

APPENDIX J: HYDROLOGY REPORT

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September 2019

PRELIMINARY HYDROLOGY REPORT

For

Tentative Tract No. 82874

City of Covina
County of Los Angeles

Prepared For:

TRUMARKHOMES

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Prepared By:



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WO #: 3593-42X-HydrlygRprt-TT82874

DRAINAGE CONCEPT/HYDROLOGY REPORT

**FOR
VTTM NO. 82874
CITY OF COVINA
COUNTY OF LOS ANGELES**

Prepared Date: 05/01/2020



PREPARED UNDER THE SUPERVISION OF:

A handwritten signature in black ink, appearing to read "Jian Guan".

5/01/2020

Jianhua "Gary" Guan, R.C.E. 64519, Exp. 06/30/21 Date:

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SECTION 1

INTRODUCTION & DISCUSSION

A. INTRODUCTION

The proposed residential development for Covina Bowl – Vesting Tentative Tract Map (VTTM) No. 82874 is located at 1060 West San Bernardino Road, in the City of Covina, County of Los Angeles. The subject site is located on the north side of Badillo Street Drive, south of San Bernardino Road, west of Rimsdale Avenue, and east of existing residential. The general location can be found from the vicinity map attached.

The site presently encompasses commercial/retail buildings with parking lots and a preschool building structure. The overall property is approximately +/-4.50 gross acres and is generally a Trapezoid-shaped parcel. The project site is vacated and not in use. The proposed project would demolish all asphalt and paved areas, buildings, structures and landscaping.

Surrounding land uses include primarily residential and commercial land uses.

The project site is located within Flood Zone "X" per FIRM Map 06037C1700F dated September 26, 2008.

Trumark Homes proposes Vesting Tentative Tract Map No. 82874 for the development of residential lots, parkways, on-street parking, private drives, curb, gutter, sidewalk and storm drain improvements, wet and dry utilities and related infrastructure improvements.

B. DRAINAGE PATTERNS

The overall property is approximately +/-4.55 gross acres in size and the Stormwater and surface water onsite generally flow from northeast to southwest direction. The onsite storm runoffs discharge into Rimsdale Avenue and Badillo Street. Currently, there are catch basins and storm drain systems in the perimeter Streets – one at the northwest intersection of Rimsdale Avenue and Badillo Street and one at the southwest project boundary along Badillo Street. The catch basin flows discharge into the existing 81" storm drain (Regional Project No. 1123) along Badillo Street; (Refer to the hydrology map for detailed locations). The existing storm drain plans for Regional Project No. 1123 can be found in Reference Section 5.

During the proposed condition, the project site will be proposed to follow the existing condition drainage pattern – discharging into the existing 81" storm drain (Regional Project No. 1123) with the proposed onsite storm drains and the new connections. The proposed Modular Wetland Systems (MWS) are provided for the treatment of the water quality flows.

C. STUDY PURPOSE

The purpose of this study is to analyze pre-project and post-project hydrology of the project site to determine the peak flow rates of storm runoff and to analyze the negative impacts, if any, due to the project developments.

D. HYDROLOGIC INFORMATION

A 25-year storm was analyzed for the project site. The project site encompasses the No. 006 soil group. The 50-year 24-hour isohyet is approximately 7.1 inches. The project falls into DPA zone 6. The 85th Percentile, 24-hr Rainfall is approximately 1.0 inches. The reference Los Angeles County Hydrology Map GIS information can be found in this Section.

The area averaged 96% of impervious percentage (Retail Center Land Use) was applied for the existing condition hydrology analysis and a uniform 86% of impervious area (Apartments and Condominiums Residential) was applied for the proposed condition hydrology analysis.

E. METHODOLOGY

The methodology described in the Los Angeles County Department of Public Works (LACDPW) Hydrology Manual dated January 2006, was used to compute storm run-off from the project site. The LACDPW HydroCalc computer program was used to compute subarea time of concentration (TC), Peak Flow Rates and Runoff Volume. The hydrology calculations are included in Section 2 for existing (pre-project) and Section 3 proposed (post-project) conditions of this report.

F. HYDROLOGY CALCULATION RESULTS

The summary of the hydrology study results and the comparisons between the existing and proposed conditions can be found in the following Hydrology Summary Table.

Hydrology Summary Table
Covina Bowl - VTTM 82874
City of Covina, County Of Los Angeles

Drainage Area	Existing Condition (1)		Proposed Condition (2)		Differences (3)=(2)-(1)	
	Area	25-yr Storm	Area	25-yr Storm	Area	25-yr Storm
	(acre)	(cfs)	(acre)	(cfs)	(acre)	(cfs)
1A	4.55	11.51	4.44	10.56	-0.11	-0.95
2B	1.47	3.72	1.58	3.80	0.11	0.08
Total	6.02	15.23	6.02	14.36	0.00	-0.87

As indicated from the summary table, the overall peak flow rates decreases due to the project development. The overall peak flow rate decreases 0.87 cfs for 25-year storm. Overall, it is concluded that there will have no adverse impacts to the existing drainage systems due to the project developments.

G. LID/WATER QUALITY

This will require all filtration water quality devices to be sized per Adjusted Design Intensity to Provide Additional Capture In Lieu of Volume Reduction (see attached below).

July 2018

Table 6: Adjusted Design Intensity to Provide Additional Capture In Lieu of Volume Reduction (Option B)

Adjusted Time of Concentration (min)	Reliable Infiltration Rate at Site			
	0 in/hr (ET only)	0.01 in/hr	0.05 in/hr	0.15 in/hr
	Capture Efficiency Target = 93.8%	Capture Efficiency Target = 94.1%	Capture Efficiency Target = 95.4%	Capture Efficiency Target = 98.1%
Adjusted MWS Design Precipitation Intensities, in/hr				
5	0.55	0.57	0.66	N/A
7.5	0.51	0.53	0.60	0.96
10	0.48	0.49	0.57	0.90
15	0.44	0.45	0.52	0.79
20	0.41	0.42	0.48	0.74
30	0.37	0.38	0.43	0.64
60	0.31	0.31	0.35	0.50

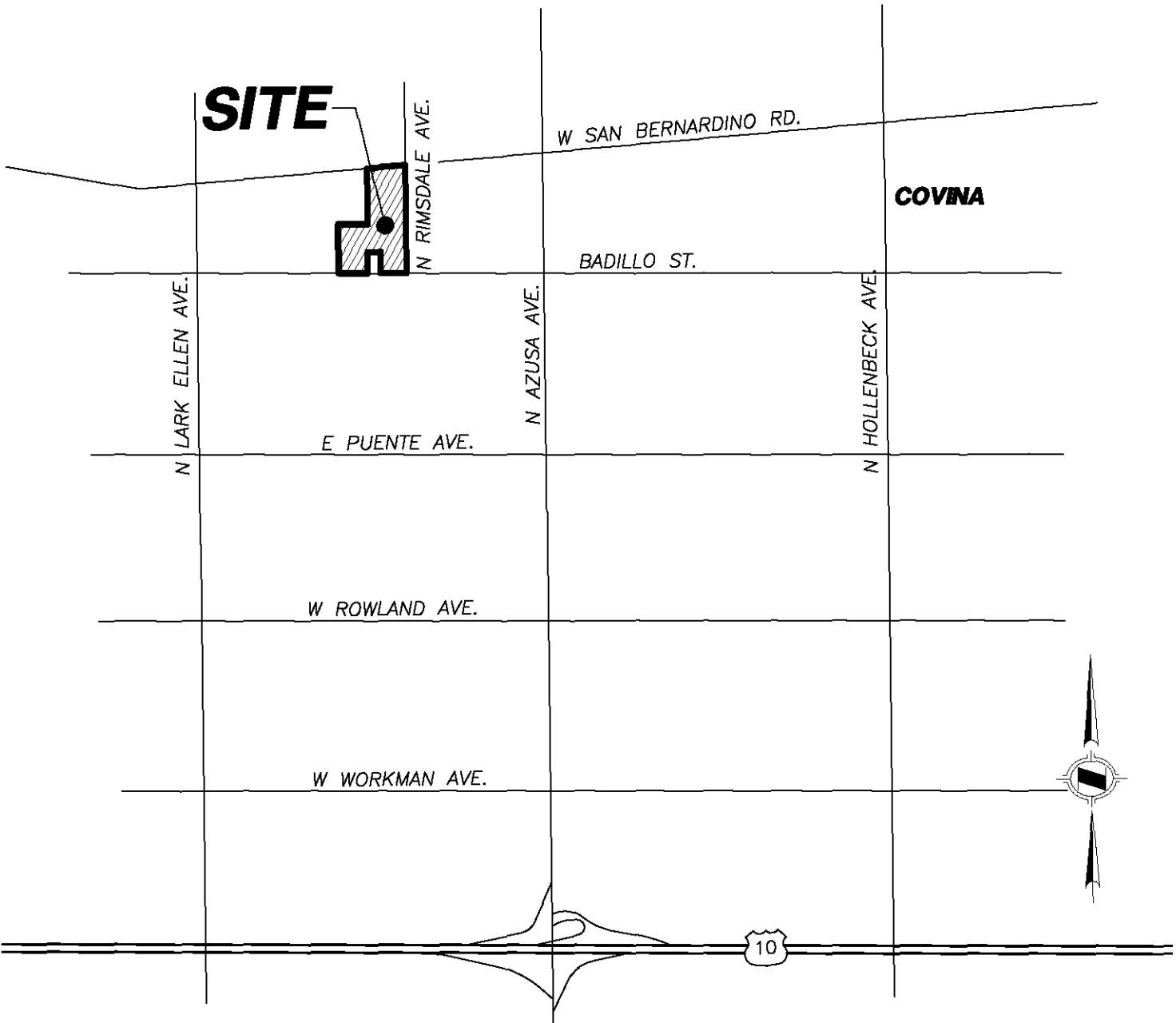
NA = additional capture is not a viable option to offset volume reduction in these cases.

The design storm is determined using the 0.75 inch storm or the 85th percentile storm, whichever is greater. The 85th Percentile, 24-hr Rainfall is approximately 1.0 inches per Los Angeles County Hydrology Map GIS information. The 85th percentile storm (1.0 inches) was selected as the project design storm. The Time of Concentration (TC) calculations from the 85th percentile storm can be found in Section 4 by applying the LACDPW HydroCalc computer program.

There are 2 Modular Wetland Systems (MWS) provided for the on-site project developments. The water quality peak flow calculations can be found in Section 4. The calculated water quality flow rate is about 1.2418 cfs and the total provided treatment capacity by the 2 MWS systems is about 1.3860 cfs with 0.693 cfs treatment capacity for each MWS-8-24.

There is one MWS provided for the Rimsdale Avenue widening. The water quality peak flow calculations can be found in Section 4. The calculated water quality flow rate is about 0.229 cfs and the provided treatment capacity by the MWS system is about 0.237 cfs for the proposed MWS-4-19.

The detailed Low Impact Development (LID) can be found from the separate LID report and preliminary sizing for the MWS systems can be found in Section 4.



Hydrology Map A GIS viewer application to view the data for the hydrology manual.

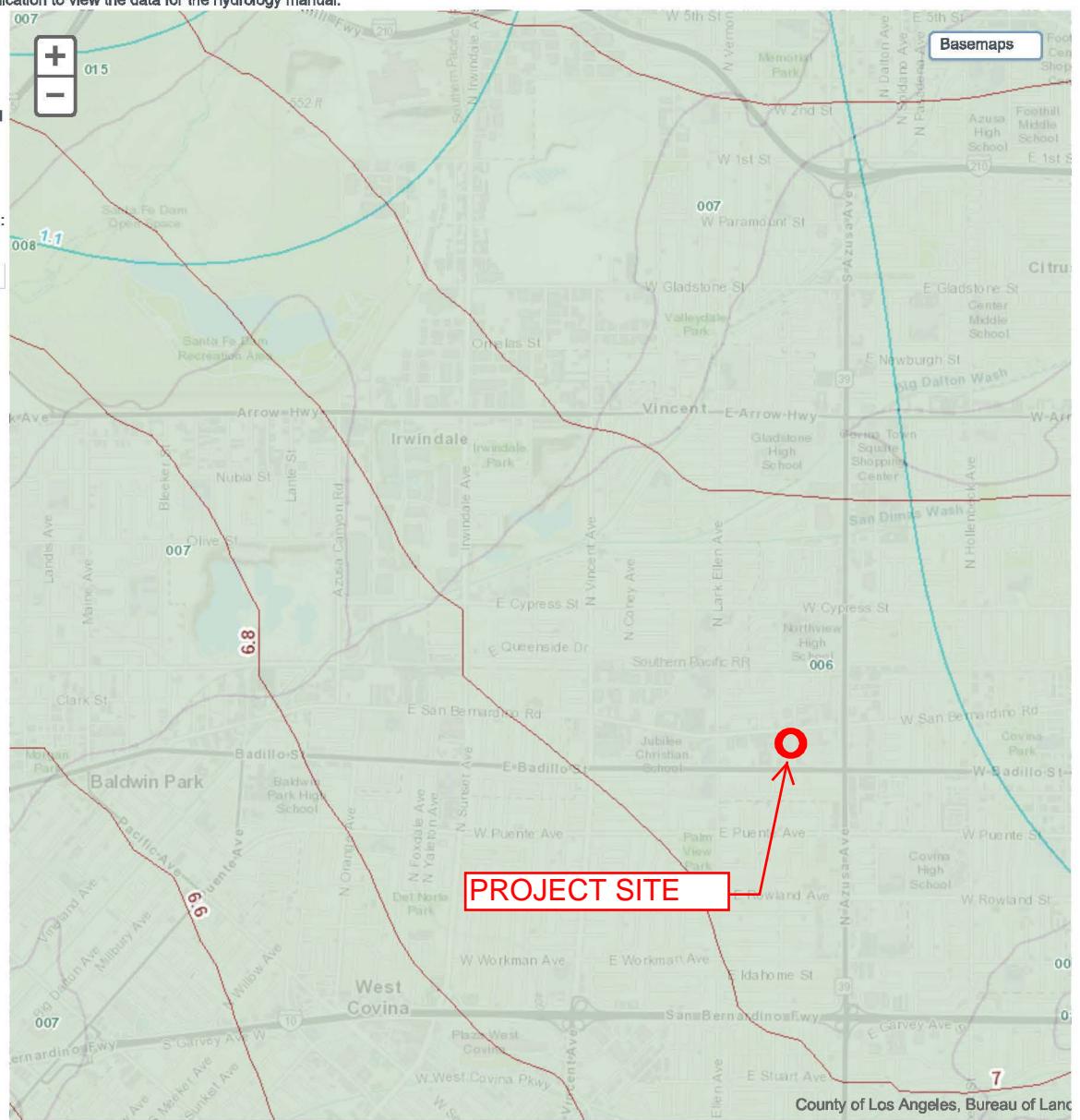
LAYERS

- 50yr Two Tents (Rainfall)
- DPA Zones
- Soils 2004
- Final 85th Percentile, 24-hr Rainfall
- Final 95th Percentile, 24-hr Rainfall
- 1-year, 1-hour Rainfall Intensity

