APPENDIX H:
TRANSPORTATION ASSESSMENT

# MEMORANDUM 

From: Frederik Venter, P.E. and Anthony Nuti, Kimley-Horn and Associates

## To: Mark Tersini, KT Urban

Date: November 27, 2018

## Re: Westport Cupertino - Transportation Analysis

The purpose of this memorandum is to present traffic analysis findings for the proposed redevelopment of the Oaks Shopping Center, referred to as the "Westport Cupertino" Project. Trip generation, Distribution, and Assignment for the project are presented below as well as a level of service analysis for the intersection of Mary Avenue and Stevens Creek Boulevard.

## 1. Introduction

The existing site is 71,254 square feet of shopping center use (The Oaks), which includes specialty restaurants, retailers, and other commercial space.

The proposed project would demolish the existing buildings and construct a mixed-use urban village with 203 multifamily residential units ( 88 low-rise and 115 mid-rise), 39 senior residential units, and 20,000 square feet of general retail. The proposed site provides a total of 525 parking spaces (293 at-grade spaces and 232 below-grade parking spaces) and 40 spaces for bike parking. Figure 1 shows the project vicinity and the surrounding street network. Figure 2 shows the proposed site plan.

The proposed project land uses are consistent with the City of Cupertino General Plan Buildout.

## 2. Analysis Methodology

The Santa Clara Valley Transportation Authority (VTA) Traffic Impact Analysis Guidelines, dated October 2014, and the City of Cupertino guidelines and criteria were utilized in this analysis to determine project requirements and potential impacts. Intersection delay and level of service (LOS) calculations were performed using Highway Capacity Manual (HCM) 2000 methodology in Synchro Version 9, which is consistent with TRAFFIX software. Synchro was used instead of TRAFFIX because it provides improved signal timing evaluation at the intersection of Mary Avenue and Stevens Creek Boulevard. Vehicle miles traveled (VMT) was calculated using CalEEMod. The City of Cupertino 2040 General Plan Amendment Draft EIR states that at signalized intersections, a LOS D is acceptable for both the AM and PM peak hour.

## 3. Existing Conditions

The existing site is 71,254 square feet of shopping center use (The Oaks), which includes specialty restaurants, retailers, and other commercial space. Existing trips distribute to the east and west on Stevens Creek Boulevard, and onto SR-85. A few trips also distribute into the adjacent neighborhoods.



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Surrounding the site is Mary Avenue to the north and east, Stevens Creek Boulevard to the south, and SR-85 to the west. Along Mary Avenue and Stevens Creek Boulevard there are Class II bike lanes. West of Driveway 4, the westbound Class II bike lane transitions across the outside lane that becomes a right turn only lane onto northbound SR-85.

VTA bus stops are located near the project site, within one-half mile, at the following locations:

- East of the intersection of Mary Avenue and Stevens Creek Boulevard (approximately 550 feet from the project site)
- North Stelling Rd and Stevens Creek Boulevard (approximately 1,500 feet from the project site)
- De Anza College, a major transit station (approximately 1,100 feet from the project site)
- N. Stelling Road (approximately 1,760 feet from the project site)
- South Stelling Road (approximately 1,950 feet from the project site)

The presence of several bus lines within proximity to the site, render the site a transit-rich location. Major land uses near the site are De Anza College to the south, Garden Gate Elementary School to the north, and Cupertino Memorial Park to the east. The site is otherwise surrounded by residential uses.

To the north of the project site along Mary Avenue, an informal Park-and-Ride facility exists for private shuttles. Vehicles park on both sides of the street during the day and shuttles transport passengers to major employment centers all over the Bay Area.

Based on the existing count data, the heaviest movement at the intersection of Mary Avenue and Stevens Creek Boulevard occurs in the eastbound direction in the PM peak hour. The eastbound AM peak hour volume is only $69 \%$ of the PM peak hour volume, and thus, the PM peak hour volume is most critical.

In the westbound direction, the AM and PM peak hour volumes are approximately the same (the AM is $94 \%$ of the PM peak hour volume). The westbound PM peak hour volume is only $59 \%$ of the eastbound PM peak hour volume. The total entering PM peak hour volumes are higher than the AM volumes at the intersection by $25 \%$. Thus, the PM peak hour is critical for analysis.

## 4. Trip Generation

To determine the change in the number of daily, AM peak hour, and PM peak hour trips with construction of the proposed Project, trip generation for both existing (trip credits) and proposed conditions was calculated. The Institute of Transportation Engineers (ITE) Trip Generation Manual, $10^{\text {th }}$ Edition, was used to develop trip generation estimates.

The existing shopping center has been approximately $85 \%$ occupied over the last 2 years. At $85 \%$ occupancy, the existing shopping center generates approximately 2,287 daily trips, 57 AM peak hour trips ( 36 IN / 21 OUT), and 230 PM peak hour trips ( 110 IN / 120 OUT). It should be noted that if full occupancy was assumed for the existing shopping center, the trips credited would have been even higher. This is a conservative estimate since ITE is based on gross lease area, which typically includes unoccupied units between $5 \%$ and $15 \%$.

The proposed project is anticipated to generate approximately 2,174 gross daily trips, 108 gross AM peak hour trips ( $35 \mathrm{IN} / 73$ OUT), and 186 gross PM peak hour trips ( $104 \mathrm{IN} / 82$ OUT).

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## Trip Credits

Internal trip capture was then applied using the National Cooperative Highway Research Program Report 684 (NCHRP 684), dated 2011. This methodology estimates the number of trips that have both the origin and destination within the proposed development. These internal trips are then subtracted from the total gross trips. After applying internal capture to the proposed project, reductions of $9 \%$ daily trips, $2 \%$ AM ( $3 \% \mathrm{IN} / 1 \%$ OUT), and $15 \%$ PM ( $13 \% \mathrm{IN} / 17 \%$ OUT) were applied to gross trips.

VTA defines a major bus stop as a stop where six or more buses per hour stop during the peak period and is also referred to as a high-quality transit area. A major bus stop is located at De Anza College approximately 1900 feet from the project site. The residents of the proposed project are expected to use the crosswalk at Mary Avenue and Stevens Creek Boulevard to access this major stop. According to VTA TIA Guidelines, a 2\% trip reduction can be used for housing within 2000 feet ( 0.38 miles) of a major bus stop. Applying the $2 \%$ trip reduction results in a reduction of -28 daily trips, -2 AM peak hour trips (-1 IN / -1 OUT), and -2 PM peak hour trips ( -1 IN / -1 OUT). This trip reduction was only taken for residential trips.

Table 1 shows the current bus routes located in the study area.
Table 1 - Bus Routes Near Westport ${ }^{1}$

| Route | From | To | Weekdays |  |  | Weekends |  | Distance from Oaks Site (mi) | High Quality Transit Area |  | High Quality Area (Y/N) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Operating Hours ${ }^{2}$ | Headway ${ }^{3}$ (minutes)  |  | Operating Hours ${ }^{2,3}$ | $\begin{gathered} \text { Head-way }{ }^{3} \\ \text { (minutes) } \end{gathered}$ |  | High Quality <br> Line | High Quality Stop |  |
|  |  |  |  | Peak | Mid-day |  |  |  |  |  |  |
| Local Bus |  |  |  |  |  |  |  |  |  |  |  |
| 23 | De Anza College | Alum Rock Transit Center | 530 AM - 1:00 AM | 10 | 10 | 5:30 AM - 1:00 AM | 20 | 0.25 | $Y$ | $Y$ | $Y$ |
| 25 | De Anza College | Alum Rock Transit Center | 5:00 AM - 11:30 PM | 10 | 10 | 7:40 AM - 12:00 AM | 30 | 0.4 | Y | $Y$ | Y |
| 53 | De Anza College | Sunnyvale Transit Center | 6:50 AM - 7:10 PM | 60 | 60 | - | - | 0.4 | N | $Y$ | $Y$ |
| 54 | De Anza College | Lockheed Martin Transit Center | 6:00 AM - 9:30 PM | 30 | 30 | 8:30 AM - 7:30 PM | 60 | 0.4 | N | Y | $Y$ |
| 55 | De Anza College | Great America | 5:30 AM - 11:00 PM | 30 | 30 | 8:20 AM - 8:30 PM | 60 | 0.4 | N | Y | Y |
| 81 | Moffett Field Ames Center | San Jose State University | 6:00 AM -9:00 PM | 30 | 30 | 9:30 AM - 6:20 PM | 60 | 0.25 | N | Y | $Y$ |
| Limited Bus Stop Routes |  |  |  |  |  |  |  |  |  |  |  |
| 323 | Downtown San Jose | De Anza College | 7:00 AM - 10:30 PM | 20 | 20 | 8:00 AM -10:30 PM | 15 | 0.4 | N | $Y$ | $Y$ |
| Notes: |  |  |  |  |  |  |  |  |  |  |  |
| 'Bus data taken from VTA Bus and Rail Map F dated Janurary 2016 |  |  |  |  |  |  |  |  |  |  |  |
| * Operating Hours rounded to the nearest 5 minutes for weekdays and weekends. |  |  |  |  |  |  |  |  |  |  |  |
| ${ }^{2}$ Headways are defined as the time between transit vehicles on the same route. |  |  |  |  |  |  |  |  |  |  |  |
| * Operatin | Bing hours for Sund | days may have differ | rent schedule or flexible scher kup/drop off north of the | schedule comp site | pared to Satur | days. |  |  |  |  |  |

Pass-by trip credits for the shopping center were applied only to the PM peak hour based on average rates from Appendix E of the ITE Trip Generation Handbook, $3^{\text {rd }}$ Edition. A pass-by trip is a trip that already exists on the network that will now visit the project site. Since the project is not producing these trips, pass-by trips are removed from the gross trip generation. This reduction was calculated to be -26 PM Peak hour trips (-12 IN /-14 OUT).

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Therefore, the net new project trips are anticipated to be -275 daily trips, +47 AM peak hour trips (-3 IN / +50 OUT), and -22 PM peak hour trips (+4 IN / -26 OUT) after applying existing shopping center trip credits, as well as internal capture, VTA reductions, and pass-by reductions.

Per VTA TIA Guidelines, as adopted by the City of Cupertino, a complete TIA for Congestion Management Plan (CMP) purposes is required for any project in Santa Clara County that is expected to generate 100 or more net new weekday trips during any peak hour. The proposed Project is anticipated to generate fewer trips than the 100 peak hour trips required by VTA ( 36 AM peak and -109 PM peak), therefore a comprehensive TIA is not required, based on VTA guidelines.

Table 2 below summarizes the trip generation calculations.
Table 2 - Project Trip Generation

| Land Uses |  | Project Size |  | WEEKDAY | AM PEAK HOUR |  |  |  | PM PEAK HOUR |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Land Use Code |  |  | Daily Trips | Total Peak Hour | IN | I | OUT | Total <br> Peak <br> Hour | IN | 1 | OUT |
| Multifamily Housing (Low Rise) | 220 | - | Dwelling Unit(s) | 7.32 | 0.46 | 23\% | 1 | 77\% | 0.56 | 63\% | 1 | 37\% |
| Multifamily Housing (Mid-Rise) | 221 | - | Dwelling Unit(s) | 5.44 | 0.36 | 26\% | 1 | 74\% | 0.44 | 61\% | $t$ | 39\% |
| Senior Adult Housing-Attached | 252 | - | Dwelling Unit(s) | 3.70 | 0.20 | 35\% | 1 | 65\% | 0.26 | 55\% | 1 | 45\% |
| Shopping Center | 820 | - | 1.000 Sq Ft GLA | 37.75 | 0.94 | 62\% | 1 | 38\% | 3.81 | 48\% | 1 | 52\% |
| Existing Conditions |  |  |  |  |  |  |  |  |  |  |  |  |
| Shopping Center (100\% Occupancy) | 820 | 71.254 | 1.000 Sq Ft GLA | 2690 | 67 | 42 | 1 | 25 | 271 | 130 | 1 | 141 |
| Shopping Center ( $85 \%$ Occupancy) ${ }^{1}$ | 820 | 60.586 | 1.000 Sq Ft GLA | 2287 | 57 | 36 | $t$ | 21 | 230 | 110 | 1 | 120 |
| Paso-By Trips for Shopping Center ( $P M=34 \%)^{3,4}$ |  |  |  | (78) | 0 | 0 | 1 | 0 | (78) | (37) | 1 | (41) |
| TOAL EXISTING TRIP CREDIT |  |  |  | 2209 | 57 | 36 | 1 | 21 | 152 | 73 | 1 | 79 |
| Proposed Conditions |  |  |  |  |  |  |  |  |  |  |  |  |
| Multifamily Housing (Low-Rise) | 220 | 88 | Dwelling Unit(s) | 648 | 40 | 9 | I | 31 | 49 | 31 | 1 | 18 |
| Multifamily Housing (Mid-Rise) | 221 | 115 | Dwelling Unit(s) | 626 | 41 | 11 | 1 | 30 | 51 | 31 | 1 | 20 |
| Senior Adult Housing-Attached | 252 | 39 | Dwelling Unit(s) | 148 | 8 | 3 | $t$ | 5 | 10 | 6 | 1 | 4 |
| Shopping Center | 820 | 20.000 | 1.000 Sq Ft GLA | 756 | 19 | 12 | 1 | 7 | 78 | 36 | 1 | 40 |
|  | Gross Trips Generated before Internal Capture |  |  | 2.174 | 108 | 35 | 1 | 73 | 186 | 104 | 1 | 82 |
| Internal Capture Trips |  |  |  |  |  |  |  |  |  |  |  |  |
| Multifamily Housing (Low-Rise) | 220 | 88 | Dwelling Unit(s) | (44) | (1) | 0 | , | (1) | (6) | (4) | 1 | (2) |
| Multifamily Housing (Mid-Rise) | 221 | 115 | Dwelling Unit(s) | (42) | 0 | 0 | 1 | 0 | (7) | (5) | 1 | (2) |
| Senior Adult Housing-Attached | 252 | 39 | Dwelling Unit(s) | (10) | 0 | 0 | 1 | 0 | (1) | (1) | 1 | 0 |
| Shopping Center | 820 | 20.000 | 1.000 Sq Ft GLA | (90) | (1) | (1) | $t$ | 0 | (14) | (4) | 1 |  |
|  | Internal Capture Reduction |  |  | (186) | (2) | (1) | 1 | (1) | (28) | (14) | 1 | (14) |
|  | Trip Reductions due to Internal Capture ${ }^{6}$ |  |  | 9\% | 2\% | 3\% | 1 | 1\% | 15\% | 13\% | 1 | 17\% |
| Additional Project Trip Reductions |  |  |  |  |  |  |  |  |  |  |  |  |
| $\begin{aligned} & \text { VTA Major Buo Stop (Daily, AM, PM }=2 \%)^{2} \\ & \text { oc-By Trips for Shopping Center }(P M=34 \%)^{3,4} \end{aligned}$ |  |  |  | (28) | (2) |  | $t$ |  |  | (1) |  |  |
|  |  |  |  | (26) | 0 | 0 |  | 0 | (26) | (12) | 1 | (14) |
| Project Trips |  |  |  | 1,934 | 104 | 33 | 1 | 71 | 130 | 77 | 1 | 53 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  | Existing Trip Credit |  | (2209) | (57) | (36) | 1 | (21) | (152) | (73) | 1 | (79) |
|  |  | Total Project Trips |  | 1934 | 104 | 33 | 1 | 71 | 130 | 77 | 1 | 53 |
| Net New Project Trips |  |  |  | (275) | 47 | (3) | 1 | 50 | (22) | 4 | 1 | (26) |
| Notes: |  |  |  |  |  |  |  |  |  |  |  |  |
| 1. Assume current retal is $85 \%$ occupied <br> 2. Per VTA Transportation Impact Analysis guidelines, a $2 \%$ vehicle trip reduction for housing trips can be appled for a nearby major bus stop <br> 3. Pass-By trip reduction applied to shopping center PM peak hour trips and based on average rates from Appendix E ITE Trip Generation Handbook 3rd Edition <br> 4. Daily pass-by trips only represent PM peak hour pass-by trips because no dally pass-by trip is resented in the ITE Trip Generation Handbook. <br> 5. Trips reductions due to internal capture was calculated using NCHRP 684 methodology <br> 6. Trip generation land uses based on average rates from ITE Trip Generation 10th Edition |  |  |  |  |  |  |  |  |  |  |  |  |

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## 5. Trip Distribution and Assignment

Due to the nature of the proposed redevelopment of the project site into a mixed-use urban village, trip assignment was split into two groups: retail and residential trips. Separate trip distribution and assignments were calculated for the retail and residential land use types. Distribution assumptions for residential and retail trips are discussed below. The volumes indicated at the driveways represent the actual driveway volume that would be observed and include the gross volumes minus the internal capture and minus the VTA bus stop trip credits. The driveway volumes do not include the existing land use credits or pass-by trip reductions, which are incorporated in the analysis for the Mary Avenue and Stevens Creek Boulevard intersection only.

## Residential Trips

Residential project trips were distributed among project Driveways 1, 2, and 4. Residential trips are not anticipated to use the project Driveway 3, which will be used by retail only. Trips were distributed throughout the roadway network with approximately 8\% (AM and PM Peak) of trips to/from the north on Mary Avenue and approximately 68\% (AM and PM Peak) of trips to/from the west on Stevens Creek Boulevard and approximately 24\% (AM and PM Peak) of trips to/from the east on Stevens Creek Boulevard.

The distribution for residential trips are illustrated in Figure 3. Figure 4 shows the project trip assignment for AM and PM peak hour periods at the project driveways for residential trips. The volumes shown account for internal capture and VTA reductions only.

## Retail Trips

Retail project trips were distributed among project Driveways 2, 3, and 4. Retail trips are not expected to use project Driveway 1, because there is no retail in this section of proposed site. Trips were distributed throughout the roadway network with approximately 35\% (AM and PM Peak) of trips to/from the north on Mary Avenue and approximately 30\% (AM and PM Peak) of trips to/from the west on Stevens Creek Boulevard and approximately 30\% (AM and PM Peak) of trips to/from the east on Stevens Creek Boulevard. Approximately 5\% (AM and PM Peak) of the trips are anticipated to use Parkwood Drive (just north of the site). No trips were distributed at the driveway entrance to the senior center and park since retail visitors are expected to walk to the stores using the crosswalk with a flashing beacon on Mary Avenue.

The trips distributed along Mary Avenue are expected to already be on the roadway and are not new trips for the Project, since the existing site is used for retail purposes.

The distribution estimates for retail trips are illustrated in Figure 5. Figure 6 shows the project trip assignment for AM and PM peak hour periods at the project driveway for retail trips. The volumes shown account for internal capture only.

The trip distribution is based on existing travel patterns at the intersection of Mary Avenue and Stevens Creek Boulevard.

Project driveway volumes for both residential and retail land uses, as well as through volumes on Mary Avenue, are relatively low. Therefore, LOS analyses at the Project driveways are not warranted.


Westport
Figure 4
Proposed Residential Trip Assignment



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## 6. Traffic Analysis at Mary Avenue and Stevens Creek Boulevard

Analysis of intersections is based on the concept of Level of Service (LOS). The LOS of an intersection is a qualitative measurement used to describe operational conditions. LOS ranges from A (best), which represents minimal delay, to F (worst), which represents heavy delay and a facility that is operating at or near its functional capacity. The City of Cupertino 2040 General Plan Amendment Draft EIR states that at signalized intersections, a LOS D is acceptable for both the AM and PM peak hour. The Mary Avenue and Stevens Creek Boulevard intersection is signalized, and therefore, a LOS D or better is required at this intersection.

