIONS - AREA



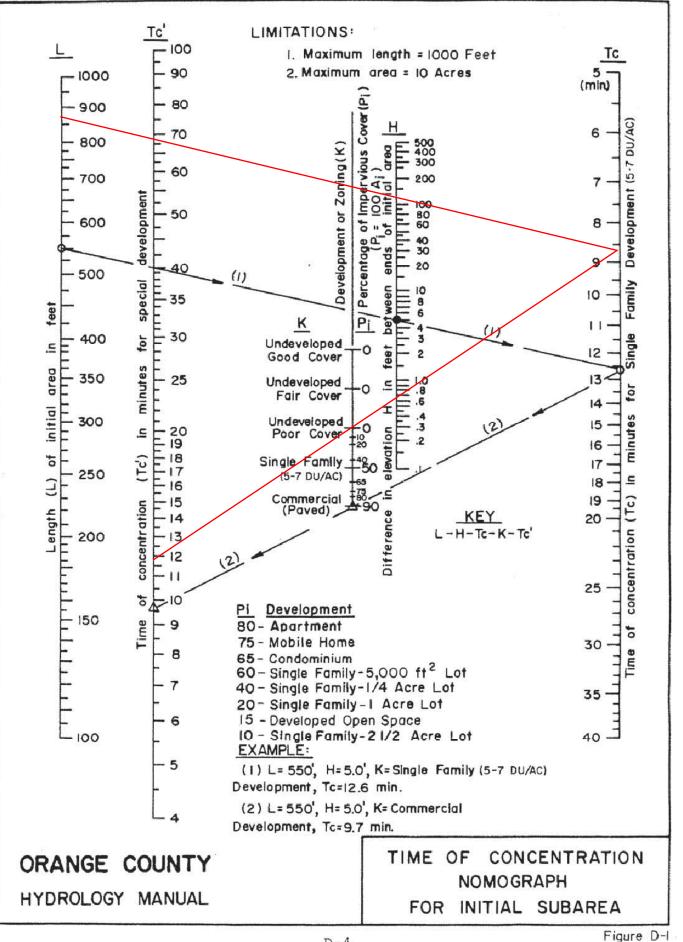
EXISTING CONDITIONS - AREA M



EXISTING CONDITIONS - AREA R

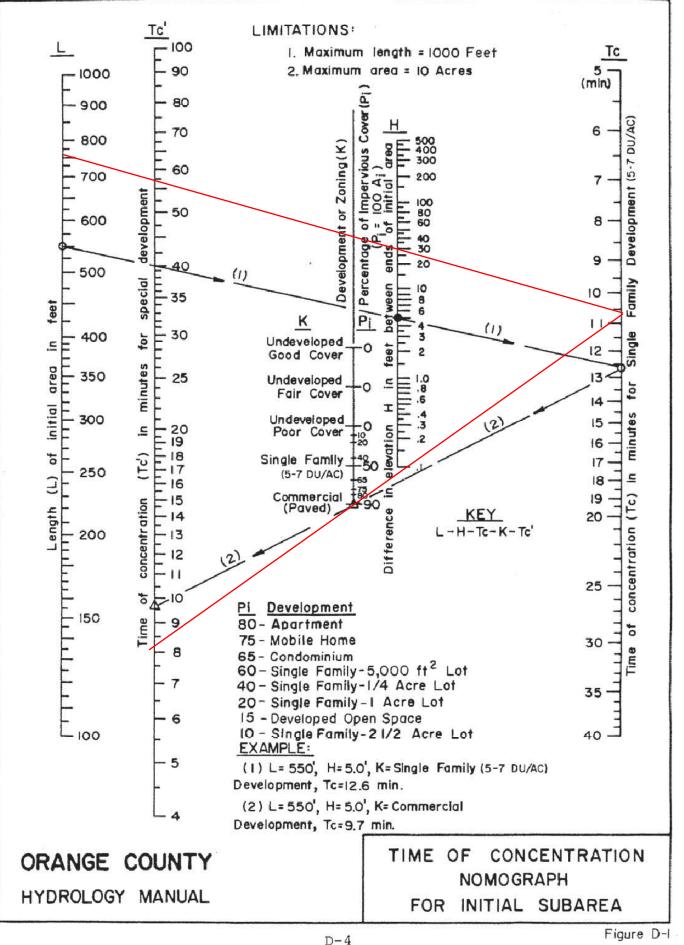


PROPOSED – *AREA* A

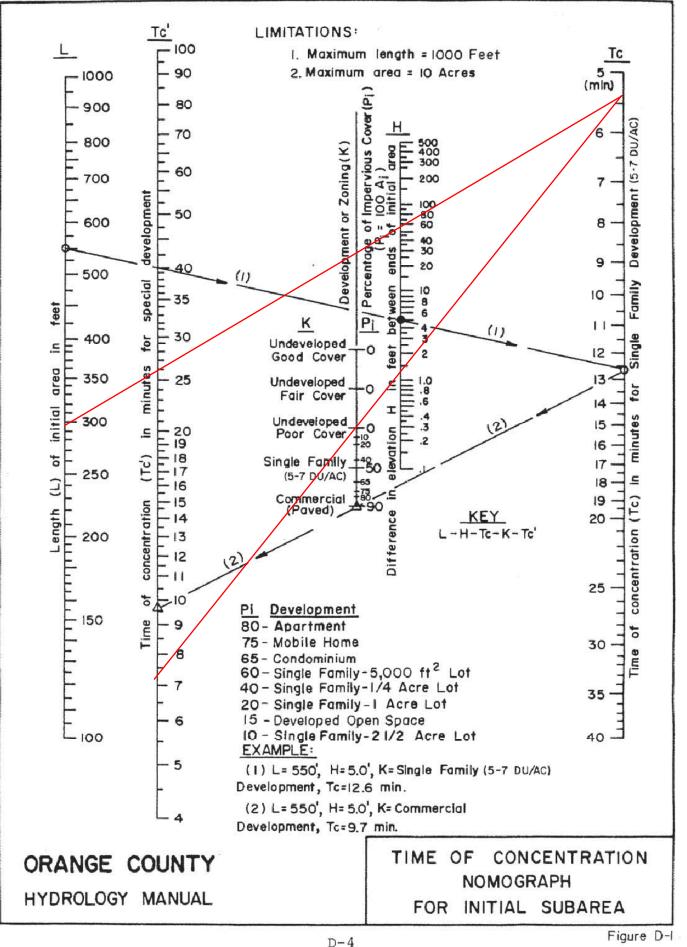


D-4

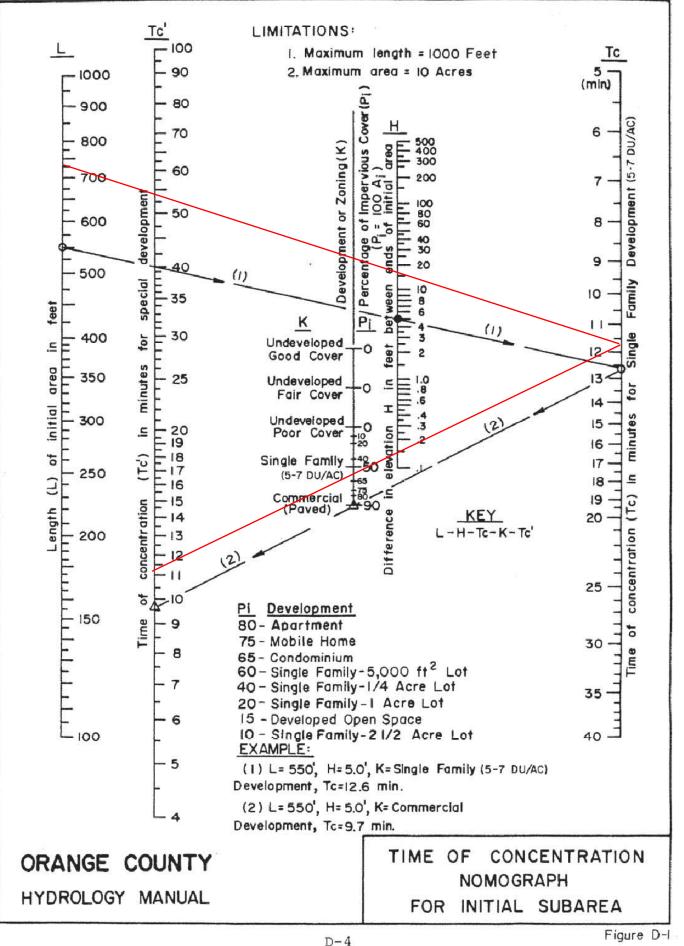
AREA D イ



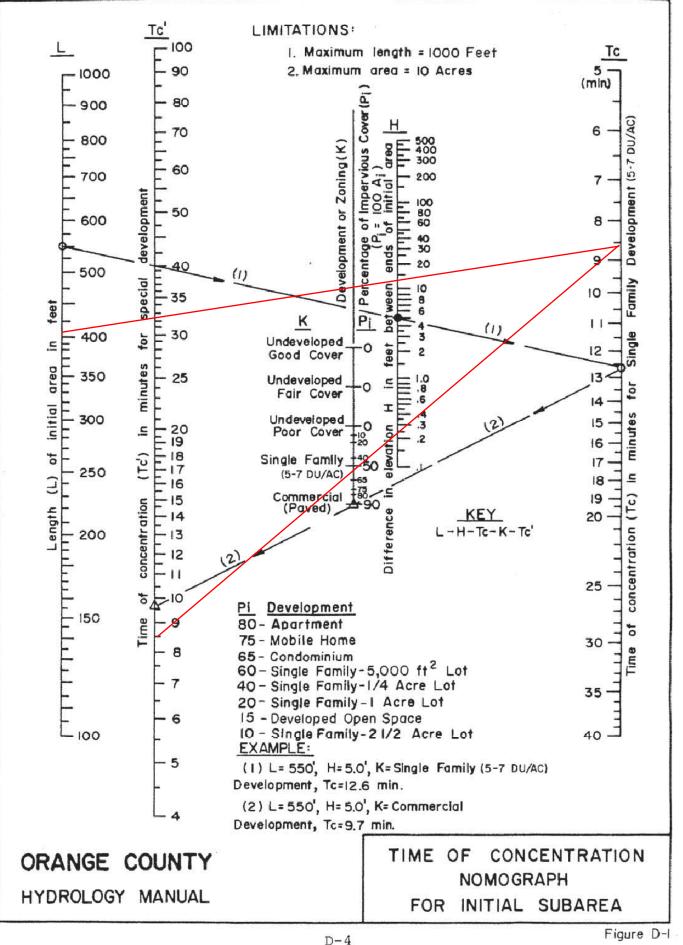
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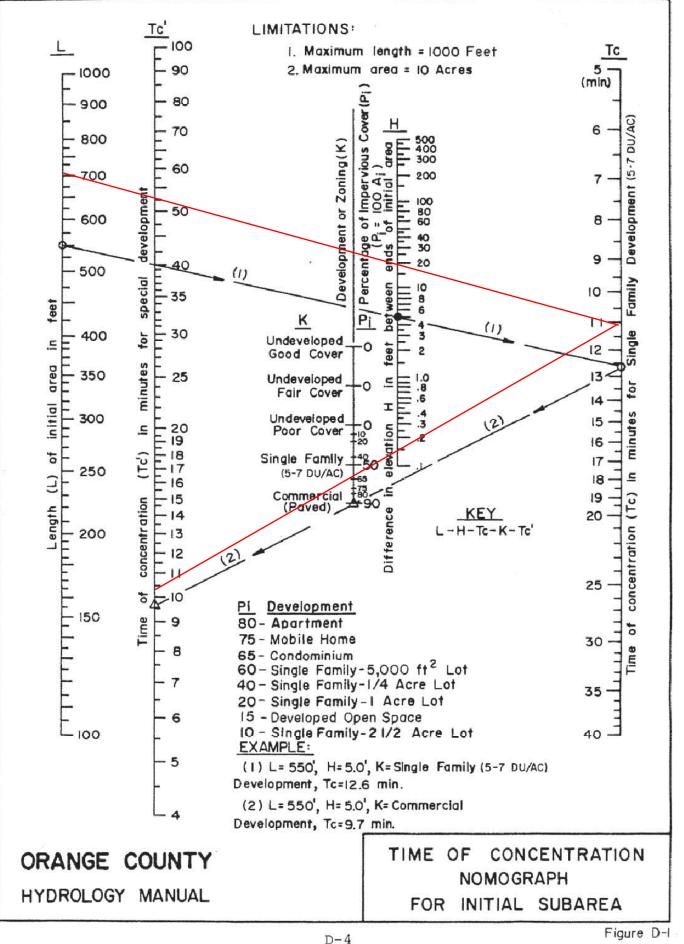
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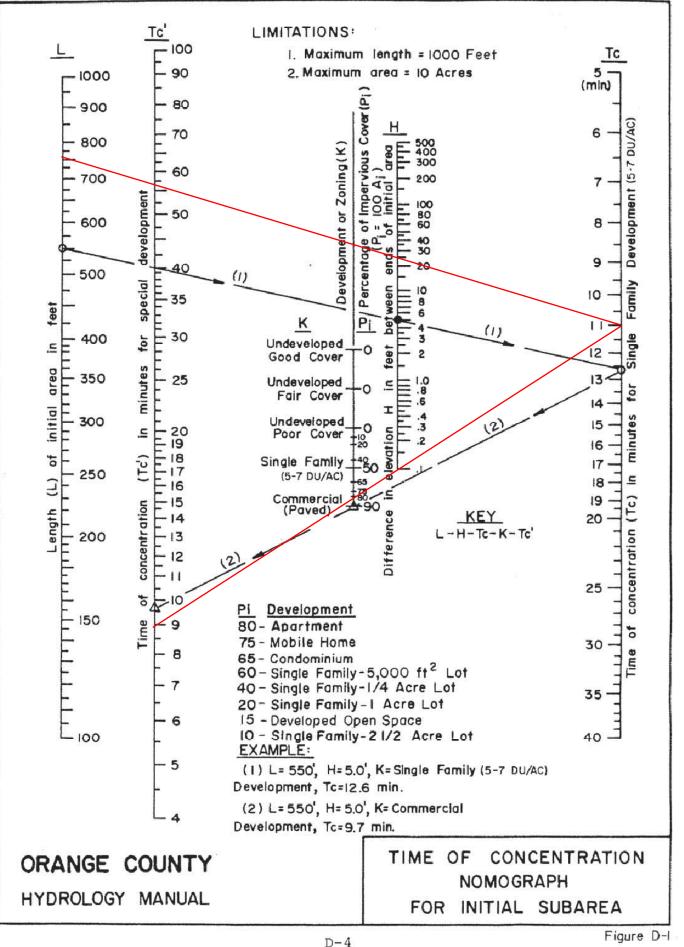
