# TRAFFIC IMPACT ANALYSIS 

## FOR

## ORLAND TRUCK WASH / COMMERCIAL

Orland, CA

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# TRAFFIC IMPACT ANALYSIS FOR ORLAND TRUCK WASH / COMMERCIAL <br> Orland, CA 

## INTRODUCTION

This report summarizes KD Anderson \& Associates analysis of the potential traffic impacts associated with development of the Orland Truck Wash / Commercial properties involved in rezoning $5 \pm$ acres in the area of the County Road 13 / Commerce Lane (County Road HH) intersection in western Orland. The project site is located south of Newville Road and west of Interstate 5 near the Flying J Travel Stop as noted in Figure 1.

The proposed project would create an area zoned for highway commercial, as well as a specific use catering to the trucking industry. Roughly two and one-quarter acres will be occupied by a Truck Wash. An adjoining 2.8 acres is designated for future highway commercial uses. As noted in Figure 2, access to the site is proposed via driveways on Commerce Lane (County Road HH), County Road 13, and County Road 14.

The purpose of this analysis is to identify the potential traffic-related impacts of the project within the context of current traffic conditions and to evaluate the cumulative impacts of the annexation within the context of future traffic conditions in the Orland area. This analysis includes evaluation of existing circulation conditions in the area based upon current weekday a.m. and p.m. peak hour traffic volumes. The extent to which improvements may already be needed to meet minimum standards has been determined. The characteristics of the proposed project have been determined based on probable peak hour and daily trip generation, regional trip distribution and local trip assignment. Forecasts of future year traffic conditions, including other development anticipated under the Orland General Plan have been analyzed with and without the proposed Re-Zone. Mitigation measures needed to ensure satisfactory operation of area intersections under each development scenario have been identified, and the project's fair share contribution at each location has been calculated.



## EXISTING SETTING

## Existing Street and Highway System

The proposed project will be served by several major roadways. Regional access is provided by Interstate 5 and State Route 32, which link the site with the other Northern California communities to the north and south and with the City of Orland to the east. Local access to the project site is provided via Newville Road and County Road HH. The following is a description of these facilities, as well as other roadways in the area of the project site.

Interstate 5 (I-5) is a north-south four-lane freeway that adjoins western Orland. Interstate 5 is the primary route through California and begins at the US-Mexico border in southern California and extends northerly to the California-Oregon border. Access to Interstate 5 is controlled and in the area of the project interchanges at South Street (County Road 16) and at SR 32-Newville Road are available. The most recent traffic volume counts published by Caltrans indicate that I-5 carried an Annual Average Daily Traffic (AADT) volume of 28,000 to 27,000 vehicles per day through the City of Orland. Trucks comprise $29 \%$ of the daily volume south of SR 32 and $25 \%$ north of SR 32 according to Caltrans data.

State Route 32 is an east-west route that connects with I-5 in Orland and SR 99 in Chico. The portion of SR 32 in the City of Orland located in the vicinity of I-5 is also known as Newville Road. In the area immediately east of the I-5 interchange Newville Road (SR 32) is a two lane/four lane arterial with left-turn lanes at intersections. The speed limit on SR 32 is 35 miles per hour (mph) east of I-5. According to the Caltrans website, the segment of Newville Road (SR 32) east of the interchange carried 8,500 AADT in 2016, with the volume rising to 10,800 AADT in the area east of the $6^{\text {th }}$ Avenue intersection. The State Route 32 Transportation Concept Report identifies the current daily traffic volume east of I-5 at 9,752, which is more in line with recent peak hour counts. Trucks comprise $12 \%$ of the daily traffic on SR 32 through Orland according to Caltrans data.

The Interstate 5 / SR 32 (Newville Road) interchange is a partial cloverleaf layout. Northbound and southbound off-ramps terminate at stop sign controlled intersections on Newville Road. Separate on-ramps to I-5 are provided in both directions which eliminates left turning traffic across mainline Newville Road. Caltrans recently approved an all-way stop for the northbound ramp intersection. SR 32 has a two-lane crossing over I-5. Caltrans publishes daily traffic volume information for freeway ramps. The most recent data from 2014 is summarized in Table 1. (Note: these counts were made before the Flying J opened).

Newville Road west of I-5 is a Glenn County road that extends for roughly 7 miles to the Tehama County line near Black Butte Lake. This portion of Newville Road is designated a Minor Arterial in the Glenn County General Plan Circulation Element and an Arterial in the City of Orland General Plan Circulation Element. Newville Road is a two-lane rural road west of I-5 with a posted speed limit of 35 mph . The most recent traffic volume counts made of the Orland GPU EIR in 2009 indicated that Newville Road carried 5,108 vehicles per day west of County Road HH, however this count was made before the Flying J opened.

| TABLE 1 |  |  |  |
| :---: | :--- | :---: | :---: |
| DAILY INTERSTATE 5 RAMP VOLUMES |  |  |  |
| Direction | Location | Daily Volume <br> $(\mathbf{2 0 1 4})$ |  |
|  | Off-ramp to Newville Road (SR 32) | 1,150 |  |
|  | On-ramp from westbound Newville Road | 1,200 |  |
|  | On-ramp from eastbound Newville Road | 580 |  |
| Northbound | Off-ramp to Newville Road (SR 32) | 1,600 |  |
|  | On-ramp from eastbound Newville Road (SR 32) | 330 |  |
|  | On-ramp from westbound Newville Road (SR 32) | 460 |  |

County Road HH (Commerce Road) is a north-south street that runs southerly from an intersection on County Road 12 across Newville Road to its southern terminus on County Road 15 (Newport Road). County Road HH provides access to existing highway commercial, light industrial and residential uses west of I-5. County Road HH is designated a Minor Collector in the Orland Circulation Element. The Orland General Plan Circulation Element indicates that County Road HH will be extended south to County Road 16 in the future. Today the portion of County Road HH near the project is called Commerce Road and was widened with the Flying J project. The rural prima facie speed limit of 55 mph is in effect on County Road HH south of Newville Road. The Orland General Plan EIR identifies the daily traffic volume on County Road HH was 945 vehicles per day in the area south of Newville Road before the Flying J opened.

The Newville Road / Commerce Lane (County Road HH) intersection is controlled by an allway stop. Improvements were made with the Flying J, and there are separate left turn lanes on the Newville Road approaches and a separate right turn lane on the northbound County Road HH approach.

County Road 13 is a-two lane local street that connects County Road HH with rural residential areas west of I-5. County Road 13 extends east from the County Road HH intersection along the Pilot Flying J Site to a turn-around near the I-5 right of way. No daily traffic volume counts are available for County Road 13.

The County Road HH / County Road 13 intersection is controlled by an all-way stop. There is a separate southbound left turn lane on County Road HH at this intersection.

County Road 14 is a-two lane local street that connects County Road HH with rural residential areas west of I-5 and with County Road HH. No daily traffic volume counts are available for County Road 14.

## Alternative Transportation Modes

Sidewalks. Concrete and asphalt sidewalks exist at various locations along most City of Orland streets but become less prevalent on Glenn County roads adjoining the community. As noted in

Table 2, there are few sidewalks in the area west of I-5 although there is existing sidewalk on the north side of Newville Road (SR 32) across I-5.

| TABLE 2 <br> SIDEWALK INVENTORY |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Street | From | To | Side | Sidewalk |
| Newville Road | County Road HH | Southbound I-5 ramps | North | Partial |
|  |  |  | South | No |
|  | Southbound I-5 ramps | Northbound I-5 ramps | North | Yes |
|  |  |  | South | No |
|  | Northbound I-5 ramps | $9^{\text {th }}$ Street - Tehama Street | North | Yes |
|  |  |  | South | Partial |
|  | $9^{\text {th }}$ Street - Tehama Street | $8^{\text {th }}$ Street | North | Yes |
|  |  |  | South | Yes |
| County Road HH | Newville Road | County Road 13 | East | Yes |
|  |  |  | West | No |
|  | County Road 13 | County Road 14 | East | No |
|  |  |  | West | No |

Bicycle Facilities. Presently there are no formally designated bicycle lanes or bicycle facilities in the City of Orland. However, the City understands the need to move people through the community. The City is planning multi-use pathways along Stony Creek, as well as multi-use pathways within the right-of-ways of undergrounded canals. Additionally, street widths can accommodate bicycle traffic in some areas, and bicycle racks are available at schools and parks.

Public Transit. Public transportation bus service is provided to the City of Orland through Glenn Ride, which is a transit service provided by Glenn County. It is a fixed-route bus system with seven round trips every weekday and three round trips on Saturday from Willows to Chico. There are currently 14 bus stops in Orland. The stop closest to the proposed project is at the $9^{\text {th }}$ Street / Newville Road intersection (i.e., CVS Pharmacy \& Burger King).

## Existing Peak Hour Traffic Volumes

To quantify existing traffic conditions, peak hour intersection turning movement count data were collected for this analysis at the four existing study intersections. The count data was collected during the 7:00 a.m. to 9:00 a.m. morning peak period and the 4:00 p.m. to 6:00 p.m. evening peak period when the Flying J was in normal operation. New traffic counts were conducted at the I-5 ramps on November 29, 2016 for the City of Orland, and this data was used to adjust counts made at the Newville Road / County Road HH intersection in June 2016 to November levels. Existing peak hour traffic volume data, as well as current intersection traffic controls and intersection lane geometry, are presented in Figure 3.



Road HH/ Newville Rd
2 (0)

County Road HH/ County Road 13


SB I-5 Ramp/ Newville Rd


## Level of Service Definition and Calculation

To quantitatively evaluate traffic conditions, and to provide a basis for comparison of operating conditions with and without traffic generated by the proposed project, Levels of Service (LOS) were determined at study area intersections and at freeway ramp terminals.

Level of Service is a quantitative measure of traffic operating conditions using letter grades "A" through " $F$ " to characterize operating conditions at an intersection, on highways and at freeway ramp terminals. LOS A through F represents progressively worsening traffic conditions. The characteristics associated with the various Levels of Service for intersections and freeway mergediverge areas are presented in Table 3.

| TABLE 3LEVEL OF SERVICE DEFINITIONS |  |  |  |
| :---: | :---: | :---: | :---: |
| Level of Service | Signalized Intersection | Unsignalized Intersection | Freeway Ramp Terminal |
| A | Uncongested operations, all queues clear in a single-signal cycle. $\text { Delay } \leq 10.0 \mathrm{sec}$ | Little or no delay. Delay $\leq 10 \mathrm{sec} / \mathrm{veh}$ | Density < $10.0 \mathrm{pc} / \mathrm{ln} / \mathrm{mi}$ |
| B | Uncongested operations, all queues clear in a single cycle. <br> Delay $>10.0 \mathrm{sec}$ and $\leq 20.0 \mathrm{sec}$ | Short traffic delays. <br> Delay > $10 \mathrm{sec} / \mathrm{veh}$ and $\leq 15$ sec/veh | Density > 10 and < 20 $\mathrm{pc} / \mathrm{ln} / \mathrm{mi}$ |
| C | Light congestion, occasional backups on critical approaches. <br> Delay $>20.0 \mathrm{sec}$ and $\leq 35.0 \mathrm{sec}$ | Average traffic delays. Delay > $15 \mathrm{sec} / \mathrm{veh}$ and $\leq 25$ sec/veh | Density $>20$ and $<28 \mathrm{pc} / \mathrm{ln} / \mathrm{mi}$ |
| D | Significant congestions of critical approaches but intersection functional. Cars required to wait through more than one cycle during short peaks. No long queues formed. <br> Delay $>35.0 \mathrm{sec}$ and $\leq 55.0 \mathrm{sec}$ | Long traffic delays. <br> Delay > 25 sec/veh and $\leq 35$ sec/veh | Density > 28 and < $35 \mathrm{pc} / \mathrm{ln} / \mathrm{mi}$ |
| E | Severe congestion with some long standing queues on critical approaches. Blockage of intersection may occur if traffic signal does not provide for protected turning movements. Traffic queue may block nearby intersection(s) upstream of critical approach(es). <br> Delay $>55.0 \mathrm{sec}$ and $\leq 80.0 \mathrm{sec}$ | Very long traffic delays, failure, extreme congestion. <br> Delay > $35 \mathrm{sec} /$ veh and $\leq 50$ sec/veh | Density > $35 \mathrm{pc} / \mathrm{ln} / \mathrm{mi}$ |
| F | Total breakdown, stop-and-go operation. Delay > 80.0 sec | Intersection blocked by external causes. Delay > $50 \mathrm{sec} / \mathrm{veh}$ | Demand Exceeds Capacity |
| Source: Transportation Research Board 2010. |  |  |  |

Levels of service were calculated for this study using the methodology contained in the 2010 Highway Capacity Manual (Transportation Research Board 2012). At signalized intersections and intersections controlled by four-way stop signs, the overall Level of Service for intersections
is based on the average length of delays for all motorists at the intersection. At two-way stop-sign-controlled unsignalized intersections (or one-way stop T intersections), the Level of Service is based on the length of the average delay experienced by motorists on the worst single movement, which is typically a left turn made from the stop-sign-controlled approach to the intersection. It should be noted that overall intersection average Level of Service at un-signalized intersections is better, often much better, than the Level of Service for the worst single movement.

Level of Service calculations for intersections specifically account for the presence of large trucks whose acceleration and deceleration characteristics differ from passenger vehicles. Both calculations include truck percentage as an input and reduce the theoretical facility capacity accordingly to account for the presence of large vehicles. As noted later in this report, current truck percentages were identified in the new traffic counts and adjusted under each scenario as needed to reflect future conditions.

## Level of Service Based on Roadway Segment Volume

The Orland General Plan EIR addressed Level of Service at a planning level on roadway segments based on daily traffic volume. The roadway segment Level of Service criteria identifies maximum daily traffic volume thresholds for each Level of Service grade. Thresholds are identified based on facility classification (i.e., arterials, major collectors, minor collectors, and local roadways) and the number of through travel lanes. The thresholds presented in the City of Orland General Plan EIR are shown in Table 4.

Traffic volumes vary substantially during a 24 -hour period and at locations within roadway segments. As a result, Level of Service based on roadway segments daily volume is an inherently generalized analysis approach that is intended to approximate conditions at the most congested locations during the peak period of the day.

| TABLE 4 <br> LEVEL OF SERVICE THRESHOLDS FOR ROADWAY SEGMENTS BASED ON DAILY TRAFFIC VOLUME |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Classification | Lanes | Maximum Daily Volume at LOS |  |  |  |  |
|  |  | A | B | C | D | E |
| Arterial | 4 | 18,000 | 21,000 | 24,000 | 27,000 | 30,000 |
|  | 2 | 9,000 | 10,500 | 12,000 | 13,500 | 15,000 |
|  | 2+ | 13,500 | 15,750 | 18,000 | 20,250 | 22,500 |
| Major Collector | 2 | 7,620 | 8,890 | 10,160 | 11,430 | 12,700 |
| Minor Collector | 2 | 4,800 | 5,600 | 6,400 | 7,200 | 8,000 |
| Local | 2 | 2,700 | 3,150 | 3,600 | 4,050 | 4,500 |
| $2+$ indicates capacity created on Newville Road by second eastbound lane dropping onto SB SR 32 per Flying J DEIR |  |  |  |  |  |  |

## Level of Service Standards

Minimum Level of Service standards are adopted by local agencies and Caltrans for their respective facilities and presented in various documents.

Caltrans is responsible for maintaining and operating I-5 and SR 32. In accordance with guidance from Caltrans District 3, methods described in the Guide for the Preparation of Traffic Impact Studies (California Department of Transportation 2002) were used in this analysis. This document notes that:
"Caltrans endeavors to maintain a target LOS at the transition between LOS ' C ' and LOS 'D' (see Appendix 'C-3') on State highway facilities . . ."

Therefore, for this analysis, LOS C and better are considered acceptable, and LOS D and worse is considered unacceptable at intersections along the SR 32. The Guide for the Preparation of Traffic Impact Studies specifies application of these criteria to signalized intersections. The document does not specify a minimum acceptable LOS for un-signalized intersections. However, for this analysis, these criteria are also applied to un-signalized intersections.

The City of Orland General Plan Circulation Element identified the minimum standard adopted by the City.
"Policy 3.3.A: Construct street and highway improvements to maintain an overall daily roadway Level of Service of "C" with an a.m. and p.m. peak hour roadway and intersection Level of Service of "D" or better, unless other public health, safety, or welfare factors determine otherwise."

## Traffic Signal Warrants Procedures

Traffic signal warrants are a series of standards which provide guidelines for determining if a traffic signal is appropriate. Signal warrant analyses are typically conducted at intersections of uncontrolled major streets and stop sign-controlled minor streets. If one or more signal warrants are met, signalization of the intersection may be appropriate. However, a signal should not be installed if none of the warrants are met, since the installation of signals would increase delays on the previously-uncontrolled major street, resulting in an undesirable increase in overall vehicle delay at the intersection. Signalization may also increase the occurrence of particular types of accidents. Therefore, if signals are installed where signal warrants are not met, the detriment of increased accidents and overall delay may be greater than the benefit in traffic operating conditions on the single worst movement at the intersection. Signal warrants, then, provide an industry-standard basis for identifying when the adverse effect on the worst movement is substantial enough to warrant signalization.

The City of Orland conducted a complete traffic signal warrant analysis for the I-5 / SR 32 ramp intersections based on November 2016 data. That assessment determined that traffic signals were not immediately justified.

For this traffic impact study, available data are limited to a.m. and p.m. peak hour volumes. Thus, un-signalized intersections were evaluated using the Peak Hour Warrant (Warrant Number 3) from the California Department of Transportation document Manual on Uniform Traffic Control Devices for Streets and Highways (FHWA's MUTCD 2010 Edition, as amended for use in California) (MUTCD) (California Department of Transportation 2012). Urban analysis criteria were employed based on the speed limit on Newville Road - SR 32 (i.e., 35 mph ).

## Current Peak Hour Traffic Conditions

Intersections. Current a.m. and p.m. peak hour LOS were calculated at existing study intersections under Existing conditions. The results of this analysis are presented in Table 5. The LOS calculation worksheets for Existing conditions are presented in the Appendix.

As shown in Table 5, all of the study intersections currently operate with peak hour Level of Service that meets the City's minimum LOS D standard but also meet the Caltrans LOS C goal. No improvements at these intersections are needed.

Current traffic volumes at un-signalized study intersections were compared to peak hour traffic signal warrant thresholds, and no location carries volumes that satisfy peak hour warrants.

| TABLE 5 <br> EXISTING PEAK HOUR INTERSECTION LEVELS OF SERVICE |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | AM Peak Hour |  | PM Peak Hour |  | Warrants Met? |
| Intersection | Control | Ave Delay (Sec/Veh) | LOS | Ave Delay (Sec/Veh) | LOS |  |
| Newville Road / County Road HH | All-Way Stop | 12 | B | 13 | B | No |
| Newville Road (SR 32) / SB I-5 ramps SB approach | SB Stop | 15 | B | 21 | C | No |
| Newville Road (SR 32) / NB I-5 ramps | All-Way Stop | 12 | B | 15 | B | No |
| County Road HH /Road 13 | All-Way Stop | 8 | A | 8 | A | No |
| LOS = Level of Service |  |  |  |  |  |  |

## PROJECT CHARACTERISTICS

## Project Description

Land Use. The proposed project involves rezoning 5 acres to accommodate specific and speculative uses. Specific uses include:

Two-Bay Truck Wash on 2.1 acres
Speculative uses include:
Highway Commercial parcels totaling 2.8 acres
Access. The site plan designates the locations of access to the Truck Wash. Inbound trucks will enter from County Road HH and will exit onto Road 13. Access to other parcels will occur via these driveways, at a driveway on County Road HH just south of County Road 13, and possible driveways on County Road 14.

## Trip Generation

The number of vehicle trips that are expected to be generated by development of the project has been estimated based on trip generation rates that are applicable to the nature and size of project land uses. Specific trip generation rates published by the Institute of Transportation Engineers (ITE) were used when available for known uses. Where no published data was available a similar use was observed. Where a range of uses is possible, composite trip generation rates were created based on the typical mix of uses that is possible.

