



GEOTECHNICAL & SEISMIC ENGINEERING, CONSTRUCTION INSPECTION & MATERIALS TESTING SERVICES



April 16, 2019 Project No. 17-1025

Mr. John R. Burroughs, LEED AP, President Commerce Construction Co., L.P. 13191 Crossroads Parkway North 6<sup>th</sup> Floor City of Industry, CA 91746

**Subject:** Limited Borrow Site Feasibility Study

**Alternative Borrow Site 5** 

Southwest Corner of Hereford Drive and Hellman Avenue

City of Chino, California

Dear Mr. Burroughs:

Presented herein are our preliminary findings and conclusions regarding the suitability of the Borrow Site 5 soils to be used as engineered fill to balance the grade for the 95 Acres OC Prado site construction located on the southeast corner of Bickmore Avenue and Mountain Avenue in the City of Chino.

Based on the conceptual grading plan, the proposed irregular-shaped Borrow Site 5 covers an area of about 723,000 square feet or roughly 16.6 acres. The site is bounded by Hereford Drive to the north, Walters Street to the west, Cucamonga Creek to the south and Hellman Avenue to the east. A Site Vicinity Map with approximate ground contour elevations is presented in Appendix A as Figure A-1.

### Field Exploration and Laboratory Testing for Feasibility Study

The field exploration program for the feasibility study consisted of excavating ten test pits on March 13, 2019. A rubber tire mounted backhoe was used to excavate the 10 test pits ranging in depths from about 11 to 17 feet below the existing ground surface. The locations of the test pits are shown on the Field Exploration Map, Figure A-2, presented in Appendix A. Bulk samples were obtained from the test pits for laboratory testing.

Laboratory tests, including moisture content, #200 sieve wash, expansion index, maximum density, pocket penetrometer, and corrosivity were performed to aid in the classification of the materials encountered and to evaluate their engineering properties. Sulfates, chlorides, resistivity, and PH tests (corrosivity tests) were also performed on selected samples. The results of pertinent laboratory tests are presented on the boring logs in Appendix B, and/or in Appendix C.

### **Site Geology**

The site is located within the Upper Santa Ana River Valley, which consists of a series of coalescing alluvial fans formed by streams flowing out of the San Gabriel Mountains to the north. The valley lies within the Peninsular Ranges geomorphic province, which is characterized by alluviated basins, elevated erosion surfaces, and northwest-trending mountain ranges bounded by northwest trending faults. The site, which is located within the Chino Basin, is underlain by sediments deposited by the Santa Ana River and its tributaries such as the Chino Creek.

Morton and Miller (2006) show the site to be underlain by very old alluvial-fan deposits (See Figure A-3 in Appendix A). The sediments encountered during the subsurface investigation consisted predominantly of clay.

#### **Surface Site Conditions**

Access to the site is presently via Hellman Avenue at the northeast corner of the site. The site is roughly rectangular in area: extending about 1200 feet in the east-west direction and 1250 feet in the northerly direction.

The site was previously used as dairy farm and cattle raising. The site is presently vacant, and the previously existing buildings and cattle shelters have been removed. However, few of the slabs on grade, foundations, fence posts, and most likely some underground utilities are still in place. At the time of the field exploration in March 2019, most of the site exposed bare ground. There was a few trees and shrubs along Hellman Ave and around the seasonal water ponds.

The south side of the site contains a 4 to 6-foot-deep water detention basin; the basin has an entry ramp in the northeast corner. Little vegetation and trash were found within the basin.

The site generally slopes gently from north to south with elevations ranging for the most part from about 555 to 545 feet. Along the east property line, within the southeast portion of the site, there is a gentle slope descending about 8 to 11 feet to the Cucamonga Creek.

In its present state, the site has been cleared of all past structures such as buildings, shelters, and above ground ancillary facilities; however, it appears that several foundations, slabs on grade, and underground conduits are still in place. There are overhead powerlines present onsite, trending north-south, west of Hellman Ave and roughly 60 feet into the property. The dominant features of the site are the many small berms and unpaved roads that were constructed across the site. Many of the berms appear to have been constructed by pushing onsite soils into piles. Most of the berms have heights in the range of 1 to 2 feet and consist of relatively loose undocumented fill.

Within the site area, there are several small piles of construction debris roughly 10 feet in diameter consisting of crushed concrete, rebar and trash.

#### **Soil Conditions**

The subsurface soil profile consists generally of artificial fill underlain by alluvial deposits. For the most part, the fill is generally on the order of 1 to 3 feet in thickness. The deeper fills appear to be associated with previous improvements that were demolished. The fill derived from onsite shallow soils consists predominantly of lean clay with sand and sandy lean clay, and includes fat clay. clayey sand, silty sand, and construction debris.

The alluvium soils consist predominantly of stiff to very stiff medium plastic to high plastic sandy clay and clay with sand. Some discrete layers of silty sand and poorly graded sand with silt were encountered in Test Pit 1 from 14½ to 17 feet, Test Pit 3 from 12½ to 14½ feet, and Test Pit 8 from 14 to 16½ feet.

The moisture contents of clay soils are highly variable, ranging from about 16½ to 49½ percent with an average of about 28 percent while the sand material moisture contents range from about 10 to 37 percent with an average of about 19 percent. Based on two maximum density tests performed and prior experience with similar soils, many of the clay sample moisture contents are about 7 to 20 percent above optimum for the soils sampled at depths between 4 and 13 feet below the ground surface.

 Test Pit Number
 TP8 @ 4-4.5
 TP2 @ 1.5-2

 Maximum Dry Density (pcf)
 97.1
 81.3

 Optimum Moisture Content (%)
 23.4
 36.4

**Table 1 – Maximum Density Test Results** 

The fine contents range from about 50 to 98 percent with an average of about 77 percent for clay and from about 8 to 42 percent with an average of about 25½ percent for the sand. The average relatively low fine contents of the clay soils are attributed to the presence of concretions (hard matter formed by precipitation of mineral cement between particles), which was observed in many of the clay samples. The pocket penetrometer tests indicate unconfined compression strength on the order of 1 to 4.5 tsf with an average of about 2.6 tsf.