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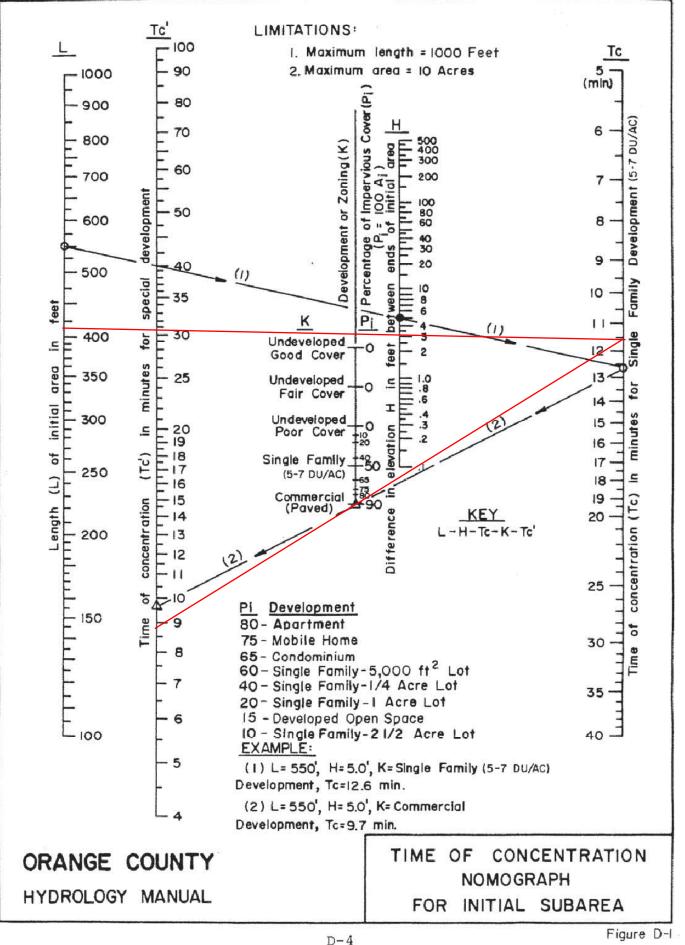


Figure D-I

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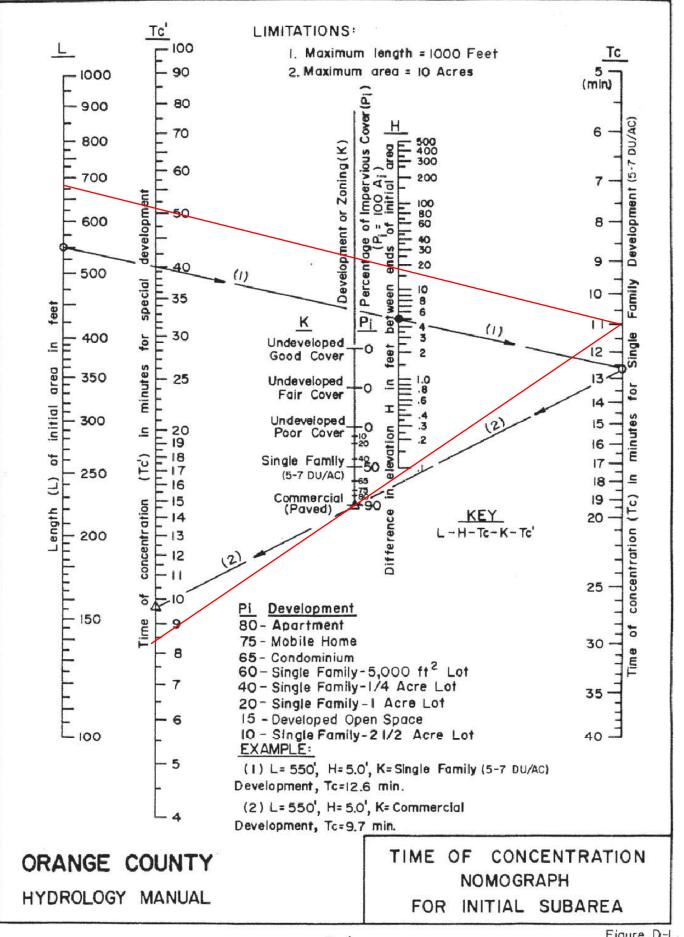


Figure D-I

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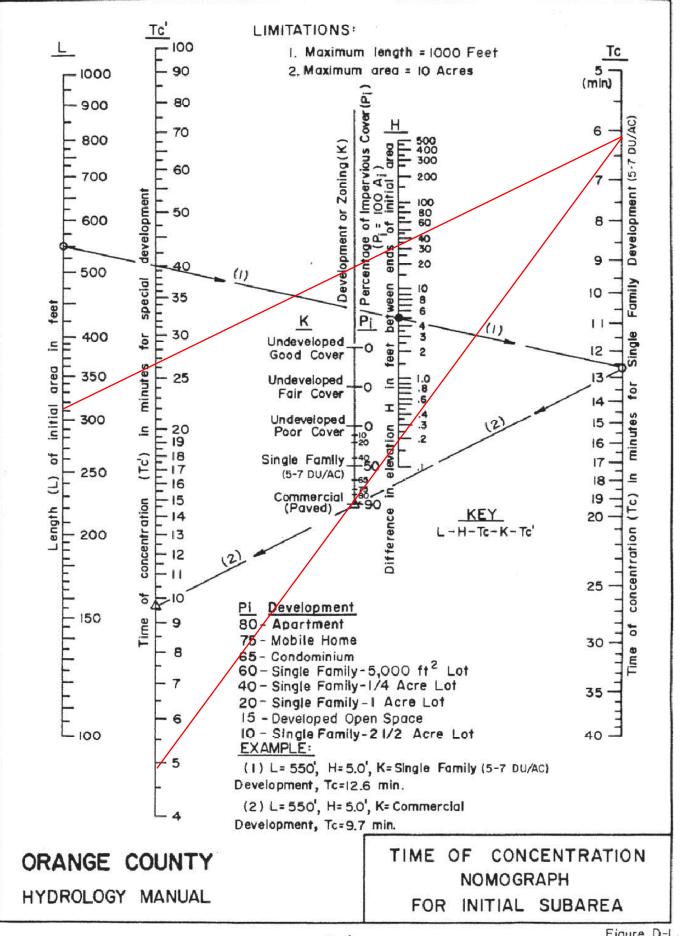


Figure D-I

Appendix 3

Hydrology Calculations for Existing Conditions-25 & 100 Year Storm

Q25 Rational Method Hydrology Calculations for Existing Improvements Project: Creekside, San Juan Capistrano