The intersection of SR-85 Northbound Ramps and Stevens Creek Boulevard was not selected for analysis because only $30 \%$ (approximately 44 vehicles) of the net AM outbound traffic would distribute to the intersection. Two-thirds of this westbound arriving traffic ( 30 vehicles) are expected to travel north onto SR-85 via a free right turn movement. The remaining westbound through traffic on Stevens Creek Boulevard does not warrant analysis, because the VTA CMP threshold of 10 vehicles per lane at the intersection is not met.

Intersection LOS for this study has been determined using methods defined in the HCM 2000 and Synchro traffic analysis software. The analysis has been conducted for the weekday AM and PM peak hours.

### 6.1 Existing Conditions

Existing Conditions traffic operations were evaluated using existing lane geometry, traffic control, and peak hour traffic volumes. Peak hour traffic volumes were collected by National Data \& Surveying Services (NDS) on Wednesday April 25, 2018. Table 3 illustrates the LOS and delay under Existing Conditions. The existing intersection was determined to be an acceptable LOS C in both the AM peak hour period (31.5-second delay) and PM peak hour period (34.9-second delay).

Table 3 - Existing Conditions Level of Service

| Intersection |  | LOS Criteria | Jurisdiction ${ }^{1}$ | Control | Existing (2018) |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | AM Peak |  |  | PM Peak |  |
|  |  | LOS |  |  | Delay (s) | LOS | Delay (s) |
| 1 | Mary Avenue and Stevens Creek Boulevard |  | D | CUP | Signal | C | 31.5 | C | 34.9 |

### 6.2 Existing Plus Project Conditions

Existing Plus Project Conditions traffic operations were evaluated using existing lane geometry, traffic control, and existing peak hour traffic volumes plus net new project volumes. Figure 7 shows the intersection volumes and Table 4 shows the LOS and delay at the intersection of Mary Avenue and Stevens Creek Boulevard under Existing Plus Project Conditions. Under Existing Plus Project conditions, the study intersection would remain at an acceptable LOS C during AM (32.6-second delay) and PM peak hours (34.8-second delay). The increase in the AM is approximately 1.1 seconds.

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Figure 7 - Existing Plus Project Intersection Volumes


Table 4 - Existing Plus Project Conditions Level of Service

|  | Intersection | LOS Criteria | Jurisdiction ${ }^{1}$ | Control | Existing (2018) + Project |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | AM Peak |  | PM Peak |  |
|  |  |  |  |  | LOS | Delay (s) | LOS | Delay (s) |
| 1 | Mary Avenue and Stevens Creek Boulevard | D | CUP | Signal | C | 32.6 | C | 34.8 |

### 6.2 Background Plus Project Conditions

No Background Plus Project Conditions were evaluated for the proposed project at the Mary Avenue and Stevens Creek Boulevard intersection, because, for PM peak hour conditions, the net added project volumes would decrease. Therefore, the proposed project would result in no impact. In addition, the PM peak hour presents the worst-case analysis because of the higher existing volumes.

Under Existing Conditions in the AM peak hour, the increase in delay would be less than 1.1seconds at the intersection of Mary Avenue and Stevens Creek Boulevard. Under Background Plus Project Conditions this increase would be less, because the percentage of project traffic related to background traffic is smaller. This marginal increase in delay does not meet VTA or City of Cupertino standards for generating impacts and the project would have no impact under Background Plus Project Conditions.

### 6.3 Cumulative Conditions

Traffic operations were evaluated for 2040 Cumulative Conditions based on data presented in the Sandis Traffic Impact Analysis Report, dated February 2017, which references the City of Cupertino General Plan EIR, 2014. It is assumed that the Cumulative Conditions intersection geometry of Mary Avenue and Stevens Creek Boulevard would be the same as Existing Conditions. Table 5 shows the LOS and delay for the traffic signal at Stevens Creek Boulevard and Mary Avenue for cumulative conditions. Under Cumulative Conditions, the intersection would

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operate at an acceptable LOS D during the AM peak hour (47.7-second delay) and PM peak hour (46.3-second delay).

Table 5 - Cumulative Conditions Level of Service

| Intersection |  | LOS Criteria | Jurisdiction ${ }^{1}$ | Control | Cumulative (2040) |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | AM Peak |  |  | PM Peak |  |
|  |  | LOS |  |  | Delay (s) | LOS | Delay (s) |
| 1 | Mary Avenue and Stevens Creek Boulevard |  | D | CUP | Signal | D | 47.7 | D | 46.3 |

### 5.4 Cumulative Plus Project Conditions

Cumulative Plus Project Conditions traffic operations were evaluated using cumulative lane geometry, traffic control, and cumulative peak hour traffic volumes plus net new project volumes. It is assumed that the Cumulative Conditions intersection geometry of Mary Avenue and Stevens Creek Boulevard would be the same as Existing Conditions. Figure 8 shows the intersection volumes and Table 6 shows the LOS and delay signalized study intersection at Mary Avenue and Stevens Creek Boulevard. The intersection operates at an acceptable LOS D in both the AM (49.1-second delay) and PM (46.3-second delay) peak hours, as presented in the Cupertino 2040 General Plan Amendment Draft EIR.

Figure 8 - Cumulative Plus Project Intersection Volumes


Table 6 - Cumulative Plus Project Conditions Level of Service

| Intersection |  | LOS Criteria | Jurisdiction ${ }^{1}$ | Control | Cumulative (2040) + Project |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | AM Peak |  |  | PM Peak |  |
|  |  | LOS |  |  | Delay (s) | LOS | Delay (s) |
| 1 | Mary Avenue and Stevens Creek Boulevard |  | D | CUP | Signal | D | 49.1 | D | 46.3 |

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## 7. Parking Requirements

Parking requirements for the site were calculated based on on-site supply only and the Park-andRide on-street parking along Mary Avenue was not included in the parking analysis. The Mary Avenue on-street parking is public and is not anticipated to be impacted by the site uses or activities. Furthermore, the project has no jurisdiction over the public parking and usage along Mary Avenue. Table 7 provides the project parking supply and City requirements.

Table 7 - Vehicle Parking Requirements

| Land Use | Project Size | City <br> Municipal <br> Code $^{1}$ | City <br> Requirement | Project <br> Supply | Surplus <br> (Deficiency) |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Row Home / <br> Town Home | 2-3 bedrooms: 88 | 2-3 bedrooms: 2 | 176 | 210 | 34 |
| Building 1 |  |  |  |  |  |
| Retail | 17,600 SQFT | 1 spaces per <br> 250 SQFT | 71 | 73 | 2 |
| Multifamily <br> Housing | $0-1$ bedrooms: 45 <br> 2-3 bedrooms: 70 | $0-1$ bedrooms: 1 <br> 2-3 bedrooms: 2 | 185 | 193 | 8 |
| Building 2 | 2,400 SQFT | 1 spaces per <br> 250 SQFT | 10 | 10 | 0 |
| Retail | $0-1$ bedrooms: 39 | $0-1$ bedrooms: 1 | 39 | 39 | 0 |
| Senior <br> Housing | Total | $\mathbf{4 8 1}$ | 525 | 44 |  |

${ }^{1}$ City requirements are based on City of Cupertino Municipal Code Chapter 19.124, Section19.56.040A and Table 19.56.040B
Table 8 provides the bicycle parking requirements for the short-term bicycle parking, Table 9 provides the bicycle parking requirements for long-term retail bicycle parking, and Table 10 provides the bicycle parking requirements for long-term residential bicycle parking.

Table 8 - Short-Term Bicycle Parking Requirements

| Land Use | Project Size | Code Requirements ${ }^{1}$ | City <br> Requirement | Project Supply |
| :--- | :---: | :---: | :---: | :---: |
| Building 1 | Retail: 17,600 SQFT <br> Residential: 115 DU | Residential:1/10 units <br> (Class II) | Retail: 14.08 <br> Residential: 11.5 | Retail: 16 <br> Residential: 12 |
|  | Retail: 1.92 <br> Retail: $1 / 1,250$ SF <br> (Class II) | Retail: 2 <br> Residential: 3.9 |  |  |
| Building 2 | Retail: 2,400 SQFT <br> Residential: 39 DU | Rential |  |  |

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Table 9 - Long-Term Bicycle Parking Requirements for Retail Only

| Land Use | Code Requirements ${ }^{1}$ | Vehicle <br> Spaces | Requirement | Project <br> Supply |
| :--- | :---: | :---: | :---: | :---: |
| Building 1 - <br> Retail Only | $5 \%$ of vehicle spaces <br> (Class I) | 73 | 3.6 | 4 |
| Building 2- <br> Retail Only | $5 \%$ of vehicle spaces <br> (Class I) | 10 | 0.5 | 2 |
| Long term requirements based on Green Building Standards Non-Residential |  |  |  |  |
| Mandatory Measure 5.106.4 |  |  |  |  |

## Table 10 - Long-Term Bicycle Parking Requirements for <br> Multifamily Housing and Senior Apartments

| Land Use | Code Requirements ${ }^{1}$ | Requirement | Project <br> Supply |
| :--- | :---: | :---: | :---: |
| Building 1-115 DU | 1 space per <br> 2 residential units | 58 | 58 |
|  | Building 2-39 DU | 20 | 20 |

For the parking layouts, refer to Sheet Set A200, A201, and G202 of the C2K Westport plan set for the most up-to-date site plans with parking requirements. Based on the City of Cupertino Municipal code, the proposed project parking is sufficient.

## 8. Pedestrian Mobility

Continuous sidewalks exist along both Mary Avenue and Stevens Creek Boulevard and the project does not propose to change these sidewalks. The project would connect to the public sidewalks and provide ADA-compliant sidewalk facilities, walkways and paths throughout the site per 2010 ADA Standards for Accessible Design. The Mary Avenue and Stevens Creek Boulevard intersection provides marked crosswalks for pedestrians and bikes on the intersection's north, east, and south legs. Additionally, a marked crosswalk with a flashing beacon on Mary Avenue provides access to the project site from the Cupertino Memorial Park and Cupertino Senior Center.

De Anza College can be accessed via sidewalks on Mary Avenue and crosswalks at Mary Avenue and Stevens Creek Boulevard. Garden Gate Elementary school can be accessed via residential sidewalks along Mary Avenue and the residential streets.

As such, employees, patrons, and residents choosing to walk to and from the site would not be adversely impacted based on pedestrian mobility and accessibility.

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## 9. Bicycle Mobility

Existing Class II bicycle lanes along Stevens Creek Boulevard and Mary Avenue provide bicycle access to the proposed project site with a long transition to the through lanes across the SR-85 bridge crossing. In the future, the City of Cupertino plans to convert the existing Class II bike lanes to Class IV bikeways on Stevens Creek Boulevard.

To the north, a Class I multi-use bridge over I-280 exists. This path can be accessed from the Mary Avenue Class II bike lanes.

Students have the option to bike to Garden Gate Elementary school by using the Class II bike lane on Mary Avenue and sidewalks along various residential streets.

As such, employees, patrons, and residents choosing to bike to the site would not be adversely impacted based on bicyclist mobility and accessibility.

## 10. Vehicle Miles Traveled (VMT)

Based on the State's future requirement to conduct vehicle miles traveled (VMT) analysis for projects, a VMT analysis was performed. The VMT was determined by using CalEEMod and was calculated for Existing and Existing Plus Project Conditions. The existing 71,250 SF of commercial space, with $85 \%$ occupancy, would produce an approximate annual VMT of $2,782,747$ miles, while the proposed project would reduce the annual VMT to $2,662,683$ miles.

## 11. Conclusions

The proposed Project was evaluated to determine if significant impacts would occur at adjacent intersections or Westport Cupertino Project site driveways. The evaluation determined that the proposed Project would generate -275 daily, +47 AM peak hour ( $-3 \mathrm{IN} / 50$ OUT), and -22 PM peak hour ( $4 \mathrm{IN} /-26$ OUT) net new trips. This trip generation is below the VTA standard of 100 or more net new weekday trips; therefore, a full TIA is not required. This trip generation is also low compared to baseline volumes at adjacent study intersections and roadways, and LOS at Mary Avenue and Stevens Creek Boulevard would not degrade below acceptable levels with the addition of the Project traffic. The PM peak hour volumes are higher than the AM peak hour and present a worst-case scenario. The proposed project would result in a net reduction in PM peak hour trips and daily VMT. During the AM peak hour, the proposed project would add very few trips and would not cause impacts at the intersection of Mary Avenue and Stevens Creek Boulevard. Very few trips would be added to the SR-85 and Stevens Creek Boulevard intersections and would not cause significant impacts.

Based on the analyses conducted in this study, no potentially significant impacts are anticipated to occur due to the proposed Project. There are also no potentially significant impacts triggered by the land plan that have not already been evaluated under the City's General Plan 2040 for redevelopment of the project site.

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ${ }^{7}$ | 性中 |  | ${ }^{7}$ | 虾 |  | 17 | $\uparrow$ |  | ＊ | 4 | 「 |
| Traffic Volume（vph） | 152 | 1019 | 227 | 195 | 822 | 106 | 102 | 7 | 28 | 99 | 24 | 239 |
| Future Volume（vph） | 152 | 1019 | 227 | 195 | 822 | 106 | 102 | 7 | 28 | 99 | 24 | 239 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time（s） | 6.5 | 7.0 |  | 6.5 | 6.5 |  | 6.5 | 6.5 |  | 6.5 | 6.5 | 6.5 |
| Lane Util．Factor | 1.00 | 0.91 |  | 1.00 | 0.91 |  | 0.97 | 1.00 |  | 1.00 | 1.00 | 1.00 |
| Frpb，ped／bikes | 1.00 | 0.98 |  | 1.00 | 0.99 |  | 1.00 | 0.95 |  | 1.00 | 1.00 | 0.85 |
| Flpb，ped／bikes | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 |
| Frt | 1.00 | 0.97 |  | 1.00 | 0.98 |  | 1.00 | 0.88 |  | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 |  | 0.95 | 1.00 |  | 0.95 | 1.00 |  | 0.95 | 1.00 | 1.00 |
| Satd．Flow（prot） | 1770 | 4867 |  | 1770 | 4953 |  | 3433 | 1549 |  | 1770 | 1863 | 1347 |
| Flt Permitted | 0.95 | 1.00 |  | 0.95 | 1.00 |  | 0.95 | 1.00 |  | 0.95 | 1.00 | 1.00 |
| Satd．Flow（perm） | 1770 | 4867 |  | 1770 | 4953 |  | 3433 | 1549 |  | 1770 | 1863 | 1347 |
| Peak－hour factor，PHF | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.54 | 0.54 | 0.54 | 0.85 | 0.85 | 0.85 |
| Adj．Flow（vph） | 177 | 1185 | 264 | 227 | 956 | 123 | 189 | 13 | 52 | 116 | 28 | 281 |
| RTOR Reduction（vph） | 0 | 28 | 0 | 0 | 12 | 0 | 0 | 49 | 0 | 0 | 0 | 256 |
| Lane Group Flow（vph） | 177 | 1421 | 0 | 227 | 1067 | 0 | 189 | 16 | 0 | 116 | 28 | 25 |
| Confl．Peds．（\＃／hr） |  |  | 26 |  |  | 23 |  |  | 36 |  |  | 87 |
| Turn Type | Prot | NA |  | Prot | NA |  | Prot | NA |  | Prot | NA | Perm |
| Protected Phases | 5 | 2 |  | 1 | 6 |  | 3 | 8 |  | 7 | 4 |  |
| Permitted Phases |  |  |  |  |  |  |  |  |  |  |  | 4 |
| Actuated Green，G（s） | 15.1 | 38.6 |  | 18.1 | 42.1 |  | 10.7 | 8.0 |  | 13.3 | 10.6 | 10.6 |
| Effective Green，g（s） | 13.1 | 36.6 |  | 16.1 | 40.1 |  | 8.7 | 6.0 |  | 11.3 | 8.6 | 8.6 |
| Actuated g／C Ratio | 0.14 | 0.38 |  | 0.17 | 0.42 |  | 0.09 | 0.06 |  | 0.12 | 0.09 | 0.09 |
| Clearance Time（s） | 4.5 | 5.0 |  | 4.5 | 4.5 |  | 4.5 | 4.5 |  | 4.5 | 4.5 | 4.5 |
| Vehicle Extension（s） | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap（vph） | 240 | 1845 |  | 295 | 2058 |  | 309 | 96 |  | 207 | 166 | 120 |
| v／s Ratio Prot | 0.10 | c0．29 |  | c0．13 | c0．22 |  | 0.06 | 0.01 |  | c0．07 | 0.02 |  |
| v／s Ratio Perm |  |  |  |  |  |  |  |  |  |  |  | c0．02 |
| v／c Ratio | 0.74 | 0.77 |  | 0.77 | 0.52 |  | 0.61 | 0.17 |  | 0.56 | 0.17 | 0.21 |
| Uniform Delay，d1 | 40.0 | 26.3 |  | 38.4 | 21.0 |  | 42.3 | 42.9 |  | 40.3 | 40.6 | 40.8 |
| Progression Factor | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 |
| Incremental Delay，d2 | 11.2 | 2.0 |  | 11.4 | 0.2 |  | 3.6 | 0.8 |  | 3.4 | 0.5 | 0.9 |
| Delay（s） | 51.3 | 28.3 |  | 49.9 | 21.2 |  | 45.8 | 43.7 |  | 43.7 | 41.1 | 41.7 |
| Level of Service | D | C |  | D | C |  | D | D |  | D | D | D |
| Approach Delay（s） |  | 30.8 |  |  | 26.2 |  |  | 45.3 |  |  | 42.2 |  |

Approach LOS C C D D

| Intersection Summary |  |  |  |
| :--- | ---: | :--- | ---: |
| HCM 2000 Control Delay | 31.5 | HCM 2000 Level of Service | C |
| HCM 2000 Volume to Capacity ratio | 0.70 |  | 26.5 |
| Actuated Cycle Length（s） | 96.5 | Sum of lost time（s） | C |
| Intersection Capacity Utilization | $67.5 \%$ | ICU Level of Service |  |
| Analysis Period（min） | 15 |  |  |
| C Critical Lane Group |  |  |  |


