

**EXHIBIT E  
HYDROLOGY REPORT**

**SITE PLAN NO. PLAN 19-00029**

November 2019



**Reinforced Earth Company  
Concrete Panel Yard  
APN 0472-131-03, 04, 08, 10, 13, 16,17  
& 0472-141-16  
Victorville, CA 92394**

## **Hydrology Report**



**Prepared for:  
Reinforced Earth Company**

**Prepared By:  
JE Miller & Associates  
17995 Outer Highway 18, Suite 1  
Apple Valley, CA 92307**

Original: May 28, 2019  
Revised: August 27, 2019  
Revised: October 24, 2019

**Prepared under the supervision of:**

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## Discussion

### **INTRODUCTION – Site Discussion**

The Reinforced Earth Company New Construction Project is a proposed industrial development on the southwest side of National Trails Highway. The project proposes to grade 13.46 acres. Project improvements include an office building, parking lot, ac driveway and concrete casting beds with gravel road access (see site map in Hydrology Exhibits). 3 stormwater basins are proposed to retain and infiltrate stormwater runoff from proposed improvements. The drainage area associated with the proposed improvements spans 28.2 acres of undeveloped desert land, but this project will be limited to a graded area of 13.46 acres within the 28.2-acre watershed. This 28.3-acre watershed will be the primary focus of this report.

Proposed grading will include cut and fill slopes and create an upper and lower pad. The upper pad will be graded at an elevation of 2770 ft and include the concrete casting beds. The lower pad will be graded at an elevation of 2750 ft that will transition to lower elevations where the building pad is proposed at an elevation of 2745 ft. Drainage improvements will include construction of v swales, storm drain inlets, storm drainpipe and three infiltration basins. Drainage will be managed as to ensure flows from proposed impervious surfaces will be drained to the basins for retention and infiltration. Surface flows at the perimeter of the proposed improvements that do not include impervious improvements will be conveyed directly to National Trails Highway. An 18-inch storm drain is proposed to connect infiltration basin 1 to infiltration basin 2. Onsite flows will be collected on the surface and conveyed to the onsite infiltration basins. Infiltration basins will be sized to reduce 100 year proposed peak flow discharges to less than the existing peak. This project is a priority development project, which requires the development of a WQMP to complete the plan check process.

The site is located on the southwest side of National Trails Highway immediately southwest of the Mojave River in the City of Victorville. The site consists of sparse desert brush covering approximately 15% of the site. The site slopes to the north east at slopes of 1-8 %. Onsite runoff discharges east to the National Trails Highway and ultimately the Mojave River. Surface flow drains southwest to northeast. Surface flow concentrates and discharges in 3 main locations (Node 1, 4 an 8 See Existing Hydrology Exhibit). According to San Bernardino County hydrology Manual Hydrologic Soil Class C can be found throughout the area. FEMA Flood Insurance Rate Map 06071C5805H indicates the site is located in Zone X which is determined to be outside the 0.2% flood plain.

### **RAINFALL DATA**

Rainfall data was acquired from NOAA Atlas 14. The 1-hour rainfall rates were used rational method analysis. Hydrographs were developed for the 24-hour storm and used, 5-minute, 30-minute, 1 hour, 3-hour, 6 hour and 24 hour.

Table 1. Rainfall Data Summary  
(inches)

Duration	100 Year
5 Minute	0.413
30 Minute	0.951
1 Hour	1.08
3 Hour	1.57
6 Hour	2.02
24 Hour	3.28

## **PURPOSE**

The purpose of this report is to discuss the hydrologic characteristics of the site, demonstrate the proposed drainage improvements are adequately sized to convey the 100-year peak flow and that runoff increases as a result of development will be mitigated through the use of 3 infiltration basins.

## **CRITERIA**

The criteria utilized in this report are set forth by the San Bernardino County Hydrology Manual. AES software was used to perform computations. Rational Methods were applied to determine peak flow rates and times of concentration while unit hydrographs were applied to determine flow volumes. Hydrographs were routed thru proposed infiltration basins to estimate flow discharge.

## **RESULTS**

The proposed drainage improvements will include 5 storm drain lines (Line A, B, C, D&E) The storm drain sizes are shown on the site plan. Size will vary from 6 inches to 18 inches. Hydraulic calculations indicate pipe sizes are adequate to convey flows in a non-pressure flow condition. Two V Swales (B=1, Z=2, H=1) are proposed and are adequately sized to convey the 100-year peak flow rate. Three infiltration basins (Infiltration Basin1,2,3) are proposed that have been sized to reduce the propose 100-year peak flow to less than existing. Results indicate that proposed drainage infrastructure including storm drains, v swales and the proposed infiltration basins are adequately sized. Infiltration basin 1 was sized to be 0.53 ac/ft or 23,143 ft<sup>3</sup>. Infiltration basin 2 was sized to be 0.07 ac/ft or 3,119 ft<sup>3</sup> and infiltration basin 3 was sized to be 0.17 ac/ft 7,416.5 ft<sup>3</sup>. The proposed spillway for infiltration basins 1,2 and 3 was sized to be 10 ft wide with a maximum depth of 1 ft. ¼ ton Rip Rap will be provided at the spillways and was sized based on the LA County Hydraulic Manual (included in reference material). The seven proposed 2 ft x2 ft Storm drain inlets have been sized to intercept the 100 year peak flow rate with 50% clogging.

Hydrology analysis was applied to the 28.2 acres indicates proposed infiltration basins are adequately sized to reduce proposed peak flows to less than existing and provide a net benefit.

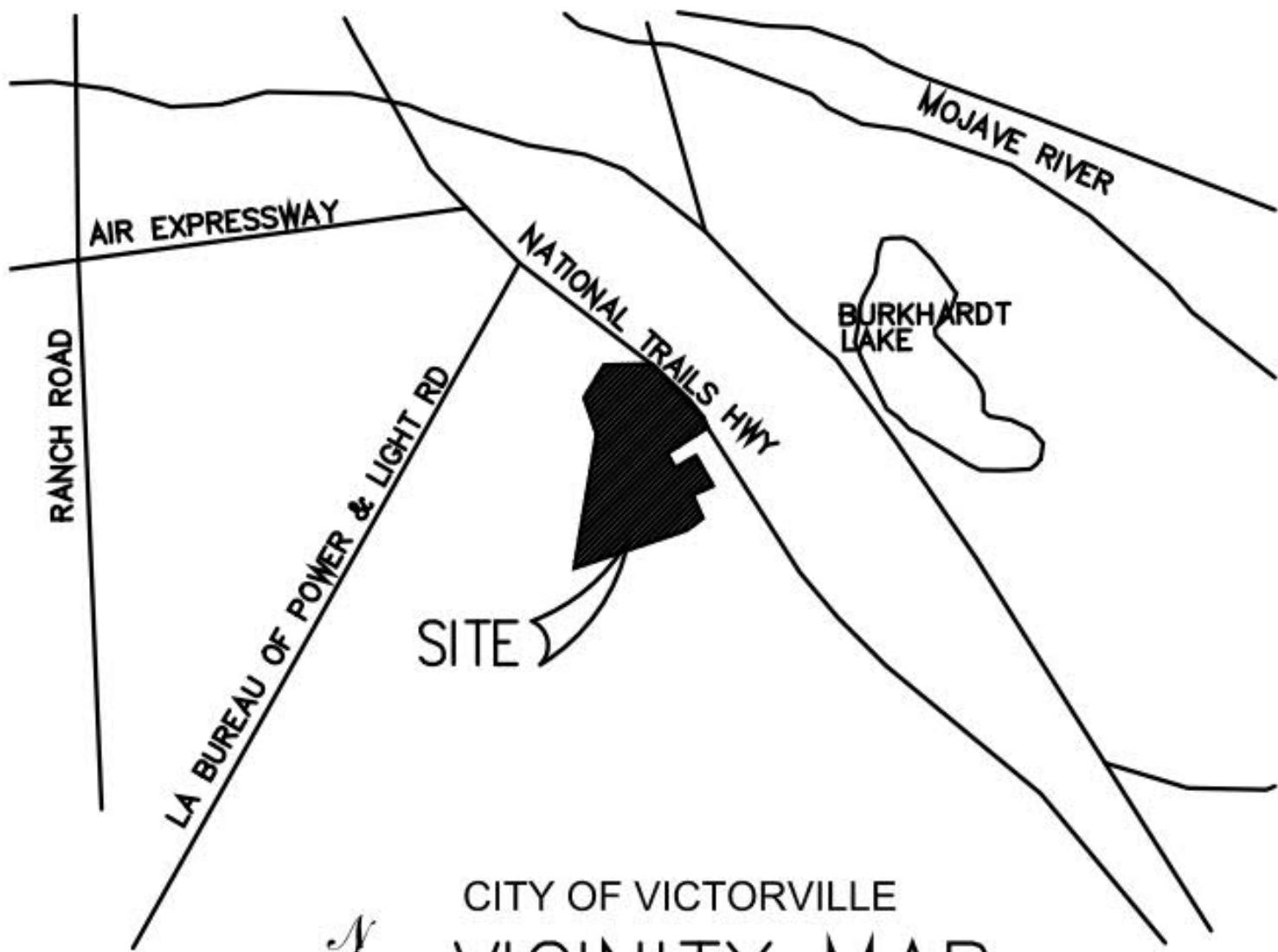
Peak Flow Summary Table

Q100 Proposed Condition (cfs)	
A1-A4	14.28
B1-B2*	11.8
C1-C3*	2.36
D1-D3	3.0
E1-E5*	28.05
Total	59.49
Q100 Existing Condition Total	64.91

\*Routed Flow Rates

The WQMP will provide additional calculations for the 10-year storm and 85% average annual runoff. However, the volumes provide in this report will govern the size of the system and exceeds that amount of storage required in the WQMP.

## Reference Material



CITY OF VICTORVILLE  
VICINITY MAP  
N.T.S.

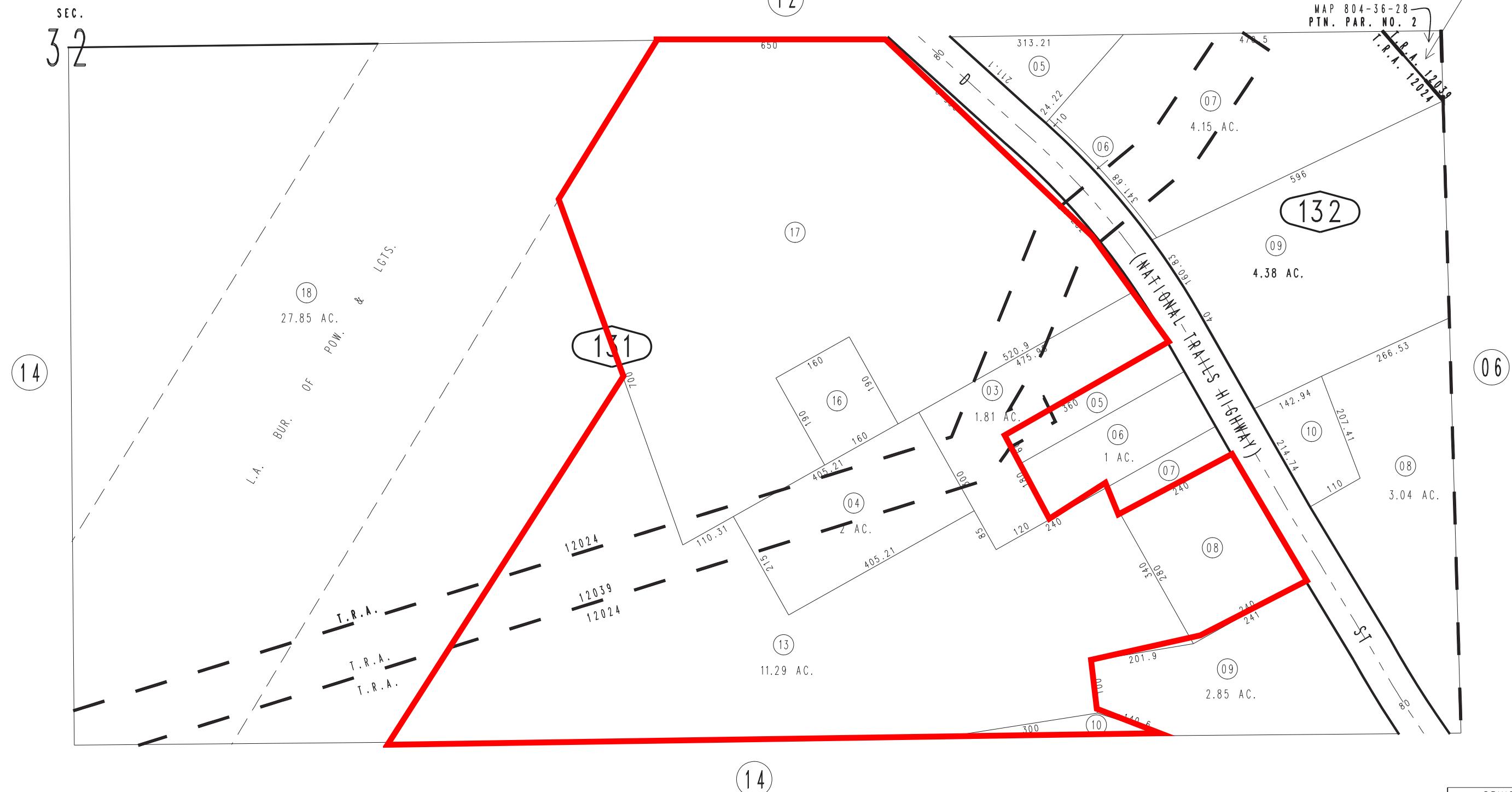
THIS MAP IS FOR THE PURPOSE  
OF AD VALOREM TAXATION ONLY.



N.1/2, S.E.1/4, Sec.32, T.6N., R.4W., S.B.B.&M.

City of Victorville  
Tax Rate Area  
12024 12039

0472- 13



REVISED  
03/04/10 RM

Assessor's Map  
Book 0472 Page 13  
San Bernardino County



**NOAA Atlas 14, Volume 6, Version 2**  
**Location name: Victorville, California, USA\***  
**Latitude: 34.5631°, Longitude: -117.3169°**  
**Elevation: 2777.35 ft\*\***

\* source: ESRI Maps  
\*\* source: USGS



### POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Sarah Dietz, Sarah Heim, Lillian Hiner, Kazungu Maitaria, Deborah Martin, Sandra Pavlovic, Ishani Roy, Carl Trypaluk, Dale Unruh, Fenglin Yan, Michael Yekta, Tan Zhao, Geoffrey Bonnin, Daniel Brewer, Li-Chuan Chen, Tye Parzybok, John Yarchao

NOAA, National Weather Service, Silver Spring, Maryland

[PF tabular](#) | [PF graphical](#) | [Maps & aerials](#)

### PF tabular

Duration	Average recurrence interval (years)									
	1	2	5	10	25	50	100	200	500	1000
5-min	<b>0.101</b> (0.083-0.124)	<b>0.138</b> (0.113-0.169)	<b>0.189</b> (0.156-0.233)	<b>0.234</b> (0.191-0.290)	<b>0.300</b> (0.237-0.384)	<b>0.354</b> (0.273-0.463)	<b>0.413</b> (0.311-0.553)	<b>0.476</b> (0.349-0.656)	<b>0.569</b> (0.401-0.817)	<b>0.647</b> (0.440-0.960)
10-min	<b>0.145</b> (0.119-0.177)	<b>0.197</b> (0.163-0.242)	<b>0.271</b> (0.223-0.334)	<b>0.336</b> (0.274-0.416)	<b>0.430</b> (0.339-0.550)	<b>0.507</b> (0.392-0.664)	<b>0.591</b> (0.446-0.792)	<b>0.683</b> (0.501-0.940)	<b>0.816</b> (0.574-1.17)	<b>0.927</b> (0.631-1.38)
15-min	<b>0.175</b> (0.144-0.214)	<b>0.239</b> (0.197-0.292)	<b>0.328</b> (0.270-0.403)	<b>0.406</b> (0.331-0.503)	<b>0.520</b> (0.410-0.666)	<b>0.614</b> (0.474-0.802)	<b>0.715</b> (0.539-0.958)	<b>0.826</b> (0.606-1.14)	<b>0.987</b> (0.695-1.42)	<b>1.12</b> (0.763-1.66)
30-min	<b>0.233</b> (0.192-0.285)	<b>0.317</b> (0.261-0.389)	<b>0.436</b> (0.359-0.536)	<b>0.540</b> (0.440-0.669)	<b>0.691</b> (0.545-0.885)	<b>0.816</b> (0.630-1.07)	<b>0.951</b> (0.717-1.27)	<b>1.10</b> (0.805-1.51)	<b>1.31</b> (0.924-1.88)	<b>1.49</b> (1.01-2.21)
60-min	<b>0.265</b> (0.218-0.324)	<b>0.361</b> (0.297-0.443)	<b>0.497</b> (0.408-0.610)	<b>0.614</b> (0.501-0.762)	<b>0.787</b> (0.620-1.01)	<b>0.929</b> (0.717-1.21)	<b>1.08</b> (0.816-1.45)	<b>1.25</b> (0.917-1.72)	<b>1.49</b> (1.05-2.14)	<b>1.70</b> (1.15-2.52)
2-hr	<b>0.367</b> (0.303-0.450)	<b>0.491</b> (0.405-0.602)	<b>0.663</b> (0.545-0.815)	<b>0.811</b> (0.661-1.00)	<b>1.02</b> (0.807-1.31)	<b>1.20</b> (0.924-1.56)	<b>1.38</b> (1.04-1.85)	<b>1.58</b> (1.16-2.17)	<b>1.86</b> (1.31-2.67)	<b>2.10</b> (1.43-3.11)
3-hr	<b>0.431</b> (0.356-0.528)	<b>0.573</b> (0.472-0.703)	<b>0.769</b> (0.632-0.945)	<b>0.936</b> (0.763-1.16)	<b>1.17</b> (0.926-1.50)	<b>1.37</b> (1.06-1.79)	<b>1.57</b> (1.18-2.10)	<b>1.79</b> (1.31-2.46)	<b>2.09</b> (1.47-3.01)	<b>2.34</b> (1.59-3.48)
6-hr	<b>0.575</b> (0.474-0.704)	<b>0.763</b> (0.628-0.935)	<b>1.02</b> (0.836-1.25)	<b>1.23</b> (1.00-1.53)	<b>1.53</b> (1.21-1.96)	<b>1.77</b> (1.37-2.32)	<b>2.02</b> (1.52-2.71)	<b>2.29</b> (1.68-3.15)	<b>2.65</b> (1.87-3.81)	<b>2.95</b> (2.01-4.38)
12-hr	<b>0.726</b> (0.599-0.889)	<b>0.975</b> (0.803-1.20)	<b>1.31</b> (1.07-1.61)	<b>1.58</b> (1.29-1.96)	<b>1.96</b> (1.54-2.50)	<b>2.25</b> (1.74-2.94)	<b>2.55</b> (1.92-3.42)	<b>2.87</b> (2.10-3.95)	<b>3.30</b> (2.32-4.73)	<b>3.63</b> (2.47-5.39)
24-hr	<b>0.912</b> (0.809-1.05)	<b>1.25</b> (1.10-1.43)	<b>1.68</b> (1.49-1.94)	<b>2.04</b> (1.79-2.38)	<b>2.52</b> (2.14-3.04)	<b>2.90</b> (2.40-3.56)	<b>3.28</b> (2.65-4.13)	<b>3.67</b> (2.89-4.75)	<b>4.19</b> (3.17-5.66)	<b>4.60</b> (3.36-6.43)
2-day	<b>1.05</b> (0.926-1.20)	<b>1.45</b> (1.28-1.67)	<b>1.99</b> (1.75-2.29)	<b>2.42</b> (2.12-2.82)	<b>3.02</b> (2.56-3.64)	<b>3.48</b> (2.89-4.28)	<b>3.95</b> (3.20-4.98)	<b>4.44</b> (3.49-5.75)	<b>5.09</b> (3.85-6.88)	<b>5.61</b> (4.09-7.83)
3-day	<b>1.14</b> (1.01-1.31)	<b>1.60</b> (1.41-1.84)	<b>2.20</b> (1.94-2.54)	<b>2.70</b> (2.36-3.14)	<b>3.37</b> (2.86-4.06)	<b>3.90</b> (3.24-4.79)	<b>4.43</b> (3.59-5.58)	<b>4.99</b> (3.93-6.46)	<b>5.75</b> (4.34-7.76)	<b>6.34</b> (4.63-8.86)
4-day	<b>1.21</b> (1.08-1.40)	<b>1.70</b> (1.50-1.96)	<b>2.34</b> (2.07-2.71)	<b>2.87</b> (2.52-3.34)	<b>3.59</b> (3.04-4.32)	<b>4.14</b> (3.44-5.09)	<b>4.71</b> (3.82-5.93)	<b>5.30</b> (4.17-6.86)	<b>6.09</b> (4.60-8.22)	<b>6.71</b> (4.90-9.37)
7-day	<b>1.30</b> (1.15-1.49)	<b>1.80</b> (1.60-2.08)	<b>2.47</b> (2.18-2.85)	<b>3.01</b> (2.64-3.51)	<b>3.75</b> (3.17-4.51)	<b>4.31</b> (3.57-5.29)	<b>4.87</b> (3.94-6.13)	<b>5.45</b> (4.29-7.05)	<b>6.22</b> (4.70-8.40)	<b>6.81</b> (4.97-9.52)
10-day	<b>1.36</b> (1.21-1.57)	<b>1.89</b> (1.67-2.17)	<b>2.58</b> (2.28-2.98)	<b>3.14</b> (2.75-3.65)	<b>3.89</b> (3.30-4.68)	<b>4.46</b> (3.71-5.49)	<b>5.04</b> (4.08-6.35)	<b>5.62</b> (4.43-7.28)	<b>6.40</b> (4.84-8.65)	<b>7.00</b> (5.11-9.77)
20-day	<b>1.54</b> (1.37-1.78)	<b>2.16</b> (1.92-2.49)	<b>2.99</b> (2.64-3.45)	<b>3.67</b> (3.21-4.27)	<b>4.59</b> (3.89-5.53)	<b>5.30</b> (4.40-6.52)	<b>6.02</b> (4.88-7.58)	<b>6.75</b> (5.32-8.74)	<b>7.73</b> (5.84-10.4)	<b>8.47</b> (6.18-11.8)
30-day	<b>1.73</b> (1.53-1.99)	<b>2.45</b> (2.17-2.82)	<b>3.44</b> (3.04-3.97)	<b>4.26</b> (3.73-4.96)	<b>5.41</b> (4.59-6.51)	<b>6.31</b> (5.24-7.75)	<b>7.23</b> (5.85-9.10)	<b>8.18</b> (6.44-10.6)	<b>9.46</b> (7.15-12.8)	<b>10.5</b> (7.63-14.6)
45-day	<b>1.99</b> (1.77-2.29)	<b>2.86</b> (2.54-3.30)	<b>4.08</b> (3.61-4.72)	<b>5.13</b> (4.49-5.97)	<b>6.64</b> (5.62-7.99)	<b>7.85</b> (6.52-9.65)	<b>9.12</b> (7.39-11.5)	<b>10.5</b> (8.24-13.5)	<b>12.3</b> (9.32-16.6)	<b>13.8</b> (10.1-19.3)
60-day	<b>2.15</b> (1.91-2.47)	<b>3.11</b> (2.76-3.59)	<b>4.50</b> (3.98-5.20)	<b>5.73</b> (5.02-6.67)	<b>7.53</b> (6.38-9.06)	<b>9.01</b> (7.48-11.1)	<b>10.6</b> (8.59-13.4)	<b>12.3</b> (9.71-16.0)	<b>14.8</b> (11.2-19.9)	<b>16.8</b> (12.2-23.4)

<sup>1</sup> Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

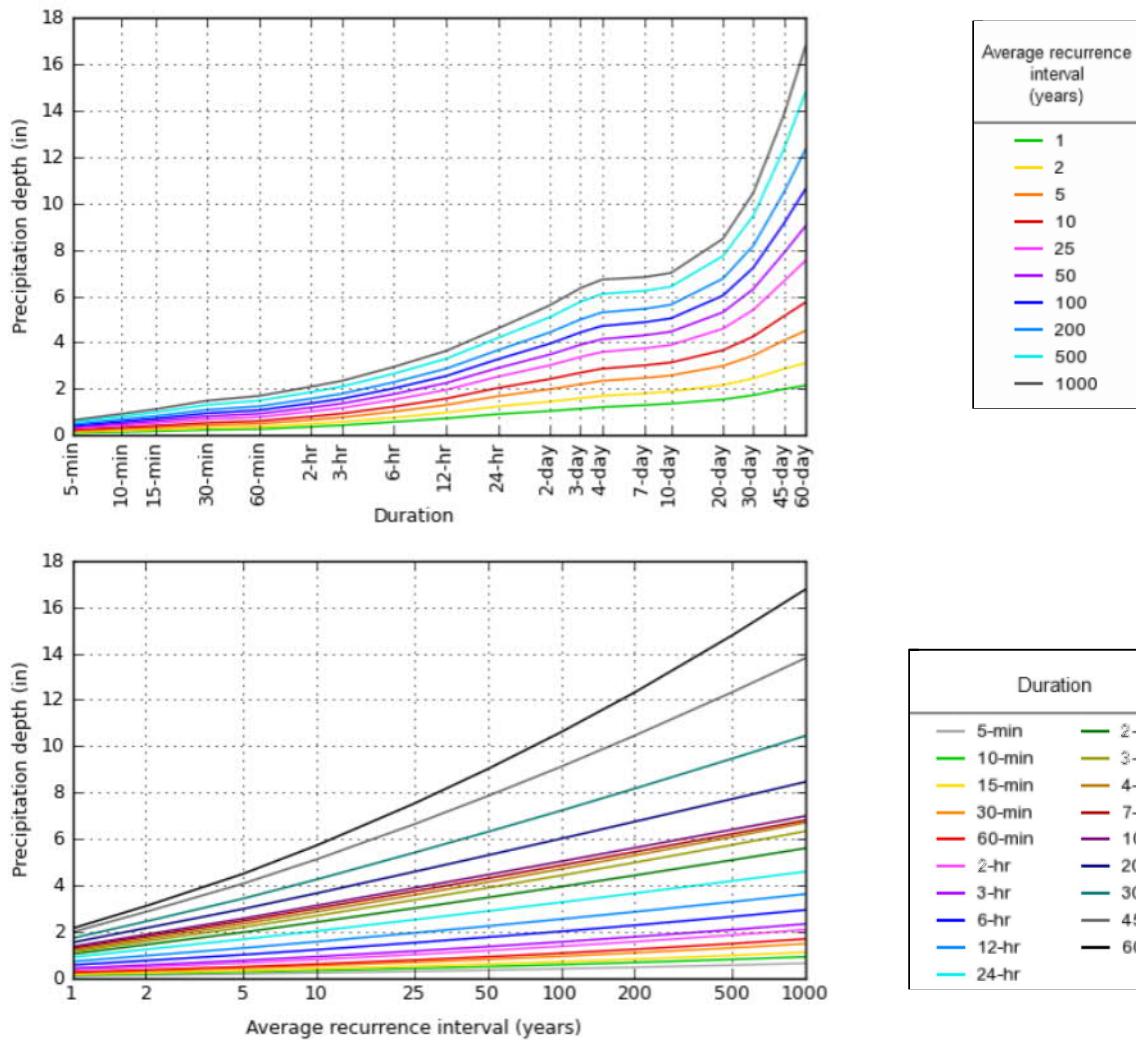
Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values.

