Appendix E

Well Feasibility Study

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- E-2 Strauss Well CW-2
- E-3 Construction Water Supply Aquifer Letter September 2019
- E-4 Construction Water Supply Aquifer Letter October 2019

Appendix E-1

Well Feasibility Study

Cleath-Harris Geologists, Inc.

71 Zaca Lane, Suite 140 San Luis Obispo, CA 93401 (805) 543-1413



November 30, 2017

Mr. Joshua Franklin Strauss Wind, LLC 5901 Priestly Drive, Suite 300 Carlsbad, CA 92008

SUBJECT: Assessment of Groundwater Well Feasibility and Siting for Strauss Wind Project Operations and Maintenance Facility, San Miguelito Road, Lompoc, Santa Barbara County.

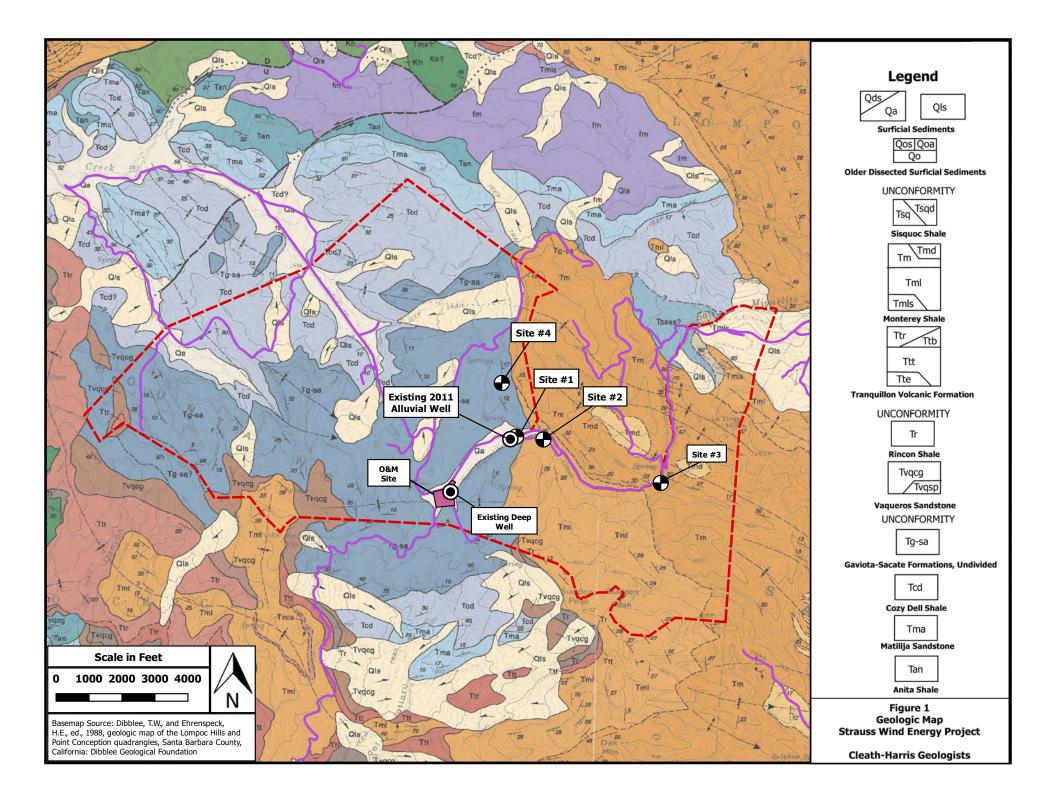
Dear Mr. Franklin:

As requested, Cleath-Harris Geologists (CHG) has completed a review of available hydrogeologic information and performed field reconnaissance in order to assess the feasibility of drilling a water well to supply the proposed Operations and Maintenance (O&M) building for the Strauss Wind Project. Field reconnaissance was performed on November 27, 2017. This letter summarizes the information obtained to date and the results of the assessment.

Site Geology

The project site is underlain primarily by undivided, early Tertiary-age Gaviota-Sacate Formations, which are described as a tan, semi-friable, thick-bedded marine sandstone, locally interbedded with gray micaceous siltstone and claystone. There is also Monterey shale mapped on the east side of the project area, and Cosy Dell shale mapped on the north side of the project area. A few outcrops of Vaqueros sandstone are shown on the geology map along the southern project boundary. Among the formations locally present, the Vaqueros sandstone and siliceous member of the Monterey shale are viable targets for groundwater development, while the Cosy Dell shale is a poor target due to water quality issues and low productivity. The Gaviota-Sacate Formations are gradational and contemporaneous with the Coldwater sandstone, portions of which are a viable target for groundwater development in other areas. Alluvial deposits are also present locally, and can provide a source of water to wells if saturated and sufficiently thick. Project site geology is shown on Figure 1.

The O&M site is covered by a thin veneer of seasonally saturated alluvial deposits underlain by the Gaviota-Sacate Formation. There is a syncline mapped through the O&M building envelope, where the Gaviota-Sacate Formation is inferred from local structure to reach a maximum thickness of 800 feet.





Available Information

There are two points of information on water wells in the area. A Well Completion Report from 2011 is available for a shallow alluvial well along the drainage channel parallel to San Miguelito Road, and results of a well test with water quality information are described in the EIR for the former Lompoc Wind Energy Project (Aspen Environmental Group, 2008). Some additional information on springs, water levels, and water quality was obtained during site reconnaissance.

Alluvial Well

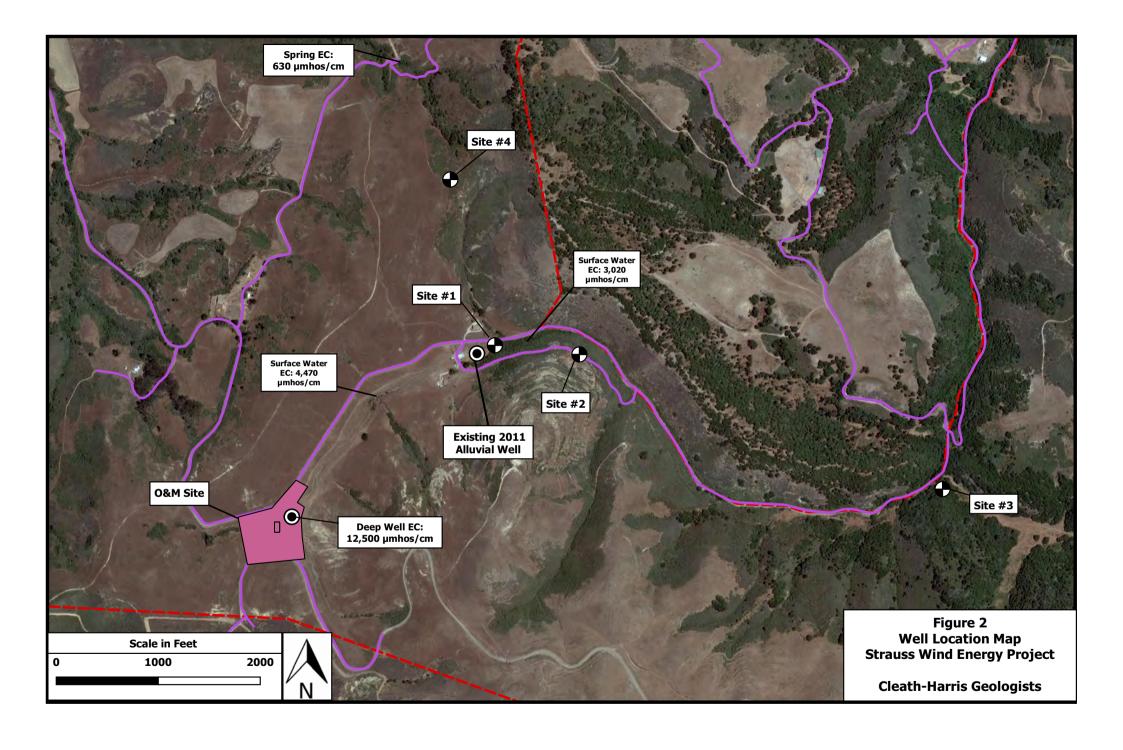
The alluvial well is located in a broad drainage swale approximately 2,500 feet northeast of the San Miguelito Road and Sudden Road intersection (Figure 2). This shallow well taps sand and gravel to a depth of 34 feet, with clay through the total well depth of 50 feet (Well Completion Report attached). Alluvium is also mapped at the O&M site, but geotechnical borings show it to be too shallow for development purposes at that location (less than 20 feet thick). Field reconnaissance indicates the 2011 alluvial well is currently equipped with a pump to serve the local ranch.

Surface water in the alluvial drainage channel was noted at two locations. The first location was approximately 1,000 feet upstream of the alluvial well, and the second location was at the beginning of the bedrock narrows approximately 500 feet downstream of the well. Electrical Conductivity (EC) of the surface water measured 4,470 micromhos per centimeter (μ mhos/cm) at the upstream location and 3,020 μ mhos/cm at the downstream location (Figure 2).

O&M Site Deep Well

Water quality and pumping test information is available for a 475-foot deep, unused well on the Signorelli Ranch. The information, from December 2005 and January 2006, indicates that water quality from the Signorelli Ranch deep well has an elevated salinity of approximately 10 times greater than drinking water standards. CHG located the well during site reconnaissance at the proposed O&M site (Figure 2; Image attached). The static water level was measured at 123.9 feet depth, compared to 125 feet depth reported on December 27, 2005. A grab sample of groundwater in the deep well was also bailed and tested during site reconnaissance. The EC of the water sample measured 12,500 μ mhos/cm, compared to 16,000 μ mhos/cm reported in 2006. The drinking water standard is 1,600 μ mhos/cm.

Data from two pumping tests are available, the first conducted on December 27, 2005, and the second on January 11, 2006 (attached). The pumping tests showed the well does not meet minimum County standards for domestic supply and may not be able to provide





the nominal 250 gallons per day supply needed for the O&M facility. These pumping tests show excessive drawdown at low production rates.

During the first test in December 2005, the well produced approximately 450 gallons in 60 minutes, with a water level decline of 187 feet. Virtually all of the water pumped was from casing storage (i.e. minimal inflow to the well from the aquifer), based on a nominal 8-inch steel casing size as observed at the wellhead. During the second test, the well produced approximately 940 gallons of water in four hours, with a water level decline of 196 feet. An estimated 510 gallons was from casing storage. The static water level at the beginning of the second test was 57 feet deeper than the static measured two weeks earlier, however, indicating poor recovery from the initial testing. Treatment for potable use from the well would require reverse osmosis, which would further diminish the well's effective yield.

Well Site Feasibility Assessment

A detail of the project site and potential well sites are shown on Figure 2. A nominal 250 gallons per day (based on 4-6 staff with 50 gallons per day per person water use) would be adequate for the O&M facility, although a minimum flow of 3 gallons per minute for 72 hours (4,320 gallons per day) would be needed from a pumping test to meet County standards for domestic supply (Santa Barbara County Code Chapter 34B-18).

Feasible Options

Site #1 A well at this location would tap the alluvial deposits at the lowest possible elevation prior to the bedrock narrows, approximately 2,700 feet to the northeast of the O&M site. The existing alluvial well met the minimum yield test for a domestic well per County standards (3 gpm for 72 hours), and similar production from a new well would be expected. Water quality may require treatment for potable use, based on the EC measurements of surface water in the alluvial drainage. There is an estimated 40 acrefeet of available groundwater stored in the alluvial aquifer, which provides drought period reliability and should be adequate for both local ranch and O&M facility needs. A new alluvial well would be approximately 150 feet from the existing well, and would need a variance from the County to install a 20-foot sanitary seal instead of the 50-foot seal required by County Code. There is power at the ranch. Water from Site #1 could be piped along the County right-of-way or through an easement on the ranch. There is a 70-foot gain in elevation between ground surface at Site #1 and the O&M site.

Site #2 A second location for groundwater development would be to tap the semisiliceous portion of the lower Monterey shale. There is a good probability of obtaining adequate water to serve the O&M facility, and water quality from the shale is expected to be generally suitable for potable use, although treatment may be required. Site #2 is



approximately 4,000 feet northeast of the O&M facility, on an elevated bench at the former Union Sugar limestone quarry. Existing power lines at the ranch are approximately 1,200 feet from the proposed well site. Pumped water would need to be piped along an easement, either within the County right-of-way or across the ranch. Depth to water in a well at Site #2 location would likely be less than 200 feet. Production capacity from a well at this location could be up to 20 gallons per minute. There is a 20-foot gain in elevation between ground surface at Site #2 and the O&M site.

Site #3 The most favorable location, based on hydrogeology, is within the siliceous Monterey shale. There is a high probability of obtaining adequate water to serve the O&M facility, and water quality from the siliceous shale is expected to be generally suitable for potable use. The preferred well location, however, is approximately 8,000 feet east of the O&M facility along San Miguelito Road, and would require water to be piped along an easement within the County right-of-way. There is also no power within a few thousand feet. Depth to water in a well at Site #3 would likely be less than 50 feet. Production capacity from a well at this location could be up to 20 gallons per minute. There is a 250-foot gain in elevation between ground surface at Site #3 and the O&M site.

Site #4 The upper Gaviota-Sacate sandstone does feed a few springs in the project area. One spring visited during site reconnaissance had been developed for stock water with an EC measuring 620 µmhos/cm. A second spring visited was not flowing but there was vegetative evidence of seeps. These springs emanate from an indurated and locally coarser grained sandstone bed that is above the alluvial valley floor. To tap the spring zone, a well would need to be drilled on the ridge above the valley floor at a distance of roughly 4,000 feet from the O&M site. Production capacity would likely be low, and may require a variance from the County standards for flow, but water quality should be suitable for potable use. Depth to water would be close to 300 feet. The closest power lines are approximately 1,400 away. Water pumped from the well would need to be piped along an easement on ranch property. Site grading for rig access would be necessary. There is a 220-foot drop in elevation between ground surface at Site #4 and the O&M site.

Options Considered Infeasible

The source of water to the existing Signorelli Ranch deep well at the proposed O&M site is interpreted to be the lower Gaviota-Secate Formation. Very low production and poor water quality effectively eliminate the feasibility of using the well or developing a new well at the O&M site.

The Vaqueros Sandstone, typically a favorable target for groundwater development, is too high in elevation and mostly unsaturated on the property. Suitable access for a drilling rig is also significantly constrained, based on site reconnaissance.



Well Facilities

A water well for the O&M facilities would be constructed using 5-inch or 6-inch diameter PVC casing, include a sanitary annular seal, and could extend up to several hundred feet below grade, pending the results of test hole drilling. Wells typically include approximately 1-2 feet of casing stickup from the surface (cement) pad.

The well may either be fenced in an enclosure or covered with a small well house. Dimensions vary, but the well house footprint is typically close to 8 x 10 feet and preferably constructed of wood, while fenced enclosures may be the same size or larger and constructed of 6-foot tall chain link. Images of a typical well house and enclosure are attached.

A submersible pump would be placed down the well, where noise levels from pump operation would be negligible at ground surface. A 2,500-gallon or larger water storage tank and small booster pump may be incorporated into the design to provide fire suppression water and greater instantaneous discharge capacity for the O&M building, but would not result in noise nuisance issues.

Well Construction

Water supply well construction and testing should be performed by a C-57 licensed drilling contractor in accordance with Santa Barbara County Code Chapters 34A (Wells) and 34B (Domestic Water Systems). During construction, the drilling rig and support vehicles would require an approximate 60 x 100 foot work area. A drilling crew typically consists of two to three personnel, although during portions of the construction operation, a geologist and County inspector may also be present. The length of time a drilling contractor would be on-site to complete a domestic well for the O&M facility to a depth of several hundred feet, from rig mobilization through development and testing, would be close to 4 weeks.

If you have any questions, please feel free to contact our office.

Sincerely,

CLEATH-HARRIS GEOLOGISTS

Spencer Harris, HG 633 Senior Hydrogeologist

Attachments



ATTACHMENTS:

Well Completion Report for 2011 Alluvial Well
Signorelli Ranch Deep Well Information
Typical Well Enclosures

Strauss well assessment 11/30/2017

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Signorelli Ranch Deep Well at Proposed O&M Site



Looking East toward Sudden Road /San Miguelito Road Intersection



Alexander Bros., Inc.
water well drilling contractors
(1805) 558 568 LIC. NO. 602322

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Alexander Bros., Inc.