The site soil expansion potential ranges from very low to very high. Table 2 presents the data for 12 tests sampled at depths ranging from 1 to 5.5 feet. These tests indicate expansion index variation from 19 to 174. Within the upper 4 feet, the test data obtained to date indicate expansion indices ranging between 19 and 98 and moisture contents between about 12 and 47 percent with an average of about 30 percent. Except for Test Pit 2, at depths of 4 to 4½ feet and Test Pit 4 at depths of 5 to 5½ feet, all the expansion index tests performed on samples at depths greater than 3½ feet indicated expansion indices greater than 65. The sample collected at Test Pit 3 between the depths of 4.8 and 5.2 feet indicated a very high expansion potential.

The moisture contents of the clay below a depth of 4 feet range predominantly between 24 and 49 percent with an average of about 30 percent. On average, this moisture content is about 6 to 12½ percent above optimum.

**Table 2 – Expansion Index Test Results** 

Test Pit	TP-1	TP-1	TP-2	TP-2	TP-3	TP-4	TP-5	TP-5	TP-7	TP-7	TP-8	TP-10
Depth (ft)	0-1	3.7-4	1.5-2	4-4.5	4.8-5.2	5-5.5	1-1.5	2.5-3	1-1.5	3.5-4	4-4.5	4.5-5.5
Expansion	43	98	52	38	174	34	39	39	19	60	80	66
Moisture	23.4	19.1	42.0	49.4	33.1	42.9	22.0	24.0	26.0	22.0	31.7	44.0
Fines	54	83	89	93	95	77	83	77	87	85	59	89

#### Groundwater

No groundwater was encountered in the excavated test pits.

#### Corrosivity

The corrosivity tests performed indicates that the site soils are generally severely corrosive to ferrous metal. In addition, test result from Test Pit 2 reveal that the soil has a moderate sulfate exposure or Class S1 exposure category in accordance with ACI 318-14, Table 19.3.1.1. The corrosivity test results are summarized in the following Table 3.

**Table 3 - Corrosion Test Results** 

Boring	Depth (ft)	Minimum Resistivity (ohm-cm)	pН	Soluble Sulfate Content (ppm)	Soluble Chloride Content (ppm)
TP-2	1.5-2.0	304	8.2	1360	700
TP-6	1.5-2.0	491	8.3	654	270

The test results from Test Pit 2 reveal a moderate sulfate exposure, which if imported, will require concrete special design considerations in accordance with ACI 318, Table 19.3.2.1 if this soil is placed against concrete.

#### **Conclusions and Recommendations**

Based on the data collected from the field to date, it appears feasible to import some material from Borrow Site 5 to use at the OC Prado site. Soil with high expansion potential was encountered at all depths throughout the soil profile. However, with proper blending and processing, it appears that mainly the upper 4 feet of soils could be suitable for foundation support. The deeper soils generally have higher moisture contents, higher plasticity and are deemed to have higher expansion potential than the soil at 4 feet and shallower, and therefore are less desirable to be used as fill. If need be, after proper processing and dry back, these deeper materials could be used as general fill in parking lots and driveway areas at the OC Prado site.

#### **CLOSURE**

The findings and recommendations presented in this report were based on the results of our field and laboratory investigations, combined with professional engineering experience and judgment. The report was prepared in accordance with generally accepted engineering principles and practice. We make no other warranty, either expressed or implied. Subsurface variations between and beyond the test pits should be anticipated. Samples obtained during this investigation will be retained in our laboratory for a period of 45 days from the date of this report and will be disposed after this period.

Should you have any questions concerning this submittal, or the recommendations contained herewith, please do not hesitate to call our office.

Respectfully submitted,

KOURY ENGINEERING & TESTING, INC

Jacques B. Roy, PE, Principal Engineer

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2.File (B)

**APPENDICES** 

Appendix A: Maps and Plans

Vicinity Map – Figure A-1 Field Exploration Map – Figure A-2 Geology Map – Figure A-3

