# Miles Lane Development Traffic Impact Study City of Watsonville, CA 

TRAFFIC IMPACT STUDY

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## Prepared For:



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## EXECUTIVE SUMMARY

This study evaluates existing and future traffic conditions for the proposed Project located along Miles Lane, west of Freedom Boulevard, in the City of Watsonville, California. This analysis evaluates traffic conditions for both onsite and surrounding area intersections within the City of Watsonville (City).

## PROJECT DESCRIPTION

The Project proposes to construct 60 affordable housing units (plus one manager's unit), as well as an Encompass Community Center, which will include a 7,100 square foot Residential Treatment Facility and a 3,810 square foot Out-Patient Center.

The Project site is located along Miles Lane and will provide vehicular access along Miles Lane only. Existing uses on the site include single family residential and a Residential Treatment Facility. The development will accommodate on-site parking for 36 bicycle spaces and 125 passenger vehicle spaces (with the future option to increase to 156 vehicle spaces).

## ANALYSIS METHODOLOGY

Impacts associated with the Project were evaluated for the weekday AM and PM peak one-hour periods, consistent with accepted City guidelines and criteria. This analysis represents the peak Project trip generation as well as the busiest one hour at each study intersection during each morning and afternoon/evening peak period. Peak road network traffic in the study area was observed between 7:00am - 9:00am and between 4:00pm-6:00pm. The peak hour traffic analysis included in this report were conducted for the following analysis scenarios:

- Existing Conditions (2018) represents current traffic count data collected in December 2018 and existing roadway geometry and traffic control.
- Project Characteristics include descriptions of Project trip generation, distribution and assignment.
- Existing plus Project Conditions (2018) represents existing traffic count data and existing roadway geometry and traffic control plus the proposed Project.
- Near Term Conditions (2021) represents existing roadway geometry and traffic control plus trips associated with the near term (3 years) growth in the City of Watsonville.
- Near Term plus Project Conditions (2021) represents existing roadway geometry and traffic control plus trips associated with both the proposed Project and the near term (3 years) growth in the City of Watsonville.
- Cumulative Conditions (2040) represents build out of the City of Watsonville General Plan. Traffic volumes for 2040 were forecasted using the regional travel demand forecasting model developed by the Association of Monterey Bay Area Governments (AMBAG). This scenario addresses cumulative intersection and roadway operations on the future transportation network as discussed in the City of Watsonville General Plan.
- Cumulative plus Project Conditions (2040) represents the addition of Project trips to the Cumulative Conditions 2040 baseline traffic volumes and roadway network.


## STUDY INTERSECTIONS

The Project trip assignment was developed based on traffic patterns in the study area and knowledge of the study area. The study intersections below were selected based on the proposed trip assignment and in consultation with City of Watsonville Staff.

| $\#$ | Intersection |
| :--- | :--- |
| 1 | Freedom Boulevard \& Miles Lane |
| 2 | Santa Clara Street/Kimberly Lane \& Miles Lane |
| 3 | Santa Clara Street \& Marin Street |
| 4 | Auto Center Drive \& Marin Street |

## TRIP GENERATION ESTIMATES

The Project will generate approximately 36 AM peak hour, 45 PM peak hour, and 422 gross daily trips on average weekdays, based on Institute of Transportation Engineers (ITE) Trip Generation $10^{\text {th }}$ Edition data and methodologies. Consistent with standard City of Watsonville traffic engineering practices, the Project will receive an existing use trip credit, which includes the existing single-family homes and a Residential Treatment Facility. The resulting gross existing trips are approximately 9 AM peak hour, 7 PM peak hour, and 70 daily trips. Therefore, the traffic analysis is based on the Project generating a net of 27 new AM peak hour trips, 38 new PM peak hour trips, and 334 daily trips.

## PARKING ANALYSIS

City of Watsonville Municipal Code (June 2014) Chapter 14-17 Parking and Loading Facilities On-Site Circulation and Sight Distance Analysis. According to the City of Watsonville Municipal Code 125 spaces are required for the Project site. The Project will provide 125 spaces with a future option to increase to 156 spaces.

## SITE CIRCULATION

To access the Encompass Community Center, patients, visitors and employees are expected to use Driveway 1 along Miles Lane. To access the affordable housing, Driveways 2, 3, and 4 along Miles Lane will be utilized by residents, employees, and patrons. Volumes to the Project site are expected to be distributed among each of the Project driveways. No significant vehicle queues or delays are expected at the Project driveways due to low peak hour volumes.

## SIGHT DISTANCE ANALYSIS AT AUTO CENTER DRIVE \& MARIN STREET

At the intersection of Auto Center Drive and Marin Street, stopping sight distance and intersection sight distance were analyzed using the American Association of State Highway Transportation Officials (AASHTO) methodology. It was determined that the existing stopping sight distance and intersection was inadequate in existing conditions.

The following mitigations are recommended for the intersection of Auto Center Drive and Marin Street to improve sight distance.

- Auto Center Drive South of Marin Street
- Provide approximately 280 feet of Striping Detail 22 (Centerline)
- Provide approximately 350 feet of Striping Detail 27B (Right Edgeline) and create a painted bulb-out for vehicles entering from Auto Center Drive. Within the painted bulb-out, add 6" diagonal white striping with 15 ' spacing. The right edgeline striping would move the center of the road away from the curb allowing for better visibility.
- Provide "Intersection Ahead" signage (W1-10e) with "Speed Sign" (W13-1P) with 20 mph speed and a custom "Limited Sight Distance" sign. Place at point of curvature for Northbound approach according to MUCTD Table 2C-4. This sign would warn drivers of the approaching intersection to be aware of cross traffic and to reduce speed.
- Marin Street
- Move the 12 inch stop bar closer to the curb line along with new "STOP" markings. This will allow drivers to pull up further into the new 8 -foot parking lane to increase visibility along Auto Center Drive.
- Provide approximately 75 feet of Striping Detail 22 (Centerline) to shift the westbound intersection approach to the north. This would allow for more visibility on the Auto Center Drive northbound approach.
- Extend red curb on the south curb approximately 85 feet. This red curb would remove approximately three on-street parking spaces. This would prevent drivers from parking in the painted bulb-out.
- Extend red curb on the north curb approximately 30 feet. This red curb would remove approximately one on-street parking space to allow more space for drivers to approach the intersection.
- Auto Center Drive North of Marin Street
- Extend red curb approximately 120 feet on the east curb and provide "No Parking Anytime" signage. This would remove approximately five (5) on-street parking spaces. Red curb would make parking illegal along the eastern curb allowing southbound sight distance to be unobstructed.
- Provide "Intersection Ahead" signage (W1-10e) with "Speed Sign" (W13-1P) with 20 mph speed and a custom "Limited Sight Distance" sign. Place at point of curvature for southbound approach according to MUCTD Table 2C-4. This sign would warn drivers of the approaching intersection to be aware of cross traffic and to reduce speed.
- Provide speed feedback sign similar to existing signage on east side of Auto Center Drive. Place at point of curvature for southbound approach according to MUCTD Table 2C-4.
- Provide approximately 200 feet of Striping Detail 22 (Centerline) and Striping Detail 27B (Right Edgeline) for the Northbound approach. Right edgeline striping would be 8-feet from the curb. This striping would reduce confusion for vehicles traveling northbound.
- Provide approximately 490 feet of Striping Detail 27B (Right Edgeline) for the Southbound approach. This striping would move the center of the road away from the curb allowing for better visibility.

With these mitigations, it was determined that both stopping sight distance and intersection sight distance would improve and would be compliant with AASHTO standards.

## IMPACTS AND MITIGATIONS MEASURES

## MITIGATIONS

Based on the analysis completed in this report, no mitigations are required for the study intersections. All intersections in each scenario will perform at a Level of Service (LOS) D or better with and without the Project.

Mitigations to improve sight distance at the intersection of Auto Center Drive and Marin Street are described in the previous section.

TRAFFIC IMPACT FEES
Based on City of Watsonville Development Summary Fees (2017-2018) the total traffic impact fee for the proposed Project would be approximately $\mathbf{\$ 1 0 9 , 5 2 0}$.

### 1.0 INTRODUCTION

This study evaluates existing and future traffic for the proposed Project and assesses the potential traffic impacts on the City of Watsonville road network. The analysis evaluates on-site and off-site traffic conditions in the Project vicinity.

The Project proposes to construct 60 affordable housing units (plus one manager's unit), as well as an Encompass Community Center, which will include a 7,100 square foot Residential Treatment Facility and a 3,810 square foot Out-Patient Center.

Primary access for the affordable housing and Encompass Community Center would be provided off Miles Lane. A total of four (4) driveways are proposed along Miles Lane and. The development will accommodate on-site parking for 36 bicycle spaces and 125 passenger vehicle spaces. Figure 1 illustrates the location of the Project site in relation to other streets in the City of Watsonville with the existing road network. Figure 2 shows the Project site plan.

### 1.1 STUDY METHODOLOGY

## DEVELOPMENT CONDITIONS

This traffic impact study is based upon the following development conditions:

- Existing Conditions (2018) represents current traffic count data collected in December 2018 and existing roadway geometry and traffic control.
- Project Characteristics include descriptions of Project trip generation, distribution and assignment.
- Existing plus Project Conditions (2018) represents existing traffic count data and existing roadway geometry and traffic control plus the proposed Project.
- Near Term Conditions (2021) represents existing roadway geometry and traffic control plus trips associated with the near term (3 years) growth in the City of Watsonville.
- Near Term plus Project Conditions (2021) represents existing roadway geometry and traffic control plus trips associated with both the proposed Project and the near term (3 years) growth in the City of Watsonville.
- Cumulative Conditions (2040) represents build out of the City of Watsonville General Plan. Traffic volumes for 2040 were forecasted using the regional travel demand forecasting model developed by the Association of Monterey Bay Area Governments (AMBAG). This scenario addresses cumulative intersection and roadway operations on the future transportation network as discussed in the City of Watsonville General Plan.
- Cumulative plus Project Conditions (2040) represents the addition of Project trips to the Cumulative Conditions 2040 baseline traffic volumes and roadway network.


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## OPERATING CONDITIONS AND CRITERIA FOR INTERSECTIONS

Analysis of potential environmental impacts at intersections is based on the concept of Level of Service (LOS). The LOS of an intersection is a qualitative measure used to describe operational conditions. LOS ranges from A (best), which represents minimal delay, to F (worst), which represents heavy delay and a facility that is operating at or near its functional capacity. Levels of Service for this study were determined using methods defined in the Highway Capacity Manual, 2010 (HCM) and Synchro traffic analysis software.

The HCM 2010 methodologies include procedures for analyzing side-street stop-controlled (SSSC), all-way stop-controlled (AWSC), and signalized intersections. The SSSC procedure defines LOS as a function of average control delay for each minor street approach movement. Conversely, the AWSC and signalized intersection procedures define LOS as a function of average control delay for the intersection. Table 1 relates the operational characteristics associated with each LOS category for signalized and unsignalized intersections.

Table 1 - Intersection Level of Service Definitions

| Level of <br> Service | Description | Signalized | Unsignalized <br> (Avg. control <br> delay per vehicle- <br> sec/vet.) |
| :---: | :---: | :---: | :---: |
| AAvg. control delay <br> per vehicle- <br> sec/veh.) |  |  |  |
| B | Free flow with no delays. Users are virtually <br> unaffected by others in the traffic stream | $<10$ | $>10-20$ |

Sources: Transportation Research Board, Highway Capacity Manual 2010, National Research Council,

Project impacts are determined by comparing conditions without the proposed Project to those with the proposed Project. Significant impacts for intersections are created when traffic from the proposed Project causes the LOS to fall below the City LOS threshold and causes any impacted intersections to deteriorate further. Significant impact criteria are discussed further in Section 2 of this report.

### 1.2 STUDY INTERSECTIONS INCLUDED IN ANALYSIS

The proposed Project will generate new vehicular trips that will increase traffic volumes on the City street network. To assess changes in traffic conditions associated with the proposed Project, the following intersections, listed with the existing control type, were selected based on City criteria for evaluation in this traffic study:

1. Freedom Boulevard \& Miles Lane (Side Street Stop Control)
2. Santa Clara Street/Kimberly Lane \& Miles Lane (All Way Stop Control)
3. Santa Clara Street \& Marin Street (All Way Stop Control)
4. Auto Center Drive \& Marin Street (Side Street Stop Control)

The Project will also construct four (4) driveways that will generate a relatively low number of trips. Therefore, the driveway operations are evaluated qualitatively in this study.

### 2.0 THRESHOLDS OF SIGNIFICANCE

Significance criteria are used to identify Project impacts. Currently, the City specifies LOS thresholds that are utilized for roadways and intersection under their respective jurisdictions. The following significance criteria were used for this TIA and are consistent with the thresholds from the 2030 General Plan Update, and Appendix $G$ of the CEQA Guidelines. Accordingly, the Project would have a significant traffic impact if any of the criteria discussed in the following sections are met.

### 2.1 LEVEL OF SERVICE STANDARDS

Per the Watsonville Vista 2030 General Plan, the City has established LOS D as the minimum acceptable LOS for overall intersection operations (Chapter 10 Transportation and Circulation - Level of Service (LOS)). However, there are certain locations where this standard does not apply. The following provides a list and description of exceptions to the LOS D standard:

- Unsignalized intersections where peak hour operations may exceed LOS D, but a traffic signal is not warranted. Unsignalized intersections that operate worse than LOS D should be evaluated for feasible improvements to improve operations.
- Roadway segments and signalized intersections identified to operate at less than LOS D in the 2005-2030 Major Streets Master Plan (MSMP). The MSMP evaluates the City's current and proposed roadway system under the proposed general plan's land use Projections to determine compliance with level of service standards. There are no intersections within the Project study area identified as operating worse than LOS D in the MSMP.


### 3.0 EXISTING CONDITIONS (2018)

### 3.1 EXISTING (2018) INTERSECTION AND ROADWAY NETWORK

To determine potential significant impacts related to the proposed Project, existing intersections were selected for analysis based on trip assignment and discussion with City Staff. All intersections were analyzed for weekday AM and PM peak periods, which are the peak periods during which the Project will generate the most trips onto the City road network. Figure 3 shows the location of existing study intersections within the Project area as well as the lane configurations.

Weekday intersection turning movement volumes were collected on Tuesday December 18, 2019. Volumes for the intersections were collected during the AM and PM peak periods of 7:00am-9:00am and 4:00pm6:00pm, respectively. These traffic counts were collected when local schools were in session and the weather was fair. Existing turning movements are shown in Figure 4. Intersection volume data sheets for all traffic counts are provided in Appendix A.

## EXISTING STUDY NETWORK

## Local Roadways

The following local roadways provide access to the site:

- Freedom Boulevard is a major arterial roadway that spans 9.5 miles from Highway 1 to State Route 152 / Main Street in the City of Watsonville. It provides local and regional access to downtown businesses and residences. The facility consists of two-lanes from Highway 1 to Buena Vista Drive, four lanes from Buena Vista Drive to Lincoln Street, and two lanes from Lincoln Street to State Route 152 / Main Street. The speed limit varies along Freedom Boulevard with a posted speed limit of 40 from State Route 1 to Buena Vista and a posted speed limit of 35 from Buena Vista to State Route 152 / Main Street.
- Auto Center Drive \& Arthur Road is an undivided two-lane collector street that provides access to local businesses and residences as well as Cesar E. Chavez Middle School and various car dealerships west of Marin Street. Auto Center Drive spans 0.4 miles from State Route 152 / Main Street to San Benito Street while Arthur Road spans 0.7 miles from San Benito Street to Freedom Boulevard. The speed limit along Auto Center Drive and Arthur Road is 25 miles per hour and on street parking is allowed.
- Miles Lane is a two-lane undivided collector street that would provide direct access to the Project site. The facility spans 0.2 miles from Freedom Boulevard to Santa Clara Street and provides access to residences. The posted speed limit is 25 miles per hour and on street parking is allowed. Vehicles wanting to access Freedom Boulevard from Miles Lane are restricted to a right turn only.
- Marin Street is a two-lane collector street that spans 0.4 miles from Auto Center Drive to Freedom Boulevard and provides access to residences. The posted speed limit is 25 miles per hour and on street parking is allowed. Vehicles wanting to access Freedom Boulevard would use Marin Street to make either a right or left turn.
- Santa Clara Street is a local two-lane undivided road that spans 0.5 miles from Arthur Road to Miles Lane. Santa Clara Street provides access to residences and Hyde Elementary School. The posted speed limit is 25 miles per hour and on street parking is allowed.






## LEGEND




### 3.2 EXISTING (2018) CONDITIONS LEVEL OF SERVICE

Traffic operations were evaluated at the study intersections under existing traffic conditions. Results of the analysis are presented in Table 2. As shown in Table 2, all study intersections are currently operating at LOS D or better during the AM and PM peak hour. Synchro analysis sheets are provided in the Appendix.

Table 2 - Existing Conditions Level of Service

| \# | Intersection | LOS <br> Standard | Control Type | Existing Conditions |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | AM Peak Hour |  |  | PM Peak Hour |  |  |
|  |  |  |  | Movement | Delay | LOS | Movement | Delay | LOS |
| 1 | Freedom Boulevard \& Miles Lane | D | SSSC | Overall | 2.4 | A | Overall | 3.1 | A |
|  |  |  | Worst Approach | EB | 11.0 | B | EB | 12.2 | B |
| 2 | Santa Clara Street \& Miles Lane | D | AWSC | Overall | 7.1 | A | Overall | 7.3 | A |
| 3 | Santa Clara Street \& Marin Street | D | AWSC | Overall | 10.7 | B | Overall | 9.2 | A |
| 4 | Auto Center Drive \& Marin Street | D | SSSC | Overall | 6.2 | A | Overall | 3.9 | A |
|  |  |  | Worst Approach | WB | 22.8 | C | WB | 16.9 | C |

Notes:

1. Analysis performed using HCM 2010 methodologies.
2. Delay indicated in seconds/vehicle.
3. Overall level of service (LOS) standard for the City is D.
4. Intersections that fall below City standard are shown in bold.

### 3.3 EXISTING (2018) PEDESTRIAN AND BICYCLE NETWORK

## BICYCLES

A map of the existing City of Watsonville bicycle network can be found in Figure 3-14, Existing and Proposed Bicycle Network in the City of Watsonville Trails and Bicycle Master Plan from November 2012. The map is included in the Appendix of this report. Existing Class I, II, \& III bikeway facilities (within $1 / 2$ mile from the Project site) are discussed below:

Class I facilities are paved bicycle paths that are physically separated from the vehicular travel lane. A Class I bike lane is provided along the south side of Main Street from Pennsylvania Drive to Main Street/Freedom Blvd and can be accessed from Auto Center Drive. To access the Class I bike lane, a bicyclist would expect to travel approximately 3,500 feet from the project site and would use Miles Lane, Santa Clara Street, Marin Street, and Auto Center Drive.

Class II facilities, which are striped bike lanes along the street, are generally found along the eastern portion of the existing urbanized area of the City. There are Class II bike lanes along Freedom Boulevard just south of Miles Lane. To access the Class II bike lane, a bicyclist would expect to travel approximately 550 feet from the project site and would use Miles Lane.

Class III bicycle facilities are bike routes denoted by signs that are shared with vehicles along the roadway. Class III bicycle facilities in the Project vicinity are located along Freedom Boulevard north and south of Miles Lane and on Auto Center Drive/Arthur Road. To access the Class III bike lanes, a bicyclist would
expect to travel approximately 2,400 feet to access Freedom Blvd and approximately 1,900 feet to access Auto Center Drive/Arthur Road. Both routes would use Miles Lanes, Santa Clara Street, and Marin Street.

## PEDESTRIANS

Existing pedestrian facilities in the study area include sidewalks along both sides of Freedom Boulevard, Miles Lane, Santa Clara Street, Marin Street, and Auto Center Drive.

There are no existing crosswalks at the intersections of Freedom Boulevard and Miles Lane, Santa Clara Street and Miles Lane, and Auto Center Drive and Marin Street. There are existing crosswalks at the intersection of Santa Clara Street and Marin Street along the west, south, and east legs.

### 3.4 EXISTING (2018) TRANSIT NETWORK

The Santa Cruz Metropolitan Transit District (SCMTD) and Monterey Salinas Transit (MST) public bus system provides local and regional connectivity to residents of the City of Watsonville. These services all route through the Watsonville Transit Center located in downtown Watsonville at the Rodriguez Street and West Lake Avenue intersection which serves as a transit hub for the county of Santa Cruz.

## SANTA CRUZ METRO BUS FIXED-ROUTE BUS SERVICE

The Santa Cruz METRO routes several bus lines through the City of Watsonville and has an existing bus stop approximately 800 feet from the Project site just south of the intersection Freedom Boulevard and Miles Lane. This bus stop only serves passengers traveling to downtown Watsonville. Residents, employees, and patrons wishing to travel to Santa Cruz may experience difficulties because there are few crosswalks along Freedom Boulevard. The nearest crosswalks on Freedom Boulevard are approximately 1,950 feet to the south and 990 feet to the north. In addition, the bus stops are far away from the crosswalks for a total distance of 2,700 feet to the south 2,300 feet to the north.