Please refer to NOAA Atlas 14 document for more information.

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## PF graphical

PDS-based depth-duration-frequency (DDF) curves  
Latitude: 34.5631°, Longitude: -117.3169°

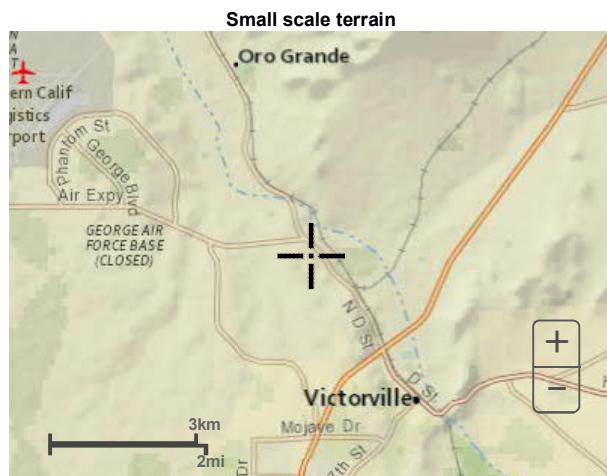


NOAA Atlas 14, Volume 6, Version 2

Created (GMT): Sat May 11 23:16:55 2019

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## Maps & aerials



**Large scale terrain**



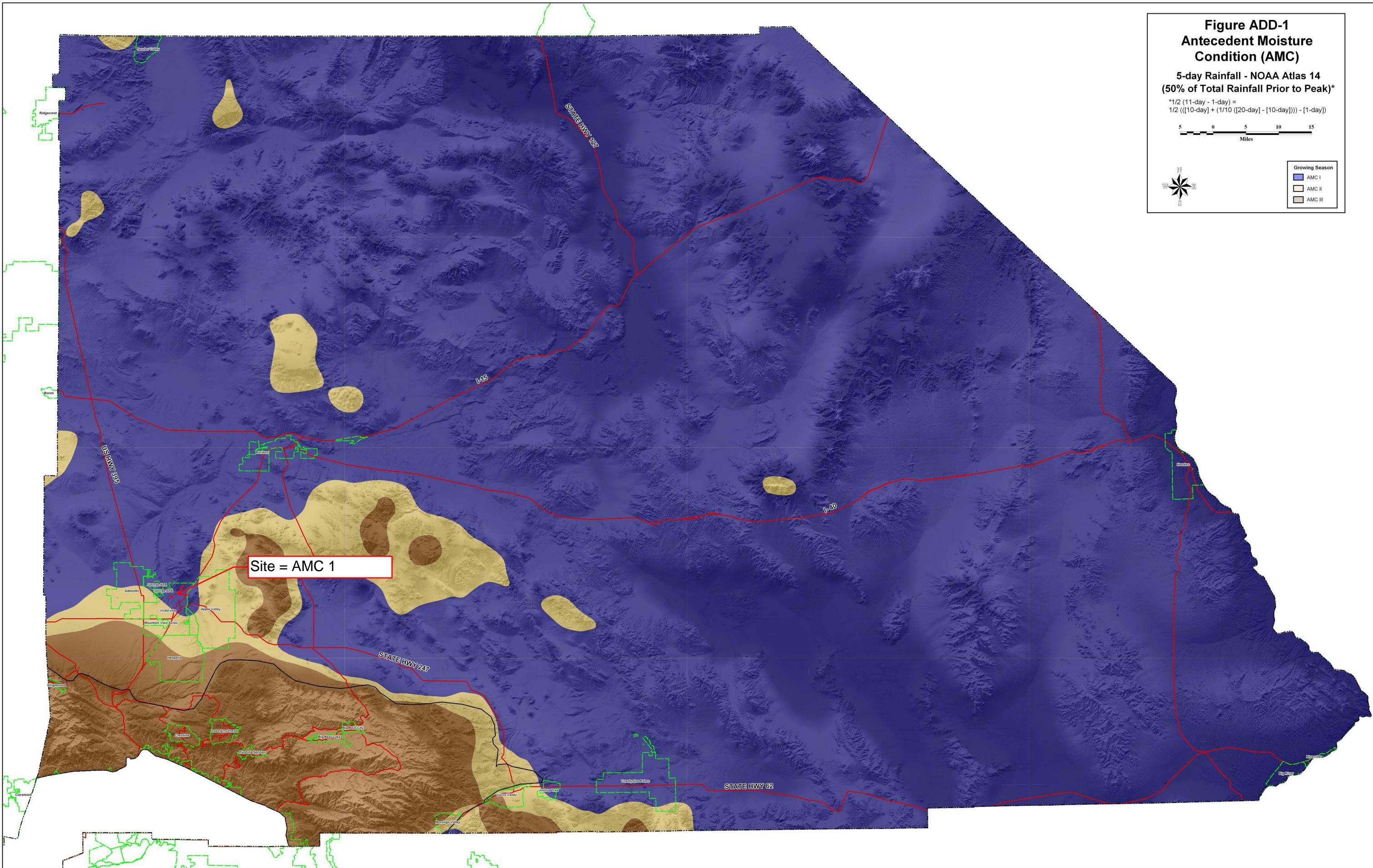
**Large scale map**



**Large scale aerial**



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SBCHM Soils Exhibit



## Rational Methods

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RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
 (Reference: 1986 SAN BERNARDINO CO. HYDROLOGY CRITERION)  
 (c) Copyright 1983-2011 Advanced Engineering Software (aes)  
 Ver. 18.0 Release Date: 07/01/2011 License ID 1501

Analysis prepared by:

JE Miller & Associates  
 17995 Outer Highway 18, Suite 1  
 Apple Valley, CA 92307

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\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*

\* APN 0472-131-03, 04, 08, 10, 13, 16, 17 & 0472-141-16 \*

\* Existing Condition \*

\* 100 Year Storm Event \*

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FILE NAME: 0472E.DAT

TIME/DATE OF STUDY: 10:27 08/25/2019

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USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:

=====

--\*TIME-OF-CONCENTRATION MODEL\*--

USER SPECIFIED STORM EVENT(YEAR) = 100.00

SPECIFIED MINIMUM PIPE SIZE(INCH) = 12.00

SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90

\*USER-DEFINED LOGARITHMIC INTERPOLATION USED FOR RAINFALL\*

SLOPE OF INTENSITY DURATION CURVE(LOG(I; IN/HR) vs. LOG(Tc; MIN)) = 0.7000  
 USER SPECIFIED 1-HOUR INTENSITY(INCH/HOUR) = 1.0800

\*ANTECEDENT MOISTURE CONDITION (AMC) I ASSUMED FOR RATIONAL METHOD\*

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

NO.	HALF-CROWN TO STREET-CROSSFALL:		CURB GUTTER-GEOMETRIES:			MANNING	
	WIDTH	CROSSFALL	IN-/OUT-/PARK-	HEIGHT	WIDTH	LIP	HKE
	(FT)	(FT)	SIDE / SIDE/WAY	(FT)	(FT)	(FT)	(n)
1	30.0	20.0	0.018/0.018/0.020	0.67	2.00	0.0312	0.167 0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET

as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)

2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
 OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

0472E100. RES

\*USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

\*\*\*\*\*  
FLOW PROCESS FROM NODE 0.00 TO NODE 0.50 IS CODE = 21

----->>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====INITIAL SUBAREA FLOW-LENGTH(FEET) = 700.00

ELEVATION DATA: UPSTREAM(FEET) = 2809.40 DOWNSTREAM(FEET) = 2743.00

Tc = K\*[(LENGTH\*\* 3.00)/(ELEVATION CHANGE)]\*\*0.20

SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 11.555

\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 3.421

SUBAREA Tc AND LOSS RATE DATA(AMC I):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
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NATURAL DESERT COVER

"DESERT BRUSH" (15.0%) C 2.00 0.43 1.000 76 11.56

SUBAREA AVERAGE PERVERIOUS LOSS RATE, Fp(INCH/HR) = 0.43

SUBAREA AVERAGE PERVERIOUS AREA FRACTION, Ap = 1.000

SUBAREA RUNOFF(CFS) = 5.39

TOTAL AREA(ACRES) = 2.00 PEAK FLOW RATE(CFS) = 5.39

\*\*\*\*\*  
FLOW PROCESS FROM NODE 0.50 TO NODE 1.00 IS CODE = 51

----->>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<

>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<

=====ELEVATION DATA: UPSTREAM(FEET) = 2745.00 DOWNSTREAM(FEET) = 2743.00

CHANNEL LENGTH THRU SUBAREA(FEET) = 254.00 CHANNEL SLOPE = 0.0079

CHANNEL BASE(FEET) = 0.00 "Z" FACTOR = 2.000

MANNING'S FACTOR = 0.025 MAXIMUM DEPTH(FEET) = 5.00

CHANNEL FLOW THRU SUBAREA(CFS) = 5.39

FLOW VELOCITY(FEET/SEC.) = 2.98 FLOW DEPTH(FEET) = 0.95

TRAVEL TIME(MIN.) = 1.42 Tc(MIN.) = 12.98

LONGEST FLOWPATH FROM NODE 0.00 TO NODE 1.00 = 954.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1.00 TO NODE 1.00 IS CODE = 1

----->>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

=====TOTAL NUMBER OF STREAMS = 2

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:

TIME OF CONCENTRATION(MIN.) = 12.98

RAINFALL INTENSITY(INCH/HR) = 3.15

AREA-AVERAGED Fm(INCH/HR) = 0.43

AREA-AVERAGED Fp(INCH/HR) = 0.43

AREA-AVERAGED Ap = 1.00

EFFECTIVE STREAM AREA(ACRES) = 2.00

TOTAL STREAM AREA(ACRES) = 2.00

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PEAK FLOW RATE(CFS) AT CONFLUENCE = 5.39

\*\*\*\*\*  
FLOW PROCESS FROM NODE 0.00 TO NODE 1.00 IS CODE = 21  
\*\*\*\*\*

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<  
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

INITIAL SUBAREA FLOW-LENGTH(FEET) = 651.00  
ELEVATION DATA: UPSTREAM(FEET) = 2809.40 DOWNSTREAM(FEET) = 2743.00

Tc = K\*[(LENGTH\*\* 3.00)/(ELEVATION CHANGE)]\*\*0.20

SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 11.063

\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 3.527

SUBAREA Tc AND LOSS RATE DATA(AMC I):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
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NATURAL DESERT COVER

"DESERT BRUSH" (15.0%) C 2.80 0.43 1.000 76 11.06

SUBAREA AVERAGE PERVERIOUS LOSS RATE, Fp(INCH/HR) = 0.43

SUBAREA AVERAGE PERVERIOUS AREA FRACTION, Ap = 1.000

SUBAREA RUNOFF(CFS) = 7.81

TOTAL AREA(ACRES) = 2.80 PEAK FLOW RATE(CFS) = 7.81

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1.00 TO NODE 1.00 IS CODE = 1  
\*\*\*\*\*

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<

TOTAL NUMBER OF STREAMS = 2

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:

TIME OF CONCENTRATION(MIN.) = 11.06

RAINFALL INTENSITY(INCH/HR) = 3.53

AREA-AVERAGED Fm(INCH/HR) = 0.43

AREA-AVERAGED Fp(INCH/HR) = 0.43

AREA-AVERAGED Ap = 1.00

EFFECTIVE STREAM AREA(ACRES) = 2.80

TOTAL STREAM AREA(ACRES) = 2.80

PEAK FLOW RATE(CFS) AT CONFLUENCE = 7.81

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	5.39	12.98	3.155	0.43( 0.43)	1.00	2.0	0.00
2	7.81	11.06	3.527	0.43( 0.43)	1.00	2.8	0.00

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO

CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
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1	13.04	11.06	3.527	0.43( 0.43)	1.00	4.5	0.00
2	12.27	12.98	3.155	0.43( 0.43)	1.00	4.8	0.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 13.04 Tc(MIN.) = 11.06

EFFECTIVE AREA(ACRES) = 4.51 AREA-AVERAGED Fm(INCH/HR) = 0.43

AREA-AVERAGED Fp(INCH/HR) = 0.43 AREA-AVERAGED Ap = 1.00

TOTAL AREA(ACRES) = 4.8

LONGEST FLOWPATH FROM NODE 0.00 TO NODE 1.00 = 954.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1.00 TO NODE 4.00 IS CODE = 51

-----

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<

>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 2743.00 DOWNSTREAM(FEET) = 2740.00

CHANNEL LENGTH THRU SUBAREA(FEET) = 160.00 CHANNEL SLOPE = 0.0188

CHANNEL BASE(FEET) = 0.00 "Z" FACTOR = 2.000

MANNING'S FACTOR = 0.025 MAXIMUM DEPTH(FEET) = 5.00

CHANNEL FLOW THRU SUBAREA(CFS) = 13.04

FLOW VELOCITY(FEET/SEC.) = 5.16 FLOW DEPTH(FEET) = 1.12

TRAVEL TIME(MIN.) = 0.52 Tc(MIN.) = 11.58

LONGEST FLOWPATH FROM NODE 0.00 TO NODE 4.00 = 1114.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 4.00 TO NODE 4.00 IS CODE = 1

-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

=====

TOTAL NUMBER OF STREAMS = 2

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:

TIME OF CONCENTRATION(MIN.) = 11.58

RAINFALL INTENSITY(INCH/HR) = 3.42

AREA-AVERAGED Fm(INCH/HR) = 0.43

AREA-AVERAGED Fp(INCH/HR) = 0.43

AREA-AVERAGED Ap = 1.00

EFFECTIVE STREAM AREA(ACRES) = 4.51

TOTAL STREAM AREA(ACRES) = 4.80

PEAK FLOW RATE(CFS) AT CONFLUENCE = 13.04

\*\*\*\*\*

FLOW PROCESS FROM NODE 2.00 TO NODE 3.00 IS CODE = 21

-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 700.00

ELEVATION DATA: UPSTREAM(FEET) = 2802.00 DOWNSTREAM(FEET) = 2765.70

Tc = K\*[(LENGTH\*\* 3.00)/(ELEVATION CHANGE)]\*\*0.20

SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 13.039

\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 3.144

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SUBAREA Tc AND LOSS RATE DATA(AMC I ):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN. )
NATURAL DESERT COVER						
"DESERT BRUSH" (15.0%)	C	5.90	0.43	1.000	76	13.04
SUBAREA AVERAGE PEROVIOUS LOSS RATE, Fp(INCH/HR) =			0.43			
SUBAREA AVERAGE PEROVIOUS AREA FRACTION, Ap =				1.000		
SUBAREA RUNOFF(CFS) =		14.43				
TOTAL AREA(ACRES) =		5.90	PEAK FLOW RATE(CFS) =		14.43	

\*\*\*\*\*

FLOW PROCESS FROM NODE 3.00 TO NODE 4.00 IS CODE = 51

-----

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 2765.70 DOWNSTREAM(FEET) = 2740.00  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 400.00 CHANNEL SLOPE = 0.0642  
 CHANNEL BASE(FEET) = 25.00 "Z" FACTOR = 2.000  
 MANNING'S FACTOR = 0.025 MAXIMUM DEPTH(FEET) = 2.00  
 \* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 2.906

SUBAREA LOSS RATE DATA(AMC I ):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
NATURAL DESERT COVER					
"DESERT BRUSH" (15.0%)	C	2.20	0.43	1.000	76
SUBAREA AVERAGE PEROVIOUS LOSS RATE, Fp(INCH/HR) =			0.43		
SUBAREA AVERAGE PEROVIOUS AREA FRACTION, Ap =				1.000	
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) =				16.89	
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) =				4.29	
AVERAGE FLOW DEPTH(FEET) =		0.16	TRAVEL TIME(MIN. ) =		1.55
Tc(MIN. ) =		14.59			
SUBAREA AREA(ACRES) =		2.20	SUBAREA RUNOFF(CFS) =		4.91
EFFECTIVE AREA(ACRES) =		8.10	AREA-AVERAGED Fm(INCH/HR) =		0.43
AREA-AVERAGED Fp(INCH/HR) =		0.43	AREA-AVERAGED Ap =		1.00
TOTAL AREA(ACRES) =		8.1	PEAK FLOW RATE(CFS) =		18.08

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.16 FLOW VELOCITY(FEET/SEC.) = 4.38  
 LONGEST FLOWPATH FROM NODE 2.00 TO NODE 4.00 = 1100.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 4.00 TO NODE 4.00 IS CODE = 1

-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<

=====

TOTAL NUMBER OF STREAMS = 2

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:

TIME OF CONCENTRATION(MIN. ) = 14.59  
 RAINFALL INTENSITY(INCH/HR) = 2.91  
 AREA-AVERAGED Fm(INCH/HR) = 0.43  
 AREA-AVERAGED Fp(INCH/HR) = 0.43

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AREA-AVERAGED Ap = 1.00  
 EFFECTIVE STREAM AREA(ACRES) = 8.10  
 TOTAL STREAM AREA(ACRES) = 8.10  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 18.08

## \*\* CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	13.04	11.58	3.416	0.43( 0.43)	1.00	4.5	0.00
1	12.27	13.50	3.068	0.43( 0.43)	1.00	4.8	0.00
2	18.08	14.59	2.906	0.43( 0.43)	1.00	8.1	2.00

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

## \*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	30.34	11.58	3.416	0.43( 0.43)	1.00	10.9	0.00
2	30.09	13.50	3.068	0.43( 0.43)	1.00	12.3	0.00
3	29.59	14.59	2.906	0.43( 0.43)	1.00	12.9	2.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 30.34 Tc(MIN.) = 11.58  
 EFFECTIVE AREA(ACRES) = 10.93 AREA-AVERAGED Fm(INCH/HR) = 0.43  
 AREA-AVERAGED Fp(INCH/HR) = 0.43 AREA-AVERAGED Ap = 1.00  
 TOTAL AREA(ACRES) = 12.9  
 LONGEST FLOWPATH FROM NODE 0.00 TO NODE 4.00 = 1114.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 4.00 TO NODE 8.00 IS CODE = 51

-----

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<  
 >>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 2740.00 DOWNSTREAM(FEET) = 2723.00  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 305.00 CHANNEL SLOPE = 0.0557  
 CHANNEL BASE(FEET) = 0.00 "Z" FACTOR = 2.000  
 MANNING'S FACTOR = 0.025 MAXIMUM DEPTH(FEET) = 5.00  
 CHANNEL FLOW THRU SUBAREA(CFS) = 30.34  
 FLOW VELOCITY(FEET/SEC.) = 9.53 FLOW DEPTH(FEET) = 1.26  
 TRAVEL TIME(MIN.) = 0.53 Tc(MIN.) = 12.11  
 LONGEST FLOWPATH FROM NODE 0.00 TO NODE 8.00 = 1419.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 8.00 TO NODE 8.00 IS CODE = 1

-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
 TIME OF CONCENTRATION(MIN.) = 12.11  
 RAINFALL INTENSITY(INCH/HR) = 3.31

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AREA-AVERAGED  $F_m$ (INCH/HR) = 0.43  
 AREA-AVERAGED  $F_p$ (INCH/HR) = 0.43  
 AREA-AVERAGED  $A_p$  = 1.00  
 EFFECTIVE STREAM AREA(ACRES) = 10.93  
 TOTAL STREAM AREA(ACRES) = 12.90  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 30.34

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 5.00 TO NODE 6.00 IS CODE = 21

-----  
 >>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<  
 >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====  
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 700.00  
 ELEVATION DATA: UPSTREAM(FEET) = 2812.00 DOWNSTREAM(FEET) = 2772.00

$T_c = K * [(LENGTH^{**} 3.00) / (ELEVATION CHANGE)]^{**} 0.20$

SUBAREA ANALYSIS USED MINIMUM  $T_c$ (MIN.) = 12.788

\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 3.187

SUBAREA  $T_c$  AND LOSS RATE DATA(AMC I):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	$F_p$ (INCH/HR)	$A_p$ (DECIMAL)	SCS CN	$T_c$ (MIN.)
NATURAL DESERT COVER						
"DESERT BRUSH" (15.0%)	C	3.90	0.43	1.000	76	12.79
SUBAREA AVERAGE PREVIOUS LOSS RATE, $F_p$ (INCH/HR)						
SUBAREA AVERAGE PREVIOUS AREA FRACTION, $A_p$						
SUBAREA RUNOFF(CFS)		9.69				
TOTAL AREA(ACRES)		3.90	PEAK FLOW RATE(CFS)			9.69

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 6.00 TO NODE 7.00 IS CODE = 51

-----  
 >>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<  
 >>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<

=====  
 ELEVATION DATA: UPSTREAM(FEET) = 2772.00 DOWNSTREAM(FEET) = 2741.00

CHANNEL LENGTH THRU SUBAREA(FEET) = 540.00 CHANNEL SLOPE = 0.0574

CHANNEL BASE(FEET) = 1.00 "Z" FACTOR = 2.000

MANNING'S FACTOR = 0.025 MAXIMUM DEPTH(FEET) = 3.00

\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 3.015

SUBAREA LOSS RATE DATA(AMC I):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	$F_p$ (INCH/HR)	$A_p$ (DECIMAL)	SCS CN
NATURAL DESERT COVER					
"DESERT BRUSH" (15.0%)	C	7.80	0.43	1.000	76
SUBAREA AVERAGE PREVIOUS LOSS RATE, $F_p$ (INCH/HR)					
SUBAREA AVERAGE PREVIOUS AREA FRACTION, $A_p$					
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS)				18.79	
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.)				8.56	
AVERAGE FLOW DEPTH(FEET)		0.83	TRAVEL TIME(MIN.)		1.05
$T_c$ (MIN.)		13.84			
SUBAREA AREA(ACRES)		7.80	SUBAREA RUNOFF(CFS)		18.18
EFFECTIVE AREA(ACRES)		11.70	AREA-AVERAGED $F_m$ (INCH/HR)		0.43

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AREA-AVERAGED Fp(INCH/HR) = 0.43 AREA-AVERAGED Ap = 1.00  
TOTAL AREA(ACRES) = 11.7 PEAK FLOW RATE(CFS) = 27.27

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.98 FLOW VELOCITY(FEET/SEC.) = 9.41  
LONGEST FLOWPATH FROM NODE 5.00 TO NODE 7.00 = 1240.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 7.00 TO NODE 8.00 IS CODE = 51

----->>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<

>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 2741.00 DOWNSTREAM(FEET) = 2723.00

CHANNEL LENGTH THRU SUBAREA(FEET) = 280.00 CHANNEL SLOPE = 0.0643

CHANNEL BASE(FEET) = 1.00 "Z" FACTOR = 2.000

MANNING'S FACTOR = 0.025 MAXIMUM DEPTH(FEET) = 3.00

\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 2.947

SUBAREA LOSS RATE DATA(AMC I):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
NATURAL DESERT COVER					
"DESERT BRUSH" (15.0%)	C	2.40	0.43	1.000	76
SUBAREA AVERAGE PREVIOUS LOSS RATE, Fp(INCH/HR)					0.43
SUBAREA AVERAGE PREVIOUS AREA FRACTION, Ap					1.000
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS)					29.99
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.)					10.09
AVERAGE FLOW DEPTH(FEET)		0.99	TRAVEL TIME(MIN.)		0.46
Tc(MIN.)		14.30			
SUBAREA AREA(ACRES)		2.40	SUBAREA RUNOFF(CFS)		5.44
EFFECTIVE AREA(ACRES)		14.10	AREA-AVERAGED Fm(INCH/HR)		0.43
AREA-AVERAGED Fp(INCH/HR)		0.43	AREA-AVERAGED Ap		1.00
TOTAL AREA(ACRES)		14.1	PEAK FLOW RATE(CFS)		31.99

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 1.03 FLOW VELOCITY(FEET/SEC.) = 10.23  
LONGEST FLOWPATH FROM NODE 5.00 TO NODE 8.00 = 1520.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 8.00 TO NODE 8.00 IS CODE = 81

----->>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<

=====

MAINLINE Tc(MIN.) = 14.30

\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 2.947

SUBAREA LOSS RATE DATA(AMC I):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
NATURAL DESERT COVER					
"DESERT BRUSH" (15.0%)	C	1.25	0.43	1.000	76
SUBAREA AVERAGE PREVIOUS LOSS RATE, Fp(INCH/HR)					0.43
SUBAREA AVERAGE PREVIOUS AREA FRACTION, Ap					1.000
SUBAREA AREA(ACRES)		1.25	SUBAREA RUNOFF(CFS)		2.84

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EFFECTIVE AREA(ACRES) = 15.35 AREA-AVERAGED Fm(INCH/HR) = 0.43  
AREA-AVERAGED Fp(INCH/HR) = 0.43 AREA-AVERAGED Ap = 1.00  
TOTAL AREA(ACRES) = 15.4 PEAK FLOW RATE(CFS) = 34.83

\*\*\*\*\*  
FLOW PROCESS FROM NODE 8.00 TO NODE 8.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<

=====  
TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 14.30  
RAINFALL INTENSITY(INCH/HR) = 2.95  
AREA-AVERAGED Fm(INCH/HR) = 0.43  
AREA-AVERAGED Fp(INCH/HR) = 0.43  
AREA-AVERAGED Ap = 1.00  
EFFECTIVE STREAM AREA(ACRES) = 15.35  
TOTAL STREAM AREA(ACRES) = 15.35  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 34.83

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	30.34	12.11	3.310	0.43( 0.43)	1.00	10.9	0.00
1	30.09	14.04	2.986	0.43( 0.43)	1.00	12.3	0.00
1	29.59	15.13	2.834	0.43( 0.43)	1.00	12.9	2.00
2	34.83	14.30	2.947	0.43( 0.43)	1.00	15.4	5.00

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	64.09	12.11	3.310	0.43( 0.43)	1.00	23.9	0.00
2	64.79	14.04	2.986	0.43( 0.43)	1.00	27.4	0.00
3	64.79	14.30	2.947	0.43( 0.43)	1.00	27.8	5.00
4	62.85	15.13	2.834	0.43( 0.43)	1.00	28.2	2.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 64.79 Tc(MIN.) = 14.04  
EFFECTIVE AREA(ACRES) = 27.36 AREA-AVERAGED Fm(INCH/HR) = 0.43  
AREA-AVERAGED Fp(INCH/HR) = 0.43 AREA-AVERAGED Ap = 1.00  
TOTAL AREA(ACRES) = 28.2

LONGEST FLOWPATH FROM NODE 5.00 TO NODE 8.00 = 1520.00 FEET.