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \% | 虾 |  | \% | 恌 ${ }^{\text {a }}$ |  | \% ${ }^{18}$ | 1 |  | ${ }^{7}$ | $\uparrow$ | F |
| Traffic Volume (vph) | 225 | 1680 | 113 | 138 | 892 | 165 | 126 | 20 | 75 | 123 | 78 | 138 |
| Future Volume (vph) | 225 | 1680 | 113 | 138 | 892 | 165 | 126 | 20 | 75 | 123 | 78 | 138 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 6.5 | 7.0 |  | 6.5 | 7.0 |  | 6.5 | 6.0 |  | 6.5 | 6.0 | 6.0 |
| Lane Util. Factor | 1.00 | 0.91 |  | 1.00 | 0.91 |  | 0.97 | 1.00 |  | 1.00 | 1.00 | 1.00 |
| Frpb, ped/bikes | 1.00 | 1.00 |  | 1.00 | 0.97 |  | 1.00 | 0.79 |  | 1.00 | 1.00 | 0.83 |
| Flpb, ped/bikes | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 |
| Frt | 1.00 | 0.99 |  | 1.00 | 0.98 |  | 1.00 | 0.88 |  | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 |  | 0.95 | 1.00 |  | 0.95 | 1.00 |  | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1770 | 5037 |  | 1770 | 4836 |  | 3433 | 1297 |  | 1770 | 1863 | 1313 |
| Flt Permitted | 0.95 | 1.00 |  | 0.95 | 1.00 |  | 0.95 | 1.00 |  | 0.95 | 1.00 | 1.00 |
| Satd. Flow (perm) | 1770 | 5037 |  | 1770 | 4836 |  | 3433 | 1297 |  | 1770 | 1863 | 1313 |
| Peak-hour factor, PHF | 0.80 | 0.90 | 0.90 | 0.93 | 0.93 | 0.93 | 0.88 | 0.88 | 0.88 | 0.80 | 0.84 | 0.84 |
| Adj. Flow (vph) | 281 | 1867 | 126 | 148 | 959 | 177 | 143 | 23 | 85 | 154 | 93 | 164 |
| RTOR Reduction (vph) | 0 | 5 | 0 | 0 | 16 | 0 | 0 | 80 | 0 | 0 | 0 | 147 |
| Lane Group Flow (vph) | 281 | 1988 | 0 | 148 | 1120 | 0 | 143 | 28 | 0 | 154 | 93 | 17 |
| Confl. Peds. (\#hr) |  |  |  |  |  | 86 |  |  | 140 |  |  | 87 |
| Turn Type | Prot | NA |  | Prot | NA |  | Prot | NA |  | Prot | NA | Perm |
| Protected Phases | 5 | 2 |  | 1 | 6 |  | 3 | 8 |  | 7 | 4 |  |
| Permitted Phases |  |  |  |  |  |  |  |  |  |  |  | 4 |
| Actuated Green, G (s) | 22.7 | 55.0 |  | 14.8 | 47.1 |  | 10.1 | 8.7 |  | 15.1 | 13.7 | 13.7 |
| Effective Green, g (s) | 20.7 | 53.0 |  | 12.8 | 45.1 |  | 8.1 | 6.7 |  | 13.1 | 11.7 | 11.7 |
| Actuated g/C Ratio | 0.19 | 0.47 |  | 0.11 | 0.40 |  | 0.07 | 0.06 |  | 0.12 | 0.10 | 0.10 |
| Clearance Time (s) | 4.5 | 5.0 |  | 4.5 | 5.0 |  | 4.5 | 4.0 |  | 4.5 | 4.0 | 4.0 |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 328 | 2392 |  | 203 | 1954 |  | 249 | 77 |  | 207 | 195 | 137 |
| v/s Ratio Prot | c0.16 | c0.39 |  | 0.08 | 0.23 |  | 0.04 | 0.02 |  | c0.09 | c0.05 |  |
| v/s Ratio Perm |  |  |  |  |  |  |  |  |  |  |  | 0.01 |
| v/c Ratio | 0.86 | 0.83 |  | 0.73 | 0.57 |  | 0.57 | 0.36 |  | 0.74 | 0.48 | 0.13 |
| Uniform Delay, d1 | 44.0 | 25.4 |  | 47.7 | 25.8 |  | 50.1 | 50.4 |  | 47.6 | 47.1 | 45.3 |
| Progression Factor | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 19.2 | 2.6 |  | 12.3 | 0.4 |  | 3.2 | 2.9 |  | 13.5 | 1.8 | 0.4 |
| Delay (s) | 63.2 | 28.0 |  | 60.0 | 26.2 |  | 53.3 | 53.3 |  | 61.1 | 48.9 | 45.7 |
| Level of Service | E | C |  | E | C |  | D | D |  | E | D | D |
| Approach Delay (s) |  | 32.4 |  |  | 30.1 |  |  | 53.3 |  |  | 52.2 |  |
| Approach LOS |  | C |  |  | C |  |  | D |  |  | D |  |


| Intersection Summary |  |  |  |
| :--- | ---: | :--- | ---: |
| HCM 2000 Control Delay | 34.9 | HCM 2000 Level of Service | C |
| HCM 2000 Volume to Capacity ratio | 0.85 |  | 26.0 |
| Actuated Cycle Length (s) | 111.6 | Sum of lost time (s) | D |
| Intersection Capacity Utilization | $73.8 \%$ | ICU Level of Service |  |
| Analysis Period (min) | 15 |  |  |
| c Critical Lane Group |  |  |  |


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ${ }^{7}$ | 性中 |  | ${ }^{1}$ | 虾 |  | 7 | $\uparrow$ |  | ${ }^{*}$ | 4 | F |
| Traffic Volume（vph） | 159 | 1019 | 227 | 195 | 821 | 105 | 102 | 7 | 28 | 111 | 24 | 271 |
| Future Volume（vph） | 159 | 1019 | 227 | 195 | 821 | 105 | 102 | 7 | 28 | 111 | 24 | 271 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time（s） | 6.5 | 7.0 |  | 6.5 | 6.5 |  | 6.5 | 6.5 |  | 6.5 | 6.5 | 6.5 |
| Lane Util．Factor | 1.00 | 0.91 |  | 1.00 | 0.91 |  | 0.97 | 1.00 |  | 1.00 | 1.00 | 1.00 |
| Frpb，ped／bikes | 1.00 | 0.98 |  | 1.00 | 0.99 |  | 1.00 | 0.94 |  | 1.00 | 1.00 | 0.85 |
| Flpb，ped／bikes | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 |
| Frt | 1.00 | 0.97 |  | 1.00 | 0.98 |  | 1.00 | 0.88 |  | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 |  | 0.95 | 1.00 |  | 0.95 | 1.00 |  | 0.95 | 1.00 | 1.00 |
| Satd．Flow（prot） | 1770 | 4866 |  | 1770 | 4953 |  | 3433 | 1548 |  | 1770 | 1863 | 1345 |
| Flt Permitted | 0.95 | 1.00 |  | 0.95 | 1.00 |  | 0.95 | 1.00 |  | 0.95 | 1.00 | 1.00 |
| Satd．Flow（perm） | 1770 | 4866 |  | 1770 | 4953 |  | 3433 | 1548 |  | 1770 | 1863 | 1345 |
| Peak－hour factor，PHF | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.54 | 0.54 | 0.54 | 0.85 | 0.85 | 0.85 |
| Adj．Flow（vph） | 185 | 1185 | 264 | 227 | 955 | 122 | 189 | 13 | 52 | 131 | 28 | 319 |
| RTOR Reduction（vph） | 0 | 28 | 0 | 0 | 12 | 0 | 0 | 48 | 0 | 0 | 0 | 279 |
| Lane Group Flow（vph） | 185 | 1421 | 0 | 227 | 1065 | 0 | 189 | 17 | 0 | 131 | 28 | 40 |
| Confl．Peds．（\＃／hr） |  |  | 26 |  |  | 23 |  |  | 36 |  |  | 87 |
| Turn Type | Prot | NA |  | Prot | NA |  | Prot | NA |  | Prot | NA | Perm |
| Protected Phases | 5 | 2 |  | 1 | 6 |  | 3 | 8 |  | 7 | 4 |  |
| Permitted Phases |  |  |  |  |  |  |  |  |  |  |  | 4 |
| Actuated Green，G（s） | 15.6 | 38.9 |  | 18.1 | 41.9 |  | 10.7 | 8.8 |  | 13.4 | 11.5 | 11.5 |
| Effective Green，g（s） | 13.6 | 36.9 |  | 16.1 | 39.9 |  | 8.7 | 6.8 |  | 11.4 | 9.5 | 9.5 |
| Actuated g／C Ratio | 0.14 | 0.38 |  | 0.16 | 0.41 |  | 0.09 | 0.07 |  | 0.12 | 0.10 | 0.10 |
| Clearance Time（s） | 4.5 | 5.0 |  | 4.5 | 4.5 |  | 4.5 | 4.5 |  | 4.5 | 4.5 | 4.5 |
| Vehicle Extension（s） | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap（vph） | 246 | 1837 |  | 291 | 2022 |  | 305 | 107 |  | 206 | 181 | 130 |
| v／s Ratio Prot | 0.10 | c0．29 |  | c0．13 | 0.22 |  | 0.06 | 0.01 |  | c0．07 | 0.02 |  |
| v／s Ratio Perm |  |  |  |  |  |  |  |  |  |  |  | c0．03 |
| v／c Ratio | 0.75 | 0.77 |  | 0.78 | 0.53 |  | 0.62 | 0.16 |  | 0.64 | 0.15 | 0.31 |
| Uniform Delay，d1 | 40.4 | 26.7 |  | 39.1 | 21.8 |  | 42.9 | 42.7 |  | 41.2 | 40.4 | 41.0 |
| Progression Factor | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 |
| Incremental Delay，d2 | 12.2 | 2.1 |  | 12.7 | 0.2 |  | 3.7 | 0.7 |  | 6.3 | 0.4 | 1.4 |
| Delay（s） | 52.6 | 28.8 |  | 51.8 | 22.0 |  | 46.6 | 43.4 |  | 47.5 | 40.8 | 42.4 |
| Level of Service | D | C |  | D | C |  | D | D |  | D | D | D |
| Approach Delay（s） |  | 31.5 |  |  | 27.2 |  |  | 45.8 |  |  | 43.7 |  |

Approach LOS C C D D

| Intersection Summary |  |  |  |
| :--- | ---: | :--- | ---: |
| HCM 2000 Control Delay | 32.6 | HCM 2000 Level of Service | C |
| HCM 2000 Volume to Capacity ratio | 0.72 |  | 26.5 |
| Actuated Cycle Length（s） | 97.7 | Sum of lost time（s） | C |
| Intersection Capacity Utilization | $67.5 \%$ | ICU Level of Service |  |
| Analysis Period（min） | 15 |  |  |
| C Critical Lane Group |  |  |  |



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ${ }^{7}$ | 性\％ |  | ${ }^{*}$ | 性中 |  | ${ }^{7} 1$ | F |  | ${ }^{*}$ | 4 | 7 |
| Traffic Volume（vph） | 156 | 1593 | 215 | 243 | 918 | 157 | 130 | 10 | 31 | 134 | 48 | 169 |
| Future Volume（vph） | 156 | 1593 | 215 | 243 | 918 | 157 | 130 | 10 | 31 | 134 | 48 | 169 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time（s） | 6.5 | 7.0 |  | 6.5 | 6.5 |  | 6.5 | 6.5 |  | 6.5 | 6.5 | 6.5 |
| Lane Util．Factor | 1.00 | 0.91 |  | 1.00 | 0.91 |  | 0.97 | 1.00 |  | 1.00 | 1.00 | 1.00 |
| Frpb，ped／bikes | 1.00 | 0.99 |  | 1.00 | 0.99 |  | 1.00 | 0.94 |  | 1.00 | 1.00 | 0.83 |
| Flpb，ped／bikes | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 |
| Frt | 1.00 | 0.98 |  | 1.00 | 0.98 |  | 1.00 | 0.89 |  | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 |  | 0.95 | 1.00 |  | 0.95 | 1.00 |  | 0.95 | 1.00 | 1.00 |
| Satd．Flow（prot） | 1770 | 4937 |  | 1770 | 4910 |  | 3433 | 1559 |  | 1770 | 1863 | 1320 |
| Flt Permitted | 0.95 | 1.00 |  | 0.95 | 1.00 |  | 0.95 | 1.00 |  | 0.95 | 1.00 | 1.00 |
| Satd．Flow（perm） | 1770 | 4937 |  | 1770 | 4910 |  | 3433 | 1559 |  | 1770 | 1863 | 1320 |
| Peak－hour factor，PHF | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.54 | 0.54 | 0.54 | 0.85 | 0.85 | 0.85 |
| Adj．Flow（vph） | 181 | 1852 | 250 | 283 | 1067 | 183 | 241 | 19 | 57 | 158 | 56 | 199 |
| RTOR Reduction（vph） | 0 | 13 | 0 | 0 | 16 | 0 | 0 | 53 | 0 | 0 | 0 | 184 |
| Lane Group Flow（vph） | 181 | 2089 | 0 | 283 | 1234 | 0 | 241 | 23 | 0 | 158 | 56 | 15 |
| Confl．Peds．（\＃／hr） |  |  | 26 |  |  | 23 |  |  | 36 |  |  | 87 |
| Turn Type | Prot | NA |  | Prot | NA |  | Prot | NA |  | Prot | NA | Perm |
| Protected Phases | 5 | 2 |  | 1 | 6 |  | 3 | 8 |  | 7 | 4 |  |
| Permitted Phases |  |  |  |  |  |  |  |  |  |  |  | 4 |
| Actuated Green，G（s） | 15.8 | 47.5 |  | 20.3 | 52.5 |  | 12.1 | 9.1 |  | 13.1 | 10.1 | 10.1 |
| Effective Green，g（s） | 13.8 | 45.5 |  | 18.3 | 50.5 |  | 10.1 | 7.1 |  | 11.1 | 8.1 | 8.1 |
| Actuated g／C Ratio | 0.13 | 0.42 |  | 0.17 | 0.47 |  | 0.09 | 0.07 |  | 0.10 | 0.07 | 0.07 |
| Clearance Time（s） | 4.5 | 5.0 |  | 4.5 | 4.5 |  | 4.5 | 4.5 |  | 4.5 | 4.5 | 4.5 |
| Vehicle Extension（s） | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap（vph） | 225 | 2070 |  | 298 | 2285 |  | 319 | 102 |  | 181 | 139 | 98 |
| v／s Ratio Prot | 0.10 | c0．42 |  | c0．16 | c0．25 |  | 0.07 | 0.01 |  | c0．09 | c0．03 |  |


| v／s Ratio Perm |  |  |  |  | 0.87 | 0.40 | 0.15 |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| v／c Ratio | 0.80 | 1.01 | 0.95 | 0.54 | 0.76 | 0.22 | 48.0 | 47.9 |
| Uniform Delay，d1 | 46.0 | 31.5 | 44.6 | 20.7 | 48.0 | 48.1 | 47.0 |  |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay，d2 | 18.5 | 22.1 | 38.3 | 0.3 | 9.8 | 1.1 | 33.9 | 1.9 |
| Delay（s） | 64.5 | 53.6 | 82.9 | 21.0 | 57.8 | 49.2 | 82.0 | 49.8 |
| Level of Service | E | D | F | C | E | D | F | D |
| Approach Delay（s） |  | 54.4 |  | 32.4 |  | 55.7 | D |  |
| Approach LOS |  | D |  | C |  | E | 61.1 |  |

Approach LOS D C E E

| Intersection Summary |  |  |  |
| :--- | ---: | :--- | ---: |
| HCM 2000 Control Delay | 47.7 | HCM 2000 Level of Service | D |
| HCM 2000 Volume to Capacity ratio | 0.94 |  | 26.5 |
| Actuated Cycle Length（s） | 108.5 | Sum of lost time（s） | D |
| Intersection Capacity Utilization | $80.9 \%$ | ICU Level of Service |  |
| Analysis Period（min） | 15 |  |  |
| C Critical Lane Group |  |  |  |


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \％ | 个中t |  | \％ | 瑯 |  | \％${ }^{1 / 1}$ | $\hat{\beta}$ |  | ${ }^{7}$ | $\uparrow$ | F |
| Traffic Volume（vph） | 265 | 1405 | 135 | 181 | 1063 | 173 | 251 | 37 | 96 | 180 | 128 | 169 |
| Future Volume（vph） | 265 | 1405 | 135 | 181 | 1063 | 173 | 251 | 37 | 96 | 180 | 128 | 169 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time（s） | 6.5 | 7.0 |  | 6.5 | 7.0 |  | 6.5 | 6.0 |  | 6.5 | 6.0 | 6.0 |
| Lane Util．Factor | 1.00 | 0.91 |  | 1.00 | 0.91 |  | 0.97 | 1.00 |  | 1.00 | 1.00 | 1.00 |
| Frpb，ped／bikes | 1.00 | 1.00 |  | 1.00 | 0.97 |  | 1.00 | 0.79 |  | 1.00 | 1.00 | 0.82 |
| Flpb，ped／bikes | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 |
| Frt | 1.00 | 0.99 |  | 1.00 | 0.98 |  | 1.00 | 0.89 |  | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 |  | 0.95 | 1.00 |  | 0.95 | 1.00 |  | 0.95 | 1.00 | 1.00 |
| Satd．Flow（prot） | 1770 | 5018 |  | 1770 | 4853 |  | 3433 | 1317 |  | 1770 | 1863 | 1294 |
| Flt Permitted | 0.95 | 1.00 |  | 0.95 | 1.00 |  | 0.95 | 1.00 |  | 0.95 | 1.00 | 1.00 |
| Satd．Flow（perm） | 1770 | 5018 |  | 1770 | 4853 |  | 3433 | 1317 |  | 1770 | 1863 | 1294 |
| Peak－hour factor，PHF | 0.80 | 0.90 | 0.90 | 0.93 | 0.93 | 0.93 | 0.88 | 0.88 | 0.88 | 0.80 | 0.84 | 0.84 |
| Adj．Flow（vph） | 331 | 1561 | 150 | 195 | 1143 | 186 | 285 | 42 | 109 | 225 | 152 | 201 |
| RTOR Reduction（vph） | 0 | 8 | 0 | 0 | 16 | 0 | 0 | 70 | 0 | 0 | 0 | 173 |
| Lane Group Flow（vph） | 331 | 1703 | 0 | 195 | 1313 | 0 | 285 | 81 | 0 | 225 | 152 | 28 |
| Confl．Peds．（\＃／hr） |  |  |  |  |  | 86 |  |  | 140 |  |  | 87 |
| Turn Type | Prot | NA |  | Prot | NA |  | Prot | NA |  | Prot | NA | Perm |
| Protected Phases | 5 | 2 |  | 1 | 6 |  | 3 | 8 |  | 7 | 4 |  |
| Permitted Phases |  |  |  |  |  |  |  |  |  |  |  | 4 |
| Actuated Green，G（s） | 27.7 | 50.3 |  | 18.5 | 41.1 |  | 14.9 | 13.0 |  | 20.4 | 18.5 | 18.5 |
| Effective Green， g （s） | 25.7 | 48.3 |  | 16.5 | 39.1 |  | 12.9 | 11.0 |  | 18.4 | 16.5 | 16.5 |
| Actuated g／C Ratio | 0.21 | 0.40 |  | 0.14 | 0.33 |  | 0.11 | 0.09 |  | 0.15 | 0.14 | 0.14 |
| Clearance Time（s） | 4.5 | 5.0 |  | 4.5 | 5.0 |  | 4.5 | 4.0 |  | 4.5 | 4.0 | 4.0 |
| Vehicle Extension（s） | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap（vph） | 378 | 2016 |  | 242 | 1578 |  | 368 | 120 |  | 270 | 255 | 177 |
| v／s Ratio Prot | c0．19 | c0．34 |  | 0.11 | 0.27 |  | 0.08 | 0.06 |  | c0．13 | c0．08 |  |
| v／s Ratio Perm |  |  |  |  |  |  |  |  |  |  |  | 0.02 |
| v／c Ratio | 0.88 | 0.84 |  | 0.81 | 0.83 |  | 0.77 | 0.68 |  | 0.83 | 0.60 | 0.16 |
| Uniform Delay，d1 | 45.7 | 32.6 |  | 50.3 | 37.5 |  | 52.2 | 52.9 |  | 49.4 | 48.7 | 45.7 |
| Progression Factor | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 |
| Incremental Delay，d2 | 19.7 | 3.4 |  | 17.5 | 3.9 |  | 9.8 | 14.0 |  | 19.3 | 3.7 | 0.4 |
| Delay（s） | 65.4 | 36.0 |  | 67.8 | 41.4 |  | 62.0 | 66.9 |  | 68.7 | 52.4 | 46.1 |
| Level of Service | E | D |  | E | D |  | E | E |  | E | D | D |
| Approach Delay（s） |  | 40.8 |  |  | 44.8 |  |  | 63.7 |  |  | 56.6 |  |
| Approach LOS |  | D |  |  | D |  |  | E |  |  | E |  |


| Intersection Summary |  |  |  |
| :--- | ---: | :--- | ---: |
| HCM 2000 Control Delay | 46.3 | HCM 2000 Level of Service | D |
| HCM 2000 Volume to Capacity ratio | 0.88 |  | 26.0 |
| Actuated Cycle Length（s） | 120.2 | Sum of lost time（s） | E |
| Intersection Capacity Utilization | $86.8 \%$ | ICU Level of Service |  |
| Analysis Period（min） | 15 |  |  |
| C Critical Lane Group |  |  |  |