Composite Highway Commercial Uses. A set of composite trip generation rates was created for the Highway Commercial zoning based on a mix of gasoline station, restaurants, motel and specialty retail uses that might typically be expected in small centers near freeways. The resulting "per acre" trip generation rates are noted in Table 6.

Truck Service Facilities. There are no published trip generation rates for facilities that cater to large trucks and provide wash and repair services. For this analysis a similar truck wash in Corning was observed, and its p.m. peak hour automobile and truck activities were assumed to be applicable to the new truck wash uses.

Forecasts. Table 7 notes the overall trip generation estimate. As shown, under these assumptions the uses in the project could generate 2,736 daily trips, with 211 trips in the a.m. peak hour and 221 trips in the p.m. peak hour.

| TABLE 6 <br> TYPICAL HIGHWAY COMMERCIAL TRIP GENERATION CHARACTERISTICS |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Land Use | Unit | Prototypical |  | Trips per Unit |  |  |  |  |  |  |
|  |  | Quantity | Acres | Daily | AM Peak Hour |  |  | PM Peak Hour |  |  |
|  |  |  |  |  | In | Out | Total | In | Out | Total |
| Gasoline with C-Store | fueling position |  |  | 152.84 | 51\% | 49\% | 11.84 | 51\% | 49\% | 13.86 |
|  |  | 12 | 1.0 | 1,834 | 72 | 70 | 142 | 85 | 81 | 166 |
| Internal | 25\% |  |  | 458 | 18 | 18 | 36 | 21 | 21 | 42 |
| External | 75\% |  |  | 1,376 | 54 | 52 | 106 | 64 | 60 | 124 |
| Pass-by | 50\% |  |  | 688 | 27 | 26 | 53 | 32 | 30 | 62 |
| Net New External Trips | 50\% |  |  | 688 | 27 | 26 | 53 | 32 | 30 | 62 |
| Fast Food Restaurant | ksf | 1 |  | 496.12 | 51\% | 49\% | 45.42 | 52\% | 48\% | 32.65 |
|  |  | 3.5 | 1.0 | 1,736 | 81 | 78 | 159 | 59 | 55 | 114 |
| Internal | 25\% |  |  | 434 | 20 | 20 | 40 | 15 | 14 | 29 |
| External | 75\% |  |  | 1,302 | 61 | 58 | 119 | 44 | 41 | 85 |
| Pass-by | 62\%-56\% |  |  | 729 | 38 | 36 | 74 | 25 | 23 | 48 |
| Net New External Trips |  |  |  | 573 | 23 | 22 | 45 | 19 | 18 | 37 |
| Sit Down Restaurant | ksf | 5.0 |  | 127.15 | 55\% | 45\% | 10.81 | 60\% | 40\% | 9.85 |
|  |  | 5.0 | 1.0 | 636 | 30 | 24 | 54 | 30 | 19 | 49 |
| Internal | 25\% |  |  | 159 | 8 | 6 | 14 | 8 | 4 | 12 |
| External | 75\% |  |  | 477 | 22 | 18 | 40 | 22 | 15 | 37 |
| Pass-by | 43\% |  |  | 205 | 9 | 8 | 17 | 9 | 7 | 16 |
| Net New External Trips |  |  |  | 272 | 13 | 10 | 23 | 13 | 8 | 21 |
| Hotel | rooms | 1 |  | 8.17 | 59\% | 41\% | 0.53 | 51\% | 49\% | 0.60 |
|  |  | 80 | 1.5 | 653 | 25 | 17 | 42 | 24 | 24 | 48 |
| Internal | 25\% |  |  | 163 | 6 | 5 | 11 | 6 | 6 | 12 |
| Net New External Trips | 75\% |  |  | 490 | 19 | 12 | 31 | 18 | 18 | 36 |


| TABLE 6 (cont'd) <br> TYPICAL HIGHWAY COMMERCIAL TRIP GENERATION CHARACTERISTICS |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Land Use | Unit | Prototypical |  | Daily | Trips per Unit |  |  |  |  |  |
|  |  | Quantity | Acres |  | AM Peak Hour |  |  | PM Peak Hour |  |  |
|  |  |  |  |  | In | Out | Total | In | Out | Total |
| Retail - Shopping Center | ksf | 1 |  | 42.70 | 62\% | 38\% | 0.96 | 48\% | 52\% | 3.71 |
|  |  | 16.0 | 1.5 | 683 | 10 | 6 | 16 | 28 | 31 | 59 |
| Internal | 25\% |  |  | 171 | 3 | 1 | 4 | 7 | 8 | 15 |
| External | 75\% |  |  | 512 | 7 | 5 | 12 | 21 | 23 | 44 |
| Pass-by | 34\% |  |  | 174 | 0 | 0 | 0 | 7 | 8 | 15 |
| Net New External Trips |  |  |  | 338 | 7 | 5 | 12 | 14 | 15 | 29 |
| Total Gross Trips | Total |  | 6 | 5,542 | 217 | 196 | 413 | 226 | 210 | 436 |
|  |  |  | acre | 923.67 | 53\% | 47\% | 68.83 | 52\% | 48\% | 72.67 |
|  | Internal |  |  | 1,385 | 54 | 49 | 103 | 57 | 53 | 110 |
|  | External |  |  | 4,155 | 163 | 147 | 310 | 169 | 157 | 326 |
|  |  |  | acre | 692.50 | 53\% | 47\% | 51.66 | 51\% | 49\% | 54.33 |
| Pass-by Trips |  |  |  | 1,796 |  |  | 192 |  |  | 188 |
| Total Net New Trips |  |  | 6 | 2,359 |  |  | 221 |  |  | 251 |
|  |  |  |  | 393.17 | 54\% | 46\% | 24.56 | 51\% | 49\% | 41.83 |


| TABLE 7PROJECT TRIP GENERATION ESTIMATES |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Area | $\begin{aligned} & \text { ITE } \\ & \text { Code } \end{aligned}$ |  | Unit | Quantity | Trips Generated |  |  |  |  |  |  |
|  |  |  |  |  | Daily | AM Peak Hour |  |  | PM Peak Hour |  |  |
|  |  |  |  |  |  | In | Out | Total | In | Out | Total |
| 1 |  | 2-Bay Truck Wash | - | - | 150 | 7 | 11 | 18 | 11 | 7 | 18 |
|  |  | Highway Commercial Rate | acre | 1 | 923.67 | 53\% | 47\% | 68.83 | 52\% | 48\% | 72.67 |
| 4 |  | Highway Commercial |  | 2.8 | 2,586 | 102 | 91 | 193 | 106 | 97 | 203 |
| Total |  |  |  |  | 2,736 | 109 | 102 | 211 | 117 | 104 | 221 |

Trip Distribution. The geographic distribution of project-related trips used in this analysis is based on consideration of the nature of the proposed uses and distribution patterns assumed in the Orland General Plan Update EIR traffic study and Flying J DEIR traffic study.

There are two key factors to be considered. Based on its location, many of the trips associated with the highway commercial uses will be drawn from the stream of traffic passing the site on I-5 or SR 32. Automobile trips would be expected to be drawn from existing traffic on state highways, but a share of the project's automobile traffic may originate in Orland. Truck traffic is expected to be drawn primarily from vehicles that are already part of the $25 \%$ of current daily traffic on I-5. Automobile and truck trips could also be drawn from the traffic already visiting the Flying J.

Under normal conditions the trips associated with retail uses are divided between "primary", "diverted linked", "pass-by" and "internal" trips. Primary or "new" trips represent those trips specifically made for the purpose of visiting the site. These trips would affect the project access as well as the local and regional circulation system. Pass-by trips are those made as part of another trip by patrons who simply turn into the project. Pass-by trips would not affect the regional circulation system. Link diverted trips are those that already occur on part of the regional circulation system but may use local streets to reach the project. In this case, trips drawn from existing traffic on I-5 to the project are diverted linked trips. "Internal" trips are those made between complimentary uses in the same area that do not actually use the circulation system.

Because the volume of through traffic on Newville Road and County Road HH is low, it has been assumed that the project's trips drawn from traffic on I-5 are diverted-linked trips that would be "new" to the local street system. Trips made by Flying J customers or trips made between complimentary on-site uses on the site would be "internal". The project would create few new "primary" trips on I-5.

Table 8 presents the assumptions made regarding the directional distribution of project trips.

| PROJECT TRIP DISTRIBUTION |  |  |
| :---: | :---: | :---: |
| Direction | Route | Percentage |
| North | Interstate 5 | $22 \%$ |
| South | Interstate 5 | $16 \%$ |
|  | County Road HH | $6 \%$ |
| East | Newville Road (SR 32) beyond 8 ${ }^{\text {th }}$ Street | $26 \%$ |
| West | Newville Road | $5 \%$ |
| Internal | (Flying J) | $25 \%$ |
| Total |  | $\mathbf{1 0 0 \%}$ |

Trip Assignment. The trips generated by the proposed project were assigned to the study area street system based on the location of site access and the regional distribution patterns noted previously. Figure 4 presents the resulting project trip assignment.



County Road HH/ County Road 13


SB I-5 Ramp/ Newville Rd


## PROJECT IMPACTS

## Traffic Operations Analysis

Traffic volumes associated with the project were estimated by superimposing project trips onto current background traffic. Figure 5 presents Existing Plus Project a.m. and p.m. peak hour traffic volumes at study locations.

Peak Hour Intersection Level of Service. Resulting Existing Plus Project peak hour LOS are presented in Table 9. The LOS calculation worksheets for Existing Plus Project conditions are presented in the Appendix.

As shown, the addition of project generated traffic results in slightly longer delays at the study intersections on Newville Road and SR 32. However, at all locations the average delays are indicative of conditions that satisfy the City's LOS D minimum standard.

Traffic Signal Warrants. Projected traffic volumes with the project remain below the level that would satisfy traffic signals.




County Road HH/ County Road 13

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| $\text { TABLE } 9$ <br> EXISTING PLUS PROJECT PEAK HOUR INTERSECTION LEVELS OF SERVICE |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Intersection | Control | AM Peak Hour |  |  |  | PM Peak Hour |  |  |  |
|  |  | Existing |  | EX plus Project |  | Existing |  | EX Plus Project |  |
|  |  | Ave Delay (Sec/Veh) | LOS | Ave Delay (sec/veh) | LOS | Ave Delay (Sec/Veh) | LOS | Ave Delay (sec/veh) | LOS |
| Newville Road / County Road HH | All-Way Stop | 12 | B | 13 | B | 13 | B | 15 | B |
| Newville Road (SR 32) / SB I-5 ramps SB approach | SB Stop | 15 | C | 16 | C | 21 | C | 25 | D |
| Newville Road (SR 32) / NB I-5 ramps | All-Way Stop | 12 | B | 13 | B | 15 | B | 16 | C |
| County Road HH /Road 13 | All-Way Stop | 8 | A | 8 | A | 8 | A | 9 | A |
| LOS $=$ Level of Service |  |  |  |  |  |  |  |  |  |

## Traffic Safety Impacts

The adequacy of the study area circulation system has been evaluated with regards to two issues:

1. Need for left turn lane channelization on Commerce Lane (County Road HH) at the new site access, and
2. Truck turning requirements.

Left Turn Channelization. The project will result in full size trucks and automobile turning into and out of the site via access on Commerce Lane (County Road HH) and via County Road 13. The City of Orland required that the recently constructed Flying J respond to that activity on County Road HH by widening the road to provide a separate southbound left turn lane at the County Road 13 intersection. Ultimately County Road HH will be widened in the area north of County Road 13 when adjoining property is developed to create a continuous Two-Way LeftTurn lane.

Development of the project will create similar turning movements but arguably many fewer trucks than Flying J. Thus, projected traffic volumes do not create the immediate need for a separate northbound left turn lane at the truck wash access, but the project's frontage improvements should be positioned so as to accommodate a continuous southbound left turn lane when west side improvements occur in the future.

Truck Turning Requirements. The project will result in full size trucks (STAA) turning into and out of the site via the access on County Road HH and on County Road 13. The Newville Road / County Road HH intersection has already been widened to accommodate trucks and the northeast corner of the County Road HH / County Road 13 intersection can accommodate truck turns. The project's truck entrance on County Road HH will need to be designed to accommodate truck movements, and the turning requirements of large trucks (i.e., STAA trucks) will need to be reviewed when final plans for project frontage improvements at the County Road HH / Road 13 intersection are prepared.

## Impacts to Alternative Transportation Modes

The project may result in pedestrians and bicyclists who would travel between the site and the balance of the Orland area east of I-5. The number of pedestrians is not likely to be appreciable, and the safe path of travel to Orland that was created with the Flying J project remains adequate with the proposed project. Development on the project should, however, be accompanied by sidewalks along the frontage and a crosswalk across Commerce Lane and County Road 13 to the Flying J site should be included.

## CUMULATIVE CONDITIONS ANALYSIS

This report section describes the cumulative impacts of the proposed project within the context of two cumulative conditions. The first condition assumes occupancy of other another approved project in this area. The second longer term cumulative condition is based on the Orland General Plan EIR. The text which follows describes the approach used to forecast future "Cumulative" traffic volumes under "No Project" and "Plus Project" conditions.

## Methodology / Assumptions - Existing Plus Approved Project

The City of Orland considered and approved an application for a development on 3 acre portion of the property across County Road HH from the Flying J. That project which involved an 80 room hotel and a 6,000 sf high turnover sit down restaurant with access to both County Road HH and County Road 13 , was the subject of a traffic analysis conducted in $2016^{1}$.

This project was forecast to generate 107 trips in the a.m. peak hour and 107 trips in the p.m. peak hour. These trips would be assigned to the local street system based on trip distribution assumptions that were similar to those identified for the proposed Truck Wash / Commercial project.

## Methodology/Assumptions - Long Term

The Orland General Plan Update EIR traffic study included creation of a local traffic assignment model to address the overall effect of community development as well as through traffic increases on state highways. For this analysis this tool was reviewed to identify assumptions regarding regional through traffic and development on the subject site.

Land Use. The General Plan EIR traffic model assumed development would occur at various locations throughout Orland over the life of the General Plan. The following list summarizes land use development assumed in that study:

- 1,209 single family dwelling units,
- 192 multiple family dwelling units,
- 290,610 building square feet of retail commercial uses,
- 8.90 acres of office land use,
- 61.97 acres of light industrial / commercial use, and
- 23.31 acres of heavy industrial use.

The GPU EIR traffic study made assumptions regarding development in the area west of I-5. A total of 8.3 acres of commercial development was assumed in the area south of Newville Road and north of County Road 14. This development was assumed to be in the general area of the Flying J site.

[^0]As noted above, the City of Orland considered and approved an application for development on a 3 acre portion of the property with an 80 room hotel and a $6,000 \mathrm{sf}$ high turnover sit down restaurant with access to both County Road HH and County Road 13. Together this project and the Flying J would occupy acreage that was similar to but larger than the allocation made in the General Plan EIR.

For this analysis two land use scenarios have been evaluated:

1. No development on project site but development per the General Plan EIR elsewhere in Orland, including the hotel and restaurant on County Road HH.
2. Same as \#1 with the proposed project.

## Existing Plus Approved Projects (EPAP) Traffic Impacts

Traffic Volumes. Figure 6 illustrates short term future peak hour traffic volumes assuming that the proposed Truck Wash / Commercial project proceeds and the hotel / restaurant project is occupied.

Intersection Level of Service. Table 10 presents the Levels of Service projected at study intersections if both the proposed and approved projects proceed. As shown the minimum LOS D standard will still be satisfied.

Traffic Signal Warrants. The volume of traffic forecast at study intersections under EPAP and EPAP Plus Project conditions was compared to MUTCD peak hour warrant requirements to see whether traffic signals will be justified. As indicated in Table 11, signal warrants do not carry volumes that satisfy peak hour warrants at the Newville Road / County Road HH intersection, either of the two I-5 ramp intersections, or the intersections on County Road HH south of Newville Road.

As noted previously in the discussion of intersection Levels of Service, funding for these traffic signals has been identified in the City traffic impact mitigation fee program.


EXISTING PLUS PROJECT AND HOTEL-RESTAURANT
KD Anderson \& Associates, Inc. Transportation Engineers

| Transportation Engine |
| :--- |
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TRAFFIC VOLUMES AND LANE CONFIGURATIONS -01


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County Road HH/ County Road 13


| TABLE 10 <br> EXISTING PLUS APPROVED PROJECT (EPAP) <br> PEAK HOUR INTERSECTION LEVELS OF SERVICE |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Intersection | Control | AM Peak Hour |  | PM Peak Hour |  |
|  |  | Existing Plus Project and Hotel-Restaurant |  | Existing Plus Project and Hotel-Restaurant |  |
|  |  | Average Delay (Sec/Veh) | LOS | Average Delay (Sec/Veh) | LOS |
| Newville Rd / County Road HH | All-Way Stop | 15 | C | 17 | C |
| Newville Rd (SR 32) / SB I-5 ramps SB approach | SB Stop | 18 | C | 31 | D |
| Newville Rd (SR 32) / NB I-5 ramps | All-Way Stop | 14 | B | 18 | C |
| County Rd HH / Road 13 | All-Way Stop | 9 | A | 9 | A |
| LOS = Level of Service |  |  |  |  |  |


| EXISTING PLUS HOTEL-RESTAURANT AND PROJECT TRAFFIC SIGNAL WARRANTS |  |  |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |

## Long Term Cumulative Impacts

Traffic Volume Forecasts. Traffic volume forecasts were created for the two cumulative scenarios using the General Plan EIR traffic model. The model was modified to make use of current traffic volumes in the area of the project and to address the presence of Flying J in those new counts. Figure 7 presents the Cumulative No Project conditions at study area intersections, while Figure 8 presents the peak hour volumes under Cumulative Plus Project conditions.

These figures also illustrate assumed intersection geometry. As shown, while the City's traffic impact fee program includes funds for improvements to study intersections, no improvements have been assumed in order to determine the extent of project impacts. Those funded improvements are presented as mitigations.

Road HH/ Newville Rd

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2 (2)

County Road HH/ County Road 13


County Road HH/ County Road 13

KD Anderson \& Associates, Inc
Transportation Engineers
Transportation Engin 7/1/2019

CUMULATIVE WITH HOTEL-RESTAURANT TRAFFIC VOLUMES AND LANE CONFIGURATIONS



County Road HH/ County Road 13


CUMULATIVE WITH PROJECT AND HOTEL-RESTAURANT TRAFFIC VOLUMES AND LANE CONFIGURATIONS

Intersection Levels of Service. Projected Levels of Service at study area intersections with and without the project assuming no improvements are made are noted in Table 12. As indicated the two un-signalized intersections on SR 32 at the I- 5 ramps intersections are projected to operate with Levels of Service which exceed the City's LOS D standard with and without the proposed project if improvements are not made. The project's trips will exacerbate conditions that are forecast to be deficient, and the project's cumulative impact is significant at these locations.

At the Newville Road / SB I-5 ramps intersection an all-way stop with auxiliary southbound right turn lane would still result in LOS F in the p.m. peak hour. A traffic signal would operate at LOS C with and without the project. A traffic signal at this location is currently included in the City traffic impact mitigation fee program.

Similarly, the Newville Road (SR 32) / NB I-5 ramps intersection would operate at LOS C with a traffic signal. A traffic signal at this location is currently included in the City's traffic impact mitigation fee program.

As indicated, the existing configuration of the Newville Road / Commerce Lane (County Road HH) intersection would deliver LOS C under Cumulative plus Project conditions. Thus, it may not be necessary to install a traffic signal at this location unless coordinated operation of multiple signalized intersections is required. Review of the City's existing traffic impact mitigation fee program indicates that a traffic signal at this location is currently included.

