

Mr. John R. Burroughs, LEED AP, President

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## Subject: Limited Borrow Site Study <br> Borrow Site No. 3 (Export Fill Dirt Site No. 3) Cucamonga Avenue and West County Road City of Chino, CA

Dear Mr. Burroughs:
Presented herein are our preliminary findings and conclusions regarding the suitability of the soils within Borrow Site 3 to be used as engineered fill to balance the grades for the OC Prado site construction located on the southeast corner of Bickmore Avenue and Mountain Avenue, in the City of Chino.

In accordance with the revised Conceptual Grading Plan, the irregular hexagonal-shaped borrow site covers an area of about $44 \pm$ acres. The site is bounded by the California Institution for Women to the north, Prado Reservoir Park to the west, vacant land to the south and Cucamonga Avenue to the east. On the east side, the site borders Cucamonga Avenue over a distance of about 2230 feet, extending approximately 910 feet south of the intersection with West County Road. The width of the site is about 850 feet in its middle and 1510 feet in its southern portion that extends about 490 feet in the southerly direction.

A Vicinity Map with approximate ground contour elevations is presented in Appendix A as Figure A-1. The site is located entirely on the west side of Cucamonga Avenue, and the nearest street intersection is Cucamonga Avenue with West County Road.

## Field Exploration and Laboratory Testing

The field exploration program for Borrow Site 3 was performed in two phases. The first phase of the field exploration was performed within the northern portion of the site and consisted of four test pits, TP-3 through TP-6, excavated on February 23, 2018. The second phase consisted of excavating thirteen test pits; TP-7 though TP-18 plus TP-15A on April 17, 2018. A rubber tire mounted backhoe was used to excavate the test pits ranging in depths from about 14 to 17 feet for the first phase and from 6 to 9 feet for the second phase. Test Pit 1 and 2 were excavated using a hand auger on April 24, 2018 due to the recent re-seeding and on-going irrigation. The locations of the test pits are shown on the Field Exploration Map, Figure A-2, presented in Appendix A. Bulk samples were obtained from the test pits and hand augering for laboratory testing.

Laboratory tests, including moisture content, \#200 sieve wash, expansion index, maximum density, pocket penetrometer and plasticity index were performed to aid in the classification of the materials encountered and to evaluate their engineering properties. The results of pertinent laboratory tests are presented on the test pit logs in Appendix B, and/or in Appendix C.

## Site Geology

The site is located within the Upper Santa Ana River Valley, which consists of a series of coalescing alluvial fans formed by streams flowing out of the San Gabriel Mountains to the north. The valley lies within the Peninsular Ranges geomorphic province, which is characterized by alluviated basins, elevated erosion surfaces, and northwest-trending mountain ranges bounded by northwest trending faults. The site, which is located within the Chino Basin, is underlain by sediments deposited by the Santa Ana River and its tributaries such as the Chino Creek.

Morton and Miller (2006) show the site to be underlain by very old alluvial-fan deposits (See Figure A-3 in Appendix A). The sediments observed during the subsurface investigation consisted predominantly of clay at shallow depths.

## Surface Site Conditions

The site has at least three entrances from Cucamonga Avenue to the east; one of these entrances is near the intersection of West County Road with Cucamonga Avenue. No buildings were present onsite at the time of our field exploration; however, there are power lines supported on pile foundations crossing the site about 100 feet north of West County Road. There are also remnants of concrete slabs on grade, which were observed in various locations. Portions of the site appear to have abandoned underground utilities. Other portions of the site support irrigation lines that are being used to water the recent seeding and other grass areas. More than one-half of the site was devoid of vegetation at the time of our field exploration and the remainder of the site contained mostly sparse to dense grass vegetation.

The southern portion of the site contains several water storage ponds that range in depth mostly from about 3 to 7 feet. At the time of our site exploration in April 2018, only the ponds located east of Test Pit 17 and northwest of Test Pit 18 contained water (approximately 1 to 3 feet). The ponds appear to have been created by excavating and mounding the native soils around the excavations. There was localized grass areas and low shrubs near the ponds at the time of our second phase of the field exploration.

The northern portion of the site slopes gently to the southwest while the southern portion generally slopes gently to the south. The existing elevations range between about 545 feet at the south end to 566 feet at the northeast corner of the site (NAVD88).