WATER WELL DRILLING CONTRACTORS
(808) 688-61000
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LIG. NO. 602322

200 LA SALLE CYN. RD. LOMPOC. CA 93436

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GRAND TERRACE, CA 92313

GENERAL MINERAL & PHYSICAL & INORGANIC ANALYSIS (9/99) Date of Report: 06/01/26 Sample ID No.M60206-1A

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Name of Sampler: R ALEXANDER

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Date Analyses Received # Lab:06/01/12/1015 Completed:06/01/25

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Cadmium (Cd) (ug/L) Chromium (Total Cr) (ug/L) L+ Copper (Cu) (ug/L) L+ Iron (Fe) (ug/L) L Lead (Pb) (ug/L) L+ Manganese (Mn) (ug/L) Mercury (Hg) (ug/L) Nickel (ug/L)	01012 01027 01034 01042 01045 01051 01055 71900	ND ND ND 7200 ND 100 ND	1.(1.(5(10) 5.(
Cadmium (Cd) (ug/L) Chromium (Total Cr) (ug/L) L+ Copper (Cu) (ug/L) L+ Iron (Fe) (ug/L) L Lead (Pb) (ug/L) L+ Manganese (Mn) (ug/L) Mercury (Hg) (ug/L) Nickel (ug/L)	51027 01034 01042 01045 61051 01055 71900	ND ND 7200 ND 100 ND	1.(5(10% 5.(2)
L+ Copper (Cu) (ug/L) L+ Iron (Fe) (ug/L) L Lead (Pb) (ug/L) L+ Manganese (Mn) (ug/L) L Mercury (Hg) (ug/L) L Nickel (ug/L)	01034 01042 01045 01051 01055 71900	ND 7200 ND 100 ND	100 100 5.0 20
L+ Copper (Cu) (ug/L) L+ Iron (Fe) (ug/L) L Lead (Pb) (ug/L) L+ Manganese (Mn) (ug/L) L Mercury (Hg) (ug/L) L Nickel (ug/L)	01042 01045 01051 01055 71900	7200 ND 100 ND	50 100 5.0 20
L+ Iron (Fe) (ug/L) L Lead (Pb) (ug/L) L+ Manganese (Mn) (ug/L) L Mercury (Hg) (ug/L) L Nickel (ug/L)	01045 01051 01055 71900	7200 ND 100 ND	100 5.0 20
Lead (Pb) (ug/L) L+ Manganese (Mn) (ug/L) Mercury (Hg) (ug/L) L Nickel (ug/L)	61051 01055 71900	ND 100 ND	5.0 20
L+ Manganese (Mn) (ug/L) Mercury (Hg) (ug/L) Nickel (ug/L)	01055 71900	LOO ND	20
Mercury (Hg) (ug/L) Nickel (ug/L)	71900	ND,	
Nickel (ug/L)			
	0_057 (מו	10
Selenium (Se) (ug/L)	01147	ND	5.0
+ Silver (Ag) (ug/L)	0.077	ND	20
Thallium (uc/L)	01059	ND	1.0
Zinc (Zn) (ug/L)	01092	NO	50
ADDITIONAL ANALYSES		·	5/24 = +3 -4 -4
	01020	43001	100
			400
Nitrice as Nitrogen(N) (uc/L)			400
Cyanide (ug/L)			100
Vanadium (ug/L)			3.¢
	ADDITIONAL ANALYSES Boron (ug/L) Nitrate + Nitrite as Nitrogen(N) (ug/L) Nitrite as Nitrogen(N) (ug/L) Cyanide (ug/L) Vanadium (ug/L)	ADDITIONAL ANALYSES Boron (ug/L) 01020 Nitrate + Nitrite as Nitrogen(N) (ug/L) A-029 Nitrite as Nitrogen(N) (ug/L) 03620 Cyanide (ug/L) 01291 Vanadium (ug/L) 01087	ADDITIONAL ANALYSES Boron (ug/L) 01020 4300 NItrate + Nitrite as Nitrogen(N) (ug/L) A-029 ND Nitrite as Nitrogen(N) (ug/L) 00620 ND Cyanide (ug/L) 01291 ND



Example of well pump house



Example of well enclosure

Appendix E-2

Strauss Well CW-2

Cleath-Harris Geologists, Inc.

71 Zaca Lane, Suite 140 San Luis Obispo, CA 93401 (805) 543-1413



March 6, 2019

Mr. Jörge Beland Strauss Wind, LLC 5901 Priestly Drive, Suite 300 Carlsbad, CA 92008

Subject: Pumping Test and Water Quality Results for Strauss Wind Energy

Project Well CW2, San Miguelito Road, Lompoc, Santa Barbara

County.

Dear Mr. Beland:

This letter summarizes the pumping test and water quality results for Well CW2, which will provide a domestic water source for the proposed Strauss Wind Energy project's operations and maintenance (O&M) facility. Well CW2 was constructed between January 29 and February 12, 2019, by Powell and Murphy Drilling of Paso Robles, California (Santa Barbara Well Permit #3208-4669). The well is located off San Miguelito Road approximately 6 miles south of Lompoc (APN 083-250-011).

Well Construction

Well CW2 is cased with 6-inch PVC to a depth of 209 feet, with 0.040-inch perforations from 129 to 209 feet depth. Construction included a 16-inch steel conductor cemented in a 23-inch borehole from surface to 38 feet depth, and a sanitary seal inside the conductor that extends to 50 feet depth. The filter pack is composed of 8x16 sand. The Well Completion Report is attached.

Pumping Test

A 12-hour constant discharge test was performed on February 15, 2019 at a rate of 60 gallons per minute (gpm). Pumping test data and graph are attached. The static water level prior to pumping was measured at 110.6 feet depth. Pumping water levels reached a maximum of 148.6 feet (38 feet of drawdown) at the conclusion of the 12-hour test. The static water level recovered to 120 feet depth within 60 minutes of pump shutdown, and a subsequent static water level of 107 feet depth was measured at 1:30 pm on February 19, indicating full recovery following the pumping test.

The long-term drawdown and reliability of Well CW2 for domestic use has been evaluated using the Jacob method of proportionality between groundwater discharge and water level drawdown. A nominal 250 gallons per day (based on 4-6 staff with 50 gallons per day per person water use) is considered adequate for domestic water use at the O&M facility. Based on the results of the 60 gpm pumping test, Well CW2 provides



a reliable, long-term source of water for the O&M facility. At 250 gallons per day average production from the well (less than 0.2 gpm continuous flow), long-term static water level drawdown is estimated to be less than a foot.

Well CW2 produced approximately 43,000 gallons of water over the 12-hour pumping test, which is enough water to serve the O&M facility for more than 5 months. The static water level in Well CW2 was fully recovered within a few days of the test; Well CW2 has ample capacity to meet the domestic water needs of the O&M facility.

Water Quality

Groundwater samples from Well CW2 were collected, preserved, and transported by an approved sampler and delivered to a State-certified analytical laboratory on February 14, 2019. Water quality testing was performed for constituents listed in Title 22 CCR Tables 64431-A, 64449-A, and 64449-B in accordance with Santa Barbara County Code (Chapter 34B) for domestic water systems.

Water quality results are attached. All constituents tested met drinking water standards except total iron, which was detected at 630 micrograms per liter (the Secondary Maximum Contaminant Level for iron in drinking water is 300 micrograms per liter). Elevated iron concentrations are not unusual for groundwater sources and iron-removal treatment options are available, such as ion exchange or oxidation/filtration. Well CW2 water is suitable for domestic use with treatment for iron removal.

No. HG 633

Signed,

CLEATH-HARRIS GEOLOGISTS

Spencer J. Harris, HG 633 Senior Hydrogeologist

DATE: March 6, 2019

attachments



ATTACHMENTS

Well Completion Report Pumping Test Report Water Quality Report

Strauss Well CW2 results 3/6/2019

State of California

Well Completion Report Form DWR 188 Submitted 2/19/2019 WCR2019-002457

Owner's Well	l Numb	er				Date Work	k Began	01/2	9/2019		ĺ	Date Wo	rk Ended	02/12/2	2019
Local Permit	Agency	/ Santa Barbai	a Count	y Enviror	mental H	ealth Servi	ices								
Secondary Pe	ermit A	gency				Permit	Numbe	r 3802	2-4669			Pe	rmit Date	01/18/2	2019
Well Ow	ner (must remair	conf	identia	al purs	uant to	Wate	er Cod	e 1375	2)		Plann	ed Use	and A	ctivity
		LLI FAMILY TRU	ST,								Activity	New	Well		
Mailing Addr	ress	P.O. Box 173									Planne	d Use	Water S	upply Do	mestic
City Lompa	ac					State	CA	Zip _	93438	_					
						Wel	II Loc	ation							
Address (0 San I	Miguelito RD								API	V 083	3-250-01	1		
City Lom				Zip 9	3438	County	/ San	ta Barbaı	ra	Tow	vnship	06 N			
Latitude	34	34 30.			ngitude	- -120	29	34.2	599 W	Ran	<u> </u>	1 W			
	Deg.	Min. S	ec.		-	Deg.	Min.	Se	c.	Sec	tion <u> </u>	30	San Berna	rdino	
Dec. Lat. 3	34.5750	117		De	ec. Long.	-120.492	285				und Surfa	_		11.6	
Vertical Datu	um			—— Horizo	ntal Datu	m WGS	84				vation Ac				
Location Acc	curacy		Loc	- cation De	etermination	on Method						•	on Method	I GPS	
		Borehole	Inform	mation					Water	Lev	el and	Yield	of Con	pleted	d Well
Orientation	Vertic	======================================			Spec	ify		Depth t	o first wat	er	1:	20	(Feet b	elow surf	ace)
Drilling Meth	nod D	rirect Rotary	Dri	Iling Fluid	– d Bentor	nite	— II		o Static	_			_		
<u> </u>	_							Water L	_			(Feet)	Date Me		02/15/2019
Total Depth	of Borir	ng 210			Feet			Estimat Test Le	ted Yield*			(GPM) (Hours)	Test Typ Total Dra		Pump 38 (feet)
Total Depth	of Com	pleted Well 209)		Feet				_	esent		,			(leet)
	*May not be representative of a well's long term yield. Geologic Log - Free Form														
Depth from							3								
Surface Feet to Fe	-							Descri	ption						
0	3	Sandy Top Soil													
3	26	Light Brown Shal	е												
26	56	Fractured Dark B	own Sha	ale with L	ight Laye	rs									
56	108	Firm Dark Brown	Shale												
108	118	Dark Brown Shal	e Hard L	aver											

118

210

Fractured Dark Brown / Black Shale

	Casings									
Casing #		m Surface o Feet	Casing Type	Material	Casings Specificatons	Wall Thickness (inches)	Outside Diameter (inches)	Screen Type	Slot Size if any (inches)	Description
1	0	129	Blank	PVC	OD: 6.625 in. SDR: 21 Thickness: 0.316 in.	0.316	6.625			
1	129	209	Screen	PVC	OD: 6.625 in. SDR: 21 Thickness: 0.316 in.	0.316	6.625	Milled Slots	0.04	

	Annular Material											
Depth from Surface Feet to Feet		Fill	Fill Type Details	Filter Pack Size	Description							
0	52	Cement	Other Cement		6 Sack Sand Slurry							
52	209	Filter Pack	8 x 16									

Other Observations:

Surface Conductor installed from surface to 38 Ft.

	Borehole Specifications								
Depth Surf Feet to	ace	Borehole Diameter (inches)							
0	38	23							
38	52	12							
52	210	10							

Certification Statement									
I, the under	I, the undersigned, certify that this report is complete and accurate to the best of my knowledge and belief								
Name	Name POWELL & MURPHY DRILLING INC								
	Person, Firm or Corporation	Person, Firm or Corporation							
	4710 PRAIRIE RD	PASO ROBLES	CA	93446					
	Address	City	State	Zip					
Signed	electronic signature received			99944					
l	C-57 Licensed Water Well Contractor Date Signed C-57 License Number								

DWR Use Only										
CSG#	State Well Number			Site Code			Local Well Number			
	_			- r		_				
	1 1	1	N							w
La	titude De	g/Min/Sec			Longitu	de	Deg	/Min	/Se	
TRS:										
APN:										
TRS:	 titude De(g/Min/Sec	N	J (Longitu	l de	Deg	 /Min	/Sed	

Powell & Murphy Drilling 4710 Prairie Road Paso Robles, CA 93446 805-369-2568 Lic # - 999944



Test Pump Report

Customer Information Date: 2/15/2019

Name: Strauss Wind LLC Address: San Miguelito Rd

City: Lompoc State: CA Zip Code: 93438

Phone Number: Email Address:

Well Information

Well Location: 34 34.5010 N 120 29.5710 W: 6 miles south of Lompoc on San Miguelito Rd, 700 Ft East of

Gate

Well Casing Size:6 InchPumping Depth:180 FeetWell Depth:209 FeetPump Size:5 HPTest Started:0600 HrsStatic Level:110.6 Feet

Test Ended: 1800 Hrs

Hours Pumped: 12 Hrs Flow Rate: 60 GPM

Test Information:

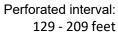
Time	Water Level	Flow Rate	Comments
	In Feet	In GPM	
0600	110.6	60	Static
0601	120.4	60	Clear with no odor
0602	130.65	60	Clear with no odor
0603	132.5	60	Clear with no odor
0604	133.4	60	Clear with no odor
0605	133.8	60	Clear with no odor
0606	134.15	60	Clear with no odor
0608	134.3	60	Clear with no odor
0610	134.55	60	Clear with no odor
0612	134.75	60	Clear with no odor
0615	134.95	60	Clear with no odor
0620	135.05	60	Clear with no odor
0625	135.4	60	Clear with no odor
0630	135.65	60	Clear with no odor
0640	136.25	60	Clear with no odor
0650	136.8	60	Clear with no odor
0700	136.95	60	Clear with no odor
0715	137.5	60	Clear with no odor
0730	137.8	60	Clear with no odor
0745	138.25	60	Clear with no odor
0800	138.6	60	Clear with no odor
0830	139.2	60	Clear with no odor

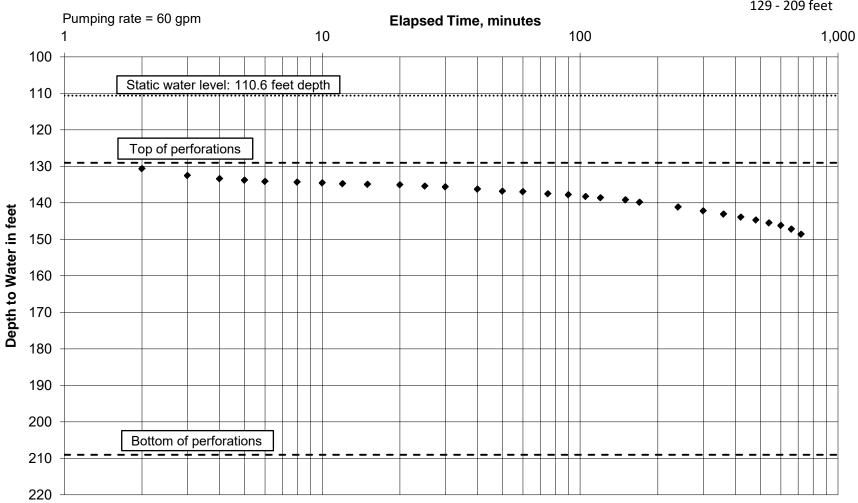
0900	139.85	60	Clear with no odor
1000	141.15	60	Clear with no odor
1100	142.2	60	Clear with no odor
1200	143.1	60	Clear with no odor
1300	143.9	60	Clear with no odor
1400	144.7	60	Clear with no odor
1500	145.5	60	Clear with no odor
1600	146.2	56	Adjust flow to 60 GPM with Stopwatch, Clear with no odor
1700	147.2	58	Adjust flow to 60 GPM with Stopwatch, Clear with no odor
1800	148.6	60	Clear with no odor

Recovery Information

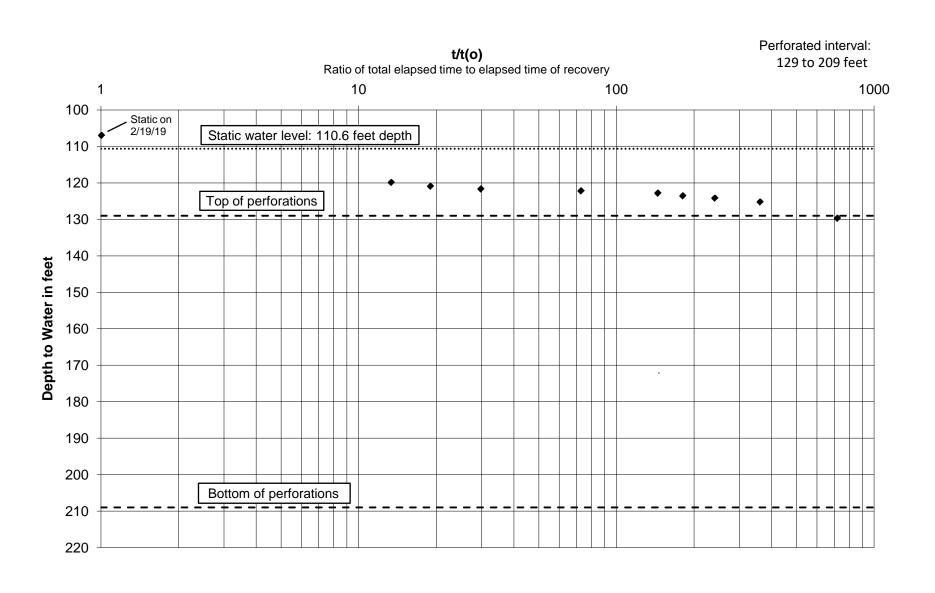
Time	Water Level	Flow Rate	Comments
	In Feet	In GPM	
1801	129.7	n/a	
1802	125.2	n/a	
1803	124.15	n/a	
1804	123.55	n/a	
1805	122.8	n/a	
1810	122.2	n/a	
1815	121.65	n/a	
1830	120.9	n/a	
1900	119.85	n/a	

Pumping Test (12-hour) - Well CW2 Strauss Wind Energy February 15, 2019





Recovery Test - Well CW2 Strauss Wind Energy February 15, 2019



February 22, 2019

Lab ID : CC 1980547 **Cleath-Harris Geologists**

Attn: Spencer Harris Customer : 8-514

71 Zaca Lane Suite 140 San Luis Obispo, CA 93401

Laboratory Report

Introduction: This report package contains total of 14 pages divided into 3 sections:

Case Narrative (3 pages): An overview of the work performed at FGL.

Sample Results (4 pages): Results for each sample submitted.

Quality Control (7 pages): Supporting Quality Control (QC) results.

Case Narrative

This Case Narrative pertains to the following samples:

Sample Description	Date Sampled	Date Received	FGL Lab ID#	Matrix
Travel Blank	02/14/2019	02/14/2019	CC 1980547-000	LBW
Strauss CW2	02/14/2019	02/14/2019	CC 1980547-001	DW

Sampling and Receipt Information: All samples were received in acceptable condition and within temperature requirements, unless noted on the Condition Upon Receipt (CUR) form. All samples arrived on ice. All samples were prepared and analyzed within the method specified hold time. All samples were checked for pH if acid or base preservation is required (except for VOAs). For details of sample receipt information, please see the attached Chain of Custody and Condition Upon Receipt Form.