SEARCH

Enter Address, Cross Street, or Parcel No.:
(ex: 900 S. Fremont Ave., Fremont@Valley,
5342005904)

Search



[Map Tips](#)

SECTION 2

EXISTING CONDITION

HYDROLOGY CALCULATIONS AND MAP

Peak Flow Hydrologic Analysis

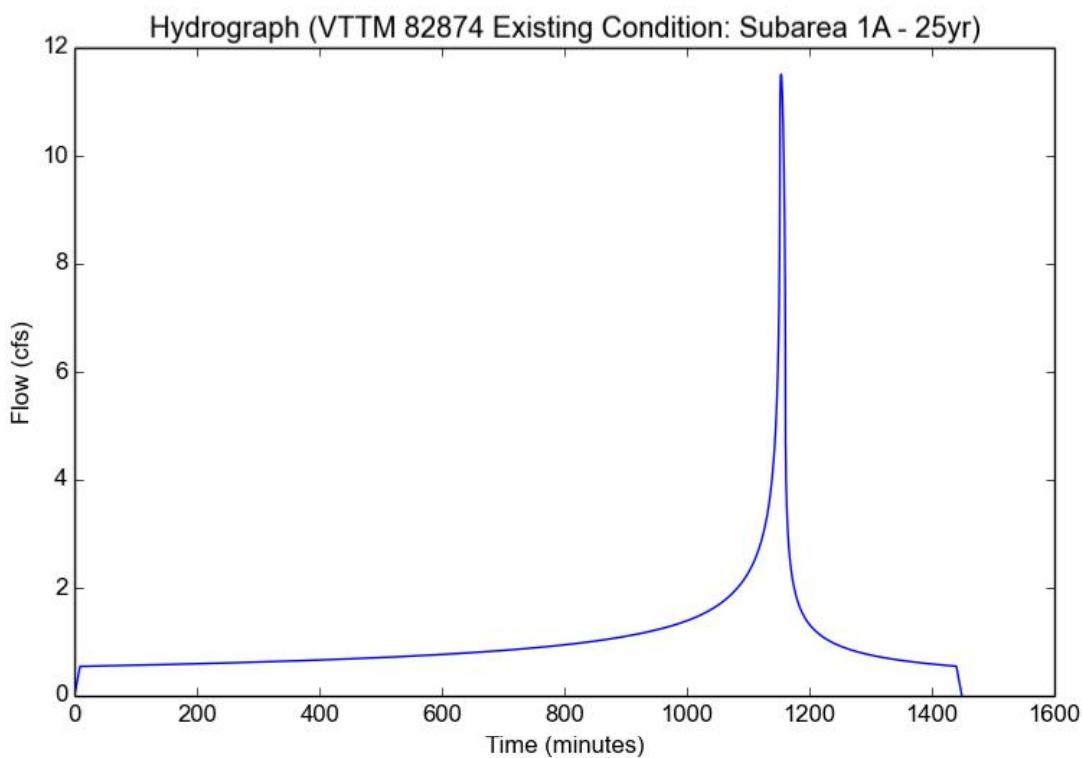
File location: C:/SD/Covina Bowl/VTTM 82874 Existing Condition - Subarea 1A - 25yr.pdf
Version: HydroCalc 1.0.3

Input Parameters

Project Name	VTTM 82874 Existing Condition
Subarea ID	Subarea 1A - 25yr
Area (ac)	4.55
Flow Path Length (ft)	775.0
Flow Path Slope (vft/hft)	0.009
50-yr Rainfall Depth (in)	7.1
Percent Impervious	0.96
Soil Type	6
Design Storm Frequency	25-yr
Fire Factor	0
LID	False

Output Results

Modeled (25-yr) Rainfall Depth (in)	6.2338
Peak Intensity (in/hr)	2.8215
Undeveloped Runoff Coefficient (Cu)	0.8097
Developed Runoff Coefficient (Cd)	0.8964
Time of Concentration (min)	9.0
Clear Peak Flow Rate (cfs)	11.5076
Burned Peak Flow Rate (cfs)	11.5076
24-Hr Clear Runoff Volume (ac-ft)	2.046
24-Hr Clear Runoff Volume (cu-ft)	89124.5903



Peak Flow Hydrologic Analysis

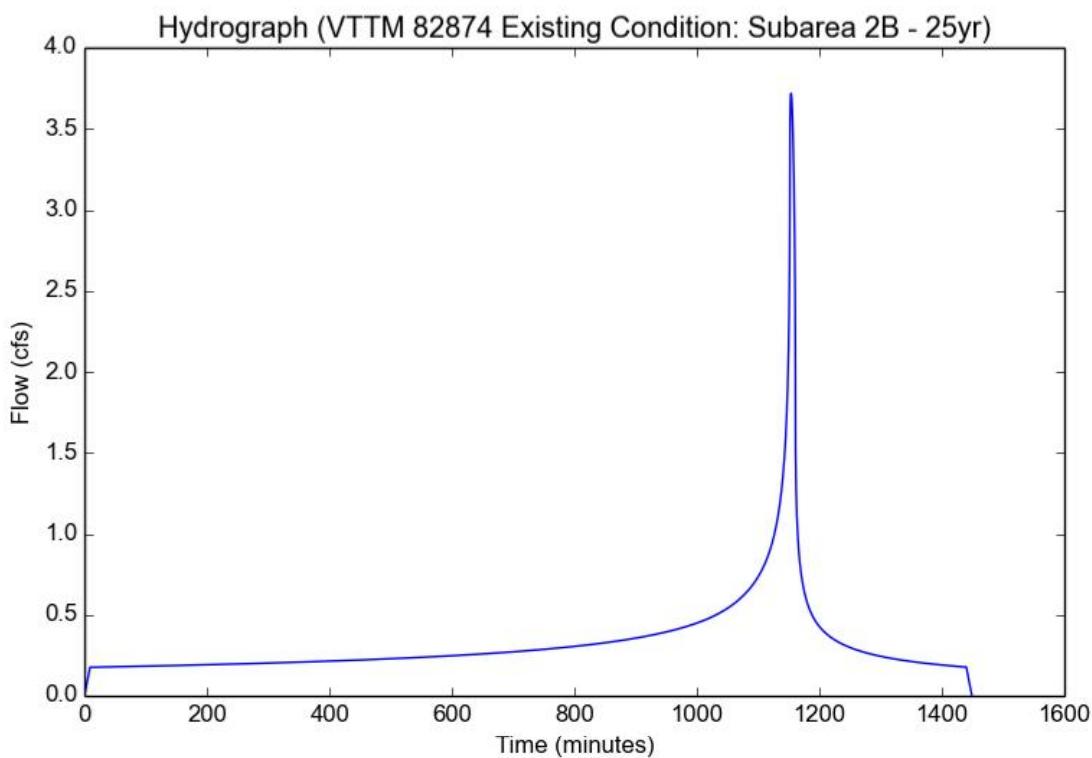
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Version: HydroCalc 1.0.3

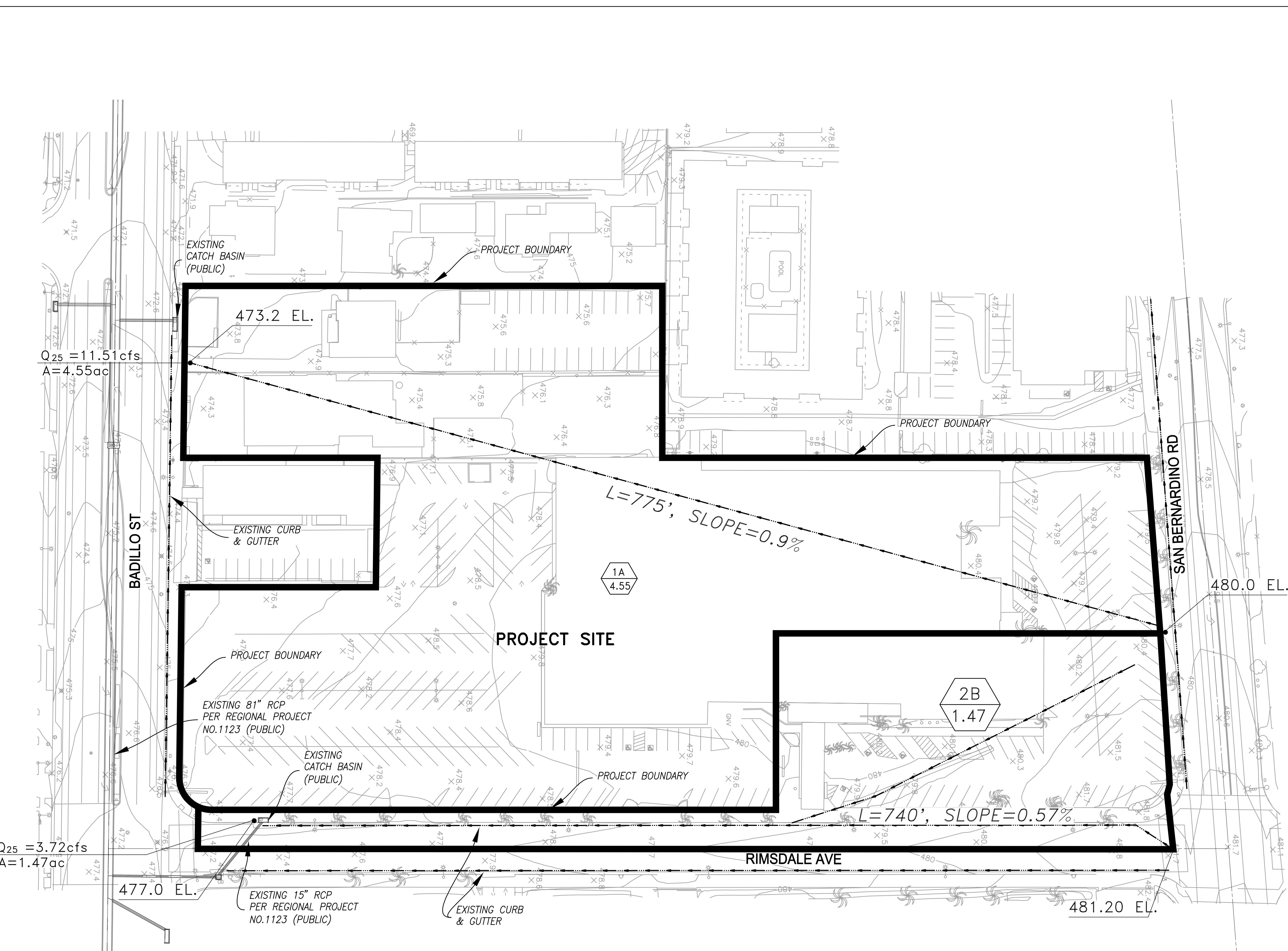
Input Parameters

Project Name	VTTM 82874 Existing Condition
Subarea ID	Subarea 2B - 25yr
Area (ac)	1.47
Flow Path Length (ft)	740.0
Flow Path Slope (vft/hft)	0.0057
50-yr Rainfall Depth (in)	7.1
Percent Impervious	0.96
Soil Type	6
Design Storm Frequency	25-yr
Fire Factor	0
LID	False

Output Results

Modeled (25-yr) Rainfall Depth (in)	6.2338
Peak Intensity (in/hr)	2.8215
Undeveloped Runoff Coefficient (Cu)	0.8097
Developed Runoff Coefficient (Cd)	0.8964
Time of Concentration (min)	9.0
Clear Peak Flow Rate (cfs)	3.7179
Burned Peak Flow Rate (cfs)	3.7179
24-Hr Clear Runoff Volume (ac-ft)	0.661
24-Hr Clear Runoff Volume (cu-ft)	28794.0984





HYDROLOGY CALCULATION TABLE

SUBAREA	AREA (ACRES)	25-YR FLOW RATE (CFS)	25-YR FLOW VOLUME (AC-FT)
1A	4.55	11.51	2.05
2B	1.47	3.72	0.66
OVERALL	6.02	15.23	2.71