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ${ }^{7}$ | 个中t |  | ${ }^{7}$ | 个中t |  | ${ }^{7+1}$ | $\hat{\beta}$ |  | ${ }^{7}$ | $\uparrow$ | F |
| Traffic Volume（vph） | 163 | 1593 | 215 | 243 | 917 | 156 | 130 | 10 | 31 | 146 | 48 | 201 |
| Future Volume（vph） | 163 | 1593 | 215 | 243 | 917 | 156 | 130 | 10 | 31 | 146 | 48 | 201 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time（s） | 6.5 | 7.0 |  | 6.5 | 6.5 |  | 6.5 | 6.5 |  | 6.5 | 6.5 | 6.5 |
| Lane Util．Factor | 1.00 | 0.91 |  | 1.00 | 0.91 |  | 0.97 | 1.00 |  | 1.00 | 1.00 | 1.00 |
| Frpb，ped／bikes | 1.00 | 0.99 |  | 1.00 | 0.99 |  | 1.00 | 0.94 |  | 1.00 | 1.00 | 0.83 |
| Flpb，ped／bikes | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 |
| Frt | 1.00 | 0.98 |  | 1.00 | 0.98 |  | 1.00 | 0.89 |  | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 |  | 0.95 | 1.00 |  | 0.95 | 1.00 |  | 0.95 | 1.00 | 1.00 |
| Satd．Flow（prot） | 1770 | 4937 |  | 1770 | 4911 |  | 3433 | 1559 |  | 1770 | 1863 | 1319 |
| Flt Permitted | 0.95 | 1.00 |  | 0.95 | 1.00 |  | 0.95 | 1.00 |  | 0.95 | 1.00 | 1.00 |
| Satd．Flow（perm） | 1770 | 4937 |  | 1770 | 4911 |  | 3433 | 1559 |  | 1770 | 1863 | 1319 |
| Peak－hour factor，PHF | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.54 | 0.54 | 0.54 | 0.85 | 0.85 | 0.85 |
| Adj．Flow（vph） | 190 | 1852 | 250 | 283 | 1066 | 181 | 241 | 19 | 57 | 172 | 56 | 236 |
| RTOR Reduction（vph） | 0 | 13 | 0 | 0 | 16 | 0 | 0 | 53 | 0 | 0 | 0 | 218 |
| Lane Group Flow（vph） | 190 | 2089 | 0 | 283 | 1231 | 0 | 241 | 23 | 0 | 172 | 56 | 18 |
| Confl．Peds．（\＃／hr） |  |  | 26 |  |  | 23 |  |  | 36 |  |  | 87 |
| Turn Type | Prot | NA |  | Prot | NA |  | Prot | NA |  | Prot | NA | Perm |
| Protected Phases | 5 | 2 |  | 1 | 6 |  | 3 | 8 |  | 7 | 4 |  |
| Permitted Phases |  |  |  |  |  |  |  |  |  |  |  | 4 |
| Actuated Green，G（s） | 16.4 | 47.6 |  | 20.3 | 52.0 |  | 12.1 | 9.4 |  | 13.1 | 10.4 | 10.4 |
| Effective Green， $\mathrm{g}(\mathrm{s})$ | 14.4 | 45.6 |  | 18.3 | 50.0 |  | 10.1 | 7.4 |  | 11.1 | 8.4 | 8.4 |
| Actuated g／C Ratio | 0.13 | 0.42 |  | 0.17 | 0.46 |  | 0.09 | 0.07 |  | 0.10 | 0.08 | 0.08 |
| Clearance Time（s） | 4.5 | 5.0 |  | 4.5 | 4.5 |  | 4.5 | 4.5 |  | 4.5 | 4.5 | 4.5 |
| Vehicle Extension（s） | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap（vph） | 234 | 2067 |  | 297 | 2254 |  | 318 | 105 |  | 180 | 143 | 101 |
| v／s Ratio Prot | 0.11 | c0．42 |  | c0．16 | c0．25 |  | 0.07 | 0.01 |  | c0．10 | c0．03 |  |
| v／s Ratio Perm |  |  |  |  |  |  |  |  |  |  |  | 0.01 |
| v／c Ratio | 0.81 | 1.01 |  | 0.95 | 0.55 |  | 0.76 | 0.22 |  | 0.96 | 0.39 | 0.18 |
| Uniform Delay，d1 | 45.9 | 31.7 |  | 44.9 | 21.3 |  | 48.2 | 48.0 |  | 48.7 | 47.8 | 47.0 |
| Progression Factor | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 |
| Incremental Delay，d2 | 18.9 | 22.5 |  | 39.4 | 0.3 |  | 9.9 | 1.0 |  | 53.7 | 1.8 | 0.9 |
| Delay（s） | 64.8 | 54.1 |  | 84.3 | 21.5 |  | 58.1 | 49.1 |  | 102.3 | 49.6 | 47.9 |
| Level of Service | E | D |  | F | C |  | E | D |  | F | D | D |
| Approach Delay（s） |  | 55.0 |  |  | 33.1 |  |  | 55.9 |  |  | 68.3 |  |
| Approach LOS |  | E |  |  | C |  |  | E |  |  | E |  |


| Intersection Summary |  |  |  |
| :--- | ---: | :--- | ---: |
| HCM 2000 Control Delay | 49.1 | HCM 2000 Level of Service | D |
| HCM 2000 Volume to Capacity ratio | 0.95 | Sum of lost time（s） | 26.5 |
| Actuated Cycle Length（s） | 108.9 | S |  |
| Intersection Capacity Utilization | $81.0 \%$ | ICU Level of Service | D |
| Analysis Period（min） | 15 |  |  |

c Critical Lane Group

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \％ | 性榢 |  | ${ }^{7}$ | 中虾 |  | \％${ }^{*}$ | $\hat{\beta}$ |  | ${ }^{7}$ | $\uparrow$ | F |
| Traffic Volume（vph） | 280 | 1405 | 135 | 181 | 1058 | 168 | 251 | 37 | 96 | 162 | 128 | 183 |
| Future Volume（vph） | 280 | 1405 | 135 | 181 | 1058 | 168 | 251 | 37 | 96 | 162 | 128 | 183 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time（s） | 6.5 | 7.0 |  | 6.5 | 7.0 |  | 6.5 | 6.0 |  | 6.5 | 6.0 | 6.0 |
| Lane Util．Factor | 1.00 | 0.91 |  | 1.00 | 0.91 |  | 0.97 | 1.00 |  | 1.00 | 1.00 | 1.00 |
| Frpb，ped／bikes | 1.00 | 0.99 |  | 1.00 | 0.96 |  | 1.00 | 0.79 |  | 1.00 | 1.00 | 0.82 |
| Flpb，ped／bikes | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 |
| Frt | 1.00 | 0.99 |  | 1.00 | 0.98 |  | 1.00 | 0.89 |  | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 |  | 0.95 | 1.00 |  | 0.95 | 1.00 |  | 0.95 | 1.00 | 1.00 |
| Satd．Flow（prot） | 1770 | 4972 |  | 1770 | 4774 |  | 3433 | 1316 |  | 1770 | 1863 | 1293 |
| Flt Permitted | 0.95 | 1.00 |  | 0.95 | 1.00 |  | 0.95 | 1.00 |  | 0.95 | 1.00 | 1.00 |
| Satd．Flow（perm） | 1770 | 4972 |  | 1770 | 4774 |  | 3433 | 1316 |  | 1770 | 1863 | 1293 |
| Peak－hour factor，PHF | 0.80 | 0.90 | 0.90 | 0.93 | 0.93 | 0.93 | 0.88 | 0.88 | 0.88 | 0.80 | 0.84 | 0.84 |
| Adj．Flow（vph） | 350 | 1561 | 150 | 195 | 1138 | 181 | 285 | 42 | 109 | 202 | 152 | 218 |
| RTOR Reduction（vph） | 0 | 8 | 0 | 0 | 15 | 0 | 0 | 70 | 0 | 0 | 0 | 189 |
| Lane Group Flow（vph） | 350 | 1703 | 0 | 195 | 1304 | 0 | 285 | 81 | 0 | 203 | 152 | 29 |
| Confl．Peds．（\＃／hr） |  |  | 26 |  |  | 86 |  |  | 140 |  |  | 87 |
| Turn Type | Prot | NA |  | Prot | NA |  | Prot | NA |  | Prot | NA | Perm |
| Protected Phases | 5 | 2 |  | ， | 6 |  | 3 | 8 |  | 7 | 4 |  |
| Permitted Phases |  |  |  |  |  |  |  |  |  |  |  | 4 |
| Actuated Green，G（s） | 29.2 | 51.2 |  | 18.6 | 40.6 |  | 14.9 | 13.6 |  | 19.1 | 17.8 | 17.8 |
| Effective Green， g （s） | 27.2 | 49.2 |  | 16.6 | 38.6 |  | 12.9 | 11.6 |  | 17.1 | 15.8 | 15.8 |
| Actuated g／C Ratio | 0.23 | 0.41 |  | 0.14 | 0.32 |  | 0.11 | 0.10 |  | 0.14 | 0.13 | 0.13 |
| Clearance Time（s） | 4.5 | 5.0 |  | 4.5 | 5.0 |  | 4.5 | 4.0 |  | 4.5 | 4.0 | 4.0 |
| Vehicle Extension（s） | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap（vph） | 399 | 2030 |  | 243 | 1529 |  | 367 | 126 |  | 251 | 244 | 169 |
| v／s Ratio Prot | c0．20 | c0．34 |  | 0.11 | 0.27 |  | 0.08 | 0.06 |  | c0．11 | c0．08 |  |
| v／s Ratio Perm |  |  |  |  |  |  |  |  |  |  |  | 0.02 |
| v／c Ratio | 0.88 | 0.84 |  | 0.80 | 0.85 |  | 0.78 | 0.65 |  | 0.81 | 0.62 | 0.17 |
| Uniform Delay，d1 | 45.0 | 32.1 |  | 50.4 | 38.3 |  | 52.4 | 52.5 |  | 50.1 | 49.5 | 46.5 |
| Progression Factor | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 |
| Incremental Delay，d2 | 19.0 | 3.2 |  | 17.2 | 4.8 |  | 9.9 | 10.8 |  | 17.2 | 4.9 | 0.5 |
| Delay（s） | 64.0 | 35.3 |  | 67.5 | 43.1 |  | 62.3 | 63.3 |  | 67.3 | 54.4 | 47.0 |
| Level of Service | E | D |  | E | D |  | E | E |  | E | D | D |
| Approach Delay（s） |  | 40.2 |  |  | 46.3 |  |  | 62.6 |  |  | 56.2 |  |
| Approach LOS |  | D |  |  | D |  |  | E |  |  | E |  |


| Intersection Summary |  |  |  |
| :--- | ---: | :--- | ---: |
| HCM 2000 Control Delay | 46.3 | HCM 2000 Level of Service | D |
| HCM 2000 Volume to Capacity ratio | 0.88 | Sum of lost time（s） | 26.0 |
| Actuated Cycle Length（s） | 120.5 | E |  |
| Intersection Capacity Utilization | $86.1 \%$ | ICU Level of Service |  |

c Critical Lane Group

Mary Ave/Campus Dr \& Stevens Creek Blvd


## Kimley»"Horn

## MEMORANDUM

From: Frederik Venter, P.E. and Anthony Nuti, Kimley-Horn and Associates
To: Winnie Pagan and Chad Mosely, City of Cupertino Public Works
Date: September 18, 2019
Re: Westport Cupertino - Stevens Creek Boulevard \& SR 85 On Ramp Signalization Analysis

The purpose of this memorandum is to present traffic analysis findings for the reconfiguration of the westbound right turn lane at the intersection of Stevens Creek Boulevard and SR 85 Northbound Ramp Terminal for pedestrian and bicycle crossing maneuvers. Level of service and queue analysis for the westbound right turn movement and the overall intersection are discussed in this memo. The effect of the Westport Cupertino mixed-use urban village project (hereinafter referred to as "Westport") on the westbound right turn movement and level of service at the intersection also were evaluated. The Westport project would demolish the existing shopping center (i.e., The Oaks Shopping Center) and construct 203 multi-family residential units, 39 senior units, and 20,000 square feet of retail space.

## 1. Introduction

The City of Cupertino is planning to reconfigure the existing westbound right turn movement from Stevens Creek Boulevard onto the Northbound State Route 85 On Ramp. This reconfiguration will include the following:

- Convert the existing westbound "free" right turn lane to a signal controlled right turn movement to allow for an exclusive protected phase for pedestrians and cyclists to cross the on-ramp leg.

The purpose of this reconfiguration is to increase pedestrian and bicycle opportunities to cross the on-ramp leg.

For this analysis, the following study intersection was analyzed:

1. Stevens Creek Boulevard \& State Route 85 Northbound Ramp Terminal

Figure 1 shows the location of the study intersection.
Figure 2 shows the reconfiguration of the Stevens Creek and Northbound State Route 85 On/Off Ramps provided by Toole Design Group. The planned intersection configuration is in the conceptual design stage.

Figure 3 shows the proposed site plan for the Westport project.
A Simtraffic microsimulation model was prepared for the analysis. The model included the Stevens Creek Boulevard/Mary Avenue intersection to the east and the Stevens Creek Boulevard/SR 85 southbound ramp terminal intersection to the west, to have accurate arrival patterns for the analysis of the study intersection, particularly the westbound right turn movement. No analysis results were reported for these adjacent intersections, since the operations at these locations will remain unaffected with the planned reconfiguration.



Proposed SR 85 NB Ramp Terminal Reconfiguration


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## 2. Analysis Methodology

The Santa Clara Valley Transportation Authority (VTA) Traffic Impact Analysis Guidelines (October 2014), City of Cupertino guidelines, and industry criteria were utilized in this analysis to determine project requirements and potential impacts.

Analysis of the study intersection is based on the concept of Level of Service (LOS). The LOS of an intersection is a qualitative measurement used to describe operational conditions. LOS ranges from A (best), which represents minimal delay, to $F$ (worst), which represents heavy delay and a facility that is operating at or near its functional capacity.

Intersection delay and level of service (LOS) calculations were performed using Highway Capacity Manual (HCM) 2000 methodology in Synchro Version 9, which is consistent with TRAFFIX software. Synchro was used instead of TRAFFIX because it provides improved signal timing evaluation at the intersection of Stevens Creek and Northbound State Route 85 On/Off Ramps.

The VTA Congestion Management Plan (CMP) (December 2017) states a LOS E, except for facilities grandfathered in at LOS F, is acceptable for both the AM and PM peak hour at the study intersection. The study intersection is not identified as an intersection operating at LOS F, so a minimum of LOS E is acceptable for the study intersection.

The following scenarios were analyzed for this report in the AM and PM peak hours:

- Existing (2019) Conditions
- Existing (2019) Plus Westport and Signalized Conditions for the Westbound Right Turn Movement
- Cumulative (2040) Conditions
- Cumulative (2040) Plus Westport and Signalized Conditions for the Westbound Right Turn Movement


## 3. Traffic Analysis

The following section discusses traffic operations at the study intersection of Stevens Creek Boulevard and Northbound State Route 85 Ramp Terminal.

### 3.1 Existing (2019) Conditions LOS Analysis

Existing Conditions traffic operations were evaluated using existing lane geometry, traffic control, and peak hour traffic, pedestrian, and bicycle volumes. Counts were collected on the following days:

- AM Peak Period: May 23, 2019 (7:00 AM - 10:00 AM)
- PM Peak Period: May 22, 2019 (4:00 PM - 7:00 PM)

Counts were collected when school was in session and the weather was fair.
Current operations at the study intersection include the following:

- Protected left turns on all approaches
- No right turn on red for the Northbound State Route 85 Off Ramp right turn onto Stevens Creek Boulevard
- No right turns allowed for the De Anza Community College approach
- "Free" movements for the westbound right turn from Stevens Creek Boulevard onto the northbound on ramp of State Route 85
- The north leg has a two-stage crosswalk that allows a pedestrian or cyclist to cross the "free" westbound right turn lane when there is a gap in traffic or traffic stops for them and wait on the small refuge island provided. Then they cross the on-ramp lanes using the pedestrian signalcontrolled crosswalk.


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Even though right turns are not permitted for the De Anza Community College approach, some vehicles were observed performing this movement. In Synchro these vehicles were modeled as through movements since a right turn is an illegal movement.

Figure 4 shows the Existing Conditions Geometry at the study intersection.
Figure 5 shows the vehicle count data, Figure 6 shows the pedestrian count data, and Figure 7 shows the bike count data.

Table 1 illustrates the LOS and delay under Existing Conditions.
The $95^{\text {th }}$ percentile queue for the westbound right turn is zero in Existing (2019) Conditions. The movement is a "free" right turn, and cars can perform the movement without stopping. Vehicles currently yield to pedestrians using the crosswalk at the northbound on-ramp; however, the low bicycle and pedestrian volumes do not generate queues when vehicles yield to them as they cross the westbound right turn movement.

The existing intersection currently operates at an acceptable level of service.
Figure 4 - Existing (2019) Conditions Geometry


Figure 5 - Existing (2019) Conditions Peak Hour Intersection Volumes


Figure 6 - Existing Peak Hour Pedestrian Count Data


Figure 7 - Existing Peak Hour Bicycle Count Data


| LEGEND |
| :---: |
|  |
| Traffic Signal |
| $\mathrm{XX}(\mathrm{YY})$ |
| $\mathrm{AM}(\mathrm{PM})$ Bicycle Volumes |

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Table 1 - Existing (2019) Conditions Level of Service

| Intersection |  | LOS Criteria | Jurisdiction | Control | Existing (2019) |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | AM Peak |  |  | PM Peak |  |
|  |  | LOS |  |  | Delay | LOS | Delay |
| 1 | Stevens Creek Boulevard and NB SR 85 On/Off Ramps |  | E | Caltrans | Signal | C | 30.0 | C | 24.7 |

1. Analysis performed using Synchro 10 with HCM 2000 methodologies
2. Delay indicated in seconds/vehicle
3. CMP level of service (LOS) standard for the County is E
4. Intersections that fall below City standards are shown in bold

### 3.2 Trip Generation Estimates and Distribution for the Westport Project

The Westport project would generate -275 net new daily trips, 47 net new AM peak hour trips, and -22 net new PM peak hour trips, consistent with the analysis completed in the Westport Cupertino - Transportation Analysis Memo (November 27, 2018).