**Appendix B: Field Exploratory Test Pits** 

Test Pits 1 through 10

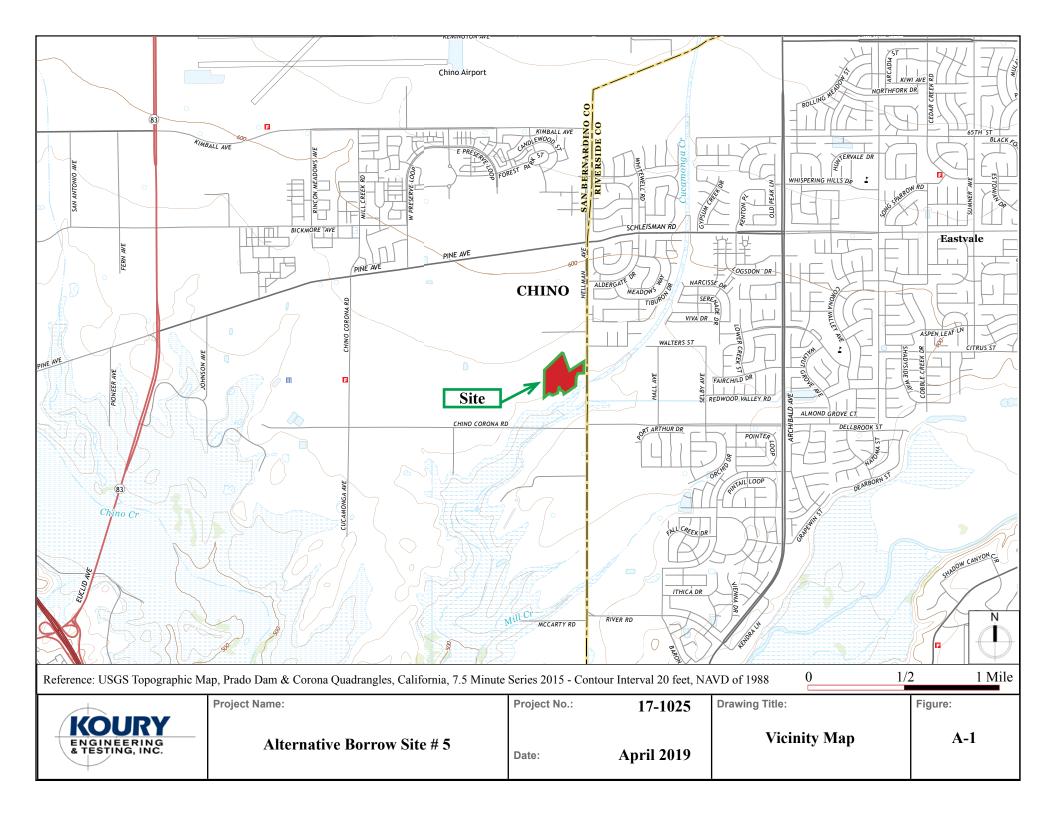
**Appendix C: Laboratory Test Results** 

#### **REFERENCES**

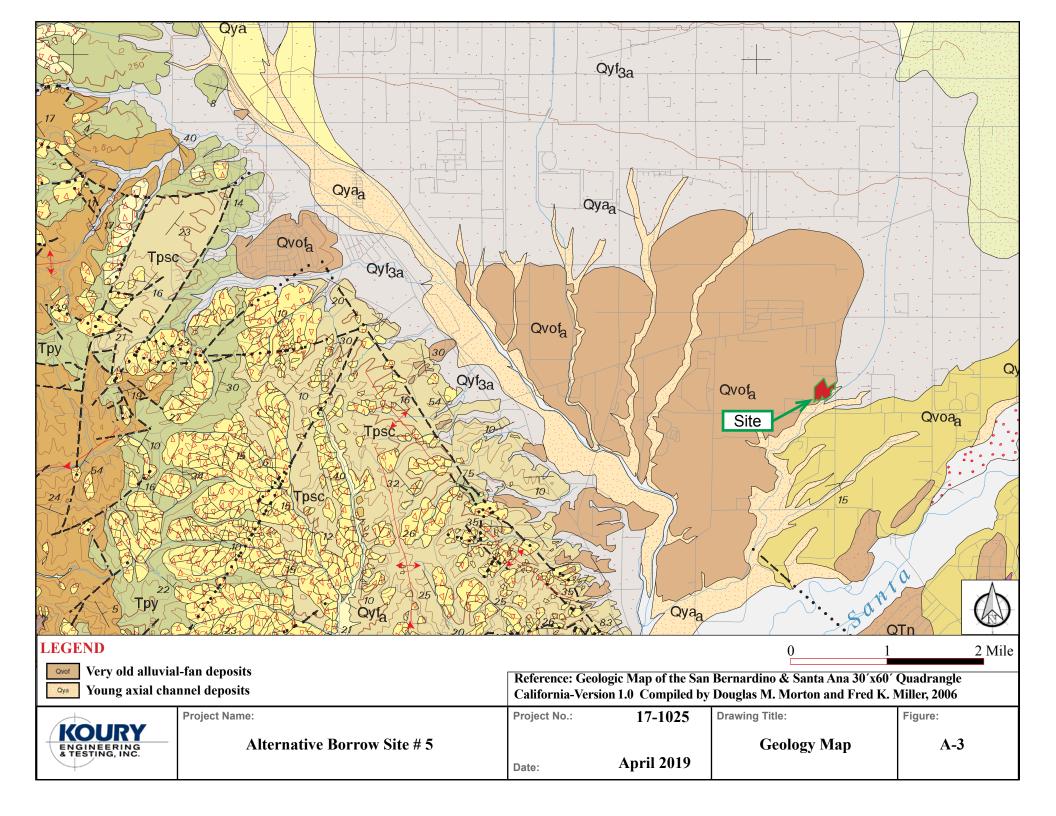
- 1. California Division of Mines and Geological Survey, 1998, Seismic Hazard Zone Report 045 for the Prado Dam 7.5 Minute Quadrangle, California.
- 2. California Division of Mines and Geological Survey, 2003, Earthquake Fault Zones, Prado Dam Quadrangle, May 1, 2003.
- 3. City of Chino General Plan, Safety Element, 2010, Final Report.
- 4. US Army Corps of Engineers, Geotechnical Investigations, Engineering Manual EM 1110-1-1804, dated 8/26/86.
- 5. US Army Corps of Engineers, Laboratory Soils Testing, Engineering Manual EM 1110-2-1906, dated 8/26/86.