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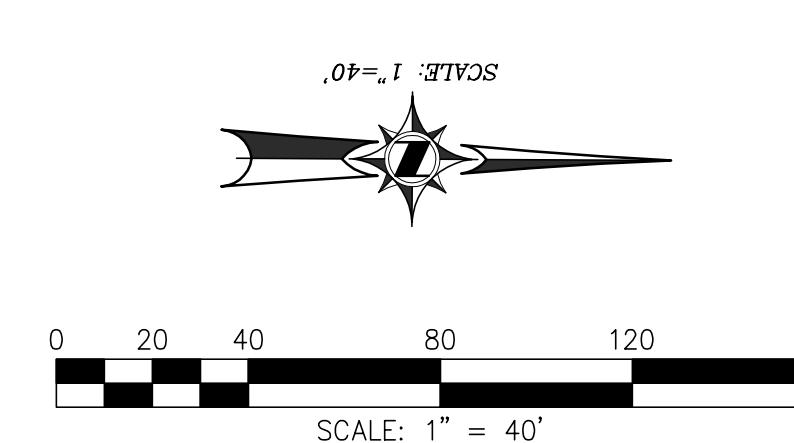
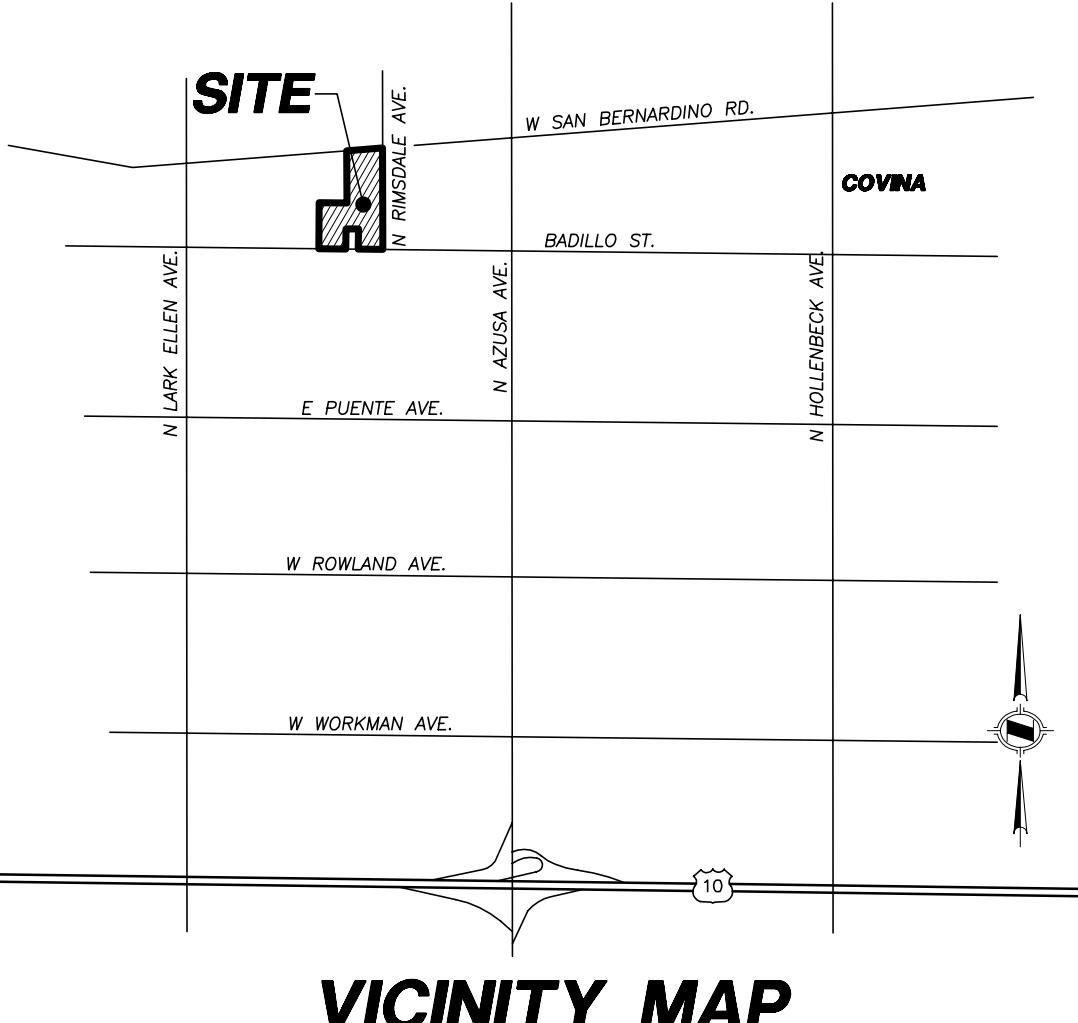


EXHIBIT 1
DRAINAGE CONCEPT/HYDROLOGY STUDY FOR
EXISTING CONDITION HYDROLOGY MAP
VESTING TENTATIVE TRACT MAP 82874
CITY OF COVINA, COUNTY OF LOS ANGELES



HYDROLOGIC INFORMATION

6	DPA ZONE
006	SOIL GROUP
7.1"	50-YEAR 24-HOUR ISOHYET
96%	AREA AVERAGE % IMPERVIOUSNESS (RETAIL CENTER)
1	BURN FACTOR
1	BULKING FACTOR
1.0"	85TH PERCENTILE RAINFALL DEPTH
85TH PERCENTILE RAINFALL DEPTH	PROJECT DESIGN STORM (0.75 INCHES OR 85TH PERCENTILE)
0%	PERCENT OF DESIGN STORM RETAINED ON-SITE
0%	PERCENT OF DESIGN STORM INFILTRATED OFF-SITE

LEGEND

DRainage Boundary
AREA DESIGNATION FOR AREA "A" AREA ACREAGE (IN ACRES)
1A 1.0
FLOW LINE
$Q_{25} = 30.0 \text{ cfs}$ $A = 10.0 \text{ ac}$
PEAK 25-YR FLOW RATE DRAINAGE AREA IN ACRES

SECTION 3

PROPOSED CONDITION

HYDROLOGY CALCULATIONS AND MAP

Peak Flow Hydrologic Analysis

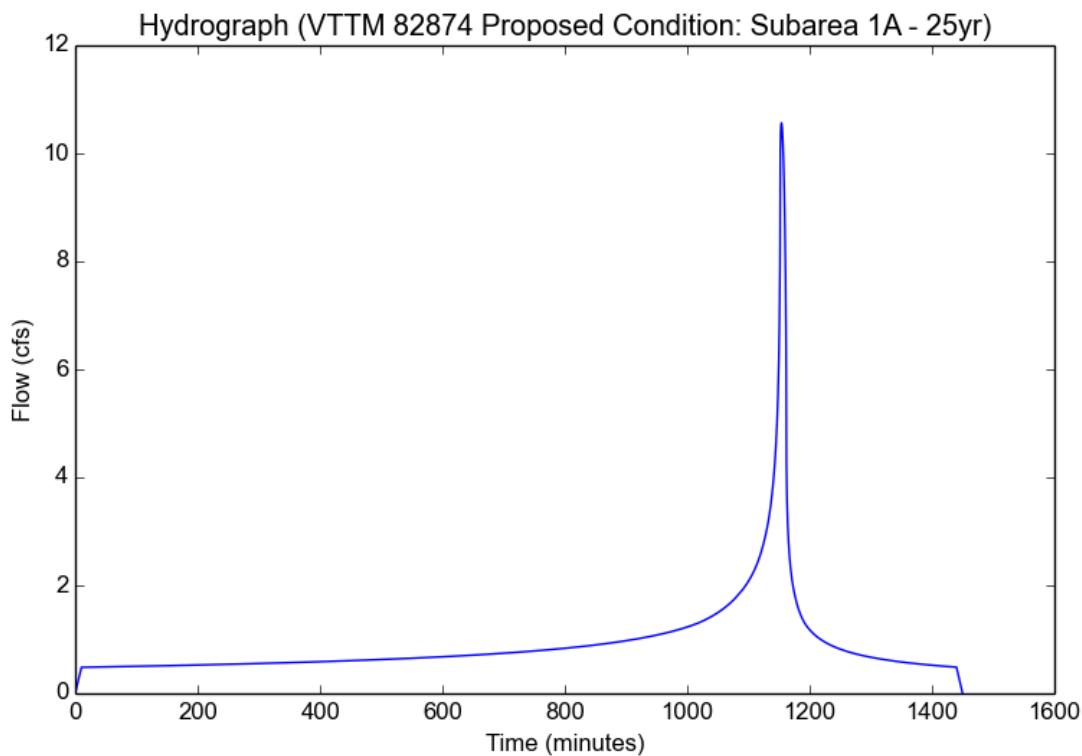
File location: C:/SD/Covina Bowl/VTTM 82874 Proposed Condition - Subarea 1A - 25yr.pdf
Version: HydroCalc 1.0.3

Input Parameters

Project Name	VTTM 82874 Proposed Condition
Subarea ID	Subarea 1A - 25yr
Area (ac)	4.44
Flow Path Length (ft)	880.0
Flow Path Slope (vft/hft)	0.007
50-yr Rainfall Depth (in)	7.1
Percent Impervious	0.86
Soil Type	6
Design Storm Frequency	25-yr
Fire Factor	0
LID	False

Output Results

Modeled (25-yr) Rainfall Depth (in)	6.2338
Peak Intensity (in/hr)	2.6852
Undeveloped Runoff Coefficient (Cu)	0.8002
Developed Runoff Coefficient (Cd)	0.886
Time of Concentration (min)	10.0
Clear Peak Flow Rate (cfs)	10.5633
Burned Peak Flow Rate (cfs)	10.5633
24-Hr Clear Runoff Volume (ac-ft)	1.8411
24-Hr Clear Runoff Volume (cu-ft)	80199.3316



Peak Flow Hydrologic Analysis

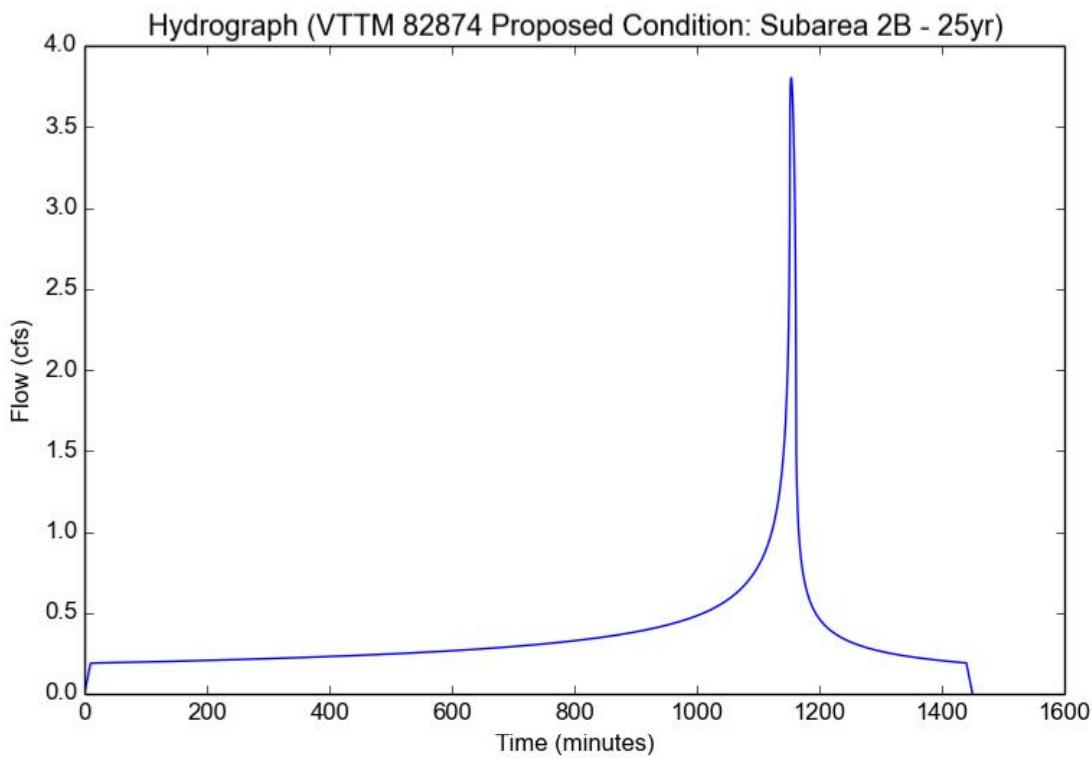
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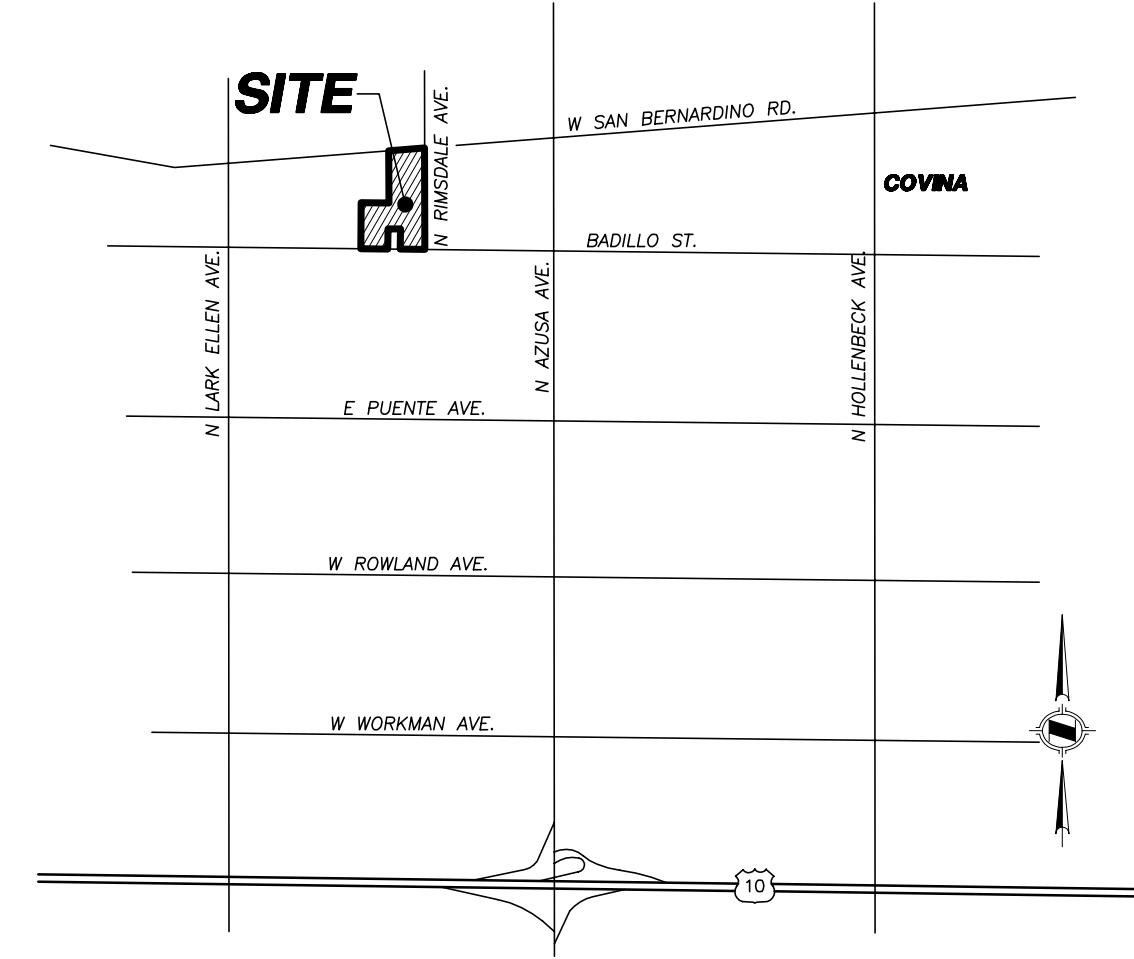
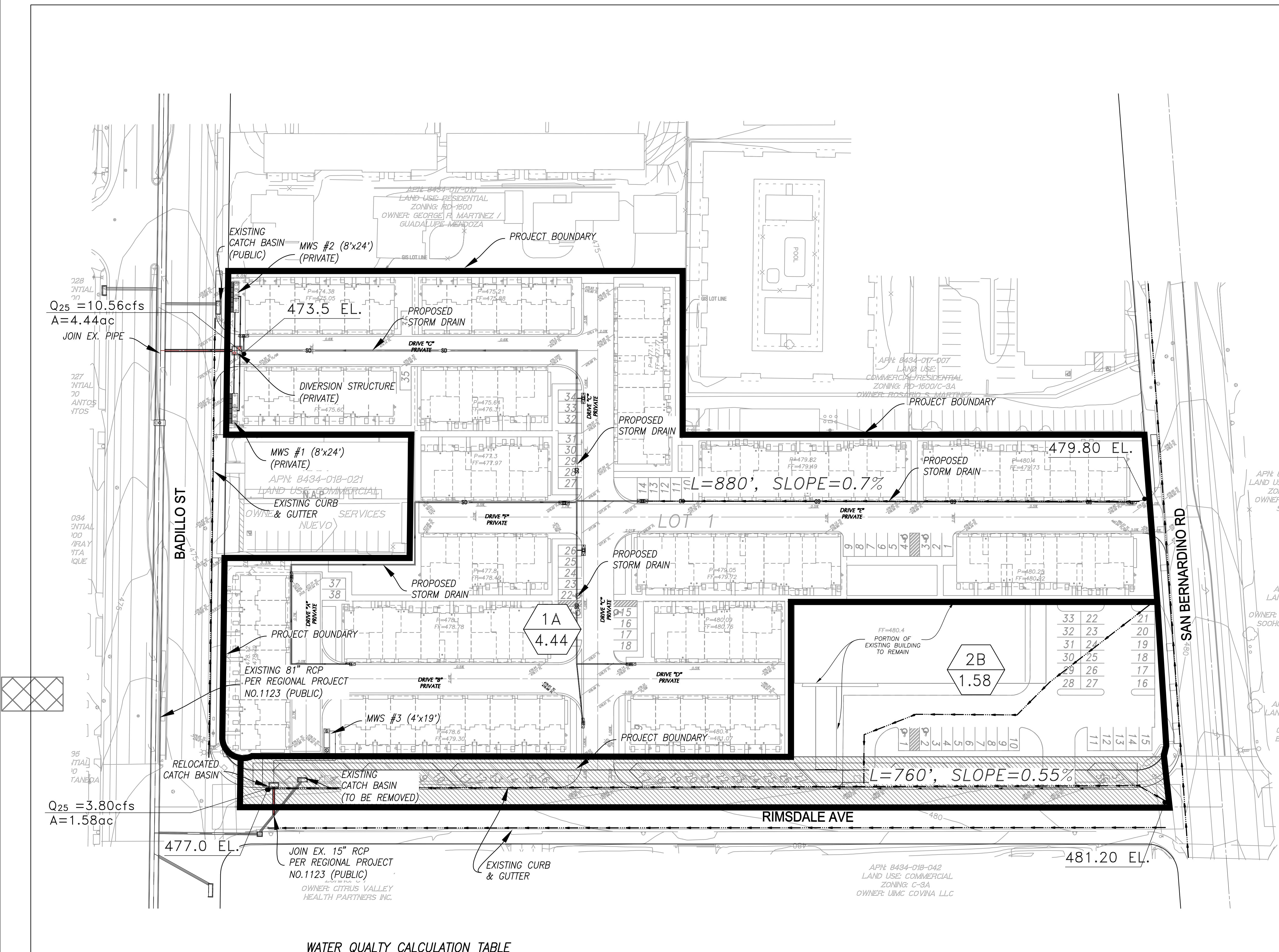
Input Parameters