Local and regional bus services that travel near the Project include the following:

- Route 71 is a regional route connecting Santa Cruz, Capitola, and Watsonville. It runs along Soquel Avenue and Freedom Boulevard and serves major destinations including the Santa Cruz and Watsonville Transit Centers and Cabrillo College. Route 71 operates on two schedules an outbound schedule (Santa Cruz to Watsonville) and an inbound schedule (Watsonville to Santa Cruz) each with a weekday and weekend schedule. Route 71 operates between 5:30am-12:00am during the weekday and weekend. The weekday and weekend schedules operate on intervals of a half an hour.
- Route 79 is a local loop that services Downtown Watsonville. It runs on East Lake Avenue, Freedom Boulevard, and East Beach Street within Watsonville and serves major destinations including East Lake Village Shopping Center, the Watsonville Transit Center, and Lake Tynan. Route 79 operates between 7:25 AM and 6:10 PM with 60-minute intervals on weekdays. On weekends, Route 79 operates between 8:30 AM and 5:15 PM with four (4) hour intervals.
- Route 69A is a regional route connecting Santa Cruz, Capitola, and Watsonville. It runs along Soquel Avenue, Capitola Road, Highway 1, Airport Boulevard, Freedom Boulevard, and Lincoln Street and serves major destinations including the Santa Cruz and Watsonville Transit Centers and Cabrillo College. Route 69A operates on two schedules an outbound schedule (Santa Cruz to

Watsonville) and an inbound schedule (Watsonville to Santa Cruz). Route 69A operates between 7:00am-6:00pm on the weekdays and 8:00am-7:00pm on the weekends. The weekday schedule operates on one (1) hour intervals, while the weekend schedule operates on half hour intervals.

## MST FIXED-ROUTE BUS SERVICE

The MST operates three regional bus lines (Route 27, 28, and 29) that connect the City of Marina and Salinas with Watsonville. These routes services major destinations including Castroville, Moss Landing, Pajaro, Prunedale, Los Lomas, and the Watsonville Transit Center. The MST routes operate daily with varying time intervals. Connection to the Watsonville Transit Center is via Route 71 and Route 79 services.

### 4.0 PROPOSED PROJECT

### 4.1 PROJECT SITE PLAN

The Project proposes to construct 60 affordable housing units (plus one manager's unit) as well as an Encompass Community Center, which will include a 7,100 square foot Residential Treatment Facility and a 3,810 square foot Out-Patient Center.

The affordable housing and Encompass Community Center would be accessed along the four (4) driveways on Miles Lane. Access to Freedom Boulevard is provided from Miles Lane approximately 550 feet to the east; however, this access point only accommodates right in right out movements. If residents, employees, or patrons wish to travel north on Freedom Boulevard, they must either travel north on Auto Center Drive or north on Santa Clara Street.

The development will accommodate on-site parking for 36 bicycle spaces and 125 passenger vehicle spaces. An overview of the proposed Project site is illustrated in Figure 2.

### 4.2 PROJECT TRIP GENERATION

Trip generation for the Project was calculated using the land use rates from the Institute of Transportation Engineer's (ITE) publication Trip Generation 10th Edition (2017), which is a standard reference used by jurisdictions throughout the country for the estimation of trip generation. A trip is defined in Trip Generation as a single or one-directional vehicle movement with either the origin or destination at the Project site. In other words, a trip can be either "to" or "from" the site. In addition, a single customer visit to a site is counted as two trips (i.e., one to and one from the site).

To determine existing trip credits, the existing land uses were categorized under the following ITE land uses:

- 4 Single Family Residential Dwelling Units - Single Family Detached Housing (Land Use 210)
- 3,442 square foot Residential Treatment Facility - Assisted Living (Land Use 254)

In existing conditions, there are a total of five (5) dwelling units; however, one dwelling unit is currently vacant due to structural deficiencies and is conservatively not assumed for existing trip credits. A small workshop also currently exists on the Project site that is used for storage. It is conservatively assumed that this storage unit does not generate any existing trips (i.e. no existing trip credits are assumed for the storage unit).

To determine Project trips, the Project land uses were categorized under the following ITE land uses based on the Project description and discussions with the developer/future tenant:

- 60 Multifamily Housing Dwelling Units (plus one manager's unit) - Multi-Family Housing (Mid Rise) (Land Use Code 221)
- 7,100 square foot Residential Treatment Facility - Assisted Living (Land Use 254)
- 3,810 square foot Out-Patient Center - Medical Office Building (Land Use 720)

The Project proposes to construct one manager's unit in addition to the 60 proposed affordable housing units. It is assumed that the manager's unit will generate trips throughout the day similar to other multifamily housing units. Furthermore, it is assumed that the property manager will not travel via motor vehicle during the AM or PM peak hours since the manager will already be onsite for work and will not need to commute.

ITE land uses for the Encompass Community Center facility were selected based on the Project description and discussions with the developer. Based on these details, ITE land use 254 (Assisted Living) and ITE land use 720 (Medical Office Building) were selected for analysis and trip generation estimation due to their similarities to the proposed uses. The following describes potential ITE land uses that were also considered:

## Residential Treatment Facility:

- Assisted Living (Land Use 254): ITE defines this land use as "typically includes dining, housekeeping, social and physical activities, medication administration, and transportation". Furthermore, ITE states "assisted care commonly bridges the gap between independent living and nursing homes and in some areas of the country, assisted living residences may be called personal care, residential care, or domiciliary care". Additionally, "staff may be provided 24-hours per day". This ITE land use description is consistent with the Project description provided by the developer/future tenant. Therefore, the ITE Assisted Living (254) land use was SELECTED FOR ANALYSIS.
- Nursing Home (Land Use 620) and Congregate Care (Land Use 253) were not selected based on the project description and activities related to these uses.


## Out-Patient Center:

- Medical Office Building (Land Use 720): ITE defines this land use as "a facility that provides diagnoses and outpatient care services on a routine basis but is unable to provide prolonged inhouse medical and surgical care." This ITE land use description is consistent with the Project description provided by the developer/future tenant. Therefore, the ITE Medical Office Building (720) land use was SELECTED FOR ANALYSIS.
- Clinic (Land Use 630) was not selected since no pharmacy or medical lab facilities will be provided on the site.

Table 3 shows trips generated by the proposed development based on the previously discussed methodology. For the baseline scenario, the existing site generates 70 daily, 9 AM peak hour trips ( $3 \mathrm{IN} / 6$ OUT), and 7 PM peak hour trips ( $4 \mathrm{IN} / 3$ OUT). Development of the proposed Project is anticipated to generate 422 daily, 36 AM peak hour trips ( $16 \mathrm{IN} / 20$ OUT), and 45 PM peak hour trips ( $22 \mathrm{IN} / 23$ OUT). As illustrated in Table 3, the proposed Project is anticipated to add a net total of 334 daily, 27 AM peak hour trips ( $13 \mathrm{IN} / 14$ OUT), and 38 PM peak hour trips ( $18 \mathrm{IN} / 20$ OUT) to the roadway network.

An existing bus stop is located approximately 800 feet from the Project Site. It is anticipated that some Project trips could use this transit mode; however, this analysis conservatively does not take any trip reductions for transit uses. The trip reduction for the bus service is approximately 1 AM peak hour trip and 1 PM peak hour trip. For more information on how these trips were determined refer to Section 7.3 Transit Mobility.

Table 3 - Project Trip Generation

| Land Use | ITE <br> Land <br> Use <br> Code | Size | Unit | Daily |  | AM Peak Hour |  |  |  | PM Peak Hour |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Rate | Trips | Rate | In | Out | Total | Rate | In | Out | Total |
| Existing Conditions |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Single-Family Detached Housing ${ }^{1}$ | 210 | 4 | DU | 13.50 | 54 | 2.00 | 2 | 6 | 8 | 1.25 | 3 | 2 | 5 |
| Assisted Living ${ }^{2}$ | 254 | 3.442 | 1,000 SQFT | 4.19 | 16 | 0.39 | 1 | 0 | 1 | 0.48 | 1 | 1 | 2 |
| Total Existing Trip Credit |  |  |  |  | 70 |  | 3 | 6 | 9 |  | 4 | 3 | 7 |
| Proposed Project |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Multifamily Housing (Mid-Rise) ${ }^{3}$ | 221 | 60 | DU | 5.43 | 326 | 0.35 | 5 | 16 | 21 | 0.45 | 17 | 10 | 27 |
| Multifamily Housing (Mid-Rise) ${ }^{6}$ | 221 | 1 | DU | 5.43 | 6 | 0.00 | 0 | 0 | 0 | 0.00 | 0 | 0 | 0 |
| Assisted Living ${ }^{4}$ | 254 | 7.100 | 1,000 SQFT | 4.19 | 30 | 0.39 | 2 | 1 | 3 | 0.48 | 1 | 2 | 3 |
| Medical Office Building ${ }^{5}$ | 720 | 3.810 | 1,000 SQFT | 15.40 | 60 | 3.19 | 9 | 3 | 12 | 3.98 | 4 | 11 | 15 |
| Total Proposed Gross Trips |  |  |  |  | 422 |  | 16 | 20 | 36 |  | 22 | 23 | 45 |
| Proposed Net New Project Trips |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Total Existing Trip Credit |  |  |  |  | -70 |  | -3 | -6 | -9 |  | -4 | -3 | -7 |
| Total Proposed Project Trips |  |  |  |  | 422 |  | 16 | 20 | 36 |  | 22 | 23 | 45 |
| Net New Project Trips |  |  |  |  | 334 |  | 13 | 14 | 27 |  | 18 | 20 | 38 |

Notes:

1. ITE Code 210 (Single-Family Detached Housing); Based on ITE equation.
2. ITE Code 720 (Medical Office Building) assumed for Residential Treatment Facility; Based on ITE equation. Storage building not included in floor area estimate.
3. ITE Code 221 (Multi-Family Housing, Mid-Rise); Based on ITE equation.
4. ITE Code 254 (Assisted Living) assumed for Residential Treatment Facility; Based on ITE average rate. No equation available.
5. ITE Code 720 (Medical Office Building) assumed for Out-Patient Center; Based on ITE equation.
6. Manager's Unit. No commute peak hour trips assumed (AM \& PM peaks). ITE Code 221 (Multi-Family Housing, Mid-Rise) used for daily trip estimate.

Source: Institute of Transportation Engineers (ITE) Trip Generation 10th Edition, 2017;

### 4.3 PROJECT TRIP DISTRIBUTION AND ASSIGNMENT

Due to the nature of the proposed development, most residents, employees, patients, and patrons accessing the site are expected to travel along Freedom Boulevard and Main Street. These roadways provide local and regional access within the City of Watsonville and Santa Cruz County.

Trip distribution and assignment for the proposed Project was determined from the Association of Monterey Bay Area Governments (AMBAG) 2040 travel demand forecast model and engineering judgement. The following illustrates the distribution assumed for the Project:

- Freedom Boulevard - Approximately $20 \%$ of Project trips would distribute north while approximately $30 \%$ would distribute south towards downtown Watsonville.
- Auto Center Drive / Arthur Road - Approximately 30\% of Project trips would distribute south towards SR 152 / Main Street while approximately 20\% would distribute north.
- Arthur Road - Approximately $20 \%$ of Project would be distributed towards the schools in the surrounding area.

Figure 5 and Figure 6 present the traffic distribution and assignment for the analysis.
During the peak hours, the four (4) driveways would experience approximately 36 AM and 45 PM total gross trips, and these Project trips would be shared by each of the Project driveways. Project driveways volumes and through volumes along Miles Lane is relatively low, therefore, LOS analysis at the Project driveways are not warranted.


8
LEGEND



| LEGEND |  |
| :---: | :--- |
| $X$ | INTERSECTION \# |
| TRAFFIC SIGNAL |  |
| STOP | STOP SIGN APPROACH |
|  | PROJECT AREA |



### 4.4 EXISTING (2018) PLUS PROJECT CONDITIONS LEVEL OF SERVICE

Traffic operations were evaluated at the study intersections under Existing Plus Project conditions and traffic generated by the proposed Project. Project trips were added to existing volumes and are shown in Figure 7. Results of the analysis are presented in Table 4. Synchro analysis sheets are provided in the Appendix. As shown in Table 4, all study intersections are anticipated to operate at LOS D or better under Existing Plus Project conditions for the AM and PM peak hour. No mitigations would be required for the Existing Plus Project conditions.

Table 4 - Existing Plus Project Level of Service

| \# | Intersection | LOS <br> Standard | Control Type | Existing Conditions |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | AM Peak Hour |  |  | PM Peak Hour |  |  |
|  |  |  |  | Movement | Delay | LOS | Movement | Delay | LOS |
| 1 | Freedom Boulevard \& Miles Lane | D | SSSC | Overall | 2.5 | A | Overall | 3.1 | A |
|  |  |  | Worst Approach | EB | 11.1 | B | EB | 12.3 | B |
| 2 | Santa Clara Street \& Miles Lane | D | AWSC | Overall | 7.1 | A | Overall | 7.4 | A |
| 3 | Santa Clara Street \& Marin Street | D | AWSC | Overall | 11.0 | B | Overall | 9.3 | A |
| 4 | Auto Center Drive \& Marin Street | D | SSSC | Overall | 6.6 | A | Overall | 4.2 | A |
|  |  |  | Worst Approach | WB | 23.8 | C | WB | 17.5 | C |

Notes:

1. Analysis performed using HCM 2010 methodologies.
2. Delay indicated in seconds/vehicle.
3. Overall level of service (LOS) standard for the City is D.
4. Intersections that fall below City standard are shown in bold.



| LEGEND |
| :---: |
| $X$ |
| INTERSECTION \# |
| TRAFFIC SIGNAL |
| STOP |
| STOP SIGN APPROACH |



### 5.0 NEAR TERM CONDITIONS (2021)

### 5.1 NEAR TERM (2021) INTERSECTION AND ROADWAY NETWORK

For the Near Term conditions, it is assumed that all existing intersection geometries and roadway networks remain the same. Traffic operations were evaluated at the study intersections under Near Term conditions and traffic generated by the Near-Term Conditions is illustrated on Figure 8.

### 5.2 NEAR TERM (2021) VOLUME GROWTH

Two sources were considered when developing the Near Term volumes:

- Sunshine Vista Phased Development Project Traffic Impact Analysis prepared by Keith Higgins (January 2017)
- The Association of Monterey Bay Area Governments (AMBAG) 2040 Model

The Sunshine Vista TIA was provided by City of Watsonville Staff and was used to determine if any Project trips would carry over to the intersections effected by the Project. No trips were assigned to the study intersections. The model was then used to determine an annual growth rate to develop near term volumes. An annual growth rate of $0.35 \%$ was determined for the neighborhood traffic, while an annual growth rate of $0.93 \%$, as determined for Freedom Boulevard.

### 5.3 NEAR TERM CONDITIONS (2021) LEVEL OF SERVICE

Results of the analysis are presented in Table 5. Analysis sheets are provided in the Appendix. As shown in Table 5, all study intersections are anticipated to operate at LOS D or better under Near Term conditions for the AM and PM peak hour. As shown in Table 5, all study intersections are anticipated to operate at LOS D or better under Near Term conditions for the AM and PM peak hour. No mitigations would be required under Near Term conditions.

Table 5 - Near Term (2021) Level of Service

| \# | Intersection | LOS <br> Standard | Control Type | Near Term (2021) Conditions |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | AM Peak Hour |  |  | PM Peak Hour |  |  |
|  |  |  |  | Movement | Delay | LOS | Movement | Delay | LOS |
| 1 | Freedom Boulevard \& Miles Lane | D | SSSC | Overall | 2.5 | A | Overall | 3.1 | A |
|  |  |  | Worst Approach | EB | 11.1 | B | EB | 12.3 | B |
| 2 | Santa Clara Street \& Miles Lane | D | AWSC | Overall | 7.1 | A | Overall | 7.3 | A |
| 3 | Santa Clara Street \& Marin Street | D | AWSC | Overall | 10.8 | B | Overall | 9.3 | A |
| 4 | Auto Center Drive \& Marin Street | D | SSSC | Overall | 6.3 | A | Overall | 3.9 | A |
|  |  |  | Worst Approach | WB | 23.2 | C | WB | 17.1 | C |

Notes:

1. Analysis performed using HCM 2010 methodologies.
2. Delay indicated in seconds/vehicle.
3. Overall level of service (LOS) standard for the City is $D$.
4. Intersections that fall below City standard are shown in bold.



### 5.4 NEAR TERM (2021) PLUS PROJECT CONDITIONS LEVEL OF SERVICE

Traffic operations were evaluated at the study intersections under Near Term Plus Project Conditions and traffic generated by this scenario is illustrated on Figure 9. Results of the analysis are presented in Table 6. Synchro Analysis sheets are provided in the Appendix. As shown in Table 6, all study intersections are anticipated to operate at LOS D or better under Near Term Plus Project conditions for the AM and PM peak hour. As shown in Table 6, all study intersections are anticipated to operate at LOS D or better under Near Term Plus Project conditions for the AM and PM peak hour. No mitigations would be required under the Near Term Plus Project conditions.

Table 6 - Existing Plus Near Term Plus Project Level of Service

| \# | Intersection | LOS <br> Standard | Control Type | Near Term Plus Project Conditions |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | AM Peak Hour |  |  | PM Peak Hour |  |  |
|  |  |  |  | Movement | Delay | LOS | Movement | Delay | LOS |
| 1 | Freedom Boulevard / Miles Lane | D | SSSC | Overall | 2.5 | A | Overall | 3.2 | A |
|  |  |  | Worst Approach | EB | 11.2 | B | EB | 12.5 | B |
| 2 | Santa Clara Street / Miles Lane | D | AWSC | Overall | 7.1 | A | Overall | 7.4 | A |
| 3 | Santa Clara Street / Marin Street | D | AWSC | Overall | 11.0 | B | Overall | 9.4 | A |
| 4 | Auto Center Drive / Marin Street | D | SSSC | Overall | 6.7 | A | Overall | 4.2 | A |
|  |  |  | Worst Approach | WB | 24.3 | C | WB | 17.7 | C |

Notes:

1. Analysis performed using HCM 2010 methodologies.
2. Delay indicated in seconds/vehicle.
3. Overall level of service (LOS) standard for the City is D.
4. Intersections that fall below City standard are shown in bold.



### 6.0 CUMULATIVE (2040) CONDITIONS

### 6.1 CUMULATIVE (2040) ROADWAY NETWORK

The Watsonville Vista 2030 General Plan and Major Street Master Plan (MSMP) describes several improvements to the City of Watsonville roadway network. According to the General Plan and the MSMP, the Project intersections that were analyzed with the Project would not be affected. Therefore, the geometry used for the Existing Conditions are assumed for the Cumulative Conditions.

### 6.2 CUMULATIVE (2040) INTERSECTION LEVEL OF SERVICE

Traffic operations at the study intersections were evaluated under cumulative traffic conditions based on the AMBAG regional travel demand forecasting model, which reflects buildout of the General Plan and other regional growth anticipated outside of the City of Watsonville. The model was used to plot bidirectional AM and PM peak hour traffic volumes on each segment along roadways within the study area. Model output was used to compare base year volumes and year 2040 model forecasts to determine the annual incremental growth in traffic volumes at study intersections. For this analysis an annual growth rate of $0.35 \%$ per year was estimated for Auto Center Drive, Arthur Road, Miles Lane, Santa Clara Street, and Marin Street roadways, while an annual growth rate of $0.93 \%$ per year was estimated for Freedom Boulevard.

Cumulative traffic volumes are shown in Figure 10. Results of the analysis are presented in Table 7. As shown in Table 7, all study intersections are anticipated to operate at LOS D or better under Cumulative conditions for the AM and PM peak hour. No mitigations would be required under the Cumulative conditions.

Table 7 - Cumulative (2040) Project Level of Service

| \# | Intersection | LOSStandard | Control Type | Cumulative (2040) Conditions |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | AM Peak Hour |  |  | PM Peak Hour |  |  |
|  |  |  |  | Movement | Delay | LOS | Movement | Delay | LOS |
| 1 | Freedom Boulevard / Miles Lane | D | SSSC | Overall | 2.9 | A | Overall | 4.3 | A |
|  |  |  | Worst Approach | EB | 12.0 | B | EB | 13.7 | B |
| 2 | Santa Clara Street / Miles Lane | D | AWSC | Overall | 7.1 | A | Overall | 7.4 | A |
| 3 | Santa Clara Street / Marin Street | D | AWSC | Overall | 11.7 | C | Overall | 9.6 | B |
| 4 | Auto Center Drive / Marin Street | D | SSSC | Overall | 7.7 | A | Overall | 4.3 | A |
|  |  |  | Worst Approach | WB | 28.7 | D | WB | 19.1 | C |

Notes:

1. Analysis performed using HCM 2010 methodologies.
2. Delay indicated in seconds/vehicle.
3. Overall level of service (LOS) standard for the City is D.
4. Intersections that fall below City standard are shown in bold.



### 6.3 CUMULATIVE (2040) PLUS PROJECT INTERSECTION LEVEL OF SERVICE

Trips generated by the Project were assigned in the cumulative Year 2040 conditions and are shown in Figure 11. Cumulative plus Project conditions were evaluated at study intersections and are presented in Table 8 with the same geometry as existing conditions. As shown in Table 8, all study intersections are anticipated to operate at LOS D or better under Cumulative Plus Project conditions for the AM and PM peak hour. No mitigations would be required under the Cumulative Plus Project conditions.

Table 8 - Cumulative (2040) Plus Project Intersection Level of Service Summary

| \# | Intersection | LOSStandard | Control Type | Cumulative (2040) Plus Project Conditions |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | AM Peak Hour |  |  | PM Peak Hour |  |  |
|  |  |  |  | Movement | Delay | LOS | Movement | Delay | LOS |
| 1 | Freedom Boulevard / Miles Lane | D | SSSC | Overall | 3.0 | A | Overall | 4.4 | A |
|  |  |  | Worst Approach | EB | 12.1 | B | EB | 13.8 | B |
| 2 | Santa Clara Street / Miles Lane | D | AWSC | Overall | 7.1 | A | Overall | 7.5 | A |
| 3 | Santa Clara Street / Marin Street | D | AWSC | Overall | 11.9 | B | Overall | 9.7 | A |
| 4 | Auto Center Drive / Marin Street | D | SSSC | Overall | 8.3 | A | Overall | 4.7 | A |
|  |  |  | Worst Approach | WB | 30.3 | D | EB | 19.9 | C |

Notes:

1. Analysis performed using HCM 2010 methodologies.
2. Delay indicated in seconds/vehicle.
3. Overall level of service (LOS) standard for the City is D.
4. Intersections that fall below City standard are shown in bold.