The Levels of Service occurring at the County Road HH / County Road 13 intersection are projected to be LOS B or better with or without the project which satisfies the City's minimum LOS D standard. No additional improvements are needed beyond the project's frontage improvements on the southeast corner.

| TABLE 12 <br> LONG TERM CUMULATIVE PLUS PROJECT PEAK HOUR INTERSECTION LEVELS OF SERVICE |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Intersection | Control | AM Peak Hour |  |  |  | PM Peak Hour |  |  |  |
|  |  | Cumulative Plus Hotel-Restaurant |  | Cumulative Plus Hotel-Restaurant Plus Project |  | Cumulative Plus <br> Hotel-Restaurant |  | Cumulative Plus Hotel-Restaurant Plus Project |  |
|  |  | Average Delay (sec/veh) | LOS | Average Delay (sec/veh) | LOS | Average Delay (sec/veh) | LOS | Average Delay (sec/veh) | LOS |
| Newville Road / County Road HH | All-Way Stop | 14 | B | 16 | B | 20 | C | 24 | C |
|  | Signal | 32 | C | 33 | C | 29 | C | 29 | C |
| Newville Road (SR 32) / SB I-5 ramps SB approach | SB Stop | 127 | F | 199 | F | 417 | F | 540 | F |
|  | Signal | 25 | C | 26 | C | 27 | C | 29 | C |
| Newville Road (SR 32) / NB I-5 ramps | All-Way Stop | 107 | F | 124 | F | 163 | F | 183 | F |
|  | Signal | 26 | C | 27 | C | 26 | C | 26 | C |
| Commerce Lane (County Road HH) / <br> County Road 13 | All-Way Stop | 8 | A | 9 | A | 9 | A | 9 | A |
| LOS = Level of Service |  |  |  |  |  |  |  |  |  |

[^1]Page 29

Traffic Signal Warrants. The volume of traffic forecast at study intersections under Cumulative and Cumulative plus Project conditions was compared to MUTCD peak hour warrant requirements to see whether traffic signals will be justified in the future. As indicated in Table 13, the Newville Road / Commerce Lane (County Road HH) intersection carries volumes that approach but may not satisfy peak hour warrants. Signal warrants are satisfied at the two I-5 ramp intersections with and without the project. None of the intersections on County Road HH south of Newville Road carry volumes that satisfy peak hour warrants.

As noted previously in the discussion of intersection Levels of Service, funding for these traffic signals has been identified in the City traffic impact mitigation fee program.

| TABLE 13 |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: |
| CUMULATIVE TRAFFIC SIGNAL WARRANTS |  |  |  |  |
|  | AM Peak Hour |  | PM Peak Hour |  |
|  | No Project | With <br> Project | No Project | With <br> Project |
| Newville Rd / Commerce Lane (County Rd HH) | No | No | No | No |
| Newville Rd / SB I-5 ramps | Yes | Yes | Yes | Yes |
| Newville Rd (SR 32) / NB I-5 ramps | Yes | Yes | Yes | Yes |
| County Rd HH / Road 13 intersection | No | No | No | No |

Roadway Segment Levels of Service. Table 14 identifies projected daily traffic volumes on study area roads with and without the proposed project and uses that information to determine the planning level LOS for each facility. Because a comprehensive analysis of existing daily traffic volumes was not performed, this analysis makes use of data from the Flying J DEIR traffic study. As noted earlier the City's minimum Level of Service based on daily volume is LOS C.

No Project Conditions. As shown, if the proposed project does not proceed, the long term background traffic volume on SR 32 will exceed the LOS C threshold between the SB I-5 ramps and the NB I-5 ramps. In addition, the daily volume on County Road HH would exceed the LOS C threshold for a 2 lane Minor Collector. Improvements to a Major Collector standard will be needed, and this improvement was acknowledged in the Flying J DEIR.

Cumulative Plus Project Conditions. The addition of trips generated by the project will increase the cumulative traffic volume on study area streets. No streets that were not deficient without the project would now operate with Level of Service that exceeds the LOS C standard.

The volume of traffic on SR 32 over I- 5 would be indicative of LOS F, and the project would exacerbate the deficient "No Project" conditions.

Measures to improve the Level of Service on study area roadway segments have been evaluated, however, it is important to note that in urban areas the flow of traffic through major intersections is generally the controlling factor for the quality of traffic flow. Thus, if the intersections can be made to operate with an adequate Level of Service, the intermediate roadway segments typically perform adequately even though the planning level LOS suggests otherwise.

Between the southbound and northbound I-5 ramps the structure over I-5 would theoretically have to be widened to deliver LOS C based on City thresholds. This level of improvement has not been contemplated in the City General Plan or in the SR 32 TCR. Modifications to the SR 32 structure over I-80 are not included in the City's traffic impact mitigation fee program.

On County Road HH development of a two lane Major Collector-Arterial type roadway would provide additional capacity and deliver LOS C under Cumulative Plus Project conditions.

## TABLE 14

CUMULATIVE PLUS PROJECT ROADWAY SEGMENT LEVELS OF SERVICE

| Street | From | To | Class | Lanes | Cumulative |  | Cumulative Plus Project |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | Daily <br> Volume | Level of Service | Daily Volume |  | Level of Service |
|  |  |  |  |  |  |  | Project Only | Total |  |
| Newville Road | Co Rd HH | I-5 SB ramps | Arterial | 2+ | 13,595 | B | 1,320 | 14,915 | B |
| SR 32 | I-5 SB ramps | I-5 NB ramps |  | 2 | 17,030 | F | 1,020 | 18,050 | F |
| County Rd HH <br> Commerce Lane | Newville Road | County Road 13 | Minor Col | 2 | 6,950 | D | 1,450 | 8,400 | E |
|  |  |  | Major Col | 2 |  |  |  | 8,400 | A |
|  | County Road 13 | County Road 15 | Minor Col | 2 | 1,320 | A | 1,310 | 2,630 | A |

Bold values exceed the City of Orland LOS C threshold for daily volume based on Level of Service.
Highlighted values are a significant impact.
$2+$ indicates the addition of a second eastbound lane dropping onto the southbound on-ramp

## FINDINGS/ MITIGATION MEASURES / RECOMMENDATIONS

The purpose of this section is to summarize significant project impacts and to describe measures which will reduce those impacts to a less than significant level. Based on City of Orland General Plan policy, "unacceptable" conditions are identified as those which exceed the City of Orland's Level of Service D threshold at intersections during peak hours (i.e., LOS E or F) or exceed the LOS C threshold on roadway segments based on daily volume (i.e., LOS D, E or F).

The feasibility of completing identified improvements has been discussed, and the extent to which funding is available to complete cumulative mitigation measures has been evaluated. The proposed project's fair share of cumulative mitigation measures follows as Table 15. Two alternative approaches to the calculation are presented assuming either the project's trips as a percentage of all traffic, or, alternatively as a percentage of future new traffic. Because Pilot Flying J was also conditioned to pay its fair share, the latter calculation is based on the difference between cumulative volumes and the original "existing" condition before Pilot Flying J was opened.

## Current Conditions

Currently the study intersections addressed herein operate with Levels of Service which satisfy the City's LOS D minimum and traffic signal warrants are not satisfied. Therefore, no capacity improvements are needed in this area of Orland at this time.

## Existing Plus Project Alone Conditions

Two traffic impacts have been identified for Existing Plus Project conditions.
Impact T-1: Impact to Safety based on left turn conflicts at County Road HH / County Road 13 intersection. The addition of project trucks will create conflict relating to the turning requirements of large trucks on the southwest corner of the intersection. Without improvements trucks turning in this area will leave the pavement or conflict with vehicles in opposing lanes. This is a significant safety impact.

Mitigation T-1: Widen the southwest corner of the County Road HH / County Road 13 intersection. The project proponents shall be responsible for widening the intersection to the satisfaction of the City Engineer. With this improvement the project's impact is less than significant.

Impact T-2: Impact to pedestrian safety. Development of the project will result in pedestrians walking between the site and the balance of the City of Orland east of I-5. Because no crossing exists along Commerce lane (County Road HH), pedestrians will be crossing County Road HH at various locations. This is a significant safety impact.

Mitigation T-2: Create safe pedestrian crossing. The project proponents shall incorporate a crosswalk into improvements to the County Road HH / County Road 13 intersection and install sidewalks along the project frontage as development proceeds. With this improvement the impact is less than significant.

## Existing Plus Project Plus Approved Project (EPAP) Impacts

Because satisfactory conditions remain, no additional mitigation are required.

## Cumulative Plus Project Impacts

Impact T-3: Impact to Level of Service at Newville Road / SB I-5 Ramps intersection. The addition of project generated automobile and truck traffic and cumulative background traffic resulting from other development and through traffic on SR 32 will result in the off-ramp approach to the Newville Road / SB I-5 ramps intersection operating with LOS F conditions. As LOS F exceeds the City's minimum LOS D standard, this is a significant impact.

Mitigation T-3: Contribute Fair Share to the cost of widening the off-ramp to provide a separate right turn lane and installing a Traffic Signal. This improvement would result in Level of Service B conditions, which satisfy the City's minimum LOS D standard. Implementation will require work within the Caltrans right of way and an encroachment permit would be required. A traffic signal is identified in the City General Plan EIR and is in the City's traffic impact mitigation fee program. Because this improvement is not required solely as a result of the project, project proponents should contribute their fair share to the cost of this mitigation. With this mitigation, the project's cumulative impact is less than significant.

Impact T-4: Impact to Level of Service at Newville Road / NB I-5 ramps intersection. The addition of project generated automobile and truck traffic and cumulative background traffic resulting from other development and through traffic on SR 32 will result in the off ramp operating with LOS F conditions. As LOS F exceeds the City's minimum LOS D standard, this is a significant impact.

Mitigation T-4: Contribute Fair Share to the cost of installing a Traffic Signal. This improvement would result in Level of Service C conditions, which satisfy the City's minimum LOS D standard. Implementation will require work within the Caltrans right of way and an encroachment permit would be required. This improvement is identified in the City General Plan EIR and is in the City's traffic impact mitigation fee program. Because this improvement is not required solely as a result of the project, project proponents should contribute their fair share to the cost of this mitigation. With this mitigation, the project's cumulative impact is less than significant.

Impact T-5: Impact to Level of Service at Newville Road / County Road HH intersection. The addition of project generated automobile and truck traffic and cumulative background traffic resulting from other development may not result in satisfaction of traffic signal warrants at the Newville Road / County Road HH intersection, but because the traffic signal is also needed to ensure coordinated operation of the signals along SR 32, this is a significant impact.

Mitigation T-5: Contribute Fair Share to the cost of installing a Traffic Signal. Signalization would result in Level of Service C conditions, which satisfy the City's minimum LOS D standard and would allow coordinated operation of the other intersections with signals. This improvement is identified in the City General Plan EIR and is in the City's traffic impact
mitigation fee program. Because this improvement is not required solely as a result of this project, project proponents should contribute their fair share to the cost of this mitigation. With this mitigation, the project's cumulative impact is less than significant.

Impact T-6: Impact to Level of Service on Newville Road (SR 32) between SB I-5 and NB I-5 ramps based on Daily Traffic Volume. The addition of project generated automobile and truck traffic and cumulative background traffic resulting from other development in Orland will result in total daily traffic volumes on Newville Road that exceed the LOS C standard for a two lane arterial street. This is a significant impact.

Mitigation T-6: Contribute Fair Share to the cost of coordinating Traffic Signals on Newville Road. To deliver LOS C conditions it would be necessary to widen SR 32 to provide additional lanes on the crossing structure. However, this improvement is not included in the General Plan EIR, or the City's traffic impact fee program. Widening the structure is not identified in the SR 32 TCR. Thus, there is no identified funding mechanism for a project of this magnitude and is unreasonable to expect that local development in Orland would be capable of funding this improvement. As noted earlier, short roadway segments can carry high traffic volumes but operate adequately when the intersections have the capacity to handle peak period traffic volumes at a good Level of Service. This is the case with the intersections on SR 32 which are expected to operate at LOS C or better with identified improvements. Coordinating the operation of the study area signals with the operation of the signals further east on SR 32 will be appropriate. Implementation will require work within the Caltrans right of way and an encroachment permit would be required. Because this improvement is not required solely as a result of the project, project proponents should contribute their fair share to the cost of this mitigation.

| TABLE 13 <br> FAIR SHARE CALCULATION |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Location | Traffic Volume |  |  |  | Fair Share |  |
|  | A | B | C | D |  |  |
|  | Existing | Pre Pilot Flying J* | Project Only | Cumulative <br> Plus Project | Percent of all Traffic (C/D) | Percent of New Traffic C/ (D-B) |
| Based on PM Peak Hour Traffic |  |  |  |  |  |  |
| Newville Rd / County Rd HH | 952 | 660 | 39 | 1,285 | 3\% | 6\% |
| Newville Rd (SR 32) / SB I-5 ramps | 1,040 | 771 | 35 | 1,879 | 2\% | 3\% |
| Newville Rd (SR 32) / NB I-5 ramps | 1,063 | 857 | 26 | 2,306 | 1\% | 2\% |
| ( $\mathrm{b} / \mathrm{c}$ ) is fair share based on all future traffic <br> $<\mathrm{b} /(\mathrm{c}-\mathrm{a})>$ is fair share as a percentage of "new" future traffic only <br> (*) source: Traffic Impact Analysis for Pilot Flying J Travel Center and Annexation, KDA, 1/7/2015 |  |  |  |  |  |  |

## APPENDICES

| Intersection |  |  |
| :--- | ---: | :--- |
| Intersection Delay, s/veh | 13.1 |  |
| Intersection LOS | B |  |


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ${ }^{7}$ | $\hat{F}$ |  | ${ }^{7}$ | $\hat{F}$ |  |  | $\uparrow$ | 「 |  | $\uparrow$ |  |
| Traffic Vol, veh/h | 12 | 228 | 20 | 188 | 152 | 11 | 8 | 4 | 199 | 55 | 3 | 3 |
| Future Vol, veh/h | 12 | 228 | 20 | 188 | 152 | 11 | 8 | 4 | 199 | 55 | 3 | 3 |
| Peak Hour Factor | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 40 | 2 | 2 | 2 | 2 | 25 | 2 | 2 | 2 |
| Mvmt Flow | 14 | 259 | 23 | 214 | 173 | 13 | 9 | 5 | 226 | 63 | 3 | 3 |
| Number of Lanes | 1 | 1 | 0 | 1 | 1 | 0 | 0 | 1 | 1 | 0 | 1 | 0 |
| Approach | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
| Opposing Approach | WB |  |  | EB |  |  | SB |  |  | NB |  |  |
| Opposing Lanes | 2 |  |  | 2 |  |  | 1 |  |  | 2 |  |  |
| Conflicting Approach Left | SB |  |  | NB |  |  | EB |  |  | WB |  |  |
| Conflicting Lanes Left | 1 |  |  | 2 |  |  | 2 |  |  | 2 |  |  |
| Conflicting Approach Right | NB |  |  | SB |  |  | WB |  |  | EB |  |  |
| Conflicting Lanes Right | 2 |  |  | 1 |  |  | 2 |  |  | 2 |  |  |
| HCM Control Delay | 14.1 |  |  | 13.2 |  |  | 12.1 |  |  | 11.4 |  |  |
| HCM LOS | B |  |  | B |  |  | B |  |  | B |  |  |


| Lane | NBLn1 | NBLn2 | EBLn1 | EBLn2 | WBLn1 | WBLn2 | SBLn1 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Vol Left, \% | $67 \%$ | $0 \%$ | $100 \%$ | $0 \%$ | $100 \%$ | $0 \%$ | $90 \%$ |
| Vol Thru, \% | $33 \%$ | $0 \%$ | $0 \%$ | $92 \%$ | $0 \%$ | $93 \%$ | $5 \%$ |
| Vol Right, \% | $0 \%$ | $100 \%$ | $0 \%$ | $8 \%$ | $0 \%$ | $7 \%$ | $5 \%$ |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 12 | 199 | 12 | 248 | 188 | 163 | 61 |
| LT Vol | 8 | 0 | 12 | 0 | 188 | 0 | 55 |
| Through Vol | 4 | 0 | 0 | 228 | 0 | 152 | 3 |
| RT Vol | 0 | 199 | 0 | 20 | 0 | 11 | 3 |
| Lane Flow Rate | 14 | 226 | 14 | 282 | 214 | 185 | 69 |
| Geometry Grp | 7 | 7 | 7 | 7 | 7 | 7 | 6 |
| Degree of Util (X) | 0.026 | 0.372 | 0.025 | 0.476 | 0.42 | 0.304 | 0.138 |
| Departure Headway (Hd) | 6.977 | 5.927 | 6.641 | 6.076 | 7.112 | 5.902 | 7.151 |
| Convergence, Y/N | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Cap | 512 | 604 | 538 | 592 | 506 | 608 | 499 |
| Service Time | 4.737 | 3.687 | 4.394 | 3.829 | 4.863 | 3.652 | 5.227 |
| HCM Lane V/C Ratio | 0.027 | 0.374 | 0.026 | 0.476 | 0.423 | 0.304 | 0.138 |
| HCM Control Delay | 9.9 | 12.2 | 9.6 | 14.3 | 15 | 11.2 | 11.4 |
| HCM Lane LOS | A | B | A | B | B | B | B |
| HCM 95th-tile Q | 0.1 | 1.7 | 0.1 | 2.6 | 2.1 | 1.3 | 0.5 |