=====  
END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 28.2 TC(MIN.) = 14.04  
EFFECTIVE AREA(ACRES) = 27.36 AREA-AVERAGED Fm(INCH/HR) = 0.43  
AREA-AVERAGED Fp(INCH/HR) = 0.43 AREA-AVERAGED Ap = 1.000  
PEAK FLOW RATE(CFS) = 64.79

## 0472E100. RES

## \*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	64.09	12.11	3.310	0.43( 0.43)	1.00	23.9	0.00
2	64.79	14.04	2.986	0.43( 0.43)	1.00	27.4	0.00
3	64.79	14.30	2.947	0.43( 0.43)	1.00	27.8	5.00
4	62.85	15.13	2.834	0.43( 0.43)	1.00	28.2	2.00

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END OF RATIONAL METHOD ANALYSIS

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RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
(Reference: 1986 SAN BERNARDINO CO. HYDROLOGY CRITERION)  
(c) Copyright 1983-2011 Advanced Engineering Software (aes)  
Ver. 18.0 Release Date: 07/01/2011 License ID 1501

Analysis prepared by:

JE Miller & Associates  
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Apple Valley, CA 92307

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*

\* APN 0472-131-03, 04, 08, 10, 13, 16, 17 & 0472-141-16 \*  
\* Developed Condition \*  
\* 100 Year Storm Event \*

FILE NAME: RE.DAT

TIME/DATE OF STUDY: 11:50 08/25/2019

===== USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:

---\*TIME-OF-CONCENTRATION MODEL\*---

USER SPECIFIED STORM EVENT(YEAR) = 100.00

SPECIFIED MINIMUM PIPE SIZE(INCH) = 6.00

SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90

\*USER-DEFINED LOGARITHMIC INTERPOLATION USED FOR RAINFALL\*

SLOPE OF INTENSITY DURATION CURVE(LOG(I; IN/HR) vs. LOG(Tc; MIN)) = 0.7000

USER SPECIFIED 1-HOUR INTENSITY(INCH/HOUR) = 1.0800

\*ANTECEDENT MOISTURE CONDITION (AMC) I ASSUMED FOR RATIONAL METHOD\*

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

NO.	HALF-CROWN TO WIDTH	CROSSFALL	STREET-CROSSFALL: IN- / OUT-/PARK- SIDE / SIDE/ WAY	CURB HEIGHT	GUTTER-GEOMETRIES: WIDTH	LIP	HIKE FACTOR	MANNING (n)
1	30.0	20.0	0.018/0.018/0.020	0.67	2.00	0.0313	0.167	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

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1. Relative Flow-Depth = 0.00 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

\*\*\*\*\*

FLOW PROCESS FROM NODE 10.00 TO NODE 11.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<  
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

INITIAL SUBAREA FLOW-LENGTH(FEET) = 704.00  
ELEVATION DATA: UPSTREAM(FEET) = 2788.60 DOWNSTREAM(FEET) = 2746.00

Tc = K\*[(LENGTH\*\* 3.00)/(ELEVATION CHANGE)]\*\*0.20

SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 12.671

\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 3.207

SUBAREA Tc AND LOSS RATE DATA(AMC 1):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
NATURAL DESERT COVER						
"DESERT BRUSH" (15.0%)	C	0.81	0.43	1.000	76	12.67
SUBAREA AVERAGE PREVIOUS LOSS RATE, Fp(INCH/HR)						
SUBAREA AVERAGE PREVIOUS AREA FRACTION, Ap						
SUBAREA RUNOFF(CFS)		2.03				
TOTAL AREA(ACRES)		0.81	PEAK FLOW RATE(CFS)	=	2.03	

\*\*\*\*\*

FLOW PROCESS FROM NODE 11.00 TO NODE 14.00 IS CODE = 52

>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<

ELEVATION DATA: UPSTREAM(FEET) = 2746.00 DOWNSTREAM(FEET) = 2744.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 140.00 CHANNEL SLOPE = 0.0143  
CHANNEL FLOW THRU SUBAREA(CFS) = 2.03  
FLOW VELOCITY(FEET/SEC) = 2.06 (PER LACFC/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 1.13 Tc(MIN.) = 13.80  
LONGEST FLOWPATH FROM NODE 10.00 TO NODE 14.00 = 844.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 14.00 TO NODE 14.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<

MAINLINE Tc(MIN.) = 13.80  
\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 3.021

RE. RES

SUBAREA LOSS RATE DATA(AMC I ):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
NATURAL DESERT COVER					
"DESERT BRUSH" (15.0%)	C	0.25	0.43	1.000	76
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) =			0.43		
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap =			1.000		
SUBAREA AREA(ACRES) =	0.25	SUBAREA RUNOFF(CFS) =	0.58		
EFFECTIVE AREA(ACRES) =	1.06	AREA-AVERAGED Fm(INCH/HR) =	0.43		
AREA-AVERAGED Fp(INCH/HR) =	0.43	AREA-AVERAGED Ap =	1.00		
TOTAL AREA(ACRES) =	1.1	PEAK FLOW RATE(CFS) =	2.48		

\*\*\*\*\*

FLOW PROCESS FROM NODE 14.00 TO NODE 14.00 IS CODE = 1

-----

>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<

=====

TOTAL NUMBER OF STREAMS = 2

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:

TIME OF CONCENTRATION(MIN.) = 13.80

RAINFALL INTENSITY(INCH/HR) = 3.02

AREA-AVERAGED Fm(INCH/HR) = 0.43

AREA-AVERAGED Fp(INCH/HR) = 0.43

AREA-AVERAGED Ap = 1.00

EFFECTIVE STREAM AREA(ACRES) = 1.06

TOTAL STREAM AREA(ACRES) = 1.06

PEAK FLOW RATE(CFS) AT CONFLUENCE = 2.48

\*\*\*\*\*

FLOW PROCESS FROM NODE 12.00 TO NODE 13.00 IS CODE = 21

-----

>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<

>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 504.00

ELEVATION DATA: UPSTREAM(FEET) = 2788.00 DOWNSTREAM(FEET) = 2769.12

Tc = K\*[(LENGTH\*\* 3.00)/(ELEVATION CHANGE)]\*\*0.20

SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 12.202

\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 3.293

SUBAREA Tc AND LOSS RATE DATA(AMC I ):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
NATURAL DESERT COVER						
"DESERT BRUSH" (15.0%)	C	4.56	0.43	1.000	76	12.20
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) =			0.43			
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap =			1.000			
SUBAREA RUNOFF(CFS) =		11.77				
TOTAL AREA(ACRES) =	4.56	PEAK FLOW RATE(CFS) =	11.77			

RE. RES

\*\*\*\*\*

FLOW PROCESS FROM NODE 13.00 TO NODE 14.00 IS CODE = 51

-----

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<

>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 2769.12 DOWNSTREAM(FEET) = 2744.00

CHANNEL LENGTH THRU SUBAREA(FEET) = 275.00 CHANNEL SLOPE = 0.0913

CHANNEL BASE(FEET) = 1.00 "Z" FACTOR = 2.000

MANNING'S FACTOR = 0.025 MAXIMUM DEPTH(FEET) = 4.00

\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 3.201

SUBAREA LOSS RATE DATA(AMC I):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
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NATURAL DESERT COVER

"DESERT BRUSH" (15.0%) C 0.18 0.43 1.000 76

SUBAREA AVERAGE PEROVIOUS LOSS RATE, Fp(INCH/HR) = 0.43

SUBAREA AVERAGE PEROVIOUS AREA FRACTION, Ap = 1.000

TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 11.99

TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 9.09

AVERAGE FLOW DEPTH(FEET) = 0.60 TRAVEL TIME(MIN.) = 0.50

Tc(MIN.) = 12.71

SUBAREA AREA(ACRES) = 0.18 SUBAREA RUNOFF(CFS) = 0.45

EFFECTIVE AREA(ACRES) = 4.74 AREA-AVERAGED Fm(INCH/HR) = 0.43

AREA-AVERAGED Fp(INCH/HR) = 0.43 AREA-AVERAGED Ap = 1.00

TOTAL AREA(ACRES) = 4.7 PEAK FLOW RATE(CFS) = 11.84

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.60 FLOW VELOCITY(FEET/SEC.) = 9.02

LONGEST FLOWPATH FROM NODE 12.00 TO NODE 14.00 = 779.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 14.00 TO NODE 14.00 IS CODE = 1

-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<

=====

TOTAL NUMBER OF STREAMS = 2

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:

TIME OF CONCENTRATION(MIN.) = 12.71

RAINFALL INTENSITY(INCH/HR) = 3.20

AREA-AVERAGED Fm(INCH/HR) = 0.43

AREA-AVERAGED Fp(INCH/HR) = 0.43

AREA-AVERAGED Ap = 1.00

EFFECTIVE STREAM AREA(ACRES) = 4.74

TOTAL STREAM AREA(ACRES) = 4.74

PEAK FLOW RATE(CFS) AT CONFLUENCE = 11.84

## RE. RES

## \*\* CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	2.48	13.80	3.021	0.43( 0.43)	1.00	1.1	10.00
2	11.84	12.71	3.201	0.43( 0.43)	1.00	4.7	12.00

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

## \*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	14.28	12.71	3.201	0.43( 0.43)	1.00	5.7	12.00
2	13.55	13.80	3.021	0.43( 0.43)	1.00	5.8	10.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 14.28 Tc(MIN.) = 12.71

EFFECTIVE AREA(ACRES) = 5.72 AREA-AVERAGED Fm(INCH/HR) = 0.43

AREA-AVERAGED Fp(INCH/HR) = 0.43 AREA-AVERAGED Ap = 1.00

TOTAL AREA(ACRES) = 5.8

LONGEST FLOWPATH FROM NODE 10.00 TO NODE 14.00 = 844.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 14.00 TO NODE 23.00 IS CODE = 52

>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<

>>>>TRAVELTIME THRU SUBAREA<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 2744.00 DOWNSTREAM(FEET) = 2740.00

CHANNEL LENGTH THRU SUBAREA(FEET) = 259.00 CHANNEL SLOPE = 0.0154

CHANNEL FLOW THRU SUBAREA(CFS) = 14.28

FLOW VELOCITY(FEET/SEC) = 3.40 (PER LACFC/RCFC&WCD HYDROLOGY MANUAL)

TRAVEL TIME(MIN.) = 1.27 Tc(MIN.) = 13.97

LONGEST FLOWPATH FROM NODE 10.00 TO NODE 23.00 = 1103.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 23.00 TO NODE 23.00 IS CODE = 1

-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

=====

TOTAL NUMBER OF STREAMS = 2

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:

TIME OF CONCENTRATION(MIN.) = 13.97

RAINFALL INTENSITY(INCH/HR) = 3.00

AREA-AVERAGED Fm(INCH/HR) = 0.43

AREA-AVERAGED Fp(INCH/HR) = 0.43

AREA-AVERAGED Ap = 1.00

EFFECTIVE STREAM AREA(ACRES) = 5.72

TOTAL STREAM AREA(ACRES) = 5.80

RE. RES  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 14.28

\*\*\*\*\*  
FLOW PROCESS FROM NODE 20.00 TO NODE 21.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<  
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

INITIAL SUBAREA FLOW-LENGTH(FEET) = 762.00  
ELEVATION DATA: UPSTREAM(FEET) = 2802.00 DOWNSTREAM(FEET) = 2769.80

Tc = K\*[(LENGTH\*\* 3.00)/(ELEVATION CHANGE)]\*\*0.20

SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 8.137

\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 4.373

SUBAREA Tc AND LOSS RATE DATA(AMC I):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
COMMERCIAL	C	1.40	0.81	0.100	50	8.14
NATURAL DESERT COVER						
"DESERT BRUSH" (15.0%)	C	3.19	0.43	1.000	76	14.05
SUBAREA AVERAGE PREVIOUS LOSS RATE, Fp(INCH/HR)						0.44
SUBAREA AVERAGE PREVIOUS AREA FRACTION, Ap						0.725
SUBAREA RUNOFF(CFS)						16.74
TOTAL AREA(ACRES)		4.59	PEAK FLOW RATE(CFS)			16.74

\*\*\*\*\*  
FLOW PROCESS FROM NODE 21.00 TO NODE 22.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<

ELEVATION DATA: UPSTREAM(FEET) = 2769.80 DOWNSTREAM(FEET) = 2737.00

CHANNEL LENGTH THRU SUBAREA(FEET) = 260.00 CHANNEL SLOPE = 0.1262

CHANNEL BASE(FEET) = 1.00 "Z" FACTOR = 2.000

MANNING'S FACTOR = 0.025 MAXIMUM DEPTH(FEET) = 5.00

\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 4.240

SUBAREA LOSS RATE DATA(AMC I):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
NATURAL DESERT COVER					
"DESERT BRUSH" (15.0%)	C	1.92	0.43	1.000	76
SUBAREA AVERAGE PREVIOUS LOSS RATE, Fp(INCH/HR)					0.43
SUBAREA AVERAGE PREVIOUS AREA FRACTION, Ap					1.000
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS)					20.03
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.)					11.75
AVERAGE FLOW DEPTH(FEET)		0.71	TRAVEL TIME(MIN.)		0.37
Tc(MIN.)		8.51			
SUBAREA AREA(ACRES)		1.92	SUBAREA RUNOFF(CFS)		6.59
EFFECTIVE AREA(ACRES)		6.51	AREA-AVERAGED Fm(INCH/HR)		0.35

RE. RES  
AREA-AVERAGED Fp(INCH/HR) = 0.44 AREA-AVERAGED Ap = 0.81  
TOTAL AREA(ACRES) = 6.5 PEAK FLOW RATE(CFS) = 22.78

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
DEPTH(FEET) = 0.75 FLOW VELOCITY(FEET/SEC.) = 12.09  
LONGEST FLOWPATH FROM NODE 20.00 TO NODE 22.00 = 1022.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 22.00 TO NODE 22.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<

=====  
MAINLINE Tc(MIN.) = 8.51  
\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 4.240  
SUBAREA LOSS RATE DATA(AMC I):  

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	C	0.19	0.81	0.100	50

  
SUBAREA AVERAGE PREVIOUS LOSS RATE, Fp(INCH/HR) = 0.81  
SUBAREA AVERAGE PREVIOUS AREA FRACTION, Ap = 0.100  
SUBAREA AREA(ACRES) = 0.19 SUBAREA RUNOFF(CFS) = 0.71  
EFFECTIVE AREA(ACRES) = 6.70 AREA-AVERAGED Fm(INCH/HR) = 0.34  
AREA-AVERAGED Fp(INCH/HR) = 0.44 AREA-AVERAGED Ap = 0.79  
TOTAL AREA(ACRES) = 6.7 PEAK FLOW RATE(CFS) = 23.49

\*\*\*\*\*  
FLOW PROCESS FROM NODE 22.00 TO NODE 23.00 IS CODE = 52

>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<

=====  
ELEVATION DATA: UPSTREAM(FEET) = 2740.01 DOWNSTREAM(FEET) = 2740.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 130.00 CHANNEL SLOPE = 0.0001  
NOTE: CHANNEL SLOPE OF .001 WAS ASSUMED IN VELOCITY ESTIMATION  
CHANNEL FLOW THRU SUBAREA(CFS) = 23.49  
FLOW VELOCITY(FEET/SEC) = 0.99 (PER LACFC/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 2.19 Tc(MIN.) = 10.69  
LONGEST FLOWPATH FROM NODE 20.00 TO NODE 23.00 = 1152.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 23.00 TO NODE 23.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<

=====  
TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 10.69  
RAINFALL INTENSITY(INCH/HR) = 3.61

RE. RES

AREA-AVERAGED Fm(INCH/HR) = 0.34  
 AREA-AVERAGED Fp(INCH/HR) = 0.44  
 AREA-AVERAGED Ap = 0.79  
 EFFECTIVE STREAM AREA(ACRES) = 6.70  
 TOTAL STREAM AREA(ACRES) = 6.70  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 23.49

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	14.28	13.97	2.995	0.43( 0.43)	1.00	5.7	12.00
1	13.55	15.09	2.839	0.43( 0.43)	1.00	5.8	10.00
2	23.49	10.69	3.612	0.44( 0.34)	0.79	6.7	20.00

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	37.04	10.69	3.612	0.43( 0.38)	0.87	11.1	20.00
2	33.33	13.97	2.995	0.43( 0.38)	0.88	12.4	12.00
3	31.48	15.09	2.839	0.43( 0.38)	0.89	12.5	10.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 37.04 Tc(MIN.) = 10.69  
 EFFECTIVE AREA(ACRES) = 11.07 AREA-AVERAGED Fm(INCH/HR) = 0.38  
 AREA-AVERAGED Fp(INCH/HR) = 0.43 AREA-AVERAGED Ap = 0.87  
 TOTAL AREA(ACRES) = 12.5  
 LONGEST FLOWPATH FROM NODE 20.00 TO NODE 23.00 = 1152.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 23.00 TO NODE 31.00 IS CODE = 52

-----  
 >>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<  
 >>>>TRAVELTIME THRU SUBAREA<<<<

=====  
 ELEVATION DATA: UPSTREAM(FEET) = 2740.00 DOWNSTREAM(FEET) = 2733.00  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 142.00 CHANNEL SLOPE = 0.0493  
 CHANNEL FLOW THRU SUBAREA(CFS) = 37.04  
 FLOW VELOCITY(FEET/SEC) = 7.89 (PER LACFC/RCFC&WCD HYDROLOGY MANUAL)  
 TRAVEL TIME(MIN.) = 0.30 Tc(MIN.) = 11.00  
 LONGEST FLOWPATH FROM NODE 20.00 TO NODE 31.00 = 1294.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 31.00 TO NODE 31.00 IS CODE = 1

-----  
 >>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

RE. RES

TOTAL NUMBER OF STREAMS = 3  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 11.00  
RAINFALL INTENSITY(INCH/HR) = 3.54  
AREA-AVERAGED Fm(INCH/HR) = 0.38  
AREA-AVERAGED Fp(INCH/HR) = 0.43  
AREA-AVERAGED Ap = 0.87  
EFFECTIVE STREAM AREA(ACRES) = 11.07  
TOTAL STREAM AREA(ACRES) = 12.50  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 37.04

\*\*\*\*\*

FLOW PROCESS FROM NODE 30.00 TO NODE 31.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<  
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 400.00  
ELEVATION DATA: UPSTREAM(FEET) = 2769.80 DOWNSTREAM(FEET) = 2733.00

$$Tc = K^*[(\text{LENGTH}^{**} 3.00)/(\text{ELEVATION CHANGE})]^{**}0.20$$

SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 9.294

\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 3.984

SUBAREA Tc AND LOSS RATE DATA(AMC I):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
NATURAL DESERT COVER						
"DESERT BRUSH" (1.0%)	C	0.73	0.40	1.000	78	9.29
SUBAREA AVERAGE PREVIOUS LOSS RATE, Fp(INCH/HR)				0.40		
SUBAREA AVERAGE PREVIOUS AREA FRACTION, Ap				1.000		
SUBAREA RUNOFF(CFS)		2.36				
TOTAL AREA(ACRES)		0.73	PEAK FLOW RATE(CFS)			2.36

\*\*\*\*\*

FLOW PROCESS FROM NODE 31.00 TO NODE 31.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

=====

TOTAL NUMBER OF STREAMS = 3  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 9.29  
RAINFALL INTENSITY(INCH/HR) = 3.98  
AREA-AVERAGED Fm(INCH/HR) = 0.40  
AREA-AVERAGED Fp(INCH/HR) = 0.40  
AREA-AVERAGED Ap = 1.00  
EFFECTIVE STREAM AREA(ACRES) = 0.73  
TOTAL STREAM AREA(ACRES) = 0.73  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 2.36

RE. RES

\*\*\*\*\*

FLOW PROCESS FROM NODE 40.00 TO NODE 41.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

INITIAL SUBAREA FLOW-LENGTH(FEET) = 238.00

ELEVATION DATA: UPSTREAM(FEET) = 2781.00 DOWNSTREAM(FEET) = 2773.00

Tc = K\*[(LENGTH\*\* 3.00)/(ELEVATION CHANGE)]\*\*0.20

SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 9.236

\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 4.002

SUBAREA Tc AND LOSS RATE DATA(AMC I):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
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NATURAL DESERT COVER

"DESERT BRUSH" (15.0%) C 0.21 0.43 1.000 76 9.24

SUBAREA AVERAGE PREVIOUS LOSS RATE, Fp(INCH/HR) = 0.43

SUBAREA AVERAGE PREVIOUS AREA FRACTION, Ap = 1.000

SUBAREA RUNOFF(CFS) = 0.68

TOTAL AREA(ACRES) = 0.21 PEAK FLOW RATE(CFS) = 0.68

\*\*\*\*\*

FLOW PROCESS FROM NODE 41.00 TO NODE 42.00 IS CODE = 61

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<

>>>>(STANDARD CURB SECTION USED)<<<<

UPSTREAM ELEVATION(FEET) = 2773.00 DOWNSTREAM ELEVATION(FEET) = 2736.69

STREET LENGTH(FEET) = 310.00 CURB HEIGHT(INCHES) = 6.0

STREET HALFWIDTH(FEET) = 10.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 1.00

INSIDE STREET CROSSFALL(DECIMAL) = 0.020

OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1

Manning's FRICTION FACTOR for Streetflow Section(curb-to-curb) = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.75

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.21

HALFSTREET FLOOD WIDTH(FEET) = 4.39

AVERAGE FLOW VELOCITY(FEET/SEC.) = 5.62

PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.20

STREET FLOW TRAVEL TIME(MIN.) = 0.92 Tc(MIN.) = 10.15

\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 3.745

SUBAREA LOSS RATE DATA(AMC I):

DEVELOPMENT TYPE/	SCS SOIL	AREA	Fp	Ap	SCS
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LAND USE	GROUP	RE. RES (ACRES)	(INCH/HR)	(DECIMAL)	CN
COMMERCIAL	C	0.17	0.81	0.100	50
NATURAL DESERT COVER					
"DESERT BRUSH" (15.0%)	C	0.53	0.43	1.000	76
SUBAREA AVERAGE PREVIOUS LOSS RATE, $F_p$ (INCH/HR) =		0.44			
SUBAREA AVERAGE PREVIOUS AREA FRACTION, $A_p$ =		0.781			
SUBAREA AREA(ACRES) =	0.70	SUBAREA RUNOFF(CFS) =	2.14		
EFFECTIVE AREA(ACRES) =	0.91	AREA-AVERAGED $F_m$ (INCH/HR) =	0.36		
AREA-AVERAGED $F_p$ (INCH/HR) =	0.43	AREA-AVERAGED $A_p$ =	0.83		
TOTAL AREA(ACRES) =	0.9	PEAK FLOW RATE(CFS) =	2.77		

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.24 HALFSTREET FLOOD WIDTH(FEET) = 5.85  
 FLOW VELOCITY(FEET/SEC.) = 6.02 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.46  
 LONGEST FLOWPATH FROM NODE 40.00 TO NODE 42.00 = 548.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 42.00 TO NODE 43.00 IS CODE = 31

-----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPE SIZE (NON-PRESSURE FLOW)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 2736.69 DOWNSTREAM(FEET) = 2732.69  
 FLOW LENGTH(FEET) = 53.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 9.0 INCH PIPE IS 5.2 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 10.36  
 ESTIMATED PIPE DIAMETER(INCH) = 9.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 2.77  
 PIPE TRAVEL TIME(MIN.) = 0.09  $T_c$ (MIN.) = 10.24  
 LONGEST FLOWPATH FROM NODE 40.00 TO NODE 43.00 = 601.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 43.00 TO NODE 43.00 IS CODE = 81

-----

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<

=====

MAINLINE  $T_c$ (MIN.) = 10.24  
 \* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 3.723  
 SUBAREA LOSS RATE DATA(AMC I):  

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	$F_p$ (INCH/HR)	$A_p$ (DECIMAL)	SCS CN
COMMERCIAL	C	0.27	0.81	0.100	50
SUBAREA AVERAGE PREVIOUS LOSS RATE, $F_p$ (INCH/HR) =		0.81			
SUBAREA AVERAGE PREVIOUS AREA FRACTION, $A_p$ =		0.100			
SUBAREA AREA(ACRES) =	0.27	SUBAREA RUNOFF(CFS) =	0.89		
EFFECTIVE AREA(ACRES) =	1.18	AREA-AVERAGED $F_m$ (INCH/HR) =	0.30		
AREA-AVERAGED $F_p$ (INCH/HR) =	0.45	AREA-AVERAGED $A_p$ =	0.66		
TOTAL AREA(ACRES) =	1.2	PEAK FLOW RATE(CFS) =	3.64		

RE. RES

\*\*\*\*\*  
FLOW PROCESS FROM NODE 43.00 TO NODE 44.00 IS CODE = 31  
-----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

=====  
ELEVATION DATA: UPSTREAM(FEET) = 2732.69 DOWNSTREAM(FEET) = 2732.00

FLOW LENGTH(FEET) = 140.00 MANNING'S N = 0.013

DEPTH OF FLOW IN 15.0 INCH PIPE IS 10.6 INCHES

PIPE-FLOW VELOCITY(FEET/SEC.) = 3.93

ESTIMATED PIPE DIAMETER(INCH) = 15.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 3.64

PIPE TRAVEL TIME(MIN.) = 0.59 Tc(MIN.) = 10.83

LONGEST FLOWPATH FROM NODE 40.00 TO NODE 44.00 = 741.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 44.00 TO NODE 44.00 IS CODE = 81  
-----

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<

MAINLINE Tc(MIN.) = 10.83

\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 3.579

SUBAREA LOSS RATE DATA(AMC I):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	C	0.10	0.81	0.100	50
SUBAREA AVERAGE PREVIOUS LOSS RATE, Fp(INCH/HR)			= 0.81		
SUBAREA AVERAGE PREVIOUS AREA FRACTION, Ap			= 0.100		
SUBAREA AREA(ACRES)	= 0.10	SUBAREA RUNOFF(CFS)	= 0.31		
EFFECTIVE AREA(ACRES)	= 1.28	AREA-AVERAGED Fm(INCH/HR)	= 0.28		
AREA-AVERAGED Fp(INCH/HR)	= 0.45	AREA-AVERAGED Ap	= 0.62		
TOTAL AREA(ACRES)	= 1.3	PEAK FLOW RATE(CFS)	= 3.80		

\*\*\*\*\*  
FLOW PROCESS FROM NODE 44.00 TO NODE 44.00 IS CODE = 81  
-----

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<

MAINLINE Tc(MIN.) = 10.83

\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 3.579

SUBAREA LOSS RATE DATA(AMC I):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
NATURAL DESERT COVER "DESERT BRUSH" (15.0%)	C	0.32	0.43	1.000	76
SUBAREA AVERAGE PREVIOUS LOSS RATE, Fp(INCH/HR)			= 0.43		
SUBAREA AVERAGE PREVIOUS AREA FRACTION, Ap			= 1.000		
SUBAREA AREA(ACRES)	= 0.32	SUBAREA RUNOFF(CFS)	= 0.91		
EFFECTIVE AREA(ACRES)	= 1.60	AREA-AVERAGED Fm(INCH/HR)	= 0.31		

RE. RES

AREA-AVERAGED $F_p$ (INCH/HR) = 0.44	AREA-AVERAGED $A_p$ = 0.70
TOTAL AREA(ACRES) = 1.6	PEAK FLOW RATE(CFS) = 4.71

---

\*\*\*\*\*  
FLOW PROCESS FROM NODE 44.00 TO NODE 31.00 IS CODE = 52  
-----

>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<

---

ELEVATION DATA: UPSTREAM(FEET) = 2736.00 DOWNSTREAM(FEET) = 2733.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 48.00 CHANNEL SLOPE = 0.0625  
CHANNEL FLOW THRU SUBAREA(CFS) = 4.71  
FLOW VELOCITY(FEET/SEC) = 5.20 (PER LACFC/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 0.15 Tc(MIN.) = 10.99  
LONGEST FLOWPATH FROM NODE 40.00 TO NODE 31.00 = 789.00 FEET.