Quality Control: All samples were prepared and analyzed according to the following tables:

Inorganic - Metals QC

200.7	02/16/2019:202307 All analysis quality controls are within established criteria.
	02/18/2019:202413 All analysis quality controls are within established criteria.
	02/16/2019:201763 All preparation quality controls are within established criteria.
200.8	02/18/2019:202419 All analysis quality controls are within established criteria, except: The following note applies to Antimony: 360 CCV above Acceptance Range (AR). Samples which were non detect for this analyte were accepted.
	02/18/2019:201817 All preparation quality controls are within established criteria.
245.1	02/19/2019:202463 All analysis quality controls are within established criteria.
	02/19/2019:201874 All preparation quality controls are within established criteria.

February 22, 2019 **Cleath-Harris Geologists**

Lab ID : CC 1980547 Customer : 8-514

Organic QC

524.2	02/15/2019:202311 All analysis quality controls are within established criteria.
	02/15/2019:201778 All preparation quality controls are within established criteria.

Inorganic - Wet Chemistry QC

2120B	02/15/2019:202351 All analysis quality controls are within established criteria.
	02/15/2019:201821 All preparation quality controls are within established criteria.
2130B	02/15/2019:202344 All analysis quality controls are within established criteria.
	02/15/2019:201812 All preparation quality controls are within established criteria.
2150B	02/15/2019:201822 All preparation quality controls are within established criteria.
2320B	02/20/2019:202491 All analysis quality controls are within established criteria.
2510B	02/18/2019:202312 All analysis quality controls are within established criteria.
	02/18/2019:201780 All preparation quality controls are within established criteria.
2540CE	02/18/2019:201793 All preparation quality controls are within established criteria.
300.0	02/15/2019:202556 All analysis quality controls are within established criteria.
	02/15/2019:201962 All preparation quality controls are within established criteria.
314.0	02/15/2019:202511 All analysis quality controls are within established criteria.
	02/15/2019:201724 All preparation quality controls are within established criteria.
4500CNCE	02/20/2019:202524 All analysis quality controls are within established criteria.
	02/20/2019:201928 All preparation quality controls are within established criteria.
5540C	02/15/2019:202349 All analysis quality controls are within established criteria.
	02/15/2019:201820 All preparation quality controls are within established criteria.

February 22, 2019 Lab ID : CC 1980547

Cleath-Harris Geologists Customer : 8-514

Certification:: I certify that this data package is in compliance with ELAP standards, both technically and for completeness, except for any conditions listed above. Release of the data contained in this data package is authorized by the Laboratory Director or his designee, as verified by the following electronic signature.

KD:DMB

Approved By Kelly A. Dunnahoo, B.S.



Analytical Chemists

February 22, 2019 Lab ID : CC 1980547-000

Customer ID: 8-514

Cleath-Harris Geologists

Attn: Spencer Harris Sampled On : February 14, 2019-13:15

71 Zaca Lane Sampled By : Andrea Berge

Suite 140 Received On : February 14, 2019-15:14

San Luis Obispo, CA 93401 Matrix : Lab. Blank Water

: Travel Blank Description

Project : Strauss Wind Energy

Sample Result - Organic

Constituent	Result	PQL	Units	Note	Sample Preparation		Sample Analysis	
Constituent	Result	1 QL	Omts	14010	Method	Date/ID	Method	Date/ID
EPA 524.2								
4-Bromofluorobenzene [‡]	101	70-130	%		524.2	02/15/19:201778	524.2	02/15/19:202311
1,2-Dichlorobenzene-d4 [‡]	98.6	70-130	%		524.2	02/15/19:201778	524.2	02/15/19:202311
Methyl tert-Butyl Ether (MTBE)	ND	1	ug/L		524.2	02/15/19:201778	524.2	02/15/19:202311

ND=Non-Detected. PQL=Practical Quantitation Limit. ‡Surrogate. * PQL adjusted for dilution.



February 22, 2019 Lab ID : CC 1980547-001

Customer ID: 8-514

Cleath-Harris Geologists

Attn: Spencer Harris Sampled On : February 14, 2019-13:15

71 Zaca Lane Sampled By : Andrea Berge

Suite 140 Received On : February 14, 2019-15:14

San Luis Obispo, CA 93401 : Drinking Water Matrix : Strauss CW2 Description

Project : Strauss Wind Energy

Sample Result - Inorganic

Constituent	Result	PQL	Units	MCL/AL	Sample	Preparation	Sample Analysis		
Constituent	Resuit	PQL	Ullits	MCL/AL	Method	Date/ID	Method	Date/ID	
General Mineral									
Total Hardness as CaCO3	439		mg/L		200.7	02/16/19:201763	200.7	02/16/19:202307	
Calcium	92	1	mg/L		200.7	02/16/19:201763	200.7	02/16/19:202307	
Magnesium	51	1	mg/L		200.7	02/16/19:201763	200.7	02/18/19:202413	
Potassium	2	1	mg/L		200.7	02/16/19:201763	200.7	02/16/19:202307	
Sodium	30	1	mg/L		200.7	02/16/19:201763	200.7	02/16/19:202307	
Total Cations	10.1		meq/L		200.7	02/16/19:201763	200.7	02/16/19:202307	
Boron	ND	0.1	mg/L		200.7	02/16/19:201763	200.7	02/16/19:202307	
Copper	ND	10	ug/L	1000^{2}	200.7	02/16/19:201763	200.7	02/16/19:202307	
Iron	630	30	ug/L	300^{2}	200.7	02/16/19:201763	200.7	02/16/19:202307	
Manganese	20	10	ug/L	50^{2}	200.7	02/16/19:201763	200.7	02/16/19:202307	
Zinc	ND	20	ug/L		200.7	02/16/19:201763	200.7	02/16/19:202307	
SAR	0.6				200.7	02/16/19:201763	200.7	02/16/19:202307	
Total Alkalinity (as	220	10	/T		22200	02/10/10 201072	22200	02/20/10 202401	
CaCO3)	320	10	mg/L		2320B	02/19/19:201873	2320B	02/20/19:202491	
Hydroxide as OH	ND	10	mg/L		2320B	02/19/19:201873	2320B	02/20/19:202491	
Carbonate as CO3	ND	10	mg/L		2320B	02/19/19:201873	2320B	02/20/19:202491	
Bicarbonate as HCO3	390	10	mg/L		2320B	02/19/19:201873	2320B	02/20/19:202491	
Sulfate	105	0.5	mg/L	500^{2}	300.0	02/15/19:201962	300.0	02/15/19:202556	
Chloride	53	1	mg/L	500^{2}	300.0	02/15/19:201962	300.0	02/15/19:202556	
Nitrate as NO3	ND	0.4	mg/L	45	300.0	02/15/19:201962	300.0	02/15/19:202556	
Nitrite as N	ND	0.2	mg/L	1	300.0	02/15/19:201962	300.0	02/15/19:202556	
Nitrate + Nitrite as N	ND	0.1	mg/L	10	300.0	02/15/19:201962	300.0	02/15/19:202556	
Fluoride	0.2	0.1	mg/L	2	300.0	02/15/19:201962	300.0	02/15/19:202556	
Total Anions	10.1		meq/L		2320B	02/19/19:201873	2320B	02/20/19:202491	
pH (Field)	7.4		units		4500-H B	02/14/19:201884	4500HB	02/14/19:202457	
Specific Conductance	953	1	umhos/cm	1600^{2}	2510B	02/18/19:201780	2510B	02/18/19:202312	
Total Dissolved Solids	550	20	mg/L	1000^{2}	2540CE	02/18/19:201793	2540C	02/19/19:202429	
MBAS Screen	Negative	0.1	mg/L	0.5^{2}	5540C	02/15/19:201820	5540C	02/15/19:202349	
Aggressiveness Index	12.3				4500-H B	02/14/19:201884	4500HB	02/14/19:202457	
Langelier Index (20°C)	0.4				4500-H B	02/14/19:201884	4500HB	02/14/19:202457	
Nitrate Nitrogen	ND	0.1	mg/L	10	300.0	02/15/19:201962	300.0	02/15/19:202556	
Metals, Total									
Aluminum	50	10	ug/L	1000	200.8	02/18/19:201817	200.8	02/18/19:202419	
Antimony	ND	1	ug/L	6	200.8	02/18/19:201817	200.8	02/18/19:202419	
Arsenic	1	1	ug/L	10	200.8	02/18/19:201817	200.8	02/18/19:202419	
Barium	101	0.2	ug/L	1000	200.8	02/18/19:201817	200.8	02/18/19:202419	

February 22, 2019 Lab ID : CC 1980547-001

Description: Strauss CW2 Customer ID: 8-514

Sample Result - Inorganic

Constituent	Result	PQL	Units	MCL/AL	Sample	Preparation	Sample Analysis	
Constituent	Result	rQL	Onits	WICL/AL	Method	Date/ID	Method	Date/ID
Metals, Total								
Beryllium	ND	1	ug/L	4	200.8	02/18/19:201817	200.8	02/18/19:202419
Cadmium	0.5	0.2	ug/L	5	200.8	02/18/19:201817	200.8	02/18/19:202419
Chromium	2	1	ug/L	50	200.8	02/18/19:201817	200.8	02/18/19:202419
Lead	1.4	0.5	ug/L	15	200.8	02/18/19:201817	200.8	02/18/19:202419
Mercury	ND	0.02	ug/L	2	245.1	02/19/19:201874	245.1	02/19/19:202463
Nickel	18	1	ug/L	100	200.8	02/18/19:201817	200.8	02/18/19:202419
Selenium	7	1	ug/L	50	200.8	02/18/19:201817	200.8	02/18/19:202419
Silver	ND	1	ug/L	100^{2}	200.8	02/18/19:201817	200.8	02/18/19:202419
Thallium	ND	0.2	ug/L	2	200.8	02/18/19:201817	200.8	02/18/19:202419
Vanadium	4	2	ug/L		200.8	02/18/19:201817	200.8	02/18/19:202419
Wet Chemistry								
Color	ND	5	units	15^{2}	2120B	02/15/19:201821	2120B	02/15/19:202351
Cyanide, Total	ND	0.004	mg/L	0.15	4500CNCE	02/20/19:201928	4500CNCE	02/20/19:202524
Odor	ND	1	TON	3^{2}	2150B	02/15/19:201822	2150B	02/15/19:202353
Turbidity	3.0	0.1	NTU	5	2130B	02/15/19:201812	2130B	02/15/19:202344
Perchlorate	ND	2	ug/L	6	314.0	02/15/19:201724	314.0	02/15/19:202511

ND=Non-Detected. PQL=Practical Quantitation Limit. * PQL adjusted for dilution.

MCL = Maximum Contamination Level. 2 - Secondary Standard. 3 - CDPH Notification Level. AL = Regulatory Action Level.



February 22, 2019 Lab ID : CC 1980547-001

Customer ID: 8-514

Cleath-Harris Geologists

Attn: Spencer Harris Sampled On : February 14, 2019-13:15

71 Zaca Lane Sampled By : Andrea Berge

Suite 140 Received On : February 14, 2019-15:14

San Luis Obispo, CA 93401 : Drinking Water Matrix

: Strauss CW2 Description

Project : Strauss Wind Energy

Sample Result - Organic

Constituent	Result	PQL	Units	MCL/AL	Sample Preparation		Sample Analysis	
Constituent					Method	Date/ID	Method	Date/ID
EPA 524.2								
4-Bromofluorobenzene [‡]	91.1	70-130	%		524.2	02/15/19:201778	524.2	02/15/19:202311
1,2-Dichlorobenzene-d4 [‡]	95.6	70-130	%		524.2	02/15/19:201778	524.2	02/15/19:202311
Methyl tert-Butyl Ether (MTBE)	ND	1	ug/L	13	524.2	02/15/19:201778	524.2	02/15/19:202311

ND=Non-Detected. PQL=Practical Quantitation Limit. ‡Surrogate. * PQL adjusted for dilution.

MCL = Maximum Contamination Level. 2 - Secondary Standard. 3 - CDPH Notification Level. AL = Regulatory Action Level.

February 22, 2019 Lab ID : CC 1980547 Customer : 8-514

Cleath-Harris Geologists

Quality Control - Organic

Constituent	Method	Date/ID	Туре	Units	Conc.	QC Data	DQO	Note
Organic								
1,2-Dichlorobenzene-d4	524.2	02/15/19:201778VRG	Blank	ug/L	10.00	91.4 %	70-130	
			MS	ug/L	10.00	108 %	70-130	
		(SP 1901992-001)	MSD	ug/L	10.00	117 %	70-130	
			MSRPD	ug/L	10.00	7.8%	≤20	
	524.2	02/15/19:202311VRG	CCV	ug/L	10.00	112 %	70-130	
4-Bromofluorobenzene	524.2	02/15/19:201778VRG	Blank	ug/L	10.00	86.1 %	70-130	
			MS	ug/L	10.00	117 %	70-130	
		(SP 1901992-001)	MSD	ug/L	10.00	113 %	70-130	
			MSRPD	ug/L	10.00	3.5%	≤30	
4-Bromofluorobenzene (BFB)	524.2	02/15/19:202311VRG	CCV	ug/L	10.00	116 %	70-130	
Methyl tert-Butyl Ether	524.2	02/15/19:202311VRG	CCV	ug/L	10.00	123 %	70-130	
Methyl tert-Butyl Ether (MTBE)	524.2	02/15/19:201778VRG	Blank	ug/L		ND	<1.0	
			MS	ug/L	10.00	134 %	11-168	
		(SP 1901992-001)	MSD	ug/L	10.00	147 %	11-168	
			MSRPD	ug/L	10.00	9.2%	≤29	

Definition

CCV : Continuing Calibration Verification - Analyzed to verify the instrument calibration is within criteria.

Blank : Method Blank - Prepared to verify that the preparation process is not contributing contamination to the samples.

: Matrix Spikes - A random sample is spiked with a known amount of analyte. The recoveries are an indication of how that sample MS

matrix affects analyte recovery.

: Matrix Spike Duplicate of MS/MSD pair - A random sample duplicate is spiked with a known amount of analyted. The recoveries MSD

are an indication of how that sample matrix affects analyte recovery.

: MS/MSD Relative Percent Difference (RPD) - The MS relative percent difference is an indication of precision for the preparation MSRPD

and analysis.

ND : Non-detect - Result was below the DQO listed for the analyte.

DQO : Data Quality Objective - This is the criteria against which the quality control data is compared.

Lab ID : CC 1980547

Customer : 8-514

Quality Control - Inorganic

Constituent	Method	Date/ID	Туре	Units	Conc.	QC Data	DQO	Note
Metals								
Boron	200.7		MS	mg/L	4.000	93.9 %	75-125	
		(STK1932317-001)	MSD	mg/L	4.000	93.0 %	75-125	
			MSRPD	mg/L	800.0	1.0%	≤20.0	
	200.7	02/16/19:202307AC	CCV	ppm	5.000	93.2 %	90-110	
			CCB	ppm		0.002	0.1	
			CCV	ppm	5.000	95.0 %	90-110	
			CCB	ppm	1.00	0.001	0.1	
Calcium	200.7	(CENTAL 0.00.17, 0.01)	MS	mg/L	12.00	94.5 %	75-125	
		(STK1932317-001)	MSD	mg/L	12.00	91.4 %	75-125	
	200.7	02/16/19:202307AC	MSRPD	mg/L	800.0	1.4%	≤20.0 90-110	
	200.7	02/16/19:20230/AC	CCV CCB	ppm ppm	25.00	97.8 % 0.003	1	
			CCV	ppm	25.00	98.6 %	90-110	
			CCB	ppm	23.00	0.001	1	
Copper	200.7		MS	ug/L	800.0	98.0 %	75-125	
Соррег	200.7	(STK1932317-001)	MSD	ug/L	800.0	96.6 %	75-125	
		(31111711111111111111111111111111111111	MSRPD	ug/L	800.0	1.5%	≤20.0	
	200.7	02/16/19:202307AC	CCV	ppm	1.000	96.9 %	90-110	
			CCB	ppm		-0.00008	0.01	
			CCV	ppm	1.000	97.0 %	90-110	
			CCB	ppm		0.0001	0.01	
Iron	200.7		MS	ug/L	4000	94.8 %	75-125	
		(STK1932317-001)	MSD	ug/L	4000	93.7 %	75-125	
			MSRPD	ug/L	800.0	1.2%	≤20.0	
	200.7	02/16/19:202307AC	CCV	ppm	5.000	93.7 %	90-110	
			CCB	ppm		0.0013	0.03	
			CCV	ppm	5.000	94.6 %	90-110	
	200.7		CCB	ppm	12.00	0.0024	0.03	
Magnesium	200.7	(CTV1022217 001)	MS	mg/L	12.00	114 %	75-125	
		(STK1932317-001)	MSD MSRPD	mg/L	12.00 800.0	115 % 0.3%	75-125	
	200.7	02/18/19:202413AC	CCV	mg/L	25.00	107 %	≤20.0 90-110	
	200.7	02/18/19:202413AC	CCB	ppm ppm	23.00	-0.03	1	
			CCV	ppm	25.00	106 %	90-110	
			CCB	ppm	23.00	-0.03	1	
Manganese	200.7		MS	ug/L	800.0	96.4 %	75-125	
	200.7	(STK1932317-001)	MSD	ug/L	800.0	94.9 %	75-125	
		(MSRPD	ug/L	800.0	1.6%	≤20.0	
	200.7	02/16/19:202307AC	CCV	ppm	1.000	95.5 %	90-110	
			CCB	ppm		-0.0002	0.01	
			CCV	ppm	1.000	96.1 %	90-110	
			CCB	ppm		-0.0002	0.01	
Potassium	200.7		MS	mg/L	12.00	103 %	75-125	
		(STK1932317-001)	MSD	mg/L	12.00	101 %	75-125	
			MSRPD	mg/L	800.0	1.0%	≤20.0	
	200.7	02/16/19:202307AC	CCV	ppm	25.00	104 %	90-110	
			CCB	ppm	25.00	0.09	1	
			CCV	ppm	25.00	104 %	90-110	
Sodium	200.7		CCB	ppm ma/I	12.00	0.06	75 125	
	200.7	(STK1932317-001)	MS MSD	mg/L	12.00 12.00	99.1 % 95.0 %	75-125 75-125	
		(31K1932317-001)	MSD MSRPD	mg/L mg/L	800.0	95.0 % 1.8%	/5-125 ≤20.0	
	200.7	02/16/19:202307AC	CCV		25.00	1.8%	90-110	
	200.7	02/10/17.20230/AC	CCB	ppm	25.00	0.02	1	
			CCV	ppm ppm	25.00	103 %	90-110	