Project Name	VTTM 82874 Proposed Condition
Subarea ID	Subarea 2B - 25yr
Area (ac)	1.58
Flow Path Length (ft)	760.0
Flow Path Slope (vft/hft)	0.0055
50-yr Rainfall Depth (in)	7.1
Percent Impervious	0.96
Soil Type	6
Design Storm Frequency	25-yr
Fire Factor	0
LID	False

Output Results

Modeled (25-yr) Rainfall Depth (in)	6.2338
Peak Intensity (in/hr)	2.6852
Undeveloped Runoff Coefficient (Cu)	0.8002
Developed Runoff Coefficient (Cd)	0.896
Time of Concentration (min)	10.0
Clear Peak Flow Rate (cfs)	3.8014
Burned Peak Flow Rate (cfs)	3.8014
24-Hr Clear Runoff Volume (ac-ft)	0.7105
24-Hr Clear Runoff Volume (cu-ft)	30948.4785





HYDROLOGIC INFORMATION

6	DPA ZONE
006	SOIL GROUP
7.1"	50-YEAR 24-HOUR ISOHYET
86%	AREA AVERAGE % IMPERVIOUSNESS (APARTMENTS AND CONDOMINIUMS)
1	BURN FACTOR
1	BULKING FACTOR
1.0"	85TH PERCENTILE RAINFALL DEPTH
85TH PERCENTILE RAINFALL DEPTH	PROJECT DESIGN STORM (0.75 INCHES OR 85TH PERCENTILE)
0%	PERCENT OF DESIGN STORM RETAINED ON-SITE
0%	PERCENT OF DESIGN STORM INFILTRATED OFF-SITE

LEGEND

- DRAINAGE BOUNDARY
- 1A 4.44 AREA DESIGNATION FOR AREA "A"
AREA ACREAGE (IN ACRES)
- FLOW LINE
- Q₂₅ = 30.0 cfs PEAK 25-YR FLOW RATE
- A = 10.0 ac DRAINAGE AREA IN ACRES
- PROPOSED STORM DRAIN
- AREA TO SIZE THE BMP FACILITIES
(HALF STREET OF RIMSDALE AVENUE, 0.71 ACRES)

HYDROLOGY CALCULATION TABLE

SUBAREA	AREA (ACRES)	25-YR FLOW RATE (CFS)	25-YR FLOW VOLUME (AC-FT)
1A	4.44	10.56	1.84
2B	1.58	3.80	0.71
OVERALL	6.02	14.36	2.55

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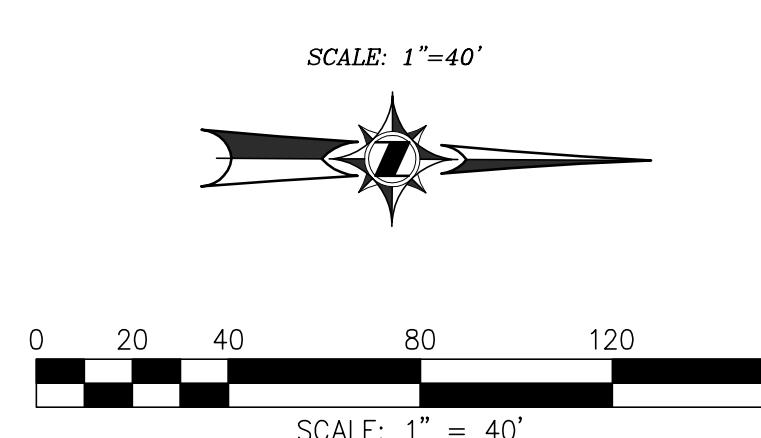


EXHIBIT 2
DRAINAGE CONCEPT/HYDROLOGY STUDY FOR PROPOSED CONDITION HYDROLOGY MAP
VESTING TENTATIVE TRACT MAP 82874
CITY OF COVINA, COUNTY OF LOS ANGELES

SECTION 4

LID CALCUALTIONS

The project will be required to comply with the newly adopted MS4 Permit. This will require all filtration water quality devices to be sized per Adjusted Design Intensity to Provide Additional Capture In Lieu of Volume Reduction (see attached below).

July 2018

Table 6: Adjusted Design Intensity to Provide Additional Capture In Lieu of Volume Reduction (Option B)

Adjusted Time of Concentration (min)	Reliable Infiltration Rate at Site			
	0 in/hr (ET only)	0.01 in/hr	0.05 in/hr	0.15 in/hr
	Capture Efficiency Target = 93.8%	Capture Efficiency Target = 94.1%	Capture Efficiency Target = 95.4%	Capture Efficiency Target = 98.1%
Adjusted MWS Design Precipitation Intensities, in/hr				
5	0.55	0.57	0.66	N/A
7.5	0.51	0.53	0.60	0.96
10	0.48	0.49	0.57	0.90
15	0.44	0.45	0.52	0.79
20	0.41	0.42	0.48	0.74
30	0.37	0.38	0.43	0.64
60	0.31	0.31	0.35	0.50

NA = additional capture is not a viable option to offset volume reduction in these cases.

On-site Area (Area 1A)

Per SUSMP flow rate calculations,

$$Q_{PM} = C_D * I_x * A_{Total} * (1.008333 \text{ ft}_3\text{-hour / acre-inches-seconds})$$

Where:

Q_{PM} =Peak Mitigation Flow Rate (cfs)

$$C_D = (0.9 * Imp.) + [(1.0 - Imp.) * C_U]$$

Imp=0.86 for Apartments and Condominiums Residential, Cu=0.1 per below

$$=0.9*0.86+ (1-0.86)*0.1$$

$$=0.788$$

C_U = Undeveloped Runoff Coefficient, (**0.1** for Soil 06)

I_x = **0.352**, Rainfall Intensity (inches / hour) (per above Table 6 using Infiltration Rate at 0 in/hour,

TC=**39** minutes per 85th Percentile HydroCalc Calculations)

A_{Total} = **4.44** acres (Total Area in acres)

Rimsdale Avenue Widending (Area 2B)

Please note, only Half Street of Rimsdale Avenue tributary areas are applied in the BMP sizings.

Per SUSMP flow rate calculations,

$$Q_{PM} = C_D * I_x * A_{Total} * (1.008333 \text{ ft}_3\text{-hour / acre-inches-seconds})$$

Where:

Q_{PM} =Peak Mitigation Flow Rate (cfs)

$$C_D = (0.9 * Imp.) + [(1.0 - Imp.) * C_U]$$

Imp=0.96 for the roadway, Cu=0.1 per below

$$=0.9*0.96+ (1-0.96)*0.1$$

$$=0.868$$

C_U = Undeveloped Runoff Coefficient, (**0.1** for Soil 06)

I_x = **0.369**, Rainfall Intensity (inches / hour) (per above Table 6 using Infiltration Rate at 0 in/hour,

TC=**35 minutes** per 85th Percentile HydroCalc Calculations)

A_{Total} = **0.71 acres** (Total Area in acres – half street of Rimsdale Avenue)

The LID flow rate calculations can be found from the following table.

LID Flow Rate and Treatment BMP Summary Table
Covina Bowl - VTTM 82874
City of Covina, County Of Los Angeles

DMA	Area (acre)	TC (Min)	C_D	I_x (in/hr)	Q_{PM} (cfs)	MWS #	MWS Size	MWS Design Capacity (cfs)	Provided Capacity (cfs)
On-Site Area	4.44	39	0.788	0.352	1.2726	#1	MWS-8-24	0.693	1.386
						#2	MWS-8-24	0.693	
Rimsdale Widening	0.71	35	0.868	0.369	0.229	#3	MWS-4-19	0.237	0.237

Peak Flow Hydrologic Analysis

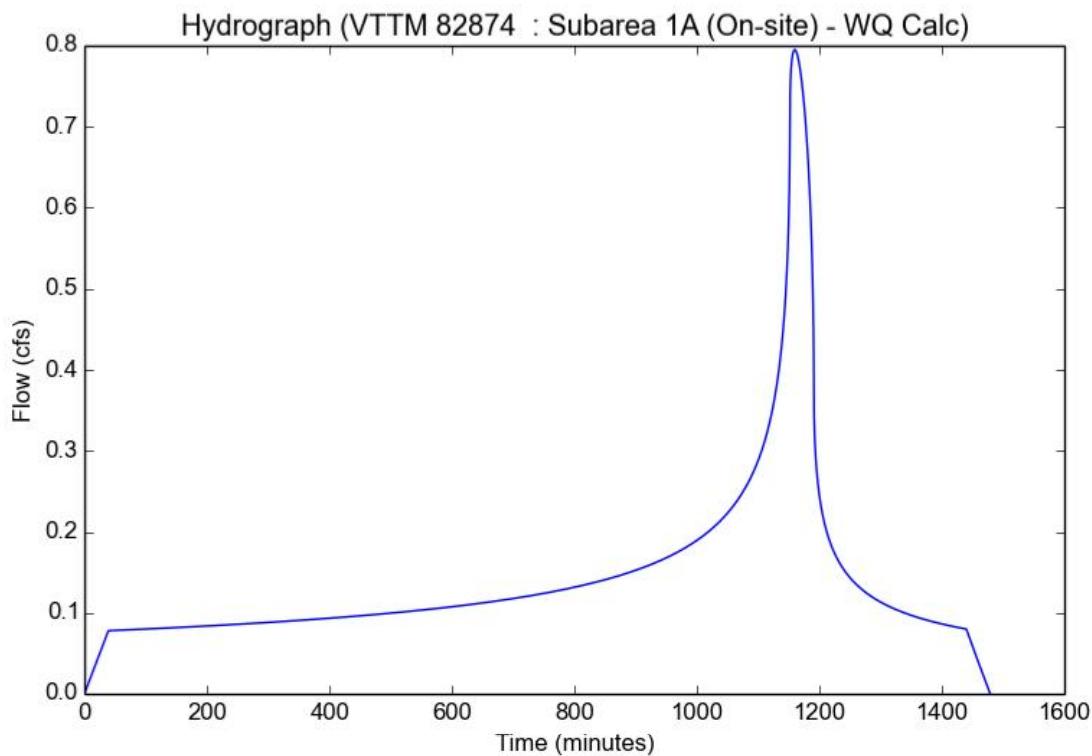
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Version: HydroCalc 1.0.3