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\*\*\*\*\*  
FLOW PROCESS FROM NODE 31.00 TO NODE 31.00 IS CODE = 1  
-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<

---

TOTAL NUMBER OF STREAMS = 3  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 3 ARE:  
TIME OF CONCENTRATION(MIN.) = 10.99  
RAINFALL INTENSITY(INCH/HR) = 3.54  
AREA-AVERAGED  $F_m$ (INCH/HR) = 0.31  
AREA-AVERAGED  $F_p$ (INCH/HR) = 0.44  
AREA-AVERAGED  $A_p$  = 0.70  
EFFECTIVE STREAM AREA(ACRES) = 1.60  
TOTAL STREAM AREA(ACRES) = 1.60  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 4.71

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	$F_p(F_m)$ (INCH/HR)	$A_p$	Ae (ACRES)	HEADWATER NODE
1	37.04	11.00	3.542	0.43( 0.38)	0.87	11.1	20.00
1	33.33	14.28	2.950	0.43( 0.38)	0.88	12.4	12.00
1	31.48	15.40	2.798	0.43( 0.38)	0.89	12.5	10.00
2	2.36	9.29	3.984	0.40( 0.40)	1.00	0.7	30.00
3	4.71	10.99	3.544	0.44( 0.31)	0.70	1.6	40.00

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 3 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	$F_p(F_m)$ (INCH/HR)	$A_p$	Ae (ACRES)	HEADWATER NODE
1	42.56	9.29	3.984	0.43( 0.37)	0.86	11.4	30.00

	RE. RES						
2	43.81	10.99	3.544	0.43( 0.37)	0.86	13.4	40.00
3	43.81	11.00	3.542	0.43( 0.37)	0.86	13.4	20.00
4	38.85	14.28	2.950	0.43( 0.37)	0.87	14.7	12.00
5	36.68	15.40	2.798	0.43( 0.38)	0.87	14.8	10.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 43.81 Tc(MIN.) = 11.00

EFFECTIVE AREA(ACRES) = 13.40 AREA-AVERAGED Fm(INCH/HR) = 0.37

AREA-AVERAGED Fp(INCH/HR) = 0.43 AREA-AVERAGED Ap = 0.86

TOTAL AREA(ACRES) = 14.8

LONGEST FLOWPATH FROM NODE 20.00 TO NODE 31.00 = 1294.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 31.00 TO NODE 56.00 IS CODE = 52

>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<

>>>>TRAVELTIME THRU SUBAREA<<<<

ELEVATION DATA: UPSTREAM(FEET) = 2733.00 DOWNSTREAM(FEET) = 2722.00

CHANNEL LENGTH THRU SUBAREA(FEET) = 273.00 CHANNEL SLOPE = 0.0403

CHANNEL FLOW THRU SUBAREA(CFS) = 43.81

FLOW VELOCITY(FEET/SEC) = 7.48 (PER LACFC/RCFC&WCD HYDROLOGY MANUAL)

TRAVEL TIME(MIN.) = 0.61 Tc(MIN.) = 11.60

LONGEST FLOWPATH FROM NODE 20.00 TO NODE 56.00 = 1567.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 56.00 TO NODE 56.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

TOTAL NUMBER OF STREAMS = 3

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:

TIME OF CONCENTRATION(MIN.) = 11.60

RAINFALL INTENSITY(INCH/HR) = 3.41

AREA-AVERAGED Fm(INCH/HR) = 0.37

AREA-AVERAGED Fp(INCH/HR) = 0.43

AREA-AVERAGED Ap = 0.86

EFFECTIVE STREAM AREA(ACRES) = 13.40

TOTAL STREAM AREA(ACRES) = 14.83

PEAK FLOW RATE(CFS) AT CONFLUENCE = 43.81

\*\*\*\*\*

FLOW PROCESS FROM NODE 50.00 TO NODE 51.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

INITIAL SUBAREA FLOW-LENGTH(FEET) = 700.00

ELEVATION DATA: UPSTREAM(FEET) = 2812.00 DOWNSTREAM(FEET) = 2774.40

RE. RES

$T_c = K^*[(\text{LENGTH}^{**} 3.00)/(\text{ELEVATION CHANGE})]^{**}0.20$   
 SUBAREA ANALYSIS USED MINIMUM  $T_c$ (MIN.) = 12.947  
 \* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 3.159  
 SUBAREA  $T_c$  AND LOSS RATE DATA(AMC I):  

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	$T_c$ (MIN.)
NATURAL DESERT COVER						
"DESERT BRUSH" (15.0%)	C	3.96	0.43	1.000	76	12.95
SUBAREA AVERAGE PREVIOUS LOSS RATE, Fp(INCH/HR)				0.43		
SUBAREA AVERAGE PREVIOUS AREA FRACTION, Ap				1.000		
SUBAREA RUNOFF(CFS)		9.74				
TOTAL AREA(ACRES)		3.96	PEAK FLOW RATE(CFS)			9.74

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 51.00 TO NODE 52.00 IS CODE = 31

-----  
 >>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPE SIZE (NON-PRESSURE FLOW)<<<<

=====  
 ELEVATION DATA: UPSTREAM(FEET) = 2774.40 DOWNSTREAM(FEET) = 2754.00  
 FLOW LENGTH(FEET) = 439.00 Manning's N = 0.013  
 DEPTH OF FLOW IN 15.0 INCH PIPE IS 9.6 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 11.77  
 ESTIMATED PIPE DIAMETER(INCH) = 15.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 9.74  
 PIPE TRAVEL TIME(MIN.) = 0.62  $T_c$ (MIN.) = 13.57  
 LONGEST FLOWPATH FROM NODE 50.00 TO NODE 52.00 = 1139.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 52.00 TO NODE 52.00 IS CODE = 81

-----  
 >>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<

=====  
 MAINLINE  $T_c$ (MIN.) = 13.57  
 \* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 3.057  
 SUBAREA LOSS RATE DATA(AMC I):  

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	C	0.27	0.81	0.100	50
NATURAL DESERT COVER					
"DESERT BRUSH" (15.0%)	C	6.64	0.43	1.000	76
SUBAREA AVERAGE PREVIOUS LOSS RATE, Fp(INCH/HR)				0.43	
SUBAREA AVERAGE PREVIOUS AREA FRACTION, Ap				0.965	
SUBAREA AREA(ACRES)		6.91	SUBAREA RUNOFF(CFS)		16.45
EFFECTIVE AREA(ACRES)		10.87	AREA-AVERAGED Fm(INCH/HR)		0.42
AREA-AVERAGED Fp(INCH/HR)		0.43	AREA-AVERAGED Ap		0.98
TOTAL AREA(ACRES)		10.9	PEAK FLOW RATE(CFS)		25.83

RE. RES

\*\*\*\*\*  
FLOW PROCESS FROM NODE 52.00 TO NODE 53.00 IS CODE = 51  
-----

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<

=====  
ELEVATION DATA: UPSTREAM(FEET) = 2754.00 DOWNSTREAM(FEET) = 2727.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 324.00 CHANNEL SLOPE = 0.0833

CHANNEL BASE(FEET) = 1.00 "Z" FACTOR = 2.000

MANNING'S FACTOR = 0.025 MAXIMUM DEPTH(FEET) = 5.00

\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 2.981

SUBAREA LOSS RATE DATA(AMC I):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	C	0.18	0.81	0.100	50

NATURAL DESERT COVER

"DESERT BRUSH" (15.0%) C 0.51 0.43 1.000 76

SUBAREA AVERAGE PEROVIOUS LOSS RATE, Fp(INCH/HR) = 0.44

SUBAREA AVERAGE PEROVIOUS AREA FRACTION, Ap = 0.765

TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 26.65

TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 10.77

AVERAGE FLOW DEPTH(FEET) = 0.89 TRAVEL TIME(MIN.) = 0.50

Tc(MIN.) = 14.07

SUBAREA AREA(ACRES) = 0.69 SUBAREA RUNOFF(CFS) = 1.64

EFFECTIVE AREA(ACRES) = 11.56 AREA-AVERAGED Fm(INCH/HR) = 0.41

AREA-AVERAGED Fp(INCH/HR) = 0.43 AREA-AVERAGED Ap = 0.96

TOTAL AREA(ACRES) = 11.6 PEAK FLOW RATE(CFS) = 26.72

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.89 FLOW VELOCITY(FEET/SEC.) = 10.80

LONGEST FLOWPATH FROM NODE 50.00 TO NODE 53.00 = 1463.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 53.00 TO NODE 56.00 IS CODE = 51  
-----

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<

=====  
ELEVATION DATA: UPSTREAM(FEET) = 2728.00 DOWNSTREAM(FEET) = 2721.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 68.00 CHANNEL SLOPE = 0.1029

CHANNEL BASE(FEET) = 1.00 "Z" FACTOR = 2.000

MANNING'S FACTOR = 0.025 MAXIMUM DEPTH(FEET) = 5.00

\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 2.967

SUBAREA LOSS RATE DATA(AMC I):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
NATURAL DESERT COVER	C	1.38	0.43	1.000	76

"DESERT BRUSH" (15.0%) C 1.38 0.43 1.000 76

SUBAREA AVERAGE PEROVIOUS LOSS RATE, Fp(INCH/HR) = 0.43

RE. RES

SUBAREA AVERAGE PERVERIOUS AREA FRACTION, Ap = 1.000  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 28.30  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 11.81  
 AVERAGE FLOW DEPTH(FEET) = 0.87 TRAVEL TIME(MIN.) = 0.10  
 Tc(MIN.) = 14.17  
 SUBAREA AREA(ACRES) = 1.38 SUBAREA RUNOFF(CFS) = 3.16  
 EFFECTIVE AREA(ACRES) = 12.94 AREA-AVERAGED Fm(INCH/HR) = 0.41  
 AREA-AVERAGED Fp(INCH/HR) = 0.43 AREA-AVERAGED Ap = 0.97  
 TOTAL AREA(ACRES) = 12.9 PEAK FLOW RATE(CFS) = 29.73

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.89 FLOW VELOCITY(FEET/SEC.) = 12.02  
 LONGEST FLOWPATH FROM NODE 50.00 TO NODE 56.00 = 1531.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 56.00 TO NODE 56.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

TOTAL NUMBER OF STREAMS = 3  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 14.17  
 RAINFALL INTENSITY(INCH/HR) = 2.97  
 AREA-AVERAGED Fm(INCH/HR) = 0.41  
 AREA-AVERAGED Fp(INCH/HR) = 0.43  
 AREA-AVERAGED Ap = 0.97  
 EFFECTIVE STREAM AREA(ACRES) = 12.94  
 TOTAL STREAM AREA(ACRES) = 12.94  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 29.73

\*\*\*\*\*

FLOW PROCESS FROM NODE 53.00 TO NODE 54.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

INITIAL SUBAREA FLOW-LENGTH(FEET) = 172.00  
 ELEVATION DATA: UPSTREAM(FEET) = 2739.00 DOWNSTREAM(FEET) = 2723.00

$$T_c = K^*[(\text{LENGTH}^{**3.00})/(\text{ELEVATION CHANGE})]^{**0.20}$$

SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 5.000

\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 6.150

SUBAREA Tc AND LOSS RATE DATA(AMC I):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
COMMERCIAL	C	0.06	0.81	0.100	50	5.00
NATURAL DESERT COVER						
"DESERT BRUSH" (15.0%)	C	0.31	0.43	1.000	76	6.62
SUBAREA AVERAGE PERVERIOUS LOSS RATE, Fp(INCH/HR)						

RE. RES

SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.854

SUBAREA RUNOFF(CFS) = 1.92

TOTAL AREA(ACRES) = 0.37 PEAK FLOW RATE(CFS) = 1.92

\*\*\*\*\*

FLOW PROCESS FROM NODE 54.00 TO NODE 55.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

ELEVATION DATA: UPSTREAM(FEET) = 2723.00 DOWNSTREAM(FEET) = 2722.50

FLOW LENGTH(FEET) = 53.00 MANNING'S N = 0.013

DEPTH OF FLOW IN 12.0 INCH PIPE IS 6.6 INCHES

PIPE-FLOW VELOCITY(FEET/SEC.) = 4.34

ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 1.92

PIPE TRAVEL TIME(MIN.) = 0.20 Tc(MIN.) = 5.20

LONGEST FLOWPATH FROM NODE 53.00 TO NODE 55.00 = 225.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 55.00 TO NODE 55.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<

MAINLINE Tc(MIN.) = 5.20

\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 5.980

SUBAREA LOSS RATE DATA(AMC I):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	C	0.03	0.81	0.100	50

NATURAL DESERT COVER

"DESERT BRUSH" (15.0%) C 0.02 0.43 1.000 76

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.48

SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.460

SUBAREA AREA(ACRES) = 0.05 SUBAREA RUNOFF(CFS) = 0.26

EFFECTIVE AREA(ACRES) = 0.42 AREA-AVERAGED Fm(INCH/HR) = 0.35

AREA-AVERAGED Fp(INCH/HR) = 0.44 AREA-AVERAGED Ap = 0.81

TOTAL AREA(ACRES) = 0.4 PEAK FLOW RATE(CFS) = 2.13

\*\*\*\*\*

FLOW PROCESS FROM NODE 55.00 TO NODE 56.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

ELEVATION DATA: UPSTREAM(FEET) = 2722.50 DOWNSTREAM(FEET) = 2722.00

FLOW LENGTH(FEET) = 16.80 MANNING'S N = 0.013

DEPTH OF FLOW IN 9.0 INCH PIPE IS 6.0 INCHES

PIPE-FLOW VELOCITY(FEET/SEC.) = 6.78

RE. RES

ESTIMATED PIPE DIAMETER(INCH) = 9.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 2.13  
 PIPE TRAVEL TIME(MIN.) = 0.04 Tc(MIN.) = 5.24  
 LONGEST FLOWPATH FROM NODE 53.00 TO NODE 56.00 = 241.80 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 56.00 TO NODE 56.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<

TOTAL NUMBER OF STREAMS = 3  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 3 ARE:  
 TIME OF CONCENTRATION(MIN.) = 5.24  
 RAINFALL INTENSITY(INCH/HR) = 5.95  
 AREA-AVERAGED Fm(INCH/HR) = 0.35  
 AREA-AVERAGED Fp(INCH/HR) = 0.44  
 AREA-AVERAGED Ap = 0.81  
 EFFECTIVE STREAM AREA(ACRES) = 0.42  
 TOTAL STREAM AREA(ACRES) = 0.42  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 2.13

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	42.56	9.91	3.810	0.43( 0.37)	0.86	11.4	30.00
1	43.81	11.60	3.413	0.43( 0.37)	0.86	13.4	40.00
1	43.81	11.60	3.411	0.43( 0.37)	0.86	13.4	20.00
1	38.85	14.91	2.862	0.43( 0.37)	0.87	14.7	12.00
1	36.68	16.04	2.719	0.43( 0.38)	0.87	14.8	10.00
2	29.73	14.17	2.967	0.43( 0.41)	0.97	12.9	50.00
3	2.13	5.24	5.947	0.44( 0.35)	0.81	0.4	53.00

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 3 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	62.53	5.24	5.947	0.43( 0.39)	0.90	11.3	53.00
2	71.54	9.91	3.810	0.43( 0.39)	0.91	20.9	30.00
3	73.56	11.60	3.413	0.43( 0.39)	0.90	24.4	40.00
4	73.56	11.60	3.411	0.43( 0.39)	0.90	24.4	20.00
5	70.69	14.17	2.967	0.43( 0.39)	0.91	27.8	50.00
6	68.31	14.91	2.862	0.43( 0.39)	0.91	28.1	12.00
7	64.42	16.04	2.719	0.43( 0.39)	0.91	28.2	10.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 73.56 Tc(MIN.) = 11.60

## RE. RES

EFFECTIVE AREA(ACRES) = 24.42 AREA-AVERAGED Fm(INCH/HR) = 0.39

AREA-AVERAGED Fp(INCH/HR) = 0.43 AREA-AVERAGED Ap = 0.90

TOTAL AREA(ACRES) = 28.2

LONGEST FLOWPATH FROM NODE 20.00 TO NODE 56.00 = 1567.00 FEET.

END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 28.2 TC(MIN.) = 11.60

EFFECTIVE AREA(ACRES) = 24.42 AREA-AVERAGED Fm(INCH/HR) = 0.39

AREA-AVERAGED Fp(INCH/HR) = 0.43 AREA-AVERAGED Ap = 0.905

PEAK FLOW RATE(CFS) = 73.56

## \*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	62.53	5.24	5.947	0.43( 0.39)	0.90	11.3	53.00
2	71.54	9.91	3.810	0.43( 0.39)	0.91	20.9	30.00
3	73.56	11.60	3.413	0.43( 0.39)	0.90	24.4	40.00
4	73.56	11.60	3.411	0.43( 0.39)	0.90	24.4	20.00
5	70.69	14.17	2.967	0.43( 0.39)	0.91	27.8	50.00
6	68.31	14.91	2.862	0.43( 0.39)	0.91	28.1	12.00
7	64.42	16.04	2.719	0.43( 0.39)	0.91	28.2	10.00

END OF RATIONAL METHOD ANALYSIS



## Hydrographs

### Hydrograph - Basin B Tributary to Infiltration Basin 1 - 100 Year Storm Event

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\*\*\* NON-HOMOGENEOUS WATERSHED AREA-AVERAGED LOSS RATE (Fm)  
AND LOW LOSS FRACTION ESTIMATIONS FOR AMC I:

TOTAL 24-HOUR DURATION RAINFALL DEPTH = 3.28 (inches)

SOIL-COVER TYPE	AREA (Acres)	PERCENT OF PERVIOUS AREA	SCS CURVE NUMBER	LOSS RATE Fp(in./hr.)	YIELD
1	5.11	100.00	90.(AMC II)	0.400	0.406
2	0.32	0.00	98.(AMC II)	0.000	0.929
3	1.27	100.00	91.(AMC II)	0.370	0.446

TOTAL AREA (Acres) = 6.70

AREA-AVERAGED LOSS RATE, Fm (in./hr.) = 0.381

AREA-AVERAGED LOW LOSS FRACTION, Y = 0.569

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RATIONAL METHOD CALIBRATION COEFFICIENT = 1.05

TOTAL CATCHMENT AREA(ACRES) = 6.70

SOIL-LOSS RATE, Fm,(INCH/HR) = 0.381

LOW LOSS FRACTION = 0.569

TIME OF CONCENTRATION(MIN.) = 8.51

SMALL AREA PEAK Q COMPUTED USING PEAK FLOW RATE FORMULA

USER SPECIFIED RAINFALL VALUES ARE USED

RETURN FREQUENCY(YEARS) = 100

5-MINUTE POINT RAINFALL VALUE(INCHES) = 0.41

30-MINUTE POINT RAINFALL VALUE(INCHES) = 0.95

1-HOUR POINT RAINFALL VALUE(INCHES) = 1.08

3-HOUR POINT RAINFALL VALUE(INCHES) = 1.57

6-HOUR POINT RAINFALL VALUE(INCHES) = 2.02

24-HOUR POINT RAINFALL VALUE(INCHES) = 3.28

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TOTAL CATCHMENT RUNOFF VOLUME(ACRE-FEET) = 1.02

TOTAL CATCHMENT SOIL-LOSS VOLUME(ACRE-FEET) = 0.81

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TIME (HOURS)	VOLUME (AF)	Q (CFS)	0.	7.5	15.0	22.5	30.0
--------------	-------------	---------	----	-----	------	------	------

0.11	0.0009	0.15 Q	.	.	.	.	.
0.26	0.0026	0.15 Q	.	.	.	.	.
0.40	0.0043	0.15 Q	.	.	.	.	.
0.54	0.0060	0.15 Q	.	.	.	.	.
0.68	0.0077	0.15 Q	.	.	.	.	.
0.82	0.0095	0.15 Q	.	.	.	.	.
0.97	0.0113	0.15 Q	.	.	.	.	.
1.11	0.0130	0.15 Q	.	.	.	.	.

1.25	0.0148	0.15 Q	.	.	.
1.39	0.0166	0.15 Q	.	.	.
1.53	0.0184	0.15 Q	.	.	.
1.67	0.0202	0.16 Q	.	.	.
1.82	0.0220	0.16 Q	.	.	.
1.96	0.0239	0.16 Q	.	.	.
2.10	0.0257	0.16 Q	.	.	.
2.24	0.0276	0.16 Q	.	.	.
2.38	0.0295	0.16 Q	.	.	.
2.53	0.0314	0.16 Q	.	.	.
2.67	0.0333	0.16 Q	.	.	.
2.81	0.0352	0.16 Q	.	.	.
2.95	0.0371	0.16 Q	.	.	.
3.09	0.0390	0.17 Q	.	.	.
3.23	0.0410	0.17 Q	.	.	.
3.38	0.0430	0.17 Q	.	.	.
3.52	0.0450	0.17 Q	.	.	.
3.66	0.0470	0.17 Q	.	.	.
3.80	0.0490	0.17 Q	.	.	.
3.94	0.0510	0.17 Q	.	.	.
4.09	0.0530	0.17 Q	.	.	.
4.23	0.0551	0.18 Q	.	.	.
4.37	0.0572	0.18 Q	.	.	.
4.51	0.0593	0.18 Q	.	.	.
4.65	0.0614	0.18 Q	.	.	.
4.80	0.0635	0.18 Q	.	.	.
4.94	0.0656	0.18 Q	.	.	.
5.08	0.0678	0.19 Q	.	.	.
5.22	0.0700	0.19 Q	.	.	.
5.36	0.0722	0.19 Q	.	.	.
5.50	0.0744	0.19 Q	.	.	.
5.65	0.0766	0.19 Q	.	.	.
5.79	0.0789	0.19 Q	.	.	.
5.93	0.0812	0.20 Q	.	.	.
6.07	0.0834	0.20 Q	.	.	.
6.21	0.0858	0.20 Q	.	.	.
6.36	0.0881	0.20 Q	.	.	.
6.50	0.0905	0.20 Q	.	.	.
6.64	0.0928	0.20 Q	.	.	.
6.78	0.0953	0.21 Q	.	.	.
6.92	0.0977	0.21 Q	.	.	.
7.06	0.1001	0.21 Q	.	.	.
7.21	0.1026	0.21 Q	.	.	.
7.35	0.1051	0.22 Q	.	.	.
7.49	0.1077	0.22 Q	.	.	.
7.63	0.1102	0.22 Q	.	.	.
7.77	0.1128	0.22 Q	.	.	.
7.92	0.1154	0.22 Q	.	.	.
8.06	0.1181	0.23 Q	.	.	.
8.20	0.1207	0.23 Q	.	.	.
8.34	0.1235	0.23 Q	.	.	.
8.48	0.1262	0.24 Q	.	.	.
8.62	0.1290	0.24 Q	.	.	.
8.77	0.1318	0.24 Q	.	.	.
8.91	0.1346	0.24 Q	.	.	.