# APPENDIX A

Maps and Plans







# **APPENDIX B**

Field Exploratory Test Pits

# **KEY TO LOGS**

		so	ILS CLAS	SSIFICA	TION
	MAJOR DIVISIONS	3	GRAPHIC LOG	USCS SYMBOL	TYPICAL NAMES
	GRAVELS	CLEAN GRAVELS		GW	WELL-GRADED GRAVELS, GRAVEL-SAND MIXTURES, LITTLE OR NO FINES
COARSE GRAINED	GRAVELS	LESS THAN 5% FINES		GP	POORLY-GRADED GRAVELS, GRAVEL-SAND MIXTURES, LITTLE OR NO FINES
SOILS	MORE THAN 50% OF COARSE FRACTION IS	GRAVELS WITH FINES		GM	SILTY GRAVELS, GRAVEL-SAND-SILT MIXTURES
	LARGER THAN NO. 4 SIEVE	MORE THAN 12% FINES		GC	CLAYEY GRAVELS, GRAVEL-SAND-CLAY MIXTURES
	SANDS	CLEAN SANDS		sw	WELL-GRADED SANDS, GRAVELLY SANDS, LITTLE OR NO FINES
MORE THAN 50% OF MATERIAL IS	SANDS	LESS THAN 5% FINES		SP	POORLY-GRADED SANDS, GRAVELLY SANDS, LITTLE OR NO FINES
LARGER THAN NO. 200 SIEVE SIZE	50% OR MORE OF COARSE FRACTION IS	SANDS WITH FINES		SM	SILTY SANDS, SAND-SILT MIXTURES
	SMALLER THAN NO. 4 SIEVE	MORE THAN 12% FINES		sc	CLAYEY SANDS, SAND-CLAY MIXTURES
	SILTS AN	ID CLAYS		ML	INORGANIC SILTS AND VERY FINE SANDS, ROCK FLOUR, SILTY OR CLAYEY FINE SANDS OR CLAYEY SILTS WITH SLIGHT PLASTICITY
FINE GRAINED SOILS		S LESS THAN 50		CL	INORGANIC CLAYS OF LOW TO MEDIUM PLASTICITY, GRAVELLY CLAYS, SANDY CLAYS, SILTY CLAYS, LEAN CLAYS
	בועטוט בוואודו וז	DELOG TRIAIN SU		OL	ORGANIC SILTS AND ORGANIC SILTY CLAYS OF LOW PLASTICITY
	SILTS AN	ID CLAYS		МН	INORGANIC SILTS, MICACEOUS OR DIATOMACEOUS FINE SANDY OR GRAVELLY ELASTIC SILTS
50% OR MORE OF MATERIAL IS SMALLER THAN NO. 200 SIEVE SIZE	LIQUID LIMIT I	S 50 OR MORE		СН	INORGANIC CLAYS OF HIGH PLASTICITY, FAT CLAYS
	בואַטוט בוואודד	O SO OIN WICINE		ОН	ORGANIC CLAYS OF MEDIUM TO HIGH PLASTICITY, ORGANIC SILTS
HIGH	ILY ORGANIC S	SOILS		PT	PEAT AND OTHER HIGHLY ORGANIC SOILS

GRAIN SIZES												
SILT AND CLAY		SAND		GR/	VEL	COBBLES	DOLU DEDO					
SILT AND CLAT	FINE	MEDIUM	COARSE	FINE	FINE COARSE		BOOLDENS					
	#200	#40	#10	#4	3/4"	ູ້ <sub>ເ</sub>	12"					
	SIEVE SIZES											

# **KEY TO LOGS (continued)**

	SPT/CD BLOW COUNTS VS. CONSISTENCY/DENSITY												
FINE-GRAINED S	OILS (SILT	S, CLAYS, etc.)	GRANULAR SOILS (S	ANDS, GRAVELS	S, etc.)								
CONSISTENCY	*BLC	WS/FOOT	RELATIVE DENSITY	*BLOWS/F	TOOT								
CONSISTENCT	SPT	CD	RELATIVE DENSITY	SPT	CD								
SOFT	0-4	0-4	VERY LOOSE	0-4	0-8								
FIRM	5-8	5-9	LOOSE	5-10	9-18								
STIFF	9-15	10-18	MEDIUM DENSE	11-30	19-54								
VERY STIFF	16-30	19-39	DENSE	31-50	55-90								
HARD	over 30	over 39	VERY DENSE	over 50	over 90								

<sup>\*</sup> CONVERSION BETWEEN CALIFORNIA DRIVE SAMPLERS (CD) AND STANDARD PENETRATION TEST (SPT) BLOW COUNT HAS BEEN CALCULATED USING "FOUNDATION ENGINEERING HAND BOOK" BY H.Y. FANG. (VALUES ARE FOR 140 Lbs HAMMER WEIGHT ONLY)

DESCRIPTIVE ADJECTIVE VS. PERCENTAGE											
DESCRIPTIVE ADJECTIVE	PERCENTAGE REQUIREMENT										
TRACE	1 - 10%										
LITTLE	10 - 20%										
SOME	20 - 35%										
AND	35 - 50%										

\*THE FOLLOWING "DESCRIPTIVE TERMINOLOGY/ RANGES OF MOISTURE CONTENTS" HAVE BEEN USED FOR MOISTURE CLASSIFICATION IN THE LOGS.

APPRO	APPROXIMATE MOISTURE CONTENT DEFINITION										
DEFINITION	DESCRIPTION										
DRY	Dry to the touch; no observable moisture										
SLIGHTLY MOIST	Some moisture but still a dry appearance										
MOIST	Damp, but no visible water										
VERY MOIST	Enough moisture to wet the hands										
WET	Almost saturated; visible free water										

**Project No.:** 17-1025 Boring No.: TP-1 Project Name: Borrow Site 5 **Sheet:** 1 of: 1 Drilling Method: Backhoe Sampling Method: Bulk **Ground Elevation:** Dry Unit Weight (pcf) Sample Location Moisture Content (%) **Graphic Log** Blows per 6" Soil Type (USCS) Sample No. Depth (ft) Drilling Co.: Bill Bastedo Hammer Weight: Location :See Figure A-2 Date Drilled: 3/13/19 Additional Description Tests #200 Wash 1 23.4 FILL: Fines = 54% EI = 43 Sandy Lean CLAY; pockets of clayey sand, stiff, moist, very dark brown Fines = 81% PP = 2.5 tsf 2 19.3 CL ALLUVIUM: Lean CLAY with SAND; stiff to very stiff, moist, dark yellowish Fines = 83% PP = 4.5 tsf EI = 98 Fines = 84% PP= 1.75-2.4 tsf 3 19.1 brown 4 23.0 Lean to Fat CLAY with SAND; stiff, moist, dark brown #200 Wash 5 26.2 Lean to Fat CLAY; very stiff, moist to very moist, dark Fines = 93% PP=2.5-3 tsf yellowish brown CL/CH 6 26.8 #200 Wash Fines= 79% PP=2.0 tsf Lean to Fat CLAY with SAND; stiff, moist to very moist, olive brown 7 40.0 #200 Wash Fines = 92% #200 Wash CH Fat CLAY; layers of silty sand, firm, moist to very moist, olive gray 8 11.3 Fines = 12% Poorly Graded SAND with SILT; fine to coarse, pockets of SP-SM #200 Wash gray clay, moist to very moist, dark yellowish brown 9 17.0 Fines = 8%End of test pit @ 16' 9" No groundwater encountered

