## Appendix G

## Traffic Impact Analysis (Kd Anderson)

# TRAFFIC IMPACT ANALYSIS 

# FOR <br> RECOLOGY HAY ROAD LANDFILL EXPANSION PROJECT <br> Solano County, CA 

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## RECOLOGY HAY ROAD LANDFILL EXPANSION PROJECT TRAFFIC IMPACT ANALYSIS

## TABLE OF CONTENTS

EXECUTIVE SUMMARY ..... I
INTRODUCTION ..... 1
Study Purpose and Objectives ..... 1
Project Description ..... 1
EXISTING SETTING ..... 3
Study Area ..... 3
Study Area Roadways .....  3
Study Area Intersections .....  3
Level of Service ..... 5
Roadway Segment Level of Service ..... 6
Existing Traffic Conditions ..... 8
Non-Automobile Transportation ..... 11
Existing Plus Project Conditions ..... 12
Existing Plus Project Level of Service Impacts ..... 19
CUMULATIVE IMPACTS ..... 22
Year 2030 Traffic Forecasts and Lane Configurations ..... 22
2030 Conditions ..... 22
2030 Plus Project Level of Service Impacts ..... 26
TEMPORARY BALE STORAGE OF RECYCLABLE MATERIALS ..... 30
MITIGATION MEASURES ..... 31
Existing Conditions ..... 31
Existing Plus Project Conditions ..... 31
2030 Conditions ..... 31
2030 Plus Project Conditions ..... 32
REFERENCES ..... 34
APPENDIX ..... 35

# RECOLOGY HAY ROAD LANDFILL EXPANSION PROJECT TRAFFIC IMPACT ANALYSIS 

## EXECUTIVE SUMMARY

Project Description. This study evaluates the traffic impacts associated with amending the existing Conditional Use Permit (CUP) to reflect changes requested for the Recology Hay Road Landfill site in Solano County. The Recology Hay Road Landfill is located in the southwest quadrant of the SR 113 / Hay Road intersection in Solano County. Access to the site is from Hay Road just west of SR 113. The project will revise the existing daily tonnage limit and establish a new peak limit as well as an average daily limit. The existing CUP allows for 2,400 tons per day (tpd) of landfill disposal. Occasionally, the site has received more than $2,400 \mathrm{tpd}$ requiring the site to turn away vehicles so as to not exceed the existing peak limit. The project would amend the CUP to allow a peak day limit of 3,400 tpd with a 7 -day average limit of $3,200 \mathrm{tpd}$. This will allow the site to not have to turn away haulers.

Existing Setting. Levels of Service were evaluated for eight intersections and six roadway segments to provide a baseline analysis to meet CEQA criteria. The intersection locations included intersections between the I-80 / Midway Road interchange, and along Midway Road and SR 113. The analysis included a.m. and p.m. peak hours at all intersections and included a Saturday peak hour analysis at four intersections closest to the site. Sunday traffic was reviewed at the project site and was consistently lower than Saturday traffic; therefore, the weekend analysis included only Saturday.

The six roadway segments considered included three along SR 113, two along Midway Road and one along Hay Road. County Level of Service policy considers LOS C as the acceptable threshold while Caltrans policy considers LOS D as the acceptable threshold.

The SR 12 / SR 113 intersection currently operates at LOS E in the a.m. peak hour and LOS F in the p.m. peak hour. Caltrans has an identified safety project that would construct a single lane roundabout at this intersection. Construction is slated to be completed Fall 2019. Under the roundabout condition the intersection will operate at LOS A in the a.m. peak period ( 7.0 spv ) and LOS C in the p.m. peak hour ( 18.8 spv ). The remaining intersections and roadway segments operate within the Caltrans and County LOS thresholds.

No additional recommendations are noted.
Existing Plus Project Specific Impacts. Under Existing plus Project conditions, all intersections except the SR 12 / SR 113 intersection will operate within acceptable County and Caltrans LOS thresholds. The SR 12 / SR 113 intersection will continue to operate at LOS E in the a.m. peak hour and LOS F in the p.m. peak hour. As identified under Existing Conditions

Caltrans has an identified safety project that would construct a single lane roundabout at this intersection. With this project completed the intersection will operate at LOS A in the a.m. peak hour (7.1 spv) and LOS C in the p.m. peak hour (19.1 spv). All roadways will continue to operate within the Caltrans and County LOS thresholds.

No additional mitigations are necessary.
2030 Conditions. Under 2030 conditions, the SR 113 / Midway Road intersection will decline to an LOS E condition in the a.m. peak hour ( 45.7 spv ) and LOS F condition in the p.m. peak hour ( 53.6 spv ). The intersection will not meet the peak hour traffic signal warrant. The SR 12 / SR 113 intersection will decline to LOS F in the p.m. peak hour (124.4 spv). One roadway segment, Midway Road between the I-80 Eastbound Ramps intersection and Porter Road will decline to LOS D in both directions. The remaining intersections and roadway segments will operate within County and Caltrans LOS thresholds.

The following recommendations are made:

## Recommendations:

- SR 113 / Midway Road: Installation of all-way stop control will improve the level of service to LOS B in both a.m. (13.3 spv) and p.m. ( 13.7 spv ) peak hours. Caltrans has identified a conceptual project to widen shoulders, construct a median and install a traffic signal at the SR 113 / Midway Road intersection to enhance safety; however, this project is not yet included in a planning or programming document.
- SR 12 / SR 113: Installation of a second eastbound lane through the roundabout will improve the level of service to a LOS C ( 21.5 spv ) condition in the p.m. peak hour. No agencies with jurisdiction currently have plans for any improvements at this intersection.
- Midway Road - I-80 Eastbound Ramps to Porter Road (both directions): A 0.30 mile long passing lane in both eastbound and westbound directions would be needed to improve the roadway segment to an acceptable level of service, LOS C (EB ATS - 45.1 / PTSF - 52.8; WB ATS - 45.3 / PTSF - 43.0). No agencies with jurisdiction currently have plans for any improvements at this intersection.

No additional recommendations are noted.
2030 Plus Project Conditions. The SR 113 / Midway Road intersection and the SR 12 / SR 113 intersection will continue to operate below the Caltrans LOS D threshold. Additionally, both directions of Midway Road, between the I-80 Eastbound Ramps intersection and Porter Road will operate at LOS D. The remaining intersections and all roadway segments will operate within County and Caltrans LOS thresholds. The following mitigations are made:

## Mitigations:

- SR 113 / Midway Road: As identified in the 2030 No Project Recommendations installation of all-way stop control will improve the level of service to LOS B in both a.m. ( 13.7 spv ) and p.m. ( 13.8 spv ) peak hours. This intersection is under the jurisdiction of Caltrans, and Caltrans has identified a conceptual project to widen shoulders, construct a median and install a traffic signal at the SR 113 / Midway Road intersection to enhance safety. However, this project is not yet included in a planning or programming document. Any improvement of the intersection would require Caltrans concurrence and approval. The project applicant and Solano County shall coordinate with Caltrans on implementation of this improvement. However, because the final approval of the proposed improvement is outside the jurisdiction and control of the Applicant and County, there is no guarantee that this mitigation measure would be implemented prior to project-related trips occurring at this intersection. Therefore, this is considered a significant and unavoidable impact.
- SR 12 / SR 113: As identified in the 2030 No Project Recommendations installation of a second eastbound lane through the roundabout will improve the level of service to a LOS $\mathrm{C}(21.7 \mathrm{spv})$ condition in the p.m. peak hour. This improvement is under the jurisdiction of Caltrans. Any improvement of the intersection would require Caltrans concurrence and approval. The project applicant and Solano County shall coordinate with Caltrans on implementation of this improvement. However, because the final approval of the proposed improvement is outside the jurisdiction and control of the Applicant and County, there is no guarantee that this mitigation measure would be implemented prior to project-related trips occurring at this intersection. Additionally, Caltrans does not currently have plans for any improvements at this intersection. Therefore, this is considered a significant and unavoidable impact.
- Midway Road - I-80 Eastbound Ramps to Porter Road (both directions): As identified in the 2030 No Project Recommendations a 0.30 mile long passing lane in both eastbound and westbound directions would be needed to improve the roadway segment LOS to an acceptable level of LOS C (EB ATS - 45.0 / PTSF - 53.2; WB ATS - 45.2 / PTSF 43.7). This improvement is under the jurisdiction of Solano County. The project applicant shall coordinate with Solano County and shall fund the improvement of this segment to be constructed prior to vehicle trips to the landfill exceeding 2,400 per day. Therefore, with mitigation, this is considered a less-than-significant impact.

No additional mitigations are identified.

# RECOLOGY HAY ROAD LANDFILL EXPANSION PROJECT TRAFFIC IMPACT ANALYSIS 

## INTRODUCTION

## Study Purpose and Objectives

This study evaluates the traffic impacts associated with amending the existing Conditional Use Permit (CUP) to reflect changes requested for the Recology Hay Road Landfill site. Regarding traffic related issues the project proposed to revise the existing daily tonnage limit and establish a new peak limit as well as an average daily limit. The existing CUP allows for 2,400 tons per day (tpd) of landfill disposal. Occasionally, the site has received more than 2,400 tpd requiring the site to turn away vehicles so as to not exceed the existing peak limit. The project would amend the CUP to allow a peak day limit of $3,400 \mathrm{tpd}$ with a 7 -day average limit of $3,200 \mathrm{tpd}$. This will allow the site to not have to turn away haulers.

The study parameters are consistent with Solano County guidelines. The study addresses the following traffic scenarios:

1. Existing (2018) Peak Hour Traffic Conditions;
2. Existing plus Project Peak Hour Traffic Conditions;
3. Year 2030 Peak Hour Traffic Conditions;
4. Year 2030 plus Project Peak Hour Traffic Conditions;

The focus of this study is to identify project-related impacts under long-term conditions as a result of accepting an additional 1,718 tpd at the site, which is the difference between existing tonnage received at the landfill and allowable tonnage to be received under the proposed CUP amendments. Analysis of an Existing condition is required to address the requirements of Sections 15125 of the State CEQA Guidelines, "an EIR must include a description of the physical environmental conditions in the vicinity of the project, as they exist at the time the notice of preparation is published, or if no notice of preparation is published, at the time environmental analysis is commenced, from both a local and regional perspective."

## Project Description

The Hay Road Landfill is located east of the City of Vacaville in Solano County. The site is located in the southwest quadrant of the SR 113 (Rio Dixon Road) / Hay Road intersection. The project will modify the previously approved Hay Road Landfill Expansion project. From a transportation perspective the proposed project will modify the existing daily limit to accept up to 3,400 tpd with an average of 3,200 tpd over a 7-day period.

Access to the site facility will remain unchanged, via its access along Hay Road. Figure 1 illustrates the location of the site relative to the surrounding areas of Solano County.


Source: Doug Brown 2012

## EXISTING SETTING

## Study Area

This study addresses traffic conditions in the vicinity of the Hay Road Landfill project site, including the project routes from the Interstate 80 (I-80) / Midway Road interchange to the north and from the SR 113 / SR 12 intersection to the south. Six roadway segments were analyzed along with eight intersections along the routes providing access to the landfill site. The text that follows describes the facilities included in this analysis.

## Study Area Roadways

State Route 113. State Route (SR) is a two-lane road between in Solano County beginning at SR 12 in the south and heads north past I-80, continuing through Davis and Woodland to its terminus in Sutter County. Between SR 12 and Midway Road, the road has varying shoulder widths, ranging from about $10^{\prime}$ at intersections to 0 ' within the segments. The speed limit is 55 miles per hour (mph). SR 113 is identified in Solano County as a major arterial.

Midway Road. Midway Road is a two-lane road providing east-west access west of I-80 and east beyond the SR 113 intersection. The road has varying shoulder widths, ranging between 0 and 8 feet. The speed limit is 55 miles per hour ( mph ). Midway Road is identified in Solano County as a County Route of Regional Significance.

Hay Road. Hay Road is a two-lane local road running east-west between Meridian Road and SR 113. The road has minimal shoulder widths, ranging between 0 and 2 feet. The speed limit is 55 miles per hour (mph). Hay Road is identified in Solano County as a collector road.

## Study Area Intersections

The quality of traffic flow is typically governed by the operation of major intersections. Eight intersections serving this site were identified for evaluation. These include:

1) I-80 Westbound Ramps / Oday Road
2) Midway Road / Oday Road
3) I-80 Eastbound Ramps / Midway Road
4) Midway Road / Porter Road
5) SR 113 / Midway Road
6) SR 113 / Hay Road
7) SR 113 / SR 12
8) Hay Road / Project Entrance
A.m. and p.m. mid-week peak hour counts were conducted at each of these intersections in late January and early February 2018. Traffic counts were also conducted at intersections 5 through 8 for the Saturday mid-day peak period in late January 2018. New counts were also conducted at intersections 1 through 3 in early October 2018; the I-80/Midway Road interchange has been
reopened since July 2018 after being replaced. The Midway Road interchange is the designated truck route for the site.

Each study intersection is described below:
I-80 Westbound Ramps / Oday Road is a tee intersection with a hook on/off ramp. The intersection is stop controlled along the I-80 off-ramp approach. The Oday Road approaches consist of single lanes providing shared through and left or right turn right turn movements. The westbound off-ramp includes a left turn lane under stop control and a short right turn lane under yield control.

Midway Road / Oday Road is an unsignalized tee intersection. Stop control is provided along Oday Road. Westbound Midway Road includes a through lane with a free right turn lane onto Oday Road. Eastbound Midway Road includes a shared through-left lane while Oday Road consists of a single lane approach.

The Midway Road / I-80 Eastbound Ramps intersection is an unsignalized diamond configuration (L-1). Both directions of Midway Road consist of a single lane with the eastbound approach providing a shared through left lane and the westbound approach providing a shared through-right lane. Stop control exists along the I-80 off-ramp for through and left turn movements while the right turn movement merges onto eastbound Midway Road.

The Midway Road / Porter intersection is an unsignalized tee intersection. Eastbound Midway Road bypasses the Porter Road intersection while westbound Midway Road tees into Porter Road. The westbound left turn is stop controlled while the right turn is yield controlled. The northbound and southbound approaches along Porter Road allow only through movements.

The SR 113 / Midway Road intersection is an unsignalized four-way intersection with stop control along Midway Road. The SR 113 approaches include left turn lanes and a shared through-right lane while Midway Road consists of a single lane.

The SR 113 / Hay Road intersection is an unsignalized tee intersection with stop control along Hay Road. All approaches are single lanes.

The SR 12 / SR 113 - Birds Landing Road intersection is an unsignalized four-way intersection with stop control along SR 113. The SR 12 approaches include a left turn lane, a through lane and a right turn lane. Both the northbound Birds Landing Road approach and the SR 113 approach include a shared through-left lane and a right turn lane. Caltrans has an identified safety project that would construct a single lane roundabout at this intersection. Construction is slated to be completed Fall 2019.

The Hay Road / Project Access intersection is an unsignalized tee intersection with stop control along the project access. Westbound Hay Road includes a through lane and a left turn lane while the eastbound approach includes a shared through-right lane. The project entrance is unstriped but wide enough to allow both right and left turning vehicles to queue.

## Level of Service

To assess the quality of existing traffic conditions and provide a basis for analyzing project impacts, Levels of Service were calculated at study area intersections and project driveways. "Level of Service" is a qualitative measure of traffic operating conditions whereby a letter grade "A" through " F ", corresponding to progressively worsening operating conditions, is assigned to an intersection or roadway segment.

The Level of Service policies of Solano County and Caltrans govern this analysis. The Solano County Road Standards documents the County's policies for Level of Service in rural and urban areas. The document notes that LOS C is the design standard for the County.

Caltrans has set a minimum Level of Service standard of LOS D in rural areas, populations less than 2,500 and LOS E in urban clusters (populations 2,500 to 49,999) and LOS E in urbanized areas (populations over 50,000 ) for state highways. These standards may vary depending on the corridor conditions. For this project LOS D is considered the significance threshold.

Various methodologies exist to determine operating Levels of Service at signalized intersections. The available techniques vary with regard to factors such as traffic signal timing, interaction between adjoining signals, etc. The procedures contained in the 2010 Highway Capacity Manual have been used for determining operating Level of Service at signalized intersections.

At unsignalized intersections the number of gaps in through traffic, gap acceptance time and corresponding delays for motorists waiting to turn are used for Level of Service analysis. Procedures used for calculating unsignalized intersection Level of Service are as presented in the Highway Capacity Manual, 2010 Edition.

Table 1 presents general characteristics associated with each Level of Service grade.

TABLE 1
LEVEL OF SERVICE DEFINITIONS

| Level of Service | Signalized Intersection | Unsignalized Intersection | Roadway (Daily) |
| :---: | :---: | :---: | :---: |
| "A" | Uncongested operations, all queues clear in a single-signal cycle. <br> Ave Delay $\leq 10$ seconds per vehicle | Little or no delay. <br> Ave Delay $\leq 10 \mathrm{sec} / \mathrm{veh}$ | Completely free flow. |
| "B" | Uncongested operations, all queues clear in a single cycle. Delay > 10 $\mathrm{sec} / \mathrm{veh}$ and $\leq 20 \mathrm{sec} / \mathrm{veh}$ | Short traffic delays. <br> Delay > $10 \mathrm{sec} / \mathrm{veh}$ and $\leq 15 \mathrm{sec} / \mathrm{veh}$ | Free flow, presence of other vehicles noticeable. |
| "C" | Light congestion, occasional backups on critical approaches. Delay >20 sec/veh and <35 sec/veh | Average traffic delays. Delay > $15 \mathrm{sec} /$ veh and $\leq 25 \mathrm{sec} / \mathrm{veh}$ | Ability to maneuver and select operating speed affected. |
| "D" | Significant congestions of critical approaches but intersection functional. Cars required to wait through more than one cycle during short peaks. No long queues formed. Delay $>35 \mathrm{sec} / \mathrm{veh}$ and < $55 \mathrm{sec} / \mathrm{veh}$ | Long traffic delays. <br> Delay > $25 \mathrm{sec} / \mathrm{veh}$ and $\leq 35 \mathrm{sec} / \mathrm{veh}$ | Unstable flow, speeds and ability to maneuver restricted. |
| "E" | Severe congestion with some long standing queues on critical approaches. Blockage of intersection may occur if traffic signal does not provide for protected turning movements. Traffic queue may block nearby intersection(s) upstream of critical approach(es). Delay $>55 \mathrm{sec}$ and $\leq 80 \mathrm{sec} /$ veh | Very long traffic delays, failure, extreme congestion. <br> Delay > $35 \mathrm{sec} / \mathrm{veh}$ and $\leq 50 \mathrm{sec} / \mathrm{veh}$ | At or near capacity, flow quite unstable. |
| "F" | Total breakdown, stop-and-go operation. Delay > $80 \mathrm{sec} / \mathrm{veh}$ | Intersection often blocked by external causes. Delay > 50 sec/veh | Forced flow, breakdown. |
| Sources: 2010 Highway Capacity Manual, |  |  |  |

## Roadway Segment Level of Service

Two-Lane Highway Roadway Segments. Roadway segments were analyzed using methods presented in the Highway Capacity Manual 2010 (HCM). A two-lane highway is an undivided roadway with one lane in each direction. Passing a slower vehicle requires use of the opposing lane as sight distance and gaps in the opposing traffic stream permit. As volumes and geometric restrictions increase, the ability to pass decreases and platoons form. Motorists in platoons are subject to delay because they are unable to pass. The HCM divides these roadways into three types: Class I, Class II and Class III. They are defined as follows:

- Class I two-lane highways are highways where motorists expect to travel at relatively high speeds. Two-lane highways that are major intercity routes, primary connectors of major traffic generators, daily commuter routes, or major links in state or national
highway networks are generally assigned to Class I. These facilities serve mostly longdistance trips or provide the connections between facilities that serve long-distance trips.
- Class II two-lane highways are highways where motorists do not necessarily expect to travel at high speeds. Two-lane highways functioning as access routes to Class I facilities, serving as scenic or recreational routes (and not as primary arterials), or passing through rugged terrain (where high-speed operation would be impossible) are assigned to Class II. Class II facilities most often serve relatively short trips, the beginning or ending portions of longer trips, or trips for which sightseeing plays a significant role.
- Class III two-lane highways are highways serving moderately developed areas. They may be portions of a Class I or Class II highway that pass through small towns or developed recreational areas. On such segments, local traffic often mixes with through traffic, and the density of unsignalized roadside access points is noticeably higher than in a purely rural area. Class III highways may also be longer segments passing through more spreadout recreational areas, also with increased roadside densities. Such segments are often accompanied by reduced speed limits that reflect the higher activity level.

Levels of Service. Three measures of effectiveness are incorporated into the methodology to determine automobile LOS:

1. Average Travel Speed (ATS) reflects mobility on a two-lane highway. It is defined as the highway segment length divided by the average travel time taken by vehicles to traverse it during a designated time interval.
2. Percent Time Spent Following (PTSF) represents the freedom to maneuver and the comfort and convenience of travel. It is the average percentage of time that vehicles must travel in platoons behind slower vehicles due to the inability to pass. Because this characteristic is difficult to measure in the field, a surrogate measure is the percentage of vehicles traveling at headways of less than 3.0 at a representative location within the highway segment. PTSF also represents the approximate percentage of vehicles traveling in platoons.
3. Percent of free-flow speed (PFFS) represents the ability of vehicles to travel at or near the posted speed limit.

Speed and delay due to passing restrictions are both important to motorists on Class I two-lane highways; therefore, LOS is defined in terms of both ATS and PTSF. Travel speed is not a significant issue on Class II highways; therefore, LOS is defined in only terms of PTSF. High speeds are not expected on Class III highways and since the length of the Class III segments may be generally limited, passing restrictions are also not a major concern. In Class III segments drivers are expected to want to travel at or near the speed limit. Therefore, PFFS is used to define LOS. The LOS criteria for two-lane highways are shown in Table 2.

TABLE 2
AUTOMOBILE LOS FOR TWO-LANE HIGHWAYS $\dagger$

| LOS | Class I Highways |  | Class II Highways | Class III Highways |
| :---: | :---: | :---: | :---: | :---: |
|  | ATS (mi /hr) | PTSF (\%) | PTSF (\%) | PFFS (\%) |
| A | $>55$ | $\leq 35$ | $\leq 40$ | $>91.7$ |
| B | $>50-55$ | $>35-50$ | $>40-55$ | $>83.3-91.7$ |
| C | $>45-50$ | $>50-65$ | $>55-70$ | $>75.0-83.3$ |
| D | $>40-45$ | $>65-80$ | $>70-85$ | $>66.7-75.0$ |
| E | $\leq 40$ | $>80$ | $>85$ | $\leq 66.7$ |

$\dagger$ HCM 2010, Chapter 15, December 2010

## Existing Traffic Conditions

Intersection Levels of Service. Level of Service is based on and measured in terms of delay (seconds) per vehicle for the peak fifteen-minute analysis period. For unsignalized minor leg stop controlled intersections the movement with the worst delay approach movement is considered the critical Level of Service for the intersection. For multiway stop-controlled intersections the Level of Service is determined based on the overall average delay in the intersection.

Figure 2 presents the intersection turning movements for each intersection. Table 3 summarizes current Levels of Service at the study area intersections during the a.m. and p.m. peak hour. Saturday peak hour level of service was also calculated along the SR 113 intersections and at the Hay Road / Project Entrance intersection. Sunday traffic was reviewed at the project site and was consistently lower than Saturday traffic; therefore, the weekend analysis included only Saturday. All intersections except the SR 12 / SR 113 intersection currently operate at LOS C or better. The SR 12/ SR 113 intersection operates at LOS E in the a.m. peak hour with a delay of 38.8 seconds per vehicle (spv) and LOS F in the p.m. with a delay of 373.3 spv . This intersection meets the peak hour signal warrant in the p.m. peak hour. Caltrans has an identified safety improvement at this intersection which will construct a single lane roundabout. This project is identified for completion in the Fall 2019.


**Note: Intersections 1-4 not analyzed on Saturday

TABLE 3
EXISTING PEAK HOUR LEVELS OF SERVICE AT INTERSECTIONS

| Location | Control | Existing AM Peak Hour |  | Existing PM Peak Hour |  | Existing <br> Saturday Peak Hour |  | $\begin{gathered} \text { Peak Hour } \\ \text { Warrant } \\ \text { Met? } \\ \hline \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | LOS | Average <br> Delay (secs) | LOS | Average <br> Delay (secs) | LOS | Average Delay (secs) |  |
| 1. I-80 Westbound Ramps / Oday Rd SB Left <br> WB | WB Stop | $\begin{aligned} & \text { A } \\ & \text { B } \end{aligned}$ | $\begin{gathered} 6.7 \\ 10.3 \end{gathered}$ | $\begin{aligned} & \mathrm{A} \\ & \mathrm{~A} \end{aligned}$ | $\begin{aligned} & 7.5 \\ & 9.6 \end{aligned}$ |  | --- <br> --- | No |
| 2. Midway Road/ Oday Rd SB <br> EB Left | SB Stop | $\begin{aligned} & \mathrm{B} \\ & \mathrm{~A} \\ & \hline \end{aligned}$ | $\begin{gathered} 11.0 \\ 7.8 \end{gathered}$ | $\begin{aligned} & \mathrm{A} \\ & \mathrm{~A} \\ & \hline \end{aligned}$ | $\begin{aligned} & 9.8 \\ & 7.6 \end{aligned}$ | --- | ---- | No |
| 3. I-80 Eastbound Ramps / Midway Rd NB <br> EB Left | NB Stop | $\begin{aligned} & \text { B } \\ & \text { A } \end{aligned}$ | $\begin{gathered} 13.0 \\ 8.1 \end{gathered}$ | $\begin{aligned} & \mathrm{B} \\ & \mathrm{~A} \end{aligned}$ | $\begin{gathered} 12.2 \\ 8.1 \end{gathered}$ | ---- | ---- | No |
| 4. Midway Rd / Porter Rd WB | WB Stop | A | 9.0 | A | 8.8 | --- | --- | No |
| 5. SR 113 / Midway Rd <br> NB Left <br> SB Left <br> EB <br> WB | $\begin{gathered} \mathrm{EB} / \mathrm{EB} \\ \text { Stop } \end{gathered}$ | $\begin{aligned} & \mathrm{A} \\ & \mathrm{~A} \\ & \mathrm{~B} \\ & \mathrm{~B} \\ & \hline \end{aligned}$ | $\begin{gathered} 7.7 \\ 7.5 \\ 13.7 \\ 11.4 \\ \hline \end{gathered}$ | $\begin{aligned} & \mathrm{A} \\ & \mathrm{~A} \\ & \mathrm{~B} \\ & \mathrm{~B} \\ & \hline \end{aligned}$ | $\begin{gathered} 7.6 \\ 7.6 \\ 12.0 \\ 13.7 \\ \hline \end{gathered}$ | $\begin{aligned} & \mathrm{A} \\ & \mathrm{~A} \\ & \mathrm{~B} \\ & \mathrm{~A} \end{aligned}$ | $\begin{gathered} 7.5 \\ 7.4 \\ 10.5 \\ 9.9 \\ \hline \end{gathered}$ | No |
| 6. SR 113 / Hay Rd NB Left EB | EB Stop | $\begin{aligned} & \text { A } \\ & \text { B } \end{aligned}$ | $\begin{gathered} 7.6 \\ 10.6 \end{gathered}$ | $\begin{aligned} & \text { A } \\ & \text { B } \end{aligned}$ | $\begin{gathered} 7.8 \\ 12.1 \end{gathered}$ | $\begin{aligned} & \mathrm{A} \\ & \mathrm{~A} \end{aligned}$ | $\begin{aligned} & 7.5 \\ & 9.5 \end{aligned}$ | No |
| 7. SR 113 / SR 12 <br> NB <br> SB <br> EB Left <br> WB Left | NB / SB <br> Stop | $\begin{aligned} & \mathrm{C} \\ & \mathrm{E} \\ & \mathrm{~A} \\ & \mathrm{~A} \\ & \hline \end{aligned}$ | $\begin{gathered} 24.1 \\ 38.8 \\ 0.0 \\ 7.8 \\ \hline \end{gathered}$ | $\begin{aligned} & \mathrm{C} \\ & \mathrm{~F} \\ & \mathrm{~A} \\ & \mathrm{~A} \\ & \hline \end{aligned}$ | $\begin{gathered} 17.8 \\ 373.3 \\ 8.6 \\ 9.3 \end{gathered}$ | $\begin{aligned} & \mathrm{B} \\ & \mathrm{C} \\ & \mathrm{~A} \\ & \mathrm{~A} \\ & \hline \end{aligned}$ | $\begin{array}{r} 12.0 \\ 20.5 \\ 8.6 \\ 7.9 \end{array}$ | Yes |
| 8. Hay Rd / Project Entrance NB <br> WB Left | NB Stop | $\begin{aligned} & \mathrm{A} \\ & \mathrm{~A} \\ & \hline \end{aligned}$ | $\begin{aligned} & 9.2 \\ & 7.4 \end{aligned}$ | $\begin{aligned} & \mathrm{A} \\ & \mathrm{~A} \\ & \hline \end{aligned}$ | $\begin{aligned} & 9.1 \\ & 7.3 \end{aligned}$ | $\begin{aligned} & \mathrm{A} \\ & \mathrm{~A} \\ & \hline \end{aligned}$ | $\begin{aligned} & 9.0 \\ & 7.4 \end{aligned}$ | No |

AWS - multi-way stop

Existing Roadway Segment Levels of Service. Table 4 summarizes the Levels of Service based on the current traffic volumes on study area roads with the existing roadway configuration. Applicable Level of Service thresholds and roadway classifications are presented. The Levels of Service along Midway Road, SR 113 and Hay Road were computed using the HCS two-lane roadway methodology. Both County roadways will operate at LOS C or better while the segments along SR 113 operate at LOS D or better. These are within the acceptable thresholds.

TABLE 4
EXISTING ROADWAY SEGMENT LEVELS OF SERVICE

|  |  | Facility | ATS/PTSF/LOS | ATS/PTSF/LOS |
| :---: | :---: | :---: | :---: | :---: |
| Roadway | Location | Classification | Existing AM | Existing PM |
| Midway Rd | I-80 to Porter Rd | Class I Highway |  |  |
|  | EB |  | 46.6 / 42.8 / C | 45.9 / 55.0 / C |
|  | WB |  | 46.5 / 53.3 / C | $46.0 / 49.8 / \mathrm{C}$ |
|  | Porter Rd to SR 113 | Class I Highway |  |  |
|  | EB |  | 48.2 / 35.3 / C | 50.0 / 13.9 / B |
|  | WB |  | 48.0 / 30.5 / C | 50.2 / 28.1/B |
| SR 113 | Midway Rd to Fry Rd | Class I Highway |  |  |
|  | NB |  | 47.7 / 29.1 / C | 45.9 / 36.8 / C |
|  |  |  | $47.5 / 25.0 / \mathrm{C}$ | $45.9 \text { / } 37.3 \text { / C }$ |
|  | Fry Rd to Hay Rd | Class I Highway |  |  |
|  | NB |  | 45.8 / 44.2 / C | 44.8 / 46.1 / D |
|  | SB |  | 45.6 / $31.7 / \mathrm{C}$ | 44.8 / 43.8 / D |
|  | Hay Rd to SR 12 | Class I Highway |  |  |
|  | NB |  | 46.1 / 48.2 / C | 44.9 / 45.3 / D |
|  | SB |  | 45.7 / 30.5 / C | 44.9 / 50.4 / D |
| Hay Rd | SR 113 to Daily Rd | Class I Highway |  |  |
|  | EB |  | 49.7 / 24.9 / C | 49.5 / 26.4 / C |
|  | WB |  | 49.7 / 24.9 / C | 49.4 / 15.1 / C |

ATS - average travel speed
PTSF - percent time spent following

## Non-Automobile Transportation

Public Transit. Various bus services are provided within Solano County. These include the Fairfield and Suisun Transit System (FAST), Rio Vista Delta Breeze, Solano Express and Vacaville City Coach. These services provide local and intercity routes along the I-80 corridor; however, there are no routes along Midway Road or SR 113.

Bicycle and Pedestrian Facilities. Due to the rural nature of the project location there are no bike facilities or pedestrian facilities present.

## Existing Plus Project Conditions

Under Section 15126.2 of the CEQA guidelines, a project must be evaluated individually and cumulatively to determine whether the project causes a significant effect on the environment. Individually, the project is evaluated under Existing conditions, i.e., Existing plus Project conditions while cumulatively, it is analyzed under future conditions which may include either a list of past, present and probably future projects producing related or cumulative impacts or a summary of projections contained in an adopted local, regional or statewide plan or related planning document.

This project is intended to amend the existing Conditional Use Permit by allowing up to 3,400 tons of refuse to be delivered to the site, while maintaining an average 7-day average of 3,200 tons per day.

The 2016 data (tonnage received and vehicle trips) is an appropriate baseline against which to assess the potential net growth in vehicles travelling to and from the landfill as a result of the project. During 2017 and 2018, the landfill assisted in the disposal of fire debris from wildfires in Northern California, which resulted in the accommodation of additional tonnage within the disposal area and additional vehicles travelling to and from the landfill. Table 5 identifies the annual tonnage received, with and without the fire debris and the number of vehicles travelling to and from the landfill during those periods. Because the acceptance of fire debris was in response to an emergency condition, the additional tonnage received and trips conducted were not subject to the established limits within the CUP for the landfill. As a result, use of either 2017 or 2018 tonnage data as part of the baseline against which the potential impacts of an amended CUP would be assessed is considered inappropriate and potentially misleading because it does not represent the landfill's typical operating condition.

TABLE 5
HISTORICAL ANNUAL TONNAGE 2016-2018

| Year | Baseline Tonnage | Baseline Vehicles |
| :--- | :---: | :---: |
| 2016 | 1,682 | 425 |
| 2017 (with fire debris) | 1,947 | 471 |
| 2018 (with fire debris) | 2,083 | 465 |

Italics: Baseline

Trip Generation. The 2016 7-day tonnage averaged about 1,682 per day. Recology Hay Road projects that most new municipal solid waste (MSW) associated with the proposed project will arrive from outside the local area using semitrailer. MSW tonnage arriving to the site is projected as follows:

- 90\% 20-ton transfer trucks
- $8 \%$ 7-ton packer trucks
- $2 \% 1 / 2$-ton self-haul vehicles

Table 6 presents the projected additional trips, broken down by vehicle type, based on the proposed expansion of the site. Both average daily and peak day MSW tonnage to the site were considered. Peak tonnage was based on the difference between the maximum proposed peak tonnage per day (maximum 3,400 tons per day) and the average 2016 weekday tonnage 1,682 tons per day). The project will generate an additional 1,718 tons of MSW under a peak day while the additional average daily MSW will be 1,518 tons per day.

Based on the projected additional daily tonnage and the various vehicles bringing MSW to the site it is projected that 195 new inbound and 195 new outbound trips will be generated daily by the project. This is shown in Table 6. Of these trips, 91 new semi-trailer trips will be generated, with 23 additional packer trucks and 81 new self-haul vehicles.

## TABLE 6

PROJECTED DAILY TRIPS*

| Average MSW Tons |  |  | Average Daily Tonnage per Week (Proposed) | Maximum Daily Tonnage (Proposed) | Net New Tonnage |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| (a) | (b) |  | (c) |  | (e) |  | (f) |
| Weekday | Weekend |  |  |  |  |  | Maximum |
| 1,682 | 924 | 3,200 |  | 3,400 | 1,518 ${ }^{1}$ |  | 1,768 ${ }^{2}$ |
| PEAK TONNAGE VEHICLES |  |  |  |  |  |  |  |
| Maximum Daily Tonnage | Transfer Trucks $\mathbf{9 0 \%}$ of entering vehicles (20 tons / vehicle) |  | Packer Trucks $\mathbf{8 \%}$ of entering vehicles (7 tons / vehicle) |  | Self-Haul vehicles $2 \%$ of entering vehicles ( 0.5 tons / vehicle) |  | Total Vehicles |
| (g) | In | Out | In | Out | In | Out |  |
| 1,718 (Inbound) | $91^{3}$ |  | $23^{4}$ |  | $81^{5}$ |  | 195 |
| Empty (Outbound) |  | 91 |  | 23 |  | 81 | 195 |

* Based on 2016 traffic at Recology Hay Road site

MSW - municipal solid waste
${ }^{1}$ (c) $-(\mathrm{a})$
2 (d) - (a)
${ }^{3}[(\mathrm{~g}) * 0.90] / 20$
${ }^{4}[(\mathrm{~g}) * 0.08] / 7$
${ }^{5}[(\mathrm{~g}) * 0.02] / 0.5$

The projected peak hour traffic was estimated based on current traffic into the site compared to historical daily traffic and proportioned based on the existing conditions. On a peak day the project is expected to generate 46 additional a.m. peak hour trips and 27 additional p.m. peak hour trips. Table 7 presents the projected a.m. and p.m. peak hour trips including a breakdown by trip type.

TABLE 7
PROJECTED PEAK HOUR TRIPS

| Existing Conditions |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Avg Total Daily Vehicles | AM |  | PM |  |
|  | In | Out | In | Out |
| 526 vehicles* | $69 \dagger$ | 53† | $3+$ | 53\% |
| Percent Traffic $\diamond$ | 13.1\% | 10.1\% | 0.6\% | 13.1\% |
| Project Traffic |  |  |  |  |
| New Daily Vehicles | AM |  | PM |  |
|  | In | Out | In | Out |
| 195 vehicles |  |  |  |  |
| Peak Hour Traffic | $26 *$ | 20 | 1 | 26 |
| Transfer Truck | 12 $\phi$ | 9 | 1 | 12 |
| Packer | $3 \mu$ | 2 | 0 | 3 |
| Self-Haul | $11 \beta$ | 8 | 0 | 11 |
| * average entering midweek vehicles $\ddagger$ existing p.m. peak hour traffic - (195 daily vehicles* $13.1 \%$ ) typ. $\mu 26^{*}(23 / 195)$ typ. | ting a.m. ctional $p$ $(91 / 195)$ $(81 / 195)$ | ur traffic |  |  |

Recology is projecting that Saturday traffic volumes will be similar to mid-week volumes. Weekend traffic generates about 459 vehicles to the site on a typical Saturday. Table 8 presents the projected Saturday peak hour trips based on current inbound and outbound peak hour Saturday trips relative to the total daily Saturday trips. Eleven inbound and nine outbound transfer trucks are projected during the peak hour with three inbound and two outbound packer trucks and ten inbound and eight outbound additional self-haul vehicles are projected with the increase in daily tonnage.

TABLE 8
PROJECTED SATURDAY DAILY TRIPS

| Existing Conditions |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Avg Total Daily Vehicles |  |  |  | In | Out |  |
| 459 vehicles |  |  |  | $55 \dagger$ | 43! |  |
| Percent Traffic |  |  |  | 12.0\% | 9.4\% |  |
| Project Traffic |  |  |  |  |  |  |
| Transfer Trucks |  | Packer Trucks |  | Self-Haul Vehicles |  | Total Vehicles |
| In | Out | In | Out | In | Out |  |
| $11^{1}$ | $9^{2}$ | $3^{3}$ | $2^{4}$ | $10^{5}$ | $8^{6}$ | 43 |
| $\dagger$ entering Saturday vehicles <br> ${ }^{1}$ (91 weekday transfer trucks)* $12.0 \%$ <br> ${ }^{3}$ (23 weekday packer trucks)* $12.0 \%$ <br> ${ }^{5}$ (81 weekday self-haul)* $12.0 \%$ |  |  | $\ddagger$ exiting Saturday vehicles <br> ${ }^{2}$ (91 weekday transfer trucks)*9.4\% <br> ${ }^{4}$ (23 weekday packer trucks)*9.4\% <br> ${ }^{6}$ (81 weekday self-haul)*9.4\% |  |  |  |

Vehicle Trip Distribution. The distribution of project vehicular traffic was determined based on the haul routes for semi-trailer and packer vehicles and a review of existing traffic counts at the surrounding intersections. Table 9 displays the trip distribution assumptions used for the proposed projects.

TABLE 9
TRIP DISTRIBUTION

| Route | \% of Total Trips |  |  |
| :--- | :---: | :---: | :---: |
|  | AM | PM | Saturday |
| To / From I-80 west of Midway Rd | $62 \%$ | $46 \%$ | $48 \%$ |
| West on Hay Road | $20 \%$ | $30 \%$ | $30 \%$ |
| To / From SR 12 east of SR 113 | $9 \%$ | $8 \%$ | $10 \%$ |
| To / From SR 12 west of SR 113 | $0 \%$ | $8 \%$ | $6 \%$ |
| North on SR 113 | $9 \%$ | $8 \%$ | $6 \%$ |
| Total | $100 \%$ | $100 \%$ | $100 \%$ |

Vehicle Trip Assignment. Traffic generated by the project was assigned to the study roadway system based on the projected distribution percentages. Figure 3 displays the project generated traffic. Figure 4 displays the resulting sum of existing a.m., p.m. and Saturday peak hour volumes and project trips at the study intersections for the Existing plus Project condition.


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| 1 <br> Oday Rd/ I-80 WB Ramps | 2 <br> Oday Rd/ Midway Rd |
| :---: | :---: |
| 3 | 4 |
|  <br> I-80 EB Ramps/ Midway Rd | Porter Rd/ Midway Rd |
|  | $6$ |
|  |  |
| SR 113/ Midway Rd | SR 113/ Hay Rd |
| 7 | 8 |
|  | $\checkmark{ }^{0}{ }^{0(0)(1)} \mathbf{0} 16$ |
|  |  |
| SR 113/ SR 12 | Project Access/ Hay Rd |

**Note: Intersections 1-4 not analyzed on Saturday

PROJECT ONLY TRAFFIC VOLUMES AND LANE CONFIGURATIONS



**Note: Intersections 1-4 not analyzed on Saturday

## Existing Plus Project Level of Service Impacts

Intersection Levels of Service. Table 10 displays the a.m., p.m. and Saturday peak period levels of service at each study intersection under Existing plus Project conditions. All intersections except the SR 12/ SR 113 intersection will continue to operate at or above the level of service thresholds, at LOS C or better. The SR 12 / SR 113 intersection will continue to operate at LOS E in the a.m. peak hour and LOS F in the p.m. peak hour. As identified in the Existing Conditions the intersection is scheduled to have a roundabout installed and completed by Fall 2019. No mitigations are necessary.

Roadway Levels of Service. Table 11 presents the peak hour roadway segment traffic volumes along the five study segments. All roadway segments along County roads will operate at LOS C or better while all roadway segments along SR 113 will operate at LOS D or better. These are within the acceptable thresholds.

TABLE 10
EXISTING PLUS PEAK HOUR LEVELS OF SERVICE AT INTERSECTIONS

| Location | Control | Existing plus Project AM Peak Hour |  | Existing plus Project PM Peak Hour |  | Existing plus Project Saturday Peak Hour |  | Peak Hour Warrant Met? |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | LOS | Average Delay (secs) | LOS | Average Delay (secs) | LOS | Average Delay (secs) |  |
| 1. I-80 Westbound Ramps / Oday Rd SB Left <br> WB | WB Stop | $\begin{aligned} & \text { A } \\ & \text { B } \end{aligned}$ | $\begin{gathered} 7.7 \\ 10.3 \end{gathered}$ | $\begin{aligned} & \text { A } \\ & \text { A } \end{aligned}$ | $\begin{aligned} & 7.5 \\ & 9.6 \end{aligned}$ |  | ---- | No |
| 2. Midway Road / Oday Rd SB <br> EB Left | SB Stop | $\begin{aligned} & \mathrm{B} \\ & \mathrm{~A} \\ & \hline \end{aligned}$ | $\begin{gathered} 11.1 \\ 7.8 \\ \hline \end{gathered}$ | $\begin{aligned} & \mathrm{A} \\ & \mathrm{~A} \\ & \hline \end{aligned}$ | $\begin{aligned} & 9.8 \\ & 7.6 \\ & \hline \end{aligned}$ | --- | --- | No |
| 3. I-80 Eastbound Ramps / Midway Rd NB <br> EB Left | NB Stop | $\begin{aligned} & \mathrm{B} \\ & \mathrm{~A} \\ & \hline \end{aligned}$ | $\begin{gathered} 13.2 \\ 8.2 \\ \hline \end{gathered}$ | $\begin{array}{r} \mathrm{B} \\ \mathrm{~A} \\ \hline \end{array}$ | $\begin{gathered} 12.4 \\ 8.1 \\ \hline \end{gathered}$ | ---- | ---- | No |
| 4. Midway Rd / Porter Rd WB | WB Stop | A | 9.1 | A | 8.9 | --- | --- | No |
|  | EB/EB <br> Stop | $\begin{aligned} & \mathrm{A} \\ & \mathrm{~A} \\ & \mathrm{~B} \\ & \mathrm{~B} \\ & \hline \end{aligned}$ | $\begin{gathered} 7.7 \\ 7.5 \\ 14.3 \\ 11.8 \\ \hline \end{gathered}$ | $\begin{aligned} & \mathrm{A} \\ & \mathrm{~A} \\ & \mathrm{~B} \\ & \mathrm{~B} \\ & \hline \end{aligned}$ | $\begin{gathered} 7.7 \\ 7.6 \\ 12.3 \\ 14.2 \\ \hline \end{gathered}$ | $\begin{aligned} & \mathrm{A} \\ & \mathrm{~A} \\ & \mathrm{~B} \\ & \mathrm{~B} \\ & \hline \end{aligned}$ | $\begin{gathered} 7.5 \\ 7.4 \\ 10.5 \\ 10.0 \\ \hline \end{gathered}$ | No |
| 6. SR 113 / Hay Rd NB Left EB | EB Stop | $\begin{aligned} & \mathrm{A} \\ & \mathrm{~B} \\ & \hline \end{aligned}$ | $\begin{gathered} 7.6 \\ 11.2 \\ \hline \end{gathered}$ | $\begin{aligned} & \mathrm{A} \\ & \mathrm{~B} \\ & \hline \end{aligned}$ | $\begin{gathered} 7.8 \\ 12.5 \\ \hline \end{gathered}$ | $\begin{aligned} & \mathrm{A} \\ & \mathrm{~A} \\ & \hline \end{aligned}$ | $\begin{array}{r} 7.5 \\ 9.9 \\ \hline \end{array}$ | No |
|  | $\begin{gathered} \text { NB / SB } \\ \text { Stop } \end{gathered}$ | $\begin{aligned} & \mathrm{B} \\ & \mathrm{E} \\ & \mathrm{~A} \\ & \mathrm{~A} \\ & \hline \end{aligned}$ | $\begin{gathered} 11.9 \\ 39.4 \\ 0.0 \\ 7.8 \\ \hline \end{gathered}$ | $\begin{aligned} & \mathrm{C} \\ & \mathrm{~F} \\ & \mathrm{~A} \\ & \mathrm{~A} \\ & \hline \end{aligned}$ | $\begin{gathered} 17.8 \\ 376.1 \\ 8.6 \\ 9.3 \\ \hline \end{gathered}$ | $\begin{aligned} & \mathrm{B} \\ & \mathrm{C} \\ & \mathrm{~A} \\ & \mathrm{~A} \\ & \hline \end{aligned}$ | $\begin{gathered} 12.0 \\ 20.6 \\ 8.6 \\ 7.9 \\ \hline \end{gathered}$ | Yes |
| 8. Hay Rd / Project Entrance NB <br> WB Left | NB Stop | $\begin{aligned} & \mathrm{A} \\ & \mathrm{~A} \\ & \hline \end{aligned}$ | $\begin{aligned} & 9.5 \\ & 7.4 \\ & \hline \end{aligned}$ | $\begin{aligned} & \mathrm{A} \\ & \mathrm{~A} \\ & \hline \end{aligned}$ | $\begin{aligned} & 9.3 \\ & 7.3 \\ & \hline \end{aligned}$ | $\begin{aligned} & \mathrm{A} \\ & \mathrm{~A} \\ & \hline \end{aligned}$ | $\begin{aligned} & 9.2 \\ & 7.4 \end{aligned}$ | No |

AWS - multi-way stop

TABLE 11
EXISTING PLUS PROJECT ROADWAY SEGMENT LEVELS OF SERVICE

|  |  |  | ATS/PTSF/LOS | ATS/PTSF/LOS |
| :---: | :---: | :---: | :---: | :---: |
| Roadway | Location | Facility Classification | Existing plus Project AM | Existing plus Project PM |
| Midway Rd | I-80 to Porter Rd | Class I Highway |  |  |
|  | EB |  | 46.4 / 45.4 / C | 45.8 / 55.6 / C |
|  | WB |  | 46.3 / 55.3 / C | 45.9 / 51.3 / C |
|  | Porter Rd to SR 113 | Class I Highway |  |  |
|  |  |  | 47.9 / 37.5 / C | 49.8 / 13.3 / C |
|  | WB |  | 47.6 / 32.3 / C | 50.1 / 29.6 / B |
| SR 113 | Midway Rd to Fry Rd | Class I Highway |  |  |
|  | NB |  | 47.2 / 31.0 / C | 45.7 / 38.5 / C |
|  | SB |  | 47.0 / 28.1 / C | 45.7 / 37.7 / C |
|  | Fry Rd to Hay Rd | Class I Highway |  |  |
|  | NB |  | 45.3 / 45.3 / C | 44.7 / 47.8 / D |
|  |  |  | $45.3 \text { / } 34.0 \text { / C }$ | 44.7 / 44.1 / D |
|  | Hay Rd to SR 12 | Class I Highway |  |  |
|  | NB |  | 46.0 / 48.5 / C | 44.8 / 45.0 / D |
|  | SB |  | 45.7 / 30.9 / C | 44.8 / 50.7 / D |
| Hay Rd | SR 113 to Daily Rd | Class I Highway |  |  |
|  | EB |  | 49.0 / 27.2 / C | 49.3 / 29.3 / C |
|  | WB |  | 49.0 / 21.8 / C | 49.2 / 13.1 / C |

ATS - average travel speed
PTSF - percent time spent following

## CUMULATIVE IMPACTS

The analysis of Cumulative impacts was considered when accommodating the peak tonnage increase for the site.