9.05	0.1375	0.25	Q	.	.	.	.
9.19	0.1404	0.25	Q	.	.	.	.
9.33	0.1434	0.25	Q	.	.	.	.
9.48	0.1464	0.26	Q	.	.	.	.
9.62	0.1494	0.26	Q	.	.	.	.
9.76	0.1525	0.26	Q	.	.	.	.
9.90	0.1556	0.27	Q	.	.	.	.
10.04	0.1588	0.27	Q	.	.	.	.
10.18	0.1620	0.28	Q	.	.	.	.
10.33	0.1653	0.28	Q	.	.	.	.
10.47	0.1686	0.29	Q	.	.	.	.
10.61	0.1720	0.29	Q	.	.	.	.
10.75	0.1754	0.30	Q	.	.	.	.
10.89	0.1789	0.30	Q	.	.	.	.
11.04	0.1825	0.31	Q	.	.	.	.
11.18	0.1861	0.31	Q	.	.	.	.
11.32	0.1898	0.32	Q	.	.	.	.
11.46	0.1936	0.32	Q	.	.	.	.
11.60	0.1974	0.33	Q	.	.	.	.
11.74	0.2013	0.34	Q	.	.	.	.
11.89	0.2053	0.35	Q	.	.	.	.
12.03	0.2094	0.35	Q	.	.	.	.
12.17	0.2137	0.38	Q	.	.	.	.
12.31	0.2182	0.38	Q	.	.	.	.
12.45	0.2227	0.40	Q	.	.	.	.
12.60	0.2274	0.40	Q	.	.	.	.
12.74	0.2322	0.42	Q	.	.	.	.
12.88	0.2371	0.42	Q	.	.	.	.
13.02	0.2422	0.44	Q	.	.	.	.
13.16	0.2474	0.45	Q	.	.	.	.
13.31	0.2528	0.47	Q	.	.	.	.
13.45	0.2583	0.48	Q	.	.	.	.
13.59	0.2641	0.50	Q	.	.	.	.
13.73	0.2700	0.51	Q	.	.	.	.
13.87	0.2762	0.54	Q	.	.	.	.
14.01	0.2826	0.56	Q	.	.	.	.
14.16	0.2891	0.55	Q	.	.	.	.
14.30	0.2957	0.57	Q	.	.	.	.
14.44	0.3027	0.61	Q	.	.	.	.
14.58	0.3100	0.64	Q	.	.	.	.
14.72	0.3179	0.70	Q	.	.	.	.
14.87	0.3262	0.73	Q	.	.	.	.
15.01	0.3352	0.81	Q	.	.	.	.
15.15	0.3450	0.86	Q	.	.	.	.
15.29	0.3559	0.99	Q	.	.	.	.
15.43	0.3678	1.05	Q	.	.	.	.
15.57	0.3783	0.75	Q	.	.	.	.
15.72	0.3879	0.88	Q	.	.	.	.
15.86	0.4217	4.90	Q	.	.	.	.
16.00	0.4936	7.37	Q	.	.	.	.
16.14	0.6745	23.49	.	.	.	Q	.
16.28	0.8237	1.97	Q	.	.	.	.
16.43	0.8390	0.65	Q	.	.	.	.
16.57	0.8482	0.92	Q	.	.	.	.
16.71	0.8581	0.77	Q	.	.	.	.

16.85	0.8665	0.67	Q	.	.	.
16.99	0.8739	0.59	Q	.	.	.
17.13	0.8807	0.57	Q	.	.	.
17.28	0.8871	0.53	Q	.	.	.
17.42	0.8931	0.49	Q	.	.	.
17.56	0.8986	0.46	Q	.	.	.
17.70	0.9038	0.43	Q	.	.	.
17.84	0.9088	0.41	Q	.	.	.
17.99	0.9134	0.39	Q	.	.	.
18.13	0.9178	0.36	Q	.	.	.
18.27	0.9220	0.34	Q	.	.	.
18.41	0.9259	0.33	Q	.	.	.
18.55	0.9297	0.32	Q	.	.	.
18.69	0.9333	0.30	Q	.	.	.
18.84	0.9368	0.29	Q	.	.	.
18.98	0.9402	0.28	Q	.	.	.
19.12	0.9434	0.27	Q	.	.	.
19.26	0.9466	0.27	Q	.	.	.
19.40	0.9497	0.26	Q	.	.	.
19.55	0.9527	0.25	Q	.	.	.
19.69	0.9556	0.25	Q	.	.	.
19.83	0.9585	0.24	Q	.	.	.
19.97	0.9612	0.23	Q	.	.	.
20.11	0.9639	0.23	Q	.	.	.
20.26	0.9666	0.22	Q	.	.	.
20.40	0.9692	0.22	Q	.	.	.
20.54	0.9717	0.21	Q	.	.	.
20.68	0.9742	0.21	Q	.	.	.
20.82	0.9766	0.21	Q	.	.	.
20.96	0.9790	0.20	Q	.	.	.
21.11	0.9813	0.20	Q	.	.	.
21.25	0.9836	0.19	Q	.	.	.
21.39	0.9859	0.19	Q	.	.	.
21.53	0.9881	0.19	Q	.	.	.
21.67	0.9903	0.18	Q	.	.	.
21.82	0.9924	0.18	Q	.	.	.
21.96	0.9945	0.18	Q	.	.	.
22.10	0.9966	0.18	Q	.	.	.
22.24	0.9987	0.17	Q	.	.	.
22.38	1.0007	0.17	Q	.	.	.
22.52	1.0026	0.17	Q	.	.	.
22.67	1.0046	0.17	Q	.	.	.
22.81	1.0065	0.16	Q	.	.	.
22.95	1.0084	0.16	Q	.	.	.
23.09	1.0103	0.16	Q	.	.	.
23.23	1.0122	0.16	Q	.	.	.
23.38	1.0140	0.15	Q	.	.	.
23.52	1.0158	0.15	Q	.	.	.
23.66	1.0176	0.15	Q	.	.	.
23.80	1.0193	0.15	Q	.	.	.
23.94	1.0211	0.15	Q	.	.	.
24.08	1.0228	0.15	Q	.	.	.
24.23	1.0236	0.00	Q	.	.	.

## Routed Hydrograph - Basin B Routed Thru Infiltration Basin 1 - 100 Year Storm Event

### FLOW-THROUGH DETENTION BASIN MODEL

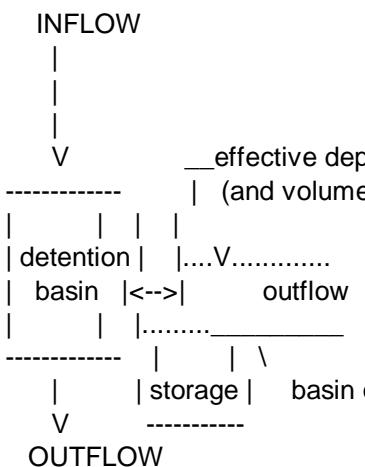
SPECIFIED BASIN CONDITIONS ARE AS FOLLOWS:

CONSTANT HYDROGRAPH TIME UNIT(MINUTES) = 8.510

DEAD STORAGE(AF) = 0.00

SPECIFIED DEAD STORAGE(AF) FILLED = 0.00

ASSUMED INITIAL DEPTH(FEET) IN STORAGE BASIN = 0.00



### DEPTH-VS.-STORAGE AND DEPTH-VS.-DISCHARGE INFORMATION:

TOTAL NUMBER OF BASIN DEPTH INFORMATION ENTRIES = 3

\*BASIN-DEPTH STORAGE    OUTFLOW \*\*BASIN-DEPTH STORAGE    OUTFLOW \*

\* (FEET) (ACRE-FEET) (CFS) \*\* (FEET) (ACRE-FEET) (CFS) \*

\*    0.000    0.000    0.000\*\*    1.000    0.250    0.010\*

\*    2.000    0.530    23.490\*\*

### BASIN STORAGE, OUTFLOW AND DEPTH ROUTING VALUES:

INTERVAL DEPTH {S-O\*DT/2} {S+O\*DT/2}

NUMBER (FEET) (ACRE-FEET) (ACRE-FEET)

1    0.00    0.00000    0.00000

2    1.00    0.24994    0.25006

3    2.00    0.39233    0.66767

WHERE S=STORAGE(AF);O=OUTFLOW(AF/MIN.);DT=UNIT INTERVAL(MIN.)

### DETENTION BASIN ROUTING RESULTS:

NOTE: COMPUTED BASIN DEPTH, OUTFLOW, AND STORAGE QUANTITIES OCCUR AT THE GIVEN TIME. BASIN INFLOW VALUES REPRESENT THE AVERAGE INFLOW DURING THE RECENT HYDROGRAPH UNIT INTERVAL.

TIME	DEAD-STORAGE	INFLOW	EFFECTIVE	OUTFLOW	EFFECTIVE
(HRS)	FILLED(AF)	(CFS)	DEPTH(FT)	(CFS)	VOLUME(AF)

0.115	0.000	0.15	0.01	0.00	0.002
0.256	0.000	0.15	0.01	0.00	0.003
0.398	0.000	0.15	0.02	0.00	0.005
0.540	0.000	0.15	0.03	0.00	0.007
0.682	0.000	0.15	0.03	0.00	0.009

0.824	0.000	0.15	0.04	0.00	0.010
0.966	0.000	0.15	0.05	0.00	0.012
1.107	0.000	0.15	0.06	0.00	0.014
1.249	0.000	0.15	0.06	0.00	0.016
1.391	0.000	0.15	0.07	0.00	0.017
1.533	0.000	0.15	0.08	0.00	0.019
1.675	0.000	0.16	0.08	0.00	0.021
1.817	0.000	0.16	0.09	0.00	0.023
1.958	0.000	0.16	0.10	0.00	0.025
2.100	0.000	0.16	0.11	0.00	0.027
2.242	0.000	0.16	0.11	0.00	0.028
2.384	0.000	0.16	0.12	0.00	0.030
2.526	0.000	0.16	0.13	0.00	0.032
2.668	0.000	0.16	0.14	0.00	0.034
2.809	0.000	0.16	0.14	0.00	0.036
2.951	0.000	0.16	0.15	0.00	0.038
3.093	0.000	0.17	0.16	0.00	0.040
3.235	0.000	0.17	0.17	0.00	0.042
3.377	0.000	0.17	0.17	0.00	0.044
3.519	0.000	0.17	0.18	0.00	0.046
3.660	0.000	0.17	0.19	0.00	0.048
3.802	0.000	0.17	0.20	0.00	0.050
3.944	0.000	0.17	0.21	0.00	0.052
4.086	0.000	0.17	0.21	0.00	0.054
4.228	0.000	0.18	0.22	0.00	0.056
4.370	0.000	0.18	0.23	0.00	0.058
4.511	0.000	0.18	0.24	0.00	0.060
4.653	0.000	0.18	0.25	0.00	0.062
4.795	0.000	0.18	0.26	0.00	0.064
4.937	0.000	0.18	0.26	0.00	0.066
5.079	0.000	0.19	0.27	0.00	0.068
5.221	0.000	0.19	0.28	0.00	0.070
5.362	0.000	0.19	0.29	0.00	0.073
5.504	0.000	0.19	0.30	0.00	0.075
5.646	0.000	0.19	0.31	0.00	0.077
5.788	0.000	0.19	0.32	0.00	0.079
5.930	0.000	0.20	0.33	0.00	0.082
6.072	0.000	0.20	0.34	0.00	0.084
6.214	0.000	0.20	0.34	0.00	0.086
6.355	0.000	0.20	0.35	0.00	0.088
6.497	0.000	0.20	0.36	0.00	0.091
6.639	0.000	0.20	0.37	0.00	0.093
6.781	0.000	0.21	0.38	0.00	0.095
6.923	0.000	0.21	0.39	0.00	0.098
7.064	0.000	0.21	0.40	0.00	0.100
7.206	0.000	0.21	0.41	0.00	0.103
7.348	0.000	0.22	0.42	0.00	0.105
7.490	0.000	0.22	0.43	0.00	0.108
7.632	0.000	0.22	0.44	0.00	0.110
7.774	0.000	0.22	0.45	0.00	0.113
7.915	0.000	0.22	0.46	0.00	0.115
8.057	0.000	0.23	0.47	0.00	0.118
8.199	0.000	0.23	0.48	0.00	0.121
8.341	0.000	0.23	0.49	0.00	0.123
8.483	0.000	0.24	0.50	0.00	0.126

8.625	0.000	0.24	0.51	0.01	0.129
8.766	0.000	0.24	0.53	0.01	0.131
8.908	0.000	0.24	0.54	0.01	0.134
9.050	0.000	0.25	0.55	0.01	0.137
9.192	0.000	0.25	0.56	0.01	0.140
9.334	0.000	0.25	0.57	0.01	0.143
9.476	0.000	0.26	0.58	0.01	0.146
9.617	0.000	0.26	0.60	0.01	0.149
9.759	0.000	0.26	0.61	0.01	0.152
9.901	0.000	0.27	0.62	0.01	0.155
10.043	0.000	0.27	0.63	0.01	0.158
10.185	0.000	0.28	0.64	0.01	0.161
10.327	0.000	0.28	0.66	0.01	0.164
10.469	0.000	0.29	0.67	0.01	0.168
10.610	0.000	0.29	0.68	0.01	0.171
10.752	0.000	0.30	0.70	0.01	0.174
10.894	0.000	0.30	0.71	0.01	0.178
11.036	0.000	0.31	0.73	0.01	0.181
11.178	0.000	0.31	0.74	0.01	0.185
11.319	0.000	0.32	0.75	0.01	0.189
11.461	0.000	0.32	0.77	0.01	0.192
11.603	0.000	0.33	0.78	0.01	0.196
11.745	0.000	0.34	0.80	0.01	0.200
11.887	0.000	0.35	0.82	0.01	0.204
12.029	0.000	0.35	0.83	0.01	0.208
12.170	0.000	0.38	0.85	0.01	0.212
12.312	0.000	0.38	0.87	0.01	0.217
12.454	0.000	0.40	0.88	0.01	0.221
12.596	0.000	0.40	0.90	0.01	0.226
12.738	0.000	0.42	0.92	0.01	0.231
12.880	0.000	0.42	0.94	0.01	0.235
13.021	0.000	0.44	0.96	0.01	0.240
13.163	0.000	0.45	0.98	0.01	0.246
13.305	0.000	0.47	1.00	0.04	0.251
13.447	0.000	0.48	1.01	0.20	0.254
13.589	0.000	0.50	1.02	0.39	0.255
13.731	0.000	0.51	1.02	0.47	0.256
13.872	0.000	0.54	1.02	0.51	0.256
14.014	0.000	0.56	1.02	0.53	0.256
14.156	0.000	0.55	1.02	0.55	0.256
14.298	0.000	0.57	1.02	0.56	0.257
14.440	0.000	0.61	1.03	0.58	0.257
14.582	0.000	0.64	1.03	0.61	0.257
14.723	0.000	0.70	1.03	0.65	0.258
14.865	0.000	0.73	1.03	0.69	0.258
15.007	0.000	0.81	1.03	0.74	0.259
15.149	0.000	0.86	1.03	0.80	0.260
15.291	0.000	0.99	1.04	0.88	0.261
15.433	0.000	1.05	1.04	0.97	0.262
15.574	0.000	0.75	1.04	0.92	0.260
15.716	0.000	0.88	1.04	0.85	0.260
15.858	0.000	4.90	1.15	2.19	0.292
16.000	0.000	7.37	1.26	4.79	0.322
16.142	0.000	23.49	1.75	11.80	0.459
16.284	0.000	1.97	1.31	12.41	0.337

16.426	0.000	0.65	1.12	5.09	0.285
16.567	0.000	0.92	1.07	2.25	0.269
16.709	0.000	0.77	1.04	1.32	0.262
16.851	0.000	0.67	1.03	0.92	0.259
16.993	0.000	0.59	1.03	0.73	0.258
17.135	0.000	0.57	1.03	0.63	0.257
17.276	0.000	0.53	1.02	0.58	0.256
17.418	0.000	0.49	1.02	0.53	0.256
17.560	0.000	0.46	1.02	0.49	0.256
17.702	0.000	0.43	1.02	0.46	0.255
17.844	0.000	0.41	1.02	0.43	0.255
17.986	0.000	0.39	1.02	0.41	0.255
18.128	0.000	0.36	1.02	0.39	0.254
18.269	0.000	0.34	1.01	0.36	0.254
18.411	0.000	0.33	1.01	0.34	0.254
18.553	0.000	0.32	1.01	0.33	0.254
18.695	0.000	0.30	1.01	0.32	0.254
18.837	0.000	0.29	1.01	0.30	0.253
18.978	0.000	0.28	1.01	0.29	0.253
19.120	0.000	0.27	1.01	0.28	0.253
19.262	0.000	0.27	1.01	0.28	0.253
19.404	0.000	0.26	1.01	0.27	0.253
19.546	0.000	0.25	1.01	0.26	0.253
19.688	0.000	0.25	1.01	0.25	0.253
19.830	0.000	0.24	1.01	0.25	0.253
19.971	0.000	0.23	1.01	0.24	0.253
20.113	0.000	0.23	1.01	0.23	0.253
20.255	0.000	0.22	1.01	0.23	0.253
20.397	0.000	0.22	1.01	0.22	0.253
20.539	0.000	0.21	1.01	0.22	0.252
20.681	0.000	0.21	1.01	0.21	0.252
20.822	0.000	0.21	1.01	0.21	0.252
20.964	0.000	0.20	1.01	0.21	0.252
21.106	0.000	0.20	1.01	0.20	0.252
21.248	0.000	0.19	1.01	0.20	0.252
21.390	0.000	0.19	1.01	0.19	0.252
21.531	0.000	0.19	1.01	0.19	0.252
21.673	0.000	0.18	1.01	0.19	0.252
21.815	0.000	0.18	1.01	0.18	0.252
21.957	0.000	0.18	1.01	0.18	0.252
22.099	0.000	0.18	1.01	0.18	0.252
22.241	0.000	0.17	1.01	0.18	0.252
22.382	0.000	0.17	1.01	0.17	0.252
22.524	0.000	0.17	1.01	0.17	0.252
22.666	0.000	0.17	1.01	0.17	0.252
22.808	0.000	0.16	1.01	0.17	0.252
22.950	0.000	0.16	1.01	0.16	0.252
23.092	0.000	0.16	1.01	0.16	0.252
23.233	0.000	0.16	1.01	0.16	0.252
23.375	0.000	0.15	1.01	0.16	0.252
23.517	0.000	0.15	1.01	0.15	0.252
23.659	0.000	0.15	1.01	0.15	0.252
23.801	0.000	0.15	1.01	0.15	0.252
23.943	0.000	0.15	1.01	0.15	0.252
24.085	0.000	0.15	1.01	0.15	0.252

24.226 0.000 0.00 1.00 0.10 0.250

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### Hydrograph - Basin D Tributary to Infiltration Basin 2 - 100 Year Storm Event

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\*\*\* NON-HOMOGENEOUS WATERSHED AREA-AVERAGED LOSS RATE (Fm)  
AND LOW LOSS FRACTION ESTIMATIONS FOR AMC I:

TOTAL 24-HOUR DURATION RAINFALL DEPTH = 3.28 (inches)

SOIL-COVER TYPE	AREA (Acres)	PERCENT OF PREVIOUS AREA	SCS CURVE NUMBER	LOSS RATE Fp(in./hr.)	YIELD
1	1.08	100.00	90.(AMC II)	0.400	0.406
2	0.52	0.00	98.(AMC II)	0.000	0.929

TOTAL AREA (Acres) = 1.60

AREA-AVERAGED LOSS RATE, Fm (in./hr.) = 0.272

AREA-AVERAGED LOW LOSS FRACTION, Y = 0.426

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RATIONAL METHOD CALIBRATION COEFFICIENT = 0.98

TOTAL CATCHMENT AREA(ACRES) = 1.60

SOIL-LOSS RATE, Fm,(INCH/HR) = 0.272

LOW LOSS FRACTION = 0.426

TIME OF CONCENTRATION(MIN.) = 10.83

SMALL AREA PEAK Q COMPUTED USING PEAK FLOW RATE FORMULA

USER SPECIFIED RAINFALL VALUES ARE USED

RETURN FREQUENCY(YEARS) = 100

5-MINUTE POINT RAINFALL VALUE(INCHES) = 0.41

30-MINUTE POINT RAINFALL VALUE(INCHES) = 0.95

1-HOUR POINT RAINFALL VALUE(INCHES) = 1.08

3-HOUR POINT RAINFALL VALUE(INCHES) = 1.57

6-HOUR POINT RAINFALL VALUE(INCHES) = 2.02

24-HOUR POINT RAINFALL VALUE(INCHES) = 3.28

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TOTAL CATCHMENT RUNOFF VOLUME(ACRE-FEET) = 0.28

TOTAL CATCHMENT SOIL-LOSS VOLUME(ACRE-FEET) = 0.16

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TIME (HOURS)	VOLUME (AF)	Q 0. (CFS)	2.5	5.0	7.5	10.0
--------------	-------------	------------	-----	-----	-----	------

0.12	0.0000	0.00 Q	.	.	.	.
0.30	0.0003	0.04 Q	.	.	.	.
0.48	0.0010	0.04 Q	.	.	.	.
0.66	0.0016	0.04 Q	.	.	.	.
0.84	0.0023	0.04 Q	.	.	.	.
1.02	0.0030	0.04 Q	.	.	.	.
1.20	0.0036	0.05 Q	.	.	.	.
1.38	0.0043	0.05 Q	.	.	.	.
1.56	0.0050	0.05 Q	.	.	.	.

1.74	0.0057	0.05	Q	.	.	.
1.92	0.0064	0.05	Q	.	.	.
2.10	0.0071	0.05	Q	.	.	.
2.28	0.0078	0.05	Q	.	.	.
2.46	0.0085	0.05	Q	.	.	.
2.64	0.0092	0.05	Q	.	.	.
2.82	0.0099	0.05	Q	.	.	.
3.00	0.0106	0.05	Q	.	.	.
3.18	0.0114	0.05	Q	.	.	.
3.37	0.0121	0.05	Q	.	.	.
3.55	0.0129	0.05	Q	.	.	.
3.73	0.0136	0.05	Q	.	.	.
3.91	0.0144	0.05	Q	.	.	.
4.09	0.0151	0.05	Q	.	.	.
4.27	0.0159	0.05	Q	.	.	.
4.45	0.0167	0.05	Q	.	.	.
4.63	0.0175	0.05	Q	.	.	.
4.81	0.0183	0.05	Q	.	.	.
4.99	0.0191	0.05	Q	.	.	.
5.17	0.0199	0.06	Q	.	.	.
5.35	0.0208	0.06	Q	.	.	.
5.53	0.0216	0.06	Q	.	.	.
5.71	0.0224	0.06	Q	.	.	.
5.89	0.0233	0.06	Q	.	.	.
6.07	0.0242	0.06	Q	.	.	.
6.25	0.0250	0.06	Q	.	.	.
6.43	0.0259	0.06	Q	.	.	.
6.61	0.0268	0.06	Q	.	.	.
6.79	0.0277	0.06	Q	.	.	.
6.97	0.0286	0.06	Q	.	.	.
7.16	0.0296	0.06	Q	.	.	.
7.34	0.0305	0.06	Q	.	.	.
7.52	0.0315	0.06	Q	.	.	.
7.70	0.0324	0.07	Q	.	.	.
7.88	0.0334	0.07	Q	.	.	.
8.06	0.0344	0.07	Q	.	.	.
8.24	0.0354	0.07	Q	.	.	.
8.42	0.0364	0.07	Q	.	.	.
8.60	0.0375	0.07	Q	.	.	.
8.78	0.0385	0.07	Q	.	.	.
8.96	0.0396	0.07	Q	.	.	.
9.14	0.0407	0.07	Q	.	.	.
9.32	0.0418	0.08	Q	.	.	.
9.50	0.0429	0.08	Q	.	.	.
9.68	0.0441	0.08	Q	.	.	.
9.86	0.0453	0.08	Q	.	.	.
10.04	0.0465	0.08	Q	.	.	.
10.22	0.0477	0.08	Q	.	.	.
10.40	0.0489	0.08	Q	.	.	.
10.59	0.0502	0.09	Q	.	.	.
10.77	0.0515	0.09	Q	.	.	.
10.95	0.0528	0.09	Q	.	.	.
11.13	0.0541	0.09	Q	.	.	.
11.31	0.0555	0.09	Q	.	.	.
11.49	0.0569	0.10	Q	.	.	.

11.67	0.0584	0.10	Q	.	.	.	.
11.85	0.0599	0.10	Q	.	.	.	.
12.03	0.0614	0.10	Q	.	.	.	.
12.21	0.0630	0.11	Q	.	.	.	.
12.39	0.0647	0.11	Q	.	.	.	.
12.57	0.0665	0.12	Q	.	.	.	.
12.75	0.0683	0.12	Q	.	.	.	.
12.93	0.0701	0.13	Q	.	.	.	.
13.11	0.0721	0.13	Q	.	.	.	.
13.29	0.0741	0.14	Q	.	.	.	.
13.47	0.0761	0.14	Q	.	.	.	.
13.65	0.0783	0.15	Q	.	.	.	.
13.83	0.0806	0.16	Q	.	.	.	.
14.01	0.0830	0.17	Q	.	.	.	.
14.20	0.0855	0.17	Q	.	.	.	.
14.38	0.0880	0.18	Q	.	.	.	.
14.56	0.0907	0.18	Q	.	.	.	.
14.74	0.0936	0.21	Q	.	.	.	.
14.92	0.0968	0.22	Q	.	.	.	.
15.10	0.1003	0.25	Q	.	.	.	.
15.28	0.1042	0.27	Q	.	.	.	.
15.46	0.1081	0.25	Q	.	.	.	.
15.64	0.1115	0.21	Q	.	.	.	.
15.82	0.1196	0.87	Q	.	.	.	.
16.00	0.1376	1.54	Q	.	.	.	.
16.18	0.1842	4.71	.	Q	.	.	.
16.36	0.2213	0.26	Q	.	.	.	.
16.54	0.2255	0.30	Q	.	.	.	.
16.72	0.2294	0.23	Q	.	.	.	.
16.90	0.2326	0.19	Q	.	.	.	.
17.08	0.2353	0.17	Q	.	.	.	.
17.26	0.2378	0.16	Q	.	.	.	.
17.44	0.2401	0.15	Q	.	.	.	.
17.62	0.2422	0.13	Q	.	.	.	.
17.81	0.2441	0.12	Q	.	.	.	.
17.99	0.2459	0.12	Q	.	.	.	.
18.17	0.2475	0.11	Q	.	.	.	.
18.35	0.2491	0.10	Q	.	.	.	.
18.53	0.2505	0.10	Q	.	.	.	.
18.71	0.2519	0.09	Q	.	.	.	.
18.89	0.2533	0.09	Q	.	.	.	.
19.07	0.2545	0.08	Q	.	.	.	.
19.25	0.2557	0.08	Q	.	.	.	.
19.43	0.2569	0.08	Q	.	.	.	.
19.61	0.2580	0.07	Q	.	.	.	.
19.79	0.2591	0.07	Q	.	.	.	.
19.97	0.2602	0.07	Q	.	.	.	.
20.15	0.2612	0.07	Q	.	.	.	.
20.33	0.2622	0.07	Q	.	.	.	.
20.51	0.2632	0.06	Q	.	.	.	.
20.69	0.2641	0.06	Q	.	.	.	.
20.87	0.2650	0.06	Q	.	.	.	.
21.05	0.2659	0.06	Q	.	.	.	.
21.23	0.2668	0.06	Q	.	.	.	.
21.42	0.2677	0.06	Q	.	.	.	.