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+	KC ENG & TES	DUI INEER STING,	RY ING INC.					Project No.: 17-1025 Project Name: Borrow Site 5  Sheet:  Drilling Method: Backhoe	<b>No. :</b> TP-2 1 of : 1
Sample No.	Moisture Content (%)	Dry Unit Weight (pcf)	Blows per 6"	Depth (ft)	Sample Location	Graphic Log	Soil Type (USCS)	Sampling Method : Bulk Ground E Hammer Weight : Drilling C	ilevation: o.: Bill Bastedo ed: 3/13/19
Sal	Cor	Wei	Blo	ă	amb	Gra	ις (	Description	Additional
1 2	34.2 42.0			0 <u> </u>	8   X    X		CL/CH	Cobbles at the surface and 8 inches of sand  FILL: Sandy Lean to Fat CLAY; organic inclusions, stiff, moist, very dark brown	Tests Fines = 64% PP = 3-4 tsf Corrosion EI = 52 Fines = 89% PP = 3.5 tsf
3	49.4			5 —	<b>※</b>		СН	ALLUVIUM: Fat CLAY; very stiff, moist, very dark gray	#200 Wash Fines = 93% PP = 4.5 tsf EI = 38
4	24.7			10-	<b>X</b>		CL/CH	Lean to Fat CLAY; very stiff, moist, mottled gray with brown inclusions	Fines = 92% PP = 4.0 tsf
5	27.2				<b>≫</b>			dark gray with rusty brown pockets	Fines = 83% PP = 2-2.5 tsf
				15 —				End of test pit @ 12' 6" No groundwater encountered	

	illig i							Project No. : 47 4005	
/	100	DU	PV					Project No.: 17-1025 Project Name: Borrow Site 5	<b>g No. :</b> TP-3
+		INEE							:1 of:1
L	4	<i></i>	1110.					Drilling Method: Backhoe	
·	%)	cf)	9		tion	эg	0	. 6	Elevation:
Š	ture (G	Unit (po	per	) (ft	oca.	ic Lo	rype cs)		Co.: Bill Bastedo
Sample No.	Moisture Content (%)	Dry Unit Weight (pcf)	Blows per 6"	Depth (ft)	Sample Location	Graphic Log	Soil Type (USCS)	Location : See Figure A-2 Date Di	illed: 3/13/19
Š	<b>-</b> 8	We	Bic		Sam	อ	0)	Description	Additional Tests
1	32.7			0_	<b>※</b>		CL	Gravel, cobbles, and construction debris FILL: Lean CLAY with SAND; some organic, stiff, moist,	#200 Wash Fines = 83% PP=2.5-2.75 tsf
2	22.7						CL/CH	dark brown  ALLUVIUM: Lean to Fat CLAY with SAND; trace concretions, stiff, moist, dark brown	#200 Wash Fines = 80% PP = 1.5 tsf
3	33.1			5 —	<b>※</b>			Fat CLAY; firm to stiff, moist to very moist, mottled dark	EI = 174 Fines = 95% PP = 1.0 tsf
4	28.1				<b>X</b>		СН	yellowish brown with dark brown	#200 Wash Fines = 90% PP=1.5-1.75 tsf
5	25.0			-    -	<b>※</b>		CL	Lean CLAY with SAND; firm, moist, dark grayish brown (mostly silt)	Fines = 83% PP = 0.5 tsf
6	38.0			10	<b>*</b>		СН	Fat CLAY; stiff, moist to very moist, grayish brown	#200 Wash Fines = 98% PP = 1.75 tsf
7	10.3						SM	<b>Silty SAND;</b> fine to coarse, lumps of sandy clay, dark yellowish brown	#200 Wash Fines = 13%
8	33.6			15—	×		ML	SILT; very stiff, trace of organic, moist to very moist, pocket	ts Fines = 89% PP = 2.5 tsf
								of dark clay and oxidation	
				-				End of test pit @ 15' 5"  No groundwater encountered	
				20					
				_	1				
				-	1				
				-	1				
				25 —	1				
				1 =	1				
				<u> </u>	1				
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+		DU INEEF STING,						Project No.: 17-1025 Project Name: Borrow Site 5  Sheet: 1 co	
Sample No.	Moisture Content (%)	Dry Unit Weight (pcf)	Blows per 6"	Depth (ft)	Sample Location	Graphic Log	Soil Type (USCS)	Drilling Method : BackhoeSampling Method : BulkGround ElevalHammer Weight :Drilling Co. :Location : See Figure A-2Date Drilled :	Bill Bastedo
ľ	ŭ	>	В		Sar	g		Description	Tests
1	16.5 45.7			0 _	<b>X</b>		sc	Cobbles, boulders, and concrete at surface  FILL: Clayey SAND; trace of concretions, trace of gravel, moist, very dark brown	#200 Wash Fines = 19% #200 Wash
3	42.9			5 —	<u> </u>		CL/CH	ALLUVIUM: Sandy Lean to Fat CLAY; trace of organic, moist, stiff, very dark brown	Fines = 65% PP = 3-4 tsf Fines = 77% PP = 2.5 tsf EI = 34
4 5	26.3			- - - -	  X		CL	Lean CLAY with SAND; firm, moist, dark grayish brown (mostly silt)	#200 Wash Fines = 84% PP = 2.5-3 tsf #200 Wash
5	24.0			10—					Fines = 83% PP = 2.0 tsf
6	25.2			<u>-</u>	<b>※</b>		CL/CH	Sandy Lean to Fat CLAY; trace of organics, rootlets, moist, very dark greenish gray	#200 Wash Fines = 73% PP = 2-2.5 tsf
				15 —				No groundwater encountered	