### 7.0 POTENTIAL IMPACTS ON PEDESTRIAN, BICYCLE, AND TRANSIT MOBILITY

The Project was evaluated to determine if it would adversely affect adopted policies, plans, or programs supporting alternative transportation (e.g., bus turnouts, bicycle racks and pedestrian flow) or generate pedestrian, bicycle, or transit travel demand that would not be accommodated by transit, bicycle, or pedestrian facilities and plans. The following sections describe the evaluation.

### 7.1 PEDESTRIAN MOBILITY

Residents, employees, patients, and patrons choosing to walk to the site would not be adversely impacted based on pedestrian mobility, accessibility, or safety once frontage improvements are constructed. Light pedestrian trips both in the weekday AM peak period and weekday PM peak period are anticipated for the Project. It is also expected that pedestrians would walk from their homes to the existing bus stop on Freedom Boulevard.

Internal pedestrian connections will link the proposed site's entrance with the parking areas.

### 7.2 BICYCLE MOBILITY

Residents, employees, patients, and patrons choosing to bike to the site would not be adversely impacted based on bicyclist mobility, accessibility, or safety. Some bicycle trips both in the weekday AM peak period and weekday PM peak period are anticipated for the Project. Existing Class II facilities exist on Freedom Boulevard just south of Miles Lane, while Class III bicycle facilities exist along Auto Center Drive, Arthur Road, and Freedom Boulevard. Pavement markings and signage indicate that bicycles will share the roadway with vehicles.

Existing bicycle facilities are discussed in Section 3.3 Existing (2018) Pedestrian and Bicycle Network.

### 7.3 TRANSIT MOBILITY

Residents, employees, and patrons choosing to utilize transit would not be adversely impacted based on pedestrian mobility, accessibility, or safety at the Project site. Pedestrian trips to the Project are anticipated as Santa Cruz Metro bus stops are located along Freedom Boulevard. Sidewalks exist along Miles Lane and Freedom Boulevard that will provide connectivity between the Project site and existing Santa Cruz Metro bus stops. A bus stop is located approximately 800 feet from the Project site. Service routes and stops are discussed in detail in Section 3.4 Existing (2018) Transit Network.

Residents, employees, and patrons of the proposed Project have the option of driving, taking transit, walking, or bicycling to the site. Those that choose to take transit have access to a bus stop on Freedom Boulevard. According to 2013-2017 American Community Survey (S0801) indicates that approximately $1.4 \%$ of City of Watsonville residents use transit to travel to/from home while approximately $2.8 \%$ of Santa Cruz County residents use transit to travel to/from home. The AM and PM commute periods typically represent the highest level of transit ridership during the day, with other periods being lower. It is anticipated that Project transit ridership will range between $1.4 \%$ and $2.8 \%$. This percentage was then applied to the net new trips determined in the Project trip generation in section 4.2 Project Trip Generation. Therefore, approximately 1 new passenger trip during the weekday AM peak period and approximately 1 new passenger trip during the weekday PM peak period, could be generated by the Project. These new trips
would have a negligible adverse impact on transit mobility, accessibility, and safety at any of the study intersections. To provide a more conservative analysis, transit trips were not reduced from the trip generation provided in Table 3.

### 8.0 PARKING REQUIREMENTS

The following sections discuss the proposed on-site parking supply to be constructed by the Project.

### 8.1 ON-SITE PARKING

## CITY OF WATSONVILLE AUTOMOBILE PARKING REQUIREMENTS

Table 9 provides the automobile parking requirements for all the land uses expected to be constructed at the Project. Automobile parking rates were taken from the City of Watsonville Municipal Code (June 2014) Chapter 14-17 Parking and Loading Facilities. For this site, guest parking is required because the site is zoned as RM-2 (Multiple Residential-Medium Density). The following sections were used for each land use:

- Multi-Family Housing (Affordable Housing) - Section 14-47.110(f) (assumes density bonus is approved by the City)
- Residential Treatment Facility - Article 3 (Section 14-17.301, DLU:0721 \& 0722 (f \& g))
- Out-Patient Center - Article 10 (Section 14-17.1001, GLU:66 (3))

Table 9 - Automobile Parking Requirements

| Land Use Description |  | te | No. of Units | Spaces <br> Required |
| :---: | :---: | :---: | :---: | :---: |
| Multi-Family Housing (Section 14-47.110(f)) | 0-1 bedrooms | 1 space per unit | 22 units | 22 |
|  | 2-3 bedrooms | 2 spaces per unit | 38 units | 76 |
| Residential Treatment Facility (Article 3) | 1 space per 3 beds |  | 30 beds | 10 |
| Employees per Shift (Article 3) | 1 space per employee on shift with maximum personnel |  | 4 employees | 4 |
| Out-Patient Center <br> (Article 10) | 1 space for each 300 SQFT of floor area |  | 3,810 | 13 |
| Total Spaces Required |  |  |  | 125 |

Based on Table 9, the Project is required to provide 125 vehicle parking spaces. According to the Property Information, located on Figure 2, the Project proposes to provide a total of 125 parking spaces. Therefore, the proposed parking supply would meet City requirements.

## AMERICANS WITH DISABILITIES ACT (ADA) PARKING REQUIREMENTS

Minimum ADA parking requirements are provided in the 2010 ADA Standards for Accessible Design (2010) Table 208.2. The Project provides 125 spaces which would require a minimum of five (5) ADA spaces. The Project provides a total of eight (8) (4 van accessible spaces and 4 standard accessible spaces) ADA spaces.

Therefore, the Project would provide enough ADA parking. Table 208.2 is provided in the Appendix of this report.

## CITY OF WATSONVILLE BICYCLE PARKING REQUIREMENTS

Table 10 provides the bicycle parking requirements for the Project. Bicycle parking rates were taken from the City of Watsonville Municipal Code (June 2014) Chapter 14-17 Parking and Loading Facilities.

According to City of Watsonville Municipal Code (14-17.113), bicycle parking shall be required except for land uses MLU-0 and MLU-9. The Project site is proposed to be zoned in the RM-2/PD zone which means that bicycle parking is required. Table 10 provides the bicycle parking requirements according to the City of Watsonville Municipal Code.

Table 10 - Bicycle Parking Requirements
Rate No. of Parking Spaces

Required

Bicycle Spaces Required 125

Base on Table 10, the Project is required to provide seven (7) bicycle parking spaces. The Project proposes to provide a total of 36 bicycle parking spaces. Therefore, the Project would provide a surplus of 29 bicycle parking spaces.

### 9.0 ON SITE CIRCULATION AND SIGHT DISTANCE ANALYSIS

### 9.1 SITE CIRCULATION

The following describes on-site circulation of the proposed Project driveways along Miles Lane and Kimberly Lane.

## MILES LANE \& PROJECT DRIVEWAY \#1

Project Driveway \#1 is located along Miles Lane and will be a full access driveway to motorists entering and leaving the Project site. The driveway will be for patrons and employees that want to access the Encompass Community Center.

Project Driveway \#1 is not expected to experience significant vehicle queues and delay since volumes to/from the site are relatively low.

## MILES LANE \& PROJECT DRIVEWAYS \#2 AND \#3

Project Driveway \#2 and \#3 are located on Miles Lane and will be a full access driveway to motorists entering and leaving the Project site. These driveways will be used primarily for residents and guests that want to access the affordable housing units; however, employees and patrons are also able to access the community gardens and the retail space using these driveways.

Project Driveways \#2 and \#3 are not expected to experience significant vehicle queues and delay since volumes to/from the site are relatively low.

## MILES LANE \& PROJECT DRIVEWAY \#4

Project Driveway \#4 is located east of driveways \#2 and \#3. This driveway will provide full access primarily for residents who want to access the residences. Residents who want to access their home on the south east portion of the Project site would use this driveway and an access road would be provided to go to/from this driveway.

Project Driveway \#4 is not expected to experience significant vehicle queues or delay since volumes to/from the site are relatively low.

### 9.2 SIGHT DISTANCE ANALYSIS AT AUTO CENTER DRIVE \& MARIN STREET

## SIGHT DISTANCE DEFINITIONS

A preliminary stopping sight distance and intersection sight distance analysis was conducted to determine if the intersection of Auto Center Drive \& Marin Street were operating at acceptable levels. AASHTO methodology was used in this analysis. The sight distance needed under various assumptions of physical conditions and driver behavior is directly related to vehicle speeds and to the resultant distances traversed during perception-reaction time and braking.

Stopping sight distance is defined as the sum of reaction distance and braking distance. The reaction distance is based upon the driver reaction time while the braking distance is dependent upon the vehicle speed and the coefficient of friction between the tires and roadway as the vehicle decelerates to a complete stop. This sight distance analysis indicates the minimum visibility that is required for an approaching vehicle
on Auto Center Drive to stop safely if a vehicle from Marin Street enters or exits the approaching road. The driver should also have an unobstructed view of the intersection, including any traffic-control devices, and sufficient lengths along the intersecting road to permit the driver to anticipate and avoid potential collisions.

For vehicles entering Auto Center Drive from Marin Street, the AASHTO method evaluates sight distance from a vehicle exiting the driveway to a vehicle approaching from either direction. The intersection sight distance is defined along intersection approach legs and across their included corners known as departure sight triangles. These specified areas should be clear of obstructions that might block a driver's view of potentially conflicting vehicles. Intersection sight distance is measured from a point 3.5 -feet above the existing grade (driver's eye) along the potential driveway to a 3.5 -foot object height in the center of the approaching lane on Auto Center Drive. A vehicle setback in a stopped position from edge of travel way was assumed for determining intersection sight distance.

## EXISTING SITE DISTANCE ANALYSIS AT AUTO CENTER DRIVE \& MARIN STREET

The critical variable for determining actual sight distance is the vehicle and driver's eye setback. The AASHTO standard setback is 14.5 feet from the edge of the vehicle traveled way. Due to existing constraints from the existing S-curve and Romo's Auto Group, a 14.5 -foot setback provides insufficient sight distance. AASHTO also states that that the distance from the front of a passenger vehicle to the driver's eye is nearly always eight (8) feet. To illustrate this intersection more realistically, sight distance was analyzed from the car stopped at the outside edge of the traveled lane ( 8 -foot setback from travelway).

Minimum sight distance criteria for the potential driveway along Auto Center Drive was determined from the AASHTO Geometric Design of Highways and Streets 6th Edition (Green Book). Speed data was provided by City of Watsonville staff and the $85^{\text {th }}$ percentile speed was determined to be 25 miles per hour. For the purposes of this analysis, a design speed of 30 mph ( 25 mph posted speed limit) was assumed along Auto Center Drive to be conservative.

Along Auto Center Drive, as southbound drivers approach the intersection, they would experience a downgrade of approximately $5 \%$, while northbound drivers would experience an upgrade of approximately $2 \%$. Along Marin Street, drivers would experience an upgrade of approximately $6.4 \%$ as they approach the intersection. These grades have been verified with field calculations.

Based on the existing traffic control, minimum sight distance was calculated for the following scenarios:

- Stopping Sight Distance on Auto Center Drive
- Intersection Sight Distance Case B - Stop control at Marin Street
- Case B1 - Left turn from the minor road
- Case B2 - Right turn from the minor road

AASHTO standard time gap variables for passenger cars stopped on the proposed project driveways were used. Additional time gap was added to Case B1 and B2 because the existing grade exceeded 3\%. This was a more conservative approach because a car may pull up into the $6.4 \%$ grade and perform a left turn or a right turn movement.

From Equations 3-4 and 3-5 of the Green Book, the minimum stopping sight distance for southbound drivers is approximately 211 feet and is approximately 192 feet for northbound drivers. From Equations 9-38 and $9-41$, the intersection sight distance is approximately 387 feet for Case B1 and approximately 315 feet for Case B2 assuming approach grades mentioned above and a design speed of 30 mph .

Figure 12 shows the intersection and stopping sight distance for an 8 -foot setback from the vehicular traveled way (8-foot setback from curb). This assumes that a vehicle has stopped at the stop bar, confirmed that no crossing pedestrians are present, pulled forward and stopped before the traveled way. Vehicles entering Auto Center Drive from the Marin Street will not have sufficient intersection sight distance in either direction to make a right or left turn onto the road per AASHTO Case B1 and B2 scenarios.

From Figure 12, stopping sight distance is adequate for vehicles traveling northbound on Auto Center Drive; however, vehicles traveling southbound on Auto Center Drive would have sight distance impeded by the existing fence and parked cars. The intersection sight distance is insufficient for both the northbound and southbound approaches due to the grade and parked vehicles.


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## RECOMMENDED IMPROVEMENTS

Figure 13 shows the recommended improvements along Auto Center Drive to improve the safety of vehicles at the Auto Center Drive \& Marin Street intersection and are summarized below. All striping details are from Caltrans Standard Plans (2018).

- Auto Center Drive South of Marin Street
- Provide approximately 280 feet of Striping Detail 22 (Centerline)
- Provide approximately 350 feet of Striping Detail 27B (Right Edgeline) and create a painted bulb-out for vehicles entering from Auto Center Drive. Within the painted bulb-out, add 6" diagonal white striping with 15 ' spacing. The right edgeline striping would move the center of the road away from the curb allowing for better visibility.
- Provide "Intersection Ahead" signage (W1-10e) with "Speed Sign" (W13-1P) with 20 mph speed and a custom "Limited Sight Distance" sign. Place at point of curvature for Northbound approach according to MUCTD Table 2C-4. This sign would warn drivers of the approaching intersection to be aware of cross traffic and to reduce speed.
- Marin Street
- Move the 12 inch stop bar closer to the curb line along with new "STOP" markings. This will allow drivers to pull up further into the new 8 -foot parking lane to increase visibility along Auto Center Drive.
- Provide approximately 75 feet of Striping Detail 22 (Centerline) to shift the westbound intersection approach to the north. This would allow for more visibility on the Auto Center Drive northbound approach.
- Extend red curb on the south curb approximately 85 feet. This red curb would remove approximately three on-street parking spaces. This would prevent drivers from parking in the painted bulb-out.
- Extend red curb on the north curb approximately 30 feet. This red curb would remove approximately one on-street parking space to allow more space for drivers to approach the intersection.
- Auto Center Drive North of Marin Street
- Extend red curb approximately 120 feet on the east curb and provide "No Parking Anytime" signage. This would remove approximately five (5) on-street parking spaces. Red curb would make parking illegal along the eastern curb allowing southbound sight distance to be unobstructed.
- Provide "Intersection Ahead" signage (W1-10e) with "Speed Sign" (W13-1P) with 20 mph speed and a custom "Limited Sight Distance" sign. Place at point of curvature for
southbound approach according to MUCTD Table 2C-4. This sign would warn drivers of the approaching intersection to be aware of cross traffic and to reduce speed.
- Provide speed feedback sign similar to existing signage on east side of Auto Center Drive. Place at point of curvature for southbound approach according to MUCTD Table 2C-4.
- Provide approximately 200 feet of Striping Detail 22 (Centerline) and Striping Detail 27B (Right Edgeline) for the Northbound approach. Right edgeline striping would be 8-feet from the curb. This striping would reduce confusion for vehicles traveling northbound.
- Provide approximately 490 feet of Striping Detail 27B (Right Edgeline) for the Southbound approach. This striping would move the center of the road away from the curb allowing for better visibility.


Kimley»)Horn

## SIGHT DISTANCE WITH RECOMMENDED IMPROVEMENTS

With the improvements to Auto Center and Marin Street the drivers eye can now be measured from the edge of the parking lane instead of the curb since the edge of the traveled way is at the edge of the parking lane. In addition, the drivers eye can be located per the AASHTO standard of 14.5 feet from the edge of the traveled way. This assumes that the vehicle has stopped at the stop bar and confirmed that no pedestrians are present; however, an additional 6.5 -foot buffer, between the front of the vehicle and the traveled way is now available. This is a more conservative analysis because this assumes that a vehicle will not completely pull up to the edge of the traveled way. This means a driver would require more visibility because they are further away from intersection.

Along with the change in the striping, warning signs are also installed to warn drivers to travel at 20 mph instead of 30 MPH . The City of Watsonville provided speed data for Auto Center Drive, and it was determined that the $85^{\text {th }}$ percentile speed is 25 miles per hour. Based on the $85^{\text {th }}$ percentile, this would mean drivers would need to travel five (5) miles per hour slower which is a reasonable reduction in speed. The reduction in speed means the required stopping sight and intersection sight distance will also decrease because vehicles are traveling slower and do not need as much time to stop. From Equations 3-3 and 3-4 of the AASHTO Green Book, the minimum stopping sight distance for southbound drivers is approximately 119 feet and is approximately 110 feet for northbound drivers. From Equations 9-38 and 9-41, the intersection sight distance is 258 feet for Case B1 and 210 feet for Case B2 assuming existing approach grades at a warning speed of 20 mph .

Figure 14 shows the new stopping sight distance and intersection sight distance for all approaches. As seen in Figure 14 there is some hatching for both the northbound and southbound intersection sight distance zones. This hatching is the area where a driver cannot see; however, the driver can see the center of the driving lane. Cars are expected to drive along the center of the lane, which means this hatching will not impede sight distance for drivers performing movements out of Marin Street.

With these improvements, the intersection of Auto Center Drive and Marin Street are now compliant with AASHTO stopping sight and intersection sight distance.


Kimley») Horn

### 10.0 TRAFFIC IMPACT FEES AND RECOMMENDED IMPROVEMENTS

### 10.1 TRAFFIC IMPACT FEES

To determine traffic impact fees, the City of Watsonville provides a Development Fee Summary (20172018) that lists all the development fees for a Project. This document is provided in the Appendix of this report.

When calculating the traffic impact fee for the Project, analysis needed to be broken into existing and proposed conditions to determine the total net traffic impact fee. For the existing conditions, Single Family detached and Non-Residential (other) were used to determine the trips per unit. For this analysis, the managers unit was included in proposed conditions because the manager will contribute to the daily traffic on the roadway network. For the proposed conditions, Multi-Family and Non-Residential (other) were used to determine the trips per unit. Table 11 summaries the traffic impact fee for the Project.

Table 11 - Traffic Impact Fee

| Land Use | Units | Rate ${ }^{1}$ | Total Trips | Fee | Total |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Existing Conditions |  |  |  |  |  |
| Single Family Residential | 4 DU | 14 trips per unit | 56 trips | \$185 per trip | \$10,360 |
| Residential Treatment Facility | 3.442 KSF | - | 16 daily trips | \$95 per trip | \$1,520 |
| Total Existing Conditions Traffic Impact Fee |  |  |  |  | \$11,880 |
| Proposed Conditions |  |  |  |  |  |
| Multi-Family Residential | 61 DU | 10 trips per unit | 610 trips | \$185 per trip | \$112,850 |
| Residential Treatment Facility | 7.100 KSF | - | 30 daily trips | \$95 per trip | \$2,850 |
| Out-Patient Care | 3.810 KSF | - | 60 daily trips | \$95 per trip | \$5,700 |
| Total Proposed Conditions Traffic Impact Fee |  |  |  |  | \$121,400 |
| Total Net Traffic Impact Fee |  |  |  |  | \$109,520 |

Based on Table 11, the Project would require a net traffic impact fee of \$109,520.

### 10.2 RECOMMENDED IMPROVEMENTS

Based on the findings of this report, the Project would require no additional improvements to study intersections or roadway network would be required. All intersections would be expected to operate at a Level of Service (LOS) of D or better with the implementation of the Project which means further intersection improvements are not necessary.

At the intersection of Auto Center Drive and Marin Street, the following improvements are recommended to improve the sight distance at the intersection:

- Auto Center Drive South of Marin Street
- Provide approximately 280 feet of Striping Detail 22 (Centerline)
- Provide approximately 350 feet of Striping Detail 27B (Right Edgeline) and create a painted bulb-out for vehicles entering from Auto Center Drive. Within the painted bulb-out, add 6" diagonal white striping with 15 ' spacing. The right edgeline striping would move the center of the road away from the curb allowing for better visibility.
- Provide "Intersection Ahead" signage (W1-10e) with "Speed Sign" (W13-1P) with 20 mph speed and a custom "Limited Sight Distance" sign. Place at point of curvature for Northbound approach according to MUCTD Table 2C-4. This sign would warn drivers of the approaching intersection to be aware of cross traffic and to reduce speed.
- Marin Street
- Move the 12-inch stop bar closer to the curb line along with new "STOP" markings. This will allow drivers to pull up further into the new 8 -foot parking lane to increase visibility along Auto Center Drive.
- Provide approximately 75 -feet of Striping Detail 22 (Centerline) to shift the westbound intersection approach to the north. This would allow for more visibility on the Auto Center Drive northbound approach.
- Extend red curb on the south curb approximately 85 feet. This red curb would remove approximately three on-street parking spaces. This would prevent drivers from parking in the painted bulb-out.
- Extend red curb on the north curb approximately 30 feet. This red curb would remove approximately one on-street parking space to allow more space for drivers to approach the intersection.
- Auto Center Drive North of Marin Street
- Extend red curb approximately 120 feet on the east curb and provide "No Parking Anytime" signage. This would remove approximately five (5) on-street parking spaces. Red curb would make parking illegal along the eastern curb allowing southbound sight distance to be unobstructed.
- Provide "Intersection Ahead" signage (W1-10e) with "Speed Sign" (W13-1P) with 20 mph speed and a custom "Limited Sight Distance" sign. Place at point of curvature for southbound approach according to MUCTD Table 2C-4. This sign would warn drivers of the approaching intersection to be aware of cross traffic and to reduce speed.
- Provide speed feedback sign similar to existing signage on east side of Auto Center Drive. Place at point of curvature for southbound approach according to MUCTD Table 2C-4.
- Provide approximately 200 feet of Striping Detail 22 (Centerline) and Striping Detail 27B (Right Edgeline) for the Northbound approach. Right edgeline striping would be 8 -feet from the curb. This striping would reduce confusion for vehicles traveling northbound.
- Provide approximately 490 feet of Striping Detail 27B (Right Edgeline) for the Southbound approach. This striping would move the center of the road away from the curb allowing for better visibility.