Figure 8 illustrates the distribution for the retail uses of the Westport project, while Figure 9 illustrates the distribution for the residential uses.



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### 3.3 Existing (2019) Plus Westport Project and Signalized Conditions for the Westbound Right Turn (WBR) Conditions

Traffic operations were evaluated with Synchro and SimTraffic software using the proposed signalized westbound right turn configuration with existing peak hour traffic volumes and adding the Westport project trips.

Figure 10 shows the intersection volumes with the Westport Project implemented. It was also estimated that bicycle and pedestrian volumes would increase by $20 \%$ at the crosswalk. This is based on the assumption that the improved facility and the added residential units from the Westport project would generate more pedestrian and bicycle demand. The new pedestrian and bicycle crossing volumes are shown on Figure 11 and Figure 12, respectively.

To be conservative, only a pedestrian signal was analyzed because a pedestrian crossing time is longer than a bicycle crossing time. A shorter bicycle crossing time would produce shorter vehicle queues in the westbound right turn lane than would occur with a longer pedestrian crossing time.

Currently, the westbound right turn movement operates independently from the existing intersection as a "free" right turn. With the addition of signal control for the westbound right turn movement, the cars would have a continuous green right-turn arrow until a cyclist or pedestrian arrives and activates the pedestrian or bike crossing signal, at which time a red right-turn arrow would stop the cars. This pedestrian/bicycle signal call could only occur on the east-west signal phasing plan of the intersection when there are no other conflicting movements with the pedestrian and/or bicycle phase. Queues would only form in the westbound right turn pocket when the right turn arrow is red.

SimTraffic software cannot accurately simulate this signal timing plan because of the random nature of pedestrian and bicycle arrivals/crossings. Thus, an equivalent simulation was developed that is more conservative and assumes a pedestrian or bicycle call with every green east-west phase. In addition, a pedestrian crossing time was used in the simulation, which is higher compared to a bicycle crossing time.

Queues would be generated by the vehicles stopping and waiting for a pedestrian or bicycle to cross when the right turn arrow is red. Queue results after five SimTraffic simulations and HCM 2000 LOS results for the westbound right turn lane are reported in Table 2.

Under Existing (2019) Plus Westport and Signalized Conditions, queues for the westbound right turn movement would increase by approximately nine cars in the AM peak hour and ten cars in the PM peak hour compared to existing conditions with no signal control. The overall intersection LOS would also remain at LOS C in both the AM and PM peak hours.

Figure 13 shows the estimated queue lengths and demonstrates that no operational issues would occur.
Note that the queues reported in Table 2 and shown on Figure 13 are the $95^{\text {th }}$ percentile vehicle queues. The $95^{\text {th }}$ percentile queue length value indicates that a queue of this length or less would occur on 95 percent of the signal cycles that include a pedestrian or bicycle call.

It is anticipated that no median will be provided at this location, consistent with the latest Caltrans and VTA policies, and that the curb return would be squared up and the radii sufficient to accommodate truck turns. A pedestrian and cyclist would then cross the on-ramp in one phase (i.e., the current two-stage crossing procedure would be eliminated). The total crosswalk length was determined to be 85 feet, which requires approximately 25 seconds (at a walking speed of 3.5 feet per second) for the pedestrian clearance interval. Right turn on red would not be allowed for the westbound right turn movement to prevent cars from yielding (instead of stopping) to pedestrians.

## Kimley»"Horn

Figure 10 - Existing (2019) Plus Westport and Signalized Conditions Peak Hour Intersection Volumes


Figure 11 - Existing (2019) Plus Westport and Signalized Conditions Peak Hour Pedestrian Volumes


## Kimley»)Horn

Figure 12 - Existing (2019) Plus Westport and Signalized Conditions Peak Hour Bicycle Volumes


Table 2 - Existing (2019) Plus Westport and Signalized Conditions Queues

| Intersection |  | MVMT | Existing (2019) + Westport + Signal |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | AM Peak | PM Peak |  |  |
|  |  | Delay | LOS ${ }^{1}$ | 95 ${ }^{\text {th }}$ Percentile Queue ${ }^{2}$ | Delay | LOS ${ }^{1}$ | 95 ${ }^{\text {th }}$ Percentile Queue ${ }^{2}$ |
| 1 | Stevens Creek Boulevard and NB SR 85 On/Off Ramps |  | WBRT | 7.6 | A | $\begin{gathered} 220 \mathrm{ft} \\ (9 \mathrm{cars}) \end{gathered}$ | 8.0 | A | $\begin{gathered} 243 \mathrm{ft} \\ (10 \mathrm{cars}) \end{gathered}$ |

1. Analysis performed using Synchro 10 with HCM 2000 methodologies
2. Analysis completed using Simtraffic simulation software

Figure 13 - Existing (2019) Plus Westport and Signalized Conditions Queue Lengths


## Kimley»"Horn

### 3.4 Cumulative (2040) Conditions

Traffic operations were evaluated for 2040 Cumulative Conditions based on data obtained from the City of Cupertino General Plan EIR, 2014 (June 6, 2014).

It is assumed that the Cumulative Conditions intersection geometry of State Route 85 and Stevens Creek Boulevard would be the same as Existing Conditions. Accordingly, vehicles would yield to pedestrians and cyclists using the crosswalk at the northbound on-ramp; however, the low bicycle and pedestrian volumes would not generate queues when vehicles yield to them as they cross the intersection.

Figure 14 shows the Cumulative (2040) volumes while Table 3 shows the LOS and delay for the traffic signal at the study intersection. The queues for the westbound right turn are assumed to be zero because in Cumulative (2040) Conditions, the movement would be "free", and cars would perform this movement without stopping. Vehicles would yield to pedestrians and cyclists using the crosswalk at the northbound on-ramp; however, the low bicycle and pedestrian volumes would not generate queues when vehicles yield to them as they cross the westbound right turn movement.

Under Cumulative (2040) Conditions the intersection would operate at an acceptable level of service.
It should be noted that for the intersection, the PM peak hour reported delay improved with Cumulative (2040) Conditions. The reason for this occurrence is because the trips were predominately added to noncritical movements, which had a lower movement delay than the average intersection delay, and thereby decreases the overall average delay.

Figure 14 - Cumulative (2040) Conditions Peak Hour Intersection Volumes


## Kimley»"Horn

Table 3 - Cumulative (2040) Conditions Level of Service

| Intersection |  | LOS Criteria | Jurisdiction | Control | Cumulative (2040) |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | AM Peak |  |  | PM Peak |  |
|  |  | LOS |  |  | Delay | LOS | Delay |
| 1 | Stevens Creek Boulevard and NB SR 85 On/Off Ramps |  | E | Caltrans | Signal | D | 46.1 | C | 20.3 |

1. Analysis performed using Synchro 10 with HCM 2000 methodologies
. Delay indicated in seconds/vehicle
2. CMP level of service (LOS) standard for the County is E
3. Intersections that fall below City standards are shown in bold

### 3.5 Cumulative (2040) Plus Westport Project and Signalized Conditions for the Westbound Right Turn (WBR) Conditions

Traffic operations were evaluated with Synchro and SimTraffic software using the proposed signalized westbound right turn configuration with Cumulative (2040) peak hour traffic volumes and adding the Westport project trips.

Figure 15 shows the intersection volumes with the Westport Project implemented. It was also assumed that bicycle and pedestrian volumes would increase by $20 \%$ at the crosswalk. The new pedestrian and bicycle crossing volumes are shown on Figure 16 and Figure 17, respectively.

The signal phasing conditions would be the same as for Existing Plus Project conditions. Queues were analyzed for the Cumulative (2040) Plus Westport Project and Signalized WBR Conditions to determine the extent of vehicle queuing that would occur along westbound Stevens Creek Boulevard as a result of the new signal control. Queue results after five SimTraffic simulations and HCM 2000 LOS results for the westbound right turn lane are reported in Table 4.

Under Cumulative (2040) Plus Westport and Signalized Conditions, queues for the westbound right turn movement would increase by approximately ten cars in the AM peak hour and twelve cars in the PM peak hour compared to existing conditions with no signal control. The overall intersection LOS would also remain at LOS D in the AM peak hour and LOS C in the PM peak hour.

Figure 18 shows the estimated queue lengths and demonstrates that no operational issues would occur.

## Kimley»)Horn

Figure 15 - Cumulative (2040) Plus Westport and Signalized Conditions Peak Hour Intersection Volumes


Figure 16 - Cumulative (2040) Plus Westport and Signalized Conditions Peak Hour Pedestrian Volumes


## Kimley»"Horn

Figure 17 - Cumulative (2040) Plus Westport and Signalized Conditions Peak Hour Bicycle Volumes


Table 4 - Cumulative (2040) Plus Westport and Signalized Conditions Queues

| Intersection |  | MVMT | Cumulative (2040) + Westport + Signal |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | AM Peak | PM Peak |  |  |
|  |  | Delay | LOS ${ }^{1}$ | 95 ${ }^{\text {th }}$ Percentile Queue ${ }^{2}$ | Delay | LOS ${ }^{1}$ | 95 ${ }^{\text {th }}$ Percentile Queue ${ }^{2}$ |
| 1 | Stevens Creek Boulevard and NB SR 85 On/Off Ramps |  | WBRT | 8.2 | A | $\begin{gathered} 246 \mathrm{ft} \\ (10 \mathrm{cars}) \end{gathered}$ | 11.1 | B | $\begin{gathered} 284 \mathrm{ft} \\ (12 \mathrm{cars}) \end{gathered}$ |

1. Analysis performed using Synchro 10 with HCM 2000 methodologies
2. Analysis completed using Simtraffic simulation software

Figure 18 - Cumulative Plus Westport and Signalized Conditions Queue Lengths


## Kimley»"Horn

## 4. Conclusions

Table 5 provides a summary for the analysis of the proposed bike and pedestrian signal control phase at the intersection of Stevens Creek Boulevard and Northbound State Route 85 On/Off Ramps. With the Westport project and signalization of the westbound right turn movement, the westbound right turn queues would increase during the AM and PM peak hours of traffic. However, the increases would be minimal and would not be substantial enough to cause any operational issues along Stevens Creek Boulevard.

Table 5 - Summary Table

| Scenario | Type | AM Peak | PM Peak |
| :---: | :---: | :---: | :---: |
| Existing (2019) Conditions | Intersection Delay (s) | 30.0 | 24.7 |
|  | Intersection LOS | C | C |
|  | WBR 95 ${ }^{\text {th }}$ Percentile Queue | 0 feet | 0 feet |
| Existing (2019) Plus Westport and Signalized Conditions | Intersection Delay (s) | 34.3 | 23.0 |
|  | Intersection LOS | C | C |
|  | WBR Delay (s) | 7.6 | 8.0 |
|  | WBR LOS | A | A |
|  | WBR 95 ${ }^{\text {th }}$ <br> Percentile Queue | $\begin{aligned} & 220 \mathrm{ft} \\ & (9 \mathrm{cars}) \end{aligned}$ | $\begin{gathered} 243 \mathrm{ft} \\ (10 \mathrm{cars}) \end{gathered}$ |
| Cumulative (2040) Conditions | Intersection Delay (s) | 46.1 | 20.3 |
|  | Intersection LOS | D | C |
|  | WBR 95 ${ }^{\text {th }}$ <br> Percentile Queue | 0 feet | 0 feet |
| Cumulative (2040) Plus Westport and Signalized Conditions | Intersection Delay (s) | 47.6 | 24.7 |
|  | Intersection LOS | D | C |
|  | WBR Delay (s) | 8.2 | 11.1 |
|  | WBR LOS | A | B |
|  | WBR 95 ${ }^{\text {th }}$ <br> Percentile Queue | $\begin{gathered} 246 \mathrm{ft} \\ (10 \mathrm{cars}) \end{gathered}$ | $\begin{gathered} 284 \mathrm{ft} \\ \text { (12 cars) } \end{gathered}$ |

## Kimley»"Horn

## 5. APPENDIX

A1: Existing Turning Movement Counts
A2: Existing Conditions Synchro Outputs
A3: Existing Plus Westport and Signal Conditions Synchro Outputs
A4: Cumulative Conditions Synchro Outputs
A5: Cumulative Plus Westport and Signal Conditions Synchro Outputs
A6: Westport Trip Generation

A1: Existing Turning Movement Counts


Three-Hour Count Summaries

| Interval Start |  | Stevens Creek Blvd |  |  |  |  | Stevens Creek Blvd |  |  |  |  | SR-85 NB Off Ramp |  |  |  |  | SR-85 NB On Ramp |  |  |  |  | Campus Dr |  |  |  |  | 15-min Total | $\begin{array}{\|c} \text { Rolling } \\ \text { One } \\ \text { Hour } \end{array}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Eastbound |  |  |  |  | Westbound |  |  |  |  | Northbound |  |  |  |  | Southbound |  |  |  |  | Northwestbound |  |  |  |  |  |  |
|  |  | UT | LT | TH | BR | RT | UT | HL | LT | TH | RT | UT | LT | TH | RT | HR | UT | LT | BL | TH | RT | UT | HL | BL | BR | HR |  |  |
| 4:00 PM |  | 0 | 115 | 377 | 0 | 0 | 0 | 0 | 0 | 133 | 106 | 0 | 35 | 0 | 38 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 14 | 26 | 1 | 845 | 0 |
| 4:15 PM |  | 0 | 94 | 424 | 0 | 0 | 0 | 0 | 0 | 114 | 103 | 0 | 55 | 0 | 87 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 9 | 14 | 1 | 901 | 0 |
| 4:30 PM |  | 0 | 147 | 445 | 0 | 0 | 0 | 0 | 0 | 111 | 102 | 0 | 23 | 0 | 37 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 8 | 20 | 2 | 895 | 0 |
| 4:45 PM |  | 0 | 113 | 387 | 0 | 0 | 0 | 0 | 0 | 121 | 97 | 0 | 39 | 0 | 47 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 7 | 19 | 1 | 831 | 3,472 |
| 5:00 PM |  | 0 | 135 | 417 | 0 | 0 | 0 | 0 | 0 | 111 | 110 | 0 | 33 | 1 | 60 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 | 32 | 1 | 906 | 3,533 |
| 5:15 PM |  | 0 | 128 | 467 | 0 | 0 | 0 | 0 | 0 | 138 | 102 | 0 | 35 | 0 | 82 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 10 | 28 | 1 | 991 | 3,623 |
| 5:30 PM |  | 0 | 129 | 370 | 0 | 0 | 0 | 0 | 0 | 128 | 122 | 0 | 47 | 0 | 74 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 16 | 43 | 0 | 929 | 3,657 |
| 5:45 PM |  | 0 | 142 | 426 | 0 | 0 | 0 | 0 | 0 | 170 | 113 | 0 | 31 | 1 | 73 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 16 | 20 | 1 | 993 | 3,819 |
| 6:00 PM |  | 0 | 133 | 348 | 0 | 0 | 0 | 0 | 0 | 111 | 108 | 0 | 43 | 0 | 74 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 19 | 56 | 1 | 893 | 3,806 |
| 6:15 PM |  | 0 | 131 | 342 | 0 | 0 | 0 | 0 | 0 | 146 | 118 | 0 | 44 | 1 | 75 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 11 | 39 | 2 | 909 | 3,724 |
| 6:30 PM |  | 0 | 135 | 254 | 0 | 0 | 0 | 0 | 0 | 157 | 122 | 0 | 36 | 1 | 59 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 13 | 20 | 3 | 800 | 3,595 |
| 6:45 PM |  | 0 | 147 | 247 | 0 | 0 | 0 | 0 | 0 | 111 | 121 | 0 | 41 | 0 | 38 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 11 | 25 | 5 | 746 | 3,348 |
| Count Total |  | 0 | 1,549 | 4,504 | 0 | 0 | 0 | 0 | 0 | 1,551 | 1,324 | 0 | 462 | 4 | 744 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 140 | 342 | 19 | 10,639 | 0 |
| Peak Hour | All | 0 | 534 | 1,680 | 0 | 0 | 0 | 0 | 0 | 547 | 447 | 0 | 146 | 2 | 289 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 48 | 123 | 3 | 3,819 | 0 |
|  | HV | 0 | 7 | 11 | 0 | 0 | 0 | 0 | 0 | 15 | 2 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 36 | 0 |
|  | HV\% | - | 1\% | 1\% | - | - | - | - | - | 3\% | 0\% | - | 0\% | 0\% | 0\% | - | - | . | . | . | . | . | . | 0\% | 0\% | 0\% | 1\% | 0 |

. Three-hour count summary volumes include heavy vehicles but exclude bicycles in overall count.

| Interval Start | Heavy Vehicle Totals |  |  |  |  |  | Bicycles |  |  |  |  |  | Pedestrians (Crossing Leg) |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | EB | WB | NB | SB | NWB | Total | EB | WB | NB | SB | NWB | Total | East | West | North | South | Southeast | Total |
| 4:00 PM | 5 | 2 | 0 | 0 | 0 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 4 | 3 | 10 |
| 4:15 PM | 1 | 4 | 0 | 0 | 0 | 5 | 1 | 3 | 0 | 0 | 0 | 4 | 0 | 0 | 2 | 0 | 0 | 2 |
| 4:30 PM | 4 | 2 | 0 | 0 | 0 | 6 | 0 | 2 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 2 | 2 | 4 |
| 4:45 PM | 4 | 5 | 0 | 0 | 0 | 9 | 3 | 2 | 0 | 0 | 0 | 5 | 0 | 0 | 2 | 3 | 3 | 8 |
| 5:00 PM | 5 | 4 | 0 | 0 | 0 | 9 | 2 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 3 | 2 | 2 | 7 |
| 5:15 PM | 5 | 6 | 0 | 0 | 0 | 11 | 0 | 4 | 0 | 0 | 0 | 4 | 0 | 0 | 1 | 2 | 2 | 5 |
| 5:30 PM | 6 | 3 | 1 | 0 | 0 | 10 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 2 | 2 | 5 |
| 5:45 PM | 2 | 4 | 0 | 0 | 0 | 6 | 1 | 2 | 0 | 0 | 0 | 3 | 0 | 0 | 1 | 0 | 0 | 1 |
| 6:00 PM | 4 | 1 | 0 | 0 | 5 | 10 | 2 | 1 | 0 | 0 | 2 | 5 | 0 | 0 | 1 | 3 | 3 | 7 |
| 6:15 PM | 2 | 3 | 0 | 0 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 3 |
| 6:30 PM | 2 | 3 | 0 | 0 | 0 | 5 | 0 | 2 | 0 | 0 | 0 | 2 | 0 | 0 | 1 | 2 | 2 | 5 |
| 6:45 PM | 9 | 3 | 0 | 0 | 0 | 12 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 2 | 2 | 2 | 6 |
| Count Total | 49 | 40 | 1 | 0 | 5 | 95 | 9 | 18 | 0 | 0 | 2 | 29 | 0 | 0 | 18 | 23 | 22 | 63 |
| Peak Hr | 18 | 17 | 1 | 0 | 0 | 36 | 3 | 7 | 0 | 0 | 0 | 10 | 0 | 0 | 6 | 6 | 6 | 18 |