	illig								
4		DU						Froject Name. Borrow Site 5	<b>No.</b> : TP-5
	+	INEEF	INC.		اءا			Sheet: Drilling Method: Backhoe	1 of : 1  Elevation:
Sample No.	Moisture Content (%)	Dry Unit Weight (pcf)	Blows per 6"	Depth (ft)	Sample Location	Graphic Log	Soil Type (USCS)	Hammer Weight : Drilling C	co.: Bill Bastedo
San	Con	Dı Weiç	Blov	۵	amp	Gra	So (1	Description	Additional
1	46.8			0	S ≫		CL/CH	Topsoil; Sandy Lean to Fat CLAY; trace of organics, very	Tests Fines = 50%
2	22.0				<b>※</b>		CL	dark brown  FILL: Lean CLAY with SAND; trace of concretions, very moist, very dark brown	EI = 39 Fines = 83% PP = 3-3.2 tsf
3	24.0			5 —	<b>※</b>		CL/CH	ALLUVIUM: Lean to Fat CLAY with SAND; trace of concretions, stiff, moist to very moist, pale brown	EI = 39 Fines = 77% PP = 2-2.5 tsf
4	21.8				<b>X</b>		СН	Fat CLAY; concretions, stiff, moist to very moist, pale brown	#200 Wash Fines = 87% PP = 1.5 tsf
5	30.0			10	<b>※</b>		CL/CH	Lean to Fat CLAY with SAND; stiff, moist, dark yellowish brown	#200 Wash Fines = 76% PP = 1.5 tsf
6	16.6				<b>※</b>		CL	Sandy CLAY; firm, moist, yellowish brown to very dark brow	
				25				No groundwater encountered	

-		DU						Froject Name. Bollow Site 5	<b>g No. :</b> TP-6 :1 of :1
Sample No.	Moisture Content (%)	Dry Unit Weight (pcf)	Blows per 6"	Depth (ft)	Sample Location	Graphic Log	Soil Type (USCS)	Sampling Method : Bulk Ground Hammer Weight : Drilling	Elevation: Co.: Bill Bastedo   illed: 3/13/19
Sa	Sor	We	Blo	Δ	Sam	Gra	S )	Description	Additional Tests
				0 _			SM	Gravel, cobbles, concrete, wood, asphalt pieces at surface FILL: Silty SAND; trace of gravel and topsoil	
1	32.9			-   -   -	X		CL/CH	ALLUVIUM: Lean to Fat CLAY; pockets of silty sand, stiff, moist, brow with pale brown	Corrosion Fines = 85% PP = 4.0 tsf
2	20.3			5 —	<b>※</b>				Fines = 75% PP = 3.5-4.5 tsf
3	21.0				<b>※</b>		CL	Lean CLAY with SAND; very stiff, moist, mottled brown	#200 Wash Fines = 77%
4	23.2			10—	<b>※</b>			Sandy Lean CLAY; very stiff, moist, olive brown	Fines = 62% PP=2.75-4.2 tsf
5	23.1				×				Fines = 61% PP=2.5-2.75 tsf
				15—15—20—25—30—30—				End of test pit @ 11' No groundwater encountered	
				25 —					

							1				
-(		DU						Project No.: 17-1025 Project Name: Borrow Site 5  Sheet: 1	<b>No.</b> : TP-7 of : 1		
Sample No.	Moisture Content (%)	Dry Unit Weight (pcf)	Blows per 6"	Depth (ft)	Sample Location	Graphic Log	Soil Type (USCS)	Hammer Weight : Drilling Co	Ground Elevation: Drilling Co.: Bill Bastedo Date Drilled: 3/13/19		
Sa	Cor Wei			Wei Do Do Gra		S O	Description	Additional Tests			
	00.0			0 _			sc	Patchy grass over clayey sand topsoil, trace of organic	#200 Wash		
3	36.8 26.0 22.0 25.8				×× ×		CL	ALLUVIUM: Lean CLAY; abundant concretions, very stiff, moist, brown	Fines = 42% EI = 19 Fines = 87% PP = 4.5 tsf Fines = 85% PP = 2.5-3 tsf EI = 60 Fines = 88%		
5	27.3			5	\times \t		сцсн	Lean to Fat CLAY with SAND; firm to stiff, moist to very moist, light olive brown	#200 Wash Fines = 77% PP = 1-1.25 tsf		
6	19.7			_	<b>※</b>		CL	Sandy Lean CLAY; firm to stiff, moist, light olive brown	Fines = 54%		
7	22.4			15—-   20—-    30—-             -				End of test pit @ 15' No groundwater encountered	Fines = 60% PP = 2.5 tsf		