Lab ID : CC 1980547 Customer : 8-514

Constituent	Method	Date/ID	Туре	Units	Conc.	QC Data	DQO	Note
Metals								
Sodium	200.7	02/16/19:202307AC	CCB	ppm		0.03	1	
Zinc	200.7		MS	ug/L	800.0	99.9 %	75-125	
		(STK1932317-001)	MSD	ug/L	800.0	101 %	75-125	
			MSRPD	ug/L	800.0	1.1%	≤20.0	
	200.7	02/16/19:202307AC	CCV	ppm	1.000	108 %	90-110	
			CCB	ppm		0.0018	0.02	
			CCV	ppm	1.000	100 %	90-110	
			CCB	ppm		0.0003	0.02	
Aluminum	200.8		MS	ug/L	5.000	100 %	75-125	
		(STK1932316-001)	MSD	ug/L	5.000	88.7 %	75-125	
	***		MSRPD	ug/L	5.000	0.58	≤10	
	200.8	02/18/19:202419AC	CCV	ppb	120.0	96.8 %	90-110	
			CCB	ppb	120.0	0.2	10	
			CCV	ppb	120.0	98.0 %	90-110	
A .:	200.0		CCB	ppb	5.000	0.2	10	
Antimony	200.8	(CTV1022216 001)	MS	ug/L	5.000	124 %	75-125	
		(STK1932316-001)	MSD MSRPD	ug/L	5.000 5.000	112 % 9.9%	75-125 ≤20	
	200.0	02/19/10-202410 A.C.		ug/L				260
	200.8	02/18/19:202419AC	CCV	ppb	120.0	111 %	90-110	360
			CCB CCV	ppb	120.0	-0.15 112 %	1 90-110	360
			CCB	ppb	120.0	-0.16	1	300
Amonio	200.8		MS	ppb	5.000	110 %	75-125	
Arsenic	200.8	(STK1932316-001)	MSD	ug/L ug/L	5.000	100 %	75-125 75-125	
		(S1K1932310-001)	MSRPD	ug/L ug/L	5.000	5.8%	≤20	
	200.8	02/18/19:202419AC	CCV		120.0	101 %	90-110	
	200.8	02/16/19.202419AC	CCB	ppb ppb	120.0	0.04	1	
			CCV	ppb ppb	120.0	102 %	90-110	
			CCB	ppb	120.0	0.02	1	
Barium	200.8		MS	ug/L	5.000	107 %	75-125	
Barram	200.0	(STK1932316-001)	MSD	ug/L ug/L	5.000	75.4 %	75-125	
		(51111/02510 001)	MSRPD	ug/L	5.000	1.6%	≤20	
	200.8	02/18/19:202419AC	CCV	ppb	120.0	102 %	90-110	
	200.0	02/10/17/202 117/110	CCB	ppb	120.0	0.017	0.2	
			CCV	ppb	120.0	102 %	90-110	
			CCB	ppb		0.024	0.2	
Beryllium	200.8		MS	ug/L	5.000	96.9 %	75-125	
-		(STK1932316-001)	MSD	ug/L	5.000	86.8 %	75-125	
			MSRPD	ug/L	5.000	0.50	≤1	
	200.8	02/18/19:202419AC	CCV	ppb	120.0	92.1 %	90-110	
			CCB	ppb		-0.015	0.2	
			CCV	ppb	120.0	93.1 %	90-110	
			CCB	ppb		-0.017	0.2	
Cadmium	200.8		MS	ug/L	5.000	113 %	75-125	
		(STK1932316-001)	MSD	ug/L	5.000	99.3 %	75-125	
			MSRPD	ug/L	5.000	12.6%	≤20	
	200.8	02/18/19:202419AC	CCV	ppb	120.0	102 %	90-110	
			CCB	ppb	120.0	0.013	0.2	
			CCV	ppb	120.0	102 %	90-110	
cri .			CCB	ppb	7.000	0.014	0.2	
Chromium	200.8	(CENTAL 0.0001 5.0000	MS	ug/L	5.000	97.4 %	75-125	
		(STK1932316-001)	MSD	ug/L	5.000	88.3 %	75-125	
	200.0	00/10/10 202/10: ~	MSRPD	ug/L	5.000	7.3%	≤20	
	200.8	02/18/19:202419AC	CCV	ppb	120.0	95.9 %	90-110	

Customer: 8-514

: CC 1980547

Lab ID

Constituent	Method	Date/ID	Туре	Units	Conc.	QC Data	DQO	Note
Metals								
Chromium	200.8	02/18/19:202419AC	ССВ	ppb		0.04	1	
Cinomium	200.8	02/16/19.202419AC	CCV	ppb ppb	120.0	96.4 %	90-110	
			CCB	ppb	120.0	0.05	1	
Lead	200.8		MS	ug/L	5.000	105 %	75-125	
Lead	200.0	(STK1932316-001)	MSD	ug/L ug/L	5.000	95.3 %	75-125	
		(51111)02010 001)	MSRPD	ug/L	5.000	9.9%	≤20	
	200.8	02/18/19:202419AC	CCV	ppb	120.0	93.1 %	90-110	
	200.0	02/10/17/202 /17/10	CCB	ppb	120.0	0.004	0.5	
			CCV	ppb	120.0	93.3 %	90-110	
			CCB	ppb		0.005	0.5	
Nickel	200.8		MS	ug/L	5.000	100 %	75-125	
		(STK1932316-001)	MSD	ug/L	5.000	90.0 %	75-125	
			MSRPD	ug/L	5.000	0.52	≤1	
	200.8	02/18/19:202419AC	CCV	ppb	120.0	97.8 %	90-110	
			CCB	ppb		-0.07	1	
			CCV	ppb	120.0	98.4 %	90-110	
			CCB	ppb		-0.11	1	
Selenium	200.8		MS	ug/L	5.000	110 %	75-125	
		(STK1932316-001)	MSD	ug/L	5.000	103 %	75-125	
			MSRPD	ug/L	5.000	6.3%	≤20	
	200.8	02/18/19:202419AC	CCV	ppb	120.0	105 %	90-110	
			CCB	ppb		0.16	1	
			CCV	ppb	120.0	105 %	90-110	
			CCB	ppb		0.02	1	
Silver	200.8		MS	ug/L	5.000	107 %	75-125	
		(STK1932316-001)	MSD	ug/L	5.000	97.3 %	75-125	
			MSRPD	ug/L	5.000	9.8%	≤20	
	200.8	02/18/19:202419AC	CCV	ppb	120.0	99.6 %	90-110	
			CCB	ppb		0.009	1	
			CCV	ppb	120.0	98.3 %	90-110	
			CCB	ppb		0.006	1	
Thallium	200.8		MS	ug/L	5.000	103 %	75-125	
		(STK1932316-001)	MSD	ug/L	5.000	93.3 %	75-125	
			MSRPD	ug/L	5.000	9.6%	≤20	
	200.8	02/18/19:202419AC	CCV	ppb	120.0	94.0 %	90-110	
			CCB	ppb	120.0	0.007	0.2	
			CCV	ppb	120.0	93.9 %	90-110	
	200.0		CCB	ppb		0.007	0.2	
Vanadium	200.8	(CTV102021 C 001)	MS	ug/L	5.000	95.2 %	75-125	
		(STK1932316-001)	MSD	ug/L	5.000	90.0 %	75-125	
	200.0	00/10/10 200410 4 C	MSRPD	ug/L	5.000	1.5%	≤20	
	200.8	02/18/19:202419AC	CCV	ppb	120.0	94.7 %	90-110	
			CCB CCV	ppb	120.0	0.03	2 90-110	
			CCV	ppb	120.0	95.2 % 0.02	2	
Managara	245 1	02/10/10/201974 4 C		ppb				
Mercury	245.1	02/19/19:201874AC	Blank LCS	ug/L	0.2000	ND 103 %	<0.02 85-115	
			MS	ug/L ug/L	0.2000	90.5 %	75-125	
		(STK1931700-001)	MSD	ug/L ug/L	0.2000	90.3 % 92.7 %	75-125 75-125	
		(311331/00-001)	MSRPD	ug/L ug/L	0.2000	2.3%	73-123 ≤20	
	245.1	02/19/19:202463AC	CCV		200.0	104 %	90-110	
	243.1	02/17/17.202403AC	CCB	ppt	200.0	-10.3	20	
			CCV	ppt ppt	200.0	104 %	90-110	
		1	CCB	ppt ppt	200.0	-10.3	20	

Lab ID : CC 1980547

Customer : 8-514

Wet Chem	QO Note	DQO	QC Data	Conc.	Units	Туре	Date/ID	Method	Constituent
Color									Wet Chem
Company	5	5	0.0		units	Dup	(CC 1980547-001)	2120B	
CCV									
Description				10.00			, , , , , , , , , , , ,		
CCB NTU 10.00 10.096 0.1	20	20	1.0%		NTU	Dup	(CC 1980547-001)	2130B	Turbidity
CCV NTU 10.00 107 % 99-110				10.00			02/15/19:202344jba	2130B	
CCB NTU									
Odor				10.00					
Alkalinity (as CaCO3) 2320B 02/20/19:202491AMM CCV mg/L 234.9 93.3 % 90-110 CCV mg/L 234.9 93.4 % 90-105 CCV mg/L 99.0 104 % 95-105 CCV mg/L 20.09 % 5-105 CCV mg/L 20.09 % 20.00 CCV mg/L 20.09 % 20.00 CCV mg/L 20.00 CCV C							(CC 1000547 001)	2150D	0.1
CCV mg/L 234.9 93.4 % 90-110	1			224.0					
Conductivity							02/20/19:202491AMM	2320B	Alkalinity (as CaCO3)
E. C. 2510B (27k/19:201780jmg (CCV umhos/cm p999.0 104 % 95-105 CCV umhos/cm p999.0 104 % 95-105 Set CCV umhos/cm p104 Set CCV p104 Set CCV p104 Set CCC p105 Set CCV p104 Set D106 Set P104 Set D106 Set				234.9			02/19/10:202212IMG	2510P	Conductivity
E. C. 2510B 02/18/19:201780jmg (CC 1980528-002) Dup umbos/cm 0.1% 5 Total Dissolved Solids (TFR) 2540CE 02/18/19:201793CTL (STK1932293-001) (CC 1980548-002) Dup umbos/cm 0.1% 5 Total Dissolved Solids (TFR) 2540CE 02/18/19:201793CTL Blank (CS mg/L 0.09% 5 Chloride 300.0 02/15/19:201962MCA Blank mg/L (STK1932316-001) MSD mg/L 50.00 102 % 85-121 (STK1932317-001) MSD mg/L 50.00 102 % 85-121 (STK1932317-001) MSD mg/L 50.00 97.7 % 85-121 (STK1932317-001) MSD mg/L 50.00 97.7 % 85-121 (CC mg/L 0.09% 51 (STK1932317-001) MSD mg/L 50.00 97.7 % 85-121 (CC mg/L 0.09% 51 (STK1932317-001) MSD mg/L 50.00 97.7 % 85-121 (CC mg/L 0.09% 51 (STK1932317-001) MSD mg/L 50.00 97.7 % 85-121 (CC mg/L 0.000 1 1000 0.04% 51 (STK1932317-001) MSD mg/L 50.00 97.7 % 85-121 (CC mg/L 0.000 1 1000 0.04% 51 (STK1932317-001) MSD mg/L 50.00 97.7 % 85-121 (CC mg/L 0.000 1 1000 0.04% 51 (STK1932317-001) MSD mg/L 50.00 99.7 % 90-110 (CC mg/L 0.000 1 1000 0.04% 51 (STK1932317-001) MSD mg/L 50.00 99.7 % 87-120 (STK1932317-001) MSD mg/L 50.00 99.2 % 90.110 (ST				999 N			02/16/19.202312JWIG	2310B	Conductivity
E. C. 2510B 02/18/19:201780jmg (CC 1980528-002) Dup umhos/cm umhos/cm umhos/cm 0.1% 5									
CCC 1980528-002 Dup umhos/cm 0.1% 5							02/18/19:201780img	2510B	E. C.
Total Dissolved Solids (TFR)									
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	20	20	9.0				02/18/19:201793CTL	2540CE	Total Dissolved Solids (TFR)
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	-110	90-110	94.9 %	994.8	mg/L	LCS			
Chloride 300.0 02/15/19:201962MCA Blank LCS mg/L 25.00 98.9 % 90-110 MSD mg/L 50.00 102 % 85-121 MSRPD mg/L 50.00 101 % 85-121 MSRPD mg/L 50.00 97.6 % 85-121 MSRPD mg/L 50.00 97.7 % 85-121 MSRPD mg/L 50.00 95.7 % 90-110 10 10 10 10 10 10 10						Dup			
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$									
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$					mg/L		02/15/19:201962MCA	300.0	Chloride
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$						LCS			
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$							(CITY 102221 6 001)		
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$							(STK1932316-001)		
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$									
MSRPD mg/L 10.00 0.04% ≤19 300.0 02/15/19:202556MCA ICB mg/L 25.00 95.7 % 90-110 CCB mg/L 25.00 95.7 % 90-110 1 CCV mg/L 25.00 95.8 % 90-110 CCV mg/L 25.00 95.8 % 90-110 MSD mg/L 5.000 95.4 % 90-110 MSD mg/L 5.000 99.7 % 87-120 MSRPD mg/L 5.000 99.7 % 87-120 MSRPD mg/L 5.000 99.2 % 87-120 MSRPD mg/L 5.000 99.2 % 87-120 MSRPD mg/L 5.000 99.4 % 87-120 MSRPD mg/L 5.000 99.4 % 87-120 MSRPD mg/L 5.000 99.4 % 87-120 MSRPD mg/L 5.000 99.2 % 90-110 CCV mg/L 5.000 99.2 % 90-110 CCB mg/L 5.000 97.1 % 90-110 CCB mg/L 5.000 97.1 % 90-110 CCV mg/L 5.000 97.1 % 90-110 MS mg/L 40.00 102 % 85-119 60.000 60.1 60.000							(STK1932317-001)		
STK1932316-001 STK1932316-001 Nitrate STK1932316-001 STK1932317-001 STTY STATE STA							(STR1)32317 001)		
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$				10.00			02/15/19:202556MCA	300.0	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$				25.00			02/10/1/120200011011	200.0	
Fluoride $ \begin{array}{c ccccccccccccccccccccccccccccccccccc$									
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	-110	90-110	95.8 %	25.00		CCV			
$ (STK1932316-001) \begin{tabular}{ c c c c c c c c c c c c c c c c c c c$							02/15/19:201962MCA	300.0	Fluoride
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$									
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$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$							(STK 1032317 001)		
300.0 02/15/19:202556MCA ICB mg/L 0.000 0.1							(S1K1932317-001)		
ICV mg/L 2.500 92.2 % 90-110				10.00	·		02/15/19·202556MCA	300.0	
CCB mg/L 0.000 0.1				2.500			02/15/17/202550MICA	200.0	
CCV mg/L 2.500 92.1 % 90-110									
LCS mg/L 20.00 97.1 % 90-110 MS mg/L 40.00 102 % 85-119 (STK1932316-001) MSD mg/L 40.00 101 % 85-119				2.500	-				
MS mg/L 40.00 102 % 85-119 (STK1932316-001) MSD mg/L 40.00 101 % 85-119	0.4	< 0.4	ND		mg/L	Blank	02/15/19:201962MCA	300.0	Nitrate
(STK1932316-001) MSD mg/L 40.00 101 % 85-119					mg/L				
							(STK1932316-001)		
		≤19	0.9%	10.00	mg/L	MSRPD			
MS mg/L 40.00 101 % 85-119							(CTV1020217 001)		
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$							(S1K1932317-001)		
				10.00			02/15/19·202556MCA	300.0	
300.0 02/15/19:202556MCA ICB mg/L 0.000 0.5 ICV mg/L 20.00 93.0 % 90-110				20.00			02/13/17.202330MCA	300.0	