Area	Α	Α	ΣΑ	Soil	Dev	Ki	Tc	125	Fm	Fp	Fm	ai	\mathbf{a}_{p}	Q25	S ₀	L	н	d	n	K _{pipe}	D/d	D	v	-	Description
No.	(sqft)	(ac)	(ac)	type	type		(min)	(in/hr)	(in/hr)	avg	avg			(cfs)		(ft)	(ft)	(in)				(ft)	(fps)	(min)	
X-A	145615	3.34	3.34	D	Poor Grass	0.697	11.70	3.0	0.18	0.20	0.18	0.10	0.90	8.43	16.32%	864.00	141.00	1							Initial Subarea - Surface FI CB #1 (Flow 1 of 8)
	01744		- 11		Poor Grass	0.007	10.20			0.20	0.00	0.01	0.00	6.07	20.00%	650.00	120.00								Initial Subarea - Surface Fl
х-в	91744	2.11	2.11	D	Poor Grass	0.697	10.20	3.2	0.02	0.20	0.02	0.91	0.09	0.07	20.00%	650.00	139.00								Drainage Ditch
																									Area #1 (Flow 1 of 5)
X-C	26005	0.60	0.60	D	Poor Grass	0.697		3.0	0.02	0.20	0.02	0.91	0.09	1.61	19.00%	478.00	96.00							11.46	
																									36" City Storm Drain
		2.70					21.66							7.68					_			_			Area #1 (Flow 2 of 5)
(-D	46214	1.06	1.06	D	Poor Grass	0.697	8.0	3.7	0.02	0.20	0.02	0.91	0.09	3.51	19.31%	352.00	68.00								Initial Subarea - Surface
																									CB #1 (Flow 2 of 8)
K-E	12804	0.29	0.29	D	Poor Grass	0.697		3.7						0.99	17.51%	177.00	31.00							7.83	Surface Flow
		1.35					15.8							4.503											(D+E)
																									CB #1 (Flow 3 of 8)
X-F	23652		0.54	D	Commercial	0.298			0.02	0.20	0.02	0.91	0.09		0.10%	398	0.50							13.01	
		1.90					28.8							5.87											(E+F) CB #1 (Flow 4 of 8)
K-G	29195	0.67	0.67		Commercial	0 298	_	40						2.39	2.69%	446	12.00					-		7.05	
	20100	0.01	0.07	-	Commercial	0.200		1.0						2.00	2.0070	110	12.00							1.00	Existing Inlet #1 (F+0
		2.57					35.9							8.25											CB #1 (Flow 5 of 8)
к-н	10973	0.25	0.25	D	Commercial	0.298	6.00	4.4	0.02	0.20	0.02	0.91	0.09	0.98	4.89%	327	16.00								Initial Subarea - Surface
																									CB #1 (Flow 6 of 8)
X-I	34976	0.80	0.80	D	Commercial	0.298		4.0						2.90	2.00%	367	7.00							6.92	Surface Flow
																									(G+H)
		1.05					12.9							3.88											CB #1 (Flow 7 of 8)
(-J	223152	5.12	5.12	D	Commercial	0.298	8.0	3.7	0.02	0.20	0.02	0.91	0.09	16.96	4.00%	714	29.00								Initial Subarea - Surface
		5.12					8.0							16.96											Area #1 (Flow 3 of 5)
(-K	26759	0.61	0.61	D	Commercial	0.298	5.0	4.8	0.02	0.20	0.02	0.91	0.09	2.66	12.14%	280.00	34.00								Initial Subarea - Surface
		0.61												2.66											Area #1 (Flow 4 of 5)
(-L	151872		3.49	D	Commercial	0.298	<u>5.0</u> 7.5	3.8	0.02	0.20	0.02	0.91	0.09		5.18%	598.00	31.00							6.95	Initial Subarea - Surface
																									Area #1 (Flow 5 of 5)
N.4	60216	3.49	1.00		Poor Grass	0.007	7.5			0.00		0.01	0.00	11.98	15.040/		77.00								Initial Subarea - Surface
-IVI	60216	1.38	1.38	D	Poor Grass	0.697	9.4	3.4	0.02	0.20	0.02	0.91	0.09	4.18	15.24%	505	77.00								Area #2 (Flow 1 of 3)
-N	26949	0.62	0.62		Poor Grass	0.697	_	32						1.76	11.68%	308	36.00					-		10.60	Surface Flow
	20040	2.00	0.02		1 001 01033	0.007	20.0							5.93	11.0070	000	00.00							10.00	Area #2 (Flow 2 of 3)
-0	29467	0.68	0.68	D	Commercial	0.298		4.1						2.52	4.25%	470	20.00							6.57	
		2.68					26.6							8.45											Area #2 (Flow 3 of 3)
(-P	21943	0.50	0.50	D	Poor Grass	0.697		4.1						1.86	14.81%	108	16.00						_	6.64	
							6.6																		CB #2 (Flow 1 out of 3)
(-Q	39650	0.91	0.91	D	Poor Grass	0.697		3.7						3.01	17.27%	191	33.00							8.09	
							14.7								1 00%										CB #2 (Flow 2 out of 3)
K-R	5/6/1	1.32	1.32	U	Commercial	0.298	10.2	3.2						3.84	1.82%	/14	13.00								Initial Subarea - Surface CB #2 (Flow 3 out of 3)
		2.74					24.9							8.71											55 #2 (1 10W 5 Out 01 5)
<-S	153982	3.53	3.53	D	Commercial	0.298	9.5	3.4	0.02	0.20	0.02	0.91	0.09	10.61	3.00%	929	26.00								Initial Subarea - Surface
																									CB #1 (Flow 8 of 8)

Q25 Rational Method Hydrology Calculations for Existing Improvements Project: Creekside, San Juan Capistrano

Legena:

A Area of subarea (acres)

- ΣA Total area (acres)
- **a**_i Fractional portion of impervious area
- **a**_p Fractional portion of pervious area
- **F**_p Infiltration rate (in inches per hour)
- F_m Rate of runoff (in inches per hour) = $a_p F_p$

Length Flowpath length (feet)

Ave S Average slope of subarea (ft/ft)

- **T**_c Time of concentration (minutes; 5 minute minimum)
- T_t Travel time (minutes) between points of concentration
- I Rainfall intensity (in/hr) in non-mountainous areas for 100-yr frequency, $I_t = 11.995 t^{-0.566}$

 Q_{100} Peak discharge (cfs) = 0.9(I-F_m) Σ A

 K_i Development type constant for initial time of concentration: Tc=K_i(L³/H)^{0.2}

OVERALL SITE		
Total incoming flow at CB #1	31.18 cfs	10.50 acres
A+D+E+F+G+H+I+S		
Total incoming flow at CB #2	8.71 cfs	2.74 acres
P+Q+R		
Total incoming flow at Area #1	39.28 cfs	11.93 acres
B+C+J+K+L		
Total incoming flow at Catch Basin #3	8.45 cfs	2.68 acres
M+N+O		
Total Flow	87.62 cfs	

Q100 Rational Method Hydrology Calculations for Existing Improvements Project: Creekside, San Juan Capistrano

Area	Α	Α	ΣΑ	Soil	Dev	Ki	T _c	125	Fm	Fp	F _m	ai	\mathbf{a}_{p}	Q25	S ₀	L	н	n	\mathbf{K}_{pipe}	D/d	D	v		Description
No.	(sqft)	(ac)	(ac)	type					(in/hr)					(cfs)		(ft)	(ft)				(ft)	(fps) (min	
EX-A	145615	3.34	3.34	D	Poor Grass	0.697	11.70	3.8	0.18	0.20	0.18	0.10	0.90	10.90	16.32%	864.00	141.00							Initial Subarea - Surface Flow CB #1 (Flow 1 of 8)
EX-B	91744	2.11	2.11	D	Poor Grass	0.697	10.20	4.1	0.02	0.20	0.02	0.91	0.09	7.76	20.00%	650.00	139.00	 						Initial Subarea - Surface Flow
																								Drainage Ditch
ХC	26005	0.60	0.60		Poor Grass	0.607		30	0.02	0.20	0.02	0.01	0.00	2.06	10.00%	479.00	06.00	 					11.40	Area #1 (Flow 1 of 5) Surface Flow
	20005	0.00	0.00	U	FUUI GIASS	0.097		5.0	0.02	0.20	0.02	0.91	0.09	2.00	19.00 %	470.00	90.00						11.40	36" City Storm Drain
		2.70					21.66							9.82				 			_			Area #1 (Flow 2 of 5)
X-D	46214	1.06	1.06	D	Poor Grass	0.697	8.0	4.7	0.02	0.20	0.02	0.91	0.09	4.50	19.31%	352.00	68.00							Initial Subarea - Surface F
																								CB #1 (Flow 2 of 8)
X-E	12804	0.29	0.29	D	Poor Grass	0.697		4.8						1.27	17.51%	177.00	31.00	 					7.83	Surface Flow
		1.35					15.8							5.762										(D+E)
V F	23652	0.54	0.54		Commercial	0.209		3.6	0.02	0.20	0.02	0.01	0.00	1 74	0 10%	398	0.50	 					13.0 ⁻	CB #1 (Flow 3 of 8) Surface Flow
=л-г	23032	1.90	0.54	U	Commercial	0.290	28.8	3.0	0.02	0.20	0.02	0.91	0.09	7.50	0.10%	390	0.50						13.0	(E+F)
																		 						CB #1 (Flow 4 of 8)
EX-G	29195	0.67	0.67	D	Commercial	0.298		5.1						3.06	2.69%	446	12.00						7.05	
		2.57					35.9							10.56										Existing Inlet #1 (F+G) CB #1 (Flow 5 of 8)
X-H	10973		0.25	D	Commercial	0.298		5.6	0.02	0.20	0.02	0.91	0.09		4.89%	327	16.00	 			-			Initial Subarea - Surface F
																								CB #1 (Flow 6 of 8)
EX-I	34976	0.80	0.80	D	Commercial	0.298		5.1						3.71	2.00%	367	7.00	 					6.92	
		4.05					40.0							4.07										(G+H)
EX.I	223152	1.05 5.12	5 12		Commercial	0 298	<u>12.9</u>	47	0.02	0.20	0.02	0.91	0.09	4.97	4 00%	714	29.00	 			-			CB #1 (Flow 7 of 8) Initial Subarea - Surface Fl
_// 0	220102	0.12	0.12	2	Commercial	0.200	0.0		0.02	0.20	0.02	0.01	0.00	2	1.0070		20.00							Area #1 (Flow 3 of 5)
		5.12					8.0							21.71				 						
EX-K	26759	0.61	0.61	D	Commercial	0.298	5.0	6.2	0.02	0.20	0.02	0.91	0.09	3.41	12.14%	280.00	34.00							Initial Subarea - Surface Fl Area #1 (Flow 4 of 5)
		0.61					5.0							3.41										
EX-L	151872	3.49	3.49	D	Commercial	0.298	7.5	4.9	0.02	0.20	0.02	0.91	0.09	15.33	5.18%	598.00	31.00						6.95	Initial Subarea - Surface Fl
		3.49					7.5							15.33										Area #1 (Flow 5 of 5)
X-M	60216		1.38		Poor Grass	0.697		4.3	0.02	0.20	0.02	0.91	0.09		15.24%	505	77.00	 						Initial Subarea - Surface Fl
																		 						Area #2 (Flow 1 of 3)
EX-N	26949		0.62	D	Poor Grass	0.697									11.68%	308	36.00	 					10.60	Surface Flow
Y-0	29467	2.00	0.68		Commercial	0 208	20.0						-	7.58 3.22	4.25%	470	20.00	 					6.57	Area #2 (Flow 2 of 3) Surface Flow
	23407	2.68	0.00	U	Commercial	0.230	26.6							10.80	4.2370	470	20.00						0.57	Area #2 (Flow 3 of 3)
EX-P	21943	0.50	0.50	D	Poor Grass	0.697		5.3						2.38	14.81%	108	16.00	 					6.64	
TX O	39650		0.01			0.007	6.6							0.05	47.070/		00.00	 					8.09	CB #2 (Flow 1 out of 3)
=X-Q	39650	0.91	0.91	D	Poor Grass	0.697	14.7	4.7						3.85	17.27%	191	33.00						8.09	Surface Flow CB #2 (Flow 2 out of 3)
EX-R	57671	1.32	1.32	D	Commercial	0.298		4.1						4.90	1.82%	714	13.00	 			-			Initial Subarea - Surface F
		2.74					24.0							44.42										CB #2 (Flow 3 out of 3)
X-S	153982	2.74 3.53		D	Commercial	0.298	24.9 9.5	4.3	0.02	0.20	0.02	0.91	0.09	11.13 13.57	3.00%	929	26.00							Initial Subarea - Surface F
-																								CB #1 (Flow 8 of 8)