## APPENDIX

A: TURNING MOVEMENT VOLUMES

B: EXISTING TRAFFIC CONDITIONS (2018) ANALYSIS SHEETS

C: EXISTING (2018) PLUS PROJECT TRAFFIC CONDITIONS ANALYSIS SHEETS

D: NEAR TERM (2021) TRAFFIC CONDITIONS ANALYSIS SHEETS

E: NEAR TERM (2021) PLUS PROJECT TRAFFIC CONDITIONS ANALYSIS SHEETS

F: CUMULATIVE (2040) TRAFFIC CONDITIONS ANALYSIS SHEETS

G: CUMULATIVE (2040) PLUS PROJECT TRAFFIC CONDITIONS ANALYSIS SHEETS

H: CITY OF WATSONVILLE DEVELOPMENT FEE SUMMARY 2017-2018

I: ADA 2010 STANDARDS FOR ACCESSIBLE DESIGN: TABLE 208.2 PARKING SPACES

J: EXISTING AND PROPOSED BICYCLE NETWORK AND TRANSIT FACILITIES

## APPENDIX A: TURNING MOVEMENT VOLUMES



Two-Hour Count Summaries

| Interval Start |  | Miles Ln |  |  |  | 0 |  |  |  | Freedom Blvd |  |  |  | Freedom Blvd |  |  |  | 15-min Total | Rolling One Hour |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Eastbound |  |  |  | Westbound |  |  |  | Northbound |  |  |  | Southbound |  |  |  |  |  |
|  |  | UT | LT | TH | RT | UT | LT | TH | RT | UT | LT | TH | RT | UT | LT | TH | RT |  |  |
| 7:00 |  | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 1 | 60 | 0 | 0 | 32 | 59 | 0 | 155 | 0 |
| 7:15 | AM | 0 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 2 | 82 | 0 | 0 | 48 | 77 | 0 | 213 | 0 |
| 7:30 | AM | 0 | 0 | 0 | 13 | 0 | 0 | 0 | 0 | 0 | 7 | 124 | 0 | 0 | 81 | 138 | 0 | 363 | 0 |
| 7:45 | AM | 0 | 0 | 0 | 6 | 0 | 0 | 0 | 0 | 0 | 11 | 154 | 1 | 0 | 81 | 172 | 1 | 426 | 1,157 |
| 8:00 | AM | 0 | 0 | 0 | 6 | 0 | 0 | 0 | 0 | 0 | 4 | 120 | 0 | 0 | 76 | 148 | 0 | 354 | 1,356 |
| 8:15 | AM | 0 | 1 | 0 | 8 | 0 | 0 | 0 | 0 | 0 | 2 | 107 | 0 | 0 | 46 | 153 | 2 | 319 | 1,462 |
| 8:30 | AM | 0 | 0 | 0 | 8 | 0 | 0 | 0 | 0 | 0 | 2 | 104 | 0 | 0 | 53 | 134 | 0 | 301 | 1,400 |
| 8:45 | AM | 0 | 0 | 0 | 10 | 0 | 0 | 0 | 0 | 0 | 3 | 84 | 0 | 0 | 36 | 96 | 2 | 231 | 1,205 |
| Count | Total | 0 | 1 | 0 | 58 | 0 | 0 | 0 | 0 | 0 | 32 | 835 | 1 | 0 | 453 | 977 | 5 | 2,362 | 0 |
|  | All | 0 | 1 | 0 | 33 | 0 | 0 | 0 | 0 | 0 | 24 | 505 | 1 | 0 | 284 | 611 | 3 | 1,462 | 0 |
| Peak <br> Hour | HV | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 14 | 1 | 0 | 6 | 8 | 0 | 30 | 0 |
|  | HV\% | - | 0\% | - | 0\% | - | - | - | - | - | 4\% | 3\% | 100\% | - | 2\% | 1\% | 0\% | 2\% | 0 |

Note: Two-hour count summary volumes include heavy vehicles but exclude bicycles in overall count.

| Interval Start | Heavy Vehicle Totals |  |  |  |  | Bicycles |  |  |  |  | Pedestrians (Crossing Leg) |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | EB | WB | NB | SB | Total | EB | WB | NB | SB | Total | East | West | North | South | Total |
| 7:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 1 | 0 | 0 | 3 |
| 7:15 AM | 0 | 0 | 2 | 3 | 5 | 0 | 0 | 0 | 0 | 0 | 6 | 7 | 0 | 0 | 13 |
| 7:30 AM | 0 | 0 | 5 | 5 | 10 | 0 | 0 | 0 | 1 | 1 | 6 | 2 | 0 | 0 | 8 |
| 7:45 AM | 0 | 0 | 4 | 5 | 9 | 0 | 0 | 0 | 0 | 0 | 5 | 1 | 0 | 0 | 6 |
| 8:00 AM | 0 | 0 | 4 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 2 |
| 8:15 AM | 0 | 0 | 3 | 4 | 7 | 0 | 0 | 0 | 0 | 0 | 1 | 3 | 0 | 0 | 4 |
| 8:30 AM | 1 | 0 | 4 | 6 | 11 | 0 | 0 | 0 | 0 | 0 | 1 | 2 | 0 | 2 | 5 |
| 8:45 AM | 0 | 0 | 3 | 4 | 7 | 0 | 0 | 0 | 0 | 0 | 4 | 6 | 0 | 0 | 10 |
| Count Total | 1 | 0 | 25 | 27 | 53 | 0 | 0 | 0 | 1 | 1 | 27 | 22 | 0 | 2 | 51 |
| Peak Hr | 0 | 0 | 16 | 14 | 30 | 0 | 0 | 0 | 1 | 1 | 14 | 6 | 0 | 0 | 20 |

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Two-Hour Count Summaries - Heavy Vehicles

| Interval Start | Miles Ln |  |  |  | 0 |  |  |  | Freedom Blvd |  |  |  | Freedom Blvd |  |  |  | 15-min Total | Rolling One Hour |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Eastbound |  |  |  | Westbound |  |  |  | Northbound |  |  |  | Southbound |  |  |  |  |  |
|  | UT | LT | TH | RT | UT | LT | TH | RT | UT | LT | TH | RT | UT | LT | TH | RT |  |  |
| 7:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 3 | 0 | 5 | 0 |
| 7:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 4 | 0 | 0 | 3 | 2 | 0 | 10 | 0 |
| 7:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 1 | 0 | 2 | 3 | 0 | 9 | 24 |
| 8:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 4 | 28 |
| 8:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 1 | 3 | 0 | 7 | 30 |
| 8:30 AM | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 3 | 0 | 0 | 1 | 5 | 0 | 11 | 31 |
| 8:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 1 | 3 | 0 | 7 | 29 |
| Count Total | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 2 | 22 | 1 | 0 | 8 | 19 | 0 | 53 | 0 |
| Peak Hour | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 14 | 1 | 0 | 6 | 8 | 0 | 30 | 0 |

Two-Hour Count Summaries - Bikes

| Interval Start | Miles Ln |  |  | 0 |  |  | Freedom Blvd |  |  | Freedom Blvd |  |  | 15-min Total | Rolling One Hour |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Eastbound |  |  | Westbound |  |  | Northbound |  |  | Southbound |  |  |  |  |
|  | LT | TH | RT | LT | TH | RT | LT | TH | RT | LT | TH | RT |  |  |
| 7:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 |
| 7:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 8:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 8:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 8:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Count Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 |
| Peak Hour | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 |

Note: U-Turn volumes for bikes are included in Left-Turn, if any.


Two-Hour Count Summaries

| Interval Start |  | Miles Ln |  |  |  | 0 |  |  |  | Freedom Blvd |  |  |  | Freedom Blvd |  |  |  | $\begin{aligned} & \text { 15-min } \\ & \text { Total } \end{aligned}$ | Rolling One Hour |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Eastbound |  |  |  | Westbound |  |  |  | Northbound |  |  |  | Southbound |  |  |  |  |  |
|  |  | UT | LT | TH | RT | UT | LT | TH | RT | UT | LT | TH | RT | UT | LT | TH | RT |  |  |
| 4:00 |  | 0 | 0 | 0 | 12 | 0 | 0 | 0 | 0 | 0 | 8 | 176 | 2 | 0 | 83 | 172 | 1 | 454 | 0 |
| 4:15 | PM | 0 | 0 | 0 | 12 | 0 | 0 | 0 | 0 | 0 | 6 | 154 | 1 | 0 | 94 | 181 | 4 | 452 | 0 |
| 4:30 | PM | 0 | 0 | 0 | 8 | 0 | 0 | 0 | 0 | 0 | 5 | 157 | 0 | 0 | 85 | 158 | 5 | 418 | 0 |
| 4:4 | PM | 0 | 0 | 0 | 14 | 0 | 0 | 0 | 0 | 0 | 5 | 145 | 0 | 0 | 85 | 174 | 7 | 430 | 1,754 |
| 5:00 | PM | 0 | 0 | 0 | 13 | 0 | 0 | 0 | 0 | 0 | 8 | 179 | 0 | 0 | 98 | 198 | 3 | 499 | 1,799 |
| 5:1 | PM | 0 | 0 | 0 | 16 | 0 | 0 | 0 | 0 | 0 | 7 | 151 | 2 | 0 | 113 | 195 | 6 | 490 | 1,837 |
| 5:30 | PM | 0 | 0 | 0 | 15 | 0 | 0 | 0 | 0 | 0 | 8 | 156 | 1 | 0 | 100 | 191 | 1 | 472 | 1,891 |
| 5:4 | PM | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 6 | 160 | 0 | 0 | 73 | 135 | 1 | 377 | 1,838 |
| Count | Total | 0 | 0 | 0 | 92 | 0 | 0 | 0 | 0 | 0 | 53 | 1,278 | 6 | 0 | 731 | 1,404 | 28 | 3,592 | 0 |
|  | All | 0 | 0 | 0 | 58 | 0 | 0 | 0 | 0 | 0 | 28 | 631 | 3 | 0 | 396 | 758 | 17 | 1,891 | 0 |
| Peak <br> Hour | HV | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 2 | 3 | 0 | 0 | 3 | 3 | 1 | 15 | 0 |
|  | HV\% | - | - | - | 5\% | - | - | - | - | - | 7\% | 0\% | 0\% | - | 1\% | 0\% | 6\% | 1\% | 0 |

Note: Two-hour count summary volumes include heavy vehicles but exclude bicycles in overall count.

| Interval Start | Heavy Vehicle Totals |  |  |  |  | Bicycles |  |  |  |  | Pedestrians (Crossing Leg) |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | EB | WB | NB | SB | Total | EB | WB | NB | SB | Total | East | West | North | South | Total |
| 4:00 PM | 0 | 0 | 1 | 2 | 3 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 0 | 0 | 4 |
| 4:15 PM | 0 | 0 | 1 | 2 | 3 | 0 | 0 | 1 | 0 | 1 | 4 | 3 | 1 | 0 | 8 |
| 4:30 PM | 1 | 0 | 0 | 3 | 4 | 0 | 0 | 0 | 0 | 0 | 4 | 4 | 0 | 0 | 8 |
| 4:45 PM | 0 | 0 | 3 | 2 | 5 | 0 | 0 | 0 | 1 | 1 | 8 | 3 | 0 | 0 | 11 |
| 5:00 PM | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 1 | 3 | 3 | 0 | 2 | 8 |
| 5:15 PM | 1 | 0 | 1 | 3 | 5 | 0 | 0 | 1 | 0 | 1 | 8 | 9 | 0 | 0 | 17 |
| 5:30 PM | 1 | 0 | 1 | 2 | 4 | 0 | 0 | 1 | 1 | 2 | 1 | 1 | 0 | 0 | 2 |
| 5:45 PM | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 4 | 0 | 1 | 6 |
| Count Total | 4 | 0 | 7 | 15 | 26 | 0 | 0 | 3 | 3 | 6 | 33 | 27 | 1 | 3 | 64 |
| Peak Hr | 3 | 0 | 5 | 7 | 15 | 0 | 0 | 2 | 3 | 5 | 20 | 16 | 0 | 2 | 38 |

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Two-Hour Count Summaries - Heavy Vehicles

| Interval Start | Miles Ln |  |  |  | 0 |  |  |  | Freedom Blvd |  |  |  | Freedom Blvd |  |  |  | 15-min Total | Rolling One Hour |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Eastbound |  |  |  | Westbound |  |  |  | Northbound |  |  |  | Southbound |  |  |  |  |  |
|  | UT | LT | TH | RT | UT | LT | TH | RT | UT | LT | TH | RT | UT | LT | TH | RT |  |  |
| 4:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 1 | 0 | 3 | 0 |
| 4:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 1 | 3 | 0 |
| 4:30 PM | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 2 | 0 | 4 | 0 |
| 4:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 2 | 0 | 0 | 1 | 1 | 0 | 5 | 15 |
| 5:00 PM | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 13 |
| 5:15 PM | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 2 | 0 | 1 | 5 | 15 |
| 5:30 PM | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 2 | 0 | 4 | 15 |
| 5:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 11 |
| Count Total | 0 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 3 | 4 | 0 | 0 | 6 | 7 | 2 | 26 | 0 |
| Peak Hour | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 2 | 3 | 0 | 0 | 3 | 3 | 1 | 15 | 0 |

Two-Hour Count Summaries - Bikes

| Interval Start | Miles Ln |  |  | 0 |  |  | Freedom Blvd |  |  | Freedom Blvd |  |  | $\begin{gathered} \text { 15-min } \\ \text { Total } \end{gathered}$ | Rolling One Hour |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Eastbound |  |  | Westbound |  |  | Northbound |  |  | Southbound |  |  |  |  |
|  | LT | TH | RT | LT | TH | RT | LT | TH | RT | LT | TH | RT |  |  |
| 4:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 0 |
| 4:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 2 |
| 5:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 3 |
| 5:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 3 |
| 5:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 2 | 5 |
| 5:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 |
| Count Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 3 | 0 | 6 | 0 |
| Peak Hour | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 3 | 0 | 5 | 0 |

Note: U-Turn volumes for bikes are included in Left-Turn, if any.


Note: Two-hour count summary volumes include heavy vehicles but exclude bicycles in overall count.

| Interval Start | Heavy Vehicle Totals |  |  |  |  | Bicycles |  |  |  |  | Pedestrians (Crossing Leg) |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | EB | WB | NB | SB | Total | EB | WB | NB | SB | Total | East | West | North | South | Total |
| 7:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 |
| 7:30 AM | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 2 |
| 7:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 2 |
| 8:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 2 |
| 8:30 AM | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:45 AM | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Count Total | 0 | 2 | 0 | 1 | 3 | 0 | 0 | 0 | 0 | 0 | 3 | 2 | 1 | 1 | 7 |
| Peak Hour | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 2 | 2 | 1 | 1 | 6 |

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Two-Hour Count Summaries - Heavy Vehicles

| Interval Start | Miles Ln |  |  |  | Miles Ln |  |  |  | Santa Clara St |  |  |  | Santa Clara St |  |  |  | $\begin{gathered} \text { 15-min } \\ \text { Total } \end{gathered}$ | Rolling One Hour |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Eastbound |  |  |  | Westbound |  |  |  | Northbound |  |  |  | Southbound |  |  |  |  |  |
|  | UT | LT | TH | RT | UT | LT | TH | RT | UT | LT | TH | RT | UT | LT | TH | RT |  |  |
| 7:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 |
| 7:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 8:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 8:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 8:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 |
| 8:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 2 |
| Count Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 3 | 0 |
| Peak Hour | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 |

Two-Hour Count Summaries - Bikes

| Interval Start | Miles Ln |  |  | Miles Ln |  |  | Santa Clara St |  |  | Santa Clara St |  |  | 15-min Total | Rolling One Hour |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Eastbound |  |  | Westbound |  |  | Northbound |  |  | Southbound |  |  |  |  |
|  | LT | TH | RT | LT | TH | RT | LT | TH | RT | LT | TH | RT |  |  |
| 7:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Count Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Peak Hour | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |

Note: U-Turn volumes for bikes are included in Left-Turn, if any.


Two-Hour Count Summaries

| Interval Start |  | Miles Ln |  |  |  | Miles Ln |  |  |  | Santa Clara St |  |  |  | Santa Clara St |  |  |  | 15-min Total | Rolling One Hour |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Eastbound |  |  |  | Westbound |  |  |  | Northbound |  |  |  | Southbound |  |  |  |  |  |
|  |  | UT | LT | TH | RT | UT | LT | TH | RT | UT | LT | TH | RT | UT | LT | TH | RT |  |  |
| 4:00 | PM | 0 | 1 | 1 | 0 | 0 | 0 | 3 | 7 | 0 | 0 | 2 | 1 | 0 | 16 | 5 | 1 | 37 | 0 |
| 4:15 | PM | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 7 | 0 | 0 | 2 | 0 | 0 | 12 | 2 | 1 | 26 | 0 |
| 4:30 | PM | 0 | 2 | 0 | 0 | 0 | 1 | 0 | 8 | 0 | 0 | 1 | 0 | 0 | 5 | 2 | 4 | 23 | 0 |
| 4:45 | PM | 0 | 2 | 1 | 0 | 0 | 1 | 1 | 8 | 0 | 1 | 5 | 1 | 0 | 16 | 2 | 4 | 42 | 128 |
| 5:00 | PM | 0 | 0 | 1 | 0 | 0 | 1 | 1 | 8 | 0 | 0 | 0 | 0 | 0 | 13 | 1 | 4 | 29 | 120 |
| 5:15 | PM | 0 | 0 | 1 | 0 | 1 | 0 | 2 | 10 | 0 | 0 | 1 | 3 | 0 | 12 | 1 | 0 | 31 | 125 |
| 5:30 | PM | 0 | 5 | 0 | 0 | 0 | 0 | 1 | 11 | 0 | 0 | 0 | 1 | 0 | 10 | 0 | 1 | 29 | 131 |
| 5:45 | PM | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 8 | 0 | 0 | 4 | 0 | 0 | 7 | 3 | 3 | 26 | 115 |
| Count | Total | 0 | 11 | 5 | 0 | 1 | 4 | 8 | 67 | 0 | 1 | 15 | 6 | 0 | 91 | 16 | 18 | 243 | 0 |
|  | All | 0 | 7 | 3 | 0 | 1 | 2 | 5 | 37 | 0 | 1 | 6 | 5 | 0 | 51 | 4 | 9 | 131 | 0 |
| Peak Hour | HV | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 3 | 0 |
|  | HV\% | - | 0\% | 0\% | - | 0\% | 0\% | 0\% | 5\% | - | 0\% | 0\% | 0\% | - | 2\% | 0\% | 0\% | 2\% | 0 |

Note: Two-hour count summary volumes include heavy vehicles but exclude bicycles in overall count.

| Interval Start | Heavy Vehicle Totals |  |  |  |  | Bicycles |  |  |  |  | Pedestrians (Crossing Leg) |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | EB | WB | NB | SB | Total | EB | WB | NB | SB | Total | East | West | North | South | Total |
| 4:00 PM | 1 | 1 | 0 | 1 | 3 | 0 | 0 | 0 | 1 | 1 | 0 | 1 | 0 | 0 | 1 |
| 4:15 PM | 0 | 1 | 1 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:45 PM | 0 | 1 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 |
| 5:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 3 | 4 | 0 | 1 | 8 |
| 5:30 PM | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 |
| 5:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 2 | 0 | 2 | 5 |
| Count Total | 1 | 4 | 1 | 2 | 8 | 0 | 0 | 0 | 2 | 2 | 5 | 8 | 0 | 3 | 16 |
| Peak Hour | 0 | 2 | 0 | 1 | 3 | 0 | 0 | 0 | 1 | 1 | 4 | 5 | 0 | 1 | 10 |

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Two-Hour Count Summaries - Heavy Vehicles

| Interval Start | Miles Ln |  |  |  | Miles Ln |  |  |  | Santa Clara St |  |  |  | Santa Clara St |  |  |  | $\begin{gathered} \text { 15-min } \\ \text { Total } \end{gathered}$ | Rolling One Hour |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Eastbound |  |  |  | Westbound |  |  |  | Northbound |  |  |  | Southbound |  |  |  |  |  |
|  | UT | LT | TH | RT | UT | LT | TH | RT | UT | LT | TH | RT | UT | LT | TH | RT |  |  |
| 4:00 PM | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 3 | 0 |
| 4:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 2 | 0 |
| 4:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 2 | 7 |
| 5:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 |
| 5:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| 5:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 3 |
| 5:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| Count Total | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 3 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 1 | 8 | 0 |
| Peak Hour | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 3 | 0 |

Two-Hour Count Summaries - Bikes

| Interval Start | Miles Ln |  |  | Miles Ln |  |  | Santa Clara St |  |  | Santa Clara St |  |  | $\begin{aligned} & \text { 15-min } \\ & \text { Total } \end{aligned}$ | Rolling One Hour |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Eastbound |  |  | Westbound |  |  | Northbound |  |  | Southbound |  |  |  |  |
|  | LT | TH | RT | LT | TH | RT | LT | TH | RT | LT | TH | RT |  |  |
| 4:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 |
| 4:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 5:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 1 |
| 5:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 5:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| Count Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 2 | 0 |
| Peak Hour | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |

Note: U-Turn volumes for bikes are included in Left-Turn, if any.