## Intersection

Intersection Delay, s/veh 8.4
Intersection LOS
A

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations |  | \& |  |  | \$ |  |  | \$ |  | \% | 个 |  |
| Traffic Vol, veh/h | 11 | 9 | 5 | 0 | 5 | 4 | 4 | 74 | 0 | 36 | 67 | 12 |
| Future Vol, veh/h | 11 | 9 | 5 | 0 | 5 | 4 | 4 | 74 | 0 | 36 | 67 | 12 |
| Peak Hour Factor | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 50 | 2 | 2 | 2 | 75 | 50 | 2 |
| Mvmt Flow | 13 | 10 | 6 | 0 | 6 | 5 | 5 | 84 | 0 | 41 | 76 | 14 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 1 | 1 | 0 |
| Approach | EB |  |  |  | WB |  | NB |  |  | SB |  |  |
| Opposing Approach | WB |  |  |  | EB |  | SB |  |  | NB |  |  |
| Opposing Lanes | 1 |  |  |  | 1 |  | 2 |  |  | 1 |  |  |
| Conflicting Approach Let | ft SB |  |  |  | NB |  | EB |  |  | WB |  |  |
| Conflicting Lanes Left | 2 |  |  |  | 1 |  | 1 |  |  | 1 |  |  |
| Conflicting Approach R | ighNB |  |  |  | SB |  | WB |  |  | EB |  |  |
| Conflicting Lanes Right | 1 |  |  |  | 2 |  | 1 |  |  | 1 |  |  |
| HCM Control Delay | 7.6 |  |  |  | 7.3 |  | 7.8 |  |  | 9.1 |  |  |
| HCM LOS | A |  |  |  | A |  | A |  |  | A |  |  |


| Lane | NBLn1 EBLn1WBLn1 SBLn1 SBLn2 |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Vol Left, \% | $5 \%$ | $44 \%$ | $0 \%$ | $100 \%$ | $0 \%$ |
| Vol Thru, $\%$ | $95 \%$ | $36 \%$ | $56 \%$ | $0 \%$ | $85 \%$ |
| Vol Right, \% | $0 \%$ | $20 \%$ | $44 \%$ | $0 \%$ | $15 \%$ |
| Sign Control | Stop | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 78 | 25 | 9 | 36 | 79 |
| LT Vol | 4 | 11 | 0 | 36 | 0 |
| Through Vol | 74 | 9 | 5 | 0 | 67 |
| RT Vol | 0 | 5 | 4 | 0 | 12 |
| Lane Flow Rate | 89 | 28 | 10 | 41 | 90 |
| Geometry Grp | 5 | 2 | 2 | 7 | 7 |
| Degree of Util (X) | 0.104 | 0.035 | 0.012 | 0.073 | 0.134 |
| Departure Headway (Hd) | 4.206 | 4.484 | 4.27 | 6.389 | 5.356 |
| Convergence, Y/N | Yes | Yes | Yes | Yes | Yes |
| Cap | 838 | 803 | 843 | 560 | 669 |
| Service Time | 2.303 | 2.484 | 2.271 | 4.13 | 3.097 |
| HCM Lane VIC Ratio | 0.106 | 0.035 | 0.012 | 0.073 | 0.135 |
| HCM Control Delay | 7.8 | 7.6 | 7.3 | 9.6 | 8.9 |
| HCM Lane LOS | A | A | A | A | A |
| HCM 95th-tile Q | 0.3 | 0.1 | 0 | 0.2 | 0.5 |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 3 |  |  |  |  |  |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations |  | 4 | \& |  | r |  |
| Traffic Vol, veh/h | 0 | 414 | 246 | 0 | 66 | 86 |
| Future Vol, veh/h | 0 | 414 | 246 | 0 | 66 | 86 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | - | 0 | 0 | - | 0 | - |
| Grade, \% | - | 5 | -5 | - | 0 | - |
| Peak Hour Factor | 88 | 88 | 88 | 88 | 88 | 88 |
| Heavy Vehicles, $\%$ | 2 | 5 | 10 | 10 | 8 | 40 |
| Mvmt Flow | 0 | 470 | 280 | 0 | 75 | 98 |


| Major/Minor | Major1 | Major2 |  | Minor2 |  |  |
| :--- | :---: | ---: | ---: | ---: | ---: | ---: |
| Conflicting Flow All | - | 0 | - | 0 | 750 | 280 |
| $\quad$ Stage 1 | - | - | - | - | 280 | - |
| $\quad$ Stage 2 | - | - | - | - | 470 | - |
| Critical Hdwy | - | - | - | - | 6.48 | 6.6 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.48 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.48 | - |
| Follow-up Hdwy | - | - | - | -3.572 | 3.66 |  |
| Pot Cap-1 Maneuver | 0 | - | - | 0 | 370 | 676 |
| $\quad$ Stage 1 | 0 | - | - | 0 | 754 | - |
| $\quad$ Stage 2 | 0 | - | - | 0 | 617 | - |
| Platoon blocked, \% |  | - | - |  |  |  |
| Mov Cap-1 Maneuver | - | - | - | - | 370 | 676 |
| Mov Cap-2 Maneuver | - | - | - | - | 370 | - |
| $\quad$ Stage 1 | - | - | - | - | 754 | - |
| Stage 2 | - | - | - | - | 617 | - |


| Approach | EB | WB | SB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s | 0 | 0 | 16.1 |
| HCM LOS |  | C |  |


| Minor Lane/Major Mvmt | EBT | WBT SBLn1 |
| :--- | :---: | ---: |
| Capacity (veh/h) | - | - |
| HCM Lane V/C Ratio | - | -0.348 |
| HCM Control Delay (s) | - | - |
| HCM Lane LOS | - | - |
| HCM 95th \%tile Q(veh) | - | - |


| Intersection |  |
| :--- | ---: | :--- |
| Intersection Delay, s/veh | 13 |
| Intersection LOS | B |


| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | 4 |  |  | 4 | ${ }^{1}$ | 「 |
| Traffic Vol, veh/h | 407 | 0 | 0 | 301 | 30 | 54 |
| Future Vol, veh/h | 407 | 0 | 0 | 301 | 30 | 54 |
| Peak Hour Factor | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 |
| Heavy Vehicles, \% | 5 | 2 | 2 | 5 | 40 | 10 |
| Mvmt Flow | 463 | 0 | 0 | 342 | 34 | 61 |
| Number of Lanes | 1 | 0 | 0 | 1 | 1 | 1 |
| Approach | EB |  |  | WB | NB |  |
| Opposing Approach | WB |  |  | EB |  |  |
| Opposing Lanes | 1 |  |  | 1 | 0 |  |
| Conflicting Approach Left |  |  |  | NB | EB |  |
| Conflicting Lanes Left | 0 |  |  | 2 | 1 |  |
| Conflicting Approach Right | NB |  |  |  | WB |  |
| Conflicting Lanes Right | 2 |  |  | 0 | 1 |  |
| HCM Control Delay | 14.5 |  |  | 11.8 | 9.8 |  |
| HCM LOS | B |  |  | B | A |  |


| Lane | NBLn1 | NBLn2 | EBLn1 | WBLn1 |
| :--- | ---: | ---: | ---: | ---: |
| Vol Left, \% | $100 \%$ | $0 \%$ | $0 \%$ | $0 \%$ |
| Vol Thru, \% | $0 \%$ | $0 \%$ | $100 \%$ | $100 \%$ |
| Vol Right, \% | $0 \%$ | $100 \%$ | $0 \%$ | $0 \%$ |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 30 | 54 | 407 | 301 |
| LT Vol | 30 | 0 | 0 | 0 |
| Through Vol | 0 | 0 | 407 | 301 |
| RT Vol | 0 | 54 | 0 | 0 |
| Lane Flow Rate | 34 | 61 | 462 | 342 |
| Geometry Grp | 7 | 7 | 2 | 2 |
| Degree of Util (X) | 0.071 | 0.098 | 0.599 | 0.455 |
| Departure Headway (Hd) | 7.485 | 5.749 | 4.663 | 4.788 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 475 | 617 | 772 | 749 |
| Service Time | 5.282 | 3.543 | 2.713 | 2.844 |
| HCM Lane V/C Ratio | 0.072 | 0.099 | 0.598 | 0.457 |
| HCM Control Delay | 10.9 | 9.2 | 14.5 | 11.8 |
| HCM Lane LOS | B | A | B | B |
| HCM 95th-tile Q | 0.2 | 0.3 | 4.1 | 2.4 |



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ${ }^{1}$ | $\uparrow$ |  | ${ }^{*}$ | F |  |  | $\uparrow$ | 「 |  | * |  |
| Traffic Vol, veh/h | 9 | 192 | 20 | 206 | 271 | 71 | 21 | 7 | 194 | 58 | 6 | 14 |
| Future Vol, veh/h | 9 | 192 | 20 | 206 | 271 | 71 | 21 | 7 | 194 | 58 | 6 | 14 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 40 | 2 | 2 | 2 | 2 | 25 | 2 | 2 | 2 |
| Mvmt Flow | 10 | 209 | 22 | 224 | 295 | 77 | 23 | 8 | 211 | 63 | 7 | 15 |
| Number of Lanes | 1 | 1 | 0 | 1 | 1 | 0 | 0 | 1 | 1 | 0 | 1 | 0 |
| Approach | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
| Opposing Approach | WB |  |  | EB |  |  | SB |  |  | NB |  |  |
| Opposing Lanes | 2 |  |  | 2 |  |  | 1 |  |  | 2 |  |  |
| Conflicting Approach Left | SB |  |  | NB |  |  | EB |  |  | WB |  |  |
| Conflicting Lanes Left | 1 |  |  | 2 |  |  | 2 |  |  | 2 |  |  |
| Conflicting Approach Right | NB |  |  | SB |  |  | WB |  |  | EB |  |  |
| Conflicting Lanes Right | 2 |  |  | 1 |  |  | 2 |  |  | 2 |  |  |
| HCM Control Delay | 13.5 |  |  | 16.6 |  |  | 12.3 |  |  | 11.9 |  |  |
| HCM LOS | B |  |  | C |  |  | B |  |  | B |  |  |


| Lane | NBLn1 | NBLn2 | EBLn1 | EBLn2 | WBLn1 | WBLn2 | SBLn1 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Vol Left, \% | $75 \%$ | $0 \%$ | $100 \%$ | $0 \%$ | $100 \%$ | $0 \%$ | $74 \%$ |
| Vol Thu, \% | $25 \%$ | $0 \%$ | $0 \%$ | $91 \%$ | $0 \%$ | $79 \%$ | $8 \%$ |
| Vol Right, \% | $0 \%$ | $100 \%$ | $0 \%$ | $9 \%$ | $0 \%$ | $21 \%$ | $18 \%$ |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 28 | 194 | 9 | 212 | 206 | 342 | 78 |
| LT Vol | 21 | 0 | 9 | 0 | 206 | 0 | 58 |
| Through Vol | 7 | 0 | 0 | 192 | 0 | 271 | 6 |
| RT Vol | 0 | 194 | 0 | 20 | 0 | 71 | 14 |
| Lane Flow Rate | 30 | 211 | 10 | 230 | 224 | 372 | 85 |
| Geometry Grp | 7 | 7 | 7 | 7 | 7 | 7 | 6 |
| Degree of Util (X) | 0.062 | 0.366 | 0.019 | 0.412 | 0.445 | 0.603 | 0.172 |
| Departure Headway (Hd) | 7.338 | 6.244 | 7.01 | 6.434 | 7.15 | 5.841 | 7.29 |
| Convergence, Y/N | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Cap | 486 | 574 | 508 | 558 | 502 | 617 | 489 |
| Service Time | 5.111 | 4.017 | 4.785 | 4.208 | 4.911 | 3.601 | 5.379 |
| HCM Lane V/C Ratio | 0.062 | 0.368 | 0.02 | 0.412 | 0.446 | 0.603 | 0.174 |
| HCM Control Delay | 10.6 | 12.6 | 9.9 | 13.7 | 15.6 | 17.2 | 11.9 |
| HCM Lane LOS | B | B | A | B | C | C | B |
| HCM 95th-tile Q | 0.2 | 1.7 | 0.1 | 2 | 2.3 | 4 | 0.6 |

## Intersection

Intersection Delay, s/veh 8.6
Intersection LOS
A

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations |  | 4 |  |  | \$ |  |  | 4 |  | ${ }^{7}$ | $\uparrow$ |  |
| Traffic Vol, veh/h | 10 | 9 | 4 | 0 | 5 | 4 | 5 | 46 | 0 | 35 | 88 | 11 |
| Future Vol, veh/h | 10 | 9 | 4 | 0 | 5 | 4 | 5 | 46 | 0 | 35 | 88 | 11 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 50 | 2 | 2 | 2 | 75 | 50 | 2 |
| Mvmt Flow | 11 | 10 | 4 | 0 | 5 | 4 | 5 | 50 | 0 | 38 | 96 | 12 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 1 | 1 | 0 |
| Approach | EB |  |  |  | WB |  | NB |  |  | SB |  |  |
| Opposing Approach | WB |  |  |  | EB |  | SB |  |  | NB |  |  |
| Opposing Lanes | 1 |  |  |  | 1 |  | 2 |  |  | 1 |  |  |
| Conflicting Approach Left | eft SB |  |  |  | NB |  | EB |  |  | WB |  |  |
| Conflicting Lanes Left | 2 |  |  |  | 1 |  | 1 |  |  | 1 |  |  |
| Conflicting Approach Righer | ghNB |  |  |  | SB |  | WB |  |  | EB |  |  |
| Conflicting Lanes Right | 1 |  |  |  | 2 |  | 1 |  |  | 1 |  |  |
| HCM Control Delay | 7.6 |  |  |  | 7.3 |  | 7.6 |  |  | 9.2 |  |  |
| HCM LOS | A |  |  |  | A |  | A |  |  | A |  |  |


| Lane | NBLn1 EBLn1WBLn1 SBLn1 SBLn2 |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Vol Left, \% | $10 \%$ | $43 \%$ | $0 \%$ | $100 \%$ | $0 \%$ |
| Vol Thru, $\%$ | $90 \%$ | $39 \%$ | $56 \%$ | $0 \%$ | $89 \%$ |
| Vol Right, \% | $0 \%$ | $17 \%$ | $44 \%$ | $0 \%$ | $11 \%$ |
| Sign Control | Stop | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 51 | 23 | 9 | 35 | 99 |
| LT Vol | 5 | 10 | 0 | 35 | 0 |
| Through Vol | 46 | 9 | 5 | 0 | 88 |
| RT Vol | 0 | 4 | 4 | 0 | 11 |
| Lane Flow Rate | 55 | 25 | 10 | 38 | 108 |
| Geometry Grp | 5 | 2 | 2 | 7 | 7 |
| Degree of Util (X) | 0.065 | 0.031 | 0.011 | 0.067 | 0.16 |
| Departure Headway (Hd) | 4.22 | 4.463 | 4.231 | 6.365 | 5.361 |
| Convergence, Y/N | Yes | Yes | Yes | Yes | Yes |
| Cap | 834 | 807 | 851 | 563 | 669 |
| Service Time | 2.318 | 2.463 | 2.232 | 4.097 | 3.093 |
| HCM Lane V/C Ratio | 0.066 | 0.031 | 0.012 | 0.067 | 0.161 |
| HCM Control Delay | 7.6 | 7.6 | 7.3 | 9.6 | 9.1 |
| HCM Lane LOS | A | A | A | A | A |
| HCM 95th-tile Q | 0.2 | 0.1 | 0 | 0.2 | 0.6 |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 5.2 |  |  |  |  |  |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations |  | 4 | 个 |  | Mr |  |
| Traffic Vol, veh/h | 0 | 363 | 439 | 0 | 97 | 109 |
| Future Vol, veh/h | 0 | 363 | 439 | 0 | 97 | 109 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | - | 0 | 0 | - | 0 | - |
| Grade, \% | - | 5 | -5 | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, $\%$ | 2 | 5 | 10 | 10 | 8 | 40 |
| Mvmt Flow | 0 | 395 | 477 | 0 | 105 | 118 |


| Major/Minor | Major1 | Major2 |  | Minor2 |  |  |
| :---: | :---: | :---: | :---: | :---: | ---: | ---: |
| Conflicting Flow All | - | 0 | - | 0 | 872 | 477 |
| Stage 1 | - | - | - | - | 477 | - |
| Stage 2 | - | - | - | - | 395 | - |
| Critical Hdwy | - | - | - | - | 6.48 | 6.6 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.48 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.48 | - |
| Follow-up Hdwy | - | - | - | -3.572 | 3.66 |  |
| Pot Cap-1 Maneuver | 0 | - | - | 0 | 313 | 518 |
| $\quad$ Stage 1 | 0 | - | - | 0 | 612 | - |
| Stage 2 | 0 | - | - | 0 | 668 | - |
| Platoon blocked, \% |  | - | - |  |  |  |
| Mov Cap-1 Maneuver | - | - | - | - | 313 | 518 |
| Mov Cap-2 Maneuver | - | - | - | - | 313 | - |
| Stage 1 | - | - | - | - | 612 | - |
| Stage 2 | - | - | - | - | 668 | - |


| Approach | EB | WB | SB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s | 0 | 0 | 25.3 |
| HCM LOS |  |  | D |


| Minor Lane/Major Mvmt | EBT | WBT SBLn1 |
| :--- | :---: | ---: |
| Capacity (veh/h) | - | -396 |
| HCM Lane V/C Ratio | - | -0.565 |
| HCM Control Delay (s) | - | -25.3 |
| HCM Lane LOS | - | - |
| HCM 95th \%tile Q(veh) | - | - |


| Intersection |
| :--- |
| Intersection Delay, s/veh 16.3 |
| Intersection LOS |


| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | 4 |  |  | 4 | ${ }^{1}$ | 「 |
| Traffic Vol, veh/h | 384 | 0 | 0 | 441 | 60 | 99 |
| Future Vol, veh/h | 384 | 0 | 0 | 441 | 60 | 99 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, \% | 5 | 2 | 2 | 5 | 40 | 10 |
| Mumt Flow | 417 | 0 | 0 | 479 | 65 | 108 |
| Number of Lanes | 1 | 0 | 0 | 1 | 1 | 1 |
| Approach | EB |  |  | WB | NB |  |
| Opposing Approach | WB |  |  | EB |  |  |
| Opposing Lanes | 1 |  |  | 1 | 0 |  |
| Conflicting Approach Left |  |  |  | NB | EB |  |
| Conflicting Lanes Left | 0 |  |  | 2 | 1 |  |
| Conflicting Approach Right | NB |  |  |  | WB |  |
| Conflicting Lanes Right | 2 |  |  | 0 | 1 |  |
| HCM Control Delay | 15.9 |  |  | 18.7 | 10.9 |  |
| HCM LOS | C |  |  | C | B |  |


| Lane | NBLn1 | NBLn2 | EBLn1 | WBLn1 |
| :--- | ---: | ---: | ---: | ---: |
| Vol Left, \% | $100 \%$ | $0 \%$ | $0 \%$ | $0 \%$ |
| Vol Thru, \% | $0 \%$ | $0 \%$ | $100 \%$ | $100 \%$ |
| Vol Right, \% | $0 \%$ | $100 \%$ | $0 \%$ | $0 \%$ |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 60 | 99 | 384 | 441 |
| LT Vol | 60 | 0 | 0 | 0 |
| Through Vol | 0 | 0 | 384 | 441 |
| RT Vol | 0 | 99 | 0 | 0 |
| Lane Flow Rate | 65 | 108 | 417 | 479 |
| Geometry Grp | 7 | 7 | 2 | 2 |
| Degree of Util (X) | 0.143 | 0.184 | 0.604 | 0.687 |
| Departure Headway (Hd) | 7.907 | 6.164 | 5.206 | 5.157 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 453 | 581 | 693 | 705 |
| Service Time | 5.654 | 3.909 | 3.237 | 3.157 |
| HCM Lane V/C Ratio | 0.143 | 0.186 | 0.602 | 0.679 |
| HCM Control Delay | 12 | 10.3 | 15.9 | 18.7 |
| HCM Lane LOS | B | B | C | C |
| HCM 95th-tile Q | 0.5 | 0.7 | 4.1 | 5.5 |



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ${ }^{1}$ | $\uparrow$ |  | ${ }^{*}$ | F |  |  | $\uparrow$ | 「 |  | \& |  |
| Traffic Vol, veh/h | 12 | 228 | 24 | 244 | 152 | 11 | 10 | 4 | 242 | 55 | 3 | 3 |
| Future Vol, veh/h | 12 | 228 | 24 | 244 | 152 | 11 | 10 | 4 | 242 | 55 | 3 | 3 |
| Peak Hour Factor | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 40 | 2 | 2 | 2 | 2 | 25 | 2 | 2 | 2 |
| Mvmt Flow | 14 | 259 | 27 | 277 | 173 | 13 | 11 | 5 | 275 | 63 | 3 | 3 |
| Number of Lanes | 1 | 1 | 0 | 1 | 1 | 0 | 0 | 1 | 1 | 0 | 1 | 0 |
| Approach | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
| Opposing Approach | WB |  |  | EB |  |  | SB |  |  | NB |  |  |
| Opposing Lanes | 2 |  |  | 2 |  |  | 1 |  |  | 2 |  |  |
| Conflicting Approach Left | SB |  |  | NB |  |  | EB |  |  | WB |  |  |
| Conflicting Lanes Left | 1 |  |  | 2 |  |  | 2 |  |  | 2 |  |  |
| Conflicting Approach Right | NB |  |  | SB |  |  | WB |  |  | EB |  |  |
| Conflicting Lanes Right | 2 |  |  | 1 |  |  | 2 |  |  | 2 |  |  |
| HCM Control Delay | 15.5 |  |  | 16.4 |  |  | 14.2 |  |  | 12 |  |  |
| HCM LOS | C |  |  | C |  |  | B |  |  | B |  |  |


| Lane | NBLn1 | NBLn2 | EBLn1 | EBLn2 | WBLn1 | WBLn2 | SBLn1 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Vol Left, \% | $71 \%$ | $0 \%$ | $100 \%$ | $0 \%$ | $100 \%$ | $0 \%$ | $90 \%$ |
| Vol Thru, \% | $29 \%$ | $0 \%$ | $0 \%$ | $90 \%$ | $0 \%$ | $93 \%$ | $5 \%$ |
| Vol Right, \% | $0 \%$ | $100 \%$ | $0 \%$ | $10 \%$ | $0 \%$ | $7 \%$ | $5 \%$ |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 14 | 242 | 12 | 252 | 244 | 163 | 61 |
| LT Vol | 10 | 0 | 12 | 0 | 244 | 0 | 55 |
| Through Vol | 4 | 0 | 0 | 228 | 0 | 152 | 3 |
| RT Vol | 0 | 242 | 0 | 24 | 0 | 11 | 3 |
| Lane Flow Rate | 16 | 275 | 14 | 286 | 277 | 185 | 69 |
| Geometry Grp | 7 | 7 | 7 | 7 | 7 | 7 | 6 |
| Degree of Util (X) | 0.032 | 0.472 | 0.027 | 0.511 | 0.568 | 0.317 | 0.148 |
| Departure Headway (Hd) | 7.255 | 6.179 | 6.998 | 6.421 | 7.372 | 6.159 | 7.684 |
| Convergence, Y/N | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Cap | 491 | 578 | 508 | 558 | 488 | 580 | 469 |
| Service Time | 5.04 | 3.964 | 4.785 | 4.207 | 5.152 | 3.938 | 5.684 |
| HCM Lane VIC Ratio | 0.033 | 0.476 | 0.028 | 0.513 | 0.568 | 0.319 | 0.147 |
| HCM Control Delay | 10.3 | 14.4 | 10 | 15.8 | 19.5 | 11.8 | 12 |
| HCM Lane LOS | B | B | A | C | C | B | B |
| HCM 95th-tile Q | 0.1 | 2.5 | 0.1 | 2.9 | 3.5 | 1.4 | 0.5 |