## Soil Conditions

The subsurface soil profile consists generally of artificial fill underlain by alluvial deposits. The fill depth is variable, ranging from less than one foot to about 6 feet at the test pit locations. For
the most part, the fill materials are derived from onsite shallow soils and consist generally of lean clay with sand, sandy lean clay, and thin layers of clayey sand and silty sand at or near the surface with localized areas of fat clay. Organic material, including manure, was encountered in Test Pit 15A, which was excavated through a pond berm near the southwest corner of the site.

The alluvium soils consist predominantly of stiff to very stiff, medium to high plastic sandy clay, lean clay with sand, fat clay and sandy silt. Some clayey sand and silty sand layers were encountered below a depth of about 12 feet in some of the deeper test pits.

The soils were generally dry near the surface at the time of the Phase 2 field exploration. Except for organic material, for the soils below a depth of about 1 to 2 feet, the moisture contents of the clay soils are highly variable, ranging from about 9 to $41 \frac{1}{2}$ percent with an average on the order of 23 percent. At the time of our field exploration, the silty sand and clayey sand moisture contents ranged from about 3 to $231 / 2$ percent with an average of about $121 / 2$ percent. Based on the maximum density test performed and prior experience with similar soils, many of the clay sample moisture contents are about 8 to 12 percent above optimum for the soils sampled within the upper 8 feet of the ground surface (see Table 1 and Appendix $C$ for maximum density test results).

The fines contents of the clay soils range from about 50 to 93 percent with an average of about 69 percent while the fine contents of the sands range from about 14 to 44 percent with an average of about $261 / 2$ percent. The average relatively low fines contents of the clay soils are attributed to the presence of concretions (hard matter formed by precipitation of mineral cement between particles) observed in many of the clay samples. The pocket penetrometer tests indicate unconfined compression strength on the order of 1 to 4.5 tsf with an average of about 2.8 tsf.

To aid in the soil classification and to correlate the soil plasticity with the soil expansion, one plasticity index test (Atterberg Limits) was performed on a sample of Test Pit 6 at a depth of 8 to 9 feet. As shown in Table 1, the Liquid limit, Plastic Limit and Plasticity Index for the tested sample are 75, 18 and 57 respectively, which indicate a high plasticity soil at that depth for this test pit.

Table 1 - Maximum Density and Plasticity Index

| Test Pit Number | TP-6 @ 8 to 9 feet |
| :--- | :---: |
| Maximum Dry Density (pcf) | 111.1 |
| Optimum Moisture Content (\%) | 16.2 |
| Liquid Limit | 75 |
| Plastic Limit | 18 |
| Plasticity Index | 57 |

The site soil expansion potential ranges from low to very high. Table 2 presents the data for 26 expansion index tests at depths ranging from 1 to 11 feet. These tests indicate expansion index variations from 32 to 208 with an average of about 94 . For the 13 tests on samples at depths
between 1 and $41 / 2$ feet, the expansion index ranges from about 32 to 100 with an average of approximately 65.

Table 2 - Expansion Index Test Results

| Test Pit No. | Depth <br> (feet) | Expansion Index | Field Moisture <br> $\mathbf{( \% )}$ | Fines Percent |
| :---: | :---: | :---: | :---: | :---: |
| *TP-1 | $2-3$ | 64 | 17.7 | 76 |
| *TP-1 | $5-6$ | 175 | 22.4 | 50 |
| *TP-2 | $3-4$ | 100 | 21.8 | 71 |
| *TP-3 | $1.5-2.5$ | 53 | 17.9 | 66 |
| *TP-3 | $4-4.5$ | 99 | 23.7 | 63 |
| *TP-3 | $10-11$ | 96 | 25.5 | 51 |
| *TP-4 | $3-3.5$ | 80 | 33.8 | 54 |
| *TP-4 | $4-4.5$ | 56 | 29.1 | 60 |
| *TP-5 | $6-7$ | 176 | 28.4 | 74 |
| *TP-5 | $8-10$ | 190 | 31.3 | 50 |
| *TP-6 | $1-2$ | 32 | 17.9 | 56 |
| *TP-6 | $7-8$ | 172 | 30.6 | 73 |
| *TP-6 | $8-9$ | 208 | 30.4 | 57 |
| TP-7 | $4-4.5$ | 92 | 18.3 | 79 |
| TP-7 | $5.7-6.5$ | 101 | 22.8 | 68 |
| TP-8 | $6-6.5$ | 60 | 15.7 | 83 |
| TP-9 | $4-4.5$ | 62 | 18.4 | 65 |
| TP-10 | $6-7$ | 37 | 25.8 | 93 |
| TP-11 | $3.7-4.2$ | 32 | 22.0 | 50 |
| TP-11 | $5.5-6$ | 50 | 16.1 | 50 |
| TP-13 | $4.75-5$ | 100 | 18.7 | 53 |
| TP-14 | $6.7-7$ | 40 | 18.0 | 82 |
| TP-15 | $4.2-4.7$ | 79 | 25.0 | 82 |
| TP-15 | $5.5-6$ | 195 | 23.4 | 84 |
| TP-17 | $4-4.5$ | 40 | 22.8 | 90 |
| TP-18 | $4.5-5$ | 55 |  | 79 |