## Two-Hour Count Summaries

| Interval Start |  | Marin St |  |  |  | Marin St |  |  |  | Santa Clara St |  |  |  | Santa Clara St |  |  |  | 15-min Total | Rolling One Hour |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Eastbound |  |  |  | Westbound |  |  |  | Northbound |  |  |  | Southbound |  |  |  |  |  |
|  |  | UT | LT | TH | RT | UT | LT | TH | RT | UT | LT | TH | RT | UT | LT | TH | RT |  |  |
| 7:00 | AM | 0 | 0 | 6 | 2 | 0 | 0 | 20 | 6 | 0 | 6 | 2 | 1 | 0 | 9 | 0 | 0 | 52 | 0 |
| 7:15 | AM | 0 | 0 | 12 | 3 | 0 | 0 | 25 | 16 | 0 | 6 | 5 | 0 | 0 | 14 | 5 | 1 | 87 | 0 |
| 7:30 | AM | 0 | 4 | 18 | 3 | 0 | 0 | 27 | 18 | 0 | 7 | 11 | 2 | 0 | 34 | 8 | 2 | 134 | 0 |
| 7:45 | AM | 0 | 4 | 19 | 5 | 1 | 1 | 45 | 54 | 0 | 8 | 15 | 1 | 0 | 30 | 9 | 3 | 195 | 468 |
| 8:00 | AM | 0 | 3 | 15 | 4 | 0 | 0 | 41 | 24 | 0 | 6 | 8 | 0 | 0 | 22 | 6 | 2 | 131 | 547 |
| 8:15 | AM | 0 | 1 | 10 | 2 | 0 | 0 | 29 | 24 | 0 | 3 | 5 | 0 | 0 | 14 | 10 | 3 | 101 | 561 |
| 8:30 | AM | 0 | 2 | 15 | 2 | 1 | 0 | 20 | 15 | 0 | 3 | 4 | 0 | 0 | 18 | 7 | 0 | 87 | 514 |
| 8:45 | AM | 0 | 1 | 5 | 6 | 0 | 0 | 28 | 8 | 0 | 5 | 2 | 0 | 0 | 5 | 4 | 0 | 64 | 383 |
| Count | Total | 0 | 15 | 100 | 27 | 2 | 1 | 235 | 165 | 0 | 44 | 52 | 4 | 0 | 146 | 49 | 11 | 851 | 0 |
|  | All | 0 | 12 | 62 | 14 | 1 | 1 | 142 | 120 | 0 | 24 | 39 | 3 | 0 | 100 | 33 | 10 | 561 | 0 |
| Peak Hour | HV | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 1 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 5 | 0 |
|  | HV\% | - | 0\% | 0\% | 0\% | 0\% | 0\% | 1\% | 1\% | - | 0\% | 0\% | 33\% | - | 1\% | 0\% | 0\% | 1\% | 0 |

Note: Two-hour count summary volumes include heavy vehicles but exclude bicycles in overall count.

| Interval Start | Heavy Vehicle Totals |  |  |  |  | Bicycles |  |  |  |  | Pedestrians (Crossing Leg) |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | EB | WB | NB | SB | Total | EB | WB | NB | SB | Total | East | West | North | South | Total |
| 7:00 AM | 1 | 0 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 |
| 7:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 |
| 7:30 AM | 0 | 1 | 1 | 1 | 3 | 0 | 0 | 0 | 0 | 0 | 1 | 2 | 2 | 0 | 5 |
| 7:45 AM | 0 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 3 | 0 | 1 | 5 |
| 8:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 2 |
| 8:30 AM | 0 | 1 | 1 | 1 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 3 |
| 8:45 AM | 0 | 1 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 |
| Count Total | 1 | 5 | 2 | 4 | 12 | 0 | 0 | 0 | 0 | 0 | 3 | 10 | 4 | 1 | 18 |
| Peak Hour | 0 | 3 | 1 | 1 | 5 | 0 | 0 | 0 | 0 | 0 | 3 | 6 | 2 | 1 | 12 |

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Two-Hour Count Summaries - Heavy Vehicles

| Interval Start | Marin St |  |  |  | Marin St |  |  |  | Santa Clara St |  |  |  | Santa Clara St |  |  |  | $\begin{gathered} \text { 15-min } \\ \text { Total } \end{gathered}$ | Rolling One Hour |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Eastbound |  |  |  | Westbound |  |  |  | Northbound |  |  |  | Southbound |  |  |  |  |  |
|  | UT | LT | TH | RT | UT | LT | TH | RT | UT | LT | TH | RT | UT | LT | TH | RT |  |  |
| 7:00 AM | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 2 | 0 |
| 7:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 3 | 0 |
| 7:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 7 |
| 8:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 |
| 8:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 |
| 8:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 3 | 5 |
| 8:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 2 | 5 |
| Count Total | 0 | 0 | 1 | 0 | 0 | 0 | 4 | 1 | 0 | 0 | 1 | 1 | 0 | 3 | 1 | 0 | 12 | 0 |
| Peak Hour | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 1 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 5 | 0 |

Two-Hour Count Summaries - Bikes

| Interval Start | Marin St |  |  | Marin St |  |  | Santa Clara St |  |  | Santa Clara St |  |  | 15-min Total | Rolling One Hour |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Eastbound |  |  | Westbound |  |  | Northbound |  |  | Southbound |  |  |  |  |
|  | LT | TH | RT | LT | TH | RT | LT | TH | RT | LT | TH | RT |  |  |
| 7:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Count Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Peak Hour | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |

Note: U-Turn volumes for bikes are included in Left-Turn, if any.


Two-Hour Count Summaries

| Interval Start |  | Marin St |  |  |  | Marin St |  |  |  | Santa Clara St |  |  |  | Santa Clara St |  |  |  | 15-min Total | Rolling One Hour |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Eastbound |  |  |  | Westbound |  |  |  | Northbound |  |  |  | Southbound |  |  |  |  |  |
|  |  | UT | LT | TH | RT | UT | LT | TH | RT | UT | LT | TH | RT | UT | LT | TH | RT |  |  |
| 4:00 | PM | 0 | 2 | 29 | 11 | 0 | 2 | 19 | 12 | 0 | 3 | 6 | 1 | 0 | 12 | 12 | 2 | 111 | 0 |
| 4:15 | PM | 0 | 2 | 34 | 11 | 0 | 1 | 17 | 24 | 0 | 1 | 8 | 1 | 0 | 20 | 5 | 0 | 124 | 0 |
| 4:30 | PM | 0 | 2 | 25 | 6 | 0 | 0 | 18 | 16 | 0 | 9 | 3 | 1 | 0 | 11 | 6 | 3 | 100 | 0 |
| 4:45 | PM | 0 | 0 | 27 | 14 | 0 | 2 | 32 | 25 | 0 | 8 | 8 | 1 | 0 | 26 | 9 | 2 | 154 | 489 |
| 5:00 | PM | 0 | 2 | 31 | 5 | 0 | 0 | 25 | 22 | 0 | 6 | 1 | 2 | 0 | 29 | 12 | 2 | 137 | 515 |
| 5:15 | PM | 0 | 0 | 43 | 8 | 0 | 1 | 29 | 24 | 0 | 6 | 4 | 2 | 0 | 32 | 8 | 1 | 158 | 549 |
| 5:30 | PM | 0 | 1 | 31 | 3 | 0 | 0 | 29 | 15 | 0 | 8 | 6 | 0 | 0 | 13 | 7 | 2 | 115 | 564 |
| 5:45 | PM | 0 | 3 | 25 | 9 | 0 | 1 | 25 | 14 | 0 | 6 | 7 | 1 | 0 | 18 | 7 | 2 | 118 | 528 |
| Count | Total | 0 | 12 | 245 | 67 | 0 | 7 | 194 | 152 | 0 | 47 | 43 | 9 | 0 | 161 | 66 | 14 | 1,017 | 0 |
|  | All | 0 | 3 | 132 | 30 | 0 | 3 | 115 | 86 | 0 | 28 | 19 | 5 | 0 | 100 | 36 | 7 | 564 | 0 |
| Peak <br> Hour | HV | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 2 | 0 |
|  | HV\% | - | 0\% | 1\% | 0\% | - | 0\% | 0\% | 0\% | - | 0\% | 0\% | 0\% | - | 1\% | 0\% | 0\% | 0\% | 0 |

Note: Two-hour count summary volumes include heavy vehicles but exclude bicycles in overall count.

| Interval Start | Heavy Vehicle Totals |  |  |  |  | Bicycles |  |  |  |  | Pedestrians (Crossing Leg) |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | EB | WB | NB | SB | Total | EB | WB | NB | SB | Total | East | West | North | South | Total |
| 4:00 PM | 0 | 1 | 0 | 1 | 2 | 1 | 1 | 0 | 0 | 2 | 1 | 2 | 2 | 0 | 5 |
| 4:15 PM | 0 | 0 | 2 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 0 | 4 |
| 4:30 PM | 0 | 0 | 1 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 1 | 3 | 2 | 2 | 8 |
| 4:45 PM | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 0 | 4 |
| 5:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 3 | 1 | 7 |
| 5:15 PM | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 2 |
| 5:45 PM | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 4 |
| Count Total | 1 | 1 | 4 | 3 | 9 | 1 | 1 | 0 | 0 | 2 | 6 | 14 | 7 | 7 | 34 |
| Peak Hour | 1 | 0 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 2 | 7 | 3 | 1 | 13 |

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Two-Hour Count Summaries - Heavy Vehicles

| Interval Start | Marin St |  |  |  | Marin St |  |  |  | Santa Clara St |  |  |  | Santa Clara St |  |  |  | $\begin{gathered} \text { 15-min } \\ \text { Total } \end{gathered}$ | Rolling One Hour |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Eastbound |  |  |  | Westbound |  |  |  | Northbound |  |  |  | Southbound |  |  |  |  |  |
|  | UT | LT | TH | RT | UT | LT | TH | RT | UT | LT | TH | RT | UT | LT | TH | RT |  |  |
| 4:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 2 | 0 |
| 4:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 2 | 0 |
| 4:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 2 | 0 |
| 4:45 PM | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 7 |
| 5:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 |
| 5:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 4 |
| 5:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| 5:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 2 |
| Count Total | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 1 | 2 | 0 | 1 | 2 | 0 | 9 | 0 |
| Peak Hour | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 2 | 0 |

Two-Hour Count Summaries - Bikes

| Interval Start | Marin St |  |  | Marin St |  |  | Santa Clara St |  |  | Santa Clara St |  |  | 15-min Total | Rolling One Hour |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Eastbound |  |  | Westbound |  |  | Northbound |  |  | Southbound |  |  |  |  |
|  | LT | TH | RT | LT | TH | RT | LT | TH | RT | LT | TH | RT |  |  |
| 4:00 PM | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 |
| 4:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| 5:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Count Total | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 |
| Peak Hour | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |

Note: U-Turn volumes for bikes are included in Left-Turn, if any.


Note: Two-hour count summary volumes include heavy vehicles but exclude bicycles in overall count.

| Interval Start | Heavy Vehicle Totals |  |  |  |  | Bicycles |  |  |  |  | Pedestrians (Crossing Leg) |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | EB | WB | NB | SB | Total | EB | WB | NB | SB | Total | East | West | North | South | Total |
| 7:00 AM | 0 | 0 | 1 | 2 | 3 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 |
| 7:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:30 AM | 0 | 1 | 0 | 2 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 1 | 0 | 6 |
| 7:45 AM | 0 | 1 | 1 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 1 | 7 | 1 | 2 | 11 |
| 8:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 1 | 2 | 0 | 8 |
| 8:15 AM | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 |
| 8:30 AM | 0 | 1 | 0 | 1 | 2 | 0 | 0 | 0 | 1 | 1 | 0 | 5 | 0 | 0 | 5 |
| 8:45 AM | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 0 | 0 | 4 |
| Count Total | 0 | 3 | 4 | 5 | 12 | 0 | 0 | 0 | 1 | 1 | 11 | 19 | 4 | 2 | 36 |
| Peak Hour | 0 | 2 | 2 | 2 | 6 | 0 | 0 | 0 | 0 | 0 | 6 | 14 | 4 | 2 | 26 |

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Two-Hour Count Summaries - Heavy Vehicles

| Interval Start | Driveway |  |  |  | Marin St |  |  |  | Auto Center Dr |  |  |  | Auto Center Dr |  |  |  | 15-min Total | Rolling One Hour |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Eastbound |  |  |  | Westbound |  |  |  | Northbound |  |  |  | Southbound |  |  |  |  |  |
|  | UT | LT | TH | RT | UT | LT | TH | RT | UT | LT | TH | RT | UT | LT | TH | RT |  |  |
| 7:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 1 | 0 | 3 | 0 |
| 7:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:30 AM | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 3 | 0 |
| 7:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 2 | 8 |
| 8:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 |
| 8:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 6 |
| 8:30 AM | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 2 | 5 |
| 8:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 4 |
| Count Total | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 1 | 0 | 0 | 4 | 0 | 0 | 1 | 4 | 0 | 12 | 0 |
| Peak Hour | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 2 | 0 | 0 | 0 | 2 | 0 | 6 | 0 |

Two-Hour Count Summaries - Bikes

| Interval Start | Driveway |  |  | Marin St |  |  | Auto Center Dr |  |  | Auto Center Dr |  |  | 15-min Total | Rolling One Hour |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Eastbound |  |  | Westbound |  |  | Northbound |  |  | Southbound |  |  |  |  |
|  | LT | TH | RT | LT | TH | RT | LT | TH | RT | LT | TH | RT |  |  |
| 7:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 1 |
| 8:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| Count Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 |
| Peak Hour | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |

Note: U-Turn volumes for bikes are included in Left-Turn, if any.


Note: Two-hour count summary volumes include heavy vehicles but exclude bicycles in overall count.

| Interval Start | Heavy Vehicle Totals |  |  |  |  | Bicycles |  |  |  |  | Pedestrians (Crossing Leg) |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | EB | WB | NB | SB | Total | EB | WB | NB | SB | Total | East | West | North | South | Total |
| 4:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 3 | 2 | 0 | 5 |
| 4:15 PM | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 6 | 4 | 0 | 0 | 10 |
| 4:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 1 | 0 | 5 |
| 4:45 PM | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 1 | 0 | 1 | 0 | 4 | 0 | 0 | 4 |
| 5:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 2 |
| 5:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 3 | 0 | 0 | 4 |
| 5:30 PM | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 2 |
| 5:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Count Total | 0 | 1 | 2 | 0 | 3 | 0 | 0 | 2 | 0 | 2 | 8 | 21 | 3 | 0 | 32 |
| Peak Hour | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 1 | 0 | 1 | 1 | 13 | 1 | 0 | 15 |

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Two-Hour Count Summaries - Heavy Vehicles

| Interval Start | Driveway |  |  |  | Marin St |  |  |  | Auto Center Dr |  |  |  | Auto Center Dr |  |  |  | $\begin{aligned} & \text { 15-min } \\ & \text { Total } \end{aligned}$ | Rolling One Hour |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Eastbound |  |  |  | Westbound |  |  |  | Northbound |  |  |  | Southbound |  |  |  |  |  |
|  | UT | LT | TH | RT | UT | LT | TH | RT | UT | LT | TH | RT | UT | LT | TH | RT |  |  |
| 4:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:15 PM | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 |
| 4:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 2 |
| 5:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| 5:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 5:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 2 |
| 5:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| Count Total | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 3 | 0 |
| Peak Hour | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 0 |

Two-Hour Count Summaries - Bikes

| Interval Start | Driveway |  |  | Marin St |  |  | Auto Center Dr |  |  | Auto Center Dr |  |  | 15-min Total | Rolling One Hour |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Eastbound |  |  | Westbound |  |  | Northbound |  |  | Southbound |  |  |  |  |
|  | LT | TH | RT | LT | TH | RT | LT | TH | RT | LT | TH | RT |  |  |
| 4:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 0 |
| 4:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 2 |
| 5:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 5:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 5:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 5:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Count Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 2 | 0 |
| Peak Hour | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 0 |

Note: U-Turn volumes for bikes are included in Left-Turn, if any.

# APPENDIX B: EXISTING (2018) TRAFFIC CONDITIONS ANALYSIS SHEETS 




| Intersection |  |  |
| :--- | ---: | :--- |
| Intersection Delay, s/veh | 7.1 | A |
| Intersection LOS | A |  |


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations |  | \$ |  |  | $\ddagger$ |  |  | \$ |  |  | \$ |  |
| Traffic Vol, veh/h | 8 | 1 | 0 | 1 | 0 | 41 | 0 | 4 | 4 | 37 | 3 | 3 |
| Future Vol, veh/h | 8 | 1 | 0 | 1 | 0 | 41 | 0 | 4 | 4 | 37 | 3 | 3 |
| Peak Hour Factor | 0.82 | 0.82 | 0.82 | 0.82 | 0.82 | 0.82 | 0.82 | 0.82 | 0.82 | 0.82 | 0.82 | 0.82 |
| Heavy Vehicles, \% | 0 | 0 | 0 | 2 | 2 | 2 | 0 | 0 | 0 | 0 | 0 | 0 |
| Mvmt Flow | 10 | 1 | 0 | 1 | 0 | 50 | 0 | 5 | 5 | 45 | 4 | 4 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | EB |  |  | WB |  |  |  | NB |  | SB |  |  |
| Opposing Approach | WB |  |  | EB |  |  |  | SB |  | NB |  |  |
| Opposing Lanes | 1 |  |  | 1 |  |  |  | 1 |  | 1 |  |  |
| Conflicting Approach Left | SB |  |  | NB |  |  |  | EB |  | WB |  |  |
| Conflicting Lanes Left | 1 |  |  | 1 |  |  |  | 1 |  | 1 |  |  |
| Conflicting Approach Right | NB |  |  | SB |  |  |  | WB |  | EB |  |  |
| Conflicting Lanes Right | 1 |  |  | 1 |  |  |  | 1 |  | 1 |  |  |
| HCM Control Delay | 7.3 |  |  | 6.7 |  |  |  | 6.8 |  | 7.4 |  |  |
| HCM LOS | A |  |  | A |  |  |  | A |  | A |  |  |


| Lane | NBLn1 | EBLn1 | WBLn1 | SBLn1 |
| :--- | ---: | ---: | ---: | ---: |
| Vol Left, \% | $0 \%$ | $89 \%$ | $2 \%$ | $86 \%$ |
| Vol Thru, \% | $50 \%$ | $11 \%$ | $0 \%$ | $7 \%$ |
| Vol Right, \% | $50 \%$ | $0 \%$ | $98 \%$ | $7 \%$ |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 8 | 9 | 42 | 43 |
| LT Vol | 0 | 8 | 1 | 37 |
| Through Vol | 4 | 1 | 0 | 3 |
| RT Vol | 4 | 0 | 41 | 3 |
| Lane Flow Rate | 10 | 11 | 51 | 52 |
| Geometry Grp | 1 | 1 | 1 | 1 |
| Degree of Util (X) | 0.01 | 0.013 | 0.049 | 0.06 |
| Departure Headway (Hd) | 3.749 | 4.227 | 3.471 | 4.148 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 955 | 846 | 1030 | 866 |
| Service Time | 1.772 | 2.257 | 1.5 | 2.16 |
| HCM Lane VIC Ratio | 0.01 | 0.013 | 0.05 | 0.06 |
| HCM Control Delay | 6.8 | 7.3 | 6.7 | 7.4 |
| HCM Lane LOS | A | A | A | A |
| HCM 95th-tile Q | 0 | 0 | 0.2 | 0.2 |


| Intersection |
| :--- |
| Intersection Delay, s/veh10.7 |
| Intersection LOS $\quad$ B |



| Lane | NBLn1 EBLn1WBLn1 SBLn1 |  |  |  |
| :--- | ---: | ---: | ---: | ---: |
| Vol Left, \% | $36 \%$ | $14 \%$ | $1 \%$ | $70 \%$ |
| Vol Thru, \% | $59 \%$ | $70 \%$ | $54 \%$ | $23 \%$ |
| Vol Right, \% | $5 \%$ | $16 \%$ | $45 \%$ | $7 \%$ |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 66 | 88 | 264 | 143 |
| LT Vol | 24 | 12 | 2 | 100 |
| Through Vol | 39 | 62 | 142 | 33 |
| RT Vol | 3 | 14 | 120 | 10 |
| Lane Flow Rate | 92 | 122 | 367 | 199 |
| Geometry Grp | 1 | 1 | 1 | 1 |
| Degree of Util (X) | 0.141 | 0.175 | 0.465 | 0.297 |
| Departure Headway (Hd) | 5.518 | 5.143 | 4.566 | 5.375 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 652 | 700 | 777 | 671 |
| Service Time | 3.532 | 3.155 | 2.659 | 3.382 |
| HCM Lane V/C Ratio | 0.141 | 0.174 | 0.472 | 0.297 |
| HCM Control Delay | 9.4 | 9.2 | 11.6 | 10.6 |
| HCM Lane LOS | A | A | B | B |
| HCM 95th-tile Q | 0.5 | 0.6 | 2.5 | 1.2 |






| Intersection |  |
| :--- | ---: | :--- |
| Intersection Delay, s/veh | 7.3 |
| Intersection LOS | A |