Intersection Delay, s/veh 8.5
Intersection LOS
A

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations |  | $\uparrow$ |  |  | \$ |  |  | ¢ |  | \% | $\hat{F}$ |  |
| Traffic Vol, veh/h | 17 | 9 | 6 | 0 | 5 | 4 | 5 | 75 | 0 | 36 | 68 | 20 |
| Future Vol, veh/h | 17 | 9 | 6 | 0 | 5 | 4 | 5 | 75 | 0 | 36 | 68 | 20 |
| Peak Hour Factor | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 50 | 2 | 2 | 2 | 75 | 50 | 2 |
| Mumt Flow | 19 | 10 | 7 | 0 | 6 | 5 | 6 | 85 | 0 | 41 | 77 | 23 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 1 | 1 | 0 |
| Approach | EB |  |  |  | WB |  | NB |  |  | SB |  |  |
| Opposing Approach | WB |  |  |  | EB |  | SB |  |  | NB |  |  |
| Opposing Lanes | 1 |  |  |  | 1 |  | 2 |  |  | 1 |  |  |
| Conflicting Approach L | ft SB |  |  |  | NB |  | EB |  |  | WB |  |  |
| Conflicting Lanes Left | 2 |  |  |  | 1 |  | 1 |  |  | 1 |  |  |
| Conflicting Approach R | ghNB |  |  |  | SB |  | WB |  |  | EB |  |  |
| Conflicting Lanes Right | 1 |  |  |  | 2 |  | 1 |  |  | 1 |  |  |
| HCM Control Delay | 7.8 |  |  |  | 7.4 |  | 7.9 |  |  | 9.2 |  |  |
| HCM LOS | A |  |  |  | A |  | A |  |  | A |  |  |


| Lane | NBLn1 EBLn1WBLn1 SBLn1 SBLn2 |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Vol Left, \% | $6 \%$ | $53 \%$ | $0 \%$ | $100 \%$ | $0 \%$ |
| Vol Thru, \% | $94 \%$ | $28 \%$ | $56 \%$ | $0 \%$ | $77 \%$ |
| Vol Right, \% | $0 \%$ | $19 \%$ | $44 \%$ | $0 \%$ | $23 \%$ |
| Sign Control | Stop | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 80 | 32 | 9 | 36 | 88 |
| LT Vol | 5 | 17 | 0 | 36 | 0 |
| Through Vol | 75 | 9 | 5 | 0 | 68 |
| RT Vol | 0 | 6 | 4 | 0 | 20 |
| Lane Flow Rate | 91 | 36 | 10 | 41 | 100 |
| Geometry Grp | 5 | 2 | 2 | 7 | 7 |
| Degree of Util (X) | 0.109 | 0.046 | 0.012 | 0.073 | 0.148 |
| Departure Headway (Hd) | 4.335 | 4.539 | 4.309 | 6.404 | 5.318 |
| Convergence, Y/N | Yes | Yes | Yes | Yes | Yes |
| Cap | 831 | 793 | 834 | 558 | 672 |
| Service Time | 2.339 | 2.543 | 2.315 | 4.156 | 3.069 |
| HCM Lane V/C Ratio | 0.11 | 0.045 | 0.012 | 0.073 | 0.149 |
| HCM Control Delay | 7.9 | 7.8 | 7.4 | 9.7 | 9 |
| HCM Lane LOS | A | A | A | A | A |
| HCM 95th-tile Q | 0.4 | 0.1 | 0 | 0.2 | 0.5 |



| Major/Minor | Major1 | Major2 |  | Minor2 |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | - | 0 | - | 0 | 829 | 323 |
| $\quad$ Stage 1 | - | - | - | - | 323 | - |
| $\quad$ Stage 2 | - | - | - | - | 506 | - |
| Critical Hdwy | - | - | - | - | 6.48 | 6.6 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.48 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.48 | - |
| Follow-up Hdwy | - | - | - | -3.572 | 3.66 |  |
| Pot Cap-1 Maneuver | 0 | - | - | 0 | 332 | 638 |
| $\quad$ Stage 1 | 0 | - | - | 0 | 720 | - |
| $\quad$ Stage 2 | 0 | - | - | 0 | 593 | - |
| Platoon blocked, \% |  | - | - |  |  |  |
| Mov Cap-1 Maneuver | - | - | - | - | 332 | 638 |
| Mov Cap-2 Maneuver | - | - | - | - | 332 | - |
| $\quad$ Stage 1 | - | - | - | - | 720 | - |
| Stage 2 | - | - | - | - | 593 | - |
|  |  |  |  |  |  |  |


| Approach | EB | WB | SB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, $s$ | 0 | 0 | 17.9 |
| HCM LOS |  |  | $C$ |


| Minor Lane/Major Mvmt | EBT | WBT SBLn1 |
| :--- | ---: | ---: |
| Capacity (veh/h) | - | -470 |
| HCM Lane V/C Ratio | - | -0.411 |
| HCM Control Delay (s) | - | -17.9 |
| HCM Lane LOS | - | - |
| HCM 95th \%tile Q(veh) | - | - |
| C | 2 |  |


| Intersection |  |
| :--- | ---: | :--- |
| Intersection Delay, s/veh $\quad 14.1$ |  |
| Intersection LOS | B |



| Lane | NBLn1 | NBLn2 | EBLn1 | WBLn1 |
| :--- | ---: | ---: | ---: | ---: |
| Vol Left, \% | $100 \%$ | $0 \%$ | $0 \%$ | $0 \%$ |
| Vol Thru, \% | $0 \%$ | $0 \%$ | $100 \%$ | $100 \%$ |
| Vol Right, \% | $0 \%$ | $100 \%$ | $0 \%$ | $0 \%$ |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 46 | 54 | 423 | 323 |
| LT Vol | 46 | 0 | 0 | 0 |
| Through Vol | 0 | 0 | 423 | 323 |
| RT Vol | 0 | 54 | 0 | 0 |
| Lane Flow Rate | 52 | 61 | 481 | 367 |
| Geometry Grp | 7 | 7 | 2 | 2 |
| Degree of Util (X) | 0.112 | 0.102 | 0.637 | 0.499 |
| Departure Headway (Hd) | 7.713 | 5.973 | 4.77 | 4.891 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 467 | 604 | 750 | 730 |
| Service Time | 5.413 | 3.673 | 2.841 | 2.969 |
| HCM Lane V/C Ratio | 0.111 | 0.101 | 0.641 | 0.503 |
| HCM Control Delay | 11.4 | 9.4 | 15.9 | 12.8 |
| HCM Lane LOS | B | A | C | B |
| HCM 95th-tile Q | 0.4 | 0.3 | 4.6 | 2.8 |



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ${ }^{7}$ | $\hat{F}$ |  | ${ }^{7}$ | $\hat{F}$ |  |  | $\uparrow$ | 「 |  | $\uparrow$ |  |
| Traffic Vol, veh/h | 9 | 192 | 23 | 261 | 271 | 71 | 24 | 7 | 238 | 58 | 6 | 14 |
| Future Vol, veh/h | 9 | 192 | 23 | 261 | 271 | 71 | 24 | 7 | 238 | 58 | 6 | 14 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 40 | 2 | 2 | 2 | 2 | 25 | 2 | 2 | 2 |
| Mvmt Flow | 10 | 209 | 25 | 284 | 295 | 77 | 26 | 8 | 259 | 63 | 7 | 15 |
| Number of Lanes | 1 | 1 | 0 | 1 | 1 | 0 | 0 | 1 | 1 | 0 | 1 | 0 |
| Approach | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
| Opposing Approach | WB |  |  | EB |  |  | SB |  |  | NB |  |  |
| Opposing Lanes | 2 |  |  | 2 |  |  | 1 |  |  | 2 |  |  |
| Conflicting Approach Left | SB |  |  | NB |  |  | EB |  |  | WB |  |  |
| Conflicting Lanes Left | 1 |  |  | 2 |  |  | 2 |  |  | 2 |  |  |
| Conflicting Approach Right | NB |  |  | SB |  |  | WB |  |  | EB |  |  |
| Conflicting Lanes Right | 2 |  |  | 1 |  |  | 2 |  |  | 2 |  |  |
| HCM Control Delay | 14.8 |  |  | 19.3 |  |  | 14.4 |  |  | 12.5 |  |  |
| HCM LOS | B |  |  | C |  |  | B |  |  | B |  |  |


| Lane | NBLn1 | NBLn2 | EBLn1 | EBLn2 | WBLn1 | WBLn2 | SBLn1 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Vol Left, \% | $77 \%$ | $0 \%$ | $100 \%$ | $0 \%$ | $100 \%$ | $0 \%$ | $74 \%$ |
| Vol Thư, \% | $23 \%$ | $0 \%$ | $0 \%$ | $89 \%$ | $0 \%$ | $79 \%$ | $8 \%$ |
| Vol Right, \% | $0 \%$ | $100 \%$ | $0 \%$ | $11 \%$ | $0 \%$ | $21 \%$ | $18 \%$ |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 31 | 238 | 9 | 215 | 261 | 342 | 78 |
| LT Vol | 24 | 0 | 9 | 0 | 261 | 0 | 58 |
| Through Vol | 7 | 0 | 0 | 192 | 0 | 271 | 6 |
| RT Vol | 0 | 238 | 0 | 23 | 0 | 71 | 14 |
| Lane Flow Rate | 34 | 259 | 10 | 234 | 284 | 372 | 85 |
| Geometry Grp | 7 | 7 | 7 | 7 | 7 | 7 | 6 |
| Degree of Util (X) | 0.071 | 0.463 | 0.02 | 0.446 | 0.583 | 0.628 | 0.182 |
| Departure Headway (Hd) | 7.65 | 6.442 | 7.456 | 6.868 | 7.394 | 6.081 | 7.734 |
| Convergence, Y/N | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Cap | 471 | 554 | 483 | 528 | 485 | 587 | 466 |
| Service Time | 5.35 | 4.241 | 5.156 | 4.568 | 5.184 | 3.87 | 5.748 |
| HCM Lane V/C Ratio | 0.072 | 0.468 | 0.021 | 0.443 | 0.586 | 0.634 | 0.182 |
| HCM Control Delay | 10.9 | 14.8 | 10.3 | 15 | 20.1 | 18.7 | 12.5 |
| HCM Lane LOS | B | B | B | B | C | C | B |
| HCM 95th-tile Q | 0.2 | 2.4 | 0.1 | 2.3 | 3.7 | 4.4 | 0.7 |

```
Intersection
Intersection Delay, s/veh 8.7
Intersection LOS
A
```

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations |  | \& |  |  | \$ |  |  | 4 |  | ${ }^{7}$ | F |  |
| Traffic Vol, veh/h | 17 | 9 | 5 | 0 | 5 | 4 | 5 | 89 | 0 | 35 | 89 | 19 |
| Future Vol, veh/h | 17 | 9 | 5 | 0 | 5 | 4 | 5 | 89 | 0 | 35 | 89 | 19 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 50 | 2 | 2 | 2 | 75 | 50 | 2 |
| Mvmt Flow | 18 | 10 | 5 | 0 | 5 | 4 | 5 | 97 | 0 | 38 | 97 | 21 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 1 | 1 | 0 |
| Approach | EB |  |  |  | WB |  | NB |  |  | SB |  |  |
| Opposing Approach | WB |  |  |  | EB |  | SB |  |  | NB |  |  |
| Opposing Lanes | 1 |  |  |  | 1 |  | 2 |  |  | 1 |  |  |
| Conflicting Approach Let | ft SB |  |  |  | NB |  | EB |  |  | WB |  |  |
| Conflicting Lanes Left | 2 |  |  |  | 1 |  | 1 |  |  | 1 |  |  |
| Conflicting Approach R | ighNB |  |  |  | SB |  | WB |  |  | EB |  |  |
| Conflicting Lanes Right | 1 |  |  |  | 2 |  | 1 |  |  | 1 |  |  |
| HCM Control Delay | 7.8 |  |  |  | 7.4 |  | 8 |  |  | 9.4 |  |  |
| HCM LOS | A |  |  |  | A |  | A |  |  | A |  |  |


| Lane | NBLn1 EBLn1WBLn1 SBLn1 SBLn2 |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Vol Left, \% | $5 \%$ | $55 \%$ | $0 \%$ | $100 \%$ | $0 \%$ |
| Vol Thru, \% | $95 \%$ | $29 \%$ | $56 \%$ | $0 \%$ | $82 \%$ |
| Vol Right, \% | $0 \%$ | $16 \%$ | $44 \%$ | $0 \%$ | $18 \%$ |
| Sign Control | Stop | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 94 | 31 | 9 | 35 | 108 |
| LT Vol | 5 | 17 | 0 | 35 | 0 |
| Through Vol | 89 | 9 | 5 | 0 | 89 |
| RT Vol | 0 | 5 | 4 | 0 | 19 |
| Lane Flow Rate | 102 | 34 | 10 | 38 | 117 |
| Geometry Grp | 5 | 2 | 2 | 7 | 7 |
| Degree of Util (X) | 0.123 | 0.043 | 0.012 | 0.068 | 0.175 |
| Departure Headway (Hd) | 4.342 | 4.62 | 4.369 | 6.406 | 5.356 |
| Convergence, Y/N | Yes | Yes | Yes | Yes | Yes |
| Cap | 830 | 779 | 823 | 558 | 668 |
| Service Time | 2.348 | 2.626 | 2.377 | 4.158 | 3.107 |
| HCM Lane V/C Ratio | 0.123 | 0.044 | 0.012 | 0.068 | 0.175 |
| HCM Control Delay | 8 | 7.8 | 7.4 | 9.6 | 9.3 |
| HCM Lane LOS | A | A | A | A | A |
| HCM 95th-tile Q | 0.4 | 0.1 | 0 | 0.2 | 0.6 |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 6.4 |  |  |  |  |  |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations |  | 4 | 个 |  | Mr |  |
| Traffic Vol, veh/h | 0 | 394 | 477 | 0 | 97 | 127 |
| Future Vol, veh/h | 0 | 394 | 477 | 0 | 97 | 127 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | - | 0 | 0 | - | 0 | - |
| Grade, \% | - | 5 | -5 | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, $\%$ | 2 | 5 | 10 | 10 | 8 | 40 |
| Mvmt Flow | 0 | 428 | 518 | 0 | 105 | 138 |


| Major/Minor | Major1 | Major2 |  | Minor2 |  |  |
| :--- | :---: | :--- | :--- | :--- | ---: | ---: |
| Conflicting Flow All | - | 0 | - | 0 | 946 | 518 |
| Stage 1 | - | - | - | - | 518 | - |
| Stage 2 | - | - | - | - | 428 | - |
| Critical Hdwy | - | - | - | - | 6.48 | 6.6 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.48 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.48 | - |
| Follow-up Hdwy | - | - | - | - | 3.572 | 3.66 |
| Pot Cap-1 Maneuver | 0 | - | - | 0 | 283 | 489 |
| Stage 1 | 0 | - | - | 0 | 586 | - |
| Stage 2 | 0 | - | - | 0 | 645 | - |
| Platoon blocked, \% |  | - | - |  |  |  |
| Mov Cap-1 Maneuver | - | - | - | - | 283 | 489 |
| Mov Cap-2 Maneuver | - | - | - | - | 283 | - |
| Stage 1 | - | - | - | - | 586 | - |
| Stage 2 | - | - | - | - | 645 | - |


| Approach | EB | WB | SB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s | 0 | 0 | 31.2 |
| HCM LOS |  |  | D |


| Minor Lane/Major Mvmt | EBT | WBT SBLn1 |
| :--- | :---: | ---: |
| Capacity (veh/h) | - | -372 |
| HCM Lane V/C Ratio | - | -0.655 |
| HCM Control Delay (s) | - | -31.2 |
| HCM Lane LOS | - | - |
| HCM 95th \%tile Q(veh) | - | - |


| Intersection |  |
| :--- | ---: | :--- |
| Intersection Delay, s/veh | 18.2 |
| Intersection LOS | C |


| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Lane Configurations | 4 |  |  | 4 | 1 | $\mathbf{r}$ |
| Traffic Vol, veh/h | 401 | 0 | 0 | 462 | 76 | 99 |
| Future Vol, veh/h | 401 | 0 | 0 | 462 | 76 | 99 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, \% | 5 | 2 | 2 | 5 | 40 | 10 |
| Mvmt Flow | 436 | 0 | 0 | 502 | 83 | 108 |
| Number of Lanes | 1 | 0 | 0 | 1 | 1 | 1 |
| Approach | EB |  |  | WB | NB |  |
| Opposing Approach | WB |  |  | EB |  |  |
| Opposing Lanes | 1 |  |  | 1 | 0 |  |
| Conflicting Approach Left |  |  |  | NB | EB |  |
| Conflicting Lanes Left | 0 |  |  | 2 | 1 |  |
| Conflicting Approach Right | NB |  |  | 0 | WB |  |
| Conflicting Lanes Right | 2 |  |  | 1 |  |  |
| HCM Control Delay | 17.6 |  |  | 21.3 | 11.4 |  |
| HCM LOS | C |  |  | B |  |  |


| Lane | NBLn1 | NBLn2 | EBLn1 | WBLn1 |
| :--- | ---: | ---: | ---: | ---: |
| Vol Left, \% | $100 \%$ | $0 \%$ | $0 \%$ | $0 \%$ |
| Vol Thru, \% | $0 \%$ | $0 \%$ | $100 \%$ | $100 \%$ |
| Vol Right, \% | $0 \%$ | $100 \%$ | $0 \%$ | $0 \%$ |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 76 | 99 | 401 | 462 |
| LT Vol | 76 | 0 | 0 | 0 |
| Through Vol | 0 | 0 | 401 | 462 |
| RT Vol | 0 | 99 | 0 | 0 |
| Lane Flow Rate | 83 | 108 | 436 | 502 |
| Geometry Grp | 7 | 7 | 2 | 2 |
| Degree of Util (X) | 0.184 | 0.188 | 0.645 | 0.732 |
| Departure Headway (Hd) | 8.036 | 6.29 | 5.329 | 5.246 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 447 | 569 | 676 | 688 |
| Service Time | 5.785 | 4.038 | 3.365 | 3.279 |
| HCM Lane V/C Ratio | 0.186 | 0.19 | 0.645 | 0.73 |
| HCM Control Delay | 12.6 | 10.5 | 17.6 | 21.3 |
| HCM Lane LOS | B | B | C | C |
| HCM 95th-tile Q | 0.7 | 0.7 | 4.7 | 6.4 |


| Intersection |  |
| :--- | :--- |
| Intersection Delay, s/veh | 16 |
| Intersection LOS | C |