## Year 2030 Traffic Forecasts and Lane Configurations

The traffic impacts associated with revising the allowable daily tonnage increase at the Hay Road Landfill site was evaluated within the context of future traffic conditions occurring in this area of Solano County. The most recent Napa-Solano regional travel demand model was used to estimate cumulative traffic in the project's vicinity.

Year 2030 daily traffic volume forecasts generated by the traffic model was the basis for future background traffic conditions. Cumulative volumes along the roadway links were developed using the difference method, i.e., using the projected model growth (i.e. 2010 to 2030) and adding this to existing traffic counts.

The "balancing" of future year intersection turning movement traffic volumes was conducted using methods described in the Transportation Research Board's (TRB's) National Cooperative Highway Research Program (NCHRP) Report 255, Highway Traffic Data for Urbanized Area Project Planning and Design. The NCHRP 255 method applies the desired peak hour directional volumes to the intersection turning movement volumes, using an iterative process to balance and adjust the resulting forecasts to match the desired peak hour directional volumes. The development of future year intersection turning movement traffic volumes requires that the turning movements at each intersection "balance". To achieve the balance, inbound traffic volumes must equal the outbound traffic volumes, and the volumes must be distributed among the various left-turn, through, and right-turn movements at each intersection. Figure 5 presents the projected turning movements at the study intersections.

A single lane roundabout at the SR 12 / SR 113 intersection is the only road improvement identified within the project limits.

## 2030 Conditions

Intersection Levels of Service. Table 12 displays the a.m. peak hour Levels of Service at each study intersection in the Cumulative 2030 condition. Two intersections will operate below County and Caltrans LOS thresholds in the 2030 No Project condition. The SR 113 / Midway Road intersection will decline to a LOS E condition in the a.m. peak hour ( 38.5 spv ) and p.m. peak hour ( 46.0 spv ). The SR 12/ SR 113 intersection is projected to operate at a LOS F condition in the p.m. peak hour ( 124.4 spv ). The SR 113 / Midway Road intersection will meet the peak hour signal warrant in the a.m. and p.m. peak hours. The SR 113 / Hay Road intersection will also meet the peak hour signal warrant in the p.m. peak hour; however, the intersection operates at LOS C or better.

TABLE 12
2030 PEAK HOUR LEVELS OF SERVICE AT INTERSECTIONS

| Location | Control | 2030 <br> AM Peak Hour |  | 2030PM Peak Hour |  | 2030Saturday Peak Hour |  | Peak Hour Warrant Met? |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | LOS | Average Delay (secs) | LOS | Average Delay (secs) | LOS | Average Delay (secs) |  |
| 1. I-80 Westbound Ramps / Oday Rd SB Left WB | WB Stop | $\begin{aligned} & \text { A } \\ & \text { B } \end{aligned}$ | $\begin{gathered} 7.9 \\ 11.2 \end{gathered}$ | $\begin{aligned} & \text { A } \\ & \text { B } \end{aligned}$ | $\begin{gathered} 7.6 \\ 10.1 \end{gathered}$ | ---- | ---- | No |
| 2. Midway Road / Oday Rd SB <br> EB Left | SB Stop | $\begin{aligned} & \mathrm{B} \\ & \mathrm{~A} \\ & \hline \end{aligned}$ | $\begin{gathered} 13.3 \\ 8.1 \\ \hline \end{gathered}$ | $\begin{aligned} & \mathrm{B} \\ & \mathrm{~A} \\ & \hline \end{aligned}$ | $\begin{gathered} 11.2 \\ 7.9 \\ \hline \end{gathered}$ | ---- | --- | No |
| 3. I-80 Eastbound Ramps / Midway Rd NB <br> EB Left | NB Stop | $\begin{aligned} & \mathrm{C} \\ & \mathrm{~A} \end{aligned}$ | $\begin{gathered} 16.4 \\ 8.6 \end{gathered}$ | $\begin{aligned} & \mathrm{C} \\ & \mathrm{~A} \end{aligned}$ | $\begin{gathered} 16.0 \\ 8.5 \end{gathered}$ | --- | --- | No |
| 4. Midway Rd / Porter Rd WB | WB Stop | A | 9.2 | A | 9.1 | --- | --- | No |
| 5. SR 113 / Midway Rd NB Left SB Left EB WB | EB/EB Stop | $\begin{aligned} & \mathrm{A} \\ & \mathrm{~A} \\ & \mathrm{E} \\ & \mathrm{C} \end{aligned}$ | $\begin{gathered} 8.0 \\ 7.8 \\ 38.5 \\ 16.1 \\ \hline \end{gathered}$ | $\begin{aligned} & \mathrm{A} \\ & \mathrm{~A} \\ & \mathrm{C} \\ & \mathrm{E} \\ & \hline \end{aligned}$ | $\begin{gathered} 8.1 \\ 7.9 \\ 23.6 \\ 46.0 \\ \hline \end{gathered}$ | $\begin{aligned} & \mathrm{A} \\ & \mathrm{~A} \\ & \mathrm{~B} \\ & \mathrm{~B} \\ & \hline \end{aligned}$ | $\begin{gathered} 7.7 \\ 7.6 \\ 13.2 \\ 11.1 \\ \hline \end{gathered}$ | Yes ${ }^{1}$ |
| 6. SR 113 / Hay Rd NB Left EB | EB Stop | $\begin{aligned} & \mathrm{A} \\ & \mathrm{~B} \\ & \hline \end{aligned}$ | $\begin{gathered} 8.0 \\ 14.1 \end{gathered}$ | $\begin{aligned} & \mathrm{A} \\ & \mathrm{C} \\ & \hline \end{aligned}$ | $\begin{gathered} 8.4 \\ 21.2 \end{gathered}$ | $\begin{aligned} & \mathrm{A} \\ & \mathrm{~B} \\ & \hline \end{aligned}$ | $\begin{gathered} 7.6 \\ 10.7 \end{gathered}$ | Yes ${ }^{2}$ |
| 7. SR 113 / SR 12 | Roundabout | C | 20.8 | F | 124.4 | B | 10.4 | N/A |
| 8. Hay Rd / Project Entrance NB <br> WB Left | NB Stop | $\begin{aligned} & \mathrm{A} \\ & \mathrm{~A} \\ & \hline \end{aligned}$ | $\begin{aligned} & 9.6 \\ & 7.4 \end{aligned}$ | $\begin{aligned} & \mathrm{A} \\ & \mathrm{~A} \\ & \hline \end{aligned}$ | $\begin{aligned} & 9.5 \\ & 7.5 \end{aligned}$ | $\begin{aligned} & \mathrm{A} \\ & \mathrm{~A} \\ & \hline \end{aligned}$ | $\begin{aligned} & 9.2 \\ & 7.4 \end{aligned}$ | No |

AWS - multi-way stop
N/A - not applicable
${ }^{1}$ meets peak hour traffic signal warrant (a.m. and p.m.)
${ }^{2}$ meets peak hour traffic signal warrant (p.m.)


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| :--- |
| $0563-002$ RA 10/18/2018 |


**NOTE: Intersections 1-4 not analyzed on Saturday

2030 Roadway Segment Levels of Service. Table 13 summarizes the Levels of Service based on the projected 2030 traffic volumes on study area roads with the existing two-lane roadway configuration. All roadway segments except the Midway Road segment between I-80 and Porter Road are projected to operate acceptably, at LOS C along County roads and at LOS D or better along SR 113. The Level of Service along Midway Road between I-80 and Porter Road is projected to decline to LOS D in the p.m. peak hour in both eastbound and westbound directions.

TABLE 13
2030 ROADWAY SEGMENT LEVELS OF SERVICE

|  |  | Facility | ATS/PTSF/LOS | ATS/PTSF/LOS |
| :---: | :---: | :---: | :---: | :---: |
| Roadway | Location | Classification | 2030 AM | 2030 PM |
| Midway Rd | I-80 to Porter Rd | Class I Highway |  |  |
|  | EB |  | 45.5 / 45.3 / C | 42.6 / 72.3 / D |
|  | WB |  | 45.4 / 62.2 / C | 43.0 / 59.2 / D |
|  | Porter Rd to SR 113 | Class I Highway |  |  |
|  | EB |  | 46.5 / 44.5 / C | 47.3 / 36.1 / C |
|  | WB |  | 46.7 / 42.3 / C | 47.3 / 39.8 / C |
| SR 113 | Midway Rd to Fry Rd | Class I Highway |  |  |
|  | NB |  | 44.3 / 41.4 / D | 43.5 / 52.8 / D |
|  |  |  | $43.7 \text { / } 53.6 \text { / D }$ | $43.5 / 53.1 / \mathrm{D}$ |
|  | Fry Rd to Hay Rd | Class I Highway |  |  |
|  | NB |  | 42.9 / 59.6 / D | 41.7 / 63.1 / D |
|  | SB |  | 43.1 / 46.6 / D | 41.8 / 60.4 / D |
|  | Hay Rd to SR 12 | Class I Highway |  |  |
|  | NB |  | 43.1 / 63.0 / D | 41.9 / 59.6 / D |
|  | SB |  | 43.4 / 44.2 / D | 41.8 / 65.7 / D |
| Hay Rd | SR 113 to Daily Rd | Class I Highway |  |  |
|  | EB |  | 49.2 / 16.6 / C | 49.0 / 36.7 / C |
|  | WB |  | 49.2 / 29.3 / C | 48.6 / 7.9 / C |

ATS - average travel speed
PTSF - percent time spent following

## 2030 Plus Project Level of Service Impacts

Intersection Levels of Service. Figure 6 presents the projected turning movements at the study intersections under 2030 plus Project conditions. Table 14 displays the a.m. peak hour Levels of Service at each study intersection in the 2030 plus Project condition. Two intersections will operate below County and Caltrans LOS thresholds. The SR 113 / Midway Road intersection will operate at a LOS E condition in the a.m. peak hour ( 45.7 spv ) and LOS F condition in the p.m. peak hour ( 53.6 spv ). This intersection will meet the peak hour signal warrant in the a.m. and p.m. peak hour. The SR 12/ SR 113 intersection is projected to operate at a LOS F condition in the p.m. peak hour ( 125.3 spv ). The SR 113 / Hay Road intersection will also meet the peak hour signal warrant in the p.m. peak hour; however, the intersection operates at LOS C or better.

Roadway Levels of Service. Table 15 summarizes the Levels of Service based on the projected 2030 plus Project traffic volumes on study area roads. All roadway segments except the Midway Road segment between I-80 and Porter Road are projected to operate acceptably, at LOS C along County roads and at LOS D or better along SR 113. The Level of Service along Midway Road between I-80 and Porter Road is projected to decline to LOS D in the p.m. peak hour in both eastbound and westbound directions.


**Note: Intersections 1-4 not analyzed on Saturday

TABLE 14
2030 PLUS PEAK HOUR LEVELS OF SERVICE AT INTERSECTIONS

| Location | Control | 2030 plus Project <br> AM Peak Hour |  | 2030 plus Project PM Peak Hour |  | 2030 plus Project Saturday Peak Hour |  | Peak Hour Warrant Met? |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | LOS | Average Delay (secs) | LOS | Average Delay (secs) | LOS | Average Delay (secs) |  |
| 1. I-80 Westbound Ramps / Oday Rd SB Left <br> WB | WB Stop | $\begin{aligned} & \text { A } \\ & \text { B } \end{aligned}$ | $\begin{gathered} 8.0 \\ 11.3 \end{gathered}$ | $\begin{aligned} & \text { A } \\ & \text { B } \end{aligned}$ | $\begin{gathered} 7.7 \\ 10.2 \end{gathered}$ | ---- | ---- | No |
| 2. Midway Road / Oday Rd SB <br> EB Left | SB Stop | $\begin{aligned} & \mathrm{B} \\ & \mathrm{~A} \\ & \hline \end{aligned}$ | $\begin{gathered} 13.4 \\ 8.1 \\ \hline \end{gathered}$ | $\begin{aligned} & \mathrm{B} \\ & \mathrm{~A} \\ & \hline \end{aligned}$ | $\begin{gathered} 11.3 \\ 7.9 \\ \hline \end{gathered}$ | --- | ---- | No |
| 3. I-80 Eastbound Ramps / Midway Rd NB <br> EB Left | NB Stop | $\begin{aligned} & \mathrm{C} \\ & \mathrm{~A} \end{aligned}$ | $\begin{gathered} 16.6 \\ 8.6 \end{gathered}$ | $\begin{aligned} & \mathrm{C} \\ & \mathrm{~A} \end{aligned}$ | $\begin{gathered} 16.2 \\ 8.6 \end{gathered}$ | ---- | ---- | No |
| 4. Midway Rd / Porter Rd WB | WB Stop | A | 9.3 | A | 9.2 | --- | --- | No |
| 5. SR 113 / Midway Rd NB Left SB Left EB WB | EB/EB Stop | $\begin{aligned} & \mathrm{A} \\ & \mathrm{~A} \\ & \mathrm{E} \\ & \mathrm{C} \end{aligned}$ | $\begin{gathered} 8.1 \\ 7.8 \\ 45.7 \\ 17.0 \\ \hline \end{gathered}$ | $\begin{aligned} & \mathrm{A} \\ & \mathrm{~A} \\ & \mathrm{D} \\ & \mathrm{~F} \\ & \hline \end{aligned}$ | $\begin{gathered} 8.1 \\ 7.9 \\ 25.3 \\ 53.6 \\ \hline \end{gathered}$ | $\begin{aligned} & \mathrm{A} \\ & \mathrm{~A} \\ & \mathrm{~B} \\ & \mathrm{~B} \\ & \hline \end{aligned}$ | $\begin{gathered} 7.7 \\ 7.6 \\ 13.3 \\ 11.3 \\ \hline \end{gathered}$ | Yes ${ }^{1}$ |
| 6. SR 113 / Hay Rd <br> NB Left <br> EB | EB Stop | A <br> C | $\begin{gathered} 8.0 \\ 15.4 \\ \hline \end{gathered}$ | A <br> C | $\begin{gathered} 8.4 \\ 23.1 \\ \hline \end{gathered}$ | $\begin{aligned} & \mathrm{A} \\ & \mathrm{~B} \\ & \hline \end{aligned}$ | $\begin{gathered} 7.6 \\ 11.1 \end{gathered}$ | Yes ${ }^{2}$ |
| 7. SR 113 / SR 12 | Roundabout | C | 21.0 | F | 125.3 | B | 10.5 | N/A |
| 8. Hay Rd / Project Entrance NB <br> WB Left | NB Stop | $\begin{aligned} & \mathrm{A} \\ & \mathrm{~A} \\ & \hline \end{aligned}$ | $\begin{aligned} & 9.8 \\ & 7.5 \end{aligned}$ | $\begin{aligned} & \mathrm{A} \\ & \mathrm{~A} \\ & \hline \end{aligned}$ | $\begin{aligned} & 9.7 \\ & 7.5 \end{aligned}$ | $\begin{aligned} & \mathrm{A} \\ & \mathrm{~A} \\ & \hline \end{aligned}$ | $\begin{aligned} & 9.4 \\ & 7.4 \end{aligned}$ | No |

AWS - multi-way stop
N/A - not applicable
${ }^{1}$ meets peak hour traffic signal warrant (a.m. and p.m.)
${ }^{2}$ meets peak hour traffic signal warrant (p.m.)

TABLE 15
2030 PLUS PROJECT ROADWAY SEGMENT LEVELS OF SERVICE

| Roadway | Location | Facility Classification | ATS/PTSF/LOS | ATS/PTSF/LOS |
| :---: | :---: | :---: | :---: | :---: |
|  |  |  | 2030 plus Project AM | 2030 plus Project PM |
| Midway Rd | I-80 to Porter Rd <br> EB <br> WB | Class I Highway | $\begin{aligned} & 45.3 / 47.4 / \mathrm{C} \\ & 45.1 / 61.4 / \mathrm{C} \end{aligned}$ | $\begin{aligned} & 42.6 / 72.9 / D \\ & 42.9 / 60.2 / D \end{aligned}$ |
|  | Porter Rd to SR 113 <br> EB <br> WB | Class I Highway | $\begin{aligned} & 46.5 / 44.5 / \mathrm{C} \\ & 46.5 / 44.0 / \mathrm{C} \\ & \hline \end{aligned}$ | $\begin{aligned} & 47.2 / 35.1 / \mathrm{C} \\ & 47.2 / 41.1 / \mathrm{C} \end{aligned}$ |
| SR 113 | Midway Rd to Fry Rd <br> NB <br> SB | Class I Highway | $\begin{aligned} & 44.0 / 42.8 / D \\ & 42.9 / 47.7 / D \end{aligned}$ | $\begin{aligned} & 43.4 / 54.1 / \mathrm{D} \\ & 43.4 / 53.6 / \mathrm{D} \end{aligned}$ |
|  | Fry Rd to Hay Rd <br> NB <br> SB | Class I Highway | $\begin{aligned} & 42.6 / 61.1 / D \\ & 42.8 / 49.2 / D \end{aligned}$ | $\begin{aligned} & 41.6 / 63.7 / D \\ & 41.7 / 60.7 / D \end{aligned}$ |
|  | Hay Rd to SR 12 <br> NB <br> SB | Class I Highway | $\begin{aligned} & 43.0 / 63.0 / D \\ & 43.3 / 44.4 / D \end{aligned}$ | $\begin{aligned} & 41.9 / 60.5 / D \\ & 41.7 / 66.0 / D \end{aligned}$ |
| Hay Rd | SR 113 to Daily Rd <br> EB <br> WB | Class I Highway | $\begin{aligned} & 48.7 / 19.0 / \mathrm{C} \\ & 48.9 / 31.6 / \mathrm{C} \end{aligned}$ | $\begin{gathered} 48.9 / 38.7 / \mathrm{C} \\ 48.3 / 7.6 / \mathrm{C} \end{gathered}$ |

ATS - average travel speed
PTSF - percent time spent following

## TEMPORARY BALE STORAGE OF RECYCLABLE MATERIALS

Due to recent import restrictions imposed by China on recyclable materials, baled, single-stream recyclable materials are planned to be temporarily stored at the Hay Road landfill site until the restrictions are lifted and/or new markets are developed to accept the material. The landfill site is proposing to store up to 3,680 bales for up to six months before being transported to off-site processing facilities. Each truck delivering bales would contain approximately 50 bales. The project applicant proposes to deliver on average five trucks per day and up to twenty trucks on a given day of baled recyclable materials. If deliveries were to occur daily the landfill would reach its storage limit in 4 to 15 days. It is assumed that similar shipments outbound would be made to the processing facilities or buyer, however, the potential destination of the material is not able to be determined. Trucks could return to the San Francisco Bay Area along westbound I-80, could head east toward Sacramento along eastbound I-80 or east toward Stockton via SR 12.

Because a reasonable projection of the number of vehicles (591) traveling to the landfill with implementation of the proposed project are not anticipated to exceed the daily vehicle limit (620) evaluated in this analysis, the potential additional truck trips associated with the delivery of bales to the landfill is within the modeling results identified above. A further qualitative assessment was conducted to determine what impacts the addition of five trucks per day would have on the local road system. As noted above the site could be filled in 15 days with no additional storage available until on-site material is shipped off-site. It is expected that the maximum of 20 truck shipments could occur on a rare basis, with the five-truck average being more likely, given the amount of storage space available and the expected storage time. With five trucks delivering recyclables and five trucks hauling recyclables to a processing facility this would add 10 round trip truck trips per day to the roadway network. While delivery and shipping times are unknown Recology has stated in their Bale Storage Management Plan that they would attempt to avoid peak hours to the extent possible. All bales would be shipped along I- 80 with $75 \%$ of the baled material west of the Midway Road interchange and $25 \%$ of the baled material east of the interchange. Since Recology aims to avoid the peak hours these vehicles would not be part of the intersection or roadway analyses. The additional trips would not occur every day and would be part of the daily fluctuation in traffic. Based on this information the quantitative analysis did not include these recyclable material trips. Under Existing plus Project conditions all study intersections between the I-80 / Midway Road interchange and the site have adequate capacity to accommodate additional peak hour round trips. All roadway segments will have capacity to accommodate the additional peak hour truck traffic.

If the import restriction continues through 2030 the two intersections identified under 2030 Cumulative plus Project conditions, SR 113 at Midway Road and SR 12 at SR 113, will continue to operate at LOS E or F, below Caltrans' LOS D threshold. The Midway Road segment between I-80 and Porter Road will also continue to operate below the County's LOS C threshold.

## MITIGATION MEASURES

The preceding analysis has identified project-specific and cumulative (2030) impacts that may occur without mitigation. The following discussion identifies a strategy for mitigating the impacts and contribution to impacts of the proposed project. Recommendations are identified for facilities that require improvement but the need for improvement is not a result of the proposed project. If the project causes or contributes to a significant impact, mitigations are identified for the facility.

## Existing Conditions

The SR 12 / SR 113 intersection currently operates at LOS E in the a.m. peak hour and LOS F in the p.m. peak hour. Caltrans has an identified safety project that would construct a single lane roundabout at this intersection. Construction is slated to be completed Fall 2019. Under the roundabout condition the intersection will operate at LOS A in the a.m. peak period ( 7.0 spv ) and LOS C in the p.m. peak hour ( 18.8 spv ). The remaining intersections and roadway segments operate within the Caltrans and County LOS thresholds.

## Existing Plus Project Conditions

Under Existing plus Project conditions, all intersections except the SR 12 / SR 113 intersection will operate within acceptable County and Caltrans LOS thresholds. The SR 12 / SR 113 intersection will continue to operate at LOS E in the a.m. peak hour and LOS F in the p.m. peak hour. As identified under Existing Conditions Caltrans has an identified safety project that would construct a single lane roundabout at this intersection. With this project completed the intersection will operate at LOS A in the a.m. peak hour ( 7.1 spv ) and LOS C in the p.m. peak hour ( 19.1 spv ). All roadways will continue to operate within the Caltrans and County LOS thresholds.

No additional mitigations are necessary.

## 2030 Conditions

Under 2030 conditions the SR 113 / Midway Road intersection will decline to an LOS E condition in the a.m. peak hour ( 45.7 spv ) and LOS F condition in the p.m. peak hour ( 53.6 spv ). The intersection will not meet the peak hour traffic signal warrant. The SR 12 / SR 113 intersection will decline to LOS F in the p.m. peak hour ( 124.4 spv ). One roadway segment, Midway Road between the I-80 Eastbound Ramps intersection and Porter Road will decline to LOS D in both directions. The remaining intersections and roadway segments will operate within County and Caltrans LOS thresholds.

The following recommendations are made:

## Recommendations:

- SR 113 / Midway Road: Installation of all-way stop control will improve the level of service to LOS B in both a.m. (13.3 spv) and p.m. (13.7 spv) peak hours. Caltrans has
identified a conceptual project to widen shoulders, construct a median and install a traffic signal at the SR 113 / Midway Road intersection to enhance safety; however, this project is not yet included in a planning or programming document.
- SR 12 / SR 113: Installation of a second eastbound lane through the roundabout will improve the level of service to a LOS C ( 21.5 spv ) condition in the p.m. peak hour. Caltrans would have jurisdiction over this improvement. Additionally, there is no funding mechanism for this improvement, and no agencies with jurisdiction currently have plans for any improvements at this intersection.
- Midway Road - I-80 Eastbound Ramps to Porter Road (both directions): A 0.30 mile long passing lane in both eastbound and westbound directions would be needed to improve the roadway segment to an acceptable level of service, LOS C (EB ATS - 45.1 / PTSF - 52.8; WB ATS - 45.3 / PTSF - 43.0). However, Caltrans would have jurisdiction over these improvements. Additionally, there is no funding mechanism for this improvement, and no agencies with jurisdiction currently have plans for any improvements at this intersection.

No additional recommendations are noted.

## 2030 Plus Project Conditions

The SR 113 / Midway Road intersection and the SR 12 / SR 113 intersection will continue to operate below the Caltrans LOS D threshold with implementation of the project. Additionally, both directions of Midway Road, between the I-80 Eastbound Ramps intersection and Porter Road will operate at LOS D with implementation of the project. The remaining intersections and all roadway segments will operate within County and Caltrans LOS thresholds. The following mitigation measures have been identified for the aforementioned facilities to which the project would contribute to unacceptable LOS:

## Mitigations:

- SR 113 / Midway Road: As identified in the 2030 No Project Recommendations installation of all-way stop control will improve the level of service to LOS B in both a.m. ( 13.7 spv ) and p.m. (13.8 spv) peak hours. This intersection is under the jurisdiction of Caltrans, and Caltrans has identified a conceptual project to widen shoulders, construct a median and install a traffic signal at the SR 113 / Midway Road intersection to enhance safety. However, this project is not yet included in a planning or programming document. Any improvement of the intersection would require Caltrans concurrence and approval. The project applicant and Solano County shall coordinate with Caltrans on implementation of this improvement. However, because the final approval of the proposed improvement is outside the jurisdiction and control of the Applicant and County, there is no guarantee that this mitigation measure would be implemented prior to project-related trips occurring at this intersection. Therefore, this is considered a significant and unavoidable impact.
- SR 12 / SR 113: As identified in the 2030 No Project Recommendations installation of a second eastbound lane through the roundabout will improve the level of service to a LOS C ( 21.7 spv ) condition in the p.m. peak hour. This improvement is under the jurisdiction of Caltrans. Any improvement of the intersection would require Caltrans concurrence and approval. The project applicant and Solano County shall coordinate with Caltrans on implementation of this improvement. However, because the final approval of the proposed improvement is outside the jurisdiction and control of the Applicant and County, there is no guarantee that this mitigation measure would be implemented prior to project-related trips occurring at this intersection. Additionally, Caltrans does not currently have plans for any improvements at this intersection. Therefore, this is considered a significant and unavoidable impact.
- Midway Road - I-80 Eastbound Ramps to Porter Road (both directions): As identified in the 2030 No Project Recommendations a 0.30 mile long passing lane in both eastbound and westbound directions would be needed to improve the roadway segment LOS to an acceptable level of LOS C (EB ATS - $45.0 /$ PTSF - 53.2; WB ATS - 45.2 / PTSF 43.7). This improvement is under the jurisdiction of Solano County. The project applicant shall coordinate with Solano County and shall fund the improvement of this segment to be constructed prior to vehicle trips to the landfill exceeding 2,400 per day. Therefore, with mitigation, this is considered a less-than-significant impact.

No additional mitigations are identified.

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## APPENDIX

## (under separate cover)

# TECHNICAL APPENDIX 

## FOR

# RECOLOGY HAY ROAD LANDFILL EXPANSION PROJECT TRAFFIC IMPACT ANALYSIS 

Solano County, CA

Prepared For:

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December 5, 2018


0563-002



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 3.5 |  |  |  |  |  |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations |  |  | F |  | F |  |
| Traffic Vol, veh/h | 5 |  | 44 | 192 | 95 | 60 |
| Future Vol, veh/h | 5 | 102 | 44 | 192 | 95 | 60 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | - | 0 | 0 | - | 0 | - |
| Grade, \% | - | 0 | 0 | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 7 | 7 | 2 |
| Mvmt Flow | 5 | 111 | 48 | 209 | 103 | 65 |


| Major/Minor | Major1 | Major2 |  |  |  |  |  | Minor2 |  |  |
| :--- | ---: | :--- | ---: | :--- | ---: | ---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 257 | 0 | - | 0 | 274 | 153 |  |  |  |  |
| $\quad$ Stage 1 | - | - | - | - | 153 | - |  |  |  |  |
| $\quad$ Stage 2 | - | - | - | - | 121 | - |  |  |  |  |
| Critical Hdwy | 4.12 | - | - | - | 6.47 | 6.22 |  |  |  |  |
| Critical Hdwy Stg 1 | - | - | - | - | 547 | - |  |  |  |  |
| Critical Hdwy Stg 2 | - | - | - | -5.47 | - |  |  |  |  |  |
| Follow-up Hdwy | 2.218 | - | - | -3.563 | 3.318 |  |  |  |  |  |
| Pot Cap-1 Maneuver | 1308 | - | - | -705 | 893 |  |  |  |  |  |
| $\quad$ Stage 1 | - | - | - | - | 863 | - |  |  |  |  |


| Stage 2 | - | - | - | - | 892 |
| :---: | :---: | :---: | :---: | :---: | ---: |
| Platoon blocked, \% |  | - | - | - |  |
| Mov Cap-1 Maneuver | 1308 | - | - | - | 702 |
| Mov Cap-2 Maneuver | - | - | - | - | 702 |
| Stage 1 | - | - | - | - |  |
| Stage 2 | - | - | - | -860 | - |
|  |  |  |  |  |  |


| Approach | EB | WB | SB |
| :--- | :---: | :---: | :---: |
| HCM Control Delay, s | 0.4 | 0 | 11 |
| HCM LOS |  |  | B |


| Minor Lane/Major Mvmt | EBL | EBT | WBT | WBR SBLn1 |
| :--- | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 1308 | - | - | - |
| 665 |  |  |  |  |
| HCM Lane V/C Ratio | 0.004 | - | - | - |
| HCM Control Delay (s) | 7.8 | 0 | - | - |
| HCM Lane LOS | A | A | - | - |
| HCM 95 th \%tile Q(veh) | 0 | - | - | - |
| H | 0.8 |  |  |  |









| Major/Minor | Minor2 | Major1 | Major2 |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Conflicting Flow All | 443 | 157 | 172 | 0 | - | 0 |
| $\quad$ Stage 1 | 157 | - | - | - | - | - |
| Stage 2 | 286 | - | - | - | - | - |
| Critical Hdwy | 6.47 | 6.22 | 4.12 | - | - | - |
| Critical Hdwy Stg 1 | 5.47 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.47 | - | - | - | - | - |
| Follow-up Hdwy | 3.563 | 3.318 | 2.218 | - | - | - |
| Pot Cap-1 Maneuver | 563 | 889 | 1405 | - | - | - |
| $\quad$ Stage 1 | 859 | - | - | - | - | - |
| $\quad$ Stage 2 | 751 | - | - | - | - | - |
| Platoon blocked, \% |  |  |  | - | - | - |
| Mov Cap-1 Maneuver | 555 | 889 | 1405 | - | - | - |
| Mov Cap-2 Maneuver | 555 | - | - | - | - | - |
| Stage 1 | 847 | - | - | - | - | - |
| Stage 2 | 751 | - | - | - | - | - |


| Approach | EB | NB | SB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s | 10.6 | 0.5 | 0 |

## HCMLOS B

| Minor Lane/Major Mvmt | NBL | NBT EBLn1 | SBT | SBR |  |
| :--- | ---: | ---: | ---: | ---: | :--- |
| Capacity (veh/h) | 1405 | -670 | - | - |  |
| HCM Lane V/C Ratio | 0.012 | -0.039 | - | - |  |
| HCM Control Delay (s) | 7.6 | 0 | 10.6 | - | - |
| HCM Lane LOS | A | A | B | - | - |
| HCM 95th \%tile Q(veh) | 0 | - | 0.1 | - | - |




| Minor Lane/Major Mvmt | NBLn1 NBLn2 | EBL | EBT | EBR | WBL | WBT | WBR SBLn1 SBLn2 |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 190 | 802 | 742 | - | -1327 | - | -1235 | 460 |  |
| HCM Lane V/C Ratio | 0.006 | 0.007 | - | - | -0.016 | - | -0.578 | 0.007 |  |
| HCM Control Delay (s) | 24.1 | 9.5 | 0 | - | - | 7.8 | - | -39.4 | 12.9 |
| HCM Lane LOS | C | A | A | - | - | A | - | - | E | B


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 4.6 |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | $\uparrow$ |  |  | $\mathbf{7}$ | Mr |  |
| Traffic Vol, veh/h | 8 | 49 | 30 | 14 | 36 | 17 |
| Future Vol, veh/h | 8 | 49 | 30 | 14 | 36 | 17 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 9 | 53 | 33 | 15 | 39 | 18 |





| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 2.5 |  |  |  |  |  |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations |  | $\neq$ | $\uparrow$ |  | Mr |  |
| Traffic Vol, veh/h | 10 | 143 | 51 | 122 | 22 | 78 |
| Future Vol, veh/h | 10 | 143 | 51 | 122 | 22 | 78 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | - | 0 | 0 | - | 0 | - |
| Grade, \% | - | 0 | 0 | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 7 | 7 | 2 |
| Mvmt Flow | 11 | 155 | 55 | 133 | 24 | 85 |


| Major/Minor | Major1 | Major2 |  | Minor2 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 188 | 0 | - | 0 | 299 | 122 |
| Stage 1 |  |  |  |  | 122 |  |
| Stage 2 | - |  |  |  | 177 |  |
| Critical Hdwy | 4.12 | - | - | - | 6.47 | 6.22 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.47 |  |
| Critical Hdwy Stg 2 |  | - | - | - | 5.47 |  |
| Follow-up Hdwy | 2.218 | - |  |  | 3.563 | 3.318 |
| Pot Cap-1 Maneuver | 1386 |  |  |  | 682 | 929 |
| Stage 1 | - | - | - | - | 891 |  |
| Stage 2 | - | - | - | - | 842 |  |
| Platoon blocked, \% |  |  | - | - |  |  |
| Mov Cap-1 Maneuver | 1386 | - | - |  | 676 | 929 |
| Mov Cap-2 Maneuver | - |  | - |  | 676 |  |
| Stage 1 |  | - | - |  | 883 |  |
| Stage 2 | - | - | - | - | 842 |  |


| Approach | EB | WB | SB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s | 0.5 | 0 | 9.8 |
| HCM LOS |  |  | A |


| Minor Lane/Major Mvmt | EBL | EBT | WBT | WBR SBLn1 |
| :--- | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 1386 | - | - | -858 |
| HCM Lane V/C Ratio | 0.008 | - | - | -0.127 |
| HCM Control Delay (s) | 7.6 | 0 | - | - |
| HCM Lane LOS | A | A | - | - |
| HCM 95th \%tile Q(veh) | 0 | - | - | - |
| A | 0.4 |  |  |  |


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 1.8 |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |  |
| Lane Configurations |  | $\uparrow$ |  |  | $\hat{\square}$ |  |  | $\uparrow$ | 「 |  |  |  |  |
| Traffic Vol, veh/h | 72 | 76 | 0 | 0 | 150 | 112 | 13 | 1 | 227 | 0 | 0 | 0 |  |
| Future Vol, veh/h | 72 | 76 | 0 | 0 | 150 | 112 | 13 | 1 | 227 | 0 | 0 | 0 |  |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Sign Control F | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Free | Free | Free |  |
| RT Channelized | - | - | None | - | - | None | - | - | Free | - | - | None |  |
| Storage Length | - | - | - | - | - | - | 50 | - | 0 | - | - | - |  |
| Veh in Median Storage, \# | \# | 0 | - | - | 0 | - | - | 0 | - |  | 6965 | - |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |  |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |  |
| Heavy Vehicles, \% | 7 | 7 | 2 | 2 | 7 | 7 | 7 | 2 | 7 | 2 | 2 | 2 |  |
| Mvmt Flow | 78 | 83 | 0 | 0 | 163 | 122 | 14 | 1 | 247 | 0 | 0 | 0 |  |





| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 4.9 |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | \& |  |  | $\uparrow$ |  | ${ }^{*}$ | 个 |  | ${ }^{1 /}$ | $\uparrow$ |  |
| Traffic Vol, veh/h | 12 | 27 | 11 | 80 | 24 | 15 | 24 | 111 | 48 | 22 | 94 | 56 |
| Future Vol, veh/h | 12 | 27 | 11 | 80 | 24 | 15 | 24 | 111 | 48 | 22 | 94 | 56 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | - | - | - | - | 120 | - | - | 120 | - | - |
| Veh in Median Storage, \# | \# | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 7 | 2 | 2 | 2 | 7 | 7 | 2 | 2 | 7 | 2 |
| Mvmt Flow | 13 | 29 | 12 | 87 | 26 | 16 | 26 | 121 | 52 | 24 | 102 | 61 |




| Major/Minor | Minor2 | Major1 |  | Major2 |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Conflicting Flow All | 521 | 263 | 264 | 0 | - | 0 |
| $\quad$ Stage 1 | 263 | - | - | - | - | - |
| Stage 2 | 258 | - | - | - | - | - |
| Critical Hdwy | 6.47 | 6.22 | 4.12 | - | - | - |
| Critical Hdwy Stg 1 | 5.47 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.47 | - | - | - | - | - |
| Follow-up Hdwy | 3.563 | 3.318 | 2.218 | - | - | - |
| Pot Cap-1 Maneuver | 507 | 776 | 1300 | - | - | - |
| $\quad$ Stage 1 | 770 | - | - | - | - | - |
| $\quad$ Stage 2 | 774 | - | - | - | - | - |
| Platoon blocked, \% |  |  |  | - | - | - |
| Mov Cap-1 Maneuver | 501 | 776 | 1300 | - | - | - |
| Mov Cap-2 Maneuver | 501 | - | - | - | - | - |
| Stage 1 | 762 | - | - | - | - | - |
| Stage 2 | 774 | - | - | - | - | - |


| Approach | EB | NB | SB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s | 12.1 | 0.4 | 0 |
| HCM LOS | B |  |  |


| Minor Lane/Major Mvmt | NBL | NBT EBLn1 | SBT | SBR |  |
| :--- | ---: | ---: | ---: | ---: | :--- |
| Capacity (veh/h) | 1300 | -576 | - | - |  |
| HCM Lane V/C Ratio | 0.009 | -0.123 | - | - |  |
| HCM Control Delay (s) | 7.8 | 0 | 12.1 | - | - |
| HCM Lane LOS | A | A | B | - | - |
| HCM 95th \%tile Q(veh) | 0 | - | 0.4 | - | - |



| Major/Minor $\quad$ N | Major1 | Major2 |  |  |  | Minor1 |  |  |  | Minor2 |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 547 | 0 | 0 | 784 | 0 |  | 0 | 1248 | 1351 | 782 | 1149 | 1140 | 334 |  |
| Stage 1 | - | - | - |  | - |  |  | 796 | 796 |  | 342 | 342 |  |  |
| Stage 2 | - | - | - |  | - |  | - | 452 | 555 |  | 807 | 798 |  |  |
| Critical Hdwy | 4.17 | - | - | 4.12 | - |  |  | 7.12 | 6.52 | 6.22 | 7.17 | 6.52 | 6.27 |  |
| Critical Hdwy Stg 1 | - | - | - | - | - |  |  | 6.12 | 5.52 | - | 6.17 | 5.52 | - |  |
| Critical Hdwy Stg 2 | - | - | - | - | - |  |  | 6.12 | 5.52 | - | 6.17 | 5.52 | - |  |
| Follow-up Hdwy | 2.263 | - |  | 2.218 | - |  |  | - 3.518 | 4.018 | 3.318 | 3.563 | 4.018 | 3.363 |  |
| Pot Cap-1 Maneuver | 998 | - | - | 834 | - |  | - | 150 | 150 | 394 | $\sim 172$ | 201 | 697 |  |
| Stage 1 | - | - | - | - | - |  |  | 380 | 399 |  | 663 | 638 | - |  |
| Stage 2 | - | - | - | - | - |  |  | 587 | 513 | - | 368 | 398 | - |  |
| Platoon blocked, \% |  | - | - |  | - |  | - |  |  |  |  |  |  |  |
| Mov Cap-1 Maneuver | 998 | - | - | 834 | - |  | - | 146 | 148 | 394 | ~160 | 199 | 697 |  |
| Mov Cap-2 Maneuver | - | - | - | - | - |  | - | 146 | 148 |  | ~160 | 199 | - |  |
| Stage 1 | - | - | - | - | - |  |  | 377 | 396 |  | 658 | 635 | - |  |
| Stage 2 | - | - | - | - | - |  |  | 578 | 510 | - | 346 | 395 | - |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Approach | EB |  |  | WB |  |  |  | NB |  |  | SB |  |  |  |
| HCM Control Delay, s | 0.1 |  |  | 0.1 |  |  |  | 17.8 |  |  | \$ 373.3 |  |  |  |
| HCM LOS |  |  |  |  |  |  |  | C |  |  | F |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | NBLn1 | NBLn2 | EBL | EBT |  | EBR | WBL | WBT | WBR | SBLn1 | SBLn2 |  |  |
| Capacity (veh/h) |  | 148 | 394 | 998 | - |  | - | - 834 | - | - | 160 | 697 |  |  |
| HCM Lane V/C Ratio |  | 0.029 | 0.041 | 0.007 | - |  | - | - 0.005 | - | - | 1.678 | 0.008 |  |  |
| HCM Control Delay (s) |  | 30.1 | 14.5 | 8.6 | - |  | - | 9.3 | - |  | \$ 380.7 | 10.2 |  |  |
| HCM Lane LOS |  | D | B | A | - |  | - | A | - |  | F | B |  |  |
| HCM 95th \%tile Q(veh) |  | 0.1 | 0.1 | 0 | - |  | - | 0 | - | - | 18.9 | 0 |  |  |
| Notes |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| $\sim$ : Volume exceeds cap | pacity | \$: De | lay exc | ceeds |  |  | Com | mputation | Not D | efined | *: All | major v | volume | in platoon |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |





| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |






| Major/Minor $\quad$ M | Major1 |  | Major2 |  | Minor1 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 0 | 0 | 67 | 0 | 68 | 41 |  |
| Stage 1 | - | - | - | - | 41 | - |  |
| Stage 2 | - | - | - | - | 27 | - |  |
| Critical Hdwy | - | - | 4.12 | - | 6.42 | 6.22 |  |
| Critical Hdwy Stg 1 | - | - | - |  | 5.42 | - |  |
| Critical Hdwy Stg 2 | - | - | - |  | 5.42 | - |  |
| Follow-up Hdwy | - |  | 2.218 |  | 3.518 | 3.318 |  |
| Pot Cap-1 Maneuver | - | - | 1535 | - | 937 | 1030 |  |
| Stage 1 | - | - | - |  | 981 | - |  |
| Stage 2 | - | - | - |  | 996 | - |  |
| Platoon blocked, \% | - | - |  | - |  |  |  |
| Mov Cap-1 Maneuver | - | - | 1535 |  | 932 | 1030 |  |
| Mov Cap-2 Maneuver | - | - | - |  | 932 | - |  |
| Stage 1 | - | - | - |  | 976 | - |  |
| Stage 2 | - | - | - |  | 996 | - |  |
|  |  |  |  |  |  |  |  |
| Approach | EB |  | WB |  | NB |  |  |
| HCM Control Delay, s | 0 |  | 3 |  | 9 |  |  |
| HCM LOS |  |  |  |  | A |  |  |
|  |  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | NBLn1 | EBT | EBR WBL WBT |  |  |  |
| Capacity (veh/h) |  | 55 | - | - | 1535 | - |  |
| HCM Lane V/C Ratio |  |  | - |  | 0.005 | - |  |
| HCM Control Delay (s) |  | 9 | - | - | 7.4 | 0 |  |
| HCM Lane LOS |  | A | - | - | A | A |  |
| HCM 95th \%tile Q(veh) |  | 0.2 | - | - | 0 | - |  |





| Major/Minor | Major1 | Major2 | Minor2 |  |
| :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 270 | 0 | 0280 | 159 |
| Stage 1 | - | - - | 159 |  |
| Stage 2 | - | - - | 121 |  |
| Critical Hdwy | 4.12 | - - | - 6.47 | 6.22 |
| Critical Hdwy Stg 1 |  | - - | - 5.47 |  |
| Critical Hdwy Stg 2 |  | - - | 5.47 |  |
| Follow-up Hdwy | 2.218 | - - | - 3.563 | 3.318 |
| Pot Cap-1 Maneuver | 1293 | - - | - 699 | 886 |
| Stage 1 |  | - - | - 858 |  |


| Stage 2 | - | - | - | - | 892 | - |
| :---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Platoon blocked, \% |  | - | - | - |  |  |
| Mov Cap-1 Maneuver | 1293 | - | - | - | 696 | 886 |
| Mov Cap-2 Maneuver | - | - | - | - | 696 | - |
| Stage 1 | - | - | - | - | 855 | - |
| Stage 2 | - | - | - | - | 892 | - |


| Approach | EB | WB | SB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s | 0.4 | 0 | 11.1 |

HCMLOS B

| Minor Lane/Major Mvmt | EBL | EBT | WBT | WBR SBLn1 |  |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 1293 | - | - | -759 |  |
| HCM Lane V/C Ratio | 0.004 | - | - | -0.222 |  |
| HCM Control Delay (s) | 7.8 | 0 | - | -11.1 |  |
| HCM Lane LOS | A | A | - | - | B |
| HCM 95th \%tile Q(veh) | 0 | - | - | - | 0.8 |





| Major/Minor | Minor1 | Major1 | Major2 |  |  |
| :--- | ---: | ---: | ---: | ---: | :--- |
| Conflicting Flow All | 1 | 0 | 0 | - | - |
| Stage 1 | 0 | - | - | - | - |
| $\quad$ Stage 2 | 1 | - | - | - | - |


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 6.4 |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |  |
| Lane Configurations |  | ¢ |  |  | ¢ |  | \% | F |  | \% | F |  |  |
| Traffic Vol, veh/h | 128 | 19 | 36 | 15 | 23 | 13 | 37 | 89 | 18 | 14 | 78 | 95 |  |
| Future Vol, veh/h | 128 | 19 | 36 | 15 | 23 | 13 | 37 | 89 | 18 | 14 | 78 | 95 |  |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Sign Control St | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |  |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |  |
| Storage Length | - | - | - | - | - | - | 120 | - | - | 120 | - | - |  |
| Veh in Median Storage, \# | \# | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |  |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |  |
| Heavy Vehicles, \% | 2 | 2 | 7 | 2 | 2 | 2 | 7 | 7 | 2 | 2 | 7 | 2 |  |
| Mvmt Flow | 139 | 21 | 39 | 16 | 25 | 14 | 40 | 97 | 20 | 15 | 85 | 103 |  |



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |





| Minor Lane/Major Mvmt | NBLn1 NBLn2 | EBL | EBT | EBR | WBL | WBT | WBR SBLn1 SBLn2 |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 190 | 802 | 740 | - | -1327 | - | -235 | 460 |  |
| HCM Lane V/C Ratio | 0.006 | 0.007 | - | - | -0.016 | - | -0.587 | 0.007 |  |
| HCM Control Delay (s) | 24.1 | 9.5 | 0 | - | - | 7.8 | - | - | 40 |
| 12.9 |  |  |  |  |  |  |  |  |  |
| HCM Lane LOS | C | A | A | - | - | A | - | - | E | B


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 5.3 |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | $\mathbf{F}$ |  |  | $\uparrow$ |  |  |
| Traffic Vol, veh/h | 8 | 54 | 51 | 14 | 40 | 32 |
| Future Vol, veh/h | 8 | 54 | 51 | 14 | 40 | 32 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - None | - | None |  |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, $\%$ | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 9 | 59 | 55 | 15 | 43 | 35 |

Stage 2 - - - - 901

| Approach | EB | WB | NB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s | 0 | 5.8 | 9.5 |