*Northern portion of proposed borrow site
We noted that the light-colored clay samples containing concretions tend to have higher expansion index. The expansion potential can change rapidly with depth as shown by two tests on TP-15 for depths of about $41 / 2$ and $51 / 2$ feet, where the expansion indices are 79 and 195, respectively.

There is a rough correlation between in situ natural moisture content and expansion index. For the same amounts of fines, site clay below the depth of seasonal moisture variation, soils with higher moisture and higher plasticity index tend to have higher expansion potential.

## Corrosivity

The corrosivity tests performed indicates that the site soils are generally severely corrosive to metal. However, the tests performed did not indicate high corrosivity to concrete. The corrosivity test results are summarized in the following Table 3.

Table 3-Corrosion Test Results

| Boring | Depth <br> (ft) | Minimum <br> Resistivity <br> (ohm-cm) | $\mathbf{p H}$ | Soluble <br> Sulfate Content <br> (ppm) | Soluble <br> Chloride Content <br> (ppm) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| TP-5 | $5-6$ | 566 | 7.7 | 235 | 490 |

## Groundwater

Groundwater seepage was encountered in Test Pit 18 which was excavated within the slope of a pond containing water. The wet soil level in the test pit was at about the pond water level. Groundwater seepage was encountered at a depth of about $131 / 2$ feet in Test Pit 3. No seepage was encountered in the other test pits excavated to a maximum depth of 17 feet. Borings should be drilled if the groundwater level needs to be determined.

## Conclusions and Recommendations

Based on the data collected from the field to date, it appears feasible to import material from Borrow Site 3 to use at the OC Prado site. However, it appears that on average only the upper 4 to $41 / 2$ feet of soils (once well blended and once clearing, grubbing and stripping of the topsoil is complete) could be suitable for foundation. It should be noted that for the southernmost portion of the site, the construction of the ponds has resulted in some of the expansive clay soils to be mixed with the less expansive soils and with some organics. Therefore, some material at shallow depth in the southernmost portion of the site may not be suitable for export to be used as engineered fill. Therefore, observation and testing during export of the material to the OC Prado site is advisable. All organic material, construction debris, and other unsuitable materials should be removed prior to export to the OC Prado site.

During the second phase of field exploration, we noted that the upper one to two feet of soils had low moisture contents due to drying weather conditions. Dry clay soils are undesirable from a geotechnical performance standpoint and require time to absorb moisture. Therefore, the surface conditions should be checked prior to export, and where the moisture contents are not above optimum, we recommend that the soils be pre-moisture conditioned in the borrow site prior to export. For the areas under active irrigation, the irrigation system should be stopped at least 3 to 4 weeks prior to soil export.

We anticipate that an excavation plan will be prepared by the project civil engineer. Appropriate setback should be set from existing foundations, slopes and property lines.

## LIMITATIONS

Our work was performed in a manner consistent with that level of care and skill ordinarily exercised by other members of Koury's profession practicing in the same locality, under similar conditions and at the date the services are provided.

## CLOSURE

The findings and recommendations presented in this report were based on the results of our field and laboratory investigations, combined with professional engineering experience and judgment. The report was prepared in accordance with generally accepted engineering principles and practice. We make no other warranty, either expressed or implied. Subsurface variations between and beyond the test pits should be anticipated. Koury should be notified if subsurface conditions are encountered, which differ from those described in this report. Samples obtained during this investigation will be retained in our laboratory for a period of 45 days from the date of this report and will be disposed after this period.

Should you have any questions concerning this submittal, or the recommendations contained herewith, please do not hesitate to call our office.