Lab ID : CC 1980547

Customer : 8-514

Constituent	Method	Date/ID	Туре	Units	Conc.	QC Data	DQO	Note
Wet Chem								
Nitrate	300.0	02/15/19:202556MCA	ССВ	mg/L		0.000	0.5	
			CCV	mg/L	20.00	93.1 %	90-110	
Nitrate + Nitrite as N	300.0	02/15/19:201962MCA	Blank	mg/L		ND	< 0.1	
Nitrate Nitrogen	300.0	02/15/19:201962MCA	Blank	mg/L		ND	< 0.1	
Nitrite	300.0	02/15/19:201962MCA	Blank	mg/L		ND	< 0.5	
			LCS	mg/L	15.00	95.8 %	90-110	
			MS	mg/L	30.00	99.7 %	74-126	
		(STK1932316-001)	MSD	mg/L	30.00	98.8 %	74-126	
			MSRPD	mg/L	10.00	0.9%	≤20	
		(STK1932317-001)	MS MSD	mg/L	30.00 30.00	98.5 % 98.8 %	74-126 74-126	
		(S1K1932317-001)	MSD MSRPD	mg/L mg/L	10.00	98.8 % 0.3%	/4-126 ≤20	
	300.0	02/15/19:202556MCA	ICB	mg/L mg/L	10.00	0.000	0.5	
	300.0	02/13/19.202330MCA	ICV	mg/L	15.00	92.8 %	90-110	
			CCB	mg/L	13.00	0.000	0.5	
			CCV	mg/L	15.00	93.5 %	90-110	
Nitrite Nitrogen	300.0	02/15/19:201962MCA	Blank	mg/L		ND	< 0.2	
Sulfate	300.0	02/15/19:201962MCA	Blank	mg/L		ND	< 0.5	
			LCS	mg/L	50.00	102 %	90-110	
			MS	mg/L	100.0	104 %	82-124	
		(STK1932316-001)	MSD	mg/L	100.0	104 %	82-124	
			MSRPD	mg/L	10.00	0.6%	≤23	
			MS	mg/L	100.0	104 %	82-124	
		(STK1932317-001)	MSD	mg/L	100.0	104 %	82-124	
			MSRPD	mg/L	10.00	0.2%	≤23	
	300.0	02/15/19:202556MCA	ICB	mg/L	5 0.00	0.000	0.5	
			ICV	mg/L	50.00	99.1 %	90-110	
			CCB CCV	mg/L mg/L	50.00	0.222 99.4 %	0.5 90-110	
Perchlorate	314.0	02/15/19:201724MCA	Blank		30.00	99.4 % ND	<2	
Perchiorate	314.0	02/15/19:201/24MCA	LCS	ug/L ug/L	25.00	101 %	85-115	
			MS	ug/L ug/L	25.00	85.0 %	80-110	
		(SP 1902013-001)	MSD	ug/L ug/L	25.00	90.5 %	80-120	
		(81 1)02018 001)	MSRPD	ug/L	25.00	6.3%	≤15	
		(SP 1902013-001)	Dup	ug/L		0.0	2	
	314.0	02/15/19:202511MCA	ICB	ppb		0.00	2.0	
			ICV	ppb	2.000	94.7 %	85-115	
			CCB	ppb		0.00	2.0	
			CCV	ppb	10.00	98.5 %	85-115	
Cyanide	4500CNCE	02/20/19:202524AMM		mg/L	0.1000	102 %	90-110	
			CCB	mg/L	0.1000	-0.00130	0.004	
			CCV	mg/L	0.1000	106 %	90-110	
C :1 T :1	450000100	00/00/10 001000 47 57	CCB	mg/L	-	-0.00130	0.004	
Cyanide, Total	4500CNCE	02/20/19:201928AMM		mg/L	0.1000	ND	<0.004	
			LCS LCS	mg/L mg/L	0.1000 0.4000	101 % 97.8 %	90-110 90-110	
			MS	mg/L	0.4000	97.8 % 161 %	26-226	
		(SP 1901944-001)	MSD	mg/L mg/L	0.05000	158 %	26-226	
		(51 1/01/11 001)	MSRPD	mg/L	0.05000	2.1%	≤36	
MBAS	5540C	02/15/19:202349jmg	CCB	mg/L		0.000	0.1	
		J	CCV	mg/L	0.1000	100 %	99-101	
MBAS Screen	5540C		MS	mg/L	0.1000	100 %	90-110	
		(SP 1902129-001)	MSD	mg/L	0.1000	100 %	90-110	
			MSRPD	mg/L	0.1000	0.0	≤0.1	

February 22, 2019 Cleath-Harris Geologists

Customer : 8-514

: CC 1980547

Lab ID

Definition	
ICV	: Initial Calibration Verification - Analyzed to verify the instrument calibration is within criteria.
ICB	: Initial Calibration Blank - Analyzed to verify the instrument baseline is within criteria.
CCV	: Continuing Calibration Verification - Analyzed to verify the instrument calibration is within criteria.
CCB	: Continuing Calibration Blank - Analyzed to verify the instrument baseline is within criteria.
Blank	: Method Blank - Prepared to verify that the preparation process is not contributing contamination to the samples.
LCS	: Laboratory Control Standard/Sample - Prepared to verify that the preparation process is not affecting analyte recovery.
MS	: Matrix Spikes - A random sample is spiked with a known amount of analyte. The recoveries are an indication of how that sample
	matrix affects analyte recovery.
MSD	: Matrix Spike Duplicate of MS/MSD pair - A random sample duplicate is spiked with a known amount of analyted. The recoveries are an indication of how that sample matrix affects analyte recovery.
	: Duplicate Sample - A random sample with each batch is prepared and analyzed in duplicate. The relative percent difference is an
Dup	indication of precision for the preparation and analysis.
MSRPD	: MS/MSD Relative Percent Difference (RPD) - The MS relative percent difference is an indication of precision for the preparation
MSKFD	and analysis.
ND	: Non-detect - Result was below the DQO listed for the analyte.
DQO	: Data Quality Objective - This is the criteria against which the quality control data is compared.
Explanation	
360	: CCV above Acceptance Range (AR). Samples which were non detect for this analyte were accepted.

February 22, 2019

Cleath-Harris Geologists Attn: Spencer Harris 71 Zaca Lane Suite 140 San Luis Obispo, CA 93401

Subject: Subcontract Analysis for FGL Lab No. CC 1980547

Enclosed please find results for the following sample(s) which were received by FGL.

Asbestos

Please note that this analysis was performed by LA Testing

Thank you for using FGL Environmental.

Sincerely,



Enclosure



LA Testing

520 Mission Street South Pasadena, CA 91030 Phone/Fax: (323) 254-9960 / (323) 254-9982 http://www.LATesting.com / pasadenalab@latesting.com LA Testing Order ID: 321904102 FGLE25 Customer ID:

Customer PO: Project ID:

Attn: Confirmations Log in

FGL Environmental

853 Corporation St Santa Paula, CA 93060 Phone:

(805) 392-2024

Fax:

Received: 02/15/2019 Analyzed: 02/21/2019

Proj: CC1980547- (8-514)

Test Report: Determination of Asbestos Structures >10µm in Drinking Water Performed by the 100.2 Method (EPA 600/R-94/134)

ASBESTOS

Sample ID Client / EMSL	Sample Filtration Date/Time	Original Sample Vol. Filtered	Effective Filter Area	Area Analyzed	Asbestos Types	Fibers Detected	Analytical Sensitivity	Concentration	Confidence Limits
		(ml)	(mm²)	(mm²)			MFL	(million fibers per	liter)
1	2/15/2019	15	1288	0.2580	None Detected	ND	0.33	<0.33	0.00 - 1.20
321904102-0001	12:30 PM								

Collection Date/Time: 02/14/2019 13:15

Due to excessive particulate the analytical sensitivity of 0.2 MFL as required by the method was not reached.

12:30 PM

Analyst(s) Feng Liang

> Jerry Drapala Ph.D, Laboratory Manager or Other Approved Signatory

Any questions please contact Jerry Drapala.

Initial report from: 02/22/2019 06:51:13

Sample collection and containers provided by the client, acceptable bottle blank level is defined as ≤0.01MFL>10um. ND=None Detected. This report relates only to those items tested. This report may not be reproduced, except in full, without written permission by LA Testing. Samples received in good condition unless otherwise noted.

Samples analyzed by LA Testing South Pasadena, CA CA ELAP 2283

February 22, 2019

Cleath-Harris Geologists Attn: Spencer Harris 71 Zaca Lane Suite 140 San Luis Obispo, CA 93401

Subject: Subcontract Analysis for FGL Lab No. CC 1980547

Enclosed please find results for the following sample(s) which were received by FGL.

• Sub Contracted-EPA 507 - Thiobencarb

Please note that this analysis was performed by Weck Laboratories, Inc. (ELAP Certified Laboratory)

Thank you for using FGL Environmental.

Sincerely,



Enclosure



Certificate of Analysis

FINAL REPORT

Work Orders: 9B15020

Report Date: 2/22/2019

Received Date: 2/15/2019

Turnaround Time: 4 workdays

Phones: (805) 392-2012

Fax: (805) 525-4172

P.O. #:

Billing Code:

Project: CC1980547 - (8-514)

Attn: Cindy Aguirre

Client: FGL Environmental

853 Corporation Street Santa Paula, CA 93060

Dear Cindy Aguirre,

Enclosed are the results of analyses for samples received 2/15/19 with the Chain-of-Custody document. The samples were received in good condition, at 4.8 °C and on ice. All analyses met the method criteria except as noted in the case narrative or in the report with data qualifiers.

Sample Results

Sample:	Strauss CW2					Sample	d: 02/14/19 13:15 by Ar	ndrea Bage
	9B15020-01 (Water)							
Analyte			Result	MRL	Units	Dil	Analyzed	Qualifier
Method: EPA	A 525.2	Batch ID: W9B0982	Instr: GCMS16	Prepared: 0	2/19/19 08:54		Analyst: rmr	
Thiobenca	ırb		ND	0.10	ug/l	1	02/21/19 10:28	
Surrogate(s)								
1,3-Dimeth	hyl-2-nitrobenzene		238%	70-130	Conc: 11	1.9	02/21/19 10:28	S-GC
Perylene-c	d12		100%	50-120	Conc: 0.0	702	02/21/19 10:28	S-GC
Triphenyl p	phosphate		108%	70-130	Conc: 5.	42	02/21/19 10:28	

9B15020 Page 1 of 3



Certificate of Analysis

FINAL REPORT

Quality Control Results

Semivolatile Organic Compounds by GC/N	IS								
				Spike	Source	%REC		RPD	
Analyte	Result	MRL	Units	Level	Result %REC	Limits	RPD	Limit	Qualifie
atch: W9B0982 - EPA 525.2/SPE									
Blank (W9B0982-BLK1)			P	repared: 02/19/	19 Analyzed: 02/21/19				
Thiobencarb	ND	0.10	ug/l						
Surrogate(s) 1,3-Dimethyl-2-nitrobenzene	5.00		ug/l	5.00	100	70-130			
Perylene-d12			ug/l	5.00	91	50-120			
Triphenyl phosphate			ug/l	5.00	97	70-130			
LCS (W9B0982-BS1)			P	renared: 02/19/	19 Analyzed: 02/21/19				
Thiobencarb	6.09	0.10	ug/l	5.00	122	70-130			
Surrogate(s)									
1,3-Dimethyl-2-nitrobenzene			ug/l	5.00	96	70-130			
Perylene-d12	4.92		ug/l	5.00	98	50-120			
Triphenyl phosphate	5.27		ug/l	5.00	105	70-130			
LCS Dup (W9B0982-BSD1)			P	repared: 02/19/	19 Analyzed: 02/21/19				
Thiobencarb	5.95	0.10	ug/l	5.00	119	70-130	2	30	
Surrogate(s) 1,3-Dimethyl-2-nitrobenzene			ug/l	5.00	100	70-130			
•			J						
Perylene-d12			ug/l	5.00	96	50-120			
Triphenyl phosphate	5.27		ug/l	5.00	105	70-130			

9B15020 Page 2 of 3



Definition

Certificate of Analysis

FINAL REPORT



Notes and Definitions

S-GC	Surrogate recovery outside of control limits due to a possible matrix effect . The data was accepted based on valid recovery of the remaining surrogate.
ND	NOT DETECTED at or above the Method Reporting Limit (MRL). If Method Detection Limit (MDL) is reported, then ND means not detected at or above the MDL.
Dil	Dilution
dry	Sample results reported on a dry weight basis
RPD	Relative Percent Difference
% Rec	Percent Recovery
Source	Sample that was matrix spiked or duplicated.
MDL	Method Detection Limit
MRL	The minimum levels, concentrations, or quantities of a target variable (e.g., target analyte) that can be reported with a specified degree of confidence. The MRL is also known as Limit of Quantitation (LOQ) and Detection Limit for Reporting (DLR)
MDA	Minimum Detectable Activity
NR	Not Reportable
TIC	Tentatively Identified Compound (TIC) using mass spectrometry. The reported concentration is relative concentration based on the nearest internal

Any remaining sample(s) will be disposed of one month from the final report date unless other arrangements are made in advance.

standard. If the library search produces no matches at, or above 85%, the compound is reported as unknown.

An Absence of Total Coliform meets the drinking water standards as established by the California State Water Resources Control Board (SWRCB)

All results are expressed on wet weight basis unless otherwise specified.

All samples collected by Weck Laboratories have been sampled in accordance to laboratory SOP Number MIS 002.

Reviewed by:

Regina Giancola Project Manager









ELAP-CA #1132 • EPA-UCMR #CA00211 • Guam-EPA #17-008R • HW-DOH # • ISO 17025 #L2457.01 • LACSD #10143 • NELAP-CA #04229CA • NELAP-OR #4047 • NJ-DEP #CA015 • NV-DEP #NAC 445A • SCAQMD #93LA1006

This is a complete final report. The information in this report applies to the samples analyzed in accordance with the chain-of-custody document. Weck Laboratories certifies that the test results meet all requirements of TNI unless noted by qualifiers or written in the Case Narrative. This analytical report must be reproduced in its entirety.

Appendix E-3

Construction Water Supply Aquifer Letter – September 2019

Cleath-Harris Geologists, Inc.

75 Zaca Lane, Suite 110 San Luis Obispo, CA 93401 (805) 543-1413



September 25, 2019

Dear Mr. Beland:

Mr. Jörg Beland Strauss Wind, LLC 5901 Priestly Drive, Suite 300 Carlsbad, CA 92008

Subject: Response to comments on construction water supply aquifer for Strauss Wind Energy Project, Lompoc, Santa Barbara County.

As requested, Cleath-Harris Geologists (CHG) has prepared a response to the comments received from Santa Barbara County regarding the proposed construction water supply aquifer for the Strauss Wind Energy Project (Project). The comments received are as follows:

Regarding the hydrology report, please provide a map showing all of the existing wells within the aquifer to be used for construction water, descriptions of well ownership and current use, and technical justification for a reasonable drawdown at each well that would be of sufficient magnitude to adversely affect the water supply delivered by that well. This drawdown will be used in the mitigation measure to trigger cessation of pumping of construction water. Information regarding the extent of this aquifer relative to any potential impact to Frick's Spring is also requested.

The above referenced hydrology report is a description of the construction water supply aquifer provided in correspondence from CHG¹. Additional details and technical justification for mitigation measures have been prepared herein based on the available information.

Limits of Source Aquifer

The source aquifer for construction water wells forms a syncline within siliceous shale of the upper Monterey Formation. The lateral extent of the aquifer is interpreted to be where the limbs of the syncline rise to the water table, encompassing a trough-shaped groundwater storage reservoir. To the east, the effective lateral extent of the reservoir is the San Miguelito Canyon watershed boundary.

Figure 1 shows the limits of the groundwater storage reservoir and associated source aquifer. Construction water wells would tap fractured shale zones within the

¹ CHG, Comments on Draft SEIR for Strauss Wind Energy Project, Lompoc, Santa Barbara County, May 21, 2019



groundwater storage reservoir. Cross-sections showing interpreted hydrogeologic profiles through the groundwater storage reservoir are shown in Figures 2-4.

Existing Wells

Two existing wells have been identified within the limits of the groundwater storage reservoir. These wells are labeled O&M Well (CW2) and Offsite Well A on Figure 1. A third existing well, Offsite Well B, has been located just outside the groundwater storage reservoir limit east of the watershed divide.

Well CW2 is a Project well owned by Signorelli Family Trust and will be used for supplying water to the Operations and Maintenance Building. Offsite Well A is within a small enclosure near the entrance to a ranch along San Miguelito Road. Groundwater from this private domestic well is pumped uphill to a tank near the ranch residence.

A water well log search was performed using the California Department of Water Resources (DWR) database to help identify wells in the vicinity of the groundwater storage reservoir. Two logs were found and are attached. DWR log #40446, dated October 1961, is for a test well "5 miles south of Lompoc in Miguelito Canyon" which plots within the groundwater reservoir area at the approximate location of Offsite Well A. The test well log shows clay through a total depth of 51 feet, and the standing water level is reported as "none", with no indication of a well being constructed. Therefore, the construction details of Offsite Well A are unknown. A second log, No. E0094758 is labeled Offsite Well B on Figure 1. This well was drilled for irrigation purposes in 2009, and is completed in fractured brown shale to 513 feet depth. Offsite Well B is on property currently owned by The Nature Conservancy and is likely inactive, based on a review of aerial images.

Reasonable Drawdown

The County has requested technical justification for a reasonable drawdown at each well that would be of sufficient magnitude to adversely affect the water supply delivered by that well. Factors to consider when estimating reasonable drawdown include well construction, pump size and flow rate, pump depth setting, and well specific capacity.

Offsite Well A is the only non-Project well within the effective limits of the groundwater storage reservoir, based on the well log search and local driller input. The 1961 test well log (#40446; attached) indicates a well in the vicinity of Offsite Well A would need to be over 50 feet deep to be productive and it is conservatively assumed that the currently active domestic well is at least 100 feet deep and taps fractured shale aquifer zones similar to Project O&M Well CW2.