HCMLOS A




| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 2.4 |  |  |  |  |  |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations |  | $\neq$ | 1 |  | M |  |
| Traffic Vol, veh/h | 10 | 143 | 51 | 134 | 22 | 78 |
| Future Vol, veh/h | 10 | 143 | 51 | 134 | 22 | 78 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | - | 0 | 0 | - | 0 | - |
| Grade, \% | - | 0 | 0 | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 7 | 7 | 2 |
| Mvmt Flow | 11 | 155 | 55 | 146 | 24 | 85 |





| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 8.8 |  |  |  |  |  |
| Movement | NBL | NBR | NET | NER | SWL | SWT |
| Lane Configurations | $\mathbf{1}$ | $\mathbf{T}$ | $\mathbf{4}$ |  |  | 4 |
| Traffic Vol, veh/h | 75 | 0 | 0 | 0 | 0 | 0 |
| Future Vol, veh/h | 75 | 0 | 0 | 0 | 0 | 0 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | 50 | - | - | - | - |
| Veh in Median Storage, | 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 7 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 82 | 0 | 0 | 0 | 0 | 0 |





| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 2 |  |  |  |  |  |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | Mr |  |  | $\uparrow$ | $\uparrow$ |  |
| Traffic Vol, veh/h | 55 | 28 | 11 | 215 | 240 | 4 |
| Future Vol, veh/h | 55 | 28 | 11 | 215 | 240 | 4 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 7 | 2 | 2 | 7 | 7 | 7 |
| Mvmt Flow | 60 | 30 | 12 | 234 | 261 | 4 |



| Approach | EB | NB | SB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s | 12.5 | 0.4 | 0 |
| HCM LOS | B |  |  |


| Minor Lane/Major Mvmt | NBL | NBT EBLn1 | SBT | SBR |  |
| :--- | ---: | ---: | ---: | ---: | :--- |
| Capacity (veh/h) | 1299 | -569 | - | - |  |
| HCM Lane V/C Ratio | 0.009 | -0.159 | - | - |  |
| HCM Control Delay (s) | 7.8 | 0 | 12.5 | - | - |
| HCM Lane LOS | A | A | B | - | - |
| HCM 95th \%tile Q(veh) | 0 | - | 0.6 | - | - |



| Major/Minor $\quad$ N | Major1 | Major2 |  |  |  |  | Minor1 |  |  | Minor2 |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 547 | 0 | 0 | 784 | 0 |  | 0 | 1250 | 1351 | 782 | 1149 | 1140 | 334 |  |
| Stage 1 | - | - | - |  | - |  |  | 796 | 796 |  | 342 | 342 |  |  |
| Stage 2 | - | - | - |  | - |  | - | 454 | 555 |  | 807 | 798 |  |  |
| Critical Hdwy | 4.17 | - | - | 4.12 | - |  |  | 7.12 | 6.52 | 6.22 | 7.17 | 6.52 | 6.27 |  |
| Critical Hdwy Stg 1 | - | - | - | - | - |  |  | 6.12 | 5.52 | - | 6.17 | 5.52 | - |  |
| Critical Hdwy Stg 2 | - | - | - | - | - |  |  | 6.12 | 5.52 | - | 6.17 | 5.52 | - |  |
| Follow-up Hdwy | 2.263 | - |  | 2.218 | - |  |  | - 3.518 | 4.018 | 3.318 | 3.563 | 4.018 | 3.363 |  |
| Pot Cap-1 Maneuver | 998 | - | - | 834 | - |  | - | 150 | 150 | 394 | $\sim 172$ | 201 | 697 |  |
| Stage 1 | - | - | - | - | - |  |  | 380 | 399 |  | 663 | 638 | - |  |
| Stage 2 | - | - | - | - | - |  |  | 586 | 513 | - | 368 | 398 | - |  |
| Platoon blocked, \% |  | - | - |  | - |  | - |  |  |  |  |  |  |  |
| Mov Cap-1 Maneuver | 998 | - | - | 834 | - |  | - | 146 | 148 | 394 | ~160 | 199 | 697 |  |
| Mov Cap-2 Maneuver | - | - | - | - | - |  | - | 146 | 148 |  | ~160 | 199 | - |  |
| Stage 1 | - | - | - | - | - |  |  | 377 | 396 |  | 658 | 635 | - |  |
| Stage 2 | - | - | - | - | - |  |  | 575 | 510 | - | 346 | 395 | - |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Approach | EB |  |  | WB |  |  |  | NB |  |  | SB |  |  |  |
| HCM Control Delay, s | 0.1 |  |  | 0.1 |  |  |  | 17.8 |  |  | \$ 376.1 |  |  |  |
| HCM LOS |  |  |  |  |  |  |  | C |  |  | F |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | NBLn1 | NBLn2 | EBL | EBT |  | EBR | WBL | WBT | WBR | SBLn1 | SBLn2 |  |  |
| Capacity (veh/h) |  | 148 | 394 | 998 | - |  | - | - 834 | - | - | 160 | 697 |  |  |
| HCM Lane V/C Ratio |  | 0.029 | 0.041 | 0.007 | - |  | - | - 0.005 | - | - | 1.692 | 0.011 |  |  |
| HCM Control Delay (s) |  | 30.1 | 14.5 | 8.6 | - |  | - | 9.3 | - |  | \$ 386.4 | 10.2 |  |  |
| HCM Lane LOS |  | D | B | A | - |  | - | A | - |  | F | B |  |  |
| HCM 95th \%tile Q(veh) |  | 0.1 | 0.1 | 0 | - |  | - | 0 | - | - | 19.1 | 0 |  |  |
| Notes |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| $\sim$ : Volume exceeds cap | pacity | \$: De | lay exc | ceeds |  |  | Com | mputation | Not D | efined | *: All | major v | volume | in platoon |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 5.8 |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | $\uparrow$ |  |  | $\mathbf{7}$ | Mr |  |
| Traffic Vol, veh/h | 28 | 20 | 18 | 15 | 51 | 47 |
| Future Vol, veh/h | 28 | 20 | 18 | 15 | 51 | 47 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 30 | 22 | 20 | 16 | 55 | 51 |




| Major/Minor | Minor2 | Minor1 |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Conflicting Flow All | 237 | 229 | 80 | 241 | 242 | 72 | 98 | 0 | 0 | 77 | 0 |
| $\quad$ Stage 1 | 96 | 96 | - | 128 | 128 | - | - | - | - | - | - |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |







## MOVEMENT SUMMARY

Site: 7 [SR 12 / SR 113]
Cumulative AM
Site Category: (None)
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ |  | Deman Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed mph |
| South: Birds Landing Rd |  |  |  |  |  |  |  |  |  |  |  |  |
| 3 | L2 | 5 | 3.0 | 0.032 | 7.5 | LOS A | 0.1 | 2.6 | 0.56 | 0.52 | 0.56 | 33.0 |
| 8 | T1 | 5 | 3.0 | 0.032 | 7.5 | LOS A | 0.1 | 2.6 | 0.56 | 0.52 | 0.56 | 33.0 |
| 18 | R2 | 5 | 3.0 | 0.032 | 7.5 | LOS A | 0.1 | 2.6 | 0.56 | 0.52 | 0.56 | 32.0 |
| Appr |  | 16 | 3.0 | 0.032 | 7.5 | LOS A | 0.1 | 2.6 | 0.56 | 0.52 | 0.56 | 32.7 |
| East: SR 12 |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 16 | 3.0 | 0.858 | 17.2 | LOS C | 11.8 | 317.6 | 0.23 | 0.06 | 0.23 | 29.6 |
| 6 | T1 | 1201 | 10.0 | 0.858 | 17.3 | LOS C | 11.8 | 317.6 | 0.23 | 0.06 | 0.23 | 29.5 |
| 16 | R2 | 250 | 7.0 | 0.858 | 17.2 | LOS C | 11.8 | 317.6 | 0.23 | 0.06 | 0.23 | 28.7 |
| Appr |  | 1467 | 9.4 | 0.858 | 17.3 | LOS C | 11.8 | 317.6 | 0.23 | 0.06 | 0.23 | 29.3 |
| North: SR 113 |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 217 | 7.0 | 0.847 | 61.4 | LOS F | 5.7 | 150.1 | 0.93 | 1.36 | 2.57 | 18.2 |
| 4 | T1 | 5 | 3.0 | 0.847 | 60.9 | LOS F | 5.7 | 150.1 | 0.93 | 1.36 | 2.57 | 18.2 |
| 14 | R2 | 11 | 7.0 | 0.847 | 61.4 | LOS F | 5.7 | 150.1 | 0.93 | 1.36 | 2.57 | 17.9 |
| Appr |  | 234 | 6.9 | 0.847 | 61.4 | LOS F | 5.7 | 150.1 | 0.93 | 1.36 | 2.57 | 18.2 |
| West: SR 12 |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 | L2 | 5 | 7.0 | 0.574 | 12.3 | LOS B | 4.4 | 117.8 | 0.54 | 0.55 | 0.74 | 31.5 |
| 2 | T1 | 489 | 10.0 | 0.574 | 12.4 | LOS B | 4.4 | 117.8 | 0.54 | 0.55 | 0.74 | 31.5 |
| 12 | R2 | 5 | 3.0 | 0.574 | 12.1 | LOS B | 4.4 | 117.8 | 0.54 | 0.55 | 0.74 | 30.8 |
| Approach |  | 500 | 9.9 | 0.574 | 12.4 | LOS B | 4.4 | 117.8 | 0.54 | 0.55 | 0.74 | 31.5 |
| All V | icles | 2217 | 9.2 | 0.858 | 20.8 | LOS C | 11.8 | 317.6 | 0.38 | 0.31 | 0.60 | 27.9 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Roundabout LOS Method: Same as Sign Control.
Vehicle movement LOS values are based on average delay and $\mathrm{v} / \mathrm{c}$ ratio (degree of saturation) per movement.
LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 6).
Roundabout Capacity Model: US HCM 2010.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies. Gap-Acceptance Capacity: Traditional M1.
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |




| Major/Minor | Major1 | Major2 |  | Minor2 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 375 | 0 |  | 0 | 419 | 223 |
| Stage 1 | - | - |  | - | 223 |  |
| Stage 2 | - | - | - | - | 196 |  |
| Critical Hdwy | 4.12 | - | - | - | 6.47 | 6.22 |
| Critical Hdwy Stg 1 | - | - |  | - | 5.47 |  |
| Critical Hdwy Stg 2 | - | - |  | - | 5.47 |  |
| Follow-up Hdwy | 2.218 | - |  |  | 3.563 | 3.318 |
| Pot Cap-1 Maneuver | 1183 | - | - | - | 581 | 817 |
| Stage 1 | - | - | - | - | 802 |  |
| Stage 2 | - | - | - | - | 825 |  |
| Platoon blocked, \% |  | - |  |  |  |  |
| Mov Cap-1 Maneuver | 1183 | - |  |  | 575 | 817 |
| Mov Cap-2 Maneuver | - | - | - | - |  |  |
| Stage 1 | - | - |  |  | 794 |  |
| Stage 2 | - | - | - | - | 825 |  |


| Approach | EB | WB | SB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s | 0.5 | 0 | 13.3 |
| HCM LOS |  |  | B |


| Minor Lane/Major Mvmt | EBL | EBT | WBT | WBR SBLn1 |
| :--- | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 1183 | - | - | -640 |
| HCM Lane V/C Ratio | 0.009 | - | - | -0.323 |
| HCM Control Delay (s) | 8.1 | 0 | - | -13.3 |
| HCM Lane LOS | A | A | - | - |
| HCM 95th \%tile Q(veh) | 0 | - | - | -1.4 |








| Minor Lane/Major Mvmt | NBL | NBT | NBR EBLn1WBLn1 | SBL | SBT | SBR |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 1211 | - | -340 | 464 | 1339 | - | - |
| HCM Lane V/C Ratio | 0.022 | - | -0.719 | 0.305 | 0.028 | - | - |
| HCM Control Delay (s) | 8 | - | - | 38.5 | 16.1 | 7.8 | - |
| HCM Lane LOS | A | - | - | E | C | A | - |
| HCM 95th \%tile Q(veh) | 0.1 | - | - | 5.3 | 1.3 | 0.1 | - |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 1.1 |  |  |  |  |  |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | Mr |  |  | - | F |  |
| Traffic Vol, veh/h | 25 | 20 | 30 | 420 | 235 | 50 |
| Future Vol, veh/h | 25 | 20 | 30 | 420 | 235 | 50 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 7 | 2 | 2 | 7 | 7 | 7 |
| Mvmt Flow | 27 | 22 | 33 | 457 | 255 | 54 |





## MOVEMENT SUMMARY

Site: 7 [SR 12 / SR 113]
Cumulative PM
Site Category: (None)
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \text { Mov } \\ \text { ID } \end{gathered}$ | Turn | Deman Total veh/h | $\begin{array}{r} \text { Flows } \\ \text { HV } \\ \% \end{array}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back <br> Vehicles <br> veh | of Queue Distance ft | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed mph |
| South: Birds Landing Rd |  |  |  |  |  |  |  |  |  |  |  |  |
| 3 | L2 | 5 | 3.0 | 0.088 | 13.2 | LOS B | 0.3 | 6.7 | 0.74 | 0.74 | 0.74 | 30.8 |
| 8 | T1 | 11 | 3.0 | 0.088 | 13.2 | LOS B | 0.3 | 6.7 | 0.74 | 0.74 | 0.74 | 30.8 |
| 18 | R2 | 11 | 3.0 | 0.088 | 13.2 | LOS B | 0.3 | 6.7 | 0.74 | 0.74 | 0.74 | 30.0 |
| Appr |  | 27 | 3.0 | 0.088 | 13.2 | LOS B | 0.3 | 6.7 | 0.74 | 0.74 | 0.74 | 30.4 |
| East: SR 12 |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 5 | 3.0 | 0.685 | 10.7 | LOS B | 5.4 | 145.8 | 0.24 | 0.09 | 0.24 | 32.3 |
| 6 | T1 | 647 | 10.0 | 0.685 | 10.9 | LOS B | 5.4 | 145.8 | 0.24 | 0.09 | 0.24 | 32.1 |
| 16 | R2 | 375 | 7.0 | 0.685 | 10.8 | LOS B | 5.4 | 145.8 | 0.24 | 0.09 | 0.24 | 31.3 |
| Appr |  | 1027 | 8.9 | 0.685 | 10.9 | LOS B | 5.4 | 145.8 | 0.24 | 0.09 | 0.24 | 31.8 |
| North: SR 113 |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 321 | 7.0 | 0.709 | 25.8 | LOS D | 5.5 | 146.2 | 0.79 | 1.08 | 1.72 | 25.3 |
| 4 | T1 | 22 | 3.0 | 0.709 | 25.6 | LOS D | 5.5 | 146.2 | 0.79 | 1.08 | 1.72 | 25.3 |
| 14 | R2 | 22 | 7.0 | 0.709 | 25.8 | LOS D | 5.5 | 146.2 | 0.79 | 1.08 | 1.72 | 24.7 |
| Approach |  | 364 | 6.8 | 0.709 | 25.8 | LOS D | 5.5 | 146.2 | 0.79 | 1.08 | 1.72 | 25.3 |
| West: SR 12 |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 | L2 | 33 | 7.0 | 1.499 | 245.7 | LOS F | 162.5 | 4380.5 | 1.00 | 5.40 | 11.51 | 7.4 |
| 2 | T1 | 1223 | 10.0 | 1.499 | 245.8 | LOS F | 162.5 | 4380.5 | 1.00 | 5.40 | 11.51 | 7.4 |
| 12 | R2 | 27 | 3.0 | 1.499 | 245.5 | LOS F | 162.5 | 4380.5 | 1.00 | 5.40 | 11.51 | 7.4 |
| Appr |  | 1283 | 9.8 | 1.499 | 245.8 | LOS F | 162.5 | 4380.5 | 1.00 | 5.40 | 11.51 | 7.4 |
| All V | icles | 2701 | 9.0 | 1.499 | 124.4 | LOS F | 162.5 | 4380.5 | 0.68 | 2.75 | 5.80 | 12.3 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Roundabout LOS Method: Same as Sign Control.
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.
LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 6).
Roundabout Capacity Model: US HCM 2010.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies. Gap-Acceptance Capacity: Traditional M1.
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 2.1 |  |  |  |  |  |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations |  | -1 | F |  | Mr |  |
| Traffic Vol, veh/h | 10 | 245 | 120 | 170 | 30 | 85 |
| Future Vol, veh/h | 10 | 245 | 120 | 170 | 30 | 85 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | - | 0 | 0 | - | 0 | - |
| Grade, \% | - | 0 | 0 | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 7 | 7 | 2 |
| Mvmt Flow | 11 | 266 | 130 | 185 | 33 | 92 |


| Major/Minor M | Major1 |  | Major2 |  | Minor2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 315 | 0 | 0 | 0 | 511 | 223 |
| Stage 1 | - | - | - | - | 223 | - |
| Stage 2 | - | - | - | - | 288 | - |
| Critical Hdwy | 4.12 | - | - | - | 6.47 | 6.22 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.47 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.47 | - |
| Follow-up Hdwy | 2.218 | - | - | - | 3.563 | 3.318 |
| Pot Cap-1 Maneuver | 1245 | - | - | - | 514 | 817 |
| Stage 1 | - |  | - | - | 802 | - |
| Stage 2 | - |  | - | - | 750 | - |
| Platoon blocked, \% |  |  | - | - |  |  |
| Mov Cap-1 Maneuver | 1245 | - | - | - | 509 | 817 |
| Mov Cap-2 Maneuver | - |  | - | - | 509 | - |
| Stage 1 | - |  | - - | - | 794 | - |
| Stage 2 | - |  | - - | - | 750 | - |
|  |  |  |  |  |  |  |
| Approach | EB |  | WB |  | SB |  |
| HCM Control Delay, s | 0.3 |  | 0 |  | 11.2 |  |
| HCM LOS |  |  |  |  | B |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | EBL | EBT | WBT WBR SBLn1 |  |  |
| Capacity (veh/h) |  | 1245 | - | - | - | 706 |
| HCM Lane V/C Ratio |  | 0.009 | 9 | - | - | 0.177 |
| HCM Control Delay (s) |  | 7.9 | 0 | - | - | 11.2 |
| HCM Lane LOS |  | A | A A | - | - | B |
| HCM 95th \%tile Q(veh) |  | 0 | 0 | - | - | 0.6 |



| Major/Minor | Major1 | Major2 |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | :--- | :--- | :--- | :--- | :--- |
| Conflicting Flow All | 440 | 0 | - | - | - | 0 | 770 | 859 | - |
| $\quad$ Stage 1 | - | - | - | - | - | - | 419 | 419 | - |
| $\quad$ Stage 2 | - | - | - | - | - | - | 351 | 440 | - |
| Criticat Hdwy | 4.17 | - | - | - | - | - | 6.47 | 6.52 | - |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | 5.47 | 5.52 | - |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 5.47 | 5.52 | - |
| Follow-up Hdwy | 2.263 | - | - | - | - | -3.563 | 4.018 | - |  |
| Pot Cap-1 Maneuver | 1094 | - | 0 | 0 | - | - | 362 | 294 | 0 |
| $\quad$ Stage 1 | - | - | 0 | 0 | - | - | 653 | 590 | 0 |
| $\quad$ Stage 2 | - | - | 0 | 0 | - | - | 702 | 578 | 0 |
| Platoon blocked, \% |  | - |  |  | - | - |  |  |  |
| Mov Cap-1 Maneuver | 1094 | - | - | - | - | - | 334 | 0 | - |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | 334 | 0 | - |
| $\quad$ Stage 1 | - | - | - | - | - | - | 603 | 0 | - |
| Stage 2 | - | - | - | - | - | - | 702 | 0 | - |
|  |  |  |  |  |  |  |  |  |  |


| Approach | EB | WB | NB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s | 1.7 | 0 | 16 |
| HCM LOS |  | C |  |


|  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | :--- |
| Minor Lane/Major Mvmt | NBLn1 NBLn2 | EBL | EBT | WBT | WBR |
| Capacity (veh/h) | 334 | -1094 | - | - | - |
| HCM Lane V/C Ratio | 0.016 | -0.065 | - | - | - |
| HCM Control Delay (s) | 16 | 0 | 8.5 | 0 | - |
| HCM Lane LOS | C | A | A | A | - |
| HCM 95th \%tile Q(veh) | 0.1 | - | 0.2 | - | - |






| Intersection |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |



| Approach | EB | NB | SB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s | 21.2 | 0.4 | 0 |
| HCM LOS | C |  |  |


| Minor Lane/Major Mvmt | NBL | NBT EBLn1 | SBT | SBR |  |
| :--- | ---: | ---: | ---: | ---: | :--- |
| Capacity (veh/h) | 1090 | -351 | - | - |  |
| HCM Lane V/C Ratio | 0.02 | -0.372 | - | - |  |
| HCM Control Delay (s) | 8.4 | 0 | 21.2 | - | - |
| HCM Lane LOS | A | A | C | - | - |
| HCM 95th \%tile Q(veh) | 0.1 | - | 1.7 | - | - |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 3.9 |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | F |  |  | -1 | Mr |  |
| Traffic Vol, veh/h | 90 | 20 | 15 | 10 | 45 | 30 |
| Future Vol, veh/h | 90 | 20 | 15 | 10 | 45 | 30 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 98 | 22 | 16 | 11 | 49 | 33 |


| Major/Minor | Major1 | Major2 |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Minor1 |  |  |  |  |  |  |
| Conflicting Flow All | 0 | 0 | 120 | 0 | 152 | 109 |
| $\quad$ Stage 1 | - | - | - | - | 109 | - |
| Stage 2 | - | - | - | - | 43 | - |
| Critical Hdwy | - | - | 4.12 | - | 6.42 | 6.22 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.42 | - |
| Critical Hdwy Stg 2 | - | - | - | -5.42 | - |  |
| Follow-up Hdwy | - | -2.218 | -3.518 | 3.318 |  |  |
| Pot Cap-1 Maneuver | - | -1468 | -840 | 945 |  |  |
| $\quad$ Stage 1 | - | - | - | - | 916 | - |
| Stage 2 | - | - | - | - | 979 | - |
| Platoon blocked, \% | - | - | - |  |  |  |
| Mov Cap-1 Maneuver | - | - | 1468 | - | 831 | 945 |
| Mov Cap-2 Maneuver | - | - | - | - | 831 | - |
| Stage 1 | - | - | - | - | 906 | - |
| Stage 2 | - | - | - | - | 979 | - |


|  | EB | WB | NB |
| :--- | ---: | ---: | ---: |
| Approach |  |  |  |
| HCM Control Delay, s | 0 | 4.5 | 9.5 |
| HCM LOS |  |  | A |



## MOVEMENT SUMMARY

## Site: 7 [SR 12 / SR 113]

Cumulative Saturday
Site Category: (None)
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ |  | Deman Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed mph |
| South: Birds Landing Rd |  |  |  |  |  |  |  |  |  |  |  |  |
| 3 | L2 | 5 | 3.0 | 0.047 | 8.4 | LOS A | 0.1 | 3.7 | 0.59 | 0.59 | 0.59 | 32.8 |
| 8 | T1 | 5 | 3.0 | 0.047 | 8.4 | LOS A | 0.1 | 3.7 | 0.59 | 0.59 | 0.59 | 32.7 |
| 18 | R2 | 11 | 3.0 | 0.047 | 8.4 | LOS A | 0.1 | 3.7 | 0.59 | 0.59 | 0.59 | 31.8 |
| Appr |  | 22 | 3.0 | 0.047 | 8.4 | LOS A | 0.1 | 3.7 | 0.59 | 0.59 | 0.59 | 32.3 |
| East: SR 12 |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 5 | 3.0 | 0.543 | 7.3 | LOS A | 3.3 | 88.2 | 0.10 | 0.03 | 0.10 | 34.0 |
| 6 | T1 | 723 | 10.0 | 0.543 | 7.5 | LOS A | 3.3 | 88.2 | 0.10 | 0.03 | 0.10 | 33.8 |
| 16 | R2 | 163 | 7.0 | 0.543 | 7.4 | LOS A | 3.3 | 88.2 | 0.10 | 0.03 | 0.10 | 32.8 |
| Appr |  | 891 | 9.4 | 0.543 | 7.5 | LOS A | 3.3 | 88.2 | 0.10 | 0.03 | 0.10 | 33.6 |
| North: SR 113 |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 168 | 7.0 | 0.414 | 15.0 | LOS B | 1.8 | 46.9 | 0.68 | 0.76 | 0.96 | 28.7 |
| 4 | T1 | 11 | 3.0 | 0.414 | 14.7 | LOS B | 1.8 | 46.9 | 0.68 | 0.76 | 0.96 | 28.8 |
| 14 | R2 | 16 | 7.0 | 0.414 | 15.0 | LOS B | 1.8 | 46.9 | 0.68 | 0.76 | 0.96 | 28.0 |
| Appr |  | 196 | 6.8 | 0.414 | 15.0 | LOS B | 1.8 | 46.9 | 0.68 | 0.76 | 0.96 | 28.6 |
| West: SR 12 |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 | L2 | 5 | 7.0 | 0.641 | 13.0 | LOS B | 5.7 | 154.4 | 0.53 | 0.48 | 0.68 | 31.2 |
| 2 | T1 | 620 | 10.0 | 0.641 | 13.1 | LOS B | 5.7 | 154.4 | 0.53 | 0.48 | 0.68 | 31.2 |
| 12 | R2 | 5 | 3.0 | 0.641 | 12.9 | LOS B | 5.7 | 154.4 | 0.53 | 0.48 | 0.68 | 30.5 |
| Approach |  | 630 | 9.9 | 0.641 | 13.1 | LOS B | 5.7 | 154.4 | 0.53 | 0.48 | 0.68 | 31.2 |
| All V | icles | 1739 | 9.2 | 0.641 | 10.4 | LOS B | 5.7 | 154.4 | 0.33 | 0.28 | 0.42 | 32.0 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Roundabout LOS Method: Same as Sign Control.
Vehicle movement LOS values are based on average delay and $\mathrm{v} / \mathrm{c}$ ratio (degree of saturation) per movement.
LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 6).
Roundabout Capacity Model: US HCM 2010.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies. Gap-Acceptance Capacity: Traditional M1.
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.



| Minor Lane/Major Mvmt | NBL | NBT | NBR EBLn1WBLn1 | SBL | SBT | SBR |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 1373 | - | - | 524 | 673 | 1429 | - |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| $l$ |  |  |  |  |  |  |



HCM LOS B

| Minor Lane/Major Mvmt | NBL | NBT EBLn1 | SBT | SBR |  |
| :--- | ---: | ---: | ---: | ---: | :--- |
| Capacity (veh/h) | 1416 | -661 | - | - |  |
| HCM Lane V/C Ratio | 0.012 | -0.041 | - | - |  |
| HCM Control Delay (s) | 7.6 | 0 | 10.7 | - | - |
| HCM Lane LOS | A | A | B | - | - |
| HCM 95th \%tile Q(veh) | 0 | - | 0.1 | - | - |




## MOVEMENT SUMMARY

Site: 7 [SR 12/SR 113]
Cumulative plus Project AM
Site Category: (None)
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | Turn | Deman Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance ft | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed mph |
| South: Birds Landing Rd |  |  |  |  |  |  |  |  |  |  |  |  |
| 3 | L2 | 5 | 3.0 | 0.032 | 7.6 | LOS A | 0.1 | 2.6 | 0.56 | 0.52 | 0.56 | 33.0 |
| 8 | T1 | 5 | 3.0 | 0.032 | 7.6 | LOS A | 0.1 | 2.6 | 0.56 | 0.52 | 0.56 | 32.9 |
| 18 | R2 | 5 | 3.0 | 0.032 | 7.6 | LOS A | 0.1 | 2.6 | 0.56 | 0.52 | 0.56 | 32.0 |
| Appr |  | 16 | 3.0 | 0.032 | 7.6 | LOS A | 0.1 | 2.6 | 0.56 | 0.52 | 0.56 | 32.7 |
| East: SR 12 |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 16 | 3.0 | 0.859 | 17.2 | LOS C | 11.9 | 319.5 | 0.23 | 0.06 | 0.23 | 29.6 |
| 6 | T1 | 1201 | 10.0 | 0.859 | 17.4 | LOS C | 11.9 | 319.5 | 0.23 | 0.06 | 0.23 | 29.4 |
| 16 | R2 | 252 | 7.0 | 0.859 | 17.3 | LOS C | 11.9 | 319.5 | 0.23 | 0.06 | 0.23 | 28.7 |
| Appr |  | 1470 | 9.4 | 0.859 | 17.4 | LOS C | 11.9 | 319.5 | 0.23 | 0.06 | 0.23 | 29.3 |
| North: SR 113 |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 220 | 7.0 | 0.855 | 62.8 | LOS F | 5.9 | 154.8 | 0.93 | 1.37 | 2.63 | 18.0 |
| 4 | T1 | 5 | 3.0 | 0.855 | 62.3 | LOS F | 5.9 | 154.8 | 0.93 | 1.37 | 2.63 | 18.0 |
| 14 | R2 | 11 | 7.0 | 0.855 | 62.8 | LOS F | 5.9 | 154.8 | 0.93 | 1.37 | 2.63 | 17.7 |
| Appr |  | 236 | 6.9 | 0.855 | 62.8 | LOS F | 5.9 | 154.8 | 0.93 | 1.37 | 2.63 | 18.0 |
| West: SR 12 |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 | L2 | 5 | 7.0 | 0.576 | 12.4 | LOS B | 4.4 | 119.9 | 0.55 | 0.56 | 0.75 | 31.5 |
| 2 | T1 | 489 | 10.0 | 0.576 | 12.5 | LOS B | 4.4 | 119.9 | 0.55 | 0.56 | 0.75 | 31.5 |
| 12 | R2 | 5 | 3.0 | 0.576 | 12.2 | LOS B | 4.4 | 119.9 | 0.55 | 0.56 | 0.75 | 30.7 |
| Approach |  | 500 | 9.9 | 0.576 | 12.5 | LOS B | 4.4 | 119.9 | 0.55 | 0.56 | 0.75 | 31.4 |
| All V | icles | 2222 | 9.2 | 0.859 | 21.0 | LOS C | 11.9 | 319.5 | 0.38 | 0.31 | 0.61 | 27.9 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Roundabout LOS Method: Same as Sign Control.
Vehicle movement LOS values are based on average delay and $\mathrm{v} / \mathrm{c}$ ratio (degree of saturation) per movement.
LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 6).
Roundabout Capacity Model: US HCM 2010.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies. Gap-Acceptance Capacity: Traditional M1.
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 3.7 |  |  |  |  |  |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations |  | -1 | F |  | Mr |  |
| Traffic Vol, veh/h | 10 | 160 | 65 | 292 | 125 | 65 |
| Future Vol, veh/h | 10 | 160 | 65 | 292 | 125 | 65 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | - | 0 | 0 | - | 0 | - |
| Grade, \% | - | 0 | 0 | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 7 | 7 | 2 |
| Mvmt Flow | 11 | 174 | 71 | 317 | 136 | 71 |







| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 14.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |  |
| Lane Configurations |  | ${ }_{*}$ |  |  | ¢ |  | \% | F |  | \% | ¢ |  |  |
| Trafic Vol, veh/h | 185 | 20 | 36 | 35 | 45 | 50 | 37 | 182 | 30 | 35 | 147 | 150 |  |
| Future Vol, veh/h | 185 | 20 | 36 | 35 | 45 | 50 | 37 | 182 | 30 | 35 | 147 | 150 |  |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |  |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |  |
| Storage Length | - | - | - | - | - | - | 120 | - | - | 120 | - | - |  |
| Veh in Median Storage, | \# | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |  |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |  |
| Heavy Vehicles, \% | 2 | 2 | 7 | 2 | 2 | 2 | 7 | 7 | 2 | 2 | 7 | 2 |  |
| Mumt Flow | 201 | 22 | 39 | 38 | 49 | 54 | 40 | 198 | 33 | 38 | 160 | 163 |  |



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| $l$ |  |  |  |  |  |  |



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 4.2 |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | $\uparrow$ |  |  | $\uparrow$ | Mr |  |
| Traffic Vol, veh/h | 30 | 55 | 51 | 50 | 39 | 30 |
| Future Vol, veh/h | 30 | 55 | 51 | 50 | 39 | 30 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 33 | 60 | 55 | 54 | 42 | 33 |


| Major/Minor | Major1 | Major2 | Minor1 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 0 | 93 | 0 | 227 | 63 |
| Stage 1 | - | - - | - | 63 |  |
| Stage 2 | - | - - | - | 164 |  |
| Critical Hdwy |  | 4.12 | - | 6.42 | 6.22 |
| Critical Hdwy Stg 1 | - | - - | - | 5.42 |  |
| Critical Hdwy Stg 2 |  | - - | - | 5.42 |  |
| Follow-up Hdwy |  | - 2.218 |  | 3.518 | 3.318 |
| Pot Cap-1 Maneuver |  | 1501 | - | 761 | 1002 |
| Stage 1 |  | - - | - | 960 |  |
| Stage 2 |  | - - | - | 865 |  |
| Platoon blocked, \% | - | - | - |  |  |
| Mov Cap-1 Maneuver |  | - 1501 | - | 732 | 1002 |
| Mov Cap-2 Maneuver | - | - - | - | 732 |  |
| Stage 1 |  | - - | - | 924 |  |
| Stage 2 | - | - - | - | 865 |  |


|  | EB | WB | NB |
| :--- | ---: | ---: | ---: |
| Approach | HCM Control Delay, s | 0 | 3.8 |
| HCM LOS |  | 9.8 |  |
| A |  |  |  |



## MOVEMENT SUMMARY

Site: 7 [SR 12/SR 113]
Cumulative plus Project PM
Site Category: (None)
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \mathrm{Mov} \\ \mathrm{ID} \end{gathered}$ | Turn | Deman <br> Total veh/h | $\begin{array}{r} \text { Flows } \\ \text { HV } \\ \% \end{array}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back <br> Vehicles <br> veh | of Queue Distance ft | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed mph |
| South: Birds Landing Rd |  |  |  |  |  |  |  |  |  |  |  |  |
| 3 | L2 | 5 | 3.0 | 0.088 | 13.2 | LOS B | 0.3 | 6.7 | 0.73 | 0.73 | 0.73 | 30.8 |
| 8 | T1 | 11 | 3.0 | 0.088 | 13.2 | LOS B | 0.3 | 6.7 | 0.73 | 0.73 | 0.73 | 30.8 |
| 18 | R2 | 11 | 3.0 | 0.088 | 13.2 | LOS B | 0.3 | 6.7 | 0.73 | 0.73 | 0.73 | 30.0 |
| Appr |  | 27 | 3.0 | 0.088 | 13.2 | LOS B | 0.3 | 6.7 | 0.73 | 0.73 | 0.73 | 30.4 |
| East: SR 12 |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 5 | 3.0 | 0.684 | 10.7 | LOS B | 5.4 | 145.7 | 0.24 | 0.09 | 0.24 | 32.3 |
| 6 | T1 | 647 | 10.0 | 0.684 | 10.9 | LOS B | 5.4 | 145.7 | 0.24 | 0.09 | 0.24 | 32.1 |
| 16 | R2 | 375 | 7.0 | 0.684 | 10.8 | LOS B | 5.4 | 145.7 | 0.24 | 0.09 | 0.24 | 31.3 |
| Appr |  | 1027 | 8.9 | 0.684 | 10.8 | LOS B | 5.4 | 145.7 | 0.24 | 0.09 | 0.24 | 31.8 |
| North: SR 113 |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 323 | 7.0 | 0.717 | 26.4 | LOS D | 5.7 | 150.9 | 0.80 | 1.10 | 1.76 | 25.1 |
| 4 | T1 | 22 | 3.0 | 0.717 | 26.1 | LOS D | 5.7 | 150.9 | 0.80 | 1.10 | 1.76 | 25.2 |
| 14 | R2 | 24 | 7.0 | 0.717 | 26.4 | LOS D | 5.7 | 150.9 | 0.80 | 1.10 | 1.76 | 24.6 |
| Approach |  | 368 | 6.8 | 0.717 | 26.4 | LOS D | 5.7 | 150.9 | 0.80 | 1.10 | 1.76 | 25.1 |
| West: SR 12 |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 | L2 | 33 | 7.0 | 1.504 | 247.7 | LOS F | 163.1 | 4397.0 | 1.00 | 5.43 | 11.59 | 7.4 |
| 2 | T1 | 1223 | 10.0 | 1.504 | 247.8 | LOS F | 163.1 | 4397.0 | 1.00 | 5.43 | 11.59 | 7.4 |
| 12 | R2 | 27 | 3.0 | 1.504 | 247.5 | LOS F | 163.1 | 4397.0 | 1.00 | 5.43 | 11.59 | 7.3 |
| Approach |  | 1283 | 9.8 | 1.504 | 247.8 | LOS F | 163.1 | 4397.0 | 1.00 | 5.43 | 11.59 | 7.4 |
| All Vehicles |  | 2705 | 9.0 | 1.504 | 125.3 | LOS F | 163.1 | 4397.0 | 0.68 | 2.76 | 5.83 | 12.2 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Roundabout LOS Method: Same as Sign Control.
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.
LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 6).
Roundabout Capacity Model: US HCM 2010.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies. Gap-Acceptance Capacity: Traditional M1.
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 4.3 |  |  |  |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | T | $\mathbf{7}$ | $\mathbf{F}$ |  |  | $\mathbf{-}$ |
| Traffic Vol, veh/h | 145 | 0 | 5 | 192 | 5 | 5 |
| Future Vol, veh/h | 145 | 0 | 5 | 192 | 5 | 5 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | 25 | - | - | - | - |
| Veh in Median Storage, \# | 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 7 | 2 | 2 | 7 | 2 | 2 |
| Mvmt Flow | 158 | 0 | 5 | 209 | 5 | 5 |


| Major/Minor | Minor1 |  | Major1 |  | Major2 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 125 | 110 | 0 | 0 | 214 | 0 |  |
| Stage 1 | 110 | - | - | - | - | - |  |
| Stage 2 | 15 | - | - | - | - | - |  |
| Critical Hdwy | 6.47 | 6.22 | - | - | 4.12 | - |  |
| Critical Hdwy Stg 1 | 5.47 |  | - | - | - | - |  |
| Critical Hdwy Stg 2 | 5.47 | - | - | - | - | - |  |
| Follow-up Hdwy | 3.563 | 3.318 | - | - | 2.218 | - |  |
| Pot Cap-1 Maneuver | 858 | 943 | - | - | 1356 | - |  |
| Stage 1 | 902 | - | - | - | - | - |  |
| Stage 2 | 995 | - | - | - | - | - |  |
| Platoon blocked, \% |  |  | - | - |  | - |  |
| Mov Cap-1 Maneuver | 855 | 943 | - | - | 1356 | - |  |
| Mov Cap-2 Maneuver | 855 | - | - | - | - | - |  |
| Stage 1 | 898 | - | - | - | - | - |  |
| Stage 2 | 995 | - | - | - | - | - |  |
|  |  |  |  |  |  |  |  |
| Approach | WB |  | NB |  | SB |  |  |
| HCM Control Delay, s | 10.2 |  | 0 |  | 3.8 |  |  |
| HCM LOS | B |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | NBT NBRWBLn1WBLn2 |  |  |  | NBRWBLn1WBLn2 SBL SBT |  |
| Capacity (veh/h) |  | - | - | 855 | - | 1356 | - |
| HCM Lane V/C Ratio |  | - | - | 0.184 | - | 0.004 | - |
| HCM Control Delay (s) |  | - | - | 10.2 | 0 | 7.7 | 0 |
| HCM Lane LOS |  | - | - | B | A | A | A |
| HCM 95th \%tile Q(veh) |  | - | - | 0.7 | - | 0 | - |



| Major/Minor M | Major1 |  | Major2 |  | Minor2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 328 | 0 |  | 0 | 517 | 229 |
| Stage 1 | - | - | - - | - | 229 | - |
| Stage 2 | - | - | - - | - | 288 | - |
| Critical Hdwy | 4.12 | - | - | - | 6.47 | 6.22 |
| Critical Hdwy Stg 1 | - | - | - - | - | 5.47 | - |
| Critical Hdwy Stg 2 | - | - | - - | - | 5.47 | - |
| Follow-up Hdwy | 2.218 | - | - - | - | 3.563 | 3.318 |
| Pot Cap-1 Maneuver | 1232 | - | - - | - | 510 | 810 |
| Stage 1 | - | - | - - | - | 797 | - |
| Stage 2 | - | - | - - | - | 750 | - |
| Platoon blocked, \% |  | - | - - | - |  |  |
| Mov Cap-1 Maneuver | 1232 | - | - - | - | 505 | 810 |
| Mov Cap-2 Maneuver | - | - | - - | - | 505 | - |
| Stage 1 | - | - | - - | - | 789 | - |
| Stage 2 | - | - | - - | - | 750 | - |
|  |  |  |  |  |  |  |
| Approach | EB |  | WB |  | SB |  |
| HCM Control Delay, s | S 0.3 |  | 0 |  | 11.3 |  |
| HCM LOS |  |  |  |  | B |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | EBL | EBT | WBT | WBR SBLn1 |  |
| Capacity (veh/h) |  | 1232 | - | - | - | 700 |
| HCM Lane V/C Ratio |  | 0.009 | - | - | - | 0.179 |
| HCM Control Delay (s) |  | 7.9 | 0 | - | - | 11.3 |
| HCM Lane LOS |  | A | A | - | - | B |
| HCM 95th \%tile Q(veh) |  | 0 | A | - | - | 0.6 |


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 0.8 |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |  |
| Lane Configurations |  | $\uparrow$ |  |  | F |  |  | $\uparrow$ | F |  |  |  |  |
| Traffic Vol, veh/h | 65 | 255 | 0 | 0 | 252 | 165 | 5 | 0 | 325 | 0 | 0 | 0 |  |
| Future Vol, veh/h | 65 | 255 | 0 | 0 | 252 | 165 | 5 | 0 | 325 | 0 | 0 | 0 |  |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Sign Control F | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Free | Free | Free |  |
| RT Channelized | - | - | None | - | - | None | - | - | Free | - | - | None |  |
| Storage Length | - | - | - | - | - | - | 50 | - | 0 | - | - | - |  |
| Veh in Median Storage, \# | \# | 0 | - | - | 0 | - | - | 0 | - |  | 16965 | - |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |  |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |  |
| Heavy Vehicles, \% | 7 | 7 | 2 | 2 | 7 | 7 | 7 | 2 | 7 | 2 | 2 | 2 |  |
| Mvmt Flow | 71 | 277 | 0 | 0 | 274 | 179 | 5 | 0 | 353 | 0 | 0 | 0 |  |


| Major/Minor | Major1 | Major2 |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | :--- | :--- | :--- | :--- |
| Conflicting Flow All | 453 | 0 | - | - | - | 0 | 783 | 872 |
| $\quad$ Stage 1 | - | - | - | - | - | - | 419 | 419 |
| $\quad$ Stage 2 | - | - | - | - | - | - | 364 | 453 |


| Approach | EB | WB | NB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s | 1.7 | 0 | 16.2 |

HCM LOS ..... C

| Minor Lane/Major Mvmt | NBLn1 NBLn2 |  | EBL | EBT | WBT | WBR |
| :--- | ---: | ---: | ---: | ---: | :---: | ---: |
| Capacity (veh/h) | 327 | -1082 | - | - | - |  |
| HCM Lane V/C Ratio | 0.017 | -0.065 | - | - | - |  |
| HCM Control Delay (s) | 16.2 | 0 | 8.6 | 0 | - | - |
| HCM Lane LOS | C | A | A | A | - | - |
| HCM 95th \%tile Q(veh) | 0.1 | - | 0.2 | - | - | - |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |





| Minor Lane/Major Mvmt | NBL | NBT | NBR EBLn1WBLn1 | SBL | SBT | SBR |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | :--- |
| Capacity (veh/h) | 1228 | - | - | 363 | 241 | 1265 | - |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 3.4 |  |  |  |  |  |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | Mr |  |  | -1 | $\uparrow$ |  |
| Traffic Vol, veh/h | 89 | 49 | 20 | 385 | 430 | 6 |
| Future Vol, veh/h | 89 | 49 | 20 | 385 | 430 | 6 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 7 | 2 | 2 | 7 | 7 | 7 |
| Mvmt Flow | 97 | 53 | 22 | 418 | 467 | 7 |



| Approach | EB | NB | SB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s | 23.1 | 0.4 | 0 |
| HCM LOS | C |  |  |


| Minor Lane/Major Mvmt | NBL | NBT EBLn1 | SBT | SBR |  |
| :--- | ---: | ---: | ---: | ---: | :--- |
| Capacity (veh/h) | 1088 | -346 | - | - |  |
| HCM Lane V/C Ratio | 0.02 | -0.434 | - | - |  |
| HCM Control Delay (s) | 8.4 | 0 | 23.1 | - | - |
| HCM Lane LOS | A | A | C | - | - |
| HCM 95th \%tile Q(veh) | 0.1 | - | 2.1 | - | - |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 4.6 |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | F |  |  | -1 | Mr |  |
| Traffic Vol, veh/h | 90 | 20 | 16 | 10 | 53 | 48 |
| Future Vol, veh/h | 90 | 20 | 16 | 10 | 53 | 48 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 98 | 22 | 17 | 11 | 58 | 52 |


| Major/Minor | Major1 | Major2 |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Minor1 |  |  |  |  |  |  |
| Conflicting Flow All | 0 | 0 | 120 | 0 | 154 | 109 |
| $\quad$ Stage 1 | - | - | - | - | 109 | - |
| Stage 2 | - | - | - | - | 45 | - |
| Critical Hdwy | - | - | 4.12 | - | 6.42 | 6.22 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.42 | - |
| Critical Hdwy Stg 2 | - | - | - | -5.42 | - |  |
| Follow-up Hdwy | - | -2.218 | -3.518 | 3.318 |  |  |
| Pot Cap-1 Maneuver | - | -1468 | -838 | 945 |  |  |
| $\quad$ Stage 1 | - | - | - | - | 916 | - |
| Stage 2 | - | - | - | - | 977 | - |
| Platoon blocked, \% | - | - | - |  |  |  |
| Mov Cap-1 Maneuver | - | - | 1468 | - | 828 | 945 |
| Mov Cap-2 Maneuver | - | - | - | - | 828 | - |
| Stage 1 | - | - | - | - | 905 | - |
| Stage 2 | - | - | - | - | 977 | - |


|  | EB | WB | NB |
| :--- | ---: | ---: | ---: |
| Approach | CCM Control Delay, s | 0 | 4.6 |
| HCM LOS |  | 9.7 |  |
| A |  |  |  |



## MOVEMENT SUMMARY

## Site: 7 [SR 12 / SR 113]

Cumulative plus Project Saturday
Site Category: (None)
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ |  | Deman Total veh/h | $\begin{gathered} \text { =lows } \\ \text { HV } \\ \% \\ \hline \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed mph |
| South: Birds Landing Rd |  |  |  |  |  |  |  |  |  |  |  |  |
| 3 | L2 | 5 | 3.0 | 0.047 | 8.5 | LOS A | 0.1 | 3.7 | 0.59 | 0.59 | 0.59 | 32.8 |
| 8 | T1 | 5 | 3.0 | 0.047 | 8.5 | LOS A | 0.1 | 3.7 | 0.59 | 0.59 | 0.59 | 32.7 |
| 18 | R2 | 11 | 3.0 | 0.047 | 8.5 | LOS A | 0.1 | 3.7 | 0.59 | 0.59 | 0.59 | 31.8 |
| Appr |  | 22 | 3.0 | 0.047 | 8.5 | LOS A | 0.1 | 3.7 | 0.59 | 0.59 | 0.59 | 32.3 |
| East: SR 12 |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 5 | 3.0 | 0.548 | 7.5 | LOS A | 3.3 | 89.8 | 0.11 | 0.03 | 0.11 | 33.9 |
| 6 | T1 | 723 | 10.0 | 0.548 | 7.6 | LOS A | 3.3 | 89.8 | 0.11 | 0.03 | 0.11 | 33.7 |
| 16 | R2 | 165 | 7.0 | 0.548 | 7.5 | LOS A | 3.3 | 89.8 | 0.11 | 0.03 | 0.11 | 32.8 |
| Appr |  | 893 | 9.4 | 0.548 | 7.6 | LOS A | 3.3 | 89.8 | 0.11 | 0.03 | 0.11 | 33.6 |
| North: SR 113 |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 171 | 7.0 | 0.421 | 15.2 | LOS C | 1.8 | 48.2 | 0.68 | 0.77 | 0.98 | 28.6 |
| 4 | T1 | 11 | 3.0 | 0.421 | 14.9 | LOS B | 1.8 | 48.2 | 0.68 | 0.77 | 0.98 | 28.7 |
| 14 | R2 | 17 | 7.0 | 0.421 | 15.2 | LOS C | 1.8 | 48.2 | 0.68 | 0.77 | 0.98 | 27.9 |
| Appr |  | 199 | 6.8 | 0.421 | 15.2 | LOS C | 1.8 | 48.2 | 0.68 | 0.77 | 0.98 | 28.6 |
| West: SR 12 |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 | L2 | 7 | 7.0 | 0.644 | 13.2 | LOS B | 6.0 | 161.0 | 0.54 | 0.50 | 0.71 | 31.2 |
| 2 | T1 | 620 | 10.0 | 0.644 | 13.3 | LOS B | 6.0 | 161.0 | 0.54 | 0.50 | 0.71 | 31.1 |
| 12 | R2 | 5 | 3.0 | 0.644 | 13.1 | LOS B | 6.0 | 161.0 | 0.54 | 0.50 | 0.71 | 30.4 |
| Approach |  | 632 | 9.9 | 0.644 | 13.3 | LOS B | 6.0 | 161.0 | 0.54 | 0.50 | 0.71 | 31.1 |
| All V | icles | 1746 | 9.2 | 0.644 | 10.5 | LOS B | 6.0 | 161.0 | 0.33 | 0.29 | 0.43 | 32.0 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Roundabout LOS Method: Same as Sign Control.
Vehicle movement LOS values are based on average delay and $\mathrm{v} / \mathrm{c}$ ratio (degree of saturation) per movement.
LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 6).
Roundabout Capacity Model: US HCM 2010.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies. Gap-Acceptance Capacity: Traditional M1.
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.