Respectfully submitted,
KOURY ENGINEERING \& TESTING, INC


Distribution:

1. Addressee (pdf copy via e-mail)
2.File (B)

## REFERENCES

1. California Division of Mines and Geological Survey, 1998, Seismic Hazard Zone Report 045 for the Prado Dam 7.5 Minute Quadrangle, California.
2. California Division of Mines and Geological Survey, 2003, Earthquake Fault Zones, Prado Dam Quadrangle, May 1, 2003.
3. City of Chino General Plan, Safety Element, 2010, Final Report.
4. US Army Corps of Engineers, Soil Investigations, Engineering Manual EM 1110-1-1804, dated 8/26/86.
5. US Army Corps of Engineers, Laboratory Soils Testing, Engineering Manual EM 1110-21906, dated 8/26/86.

## APPENDICES

## Appendix A: Maps and Plans

Vicinity Map - Figure A-1
Field Exploration Map - Figure A-2
Geology Map - Figure A-3
Appendix B: Field Exploratory Test Pits
Test Pits 1 through 18

## Appendix C: Laboratory Test Results

## APPENDIX A

## Maps and Plans





## APPENDIX B

Field Exploratory Test Pits

KEY TO LOGS

| SOILS CLASSIFICATION |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| MAJOR DIVISIONS |  |  | GRAPHIC LOG | USCS SYMBOL | TYPICAL NAMES |
| COARSE GRAINED SOILS | GRAVELS | CLEAN GRAVELS <br> LESS THAN 5\% FINES |  | GW | WELL-GRADED GRAVELS, GRAVEL-SAND MIXTURES, LITTLE OR NO FINES |
|  |  |  |  | GP | POORLY-GRADED GRAVELS, GRAVEL-SAND MIXTURES, LItTLE OR NO FINES |
|  | $\begin{aligned} & \text { MORE THAN 50\% } \\ & \text { OF COARSE } \end{aligned}$ | GRAVELS WITH FINES |  | GM | SILTY GRAVELS, GRAVEL-SAND-SILT MIXTURES |
|  | LARGER THAN NO. 4 SIEVE | MORE THAN $12 \%$ FINES |  | GC | CLAYEY GRAVELS, GRAVEL-SAND-CLAY MIXTURES |
| MORE THAN 50\% OF MATERIAL IS LARGER THAN NO. 200 SIEVE SIZE | SANDS | CLEAN SANDS |  | SW | WELL-GRADED SANDS, GRAVELLY SANDS, LITTLE OR NO FINES |
|  |  | LESS THAN 5\% FINES |  | SP | POORLY-GRADED SANDS, GRAVELLY SANDS, LITTLE OR NO FINES |
|  | 50\% OR MORE OF COARSE FRACTION IS SMALLER THAN NO. 4 SIEVE | SANDS WITH FINES |  | SM | SILTY SANDS, SAND-SILT MIXTURES |
|  |  | MORE THAN 12\% FINES |  | SC | CLAYEY SANDS, SAND-CLAY MIXTURES |
| FINE GRAINED SOILS |  |  |  | ML | INORGANIC SILTS AND VERY FINE SANDS, ROCK FLOUR, SILTY OR CLAYEY FINE SANDS OR CLAYEY SILTS WITH SLIGHT PLASTICITY |
|  | LIOUID LIMIT IS | LESS THAN 50 |  | CL | INORGANIC CLAYS OF LOW TO MEDIUM PLASTICITY, GRAVELLY CLAYS, SANDY CLAYS, SILTY CLAYS, LEAN CLAYS |
|  |  |  |  | OL | ORGANIC SILTS AND ORGANIC SILTY CLAYS OF LOW PLASTICITY |
| 50\% OR MORE OF MATERIAL IS SMALLER THAN NO. 200 SIEVE SIZE | SILTS AND CLAYS |  |  | MH | INORGANIC SILTS, MICACEOUS OR DIATOMACEOUS FINE SANDY OR GRAVELLY ELASTIC SILTS |
|  | LIQUID LIMIT IS 50 OR MORE |  |  | CH | INORGANIC CLAYS OF HIGH PLASTICITY, FAT CLAYS |
|  |  |  | $88$ | OH | ORGANIC CLAYS OF MEDIUM TO HIGH PLASTICITY, ORGANIC SILTS |
| HIGHLY ORGANIC SOILS |  |  |  | PT | PEAT AND OTHER HIGHLY ORGANIC SOILS |


| GRAIN SIZES |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SILT AND CLAY | SAND |  |  | GRAVEL |  | COBBLES | BOULDERS |
|  | FINE | MEDIUM | COARSE | FINE | COARSE |  |  |
|  | - | 号 |  | \# | 遃 | - | \# |