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ${ }^{7}$ | $\hat{\beta}$ |  | ${ }_{1}$ | $\hat{\beta}$ |  |  | $\uparrow$ | F' |  | $\dagger$ |  |
| Traffic Vol, veh/h | 12 | 230 | 24 | 251 | 159 | 29 | 10 | 4 | 245 | 64 | 3 | 3 |
| Future Vol, veh/h | 12 | 230 | 24 | 251 | 159 | 29 | 10 | 4 | 245 | 64 | 3 | 3 |
| Peak Hour Factor | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 40 | 2 | 2 | 2 | 2 | 25 | 2 | 2 | 2 |
| Mvmt Flow | 14 | 261 | 27 | 285 | 181 | 33 | 11 | 5 | 278 | 73 | 3 | 3 |
| Number of Lanes | 1 | 1 | 0 | 1 | 1 | 0 | 0 | 1 | 1 | 0 | 1 | 0 |
| Approach | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
| Opposing Approach | WB |  |  | EB |  |  | SB |  |  | NB |  |  |
| Opposing Lanes | 2 |  |  | 2 |  |  | 1 |  |  | 2 |  |  |
| Conflicting Approach Left | SB |  |  | NB |  |  | EB |  |  | WB |  |  |
| Conflicting Lanes Left | 1 |  |  | 2 |  |  | 2 |  |  | 2 |  |  |
| Conflicting Approach Right | NB |  |  | SB |  |  | WB |  |  | EB |  |  |
| Conflicting Lanes Right | 2 |  |  | 1 |  |  | 2 |  |  | 2 |  |  |
| HCM Control Delay | 16.2 |  |  | 17.2 |  |  | 14.8 |  |  | 12.5 |  |  |
| HCM LOS | C |  |  | C |  |  | B |  |  | B |  |  |


| Lane | NBLn1 | NBLn2 | EBLn1 | EBLn2 | WBLn1 | WBLn2 | SBLn1 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Vol Left, \% | $71 \%$ | $0 \%$ | $100 \%$ | $0 \%$ | $100 \%$ | $0 \%$ | $91 \%$ |
| Vol Thu, $\%$ | $29 \%$ | $0 \%$ | $0 \%$ | $91 \%$ | $0 \%$ | $85 \%$ | $4 \%$ |
| Vol Right, $\%$ | $0 \%$ | $100 \%$ | $0 \%$ | $9 \%$ | $0 \%$ | $15 \%$ | $4 \%$ |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 14 | 245 | 12 | 254 | 251 | 188 | 70 |
| LT Vol | 10 | 0 | 12 | 0 | 251 | 0 | 64 |
| Through Vol | 4 | 0 | 0 | 230 | 0 | 159 | 3 |
| RT Vol | 0 | 245 | 0 | 24 | 0 | 29 | 3 |
| Lane Flow Rate | 16 | 278 | 14 | 289 | 285 | 214 | 80 |
| Geometry Grp | 7 | 7 | 7 | 7 | 7 | 7 | 6 |
| Degree of Util (X) | 0.033 | 0.488 | 0.027 | 0.526 | 0.591 | 0.367 | 0.173 |
| Departure Headway (Hd) | 7.382 | 6.304 | 7.137 | 6.559 | 7.464 | 6.188 | 7.824 |
| Convergence, Y/N | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Cap | 482 | 568 | 498 | 546 | 482 | 577 | 461 |
| Service Time | 5.178 | 4.1 | 4.936 | 4.357 | 5.257 | 3.979 | 5.824 |
| HCM Lane V/C Ratio | 0.033 | 0.489 | 0.028 | 0.529 | 0.591 | 0.371 | 0.174 |
| HCM Control Delay | 10.4 | 15 | 10.1 | 16.5 | 20.6 | 12.6 | 12.5 |
| HCM Lane LOS | B | B | B | C | C | B | B |
| HCM 95th-tile Q | 0.1 | 2.7 | 0.1 | 3 | 3.8 | 1.7 | 0.6 |

## Intersection

Intersection Delay, s/veh 8.6
Intersection LOS
A


| Lane | NBLn1 EBLn1WBLn1 SBLn1 SBLn2 |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Vol Left, \% | $6 \%$ | $53 \%$ | $0 \%$ | $100 \%$ | $0 \%$ |
| Vol Thru, $\%$ | $94 \%$ | $28 \%$ | $56 \%$ | $0 \%$ | $78 \%$ |
| Vol Right, \% | $0 \%$ | $19 \%$ | $44 \%$ | $0 \%$ | $22 \%$ |
| Sign Control | Stop | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 83 | 32 | 9 | 36 | 93 |
| LT Vol | 5 | 17 | 0 | 36 | 0 |
| Through Vol | 78 | 9 | 5 | 0 | 73 |
| RT Vol | 0 | 6 | 4 | 0 | 20 |
| Lane Flow Rate | 94 | 36 | 10 | 41 | 106 |
| Geometry Grp | 5 | 2 | 2 | 7 | 7 |
| Degree of Util (X) | 0.114 | 0.046 | 0.012 | 0.073 | 0.156 |
| Departure Headway (Hd) | 4.34 | 4.56 | 4.331 | 6.406 | 5.329 |
| Convergence, Y/N | Yes | Yes | Yes | Yes | Yes |
| Cap | 830 | 789 | 830 | 558 | 671 |
| Service Time | 2.345 | 2.566 | 2.338 | 4.159 | 3.081 |
| HCM Lane V/C Ratio | 0.113 | 0.046 | 0.012 | 0.073 | 0.158 |
| HCM Control Delay | 7.9 | 7.8 | 7.4 | 9.7 | 9.1 |
| HCM Lane LOS | A | A | A | A | A |
| HCM 95th-tile Q | 0.4 | 0.1 | 0 | 0.2 | 0.6 |



| Major/Minor | Major1 | Major2 |  |  |  |  |  | Minor2 |  |  |
| :--- | ---: | :--- | ---: | :--- | ---: | ---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | - | 0 | - | 0 | 927 | 410 |  |  |  |  |
| $\quad$ Stage 1 | - | - | - | - | 410 | - |  |  |  |  |
| Stage 2 | - | - | - | - | 517 | - |  |  |  |  |
| Critical Hdwy | - | - | - | - | 6.48 | 6.6 |  |  |  |  |
| Critical Hdwy Stg 1 | - | - | - | - | 5.48 | - |  |  |  |  |
| Critical Hdwy Stg 2 | - | - | - | -5.48 | - |  |  |  |  |  |
| Follow-up Hdwy | - | - | - | -3.572 | 3.66 |  |  |  |  |  |
| Pot Cap-1 Maneuver | 0 | - | - | 0 | $\sim 291$ | 567 |  |  |  |  |
| $\quad$ Stage 1 | 0 | - | - | 0 | 657 | - |  |  |  |  |
| Stage 2 | 0 | - | - | 0 | 586 | - |  |  |  |  |
| Platoon blocked, \% |  | - | - |  |  |  |  |  |  |  |
| Mov Cap-1 Maneuver | - | - | - | $-\sim 291$ | 567 |  |  |  |  |  |
| Mov Cap-2 Maneuver | - | - | - | $-\sim 291$ | - |  |  |  |  |  |
| Stage 1 | - | - | - | - | 657 | - |  |  |  |  |
| Stage 2 | - | - | - | - | 586 | - |  |  |  |  |


| Approach | EB | WB | SB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, $s$ | 0 | 0 | 198.8 |
| HCM LOS |  |  | F |


| Minor Lane/Major Mvmt | EBT | WBT SBLn1 |  |
| :--- | ---: | ---: | ---: |
| Capacity (veh/h) | - | -336 |  |
| HCM Lane V/C Ratio | - | -1.329 |  |
| HCM Control Delay (s) | - | -198.8 |  |
| HCM Lane LOS | - | - | $F$ |
| HCM 95th \%otile Q(veh) | - | -21.6 |  |
| Notes |  |  |  |
| $:$ Volume exceeds capacity | $\$:$ Delay exceeds 300s | + Computation Not Defined $\quad *:$ All major volume in platoon |  |


| Intersection |  |
| :--- | ---: |
| Intersection Delay, s/veh | 124.1 |
| Intersection LOS | F |


| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Lane Configurations | $\mathbf{4}$ |  |  | 个 | a | $\overrightarrow{\mathbf{F}}$ |
| Traffic Vol, veh/h | 648 | 0 | 0 | 612 | 51 | 269 |
| Future Vol, veh/h | 648 | 0 | 0 | 612 | 51 | 269 |
| Peak Hour Factor | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 |
| Heavy Vehicles, \% | 5 | 2 | 2 | 5 | 40 | 10 |
| Mvmt Flow | 736 | 0 | 0 | 695 | 58 | 306 |
| Number of Lanes | 1 | 0 | 0 | 1 | 1 | 1 |


| Approach | EB | WB | NB |
| :--- | ---: | ---: | ---: |
| Opposing Approach | WB | EB |  |
| Opposing Lanes | 1 | 1 | 0 |
| Conflicting Approach Left |  | NB | EB |
| Conflicting Lanes Left | 0 | 2 | 1 |
| Conflicting Approach Right | NB |  | WB |
| Conflicting Lanes Right | 2 | 0 | 1 |
| HCM Control Delay | 164.2 | 136 | 20.3 |
| HCM LOS | F | F | C |


| Lane | NBLn1 | NBLn2 | EBLn1 | WBLn1 |
| :--- | ---: | ---: | ---: | ---: |
| Vol Left, \% | $100 \%$ | $0 \%$ | $0 \%$ | $0 \%$ |
| Vol Thru, \% | $0 \%$ | $0 \%$ | $100 \%$ | $100 \%$ |
| Vol Right, \% | $0 \%$ | $100 \%$ | $0 \%$ | $0 \%$ |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 51 | 269 | 648 | 612 |
| LT Vol | 51 | 0 | 0 | 0 |
| Through Vol | 0 | 0 | 648 | 612 |
| RT Vol | 0 | 269 | 0 | 0 |
| Lane Flow Rate | 58 | 306 | 736 | 695 |
| Geometry Grp | 7 | 7 | 2 | 2 |
| Degree of Util (X) | 0.141 | 0.6 | 1.288 | 1.216 |
| Departure Headway (Hd) | 9.569 | 7.792 | 6.641 | 6.722 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 377 | 468 | 552 | 549 |
| Service Time | 7.269 | 5.492 | 4.641 | 4.722 |
| HCM Lane V/C Ratio | 0.154 | 0.654 | 1.333 | 1.266 |
| HCM Control Delay | 13.8 | 21.5 | 164.2 | 136 |
| HCM Lane LOS | B | C | F | F |
| HCM 95th-tile Q | 0.5 | 3.9 | 28.7 | 24.4 |



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ${ }^{1}$ | $\uparrow$ |  | ${ }^{*}$ | F |  |  | $\uparrow$ | 「 |  | * |  |
| Traffic Vol, veh/h | 9 | 200 | 23 | 312 | 276 | 126 | 24 | 7 | 262 | 105 | 6 | 14 |
| Future Vol, veh/h | 9 | 200 | 23 | 312 | 276 | 126 | 24 | 7 | 262 | 105 | 6 | 14 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 40 | 2 | 2 | 2 | 2 | 25 | 2 | 2 | 2 |
| Mvmt Flow | 10 | 217 | 25 | 339 | 300 | 137 | 26 | 8 | 285 | 114 | 7 | 15 |
| Number of Lanes | 1 | 1 | 0 | 1 | 1 | 0 | 0 | 1 | 1 | 0 | 1 | 0 |
| Approach | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
| Opposing Approach | WB |  |  | EB |  |  | SB |  |  | NB |  |  |
| Opposing Lanes | 2 |  |  | 2 |  |  | 1 |  |  | 2 |  |  |
| Conflicting Approach Left | SB |  |  | NB |  |  | EB |  |  | WB |  |  |
| Conflicting Lanes Left | 1 |  |  | 2 |  |  | 2 |  |  | 2 |  |  |
| Conflicting Approach Right | NB |  |  | SB |  |  | WB |  |  | EB |  |  |
| Conflicting Lanes Right | 2 |  |  | 1 |  |  | 2 |  |  | 2 |  |  |
| HCM Control Delay | 17.6 |  |  | 31 |  |  | 17.7 |  |  | 15.1 |  |  |
| HCM LOS | C |  |  | D |  |  | C |  |  | C |  |  |


| Lane | NBLn1 | NBLn2 | EBLn1 | EBLn2 | WBLn1 | WBLn2 | SBLn1 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Vol Left, \% | $77 \%$ | $0 \%$ | $100 \%$ | $0 \%$ | $100 \%$ | $0 \%$ | $84 \%$ |
| Vol Thru, \% | $23 \%$ | $0 \%$ | $0 \%$ | $90 \%$ | $0 \%$ | $69 \%$ | $5 \%$ |
| Vol Right, \% | $0 \%$ | $100 \%$ | $0 \%$ | $10 \%$ | $0 \%$ | $31 \%$ | $11 \%$ |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 31 | 262 | 9 | 223 | 312 | 402 | 125 |
| LT Vol | 24 | 0 | 9 | 0 | 312 | 0 | 105 |
| Through Vol | 7 | 0 | 0 | 200 | 0 | 276 | 6 |
| RT Vol | 0 | 262 | 0 | 23 | 0 | 126 | 14 |
| Lane Flow Rate | 34 | 285 | 10 | 242 | 339 | 437 | 136 |
| Geometry Grp | 7 | 7 | 7 | 7 | 7 | 7 | 6 |
| Degree of Util (X) | 0.077 | 0.559 | 0.022 | 0.508 | 0.752 | 0.799 | 0.313 |
| Departure Headway (Hd) | 8.177 | 7.062 | 8.129 | 7.54 | 7.98 | 6.584 | 8.282 |
| Convergence, Y/N | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Cap | 438 | 510 | 440 | 478 | 454 | 551 | 433 |
| Service Time | 5.919 | 4.804 | 5.881 | 5.292 | 5.727 | 4.33 | 6.336 |
| HCM Lane VIC Ratio | 0.078 | 0.559 | 0.023 | 0.506 | 0.747 | 0.793 | 0.314 |
| HCM Control Delay | 11.6 | 18.4 | 11.1 | 17.9 | 31.3 | 30.7 | 15.1 |
| HCM Lane LOS | B | C | B | C | D | D | C |
| HCM 95th-tile Q | 0.2 | 3.4 | 0.1 | 2.8 | 6.3 | 7.6 | 1.3 |

```
Intersection
Intersection Delay, s/veh 9.2
Intersection LOS
```



| Lane | NBLn1 EBLn1WBLn1 SBLn1 SBLn2 |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Vol Left, \% | $4 \%$ | $55 \%$ | $0 \%$ | $100 \%$ | $0 \%$ |
| Vol Thru, \% | $96 \%$ | $29 \%$ | $56 \%$ | $0 \%$ | $88 \%$ |
| Vol Right, \% | $0 \%$ | $16 \%$ | $44 \%$ | $0 \%$ | $12 \%$ |
| Sign Control | Stop | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 119 | 31 | 9 | 35 | 159 |
| LT Vol | 5 | 17 | 0 | 35 | 0 |
| Through Vol | 114 | 9 | 5 | 0 | 140 |
| RT Vol | 0 | 5 | 4 | 0 | 19 |
| Lane Flow Rate | 129 | 34 | 10 | 38 | 173 |
| Geometry Grp | 5 | 2 | 2 | 7 | 7 |
| Degree of Util (X) | 0.158 | 0.045 | 0.012 | 0.068 | 0.26 |
| Departure Headway (Hd) | 4.411 | 4.826 | 4.577 | 6.42 | 5.409 |
| Convergence, Y/N | Yes | Yes | Yes | Yes | Yes |
| Cap | 817 | 745 | 784 | 556 | 660 |
| Service Time | 2.417 | 2.835 | 2.59 | 4.183 | 3.172 |
| HCM Lane V/C Ratio | 0.158 | 0.046 | 0.013 | 0.068 | 0.262 |
| HCM Control Delay | 8.2 | 8.1 | 7.6 | 9.7 | 10.1 |
| HCM Lane LOS | A | A | A | A | B |
| HCM 95th-tile Q | 0.6 | 0.1 | 0 | 0.2 | 1 |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 185.8 |  |  |  |  |  |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations |  | 4 | 个 |  | Mr |  |
| Traffic Vol, veh/h | 0 | 451 | 554 | 0 | 358 | 169 |
| Future Vol, veh/h | 0 | 451 | 554 | 0 | 358 | 169 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, $\#$ | - | 0 | 0 | - | 0 | - |
| Grade, \% | - | 5 | -5 | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 5 | 10 | 10 | 8 | 40 |
| Mvmt Flow | 0 | 490 | 602 | 0 | 389 | 184 |



| Approach | EB | WB | SB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, $s$ | 0 | 0 | $\$ 540$ |
| HCM LOS |  | $F$ |  |


| Minor Lane/Major Mvmt | EBT | WBT SBLn1 |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Capacity (veh/h) | - | - 272 |  |  |
| HCM Lane V/C Ratio | - | - 2.106 |  |  |
| HCM Control Delay (s) | - | - \$ 540 |  |  |
| HCM Lane LOS | - | F |  |  |
| HCM 95th \%taile Q(veh) | - | - 42.6 |  |  |
| Notes |  |  |  |  |
| $\sim$ : Volume exceeds capacity | \$: Delay exceeds 300s |  | +: Computation Not Defined | *: All major volume in platoon |


| Intersection |  |
| :--- | ---: | :--- |
| Intersection Delay, s/veh $\quad 183.3$ |  |
| Intersection LOS | F |


| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Lane Configurations | 个 |  |  | $\mathbf{4}$ | $\mathbf{7}$ | $\mathbf{7}$ |
| Traffic Vol, veh/h | 695 | 0 | 0 | 736 | 125 | 355 |
| Future Vol, veh/h | 695 | 0 | 0 | 736 | 125 | 355 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, \% | 5 | 2 | 2 | 5 | 40 | 10 |
| Mvmt Flow | 755 | 0 | 0 | 800 | 136 | 386 |
| Number of Lanes | 1 | 0 | 0 | 1 | 1 | 1 |
| Approach | EB |  |  | WB | NB |  |
| Opposing Approach | WB |  |  | EB |  |  |
| Opposing Lanes | 1 |  | 1 | 0 |  |  |
| Conflicting Approach Left |  |  | NB | EB |  |  |
| Conflicting Lanes Left | 0 |  |  | 2 | 1 |  |
| Conflicting Approach Right | NB |  |  | WB |  |  |
| Conflicting Lanes Right | 2 |  | 0 | 1 |  |  |
| HCM Control Delay | 217.3 |  | 252.1 | 28.5 |  |  |
| HCM LOS | F |  | F | D |  |  |


| Lane | NBLn1 | NBLn2 | EBLn1 | WBLn1 |
| :--- | ---: | ---: | ---: | ---: |
| Vol Left, \% | $100 \%$ | $0 \%$ | $0 \%$ | $0 \%$ |
| Vol Thru, \% | $0 \%$ | $0 \%$ | $100 \%$ | $100 \%$ |
| Vol Right, \% | $0 \%$ | $100 \%$ | $0 \%$ | $0 \%$ |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 125 | 355 | 695 | 736 |
| LT Vol | 125 | 0 | 0 | 0 |
| Through Vol | 0 | 0 | 695 | 736 |
| RT Vol | 0 | 355 | 0 | 0 |
| Lane Flow Rate | 136 | 386 | 755 | 800 |
| Geometry Grp | 7 | 7 | 2 | 2 |
| Degree of Util (X) | 0.331 | 0.757 | 1.409 | 1.492 |
| Departure Headway (Hd) | 9.988 | 8.202 | 7.429 | 7.328 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 363 | 444 | 499 | 504 |
| Service Time | 7.688 | 5.902 | 5.429 | 5.328 |
| HCM Lane V/C Ratio | 0.375 | 0.869 | 1.513 | 1.587 |
| HCM Control Delay | 17.6 | 32.3 | 217.3 | 252.1 |
| HCM Lane LOS | C | D | F | F |
| HCM 95th-tile Q | 1.4 | 6.3 | 32.6 | 37.5 |