21.60	0.2685	0.06	Q	.	.	.	.
21.78	0.2693	0.05	Q	.	.	.	.
21.96	0.2701	0.05	Q	.	.	.	.
22.14	0.2709	0.05	Q	.	.	.	.
22.32	0.2717	0.05	Q	.	.	.	.
22.50	0.2724	0.05	Q	.	.	.	.
22.68	0.2732	0.05	Q	.	.	.	.
22.86	0.2739	0.05	Q	.	.	.	.
23.04	0.2746	0.05	Q	.	.	.	.
23.22	0.2753	0.05	Q	.	.	.	.
23.40	0.2760	0.05	Q	.	.	.	.
23.58	0.2767	0.05	Q	.	.	.	.
23.76	0.2774	0.04	Q	.	.	.	.
23.94	0.2780	0.04	Q	.	.	.	.
24.12	0.2787	0.04	Q	.	.	.	.
24.30	0.2790	0.00	Q	.	.	.	.

## Routed Hydrograph - Basin D Routed Thru Infiltration Basin 2 - 100 Year Storm Event

### FLOW-THROUGH DETENTION BASIN MODEL

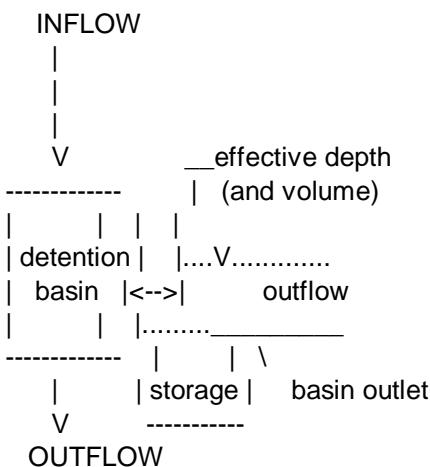
SPECIFIED BASIN CONDITIONS ARE AS FOLLOWS:

CONSTANT HYDROGRAPH TIME UNIT(MINUTES) = 10.830

DEAD STORAGE(AF) = 0.00

SPECIFIED DEAD STORAGE(AF) FILLED = 0.00

ASSUMED INITIAL DEPTH(FEET) IN STORAGE BASIN = 0.00



### DEPTH-VS.-STORAGE AND DEPTH-VS.-DISCHARGE INFORMATION:

TOTAL NUMBER OF BASIN DEPTH INFORMATION ENTRIES = 4

\*BASIN-DEPTH STORAGE OUTFLOW \*\*BASIN-DEPTH STORAGE OUTFLOW \*

\* (FEET) (ACRE-FEET) (CFS) \*\* (FEET) (ACRE-FEET) (CFS) \*

\* 0.000 0.000 0.000\*\* 1.000 0.010 0.010\*

\* 2.000 0.030 0.010\*\* 3.000 0.070 4.710\*

### BASIN STORAGE, OUTFLOW AND DEPTH ROUTING VALUES:

INTERVAL DEPTH {S-O\*DT/2} {S+O\*DT/2}

NUMBER (FEET) (ACRE-FEET) (ACRE-FEET)

1 0.00 0.00000 0.00000

2 1.00 0.00993 0.01007

3 2.00 0.02993 0.03007

4 3.00 0.03487 0.10513

WHERE S=STORAGE(AF);O=OUTFLOW(AF/MIN.);DT=UNIT INTERVAL(MIN.)

### DETENTION BASIN ROUTING RESULTS:

NOTE: COMPUTED BASIN DEPTH, OUTFLOW, AND STORAGE QUANTITIES

OCCUR AT THE GIVEN TIME. BASIN INFLOW VALUES REPRESENT THE  
AVERAGE INFLOW DURING THE RECENT HYDROGRAPH UNIT INTERVAL.

TIME (HRS)	DEAD-STORAGE FILLED(AF)	INFLOW (CFS)	EFFECTIVE DEPTH(FT)	OUTFLOW (CFS)	EFFECTIVE VOLUME(AF)
------------	-------------------------	--------------	---------------------	---------------	----------------------

0.116	0.000	0.00	0.00	0.00	0.000
-------	-------	------	------	------	-------

0.297	0.000	0.04	0.06	0.00	0.001
-------	-------	------	------	------	-------

0.477	0.000	0.04	0.13	0.00	0.001
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0.658	0.000	0.04	0.19	0.00	0.002
-------	-------	------	------	------	-------

0.838	0.000	0.04	0.25	0.00	0.003
1.019	0.000	0.04	0.32	0.00	0.003
1.199	0.000	0.05	0.38	0.00	0.004
1.380	0.000	0.05	0.44	0.00	0.004
1.560	0.000	0.05	0.50	0.00	0.005
1.741	0.000	0.05	0.56	0.01	0.006
1.921	0.000	0.05	0.62	0.01	0.006
2.102	0.000	0.05	0.68	0.01	0.007
2.282	0.000	0.05	0.74	0.01	0.007
2.463	0.000	0.05	0.80	0.01	0.008
2.643	0.000	0.05	0.86	0.01	0.009
2.824	0.000	0.05	0.92	0.01	0.009
3.004	0.000	0.05	0.98	0.01	0.010
3.185	0.000	0.05	1.02	0.01	0.010
3.365	0.000	0.05	1.05	0.01	0.011
3.546	0.000	0.05	1.08	0.01	0.012
3.726	0.000	0.05	1.11	0.01	0.012
3.907	0.000	0.05	1.14	0.01	0.013
4.087	0.000	0.05	1.17	0.01	0.013
4.268	0.000	0.05	1.20	0.01	0.014
4.448	0.000	0.05	1.24	0.01	0.015
4.628	0.000	0.05	1.27	0.01	0.015
4.809	0.000	0.05	1.30	0.01	0.016
4.990	0.000	0.05	1.33	0.01	0.017
5.170	0.000	0.06	1.37	0.01	0.017
5.351	0.000	0.06	1.40	0.01	0.018
5.531	0.000	0.06	1.44	0.01	0.019
5.712	0.000	0.06	1.47	0.01	0.019
5.892	0.000	0.06	1.51	0.01	0.020
6.073	0.000	0.06	1.54	0.01	0.021
6.253	0.000	0.06	1.58	0.01	0.022
6.434	0.000	0.06	1.62	0.01	0.022
6.614	0.000	0.06	1.65	0.01	0.023
6.795	0.000	0.06	1.69	0.01	0.024
6.975	0.000	0.06	1.73	0.01	0.025
7.156	0.000	0.06	1.77	0.01	0.025
7.336	0.000	0.06	1.81	0.01	0.026
7.516	0.000	0.06	1.85	0.01	0.027
7.697	0.000	0.07	1.89	0.01	0.028
7.878	0.000	0.07	1.93	0.01	0.029
8.058	0.000	0.07	1.98	0.01	0.030
8.238	0.000	0.07	2.01	0.02	0.030
8.419	0.000	0.07	2.01	0.05	0.030
8.600	0.000	0.07	2.01	0.07	0.031
8.780	0.000	0.07	2.01	0.07	0.031
8.960	0.000	0.07	2.01	0.07	0.031
9.141	0.000	0.07	2.01	0.07	0.031
9.321	0.000	0.08	2.01	0.07	0.031
9.502	0.000	0.08	2.01	0.08	0.031
9.682	0.000	0.08	2.01	0.08	0.031
9.863	0.000	0.08	2.01	0.08	0.031
10.043	0.000	0.08	2.02	0.08	0.031
10.224	0.000	0.08	2.02	0.08	0.031
10.405	0.000	0.08	2.02	0.08	0.031
10.585	0.000	0.09	2.02	0.08	0.031

10.766	0.000	0.09	2.02	0.09	0.031
10.946	0.000	0.09	2.02	0.09	0.031
11.127	0.000	0.09	2.02	0.09	0.031
11.307	0.000	0.09	2.02	0.09	0.031
11.488	0.000	0.10	2.02	0.09	0.031
11.668	0.000	0.10	2.02	0.10	0.031
11.848	0.000	0.10	2.02	0.10	0.031
12.029	0.000	0.10	2.02	0.10	0.031
12.210	0.000	0.11	2.02	0.11	0.031
12.390	0.000	0.11	2.02	0.11	0.031
12.570	0.000	0.12	2.02	0.12	0.031
12.751	0.000	0.12	2.02	0.12	0.031
12.932	0.000	0.13	2.02	0.12	0.031
13.112	0.000	0.13	2.03	0.13	0.031
13.292	0.000	0.14	2.03	0.13	0.031
13.473	0.000	0.14	2.03	0.14	0.031
13.654	0.000	0.15	2.03	0.15	0.031
13.834	0.000	0.16	2.03	0.15	0.031
14.014	0.000	0.17	2.03	0.16	0.031
14.195	0.000	0.17	2.03	0.17	0.031
14.376	0.000	0.18	2.04	0.17	0.031
14.556	0.000	0.18	2.04	0.18	0.031
14.736	0.000	0.21	2.04	0.19	0.032
14.917	0.000	0.22	2.04	0.21	0.032
15.097	0.000	0.25	2.05	0.23	0.032
15.278	0.000	0.27	2.06	0.26	0.032
15.458	0.000	0.25	2.05	0.26	0.032
15.639	0.000	0.21	2.04	0.23	0.032
15.819	0.000	0.87	2.17	0.52	0.037
16.000	0.000	1.54	2.32	1.16	0.043
16.181	0.000	4.71	2.95	3.00	0.068
16.361	0.000	0.26	2.11	2.52	0.035
16.542	0.000	0.30	2.06	0.43	0.033
16.722	0.000	0.23	2.05	0.28	0.032
16.903	0.000	0.19	2.04	0.22	0.032
17.083	0.000	0.17	2.03	0.18	0.031
17.264	0.000	0.16	2.03	0.17	0.031
17.444	0.000	0.15	2.03	0.15	0.031
17.625	0.000	0.13	2.03	0.14	0.031
17.805	0.000	0.12	2.02	0.13	0.031
17.986	0.000	0.12	2.02	0.12	0.031
18.166	0.000	0.11	2.02	0.11	0.031
18.347	0.000	0.10	2.02	0.10	0.031
18.527	0.000	0.10	2.02	0.10	0.031
18.707	0.000	0.09	2.02	0.09	0.031
18.888	0.000	0.09	2.02	0.09	0.031
19.069	0.000	0.08	2.02	0.09	0.031
19.249	0.000	0.08	2.01	0.08	0.031
19.430	0.000	0.08	2.01	0.08	0.031
19.610	0.000	0.07	2.01	0.08	0.031
19.791	0.000	0.07	2.01	0.07	0.031
19.971	0.000	0.07	2.01	0.07	0.031
20.151	0.000	0.07	2.01	0.07	0.030
20.332	0.000	0.07	2.01	0.07	0.030
20.513	0.000	0.06	2.01	0.07	0.030

20.693	0.000	0.06	2.01	0.06	0.030
20.874	0.000	0.06	2.01	0.06	0.030
21.054	0.000	0.06	2.01	0.06	0.030
21.234	0.000	0.06	2.01	0.06	0.030
21.415	0.000	0.06	2.01	0.06	0.030
21.595	0.000	0.06	2.01	0.06	0.030
21.776	0.000	0.05	2.01	0.05	0.030
21.957	0.000	0.05	2.01	0.05	0.030
22.137	0.000	0.05	2.01	0.05	0.030
22.318	0.000	0.05	2.01	0.05	0.030
22.498	0.000	0.05	2.01	0.05	0.030
22.678	0.000	0.05	2.01	0.05	0.030
22.859	0.000	0.05	2.01	0.05	0.030
23.039	0.000	0.05	2.01	0.05	0.030
23.220	0.000	0.05	2.01	0.05	0.030
23.401	0.000	0.05	2.01	0.05	0.030
23.581	0.000	0.05	2.01	0.05	0.030
23.761	0.000	0.04	2.01	0.04	0.030
23.942	0.000	0.04	2.01	0.04	0.030
24.122	0.000	0.04	2.01	0.04	0.030
24.303	0.000	0.00	1.99	0.03	0.030

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### Hydrograph - Basin E Tributary to Infiltration Basin 3 - 100 Year Storm Event

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\*\*\* NON-HOMOGENEOUS WATERSHED AREA-AVERAGED LOSS RATE (Fm)  
AND LOW LOSS FRACTION ESTIMATIONS FOR AMC I:

TOTAL 24-HOUR DURATION RAINFALL DEPTH = 3.28 (inches)

SOIL-COVER TYPE	AREA (Acres)	PERCENT OF PREVIOUS AREA	SCS CURVE NUMBER	LOSS RATE Fp(in./hr.)	YIELD
1	0.53	0.00	98.(AMC II)	0.000	0.929
2	12.84	100.00	90.(AMC II)	0.400	0.406

TOTAL AREA (Acres) = 13.37

AREA-AVERAGED LOSS RATE, Fm (in./hr.) = 0.384

AREA-AVERAGED LOW LOSS FRACTION, Y = 0.573

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RATIONAL METHOD CALIBRATION COEFFICIENT = 0.93

TOTAL CATCHMENT AREA(ACRES) = 13.37

SOIL-LOSS RATE, Fm,(INCH/HR) = 0.384

LOW LOSS FRACTION = 0.573

TIME OF CONCENTRATION(MIN.) = 14.17

SMALL AREA PEAK Q COMPUTED USING PEAK FLOW RATE FORMULA

USER SPECIFIED RAINFALL VALUES ARE USED

RETURN FREQUENCY(YEARS) = 100

5-MINUTE POINT RAINFALL VALUE(INCHES) = 0.41

30-MINUTE POINT RAINFALL VALUE(INCHES) = 0.95

1-HOUR POINT RAINFALL VALUE(INCHES) = 1.08

3-HOUR POINT RAINFALL VALUE(INCHES) = 1.57

6-HOUR POINT RAINFALL VALUE(INCHES) = 2.02

24-HOUR POINT RAINFALL VALUE(INCHES) = 3.28

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TOTAL CATCHMENT RUNOFF VOLUME(ACRE-FEET) = 1.79

TOTAL CATCHMENT SOIL-LOSS VOLUME(ACRE-FEET) = 1.86

\*\*\*\*\*

TIME (HOURS)	VOLUME (AF)	Q 0. (CFS)	10.0	20.0	30.0	40.0
--------------	-------------	------------	------	------	------	------

0.18	0.0018	0.25 Q	.	.	.	.
0.41	0.0068	0.25 Q	.	.	.	.
0.65	0.0118	0.26 Q	.	.	.	.
0.89	0.0169	0.26 Q	.	.	.	.
1.12	0.0220	0.26 Q	.	.	.	.
1.36	0.0271	0.26 Q	.	.	.	.
1.59	0.0323	0.27 Q	.	.	.	.
1.83	0.0376	0.27 Q	.	.	.	.
2.07	0.0429	0.27 Q	.	.	.	.
2.30	0.0483	0.28 Q	.	.	.	.

2.54	0.0537	0.28	Q	.	.	.
2.77	0.0592	0.28	Q	.	.	.
3.01	0.0648	0.29	Q	.	.	.
3.25	0.0704	0.29	Q	.	.	.
3.48	0.0761	0.29	Q	.	.	.
3.72	0.0818	0.30	Q	.	.	.
3.96	0.0877	0.30	Q	.	.	.
4.19	0.0936	0.30	Q	.	.	.
4.43	0.0996	0.31	Q	.	.	.
4.66	0.1056	0.31	Q	.	.	.
4.90	0.1118	0.32	Q	.	.	.
5.14	0.1180	0.32	Q	.	.	.
5.37	0.1243	0.33	Q	.	.	.
5.61	0.1307	0.33	Q	.	.	.
5.84	0.1372	0.34	Q	.	.	.
6.08	0.1438	0.34	Q	.	.	.
6.32	0.1505	0.35	Q	.	.	.
6.55	0.1573	0.35	Q	.	.	.
6.79	0.1642	0.36	Q	.	.	.
7.03	0.1712	0.36	Q	.	.	.
7.26	0.1784	0.37	Q	.	.	.
7.50	0.1856	0.37	Q	.	.	.
7.73	0.1930	0.38	Q	.	.	.
7.97	0.2006	0.39	Q	.	.	.
8.21	0.2082	0.40	Q	.	.	.
8.44	0.2160	0.40	Q	.	.	.
8.68	0.2240	0.41	Q	.	.	.
8.91	0.2322	0.42	Q	.	.	.
9.15	0.2405	0.43	Q	.	.	.
9.39	0.2490	0.44	Q	.	.	.
9.62	0.2577	0.45	Q	.	.	.
9.86	0.2666	0.46	Q	.	.	.
10.10	0.2757	0.47	Q	.	.	.
10.33	0.2850	0.48	Q	.	.	.
10.57	0.2946	0.50	Q	.	.	.
10.80	0.3045	0.51	Q	.	.	.
11.04	0.3147	0.53	Q	.	.	.
11.28	0.3251	0.54	Q	.	.	.
11.51	0.3359	0.56	Q	.	.	.
11.75	0.3471	0.58	Q	.	.	.
11.99	0.3586	0.61	Q	.	.	.
12.22	0.3707	0.63	Q	.	.	.
12.46	0.3835	0.68	Q	.	.	.
12.69	0.3969	0.70	Q	.	.	.
12.93	0.4110	0.74	Q	.	.	.
13.17	0.4257	0.77	Q	.	.	.
13.40	0.4412	0.82	Q	.	.	.
13.64	0.4575	0.85	Q	.	.	.
13.87	0.4748	0.92	Q	.	.	.
14.11	0.4933	0.97	Q	.	.	.
14.35	0.5126	1.01	.Q	.	.	.
14.58	0.5328	1.07	.Q	.	.	.
14.82	0.5553	1.23	.Q	.	.	.
15.06	0.5803	1.33	.Q	.	.	.
15.29	0.6093	1.64	.Q	.	.	.

15.53	0.6415	1.66	.Q	.	.	.	.
15.76	0.6770	1.98	.Q	.	.	.	.
16.00	0.7812	8.70	.	Q.	.	.	.
16.24	1.1616	30.28	.	.	Q	.	.
16.47	1.4692	1.24	.Q	.	.	.	.
16.71	1.4956	1.47	.Q	.	.	.	.
16.94	1.5211	1.14	.Q	.	.	.	.
17.18	1.5417	0.97	Q	.	.	.	.
17.42	1.5598	0.89	Q	.	.	.	.
17.65	1.5762	0.79	Q	.	.	.	.
17.89	1.5910	0.72	Q	.	.	.	.
18.13	1.6045	0.66	Q	.	.	.	.
18.36	1.6167	0.59	Q	.	.	.	.
18.60	1.6279	0.55	Q	.	.	.	.
18.83	1.6383	0.52	Q	.	.	.	.
19.07	1.6482	0.49	Q	.	.	.	.
19.31	1.6576	0.47	Q	.	.	.	.
19.54	1.6665	0.45	Q	.	.	.	.
19.78	1.6750	0.43	Q	.	.	.	.
20.01	1.6831	0.41	Q	.	.	.	.
20.25	1.6909	0.39	Q	.	.	.	.
20.49	1.6985	0.38	Q	.	.	.	.
20.72	1.7057	0.37	Q	.	.	.	.
20.96	1.7128	0.35	Q	.	.	.	.
21.20	1.7196	0.34	Q	.	.	.	.
21.43	1.7262	0.33	Q	.	.	.	.
21.67	1.7326	0.32	Q	.	.	.	.
21.90	1.7388	0.31	Q	.	.	.	.
22.14	1.7449	0.31	Q	.	.	.	.
22.38	1.7508	0.30	Q	.	.	.	.
22.61	1.7565	0.29	Q	.	.	.	.
22.85	1.7621	0.28	Q	.	.	.	.
23.08	1.7676	0.28	Q	.	.	.	.
23.32	1.7730	0.27	Q	.	.	.	.
23.56	1.7783	0.27	Q	.	.	.	.
23.79	1.7834	0.26	Q	.	.	.	.
24.03	1.7885	0.26	Q	.	.	.	.
24.27	1.7910	0.00	Q	.	.	.	.

## Routed Hydrograph - Basin E Routed Thru Infiltration Basin 3 - 100 Year Storm Event

### FLOW-THROUGH DETENTION BASIN MODEL

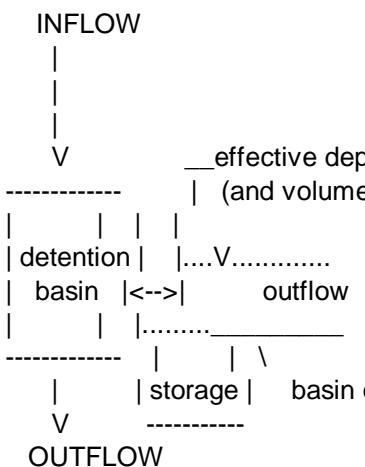
SPECIFIED BASIN CONDITIONS ARE AS FOLLOWS:

CONSTANT HYDROGRAPH TIME UNIT(MINUTES) = 14.170

DEAD STORAGE(AF) = 0.00

SPECIFIED DEAD STORAGE(AF) FILLED = 0.00

ASSUMED INITIAL DEPTH(FEET) IN STORAGE BASIN = 0.00



### DEPTH-VS.-STORAGE AND DEPTH-VS.-DISCHARGE INFORMATION:

TOTAL NUMBER OF BASIN DEPTH INFORMATION ENTRIES = 3

\*BASIN-DEPTH STORAGE OUTFLOW \*\*BASIN-DEPTH STORAGE OUTFLOW \*

\* (FEET) (ACRE-FEET) (CFS) \*\* (FEET) (ACRE-FEET) (CFS) \*

\* 0.000 0.000 0.000\*\* 1.000 0.080 0.010\*

\* 2.000 0.170 43.500\*\*

### BASIN STORAGE, OUTFLOW AND DEPTH ROUTING VALUES:

INTERVAL DEPTH {S-O\*DT/2} {S+O\*DT/2}

NUMBER (FEET) (ACRE-FEET) (ACRE-FEET)

1 0.00 0.00000 0.00000

2 1.00 0.07990 0.08010

3 2.00 -0.25451 0.59451

WHERE S=STORAGE(AF);O=OUTFLOW(AF/MIN.);DT=UNIT INTERVAL(MIN.)

### DETENTION BASIN ROUTING RESULTS:

NOTE: COMPUTED BASIN DEPTH, OUTFLOW, AND STORAGE QUANTITIES OCCUR AT THE GIVEN TIME. BASIN INFLOW VALUES REPRESENT THE AVERAGE INFLOW DURING THE RECENT HYDROGRAPH UNIT INTERVAL.

TIME (HRS)	DEAD-STORAGE FILLED(AF)	INFLOW (CFS)	EFFECTIVE DEPTH(FT)	OUTFLOW (CFS)	EFFECTIVE VOLUME(AF)
------------	-------------------------	--------------	---------------------	---------------	----------------------

0.177	0.000	0.25	0.06	0.00	0.005
0.413	0.000	0.25	0.12	0.00	0.010
0.649	0.000	0.26	0.19	0.00	0.015
0.885	0.000	0.26	0.25	0.00	0.020
1.121	0.000	0.26	0.31	0.00	0.025

1.358	0.000	0.26	0.38	0.00	0.030
1.594	0.000	0.27	0.44	0.00	0.035
1.830	0.000	0.27	0.51	0.00	0.040
2.066	0.000	0.27	0.57	0.01	0.046
2.302	0.000	0.28	0.64	0.01	0.051
2.539	0.000	0.28	0.70	0.01	0.056
2.775	0.000	0.28	0.77	0.01	0.062
3.011	0.000	0.29	0.84	0.01	0.067
3.247	0.000	0.29	0.91	0.01	0.073
3.483	0.000	0.29	0.98	0.01	0.078
3.719	0.000	0.30	1.01	0.17	0.081
3.956	0.000	0.30	1.01	0.31	0.081
4.192	0.000	0.30	1.01	0.30	0.081
4.428	0.000	0.31	1.01	0.31	0.081
4.664	0.000	0.31	1.01	0.31	0.081
4.900	0.000	0.32	1.01	0.32	0.081
5.136	0.000	0.32	1.01	0.32	0.081
5.372	0.000	0.33	1.01	0.33	0.081
5.609	0.000	0.33	1.01	0.33	0.081
5.845	0.000	0.34	1.01	0.34	0.081
6.081	0.000	0.34	1.01	0.34	0.081
6.317	0.000	0.35	1.01	0.35	0.081
6.553	0.000	0.35	1.01	0.35	0.081
6.789	0.000	0.36	1.01	0.36	0.081
7.026	0.000	0.36	1.01	0.36	0.081
7.262	0.000	0.37	1.01	0.37	0.081
7.498	0.000	0.37	1.01	0.37	0.081
7.734	0.000	0.38	1.01	0.38	0.081
7.970	0.000	0.39	1.01	0.39	0.081
8.207	0.000	0.40	1.01	0.40	0.081
8.443	0.000	0.40	1.01	0.40	0.081
8.679	0.000	0.41	1.01	0.41	0.081
8.915	0.000	0.42	1.01	0.42	0.081
9.151	0.000	0.43	1.01	0.43	0.081
9.387	0.000	0.44	1.01	0.44	0.081
9.623	0.000	0.45	1.01	0.45	0.081
9.860	0.000	0.46	1.01	0.46	0.081
10.096	0.000	0.47	1.01	0.47	0.081
10.332	0.000	0.48	1.01	0.48	0.081
10.568	0.000	0.50	1.01	0.50	0.081
10.804	0.000	0.51	1.01	0.51	0.081
11.040	0.000	0.53	1.01	0.53	0.081
11.277	0.000	0.54	1.01	0.54	0.081
11.513	0.000	0.56	1.01	0.56	0.081
11.749	0.000	0.58	1.01	0.58	0.081
11.985	0.000	0.61	1.01	0.60	0.081
12.221	0.000	0.63	1.01	0.63	0.081
12.458	0.000	0.68	1.02	0.67	0.081
12.694	0.000	0.70	1.02	0.70	0.081
12.930	0.000	0.74	1.02	0.73	0.082
13.166	0.000	0.77	1.02	0.77	0.082
13.402	0.000	0.82	1.02	0.81	0.082
13.638	0.000	0.85	1.02	0.85	0.082
13.874	0.000	0.92	1.02	0.91	0.082
14.111	0.000	0.97	1.02	0.97	0.082