## KEY TO LOGS (continued)

| SPT/CD BLOW COUNTS VS. CONSISTENCYIDENSITY |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| FINE-GRAINED SOILS (SILTS, CLAYS, etc.) |  | GRANULAR SOILS (SANDS, GRAVELS, etc.) |  |  |  |
| CONSISTENCY | *BLOWS/FOOT |  | RELATIVE DENSITY | *BLOWS/FOOT |  |
|  | SPT | CD |  | CD |  |
| SOFT | $0-4$ | $0-4$ | VERY LOOSE | $0-4$ | $0-8$ |
| FIRM | $5-8$ | $5-9$ | LOOSE | $5-10$ | $9-18$ |
| STIFF | $9-15$ | $10-18$ | MEDIUM DENSE | $11-30$ | $19-54$ |
| VERY STIFF | $16-30$ | $19-39$ | DENSE | $31-50$ | $55-90$ |
| HARD | over 30 | over 39 | VERY DENSE | over 50 | over 90 |

* CONVERSION BETWEEN CALIFORNIA DRIVE SAMPLERS (CD) AND STANDARD PENETRATION TEST (SPT) BLOW COUNT HAS BEEN CALCULATED USING "FOUNDATION ENGINEERING HAND BOOK" BY H.Y. FANG. (VALUES ARE FOR 140 Lbs HAMMER WEIGHT ONLY)

| DESCRIPTIVE ADJECTIVE VS. PERCENTAGE |  |
| :---: | :---: |
| DESCRIPTIVE ADJECTIVE | PERCENTAGE REQUIREMENT |
| TRACE | $1-10 \%$ |
| LITTLE | $10-20 \%$ |
| SOME | $20-35 \%$ |
| AND | $35-50 \%$ |

*THE FOLLOWING "DESCRIPTIVE TERMINOLOGY/ RANGES OF MOISTURE CONTENTS" HAVE BEEN USED FOR MOISTURE CLASSIFICATION IN THE LOGS.

| APPROXIMATE MOISTURE CONTENT DEFINITION |  |
| :---: | :---: |
| DEFINITION | DESCRIPTION |
| DRY | Dry to the touch; no observable moisture |
| SLIGHTLY MOIST | Some moisture but still a dry appearance |
| MOIST | Damp, but no visible water |
| VERY MOIST | Enough moisture to wet the hands |
| WET | Almost saturated; visible free water |