|  | $\rangle$ | $\rightarrow$ | 7 | $\dagger$ |  | 4 | 4 | 4 | $p$ |  | $\dagger$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{*}$ | $\hat{\beta}$ |  | ${ }^{7}$ | $\hat{\beta}$ |  |  | $\uparrow$ | 「 |  | ¢ |  |
| Traffic Volume (veh/h) | 12 | 230 | 24 | 251 | 159 | 29 | 10 | 4 | 245 | 64 | 3 | 3 |
| Future Volume (veh/h) | 12 | 230 | 24 | 251 | 159 | 29 | 10 | 4 | 245 | 64 | 3 | 3 |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | 5 | 2 | 12 | 1 | 6 | 16 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 1863 | 1863 | 1900 | 1357 | 1863 | 1900 | 1900 | 1863 | 1520 | 1900 | 1863 | 1900 |
| Adj Flow Rate, veh/h | 14 | 261 | 27 | 285 | 181 | 33 | 11 | 5 | 0 | 73 | 3 | 3 |
| Adj No. of Lanes | 1 | 1 | 0 | 1 | 1 | 0 | 0 | 1 | 1 | 0 | 1 | 0 |
| Peak Hour Factor | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 |
| Percent Heavy Veh, \% | 2 | 2 | 2 | 40 | 2 | 2 | 2 | 2 | 25 | 2 | 2 | 2 |
| Cap, veh/h | 24 | 305 | 32 | 321 | 643 | 117 | 505 | 216 | 539 | 635 | 26 | 23 |
| Arrive On Green | 0.01 | 0.18 | 0.18 | 0.25 | 0.42 | 0.42 | 0.42 | 0.42 | 0.00 | 0.42 | 0.42 | 0.42 |
| Sat Flow, veh/h | 1774 | 1661 | 172 | 1293 | 1534 | 280 | 1027 | 518 | 1292 | 1312 | 63 | 54 |
| Grp Volume(v), veh/h | 14 | 0 | 288 | 285 | 0 | 214 | 16 | 0 | 0 | 79 | 0 | 0 |
| Grp Sat Flow(s),veh/h/n | 1774 | 0 | 1832 | 1293 | 0 | 1813 | 1545 | 0 | 1292 | 1429 | 0 | 0 |
| Q Serve(g_s), s | 0.6 | 0.0 | 12.2 | 17.0 | 0.0 | 6.2 | 0.0 | 0.0 | 0.0 | 2.2 | 0.0 | 0.0 |
| Cycle Q Clear(g_c), s | 0.6 | 0.0 | 12.2 | 17.0 | 0.0 | 6.2 | 0.4 | 0.0 | 0.0 | 2.6 | 0.0 | 0.0 |
| Prop In Lane | 1.00 |  | 0.09 | 1.00 |  | 0.15 | 0.69 |  | 1.00 | 0.92 |  | 0.04 |
| Lane Grp Cap(c), veh/h | 24 | 0 | 337 | 321 | 0 | 760 | 721 | 0 | 539 | 683 | 0 | 0 |
| VIC Ratio(X) | 0.59 | 0.00 | 0.85 | 0.89 | 0.00 | 0.28 | 0.02 | 0.00 | 0.00 | 0.12 | 0.00 | 0.00 |
| Avail Cap(c_a), veh/h | 89 | 0 | 458 | 501 | 0 | 1065 | 721 | 0 | 539 | 683 | 0 | 0 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| Uniform Delay (d), s/veh | 39.2 | 0.0 | 31.6 | 29.0 | 0.0 | 15.3 | 13.7 | 0.0 | 0.0 | 14.3 | 0.0 | 0.0 |
| Incr Delay (d2), s/veh | 21.2 | 0.0 | 11.2 | 11.6 | 0.0 | 0.2 | 0.1 | 0.0 | 0.0 | 0.3 | 0.0 | 0.0 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/ln | 0.4 | 0.0 | 7.2 | 7.1 | 0.0 | 3.1 | 0.2 | 0.0 | 0.0 | 1.1 | 0.0 | 0.0 |
| LnGrp Delay (d),s/veh | 60.4 | 0.0 | 42.8 | 40.6 | 0.0 | 15.5 | 13.7 | 0.0 | 0.0 | 14.7 | 0.0 | 0.0 |
| LnGrp LOS | E |  | D | D |  | B | B |  |  | B |  |  |
| Approach Vol, veh/h |  | 302 |  |  | 499 |  |  | 16 |  |  | 79 |  |
| Approach Delay, s/veh |  | 43.6 |  |  | 29.8 |  |  | 13.7 |  |  | 14.7 |  |
| Approach LOS |  | D |  |  | C |  |  | B |  |  | B |  |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |  |  |  |  |
| Assigned Phs |  | 2 | 3 | 4 |  | 6 | 7 | 8 |  |  |  |  |
| Phs Duration ( $\mathrm{G}+\mathrm{Y}+\mathrm{Rc}$ ), s |  | 37.4 | 23.9 | 18.7 |  | 37.4 | 5.1 | 37.5 |  |  |  |  |
| Change Period ( $Y+R \mathrm{C})$, s |  | 4.0 | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 |  |  |  |  |
| Max Green Setting (Gmax), s |  | 17.0 | 31.0 | 20.0 |  | 17.0 | 4.0 | 47.0 |  |  |  |  |
| Max Q Clear Time ( $\left.\mathrm{g}_{\text {c }} \mathrm{c}+11\right)$, s |  | 2.4 | 19.0 | 14.2 |  | 4.6 | 2.6 | 8.2 |  |  |  |  |
| Green Ext Time (p_c), s |  | 0.0 | 0.9 | 0.5 |  | 0.2 | 0.0 | 0.8 |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 2010 Ctrl Delay |  |  | 32.9 |  |  |  |  |  |  |  |  |  |
| HCM 2010 LOS |  |  | C |  |  |  |  |  |  |  |  |  |


|  | 4 | $\rightarrow$ |  | 4 | $\pm$ | 4 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |  |  |
| Lane Configurations |  | 4 | 4 |  | * |  |  |  |
| Traffic Volume (veh/h) | 0 | 455 | 361 | 0 | 285 | 108 |  |  |
| Future Volume (veh/h) | 0 | 455 | 361 | 0 | 285 | 108 |  |  |
| Number | 7 | 4 | 8 | 18 | 1 | 16 |  |  |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 |  |  |
| Ped-Bike Adj(A_pbT) | 1.00 |  |  | 1.00 | 1.00 | 1.00 |  |  |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |
| Adj Sat Flow, veh/h/ln | 0 | 1764 | 1770 | 0 | 1627 | 1900 |  |  |
| Adj Flow Rate, veh/h | 0 | 517 | 410 | 0 | 324 | 123 |  |  |
| Adj No. of Lanes | 0 | 1 | 1 | 0 | 0 | 0 |  |  |
| Peak Hour Factor | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 |  |  |
| Percent Heavy Veh, \% | 0 | 5 | 10 | 0 | 0 | 0 |  |  |
| Cap, veh/h | 0 | 574 | 576 | 0 | 623 | 237 |  |  |
| Arrive On Green | 0.00 | 0.33 | 0.33 | 0.00 | 0.57 | 0.57 |  |  |
| Sat Flow, veh/h | 0 | 1764 | 1770 | 0 | 1085 | 412 |  |  |
| Grp Volume(v), veh/h | 0 | 517 | 410 | 0 | 448 | 0 |  |  |
| Grp Sat Flow(s),veh/h/ln | 0 | 1764 | 1770 | 0 | 1500 | 0 |  |  |
| Q Serve(g_s), s | 0.0 | 22.4 | 16.3 | 0.0 | 14.5 | 0.0 |  |  |
| Cycle Q Clear(g_c), s | 0.0 | 22.4 | 16.3 | 0.0 | 14.5 | 0.0 |  |  |
| Prop In Lane | 0.00 |  |  | 0.00 | 0.72 | 0.27 |  |  |
| Lane Grp Cap(c), veh/h | 0 | 574 | 576 | 0 | 862 | 0 |  |  |
| V/C Ratio(X) | 0.00 | 0.90 | 0.71 | 0.00 | 0.52 | 0.00 |  |  |
| Avail Cap(c_a), veh/h | 0 | 772 | 775 | 0 | 862 | 0 |  |  |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |
| Upstream Filter(I) | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 | 0.00 |  |  |
| Uniform Delay (d), s/veh | 0.0 | 25.7 | 23.7 | 0.0 | 10.3 | 0.0 |  |  |
| Incr Delay (d2), s/veh | 0.0 | 11.0 | 2.0 | 0.0 | 2.2 | 0.0 |  |  |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |
| \%ile BackOfQ(50\%),veh/ln | 0.0 | 12.5 | 8.2 | 0.0 | 6.5 | 0.0 |  |  |
| LnGrp Delay(d),s/veh | 0.0 | 36.7 | 25.7 | 0.0 | 12.6 | 0.0 |  |  |
| LnGrp LOS |  | D | C |  | B |  |  |  |
| Approach Vol, veh/h |  | 517 | 410 |  | 448 |  |  |  |
| Approach Delay, s/veh |  | 36.7 | 25.7 |  | 12.6 |  |  |  |
| Approach LOS |  | D | C |  | B |  |  |  |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| Assigned Phs |  |  |  | 4 |  | 6 |  | 8 |
| Phs Duration ( $G+Y+R \mathrm{c}$ ), s |  |  |  | 30.0 |  | 50.0 |  | 30.0 |
| Change Period ( $\mathrm{Y}+\mathrm{Rc}$ ), s |  |  |  | 4.0 |  | 4.0 |  | 4.0 |
| Max Green Setting (Gmax), s |  |  |  | 35.0 |  | 37.0 |  | 35.0 |
| Max Q Clear Time ( $\left.g_{-} \mathrm{c}+11\right)$, s |  |  |  | 24.4 |  | 16.5 |  | 18.3 |
| Green Ext Time (p_c), s |  |  |  | 1.7 |  | 2.0 |  | 1.5 |
| Intersection Summary |  |  |  |  |  |  |  |  |
| HCM 2010 Ctrl Delay |  |  | 25.6 |  |  |  |  |  |
| HCM 2010 LOS |  |  | C |  |  |  |  |  |
| Notes |  |  |  |  |  |  |  |  |


|  | $\rightarrow$ | \% | 7 |  | 4 | $p$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |  |  |
| Lane Configurations | 4 |  |  | 4 | ${ }^{1}$ | 「 |  |  |
| Traffic Volume (veh/h) | 648 | 0 | 0 | 612 | 51 | 269 |  |  |
| Future Volume (veh/h) | 648 | 0 | 0 | 612 | 51 | 269 |  |  |
| Number | 4 | 14 | 3 | 8 | 5 | 12 |  |  |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 |  |  |
| Ped-Bike Adj(A_pbT) |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  |  |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |
| Adj Sat Flow, veh/h/ln | 1855 | 0 | 0 | 1764 | 1357 | 1727 |  |  |
| Adj Flow Rate, veh/h | 736 | 0 | 0 | 695 | 58 | 306 |  |  |
| Adj No. of Lanes | 1 | 0 | 0 | 1 | 1 | 1 |  |  |
| Peak Hour Factor | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 |  |  |
| Percent Heavy Veh, \% | 5 | 0 | 0 | 5 | 40 | 10 |  |  |
| Cap, veh/h | 807 | 0 | 0 | 768 | 601 | 682 |  |  |
| Arrive On Green | 0.44 | 0.00 | 0.00 | 0.44 | 0.46 | 0.46 |  |  |
| Sat Flow, veh/h | 1855 | 0 | 0 | 1764 | 1293 | 1468 |  |  |
| Grp Volume(v), veh/h | 736 | 0 | 0 | 695 | 58 | 306 |  |  |
| Grp Sat Flow(s),veh/h/ln | 1855 | 0 | 0 | 1764 | 1293 | 1468 |  |  |
| Q Serve(g_s), s | 29.7 | 0.0 | 0.0 | 29.4 | 2.0 | 11.3 |  |  |
| Cycle Q Clear(g_c), s | 29.7 | 0.0 | 0.0 | 29.4 | 2.0 | 11.3 |  |  |
| Prop In Lane |  | 0.00 | 0.00 |  | 1.00 | 1.00 |  |  |
| Lane Grp Cap(c), veh/h | 807 | 0 | 0 | 768 | 601 | 682 |  |  |
| V/C Ratio(X) | 0.91 | 0.00 | 0.00 | 0.90 | 0.10 | 0.45 |  |  |
| Avail Cap(c_a), veh/h | 1090 | 0 | 0 | 1037 | 601 | 682 |  |  |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |
| Upstream Filter(I) | 1.00 | 0.00 | 0.00 | 1.00 | 1.00 | 1.00 |  |  |
| Uniform Delay (d), s/veh | 21.1 | 0.0 | 0.0 | 21.0 | 12.0 | 14.5 |  |  |
| Incr Delay (d2), s/veh | 9.2 | 0.0 | 0.0 | 8.9 | 0.3 | 2.1 |  |  |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |
| \%ile BackOfQ(50\%),veh/ln | 17.2 | 0.0 | 0.0 | 16.0 | 0.8 | 4.9 |  |  |
| LnGrp Delay(d),s/veh | 30.3 | 0.0 | 0.0 | 30.0 | 12.3 | 16.6 |  |  |
| LnGrp LOS | C |  |  | C | B | B |  |  |
| Approach Vol, veh/h | 736 |  |  | 695 | 364 |  |  |  |
| Approach Delay, s/veh | 30.3 |  |  | 30.0 | 15.9 |  |  |  |
| Approach LOS | C |  |  | C | B |  |  |  |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| Assigned Phs |  | 2 |  | 4 |  |  |  | 8 |
| Phs Duration ( $\mathrm{G}+\mathrm{Y}+\mathrm{Rc}$ ), s |  | 41.2 |  | 38.8 |  |  |  | 38.8 |
| Change Period ( $\mathrm{Y}+\mathrm{Rc}$ ), s |  | 4.0 |  | 4.0 |  |  |  | 4.0 |
| Max Green Setting (Gmax), s |  | 25.0 |  | 47.0 |  |  |  | 47.0 |
| Max Q Clear Time (g_c+l1), s |  | 13.3 |  | 31.7 |  |  |  | 31.4 |
| Green Ext Time (p_c), s |  | 1.3 |  | 3.1 |  |  |  | 2.9 |
| Intersection Summary |  |  |  |  |  |  |  |  |
| HCM 2010 Ctrl Delay |  |  | 27.3 |  |  |  |  |  |
| HCM 2010 LOS |  |  | C |  |  |  |  |  |


|  | $y$ |  |  | $\checkmark$ |  |  | 4 | 4 | 7 |  | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \% | $\uparrow$ |  | \% | $\uparrow$ |  |  | $\uparrow$ | 「 |  | \$ |  |
| Traffic Volume (veh/h) | 9 | 200 | 23 | 312 | 276 | 126 | 24 | 7 | 262 | 105 | 6 | 14 |
| Future Volume (veh/h) | 9 | 200 | 23 | 312 | 276 | 126 | 24 | 7 | 262 | 105 | 6 | 14 |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | 5 | 2 | 12 | 1 | 6 | 16 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 1863 | 1863 | 1900 | 1357 | 1863 | 1900 | 1900 | 1863 | 1520 | 1900 | 1863 | 1900 |
| Adj Flow Rate, veh/h | 10 | 217 | 25 | 339 | 300 | 137 | 26 | 8 | 0 | 114 | 7 | 15 |
| Adj No. of Lanes | 1 | 1 | 0 | 1 | 1 | 0 | 0 | 1 | 1 | 0 | 1 | 0 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh, \% | 2 | 2 | 2 | 40 | 2 | 2 | 2 | 2 | 25 | 2 | 2 | 2 |
| Cap, veh/h | 18 | 259 | 30 | 377 | 532 | 243 | 535 | 154 | 518 | 562 | 37 | 64 |
| Arrive On Green | 0.01 | 0.16 | 0.16 | 0.29 | 0.44 | 0.44 | 0.40 | 0.40 | 0.00 | 0.40 | 0.40 | 0.40 |
| Sat Flow, veh/h | 1774 | 1640 | 189 | 1293 | 1212 | 553 | 1137 | 385 | 1292 | 1196 | 93 | 160 |
| Grp Volume(v), veh/h | 10 | 0 | 242 | 339 | 0 | 437 | 34 | 0 | 0 | 136 | 0 | 0 |
| Grp Sat Flow(s),veh/h/n | 1774 | 0 | 1829 | 1293 | 0 | 1765 | 1522 | 0 | 1292 | 1448 | 0 | 0 |
| Q Serve(g_s), s | 0.4 | 0.0 | 10.3 | 20.2 | 0.0 | 14.8 | 0.0 | 0.0 | 0.0 | 3.9 | 0.0 | 0.0 |
| Cycle Q Clear(g_c), s | 0.4 | 0.0 | 10.3 | 20.2 | 0.0 | 14.8 | 0.9 | 0.0 | 0.0 | 4.8 | 0.0 | 0.0 |
| Prop In Lane | 1.00 |  | 0.10 | 1.00 |  | 0.31 | 0.76 |  | 1.00 | 0.84 |  | 0.11 |
| Lane Grp Cap(c), veh/h | 18 | 0 | 289 | 377 | 0 | 776 | 689 | 0 | 518 | 663 | 0 | 0 |
| VIC Ratio(X) | 0.57 | 0.00 | 0.84 | 0.90 | 0.00 | 0.56 | 0.05 | 0.00 | 0.00 | 0.21 | 0.00 | 0.00 |
| Avail Cap(c_a), veh/h | 89 | 0 | 389 | 565 | 0 | 1059 | 689 | 0 | 518 | 663 | 0 | 0 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(1) | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| Uniform Delay (d), s/veh | 39.4 | 0.0 | 32.7 | 27.2 | 0.0 | 16.7 | 14.6 | 0.0 | 0.0 | 15.7 | 0.0 | 0.0 |
| Incr Delay (d2), s/veh | 25.4 | 0.0 | 11.4 | 12.5 | 0.0 | 0.6 | 0.1 | 0.0 | 0.0 | 0.7 | 0.0 | 0.0 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/ln | 0.3 | 0.0 | 6.1 | 8.5 | 0.0 | 7.3 | 0.5 | 0.0 | 0.0 | 2.1 | 0.0 | 0.0 |
| LnGrp Delay ${ }^{\text {d }}$ ),s/veh | 64.8 | 0.0 | 44.0 | 39.7 | 0.0 | 17.4 | 14.8 | 0.0 | 0.0 | 16.4 | 0.0 | 0.0 |
| LnGrp LOS | E |  | D | D |  | B | B |  |  | B |  |  |
| Approach Vol, veh/h |  | 252 |  |  | 776 |  |  | 34 |  |  | 136 |  |
| Approach Delay, s/veh |  | 44.9 |  |  | 27.1 |  |  | 14.8 |  |  | 16.4 |  |
| Approach LOS |  | D |  |  | C |  |  | B |  |  | B |  |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |  |  |  |  |
| Assigned Phs |  | 2 | 3 | 4 |  | 6 | 7 | 8 |  |  |  |  |
| Phs Duration ( $\mathrm{G}+\mathrm{Y}+\mathrm{Rc}$ ), s |  | 36.1 | 27.3 | 16.6 |  | 36.1 | 4.8 | 39.2 |  |  |  |  |
| Change Period ( $Y+R \mathrm{R}$ ), s |  | 4.0 | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 |  |  |  |  |
| Max Green Setting (Gmax), s |  | 16.0 | 35.0 | 17.0 |  | 16.0 | 4.0 | 48.0 |  |  |  |  |
| Max Q Clear Time (g_c+1), $s$ |  | 2.9 | 22.2 | 12.3 |  | 6.8 | 2.4 | 16.8 |  |  |  |  |
| Green Ext Time (p_c), s |  | 0.0 | 1.2 | 0.4 |  | 0.3 | 0.0 | 1.9 |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 2010 Ctrl Delay |  |  | 29.3 |  |  |  |  |  |  |  |  |  |
| HCM 2010 LOS |  |  | C |  |  |  |  |  |  |  |  |  |