HCMLOS B B

| Minor Lane/Major Mvmt | NBL | NBT | NBR EBLn1WBLn1 | SBL | SBT | SBR |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | :--- |
| Capacity (veh/h) | 1372 | - | -533 | 654 | 1428 | - | - |
| HCM Lane V/C Ratio | 0.019 | - | -0.186 | 0.133 | 0.015 | - | - |
| HCM Control Delay (s) | 7.7 | - | -13.3 | 11.3 | 7.6 | - | - |
| HCM Lane LOS | A | - | - | B | B | A | - |
| HCM 95th \%tile Q(veh) | 0.1 | - | - | 0.7 | 0.5 | 0 | - |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |


| Major/Minor | Minor2 | Major1 |  | Major2 |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Conflicting Flow All | 451 | 159 | 176 | 0 | - | 0 |
| $\quad$ Stage 1 | 159 | - | - | - | - | - |
| Stage 2 | 292 | - | - | - | - | - |
| Critical Hdwy | 6.47 | 6.22 | 4.12 | - | - | - |
| Critical Hdwy Stg 1 | 5.47 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.47 | - | - | - | - | - |
| Follow-up Hdwy | 3.563 | 3.318 | 2.218 | - | - | - |
| Pot Cap-1 Maneuver | 557 | 886 | 1400 | - | - | - |
| $\quad$ Stage 1 | 858 | - | - | - | - | - |
| $\quad$ Stage 2 | 747 | - | - | - | - | - |
| Platoon blocked, \% |  |  |  | - | - | - |
| Mov Cap-1 Maneuver | 548 | 886 | 1400 | - | - | - |
| Mov Cap-2 Maneuver | 548 | - | - | - | - | - |
| Stage 1 | 843 | - | - | - | - | - |
| Stage 2 | 747 | - | - | - | - | - |
|  |  |  |  |  |  |  |


| Approach | EB | NB | SB |
| :--- | :---: | :---: | :---: |
| HCM Control Delay, s | 11.1 | 0.6 | 0 |

HCM LOS B

| Minor Lane/Major Mvmt | NBL | NBT EBLn1 | SBT | SBR |  |
| :--- | ---: | ---: | ---: | ---: | :--- |
| Capacity (veh/h) | 1400 | -630 | - | - |  |
| HCM Lane V/C Ratio | 0.015 | -0.066 | - | - |  |
| HCM Control Delay (s) | 7.6 | 0 | 11.1 | - | - |
| HCM Lane LOS | A | A | B | - | - |
| HCM 95th \%tile Q(veh) | 0 | - | 0.2 | - | - |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 5.3 |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | F |  |  | -1 | Mr |  |
| Traffic Vol, veh/h | 10 | 57 | 46 | 5 | 41 | 28 |
| Future Vol, veh/h | 10 | 57 | 46 | 5 | 41 | 28 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 11 | 62 | 50 | 5 | 45 | 30 |



## MOVEMENT SUMMARY

Site: 7 [SR 12/SR 113]
MITIG8 Existing AM
Site Category: (None)
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \text { Mov } \\ \text { ID } \end{gathered}$ | Turn | Deman Total veh/h | $\begin{array}{r} \text { Flows } \\ \text { HV } \\ \% \end{array}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back <br> Vehicles <br> veh | of Queue Distance ft | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed mph |
| South: Birds Landing Rd |  |  |  |  |  |  |  |  |  |  |  |  |
| 3 | L2 | 1 | 3.0 | 0.010 | 5.0 | LOS A | 0.0 | 0.9 | 0.42 | 0.28 | 0.42 | 34.8 |
| 8 | T1 | 1 | 3.0 | 0.010 | 5.0 | LOS A | 0.0 | 0.9 | 0.42 | 0.28 | 0.42 | 34.7 |
| 18 | R2 | 5 | 3.0 | 0.010 | 5.0 | LOS A | 0.0 | 0.9 | 0.42 | 0.28 | 0.42 | 33.7 |
| Appr |  | 8 | 3.0 | 0.010 | 5.0 | LOS A | 0.0 | 0.9 | 0.42 | 0.28 | 0.42 | 34.0 |
| East: SR 12 |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 21 | 3.0 | 0.502 | 6.4 | LOS A | 2.9 | 76.9 | 0.04 | 0.00 | 0.04 | 34.4 |
| 6 | T1 | 650 | 10.0 | 0.502 | 6.5 | LOS A | 2.9 | 76.9 | 0.04 | 0.00 | 0.04 | 34.2 |
| 16 | R2 | 239 | 7.0 | 0.502 | 6.4 | LOS A | 2.9 | 76.9 | 0.04 | 0.00 | 0.04 | 33.3 |
| Appr |  | 910 | 9.1 | 0.502 | 6.5 | LOS A | 2.9 | 76.9 | 0.04 | 0.00 | 0.04 | 34.0 |
| North: SR 113 |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 134 | 7.0 | 0.275 | 11.2 | LOS B | 0.9 | 24.5 | 0.62 | 0.62 | 0.62 | 29.9 |
| 4 | T1 | 2 | 3.0 | 0.275 | 10.9 | LOS B | 0.9 | 24.5 | 0.62 | 0.62 | 0.62 | 30.0 |
| 14 | R2 | 3 | 7.0 | 0.275 | 11.2 | LOS B | 0.9 | 24.5 | 0.62 | 0.62 | 0.62 | 29.2 |
| Approach |  | 139 | 6.9 | 0.275 | 11.2 | LOS B | 0.9 | 24.5 | 0.62 | 0.62 | 0.62 | 29.9 |
| West: SR 12 |  |  |  |  |  |  |  |  |  |  |  |  |
| $\begin{aligned} & 5 \\ & 2 \\ & 12 \\ & \hline \end{aligned}$ | L2 | 1 | 7.0 | 0.266 | 6.6 | LOS A | 1.0 | 27.4 | 0.33 | 0.22 | 0.33 | 34.2 |
|  | T1 | 237 | 10.0 | 0.266 | 6.7 | LOS A | 1.0 | 27.4 | 0.33 | 0.22 | 0.33 | 34.2 |
|  | R2 | 3 | 3.0 | 0.266 | 6.5 | LOS A | 1.0 | 27.4 | 0.33 | 0.22 | 0.33 | 33.3 |
| Approach |  | 241 | 9.9 | 0.266 | 6.7 | LOS A | 1.0 | 27.4 | 0.33 | 0.22 | 0.33 | 34.2 |
| All Vehicles |  | 1298 | 8.9 | 0.502 | 7.0 | LOS A | 2.9 | 76.9 | 0.15 | 0.11 | 0.15 | 33.5 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Roundabout LOS Method: Same as Sign Control.
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.
LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 6).
Roundabout Capacity Model: US HCM 2010.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies. Gap-Acceptance Capacity: Traditional M1.
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

Site: 7 [SR 12 / SR 113]
mitig8 Existing PM
Site Category: (None)
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | Turn | Deman <br> Total veh/h | $\begin{gathered} =\text { lows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back <br> Vehicles veh | of Queue Distance ft | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed mph |
| South: Birds Landing Rd |  |  |  |  |  |  |  |  |  |  |  |  |
| 3 | L2 | 1 | 3.0 | 0.063 | 11.4 | LOS B | 0.2 | 4.8 | 0.70 | 0.70 | 0.70 | 31.9 |
| 8 | T1 | 4 | 3.0 | 0.063 | 11.4 | LOS B | 0.2 | 4.8 | 0.70 | 0.70 | 0.70 | 31.8 |
| 18 | R2 | 16 | 3.0 | 0.063 | 11.4 | LOS B | 0.2 | 4.8 | 0.70 | 0.70 | 0.70 | 31.0 |
| Appr |  | 22 | 3.0 | 0.063 | 11.4 | LOS B | 0.2 | 4.8 | 0.70 | 0.70 | 0.70 | 31.2 |
| East: SR 12 |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 4 | 3.0 | 0.339 | 4.9 | LOS A | 1.5 | 40.6 | 0.07 | 0.01 | 0.07 | 35.2 |
| 6 | T1 | 334 | 10.0 | 0.339 | 5.1 | LOS A | 1.5 | 40.6 | 0.07 | 0.01 | 0.07 | 35.0 |
| 16 | R2 | 213 | 7.0 | 0.339 | 5.0 | LOSA | 1.5 | 40.6 | 0.07 | 0.01 | 0.07 | 34.0 |
| Appr |  | 551 | 8.8 | 0.339 | 5.0 | LOS A | 1.5 | 40.6 | 0.07 | 0.01 | 0.07 | 34.6 |
| North: SR 113 |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 266 | 7.0 | 0.376 | 9.8 | LOS A | 1.5 | 40.2 | 0.53 | 0.50 | 0.53 | 30.4 |
| 4 | T1 | 2 | 3.0 | 0.376 | 9.6 | LOS A | 1.5 | 40.2 | 0.53 | 0.50 | 0.53 | 30.5 |
| 14 | R2 | 5 | 7.0 | 0.376 | 9.8 | LOS A | 1.5 | 40.2 | 0.53 | 0.50 | 0.53 | 29.7 |
| Appr |  | 274 | 7.0 | 0.376 | 9.8 | LOS A | 1.5 | 40.2 | 0.53 | 0.50 | 0.53 | 30.4 |
| West: SR 12 |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 | L2 | 7 | 7.0 | 0.895 | 31.7 | LOS D | 25.8 | 697.7 | 0.90 | 1.56 | 2.55 | 24.9 |
| 2 | T1 | 782 | 10.0 | 0.895 | 31.8 | LOS D | 25.8 | 697.7 | 0.90 | 1.56 | 2.55 | 24.8 |
| 12 | R2 | 2 | 3.0 | 0.895 | 31.6 | LOS D | 25.8 | 697.7 | 0.90 | 1.56 | 2.55 | 24.4 |
| Approach |  | 790 | 10.0 | 0.895 | 31.8 | LOS D | 25.8 | 697.7 | 0.90 | 1.56 | 2.55 | 24.8 |
| All V | icles | 1637 | 9.0 | 0.895 | 18.8 | LOS C | 25.8 | 697.7 | 0.56 | 0.85 | 1.35 | 28.5 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Roundabout LOS Method: Same as Sign Control.
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.
LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 6).
Roundabout Capacity Model: US HCM 2010.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies. Gap-Acceptance Capacity: Traditional M1.
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

Site: 7 [SR 12 / SR 113]
MITIG8 Existing plus Project AM
Site Category: (None)
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | Turn | Deman Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance ft | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed mph |
| South: Birds Landing Rd 0 des |  |  |  |  |  |  |  |  |  |  |  |  |
| 3 | L2 | 1 | 3.0 | 0.010 | 5.0 | LOS A | 0.0 | 0.9 | 0.42 | 0.29 | 0.42 | 34.8 |
| 8 | T1 | 1 | 3.0 | 0.010 | 5.0 | LOS A | 0.0 | 0.9 | 0.42 | 0.29 | 0.42 | 34.7 |
| 18 | R2 | 5 | 3.0 | 0.010 | 5.0 | LOS A | 0.0 | 0.9 | 0.42 | 0.29 | 0.42 | 33.7 |
| Appr |  | 8 | 3.0 | 0.010 | 5.0 | LOS A | 0.0 | 0.9 | 0.42 | 0.29 | 0.42 | 34.0 |
| East: SR 12 |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 21 | 3.0 | 0.503 | 6.4 | LOS A | 2.9 | 77.3 | 0.04 | 0.00 | 0.04 | 34.4 |
| 6 | T1 | 650 | 10.0 | 0.503 | 6.5 | LOS A | 2.9 | 77.3 | 0.04 | 0.00 | 0.04 | 34.2 |
| 16 | R2 | 241 | 7.0 | 0.503 | 6.5 | LOS A | 2.9 | 77.3 | 0.04 | 0.00 | 0.04 | 33.3 |
| Appr |  | 912 | 9.0 | 0.503 | 6.5 | LOS A | 2.9 | 77.3 | 0.04 | 0.00 | 0.04 | 34.0 |
| North: SR 113 |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 136 | 7.0 | 0.280 | 11.3 | LOS B | 1.0 | 25.1 | 0.62 | 0.62 | 0.63 | 29.9 |
| 4 | T1 | 2 | 3.0 | 0.280 | 11.0 | LOS B | 1.0 | 25.1 | 0.62 | 0.62 | 0.63 | 29.9 |
| 14 | R2 | 3 | 7.0 | 0.280 | 11.3 | LOS B | 1.0 | 25.1 | 0.62 | 0.62 | 0.63 | 29.1 |
| Approach |  | 141 | 6.9 | 0.280 | 11.3 | LOS B | 1.0 | 25.1 | 0.62 | 0.62 | 0.63 | 29.9 |
| West: SR 12 |  |  |  |  |  |  |  |  |  |  |  |  |
| $\begin{array}{\|l\|} \hline 5 \\ 2 \\ 12 \\ \hline \end{array}$ | L2 | 1 | 7.0 | 0.267 | 6.7 | LOS A | 1.0 | 27.5 | 0.33 | 0.22 | 0.33 | 34.2 |
|  | T1 | 237 | 10.0 | 0.267 | 6.8 | LOS A | 1.0 | 27.5 | 0.33 | 0.22 | 0.33 | 34.2 |
|  | R2 | 3 | 3.0 | 0.267 | 6.5 | LOS A | 1.0 | 27.5 | 0.33 | 0.22 | 0.33 | 33.3 |
| Approach |  | 241 | 9.9 | 0.267 | 6.8 | LOS A | 1.0 | 27.5 | 0.33 | 0.22 | 0.33 | 34.2 |
| All Vehicles |  | 1302 | 8.9 | 0.503 | 7.1 | LOS A | 2.9 | 77.3 | 0.16 | 0.11 | 0.16 | 33.5 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Roundabout LOS Method: Same as Sign Control.
Vehicle movement LOS values are based on average delay and $\mathrm{v} / \mathrm{c}$ ratio (degree of saturation) per movement.
LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 6).
Roundabout Capacity Model: US HCM 2010.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies. Gap-Acceptance Capacity: Traditional M1.
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

Site: 7 [SR 12/SR 113]
MITIG8 Existing plus Project PM
Site Category: (None)
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \text { Mov } \\ \text { ID } \end{gathered}$ | Turn | Deman Total veh/h | $\begin{array}{r} \text { Flows } \\ \text { HV } \\ \% \end{array}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back <br> Vehicles <br> veh | of Queue Distance ft | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed mph |
| South: Birds Landing Rd |  |  |  |  |  |  |  |  |  |  |  |  |
| 3 | L2 | 1 | 3.0 | 0.063 | 11.4 | LOS B | 0.2 | 4.8 | 0.70 | 0.70 | 0.70 | 31.9 |
| 8 | T1 | 4 | 3.0 | 0.063 | 11.4 | LOS B | 0.2 | 4.8 | 0.70 | 0.70 | 0.70 | 31.8 |
| 18 | R2 | 16 | 3.0 | 0.063 | 11.4 | LOS B | 0.2 | 4.8 | 0.70 | 0.70 | 0.70 | 30.9 |
| Appr |  | 22 | 3.0 | 0.063 | 11.4 | LOS B | 0.2 | 4.8 | 0.70 | 0.70 | 0.70 | 31.2 |
| East: SR 12 |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 4 | 3.0 | 0.339 | 4.9 | LOS A | 1.5 | 40.6 | 0.07 | 0.01 | 0.07 | 35.2 |
| 6 | T1 | 334 | 10.0 | 0.339 | 5.1 | LOS A | 1.5 | 40.6 | 0.07 | 0.01 | 0.07 | 35.0 |
| 16 | R2 | 213 | 7.0 | 0.339 | 5.0 | LOS A | 1.5 | 40.6 | 0.07 | 0.01 | 0.07 | 34.0 |
| Appr |  | 551 | 8.8 | 0.339 | 5.0 | LOS A | 1.5 | 40.6 | 0.07 | 0.01 | 0.07 | 34.6 |
| North: SR 113 |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 268 | 7.0 | 0.382 | 9.9 | LOS A | 1.6 | 41.0 | 0.53 | 0.50 | 0.53 | 30.4 |
| 4 | T1 | 2 | 3.0 | 0.382 | 9.7 | LOS A | 1.6 | 41.0 | 0.53 | 0.50 | 0.53 | 30.5 |
| 14 | R2 | 8 | 7.0 | 0.382 | 9.9 | LOS A | 1.6 | 41.0 | 0.53 | 0.50 | 0.53 | 29.6 |
| Approach |  | 278 | 7.0 | 0.382 | 9.9 | LOS A | 1.6 | 41.0 | 0.53 | 0.50 | 0.53 | 30.4 |
| West: SR 12 |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 | L2 | 7 | 7.0 | 0.898 | 32.2 | LOS D | 26.1 | 704.6 | 0.91 | 1.58 | 2.58 | 24.7 |
| 2 | T1 | 782 | 10.0 | 0.898 | 32.3 | LOS D | 26.1 | 704.6 | 0.91 | 1.58 | 2.58 | 24.7 |
| 12 | R2 | 2 | 3.0 | 0.898 | 32.0 | LOS D | 26.1 | 704.6 | 0.91 | 1.58 | 2.58 | 24.2 |
| Appr |  | 790 | 10.0 | 0.898 | 32.3 | LOS D | 26.1 | 704.6 | 0.91 | 1.58 | 2.58 | 24.7 |
| All V | icles | 1641 | 9.0 | 0.898 | 19.1 | LOS C | 26.1 | 704.6 | 0.56 | 0.86 | 1.36 | 28.4 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Roundabout LOS Method: Same as Sign Control.
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.
LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 6).
Roundabout Capacity Model: US HCM 2010.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies. Gap-Acceptance Capacity: Traditional M1.
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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| Intersection |  |
| :--- | ---: | :--- |
| Intersection Delay, s/veh | 13.3 |
| Intersection LOS | B |


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations |  | $\leqslant$ |  |  | \& |  | ${ }^{*}$ | $\hat{\beta}$ |  | * | $\uparrow$ |  |
| Traffic Vol, veh/h | 185 | 20 | 20 | 35 | 45 | 50 | 25 | 180 | 30 | 35 | 145 | 150 |
| Future Vol, veh/h | 185 | 20 | 20 | 35 | 45 | 50 | 25 | 180 | 30 | 35 | 145 | 150 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, \% | 2 | 2 | 7 | 2 | 2 | 2 | 7 | 7 | 2 | 2 | 7 | 2 |
| Mvmt Flow | 201 | 22 | 22 | 38 | 49 | 54 | 27 | 196 | 33 | 38 | 158 | 163 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 1 | 1 | 0 | 1 | 1 | 0 |
| Approach | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
| Opposing Approach | WB |  |  | EB |  |  | SB |  |  | NB |  |  |
| Opposing Lanes | 1 |  |  | 1 |  |  | 2 |  |  | 2 |  |  |
| Conflicting Approach Left | SB |  |  | NB |  |  | EB |  |  | WB |  |  |
| Conflicting Lanes Left | 2 |  |  | 2 |  |  | 1 |  |  | 1 |  |  |
| Conflicting Approach Right | NB |  |  | SB |  |  | WB |  |  | EB |  |  |
| Conflicting Lanes Right | 2 |  |  | 2 |  |  | 1 |  |  | 1 |  |  |
| HCM Control Delay | 13.4 |  |  | 11 |  |  | 12.8 |  |  | 14.5 |  |  |
| HCM LOS | B |  |  | B |  |  | B |  |  | B |  |  |


| Lane | NBLn1 | NBLn2 | EBLn1 | WBLn1 | SBLn1 | SBLn2 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Vol Left, \% | $100 \%$ | $0 \%$ | $82 \%$ | $27 \%$ | $100 \%$ | $0 \%$ |
| Vol Thru, \% | $0 \%$ | $86 \%$ | $9 \%$ | $35 \%$ | $0 \%$ | $49 \%$ |
| Vol Right, \% | $0 \%$ | $14 \%$ | $9 \%$ | $38 \%$ | $0 \%$ | $51 \%$ |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 25 | 210 | 225 | 130 | 35 | 295 |
| LT Vol | 25 | 0 | 185 | 35 | 35 | 0 |
| Through Vol | 0 | 180 | 20 | 45 | 0 | 145 |
| RT Vol | 0 | 30 | 20 | 50 | 0 | 150 |
| Lane Flow Rate | 27 | 228 | 245 | 141 | 38 | 321 |
| Geometry Grp | 7 | 7 | 2 | 2 | 7 | 7 |
| Degree of Util (X) | 0.052 | 0.397 | 0.412 | 0.237 | 0.07 | 0.523 |
| Departure Headway (Hd) | 6.874 | 6.263 | 6.067 | 6.028 | 6.652 | 5.867 |
| Convergence, Y/N | Yes | Yes | Yes | Yes | Yes | Yes |
| Cap | 519 | 571 | 589 | 591 | 536 | 612 |
| Service Time | 4.647 | 4.036 | 4.143 | 4.115 | 4.418 | 3.633 |
| HCM Lane V/C Ratio | 0.052 | 0.399 | 0.416 | 0.239 | 0.071 | 0.525 |
| HCM Control Delay | 10 | 13.1 | 13.4 | 11 | 9.9 | 15 |
| HCM Lane LOS | A | B | B | B | A | B |
| HCM 95th-tile Q | 0.2 | 1.9 | 2 | 0.9 | 0.2 | 3 |


| Intersection |  |  |
| :--- | ---: | :--- |
| Intersection Delay, s/veh | 13.7 |  |
| Intersection LOS | B |  |


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations |  | ${ }_{*}$ |  |  | ¢ |  | * | ¢ |  | * | ¢ |  |
| Traffic Vol, veh/h | 40 | 85 | 50 | 115 | 35 | 15 | 55 | 190 | 80 | 30 | 170 | 110 |
| Future Vol, veh/h | 40 | 85 | 50 | 115 | 35 | 15 | 55 | 190 | 80 | 30 | 170 | 110 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, \% | 2 | 2 | 7 | 2 | 2 | 2 | 7 | 7 | 2 | 2 | 7 | 2 |
| Mvmt Flow | 43 | 92 | 54 | 125 | 38 | 16 | 60 | 207 | 87 | 33 | 185 | 120 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 1 | 1 | 0 | 1 | 1 | 0 |
| Approach | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
| Opposing Approach | WB |  |  | EB |  |  | SB |  |  | NB |  |  |
| Opposing Lanes | 1 |  |  | 1 |  |  | 2 |  |  | 2 |  |  |
| Conflicting Approach Left | SB |  |  | NB |  |  | EB |  |  | WB |  |  |
| Conflicting Lanes Left | 2 |  |  | 2 |  |  | 1 |  |  | 1 |  |  |
| Conflicting Approach Right | NB |  |  | SB |  |  | WB |  |  | EB |  |  |
| Conflicting Lanes Right | 2 |  |  | 2 |  |  | 1 |  |  | 1 |  |  |
| HCM Control Delay | 12.2 |  |  | 12.4 |  |  | 14.2 |  |  | 14.6 |  |  |
| HCM LOS | B |  |  | B |  |  | B |  |  | B |  |  |


| Lane | NBLn1 | NBLn2 | EBLn1 | WBLn1 | SBLn1 | SBLn2 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Vol Left, \% | $100 \%$ | $0 \%$ | $23 \%$ | $70 \%$ | $100 \%$ | $0 \%$ |
| Vol Thru, \% | $0 \%$ | $70 \%$ | $49 \%$ | $21 \%$ | $0 \%$ | $61 \%$ |
| Vol Right, \% | $0 \%$ | $30 \%$ | $29 \%$ | $9 \%$ | $0 \%$ | $39 \%$ |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 55 | 270 | 175 | 165 | 30 | 280 |
| LT Vol | 55 | 0 | 40 | 115 | 30 | 0 |
| Through Vol | 0 | 190 | 85 | 35 | 0 | 170 |
| RT Vol | 0 | 80 | 50 | 15 | 0 | 110 |
| Lane Flow Rate | 60 | 293 | 190 | 179 | 33 | 304 |
| Geometry Grp | 7 | 7 | 2 | 2 | 7 | 7 |
| Degree of Util (X) | 0.113 | 0.498 | 0.325 | 0.317 | 0.061 | 0.513 |
| Departure Headway (Hd) | 6.829 | 6.109 | 6.142 | 6.368 | 6.772 | 6.069 |
| Convergence, Y/N | Yes | Yes | Yes | Yes | Yes | Yes |
| Cap | 522 | 587 | 580 | 560 | 526 | 590 |
| Service Time | 4.61 | 3.889 | 4.235 | 4.463 | 4.552 | 3.849 |
| HCM Lane V/C Ratio | 0.115 | 0.499 | 0.328 | 0.32 | 0.063 | 0.515 |
| HCM Control Delay | 10.5 | 14.9 | 12.2 | 12.4 | 10 | 15.1 |
| HCM Lane LOS | B | B | B | B | A | C |
| HCM 95th-tile Q | 0.4 | 2.8 | 1.4 | 1.4 | 0.2 | 2.9 |

## MOVEMENT SUMMARY

Site: 7 [SR 12/SR 113]
MITIG8 Cumulative PM
Add 2nd EB Lane
Site Category: (None)
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | Turn | Deman <br> Total veh/h |  | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance ft | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed mph |
| South: Birds Landing Rd |  |  |  |  |  |  |  |  |  |  |  |  |
| 3 | L2 | 5 | 3.0 | 0.083 | 12.4 | LOS B | 0.2 | 5.1 | 0.72 | 0.72 | 0.72 | 31.1 |
| 8 | T1 | 11 | 3.0 | 0.083 | 12.4 | LOS B | 0.2 | 5.1 | 0.72 | 0.72 | 0.72 | 31.1 |
| 18 | R2 | 11 | 3.0 | 0.083 | 12.4 | LOS B | 0.2 | 5.1 | 0.72 | 0.72 | 0.72 | 30.3 |
| Appr |  | 27 | 3.0 | 0.083 | 12.4 | LOS B | 0.2 | 5.1 | 0.72 | 0.72 | 0.72 | 30.8 |
| East: SR 12 |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 5 | 3.0 | 0.713 | 11.8 | LOS B | 6.0 | 159.9 | 0.30 | 0.12 | 0.30 | 31.8 |
| 6 | T1 | 647 | 10.0 | 0.713 | 12.0 | LOS B | 6.0 | 159.9 | 0.30 | 0.12 | 0.30 | 31.6 |
| 16 | R2 | 375 | 7.0 | 0.713 | 11.9 | LOS B | 6.0 | 159.9 | 0.30 | 0.12 | 0.30 | 30.8 |
| Appr |  | 1027 | 8.9 | 0.713 | 12.0 | LOS B | 6.0 | 159.9 | 0.30 | 0.12 | 0.30 | 31.3 |
| North: SR 113 |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 321 | 7.0 | 0.709 | 25.8 | LOS D | 5.5 | 146.2 | 0.79 | 1.08 | 1.72 | 25.3 |
| 4 | T1 | 22 | 3.0 | 0.709 | 25.6 | LOS D | 5.5 | 146.2 | 0.79 | 1.08 | 1.72 | 25.3 |
| 14 | R2 | 22 | 7.0 | 0.709 | 25.8 | LOS D | 5.5 | 146.2 | 0.79 | 1.08 | 1.72 | 24.7 |
| Appr |  | 364 | 6.8 | 0.709 | 25.8 | LOS D | 5.5 | 146.2 | 0.79 | 1.08 | 1.72 | 25.3 |
| West: SR 12 |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 | L2 | 33 | 7.0 | 0.855 | 29.7 | LOS D | 17.3 | 466.8 | 0.86 | 1.47 | 2.37 | 25.3 |
| 2 | T1 | 1223 | 10.0 | 0.855 | 28.0 | LOS D | 17.3 | 466.8 | 0.84 | 1.40 | 2.23 | 25.9 |
| 12 | R2 | 27 | 3.0 | 0.817 | 25.9 | LOS D | 14.3 | 385.7 | 0.82 | 1.33 | 2.08 | 25.9 |
| Approach |  | 1283 | 9.8 | 0.855 | 28.0 | LOS D | 17.3 | 466.8 | 0.84 | 1.40 | 2.23 | 25.9 |
| All Vehicles |  | 2701 | 9.0 | 0.855 | 21.5 | LOS C | 17.3 | 466.8 | 0.63 | 0.87 | 1.41 | 27.6 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Roundabout LOS Method: Same as Sign Control.
Vehicle movement LOS values are based on average delay and $\mathrm{v} / \mathrm{c}$ ratio (degree of saturation) per movement.
LOS $F$ will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 6).
Roundabout Capacity Model: US HCM 2010.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies. Gap-Acceptance Capacity: Traditional M1.
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## SITE LAYOUT

Site: 7 [SR 12 /SR 113]
MITIG8 Cumulative PM
Add 2nd EB Lane
Site Category: (None)
Roundabout


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| Intersection |  |  |
| :--- | ---: | :--- |
| Intersection Delay, s/veh | 13.7 | B |
| Intersection LOS | B |  |


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations |  | ¢ |  |  | ¢ |  | ${ }^{7}$ | F |  | ${ }^{7}$ | F |  |
| Traffic Vol, veh/h | 185 | 20 | 36 | 35 | 45 | 50 | 37 | 182 | 30 | 35 | 147 | 150 |
| Future Vol, veh/h | 185 | 20 | 36 | 35 | 45 | 50 | 37 | 182 | 30 | 35 | 147 | 150 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, \% | 2 | 2 | 7 | 2 | 2 | 2 | 7 | 7 | 2 | 2 | 7 | 2 |
| Mvmt Flow | 201 | 22 | 39 | 38 | 49 | 54 | 40 | 198 | 33 | 38 | 160 | 163 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 1 | 1 | 0 | 1 | 1 | 0 |
| Approach | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
| Opposing Approach | WB |  |  | EB |  |  | SB |  |  | NB |  |  |
| Opposing Lanes | 1 |  |  | 1 |  |  | 2 |  |  | 2 |  |  |
| Conflicting Approach Left | SB |  |  | NB |  |  | EB |  |  | WB |  |  |
| Conflicting Lanes Left | 2 |  |  | 2 |  |  | 1 |  |  | 1 |  |  |
| Conflicting Approach Right | NB |  |  | SB |  |  | WB |  |  | EB |  |  |
| Conflicting Lanes Right | 2 |  |  | 2 |  |  | 1 |  |  | 1 |  |  |
| HCM Control Delay | 14 |  |  | 11.2 |  |  | 13 |  |  | 14.9 |  |  |
| HCMLOS | B |  |  | B |  |  | B |  |  | B |  |  |


| Lane | NBLn1 | NBLn2 | EBLn1 | WBLn1 | SBLn1 | SBLn2 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Vol Left, \% | $100 \%$ | $0 \%$ | $77 \%$ | $27 \%$ | $100 \%$ | $0 \%$ |
| Vol Thru, \% | $0 \%$ | $86 \%$ | $8 \%$ | $35 \%$ | $0 \%$ | $49 \%$ |
| Vol Right, \% | $0 \%$ | $14 \%$ | $15 \%$ | $38 \%$ | $0 \%$ | $51 \%$ |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 37 | 212 | 241 | 130 | 35 | 297 |
| LT Vol | 37 | 0 | 185 | 35 | 35 | 0 |
| Through Vol | 0 | 182 | 20 | 45 | 0 | 147 |
| RT Vol | 0 | 30 | 36 | 50 | 0 | 150 |
| Lane Flow Rate | 40 | 230 | 262 | 141 | 38 | 323 |
| Geometry Grp | 7 | 7 | 2 | 2 | 7 | 7 |
| Degree of Util (X) | 0.078 | 0.406 | 0.443 | 0.241 | 0.071 | 0.535 |
| Departure Headway (Hd) | 6.957 | 6.347 | 6.084 | 6.138 | 6.75 | 5.968 |
| Convergence, Y/N | Yes | Yes | Yes | Yes | Yes | Yes |
| Cap | 512 | 565 | 587 | 579 | 528 | 600 |
| Service Time | 4.739 | 4.128 | 4.166 | 4.233 | 4.525 | 3.742 |
| HCM Lane V/C Ratio | 0.078 | 0.407 | 0.446 | 0.244 | 0.072 | 0.538 |
| HCM Control Delay | 10.3 | 13.5 | 14 | 11.2 | 10 | 15.5 |
| HCM Lane LOS | B | B | B | B | A | C |
| HCM 95th-tile Q | 0.3 | 2 | 2.3 | 0.9 | 0.2 | 3.2 |


| Intersection |  |  |
| :--- | ---: | :--- |
| Intersection Delay, s/veh | 13.8 |  |
| Intersection LOS | B |  |


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations |  | $\uparrow$ |  |  | ${ }_{\text {¢ }}$ |  | ${ }^{7}$ | $\hat{}$ |  | \% | $\hat{\dagger}$ |  |
| Traffic Vol, veh/h | 40 | 85 | 50 | 115 | 35 | 15 | 67 | 192 | 80 | 30 | 170 | 110 |
| Future Vol, veh/h | 40 | 85 | 50 | 115 | 35 | 15 | 67 | 192 | 80 | 30 | 170 | 110 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, \% | 2 | 2 | 7 | 2 | 2 | 2 | 7 | 7 | 2 | 2 | 7 | 2 |
| Mvmt Flow | 43 | 92 | 54 | 125 | 38 | 16 | 73 | 209 | 87 | 33 | 185 | 120 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 1 | 1 | 0 | 1 | 1 | 0 |
| Approach | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
| Opposing Approach | WB |  |  | EB |  |  | SB |  |  | NB |  |  |
| Opposing Lanes | 1 |  |  | 1 |  |  | 2 |  |  | 2 |  |  |
| Conflicting Approach Left | SB |  |  | NB |  |  | EB |  |  | WB |  |  |
| Conflicting Lanes Left | 2 |  |  | 2 |  |  | 1 |  |  | 1 |  |  |
| Conflicting Approach Right | NB |  |  | SB |  |  | WB |  |  | EB |  |  |
| Conflicting Lanes Right | 2 |  |  | 2 |  |  | 1 |  |  | 1 |  |  |
| HCM Control Delay | 12.3 |  |  | 12.5 |  |  | 14.2 |  |  | 14.8 |  |  |
| HCMLOS | B |  |  | B |  |  | B |  |  | B |  |  |


| Lane | NBLn1 | NBLn2 | EBLn1 | WBLn1 | SBLn1 | SBLn2 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Vol Left, \% | $100 \%$ | $0 \%$ | $23 \%$ | $70 \%$ | $100 \%$ | $0 \%$ |
| Vol Thu, $\%$ | $0 \%$ | $71 \%$ | $49 \%$ | $21 \%$ | $0 \%$ | $61 \%$ |
| Vol Right, \% | $0 \%$ | $29 \%$ | $29 \%$ | $9 \%$ | $0 \%$ | $39 \%$ |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 67 | 272 | 175 | 165 | 30 | 280 |
| LT Vol | 67 | 0 | 40 | 115 | 30 | 0 |
| Through Vol | 0 | 192 | 85 | 35 | 0 | 170 |
| RT Vol | 0 | 80 | 50 | 15 | 0 | 110 |
| Lane Flow Rate | 73 | 296 | 190 | 179 | 33 | 304 |
| Geometry Grp | 7 | 7 | 2 | 2 | 7 | 7 |
| Degree of Util (X) | 0.138 | 0.503 | 0.326 | 0.319 | 0.062 | 0.516 |
| Departure Headway (Hd) | 6.84 | 6.121 | 6.179 | 6.405 | 6.805 | 6.102 |
| Convergence, Y/N | Yes | Yes | Yes | Yes | Yes | Yes |
| Cap | 521 | 585 | 576 | 556 | 523 | 587 |
| Service Time | 4.62 | 3.901 | 4.276 | 4.503 | 4.584 | 3.881 |
| HCM Lane V/C Ratio | 0.14 | 0.506 | 0.33 | 0.322 | 0.063 | 0.518 |
| HCM Control Delay | 10.7 | 15 | 12.3 | 12.5 | 10 | 15.3 |
| HCM Lane LOS | B | B | B | B | A | C |
| HCM 95th-tile Q | 0.5 | 2.8 | 1.4 | 1.4 | 0.2 | 3 |

## MOVEMENT SUMMARY

## Site: 7 [SR 12 / SR 113]

MITIG8 Cumulative plus Project PM
Add 2nd EB Lane
Site Category: (None)
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | Turn | Deman <br> Total veh/h |  | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance ft | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed mph |
| South: Birds Landing Rd |  |  |  |  |  |  |  |  |  |  |  |  |
| 3 | L2 | 5 | 3.0 | 0.083 | 12.4 | LOS B | 0.2 | 5.1 | 0.72 | 0.72 | 0.72 | 31.1 |
| 8 | T1 | 11 | 3.0 | 0.083 | 12.4 | LOS B | 0.2 | 5.1 | 0.72 | 0.72 | 0.72 | 31.1 |
| 18 | R2 | 11 | 3.0 | 0.083 | 12.4 | LOS B | 0.2 | 5.1 | 0.72 | 0.72 | 0.72 | 30.3 |
| Appr |  | 27 | 3.0 | 0.083 | 12.4 | LOS B | 0.2 | 5.1 | 0.72 | 0.72 | 0.72 | 30.8 |
| East: SR 12 |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 5 | 3.0 | 0.713 | 11.8 | LOS B | 6.0 | 159.9 | 0.30 | 0.12 | 0.30 | 31.8 |
| 6 | T1 | 647 | 10.0 | 0.713 | 12.0 | LOS B | 6.0 | 159.9 | 0.30 | 0.12 | 0.30 | 31.6 |
| 16 | R2 | 375 | 7.0 | 0.713 | 11.9 | LOS B | 6.0 | 159.9 | 0.30 | 0.12 | 0.30 | 30.8 |
| Appr |  | 1027 | 8.9 | 0.713 | 12.0 | LOS B | 6.0 | 159.9 | 0.30 | 0.12 | 0.30 | 31.3 |
| North: SR 113 |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 323 | 7.0 | 0.717 | 26.4 | LOS D | 5.7 | 150.9 | 0.80 | 1.10 | 1.76 | 25.1 |
| 4 | T1 | 22 | 3.0 | 0.717 | 26.1 | LOS D | 5.7 | 150.9 | 0.80 | 1.10 | 1.76 | 25.2 |
| 14 | R2 | 24 | 7.0 | 0.717 | 26.4 | LOS D | 5.7 | 150.9 | 0.80 | 1.10 | 1.76 | 24.6 |
| Appr |  | 368 | 6.8 | 0.717 | 26.4 | LOS D | 5.7 | 150.9 | 0.80 | 1.10 | 1.76 | 25.1 |
| West: SR 12 |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 | L2 | 33 | 7.0 | 0.857 | 30.1 | LOS D | 17.5 | 471.0 | 0.87 | 1.49 | 2.39 | 25.2 |
| 2 | T1 | 1223 | 10.0 | 0.857 | 28.4 | LOS D | 17.5 | 471.0 | 0.85 | 1.42 | 2.25 | 25.8 |
| 12 | R2 | 27 | 3.0 | 0.820 | 26.2 | LOS D | 14.4 | 388.9 | 0.83 | 1.34 | 2.10 | 25.8 |
| Approach |  | 1283 | 9.8 | 0.857 | 28.4 | LOS D | 17.5 | 471.0 | 0.85 | 1.42 | 2.25 | 25.8 |
| All Vehicles |  | 2705 | 9.0 | 0.857 | 21.7 | LOS C | 17.5 | 471.0 | 0.63 | 0.87 | 1.43 | 27.5 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Roundabout LOS Method: Same as Sign Control.
Vehicle movement LOS values are based on average delay and $\mathrm{v} / \mathrm{c}$ ratio (degree of saturation) per movement.
LOS $F$ will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 6).
Roundabout Capacity Model: US HCM 2010.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies. Gap-Acceptance Capacity: Traditional M1.
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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Organisation: KD ANDERSON \& ASSOCIATES INC. | Processed: Monday, October 8, 2018 1:25:25 PM
Project: C:IUsers\JDFIKDAIReports\Solano County/Hay Road Landfilll00 UPDATED PROJECT 9-2018ISIDRAI13 MITIG8 11 SR 12_SR 113 CPP PM.sip8

| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |
| :---: | :---: |
| General Information | Site Information |
| Analyst JF <br> Agency or Company  <br> Date Performed $10 / 8 / 18$ <br> Analysis Time Period Exist AM | Highway / Direction of Travel Midway Rd <br> From/To west of Porter Rd EB <br> Jurisdiction Solano County <br> Analysis Year 2018 |
| Project Description: Recology Hay Rd Landfill |  |
| Input Data |  |
|  |  |
| Average Travel Speed |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.5 1.4 |
| Passenger-car equivalents for RVs , $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 0.966 0.973 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \text { ATS }}$ (Exhibit 15-9) | 1.00 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 234 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |
| Mean speed of sample ${ }^{3}, \mathrm{~S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(\mathrm{~V} / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ (Exhibit 15-15) <br> $1.3 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}, \mathrm{BFFS}$ $55.0 \mathrm{mi} / \mathrm{h}$ <br> Adj. for lane and shoulder width, ${ }^{4} \mathrm{f}_{\mathrm{LS}}($ (Exhibit 15-7) $2.6 \mathrm{mi} / \mathrm{h}$ <br> Adj. for access points ${ }^{4}, \mathrm{f}_{\mathrm{A}}$ (Exhibit $\left.15-8\right)$ $0.3 \mathrm{mi} / \mathrm{h}$ <br> Free-flow speed, FFS $\left(\mathrm{FSS}=\mathrm{BFFS}-\mathrm{f}_{\mathrm{LS}^{-}} \mathrm{f}_{\mathrm{A}}\right)$ $52.2 \mathrm{mi} / \mathrm{h}$ <br> Average travel speed, ATS $\mathrm{d}_{\mathrm{d}}=\mathrm{FFS}-0.00776\left(\mathrm{v}_{\mathrm{d}, \mathrm{ATS}}{ }^{+}\right.$ $46.6 \mathrm{mi} / \mathrm{h}$ <br> $\left.\mathrm{v}_{\mathrm{o}, \mathrm{ATS}}\right)-\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ $89.4 \%$ <br> Percent free flow speed, PFFS   |
| Percent Time-Spent-Following |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.1 |
| Passenger-car equivalents for $\mathrm{RVs}, \mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 0.993 0.993 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{\star} \mathrm{f}_{\mathrm{HV}, \mathrm{PTSF}^{*}} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 228 305 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{d}(\%)=100\left(1-e^{\text {av }}{ }_{d}{ }^{\text {b }}\right.$ ) | 26.5 |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \mathrm{PTSF}}$ (Exhibit 15-21) | 38.2 |
| Percent time-spent-following, $\operatorname{PTSF}_{d}(\%)=$ BPTSF $_{d}+{ }_{n p, \mathrm{PTSF}}{ }^{*}\left(v_{d, \mathrm{PTSF}} / \mathrm{v}_{d, \mathrm{PTSF}}{ }^{+}\right.$ <br> $\mathrm{V}_{\mathrm{o}, \mathrm{PTSF}}$ ) | 42.8 |
| Level of Service and Other Performance Measures |  |
| Level of service, LOS (Exhibit 15-3) | C |
| Volume to capacity ratio, v/c | 0.14 |



| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |
| :---: | :---: |
| General Information | Site Information |
| Analyst JF <br> Agency or Company  <br> Date Performed $10 / 8 / 18$ <br> Analysis Time Period Exist AM | Highway / Direction of Travel Midway Rd <br> From/To west of Porter Rd WB <br> Jurisdiction Solano County <br> Analysis Year 2018 |
| Project Description: Recology Hay Rd Landfill |  |
| Input Data |  |
|  |  |
| Average Travel Speed |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.4 1.5 |
| Passenger-car equivalents for RV s, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 0.973 0.966 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \text { ATS }}$ (Exhibit 15-9) | 1.00 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 312 234 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |
| Mean speed of sample ${ }^{3}$, $\mathrm{S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(\mathrm{v} / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ (Exhibit 15-15) <br> $1.4 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}, \mathrm{BFFS}$ $55.0 \mathrm{mi} / \mathrm{h}$ <br> Adj. for lane and shoulder width, ${ }^{4} \mathrm{f}_{\mathrm{LS}}($ Exhibit 15-7) $2.6 \mathrm{mi} / \mathrm{h}$ <br> Adj. for access points ${ }^{4}, \mathrm{f}_{\mathrm{A}}$ (Exhibit 15-8) $0.3 \mathrm{mi} / \mathrm{h}$ <br> Free-flow speed, FFS $\left(\mathrm{FSS}=\mathrm{BFFS}-\mathrm{f}_{\mathrm{LS}}{ }^{-\mathrm{f}_{\mathrm{A}}}\right)$ $52.2 \mathrm{mi} / \mathrm{h}$ <br> Average travel speed, ATS $\mathrm{d}_{\mathrm{d}}=\mathrm{FFS}-0.00776\left(\mathrm{v}_{\mathrm{d}, \mathrm{ATS}}{ }^{+}\right.$ $46.5 \mathrm{mi} / \mathrm{h}$ <br> $\left.\mathrm{v}_{\mathrm{o}, \mathrm{ATS}}\right)-\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ $89.2 \%$ <br> Percent free flow speed, PFFS  |
| Percent Time-Spent-Following |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.1 |
| Passenger-car equivalents for RV s, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 0.993 0.993 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 305 228 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{d}(\%)=100\left(1-e^{\text {av }}{ }_{\text {d }}{ }^{\text {b }}\right.$ ) | 31.4 |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \text { PTSF }}$ (Exhibit 15-21) | 38.2 |
| Percent time-spent-following, PTSF $_{d}(\%)=$ BPTSF $_{d}+{ }_{n p, \mathrm{PTSF}}{ }^{*}\left(v_{d, \mathrm{PTSF}} / v_{d, \mathrm{PTSF}}+\right.$ $\mathrm{v}_{\mathrm{o}, \mathrm{PTSF}}$ ) | 53.3 |
| Level of Service and Other Performance Measures |  |
| Level of service, LOS (Exhibit 15-3) | C |
| Volume to capacity ratio, v/c | 0.18 |



| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |
| :---: | :---: |
| General Information | Site Information |
| Analyst JF <br> Agency or Company  <br> Date Performed $10 / 8 / 19$ <br> Analysis Time Period Exist PM | Highway / Direction of Travel Midway Rd <br> From/To west of Porter Rd EB <br> Jurisdiction Solano County <br> Analysis Year 2018 |
| Project Description: Recology Hay Rd Landfill |  |
| Input Data |  |
|  |  |
| Average Travel Speed |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.4 1.4 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 0.973 0.973 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \text { ATS }}($ Exhibit 15-9) | 1.00 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 338 293 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |
| Mean speed of sample ${ }^{3}$, $\mathrm{S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(\mathrm{~V} / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ (Exhibit 15-15) <br> $1.3 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}, \mathrm{BFFS}$ $55.0 \mathrm{mi} / \mathrm{h}$ <br> Adj. for lane and shoulder width, ${ }^{4} \mathrm{f}_{\mathrm{LS}}($ Exhibit 15-7) $2.6 \mathrm{mi} / \mathrm{h}$ <br> Adj. for access points ${ }^{4}, \mathrm{f}_{\mathrm{A}}$ (Exhibit $\left.15-8\right)$ $0.3 \mathrm{mi} / \mathrm{h}$ <br> Free-flow speed, FFS $\left(\mathrm{FSS}=\mathrm{BFFS}-\mathrm{f}_{\mathrm{LS}} \mathrm{f}_{\mathrm{A}}\right)$ $52.2 \mathrm{mi} / \mathrm{h}$ <br> Average travel speed, ATS $\mathrm{d}_{\mathrm{d}}=\mathrm{FFS}-0.00776\left(\mathrm{v}_{\mathrm{d}, \mathrm{ATS}}{ }^{+}\right.$ $45.9 \mathrm{mi} / \mathrm{h}$ <br> $\left.\mathrm{v}_{\mathrm{o}, \mathrm{ATS}}\right)-\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ $88.1 \mathrm{\%}$ <br> Percent free flow speed, PFFS   |
| Percent Time-Spent-Following |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.1 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 0.993 0.993 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 332 287 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{\text {d }}(\%)=100\left(1-\mathrm{e}^{\text {av }}{ }_{\mathrm{d}}{ }^{\text {b }}\right.$ ) | 34.6 |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \mathrm{PTSF}}$ (Exhibit 15-21) | 38.0 |
| $\begin{aligned} & \text { Percent time-spent-following, } \text { PTSF }_{d}(\%)=\text { BPTSF }_{d}+f_{n p, P T S F}{ }^{*}\left(v_{d, \text { PTSF }} / v_{d, \text { PTSF }}+\right. \\ & \left.v_{o, P T S F}\right) \end{aligned}$ | 55.0 |
| Level of Service and Other Performance Measures |  |
| Level of service, LOS (Exhibit 15-3) | C |
| Volume to capacity ratio, v/c | 0.20 |



| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |
| :---: | :---: |
| General Information | Site Information |
| Analyst JF <br> Agency or Company  <br> Date Performed $10 / 8 / 18$ <br> Analysis Time Period Exist PM | Highway / Direction of Travel Midway Rd <br> From/To west of Porter Rd WB <br> Jurisdiction Solano County <br> Analysis Year 2018 |
| Project Description: Recology Hay Rd Landfill |  |
| Input Data |  |
|  |  |
| Average Travel Speed |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.4 1.4 |
| Passenger-car equivalents for RV s, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 0.973 0.973 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \text { ATS }}$ (Exhibit 15-9) | 1.00 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 293 338 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |
| Mean speed of sample ${ }^{3}$, $\mathrm{S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(\mathrm{v} / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ (Exhibit 15-15) <br> $1.3 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}, \mathrm{BFFS}$ $55.0 \mathrm{mi} / \mathrm{h}$ <br> Adj. for lane and shoulder width, ${ }^{4} \mathrm{f}_{\mathrm{LS}}($ Exhibit 15-7) $2.6 \mathrm{mi} / \mathrm{h}$ <br> Adj. for access points ${ }^{4}, \mathrm{f}_{\mathrm{A}}$ (Exhibit 15-8) $0.3 \mathrm{mi} / \mathrm{h}$ <br> Free-flow speed, FFS $\left(\mathrm{FSS}=\mathrm{BFFS}-\mathrm{f}_{\mathrm{LS}} \mathrm{f}_{\mathrm{A}}\right)$ $52.2 \mathrm{mi} / \mathrm{h}$ <br> Average travel speed, ATS $\mathrm{d}_{\mathrm{d}}=\mathrm{FFS}-0.00776\left(\mathrm{v}_{\mathrm{d}, \mathrm{ATS}}{ }^{+}\right.$ $46.0 \mathrm{mi} / \mathrm{h}$ <br> $\left.\mathrm{v}_{\mathrm{o}, \mathrm{ATS}}\right)-\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ $88.1 \%$ <br> Percent free flow speed, PFFS 8 |
| Percent Time-Spent-Following |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.1 |
| Passenger-car equivalents for RV s, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 0.993 0.993 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 287 - 332 |
| Base percent time-spent-following ${ }^{4}$, PPTSF $_{\text {d }}(\%)=100\left(1-\mathrm{e}^{\text {av }}{ }_{\mathrm{d}}{ }^{\text {b }}\right.$ ) | 32.2 |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \mathrm{PTSF}}$ (Exhibit 15-21) | 38.0 |
| Percent time-spent-following, PTSF $_{d}(\%)=$ BPTSF $_{d}+f_{n p, \text { PTSF }}{ }^{*}\left(v_{d, \text { PTSF }} / v_{d, \text { PTSF }}+\right.$ $\mathrm{V}_{\mathrm{o}, \mathrm{PTSF}}$ ) | 49.8 |
| Level of Service and Other Performance Measures |  |
| Level of service, LOS (Exhibit 15-3) | C |
| Volume to capacity ratio, v/c | 0.17 |











| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |
| :---: | :---: |
| General Information | Site Information |
| Analyst $J F$ <br> Agency or Company $4 / 13 / 2018$ <br> Date Performed Analysis Time Period | Highway / Direction of Travel SR 113 <br> south of Midway Rd NB  <br> From/To  <br> Jurisiction Caltrans <br> Analysis Year 2018 |
| Project Description: Recology Hay Rd Landfill |  |
| Input Data |  |
|  |  |
| Average Travel Speed |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.7 1.8 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 0.953 0.947 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{ATS}}$ (Exhibit 15-9) | 1.00 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 148 127 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |
| Mean speed of sample ${ }^{3}$, $\mathrm{S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(\mathrm{~V} / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\text {np,ATS }}$ (Exhibit 15-15) <br> $0.5 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}, \mathrm{BFFS}$ $55.0 \mathrm{mi} / \mathrm{h}$ <br> Adj. for lane and shoulder width, ${ }^{4} \mathrm{f}_{\mathrm{LS}}($ Exhibit 15-7) $4.2 \mathrm{mi} / \mathrm{h}$ <br> Adj. for access points ${ }^{4}, \mathrm{f}_{\mathrm{A}}($ Exhibit $15-8)$ $0.5 \mathrm{mi} / \mathrm{h}$ <br> Free-flow speed, FFS $\left(\right.$ FSS $\left.=\mathrm{BFFS}-\mathrm{f}_{\mathrm{Ls}}{ }^{-\mathrm{f}_{\mathrm{A}}}\right)$ $50.3 \mathrm{mi} / \mathrm{h}$ <br> Average travel speed, ATS ${ }_{\mathrm{d}}=$ FFSS- $0.00776\left(\mathrm{v}_{\mathrm{d}, \mathrm{ATS}}{ }^{+}\right.$ $47.7 \mathrm{mi} / \mathrm{h}$ <br> $\left.\mathrm{v}_{\mathrm{o}, \mathrm{ATS}}\right)-\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$  <br> Percent free flow speed, PFFS $94.8 \%$  |
| Percent Time-Spent-Following |  |
|  | Analysis Direction (d) ${ }^{\text {d }}$ (\|l| Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.1 1.1 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 0.993 0.993 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}\right.$ g,PTSF $)$ | 142 \| 121 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{\text {d }}(\%)=100\left(1-\mathrm{e}^{\text {av }}{ }_{\mathrm{d}}{ }^{\text {b }}\right.$ ) | 16.0 |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \text { PTSF }}$ (Exhibit 15-21) | 24.3 |
| Percent time-spent-following, PTSF $_{d}(\%)=$ BPTSF $_{d}{ }^{+f}{ }_{n p, \text { PTSF }}{ }^{*}\left(v_{d, \text { PTSF }} / v_{d, \text { PTSF }}{ }^{+}\right.$ $\mathrm{v}_{\mathrm{o}, \mathrm{PTSF}}$ ) | 29.1 |
| Level of Service and Other Performance Measures |  |
| Level of service, LOS (Exhibit 15-3) | C |
| Volume to capacity ratio, $\mathrm{V} / \mathrm{c}$ | 0.09 |



| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |
| :---: | :---: |
| General Information | Site Information |
| Analyst $J F$ <br> Agency or Company $4 / 13 / 2018$ <br> Date Performed Analysis Time Period | Highway / Direction of Travel SR 113 <br> south of Midway Rd SB  <br> From/To  <br> Jurisidition Caltrans <br> Analysis Year 2018 |
| Project Description: Recology Hay Rd Landfill |  |
| Input Data |  |
|  |  |
| Average Travel Speed |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.8 1.7 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 0.947 0.953 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{ATS}}$ (Exhibit 15-9) | 1.00 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 127 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |
| Mean speed of sample ${ }^{3}, \mathrm{~S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(\mathrm{v} / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ (Exhibit 15-15) <br> $0.7 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}, \mathrm{BFFS}$ $55.0 \mathrm{mi} / \mathrm{h}$ <br> Adj. for lane and shoulder width, ${ }^{4} \mathrm{f}_{\mathrm{LS}}($ Exhibit $15-7)$ $4.2 \mathrm{mi} / \mathrm{h}$ <br> Adj. for access points ${ }^{4}, \mathrm{f}_{\mathrm{A}}($ Exhibit $15-8)$ $0.5 \mathrm{mi} / \mathrm{h}$ <br> Free-flow speed, FFS $\left(\right.$ FSS $=$ BFFS- $\left.\mathrm{f}_{\mathrm{LS}} \mathrm{f}_{\mathrm{A}}\right)$ $50.3 \mathrm{mi} / \mathrm{h}$ <br> Average travel speed, ATS ${ }_{\mathrm{d}}=$ FFSS- $0.00776\left(\mathrm{v}_{\mathrm{d}, \mathrm{ATS}}{ }^{+}\right.$ $47.5 \mathrm{mi} / \mathrm{h}$ <br> $\left.v_{\mathrm{o}, \mathrm{ATS}}\right)-\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$  <br> Percent free flow speed, PFFS $94.4 \%$  |
| Percent Time-Spent-Following |  |
|  | Analysis Direction (d) ${ }^{\text {d }}$ (\|l| Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.1 1.1 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 0.993 0.993 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}\right.$ g,PTSF $)$ | 121 \|l|r |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{\text {d }}(\%)=100\left(1-\mathrm{e}^{\text {av }}{ }_{\mathrm{d}}{ }^{\text {b }}\right.$ ) | 13.8 |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \text { PTSF }}$ (Exhibit 15-21) | 24.3 |
| Percent time-spent-following, PTSF $_{d}(\%)=$ BPTSF $_{d}{ }^{+f}{ }_{n p, \text { PTSF }}{ }^{*}\left(v_{d, \text { PTSF }} / v_{d, \text { PTSF }}{ }^{+}\right.$ $\mathrm{v}_{\mathrm{o}, \mathrm{PTSF}}$ ) | 25.0 |
| Level of Service and Other Performance Measures |  |
| Level of service, LOS (Exhibit 15-3) | C |
| Volume to capacity ratio, $\mathrm{V} / \mathrm{c}$ | 0.07 |



| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |
| :---: | :---: |
| General Information | Site Information |
| Analyst $J F$ <br> Agency or Company $4 / 13 / 2018$ <br> Date Performed Analysis Time Period | Highway / Direction of Travel SR 113 <br> south of Midway Rd NB  <br> From/To  <br> Jurisiction Caltrans <br> Analysis Year 2018 |
| Project Description: Recology Hay Rd Landfill |  |
| Input Data |  |
|  |  |
| Average Travel Speed |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.5 1.5 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 0.966 0.966 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{ATS}}$ (Exhibit 15-9) | 1.00 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 206 208 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |
| Mean speed of sample ${ }^{3}, \mathrm{~S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(\mathrm{v} / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ (Exhibit 15-15) <br> $1.2 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}, \mathrm{BFFS}$ $55.0 \mathrm{mi} / \mathrm{h}$ <br> Adj. for lane and shoulder width, ${ }^{4} \mathrm{f}_{\mathrm{LS}}($ Exhibit $15-7)$ $4.2 \mathrm{mi} / \mathrm{h}$ <br> Adj. for access points ${ }^{4}, \mathrm{f}_{\mathrm{A}}($ (Exhibit $15-8)$ $0.5 \mathrm{mi} / \mathrm{h}$ <br> Free-flow speed, FFS $\left(\mathrm{FSS}=\mathrm{BFFS}-\mathrm{f}_{\mathrm{LS}} \mathrm{f}_{\mathrm{A}}\right)$ $50.3 \mathrm{mi} / \mathrm{h}$ <br> Average travel speed, ATS ${ }_{\mathrm{d}}=\mathrm{FFS}-0.00776\left(\mathrm{v}_{\mathrm{d}, \mathrm{ATS}}{ }^{+}\right.$ $45.9 \mathrm{mi} / \mathrm{h}$ <br> $\left.\mathrm{v}_{\mathrm{o}, \mathrm{ATS}}\right)$ <br> Percent free flow speed, PFFS $91.2 \%$ |
| Percent Time-Spent-Following |  |
|  | Analysis Direction (d) ${ }^{\text {d }}$ (\|l| Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.1 1.1 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 0.993 0.993 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}\right.$ g,PTSF $)$ | 200 202 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{\text {d }}(\%)=100\left(1-\mathrm{e}^{\text {av }}{ }_{\mathrm{d}}{ }^{\text {b }}\right.$ ) | 21.4 |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \text { PTSF }}$ (Exhibit 15-21) | 31.0 |
| Percent time-spent-following, PTSF $_{d}(\%)=$ BPTSF $_{d}{ }^{+f}{ }_{n p, \text { PTSF }}{ }^{*}\left(v_{d, \text { PTSF }} / v_{d, \text { PTSF }}{ }^{+}\right.$ $\mathrm{v}_{\mathrm{o}, \mathrm{PTSF}}$ ) | 36.8 |
| Level of Service and Other Performance Measures |  |
| Level of service, LOS (Exhibit 15-3) | C |
| Volume to capacity ratio, $\mathrm{V} / \mathrm{c}$ | 0.12 |



| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |
| :---: | :---: |
| General Information | Site Information |
| Analyst $J F$ <br> Agency or Company $4 / 13 / 2018$ <br> Date Performed Analysis Time Period | Highway / Direction of Travel SR 113 <br> south of Midway Rd SB  <br> From/To  <br> Jurisidition Caltrans <br> Analysis Year 2018 |
| Project Description: Recology Hay Rd Landfill |  |
| Input Data |  |
|  |  |
| Average Travel Speed |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.5 1.5 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 0.966 0.966 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{ATS}}$ (Exhibit 15-9) | 1.00 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 208 206 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |
| Mean speed of sample ${ }^{3}, \mathrm{~S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(\mathrm{v} / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ (Exhibit 15-15) <br> $1.2 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}, \mathrm{BFFS}$ $55.0 \mathrm{mi} / \mathrm{h}$ <br> Adj. for lane and shoulder width, ${ }^{4} \mathrm{f}_{\mathrm{LS}}($ Exhibit 15-7) $4.2 \mathrm{mi} / \mathrm{h}$ <br> Adj. for access points ${ }^{4}, \mathrm{f}_{\mathrm{A}}($ Exhibit $15-8)$ $0.5 \mathrm{mi} / \mathrm{h}$ <br> Free-flow speed, FFS (FSS=BFFS-f $\left.\mathrm{f}^{-\mathrm{f}_{\mathrm{A}}}\right)$ $50.3 \mathrm{mi} / \mathrm{h}$ <br> Average travel speed, ATS $\mathrm{d}_{\mathrm{d}}=\mathrm{FFS}-0.00776\left(\mathrm{v}_{\mathrm{d}, \mathrm{ATS}}{ }^{+}\right.$ $45.9 \mathrm{mi} / \mathrm{h}$ <br> $\left.\mathrm{v}_{\mathrm{o}, \mathrm{ATS}}\right)$ - $\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ $91.2 \%$ <br> Percent free flow speed, PFFS  |
| Percent Time-Spent-Following |  |
|  | Analysis Direction (d) ${ }^{\text {d }}$ (\|l| Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.1 1.1 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 0.993 0.993 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}\right.$ g,PTSF $)$ | 202 200 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{\text {d }}(\%)=100\left(1-\mathrm{e}^{\text {av }}{ }_{\mathrm{d}}{ }^{\text {b }}\right.$ ) | 21.7 |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \text { PTSF }}$ (Exhibit 15-21) | 31.0 |
| Percent time-spent-following, PTSF $_{d}(\%)=$ BPTSF $_{d}{ }^{+f}{ }_{n p, \text { PTSF }}{ }^{*}\left(v_{d, \text { PTSF }} / v_{d, \text { PTSF }}{ }^{+}\right.$ $\mathrm{v}_{\mathrm{o}, \mathrm{PTSF}}$ ) | 37.3 |
| Level of Service and Other Performance Measures |  |
| Level of service, LOS (Exhibit 15-3) | C |
| Volume to capacity ratio, $\mathrm{V} / \mathrm{c}$ | 0.12 |











| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |
| :---: | :---: |
| General Information | Site Information |
| Analyst $J F$ <br> Agency or Company $4 / 13 / 2018$ <br> Date Performed Analysis Time Period | Highway / Direction of Travel SR 113 <br> south of Hay Rd NB  <br> From/To  <br> Jurisdiction Caltrans <br> Analysis Year 2018 |
| Project Description: Recology Hay Rd Landfill |  |
| Input Data |  |
|  |  |
| Average Travel Speed |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.4 1.7 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 0.973 0.953 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{ATS}}$ (Exhibit 15-9) | 1.00 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 277 162 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |
| Mean speed of sample ${ }^{3}$, $\mathrm{S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(\mathrm{~V} / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\text {np,ATS }}$ (Exhibit 15-15) <br> $0.8 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}, \mathrm{BFFS}$ $55.0 \mathrm{mi} / \mathrm{h}$ <br> Adj. for lane and shoulder width, ${ }^{4} \mathrm{f}_{\mathrm{LS}}($ Exhibit $15-7)$ $4.2 \mathrm{mi} / \mathrm{h}$ <br> Adj. for access points ${ }^{4}, \mathrm{f}_{\mathrm{A}}($ (Exhibit $15-8)$ $0.5 \mathrm{mi} / \mathrm{h}$ <br> Free-flow speed, FFS $\left(\mathrm{FSS}=\mathrm{BFFS}-\mathrm{f}_{\mathrm{LS}} \mathrm{f}_{\mathrm{A}}\right)$ $50.3 \mathrm{mi} / \mathrm{h}$ <br> Average travel speed, ATS ${ }_{\mathrm{d}}=\mathrm{FFS}-0.00776\left(\mathrm{v}_{\mathrm{d}, \mathrm{ATS}}{ }^{+}\right.$ $46.1 \mathrm{mi} / \mathrm{h}$ <br> $\left.\mathrm{v}_{\mathrm{o}, \mathrm{ATS}}\right)$ <br> Percent free flow speed, PFFS $91.6 \%$ |
| Percent Time-Spent-Following |  |
|  | Analysis Direction (d) ${ }^{\text {d }}$ (\|l| Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.1 1.1 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 0.993 0.993 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}\right.$ g,PTSF $)$ | 271 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{\text {d }}(\%)=100\left(1-\mathrm{e}^{\text {av }}{ }_{\mathrm{d}}{ }^{\text {b }}\right.$ ) | 27.8 |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \text { PTSF }}$ (Exhibit 15-21) | 32.0 |
| Percent time-spent-following, PTSF $_{d}(\%)=$ BPTSF $_{d}{ }^{+f}{ }_{n p, \text { PTSF }}{ }^{*}\left(v_{d, \text { PTSF }} / v_{d, \text { PTSF }}{ }^{+}\right.$ $\mathrm{v}_{\mathrm{o}, \mathrm{PTSF}}$ ) | 48.2 |
| Level of Service and Other Performance Measures |  |
| Level of service, LOS (Exhibit 15-3) | C |
| Volume to capacity ratio, $\mathrm{V} / \mathrm{c}$ | 0.16 |



| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |
| :---: | :---: |
| General Information | Site Information |
| Analyst $J F$ <br> Agency or Company $4 / 13 / 2018$ <br> Date Performed Analysis Time Period | Highway / Direction of Travel SR 113 <br> south of Hay Rd SB  <br> From/To Caltrans <br> Jurisdiction <br> Analysis Year |
| Project Description: Recology Hay Rd Landfill |  |
| Input Data |  |
|  |  |
| Average Travel Speed |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.7 1.4 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 0.953 0.973 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{ATS}}$ (Exhibit 15-9) | 1.00 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 162 277 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |
| Mean speed of sample ${ }^{3}, \mathrm{~S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(\mathrm{v} / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ (Exhibit 15-15) <br> $1.2 \mathrm{mi} / \mathrm{h}$ |  |
| Percent Time-Spent-Following |  |
|  | Analysis Direction (d) ${ }^{\text {d }}$ (\|l| Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.1 1.1 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 0.993 0.993 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}\right.$ g,PTSF $)$ | 155 271 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{\text {d }}(\%)=100\left(1-\mathrm{e}^{\text {av }}{ }_{\mathrm{d}}{ }^{\text {b }}\right.$ ) | 18.9 |
| Adj. for no-passing zone, $\mathrm{f}_{\text {np, PTSF }}$ (Exhibit 15-21) | 32.0 |
| Percent time-spent-following, PTSF $_{d}(\%)=$ BPTSF $_{d}{ }^{+f}{ }_{n p, \text { PTSF }}{ }^{*}\left(v_{d, \text { PTSF }} / v_{d, \text { PTSF }}{ }^{+}\right.$ $\mathrm{v}_{\mathrm{o}, \mathrm{PTSF}}$ ) | 30.5 |
| Level of Service and Other Performance Measures |  |
| Level of service, LOS (Exhibit 15-3) | C |
| Volume to capacity ratio, $\mathrm{V} / \mathrm{c}$ | 0.10 |



| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |
| :---: | :---: |
| General Information | Site Information |
| Analyst $J F$ <br> Agency or Company $4 / 13 / 2018$ <br> Date Performed Analysis Time Period | Highway / Direction of Travel SR 113 <br> south of Hay Rd NB  <br> From/To  <br> Jurisdiction Caltrans <br> Analysis Year 2018 |
| Project Description: Recology Hay Rd Landfill |  |
| Input Data |  |
|  |  |
| Average Travel Speed |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.5 1.4 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 0.966 0.973 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{ATS}}$ (Exhibit 15-9) | 1.00 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 254 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |
| Mean speed of sample ${ }^{3}, \mathrm{~S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(\mathrm{v} / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ (Exhibit 15-15) <br> $1.2 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}, \mathrm{BFFS}$ $55.0 \mathrm{mi} / \mathrm{h}$ <br> Adj. for lane and shoulder width, ${ }^{4} \mathrm{f}_{\mathrm{LS}}($ Exhibit 15-7) $4.2 \mathrm{mi} / \mathrm{h}$ <br> Adj. for access points ${ }^{4}, \mathrm{f}_{\mathrm{A}}($ Exhibit $15-8)$ $0.5 \mathrm{mi} / \mathrm{h}$ <br> Free-flow speed, FFS (FSS=BFFS-f $\left.\mathrm{f}^{-\mathrm{f}_{\mathrm{A}}}\right)$ $50.3 \mathrm{mi} / \mathrm{h}$ <br> Average travel speed, ATS $\mathrm{d}_{\mathrm{d}}=\mathrm{FFS}-0.00776\left(\mathrm{v}_{\mathrm{d}, \mathrm{ATS}}{ }^{+}\right.$ $44.9 \mathrm{mi} / \mathrm{h}$ <br> $\left.\mathrm{v}_{\mathrm{o}, \mathrm{ATS}}\right)$ - $\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ $89.2 \%$ <br> Percent free flow speed, PFFS  |
| Percent Time-Spent-Following |  |
|  | Analysis Direction (d) ${ }^{\text {d }}$ (\|l| Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.1 1.1 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 0.993 0.993 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}\right.$ g,PTSF $)$ | 247 289 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{\text {d }}(\%)=100\left(1-\mathrm{e}^{\text {av }}{ }_{\mathrm{d}}{ }^{\text {b }}\right.$ ) | 28.8 |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \text { PTSF }}$ (Exhibit 15-21) | 35.9 |
| Percent time-spent-following, PTSF $_{d}(\%)=$ BPTSF $_{d}{ }^{+f}{ }_{n p, \text { PTSF }}{ }^{*}\left(v_{d, \text { PTSF }} / v_{d, \text { PTSF }}{ }^{+}\right.$ $\mathrm{v}_{\mathrm{o}, \mathrm{PTSF}}$ ) | 45.3 |
| Level of Service and Other Performance Measures |  |
| Level of service, LOS (Exhibit 15-3) | D |
| Volume to capacity ratio, $\mathrm{V} / \mathrm{c}$ | 0.15 |



| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |
| :---: | :---: |
| General Information | Site Information |
| Analyst $J F$ <br> Agency or Company $4 / 13 / 2018$ <br> Date Performed Analysis Time Period | Highway / Direction of Travel SR 113 <br> south of Hay Rd SB  <br> From/To Caltrans <br> Jurisdiction <br> Analysis Year |
| Project Description: Recology Hay Rd Landfill |  |
| Input Data |  |
|  |  |
| Average Travel Speed |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.4 1.5 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 0.973 0.966 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{ATS}}$ (Exhibit 15-9) | 1.00 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 295 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |
| Mean speed of sample ${ }^{3}, \mathrm{~S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(\mathrm{v} / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ (Exhibit 15-15) <br> $1.2 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}, \mathrm{BFFS}$ $55.0 \mathrm{mi} / \mathrm{h}$ <br> Adj. for lane and shoulder width, ${ }^{4} \mathrm{f}_{\mathrm{LS}}($ Exhibit 15-7) $4.2 \mathrm{mi} / \mathrm{h}$ <br> Adj. for access points ${ }^{4}, \mathrm{f}_{\mathrm{A}}($ Exhibit $15-8)$ $0.5 \mathrm{mi} / \mathrm{h}$ <br> Free-flow speed, FFS $\left(\right.$ FSS $\left.=\mathrm{BFFS}-\mathrm{f}_{\mathrm{Ls}}{ }^{-\mathrm{f}_{\mathrm{A}}}\right)$ $50.3 \mathrm{mi} / \mathrm{h}$ <br> Average travel speed, ATS ${ }_{\mathrm{d}}=$ FFSS- $0.00776\left(\mathrm{v}_{\mathrm{d}, \mathrm{ATS}}{ }^{+}\right.$ $44.9 \mathrm{mi} / \mathrm{h}$ <br> $\left.\mathrm{v}_{\mathrm{o}, \mathrm{ATS}}\right)-\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$  <br> Percent free flow speed, PFFS $89.2 \%$  |
| Percent Time-Spent-Following |  |
|  | Analysis Direction (d) ${ }^{\text {d }}$ (\|l| Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.1 1.1 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 0.993 0.993 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}\right.$ g,PTSF $)$ | 289 247 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{\text {d }}(\%)=100\left(1-\mathrm{e}^{\text {av }}{ }_{\mathrm{d}}{ }^{\text {b }}\right.$ ) | 31.0 |
| Adj. for no-passing zone, $\mathrm{f}_{\text {np, PTSF }}$ (Exhibit 15-21) | 35.9 |
| Percent time-spent-following, PTSF $_{d}(\%)=$ BPTSF $_{d}{ }^{+f}{ }_{n p, \text { PTSF }}{ }^{*}\left(v_{d, \text { PTSF }} / v_{d, \text { PTSF }}{ }^{+}\right.$ $\mathrm{v}_{\mathrm{o}, \mathrm{PTSF}}$ ) | 50.4 |
| Level of Service and Other Performance Measures |  |
| Level of service, LOS (Exhibit 15-3) | D |
| Volume to capacity ratio, $\mathrm{V} / \mathrm{c}$ | 0.17 |











| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |
| :---: | :---: |
| General Information | Site Information |
| Analyst JF <br> Agency or Company  <br> Date Performed $10 / 8 / 18$ <br> Analysis Time Period Exist + Project AM | Highway / Direction of Travel Midway Rd <br> From/To west of Porter Rd EB <br> Jurisdiction Solano County <br> Analysis Year 2018 |
| Project Description: Recology Hay Rd Landfill |  |
| Input Data |  |
|  |  |
| Average Travel Speed |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.5 1.4 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 0.966 0.973 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \text { ATS }}$ (Exhibit 15-9) | 1.00 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 252 325 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |
| Mean speed of sample ${ }^{3}, \mathrm{~S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(\mathrm{v} / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ (Exhibit 15-15) <br> $1.3 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}$, BFFS $55.0 \mathrm{mi} / \mathrm{h}$ <br> Adj. for lane and shoulder width, ${ }^{4} \mathrm{f}_{\mathrm{LS}}($ Exhibit 15-7) $2.6 \mathrm{mi} / \mathrm{h}$ <br> Adj. for access points ${ }^{4}, \mathrm{f}_{\mathrm{A}}$ (Exhibit $\left.15-8\right)$ $0.3 \mathrm{mi} / \mathrm{h}$ <br> Free-flow speed, FFS $\left(\mathrm{FSS}=\mathrm{BFFS}-\mathrm{f}_{\mathrm{LS}} \mathrm{ff}_{\mathrm{A}}\right)$ $52.2 \mathrm{mi} / \mathrm{h}$ <br> Average travel speed, ATS $\mathrm{d}_{\mathrm{d}}=\mathrm{FFS}-0.00776\left(\mathrm{v}_{\mathrm{d}, \mathrm{ATS}}{ }^{+}\right.$ $46.4 \mathrm{mi} / \mathrm{h}$ <br> $\left.\mathrm{v}_{\mathrm{o}, \mathrm{ATS}}\right)-\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ $88.9 \%$ <br> Percent free flow speed, PFFS 8.9 |
| Percent Time-Spent-Following |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.1 1.1 |
| Passenger-car equivalents for $\mathrm{RVs}, \mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 0.993 0.993 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{~F}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 245 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{d}(\%)=100\left(1-e^{\text {av }}{ }_{d}{ }^{\text {b }}\right.$ ) | 28.8 |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \mathrm{PTSF}}$ (Exhibit 15-21) | 38.3 |
| Percent time-spent-following, $\operatorname{PTSF}_{d}(\%)=$ BPTSF $_{d}+{ }_{n p, \mathrm{PTSF}}{ }^{*}\left(v_{d, \mathrm{PTSF}} / v_{d, \mathrm{PTSF}}{ }^{+}\right.$ $\mathrm{V}_{\mathrm{o}, \mathrm{PTSF}}$ ) | 45.4 |
| Level of Service and Other Performance Measures |  |
| Level of service, LOS (Exhibit 15-3) | C |
| Volume to capacity ratio, v/c | 0.15 |



| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |
| :---: | :---: |
| General Information | Site Information |
| Analyst JF <br> Agency or Company  <br> Date Performed $10 / 8 / 18$ <br> Analysis Time Period Exist AM | Highway / Direction of Travel Midway Rd <br> From/To west of Porter Rd WB <br> Jurisdiction Solano County <br> Analysis Year 2018 |
| Project Description: Recology Hay Rd Landfill |  |
| Input Data |  |
|  |  |
| Average Travel Speed |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.4 1.5 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 0.973 0.966 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \text { ATS }}($ Exhibit 15-9) | 1.00 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 325 252 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |
| Mean speed of sample ${ }^{3}$, $\mathrm{S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(\mathrm{~V} / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ (Exhibit 15-15) <br> $1.4 \mathrm{mi} / \mathrm{h}$ |  |
| Percent Time-Spent-Following |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.1 1.1 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 0.993 0.993 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 319 245 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{d}(\%)=100\left(1-e^{\text {av }}{ }_{\text {d }}{ }^{\text {b }}\right.$ ) | 33.6 |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \mathrm{PTSF}}$ (Exhibit 15-21) | 38.3 |
| $\begin{aligned} & \text { Percent time-spent-following, } \text { PTSF }_{d}(\%)=\text { BPTSF }_{d}+f_{n p, P T S F}{ }^{*}\left(v_{d, \text { PTSF }} / v_{d, \text { PTSF }}+\right. \\ & \left.v_{o, P T S F}\right) \end{aligned}$ | 55.3 |
| Level of Service and Other Performance Measures |  |
| Level of service, LOS (Exhibit 15-3) | C |
| Volume to capacity ratio, v/c | 0.19 |



| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |
| :---: | :---: |
| General Information | Site Information |
| Analyst JF <br> Agency or Company  <br> Date Performed $10 / 8 / 18$ <br> Analysis Time Period Exist plus Project PM | Highway / Direction of Travel Midway Rd <br> From/To west of Porter Rd EB <br> Jurisdiction Solano County <br> Analysis Year 2018 |
| Project Description: Recology Hay Rd Landfill |  |
| Input Data |  |
|  |  |
| Average Travel Speed |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.4 1.4 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 0.973 0.973 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \text { ATS }}($ Exhibit 15-9) | 1.00 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 338 306 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |
| Mean speed of sample ${ }^{3}$, $\mathrm{S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(\mathrm{~V} / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ (Exhibit 15-15) <br> $1.3 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}, \mathrm{BFFS}$ $55.0 \mathrm{mi} / \mathrm{h}$ <br> Adj. for lane and shoulder width, ${ }^{4} \mathrm{f}_{\mathrm{LS}}($ Exhibit 15-7) $2.6 \mathrm{mi} / \mathrm{h}$ <br> Adj. for access points ${ }^{4}, \mathrm{f}_{\mathrm{A}}$ (Exhibit $\left.15-8\right)$ $0.3 \mathrm{mi} / \mathrm{h}$ <br> Free-flow speed, FFS $\left(\mathrm{FSS}=\mathrm{BFFS}-\mathrm{f}_{\mathrm{LS}} \mathrm{f}_{\mathrm{A}}\right)$ $52.2 \mathrm{mi} / \mathrm{h}$ <br> Average travel speed, ATS $\mathrm{d}_{\mathrm{d}}=\mathrm{FFS}-0.00776\left(\mathrm{v}_{\mathrm{d}, \mathrm{ATS}}{ }^{+}\right.$ $45.8 \mathrm{mi} / \mathrm{h}$ <br> $\left.\mathrm{v}_{\mathrm{o}, \mathrm{ATS}}\right)-\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ $87.9 \%$ <br> Percent free flow speed, PFFS   |
| Percent Time-Spent-Following |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.1 1.1 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 0.993 0.993 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 332 300 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{\text {d }}(\%)=100\left(1-\mathrm{e}^{\text {av }}{ }_{\mathrm{d}}{ }^{\text {b }}\right.$ ) | 35.7 |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \mathrm{PTSF}}$ (Exhibit 15-21) | 37.9 |
| $\begin{aligned} & \text { Percent time-spent-following, } \text { PTSF }_{d}(\%)=\text { BPTSF }_{d}+f_{n p, P T S F}{ }^{*}\left(v_{d, \text { PTSF }} / v_{d, \text { PTSF }}+\right. \\ & \left.v_{o, P T S F}\right) \end{aligned}$ | 55.6 |
| Level of Service and Other Performance Measures |  |
| Level of service, LOS (Exhibit 15-3) | C |
| Volume to capacity ratio, v/c | 0.20 |



| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |
| :---: | :---: |
| General Information | Site Information |
| Analyst JF <br> Agency or Company  <br> Date Performed $10 / 8 / 18$ <br> Analysis Time Period Exist plus Project PM | Highway / Direction of Travel Midway Rd <br> From/To west of Porter Rd WB <br> Jurisdiction Solano County <br> Analysis Year 2018 |
| Project Description: Recology Hay Rd Landfill |  |
| Input Data |  |
|  |  |
| Average Travel Speed |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.4 1.4 |
| Passenger-car equivalents for RV s, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 0.973 0.973 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \text { ATS }}$ (Exhibit 15-9) | 1.00 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 306 338 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |
| Mean speed of sample ${ }^{3}$, $\mathrm{S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(\mathrm{v} / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ (Exhibit 15-15) <br> $1.3 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}, \mathrm{BFFS}$ $55.0 \mathrm{mi} / \mathrm{h}$ <br> Adj. for lane and shoulder width, ${ }^{4} \mathrm{f}_{\mathrm{LS}}($ Exhibit 15-7) $2.6 \mathrm{mi} / \mathrm{h}$ <br> Adj. for access points ${ }^{4}, \mathrm{f}_{\mathrm{A}}$ (Exhibit $\left.15-8\right)$ $0.3 \mathrm{mi} / \mathrm{h}$ <br> Free-flow speed, FFS $\left(\mathrm{FSS}=\mathrm{BFFS}-\mathrm{f}_{\mathrm{LS}} \mathrm{f}_{\mathrm{A}}\right)$ $52.2 \mathrm{mi} / \mathrm{h}$ <br> Average travel speed, ATS $\mathrm{d}_{\mathrm{d}}=\mathrm{FFS}-0.00776\left(\mathrm{v}_{\mathrm{d}, \mathrm{ATS}}{ }^{+}\right.$ $45.9 \mathrm{mi} / \mathrm{h}$ <br> $\left.\mathrm{v}_{\mathrm{o}, \mathrm{ATS}}\right)-\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ $87.9 \%$ <br> Percent free flow speed, PFFS   |
| Percent Time-Spent-Following |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.1 1.1 |
| Passenger-car equivalents for RV s, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 0.993 0.993 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 300 332 |
| Base percent time-spent-following ${ }^{4}$, PPTSF $_{\text {d }}(\%)=100\left(1-\mathrm{e}^{\text {av }}{ }_{\mathrm{d}}{ }^{\text {b }}\right.$ ) | 33.3 |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \mathrm{PTSF}}$ (Exhibit 15-21) | 37.9 |
| $\qquad$ | 51.3 |
| Level of Service and Other Performance Measures |  |
| Level of service, LOS (Exhibit 15-3) | C |
| Volume to capacity ratio, v/c | 0.18 |



| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |
| :---: | :---: |
| General Information | Site Information |
| Analyst JF <br> Agency or Company  <br> Date Performed $10 / 8 / 18$ <br> Analysis Time Period Exist + Project AM | Highway / Direction of Travel Midway Rd <br> From/To west of SR 113 EB <br> Jurisdiction Solano County <br> Analysis Year 2018 |
| Project Description: Recology Hay Rd Landfill |  |
| Input Data |  |
|  |  |
| Average Travel Speed |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.5 1.6 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 0.966 0.960 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \text { ATS }}($ Exhibit 15-9) | 1.00 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 206175 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |
| Mean speed of sample ${ }^{3}$, $\mathrm{S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(\mathrm{~V} / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ (Exhibit 15-15) <br> $1.1 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}, \mathrm{BFFS}$ $55.0 \mathrm{mi} / \mathrm{h}$ <br> Adj. for lane and shoulder width, ${ }^{4} \mathrm{f}_{\mathrm{LS}}($ Exhibit 15-7) $2.6 \mathrm{mi} / \mathrm{h}$ <br> Adj. for access points ${ }^{4}, \mathrm{f}_{\mathrm{A}}$ (Exhibit 15-8) $0.5 \mathrm{mi} / \mathrm{h}$ <br> Free-flow speed, FFS $\left(\mathrm{FSS}=\mathrm{BFFS}-\mathrm{f}_{\mathrm{LS}} \mathrm{f}_{\mathrm{A}}\right)$ $51.9 \mathrm{mi} / \mathrm{h}$ <br> Average travel speed, ATS $\mathrm{d}_{\mathrm{d}}=\mathrm{FFS}-0.00776\left(\mathrm{v}_{\mathrm{d}, \mathrm{ATS}}{ }^{+}\right.$ $47.9 \mathrm{mi} / \mathrm{h}$ <br> $\left.\mathrm{v}_{\mathrm{o}, \mathrm{ATS}}\right)-\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ $92.3 \%$ <br> Percent free flow speed, PFFS 9. |
| Percent Time-Spent-Following |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.1 1.1 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 0.993 0.993 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 200 170 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{\text {d }}(\%)=100\left(1-\mathrm{e}^{\text {av }}{ }_{\mathrm{d}}{ }^{\text {b }}\right.$ ) | 21.5 |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \mathrm{PTSF}}$ (Exhibit 15-21) | 29.6 |
| $\begin{aligned} & \text { Percent time-spent-following, } \text { PTSF }_{d}(\%)=\text { BPTSF }_{d}+f_{n p, P T S F}{ }^{*}\left(v_{d, \text { PTSF }} / v_{d, \text { PTSF }}+\right. \\ & \left.v_{o, P T S F}\right) \end{aligned}$ | 37.5 |
| Level of Service and Other Performance Measures |  |
| Level of service, LOS (Exhibit 15-3) | C |
| Volume to capacity ratio, v/c | 0.12 |



| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |
| :---: | :---: |
| General Information | Site Information |
| Analyst JF <br> Agency or Company  <br> Date Performed $10 / 8 / 18$ <br> Analysis Time Period Exist + Project AM | Highway / Direction of Travel Midway Rd <br> From/To west of SR 113 WB <br> Jurisdiction Solano County <br> Analysis Year 2018 |
| Project Description: Recology Hay Rd Landfill |  |
| Input Data |  |
|  |  |
| Average Travel Speed |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.6 1.5 |
| Passenger-car equivalents for RVs , $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 0.960 0.966 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \text { ATS }}$ (Exhibit 15-9) | 1.00 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 175 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |
| Mean speed of sample ${ }^{3}$, $\mathrm{S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776(\mathrm{v} / \mathrm{f} \mathrm{HV}, \mathrm{ATS}$ ) <br> Adj. for no-passing zones, $\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ (Exhibit 15-15) <br> $1.3 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}, \mathrm{BFFS}$ $55.0 \mathrm{mi} / \mathrm{h}$ <br> Adj. for lane and shoulder width, ${ }^{4} \mathrm{f}_{\mathrm{LS}}($ Exhibit 15-7) $2.6 \mathrm{mi} / \mathrm{h}$ <br> Adj. for access points ${ }^{4}, \mathrm{f}_{\mathrm{A}}$ (Exhibit 15-8) $0.5 \mathrm{mi} / \mathrm{h}$ <br> Free-flow speed, FFS (FSS=BFFS-f $\left.\mathrm{LS}^{-\mathrm{f}_{\mathrm{A}}}\right)$ $51.9 \mathrm{mi} / \mathrm{h}$ <br> Average travel speed, ATS $=\mathrm{FFS}-0.00776\left(\mathrm{v}_{\mathrm{d}, \mathrm{ATS}}{ }^{+}\right.$ $47.6 \mathrm{mi} / \mathrm{h}$ <br> $\left.\mathrm{v}_{\mathrm{o}, \mathrm{ATS}}\right)-\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ <br> Percent free flow speed, PFFS $91.8 \%$ |
| Percent Time-Spent-Following |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.1 1.1 |
| Passenger-car equivalents for RVs , $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 0.993 0.993 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{\star} \mathrm{f}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 170 200 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{d}(\%)=100\left(1-e^{\text {av }}{ }_{d}{ }^{\text {b }}\right.$ ) | 18.7 |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \text { PTSF }}$ (Exhibit 15-21) | 29.6 |
| Percent time-spent-following, $\operatorname{PTSF}_{d}(\%)=$ BPTSF $_{d}+{ }_{n p, \mathrm{PTSF}}{ }^{*}\left(v_{d, \mathrm{PTSF}} / \mathrm{v}_{d, \mathrm{PTSF}}{ }^{+}\right.$ $\mathrm{V}_{\mathrm{o}, \mathrm{PTSF}}$ ) | 32.3 |
| Level of Service and Other Performance Measures |  |
| Level of service, LOS (Exhibit 15-3) | C |
| Volume to capacity ratio, v/c | 0.10 |



| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |
| :---: | :---: |
| General Information | Site Information |
| Analyst JF <br> Agency or Company  <br> Date Performed $10 / 8 / 18$ <br> Analysis Time Period Exist plus Projcet PM | Highway / Direction of Travel Midway Rd <br> From/To west of SR 113 EB <br> Jurisdiction Solano County <br> Analysis Year 2018 |
| Project Description: Recology Hay Rd Landfill |  |
| Input Data |  |
|  |  |
| Average Travel Speed |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.9 1.8 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 0.941 0.947 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \text { ATS }}$ (Exhibit 15-9) | 1.00 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 58 133 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |
| Mean speed of sample ${ }^{3}, \mathrm{~S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\text {FM }}+0.00776\left(\mathrm{v} / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ (Exhibit 15-15) <br> $0.6 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}, \mathrm{BFFS}$ $55.0 \mathrm{mi} / \mathrm{h}$ <br> Adj. for lane and shoulder width, ${ }^{4} \mathrm{f}_{\mathrm{LS}}($ Exhibit 15-7) $2.6 \mathrm{mi} / \mathrm{h}$ <br> Adj. for access points ${ }^{4}, \mathrm{f}_{\mathrm{A}}$ (Exhibit $\left.15-8\right)$ $0.5 \mathrm{mi} / \mathrm{h}$ <br> Free-flow speed, FFS $\left(\mathrm{FSS}=\mathrm{BFFS}-\mathrm{f}_{\mathrm{LS}} \mathrm{ff}_{\mathrm{A}}\right)$ $51.9 \mathrm{mi} / \mathrm{h}$ <br> Average travel speed, ATS $\mathrm{d}_{\mathrm{d}}=\mathrm{FFS}-0.00776\left(\mathrm{v}_{\mathrm{d}, \mathrm{ATS}}{ }^{+}\right.$ $49.8 \mathrm{mi} / \mathrm{h}$ <br> $\left.\mathrm{v}_{\mathrm{o}, \mathrm{ATS}}\right)-\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ $95.9 \%$ <br> Percent free flow speed, PFFS 9.9 |
| Percent Time-Spent-Following |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.1 1.1 |
| Passenger-car equivalents for $\mathrm{RVs}, \mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 0.993 0.993 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{~F}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 55 127 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{d}(\%)=100\left(1-e^{\text {av }}{ }_{d}{ }^{\text {b }}\right.$ ) | 6.7 |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \mathrm{PTSF}}$ (Exhibit 15-21) | 21.8 |
| Percent time-spent-following, PTSF $_{d}(\%)=$ BPTSF $_{d}+{ }_{n p, \mathrm{PTSF}}{ }^{*}\left(v_{d, \mathrm{PTSF}} / \mathrm{v}_{d, \mathrm{PTSF}}{ }^{+}\right.$ $\mathrm{V}_{\mathrm{o}, \mathrm{PTSF}}$ ) | 13.3 |
| Level of Service and Other Performance Measures |  |
| Level of service, LOS (Exhibit 15-3) | C |
| Volume to capacity ratio, v/c | 0.03 |



| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |
| :---: | :---: |
| General Information | Site Information |
| Analyst JF <br> Agency or Company  <br> Date Performed $10 / 8 / 18$ <br> Analysis Time Period Exist plus Project PM | Highway / Direction of Travel Midway Rd <br> From/To west of SR 113 WB <br> Jurisdiction Solano County <br> Analysis Year 2018 |
| Project Description: Recology Hay Rd Landfill |  |
| Input Data |  |
|  |  |
| Average Travel Speed |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.8 1.9 |
| Passenger-car equivalents for RV s, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 0.947 0.941 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \text { ATS }}$ (Exhibit 15-9) | 1.00 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 133 58 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |
| Mean speed of sample ${ }^{3}$, $\mathrm{S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(\mathrm{v} / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ (Exhibit 15-15) <br> $0.3 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}, \mathrm{BFFS}$ $55.0 \mathrm{mi} / \mathrm{h}$ <br> Adj. for lane and shoulder width, ${ }^{4} \mathrm{f}_{\mathrm{LS}}($ Exhibit 15-7) $2.6 \mathrm{mi} / \mathrm{h}$ <br> Adj. for access points ${ }^{4}, \mathrm{f}_{\mathrm{A}}$ (Exhibit 15-8) $0.5 \mathrm{mi} / \mathrm{h}$ <br> Free-flow speed, FFS (FSS=BFFS-f $\left.\mathrm{LS}^{-\mathrm{f}_{\mathrm{A}}}\right)$ $51.9 \mathrm{mi} / \mathrm{h}$ <br> Average travel speed, ATS $=\mathrm{FFS}-0.00776\left(\mathrm{v}_{\mathrm{d}, \mathrm{ATS}}{ }^{+}\right.$ $50.1 \mathrm{mi} / \mathrm{h}$ <br> $\left.\mathrm{v}_{\mathrm{o}, \mathrm{ATS}}\right)-\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ <br> Percent free flow speed, PFFS $96.5 \%$ |
| Percent Time-Spent-Following |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.1 1.1 |
| Passenger-car equivalents for RV s, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 0.993 0.993 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 127 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{d}(\%)=100\left(1-e^{\text {av }}{ }_{\text {d }}{ }^{\text {b }}\right.$ ) | 14.4 |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \text { PTSF }}$ (Exhibit 15-21) | 21.8 |
| Percent time-spent-following, PTSF $_{d}(\%)=$ BPTSF $_{d}+{ }_{n p, \mathrm{PTSF}}{ }^{*}\left(v_{d, \mathrm{PTSF}} / v_{d, \mathrm{PTSF}}+\right.$ $\mathrm{v}_{\mathrm{o}, \mathrm{PTSF}}$ ) | 29.6 |
| Level of Service and Other Performance Measures |  |
| Level of service, LOS (Exhibit 15-3) | B |
| Volume to capacity ratio, v/c | 0.08 |



| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |
| :---: | :---: |
| General Information | Site Information |
| Analyst JF <br> Agency or Company  <br> Date Performed $10 / 8 / 18$ <br> Analysis Time Period Exist + Project AM <br> Prol  | Highway / Direction of Travel SR 113 <br> From/To south of Midway Rd NB <br> Jurisdiction Caltrans <br> Analysis Year 2018 |
| Project Description: Recology Hay Rd Landfill |  |
| Input Data |  |
|  |  |
| Average Travel Speed |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.7 1.7 |
| Passenger-car equivalents for RVs , $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 0.953 0.953 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \text { ATS }}$ (Exhibit 15-9) | 1.00 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 163 147 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |
| Mean speed of sample ${ }^{3}, \mathrm{~S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(\mathrm{~V} / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ (Exhibit 15-15) <br> $0.7 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}, \mathrm{BFFS}$ $55.0 \mathrm{mi} / \mathrm{h}$ <br> Adj. for lane and shoulder width, ${ }^{4} \mathrm{f}_{\mathrm{LS}}($ Exhibit 15-7) $4.2 \mathrm{mi} / \mathrm{h}$ <br> Adj. for access points ${ }^{4}, \mathrm{f}_{\mathrm{A}}$ (Exhibit 15-8) $0.5 \mathrm{mi} / \mathrm{h}$ <br> Free-flow speed, FFS $\left(\mathrm{FSS}=\mathrm{BFFS}-\mathrm{f}_{\mathrm{LS}}{ }^{-\mathrm{f}_{\mathrm{A}}}\right)$ $50.3 \mathrm{mi} / \mathrm{h}$ <br> Average travel speed, ATS $\mathrm{d}_{\mathrm{d}}=\mathrm{FFS}-0.00776\left(\mathrm{v}_{\mathrm{d}, \mathrm{ATS}}{ }^{+}\right.$ $47.2 \mathrm{mi} / \mathrm{h}$ <br> $\left.\mathrm{v}_{\mathrm{o}, \mathrm{ATS}}\right)-\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ <br> Percent free flow speed, PFFS $93.8 \%$ |
| Percent Time-Spent-Following |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.1 1.1 |
| Passenger-car equivalents for RVs , $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 0.993 0.993 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{\star} \mathrm{f}_{\mathrm{HV}, \mathrm{PTSF}^{*}} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 157 141 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{d}(\%)=100\left(1-e^{\text {av }}{ }_{d}{ }^{\text {b }}\right.$ ) | 17.4 |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \mathrm{PTSF}}$ (Exhibit 15-21) | 25.8 |
| Percent time-spent-following, $\operatorname{PTSF}_{d}(\%)=$ BPTSF $_{d}+{ }_{n p, \mathrm{PTSF}}{ }^{*}\left(v_{d, \mathrm{PTSF}} / \mathrm{v}_{d, \mathrm{PTSF}}{ }^{+}\right.$ <br> $\mathrm{V}_{\mathrm{o}, \mathrm{PTSF}}$ ) | 31.0 |
| Level of Service and Other Performance Measures |  |
| Level of service, LOS (Exhibit 15-3) | C |
| Volume to capacity ratio, v/c | 0.10 |



| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |
| :---: | :---: |
| General Information | Site Information |
| Analyst JF <br> Agency or Company  <br> Date Performed $10 / 8 / 18$ <br> Analysis Time Period Exist + Project AM <br> Prol  | Highway / Direction of Travel SR 113 <br> From/To south of Midway Rd SB <br> Jurisdiction Caltrans <br> Analysis Year 2018 |
| Project Description: Recology Hay Rd Landfill |  |
| Input Data |  |
|  |  |
| Average Travel Speed |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.7 1.7 |
| Passenger-car equivalents for RVs , $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 0.953 0.953 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \text { ATS }}$ (Exhibit 15-9) | 1.00 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 147 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |
| Mean speed of sample ${ }^{3}, \mathrm{~S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(\mathrm{~V} / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ (Exhibit 15-15) <br> $0.8 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}, \mathrm{BFFS}$ $55.0 \mathrm{mi} / \mathrm{h}$ <br> Adj. for lane and shoulder width, ${ }^{4} \mathrm{f}_{\mathrm{LS}}($ (Exhibit 15-7) $4.2 \mathrm{mi} / \mathrm{h}$ <br> Adj. for access points ${ }^{4}, \mathrm{f}_{\mathrm{A}}$ (Exhibit $\left.15-8\right)$ $0.5 \mathrm{mi} / \mathrm{h}$ <br> Free-flow speed, FFS $\left(\mathrm{FSS}=\mathrm{BFFS}-\mathrm{f}_{\mathrm{LS}^{-}} \mathrm{f}_{\mathrm{A}}\right)$ $50.3 \mathrm{mi} / \mathrm{h}$ <br> Average travel speed, ATS $\mathrm{d}_{\mathrm{d}}=\mathrm{FFS}-0.00776\left(\mathrm{v}_{\mathrm{d}, \mathrm{ATS}}{ }^{+}\right.$ $47.0 \mathrm{mi} / \mathrm{h}$ <br> $\left.\mathrm{v}_{\mathrm{o}, \mathrm{ATS}}\right)-\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ $93.5 \%$ <br> Percent free flow speed, PFFS   |
| Percent Time-Spent-Following |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.1 1.1 |
| Passenger-car equivalents for RVs , $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 0.993 0.993 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{\star} \mathrm{f}_{\mathrm{HV}, \mathrm{PTSF}^{*}} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 141 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{d}(\%)=100\left(1-e^{\text {av }}{ }_{d}{ }^{\text {b }}\right.$ ) | 15.9 |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \mathrm{PTSF}}$ (Exhibit 15-21) | 25.8 |
| Percent time-spent-following, $\operatorname{PTSF}_{d}(\%)=$ BPTSF $_{d}+{ }_{n p, \mathrm{PTSF}}{ }^{*}\left(v_{d, \mathrm{PTSF}} / \mathrm{v}_{d, \mathrm{PTSF}}{ }^{+}\right.$ <br> $\mathrm{V}_{\mathrm{o}, \mathrm{PTSF}}$ ) | 28.1 |
| Level of Service and Other Performance Measures |  |
| Level of service, LOS (Exhibit 15-3) | C |
| Volume to capacity ratio, v/c | 0.09 |



| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |
| :---: | :---: |
| General Information | Site Information |
| Analyst JF <br> Agency or Company  <br> Date Performed $10 / 8 / 18$ <br> Analysis Time Period Exist plus Project PM | Highway / Direction of Travel SR 113 <br> From/To south of Midway Rd NB <br> Jurisdiction Caltrans <br> Analysis Year 2018 |
| Project Description: Recology Hay Rd Landfill |  |
| Input Data |  |
|  |  |
| Average Travel Speed |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.5 1.5 |
| Passenger-car equivalents for RVs , $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 0.966 0.966 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \text { ATS }}$ (Exhibit 15-9) | 1.00 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 222 209 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |
| Mean speed of sample ${ }^{3}, \mathrm{~S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(\mathrm{~V} / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ (Exhibit 15-15) <br> $1.2 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}, \mathrm{BFFS}$ $55.0 \mathrm{mi} / \mathrm{h}$ <br> Adj. for lane and shoulder width, ${ }^{4} \mathrm{f}_{\mathrm{LS}}($ Exhibit 15-7) $4.2 \mathrm{mi} / \mathrm{h}$ <br> Adj. for access points ${ }^{4}, \mathrm{f}_{\mathrm{A}}$ (Exhibit 15-8) $0.5 \mathrm{mi} / \mathrm{h}$ <br> Free-flow speed, FFS $\left(\mathrm{FSS}=\mathrm{BFFS}-\mathrm{f}_{\mathrm{LS}}{ }^{-\mathrm{f}_{\mathrm{A}}}\right)$ $50.3 \mathrm{mi} / \mathrm{h}$ <br> Average travel speed, ATS $\mathrm{d}_{\mathrm{d}}=\mathrm{FFS}-0.00776\left(\mathrm{v}_{\mathrm{d}, \mathrm{ATS}}{ }^{+}\right.$ $45.7 \mathrm{mi} / \mathrm{h}$ <br> $\left.\mathrm{v}_{\mathrm{o}, \mathrm{ATS}}\right)-\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ <br> Percent free flow speed, PFFS $90.9 \%$ |
| Percent Time-Spent-Following |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.1 1.1 |
| Passenger-car equivalents for RVs , $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 0.993 0.993 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{\star} \mathrm{f}_{\mathrm{HV}, \mathrm{PTSF}^{*}} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 216 204 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{d}(\%)=100\left(1-e^{\text {av }}{ }_{d}{ }^{\text {b }}\right.$ ) | 22.9 |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \mathrm{PTSF}}$ (Exhibit 15-21) | 30.4 |
| Percent time-spent-following, $\operatorname{PTSF}_{d}(\%)=$ BPTSF $_{d}+{ }_{n p, \mathrm{PTSF}}{ }^{*}\left(v_{d, \mathrm{PTSF}} / \mathrm{v}_{d, \mathrm{PTSF}}{ }^{+}\right.$ <br> $\mathrm{V}_{\mathrm{o}, \mathrm{PTSF}}$ ) | 38.5 |
| Level of Service and Other Performance Measures |  |
| Level of service, LOS (Exhibit 15-3) | C |
| Volume to capacity ratio, v/c | 0.13 |



| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |
| :---: | :---: |
| General Information | Site Information |
| Analyst JF <br> Agency or Company  <br> Date Performed $10 / 8 / 18$ <br> Analysis Time Period Exist plus Projcet PM | Highway / Direction of Travel SR 113 <br> From/To south of Midway Rd SB <br> Jurisdiction Caltrans <br> Analysis Year 2018 |
| Project Description: Recology Hay Rd Landfill |  |
| Input Data |  |
|  |  |
| Average Travel Speed |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.5 1.5 |
| Passenger-car equivalents for RVs , $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 0.966 0.966 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \text { ATS }}$ (Exhibit 15-9) | 1.00 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 209222 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |
| Mean speed of sample ${ }^{3}, \mathrm{~S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(\mathrm{~V} / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ (Exhibit 15-15) <br> $1.2 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}, \mathrm{BFFS}$ $55.0 \mathrm{mi} / \mathrm{h}$ <br> Adj. for lane and shoulder width, ${ }^{4} \mathrm{f}_{\mathrm{LS}}($ (Exhibit 15-7) $4.2 \mathrm{mi} / \mathrm{h}$ <br> Adj. for access points ${ }^{4}, \mathrm{f}_{\mathrm{A}}$ (Exhibit $\left.15-8\right)$ $0.5 \mathrm{mi} / \mathrm{h}$ <br> Free-flow speed, FFS $\left(\mathrm{FSS}=\mathrm{BFFS}-\mathrm{f}_{\mathrm{LS}^{-}} \mathrm{f}_{\mathrm{A}}\right)$ $50.3 \mathrm{mi} / \mathrm{h}$ <br> Average travel speed, ATS $\mathrm{d}_{\mathrm{d}}=\mathrm{FFS}-0.00776\left(\mathrm{v}_{\mathrm{d}, \mathrm{ATS}}{ }^{+}\right.$ $45.7 \mathrm{mi} / \mathrm{h}$ <br> $\left.\mathrm{v}_{\mathrm{o}, \mathrm{ATS}}\right)-\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ $91.0 \%$ <br> Percent free flow speed, PFFS   |
| Percent Time-Spent-Following |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.1 1.1 |
| Passenger-car equivalents for RVs , $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 0.993 0.993 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{\star} \mathrm{f}_{\mathrm{HV}, \mathrm{PTSF}^{*}} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 204 216 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{d}(\%)=100\left(1-e^{\text {av }}{ }_{d}{ }^{\text {b }}\right.$ ) | 22.9 |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \mathrm{PTSF}}$ (Exhibit 15-21) | 30.4 |
| Percent time-spent-following, $\operatorname{PTSF}_{d}(\%)=$ BPTSF $_{d}+{ }_{n p, \mathrm{PTSF}}{ }^{*}\left(v_{d, \mathrm{PTSF}} / \mathrm{v}_{d, \mathrm{PTSF}}{ }^{+}\right.$ <br> $\mathrm{V}_{\mathrm{o}, \mathrm{PTSF}}$ ) | 37.7 |
| Level of Service and Other Performance Measures |  |
| Level of service, LOS (Exhibit 15-3) | C |
| Volume to capacity ratio, v/c | 0.12 |



| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |
| :---: | :---: |
| General Information | Site Information |
| Analyst JF <br> Agency or Company  <br> Date Performed $10 / 8 / 18$ <br> Analysis Time Period Exist + Project AM | Highway / Direction of Travel SR 113 <br> From/To north of Hay Rd NB <br> Jurisdiction Caltrans <br> Analysis Year 2018 |
| Project Description: Recology Hay Rd Landfill |  |
| Input Data |  |
|  |  |
| Average Travel Speed |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.4 1.5 |
| Passenger-car equivalents for RVs , $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 0.973 0.966 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \text { ATS }}$ (Exhibit 15-9) | 1.00 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 288 199 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |
| Mean speed of sample ${ }^{3}$, $\mathrm{S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776(\mathrm{~V} / \mathrm{f} \mathrm{HV}, \mathrm{ATS}$ ) <br> Adj. for no-passing zones, $\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ (Exhibit 15-15) <br> $1.2 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}, \mathrm{BFFS}$ $55.0 \mathrm{mi} / \mathrm{h}$ <br> Adj. for lane and shoulder width, ${ }^{4} \mathrm{f}_{\mathrm{LS}}($ Exhibit 15-7) $4.2 \mathrm{mi} / \mathrm{h}$ <br> Adj. for access points ${ }^{4}, \mathrm{f}_{\mathrm{A}}$ (Exhibit 15-8) $0.5 \mathrm{mi} / \mathrm{h}$ <br> Free-flow speed, FFS (FSS=BFFS-f $\left.\mathrm{LS}^{-\mathrm{f}_{\mathrm{A}}}\right)$ $50.3 \mathrm{mi} / \mathrm{h}$ <br> Average travel speed, ATS $=\mathrm{FFS}-0.00776\left(\mathrm{v}_{\mathrm{d}, \mathrm{ATS}}{ }^{+}\right.$ $45.3 \mathrm{mi} / \mathrm{h}$ <br> $\left.\mathrm{v}_{\mathrm{o}, \mathrm{ATS}}\right)-\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ <br> Percent free flow speed, PFFS $90.1 \%$ |
| Percent Time-Spent-Following |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.1 1.1 |
| Passenger-car equivalents for RVs , $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 0.993 0.993 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{\star} \mathrm{f}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 282 194 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{d}(\%)=100\left(1-e^{\text {av }}{ }_{d}{ }^{\text {b }}\right.$ ) | 28.8 |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \mathrm{PTSF}}$ (Exhibit 15-21) | 27.9 |
| $\qquad$ | 45.3 |
| Level of Service and Other Performance Measures |  |
| Level of service, LOS (Exhibit 15-3) | C |
| Volume to capacity ratio, v/c | 0.17 |



| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |
| :---: | :---: |
| General Information | Site Information |
| Analyst JF <br> Agency or Company  <br> Date Performed $10 / 8 / 18$ <br> Analysis Time Period Exist + Project AM | Highway / Direction of Travel SR 113 <br> From/To north of Hay Rd SB <br> Jurisdiction Caltrans <br> Analysis Year 2018 |
| Project Description: Recology Hay Rd Landfill |  |
| Input Data |  |
|  |  |
| Average Travel Speed |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.5 1.4 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 0.966 0.973 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \text { ATS }}($ Exhibit 15-9) | 1.00 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 199 288 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |
| Mean speed of sample ${ }^{3}$, $\mathrm{S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(\mathrm{~V} / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ (Exhibit 15-15) <br> $1.2 \mathrm{mi} / \mathrm{h}$ |  |
| Percent Time-Spent-Following |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.1 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 0.993 0.993 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 194 282 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{\text {d }}(\%)=100\left(1-\mathrm{e}^{\text {av }}{ }_{\mathrm{d}}{ }^{\text {b }}\right.$ ) | 22.6 |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \mathrm{PTSF}}$ (Exhibit 15-21) | 27.9 |
| $\begin{aligned} & \text { Percent time-spent-following, } \text { PTSF }_{d}(\%)=\text { BPTSF }_{d}+f_{n p, P T S F}{ }^{*}\left(v_{d, \text { PTSF }} / v_{d, \text { PTSF }}+\right. \\ & \left.v_{o, P T S F}\right) \end{aligned}$ | 34.0 |
| Level of Service and Other Performance Measures |  |
| Level of service, LOS (Exhibit 15-3) | C |
| Volume to capacity ratio, v/c | 0.12 |



| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |
| :---: | :---: |
| General Information | Site Information |
| Analyst JF <br> Agency or Company  <br> Date Performed $10 / 8 / 18$ <br> Analysis Time Period Exist plus Project PM | Highway / Direction of Travel SR 113 <br> From/To north of Hay Rd NB <br> Jurisdiction Caltrans <br> Analysis Year 2018 |
| Project Description: Recology Hay Rd Landfill |  |
| Input Data |  |
|  |  |
| Average Travel Speed |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.4 1.4 |
| Passenger-car equivalents for RVs , $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 0.973 0.973 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \text { ATS }}$ (Exhibit 15-9) | 1.00 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 302 273 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |
| Mean speed of sample ${ }^{3}, \mathrm{~S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(\mathrm{~V} / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ (Exhibit 15-15) <br> $1.2 \mathrm{mi} / \mathrm{h}$ |  |
| Percent Time-Spent-Following |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.1 1.1 |
| Passenger-car equivalents for RVs , $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 0.993 0.993 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{\star} \mathrm{f}_{\mathrm{HV}, \mathrm{PTSF}^{*}} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 296 267 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{d}(\%)=100\left(1-e^{\text {av }}{ }_{d}{ }^{\text {b }}\right.$ ) | 32.4 |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \mathrm{PTSF}}$ (Exhibit 15-21) | 29.2 |
| Percent time-spent-following, $\operatorname{PTSF}_{d}(\%)=$ BPTSF $_{d}+{ }_{n p, \mathrm{PTSF}}{ }^{*}\left(v_{d, \mathrm{PTSF}} / \mathrm{v}_{d, \mathrm{PTSF}}{ }^{+}\right.$ <br> $\mathrm{V}_{\mathrm{o}, \mathrm{PTSF}}$ ) | 47.8 |
| Level of Service and Other Performance Measures |  |
| Level of service, LOS (Exhibit 15-3) | D |
| Volume to capacity ratio, v/c | 0.18 |



| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |
| :---: | :---: |
| General Information | Site Information |
| Analyst JF <br> Agency or Company  <br> Date Performed $10 / 8 / 18$ <br> Analysis Time Period Exist plus Project PM | Highway / Direction of Travel SR 113 <br> From/To north of Hay Rd SB <br> Jurisdiction Caltrans <br> Analysis Year 2018 |
| Project Description: Recology Hay Rd Landfill |  |
| Input Data |  |
|  |  |
| Average Travel Speed |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.4 1.4 |
| Passenger-car equivalents for RV s, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 0.973 0.973 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \text { ATS }}$ (Exhibit 15-9) | 1.00 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 273 302 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |
| Mean speed of sample ${ }^{3}$, $\mathrm{S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(\mathrm{v} / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ (Exhibit 15-15) <br> $1.2 \mathrm{mi} / \mathrm{h}$ |  |
| Percent Time-Spent-Following |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.1 |
| Passenger-car equivalents for RV s, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 0.993 0.993 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 267 296 |
| Base percent time-spent-following ${ }^{4}$, PPTSF $_{\text {d }}(\%)=100\left(1-\mathrm{e}^{\text {av }}{ }_{\mathrm{d}}{ }^{\text {b }}\right.$ ) | 30.3 |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \mathrm{PTSF}}$ (Exhibit 15-21) | 29.2 |
| $\qquad$ | 44.1 |
| Level of Service and Other Performance Measures |  |
| Level of service, LOS (Exhibit 15-3) | D |
| Volume to capacity ratio, v/c | 0.16 |



| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |
| :---: | :---: |
| General Information | Site Information |
| Analyst JF <br> Agency or Company  <br> Date Performed $10 / 8 / 18$ <br> Analysis Time Period Exist + Project AM | Highway / Direction of Travel SR 113 <br> From/To south of Hay Rd NB <br> Jurisdiction Caltrans <br> Analysis Year 2018 |
| Project Description: Recology Hay Rd Landfill |  |
| Input Data |  |
|  |  |
| Average Travel Speed |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.4 1.7 |
| Passenger-car equivalents for RV s, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 0.973 0.953 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \text { ATS }}$ (Exhibit 15-9) | 1.00 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 279 164 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |
| Mean speed of sample ${ }^{3}$, $\mathrm{S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(\mathrm{v} / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ (Exhibit 15-15) <br> $0.9 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}, \mathrm{BFFS}$ $55.0 \mathrm{mi} / \mathrm{h}$ <br> Adj. for lane and shoulder width, ${ }^{4} \mathrm{f}_{\mathrm{LS}}($ Exhibit 15-7) $4.2 \mathrm{mi} / \mathrm{h}$ <br> Adj. for access points ${ }^{4}, \mathrm{f}_{\mathrm{A}}$ (Exhibit 15-8) $0.5 \mathrm{mi} / \mathrm{h}$ <br> Free-flow speed, FFS $\left(\mathrm{FSS}=\mathrm{BFFS}-\mathrm{f}_{\mathrm{LS}} \mathrm{f}_{\mathrm{A}}\right)$ $50.3 \mathrm{mi} / \mathrm{h}$ <br> Average travel speed, ATS $\mathrm{d}_{\mathrm{d}}=\mathrm{FFS}-0.00776\left(\mathrm{v}_{\mathrm{d}, \mathrm{ATS}}{ }^{+}\right.$ $46.0 \mathrm{mi} / \mathrm{h}$ <br> $\left.\mathrm{v}_{\mathrm{o}, \mathrm{ATS}}\right)-\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ $91.5 \%$ <br> Percent free flow speed, PFFS  |
| Percent Time-Spent-Following |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.1 |
| Passenger-car equivalents for RV s, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 0.993 0.993 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 274 |
| Base percent time-spent-following ${ }^{4}$, PPTSF $_{\text {d }}(\%)=100\left(1-\mathrm{e}^{\text {av }}{ }_{\mathrm{d}}{ }^{\text {b }}\right.$ ) | 28.1 |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \mathrm{PTSF}}$ (Exhibit 15-21) | 32.1 |
| Percent time-spent-following, PTSF $_{d}(\%)=$ BPTSF $_{d}+{ }_{n p, \mathrm{PTSF}}{ }^{*}\left(v_{d, \mathrm{PTSF}} / v_{d, \mathrm{PTSF}}+\right.$ $\mathrm{v}_{\mathrm{o}, \mathrm{PTSF}}$ ) | 48.5 |
| Level of Service and Other Performance Measures |  |
| Level of service, LOS (Exhibit 15-3) | C |
| Volume to capacity ratio, v/c | 0.16 |



| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |
| :---: | :---: |
| General Information | Site Information |
| Analyst JF <br> Agency or Company  <br> Date Performed $10 / 8 / 18$ <br> Analysis Time Period Exist + Project AM | Highway / Direction of Travel SR 113 <br> From/To south of Hay Rd SB <br> Jurisdiction Caltrans <br> Analysis Year 2018 |
| Project Description: Recology Hay Rd Landfill |  |
| Input Data |  |
|  |  |
| Average Travel Speed |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.7 1.4 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 0.953 0.973 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \text { ATS }}($ Exhibit 15-9) | 1.00 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 164 279 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |
| Mean speed of sample ${ }^{3}$, $\mathrm{S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(\mathrm{~V} / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ (Exhibit 15-15) <br> $1.2 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}, \mathrm{BFFS}$ $55.0 \mathrm{mi} / \mathrm{h}$ <br> Adj. for lane and shoulder width, ${ }^{4} \mathrm{f}_{\mathrm{LS}}($ Exhibit $15-7)$ $4.2 \mathrm{mi} / \mathrm{h}$ <br> Adj. for access points ${ }^{4}, \mathrm{f}_{\mathrm{A}}$ (Exhibit $\left.15-8\right)$ $0.5 \mathrm{mi} / \mathrm{h}$ <br> Free-flow speed, FFS $\left(\mathrm{FSS}=\mathrm{BFFS}-\mathrm{f}_{\mathrm{LS}} \mathrm{f}_{\mathrm{A}}\right)$ $50.3 \mathrm{mi} / \mathrm{h}$ <br> Average travel speed, ATS $\mathrm{d}_{\mathrm{d}}=\mathrm{FFS}-0.00776\left(\mathrm{v}_{\mathrm{d}, \mathrm{ATS}}{ }^{+}\right.$ $45.7 \mathrm{mi} / \mathrm{h}$ <br> $\left.\mathrm{v}_{\mathrm{o}, \mathrm{ATS}}\right)-\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ 90.8 m <br> Percent free flow speed, PFFS   |
| Percent Time-Spent-Following |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.1 1.1 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 0.993 0.993 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 158 274 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{\text {d }}(\%)=100\left(1-\mathrm{e}^{\text {av }}{ }_{\mathrm{d}}{ }^{\text {b }}\right.$ ) | 19.2 |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \mathrm{PTSF}}$ (Exhibit 15-21) | 32.1 |
| $\begin{aligned} & \text { Percent time-spent-following, } \text { PTSF }_{d}(\%)=\text { BPTSF }_{d}+f_{n p, P T S F}{ }^{*}\left(v_{d, \text { PTSF }} / v_{d, \text { PTSF }}+\right. \\ & \left.v_{o, P T S F}\right) \end{aligned}$ | 30.9 |
| Level of Service and Other Performance Measures |  |
| Level of service, LOS (Exhibit 15-3) | C |
| Volume to capacity ratio, v/c | 0.10 |



| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |
| :---: | :---: |
| General Information | Site Information |
| Analyst JF <br> Agency or Company  <br> Date Performed $10 / 8 / 18$ <br> Analysis Time Period Exist plus Project PM | Highway / Direction of Travel SR 113 <br> From/To south of Hay Rd NB <br> Jurisdiction Caltrans <br> Analysis Year 2018 |
| Project Description: Recology Hay Rd Landfill |  |
| Input Data |  |
|  |  |
| Average Travel Speed |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.5 1.4 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 0.966 0.973 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \text { ATS }}($ Exhibit 15-9) | 1.00 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 254 299 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |
| Mean speed of sample ${ }^{3}$, $\mathrm{S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(\mathrm{~V} / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ (Exhibit 15-15) <br> $1.2 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}, \mathrm{BFFS}$ $55.0 \mathrm{mi} / \mathrm{h}$ <br> Adj. for lane and shoulder width, ${ }^{4} \mathrm{f}_{\mathrm{LS}}($ Exhibit 15-7) $4.2 \mathrm{mi} / \mathrm{h}$ <br> Adj. for access points ${ }^{4}, \mathrm{f}_{\mathrm{A}}$ (Exhibit 15-8) $0.5 \mathrm{mi} / \mathrm{h}$ <br> Free-flow speed, FFS $\left(\mathrm{FSS}=\mathrm{BFFS}-\mathrm{f}_{\mathrm{LS}} \mathrm{f}_{\mathrm{A}}\right)$ $50.3 \mathrm{mi} / \mathrm{h}$ <br> Average travel speed, ATS $\mathrm{d}_{\mathrm{d}}=\mathrm{FFS}-0.00776\left(\mathrm{v}_{\mathrm{d}, \mathrm{ATS}}{ }^{+}\right.$ $44.8 \mathrm{mi} / \mathrm{h}$ <br> $\left.\mathrm{v}_{\mathrm{o}, \mathrm{ATS}}\right)-\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ $89.2 \%$ <br> Percent free flow speed, PFFS 8.2 |
| Percent Time-Spent-Following |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.1 1.1 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 0.993 0.993 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 247 293 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{\text {d }}(\%)=100\left(1-\mathrm{e}^{\text {av }}{ }_{\mathrm{d}}{ }^{\text {b }}\right.$ ) | 28.6 |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \mathrm{PTSF}}$ (Exhibit 15-21) | 35.8 |
| $\begin{aligned} & \text { Percent time-spent-following, } \text { PTSF }_{d}(\%)=\text { BPTSF }_{d}+f_{n p, P T S F}{ }^{*}\left(v_{d, \text { PTSF }} / v_{d, \text { PTSF }}+\right. \\ & \left.v_{o, P T S F}\right) \end{aligned}$ | 45.0 |
| Level of Service and Other Performance Measures |  |
| Level of service, LOS (Exhibit 15-3) | D |
| Volume to capacity ratio, v/c | 0.15 |



| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |
| :---: | :---: |
| General Information | Site Information |
| Analyst JF <br> Agency or Company  <br> Date Performed $10 / 8 / 18$ <br> Analysis Time Period Exist plus Project PM | Highway / Direction of Travel SR 113 <br> From/To south of Hay Rd SB <br> Jurisdiction Caltrans <br> Analysis Year 2018 |
| Project Description: Recology Hay Rd Landfill |  |
| Input Data |  |
|  |  |
| Average Travel Speed |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.4 1.5 |
| Passenger-car equivalents for RV s, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 0.973 0.966 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \text { ATS }}$ (Exhibit 15-9) | 1.00 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 299 254 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |
| Mean speed of sample ${ }^{3}$, $\mathrm{S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(\mathrm{v} / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ (Exhibit 15-15) <br> $1.2 \mathrm{mi} / \mathrm{h}$ |  |
| Percent Time-Spent-Following |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.1 |
| Passenger-car equivalents for RV s, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 0.993 0.993 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 293 247 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{d}(\%)=100\left(1-e^{\text {av }}{ }_{\text {d }}{ }^{\text {b }}\right.$ ) | 31.3 |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \mathrm{PTSF}}$ (Exhibit 15-21) | 35.8 |
| $\qquad$ | 50.7 |
| Level of Service and Other Performance Measures |  |
| Level of service, LOS (Exhibit 15-3) | D |
| Volume to capacity ratio, v/c | 0.18 |



| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |
| :---: | :---: |
| General Information | Site Information |
| Analyst JF <br> Agency or Company  <br> Date Performed $10 / 8 / 18$ <br> Analysis Time Period Exist + Project AM | Highway / Direction of Travel Hay Rd <br> From/To west of SR 113 EB <br> Jurisdiction Solano County <br> Analysis Year 2018 |
| Project Description: Recology Hay Rd Landfill |  |
| Input Data |  |
|  |  |
| Average Travel Speed |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.9 1.9 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 0.941 0.941 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \text { ATS }}$ (Exhibit 15-9) | 1.00 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 94 75 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |
| Mean speed of sample ${ }^{3}, \mathrm{~S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(\mathrm{v} / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ (Exhibit 15-15) <br> $0.2 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}, \mathrm{BFFS}$ $55.0 \mathrm{mi} / \mathrm{h}$ <br> Adj. for lane and shoulder width, ${ }^{4} \mathrm{f}_{\mathrm{LS}}($ Exhibit 15-7) $4.2 \mathrm{mi} / \mathrm{h}$ <br> Adj. for access points ${ }^{4}, \mathrm{f}_{\mathrm{A}}$ (Exhibit $\left.15-8\right)$ $0.3 \mathrm{mi} / \mathrm{h}$ <br> Free-flow speed, FFS $\left(\mathrm{FSS}=\mathrm{BFFS}-\mathrm{f}_{\mathrm{LS}} \mathrm{ff}_{\mathrm{A}}\right)$ $50.5 \mathrm{mi} / \mathrm{h}$ <br> Average travel speed, ATS $\mathrm{d}_{\mathrm{d}}=\mathrm{FFS}-0.00776\left(\mathrm{v}_{\mathrm{d}, \mathrm{ATS}}{ }^{+}\right.$ $49.0 \mathrm{mi} / \mathrm{h}$ <br> $\left.\mathrm{v}_{\mathrm{o}, \mathrm{ATS}}\right)-\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ $96.9 \%$ <br> Percent free flow speed, PFFS 9.9 |
| Percent Time-Spent-Following |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.1 1.1 |
| Passenger-car equivalents for $\mathrm{RVs}, \mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 0.993 0.993 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{~F}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 89 71 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{d}(\%)=100\left(1-e^{\text {av }}{ }_{d}{ }^{\text {b }}\right.$ ) | 10.5 |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \mathrm{PTSF}}$ (Exhibit 15-21) | 30.0 |
| Percent time-spent-following, PTSF $_{d}(\%)=$ BPTSF $_{d}+{ }_{n p, \mathrm{PTSF}}{ }^{*}\left(v_{d, \mathrm{PTSF}} / \mathrm{v}_{d, \mathrm{PTSF}}{ }^{+}\right.$ $\mathrm{V}_{\mathrm{o}, \mathrm{PTSF}}$ ) | 27.2 |
| Level of Service and Other Performance Measures |  |
| Level of service, LOS (Exhibit 15-3) | C |
| Volume to capacity ratio, v/c | 0.05 |



| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |
| :---: | :---: |
| General Information | Site Information |
| Analyst JF <br> Agency or Company  <br> Date Performed $10 / 8 / 18$ <br> Analysis Time Period Exist AM | Highway / Direction of Travel Hay Rd <br> From/To west of SR 113 WB <br> Jurisdiction Solano County <br> Analysis Year 2018 |
| Project Description: Recology Hay Rd Landfill |  |
| Input Data |  |
|  |  |
| Average Travel Speed |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.9 1.9 |
| Passenger-car equivalents for RV s, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 0.941 0.941 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{ATS}}$ (Exhibit 15-9) | 1.00 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 75 94 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |
| Mean speed of sample ${ }^{3}$, $\mathrm{S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776(\mathrm{v/f} \mathrm{fV}, \mathrm{ATS})$ <br> Adj. for no-passing zones, $\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ (Exhibit 15-15) <br> $0.2 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}, \mathrm{BFFS}$ $55.0 \mathrm{mi} / \mathrm{h}$ <br> Adj. for lane and shoulder width, ${ }^{4} \mathrm{f}_{\mathrm{LS}}($ (Exhibit 15-7) $4.2 \mathrm{mi} / \mathrm{h}$ <br> Adj. for access points ${ }^{4}, \mathrm{f}_{\mathrm{A}}$ (Exhibit $\left.15-8\right)$ $0.3 \mathrm{mi} / \mathrm{h}$ <br> Free-flow speed, FFS $\left(\mathrm{FSS}=\mathrm{BFFS}-\mathrm{f}_{\mathrm{LS}^{-}} \mathrm{f}_{\mathrm{A}}\right)$ $50.5 \mathrm{mi} / \mathrm{h}$ <br> Average travel speed, ATS $\mathrm{d}_{\mathrm{d}}=\mathrm{FFS}-0.00776\left(\mathrm{v}_{\mathrm{d}, \mathrm{ATS}}{ }^{+}\right.$ $49.0 \mathrm{mi} / \mathrm{h}$ <br> $\left.\mathrm{v}_{\mathrm{o}, \mathrm{ATS}}\right)-\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ $96.9 \%$ <br> Percent free flow speed, PFFS   |
| Percent Time-Spent-Following |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.1 1.1 |
| Passenger-car equivalents for RV , $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 0.993 0.993 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{\star} \mathrm{f}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 71 年 89 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{d}(\%)=100\left(1-e^{\text {av }}{ }_{d}{ }^{\text {b }}\right.$ ) | 8.5 |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \mathrm{PTSF}}$ (Exhibit 15-21) | 30.0 |
| $\begin{aligned} & \text { Percent time-spent-following, } \text { PTSF }_{d}(\%)=\text { BPTSF }_{d}+f_{n p, P T S F}{ }^{*}\left(v_{d, \text { PTSF }} / v_{d, \text { PTSF }}+\right. \\ & \left.v_{o, P T S F}\right) \end{aligned}$ | 21.8 |
| Level of Service and Other Performance Measures |  |
| Level of service, LOS (Exhibit 15-3) | C |
| Volume to capacity ratio, v/c | 0.04 |



| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |
| :---: | :---: |
| General Information | Site Information |
| Analyst JF <br> Agency or Company  <br> Date Performed $10 / 8 / 18$ <br> Analysis Time Period Exist plus Project PM | Highway / Direction of Travel Hay Rd <br> From/To west of SR 113 EB <br> Jurisdiction Solano County <br> Analysis Year 2018 |
| Project Description: Recology Hay Rd Landfill |  |
| Input Data |  |
|  |  |
| Average Travel Speed |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.9 1.9 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 0.941 0.941 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \text { ATS }}$ (Exhibit 15-9) | 1.00 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 87 ( 38 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |
| Mean speed of sample ${ }^{3}, \mathrm{~S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(\mathrm{v} / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ (Exhibit 15-15) <br> $0.2 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}, \mathrm{BFFS}$ $55.0 \mathrm{mi} / \mathrm{h}$ <br> Adj. for lane and shoulder width, ${ }^{4} \mathrm{f}_{\mathrm{LS}}($ Exhibit 15-7) $4.2 \mathrm{mi} / \mathrm{h}$ <br> Adj. for access points ${ }^{4}, \mathrm{f}_{\mathrm{A}}$ (Exhibit $\left.15-8\right)$ $0.3 \mathrm{mi} / \mathrm{h}$ <br> Free-flow speed, FFS $\left(\mathrm{FSS}=\mathrm{BFFS}-\mathrm{f}_{\mathrm{LS}} \mathrm{ff}_{\mathrm{A}}\right)$ $50.5 \mathrm{mi} / \mathrm{h}$ <br> Average travel speed, ATS $\mathrm{d}_{\mathrm{d}}=\mathrm{FFS}-0.00776\left(\mathrm{v}_{\mathrm{d}, \mathrm{ATS}}{ }^{+}\right.$ $49.3 \mathrm{mi} / \mathrm{h}$ <br> $\left.\mathrm{v}_{\mathrm{o}, \mathrm{ATS}}\right)-\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ $97.6 \%$ <br> Percent free flow speed, PFFS 9.6 |
| Percent Time-Spent-Following |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.1 1.1 |
| Passenger-car equivalents for $\mathrm{RVs}, \mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 0.993 0.993 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{~F}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 82 36 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{d}(\%)=100\left(1-e^{\text {av }}{ }_{d}{ }^{\text {b }}\right.$ ) | 9.7 |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \mathrm{PTSF}}$ (Exhibit 15-21) | 28.2 |
| Percent time-spent-following, PTSF $_{d}(\%)=$ BPTSF $_{d}+{ }_{n p, \mathrm{PTSF}}{ }^{*}\left(v_{d, \mathrm{PTSF}} / v_{d, \mathrm{PTSF}}+\right.$ $\mathrm{V}_{\mathrm{o}, \mathrm{PTSF}}$ ) | 29.3 |
| Level of Service and Other Performance Measures |  |
| Level of service, LOS (Exhibit 15-3) | C |
| Volume to capacity ratio, v/c | 0.05 |



| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |  |
| :---: | :---: | :---: |
| General Information | Site Information |  |
| Analyst $J F$ <br> Agency or Company $10 / 8 / 18$ <br> Date Performed Exist plus Project PM <br> Analysis Time Period  | Highway / Direction of Travel Hay Rd <br> From/To west of SR 113 WB <br> Jurisdiction Solano County <br> Analysis Year 2018 |  |
| Project Description: Recology Hay Rd Landfill |  |  |
| Input Data |  |  |
|  |  <br> highway <br> Terrain <br> Grade Le <br> Peak-hou <br> No-passin <br> \% Trucks <br> \% Recrea <br> Access p |  |
| Average Travel Speed |  |  |
|  | Analysis Direction (d) | Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 2.6 | 1.9 |
| Passenger-car equivalents for $\mathrm{RVs}, \mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.1 | 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 0.899 | 0.941 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \text { ATS }}$ (Exhibit 15-9) | 0.78 | 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 51 | 87 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |  |
| Mean speed of sample ${ }^{3}$, $\mathrm{S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(\mathrm{~V} / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ (Exhibit 15-15) <br> $0.2 \mathrm{mi} / \mathrm{h}$ |  |  |
| Percent Time-Spent-Following |  |  |
|  | Analysis Direction (d) | Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.0 | 1.1 |
| Passenger-car equivalents for $\mathrm{RVs}, \mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 | 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 1.000 | 0.993 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 | 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{\star} \mathrm{f}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 36 | 82 |
| Base percent time-spent-following ${ }^{4}$, PPTSF $_{\text {d }}(\%)=100\left(1-\mathrm{e}^{\text {av }}{ }_{\text {d }}{ }^{\text {b }}\right.$ ) | 4.5 |  |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \mathrm{PTSF}}$ (Exhibit 15-21) | 28.2 |  |
| $\begin{aligned} & \text { Percent time-spent-following, } \text { PTSF }_{d}(\%)=\text { BPTSF }_{d}+f_{n p, P T S F}{ }^{*}\left(v_{d, \text { PTSF }} / v_{d, \text { PTSF }}+\right. \\ & \left.v_{o, P T S F}\right) \end{aligned}$ | 13.1 |  |
| Level of Service and Other Performance Measures |  |  |
| Level of service, LOS (Exhibit 15-3) | C |  |
| Volume to capacity ratio, v/c | 0.03 |  |



| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |
| :---: | :---: |
| General Information | Site Information |
| Analyst $J F$ <br> Agency or Company  <br> Date Performed $10 / 8 / 18$ <br> Analysis Time Period $A M$ | Highway / Direction of Travel Midway Rd <br> From/To west of Porter Rd EB <br> Jurisdiction Solano County <br> Analysis Year Cumulative |
| Project Description: Recology Hay Rd Landfill |  |
| Input Data |  |
|  |  |
| Average Travel Speed |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.4 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 0.973 0.979 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \text { ATS }}$ (Exhibit 15-9) | 1.00 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 274 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |
| Mean speed of sample ${ }^{3}, \mathrm{~S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\text {FM }}+0.00776\left(\mathrm{v} / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ (Exhibit 15-15) <br> $1.2 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}$, BFFS $55.0 \mathrm{mi} / \mathrm{h}$ <br> Adj. for lane and shoulder width, ${ }^{4} \mathrm{f}_{\mathrm{LS}}($ Exhibit 15-7) $2.6 \mathrm{mi} / \mathrm{h}$ <br> Adj. for access points ${ }^{4}, \mathrm{f}_{\mathrm{A}}$ (Exhibit $\left.15-8\right)$ $0.3 \mathrm{mi} / \mathrm{h}$ <br> Free-flow speed, FFS $\left(\mathrm{FSS}=\mathrm{BFFS}-\mathrm{f}_{\mathrm{LS}} \mathrm{ff}_{\mathrm{A}}\right)$ $52.2 \mathrm{mi} / \mathrm{h}$ <br> Average travel speed, ATS $\mathrm{d}_{\mathrm{d}}=\mathrm{FFS}-0.00776\left(\mathrm{v}_{\mathrm{d}, \mathrm{ATS}}{ }^{+}\right.$ $45.5 \mathrm{mi} / \mathrm{h}$ <br> $\left.\mathrm{v}_{\mathrm{o}, \mathrm{ATS}}\right)-\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ $87.3 \%$ <br> Percent free flow speed, PFFS 8.3 |
| Percent Time-Spent-Following |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.1 1.0 |
| Passenger-car equivalents for $\mathrm{RVs}, \mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 0.993 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{~F}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 268 早 418 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{d}(\%)=100\left(1-e^{\text {av }}{ }_{d}{ }^{\text {b }}\right.$ ) | 32.3 |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \mathrm{PTSF}}$ (Exhibit 15-21) | 33.2 |
| Percent time-spent-following, $\operatorname{PTSF}_{d}(\%)=$ BPTSF $_{d}+{ }_{n p, \mathrm{PTSF}}{ }^{*}\left(v_{d, \mathrm{PTSF}} / v_{d, \mathrm{PTSF}}{ }^{+}\right.$ $\mathrm{V}_{\mathrm{o}, \mathrm{PTSF}}$ ) | 45.3 |
| Level of Service and Other Performance Measures |  |
| Level of service, LOS (Exhibit 15-3) | C |
| Volume to capacity ratio, v/c | 0.16 |



| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |
| :---: | :---: |
| General Information | Site Information |
| Analyst $J F$ <br> Agency or Company $10 / 8 / 18$ <br> Date Performed AM <br> Analysis Time Period  | Highway / Direction of Travel Midway Rd <br> From/To west of Porter Rd WB <br> Jurisdiction Solano County <br> Analysis Year Cumulative |
| Project Description: Recology Hay Rd Landfill |  |
| Input Data |  |
|  |  |
| Average Travel Speed |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.3 1.4 |
| Passenger-car equivalents for RV s, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 0.979 0.973 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \text { ATS }}$ (Exhibit 15-9) | 1.00 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 427 274 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |
| Mean speed of sample ${ }^{3}$, $\mathrm{S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(\mathrm{v} / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ (Exhibit 15-15) <br> $1.3 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}, \mathrm{BFFS}$ $55.0 \mathrm{mi} / \mathrm{h}$ <br> Adj. for lane and shoulder width, ${ }^{4} \mathrm{f}_{\mathrm{LS}}($ Exhibit 15-7) $2.6 \mathrm{mi} / \mathrm{h}$ <br> Adj. for access points ${ }^{4}, \mathrm{f}_{\mathrm{A}}$ (Exhibit 15-8) $0.3 \mathrm{mi} / \mathrm{h}$ <br> Free-flow speed, FFS $\left(\mathrm{FSS}=\mathrm{BFFS}-\mathrm{f}_{\mathrm{LS}} \mathrm{f}_{\mathrm{A}}\right)$ $52.2 \mathrm{mi} / \mathrm{h}$ <br> Average travel speed, ATS $\mathrm{d}_{\mathrm{d}}=\mathrm{FFS}-0.00776\left(\mathrm{v}_{\mathrm{d}, \mathrm{ATS}}{ }^{+}\right.$ $45.4 \mathrm{mi} / \mathrm{h}$ <br> $\left.\mathrm{v}_{\mathrm{o}, \mathrm{ATS}}\right)-\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ $87.0 \%$ <br> Percent free flow speed, PFFS 8 |
| Percent Time-Spent-Following |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.0 1.1 |
| Passenger-car equivalents for RV s, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 1.000 0.993 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 418 268 |
| Base percent time-spent-following ${ }^{4}$, PPTSF $_{\text {d }}(\%)=100\left(1-\mathrm{e}^{\text {av }}{ }_{\mathrm{d}}{ }^{\text {b }}\right.$ ) | 42.0 |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \mathrm{PTSF}}$ (Exhibit 15-21) | 33.2 |
| Percent time-spent-following, PTSF $_{d}(\%)=$ BPTSF $_{d}+{ }_{n p, \mathrm{PTSF}}{ }^{*}\left(v_{d, \mathrm{PTSF}} / v_{d, \mathrm{PTSF}}+\right.$ $\mathrm{v}_{\mathrm{o}, \mathrm{PTSF}}$ ) | 62.2 |
| Level of Service and Other Performance Measures |  |
| Level of service, LOS (Exhibit 15-3) | C |
| Volume to capacity ratio, v/c | 0.25 |



| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |
| :---: | :---: |
| General Information | Site Information |
| Analyst $J F$ <br> Agency or Company $10 / 8 / 18$ <br> Date Performed $P M$ <br> Analysis Time Period  | Highway / Direction of Travel Midway Rd <br> From/To west of Porter Rd EB <br> Jurisdiction Solano County <br> Analysis Year Cumulative |
| Project Description: Recology Hay Rd Landfill |  |
| Input Data |  |
|  |  |
| Average Travel Speed |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.1 1.3 |
| Passenger-car equivalents for $\mathrm{RVs}, \mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 0.993 0.979 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \text { ATS }}$ (Exhibit 15-9) | 1.00 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 635 450 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |
| Mean speed of sample ${ }^{3}, \mathrm{~S}_{\text {FM }}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(\mathrm{v/} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ (Exhibit 15-15) <br> $1.1 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}, \mathrm{BFFS}$ $55.0 \mathrm{mi} / \mathrm{h}$ <br> Adj. for lane and shoulder width, ${ }^{4} \mathrm{f}_{\mathrm{LS}}($ Exhibit 15-7) $2.6 \mathrm{mi} / \mathrm{h}$ <br> Adj. for access points ${ }^{4}, \mathrm{f}_{\mathrm{A}}$ (Exhibit $\left.15-8\right)$ $0.3 \mathrm{mi} / \mathrm{h}$ <br> Free-flow speed, FFS $\left(\mathrm{FSS}=\mathrm{BFFS}-\mathrm{f}_{\mathrm{LS}} \mathrm{ff}_{\mathrm{A}}\right)$ $52.2 \mathrm{mi} / \mathrm{h}$ <br> Average travel speed, ATS $\mathrm{d}_{\mathrm{d}}=\mathrm{FFS}-0.00776\left(\mathrm{v}_{\mathrm{d}, \mathrm{ATS}}{ }^{+}\right.$ $42.6 \mathrm{mi} / \mathrm{h}$ <br> $\left.\mathrm{v}_{\mathrm{o}, \mathrm{ATS}}\right)-\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ $81.7 \%$ <br> Percent free flow speed, PFFS 8.7 |
| Percent Time-Spent-Following |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Passenger-car equivalents for $\mathrm{RVs}, \mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 1.000 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{\star} \mathrm{f}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 630 440 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{d}(\%)=100\left(1-e^{\text {av }}{ }_{d}{ }^{\text {b }}\right.$ ) | 57.6 |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \mathrm{PTSF}}$ (Exhibit 15-21) | 24.9 |
| $\begin{aligned} & \text { Percent time-spent-following, } \text { PTSF }_{d}(\%)=\text { BPTSF }_{d}+f_{n p, P T S F}{ }^{*}\left(v_{d, \text { PTSF }} / v_{d, \text { PTSF }}+\right. \\ & \left.v_{o, P T S F}\right) \end{aligned}$ | 72.3 |
| Level of Service and Other Performance Measures |  |
| Level of service, LOS (Exhibit 15-3) | D |
| Volume to capacity ratio, v/c | 0.37 |



| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |
| :---: | :---: |
| General Information | Site Information |
| Analyst $J F$ <br> Agency or Company  <br> Date Performed $10 / 8 / 18$ <br> Analysis Time Period PM | Highway / Direction of Travel Midway Rd <br> From/To west of Porter Rd WB <br> Jurisdiction Solano County <br> Analysis Year Cumulative |
| Project Description: Recology Hay Rd Landfill |  |
| Input Data |  |
|  |  |
| Average Travel Speed |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.3 1.1 |
| Passenger-car equivalents for RVs , $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 0.979 0.993 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \text { ATS }}$ (Exhibit 15-9) | 1.00 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 450 635 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |
| Mean speed of sample ${ }^{3}$, $\mathrm{S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776(\mathrm{~V} / \mathrm{f} \mathrm{HV}, \mathrm{ATS}$ ) <br> Adj. for no-passing zones, $\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ (Exhibit 15-15) <br> $0.7 \mathrm{mi} / \mathrm{h}$ |  |
| Percent Time-Spent-Following |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Passenger-car equivalents for RVs , $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 1.000 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{\star} \mathrm{f}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 440 年 630 |
| Base percent time-spent-following ${ }^{4}$, PPTSF $_{\text {d }}(\%)=100\left(1-\mathrm{e}^{\text {av }}{ }_{\mathrm{d}}{ }^{\text {b }}\right.$ ) | 49.0 |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \mathrm{PTSF}}$ (Exhibit 15-21) | 24.9 |
| $\qquad$ | 59.2 |
| Level of Service and Other Performance Measures |  |
| Level of service, LOS (Exhibit 15-3) | D |
| Volume to capacity ratio, v/c | 0.26 |



| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |
| :---: | :---: |
| General Information | Site Information |
| Analyst $J F$ <br> Agency or Company  <br> Date Performed $10 / 8 / 18$ <br> Analysis Time Period $A M$ | Highway / Direction of Travel Midway Rd <br> From/To west of SR 113 EB <br> Jurisdiction Solano County <br> Analysis Year Cumulative plus Project |
| Project Description: Recology Hay Rd Landfill |  |
| Input Data |  |
|  |  |
| Average Travel Speed |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.4 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 0.973 0.973 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \text { ATS }}$ (Exhibit 15-9) | 1.00 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 269 259 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |
| Mean speed of sample ${ }^{3}, \mathrm{~S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(\mathrm{v} / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ (Exhibit 15-15) <br> $1.3 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}, \mathrm{BFFS}$ $55.0 \mathrm{mi} / \mathrm{h}$ <br> Adj. for lane and shoulder width, ${ }^{4} \mathrm{f}_{\mathrm{LS}}($ Exhibit 15-7) $2.6 \mathrm{mi} / \mathrm{h}$ <br> Adj. for access points ${ }^{4}, \mathrm{f}_{\mathrm{A}}$ (Exhibit $\left.15-8\right)$ $0.5 \mathrm{mi} / \mathrm{h}$ <br> Free-flow speed, FFS $\left(\mathrm{FSS}=\mathrm{BFFS}-\mathrm{f}_{\mathrm{LS}} \mathrm{ff}_{\mathrm{A}}\right)$ $51.9 \mathrm{mi} / \mathrm{h}$ <br> Average travel speed, ATS $\mathrm{d}_{\mathrm{d}}=\mathrm{FFS}-0.00776\left(\mathrm{v}_{\mathrm{d}, \mathrm{ATS}}{ }^{+}\right.$ $46.5 \mathrm{mi} / \mathrm{h}$ <br> $\left.\mathrm{v}_{\mathrm{o}, \mathrm{ATS}}\right)-\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ $89.7 \%$ <br> Percent free flow speed, PFFS 8.7 |
| Percent Time-Spent-Following |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.1 1.1 |
| Passenger-car equivalents for $\mathrm{RVs}, \mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 0.993 0.993 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{~F}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 264 254 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{d}(\%)=100\left(1-e^{\text {av }}{ }_{d}{ }^{\text {b }}\right.$ ) | 28.7 |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \mathrm{PTSF}}$ (Exhibit 15-21) | 31.0 |
| Percent time-spent-following, $\operatorname{PTSF}_{d}(\%)=$ BPTSF $_{d}+{ }_{n p, \mathrm{PTSF}}{ }^{*}\left(v_{d, \mathrm{PTSF}} / v_{d, \mathrm{PTSF}}{ }^{+}\right.$ $\mathrm{V}_{\mathrm{o}, \mathrm{PTSF}}$ ) | 44.5 |
| Level of Service and Other Performance Measures |  |
| Level of service, LOS (Exhibit 15-3) | C |
| Volume to capacity ratio, v/c | 0.16 |









| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |
| :---: | :---: |
| General Information | Site Information |
| Analyst $J F$ <br> Agency or Company $4 / 13 / 2018$ <br> Date Performed An <br> Analysis Time Period $A M$ | Highway / Direction of Travel SR 113 <br> Fouth of Midway Rd NB  <br> From/To  <br> Jurisiction Caltrans <br> Analysis Year Cumulative |
| Project Description: Recology Hay Rd Landfill |  |
| Input Data |  |
|  |  |
| Average Travel Speed |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.4 1.3 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 0.973 0.979 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{ATS}}$ (Exhibit 15-9) | 1.00 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 263 366 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |
| Mean speed of sample ${ }^{3}, \mathrm{~S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(\mathrm{v} / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ (Exhibit 15-15) <br> $1.1 \mathrm{mi} / \mathrm{h}$ |  |
| Percent Time-Spent-Following |  |
|  | Analysis Direction (d) ${ }^{\text {d }}$ (\|l| Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.1 1.1 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 0.993 0.993 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}\right.$ g,PTSF $)$ | 257 \| 361 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{\text {d }}(\%)=100\left(1-\mathrm{e}^{\text {av }}{ }_{\mathrm{d}}{ }^{\text {b }}\right.$ ) | 29.8 |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \text { PTSF }}$ (Exhibit 15-21) | 27.8 |
| Percent time-spent-following, PTSF $_{d}(\%)=$ BPTSF $_{d}{ }^{+f}{ }_{n p, \text { PTSF }}{ }^{*}\left(v_{d, \text { PTSF }} / v_{d, \text { PTSF }}{ }^{+}\right.$ $\mathrm{v}_{\mathrm{o}, \mathrm{PTSF}}$ ) | 41.4 |
| Level of Service and Other Performance Measures |  |
| Level of service, LOS (Exhibit 15-3) | D |
| Volume to capacity ratio, $\mathrm{V} / \mathrm{c}$ | 0.15 |





| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |
| :---: | :---: |
| General Information | Site Information |
| Analyst $J F$ <br> Agency or Company $4 / 13 / 2018$ <br> Date Performed Analysis Time Period | Highway / Direction of Travel SR 113 <br> Fouth of Midway Rd NB  <br> From/To  <br> Jurisiction Caltrans <br> Analysis Year Cumulative |
| Project Description: Recology Hay Rd Landfill |  |
| Input Data |  |
|  |  |
| Average Travel Speed |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.3 1.3 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 0.979 0.979 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{ATS}}$ (Exhibit 15-9) | 1.00 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 361 372 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |
| Mean speed of sample ${ }^{3}, \mathrm{~S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(\mathrm{v} / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ (Exhibit 15-15) <br> $1.1 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}, \mathrm{BFFS}$ $55.0 \mathrm{mi} / \mathrm{h}$ <br> Adj. for lane and shoulder width, ${ }^{4} \mathrm{f}_{\mathrm{LS}}($ Exhibit $15-7)$ $4.2 \mathrm{mi} / \mathrm{h}$ <br> Adj. for access points ${ }^{4}, \mathrm{f}_{\mathrm{A}}($ Exhibit $15-8)$ $0.5 \mathrm{mi} / \mathrm{h}$ <br> Free-flow speed, FFS $\left(\right.$ FSS $=$ BFFS- $\left.\mathrm{f}_{\mathrm{LS}} \mathrm{f}_{\mathrm{A}}\right)$ $50.3 \mathrm{mi} / \mathrm{h}$ <br> Average travel speed, ATS ${ }_{\mathrm{d}}=$ FFSS- $0.00776\left(\mathrm{v}_{\mathrm{d}, \mathrm{ATS}}{ }^{+}\right.$ $43.5 \mathrm{mi} / \mathrm{h}$ <br> $\left.v_{\mathrm{o}, \mathrm{ATS}}\right)-\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$  <br> Percent free flow speed, PFFS $86.5 \%$  |
| Percent Time-Spent-Following |  |
|  | Analysis Direction (d) ${ }^{\text {d }}$ (\|l| Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.1 1.1 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 0.993 0.993 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}\right.$ g,PTSF $)$ | 356 \||r 367 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{\text {d }}(\%)=100\left(1-\mathrm{e}^{\text {av }}{ }_{\mathrm{d}}{ }^{\text {b }}\right.$ ) | 39.3 |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \text { PTSF }}$ (Exhibit 15-21) | 27.4 |
| Percent time-spent-following, PTSF $_{d}(\%)=$ BPTSF $_{d}{ }^{+f}{ }_{n p, \text { PTSF }}{ }^{*}\left(v_{d, \text { PTSF }} / v_{d, \text { PTSF }}{ }^{+}\right.$ $\mathrm{v}_{\mathrm{o}, \mathrm{PTSF}}$ ) | 52.8 |
| Level of Service and Other Performance Measures |  |
| Level of service, LOS (Exhibit 15-3) | D |
| Volume to capacity ratio, $\mathrm{V} / \mathrm{c}$ | 0.21 |



| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |
| :---: | :---: |
| General Information | Site Information |
| Analyst $J F$ <br> Agency or Company $4 / 13 / 2018$ <br> Date Performed Analysis Time Period | Highway / Direction of Travel SR 113 <br> South of Midway Rd SB  <br> From/To  <br> Jurisiction Caltrans <br> Analysis Year Cumulative |
| Project Description: Recology Hay Rd Landfill |  |
| Input Data |  |
|  |  |
| Average Travel Speed |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.3 1.3 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 0.979 0.979 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{ATS}}$ (Exhibit 15-9) | 1.00 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 372 361 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |
| Mean speed of sample ${ }^{3}, \mathrm{~S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(\mathrm{v} / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ (Exhibit 15-15) <br> $1.1 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}, \mathrm{BFFS}$ $55.0 \mathrm{mi} / \mathrm{h}$ <br> Adj. for lane and shoulder width, ${ }^{4} \mathrm{f}_{\mathrm{LS}}($ Exhibit $15-7)$ $4.2 \mathrm{mi} / \mathrm{h}$ <br> Adj. for access points ${ }^{4}, \mathrm{f}_{\mathrm{A}}($ (Exhibit $15-8)$ $0.5 \mathrm{mi} / \mathrm{h}$ <br> Free-flow speed, FFS $\left(\mathrm{FSS}=\mathrm{BFFS}-\mathrm{f}_{\mathrm{LS}} \mathrm{f}_{\mathrm{A}}\right)$ $50.3 \mathrm{mi} / \mathrm{h}$ <br> Average travel speed, ATS ${ }_{\mathrm{d}}=\mathrm{FFS}-0.00776\left(\mathrm{v}_{\mathrm{d}, \mathrm{ATS}}{ }^{+}\right.$ $43.5 \mathrm{mi} / \mathrm{h}$ <br> $\left.\mathrm{v}_{\mathrm{o}, \mathrm{ATS}}\right)$ <br> Percent free flow speed, PFFS $86.4 \%$ |
| Percent Time-Spent-Following |  |
|  | Analysis Direction (d) ${ }^{\text {d }}$ (\|l| Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.1 1.1 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 0.993 0.993 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}\right.$ g,PTSF $)$ | 367 \||r 356 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{\text {d }}(\%)=100\left(1-\mathrm{e}^{\text {av }}{ }_{\mathrm{d}}{ }^{\text {b }}\right.$ ) | 39.2 |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \text { PTSF }}$ (Exhibit 15-21) | 27.4 |
| Percent time-spent-following, PTSF $_{d}(\%)=$ BPTSF $_{d}{ }^{+f}{ }_{n p, \text { PTSF }}{ }^{*}\left(v_{d, \text { PTSF }} / v_{d, \text { PTSF }}{ }^{+}\right.$ $\mathrm{v}_{\mathrm{o}, \mathrm{PTSF}}$ ) | 53.1 |
| Level of Service and Other Performance Measures |  |
| Level of service, LOS (Exhibit 15-3) | D |
| Volume to capacity ratio, $\mathrm{V} / \mathrm{c}$ | 0.22 |











| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |
| :---: | :---: |
| General Information | Site Information |
| Analyst $J F$ <br> Agency or Company $4 / 13 / 2018$ <br> Date Performed An <br> Analysis Time Period $A M$ | Highway / Direction of Travel SR 113 <br> From/To south of Hay Rd NB <br> Jurisdiction Caltrans <br> Analysis Year Cumulative |
| Project Description: Recology Hay Rd Landfill |  |
| Input Data |  |
|  |  |
| Average Travel Speed |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.2 1.4 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 0.986 0.973 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{ATS}}$ (Exhibit 15-9) | 1.00 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 496 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |
| Mean speed of sample ${ }^{3}, \mathrm{~S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(\mathrm{v} / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ (Exhibit 15-15) <br> $1.2 \mathrm{mi} / \mathrm{h}$ |  |
| Percent Time-Spent-Following |  |
|  | Analysis Direction (d) ${ }^{\text {d }}$ (\|l| Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.0 1.1 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 1.000 0.993 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}\right.$ g,PTSF $)$ | 489 279 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{\text {d }}(\%)=100\left(1-\mathrm{e}^{\text {av }}{ }_{\mathrm{d}}{ }^{\text {b }}\right.$ ) | 46.3 |
| Adj. for no-passing zone, $\mathrm{f}_{\text {np, PTSF }}$ (Exhibit 15-21) | 26.2 |
| Percent time-spent-following, PTSF $_{d}(\%)=$ BPTSF $_{d}{ }^{+f}{ }_{n p, \text { PTSF }}{ }^{*}\left(v_{d, \text { PTSF }} / v_{d, \text { PTSF }}{ }^{+}\right.$ $\mathrm{v}_{\mathrm{o}, \mathrm{PTSF}}$ ) | 63.0 |
| Level of Service and Other Performance Measures |  |
| Level of service, LOS (Exhibit 15-3) | D |
| Volume to capacity ratio, $\mathrm{v} / \mathrm{c}$ | 0.29 |


| Capacity, $\mathrm{C}_{\mathrm{d}, \mathrm{ATS}}$ (Equation 15-12) veh/h | 1654 |
| :---: | :---: |
| Capacity, $\mathrm{C}_{\mathrm{d}, \text { PTSF }}$ (Equation 15-13) veh/h | 1688 |
| Percent Free-Flow Speed PFFS d $^{\text {(Equation 15-11-Class III only) }}$ | 85.6 |
| Bicycle Level of Service |  |
| Directional demand flow rate in outside lane, $v_{\mathrm{OL}}$ (Eq. 15-24) veh/h | 489.1 |
| Effective width, Wv (Eq. 15-29) ft | 12.50 |
| Effective speed factor, $\mathrm{S}_{t}$ (Eq. 15-30) | 4.79 |
| Bicycle level of service score, BLOS (Eq. 15-31) | 6.06 |
| Bicycle level of service (Exhibit 15-4) | $F$ |
| Notes |  |
| 1. Note that the adjustment factor for level terrain is 1.00 ,as level ter downgrade segments are treated as level terrain. <br> 2. If $v_{i}\left(v_{d}\right.$ or $\left.v_{o}\right)>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis--the LOS is $F$. <br> 3. For the analysis direction only and for $v>200$ veh $/ h$. <br> 4. For the analysis direction only <br> 5. Exhibit 15-20 provides coefficients a and b for Equation 15-10. <br> 6. Use alternative Exhibit $15-14$ if some trucks operate at crawl spee | ose ol |




| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |
| :---: | :---: |
| General Information | Site Information |
| Analyst $J F$ <br> Agency or Company $4 / 13 / 2018$ <br> Date Performed Analysis Time Period | Highway / Direction of Travel SR 113 <br> From/To south of Hay Rd NB <br> Jurisdiction Caltrans <br> Analysis Year Cumulative |
| Project Description: Recology Hay Rd Landfill |  |
| Input Data |  |
|  |  |
| Average Travel Speed |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.3 \||r 1.2 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 0.979 0.986 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{ATS}}$ (Exhibit 15-9) | 1.00 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 450 524 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |
| Mean speed of sample ${ }^{3}$, $\mathrm{S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(\mathrm{~V} / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\text {np,ATS }}$ (Exhibit 15-15) <br> $0.8 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}, \mathrm{BFFS}$ $55.0 \mathrm{mi} / \mathrm{h}$ <br> Adj. for lane and shoulder width, ${ }^{4} \mathrm{f}_{\mathrm{LS}}($ Exhibit $15-7)$ $4.2 \mathrm{mi} / \mathrm{h}$ <br> Adj. for access points ${ }^{4}, \mathrm{f}_{\mathrm{A}}($ Exhibit $15-8)$ $0.5 \mathrm{mi} / \mathrm{h}$ <br> Free-flow speed, FFS $\left(\right.$ FSS $=$ BFFS- $\left.\mathrm{f}_{\mathrm{LS}} \mathrm{f}_{\mathrm{A}}\right)$ $50.3 \mathrm{mi} / \mathrm{h}$ <br> Average travel speed, ATS ${ }_{\mathrm{d}}=$ FFSS- $0.00776\left(\mathrm{v}_{\mathrm{d}, \mathrm{ATS}}{ }^{+}\right.$ $41.9 \mathrm{mi} / \mathrm{h}$ <br> $\left.v_{\mathrm{o}, \mathrm{ATS}}\right)-\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$  <br> Percent free flow speed, PFFS $83.4 \%$  |
| Percent Time-Spent-Following |  |
|  | Analysis Direction (d) ${ }^{\text {d }}$ (\|l| Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 1.000 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}\right.$ g,PTSF $)$ | 440 516 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{\text {d }}(\%)=100\left(1-\mathrm{e}^{\text {av }}{ }_{\mathrm{d}}{ }^{\text {b }}\right.$ ) | 47.2 |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \text { PTSF }}$ (Exhibit 15-21) | 27.0 |
| Percent time-spent-following, PTSF $_{d}(\%)=$ BPTSF $_{d}{ }^{+f}{ }_{n p, \text { PTSF }}{ }^{*}\left(v_{d, \text { PTSF }} / v_{d, \text { PTSF }}{ }^{+}\right.$ $\mathrm{v}_{\mathrm{o}, \mathrm{PTSF}}$ ) | 59.6 |
| Level of Service and Other Performance Measures |  |
| Level of service, LOS (Exhibit 15-3) | D |
| Volume to capacity ratio, $\mathrm{V} / \mathrm{c}$ | 0.26 |



| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |
| :---: | :---: |
| General Information | Site Information |
| Analyst $J F$ <br> Agency or Company $4 / 13 / 2018$ <br> Date Performed Analysis Time Period | Highway / Direction of Travel SR 113 <br> south of Hay Rd SB  <br> From/To  <br> Jurisdiction Caltrans <br> Analysis Year Cumulative |
| Project Description: Recology Hay Rd Landfill |  |
| Input Data |  |
|  |  |
| Average Travel Speed |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.2 1.3 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 0.986 0.979 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{ATS}}$ (Exhibit 15-9) | 1.00 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 524 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |
| Mean speed of sample ${ }^{3}, \mathrm{~S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(\mathrm{v} / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ (Exhibit 15-15) <br> $1.0 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}, \mathrm{BFFS}$ $55.0 \mathrm{mi} / \mathrm{h}$ <br> Adj. for lane and shoulder width, ${ }^{4} \mathrm{f}_{\mathrm{LS}}($ Exhibit 15-7) $4.2 \mathrm{mi} / \mathrm{h}$ <br> Adj. for access points ${ }^{4}, \mathrm{f}_{\mathrm{A}}($ Exhibit $15-8)$ $0.5 \mathrm{mi} / \mathrm{h}$ <br> Free-flow speed, FFS (FSS=BFFS-f $\left.\mathrm{f}^{-\mathrm{f}_{\mathrm{A}}}\right)$ $50.3 \mathrm{mi} / \mathrm{h}$ <br> Average travel speed, ATS $\mathrm{d}_{\mathrm{d}}=\mathrm{FFS}-0.00776\left(\mathrm{v}_{\mathrm{d}, \mathrm{ATS}}{ }^{+}\right.$ $41.8 \mathrm{mi} / \mathrm{h}$ <br> $\left.\mathrm{v}_{\mathrm{o}, \mathrm{ATS}}\right)$ - $\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ $83.0 \%$ <br> Percent free flow speed, PFFS 8 |
| Percent Time-Spent-Following |  |
|  | Analysis Direction (d) ${ }^{\text {d }}$ (\|l| Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 1.000 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}\right.$ g,PTSF $)$ | 516 440 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{\text {d }}(\%)=100\left(1-\mathrm{e}^{\text {av }}{ }_{\mathrm{d}}{ }^{\text {b }}\right.$ ) | 51.1 |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \text { PTSF }}$ (Exhibit 15-21) | 27.0 |
| Percent time-spent-following, PTSF $_{d}(\%)=$ BPTSF $_{d}{ }^{+f}{ }_{n p, \text { PTSF }}{ }^{*}\left(v_{d, \text { PTSF }} / v_{d, \text { PTSF }}{ }^{+}\right.$ $\mathrm{v}_{\mathrm{o}, \mathrm{PTSF}}$ ) | 65.7 |
| Level of Service and Other Performance Measures |  |
| Level of service, LOS (Exhibit 15-3) | D |
| Volume to capacity ratio, $\mathrm{v} / \mathrm{c}$ | 0.31 |




| Capacity, $\mathrm{C}_{\mathrm{d}, \mathrm{ATS}}$ (Equation 15-12) veh/h | 1600 |
| :---: | :---: |
| Capacity, $\mathrm{C}_{\mathrm{d}, \text { PTSF }}$ (Equation 15-13) veh/h | 1688 |
| Percent Free-Flow Speed PFFS ${ }_{\text {d }}$ (Equation 15-11-Class III only) | 97.3 |
| Bicycle Level of Service |  |
| Directional demand flow rate in outside lane, $v_{\text {OL }}$ (Eq. 15-24) veh/h | 48.9 |
| Effective width, Wv (Eq. 15-29) ft | 23.08 |
| Effective speed factor, $\mathrm{S}_{t}$ (Eq. 15-30) | 4.79 |
| Bicycle level of service score, BLOS (Eq. 15-31) | 3.01 |
| Bicycle level of service (Exhibit 15-4) | C |
| Notes |  |
| 1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific downgrade segments are treated as level terrain. <br> 2. If $v_{i}\left(v_{d}\right.$ or $\left.v_{o}\right)>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis--the LOS is $F$. <br> 3. For the analysis direction only and for $v>200$ veh $/ \mathrm{h}$. <br> 4. For the analysis direction only <br> 5. Exhibit 15-20 provides coefficients $a$ and $b$ for Equation 15-10. <br> 6. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade. |  |








| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |
| :---: | :---: |
| General Information | Site Information |
| Analyst $J F$ <br> Agency or Company  <br> Date Performed $10 / 8 / 18$ <br> Analysis Time Period $A M$ | Highway / Direction of Travel Midway Rd <br> From/To west of Porter Rd EB <br> Jurisdiction Solano County <br> Analysis Year Cumulative + Project |
| Project Description: Recology Hay Rd Landfill |  |
| Input Data |  |
|  |  |
| Average Travel Speed |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.4 1.3 |
| Passenger-car equivalents for RVs , $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 0.973 0.979 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \text { ATS }}$ (Exhibit 15-9) | 1.00 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 292441 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |
| Mean speed of sample ${ }^{3}$, $\mathrm{S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776(\mathrm{~V} / \mathrm{f} \mathrm{HV}, \mathrm{ATS}$ ) <br> Adj. for no-passing zones, $\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ (Exhibit 15-15) <br> $1.1 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}, \mathrm{BFFS}$ $55.0 \mathrm{mi} / \mathrm{h}$ <br> Adj. for lane and shoulder width, ${ }^{4} \mathrm{f}_{\mathrm{LS}}($ Exhibit 15-7) $2.6 \mathrm{mi} / \mathrm{h}$ <br> Adj. for access points ${ }^{4}, \mathrm{f}_{\mathrm{A}}$ (Exhibit 15-8) $0.3 \mathrm{mi} / \mathrm{h}$ <br> Free-flow speed, FFS (FSS=BFFS-f $\left.\mathrm{LS}^{-\mathrm{f}_{\mathrm{A}}}\right)$ $52.2 \mathrm{mi} / \mathrm{h}$ <br> Average travel speed, ATS $=\mathrm{FFS}-0.00776\left(\mathrm{v}_{\mathrm{d}, \mathrm{ATS}}{ }^{+}\right.$ $45.3 \mathrm{mi} / \mathrm{h}$ <br> $\left.\mathrm{v}_{\mathrm{o}, \mathrm{ATS}}\right)-\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ <br> Percent free flow speed, PFFS $86.9 \%$ |
| Percent Time-Spent-Following |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.1 1.0 |
| Passenger-car equivalents for RVs , $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 0.993 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{\star} \mathrm{f}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 286 |
| Base percent time-spent-following ${ }^{4}$, PPTSF $_{\text {d }}(\%)=100\left(1-\mathrm{e}^{\text {av }}{ }_{\mathrm{d}}{ }^{\text {b }}\right.$ ) | 34.6 |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \mathrm{PTSF}}$ (Exhibit 15-21) | 32.2 |
| $\qquad$ | 47.4 |
| Level of Service and Other Performance Measures |  |
| Level of service, LOS (Exhibit 15-3) | C |
| Volume to capacity ratio, v/c | 0.17 |



| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |
| :---: | :---: |
| General Information | Site Information |
| Analyst $J F$ <br> Agency or Company $10 / 8 / 18$ <br> Date Performed AM <br> Analysis Time Period  | Highway / Direction of Travel Midway Rd <br> From/To west of Porter Rd WB <br> Jurisdiction Solano County <br> Analysis Year Cumulative plus Project |
| Project Description: Recology Hay Rd Landfill |  |
| Input Data |  |
|  |  |
| Average Travel Speed |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.3 1.4 |
| Passenger-car equivalents for RV s, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 0.979 0.973 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \text { ATS }}$ (Exhibit 15-9) | 1.00 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 441 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |
| Mean speed of sample ${ }^{3}$, $\mathrm{S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(\mathrm{v} / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ (Exhibit 15-15) <br> $1.3 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}, \mathrm{BFFS}$ $55.0 \mathrm{mi} / \mathrm{h}$ <br> Adj. for lane and shoulder width, ${ }^{4} \mathrm{f}_{\mathrm{LS}}($ Exhibit 15-7) $2.6 \mathrm{mi} / \mathrm{h}$ <br> Adj. for access points ${ }^{4}, \mathrm{f}_{\mathrm{A}}$ (Exhibit 15-8) $0.3 \mathrm{mi} / \mathrm{h}$ <br> Free-flow speed, FFS (FSS=BFFS-f $\left.\mathrm{LS}^{-\mathrm{f}_{\mathrm{A}}}\right)$ $52.2 \mathrm{mi} / \mathrm{h}$ <br> Average travel speed, ATS $=\mathrm{FFS}-0.00776\left(\mathrm{v}_{\mathrm{d}, \mathrm{ATS}}{ }^{+}\right.$ $45.1 \mathrm{mi} / \mathrm{h}$ <br> $\left.\mathrm{v}_{\mathrm{o}, \mathrm{ATS}}\right)-\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ <br> Percent free flow speed, PFFS $86.5 \%$ |
| Percent Time-Spent-Following |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.0 1.1 |
| Passenger-car equivalents for RV s, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 1.000 0.993 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 432 286 |
| Base percent time-spent-following ${ }^{4}$, PPTSF $_{\text {d }}(\%)=100\left(1-\mathrm{e}^{\text {av }}{ }_{\mathrm{d}}{ }^{\text {b }}\right.$ ) | 42.0 |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \text { PTSF }}$ (Exhibit 15-21) | 32.2 |
| Percent time-spent-following, PTSF $_{d}(\%)=$ BPTSF $_{d}+f_{n p, \text { PTSF }}{ }^{*}\left(v_{d, \text { PTSF }} / v_{d, \text { PTSF }}+\right.$ $\mathrm{v}_{\mathrm{o}, \mathrm{PTSF}}$ ) | 61.4 |
| Level of Service and Other Performance Measures |  |
| Level of service, LOS (Exhibit 15-3) | C |
| Volume to capacity ratio, v/c | 0.26 |



| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |
| :---: | :---: |
| General Information | Site Information |
| Analyst $J F$ <br> Agency or Company $10 / 8 / 18$ <br> Date Performed $P M$ <br> Analysis Time Period  | Highway / Direction of Travel Midway Rd <br> From/To west of Porter Rd EB <br> Jurisdiction Solano County <br> Analysis Year Cumulative plus Project |
| Project Description: Recology Hay Rd Landfill |  |
| Input Data |  |
|  |  |
| Average Travel Speed |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.1 1.2 |
| Passenger-car equivalents for RV s, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 0.993 0.986 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \text { ATS }}$ (Exhibit 15-9) | 1.00 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 635 460 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |
| Mean speed of sample ${ }^{3}$, $\mathrm{S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(\mathrm{v} / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ (Exhibit 15-15) <br> $1.1 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}, \mathrm{BFFS}$ $55.0 \mathrm{mi} / \mathrm{h}$ <br> Adj. for lane and shoulder width, ${ }^{4} \mathrm{f}_{\mathrm{LS}}($ Exhibit 15-7) $2.6 \mathrm{mi} / \mathrm{h}$ <br> Adj. for access points ${ }^{4}, \mathrm{f}_{\mathrm{A}}$ (Exhibit 15-8) $0.3 \mathrm{mi} / \mathrm{h}$ <br> Free-flow speed, FFS $\left(\mathrm{FSS}=\mathrm{BFFS}-\mathrm{f}_{\mathrm{LS}} \mathrm{f}_{\mathrm{A}}\right)$ $52.2 \mathrm{mi} / \mathrm{h}$ <br> Average travel speed, ATS $\mathrm{d}_{\mathrm{d}}=\mathrm{FFS}-0.00776\left(\mathrm{v}_{\mathrm{d}, \mathrm{ATS}}{ }^{+}\right.$ $42.6 \mathrm{mi} / \mathrm{h}$ <br> $\left.\mathrm{v}_{\mathrm{o}, \mathrm{ATS}}\right)-\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ $81.6 \%$ <br> Percent free flow speed, PFFS 8 |
| Percent Time-Spent-Following |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Passenger-car equivalents for RV s, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 1.000 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 630 453 |
| Base percent time-spent-following ${ }^{4}$, PPTSF $_{\text {d }}(\%)=100\left(1-\mathrm{e}^{\text {av }}{ }_{\mathrm{d}}{ }^{\text {b }}\right.$ ) | 58.4 |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \mathrm{PTSF}}$ (Exhibit 15-21) | 24.9 |
| Percent time-spent-following, PTSF $_{d}(\%)=$ BPTSF $_{d}+f_{n p, \text { PTSF }}{ }^{*}\left(v_{d, \text { PTSF }} / v_{d, \text { PTSF }}+\right.$ $\mathrm{V}_{\mathrm{o}, \mathrm{PTSF}}$ ) | 72.9 |
| Level of Service and Other Performance Measures |  |
| Level of service, LOS (Exhibit 15-3) | D |
| Volume to capacity ratio, v/c | 0.37 |



| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |
| :---: | :---: |
| General Information | Site Information |
| Analyst $J F$ <br> Agency or Company $10 / 8 / 18$ <br> Date Performed $P M$ <br> Analysis Time Period  | Highway / Direction of Travel Midway Rd <br> From/To west of Porter Rd WB <br> Jurisdiction Solano County <br> Analysis Year Cumulative plus Project |
| Project Description: Recology Hay Rd Landfill |  |
| Input Data |  |
|  |  |
| Average Travel Speed |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.2 1.1 |
| Passenger-car equivalents for RV s, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 0.986 0.993 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \text { ATS }}$ (Exhibit 15-9) | 1.00 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 460 635 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |
| Mean speed of sample ${ }^{3}$, $\mathrm{S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(\mathrm{v} / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ (Exhibit 15-15) <br> $0.7 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}, \mathrm{BFFS}$ $55.0 \mathrm{mi} / \mathrm{h}$ <br> Adj. for lane and shoulder width, ${ }^{4} \mathrm{f}_{\mathrm{LS}}($ Exhibit 15-7) $2.6 \mathrm{mi} / \mathrm{h}$ <br> Adj. for access points ${ }^{4}, \mathrm{f}_{\mathrm{A}}$ (Exhibit 15-8) $0.3 \mathrm{mi} / \mathrm{h}$ <br> Free-flow speed, FFS (FSS=BFFS-f $\left.\mathrm{LS}^{-\mathrm{f}_{\mathrm{A}}}\right)$ $52.2 \mathrm{mi} / \mathrm{h}$ <br> Average travel speed, ATS $=\mathrm{FFS}-0.00776\left(\mathrm{v}_{\mathrm{d}, \mathrm{ATS}}{ }^{+}\right.$ $42.9 \mathrm{mi} / \mathrm{h}$ <br> $\left.\mathrm{v}_{\mathrm{o}, \mathrm{ATS}}\right)-\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ <br> Percent free flow speed, PFFS $82.4 \%$ |
| Percent Time-Spent-Following |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Passenger-car equivalents for RV s, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 1.000 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 453 年 630 |
| Base percent time-spent-following ${ }^{4}$, PPTSF $_{\text {d }}(\%)=100\left(1-\mathrm{e}^{\text {av }}{ }_{\mathrm{d}}{ }^{\text {b }}\right.$ ) | 49.8 |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \text { PTSF }}$ (Exhibit 15-21) | 24.9 |
| $\begin{aligned} & \text { Percent time-spent-following, } \text { PTSF }_{d}(\%)=\text { BPTSF }_{d}+f_{n p, P T S F}{ }^{*}\left(v_{d, \text { PTSF }} / v_{d, \text { PTSF }}+\right. \\ & \left.v_{o, P T S F}\right) \end{aligned}$ | 60.2 |
| Level of Service and Other Performance Measures |  |
| Level of service, LOS (Exhibit 15-3) | D |
| Volume to capacity ratio, v/c | 0.27 |



| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |
| :---: | :---: |
| General Information | Site Information |
| Analyst $J F$ <br> Agency or Company  <br> Date Performed $10 / 8 / 18$ <br> Analysis Time Period $A M$ | Highway / Direction of Travel Midway Rd <br> From/To west of SR 113 EB <br> Jurisdiction Solano County <br> Analysis Year Cumulative plus Project |
| Project Description: Recology Hay Rd Landfill |  |
| Input Data |  |
|  |  |
| Average Travel Speed |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.4 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 0.973 0.973 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \text { ATS }}$ (Exhibit 15-9) | 1.00 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 269 259 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |
| Mean speed of sample ${ }^{3}, \mathrm{~S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(\mathrm{v} / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ (Exhibit 15-15) <br> $1.3 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}, \mathrm{BFFS}$ $55.0 \mathrm{mi} / \mathrm{h}$ <br> Adj. for lane and shoulder width, ${ }^{4} \mathrm{f}_{\mathrm{LS}}($ Exhibit 15-7) $2.6 \mathrm{mi} / \mathrm{h}$ <br> Adj. for access points ${ }^{4}, \mathrm{f}_{\mathrm{A}}$ (Exhibit $\left.15-8\right)$ $0.5 \mathrm{mi} / \mathrm{h}$ <br> Free-flow speed, FFS $\left(\mathrm{FSS}=\mathrm{BFFS}-\mathrm{f}_{\mathrm{LS}} \mathrm{ff}_{\mathrm{A}}\right)$ $51.9 \mathrm{mi} / \mathrm{h}$ <br> Average travel speed, ATS $\mathrm{d}_{\mathrm{d}}=\mathrm{FFS}-0.00776\left(\mathrm{v}_{\mathrm{d}, \mathrm{ATS}}{ }^{+}\right.$ $46.5 \mathrm{mi} / \mathrm{h}$ <br> $\left.\mathrm{v}_{\mathrm{o}, \mathrm{ATS}}\right)-\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ $89.7 \%$ <br> Percent free flow speed, PFFS 8.7 |
| Percent Time-Spent-Following |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.1 1.1 |
| Passenger-car equivalents for $\mathrm{RVs}, \mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 0.993 0.993 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{~F}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 264 254 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{d}(\%)=100\left(1-e^{\text {av }}{ }_{d}{ }^{\text {b }}\right.$ ) | 28.7 |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \mathrm{PTSF}}$ (Exhibit 15-21) | 31.0 |
| Percent time-spent-following, $\operatorname{PTSF}_{d}(\%)=$ BPTSF $_{d}+{ }_{n p, \mathrm{PTSF}}{ }^{*}\left(v_{d, \mathrm{PTSF}} / v_{d, \mathrm{PTSF}}{ }^{+}\right.$ $\mathrm{V}_{\mathrm{o}, \mathrm{PTSF}}$ ) | 44.5 |
| Level of Service and Other Performance Measures |  |
| Level of service, LOS (Exhibit 15-3) | C |
| Volume to capacity ratio, v/c | 0.16 |



| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |
| :---: | :---: |
| General Information | Site Information |
| Analyst $J F$ <br> Agency or Company  <br> Date Performed $10 / 8 / 18$ <br> Analysis Time Period $A M$ | Highway / Direction of Travel Midway Rd <br> From/To west of SR 113 WB <br> Jurisdiction Solano County <br> Analysis Year Cumulative plus Project |
| Project Description: Recology Hay Rd Landfill |  |
| Input Data |  |
|  |  |
| Average Travel Speed |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.4 1.4 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 0.973 0.973 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \text { ATS }}($ Exhibit 15-9) | 1.00 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 259 269 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |
| Mean speed of sample ${ }^{3}$, $\mathrm{S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(\mathrm{~V} / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ (Exhibit 15-15) <br> $1.3 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}, \mathrm{BFFS}$ $55.0 \mathrm{mi} / \mathrm{h}$ <br> Adj. for lane and shoulder width, ${ }^{4} \mathrm{f}_{\mathrm{LS}}($ Exhibit 15-7) $2.6 \mathrm{mi} / \mathrm{h}$ <br> Adj. for access points ${ }^{4}, \mathrm{f}_{\mathrm{A}}$ (Exhibit 15-8) $0.5 \mathrm{mi} / \mathrm{h}$ <br> Free-flow speed, FFS $\left(\mathrm{FSS}=\mathrm{BFFS}-\mathrm{f}_{\mathrm{LS}} \mathrm{f}_{\mathrm{A}}\right)$ $51.9 \mathrm{mi} / \mathrm{h}$ <br> Average travel speed, ATS $\mathrm{d}_{\mathrm{d}}=\mathrm{FFS}-0.00776\left(\mathrm{v}_{\mathrm{d}, \mathrm{ATS}}{ }^{+}\right.$ $46.5 \mathrm{mi} / \mathrm{h}$ <br> $\left.\mathrm{v}_{\mathrm{o}, \mathrm{ATS}}\right)-\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ $89.7 \mathrm{\%}$ <br> Percent free flow speed, PFFS 8 |
| Percent Time-Spent-Following |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.1 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 0.993 0.993 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 254 264 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{\text {d }}(\%)=100\left(1-\mathrm{e}^{\text {av }}{ }_{\mathrm{d}}{ }^{\text {b }}\right.$ ) | 28.8 |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \mathrm{PTSF}}$ (Exhibit 15-21) | 31.0 |
| $\qquad$ | 44.0 |
| Level of Service and Other Performance Measures |  |
| Level of service, LOS (Exhibit 15-3) | C |
| Volume to capacity ratio, v/c | 0.15 |



| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |
| :---: | :---: |
| General Information | Site Information |
| Analyst $J F$ <br> Agency or Company  <br> Date Performed $10 / 8 / 18$ <br> Analysis Time Period PM | Highway / Direction of Travel Midway Rd <br> From/To west of SR 113 EB <br> Jurisdiction Solano County <br> Analysis Year Cumulative plus Project |
| Project Description: Recology Hay Rd Landfill |  |
| Input Data |  |
|  |  |
| Average Travel Speed |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.5 1.5 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 0.966 0.966 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \text { ATS }}$ (Exhibit 15-9) | 1.00 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 197 239 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |
| Mean speed of sample ${ }^{3}, \mathrm{~S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(\mathrm{v} / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ (Exhibit 15-15) <br> $1.3 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}, \mathrm{BFFS}$ $55.0 \mathrm{mi} / \mathrm{h}$ <br> Adj. for lane and shoulder width, ${ }^{4} \mathrm{f}_{\mathrm{LS}}($ Exhibit 15-7) $2.6 \mathrm{mi} / \mathrm{h}$ <br> Adj. for access points ${ }^{4}, \mathrm{f}_{\mathrm{A}}$ (Exhibit $\left.15-8\right)$ $0.5 \mathrm{mi} / \mathrm{h}$ <br> Free-flow speed, FFS $\left(\mathrm{FSS}=\mathrm{BFFS}-\mathrm{f}_{\mathrm{LS}} \mathrm{f}_{\mathrm{A}}\right)$ $51.9 \mathrm{mi} / \mathrm{h}$ <br> Average travel speed, ATS $\mathrm{d}_{\mathrm{d}}=\mathrm{FFS}-0.00776\left(\mathrm{v}_{\mathrm{d}, \mathrm{ATS}}{ }^{+}\right.$ $47.2 \mathrm{mi} / \mathrm{h}$ <br> $\left.\mathrm{v}_{\mathrm{o}, \mathrm{ATS}}\right)-\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ $91.0 \%$ <br> Percent free flow speed, PFFS 9.0 |
| Percent Time-Spent-Following |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.1 1.1 |
| Passenger-car equivalents for $\mathrm{RVs}, \mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 0.993 0.993 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{~F}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 192 232 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{d}(\%)=100\left(1-e^{\text {av }}{ }_{d}{ }^{\text {b }}\right.$ ) | 21.3 |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \mathrm{PTSF}}$ (Exhibit 15-21) | 30.4 |
| Percent time-spent-following, PTSF $_{d}(\%)=$ BPTSF $_{d}+{ }_{n p, \mathrm{PTSF}}{ }^{*}\left(v_{d, \mathrm{PTSF}} / \mathrm{v}_{d, \mathrm{PTSF}}{ }^{+}\right.$ $\mathrm{V}_{\mathrm{o}, \mathrm{PTSF}}$ ) | 35.1 |
| Level of Service and Other Performance Measures |  |
| Level of service, LOS (Exhibit 15-3) | C |
| Volume to capacity ratio, v/c | 0.12 |



| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |
| :---: | :---: |
| General Information | Site Information |
| Analyst $J F$ <br> Agency or Company  <br> Date Performed $10 / 8 / 18$ <br> Analysis Time Period PM | Highway / Direction of Travel Midway Rd <br> From/To west of SR 113 WB <br> Jurisdiction Solano County <br> Analysis Year Cumulative plus Project |
| Project Description: Recology Hay Rd Landfill |  |
| Input Data |  |
|  |  |
| Average Travel Speed |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.5 1.5 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 0.966 0.966 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \text { ATS }}$ (Exhibit 15-9) | 1.00 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 239 197 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |
| Mean speed of sample ${ }^{3}, \mathrm{~S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(\mathrm{v} / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ (Exhibit 15-15) <br> $1.3 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}, \mathrm{BFFS}$ $55.0 \mathrm{mi} / \mathrm{h}$ <br> Adj. for lane and shoulder width, ${ }^{4} \mathrm{f}_{\mathrm{LS}}($ Exhibit 15-7) $2.6 \mathrm{mi} / \mathrm{h}$ <br> Adj. for access points ${ }^{4}, \mathrm{f}_{\mathrm{A}}$ (Exhibit $\left.15-8\right)$ $0.5 \mathrm{mi} / \mathrm{h}$ <br> Free-flow speed, FFS $\left(\mathrm{FSS}=\mathrm{BFFS}-\mathrm{f}_{\mathrm{LS}} \mathrm{f}_{\mathrm{A}}\right)$ $51.9 \mathrm{mi} / \mathrm{h}$ <br> Average travel speed, ATS $\mathrm{d}_{\mathrm{d}}=\mathrm{FFS}-0.00776\left(\mathrm{v}_{\mathrm{d}, \mathrm{ATS}}{ }^{+}\right.$ $47.2 \mathrm{mi} / \mathrm{h}$ <br> $\left.\mathrm{v}_{\mathrm{o}, \mathrm{ATS}}\right)-\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ $91.0 \%$ <br> Percent free flow speed, PFFS 9.0 |
| Percent Time-Spent-Following |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.1 1.1 |
| Passenger-car equivalents for $\mathrm{RVs}, \mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 0.993 0.993 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{~F}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 232 192 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{d}(\%)=100\left(1-e^{\text {av }}{ }_{d}{ }^{\text {b }}\right.$ ) | 24.5 |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \mathrm{PTSF}}$ (Exhibit 15-21) | 30.4 |
| Percent time-spent-following, PTSF $_{d}(\%)=$ BPTSF $_{d}+{ }_{n p, \mathrm{PTSF}}{ }^{*}\left(v_{d, \mathrm{PTSF}} / \mathrm{v}_{d, \mathrm{PTSF}}{ }^{+}\right.$ $\mathrm{V}_{\mathrm{o}, \mathrm{PTSF}}$ ) | 41.1 |
| Level of Service and Other Performance Measures |  |
| Level of service, LOS (Exhibit 15-3) | C |
| Volume to capacity ratio, v/c | 0.14 |



| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |
| :---: | :---: |
| General Information | Site Information |
| Analyst $J F$ <br> Agency or Company  <br> Date Performed $10 / 8 / 18$ <br> Analysis Time Period AM | Highway / Direction of Travel SR 113 <br> From/To south of Midway Rd NB <br> Jurisdiction Caltrans <br> Analysis Year Cumulative plus Project |
| Project Description: Recology Hay Rd Landfill |  |
| Input Data |  |
|  |  |
| Average Travel Speed |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.4 1.3 |
| Passenger-car equivalents for RVs , $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 0.973 0.979 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \text { ATS }}$ (Exhibit 15-9) | 1.00 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 277 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |
| Mean speed of sample ${ }^{3}, \mathrm{~S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(\mathrm{~V} / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ (Exhibit 15-15) <br> $1.1 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}, \mathrm{BFFS}$ $55.0 \mathrm{mi} / \mathrm{h}$ <br> Adj. for lane and shoulder width, ${ }^{4} \mathrm{f}_{\mathrm{LS}}($ (Exhibit 15-7) $4.2 \mathrm{mi} / \mathrm{h}$ <br> Adj. for access points ${ }^{4}, \mathrm{f}_{\mathrm{A}}$ (Exhibit $\left.15-8\right)$ $0.5 \mathrm{mi} / \mathrm{h}$ <br> Free-flow speed, FFS $\left(\mathrm{FSS}=\mathrm{BFFS}-\mathrm{f}_{\mathrm{LS}^{-}} \mathrm{f}_{\mathrm{A}}\right)$ $50.3 \mathrm{mi} / \mathrm{h}$ <br> Average travel speed, ATS $\mathrm{d}_{\mathrm{d}}=\mathrm{FFS}-0.00776\left(\mathrm{v}_{\mathrm{d}, \mathrm{ATS}}{ }^{+}\right.$ $44.0 \mathrm{mi} / \mathrm{h}$ <br> $\left.\mathrm{v}_{\mathrm{o}, \mathrm{ATS}}\right)-\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ $87.5 \%$ <br> Percent free flow speed, PFFS   |
| Percent Time-Spent-Following |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.1 1.1 |
| Passenger-car equivalents for RVs , $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 0.993 0.993 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{\star} \mathrm{f}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 271 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{d}(\%)=100\left(1-e^{\text {av }}{ }_{d}{ }^{\text {b }}\right.$ ) | 31.6 |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \mathrm{PTSF}}$ (Exhibit 15-21) | 26.9 |
| Percent time-spent-following, $\operatorname{PTSF}_{d}(\%)=$ BPTSF $_{d}+{ }_{n p, \mathrm{PTSF}}{ }^{*}\left(v_{d, \mathrm{PTSF}} / \mathrm{v}_{d, \mathrm{PTSF}}{ }^{+}\right.$ <br> $\mathrm{V}_{\mathrm{o}, \mathrm{PTSF}}$ ) | 42.8 |
| Level of Service and Other Performance Measures |  |
| Level of service, LOS (Exhibit 15-3) | D |
| Volume to capacity ratio, $\mathrm{v} / \mathrm{c}$ | 0.16 |



| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |  |
| :---: | :---: | :---: |
| General Information | Site Information |  |
| Analyst $J F$ <br> Agency or Company $1018 / 18$ <br> Date Performed AM <br> Analysis Time Period  <br> Pre  | Highway / Direction of Travel SR 113 <br> From/To south of Midway Rd SB <br> Jurisdiction Caltrans <br> Analysis Year Cumulative plus Project |  |
| Project Description: Recology Hay Rd Landfill |  |  |
| Input Data |  |  |
|  |  |  |
| Average Travel Speed |  |  |
|  | Analysis Direction (d) | Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.3 | 1.4 |
| Passenger-car equivalents for $\mathrm{RVs}, \mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 | 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 0.979 | 0.973 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \text { ATS }}$ (Exhibit 15-9) | 1.00 | 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 386 | 277 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |  |
| Mean speed of sample ${ }^{3}, \mathrm{~S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(\mathrm{v} / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ (Exhibit 15-15) <br> $1.2 \mathrm{mi} / \mathrm{h}$ |  |  |
| Percent Time-Spent-Following |  |  |
|  | Analysis Direction (d) | Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.1 | 1.1 |
| Passenger-car equivalents for $\mathrm{RVs}, \mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 | 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 0.993 | 0.993 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \text { PTSF }}$ (Exhibit 15-16 or Ex 15-17) | 1.00 | 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{\star} \mathrm{f}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 381 | 271 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{\mathrm{d}}(\%)=100\left(1-\mathrm{e}^{\mathrm{av}_{\mathrm{d}}{ }^{\text {b }} \text { ) }}\right.$ | 39.1 |  |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \text { PTSF }}$ (Exhibit 15-21) | 26.9 |  |
| Percent time-spent-following, PTSF $_{d}(\%)=$ BPTSF $_{d}+{ }_{n p, P T S F}{ }^{*}\left(v_{d, \text { PTSF }} / v_{d, \text { PTSF }}+\right.$ $\mathrm{V}_{\mathrm{o}, \mathrm{PTSF}}$ ) | 54.8 |  |
| Level of Service and Other Performance Measures |  |  |
| Level of service, LOS (Exhibit 15-3) | D |  |
| Volume to capacity ratio, $v / c$ | 0.23 |  |



| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |
| :---: | :---: |
| General Information | Site Information |
| Analyst $J F$ <br> Agency or Company  <br> Date Performed $10 / 8 / 18$ <br> Analysis Time Period PM | Highway / Direction of Travel SR 113 <br> From/To south of Midway Rd NB <br> Jurisdiction Caltrans <br> Analysis Year Cumulative plus Project |
| Project Description: Recology Hay Rd Landfill |  |
| Input Data |  |
|  |  |
| Average Travel Speed |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.3 1.3 |
| Passenger-car equivalents for RVs , $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 0.979 0.979 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \text { ATS }}$ (Exhibit 15-9) | 1.00 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 376 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |
| Mean speed of sample ${ }^{3}, \mathrm{~S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(\mathrm{~V} / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ (Exhibit 15-15) <br> $1.1 \mathrm{mi} / \mathrm{h}$ |  |
| Percent Time-Spent-Following |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.1 1.1 |
| Passenger-car equivalents for RVs , $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 0.993 0.993 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{\star} \mathrm{f}_{\mathrm{HV}, \mathrm{PTSF}^{*}} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 371 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{d}(\%)=100\left(1-e^{\text {av }}{ }_{d}{ }^{\text {b }}\right.$ ) | 40.4 |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \mathrm{PTSF}}$ (Exhibit 15-21) | 27.3 |
| Percent time-spent-following, $\operatorname{PTSF}_{d}(\%)=$ BPTSF $_{d}+{ }_{n p, \mathrm{PTSF}}{ }^{*}\left(v_{d, \mathrm{PTSF}} / \mathrm{v}_{d, \mathrm{PTSF}}{ }^{+}\right.$ <br> $\mathrm{V}_{\mathrm{o}, \mathrm{PTSF}}$ ) | 54.1 |
| Level of Service and Other Performance Measures |  |
| Level of service, LOS (Exhibit 15-3) | D |
| Volume to capacity ratio, v/c | 0.22 |



| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |
| :---: | :---: |
| General Information | Site Information |
| Analyst JF <br> Agency or Company  <br> Date Performed $10 / 8 / 18$ <br> Analysis Time Period $P M$ | Highway / Direction of Travel SR 113 <br> From/To south of Midway Rd SB <br> Jurisdiction Caltrans <br> Analysis Year Cumulative plus Project |
| Project Description: Recology Hay Rd Landfill |  |
| Input Data |  |
|  |  |
| Average Travel Speed |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.3 1.3 |
| Passenger-car equivalents for RV s, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 0.979 0.979 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{ATS}}$ (Exhibit 15-9) | 1.00 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 373 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |
| Mean speed of sample ${ }^{3}$, $\mathrm{S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(\mathrm{~V} / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ (Exhibit 15-15) <br> $1.1 \mathrm{mi} / \mathrm{h}$ |  |
| Percent Time-Spent-Following |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.1 1.1 |
| Passenger-car equivalents for RV , $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 0.993 0.993 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{\star} \mathrm{f}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 368 371 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{d}(\%)=100\left(1-e^{\text {av }}{ }_{d}{ }^{\text {b }}\right.$ ) | 40.0 |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \mathrm{PTSF}}$ (Exhibit 15-21) | 27.3 |
| Percent time-spent-following, PTSF $_{d}(\%)=$ BPTSF $_{d}+{ }_{n p, \mathrm{PTSF}}{ }^{*}\left(v_{d, \mathrm{PTSF}} / v_{d, \mathrm{PTSF}}+\right.$ $\mathrm{v}_{\mathrm{o}, \mathrm{PTSF}}$ ) | 53.6 |
| Level of Service and Other Performance Measures |  |
| Level of service, LOS (Exhibit 15-3) | D |
| Volume to capacity ratio, $\mathrm{v} / \mathrm{c}$ | 0.22 |



| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |
| :---: | :---: |
| General Information | Site Information |
| Analyst $J F$ <br> Agency or Company $10 / 8 / 18$ <br> Date Performed AM <br> Analysis Time Period  | Highway / Direction of Travel SR 113 <br> From/To north of Hay Rd NB <br> Jurisdiction Caltrans <br> Analysis Year Cumulative plus Project |
| Project Description: Recology Hay Rd Landfill |  |
| Input Data |  |
|  |  |
| Average Travel Speed |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.2 1.4 |
| Passenger-car equivalents for RV s, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 0.986 0.973 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \text { ATS }}$ (Exhibit 15-9) | 1.00 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 505 338 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |
| Mean speed of sample ${ }^{3}$, $\mathrm{S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(\mathrm{v} / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ (Exhibit 15-15) <br> $1.1 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}, \mathrm{BFFS}$ $55.0 \mathrm{mi} / \mathrm{h}$ <br> Adj. for lane and shoulder width, ${ }^{4} \mathrm{f}_{\mathrm{LS}}($ Exhibit 15-7) $4.2 \mathrm{mi} / \mathrm{h}$ <br> Adj. for access points ${ }^{4}, \mathrm{f}_{\mathrm{A}}$ (Exhibit 15-8) $0.5 \mathrm{mi} / \mathrm{h}$ <br> Free-flow speed, FFS (FSS=BFFS-f $\left.\mathrm{LS}^{-\mathrm{f}_{\mathrm{A}}}\right)$ $50.3 \mathrm{mi} / \mathrm{h}$ <br> Average travel speed, ATS $=\mathrm{FFS}-0.00776\left(\mathrm{v}_{\mathrm{d}, \mathrm{ATS}}{ }^{+}\right.$ $42.6 \mathrm{mi} / \mathrm{h}$ <br> $\left.\mathrm{v}_{\mathrm{o}, \mathrm{ATS}}\right)-\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ <br> Percent free flow speed, PFFS $84.7 \%$ |
| Percent Time-Spent-Following |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.0 1.1 |
| Passenger-car equivalents for RV s, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 1.000 0.993 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 498 332 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{d}(\%)=100\left(1-e^{\text {av }}{ }_{\text {d }}{ }^{\text {b }}\right.$ ) | 47.9 |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \text { PTSF }}$ (Exhibit 15-21) | 22.0 |
| Percent time-spent-following, PTSF $_{d}(\%)=$ BPTSF $_{d}+{ }_{n p, \mathrm{PTSF}}{ }^{*}\left(v_{d, \mathrm{PTSF}} / v_{d, \mathrm{PTSF}}+\right.$ $\mathrm{v}_{\mathrm{o}, \mathrm{PTSF}}$ ) | 61.1 |
| Level of Service and Other Performance Measures |  |
| Level of service, LOS (Exhibit 15-3) | D |
| Volume to capacity ratio, v/c | 0.30 |



| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |
| :---: | :---: |
| General Information | Site Information |
| Analyst $J F$ <br> Agency or Company  <br> Date Performed $10 / 8 / 18$ <br> Analysis Time Period AM | Highway / Direction of Travel SR 113 <br> From/To north of Hay Rd SB <br> Jurisdiction Caltrans <br> Analysis Year Cumulative plus Project |
| Project Description: Recology Hay Rd Landfill |  |
| Input Data |  |
|  |  |
| Average Travel Speed |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.4 1.2 |
| Passenger-car equivalents for RVs , $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 0.973 0.986 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \text { ATS }}$ (Exhibit 15-9) | 1.00 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 338 505 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |
| Mean speed of sample ${ }^{3}, \mathrm{~S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(\mathrm{~V} / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ (Exhibit 15-15) <br> $0.9 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}, \mathrm{BFFS}$ $55.0 \mathrm{mi} / \mathrm{h}$ <br> Adj. for lane and shoulder width, ${ }^{4} \mathrm{f}_{\mathrm{LS}}($ Exhibit 15-7) $4.2 \mathrm{mi} / \mathrm{h}$ <br> Adj. for access points ${ }^{4}, \mathrm{f}_{\mathrm{A}}$ (Exhibit 15-8) $0.5 \mathrm{mi} / \mathrm{h}$ <br> Free-flow speed, FFS $\left(\mathrm{FSS}=\mathrm{BFFS}-\mathrm{f}_{\mathrm{LS}}{ }^{-\mathrm{f}_{\mathrm{A}}}\right)$ $50.3 \mathrm{mi} / \mathrm{h}$ <br> Average travel speed, ATS $\mathrm{d}_{\mathrm{d}}=\mathrm{FFS}-0.00776\left(\mathrm{v}_{\mathrm{d}, \mathrm{ATS}}{ }^{+}\right.$ $42.9 \mathrm{mi} / \mathrm{h}$ <br> $\left.\mathrm{v}_{\mathrm{o}, \mathrm{ATS}}\right)-\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ $85.3 \%$ <br> Percent free flow speed, PFFS  |
| Percent Time-Spent-Following |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.1 1.0 |
| Passenger-car equivalents for RVs , $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 0.993 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{\star} \mathrm{f}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 332 498 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{d}(\%)=100\left(1-e^{\text {av }}{ }_{d}{ }^{\text {b }}\right.$ ) | 38.9 |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \mathrm{PTSF}}$ (Exhibit 15-21) | 22.0 |
| Percent time-spent-following, $\operatorname{PTSF}_{d}(\%)=$ BPTSF $_{d}+{ }_{n p, \mathrm{PTSF}}{ }^{*}\left(v_{d, \mathrm{PTSF}} / \mathrm{v}_{d, \mathrm{PTSF}}{ }^{+}\right.$ <br> $\mathrm{V}_{\mathrm{o}, \mathrm{PTSF}}$ ) | 47.7 |
| Level of Service and Other Performance Measures |  |
| Level of service, LOS (Exhibit 15-3) | D |
| Volume to capacity ratio, $\mathrm{v} / \mathrm{c}$ | 0.20 |



| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |
| :---: | :---: |
| General Information | Site Information |
| Analyst $J F$ <br> Agency or Company $10 / 8 / 18$ <br> Date Performed $P M$ <br> Analysis Time Period  | Highway / Direction of Travel SR 113 <br> From/To north of Hay Rd NB <br> Jurisdiction Caltrans <br> Analysis Year Cumulative plus Project |
| Project Description: Recology Hay Rd Landfill |  |
| Input Data |  |
|  |  |
| Average Travel Speed |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.2 1.2 |
| Passenger-car equivalents for RV s, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 0.986 0.986 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \text { ATS }}$ (Exhibit 15-9) | 1.00 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 523 481 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |
| Mean speed of sample ${ }^{3}$, $\mathrm{S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(\mathrm{v} / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ (Exhibit 15-15) <br> $0.9 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}, \mathrm{BFFS}$ $55.0 \mathrm{mi} / \mathrm{h}$ <br> Adj. for lane and shoulder width, ${ }^{4} \mathrm{f}_{\mathrm{LS}}($ Exhibit 15-7) $4.2 \mathrm{mi} / \mathrm{h}$ <br> Adj. for access points ${ }^{4}, \mathrm{f}_{\mathrm{A}}$ (Exhibit 15-8) $0.5 \mathrm{mi} / \mathrm{h}$ <br> Free-flow speed, FFS (FSS=BFFS-f $\left.\mathrm{LS}^{-\mathrm{f}_{\mathrm{A}}}\right)$ $50.3 \mathrm{mi} / \mathrm{h}$ <br> Average travel speed, ATS $=\mathrm{FFS}-0.00776\left(\mathrm{v}_{\mathrm{d}, \mathrm{ATS}}{ }^{+}\right.$ $41.6 \mathrm{mi} / \mathrm{h}$ <br> $\left.\mathrm{v}_{\mathrm{o}, \mathrm{ATS}}\right)-\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ <br> Percent free flow speed, PFFS $82.7 \%$ |
| Percent Time-Spent-Following |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Passenger-car equivalents for RV s, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 1.000 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 515 474 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{d}(\%)=100\left(1-e^{\text {av }}{ }_{\text {d }}{ }^{\text {b }}\right.$ ) | 51.8 |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \mathrm{PTSF}}$ (Exhibit 15-21) | 22.9 |
| $\qquad$ | 63.7 |
| Level of Service and Other Performance Measures |  |
| Level of service, LOS (Exhibit 15-3) | D |
| Volume to capacity ratio, v/c | 0.31 |



| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |
| :---: | :---: |
| General Information | Site Information |
| Analyst $J F$ <br> Agency or Company $10 / 8 / 18$ <br> Date Performed $P M$ <br> Analysis Time Period  | Highway / Direction of Travel SR 113 <br> From/To north of Hay Rd SB <br> Jurisdiction Caltrans <br> Analysis Year Cumulative plus Project |
| Project Description: Recology Hay Rd Landfill |  |
| Input Data |  |
|  |  |
| Average Travel Speed |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.2 1.2 |
| Passenger-car equivalents for RV s, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 0.986 0.986 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \text { ATS }}$ (Exhibit 15-9) | 1.00 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 481523 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |
| Mean speed of sample ${ }^{3}$, $\mathrm{S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(\mathrm{v} / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ (Exhibit 15-15) <br> $0.8 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}, \mathrm{BFFS}$ $55.0 \mathrm{mi} / \mathrm{h}$ <br> Adj. for lane and shoulder width, ${ }^{4} \mathrm{f}_{\mathrm{LS}}($ (Exhibit 15-7) $4.2 \mathrm{mi} / \mathrm{h}$ <br> Adj. for access points ${ }^{4}, \mathrm{f}_{\mathrm{A}}$ (Exhibit 15-8) $0.5 \mathrm{mi} / \mathrm{h}$ <br> Free-flow speed, FFS (FSS=BFFS-f $\left.\mathrm{fsS}^{-\mathrm{f}_{\mathrm{A}}}\right)$ $50.3 \mathrm{mi} / \mathrm{h}$ <br> Average travel speed, ATS $\mathrm{d}_{\mathrm{d}}=\mathrm{FFS}-0.00776\left(\mathrm{v}_{\mathrm{d}, \mathrm{ATS}}{ }^{+}\right.$ $41.7 \mathrm{mi} / \mathrm{h}$ <br> $\left.\mathrm{v}_{\mathrm{o}, \mathrm{ATS}}\right)-\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ <br> Percent free flow speed, PFFS $82.9 \%$ |
| Percent Time-Spent-Following |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Passenger-car equivalents for RV s, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 1.000 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 474 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{d}(\%)=100\left(1-e^{\text {av }}{ }_{\text {d }}{ }^{\text {b }}\right.$ ) | 49.7 |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \text { PTSF }}$ (Exhibit 15-21) | 22.9 |
| Percent time-spent-following, PTSF $_{d}(\%)=$ BPTSF $_{d}+{ }_{n p, \mathrm{PTSF}}{ }^{*}\left(v_{d, \mathrm{PTSF}} / v_{d, \mathrm{PTSF}}+\right.$ $\mathrm{v}_{\mathrm{o}, \mathrm{PTSF}}$ ) | 60.7 |
| Level of Service and Other Performance Measures |  |
| Level of service, LOS (Exhibit 15-3) | D |
| Volume to capacity ratio, v/c | 0.28 |



| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |
| :---: | :---: |
| General Information | Site Information |
| Analyst JF <br> Agency or Company $10 / 8 / 18$ <br> Date Performed AM <br> Analysis Time Period  | Highway / Direction of Travel SR 113 <br> From/To south of Hay Rd NB <br> Jurisdiction Caltrans <br> Analysis Year Cumulative plus Project |
| Project Description: Recology Hay Rd Landfill |  |
| Input Data |  |
|  |  |
| Average Travel Speed |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.2 1.4 |
| Passenger-car equivalents for $\mathrm{RVs}, \mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 0.986 0.973 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \text { ATS }}$ (Exhibit 15-9) | 1.00 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 498 287 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |
| Mean speed of sample ${ }^{3}$, $\mathrm{S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776(\mathrm{v/f} \mathrm{fV}, \mathrm{ATS})$ <br> Adj. for no-passing zones, $\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ (Exhibit 15-15) <br> $1.2 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}, \mathrm{BFFS}$ $55.0 \mathrm{mi} / \mathrm{h}$ <br> Adj. for lane and shoulder width, ${ }^{4} \mathrm{f}_{\mathrm{LS}}($ (Exhibit 15-7) $4.2 \mathrm{mi} / \mathrm{h}$ <br> Adj. for access points ${ }^{4}, \mathrm{f}_{\mathrm{A}}$ (Exhibit $\left.15-8\right)$ $0.5 \mathrm{mi} / \mathrm{h}$ <br> Free-flow speed, FFS $\left(\mathrm{FSS}=\mathrm{BFFS}-\mathrm{f}_{\mathrm{LS}^{-}} \mathrm{f}_{\mathrm{A}}\right)$ $50.3 \mathrm{mi} / \mathrm{h}$ <br> Average travel speed, ATS $\mathrm{d}_{\mathrm{d}}=\mathrm{FFS}-0.00776\left(\mathrm{v}_{\mathrm{d}, \mathrm{ATS}}{ }^{+}\right.$ $43.0 \mathrm{mi} / \mathrm{h}$ <br> $\left.\mathrm{v}_{\mathrm{o}, \mathrm{ATS}}\right)-\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ $85.6 \%$ <br> Percent free flow speed, PFFS   |
| Percent Time-Spent-Following |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.0 1.1 |
| Passenger-car equivalents for RV s, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 1.000 0.993 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{\star} \mathrm{f}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 491 281 |
| Base percent time-spent-following ${ }^{4}$, PPTSF $_{\text {d }}(\%)=100\left(1-\mathrm{e}^{\text {av }}{ }_{\text {d }}{ }^{\text {b }}\right.$ ) | 46.4 |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \mathrm{PTSF}}$ (Exhibit 15-21) | 26.1 |
| $\begin{aligned} & \text { Percent time-spent-following, } \text { PTSF }_{d}(\%)=\text { BPTSF }_{d}+f_{n p, P T S F}{ }^{*}\left(v_{d, \text { PTSF }} / v_{d, \text { PTSF }}+\right. \\ & \left.v_{o, P T S F}\right) \end{aligned}$ | 63.0 |
| Level of Service and Other Performance Measures |  |
| Level of service, LOS (Exhibit 15-3) | D |
| Volume to capacity ratio, v/c | 0.29 |



| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |
| :---: | :---: |
| General Information | Site Information |
| Analyst $J F$ <br> Agency or Company  <br> Date Performed $10 / 8 / 18$ <br> Analysis Time Period $A M$ | Highway / Direction of Travel SR 113 <br> From/To south of Hay Rd SB <br> Jurisdiction Caltrans <br> Analysis Year Cumulative plus Project |
| Project Description: Recology Hay Rd Landfill |  |
| Input Data |  |
|  |  |
| Average Travel Speed |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.4 1.2 |
| Passenger-car equivalents for RVs , $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 0.973 0.986 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \text { ATS }}$ (Exhibit 15-9) | 1.00 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 287 年 498 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |
| Mean speed of sample ${ }^{3}$, $\mathrm{S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(\mathrm{~V} / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ (Exhibit 15-15) <br> $0.9 \mathrm{mi} / \mathrm{h}$ |  |
| Percent Time-Spent-Following |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.1 1.0 |
| Passenger-car equivalents for RVs , $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 0.993 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{\star} \mathrm{f}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 281 |
| Base percent time-spent-following ${ }^{4}$, PPTSF $_{\text {d }}(\%)=100\left(1-\mathrm{e}^{\text {av }}{ }_{\mathrm{d}}{ }^{\text {b }}\right.$ ) | 34.9 |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \mathrm{PTSF}}$ (Exhibit 15-21) | 26.1 |
| $\qquad$ | 44.4 |
| Level of Service and Other Performance Measures |  |
| Level of service, LOS (Exhibit 15-3) | D |
| Volume to capacity ratio, v/c | 0.17 |



| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |
| :---: | :---: |
| General Information | Site Information |
| Analyst $J F$ <br> Agency or Company $10 / 8 / 18$ <br> Date Performed $P M$ <br> Analysis Time Period  | Highway / Direction of Travel SR 113 <br> From/To south of Hay Rd NB <br> Jurisdiction Caltrans <br> Analysis Year Cumulative plus Project |
| Project Description: Recology Hay Rd Landfill |  |
| Input Data |  |
|  |  |
| Average Travel Speed |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.3 1.2 |
| Passenger-car equivalents for RV s, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 0.979 0.986 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \text { ATS }}$ (Exhibit 15-9) | 1.00 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 450528 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |
| Mean speed of sample ${ }^{3}$, $\mathrm{S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(\mathrm{v} / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ (Exhibit 15-15) <br> $0.8 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}, \mathrm{BFFS}$ $55.0 \mathrm{mi} / \mathrm{h}$ <br> Adj. for lane and shoulder width, ${ }^{4} \mathrm{f}_{\mathrm{LS}}($ Exhibit 15-7) $4.2 \mathrm{mi} / \mathrm{h}$ <br> Adj. for access points ${ }^{4}, \mathrm{f}_{\mathrm{A}}$ (Exhibit 15-8) $0.5 \mathrm{mi} / \mathrm{h}$ <br> Free-flow speed, FFS (FSS=BFFS-f $\left.\mathrm{LS}^{-\mathrm{f}_{\mathrm{A}}}\right)$ $50.3 \mathrm{mi} / \mathrm{h}$ <br> Average travel speed, ATS $=\mathrm{FFS}-0.00776\left(\mathrm{v}_{\mathrm{d}, \mathrm{ATS}}{ }^{+}\right.$ $41.9 \mathrm{mi} / \mathrm{h}$ <br> $\left.\mathrm{v}_{\mathrm{o}, \mathrm{ATS}}\right)-\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ <br> Percent free flow speed, PFFS $83.3 \%$ |
| Percent Time-Spent-Following |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Passenger-car equivalents for RV s, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 1.000 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 440 521 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{d}(\%)=100\left(1-e^{\text {av }}{ }_{\text {d }}{ }^{\text {b }}\right.$ ) | 48.2 |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \mathrm{PTSF}}$ (Exhibit 15-21) | 26.9 |
| $\qquad$ | 60.5 |
| Level of Service and Other Performance Measures |  |
| Level of service, LOS (Exhibit 15-3) | D |
| Volume to capacity ratio, v/c | 0.26 |



| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |
| :---: | :---: |
| General Information | Site Information |
| Analyst $J F$ <br> Agency or Company $10 / 8 / 18$ <br> Date Performed $P M$ <br> Analysis Time Period  | Highway / Direction of Travel SR 113 <br> From/To south of Hay Rd SB <br> Jurisdiction Caltrans <br> Analysis Year Cumulative plus Project |
| Project Description: Recology Hay Rd Landfill |  |
| Input Data |  |
|  |  |
| Average Travel Speed |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.2 1.3 |
| Passenger-car equivalents for RV s, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 0.986 0.979 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \text { ATS }}$ (Exhibit 15-9) | 1.00 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 528 450 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |
| Mean speed of sample ${ }^{3}$, $\mathrm{S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(\mathrm{v} / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ (Exhibit 15-15) <br> $1.0 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}, \mathrm{BFFS}$ $55.0 \mathrm{mi} / \mathrm{h}$ <br> Adj. for lane and shoulder width, ${ }^{4} \mathrm{f}_{\mathrm{LS}}($ (Exhibit 15-7) $4.2 \mathrm{mi} / \mathrm{h}$ <br> Adj. for access points ${ }^{4}, \mathrm{f}_{\mathrm{A}}$ (Exhibit 15-8) $0.5 \mathrm{mi} / \mathrm{h}$ <br> Free-flow speed, FFS (FSS=BFFS-f $\left.\mathrm{fsS}^{-\mathrm{f}_{\mathrm{A}}}\right)$ $50.3 \mathrm{mi} / \mathrm{h}$ <br> Average travel speed, ATS $\mathrm{d}_{\mathrm{d}}=\mathrm{FFS}-0.00776\left(\mathrm{v}_{\mathrm{d}, \mathrm{ATS}}{ }^{+}\right.$ $41.7 \mathrm{mi} / \mathrm{h}$ <br> $\left.\mathrm{v}_{\mathrm{o}, \mathrm{ATS}}\right)-\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ <br> Percent free flow speed, PFFS $82.9 \%$ |
| Percent Time-Spent-Following |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Passenger-car equivalents for RV s, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 1.000 1.000 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 521 440 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{d}(\%)=100\left(1-e^{\text {av }}{ }_{\text {d }}{ }^{\text {b }}\right.$ ) | 51.4 |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \text { PTSF }}$ (Exhibit 15-21) | 26.9 |
| Percent time-spent-following, PTSF $_{d}(\%)=$ BPTSF $_{d}+{ }_{n p, \mathrm{PTSF}}{ }^{*}\left(v_{d, \mathrm{PTSF}} / v_{d, \mathrm{PTSF}}+\right.$ $\mathrm{v}_{\mathrm{o}, \mathrm{PTSF}}$ ) | 66.0 |
| Level of Service and Other Performance Measures |  |
| Level of service, LOS (Exhibit 15-3) | D |
| Volume to capacity ratio, v/c | 0.31 |



| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |
| :---: | :---: |
| General Information | Site Information |
| Analyst $J F$ <br> Agency or Company $10 / 8 / 18$ <br> Date Performed AM <br> Analysis Time Period  | Highway / Direction of Travel Hay Rd <br> From/To west of SR 113 EB <br> Jurisdiction Solano County <br> Analysis Year Cumulative plus Project |
| Project Description: Recology Hay Rd Landfill |  |
| Input Data |  |
|  |  |
| Average Travel Speed |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.9 1.9 |
| Passenger-car equivalents for RV s, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 0.941 0.941 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \text { ATS }}$ (Exhibit 15-9) | 1.00 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 69 117 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |
| Mean speed of sample ${ }^{3}$, $\mathrm{S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(\mathrm{v} / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ (Exhibit 15-15) <br> $0.4 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}, \mathrm{BFFS}$ $55.0 \mathrm{mi} / \mathrm{h}$ <br> Adj. for lane and shoulder width, ${ }^{4} \mathrm{f}_{\mathrm{LS}}($ Exhibit 15-7) $4.2 \mathrm{mi} / \mathrm{h}$ <br> Adj. for access points ${ }^{4}, \mathrm{f}_{\mathrm{A}}$ (Exhibit 15-8) $0.3 \mathrm{mi} / \mathrm{h}$ <br> Free-flow speed, FFS (FSS=BFFS-f $\left.\mathrm{LS}^{-\mathrm{f}_{\mathrm{A}}}\right)$ $50.5 \mathrm{mi} / \mathrm{h}$ <br> Average travel speed, ATS $=\mathrm{FFS}-0.00776\left(\mathrm{v}_{\mathrm{d}, \mathrm{ATS}}{ }^{+}\right.$ $48.7 \mathrm{mi} / \mathrm{h}$ <br> $\left.\mathrm{v}_{\mathrm{o}, \mathrm{ATS}}\right)-\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ <br> Percent free flow speed, PFFS $96.3 \%$ |
| Percent Time-Spent-Following |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.1 |
| Passenger-car equivalents for RV s, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 0.993 0.993 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 66 111 |
| Base percent time-spent-following ${ }^{4}$, PPTSF $_{\text {d }}(\%)=100\left(1-\mathrm{e}^{\text {av }}{ }_{\mathrm{d}}{ }^{\text {b }}\right.$ ) | 7.9 |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \text { PTSF }}$ (Exhibit 15-21) | 29.9 |
| Percent time-spent-following, PTSF $_{d}(\%)=$ BPTSF $_{d}+f_{n p, \text { PTSF }}{ }^{*}\left(v_{d, \text { PTSF }} / v_{d, \text { PTSF }}+\right.$ $\mathrm{V}_{\mathrm{o}, \mathrm{PTSF}}$ ) | 19.0 |
| Level of Service and Other Performance Measures |  |
| Level of service, LOS (Exhibit 15-3) | C |
| Volume to capacity ratio, v/c | 0.04 |



| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |
| :---: | :---: |
| General Information | Site Information |
| Analyst $J F$ <br> Agency or Company  <br> Date Performed $10 / 8 / 18$ <br> Analysis Time Period $A M$ | Highway / Direction of Travel Hay Rd <br> From/To west of SR 113 WB <br> Jurisdiction Solano County <br> Analysis Year Cumulative plus Project |
| Project Description: Recology Hay Rd Landfill |  |
| Input Data |  |
|  |  |
| Average Travel Speed |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.9 1.9 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 0.941 0.941 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \text { ATS }}($ Exhibit 15-9) | 1.00 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 117 年 69 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |
| Mean speed of sample ${ }^{3}$, $\mathrm{S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(\mathrm{~V} / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ (Exhibit 15-15) <br> $0.2 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}, \mathrm{BFFS}$ $55.0 \mathrm{mi} / \mathrm{h}$ <br> Adj. for lane and shoulder width, ${ }^{4} \mathrm{f}_{\mathrm{LS}}($ Exhibit 15-7) $4.2 \mathrm{mi} / \mathrm{h}$ <br> Adj. for access points ${ }^{4}, \mathrm{f}_{\mathrm{A}}$ (Exhibit 15-8) $0.3 \mathrm{mi} / \mathrm{h}$ <br> Free-flow speed, FFS (FSS=BFFS-f $\left.\mathrm{LS}^{-\mathrm{f}_{\mathrm{A}}}\right)$ $50.5 \mathrm{mi} / \mathrm{h}$ <br> Average travel speed, ATS $=\mathrm{FFS}-0.00776\left(\mathrm{v}_{\mathrm{d}, \mathrm{ATS}}{ }^{+}\right.$ $48.9 \mathrm{mi} / \mathrm{h}$ <br> $\left.\mathrm{v}_{\mathrm{o}, \mathrm{ATS}}\right)-\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ <br> Percent free flow speed, PFFS $96.7 \%$ |
| Percent Time-Spent-Following |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.1 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 0.993 0.993 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 111 年 66 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{\text {d }}(\%)=100\left(1-\mathrm{e}^{\text {av }}{ }_{\mathrm{d}}{ }^{\text {b }}\right.$ ) | 12.8 |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \mathrm{PTSF}}$ (Exhibit 15-21) | 29.9 |
| $\begin{aligned} & \text { Percent time-spent-following, } \text { PTSF }_{d}(\%)=\text { BPTSF }_{d}+f_{n p, P T S F}{ }^{*}\left(v_{d, \text { PTSF }} / v_{d, \text { PTSF }}+\right. \\ & \left.v_{o, P T S F}\right) \end{aligned}$ | 31.6 |
| Level of Service and Other Performance Measures |  |
| Level of service, LOS (Exhibit 15-3) | C |
| Volume to capacity ratio, v/c | 0.07 |



| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |
| :---: | :---: |
| General Information | Site Information |
| Analyst $J F$ <br> Agency or Company $10 / 8 / 18$ <br> Date Performed $P M$ <br> Analysis Time Period  | Highway / Direction of Travel Hay Rd <br> From/To west of SR 113 EB <br> Jurisdiction Solano County <br> Analysis Year Cumulative plus Project |
| Project Description: Recology Hay Rd Landfill |  |
| Input Data |  |
|  |  |
| Average Travel Speed |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.7 1.9 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 0.953 0.941 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \text { ATS }}($ Exhibit 15-9) | 1.00 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 157 ( 30 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |
| Mean speed of sample ${ }^{3}$, $\mathrm{S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(\mathrm{~V} / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ (Exhibit 15-15) <br> $0.2 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}, \mathrm{BFFS}$ $55.0 \mathrm{mi} / \mathrm{h}$ <br> Adj. for lane and shoulder width, ${ }^{4} \mathrm{f}_{\mathrm{LS}}($ Exhibit 15-7) $4.2 \mathrm{mi} / \mathrm{h}$ <br> Adj. for access points ${ }^{4}, \mathrm{f}_{\mathrm{A}}$ (Exhibit 15-8) $0.3 \mathrm{mi} / \mathrm{h}$ <br> Free-flow speed, FFS $\left(\mathrm{FSS}=\mathrm{BFFS}-\mathrm{f}_{\mathrm{LS}} \mathrm{f}_{\mathrm{A}}\right)$ $50.5 \mathrm{mi} / \mathrm{h}$ <br> Average travel speed, ATS $\mathrm{d}_{\mathrm{d}}=\mathrm{FFS}-0.00776\left(\mathrm{v}_{\mathrm{d}, \mathrm{ATS}}{ }^{+}\right.$ $48.9 \mathrm{mi} / \mathrm{h}$ <br> $\left.\mathrm{v}_{\mathrm{o}, \mathrm{ATS}}\right)-\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ $96.7 \%$ <br> Percent free flow speed, PFFS  |
| Percent Time-Spent-Following |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.1 |
| Passenger-car equivalents for RVs, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 0.993 0.993 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 151 28 |
| Base percent time-spent-following ${ }^{4}$, BPTSF $_{\text {d }}(\%)=100\left(1-\mathrm{e}^{\text {av }}{ }_{\mathrm{d}}{ }^{\text {b }}\right.$ ) | 16.9 |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \mathrm{PTSF}}$ (Exhibit 15-21) | 25.9 |
| $\qquad$ | 38.7 |
| Level of Service and Other Performance Measures |  |
| Level of service, LOS (Exhibit 15-3) | C |
| Volume to capacity ratio, v/c | 0.09 |



| DIRECTIONAL TWO-LANE HIGHWAY SEGMENT WORKSHEET |  |
| :---: | :---: |
| General Information | Site Information |
| Analyst $J F$ <br> Agency or Company $10 / 8 / 18$ <br> Date Performed $P M$ <br> Analysis Time Period  | Highway / Direction of Travel Hay Rd <br> From/To west of SR 113 WB <br> Jurisdiction Solano County <br> Analysis Year Cumulative plus Project |
| Project Description: Recology Hay Rd Landfill |  |
| Input Data |  |
|  |  |
| Average Travel Speed |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-11 or 15-12) | 1.9 1.7 |
| Passenger-car equivalents for RV s, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-11 or 15-13) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}=1 /\left(1+\mathrm{P}_{T}\left(\mathrm{E}_{T}-1\right)+\mathrm{P}_{R}\left(\mathrm{E}_{R}-1\right)\right)$ | 0.941 0.953 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \text { ATS }}$ (Exhibit 15-9) | 1.00 1.00 |
| Demand flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=V_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{g}, \mathrm{ATS}}{ }^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ | 30 157 |
| Free-Flow Speed from Field Measurement | Estimated Free-Flow Speed |
| Mean speed of sample ${ }^{3}$, $\mathrm{S}_{F M}$ <br> Total demand flow rate, both directions, $v$ <br> Free-flow speed, $\mathrm{FFS}=\mathrm{S}_{\mathrm{FM}}+0.00776\left(\mathrm{v} / \mathrm{f}_{\mathrm{HV}, \mathrm{ATS}}\right)$ <br> Adj. for no-passing zones, $\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ (Exhibit 15-15) <br> $0.8 \mathrm{mi} / \mathrm{h}$ | Base free-flow speed ${ }^{4}, \mathrm{BFFS}$ $55.0 \mathrm{mi} / \mathrm{h}$ <br> Adj. for lane and shoulder width, ${ }^{4} \mathrm{f}_{\mathrm{LS}}($ Exhibit 15-7) $4.2 \mathrm{mi} / \mathrm{h}$ <br> Adj. for access points ${ }^{4}, \mathrm{f}_{\mathrm{A}}$ (Exhibit 15-8) $0.3 \mathrm{mi} / \mathrm{h}$ <br> Free-flow speed, FFS (FSS=BFFS-f $\left.\mathrm{LS}^{-\mathrm{f}_{\mathrm{A}}}\right)$ $50.5 \mathrm{mi} / \mathrm{h}$ <br> Average travel speed, ATS $=\mathrm{FFS}-0.00776\left(\mathrm{v}_{\mathrm{d}, \mathrm{ATS}}{ }^{+}\right.$ $48.3 \mathrm{mi} / \mathrm{h}$ <br> $\left.\mathrm{v}_{\mathrm{o}, \mathrm{ATS}}\right)-\mathrm{f}_{\mathrm{np}, \mathrm{ATS}}$ <br> Percent free flow speed, PFFS $95.5 \%$ |
| Percent Time-Spent-Following |  |
|  | Analysis Direction (d) $\quad$ Opposing Direction (o) |
| Passenger-car equivalents for trucks, $\mathrm{E}_{\mathrm{T}}$ (Exhibit 15-18 or 15-19) | 1.1 |
| Passenger-car equivalents for RV s, $\mathrm{E}_{\mathrm{R}}$ (Exhibit 15-18 or 15-19) | 1.0 1.0 |
| Heavy-vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=1 /\left(1+\mathrm{P}_{\mathrm{T}}\left(\mathrm{E}_{\mathrm{T}}-1\right)+\mathrm{P}_{\mathrm{R}}\left(\mathrm{E}_{\mathrm{R}}-1\right)\right)$ | 0.993 0.993 |
| Grade adjustment factor ${ }^{1}$, $\mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}$ (Exhibit 15-16 or Ex 15-17) | 1.00 1.00 |
| Directional flow rate ${ }^{2}, v_{i}(\mathrm{pc} / \mathrm{h}) v_{\mathrm{i}}=\mathrm{V}_{\mathrm{i}} /\left(\mathrm{PHF}^{*} \mathrm{f}_{\mathrm{HV}, \mathrm{PTSF}}{ }^{*} \mathrm{f}_{\mathrm{g}, \mathrm{PTSF}}\right)$ | 28 \| 151 |
| Base percent time-spent-following ${ }^{4}$, PPTSF $_{\text {d }}(\%)=100\left(1-\mathrm{e}^{\text {av }}{ }_{\mathrm{d}}{ }^{\text {b }}\right.$ ) | 3.5 |
| Adj. for no-passing zone, $\mathrm{f}_{\mathrm{np}, \text { PTSF }}$ (Exhibit 15-21) | 25.9 |
| $\begin{aligned} & \text { Percent time-spent-following, } \text { PTSF }_{d}(\%)=\text { BPTSF }_{d}+f_{n p, P T S F}{ }^{*}\left(v_{d, \text { PTSF }} / v_{d, \text { PTSF }}+\right. \\ & \left.v_{o, \text { PTSF }}\right) \end{aligned}$ | 7.6 |
| Level of Service and Other Performance Measures |  |
| Level of service, LOS (Exhibit 15-3) | C |
| Volume to capacity ratio, v/c | 0.02 |






| Percent time-spent-following including passing lane ${ }^{3}$, PTSF $_{\text {pl }}(\%)$ $\operatorname{PTSF}_{\mathrm{pl}}=\mathrm{PTSF}_{\mathrm{d}}\left[\mathrm{~L}_{\mathrm{u}}+\mathrm{L}_{\mathrm{d}}+\mathrm{f}_{\mathrm{pl}, P T S F} \mathrm{~L}_{\mathrm{pl}}+\left(\left(1+\mathrm{f}_{p l, P T S F}\right) / 2\right) \mathrm{L}_{\mathrm{de}} / \mathrm{L}_{\mathrm{t}}\right.$ | 43.0 |
| :---: | :---: |
| Level of Service and Other Performance Measures ${ }^{4}$ |  |
| Level of service including passing lane LOS ${ }_{\text {pl }}$ (Exhibit 15-3) | C |
| Peak 15-min total travel time, $\mathrm{TT}_{15}\left(\right.$ veh-h) $\quad \mathrm{TT}_{15}=\mathrm{VMT}_{15} / \mathrm{ATS}_{\mathrm{pl}}$ | 4.9 |
| Bicycle Level of Service |  |
| Directional demand flow rate in outside lane, $v_{\text {OL }}$ (Eq. 15-24) veh/h | 440.2 |
| Effective width, $\mathrm{W}_{v}$ (Eq. 15-29) ft | 15.00 |
| Effective speed factor, $\mathrm{S}_{t}$ (Eq. 15-30) | 4.79 |
| Bicycle level of service score, BLOS (Eq. 15-31) | 5.66 |
| Bicycle level of service (Exhibit 15-4) | $F$ |
| Notes |  |
| 1. If $\operatorname{LOS}_{d}=F$, passing lane analysis cannot be performed. <br> 2. If $\mathrm{L}_{\mathrm{d}}<0$, use alternative Equation 15-18. <br> 3. If $\mathrm{L}_{\mathrm{d}}<0$, use alternative Equation 15-16. <br> 4. v/c, $\mathrm{VMT}_{15}$ and $\mathrm{VMT}_{60}$ are calculated on Directional Two-Lane |  |



| Percent time-spent-following including passing lane ${ }^{3}, \operatorname{PTSF}_{\mathrm{pl}}(\%)$ $\operatorname{PTSF}_{\mathrm{pl}}=\operatorname{PTSF}_{\mathrm{d}}\left[\mathrm{~L}_{\mathrm{u}}+\mathrm{L}_{\mathrm{d}}+\mathrm{f}_{\mathrm{pl}, P T S F} \mathrm{~L}_{\mathrm{pl}}+\left(\left(1+\mathrm{f}_{p l, P T S F}\right) / 2\right) \mathrm{L}_{\mathrm{de}}\right] / \mathrm{L}_{\mathrm{t}}$ | 53.2 |
| :---: | :---: |
| Level of Service and Other Performance Measures ${ }^{4}$ |  |
| Level of service including passing lane LOS ${ }_{\text {pl }}$ (Exhibit 15-3) | C |
| Peak 15-min total travel time, $\mathrm{TT}_{15}(\mathrm{veh}-\mathrm{h}) \quad \mathrm{TT}_{15}=\mathrm{VMT}_{15} / \mathrm{ATS}_{\mathrm{pl}}$ | 7.0 |
| Bicycle Level of Service |  |
| Directional demand flow rate in outside lane, $v_{\text {OL }}$ (Eq. 15-24) veh/h | 630.4 |
| Effective width, $\mathrm{W}_{v}$ (Eq. 15-29) ft | 15.00 |
| Effective speed factor, $\mathrm{S}_{t}$ (Eq. 15-30) | 4.79 |
| Bicycle level of service score, BLOS (Eq. 15-31) | 5.84 |
| Bicycle level of service (Exhibit 15-4) | F |
| Notes |  |
| 1. If $\operatorname{LOS}_{d}=F$, passing lane analysis cannot be performed. <br> 2. If $\mathrm{L}_{\mathrm{d}}<0$, use alternative Equation 15-18. <br> 3. If $L_{d}<0$, use alternative Equation 15-16. <br> 4. $\mathrm{v} / \mathrm{c}, \mathrm{VMT}_{15}$ and $\mathrm{VMT}_{60}$ are calculated on Directional Two-Lane H |  |



| Percent time-spent-following including passing lane ${ }^{3}, \operatorname{PTSF}_{\mathrm{pl}}(\%)$ $\operatorname{PTSF}_{\mathrm{pl}}=\operatorname{PTSF}_{\mathrm{d}}\left[\mathrm{~L}_{\mathrm{u}}+\mathrm{L}_{\mathrm{d}}+\mathrm{f}_{\mathrm{pl}, P T S F} \mathrm{~L}_{\mathrm{pl}}+\left(\left(1+\mathrm{f}_{p l, P T S F}\right) / 2\right) \mathrm{L}_{\mathrm{de}}\right] / \mathrm{L}_{\mathrm{t}}$ | 43.7 |
| :---: | :---: |
| Level of Service and Other Performance Measures ${ }^{4}$ |  |
| Level of service including passing lane LOS ${ }_{\text {pl }}$ (Exhibit 15-3) | C |
| Peak 15-min total travel time, $\mathrm{TT}_{15}(\mathrm{veh}-\mathrm{h}) \quad \mathrm{TT}_{15}=\mathrm{VMT}_{15} / \mathrm{ATS}_{\mathrm{pl}}$ | 5.0 |
| Bicycle Level of Service |  |
| Directional demand flow rate in outside lane, $v_{\text {OL }}$ (Eq. 15-24) veh/h | 453.3 |
| Effective width, $\mathrm{W}_{v}$ (Eq. 15-29) ft | 15.00 |
| Effective speed factor, $\mathrm{S}_{t}$ (Eq. 15-30) | 4.79 |
| Bicycle level of service score, BLOS (Eq. 15-31) | 5.67 |
| Bicycle level of service (Exhibit 15-4) | F |
| Notes |  |
| 1. If $\operatorname{LOS}_{d}=F$, passing lane analysis cannot be performed. <br> 2. If $\mathrm{L}_{\mathrm{d}}<0$, use alternative Equation 15-18. <br> 3. If $L_{d}<0$, use alternative Equation 15-16. <br> 4. $\mathrm{v} / \mathrm{c}, \mathrm{VMT}_{15}$ and $\mathrm{VMT}_{60}$ are calculated on Directional Two-Lane H |  |

Figure 4C-3. Warrant 3, Peak Hour


Note: 150 vph applies as the lower threshold volume for a minor-street approach with two or more lanes and 100 vph applies as the lower threshoid volume for a minor-street approach with one lane.

Figure 4C-4. Warrant 3, Peak Hour (70\% Factor) (COMMUNITY LESS THAN 10,000 POPULATION OR ABOVE 40 RAPH ON MA.JOR STREET) ODAY/I. 80 WB RAMP ${ }^{\circ}$

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        - AM
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- DAY/midmay
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$\times \quad P M$

MIDWAY/I-80 EB RAMP
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$\times{ }^{\circ} \mathrm{Am}$

Chapter 4C - Traffic Control Signal Needs Studies Part 4 - Highway Traffic Signals

Figure 4C-3. Warrant 3, Peak Hour

-Note: 150 yph applies as the lower threshold volume for a minor-street approach with two or more, lanes and 100 yph applies as the lower limeshold volume for a minor-street approach with one lane.

Figure 4C-4. Warrant 3, Peak Hour (70\% Factor) (COMMUNITY LESS THAN 10,000 POPULATION OR ABOVE 40 MPH ON MAJOR STREET)


- DAM/mIDMAY $0 A M$
$\times \quad P M$

MIDWAY/I-80 EG RAMP $\therefore A_{\rho M}$

PORTER /m DWA,
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MAJOR STREET -TOTAL OF BOTH APPROACHES-
VEHICLES PER HOUR (VPH)
'Note: 100 yph applies ass the lower threshold volume for a minor-streat approach with two or more lanes and 75 vph applies as the lower threshold volume for a minor-street approach with one lane.
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November 7, 2014

Figure $4 \mathrm{C}-3$. Warrant 3 , Peak Hour

-Note: 150 yph applies as the lower threshold volume for a minor-street approach with two or more lanes and 100 vph applies as the lower threshold volume for a minor-street approach with one lane.

Figure 4C-4. Warrant 3, Peak Hour (70\% Factor) (COMMUNITY LESS THAN 10,000 POPULATION OR ABOVE 40 MPH ON MAJOR STREET)


- DAY/indDwAy
$O A M$
$\times \quad P M$

MIDWAY/I-80 EG RAMP

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MAJOR STREET - TOTAL OF BOTH APPROACHESVEHICLES PER HOUR (VPH)
'Note: 100 yph applies as the lower threshold volume for a minor-street approach with two or more lanes and 75 yph applies as the lower threshold volume for a minor-street approach with one lane.

52113/.0000 andy

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SAT


Figure 4C-3. Warrani 3, Peak Hour

-Note: 150 vph applies as the lower threshold volume for a minor-street approach with two or more lanes and 100 vph applies as the fower threshold volume for a minor-street approach with one lane.

Figure 4C-4. Warrant 3, Peak Hour (70\% Factor) (COMMUNITY LESS THAN 10,000 POPULATION OR ABOVE 40 HPH ON MAAJOR STREET)


- DAM/AIDWAy
$O A M$
$\times \quad P M$

MIDWAY/I-8O EB RAMP
$\therefore \quad A M$
PORTER/MIDNA1
O AM
$\times \mathrm{Am}$

Chapter 4 C - Traffic Control Signal Needs Studies Part 4-Highway Traffic Signals