Test Pit Log


Test Pit Log


Test Pit Log


Test Pit Log






Test Pit Log


Test Pit Log


Test Pit Log


Test Pit Log



Test Pit Log


Test Pit Log


Test Pit Log




## APPENDIX C

Laboratory Test Results

DENSITY AND MOISTURE CONTENT DATA - EI TEST

| Location/ Elevation | TP7 @ 4' - 4.5' |  | TP7 @ 5.75' - 6.5' |  | TP9 @ 4' - 4.5' |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| USCS Symbol | CH/CL |  | CH / CL |  | CH / CL |  |  |  |  |
| Normal Load (psf) | 144 |  | 144 |  | 144 |  |  |  |  |
| SAMPLE CONDITION | Initial | Final | Initial | Final | Initial | Final |  |  |  |
| Wt Specimen \& Ring (gr) | 761.380 |  | 703.070 |  | 742.100 |  |  |  |  |
| Wt. of ring (gr) | 367.47 |  | 364.16 |  | 366.64 |  |  |  |  |
| Wt. Specimen (gr) | 393.910 |  | 338.910 |  | 375.460 |  |  |  |  |
| Specimen diameter (in) | 4.010 |  | 4.010 |  | 4.010 |  |  |  |  |
| Specimen radius (cm) | 5.09 |  | 5.09 |  | 5.09 |  |  |  |  |
| Area of Specimen ( $\mathrm{cm}^{2}$ ) | 81.479 |  | 81.479 |  | 81.479 |  |  |  |  |
| Init. Spec. height (in) | 1.0020 | N/A | 0.9993 | N/A | 1.0020 | N/A |  |  |  |
| Height change (final)(in) | N/A | 0.0926 | N/A | 0.1006 | N/A | 0.0623 |  |  |  |
| Adjusted Spec.height(in) | 1.00 | 0.9094 | 1.00 | 0.8987 | 1.00 | 0.9397 |  |  |  |
| " ${ }^{\text {a }}$ (cm) | 2.545 | 2.310 | 2.538 | 2.283 | 2.545 | 2.387 |  |  |  |
| Specimen Volume ( $\mathrm{cm}^{3}$ ) | 207.371 |  | 206.812 |  | 207.371 |  |  |  |  |
| Moist Density (pcf) | 118.59 |  | 102.31 |  | 113.03 |  |  |  |  |
| MOISTURE CONTENT |  |  |  |  |  |  |  |  |  |
| Wt. moist soil+tare(gr) | 126.54 | 126.54 | 130.33 | 130.33 | 125.87 | 125.87 |  |  |  |
| Wt. dry soil+tare(gr) | 115.59 | 115.59 | 113.23 | 113.23 | 113.23 | 113.23 |  |  |  |
| Wt. of tare(gr) | 19.64 | 19.64 | 19.71 | 19.71 | 19.74 | 19.74 |  |  |  |
| Wt. dry soil (gr) | 95.95 | 95.95 | 93.52 | 93.52 | 93.49 | 93.49 |  |  |  |
| Wt. of water (gr) | 10.95 | 10.95 | 17.10 | 17.10 | 12.64 | 12.64 |  |  |  |
| M/C (\%) | 11.41 | 11.41 | 18.28 | 18.28 | 13.52 | 13.52 |  |  |  |
| DRY DENSITY (pcf) | 106.4 |  | 86.5 |  | 99.6 |  |  |  |  |
| \% Saturation* (48\%-52\%) | 52.8 |  | 52.0 |  | 52.7 |  |  |  |  |
| *Assumes Gs = | 2.7 |  | 2.7 |  | 2.7 |  |  |  |  |
| EXPANSION INDEX = | 92 |  | 101 |  | 62 |  |  |  |  |
| Potential Expansion (per ASTM 4829-08) | High |  | High |  | Medium |  |  |  |  |
| KOURY <br>  |  |  | Project Name: $\quad$ Borrow Site \#2 |  |  |  | Project No.: 17-1021 <br> Date: 4/25/18 | Run by: MFP QA: | Lab: <br> 18-0023 Series |

DENSITY AND MOISTURE CONTENT DATA - EI TEST

| Location/ Elevation | TP8 @ 6' - 6.5' |  | TP10 @ 6' - 7' |  | TP14 @ 6.5' - 7' |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| USCS Symbol | CL |  | CL |  | CL |  |  |  |  |
| Normal Load (psf) | 144 |  | 144 |  | 144 |  |  |  |  |
| SAMPLE CONDITION | Initial | Final | Initial | Final | Initial | Final |  |  |  |
| Wt Specimen \& Ring (gr) | 752.450 |  | 718.350 |  | 762.070 |  |  |  |  |
| Wt. of ring (gr) | 367.45 |  | 364.18 |  | 366.65 |  |  |  |  |
| Wt. Specimen (gr) | 385.000 |  | 354.170 |  | 395.420 |  |  |  |  |
| Specimen diameter (in) | 4.010 |  | 4.010 |  | 4.010 |  |  |  |  |
| Specimen radius (cm) | 5.09 |  | 5.09 |  | 5.09 |  |  |  |  |
| Area of Specimen ( $\mathrm{cm}^{2}$ ) | 81.479 |  | 81.479 |  | 81.479 |  |  |  |  |
| Init. Spec. height (in) | 1.0020 | N/A | 0.9993 | N/A | 1.0020 | N/A |  |  |  |
| Height change (final)(in) | N/A | 0.0606 | N/A | 0.0369 | N/A | 0.0404 |  |  |  |
| Adjusted Spec.height(in) | 1.00 | 0.9414 | 1.00 | 0.9624 | 1.00 | 0.9616 |  |  |  |
| " ${ }^{\text {a }}$ (cm) | 2.545 | 2.391 | 2.538 | 2.444 | 2.545 | 2.442 |  |  |  |
| Specimen Volume ( $\mathrm{cm}^{3}$ ) | 207.371 |  | 206.812 |  | 207.371 |  |  |  |  |
| Moist Density (pcf) | 115.91 |  | 106.91 |  | 119.04 |  |  |  |  |
| MOISTURE CONTENT |  |  |  |  |  |  |  |  |  |
| Wt. moist soil+tare(gr) | 132.38 | 132.38 | 136.31 | 136.31 | 148.38 | 148.38 |  |  |  |
| Wt. dry soil+tare(gr) | 119.95 | 119.95 | 122.87 | 122.87 | 135.41 | 135.41 |  |  |  |
| Wt. of tare(gr) | 19.71 | 19.71 | 31.57 | 31.57 | 17.30 | 17.30 |  |  |  |
| Wt. dry soil (gr) | 100.24 | 100.24 | 91.30 | 91.30 | 118.11 | 118.11 |  |  |  |
| Wt. of water (gr) | 12.43 | 12.43 | 13.44 | 13.44 | 12.97 | 12.97 |  |  |  |
| M/C (\%) | 12.40 | 12.40 | 14.72 | 14.72 | 10.98 | 10.98 |  |  |  |
| DRY DENSITY (pcf) | 103.1 |  | 93.2 |  | 107.3 |  |  |  |  |
| \% Saturation* (48\%-52\%) | 52.8 |  | 49.1 |  | 107.3 |  |  |  |  |
| *Assumes Gs = | 2.7 |  | 2.7 |  | 2.7 |  |  |  |  |
| EXPANSION INDEX = | 60 |  | 37 |  | 40 |  |  |  |  |
| Potential Expansion (per ASTM 4829-08) | Medium |  | Low |  | Low |  |  |  |  |
| KOURY <br>  |  |  | Project Name: $\quad 10$ |  |  |  | Project No.: 17-1021 <br> Date: 4/27/18 | Run by: MFP QA: | Lab: <br> 18-0023 Series |