The technical justification for a reasonable drawdown at Offsite Well A, for which impacts would be measured and mitigation implemented, includes the following assumptions:

- The domestic well is 100 feet deep with the bottom 40 feet screened in the fractured shale groundwater reservoir.
- A 2 horsepower pump is set 10 feet above the well bottom.
- Static water level is 20 feet deep under existing conditions (close to the invert of San Miguelito Creek).
- Aquifer transmissivity and well specific capacity is similar to nearby O&M Well CW2, adjusted for the aquifer thickness tapped by each well.
- A nominal discharge capacity for the well pump of 4-5 gallons per minute (gpm) needs to be maintained to serve the residence. This is more than sufficient to provide a few thousand gallons per day for ranch use.
- Impacts to the producing aquifer zones at the well will be avoided.

Using these assumptions, the 12-hour specific capacity of Offsite Well A is estimated at 0.75 gpm per foot of drawdown, and therefore would require up to 6.7 feet of drawdown during a 12-hour pumping cycle at 5 gpm. In order to avoid impacts to the producing aquifer zone (i.e. maintain pumping water levels above the well screen), the maximum reasonable drawdown before impacts to Offsite Well A occur is estimated to be 30 feet², based on the available information and assumptions.

Monitoring of water level drawdown in the vicinity of Offsite Well A will be performed at a designated monitoring well constructed on Project property across San Miguelito Road, as close as possible to Offsite Well A (Figure 1). The monitoring well will be equipped with a pressure transducer that will provide detailed water level trends and allow the Project applicant (and County) to anticipate impacts at Offsite Well A before they occur.

² Maintaining 40 feet of saturated aquifer thickness + 6.7 feet of anticipated drawdown at 5 gpm = 46.7 feet of minimum water column in the well. The exiting water column is assumed to be 80 feet (100 feet well depth – 20 feet depth static level), therefore a reasonable drawdown of 80-46.7 = 33.3 feet would be estimated (rounded down to a nominal 30 feet). An additional 30 feet of lift would decrease pump discharge by approximately 0.2 gpm, based on the representative performance curve.



Mitigation Measures

Recommendations for mitigation measure MM WAT-1 (Construction Water Source) were provided in previous correspondence³. Based on the comments received from the County, revised mitigation measures are recommended as follows:

- a) Allow use of on-site wells for construction water.
- b) Require the Applicant to construct a monitoring well in order to monitoring water levels within the aquifer. The monitoring well will be equipped with an automatic water level recorder (e.g. pressure transducer).
- c) Water level data from the monitoring well will be reported to the County on a biweekly basis during the first six months of construction, and monthly thereafter until three months following the end of construction, or as agreed to between the Applicant and the County. Water level data reported to the County will include an interpretation of water level trends and anticipated construction activity and water use.
- d) If water level trends at the monitoring well indicate a drawdown of 30 feet or more is anticipated at any time during the course of construction water use, the Applicant with concurrence from the County will either:
 - Adjust and/or reduce construction well production to the extent feasible to avoid water levels reaching the reasonable drawdown threshold of 30 feet, or
 - b. Provide water of suitable quantity and quality, as needed, to replace any loss in production at the well. The Applicant would be responsible for the costs and transportation of water to the existing tank(s) in order to provide the required quantity of supplemental water.

Note that the recommended mitigation for significant impact to Offsite Well A are acceptable industry practices. These measures would also ensure that the additional impacts of trucking in construction water would be avoided.

Potential Impacts to Frick Springs

Frick Springs consists of developed springs that are part of the water system for the City of Lompoc. These springs are located along the formation contact between the Monterey Formation and the Sacate Formation (Figure 1), approximately ³/₄ miles from the construction water wells. The approximately elevations of the individual springs at Frick Springs range from 900-950 feet above sea level and are 50-100 feet above the adjacent

³ CHG, Comments on Draft SEIR for Strauss Wind Energy Project, Lompoc, Santa Barbara County, May 21, 2019



invert elevation of San Miguelito Creek (i.e. the springs are at greater pressure head than the creek). The geologic structure in the Monterey Formation approaching Frick Springs consists of steeply dipping and tightly folded beds (Figure 4), which would transmit groundwater preferentially along a northwest-southeast direction (parallel to the fold axis) and restrict groundwater flow in the direction of the groundwater storage reservoir shown in Figure 1. Given the distance from the construction water wells, elevation relative to the creek, and geologic structure surrounding Frick Springs, the Project's use of the construction water wells are not expected to impact the Frick Springs water system.

No. HG 633

Respectfully submitted,

CLEATH-HARRIS GEOLOGISTS

Spencer J. Harris, HG 633 Senior Hydrogeologist

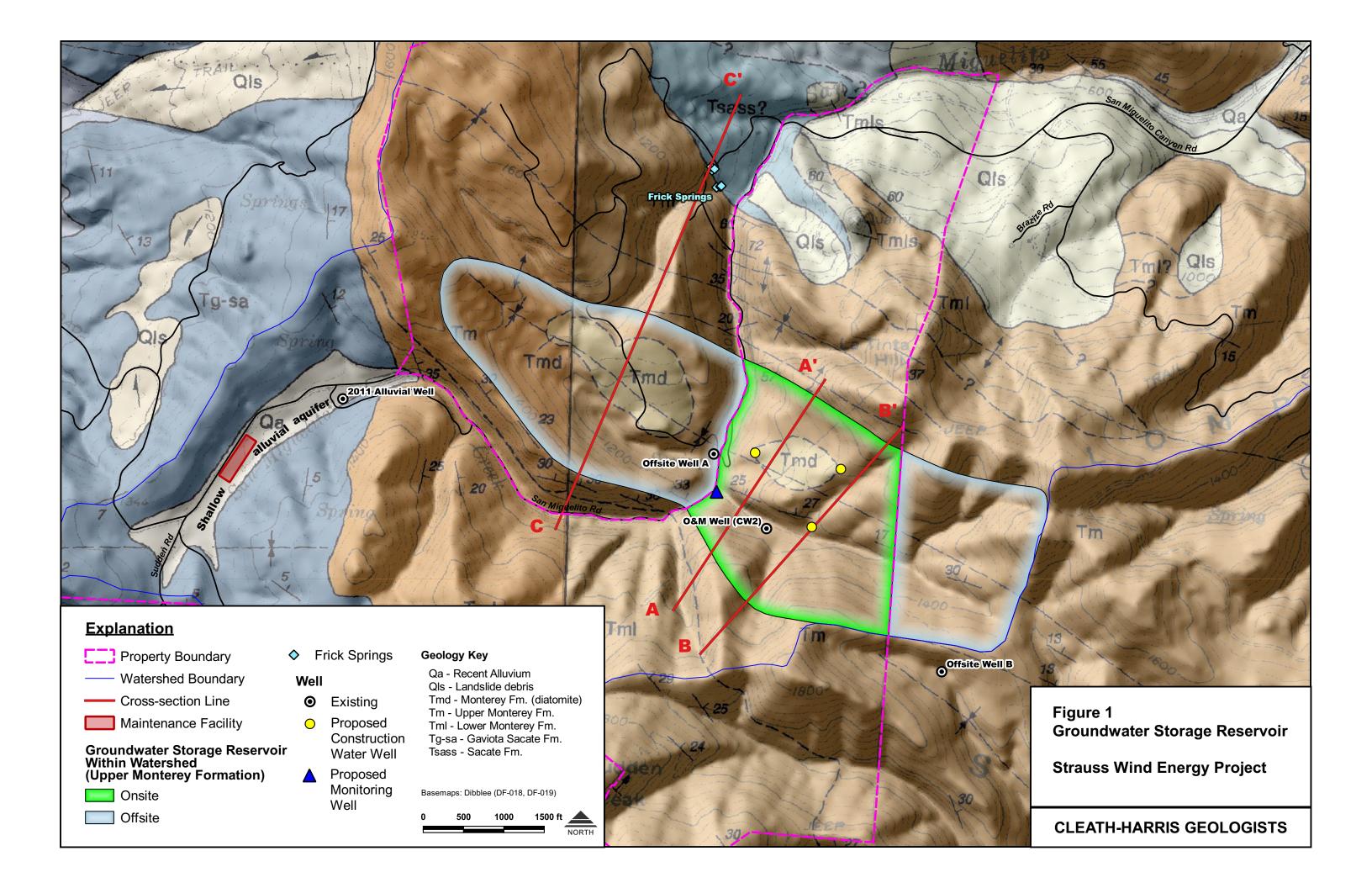
attachments

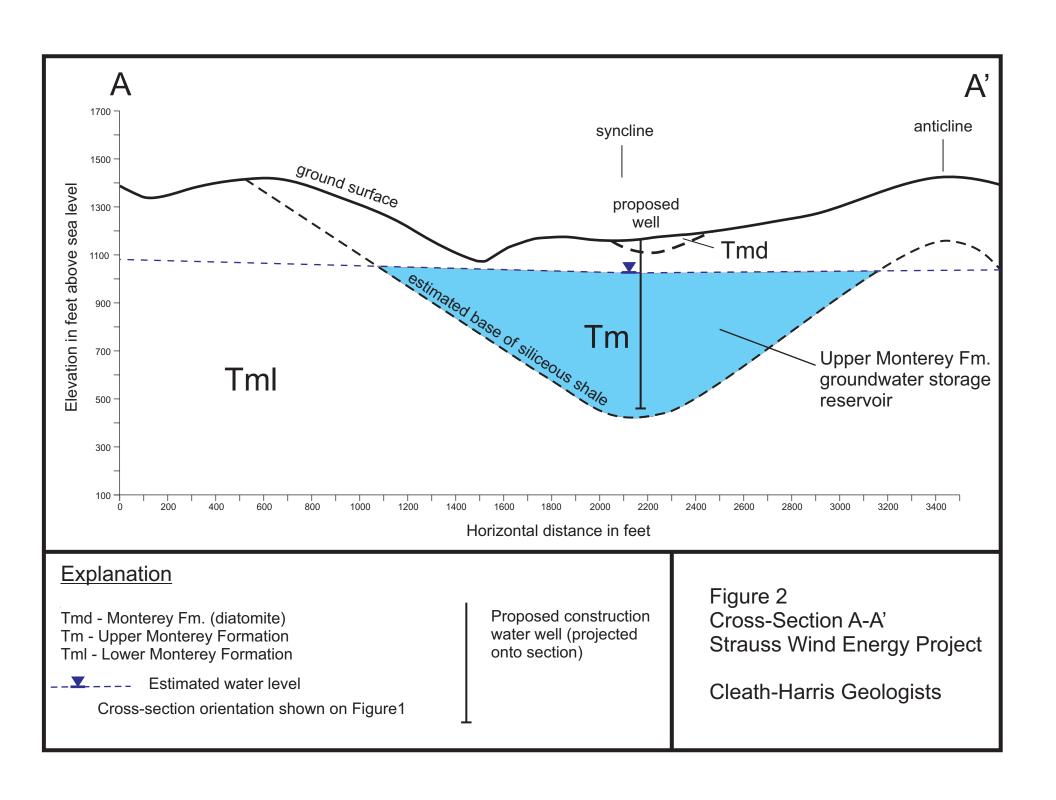


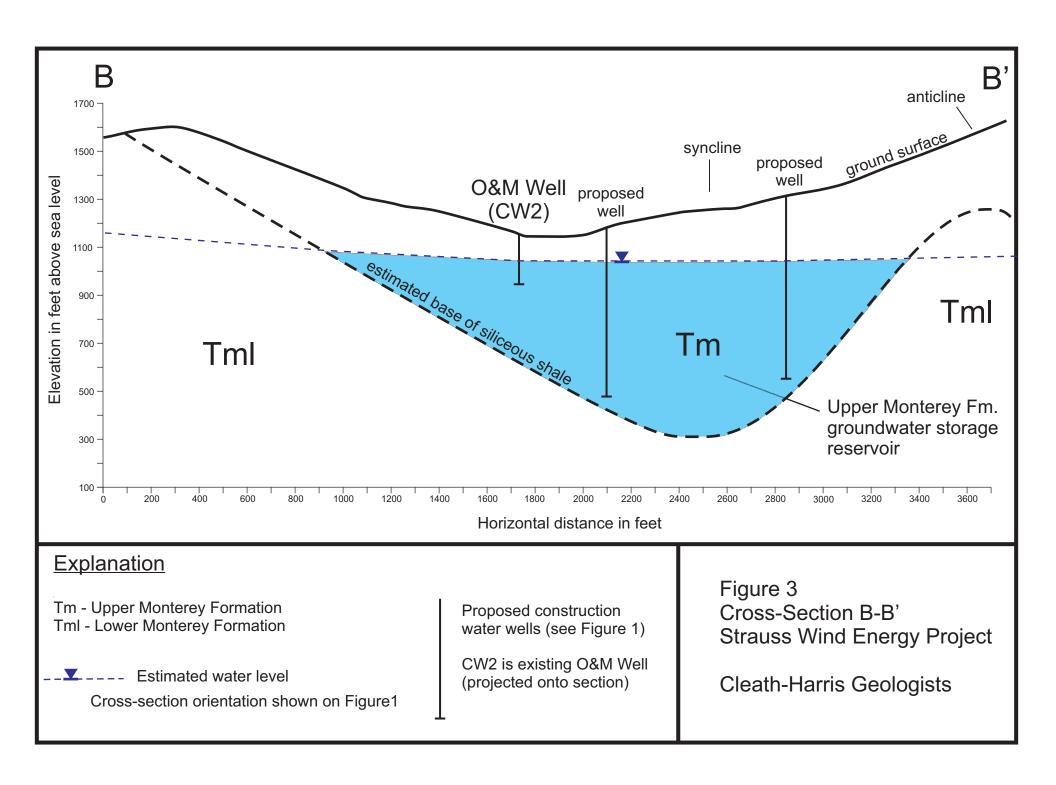
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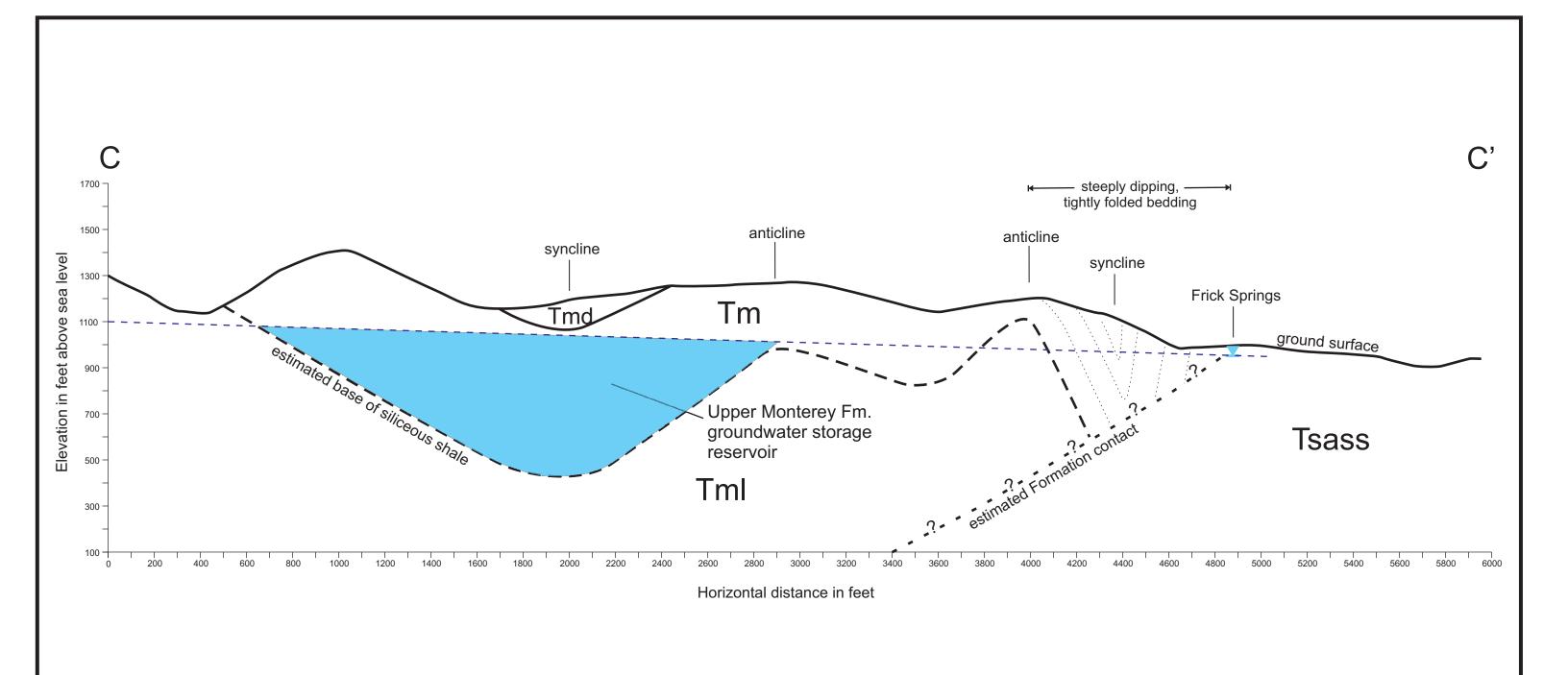
Figures 1-4 DWR Well Log #40446 DWR Well Log #E0094758

Source Aquifer comments 9/25/2019









Explanation

Tmd - Monterey Fm. (diatomite)
Tm - Upper Monterey Formation
Tml - Lower Monterey Formation
Tsass - Sacate Formation

Cross-section orientation shown on Figure1

Figure 4 Cross-Section C-C' Strauss Wind Energy Project

Cleath-Harris Geologists

File Original, Duplicate and Triplicate with the REGIONAL WATER POLLUTION

CONTROL BOARD No. 3.