Three-Hour Count Summaries - Heavy Vehicles

| Interval Start | Stevens Creek Blvd |  |  |  |  | Stevens Creek Blvd |  |  |  |  | SR-85 NB Off Ramp |  |  |  |  | SR-85 NB On Ramp |  |  |  |  | Campus Dr |  |  |  |  | 15-min Total | Rolling <br> One <br> Hour <br> 0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Eastbound |  |  |  |  | Westbound |  |  |  |  | Northbound |  |  |  |  | Southbound |  |  |  |  | Northwestbound |  |  |  |  |  |  |
|  | UT | LT | TH | BR | RT | UT | HL | LT | TH | RT | UT | LT | TH | RT | HR | UT | LT | BL | TH | RT | UT | HL | BL | BR | HR |  |  |
| 4:00 PM | 0 | 1 | 4 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 7 | 0 |
| 4:15 PM | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 0 |
| 4:30 PM | 0 | 1 | 3 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 | 0 |
| 4:45 PM | 0 | 1 | 3 | 0 | 0 | 0 | 0 | 0 | 3 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 9 | 27 |
| 5:00 PM | 0 | 3 | 2 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 9 | 29 |
| 5:15 PM | 0 | 2 | 3 | 0 | 0 | 0 | 0 | 0 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 11 | 35 |
| 5:30 PM | 0 | 1 | 5 | 0 | 0 | 0 | 0 | 0 | 2 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 10 | 39 |
| 5:45 PM | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 3 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 | 36 |
| 6:00 PM | 0 | 1 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 0 | 10 | 37 |
| 6:15 PM | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 31 |
| 6:30 PM | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 26 |
| 6:45 PM | 0 | 1 | 8 | 0 | 0 | 0 | 0 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 12 | 32 |
| Count Total | 0 | 15 | 34 | 0 | 0 | 0 | 0 | 0 | 30 | 10 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 0 | 95 | 0 |
| Peak Hour | 0 | 7 | 11 | 0 | 0 | 0 | 0 | 0 | 15 | 2 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 36 | 0 |

Three-Hour Count Summaries - Bikes

| Interval Start | Stevens Creek Blvd |  |  |  |  | Stevens Creek Blvd |  |  |  |  | SR-85 NB Off Ramp |  |  |  |  | SR-85 NB On Ramp |  |  |  |  | Campus Dr |  |  |  |  | $\begin{aligned} & \text { 15-min } \\ & \text { Total } \end{aligned}$ | $\begin{gathered} \text { Rolling } \\ \text { One } \\ \text { Hour } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Eastbound |  |  |  |  | Westbound |  |  |  |  | Northbound |  |  |  |  | Southbound |  |  |  |  | Northwestbound |  |  |  |  |  |  |
|  | UT | LT | TH | BR | RT | UT | HL | LT | TH | RT | UT | LT | TH | RT | HR | UT | LT | BL | TH | RT | UT | HL | BL | BR | HR |  |  |
| 4:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:15 PM | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 0 |
| 4:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 |
| 4:45 PM | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 11 |
| 5:00 PM | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 13 |
| 5:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 13 |
| 5:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 12 |
| 5:45 PM | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 10 |
| 6:00 PM | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 5 | 13 |
| 6:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 9 |
| 6:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 10 |
| 6:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 8 |
| Count Total | 0 | 0 | 9 | 0 | 0 | 0 | 0 | 0 | 18 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 29 | 0 |
| Peak Hour | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 10 | 0 |



Three-Hour Count Summaries

| Interval Start |  | Stevens Creek Blvd |  |  |  |  | Stevens Creek Blvd |  |  |  |  | SR-85 NB Off Ramp |  |  |  |  | SR-85 NB On Ramp |  |  |  |  | Campus Dr |  |  |  |  | $\begin{aligned} & \text { 15-min } \\ & \text { Total } \end{aligned}$ | $\begin{array}{\|c} \text { Rolling } \\ \text { One } \\ \text { Hour } \end{array}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Eastbound |  |  |  |  | Westbound |  |  |  |  | Northbound |  |  |  |  | Southbound |  |  |  |  | Northwestbound |  |  |  |  |  |  |
|  |  | UT | LT | TH | BR | RT | UT | HL | LT | TH | RT | UT | LT | TH | RT | HR | UT | LT | BL | TH | RT | UT | HL | BL | BR | HR |  |  |
| 7:00 AM |  | 0 | 86 | 96 | 0 | 0 | 0 | 0 | 0 | 50 | 82 | 0 | 44 | 1 | 45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 406 | 0 |
| 7:15 AM |  | 0 | 106 | 147 | 0 | 0 | 0 | 0 | 0 | 70 | 103 | 0 | 40 | 0 | 35 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 11 | 0 | 514 | 0 |
| 7:30 AM |  | 0 | 149 | 127 | 0 | 0 | 0 | 0 | 0 | 138 | 126 | 0 | 54 | 1 | 38 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 8 | 0 | 643 | 0 |
| 7:45 AM |  | 0 | 187 | 206 | 0 | 0 | 0 | 0 | 0 | 188 | 112 | 0 | 75 | 1 | 38 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 12 | 0 | 821 | 2,384 |
| 8:00 AM |  | 0 | 163 | 212 | 0 | 0 | 0 | 0 | 0 | 157 | 126 | 0 | 106 | 3 | 95 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 4 | 1 | 869 | 2,847 |
| 8:15 AM |  | 0 | 163 | 265 | 0 | 0 | 0 | 0 | 0 | 201 | 115 | 0 | 94 | 4 | 78 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 13 | 21 | 1 | 955 | 3,288 |
| 8:30 AM |  | 0 | 195 | 186 | 0 | 0 | 0 | 0 | 0 | 135 | 113 | 0 | 107 | 3 | 54 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 7 | 11 | 1 | 812 | 3,457 |
| 8:45 AM |  | 0 | 139 | 167 | 0 | 0 | 0 | 0 | 0 | 138 | 127 | 0 | 104 | 3 | 67 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 8 | 11 | 0 | 764 | 3,400 |
| 9:00 AM |  | 0 | 126 | 193 | 0 | 0 | 0 | 0 | 0 | 110 | 109 | 0 | 56 | 0 | 44 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 15 | 2 | 658 | 3,189 |
| 9:15 AM |  | 0 | 145 | 283 | 0 | 0 | 0 | 0 | 0 | 107 | 131 | 0 | 21 | 1 | 49 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 12 | 34 | 0 | 783 | 3,017 |
| 9:30 AM |  | 0 | 191 | 187 | 0 | 0 | 0 | 0 | 0 | 114 | 163 | 0 | 24 | 1 | 20 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 12 | 32 | 0 | 744 | 2,949 |
| 9:45 AM |  | 0 | 169 | 186 | 0 | 0 | 0 | 0 | 0 | 97 | 140 | 0 | 30 | 0 | 29 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 8 | 18 | 0 | 677 | 2,862 |
| Count Total |  | 0 | 1,819 | 2,255 | 0 | 0 | 0 | 0 | 0 | 1,505 | 1,447 | 0 | 755 | 18 | 592 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 71 | 179 | 5 | 8,646 | 0 |
| Peak Hour | All | 0 | 708 | 869 | 0 | 0 | 0 | 0 | 0 | 681 | 466 | 0 | 382 | 11 | 265 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 24 | 48 | 3 | 3,457 | 0 |
|  | HV | 0 | 4 | 12 | 0 | 0 | 0 | 0 | 0 | 13 | 13 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 44 | 0 |
|  | HV\% | - | 1\% | 1\% | - | - | - | - | - | 2\% | 3\% | - | 0\% | 9\% | 0\% | . | - | - | . | . | - | . | . | 0\% | 0\% | 0\% | 1\% | 0 |

.

| Interval Start | Heavy Vehicle Totals |  |  |  |  |  | Bicycles |  |  |  |  |  | Pedestrians (Crossing Leg) |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | EB | WB | NB | SB | NWB | Total | EB | WB | NB | SB | NWB | Total | East | West | North | South | Southeast | Total |
| 7:00 AM | 5 | 8 | 2 | 0 | 0 | 15 |  | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 3 | 0 | 0 | 3 |
| 7:15 AM | 6 | 7 | 1 | 0 | 0 | 14 | 2 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 1 | 1 | 2 |
| 7:30 AM | 4 | 2 | 0 | 0 | 0 | 6 | 0 | 2 | 0 | 0 | 0 | 2 | 0 | 0 | 2 | 1 | 1 | 4 |
| 7:45 AM | 5 | 9 | 0 | 0 | 0 | 14 | 1 | 2 | 0 | 0 | 0 | 3 | 0 | 0 | 1 | 0 | 0 | 1 |
| 8:00 AM | 2 | 8 | 0 | 0 | 0 | 10 | 3 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 4 | 4 | 4 | 12 |
| 8:15 AM | 3 | 6 | 1 | 0 | 0 | 10 | 2 | 2 | 0 | 0 | 0 | 4 | 0 | 0 | 6 | 3 | 3 | 12 |
| 8:30 AM | 6 | 3 | 1 | 0 | 0 | 10 | 3 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 1 | 3 | 3 | 7 |
| 8:45 AM | 6 | 9 | 1 | 0 | 0 | 16 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 1 | 1 | 7 |
| 9:00 AM | 5 | 8 | 1 | 0 | 0 | 14 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 6 | 6 | 13 |
| 9:15 AM | 5 | 7 | 0 | 0 | 0 | 12 | 2 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 1 | 5 | 5 | 11 |
| 9:30 AM | 9 | 4 | 1 | 0 | 0 | 14 | 2 | 3 | 0 | 0 | 0 | 5 | 0 | 0 | 6 | 2 | 2 | 10 |
| 9:45 AM | 5 | 7 | 0 | 0 | 1 | 13 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 4 | 4 | 10 |
| Count Total | 61 | 78 | 8 | 0 | 1 | 148 | 16 | 9 | 1 | 0 | 0 | 26 | 0 | 0 | 32 | 30 | 30 | 92 |
| Peak Hr | 16 | 26 | 2 | 0 | 0 | 44 | 9 | 4 | 0 | 0 | 0 | 13 | 0 | 0 | 12 | 10 | 10 | 32 |

Three-Hour Count Summaries - Heavy Vehicles

| Interval Start | Stevens Creek Blvd |  |  |  |  | Stevens Creek Blvd |  |  |  |  | SR-85 NB Off Ramp |  |  |  |  | SR-85 NB On Ramp |  |  |  |  | Campus Dr |  |  |  |  | 15-min Total | $\begin{array}{\|c\|} \hline \text { Rolling } \\ \text { One } \\ \text { Hour } \end{array}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Eastbound |  |  |  |  | Westbound |  |  |  |  | Northbound |  |  |  |  | Southbound |  |  |  |  | Northwestbound |  |  |  |  |  |  |
|  | UT | LT | TH | BR | RT | UT | HL | LT | TH | RT | UT | LT | TH | RT | HR | UT | LT | BL | TH | RT | UT | HL | BL | BR | HR |  |  |
| 7:00 AM | 0 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 3 | 5 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 15 | 0 |
| 7:15 AM | 0 | 1 | 5 | 0 | 0 | 0 | 0 | 0 | 3 | 4 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 14 | 0 |
| 7:30 AM | 0 | 1 | 3 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 | 0 |
| 7:45 AM | 0 | 2 | 3 | 0 | 0 | 0 | 0 | 0 | 5 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 14 | 49 |
| 8:00 AM | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 4 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 10 | 44 |
| 8:15 AM | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 2 | 4 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 10 | 40 |
| 8:30 AM | 0 | 1 | 5 | 0 | 0 | 0 | 0 | 0 | 2 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 10 | 44 |
| 8:45 AM | 0 | 5 | 1 | 0 | 0 | 0 | 0 | 0 | 4 | 5 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 16 | 46 |
| 9:00 AM | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 3 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 14 | 50 |
| 9:15 AM | 0 | 1 | 4 | 0 | 0 | 0 | 0 | 0 | 4 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 12 | 52 |
| 9:30 AM | 0 | 3 | 6 | 0 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 14 | 56 |
| 9:45 AM | 0 | 1 | 4 | 0 | 0 | 0 | 0 | 0 | 3 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 13 | 53 |
| Count Total | 0 | 21 | 40 | 0 | 0 | 0 | 0 | 0 | 38 | 40 | 0 | 5 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 148 | 0 |
| Peak Hour | 0 | 4 | 12 | 0 | 0 | 0 | 0 | 0 | 13 | 13 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 44 | 0 |

Three-Hour Count Summaries - Bikes

| Interval Start | Stevens Creek Blvd |  |  |  |  | Stevens Creek Blvd |  |  |  |  | SR-85 NB Off Ramp |  |  |  |  | SR-85 NB On Ramp |  |  |  |  | Campus Dr |  |  |  |  | $\begin{aligned} & \text { 15-min } \\ & \text { Total } \end{aligned}$ | $\begin{gathered} \text { Rolling } \\ \text { One } \\ \text { Hour } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Eastbound |  |  |  |  | Westbound |  |  |  |  | Northbound |  |  |  |  | Southbound |  |  |  |  | Northwestbound |  |  |  |  |  |  |
|  | UT | LT | TH | BR | RT | UT | HL | LT | TH | RT | UT | LT | TH | RT | HR | UT | LT | BL | TH | RT | UT | HL | BL | BR | HR |  |  |
| 7:00 AM | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |  |
| 7:15 AM | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 |
| 7:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 |
| 7:45 AM | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 8 |
| 8:00 AM | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 10 |
| 8:15 AM | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 12 |
| 8:30 AM | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 13 |
| 8:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 10 |
| 9:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 8 |
| 9:15 AM | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 6 |
| 9:30 AM | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 8 |
| 9:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 8 |
| Count Total | 0 | 0 | 16 | 0 | 0 | 0 | 0 | 0 | 9 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 26 | 0 |
| Peak Hour | 0 | 0 | 9 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 13 | 0 |

A2: Existing Conditions Synchro Outputs

|  | 4 | $\rightarrow$ | $4$ |  | 4 | $\dagger$ |  |  | $4$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | WBT | WBR | NBL | NBT | NBR | NWL | NWR |
| Lane Configurations | 7 | 444 | 坐坐 | 「 |  | \＄ | 「 | ＊ | 右 |
| Traffic Volume（vph） | 708 | 869 | 681 | 466 | 382 | 11 | 265 | 24 | 51 |
| Future Volume（vph） | 708 | 869 | 681 | 466 | 382 | 11 | 265 | 24 | 51 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time（s） | 6.0 | 6.0 | 6.0 | 6.0 |  | 6.0 | 6.0 | 6.0 | 6.0 |
| Lane Util．Factor | ＊0．83 | ＊1．00 | ＊1．00 | ＊0．92 |  | ＊0．92 | ＊0．92 | ＊0．92 | ＊1．00 |
| Frpb，ped／bikes | 1.00 | 1.00 | 1.00 | 0.98 |  | 1.00 | 1.00 | 1.00 | 1.00 |
| Flpb，ped／bikes | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt | 1.00 | 1.00 | 1.00 | 0.85 |  | 1.00 | 1.00 | 1.00 | 1.00 |
| Flt Protected | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 |
| Satd．Flow（prot） | 3123 | 5644 | 5588 | 1433 |  | 1731 | 1731 | 1748 | 1900 |
| Flt Permitted | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 |
| Satd．Flow（perm） | 3123 | 5644 | 5588 | 1433 |  | 1731 | 1731 | 1748 | 1900 |
| Peak－hour factor，PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj．Flow（vph） | 708 | 869 | 681 | 466 | 382 | 11 | 265 | 24 | 51 |
| RTOR Reduction（vph） | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Lane Group Flow（vph） | 708 | 869 | 681 | 466 | 0 | 420 | 238 | 39 | 36 |
| Confl．Peds．（\＃／hr） | 12 |  |  | 12 |  |  |  |  |  |
| Confl．Bikes（\＃／hr） |  |  |  | 4 |  |  |  |  |  |
| Heavy Vehicles（\％） | 1\％ | 1\％ | 2\％ | 2\％ | 1\％ | 1\％ | 1\％ | 0\％ | 0\％ |
| Turn Type | Prot | NA | NA | Free | Split | NA | Perm | Prot | Prot |
| Protected Phases | 7 | 4 | 8 |  | 2 | 2 |  | 1 | 1 |
| Permitted Phases |  |  |  | Free |  |  | 2 |  |  |
| Actuated Green，G（s） | 26.7 | 45.8 | 15.1 | 93.2 |  | 29.8 | 29.8 | 5.6 | 5.6 |
| Effective Green，g（s） | 24.7 | 43.8 | 13.1 | 93.2 |  | 27.8 | 27.8 | 3.6 | 3.6 |
| Actuated g／C Ratio | 0.27 | 0.47 | 0.14 | 1.00 |  | 0.30 | 0.30 | 0.04 | 0.04 |
| Clearance Time（s） | 4.0 | 4.0 | 4.0 |  |  | 4.0 | 4.0 | 4.0 | 4.0 |
| Vehicle Extension（s） | 3.0 | 3.0 | 3.0 |  |  | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap（vph） | 827 | 2652 | 785 | 1433 |  | 516 | 516 | 67 | 73 |
| v／s Ratio Prot | c0．23 | 0.15 | c0．12 |  |  | 0.24 |  | 0.02 | 0.02 |
| v／s Ratio Perm |  |  |  | c0．33 |  |  | 0.14 |  |  |
| v／c Ratio | 0.86 | 0.33 | 0.87 | 0.33 |  | 0.81 | 0.46 | 0.58 | 0.49 |
| Uniform Delay，d1 | 32.6 | 15.5 | 39.2 | 0.0 |  | 30.3 | 26.6 | 44.1 | 43.9 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay，d2 | 8.7 | 0.1 | 10.0 | 0.6 |  | 9.5 | 0.7 | 12.2 | 5.2 |
| Delay（s） | 41.2 | 15.5 | 49.2 | 0.6 |  | 39.8 | 27.3 | 56.3 | 49.1 |
| Level of Service | D | B | D | A |  | D | C | E | D |
| Approach Delay（s） |  | 27.1 | 29.4 |  |  | 35.3 |  | 52.8 |  |
| Approach LOS |  | C | C |  |  | D |  | D |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |
| HCM 2000 Control Delay |  |  | 30.0 |  | M 2000 | evel of | ervice |  | C |
| HCM 2000 Volume to Capacity ratio |  |  | 0.84 |  |  |  |  |  |  |
| Actuated Cycle Length（s） |  |  | 93.2 |  | of los | me（s） |  |  | 24.0 |
| Intersection Capacity Utilization |  |  | 101．6\％ |  | Level | Service |  |  | G |
| Analysis Period（min） |  |  | 15 |  |  |  |  |  |  |
| c Critical Lane Group |  |  |  |  |  |  |  |  |  |