Input Parameters

Project Name	VTTM 82874
Subarea ID	Subarea 1A (On-site) - WQ Calc
Area (ac)	4.44
Flow Path Length (ft)	880.0
Flow Path Slope (vft/hft)	0.007
85th Percentile Rainfall Depth (in)	1.0
Percent Impervious	0.86
Soil Type	6
Design Storm Frequency	85th percentile storm
Fire Factor	0
LID	True

Output Results

Modeled (85th percentile storm) Rainfall Depth (in)	1.0
Peak Intensity (in/hr)	0.2272
Undeveloped Runoff Coefficient (Cu)	0.1
Developed Runoff Coefficient (Cd)	0.788
Time of Concentration (min)	39.0
Clear Peak Flow Rate (cfs)	0.7949
Burned Peak Flow Rate (cfs)	0.7949
24-Hr Clear Runoff Volume (ac-ft)	0.2892
24-Hr Clear Runoff Volume (cu-ft)	12595.6378



Peak Flow Hydrologic Analysis

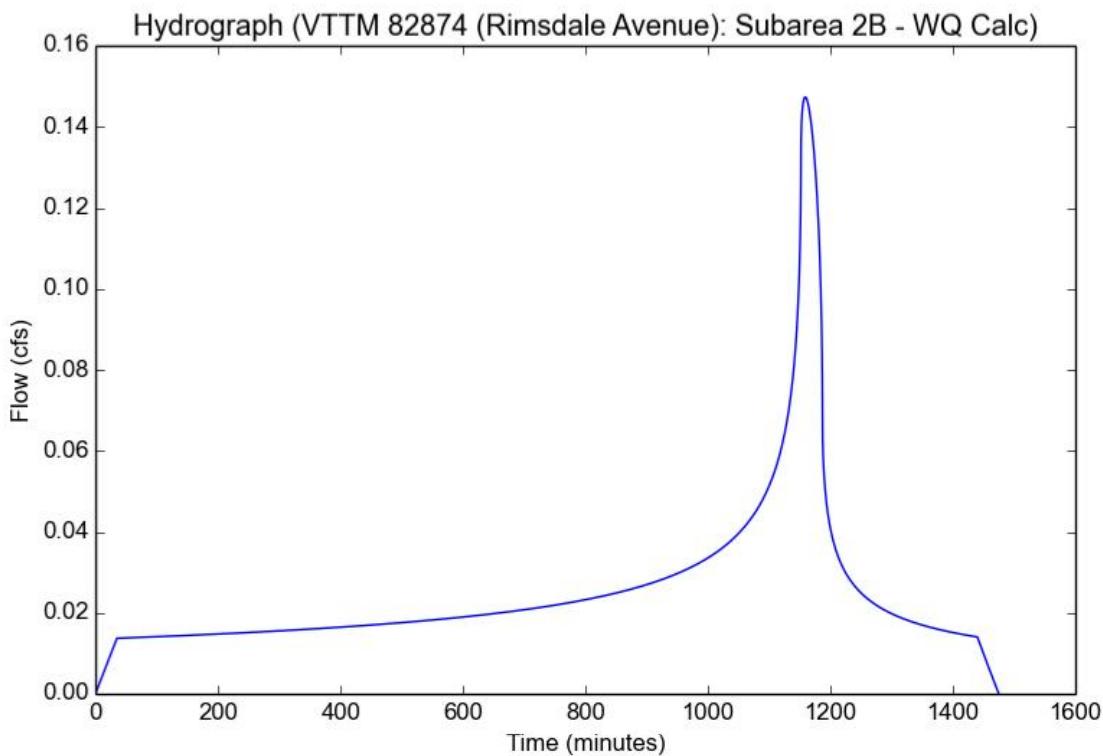
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Version: HydroCalc 1.0.3

Input Parameters

Project Name	VTTM 82874 (Rimsdale Avenue)
Subarea ID	Subarea 2B - WQ Calc
Area (ac)	0.71
Flow Path Length (ft)	760.0
Flow Path Slope (vft/hft)	0.0055
85th Percentile Rainfall Depth (in)	1.0
Percent Impervious	0.96
Soil Type	6
Design Storm Frequency	85th percentile storm
Fire Factor	0
LID	True

Output Results

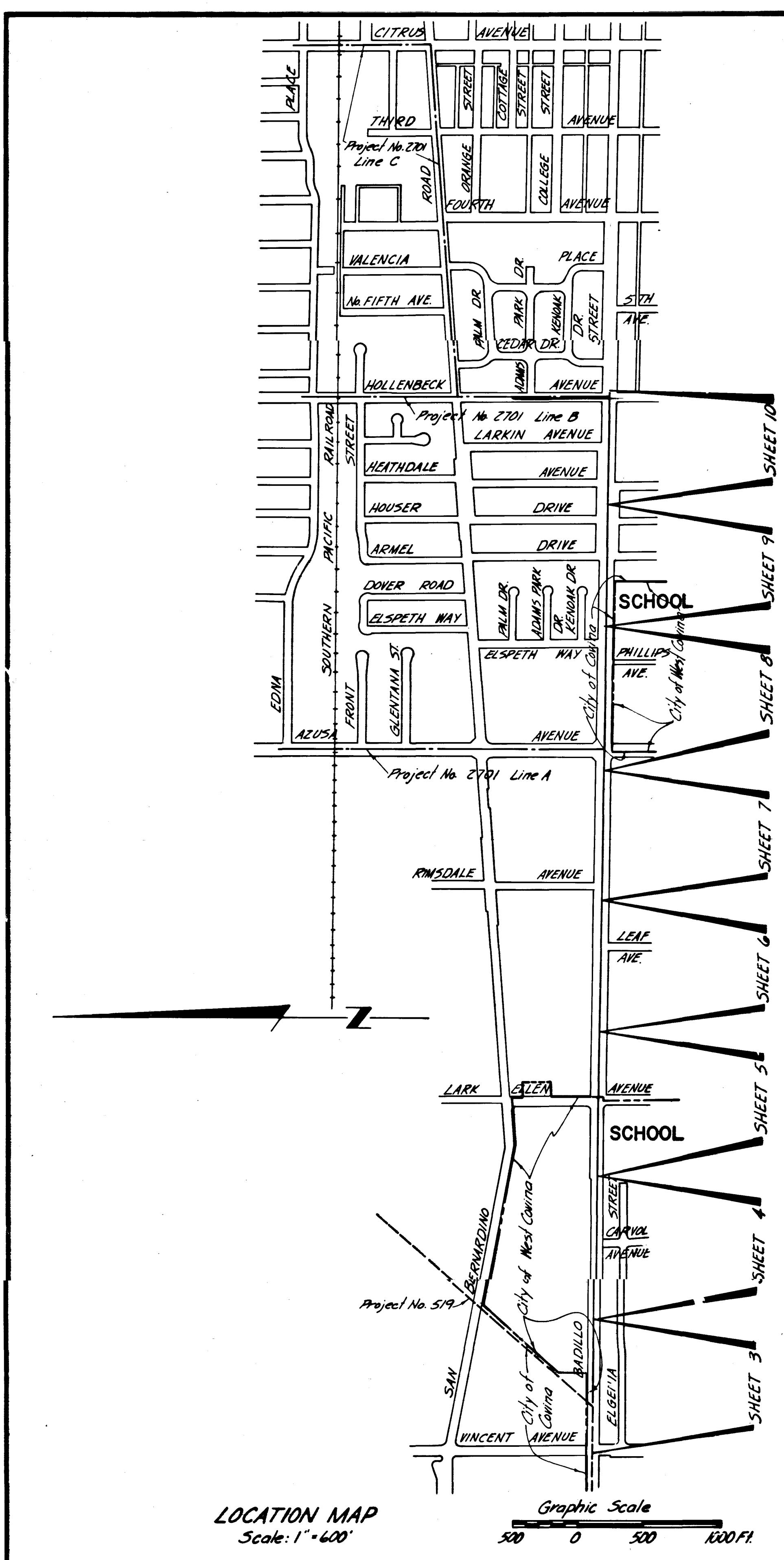
Modeled (85th percentile storm) Rainfall Depth (in)	1.0
Peak Intensity (in/hr)	0.2391
Undeveloped Runoff Coefficient (Cu)	0.1
Developed Runoff Coefficient (Cd)	0.868
Time of Concentration (min)	35.0
Clear Peak Flow Rate (cfs)	0.1473
Burned Peak Flow Rate (cfs)	0.1473
24-Hr Clear Runoff Volume (ac-ft)	0.0509
24-Hr Clear Runoff Volume (cu-ft)	2218.6428



SECTION 5

REFERENCES

- **EXISTING STORM DRAIN PLANS FOR REGIONAL PROJECT NO. 1123**



GENERAL NOTES

1. NUMBERS IN CIRCLES INDICATE ITEMS UNDER WHICH PAYMENT WILL BE MADE.
2. ELEVATIONS SHOWN ARE IN FEET ABOVE THE U.S.G.S. MEAN SEA LEVEL DATUM.
3. STATIONS SHOWN ON DRAWINGS ARE ALONG CENTER LINE OF CONDUIT OR ON A LINE NORMAL TO CENTER LINE OF CONDUIT.
4. STATIONS AND INVERT ELEVATIONS OF PIPE INLETS SHOWN ON THE PROFILES ARE AT THE INSIDE FACE OF THE CONDUIT, UNLESS OTHERWISE SHOWN.
5. ALL PIPE IN OPEN TRENCH SHALL BE BEDDED ACCORDING TO STANDARD DRAWING 2-D177, CASE III, EXCEPT BELL AND SPIGOT PIPE WHICH SHALL BE CASE II BEDDING, UNLESS OTHERWISE SHOWN OR MODIFIED IN THE SPECIFICATIONS.
6. PIPE CONNECTIONS TO STORM DRAIN SHALL CONFORM TO STANDARD DRAWINGS 2-D191 OR 2-D193, UNLESS OTHERWISE SHOWN.
7. WHERE REQUIRED BY STANDARD DRAWING 2-D 213.1, CONCRETE BACKFILL SHALL BE USED AROUND CONNECTOR PIPES 36 INCHES OR LESS IN DIAMETER. CONCRETE BACKFILL FOR MAIN LINE PIPE SHALL BE USED ONLY WHEN DIRECTED BY THE ENGINEER.
8. TIES FOR CATCH BASINS AS SHOWN ON THE DRAWINGS ARE FROM CURB RETURN TO CENTER LINE OF CATCH BASIN, UNLESS OTHERWISE SHOWN.
9. 'BLANKET S.S.', WHERE NOTED ON THE DRAWINGS, SHALL BE PER STANDARD DRAWING 2-D 251, CASE IV, HALF-SECTION-D.
10. CURB FACES(C.F) AT THE CATCH BASIN OPENINGS SHALL BE THAT OF EXISTING CURB PLUS: 4" WHERE L.D. NO. 2 IS SPECIFIED AND 2" WHERE L.D. NO. 4 IS SPECIFIED, UNLESS OTHERWISE SHOWN.
11. THE OPENINGS AND TOP SLABS OF ALL SIDE INLET CATCH BASINS SHALL BE MODIFIED TO MEET THE REQUIREMENTS SHOWN ON STANDARD DRAWING 2-D 232.
12. LOCATIONS OF CATCH BASIN CONNECTOR PIPE JUNCTIONS WITH CATCH BASINS AS SHOWN ON THE DRAWINGS ARE SCHEMATIC. IT IS INTENDED THAT SUCH JUNCTIONS BE LOCATED AT THE DOWNSTREAM ENDS OF THE CATCH BASINS, UNLESS OTHERWISE SHOWN. IN ALL CASES THE EXACT LOCATIONS WILL BE DETERMINED IN THE FIELD BY THE ENGINEER TO MEET FIELD CONDITIONS.
13. MONOLITHIC CATCH BASIN CONNECTIONS SHALL BE CONSTRUCTED, WHERE APPLICABLE, PER STANDARD DRAWING 2-D 224.
14. THE DEPTH AT THE UPSTREAM END OF CATCH BASINS 10 FEET OR MORE IN LENGTH SHALL BE CURB FACE PLUS 12 INCHES, UNLESS OTHERWISE SHOWN.
15. "V_i" IS THE DEPTH OF INLET OF CATCH BASINS IN SERIES MEASURED FROM TOP OF CURB TO INVERT OF CONNECTOR PIPE.
16. EXISTING UTILITIES SHALL BE MAINTAINED IN PLACE BY THE CONTRACTOR, UNLESS OTHERWISE NOTED.
17. DELETED.
18. LOCATIONS SHOWN ON THE PLANS FOR EXISTING SANITARY SEWER HOUSE CONNECTIONS ARE APPROXIMATE ONLY.
19. DELETED
20. SANITARY SEWERS AND HOUSE CONNECTIONS CROSSING OVER THE STORM DRAIN TRENCH SHALL BE SUPPORTED IN ACCORDANCE WITH STANDARD DRAWING 2-D173.1 TO .3 AND ENCASED PER GENERAL NOTE 1 ON STANDARD DRAWING 2-D173.1.
21. WHEN INDICATED ON THE DRAWINGS, SANITARY SEWERS AND HOUSE CONNECTIONS SHALL BE ENCASED OR BLANKETED IN ACCORDANCE WITH STANDARD DRAWING 2-D 251.
22. ALL OPENINGS RESULTING FROM THE CUTTING OR PARTIAL REMOVAL OF EXISTING CULVERTS, PIPES OR SIMILAR STRUCTURES SHALL BE SEALED NORMAL TO CENTERLINE OF CONDUIT WITH 8 INCHES OF BRICK AND MORTAR OR 6 INCHES OF CONCRETE UNLESS OTHERWISE SHOWN.
23. ALL RESURFACING, CURBS, GUTTERS, SIDEWALKS, DRIVEWAYS AND OTHER EXISTING IMPROVEMENTS TO BE RECONSTRUCTED SHALL BE CONSTRUCTED AT THE SAME ELEVATION AND LOCATION AS THE EXISTING IMPROVEMENTS, UNLESS OTHERWISE SHOWN.
24. REFER TO SHEET 12 FOR TYPICAL CATCH BASIN CONNECTOR PIPE DETAIL.
25. STREET RESURFACING PLANS ARE SHOWN ON SHEET 2.
26. SOIL TEST BORINGS FOR THIS PROJECT WERE MADE MARCH, 1966
27. ELEVATIONS SHOWN ON PLANS FOR CURBS AT CATCH BASINS ARE TOP OF CURB, UNLESS OTHERWISE NOTED.