WATER WELL DRILLERS REPORT (Sections 7076, 7077, 7078, Water Code)

Do	Not Fill In
No	40446
- ·	

STATE OF CALIFORNIA

T.A. o	#0##0 :
State Well No	06 N/34W-19
Other Well No.	
Oction A cir 2 (or	***************************************

(1) OWNER: plots near location of	(11) WELL LOG:
Nama	Total depth 137 fr. Depth of completed well fr.
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(3) TYPE OF WORK (check):	
New well Deepening Reconditioning Abandon	
If abandonment, describe material and procedure in Item 11.	0.5
(4) PROPOSED USE (check): (5) EQUIPMENT:	
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IF ADDITIONAL SPACE IS NEEDED, USE NEXT CONSECUTIVELY NUMBERED FORM

Appendix E-4

Construction Water Supply Aquifer Letter – October 2019

Cleath-Harris Geologists, Inc.

75 Zaca Lane, Suite 110 San Luis Obispo, CA 93401 (805) 543-1413



October 28, 2019

Mr. Jörg Beland Strauss Wind, LLC 5901 Priestly Drive, Suite 300 Carlsbad, CA 92008

Subject: Revised response to comments on construction water supply aquifer

for Strauss Wind Energy Project, Lompoc, Santa Barbara County.

Dear Mr. Beland:

Cleath-Harris Geologists (CHG) has prepared a revised response to the comments received from the County of Santa Barbara (County) regarding the proposed construction water supply aquifer for the Strauss Wind Energy Project (Project). The comments received are as follows:

Regarding the hydrology report, please provide a map showing all of the existing wells within the aquifer to be used for construction water, descriptions of well ownership and current use, and technical justification for a reasonable drawdown at each well that would be of sufficient magnitude to adversely affect the water supply delivered by that well. This drawdown will be used in the mitigation measure to trigger cessation of pumping of construction water. Information regarding the extent of this aquifer relative to any potential impact to Frick's Spring is also requested.

The above referenced hydrology report is a description of the construction water supply aquifer provided in correspondence from CHG¹. Additional details and technical justification for mitigation measures have been prepared herein based on new information that updates and revises the response to comments dated September 25, 2019. A discussion of Project water use and the County's Thresholds of Significance is also included herein.

Limits of Source Aquifer

The source aquifer for construction water wells forms a syncline within siliceous shale of the upper Monterey Formation. The lateral extent of the aquifer is interpreted to be where the limbs of the syncline rise to the water table, encompassing a trough-shaped groundwater storage reservoir. To the east, the effective lateral extent of the reservoir is the Miguelito Canyon watershed boundary.

¹ CHG, Comments on Draft SEIR for Strauss Wind Energy Project, Lompoc, Santa Barbara County, May 21, 2019



Figure 1 shows the limits of the groundwater storage reservoir and associated source aquifer. Construction water wells would tap fractured shale zones within the groundwater storage reservoir. Cross-sections showing interpreted hydrogeologic profiles through the groundwater storage reservoir are shown in Figures 2-4.

Existing Wells and Developed Springs

Three existing wells have been identified within the limits of the groundwater storage reservoir. These wells are labeled O&M Well (CW2), Offsite Well A, and Offsite Well B on Figure 1. A fourth existing well, Offsite Well C, has been located just outside the groundwater storage reservoir limit east of the watershed divide. The developed springs identified in the project vicinity are outside of the groundwater storage reservoir, and include Frick Springs (City of Lompoc) and a private Ranch Spring (Figure 1).

Well CW2 is a Project well owned by Signorelli Family Trust and will be used for supplying water to the Operations and Maintenance Building. Offsite Well A, Offsite Well B, and the Ranch Spring serve the adjacent ranch property across San Miguelito Road. Frick Springs is a public water system serving residents of Miguelito canyon.

Information for Offsite Well A (49 feet deep), Offsite Well B (155 feet deep), and the Ranch Spring was obtained from County records. Construction details for the wells are attached. A search of Well Completion Reports was also performed using the California Department of Water Resources (DWR) database to help identify wells in the vicinity of the groundwater storage reservoir. Two logs were found and are attached. DWR log #40446, dated October 1961, is for a test well "5 miles south of Lompoc in Miguelito Canyon" which plots within the groundwater reservoir area at the approximate location of Offsite Well A. The test well log shows clay through a total depth of 51 feet, and the standing water level is reported as "none", with no indication of a well being constructed. A second log, No. E0094758 is labeled Offsite Well C on Figure 1. This well was drilled for irrigation purposes in 2009, and is completed in fractured brown shale to 513 feet depth. Offsite Well C is on property currently owned by The Nature Conservancy and is likely inactive, based on a review of aerial images.

A source yield test for the Ranch Spring in 2002 reported that the spring source exceeded the minimum continuous flow requirement 1.5 gallons per minute (gpm) for domestic supply from springs (County ordinance 12-4843). Construction of the existing ranch residence was subsequently permitted by the County, and based on the results of this source yield test, the spring is likely the primary water supply for the residence. The Ranch Spring, at an elevation of approximately 1,500 feet above sea level and outside of the limits of the source aquifer for the Project wells, will not be impacted by Project water use.



Reasonable Drawdown

The County has requested technical justification for a reasonable drawdown at each well that would be of sufficient magnitude to adversely affect the water supply delivered by that well. Factors to consider when estimating reasonable drawdown include well construction, pump size and flow rate, pump depth setting, and well specific capacity.

Offsite Well A and Offsite Well B are the only non-Project wells within the effective limits of the groundwater storage reservoir, based on the County records and DWR database search. Offsite Well A (49 feet deep) is approximately 2,400 feet closer to the proposed construction water wells than Offsite Well B (155 feet deep), and has the potential for water level impacts from the Project. Mitigation measures that address water level impacts to Offsite Well A will also mitigate potential water level impacts to Offsite Well B.

The technical justification for a reasonable drawdown at Offsite Well A, for which impacts would be measured and mitigation implemented, includes the following assumptions:

- The well is 49 feet deep with the bottom 20 feet screened in the fractured shale groundwater reservoir.
- The pump is set 5 feet above the well bottom, with an additional 5 feet of water column above the pump required (10 feet minimum water column).
- Static water level is 20 feet deep under existing conditions (close to the invert of San Miguelito Creek).
- Aquifer transmissivity and well specific capacity is similar to nearby O&M Well CW2, adjusted for the aquifer thickness tapped by each well.
- A nominal discharge capacity for the well pump of 1-2 gallon per minute (gpm) needs to be maintained. This is sufficient to provide a few hundred gallons per day, and supplements the developed Ranch Spring, which will not be impacted by Project water use. Additional yield from Offsite Well B would also be available.

Using these assumptions, the 12-hour specific capacity of Offsite Well A is estimated at 0.4 gpm per foot of drawdown, and therefore would require up to 5 feet of drawdown during a 12-hour pumping cycle at 2 gpm. In order to maintain a 1-2 gpm flow rate with adequate water above the pump, the maximum reasonable drawdown due to Project water use before significant impacts to Offsite Well A occur is estimated to be 14 feet².

² The exiting water column is assumed to be 29 feet (49 feet well depth – 20 feet depth static level). A reasonable drawdown of 14 feet would reduce the water column to 15 feet (29 feet existing conditions – 14 feet reasonable drawdown = 15 feet). An additional 5 feet of pumping water level drawdown would maintain 10 feet of water column in the well.



Monitoring of water level drawdown in the vicinity of Offsite Well A will be performed at a designated monitoring well to be constructed on Project property across San Miguelito Road, as close as possible to Offsite Well A (Figure 1). The monitoring well will be equipped with a pressure transducer that will provide detailed water level trends and allow the Project applicant (and County) to anticipate impacts at Offsite Well A before they occur.

Mitigation Measures

Recommendations for mitigation measure MM WAT-1 (Construction Water Source) were provided in previous correspondence³. Based on the comments received from the County, revised mitigation measures are recommended as follows:

- a) Allow use of on-site wells for construction water.
- b) Require the Applicant to construct a monitoring well in order to monitoring water levels within the aquifer. The monitoring well will be equipped with an automatic water level recorder (e.g. pressure transducer).
- c) Water levels in the monitoring well will be recorded hourly by the pressure transducer and will be reported to the County on a bi-weekly basis during the first six months of construction, and monthly thereafter until three months following the end of construction, or as agreed to between the Applicant and the County. Water level data reported to the County will include an interpretation of water level trends and anticipated construction activity and water use. The reporting interval would change from bi-weekly to weekly if water level declines in the monitoring well exceed 7 feet (half of the reasonable drawdown threshold).
- d) If water level trends at the monitoring well indicate that a drawdown of 14 feet or more is anticipated at any time during the course of construction water use, the Applicant with concurrence from the County will either:
 - Adjust and/or reduce construction well production to the extent feasible to avoid water levels reaching the reasonable drawdown threshold of 14 feet, or
 - b. Provide water of suitable quantity and quality, as needed, to replace any loss in production at the well. The Applicant would be responsible for the costs and transportation of water to the existing tank(s) in order to provide the required quantity of supplemental water.

³ CHG, Comments on Draft SEIR for Strauss Wind Energy Project, Lompoc, Santa Barbara County, May 21, 2019



Note that the recommended mitigation for significant impact to Offsite Well A are acceptable industry practices. These measures would also ensure that the traffic and air quality impacts of trucking in construction water would be avoided.

Potential Impacts to Frick Springs

Frick Springs consists of developed springs that are part of the water system for the City of Lompoc. These springs are located along the formation contact between the Monterey Formation and the Sacate Formation (Figure 1), approximately $\frac{3}{4}$ miles from the construction water wells. The approximately elevations of the individual springs at Frick Springs range from 900-950 feet above sea level and are 50-100 feet above the adjacent invert elevation of San Miguelito Creek (i.e. the springs are at greater pressure head than the creek). The geologic structure in the Monterey Formation approaching Frick Springs consists of steeply dipping and tightly folded beds (Figure 4), which would transmit groundwater preferentially along a northwest-southeast direction (parallel to the fold axis) and restrict groundwater flow in the direction of the groundwater storage reservoir shown in Figure 1. Given the distance from the construction water wells, elevation relative to the creek, and geologic structure surrounding Frick Springs, the Project's use of the construction water wells are not expected to impact the Frick Springs water system.

Thresholds of Significance

The Santa Barbara County Environmental Thresholds and Guidelines Manual, last revised in February 2018, "has been prepared to assist the public, the applicant, environmental consulting firms, and County decision makers in understanding the use and application of various environmental thresholds as they relate to project proposals" (pg. 1).

Chapter 2 (Rules for Use and Criteria for Amendment) of the Environmental Thresholds and Guidelines Manual states: "A project which has no effect above threshold values individually or cumulatively shall be determined not to have any significant effect, and a negative declaration shall be prepared as provided in Article IV. Projects which have a potential effect above a threshold of significance will require an EIR" (pg. 3). Furthermore, "Thresholds of significance are intended to supplement provisions in the State Guidelines for determination of significant environmental effect including Sections 15604, 15605, 15382 and Appendix G incorporated herein" (pg. 2).

In general, thresholds of significance are intended to be used during the Initial Study phase of project review to help determine whether a negative declaration is, or is not, appropriate. Since the Strauss Wind Energy Project is already subject to an environmental impact analysis (no negative declaration), use of thresholds of significance for the intended purpose is not needed.



With respect to groundwater use by the Project, "The Threshold of Significance for consolidated rock ("bedrock") aquifers is considered the amount of new pumpage by a proposed project, which would place the aquifer in a state of overdraft" (pg. 85). A state of overdraft can occur when "The amount by which the average long term demand on a basin exceeds the safe yield of the basin after allowances are made for return flows" (page 76). Finally, the safe yield of a basin is defined as "The maximum amount of water which can be withdrawn from a basin (or aquifer) on an average annual basis without inducing a long-term progressive drop in water level" (pg. 76). The average long term operating demand for the Project is estimated to be 250 gallons per day, equivalent to 0.28 acre-feet per year. Given the minimal long-term Project water use, and the relatively undeveloped condition of the groundwater reservoir, the threshold of significance for consolidated rock aquifers will not be exceeded under project conditions.

No. HG 633

Respectfully submitted,

CLEATH-HARRIS GEOLOGISTS

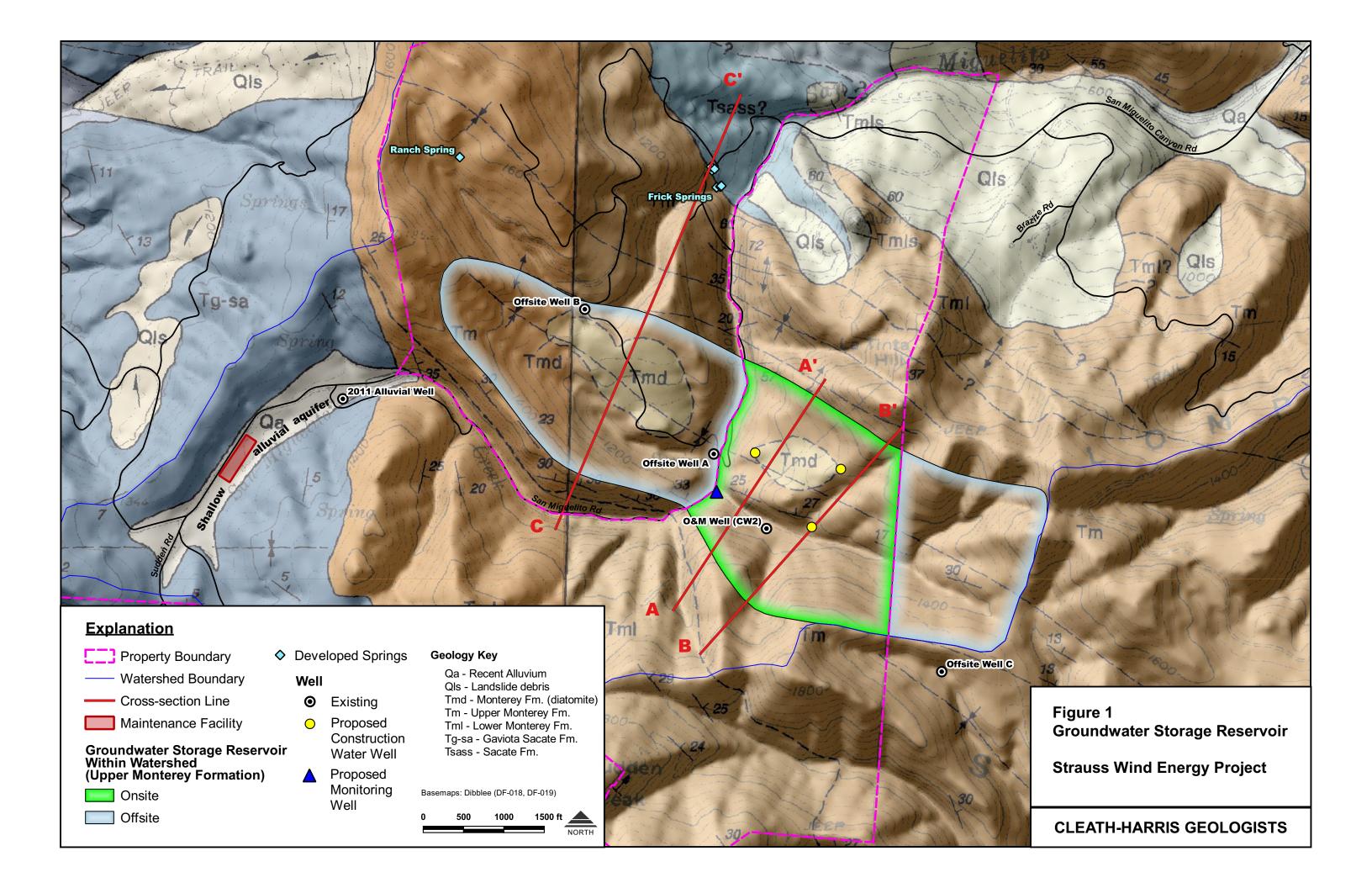
Spencer J. Harris, HG 633 Senior Hydrogeologist