Q100 Rational Method Hydrology Calculations for Existing Improvements Project: Creekside, San Juan Capistrano

Legen	<u>d:</u>	OVERALL SITE		
Α	Area of subarea (acres)	Total incoming flow at CB #1	39.99 cfs	10.50 acres
ΣΑ	Total area (acres)	A+D+E+F+G+H+I+S		
ai	Fractional portion of impervious area	Total incoming flow at CB #2	11.13 cfs	2.74 acres
a _p	Fractional portion of pervious area	P+Q+R		
Fp	Infiltration rate (in inches per hour)	Total incoming flow at Area #1	50.27 cfs	11.93 acres
Fm	Rate of runoff (in inches per hour) = $a_p F_p$	B+C+J+K+L		
Length	n Flowpath length (feet)	Total incoming flow at Catch Basin #3	10.80 cfs	2.68 acres
Ave S	Average slope of subarea (ft/ft)	M+N+O		
Tc	Time of concentration (minutes; 5 minute minimum)	Total Flow	112.19 cfs	
Tt	Travel time (minutes) between points of concentration			
1	Rainfall intensity (in/hr) in non-mountainous areas for 100-yr frequency, I_t = 11.995 $t^{0.566}$	ON-SITE		
Q ₁₀₀	Peak discharge (cfs) = $0.9(I-F_m)\Sigma A$	Total incoming flow at Discharge Point #1	52.09 cfs	12.14 acres

 \mathbf{K}_{i} Development type constant for initial time of concentration: Tc=K_i(L³/H)^{0.2}

Appendix 4 Hydrology Calculations for Proposed Conditions-25 & 100 Year Storm

Q 25 Rational Method Hydrology Calculations for Proposed Development Project: Creekside, San Juan Capistrano

Area	Α	Α	ΣΑ	Soil	Dev	K	Tc	I ₂₅	F _m	Fp	F _m	ai	a _p	Q25	S ₀	L	н		n K _{pipe}	D/d	D			Description
No.	(sqft)	(ac)	(ac)	type	type		(min)	(in/hr)	(in/hr)	avg	avg			(cfs)		(ft)	(ft)	(in)			(ft)	(fps)	(min)	
Α	145405.0	3.338	3.34	D	Poor Grass	0.697	11.7	3.0	0.18	0.20	0.18	0.10	0.90	8.42	16.31%	864	141							Initial Subarea - Surface Flow CB #1 (Flow 1 of 5)
в	69573.0	1.597	1.60	D	Poor Grass	0.697	10.5	3.2	0.18	0.20	0.18	0.10	0.90	4.30	15.08%	696	105							Surface Flow CB #1 (Flow 2 of 5)
- <u>c</u>	17577.0	0.404	0.40	D	Poor Grass	0.697	8.5	3.6	0.18	0.20	0.18	0.10	0.90	1.23	18.13%	375	68							Surface Flow CB #1 (Flow 3 of 5)
D	44077.0	1.012	1.01	D	Asphalt Concrete	0.298	8.1	3.7	0.00	0.20	0.00	1.00	0.00	3.34	3.91%	766	30							Initial Subarea - Surface Flow Area (Flow 1 of 14)
Ē	40120.0	0.921	0.92	D	Apartments	0.325	7.3	3.9	0.02	0.20	0.02	0.90	0.10	3.21	1.63%	307	5							Surface Flow Area 1 (Flow 2 of 14)
F	31252.0	0.717	0.72	D	Poor Grass	0.697	7.0	4.0	0.18	0.20	0.18	0.10	0.90	2.46	25.94%	316	82							Surface Flow CB #3 (Flow 1 of 3)
G	39078.0	0.897	0.90		Apartments	0.325	7.2	3.9	0.02	0.20	0.02	0.92	0.08	3.17	1.69%	296	5							Surface Flow Modular Wetlands
н	38179.0	0.876	0.88	D	Poor Grass	0.697	7.2	3.9	0.18	0.20	0.18	0.10	0.90	2.95	18.72%	299	56							Area 1 (Flow 3 of 14) Initial Subarea - Surface Flow CB #3 (Flow 2 of 3)
	46189.0	1.060	1.06	D	Apartments	0.325	6.9	4.0	0.02	0.20	0.02	0.90	0.10	3.81	1.78%	281	5							Surface Flow Modular Wetlands
- <u>1</u>	68310.0	1.568	1.57	D	Single Family	0.391	11.1	3.1	0.02	0.20	0.02	0.90	0.10	4.31	2.20%	726	16							Area 1 (Flow 4 of 14) Initial Subarea - Surface Flow Modular Wetlands
-к	45741.0	1.050	1.05	- <u>-</u>	Single Family	0.391	6.4	4.2	0.02	0.20	0.02	0.90	0.10	3.95	3.90%	256	10							Area 1 (Flow 5 of 14) Surface Flow Modular Wetlands
	53432.0	1.227	1.23	D	Single Family	0.391	7.4	3.9	0.02	0.20	0.02	0.90	0.10	4.24	3.97%	352	14							Area 1 (Flow 6 of 14) Surface Flow Modular Wetlands
<u>м</u> .	43135.0	0.990	0.99		Single Family	0.391	8.5	3.6	0.02	0.20	0.02	0.90	0.10	3.17	2.93%	410	12							Area 1 (Flow 7 of 14) Surface Flow Modular Wetlands
- <u>-</u>	75395.0	1.731	1.73	D	Single Family	0.391	8.1	3.7	0.02	0.20	0.02	0.90	0.10	5.69	3.18%	377	12							Area 1 (Flow 8 of 14) Surface Flow Modular Wetlands
0	8654.0	0.199	0.20	D	Single Family	0.391	5.4	4.6	0.09	0.20	0.09	0.54	0.46	0.81	4.54%	154	7							Area 1 (Flow 9 of 14) Surface Flow Modular Wetlands
- <u>P</u> -	20003.0	0.459	0.46		Single Family	0.391	6.9	4.0	0.04	0.20	0.04	0.81	0.19	1.65	2.65%	226	6							Area 1 (Flow 10 of 14) Surface Flow Modular Wetlands
<u> </u>	38162.0	0.876	0.88	- <u>-</u>	Single Family	0.391	10.2	3.2	0.02	0.20	0.02	0.90	0.10	2.52	2.82%	283	11							Area 1 (Flow 11 of 14) Initial Subarea - Surface Flow Area 1 (Flow 12 of 14)
Q-1	60080.0	1.379	1.38	- <u>-</u>	Single Family	0.391	10.2	3.2	0.02	0.20	0.02	0.90	0.10	3.97	2.82%	425	11							Initial Subarea - Surface Flow
R	37943.0	0.871	0.87		Single Family	0.391	6.4	4.2	0.02	0.20	0.02	0.90	0.10	3.26	4.92%	244	12							Area 1 (Flow 12 of 14) Surface Flow
- <u>s</u> -	21012.0	0.482	0.48		Single Family	0.391	5.3	4.7	0.02	0.20	0.02	0.90	0.10	2.01	5.98%	167	10							Area 1 (Flow 13 of 14) Surface Flow
- <u>ד</u> -	153834.0	3.532	3.53	- <u>-</u>	Commercial	0.298	9.5	3.4	0.02	0.20	0.02	0.90	0.10	10.60	3.28%	760	25							Area 1 (Flow 14 of 14) Initial Subarea - Surface Flow
- <u>u</u>	47660.0	1.094	1.09		Asphalt Concrete	0.298	8.7	3.5	0.04	0.20	0.04	0.81	0.19	3.43	0.69%	432	3							CB #1 (Flow 4 of 5) Initial Subarea - Surface Flow
- <u>v</u>	73723.0	1.692	1.69		Asphalt Concrete	0.298	8.3	3.6	0.04	0.20	0.04	0.80	0.20	5.45	2.51%	676	17							CB #1 (Flow 5 of 5) Initial Subarea - Surface Flow
- <u>w</u>	5682.0	0.130	0.13	- <u>-</u>	Asphalt Concrete	0.298	5.0	4.8	0.00	0.20	0.00	1.00	0.00	0.57	10.09%	317	32							CB #2 (Flow 1 of 1) Initial Subarea - Surface Flow
																								CB #3 (Flow 3 of 3)

Q 25 Rational Method Hydrology Calculations for Proposed Development Project: Creekside, San Juan Capistrano

gend:		OVERALL SITE		
Α ΣΑ	Area of subarea (acres) Total area (acres)	Total incoming flow at CB #1 (Off-site) A+B+C+T+U	27.98 cfs	9.96 acres
a _i a _p	Fractional portion of impervious area Fractional portion of pervious area	Total incoming flow at CB #2 V	5.45 cfs	1.69 acres
F _p F _m	Infiltration rate (in inches per hour) = $a_p F_p$	Total incoming flow at CB #3 F+H+W	5.98 cfs	1.72 acres
ength Ave S	Flowpath length (feet) Average slope of subarea (ft/ft)	Incoming flow at Area 1 D+E+G+I+J+K+L+M+N+O+P+Q+Q1+R+S	49.09 cfs	13.34 acres
T _c T _t	Time of concentration (minutes; 5 minute minimum) Travel time (minutes) between points of concentration	Total	88.50 cfs	26.72 acres
I.	Rainfall intensity (in/hr) in non-mountainous areas for 100-yr frequency, $I_t = 11.995 t^{-0.566}$	ON-SITE		
Q25	Peak discharge (cfs) = $0.9(I-F_m)\Sigma A$	Total incoming flow at Dicharge Point #1	45.12 cfs	13.34 acres
Ki	Development type constant for initial time of concentration: Tc=K (L ³ /H) ^{0.2}			•