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations |  | \$ |  |  | $\ddagger$ |  |  | \$ |  |  | \& |  |
| Traffic Vol, veh/h | 7 | 3 | 0 | 3 | 5 | 37 | 1 | 6 | 5 | 51 | 4 | 9 |
| Future Vol, veh/h | 7 | 3 | 0 | 3 | 5 | 37 | 1 | 6 | 5 | 51 | 4 | 9 |
| Peak Hour Factor | 0.78 | 0.78 | 0.78 | 0.78 | 0.78 | 0.78 | 0.78 | 0.78 | 0.78 | 0.78 | 0.78 | 0.78 |
| Heavy Vehicles, \% | 0 | 0 | 0 | 4 | 4 | 4 | 0 | 0 | 0 | 2 | 2 | 2 |
| Mvmt Flow | 9 | 4 | 0 | 4 | 6 | 47 | 1 | 8 | 6 | 65 | 5 | 12 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
| Opposing Approach | WB |  |  | EB |  |  | SB |  |  | NB |  |  |
| Opposing Lanes | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| Conflicting Approach Left | SB |  |  | NB |  |  | EB |  |  | WB |  |  |
| Conflicting Lanes Left | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| Conflicting Approach Right | NB |  |  | SB |  |  | WB |  |  | EB |  |  |
| Conflicting Lanes Right | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| HCM Control Delay | 7.4 |  |  | 6.9 |  |  | 7 |  |  | 7.6 |  |  |
| HCM LOS | A |  |  | A |  |  | A |  |  | A |  |  |


| Lane | NBLn1 | EBLn1 | WBLn1 | SBLn1 |
| :--- | ---: | ---: | ---: | ---: |
| Vol Left, \% | $8 \%$ | $70 \%$ | $7 \%$ | $80 \%$ |
| Vol Thru, \% | $50 \%$ | $30 \%$ | $11 \%$ | $6 \%$ |
| Vol Right, \% | $42 \%$ | $0 \%$ | $82 \%$ | $14 \%$ |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 12 | 10 | 45 | 64 |
| LT Vol | 1 | 7 | 3 | 51 |
| Through Vol | 6 | 3 | 5 | 4 |
| RT Vol | 5 | 0 | 37 | 9 |
| Lane Flow Rate | 15 | 13 | 58 | 82 |
| Geometry Grp | 1 | 1 | 1 | 1 |
| Degree of Util (X) | 0.016 | 0.015 | 0.059 | 0.094 |
| Departure Headway (Hd) | 3.85 | 4.255 | 3.667 | 4.142 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 925 | 836 | 970 | 865 |
| Service Time | 1.892 | 2.307 | 1.715 | 2.167 |
| HCM Lane VIC Ratio | 0.016 | 0.016 | 0.06 | 0.095 |
| HCM Control Delay | 7 | 7.4 | 6.9 | 7.6 |
| HCM Lane LOS | A | A | A | A |
| HCM 95th-tile Q | 0 | 0 | 0.2 | 0.3 |

## Intersection

Intersection Delay, s/veh 9.2
Intersection LOS
A


| Lane | NBLn1 EBLn1WBLn1 SBLn1 |  |  |  |
| :--- | ---: | ---: | ---: | ---: |
| Vol Left, \% | $54 \%$ | $2 \%$ | $1 \%$ | $70 \%$ |
| Vol Thru, $\%$ | $37 \%$ | $80 \%$ | $56 \%$ | $25 \%$ |
| Vol Right, $\%$ | $10 \%$ | $18 \%$ | $42 \%$ | $5 \%$ |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 52 | 165 | 204 | 143 |
| LT Vol | 28 | 3 | 3 | 100 |
| Through Vol | 19 | 132 | 115 | 36 |
| RT Vol | 5 | 30 | 86 | 7 |
| Lane Flow Rate | 58 | 185 | 229 | 161 |
| Geometry Grp | 1 | 1 | 1 | 1 |
| Degree of Util (X) | 0.083 | 0.238 | 0.282 | 0.225 |
| Departure Headway (Hd) | 5.107 | 4.629 | 4.427 | 5.036 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 696 | 773 | 809 | 709 |
| Service Time | 3.176 | 2.679 | 2.473 | 3.095 |
| HCM Lane V/C Ratio | 0.083 | 0.239 | 0.283 | 0.227 |
| HCM Control Delay | 8.6 | 9.1 | 9.2 | 9.6 |
| HCM Lane LOS | A | A | A | A |
| HCM 95th-tile Q | 0.3 | 0.9 | 1.2 | 0.9 |




## APPENDIX C: EXISTING (2018) PLUS PROJECT TRAFFIC CONDITIONS ANALYSIS

 SHEETS


| Intersection |  |
| :--- | ---: |
| Intersection Delay, s/veh $\quad 7.1$ |  |
| Intersection LOS | A |


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations |  | $\uparrow$ |  |  | ¢ |  |  | \$ |  |  | ${ }_{*}$ |  |
| Traffic Vol, veh/h | 8 | 1 | 0 | 1 | 0 | 51 | 0 | 4 | 4 | 43 | 3 | 3 |
| Future Vol, veh/h | 8 | 1 | 0 | 1 | 0 | 51 | 0 | 4 | 4 | 43 | 3 | 3 |
| Peak Hour Factor | 0.82 | 0.82 | 0.82 | 0.82 | 0.82 | 0.82 | 0.82 | 0.82 | 0.82 | 0.82 | 0.82 | 0.82 |
| Heavy Vehicles, \% | 0 | 0 | 0 | 2 | 2 | 2 | 0 | 0 | 0 | 0 | 0 | 0 |
| Mvmt Flow | 10 | 1 | 0 | 1 | 0 | 62 | 0 | 5 | 5 | 52 | 4 | 4 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | EB |  |  | WB |  |  |  | NB |  | SB |  |  |
| Opposing Approach | WB |  |  | EB |  |  |  | SB |  | NB |  |  |
| Opposing Lanes | 1 |  |  | 1 |  |  |  | 1 |  | 1 |  |  |
| Conflicting Approach Left | SB |  |  | NB |  |  |  | EB |  | WB |  |  |
| Conflicting Lanes Left | 1 |  |  | 1 |  |  |  | 1 |  | 1 |  |  |
| Conflicting Approach Right | NB |  |  | SB |  |  |  | WB |  | EB |  |  |
| Conflicting Lanes Right | 1 |  |  | 1 |  |  |  | 1 |  | 1 |  |  |
| HCM Control Delay | 7.3 |  |  | 6.7 |  |  |  | 6.8 |  | 7.5 |  |  |
| HCM LOS | A |  |  | A |  |  |  | A |  | A |  |  |


| Lane | NBLn1 | EBLn1 | WBLn1 | SBLn1 |
| :--- | ---: | ---: | ---: | ---: |
| Vol Left, \% | $0 \%$ | $89 \%$ | $2 \%$ | $88 \%$ |
| Vol Thru, \% | $50 \%$ | $11 \%$ | $0 \%$ | $6 \%$ |
| Vol Right, \% | $50 \%$ | $0 \%$ | $98 \%$ | $6 \%$ |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 8 | 9 | 52 | 49 |
| LT Vol | 0 | 8 | 1 | 43 |
| Through Vol | 4 | 1 | 0 | 3 |
| RT Vol | 4 | 0 | 51 | 3 |
| Lane Flow Rate | 10 | 11 | 63 | 60 |
| Geometry Grp | 1 | 1 | 1 | 1 |
| Degree of Util (X) | 0.01 | 0.013 | 0.061 | 0.069 |
| Departure Headway (Hd) | 3.774 | 4.247 | 3.479 | 4.176 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 947 | 880 | 1025 | 860 |
| Service Time | 1.804 | 2.285 | 1.514 | 2.192 |
| HCM Lane V/C Ratio | 0.011 | 0.013 | 0.061 | 0.07 |
| HCM Control Delay | 6.8 | 7.3 | 6.7 | 7.5 |
| HCM Lane LOS | A | A | A | A |
| HCM 95th-tile Q | 0 | 0 | 0.2 | 0.2 |

Intersection
Intersection Delay, s/veh 11
Intersection LOS $\quad$ B

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations |  | $\uparrow$ |  |  | * |  |  | ¢ |  |  | ¢ |  |
| Traffic Vol, veh/h | 12 | 62 | 20 | 2 | 142 | 120 | 31 | 40 | 5 | 100 | 33 | 10 |
| Future Vol, veh/h | 12 | 62 | 20 | 2 | 142 | 120 | 31 | 40 | 5 | 100 | 33 | 10 |
| Peak Hour Factor | 0.72 | 0.72 | 0.72 | 0.72 | 0.72 | 0.72 | 0.72 | 0.72 | 0.72 | 0.72 | 0.72 | 0.72 |
| Heavy Vehicles, \% | 0 | 0 | 0 | 1 | 1 | 1 | 2 | 2 | 2 | 1 | 1 | 1 |
| Mvmt Flow | 17 | 86 | 28 | 3 | 197 | 167 | 43 | 56 | 7 | 139 | 46 | 14 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
| Opposing Approach | WB |  |  | EB |  |  | SB |  |  | NB |  |  |
| Opposing Lanes |  |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| Conflicting Approach L | ft SB |  |  | NB |  |  | EB |  |  | WB |  |  |
| Conflicting Lanes Left | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| Conflicting Approach R | ghNB |  |  | SB |  |  | WB |  |  | EB |  |  |
| Conflicting Lanes Righ | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| HCM Control Delay | 9.4 |  |  | 12 |  |  | 9.7 |  |  | 10.8 |  |  |
| HCM LOS | A |  |  | B |  |  | A |  |  | B |  |  |


| Lane | NBLn1 EBLn1WBLn1 SBLn1 |  |  |  |
| :--- | ---: | ---: | ---: | ---: |
| Vol Left, \% | $41 \%$ | $13 \%$ | $1 \%$ | $70 \%$ |
| Vol Thru, \% | $53 \%$ | $66 \%$ | $54 \%$ | $23 \%$ |
| Vol Right, \% | $7 \%$ | $21 \%$ | $45 \%$ | $7 \%$ |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 76 | 94 | 264 | 143 |
| LT Vol | 31 | 12 | 2 | 100 |
| Through Vol | 40 | 62 | 142 | 33 |
| RT Vol | 5 | 20 | 120 | 10 |
| Lane Flow Rate | 106 | 131 | 367 | 199 |
| Geometry Grp | 1 | 1 | 1 | 1 |
| Degree of Util (X) | 0.163 | 0.187 | 0.48 | 0.299 |
| Departure Headway (Hd) | 5.551 | 5.157 | 4.717 | 5.428 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 646 | 696 | 770 | 663 |
| Service Time | 3.584 | 3.187 | 2.717 | 3.459 |
| HCM Lane V/C Ratio | 0.164 | 0.188 | 0.477 | 0.3 |
| HCM Control Delay | 9.7 | 9.4 | 12 | 10.8 |
| HCM Lane LOS | A | A | B | B |
| HCM 95th-tile Q | 0.6 | 0.7 | 2.6 | 1.3 |






| Intersection |  |
| :--- | ---: |
| Intersection Delay, s/veh | 7.4 |
| Intersection LOS | A |


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations |  | $\uparrow$ |  |  | ¢ |  |  | ¢ |  |  | \$ |  |
| Traffic Vol, veh/h | 7 | 3 | 0 | 3 | 5 | 50 | 1 | 6 | 5 | 60 | 4 | 9 |
| Future Vol, veh/h | 7 | 3 | 0 | 3 | 5 | 50 | 1 | 6 | 5 | 60 | 4 | 9 |
| Peak Hour Factor | 0.78 | 0.78 | 0.78 | 0.78 | 0.78 | 0.78 | 0.78 | 0.78 | 0.78 | 0.78 | 0.78 | 0.78 |
| Heavy Vehicles, \% | 0 | 0 | 0 | 4 | 4 | 4 | 0 | 0 | 0 | 2 | 2 | 2 |
| Mvmt Flow | 9 | 4 | 0 | 4 | 6 | 64 | 1 | 8 | 6 | 77 | 5 | 12 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
| Opposing Approach | WB |  |  | EB |  |  | SB |  |  | NB |  |  |
| Opposing Lanes | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| Conflicting Approach Left | SB |  |  | NB |  |  | EB |  |  | WB |  |  |
| Conflicting Lanes Left | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| Conflicting Approach Right | NB |  |  | SB |  |  | WB |  |  | EB |  |  |
| Conflicting Lanes Right | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| HCM Control Delay | 7.4 |  |  | 7 |  |  | 7 |  |  | 7.7 |  |  |
| HCM LOS | A |  |  | A |  |  | A |  |  | A |  |  |


| Lane | NBLn1 | EBLn1 | WBLn1 | SBLn1 |
| :--- | ---: | ---: | ---: | ---: |
| Vol Left, \% | $8 \%$ | $70 \%$ | $5 \%$ | $82 \%$ |
| Vol Thru, \% | $50 \%$ | $30 \%$ | $9 \%$ | $5 \%$ |
| Vol Right, \% | $42 \%$ | $0 \%$ | $86 \%$ | $12 \%$ |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 12 | 10 | 58 | 73 |
| LT Vol | 1 | 7 | 3 | 60 |
| Through Vol | 6 | 3 | 5 | 4 |
| RT Vol | 5 | 0 | 50 | 9 |
| Lane Flow Rate | 15 | 13 | 74 | 94 |
| Geometry Grp | 1 | 1 | 1 | 1 |
| Degree of Util (X) | 0.017 | 0.015 | 0.076 | 0.109 |
| Departure Headway (Hd) | 3.889 | 4.287 | 3.659 | 4.187 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 914 | 827 | 969 | 855 |
| Service Time | 1.939 | 2.354 | 1.719 | 2.217 |
| HCM Lane V/C Ratio | 0.016 | 0.016 | 0.076 | 0.11 |
| HCM Control Delay | 7 | 7.4 | 7 | 7.7 |
| HCM Lane LOS | A | A | A | A |
| HCM 95th-tile Q | 0.1 | 0 | 0.2 | 0.4 |

```
Intersection
Intersection Delay, s/veh 9.3
Intersection LOS
A
```



| Lane | NBLn1 EBLn1WBLn1 SBLn1 |  |  |  |
| :--- | ---: | ---: | ---: | ---: |
| Vol Left, \% | $60 \%$ | $2 \%$ | $1 \%$ | $70 \%$ |
| Vol Thru, \% | $31 \%$ | $76 \%$ | $56 \%$ | $25 \%$ |
| Vol Right, \% | $9 \%$ | $22 \%$ | $42 \%$ | $5 \%$ |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 65 | 174 | 204 | 143 |
| LT Vol | 39 | 3 | 3 | 100 |
| Through Vol | 20 | 132 | 115 | 36 |
| RT Vol | 6 | 39 | 86 | 7 |
| Lane Flow Rate | 73 | 196 | 229 | 161 |
| Geometry Grp | 1 | 1 | 1 | 1 |
| Degree of Util (X) | 0.105 | 0.252 | 0.285 | 0.227 |
| Departure Headway (Hd) | 5.153 | 4.649 | 4.482 | 5.086 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 690 | 768 | 798 | 701 |
| Service Time | 3.226 | 2.704 | 2.534 | 3.151 |
| HCM Lane V/C Ratio | 0.106 | 0.255 | 0.287 | 0.23 |
| HCM Control Delay | 8.8 | 9.3 | 9.3 | 9.7 |
| HCM Lane LOS | A | A | A | A |
| HCM 95th-tile Q | 0.4 | 1 | 1.2 | 0.9 |




APPENDIX D: NEAR TERM (2021) TRAFFIC CONDITIONS ANALYSIS SHEETS



| Intersection |  |  |
| :--- | ---: | :--- |
| Intersection Delay, s/veh | 7.1 | A |
| Intersection LOS | A |  |


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations |  | \$ |  |  | $\ddagger$ |  |  | \$ |  |  | \$ |  |
| Traffic Vol, veh/h | 8 | 1 | 0 | 1 | 0 | 41 | 0 | 4 | 4 | 37 | 3 | 3 |
| Future Vol, veh/h | 8 | 1 | 0 | 1 | 0 | 41 | 0 | 4 | 4 | 37 | 3 | 3 |
| Peak Hour Factor | 0.82 | 0.82 | 0.82 | 0.82 | 0.82 | 0.82 | 0.82 | 0.82 | 0.82 | 0.82 | 0.82 | 0.82 |
| Heavy Vehicles, \% | 0 | 0 | 0 | 2 | 2 | 2 | 0 | 0 | 0 | 0 | 0 | 0 |
| Mvmt Flow | 10 | 1 | 0 | 1 | 0 | 50 | 0 | 5 | 5 | 45 | 4 | 4 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | EB |  |  | WB |  |  |  | NB |  | SB |  |  |
| Opposing Approach | WB |  |  | EB |  |  |  | SB |  | NB |  |  |
| Opposing Lanes | 1 |  |  | 1 |  |  |  | 1 |  | 1 |  |  |
| Conflicting Approach Left | SB |  |  | NB |  |  |  | EB |  | WB |  |  |
| Conflicting Lanes Left | 1 |  |  | 1 |  |  |  | 1 |  | 1 |  |  |
| Conflicting Approach Right | NB |  |  | SB |  |  |  | WB |  | EB |  |  |
| Conflicting Lanes Right | 1 |  |  | 1 |  |  |  | 1 |  | 1 |  |  |
| HCM Control Delay | 7.3 |  |  | 6.7 |  |  |  | 6.8 |  | 7.4 |  |  |
| HCM LOS | A |  |  | A |  |  |  | A |  | A |  |  |


| Lane | NBLn1 | EBLn1 | WBLn1 | SBLn1 |
| :--- | ---: | ---: | ---: | ---: |
| Vol Left, \% | $0 \%$ | $89 \%$ | $2 \%$ | $86 \%$ |
| Vol Thru, \% | $50 \%$ | $11 \%$ | $0 \%$ | $7 \%$ |
| Vol Right, \% | $50 \%$ | $0 \%$ | $98 \%$ | $7 \%$ |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 8 | 9 | 42 | 43 |
| LT Vol | 0 | 8 | 1 | 37 |
| Through Vol | 4 | 1 | 0 | 3 |
| RT Vol | 4 | 0 | 41 | 3 |
| Lane Flow Rate | 10 | 11 | 51 | 52 |
| Geometry Grp | 1 | 1 | 1 | 1 |
| Degree of Util (X) | 0.01 | 0.013 | 0.049 | 0.06 |
| Departure Headway (Hd) | 3.749 | 4.227 | 3.471 | 4.148 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 955 | 846 | 1030 | 866 |
| Service Time | 1.772 | 2.257 | 1.5 | 2.16 |
| HCM Lane VIC Ratio | 0.01 | 0.013 | 0.05 | 0.06 |
| HCM Control Delay | 6.8 | 7.3 | 6.7 | 7.4 |
| HCM Lane LOS | A | A | A | A |
| HCM 95th-tile Q | 0 | 0 | 0.2 | 0.2 |


| Intersection |
| :--- |
| Intersection Delay, s/veh10.8 |
| Intersection LOS $\quad$ B |



| Lane | NBLn1 EBLn1WBLn1 SBLn1 |  |  |  |
| :--- | ---: | ---: | ---: | ---: |
| Vol Left, \% | $36 \%$ | $13 \%$ | $1 \%$ | $70 \%$ |
| Vol Thru, \% | $59 \%$ | $71 \%$ | $54 \%$ | $23 \%$ |
| Vol Right, \% | $5 \%$ | $16 \%$ | $45 \%$ | $7 \%$ |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 66 | 89 | 266 | 144 |
| LT Vol | 24 | 12 | 2 | 101 |
| Through Vol | 39 | 63 | 143 | 33 |
| RT Vol | 3 | 14 | 121 | 10 |
| Lane Flow Rate | 92 | 124 | 369 | 200 |
| Geometry Grp | 1 | 1 | 1 | 1 |
| Degree of Util (X) | 0.141 | 0.177 | 0.469 | 0.299 |
| Departure Headway (Hd) | 5.532 | 5.165 | 4.571 | 5.384 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 650 | 698 | 776 | 670 |
| Service Time | 3.547 | 3.165 | 2.665 | 3.394 |
| HCM Lane V/C Ratio | 0.142 | 0.178 | 0.476 | 0.299 |
| HCM Control Delay | 9.5 | 9.3 | 11.7 | 10.7 |
| HCM Lane LOS | A | A | B | B |
| HCM 95th-tile Q | 0.5 | 0.6 | 2.5 | 1.3 |






| Intersection |  |
| :--- | ---: | :--- |
| Intersection Delay, s/veh | 7.3 |
| Intersection LOS | A |