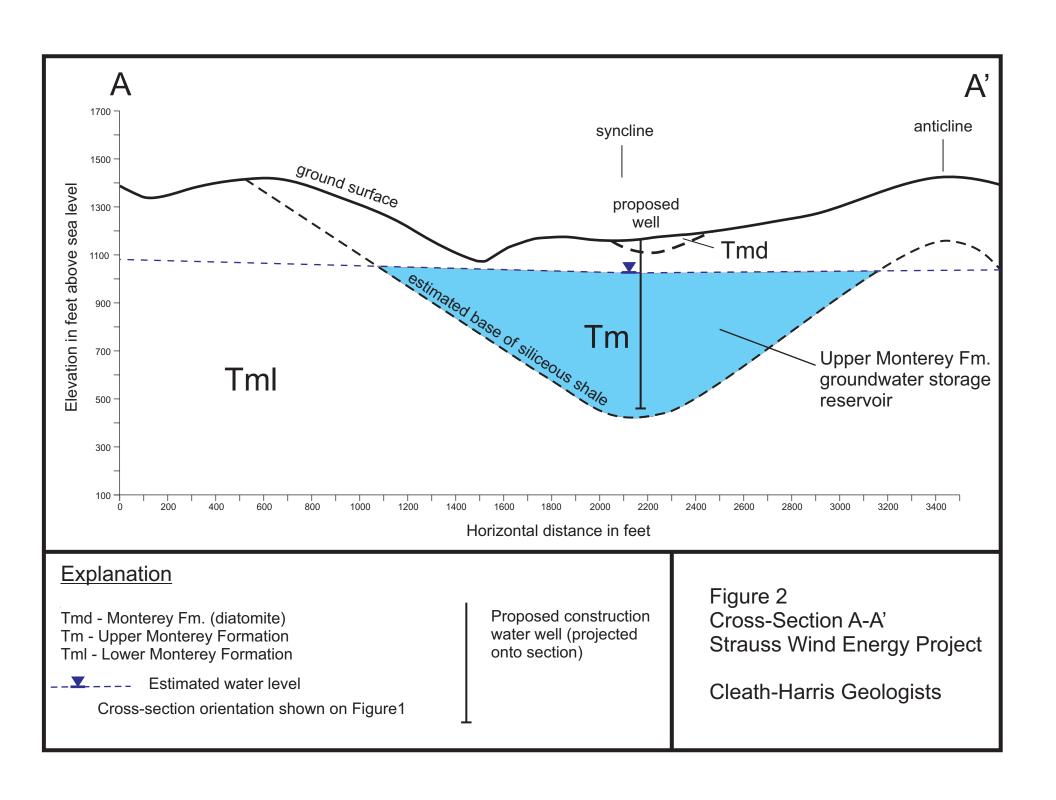
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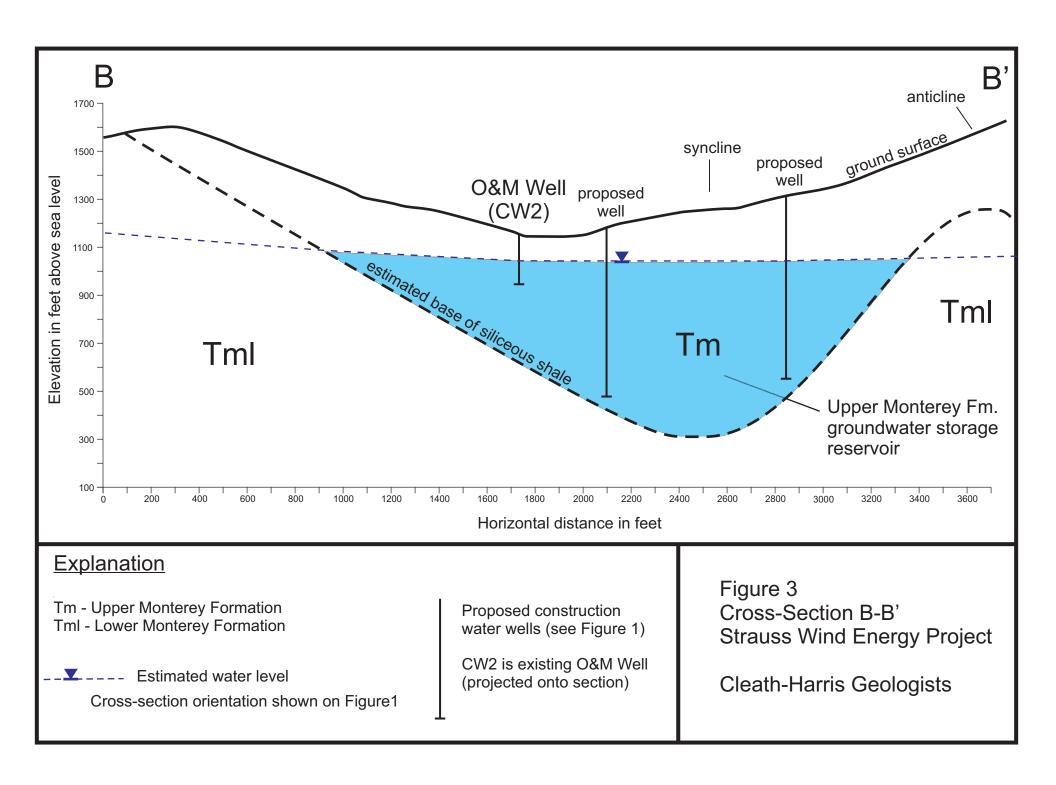


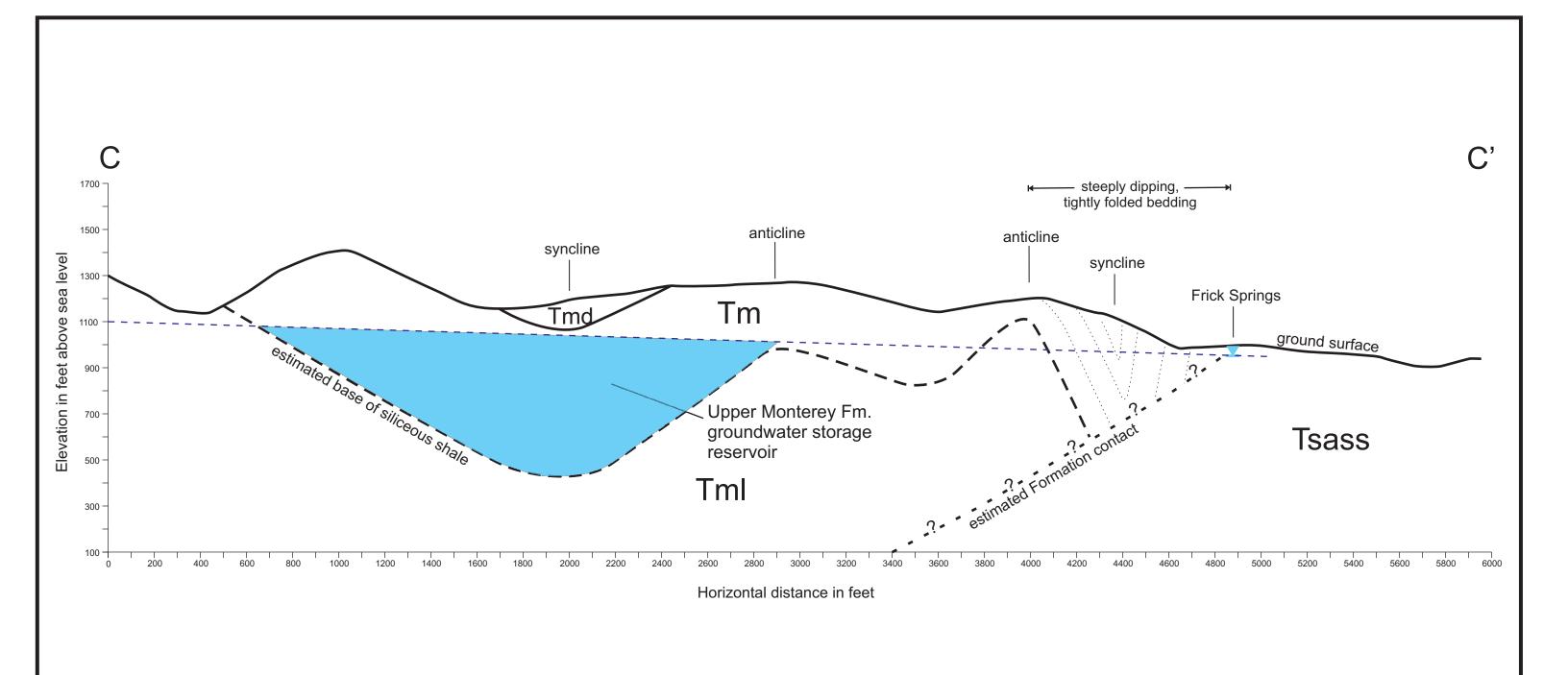
ATTACHMENTS

Figures 1-4
Offsite Well A - Well Permit Field Record
Offsite Well B – Well Permit Field Record
DWR Well Log #40446
DWR Well Log #E0094758









Explanation

Tmd - Monterey Fm. (diatomite)
Tm - Upper Monterey Formation
Tml - Lower Monterey Formation
Tsass - Sacate Formation

Cross-section orientation shown on Figure1

Figure 4 Cross-Section C-C' Strauss Wind Energy Project

Cleath-Harris Geologists

Offsite Well A

Permit No. 102766 Page _____of ___ pages

ENVIRONMENTAL HEALTH DIVISION SANTA BARBARA COUNTY HEALTH CARE SERVICES WELL PERMIT FIELD INVESTIGATION RECORD

Well Permit Application Received: Date	= 312+103
Site Investigation By Kashy Can	dul Date 3/27-103
Findings: (Check applicable boxes and o	
Overhead Power Lines Sewer Lines	Creek or Watercourse
Leach Field	Petroleum Tank or Pipeline
Cesspool/Drywell	Other
AP -OK	
Sofe Cheen - OK	
Application Reviewed and Approved: By	<u>AC.</u> Date 3127-103.
Work Investigation Record	
Date 4//8/03	Well Site #: 2 2
Casing Information	Borehole
Type: Steel PVC Other	Total Depth of Well: 49
Class/Gage/NSF:	Annular Seal Depth: 22
ASTM#:	Well Bore Diameter: /5/
Diameter: 6" Total Depth: 49"	Sealing Material: (o Salk Comed
Casing Schedule	Amount: 22 4ds.
0' - 29' = Blank	Method of Pour: Gravity
	Use of Tremie: ///
	Driller(s): Ron Taylon
	Drilling "
Comments: Ste #1 Corp on	
Final Inspection and Approval/Denial: E	By Karly (and Date 4/18/03.
Notice of Work Acceptance/Rejection Sen	it to Well owner On 4 / 2// 03
W-320P Rev. 12/89	

(SR : 4/23/03)

Permit No. SUDIO 794
Page of pages

Offsite Well B

ENVIRONMENTAL HEALTH DIVISION SANTA BARBARA COUNTY HEALTH CARE SERVICES WELL PERMIT FIELD INVESTIGATION RECORD

Well Permit Application Received: Date	4//3/03
Site Investigation By Kaylag Ca	10/el Date 3/07/03
Findings: (Check applicable boxes and g	ive clearance)
Overhead Power Lines	Animal Enclosure
Sewer Lines	Creek or Watercourse
Leach Field	Petroleum Tank or Pipeline
Cesspool/Drywell	Other
Site cheek OK	
Application Reviewed and Approved: By_	Kishy (uch) Date 4/17/03
Work Investigation Record	•
Date 4/18/03	Well Site #: 2 of 2
Casing Information	Borehole
Type: Steel PVC Other -	Total Depth of Well: /55
Class/Gage/NSF:	Annular Seal Depth: 30'
ASTM#:	Well Bore Diameter: ////
Diameter: 6 / Total Depth: 155 /	Sealing Material: lo Sach Consul
Casing Schedule	Amount: <u>22 y ds</u> .
0', -55', = Jalank	Method of Pour: 6 10 10
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	Driller(s): Lon Juylo 1101
	Dollas
Comments: Can on 876	
Final Inspection and Approval/Denial: By	Katherlander Date 41 18103
Notice of Work Acceptance/Rejection Sent	
V-320P Rev. 12/89	

File Original, Duplicate and Triplicate with the REGIONAL WATER POLLUTION

CONTROL BOARD No. 3.

WATER WELL DRILLERS REPORT (Sections 7076, 7077, 7078, Water Code)

Do	Not Fill In
No	40446
- ·	

STATE OF CALIFORNIA

T.A. o	#0##0 :
State Well No	06 N/34W-19
Other Well No.	
Oction A cir 2 (or	***************************************

(1) OWNER: plots near location of	(11) WELL LOG:
Nama	Total depth 47 ft. Depth of completed well ft.
Addres Offsite "Well A" but no	Formation: Describe by color, character, size of material, and structure,
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well constructed	10 2/ VC 10 C' 00
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	FOR PUBLIC RELEASE
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New well - Deepening Reconditioning Abandon	
If abandonment, describe material and procedure in Item 11.	10 10 10 10 10 10 10 10 10 10 10 10 10 1
(4) PROPOSED USE (check): (5) EQUIPMENT:	
Domestic Industrial Municipal Rotary	() () () () () () () () () ()
Cable The Cable	711 (1
Irrigation Test Well Other Dug Well	
(6) CASING INSTALLED: If gravel packed	
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te transfer to the second seco	Maria de Mar
Method of Sealing	Work started 19 , Completed 19
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(9) WATER LEVELS:	This well was drilled under my jurisdiction and this report is true to the best of
Depth at which water was first found ft.	my knowledge and belief.
ading level before perforating ft.	NAME (Person, firm, or corporation) (Typed or printed)
nding level after perforating ft.	· I and a second secon
Anta Samuel Mariane	Address 11% work with the wife of the second
(10) WELL TESTS:	
Was a pump test made? 🔲 Yes 📋 No If yes, by whom?	
Yield: gal./min. with ft. draw down after hrs.	[SIGNED] Committee State Company Committee
Temperature of water Was a chemical analysis made? 🗌 Yes 📋 No	License No. 1723 Dated Unit 1961
Was electric log made of well? Yes No	93689 3-54 50M QUIN (9) SPO DWR FORM NO. 246 (REV. 3-54)

			e used to view		this form.	However, :	software me	ust be purchase	ed to comple	ete, save,	and reuse	e a saved fo	m.					
File Orig	File Original with DWR $O6N34W29$ State of Califo																	
Page 1	Page 1 of 1 Well Completion							on Repo	rt		1	1 1						
Owner's	Page 1								Î			e Well Nun	ber/Site	e Number				
Date Wo	Date Work Began 07/07/2009 Date Work Ended 7/14/2009								. 1		Latitude	- N		Longitude				
Local Pe	_ocal Permit Agency Santa Barbara County																	
Permit N	Permit Number <u>SR # 0106570</u> Permit Date <u>7/9/09</u>								L			APN/T	RS/Othe	er				
Sai 3	Geologic Log								. /		Well	Owner		m deale said.				
Orie	entation	Vertice	cal O Hori		OAngle	Specify	y	3										
Drilling	Method_R	OTARY	The major them to the second			uid MUD		_ (Offsite	Wel	1 C							
Depth	from Sur	face	Desc	Desc	ription.	color etc	and The said			, , , , C1								
Depth from Surface Peet to Feet Describe material, grain size, color, etc TOP SOIL									Well Location									
3	15		AY & GRAV	/ELS				Address Off Jalama Beach Road - Tinta Well #6										
15	18		RM LIGHT E		AY			City Lompoc County Santa Barbara										
18	21		ROWN CLAY			EL												
21	35		ROWN SHAL					Latitude N. Longitude W Deg. Min. Sec. Deg. Min. Sec.										
35	45		ROWN CLAY		<u> </u>			Datum Decimal Lat Decimal Long										
45	520	FF	RACTURED	BROWN S	SHALE			APN Book 083 Page 260 Parcel 012										
		· ·			-			Township	<u> </u>	Range		tariba	Sectio	on				
1			······································						Locati	on Ske	tch							
			,					(Sketch m	nust be drawn	by hand aff North	er form is	orinted.)		w Well				
<u> </u>		T	ne Air Lift Te	st is only a	pproxima	ate. A Te	est Pump	<u>, </u>		North	(4.2		O Modification/Repair					
					· · · · · · · · · · · · · · · · · · ·	ccurate account. (WP)				".		1	O Deepen O Other					
							, , ,	- 10 m	No.	ie			O De	estroy scribe procedures and materials				
								1 1. * .				1	un	der "GEOLOGIC LOG"				
<u> </u>								7 1/2 gr	1000	, 194 Se			2.05	Planned Uses				
							1.5		dete			i		ater Supply				
	<u> </u>						·. · · · · · · · · · · · · · · · · · ·	□ Domestic □ Public If Irrigation □ Industr										
							18 18 B											
l								O Cathodic Protection O Dewatering										
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					\$ 5g.	Y		, 11 0	•			i i		emediation				
							Υ	O Sparging										
					,			South O Test Well O Vapor Extraction										
l				1.79		- C.		Histrate or describe distance of well from roads, buildings, fences, rivers, etc. and attach a map. Use additional paper if necessary.										
·		·		7		-		Please be acc	Please be accurate and complete.									
 			~80k5 W.	1876	·-	وما كومين		Water Level and Yield of Completed Well										
			200	,			565	Depth to first water (Feet below surface)										
<u> </u>	<u> </u>						-i-	Depth to Static Water Level 170 (Feet) Date Measured 07/10/2009										
Total	Depth of B	orina 	520	- 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1		Feet		Estimated Yield * 100 (GPM) Test Type Air Lift										
ł		7				 , 1		Test Length 6.0 (Hours) Total Drawdown (Feet)										
Total [Depth of C	ompleted	Well <u>513</u>		7 7	Feet		*May no	t be repres	entative	of a wel	l's long te	rm yiek	d.				
[8,70°]	40°		NAC APE	Cas	ings			M. A. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1.	j	*		Annul	ar Mat	terial				
	h from	Borehol		Mate	rial .	Wall	Outside		Slot Size		h from rface	Fil		Description				
	rface to Feet	Diamete (Inches)			,	(Inches)	Dlameter (Inches)	т Туре	If Any (inches)		rrace to Feet		1	Description				
0	58	18	Conductor	F-480 PVC		SDR 21	12			0	58	CEMENT						
0	233	11	BLANK	F-480 PVC		SDR 21				58	513	FILL		Monterey Mix				
233	513	11 *	SCREEN	F-480 PVC		SDR 21	6	ļ	0.040	I		_						
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<u></u>			7 "				<u> </u>			<u> </u>								
		Attach	ments	and A	,,,	<u> </u>			Certificat					In-adam ** ** **				
	Geologic				I, the un	dersigned Filingoni	d, certify the & Thomas	nat this report pson Drilling	at this report is complete and accurate to the best of my knowledge and belief son Drilling, Inc.									
	Well Cor		-		·	Person,	Firm or Corp	oration	ration									
	Geophys Soil/Mat		s) cal Analyses		<u> P.O. E</u>	30x 845	Address	Atascadero City State Zip										
	Other	ei Oneini	vai AlialySCS		Signed		2 <u>.</u>	Chon	~~ ~			-09 4	32680	<u> </u>				
	Iditional infor	mation, i it e	exista.		<u> </u>	C-57 Lic	ensed Water	or Well Contractor Date Signed C-57 License Number										
DWR 188	DWR 188 REV. 1/2006 IF ADDITIONAL SPACE IS NEEDED, USE NEXT CONSECUTIVELY NUMBERED FORM																	

408/25/09