|  | 4 |  |  |  |  | $\downarrow$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |  |  |
| Lane Configurations |  | 4 | 4 |  | */ |  |  |  |
| Traffic Volume (veh/h) | 0 | 451 | 554 | 0 | 358 | 169 |  |  |
| Future Volume (veh/h) | 0 | 451 | 554 | 0 | 358 | 169 |  |  |
| Number | 7 | 4 | 8 | 18 | 1 | 16 |  |  |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 |  |  |
| Ped-Bike Adj(A_pbT) | 1.00 |  |  | 1.00 | 1.00 | 1.00 |  |  |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |
| Adj Sat Flow, veh/h/ln | 0 | 1764 | 1770 | 0 | 1606 | 1900 |  |  |
| Adj Flow Rate, veh/h | 0 | 490 | 602 | 0 | 389 | 184 |  |  |
| Adj No. of Lanes | 0 | 1 | 1 | 0 | 0 | 0 |  |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |  |  |
| Percent Heavy Veh, \% | 0 | 5 | 10 | 0 | 0 | 0 |  |  |
| Cap, veh/h | 0 | 652 | 655 | 0 | 529 | 250 |  |  |
| Arrive On Green | 0.00 | 0.37 | 0.37 | 0.00 | 0.53 | 0.53 |  |  |
| Sat Flow, veh/h | 0 | 1764 | 1770 | 0 | 998 | 472 |  |  |
| Grp Volume(v), veh/h | 0 | 490 | 602 | 0 | 574 | 0 |  |  |
| Grp Sat Flow(s),veh/h/ln | 0 | 1764 | 1770 | 0 | 1473 | 0 |  |  |
| Q Serve(g_s), s | 0.0 | 19.4 | 26.0 | 0.0 | 24.0 | 0.0 |  |  |
| Cycle Q Clear(g_c), s | 0.0 | 19.4 | 26.0 | 0.0 | 24.0 | 0.0 |  |  |
| Prop In Lane | 0.00 |  |  | 0.00 | 0.68 | 0.32 |  |  |
| Lane Grp Cap(c), veh/h | 0 | 652 | 655 | 0 | 781 | 0 |  |  |
| V/C Ratio(X) | 0.00 | 0.75 | 0.92 | 0.00 | 0.73 | 0.00 |  |  |
| Avail Cap(c_a), veh/h | 0 | 772 | 775 | 0 | 781 | 0 |  |  |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |
| Upstream Filter(I) | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 | 0.00 |  |  |
| Uniform Delay (d), s/veh | 0.0 | 22.0 | 24.1 | 0.0 | 14.5 | 0.0 |  |  |
| Incr Delay (d2), s/veh | 0.0 | 3.5 | 14.6 | 0.0 | 6.1 | 0.0 |  |  |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |
| \%ile BackOfQ(50\%),veh/ln | 0.0 | 10.0 | 15.4 | 0.0 | 10.9 | 0.0 |  |  |
| LnGrp Delay(d),s/veh | 0.0 | 25.4 | 38.6 | 0.0 | 20.5 | 0.0 |  |  |
| LnGrp LOS |  | C | D |  | C |  |  |  |
| Approach Vol, veh/h |  | 490 | 602 |  | 574 |  |  |  |
| Approach Delay, s/veh |  | 25.4 | 38.6 |  | 20.5 |  |  |  |
| Approach LOS |  | C | D |  | C |  |  |  |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| Assigned Phs |  |  |  | 4 |  | 6 |  | 8 |
| Phs Duration ( $G+Y+R c$ ), $s$ |  |  |  | 33.6 |  | 46.4 |  | 33.6 |
| Change Period (Y+Rc), s |  |  |  | 4.0 |  | 4.0 |  | 4.0 |
| Max Green Setting (Gmax), s |  |  |  | 35.0 |  | 37.0 |  | 35.0 |
| Max Q Clear Time (g_c+l1), s |  |  |  | 21.4 |  | 26.0 |  | 28.0 |
| Green Ext Time (p_c), s |  |  |  | 1.7 |  | 2.2 |  | 1.6 |
| Intersection Summary |  |  |  |  |  |  |  |  |
| HCM 2010 Ctrl Delay |  |  | 28.5 |  |  |  |  |  |
| HCM 2010 LOS |  |  | C |  |  |  |  |  |
| Notes |  |  |  |  |  |  |  |  |


|  | $\rightarrow$ |  | $\%$ |  | 4 | $p$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |  |  |
| Lane Configurations | 4 |  |  | 4 | ${ }^{1}$ | 「 |  |  |
| Traffic Volume (veh/h) | 695 | 0 | 0 | 736 | 125 | 355 |  |  |
| Future Volume (veh/h) | 695 | 0 | 0 | 736 | 125 | 355 |  |  |
| Number | 4 | 14 | 3 | 8 | 5 | 12 |  |  |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 |  |  |
| Ped-Bike Adj(A_pbT) |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  |  |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |
| Adj Sat Flow, veh/h/ln | 1855 | 0 | 0 | 1764 | 1357 | 1727 |  |  |
| Adj Flow Rate, veh/h | 755 | 0 | 0 | 800 | 136 | 386 |  |  |
| Adj No. of Lanes | 1 | 0 | 0 | 1 | 1 | 1 |  |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |  |  |
| Percent Heavy Veh, \% | 5 | 0 | 0 | 5 | 40 | 10 |  |  |
| Cap, veh/h | 905 | 0 | 0 | 861 | 533 | 605 |  |  |
| Arrive On Green | 0.49 | 0.00 | 0.00 | 0.49 | 0.41 | 0.41 |  |  |
| Sat Flow, veh/h | 1855 | 0 | 0 | 1764 | 1293 | 1468 |  |  |
| Grp Volume(v), veh/h | 755 | 0 | 0 | 800 | 136 | 386 |  |  |
| Grp Sat Flow(s), veh/h/ln | 1855 | 0 | 0 | 1764 | 1293 | 1468 |  |  |
| Q Serve(g_s), s | 28.1 | 0.0 | 0.0 | 34.0 | 5.5 | 16.8 |  |  |
| Cycle Q Clear(g_c), s | 28.1 | 0.0 | 0.0 | 34.0 | 5.5 | 16.8 |  |  |
| Prop In Lane |  | 0.00 | 0.00 |  | 1.00 | 1.00 |  |  |
| Lane Grp Cap(c), veh/h | 905 | 0 | 0 | 861 | 533 | 605 |  |  |
| V/C Ratio(X) | 0.83 | 0.00 | 0.00 | 0.93 | 0.26 | 0.64 |  |  |
| Avail Cap(c_a), veh/h | 1090 | 0 | 0 | 1037 | 533 | 605 |  |  |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |
| Upstream Filter(I) | 1.00 | 0.00 | 0.00 | 1.00 | 1.00 | 1.00 |  |  |
| Uniform Delay (d), s/veh | 17.7 | 0.0 | 0.0 | 19.2 | 15.4 | 18.7 |  |  |
| Incr Delay (d2), s/veh | 4.9 | 0.0 | 0.0 | 12.7 | 1.2 | 5.1 |  |  |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |
| \%ile BackOfQ(50\%),veh/ln | 15.5 | 0.0 | 0.0 | 19.5 | 2.1 | 7.6 |  |  |
| LnGrp Delay(d),s/veh | 22.6 | 0.0 | 0.0 | 31.9 | 16.6 | 23.8 |  |  |
| LnGrp LOS | C |  |  | C | B | C |  |  |
| Approach Vol, veh/h | 755 |  |  | 800 | 522 |  |  |  |
| Approach Delay, s/veh | 22.6 |  |  | 31.9 | 21.9 |  |  |  |
| Approach LOS | C |  |  | C | C |  |  |  |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| Assigned Phs |  | 2 |  | 4 |  |  |  | 8 |
| Phs Duration ( $\mathrm{G}+\mathrm{Y}+\mathrm{Rc}$ ), s |  | 37.0 |  | 43.0 |  |  |  | 43.0 |
| Change Period ( $\mathrm{Y}+\mathrm{Rc}$ ), s |  | 4.0 |  | 4.0 |  |  |  | 4.0 |
| Max Green Setting (Gmax), s |  | 25.0 |  | 47.0 |  |  |  | 47.0 |
| Max Q Clear Time (g_c+l1), s |  | 18.8 |  | 30.1 |  |  |  | 36.0 |
| Green Ext Time (p_c), s |  | 1.4 |  | 3.3 |  |  |  | 3.0 |
| Intersection Summary |  |  |  |  |  |  |  |  |
| HCM 2010 Ctrl Delay |  |  | 26.0 |  |  |  |  |  |
| HCM 2010 LOS |  |  | C |  |  |  |  |  |

Figure 4C-3. Warrant 3, Peak Hour

*Note: 150 vph applies as the lower threshold volume for a minor-street approach with two or more lanes and 100 vph applies as the lower threshold volume for a minor-street approach with one lane.

Figure 4C-4. Warrant 3, Peak Hour (70\% Factor) (COMMUNITY LESS THAN 10,000 POPULATION OR ABOVE 40 MPH ON MAJOR STREET)

*Note: 100 vph applies as the lower threshold volume for a minor-street approach with two or more lanes and 75 vph applies as the lower threshold volume for a minor-street approach with one lane.

## ROAD HH - NEWVILLE RD : EXISTING

AM (•) : MAJOR 554
PM (■) : MAJOR 707157
MINOR ..... 167

Figure 4C-3. Warrant 3, Peak Hour

*Note: 150 vph applies as the lower threshold volume for a minor-street approach with two or more lanes and 100 vph applies as the lower threshold volume for a minor-street approach with one lane.

Figure 4C-4. Warrant 3, Peak Hour (70\% Factor) (COMMUNITY LESS THAN 10,000 POPULATION OR ABOVE 40 MPH ON MAJOR STREET)

*Note: 100 vph applies as the lower threshold volume for a minor-street approach with two or more lanes and 75 vph applies as the lower threshold volume for a minor-street approach with one lane.

## SB I-5 RAMP - NEWVILLE RD : EXISTING

$$
\begin{array}{ll}
\text { AM (•) : MAJOR } 730 & \text { MINOR } 128 \\
\text { PM (■) : MAJOR } 860 & \text { MINOR } 180
\end{array}
$$

Figure 4C-3. Warrant 3, Peak Hour

*Note: 150 vph applies as the lower threshold volume for a minor-street approach with two or more lanes and 100 vph applies as the lower threshold volume for a minor-street approach with one lane.

Figure 4C-4. Warrant 3, Peak Hour (70\% Factor) (COMMUNITY LESS THAN 10,000 POPULATION OR ABOVE 40 MPH ON MAJOR STREET)

*Note: 100 vph applies as the lower threshold volume for a minor-street approach with two or more lanes and 75 vph applies as the lower threshold volume for a minor-street approach with one lane.

## NB I-5 RAMP - NEWVILLE RD : EXISTING

AM (•) : MAJOR 762
PM (■) : MAJOR 904

MINOR84

MINOR 159

Figure 4C-3. Warrant 3, Peak Hour

*Note: 150 vph applies as the lower threshold volume for a minor-street approach with two or more lanes and 100 vph applies as the lower threshold volume for a minor-street approach with one lane.

Figure 4C-4. Warrant 3, Peak Hour (70\% Factor) (COMMUNITY LESS THAN 10,000 POPULATION OR ABOVE 40 MPH ON MAJOR STREET)

*Note: 100 vph applies as the lower threshold volume for a minor-street approach with two or more lanes and 75 vph applies as the lower threshold volume for a minor-street approach with one lane.

ROAD HH - NEWVILLE RD : EXISTING PLUS PROJECT
AM (•) : MAJOR 611 MINOR 211
PM (■) : MAJOR 769 MINOR 222

Figure 4C-3. Warrant 3, Peak Hour

*Note: 150 vph applies as the lower threshold volume for a minor-street approach with two or more lanes and 100 vph applies as the lower threshold volume for a minor-street approach with one lane.

Figure 4C-4. Warrant 3, Peak Hour (70\% Factor) (COMMUNITY LESS THAN 10,000 POPULATION OR ABOVE 40 MPH ON MAJOR STREET)

*Note: 100 vph applies as the lower threshold volume for a minor-street approach with two or more lanes and 75 vph applies as the lower threshold volume for a minor-street approach with one lane.

## SB I-5 RAMP - NEWVILLE RD : EXISTING PLUS PROJECT

AM (•) : MAJOR 660
PM (■) : MAJOR 802
MINOR
152
MINOR 206

Figure 4C-3. Warrant 3, Peak Hour

*Note: 150 vph applies as the lower threshold volume for a minor-street approach with two or more lanes and 100 vph applies as the lower threshold volume for a minor-street approach with one lane.

Figure 4C-4. Warrant 3, Peak Hour (70\% Factor) (COMMUNITY LESS THAN 10,000 POPULATION OR ABOVE 40 MPH ON MAJOR STREET)

*Note: 100 vph applies as the lower threshold volume for a minor-street approach with two or more lanes and 75 vph applies as the lower threshold volume for a minor-street approach with one lane.

## NB I-5 RAMP - NEWVILLE RD : EXISTING PLUS PROJECT

AM (•) : MAJOR 708
PM (■) : MAJOR 825
MINOR
84
MINOR 159

Figure 4C-3. Warrant 3, Peak Hour

*Note: 150 vph applies as the lower threshold volume for a minor-street approach with two or more lanes and 100 vph applies as the lower threshold volume for a minor-street approach with one lane.

Figure 4C-4. Warrant 3, Peak Hour (70\% Factor) (COMMUNITY LESS THAN 10,000 POPULATION OR ABOVE 40 MPH ON MAJOR STREET)

*Note: 100 vph applies as the lower threshold volume for a minor-street approach with two or more lanes and 75 vph applies as the lower threshold volume for a minor-street approach with one lane.

ROAD HH - NEWVILLE RD : EXISTING PLUS PROJECT AND HOTEL-RESTAURANT
AM (•) : MAJOR 671 MINOR 256
PM (■) : MAJOR 827 MINOR 269

Figure 4C-3. Warrant 3, Peak Hour

*Note: 150 vph applies as the lower threshold volume for a minor-street approach with two or more lanes and 100 vph applies as the lower threshold volume for a minor-street approach with one lane.

Figure 4C-4. Warrant 3, Peak Hour (70\% Factor) (COMMUNITY LESS THAN 10,000 POPULATION OR ABOVE 40 MPH ON MAJOR STREET)

*Note: 100 vph applies as the lower threshold volume for a minor-street approach with two or more lanes and 75 vph applies as the lower threshold volume for a minor-street approach with one lane.

AM (•) : MAJOR 72
PM (■) : MAJOR 871 MINOR

Figure 4C-3. Warrant 3, Peak Hour

*Note: 150 vph applies as the lower threshold volume for a minor-street approach with two or more lanes and 100 vph applies as the lower threshold volume for a minor-street approach with one lane.

Figure 4C-4. Warrant 3, Peak Hour (70\% Factor) (COMMUNITY LESS THAN 10,000 POPULATION OR ABOVE 40 MPH ON MAJOR STREET)

*Note: 100 vph applies as the lower threshold volume for a minor-street approach with two or more lanes and 75 vph applies as the lower threshold volume for a minor-street approach with one lane.

NB I-5 RAMP - NEWVILLE RD : EXISTING PLUS PROJECT AND HOTEL-RESTAURANT

AM (•) : MAJOR 746
MINOR 100
PM (■) : MAJOR 863 MINOR 175

Figure 4C-3. Warrant 3, Peak Hour

*Note: 150 vph applies as the lower threshold volume for a minor-street approach with two or more lanes and 100 vph applies as the lower threshold volume for a minor-street approach with one lane.

Figure 4C-4. Warrant 3, Peak Hour (70\% Factor) (COMMUNITY LESS THAN 10,000 POPULATION OR ABOVE 40 MPH ON MAJOR STREET)

*Note: 100 vph applies as the lower threshold volume for a minor-street approach with two or more lanes and 75 vph applies as the lower threshold volume for a minor-street approach with one lane.

ROAD HH - NEWVILLE RD : CUMULATIVE PLUS HOTEL-RESTAURANT

AM (•) : MAJOR 646
PM (■) : MAJOR 884

Figure 4C-3. Warrant 3, Peak Hour

*Note: 150 vph applies as the lower threshold volume for a minor-street approach with two or more lanes and 100 vph applies as the lower threshold volume for a minor-street approach with one lane.

Figure 4C-4. Warrant 3, Peak Hour (70\% Factor) (COMMUNITY LESS THAN 10,000 POPULATION OR ABOVE 40 MPH ON MAJOR STREET)

*Note: 100 vph applies as the lower threshold volume for a minor-street approach with two or more lanes and 75 vph applies as the lower threshold volume for a minor-street approach with one lane.

Figure 4C-3. Warrant 3, Peak Hour

*Note: 150 vph applies as the lower threshold volume for a minor-street approach with two or more lanes and 100 vph applies as the lower threshold volume for a minor-street approach with one lane.

Figure 4C-4. Warrant 3, Peak Hour (70\% Factor) (COMMUNITY LESS THAN 10,000 POPULATION OR ABOVE 40 MPH ON MAJOR STREET)

*Note: 100 vph applies as the lower threshold volume for a minor-street approach with two or more lanes and 75 vph applies as the lower threshold volume for a minor-street approach with one lane.

NB I-5 RAMP - NEWVILLE RD : CUMULATIVE PLUS HOTEL-RESTAURANT
AM (•) : MAJOR 1561 MINOR 320
PM (■) : MAJOR 1800 MINOR 480

Figure 4C-3. Warrant 3, Peak Hour

*Note: 150 vph applies as the lower threshold volume for a minor-street approach with two or more lanes and 100 vph applies as the lower threshold volume for a minor-street approach with one lane.

Figure 4C-4. Warrant 3, Peak Hour (70\% Factor) (COMMUNITY LESS THAN 10,000 POPULATION OR ABOVE 40 MPH ON MAJOR STREET)

*Note: 100 vph applies as the lower threshold volume for a minor-street approach with two or more lanes and 75 vph applies as the lower threshold volume for a minor-street approach with one lane.

ROAD HH - NEWVILLE RD : CUMULATIVE PLUS PROJECT AND HOTEL-RESTAURANT
AM (•) : MAJOR 705 MINOR 259
PM (■) : MAJOR 946
MINOR 293

Figure 4C-3. Warrant 3, Peak Hour

*Note: 150 vph applies as the lower threshold volume for a minor-street approach with two or more lanes and 100 vph applies as the lower threshold volume for a minor-street approach with one lane.

Figure 4C-4. Warrant 3, Peak Hour (70\% Factor) (COMMUNITY LESS THAN 10,000 POPULATION OR ABOVE 40 MPH ON MAJOR STREET)

*Note: 100 vph applies as the lower threshold volume for a minor-street approach with two or more lanes and 75 vph applies as the lower threshold volume for a minor-street approach with one lane.

Figure 4C-3. Warrant 3, Peak Hour

*Note: 150 vph applies as the lower threshold volume for a minor-street approach with two or more lanes and 100 vph applies as the lower threshold volume for a minor-street approach with one lane.

Figure 4C-4. Warrant 3, Peak Hour (70\% Factor) (COMMUNITY LESS THAN 10,000 POPULATION OR ABOVE 40 MPH ON MAJOR STREET)

*Note: 100 vph applies as the lower threshold volume for a minor-street approach with two or more lanes and 75 vph applies as the lower threshold volume for a minor-street approach with one lane.


[^0]:    ${ }^{1}$ Traffic Impact Assessment For Hotel / Restaurant Near Flying J Truck Stop In Orland, CA, KDA, August 8, 2016.

[^1]:    Traffic Impact Analysis for the Orland Truck Wash / Commercial Project
    Orland, California (July 8, 2019)