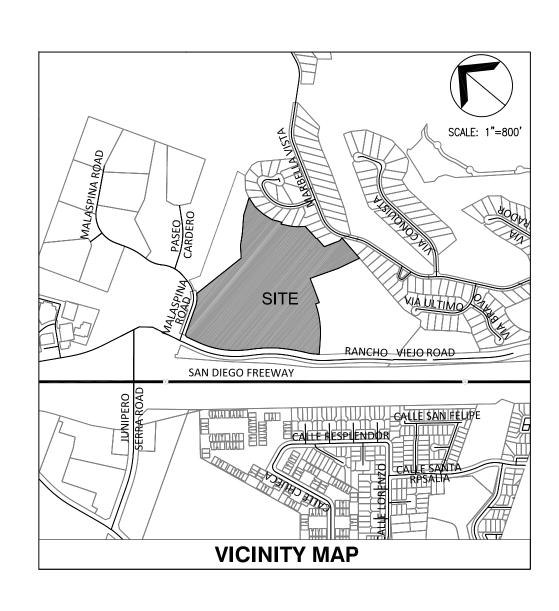
Q 100 Rational Method Hydrology Calculations for Proposed Development Project: Creekside, San Juan Capistrano

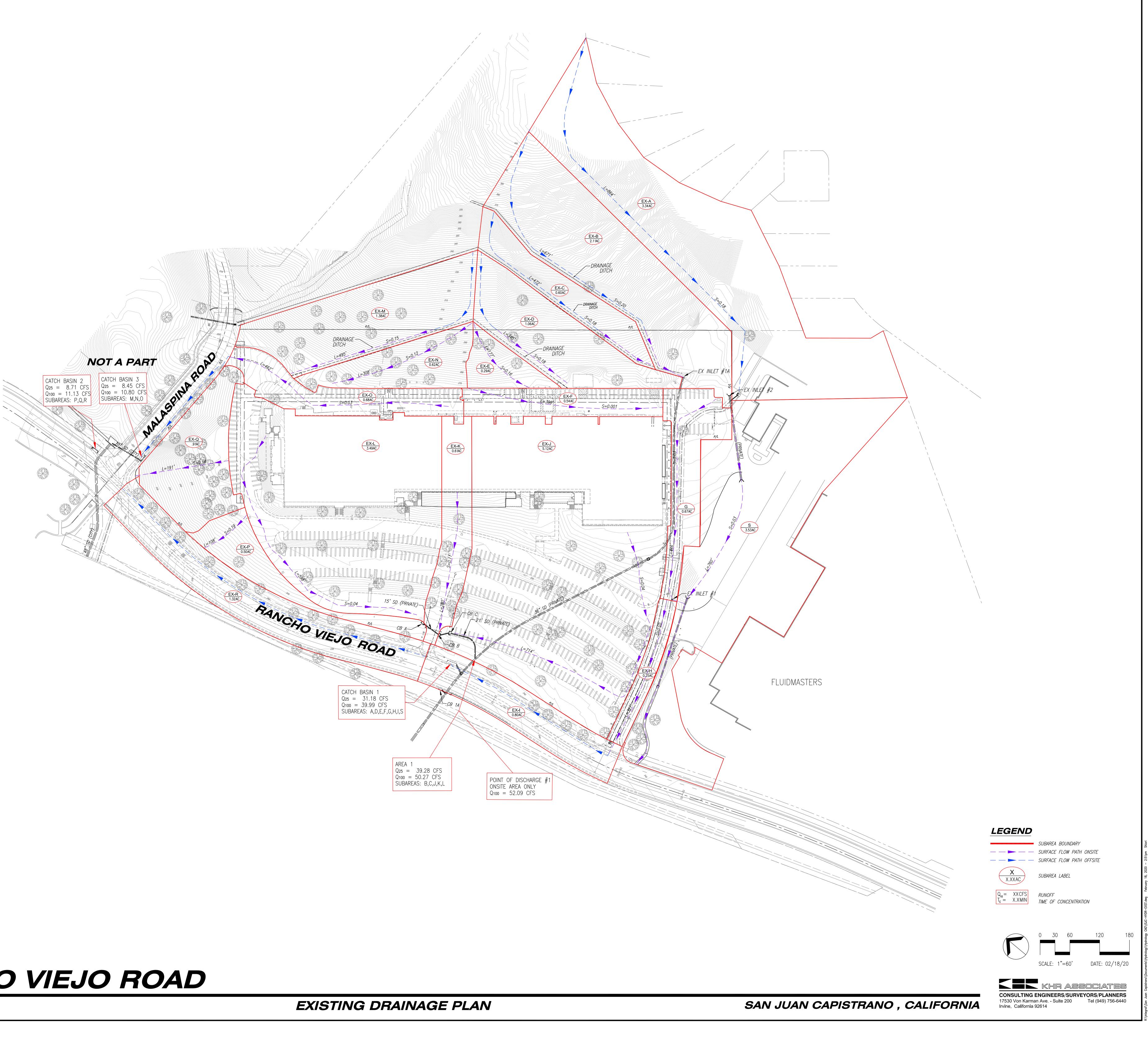
Area No.	A (sqft)	A (ac)	ΣΑ (ac)	Soil type	Dev type	K	T _c (min)	I ₂₅ (in/hr)	F _m (in/hr)	F _p avg	F _m avg	a _i	a _p	Q25 (cfs)	S ₀	L (ft)	H (ft)	du (in)	n K _{pipe}	D/d		V (fps)		Description
		. /	. ,				. ,	. ,						. ,		. /	. ,	(,			(11)	(195)	()	
A	145405.0	3.338	3.34	D	Poor Grass	0.697	11.7	3.8	0.18	0.20	0.18	0.10	0.90	10.88	16.31%	864	141							Initial Subarea - Surface Flow CB #1 (Flow 1 of 5)
в	69573.0	1.597	1.60	D	Poor Grass	0.697	10.5	4.0	0.18	0.20	0.18	0.10	0.90	5.56	15.08%	696	105							Surface Flow CB #1 (Flow 2 of 5)
c	17577.0	0.404	0.40	D	Poor Grass	0.697	8.5	4.6	0.18	0.20	0.18	0.10	0.90	1.59	18.13%	375	68							Surface Flow CB #1 (Flow 3 of 5)
- <u>-</u>	44077.0	1.012	1.01		Asphalt Concrete	0.298	8.1	4.7	0.00	0.20	0.00	1.00	0.00	4.27	3.91%	766	30							Initial Subarea - Surface Flow Area (Flow 1 of 14)
Ē	40120.0	0.921	0.92	D	Apartments	0.325	7.3	5.0	0.02	0.20	0.02	0.90	0.10	4.11	1.63%	307	5							Surface Flow Area 1 (Flow 2 of 14)
F	31252.0	0.717	0.72	D	Poor Grass	0.697	7.0	5.1	0.18	0.20	0.18	0.10	0.90	3.18	25.94%	316	82							Surface Flow CB #3 (Flow 1 of 3)
G	39078.0	0.897	0.90	- <u>-</u>	Apartments	0.325	7.2	5.0	0.02	0.20	0.02	0.92	0.08	4.05	1.69%	296	5							Surface Flow
-н-	38179.0	0.876	0.88	D	Poor Grass	0.697	7.2	5.0	0.18	0.20	0.18	0.10	0.90	3.82	18.72%	299	56							Modular Wetlands Area 1 (Flow 3 of 14) Initial Subarea - Surface Flow
	46189.0	1.060	1.06	D	Apartments	0.325	6.9	5.1	0.02	0.20	0.02	0.90	0.10	4.87	1.78%	281	5							CB #3 (Flow 2 of 3) Surface Flow
<u>-</u>	68310.0	1.568	1.57		Single Family	0.391	11.1	3.9	0.02	0.20	0.02	0.90	0.10	5.50	2.20%	726	16							Modular Wetlands Area 1 (Flow 4 of 14) Initial Subarea - Surface Flow
- <u>-</u>	45741.0	1.050	1.05	- <u>-</u>		0.391			0.02	0.20	0.02	0.90	0.10	5.06	3.90%	256	10							Modular Wetlands Area 1 (Flow 5 of 14) Surface Flow
	53432.0	1.227	1.23			0.391				0.20		0.90	0.10	5.43	3.97%	352	- 14							Modular Wetlands Area 1 (Flow 6 of 14) Surface Flow
														0.10			14							Modular Wetlands Area 1 (Flow 7 of 14)
M	43135.0	0.990	0.99	D	Single Family	0.391	8.5	4.6	0.02	0.20		0.90	0.10	4.05	2.93%	410	12							Surface Flow Modular Wetlands Area 1 (Flow 8 of 14)
N	75395.0	1.731	1.73	D	Single Family	0.391	8.1	4.7	0.02	0.20	0.02	0.90	0.10	7.28	3.18%	377	12							Surface Flow Modular Wetlands Area 1 (Flow 9 of 14)
0	8654.0	0.199	0.20	D	Single Family	0.391	5.4	5.9	0.09	0.20	0.09	0.54	0.46	1.04	4.54%	154	7							Surface Flow Modular Wetlands Area 1 (Flow 10 of 14)
Р	20003.0	0.459	0.46	D	Single Family	0.391	6.9	5.1	0.04	0.20	0.04	0.81	0.19	2.11	2.65%	226	6							Surface Flow Modular Wetlands
Q	38162.0	0.876	0.88	D	Single Family	0.391	10.2	4.1	0.02	0.20	0.02	0.90	0.10	3.23	2.82%	283	11							Area 1 (Flow 11 of 14) Initial Subarea - Surface Flow Area 1 (Flow 12 of 14)
Q-1	60080.0	1.379	1.38	D	Single Family	0.391	10.2	4.1	0.02	0.20	0.02	0.90	0.10	5.08	2.82%	425	11							Initial Subarea - Surface Flow Area 1 (Flow 12 of 14)
R	37943.0	0.871	0.87	D	Single Family	0.391	6.4	5.4	0.02	0.20	0.02	0.90	0.10	4.18	4.92%	244	12							Surface Flow Area 1 (Flow 13 of 14)
s	21012.0	0.482	0.48	D	Single Family	0.391	5.3	6.0	0.02	0.20	0.02	0.90	0.10	2.58	5.98%	167	10							Surface Flow Area 1 (Flow 14 of 14)
- T -	153834.0	3.532	3.53		Commercial	0.298	9.5	4.3	0.02	0.20	0.02	0.90	0.10	13.55	3.28%	760	25							Initial Subarea - Surface Flow CB #1 (Flow 4 of 5)
- 0	47660.0	1.094	1.09	D	Asphalt Concrete	0.298	8.7	4.5	0.04	0.20	0.04	0.81	0.19	4.40	0.69%	432	3							Initial Subarea - Surface Flow CB #1 (Flow 5 of 5)
- <u>v</u>	73723.0	1.692	1.69	<u> </u>	Asphalt Concrete	0.298	8.3	4.6	0.04	0.20	0.04	0.80	0.20	6.99	2.51%	676	17							Initial Subarea - Surface Flow CB #2 (Flow 1 of 1)
w	5682.0	0.130	0.13	D	Asphalt Concrete	0.298	5.0	6.2	0.00	0.20	0.00	1.00	0.00	0.73	10.09%	317	32							Initial Subarea - Surface Flow CB #3 (Flow 3 of 3)