28. UTILITIES DESIGNATED BY THE SYMBOL * WILL BE ABANDONED IN PLACE AND THE OWNER WILL INSTALL A NEW SECTION OF THE AFFECTED UTILITY AT A LOCATION IN CLOSE PROXIMITY TO, BUT WHICH DOES NOT PHYSICALLY INTERFERE WITH, THE PROPOSED STORM DRAIN CONDUIT AND APPURTENANT STRUCTURES.
29. UTILITIES DESIGNATED BY THE SYMBOL ≠ WILL BE REMOVED BY THE OWNER AND THE OWNER WILL REINSTALL A NEW SECTION OF THE AFFECTED UTILITY AT A LOCATION IN CLOSE PROXIMITY TO, BUT WHICH DOES NOT PHYSICALLY INTERFERE WITH, THE PROPOSED STORM DRAIN CONDUIT AND APPURTENANT STRUCTURES.

INDEX TO DRAWINGS

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MISCELLANEOUS DETAILS, STRUCTURAL NOTES	12

"AS BUILT" DWG.

1964 STORM DRAIN BOND ISSUE			LOS ANGELES COUNTY FLOOD CONTROL DISTRICT
REVISIONS		GENERAL NOTES, INDEX LOCATION MAP	
MARK	DATE	DESCRIPTION	
			REGIONAL PROJECT NO. II23
APPROVED BY: <i>Clyde L. Johnson</i> R.E. #379 CITY ENGINEER OF THE CITY OF COVINA DATE: 8-2-66		GENERAL NOTES, INDEX LOCATION MAP	
APPROVED BY: <i>R.E. Porter</i> R.E. #282 CITY ENGINEER OF THE CITY OF WEST COVINA DATE: Aug. 4, 1966		APPROVED BY: <i>Harold L. Johnson</i> R.E. #379 HAROLD L. JOHNSON ENGINEERING 841 W. GLENNTANA STREET, CALIF. DATE: 8-2-66	
APPROVAL RECOMMENDED BY: <i>William W. Ranson</i> ASST. CHIEF DEPUTY ENGINEER LOS ANGELES COUNTY FLOOD CONTROL DISTRICT		PLANS PREPARED BY: <i>R.E. Porter</i> R.E. #282 CITY ENGINEER OF THE CITY OF WEST COVINA DATE: Aug. 4, 1966	
DRAWN BY: <i>John G. Hall</i> TRACED BY: <i>John G. Hall</i> CHECKED BY: <i>John G. Hall</i> RECOMMENDED BY: <i>John G. Hall</i> APPROVED BY: <i>John G. Hall</i> DIVISION ENGINEER (Engineering)		DESIGNED BY: <i>John G. Hall</i> SUBMITTED BY: <i>John G. Hall</i> RECEIVED BY: <i>John G. Hall</i> SCALE: 1" = 600' NO. 364-II23-D2.1 AS SHOWN FEB. '67 SHEET 1 OF 12	

LIST OF STANDARD DRAWINGS
LOS ANGELES COUNTY FLOOD CONTROL DISTRICT

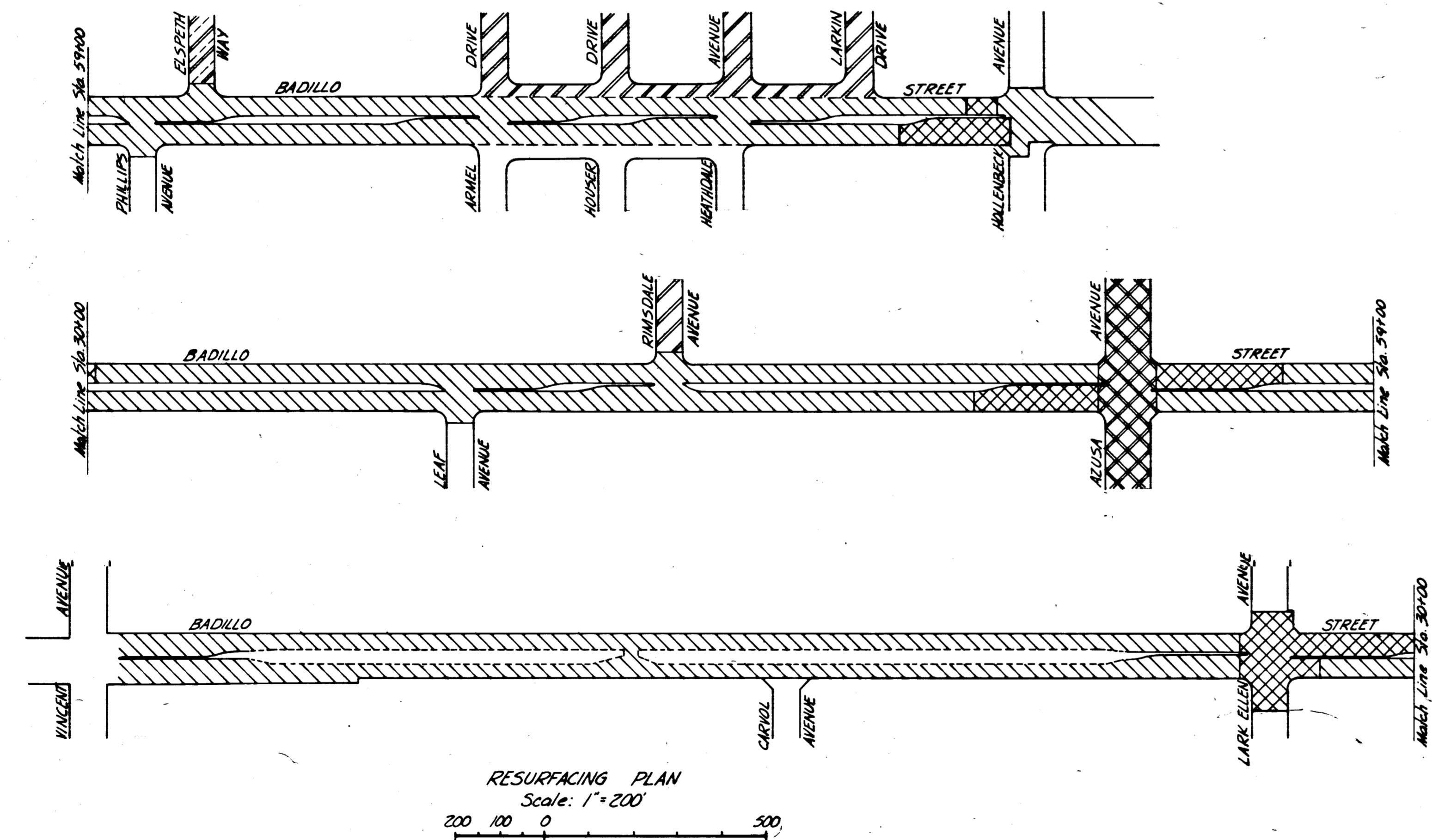
COUNTY SANITATION DISTRICTS OF LOS ANGELES COUNTY

DRAWING NO.	TITLE
2-D88	LOCAL DEPRESSION NO. 2
2-D96	STANDARD DROP STEP
2-DI04	MANHOLE NO. 3
2-DI07	CONCRETE RINGS, REDUCER, AND PIPE FOR MANHOLE SHAFT
2-DI12	JUNCTION STRUCTURE NO. 2
2-DI13	MANHOLE NO. 4
2-DI56	MANHOLE FRAME AND COVER FOR CATCH BASINS
2-DI57	CATCH BASIN REINFORCEMENT FOR ROUND MANHOLES
2-DI60	CATCH BASIN NO. 1
2-DI62	CATCH BASIN NO. 2
2-DI63	CATCH BASIN NO. 3
2-DI71	STANDARD A305 REINFORCING BARS
2-DI72	CATCH BASIN REINFORCEMENT
2-DI73.1, 2, 3	PIPE SUPPORTS ACROSS TRENCHES
2-DI75	REMOVABLE PROTECTION BAR FOR CATCH BASINS
2-DI77	PIPE BEDDING IN TRENCHES
2-DI81	STANDARD NON-ROCKING MANHOLE FRAME AND COVER
2-DI84	MANHOLE NO. 2
2-DI87	PAVEMENT REMOVAL, EXCAVATION, BACKFILL, AND RESURFACING IN STATE HIGHWAYS
2-DI88	TRANSITION STRUCTURE NO. 3
2-DI91	TRANSITION STRUCTURE NO. 3
2-DI93	JUNCTION STRUCTURE NO. 4
2-D213.1, 2	"D" LOAD TABLE FOR DESIGN OF REINFORCED CONCRETE PIPE
2-D224	CONNECTION TO CATCH BASIN FOR PIPES 12 INCHES THROUGH 72 INCHES
2-D232	DETAIL OF CATCH BASIN OPENING
2-D235	TRANSITION STRUCTURE NO. 1
2-D239	TRANSITION STRUCTURE NO. 2
2-D249.1, 2	CATCH BASIN NO. 8
2-D251	PROTECTION FOR MAINLINE AND HOUSE CONNECTION SEWERS
2-D264	ADJUSTABLE PROTECTION
2-D393	CONCRETE COLLAR
2-D399	CRITERIA FOR THE DESIGN OF SHORING FOR EXCAVATIONS
2-D400	SAMPLE SHEET FOR USE AS A GUIDE IN PREPARING CALCULATIONS FOR SHORING OF EXCAVATIONS
2-D415	LOCAL DEPRESSION NO. 4
2-D413	UNIFIED SOIL CLASSIFICATION SYSTEM