|  | 4 | $\rightarrow$ | $4$ |  | 4 | $\dagger$ |  |  | $4$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | WBT | WBR | NBL | NBT | NBR | NWL | NWR |
| Lane Configurations | ${ }^{7 \%}$ | 444 | 444 | 「 |  | \＄ | 「 | ＊ | 鹿 |
| Traffic Volume（vph） | 534 | 1680 | 547 | 447 | 146 | 2 | 289 | 48 | 126 |
| Future Volume（vph） | 534 | 1680 | 547 | 447 | 146 | 2 | 289 | 48 | 126 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time（s） | 7.0 | 7.0 | 7.0 | 6.0 |  | 7.0 | 7.0 | 7.0 | 7.0 |
| Lane Util．Factor | ＊0．83 | ＊1．00 | ＊1．00 | ＊0．92 |  | ＊0．92 | ＊0．92 | ＊0．92 | ＊1．00 |
| Frpb，ped／bikes | 1.00 | 1.00 | 1.00 | 0.98 |  | 1.00 | 1.00 | 1.00 | 1.00 |
| Flpb，ped／bikes | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt | 1.00 | 1.00 | 1.00 | 0.85 |  | 1.00 | 1.00 | 1.00 | 1.00 |
| Flt Protected | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 |
| Satd．Flow（prot） | 3123 | 5644 | 5588 | 1434 |  | 1731 | 1731 | 1748 | 1900 |
| Flt Permitted | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 |
| Satd．Flow（perm） | 3123 | 5644 | 5588 | 1434 |  | 1731 | 1731 | 1748 | 1900 |
| Peak－hour factor，PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj．Flow（vph） | 534 | 1680 | 547 | 447 | 146 | 2 | 289 | 48 | 126 |
| RTOR Reduction（vph） | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Lane Group Flow（vph） | 534 | 1680 | 547 | 447 | 0 | 226 | 211 | 90 | 84 |
| Confl．Peds．（\＃／hr） | 6 |  |  | 6 |  |  |  |  |  |
| Confl．Bikes（\＃／hr） |  |  |  | 7 |  |  |  |  |  |
| Heavy Vehicles（\％） | 1\％ | 1\％ | 2\％ | 2\％ | 1\％ | 1\％ | 1\％ | 0\％ | 0\％ |
| Turn Type | Prot | NA | NA | Free | Split | NA | Perm | Prot | Prot |
| Protected Phases | 7 | 4 | 8 |  | 2 | 2 |  | 1 | 1 |
| Permitted Phases |  |  |  | Free |  |  | 2 |  |  |
| Actuated Green，G（s） | 21.6 | 42.5 | 15.9 | 87.6 |  | 18.2 | 18.2 | 11.9 | 11.9 |
| Effective Green，g（s） | 19.6 | 40.5 | 13.9 | 87.6 |  | 16.2 | 16.2 | 9.9 | 9.9 |
| Actuated g／C Ratio | 0.22 | 0.46 | 0.16 | 1.00 |  | 0.18 | 0.18 | 0.11 | 0.11 |
| Clearance Time（s） | 5.0 | 5.0 | 5.0 |  |  | 5.0 | 5.0 | 5.0 | 5.0 |
| Vehicle Extension（s） | 3.0 | 3.0 | 3.0 |  |  | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap（vph） | 698 | 2609 | 886 | 1434 |  | 320 | 320 | 197 | 214 |
| v／s Ratio Prot | 0.17 | c0．30 | 0.10 |  |  | c0．13 |  | 0.05 | 0.04 |
| v／s Ratio Perm |  |  |  | c0．31 |  |  | 0.12 |  |  |
| v／c Ratio | 0.77 | 0.64 | 0.62 | 0.31 |  | 0.71 | 0.66 | 0.46 | 0.39 |
| Uniform Delay，d1 | 31.8 | 18.0 | 34.4 | 0.0 |  | 33.5 | 33.1 | 36.3 | 36.1 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay，d2 | 5.0 | 0.6 | 1.3 | 0.6 |  | 6.9 | 4.9 | 1.7 | 1.2 |
| Delay（s） | 36.8 | 18.6 | 35.7 | 0.6 |  | 40.4 | 38.0 | 38.0 | 37.2 |
| Level of Service | D | B | D | A |  | D | D | D | D |
| Approach Delay（s） |  | 23.0 | 19.9 |  |  | 39.2 |  | 37.6 |  |
| Approach LOS |  | C | B |  |  | D |  | D |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |
| HCM 2000 Control Delay |  |  | 24.7 |  | 2000 | evel of | ervice |  | C |
| HCM 2000 Volume to Capacity ratio |  |  | 0.72 |  |  |  |  |  |  |
| Actuated Cycle Length（s） |  |  | 87.6 |  | of los | me（s） |  |  | 28.0 |
| Intersection Capacity Utilization |  |  | 88．5\％ |  | Level | Service |  |  | E |
| Analysis Period（min） |  |  | 15 |  |  |  |  |  |  |
| c Critical Lane Group |  |  |  |  |  |  |  |  |  |

## Kimley»)Horn

## A3: Existing Plus Westport and Signal Conditions Synchro Outputs

Intersection: 2: NORTHBOUND SR 85 RAMPS \& DE ANZA COLLEGE DWY \& STEVENS CREEK BLVD

| Movement | EB | EB | EB | EB | EB | WB | WB | WB | WB | B19 | B19 | NB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Directions Served | L | L | T | T | T | T | T | T | R | T | T | LTR |
| Maximum Queue ( ft ) | 358 | 360 | 175 | 176 | 201 | 125 | 223 | 208 | 245 | 13 | 57 | 514 |
| Average Queue (ft) | 286 | 295 | 78 | 74 | 84 | 42 | 109 | 91 | 93 | 1 | 3 | 485 |
| 95th Queue (ft) | 396 | 402 | 147 | 149 | 163 | 99 | 199 | 181 | 220 | 8 | 27 | 591 |
| Link Distance (t) | 346 | 346 | 346 | 346 | 346 | 176 | 176 | 176 | 176 | 591 | 591 | 436 |
| Upstream BIk Time (\%) | 8 | 11 |  |  |  |  | 2 | 1 | 3 |  |  | 68 |
| Queuing Penalty (veh) | 33 | 44 |  |  |  |  | 7 | 3 | 8 |  |  | 0 |
| Storage Bay Dist (tt) |  |  |  |  |  |  |  |  |  |  |  |  |
| Storage BIk Time (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |  |  |  |  |  |

Intersection: 2: NORTHBOUND SR 85 RAMPS \& DE ANZA COLLEGE DWY \& STEVENS CREEK BLVD

| Movement | NB | B27 | NW | NW |
| :--- | ---: | ---: | ---: | ---: |
| Directions Served | R | T | LR | R |
| Maximum Queue (ft) | 485 | 601 | 74 | 65 |
| Average Queue (ft) | 234 | 433 | 43 | 19 |
| 95th Queue (ft) | 483 | 812 | 81 | 53 |
| Link Distance (ft) | 436 | 559 | 69 | 69 |
| Upstream Blk Time (\%) | 1 | 57 | 7 | 1 |
| Queuing Penalty (veh) | 0 | 0 | 4 | 0 |
| Storage Bay Dist (ft) |  |  |  |  |
| Storage Blk Time (\%) |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |


|  | 4 | $\rightarrow$ | $4$ |  | 4 |  |  |  | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | WBT | WBR | NBL | NBT | NBR | NWL | NWR |
| Lane Configurations | 17 | 侎4 | 侎4 | 「 |  | \＆ | F＇ | ＊ | 「 |
| Traffic Volume（vph） | 708 | 875 | 697 | 490 | 382 | 11 | 267 | 24 | 51 |
| Future Volume（vph） | 708 | 875 | 697 | 490 | 382 | 11 | 267 | 24 | 51 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time（s） | 6.0 | 6.0 | 6.0 | 6.0 |  | 6.0 | 6.0 | 6.0 | 6.0 |
| Lane Util．Factor | ＊0．83 | ＊1．00 | ＊1．00 | ＊0．92 |  | ＊0．92 | ＊0．92 | ＊0．92 | ＊1．00 |
| Frpb，ped／bikes | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 |
| Flpb，ped／bikes | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt | 1.00 | 1.00 | 1.00 | 0.85 |  | 1.00 | 1.00 | 1.00 | 1.00 |
| Flt Protected | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 |
| Satd．Flow（prot） | 3123 | 5644 | 5588 | 1457 |  | 1731 | 1731 | 1748 | 1900 |
| Flt Permitted | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 |
| Satd．Flow（perm） | 3123 | 5644 | 5588 | 1457 |  | 1731 | 1731 | 1748 | 1900 |
| Peak－hour factor，PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj．Flow（vph） | 708 | 875 | 697 | 490 | 382 | 11 | 267 | 24 | 51 |
| RTOR Reduction（vph） | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Lane Group Flow（vph） | 708 | 875 | 697 | 490 | 0 | 420 | 240 | 39 | 36 |
| Confl．Peds．（\＃／hr） | 12 |  |  | 12 |  |  |  |  |  |
| Confl．Bikes（\＃／hr） |  |  |  | 5 |  |  |  |  |  |
| Heavy Vehicles（\％） | 1\％ | 1\％ | 2\％ | 2\％ | 1\％ | 1\％ | 1\％ | 0\％ | 0\％ |
| Turn Type | Prot | NA | NA | custom | Split | NA | Prot | Prot | Prot |
| Protected Phases | 1！ | 6 | 2 | 178 ！ | 8 | $8!$ | 8 | 7 | $7!$ |
| Permitted Phases |  |  |  |  |  |  |  |  |  |
| Actuated Green，G（s） | 22.1 | 44.8 | 18.7 | 59.2 |  | 23.1 | 23.1 | 6.0 | 6.0 |
| Effective Green，g（s） | 20.1 | 42.8 | 16.7 | 57.2 |  | 21.1 | 21.1 | 4.0 | 4.0 |
| Actuated g／C Ratio | 0.23 | 0.50 | 0.19 | 0.67 |  | 0.25 | 0.25 | 0.05 | 0.05 |
| Clearance Time（s） | 4.0 | 4.0 | 4.0 |  |  | 4.0 | 4.0 | 4.0 | 4.0 |
| Vehicle Extension（s） | 3.0 | 3.0 | 3.0 |  |  | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap（vph） | 730 | 2812 | 1086 | 970 |  | 425 | 425 | 81 | 88 |
| v／s Ratio Prot | c0．23 | 0.16 | c0．12 | c0．34 |  | c0．24 | 0.14 | 0.02 | 0.02 |
| v／s Ratio Perm |  |  |  |  |  |  |  |  |  |
| v／c Ratio | 0.97 | 0.31 | 0.64 | 0.51 |  | 0.99 | 0.56 | 0.48 | 0.41 |
| Uniform Delay，d1 | 32.6 | 12.8 | 31.8 | 7.2 |  | 32.3 | 28.4 | 39.9 | 39.8 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay，d2 | 25.7 | 0.1 | 1.3 | 0.4 |  | 40.1 | 1.7 | 4.5 | 3.1 |
| Delay（s） | 58.3 | 12.9 | 33.2 | 7.6 |  | 72.4 | 30.1 | 44.4 | 42.9 |
| Level of Service | E | B | C | A |  | E | C | D | D |
| Approach Delay（s） |  | 33.2 | 22.6 |  |  | 57.0 |  | 43.7 |  |
| Approach LOS |  | C | C |  |  | E |  | D |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |
| HCM 2000 Control Delay |  |  | 34.3 |  | M 2000 | evel of | rvice |  | C |
| HCM 2000 Volume to Capacity ratio |  |  | 0.89 |  |  |  |  |  |  |
| Actuated Cycle Length（s） |  |  | 85.9 |  | of los | me（s） |  |  | 24.0 |
| Intersection Capacity Utilization |  |  | 103．1\％ |  | Level | Service |  |  | G |
| Analysis Period（min） |  |  | 15 |  |  |  |  |  |  |
| ！Phase conflict between lane groups． |  |  |  |  |  |  |  |  |  |
| c Critical Lane Group |  |  |  |  |  |  |  |  |  |

Intersection: 2: NORTHBOUND SR 85 RAMPS \& DE ANZA COLLEGE DWY \& STEVENS CREEK BLVD

| Movement | EB | EB | EB | EB | EB | WB | WB | WB | WB | B19 | B19 | NB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | L | T | T | T | T | T | T | R | T | T | LTR |
| Maximum Queue (ft) | 264 | 276 | 280 | 257 | 251 | 125 | 200 | 167 | 248 | 40 | 82 | 246 |
| Average Queue (ft) | 167 | 163 | 165 | 149 | 141 | 33 | 79 | 52 | 102 | 1 | 5 | 154 |
| 95th Queue (ft) | 253 | 262 | 250 | 240 | 233 | 89 | 171 | 125 | 243 | 32 | 38 | 224 |
| Link Distance (ft) | 346 | 346 | 346 | 346 | 346 | 176 | 176 | 176 | 176 | 591 | 591 | 436 |
| Upstream Blk Time (\%) |  |  | 0 |  |  | 0 | 1 | 0 | 4 |  |  |  |
| Queuing Penalty (veh) |  |  | 0 |  |  | 0 | 3 | 0 | 10 |  |  |  |
| Storage Bay Dist (ft) |  |  |  |  |  |  |  |  |  |  |  |  |
| Storage Blk Time (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |  |  |  |  |  |

Intersection: 2: NORTHBOUND SR 85 RAMPS \& DE ANZA COLLEGE DWY \& STEVENS CREEK BLVD

| Movement | NB | NW | NW |
| :--- | ---: | ---: | ---: |
| Directions Served | R | LR | R |
| Maximum Queue (ft) | 191 | 91 | 78 |
| Average Queue (ft) | 97 | 66 | 41 |
| 95th Queue (ft) | 171 | 89 | 77 |
| Link Distance (ft) | 436 | 69 | 69 |
| Upstream Blk Time (\%) |  | 30 | 5 |
| Queuing Penalty (veh) |  | 15 | 2 |
| Storage Bay Dist (ft) |  |  |  |
| Storage Blk Time (\%) |  |  |  |


|  | 4 | － |  |  | $4$ | 9 | $p$ |  | $4$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | WBT | WBR | NBL | NBT | NBR | NWL | NWR |
| Lane Configurations | ${ }^{1 / 1}$ | 444 | 性4 | 「＇ |  | \＆ | 「 | M | 「＇ |
| Traffic Volume（vph） | 534 | 1697 | 549 | 451 | 146 | 2 | 294 | 48 | 126 |
| Future Volume（vph） | 534 | 1697 | 549 | 451 | 146 | 2 | 294 | 48 | 126 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time（s） | 6.0 | 6.0 | 6.0 | 6.0 |  | 6.0 | 6.0 | 6.0 | 6.0 |
| Lane Util．Factor | ＊0．83 | ＊1．00 | ＊1．00 | ＊0．92 |  | ＊0．92 | ＊0．92 | ＊0．92 | ＊1．00 |
| Frpb，ped／bikes | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 |
| Flpb，ped／bikes | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt | 1.00 | 1.00 | 1.00 | 0.85 |  | 1.00 | 1.00 | 1.00 | 1.00 |
| Flt Protected | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 |
| Satd．Flow（prot） | 3123 | 5644 | 5588 | 1457 |  | 1731 | 1731 | 1748 | 1900 |
| Flt Permitted | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 |
| Satd．Flow（perm） | 3123 | 5644 | 5588 | 1457 |  | 1731 | 1731 | 1748 | 1900 |
| Peak－hour factor，PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj．Flow（vph） | 534 | 1697 | 549 | 451 | 146 | 2 | 294 | 48 | 126 |
| RTOR Reduction（vph） | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Lane Group Flow（vph） | 534 | 1697 | 549 | 451 | 0 | 230 | 212 | 90 | 84 |
| Confl．Peds．（\＃／hr） | 8 |  |  | 8 |  |  |  |  |  |
| Confl．Bikes（\＃／hr） |  |  |  | 9 |  |  |  |  |  |
| Heavy Vehicles（\％） | 1\％ | 1\％ | 2\％ | 2\％ | 1\％ | 1\％ | 1\％ | 0\％ | 0\％ |
| Turn Type | Prot | NA | NA | custom | Split | NA | Prot | Prot | Prot |
| Protected Phases | $1!$ | 6 | 2 | 178 ！ | 8 | $8!$ | 8 | 7 | $7!$ |
| Permitted Phases |  |  |  |  |  |  |  |  |  |
| Actuated Green，G（s） | 16.4 | 38.0 | 17.6 | 46.9 |  | 16.3 | 16.3 | 6.2 | 6.2 |
| Effective Green，g（s） | 14.4 | 36.0 | 15.6 | 44.9 |  | 14.3 | 14.3 | 4.2 | 4.2 |
| Actuated g／C Ratio | 0.20 | 0.50 | 0.22 | 0.62 |  | 0.20 | 0.20 | 0.06 | 0.06 |
| Clearance Time（s） | 4.0 | 4.0 | 4.0 |  |  | 4.0 | 4.0 | 4.0 | 4.0 |
| Vehicle Extension（s） | 3.0 | 3.0 | 3.0 |  |  | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap（vph） | 620 | 2802 | 1202 | 902 |  | 341 | 341 | 101 | 110 |
| v／s Ratio Prot | c0．17 | c0．30 | 0.10 | c0．31 |  | 0.13 | 0.12 | 0.05 | 0.04 |
| v／s Ratio Perm |  |  |  |  |  |  |  |  |  |
| v／c Ratio | 0.86 | 0.61 | 0.46 | 0.50 |  | 0.67 | 0.62 | 0.89 | 0.76 |
| Uniform Delay，d1 | 28.1 | 13.1 | 24.8 | 7.6 |  | 26.9 | 26.6 | 33.9 | 33.7 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay，d2 | 11.8 | 0.4 | 0.3 | 0.4 |  | 5.2 | 3.5 | 56.0 | 26.4 |
| Delay（s） | 39.9 | 13.5 | 25.0 | 8.0 |  | 32.1 | 30.1 | 90.0 | 60.1 |
| Level of Service | D | B | C | A |  | C | C | F | E |
| Approach Delay（s） |  | 19.8 | 17.4 |  |  | 31.2 |  | 75.5 |  |
| Approach LOS |  | B | B |  |  | C |  | E |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |
| HCM 2000 Control Delay |  |  | 23.0 |  | CM 2000 | evel of | ervice |  | C |
| HCM 2000 Volume to Ca | ratio |  | 0.77 |  |  |  |  |  |  |
| Actuated Cycle Length（s） |  |  | 72.5 |  | $m$ of los | me（s） |  |  | 24.0 |
| Intersection Capacity Util |  |  | 83．4\％ |  | Level | Service |  |  | E |
| Analysis Period（min） |  |  | 15 |  |  |  |  |  |  |
| ！Phase conflict between lane groups． |  |  |  |  |  |  |  |  |  |
| c Critical Lane Group |  |  |  |  |  |  |  |  |  |

A4: Cumulative Conditions Synchro Outputs



## Kimley»)Horn

A5: Cumulative Plus Westport and Signal Conditions Synchro Outputs

Intersection: 2: NORTHBOUND SR 85 RAMPS \& DE ANZA COLLEGE DWY \& STEVENS CREEK BLVD

| Movement | EB | EB | EB | EB | EB | WB | WB | WB | WB | B19 | B19 | B19 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | L | T | T | T | T | T | T | R | T | T | T |
| Maximum Queue (ft) | 361 | 359 | 354 | 369 | 363 | 207 | 234 | 224 | 242 | 118 | 23 | 107 |
| Average Queue (ft) | 320 | 322 | 217 | 227 | 227 | 88 | 141 | 116 | 104 | 8 | 1 | 7 |
| 95th Queue (ft) | 426 | 417 | 358 | 385 | 390 | 178 | 229 | 208 | 246 | 55 | 15 | 51 |
| Link Distance (ft) | 346 | 346 | 346 | 346 | 346 | 166 | 166 | 166 | 166 | 591 | 591 | 591 |
| Upstream Blk Time (\%) | 19 | 18 | 0 | 1 | 2 | 3 | 9 | 4 | 4 |  |  |  |
| Queuing Penalty (veh) | 104 | 97 | 2 | 7 | 12 | 9 | 27 | 11 | 14 |  |  |  |
| Storage Bay Dist (ft) |  |  |  |  |  |  |  |  |  |  |  |  |
| Storage Blk Time (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |  |  |  |  |  |