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations |  | \$ |  |  | $\ddagger$ |  |  | \$ |  |  | \& |  |
| Traffic Vol, veh/h | 7 | 3 | 0 | 3 | 5 | 37 | 1 | 6 | 5 | 52 | 4 | 9 |
| Future Vol, veh/h | 7 | 3 | 0 | 3 | 5 | 37 | 1 | 6 | 5 | 52 | 4 | 9 |
| Peak Hour Factor | 0.78 | 0.78 | 0.78 | 0.78 | 0.78 | 0.78 | 0.78 | 0.78 | 0.78 | 0.78 | 0.78 | 0.78 |
| Heavy Vehicles, \% | 0 | 0 | 0 | 4 | 4 | 4 | 0 | 0 | 0 | 2 | 2 | 2 |
| Mvmt Flow | 9 | 4 | 0 | 4 | 6 | 47 | 1 | 8 | 6 | 67 | 5 | 12 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
| Opposing Approach | WB |  |  | EB |  |  | SB |  |  | NB |  |  |
| Opposing Lanes | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| Conflicting Approach Left | SB |  |  | NB |  |  | EB |  |  | WB |  |  |
| Conflicting Lanes Left | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| Conflicting Approach Right | NB |  |  | SB |  |  | WB |  |  | EB |  |  |
| Conflicting Lanes Right | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| HCM Control Delay | 7.4 |  |  | 7 |  |  | 7 |  |  | 7.6 |  |  |
| HCM LOS | A |  |  | A |  |  | A |  |  | A |  |  |


| Lane | NBLn1 | EBLn1 | WBLn1 | SBLn1 |
| :--- | ---: | ---: | ---: | ---: |
| Vol Left, \% | $8 \%$ | $70 \%$ | $7 \%$ | $80 \%$ |
| Vol Thru, \% | $50 \%$ | $30 \%$ | $11 \%$ | $6 \%$ |
| Vol Right, \% | $42 \%$ | $0 \%$ | $82 \%$ | $14 \%$ |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 12 | 10 | 45 | 65 |
| LT Vol | 1 | 7 | 3 | 52 |
| Through Vol | 6 | 3 | 5 | 4 |
| RT Vol | 5 | 0 | 37 | 9 |
| Lane Flow Rate | 15 | 13 | 58 | 83 |
| Geometry Grp | 1 | 1 | 1 | 1 |
| Degree of Util (X) | 0.016 | 0.015 | 0.059 | 0.096 |
| Departure Headway (Hd) | 3.851 | 4.256 | 3.669 | 4.144 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 925 | 835 | 969 | 865 |
| Service Time | 1.894 | 2.311 | 1.719 | 2.169 |
| HCM Lane VIC Ratio | 0.016 | 0.016 | 0.06 | 0.096 |
| HCM Control Delay | 7 | 7.4 | 7 | 7.6 |
| HCM Lane LOS | A | A | A | A |
| HCM 95th-tile Q | 0 | 0 | 0.2 | 0.3 |

```
Intersection
Intersection Delay, s/veh 9.3
Intersection LOS
A
```



|  | NBLn1 EBLn1WBLn1 SBLn1 |  |  |  |
| :--- | ---: | ---: | ---: | ---: |
| Vol Left, \% | $54 \%$ | $2 \%$ | $1 \%$ | $70 \%$ |
| Vol Thru, $\%$ | $37 \%$ | $80 \%$ | $56 \%$ | $25 \%$ |
| Vol Right, \% | $10 \%$ | $18 \%$ | $42 \%$ | $5 \%$ |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 52 | 166 | 206 | 144 |
| LT Vol | 28 | 3 | 3 | 101 |
| Through Vol | 19 | 133 | 116 | 36 |
| RT Vol | 5 | 30 | 87 | 7 |
| Lane Flow Rate | 58 | 187 | 231 | 162 |
| Geometry Grp | 1 | 1 | 1 | 1 |
| Degree of Util (X) | 0.083 | 0.24 | 0.285 | 0.227 |
| Departure Headway (Hd) | 5.119 | 4.637 | 4.432 | 5.046 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 695 | 770 | 808 | 707 |
| Service Time | 3.188 | 2.687 | 2.479 | 3.105 |
| HCM Lane V/C Ratio | 0.083 | 0.243 | 0.286 | 0.229 |
| HCM Control Delay | 8.7 | 9.2 | 9.3 | 9.6 |
| HCM Lane LOS | A | A | A | A |
| HCM 95th-tile Q | 0.3 | 0.9 | 1.2 | 0.9 |




## APPENDIX E: NEAR TERM (2021) PROJECT PLUS PROJECT TRAFFIC CONDITIONS ANALYSIS SHEETS




| Intersection |  |
| :--- | ---: | :--- |
| Intersection Delay, s/veh | 7.1 |
| Intersection LOS | A |


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations |  | * |  |  | * |  |  | * |  |  | * |  |
| Traffic Vol, veh/h | 8 | 1 | 0 | 1 | 0 | 51 | 0 | 4 | 4 | 43 | 3 | 3 |
| Future Vol, veh/h | 8 | 1 | 0 | 1 | 0 | 51 | 0 | 4 | 4 | 43 | 3 | 3 |
| Peak Hour Factor | 0.82 | 0.82 | 0.82 | 0.82 | 0.82 | 0.82 | 0.82 | 0.82 | 0.82 | 0.82 | 0.82 | 0.82 |
| Heavy Vehicles, \% | 0 | 0 | 0 | 2 | 2 | 2 | 0 | 0 | 0 | 0 | 0 | 0 |
| Mvmt Flow | 10 | 1 | 0 | 1 | 0 | 62 | 0 | 5 | 5 | 52 | 4 | 4 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | EB |  |  | WB |  |  |  | NB |  | SB |  |  |
| Opposing Approach | WB |  |  | EB |  |  |  | SB |  | NB |  |  |
| Opposing Lanes | 1 |  |  | 1 |  |  |  | 1 |  | 1 |  |  |
| Conflicting Approach Left | SB |  |  | NB |  |  |  | EB |  | WB |  |  |
| Conflicting Lanes Left | 1 |  |  | 1 |  |  |  | 1 |  | 1 |  |  |
| Conflicting Approach Right | NB |  |  | SB |  |  |  | WB |  | EB |  |  |
| Conflicting Lanes Right | 1 |  |  | 1 |  |  |  | 1 |  | 1 |  |  |
| HCM Control Delay | 7.3 |  |  | 6.7 |  |  |  | 6.8 |  | 7.5 |  |  |
| HCM LOS | A |  |  | A |  |  |  | A |  | A |  |  |


| Lane | NBLn1 | EBLn1 | WBLn1 | SBLn1 |
| :--- | ---: | ---: | ---: | ---: |
| Vol Left, \% | $0 \%$ | $89 \%$ | $2 \%$ | $88 \%$ |
| Vol Thru, \% | $50 \%$ | $11 \%$ | $0 \%$ | $6 \%$ |
| Vol Right, \% | $50 \%$ | $0 \%$ | $98 \%$ | $6 \%$ |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 8 | 9 | 52 | 49 |
| LT Vol | 0 | 8 | 1 | 43 |
| Through Vol | 4 | 1 | 0 | 3 |
| RT Vol | 4 | 0 | 51 | 3 |
| Lane Flow Rate | 10 | 11 | 63 | 60 |
| Geometry Grp | 1 | 1 | 1 | 1 |
| Degree of Util (X) | 0.01 | 0.013 | 0.061 | 0.069 |
| Departure Headway (Hd) | 3.774 | 4.247 | 3.479 | 4.176 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 947 | 840 | 1025 | 860 |
| Service Time | 1.804 | 2.285 | 1.514 | 2.192 |
| HCM Lane V/C Ratio | 0.011 | 0.013 | 0.061 | 0.07 |
| HCM Control Delay | 6.8 | 7.3 | 6.7 | 7.5 |
| HCM Lane LOS | A | A | A | A |
| HCM 95th-tile Q | 0 | 0 | 0.2 | 0.2 |


| Intersection |  |
| :--- | ---: | :--- |
| Intersection Delay, s/veh 11 |  |
| Intersection LOS | B |



| Lane | NBLn1 EBLn1WBLn1 SBLn1 |  |  |  |
| :--- | ---: | ---: | ---: | ---: |
| Vol Left, \% | $41 \%$ | $13 \%$ | $1 \%$ | $70 \%$ |
| Vol Thru, \% | $53 \%$ | $66 \%$ | $54 \%$ | $23 \%$ |
| Vol Right, \% | $7 \%$ | $21 \%$ | $45 \%$ | $7 \%$ |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 76 | 95 | 266 | 144 |
| LT Vol | 31 | 12 | 2 | 101 |
| Through Vol | 40 | 63 | 143 | 33 |
| RT Vol | 5 | 20 | 121 | 10 |
| Lane Flow Rate | 106 | 132 | 369 | 200 |
| Geometry Grp | 1 | 1 | 1 | 1 |
| Degree of Util (X) | 0.163 | 0.189 | 0.485 | 0.303 |
| Departure Headway (Hd) | 5.569 | 5.17 | 4.727 | 5.445 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 644 | 694 | 768 | 660 |
| Service Time | 3.603 | 3.202 | 2.727 | 3.473 |
| HCM Lane V/C Ratio | 0.165 | 0.19 | 0.48 | 0.303 |
| HCM Control Delay | 9.7 | 9.4 | 12.1 | 10.8 |
| HCM Lane LOS | A | A | B | B |
| HCM 95th-tile Q | 0.6 | 0.7 | 2.7 | 1.3 |






| Intersection |  |
| :--- | ---: | :--- |
| Intersection Delay, s/veh | 7.4 |
| Intersection LOS | A |


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations |  | \$ |  |  | \$ |  |  | \$ |  |  | \& |  |
| Traffic Vol, veh/h | 7 | 3 | 0 | 3 | 5 | 50 | 1 | 6 | 5 | 61 | , | 9 |
| Future Vol, veh/h | 7 | 3 | 0 | 3 | 5 | 50 | 1 | 6 | 5 | 61 | 4 | 9 |
| Peak Hour Factor | 0.78 | 0.78 | 0.78 | 0.78 | 0.78 | 0.78 | 0.78 | 0.78 | 0.78 | 0.78 | 0.78 | 0.78 |
| Heavy Vehicles, \% | 0 | 0 | 0 | 4 | 4 | 4 | 0 | 0 | 0 | 2 | 2 | 2 |
| Mvmt Flow | 9 | 4 | 0 | 4 | 6 | 64 | 1 | 8 | 6 | 78 | 5 | 12 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
| Opposing Approach | WB |  |  | EB |  |  | SB |  |  | NB |  |  |
| Opposing Lanes | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| Conflicting Approach Left | SB |  |  | NB |  |  | EB |  |  | WB |  |  |
| Conflicting Lanes Left | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| Conflicting Approach Right | NB |  |  | SB |  |  | WB |  |  | EB |  |  |
| Conflicting Lanes Right | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| HCM Control Delay | 7.4 |  |  | 7 |  |  | 7 |  |  | 7.7 |  |  |
| HCM LOS | A |  |  | A |  |  | A |  |  | A |  |  |


| Lane | NBLn1 | EBLn1 | WBLn1 | SBLn1 |
| :--- | ---: | ---: | ---: | ---: |
| Vol Left, \% | $8 \%$ | $70 \%$ | $5 \%$ | $82 \%$ |
| Vol Thru, \% | $50 \%$ | $30 \%$ | $9 \%$ | $5 \%$ |
| Vol Right, \% | $42 \%$ | $0 \%$ | $86 \%$ | $12 \%$ |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 12 | 10 | 58 | 74 |
| LT Vol | 1 | 7 | 3 | 61 |
| Through Vol | 6 | 3 | 5 | 4 |
| RT Vol | 5 | 0 | 50 | 9 |
| Lane Flow Rate | 15 | 13 | 74 | 95 |
| Geometry Grp | 1 | 1 | 1 | 1 |
| Degree of Util (X) | 0.017 | 0.015 | 0.076 | 0.11 |
| Departure Headway (Hd) | 3.889 | 4.289 | 3.661 | 4.189 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 914 | 827 | 969 | 855 |
| Service Time | 1.94 | 2.356 | 1.721 | 2.219 |
| HCM Lane V/C Ratio | 0.016 | 0.016 | 0.076 | 0.111 |
| HCM Control Delay | 7 | 7.4 | 7 | 7.7 |
| HCM Lane LOS | A | A | A | A |
| HCM 95th-tile Q | 0.1 | 0 | 0.2 | 0.4 |

```
Intersection
Intersection Delay, s/veh 9.4
Intersection LOS
A
```



|  | NBLn1 EBLn1WBLn1 SBLn1 |  |  |  |
| :--- | ---: | ---: | ---: | ---: |
| Vol Left, \% | $60 \%$ | $2 \%$ | $1 \%$ | $70 \%$ |
| Vol Thru, \% | $31 \%$ | $76 \%$ | $56 \%$ | $25 \%$ |
| Vol Right, \% | $9 \%$ | $22 \%$ | $42 \%$ | $5 \%$ |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 65 | 175 | 206 | 144 |
| LT Vol | 39 | 3 | 3 | 101 |
| Through Vol | 20 | 133 | 116 | 36 |
| RT Vol | 6 | 39 | 87 | 7 |
| Lane Flow Rate | 73 | 197 | 231 | 162 |
| Geometry Grp | 1 | 1 | 1 | 1 |
| Degree of Util (X) | 0.105 | 0.254 | 0.288 | 0.229 |
| Departure Headway (Hd) | 5.163 | 4.657 | 4.487 | 5.094 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 689 | 767 | 796 | 701 |
| Service Time | 3.238 | 2.712 | 2.54 | 3.161 |
| HCM Lane V/C Ratio | 0.106 | 0.257 | 0.29 | 0.231 |
| HCM Control Delay | 8.9 | 9.3 | 9.4 | 9.7 |
| HCM Lane LOS | A | A | A | A |
| HCM 95th-tile Q | 0.4 | 1 | 1.2 | 0.9 |




## APPENDIX F: CUMULATIVE (2040) TRAFFIC CONDITIONS ANALYSIS SHEETS




| Intersection |  |  |
| :--- | ---: | :--- |
| Intersection Delay, s/veh | 7.1 | A |
| Intersection LOS | A |  |


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations |  | \$ |  |  | $\ddagger$ |  |  | \$ |  |  | \$ |  |
| Traffic Vol, veh/h | 9 | 1 | 0 | 1 | 0 | 45 | 0 | 4 | 4 | 40 | 3 | 3 |
| Future Vol, veh/h | 9 | 1 | 0 | 1 | 0 | 45 | 0 | 4 | 4 | 40 | 3 | 3 |
| Peak Hour Factor | 0.82 | 0.82 | 0.82 | 0.82 | 0.82 | 0.82 | 0.82 | 0.82 | 0.82 | 0.82 | 0.82 | 0.82 |
| Heavy Vehicles, \% | 0 | 0 | 0 | 2 | 2 | 2 | 0 | 0 | 0 | 0 | 0 | 0 |
| Mvmt Flow | 11 | 1 | 0 | 1 | 0 | 55 | 0 | 5 | 5 | 49 | 4 | 4 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | EB |  |  | WB |  |  |  | NB |  | SB |  |  |
| Opposing Approach | WB |  |  | EB |  |  |  | SB |  | NB |  |  |
| Opposing Lanes | 1 |  |  | 1 |  |  |  | 1 |  | 1 |  |  |
| Conflicting Approach Left | SB |  |  | NB |  |  |  | EB |  | WB |  |  |
| Conflicting Lanes Left | 1 |  |  | 1 |  |  |  | 1 |  | 1 |  |  |
| Conflicting Approach Right | NB |  |  | SB |  |  |  | WB |  | EB |  |  |
| Conflicting Lanes Right | 1 |  |  | 1 |  |  |  | 1 |  | 1 |  |  |
| HCM Control Delay | 7.3 |  |  | 6.7 |  |  |  | 6.8 |  | 7.5 |  |  |
| HCM LOS | A |  |  | A |  |  |  | A |  | A |  |  |


| Lane | NBLn1 | EBLn1 | WBLn1 | SBLn1 |
| :--- | ---: | ---: | ---: | ---: |
| Vol Left, \% | $0 \%$ | $90 \%$ | $2 \%$ | $87 \%$ |
| Vol Thru, \% | $50 \%$ | $10 \%$ | $0 \%$ | $7 \%$ |
| Vol Right, \% | $50 \%$ | $0 \%$ | $98 \%$ | $7 \%$ |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 8 | 10 | 46 | 46 |
| LT Vol | 0 | 9 | 1 | 40 |
| Through Vol | 4 | 1 | 0 | 3 |
| RT Vol | 4 | 0 | 45 | 3 |
| Lane Flow Rate | 10 | 12 | 56 | 56 |
| Geometry Grp | 1 | 1 | 1 | 1 |
| Degree of Util (X) | 0.01 | 0.014 | 0.054 | 0.065 |
| Departure Headway (Hd) | 3.762 | 4.239 | 3.476 | 4.162 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 951 | 842 | 1027 | 863 |
| Service Time | 1.788 | 2.274 | 1.509 | 2.176 |
| HCM Lane VIC Ratio | 0.011 | 0.014 | 0.055 | 0.065 |
| HCM Control Delay | 6.8 | 7.3 | 6.7 | 7.5 |
| HCM Lane LOS | A | A | A | A |
| HCM 95th-tile Q | 0 | 0 | 0.2 | 0.2 |



| Movement EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ¢ |  |  | \$ |  |  | \$ |  |  | \& |  |
| Traffic Vol, veh/h 13 | 68 | 15 | 2 | 155 | 131 | 26 | 43 | 3 | 109 | 36 | 11 |
| Future Vol, veh/h 13 | 68 | 15 | 2 | 155 | 131 | 26 | 43 | 3 | 109 | 36 | 11 |
| Peak Hour Factor 0.72 | 0.72 | 0.72 | 0.72 | 0.72 | 0.72 | 0.72 | 0.72 | 0.72 | 0.72 | 0.72 | 0.72 |
| Heavy Vehicles, \% 0 | 0 | 0 | 1 | 1 | 1 | 2 | 2 | 2 | 1 | 1 | 1 |
| Mvmt Flow 18 | 94 | 21 | 3 | 215 | 182 | 36 | 60 | 4 | 151 | 50 | 15 |
| Number of Lanes 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach EB |  |  | WB |  |  | NB |  |  | SB |  |  |
| Opposing Approach WB |  |  | EB |  |  | SB |  |  | NB |  |  |
| Opposing Lanes 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| Conflicting Approach Left SB |  |  | NB |  |  | EB |  |  | WB |  |  |
| Conflicting Lanes Left 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| Conflicting Approach RighNB |  |  | SB |  |  | WB |  |  | EB |  |  |
| Conflicting Lanes Right 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| HCM Control Delay 9.6 |  |  | 13.1 |  |  | 9.8 |  |  | 11.3 |  |  |
| HCM LOS A |  |  | B |  |  | A |  |  | B |  |  |


| Lane | NBLn1 EBLn1WBLn1 SBLn1 |  |  |  |
| :--- | ---: | ---: | ---: | ---: |
| Vol Left, \% | $36 \%$ | $14 \%$ | $1 \%$ | $70 \%$ |
| Vol Thru, \% | $60 \%$ | $71 \%$ | $54 \%$ | $23 \%$ |
| Vol Right, \% | $4 \%$ | $16 \%$ | $45 \%$ | $7 \%$ |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 72 | 96 | 288 | 156 |
| LT Vol | 26 | 13 | 2 | 109 |
| Through Vol | 43 | 68 | 155 | 36 |
| RT Vol | 3 | 15 | 131 | 11 |
| Lane Flow Rate | 100 | 133 | 400 | 217 |
| Geometry Grp | 1 | 1 | 1 | 1 |
| Degree of Util (X) | 0.159 | 0.196 | 0.532 | 0.333 |
| Departure Headway (Hd) | 5.71 | 5.304 | 4.786 | 5.533 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 627 | 676 | 760 | 650 |
| Service Time | 3.754 | 3.344 | 2.786 | 3.57 |
| HCM Lane V/C Ratio | 0.159 | 0.197 | 0.526 | 0.334 |
| HCM Control Delay | 9.8 | 9.6 | 13.1 | 11.3 |
| HCM Lane LOS | A | A | B | B |
| HCM 95th-tile Q | 0.6 | 0.7 | 3.2 | 1.5 |


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 7.7 |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{*}$ | $\uparrow$ |  |  | $\uparrow$ | 「' |  | $\uparrow$ |  |  | \& |  |
| Traffic Vol, veh/h | 2 | 1 | 0 | 155 | 0 | 21 | 3 | 164 | 64 | 36 | 255 | 3 |
| Future Vol, veh/h | 2 | 1 | 0 | 155 | 0 | 21 | 3 | 164 | 64 | 36 | 255 | 3 |
| Conflicting Peds, \#/hr | 4 | 0 | 2 | 2 | 0 | 4 | 14 | 0 | 6 | 6 | 0 | 14 |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | 20 | - | - | - | - | 20 | - | - | - | - | - | - |
| Veh in Median Storage, \# | \# | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 76 | 76 | 76 | 76 | 76 | 76 | 76 | 76 | 76 | 76 | 76 | 76 |
| Heavy Vehicles, \% | 0 | 0 | 0 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| Mvmt Flow | 3 | 1 | 0 | 204 | 0 | 28 | 4 | 216 | 84 | 47 | 336 | 4 |





| Intersection |  |
| :--- | ---: | :--- |
| Intersection Delay, s/veh | 7.4 |
| Intersection LOS | A |