	Borning Log											
								Project No. : 17-1025  Broiget Name : Perrow Site 5  Boring No	• TD_Ω			
KOURY								Project Name : Borrow Site 5	IF-0			
	ENG & TE	INEEF	INC.					Sheet: 1 o	f : 1			
	1							Drilling Method: Backhoe				
								Sampling Method : Bulk Ground Eleva	tion:			
No	ر% (%	it pc	∍r 6	Œ	cati	Γοί	be 3)	Hammer Weight : Drilling Co. :	Bill Bastedo			
ple	Moisture Content (%) Dry Unit Weight (pcf) Blows per 6"					hic	I Ty	Location : See Figure A-2 Date Drilled :				
Sample No.	Mo	Dr. eig	MΟ	Depth (ft)	Sample Location	Graphic Log	Soil Type (USCS)		Additional			
S	Ö	>	В		Sar	g		Description	Tests			
	40.0			0 _	$\vee$		sc	Retention basin slope	#200 Wash			
1 2	12.6 44.1			_	<u>**</u>		30	FILL: Clayey SAND; layers of sandy clay, moist, trace of	Fines = 33% Fines = 74%			
3	42.0			_	<b>※</b>			gravel, concretions and organic	Fines = 84% PP=3.75 tsf			
	12.0			_								
				_	Ш		CL/CH	ALLUVIUM:  Lean to Fat CLAY with SAND; trace of organic, stiff, moist,	EI = 80 Fines = 59%			
4	31.7				<b>※</b>		OLJOIT	dark gray (max density 97.1 pcf @ 23.4% moisture)	PP = 3.5-4 tsf			
				5 —	1			, , , , , , , , , , , , , , , , , , ,	Fines = 83% PP = 2.5-3 tsf			
5	27.8			_	<b>※</b>				PP = 2.5-3 (SI			
6	26.3			_	×				PP = 1-1.5 tsf			
	20.0			_					Fines = 68%			
					11							
				10—	1 1			Sandy Lean CLAY; stiff, moist to very moist, concretions,	#200 Wash			
7	22.1			10-			CL	olive brown with dark brown inclusions	#200 Wash Fines = 50% PP = 2.0 tsf			
8	7 23.1 8 28.5			_	8							
					1		Fines = 71.3% PP = 2-2.2 tsf					
				_	1							
				_	11							
9	16.1			15 <b>—</b>	<b>※</b>			Silty SAND; fine to medium, lumps of clay, moist to very	Fines = 40%			
				-	1 1		SM	moist, dark yellowish brown	Fines = 22%			
10	17.5							<u> </u>	1 11103 = 2270			
				_	1			End of test pit @ 16' 6"				
					1			No groundwater encountered				
				_	11							
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+		DU INEER STING		-				Project No.: 17-1025 Project Name: Borrow Site 5  Drilling Method: Backhoe	Boring No		
Sample No.	Moisture Content (%)	Dry Unit Weight (pcf)	Blows per 6"	Depth (ft)	Sample Location	Graphic Log	Soil Type (USCS)	Sampling Method: Bulk Hammer Weight: Location: See Figure A-2	ration: : Bill Bastedo : 3/13/19		
Sa	_ လ	Me	Blo		Sam	Ğ	o -	Description		Additional Tests	
				0 _				FILL: Sandy Lean CLAY			
1	31.6				<b>※</b>			ALLUVIUM: Lean CLAY with SAND; stiff, mo yellowish brown	ist, dark	Fines = 76% PP = 2.5 tsf Fines = 85% PP=2.75-3.5 tsf	
3	21.0 20.3			5 —	<u> </u>		CL	Sandy Lean CLAY; concretions, stiff, moist to yellowish brown	very moist,	Fines = 69%	
4	18.5				×			Lean CLAY with SAND; concretions, moist, o white	#200 Wash Fines = 82%		
5	19.3 17.9			10	<b>X</b>			Sandy Lean CLAY; caliche stringers, very stif olive brown with white specs	Fines = 74% PP = 3-4 tsf Fines = 60%		
				15 —				End of test pit @ 11' 6" No groundwater encountered			

_	illig i	3							
+	K(C ENG & TE	<b>DU</b>	RY RING , INC.					Sheet: 1	<b>No. :</b> TP-10 of : 1
Sample No.	Moisture Content (%)	Dry Unit Weight (pcf)	Blows per 6"	Depth (ft)	Sample Location	Graphic Log	Soil Type (USCS)	Location : See Figure A-2 Date Drille	evation:  b.: Bill Bastedo  d: 3/13/19  Additional
တ	_ ပ	Š	ā	-	San	Ō	•	Description	Tests
1	36.0			0 _	<b>※</b>		sc	FILL: Clayey SAND; topsoil, trace of organics, moist, dark brown	#200 Wash Fines = 41%
2	30.8				<b>X</b>		CL/CH	ALLUVIUM: Sandy Lean to Fat CLAY; trace of organic, very moist, very dark grayish brown	#200 Wash Fines = 57%
3	44.0			5 -	X		СН	Fat CLAY; stiff, moist to very moist, black	#200 Wash Fines = 89% PP = 4.0 tsf EI = 66
4	28.5				<b>※</b>				Fines = 88% PP = 1-1.5 tsf
5	24.0			10—	<b>※</b>		CL	<b>Lean CLAY with SAND;</b> stiff, moist to very moist, dark grayis brown	Fines = 76% PP = 2.0 tsf
6	24.8			15 —				End of test pit @ 13' No groundwater encountered	PP=1.75-2.2 tsf

# **APPENDIX C**

Laboratory Test Results

#### **EXPANSION INDEX TESTS** DENSITY AND MOISTURE CONTENT DATA - EI TEST Location/ Elevation TP 5 @ 2.5-3' TP 1 @ 0-1' TP 1 @ 3.75-4' TP 2 @ 1.5-2' **USCS Symbol** Normal Load (psf) **SAMPLE CONDITION** Initial Final Initial Final Initial **Final** Initial Final Wt Specimen & Ring (gr) 726.100 753.180 657,110 720,710 364.10 367.40 366.64 367.31 Wt. of ring (gr) Wt. Specimen (gr) 362.000 385.780 290.470 353.400 Specimen diameter (in) 4.010 4.010 4.010 4.010 Specimen radius (cm) 5.09 5.09 5.09 5.09 Area of Specimen (cm<sup>2</sup>) 81.479 81.479 81.479 81.479 N/A Init. Spec. height (in) 1.0005 N/A 1.0030 N/A N/A 1.0030 1.0030 Height change (final)(in) N/A 0.0427 N/A 0.0983 N/A 0.0520 N/A 0.0389 Adjusted Spec.height(in) 1.00 0.9578 1.00 0.9047 1.00 0.9510 1.00 0.9641 (cm) 2.541 2.433 2.548 2.298 2.548 2.416 2.548 2.449 Specimen Volume (cm<sup>3</sup>) 207.061 207.578 207.578 207.578 Moist Density (pcf) 109.15 116.02 87.36 106.29 MOISTURE CONTENT Wt. moist soil+tare(gr) 445.45 445.45 482.74 482.74 276.47 276.47 442.91 442.91 Wt. dry soil+tare(gr) 402.84 239.60 402.84 441.09 441.09 239.60 397.43 397.43 Wt. of tare(gr) 83.45 83.45 96.96 96.96 96.96 96.96 90.02 90.02 319.39 142.64 142.64 Wt. dry soil (gr) 319.39 344.13 344.13 307.41 307.41 Wt. of water (gr) 42.61 42.61 41.65 41.65 36.87 36.87 45.48 45.48 M/C (%) 13.34 13.34 12.10 12.10 25.85 25.85 14.79 14.79 DRY DENSITY (pcf) 96.3 103.5 69.4 92.6 48.0 52.0 48.9 48.7 % Saturation\* (48%-52%) 2.7 2.7 2.7 \*Assumes Gs = 2.7 EXPANSION INDEX = 52 43 98 39 **Potential Expansion** High Medium Low Low (per ASTM 4829-08) Run by: Project Name: Project No.: 17-1025 Lab: KOURY QA: **Borrow Site 5** Date: 04-15-2019