Q 100 Rational Method Hydrology Calculations for Proposed Development Project: Creekside, San Juan Capistrano

egend:		OVERALL SITE		
Α ΣΑ	Area of subarea (acres) Total area (acres)	Total incoming flow at CB #1 (Off-site) A+B+C+T+U	35.98 cfs	9.96 acres
a _i a _p	Fractional portion of impervious area Fractional portion of pervious area	Total incoming flow at CB #2 V	6.99 cfs	1.69 acres
F _p Fm	Infiltration rate (in inches per hour) Rate of runoff (in inches per hour) = $a_p F_p$	Total incoming flow at CB #3 F+H+W	7.72 cfs	1.72 acres
Length Ave S	Flowpath length (feet) Average slope of subarea (ft/ft)	Incoming flow at Area 1 D+E+G+I+J+K+L+M+N+O+P+Q+Q1+R+S	62.85 cfs	13.34 acres
Г _с	Time of concentration (minutes; 5 minute minimum)	Total	113.53 cfs	26.72 acres
Tt	Travel time (minutes) between points of concentration			
1	Rainfall intensity (in/hr) in non-mountainous areas for 100-yr frequency, I_t = 11.995 $t^{-0.566}$	ON-SITE		
100	Peak discharge (cfs) = $0.9(I-F_m)\Sigma A$	Total incoming flow at Dicharge Point #1	62.85 cfs	13.34 acres
Ki	Development type constant for initial time of concentration: Tc=K _i (L ³ /H) ^{0.2}			

Appendix 5 Existing Conditions Hydrology Map

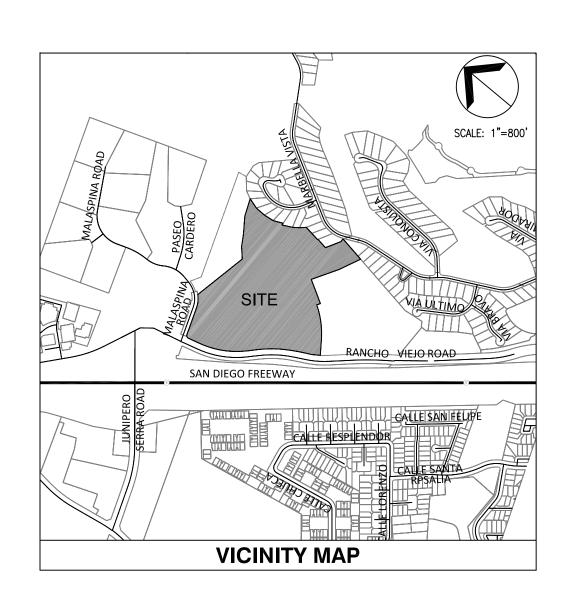


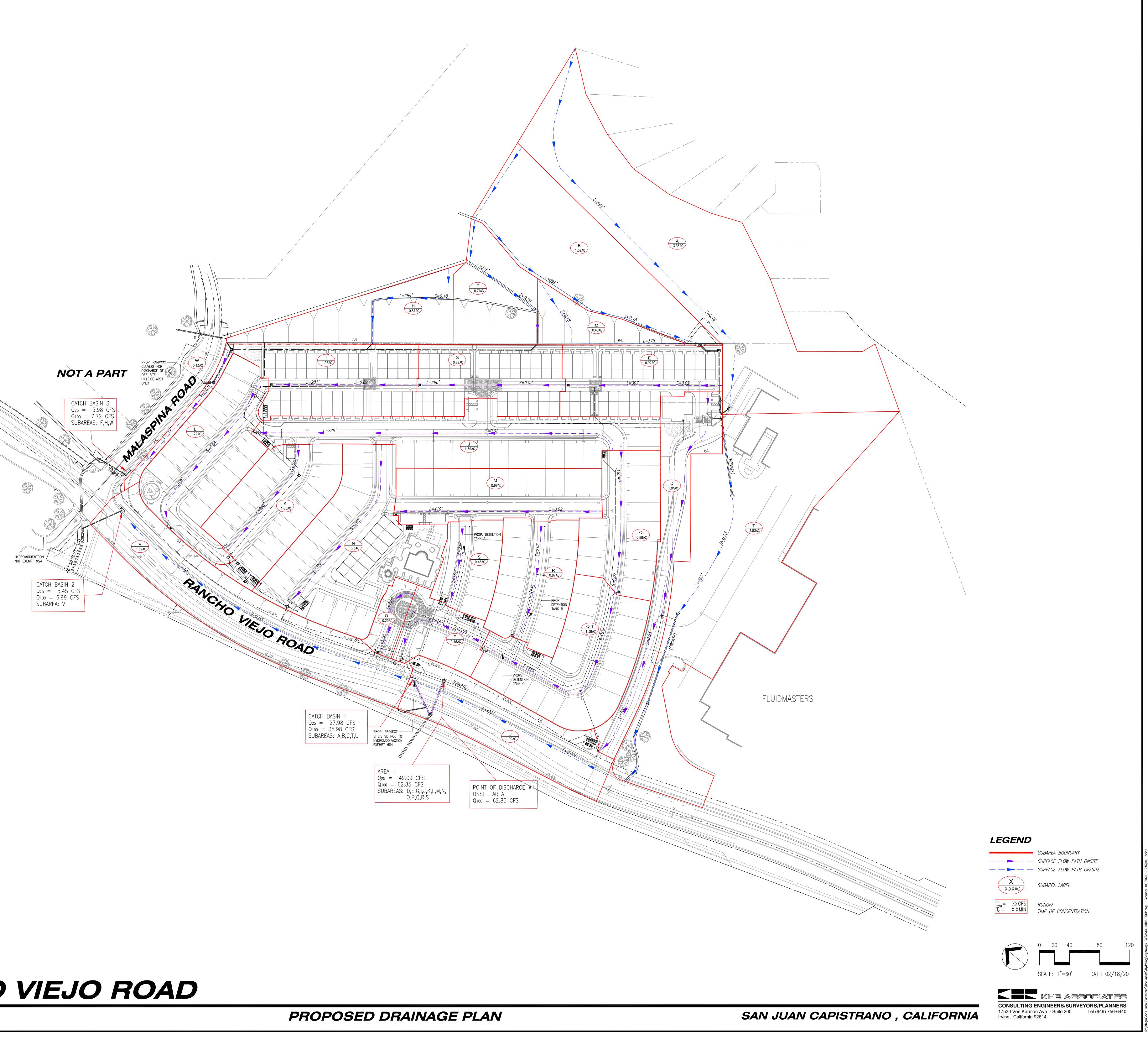




INTEGRAL COMMUNITIES

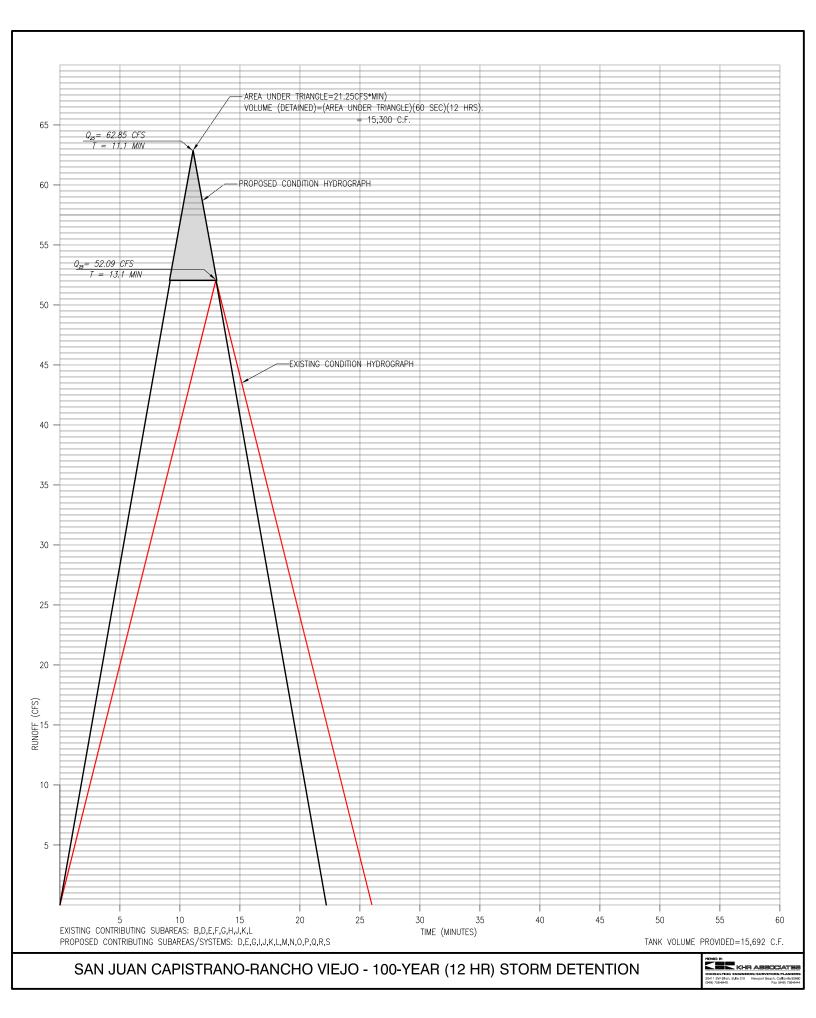
Appendix 6 Proposed Conditions Hydrology Map







Appendix 7 Hydrograph



Appendix 8 South Orange County Hydrology Model Calculations



General Model Information

Project Name:	Malaspina Road
Site Name:	
Site Address:	
City:	SAN JUAN CAPISTRANO
Report Date:	1/29/2020
Gage:	Laguna Beach
Data Start:	10/01/1949
Data End:	09/30/2006
Timestep:	15 Minute
Precip Scale:	1.000
Version Date:	2018/07/12

POC Thresholds

Low Flow Threshold for POC1:	10 Percent of the 2 Year
High Flow Threshold for POC1:	10 Year

Landuse Basin Data Predeveloped Land Use

M,N,O,P,Q,R,S Bypass:	No
GroundWater:	No
Pervious Land Use	acre
Pervious Total	0
Impervious Land Use Impervious,Mod(5-10)	acre 5.34
Impervious Total	5.34
Basin Total	5.34
Element Flows To: Surface	Interflow