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations |  | \$ |  |  | \$ |  |  | \$ |  |  | \& |  |
| Traffic Vol, veh/h | 8 | 3 | 0 | 3 | 5 | 40 | 1 | 7 | 5 | 56 | 4 | 10 |
| Future Vol, veh/h | 8 | 3 | 0 | 3 | 5 | 40 | 1 | 7 | 5 | 56 | 4 | 10 |
| Peak Hour Factor | 0.78 | 0.78 | 0.78 | 0.78 | 0.78 | 0.78 | 0.78 | 0.78 | 0.78 | 0.78 | 0.78 | 0.78 |
| Heavy Vehicles, \% | 0 | 0 | 0 | 4 | 4 | 4 | 0 | 0 | 0 | 2 | 2 | 2 |
| Mvmt Flow | 10 | 4 | 0 | 4 | 6 | 51 | 1 | 9 | 6 | 72 | 5 | 13 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
| Opposing Approach | WB |  |  | EB |  |  | SB |  |  | NB |  |  |
| Opposing Lanes | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| Conflicting Approach Left | SB |  |  | NB |  |  | EB |  |  | WB |  |  |
| Conflicting Lanes Left | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| Conflicting Approach Right | NB |  |  | SB |  |  | WB |  |  | EB |  |  |
| Conflicting Lanes Right | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| HCM Control Delay | 7.4 |  |  | 7 |  |  | 7 |  |  | 7.7 |  |  |
| HCM LOS | A |  |  | A |  |  | A |  |  | A |  |  |


| Lane | NBLn1 | EBLn1 | WBLn1 | SBLn1 |
| :--- | ---: | ---: | ---: | ---: |
| Vol Left, \% | $8 \%$ | $73 \%$ | $6 \%$ | $80 \%$ |
| Vol Thru, \% | $54 \%$ | $27 \%$ | $10 \%$ | $6 \%$ |
| Vol Right, \% | $38 \%$ | $0 \%$ | $83 \%$ | $14 \%$ |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 13 | 11 | 48 | 70 |
| LT Vol | 1 | 8 | 3 | 56 |
| Through Vol | 7 | 3 | 5 | 4 |
| RT Vol | 5 | 0 | 40 | 10 |
| Lane Flow Rate | 17 | 14 | 62 | 90 |
| Geometry Grp | 1 | 1 | 1 | 1 |
| Degree of Util (X) | 0.018 | 0.017 | 0.063 | 0.104 |
| Departure Headway (Hd) | 3.886 | 4.279 | 3.677 | 4.154 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 916 | 830 | 966 | 862 |
| Service Time | 1.93 | 2.34 | 1.732 | 2.18 |
| HCM Lane V/C Ratio | 0.019 | 0.017 | 0.064 | 0.104 |
| HCM Control Delay | 7 | 7.4 | 7 | 7.7 |
| HCM Lane LOS | A | A | A | A |
| HCM 95th-tile Q | 0.1 | 0.1 | 0.2 | 0.3 |

```
Intersection
Intersection Delay, s/veh 9.6
Intersection LOS
A
```



|  | NBLn1 EBLn1WBLn1 SBLn1 |  |  |  |
| :--- | ---: | ---: | ---: | ---: |
| Vol Left, \% | $54 \%$ | $2 \%$ | $1 \%$ | $70 \%$ |
| Vol Thru, $\%$ | $37 \%$ | $80 \%$ | $56 \%$ | $25 \%$ |
| Vol Right, \% | $9 \%$ | $18 \%$ | $42 \%$ | $5 \%$ |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 57 | 180 | 222 | 156 |
| LT Vol | 31 | 3 | 3 | 109 |
| Through Vol | 21 | 144 | 125 | 39 |
| RT Vol | 5 | 33 | 94 | 8 |
| Lane Flow Rate | 64 | 202 | 249 | 175 |
| Geometry Grp | 1 | 1 | 1 | 1 |
| Degree of Util (X) | 0.093 | 0.265 | 0.313 | 0.25 |
| Departure Headway (Hd) | 5.238 | 4.719 | 4.513 | 5.138 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 677 | 756 | 791 | 694 |
| Service Time | 3.324 | 2.78 | 2.569 | 3.211 |
| HCM Lane V/C Ratio | 0.095 | 0.267 | 0.315 | 0.252 |
| HCM Control Delay | 8.9 | 9.5 | 9.6 | 9.9 |
| HCM Lane LOS | A | A | A | A |
| HCM 95th-tile Q | 0.3 | 1.1 | 1.3 | 1 |




## APPENDIX G: CUMULATIVE (2040) PLUS PROJECT TRAFFIC CONDITIONS

 ANALYSIS SHEETS


| Intersection |  |
| :--- | ---: | :--- |
| Intersection Delay, s/veh | 7.1 |
| Intersection LOS | A |


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations |  | * |  |  | 4 |  |  | * |  |  | * |  |
| Traffic Vol, veh/h | 9 | 1 | 0 | 1 | 0 | 55 | 0 | 4 | 4 | 46 | 3 | 3 |
| Future Vol, veh/h | 9 | 1 | 0 | 1 | 0 | 55 | 0 | 4 | 4 | 46 | 3 | 3 |
| Peak Hour Factor | 0.82 | 0.82 | 0.82 | 0.82 | 0.82 | 0.82 | 0.82 | 0.82 | 0.82 | 0.82 | 0.82 | 0.82 |
| Heavy Vehicles, \% | 0 | 0 | 0 | 2 | 2 | 2 | 0 | 0 | 0 | 0 | 0 | 0 |
| Mvmt Flow | 11 | 1 | 0 | 1 | 0 | 67 | 0 | 5 | 5 | 56 | 4 | 4 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | EB |  |  | WB |  |  |  | NB |  | SB |  |  |
| Opposing Approach | WB |  |  | EB |  |  |  | SB |  | NB |  |  |
| Opposing Lanes | 1 |  |  | 1 |  |  |  | 1 |  | 1 |  |  |
| Conflicting Approach Left | SB |  |  | NB |  |  |  | EB |  | WB |  |  |
| Conflicting Lanes Left | 1 |  |  | 1 |  |  |  | 1 |  | 1 |  |  |
| Conflicting Approach Right | NB |  |  | SB |  |  |  | WB |  | EB |  |  |
| Conflicting Lanes Right | 1 |  |  | 1 |  |  |  | 1 |  | 1 |  |  |
| HCM Control Delay | 7.4 |  |  | 6.8 |  |  |  | 6.9 |  | 7.5 |  |  |
| HCM LOS | A |  |  | A |  |  |  | A |  | A |  |  |


| Lane | NBLn1 | EBLn1 | WBLn1 | SBLn1 |
| :--- | ---: | ---: | ---: | ---: |
| Vol Left, \% | $0 \%$ | $90 \%$ | $2 \%$ | $88 \%$ |
| Vol Thru, \% | $50 \%$ | $10 \%$ | $0 \%$ | $6 \%$ |
| Vol Right, \% | $50 \%$ | $0 \%$ | $98 \%$ | $6 \%$ |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 8 | 10 | 56 | 52 |
| LT Vol | 0 | 9 | 1 | 46 |
| Through Vol | 4 | 1 | 0 | 3 |
| RT Vol | 4 | 0 | 55 | 3 |
| Lane Flow Rate | 10 | 12 | 68 | 63 |
| Geometry Grp | 1 | 1 | 1 | 1 |
| Degree of Util (X) | 0.01 | 0.014 | 0.066 | 0.074 |
| Departure Headway (Hd) | 3.789 | 4.26 | 3.484 | 4.191 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 943 | 837 | 1022 | 857 |
| Service Time | 1.82 | 2.302 | 1.524 | 2.207 |
| HCM Lane V/C Ratio | 0.011 | 0.014 | 0.067 | 0.074 |
| HCM Control Delay | 6.9 | 7.4 | 6.8 | 7.5 |
| HCM Lane LOS | A | A | A | A |
| HCM 95th-tile Q | 0 | 0 | 0.2 | 0.2 |


| Intersection |
| :--- |
| Intersection Delay, s/veh11.9 |
| Intersection LOS |



| Lane | NBLn1 EBLn1WBLn1 SBLn1 |  |  |  |
| :--- | ---: | ---: | ---: | ---: |
| Vol Left, \% | $40 \%$ | $13 \%$ | $1 \%$ | $70 \%$ |
| Vol Thru, \% | $54 \%$ | $67 \%$ | $54 \%$ | $23 \%$ |
| Vol Right, \% | $6 \%$ | $21 \%$ | $45 \%$ | $7 \%$ |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 82 | 102 | 288 | 156 |
| LT Vol | 33 | 13 | 2 | 109 |
| Through Vol | 44 | 68 | 155 | 36 |
| RT Vol | 5 | 21 | 131 | 11 |
| Lane Flow Rate | 114 | 142 | 400 | 217 |
| Geometry Grp | 1 | 1 | 1 | 1 |
| Degree of Util (X) | 0.182 | 0.21 | 0.536 | 0.337 |
| Departure Headway (Hd) | 5.745 | 5.331 | 4.82 | 5.593 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 623 | 671 | 748 | 643 |
| Service Time | 3.79 | 3.375 | 2.852 | 3.631 |
| HCM Lane V/C Ratio | 0.183 | 0.212 | 0.535 | 0.337 |
| HCM Control Delay | 10.1 | 9.8 | 13.3 | 11.5 |
| HCM Lane LOS | B | A | B | B |
| HCM 95th-tile Q | 0.7 | 0.8 | 3.2 | 1.5 |




| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 4.4 |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  | 「 |  |  |  | ${ }^{*}$ | $\uparrow$ |  | ${ }^{1}$ | 中 $\uparrow$ |  |
| Traffic Vol, veh/h | 0 | 0 | 70 | 0 | 0 | 0 | 37 | 795 | 4 | 499 | 955 | 22 |
| Future Vol, veh/h | 0 | 0 | 70 | 0 | 0 | 0 | 37 | 795 | 4 | 499 | 955 | 22 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 16 | 0 | 0 | 0 | 0 | 16 |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | 0 | - | - | - | 190 | - | - | 100 | - | - |
| Veh in Median Storage, \# | \# | 0 | - | - | - | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 95 | 95 | 95 | 82 | 82 | 82 | 95 | 95 | 95 | 95 | 95 | 95 |
| Heavy Vehicles, \% | 5 | 2 | 5 | 2 | 2 | 2 | 1 | 1 | 2 | 2 | 1 | 1 |
| Mvmt Flow | 0 | 0 | 74 | 0 | 0 | 0 | 39 | 837 | 4 | 525 | 1005 | 23 |



| Intersection |  |
| :--- | ---: |
| Intersection Delay, s/veh | 7.5 |
| Intersection LOS | A |


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations |  | * |  |  | * |  |  | \& |  |  | * |  |
| Traffic Vol, veh/h | 8 | 3 | 0 | 3 | 5 | 53 | 1 | 7 | 5 | 65 | 4 | 10 |
| Future Vol, veh/h | 8 | 3 | 0 | 3 | 5 | 53 | 1 | 7 | 5 | 65 | 4 | 10 |
| Peak Hour Factor | 0.78 | 0.78 | 0.78 | 0.78 | 0.78 | 0.78 | 0.78 | 0.78 | 0.78 | 0.78 | 0.78 | 0.78 |
| Heavy Vehicles, \% | 0 | 0 | 0 | 4 | 4 | 4 | 0 | 0 | 0 | 2 | 2 | 2 |
| Mvmt Flow | 10 | 4 | 0 | 4 | 6 | 68 | 1 | 9 | 6 | 83 | 5 | 13 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
| Opposing Approach | WB |  |  | EB |  |  | SB |  |  | NB |  |  |
| Opposing Lanes | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| Conflicting Approach Left | SB |  |  | NB |  |  | EB |  |  | WB |  |  |
| Conflicting Lanes Left | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| Conflicting Approach Right | NB |  |  | SB |  |  | WB |  |  | EB |  |  |
| Conflicting Lanes Right | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| HCM Control Delay | 7.5 |  |  | 7.1 |  |  | 7 |  |  | 7.8 |  |  |
| HCM LOS | A |  |  | A |  |  | A |  |  | A |  |  |


| Lane | NBLn1 | EBLn1 | WBLn1 | SBLn1 |
| :--- | ---: | ---: | ---: | ---: |
| Vol Left, \% | $8 \%$ | $73 \%$ | $5 \%$ | $82 \%$ |
| Vol Thru, \% | $54 \%$ | $27 \%$ | $8 \%$ | $5 \%$ |
| Vol Right, \% | $38 \%$ | $0 \%$ | $87 \%$ | $13 \%$ |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 13 | 11 | 61 | 79 |
| LT Vol | 1 | 8 | 3 | 65 |
| Through Vol | 7 | 3 | 5 | 4 |
| RT Vol | 5 | 0 | 53 | 10 |
| Lane Flow Rate | 17 | 14 | 78 | 101 |
| Geometry Grp | 1 | 1 | 1 | 1 |
| Degree of Util (X) | 0.018 | 0.017 | 0.08 | 0.118 |
| Departure Headway (Hd) | 3.924 | 4.312 | 3.672 | 4.198 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 905 | 822 | 965 | 853 |
| Service Time | 1.977 | 2.382 | 1.736 | 2.228 |
| HCM Lane V/C Ratio | 0.019 | 0.017 | 0.081 | 0.118 |
| HCM Control Delay | 7 | 7.5 | 7.1 | 7.8 |
| HCM Lane LOS | A | A | A | A |
| HCM 95th-tile Q | 0.1 | 0.1 | 0.3 | 0.4 |

Intersection
Intersection Delay, s/veh 9.7
Intersection LOS $\quad$ A

| Movement EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | 4 |  |  | * |  |  | 4 |  |  | * |  |
| Traffic Vol, veh/h 3 | 144 | 42 | 3 | 125 | 94 | 42 | 22 | 6 | 109 | 39 | 8 |
| Future Vol, veh/h 3 | 144 | 42 | 3 | 125 | 94 | 42 | 22 | 6 | 109 | 39 | 8 |
| Peak Hour Factor 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 |
| Heavy Vehicles, \% 1 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 1 |
| Mvmt Flow 3 | 162 | 47 | 3 | 140 | 106 | 47 | 25 | 7 | 122 | 44 | 9 |
| Number of Lanes 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach EB |  |  | WB |  |  | NB |  |  | SB |  |  |
| Opposing Approach WB |  |  | EB |  |  | SB |  |  | NB |  |  |
| Opposing Lanes 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| Conflicting Approach Left SB |  |  | NB |  |  | EB |  |  | WB |  |  |
| Conflicting Lanes Left 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| Conflicting Approach RighNB |  |  | SB |  |  | WB |  |  | EB |  |  |
| Conflicting Lanes Right 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| HCM Control Delay 9.7 |  |  | 9.8 |  |  | 9.1 |  |  | 10 |  |  |
| HCM LOS A |  |  | A |  |  | A |  |  | A |  |  |


| Lane | NBLn1 EBLn1WBLn1 SBLn1 |  |  |  |
| :--- | ---: | ---: | ---: | ---: |
| Vol Left, \% | $60 \%$ | $2 \%$ | $1 \%$ | $70 \%$ |
| Vol Thru, \% | $31 \%$ | $76 \%$ | $56 \%$ | $25 \%$ |
| Vol Right, \% | $9 \%$ | $22 \%$ | $42 \%$ | $5 \%$ |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 70 | 189 | 222 | 156 |
| LT Vol | 42 | 3 | 3 | 109 |
| Through Vol | 22 | 144 | 125 | 39 |
| RT Vol | 6 | 42 | 94 | 8 |
| Lane Flow Rate | 79 | 212 | 249 | 175 |
| Geometry Grp | 1 | 1 | 1 | 1 |
| Degree of Util (X) | 0.115 | 0.28 | 0.316 | 0.253 |
| Departure Headway (Hd) | 5.278 | 4.74 | 4.566 | 5.187 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 671 | 752 | 781 | 685 |
| Service Time | 3.374 | 2.81 | 2.633 | 3.27 |
| HCM Lane V/C Ratio | 0.118 | 0.282 | 0.319 | 0.255 |
| HCM Control Delay | 9.1 | 9.7 | 9.8 | 10 |
| HCM Lane LOS | A | A | A | A |
| HCM 95th-tile Q | 0.4 | 1.1 | 1.4 | 1 |




APPENDIX H: CITY OF WATSONVILLE (2017-2018) DEVELOPMENT FEES

# DEVELOPMENT FEE SUMMARY 2017-2018 

 CITY OF WATSONVILLE - Community Development Department250 Main Street, Watsonville CA 95076
(831) 768-3050

This reference is a summary of common development and impact fees. Actual project fees are calculated from submittal plans. Additional fees may include permits, plan review, and inspections.
A. CITY-WIDE TRAFFIC IMPACT FEE

Single Family detached 14 trips per unit
Multi-Family (apartments, townhouses 10 trips per unit
Non-Residential (remodel/addition) trips based on use
Non-Residential (other)
trips based on use

## B. SANITARY SEWER CONNECTION FEE

Residential and all others
Commercial \& Industrial: Sum of following, but not less than
Based on peak month discharge of flow BOD (Biochemical oxygen demand)
SS (suspended solids)
C. WATER SERVICE

Connection Fee (residential)
Construction Fee (1" domestic/fire service combination meter)
D. GROUNDWATER IMPACT FEE

Residential

Commercial \& Industrial
E. STORM DRAINAGE FEE

Additions to Existing (per acre of new impermeable area)
New Development Projects:
Low residential (4.5 units/acre)
Med. Residential (4.5-7.5 units /acre)
High residential (7.5 units/acre)
Commercial \& Industrial
Area "C" (NE of City, S of Corralitos \& Salsipuedes Creeks)

## F. IMPERVIOUS AREA IMPACT FEE

per square foot of new impervious area
G. RECREATION \& PARKS FACILITIES FEE
(New construction, bedroom additions)
1-2 bedroom dwelling unit
3 bedroom dwelling unit
$\$ 0.40$ per sq. ft.
\$185.00 per trip
$\$ 185.00$ per trip
$\$ 141.00$ per trip
$\$ 95.00$ per trip

$$
\begin{aligned}
\$ 1,868.47 & \text { per unit } \\
\$ 1,868.47 & \text { minimum } \\
\$ 5.20 & \text { per gpd } \\
\$ 330.41 & \text { lb/day BOD } \\
\$ 417.29 & \text { lb/day SS }
\end{aligned}
$$

\$2,414.52 per connection
\$5,544.61 per meter

$$
\begin{aligned}
\$ 429.68 & \text { per bedroom } \\
\$ 0.00 & \text { no fees }
\end{aligned}
$$

$\$ 11,413.00$ per acre
$\$ 4,594.00$ per acre
\$5,711.00 per acre
\$6,846.00 per acre
\$9,134.00 per acre
\$23,964.00 per acre
\$1,500.00 per bedroom
\$1,667.00 per bedroom

4+ bedroom dwelling unit
Commercial \& Industrial
\$1,875.00
$\$ 0.50$
$\$ 0.40$ per sq. ft.
Calcuated on total square footage.
I. FIRE IMPACT FEE

Residential new construction
Residential addition
Commercial \& Industrial

## J. AFFORDABLE HOUSING ORDINANCE - IN LIEU FEES

Residential
Single-Family detached
Accessory dwelling unit (14-46.050 exceptions)
Multi-Family (apartments, townhouses, co-op, condos
\$12,730.00 per unit
cial
$0-1,000 \mathrm{sq}$. ft.
$1,001 \mathrm{sq} . \mathrm{ft}$ or more
IMPROVEMENT IN-LIEU FEES
Industrially Zoned Parcels
$\$ 107.00$ per lineal ft fee per lineal foot of street frontage or $5 \%$ of actual on-site project improvements whichever is less Other Parcels
$\$ 178.00$ per lineal ft fee per lineal foot of street frontage or $10 \%$ of actual on-site project improvements whichever is less

## L. CARBON FUND IMPACT FEE

Carbon fund fee is based on a percentage of the total building permit fees paid including engineering pan check and review fees. Building permit fees do not include planning permit fees, inspection fees, utility fees or impact fees.
New residential and nonresidential construction $50 \%$ of total
Multi family residential \& nonresidential additions and alteration $30 \%$ of total
Single family residential additions of 500 SF or greater
$30 \%$ of total
building permit fee building permit fee building permit fee
M. UNDERGROUND UTILITY IN-LIEU FEE
$\$ 69.00$ per lineal ft fee per lineal foot of frontage or $1.25 \%$ of actual project improvement whichever is less
N. SCHOOL FEE

Collected by Pajaro Valley Unified School District 831-786-2380

Residential
Commercial \& Industrial
Parking lots/structures
Self Storage
\$5.56
\$0.51
\$0.10
$\$ 0.30$ per sq. ft.

# APPENDIX I: ADA 2010 STANDARDS FOR ACCESSIBLE DESIGN: TABLE 208.2 PARKING SPACES 

## 208 Parking Spaces

208.1 General. Where parking spaces are provided, parking spaces shall be provided in accordance with 208.

EXCEPTION: Parking spaces used exclusively for buses, trucks, other delivery vehicles, law enforcement vehicles, or vehicular impound shall not be required to comply with 208 provided that lots accessed by the public are provided with a passenger loading zone complying with 503.
208.2 Minimum Number. Parking spaces complying with 502 shall be provided in accordance with Table 208.2 except as required by 208.2.1, 208.2.2, and 208.2.3. Where more than one parking facility is provided on a site, the number of accessible spaces provided on the site shall be calculated according to the number of spaces required for each parking facility.

Table 208.2 Parking Spaces

| Total Number of Parking Spaces <br> Provided in Parking Facility | Minimum Number of Required <br> Accessible Parking Spaces |
| :---: | :---: |
| 1 to 25 | 1 |
| 26 to 50 | 2 |
| 51 to 75 | 3 |
| 76 to 100 | 4 |
| 101 to 150 | 5 |
| 151 to 200 | 6 |
| 201 to 300 | 7 |
| 301 to 400 | 8 |
| 401 to 500 | 9 |
| 501 to 1000 | 20, plus 1 for each 100, or fraction thereof, |
| over 1000 |  |
| 1001 and over |  |

Advisory 208.2 Minimum Number. The term "parking facility" is used Section 208.2 instead of the term "parking lot" so that it is clear that both parking lots and parking structures are required to comply with this section. The number of parking spaces required to be accessible is to be calculated separately for each parking facility; the required number is not to be based on the total number of parking spaces provided in all of the parking facilities provided on the site.

## APPENDIX J: EXISTING AND PROPOSED BICYCLE NETWORK \& TRANSIT FACILITIES

Figure 3-14: Existing \& Proposed Bicycle Network \& Transit Facilities


Source: City of Watsonville and RBF Consulting, 2012.