14.347	0.000	1.01	1.02	1.00	0.082
14.583	0.000	1.07	1.02	1.06	0.082
14.819	0.000	1.23	1.03	1.20	0.083
15.055	0.000	1.33	1.03	1.33	0.083
15.292	0.000	1.64	1.04	1.59	0.084
15.528	0.000	1.66	1.04	1.69	0.083
15.764	0.000	1.98	1.05	1.90	0.085
16.000	0.000	8.70	1.30	7.57	0.107
16.236	0.000	30.28	1.99	28.05	0.169
16.472	0.000	1.24	0.30	21.60	0.024
16.708	0.000	1.47	0.66	0.00	0.053
16.945	0.000	1.14	0.94	0.01	0.075
17.181	0.000	0.97	1.03	0.59	0.082
17.417	0.000	0.89	1.02	0.93	0.081
17.653	0.000	0.79	1.02	0.78	0.082
17.889	0.000	0.72	1.01	0.74	0.081
18.125	0.000	0.66	1.02	0.66	0.081
18.362	0.000	0.59	1.01	0.61	0.081
18.598	0.000	0.55	1.01	0.55	0.081
18.834	0.000	0.52	1.01	0.53	0.081
19.070	0.000	0.49	1.01	0.49	0.081
19.306	0.000	0.47	1.01	0.47	0.081
19.543	0.000	0.45	1.01	0.45	0.081
19.779	0.000	0.43	1.01	0.43	0.081
20.015	0.000	0.41	1.01	0.41	0.081
20.251	0.000	0.39	1.01	0.40	0.081
20.487	0.000	0.38	1.01	0.38	0.081
20.723	0.000	0.37	1.01	0.37	0.081
20.959	0.000	0.35	1.01	0.36	0.081
21.196	0.000	0.34	1.01	0.34	0.081
21.432	0.000	0.33	1.01	0.33	0.081
21.668	0.000	0.32	1.01	0.32	0.081
21.904	0.000	0.31	1.01	0.32	0.081
22.140	0.000	0.31	1.01	0.31	0.081
22.376	0.000	0.30	1.01	0.30	0.081
22.613	0.000	0.29	1.01	0.29	0.081
22.849	0.000	0.28	1.01	0.29	0.081
23.085	0.000	0.28	1.01	0.28	0.081
23.321	0.000	0.27	1.01	0.27	0.081
23.557	0.000	0.27	1.01	0.27	0.081
23.793	0.000	0.26	1.01	0.26	0.081
24.030	0.000	0.26	1.01	0.26	0.081
24.266	0.000	0.00	0.97	0.13	0.078

## Hydraulic Calculations

## Line A Inlet 1 Calculation

Purpose - To size spillway

$$H=((Q^2)/(CL^2))^{(1/3)}$$

H = depth of water flowing into inlet

C	3.4
Length (ft)	4

Q (cfs)	H = depth (ft)
0.36	0.09

User Input

## Line A Inlet 2 Calculation

Purpose - To size spillway

$$H=((Q^2)/(CL^2))^{(1/3)}$$

H = depth of water flowing into inlet

C	3.4
Length (ft)	4

Q (cfs)	H = depth (ft)
0.36	0.09

User Input

## Line B Inlet 1 Calculation

Purpose - To size spillway

$$H=((Q^2)/(CL^2))^{(1/3)}$$

H = depth of water flowing into inlet

C	3.4
Length (ft)	4

Q (cfs)	H = depth (ft)
2.77	0.35

User Input

## Line B Inlet 2 Calculation

Purpose - To size spillway

$$H=((Q^2)/(CL^2))^{(1/3)}$$

H = depth of water flowing into inlet

C	3.4
Length (ft)	4

Q (cfs)	H = depth (ft)
0.89	0.16

User Input

## Line C Inlet 1 Calculation

Purpose - To size spillway

$$H=((Q^2)/(CL^2))^{(1/3)}$$

H = depth of water flowing into inlet

C	3.4
Length (ft)	4

Q (cfs)	H = depth (ft)
0.31	0.08

User Input

## Line D Inlet 1 Calculation

Purpose - To size spillway

$$H=((Q^2)/(CL^2))^{(1/3)}$$

H = depth of water flowing into inlet

C	3.4
Length (ft)	4

Q (cfs)	H = depth (ft)
1.92	0.27

User Input

## Line D Inlet 2 Calculation

Purpose - To size spillway

$$H = ((Q^2)/(CL^2))^{(1/3)}$$

H = depth of water flowing into inlet

C	3.4
Length (ft)	4

Q (cfs)	H = depth (ft)
0.26	0.07

User Input

Line A - 12" Storm Drain

\*\*\*\*\*

>>>PIPEFLOW HYDRAULIC INPUT INFORMATION<<<

PIPE DIAMETER(FEET) = 1.000  
PIPE SLOPE(FEET/FEET) = 0.0050  
PIPEFLOW(CFS) = 0.71  
MANNINGS FRICTION FACTOR = 0.013000

=====

CRITICAL-DEPTH FLOW INFORMATION:

=====

CRITICAL DEPTH(FEET) = 0.35  
CRITICAL FLOW AREA(SQUARE FEET) = 0.246  
CRITICAL FLOW TOP-WIDTH(FEET) = 0.955  
CRITICAL FLOW PRESSURE + MOMENTUM(POUNDS) = 6.22  
CRITICAL FLOW VELOCITY(FEET/SEC.) = 2.882  
CRITICAL FLOW VELOCITY HEAD(FEET) = 0.13  
CRITICAL FLOW HYDRAULIC DEPTH(FEET) = 0.26  
CRITICAL FLOW SPECIFIC ENERGY(FEET) = 0.48

=====

NORMAL-DEPTH FLOW INFORMATION:

=====

NORMAL DEPTH(FEET) = 0.36  
FLOW AREA(SQUARE FEET) = 0.26  
FLOW TOP-WIDTH(FEET) = 0.962  
FLOW PRESSURE + MOMENTUM(POUNDS) = 6.22  
FLOW VELOCITY(FEET/SEC.) = 2.756  
FLOW VELOCITY HEAD(FEET) = 0.118  
HYDRAULIC DEPTH(FEET) = 0.27  
FROUDE NUMBER = 0.939  
SPECIFIC ENERGY(FEET) = 0.48

Line B - 15" Storm Drain

\*\*\*\*\*

>>>PIPEFLOW HYDRAULIC INPUT INFORMATION<<<

PIPE DIAMETER(FEET) = 1.250  
PIPE SLOPE(FEET/FEET) = 0.0050  
PIPEFLOW(CFS) = 3.64  
MANNINGS FRICTION FACTOR = 0.013000

=====

CRITICAL-DEPTH FLOW INFORMATION:

=====

CRITICAL DEPTH(FEET) = 0.77  
CRITICAL FLOW AREA(SQUARE FEET) = 0.794  
CRITICAL FLOW TOP-WIDTH(FEET) = 1.216  
CRITICAL FLOW PRESSURE + MOMENTUM(POUNDS) = 48.89  
CRITICAL FLOW VELOCITY(FEET/SEC.) = 4.585  
CRITICAL FLOW VELOCITY HEAD(FEET) = 0.33  
CRITICAL FLOW HYDRAULIC DEPTH(FEET) = 0.65  
CRITICAL FLOW SPECIFIC ENERGY(FEET) = 1.10

=====

NORMAL-DEPTH FLOW INFORMATION:

=====

NORMAL DEPTH(FEET) = 0.84  
FLOW AREA(SQUARE FEET) = 0.88  
FLOW TOP-WIDTH(FEET) = 1.171  
FLOW PRESSURE + MOMENTUM(POUNDS) = 49.51  
FLOW VELOCITY(FEET/SEC.) = 4.132  
FLOW VELOCITY HEAD(FEET) = 0.265  
HYDRAULIC DEPTH(FEET) = 0.75  
FROUDE NUMBER = 0.840  
SPECIFIC ENERGY(FEET) = 1.11

Line C - 6 " Storm Drain

\*\*\*\*\*  
>>>PIPEFLOW HYDRAULIC INPUT INFORMATION<<<

PIPE DIAMETER(FEET) = 0.500  
PIPE SLOPE(FEET/FEET) = 0.0050  
PIPEFLOW(CFS) = 0.31  
MANNINGS FRICTION FACTOR = 0.013000

=====  
CRITICAL-DEPTH FLOW INFORMATION:

CRITICAL DEPTH(FEET) = 0.28  
CRITICAL FLOW AREA(SQUARE FEET) = 0.114  
CRITICAL FLOW TOP-WIDTH(FEET) = 0.496  
CRITICAL FLOW PRESSURE + MOMENTUM(POUNDS) = 4.27  
CRITICAL FLOW VELOCITY(FEET/SEC.) = 2.720  
CRITICAL FLOW VELOCITY HEAD(FEET) = 0.11  
CRITICAL FLOW HYDRAULIC DEPTH(FEET) = 0.23  
CRITICAL FLOW SPECIFIC ENERGY(FEET) = 0.40

=====  
NORMAL-DEPTH FLOW INFORMATION:

NORMAL DEPTH(FEET) = 0.33  
FLOW AREA(SQUARE FEET) = 0.14  
FLOW TOP-WIDTH(FEET) = 0.472  
FLOW PRESSURE + MOMENTUM(POUNDS) = 4.55  
FLOW VELOCITY(FEET/SEC.) = 2.235  
FLOW VELOCITY HEAD(FEET) = 0.078  
HYDRAULIC DEPTH(FEET) = 0.29  
FROUDE NUMBER = 0.727  
SPECIFIC ENERGY(FEET) = 0.41

Line D - 12 " Storm Drain

\*\*\*\*\*  
>>>PIPEFLOW HYDRAULIC INPUT INFORMATION<<<

PIPE DIAMETER(FEET) = 1.000  
PIPE SLOPE(FEET/FEET) = 0.0050  
PIPEFLOW(CFS) = 2.13  
MANNINGS FRICTION FACTOR = 0.013000

=====  
CRITICAL-DEPTH FLOW INFORMATION:

CRITICAL DEPTH(FEET) = 0.62  
CRITICAL FLOW AREA(SQUARE FEET) = 0.515  
CRITICAL FLOW TOP-WIDTH(FEET) = 0.969  
CRITICAL FLOW PRESSURE + MOMENTUM(POUNDS) = 25.77  
CRITICAL FLOW VELOCITY(FEET/SEC.) = 4.137  
CRITICAL FLOW VELOCITY HEAD(FEET) = 0.27  
CRITICAL FLOW HYDRAULIC DEPTH(FEET) = 0.53  
CRITICAL FLOW SPECIFIC ENERGY(FEET) = 0.89

=====  
NORMAL-DEPTH FLOW INFORMATION:

NORMAL DEPTH(FEET) = 0.71  
FLOW AREA(SQUARE FEET) = 0.59  
FLOW TOP-WIDTH(FEET) = 0.912  
FLOW PRESSURE + MOMENTUM(POUNDS) = 26.36  
FLOW VELOCITY(FEET/SEC.) = 3.598  
FLOW VELOCITY HEAD(FEET) = 0.201  
HYDRAULIC DEPTH(FEET) = 0.65  
FROUDE NUMBER = 0.787  
SPECIFIC ENERGY(FEET) = 0.91

Line E - 18 " Storm Drain

\*\*\*\*\*

>>>PIPEFLOW HYDRAULIC INPUT INFORMATION<<<

PIPE DIAMETER(FEET) = 1.500  
PIPE SLOPE(FEET/FEET) = 0.0450  
PIPEFLOW(CFS) = 9.74  
MANNINGS FRICTION FACTOR = 0.013000

=====

CRITICAL-DEPTH FLOW INFORMATION:

=====

CRITICAL DEPTH(FEET) = 1.20  
CRITICAL FLOW AREA(SQUARE FEET) = 1.521  
CRITICAL FLOW TOP-WIDTH(FEET) = 1.194  
CRITICAL FLOW PRESSURE + MOMENTUM(POUNDS) = 172.93  
CRITICAL FLOW VELOCITY(FEET/SEC.) = 6.405  
CRITICAL FLOW VELOCITY HEAD(FEET) = 0.64  
CRITICAL FLOW HYDRAULIC DEPTH(FEET) = 1.27  
CRITICAL FLOW SPECIFIC ENERGY(FEET) = 1.84

=====

NORMAL-DEPTH FLOW INFORMATION:

=====

NORMAL DEPTH(FEET) = 0.69  
FLOW AREA(SQUARE FEET) = 0.80  
FLOW TOP-WIDTH(FEET) = 1.496  
FLOW PRESSURE + MOMENTUM(POUNDS) = 244.61  
FLOW VELOCITY(FEET/SEC.) = 12.186  
FLOW VELOCITY HEAD(FEET) = 2.306  
HYDRAULIC DEPTH(FEET) = 0.53  
FROUDE NUMBER = 2.938  
SPECIFIC ENERGY(FEET) = 3.00

=====

## Infiltration Basin 1 Spillway Calculation

Purpose - To size spillway

$$H = ((Q^2)/(CL^2))^{(1/3)}$$

H = depth of water flowing over spillway

C	3.4
Length (ft)	10

Q (cfs) H = depth (ft)

23.49 0.78

User Input

## Infiltration Basin 2 Spillway Calculation

Purpose - To size spillway

$$H = ((Q^2)/(CL^2))^{(1/3)}$$

H = depth of water flowing over spillway

C	3.4
Length (ft)	10

Q (cfs) H = depth (ft)

4.71 0.27

User Input

## Infiltration Basin 3 Spillway Calculation

Purpose - To size spillway

$$H = ((Q^2)/(CL^2))^{(1/3)}$$

H = depth of water flowing over spillway

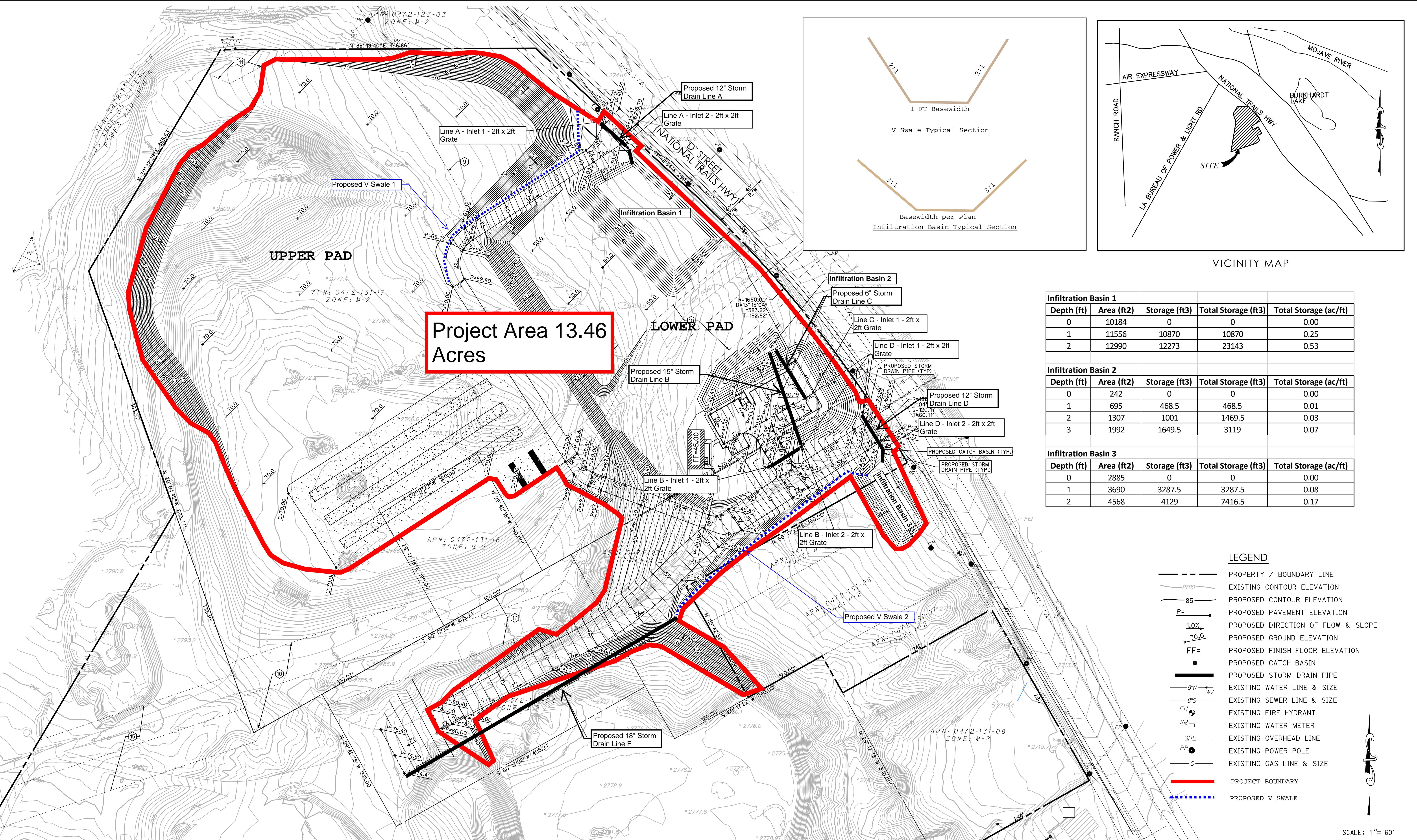
C	3.4
Length (ft)	10

Q (cfs) H = depth (ft)

31.86 0.96

User Input

## Hydrology Exhibits



Infiltration Basin 1				
Depth (ft)	Area (ft <sup>2</sup> )	Storage (ft <sup>3</sup> )	Total Storage (ft <sup>3</sup> )	Total Storage (ac/ft)
0	10184	0	0	0.00
1	11556	10870	10870	0.25
2	12990	12273	23143	0.53

Infiltration Basin 2				
Depth (ft)	Area (ft <sup>2</sup> )	Storage (ft <sup>3</sup> )	Total Storage (ft <sup>3</sup> )	Total Storage (ac/ft)
0	242	0	0	0.00
1	695	468.5	468.5	0.01
2	1307	1001	1469.5	0.03
3	1992	1649.5	3119	0.07

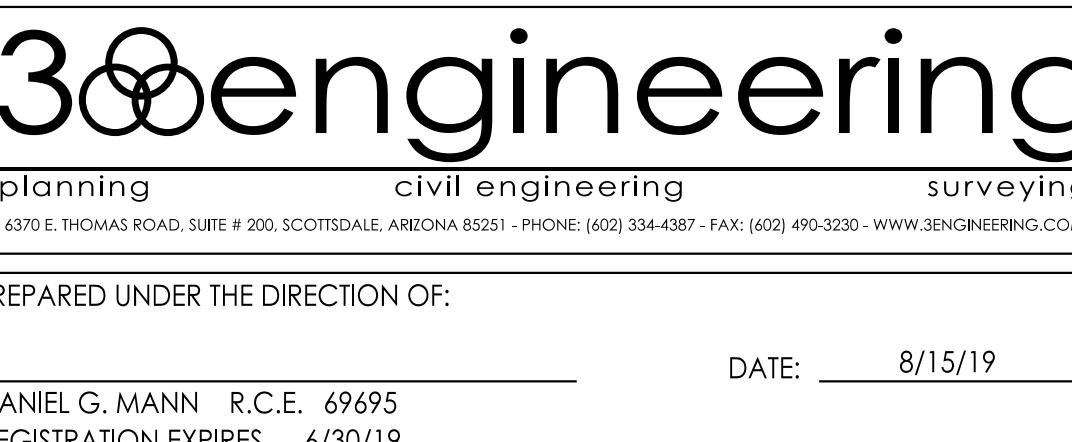
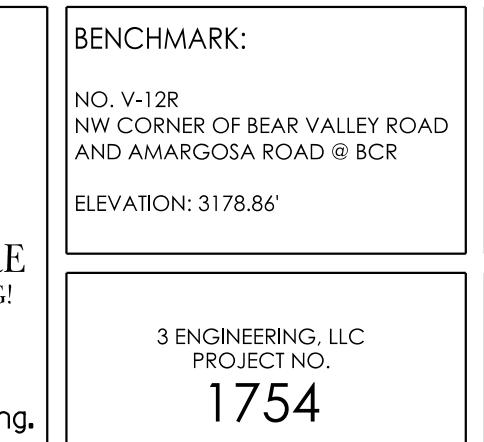
  

Infiltration Basin 3				
Depth (ft)	Area (ft <sup>2</sup> )	Storage (ft <sup>3</sup> )	Total Storage (ft <sup>3</sup> )	Total Storage (ac/ft)
0	2885	0	0	0.00
1	3690	3287.5	3287.5	0.08
2	4568	4129	7416.5	0.17

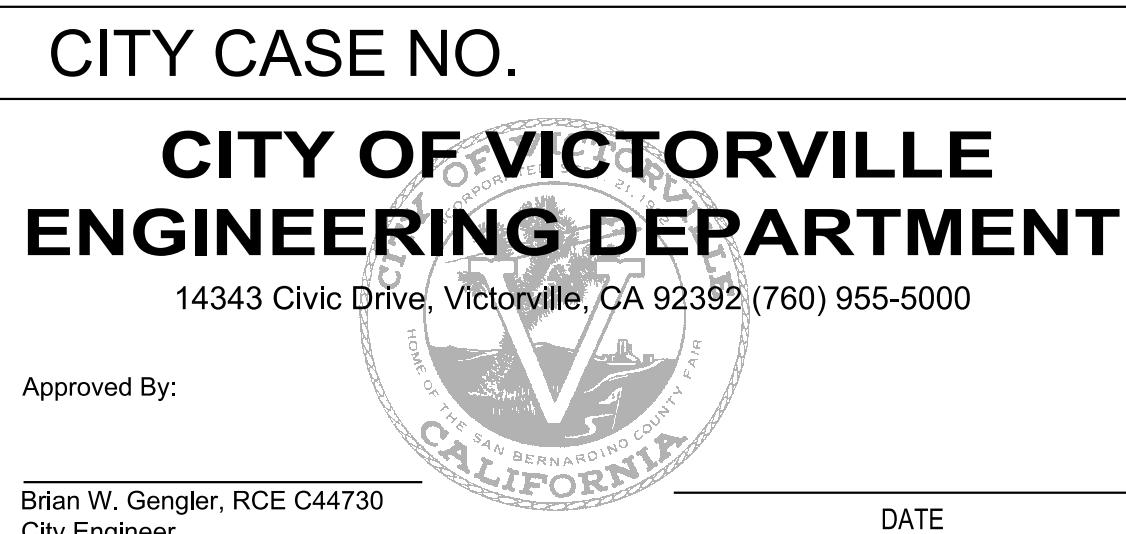
**LEGEND:**

- PROPERTY / BOUNDARY LINE
- EXISTING CONTOUR ELEVATION
- PROPOSED CONTOUR ELEVATION
- PROPOSED PAVEMENT ELEVATION
- PROPOSED DIRECTION OF FLOW & SLOPE
- PROPOSED GROUND ELEVATION
- PROPOSED FINISH FLOOR ELEVATION
- PROPOSED CATCH BASIN
- PROPOSED STORM DRAIN PIPE
- EXISTING WATER LINE & SIZE
- EXISTING SEWER LINE & SIZE
- EXISTING FIRE HYDRANT
- EXISTING WATER METER
- EXISTING OVERHEAD LINE
- EXISTING POWER POLE
- EXISTING GAS LINE & SIZE
- PROJECT BOUNDARY
- PROPOSED V SWALE

SCALE: 1" = 60'  
0' 30' 60' 120'



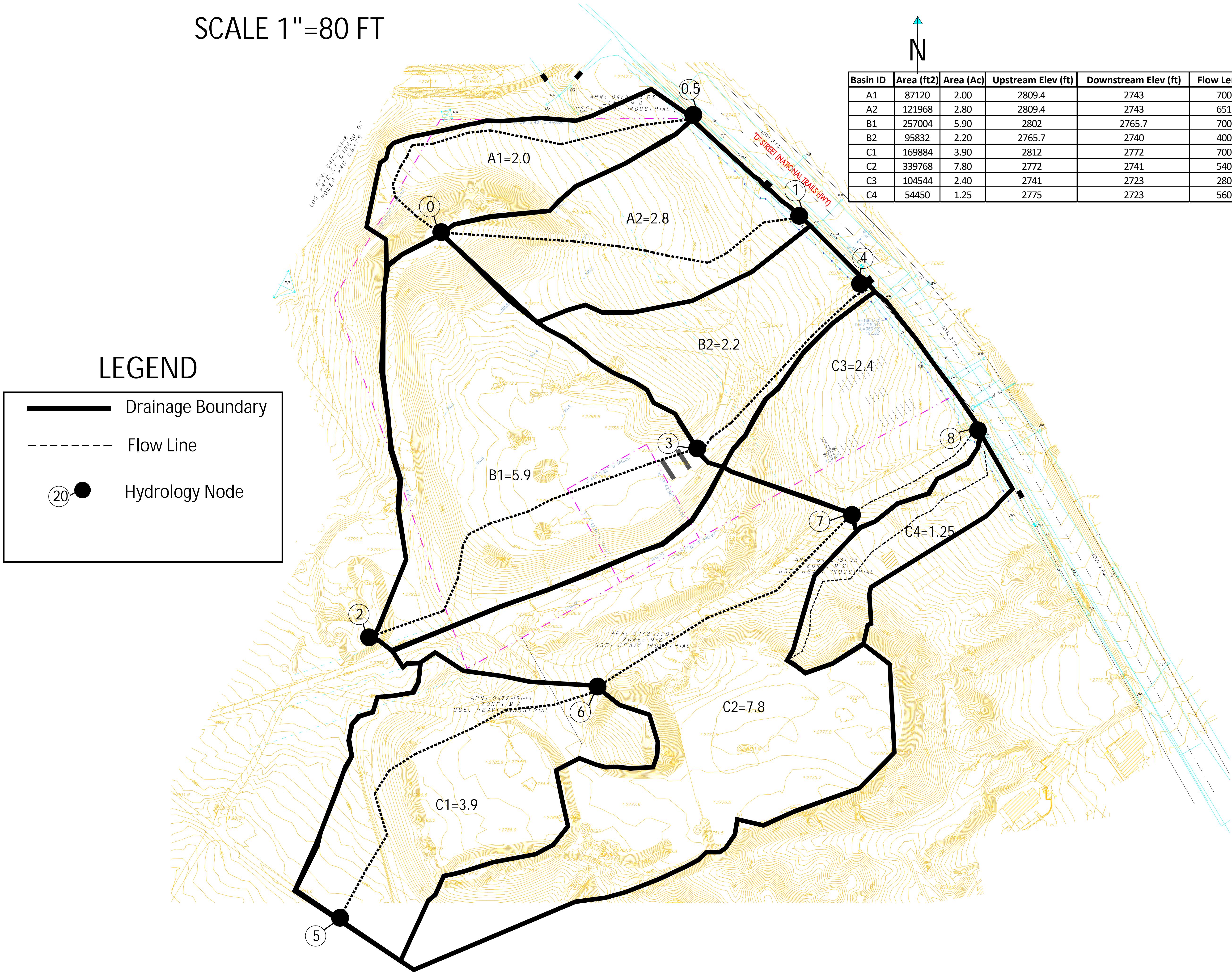
REVISIONS			
No.	Description	Date	Approved