DRAWING NO. **G-b-48** TITLE **TEMPORARY SUPPORT**

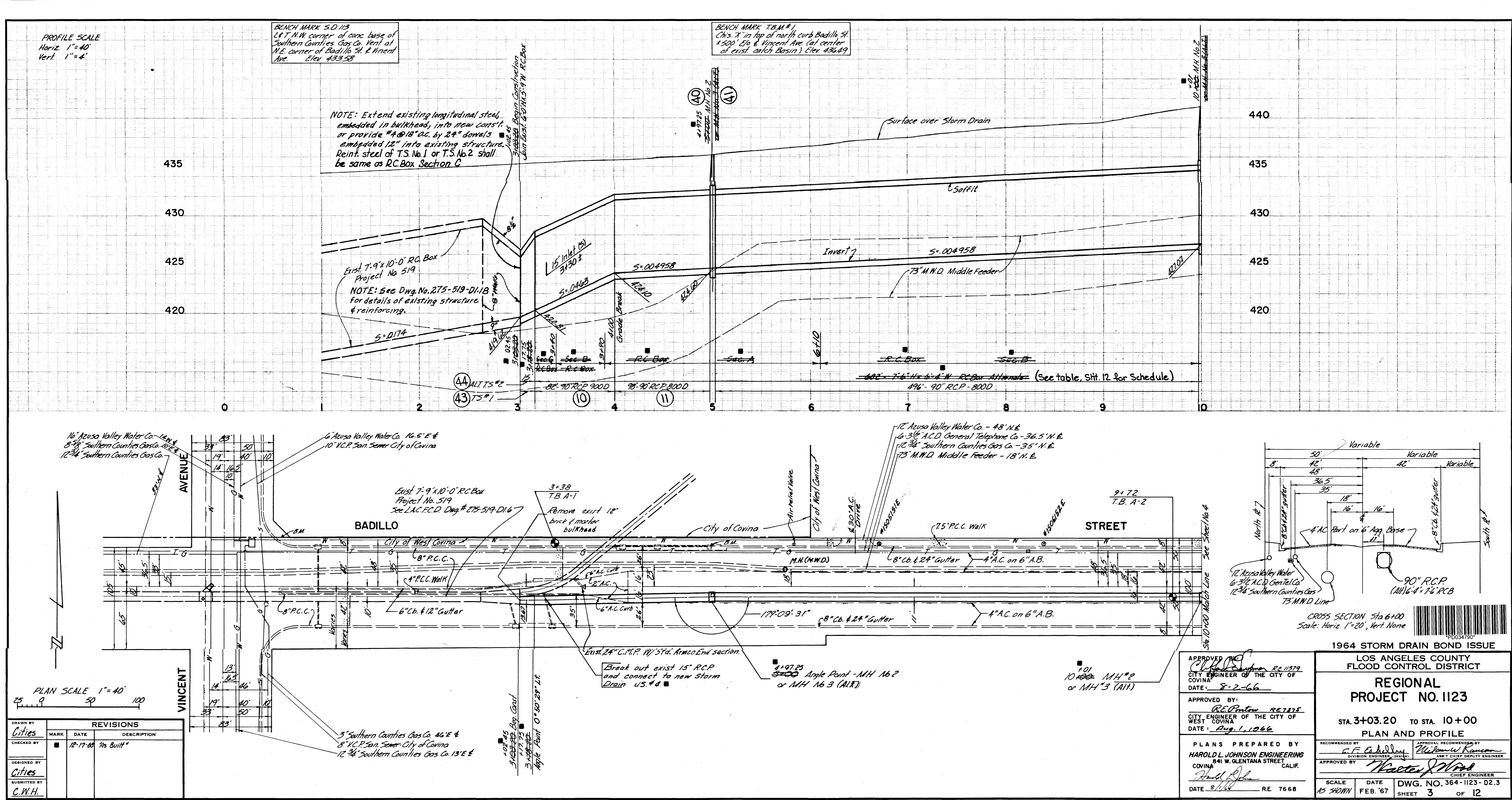
LEGEND

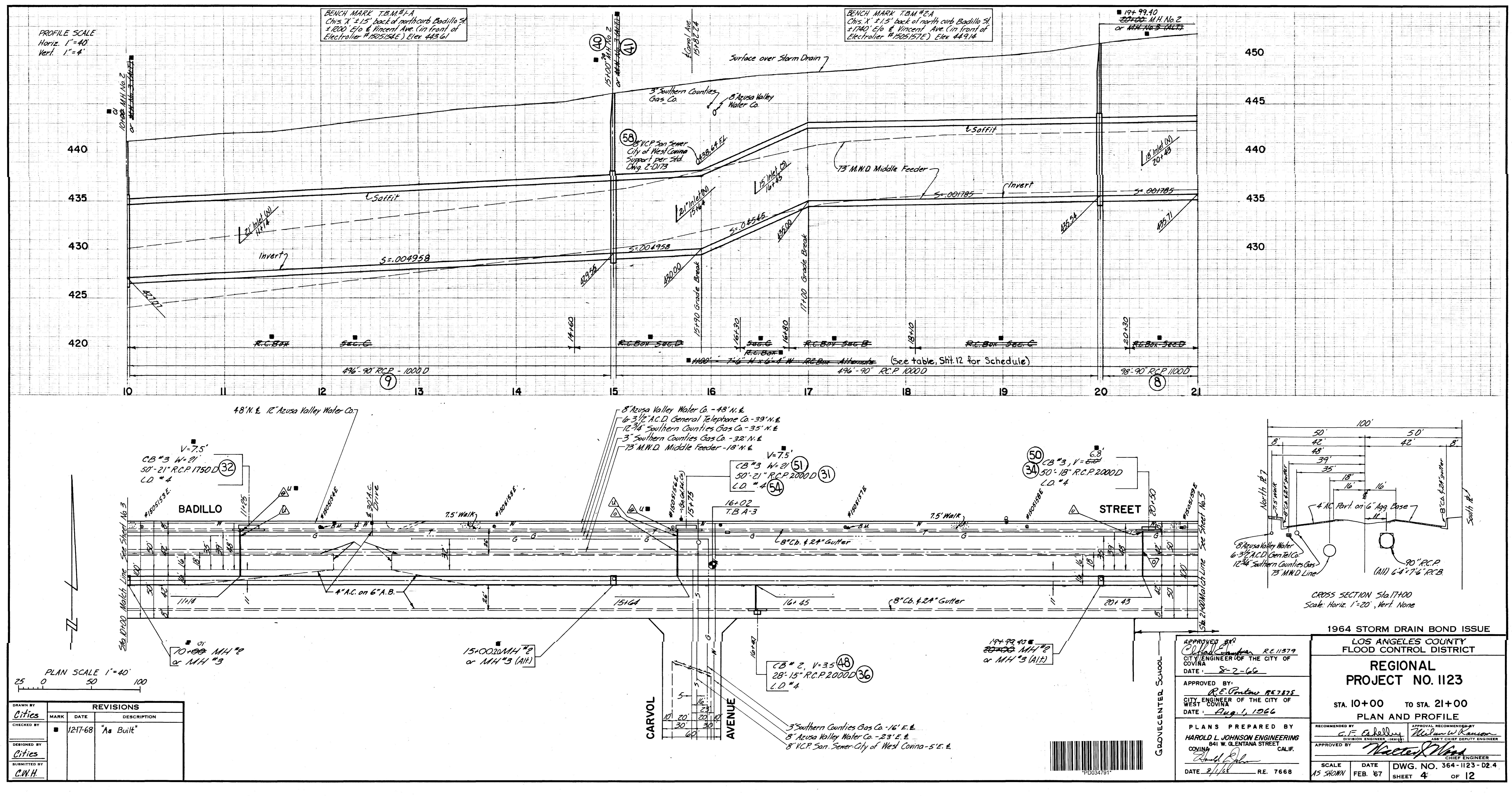
POWER POLE	_____
GUY ANCHOR	_____
TRAFFIC SIGN OR STREET SIGN	_____
FIRE HYDRANT	_____
SEWER MANHOLE	_____
WATER METER OR WEIR BOX	_____
GAS METER OR BOX	_____
TELEPHONE MANHOLE	_____
MAIL BOX	_____
WATER VALVE	_____
CONCRETE DRIVEWAY	_____
CURB & GUTTER	_____
ELECTROLIER OR TRAFFIC SIGNAL	_____
TRAFFIC SIGNAL BOX	_____
EDGE OF PAVEMENT	_____
TREE	_____
PROPERTY LINE	_____
PALM TREE	_____

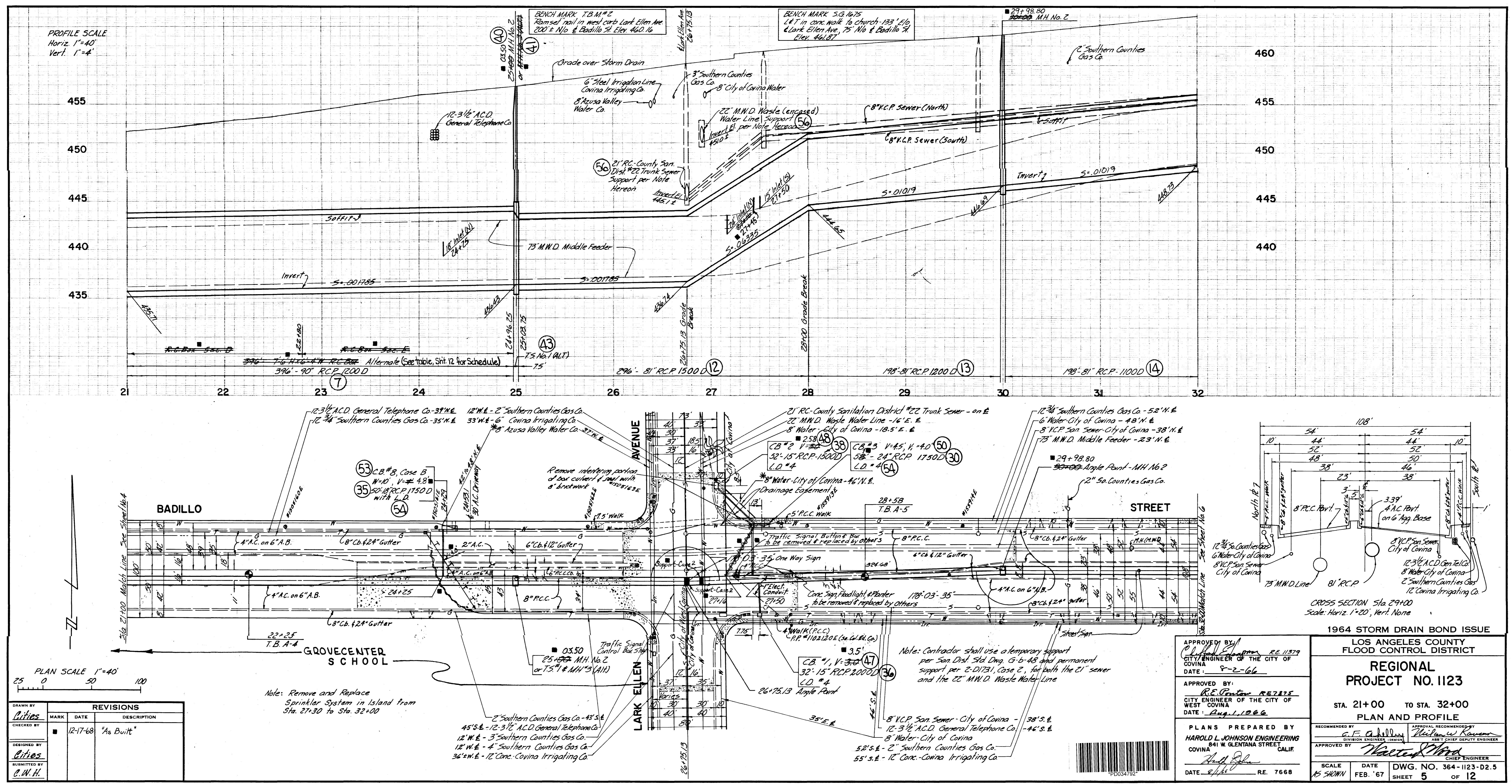


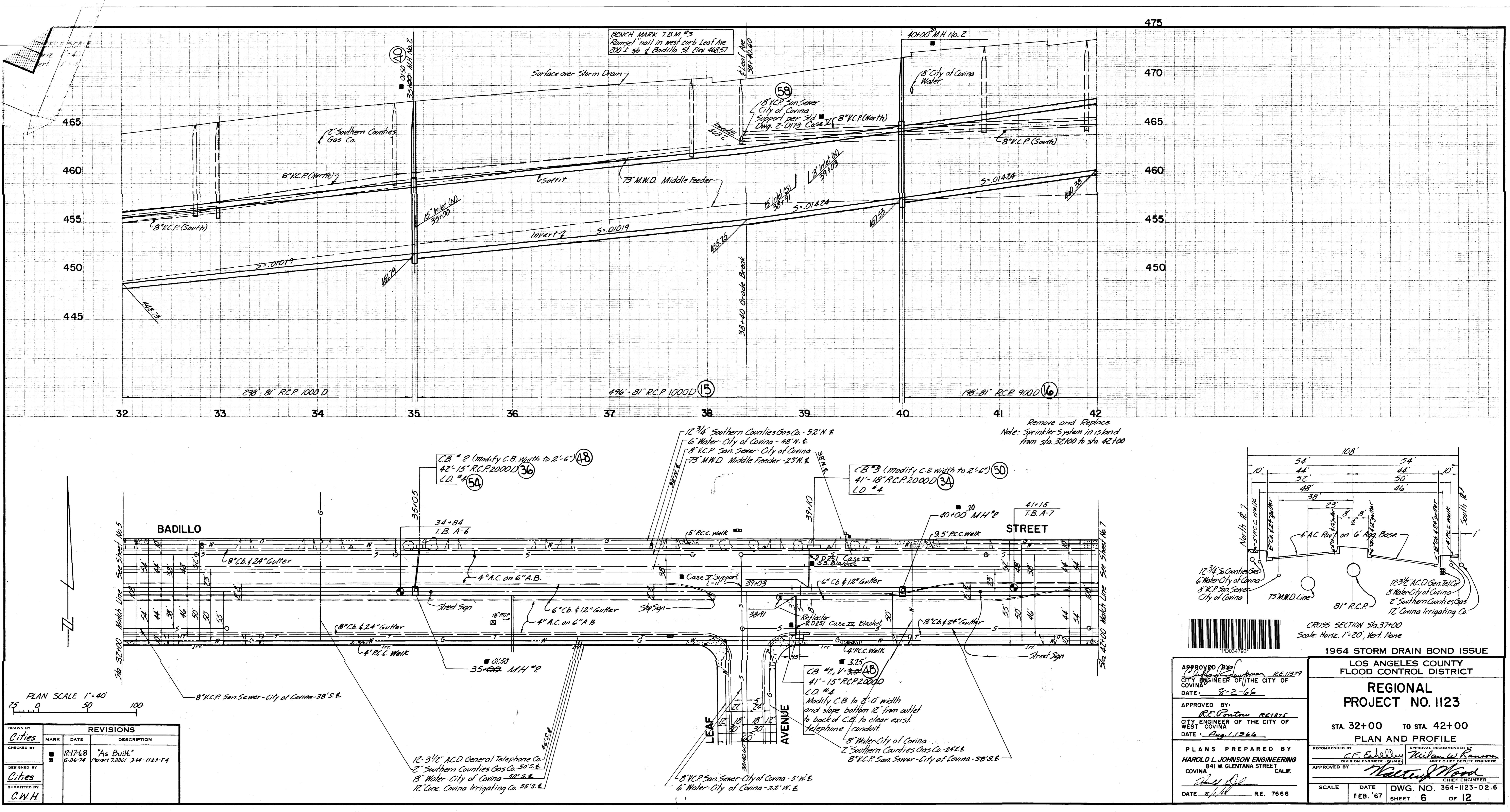
APPROVAL RECOMMENDED BY: <i>Milam W. Ranson</i> ASST. CHIEF DEPUTY ENGINEER LOS ANGELES COUNTY FLOOD CONTROL DISTRICT	APPROVED BY: <i>Clifford C. Anderson</i> CITY ENGINEER OF THE CITY OF COVINA DATE: 8-2-66
PLANS PREPARED BY: <i>R.E. Pontow</i> HAROLD L. JOHNSON ENGINEERING CITY ENGINEER OF THE CITY OF WEST COVINA DATE: Aug. 1, 1966	REVISIONS
DRAWN BY: <i>C. E. Johnson</i> TRACED BY: <i>C. E. Johnson</i> CHECKED BY: <i>C. E. Johnson</i> SUBMITTED BY: <i>C. E. Johnson</i> RECOMMENDED BY: <i>C. E. Johnson</i>	MARK DATE DESCRIPTION