Groundwater

Mitigated Land Use

H,F,V,W

Bypass:	No
GroundWater:	No
Pervious Land Use A,Scrub,Steep(10-15)	acre 1.59
Pervious Total	1.59
Impervious Land Use Impervious,Mod(5-10)	acre 1.84
Impervious Total	1.84
Basin Total	3.43

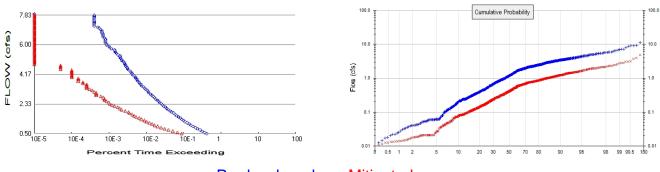
Element Flows To: Surface Inte

Interflow

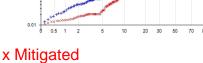
Groundwater

Routing Elements Predeveloped Routing Mitigated Routing

Analysis Results POC 1



+ Predeveloped



Predeveloped Landuse	Totals for POC #1
Total Pervious Area:	0
Total Impervious Area:	5.34

Mitigated Landuse Totals for POC #1 Total Pervious Area: 1.59 **Total Impervious Area:** 1.84

Flow Frequency Method: Cunnane

Flow Frequency Return Periods for Predeveloped. POC #1 **Return Period** Flow(cfs) 5.014565 2 year 6.377922 5 year 10 year 7.833882 25 year 9.08618

Flow Frequency Return Periods for Mitigated. POC #1 Flow(cfs) **Return Period** 2 year 1.937365 2.430261 5 year 10 year 3.041172 25 year 3.751238

Duration Flows

The Facility PASSED

Flow(cfs) 0.5015 0.5755 0.6496 0.7237 0.7977 0.8718 0.9458 1.0199 1.0940 1.1680 1.2421 1.3162 1.3902 1.4643 1.5384 1.6124 1.6865 1.7606 1.8346 1.9087 1.9828 2.0568 2.1309 2.2049 2.2790 2.3531 2.4271 2.5753 2.6493 2.7234 2.7975 2.8715 2.9456 3.0197 3.0937 3.1678 3.2419 3.3900 3.4641 3.5381 3.6122 3.6862 3.7603 3.8344 3.9084 3.9825	Predev 8250 7201 6278 5462 4703 4113 3560 3150 2776 2460 2177 1976 1785 1605 1455 1301 1190 1075 955 859 770 700 652 585 536 494 456 422 389 358 331 301 280 257 238 224 213 194 179 169 152 143 132 126 118 113 106 101	$\begin{array}{c} \text{Mit} \\ 1766 \\ 1357 \\ 1024 \\ 782 \\ 617 \\ 497 \\ 403 \\ 333 \\ 281 \\ 239 \\ 202 \\ 178 \\ 148 \\ 106 \\ 94 \\ 83 \\ 70 \\ 66 \\ 54 \\ 43 \\ 39 \\ 34 \\ 28 \\ 24 \\ 21 \\ 20 \\ 17 \\ 15 \\ 14 \\ 12 \\ 9 \\ 9 \\ 9 \\ 8 \\ 7 \\ 6 \\ 5 \\ 5 \\ 5 \\ 5 \\ 5 \\ 4 \\ 4 \\ 3 \\ 3 \\ 2 \\ 2 \\ 2 \\ 2 \\ 2 \\ 2 \\ 2 \\ 2$	Percentage 21 18 16 14 13 12 11 10 10 9 9 9 9 8 7 7 7 6 6 6 6 6 6 5 5 5 4 4 4 4 3 3 3 3 3 3 3 3 3 3 3 3 3	Pass/Fail Pass Pass Pass Pass Pass Pass Pass Pas
3.6862 3.7603 3.8344 3.9084	126 118 113	4 3 3 2 2 2 2 2 2 2 2 2	3 2 2 2 1 2 2 2 2 2 2 2 2	Pass Pass Pass

Water Quality

Model Default Modifications

Total of 0 changes have been made.

PERLND Changes

No PERLND changes have been made.

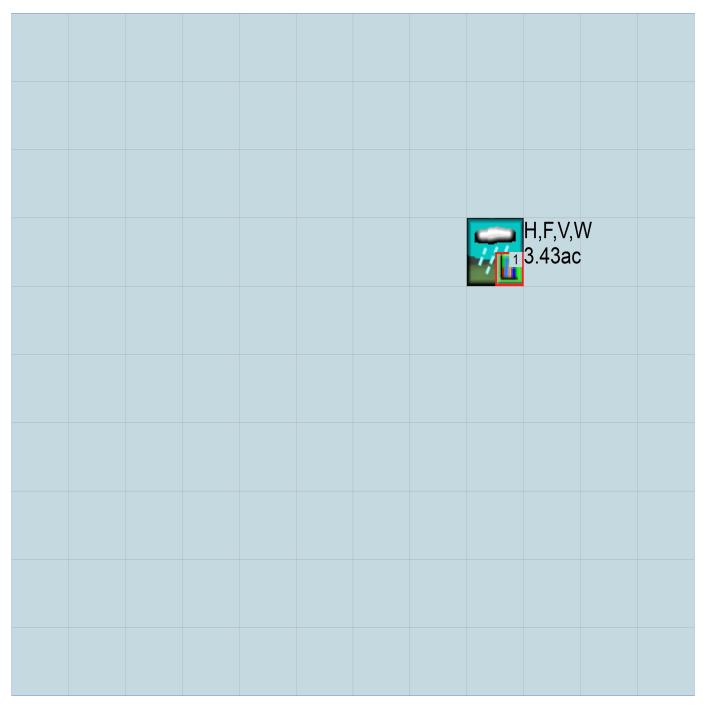
IMPLND Changes

No IMPLND changes have been made.

Appendix Predeveloped Schematic

					M,N,O,	P,Q,R,	

Mitigated Schematic



Predeveloped UCI File

RUN

GLOBAL WWHM4 model simulation START1949 10 01END2006 09 30RUN INTERP OUTPUT LEVEL30 RESUME 0 RUN 1 UNIT SYSTEM 1 END GLOBAL FILES <File> <Un#> <-----File Name----->*** * * * <-ID-> WDM 26 Malaspina Road.wdm MESSU 25 PreMalaspina Road.MES 27 PreMalaspina Road.L61 28 PreMalaspina Road.L62 30 POCMalaspina Road1.dat END FILES OPN SEOUENCE 2 INGRP INDELT 00:15 IMPLND 501 COPY DISPLY 1 END INGRP END OPN SEQUENCE DISPLY DISPLY-INF01 # - #<-----Title---->***TRAN PIVL DIG1 FIL1 PYR DIG2 FIL2 YRND 1 M,N,O,P,Q,R,S 1 2 30 MAX 9 END DISPLY-INF01 END DISPLY COPY TIMESERIES # - # NPT NMN *** 1 1)1 1 1 501 1 END TIMESERIES END COPY GENER OPCODE # # OPCD *** END OPCODE PARM K *** # # END PARM END GENER PERLND GEN-INFO <PLS ><-----Name---->NBLKS Unit-systems Printer *** User t-series Engl Metr *** # - # in out * * * END GEN-INFO *** Section PWATER*** ACTIVITY # - # ATMP SNOW PWAT SED PST PWG POAL MSTL PEST NITR PHOS TRAC *** END ACTIVITY PRINT-INFO # - # ATMP SNOW PWAT SED PST PWG PQAL MSTL PEST NITR PHOS TRAC ******** END PRINT-INFO PWAT-PARM1 <PLS > PWATER variable monthly parameter value flags *** # - # CSNO RTOP UZFG VCS VUZ VNN VIFW VIRC VLE INFC HWT ***

PWAT-PARM2 <PLS > PWATER input info: Part 2 *** # - # ***FOREST LZSN INFILT LSUR SLSUR KVARY AGWRC END PWAT-PARM2 PWAT-PARM3 <PLS > PWATER input info: Part 3 ***
- # ***PETMAX PETMIN INFEXP INFILD DEEPFR BASETP <PLS > AGWETP END PWAT-PARM3 PWAT-PARM4 <PLS > PWATER input info: Part 4
- # CEPSC UZSN NSUR * * * INTFW IRC LZETP *** END PWAT-PARM4 MON-LZETPARM <PLS > PWATER input info: Part 3 *** # - # JAN FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC *** END MON-LZETPARM MON-INTERCEP PWATER input info: Part 3 * * * <PLS > # - # JAN FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC *** END MON-INTERCEP PWAT-STATE1 <PLS > *** Initial conditions at start of simulation ran from 1990 to end of 1992 (pat 1-11-95) RUN 21 *** # - # *** CEPS SURS UZS IFWS LZS AGWS GWVS END PWAT-STATE1 END PERLND IMPLND GEN-INFO <PLS ><-----Name----> Unit-systems Printer *** # - # User t-series Engl Metr *** in out *** 1 1 1 27 0 2 Impervious,Mod(5-10) END GEN-INFO *** Section IWATER*** ACTIVITY # - # ATMP SNOW IWAT SLD IWG IQAL *** 2 0 0 1 0 0 0 END ACTIVITY PRINT-INFO <ILS > ******* Print-flags ******* PIVL PYR # - # ATMP SNOW IWAT SLD IWG IQAL ********* 2 0 0 4 0 0 1 9 END PRINT-INFO IWAT-PARM1 <PLS > IWATER variable monthly parameter value flags *** # - # CSNO RTOP VRS VNN RTLI *** 2 0 0 0 0 0 0 END IWAT-PARM1 IWAT-PARM2 <PLS > IWATER input info: Part 2 * * *
 # - # ***
 LSUR
 SLSUR
 NSUR
 RETSC

 2
 100
 0.1
 0.1
 0.09
 END IWAT-PARM2 IWAT-PARM3 <PLS > IWATER input info: Part 3 * * * # - # ***PETMAX PETMIN π ---- 0 2 0 END IWAT-PARM3