#### **EXPANSION INDEX TESTS** DENSITY AND MOISTURE CONTENT DATA - EI TEST **Location/ Elevation** TP 2 @ 4-4.5' TP 7 @ 3.5-4' TP 8 @ 4-4.5' TP 7 @ 1-1.5' **USCS Symbol** Normal Load (psf) SAMPLE CONDITION Initial Final Initial Final Initial Final Initial Final Wt Specimen & Ring (gr) 649.030 744.340 705.390 700.250 366.37 366.31 Wt. of ring (gr) 366.44 363.90 Wt. Specimen (gr) 282.660 378.030 338.950 336.350 Specimen diameter (in) 4.010 4.010 4.010 4.010 Specimen radius (cm) 5.09 5.09 5.09 5.09 Area of Specimen (cm<sup>2</sup>) 81.479 81.479 81.479 81,479 Init. Spec. height (in) 0.9955 N/A 1.0000 N/A 1.0020 N/A 1.0020 N/A Height change (final)(in) 0.0381 0.0598 N/A N/A N/A 0.0800 N/A 0.0189 Adjusted Spec.height(in) 0.9574 1.00 1.00 0.9402 1.00 0.9220 1.00 0.9831 (cm) 2.529 2.432 2.540 2.388 2.545 2.342 2.545 2.497 Specimen Volume (cm<sup>3</sup>) 206.026 206.957 207.371 207.371 **Moist Density (pcf)** 85.65 114.04 102.04 101.26 **MOISTURE CONTENT** Wt. moist soil+tare(gr) 375.45 375.45 475.25 475.25 431.23 431.23 416.46 416.46 Wt. dry soil+tare(gr) 315.22 315.22 435.34 382.96 367.22 435.34 382.96 367.22 Wt. of tare(gr) 92.79 92.79 97.22 97.22 92.28 92.28 80.11 80.11 Wt. dry soil (gr) 222.43 222.43 338.12 338.12 290.68 290.68 287.11 287.11 Wt. of water (gr) 60.23 60.23 39.91 39.91 48.27 48.27 49.24 49.24 M/C (%) 27.08 27.08 11.80 11.80 16.61 16.61 17.15 17.15 DRY DENSITY (pcf) 67.4 102.0 87.5 86.4 48.7 48.8 48.4 % Saturation\* (48%-52%) 48.7 2.7 \*Assumes Gs = 2.7 2.7 2.7 **EXPANSION INDEX =** 38 60 80 19 **Potential Expansion** Medium Medium Low Very Low (per ASTM 4829-08) Project Name: Project No.: 17-1025 Run by: Lab: KOURY **Borrow Site 5** Date: 04-15-2019 QA:

# EXPANSION INDEX TESTS DENSITY AND MOISTURE CONTENT DATA - EI TEST

Location/ Elevation	TP 10 @	4.5-5.5'	TP 3 @	4.8-5.2'	TP 4 @	5-5.5	TP 5 @	0 1-1.5'		
USCS Symbol						2			1	
Normal Load (psf)		***************************************	<u> </u>				- I			
SAMPLE CONDITION	Initial	Final	Initial	Final	Initial	Final	Initial	Final	1	
Wt Specimen & Ring (gr)	688.900		714.510		665.470		744.140			
Wt. of ring (gr)	366.61		366.48		366.64		364.14			
Wt. Specimen (gr)	322.290		348.030		298.830		380.000			
Specimen diameter (in)	4.010		4.010		4.010		4.010			
Specimen radius (cm)	5.09		5.09		5.09		5.09			
Area of Specimen (cm²)	81.479		81.479		81.479		81.479			
Init. Spec. height (in)	1.0020	N/A	1.0000	N/A	1.0000	N/A	1.0030	N/A		
Height change (final)(in)	N/A	0.0659	N/A	0.1744	N/A	0.0339	N/A	0.0396		
Adjusted Spec.height(in)	1.00	0.9361	1.00	0.8256	1.00	0.9661	1.00	0.9634		
" " (cm)	2.545	2.378	2.540	2.097	2.540	2.454	2.548	2.447		
Specimen Volume (cm³)	207.371		206.957		206.957		207.578	***************************************		
Moist Density (pcf)	97.03		104.99		90.14		114.29			
MOISTURE CONTENT										
Wt. moist soil+tare(gr)	408.59	408.59	440.82	440.82	382.28	382.28	472.30	472.30		
Wt. dry soil+tare(gr)	355.77	355.77	390.75	390.75	325.40	325.40	429.76	429.76		
Wt. of tare(gr)	86.30	86.30	92.79	92.79	83.45	83.45	92.30	92.30		
Wt. dry soil (gr)	269.47	269.47	297.96	297.96	241.95	241.95	337.46	337.46	•	
Wt. of water (gr)	52.82	52.82	50.07	50.07	56.88	56.88	42.54	42.54		
M/C (%)	19.60	19.60	16.80	16.80	23.51	23.51	12.61	12.61		
DRY DENSITY (pcf)	81.1		89.9		73.0		101.5		<del>-</del>	
% Saturation* (48%-52%)	49.1		51.8		48.5		51.5			
*Assumes Gs =	2.7		2.7		2.7		2.7			
EXPANSION INDEX =	66		174		34		39			
Potential Expansion (per ASTM 4829-08)	Medium		Very High		Low		Low			
KOURY		1	Project Name:				Project No.:	17-1025	Run by:	La

KOURY

|Project Name

Project No.: 17

tun by:

Lab:

**Borrow Site 5** 

Date: 04-15-2019

QA:

We are a key member of the construction team while safeguarding the public. We improve operational logistics and provide superior quality control through the continuing development of our engineering staff and technical expertise, utilization of classroom training and field supervisors, thus defining the industry standard.

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