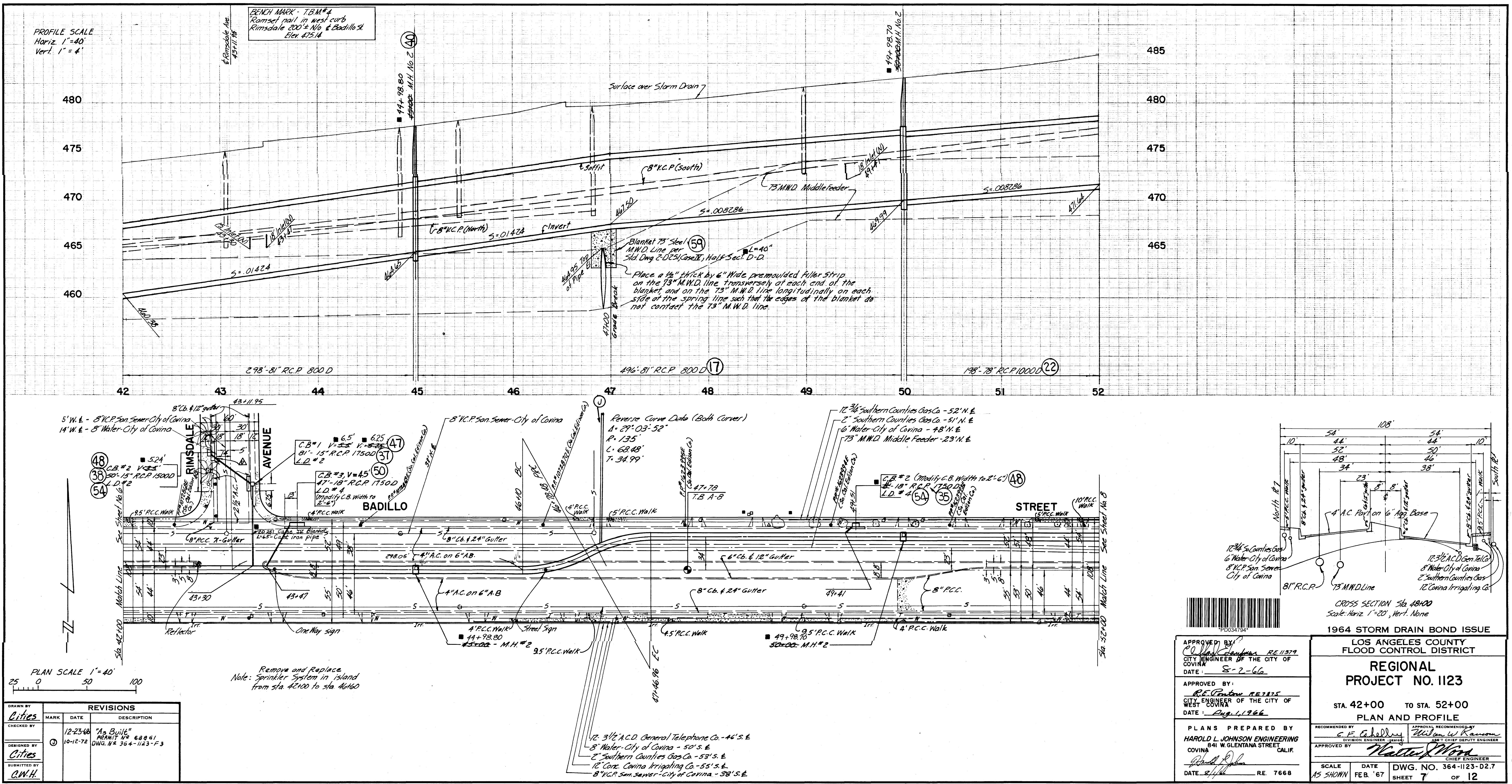
1964 STORM DRAIN BOND ISSUE		
LOS ANGELES COUNTY FLOOD CONTROL DISTRICT		
REGIONAL PROJECT NO. II23		
RESURFACING PLAN, LIST OF STANDARD DRAWINGS, LEGEND		
DRAWN BY: <i>C. E. Johnson</i> TRACED BY: <i>C. E. Johnson</i> CHECKED BY: <i>C. E. Johnson</i> SUBMITTED BY: <i>C. E. Johnson</i> RECOMMENDED BY: <i>C. E. Johnson</i>	REVISIONS	APPROVED BY: <i>Walter J. Schellberg</i> DIVISION ENGINEER
SCALE: AS SHOWN	DATE: FEB. '67	NO. 364-II23-D2.2
SHEET 2 of 12		

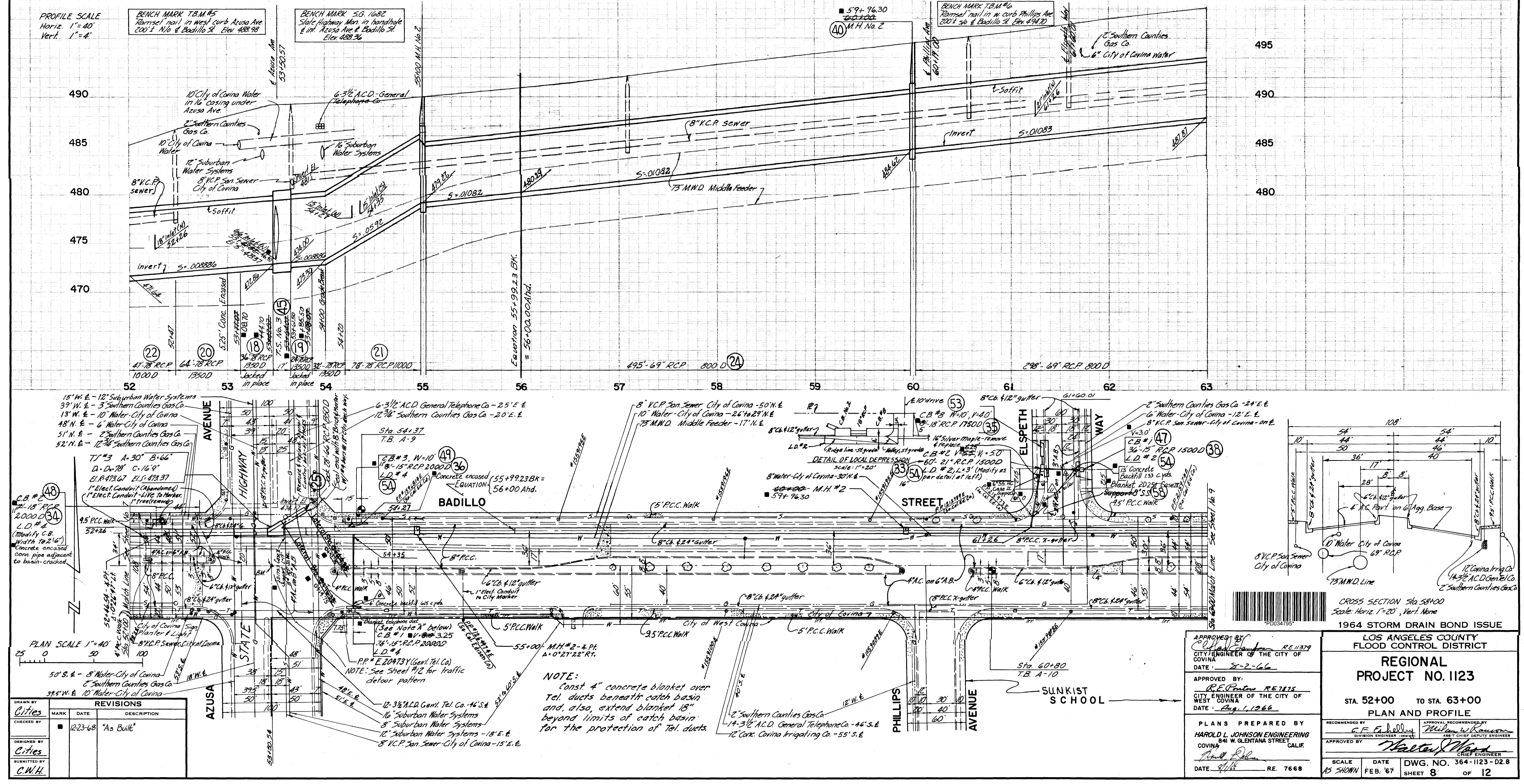


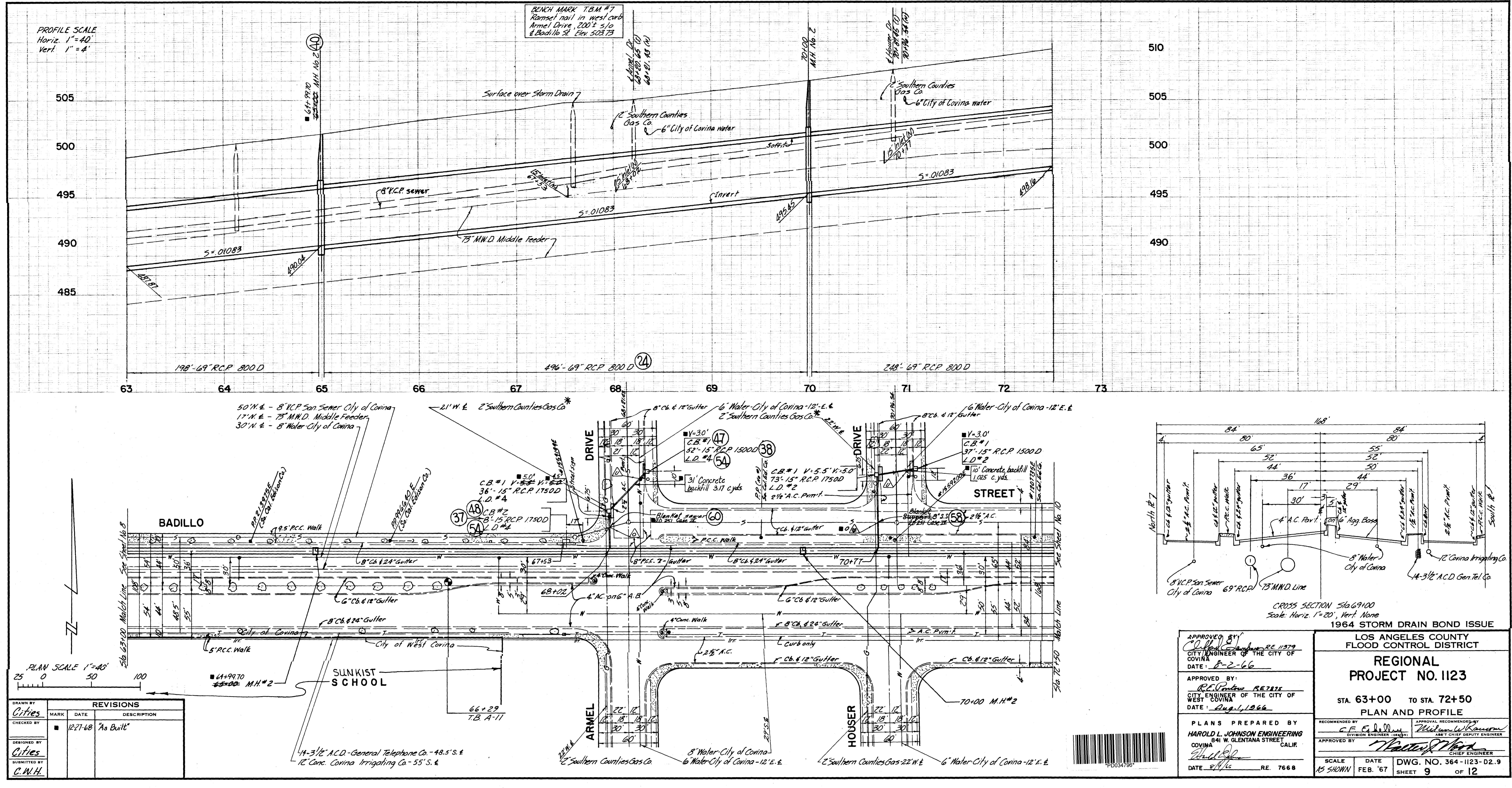


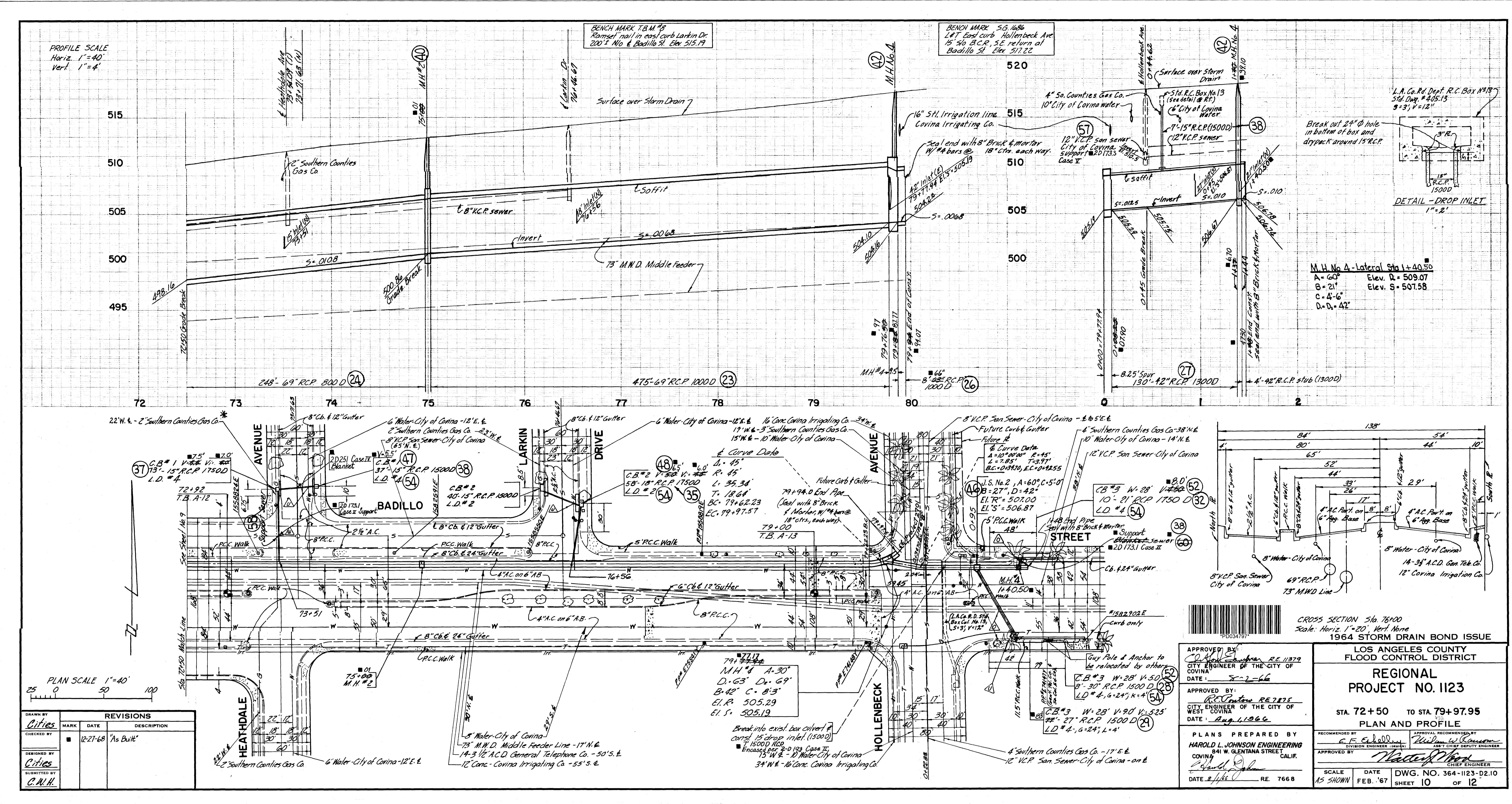












September 2019

PRELIMINARY
HYDROLOGY REPORT
For
Tentative Tract No. 82874
City of Covina
County of Los Angeles



HUNSAKER & ASSOCIATES IRVINE, INC.

PRELIMINARY HYDROLOGY REPORT
Tentative Tract No. 82874
City of Covina | County of Los Angeles



HUNSAKER
&
ASSOCIATES
IRVINE INC.

September
2019