DENSITY AND MOISTURE CONTENT DATA - EI TEST

| Location/ Elevation | TP11 @ 3.7' - 4.3' |  | TP11 @ 5.5' - 6.0' |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| USCS Symbol | CL |  | CL / CH |  |  |  |  |
| Normal Load (psf) | 144 |  | 144 |  |  |  |  |
| SAMPLE CONDITION | Initial | Final | Initial | Final |  |  |  |
| Wt Specimen \& Ring (gr) | 716.340 |  | 743.890 |  |  |  |  |
| Wt. of ring (gr) | 367.47 |  | 364.17 |  |  |  |  |
| Wt. Specimen (gr) | 348.870 |  | 379.720 |  |  |  |  |
| Specimen diameter (in) | 4.010 |  | 4.010 |  |  |  |  |
| Specimen radius (cm) | 5.09 |  | 5.09 |  |  |  |  |
| Area of Specimen ( $\mathrm{cm}^{2}$ ) | 81.479 |  | 81.479 |  |  |  |  |
| Init. Spec. height (in) | 1.0020 | N/A | 0.9993 | N/A |  |  |  |
| Height change (final)(in) | N/A | 0.0321 | N/A | 0.0502 |  |  |  |
| Adjusted Spec.height(in) | 1.00 | 0.9699 | 1.00 | 0.9491 |  |  |  |
| " " (cm) | 2.545 | 2.464 | 2.538 | 2.411 |  |  |  |
| Specimen Volume ( $\mathrm{cm}^{3}$ ) | 207.371 |  | 206.812 |  |  |  |  |
| Moist Density (pcf) | 105.03 |  | 114.63 |  |  |  |  |
| MOISTURE CONTENT |  |  |  |  |  |  |  |
| Wt. moist soil+tare(gr) | 142.42 | 142.42 | 133.92 | 133.92 |  |  |  |
| Wt. dry soil+tare(gr) | 125.20 | 125.20 | 120.63 | 120.63 |  |  |  |
| Wt. of tare(gr) | 19.62 | 19.62 | 17.33 | 17.33 |  |  |  |
| Wt. dry soil (gr) | 105.58 | 105.58 | 103.30 | 103.30 |  |  |  |
| Wt. of water (gr) | 17.22 | 17.22 | 13.29 | 13.29 |  |  |  |
| M/C (\%) | 16.31 | 16.31 | 12.87 | 12.87 |  |  |  |
| DRY DENSITY (pcf) | 90.3 |  | 101.6 |  |  |  |  |
| \% Saturation* (48\%-52\%) | 50.8 |  | 52.7 |  |  |  |  |
| *Assumes Gs = | 2.7 |  | 2.7 |  |  |  |  |
| EXPANSION INDEX = | 32 |  | 50 |  |  |  |  |
| Potential Expansion (per ASTM 4829-08) | Low |  | Medium |  |  |  |  |
| KOURY <br>  |  |  | Project Name | Borro | Project No.: 17-1021 <br> Date: 4/23/18 | Run by: MFP QA: | $\begin{array}{\|l} \text { Lab: } \\ 18-0023 \\ \text { Series } \end{array}$ |