END PWAT-PARM1

IWAT-STATE1 <PLS > *** Initial conditions at start of simulation # - # *** RETS SURS 2 0 0 END IWAT-STATE1 END IMPLND SCHEMATIC <--Area--> <-Target-> MBLK *** <-factor-> <Name> # Tbl# *** <-Source-> <Name> # <Name> # Tbl# *** M,N,O,P,Q,R,S*** 5.34 COPY 501 15 IMPLND 2 *****Routing***** END SCHEMATIC NETWORK <-Volume-> <-Grp> <-Member-><--Mult-->Tran <-Target vols> <-Grp> <-Member-> *** <Name> # <Name> # #<-factor->strg <Name> # # <Name> # # *** COPY 501 OUTPUT MEAN 1 1 48.4 DISPLY 1 INPUT TIMSER 1 <-Volume-> <-Grp> <-Member-><--Mult-->Tran <-Target vols> <-Grp> <-Member-> *** <Name> # <Name> # #<-factor->strg <Name> # # <Name> # # *** END NETWORK RCHRES GEN-INFO Name Nexits Unit Systems Printer * * * RCHRES # - #<----- User T-series Engl Metr LKFG * * * * * * in out END GEN-INFO *** Section RCHRES*** ACTIVITY # - # HYFG ADFG CNFG HTFG SDFG GQFG OXFG NUFG PKFG PHFG *** END ACTIVITY PRINT-INFO # - # HYDR ADCA CONS HEAT SED GQL OXRX NUTR PLNK PHCB PIVL PYR ******** END PRINT-INFO HYDR-PARM1 RCHRES Flags for each HYDR Section END HYDR-PARM1 HYDR-PARM2 # - # FTABNO LEN DELTH STCOR KS DB50 *** <----><----><----><----> * * * END HYDR-PARM2 HYDR-INIT RCHRES Initial conditions for each HYDR section * * * *** ac-ft <---><---><---> *** <---><---> <----> END HYDR-INIT END RCHRES SPEC-ACTIONS END SPEC-ACTIONS FTABLES END FTABLES

EXT SOURCES <-Volume-> <Member> SsysSgap<--Mult-->Tran <Name> # <Name> # tem strg<-factor->strg VOM 2 PREC ENGL 1 PREC WDM 2 PREC ENGL 1 PREC WDM 1 EVAP ENGL 1 PREC WDM 1 EVAP ENGL 1 PREC WDM 1 EVAP ENGL 1 PREC EXT TARGETS <-Volume-> <-Grp> <-Member-><--Mult-->Tran <Name> # </br>

EXT TARGETS

<-Volume-> <-Grp> <-Member-><--Mult-->Tran <Name> # </br>

<Name> # #
<Name> # #

MSS-LINK

<Volume> <-Grp> <-Member-><--Mult-->

MASS-LINK

<Volume> <-Grp> <-Member-><--Mult-->

Konme> # #
<Name> # #

<Name> # #

<Name> # #

<Name> # #

<Name> # #

<Name> # #

<Name> # #

<Name> # #

<Name> # #

<Name> # #

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<Name> # #

<Name> # #

<Name> # #

<Name> # #

<Name> # #***

<Name> # #****

MASS-LINK
MASS-LINK

IMPLND

IWATER SURO
0.083333

COPY

IMPLND

IWATER SURO
0.083333

COPY

IMPLND

IWATER SURO

0.083333

COPY

INPUT

MASS-LINK

15

END MASS-LINK

END RUN

Mitigated UCI File

RUN

GLOBAL WWHM4 model simulation
 START
 1949 10 01
 END
 2006 09 30

 RUN INTERP OUTPUT LEVEL
 3
 0
 RESUME 0 RUN 1 UNIT SYSTEM 1 END GLOBAL FILES <File> <Un#> <-----File Name---->*** * * * <-ID-> WDM 26 Malaspina Road.wdm MESSU 25 MitMalaspina Road.MES 27 MitMalaspina Road.L61 28 MitMalaspina Road.L62 MitMalaspina Roadl.dat 30 END FILES OPN SEOUENCE INGRP 3 2 INDELT 00:15 PERLND IMPLND COPY 501 1 DISPLY END INGRP END OPN SEQUENCE DISPLY DISPLY-INFO1

 # #<-----Title---->***TRAN PIVL DIG1 FIL1
 PYR DIG2 FIL2 YRND

 1
 H,F,V,W
 MAX
 1
 2
 30
 9

 END DISPLY-INFO1 END DISPLY COPY TIMESERIES # - # NPT NMN *** 1 1 501 1 1 1 END TIMESERIES END COPY GENER OPCODE # # OPCD *** END OPCODE PARM K *** # # END PARM END GENER PERLND GEN-INFO <PLS ><-----Name----->NBLKS Unit-systems Printer *** User t-series Engl Metr *** # - # in out 1 1 1 1 * * * 3 A,Scrub,Steep(10-15) 27 0 END GEN-INFO *** Section PWATER*** ACTIVITY # -# ATMP SNOW PWATSEDPSTPWGPQALMSTLPESTNITRPHOSTRAC***300100000000 END ACTIVITY PRINT-INFO # - # ATMP SNOW PWAT SED PST PWG PQAL MSTL PEST NITR PHOS TRAC ******** 3 0 0 4 0 0 0 0 0 0 0 0 1 9 END PRINT-INFO

PWAT-PARM1 <PLS > PWATER variable monthly parameter value flags ***

 # - # CSNO RTOP UZFG VCS VUZ VNN VIFW VIRC VLE INFC HWT ***

 3
 0
 0
 1
 0
 0
 1
 0

 END PWAT-PARM1 PWAT-PARM2 <PLS > PWATER input info: Part 2 ***
- # ***FOREST LZSN INFILT LSUR SLSUR KVARY AGWRC
3 0 4.5 0.045 300 0.15 0.8 0.955 <PLS > 3 END PWAT-PARM2 PWAT-PARM3 <PLS > PWATER input info: Part 3 ***
 # - # ***PETMAX
 PETMIN
 INFEXP

 3
 40
 35
 2
 INFILD DEEPFR BASETP AGWETP 2 0 0.03 0 2 0 3 END PWAT-PARM3 PWAT-PARM4 <PLS > PWATER input info: Part 4 # - # CEPSC UZSN NSUR INTFW IRC LZETP *** 3 0 0.5 0.3 2.6 0.4 0 MON-LZETPARM * * * <PLS > PWATER input info: Part 3 # - # JAN FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC *** END MON-LZETPARM MON-INTERCEP <PLS > PWATER input info: Part 3 * * * # - # JAN FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC *** END MON-INTERCEP PWAT-STATE1 <PLS > *** Initial conditions at start of simulation ran from 1990 to end of 1992 (pat 1-11-95) RUN 21 *** # *** CEPS SURS UZS IFWS LZS AGWS 0 0 0.05 0 0.9 0.3 GWVS # 0.3 3 0.01 END PWAT-STATE1 END PERLND TMPLND GEN-INFO <PLS ><----Name----> Unit-systems Printer *** User t-series Engl Metr *** # in out *** 2 Impervious,Mod(5-10) 1 1 27 0 END GEN-INFO *** Section IWATER*** ACTIVITY # - # ATMP SNOW IWAT SLD IWG IQAL 2 0 0 1 0 0 0 * * * END ACTIVITY PRINT-INFO <ILS > ******* Print-flags ******* PIVL PYR # - # ATMP SNOW IWAT SLD IWG IQAL ******** 2 0 0 4 0 0 0 1 9 END PRINT-INFO IWAT-PARM1 <PLS > IWATER variable monthly parameter value flags *** # - # CSNO RTOP VRS VNN RTLI *** 2 0 0 0 0 0 0 2 END IWAT-PARM1

IWAT-PARM2
 <PLS >
 IWATER input info: Part 2
 *

 # - # *** LSUR
 SLSUR
 NSUR
 RETSC

 2
 100
 0.1
 0.1
 0.09
 * * * <PLS > END IWAT-PARM2 IWAT-PARM3 <PLS > IWATER input info: Part 3 * * * # - # ***PETMAX PETMIN п 0 2 0 END IWAT-PARM3 IWAT-STATE1 <PLS > *** Initial conditions at start of simulation # - # *** RETS SURS 2 0 0 0 END IWAT-STATE1 END IMPLND SCHEMATIC <--Area--> <-Target-> MBLK *** <-factor-> <Name> # Tbl# *** <-Source-> <Name> # H,F,V,W*** 1.59COPY501121.59COPY501131.84COPY50115 perlnd 3 perlnd 3 IMPLND 2 *****Routing***** END SCHEMATIC NETWORK <-Volume-> <-Grp> <-Member-><--Mult-->Tran <-Target vols> <-Grp> <-Member-> *** <Name> # <Name> # #<-factor->strg <Name> # # <Name> # # *** COPY 501 OUTPUT MEAN 1 1 48.4 DISPLY 1 INPUT TIMSER 1 <-Volume-> <-Grp> <-Member-><--Mult-->Tran <-Target vols> <-Grp> <-Member-> *** <Name> # _____ <Name> # #<-factor->strg <Name> # # _____ <Name> # # *** END NETWORK RCHRES GEN-INFO RCHRES Name Nexits Unit Systems Printer * * * # - #<----> User T-series Engl Metr LKFG * * * * * * in out END GEN-INFO *** Section RCHRES*** ACTIVITY # - # HYFG ADFG CNFG HTFG SDFG GQFG OXFG NUFG PKFG PHFG *** END ACTIVITY PRINT-INFO END PRINT-INFO HYDR-PARM1 RCHRES Flags for each HYDR Section * * * END HYDR-PARM1 HYDR-PARM2 # – # FTABNO LEN KS DB50 * * * DELTH STCOR * * * <----><----><----><---->

END HYDR-PARM2 HYDR-INIT RCHRES Initial conditions for each HYDR section * * * Initial value of OUTDGT <----> <---> <---> *** <---> --><---> <---> END HYDR-INIT END RCHRES SPEC-ACTIONS END SPEC-ACTIONS FTABLES END FTABLES EXT SOURCES <-Volume-> <Member> SsysSgap<--Mult-->Tran <-Target vols> <-Grp> <-Member-> *** <Name> # <Name> # tem strg<-factor->strg <Name> # # <Name> # # *** 2 PRECENGL1PERLND1999EXTNLPREC2 PRECENGL1IMPLND1999EXTNLPREC1 EVAPENGL1PERLND1999EXTNLPETINP1 EVAPENGL1IMPLND1999EXTNLPETINP WDM WDM WDM WDM END EXT SOURCES EXT TARGETS <-Volume-> <-Grp> <-Member-><--Mult-->Tran <-Volume-> <Member> Tsys Tgap Amd *** <Name> # <Name> # #<-factor->strg <Name> # <Name> tem strg strg*** COPY 1 OUTPUT MEAN 1 1 48.4 WDM 701 FLOW ENGL REPL COPY 501 OUTPUT MEAN 1 1 48.4 WDM 801 FLOW ENGL REPL END EXT TARGETS MASS-LINK <Volume> <-Grp> <-Member-><--Mult--> Name>
wame> - Mult-->

 Name> # #<-factor->

 MASS-LINK
 12
 <Target> <-Grp> <-Member->*** <Name> # #*** <Name> <Name> PERLND PWATER SURO 0.083333 COPY INPUT MEAN END MASS-LINK 12 MASS-LINK 13 PERLND PWATER IFWO 0.083333 COPY INPUT MEAN END MASS-LINK 13 MASS-LINK 15 IMPLND IWATER SURO 0.083333 COPY INPUT MEAN END MASS-LINK 15

END MASS-LINK

END RUN

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Appendix 9 San Juan Capistrano Hydromodification Exemption Map