PGRD01  
SHEET NO.  
1 of 1

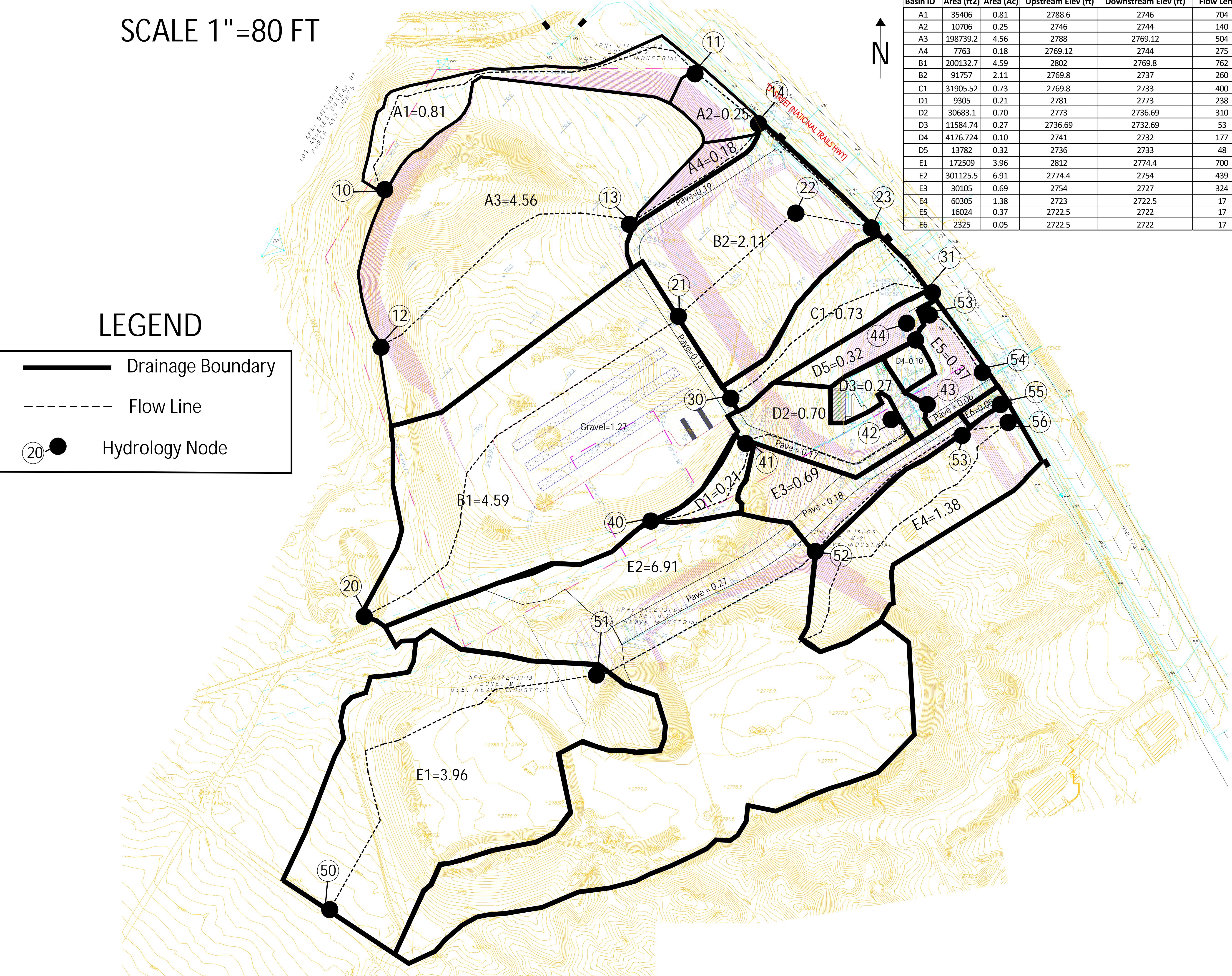
# EXISTING CONDITION HYDROLOGY

**SCALE 1"=80 FT**



# PROPOSED CONDITION HYDROLOGY

SCALE 1"=80 FT



## NOTES TO USERS

This map is for use in administering the National Flood Insurance Program. It does not necessarily identify all areas subject to flooding, particularly from local drainage sources of small size. The **community map repository** should be consulted for possible updated or additional flood hazard information.

To obtain more detailed information in areas where **Base Flood Elevations** (BFEs) and/or **floodways** have been determined, users are encouraged to consult the Flood Profiles and Floodway Data and/or Summary of Stillwater Elevations tables contained within the Flood Insurance Study (FIS) report that accompanies this FIRM. Users should be aware that BFEs shown on the FIRM represent rounded whole-foot elevations. These BFEs are intended for flood insurance rating purposes only and should not be used as the sole source of flood elevation information. Accordingly, flood elevation data presented in the FIS report should be utilized in conjunction with the FIRM for purposes of construction and/or floodplain management.

**Coastal Base Flood Elevations** shown on this map apply only landward of 0° North American Vertical Datum of 1988 (NAVD 88). Users of this FIRM should be aware that coastal base elevations are also shown in the Summary of Stillwater Elevations tables in the Flood Insurance Study report for this jurisdiction. Elevations shown in the Summary of Stillwater Elevations tables should be used for construction and/or floodplain management purposes when they are higher than the elevations shown on this FIRM.

Boundaries of the **floodways** were computed at cross sections and interpolated between cross sections. The floodways were based on hydraulic considerations with regard to requirements of the National Flood Insurance Program. Floodway widths and other pertinent floodway data are provided in the Flood Insurance Study report for this jurisdiction.

Certain areas not in Special Flood Hazard Areas may be protected by **flood control structures**. Refer to Section 2.4 "Flood Protection Measures" of the Flood Insurance Study report for information on flood control structures for this jurisdiction.

The projection used in the preparation of this map was Universal Transverse Mercator (UTM) zone 11 North. The **horizontal datum** was NAD 83, GRS80 spheroid. Differences in datum, spheroid, projection or UTM zones used in the production of FIRMs for adjacent jurisdictions may result in slight positional differences in map features across jurisdiction boundaries. These differences do not affect the accuracy of this FIRM.

Flood elevations on this map are referenced to the North American Vertical Datum of 1988. These flood elevations must be compared to structure and ground elevations referenced to the same **vertical datum**. For information regarding conversion between the National Geodetic Vertical Datum of 1929 and the North American Vertical Datum of 1988, visit the National Geodetic Survey website at <http://www.ngs.noaa.gov> or contact the National Geodetic Survey at the following address:

NGS Information Services  
NOAA, NNGS12  
National Geodetic Survey  
SSMC-3, #9202  
1315 East-West Highway  
Silver Spring, Maryland 20910-3282  
(301) 713-3242

To obtain current elevation, description, and/or location information for **bench marks** shown on this map, please contact the Information Services Branch of the National Geodetic Survey at (301) 713-3242, or visit its website at <http://www.ngs.noaa.gov>.

**Base map** information shown on this FIRM was derived from digital orthophotography collected by the U.S. Department of Agriculture Farm Service Agency. This imagery was flown in 2005 and was produced with a 1-meter ground sample distance.

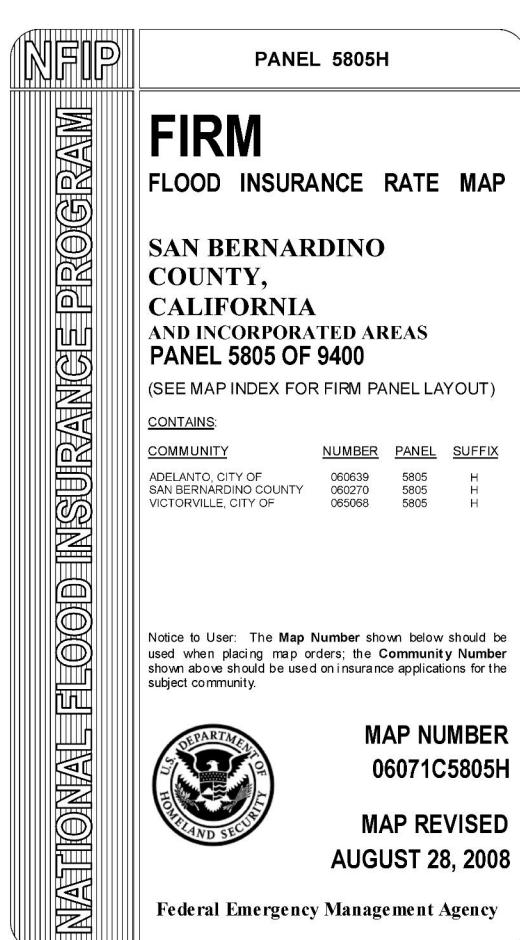
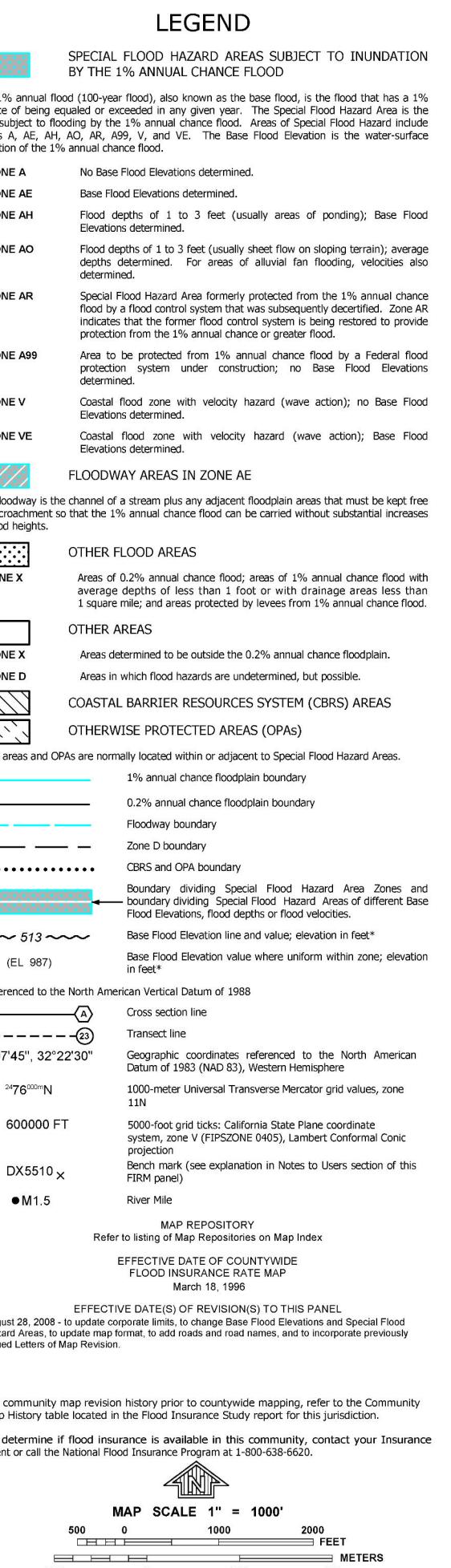
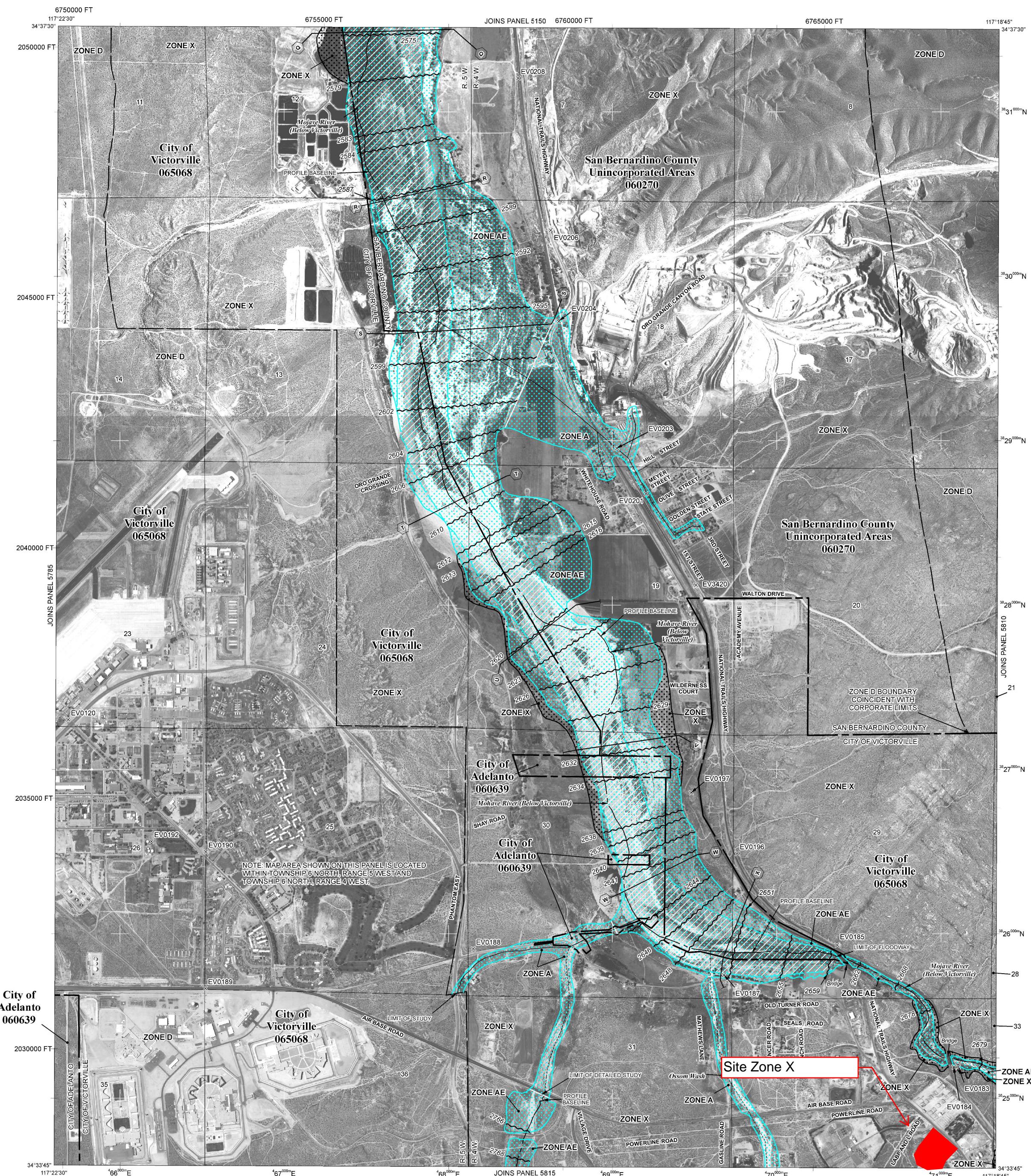
This map may reflect more detailed and up-to-date stream channel configurations than those shown in the previous FIRM for this jurisdiction. The floodplains and floodways that were transferred from the previous FIRM may have been adjusted to conform to these new stream channel configurations. As a result, the Flood Profiles and Floodway Data tables in the Flood Insurance Study Report (which contains authoritative hydraulic data) may reflect stream channel distances that differ from what is shown on this map.

**Corporate limits** shown on this map are based on the best data available at the time of publication. Because changes due to annexations or de-annexations may have occurred after this map was published, map users should contact appropriate community officials to verify current corporate limit locations.

Please refer to the separately printed **Map Index** for an overview map of the county showing the layout of map panels, community map repository addresses, and a listing of communities table containing National Flood Insurance Program dates for each community as well as a listing of the panels on which each community is located.

Contact the **FEMA Map Service Center** at 1-800-338-9918 for information on available products associated with this FIRM. Available products may include previously issued Letters of Map Change, a Flood Insurance Study report, and/or digital versions of this map. The FEMA Map Service Center may also be reached by Fax at 1-800-358-9820 and its website at <http://msc.fema.gov>.

If you have questions about this map or questions concerning the National Flood Insurance Program in general, please call 1-877-FEMA MAP (1-877-336-2627) or visit the FEMA website at <http://www.fema.gov>.



## NOTES TO USERS

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**Coastal Base Flood Elevations** shown on this map apply only landward of 0.0 North American Vertical Datum of 1988 (NAVD 88). Users of this FIRM should be aware that coastal flood elevations are also provided in the Summary of Stillwater Elevations tables in the Flood Insurance Study report for this jurisdiction. Elevations shown in the Summary of Stillwater Elevations tables should be used for construction and/or floodplain management purposes when they are higher than the elevations shown on this FIRM.

Boundaries of the floodways were computed at cross sections and interpolated between cross sections. The floodways were based on hydraulic considerations with regard to requirements of the National Flood Insurance Program. Floodway widths and other pertinent floodway data are provided in the Flood Insurance Study report for this jurisdiction.

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The projection used in the preparation of this map was Universal Transverse Mercator (UTM) zone 11N, North. The horizontal datum was NAD 83, GRS80 ellipsoid. Differences in the UTM, spheroid, projection or UTM zones used in the production of FIRMs for adjacent jurisdictions may result in slight positional differences in map features across jurisdiction boundaries. These differences do not affect the accuracy of this FIRM.

Flood elevations on this map are referenced to the North American Vertical Datum of 1988. These flood elevations must be compared to stream and ground elevations measured in the same vertical datum. For information regarding conversion between the National Geodetic Vertical Datum of 1928 and the North American Vertical Datum of 1988, visit the National Geodetic Survey website at <http://www.ngs.noaa.gov> or contact the National Geodetic Survey at the following address:

NGS Information Services  
NGS Reference Center  
National Geodetic Survey  
SSMC-3 #9202  
1315 East-West Highway  
Silver Spring, Maryland 20910-3282  
(301) 713-3242

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**Base map** information shown on this FIRM was derived from digital orthophotography collected by the U.S. Department of Agriculture Farm Service Agency. This imagery was flown in 2005 and was produced with a 1-meter ground sample distance.

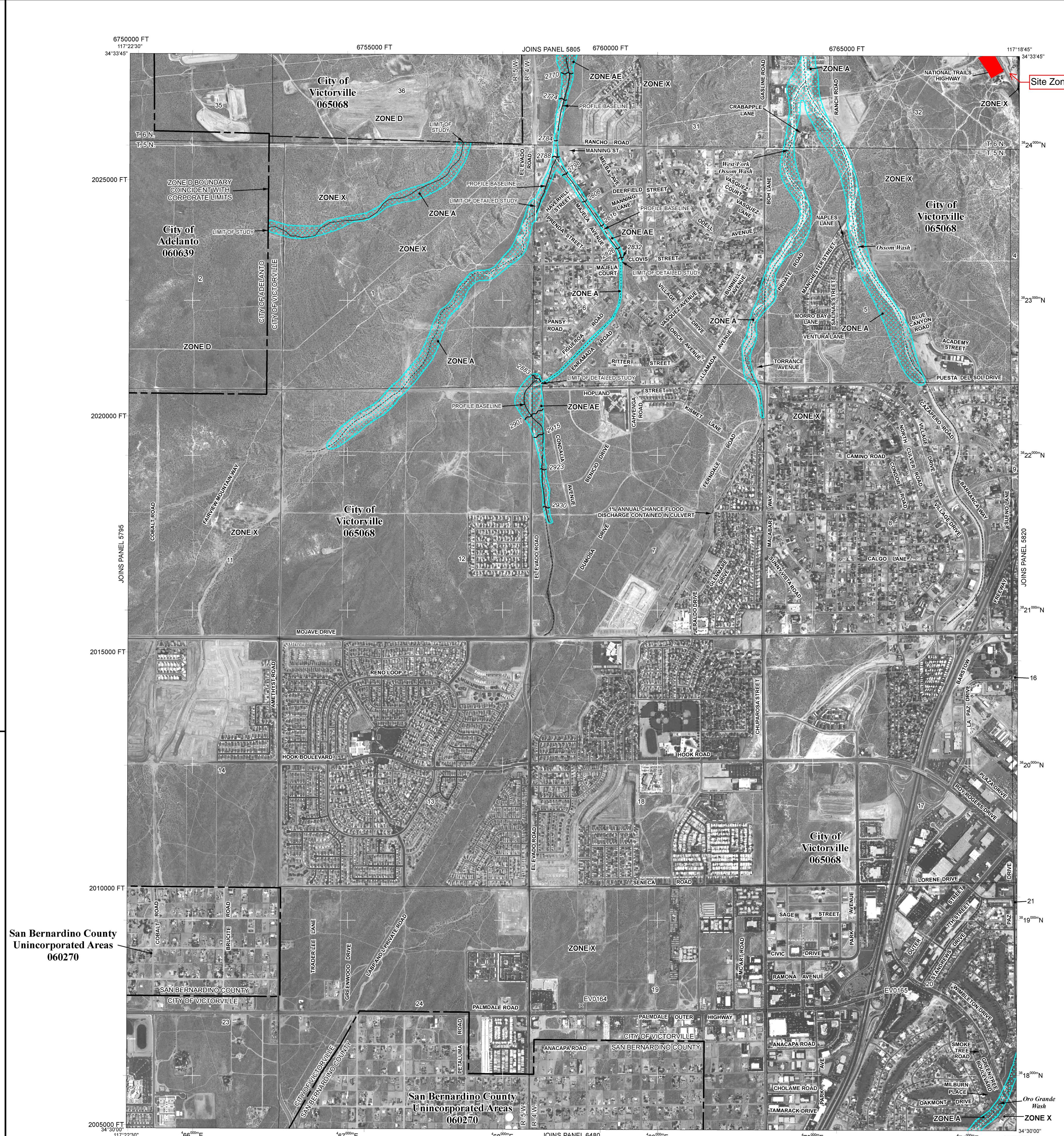
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Contact the **FEMA Map Service Center** at 1-800-358-9616 for information on available products associated with this FIRM. Available products may include previously issued Letters of Map Change, a Flood Insurance Study report, and/or digital versions of this map. The FEMA Map Service Center may also be reached by Fax at 1-800-358-9620 and its website at <http://msc.fema.gov>.

If you have questions about this map or questions concerning the National Flood Insurance Program in general, please call 1-877-FEMA MAP (1-877-336-2627) or visit the FEMA website at <http://www.fema.gov>.



## LEGEND

SPECIAL FLOOD HAZARD AREAS SUBJECT TO INUNDATION BY THE 1% ANNUAL CHANCE FLOOD

The 1% annual flood (100-year flood), also known as the base flood, is the flood that has a 1% chance of being equaled or exceeded in any given year. The Special Flood Hazard Area is the area subject to flooding by the 1% annual chance flood. Areas of Special Flood Hazard include Zones A, AE, AH, AO, AR, A99, V, and VE. The Base Flood Elevation is the water-surface elevation of the 1% annual chance flood.

ZONE A No Base Flood Elevations determined.

ZONE AH Base Flood Elevations determined.

ZONE AO Flood depths of 1 to 3 feet (usually areas of ponding); Base Flood Elevations determined.

ZONE AR Special Flood Hazard Area formerly protected from the 1% annual chance flood by a flood control system that was subsequently decommissioned. Zone AR indicates that the former flood control system is being restored to provide protection from the 1% annual chance or greater flood.

ZONE A99 Area to be protected from 1% annual chance flood by a Federal flood protection system under construction; no Base Flood Elevations determined.

ZONE V Coastal flood zone with velocity hazard (wave action); no Base Flood Elevations determined.

ZONE VE Coastal flood zone with velocity hazard (wave action); Base Flood Elevations determined.

FLOODWAY AREAS IN ZONE AE

The floodway is the channel of a stream plus any adjacent floodplain areas that must be kept free of encroachment so that the 1% annual chance flood can be carried without substantial increases in flood heights.

OTHER FLOOD AREAS

ZONE X Areas of 0.2% annual chance flood; areas of 1% annual chance flood with average depths of less than 1 foot or with drainage areas less than 1 square mile; and areas protected by levees from 1% annual chance flood.

OTHER AREAS

ZONE D Areas determined to be outside the 0.2% annual chance floodplain.

AREAS IN WHICH FLOOD HAZARDS ARE UNDETERMINED, BUT POSSIBLE.

COASTAL BARRIER RESOURCES SYSTEM (CBRS) AREAS

OTHERWISE PROTECTED AREAS (OPAs)

CBRS areas and OPAs are normally located within or adjacent to Special Flood Hazard Areas.

1% annual chance floodplain boundary

0.2% annual chance floodplain boundary

Floodway boundary

Zone D boundary

CBRS and OPA boundary

Boundary dividing Special Flood Hazard Area Zones and

Boundary dividing Special Flood Hazard Areas of different Base

Flood Elevations, flood depths or flood velocities.

Base Flood Elevation line and value; elevation in feet\*

Base Flood Elevation value where uniform within zone; elevation in feet\*

(EL 98)\*

\* Referenced to the North American Vertical Datum of 1988

Cross section line

Transect line

Geographic coordinates referenced to the North American Datum of 1983 (NAD 83), Western Hemisphere

1000-meter Universal Transverse Mercator grid values, zone 11N

5000-foot grid ticks; California State Plane coordinate system, zone V (FIPSZONE 0405), Lambert Conformal Conic projection

Bench mark (see explanation in Notes to Users of this panel)

River Mile

MAP REPOSITORY

Refer to listing of Map Repositories on Map Index

EFFECTIVE DATE OF COUNTYWIDE FLOOD INSURANCE RATE MAP

March 18, 1998

EFFECTIVE DATE(S) OF REVISION(S) TO THIS PANEL

August 28, 2008 - to update corporate limits, to change Base Flood Elevations and Special Flood Hazard Areas, to update map format, to add roads and road names, and to incorporate previously issued Letters of Map Revision

For community map revision history prior to countywide mapping, refer to the Community Map History table located in the Flood Insurance Study report for this jurisdiction.

To determine if flood insurance is available in this community, contact your Insurance agent or call the National Flood Insurance Program at 1-800-638-6520.

MAP SCALE 1" = 1000'

500 0 1000 2000 FEET

300 0 300 600 METERS

NFP

PANEL 5815H

FIRM

FLOOD INSURANCE RATE MAP

SAN BERNARDINO COUNTY,  
CALIFORNIA  
AND INCORPORATED AREAS

PANEL 5815 OF 9400

(SEE MAP INDEX FOR FIRM PANEL LAYOUT)

CONTAINS:

COMMUNITY	NUMBER	PANEL	SUFFIX
ADMS-CITY OF SAN BERNARDINO COUNTY	065068	5815	H
VICTORVILLE, CITY OF	065068	5815	H

Notice to User: The Map Number shown below should be used when placing map orders; the Community Number shown above should be used on insurance applications for the subject community.

MAP NUMBER  
06071C5815H

MAP REVISED  
AUGUST 28, 2008

Federal Emergency Management Agency