DENSITY AND MOISTURE CONTENT DATA - EI TEST




|  |  |  | EXPANSION IND DENSITY AND MOISTURE CO | El TEST |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Location/ Elevation | TP17 @ | ' - 4.5' |  |  |  |  |
| USCS Symbol |  |  |  |  |  |  |
| Normal Load (psf) |  |  |  |  |  |  |
| SAMPLE CONDITION | Initial | Final |  |  |  |  |
| Wt Specimen \& Ring (gr) | 714.050 |  |  |  |  |  |
| Wt. of ring (gr) | 366.68 |  |  |  |  |  |
| Wt. Specimen (gr) | 347.370 |  |  |  |  |  |
| Specimen diameter (in) | 4.010 |  |  |  |  |  |
| Specimen radius (cm) | 5.09 |  |  |  |  |  |
| Area of Specimen ( $\mathrm{cm}^{2}$ ) | 81.479 |  |  |  |  |  |
| Init. Spec. height (in) | 1.0020 | N/A |  |  |  |  |
| Height change (final)(in) | N/A | 0.0399 |  |  |  |  |
| Adjusted Spec.height(in) | $1.00$ | 0.9621 |  |  |  |  |
| $" \quad " \quad(\mathrm{~cm})$ | 2.545 | 2.444 |  |  |  |  |
| Specimen Volume ( $\mathrm{cm}^{3}$ ) | 207.371 |  |  |  |  |  |
| Moist Density (pcf) | 104.58 |  |  |  |  |  |
| MOISTURE CONTENT |  |  |  |  |  |  |
| Wt. moist soil+tare(gr) | 155.07 | 155.07 |  |  |  |  |
| Wt. dry soil+tare(gr) | 135.10 | 135.10 |  |  |  |  |
| Wt. of tare(gr) | 19.73 | 19.73 |  |  |  |  |
| Wt. dry soil (gr) | 115.37 | 115.37 |  |  |  |  |
| Wt. of water (gr) | 19.97 | 19.97 |  |  |  |  |
| M/C (\%) | 17.31 | 17.31 |  |  |  |  |
| DRY DENSITY (pcf) | 89.1 |  |  |  |  |  |
| \% Saturation* (48\%-52\%) | 52.5 |  |  |  |  |  |
| *Assumes Gs = EXPANSION INDEX = | $\begin{aligned} & \hline 2.7 \\ & 40 \end{aligned}$ |  |  |  |  |  |
| Potential Expansion (per ASTM 4829-08) | Low |  |  |  |  |  |
| KOURY <br>  |  |  | Project Name: <br> Borrow Site \#2 | Project No.: 17-1021 <br> Date: 4/26/18 | Run by: MFP QA: | $\begin{array}{\|c\|} \hline \text { Lab: } \\ 18-0023 \\ \text { Series } \\ \hline \end{array}$ |

These results are for the exclusive use of the client for whom they were obtained. They apply only to the samples tested and are not indicitive of apparently identical samples.


| MATERIAL DESCRIPTION | LL | PL | PI | \%<\#40 | \%<\#200 | USCS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Light Pale Olive to Light Yellowish Brown Clay | 75 | 18 | 57 |  |  | CH |

Project No. 17-1024 Client:
Project: Borrow Site \#2

Location: TP-6 @ 8' - 9'
Sample Number: 4838 Series
Koury Engineering \& Testing, Inc.
Chino, CA
Remarks:

- Lab \#4838 Series.


## MAXIMUM DENSITY TEST REPORT

Curve No.: 4838 Series
Project No.: 17-1024
Date: 3/10/18
Project: Borrow Site \#2
Client:
Location: TP-6 @ 8' - 9'
Sample Number: 4838 Series
Remarks: Less than 5\% Material retained on the \#4 Sieve.

## MATERIAL DESCRIPTION

Description: Light Pale Olive to Light Yellowish Brown Clay

Classifications -
Nat. Moist. =
Liquid Limit =

USCS: CH

| TEST RESULTS |  |
| :--- | :--- |
| Maximum dry density $=111.1 \mathrm{pcf}$ |  |
| Optimum moisture $=16.2 \%$ |  |



Figure
$\qquad$

# e are a key member of the construction team while safeguarding the public. We improve operational logistics and provide superior quality control through the continuing development of our engineering staff and technical expertise, utilization of classroom training and field supervisors, thus defining the industry standard. 

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