Intersection: 2: NORTHBOUND SR 85 RAMPS \& DE ANZA COLLEGE DWY \& STEVENS CREEK BLVD

| Movement | NB | NB | B27 | NW | NW |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Directions Served | LTR | R | T | LR | R> |
| Maximum Queue (ft) | 521 | 433 | 594 | 66 | 77 |
| Average Queue (ft) | 505 | 234 | 543 | 42 | 55 |
| 95th Queue (ft) | 518 | 419 | 694 | 73 | 85 |
| Link Distance (ft) | 436 | 436 | 559 | 58 | 58 |
| Upstream BIk Time (\%) | 66 | 0 | 57 | 11 | 25 |
| Queuing Penalty (veh) | 0 | 0 | 0 | 6 | 13 |
| Storage Bay Dist (ft) |  |  |  |  |  |
| Storage Blk Time (\%) |  |  |  |  |  |


|  | 4 | $\rightarrow$ |  |  | $4$ | 4 |  |  | $4$ | $\stackrel{+}{ }$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | WBT | WBR | NBL | NBT | NBR | NWL | NWR | NWR2 |
| Lane Configurations | \％ | 444 | 个44 | F |  | \＆ | 「 | ＊ | 「 |  |
| Traffic Volume（vph） | 904 | 1529 | 703 | 575 | 455 | 49 | 395 | 4 | 84 | 47 |
| Future Volume（vph） | 904 | 1529 | 703 | 575 | 455 | 49 | 395 | 4 | 84 | 47 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time（s） | 6.0 | 6.0 | 6.0 | 6.0 |  | 6.0 | 6.0 | 6.0 | 6.0 |  |
| Lane Util．Factor | ＊0．83 | ＊1．00 | ＊1．00 | ＊0．92 |  | ＊0．92 | ＊0．92 | ＊0．92 | ＊1．00 |  |
| Frpb，ped／bikes | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Flpb，ped／bikes | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Frt | 1.00 | 1.00 | 1.00 | 0.85 |  | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Flt Protected | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Satd．Flow（prot） | 3123 | 5644 | 5588 | 1457 |  | 1731 | 1731 | 1748 | 1900 |  |
| Flt Permitted | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Satd．Flow（perm） | 3123 | 5644 | 5588 | 1457 |  | 1731 | 1731 | 1748 | 1900 |  |
| Peak－hour factor，PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj．Flow（vph） | 904 | 1529 | 703 | 575 | 455 | 49 | 395 | 4 | 84 | 47 |
| RTOR Reduction（vph） | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Lane Group Flow（vph） | 904 | 1529 | 703 | 575 | 0 | 544 | 355 | 68 | 67 | 0 |
| Confl．Peds．（\＃／hr） | 12 |  |  | 12 |  |  |  |  |  |  |
| Confl．Bikes（\＃／hr） |  |  |  | 5 |  |  |  |  |  |  |
| Heavy Vehicles（\％） | 1\％ | 1\％ | 2\％ | 2\％ | 1\％ | 1\％ | 1\％ | 0\％ | 0\％ | 0\％ |
| Turn Type | Prot | NA | NA | custom | Split | NA | Prot | Prot | Prot |  |
| Protected Phases | $1!$ | 6 | 2 | 178 ！ | 8 | $8!$ | 8 | 7 | $7!$ |  |
| Permitted Phases |  |  |  |  |  |  |  |  |  |  |
| Actuated Green，G（s） | 40.1 | 68.9 | 24.8 | 98.2 |  | 43.1 | 43.1 | 7.0 | 7.0 |  |
| Effective Green，g（s） | 38.1 | 66.9 | 22.8 | 96.2 |  | 41.1 | 41.1 | 5.0 | 5.0 |  |
| Actuated g／C Ratio | 0.29 | 0.51 | 0.17 | 0.73 |  | 0.31 | 0.31 | 0.04 | 0.04 |  |
| Clearance Time（s） | 4.0 | 4.0 | 4.0 |  |  | 4.0 | 4.0 | 4.0 | 4.0 |  |
| Vehicle Extension（s） | 3.0 | 3.0 | 3.0 |  |  | 3.0 | 3.0 | 3.0 | 3.0 |  |
| Lane Grp Cap（vph） | 908 | 2882 | 972 | 1069 |  | 543 | 543 | 66 | 72 |  |
| v／s Ratio Prot | c0．29 | 0.27 | c0．13 | 0.39 |  | c0．31 | 0.21 | c0．04 | 0.04 |  |
| v／s Ratio Perm |  |  |  |  |  |  |  |  |  |  |
| v／c Ratio | 1.00 | 0.53 | 0.72 | 0.54 |  | 1.00 | 0.65 | 1.03 | 0.93 |  |
| Uniform Delay，d1 | 46.4 | 21.5 | 51.1 | 7.6 |  | 45.0 | 38.8 | 63.0 | 62.8 |  |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Incremental Delay，d2 | 28.6 | 0.2 | 2.7 | 0.5 |  | 39.1 | 2.8 | 119.5 | 82.0 |  |
| Delay（s） | 75.0 | 21.7 | 53.8 | 8.2 |  | 84.0 | 41.6 | 182.5 | 144.9 |  |
| Level of Service | E | C | D | A |  | F | D | F | F |  |
| Approach Delay（s） |  | 41.5 | 33.3 |  |  | 67.3 |  | 163.8 |  |  |
| Approach LOS |  | D | C |  |  | E |  | F |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |
| HCM 2000 Control Delay |  |  | 47.6 |  | CM 2000 | evel of | ervice |  | D |  |
| HCM 2000 Volume to Capacity ratio |  |  | 0.94 |  |  |  |  |  |  |  |
| Actuated Cycle Length（s） |  |  | 131.0 |  | m of los | ime（s） |  |  | 24.0 |  |
| Intersection Capacity Utilization |  |  | 123．9\％ |  | U Level | Service |  |  | H |  |
| Analysis Period（min） |  |  | 15 |  |  |  |  |  |  |  |
| ！Phase conflict between lane groups． |  |  |  |  |  |  |  |  |  |  |
| c Critical Lane Group |  |  |  |  |  |  |  |  |  |  |

Intersection: 2: NORTHBOUND SR 85 RAMPS \& DE ANZA COLLEGE DWY \& STEVENS CREEK BLVD

| Movement | EB | EB | EB | EB | EB | WB | WB | WB | WB | B19 | B19 | B19 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | L | T | T | T | T | T | T | R | T | T | T |
| Maximum Queue (ft) | 334 | 331 | 299 | 308 | 292 | 228 | 204 | 209 | 265 | 39 | 8 | 188 |
| Average Queue ( ft$)$ | 197 | 205 | 159 | 142 | 140 | 85 | 93 | 81 | 155 | 1 | 0 | 20 |
| 95th Queue (ft) | 312 | 321 | 278 | 264 | 257 | 174 | 182 | 170 | 284 | 19 | 6 | 100 |
| Link Distance (ft) | 346 | 346 | 346 | 346 | 346 | 176 | 176 | 176 | 176 | 591 | 591 | 591 |
| Upstream Blk Time (\%) | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 8 |  |  |  |
| Queuing Penalty (veh) | 2 | 1 | 0 | 0 | 0 | 3 | 5 | 3 | 30 |  |  |  |
| Storage Bay Dist (ft) |  |  |  |  |  |  |  |  |  |  |  |  |
| Storage Bk Time (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |  |  |  |  |  |

Intersection: 2: NORTHBOUND SR 85 RAMPS \& DE ANZA COLLEGE DWY \& STEVENS CREEK BLVD

| Movement | NB | NB | B27 | NW | NW |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Directions Served | LTR | R | T | LR | R |
| Maximum Queue (ft) | 336 | 243 | 96 | 61 | 41 |
| Average Queue (ft) | 178 | 91 | 12 | 20 | 3 |
| 95th Queue (ft) | 318 | 195 | 121 | 55 | 21 |
| Link Distance (ft) | 436 | 436 | 559 | 69 | 69 |
| Upstream Blk Time (\%) | 3 |  | 0 | 0 | 0 |
| Queuing Penalty (veh) | 0 |  | 0 | 0 | 0 |
| Storage Bay Dist (ft) |  |  |  |  |  |


|  | 4 |  |  |  | $4$ | 4 | $p$ |  | $4$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | WBT | WBR | NBL | NBT | NBR | NWL | NWR |
| Lane Configurations | ${ }^{1 / 1}$ | 4坐 | 种4 | 「 |  | \＄ | 「 | ＊ | F |
| Traffic Volume（vph） | 567 | 1589 | 781 | 584 | 200 | 4 | 239 | 11 | 9 |
| Future Volume（vph） | 567 | 1589 | 781 | 584 | 200 | 4 | 239 | 11 | 9 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time（s） | 6.0 | 6.0 | 6.0 | 6.0 |  | 6.0 | 6.0 | 6.0 | 6.0 |
| Lane Util．Factor | ＊0．83 | ＊1．00 | ＊1．00 | ＊0．92 |  | ＊0．92 | ＊0．92 | ＊0．92 | ＊1．00 |
| Frpb，ped／bikes | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 |
| Flpb，ped／bikes | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt | 1.00 | 1.00 | 1.00 | 0.85 |  | 1.00 | 1.00 | 1.00 | 1.00 |
| Flt Protected | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 |
| Satd．Flow（prot） | 3123 | 5644 | 5588 | 1457 |  | 1731 | 1731 | 1748 | 1900 |
| Flt Permitted | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 |
| Satd．Flow（perm） | 3123 | 5644 | 5588 | 1457 |  | 1731 | 1731 | 1748 | 1900 |
| Peak－hour factor，PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj．Flow（vph） | 567 | 1589 | 781 | 584 | 200 | 4 | 239 | 11 | 9 |
| RTOR Reduction（vph） | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Lane Group Flow（vph） | 567 | 1589 | 781 | 584 | 0 | 233 | 210 | 12 | 8 |
| Confl．Peds．（\＃／hr） | 8 |  |  | 8 |  |  |  |  |  |
| Confl．Bikes（\＃／hr） |  |  |  | 9 |  |  |  |  |  |
| Heavy Vehicles（\％） | 1\％ | 1\％ | 2\％ | 2\％ | 1\％ | 1\％ | 1\％ | 0\％ | 0\％ |
| Turn Type | Prot | NA | NA | custom | Split | NA | Prot | Prot | Prot |
| Protected Phases | $1!$ | 6 | 2 | 178 ！ | 8 | $8!$ | 8 | 7 | $7!$ |
| Permitted Phases |  |  |  |  |  |  |  |  |  |
| Actuated Green，G（s） | 16.2 | 39.4 | 19.2 | 48.9 |  | 18.6 | 18.6 | 6.1 | 6.1 |
| Effective Green，g（s） | 14.2 | 37.4 | 17.2 | 46.9 |  | 16.6 | 16.6 | 4.1 | 4.1 |
| Actuated g／C Ratio | 0.19 | 0.49 | 0.23 | 0.62 |  | 0.22 | 0.22 | 0.05 | 0.05 |
| Clearance Time（s） | 4.0 | 4.0 | 4.0 |  |  | 4.0 | 4.0 | 4.0 | 4.0 |
| Vehicle Extension（s） | 3.0 | 3.0 | 3.0 |  |  | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap（vph） | 582 | 2773 | 1262 | 897 |  | 377 | 377 | 94 | 102 |
| v／s Ratio Prot | c0．18 | c0．28 | 0.14 | c0．40 |  | 0.13 | 0.12 | 0.01 | 0.00 |
| v／s Ratio Perm |  |  |  |  |  |  |  |  |  |
| v／c Ratio | 0.97 | 0.57 | 0.62 | 0.65 |  | 0.62 | 0.56 | 0.13 | 0.08 |
| Uniform Delay，d1 | 30.8 | 13.7 | 26.5 | 9.4 |  | 26.9 | 26.5 | 34.3 | 34.2 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay，d2 | 30.6 | 0.3 | 0.9 | 1.7 |  | 3.0 | 1.8 | 0.6 | 0.3 |
| Delay（s） | 61.4 | 14.0 | 27.4 | 11.1 |  | 29.9 | 28.3 | 34.9 | 34.5 |
| Level of Service | E | B | C | B |  | C | C | C | C |
| Approach Delay（s） |  | 26.4 | 20.4 |  |  | 29.1 |  | 34.8 |  |
| Approach LOS |  | C | C |  |  | C |  | C |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |
| HCM 2000 Control Delay |  |  | 24.7 |  | CM 2000 | evel of | ervice |  | C |
| HCM 2000 Volume to Ca | ratio |  | 0.86 |  |  |  |  |  |  |
| Actuated Cycle Length（s） |  |  | 76.1 |  | $m$ of los | me（s） |  |  | 24.0 |
| Intersection Capacity Util |  |  | 93．5\％ |  | Level | Service |  |  | F |
| Analysis Period（min） |  |  | 15 |  |  |  |  |  |  |
| ！Phase conflict between lane groups． |  |  |  |  |  |  |  |  |  |
| c Critical Lane Group |  |  |  |  |  |  |  |  |  |


| $\begin{array}{\|l\|} \hline \text { Table } 1 \\ \text { Project } \end{array}$ |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TRIP GENERATION - WESTPORT |  |  |  |  |  |  |  |  |  |  |  |  |
| Land Uses |  | Project Size |  | WEEKDAY | AM PEAK HOUR |  |  |  | PM PEAK HOUR |  |  |  |
|  | Land Use Code |  |  | Daily Trips | Total Peak Hour | IN | I | OUT | Total Peak Hour | IN | I | OUT |
| Multifamily Housing (Low Rise) | 220 | - | Dwelling Unit(s) | 7.32 | 0.46 | 23\% | 1 | 77\% | 0.56 | 63\% | 1 | 37\% |
| Multifamily Housing (Mid-Rise) | 221 | - | Dwelling Unit(s) | 5.44 | 0.36 | 26\% | 1 | 74\% | 0.44 | 61\% | 1 | 39\% |
| Senior Adult Housing-Attached | 252 | - | Dwelling Unit(s) | 3.70 | 0.20 | 35\% | 1 | 65\% | 0.26 | 55\% | 1 | 45\% |
| Shopping Center | 820 | - | 1,000 Sq Ft GLA | 37.75 | 0.94 | 62\% | 1 | 38\% | 3.81 | 48\% | 1 | 52\% |
| Existing Conditions |  |  |  |  |  |  |  |  |  |  |  |  |
| Shopping Center (100\% Occupancy) | 820 | 71.254 | 1,000 Sq Ft GLA | 2690 | 67 | 42 | 1 | 25 | 271 | 130 | I | 141 |
| Shopping Center (85\% Occupancy) ${ }^{1}$ | 820 | 60.566 | 1,000 Sq Ft GLA | 2287 | 57 | 36 | 1 | 21 | 230 | 110 | 1 | 120 |
| Pass-By Trips for Shopping Center (PM $=34 \%$ ) ${ }^{3,4}$ |  |  |  | (78) | 0 | 0 | 1 | 0 | (78) | (37) |  | (41) |
| TOAL EXISTING TRIP CREDIT |  |  |  | 2209 | 57 | 36 | 1 | 21 | 152 | 73 | 1 | 79 |
| Proposed Conditions |  |  |  |  |  |  |  |  |  |  |  |  |
| Multifamily Housing (Low-Rise) | 220 | 88 | Dwelling Unit(s) | 646 | 40 | 9 | 1 | 31 | 49 | 31 | 1 | 18 |
| Multifamily Housing (Mid-Rise) | 221 | 115 | Dwelling Unit(s) | 626 | 41 | 11 | 1 | 30 | 51 | 31 | 1 | 20 |
| Senior Adult Housing-Attached | 252 | 39 | Dwelling Unit(s) | 146 | 8 | 3 | 1 | 5 | 10 | 6 | 1 | 4 |
| Shopping Center | 820 | 20.000 | 1,000 Sq Ft GLA | 756 | 19 | 12 | 1 | 7 | 76 | 36 | 1 | 40 |
| Gross Trips Generated before Internal Capture |  |  |  | 2,174 | 108 | 35 | 1 | 73 | 186 | 104 | 1 | 82 |
| Internal Capture Trips |  |  |  |  |  |  |  |  |  |  |  |  |
| Multifamily Housing (Low-Rise) | 220 | 88 | Dwelling Unit(s) | (44) | (1) | 0 | 1 | (1) | (6) | (4) |  | (2) |
| Multifamily Housing (Mid-Rise) | 221 | 115 | Dwelling Unit(s) | (42) | 0 | 0 | 1 | 0 | (7) | (5) |  | (2) |
| Senior Adult Housing-Attached | 252 | 39 | Dwelling Unit(s) | (10) | 0 | 0 | 1 | 0 | (1) | (1) | 1 | 0 |
| Shopping Center | 820 | 20.000 | 1,000 Sq Ft GLA | (90) | (1) | (1) | 1 | 0 | (14) | (4) |  | (10) |
| Internal Capture Reduction |  |  |  | (186) | (2) | (1) | 1 | (1) | (28) | (14) | 1 | (14) |
| Trip Reductions due to Internal Capture ${ }^{5}$ |  |  |  | 9\% | 2\% | 3\% | 1 | 1\% | 15\% | 13\% | 1 | 17\% |
| Additional Project Trip Reductions |  |  |  |  |  |  |  |  |  |  |  |  |
| VTA Major Bus Stop (Daily, AM, PM $=2 \%)^{2}$ <br> Pass-By Trips for Shopping Center (PM $=34 \%)^{3,4}$ |  |  |  | (28) | (2) | (1) | 1 |  | (2) | (1) |  |  |
|  |  |  |  | (26) | 0 | 0 |  | 0 | (26) | (12) |  |  |
| Project Trips |  |  |  | 1,934 | 104 | 33 | 1 | 71 | 130 | 77 | 1 | 53 |
| Existing Trip Credit |  |  |  | (2209) | (57) | (36) | 1 | (21) | (152) | (73) | 1 | (79) |
| Total Project Trips |  |  |  | 1934 | 104 | 33 | 1 |  | 130 | 77 | 1 | 53 |
| Net New Project Trips |  |  |  | (275) | 47 | (3) | I | 50 | (22) | 4 | 1 | (26) |
| Notes: <br> 1. Assume current retail is $85 \%$ occupied <br> 2. Per VTA Transportation Impact Analysis guidelines, a $2 \%$ vehicle trip reduction for housing trips can be applied for a nearby major bus stop <br> 3. Pass-By trip reduction applied to shopping center PM peak hour trips and based on average rates from Appendix E ITE Trip Generation Handbook 3rd Edition <br> 4. Daily pass-by trips only represent PM peak hour pass-by trips because no daily pass-by trip is resented in the ITE Trip Generation Handbook. <br> 5. Trips reductions due to internal capture was calculated using NCHRP 684 methodology <br> 6. Trip generation land uses based on average rates from ITE Trip Generation 10th Edition |  |  |  |  |  |  |  |  |  |  |  |  |


[^0]:    ${ }^{1}$ Short term requirements based on City of Cupertino Municipal Code Chapter 19.124

